



**ENGINEERING REVIEW COMMENTS IN
BLUE BOXES WITH BLUE TEXT**

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**Eastonville Road – Londonderry Drive to Rex Road
Segment 1 Improvements
Stationing 14+55.00 – 47+00.00**

Final Drainage Report

March 2024

HR Green Project No: 201662.08

Prepared For:

D.R. Horton

Contact: Riley Hillen, P.E.

9555 S. Kingston Ct.

Englewood, CO 80112

Prepared By:

HR Green Development, LLC

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Add text:

EDARP File No.:
CDR2321

Engineer's Statement:

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the County for drainage reports and said report is in conformity with the applicable master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.



Colleen Monahan, P.E., LEED AP

State of Colorado No. 56067

For and on behalf of HR Green Development, LLC

Date



Owner/Developer's Statement:

I, the developer, have read and will comply with all of the requirements specified in this drainage report and plan.

By: _____

Authorized Signature

Date

Address: D.R. Horton
9555 S. Kingston Court
Englewood, CO

El Paso County Statement

Filed in accordance with the requirements of the Drainage Criteria Manual, Volumes 1 and 2, El Paso County Engineering Criteria Manual and Land Development code, as amended.

Joshua Palmer, P.E.

Date

County Engineer/ECM Administrator

Conditions:

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Reference material missing from appendix. Please include back in.

I. General Purpose, Location and Description

a. Purpose

The purpose of this Final Drainage Report (FDR) for the Eastonville Road from Londonderry Drive to Rex Road Segment 1 Improvements is to describe the onsite and offsite drainage patterns, size drainage infrastructure to safely capture and convey developed runoff to water quality and detention facilities, and to safely route detained stormwater to adequate outfalls. This drainage report will detail the improvements of Eastonville Road from Londonderry Drive to Grandview Filing No. 1 (Stations 14+55.00 to 47+00.00). Stations 47+00.00 to 79+32.00 contain the Segment 2 Improvements for the Eastonville Road from Londonderry Drive to Rex Road for the portion of the project north of Grandview Filing No. 1. The project is all one project, however, the planset has been broken into two segments to align with the Grandview Reserve Filings. A separate FDR describes Segment 2 of the project.

b. Location

Eastonville Road from Londonderry Drive to Grandview Filing No. 1, referred to as 'the site' herein, is an existing 26' wide temporary pavement (per field inspection- the existing pavement is not full depth, see Appendix A) road in El Paso County, Colorado. The site lies in existing 60' wide El Paso County Right-of-Way within Sections 21 and 28, Township 12 South, Range 64 West of the 6th Principal Meridian, in El Paso County, State of Colorado.

The site is bound by undeveloped land to the east and west that has historically been used as ranching lands. Falcon Regional Park, which contains ballparks and parking, and Falcon High School also border the site to the west. All lands to the east and west of the site are unplatted. A vicinity map is presented in Appendix A.

c. Description of Property

The site is approximately 0.61 miles (2.06 acres) of existing temporary pavement roadway north of Londonderry Drive and south of Grandview Reserve Filing No. 1. Per field inspection the existing pavement is not full depth, and therefore described as 'temporary' for the purpose of this report. The existing temporary pavement width for the length of the project is 26' wide. There are 4' wide gravel shoulders and native landscaped swales are located on both sides of the roadway. Offsite stormwater is bypassed under the road through a series of existing culverts. See Appendix A for an existing conditions photo.

The existing roadway has slopes ranging from 0.3% up to approximately 4%. The general topography of the surrounding area is typical of high desert, short prairie grass with gently rolling hillside with slopes ranging from 2% to 4%. The project site drains generally from the west to the east and is tributary to Black Squirrel Creek.

Per a NRCS soil survey, the site is made up of Type A Columbine gravelly sandy loam, Type A Blakeland loamy sand and Type B Stapleton sandy loam. The NRCS soil survey is presented in Appendix A.

Gieck Ranch Tributary #1 (Channel A) is the only drainageway that traverses the site in the west to east direction through an existing culvert under Eastonville Road that is just north of Segment 1. The channel is a mapped wetland and a wetland permit will be required for Segment 2 of this Eastonville Road improvement project. Channel A is not within a FEMA floodplain.

replace all "temporary pavement" with "treated gravel"

Existing utilities include an underground gas line that runs along the east and west sides of Eastonville, an existing raw water line that follows the west side of Eastonville north of Falcon Regional Park, an existing underground electric line along the west side of Eastonville Road, and an existing aboveground electrical line along the east side of Eastonville Road. An existing drainage map with these facilities is presented in Appendix F.

d. Floodplain Statement

Based on FEMA Firm map 08041C0552G December 7, 2018, the site is not located in any FEMA designated floodplain. See FEMA Firm Map in Appendix A. There is a Zone A floodplain north of the site and a Zone AE south of the site, both of which will not be altered with the associated Eastonville Road Segment 1 improvements.

II. Drainage Design Criteria

a. Drainage Criteria

Hydrologic data and calculations were performed using Drainage Criteria Manual Volume 1 of El Paso County (EPCDCM), with County adopted Chapter 6 and Section 3.2.1 of Chapter 13 of the City of Colorado Springs Drainage Criteria Manual (CCSDCM), May 2014 revised January 2021.

Onsite drainage improvements are designed for the 5-year storm (minor event) and 100-year storm (major event) using rainfall values from the NOAA Atlas 14 Point Precipitation Frequency Data Server. Runoff was calculated per CCSDCM Section 6.3.0 - Rational Method. Private, full spectrum pond design was completed using the latest version of Mile High Flood District’s (MHFD) UD-Detention per CCSDCM Section 13.3.2.1 – Private, full spectrum Detention. The detention pond allowable release rate will be limited to less than historic rates.

| Rainfall Depths per NOAA Atlas 14 | | |
|-----------------------------------|------|------|
| Return Period (yr) | 5 | 100 |
| 1-hr Rainfall Depth (in) | 1.21 | 2.49 |

Inlet sizing was performed per the methods described in EPCDCM Section III Chapter 7 – Street Drainage and Storm Water Inlets. Storm sewer sizing was performed per the methods described in EPCDCM Section III Chapter 8 – Storm Drains and Appurtenances.

III. Drainage Basins and Subbasins

a. Major Basin Description

The site is located within the Gieck Ranch Drainage Basin. The site’s drainage characteristics were previously studied in the following reports:

1. “Gieck Ranch Drainage Basin Planning Study” prepared by Drexel, Barrel & Co, February 2010.
2. “Master Development Drainage Plan Meridian Ranch” prepared by Tech Contractors, July 2021.
3. “Final Drainage Report for The Sanctuary Filing 1 at Meridian Ranch” by Tech Contractors, August 2022.

Gieck Ranch Drainage Basin is a 22.05 square mile watershed located in El Paso County, Colorado. Gieck Ranch Drainage Basin is tributary to Black Squirrel Creek which drains to the Arkansas River. The majority of the basin is undeveloped and is rolling range land typical of Colorado's semi-arid climates.

Within the Gieck Ranch Drainage Basin, ranching has historically been the predominant land use, with rolling topography between 2%-4% slopes. Recently urbanization is occurring within the drainage basin, most notably for this project are Meridian Ranch and Latigo Trails Developments. Both are single family residential neighborhoods located upstream to the west and northwest of the Eastonville Segment 1 Improvements project site.

b. Existing Subbasin Description

replace all "temporary pavement"

Basin E1 is 0.47 acres of temporary pavement to the crown of Eastonville Road roadway and existing swale native landscaped area. Stormwater from this basin ($Q_5 = 0.7$ cfs $Q_{100} = 1.7$ cfs) is conveyed by an existing roadside swale on the northwest edge of Eastonville Road to DP1. Flows at DP1 then drain across Eastonville Road through an existing public 36" CMP culvert to DP2.

Basin E2 is 1.25 acres of temporary pavement to the crown of Eastonville Road roadway and existing swale native landscaped area. Stormwater from this basin ($Q_5 = 1.0$ cfs $Q_{100} = 3.5$ cfs) is conveyed by an existing swale on the southeast edge of Eastonville Road to DP2. Flows at DP2 then drain southeast offsite in historic drainage patterns.

Basin E3 is 0.47 acres of temporary pavement to the crown of Eastonville Road roadway and existing swale native landscaped area. Stormwater from this basin ($Q_5 = 1.0$ cfs $Q_{100} = 2.1$ cfs) is conveyed by an existing roadside swale on the northwest edge of Eastonville Road to DP3. Flows at DP3 then drain across Eastonville Road through an existing public 24" CMP culvert to DP4.

Basin E4 is 1.67 acres of temporary pavement to the crown of Eastonville Road roadway and existing swale native landscaped area. Stormwater from this basin ($Q_5 = 1.4$ cfs $Q_{100} = 4.6$ cfs) is conveyed by an existing swale on the southeast edge of Eastonville Road to DP4. Flows at DP4 then drain southeast offsite in historic drainage patterns.

Basin E5 is 0.23 acres of temporary pavement to the crown of Eastonville Road roadway and existing swale native landscaped area. Stormwater from this basin ($Q_5 = 0.5$ cfs $Q_{100} = 1.1$ cfs) is conveyed by an existing roadside swale on the northwest edge of Eastonville Road to DP5. Flows at DP5 then drain across Eastonville Road through an existing public 18" CMP culvert to DP6.

Basin E6 is 0.21 acres of temporary pavement to the crown of Eastonville Road roadway and existing swale native landscaped area. Stormwater from this basin ($Q_5 = 0.5$ cfs $Q_{100} = 1.1$ cfs) is conveyed by an existing swale on the southeast edge of Eastonville Road to DP6. Flows at DP6 then drain southeast offsite in historic drainage patterns ultimately to the Gieck Ranch Tributary #1.

Basin E7 is 0.23 acres of temporary pavement to the crown of Eastonville Road roadway and existing swale native landscaped area. Stormwater from this basin ($Q_5 = 0.5$ cfs $Q_{100} = 1.2$ cfs) is conveyed by an existing roadside swale on the northwest edge of Eastonville Road to DP7.1. Flows at DP7.1 then drain across Eastonville Road through an existing public 18" CMP culvert to DP8.1.

Basin E8 is 0.18 acres of temporary pavement to the crown of Eastonville Road roadway and existing swale native landscaped area. Stormwater from this basin ($Q_5 = 0.4$ cfs $Q_{100} = 0.9$ cfs) is conveyed by an existing swale on the southeast edge of Eastonville Road to DP8.1. Flows at DP8.1 then drain southeast offsite in historic drainage patterns ultimately to the Gieck Ranch Tributary #1.

Basin E9 is 0.72 acres of temporary pavement to the crown of Eastonville Road roadway and existing swale native landscaped area. Stormwater from this basin ($Q_5 = 1.2$ cfs $Q_{100} = 2.7$ cfs) is conveyed by an existing roadside swale on the northwest edge of Eastonville Road to DP7.2. Flows at DP7.2 then drain across Eastonville Road through an existing public 18" CMP culvert to DP8.2.

Basin E10 is 0.72 acres of temporary pavement to the crown of Eastonville Road roadway and existing swale native landscaped area. Stormwater from this basin ($Q_5 = 1.3$ cfs $Q_{100} = 2.8$ cfs) is conveyed by an existing swale on the southeast edge of Eastonville Road to DP8.2. Flows at DP8.2 then drain southeast offsite in historic drainage patterns ultimately to the Gieck Ranch Tributary #1.

Basin OS1 is 1.58 acres of offsite undeveloped area. Stormwater from this basin ($Q_5 = 0.5$ cfs $Q_{100} = 3.6$ cfs) drains via sheet flow into an existing roadside swale on the northwest side of Eastonville Road. Stormwater then drains to DP1. Flows at DP1 then drain across Eastonville Road through an existing public 36" CMP culvert to DP2. Flows at DP2 then drain southeast offsite in historic drainage patterns.

Basin OS2 is 12.21 acres of offsite undeveloped area. Stormwater from this basin ($Q_5 = 3.6$ cfs $Q_{100} = 24.3$ cfs) drains via sheet flow into an existing roadside swale on the northwest side of Eastonville Road. Stormwater then drains to DP3. Flows at DP3 then drain across Eastonville Road through an existing public 24" CMP culvert to DP4. Flows at DP4 then drain southeast offsite in historic drainage patterns.

Basin OS3.1 is 1.51 acres of offsite undeveloped area. Stormwater from this basin ($Q_5 = 0.5$ cfs $Q_{100} = 3.6$ cfs) drains via sheet flow into an existing roadside swale on the northwest side of Eastonville Road. Stormwater then drains to DP5. Flows at DP5 then drain across Eastonville Road through an existing public 18" CMP culvert to DP6. Flows at DP6 then drain southeast offsite in historic drainage patterns ultimately to the Gieck Ranch Tributary #1.

Basin OS3.2 is 2.86 acres of offsite undeveloped area. Stormwater from this basin ($Q_5 = 1.0$ cfs $Q_{100} = 6.6$ cfs) drains via sheet flow into an existing roadside swale on the northwest side of Eastonville Road. Stormwater then drains to DP7.1. Flows at DP7.1 then drain across Eastonville Road through an existing public 18" CMP culvert to DP8.1. Flows at DP8.1 then drain southeast offsite in historic drainage patterns ultimately to the Gieck Ranch Tributary #1.

Basin OS3.3 is 21.12 acres of offsite undeveloped area. Stormwater from this basin ($Q_5 = 6.4$ cfs $Q_{100} = 42.7$ cfs) drains via sheet flow into an existing roadside swale on the northwest side of Eastonville Road. Stormwater then drains to DP7.2. Flows at DP7.2 then drain across Eastonville Road through an existing public 18" CMP culvert to DP8.2. Flows at DP8.2 then drain southeast offsite in historic drainage patterns ultimately to the Gieck Ranch Tributary #1.

c. Proposed Subbasin Description

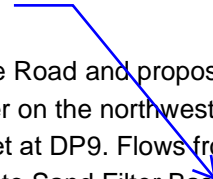
Description of Proposed Project

The proposed project includes improvements to Eastonville Road from Londonderry Drive to the north part of Grandview Filing No. 1. As described above, the current condition of the existing roadway in this area consists of 26' wide temporary pavement roadway with 4' wide gravel shoulders and native landscaped swales located on both sides of the roadway. Offsite stormwater is bypassed under the proposed roadway via proposed public RCP culverts.

The proposed improvements to Eastonville Road from Londonderry Drive to the north part of Grandview Filing No. 1 include removal of the 26' wide temporary pavement and replacing the road with a Modified Urban Minor Arterial Roadway Cross-Section consisting of 48' pavement and Type A EPC curb (53' back of curb to back of curb).

Eastonville Road Basins

coordinate with
PPRTA Pond E



Basin EA1 is 0.61 acres of proposed pavement to the crown of Eastonville Road and proposed landscaped area. Stormwater ($Q_5 = 2.2$ cfs $Q_{100} = 4.1$ cfs) is conveyed by curb & gutter on the northwest side of Eastonville Road. Runoff is then captured in a public 5' CDOT Type R Inlet at DP9. Flows from DP9 are conveyed through a proposed public storm sewer system which outfalls into Sand Filter Basin D. Sand Filter Basin D is located southeast of the proposed Eastonville Road Segment 1 improvements outside of the proposed right-of-way within a proposed drainage easement.

Basin EA2 is 1.23 acres of proposed pavement to the crown of Eastonville Road and proposed landscaped area. Stormwater ($Q_5 = 2.2$ cfs $Q_{100} = 5.3$ cfs) is conveyed by curb & gutter on the southeast side of Eastonville Road. Runoff is then captured in a public 5' CDOT Type R Inlet at DP10. Flows from DP10 are conveyed through a proposed public storm sewer system which outfalls into Sand Filter Basin D. Sand Filter Basin D is located southeast of the proposed Eastonville Road Segment 1 improvements outside of the proposed right-of-way within a proposed drainage easement.

Basin EA3 is 0.53 acres of proposed pavement to the crown of Eastonville Road and proposed landscaped area. Stormwater ($Q_5 = 2.1$ cfs $Q_{100} = 3.4$ cfs) is conveyed by curb & gutter on the northwest side of Eastonville Road. Runoff is then captured in a public 5' CDOT Type R Inlet at DP13. Flows at DP13 are conveyed across Eastonville Road through a public storm sewer system to Sand Filter Basin A. Sand Filter Basin A is located southeast of the proposed Eastonville Road Segment 1 improvements outside of the proposed right-of-way within a proposed drainage easement.

Basin EA4 is 0.90 acres of proposed pavement to the crown of Eastonville Road and proposed landscaped area. Stormwater ($Q_5 = 2.0$ cfs and 3.4 cfs) is conveyed by curb & gutter on the southeast side of Eastonville Road. Runoff is then captured in a public 5' CDOT Type R Inlet at DP10. Flows at DP14 are conveyed through a public storm sewer system to Sand Filter Basin A. Sand Filter Basin A is located southeast of the proposed Eastonville Road Segment 1 improvements outside of the proposed right-of-way within a proposed drainage easement.

Basin EA5 is 0.29 acres of landscaped area, gravel access road, and contains the private full spectrum sand filter basin A. Stormwater ($Q_5 = 0.2$ cfs $Q_{100} = 0.3$ cfs) from this basin sheet flows directly into Sand Filter Basin A. Sand Filter Basin A is located southeast of the proposed Eastonville Road Segment 1 improvements outside of the proposed right-of-way within a proposed drainage easement.

Basin EA6 is 1.11 acres of proposed pavement to the crown of Eastonville Road and proposed landscaped area. Stormwater ($Q_5 = 3.0$ cfs $Q_{100} = 5.1$ cfs) is conveyed by curb & gutter on the west side of Eastonville Road. Runoff is then captured in a public 10' CDOT Type R Inlet at DP16. Flows at DP16 are conveyed across Eastonville Road through a public storm sewer system to Extended Detention Basin B. Extended Detention Basin B is located southeast of the proposed Eastonville Road Segment 1 improvements outside of the proposed right-of-way within a proposed drainage easement.

Basin EA7 is 1.91 acres of proposed pavement to the crown of Eastonville Road and proposed landscaped area. Stormwater ($Q_5 = 3.3$ cfs $Q_{100} = 5.6$ cfs) is conveyed by curb & gutter on the east side of Eastonville

Must be supported with RR calcs. But these two basins are small enough to count towards the exclusion in ECM App I.7.1.C.1 (20% up to 1ac of development can be excluded). Revise these sentences accordingly based on what you decide.

Road. Runoff is then captured in a public 10' CDOT Type R Inlet at DP17. Flows at DP17 are conveyed through a public storm sewer system to Extended Detention Basin B. Extended Detention Basin B is located southeast of the proposed Eastonville Road Segment 1 improvements outside of the proposed right-of-way within a proposed drainage easement.

Basin EA8 is 0.86 acres of landscaped area, gravel access road, and contains extended detention basin B. Stormwater ($Q_5 = 0.5$ cfs $Q_{100} = 0.8$ cfs) from this basin sheet flows directly into Extended Detention Basin B. Extended Detention Basin B is located southeast of the proposed Eastonville Road Segment 1 improvements outside of the proposed right-of-way within a proposed drainage easement.

Basin EA9 is 0.92 acres of landscaped area. Stormwater ($Q_5 = 0.4$ cfs $Q_{100} = 0.6$ cfs) from this basin sheet flows directly offsite towards DP20. Water quality will be accounted for via runoff reduction swales & grass buffers.

Basin EA10 is 0.37 acres of landscaped area. Stormwater ($Q_5 = 0.2$ cfs $Q_{100} = 0.3$ cfs) from this basin sheet flows directly offsite towards DP21. Water quality will be accounted for via runoff reduction swales & grass buffers.

Basin EA11 is 0.15 acres of landscaped area. Stormwater ($Q_5 = 0.1$ cfs $Q_{100} = 0.1$ cfs) from this basin sheet flows directly offsite towards DP22. Water quality will be accounted for via runoff reduction swales & grass buffers.

Basin EA12 is 0.26 acres of landscaped area. Stormwater ($Q_5 = 0.2$ cfs $Q_{100} = 0.8$ cfs) from this basin sheet flows directly into Pond D.

Revise to SFB D for consistency.

Basin EA13 is 0.21 acres of landscaped area. Stormwater ($Q_5 = 0.1$ cfs $Q_{100} = 0.1$ cfs) from this basin sheet flows directly offsite towards DP12. Water quality will be accounted for via runoff reduction swales & grass buffers.

2 and 12?

Basin OS1 is 1.63 acres of offsite undeveloped area. Stormwater from this basin ($Q_5 = 0.5$ cfs $Q_{100} = 3.6$ cfs) drains via sheet flow into a proposed roadside swale on the northwest side of Eastonville Road. Stormwater then drains to DP1. Flows at DP1 then drain across Eastonville Road through a proposed public 18" RCP culvert to DP2. Flows at DP2 then drain southeast offsite in historic drainage patterns. Water quality treatment for the disturbed area within this basin is accounted for by infiltration by grass overland flow.

Basin OS2 is 12.33 acres of offsite undeveloped area. Stormwater from this basin ($Q_5 = 3.7$ cfs $Q_{100} = 24.5$ cfs) drains via sheet flow into a proposed roadside swale on the northwest side of Eastonville Road. Stormwater then drains to DP3. Flows at DP3 then drain across Eastonville Road through a proposed public 30" RCP culvert to DP4. Flows at DP4 then drain southeast offsite in historic drainage patterns. Water quality treatment for the disturbed area within this basin is accounted for by infiltration by grass overland flow.

Basin OS3 is 25.35 acres of offsite undeveloped area. Stormwater from this basin ($Q_5 = 7.9$ cfs $Q_{100} = 53.3$ cfs) drains via sheet flow into a proposed roadside swale on the northwest side of Eastonville Road. Stormwater then drains to a proposed public CDOT type D inlet at DP7. Flows at DP7 then drain across Eastonville Road through a proposed public storm sewer system. This storm sewer system outfalls at DP8 into the Gieck Ranch Tributary #1 where drainage will follow historic patterns. Water quality treatment for the disturbed area within this basin is accounted for by infiltration by grass overland flow.

Unresolved comment from Review 1:

Basins OS1, OS2, OS3, and the unnamed basins that are east of Eastonville Rd all have proposed soil disturbances within them, which all must be accounted for via WQ treatment or an applicable WQ exclusion. So please address this in the respective Basin paragraphs and create new proposed sub-basins as necessary.

Review 2 update: these 3 "offsite undeveloped areas" are still shown on the drainage map as having proposed disturbances. Meaning that they are neither "offsite" or "undeveloped." Please revise map and descriptions to add onsite basins for the areas of disturbance and discuss WQ treatment or applicable WQ exclusions. Just stating that infiltration is occurring is not enough. You'll need to show Runoff Reduction calcs for RPAs and/or SPAs or an applicable exclusion.

IV. Drainage Facility Design

a. General Concept

The proposed improvements to Eastonville Road from Londonderry Drive to the north part of Grandview Filing No. 1 include removal of the 26' wide temporary pavement and replacing the road with a Modified Urban Minor Arterial Roadway Cross-Section consisting of 48' pavement and Type A EPC curb (53' back of curb to back of curb). Inlets will be placed at low points. Stormwater from this roadway will be piped to either a full spectrum detention basin or full spectrum sand filters. All detention basins and water quality features will discharge at less than historic rates. Runoff generated from the site will release at historic design points at less than historic flow rates. A flow comparison of existing/proposed stormwater release rates offsite from the project is below:

| DESIGN POINT | EX Q ₅ (cfs) | PR Q ₅ (cfs) | EX Q ₁₀₀ (cfs) | PR Q ₁₀₀ (cfs) |
|-----------------|-------------------------|-------------------------|---------------------------|---------------------------|
| DP2 | 2.1 | 0.9 | 8.2 | 5.0 |
| DP4 | 5.8 | 4.0 | 30.4 | 26.4 |
| DP6 | 1.3 | - | 5.4 | - |
| DP8 (8.1 & 8.2) | 10.3 | 8.3 | 55.9 | 54.3 |
| TOTAL | 19.5 | 12.7 | 99.9 | 84.2 |

b. Water Quality & Detention

Sand Filter Basin A (Full Spectrum SFB)

Water quality and stormwater detention for Basins EA3-EA5 is provided in Sand Filter Basin A. SFB A is a private, full spectrum sand filter basin within the ACM ALF VIII JV SUB II LLC (previous Waterbury) property within a proposed drainage easement. In SFB A, a total of 1.72 acres of disturbed area from the proposed project at 55% composite imperviousness will be detained and treated for water quality. The WQCV is 0.025 ac-ft, the EURV is 0.102 ac-ft, and the 100-year detention volume is 0.173 ac-ft. The WQCV, EURV and 100-year storms are released in 13, 44 and 49 hours, respectively. A 15' access and maintenance road is provided to the bottom of the pond to facilitate maintenance of the pond facilities. A 4.75' emergency overflow spillway is provided that conveys the developed, peak 100-yr flow rate with 1.0' of freeboard south toward DP4. SFB A outfalls towards DP4 at historic runoff rates. Runoff from DP4 will follow historic drainage patterns and not exceed historic flow rates.

0.291 per MHFD-Detention calcs on pg 94 below.

County-owned

| SFB A Water Quality Treatment Summary Table | | | | |
|---|-----------------|------------------------------------|-------------------------|--|
| Basin ID | Total Area (ac) | Total Proposed Disturbed Area (ac) | Area Trib to SFB A (ac) | Disturbed Area Treated via Runoff Reduction (ac) |
| EA3 | 0.53 | 0.53 | 0.66 | 0 |
| EA4 | 0.90 | 0.90 | 1.12 | 0 |
| EA5 | 0.29 | 0.29 | 0.29 | 0 |
| Total | 1.72 | 1.72 | 1.72 | 0 |

3.88ac per table at the bottom of this page. Revise to remove discrepancy or to explain the reasoning for it.

Extended Detention Basin B (Full Spectrum EDB)

Water quality and detention for Basins EA6 – EA8 is provided in Extended Detention Basin B; a private, full spectrum extended detention basin within Filing No. 1 of Grandview Reserve within a proposed drainage easement. A total of 9.32 acres of disturbed area from the proposed project at 68% composite imperviousness will be treated and detained by EDB B for this phase of the Eastonville Road Improvements. The pond has been sized with consideration for the future segments of Eastonville Road and provides water quality and detention for the ultimate conditions at a future date. The ultimate conditions of EDB B calculations have been provided in the Appendix of this report. Ultimate conditions include fully built sections of Eastonville Road from Londonderry Road to Rex Road and is anticipated for Spring 2025. Interim condition pond sizing calculations have also been provided in the Appendix of this report. Interim conditions only include Eastonville road from Londonderry to Grandview Filing No.1. The ultimate conditions WQCV is 0.207 ac-ft, the EURV is 0.796 ac-ft, and the 100-year detention volume is 1.175 ac-ft. The WQCV, EURV and 100-year storms are released in 41, 69 and 70 hours, respectively. A forebay is located at the outfall into the pond and a 40" trickle channel conveys flow towards the outlet structure. A 15' access and maintenance road is provided to the bottom of the pond to facilitate maintenance of the pond facilities. A 15.5' emergency overflow spillway is provided that conveys the developed, peak 100-yr flow rate with 1.0' of freeboard towards Gieck Ranch Tributary #1. EDB B outfalls towards DP8 at historic runoff rates. Runoff from DP8 will follow historic drainage patterns and not exceed historic flow rates.

District?

| EDB B Water Quality Treatment Summary Table | | | | |
|---|-----------------|------------------------------------|-------------------------|--|
| Basin ID | Total Area (ac) | Total Proposed Disturbed Area (ac) | Area Trib to SFB A (ac) | Disturbed Area Treated via Runoff Reduction (ac) |
| EA6 | 1.11 | 1.11 | 1.11 | 0 |
| EA7 | 1.91 | 1.91 | 1.91 | 0 |
| EA8 | 0.86 | 0.86 | 0.86 | 0 |
| Total | 3.88 | 3.88 | 3.88 | 0 |

The FDR for Segment 2 just states that the design of EDB B was done with Segment 1. But this Segment 1 FDR does not discuss in the report text, show in calcs, or show in drainage maps the Segment 2 basins (EA8 - EA11) that will be treated by EDB B... So please do so. Otherwise there is no way for us to review the design of this pond and compare to CDs, since not enough information has been provided...

Unresolved comment from Review that was on the "Pond B - Ultimate" MHFD Calcs page for reference, since it is related to my new comment on the left.

EA9 and EA10 are not shown on the drainage map. My understanding is that in the Ultimate Condition (Segment 1 & 2), Pond B will detain flows from Segment 1's Basins EA6-EA8 and Segment 2's Basins EA8-EA11. This is potentially confusing because the two segment basins EA8 are completely different basins. So just clarify here which basin is from each segment like I have above.

Here's my understanding of EDB B, summarized in a table:

| Segment | Basin | Area (ac) | Total |
|-----------|-------|-----------|-------|
| Segment 1 | EA6 | 1.11 | 3.88 |
| | EA7 | 1.91 | |
| | EA8 | 0.86 | |
| Segment 2 | EA8 | 2.08 | 5.38 |
| | EA9 | 2.99 | |
| | EA10 | 0.12 | |
| | EA11 | 0.19 | |
| | | | 9.26 |



coordinate with Pond E
County-owned

Sand Filter Basin D (Full Spectrum SFB).

Water quality and stormwater detention for Basins EA1-EA2, EA12 is provided in Sand Filter Basin D. SFB D is a private, full spectrum sand filter basin the ACM ALF VIII JV SUB II LLC (previous Waterbury) property within a proposed drainage easement. In SFB D, a total of 2.10 acres of disturbed area from the proposed project at 52% composite imperviousness will be detained and treated for water quality. The WQCV is 0.030 ac-ft, the EURV is 0.117 ac-ft, and the 100-year detention volume is 0.202 ac-ft. The WQCV, EURV and 100-year storms are released in 12, 40 and 43 hours, respectively. A 15' access and maintenance road is provided to the bottom of the pond to facilitate maintenance of the pond facilities. A 30' emergency overflow spillway is provided that conveys the developed, peak 100-yr flow rate with 1.0' of freeboard south toward DP2. SFB D outfalls towards DP4 at historic runoff rates. Runoff from DP2 will follow historic drainage patterns and not exceed historic flow rates

DP 4 is cross culvert under Eastonville Rd just north of this pond. Do not see how flows from the pond will reach DP4.

Summary Table

| Basin ID | Total Area (ac) | Total Proposed Disturbed Area (ac) | Area Trib to SFB A (ac) | Disturbed Area Treated via Runoff Reduction (ac) |
|----------|-----------------|------------------------------------|-------------------------|--|
| EA1 | 0.61 | 0.61 | 0.61 | 0 |
| EA2 | 1.23 | 1.23 | 1.23 | 0 |
| EA12 | 0.26 | 0.26 | 0.26 | 0 |
| Total | 2.10 | 2.10 | 2.10 | 0 |

c. Inspection and Maintenance

After completion of construction and upon the Board of County Commissioners acceptance, it is anticipated that all drainage facilities within the public Right-of-Way are to be owned and maintained by El Paso County.

All private detention ponds are to be owned and maintained by the Grandview Reserve Metropolitan District NO. 2 (DISTRICT), once established, unless an agreement is reached stating otherwise. Maintenance access for all full spectrum detention facilities will be provided from public Right-of-Way. Maintenance access for the drainageways will be provided through the proposed tracts.

V. Wetlands Mitigation

There are no wetlands in Segment 1 of the project and therefore no wetland permit is required for Segment 1.

VI. Four Step Method to Minimize Adverse Impacts of Urbanization

Step 1 – Reducing Runoff Volumes: Low impact development (LID) practices are utilized to reduce runoff at the source. Storm sewer outfalls have been designed at the upstream end of detention basins. This practice promotes infiltration in the detention basins and reduces peak runoff rates prior to runoff reaching outlet structures.

Step 2 – Treat and slowly release the WQCV: This step utilizes full spectrum water quality and detention to capture the WQCV and slowly release runoff from the site. Onsite full spectrum sand filter basins & an extended detention basin provide water quality treatment for the site. The WQCV is released over a period of at least 12 hours for SFBs and 40 hours for EDBs while the EURV is released over a period of 40-44 hours for SFBs and 68 - 72 hours for EDBs.

Step 3 – Stabilize stream channels: This step establishes practices to stabilize drainageways and provide scour protection at stormwater outfalls. Erosion protection is provided at all concentrated stormwater discharge points in the form of riprap pads. No impact will be made to the Gieck Ranch Tributary #1 by this project that requires additional stream stabilization.

Step 4 – Consider the need for source controls: No industrial or commercial uses are proposed within this development and therefore no source controls are proposed.

VII. Drainage and Bridge Fees

Gieck Ranch drainage basin has not been established as a fee basin within El Paso County. Therefore, no drainage basin fees are due at time of platting.

VIII. Opinion of Probable Cost

An engineer's opinion of probable cost has been provided below for public and private drainage infrastructure improvements. This includes cost estimates for the private full spectrum sand filter basin A, private full spectrum sand filter basin D and the private full spectrum extended detention basin B. All required stormwater infrastructure will be installed per El Paso County Requirements. The unit cost includes both materials and labor.

| Private Infrastructure Cost Estimate | | | |
|--------------------------------------|----------|------------|-----------------|
| Line Item | Quantity | Unit Price | Cost |
| 18" Reinforced Concrete Pipe | 239 | \$76 LF | \$18,164 |
| 24" Reinforced Concrete Pipe | 191.5 | \$91 LF | \$17,427 |
| 18" CDOT FES | 1 | \$456 EA | \$456 |
| 10% Contingency | | | \$3,605 |
| TOTAL: | | | \$39,651 |

| Public Infrastructure Cost Estimate | | | |
|-------------------------------------|----------|------------|------------------|
| Line Item | Quantity | Unit Price | Cost |
| 18" Reinforced Concrete Pipe | 532 | \$76 LF | \$29,032 |
| 30" Reinforced Concrete Pipe | 632.5 | \$114 LF | \$72,105 |
| 42" Reinforced Concrete Pipe | 420 | \$187 LF | \$51,986 |
| 18" CDOT FES | 2 | \$456 EA | \$912 |
| 30" CDOT FES | 2 | \$684 EA | \$1,368 |
| 42" CDOT FES | 1 | \$912 EA | \$912 |
| 6' DIA Storm Manhole | 9 | \$7,734 EA | \$69,606 |
| 5' CDOT Type R Inlet | 6 | \$6,703 EA | \$40,218 |
| CDOT Type D Inlet | 1 | \$6,931 EA | \$6,931 |
| Rip Rap, d50 size from 6"-24" | 5 | \$97 Tons | \$485 |
| 10% Contingency | | | \$27,356 |
| TOTAL: | | | \$300,911 |

| Private SFB A Cost Estimate | | | |
|--|----------|------------|-----------------|
| Line Item | Quantity | Unit Price | Cost |
| Rip Rap, d50 size from 6"-24" (Inflow) | 2 | \$97 Tons | \$194 |
| Sand Filter Media | 72.5 | \$100 /CY | \$7,250 |
| 4" Perforated PVC Underdrain | 100 | \$10 /LF | \$1,000 |
| 12" ABC Maintenance Access | 25 | \$40 /CY | \$1,000 |
| Outlet Structure w/ Orifice Plate | 1 | \$5,000 EA | \$5,000 |
| Rip Rap, d50 size from 6"-24" (Spillway) | 60.5 | \$97 Tons | \$5,869 |
| 18" RCP Outlet Pipe | 54 | \$82 /LF | \$4,428 |
| 18" RCP FES | 1 | \$492 EA | \$492 |
| 10% Contingency | | | \$2,523 |
| TOTAL: | | | \$27,756 |

does not match what is shown in Section 1 of FAE

| Private SFB D Cost Estimate | | | |
|--|----------|------------|-----------------|
| Line Item | Quantity | Unit Price | Cost |
| Rip Rap, d50 size from 6"-24" (Inflow) | 2 | \$97 Tons | \$194 |
| Sand Filter Media | 72.5 | \$100 /CY | \$7,250 |
| 4" Perforated PVC Underdrain | 100 | \$10 /LF | \$1,000 |
| 12" ABC Maintenance Access | 25 | \$40 /CY | \$1,000 |
| Outlet Structure w/ Orifice Plate | 1 | \$5,000 EA | \$5,000 |
| Rip Rap, d50 size from 6"-24" (Spillway) | 60.5 | \$97 Tons | \$5,869 |
| 18" RCP Outlet Pipe | 54 | \$82 /LF | \$4,428 |
| 18" RCP FES | 1 | \$492 EA | \$492 |
| 10% Contingency | | | \$2,523 |
| TOTAL: | | | \$27,756 |

| Private EDB B Cost Estimate | | | |
|---|----------|------------|-----------------|
| Line Item | Quantity | Unit Price | Cost |
| Concrete Forebay | 1 | \$5,000 EA | \$5,000 |
| Rip Rap, d50 size from 6"-24" (Inflow) | 2.75 | \$97 Tons | \$267 |
| Concrete Trickle Channel | 36 | \$100 /SY | \$3,600 |
| 12" ABC Maintenance Access | 114 | \$40 /CY | \$4,560 |
| Outlet Structure w/ Micropool, Trash Rack, Railing, Orifice Plate | 1 | \$8,000 EA | \$8,000 |
| Rip Rap, d50 size from 6"-24" (Spillway) | 87 | \$97 Tons | \$8,439 |
| 18" RCP Outlet Pipe | 31 | \$76 /LF | \$2,356 |
| 10% Contingency | | | \$3,222 |
| TOTAL: | | | \$35,444 |

IX. Hydraulic Grade Line Analysis

Hydraulic grade line analysis and final pipe sizes were analyzed, and calculations are provided in Appendix C. All proposed storm sewer has been designed in accordance with El Paso County Drainage Criteria Manuals.

X. Summary

Eastonville Road lies within the Gieck Ranch Drainage Basin. Water quality and detention for the proposed improvements is provided in full spectrum extended detention basins and two full spectrum sand filter basins, both within proposed drainage easements. There is one major drainageway that traverses north of the Segment 1 site: Gieck Ranch Tributary 1. This major drainage way will not be impacted by the proposed improvements. **The water quality and detention ponds will be maintained by the Grandview Reserve Metropolitan District No. 2 (DISTRICT).** All drainage facilities were sized per the El Paso County Drainage Criteria Manuals. *verify - 2 by County?*

The development of this project will not adversely affect downstream properties.

XI. Drawings

Please refer to the appendices for vicinity and drainage basin maps.

XII. References

1. City of Colorado Springs – Drainage Criteria Manual, May 2014, Revised January 2021.
2. Drainage Criteria Manual of El Paso, Colorado, October 2018.
3. Urban Storm Drainage Criteria Manual, Urban Drainage Flood Control District, January 2018.
4. “Gieck Ranch Drainage Basin Planning Study” prepared by Drexel, Barrel & Co, February 2010.
5. “Master Development Drainage Plan Meridian Ranch” prepared by Tech Contractors, July 2021.
6. “The Sanctuary Filing 1 at Meridian Ranch” prepared by Tech Contractors, August 2022.

APPENDIX A – VICINITY MAP, PHOTOS, SOIL MAP, FEMA MAP

MERIDIAN RANCH

FALCON REGIONAL PARK

GIECK RANCH TRIBUTARY 2

REX RD

EASTONVILLE ROAD

GRANDVIEW RESERVE METROPOLITAN DISTRICT NO. 2

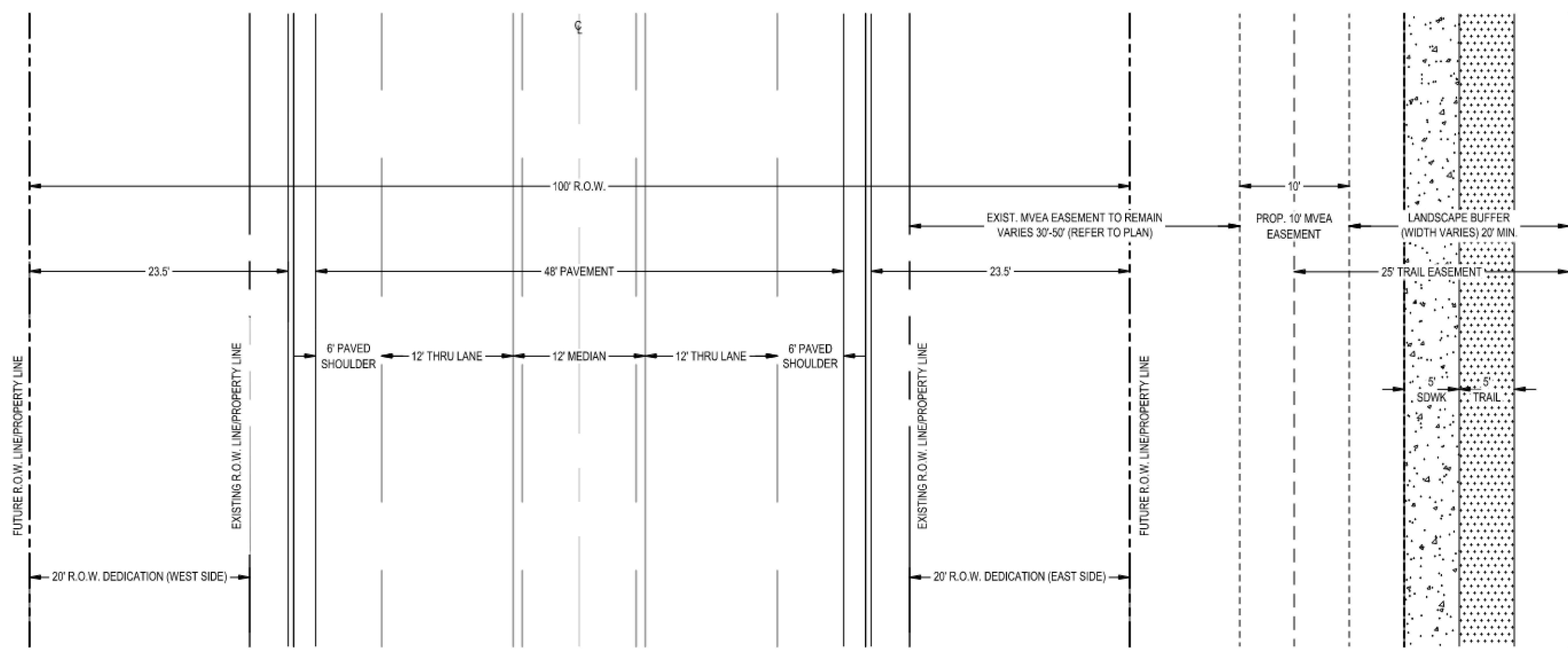
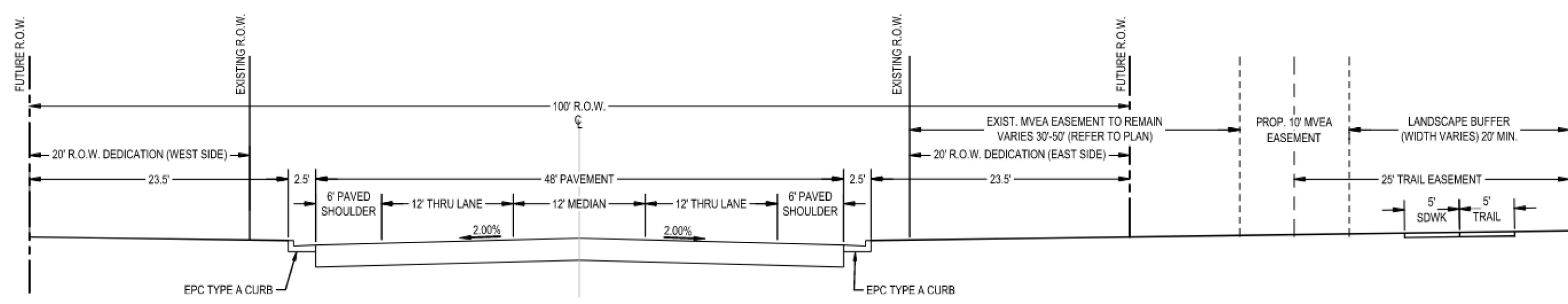
GIECK RANCH TRIBUTARY 1

GRANDVIEW RESERVE FILING 1

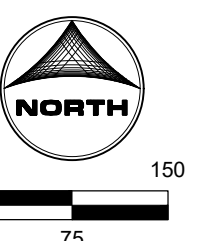
FALCON HIGH SCHOOL

SEGMENT 1
MODIFIED MINOR
ARTERIAL
CROSS-SECTION WITH
48' PAVEMENT AND
TYPE A EPC CURB (53'
BACK OF CURB TO
BACK OF CURB)

LONDONDERRY DR



VICINITY MAP
N.T.S.



HR GREEN ARCHITECTS & ENGINEERS, P.C. 7222 COMMERCE CENTER DR, SUITE 220, COLORADO SPRINGS, CO 80919, PHONE: 719.622.6222, FAX: 844.273.1057

DRAWN BY: CPM JOB DATE: 8/29/2023
 APPROVED: [Signature] JOB NUMBER: 201862.08
 CAD DATE: 8/29/2023
 CAD FILE: J:\2020\201862.08\CAD\Drawings\Exhibits-Overall-Exhibit

| NO. | DATE | BY | REVISION DESCRIPTION |
|-----|------|----|----------------------|
| | | | |

HR GREEN - COLORADO SPRINGS
 7222 COMMERCE CENTER DR, SUITE 220
 COLO. SPRINGS, CO 80919
 PHONE: 719.622.6222
 FAX: 844.273.1057

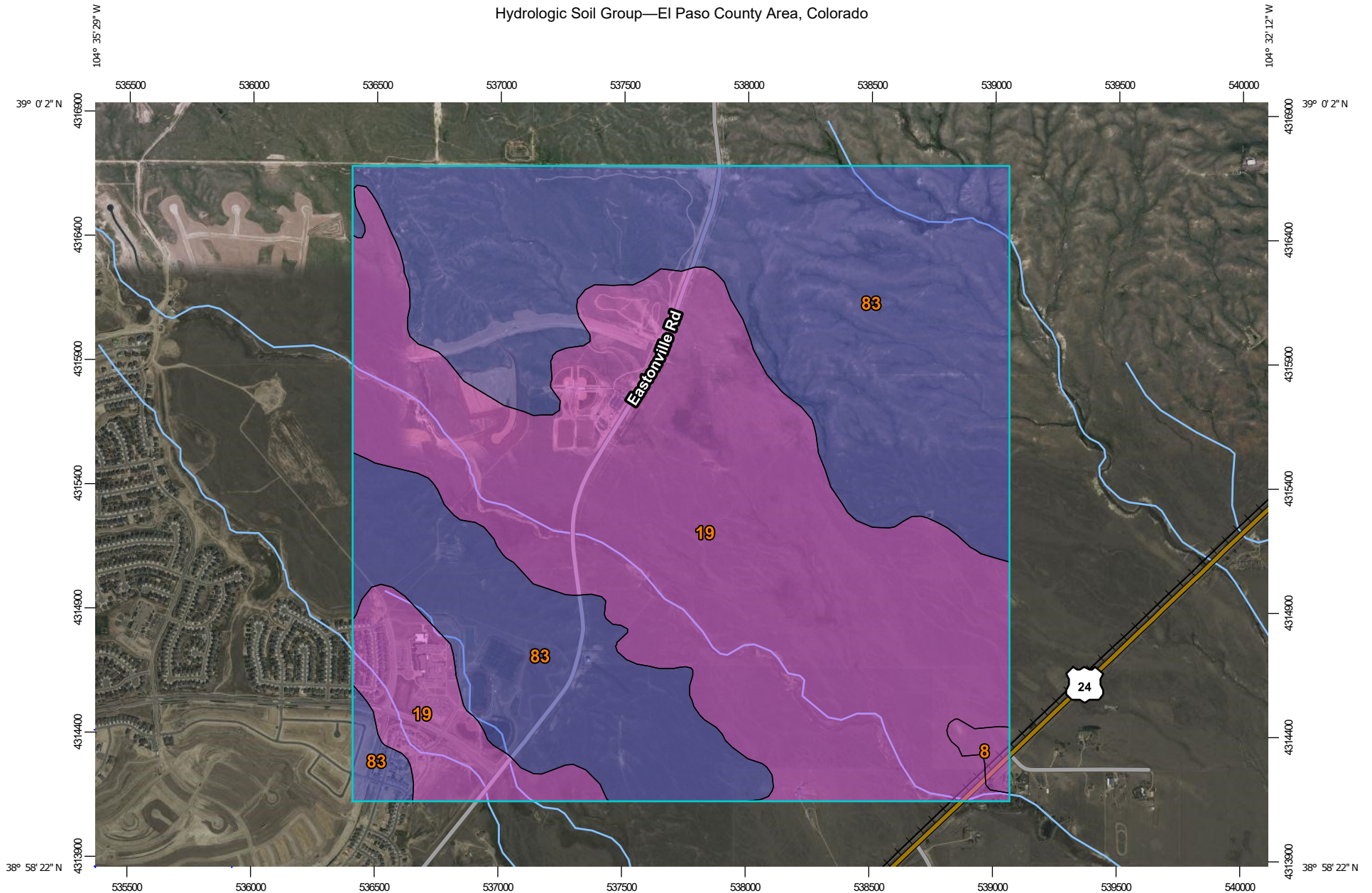
EASTONVILLE ROAD
 DR HORTON
 EL PASO COUNTY, CO

OVERALL EASTONVILLE PLAN

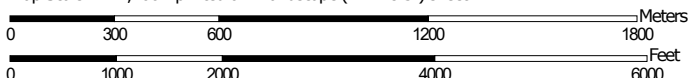
Photo - at Londonderry and Eastonville looking north



Hydrologic Soil Group—El Paso County Area, Colorado



Map Scale: 1:21,700 if printed on A landscape (11" x 8.5") sheet.




Map projection: Web Mercator Corner coordinates: WGS84 Edge tics: UTM Zone 13N WGS84



MAP LEGEND

Area of Interest (AOI)









 Area of Interest (AOI)

Soils

Soil Rating Polygons





-  A
-  A/D
-  B
-  B/D
-  C
-  C/D
-  D
-  Not rated or not available

Soil Rating Lines

-  A
-  A/D
-  B
-  B/D
-  C
-  C/D
-  D
-  Not rated or not available

Soil Rating Points


-  A
-  A/D
-  B
-  B/D

-  C
-  C/D
-  D
-  Not rated or not available


Water Features

 Streams and Canals

Transportation

-  Rails
-  Interstate Highways
-  US Routes
-  Major Roads
-  Local Roads

Background

 Aerial Photography

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24,000.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service
 Web Soil Survey URL:
 Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: El Paso County Area, Colorado
 Survey Area Data: Version 19, Aug 31, 2021

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Sep 11, 2018—Jun 12, 2021

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Hydrologic Soil Group

| Map unit symbol | Map unit name | Rating | Acres in AOI | Percent of AOI |
|------------------------------------|--|--------|----------------|----------------|
| 8 | Blakeland loamy sand, 1 to 9 percent slopes | A | 10.4 | 0.6% |
| 19 | Columbine gravelly sandy loam, 0 to 3 percent slopes | A | 839.5 | 49.8% |
| 83 | Stapleton sandy loam, 3 to 8 percent slopes | B | 835.7 | 49.6% |
| Totals for Area of Interest | | | 1,685.6 | 100.0% |

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

Rating Options

Aggregation Method: Dominant Condition

Component Percent Cutoff: None Specified

Tie-break Rule: Higher

NOTES TO USERS

This map is for use in administering the National Flood Insurance Program. It does not necessarily identify all areas subject to flooding, particularly from local drainage sources of small size. The community map repository should be consulted for possible updated or additional flood hazard information.

To obtain more detailed information in areas where **Base Flood Elevations (BFEs)** have been determined, users are encouraged to consult the Flood Profiles and Floodway Data and/or Summary of Stillwater Elevations tables contained within the Flood Insurance Study (FIS) report that accompanies this FIRM. Users should be aware that BFEs shown on the FIRM represent rounded whole-foot elevations. These BFEs are intended for flood insurance rating purposes only and should not be used as the sole source of flood elevation information. Accordingly, flood elevation data presented in the FIS report should be utilized in conjunction with the FIRM for purposes of construction and/or floodplain management.

Coastal Base Flood Elevations shown on this map apply only to landward of 0' North American Vertical Datum of 1988 (NAVD88). Users of this FIRM should be aware that coastal flood elevations are also provided in the Summary of Stillwater Elevations table in the Flood Insurance Study report for this jurisdiction. Elevations shown in the Summary of Stillwater Elevations table should be used for construction and/or floodplain management purposes when they are higher than the elevations shown on this FIRM.

Boundaries of the floodways were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations with regard to requirements of the National Flood Insurance Program. Floodway widths and other pertinent floodway data are provided in the Flood Insurance Study report for this jurisdiction.

Certain areas not in Special Flood Hazard Areas may be protected by **flood control structures**. Refer to section 2.4 "Flood Protection Measures" of the Flood Insurance Study report for information on flood control structures for this jurisdiction.

The projection used in the preparation of this map was Universal Transverse Mercator (UTM) zone 13. The horizontal datum was NAD83, GRS80 spheroid. Differences in datum, spheroid, projection or UTM zones used in the production of FIRMs for adjacent jurisdictions may result in slight positional differences in map features across jurisdiction boundaries. These differences do not affect the accuracy of this FIRM.

Flood elevations on this map are referenced to the **North American Vertical Datum of 1988 (NAVD88)**. These flood elevations must be compared to structure and ground elevations referenced to the same vertical datum. For information regarding conversion between the National Geodetic Vertical Datum of 1929 and the North American Vertical Datum of 1988, visit the National Geodetic Survey website at <http://www.ngs.noaa.gov/> or contact the National Geodetic Survey at the following address:

NGS Information Services
NOAA, NNGS12
National Geodetic Survey
SSMC-3, #9022
1313 East West Highway
Silver Spring, MD 20910-3282

To obtain current elevation, description, and/or location information for **bench marks** shown on this map, please contact the Information Services Branch of the National Geodetic Survey at (301) 713-3242 or visit its website at <http://www.ngs.noaa.gov>.

Base Map information shown on this FIRM was provided in digital form by El Paso County, Colorado Springs Utilities, City of Fountain, Bureau of Land Management, National Oceanic and Atmospheric Administration, United States Geological Survey, and Anderson Consulting Engineers, Inc. These data are current as of 2006.

This map reflects more detailed and up-to-date stream channel configurations and floodplain delineations than those shown on the previous FIRM for this jurisdiction. The floodplains and floodways that were transferred from the previous FIRM may have been adjusted to conform to these new stream channel configurations. As a result, the Flood Profiles and Floodway Data tables in the Flood Insurance Study Report (which contains authoritative hydraulic data) may reflect stream channel distances that differ from what is shown on this map. The profile baselines depicted on this map represent the hydraulic modeling baselines that match the flood profiles and Floodway Data Tables if applicable, in the FIS report. As a result, the profile baselines may deviate significantly from the new base map channel representation and may appear outside of the floodplain.

Corporate limits shown on this map are based on the best data available at the time of publication. Because changes due to annexations or de-annexations may have occurred after this map was published, map users should contact appropriate community officials to verify current corporate limit locations.

Please refer to the separately printed **Map Index** for an overview map of the county showing the layout of map panels, community map repository addresses, and a Listing of Communities table containing National Flood Insurance Program dates for each community as well as a listing of the panels on which each community is located.

Contact **FEMA Map Service Center (MSC)** via the FEMA Map Information eXchange (FMIX) 1-877-336-2627 for information on available products associated with this FIRM. Available products may include previously issued Letters of Map Change, Flood Insurance Study Report, and/or digital versions of this map. The MSC may also be reached by Fax at 1-800-358-9620 and its website at <http://www.msc.fema.gov/>.

If you have **questions about this map** or questions concerning the National Flood Insurance Program in general, please call 1-877-FEMA-MAP (1-877-336-2627) or visit the FEMA website at <http://www.fema.gov>.

El Paso County Vertical Datum Offset Table

| Flooding Source | Vertical Datum Offset |
|---|-----------------------|
| REFER TO SECTION 3.3 OF THE EL PASO COUNTY FLOOD INSURANCE STUDY FOR STREAM BY STREAM VERTICAL DATUM CONVERSION INFORMATION | |

Panel Location Map

This Digital Flood Insurance Rate Map (DFIRM) was produced through a Cooperating Technical Partner (CTP) agreement between the State of Colorado Water Conservation Board (CWCB) and the Federal Emergency Management Agency (FEMA).

Additional Flood Hazard information and resources are available from local communities and the Colorado Water Conservation Board.

Additional Flood Hazard information and resources are available from local communities and the Colorado Water Conservation Board.

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NOTE: MAP AREA SHOWN ON THIS PANEL IS LOCATED WITHIN TOWNSHIP 12 SOUTH, RANGE 64 WEST

LEGEND

SPECIAL FLOOD HAZARD AREAS (SFHAS) SUBJECT TO INUNDATION BY THE 1% ANNUAL CHANCE FLOOD

The 1% annual chance flood (100-year flood), also known as the base flood, is the flood that has a 1% chance of being equaled or exceeded in any given year. The Special Flood Hazard Area is the area subject to flooding by the 1% annual chance flood. Areas of Special Flood Hazard include Zone AE, Zone AH, Zone A, Zone V, and Zone VE. The Base Flood Elevation is the water surface elevation of the 1% annual chance flood.

ZONE A No Base Flood Elevation determined.
ZONE AE Base Flood Elevation determined.
ZONE AH Flood depths of 1 to 3 feet (usually areas of ponding); Base Flood Elevation determined.
ZONE AO Flood depths of 1 to 3 feet (usually shear flow on sloping terrain); average depths determined. For areas of alluvial fan flooding, velocities also determined.
ZONE AR Special Flood Hazard Area formerly protected from the 1% annual chance flood by a flood control system that was subsequently destroyed. Zone AR indicates that the former flood control system is being restored to provide protection from the 1% annual chance or greater flood.
ZONE ASB Area to be protected from 1% annual chance flood by a Federal Flood protection system under construction; no Base Flood Elevation determined.
ZONE V Coastal flood zone with velocity hazard (wave action); no Base Flood Elevation determined.
ZONE VE Coastal flood zone with velocity hazard (wave action); Base Flood Elevation determined.

FLOODWAY AREAS IN ZONE AE

The floodway is the channel of a stream plus any adjacent floodplain areas that must be kept free of encroachment so that the 1% annual chance flood can be carried without substantial increases in flood heights.

OTHER FLOOD AREAS

ZONE X Areas of 0.2% annual chance flood; areas of 1% annual chance flood with average depths of less than 1 foot or with average areas less than 1 square mile, and areas protected by levees from 1% annual chance flood.
ZONE X Areas determined to be outside the 0.2% annual chance floodplain. Areas in which flood hazards are undetermined, but possible.
ZONE D Areas determined to be outside the 0.2% annual chance floodplain. Areas in which flood hazards are undetermined, but possible.

COASTAL BARRIER RESOURCES SYSTEM (CBRS) AREAS

OTHERWISE PROTECTED AREAS (OPAs)

CBRS areas and OPAs are normally isolated within or adjacent to Special Flood Hazard Areas.

Floodplain boundary
 Floodway boundary
 Zone D boundary
 CBRS and OPA boundary

Boundary dividing Special Flood Hazard Areas of different Base Flood Elevations, flood depths or flood velocities
 Base Flood Elevation line and value, elevation in feet
 Base Flood Elevation value where uniform within zone; elevation in feet

1' referenced to the North American Vertical Datum of 1988 (NAVD 88)

○ A ○ A Cross section line
 (23) (23) Transect line
 11° 07' 30.00" 32° 22' 30.00" Geographic coordinates referenced to the North American Datum of 1983 (NAD 83)
 4759°N 1000-meter Universal Transverse Mercator grid ticks, zone 13
 8000000 FT 5000-foot grid ticks; Colorado State Plane coordinate system, central zone 10 (EPSG:9802), Lambert Conformal Conic Projection
 DX5510 Bench mark (see explanation in Notes to Users section of the FIRM panel)
 ● M1.5 River Mile

MAP REPOSITORIES
 Refer to Map Repository list on Map Index

EFFECTIVE DATE OF COUNTRYWIDE FLOOD INSURANCE RATE MAP
 MARCH 17, 1997

EFFECTIVE DATE(S) OF REVISION(S) TO THIS PANEL
 DECEMBER 7, 2018 To update corporate limits, to change Base Flood Elevations and Special Flood Hazard Areas, to update map format, to add roads and road names, and to incorporate previously issued Letters of Map Revision.

For community map revision history prior to countywide mapping, refer to the Community Map History Table located in the Flood Insurance Study report for this jurisdiction.

To determine if flood insurance is available in this community, contact your insurance agent or call the National Flood Insurance Program at 1-800-638-6620.

MAP SCALE 1" = 500'

0 250 500 1000 FEET
 0 150 300 METERS

NFP NATIONAL FLOOD INSURANCE PROGRAM

PANEL 0552G

FIRM FLOOD INSURANCE RATE MAP EL PASO COUNTY, COLORADO AND INCORPORATED AREAS

PANEL 552 OF 1300
 (SEE MAP INDEX FOR FIRM PANEL LAYOUT)

CONTAINS:
 COMMUNITY NUMBER PANEL SUFFIX
 EL PASO COUNTY 0552 100 0

Notice to User: The Map Number shown below should be used only during map sales. The Community Number shown above should be used on insurance applications for the highest community.

MAP NUMBER 08041C0552G

MAP REVISED DECEMBER 7, 2018
 Federal Emergency Management Agency



NOAA Atlas 14, Volume 8, Version 2
Location name: Elbert, Colorado, USA*
Latitude: 38.9796°, Longitude: -104.5696°
Elevation: 6996 ft**



* source: ESRI Maps
 ** source: USGS

POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Deborah Martin, Sandra Pavlovic, Ishani Roy, Michael St. Laurent, Carl Trypaluk, Dale Unruh, Michael Yekta, Geoffrey Bonnin

NOAA, National Weather Service, Silver Spring, Maryland

[PF tabular](#) | [PF graphical](#) | [Maps & aerals](#)

PF tabular

| PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches)¹ | | | | | | | | | | |
|--|--|-------------------------------|-------------------------------|-------------------------------|-------------------------------|-------------------------------|------------------------------|------------------------------|-----------------------------|-----------------------------|
| Duration | Average recurrence interval (years) | | | | | | | | | |
| | 1 | 2 | 5 | 10 | 25 | 50 | 100 | 200 | 500 | 1000 |
| 5-min | 0.239 (0.189-0.303) | 0.291 (0.231-0.370) | 0.381 (0.301-0.486) | 0.461 (0.361-0.589) | 0.576 (0.440-0.768) | 0.671 (0.499-0.904) | 0.770 (0.554-1.06) | 0.875 (0.604-1.24) | 1.02 (0.678-1.48) | 1.14 (0.733-1.67) |
| 10-min | 0.350 (0.277-0.444) | 0.426 (0.338-0.542) | 0.558 (0.441-0.711) | 0.674 (0.529-0.863) | 0.844 (0.644-1.12) | 0.982 (0.731-1.32) | 1.13 (0.811-1.56) | 1.28 (0.884-1.81) | 1.49 (0.992-2.17) | 1.66 (1.07-2.44) |
| 15-min | 0.426 (0.338-0.541) | 0.520 (0.412-0.660) | 0.681 (0.537-0.867) | 0.823 (0.645-1.05) | 1.03 (0.785-1.37) | 1.20 (0.891-1.62) | 1.37 (0.988-1.90) | 1.56 (1.08-2.21) | 1.82 (1.21-2.65) | 2.03 (1.31-2.98) |
| 30-min | 0.608 (0.482-0.771) | 0.740 (0.586-0.940) | 0.968 (0.764-1.23) | 1.17 (0.916-1.49) | 1.46 (1.11-1.94) | 1.70 (1.26-2.28) | 1.94 (1.40-2.68) | 2.20 (1.52-3.12) | 2.57 (1.71-3.73) | 2.86 (1.84-4.19) |
| 60-min | 0.775 (0.615-0.984) | 0.933 (0.739-1.18) | 1.21 (0.956-1.54) | 1.46 (1.15-1.87) | 1.84 (1.41-2.47) | 2.16 (1.61-2.92) | 2.49 (1.80-3.45) | 2.85 (1.97-4.05) | 3.37 (2.24-4.90) | 3.78 (2.44-5.54) |
| 2-hr | 0.943 (0.754-1.19) | 1.12 (0.898-1.42) | 1.46 (1.16-1.84) | 1.76 (1.39-2.23) | 2.22 (1.72-2.97) | 2.62 (1.97-3.52) | 3.04 (2.21-4.19) | 3.50 (2.45-4.95) | 4.16 (2.80-6.03) | 4.70 (3.06-6.85) |
| 3-hr | 1.03 (0.829-1.29) | 1.22 (0.978-1.53) | 1.57 (1.25-1.97) | 1.90 (1.51-2.40) | 2.41 (1.88-3.22) | 2.86 (2.17-3.84) | 3.34 (2.45-4.60) | 3.88 (2.73-5.48) | 4.66 (3.15-6.74) | 5.29 (3.46-7.69) |
| 6-hr | 1.20 (0.968-1.48) | 1.40 (1.13-1.74) | 1.78 (1.44-2.22) | 2.16 (1.73-2.70) | 2.76 (2.18-3.66) | 3.28 (2.52-4.39) | 3.86 (2.86-5.29) | 4.51 (3.20-6.34) | 5.46 (3.73-7.86) | 6.24 (4.12-9.01) |
| 12-hr | 1.38 (1.13-1.70) | 1.61 (1.31-1.98) | 2.05 (1.66-2.53) | 2.48 (2.00-3.07) | 3.15 (2.51-4.15) | 3.74 (2.89-4.96) | 4.39 (3.28-5.96) | 5.12 (3.66-7.13) | 6.17 (4.25-8.82) | 7.04 (4.69-10.1) |
| 24-hr | 1.60 (1.31-1.95) | 1.87 (1.54-2.28) | 2.38 (1.94-2.91) | 2.85 (2.32-3.51) | 3.60 (2.88-4.67) | 4.24 (3.29-5.56) | 4.94 (3.71-6.63) | 5.71 (4.12-7.87) | 6.82 (4.73-9.66) | 7.73 (5.20-11.0) |
| 2-day | 1.85 (1.54-2.24) | 2.18 (1.80-2.63) | 2.76 (2.28-3.34) | 3.29 (2.70-4.01) | 4.11 (3.30-5.27) | 4.80 (3.76-6.22) | 5.54 (4.19-7.36) | 6.35 (4.62-8.68) | 7.50 (5.25-10.5) | 8.44 (5.73-11.9) |
| 3-day | 2.03 (1.69-2.44) | 2.39 (1.98-2.87) | 3.02 (2.50-3.64) | 3.60 (2.97-4.36) | 4.47 (3.60-5.69) | 5.20 (4.08-6.70) | 5.98 (4.55-7.90) | 6.83 (4.99-9.28) | 8.03 (5.65-11.2) | 9.00 (6.15-12.7) |
| 4-day | 2.18 (1.82-2.61) | 2.56 (2.13-3.06) | 3.22 (2.68-3.87) | 3.82 (3.16-4.62) | 4.73 (3.83-6.00) | 5.49 (4.33-7.04) | 6.30 (4.81-8.30) | 7.18 (5.26-9.72) | 8.43 (5.94-11.7) | 9.43 (6.46-13.3) |
| 7-day | 2.58 (2.17-3.07) | 2.98 (2.50-3.54) | 3.68 (3.08-4.39) | 4.32 (3.60-5.18) | 5.29 (4.30-6.65) | 6.09 (4.84-7.76) | 6.96 (5.34-9.09) | 7.89 (5.82-10.6) | 9.21 (6.55-12.8) | 10.3 (7.10-14.4) |
| 10-day | 2.93 (2.48-3.47) | 3.36 (2.84-3.98) | 4.13 (3.47-4.90) | 4.81 (4.02-5.74) | 5.83 (4.76-7.28) | 6.68 (5.32-8.45) | 7.58 (5.85-9.86) | 8.55 (6.34-11.4) | 9.92 (7.08-13.7) | 11.0 (7.65-15.4) |
| 20-day | 3.91 (3.33-4.58) | 4.51 (3.84-5.29) | 5.52 (4.68-6.50) | 6.39 (5.39-7.55) | 7.63 (6.25-9.37) | 8.62 (6.90-10.8) | 9.64 (7.47-12.4) | 10.7 (7.98-14.1) | 12.2 (8.74-16.6) | 13.3 (9.31-18.4) |
| 30-day | 4.70 (4.02-5.47) | 5.44 (4.65-6.34) | 6.65 (5.66-7.78) | 7.66 (6.49-9.00) | 9.06 (7.44-11.0) | 10.1 (8.15-12.5) | 11.2 (8.74-14.3) | 12.3 (9.24-16.2) | 13.8 (9.98-18.7) | 15.0 (10.5-20.6) |
| 45-day | 5.67 (4.88-6.57) | 6.55 (5.63-7.60) | 7.97 (6.82-9.27) | 9.12 (7.77-10.7) | 10.7 (8.79-12.9) | 11.9 (9.56-14.5) | 13.0 (10.2-16.4) | 14.2 (10.6-18.4) | 15.6 (11.3-21.0) | 16.7 (11.9-23.0) |
| 60-day | 6.48 (5.60-7.48) | 7.46 (6.43-8.62) | 9.01 (7.74-10.4) | 10.3 (8.77-11.9) | 11.9 (9.82-14.3) | 13.1 (10.6-16.0) | 14.3 (11.2-18.0) | 15.5 (11.7-20.0) | 16.9 (12.3-22.6) | 18.0 (12.8-24.6) |

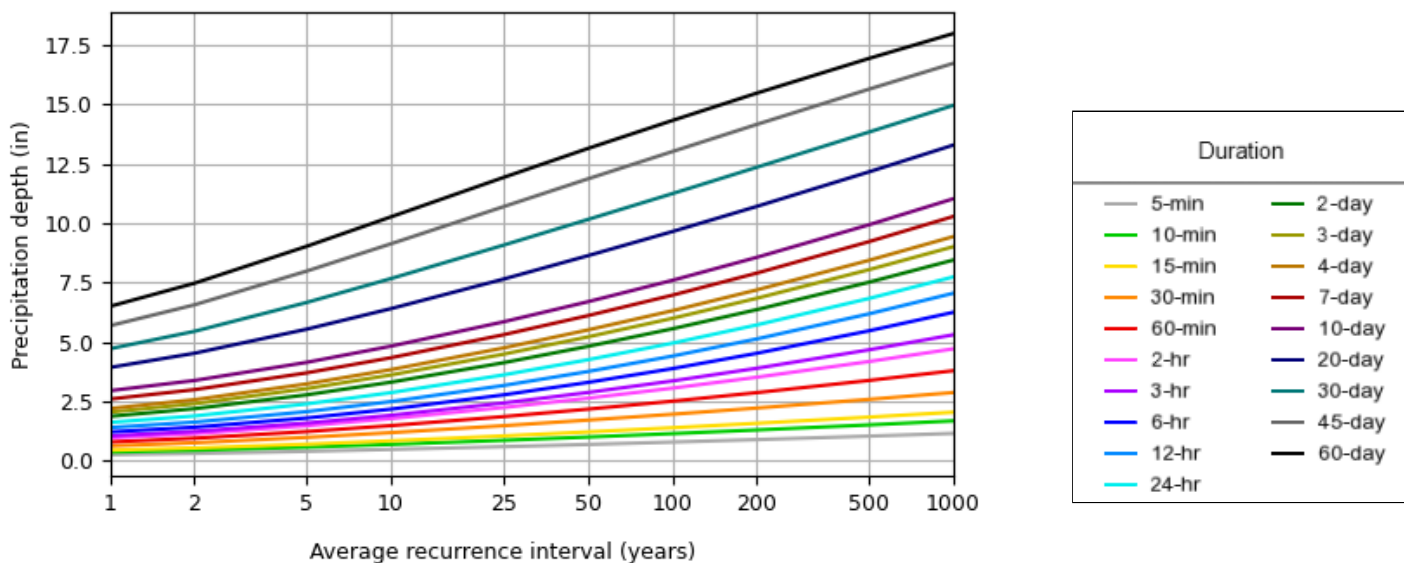
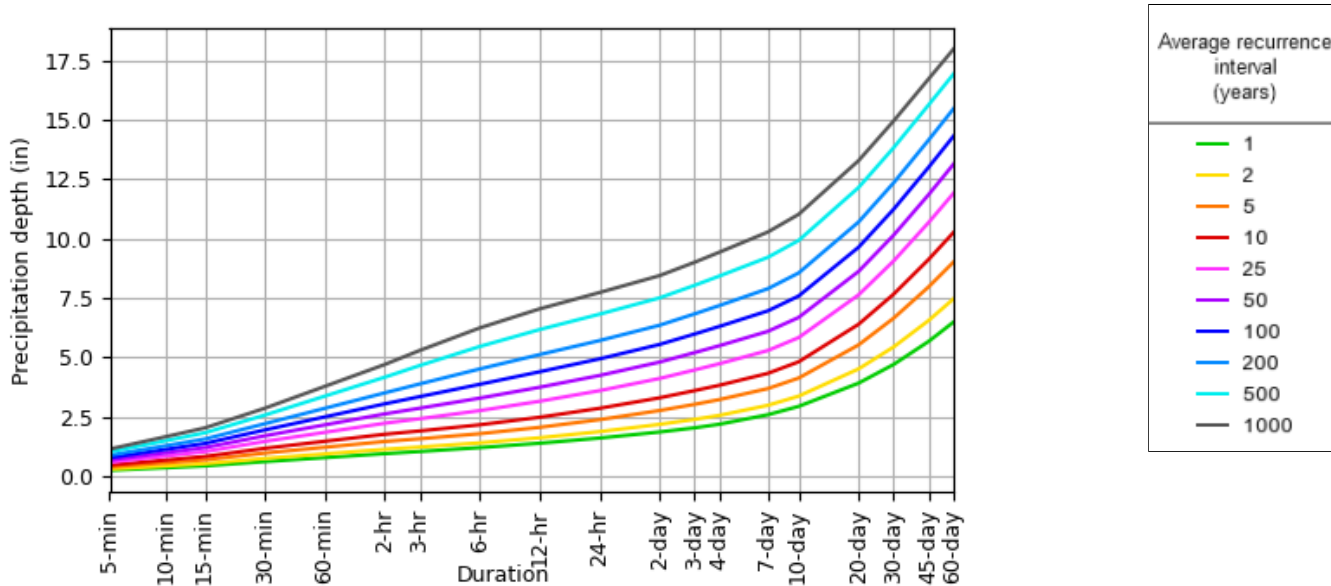
¹ Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS). Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values. Please refer to NOAA Atlas 14 document for more information.

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PF graphical

PDS-based depth-duration-frequency (DDF) curves

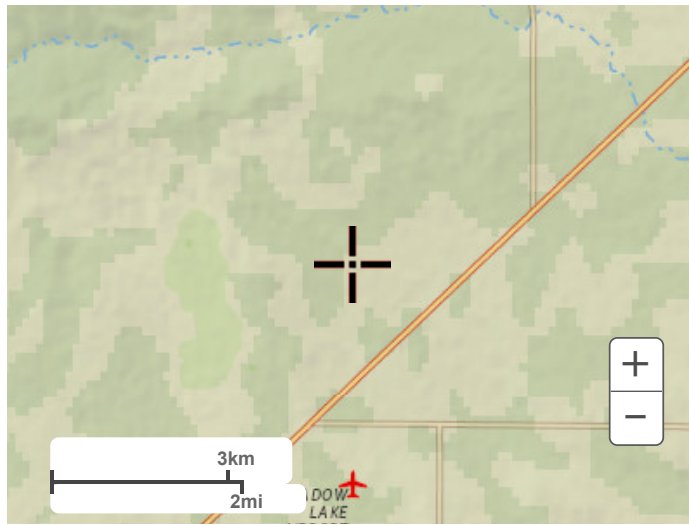
Latitude: 38.9796°, Longitude: -104.5696°



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Maps & aerials

Small scale terrain



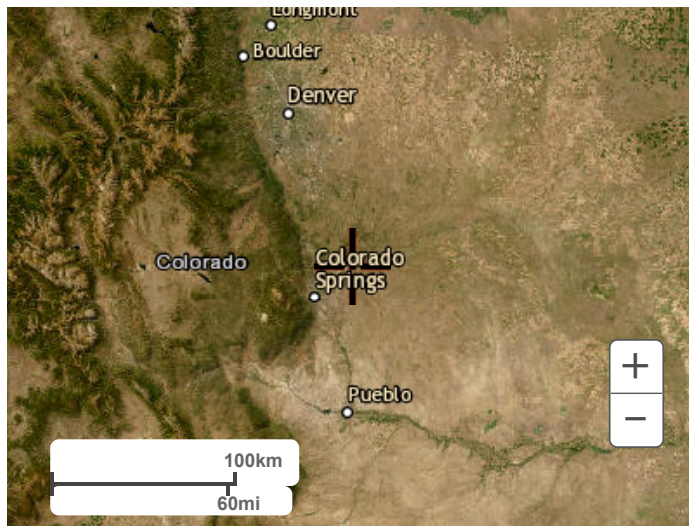
Large scale terrain



Large scale map



Large scale aerial




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[National Water Center](#)
1325 East West Highway
Silver Spring, MD 20910
Questions?: HDSC.Questions@noaa.gov

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APPENDIX B – HYDROLOGIC CALCULATIONS

please rotate

| | | | |
|---|----------------------------|-------------|-----------------|
|  HRGreen | EASTONVILLE ROAD | Calc'd by: | SPC |
| | EXISTING CONDITIONS | Checked by: | CM |
| | EL PASO COUNTY, CO | Date: | 3/1/2024 |

| BASIN | AREA (ac) | % IMPERVIOUS | Q _s (cfs) | Q ₁₀₀ (cfs) |
|-------|-----------|--------------|----------------------|------------------------|
| E1 | 0.47 | 46 | 0.7 | 1.7 |
| E2 | 1.25 | 18 | 1.0 | 3.5 |
| E3 | 0.47 | 58 | 1.0 | 2.1 |
| E4 | 1.67 | 20 | 1.4 | 4.6 |
| E5 | 0.23 | 45 | 0.5 | 1.1 |
| E6 | 0.21 | 49 | 0.5 | 1.1 |
| E7 | 0.23 | 45 | 0.5 | 1.2 |
| E8 | 0.18 | 56 | 0.4 | 0.9 |
| E9 | 0.72 | 46 | 1.2 | 2.7 |
| E10 | 0.72 | 50 | 1.3 | 2.8 |
| OS1 | 1.58 | 2 | 0.5 | 3.6 |
| OS2 | 12.21 | 2 | 3.6 | 24.3 |
| OS3.1 | 1.51 | 2 | 0.5 | 3.6 |
| OS3.2 | 2.86 | 2 | 1.0 | 6.6 |
| OS3.3 | 21.12 | 2 | 6.4 | 42.7 |


| DESIGN POINT | CONTRIBUTING BASINS | ΣQ _s (cfs) | ΣQ ₁₀₀ (cfs) |
|--------------|---------------------|-----------------------|-------------------------|
| 1 | E1,OS1 | 1.2 | 4.9 |
| 2 | E2,DP1 | 2.1 | 8.2 |
| 3 | E3,OS2 | 4.5 | 26.1 |
| 4 | DP3,E4 | 5.8 | 30.4 |
| 5 | E5,OS3.1 | 0.9 | 4.5 |
| 6 | DP5,E6 | 1.3 | 5.4 |
| 7.1 | E7,OS3.2 | 1.4 | 7.5 |
| 8.1 | DP7.1,E8 | 1.7 | 8.2 |
| 7.2 | OS3.3,E9 | 7.4 | 45.3 |
| 8.2 | DP7.2,E10 | 8.6 | 47.7 |

| | |
|--|----------------------------|
|  | EASTONVILLE ROAD |
| | EXISTING CONDITIONS |
| | EL PASO COUNTY, CO |

| | |
|--------------------|-------------------|
| Calc'd by: | SPC |
| Checked by: | |
| Date: | 11/27/2023 |

| | |
|-------------------|--------------------|
| SOIL TYPE: | HSG A&B |
|-------------------|--------------------|

| COMPOSITE 'C' FACTORS | | | | | | | | | | | | | | | | | | | |
|------------------------------|----------------------|----------------------|------------------------|---|----------------------|------------------------|---------------------------|----------------------|------------------------|---------------------------|----------------------|------------------------|---------------------------|----------------------|------------------------|--------------|--|--|--|
| BASIN | LAND USE TYPE | | | | | | | | | | | | | | | TOTAL | COMPOSITE IMPERVIOUSNESS & C FACTOR | | |
| | Paved | | | Historic Flow Analysis-- Greenbelts, Agriculture | | | Land Use Undefined | | | Land Use Undefined | | | Land Use Undefined | | | | | | |
| | %I | C₅ | C₁₀₀ | %I | C₅ | C₁₀₀ | %I | C₅ | C₁₀₀ | %I | C₅ | C₁₀₀ | %I | C₅ | C₁₀₀ | | | | |
| | 100 | 0.90 | 0.96 | 2 | 0.09 | 0.36 | 0 | 0.00 | 0.00 | 0 | 0.00 | 0.00 | 0 | 0.00 | 0.00 | | | | |
| ACRES | ACRES | | ACRES | | | ACRES | | | ACRES | | | ACRES | %I | C₅ | C₁₀₀ | | | | |
| E1 | 0.21 | 0.26 | | | | | | | | | | | 0.47 | 46 | 0.45 | 0.63 | | | |
| E2 | 0.20 | 1.05 | | | | | | | | | | | 1.25 | 18 | 0.22 | 0.46 | | | |
| E3 | 0.27 | 0.20 | | | | | | | | | | | 0.47 | 58 | 0.56 | 0.70 | | | |
| E4 | 0.31 | 1.36 | | | | | | | | | | | 1.67 | 20 | 0.24 | 0.47 | | | |
| E5 | 0.10 | 0.13 | | | | | | | | | | | 0.23 | 45 | 0.44 | 0.62 | | | |
| E6 | 0.10 | 0.11 | | | | | | | | | | | 0.21 | 49 | 0.48 | 0.65 | | | |
| E7 | 0.10 | 0.13 | | | | | | | | | | | 0.23 | 45 | 0.44 | 0.62 | | | |
| E8 | 0.10 | 0.08 | | | | | | | | | | | 0.18 | 56 | 0.54 | 0.69 | | | |
| E9 | 0.32 | 0.40 | | | | | | | | | | | 0.72 | 46 | 0.45 | 0.63 | | | |
| E10 | 0.35 | 0.37 | | | | | | | | | | | 0.72 | 50 | 0.48 | 0.65 | | | |
| OS1 | | 1.58 | | | | | | | | | | | 1.58 | 2 | 0.09 | 0.36 | | | |
| OS2 | | 12.21 | | | | | | | | | | | 12.21 | 2 | 0.09 | 0.36 | | | |
| OS3.1 | | 1.51 | | | | | | | | | | | 1.51 | 2 | 0.09 | 0.36 | | | |
| OS3.2 | | 2.86 | | | | | | | | | | | 2.86 | 2 | 0.09 | 0.36 | | | |
| OS3.3 | | 21.12 | | | | | | | | | | | 21.12 | 2 | 0.09 | 0.36 | | | |

| | | | |
|---|----------------------------|--------------------|------------------|
|  | EASTONVILLE ROAD | Calc'd by: | SPC |
| | EXISTING CONDITIONS | Checked by: | |
| | EL PASO COUNTY, CO | Date: | 3/11/2024 |

TIME OF CONCENTRATION

| BASIN DATA | | | OVERLAND TIME (T _i) | | | TRAVEL TIME (T _t) | | | | | TOTAL |
|-------------|----------------|-----------|---------------------------------|---------|----------------------|-------------------------------|-------------|---------|----------|----------------------|----------------------|
| DESIGNATION | C _s | AREA (ac) | LENGTH (ft) | SLOPE % | t _i (min) | C _v | LENGTH (ft) | SLOPE % | V (ft/s) | t _t (min) | t _c (min) |
| E1 | 0.45 | 0.47 | 117 | 11.6 | 5.7 | 10 | 1162 | 3.4 | 1.8 | 10.5 | 16.2 |
| E2 | 0.22 | 1.25 | 87 | 2.4 | 11.2 | 10 | 518 | 1.7 | 1.3 | 6.6 | 17.9 |
| E3 | 0.56 | 0.47 | 40 | 2.0 | 5.0 | 10 | 794 | 2.5 | 1.6 | 8.4 | 13.4 |
| E4 | 0.24 | 1.67 | 113 | 5.5 | 9.5 | 10 | 830 | 2.5 | 1.6 | 8.7 | 18.2 |
| E5 | 0.44 | 0.23 | 30 | 13.8 | 2.8 | 10 | 310 | 1.4 | 1.2 | 4.4 | 7.1 |
| E6 | 0.48 | 0.21 | 30 | 13.8 | 2.6 | 10 | 310 | 1.4 | 1.2 | 4.4 | 7.0 |
| E7 | 0.44 | 0.23 | 35 | 25.0 | 2.4 | 10 | 161 | 0.6 | 0.8 | 3.5 | 5.9 |
| E8 | 0.54 | 0.18 | 25 | 1.0 | 5.1 | 10 | 161 | 0.6 | 0.8 | 3.5 | 8.6 |
| E9 | 0.45 | 0.72 | 30 | 2.0 | 5.2 | 10 | 711 | 0.5 | 0.7 | 16.8 | 21.9 |
| E10 | 0.48 | 0.72 | 30 | 2.0 | 4.9 | 10 | 711 | 0.5 | 0.7 | 16.8 | 21.7 |
| OS1 | 0.09 | 1.58 | 300 | 2.8 | 22.8 | 10 | 213 | 4.5 | 2.1 | 1.7 | 24.4 |
| OS2 | 0.09 | 12.21 | 300 | 4.1 | 20.0 | 10 | 1042 | 3.4 | 1.8 | 9.4 | 29.5 |
| OS3.1 | 0.09 | 1.51 | 136 | 3.9 | 13.7 | 10 | 150 | 8.9 | 3.0 | 0.8 | 14.6 |
| OS3.2 | 0.09 | 2.86 | 174 | 8.6 | 11.9 | 10 | 267 | 4.4 | 2.1 | 2.1 | 14.0 |
| OS3.3 | 0.09 | 21.12 | 300 | 6.0 | 17.7 | 10 | 930 | 3.4 | 1.8 | 8.4 | 26.1 |

FORMULAS:

$$t_i = \frac{0.395(1.1 - C_s)\sqrt{L}}{S^{0.33}} \quad V = C_v S_w^{0.5}$$

Table 6-7. Conveyance Coefficient, C_v

| Type of Land Surface | C _v |
|--------------------------------------|----------------|
| Heavy meadow | 2.5 |
| Tillage/field | 5 |
| Riprap (not buried)* | 6.5 |
| Short pasture and lawns | 7 |
| Nearly bare ground | 10 |
| Grassed waterway | 15 |
| Paved areas and shallow paved swales | 20 |

*For buried riprap, select C_v value based on type of vegetative cover.



EASTONVILLE ROAD
EXISTING CONDITIONS
DESIGN STORM: 5-YEAR

Calc'd by:
 Checked by:
 Date:

SPC

3/11/2024

| STREET | DESIGN POINT | BASIN ID | DIRECT RUNOFF | | | | | | TOTAL RUNOFF | | | | STREET | | | PIPE | | | | TRAVEL TIME | | | REMARKS |
|--------|--------------|----------|---------------|----------------|----------------------|------------------------|-------------|---------|----------------------|------------------------|-------------|---------|---------------------------|------------------------|---------|-------------------------|------------------------|---------|----------------|-------------|------------|---|-------------------------|
| | | | AREA (ac) | C _s | f _c (min) | C ₅ *A (ac) | f (in./hr.) | Q (cfs) | f _c (min) | C ₅ *A (ac) | f (in./hr.) | Q (cfs) | Q _{street} (cfs) | C ₅ *A (ac) | SLOPE % | Q _{pipe} (cfs) | C ₅ *A (ac) | SLOPE % | PIPE SIZE (ft) | LENGTH (FT) | VEL. (FPS) | TRAVEL TIME (min) | |
| | | E1 | 0.47 | 0.45 | 16.2 | 0.21 | 3.41 | 0.7 | | | | | | | | | | | | | | | BASIN E1 CAPTURED @ DP1 |
| | 1 | OS1 | 1.58 | 0.09 | 12.9 | 0.14 | 3.75 | 0.5 | 16.2 | 0.35 | 3.41 | 1.2 | | | 1.2 | 0.35 | 0.6 | 3.0 | 73 | 7.5 | 0.16 | BASIN E1 AND OS1 COMBINE @ DP1 CAPTURED IN 36" CMP CULVERT, PIPED TO BASIN E2 | |
| | 2 | E2 | 1.25 | 0.22 | 13.4 | 0.27 | 3.69 | 1.0 | 16.3 | 0.63 | 3.39 | 2.1 | | | | | | | | | | FLOW @ DP2 CONVEYED OFFSITE | |
| | | E3 | 0.47 | 0.56 | 13.4 | 0.26 | 3.69 | 1.0 | | | | | | | | | | | | | | BASIN E3 CAPTURED @ DP3 | |
| | 3 | OS2 | 12.21 | 0.09 | 17.5 | 1.10 | 3.29 | 3.6 | 17.5 | 1.36 | 3.29 | 4.5 | | | 4.5 | 1.36 | 1.1 | 2.0 | 47 | 7.6 | 0.10 | BASIN E3 AND OS2 COMBINE @ DP3 CAPTURED IN 24" CMP CULVERT, PIPED TO BASIN E4 | |
| | 4 | E4 | 1.67 | 0.24 | 15.2 | 0.40 | 3.50 | 1.4 | 17.6 | 1.76 | 3.28 | 5.8 | | | | | | | | | | FLOW @ DP4 CONVEYED OFFSITE | |
| | | E5 | 0.23 | 0.44 | 7.1 | 0.10 | 4.64 | 0.5 | | | | | | | | | | | | | | BASIN E5 CAPTURED @ DP5 | |
| | 5 | OS3.1 | 1.51 | 0.09 | 11.6 | 0.14 | 3.91 | 0.5 | 11.6 | 0.24 | 3.91 | 0.9 | | | 0.9 | 0.24 | 1.3 | 1.5 | 56 | 6.8 | 0.14 | BASIN E5 AND OS3 COMBINE @ DP5 CAPTURED IN 18" CMP CULVERT, PIPED TO BASIN E6 | |
| | 6 | E6 | 0.21 | 0.48 | 7.0 | 0.10 | 4.67 | 0.5 | 11.7 | 0.34 | 3.89 | 1.3 | | | | | | | | | | FLOW @ DP6 CONVEYED OFFSITE | |
| | | E7 | 0.23 | 0.44 | 5.9 | 0.10 | 4.92 | 0.5 | | | | | | | | | | | | | | BASIN E7 CAPTURED @ DP7 | |
| | 7.1 | OS3.2 | 2.86 | 0.09 | 12.5 | 0.26 | 3.80 | 1.0 | 12.5 | 0.36 | 3.80 | 1.4 | | | 1.4 | 0.36 | 0.2 | 1.5 | 53 | 2.3 | 0.38 | BASIN E7 AND OS4.1 COMBINE @ DP7.1 CAPTURED IN 18" CMP CULVERT, PIPED TO BASIN E8 | |
| | 8.1 | E8 | 0.18 | 0.54 | 8.6 | 0.10 | 4.36 | 0.4 | 12.8 | 0.46 | 3.75 | 1.7 | | | | | | | | | | FLOW @ DP8.1 CONVEYED OFFSITE | |
| | | E9 | 0.72 | 0.45 | 14.1 | 0.32 | 3.61 | 1.2 | | | | | | | | | | | | | | BASIN E9 CAPTURED @ DP7.2 | |
| | 7.2 | OS3.3 | 21.12 | 0.09 | 16.8 | 1.90 | 3.35 | 6.4 | 16.8 | 2.22 | 3.35 | 7.4 | | | 7.4 | 2.22 | 0.8 | 1.5 | 43 | 5.3 | 0.13 | BASIN E9 AND OS 4.2 COMBINE @ DP7.2 CAPTURED IN 18" CMP CULVERT, PIPED TO BASIN E10 | |
| | 8.2 | E10 | 0.72 | 0.48 | 14.1 | 0.35 | 3.61 | 1.3 | 17.0 | 2.57 | 3.34 | 8.6 | | | | | | | | | | FLOW @ DP8.2 CONVEYED OFFSITE | |



EASTONVILLE ROAD
EXISTING CONDITIONS
DESIGN STORM: 100-YEAR

Calc'd by: **SPC**
 Checked by:
 Date: **3/11/2024**

| STREET | DESIGN POINT | BASIN ID | DIRECT RUNOFF | | | | | | | TOTAL RUNOFF | | | | STREET | | | PIPE | | | | TRAVEL TIME | | | REMARKS |
|--------|--------------|----------|---------------|------------------|----------------------|--------------------------|-------------|---------|----------------------|--------------------------|-------------|---------|---------------------------|--------------------------|---------|-------------------------|--------------------------|---------|----------------|-------------|-------------|---|-------------------------|---------|
| | | | AREA (ac) | C ₁₀₀ | t _c (min) | C ₁₀₀ *A (ac) | I (in./hr.) | Q (cfs) | t _c (min) | C ₁₀₀ *A (ac) | I (in./hr.) | Q (cfs) | Q _{street} (cfs) | C ₁₀₀ *A (ac) | SLOPE % | Q _{PIPE} (cfs) | C ₁₀₀ *A (ac) | SLOPE % | PIPE SIZE (ft) | LENGTH (ft) | VEL. (ft/s) | TRAVEL TIME (min) | | |
| | | E1 | 0.47 | 0.63 | 16.2 | 0.30 | 5.72 | 1.7 | | | | | | | | | | | | | | | BASIN E1 CAPTURED @ DP1 | |
| | 1 | OS1 | 1.58 | 0.36 | 12.9 | 0.57 | 6.30 | 3.6 | 16.2 | 0.86 | 5.72 | 4.9 | | 4.9 | 0.86 | 0.6 | 3.0 | 73 | 7.5 | 0.16 | | BASIN E1 AND OS1 COMBINE @ DP1 CAPTURED IN 36" CMP CULVERT, PIPED TO BASIN E2 | | |
| | 2 | E2 | 1.25 | 0.46 | 13.4 | 0.57 | 6.20 | 3.5 | 16.3 | 1.43 | 5.69 | 8.2 | | | | | | | | | | FLOW @ DP2 CONVEYED OFFSITE | | |
| | | E3 | 0.47 | 0.70 | 13.4 | 0.33 | 6.20 | 2.1 | | | | | | 26.1 | 4.73 | 1.1 | 2.0 | 47 | 7.6 | 0.10 | | BASIN E3 CAPTURED @ DP3 | | |
| | 3 | OS2 | 12.21 | 0.36 | 17.5 | 4.40 | 5.53 | 24.3 | 17.5 | 4.73 | 5.53 | 26.1 | | | | | | | | | | BASIN E3 AND OS2 COMBINE @ DP3 CAPTURED IN 24" CMP CULVERT, PIPED TO BASIN E4 | | |
| | 4 | E4 | 1.67 | 0.47 | 15.2 | 0.79 | 5.87 | 4.6 | 17.6 | 5.51 | 5.51 | 30.4 | | | | | | | | | | FLOW @ DP4 CONVEYED OFFSITE | | |
| | | E5 | 0.23 | 0.62 | 7.1 | 0.14 | 7.79 | 1.1 | | | | | | | | | | | | | | BASIN E5 CAPTURED @ DP5 | | |
| | 5 | OS3.1 | 1.51 | 0.36 | 11.6 | 0.54 | 6.56 | 3.6 | 11.6 | 0.69 | 6.56 | 4.5 | | 4.5 | 0.69 | 1.3 | 1.5 | 56 | 6.8 | 0.14 | | BASIN E5 AND OS3 COMBINE @ DP5 CAPTURED IN 18" CMP CULVERT, PIPED TO BASIN E6 | | |
| | 6 | E6 | 0.21 | 0.65 | 7.0 | 0.14 | 7.84 | 1.1 | 11.7 | 0.82 | 6.53 | 5.4 | | | | | | | | | | FLOW @ DP6 CONVEYED OFFSITE | | |
| | | E7 | 0.23 | 0.62 | 5.9 | 0.14 | 8.26 | 1.2 | | | | | | | | | | | | | | BASIN E7 CAPTURED @ DP7 | | |
| | 7.1 | OS3.2 | 2.86 | 0.36 | 12.5 | 1.03 | 6.38 | 6.6 | 12.5 | 1.17 | 6.38 | 7.5 | | 7.5 | 1.17 | 0.2 | 1.5 | 53 | 2.3 | 0.38 | | BASIN E7 AND OS4.1 COMBINE @ DP7.1 CAPTURED IN 18" CMP CULVERT, PIPED TO BASIN E8 | | |
| | 8.1 | E8 | 0.18 | 0.69 | 8.6 | 0.12 | 7.31 | 0.9 | 12.8 | 1.30 | 6.30 | 8.2 | | | | | | | | | | FLOW @ DP8.1 CONVEYED OFFSITE | | |
| | | E9 | 0.72 | 0.63 | 14.1 | 0.45 | 6.06 | 2.7 | | | | | | | | | | | | | | BASIN E9 CAPTURED @ DP7.2 | | |
| | 7.2 | OS3.3 | 21.12 | 0.36 | 16.8 | 7.60 | 5.62 | 42.7 | 16.8 | 8.05 | 5.62 | 45.3 | | 45.3 | 8.05 | 0.8 | 1.5 | 43 | 5.3 | 0.13 | | BASIN E9 AND OS 4.2 COMBINE @ DP7.2 CAPTURED IN 18" CMP CULVERT, PIPED TO BASIN E10 | | |
| | 8.2 | E10 | 0.72 | 0.65 | 14.1 | 0.47 | 6.06 | 2.8 | 17.0 | 8.52 | 5.60 | 47.7 | | | | | | | | | | FLOW @ DP8.2 CONVEYED OFFSITE | | |



**EASTONVILLE ROAD
PROPOSED CONDITIONS
EL PASO COUNTY, CO**

| | |
|--------------------|------------------|
| Calc'd by: | SPC |
| Checked by: | CM |
| Date: | 3/14/2024 |

Revise to SFB D for consistency.

| BASIN | AREA (ac) | % IMPERVIOUS | Q ₅ (cfs) | Q ₁₀₀ (cfs) |
|------------------------------|-----------|--------------|----------------------|------------------------|
| EA1 | 0.61 | 86 | 2.2 | 4.1 |
| EA2 | 1.23 | 44 | 2.2 | 5.3 |
| EA3 | 0.53 | 87 | 2.1 | 3.4 |
| EA4 | 0.90 | 52 | 2.0 | 3.4 |
| EA5 | 0.29 | 4 | 0.2 | 0.3 |
| EA6 | 1.11 | 88 | 3.0 | 5.1 |
| EA7 | 1.91 | 55 | 3.3 | 5.6 |
| EA8 | 0.86 | 50 | 0.5 | 0.8 |
| EA9 | 0.92 | 35 | 0.4 | 0.6 |
| EA10 | 0.37 | 23 | 0.2 | 0.3 |
| EA11 | 0.15 | 0 | 0.1 | 0.1 |
| EA12 | 0.26 | 10 | 0.2 | 0.8 |
| EA13 | 0.21 | 0 | 0.1 | 0.5 |
| EA8 & EA9 *Per Segment 2 FDR | 5.07 | 78 | 10.2 | 17.2 |
| OS1 | 1.63 | 2 | 0.5 | 3.6 |
| OS2 | 12.33 | 2 | 3.7 | 24.5 |
| OS3 | 25.36 | 2 | 7.9 | 53.3 |

| DESIGN POINT | CONTRIBUTING BASINS | ΣQ ₅ (cfs) | ΣQ ₁₀₀ (cfs) |
|--------------|------------------------------------|-----------------------|-------------------------|
| 1 | OS1 | 0.5 | 3.6 |
| 2 | OS1, Pond D Release | 0.9 | 5.0 |
| 3 | OS2 | 3.7 | 24.5 |
| 4 | OS2, POND A RELEASE | 4.0 | 25.7 |
| 7 | OS3 | 7.9 | 53.3 |
| 8 | OS3, POND B RELEASE | 8.3 | 54.3 |
| 9 | EA1 | 2.2 | 4.1 |
| 10 | DP9, EA2 | 4.2 | 9.0 |
| 11 | DP10, EA12 | 4.3 | 9.5 |
| 12 | EA13 | 0.1 | 0.5 |
| 13 | EA3 | 2.1 | 3.4 |
| 14 | DP13, EA4 | 3.9 | 6.5 |
| 15 | DP14, EA5 | 4.0 | 6.7 |
| 16 | EA6 | 3.0 | 5.1 |
| 17 | DP16, EA7 | 6.3 | 10.5 |
| 18 | DP17 | 6.3 | 10.5 |
| 19 | DP18, EA8 | 6.6 | 11.1 |
| 18U | DP17, EA8 & EA9 *PER SEGMENT 2 FDR | 15.6 | 26.2 |
| 19U | DP18, EA8 | 15.9 | 26.6 |
| 20 | EA9 | 0.4 | 0.6 |
| 21 | EA10 | 0.2 | 0.3 |
| 22 | EA11 | 0.1 | 0.1 |

Why is a separate DP needed for just another DP? Only need another design point if additional flows are being added.

Same basins/DPs being combined at DP's please delete duplicate

Explain what difference is between DP's 18/18U and 19/19U. Is a 19 and 19U both needed? They have the same flows/same basin.




EASTONVILLE ROAD
PROPOSED CONDITIONS
 EL PASO COUNTY, CO

Calc'd by: SPC
Checked by: CM
Date: 11/27/2023

SOIL TYPE: HSG A&B

| COMPOSITE 'C' FACTORS | | | | | | | | | | | | | | | | | | | |
|------------------------------|----------------------|----------------------|------------------------|--|----------------------|------------------------|--------------|----------------------|------------------------|---------------|----------------------|------------------------|---------------------------|----------------------|------------------------|--------------|--|----------------------|------------------------|
| BASIN | LAND USE TYPE | | | | | | | | | | | | | | | TOTAL | COMPOSITE IMPERVIOUSNESS & C FACTOR | | |
| | Paved | | | Historic Flow Analysis--Greenbelts, Agriculture | | | Lawns | | | Gravel | | | Land Use Undefined | | | | | | |
| | %I | C₅ | C₁₀₀ | %I | C₅ | C₁₀₀ | %I | C₅ | C₁₀₀ | %I | C₅ | C₁₀₀ | %I | C₅ | C₁₀₀ | | | | |
| | 100 | 0.90 | 0.96 | 2 | 0.09 | 0.36 | 0 | 0.08 | 0.35 | 80 | 0.59 | 0.70 | 0 | 0.00 | 0.00 | | | | |
| | ACRES | | | ACRES | | | ACRES | | | ACRES | | | ACRES | | | ACRES | %I | C₅ | C₁₀₀ |
| EA1 | 0.52 | | | | | | 0.09 | | | | | | | | | 0.61 | 86 | 0.78 | 0.87 |
| EA2 | 0.54 | | | | | | 0.69 | | | | | | | | | 1.23 | 44 | 0.44 | 0.62 |
| EA3 | 0.46 | | | | | | 0.07 | | | | | | | | | 0.53 | 87 | 0.79 | 0.88 |
| EA4 | 0.47 | | | | | | 0.43 | | | | | | | | | 0.90 | 52 | 0.51 | 0.67 |
| EA5 | | | | | | | 0.28 | | | 0.01 | | | | | | 0.29 | 4 | 0.11 | 0.37 |
| EA6 | 0.97 | | | | | | 0.14 | | | | | | | | | 1.11 | 88 | 0.80 | 0.88 |
| EA7 | 1.05 | | | | | | 0.86 | | | | | | | | | 1.91 | 55 | 0.53 | 0.69 |
| EA8 | | | | | | | 0.76 | | | 0.10 | | | | | | 0.86 | 9 | 0.14 | 0.39 |
| EA9 | | | | | | | 0.92 | | | | | | | | | 0.92 | 0 | 0.08 | 0.35 |
| EA10 | | | | | | | 0.37 | | | | | | | | | 0.37 | 0 | 0.08 | 0.35 |
| EA11 | | | | | | | 0.15 | | | | | | | | | 0.15 | 0 | 0.08 | 0.35 |
| EA12 | | | | | | | 0.23 | | | 0.03 | | | | | | 0.26 | 10 | 0.14 | 0.39 |
| EA13 | | | | | | | 0.21 | | | | | | | | | 0.21 | 0 | 0.08 | 0.35 |
| OS1 | | | | 1.63 | | | | | | | | | | | | 1.63 | 2 | 0.09 | 0.36 |
| OS2 | | | | 12.33 | | | | | | | | | | | | 12.33 | 2 | 0.09 | 0.36 |
| OS3 | | | | 25.36 | | | | | | | | | | | | 25.36 | 2 | 0.09 | 0.36 |
| EA8 & EA9 *Per Segment 2 FDR | 3.94 | | | | | | 1.13 | | | | | | | | | 5.07 | 78 | 0.72 | 0.82 |
| SFB A | 0.93 | | | 0.00 | | | 0.77 | | | 0.01 | | | 0.00 | | | 1.72 | 55 | | |
| EDB B | 2.02 | | | 0.00 | | | 1.76 | | | 0.10 | | | 0.00 | | | 3.88 | 54 | | |
| SFB D | 1.06 | | | 0.00 | | | 1.01 | | | 0.03 | | | 0.00 | | | 2.10 | 52 | | |

| | | | |
|---|----------------------------|--------------------|------------------|
|  | EASTONVILLE ROAD | Calc'd by: | SPC |
| | PROPOSED CONDITIONS | Checked by: | CM |
| | EL PASO COUNTY, CO | Date: | 3/14/2024 |

TIME OF CONCENTRATION

| BASIN DATA | | | OVERLAND TIME (T _i) | | | TRAVEL TIME (T _t) | | | | | TOTAL |
|------------------------------|----------------|-----------|---------------------------------|---------|----------------------|-------------------------------|-------------|---------|----------|----------------------|----------------------|
| DESIGNATION | C _s | AREA (ac) | LENGTH (ft) | SLOPE % | t _i (min) | C _v | LENGTH (ft) | SLOPE % | V (ft/s) | t _t (min) | t _c (min) |
| EA1 | 0.78 | 0.61 | 26 | 2.0 | 2.3 | 20 | 734 | 1.6 | 2.5 | 4.9 | 7.3 |
| EA2 | 0.44 | 1.23 | 26 | 2.0 | 4.9 | 20 | 734 | 1.6 | 2.5 | 4.9 | 9.8 |
| EA3 | 0.79 | 0.53 | 26 | 2.0 | 2.3 | 20 | 326 | 0.5 | 1.4 | 3.8 | 6.1 |
| EA4 | 0.51 | 0.90 | 26 | 2.0 | 4.4 | 20 | 326 | 0.5 | 1.4 | 3.8 | 8.2 |
| EA5 | 0.11 | 0.29 | 25 | 25.0 | 3.1 | 10 | 100 | 0.5 | 0.7 | 2.4 | 5.5 |
| EA6 | 0.80 | 1.11 | 26 | 2.0 | 2.2 | 20 | 1304 | 0.6 | 1.5 | 14.0 | 16.3 |
| EA7 | 0.53 | 1.91 | 26 | 2.0 | 4.2 | 20 | 1304 | 0.6 | 1.5 | 14.0 | 18.3 |
| EA8 | 0.14 | 0.86 | 100 | 9.0 | 8.5 | 10 | 102 | 0.5 | 0.7 | 2.4 | 10.9 |
| EA9 | 0.08 | 0.92 | 50 | 24.4 | 4.6 | 10 | 0 | 0 | 0.0 | 0.0 | 5.0 |
| EA10 | 0.08 | 0.37 | 35 | 24.4 | 3.8 | 10 | 0 | 0 | 0.0 | 0.0 | 5.0 |
| EA11 | 0.08 | 0.15 | 23 | 18.0 | 3.4 | 10 | 0 | 0 | 0.0 | 0.0 | 5.0 |
| EA12 | 0.14 | 0.26 | 117 | 12.0 | 8.3 | 10 | 0 | 0 | 0.0 | 0.0 | 8.3 |
| EA13 | 0.08 | 0.21 | 82 | 2.0 | 13.4 | 10 | 0 | 0 | 0.0 | 0.0 | 13.4 |
| EA8 & EA9 *Per Segment 2 FDR | 0.72 | 5.07 | 26 | 2.0 | 2.8 | 20 | 2500 | 0.7 | 1.7 | 24.9 | 27.7 |
| OS1 | 0.09 | 1.63 | 100 | 2.7 | 13.3 | 10 | 633 | 1.5 | 1.2 | 8.6 | 22.0 |
| OS2 | 0.09 | 12.33 | 100 | 4.3 | 11.4 | 10 | 1243 | 3.2 | 1.8 | 11.6 | 23.0 |
| OS3 | 0.09 | 25.36 | 100 | 6.5 | 9.9 | 10 | 879 | 3.2 | 1.8 | 8.2 | 18.1 |

FORMULAS:

$$t_i = \frac{0.395(1.1 - C_s)\sqrt{L}}{S^{0.33}} \quad V = C_v S_w^{0.5}$$

Table 6-7. Conveyance Coefficient, C_v

| Type of Land Surface | C _v |
|--------------------------------------|----------------|
| Heavy meadow | 2.5 |
| Tillage/field | 5 |
| Riprap (not buried)* | 6.5 |
| Short pasture and lawns | 7 |
| Nearly bare ground | 10 |
| Grassed waterway | 15 |
| Paved areas and shallow paved swales | 20 |

*For buried riprap, select C_v value based on type of vegetative cover.

Revise to SFB D for consistency.



**EASTONVILLE ROAD
PROPOSED CONDITIONS
DESIGN STORM: 5-YEAR**

Calc'd by:
Checked by:
Date:

SPC
CM
3/14/2024

PPRTA Pond E?

| STREET | DESIGN POINT | BASIN ID | DIRECT RUNOFF | | | | | | TOTAL RUNOFF | | | | STREET | | | PIPE | | | | TRAVEL TIME | | | REMARKS | | |
|--------|--------------|-------------------------------|---------------|----------------|----------------------|------------------------|-------------|---------|----------------------|------------------------|-------------|---------|---------------------------|------------------------|---------|-------------------------|------------------------|---------|----------------|-------------|------------|-------------------|---------|--|--|
| | | | AREA (ac) | C _s | f _c (min) | C _s *A (ac) | f (in./hr.) | Q (cfs) | f _c (min) | C _s *A (ac) | f (in./hr.) | Q (cfs) | Q _{street} (cfs) | C _s *A (ac) | SLOPE % | Q _{pipe} (cfs) | C _s *A (ac) | SLOPE % | PIPE SIZE (ft) | LENGTH (FT) | VEL. (FPS) | TRAVEL TIME (min) | | | |
| | 1 | OS1 | 1.63 | 0.09 | 14.1 | 0.15 | 3.62 | 0.5 | 14.1 | 0.15 | 3.62 | 0.5 | | | | | | 0.5 | 0.15 | 0.5 | 1.5 | 115 | 4.2 | 0.46 | BASIN OS1 @ DP1 CAPTURED IN 18" RCP CULVERT, DRAINS TO BASIN DP2 |
| | 2 | | | | | | | | 14.5 | 0.15 | 3.62 | 0.9 | | | | | | | | | | | | | FLOW @ DP2 CONVEYED OFFSITE (INCLUDES POND D 5-YR RELEASE RATE @ 0.4 CFS) |
| | 3 | OS2 | 12.33 | 0.09 | 17.5 | 1.11 | 3.29 | 3.7 | 17.5 | 1.11 | 3.29 | 3.7 | | | 3.7 | 1.11 | 2.6 | 2.5 | 186 | 13.5 | 0.23 | | | BASIN OS2 @ DP3 CAPTURED IN 30" RCP CULVERT, DRAINS TO BASIN DP4 | |
| | 4 | | | | | | | | 17.7 | 1.11 | 3.29 | 4.0 | | | | | | | | | | | | | FLOW @ DP4 CONVEYED OFFSITE (INCLUDES DETENTION POND A 5-YR RELEASE RATE @ 0.3 CFS) |
| | 7 | OS3 | 25.36 | 0.09 | 15.4 | 2.28 | 3.48 | 7.9 | 15.4 | 2.28 | 3.48 | 7.9 | | | 7.9 | 2.28 | 0.6 | 3.0 | 445 | 7.3 | 1.01 | | | BASIN OS3 FLOW @ DP7 CAPTURED IN CDOT TYPE D INLET, PIPED TO DP8 | |
| | 8 | | | | | | | | 16.5 | 2.28 | 3.48 | 8.3 | | | | | | | | | | | | | FLOW @ DP4 CONVEYED OFFSITE (INCLUDES DETENTION POND B 5-YR RELEASE RATE @ 0.4 CFS) |
| | 9 | EA1 | 0.61 | 0.78 | 7.3 | 0.48 | 4.61 | 2.2 | 7.3 | 0.48 | 4.61 | 2.2 | | | 2.2 | 0.48 | 0.5 | 1.5 | 52 | 4.2 | 0.21 | | | BASIN EA1 CAPTURED @ DP9 BY TYPE R INLET | |
| | 10 | EA2 | 1.23 | 0.44 | 9.8 | 0.54 | 4.15 | 2.2 | 9.8 | 1.02 | 4.15 | 4.2 | | | 4.2 | 1.02 | 0.5 | 1.5 | 128 | 4.2 | 0.51 | | | BASIN EA2 CAPTURED @ DP10 BY TYPE R INLET | |
| | 11 | EA12 | 0.26 | 0.14 | 8.3 | 0.04 | 4.41 | 0.2 | 10.3 | 1.05 | 4.08 | 4.3 | | | | | | | | | | | | | BASIN EA12 SHEET FLOWS DIRECTLY TO SFB D |
| | 12 | EA13 | 0.21 | 0.08 | 10.5 | 0.02 | 4.06 | 0.1 | 10.5 | 0.02 | 4.08 | 0.1 | | | | | | | | | | | | | FLOW @ DP12 CONVEYED OFFSITE |
| | 13 | EA3 | 0.53 | 0.79 | 6.1 | 0.42 | 4.87 | 2.1 | 6.1 | 0.42 | 4.87 | 2.1 | | | 2.1 | 0.42 | 1.3 | 1.5 | 56 | 6.8 | 0.14 | | | BASIN EA3 CAPTURED @ DP13 BY TYPE R INLET | |
| | 14 | EA4 | 0.90 | 0.51 | 8.2 | 0.46 | 4.42 | 2.0 | 8.2 | 0.88 | 4.42 | 3.9 | | | 3.9 | 0.88 | 1.3 | 1.5 | 56 | 6.8 | 0.14 | | | BASIN EA4 CAPTURED @ DP14 BY TYPE R INLET | |
| | 15 | EA5 | 0.29 | 0.11 | 5.5 | 0.03 | 5.03 | 0.2 | 8.4 | 0.91 | 4.40 | 4.0 | | | 4.0 | 0.91 | 0.5 | 1.5 | 36 | 4.2 | 0.14 | | | BASIN EA5 SHEET FLOWS DIRECTLY TO SFB A | |
| | 16 | EA6 | 1.11 | 0.80 | 16.3 | 0.89 | 3.40 | 3.0 | 16.3 | 0.89 | 3.40 | 3.0 | | | 3.0 | 0.89 | 0.5 | 1.5 | 52 | 4.2 | 0.21 | | | BASIN EA6 CAPTURED @ DP16 BY TYPE R INLET | |
| | 17 | EA7 | 1.91 | 0.53 | 17.4 | 1.01 | 3.30 | 3.3 | 17.4 | 1.90 | 3.30 | 6.3 | | | 6.3 | 1.90 | 0.5 | 2.0 | 196 | 5.1 | 0.64 | | | BASIN EA7 CAPTURED @ DP17 BY TYPE R INLET | |
| | 18 | | | | | | | | 17.4 | 1.90 | 3.30 | 6.3 | | | 6.3 | 1.90 | 0.5 | 2.0 | 42 | 5.1 | 0.14 | | | | STORM MH @ D18, NO FUTURE FLOW |
| | 19 | EA8 | 0.86 | 0.14 | 10.9 | 0.12 | 4.00 | 0.5 | 17.5 | 2.02 | 3.29 | 6.6 | | | 6.6 | 2.02 | 0.5 | 2.0 | 196 | 5.1 | 0.64 | | | | BASIN EA8 SHEET FLOWS DIRECTLY TO EDB B (NO FUTURE FLOWS) |
| | 18U | EA8 & EA9 * Per Segment 2 FDR | 5.07 | 0.72 | 24.0 | 3.64 | 2.81 | 10.2 | 24.0 | 5.54 | 2.81 | 15.6 | | | 15.6 | 5.54 | 0.5 | 2.0 | 42 | 5.1 | 0.14 | | | | FUTURE FLOW COMBINES @ DP18 WITH SEGMENT 1 FLOWS @ STORM MH |
| | 19U | EA8 | 0.86 | 0.14 | 10.9 | 0.12 | 4.00 | 0.5 | 24.2 | 5.66 | 2.81 | 15.9 | | | | | | | | | | | | | BASIN EA8 SHEET FLOWS DIRECTLY TO EDB B INCLUDING FUTURE TRIBUTARY FLOW FROM SUBBASIN EA8 & EA9 PER THE EASTONVILLE ROAD SEGMENT 2 FDR |
| | 20 | EA9 | 0.92 | 0.08 | 5.0 | 0.07 | 5.17 | 0.4 | 5.0 | 0.07 | 5.17 | 0.4 | | | | | | | | | | | | | BASIN EA9 SHEET FLOWS OFFSITE |
| | 21 | EA10 | 0.37 | 0.08 | 5.0 | 0.03 | 5.17 | 0.2 | 5.0 | 0.03 | 5.17 | 0.2 | | | | | | | | | | | | | BASIN EA10 SHEET FLOWS OFFSITE |
| | 22 | EA11 | 0.15 | 0.08 | 5.0 | 0.01 | 5.17 | 0.1 | 5.0 | 0.01 | 5.17 | 0.1 | | | | | | | | | | | | | BASIN EA11 SHEET FLOWS OFFSITE |

Unresolved:
Basin listed twice. Please
remove one.

additional?

Revise to SFB D for consistency.



**EASTONVILLE ROAD
PROPOSED CONDITIONS
DESIGN STORM: 100-YEAR**

Calc'd by:
Checked by:
Date:

SPC
CM
3/14/2024

| STREET | DESIGN POINT | BASIN ID | DIRECT RUNOFF | | | | | | TOTAL RUNOFF | | | | STREET | | | PIPE | | | | TRAVEL TIME | | REMARKS |
|--------|--------------|------------------------------|---------------|------------------|----------------------|--------------------------|-------------|---------|----------------------|--------------------------|-------------|---------|---------------------------|--------------------------|---------|-------------------------|--------------------------|---------|----------------|-------------|--|---|
| | | | AREA (ac) | C ₁₀₀ | f _c (min) | C ₁₀₀ *A (ac) | I (in./hr.) | Q (cfs) | f _c (min) | C ₁₀₀ *A (ac) | I (in./hr.) | Q (cfs) | Q _{street} (cfs) | C ₁₀₀ *A (ac) | SLOPE % | Q _{PIPE} (cfs) | C ₁₀₀ *A (ac) | SLOPE % | PIPE SIZE (ft) | LENGTH (ft) | VEL. (ft/s) | |
| | 1 | OS1 | 1.63 | 0.36 | 14.1 | 0.59 | 6.07 | 3.6 | 14.1 | 0.59 | 6.07 | 3.6 | | | 3.6 | 0.59 | 0.5 | 1.5 | 115 | 4.2 | 0.46 | BASIN OS1 @ DP1 CAPTURED IN 18" RCP CULVERT, DRAINS TO BASIN DP2 |
| | 2 | | | | | | | | 14.5 | 0.59 | 6.07 | 5.0 | | | | | | | | | | FLOW @ DP2 CONVEYED OFFSITE (INCLUDES POND D 100-YR RELEASE RATE @ 1.4 CFS) |
| | 3 | OS2 | 12.33 | 0.36 | 17.5 | 4.44 | 5.53 | 24.5 | 17.5 | 4.44 | 5.53 | 24.5 | | 24.5 | 4.44 | 2.6 | 2.5 | 186 | 13.5 | 0.23 | BASIN OS2 @ DP3 CAPTURED IN 30" RCP CULVERT, DRAINS TO BASIN DP4 | |
| | 4 | | | 2.00 | | | | | 17.7 | 4.44 | 5.53 | 25.7 | | | | | | | | | | FLOW @ DP4 CONVEYED OFFSITE (INCLUDES DETENTION POND A 100-YR RELEASE RATE @ 1.2 CFS) |
| | 7 | OS3 | 25.36 | 0.36 | 15.4 | 9.13 | 5.84 | 53.3 | 15.4 | 9.13 | 5.84 | 53.3 | | 53.3 | 9.13 | 0.6 | 3.0 | 445 | 7.3 | 1.01 | BASIN OS3 FLOW @ DP7 CAPTURED IN CDOT TYPE D INLET, PIPED TO DP8 | |
| | 8 | | | | | | | | 16.5 | 9.13 | 5.84 | 54.3 | | | | | | | | | | FLOW @ DP4 CONVEYED OFFSITE (INCLUDES DETENTION POND B 100-YR RELEASE RATE @ 1.0 CFS) |
| | 9 | EA1 | 0.61 | 0.87 | 7.3 | 0.53 | 7.74 | 4.1 | 7.3 | 0.53 | 7.74 | 4.1 | | 4.1 | 0.53 | 0.5 | 1.5 | 52 | 4.2 | 0.21 | BASIN EA1 CAPTURED @ DP9 BY TYPE R INLET | |
| | 10 | EA2 | 1.23 | 0.62 | 9.8 | 0.76 | 6.97 | 5.3 | 9.8 | 1.29 | 6.97 | 9.0 | | 9.0 | 1.29 | 0.5 | 1.5 | 128 | 4.2 | 0.51 | BASIN EA2 CAPTURED @ DP10 BY TYPE R INLET | |
| | 11 | EA12 | 0.26 | 0.39 | 8.3 | 0.10 | 7.40 | 0.8 | 10.3 | 1.39 | 6.85 | 9.5 | | | | | | | | | | BASIN EA12 SHEET FLOWS DIRECTLY TO SFB D |
| | 12 | EA13 | 0.21 | 0.35 | 10.5 | 0.07 | 6.82 | 0.5 | 10.5 | 0.07 | 6.85 | 0.5 | | | | | | | | | | FLOW @ DP12 CONVEYED OFFSITE |
| | 13 | EA3 | 0.53 | 0.79 | 6.1 | 0.42 | 8.18 | 3.4 | 6.1 | 0.42 | 8.18 | 3.4 | | 3.4 | 0.42 | 1.3 | 1.5 | 56 | 6.8 | 0.14 | BASIN EA3 CAPTURED @ DP13 BY TYPE R INLET | |
| | 14 | EA4 | 0.90 | 0.51 | 8.2 | 0.46 | 7.42 | 3.4 | 8.2 | 0.88 | 7.42 | 6.5 | | 6.5 | 0.88 | 1.3 | 1.5 | 56 | 6.8 | 0.14 | BASIN EA4 CAPTURED @ DP14 BY TYPE R INLET | |
| | 15 | EA5 | 0.29 | 0.11 | 5.5 | 0.03 | 8.45 | 0.3 | 8.4 | 0.91 | 7.38 | 6.7 | | 6.7 | 0.91 | 0.5 | 1.5 | 36 | 4.2 | 0.14 | BASIN EA5 SHEET FLOWS DIRECTLY TO SFB A | |
| | 16 | EA6 | 1.11 | 0.80 | 16.3 | 0.89 | 5.71 | 5.1 | 16.3 | 0.89 | 5.71 | 5.1 | | 5.1 | 0.89 | 0.5 | 1.5 | 52 | 4.2 | 0.21 | BASIN EA6 CAPTURED @ DP16 BY TYPE R INLET | |
| | 17 | EA7 | 1.91 | 0.53 | 17.4 | 1.01 | 5.54 | 5.6 | 17.4 | 1.90 | 5.54 | 10.5 | | 10.5 | 1.90 | 0.5 | 2.0 | 196 | 5.1 | 0.64 | BASIN EA7 CAPTURED @ DP17 BY TYPE R INLET | |
| | 18 | | | | | | | | 17.4 | 1.90 | 5.54 | 10.5 | | 10.5 | 1.90 | 0.5 | 2.0 | 42 | 5.1 | 0.14 | STORM MH @ D18, NO FUTURE FLOW | |
| | 19 | EA8 | 0.86 | 0.14 | 10.9 | 0.12 | 6.72 | 0.8 | 17.5 | 2.02 | 5.52 | 11.1 | | 11.1 | 2.02 | 0.5 | 2.0 | 196 | 5.1 | 0.64 | BASIN EA8 SHEET FLOWS DIRECTLY TO EDB B (NO FUTURE FLOWS) | |
| | 18U | EA8 & EA9 *Per Segment 2 FDR | 5.07 | 0.72 | 24.0 | 3.64 | 4.72 | 17.2 | 24.0 | 5.54 | 4.72 | 26.2 | | 26.2 | 5.54 | 0.5 | 2.0 | 42 | 5.1 | 0.14 | FUTURE FLOW COMBINES @ DP18 WITH SEGMENT 1 FLOWS @ STORM MH | |
| | 19U | EA8 | 0.86 | 0.14 | 10.9 | 0.12 | 6.72 | 0.8 | 24.2 | 5.66 | 4.71 | 26.6 | | | | | | | | | BASIN EA8 SHEET FLOWS DIRECTLY TO EDB B INCLUDING FUTURE TRIBUTARY FLOW FROM SUBBASIN EA8 & EA9 PER THE EASTONVILLE ROAD SEGMENT 2 FDR | |
| | 20 | EA9 | 0.92 | 0.08 | 5.0 | 0.07 | 8.68 | 0.6 | 5.0 | 0.07 | 8.68 | 0.6 | | | | | | | | | | BASIN EA9 SHEET FLOWS OFFSITE |
| | 21 | EA10 | 0.37 | 0.08 | 5.0 | 0.03 | 8.68 | 0.3 | 5.0 | 0.03 | 8.68 | 0.3 | | | | | | | | | | BASIN EA10 SHEET FLOWS OFFSITE |
| | 22 | EA11 | 0.15 | 0.08 | 5.0 | 0.01 | 8.68 | 0.1 | 5.0 | 0.01 | 8.68 | 0.1 | | | | | | | | | | BASIN EA11 SHEET FLOWS OFFSITE |

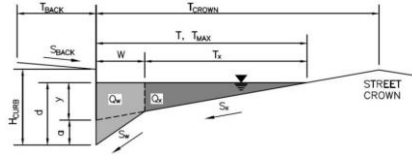
APPENDIX C – HYDRAULIC CALCULATIONS

Provide calculation for
Type 13 inlet at DP1 &
Type D inlet at DP7

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: Eastonville Road - Segment 1 Improvements
Inlet ID: Eastonville Rd Capacity

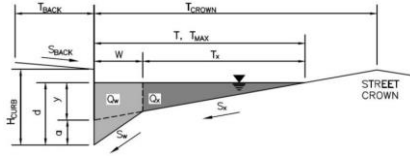


| Gutter Geometry: | | | | | | | |
|---|--|--------------------------|-------------------------------------|--------|------------------|-------------|--|
| Maximum Allowable Width for Spread Behind Curb | $T_{BACK} = 2.5$ ft | | | | | | |
| Side Slope Behind Curb (leave blank for no conveyance credit behind curb) | $S_{BACK} = 0.020$ ft/ft | | | | | | |
| Manning's Roughness Behind Curb (typically between 0.012 and 0.020) | $n_{BACK} = 0.020$ | | | | | | |
| Height of Curb at Gutter Flow Line | $H_{CURB} = 6.00$ inches | | | | | | |
| Distance from Curb Face to Street Crown | $T_{CROWN} = 26.0$ ft | | | | | | |
| Gutter Width | $W = 2.00$ ft | | | | | | |
| Street Transverse Slope | $S_x = 0.020$ ft/ft | | | | | | |
| Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) | $S_w = 0.083$ ft/ft | | | | | | |
| Street Longitudinal Slope - Enter 0 for sump condition | $S_o = 0.006$ ft/ft | | | | | | |
| Manning's Roughness for Street Section (typically between 0.012 and 0.020) | $n_{STREET} = 0.012$ | | | | | | |
| Max. Allowable Spread for Minor & Major Storm | <table border="1" style="display: inline-table; border-collapse: collapse;"> <tr> <td style="padding: 2px 10px;">Minor Storm</td> <td style="padding: 2px 10px;">Major Storm</td> <td style="padding: 2px 10px;">ft</td> </tr> <tr> <td style="padding: 2px 10px;">$T_{MAX} = 20.0$</td> <td style="padding: 2px 10px;">26.0</td> <td></td> </tr> </table> | Minor Storm | Major Storm | ft | $T_{MAX} = 20.0$ | 26.0 | |
| Minor Storm | Major Storm | ft | | | | | |
| $T_{MAX} = 20.0$ | 26.0 | | | | | | |
| Max. Allowable Depth at Gutter Flowline for Minor & Major Storm | <table border="1" style="display: inline-table; border-collapse: collapse;"> <tr> <td style="padding: 2px 10px;">Minor Storm</td> <td style="padding: 2px 10px;">Major Storm</td> <td style="padding: 2px 10px;">inches</td> </tr> <tr> <td style="padding: 2px 10px;">$d_{MAX} = 6.0$</td> <td style="padding: 2px 10px;">6.5</td> <td></td> </tr> </table> | Minor Storm | Major Storm | inches | $d_{MAX} = 6.0$ | 6.5 | |
| Minor Storm | Major Storm | inches | | | | | |
| $d_{MAX} = 6.0$ | 6.5 | | | | | | |
| Allow Flow Depth at Street Crown (check box for yes, leave blank for no) | <table border="1" style="display: inline-table; border-collapse: collapse;"> <tr> <td style="padding: 2px 10px;"><input type="checkbox"/></td> <td style="padding: 2px 10px;"><input checked="" type="checkbox"/></td> <td></td> </tr> </table> | <input type="checkbox"/> | <input checked="" type="checkbox"/> | | | | |
| <input type="checkbox"/> | <input checked="" type="checkbox"/> | | | | | | |
| MINOR STORM Allowable Capacity is based on Depth Criterion | | | | | | | |
| MAJOR STORM Allowable Capacity is based on Depth Criterion | | | | | | | |
| Minor storm max. allowable capacity GOOD - greater than the design peak flow of 3.30 cfs on sheet 'Inlet Management' | | | | | | | |
| Major storm max. allowable capacity GOOD - greater than the design peak flow of 5.50 cfs on sheet 'Inlet Management' | | | | | | | |
| $Q_{allow} =$ | <table border="1" style="display: inline-table; border-collapse: collapse;"> <tr> <td style="padding: 2px 10px;">Minor Storm</td> <td style="padding: 2px 10px;">Major Storm</td> <td style="padding: 2px 10px;">cfs</td> </tr> <tr> <td style="padding: 2px 10px;">14.2</td> <td style="padding: 2px 10px;">18.6</td> <td></td> </tr> </table> | Minor Storm | Major Storm | cfs | 14.2 | 18.6 | |
| Minor Storm | Major Storm | cfs | | | | | |
| 14.2 | 18.6 | | | | | | |

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: Eastonville Road - Segment 1 Improvements
Inlet ID: Inlet DP9



Gutter Geometry:

Maximum Allowable Width for Spread Behind Curb
 Side Slope Behind Curb (leave blank for no conveyance credit behind curb)
 Manning's Roughness Behind Curb (typically between 0.012 and 0.020)
 Height of Curb at Gutter Flow Line
 Distance from Curb Face to Street Crown
 Gutter Width
 Street Transverse Slope
 Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)
 Street Longitudinal Slope - Enter 0 for sump condition
 Manning's Roughness for Street Section (typically between 0.012 and 0.020)

$T_{BACK} = 2.5$ ft
 $S_{BACK} = 0.020$ ft/ft
 $n_{BACK} = 0.020$

$H_{CURB} = 6.00$ inches
 $T_{CROWN} = 26.0$ ft
 $W = 2.00$ ft
 $S_X = 0.020$ ft/ft
 $S_W = 0.083$ ft/ft
 $S_O = 0.000$ ft/ft
 $n_{STREET} = 0.012$

Max. Allowable Spread for Minor & Major Storm
 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm
 Check boxes are not applicable in SUMP conditions

| | | | |
|-------------|--------------------------|--------------------------|--------|
| | Minor Storm | Major Storm | |
| $T_{MAX} =$ | 20.0 | 26.0 | ft |
| $d_{MAX} =$ | 6.0 | 6.5 | inches |
| | <input type="checkbox"/> | <input type="checkbox"/> | |

MINOR STORM Allowable Capacity is not applicable to Sump Condition
 MAJOR STORM Allowable Capacity is not applicable to Sump Condition

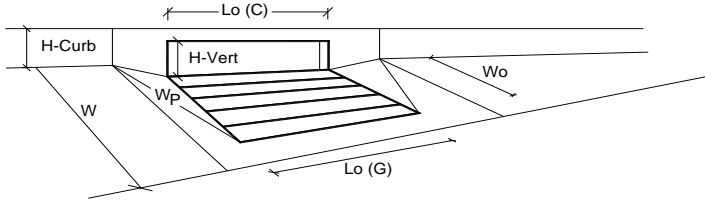
$Q_{allow} =$

| | |
|-------------|-------------|
| Minor Storm | Major Storm |
| SUMP | SUMP |

 cfs

INLET IN A SUMP OR SAG LOCATION

MHFD-Inlet, Version 5.03 (August 2023)



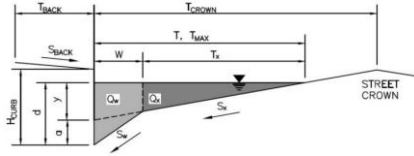
| <p>Design Information (Input)</p> <p>Type of Inlet: CDOT Type R Curb Opening</p> <p>Local Depression (additional to continuous gutter depression 'a' from above)</p> <p>Number of Unit Inlets (Grate or Curb Opening)</p> <p>Water Depth at Flowline (outside of local depression)</p> <p>Grate Information</p> <p>Length of a Unit Grate</p> <p>Width of a Unit Grate</p> <p>Open Area Ratio for a Grate (typical values 0.15-0.90)</p> <p>Clogging Factor for a Single Grate (typical value 0.50 - 0.70)</p> <p>Grate Weir Coefficient (typical value 2.15 - 3.60)</p> <p>Grate Orifice Coefficient (typical value 0.60 - 0.80)</p> <p>Curb Opening Information</p> <p>Length of a Unit Curb Opening</p> <p>Height of Vertical Curb Opening in Inches</p> <p>Height of Curb Orifice Throat in Inches</p> <p>Angle of Throat</p> <p>Side Width for Depression Pan (typically the gutter width of 2 feet)</p> <p>Clogging Factor for a Single Curb Opening (typical value 0.10)</p> <p>Curb Opening Weir Coefficient (typical value 2.3-3.7)</p> <p>Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)</p> <p>Low Head Performance Reduction (Calculated)</p> <p>Depth for Grate Midwidth</p> <p>Depth for Curb Opening Weir Equation</p> <p>Grated Inlet Performance Reduction Factor for Long Inlets</p> <p>Curb Opening Performance Reduction Factor for Long Inlets</p> <p>Combination Inlet Performance Reduction Factor for Long Inlets</p> <p>Total Inlet Interception Capacity (assumes clogged condition)</p> <p style="color: blue;">Inlet Capacity IS GOOD for Minor and Major Storms (>Q Peak)</p> | <table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th></th> <th style="text-align: center;">MINOR</th> <th style="text-align: center;">MAJOR</th> <th></th> </tr> </thead> <tbody> <tr> <td>Type =</td> <td colspan="2" style="text-align: center;">CDOT Type R Curb Opening</td> <td></td> </tr> <tr> <td>a_{local} =</td> <td style="text-align: center;">3.00</td> <td style="text-align: center;">3.00</td> <td>inches</td> </tr> <tr> <td>No =</td> <td style="text-align: center;">1</td> <td style="text-align: center;">1</td> <td></td> </tr> <tr> <td>Ponding Depth =</td> <td style="text-align: center;">6.0</td> <td style="text-align: center;">6.5</td> <td>inches</td> </tr> <tr> <td></td> <th style="text-align: center;">MINOR</th> <th style="text-align: center;">MAJOR</th> <td><input checked="" type="checkbox"/> Override Depths</td> </tr> <tr> <td>L_o (G) =</td> <td style="text-align: center;">N/A</td> <td style="text-align: center;">N/A</td> <td>feet</td> </tr> <tr> <td>W_o =</td> <td style="text-align: center;">N/A</td> <td style="text-align: center;">N/A</td> <td>feet</td> </tr> <tr> <td>A_{ratio} =</td> <td style="text-align: center;">N/A</td> <td style="text-align: center;">N/A</td> <td></td> </tr> <tr> <td>C_f (G) =</td> <td style="text-align: center;">N/A</td> <td style="text-align: center;">N/A</td> <td></td> </tr> <tr> <td>C_w (G) =</td> <td style="text-align: center;">N/A</td> <td style="text-align: center;">N/A</td> <td></td> </tr> <tr> <td>C_o (G) =</td> <td style="text-align: center;">N/A</td> <td style="text-align: center;">N/A</td> <td></td> </tr> <tr> <td></td> <th style="text-align: center;">MINOR</th> <th style="text-align: center;">MAJOR</th> <td></td> </tr> <tr> <td>L_o (C) =</td> <td style="text-align: center;">5.00</td> <td style="text-align: center;">5.00</td> <td>feet</td> </tr> <tr> <td>H_{vert} =</td> <td style="text-align: center;">6.00</td> <td style="text-align: center;">6.00</td> <td>inches</td> </tr> <tr> <td>H_{throat} =</td> <td style="text-align: center;">6.00</td> <td style="text-align: center;">6.00</td> <td>inches</td> </tr> <tr> <td>Theta =</td> <td style="text-align: center;">63.40</td> <td style="text-align: center;">63.40</td> <td>degrees</td> </tr> <tr> <td>W_o =</td> <td style="text-align: center;">2.00</td> <td style="text-align: center;">2.00</td> <td>feet</td> </tr> <tr> <td>C_f (C) =</td> <td style="text-align: center;">0.10</td> <td style="text-align: center;">0.10</td> <td></td> </tr> <tr> <td>C_w (C) =</td> <td style="text-align: center;">3.60</td> <td style="text-align: center;">3.60</td> <td></td> </tr> <tr> <td>C_o (C) =</td> <td style="text-align: center;">0.67</td> <td style="text-align: center;">0.67</td> <td></td> </tr> <tr> <td></td> <th style="text-align: center;">MINOR</th> <th style="text-align: center;">MAJOR</th> <td></td> </tr> <tr> <td>d_{Grate} =</td> <td style="text-align: center;">N/A</td> <td style="text-align: center;">N/A</td> <td>ft</td> </tr> <tr> <td>d_{Curb} =</td> <td style="text-align: center;">0.33</td> <td style="text-align: center;">0.38</td> <td>ft</td> </tr> <tr> <td>RF_{Grate} =</td> <td style="text-align: center;">N/A</td> <td style="text-align: center;">N/A</td> <td></td> </tr> <tr> <td>RF_{Curb} =</td> <td style="text-align: center;">1.00</td> <td style="text-align: center;">1.00</td> <td></td> </tr> <tr> <td>RF_{combination} =</td> <td style="text-align: center;">N/A</td> <td style="text-align: center;">N/A</td> <td></td> </tr> <tr> <td></td> <th style="text-align: center;">MINOR</th> <th style="text-align: center;">MAJOR</th> <td></td> </tr> <tr> <td>Q_s =</td> <td style="text-align: center;">5.4</td> <td style="text-align: center;">6.4</td> <td>cfs</td> </tr> <tr> <td>Q_{PEAK REQUIRED} =</td> <td style="text-align: center;">1.8</td> <td style="text-align: center;">3.3</td> <td>cfs</td> </tr> </tbody> </table> | | MINOR | MAJOR | | Type = | CDOT Type R Curb Opening | | | a _{local} = | 3.00 | 3.00 | inches | No = | 1 | 1 | | Ponding Depth = | 6.0 | 6.5 | inches | | MINOR | MAJOR | <input checked="" type="checkbox"/> Override Depths | L _o (G) = | N/A | N/A | feet | W _o = | N/A | N/A | feet | A _{ratio} = | N/A | N/A | | C _f (G) = | N/A | N/A | | C _w (G) = | N/A | N/A | | C _o (G) = | N/A | N/A | | | MINOR | MAJOR | | L _o (C) = | 5.00 | 5.00 | feet | H _{vert} = | 6.00 | 6.00 | inches | H _{throat} = | 6.00 | 6.00 | inches | Theta = | 63.40 | 63.40 | degrees | W _o = | 2.00 | 2.00 | feet | C _f (C) = | 0.10 | 0.10 | | C _w (C) = | 3.60 | 3.60 | | C _o (C) = | 0.67 | 0.67 | | | MINOR | MAJOR | | d _{Grate} = | N/A | N/A | ft | d _{Curb} = | 0.33 | 0.38 | ft | RF _{Grate} = | N/A | N/A | | RF _{Curb} = | 1.00 | 1.00 | | RF _{combination} = | N/A | N/A | | | MINOR | MAJOR | | Q _s = | 5.4 | 6.4 | cfs | Q _{PEAK REQUIRED} = | 1.8 | 3.3 | cfs |
|--|---|-------|---|-------|--|--------|--------------------------|--|--|----------------------|------|------|--------|------|---|---|--|-----------------|-----|-----|--------|--|-------|-------|---|----------------------|-----|-----|------|------------------|-----|-----|------|----------------------|-----|-----|--|----------------------|-----|-----|--|----------------------|-----|-----|--|----------------------|-----|-----|--|--|-------|-------|--|----------------------|------|------|------|---------------------|------|------|--------|-----------------------|------|------|--------|---------|-------|-------|---------|------------------|------|------|------|----------------------|------|------|--|----------------------|------|------|--|----------------------|------|------|--|--|-------|-------|--|----------------------|-----|-----|----|---------------------|------|------|----|-----------------------|-----|-----|--|----------------------|------|------|--|-----------------------------|-----|-----|--|--|-------|-------|--|------------------|-----|-----|-----|------------------------------|-----|-----|-----|
| | MINOR | MAJOR | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Type = | CDOT Type R Curb Opening | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| a _{local} = | 3.00 | 3.00 | inches | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| No = | 1 | 1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Ponding Depth = | 6.0 | 6.5 | inches | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | MINOR | MAJOR | <input checked="" type="checkbox"/> Override Depths | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| L _o (G) = | N/A | N/A | feet | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| W _o = | N/A | N/A | feet | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| A _{ratio} = | N/A | N/A | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| C _f (G) = | N/A | N/A | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| C _w (G) = | N/A | N/A | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| C _o (G) = | N/A | N/A | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | MINOR | MAJOR | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| L _o (C) = | 5.00 | 5.00 | feet | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| H _{vert} = | 6.00 | 6.00 | inches | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| H _{throat} = | 6.00 | 6.00 | inches | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Theta = | 63.40 | 63.40 | degrees | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| W _o = | 2.00 | 2.00 | feet | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| C _f (C) = | 0.10 | 0.10 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| C _w (C) = | 3.60 | 3.60 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| C _o (C) = | 0.67 | 0.67 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | MINOR | MAJOR | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| d _{Grate} = | N/A | N/A | ft | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| d _{Curb} = | 0.33 | 0.38 | ft | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| RF _{Grate} = | N/A | N/A | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| RF _{Curb} = | 1.00 | 1.00 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| RF _{combination} = | N/A | N/A | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | MINOR | MAJOR | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Q _s = | 5.4 | 6.4 | cfs | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Q _{PEAK REQUIRED} = | 1.8 | 3.3 | cfs | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |

Inlet appears to be still be ok, but flows at DP9 per hydrology spreadsheet are 2.2 & 4.1

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

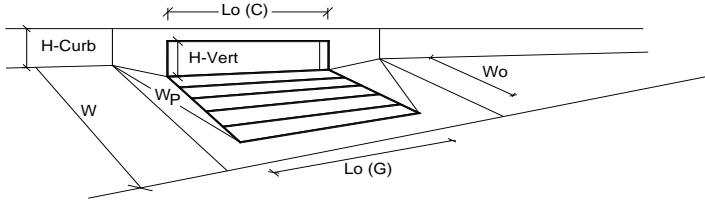
Project: Eastonville Road - Segment 1 Improvements
 Inlet ID: Inlet DP10



| | | | | | | | | | |
|--|--|-------------|-------------|-------------|--------|---------------|------|------|--|
| Gutter Geometry: | | | | | | | | | |
| Maximum Allowable Width for Spread Behind Curb | $T_{BACK} = 23.5$ ft | | | | | | | | |
| Side Slope Behind Curb (leave blank for no conveyance credit behind curb) | $S_{BACK} = 0.020$ ft/ft | | | | | | | | |
| Manning's Roughness Behind Curb (typically between 0.012 and 0.020) | $n_{BACK} = 0.020$ | | | | | | | | |
| Height of Curb at Gutter Flow Line | $H_{CURB} = 6.00$ inches | | | | | | | | |
| Distance from Curb Face to Street Crown | $T_{CROWN} = 26.0$ ft | | | | | | | | |
| Gutter Width | $W = 2.00$ ft | | | | | | | | |
| Street Transverse Slope | $S_X = 0.020$ ft/ft | | | | | | | | |
| Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) | $S_W = 0.083$ ft/ft | | | | | | | | |
| Street Longitudinal Slope - Enter 0 for sump condition | $S_0 = 0.000$ ft/ft | | | | | | | | |
| Manning's Roughness for Street Section (typically between 0.012 and 0.020) | $n_{STREET} = 0.012$ | | | | | | | | |
| Max. Allowable Spread for Minor & Major Storm | <table border="1"> <tr> <td></td> <td>Minor Storm</td> <td>Major Storm</td> <td>ft</td> </tr> <tr> <td>$T_{MAX} =$</td> <td>20.0</td> <td>26.0</td> <td></td> </tr> </table> | | Minor Storm | Major Storm | ft | $T_{MAX} =$ | 20.0 | 26.0 | |
| | Minor Storm | Major Storm | ft | | | | | | |
| $T_{MAX} =$ | 20.0 | 26.0 | | | | | | | |
| Max. Allowable Depth at Gutter Flowline for Minor & Major Storm | <table border="1"> <tr> <td></td> <td>Minor Storm</td> <td>Major Storm</td> <td>inches</td> </tr> <tr> <td>$d_{MAX} =$</td> <td>6.0</td> <td>6.5</td> <td></td> </tr> </table> | | Minor Storm | Major Storm | inches | $d_{MAX} =$ | 6.0 | 6.5 | |
| | Minor Storm | Major Storm | inches | | | | | | |
| $d_{MAX} =$ | 6.0 | 6.5 | | | | | | | |
| Check boxes are not applicable in SUMP conditions | <input type="checkbox"/> <input type="checkbox"/> | | | | | | | | |
| MINOR STORM Allowable Capacity is not applicable to Sump Condition | | | | | | | | | |
| MAJOR STORM Allowable Capacity is not applicable to Sump Condition | | | | | | | | | |
| | <table border="1"> <tr> <td></td> <td>Minor Storm</td> <td>Major Storm</td> <td>cfs</td> </tr> <tr> <td>$Q_{allow} =$</td> <td>SUMP</td> <td>SUMP</td> <td></td> </tr> </table> | | Minor Storm | Major Storm | cfs | $Q_{allow} =$ | SUMP | SUMP | |
| | Minor Storm | Major Storm | cfs | | | | | | |
| $Q_{allow} =$ | SUMP | SUMP | | | | | | | |

INLET IN A SUMP OR SAG LOCATION

MHFD-Inlet, Version 5.03 (August 2023)



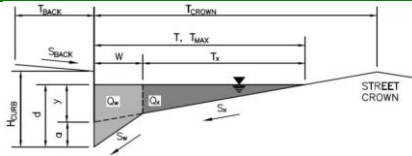
| Design Information (Input) | MINOR | | MAJOR | |
|--|------------------------------|-------|-------|---------|
| Type of Inlet | CDOT Type R Curb Opening | | | |
| Local Depression (additional to continuous gutter depression 'a' from above) | a _{local} = | 3.00 | 3.00 | inches |
| Number of Unit Inlets (Grate or Curb Opening) | No = | 1 | 1 | |
| Water Depth at Flowline (outside of local depression) | Ponding Depth = | 6.0 | 6.5 | inches |
| Grate Information | | | | |
| Length of a Unit Grate | L _o (G) = | N/A | N/A | feet |
| Width of a Unit Grate | W _o = | N/A | N/A | feet |
| Open Area Ratio for a Grate (typical values 0.15-0.90) | A _{ratio} = | N/A | N/A | |
| Clogging Factor for a Single Grate (typical value 0.50 - 0.70) | C _f (G) = | N/A | N/A | |
| Grate Weir Coefficient (typical value 2.15 - 3.60) | C _w (G) = | N/A | N/A | |
| Grate Orifice Coefficient (typical value 0.60 - 0.80) | C _o (G) = | N/A | N/A | |
| Curb Opening Information | | | | |
| Length of a Unit Curb Opening | L _o (C) = | 5.00 | 5.00 | feet |
| Height of Vertical Curb Opening in Inches | H _{vert} = | 6.00 | 6.00 | inches |
| Height of Curb Orifice Throat in Inches | H _{throat} = | 6.00 | 6.00 | inches |
| Angle of Throat | Theta = | 63.40 | 63.40 | degrees |
| Side Width for Depression Pan (typically the gutter width of 2 feet) | W _o = | 2.00 | 2.00 | feet |
| Clogging Factor for a Single Curb Opening (typical value 0.10) | C _f (C) = | 0.10 | 0.10 | |
| Curb Opening Weir Coefficient (typical value 2.3-3.7) | C _w (C) = | 3.60 | 3.60 | |
| Curb Opening Orifice Coefficient (typical value 0.60 - 0.70) | C _o (C) = | 0.67 | 0.67 | |
| Low Head Performance Reduction (Calculated) | | | | |
| Depth for Grate Midwidth | d _{Grate} = | N/A | N/A | ft |
| Depth for Curb Opening Weir Equation | d _{Curb} = | 0.33 | 0.38 | ft |
| Grated Inlet Performance Reduction Factor for Long Inlets | RF _{Grate} = | N/A | N/A | |
| Curb Opening Performance Reduction Factor for Long Inlets | RF _{Curb} = | 1.00 | 1.00 | |
| Combination Inlet Performance Reduction Factor for Long Inlets | RF _{combination} = | N/A | N/A | |
| Total Inlet Interception Capacity (assumes clogged condition) | | | | |
| | Q _s = | 5.4 | 6.4 | cfs |
| | Q _{PEAK REQUIRED} = | 1.8 | 4.0 | cfs |

Flows at DP10 per hydrology spreadsheet are 4.2 & 9.0

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

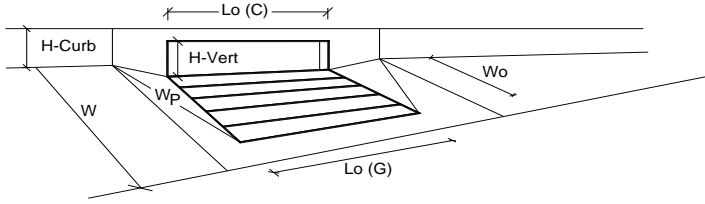
Project: Eastonville Road - Segment 1 Improvements
Inlet ID: Inlet DP13



| | | | | | | |
|--|---|-------------|-------------|--------|------------------|-------------|
| Gutter Geometry: | | | | | | |
| Maximum Allowable Width for Spread Behind Curb | $T_{BACK} = 2.5$ ft | | | | | |
| Side Slope Behind Curb (leave blank for no conveyance credit behind curb) | $S_{BACK} = 0.020$ ft/ft | | | | | |
| Manning's Roughness Behind Curb (typically between 0.012 and 0.020) | $n_{BACK} = 0.020$ | | | | | |
| Height of Curb at Gutter Flow Line | $H_{CURB} = 6.00$ inches | | | | | |
| Distance from Curb Face to Street Crown | $T_{CROWN} = 26.0$ ft | | | | | |
| Gutter Width | $W = 2.00$ ft | | | | | |
| Street Transverse Slope | $S_X = 0.020$ ft/ft | | | | | |
| Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) | $S_W = 0.083$ ft/ft | | | | | |
| Street Longitudinal Slope - Enter 0 for sump condition | $S_0 = 0.000$ ft/ft | | | | | |
| Manning's Roughness for Street Section (typically between 0.012 and 0.020) | $n_{STREET} = 0.012$ | | | | | |
| Max. Allowable Spread for Minor & Major Storm | <table border="1" style="display: inline-table; border-collapse: collapse;"> <tr> <td style="text-align: center;">Minor Storm</td> <td style="text-align: center;">Major Storm</td> <td rowspan="2" style="text-align: center;">ft</td> </tr> <tr> <td style="text-align: center;">$T_{MAX} = 20.0$</td> <td style="text-align: center;">26.0</td> </tr> </table> | Minor Storm | Major Storm | ft | $T_{MAX} = 20.0$ | 26.0 |
| Minor Storm | Major Storm | ft | | | | |
| $T_{MAX} = 20.0$ | 26.0 | | | | | |
| Max. Allowable Depth at Gutter Flowline for Minor & Major Storm | <table border="1" style="display: inline-table; border-collapse: collapse;"> <tr> <td style="text-align: center;">Minor Storm</td> <td style="text-align: center;">Major Storm</td> <td rowspan="2" style="text-align: center;">inches</td> </tr> <tr> <td style="text-align: center;">$d_{MAX} = 6.0$</td> <td style="text-align: center;">6.5</td> </tr> </table> | Minor Storm | Major Storm | inches | $d_{MAX} = 6.0$ | 6.5 |
| Minor Storm | Major Storm | inches | | | | |
| $d_{MAX} = 6.0$ | 6.5 | | | | | |
| Check boxes are not applicable in SUMP conditions | <input type="checkbox"/> <input type="checkbox"/> | | | | | |
| MINOR STORM Allowable Capacity is not applicable to Sump Condition | | | | | | |
| MAJOR STORM Allowable Capacity is not applicable to Sump Condition | | | | | | |
| Q_{allow} = | <table border="1" style="display: inline-table; border-collapse: collapse;"> <tr> <td style="text-align: center;">Minor Storm</td> <td style="text-align: center;">Major Storm</td> <td rowspan="2" style="text-align: center;">cfs</td> </tr> <tr> <td style="text-align: center;">SUMP</td> <td style="text-align: center;">SUMP</td> </tr> </table> | Minor Storm | Major Storm | cfs | SUMP | SUMP |
| Minor Storm | Major Storm | cfs | | | | |
| SUMP | SUMP | | | | | |

INLET IN A SUMP OR SAG LOCATION

MHFD-Inlet, Version 5.03 (August 2023)

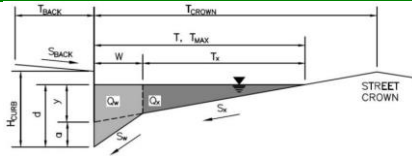


| Design Information (Input) | MINOR | MAJOR | |
|--|--------------------------|------------|------------|
| Type of Inlet | CDOT Type R Curb Opening | | |
| Local Depression (additional to continuous gutter depression 'a' from above) | 3.00 | 3.00 | inches |
| Number of Unit Inlets (Grate or Curb Opening) | 1 | 1 | |
| Water Depth at Flowline (outside of local depression) | 6.0 | 6.5 | inches |
| Grate Information | | | |
| Length of a Unit Grate | N/A | N/A | feet |
| Width of a Unit Grate | N/A | N/A | feet |
| Open Area Ratio for a Grate (typical values 0.15-0.90) | N/A | N/A | |
| Clogging Factor for a Single Grate (typical value 0.50 - 0.70) | N/A | N/A | |
| Grate Weir Coefficient (typical value 2.15 - 3.60) | N/A | N/A | |
| Grate Orifice Coefficient (typical value 0.60 - 0.80) | N/A | N/A | |
| Curb Opening Information | | | |
| Length of a Unit Curb Opening | 5.00 | 5.00 | feet |
| Height of Vertical Curb Opening in Inches | 6.00 | 6.00 | inches |
| Height of Curb Orifice Throat in Inches | 6.00 | 6.00 | inches |
| Angle of Throat | 63.40 | 63.40 | degrees |
| Side Width for Depression Pan (typically the gutter width of 2 feet) | 2.00 | 2.00 | feet |
| Clogging Factor for a Single Curb Opening (typical value 0.10) | 0.10 | 0.10 | |
| Curb Opening Weir Coefficient (typical value 2.3-3.7) | 3.60 | 3.60 | |
| Curb Opening Orifice Coefficient (typical value 0.60 - 0.70) | 0.67 | 0.67 | |
| Low Head Performance Reduction (Calculated) | | | |
| Depth for Grate Midwidth | N/A | N/A | ft |
| Depth for Curb Opening Weir Equation | 0.33 | 0.38 | ft |
| Grated Inlet Performance Reduction Factor for Long Inlets | N/A | N/A | |
| Curb Opening Performance Reduction Factor for Long Inlets | 1.00 | 1.00 | |
| Combination Inlet Performance Reduction Factor for Long Inlets | N/A | N/A | |
| Total Inlet Interception Capacity (assumes clogged condition) | | | |
| Inlet Capacity IS GOOD for Minor and Major Storms (>Q Peak) | 5.4 | 6.4 | cfs |
| Q _{PEAK REQUIRED} | 2.6 | 4.4 | cfs |

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

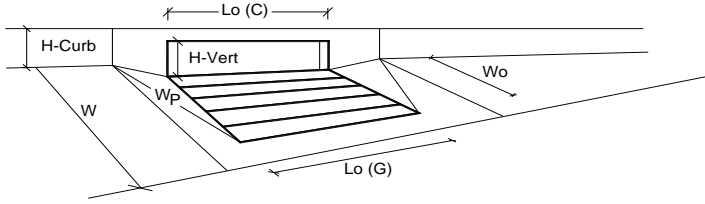
Project: Eastonville Road - Segment 1 Improvements
Inlet ID: Inlet DP14



| | | | | | | | | | |
|--|---|-------------|-------------|-------------|--|-------------|-------------|-------------|------------|
| Gutter Geometry: | | | | | | | | | |
| Maximum Allowable Width for Spread Behind Curb | $T_{BACK} = 23.5$ ft | | | | | | | | |
| Side Slope Behind Curb (leave blank for no conveyance credit behind curb) | $S_{BACK} = 0.020$ ft/ft | | | | | | | | |
| Manning's Roughness Behind Curb (typically between 0.012 and 0.020) | $n_{BACK} = 0.020$ | | | | | | | | |
| Height of Curb at Gutter Flow Line | $H_{CURB} = 6.00$ inches | | | | | | | | |
| Distance from Curb Face to Street Crown | $T_{CROWN} = 26.0$ ft | | | | | | | | |
| Gutter Width | $W = 2.00$ ft | | | | | | | | |
| Street Transverse Slope | $S_X = 0.020$ ft/ft | | | | | | | | |
| Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) | $S_W = 0.083$ ft/ft | | | | | | | | |
| Street Longitudinal Slope - Enter 0 for sump condition | $S_0 = 0.000$ ft/ft | | | | | | | | |
| Manning's Roughness for Street Section (typically between 0.012 and 0.020) | $n_{STREET} = 0.012$ | | | | | | | | |
| Max. Allowable Spread for Minor & Major Storm | <table border="1" style="display: inline-table; border-collapse: collapse;"> <tr> <td></td> <td style="text-align: center;">Minor Storm</td> <td style="text-align: center;">Major Storm</td> <td></td> </tr> <tr> <td>$T_{MAX} =$</td> <td style="text-align: center;">20.0</td> <td style="text-align: center;">26.0</td> <td>ft</td> </tr> </table> | | Minor Storm | Major Storm | | $T_{MAX} =$ | 20.0 | 26.0 | ft |
| | Minor Storm | Major Storm | | | | | | | |
| $T_{MAX} =$ | 20.0 | 26.0 | ft | | | | | | |
| Max. Allowable Depth at Gutter Flowline for Minor & Major Storm | <table border="1" style="display: inline-table; border-collapse: collapse;"> <tr> <td></td> <td style="text-align: center;">Minor Storm</td> <td style="text-align: center;">Major Storm</td> <td></td> </tr> <tr> <td>$d_{MAX} =$</td> <td style="text-align: center;">6.0</td> <td style="text-align: center;">6.5</td> <td>inches</td> </tr> </table> | | Minor Storm | Major Storm | | $d_{MAX} =$ | 6.0 | 6.5 | inches |
| | Minor Storm | Major Storm | | | | | | | |
| $d_{MAX} =$ | 6.0 | 6.5 | inches | | | | | | |
| Check boxes are not applicable in SUMP conditions | <input type="checkbox"/> <input type="checkbox"/> | | | | | | | | |
| MINOR STORM Allowable Capacity is not applicable to Sump Condition | | | | | | | | | |
| MAJOR STORM Allowable Capacity is not applicable to Sump Condition | | | | | | | | | |
| Q_{allow} = | <table border="1" style="display: inline-table; border-collapse: collapse;"> <tr> <td></td> <td style="text-align: center;">Minor Storm</td> <td style="text-align: center;">Major Storm</td> <td></td> </tr> <tr> <td></td> <td style="text-align: center;">SUMP</td> <td style="text-align: center;">SUMP</td> <td>cfs</td> </tr> </table> | | Minor Storm | Major Storm | | | SUMP | SUMP | cfs |
| | Minor Storm | Major Storm | | | | | | | |
| | SUMP | SUMP | cfs | | | | | | |

INLET IN A SUMP OR SAG LOCATION

MHFD-Inlet, Version 5.03 (August 2023)



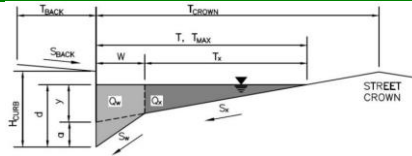
| Design Information (Input) | | <table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th style="width: 50%;"></th> <th style="width: 25%;">MINOR</th> <th style="width: 25%;">MAJOR</th> <th style="width: 10%;"></th> </tr> </thead> <tbody> <tr> <td>Type of Inlet</td> <td colspan="2" style="text-align: center;">CDOT Type R Curb Opening</td> <td></td> </tr> <tr> <td>Local Depression (additional to continuous gutter depression 'a' from above)</td> <td style="text-align: center;">3.00</td> <td style="text-align: center;">3.00</td> <td>inches</td> </tr> <tr> <td>Number of Unit Inlets (Grate or Curb Opening)</td> <td style="text-align: center;">1</td> <td style="text-align: center;">1</td> <td></td> </tr> <tr> <td>Water Depth at Flowline (outside of local depression)</td> <td style="text-align: center;">6.0</td> <td style="text-align: center;">6.5</td> <td>inches</td> </tr> <tr> <td colspan="4">Grate Information</td> </tr> <tr> <td>Length of a Unit Grate</td> <td style="text-align: center;">N/A</td> <td style="text-align: center;">N/A</td> <td>feet</td> </tr> <tr> <td>Width of a Unit Grate</td> <td style="text-align: center;">N/A</td> <td style="text-align: center;">N/A</td> <td>feet</td> </tr> <tr> <td>Open Area Ratio for a Grate (typical values 0.15-0.90)</td> <td style="text-align: center;">N/A</td> <td style="text-align: center;">N/A</td> <td></td> </tr> <tr> <td>Clogging Factor for a Single Grate (typical value 0.50 - 0.70)</td> <td style="text-align: center;">N/A</td> <td style="text-align: center;">N/A</td> <td></td> </tr> <tr> <td>Grate Weir Coefficient (typical value 2.15 - 3.60)</td> <td style="text-align: center;">N/A</td> <td style="text-align: center;">N/A</td> <td></td> </tr> <tr> <td>Grate Orifice Coefficient (typical value 0.60 - 0.80)</td> <td style="text-align: center;">N/A</td> <td style="text-align: center;">N/A</td> <td></td> </tr> <tr> <td colspan="4">Curb Opening Information</td> </tr> <tr> <td>Length of a Unit Curb Opening</td> <td style="text-align: center;">5.00</td> <td style="text-align: center;">5.00</td> <td>feet</td> </tr> <tr> <td>Height of Vertical Curb Opening in Inches</td> <td style="text-align: center;">6.00</td> <td style="text-align: center;">6.00</td> <td>inches</td> </tr> <tr> <td>Height of Curb Orifice Throat in Inches</td> <td style="text-align: center;">6.00</td> <td style="text-align: center;">6.00</td> <td>inches</td> </tr> <tr> <td>Angle of Throat</td> <td style="text-align: center;">63.40</td> <td style="text-align: center;">63.40</td> <td>degrees</td> </tr> <tr> <td>Side Width for Depression Pan (typically the gutter width of 2 feet)</td> <td style="text-align: center;">2.00</td> <td style="text-align: center;">2.00</td> <td>feet</td> </tr> <tr> <td>Clogging Factor for a Single Curb Opening (typical value 0.10)</td> <td style="text-align: center;">0.10</td> <td style="text-align: center;">0.10</td> <td></td> </tr> <tr> <td>Curb Opening Weir Coefficient (typical value 2.3-3.7)</td> <td style="text-align: center;">3.60</td> <td style="text-align: center;">3.60</td> <td></td> </tr> <tr> <td>Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)</td> <td style="text-align: center;">0.67</td> <td style="text-align: center;">0.67</td> <td></td> </tr> <tr> <td colspan="4">Low Head Performance Reduction (Calculated)</td> </tr> <tr> <td>Depth for Grate Midwidth</td> <td style="text-align: center;">N/A</td> <td style="text-align: center;">N/A</td> <td>ft</td> </tr> <tr> <td>Depth for Curb Opening Weir Equation</td> <td style="text-align: center;">0.33</td> <td style="text-align: center;">0.38</td> <td>ft</td> </tr> <tr> <td>Grated Inlet Performance Reduction Factor for Long Inlets</td> <td style="text-align: center;">N/A</td> <td style="text-align: center;">N/A</td> <td></td> </tr> <tr> <td>Curb Opening Performance Reduction Factor for Long Inlets</td> <td style="text-align: center;">1.00</td> <td style="text-align: center;">1.00</td> <td></td> </tr> <tr> <td>Combination Inlet Performance Reduction Factor for Long Inlets</td> <td style="text-align: center;">N/A</td> <td style="text-align: center;">N/A</td> <td></td> </tr> <tr> <td colspan="4">Total Inlet Interception Capacity (assumes clogged condition)</td> </tr> <tr> <td>Inlet Capacity IS GOOD for Minor and Major Storms (>Q Peak)</td> <td style="text-align: center;">5.4</td> <td style="text-align: center;">6.4</td> <td>cfs</td> </tr> <tr> <td>Q PEAK REQUIRED =</td> <td style="text-align: center;">2.6</td> <td style="text-align: center;">4.4</td> <td>cfs</td> </tr> </tbody> </table> | | | MINOR | MAJOR | | Type of Inlet | CDOT Type R Curb Opening | | | Local Depression (additional to continuous gutter depression 'a' from above) | 3.00 | 3.00 | inches | Number of Unit Inlets (Grate or Curb Opening) | 1 | 1 | | Water Depth at Flowline (outside of local depression) | 6.0 | 6.5 | inches | Grate Information | | | | Length of a Unit Grate | N/A | N/A | feet | Width of a Unit Grate | N/A | N/A | feet | Open Area Ratio for a Grate (typical values 0.15-0.90) | N/A | N/A | | Clogging Factor for a Single Grate (typical value 0.50 - 0.70) | N/A | N/A | | Grate Weir Coefficient (typical value 2.15 - 3.60) | N/A | N/A | | Grate Orifice Coefficient (typical value 0.60 - 0.80) | N/A | N/A | | Curb Opening Information | | | | Length of a Unit Curb Opening | 5.00 | 5.00 | feet | Height of Vertical Curb Opening in Inches | 6.00 | 6.00 | inches | Height of Curb Orifice Throat in Inches | 6.00 | 6.00 | inches | Angle of Throat | 63.40 | 63.40 | degrees | Side Width for Depression Pan (typically the gutter width of 2 feet) | 2.00 | 2.00 | feet | Clogging Factor for a Single Curb Opening (typical value 0.10) | 0.10 | 0.10 | | Curb Opening Weir Coefficient (typical value 2.3-3.7) | 3.60 | 3.60 | | Curb Opening Orifice Coefficient (typical value 0.60 - 0.70) | 0.67 | 0.67 | | Low Head Performance Reduction (Calculated) | | | | Depth for Grate Midwidth | N/A | N/A | ft | Depth for Curb Opening Weir Equation | 0.33 | 0.38 | ft | Grated Inlet Performance Reduction Factor for Long Inlets | N/A | N/A | | Curb Opening Performance Reduction Factor for Long Inlets | 1.00 | 1.00 | | Combination Inlet Performance Reduction Factor for Long Inlets | N/A | N/A | | Total Inlet Interception Capacity (assumes clogged condition) | | | | Inlet Capacity IS GOOD for Minor and Major Storms (>Q Peak) | 5.4 | 6.4 | cfs | Q PEAK REQUIRED = | 2.6 | 4.4 | cfs |
|--|--------------------------|--|------------|--|-------|-------|--|---------------|--------------------------|--|--|--|------|------|--------|---|---|---|--|---|-----|-----|--------|--------------------------|--|--|--|------------------------|-----|-----|------|-----------------------|-----|-----|------|--|-----|-----|--|--|-----|-----|--|--|-----|-----|--|---|-----|-----|--|---------------------------------|--|--|--|-------------------------------|------|------|------|---|------|------|--------|---|------|------|--------|-----------------|-------|-------|---------|--|------|------|------|--|------|------|--|---|------|------|--|--|------|------|--|--|--|--|--|--------------------------|-----|-----|----|--------------------------------------|------|------|----|---|-----|-----|--|---|------|------|--|--|-----|-----|--|--|--|--|--|---|------------|------------|------------|--------------------------|------------|------------|------------|
| | MINOR | MAJOR | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Type of Inlet | CDOT Type R Curb Opening | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Local Depression (additional to continuous gutter depression 'a' from above) | 3.00 | 3.00 | inches | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Number of Unit Inlets (Grate or Curb Opening) | 1 | 1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Water Depth at Flowline (outside of local depression) | 6.0 | 6.5 | inches | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Grate Information | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Length of a Unit Grate | N/A | N/A | feet | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Width of a Unit Grate | N/A | N/A | feet | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Open Area Ratio for a Grate (typical values 0.15-0.90) | N/A | N/A | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Clogging Factor for a Single Grate (typical value 0.50 - 0.70) | N/A | N/A | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Grate Weir Coefficient (typical value 2.15 - 3.60) | N/A | N/A | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Grate Orifice Coefficient (typical value 0.60 - 0.80) | N/A | N/A | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Curb Opening Information | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Length of a Unit Curb Opening | 5.00 | 5.00 | feet | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Height of Vertical Curb Opening in Inches | 6.00 | 6.00 | inches | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Height of Curb Orifice Throat in Inches | 6.00 | 6.00 | inches | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Angle of Throat | 63.40 | 63.40 | degrees | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Side Width for Depression Pan (typically the gutter width of 2 feet) | 2.00 | 2.00 | feet | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Clogging Factor for a Single Curb Opening (typical value 0.10) | 0.10 | 0.10 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Curb Opening Weir Coefficient (typical value 2.3-3.7) | 3.60 | 3.60 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Curb Opening Orifice Coefficient (typical value 0.60 - 0.70) | 0.67 | 0.67 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Low Head Performance Reduction (Calculated) | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Depth for Grate Midwidth | N/A | N/A | ft | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Depth for Curb Opening Weir Equation | 0.33 | 0.38 | ft | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Grated Inlet Performance Reduction Factor for Long Inlets | N/A | N/A | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Curb Opening Performance Reduction Factor for Long Inlets | 1.00 | 1.00 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Combination Inlet Performance Reduction Factor for Long Inlets | N/A | N/A | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Total Inlet Interception Capacity (assumes clogged condition) | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Inlet Capacity IS GOOD for Minor and Major Storms (>Q Peak) | 5.4 | 6.4 | cfs | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Q PEAK REQUIRED = | 2.6 | 4.4 | cfs | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |

Flows at DP14 per hydrology spreadsheet are 3.9 & 6.5

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: Eastonville Road - Segment 1 Improvements
 Inlet ID: Inlet DP16



Gutter Geometry:

Maximum Allowable Width for Spread Behind Curb
 Side Slope Behind Curb (leave blank for no conveyance credit behind curb)
 Manning's Roughness Behind Curb (typically between 0.012 and 0.020)
 Height of Curb at Gutter Flow Line
 Distance from Curb Face to Street Crown
 Gutter Width
 Street Transverse Slope
 Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)
 Street Longitudinal Slope - Enter 0 for sump condition
 Manning's Roughness for Street Section (typically between 0.012 and 0.020)

| | | |
|-----------------------|-------|--------|
| T _{BACK} = | 2.5 | ft |
| S _{BACK} = | 0.020 | ft/ft |
| n _{BACK} = | 0.020 | |
| H _{CURB} = | 6.00 | inches |
| T _{CROWN} = | 26.0 | ft |
| W = | 2.00 | ft |
| S _X = | 0.020 | ft/ft |
| S _W = | 0.083 | ft/ft |
| S ₀ = | 0.000 | ft/ft |
| n _{STREET} = | 0.012 | |

Max. Allowable Spread for Minor & Major Storm
 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm
 Check boxes are not applicable in SUMP conditions

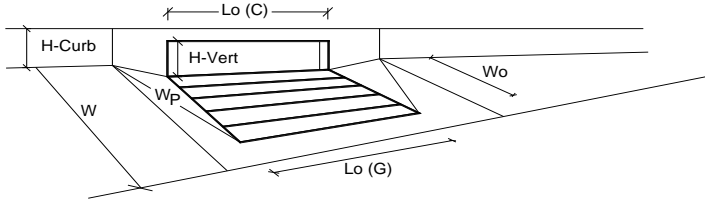
| | | | |
|--------------------|--------------------------|--------------------------|--------|
| | Minor Storm | Major Storm | |
| T _{MAX} = | 20.0 | 26.0 | ft |
| d _{MAX} = | 6.0 | 6.5 | inches |
| | <input type="checkbox"/> | <input type="checkbox"/> | |

MINOR STORM Allowable Capacity is not applicable to Sump Condition
 MAJOR STORM Allowable Capacity is not applicable to Sump Condition

| | | |
|----------------------|-------------|-------------|
| | Minor Storm | Major Storm |
| Q _{allow} = | SUMP | SUMP |
| | | cfs |

INLET IN A SUMP OR SAG LOCATION

MHFD-Inlet, Version 5.03 (August 2023)

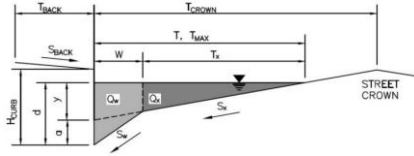


| Design Information (Input) | MINOR | MAJOR | |
|--|--------------------------|-------------|------------|
| Type of Inlet | CDOT Type R Curb Opening | | |
| Local Depression (additional to continuous gutter depression 'a' from above) | 3.00 | 3.00 | inches |
| Number of Unit Inlets (Grate or Curb Opening) | 2 | 2 | |
| Water Depth at Flowline (outside of local depression) | 6.0 | 6.5 | inches |
| Grate Information | | | |
| Length of a Unit Grate | N/A | N/A | feet |
| Width of a Unit Grate | N/A | N/A | feet |
| Open Area Ratio for a Grate (typical values 0.15-0.90) | N/A | N/A | |
| Clogging Factor for a Single Grate (typical value 0.50 - 0.70) | N/A | N/A | |
| Grate Weir Coefficient (typical value 2.15 - 3.60) | N/A | N/A | |
| Grate Orifice Coefficient (typical value 0.60 - 0.80) | N/A | N/A | |
| Curb Opening Information | | | |
| Length of a Unit Curb Opening | 5.00 | 5.00 | feet |
| Height of Vertical Curb Opening in Inches | 6.00 | 6.00 | inches |
| Height of Curb Orifice Throat in Inches | 6.00 | 6.00 | inches |
| Angle of Throat | 63.40 | 63.40 | degrees |
| Side Width for Depression Pan (typically the gutter width of 2 feet) | 2.00 | 2.00 | feet |
| Clogging Factor for a Single Curb Opening (typical value 0.10) | 0.10 | 0.10 | |
| Curb Opening Weir Coefficient (typical value 2.3-3.7) | 3.60 | 3.60 | |
| Curb Opening Orifice Coefficient (typical value 0.60 - 0.70) | 0.67 | 0.67 | |
| Low Head Performance Reduction (Calculated) | | | |
| Depth for Grate Midwidth | N/A | N/A | ft |
| Depth for Curb Opening Weir Equation | 0.33 | 0.38 | ft |
| Grated Inlet Performance Reduction Factor for Long Inlets | N/A | N/A | |
| Curb Opening Performance Reduction Factor for Long Inlets | 0.93 | 0.96 | |
| Combination Inlet Performance Reduction Factor for Long Inlets | N/A | N/A | |
| Total Inlet Interception Capacity (assumes clogged condition) | | | |
| Inlet Capacity IS GOOD for Minor and Major Storms (>Q Peak) | 8.3 | 10.2 | cfs |
| Q PEAK REQUIRED = | 3.0 | 5.0 | cfs |

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

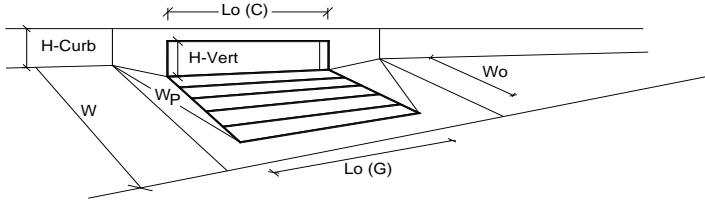
Project: Eastonville Road - Segment 1 Improvements
 Inlet ID: Inlet DP17



| | |
|--|--|
| Gutter Geometry: | |
| Maximum Allowable Width for Spread Behind Curb | $T_{BACK} = 23.5$ ft |
| Side Slope Behind Curb (leave blank for no conveyance credit behind curb) | $S_{BACK} = 0.020$ ft/ft |
| Manning's Roughness Behind Curb (typically between 0.012 and 0.020) | $n_{BACK} = 0.020$ |
| Height of Curb at Gutter Flow Line | $H_{CURB} = 6.00$ inches |
| Distance from Curb Face to Street Crown | $T_{CROWN} = 26.0$ ft |
| Gutter Width | $W = 2.00$ ft |
| Street Transverse Slope | $S_x = 0.020$ ft/ft |
| Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) | $S_w = 0.083$ ft/ft |
| Street Longitudinal Slope - Enter 0 for sump condition | $S_o = 0.000$ ft/ft |
| Manning's Roughness for Street Section (typically between 0.012 and 0.020) | $n_{STREET} = 0.012$ |
| Max. Allowable Spread for Minor & Major Storm | $T_{MAX} = \begin{matrix} \text{Minor Storm} & \text{Major Storm} \\ 20.0 & 26.0 \end{matrix}$ ft |
| Max. Allowable Depth at Gutter Flowline for Minor & Major Storm | $d_{MAX} = \begin{matrix} \text{Minor Storm} & \text{Major Storm} \\ 6.0 & 6.5 \end{matrix}$ inches |
| Check boxes are not applicable in SUMP conditions | <input type="checkbox"/> <input type="checkbox"/> |
| MINOR STORM Allowable Capacity is not applicable to Sump Condition | |
| MAJOR STORM Allowable Capacity is not applicable to Sump Condition | |
| $Q_{allow} =$ | $\begin{matrix} \text{Minor Storm} & \text{Major Storm} \\ \text{SUMP} & \text{SUMP} \end{matrix}$ cfs |

INLET IN A SUMP OR SAG LOCATION

MHFD-Inlet, Version 5.03 (August 2023)



| Design Information (Input) | MINOR | | MAJOR | |
|--|------------------------------|-------|-------|---------|
| Type of Inlet | CDOT Type R Curb Opening | | | |
| Local Depression (additional to continuous gutter depression 'a' from above) | a _{local} = | 3.00 | 3.00 | inches |
| Number of Unit Inlets (Grate or Curb Opening) | No = | 2 | 2 | |
| Water Depth at Flowline (outside of local depression) | Ponding Depth = | 6.0 | 6.5 | inches |
| Grate Information | | | | |
| Length of a Unit Grate | L _o (G) = | N/A | N/A | feet |
| Width of a Unit Grate | W _o = | N/A | N/A | feet |
| Open Area Ratio for a Grate (typical values 0.15-0.90) | A _{ratio} = | N/A | N/A | |
| Clogging Factor for a Single Grate (typical value 0.50 - 0.70) | C _f (G) = | N/A | N/A | |
| Grate Weir Coefficient (typical value 2.15 - 3.60) | C _w (G) = | N/A | N/A | |
| Grate Orifice Coefficient (typical value 0.60 - 0.80) | C _o (G) = | N/A | N/A | |
| Curb Opening Information | | | | |
| Length of a Unit Curb Opening | L _o (C) = | 5.00 | 5.00 | feet |
| Height of Vertical Curb Opening in Inches | H _{vert} = | 6.00 | 6.00 | inches |
| Height of Curb Orifice Throat in Inches | H _{throat} = | 6.00 | 6.00 | inches |
| Angle of Throat | Theta = | 63.40 | 63.40 | degrees |
| Side Width for Depression Pan (typically the gutter width of 2 feet) | W _o = | 2.00 | 2.00 | feet |
| Clogging Factor for a Single Curb Opening (typical value 0.10) | C _f (C) = | 0.10 | 0.10 | |
| Curb Opening Weir Coefficient (typical value 2.3-3.7) | C _w (C) = | 3.60 | 3.60 | |
| Curb Opening Orifice Coefficient (typical value 0.60 - 0.70) | C _o (C) = | 0.67 | 0.67 | |
| Low Head Performance Reduction (Calculated) | | | | |
| Depth for Grate Midwidth | d _{Grate} = | N/A | N/A | ft |
| Depth for Curb Opening Weir Equation | d _{Curb} = | 0.33 | 0.38 | ft |
| Grated Inlet Performance Reduction Factor for Long Inlets | RF _{Grate} = | N/A | N/A | |
| Curb Opening Performance Reduction Factor for Long Inlets | RF _{Curb} = | 0.93 | 0.96 | |
| Combination Inlet Performance Reduction Factor for Long Inlets | RF _{combination} = | N/A | N/A | |
| Total Inlet Interception Capacity (assumes clogged condition) | | | | |
| | Q _s = | 8.3 | 10.2 | cfs |
| | Q _{PEAK REQUIRED} = | 3.3 | 5.5 | cfs |

↗
 Flows at DP17 per hydrology spreadsheet are 6.3 & 10.5

Culvert Report

DP3

| | |
|---------------------|--------------------------------|
| Invert Elev Dn (ft) | = 6973.30 |
| Pipe Length (ft) | = 186.30 |
| Slope (%) | = 2.61 |
| Invert Elev Up (ft) | = 6978.16 |
| Rise (in) | = 30.0 |
| Shape | = Circular |
| Span (in) | = 30.0 |
| No. Barrels | = 1 |
| n-Value | = 0.012 |
| Culvert Type | = Circular Concrete |
| Culvert Entrance | = Square edge w/headwall (C) |
| Coeff. K,M,c,Y,k | = 0.0098, 2, 0.0398, 0.67, 0.5 |

Embankment

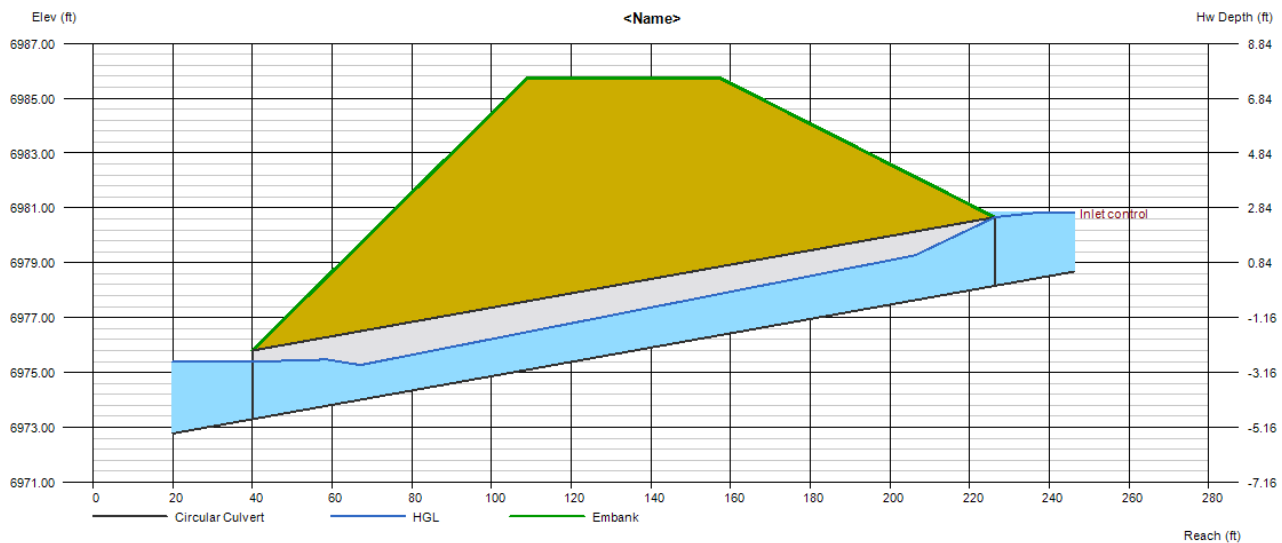
| | |
|--------------------|-----------|
| Top Elevation (ft) | = 6985.75 |
| Top Width (ft) | = 48.00 |
| Crest Width (ft) | = 15.00 |

Calculations

| | |
|---------------------|------------|
| Qmin (cfs) | = 24.60 |
| Qmax (cfs) | = 24.60 |
| Tailwater Elev (ft) | = (dc+D)/2 |

Highlighted

| | |
|-----------------|-----------------|
| Qtotal (cfs) | = 24.60 |
| Qpipe (cfs) | = 24.60 |
| Qovertop (cfs) | = 0.00 |
| Veloc Dn (ft/s) | = 5.60 |
| Veloc Up (ft/s) | = 6.97 |
| HGL Dn (ft) | = 6975.39 |
| HGL Up (ft) | = 6979.85 |
| Hw Elev (ft) | = 6980.82 |
| Hw/D (ft) | = 1.06 |
| Flow Regime | = Inlet Control |



Provide calculations for riprap outlet protection & all other pipe outlet locations.

Channel Report

Roadside Swale Capacity DP1

Trapezoidal

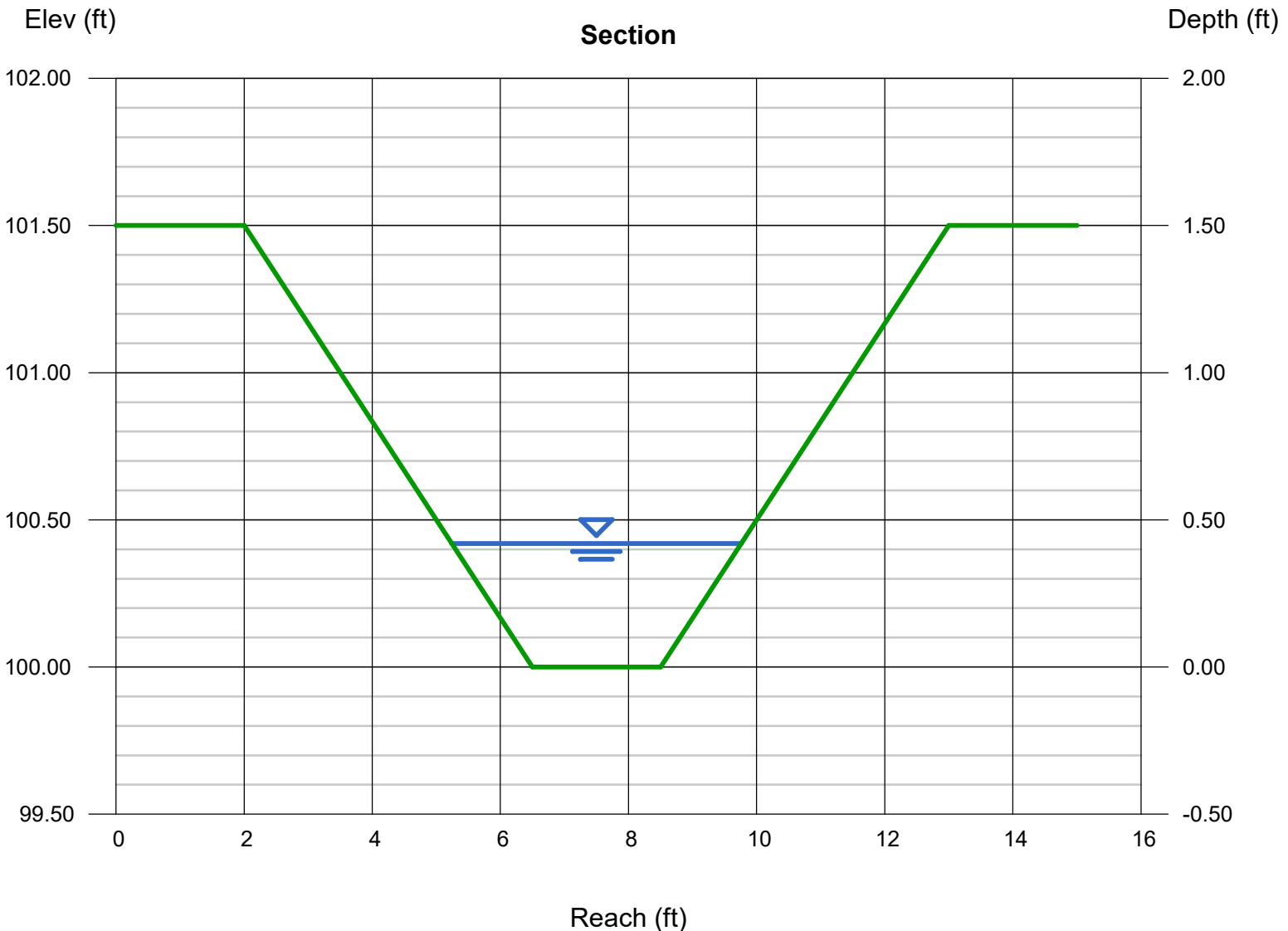
Bottom Width (ft) = 2.00
Side Slopes (z:1) = 3.00, 3.00
Total Depth (ft) = 1.50
Invert Elev (ft) = 100.00
Slope (%) = 1.00
N-Value = 0.025

Highlighted

Depth (ft) = 0.42
Q (cfs) = 3.500
Area (sqft) = 1.37
Velocity (ft/s) = 2.56
Wetted Perim (ft) = 4.66
Crit Depth, Yc (ft) = 0.38
Top Width (ft) = 4.52
EGL (ft) = 0.52

Calculations

Compute by: Known Q
Known Q (cfs) = 3.50



Channel Report

Roadside Swale Capacity DP3

Trapezoidal

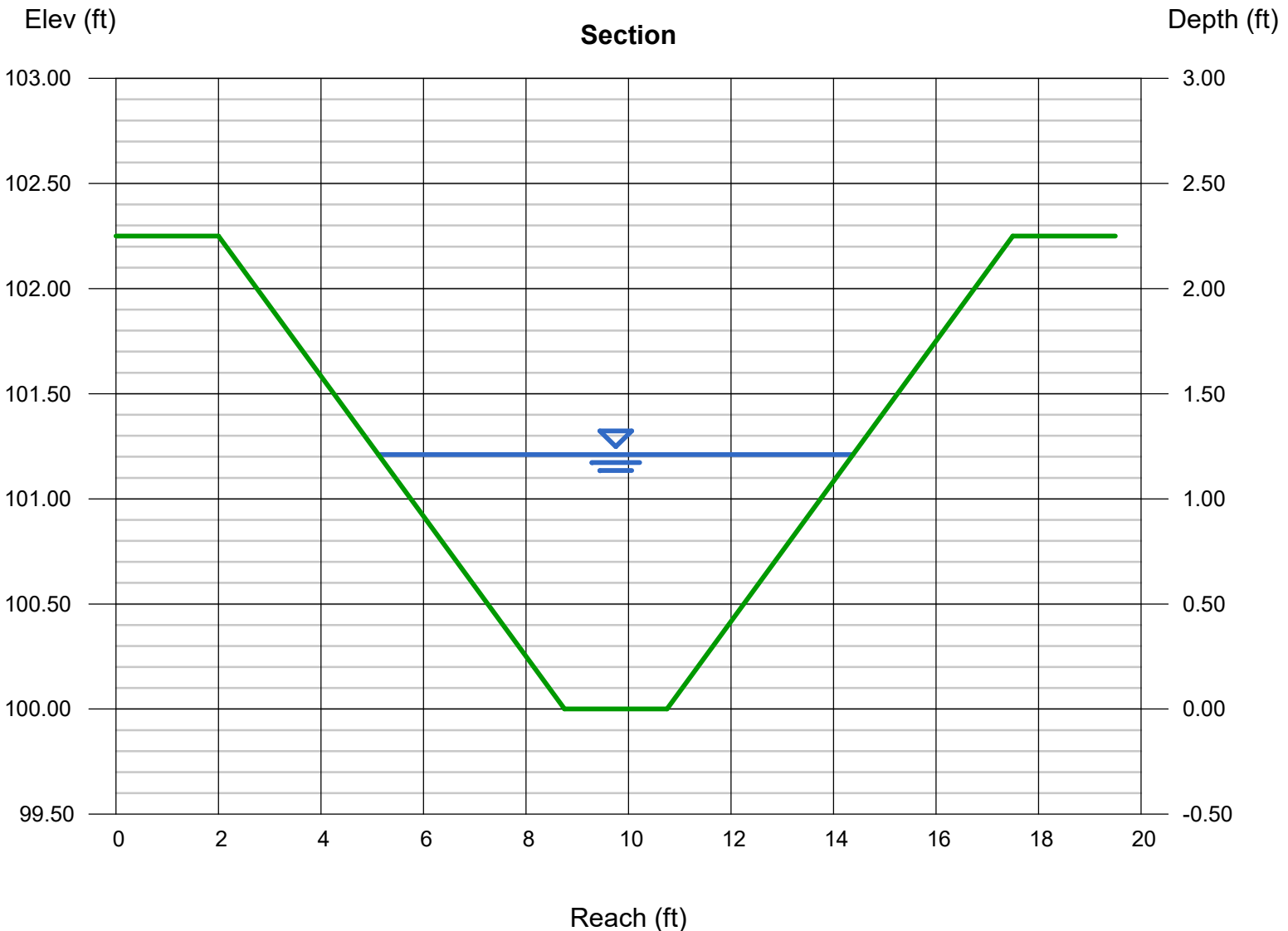
Bottom Width (ft) = 2.00
Side Slopes (z:1) = 3.00, 3.00
Total Depth (ft) = 2.25
Invert Elev (ft) = 100.00
Slope (%) = 0.60
N-Value = 0.025

Highlighted

Depth (ft) = 1.21
Q (cfs) = 24.60
Area (sqft) = 6.81
Velocity (ft/s) = 3.61
Wetted Perim (ft) = 9.65
Crit Depth, Yc (ft) = 1.05
Top Width (ft) = 9.26
EGL (ft) = 1.41

Calculations

Compute by: Known Q
Known Q (cfs) = 24.60



Channel Report

Roadside Swale Capacity DP7

Trapezoidal

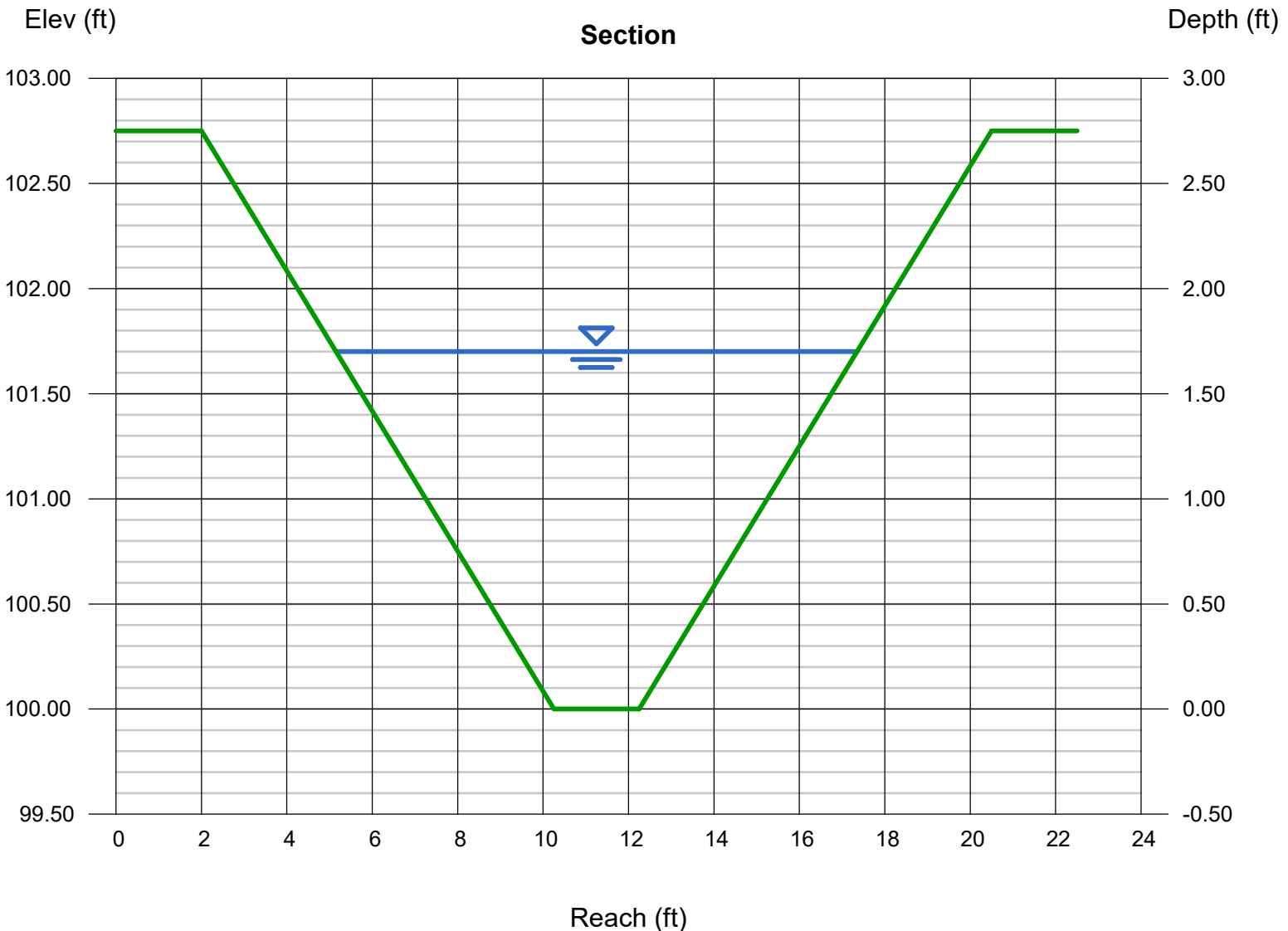
Bottom Width (ft) = 2.00
Side Slopes (z:1) = 3.00, 3.00
Total Depth (ft) = 2.75
Invert Elev (ft) = 100.00
Slope (%) = 0.60
N-Value = 0.025

Highlighted

Depth (ft) = 1.70
Q (cfs) = 53.30
Area (sqft) = 12.07
Velocity (ft/s) = 4.42
Wetted Perim (ft) = 12.75
Crit Depth, Yc (ft) = 1.52
Top Width (ft) = 12.20
EGL (ft) = 2.00

Calculations

Compute by: Known Q
Known Q (cfs) = 53.30



Channel Report

EDB B Trickle Channel Capacity

Rectangular

Bottom Width (ft) = 3.33
Total Depth (ft) = 0.50

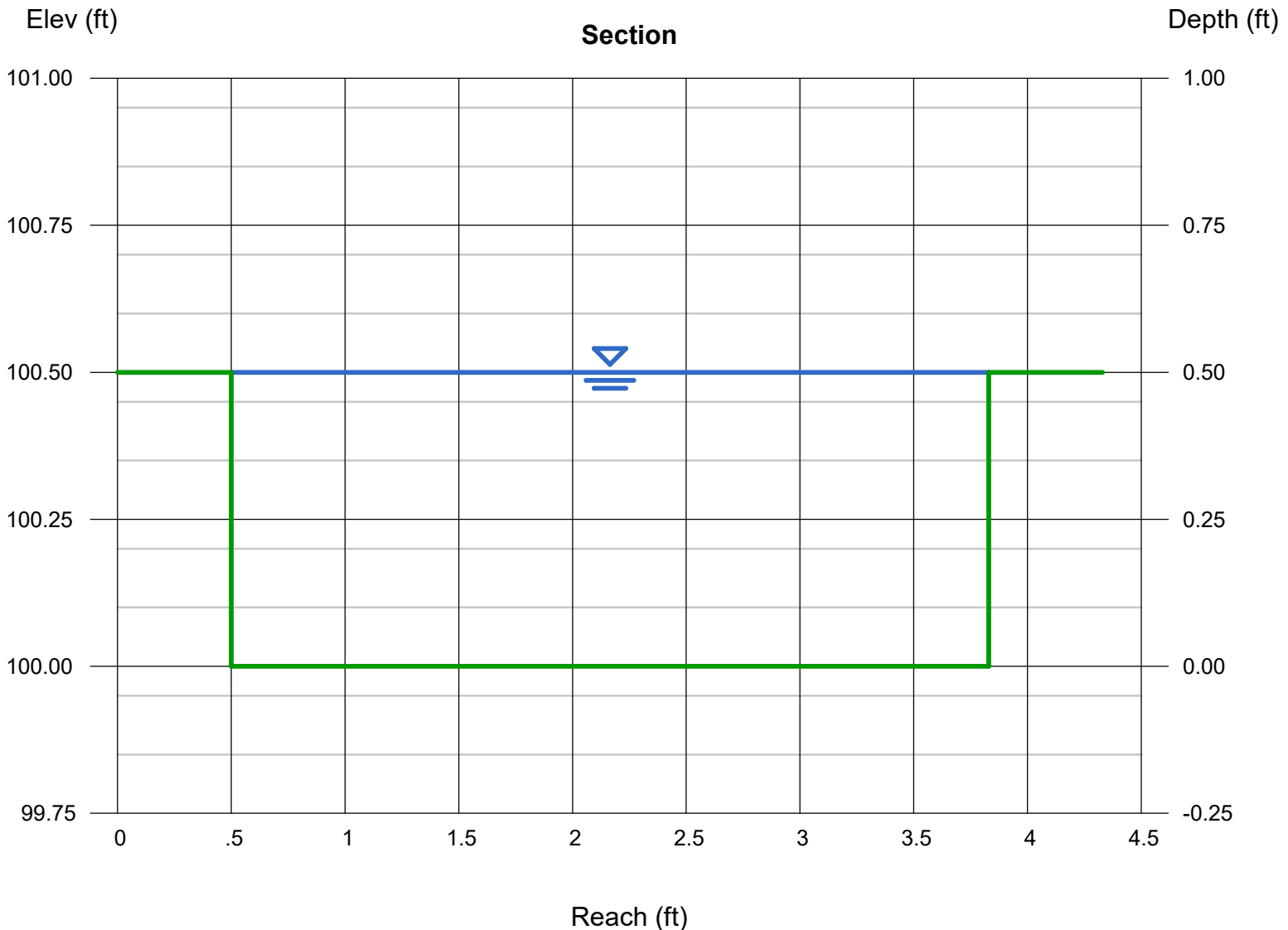
Invert Elev (ft) = 100.00
Slope (%) = 0.50
N-Value = 0.012

Calculations

Compute by: Known Depth
Known Depth (ft) = 0.50

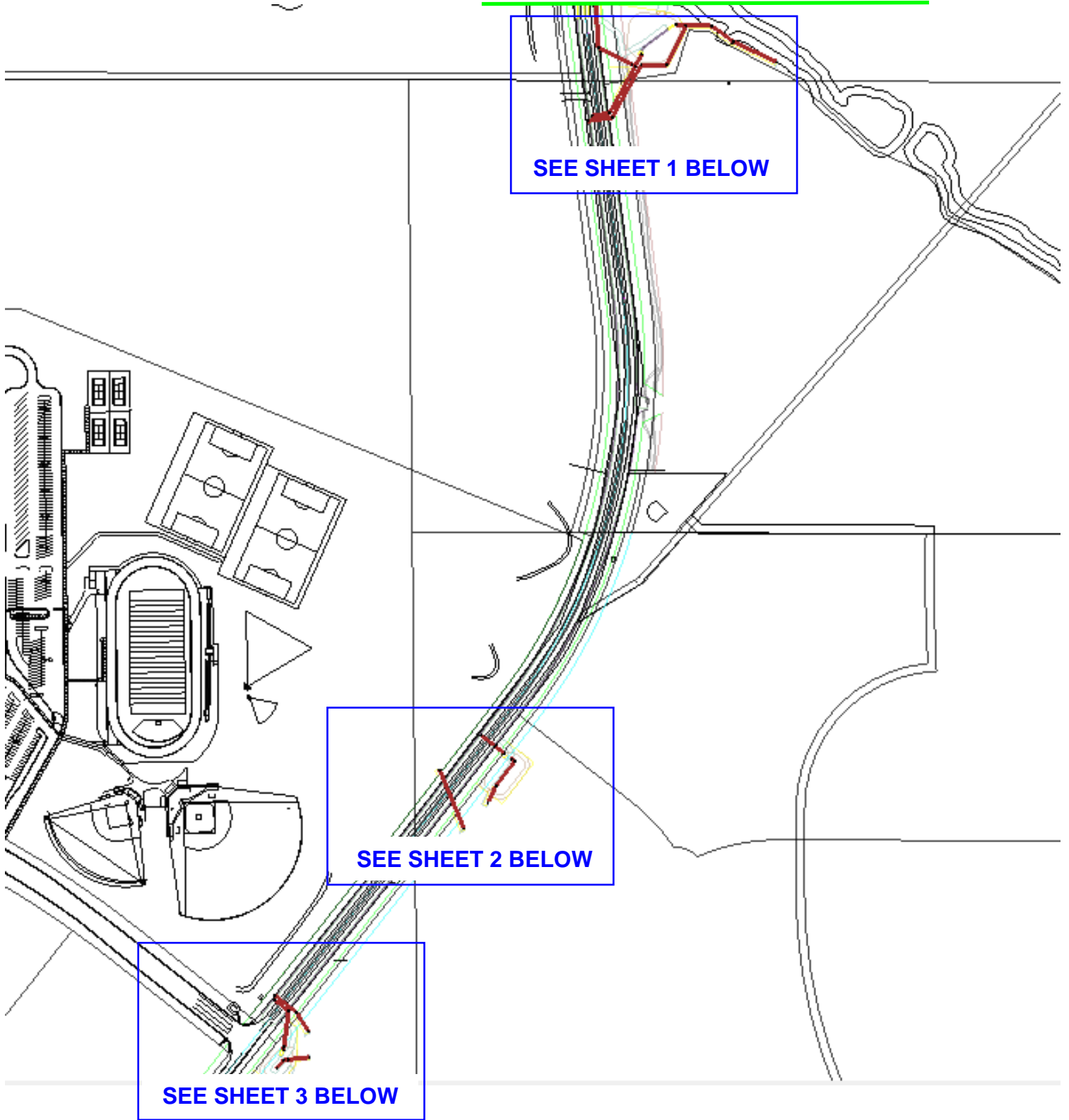
Highlighted

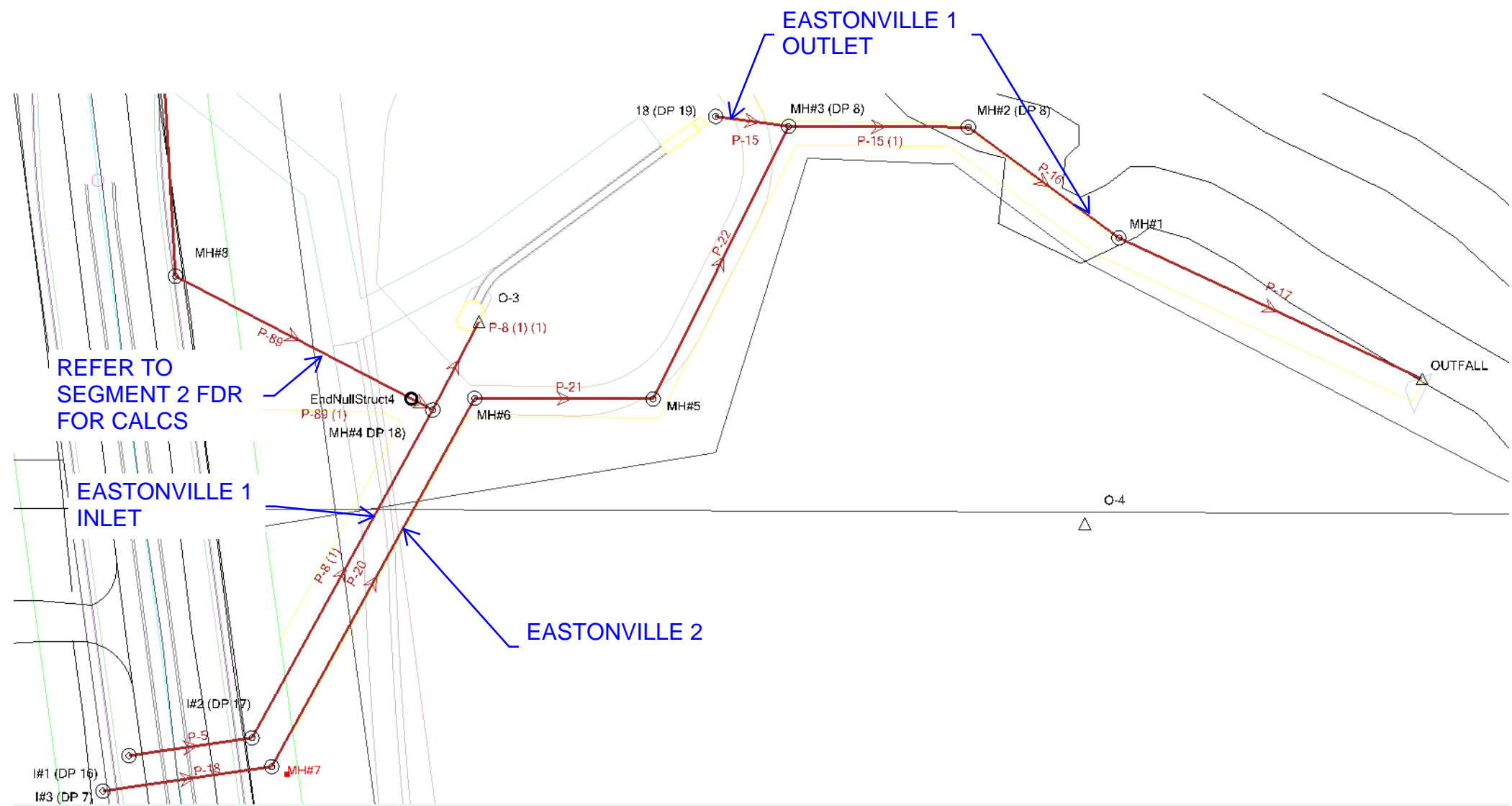
Depth (ft) = 0.50
Q (cfs) = 7.707
Area (sqft) = 1.67
Velocity (ft/s) = 4.63
Wetted Perim (ft) = 4.33
Crit Depth, Yc (ft) = 0.50
Top Width (ft) = 3.33
EGL (ft) = 0.83

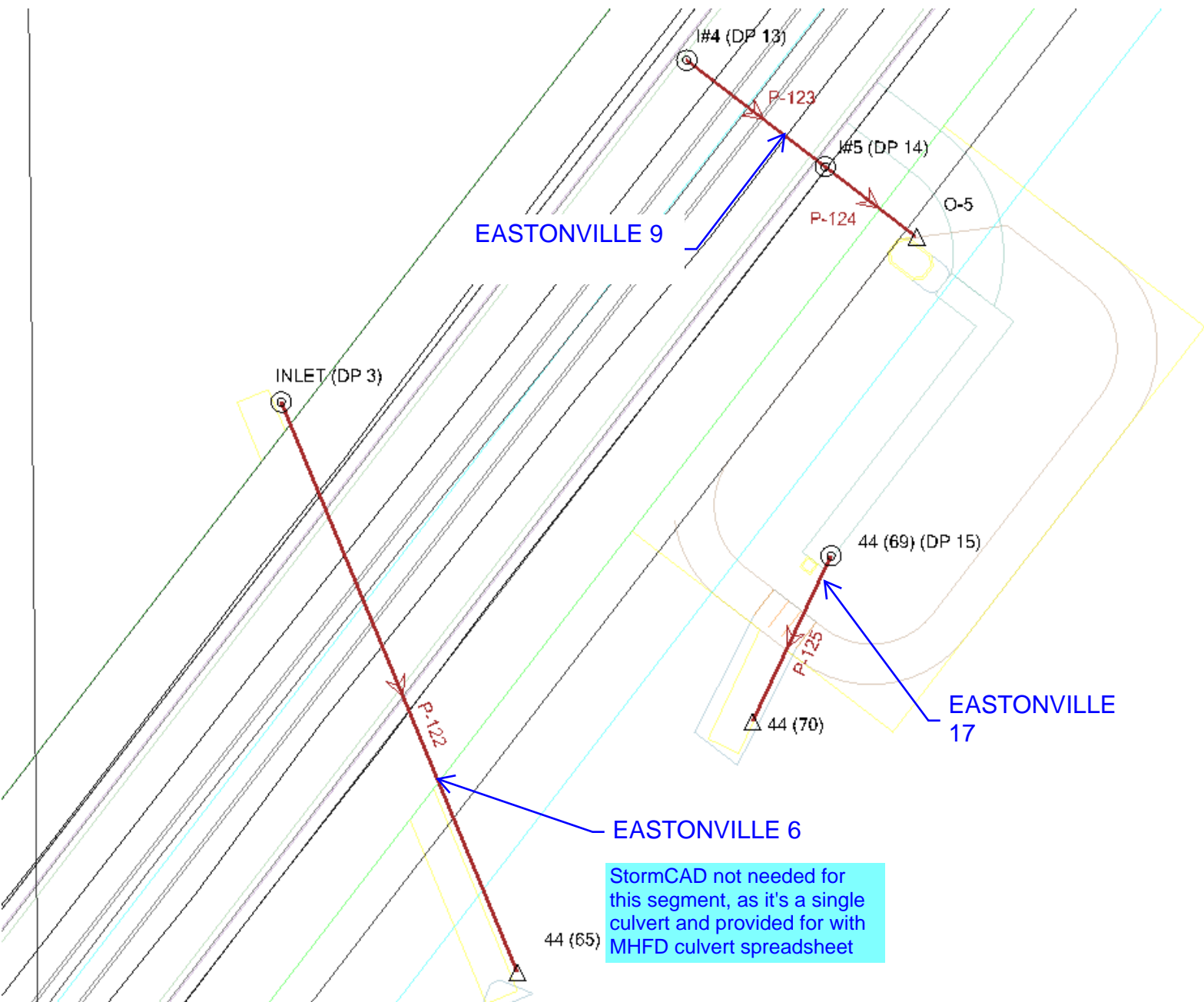


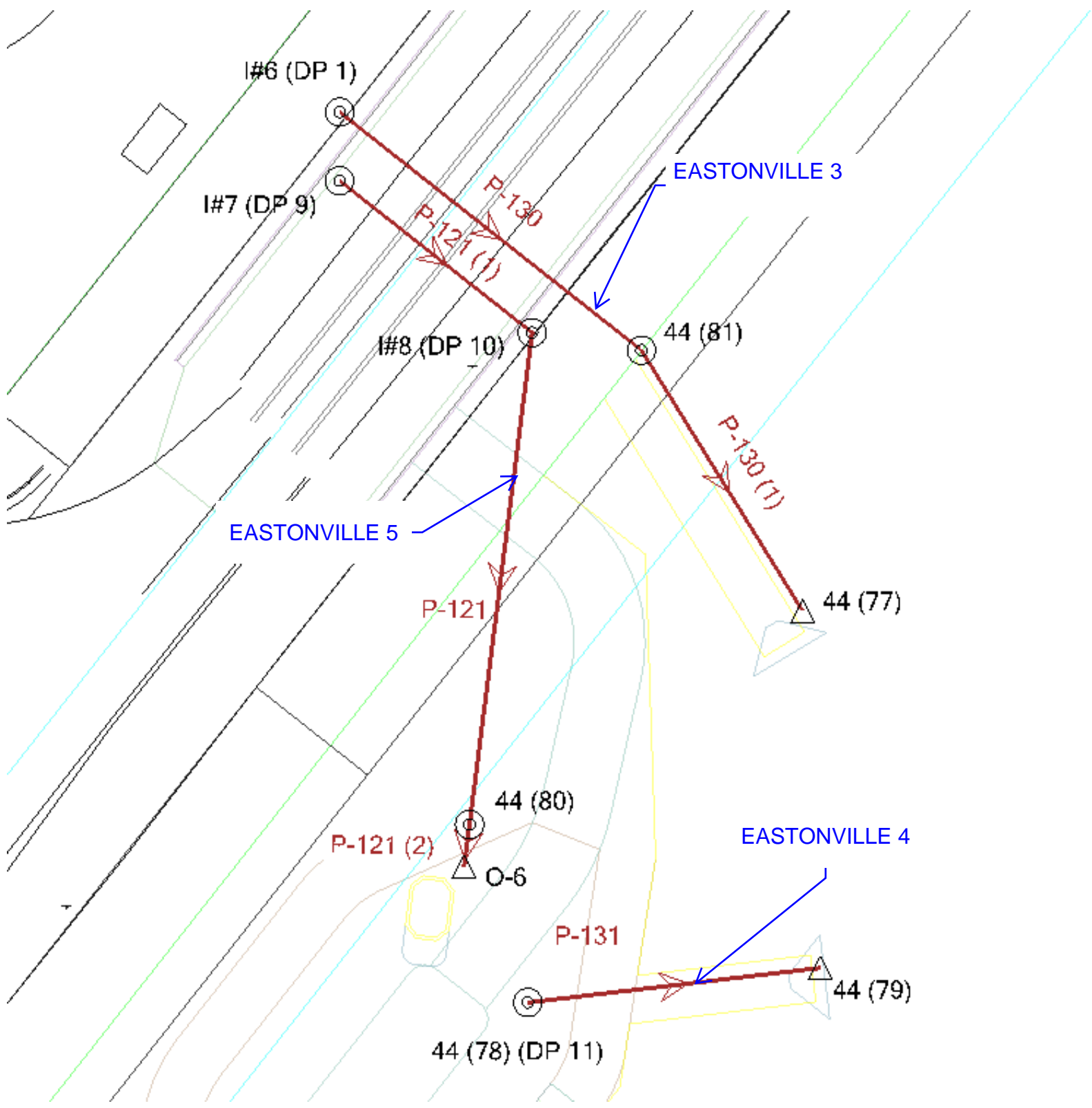
STORMCAD NETWORK LAYOUT: SEGMENT 1

MATCHLINE REFER TO SEGMENT 2 FDR









100 YEAR TAILWATER CONDITION: PIPE SUMMARY TABLE

| | Label | Start Node | Invert (Start) (ft) | Stop Node | Invert (Stop) (ft) | Length (User Defined) (ft) | Slope (Calculated) (ft/ft) | Diameter (in) | Manning's n | Flow (cfs) | Velocity (ft/s) | Capacity (Full Flow) (cfs) | Flow / Capacity (Design) (%) | Notes | Hydraulic Grade Line (In) (ft) | Hydraulic Grade Line (Out) (ft) |
|------------------|---------------|-----------------|---------------------|-----------------|--------------------|----------------------------|----------------------------|---------------|-------------|------------|-----------------|----------------------------|------------------------------|----------------|--------------------------------|---------------------------------|
| 66: P-8 (1) (1) | P-8 (1) (1) | MH#4 DP 18) | 6,985.66 | O-3 | 6,984.83 | 41.6 | 0.020 | 24.0 | 0.013 | 26.20 | 8.34 | 31.99 | 81.9 | Concrete Pipe | 6,988.54 | 6,987.98 |
| 67: P-124 | P-124 | I#5 (DP 14) | 6,981.25 | O-5 | 6,981.08 | 34.3 | 0.005 | 18.0 | 0.013 | 6.50 | 4.74 | 7.43 | 87.5 | Concrete Pipe | 6,982.33 | 6,982.10 |
| 68: P-121 (2) | P-121 (2) | 44 (80) | 6,970.65 | O-6 | 6,970.61 | 9.0 | 0.005 | 24.0 | 0.013 | 9.00 | 2.86 | 15.95 | 56.4 | Concrete Pipe | 6,972.88 | 6,972.87 |
| 69: P-18 | P-18 | I#3 (DP 7) | 6,985.73 | MH#7 | 6,985.38 | 71.3 | 0.005 | 42.0 | 0.013 | 53.30 | 8.11 | 71.14 | 74.9 | Concrete Pipe | 6,988.48 | 6,988.38 |
| 70: P-20 | P-20 | MH#7 | 6,985.38 | MH#6 | 6,984.50 | 175.6 | 0.005 | 42.0 | 0.013 | 53.30 | 8.11 | 71.14 | 74.9 | Concrete Pipe | 6,987.84 | 6,987.61 |
| 71: P-5 | P-5 | I#2 (DP 17) | 6,989.29 | I#1 (DP 16) | 6,989.74 | 52.0 | -0.009 | 18.0 | 0.013 | 5.10 | 5.59 | 9.77 | 52.2 | Concrete Pipe | 6,990.61 | 6,990.44 |
| 72: P-8 (1) | P-8 (1) | I#2 (DP 17) | 6,988.79 | MH#4 DP 18) | 6,985.66 | 156.4 | 0.020 | 24.0 | 0.013 | 10.50 | 9.12 | 31.99 | 32.8 | Concrete Pipe | 6,989.95 | 6,989.64 |
| 73: P-21 | P-21 | MH#6 | 6,984.50 | MH#5 | 6,984.13 | 74.6 | 0.005 | 42.0 | 0.013 | 53.30 | 8.11 | 71.14 | 74.9 | Concrete Pipe | 6,987.15 | 6,987.05 |
| 74: P-22 | P-22 | MH#5 | 6,984.13 | MH#3 (DP 8) | 6,981.11 | 127.1 | 0.024 | 42.0 | 0.013 | 53.30 | 14.61 | 154.95 | 34.4 | Concrete Pipe | 6,986.41 | 6,983.59 |
| 75: P-15 | P-15 | 18 (DP 19) | 6,983.26 | MH#3 (DP 8) | 6,983.11 | 30.8 | 0.005 | 18.0 | 0.013 | 3.00 | 3.98 | 7.43 | 40.4 | Concrete Pipe | 6,983.93 | 6,983.77 |
| 76: P-15 (1) | P-15 (1) | MH#3 (DP 8) | 6,981.11 | MH#2 (DP 8) | 6,980.73 | 75.1 | 0.005 | 42.0 | 0.013 | 1.77 | 3.13 | 71.14 | 2.5 | Concrete Pipe | 6,983.59 | 6,983.59 |
| 77: P-16 | P-16 | MH#2 (DP 8) | 6,980.63 | MH#1 | 6,980.24 | 78.1 | 0.005 | 42.0 | 0.013 | 54.30 | 8.14 | 71.14 | 76.3 | Concrete Pipe | 6,982.94 | 6,982.55 |
| 78: P-123 | P-123 | I#4 (DP 13) | 6,981.51 | I#5 (DP 14) | 6,981.25 | 52.0 | 0.005 | 18.0 | 0.013 | 3.40 | 4.11 | 7.43 | 45.8 | Concrete Pipe | 6,982.73 | 6,982.69 |
| 79: P-17 | P-17 | MH#1 | 6,980.14 | OUTFALL | 6,979.44 | 139.8 | 0.005 | 42.0 | 0.013 | 54.30 | 8.14 | 71.14 | 76.3 | Concrete Pipe | 6,982.45 | 6,981.73 |
| 80: P-125 | P-125 | 44 (69) (DP 15) | 6,978.42 | 44 (70) | 6,977.55 | 54.5 | 0.016 | 18.0 | 0.013 | 1.20 | 4.67 | 13.30 | 9.0 | Concrete Pipe | 6,978.83 | 6,977.85 |
| 83: P-122 | P-122 | INLET (DP 3) | 6,978.16 | 44 (65) | 6,973.52 | 183.8 | 0.025 | 30.0 | 0.013 | 24.50 | 12.34 | 65.19 | 37.6 | Concrete Pipe | 6,979.85 | 6,974.58 |
| 84: P-121 | P-121 | I#8 (DP 10) | 6,971.18 | 44 (80) | 6,970.65 | 105.1 | 0.005 | 24.0 | 0.013 | 9.00 | 5.26 | 16.06 | 56.0 | Concrete Pipe | 6,973.03 | 6,972.89 |
| 85: P-130 | P-130 | I#6 (DP 1) | 6,970.85 | 44 (81) | 6,970.04 | 81.5 | 0.010 | 18.0 | 0.013 | 3.60 | 5.37 | 10.47 | 34.4 | Concrete Pipe | 6,971.57 | 6,970.79 |
| 86: P-130 (1) | P-130 (1) | 44 (81) | 6,970.04 | 44 (77) | 6,969.39 | 65.0 | 0.010 | 18.0 | 0.013 | 3.60 | 5.39 | 10.50 | 34.3 | Concrete Pipe | 6,970.76 | 6,970.00 |
| 87: P-121 (1) | P-121 (1) | I#8 (DP 10) | 6,971.68 | I#7 (DP 9) | 6,971.95 | 52.0 | -0.005 | 18.0 | 0.013 | 4.10 | 4.37 | 7.57 | 54.2 | Concrete Pipe | 6,973.24 | 6,973.18 |
| 88: P-131 | P-131 | 44 (78) (DP 11) | 6,968.42 | 44 (79) | 6,967.50 | 62.5 | 0.015 | 18.0 | 0.013 | 1.40 | 4.75 | 12.77 | 11.0 | Concrete Pipe | 6,968.87 | 6,967.84 |
| 126: P-111 | P-111 | MH#34 | 7,019.01 | MH#39 | 7,017.01 | 146.6 | 0.014 | 18.0 | 0.013 | 3.40 | 5.94 | 12.28 | 27.7 | Concrete Pipe | 7,019.72 | 7,017.55 |
| 127: P-89 | P-89 | MH#8 | 6,986.87 | MH#4 DP 18) | 6,985.66 | 111.1 | 0.011 | 24.0 | 0.013 | 19.10 | 6.08 | 23.64 | 80.8 | Concrete Pipe | 6,990.43 | 6,989.64 |
| 128: P-25 (1) | P-25 (1) | CULVERT 2 (...) | 6,997.01 | O-10 | 6,995.27 | 116.5 | 0.015 | | 0.013 | 295.50 | 16.72 | 461.86 | 64.0 | Concrete Box C | 7,000.01 | 6,997.28 |
| 129: P-25 | P-25 | CULVERT 1 (...) | 6,997.01 | O-7 | 6,995.27 | 116.6 | 0.015 | | 0.013 | 245.50 | 15.71 | 461.72 | 53.2 | Concrete Box C | 6,999.67 | 6,997.02 |
| 131: P-107 (2) | P-107 (2) (1) | MH#26 (DP6.1) | 7,021.10 | DP9 | 7,020.49 | 60.7 | 0.010 | 24.0 | 0.013 | 22.40 | 8.21 | 22.62 | 99.0 | Concrete Pipe | 7,022.79 | 7,022.11 |
| 132: P-103 | P-103 | I#9 (DP6) | 7,022.86 | MH#26 (DP6.1) | 7,021.84 | 42.7 | 0.024 | 18.0 | 0.013 | 2.40 | 1.36 | 16.22 | 14.8 | Concrete Pipe | 7,024.53 | 7,024.51 |
| 133: P-107 (2) | P-107 (2) | MH#27 (DP8) | 7,021.66 | MH#26 (DP6.1) | 7,021.09 | 56.6 | 0.010 | 24.0 | 0.013 | 21.00 | 6.68 | 22.62 | 92.8 | Concrete Pipe | 7,025.00 | 7,024.51 |
| 134: P-107 | P-107 | DP 7 | 7,023.01 | MH#27 (DP8) | 7,022.41 | 37.8 | 0.016 | 15.0 | 0.013 | 2.20 | 1.79 | 8.13 | 27.1 | Concrete Pipe | 7,025.67 | 7,025.62 |
| 135: P-107 (1) | P-107 (1) | MH#27 (DP8) | 7,021.66 | DP 2 | 7,021.66 | 43.9 | 0.000 | 24.0 | 0.013 | 18.80 | 5.98 | 2.17 | 865.7 | Concrete Pipe | 7,025.93 | 7,025.62 |
| 136: P-95 | P-95 | I#8 (DP5) | 7,023.30 | I#9 (DP6) | 7,023.06 | 47.5 | 0.005 | 18.0 | 0.013 | 1.30 | 3.16 | 7.43 | 17.5 | Concrete Pipe | 7,024.57 | 7,024.56 |
| 137: P-93 | P-93 | I#6 (DP2.1) | 7,022.36 | I#7 (DP3.1) | 7,021.80 | 55.9 | 0.010 | 18.0 | 0.013 | 1.50 | 4.22 | 10.51 | 14.3 | Concrete Pipe | 7,022.99 | 7,023.02 |
| 138: Pipe - (34) | Pipe - (34) | I#7 (DP3.1) | 7,021.80 | FES OUTFALL 1 | 7,021.01 | 33.5 | 0.023 | 18.0 | 0.013 | 3.20 | 7.09 | 16.07 | 19.9 | Concrete Pipe | 7,023.01 | 7,023.00 |
| 140: P-44 (1) | P-44 (1) | MH#20 | 7,001.18 | MH#21 | 6,998.52 | 266.5 | 0.010 | 48.0 | 0.013 | 112.10 | 8.92 | 143.63 | 78.0 | Concrete Pipe | 7,005.57 | 7,003.94 |
| 141: P-64 | P-64 | MH#21 | 6,998.52 | MH#22 | 6,995.26 | 316.5 | 0.010 | 48.0 | 0.013 | 112.10 | 12.80 | 145.88 | 76.8 | Concrete Pipe | 7,001.72 | 6,997.89 |
| 142: P-44 | P-44 | MH#19 | 7,003.94 | MH#20 | 7,001.28 | 266.5 | 0.010 | 48.0 | 0.013 | 112.10 | 12.64 | 143.63 | 78.0 | Concrete Pipe | 7,007.14 | 7,005.63 |
| 143: P-26 | P-26 | DP 3 | 7,005.01 | MH#19 | 7,004.04 | 81.5 | 0.012 | 48.0 | 0.013 | 112.10 | 8.92 | 156.73 | 71.5 | Concrete Pipe | 7,009.86 | 7,009.36 |
| 144: P-64 (1) | P-64 (1) | MH#22 | 6,995.15 | MH#23 | 6,988.82 | 316.6 | 0.020 | 48.0 | 0.013 | 112.10 | 16.57 | 203.15 | 55.2 | Concrete Pipe | 6,998.35 | 6,994.29 |
| 145: P-87 | P-87 | MH#10 (DP 1...) | 6,994.25 | MH#9 | 6,989.76 | 320.7 | 0.014 | 24.0 | 0.013 | 19.10 | 9.26 | 26.78 | 71.3 | Concrete Pipe | 6,995.82 | 6,992.24 |
| 146: P-87 (1) | P-87 (1) | MH#9 | 6,989.76 | MH#8 | 6,986.87 | 197.4 | 0.015 | 24.0 | 0.013 | 19.10 | 6.08 | 27.33 | 69.9 | Concrete Pipe | 6,992.21 | 6,990.80 |
| 147: P-84 | P-84 | I#4 (DP14) | 6,995.69 | MH#10 (DP 1...) | 6,994.25 | 8.1 | 0.179 | 18.0 | 0.013 | 8.80 | 4.98 | 44.40 | 19.8 | Concrete Pipe | 6,997.31 | 6,997.25 |
| 148: P-84 (1) | P-84 (1) | MH#10 (DP 1...) | 6,994.75 | I#5 (DP 15) | 6,995.50 | 53.9 | -0.014 | 18.0 | 0.013 | 10.40 | 5.89 | 12.40 | 83.9 | Concrete Pipe | 6,997.78 | 6,997.25 |
| 149: P-66 | P-66 | MH#23 | 6,988.82 | MH#24 | 6,988.08 | 149.0 | 0.005 | 48.0 | 0.013 | 112.10 | 8.92 | 101.56 | 110.4 | Concrete Pipe | 6,994.23 | 6,993.32 |
| 150: P-68 | P-68 | MH#24 | 6,988.08 | MH#25 (DP13) | 6,987.54 | 107.8 | 0.005 | 48.0 | 0.013 | 112.10 | 8.92 | 101.56 | 110.4 | Concrete Pipe | 6,993.36 | 6,992.70 |
| 151: P-77 | P-77 | DP12 | 6,990.32 | MH#25 (DP13) | 6,990.03 | 28.1 | 0.010 | 18.0 | 0.013 | 24.40 | 13.81 | 10.66 | 228.8 | Concrete Pipe | 6,994.22 | 6,992.70 |
| 152: P-74 | P-74 | MH#25 (DP13) | 6,987.54 | OUTLET SEGM... | 6,986.67 | 173.3 | 0.005 | 48.0 | 0.013 | 136.40 | 10.85 | 101.56 | 134.3 | Concrete Pipe | 6,991.97 | 6,990.15 |

NOTE: EASTONVILLE 5 SEGMENTS HAVE BEEN ANALYZED IN THE FREE OUTFALL CONDITION BELOW TO MEET CAPACITY & VELOCITY REQUIREMENTS. SEGMENT 2 PIPES & STRUCTURES INCLUDED IN TABLE, REFER TO FDR FOR COMPLETE ANALYSIS.

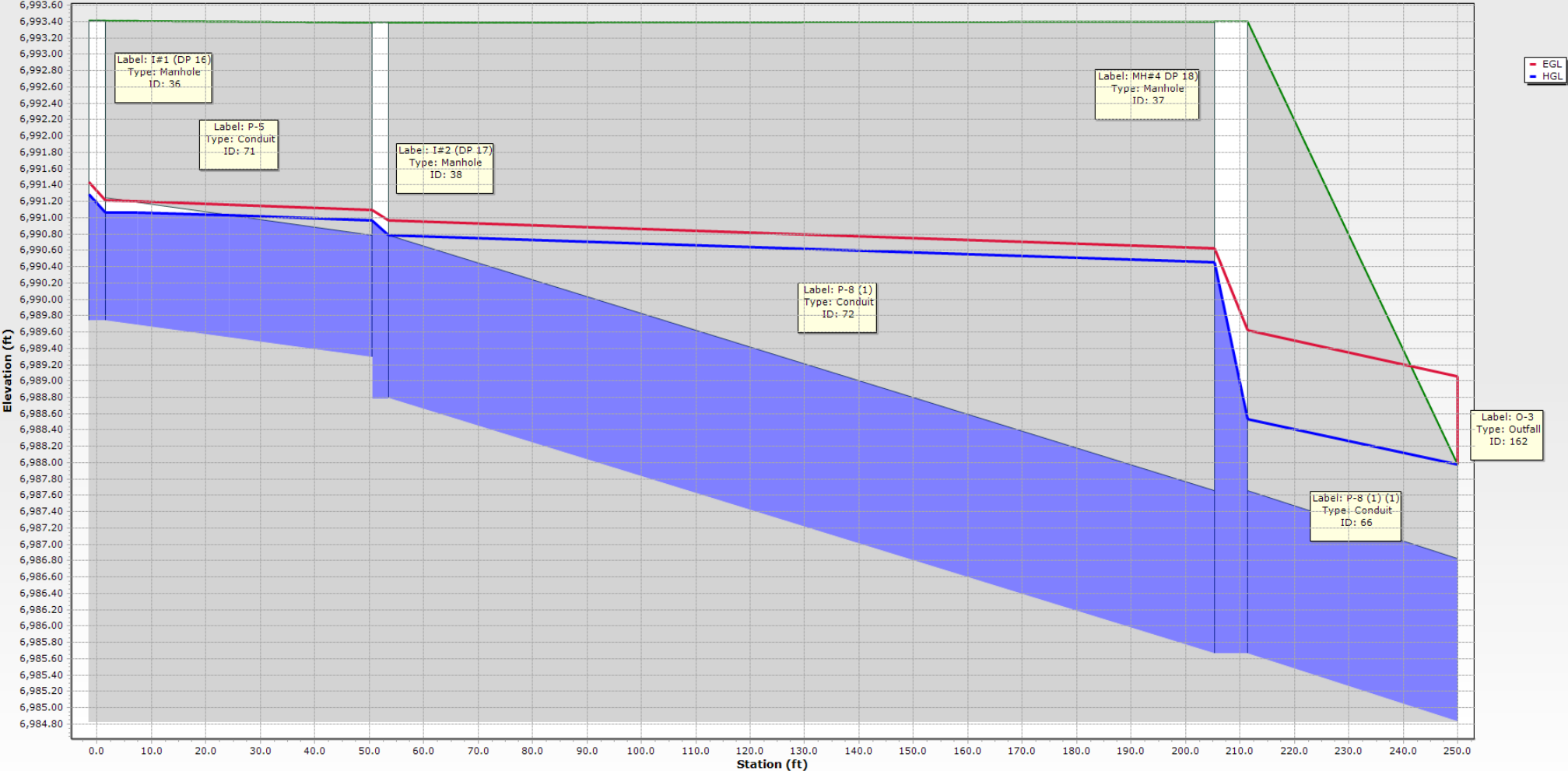
100 YEAR TAILWATER CONDITION: STRUCTURE SUMMARY TABLE

| | Label | Elevation (Ground) (ft) | Elevation (Rim) (ft) | Flow (Total Out) (cfs) | Depth (Out) (ft) | Hydraulic Grade Line (Out) (ft) | Hydraulic Grade Line (In) (ft) | Notes | Elevation (Invert Out) (ft) | Headloss (ft) |
|-----------------|-----------------|-------------------------|----------------------|------------------------|------------------|---------------------------------|--------------------------------|---------------|-----------------------------|---------------|
| 35: MH#7 | MH#7 | 6,993.52 | 6,993.52 | 53.30 | 2.47 | 6,987.84 | 6,988.38 | STORM MH | 6,985.38 | 0.54 |
| 36: I#1 (DP 16) | I#1 (DP 16) | 6,993.41 | 6,993.41 | 5.10 | 0.87 | 6,990.61 | 6,991.15 | CDOT Type- | 6,989.74 | 0.54 |
| 37: MH#4 DP | MH#4 DP 18) | 6,993.40 | 6,993.40 | 26.20 | 2.88 | 6,988.54 | 6,989.64 | STORM MH | 6,985.66 | 1.10 |
| 38: I#2 (DP 17) | I#2 (DP 17) | 6,993.39 | 6,993.39 | 10.50 | 1.17 | 6,989.95 | 6,990.44 | CDOT Type- | 6,988.79 | 0.49 |
| 39: MH#6 | MH#6 | 6,993.02 | 6,993.02 | 53.30 | 2.65 | 6,987.15 | 6,987.61 | STORM MH | 6,984.50 | 0.46 |
| 40: MH#5 | MH#5 | 6,991.91 | 6,991.91 | 53.30 | 2.28 | 6,986.41 | 6,987.05 | STORM MH | 6,984.13 | 0.64 |
| 41: MH#3 (DP | MH#3 (DP 8) | 6,991.13 | 6,991.13 | 1.77 | 2.48 | 6,983.59 | 6,983.59 | STORM MH | 6,981.11 | 0.00 |
| 42: I#3 (DP 7) | I#3 (DP 7) | 6,990.73 | 6,990.73 | 53.30 | 2.83 | 6,988.48 | 6,989.49 | CDOT Type- | 6,985.73 | 1.01 |
| 43: 18 (DP 19) | 18 (DP 19) | 6,988.71 | 6,988.71 | 3.00 | 2.43 | 6,983.93 | 6,984.30 | CDOT Type- | 6,983.26 | 0.37 |
| 44: MH#2 (DP | MH#2 (DP 8) | 6,985.74 | 6,985.74 | 54.30 | 2.31 | 6,982.94 | 6,983.59 | STORM MH | 6,980.63 | 0.65 |
| 45: I#4 (DP 13) | I#4 (DP 13) | 6,985.02 | 6,985.02 | 3.40 | 1.42 | 6,982.73 | 6,982.84 | CDOT Type- | 6,981.51 | 0.12 |
| 46: I#5 (DP 14) | I#5 (DP 14) | 6,985.02 | 6,985.02 | 6.50 | 1.28 | 6,982.33 | 6,982.69 | CDOT Type- | 6,981.25 | 0.36 |
| 47: MH#1 | MH#1 | 6,984.95 | 6,984.95 | 54.30 | 2.31 | 6,982.45 | 6,982.55 | STORM MH | 6,980.14 | 0.10 |
| 49: 44 (69) (D | 44 (69) (DP 15) | 6,982.64 | 6,982.64 | 1.20 | 0.41 | 6,978.83 | 6,978.85 | CDOT Type- | 6,978.42 | 0.01 |
| 55: 44 (80) | 44 (80) | 6,975.21 | 6,975.21 | 9.00 | 2.13 | 6,972.88 | 6,972.89 | Cylindrical S | 6,970.65 | 0.01 |
| 56: 44 (81) | 44 (81) | 6,975.03 | 6,975.03 | 3.60 | 0.72 | 6,970.76 | 6,970.79 | Cylindrical S | 6,970.04 | 0.03 |
| 57: I#7 (DP 9) | I#7 (DP 9) | 6,974.64 | 6,974.64 | 4.10 | 1.29 | 6,973.24 | 6,973.39 | CDOT Type- | 6,971.95 | 0.15 |
| 58: I#8 (DP 10) | I#8 (DP 10) | 6,974.64 | 6,974.64 | 9.00 | 1.85 | 6,973.03 | 6,973.18 | CDOT Type- | 6,971.18 | 0.15 |
| 59: I#6 (DP 1) | I#6 (DP 1) | 6,973.20 | 6,973.20 | 3.60 | 0.72 | 6,971.57 | 6,972.00 | CDOT Type- | 6,970.85 | 0.42 |
| 60: 44 (78) (D | 44 (78) (DP 11) | 6,973.16 | 6,973.16 | 1.40 | 0.44 | 6,968.87 | 6,969.03 | CDOT Type- | 6,968.42 | 0.16 |
| 98: MH#26 (D | MH#26 (DP6.1) | 7,027.15 | 7,027.15 | 22.40 | 1.69 | 7,022.79 | 7,024.51 | STORM MH | 7,021.10 | 1.73 |
| 99: MH#27 (D | MH#27 (DP8) | 7,027.09 | 7,027.09 | 21.00 | 3.34 | 7,025.00 | 7,025.62 | STORM MH | 7,021.66 | 0.62 |
| 100: I#9 (DP6) | I#9 (DP6) | 7,027.04 | 7,027.04 | 2.40 | 1.67 | 7,024.53 | 7,024.56 | CDOT Type- | 7,022.86 | 0.03 |
| 101: I#8 (DP5) | I#8 (DP5) | 7,026.63 | 7,026.63 | 1.30 | 1.27 | 7,024.57 | 7,024.58 | CDOT Type- | 7,023.30 | 0.02 |
| 102: I#7 (DP3) | I#7 (DP3.1) | 7,026.51 | 7,026.51 | 3.20 | 1.71 | 7,023.01 | 7,023.02 | CDOT Type- | 7,021.80 | 0.00 |
| 103: I#6 (DP2) | I#6 (DP2.1) | 7,026.40 | 7,026.40 | 1.50 | 0.63 | 7,022.99 | 7,023.10 | CDOT Type- | 7,022.36 | 0.10 |
| 106: MH#34 | MH#34 | 7,023.51 | 7,023.51 | 3.40 | 0.70 | 7,019.72 | 7,019.84 | CDOT Type- | 7,019.01 | 0.13 |
| 111: MH#21 | MH#21 | 7,014.03 | 7,014.03 | 112.10 | 3.20 | 7,001.72 | 7,003.94 | STORM MH | 6,998.52 | 2.22 |
| 112: MH#20 | MH#20 | 7,012.41 | 7,012.41 | 112.10 | 4.38 | 7,005.57 | 7,005.63 | STORM MH | 7,001.18 | 0.06 |
| 113: MH#19 | MH#19 | 7,010.85 | 7,010.85 | 112.10 | 3.20 | 7,007.14 | 7,009.36 | STORM MH | 7,003.94 | 2.22 |
| 115: MH#22 | MH#22 | 7,005.85 | 7,005.85 | 112.10 | 3.20 | 6,998.35 | 6,998.44 | STORM MH | 6,995.15 | 0.08 |
| 116: MH#9 | MH#9 | 7,001.03 | 7,001.03 | 19.10 | 2.45 | 6,992.21 | 6,992.24 | STORM MH | 6,989.76 | 0.03 |
| 117: I#4 (DP1) | I#4 (DP14) | 7,000.17 | 7,000.17 | 8.80 | 1.62 | 6,997.31 | 6,997.89 | CDOT Type- | 6,995.69 | 0.58 |
| 118: MH#10 (| MH#10 (DP 1... | 7,000.01 | 7,000.01 | 19.10 | 1.57 | 6,995.82 | 6,997.25 | STORM MH | 6,994.25 | 1.43 |
| 119: I#5 (DP 1 | I#5 (DP 15) | 6,999.67 | 6,999.67 | 10.40 | 1.88 | 6,997.78 | 6,998.59 | CDOT Type- | 6,995.50 | 0.81 |
| 120: MH#8 | MH#8 | 6,996.13 | 6,996.13 | 19.10 | 3.77 | 6,990.43 | 6,990.80 | STORM MH | 6,986.87 | 0.37 |
| 121: MH#23 | MH#23 | 6,995.25 | 6,995.25 | 112.10 | 5.41 | 6,994.23 | 6,994.29 | STORM MH | 6,988.82 | 0.06 |
| 122: MH#24 | MH#24 | 6,993.32 | 6,993.32 | 112.10 | 5.25 | 6,993.32 | 6,993.39 | STORM MH | 6,988.08 | 0.06 |
| 123: DP12 | DP12 | 6,993.02 | 6,993.02 | 24.40 | 2.71 | 6,993.02 | 6,997.47 | CDOT Type- | 6,990.32 | 4.44 |
| 124: MH#25 (| MH#25 (DP13) | 6,992.79 | 6,992.79 | 136.40 | 4.43 | 6,991.97 | 6,992.70 | STORM MH | 6,987.54 | 0.73 |
| 190: INLET (D | INLET (DP 3) | 6,980.96 | 6,980.96 | 24.50 | 1.69 | 6,979.85 | 6,980.98 | CDOT FES | 6,978.16 | 1.13 |
| 192: DP 7 | DP 7 | 7,024.45 | 7,024.45 | 2.20 | 1.44 | 7,024.45 | 7,024.52 | CDOT FES | 7,023.01 | 0.07 |
| 193: DP 2 | DP 2 | 7,024.26 | 7,024.26 | 18.80 | 2.25 | 7,024.26 | 7,025.10 | CDOT FES | 7,021.66 | 0.83 |
| 194: DP 3 | DP 3 | 7,009.43 | 7,009.43 | 112.10 | 4.42 | 7,009.43 | 7,011.29 | CDOT FES | 7,005.01 | 1.86 |
| 196: CULVERT | CULVERT 1 (...) | 7,000.01 | 7,000.01 | 245.50 | 2.66 | 6,999.67 | 7,001.66 | Dummy Null | 6,997.01 | 1.99 |
| 197: CULVERT | CULVERT 2 (...) | 7,000.01 | 7,000.01 | 295.50 | 3.00 | 7,000.01 | 7,002.27 | Dummy Null | 6,997.01 | 2.26 |

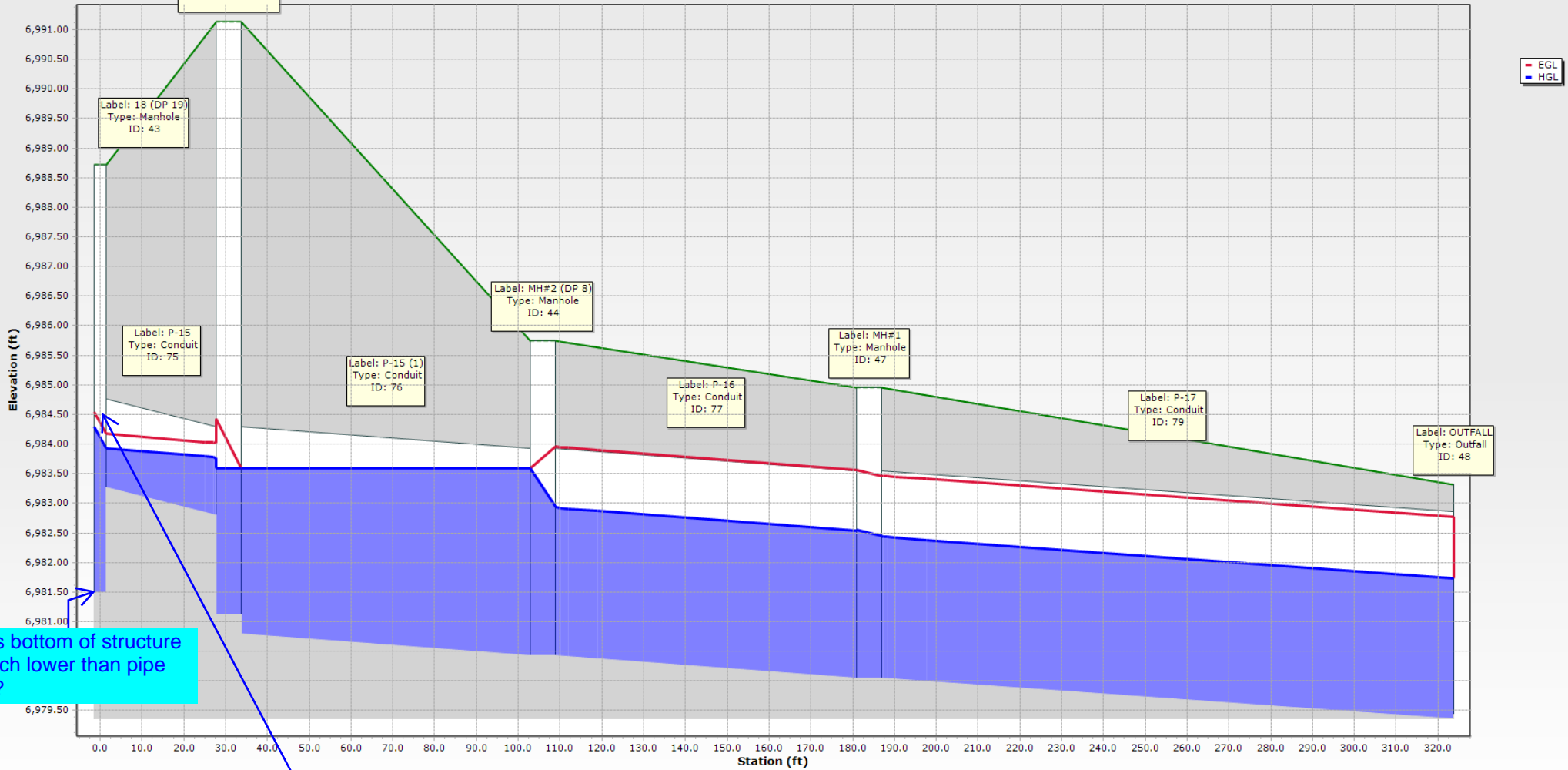
| | ID | Label | Elevation (Ground) (ft) | Elevation (Invert) (ft) | Elevation (User Defined Tailwater) (ft) | Hydraulic Grade (ft) | Flow (Total Out) (cfs) | Notes |
|-----------------------|-----|---------------|-------------------------|-------------------------|---|----------------------|------------------------|------------|
| 48: OUTFALL | 48 | OUTFALL | 6,983.32 | 6,979.44 | | 6,981.73 | 54.30 | CDOT FES |
| 53: 44 (70) | 53 | 44 (70) | 6,979.33 | 6,977.55 | | 6,977.85 | 1.20 | CDOT FES |
| 54: 44 (65) | 54 | 44 (65) | 6,976.31 | 6,973.52 | | 6,974.58 | 24.50 | CDOT FES |
| 61: 44 (77) | 61 | 44 (77) | 6,971.10 | 6,969.39 | | 6,970.00 | 3.60 | CDOT FES |
| 64: 44 (79) | 64 | 44 (79) | 6,969.82 | 6,967.50 | | 6,967.84 | 1.40 | CDOT FES |
| 107: DP9 | 107 | DP9 | 7,022.74 | 7,020.49 | | 7,022.11 | 22.40 | CDOT FES |
| 108: FES OUTFALL 1 | 108 | FES OUTFALL 1 | 7,023.00 | 7,021.01 | 7,023.00 | 7,023.00 | 3.20 | CDOT FES |
| 110: MH#39 | 110 | MH#39 | 7,018.18 | 7,017.01 | | 7,017.55 | 3.40 | CDOT FES |
| 125: OUTLET SEGMENT 3 | 125 | OUTLET SEG... | 6,991.09 | 6,986.67 | 6,988.30 | 6,990.15 | 136.40 | CDOT FES |
| 162: O-3 | 162 | O-3 | 6,987.98 | 6,984.83 | 6,987.98 | 6,987.98 | 26.20 | Dummy Null |
| 164: O-5 | 164 | O-5 | 6,982.10 | 6,981.08 | 6,982.10 | 6,982.10 | 6.50 | Dummy Null |
| 165: O-6 | 165 | O-6 | 6,972.87 | 6,970.61 | 6,972.87 | 6,972.87 | 9.00 | Dummy Null |
| 203: O-7 | 203 | O-7 | 6,998.27 | 6,995.27 | | 6,997.02 | 245.50 | Dummy Null |
| 207: O-10 | 207 | O-10 | 6,998.27 | 6,995.27 | | 6,997.28 | 295.50 | Dummy Null |

NOTE: EASTONVILLE 5 SEGMENTS HAVE BEEN ANALYZED IN THE FREE OUTFALL CONDITION BELOW TO MEET CAPACITY & VELOCITY REQUIREMENTS. SEGMENT 2 PIPES & STRUCTURES INCLUDED IN TABLE, REFER TO FDR FOR COMPLETE ANALYSIS.

EASTONVILLE 1 - INLET - 100-YR TAILWATER CONDITION



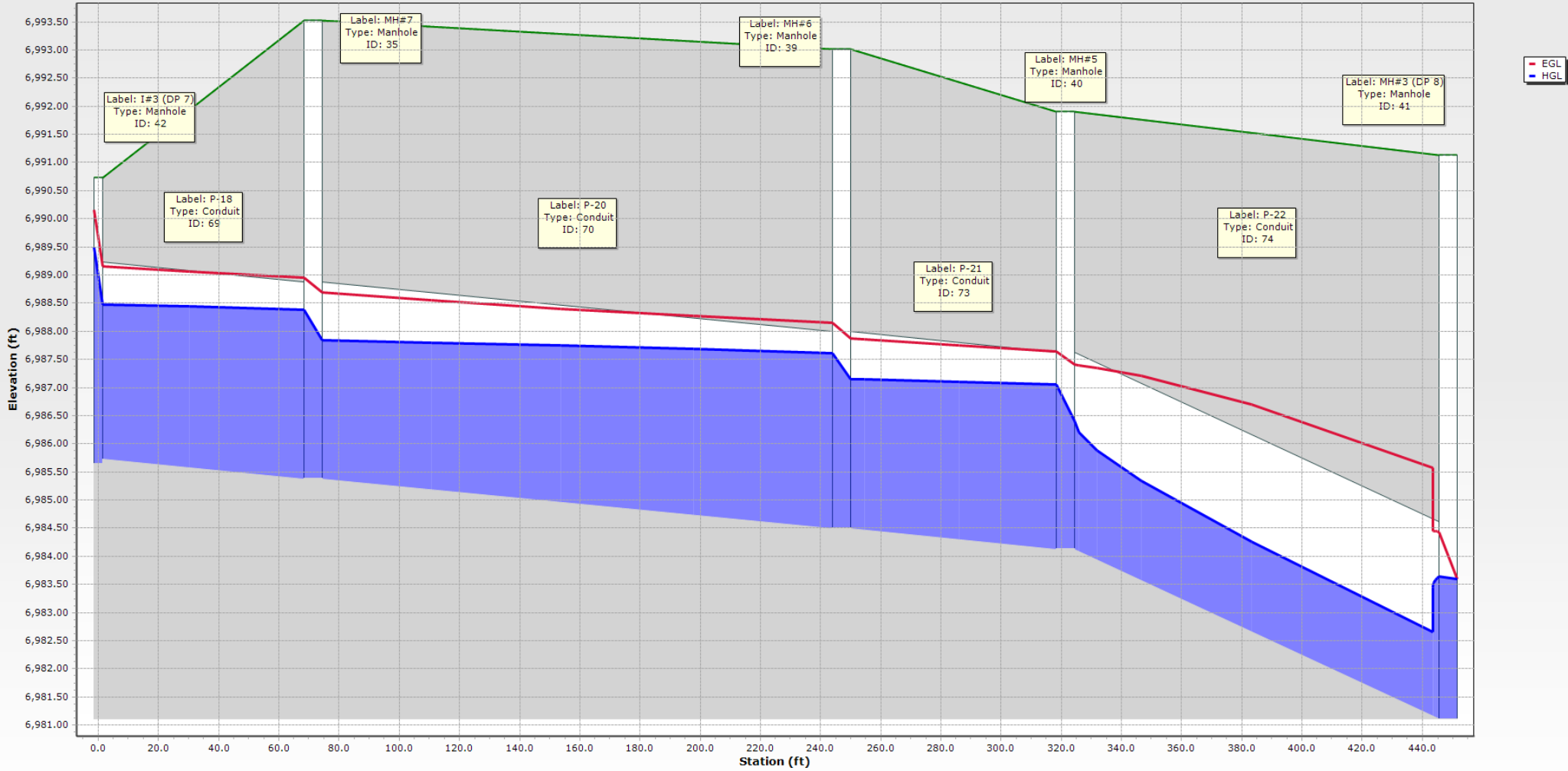
EASTONVILLE 1 - OUTLET - 100-YR TAILWATER CONDITION



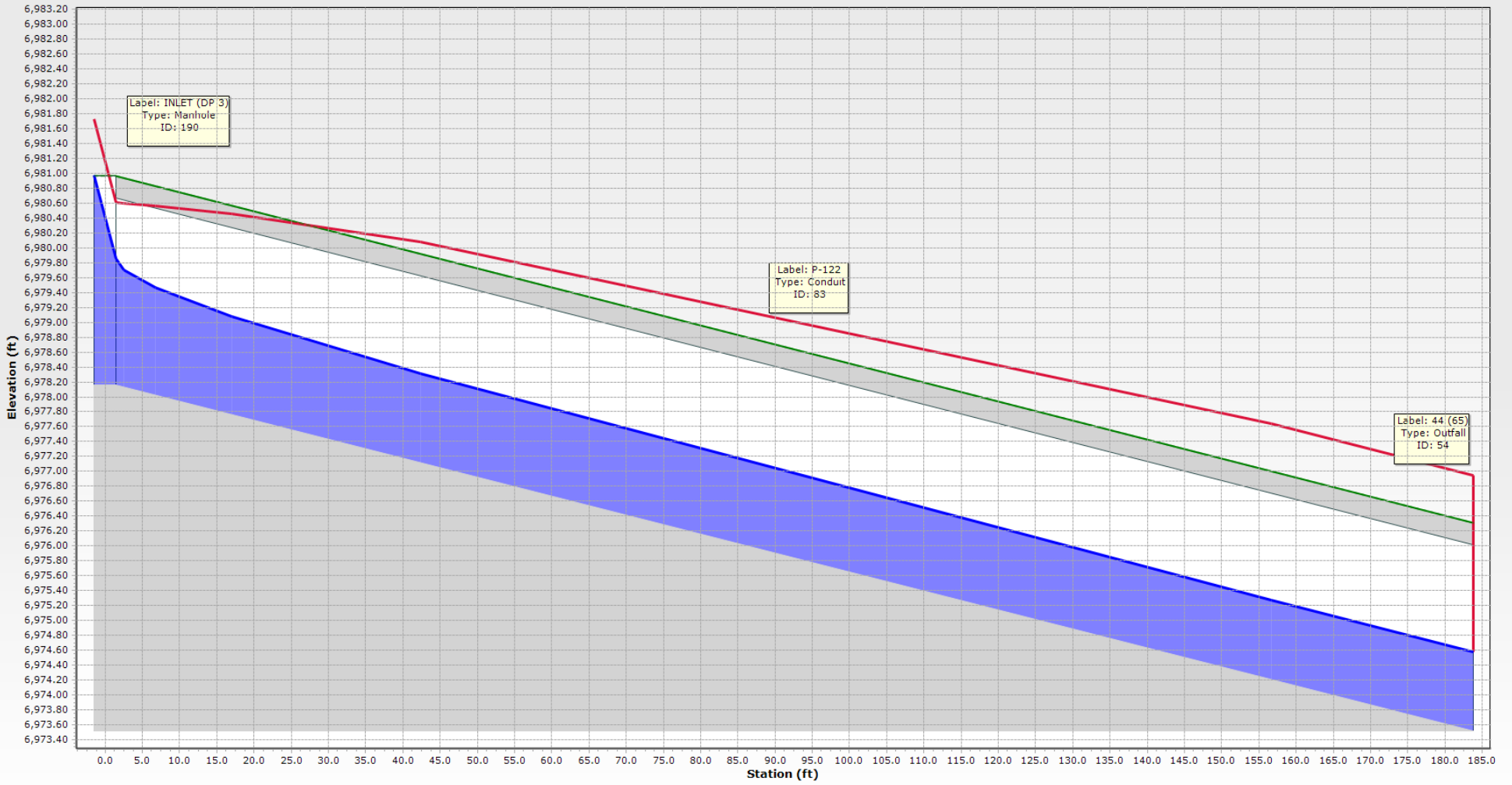
Why is bottom of structure much lower than pipe invert?

System design needs to start with 100-year water surface elevation in the pond

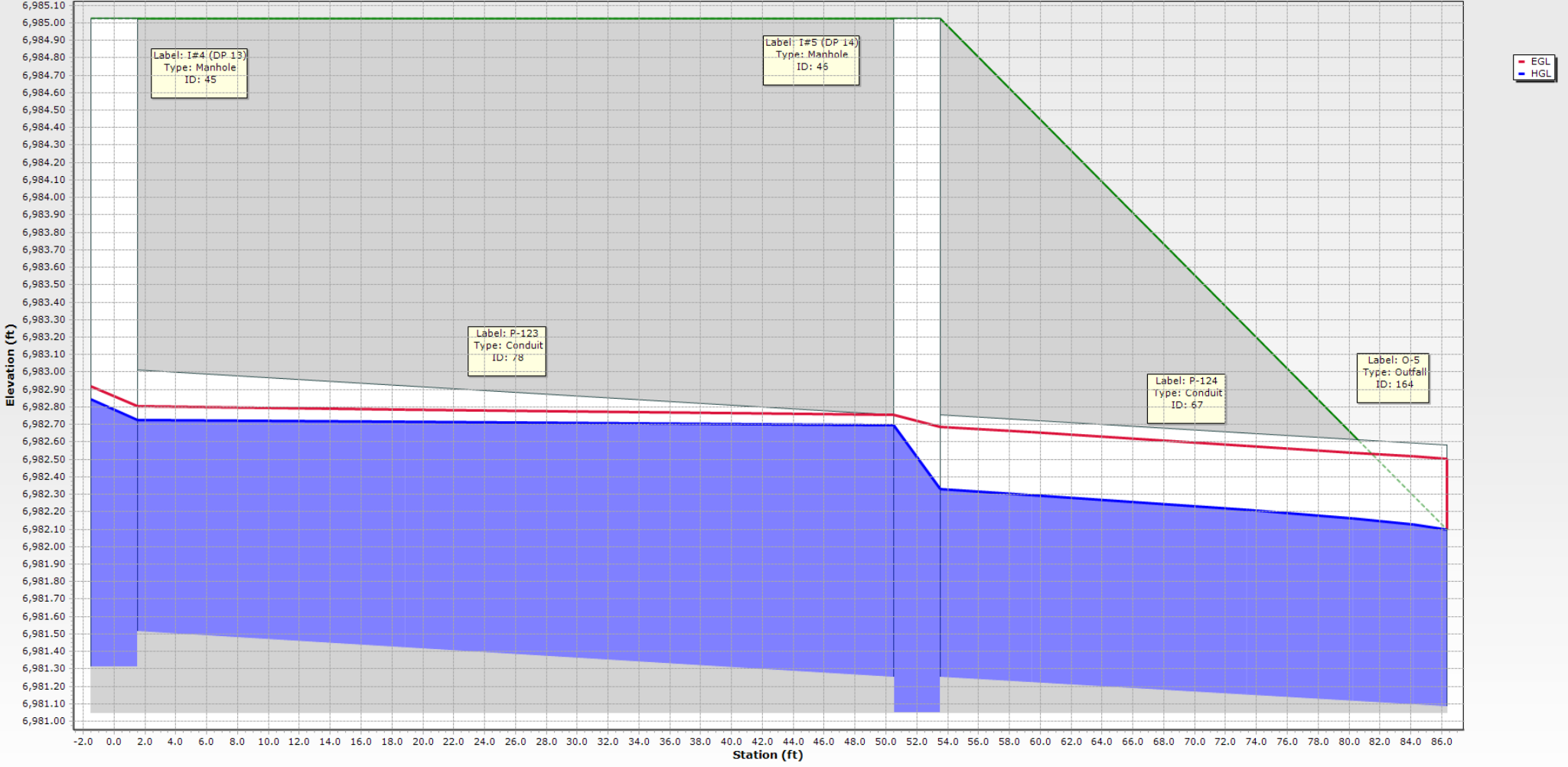
EASTONVILLE 2 - 100-YR TAILWATER CONDITION



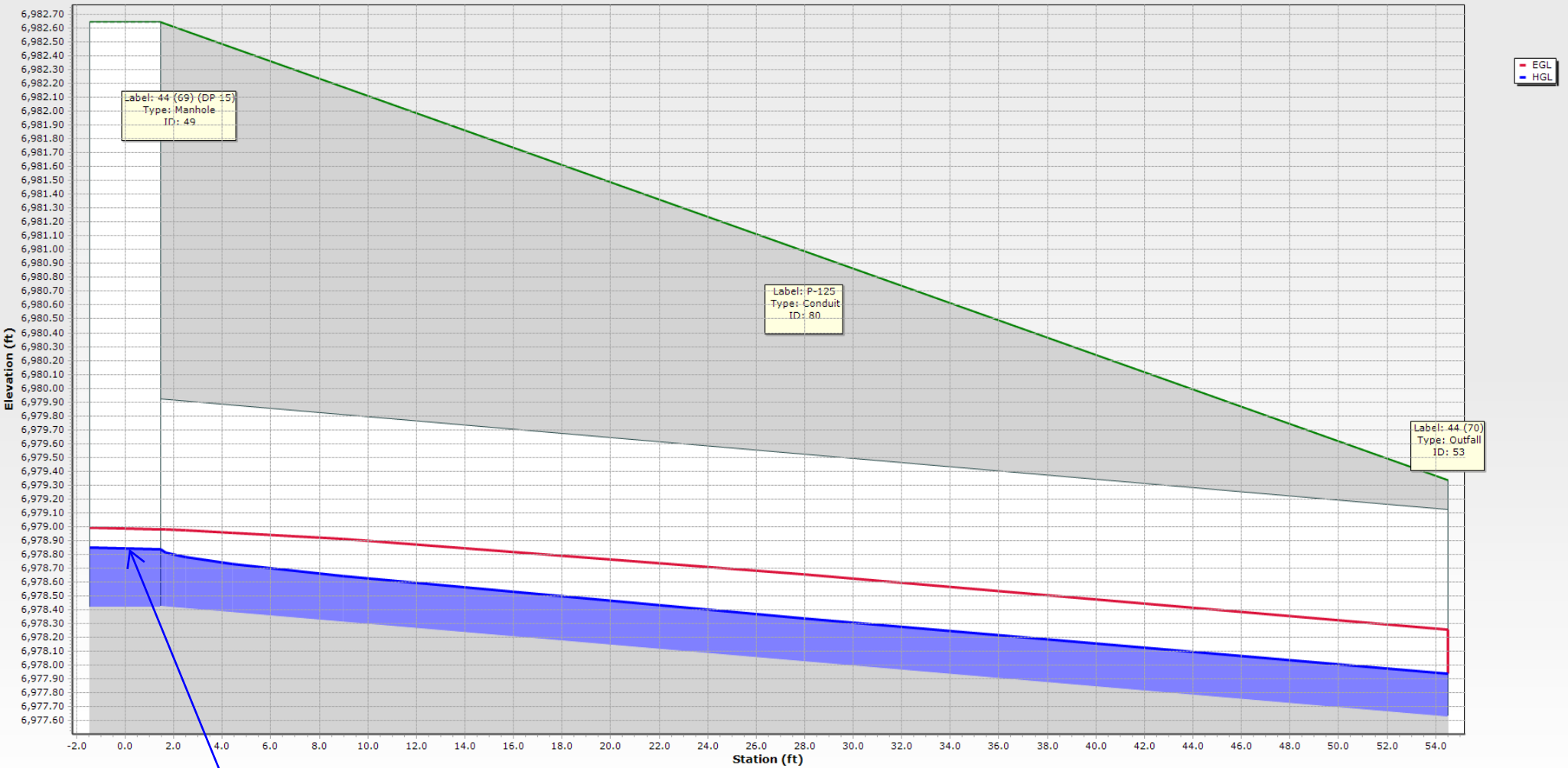
EASTONVILLE 6 - 100-YR TAILWATER CONDITION



EASTONVILLE 9 - 100-YR TAILWATER CONDITION

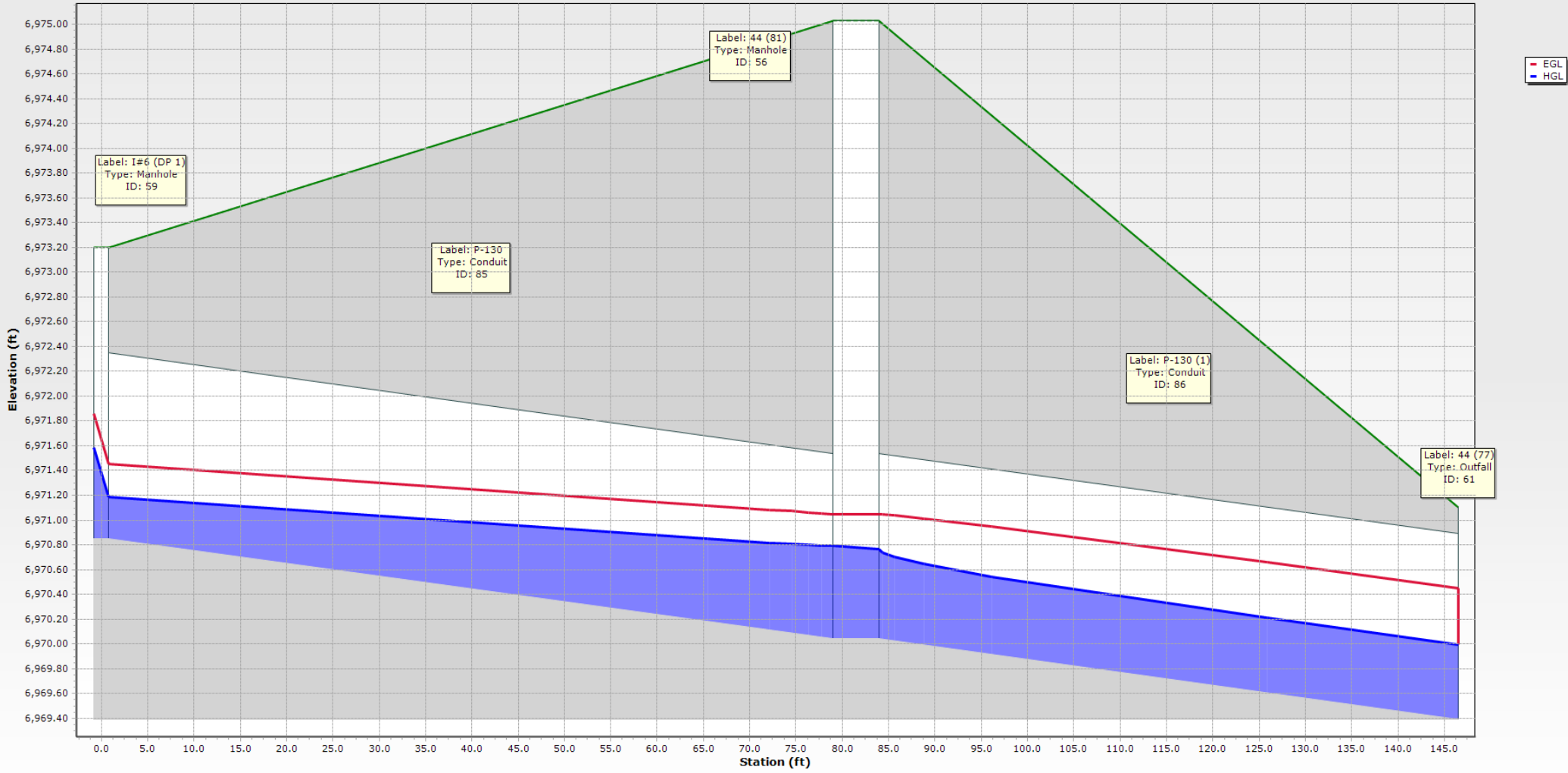


EASTONVILLE 17 - 100-YR TAILWATER CONDITION - Time: 0.00

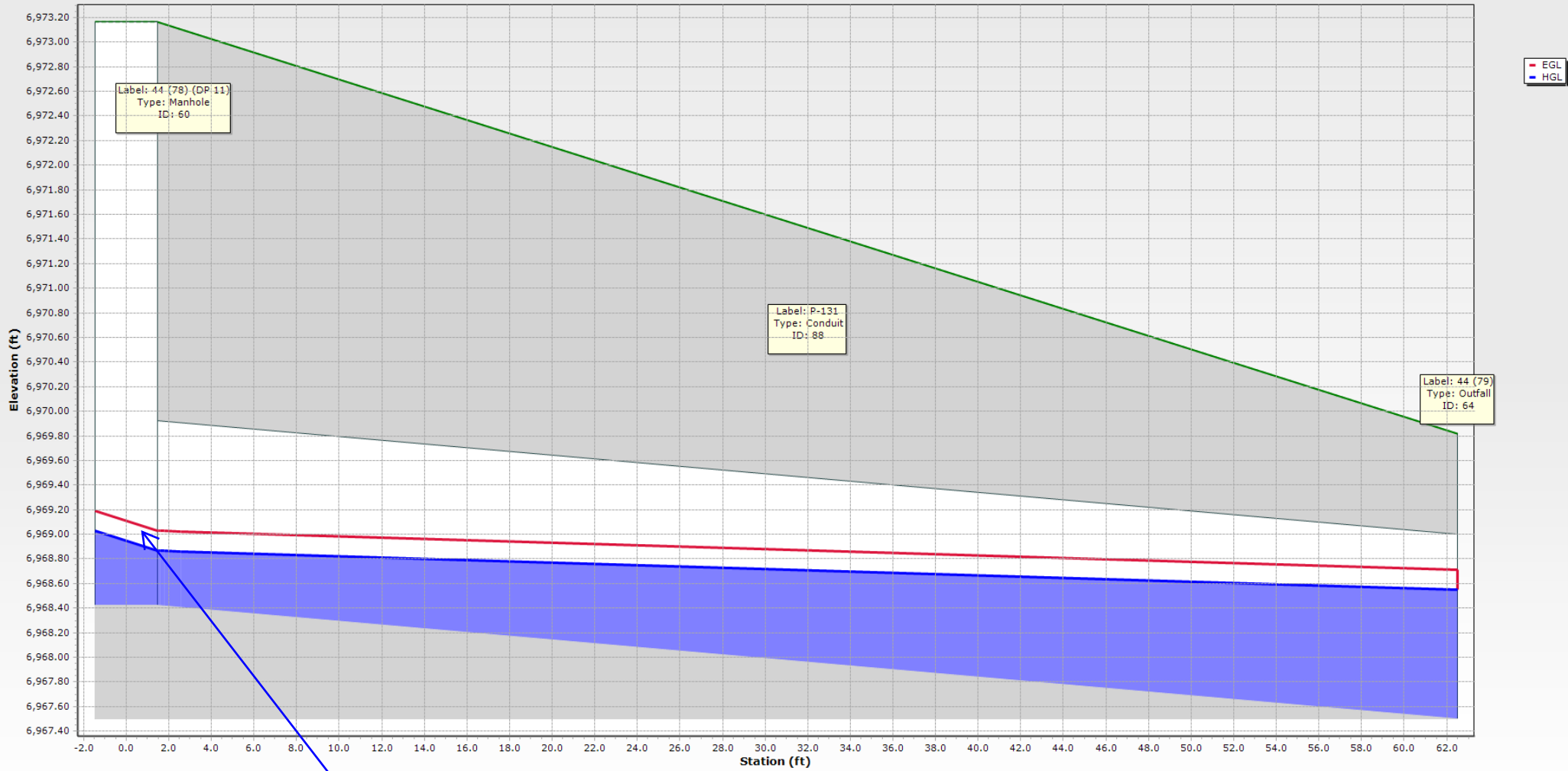


System design needs to start with 100-year water surface elevation in the pond

EASTONVILLE 3 - 100-YR TAILWATER CONDITION

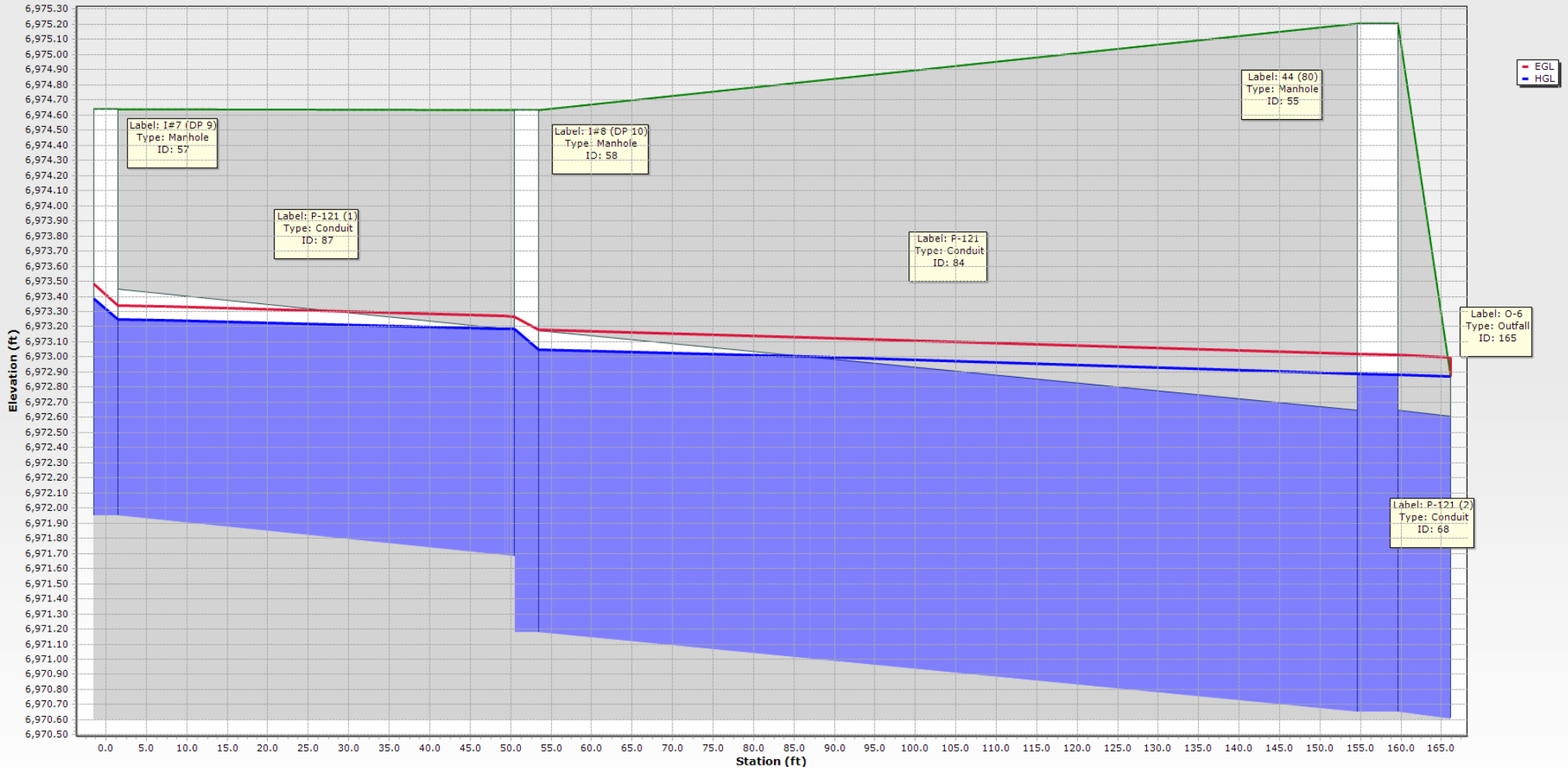


EASTONVILLE 4 - 100-YR TAILWATER CONDITION



System design needs to start with 100-year water surface elevation in the pond

EASTONVILLE 5 - 100-YR TAILWATER CONDITION



**NOTE: THIS SEGMENT HAS BEEN ANALYZED IN THE FREE
OUTFALL CONDITION BLEW TO MEET CAPACITY & VELOCITY
REQUIREMENTS**

5 YEAR TAILWATER CONDITION: PIPE SUMMARY TABLE

| | Label | Start Node | Invert (Start) (ft) | Stop Node | Invert (Stop) (ft) | Length (User Defined) (ft) | Slope (Calculated) (ft/ft) | Diameter (in) | Manning's n | Flow (cfs) | Velocity (ft/s) | Capacity (Full Flow) (cfs) | Flow / Capacity (Design) (%) | Notes | Hydraulic Grade Line (In) (ft) | Hydraulic Grade Line (Out) (ft) |
|------------------|---------------|-----------------|---------------------|----------------|--------------------|----------------------------|----------------------------|---------------|-------------|------------|-----------------|----------------------------|------------------------------|----------------|--------------------------------|---------------------------------|
| 66: P-8 (1) (1) | P-8 (1) (1) | MH#4 DP 18) | 6,985.66 | O-3 | 6,984.83 | 41.6 | 0.020 | 24.0 | 0.013 | 15.60 | 4.97 | 31.99 | 48.8 | Concrete Pipe | 6,988.57 | 6,988.37 |
| 67: P-124 | P-124 | I#5 (DP 14) | 6,981.25 | O-5 | 6,981.08 | 34.3 | 0.005 | 18.0 | 0.013 | 3.90 | 4.25 | 7.43 | 52.5 | Concrete Pipe | 6,982.28 | 6,982.25 |
| 68: P-121 (2) | P-121 (2) | 44 (80) | 6,970.65 | O-6 | 6,970.61 | 9.0 | 0.005 | 24.0 | 0.013 | 4.20 | 1.34 | 15.95 | 26.3 | Concrete Pipe | 6,973.23 | 6,973.23 |
| 69: P-18 | P-18 | I#3 (DP 7) | 6,985.73 | MH#7 | 6,985.38 | 71.3 | 0.005 | 42.0 | 0.013 | 7.90 | 4.88 | 71.14 | 11.1 | Concrete Pipe | 6,986.58 | 6,986.42 |
| 70: P-20 | P-20 | MH#7 | 6,985.38 | MH#6 | 6,984.50 | 175.6 | 0.005 | 42.0 | 0.013 | 7.90 | 4.88 | 71.14 | 11.1 | Concrete Pipe | 6,986.22 | 6,985.54 |
| 71: P-5 | P-5 | I#2 (DP 17) | 6,989.29 | I#1 (DP 16) | 6,989.74 | 52.0 | -0.009 | 18.0 | 0.013 | 3.00 | 4.87 | 9.77 | 30.7 | Concrete Pipe | 6,990.40 | 6,990.02 |
| 72: P-8 (1) | P-8 (1) | I#2 (DP 17) | 6,988.79 | MH#4 DP 18) | 6,985.66 | 156.4 | 0.020 | 24.0 | 0.013 | 6.30 | 7.92 | 31.99 | 19.7 | Concrete Pipe | 6,989.68 | 6,988.96 |
| 73: P-21 | P-21 | MH#6 | 6,984.50 | MH#5 | 6,984.13 | 74.6 | 0.005 | 42.0 | 0.013 | 7.90 | 4.88 | 71.14 | 11.1 | Concrete Pipe | 6,985.35 | 6,985.17 |
| 74: P-22 | P-22 | MH#5 | 6,984.13 | MH#3 (DP 8) | 6,981.11 | 127.1 | 0.024 | 42.0 | 0.013 | 7.90 | 8.44 | 154.95 | 5.1 | Concrete Pipe | 6,984.97 | 6,982.26 |
| 75: P-15 | P-15 | 18 (DP 19) | 6,983.26 | MH#3 (DP 8) | 6,983.11 | 30.8 | 0.005 | 18.0 | 0.013 | 0.30 | 2.06 | 7.43 | 4.0 | Concrete Pipe | 6,983.47 | 6,983.31 |
| 76: P-15 (1) | P-15 (1) | MH#3 (DP 8) | 6,981.11 | MH#2 (DP 8) | 6,980.73 | 75.1 | 0.005 | 42.0 | 0.013 | 8.30 | 4.95 | 71.14 | 11.7 | Concrete Pipe | 6,981.98 | 6,981.70 |
| 77: P-16 | P-16 | MH#2 (DP 8) | 6,980.63 | MH#1 | 6,980.24 | 78.1 | 0.005 | 42.0 | 0.013 | 8.30 | 4.95 | 71.14 | 11.7 | Concrete Pipe | 6,981.50 | 6,981.05 |
| 78: P-123 | P-123 | I#4 (DP 13) | 6,981.51 | I#5 (DP 14) | 6,981.25 | 52.0 | 0.005 | 18.0 | 0.013 | 2.10 | 3.61 | 7.43 | 28.3 | Concrete Pipe | 6,982.43 | 6,982.42 |
| 79: P-17 | P-17 | MH#1 | 6,980.14 | OUTFALL | 6,979.44 | 139.8 | 0.005 | 42.0 | 0.013 | 8.30 | 4.95 | 71.14 | 11.7 | Concrete Pipe | 6,981.01 | 6,980.25 |
| 80: P-125 | P-125 | 44 (69) (DP 15) | 6,978.42 | 44 (70) | 6,977.55 | 54.5 | 0.016 | 18.0 | 0.013 | 0.30 | 3.09 | 13.30 | 2.3 | Concrete Pipe | 6,978.63 | 6,977.71 |
| 83: P-122 | P-122 | INLET (DP 3) | 6,978.16 | 44 (65) | 6,973.52 | 183.8 | 0.025 | 30.0 | 0.013 | 3.70 | 7.19 | 65.19 | 5.7 | Concrete Pipe | 6,978.80 | 6,973.93 |
| 84: P-121 | P-121 | I#8 (DP 10) | 6,971.18 | 44 (80) | 6,970.65 | 105.1 | 0.005 | 24.0 | 0.013 | 4.20 | 1.34 | 16.06 | 26.1 | Concrete Pipe | 6,973.27 | 6,973.23 |
| 85: P-130 | P-130 | I#6 (DP 1) | 6,970.85 | 44 (81) | 6,970.04 | 81.5 | 0.010 | 18.0 | 0.013 | 0.50 | 3.05 | 10.47 | 4.8 | Concrete Pipe | 6,971.11 | 6,970.31 |
| 86: P-130 (1) | P-130 (1) | 44 (81) | 6,970.04 | 44 (77) | 6,969.39 | 65.0 | 0.010 | 18.0 | 0.013 | 0.50 | 3.05 | 10.50 | 4.8 | Concrete Pipe | 6,970.30 | 6,969.61 |
| 87: P-121 (1) | P-121 (1) | I#8 (DP 10) | 6,971.68 | I#7 (DP 9) | 6,971.95 | 52.0 | -0.005 | 18.0 | 0.013 | 2.20 | 3.71 | 7.57 | 29.1 | Concrete Pipe | 6,973.32 | 6,973.30 |
| 88: P-131 | P-131 | 44 (78) (DP 11) | 6,968.42 | 44 (79) | 6,967.50 | 62.5 | 0.015 | 18.0 | 0.013 | 0.40 | 3.27 | 12.77 | 3.1 | Concrete Pipe | 6,968.66 | 6,967.68 |
| 126: P-111 | P-111 | MH#34 | 7,019.01 | MH#39 | 7,017.01 | 146.6 | 0.014 | 18.0 | 0.013 | 1.70 | 4.88 | 12.28 | 13.8 | Concrete Pipe | 7,019.50 | 7,017.39 |
| 127: P-89 | P-89 | MH#8 | 6,986.87 | MH#4 DP 18) | 6,985.66 | 111.1 | 0.011 | 24.0 | 0.013 | 10.20 | 3.25 | 23.64 | 43.2 | Concrete Pipe | 6,989.18 | 6,988.96 |
| 128: P-25 (1) | P-25 (1) | CULVERT 2 (...) | 6,997.01 | O-10 | 6,995.27 | 116.5 | 0.015 | | 0.013 | 11.20 | 5.01 | 461.86 | 2.4 | Concrete Box C | 6,997.35 | 6,995.49 |
| 129: P-25 | P-25 | CULVERT 1 (...) | 6,997.01 | O-7 | 6,995.27 | 116.6 | 0.015 | | 0.013 | 11.20 | 5.01 | 461.72 | 2.4 | Concrete Box C | 6,997.35 | 6,995.49 |
| 131: P-107 (2) | P-107 (2) (1) | MH#26 (DP6.1) | 7,021.10 | DP9 | 7,020.49 | 60.7 | 0.010 | 24.0 | 0.013 | 2.90 | 4.95 | 22.62 | 12.8 | Concrete Pipe | 7,021.69 | 7,020.97 |
| 132: P-103 | P-103 | I#9 (DP6) | 7,022.86 | MH#26 (DP6.1) | 7,021.84 | 42.7 | 0.024 | 18.0 | 0.013 | 1.20 | 5.37 | 16.22 | 7.4 | Concrete Pipe | 7,023.27 | 7,022.12 |
| 133: P-107 (2) | P-107 (2) | MH#27 (DP8) | 7,021.66 | MH#26 (DP6.1) | 7,021.09 | 56.6 | 0.010 | 24.0 | 0.013 | 2.00 | 4.44 | 22.62 | 8.8 | Concrete Pipe | 7,022.15 | 7,022.07 |
| 134: P-107 | P-107 | DP 7 | 7,023.01 | MH#27 (DP8) | 7,022.41 | 37.8 | 0.016 | 15.0 | 0.013 | 0.30 | 3.15 | 8.13 | 3.7 | Concrete Pipe | 7,023.22 | 7,022.58 |
| 135: P-107 (1) | P-107 (1) | MH#27 (DP8) | 7,021.66 | DP 2 | 7,021.66 | 43.9 | 0.000 | 24.0 | 0.013 | 1.70 | 0.76 | 2.17 | 78.3 | Concrete Pipe | 7,022.36 | 7,022.31 |
| 136: P-95 | P-95 | I#8 (DP5) | 7,023.30 | I#9 (DP6) | 7,023.06 | 47.5 | 0.005 | 18.0 | 0.013 | 0.70 | 2.64 | 7.43 | 9.4 | Concrete Pipe | 7,023.61 | 7,023.42 |
| 137: P-93 | P-93 | I#6 (DP2.1) | 7,022.36 | I#7 (DP3.1) | 7,021.80 | 55.9 | 0.010 | 18.0 | 0.013 | 0.80 | 3.51 | 10.51 | 7.6 | Concrete Pipe | 7,023.00 | 7,023.00 |
| 138: Pipe - (34) | Pipe - (34) | I#7 (DP3.1) | 7,021.80 | FES OUTFALL 1 | 7,021.01 | 33.5 | 0.023 | 18.0 | 0.013 | 1.60 | 5.81 | 16.07 | 10.0 | Concrete Pipe | 7,023.00 | 7,023.00 |
| 140: P-44 (1) | P-44 (1) | MH#20 | 7,001.18 | MH#21 | 6,998.52 | 266.5 | 0.010 | 48.0 | 0.013 | 6.10 | 5.68 | 143.63 | 4.2 | Concrete Pipe | 7,001.90 | 6,999.57 |
| 141: P-64 | P-64 | MH#21 | 6,998.52 | MH#22 | 6,995.26 | 316.5 | 0.010 | 48.0 | 0.013 | 6.10 | 5.74 | 145.88 | 4.2 | Concrete Pipe | 6,999.24 | 6,995.82 |
| 142: P-44 | P-44 | MH#19 | 7,003.94 | MH#20 | 7,001.28 | 266.5 | 0.010 | 48.0 | 0.013 | 6.10 | 5.68 | 143.63 | 4.2 | Concrete Pipe | 7,004.66 | 7,001.84 |
| 143: P-26 | P-26 | DP 3 | 7,005.01 | MH#19 | 7,004.04 | 81.5 | 0.012 | 48.0 | 0.013 | 6.10 | 6.03 | 156.73 | 3.9 | Concrete Pipe | 7,005.73 | 7,004.99 |
| 144: P-64 (1) | P-64 (1) | MH#22 | 6,995.15 | MH#23 | 6,988.82 | 316.6 | 0.020 | 48.0 | 0.013 | 6.10 | 7.23 | 203.15 | 3.0 | Concrete Pipe | 6,995.87 | 6,989.55 |
| 145: P-87 | P-87 | MH#10 (DP 1... | 6,994.25 | MH#9 | 6,989.76 | 320.7 | 0.014 | 24.0 | 0.013 | 10.20 | 7.94 | 26.78 | 38.1 | Concrete Pipe | 6,995.39 | 6,990.92 |
| 146: P-87 (1) | P-87 (1) | MH#9 | 6,989.76 | MH#8 | 6,986.87 | 197.4 | 0.015 | 24.0 | 0.013 | 10.20 | 8.07 | 27.33 | 37.3 | Concrete Pipe | 6,990.90 | 6,989.29 |
| 147: P-84 | P-84 | I#4 (DP14) | 6,995.69 | MH#10 (DP 1... | 6,994.25 | 8.1 | 0.179 | 18.0 | 0.013 | 5.20 | 16.82 | 44.40 | 11.7 | Concrete Pipe | 6,996.57 | 6,996.22 |
| 148: P-84 (1) | P-84 (1) | MH#10 (DP 1... | 6,994.75 | I#5 (DP 15) | 6,995.50 | 53.9 | -0.014 | 18.0 | 0.013 | 5.00 | 6.64 | 12.40 | 40.3 | Concrete Pipe | 6,996.36 | 6,996.22 |
| 149: P-66 | P-66 | MH#23 | 6,988.82 | MH#24 | 6,988.08 | 149.0 | 0.005 | 48.0 | 0.013 | 6.10 | 4.45 | 101.56 | 6.0 | Concrete Pipe | 6,989.54 | 6,989.26 |
| 150: P-68 | P-68 | MH#24 | 6,988.08 | MH#25 (DP13) | 6,987.54 | 107.8 | 0.005 | 48.0 | 0.013 | 6.10 | 4.45 | 101.56 | 6.0 | Concrete Pipe | 6,989.26 | 6,989.27 |
| 151: P-77 | P-77 | DP12 | 6,990.32 | MH#25 (DP13) | 6,990.03 | 28.1 | 0.010 | 18.0 | 0.013 | 3.60 | 5.45 | 10.66 | 33.8 | Concrete Pipe | 6,991.04 | 6,990.64 |
| 152: P-74 | P-74 | MH#25 (DP13) | 6,987.54 | OUTLET SEGM... | 6,986.67 | 173.3 | 0.005 | 48.0 | 0.013 | 26.00 | 6.76 | 101.56 | 25.6 | Concrete Pipe | 6,989.05 | 6,988.30 |

NOTE: EASTONVILLE 1 - INLET & EASTONVILLE 5 SEGMENTS HAVE BEEN ANALYZED IN THE FREE OUTFALL CONDITION BELOW TO MEET CAPACITY & VELOCITY REQUIREMENTS. SEGMENT 2 PIPES & STRUCTURES INCLUDED IN TABLE, REFER TO FDR FOR COMPLETE ANALYSIS.

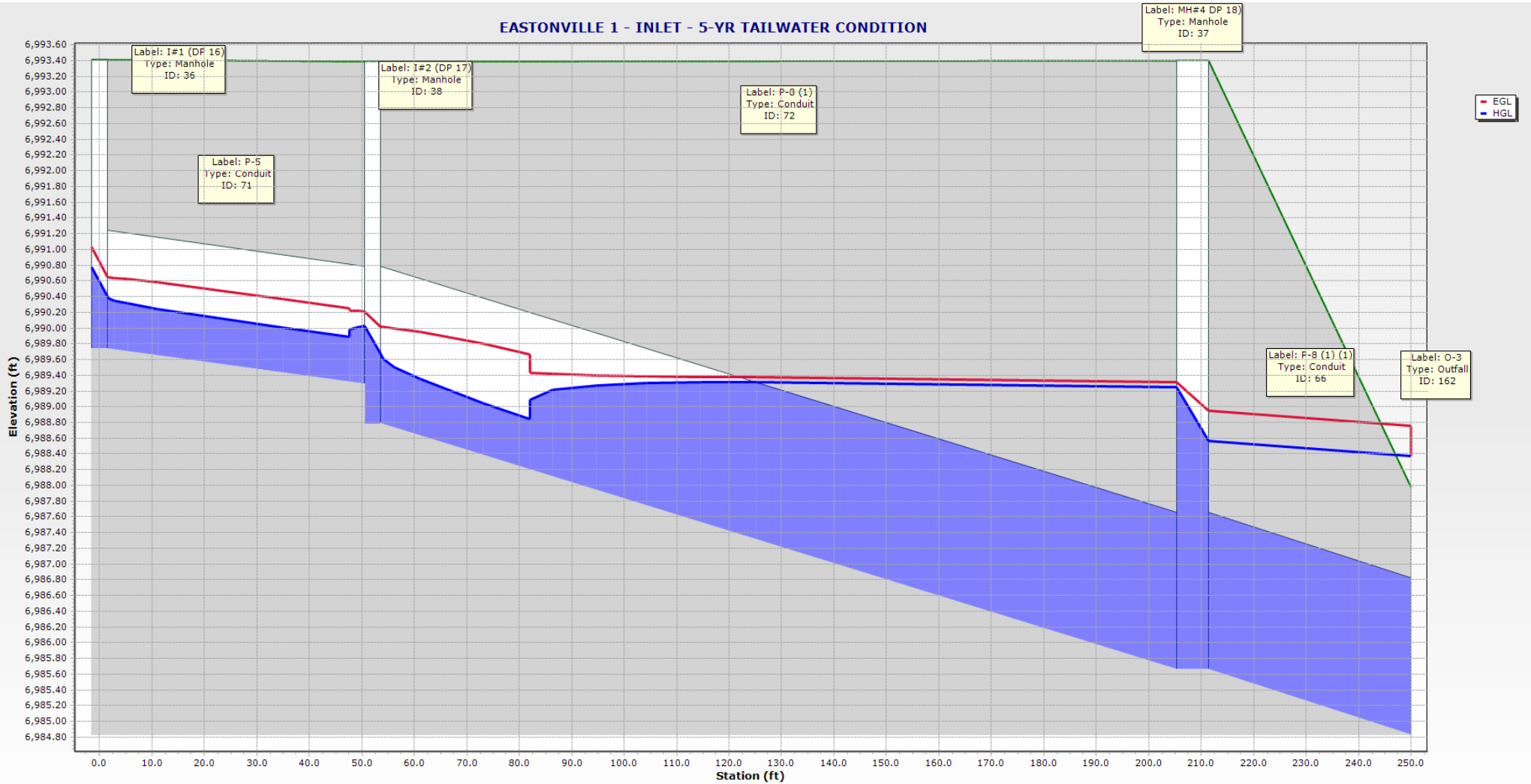
5 YEAR TAILWATER CONDITION: STRUCTURE SUMMARY TABLE

| | Label | Elevation (Ground) (ft) | Elevation (Rim) (ft) | Flow (Total Out) (cfs) | Depth (Out) (ft) | Hydraulic Grade Line (Out) (ft) | Hydraulic Grade Line (In) (ft) | Notes | Elevation (Invert Out) (ft) | Headloss (ft) |
|-----------------|-----------------|-------------------------|----------------------|------------------------|------------------|---------------------------------|--------------------------------|---------------|-----------------------------|---------------|
| 35: MH#7 | MH#7 | 6,993.52 | 6,993.52 | 7.90 | 0.85 | 6,986.22 | 6,986.42 | STORM MH | 6,985.38 | 0.19 |
| 36: I#1 (DP 16) | I#1 (DP 16) | 6,993.41 | 6,993.41 | 3.00 | 0.66 | 6,990.40 | 6,990.77 | CDOT Type- | 6,989.74 | 0.38 |
| 37: MH#4 DP | MH#4 DP 18) | 6,993.40 | 6,993.40 | 15.60 | 2.91 | 6,988.57 | 6,988.96 | STORM MH | 6,985.66 | 0.39 |
| 38: I#2 (DP 17) | I#2 (DP 17) | 6,993.39 | 6,993.39 | 6.30 | 0.90 | 6,989.68 | 6,990.02 | CDOT Type- | 6,988.79 | 0.35 |
| 39: MH#6 | MH#6 | 6,993.02 | 6,993.02 | 7.90 | 0.85 | 6,985.35 | 6,985.54 | STORM MH | 6,984.50 | 0.19 |
| 40: MH#5 | MH#5 | 6,991.91 | 6,991.91 | 7.90 | 0.85 | 6,984.97 | 6,985.17 | STORM MH | 6,984.13 | 0.19 |
| 41: MH#3 (DP | MH#3 (DP 8) | 6,991.13 | 6,991.13 | 8.30 | 0.87 | 6,981.98 | 6,982.26 | STORM MH | 6,981.11 | 0.28 |
| 42: I#3 (DP 7) | I#3 (DP 7) | 6,990.73 | 6,990.73 | 7.90 | 0.93 | 6,986.58 | 6,987.03 | CDOT Type- | 6,985.73 | 0.45 |
| 43: 18 (DP 19) | 18 (DP 19) | 6,988.71 | 6,988.71 | 0.30 | 1.97 | 6,983.47 | 6,983.57 | CDOT Type- | 6,983.26 | 0.10 |
| 44: MH#2 (DP | MH#2 (DP 8) | 6,985.74 | 6,985.74 | 8.30 | 0.87 | 6,981.50 | 6,981.70 | STORM MH | 6,980.63 | 0.20 |
| 45: I#4 (DP 13) | I#4 (DP 13) | 6,985.02 | 6,985.02 | 2.10 | 1.13 | 6,982.43 | 6,982.51 | CDOT Type- | 6,981.51 | 0.08 |
| 46: I#5 (DP 14) | I#5 (DP 14) | 6,985.02 | 6,985.02 | 3.90 | 1.23 | 6,982.28 | 6,982.42 | CDOT Type- | 6,981.25 | 0.15 |
| 47: MH#1 | MH#1 | 6,984.95 | 6,984.95 | 8.30 | 0.87 | 6,981.01 | 6,981.04 | STORM MH | 6,980.14 | 0.03 |
| 49: 44 (69) (D | 44 (69) (DP 15) | 6,982.64 | 6,982.64 | 0.30 | 0.20 | 6,978.63 | 6,978.63 | CDOT Type- | 6,978.42 | 0.01 |
| 55: 44 (80) | 44 (80) | 6,975.21 | 6,975.21 | 4.20 | 2.58 | 6,973.23 | 6,973.23 | Cylindrical S | 6,970.65 | 0.00 |
| 56: 44 (81) | 44 (81) | 6,975.03 | 6,975.03 | 0.50 | 0.26 | 6,970.30 | 6,970.31 | Cylindrical S | 6,970.04 | 0.01 |
| 57: I#7 (DP 9) | I#7 (DP 9) | 6,974.64 | 6,974.64 | 2.20 | 1.37 | 6,973.32 | 6,973.36 | CDOT Type- | 6,971.95 | 0.04 |
| 58: I#8 (DP 10) | I#8 (DP 10) | 6,974.64 | 6,974.64 | 4.20 | 2.09 | 6,973.27 | 6,973.30 | CDOT Type- | 6,971.18 | 0.03 |
| 59: I#6 (DP 1) | I#6 (DP 1) | 6,973.20 | 6,973.20 | 0.50 | 0.26 | 6,971.11 | 6,971.25 | CDOT Type- | 6,970.85 | 0.14 |
| 60: 44 (78) (D | 44 (78) (DP 11) | 6,973.16 | 6,973.16 | 0.40 | 0.23 | 6,968.66 | 6,968.74 | CDOT Type- | 6,968.42 | 0.08 |
| 98: MH#26 (D | MH#26 (DP6.1) | 7,027.15 | 7,027.15 | 2.90 | 0.60 | 7,021.69 | 7,022.07 | STORM MH | 7,021.10 | 0.38 |
| 99: MH#27 (D | MH#27 (DP8) | 7,027.09 | 7,027.09 | 2.00 | 0.49 | 7,022.15 | 7,022.31 | STORM MH | 7,021.66 | 0.16 |
| 100: I#9 (DP6) | I#9 (DP6) | 7,027.04 | 7,027.04 | 1.20 | 0.41 | 7,023.27 | 7,023.42 | CDOT Type- | 7,022.86 | 0.15 |
| 101: I#8 (DP5) | I#8 (DP5) | 7,026.63 | 7,026.63 | 0.70 | 0.31 | 7,023.61 | 7,023.77 | CDOT Type- | 7,023.30 | 0.16 |
| 102: I#7 (DP3. | I#7 (DP3.1) | 7,026.51 | 7,026.51 | 1.60 | 1.70 | 7,023.00 | 7,023.00 | CDOT Type- | 7,021.80 | 0.00 |
| 103: I#6 (DP2. | I#6 (DP2.1) | 7,026.40 | 7,026.40 | 0.80 | 0.64 | 7,023.00 | 7,023.03 | CDOT Type- | 7,022.36 | 0.03 |
| 106: MH#34 | MH#34 | 7,023.51 | 7,023.51 | 1.70 | 0.49 | 7,019.50 | 7,019.59 | CDOT Type- | 7,019.01 | 0.08 |
| 111: MH#21 | MH#21 | 7,014.03 | 7,014.03 | 6.10 | 0.72 | 6,999.24 | 6,999.57 | STORM MH | 6,998.52 | 0.33 |
| 112: MH#20 | MH#20 | 7,012.41 | 7,012.41 | 6.10 | 0.72 | 7,001.90 | 7,001.91 | STORM MH | 7,001.18 | 0.01 |
| 113: MH#19 | MH#19 | 7,010.85 | 7,010.85 | 6.10 | 0.72 | 7,004.66 | 7,004.99 | STORM MH | 7,003.94 | 0.33 |
| 115: MH#22 | MH#22 | 7,005.85 | 7,005.85 | 6.10 | 0.72 | 6,995.87 | 6,995.88 | STORM MH | 6,995.15 | 0.01 |
| 116: MH#9 | MH#9 | 7,001.03 | 7,001.03 | 10.20 | 1.14 | 6,990.90 | 6,990.92 | STORM MH | 6,989.76 | 0.02 |
| 117: I#4 (DP1 | I#4 (DP14) | 7,000.17 | 7,000.17 | 5.20 | 0.88 | 6,996.57 | 6,997.11 | CDOT Type- | 6,995.69 | 0.55 |
| 118: MH#10 (| MH#10 (DP 1... | 7,000.01 | 7,000.01 | 10.20 | 1.14 | 6,995.39 | 6,996.22 | STORM MH | 6,994.25 | 0.83 |
| 119: I#5 (DP 1 | I#5 (DP 15) | 6,999.67 | 6,999.67 | 5.00 | 0.46 | 6,996.36 | 6,996.89 | CDOT Type- | 6,995.50 | 0.53 |
| 120: MH#8 | MH#8 | 6,996.13 | 6,996.13 | 10.20 | 2.52 | 6,989.18 | 6,989.29 | STORM MH | 6,986.87 | 0.10 |
| 121: MH#23 | MH#23 | 6,995.25 | 6,995.25 | 6.10 | 0.72 | 6,989.54 | 6,989.55 | STORM MH | 6,988.82 | 0.01 |
| 122: MH#24 | MH#24 | 6,993.32 | 6,993.32 | 6.10 | 1.18 | 6,989.26 | 6,989.26 | STORM MH | 6,988.08 | 0.00 |
| 123: DP12 | DP12 | 6,993.02 | 6,993.02 | 3.60 | 0.73 | 6,991.04 | 6,991.47 | CDOT Type- | 6,990.32 | 0.42 |
| 124: MH#25 (| MH#25 (DP13) | 6,992.79 | 6,992.79 | 26.00 | 1.51 | 6,989.05 | 6,989.27 | STORM MH | 6,987.54 | 0.22 |
| 190: INLET (D | INLET (DP 3) | 6,980.96 | 6,980.96 | 3.70 | 0.63 | 6,978.80 | 6,979.13 | CDOT FES | 6,978.16 | 0.34 |
| 192: DP 7 | DP 7 | 7,024.45 | 7,024.45 | 0.30 | 0.21 | 7,023.22 | 7,023.33 | CDOT FES | 7,023.01 | 0.11 |
| 193: DP 2 | DP 2 | 7,024.26 | 7,024.26 | 1.70 | 0.35 | 7,022.36 | 7,022.43 | CDOT FES | 7,021.66 | 0.07 |
| 194: DP 3 | DP 3 | 7,009.43 | 7,009.43 | 6.10 | 0.72 | 7,005.73 | 7,006.10 | CDOT FES | 7,005.01 | 0.37 |
| 196: CULVERT | CULVERT 1 (...) | 7,000.01 | 7,000.01 | 11.20 | 0.34 | 6,997.35 | 6,997.61 | Dummy Null | 6,997.01 | 0.25 |
| 197: CULVERT | CULVERT 2 (...) | 7,000.01 | 7,000.01 | 11.20 | 0.34 | 6,997.35 | 6,997.61 | Dummy Null | 6,997.01 | 0.25 |

| | ID | Label | Elevation (Ground) (ft) | Elevation (Invert) (ft) | Elevation (User Defined Tailwater) (ft) | Hydraulic Grade (ft) | Flow (Total Out) (cfs) | Notes |
|-----------------------|-----|---------------|-------------------------|-------------------------|---|----------------------|------------------------|------------|
| 48: OUTFALL | 48 | OUTFALL | 6,983.32 | 6,979.44 | | 6,980.25 | 8.30 | CDOT FES |
| 53: 44 (70) | 53 | 44 (70) | 6,979.33 | 6,977.55 | | 6,977.71 | 0.30 | CDOT FES |
| 54: 44 (65) | 54 | 44 (65) | 6,976.31 | 6,973.52 | | 6,973.93 | 3.70 | CDOT FES |
| 61: 44 (77) | 61 | 44 (77) | 6,971.10 | 6,969.39 | | 6,969.61 | 0.50 | CDOT FES |
| 64: 44 (79) | 64 | 44 (79) | 6,969.82 | 6,967.50 | | 6,967.68 | 0.40 | CDOT FES |
| 107: DP9 | 107 | DP9 | 7,022.74 | 7,020.49 | | 7,020.97 | 2.90 | CDOT FES |
| 108: FES OUTFALL 1 | 108 | FES OUTFALL 1 | 7,023.00 | 7,021.01 | 7,023.00 | 7,023.00 | 1.60 | CDOT FES |
| 110: MH#39 | 110 | MH#39 | 7,018.18 | 7,017.01 | | 7,017.39 | 1.70 | CDOT FES |
| 125: OUTLET SEGMENT 3 | 125 | OUTLET SEG... | 6,991.09 | 6,986.67 | 6,988.30 | 6,988.30 | 26.00 | CDOT FES |
| 162: O-3 | 162 | O-3 | 6,987.98 | 6,984.83 | 6,988.37 | 6,988.37 | 15.60 | Dummy Null |
| 164: O-5 | 164 | O-5 | 6,982.10 | 6,981.08 | 6,982.25 | 6,982.25 | 3.90 | Dummy Null |
| 165: O-6 | 165 | O-6 | 6,972.87 | 6,970.61 | 6,973.23 | 6,973.23 | 4.20 | Dummy Null |
| 203: O-7 | 203 | O-7 | 6,998.27 | 6,995.27 | | 6,995.49 | 11.20 | Dummy Null |
| 207: O-10 | 207 | O-10 | 6,998.27 | 6,995.27 | | 6,995.49 | 11.20 | Dummy Null |

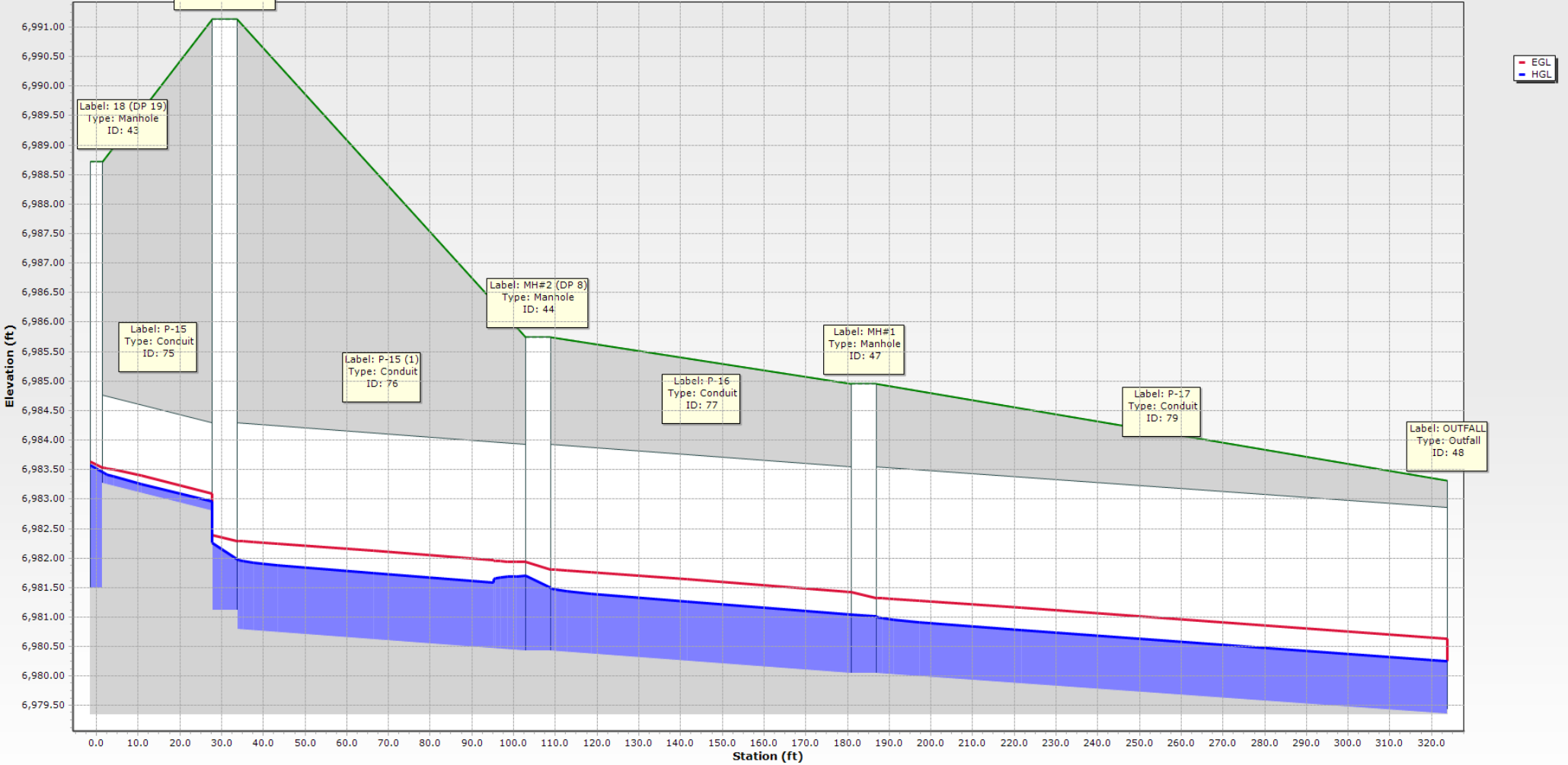
NOTE: EASTONVILLE 1 - INLET & EASTONVILLE 5 SEGMENTS HAVE BEEN ANALYZED IN THE FREE OUTFALL CONDITION BELOW TO MEET CAPACITY & VELOCITY REQUIREMENTS. SEGMENT 2 PIPES & STRUCTURES INCLUDED IN TABLE, REFER TO FDR FOR COMPLETE ANALYSIS.

EASTONVILLE 1 - INLET - 5-YR TAILWATER CONDITION



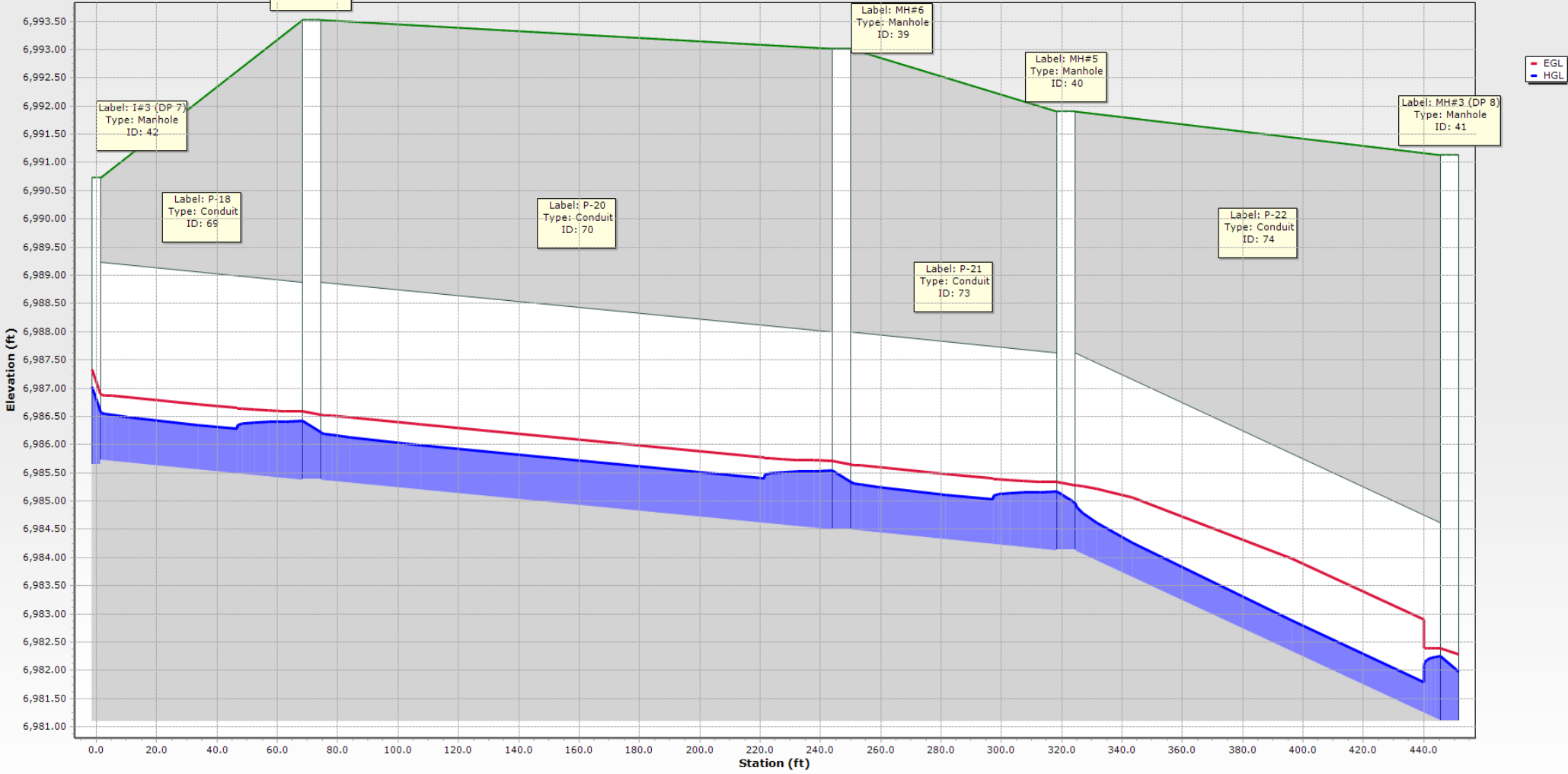
**NOTE: THIS SEGMENT HAS BEEN ANALYZED IN THE FREE
OUTFALL CONDITION BLEW TO MEET CAPACITY & VELOCITY
REQUIREMENTS**

EASTONVILLE 1 - OUTLET - 5-YR TAILWATER CONDITION

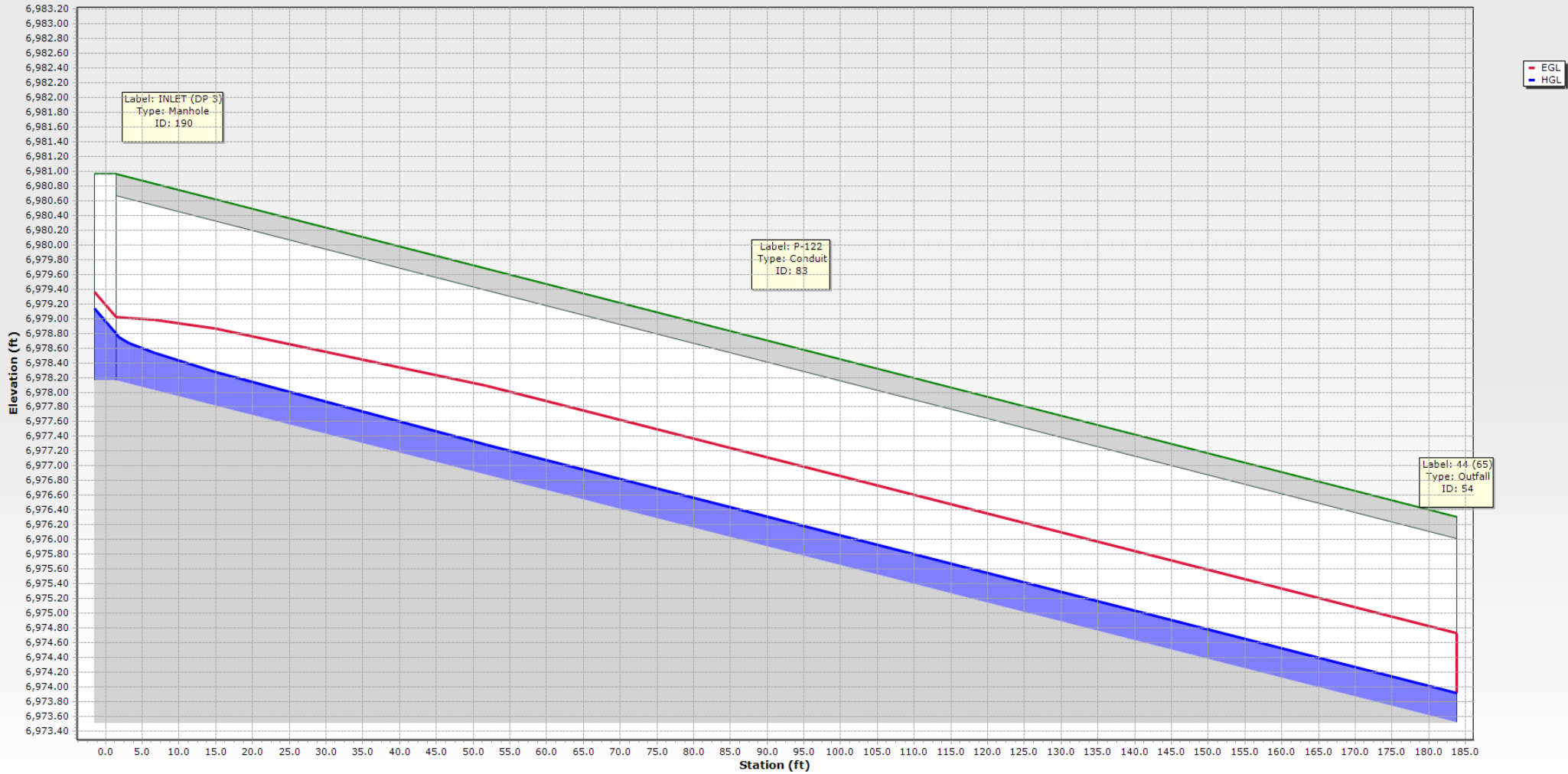


**NOTE: THIS SEGMENT HAS BEEN ANALYZED IN THE FREE
OUTFALL CONDITION BLEW TO MEET CAPACITY & VELOCITY
REQUIREMENTS**

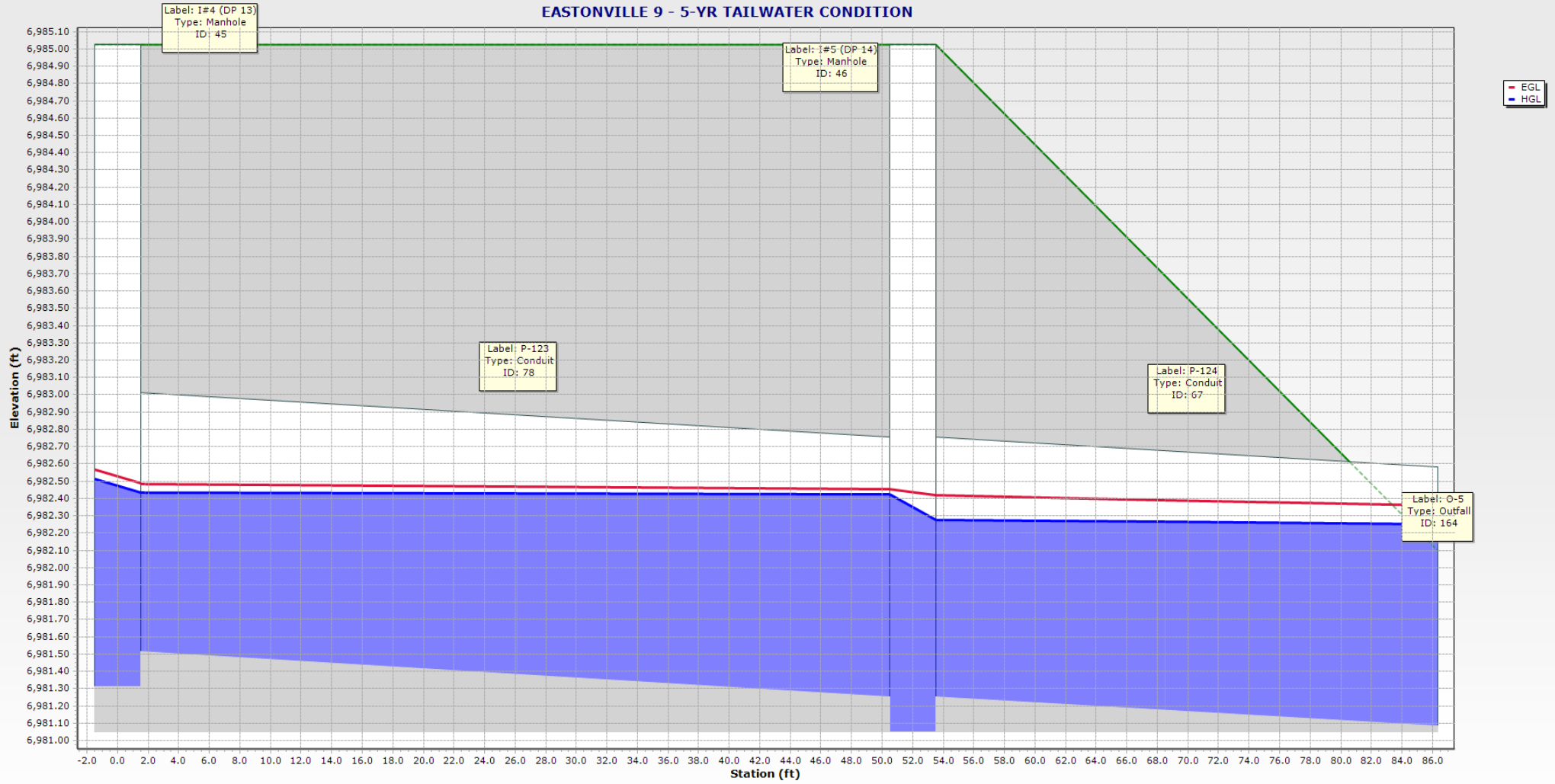
EASTONVILLE 2 - 5-YR TAILWATER CONDITION



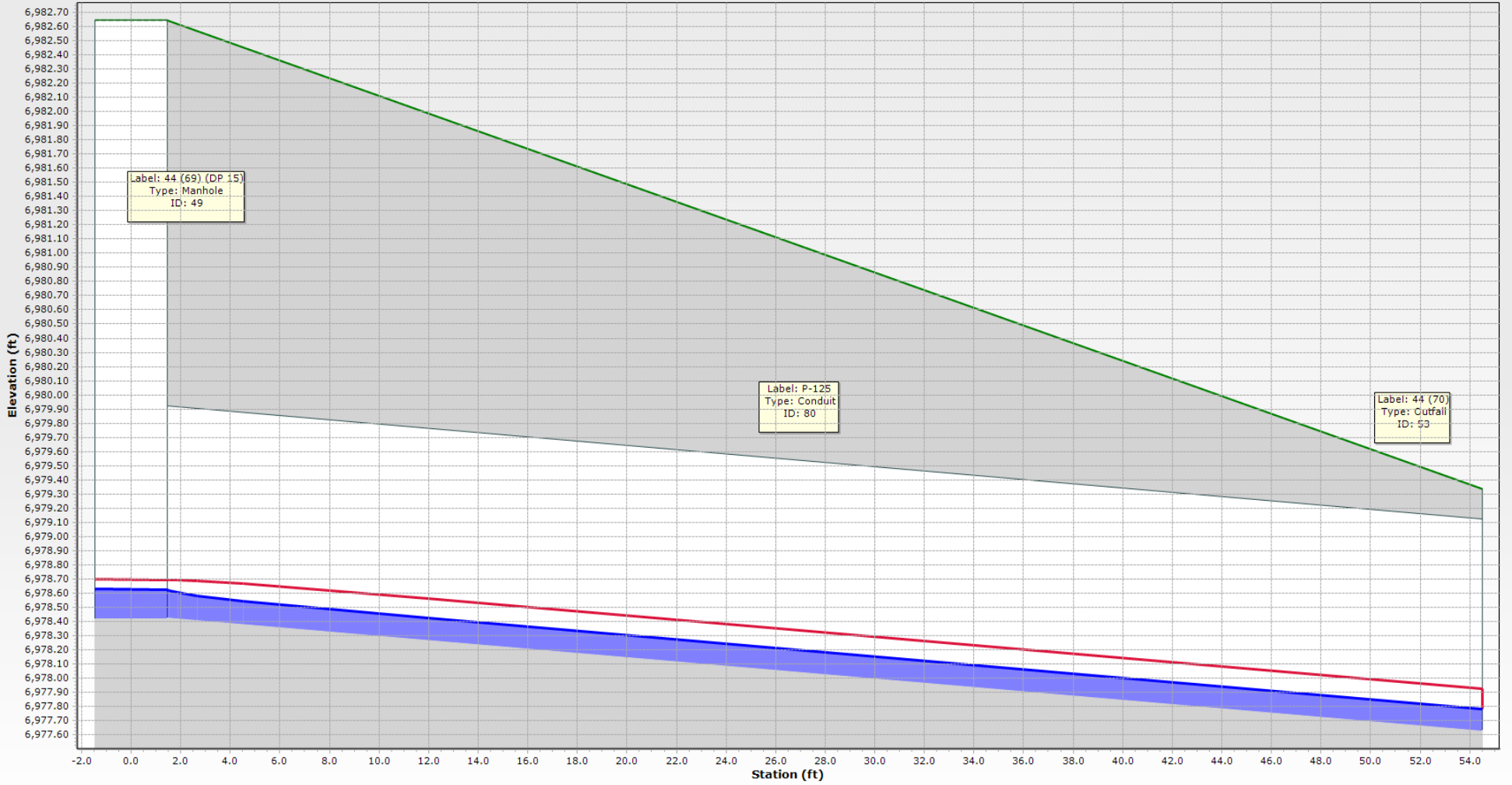
EASTONVILLE 6 - 5-YR TAILWATER CONDITION



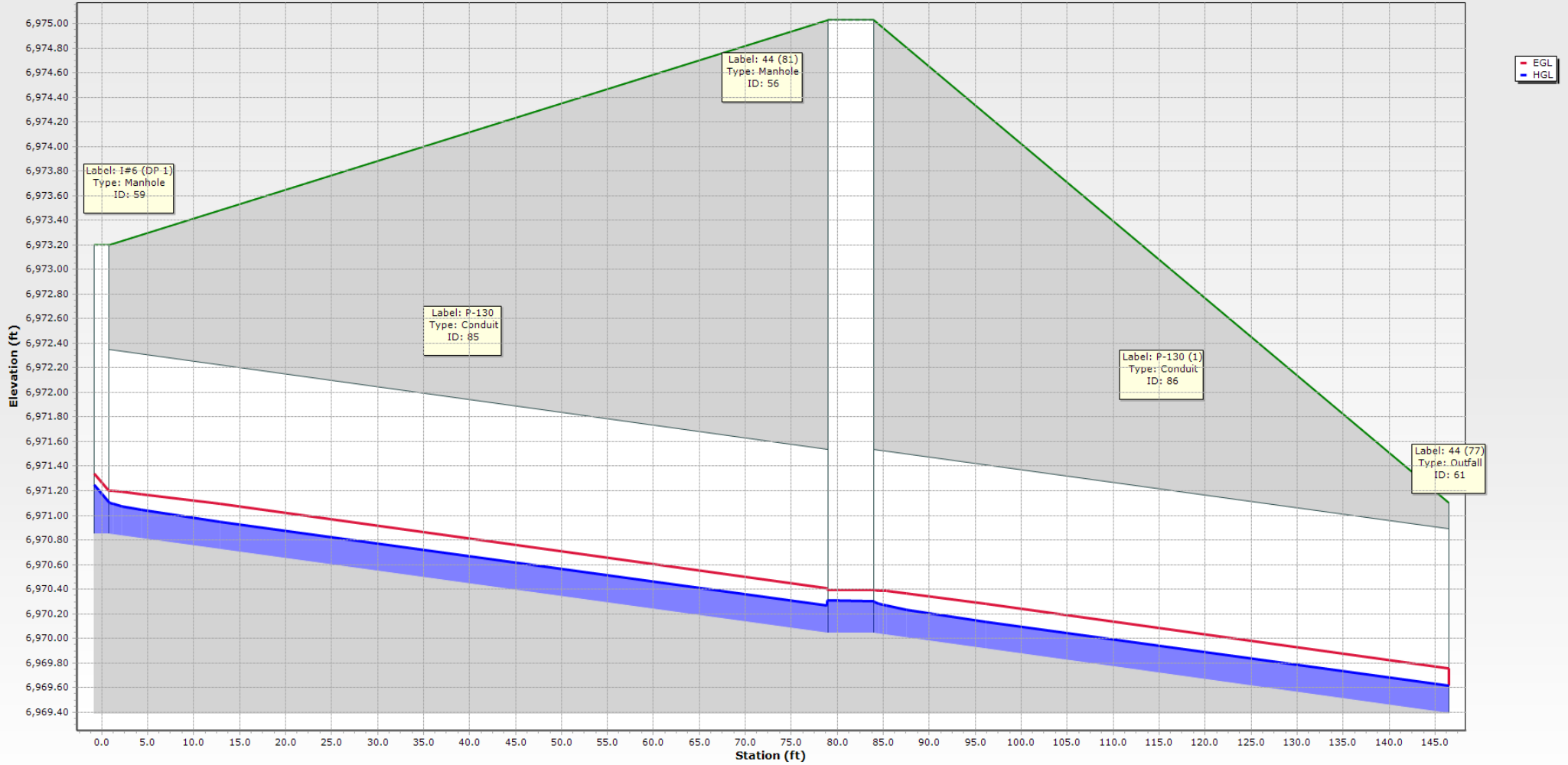
EASTONVILLE 9 - 5-YR TAILWATER CONDITION



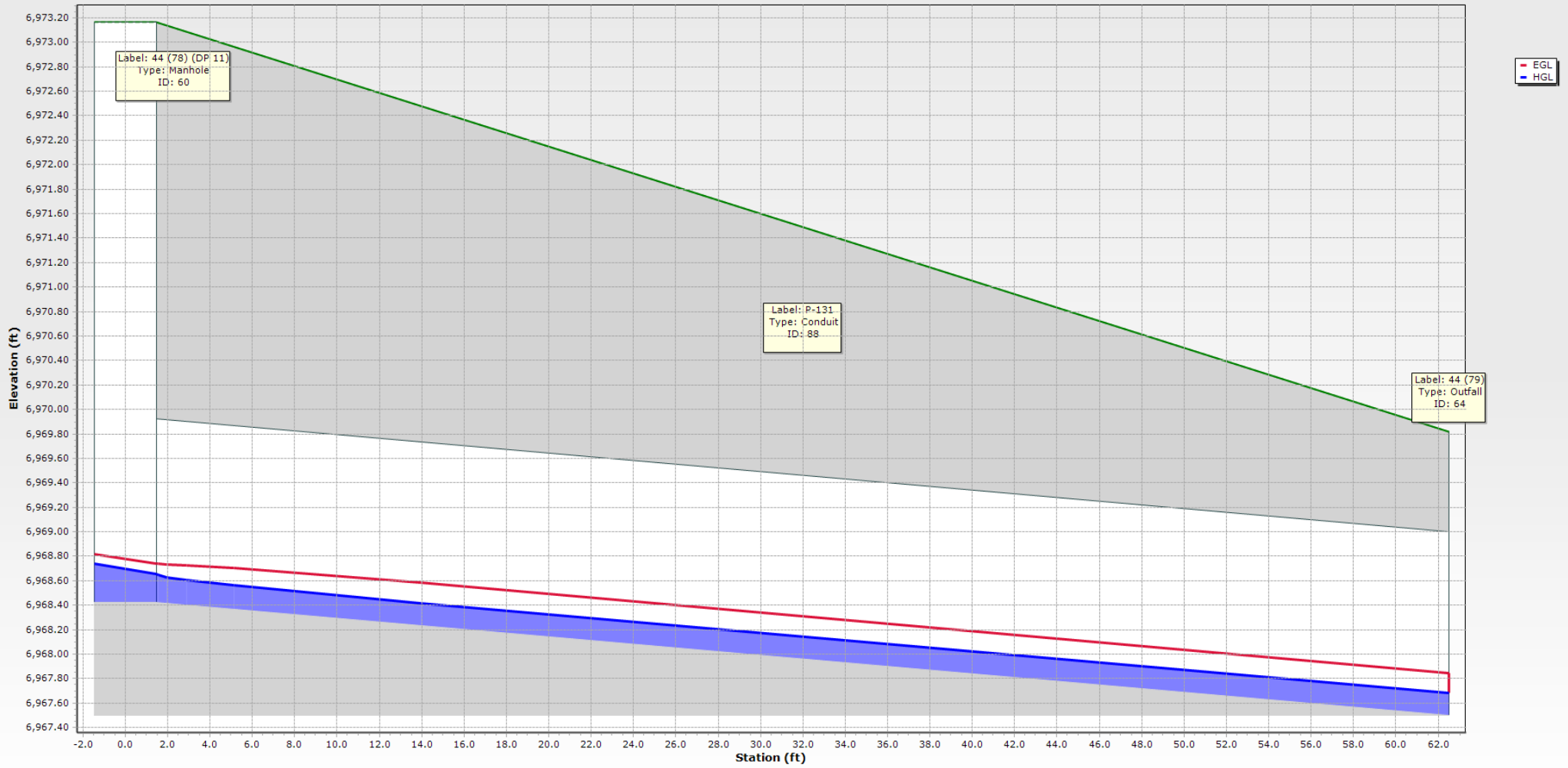
EASTONVILLE 17 - 5-YR TAILWATER CONDITION - Time: 0.00



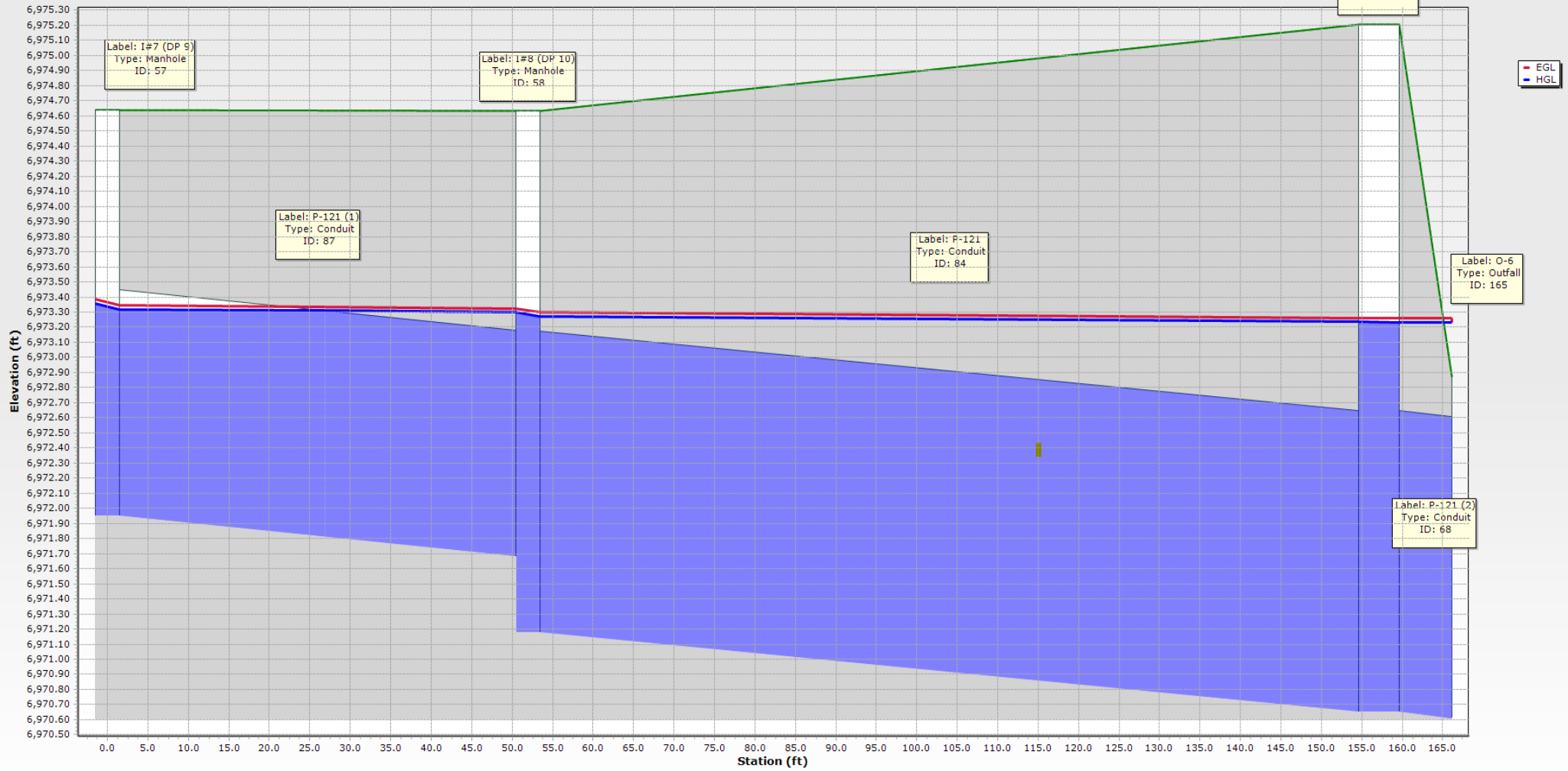
EASTONVILLE 3 - 5-YR TAILWATER CONDITION



EASTONVILLE 4 - 5-YR TAILWATER CONDITION



EASTONVILLE 5 - 5-YR TAILWATER CONDITION



**NOTE: THIS SEGMENT HAS BEEN ANALYZED IN THE FREE
OUTFALL CONDITION BLEW TO MEET CAPACITY & VELOCITY
REQUIREMENTS**

100 YEAR FREE OUTFALL CONDITION: PIPE SUMMARY TABLE

| | Label | Start Node | Invert (Start) (ft) | Stop Node | Invert (Stop) (ft) | Length (User Defined) (ft) | Slope (Calculated) (ft/ft) | Diameter (in) | Manning's n | Flow (cfs) | Velocity (ft/s) | Capacity (Full Flow) (cfs) | Flow / Capacity (Design) (%) | Notes | Hydraulic Grade Line (In) (ft) | Hydraulic Grade Line (Out) (ft) |
|------------------|---------------|-----------------|---------------------|-----------------|--------------------|----------------------------|----------------------------|---------------|-------------|------------|-----------------|----------------------------|------------------------------|----------------|--------------------------------|---------------------------------|
| 66: P-8 (1) (1) | P-8 (1) (1) | MH#4 DP 18) | 6,985.66 | O-3 | 6,984.83 | 41.6 | 0.020 | 24.0 | 0.013 | 26.20 | 8.34 | 31.99 | 81.9 | Concrete Pipe | 6,988.54 | 6,987.98 |
| 67: P-124 | P-124 | I#5 (DP 14) | 6,981.25 | O-5 | 6,981.08 | 34.3 | 0.005 | 18.0 | 0.013 | 6.50 | 4.74 | 7.43 | 87.5 | Concrete Pipe | 6,982.33 | 6,982.10 |
| 68: P-121 (2) | P-121 (2) | 44 (80) | 6,970.65 | O-6 | 6,970.61 | 9.0 | 0.005 | 24.0 | 0.013 | 9.00 | 5.23 | 15.95 | 56.4 | Concrete Pipe | 6,971.73 | 6,971.68 |
| 69: P-18 | P-18 | I#3 (DP 7) | 6,985.73 | MH#7 | 6,985.38 | 71.3 | 0.005 | 42.0 | 0.013 | 53.30 | 8.11 | 71.14 | 74.9 | Concrete Pipe | 6,988.48 | 6,988.38 |
| 70: P-20 | P-20 | MH#7 | 6,985.38 | MH#6 | 6,984.50 | 175.6 | 0.005 | 42.0 | 0.013 | 53.30 | 8.11 | 71.14 | 74.9 | Concrete Pipe | 6,987.84 | 6,987.61 |
| 71: P-5 | P-5 | I#2 (DP 17) | 6,989.29 | I#1 (DP 16) | 6,989.74 | 52.0 | -0.009 | 18.0 | 0.013 | 5.10 | 5.59 | 9.77 | 52.2 | Concrete Pipe | 6,990.61 | 6,990.44 |
| 72: P-8 (1) | P-8 (1) | I#2 (DP 17) | 6,988.79 | MH#4 DP 18) | 6,985.66 | 156.4 | 0.020 | 24.0 | 0.013 | 10.50 | 9.12 | 31.99 | 32.8 | Concrete Pipe | 6,989.95 | 6,989.64 |
| 73: P-21 | P-21 | MH#6 | 6,984.50 | MH#5 | 6,984.13 | 74.6 | 0.005 | 42.0 | 0.013 | 53.30 | 8.11 | 71.14 | 74.9 | Concrete Pipe | 6,987.15 | 6,987.05 |
| 74: P-22 | P-22 | MH#5 | 6,984.13 | MH#3 (DP 8) | 6,981.11 | 127.1 | 0.024 | 42.0 | 0.013 | 53.30 | 14.61 | 154.95 | 34.4 | Concrete Pipe | 6,986.41 | 6,983.59 |
| 75: P-15 | P-15 | 18 (DP 19) | 6,983.26 | MH#3 (DP 8) | 6,983.11 | 30.8 | 0.005 | 18.0 | 0.013 | 3.00 | 3.98 | 7.43 | 40.4 | Concrete Pipe | 6,983.93 | 6,983.77 |
| 76: P-15 (1) | P-15 (1) | MH#3 (DP 8) | 6,981.11 | MH#2 (DP 8) | 6,980.73 | 75.1 | 0.005 | 42.0 | 0.013 | 1.77 | 3.13 | 71.14 | 2.5 | Concrete Pipe | 6,983.59 | 6,983.59 |
| 77: P-16 | P-16 | MH#2 (DP 8) | 6,980.63 | MH#1 | 6,980.24 | 78.1 | 0.005 | 42.0 | 0.013 | 54.30 | 8.14 | 71.14 | 76.3 | Concrete Pipe | 6,982.94 | 6,982.55 |
| 78: P-123 | P-123 | I#4 (DP 13) | 6,981.51 | I#5 (DP 14) | 6,981.25 | 52.0 | 0.005 | 18.0 | 0.013 | 3.40 | 4.11 | 7.43 | 45.8 | Concrete Pipe | 6,982.73 | 6,982.69 |
| 79: P-17 | P-17 | MH#1 | 6,980.14 | OUTFALL | 6,979.44 | 139.8 | 0.005 | 42.0 | 0.013 | 54.30 | 8.14 | 71.14 | 76.3 | Concrete Pipe | 6,982.45 | 6,981.73 |
| 80: P-125 | P-125 | 44 (69) (DP 15) | 6,978.42 | 44 (70) | 6,977.55 | 54.5 | 0.016 | 18.0 | 0.013 | 1.20 | 4.67 | 13.30 | 9.0 | Concrete Pipe | 6,978.83 | 6,977.85 |
| 83: P-122 | P-122 | INLET (DP 3) | 6,978.16 | 44 (65) | 6,973.52 | 183.8 | 0.025 | 30.0 | 0.013 | 24.50 | 12.34 | 65.19 | 37.6 | Concrete Pipe | 6,979.85 | 6,974.58 |
| 84: P-121 | P-121 | I#8 (DP 10) | 6,971.18 | 44 (80) | 6,970.65 | 105.1 | 0.005 | 24.0 | 0.013 | 9.00 | 5.26 | 16.06 | 56.0 | Concrete Pipe | 6,972.25 | 6,971.75 |
| 85: P-130 | P-130 | I#6 (DP 1) | 6,970.85 | 44 (81) | 6,970.04 | 81.5 | 0.010 | 18.0 | 0.013 | 3.60 | 5.37 | 10.47 | 34.4 | Concrete Pipe | 6,971.57 | 6,970.79 |
| 86: P-130 (1) | P-130 (1) | 44 (81) | 6,970.04 | 44 (77) | 6,969.39 | 65.0 | 0.010 | 18.0 | 0.013 | 3.60 | 5.39 | 10.50 | 34.3 | Concrete Pipe | 6,970.76 | 6,970.00 |
| 87: P-121 (1) | P-121 (1) | I#8 (DP 10) | 6,971.68 | I#7 (DP 9) | 6,971.95 | 52.0 | -0.005 | 18.0 | 0.013 | 4.10 | 4.37 | 7.57 | 54.2 | Concrete Pipe | 6,972.75 | 6,972.69 |
| 88: P-131 | P-131 | 44 (78) (DP 11) | 6,968.42 | 44 (79) | 6,967.50 | 62.5 | 0.015 | 11.0 | 0.013 | 1.40 | 4.75 | 12.77 | 11.0 | Concrete Pipe | 6,968.87 | 6,967.84 |
| 126: P-111 | P-111 | MH#34 | 7,019.01 | MH#39 | 7,017.01 | 146.6 | 0.014 | 18.0 | 0.013 | 3.40 | 5.94 | 12.28 | 27.7 | Concrete Pipe | 7,019.72 | 7,017.55 |
| 127: P-89 | P-89 | MH#8 | 6,986.87 | MH#4 DP 18) | 6,985.66 | 111.1 | 0.011 | 24.0 | 0.013 | 19.10 | 6.08 | 23.64 | 80.8 | Concrete Pipe | 6,990.43 | 6,989.64 |
| 128: P-25 (1) | P-25 (1) | CULVERT 2 (...) | 6,997.01 | O-10 | 6,995.27 | 116.5 | 0.015 | | 0.013 | 295.50 | 16.72 | 461.86 | 64.0 | Concrete Box C | 7,000.01 | 6,997.28 |
| 129: P-25 | P-25 | CULVERT 1 (...) | 6,997.01 | O-7 | 6,995.27 | 116.6 | 0.015 | | 0.013 | 245.50 | 15.71 | 461.72 | 53.2 | Concrete Box C | 6,999.67 | 6,997.02 |
| 131: P-107 (2) | P-107 (2) (1) | MH#26 (DP6.1) | 7,021.10 | DP9 | 7,020.49 | 60.7 | 0.010 | 24.0 | 0.013 | 22.40 | 8.21 | 22.62 | 99.0 | Concrete Pipe | 7,022.79 | 7,022.11 |
| 132: P-103 | P-103 | I#9 (DP6) | 7,022.86 | MH#26 (DP6.1) | 7,021.84 | 42.7 | 0.024 | 18.0 | 0.013 | 2.40 | 1.36 | 16.22 | 14.8 | Concrete Pipe | 7,024.53 | 7,024.51 |
| 133: P-107 (2) | P-107 (2) | MH#27 (DP8) | 7,021.66 | MH#26 (DP6.1) | 7,021.09 | 56.6 | 0.010 | 24.0 | 0.013 | 21.00 | 6.68 | 22.62 | 92.8 | Concrete Pipe | 7,025.00 | 7,024.51 |
| 134: P-107 | P-107 | DP 7 | 7,023.01 | MH#27 (DP8) | 7,022.41 | 37.8 | 0.016 | 15.0 | 0.013 | 2.20 | 1.79 | 8.13 | 27.1 | Concrete Pipe | 7,025.67 | 7,025.62 |
| 135: P-107 (1) | P-107 (1) | MH#27 (DP8) | 7,021.66 | DP 2 | 7,021.66 | 43.9 | 0.000 | 24.0 | 0.013 | 18.80 | 5.98 | 2.17 | 865.7 | Concrete Pipe | 7,025.93 | 7,025.62 |
| 136: P-95 | P-95 | I#8 (DP5) | 7,023.30 | I#9 (DP6) | 7,023.06 | 47.5 | 0.005 | 18.0 | 0.013 | 1.30 | 3.16 | 7.43 | 17.5 | Concrete Pipe | 7,024.57 | 7,024.56 |
| 137: P-93 | P-93 | I#6 (DP2.1) | 7,022.36 | I#7 (DP3.1) | 7,021.80 | 55.9 | 0.010 | 18.0 | 0.013 | 1.50 | 4.22 | 10.51 | 14.3 | Concrete Pipe | 7,022.99 | 7,023.02 |
| 138: Pipe - (34) | Pipe - (34) | I#7 (DP3.1) | 7,021.80 | FES OUTFALL 1 | 7,021.01 | 33.5 | 0.023 | 18.0 | 0.013 | 3.20 | 7.09 | 16.07 | 19.9 | Concrete Pipe | 7,023.01 | 7,023.00 |
| 140: P-44 (1) | P-44 (1) | MH#20 | 7,001.18 | MH#21 | 6,998.52 | 266.5 | 0.010 | 48.0 | 0.013 | 112.10 | 8.92 | 143.63 | 78.0 | Concrete Pipe | 7,005.57 | 7,003.94 |
| 141: P-64 | P-64 | MH#21 | 6,998.52 | MH#22 | 6,995.26 | 316.5 | 0.010 | 48.0 | 0.013 | 112.10 | 12.80 | 145.88 | 76.8 | Concrete Pipe | 7,001.72 | 6,997.89 |
| 142: P-44 | P-44 | MH#19 | 7,003.94 | MH#20 | 7,001.28 | 266.5 | 0.010 | 48.0 | 0.013 | 112.10 | 12.64 | 143.63 | 78.0 | Concrete Pipe | 7,007.14 | 7,005.63 |
| 143: P-26 | P-26 | DP 3 | 7,005.01 | MH#19 | 7,004.04 | 81.5 | 0.012 | 48.0 | 0.013 | 112.10 | 8.92 | 156.73 | 71.5 | Concrete Pipe | 7,009.86 | 7,009.36 |
| 144: P-64 (1) | P-64 (1) | MH#22 | 6,995.15 | MH#23 | 6,988.82 | 316.6 | 0.020 | 48.0 | 0.013 | 112.10 | 16.57 | 203.15 | 55.2 | Concrete Pipe | 6,998.35 | 6,994.29 |
| 145: P-87 | P-87 | MH#10 (DP 1...) | 6,994.25 | MH#9 | 6,989.76 | 320.7 | 0.014 | 24.0 | 0.013 | 19.10 | 9.26 | 26.78 | 71.3 | Concrete Pipe | 6,995.82 | 6,992.24 |
| 146: P-87 (1) | P-87 (1) | MH#9 | 6,989.76 | MH#8 | 6,986.87 | 197.4 | 0.015 | 24.0 | 0.013 | 19.10 | 6.08 | 27.33 | 69.9 | Concrete Pipe | 6,992.21 | 6,990.80 |
| 147: P-84 | P-84 | I#4 (DP14) | 6,995.69 | MH#10 (DP 1...) | 6,994.25 | 8.1 | 0.179 | 18.0 | 0.013 | 8.80 | 4.98 | 44.40 | 19.8 | Concrete Pipe | 6,997.31 | 6,997.25 |
| 148: P-84 (1) | P-84 (1) | MH#10 (DP 1...) | 6,994.75 | I#5 (DP 15) | 6,995.50 | 53.9 | -0.014 | 18.0 | 0.013 | 10.40 | 5.89 | 12.40 | 83.9 | Concrete Pipe | 6,997.78 | 6,997.25 |
| 149: P-66 | P-66 | MH#23 | 6,988.82 | MH#24 | 6,988.08 | 149.0 | 0.005 | 48.0 | 0.013 | 112.10 | 8.92 | 101.56 | 110.4 | Concrete Pipe | 6,994.23 | 6,993.32 |
| 150: P-68 | P-68 | MH#24 | 6,988.08 | MH#25 (DP13) | 6,987.54 | 107.8 | 0.005 | 48.0 | 0.013 | 112.10 | 8.92 | 101.56 | 110.4 | Concrete Pipe | 6,993.36 | 6,992.70 |
| 151: P-77 | P-77 | DP 12 | 6,990.32 | MH#25 (DP13) | 6,990.03 | 28.1 | 0.010 | 18.0 | 0.013 | 24.40 | 13.81 | 10.66 | 228.8 | Concrete Pipe | 6,994.22 | 6,992.70 |
| 152: P-74 | P-74 | MH#25 (DP13) | 6,987.54 | OUTLET SEGM... | 6,986.67 | 173.3 | 0.005 | 48.0 | 0.013 | 136.40 | 10.85 | 101.56 | 134.3 | Concrete Pipe | 6,991.97 | 6,990.15 |

NOTE: SEE PROFILES FOR PIPES STUDIED WITH THIS ANALYSIS

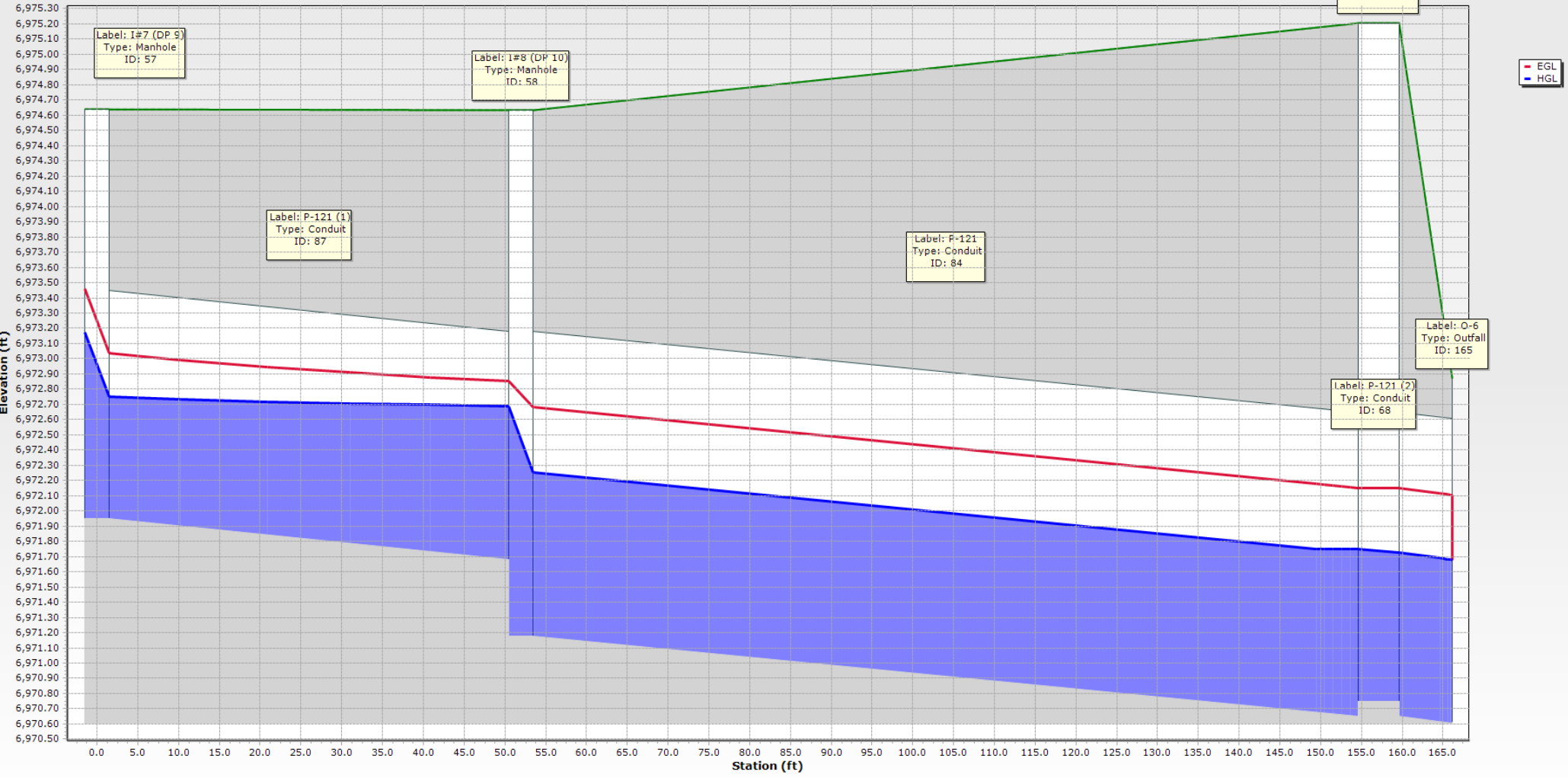
100 YEAR FREE OUTFALL CONDITION: STRUCTURE SUMMARY TABLE

| | Label | Elevation (Ground) (ft) | Elevation (Rim) (ft) | Flow (Total Out) (cfs) | Depth (Out) (ft) | Hydraulic Grade Line (Out) (ft) | Hydraulic Grade Line (In) (ft) | Notes | Elevation (Invert Out) (ft) | Headloss (ft) |
|-----------------|-----------------|-------------------------|----------------------|------------------------|------------------|---------------------------------|--------------------------------|----------------|-----------------------------|---------------|
| 35: MH#7 | MH#7 | 6,993.52 | 6,993.52 | 53.30 | 2.47 | 6,987.84 | 6,988.38 | STORM MH | 6,985.38 | 0.54 |
| 36: I#1 (DP 16) | I#1 (DP 16) | 6,993.41 | 6,993.41 | 5.10 | 0.87 | 6,990.61 | 6,991.15 | CDOT Type- | 6,989.74 | 0.54 |
| 37: MH#4 DP | MH#4 DP 18) | 6,993.40 | 6,993.40 | 26.20 | 2.88 | 6,988.54 | 6,989.64 | STORM MH | 6,985.66 | 1.10 |
| 38: I#2 (DP 17) | I#2 (DP 17) | 6,993.39 | 6,993.39 | 10.50 | 1.17 | 6,989.95 | 6,990.44 | CDOT Type- | 6,988.79 | 0.49 |
| 39: MH#6 | MH#6 | 6,993.02 | 6,993.02 | 53.30 | 2.65 | 6,987.15 | 6,987.61 | STORM MH | 6,984.50 | 0.46 |
| 40: MH#5 | MH#5 | 6,991.91 | 6,991.91 | 53.30 | 2.28 | 6,986.41 | 6,987.05 | STORM MH | 6,984.13 | 0.64 |
| 41: MH#3 (DP | MH#3 (DP 8) | 6,991.13 | 6,991.13 | 1.77 | 2.48 | 6,983.59 | 6,983.59 | STORM MH | 6,981.11 | 0.00 |
| 42: I#3 (DP 7) | I#3 (DP 7) | 6,990.73 | 6,990.73 | 53.30 | 2.83 | 6,988.48 | 6,989.49 | CDOT Type- | 6,985.73 | 1.01 |
| 43: 18 (DP 19) | 18 (DP 19) | 6,988.71 | 6,988.71 | 3.00 | 2.43 | 6,983.93 | 6,984.30 | CDOT Type- | 6,983.26 | 0.37 |
| 44: MH#2 (DP | MH#2 (DP 8) | 6,985.74 | 6,985.74 | 54.30 | 2.31 | 6,982.94 | 6,983.59 | STORM MH | 6,980.63 | 0.65 |
| 45: I#4 (DP 13) | I#4 (DP 13) | 6,985.02 | 6,985.02 | 3.40 | 1.42 | 6,982.73 | 6,982.84 | CDOT Type- | 6,981.51 | 0.12 |
| 46: I#5 (DP 14) | I#5 (DP 14) | 6,985.02 | 6,985.02 | 6.50 | 1.28 | 6,982.33 | 6,982.69 | CDOT Type- | 6,981.25 | 0.36 |
| 47: MH#1 | MH#1 | 6,984.95 | 6,984.95 | 54.30 | 2.31 | 6,982.45 | 6,982.55 | STORM MH | 6,980.14 | 0.10 |
| 49: 44 (69) (D | 44 (69) (DP 15) | 6,982.64 | 6,982.64 | 1.20 | 0.41 | 6,978.83 | 6,978.85 | CDOT Type- | 6,978.42 | 0.01 |
| 55: 44 (80) | 44 (80) | 6,975.21 | 6,975.21 | 9.00 | 0.98 | 6,971.73 | 6,971.75 | Cylindrical S' | 6,970.65 | 0.02 |
| 56: 44 (81) | 44 (81) | 6,975.03 | 6,975.03 | 3.60 | 0.72 | 6,970.76 | 6,970.79 | Cylindrical S' | 6,970.04 | 0.03 |
| 57: I#7 (DP 9) | I#7 (DP 9) | 6,974.64 | 6,974.64 | 4.10 | 0.80 | 6,972.75 | 6,973.18 | CDOT Type- | 6,971.95 | 0.43 |
| 58: I#8 (DP 10) | I#8 (DP 10) | 6,974.64 | 6,974.64 | 9.00 | 1.07 | 6,972.25 | 6,972.69 | CDOT Type- | 6,971.18 | 0.44 |
| 59: I#6 (DP 1) | I#6 (DP 1) | 6,973.20 | 6,973.20 | 3.60 | 0.72 | 6,971.57 | 6,972.00 | CDOT Type- | 6,970.85 | 0.42 |
| 60: 44 (78) (D | 44 (78) (DP 11) | 6,973.16 | 6,973.16 | 1.40 | 0.44 | 6,968.87 | 6,969.03 | CDOT Type- | 6,968.42 | 0.16 |
| 98: MH#26 (D | MH#26 (DP6.1) | 7,027.15 | 7,027.15 | 22.40 | 1.69 | 7,022.79 | 7,024.51 | STORM MH | 7,021.10 | 1.73 |
| 99: MH#27 (D | MH#27 (DP8) | 7,027.09 | 7,027.09 | 21.00 | 3.34 | 7,025.00 | 7,025.62 | STORM MH | 7,021.66 | 0.62 |
| 100: I#9 (DP6) | I#9 (DP6) | 7,027.04 | 7,027.04 | 2.40 | 1.67 | 7,024.53 | 7,024.56 | CDOT Type- | 7,022.86 | 0.03 |
| 101: I#8 (DP5) | I#8 (DP5) | 7,026.63 | 7,026.63 | 1.30 | 1.27 | 7,024.57 | 7,024.58 | CDOT Type- | 7,023.30 | 0.02 |
| 102: I#7 (DP3. | I#7 (DP3.1) | 7,026.51 | 7,026.51 | 3.20 | 1.71 | 7,023.01 | 7,023.02 | CDOT Type- | 7,021.80 | 0.00 |
| 103: I#6 (DP2. | I#6 (DP2.1) | 7,026.40 | 7,026.40 | 1.50 | 0.63 | 7,022.99 | 7,023.10 | CDOT Type- | 7,022.36 | 0.10 |
| 106: MH#34 | MH#34 | 7,023.51 | 7,023.51 | 3.40 | 0.70 | 7,019.72 | 7,019.84 | CDOT Type- | 7,019.01 | 0.13 |
| 111: MH#21 | MH#21 | 7,014.03 | 7,014.03 | 112.10 | 3.20 | 7,001.72 | 7,003.94 | STORM MH | 6,998.52 | 2.22 |
| 112: MH#20 | MH#20 | 7,012.41 | 7,012.41 | 112.10 | 4.38 | 7,005.57 | 7,005.63 | STORM MH | 7,001.18 | 0.06 |
| 113: MH#19 | MH#19 | 7,010.85 | 7,010.85 | 112.10 | 3.20 | 7,007.14 | 7,009.36 | STORM MH | 7,003.94 | 2.22 |
| 115: MH#22 | MH#22 | 7,005.85 | 7,005.85 | 112.10 | 3.20 | 6,998.35 | 6,998.44 | STORM MH | 6,995.15 | 0.08 |
| 116: MH#9 | MH#9 | 7,001.03 | 7,001.03 | 19.10 | 2.45 | 6,992.21 | 6,992.24 | STORM MH | 6,989.76 | 0.03 |
| 117: I#4 (DP1) | I#4 (DP14) | 7,000.17 | 7,000.17 | 8.80 | 1.62 | 6,997.31 | 6,997.89 | CDOT Type- | 6,995.69 | 0.58 |
| 118: MH#10 (| MH#10 (DP 1... | 7,000.01 | 7,000.01 | 19.10 | 1.57 | 6,995.82 | 6,997.25 | STORM MH | 6,994.25 | 1.43 |
| 119: I#5 (DP 1 | I#5 (DP 15) | 6,999.67 | 6,999.67 | 10.40 | 1.88 | 6,997.78 | 6,998.59 | CDOT Type- | 6,995.50 | 0.81 |
| 120: MH#8 | MH#8 | 6,996.13 | 6,996.13 | 19.10 | 3.77 | 6,990.43 | 6,990.80 | STORM MH | 6,986.87 | 0.37 |
| 121: MH#23 | MH#23 | 6,995.25 | 6,995.25 | 112.10 | 5.41 | 6,994.23 | 6,994.29 | STORM MH | 6,988.82 | 0.06 |
| 122: MH#24 | MH#24 | 6,993.32 | 6,993.32 | 112.10 | 5.25 | 6,993.32 | 6,993.39 | STORM MH | 6,988.08 | 0.06 |
| 123: DP12 | DP 12 | 6,993.02 | 6,993.02 | 24.40 | 2.71 | 6,993.02 | 6,997.47 | CDOT Type- | 6,990.32 | 4.44 |
| 124: MH#25 (| MH#25 (DP13) | 6,992.79 | 6,992.79 | 136.40 | 4.43 | 6,991.97 | 6,992.70 | STORM MH | 6,987.54 | 0.73 |
| 190: INLET (D | INLET (DP 3) | 6,980.96 | 6,980.96 | 24.50 | 1.69 | 6,979.85 | 6,980.98 | CDOT FES | 6,978.16 | 1.13 |
| 192: DP 7 | DP 7 | 7,024.45 | 7,024.45 | 2.20 | 1.44 | 7,024.45 | 7,024.52 | CDOT FES | 7,023.01 | 0.07 |
| 193: DP 2 | DP 2 | 7,024.26 | 7,024.26 | 18.80 | 2.25 | 7,024.26 | 7,025.10 | CDOT FES | 7,021.66 | 0.83 |
| 194: DP 3 | DP 3 | 7,009.43 | 7,009.43 | 112.10 | 4.42 | 7,009.43 | 7,011.29 | CDOT FES | 7,005.01 | 1.86 |
| 196: CULVERT | CULVERT 1 (... | 7,000.01 | 7,000.01 | 245.50 | 2.66 | 6,999.67 | 7,001.66 | Dummy Null | 6,997.01 | 1.99 |
| 197: CULVERT | CULVERT 2 (... | 7,000.01 | 7,000.01 | 295.50 | 3.00 | 7,000.01 | 7,002.27 | Dummy Null | 6,997.01 | 2.26 |

| | ID | Label | Elevation (Ground) (ft) | Elevation (Invert) (ft) | Elevation (User Defined Tailwater) (ft) | Hydraulic Grade (ft) | Flow (Total Out) (cfs) | Notes |
|-----------------------|-----|---------------|-------------------------|-------------------------|---|----------------------|------------------------|------------|
| 48: OUTFALL | 48 | OUTFALL | 6,983.32 | 6,979.44 | | 6,981.73 | 54.30 | CDOT FES |
| 53: 44 (70) | 53 | 44 (70) | 6,979.33 | 6,977.55 | | 6,977.85 | 1.20 | CDOT FES |
| 54: 44 (65) | 54 | 44 (65) | 6,976.31 | 6,973.52 | | 6,974.58 | 24.50 | CDOT FES |
| 61: 44 (77) | 61 | 44 (77) | 6,971.10 | 6,969.39 | | 6,970.00 | 3.60 | CDOT FES |
| 64: 44 (79) | 64 | 44 (79) | 6,969.82 | 6,967.50 | | 6,967.84 | 1.40 | CDOT FES |
| 107: DP9 | 107 | DP9 | 7,022.74 | 7,020.49 | | 7,022.11 | 22.40 | CDOT FES |
| 108: FES OUTFALL 1 | 108 | FES OUTFALL 1 | 7,023.00 | 7,021.01 | 7,023.00 | 7,023.00 | 3.20 | CDOT FES |
| 110: MH#39 | 110 | MH#39 | 7,018.18 | 7,017.01 | | 7,017.55 | 3.40 | CDOT FES |
| 125: OUTLET SEGMENT 3 | 125 | OUTLET SEG... | 6,991.09 | 6,986.67 | 6,988.30 | 6,990.15 | 136.40 | CDOT FES |
| 162: O-3 | 162 | O-3 | 6,987.98 | 6,984.83 | 6,987.98 | 6,987.98 | 26.20 | Dummy Null |
| 164: O-5 | 164 | O-5 | 6,982.10 | 6,981.08 | 6,982.10 | 6,982.10 | 6.50 | Dummy Null |
| 165: O-6 | 165 | O-6 | 6,972.87 | 6,970.61 | 6,972.87 | 6,971.68 | 9.00 | Dummy Null |
| 203: O-7 | 203 | O-7 | 6,998.27 | 6,995.27 | | 6,997.02 | 245.50 | Dummy Null |
| 207: O-10 | 207 | O-10 | 6,998.27 | 6,995.27 | | 6,997.28 | 295.50 | Dummy Null |

NOTE: SEE PROFILES FOR PIPES STUDIED WITH THIS ANALYSIS

EASTONVILLE 5 - 100-YR FREE OUTFALL CONDITION



5 YEAR FREE OUTFALL CONDITION: PIPE SUMMARY TABLE

| | Label | Start Node | Invert (Start) (ft) | Stop Node | Invert (Stop) (ft) | Length (User Defined) (ft) | Slope (Calculated) (ft/ft) | Diameter (in) | Manning's n | Flow (cfs) | Velocity (ft/s) | Capacity (Full Flow) (cfs) | Flow / Capacity (Design) (%) | Notes | Hydraulic Grade Line (In) (ft) | Hydraulic Grade Line (Out) (ft) |
|------------------|---------------|-----------------|------------------------|-----------------|-----------------------|-------------------------------|-------------------------------|---------------|-------------|------------|-----------------|-------------------------------|---------------------------------|----------------|-----------------------------------|------------------------------------|
| 66: P-8 (1) (1) | P-8 (1) (1) | MH#4 DP 18) | 6,985.66 | O-3 | 6,984.83 | 41.6 | 0.020 | 24.0 | 0.013 | 15.60 | 10.12 | 31.99 | 48.8 | Concrete Pipe | 6,987.09 | 6,985.89 |
| 67: P-124 | P-124 | I#5 (DP 14) | 6,981.25 | O-5 | 6,981.08 | 34.3 | 0.005 | 18.0 | 0.013 | 3.90 | 4.25 | 7.43 | 52.5 | Concrete Pipe | 6,982.13 | 6,982.10 |
| 68: P-121 (2) | P-121 (2) | 44 (80) | 6,970.65 | O-6 | 6,970.61 | 9.0 | 0.005 | 24.0 | 0.013 | 4.20 | 4.29 | 15.95 | 26.3 | Concrete Pipe | 6,971.37 | 6,971.31 |
| 69: P-18 | P-18 | I#3 (DP 7) | 6,985.73 | MH#7 | 6,985.38 | 71.3 | 0.005 | 42.0 | 0.013 | 7.90 | 4.88 | 71.14 | 11.1 | Concrete Pipe | 6,986.58 | 6,986.42 |
| 70: P-20 | P-20 | MH#7 | 6,985.38 | MH#6 | 6,984.50 | 175.6 | 0.005 | 42.0 | 0.013 | 7.90 | 4.88 | 71.14 | 11.1 | Concrete Pipe | 6,986.22 | 6,985.54 |
| 71: P-5 | P-5 | I#2 (DP 17) | 6,989.29 | I#1 (DP 16) | 6,989.74 | 52.0 | -0.009 | 18.0 | 0.013 | 3.00 | 4.87 | 9.77 | 30.7 | Concrete Pipe | 6,990.40 | 6,990.02 |
| 72: P-8 (1) | P-8 (1) | I#2 (DP 17) | 6,988.79 | MH#4 DP 18) | 6,985.66 | 156.4 | 0.020 | 24.0 | 0.013 | 6.30 | 7.92 | 31.99 | 19.7 | Concrete Pipe | 6,989.68 | 6,987.76 |
| 73: P-21 | P-21 | MH#6 | 6,984.50 | MH#5 | 6,984.13 | 74.6 | 0.005 | 42.0 | 0.013 | 7.90 | 4.88 | 71.14 | 11.1 | Concrete Pipe | 6,985.35 | 6,985.17 |
| 74: P-22 | P-22 | MH#5 | 6,984.13 | MH#3 (DP 8) | 6,981.11 | 127.1 | 0.024 | 42.0 | 0.013 | 7.90 | 8.44 | 154.95 | 5.1 | Concrete Pipe | 6,984.97 | 6,982.26 |
| 75: P-15 | P-15 | 18 (DP 19) | 6,983.26 | MH#3 (DP 8) | 6,983.11 | 30.8 | 0.005 | 18.0 | 0.013 | 0.30 | 2.06 | 7.43 | 4.0 | Concrete Pipe | 6,983.47 | 6,983.31 |
| 76: P-15 (1) | P-15 (1) | MH#3 (DP 8) | 6,981.11 | MH#2 (DP 8) | 6,980.73 | 75.1 | 0.005 | 42.0 | 0.013 | 8.30 | 4.95 | 71.14 | 11.7 | Concrete Pipe | 6,981.98 | 6,981.70 |
| 77: P-16 | P-16 | MH#2 (DP 8) | 6,980.63 | MH#1 | 6,980.24 | 78.1 | 0.005 | 42.0 | 0.013 | 8.30 | 4.95 | 71.14 | 11.7 | Concrete Pipe | 6,981.50 | 6,981.05 |
| 78: P-123 | P-123 | I#4 (DP 13) | 6,981.51 | I#5 (DP 14) | 6,981.25 | 52.0 | 0.005 | 18.0 | 0.013 | 2.10 | 3.61 | 7.43 | 28.3 | Concrete Pipe | 6,982.35 | 6,982.34 |
| 79: P-17 | P-17 | MH#1 | 6,980.14 | OUTFALL | 6,979.44 | 139.8 | 0.005 | 42.0 | 0.013 | 8.30 | 4.95 | 71.14 | 11.7 | Concrete Pipe | 6,981.01 | 6,980.25 |
| 80: P-125 | P-125 | 44 (69) (DP 15) | 6,978.42 | 44 (70) | 6,977.55 | 54.5 | 0.016 | 18.0 | 0.013 | 4.00 | 6.37 | 13.30 | 30.1 | Concrete Pipe | 6,979.19 | 6,978.20 |
| 83: P-122 | P-122 | INLET (DP 3) | 6,978.16 | 44 (65) | 6,973.52 | 183.8 | 0.025 | 30.0 | 0.013 | 3.70 | 7.19 | 65.19 | 5.7 | Concrete Pipe | 6,978.80 | 6,973.93 |
| 84: P-121 | P-121 | I#8 (DP 10) | 6,971.18 | 44 (80) | 6,970.65 | 105.1 | 0.005 | 24.0 | 0.013 | 4.20 | 4.29 | 16.06 | 26.1 | Concrete Pipe | 6,971.90 | 6,971.38 |
| 85: P-130 | P-130 | I#6 (DP 1) | 6,970.85 | 44 (81) | 6,970.04 | 81.5 | 0.010 | 18.0 | 0.013 | 0.50 | 3.05 | 10.47 | 4.8 | Concrete Pipe | 6,971.11 | 6,970.31 |
| 86: P-130 (1) | P-130 (1) | 44 (81) | 6,970.04 | 44 (77) | 6,969.39 | 65.0 | 0.010 | 18.0 | 0.013 | 0.50 | 3.05 | 10.50 | 4.8 | Concrete Pipe | 6,970.30 | 6,969.61 |
| 87: P-121 (1) | P-121 (1) | I#8 (DP 10) | 6,971.68 | I#7 (DP 9) | 6,971.95 | 52.0 | -0.005 | 18.0 | 0.013 | 2.20 | 3.71 | 7.57 | 29.1 | Concrete Pipe | 6,972.51 | 6,972.23 |
| 88: P-131 | P-131 | 44 (78) (DP 11) | 6,968.42 | 44 (79) | 6,967.50 | 62.5 | 0.015 | 18.0 | 0.013 | 4.30 | 4.36 | 12.77 | 33.7 | Concrete Pipe | 6,969.24 | 6,968.91 |
| 126: P-111 | P-111 | MH#34 | 7,019.01 | MH#39 | 7,017.01 | 146.6 | 0.014 | 18.0 | 0.013 | 1.70 | 4.88 | 12.28 | 13.8 | Concrete Pipe | 7,019.50 | 7,017.39 |
| 127: P-89 | P-89 | MH#8 | 6,986.87 | MH#4 DP 18) | 6,985.66 | 111.1 | 0.011 | 24.0 | 0.013 | 10.20 | 7.25 | 23.64 | 43.2 | Concrete Pipe | 6,988.02 | 6,987.76 |
| 128: P-25 (1) | P-25 (1) | CULVERT 2 (...) | 6,997.01 | O-10 | 6,995.27 | 116.5 | 0.015 | | 0.013 | 11.20 | 5.01 | 461.86 | 2.4 | Concrete Box C | 6,997.35 | 6,995.49 |
| 129: P-25 | P-25 | CULVERT 1 (...) | 6,997.01 | O-7 | 6,995.27 | 116.6 | 0.015 | | 0.013 | 11.20 | 5.01 | 461.72 | 2.4 | Concrete Box C | 6,997.35 | 6,995.49 |
| 131: P-107 (2) | P-107 (2) (1) | MH#26 (DP6.1) | 7,021.10 | DP9 | 7,020.49 | 60.7 | 0.010 | 24.0 | 0.013 | 2.90 | 4.95 | 22.62 | 12.8 | Concrete Pipe | 7,021.69 | 7,020.97 |
| 132: P-103 | P-103 | I#9 (DP6) | 7,022.86 | MH#26 (DP6.1) | 7,021.84 | 42.7 | 0.024 | 18.0 | 0.013 | 1.20 | 5.37 | 16.22 | 7.4 | Concrete Pipe | 7,023.27 | 7,022.12 |
| 133: P-107 (2) | P-107 (2) | MH#27 (DP8) | 7,021.66 | MH#26 (DP6.1) | 7,021.09 | 56.6 | 0.010 | 24.0 | 0.013 | 2.00 | 4.44 | 22.62 | 8.8 | Concrete Pipe | 7,022.15 | 7,022.07 |
| 134: P-107 | P-107 | DP 7 | 7,023.01 | MH#27 (DP8) | 7,022.41 | 37.8 | 0.016 | 15.0 | 0.013 | 0.30 | 3.15 | 8.13 | 3.7 | Concrete Pipe | 7,023.22 | 7,022.58 |
| 135: P-107 (1) | P-107 (1) | MH#27 (DP8) | 7,021.66 | DP 2 | 7,021.66 | 43.9 | 0.000 | 24.0 | 0.013 | 1.70 | 0.76 | 2.17 | 78.3 | Concrete Pipe | 7,022.36 | 7,022.31 |
| 136: P-95 | P-95 | I#8 (DP5) | 7,023.30 | I#9 (DP6) | 7,023.06 | 47.5 | 0.005 | 18.0 | 0.013 | 0.70 | 2.64 | 7.43 | 9.4 | Concrete Pipe | 7,023.61 | 7,023.42 |
| 137: P-93 | P-93 | I#6 (DP2.1) | 7,022.36 | I#7 (DP3.1) | 7,021.80 | 55.9 | 0.010 | 18.0 | 0.013 | 0.80 | 3.51 | 10.51 | 7.6 | Concrete Pipe | 7,023.00 | 7,023.00 |
| 138: Pipe - (34) | Pipe - (34) | I#7 (DP3.1) | 7,021.80 | FES OUTFALL 1 | 7,021.01 | 33.5 | 0.023 | 18.0 | 0.013 | 1.60 | 5.81 | 16.07 | 10.0 | Concrete Pipe | 7,023.00 | 7,023.00 |
| 140: P-44 (1) | P-44 (1) | MH#20 | 7,001.18 | MH#21 | 6,998.52 | 266.5 | 0.010 | 48.0 | 0.013 | 6.10 | 5.68 | 143.63 | 4.2 | Concrete Pipe | 7,001.90 | 6,999.57 |
| 141: P-64 | P-64 | MH#21 | 6,998.52 | MH#22 | 6,995.26 | 316.5 | 0.010 | 48.0 | 0.013 | 6.10 | 5.74 | 145.88 | 4.2 | Concrete Pipe | 6,999.24 | 6,995.82 |
| 142: P-44 | P-44 | MH#19 | 7,003.94 | MH#20 | 7,001.28 | 266.5 | 0.010 | 48.0 | 0.013 | 6.10 | 5.68 | 143.63 | 4.2 | Concrete Pipe | 7,004.66 | 7,001.84 |
| 143: P-26 | P-26 | DP 3 | 7,005.01 | MH#19 | 7,004.04 | 81.5 | 0.012 | 48.0 | 0.013 | 6.10 | 6.03 | 156.73 | 3.9 | Concrete Pipe | 7,005.73 | 7,004.99 |
| 144: P-64 (1) | P-64 (1) | MH#22 | 6,995.15 | MH#23 | 6,988.82 | 316.6 | 0.020 | 48.0 | 0.013 | 6.10 | 7.23 | 203.15 | 3.0 | Concrete Pipe | 6,995.87 | 6,989.55 |
| 145: P-87 | P-87 | MH#10 (DP 1...) | 6,994.25 | MH#9 | 6,989.76 | 320.7 | 0.014 | 24.0 | 0.013 | 10.20 | 7.94 | 26.78 | 38.1 | Concrete Pipe | 6,995.39 | 6,990.92 |
| 146: P-87 (1) | P-87 (1) | MH#9 | 6,989.76 | MH#8 | 6,986.87 | 197.4 | 0.015 | 24.0 | 0.013 | 10.20 | 8.07 | 27.33 | 37.3 | Concrete Pipe | 6,990.90 | 6,988.32 |
| 147: P-84 | P-84 | I#4 (DP14) | 6,995.69 | MH#10 (DP 1...) | 6,994.25 | 8.1 | 0.179 | 18.0 | 0.013 | 5.20 | 16.82 | 44.40 | 11.7 | Concrete Pipe | 6,996.57 | 6,996.22 |
| 148: P-84 (1) | P-84 (1) | MH#10 (DP 1...) | 6,994.75 | I#5 (DP 15) | 6,995.50 | 53.9 | -0.014 | 18.0 | 0.013 | 5.00 | 6.64 | 12.40 | 40.3 | Concrete Pipe | 6,996.36 | 6,996.22 |
| 149: P-66 | P-66 | MH#23 | 6,988.82 | MH#24 | 6,988.08 | 149.0 | 0.005 | 48.0 | 0.013 | 6.10 | 4.45 | 101.56 | 6.0 | Concrete Pipe | 6,989.54 | 6,989.26 |
| 150: P-68 | P-68 | MH#24 | 6,988.08 | MH#25 (DP13) | 6,987.54 | 107.8 | 0.005 | 48.0 | 0.013 | 6.10 | 4.45 | 101.56 | 6.0 | Concrete Pipe | 6,989.26 | 6,989.27 |
| 151: P-77 | P-77 | DP 12 | 6,990.32 | MH#25 (DP13) | 6,990.03 | 28.1 | 0.010 | 18.0 | 0.013 | 3.60 | 5.45 | 10.66 | 33.8 | Concrete Pipe | 6,991.04 | 6,990.64 |
| 152: P-74 | P-74 | MH#25 (DP13) | 6,987.54 | OUTLET SEGM... | 6,986.67 | 173.3 | 0.005 | 48.0 | 0.013 | 26.00 | 6.76 | 101.56 | 25.6 | Concrete Pipe | 6,989.05 | 6,988.30 |

NOTE: SEE PROFILES FOR PIPES STUDIED WITH THIS ANALYSIS

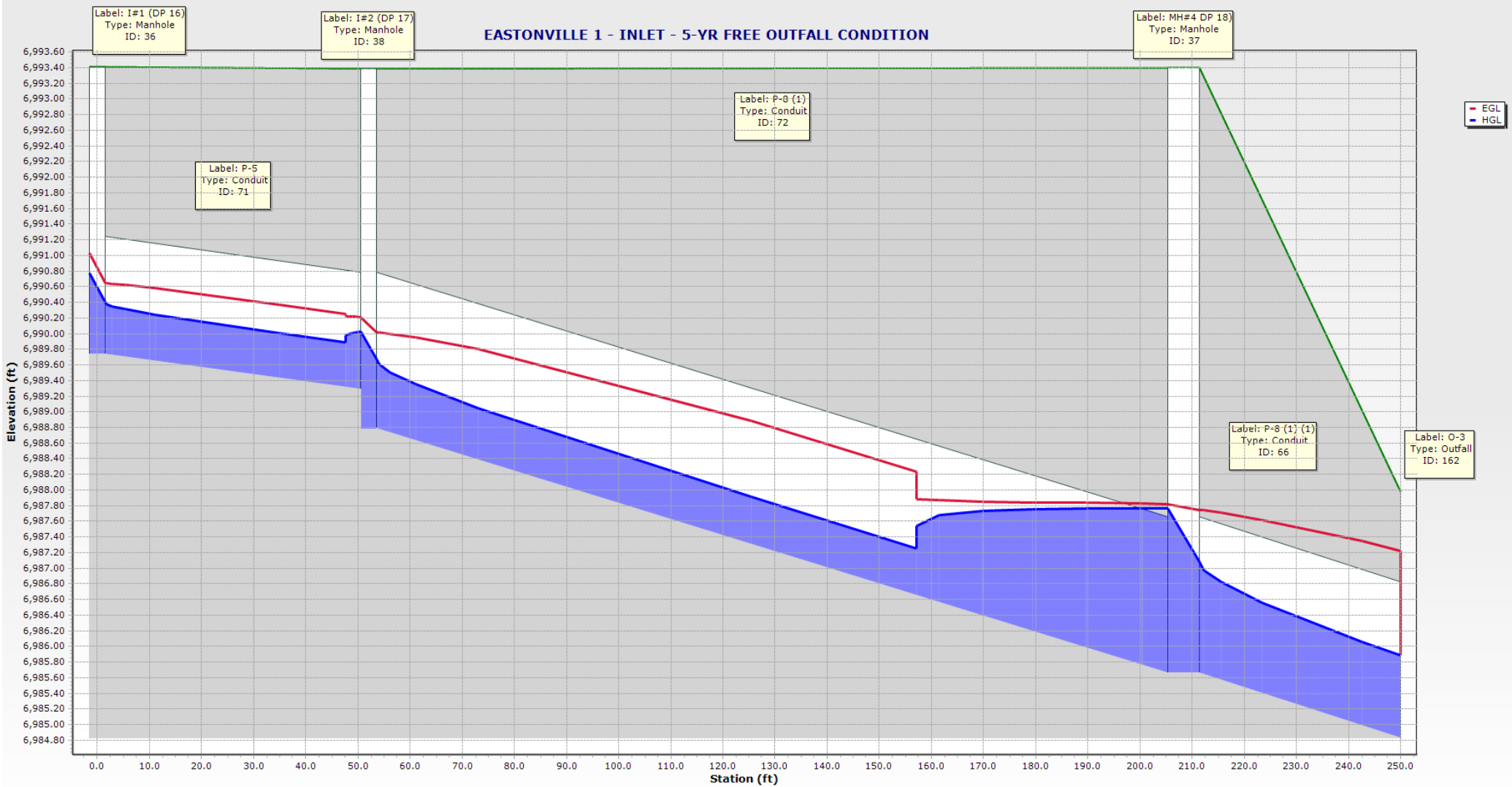
5 YEAR FREE OUTFALL CONDITION: STRUCTURE SUMMARY TABLE

| | Label | Elevation (Ground) (ft) | Elevation (Rim) (ft) | Flow (Total Out) (cfs) | Depth (Out) (ft) | Hydraulic Grade Line (Out) (ft) | Hydraulic Grade Line (In) (ft) | Notes | Elevation (Invert Out) (ft) | Headloss (ft) |
|-----------------|-----------------|-------------------------|----------------------|------------------------|------------------|---------------------------------|--------------------------------|---------------|-----------------------------|---------------|
| 35: MH#7 | MH#7 | 6,993.52 | 6,993.52 | 7.90 | 0.85 | 6,986.22 | 6,986.42 | STORM MH | 6,985.38 | 0.19 |
| 36: I#1 (DP 16) | I#1 (DP 16) | 6,993.41 | 6,993.41 | 3.00 | 0.66 | 6,990.40 | 6,990.77 | CDOT Type- | 6,989.74 | 0.38 |
| 37: MH#4 DP | MH#4 DP 18) | 6,993.40 | 6,993.40 | 15.60 | 1.42 | 6,987.09 | 6,987.76 | STORM MH | 6,985.66 | 0.67 |
| 38: I#2 (DP 17) | I#2 (DP 17) | 6,993.39 | 6,993.39 | 6.30 | 0.90 | 6,989.68 | 6,990.02 | CDOT Type- | 6,988.79 | 0.35 |
| 39: MH#6 | MH#6 | 6,993.02 | 6,993.02 | 7.90 | 0.85 | 6,985.35 | 6,985.54 | STORM MH | 6,984.50 | 0.19 |
| 40: MH#5 | MH#5 | 6,991.91 | 6,991.91 | 7.90 | 0.85 | 6,984.97 | 6,985.17 | STORM MH | 6,984.13 | 0.19 |
| 41: MH#3 (DP | MH#3 (DP 8) | 6,991.13 | 6,991.13 | 8.30 | 0.87 | 6,981.98 | 6,982.26 | STORM MH | 6,981.11 | 0.28 |
| 42: I#3 (DP 7) | I#3 (DP 7) | 6,990.73 | 6,990.73 | 7.90 | 0.93 | 6,986.58 | 6,987.03 | CDOT Type- | 6,985.73 | 0.45 |
| 43: 18 (DP 19) | 18 (DP 19) | 6,988.71 | 6,988.71 | 0.30 | 1.97 | 6,983.47 | 6,983.57 | CDOT Type- | 6,983.26 | 0.10 |
| 44: MH#2 (DP | MH#2 (DP 8) | 6,985.74 | 6,985.74 | 8.30 | 0.87 | 6,981.50 | 6,981.70 | STORM MH | 6,980.63 | 0.20 |
| 45: I#4 (DP 13) | I#4 (DP 13) | 6,985.02 | 6,985.02 | 2.10 | 1.04 | 6,982.35 | 6,982.45 | CDOT Type- | 6,981.51 | 0.10 |
| 46: I#5 (DP 14) | I#5 (DP 14) | 6,985.02 | 6,985.02 | 3.90 | 1.09 | 6,982.13 | 6,982.34 | CDOT Type- | 6,981.25 | 0.21 |
| 47: MH#1 | MH#1 | 6,984.95 | 6,984.95 | 8.30 | 0.87 | 6,981.01 | 6,981.04 | STORM MH | 6,980.14 | 0.03 |
| 49: 44 (69) (D | 44 (69) (DP 15) | 6,982.64 | 6,982.64 | 4.00 | 0.77 | 6,979.19 | 6,979.22 | CDOT Type- | 6,978.42 | 0.03 |
| 55: 44 (80) | 44 (80) | 6,975.21 | 6,975.21 | 4.20 | 0.72 | 6,971.37 | 6,971.38 | Cylindrical S | 6,970.65 | 0.01 |
| 56: 44 (81) | 44 (81) | 6,975.03 | 6,975.03 | 0.50 | 0.26 | 6,970.30 | 6,970.31 | Cylindrical S | 6,970.04 | 0.01 |
| 57: I#7 (DP 9) | I#7 (DP 9) | 6,974.64 | 6,974.64 | 2.20 | 0.56 | 6,972.51 | 6,972.82 | CDOT Type- | 6,971.95 | 0.31 |
| 58: I#8 (DP 10) | I#8 (DP 10) | 6,974.64 | 6,974.64 | 4.20 | 0.72 | 6,971.90 | 6,972.17 | CDOT Type- | 6,971.18 | 0.27 |
| 59: I#6 (DP 1) | I#6 (DP 1) | 6,973.20 | 6,973.20 | 0.50 | 0.26 | 6,971.11 | 6,971.25 | CDOT Type- | 6,970.85 | 0.14 |
| 60: 44 (78) (D | 44 (78) (DP 11) | 6,973.16 | 6,973.16 | 4.30 | 0.82 | 6,969.24 | 6,969.54 | CDOT Type- | 6,968.42 | 0.30 |
| 98: MH#26 (D | MH#26 (DP6.1) | 7,027.15 | 7,027.15 | 2.90 | 0.60 | 7,021.69 | 7,022.07 | STORM MH | 7,021.10 | 0.38 |
| 99: MH#27 (D | MH#27 (DP8) | 7,027.09 | 7,027.09 | 2.00 | 0.49 | 7,022.15 | 7,022.31 | STORM MH | 7,021.66 | 0.16 |
| 100: I#9 (DP6) | I#9 (DP6) | 7,027.04 | 7,027.04 | 1.20 | 0.41 | 7,023.27 | 7,023.42 | CDOT Type- | 7,022.86 | 0.15 |
| 101: I#8 (DP5) | I#8 (DP5) | 7,026.63 | 7,026.63 | 0.70 | 0.31 | 7,023.61 | 7,023.77 | CDOT Type- | 7,023.30 | 0.16 |
| 102: I#7 (DP3) | I#7 (DP3.1) | 7,026.51 | 7,026.51 | 1.60 | 1.70 | 7,023.00 | 7,023.00 | CDOT Type- | 7,021.80 | 0.00 |
| 103: I#6 (DP2) | I#6 (DP2.1) | 7,026.40 | 7,026.40 | 0.80 | 0.64 | 7,023.00 | 7,023.03 | CDOT Type- | 7,022.36 | 0.03 |
| 106: MH#34 | MH#34 | 7,023.51 | 7,023.51 | 1.70 | 0.49 | 7,019.50 | 7,019.59 | CDOT Type- | 7,019.01 | 0.08 |
| 111: MH#21 | MH#21 | 7,014.03 | 7,014.03 | 6.10 | 0.72 | 6,999.24 | 6,999.57 | STORM MH | 6,998.52 | 0.33 |
| 112: MH#20 | MH#20 | 7,012.41 | 7,012.41 | 6.10 | 0.72 | 7,001.90 | 7,001.91 | STORM MH | 7,001.18 | 0.01 |
| 113: MH#19 | MH#19 | 7,010.85 | 7,010.85 | 6.10 | 0.72 | 7,004.66 | 7,004.99 | STORM MH | 7,003.94 | 0.33 |
| 115: MH#22 | MH#22 | 7,005.85 | 7,005.85 | 6.10 | 0.72 | 6,995.87 | 6,995.88 | STORM MH | 6,995.15 | 0.01 |
| 116: MH#9 | MH#9 | 7,001.03 | 7,001.03 | 10.20 | 1.14 | 6,990.90 | 6,990.92 | STORM MH | 6,989.76 | 0.02 |
| 117: I#4 (DP1) | I#4 (DP14) | 7,000.17 | 7,000.17 | 5.20 | 0.88 | 6,996.57 | 6,997.11 | CDOT Type- | 6,995.69 | 0.55 |
| 118: MH#10 (| MH#10 (DP 1... | 7,000.01 | 7,000.01 | 10.20 | 1.14 | 6,995.39 | 6,996.22 | STORM MH | 6,994.25 | 0.83 |
| 119: I#5 (DP 1) | I#5 (DP 15) | 6,999.67 | 6,999.67 | 5.00 | 0.46 | 6,996.36 | 6,996.89 | CDOT Type- | 6,995.50 | 0.53 |
| 120: MH#8 | MH#8 | 6,996.13 | 6,996.13 | 10.20 | 1.35 | 6,988.02 | 6,988.32 | STORM MH | 6,986.87 | 0.30 |
| 121: MH#23 | MH#23 | 6,995.25 | 6,995.25 | 6.10 | 0.72 | 6,989.54 | 6,989.55 | STORM MH | 6,988.82 | 0.01 |
| 122: MH#24 | MH#24 | 6,993.32 | 6,993.32 | 6.10 | 1.18 | 6,989.26 | 6,989.26 | STORM MH | 6,988.08 | 0.00 |
| 123: DP12 | DP12 | 6,993.02 | 6,993.02 | 3.60 | 0.73 | 6,991.04 | 6,991.47 | CDOT Type- | 6,990.32 | 0.42 |
| 124: MH#25 (| MH#25 (DP13) | 6,992.79 | 6,992.79 | 26.00 | 1.51 | 6,989.05 | 6,989.27 | STORM MH | 6,987.54 | 0.22 |
| 190: INLET (D | INLET (DP 3) | 6,980.96 | 6,980.96 | 3.70 | 0.63 | 6,978.80 | 6,979.13 | CDOT FES | 6,978.16 | 0.34 |
| 192: DP 7 | DP 7 | 7,024.45 | 7,024.45 | 0.30 | 0.21 | 7,023.22 | 7,023.33 | CDOT FES | 7,023.01 | 0.11 |
| 193: DP 2 | DP 2 | 7,024.26 | 7,024.26 | 1.70 | 0.35 | 7,022.36 | 7,022.43 | CDOT FES | 7,021.66 | 0.07 |
| 194: DP 3 | DP 3 | 7,009.43 | 7,009.43 | 6.10 | 0.72 | 7,005.73 | 7,006.10 | CDOT FES | 7,005.01 | 0.37 |
| 196: CULVERT | CULVERT 1 (... | 7,000.01 | 7,000.01 | 11.20 | 0.34 | 6,997.35 | 6,997.61 | Dummy Null | 6,997.01 | 0.25 |
| 197: CULVERT | CULVERT 2 (... | 7,000.01 | 7,000.01 | 11.20 | 0.34 | 6,997.35 | 6,997.61 | Dummy Null | 6,997.01 | 0.25 |

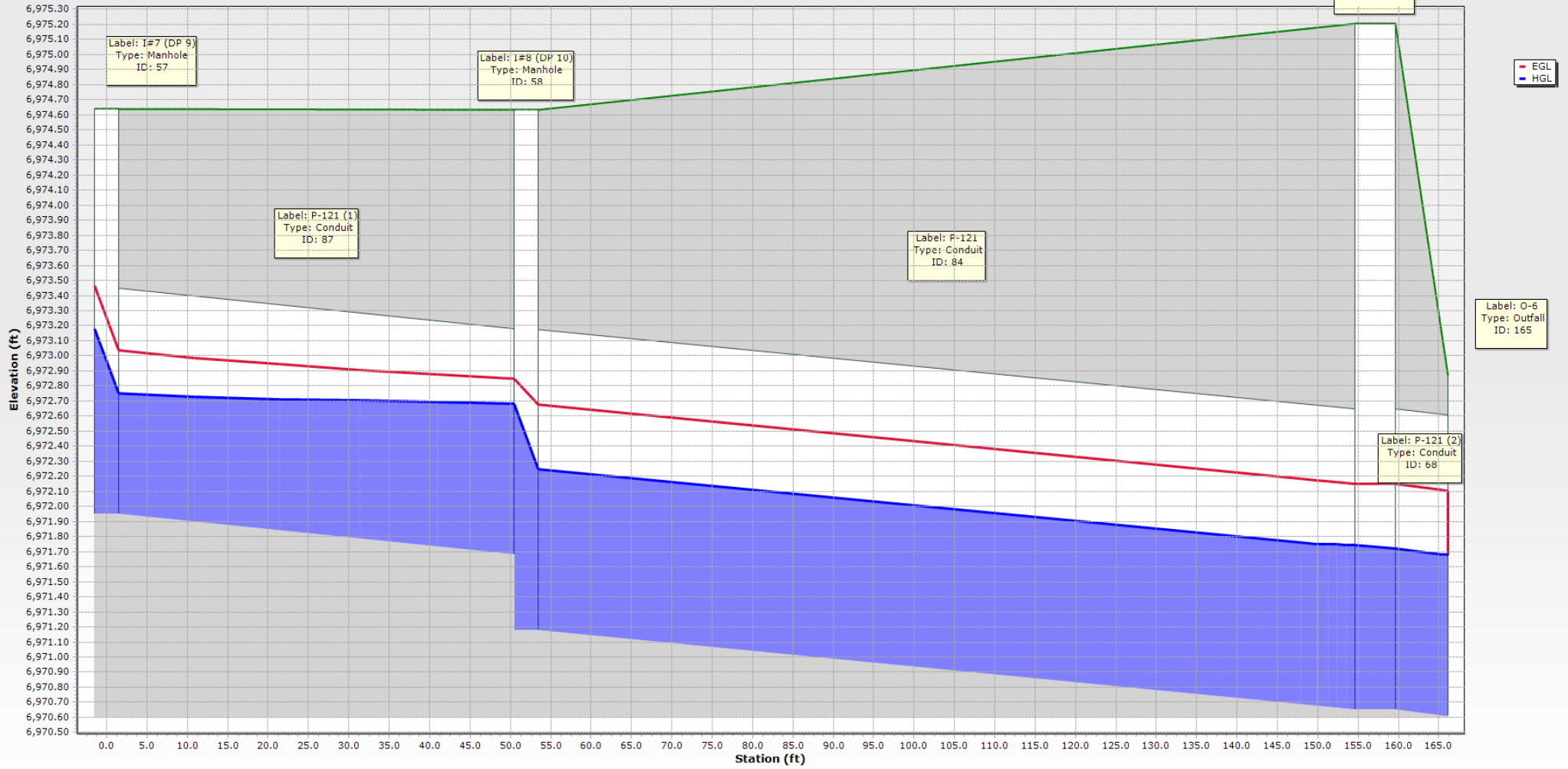
| | ID | Label | Elevation (Ground) (ft) | Elevation (Invert) (ft) | Elevation (User Defined Tailwater) (ft) | Hydraulic Grade (ft) | Flow (Total Out) (cfs) | Notes |
|-----------------------|-----|---------------|-------------------------|-------------------------|---|----------------------|------------------------|------------|
| 48: OUTFALL | 48 | OUTFALL | 6,983.32 | 6,979.44 | | 6,980.25 | 8.30 | CDOT FES |
| 53: 44 (70) | 53 | 44 (70) | 6,979.33 | 6,977.55 | | 6,978.20 | 4.00 | CDOT FES |
| 54: 44 (65) | 54 | 44 (65) | 6,976.31 | 6,973.52 | | 6,973.93 | 3.70 | CDOT FES |
| 61: 44 (77) | 61 | 44 (77) | 6,971.10 | 6,969.39 | | 6,969.61 | 0.50 | CDOT FES |
| 64: 44 (79) | 64 | 44 (79) | 6,969.82 | 6,967.50 | | 6,968.91 | 4.30 | CDOT FES |
| 107: DP9 | 107 | DP9 | 7,022.74 | 7,020.49 | | 7,020.97 | 2.90 | CDOT FES |
| 108: FES OUTFALL 1 | 108 | FES OUTFALL 1 | 7,023.00 | 7,021.01 | 7,023.00 | 7,023.00 | 1.60 | CDOT FES |
| 110: MH#39 | 110 | MH#39 | 7,018.18 | 7,017.01 | | 7,017.39 | 1.70 | CDOT FES |
| 125: OUTLET SEGMENT 3 | 125 | OUTLET SEG... | 6,991.09 | 6,986.67 | 6,988.30 | 6,988.30 | 26.00 | CDOT FES |
| 162: O-3 | 162 | O-3 | 6,987.98 | 6,984.83 | | 6,985.89 | 15.60 | Dummy Null |
| 164: O-5 | 164 | O-5 | 6,982.10 | 6,981.08 | 6,982.10 | 6,982.10 | 3.90 | Dummy Null |
| 165: O-6 | 165 | O-6 | 6,972.87 | 6,970.61 | | 6,971.31 | 4.20 | Dummy Null |
| 203: O-7 | 203 | O-7 | 6,998.27 | 6,995.27 | | 6,995.49 | 11.20 | Dummy Null |
| 207: O-10 | 207 | O-10 | 6,998.27 | 6,995.27 | | 6,995.49 | 11.20 | Dummy Null |

NOTE: SEE PROFILES FOR PIPES STUDIED WITH THIS ANALYSIS

EASTONVILLE 1 - INLET - 5-YR FREE OUTFALL CONDITION



EASTONVILLE 5 - 5-YR FREE OUTFALL CONDITION



APPENDIX D – WATER QUALITY & DETENTION

Please provide
forebay sizing calcs
for SFB A and D.

Provide sizing of riprap for
emergency overflows

Design Procedure Form: Sand Filter (SF)

UD-BMP (Version 3.07, March 2018)

Sheet 1 of 2

Designer: SPC
Company: HR Green
Date: March 12, 2024
Project: Eastonville Road - Segment 1 Improvements SFB A
Location: El Paso County, CO

1. Basin Storage Volume

- A) Effective Imperviousness of Tributary Area, I_a
(100% if all paved and roofed areas upstream of sand filter)
- B) Tributary Area's Imperviousness Ratio ($i = I_a/100$)
- C) Water Quality Capture Volume (WQCV) Based on 12-hour Drain Time
 $WQCV = 0.8 * (0.91 * i^3 - 1.19 * i^2 + 0.78 * i)$
- D) Contributing Watershed Area (including sand filter area)
- E) Water Quality Capture Volume (WQCV) Design Volume
 $V_{WQCV} = WQCV / 12 * Area$
- F) For Watersheds Outside of the Denver Region, Depth of Average Runoff Producing Storm
- G) For Watersheds Outside of the Denver Region, Water Quality Capture Volume (WQCV) Design Volume
- H) User Input of Water Quality Capture Volume (WQCV) Design Volume
(Only if a different WQCV Design Volume is desired)

$I_a =$ %
 $i =$
 WQCV = watershed inches
 Area = sq ft
 $V_{WQCV} =$ cu ft
 $d_e =$ in
 $V_{WQCV \text{ OTHER}} =$ cu ft
 $V_{WQCV \text{ USER}} =$ cu ft

does not match MHFD-Detention calcs below

2. Basin Geometry

- A) WQCV Depth
- B) Sand Filter Side Slopes (Horizontal distance per unit vertical, 4:1 or flatter preferred). Use "0" if sand filter has vertical walls.
- C) Minimum Filter Area (Flat Surface Area)
- D) Actual Filter Area
- E) Volume Provided

$D_{WQCV} =$ ft
 $Z =$ ft / ft
 $A_{Min} =$ sq ft
 $A_{Actual} =$ sq ft
 $V_T =$ cu ft

3. Filter Material

Choose One

18" CDOT Class B or C Filter Material
 Other (Explain): _____

4. Underdrain System

- A) Are underdrains provided?
- B) Underdrain system orifice diameter for 12 hour drain time
 - i) Distance From Lowest Elevation of the Storage Volume to the Center of the Orifice
 - ii) Volume to Drain in 12 Hours
 - iii) Orifice Diameter, 3/8" Minimum

Choose One

YES
 NO

$y =$ ft
 $Vol_{12} =$ cu ft
 $D_o =$ in

does not match what is shown on CDs

Unresolved from previous review: This value still does not match what is shown on the MHFD-Detention calcs below.

Design Procedure Form: Sand Filter (SF)

Sheet 2 of 2

Designer: SPC
Company: HR Green
Date: March 12, 2024
Project: Eastonville Road - Segment 1 Improvements SFB A
Location: El Paso County, CO

5. Impermeable Geomembrane Liner and Geotextile Separator Fabric

A) Is an impermeable liner provided due to proximity of structures or groundwater contamination?

Choose One

| | |
|---------------------------|-------------------------------------|
| <input type="radio"/> YES | <input checked="" type="radio"/> NO |
|---------------------------|-------------------------------------|

6. Inlet / Outlet Works

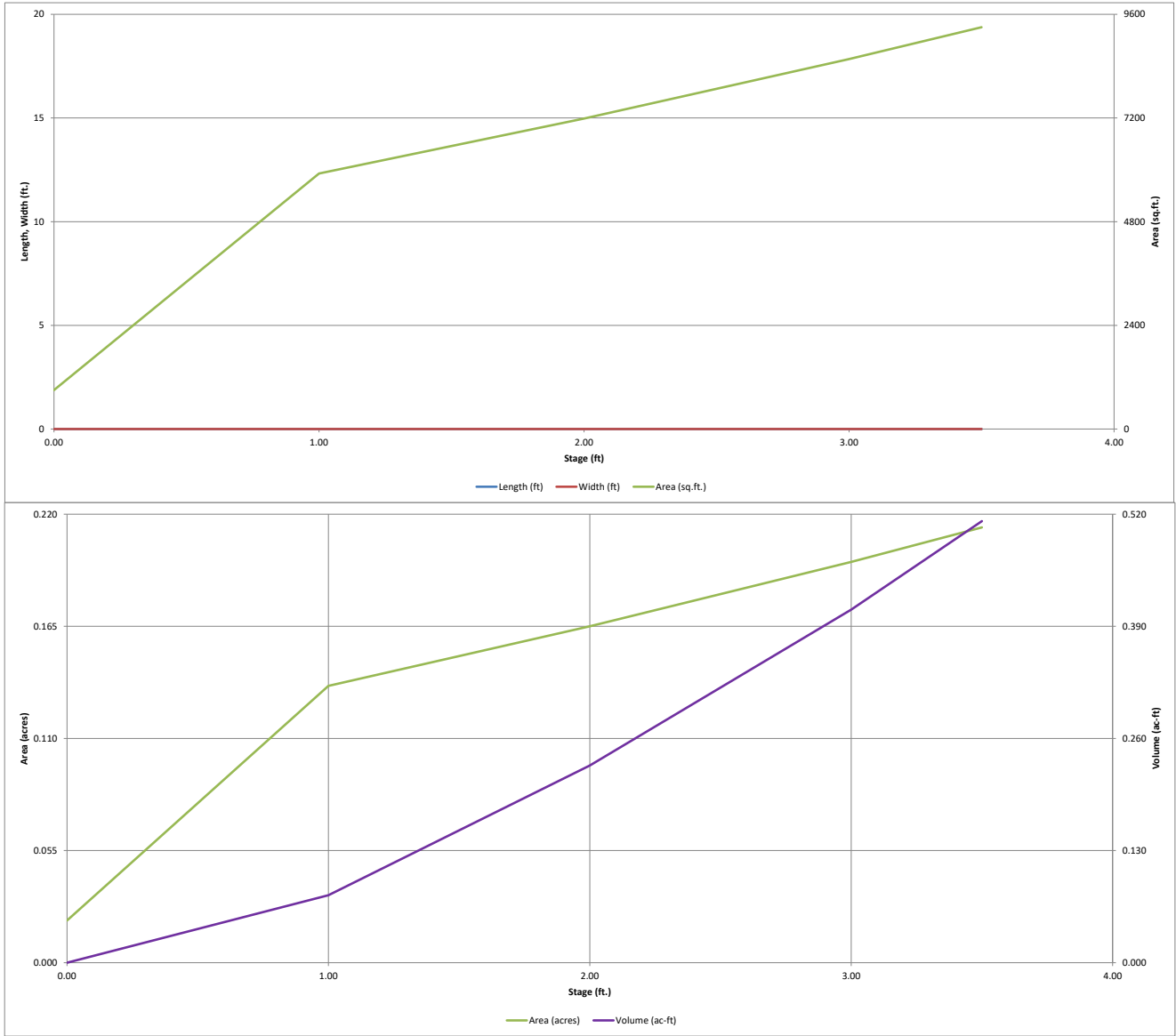
A) Describe the type of energy dissipation at inlet points and means of conveying flows in excess of the WQCV through the outlet

Energy dissipation at inlet points provided via riprap, and means of conveying flows in excess of the WQCV through the outlet is via the modified type 'C' inlet outlet structure grate, and a restricted outlet pipe.

Notes: _____

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.05 (January 2022)



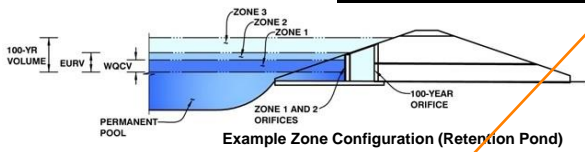
X = value does not match what is shown in the CDs.
✓ = value does match CDs.

Shown as 15/16" on UD-BMP calcs above. Revise to remove discrepancy.

DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.05 (January 2022)

Project: Eastonville Road
Basin ID: SFB A



| | Estimated Stage (ft) | Estimated Volume (ac-ft) | Outlet Type |
|-------------------|----------------------|--------------------------|----------------------|
| Zone 1 (WQCV) | 0.51 | 0.025 | Filtration Media |
| Zone 2 (EURV) | 1.18 | 0.077 | Circular Orifice |
| Zone 3 (100-year) | 1.65 | 0.071 | Weir&Pipe (Restrict) |
| Total (all zones) | | 0.173 | |

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Calculated Parameters for Underdrain

| | |
|---|---|
| Underdrain Orifice Invert Depth = 2.33 ft (distance below the filtration media surface) | Underdrain Orifice Area = 0.0 ft ² |
| Underdrain Orifice Diameter = 0.75 inches | Underdrain Orifice Centroid = 0.03 feet |

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Calculated Parameters for Plate

| | |
|--|---|
| Centroid of Lowest Orifice = N/A ft (relative to basin bottom at Stage = 0 ft) | WQ Orifice Area per Row = N/A ft ² |
| Depth at top of Zone using Orifice Plate = N/A ft (relative to basin bottom at Stage = 0 ft) | Elliptical Half-Width = N/A feet |
| Orifice Plate: Orifice Vertical Spacing = N/A inches | Elliptical Slot Centroid = N/A feet |
| Orifice Plate: Orifice Area per Row = N/A sq. inches | Elliptical Slot Area = N/A ft ² |

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

| | Row 1 (optional) | Row 2 (optional) | Row 3 (optional) | Row 4 (optional) | Row 5 (optional) | Row 6 (optional) | Row 7 (optional) | Row 8 (optional) |
|--------------------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|
| Stage of Orifice Centroid (ft) | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A |
| Orifice Area (sq. inches) | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A |

| | Row 9 (optional) | Row 10 (optional) | Row 11 (optional) | Row 12 (optional) | Row 13 (optional) | Row 14 (optional) | Row 15 (optional) | Row 16 (optional) |
|--------------------------------|------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| Stage of Orifice Centroid (ft) | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A |
| Orifice Area (sq. inches) | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A |

User Input: Vertical Orifice (Circular or Rectangular)

Calculated Parameters for Vertical Orifice

| | Zone 2 Circular | Not Selected | | Zone 2 Circular | Not Selected |
|--|-----------------|--------------|-----------------------------|-----------------|--------------|
| Invert of Vertical Orifice = 0.60 ft (relative to basin bottom at Stage = 0 ft) | N/A | N/A | Vertical Orifice Area = | 0.00 | N/A |
| Depth at top of Zone using Vertical Orifice = 1.18 ft (relative to basin bottom at Stage = 0 ft) | N/A | N/A | Vertical Orifice Centroid = | 0.02 | N/A |
| Vertical Orifice Diameter = 0.50 inches | N/A | N/A | | | |

User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir and No Outlet Pipe)

Calculated Parameters for Overflow Weir

| | Zone 3 Weir | Not Selected | | Zone 3 Weir | Not Selected |
|--|-------------|--------------|--|-------------|--------------|
| Overflow Weir Front Edge Height, H _o = 1.20 ft (relative to basin bottom at Stage = 0 ft) | N/A | N/A | Height of Grate Upper Edge, H _t = | 1.20 | N/A |
| Overflow Weir Front Edge Length = 3.00 feet | N/A | N/A | Overflow Weir Slope Length = | 3.00 | N/A |
| Overflow Weir Grate Slope = 0.00 H:V | N/A | N/A | Grate Open Area / 100-yr Orifice Area = | 49.13 | N/A |
| Horiz. Length of Weir Sides = 3.00 feet | N/A | N/A | Overflow Grate Open Area w/o Debris = | 6.26 | N/A |
| Overflow Grate Type = Type C Grate | N/A | N/A | Overflow Grate Open Area w/ Debris = | 3.13 | N/A |
| Debris Clogging % = 50% | N/A | N/A | | | |

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate

| | Zone 3 Restrictor | Not Selected | | Zone 3 Restrictor | Not Selected |
|--|-------------------|--------------|--|-------------------|--------------|
| Depth to Invert of Outlet Pipe = 2.35 ft (distance below basin bottom at Stage = 0 ft) | N/A | N/A | Outlet Orifice Area = | 0.13 | N/A |
| Outlet Pipe Diameter = 18.00 inches | N/A | N/A | Outlet Orifice Centroid = | 0.11 | N/A |
| Restrictor Plate Height Above Pipe Invert = 2.25 inches | N/A | N/A | Half-Central Angle of Restrictor Plate on Pipe = | 0.72 | N/A |

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Calculated Parameters for Spillway

| | |
|--|---|
| Spillway Invert Stage = 1.70 ft (relative to basin bottom at Stage = 0 ft) | Spillway Design Flow Depth = 0.30 feet |
| Spillway Crest Length = 4.75 feet | Stage at Top of Freeboard = 3.00 feet |
| Spillway End Slopes = 4.00 H:V | Basin Area at Top of Freeboard = 0.20 acres |
| Freeboard above Max Water Surface = 1.00 feet | Basin Volume at Top of Freeboard = 0.41 acre-ft |

Routed Hydrograph Results

The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).

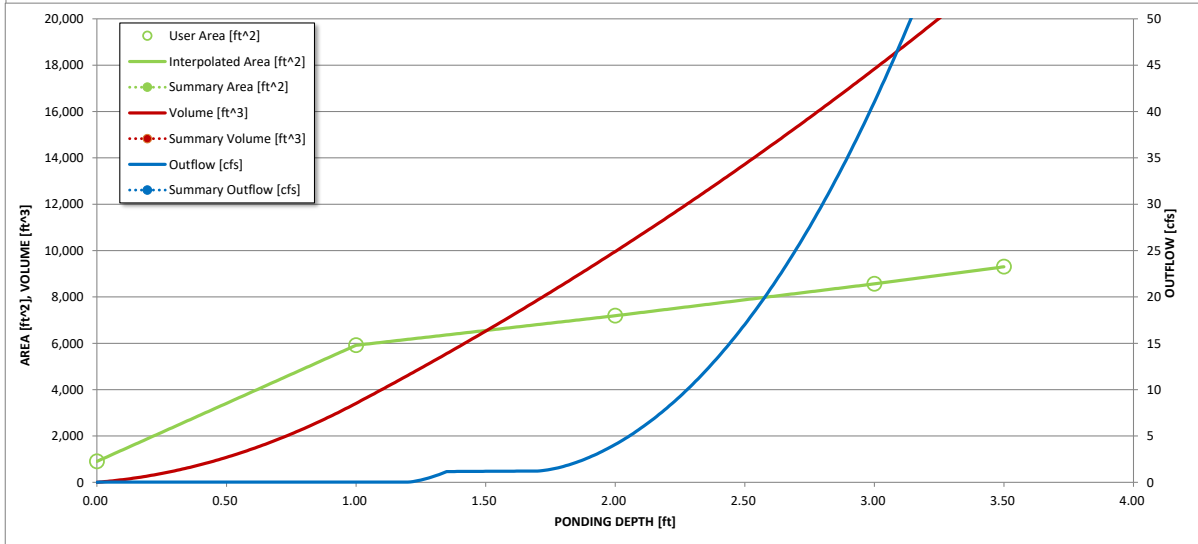
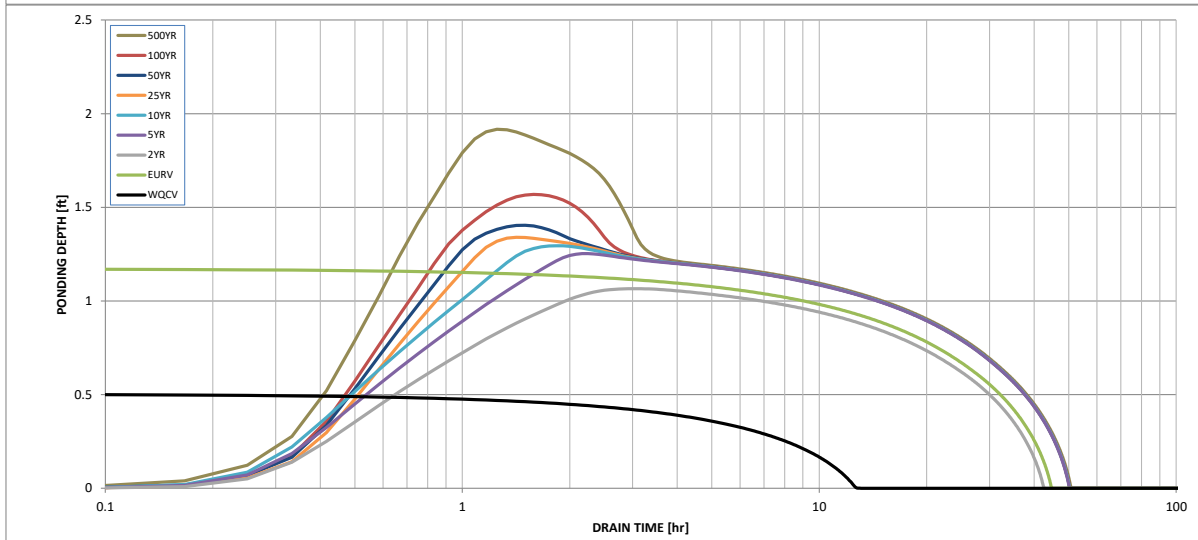
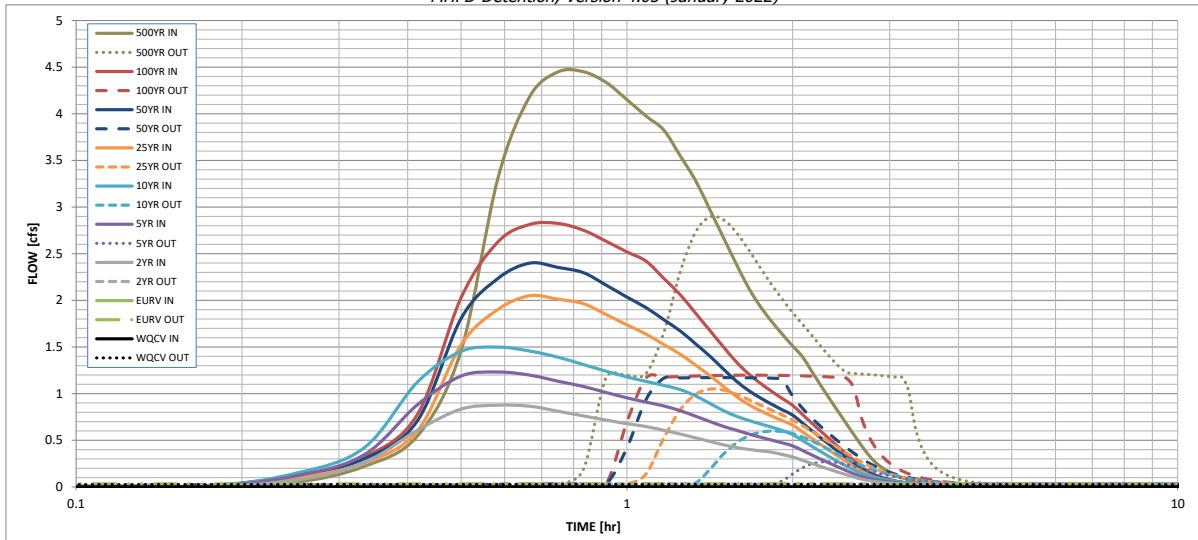
| | WQCV | EURV | 2 Year | 5 Year | 10 Year | 25 Year | 50 Year | 100 Year | 500 Year |
|---|------------------|--------------------|--------------------|-----------------|-----------------|-----------------|----------------|----------------|----------|
| Design Storm Return Period | N/A | N/A | 1.19 | 1.50 | 1.75 | 2.00 | 2.25 | 2.52 | 3.68 |
| One-Hour Rainfall Depth (in) | 0.025 | 0.102 | 0.095 | 0.133 | 0.167 | 0.210 | 0.246 | 0.291 | 0.464 |
| CUHP Runoff Volume (acre-ft) | N/A | N/A | 0.095 | 0.133 | 0.167 | 0.210 | 0.246 | 0.291 | 0.464 |
| Inflow Hydrograph Volume (acre-ft) | N/A | N/A | 0.1 | 0.3 | 0.4 | 0.7 | 0.9 | 1.2 | 2.2 |
| CUHP Predevelopment Peak Q (cfs) | N/A | N/A | 0.05 | 0.15 | 0.23 | 0.43 | 0.54 | 0.70 | 1.25 |
| OPTIONAL Override Predevelopment Peak Q (cfs) | N/A | N/A | 0.9 | 1.2 | 1.5 | 2.0 | 2.4 | 2.8 | 4.5 |
| Predevelopment Unit Peak Flow, q (cfs/acre) | N/A | N/A | 0.0 | 0.3 | 0.6 | 1.0 | 1.2 | 1.2 | 2.9 |
| Peak Inflow Q (cfs) | N/A | N/A | N/A | 1.1 | 1.5 | 1.4 | 1.3 | 1.0 | 1.3 |
| Peak Outflow Q (cfs) | N/A | N/A | N/A | 1.1 | 1.5 | 1.4 | 1.3 | 1.0 | 1.3 |
| Ratio Peak Outflow to Predevelopment Q | N/A | N/A | N/A | 1.1 | 1.5 | 1.4 | 1.3 | 1.0 | 1.3 |
| Structure Controlling Flow | Filtration Media | Vertical Orifice 1 | Vertical Orifice 1 | Overflow Weir 1 | Overflow Weir 1 | Overflow Weir 1 | Outlet Plate 1 | Outlet Plate 1 | Spillway |
| Max Velocity through Grate 1 (fps) | N/A | N/A | N/A | 0.0 | 0.1 | 0.2 | 0.2 | 0.2 | 0.2 |
| Max Velocity through Grate 2 (fps) | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A |
| Time to Drain 97% of Inflow Volume (hours) | 12 | 43 | 41 | 48 | 48 | 47 | 47 | 46 | 44 |
| Time to Drain 99% of Inflow Volume (hours) | 13 | 44 | 42 | 50 | 50 | 49 | 49 | 49 | 48 |
| Maximum Ponding Depth (ft) | 0.51 | 1.18 | 1.07 | 1.25 | 1.29 | 1.34 | 1.40 | 1.57 | 1.92 |
| Area at Maximum Ponding Depth (acres) | 0.08 | 0.14 | 0.14 | 0.14 | 0.14 | 0.15 | 0.15 | 0.15 | 0.16 |
| Maximum Volume Stored (acre-ft) | 0.026 | 0.103 | 0.086 | 0.113 | 0.119 | 0.126 | 0.135 | 0.159 | 0.214 |

Why isn't this value that is >1 highlighted in red?

Regardless, this ratio should be less than or equal to 1 for minor (5-yr) and major (100-yr) design storms. See Chapter 4.1 of DCM volume 2 (and also Chap 2 of MHFD DCM vol. 3).

DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.05 (January 2022)



| S-A-V-D Chart Axis Override | X-axis | Left Y-Axis | Right Y-Axis |
|-----------------------------|--------|-------------|--------------|
| minimum bound | | | |
| maximum bound | | | |

DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename: _____

Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

| Time Interval | SOURCE | CUHP | CUHP | CUHP | CUHP | CUHP | CUHP | CUHP | CUHP | CUHP |
|---------------|---------|------------|------------|--------------|--------------|---------------|---------------|---------------|----------------|----------------|
| | TIME | WQCV [cfs] | EURV [cfs] | 2 Year [cfs] | 5 Year [cfs] | 10 Year [cfs] | 25 Year [cfs] | 50 Year [cfs] | 100 Year [cfs] | 500 Year [cfs] |
| 5.00 min | 0:00:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 0:05:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 0:10:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.01 | 0.00 | 0.05 |
| | 0:15:00 | 0.00 | 0.00 | 0.07 | 0.12 | 0.14 | 0.10 | 0.12 | 0.12 | 0.22 |
| | 0:20:00 | 0.00 | 0.00 | 0.26 | 0.34 | 0.42 | 0.26 | 0.30 | 0.32 | 0.55 |
| | 0:25:00 | 0.00 | 0.00 | 0.61 | 0.88 | 1.12 | 0.60 | 0.71 | 0.78 | 1.46 |
| | 0:30:00 | 0.00 | 0.00 | 0.83 | 1.19 | 1.45 | 1.52 | 1.81 | 2.03 | 3.31 |
| | 0:35:00 | 0.00 | 0.00 | 0.88 | 1.23 | 1.50 | 1.90 | 2.23 | 2.63 | 4.19 |
| | 0:40:00 | 0.00 | 0.00 | 0.86 | 1.20 | 1.46 | 2.05 | 2.40 | 2.81 | 4.45 |
| | 0:45:00 | 0.00 | 0.00 | 0.81 | 1.13 | 1.39 | 2.01 | 2.35 | 2.82 | 4.45 |
| | 0:50:00 | 0.00 | 0.00 | 0.76 | 1.08 | 1.31 | 1.97 | 2.30 | 2.75 | 4.34 |
| | 0:55:00 | 0.00 | 0.00 | 0.72 | 1.01 | 1.24 | 1.85 | 2.16 | 2.63 | 4.15 |
| | 1:00:00 | 0.00 | 0.00 | 0.68 | 0.95 | 1.18 | 1.74 | 2.04 | 2.52 | 3.98 |
| | 1:05:00 | 0.00 | 0.00 | 0.65 | 0.91 | 1.13 | 1.64 | 1.92 | 2.42 | 3.83 |
| | 1:10:00 | 0.00 | 0.00 | 0.61 | 0.87 | 1.09 | 1.53 | 1.79 | 2.24 | 3.55 |
| | 1:15:00 | 0.00 | 0.00 | 0.57 | 0.82 | 1.04 | 1.42 | 1.67 | 2.06 | 3.28 |
| | 1:20:00 | 0.00 | 0.00 | 0.53 | 0.76 | 0.97 | 1.30 | 1.53 | 1.86 | 2.96 |
| | 1:25:00 | 0.00 | 0.00 | 0.49 | 0.70 | 0.89 | 1.19 | 1.40 | 1.67 | 2.66 |
| | 1:30:00 | 0.00 | 0.00 | 0.45 | 0.65 | 0.82 | 1.07 | 1.26 | 1.50 | 2.38 |
| | 1:35:00 | 0.00 | 0.00 | 0.42 | 0.61 | 0.76 | 0.97 | 1.13 | 1.33 | 2.12 |
| | 1:40:00 | 0.00 | 0.00 | 0.40 | 0.57 | 0.71 | 0.88 | 1.03 | 1.21 | 1.93 |
| | 1:45:00 | 0.00 | 0.00 | 0.39 | 0.53 | 0.67 | 0.81 | 0.95 | 1.11 | 1.77 |
| | 1:50:00 | 0.00 | 0.00 | 0.37 | 0.50 | 0.64 | 0.76 | 0.89 | 1.02 | 1.63 |
| | 1:55:00 | 0.00 | 0.00 | 0.35 | 0.47 | 0.60 | 0.71 | 0.83 | 0.95 | 1.51 |
| | 2:00:00 | 0.00 | 0.00 | 0.32 | 0.44 | 0.56 | 0.66 | 0.77 | 0.87 | 1.40 |
| | 2:05:00 | 0.00 | 0.00 | 0.28 | 0.39 | 0.50 | 0.59 | 0.68 | 0.78 | 1.24 |
| | 2:10:00 | 0.00 | 0.00 | 0.25 | 0.34 | 0.44 | 0.52 | 0.60 | 0.68 | 1.09 |
| | 2:15:00 | 0.00 | 0.00 | 0.22 | 0.30 | 0.38 | 0.45 | 0.52 | 0.60 | 0.94 |
| | 2:20:00 | 0.00 | 0.00 | 0.19 | 0.25 | 0.32 | 0.39 | 0.45 | 0.51 | 0.81 |
| | 2:25:00 | 0.00 | 0.00 | 0.16 | 0.21 | 0.27 | 0.33 | 0.38 | 0.43 | 0.68 |
| | 2:30:00 | 0.00 | 0.00 | 0.13 | 0.18 | 0.22 | 0.27 | 0.31 | 0.36 | 0.56 |
| | 2:35:00 | 0.00 | 0.00 | 0.10 | 0.14 | 0.18 | 0.22 | 0.25 | 0.28 | 0.44 |
| | 2:40:00 | 0.00 | 0.00 | 0.08 | 0.11 | 0.14 | 0.17 | 0.19 | 0.22 | 0.34 |
| | 2:45:00 | 0.00 | 0.00 | 0.07 | 0.09 | 0.12 | 0.13 | 0.15 | 0.16 | 0.26 |
| | 2:50:00 | 0.00 | 0.00 | 0.06 | 0.08 | 0.10 | 0.10 | 0.12 | 0.13 | 0.20 |
| | 2:55:00 | 0.00 | 0.00 | 0.05 | 0.06 | 0.08 | 0.08 | 0.09 | 0.10 | 0.16 |
| | 3:00:00 | 0.00 | 0.00 | 0.04 | 0.05 | 0.07 | 0.07 | 0.07 | 0.08 | 0.12 |
| | 3:05:00 | 0.00 | 0.00 | 0.03 | 0.04 | 0.06 | 0.05 | 0.06 | 0.06 | 0.10 |
| | 3:10:00 | 0.00 | 0.00 | 0.03 | 0.04 | 0.05 | 0.04 | 0.05 | 0.05 | 0.08 |
| | 3:15:00 | 0.00 | 0.00 | 0.02 | 0.03 | 0.04 | 0.04 | 0.04 | 0.04 | 0.06 |
| | 3:20:00 | 0.00 | 0.00 | 0.02 | 0.02 | 0.03 | 0.03 | 0.03 | 0.03 | 0.05 |
| | 3:25:00 | 0.00 | 0.00 | 0.02 | 0.02 | 0.03 | 0.02 | 0.03 | 0.02 | 0.04 |
| | 3:30:00 | 0.00 | 0.00 | 0.01 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 | 0.03 |
| | 3:35:00 | 0.00 | 0.00 | 0.01 | 0.01 | 0.02 | 0.01 | 0.02 | 0.02 | 0.02 |
| | 3:40:00 | 0.00 | 0.00 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 0.02 |
| | 3:45:00 | 0.00 | 0.00 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| | 3:50:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| | 3:55:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.01 |
| | 4:00:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 4:05:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 4:10:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 4:15:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 4:20:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 4:25:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 4:30:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 4:35:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 4:40:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 4:45:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 4:50:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 4:55:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 5:00:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| 5:05:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| 5:10:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| 5:15:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| 5:20:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| 5:25:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| 5:30:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| 5:35:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| 5:40:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| 5:45:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| 5:50:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| 5:55:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| 6:00:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |

Design Procedure Form: Extended Detention Basin (EDB)

UD-BMP (Version 3.07, March 2018)

Sheet 1 of 3

Designer: SPC
Company: HR Green
Date: March 12, 2024
Project: Eastonville Road - Segment 1 Improvements Pond B
Location: EL PASO COUNTY, CO

1. Basin Storage Volume

- A) Effective Imperviousness of Tributary Area, i_a
- B) Tributary Area's Imperviousness Ratio ($i = i_a / 100$)
- C) Contributing Watershed Area
- D) For Watersheds Outside of the Denver Region, Depth of Average Runoff Producing Storm
- E) Design Concept
(Select EURV when also designing for flood control)
- F) Design Volume (WQCV) Based on 40-hour Drain Time
($V_{DESIGN} = (1.0 * (0.91 * i^3 - 1.19 * i^2 + 0.78 * i) / 12 * Area)$)
- G) For Watersheds Outside of the Denver Region, Water Quality Capture Volume (WQCV) Design Volume
($V_{WQCV\ OTHER} = (d_6 * V_{DESIGN} * 0.43)$)
- H) User Input of Water Quality Capture Volume (WQCV) Design Volume
(Only if a different WQCV Design Volume is desired)
- I) NRCS Hydrologic Soil Groups of Tributary Watershed
 - i) Percentage of Watershed consisting of Type A Soils
 - ii) Percentage of Watershed consisting of Type B Soils
 - iii) Percentage of Watershed consisting of Type C/D Soils
- J) Excess Urban Runoff Volume (EURV) Design Volume
 For HSG A: $EURV_A = 1.68 * i^{1.28}$
 For HSG B: $EURV_B = 1.36 * i^{1.08}$
 For HSG C/D: $EURV_{C/D} = 1.20 * i^{1.08}$
- K) User Input of Excess Urban Runoff Volume (EURV) Design Volume
(Only if a different EURV Design Volume is desired)

$i_a =$ %
 $i =$
 Area = ac
 $d_6 =$ in

Choose One
 Water Quality Capture Volume (WQCV)
 Excess Urban Runoff Volume (EURV)

does not match MHFD-Detention calcs below

$V_{DESIGN} =$ ac-ft

$V_{DESIGN\ OTHER} =$ ac-ft

$V_{DESIGN\ USER} =$

$HSG_A =$ %
 $HSG_B =$ %
 $HSG_{C/D} =$ %

$EURV_{DESIGN} =$ ac-ft

$EURV_{DESIGN\ USER} =$

2. Basin Shape: Length to Width Ratio

(A basin length to width ratio of at least 2:1 will improve TSS reduction.)

$L : W =$: 1

3. Basin Side Slopes

- A) Basin Maximum Side Slopes
(Horizontal distance per unit vertical, 4:1 or flatter preferred)

$Z =$ ft / ft

4. Inlet

- A) Describe means of providing energy dissipation at concentrated inflow locations:

5. Forebay

- A) Minimum Forebay Volume
($V_{FMN} =$ of the WQCV)
- B) Actual Forebay Volume
- C) Forebay Depth
($D_F =$ inch maximum)
- D) Forebay Discharge
 - i) Undetained 100-year Peak Discharge
 - ii) Forebay Discharge Design Flow
($Q_F = 0.02 * Q_{100}$)
- E) Forebay Discharge Design
- F) Discharge Pipe Size (minimum 8-inches)
- G) Rectangular Notch Width

$V_{FMN} =$ ac-ft

$V_F =$ ac-ft

$D_F =$ in

$Q_{100} =$ cfs

$Q_F =$ cfs

Choose One
 Berm With Pipe
 Wall with Rect. Notch
 Wall with V-Notch Weir

Flow too small for berm w/ pipe

Calculated $D_P =$ in

Calculated $W_N =$ in

Design Procedure Form: Extended Detention Basin (EDB)

Designer: SPC
Company: HR Green
Date: March 12, 2024
Project: Eastonville Road - Segment 1 Improvements Pond B
Location: EL PASO COUNTY, CO

| | |
|---|---|
| <p>6. Trickle Channel</p> <p>A) Type of Trickle Channel</p> <p>F) Slope of Trickle Channel</p> | <div style="border: 1px solid black; padding: 2px; margin-bottom: 5px;"> Choose One <input checked="" type="radio"/> Concrete <input type="radio"/> Soft Bottom </div> <p>S = <input type="text" value="0.0050"/> ft / ft</p> |
| <p>7. Micropool and Outlet Structure</p> <p>A) Depth of Micropool (2.5-foot minimum)</p> <p>B) Surface Area of Micropool (10 ft² minimum)</p> <p>C) Outlet Type</p> <p>D) Smallest Dimension of Orifice Opening Based on Hydrograph Routing (Use UD-Detention)</p> <p>E) Total Outlet Area</p> | <p>D_M = <input type="text" value="2.5"/> ft</p> <p>A_M = <input type="text" value="10"/> sq ft</p> <div style="border: 1px solid black; padding: 2px; margin-bottom: 5px;"> Choose One <input checked="" type="radio"/> Orifice Plate <input type="radio"/> Other (Describe): </div> <hr/> <hr/> <p>D_{orifice} = <input type="text" value="0.63"/> inches</p> <p>A_{orifice} = <input type="text" value="30.18"/> square inches</p> |
| <p>8. Initial Surcharge Volume</p> <p>A) Depth of Initial Surcharge Volume (Minimum recommended depth is 4 inches)</p> <p>B) Minimum Initial Surcharge Volume (Minimum volume of 0.3% of the WQCV)</p> <p>C) Initial Surcharge Provided Above Micropool</p> | <p>D_{IS} = <input type="text" value="4"/> in</p> <p>V_{IS} = <input type="text"/> cu ft</p> <p>V_s = <input type="text" value="3.3"/> cu ft</p> |
| <p>9. Trash Rack</p> <p>A) Water Quality Screen Open Area: $A_t = A_{ot} * 38.5 * (e^{-0.095D})$</p> <p>B) Type of Screen (If specifying an alternative to the materials recommended in the USDCM, indicate "other" and enter the ratio of the total open are to the total screen are for the material specified.)</p> <p style="margin-left: 40px;">Other (Y/N): <input type="text" value="N"/></p> <p>C) Ratio of Total Open Area to Total Area (only for type 'Other')</p> <p>D) Total Water Quality Screen Area (based on screen type)</p> <p>E) Depth of Design Volume (EURV or WQCV) (Based on design concept chosen under 1E)</p> <p>F) Height of Water Quality Screen (H_{TR})</p> <p>G) Width of Water Quality Screen Opening (W_{opening}) (Minimum of 12 inches is recommended)</p> | <p>A_t = <input type="text" value="1,095"/> square inches</p> <div style="border: 1px solid black; padding: 2px; margin-bottom: 5px; width: fit-content;"> S.S. Well Screen with 60% Open Area </div> <hr/> <hr/> <p>User Ratio = <input type="text"/></p> <p>A_{total} = <input type="text" value="1825"/> sq. in.</p> <p>H = <input type="text" value="2.76"/> feet</p> <p>H_{TR} = <input type="text" value="61.12"/> inches</p> <p>W_{opening} = <input type="text" value="29.9"/> inches</p> |

Design Procedure Form: Extended Detention Basin (EDB)

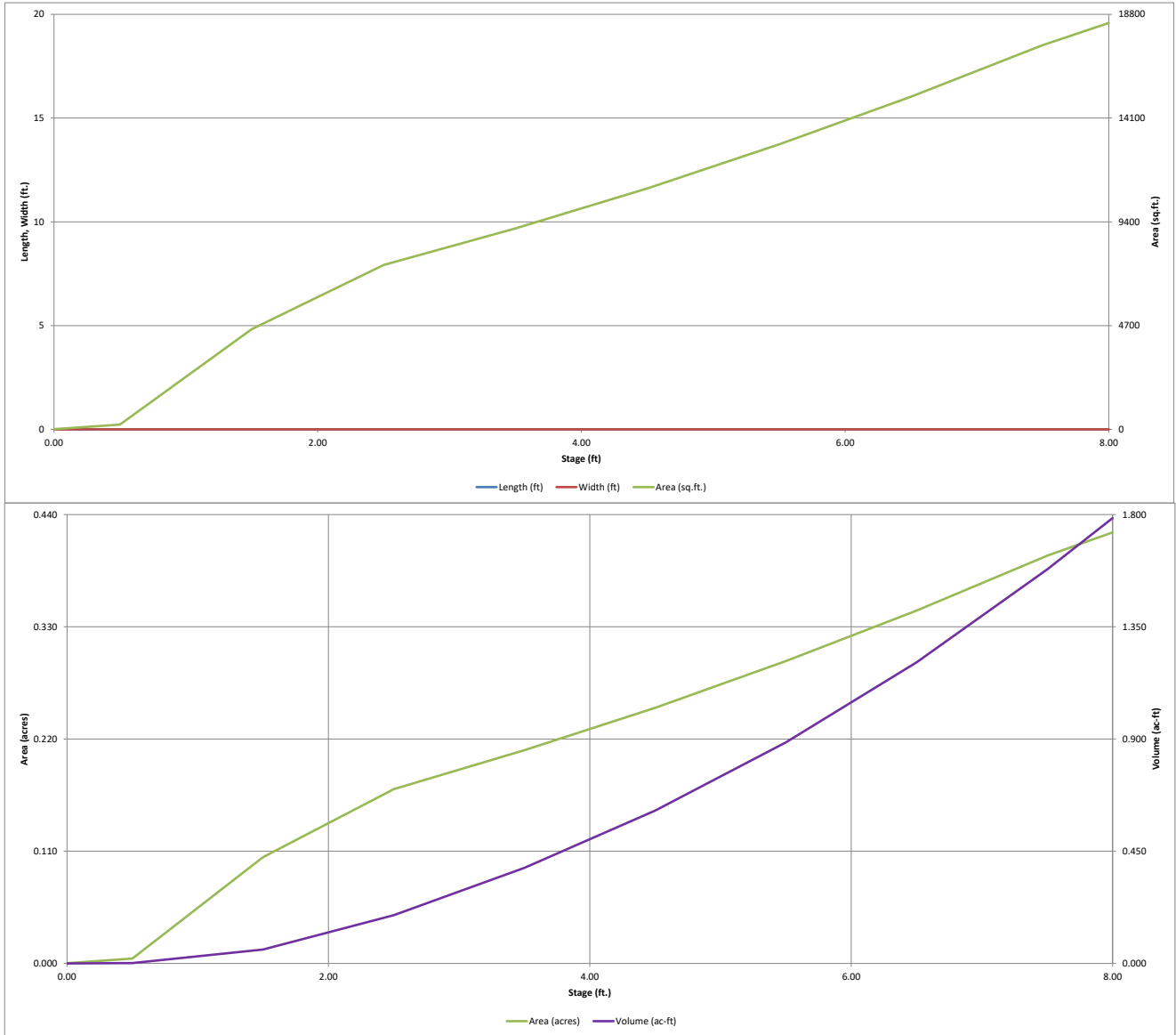
Sheet 3 of 3

Designer: SPC
Company: HR Green
Date: March 12, 2024
Project: Eastonville Road - Segment 1 Improvements Pond B
Location: EL PASO COUNTY, CO

| | |
|---|--|
| <p>10. Overflow Embankment</p> <p>A) Describe embankment protection for 100-year and greater overtopping:</p> <p>B) Slope of Overflow Embankment (Horizontal distance per unit vertical, 4:1 or flatter preferred)</p> | <p>_____</p> <p>_____</p> <p>_____</p> <p>Ze = <input type="text" value="4.00"/> ft / ft</p> |
| <p>11. Vegetation</p> | <p>Choose One</p> <p><input type="radio"/> Irrigated</p> <p><input checked="" type="radio"/> Not Irrigated</p> |
| <p>12. Access</p> <p>A) Describe Sediment Removal Procedures</p> | <p>_____</p> <p>_____</p> <p>_____</p> <p>_____</p> <p>_____</p> |
| <p>Notes: _____</p> <p>_____</p> <p>_____</p> <p>_____</p> | |

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.05 (January 2022)

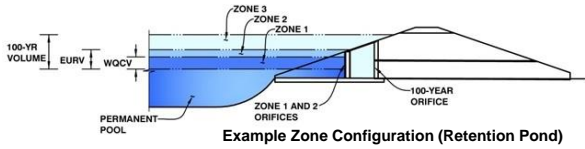


DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD- Detention, Version 4.05 (January 2022)

Project: Eastonville Road - Segment 1 Improvements

Basin ID: EDB B INTERIM CONDITIONS: BASINS [EA6 - EA8]



| | Estimated Stage (ft) | Estimated Volume (ac-ft) | Outlet Type |
|--------------------------|----------------------|--------------------------|----------------------|
| Zone 1 (WQCV) | 1.64 | 0.070 | Orifice Plate |
| Zone 2 (EURV) | 2.81 | 0.177 | Rectangular Orifice |
| Zone 3 (100-year) | 3.51 | 0.138 | Weir&Pipe (Restrict) |
| Total (all zones) | | 0.385 | |

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth = ft (distance below the filtration media surface)
 Underdrain Orifice Diameter = inches

Calculated Parameters for Underdrain
 Underdrain Orifice Area = ft²
 Underdrain Orifice Centroid = feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Centroid of Lowest Orifice = ft (relative to basin bottom at Stage = 0 ft)
 Depth at top of Zone using Orifice Plate = ft (relative to basin bottom at Stage = 0 ft)
 Orifice Plate: Orifice Vertical Spacing = inches
 Orifice Plate: Orifice Area per Row = sq. inches (diameter = 5/8 inch)

Calculated Parameters for Plate
 WQ Orifice Area per Row = ft²
 Elliptical Half-Width = feet
 Elliptical Slot Centroid = feet
 Elliptical Slot Area = ft²

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

| | Row 1 (required) | Row 2 (optional) | Row 3 (optional) | Row 4 (optional) | Row 5 (optional) | Row 6 (optional) | Row 7 (optional) | Row 8 (optional) |
|--------------------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|
| Stage of Orifice Centroid (ft) | 0.00 | 0.60 | 1.20 | | | | | |
| Orifice Area (sq. inches) | 0.31 | 0.31 | 0.31 | | | | | |

| | Row 9 (optional) | Row 10 (optional) | Row 11 (optional) | Row 12 (optional) | Row 13 (optional) | Row 14 (optional) | Row 15 (optional) | Row 16 (optional) |
|--------------------------------|------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| Stage of Orifice Centroid (ft) | | | | | | | | |
| Orifice Area (sq. inches) | | | | | | | | |

User Input: Vertical Orifice (Circular or Rectangular)

Invert of Vertical Orifice = Zone 2 Rectangular Not Selected = ft (relative to basin bottom at Stage = 0 ft)
 Depth at top of Zone using Vertical Orifice = Zone 2 Rectangular Not Selected = ft (relative to basin bottom at Stage = 0 ft)
 Vertical Orifice Height = Zone 2 Rectangular Not Selected = inches
 Vertical Orifice Width = Zone 2 Rectangular Not Selected = inches

Calculated Parameters for Vertical Orifice
 Vertical Orifice Area = ft²
 Vertical Orifice Centroid = feet

User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir and No Outlet Pipe)

Overflow Weir Front Edge Height, Ho = Zone 3 Weir Not Selected = ft (relative to basin bottom at Stage = 0 ft)
 Overflow Weir Front Edge Length = Zone 3 Weir Not Selected = feet
 Overflow Weir Grate Slope = Zone 3 Weir Not Selected = H:V
 Horiz. Length of Weir Sides = Zone 3 Weir Not Selected = feet
 Overflow Grate Type = Zone 3 Weir Not Selected =
 Debris Clogging % = Zone 3 Weir Not Selected = %

Calculated Parameters for Overflow Weir
 Height of Grate Upper Edge, H_t = feet
 Overflow Weir Slope Length = feet
 Grate Open Area / 100-yr Orifice Area =
 Overflow Grate Open Area w/o Debris = ft²
 Overflow Grate Open Area w/ Debris = ft²

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

Depth to Invert of Outlet Pipe = Zone 3 Restrictor Not Selected = ft (distance below basin bottom at Stage = 0 ft)
 Outlet Pipe Diameter = Zone 3 Restrictor Not Selected = inches
 Restrictor Plate Height Above Pipe Invert = Zone 3 Restrictor Not Selected = inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate
 Outlet Orifice Area = ft²
 Outlet Orifice Centroid = feet
 Half-Central Angle of Restrictor Plate on Pipe = radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage = Zone 3 Weir Not Selected = ft (relative to basin bottom at Stage = 0 ft)
 Spillway Crest Length = Zone 3 Weir Not Selected = feet
 Spillway End Slopes = Zone 3 Weir Not Selected = H:V
 Freeboard above Max Water Surface = Zone 3 Weir Not Selected = feet

Calculated Parameters for Spillway
 Spillway Design Flow Depth = feet
 Stage at Top of Freeboard = feet
 Basin Area at Top of Freeboard = acres
 Basin Volume at Top of Freeboard = acre-ft

Routed Hydrograph Results

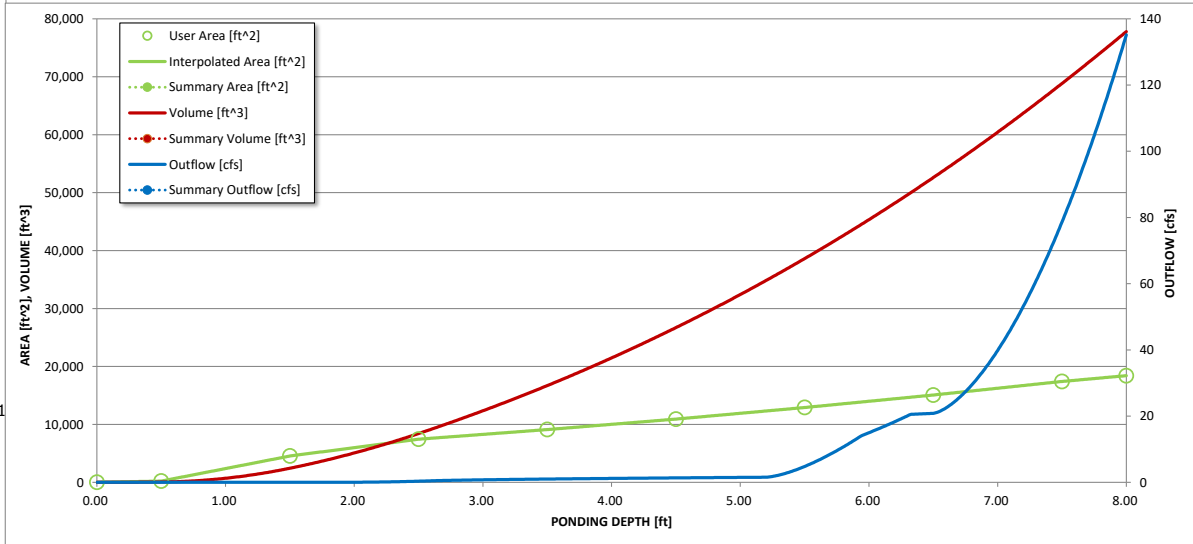
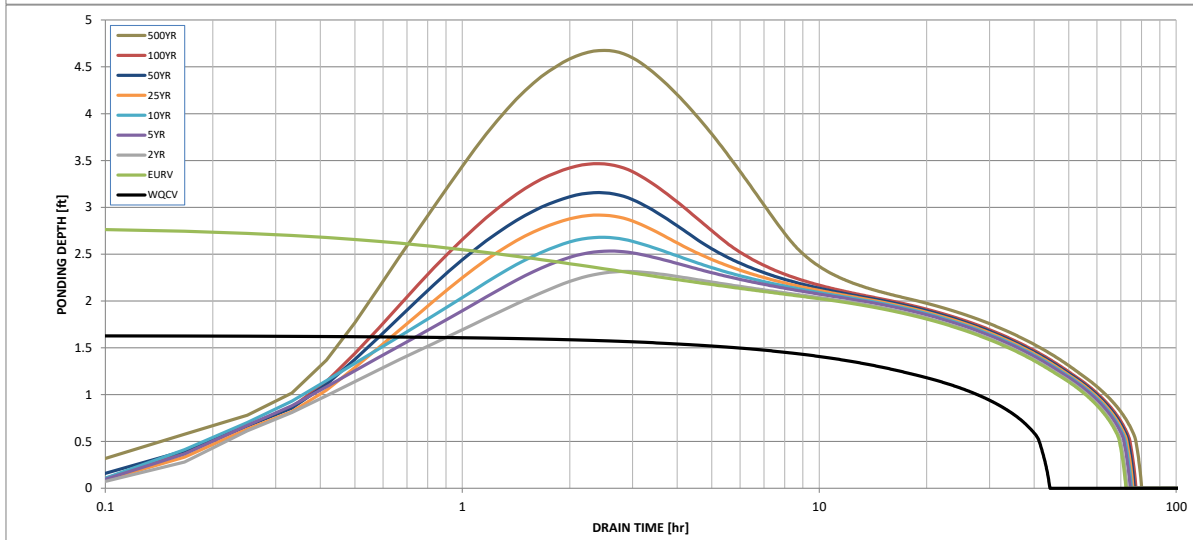
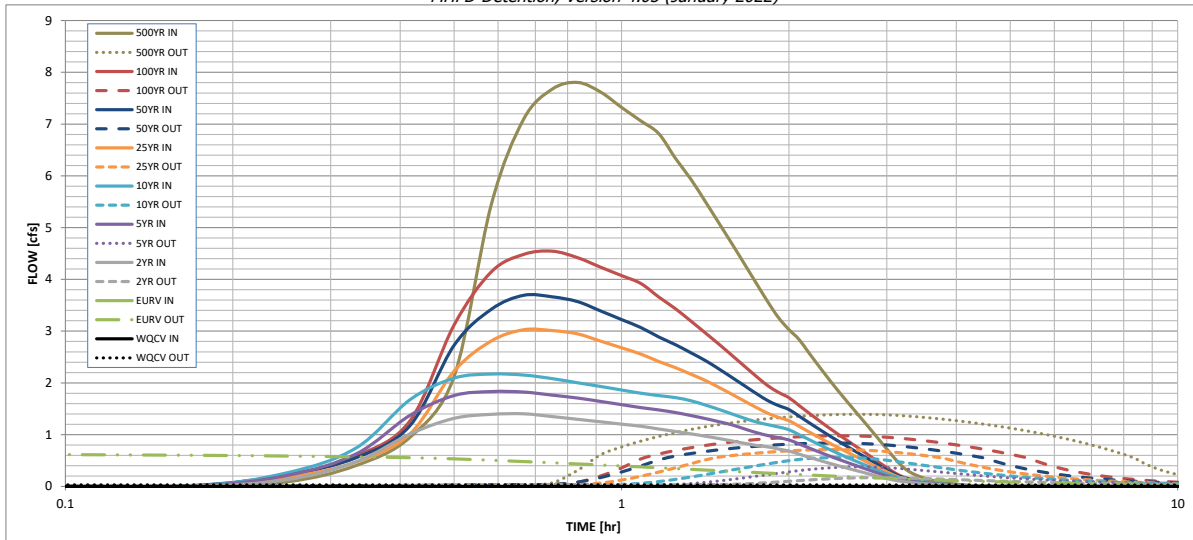
The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).

| | WQCV | EURV | 2 Year | 5 Year | 10 Year | 25 Year | 50 Year | 100 Year | 500 Year |
|---|-------|--------------------|--------------------|--------------------|--------------------|--------------------|--------------------|--------------------|--------------------|
| Design Storm Return Period | N/A | N/A | 1.19 | 1.50 | 1.75 | 2.00 | 2.25 | 2.52 | 3.68 |
| One-Hour Rainfall Depth (in) | N/A | N/A | 1.19 | 1.50 | 1.75 | 2.00 | 2.25 | 2.52 | 3.68 |
| CUHP Runoff Volume (acre-ft) | 0.070 | 0.247 | 0.185 | 0.245 | 0.293 | 0.364 | 0.434 | 0.522 | 0.888 |
| Inflow Hydrograph Volume (acre-ft) | N/A | N/A | 0.185 | 0.245 | 0.293 | 0.364 | 0.434 | 0.522 | 0.888 |
| CUHP Predevelopment Peak Q (cfs) | N/A | N/A | 0.0 | 0.0 | 0.0 | 0.3 | 0.6 | 1.0 | 2.7 |
| OPTIONAL Override Predevelopment Peak Q (cfs) | N/A | N/A | | | | | | | |
| Predevelopment Unit Peak Flow, q (cfs/acre) | N/A | N/A | 0.00 | 0.01 | 0.01 | 0.08 | 0.15 | 0.25 | 0.69 |
| Peak Inflow Q (cfs) | N/A | N/A | 1.4 | 1.8 | 2.2 | 3.0 | 3.7 | 4.5 | 7.8 |
| Peak Outflow Q (cfs) | 0.0 | 0.6 | 0.2 | 0.4 | 0.6 | 0.7 | 0.8 | 1.0 | 1.4 |
| Ratio Peak Outflow to Predevelopment Q | N/A | N/A | N/A | 16.8 | 17.6 | 2.4 | 1.4 | 1.0 | 0.5 |
| Structure Controlling Flow | Plate | Vertical Orifice 1 | Vertical Orifice 1 | Vertical Orifice 1 | Vertical Orifice 1 | Vertical Orifice 1 | Vertical Orifice 1 | Vertical Orifice 1 | Vertical Orifice 1 |
| Max Velocity through Gate 1 (fps) | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A |
| Max Velocity through Gate 2 (fps) | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A |
| Time to Drain 97% of Inflow Volume (hours) | 40 | 63 | 65 | 65 | 64 | 63 | 62 | 61 | 56 |
| Time to Drain 99% of Inflow Volume (hours) | 42 | 68 | 69 | 70 | 70 | 70 | 70 | 69 | 69 |
| Maximum Ponding Depth (ft) | 1.64 | 2.81 | 2.32 | 2.53 | 2.68 | 2.92 | 3.16 | 3.47 | 4.68 |
| Area at Maximum Ponding Depth (acres) | 0.11 | 0.18 | 0.16 | 0.17 | 0.18 | 0.19 | 0.20 | 0.21 | 0.26 |
| Maximum Volume Stored (acre-ft) | 0.071 | 0.248 | 0.162 | 0.198 | 0.225 | 0.267 | 0.312 | 0.375 | 0.656 |

Why aren't these values that are >1 highlighted in red like they were with the last submittal?
 Regardless, the ratio should be less than or equal to 1 for minor (5-yr) and major (100-yr) design storms. See Chapter 4.1 of DCM volume 2 (and also Chap 2 of MHFD DCM vol. 3).

DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.05 (January 2022)



| S-A-V-D Chart Axis Override | X-axis | Left Y-Axis | Right Y-Axis |
|-----------------------------|--------|-------------|--------------|
| minimum bound | | | |
| maximum bound | | | |

DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename: _____

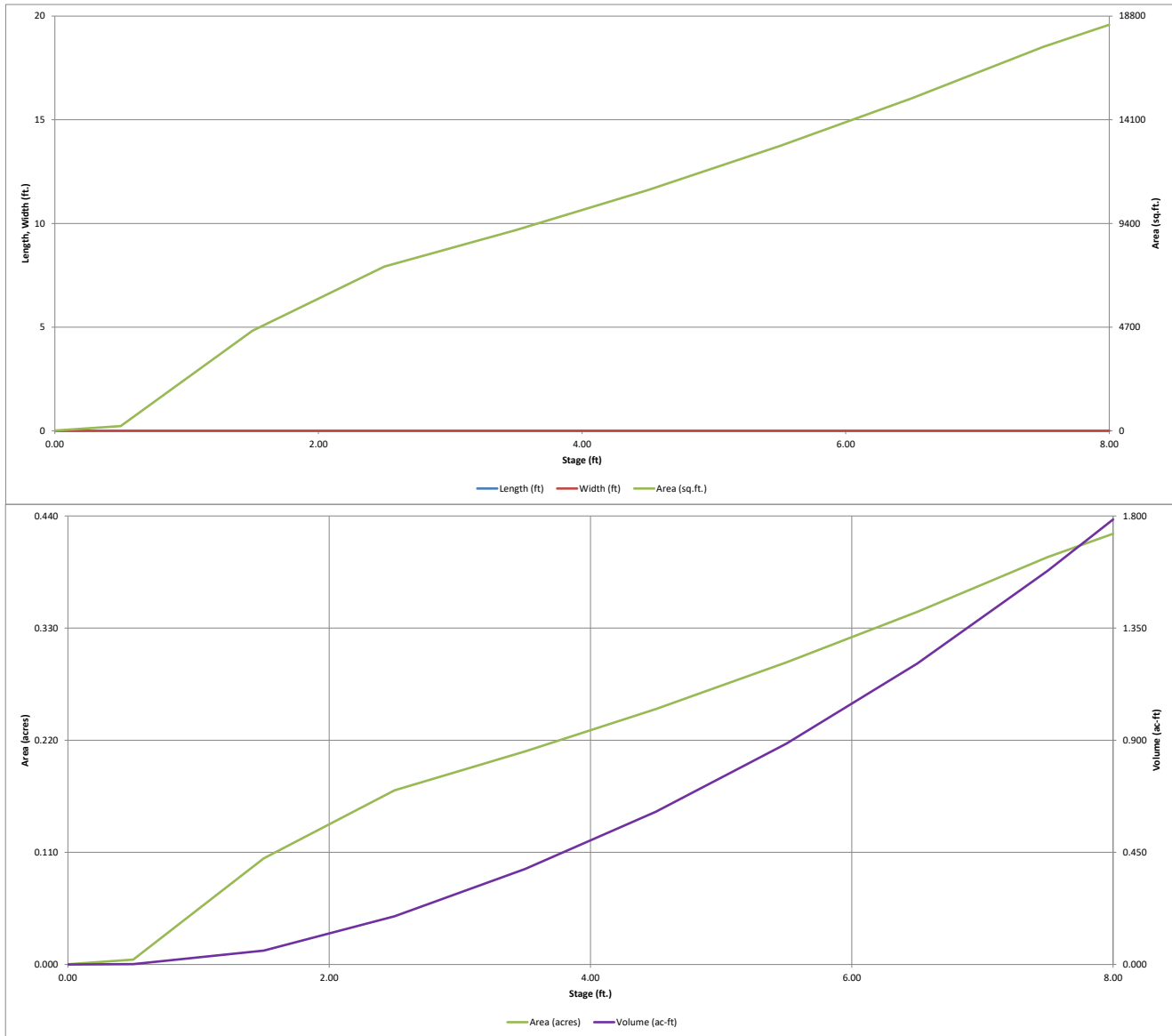
Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

| Time Interval | SOURCE | CUHP | CUHP | CUHP | CUHP | CUHP | CUHP | CUHP | CUHP | CUHP |
|---------------|---------|------------|------------|--------------|--------------|---------------|---------------|---------------|----------------|----------------|
| | TIME | WQCV [cfs] | EURV [cfs] | 2 Year [cfs] | 5 Year [cfs] | 10 Year [cfs] | 25 Year [cfs] | 50 Year [cfs] | 100 Year [cfs] | 500 Year [cfs] |
| 5.00 min | 0:00:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 0:05:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 0:10:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.01 | 0.00 | 0.09 |
| | 0:15:00 | 0.00 | 0.00 | 0.13 | 0.21 | 0.26 | 0.18 | 0.22 | 0.22 | 0.40 |
| | 0:20:00 | 0.00 | 0.00 | 0.48 | 0.63 | 0.74 | 0.47 | 0.55 | 0.59 | 0.95 |
| | 0:25:00 | 0.00 | 0.00 | 1.01 | 1.37 | 1.68 | 1.02 | 1.18 | 1.27 | 2.12 |
| | 0:30:00 | 0.00 | 0.00 | 1.32 | 1.76 | 2.09 | 2.23 | 2.73 | 3.12 | 5.45 |
| | 0:35:00 | 0.00 | 0.00 | 1.39 | 1.83 | 2.17 | 2.81 | 3.42 | 4.15 | 7.09 |
| | 0:40:00 | 0.00 | 0.00 | 1.40 | 1.82 | 2.15 | 3.03 | 3.69 | 4.48 | 7.67 |
| | 0:45:00 | 0.00 | 0.00 | 1.35 | 1.76 | 2.08 | 3.01 | 3.66 | 4.55 | 7.80 |
| | 0:50:00 | 0.00 | 0.00 | 1.30 | 1.71 | 2.00 | 2.95 | 3.57 | 4.42 | 7.62 |
| | 0:55:00 | 0.00 | 0.00 | 1.25 | 1.64 | 1.93 | 2.81 | 3.39 | 4.24 | 7.32 |
| | 1:00:00 | 0.00 | 0.00 | 1.20 | 1.58 | 1.86 | 2.68 | 3.22 | 4.07 | 7.06 |
| | 1:05:00 | 0.00 | 0.00 | 1.16 | 1.52 | 1.80 | 2.56 | 3.07 | 3.92 | 6.82 |
| | 1:10:00 | 0.00 | 0.00 | 1.11 | 1.48 | 1.75 | 2.41 | 2.89 | 3.66 | 6.34 |
| | 1:15:00 | 0.00 | 0.00 | 1.06 | 1.43 | 1.72 | 2.29 | 2.74 | 3.43 | 5.93 |
| | 1:20:00 | 0.00 | 0.00 | 1.02 | 1.37 | 1.65 | 2.17 | 2.58 | 3.19 | 5.49 |
| | 1:25:00 | 0.00 | 0.00 | 0.97 | 1.31 | 1.57 | 2.04 | 2.43 | 2.96 | 5.07 |
| | 1:30:00 | 0.00 | 0.00 | 0.92 | 1.25 | 1.48 | 1.91 | 2.26 | 2.74 | 4.67 |
| | 1:35:00 | 0.00 | 0.00 | 0.88 | 1.19 | 1.40 | 1.77 | 2.10 | 2.52 | 4.28 |
| | 1:40:00 | 0.00 | 0.00 | 0.83 | 1.11 | 1.31 | 1.64 | 1.94 | 2.32 | 3.91 |
| | 1:45:00 | 0.00 | 0.00 | 0.79 | 1.04 | 1.24 | 1.52 | 1.79 | 2.12 | 3.56 |
| | 1:50:00 | 0.00 | 0.00 | 0.76 | 0.98 | 1.19 | 1.41 | 1.66 | 1.94 | 3.26 |
| | 1:55:00 | 0.00 | 0.00 | 0.72 | 0.94 | 1.15 | 1.33 | 1.56 | 1.82 | 3.03 |
| | 2:00:00 | 0.00 | 0.00 | 0.68 | 0.90 | 1.09 | 1.27 | 1.49 | 1.71 | 2.85 |
| | 2:05:00 | 0.00 | 0.00 | 0.62 | 0.82 | 1.00 | 1.16 | 1.36 | 1.57 | 2.60 |
| | 2:10:00 | 0.00 | 0.00 | 0.57 | 0.75 | 0.91 | 1.06 | 1.24 | 1.43 | 2.36 |
| | 2:15:00 | 0.00 | 0.00 | 0.52 | 0.68 | 0.83 | 0.96 | 1.13 | 1.30 | 2.14 |
| | 2:20:00 | 0.00 | 0.00 | 0.47 | 0.61 | 0.74 | 0.87 | 1.02 | 1.17 | 1.93 |
| | 2:25:00 | 0.00 | 0.00 | 0.42 | 0.55 | 0.67 | 0.79 | 0.92 | 1.05 | 1.74 |
| | 2:30:00 | 0.00 | 0.00 | 0.38 | 0.49 | 0.60 | 0.70 | 0.82 | 0.95 | 1.56 |
| | 2:35:00 | 0.00 | 0.00 | 0.33 | 0.44 | 0.53 | 0.63 | 0.73 | 0.84 | 1.38 |
| | 2:40:00 | 0.00 | 0.00 | 0.30 | 0.39 | 0.47 | 0.55 | 0.64 | 0.74 | 1.21 |
| | 2:45:00 | 0.00 | 0.00 | 0.26 | 0.34 | 0.41 | 0.48 | 0.56 | 0.64 | 1.04 |
| | 2:50:00 | 0.00 | 0.00 | 0.22 | 0.29 | 0.35 | 0.41 | 0.48 | 0.55 | 0.88 |
| | 2:55:00 | 0.00 | 0.00 | 0.19 | 0.24 | 0.29 | 0.35 | 0.40 | 0.45 | 0.72 |
| | 3:00:00 | 0.00 | 0.00 | 0.15 | 0.20 | 0.24 | 0.28 | 0.32 | 0.36 | 0.57 |
| | 3:05:00 | 0.00 | 0.00 | 0.12 | 0.16 | 0.20 | 0.22 | 0.25 | 0.28 | 0.43 |
| | 3:10:00 | 0.00 | 0.00 | 0.10 | 0.14 | 0.16 | 0.17 | 0.19 | 0.21 | 0.32 |
| | 3:15:00 | 0.00 | 0.00 | 0.09 | 0.11 | 0.14 | 0.14 | 0.16 | 0.16 | 0.25 |
| | 3:20:00 | 0.00 | 0.00 | 0.07 | 0.10 | 0.12 | 0.11 | 0.13 | 0.13 | 0.20 |
| | 3:25:00 | 0.00 | 0.00 | 0.06 | 0.08 | 0.10 | 0.10 | 0.11 | 0.11 | 0.16 |
| | 3:30:00 | 0.00 | 0.00 | 0.05 | 0.07 | 0.09 | 0.08 | 0.09 | 0.09 | 0.13 |
| | 3:35:00 | 0.00 | 0.00 | 0.05 | 0.06 | 0.08 | 0.07 | 0.08 | 0.07 | 0.10 |
| | 3:40:00 | 0.00 | 0.00 | 0.04 | 0.05 | 0.06 | 0.06 | 0.06 | 0.06 | 0.08 |
| | 3:45:00 | 0.00 | 0.00 | 0.03 | 0.04 | 0.05 | 0.05 | 0.05 | 0.05 | 0.07 |
| | 3:50:00 | 0.00 | 0.00 | 0.03 | 0.03 | 0.04 | 0.04 | 0.04 | 0.04 | 0.05 |
| | 3:55:00 | 0.00 | 0.00 | 0.02 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 | 0.04 |
| | 4:00:00 | 0.00 | 0.00 | 0.02 | 0.02 | 0.03 | 0.02 | 0.03 | 0.02 | 0.03 |
| | 4:05:00 | 0.00 | 0.00 | 0.01 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 | 0.03 |
| | 4:10:00 | 0.00 | 0.00 | 0.01 | 0.01 | 0.02 | 0.01 | 0.02 | 0.01 | 0.02 |
| | 4:15:00 | 0.00 | 0.00 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| | 4:20:00 | 0.00 | 0.00 | 0.00 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| | 4:25:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 4:30:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 4:35:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 4:40:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 4:45:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 4:50:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 4:55:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 5:00:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| 5:05:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| 5:10:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| 5:15:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| 5:20:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| 5:25:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| 5:30:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| 5:35:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| 5:40:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| 5:45:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| 5:50:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| 5:55:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| 6:00:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

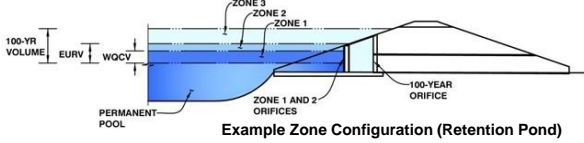
MHFD-Detention, Version 4.05 (January 2022)



DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.05 (January 2022)

Project: Eastonville Road
Basin ID: EDB B: Ultimate Conditions [BASIN EA6 - EA10]



Example Zone Configuration (Retention Pond)

| | Estimated Stage (ft) | Estimated Volume (ac-ft) | Outlet Type |
|--------------------------|----------------------|--------------------------|----------------------|
| Zone 1 (WQCV) | 2.58 | 0.207 | Orifice Plate |
| Zone 2 (EURV) | 5.19 | 0.590 | Circular Orifice |
| Zone 3 (100-year) | 6.41 | 0.378 | Weir&Pipe (Restrict) |
| Total (all zones) | | 1.175 | |

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

| | | |
|-----------------------------------|-----|--|
| Underdrain Orifice Invert Depth = | N/A | ft (distance below the filtration media surface) |
| Underdrain Orifice Diameter = | N/A | inches |

Calculated Parameters for Underdrain

| | | |
|-------------------------------|-----|-----------------|
| Underdrain Orifice Area = | N/A | ft ² |
| Underdrain Orifice Centroid = | N/A | feet |

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

| | | |
|--|------|---|
| Centroid of Lowest Orifice = | 0.00 | ft (relative to basin bottom at Stage = 0 ft) |
| Depth at top of Zone using Orifice Plate = | 2.58 | ft (relative to basin bottom at Stage = 0 ft) |
| Orifice Plate: Orifice Vertical Spacing = | N/A | inches |
| Orifice Plate: Orifice Area per Row = | 0.79 | sq. inches (diameter = 1 inch) |

Calculated Parameters for Plate

| | | |
|----------------------------|-----------|-----------------|
| WQ Orifice Area per Row = | 5.451E-03 | ft ² |
| Elliptical Half-Width = | N/A | feet |
| Elliptical Slot Centroid = | N/A | feet |
| Elliptical Slot Area = | N/A | ft ² |

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

| | Row 1 (required) | Row 2 (optional) | Row 3 (optional) | Row 4 (optional) | Row 5 (optional) | Row 6 (optional) | Row 7 (optional) | Row 8 (optional) |
|--------------------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|
| Stage of Orifice Centroid (ft) | 0.00 | 0.87 | 1.73 | | | | | |
| Orifice Area (sq. inches) | 0.79 | 0.79 | 0.79 | | | | | |

| | Row 9 (optional) | Row 10 (optional) | Row 11 (optional) | Row 12 (optional) | Row 13 (optional) | Row 14 (optional) | Row 15 (optional) | Row 16 (optional) |
|--------------------------------|------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| Stage of Orifice Centroid (ft) | | | | | | | | |
| Orifice Area (sq. inches) | | | | | | | | |

User Input: Vertical Orifice (Circular or Rectangular)

| | Zone 2 Circular | Not Selected | |
|---|-----------------|--------------|---|
| Invert of Vertical Orifice = | 2.60 | N/A | ft (relative to basin bottom at Stage = 0 ft) |
| Depth at top of Zone using Vertical Orifice = | 5.18 | N/A | ft (relative to basin bottom at Stage = 0 ft) |
| Vertical Orifice Diameter = | 2.00 | N/A | inches |

Calculated Parameters for Vertical Orifice

| | Zone 2 Circular | Not Selected | |
|-----------------------------|-----------------|--------------|-----------------|
| Vertical Orifice Area = | 0.02 | N/A | ft ² |
| Vertical Orifice Centroid = | 0.08 | N/A | feet |

User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir and No Outlet Pipe)

| | Zone 3 Weir | Not Selected | |
|---|--------------|--------------|---|
| Overflow Weir Front Edge Height, H _o = | 5.20 | N/A | ft (relative to basin bottom at Stage = 0 ft) |
| Overflow Weir Front Edge Length = | 3.00 | N/A | feet |
| Overflow Weir Grate Slope = | 0.00 | N/A | H:V |
| Horiz. Length of Weir Sides = | 3.00 | N/A | feet |
| Overflow Grate Type = | Type C Grate | N/A | |
| Debris Clogging % = | 50% | N/A | % |

Calculated Parameters for Overflow Weir

| | Zone 3 Weir | Not Selected | |
|--|-------------|--------------|-----------------|
| Height of Grate Upper Edge, H _t = | 5.20 | N/A | feet |
| Overflow Weir Slope Length = | 3.00 | N/A | feet |
| Grate Open Area / 100-yr Orifice Area = | 25.92 | N/A | |
| Overflow Grate Open Area w/o Debris = | 6.26 | N/A | ft ² |
| Overflow Grate Open Area w/ Debris = | 3.13 | N/A | ft ² |

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

| | Zone 3 Restrictor | Not Selected | |
|---|-------------------|--------------|--|
| Depth to Invert of Outlet Pipe = | 0.25 | N/A | ft (distance below basin bottom at Stage = 0 ft) |
| Outlet Pipe Diameter = | 18.00 | N/A | inches |
| Restrictor Plate Height Above Pipe Invert = | 3.50 | | inches |

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate

| | Zone 3 Restrictor | Not Selected | |
|--|-------------------|--------------|-----------------|
| Outlet Orifice Area = | 0.24 | N/A | ft ² |
| Outlet Orifice Centroid = | 0.17 | N/A | feet |
| Half-Central Angle of Restrictor Plate on Pipe = | 0.91 | N/A | radians |

User Input: Emergency Spillway (Rectangular or Trapezoidal)

| | | |
|-------------------------------------|-------|---|
| Spillway Invert Stage = | 6.50 | ft (relative to basin bottom at Stage = 0 ft) |
| Spillway Crest Length = | 15.50 | feet |
| Spillway End Slopes = | 4.00 | H:V |
| Freeboard above Max Water Surface = | 1.00 | feet |

Calculated Parameters for Spillway

| | | |
|------------------------------------|------|---------|
| Spillway Design Flow Depth = | 0.50 | feet |
| Stage at Top of Freeboard = | 8.00 | feet |
| Basin Area at Top of Freeboard = | 0.42 | acres |
| Basin Volume at Top of Freeboard = | 1.79 | acre-ft |

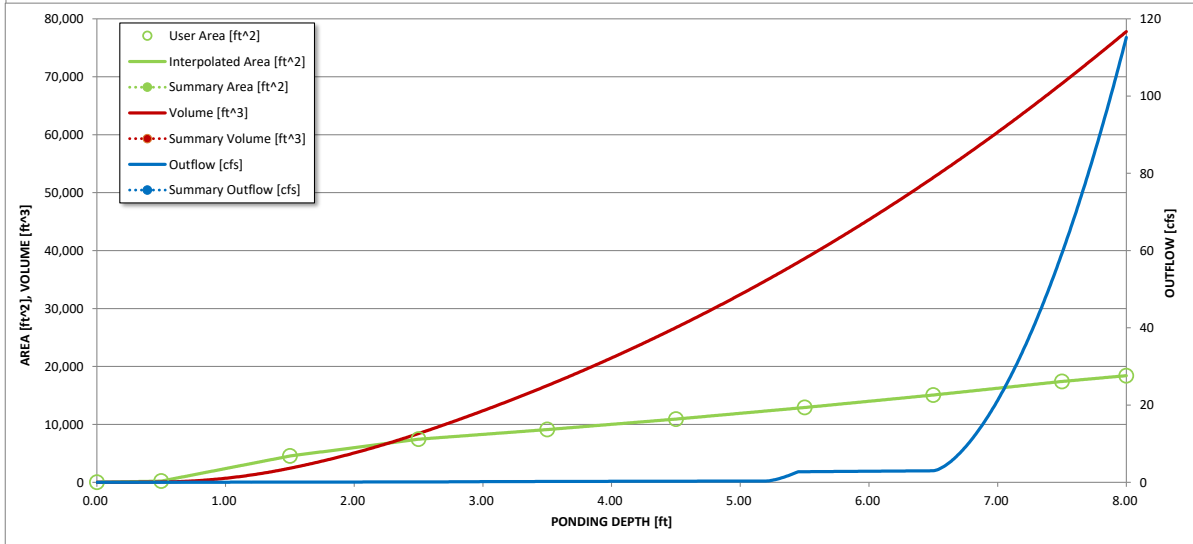
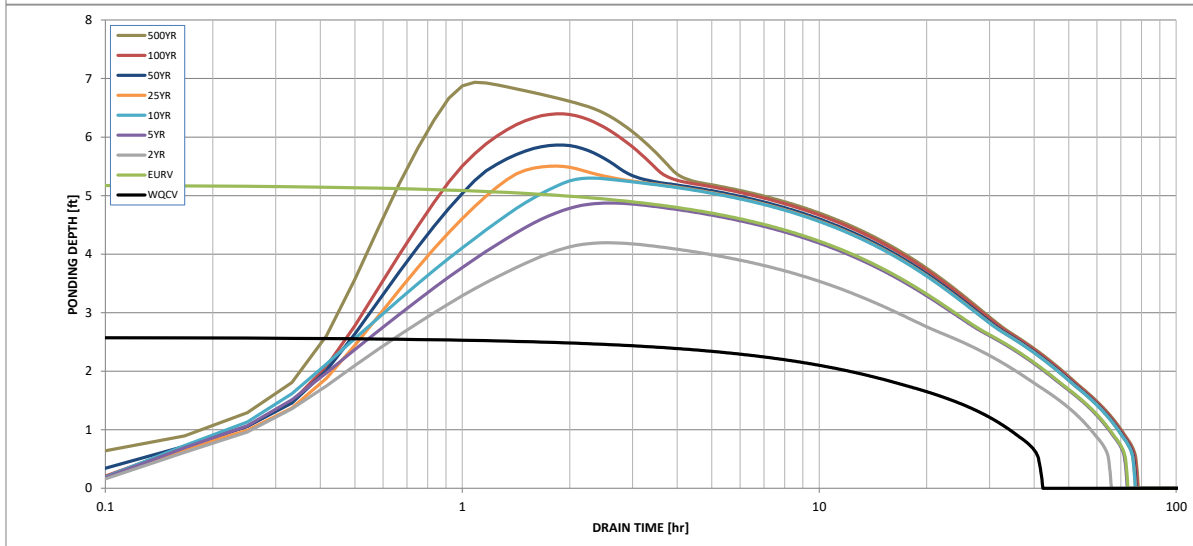
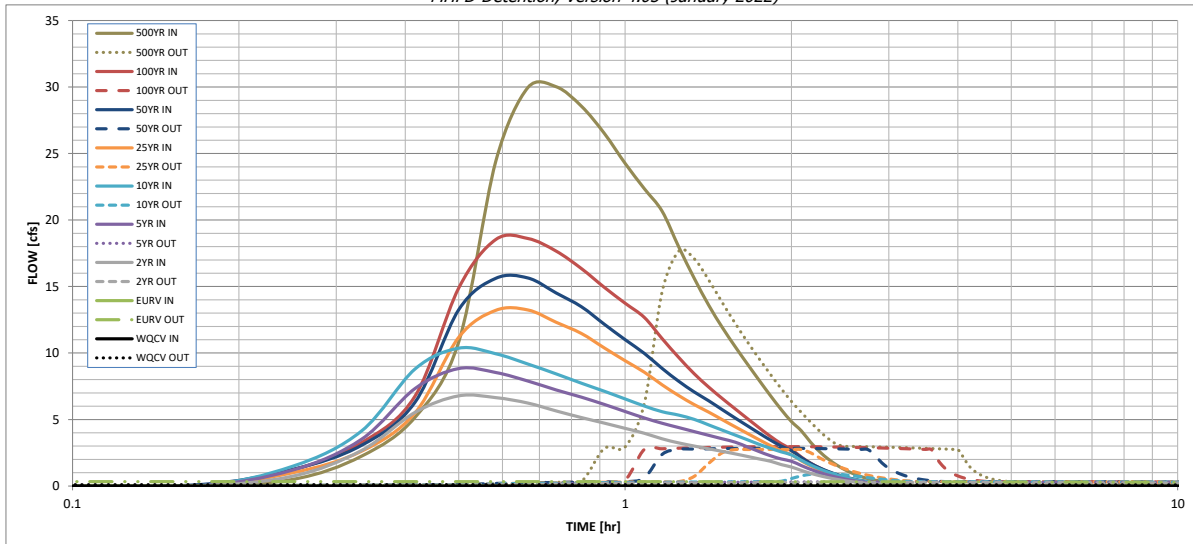
Routed Hydrograph Results

The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).

| | WQCV | EURV | 2 Year | 5 Year | 10 Year | 25 Year | 50 Year | 100 Year | 500 Year |
|---|-------|--------------------|--------------------|--------------------|-----------------|----------------|----------------|----------------|----------|
| Design Storm Return Period | N/A | N/A | 1.19 | 1.50 | 1.75 | 2.00 | 2.25 | 2.52 | 3.68 |
| One-Hour Rainfall Depth (in) | N/A | N/A | 0.584 | 0.764 | 0.909 | 1.093 | 1.274 | 1.491 | 2.398 |
| CUHP Runoff Volume (acre-ft) | 0.207 | 0.796 | 0.584 | 0.764 | 0.909 | 1.093 | 1.274 | 1.491 | 2.398 |
| Inflow Hydrograph Volume (acre-ft) | N/A | N/A | 0.584 | 0.764 | 0.909 | 1.093 | 1.274 | 1.491 | 2.398 |
| CUHP Predevelopment Peak Q (cfs) | N/A | N/A | 0.0 | 0.1 | 0.1 | 1.0 | 2.1 | 3.4 | 9.2 |
| OPTIONAL Override Predevelopment Peak Q (cfs) | N/A | N/A | | | | | | | |
| Predevelopment Unit Peak Flow, q (cfs/acre) | N/A | N/A | 0.00 | 0.01 | 0.01 | 0.11 | 0.22 | 0.37 | 0.99 |
| Peak Inflow Q (cfs) | N/A | N/A | 6.8 | 8.8 | 10.4 | 13.2 | 15.6 | 18.6 | 30.0 |
| Peak Outflow Q (cfs) | 0.1 | 0.3 | 0.3 | 0.3 | 0.9 | 2.7 | 2.8 | 3.0 | 17.7 |
| Ratio Peak Outflow to Predevelopment Q | N/A | N/A | N/A | 3.9 | 8.3 | 2.7 | 1.4 | 0.9 | 1.9 |
| Structure Controlling Flow | Plate | Vertical Orifice 1 | Vertical Orifice 1 | Vertical Orifice 1 | Overflow Weir 1 | Outlet Plate 1 | Outlet Plate 1 | Outlet Plate 1 | Spillway |
| Max Velocity through Grate 1 (fps) | N/A | N/A | N/A | N/A | 0.1 | 0.4 | 0.4 | 0.4 | 0.4 |
| Max Velocity through Grate 2 (fps) | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A |
| Time to Drain 97% of Inflow Volume (hours) | 38 | 63 | 57 | 63 | 65 | 64 | 63 | 62 | 56 |
| Time to Drain 99% of Inflow Volume (hours) | 41 | 69 | 62 | 68 | 71 | 71 | 70 | 70 | 68 |
| Maximum Ponding Depth (ft) | 2.58 | 5.19 | 4.19 | 4.87 | 5.30 | 5.51 | 5.86 | 6.40 | 6.94 |
| Area at Maximum Ponding Depth (acres) | 0.17 | 0.28 | 0.24 | 0.27 | 0.29 | 0.30 | 0.31 | 0.34 | 0.37 |
| Maximum Volume Stored (acre-ft) | 0.207 | 0.797 | 0.537 | 0.709 | 0.825 | 0.886 | 0.996 | 1.170 | 1.361 |

DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.05 (January 2022)



| S-A-V-D Chart Axis Override | X-axis | Left Y-Axis | Right Y-Axis |
|-----------------------------|--------|-------------|--------------|
| minimum bound | | | |
| maximum bound | | | |

DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename: _____

Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

| Time Interval | SOURCE | CUHP | CUHP | CUHP | CUHP | CUHP | CUHP | CUHP | CUHP | CUHP |
|---------------|---------|------------|------------|--------------|--------------|---------------|---------------|---------------|----------------|----------------|
| | TIME | WQCV [cfs] | EURV [cfs] | 2 Year [cfs] | 5 Year [cfs] | 10 Year [cfs] | 25 Year [cfs] | 50 Year [cfs] | 100 Year [cfs] | 500 Year [cfs] |
| 5.00 min | 0:00:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 0:05:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 0:10:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.08 | 0.01 | 0.49 |
| | 0:15:00 | 0.00 | 0.00 | 0.73 | 1.19 | 1.48 | 0.99 | 1.25 | 1.21 | 2.24 |
| | 0:20:00 | 0.00 | 0.00 | 2.67 | 3.51 | 4.13 | 2.61 | 3.06 | 3.26 | 5.16 |
| | 0:25:00 | 0.00 | 0.00 | 5.54 | 7.33 | 8.80 | 5.49 | 6.30 | 6.76 | 10.85 |
| | 0:30:00 | 0.00 | 0.00 | 6.78 | 8.83 | 10.36 | 11.19 | 13.26 | 14.89 | 24.41 |
| | 0:35:00 | 0.00 | 0.00 | 6.65 | 8.53 | 9.94 | 13.21 | 15.62 | 18.53 | 29.96 |
| | 0:40:00 | 0.00 | 0.00 | 6.24 | 7.89 | 9.17 | 13.24 | 15.64 | 18.61 | 30.03 |
| | 0:45:00 | 0.00 | 0.00 | 5.65 | 7.23 | 8.43 | 12.31 | 14.52 | 17.67 | 28.57 |
| | 0:50:00 | 0.00 | 0.00 | 5.15 | 6.68 | 7.73 | 11.47 | 13.48 | 16.35 | 26.52 |
| | 0:55:00 | 0.00 | 0.00 | 4.73 | 6.14 | 7.13 | 10.39 | 12.17 | 14.94 | 24.26 |
| | 1:00:00 | 0.00 | 0.00 | 4.33 | 5.60 | 6.55 | 9.42 | 11.00 | 13.74 | 22.36 |
| | 1:05:00 | 0.00 | 0.00 | 3.97 | 5.12 | 6.02 | 8.56 | 9.97 | 12.68 | 20.67 |
| | 1:10:00 | 0.00 | 0.00 | 3.55 | 4.72 | 5.59 | 7.61 | 8.84 | 11.08 | 17.99 |
| | 1:15:00 | 0.00 | 0.00 | 3.24 | 4.40 | 5.33 | 6.80 | 7.88 | 9.67 | 15.64 |
| | 1:20:00 | 0.00 | 0.00 | 3.01 | 4.09 | 5.01 | 6.12 | 7.08 | 8.45 | 13.60 |
| | 1:25:00 | 0.00 | 0.00 | 2.80 | 3.81 | 4.59 | 5.56 | 6.41 | 7.44 | 11.91 |
| | 1:30:00 | 0.00 | 0.00 | 2.60 | 3.55 | 4.20 | 4.98 | 5.73 | 6.57 | 10.46 |
| | 1:35:00 | 0.00 | 0.00 | 2.41 | 3.29 | 3.82 | 4.44 | 5.10 | 5.79 | 9.14 |
| | 1:40:00 | 0.00 | 0.00 | 2.22 | 2.93 | 3.47 | 3.94 | 4.52 | 5.05 | 7.92 |
| | 1:45:00 | 0.00 | 0.00 | 2.03 | 2.58 | 3.13 | 3.47 | 3.96 | 4.36 | 6.78 |
| | 1:50:00 | 0.00 | 0.00 | 1.86 | 2.27 | 2.83 | 3.03 | 3.45 | 3.73 | 5.75 |
| | 1:55:00 | 0.00 | 0.00 | 1.61 | 2.03 | 2.57 | 2.65 | 3.00 | 3.18 | 4.85 |
| | 2:00:00 | 0.00 | 0.00 | 1.43 | 1.86 | 2.34 | 2.36 | 2.66 | 2.75 | 4.16 |
| | 2:05:00 | 0.00 | 0.00 | 1.17 | 1.54 | 1.94 | 1.90 | 2.14 | 2.18 | 3.29 |
| | 2:10:00 | 0.00 | 0.00 | 0.95 | 1.25 | 1.58 | 1.52 | 1.70 | 1.72 | 2.58 |
| | 2:15:00 | 0.00 | 0.00 | 0.77 | 1.01 | 1.28 | 1.21 | 1.36 | 1.35 | 2.01 |
| | 2:20:00 | 0.00 | 0.00 | 0.63 | 0.82 | 1.04 | 0.97 | 1.09 | 1.06 | 1.57 |
| | 2:25:00 | 0.00 | 0.00 | 0.50 | 0.66 | 0.83 | 0.77 | 0.87 | 0.83 | 1.22 |
| | 2:30:00 | 0.00 | 0.00 | 0.40 | 0.52 | 0.66 | 0.61 | 0.69 | 0.64 | 0.94 |
| | 2:35:00 | 0.00 | 0.00 | 0.32 | 0.41 | 0.52 | 0.48 | 0.53 | 0.50 | 0.72 |
| | 2:40:00 | 0.00 | 0.00 | 0.25 | 0.32 | 0.40 | 0.37 | 0.41 | 0.39 | 0.56 |
| | 2:45:00 | 0.00 | 0.00 | 0.20 | 0.25 | 0.31 | 0.29 | 0.32 | 0.30 | 0.44 |
| | 2:50:00 | 0.00 | 0.00 | 0.15 | 0.19 | 0.24 | 0.23 | 0.25 | 0.24 | 0.35 |
| | 2:55:00 | 0.00 | 0.00 | 0.12 | 0.14 | 0.19 | 0.17 | 0.19 | 0.19 | 0.27 |
| | 3:00:00 | 0.00 | 0.00 | 0.08 | 0.10 | 0.14 | 0.13 | 0.14 | 0.14 | 0.20 |
| | 3:05:00 | 0.00 | 0.00 | 0.06 | 0.07 | 0.10 | 0.09 | 0.10 | 0.10 | 0.14 |
| | 3:10:00 | 0.00 | 0.00 | 0.03 | 0.05 | 0.06 | 0.06 | 0.07 | 0.06 | 0.09 |
| | 3:15:00 | 0.00 | 0.00 | 0.02 | 0.03 | 0.03 | 0.04 | 0.04 | 0.04 | 0.05 |
| | 3:20:00 | 0.00 | 0.00 | 0.01 | 0.01 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| | 3:25:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.01 | 0.01 | 0.01 | 0.01 |
| | 3:30:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 3:35:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 3:40:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 3:45:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 3:50:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 3:55:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 4:00:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 4:05:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 4:10:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 4:15:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 4:20:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 4:25:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 4:30:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 4:35:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 4:40:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 4:45:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 4:50:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 4:55:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 5:00:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| 5:05:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| 5:10:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| 5:15:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| 5:20:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| 5:25:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| 5:30:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| 5:35:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| 5:40:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| 5:45:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| 5:50:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| 5:55:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| 6:00:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |

Revise to SFB D for consistency.

Design Procedure Form: Sand Filter (SF)

UD-BMP (Version 3.07, March 2018)

Sheet 1 of 2

Designer: SPC
 Company: HR Green
 Date: March 13, 2024
 Project: Eastonville Road - Segment 1 Improvements Pond D
 Location: El Paso County, CO

| | |
|--|---|
| <p>1. Basin Storage Volume</p> <p>A) Effective Imperviousness of Tributary Area, I_a (100% if all paved and roofed areas upstream of sand filter)</p> <p>B) Tributary Area's Imperviousness Ratio ($i = I_a/100$)</p> <p>C) Water Quality Capture Volume (WQCV) Based on 12-hour Drain Time $WQCV = 0.8 * (0.91 * i^3 - 1.19 * i^2 + 0.78 * i)$</p> <p>D) Contributing Watershed Area (including sand filter area)</p> <p>E) Water Quality Capture Volume (WQCV) Design Volume $V_{WQCV} = WQCV / 12 * Area$</p> <p>F) For Watersheds Outside of the Denver Region, Depth of Average Runoff Producing Storm</p> <p>G) For Watersheds Outside of the Denver Region, Water Quality Capture Volume (WQCV) Design Volume</p> <p>H) User Input of Water Quality Capture Volume (WQCV) Design Volume (Only if a different WQCV Design Volume is desired)</p> | <p>$I_a =$ <input type="text" value="52.0"/> %</p> <p>$i =$ <input type="text" value="0.520"/></p> <p>WQCV = <input type="text" value="0.17"/> watershed inches</p> <p>Area = <input type="text" value="91,476"/> sq ft</p> <p>$V_{WQCV} =$ <input type="text" value="1,292"/> cu ft</p> <p>$d_b =$ <input type="text" value=""/> in</p> <p>$V_{WQCV OTHER} =$ <input type="text" value=""/> cu ft</p> <p>$V_{WQCV USER} =$ <input type="text" value=""/> cu ft</p> |
| <p>2. Basin Geometry</p> <p>A) WQCV Depth</p> <p>B) Sand Filter Side Slopes (Horizontal distance per unit vertical, 4:1 or flatter preferred). Use "0" if sand filter has vertical walls.</p> <p>C) Minimum Filter Area (Flat Surface Area)</p> <p>D) Actual Filter Area</p> <p>E) Volume Provided</p> | <p>$D_{WQCV} =$ <input type="text" value="1.0"/> ft</p> <p>$Z =$ <input type="text" value="4.00"/> ft / ft</p> <p>$A_{Min} =$ <input type="text" value="595"/> sq ft</p> <p>$A_{Actual} =$ <input type="text" value="969"/> sq ft</p> <p>$V_T =$ <input type="text" value="12536"/> cu ft</p> |
| <p>3. Filter Material</p> | <p>Choose One</p> <p><input checked="" type="radio"/> 18" CDOT Class B or C Filter Material</p> <p><input type="radio"/> Other (Explain):</p> <p>_____</p> <p>_____</p> |
| <p>4. Underdrain System</p> <p>A) Are underdrains provided?</p> <p>B) Underdrain system orifice diameter for 12 hour drain time</p> <p>i) Distance From Lowest Elevation of the Storage Volume to the Center of the Orifice</p> <p>ii) Volume to Drain in 12 Hours</p> <p>iii) Orifice Diameter, 3/8" Minimum</p> | <p>Choose One</p> <p><input checked="" type="radio"/> YES</p> <p><input type="radio"/> NO</p> <p>$y =$ <input type="text" value="2.1"/> ft</p> <p>$Vol_{12} =$ <input type="text" value="1,292"/> cu ft</p> <p>$D_o =$ <input type="text" value="13/16"/> in</p> |

does not match CDs

Design Procedure Form: Sand Filter (SF)

Sheet 2 of 2

Designer: SPC
Company: HR Green
Date: March 13, 2024
Project: Eastonville Road - Segment 1 Improvements Pond D
Location: El Paso County, CO

Revise to SFB D for consistency.

5. Impermeable Geomembrane Liner and Geotextile Separator Fabric

A) Is an impermeable liner provided due to proximity of structures or groundwater contamination?

Choose One

YES NO

6. Inlet / Outlet Works

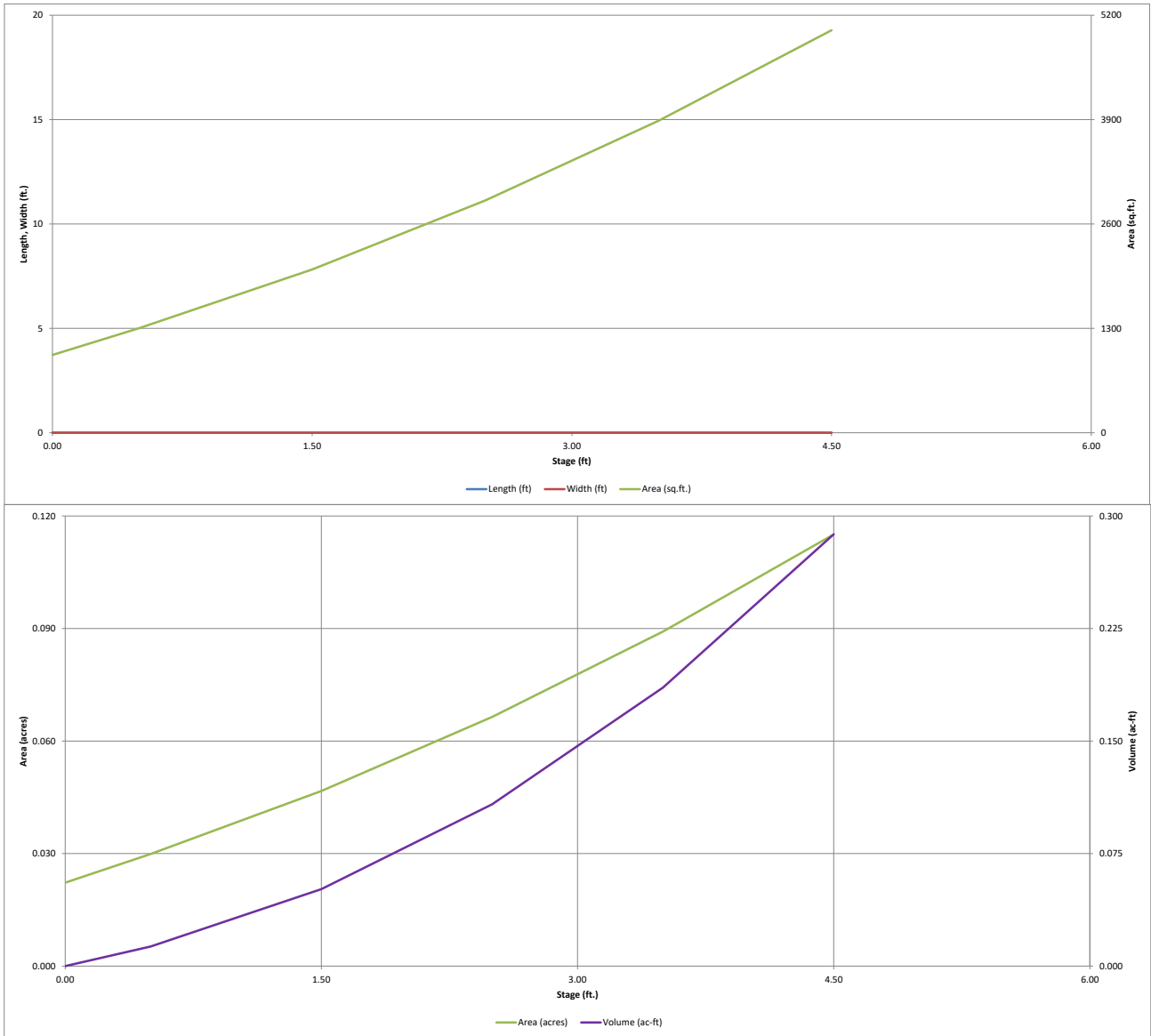
A) Describe the type of energy dissipation at inlet points and means of conveying flows in excess of the WQCV through the outlet

Engery dissipation at inlet points provided via riprap, and means of conveying flows in excess of the WQCV through the outlet is via the modified type 'C' inlet outlet structure grate, and a restricted outlet pipe.

Notes:

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-*Detention*, Version 4.05 (January 2022)



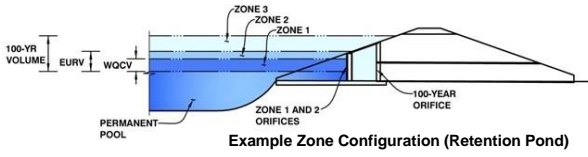
X = value does not match what is shown in the CDs.
✓ = value does match CDs.

DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.05 (January 2022)

Project: Eastonville Road

Basin ID: SFB D



Example Zone Configuration (Retention Pond)

| | Estimated Stage (ft) | Estimated Volume (ac-ft) | Outlet Type |
|--------------------------|----------------------|--------------------------|----------------------|
| Zone 1 (WQCV) | 0.99 | 0.030 | Filtration Media |
| Zone 2 (EURV) | 2.64 | 0.087 | Circular Orifice |
| Zone 3 (100-year) | 3.68 | 0.085 | Weir&Pipe (Restrict) |
| Total (all zones) | | 0.202 | |

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Calculated Parameters for Underdrain

| | | | | | |
|-----------------------------------|------|--|-------------------------------|------|-----------------|
| Underdrain Orifice Invert Depth = | 2.08 | ft (distance below the filtration media surface) | Underdrain Orifice Area = | 0.0 | ft ² |
| Underdrain Orifice Diameter = | 0.83 | inches | Underdrain Orifice Centroid = | 0.03 | feet |

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Calculated Parameters for Plate

| | | | | | |
|--|-----|---|----------------------------|-----|-----------------|
| Centroid of Lowest Orifice = | N/A | ft (relative to basin bottom at Stage = 0 ft) | WQ Orifice Area per Row = | N/A | ft ² |
| Depth at top of Zone using Orifice Plate = | N/A | ft (relative to basin bottom at Stage = 0 ft) | Elliptical Half-Width = | N/A | feet |
| Orifice Plate: Orifice Vertical Spacing = | N/A | inches | Elliptical Slot Centroid = | N/A | feet |
| Orifice Plate: Orifice Area per Row = | N/A | sq. inches | Elliptical Slot Area = | N/A | ft ² |

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

| | Row 1 (optional) | Row 2 (optional) | Row 3 (optional) | Row 4 (optional) | Row 5 (optional) | Row 6 (optional) | Row 7 (optional) | Row 8 (optional) |
|--------------------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|
| Stage of Orifice Centroid (ft) | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A |
| Orifice Area (sq. inches) | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A |

| | Row 9 (optional) | Row 10 (optional) | Row 11 (optional) | Row 12 (optional) | Row 13 (optional) | Row 14 (optional) | Row 15 (optional) | Row 16 (optional) |
|--------------------------------|------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| Stage of Orifice Centroid (ft) | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A |
| Orifice Area (sq. inches) | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A |

User Input: Vertical Orifice (Circular or Rectangular)

Calculated Parameters for Vertical Orifice

| | Zone 2 Circular | Not Selected | | Zone 2 Circular | Not Selected |
|---|-----------------|--------------|---|-----------------------------|--------------|
| Invert of Vertical Orifice = | 1.25 | N/A | ft (relative to basin bottom at Stage = 0 ft) | Vertical Orifice Area = | 0.00 |
| Depth at top of Zone using Vertical Orifice = | 2.64 | N/A | ft (relative to basin bottom at Stage = 0 ft) | Vertical Orifice Centroid = | 0.02 |
| Vertical Orifice Diameter = | 0.38 | N/A | inches | | N/A |

User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir and No Outlet Pipe)

Calculated Parameters for Overflow Weir

| | Zone 3 Weir | Not Selected | | Zone 3 Weir | Not Selected |
|---|--------------|--------------|---|--|--------------|
| Overflow Weir Front Edge Height, H _o = | 2.65 | N/A | ft (relative to basin bottom at Stage = 0 ft) | Height of Grate Upper Edge, H _t = | 2.65 |
| Overflow Weir Front Edge Length = | 3.00 | N/A | feet | Overflow Weir Slope Length = | 3.00 |
| Overflow Weir Grate Slope = | 0.00 | N/A | H:V | Grate Open Area / 100-yr Orifice Area = | 48.50 |
| Horiz. Length of Weir Sides = | 3.00 | N/A | feet | Overflow Grate Open Area w/o Debris = | 6.26 |
| Overflow Grate Type = | Type C Grate | N/A | | Overflow Grate Open Area w/ Debris = | 3.13 |
| Debris Clogging % = | 50% | N/A | % | | |

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate

| | Zone 3 Restrictor | Not Selected | | Zone 3 Restrictor | Not Selected |
|---|-------------------|--------------|--|--|--------------|
| Depth to Invert of Outlet Pipe = | 2.08 | N/A | ft (distance below basin bottom at Stage = 0 ft) | Outlet Orifice Area = | 0.13 |
| Outlet Pipe Diameter = | 18.00 | N/A | inches | Outlet Orifice Centroid = | 0.11 |
| Restrictor Plate Height Above Pipe Invert = | 2.27 | | inches | Half-Central Angle of Restrictor Plate on Pipe = | 0.73 |

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Calculated Parameters for Spillway

| | | | | | |
|-------------------------------------|-------|---|------------------------------------|------|---------|
| Spillway Invert Stage = | 3.40 | ft (relative to basin bottom at Stage = 0 ft) | Spillway Design Flow Depth = | 0.10 | feet |
| Spillway Crest Length = | 30.00 | feet | Stage at Top of Freeboard = | 4.50 | feet |
| Spillway End Slopes = | 4.00 | H:V | Basin Area at Top of Freeboard = | 0.12 | acres |
| Freeboard above Max Water Surface = | 1.00 | feet | Basin Volume at Top of Freeboard = | 0.29 | acre-ft |

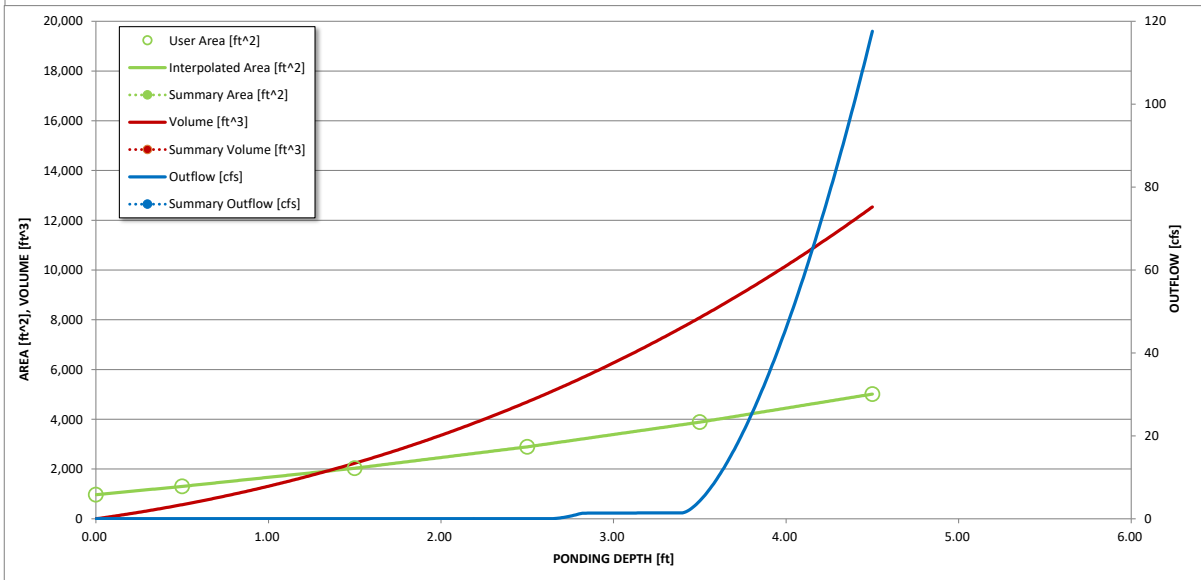
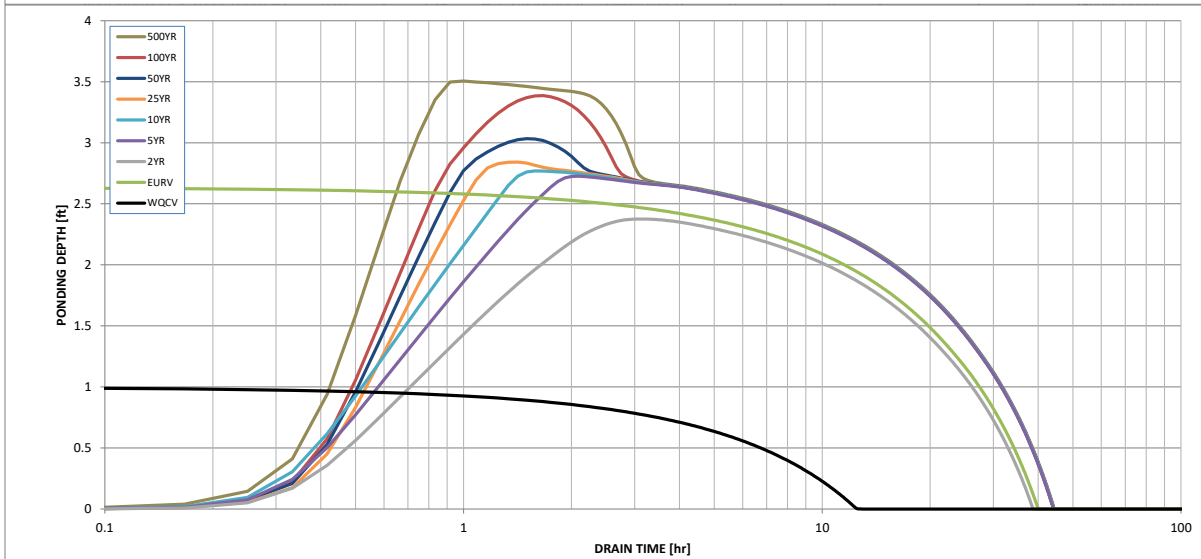
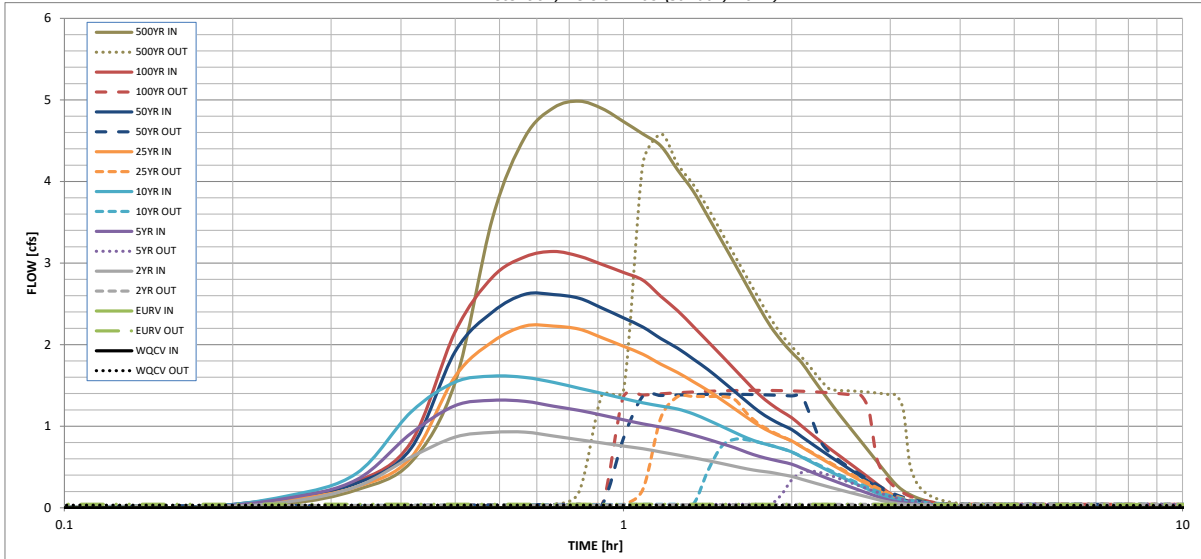
Routed Hydrograph Results

The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).

| | WQCV | EURV | 2 Year | 5 Year | 10 Year | 25 Year | 50 Year | 100 Year | 500 Year |
|---|------------------|--------------------|--------------------|-----------------|-----------------|----------------|----------------|----------------|----------|
| Design Storm Return Period = | | | | | | | | | |
| One-Hour Rainfall Depth (in) = | N/A | N/A | 1.19 | 1.50 | 1.75 | 2.00 | 2.25 | 2.52 | 3.68 |
| CUHP Runoff Volume (acre-ft) = | 0.030 | 0.117 | 0.110 | 0.157 | 0.197 | 0.251 | 0.294 | 0.350 | 0.562 |
| Inflow Hydrograph Volume (acre-ft) = | N/A | N/A | 0.110 | 0.157 | 0.197 | 0.251 | 0.294 | 0.350 | 0.562 |
| CUHP Predevelopment Peak Q (cfs) = | N/A | N/A | 0.1 | 0.3 | 0.4 | 0.8 | 1.0 | 1.4 | 2.5 |
| OPTIONAL Override Predevelopment Peak Q (cfs) = | N/A | N/A | | | | | | | |
| Predevelopment Unit Peak Flow, q (cfs/acre) = | N/A | N/A | 0.05 | 0.14 | 0.21 | 0.40 | 0.50 | 0.66 | 1.18 |
| Peak Inflow Q (cfs) = | N/A | N/A | 0.9 | 1.3 | 1.6 | 2.2 | 2.6 | 3.1 | 5.0 |
| Peak Outflow Q (cfs) = | 0.0 | 0.0 | 0.0 | 0.4 | 0.8 | 1.4 | 1.4 | 1.4 | 4.6 |
| Ratio Peak Outflow to Predevelopment Q = | N/A | N/A | N/A | 1.6 | 1.9 | 1.6 | 1.3 | 1.0 | 1.8 |
| Structure Controlling Flow = | Filtration Media | Vertical Orifice 1 | Vertical Orifice 1 | Overflow Weir 1 | Overflow Weir 1 | Outlet Plate 1 | Outlet Plate 1 | Outlet Plate 1 | Spillway |
| Max Velocity through Grate 1 (fps) = | N/A | N/A | N/A | 0.1 | 0.1 | 0.2 | 0.2 | 0.2 | 0.2 |
| Max Velocity through Grate 2 (fps) = | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A |
| Time to Drain 97% of Inflow Volume (hours) = | 12 | 38 | 37 | 42 | 42 | 41 | 40 | 40 | 37 |
| Time to Drain 99% of Inflow Volume (hours) = | 12 | 40 | 38 | 43 | 43 | 43 | 43 | 43 | 42 |
| Maximum Ponding Depth (ft) = | ✓ 1.00 | ✓ 2.64 | 2.38 | 2.73 | 2.77 | 2.84 | 3.03 | ✓ 3.39 | 3.51 |
| Area at Maximum Ponding Depth (acres) = | 0.04 | 0.07 | 0.06 | 0.07 | 0.07 | 0.07 | 0.08 | 0.09 | 0.09 |
| Maximum Volume Stored (acre-ft) = | 0.030 | 0.117 | 0.099 | 0.123 | 0.126 | 0.132 | 0.146 | 0.175 | 0.186 |

DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.05 (January 2022)



| S-A-V-D Chart Axis Override | X-axis | Left Y-Axis | Right Y-Axis |
|-----------------------------|--------|-------------|--------------|
| minimum bound | | | |
| maximum bound | | | |

DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename: _____

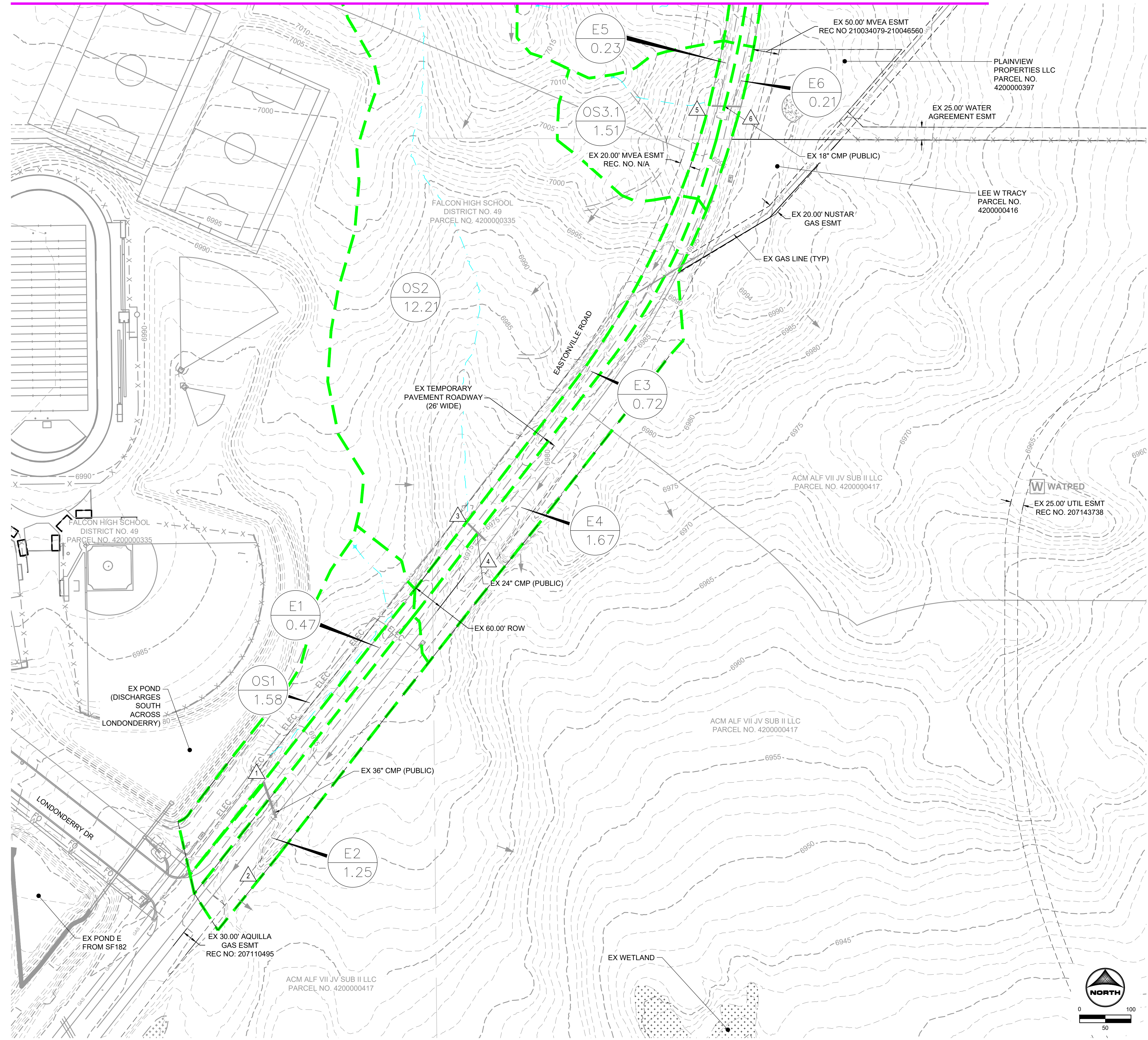
Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

| Time Interval | SOURCE | CUHP | CUHP | CUHP | CUHP | CUHP | CUHP | CUHP | CUHP | CUHP |
|---------------|---------|------------|------------|--------------|--------------|---------------|---------------|---------------|----------------|----------------|
| | TIME | WQCV [cfs] | EURV [cfs] | 2 Year [cfs] | 5 Year [cfs] | 10 Year [cfs] | 25 Year [cfs] | 50 Year [cfs] | 100 Year [cfs] | 500 Year [cfs] |
| 5.00 min | 0:00:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 0:05:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 0:10:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.01 | 0.00 | 0.05 |
| | 0:15:00 | 0.00 | 0.00 | 0.07 | 0.12 | 0.14 | 0.10 | 0.12 | 0.12 | 0.22 |
| | 0:20:00 | 0.00 | 0.00 | 0.26 | 0.34 | 0.42 | 0.26 | 0.30 | 0.32 | 0.56 |
| | 0:25:00 | 0.00 | 0.00 | 0.62 | 0.91 | 1.17 | 0.61 | 0.73 | 0.80 | 1.54 |
| | 0:30:00 | 0.00 | 0.00 | 0.87 | 1.25 | 1.54 | 1.61 | 1.92 | 2.16 | 3.55 |
| | 0:35:00 | 0.00 | 0.00 | 0.92 | 1.32 | 1.61 | 2.04 | 2.40 | 2.83 | 4.55 |
| | 0:40:00 | 0.00 | 0.00 | 0.93 | 1.30 | 1.60 | 2.23 | 2.62 | 3.08 | 4.90 |
| | 0:45:00 | 0.00 | 0.00 | 0.88 | 1.24 | 1.54 | 2.23 | 2.61 | 3.14 | 4.98 |
| | 0:50:00 | 0.00 | 0.00 | 0.83 | 1.19 | 1.47 | 2.19 | 2.57 | 3.08 | 4.89 |
| | 0:55:00 | 0.00 | 0.00 | 0.79 | 1.13 | 1.40 | 2.08 | 2.45 | 2.98 | 4.73 |
| | 1:00:00 | 0.00 | 0.00 | 0.76 | 1.08 | 1.34 | 1.98 | 2.33 | 2.88 | 4.58 |
| | 1:05:00 | 0.00 | 0.00 | 0.72 | 1.03 | 1.29 | 1.88 | 2.21 | 2.79 | 4.43 |
| | 1:10:00 | 0.00 | 0.00 | 0.68 | 0.99 | 1.25 | 1.76 | 2.07 | 2.59 | 4.14 |
| | 1:15:00 | 0.00 | 0.00 | 0.65 | 0.94 | 1.21 | 1.66 | 1.96 | 2.42 | 3.88 |
| | 1:20:00 | 0.00 | 0.00 | 0.61 | 0.89 | 1.15 | 1.55 | 1.82 | 2.22 | 3.57 |
| | 1:25:00 | 0.00 | 0.00 | 0.58 | 0.84 | 1.07 | 1.44 | 1.69 | 2.04 | 3.27 |
| | 1:30:00 | 0.00 | 0.00 | 0.54 | 0.79 | 1.00 | 1.32 | 1.56 | 1.86 | 2.98 |
| | 1:35:00 | 0.00 | 0.00 | 0.51 | 0.73 | 0.92 | 1.21 | 1.42 | 1.69 | 2.71 |
| | 1:40:00 | 0.00 | 0.00 | 0.48 | 0.68 | 0.85 | 1.10 | 1.29 | 1.53 | 2.45 |
| | 1:45:00 | 0.00 | 0.00 | 0.45 | 0.63 | 0.80 | 1.00 | 1.18 | 1.39 | 2.22 |
| | 1:50:00 | 0.00 | 0.00 | 0.43 | 0.59 | 0.76 | 0.93 | 1.09 | 1.27 | 2.05 |
| | 1:55:00 | 0.00 | 0.00 | 0.41 | 0.56 | 0.73 | 0.87 | 1.02 | 1.18 | 1.90 |
| | 2:00:00 | 0.00 | 0.00 | 0.38 | 0.53 | 0.68 | 0.82 | 0.96 | 1.10 | 1.78 |
| | 2:05:00 | 0.00 | 0.00 | 0.35 | 0.49 | 0.62 | 0.75 | 0.87 | 1.00 | 1.61 |
| | 2:10:00 | 0.00 | 0.00 | 0.32 | 0.44 | 0.56 | 0.68 | 0.79 | 0.91 | 1.46 |
| | 2:15:00 | 0.00 | 0.00 | 0.28 | 0.39 | 0.50 | 0.61 | 0.71 | 0.82 | 1.31 |
| | 2:20:00 | 0.00 | 0.00 | 0.25 | 0.35 | 0.45 | 0.55 | 0.64 | 0.73 | 1.17 |
| | 2:25:00 | 0.00 | 0.00 | 0.23 | 0.31 | 0.40 | 0.49 | 0.57 | 0.65 | 1.04 |
| | 2:30:00 | 0.00 | 0.00 | 0.20 | 0.28 | 0.35 | 0.43 | 0.50 | 0.58 | 0.92 |
| | 2:35:00 | 0.00 | 0.00 | 0.18 | 0.24 | 0.31 | 0.38 | 0.44 | 0.51 | 0.80 |
| | 2:40:00 | 0.00 | 0.00 | 0.15 | 0.21 | 0.26 | 0.33 | 0.38 | 0.43 | 0.69 |
| | 2:45:00 | 0.00 | 0.00 | 0.13 | 0.17 | 0.22 | 0.27 | 0.32 | 0.37 | 0.58 |
| | 2:50:00 | 0.00 | 0.00 | 0.10 | 0.14 | 0.18 | 0.23 | 0.26 | 0.30 | 0.47 |
| | 2:55:00 | 0.00 | 0.00 | 0.08 | 0.11 | 0.15 | 0.18 | 0.21 | 0.23 | 0.36 |
| | 3:00:00 | 0.00 | 0.00 | 0.07 | 0.09 | 0.12 | 0.14 | 0.16 | 0.18 | 0.27 |
| | 3:05:00 | 0.00 | 0.00 | 0.05 | 0.07 | 0.10 | 0.10 | 0.12 | 0.13 | 0.21 |
| | 3:10:00 | 0.00 | 0.00 | 0.05 | 0.06 | 0.08 | 0.08 | 0.09 | 0.10 | 0.16 |
| | 3:15:00 | 0.00 | 0.00 | 0.04 | 0.05 | 0.07 | 0.07 | 0.08 | 0.08 | 0.13 |
| | 3:20:00 | 0.00 | 0.00 | 0.03 | 0.04 | 0.06 | 0.05 | 0.06 | 0.06 | 0.10 |
| | 3:25:00 | 0.00 | 0.00 | 0.03 | 0.04 | 0.05 | 0.04 | 0.05 | 0.05 | 0.08 |
| | 3:30:00 | 0.00 | 0.00 | 0.02 | 0.03 | 0.04 | 0.04 | 0.04 | 0.04 | 0.06 |
| | 3:35:00 | 0.00 | 0.00 | 0.02 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 | 0.05 |
| | 3:40:00 | 0.00 | 0.00 | 0.02 | 0.02 | 0.03 | 0.02 | 0.03 | 0.02 | 0.04 |
| | 3:45:00 | 0.00 | 0.00 | 0.01 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 | 0.03 |
| | 3:50:00 | 0.00 | 0.00 | 0.01 | 0.01 | 0.02 | 0.02 | 0.02 | 0.02 | 0.03 |
| | 3:55:00 | 0.00 | 0.00 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 0.02 |
| 4:00:00 | 0.00 | 0.00 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 0.02 | |
| 4:05:00 | 0.00 | 0.00 | 0.00 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | |
| 4:10:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.01 | 0.00 | 0.01 | |
| 4:15:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| 4:20:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| 4:25:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| 4:30:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| 4:35:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| 4:40:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| 4:45:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| 4:50:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| 4:55:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| 5:00:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| 5:05:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| 5:10:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| 5:15:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| 5:20:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| 5:25:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| 5:30:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| 5:35:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| 5:40:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| 5:45:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| 5:50:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| 5:55:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| 6:00:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |

APPENDIX E – DRAINAGE MAPS

SEE SHEET 2



LEGEND:

- EXISTING MAJOR CONTOUR 5250
- EXISTING MINOR CONTOUR
- EX STORM SEWER
- EX DRAINAGE SWALE
- EX PROPERTY LINE
- EXISTING FLOW DIRECTION
- PROPOSED DRAINAGE BASIN
- DESIGN POINT
- PROPOSED BASIN LABEL

| BASIN | AREA (ac) | % IMPERVIOUS | Q5 (cfs) | Q100 (cfs) |
|-------|-----------|--------------|----------|------------|
| E1 | 0.47 | 46 | 0.7 | 1.7 |
| E2 | 1.25 | 18 | 1.0 | 3.5 |
| E3 | 0.47 | 58 | 1.0 | 2.1 |
| E4 | 1.67 | 20 | 1.4 | 4.6 |
| E5 | 0.23 | 45 | 0.5 | 1.1 |
| E6 | 0.21 | 49 | 0.5 | 1.1 |
| E7 | 0.23 | 45 | 0.5 | 1.2 |
| E8 | 0.18 | 56 | 0.4 | 0.9 |
| E9 | 0.72 | 46 | 1.2 | 2.7 |
| E10 | 0.72 | 50 | 1.3 | 2.8 |
| OS1 | 1.58 | 2 | 0.5 | 3.6 |
| OS2 | 12.21 | 2 | 3.6 | 24.3 |
| OS3.1 | 1.51 | 2 | 0.5 | 3.6 |
| OS3.2 | 2.86 | 2 | 1.0 | 6.6 |
| OS3.3 | 21.12 | 2 | 6.4 | 42.7 |

| DESIGN POINT | CONTRIBUTING BASINS | SO5 (cfs) | SO100 (cfs) |
|--------------|---------------------|-----------|-------------|
| 1 | E1,OS1 | 1.2 | 4.9 |
| 2 | E2,DP1 | 2.1 | 8.2 |
| 3 | E3,OS2 | 4.5 | 26.1 |
| 4 | DP3,E4 | 5.8 | 30.4 |
| 5 | E5,OS3.1 | 0.9 | 4.5 |
| 6 | DP5,E6 | 1.3 | 5.4 |
| 7.1 | E7,OS3.2 | 1.4 | 7.5 |
| 8.1 | DP7.1,E8 | 1.7 | 8.2 |
| 7.2 | OS3.3,E9 | 7.4 | 45.3 |
| 8.2 | DP7.2,E10 | 8.6 | 47.7 |

Indicate where Segment 1 ends/Segment 2 starts.

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 CAD DATE: 3/22/2024
 CAD FILE: J:\2020\201662\CAD\Drawings\Eastonville_Road_662.08\Drainage\201662.08_FDR_map_ex_5.dwg

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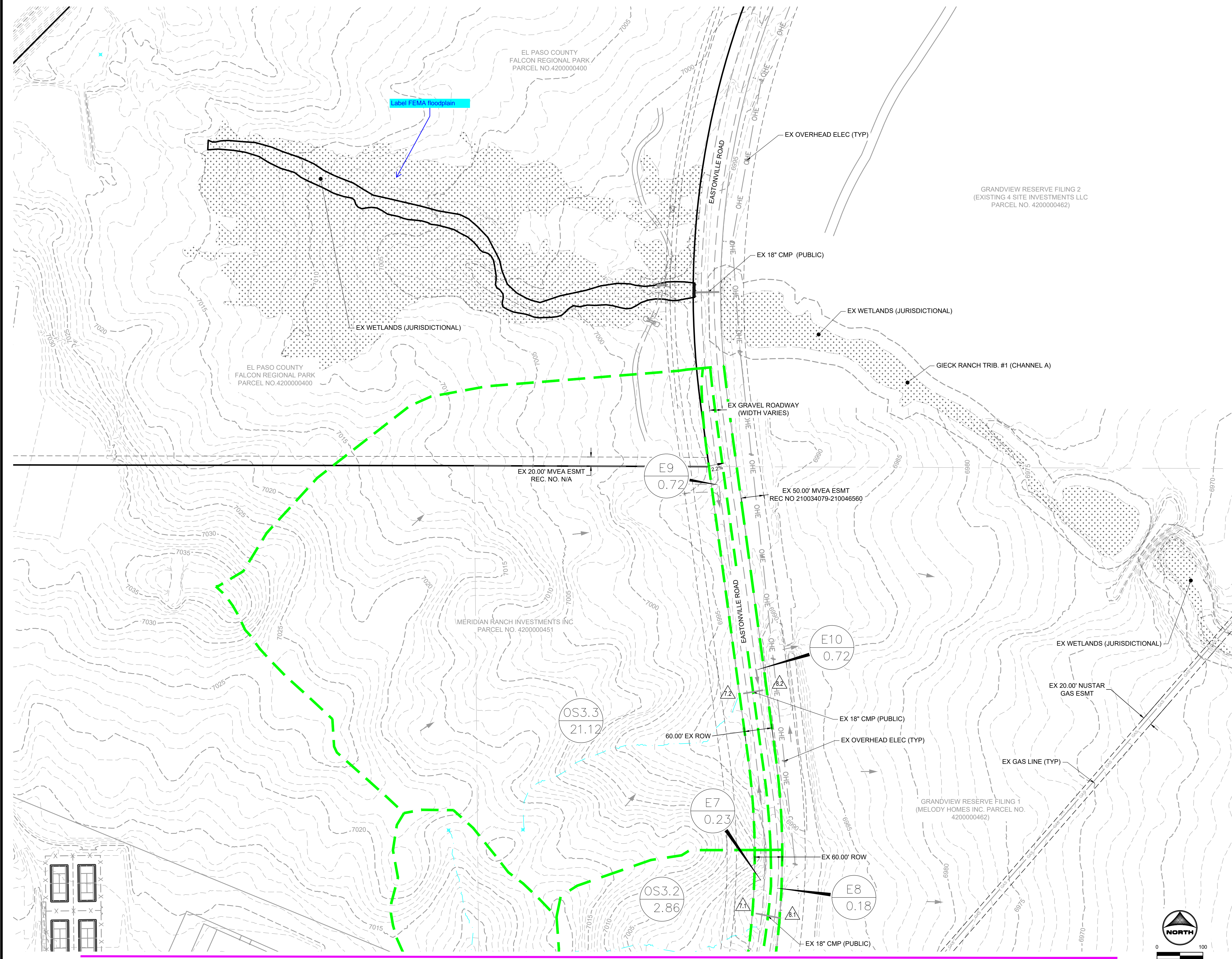
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 D.R. HORTON
 EL PASO COUNTY, CO

D-R HORTON
 America's Builder

EXISTING CONDITIONS - DRAINAGE MAP

SHEET DRN 1



LEGEND:

- EXISTING MAJOR CONTOUR
- EXISTING MINOR CONTOUR
- EX STORM SEWER
- EX DRAINAGE SWALE
- EX PROPERTY LINE
- EXISTING FLOW DIRECTION
- PROPOSED DRAINAGE BASIN
- DESIGN POINT
- PROPOSED BASIN LABEL

SUMMARY RUNOFF TABLE

| BASIN | AREA (ac) | % IMPERVIOUS | Q5 (cfs) | Q100 (cfs) |
|-------|-----------|--------------|----------|------------|
| E1 | 0.47 | 46 | 0.7 | 1.7 |
| E2 | 1.25 | 18 | 1.0 | 3.5 |
| E3 | 0.47 | 58 | 1.0 | 2.1 |
| E4 | 1.67 | 20 | 1.4 | 4.6 |
| E5 | 0.23 | 45 | 0.5 | 1.1 |
| E6 | 0.21 | 49 | 0.5 | 1.1 |
| E7 | 0.23 | 45 | 0.5 | 1.2 |
| E8 | 0.18 | 56 | 0.4 | 0.9 |
| E9 | 0.72 | 46 | 1.2 | 2.7 |
| E10 | 0.72 | 50 | 1.3 | 2.8 |
| OS1 | 1.58 | 2 | 0.5 | 3.6 |
| OS2 | 12.21 | 2 | 3.6 | 24.3 |
| OS3.1 | 1.51 | 2 | 0.5 | 3.6 |
| OS3.2 | 2.86 | 2 | 1.0 | 6.6 |
| OS3.3 | 21.12 | 2 | 6.4 | 42.7 |

DESIGN POINT SUMMARY TABLE

| DESIGN POINT | CONTRIBUTING BASINS | SQ5 (cfs) | SQ100 (cfs) |
|--------------|---------------------|-----------|-------------|
| 1 | E1,OS1 | 1.2 | 4.9 |
| 2 | E2,DP1 | 2.1 | 8.2 |
| 3 | E3,OS2 | 4.5 | 26.1 |
| 4 | DP3,E4 | 5.8 | 30.4 |
| 5 | E5,OS3.1 | 0.9 | 4.5 |
| 6 | DP5,E6 | 1.3 | 5.4 |
| 7.1 | E7,OS3.2 | 1.4 | 7.5 |
| 8.1 | DP7.1,E8 | 1.7 | 8.2 |
| 7.2 | OS3.3,E9 | 7.4 | 45.3 |
| 8.2 | DP7.2,E10 | 8.6 | 47.7 |

HR GREEN Xrefs: xref-dwg01_FDR_EX_ev_drain_map_legend_x-dwg_662_x-ref.dwg

DRAWN BY: NQJ JOB DATE: 3/18/2024 BAR IS ONE INCH ON OFFICIAL DRAWINGS.
 APPROVED: CM JOB NUMBER: 201662.08 0" = 1"
 CAD DATE: 3/22/2024 IF NOT ONE INCH, ADJUST SCALE ACCORDINGLY.
 CAD FILE: J:\2020\201662\CAD\Drawings\Eastonville_Road_662.08\Drainage\201662.08_FDR_map_ex.dwg

| NO. | DATE | BY | REVISION DESCRIPTION |
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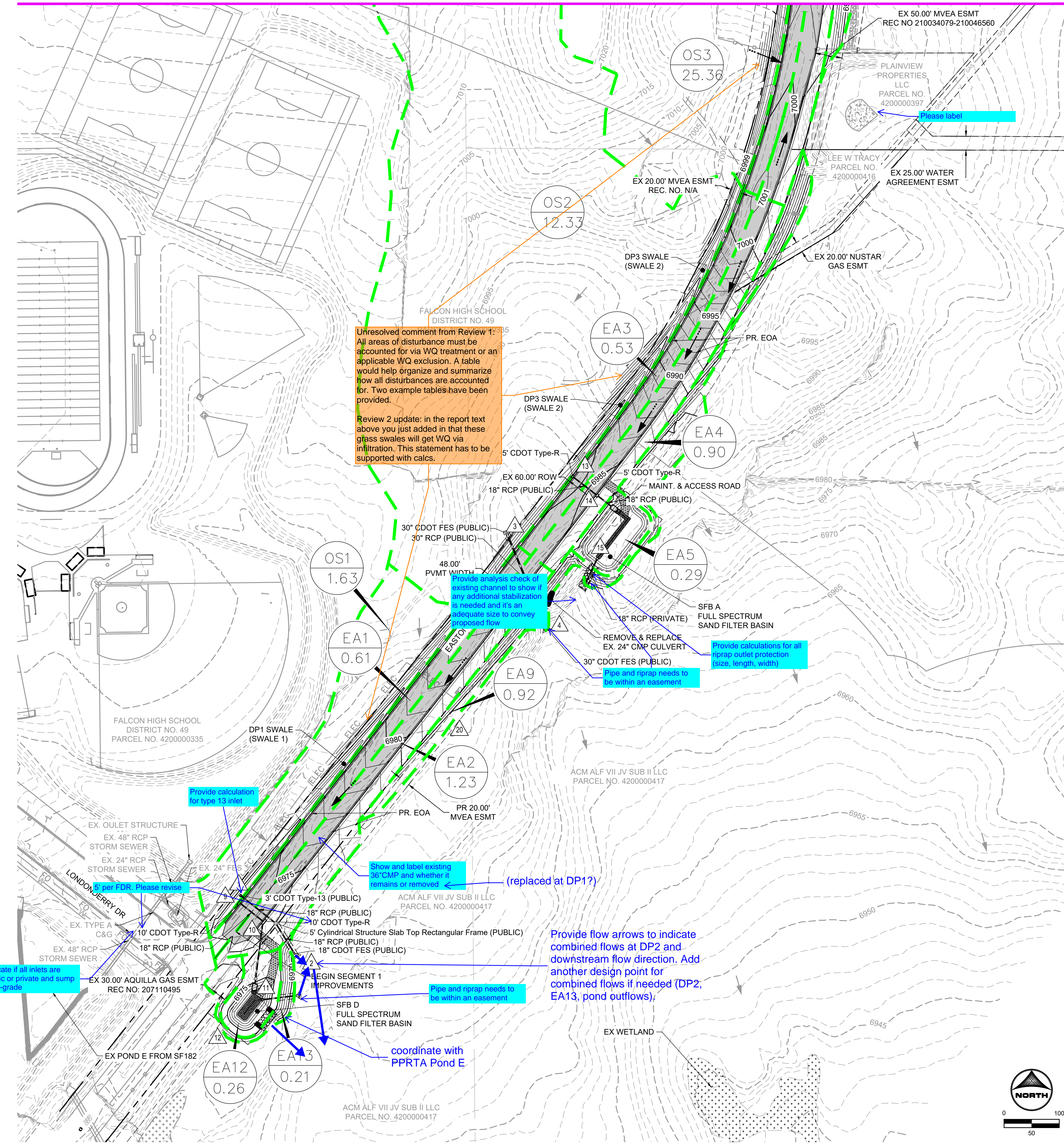
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EXISTING CONDITIONS - DRAINAGE MAP

SHEET DRN 2

SEE SHEET 2



Unresolved comment from Review 1: All areas of disturbance must be accounted for via WQ treatment or an applicable WQ exclusion. A table would help organize and summarize how all disturbances are accounted for. Two example tables have been provided.

Review 2 update: in the report text above you just added in that these glass swales will get WQ via infiltration. This statement has to be supported with calcs.

Provide analysis check of existing channel to show if any additional stabilization is needed and it's an adequate size to convey proposed flow

Provide calculations for all riprap outlet protection (size, length, width)

Provide flow arrows to indicate combined flows at DP2 and downstream flow direction. Add another design point for combined flows if needed (DP2, EA13, pond outflows)

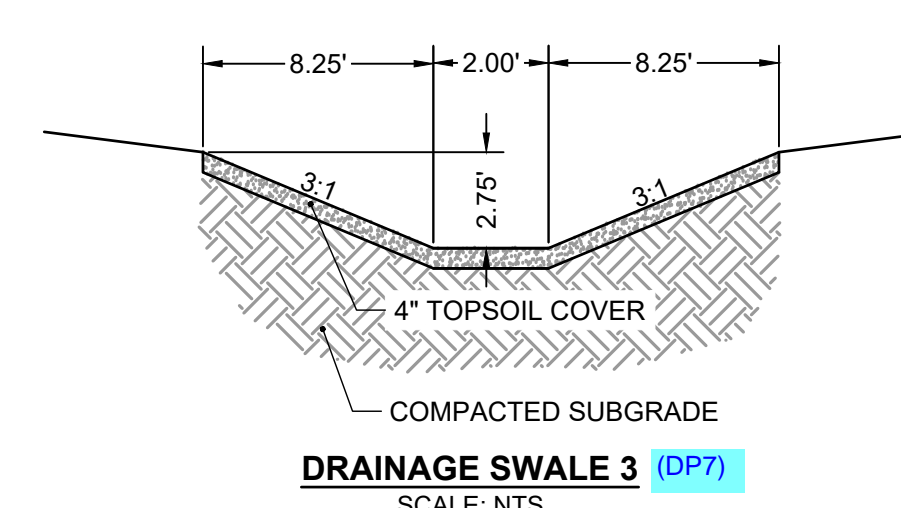
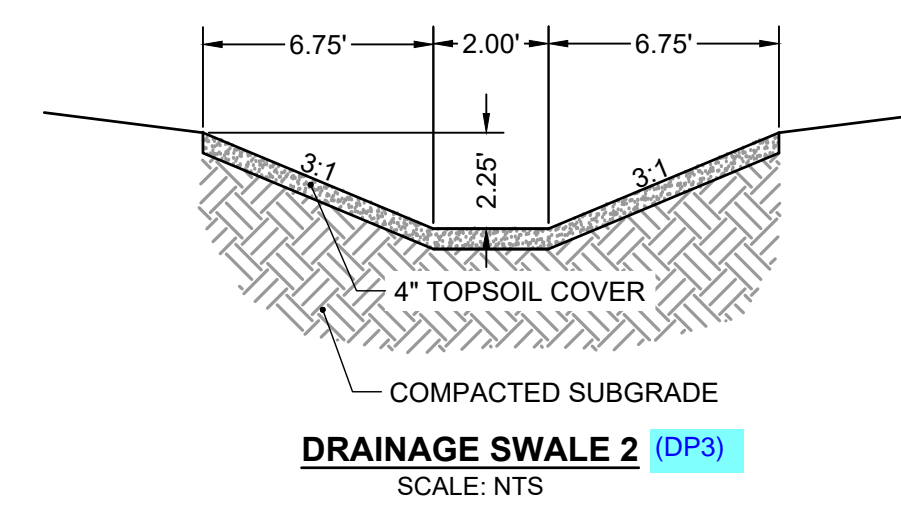
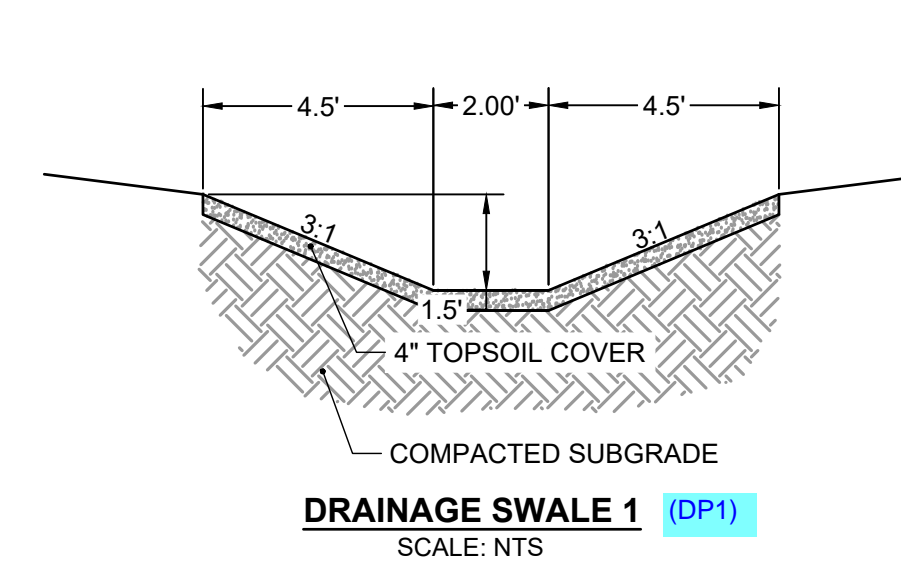
Provide calculation for type 13 inlet

Show and label existing 36" CMP and whether it remains or removed (replaced at DP1?)

Pipe and riprap needs to be within an easement

coordinate with PPRTA Pond E

Indicate if all inlets are public or private and sump or at-grade



- LEGEND:**
- PROPOSED MAJOR CONTOUR ——— 5250
 - PROPOSED MINOR CONTOUR - - - - 5250
 - EXISTING MAJOR CONTOUR ———
 - EXISTING MINOR CONTOUR - - - -
 - PROPOSED STORM SEWER ———
 - PROPOSED DRAINAGE SWALE ———
 - PROPERTY LINE ———
 - PROPOSED FLOW DIRECTION ———
 - EXISTING FLOW DIRECTION ———
 - PROPOSED DRAINAGE BASIN DESIGN POINT ———
 - PROPOSED BASIN LABEL (NAME AREA)
 - PRELIMINARY 100-YR FLOODPLAIN ———

WETLAND SUMMARY RUNOFF TABLE

| BASIN | AREA (ac) | % IMPERVIOUS | Q5 (cfs) | Q100 (cfs) |
|------------------------------|-----------|--------------|----------|------------|
| EA1 | 0.61 | 86 | 2.2 | 4.1 |
| EA2 | 1.23 | 44 | 2.2 | 5.3 |
| EA3 | 0.53 | 87 | 2.1 | 3.4 |
| EA4 | 0.90 | 52 | 2.0 | 3.4 |
| EA5 | 0.29 | 4 | 0.2 | 0.3 |
| EA6 | 1.11 | 88 | 3.0 | 5.1 |
| EA7 | 1.91 | 55 | 3.3 | 5.6 |
| EA8 | 0.86 | 50 | 0.5 | 0.8 |
| EA9 | 0.92 | 35 | 0.4 | 0.6 |
| EA10 | 0.37 | 23 | 0.2 | 0.3 |
| EA11 | 0.15 | 0 | 0.1 | 0.1 |
| EA12 | 0.26 | 10 | 0.2 | 0.8 |
| EA13 | 0.21 | 0 | 0.1 | 0.5 |
| EA8 & EA9 *Per Segment 2 FDR | 5.07 | 78 | 10.2 | 17.2 |
| OS1 | 1.63 | 2 | 0.5 | 3.6 |
| OS2 | 12.33 | 2 | 3.7 | 24.5 |
| OS3 | 25.36 | 2 | 7.9 | 53.3 |

DESIGN POINT SUMMARY TABLE

| DESIGN POINT | CONTRIBUTING BASINS | Q5 (cfs) | Q100 (cfs) |
|--------------|------------------------------------|----------|------------|
| 1 | OS1 | 0.5 | 3.6 |
| 2 | OS1, Pond D Release | 0.9 | 5.0 |
| 3 | OS2 | 3.7 | 24.5 |
| 4 | OS2, POND A RELEASE | 4.0 | 25.7 |
| 7 | OS3 | 7.9 | 53.3 |
| 8 | OS3, POND B RELEASE | 8.3 | 54.3 |
| 9 | EA1 | 2.2 | 4.1 |
| 10 | DP9, EA2 | 4.2 | 9.0 |
| 11 | DP10, EA12 | 4.3 | 9.5 |
| 12 | EA13 | 0.1 | 0.5 |
| 13 | EA3 | 2.1 | 3.4 |
| 14 | DP13, EA4 | 3.9 | 6.5 |
| 15 | DP14, EA5 | 4.0 | 6.7 |
| 16 | EA6 | 3.0 | 5.1 |
| 17 | DP16, EA7 | 6.3 | 10.5 |
| 18 | DP17 | 6.3 | 10.5 |
| 19 | DP18, EA8 | 6.6 | 11.1 |
| 18U | DP17, EA8 & EA9 *PER SEGMENT 2 FDR | 15.6 | 26.2 |
| 19U | DP18, EA8 | 15.9 | 26.6 |
| 20 | EA9 | 0.4 | 0.6 |
| 21 | EA10 | 0.2 | 0.3 |
| 22 | EA11 | 0.1 | 0.1 |

Revise to SFB D for consistency.

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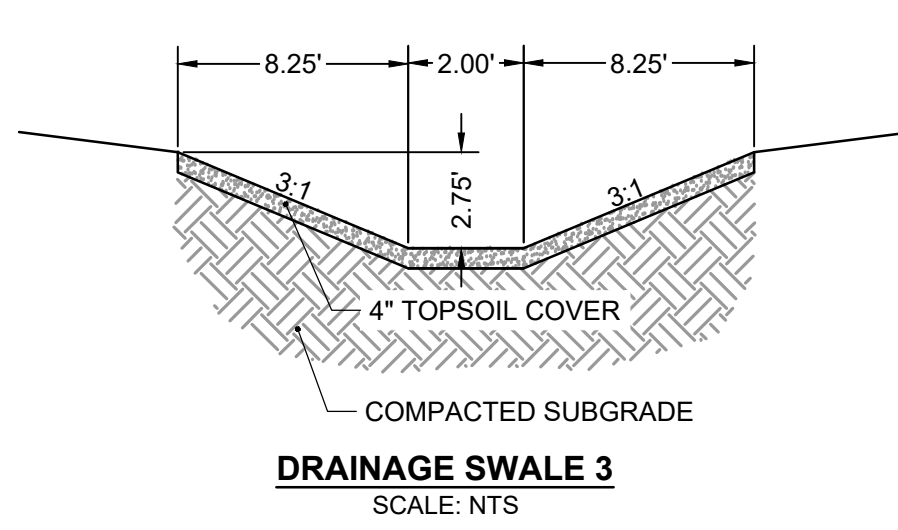
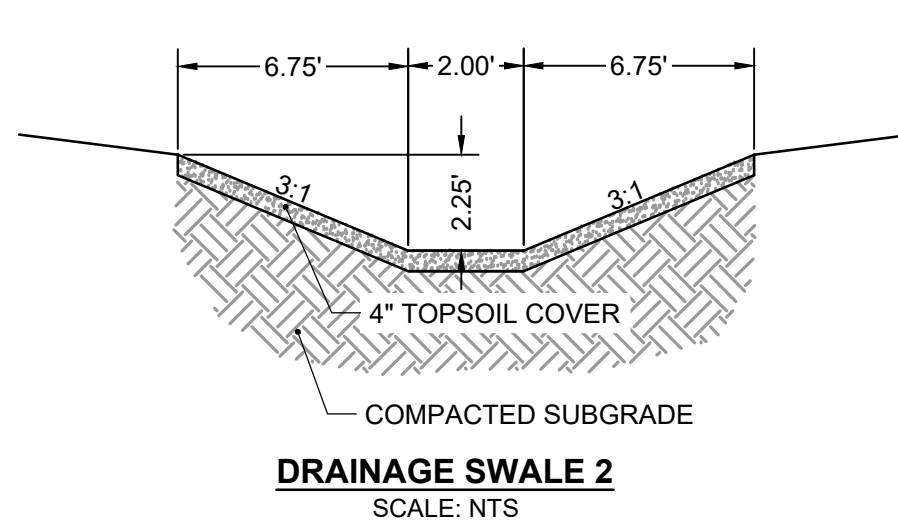
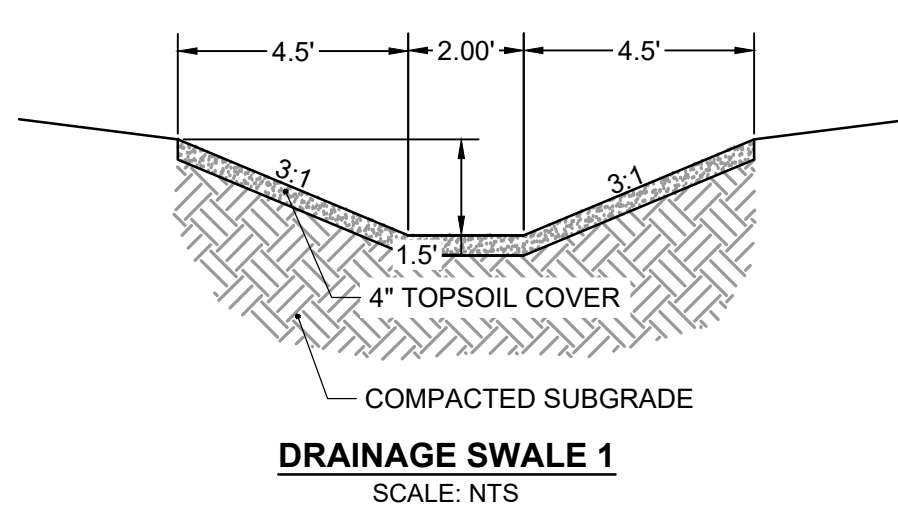
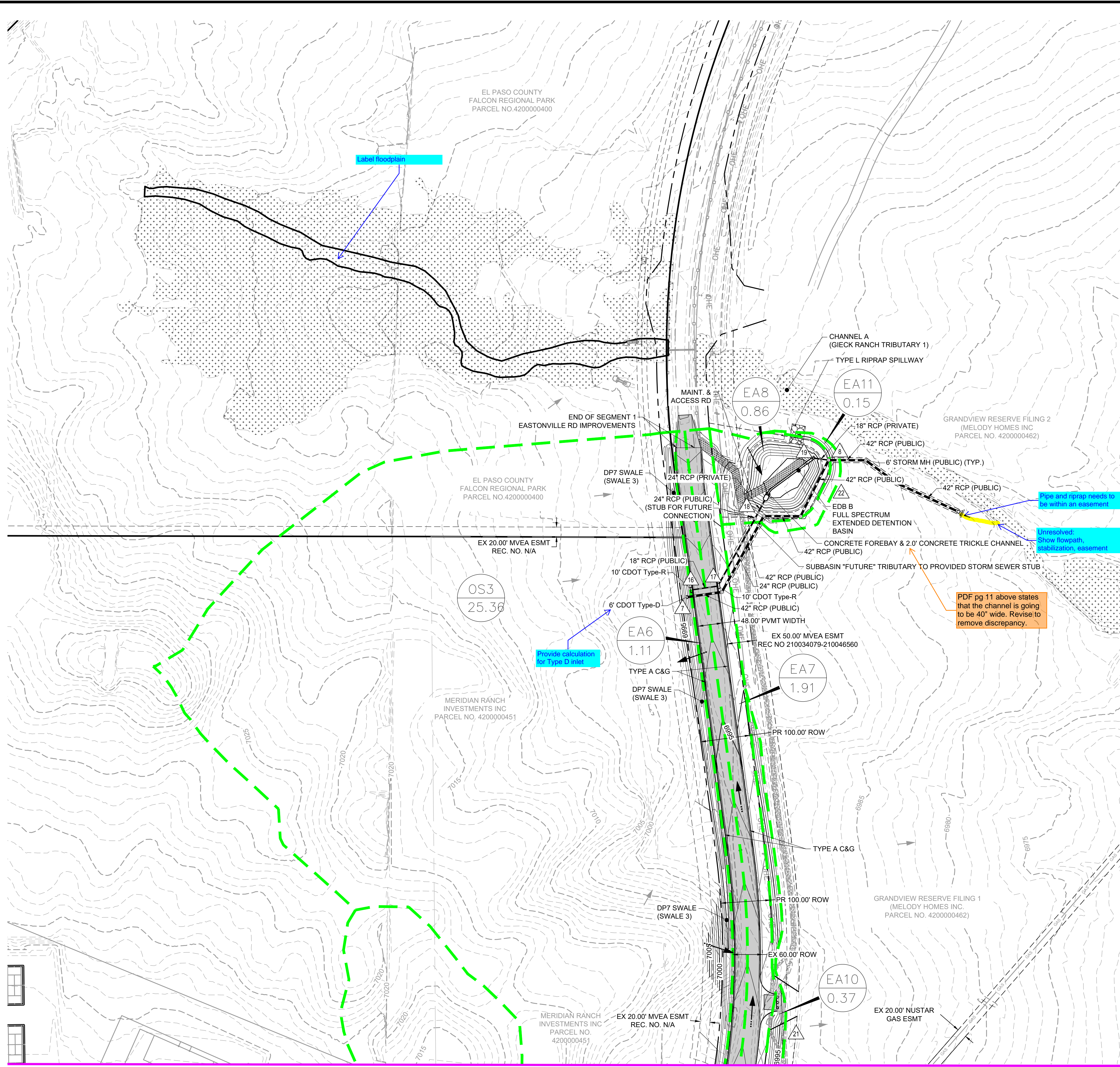
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EASTONVILLE ROAD - SEGMENT 1
 PROPOSED CONDITIONS DRAINAGE MAP



LEGEND:

- PROPOSED MAJOR CONTOUR: Solid line with dots
- PROPOSED MINOR CONTOUR: Dashed line with dots
- EXISTING MAJOR CONTOUR: Solid line
- EXISTING MINOR CONTOUR: Dashed line
- PROPOSED STORM SEWER: Thick solid line
- PROPOSED DRAINAGE SWALE: Thin solid line with arrows
- PROPERTY LINE: Dashed line
- PROPOSED FLOW DIRECTION: Arrow
- EXISTING FLOW DIRECTION: Arrow with crossbar
- PROPOSED DRAINAGE BASIN DESIGN POINT: Triangle with 'X'
- PROPOSED BASIN LABEL: Circle with 'NAME AREA'
- PRELIMINARY 100-YR FLOODPLAIN: Dotted pattern
- WETLANDS: Stippled pattern

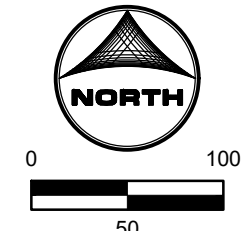
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| 12 | EA13 | 0.1 | 0.5 |
| 13 | EA3 | 2.1 | 3.4 |
| 14 | DP13, EA4 | 3.9 | 6.5 |
| 15 | DP14, EA5 | 4.0 | 6.7 |
| 16 | EA6 | 3.0 | 5.1 |
| 17 | DP16, EA7 | 6.3 | 10.5 |
| 18 | DP17 | 6.3 | 10.5 |
| 19 | DP18, EA8 | 6.6 | 11.1 |
| 18U | DP17, EA8 & EA9 *PER SEGMENT 2 FDR | 15.6 | 26.2 |
| 19U | DP18, EA8 | 15.9 | 26.6 |
| 20 | EA9 | 0.4 | 0.6 |
| 21 | EA10 | 0.2 | 0.3 |
| 22 | EA11 | 0.1 | 0.1 |

Show these DP's on map



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EASTONVILLE ROAD - SEGMENT 1
 PROPOSED CONDITIONS DRAINAGE MAP

SHEET DRN 2