



Eastonville Road – Londonderry Dr. to Rex Rd. Segment 2 Improvements Stationing 47+00.00 – 79+31.62

Final Drainage Report

January 2024 HR Green Project No: 201662.08

Prepared For:

D.R. Horton Contact: Riley Hillen, P.E. 9555 S. Kingston Ct. Englewood, CO 80112

Prepared By:

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See comment letter also.



Engineer's Statement:

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the County for drainage reports and said report is in conformity with the applicable master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.

Colleen Monahan, P.E., LEED AP	Date
State of Colorado No. 56067	
For and on behalf of HR Green Development, LLC	

Owner/Developer's Statement:

I, the developer, have read and will comply with all of the requirements specified in this drainage report and plan.

By:

Authonized Signature

Address: D.R. Horton 9555 S. Kingston Court Englewood, CO

El Paso County Statement

Filed in accordance with the requirements of the Drainage Criteria Manual, Volumes 1 and 2, El Paso County Engineering Criteria Manual and Land Development code, as amended.

Joshua Palmer, P.E.

County Engineer/ECM Administrator

Conditions:

Date

Date



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I. General Purpose, Location and Description

a. Purpose

The purpose of this Final Drainage Report (FDR) for Eastonville Road Segment 2 Improvements is to describe the onsite and offsite drainage patterns, size drainage infrastructure to safely capture and convey developed runoff to water quality and detention facilities, and to safely route detained stormwater to adequate outfalls. This drainage report will detail the improvements of Eastonville Road from Londonderry Dr. to Rex Road.

b. Location

gravel

Eastonville Road from Londonderry Dr. to Rex Road, referred to as 'the site' herein, is an existing 26' wide temporary pavement road in El Paso County, Colorado. The site lies in the existing 60' wide El Paso County Right-of-Way within Sections 21 and 28, Township 12 South, Range 64 West of the 6th Principal Meridian, in El Paso County, State of Colorado.

The site is bound by undeveloped land to the east and west that has historically been used as ranching lands. Falcon Regional Park, which contains ballparks and parking, and Falcon High School also border the site to the west. All lands to the east and west of the site are unplatted. A vicinity map is presented in Appendix A.

c. Description of Property

The site is approximately 0.69 miles (2.17 acres) of existing temporary pavement roadway north of Londonderry Dr. and south of Rex Road. The existing temporary pavement width for the length of the project is 26' wide. There are 4' wide gravel shoulders and native landscaped swales are located on both sides of the roadway. Offsite stormwater is bypassed under the road through a series of existing culverts. See Appendix A for an existing conditions photo.

The existing roadway has slopes ranging from 0.3% up to about 4%. The general topography of the surrounding area is typical of high desert, short prairie grass with gently rolling hillside with slopes ranging from 2% to 4%. The project site drains generally from the west to the east and is tributary to Black Squirrel Creek.

Per a NRCS soil survey, the site is made up of Type A Columbine gravelly sandy loam, Type A Blakeland loamy sand and Type B Stapleton sandy loam. The NRCS soil survey is presented in Appendix A.

Gieck Ranch Tributary #1 (Channel A) is the only drainageway that traverses the site in the west to east direction through an existing culvert under Eastonville Road. The channel is a mapped wetland and a wetland permit will be required for a part of this Eastonville Road improvement project. Channel A is not within a FEMA floodplain.

Gieck Ranch Tributary #2 is located on the north end of the project site and will not be impacted by this project. There are no known irrigation facilities in the area.

Existing utilities include an underground gas line that runs along the east and western sides of Eastonville, an existing raw water line that follows the west side of Eastonville north of Falcon Regional Park, and an existing aboveground electrical line along the western side of Eastonville Road. An existing drainage map with these facilities is presented in Appendix F.



d. Floodplain Statement

Based on FEMA Firm map 08041C0552G December 7, 2018, the site is not located in any FEMA designated floodplain. See FEMA Firm Map in Appendix A. There is a Zone A floodplain north of the site and a Zone AE south of the site, both of which will not be altered with the associated Eastonville Road improvements.

II. Drainage Design Criteria

a. Drainage Criteria

Hydrologic data and calculations were performed using Drainage Criteria Manual Volume 1 of El Paso County (EPCDCM), with County adopted Chapter 6 and Section 3.2.1 of Chapter 13 of the City of Colorado Springs Drainage Criteria Manual (CCSDCM), May 2014 revised January 2021.

Onsite drainage improvements are designed for the 5-year storm (minor event) and 100-year storm (major event) using rainfall values from the NOAA Atlas 14 Point Precipitation Frequency Data Server. Runoff was calculated per CCSDCM Section 6.3.0 - Rational Method. Private, full spectrum pond design was completed using the latest version of Mile High Flood District's (MHFD) UD-Detention per CCSDCM Section 13.3.2.1 – Private, full spectrum Detention. The detention pond allowable release rate will be limited to less than historic rates.

Rainfall Depths per NOAA Atlas 14				
Return Period (yr)	5	100		
1-hr Rainfall Depth (in)	1.21	2.49		

Inlet sizing was performed per the methods described in EPCDCM Section III Chapter 7 – Street Drainage and Storm Water Inlets. Storm sewer sizing was performed per the methods described in EPCDCM Section III Chapter 8 – Storm Drains and Appurtenances.

III. Drainage Basins and Subbasins

a. Major Basin Description

The site is located within the Gieck Ranch Drainage Basin. The site's drainage characteristics were previously studied in the following reports:

- 1. "Gieck Ranch Drainage Basin Planning Study" prepared by Drexel, Barrel & Co, February 2010.
- 2. "Master Development Drainage Plan Meridian Ranch" prepared by Tech Contractors, July 2021.
- 3. "Final Drainage Report for The Sanctuary Filing 1 at Meridian Ranch" by Tech Contractors, August 2022.

Gieck Ranch Drainage Basin is a 22.05 square mile watershed located in El Paso County, Colorado. Gieck Ranch Drainage Basin is tributary to Black Squirrel Creek which drains to the Arkansas River. The majority of the basin is undeveloped and is rolling range land typical of Colorado's semi-arid climates. It should be noted that the Gieck Ranch DBPS has not been approved at the time of this report.

The Meridian Ranch MDDP and The Final Drainage Report for The Sanctuary Filing 1 at Meridian Ranch indicate that the Eastonville Road culvert crossing at the Gieck Ranch Tributary #1, within the project boundary, does not provide enough capacity for the historic flow rates. This culvert will be upgraded as part of this project.



Within the Gieck Ranch Drainage Basin, ranching has historically been the predominant land use, with rolling topography between 2%-4% slopes. Recently urbanization is occurring within the drainage basin, most notably for this project are Meridian Ranch and Latigo Trails Developments. Both are single family residential neighborhoods located upstream to the west and northwest of the Eastonville Segment 1 Improvements project site.

b. Existing Subbasin Description ____ Trails

Eastonville Road Segment 2 (the site) accepts flows from areas to the west and northwest of the site, including portions of Meridian Ranch and Latigo Development. The flows and design points used in the following descriptions are taken from the approved Meridian Ranch MDDP and The Final Drainage Report for The Sanctuary Filing 1 at Meridian Ranch provides the detailed analysis of the pond releases and flows as they outfall from those developments upstream of this Eastonville Road site. For the purpose of this report, full buildout of the Meridian Ranch development was assumed; hence the developed peak flow rates from the "future buildout conditions" for the entirety of Meridian Ranch were used to evaluate the existing conditions below.

Basin EX1 (The Sanctuary Filing 1 FG-38) is 85.16 acres of undeveloped area and temporary pavement area to the crown of Eastonville Road roadway. Stormwater from this basin combines with flows from Latigo Trails South Pond (The Sanctuary Filing 1 G-17) is conveyed overland to DP1 for a total area of 321.5 acres (The Sanctuary Filing 1 G18). Flows at DP1 ($Q_5 = 28.3 \text{ cfs } Q_{100} = 365.2 \text{ cfs}$) are conveyed across Eastonville Road in an existing 24" CMP culvert and discharges to Gieck Ranch Tributary #2 (Channel B). This basin is located upstream of the Eastonville project and is presented here to show where flows go that are upstream of the project site. The Eastonville project will have no impact on this basin.

Basin EX2 (The Sanctuary Filing 1 FG36) is 18.88 acres undeveloped area, parking lot, and temporary pavement to the crown of Eastonville Road roadway. Stormwater from this basin is conveyed overland to DP2 (The Sanctuary Filing 1 FG36). Flows at DP2 ($Q_5 = 1.7$ cfs $Q_{100} = 18.8$ cfs) are conveyed southerly across Rex Road in an existing 24" RCP culvert and discharges to Basin EX3.

Basin EX3 is 51.06 acres of undeveloped area and the Falcon Regional Park ball fields and **temporary pavement** to the crown of Eastonville Road roadway. Stormwater from this basin combines with flows from The Sanctuary Filing 1 Design Point G15 via an existing roadside swale where it then combines with DP2 flows. Flows travel to DP3 for a total area of 131.3 acres (The Sanctuary Filing 1 Design Point G16) where they are conveyed across Eastonville Road in an existing 24" CMP culvert ($Q_5 = 6.1$ cfs $Q_{100} = 112.1$ cfs).

Basin EX4 is 62.87 acres of undeveloped area and temporary pavement to the crown of Eastonville Road roadway. Stormwater from this basin combines with flows from The Sanctuary Filing 1 Design Point G12 (Meridian Ranch Pond G) to Gieck Ranch Tributary #1 and an existing roadside swale to DP 4 for a total area of 832.7 acres (The Sanctuary Filing 1 Design Point G06) ($Q_5 = 22.4$ cfs $Q_{100} = 491$ cfs). Flows at DP4 are conveyed across Eastonville Road in an existing 18" CMP culvert and discharges to Gieck Ranch Tributary #1 (Channel A).

c. Proposed Subbasin Description

Description of Proposed Project

The proposed project includes improvements to Eastonville Road from Londonderry Drive to Rex Road. As described above, the current condition of the existing roadway in this area consists of 26' wide temporary



pavement roadway with 4' wide sand shoulders and weedy swales located on both sides of the roadway. Offsite stormwater is bypassed under the road through a series of existing culverts.

The proposed improvements from Rex Road south to the southern property line of the proposed Grandview Reserve Filing 1 include removal of the 26' wide temporary pavement and replacing the road with a Modified Urban Minor Arterial Roadway Cross-Section consisting of 48' pavement and Type A EPC curb (53' back of curb to back of curb). This includes Basins EA1-EA11.

Refer to the Eastonville Road Segment 1 improvements FDR for subbasin information and calculations south of subbasins EA10 & EA11.

Eastonville Road Basins

Verify all basin flows with hydrology spreadsheet

Basin EA1 is 0.22 acres of proposed roadway (Modified Urban Minor Arterial Roadway Cross-Section). Stormwater ($Q_5 = 0.7$ cfs $Q_{100} = 1.3$ cfs) is conveyed in curb and gutter to DP2. Flows at DP2 are captured in a **5** Type R sump inlet (Public) and piped to Pond A Sand Filter. Basin EA1 will be detained Pond A Sand Filter.

Basin EA2 is 0.25 acres of proposed roadway (Modified Urban Minor Arterial Roadway Cross-Section). Stormwater ($Q_5 = 0.8$ cfs $Q_{100} = 1.5$ cfs) is conveyed in curb and gutter to DP3. Flows at DP3 are captured in a **5**' Type R sump inlet (Public) and piped to Pond A. Basin EA2 will be detained Pond A Sand Filter.

DP8.1? There is no DP9.1 shown on proposed roadway (Modified Urban Minor Arterial Roadway Cross-Section). map or listed in hydrology spreadsheet $_0 = 1.4$ cfs) is conveyed in curb and gutter to DP5. Flows at DP5 are captured in

a 10' Type R sump inlet (Public) and piped to DB9.1. Basin EA3 will not be detained per the Meridian Ranch MDDP as this basin has been over-detained within Meridian Ranch. Include excerpt in appendix from Meridian Ranch MDDP and highlight this

Basin EA4 is 0.17 acres of proposed roadway (Modified Urban Minor Arterial Roadway Cross-Section). Stormwater ($Q_5 = 0.5$ cfs $Q_{100} = 1.1$ cfs) is conveyed in curb and gutter to DP6. Flows at DP6 are captured in a 5' Type R sump inlet (Public) and piped to DP9.1. Basin EA4 will not be detained per the Meridian Ranch MDDP as this basin has been over-detained within Meridian Ranch.

Basin EA5 is 0.16 acres of undeveloped area and includes Pond A Sand Filter. Stormwater ($Q_5 = 0.1$ cfs $Q_{100} = 0.4$ cfs) is flows directly into Pond A Sand Filter.

Should be Pond C Basin EA6 is 0.70 acres of undeveloped area that will be future roadway (Rex Road) once the Grandview Filing 1 development is constructed. Stormwater ($Q_5 = 3.1 \text{ cfs } Q_{100} = 5.5 \text{ cfs}$) is conveyed in a swale to DP10: Temporary Sediment Basin #1 (TSB #1). TSB #1 has been sized for the paved area of the roundabout and the future paved area of Rex Road within Basin EA6. The swale will be removed with the construction of Rex Road curb and gutter. Basin EA6 will be detained in TSB #1.

Basin EA7 is 0.65 acres of undeveloped area that will be future roadway (Rex Road) once the Grandview Filing 1 development is constructed. Stormwater ($Q_5 = 2.5$ cfs $Q_{100} = 4.7$ cfs is conveyed in a swale to DP10: Temporary Sediment Basin #1 (TSB #1). TSB #1 has been sized for the paved area of the roundabout and the future paved area of Rex Road within Basin EA7. The swale will be removed with the construction of Rex Road curb and gutter. Basin EA7 will be detained in TSB #1.

Basin EA8 is 2.08 acres of proposed roadway (Modified Urban Minor Arterial Roadway Cross-Section). Stormwater ($Q_5 = 5.0 \text{ cfs } Q_{100} = 9.0 \text{ cfs}$) is conveyed in curb and gutter to DP14. Flows at DP14 are captured in a 10' Type R sump inlet (Public) and piped to Pond B. Basin EA8 will be detained Pond B Full Spectrum Detention Basin.

Label pond on drainage map



Basin EA9 is 2.99 acres of proposed roadway (Modified Urban Minor Arterial Roadway Cross-Section). Stormwater ($Q_5 = 4.6$ cfs $Q_{100} = 9.5$ cfs) is conveyed in curb and gutter to DP15. Flows at DP15 are captured in a 10' Type R sump inlet (Public) and piped to Pond B. Basin EA9 will be detained Pond B Full Spectrum Detention Basin.

Basin EA10 is 0.12 acres of proposed roadway (Modified Urban Minor Arterial Roadway Cross-Section). Stormwater ($Q_5 = 0.6 \text{ cfs } Q_{100} = 1.1 \text{ cfs}$) is conveyed in curb and gutter to DP16.1 Flows from DP16.1 drain south and captured in a 10 Type R sump inlet (Public) and piped to Pond B. This inlet design is in the Eastonville Road Segment 1 FDR. Basin EA10 will be detained Pond B Full Spectrum Detention Basin which is detailed in the Eastonville Road Segment 1 FDR.

Basin EA11 is 0.19 acres of proposed roadway (Modified Urban Minor Arterial Roadway Cross-Section). Stormwater ($Q_5 = 0.5 \text{ cfs } Q_{100} = 1.0 \text{ cfs}$) is conveyed in curb and gutter to DP17.1. Flows from DP17.1 drain south and captured in a 10^o Type R sump inlet (Public) and piped to Pond B. This inlet design is in the Eastonville Road Segment 1 FDR. Basin EA10 will be detained Pond B Full Spectrum Detention Basin which is detailed in the Eastonville Road Segment 1 FDR.

Offsite Basins

Verify all basin flows with hydrology spreadsheet

Basin OS1 (EX1) is 85.16 acres of undeveloped area. Stormwater from this basin combines with flows from Latigo Trails South Pond (The Sanctuary Filing 1 G-17) is conveyed overland to DP1 (The Sanctuary Filing 1 G18). Flows at DP1 ($Q_5 = 28.3$ cfs $Q_{100} = 365.2$ cfs) are conveyed across Eastonville Road in an existing 24" CMP culvert and discharges to Gieck Ranch Tributary #2 (Channel B). This basin is located upstream of the Eastonville project and is presented here to show where flows go that are upstream of the project site. The Eastonville project will have no impact on this basin.

Basin OS2 is 15.03 acres of undeveloped land and parking area north of Rex Road and contains a portion of Rex Road ($Q_5 = 4.2 \text{ cfs } Q_{100} = 21.6 \text{ cfs}$). Stormwater is conveyed to DP7 and is captured in a proposed 24" RCP culvert and piped south across Rex Road. No development associated with Eastonville Road will occur in Basin OS2.

Basin OS3 is 1.00 acre of undeveloped land ($Q_5 = 0.2$ cfs $Q_{100} = 1.2$ cfs) along the western edge of Eastonville Road. Stormwater is conveyed to DP8 and is captured in a proposed 15" RCP culvert and piped south across Rex Road. No development associated with Eastonville Road will occur in Basin OS3.

Basin OS4 is 9.60 acres of undeveloped land ($Q_5 = 3.8 \text{ cfs } Q_{100} = 17.3 \text{ cfs}$) along the western edge of Eastonville Road. Stormwater is conveyed to DP11 in a roadside swale where it combines with Meridian Ranch DP G15 flows ($Q_5 = 8 \text{ cfs } Q_{100} = 54.0 \text{ cfs}$) before being captured in a proposed 30" RCP culvert and piped to Channel B. The combined flows as it reaches DP11 is $Q_5 = 10.5 \text{ cfs } Q_{100} = 144.5 \text{ cfs}$.

Basin OS5 is 40.26 acres of undeveloped land and Falcon Regional Park ($Q_5 = 13.3$ cfs $Q_{100} = 64.0$ cfs) along the western edge of Eastonville Road. Stormwater is conveyed to DP12 in a roadside swale and is captured in a proposed 48" RCP culvert and piped to Channel B.

Basin OS6 is 60.83 acres of undeveloped land ($Q_5 = 8.9 \text{ cfs } Q_{100} = 60.6 \text{ cfs}$) along the western edge of Eastonville Road. Basin OS6 flows are adapted directly from the approved The Sanctuary Filing 1 FDR. Stormwater is conveyed to DP16 in a roadside swale where it combines with Meridian Ranch DP G12 flows before being conveyed across Eastonville Road in dual 10' x 3.5' RCBC to Channel A. The combined flows at DP16 (EX4) are $Q_5 = 22.4 \text{ cfs } Q_{100} = 491 \text{ cfs}$.



Basins OS2 - OS6, and the unnamed basins that are east of Eastonville Rd all have proposed soil disturbances within them, which all must be accounted for via WQ treatment or an applicable WQ exclusion. So please address this in the respective Basin paragraphs and create new proposed sub-basins as necessary.

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Basin OS7 is future outflow of 11.42 acres of a future stormwater detention pond outflow developed land that will be detained to meet existing conditions ($Q_5 = 3.4$ cfs $Q_{100} = 22.7$ cfs) in the southeast corner of Eastonville Road and Rex Road. From there, stormwater is piped to Channel B.

Drainage Facility Design IV.

a. General Concept

The proposed improvements from Rex Road south to the southern property line of the proposed Grandview Reserve Filing 1 include removal of the 26' wide temporary pavement and replacing the road with a Modified Urban Minor Arterial Roadway Cross-Section consisting of 48' pavement and Type A EPC curb (53' back of curb to back of curb). Inlets will be placed at low points and roundabout entrances. Stormwater from this roadway will be piped to either a full spectrum detention pond, sand filter or temporary sediment basin. All ponds and water quality features will discharge at less than historic rates.

Pond C (Sand Filter)

Clarify if this 0.63ac is the area from this proposed project b. Water Quality & Detention (CDR2321) that is being treated by Pond C, and not the total treatment in the pond (CDR2321 + Grandview areas). And state the minimum reg'd acreage of treatment

Water quality and stormwater detention for Basins EA1, 2, & 5 is provided in Sand Filter Basin C. SFB C is a private, full spectrum sand filter basin within the Grandview Reserve property to be developed in the future. In Pond C, a total of 0.63 acres at 54% composite imperviousness will be detained. The WQCV is 0.009 ac-ft, the EURV is 0.037 ac-ft, and the 100-year detention volume is 0.062 ac-ft. The WQCV, EURV and 100-year storms are released in 12, 41 and 44 hours, respectively. A 10' access and maintenance road is provided to the bottom of the pond to facilitate maintenance of the pond facilities. A 12' emergency overflow spillway is provided that conveys the developed, peak 100-yr flow rate with 1.0' of freeboard south. SFB C outfalls towards the future Channel B improvements at historic runoff rates. Runoff from Pond C will follow historic drainage patterns and not exceed historic flow rates.

Pond B (Full Spectrum Detention Basin)

Refer to the Eastonville Road Segment 1 FDR. \leftarrow

Add a statement about which Segment 2 basins are tributary to this pond: EA8 - EA11.

c. Inspection and Maintenance

After completion of construction and upon the Board of County Commissioners acceptance, it is anticipated that all drainage facilities within the public Right-of-Way are to be owned and maintained by El Paso County.

All private detention ponds are to be owned and maintained by the Grandview Reserve Metropolitan District NO. 2 (DISTRICT), once established, unless an agreement is reached stating otherwise. Maintenance access for all full spectrum detention facilities will be provided from public Right-of-Way. Maintenance access for the drainageways will be provided through the proposed tracts.

Wetlands Mitigation V.

There is an existing wetland in Gieck Ranch Tributary #1 (Channel A). The wetland is contained entirely within the channel and is classified as jurisdictional. A Nationwide Wetland Permit will be applied for due to the disturbed area at the Dawlish Roundabout. Wetlands maintenance will be the responsibility of the DISTRICT.

Per DCMv2 – Chap 4.2, trickle channel should at a minimum provide capacity equal to twice the release capacity at the upstream forebay outlet. Provide these calcs in the drainage report and revise plans as needed.



VI. Four Step Method to Minimize Adverse Impacts of Urbanization

Step 1 – Reducing Runoff Volumes: Low impact development (LID) practices are utilized to reduce runoff at the source. In general, stormwater discharges are routed across pervious areas prior to capture in storm sewer. This practice promotes infiltration and reduces peak runoff rates. The Impervious Reduction Factor (IRF) method was used and is presented in Appendix D.

Step 2 – Treat and slowly release the WQCV: This step utilizes full spectrum water quality and detention to capture the WQCV and slowly release runoff from the site. Onsite full spectrum detention pond provides water quality treatment for the site. The WQCV is released over a period of 12 hours while the EURV is released over a period of 40-44 hours.

Step 3 – Stabilize stream channels: This step establishes practices to stabilize drainageways and provide scour protection at stormwater outfalls. Erosion protection is provided at all concentrated stormwater discharge points in the form of riprap pads.

Step 4 – Consider the need for source controls: No industrial or commercial uses are proposed within this development and therefore no source controls are proposed.

VII. Drainage and Bridge Fees

Gieck Ranch drainage basin has not been established as a fee basin within El Paso County. Therefore, no drainage basin fees are due at time of platting.

VIII. Opinion of Probable Cost

An engineer's opinion of probable cost has been provided below for public and private drainage infrastructure improvements. This includes cost estimates for the public full spectrum sand filter basin C. All required stormwater infrastructure will be installed per El Paso County Requirements.

Public Infrastructure Cost Estimate					
Line Item	Quantity	Unit F	Price	Cost	
[15] Reinforced Concrete Pipe	128	\$45	LF	\$5,760	
18" Reinforced Concrete Pipe	808	\$76	LF	\$61,408	
24" Reinforced Concrete Pipe	161	\$114	LF	\$18,354	
48" Reinforced Concrete Pipe	1678	\$187	LF	\$313,786	
15" CDOT FES	1	\$500	EA	\$500	
24" CDOT FES	2	\$684	EA	\$1,368	
48" CDOT FES	2	\$912	EA	\$1,824	
6' DIA Storm Manhole	12	\$7,734	EA	\$92,808	
10' CDOT Type R Inlet	6	\$6,703	EA	\$40,218	
Rip Rap, d50 size from 6"-24"	2	\$97	Tons	\$194	
3' x 10' Concrete Box Culvert w/ Wingwalls	110	\$400	Tons	\$44,000	
10% Contingency				\$58,022	
TOTAL:				\$638,242	

Quantities & Unit costs should match with FAE estimate



This cost estimate should include the full cost to install the pond (ie: labor), not just the cost of materials, which is what it currently appears to be.

Public SFB C Cost Estimate				
Line Item	Quantity	Unit F	Price	Cost
Rip Rap, d50 size from 6"-24" (Inflow)	1.5	\$97	Tons	\$146
Sand Filter Media	44	\$100	/CY	\$4,400
4" Perforated PVC Underdrain	10	\$10	/LF	\$100
12" ABC Maintenance Access	19	\$40	/CY	\$760
Outlet Structure w/ Orifice Plate	1	\$5,000	EA	\$5,000
Rip Rap, d50 size from 6"-24" (Spillway)	19.5	\$97	Tons	\$1,892
12" RCP Outlet Pipe	150	\$60	/LF	\$9,000
12" RCP FES	1	\$350	EA	\$350
10% Contingency				\$2,165
TOTAL:				\$23,812

IX. Hydraulic Grade Line Analysis

Hydraulic grade line analysis and final pipe sizes will be provided with the following submittal, and calculations provided in Appendix C. All proposed storm sewer will be designed in accordance with El Paso County Drainage Criteria Manuals.

X. Summary

Eastonville Road lies within the Gieck Ranch Drainage Basin. Water quality and detention for the site is provided in full spectrum water quality and detention ponds, sand filters and temporary sediment basins. There is one major drainageway that traverses the site: Gieck Ranch Tributary 1. The water quality and detention features ponds will be maintained by the Grandview Reserve Metropolitan District No. 2 (DISTRICT). All drainage facilities were sized per the El Paso County Drainage Criteria Manuals.

The development of this project will not adversely affect downstream properties. verify

XI. Drawings

Please refer to the appendices for vicinity and drainage basin maps.

XII. References

- 1. City of Colorado Springs Drainage Criteria Manual, May 2014, Revised January 2021.
- 2. Drainage Criteria Manual of El Paso, Colorado, October 2018.
- 3. Urban Storm Drainage Criteria Manual, Urban Drainage Flood Control District, January 2018.
- 4. "Gieck Ranch Drainage Basin Planning Study" prepared by Drexel, Barrel & Co, February 2010.
- 5. "Master Development Drainage Plan Meridian Ranch" prepared by Tech Contractors, July 2021.
- 6. "The Sanctuary Filing 1 at Meridian Ranch" prepared by Tech Contactors, August 2022.



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APPENDIX A – VICINITY MAP, PHOTOS, SOIL MAP, FEMA MAP



Photo - at Londonderry and Eastonville looking north





Natural Resources Conservation Service

USDA

Web Soil Survey National Cooperative Soil Survey



8

19

83

nyarologio con croap						
	1					
Map unit symbol	Map unit name	Rating	Acres in AOI			
	Blakeland loamy sand, 1 to 9 percent slopes	A	10.4			

A

в

Hydrologic Soil Group

Columbine gravelly sandy loam, 0 to 3 percent slopes

Stapleton sandy loam, 3

to 8 percent slopes

Description	

Totals for Area of Interest

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

Percent of AOI

839.5

835.7

1,685.6

0.6%

49.8%

49.6%

100.0%

Rating Options

Aggregation Method: Dominant Condition Component Percent Cutoff: None Specified Tie-break Rule: Higher





Precipitation Frequency Data Server

NOAA Atlas 14, Volume 8, Version 2 Location name: Elbert, Colorado, USA* Latitude: 38.9796°, Longitude: -104.5696° Elevation: 6996 ft** * source: ESRI Maps ** source: USGS



POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Deborah Martin, Sandra Pavlovic, Ishani Roy, Michael St. Laurent, Carl Trypaluk, Dale Unruh, Michael Yekta, Geoffery Bonnin

NOAA, National Weather Service, Silver Spring, Maryland

PF tabular | PF graphical | Maps & aerials

PF tabular

PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches) ¹										
Average recu					recurrence	rence interval (years)				
Duration	1	2	5	10	25	50	100	200	500	1000
5-min	0.239 (0.189-0.303)	0.291 (0.231-0.370)	0.381 (0.301-0.486)	0.461 (0.361-0.589)	0.576 (0.440-0.768)	0.671 (0.499-0.904)	0.770 (0.554-1.06)	0.875 (0.604-1.24)	1.02 (0.678-1.48)	1.14 (0.733-1.67)
10-min	0.350 (0.277-0.444)	0.426 (0.338-0.542)	0.558 (0.441-0.711)	0.674 (0.529-0.863)	0.844 (0.644-1.12)	0.982 (0.731-1.32)	1.13 (0.811-1.56)	1.28 (0.884-1.81)	1.49 (0.992-2.17)	1.66 (1.07-2.44)
15-min	0.426 (0.338-0.541)	0.520 (0.412-0.660)	0.681 (0.537-0.867)	0.823 (0.645-1.05)	1.03 (0.785-1.37)	1.20 (0.891-1.62)	1.37 (0.988-1.90)	1.56 (1.08-2.21)	1.82 (1.21-2.65)	2.03 (1.31-2.98)
30-min	0.608 (0.482-0.771)	0.740 (0.586-0.940)	0.968 (0.764-1.23)	1.17 (0.916-1.49)	1.46 (1.11-1.94)	1.70 (1.26-2.28)	1.94 (1.40-2.68)	2.20 (1.52-3.12)	2.57 (1.71-3.73)	2.86 (1.84-4.19)
60-min	0.775 (0.615-0.984)	0.933 (0.739-1.18)	1.21 (0.956-1.54)	1.46 (1.15-1.87)	1.84 (1.41-2.47)	2.16 (1.61-2.92)	2.49 (1.80-3.45)	2.85 (1.97-4.05)	3.37 (2.24-4.90)	3.78 (2.44-5.54)
2-hr	0.943 (0.754-1.19)	1.12 (0.898-1.42)	1.46 (1.16-1.84)	1.76 (1.39-2.23)	2.22 (1.72-2.97)	2.62 (1.97-3.52)	3.04 (2.21-4.19)	3.50 (2.45-4.95)	4.16 (2.80-6.03)	4.70 (3.06-6.85)
3-hr	1.03 (0.829-1.29)	1.22 (0.978-1.53)	1.57 (1.25-1.97)	1.90 (1.51-2.40)	2.41 (1.88-3.22)	2.86 (2.17-3.84)	3.34 (2.45-4.60)	3.88 (2.73-5.48)	4.66 (3.15-6.74)	5.29 (3.46-7.69)
6-hr	1.20 (0.968-1.48)	1.40 (1.13-1.74)	1.78 (1.44-2.22)	2.16 (1.73-2.70)	2.76 (2.18-3.66)	3.28 (2.52-4.39)	3.86 (2.86-5.29)	4.51 (3.20-6.34)	5.46 (3.73-7.86)	6.24 (4.12-9.01)
12-hr	1.38 (1.13-1.70)	1.61 (1.31-1.98)	2.05 (1.66-2.53)	2.48 (2.00-3.07)	3.15 (2.51-4.15)	3.74 (2.89-4.96)	4.39 (3.28-5.96)	5.12 (3.66-7.13)	6.17 (4.25-8.82)	7.04 (4.69-10.1)
24-hr	1.60 (1.31-1.95)	1.87 (1.54-2.28)	2.38 (1.94-2.91)	2.85 (2.32-3.51)	3.60 (2.88-4.67)	4.24 (3.29-5.56)	4.94 (3.71-6.63)	5.71 (4.12-7.87)	6.82 (4.73-9.66)	7.73 (5.20-11.0)
2-day	1.85 (1.54-2.24)	2.18 (1.80-2.63)	2.76 (2.28-3.34)	3.29 (2.70-4.01)	4.11 (3.30-5.27)	4.80 (3.76-6.22)	5.54 (4.19-7.36)	6.35 (4.62-8.68)	7.50 (5.25-10.5)	8.44 (5.73-11.9)
3-day	2.03 (1.69-2.44)	2.39 (1.98-2.87)	3.02 (2.50-3.64)	3.60 (2.97-4.36)	4.47 (3.60-5.69)	5.20 (4.08-6.70)	5.98 (4.55-7.90)	6.83 (4.99-9.28)	8.03 (5.65-11.2)	9.00 (6.15-12.7)
4-day	2.18 (1.82-2.61)	2.56 (2.13-3.06)	3.22 (2.68-3.87)	3.82 (3.16-4.62)	4.73 (3.83-6.00)	5.49 (4.33-7.04)	6.30 (4.81-8.30)	7.18 (5.26-9.72)	8.43 (5.94-11.7)	9.43 (6.46-13.3)
7-day	2.58 (2.17-3.07)	2.98 (2.50-3.54)	3.68 (3.08-4.39)	4.32 (3.60-5.18)	5.29 (4.30-6.65)	6.09 (4.84-7.76)	6.96 (5.34-9.09)	7.89 (5.82-10.6)	9.21 (6.55-12.8)	10.3 (7.10-14.4)
10-day	2.93 (2.48-3.47)	3.36 (2.84-3.98)	4.13 (3.47-4.90)	4.81 (4.02-5.74)	5.83 (4.76-7.28)	6.68 (5.32-8.45)	7.58 (5.85-9.86)	8.55 (6.34-11.4)	9.92 (7.08-13.7)	11.0 (7.65-15.4)
20-day	3.91 (3.33-4.58)	4.51 (3.84-5.29)	5.52 (4.68-6.50)	6.39 (5.39-7.55)	7.63 (6.25-9.37)	8.62 (6.90-10.8)	9.64 (7.47-12.4)	10.7 (7.98-14.1)	12.2 (8.74-16.6)	13.3 (9.31-18.4)
30-day	4.70 (4.02-5.47)	5.44 (4.65-6.34)	6.65 (5.66-7.78)	7.66 (6.49-9.00)	9.06 (7.44-11.0)	10.1 (8.15-12.5)	11.2 (8.74-14.3)	12.3 (9.24-16.2)	13.8 (9.98-18.7)	15.0 (10.5-20.6)
45-day	5.67 (4.88-6.57)	6.55 (5.63-7.60)	7.97 (6.82-9.27)	9.12 (7.77-10.7)	10.7 (8.79-12.9)	11.9 (9.56-14.5)	13.0 (10.2-16.4)	14.2 (10.6-18.4)	15.6 (11.3-21.0)	16.7 (11.9-23.0)
60-day	6.48 (5.60-7.48)	7.46 (6.43-8.62)	9.01 (7.74-10.4)	10.3 (8.77-11.9)	11.9 (9.82-14.3)	13.1 (10.6-16.0)	14.3 (11.2-18.0)	15.5 (11.7-20.0)	16.9 (12.3-22.6)	18.0 (12.8-24.6)

Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values. Please refer to NOAA Atlas 14 document for more information.

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PF graphical







Average recurrence

interval (years)

> 1 2

5 10

25

50 100

200 500

· 1000

NOAA Atlas 14, Volume 8, Version 2

Created (GMT): Wed Nov 22 20:22:49 2023

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Maps & aerials

Small scale terrain







Large scale aerial

Precipitation Frequency Data Server



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US Department of Commerce National Oceanic and Atmospheric Administration National Weather Service National Water Center 1325 East West Highway Silver Spring, MD 20910 Questions?: <u>HDSC.Questions@noaa.gov</u>

Disclaimer



Eastonville Road Final Drainage Report Project No.: 201662.08

APPENDIX B – HYDROLOGIC CALCULATIONS

$\left + \right $	
HRC	Green

EASTONVILLE ROAD EXISTING CONDITIONS EL PASO COUNTY, CO

	<u>Calc'd by:</u>	СМ
6	<u>Checked by:</u>	СМ
	<u>Date:</u>	2/1/2024

SUMMARY RUNOFF TABLE					
BASIN	AREA (ac)	% IMPERVIOUS	Q ₅ (cfs)	Q ₁₀₀ (cfs)	
G18*	321.53	-	28.3	365.2	
FG36*	18.88	-	1.7	18.8	
G16*	131.26	-	6.1	112.1	
G06*	832.70	-	22.4	491.0	
* AREA AND O TAKEN FROM THE SANCT					

DESIGN POINT SUMMARY TABLE														
DESIGN POINT	CONTRIBUTING BASINS	ΣQ_5 (cfs)	ΣQ_{100} (cfs)											
1	G18*	28.3	365.2											
2	FG36*	1.7	18.8											
3	G16*	6.1	112.1											
4	G06*	22.4	491.0											

* AREA AND Q TAKEN FROM THE SANCTUARY FILING 1 FDR

Basin labels not matching labels on drainage map & in report

Missing Basin EX1 (Sanc Filing 1 FG-38), EX3 & EX4.

	EASTONVIL	LE ROAD							<u>Calc'</u>	d by:		C	СМ				
ברדו ברדו	EXISTING C	ONDITIC	DNS						<u>Chec</u>	ked by:		C	M				
HRGreen	EL PASO COUNT	r y, co							Date: 2/1/2024								
				CO	MPOSI	TE '(C' F.	ACTOR	RS								
		WALKS &	SINGLE						WALKS & DRIVES SINGLE F						CO	MPOSI	ΓE
BASIN	UNDEVELOPED	DRIVES	FAMILY	TOTAL	SOIL	UNE	DEVE	LOPED	WAL	KS & DR	IVES	SINC	GLE FA	MILY	IMPERV	OUSNE	SS & C
BASIN	UNDEVELOPED	DRIVES ACRES	FAMILY	TOTAL	SOIL TYPE	UNE %I	C ₅	C ₁₀₀	WAL	KS & DR C₅	C ₁₀₀	SINC %I	GLE FA	MILY C ₁₀₀	IMPERV %I	OUSNE C ₅	SS & C C ₁₀₀
BASIN EX1 - EX4*	UNDEVELOPED	DRIVES ACRES	FAMILY	TOTAL	SOIL TYPE	UNE %I		C ₁₀₀	WAL %I	KS & DR C ₅	C ₁₀₀	SINC %I	GLE F <i>i</i>	C ₁₀₀	IMPERV %I	OUSNE C ₅	SS & C C ₁₀₀
BASIN EX1 - EX4*		DRIVES ACRES	FAMILY	TOTAL	SOIL TYPE	UNE %I		C ₁₀₀	WAL %I	KS & DR C ₅	C ₁₀₀	SINC %I	GLE F <i>A</i> C ₅		IMPERV	OUSNE C₅	SS & C C ₁₀₀

	EAST	ONVILL	.E ROAD					Calc'd by	/:	СМ			
	EXIS	FING CO	ONDITIO	NS				Checked	by:		СМ		
HRGreen	EL PAS		r y , co					Date:		2/1	/2024		
				TIME O	F CONCE	NTRAT	ION						
BAS	IN DATA	L	OVER	LAND TIM	E (T _i)		TRAV	EL TIME ('	Γ _t)		TOTAL		
DESIGNATION	C ₅	AREA (ac)	LENGTH (ft)	SLOPE %	t _i (min)	C _V	LENGTH (ft)	SLOPE %	V (ft/s)	t _t (min)	t _c (min)		
EX1-EX4*													
* FLOWS TO THE AREAS EX1 - EX4	SE DESIGN	N POINTS WE	ERE TAKEN FR	OM "THE SA	NCTUARY FI	LING 1 FDR	" SO TC WAS N	IOT CALCUL	ATED FOR (CONTRIBL	JTING		

$$t_i = \frac{0.395(1.1 - C_5)\sqrt{L}}{S^{0.33}} \qquad V = C_v S_w^{0.5}$$

Table 6-7. Conveyance Coefficient, C_{ν}

Type of Land Surface	C_{ν}
Heavy meadow	2.5
Tillage/field	5
Riprap (not buried)*	6.5
Short pasture and lawns	7
Nearly bare ground	10
Grassed waterway	15
Paved areas and shallow paved swales	20

^{*}For buried riprap, select C_v value based on type of vegetative cover.



EASTONVILLE ROAD Calc'd by: EXISTING CONDITIONS Checked by: DESIGN STORM: 5-YEAR Date:

																_							
				DI	RECT	RUNOF	F		т	OTAL	RUNG	OFF	S	TREE	T		PIF	PE		TR	RAVEL	TIME	
STREET	DESIGN POINT	BASIN ID	AREA (ac)	C5	t _c (min)	C₅*A (ac)	/ (in./ hr.)	Q (cfs)	t _c (min)	C₅*A (ac)	/ (in./ hr.)	Q (cfs)	Q _{street} (cfs)	C ₅ *A (ac)	SLOPE %	Q _{PIPE} (cfs)	C₅*A (ac)	SLOPE %	PIPE SIZE (in)	LENGTH (FT)	VEL. (FPS)	TRAVEL TIME (min	
	1	G18*	321.53									28.3											
	2	FG36*	18.88									17											
	2	1000	10.00									1.7											
	3	G16*	131.26									6.1											BASIN EX2, DP2 &
	4	G06*	832.70									22.4											BASIN EX4 & DPG12 (SA
		N N																					



СМ	
СМ	
2/1/2024	

REMARKS

DP 1 CAPTURED IN GIECK RANCH TRIB #2 (CHANNEL B)

DP 2 CAPTURED IN 24" RCP CULVERT, PIPED TO BASIN EX3

& DPG15 (SANCTUARY FDR Q5=3 CFS) CAPTURED IN 24" CMP CULVERT, PIPED ACROSS EASTONVILLE ROAD

ANCTUARY FDR Q5 = 21 CFS) CAPTURED IN 18" CMP CULVERT, PIPED ACROSS EASTONVILLE ROAD TO GIECK RANCH TRIB #1 (CHANNEL A)

* AREA AND Q TAKEN FROM THE SANCTUARY FILING 1 FDR



EASTONVILLE ROAD Calc'd by: EXISTING CONDITIONS Checked by: DESIGN STORM: 100-YEAR Date:

				DI	RECT	RUNOF	F		тс	TAL I	RUNO	FF	S	TREE	ET		PI	PE		TR	AVEL	TIME	
STREET	DESIGN POINT	BASIN ID	AREA (ac)	C100	t _c (min)	C ₁₀₀ *A (ac)	/ (in./ hr.)	Q (cfs)	t _c (min)	C ₁₀₀ *A (ac)	/ (in./ hr.)	Q (cfs)	Q _{street} (cfs)	C ₁₀₀ *A (ac)	SLOPE %	Q _{PIPE} (cfs)	C ₁₀₀ *A (ac)	SLOPE %	PIPE SIZE (ft)	LENGTH (ft)	VEL. (ft/s)	TRAVEL TIME (min)	
	1	G18*	321.53									365.2											
	2	FG36*	18.88									18.8											
	3	G16*	131.26									112.1											BASIN EX2, DP2
	4	G06*	832.70									491.0											BASIN EX4 & DPG12 (S
																						1	

СМ	
СМ	
2/1/2024	

REMARKS

DP 1 CAPTURED IN GIECK RANCH TRIB #2 (CHANNEL B)

DP 2 CAPTURED IN 24" RCP CULVERT, PIPED TO BASIN EX3

& DPG15 (SANCTUARY FDR Q5=3 CFS) CAPTURED IN 24" CMP CULVERT, PIPED ACROSS EASTONVILLE ROAD

SANCTUARY FDR Q5 = 21 CFS) CAPTURED IN 18" CMP CULVERT, PIPED ACROSS EASTONVILLE ROAD TO GIECK RANCH TRIB #1 (CHANNEL A)

* AREA AND Q TAKEN FROM THE SANCTUARY FILING 1 FDR

HRGreen

EASTONVILLE ROAD SEG 2 PROPOSED CONDITIONS

SPC <u>Calc'd by:</u> СМ Checked by: EL PASO COUNTY, CO 2/2/2024 Date:

SUMMARY RUNOFF TABLE														
BASIN	AREA (ac)	% IMPERVIOUS	Q ₅ (cfs)	Q ₁₀₀ (cfs)										
EA1	0.22	73	0.8	1.5										
EA2	0.25	72	0.9	1.7										
EA3	0.20	70	0.7	1.3										
EA4	0.17	65	0.5	1.1										
EA5	0.16	0	0.1	0.4										
EA6	0.70	100	3.2	5.3										
EA7	0.65	89	2.6	4.8										
EA8	2.08	99	5.2	8.8										
EA9	2.99	63	5.0	10.4										
EA10	0.16	75	0.6	1.1										
EA11	0.15	67	0.5	1.0										
*G18	321.53	-	28.3	365.2										
*FG36	18.88	-	1.7	18.8										
OS3	1.00	2	0.3	2.2										
OS4	9.60	9	4.8	21.6										
*G16	131.26	-	6.1	112.1										
*G06	832.70	-	22.4	491.0										
OS7	11.42	2	3.6	24.4										

* AREA AND Q TAKEN FROM THE SANCTUARY FILING 1 FDR

See comments on drainage map for summary tables. Tables shown here should match tables shown on maps.

DESIGN POINT SUMMARY TABLE													
DESIGN POINT	CONTRIBUTING BASINS	ΣQ_5 (cfs)	ΣQ_{100} (cfs)										
1	G18	28.3	365.2										
2	FG36	1.7	18.8										
2.1	EA1	0.8	1.5										
3	G16	6.1	112.1										
3.1	EA2, DP2.1	1.6	3.2										
4	G06	22.4	491.0										
4.1	EA5, DP3.1	1.7	3.4										
5	EA3	0.7	1.3										
6	DP5, EA4	1.2	2.4										
6.1	DP6, DP8	2.9	22.4										
7	OS3	0.3	2.2										
8	DP2, DP7	2.0	21.0										
9	DP6.1	2.9	22.4										
10	EA6, EA7	5.6	9.9										
11	OS4, DP9	7.5	44.0										
12	OS7	3.6	24.4										
13	DP2, DP12	26.0	515.3										
14	EA8	5.2	8.8										
15	EA9	5.0	10.4										
15.1	DP14, DP15	10.2	19.1										
16.1	EA10	0.6	1.1										
17.1	EA11	0.5	1.0										

Pr_Drainage_Calcs3

RBM 2/2/2024 10:36 AM

	EASTONVILLE ROAD SEG 2	<u>Calc'd by:</u>	SPC
	PROPOSED CONDITIONS	Checked by:	СМ
HRGreen	EL PASO COUNTY, CO	Date:	11/27/2023

SOIL TYPE: HSG A&B

	COMPOSITE 'C' FACTORS																							
							LAN	D USE	TYPE															
		Paved		Histori Greent	ic Flow Aı belts, Agı	nalysis iculture		Lawns	;	Land	Use Und	defined	Land	Use Un	defined		C							
	%I	C ₅	C ₁₀₀	%I	C ₅	C ₁₀₀	%I	C ₅	C ₁₀₀	%I	C ₅	C ₁₀₀	%I	C ₅	C ₁₀₀		IMPER	VIOUSNE	:55 & C					
	100	0.90	0.96	2	0.09	0.36	0	0.08	0.35	0	0.00	0.00	0	0.00	0.00	TOTAL		FACTOR						
BASIN		ACRES	5		ACRES	5	ACRES				ACRES	•		ACRES	5	ACRES	%	C ₅	C ₁₀₀					
EA1		0.16						0.06								0.22	73	0.68	0.79					
EA2		0.18						0.07								0.25	72	0.67	0.79					
EA3		0.14						0.06								0.20	70	0.65	0.78					
EA4		0.11						0.06								0.17	65	0.61	0.74					
EA5		0.00						0.16								0.16	0	0.08	0.35					
EA6		0.70						0.00								0.70	100	0.90	0.96					
EA7		0.58						0.07								0.65	89	0.81	0.89					
EA8		2.06						0.02								2.08	99	0.89	0.95					
EA9		1.88						1.11								2.99	63	0.60	0.73					
EA10		0.12						0.04								0.16	75	0.70	0.81					
EA11		0.10						0.05								0.15	67	0.63	0.76					
G18																321.53								
FG36																18.88								
OS3					1.00											1.00	2	0.09	0.36					
OS4		0.70			8.90											9.60	9	0.15	0.40					
G16																131.26								
G06																832.70								
OS7					11.42											11.42	2	0.09	0.36					
Pond A		0.34			0.00			0.29								0.63	54	0.52	0.68					

	EAST	ONVILI		Calc'd b	y:	ę	SPC						
	PROP	OSED (CONDITI	ONS				Checked	by:		СМ		
HRGreen	EL PAS		гү, со					Date:		2/2	2/2/2024		
TIME OF CONCENTRATION													
BAS	BASIN DATAOVERLAND TIME (T_i) TRAVEL TIME (T_t)										TOTAL		
DESIGNATION	C ₅	AREA (ac)	LENGTH (ft)	SLOPE %	t _i (min)	C _V	LENGTH (ft)	SLOPE %	V (ft/s)	t _t (min)	t _c (min)		
EA1	0.68	0.22	34	2.0	3.6	20	137	1.4	2.4	1.0	5.0		
EA2	0.67	0.25	34	2.0	3.6	20	60	1.4	2.4	0.4	5.0		
EA3	0.65	0.20	34	2.0	3.8	20	126	1.4	2.4	0.9	5.0		
EA4	0.61	0.17	34	2.0	4.2	20	126	3.8	3.9	0.5	5.0		
EA5	0.08	0.16	20	2.0	6.6	20	20	33.0	11.5	0.0	6.7		
EA6	0.90	0.70	26	2.0	1.5	20	630	1.7	2.6	4.0	5.5		
EA7	0.81	0.65	24	2.0	2.1	20	630	1.7	2.6	4.0	6.1		
EA8	0.89	2.08	26	2.0	1.5	20	2500	0.7	1.7	24.9	26.4		
EA9	0.60	2.99	26	2.0	3.7	20	2500	0.7	1.7	24.9	28.6		
EA10	0.70	0.16	26	2.0	3.0	20	157	0.6	1.5	1.7	5.0		
EA11	0.63	0.15	26	2.0	3.5	20	157	0.6	1.5	1.7	5.2		
G18													
FG36													
OS3	0.09	1.00	220	2.1	21.4	10	345	2.3	1.5	3.8	25.2		
OS4	0.15	9.60	153	3.1	14.8	10	1124	2.5	1.6	11.8	26.6		
G16	1												
G06	· ·												
OS7	0.09	11.42	200	11.6	11.6	10	675	3.4	1.8	6.1	17.7		

FORMULAS:

$$t_i = \frac{0.395(1.1 - C_5)\sqrt{L}}{S^{0.33}} \qquad V = C_v S_w^{0.5}$$

Table 6-7. Conveyance Coefficient, C_{ν}

Type of Land Surface	C_{ν}
Heavy meadow	2.5
Tillage/field	5
Riprap (not buried)*	6.5
Short pasture and lawns	7
Nearly bare ground	10
Grassed waterway	15
Paved areas and shallow paved swales	20

* For buried riprap, select C_v value based on type of vegetative cover.

	EAST	ONVILL	E ROAD		Calc'd by	y :	SPC					
	PROP	OSED C	ONDITI		Checked	by:	СМ					
HRGreen	EL PASO COUNTY, CO								Date:			
				TIME OF	CONCE	NTRATI	ON					
BAS	BASIN DATA OVERLAND TIME (T _i)							EL TIME (T_t		TOTAL	
DESIGNATION	C ₅	AREA (ac)	A (ac) LENGTH (ft) SLOPE % t _i (min) C _V LENGTH (ft) SLOPE % V								t _c (min)	



EASTONVILLE ROAD SEG 2 PROPOSED CONDITIONS DESIGN STORM: 5-YEAR

Checked by:

Date:

<u>Calc'd by:</u>

				DI	RECT	RUNO	FF		Т	OTAL	RUN	OFF	S	TREE	T		PIF	РЕ		TRAVEL TIME			
STREET	DESIGN POINT	BASIN ID	AREA (ac)	C.	t _c (min)	C ₅ *A (ac)	/ (in./ hr.)	Q (cfs)	t _c (min)	C ₅ *A (ac)	/ (in./ hr.)	Q (cfs)	Q _{street} (cfs)	C ₅ *A (ac)	SLOPE %	Q _{PIPE} (cfs)	C₅*A (ac)	SLOPE %	PIPE SIZE (ft)	LENGTH (FT)	VEL. (FPS)	TRAVEL TIME (min	
	1	010	004 50									28.3											
	2	G18	321.53					28.3				1.7											
	0.4	FG36	18.88					1.7	- 	0.45	5 47	0.0				0.0	0.45	1.0	4.5	50	5.0	0.40	
	2.1	EA1	0.22	0.68	5.0	0.15	5.17	0.8	5.0	0.15	5.17	0.8				0.8	0.15	1.0	1.5	56	5.9	0.16	
	3											6.1											
	31	G16						6.1	5.0	0.32	5 17	1.6				16	0.32	51	1.5	34	13.4	0.04	
	0.1	EA2	0.25	0.67	5.0	0.17	5.17	0.9	0.0	0.02	0.17	1.0				1.0	0.02	0.1	1.0	04	10.4	0.04	
	4	C 06						22.4				22.4											
	4.1	606						22.4	6.7	0.33	5.17	1.7											
		EA5	0.16	0.08	6.7	0.01	4.74	0.1	5.0	0.40	5 47					0.7	0.40	0.5	1.0	10	07	0.04	
	5	EA3	0.20	0.65	5.0	0.13	5.17	0.7	5.0	0.13	5.17	0.7				0.7	0.13	0.5	1.3	48	3.7	0.21	
	6								5.2	0.23	5.11	1.2				1.2	0.23	2.4	1.3	43	8.1	0.09	
	61	EA4	0.17	0.61	5.0	0.10	5.17	0.5	13.2	0.32	2 3 71	2.0				2.0	0.32	1.0	2.0	61	7.2	0.14	
hy are there	2 0.1								13.2	0.52	5.71	2.5				2.3	0.52	1.0	2.0	01	1.2	0.14	
55 Dasins :	7		1.00	0.00	40.4	0.00	0.70	0.0	13.1	0.09	3.72	0.3				0.3	0.09	0.8	2.0	43	6.4	0.11	
	8	053	1.00	0.09	13.1	0.09	3.72	0.3	13.1	0.09	3.72	2.0				2.0	0.09	1.5	1.3	38	6.4	0.10	
		OS3	1.00	0.09	13.1	0.09	3.72	0.3															
	9								13.2	0.32	3.71	2.9	2.9	0.32	2.1					615	2.9	3.56	
	10								6.1	1.16	6 4.88	5.6											
		EA6	0.70	0.90	5.5	0.63	5.02	3.2			_												
		EA7	0.65	0.81	6.1	0.53	4.88	2.6															
	11	004	0.00	0.45	47.4	4 40	0.00	4.0	17.1	1.76	3.32	7.5	7.5	1.76	0.5					530	1.4	6.25	BASIN OS4
	12	054	9.60	0.15	17.1	1.43	3.32	4.8	14.9	1.03	3.53	3.6				3.6	1.03	1.0	1.5	28	5.9	0.08	
		OS7	11.42	0.09	14.9	1.03	3.53	3.6															
	13								14.9	1.03	3 3.53	26.0											
	14								24.0	1.86	6 2.81	5.2				5.2	1.86	7.0	1.5	8	15.7	0.01	
	15	EA8	2.08	0.89	24.0	1.86	2.81	5.2	24.0	1 70	2 2 91	5.0				5.0	1 79	1 0	15	54	7.0	0.11	
	15	EA9	2.99	0.60	24.0	1.78	2.81	5.0	24.0	1.70	2.01	5.0				5.0	1.70	1.0	1.5	54	7.9	0.11	
	15.1								24.1	3.64	2.81	10.2											СС
	16.4								5.0	0.14	E 47												BASIN EA10 CONVEYE
	16.1	EA10	0.40	0.70	EO	0.11	E 47	0.0	5.0	0.11	5.17	0.6											
	17 1	EATU	0.16	0.70	5.0	0.11	5.17	0.6	5.2	0.00	5 11	0.5											BASIN EA11 CONVEYE
	17.1		0.15	0.62	5.0	0.00	5 1 1	0.5	5.2	0.08	5.11	0.5											
		CALL	0.10	0.03	5.2	0.09	0.11	0.0															

Missing Basins OS1, OS2, OS5 & OS6

Missing Design Points 8.1 & 13.1

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REMARKS

BASIN EA1 CAPTURED IN 5' TYPE R INLET @ DP2, PIPE TO DP3.1

BASIN EA2 CAPTURED IN 5' TYPE R INLET@ DP3, PIPE TO DP3.1

COMBINED DP2.1 & DP3.1 @ DP3.1, PIPE TO DP4 (POND A)

BASIN EA3 CAPTURED IN 5' TYPE R INLET @ DP5, PIPE TO DP6.1

BASIN EA4 CAPTURED IN 5' TYPE R INLET @ DP6, PIPE TO DP6.1

DP6 & DP8 FLOW @ DP6.1, PIPE TO DP9

BASIN OS3 CAPTURED IN 15" FES, PIPE TO DP8

DP2 & DP7 FLOW @ DP8, PIPE TO DP9

DP6.1 @ DP9, DISCHARGE TO ROADSIDE SWALE TO DP11

BASIN EA6 & EA7 @ DP10 (TEMPORARY SEDIMENT BASIN #1)

, DP9.1 CAPTURED & MERIDIAN RANCH DPG15 (3 CFS) IN 30" FES @ DP11, SWALE TO DP3

BASIN OS7 CAPTURED @ DP12 IN TYPE C INLET, PIPE TO DP13

COMBINED DP3 & DP12, PIPE TO CHANNEL B

BASIN EA8 CAPTURED IN 10' TYPE R SUMP @ DP14, PIPE TO DP15.1

BASIN EA8 CAPTURED IN 10' TYPE R SUMP @ DP15, PIPE TO DP15.1

MBINED DP14 & DP15, PIPE TO DP18 OF THE EASTONVILLE ROAD SEGMENT 1 FDR

ED VIA CURB & GUTTER TO 10' TYPE R INLET. INLET DESIGN IS PROVIDED IN THE EASTONVILLE ROAD SEGMENT 1 FDR

ED VIA CURB & GUTTER TO 10' TYPE R INLET. INLET DESIGN IS PROVIDED IN THE EASTONVILLE ROAD SEGMENT 1 FDR



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| DESIGN POINT | BASIN ID | AREA (ac)
C ₁₀₀ | t _c (min) | C ₁₀₀ *A (ac)

 | / (in./ hr.)
 | Q (cfs) | t _c (min) | C ₁₀₀ *A (ac) | / (in./ hr.) | Q (cfs) | Q _{street} (cfs)
 | C ₁₀₀ *A (ac) | SLOPE % | Q _{PIPE} (cfs) | C ₁₀₀ *A (ac) | SLOPE %
 | PIPE SIZE (ft) | LENGTH (ft) | VEL. (ft/s) | TRAVEL TIME (mir |
 |
| 1 | G18 | | |

 |
 | 365.2 | | | | 365.2 |
 | | | | |
 | | | | |
 |
| 2 | EC26 | | |

 |
 | 10.0 | | | | 18.8 |
 | | | | |
 | | | | |
 |
| 2.1 | FG30 | | |

 |
 | 10.0 | 5.0 | 0.17 | 8.68 | 1.5 |
 | | | 1.5 | 0.17 | 1.0
 | 1.5 | 56 | 5.9 | 0.16 | BASIN EA1 CAPTURED IN 5' TYPE R INLET @ DP2, PIPE TO DP3.1
 |
| 3 | EA1 | 0.22 0.79 | 5.0 | 0.1

 | / 8.68
 | 5 1.5 | | | | 112.1 |
 | | | 112.1 | 0.00 | 5.1
 | 1.5 | 34 | 13.4 | 0.04 |
 |
| 3.1 | G16 | | |

 |
 | 112.1 | 5.0 | 0.37 | 8.66 | 3.2 |
 | | | | |
 | | | | | BASIN EA2 CAPTURED IN 5' TYPE R INLET@ DP3, PIPE TO DP3.1
 |
| 4 | EA2 | 0.25 0.79 | 5.0 | 0.20

 | 0 8.68
 | 8 1.7 | | | | 491.0 |
 | | | 491.0 | 0.00 | 0.5
 | 1.3 | 48 | 3.7 | 0.21 |
 |
| 4.1 | G06 | | |

 |
 | 491.0 | 6.7 | 0.43 | 7.95 | 3.4 |
 | | | 3.4 | 0.43 | 2.4
 | 1.3 | 43 | 8.1 | 0.09 | COMBINED DP2.1 & DP3.1 @ DP3.1, PIPE TO DP4 (POND A)
 |
| 5 | EA5 | 0.16 0.35 | 6.7 | 7 0.00

 | 6 7.95
 | 0.4 | 5.0 | 0.16 | 8.68 | 1.3 |
 | | | 1.3 | 0.16 | 1.0
 | 2.0 | 61 | 7.2 | 0.14 | BASIN EA3 CAPTURED IN 5' TYPE R INLET @ DP5, PIPE TO DP6.1
 |
| 6 | EA3 | 0.20 0.78 | 5.0 | 0.10

 | 6 8.68
 | 8 1.3 | 51 | 0.28 | 8 61 | 2.4 |
 | | | 24 | 0.28 | 0.8
 | 2.0 | 43 | 64 | 0.11 | BASIN EA4 CAPTURED IN 5' TYPE R INLET @ DP6. PIPE TO DP6.1
 |
| 6.1 | EA4 | 0.17 0.74 | 5.0 | 0.13

 | 3 8.68
 | 1.1 | 16.7 | 0.64 | 5.64 | |
 | | | 22.4 | 0.64 | 1.5
 | 1.0 | 20 | 6.1 | 0.10 |
 |
| 0.1 | | | |

 |
 | | 10.7 | 0.04 | 5.64 | 22.4 |
 | | | 22.4 | 0.04 | 1.5
 | 1.3 | 30 | 0.4 | 0.10 |
 |
| / | OS3 | 1.00 0.36 | 13.1 | 0.3

 | 6 6.24
 | 2.2 | 13.1 | 0.36 | 6.24 | 2.2 |
 | | | 2.2 | 0.36 | 1.0
 | 2.0 | 56 | 7.2 | 0.13 | BASIN OS3 CAPTURED IN 15" FES, PIPE TO DP8
 |
| 8 | OS3 | 1.00 0.36 | 13.1 | 0.30

 | 6 6.24
 | 2.2 | 13.1 | 0.36 | 6.24 | 21.0 | 21.0
 | 0.36 | 2.1 | | |
 | | 615 | 2.9 | 3.56 | DP2 & DP7 FLOW @ DP8, PIPE TO DP9
 |
| 9 | | | |

 |
 | | 16.8 | 0.64 | 5.63 | 22.4 |
 | | | | |
 | | | | | DP6.1 @ DP9, DISCHARGE TO ROADSIDE SWALE TO DP11
 |
| 10 | EA6 | 0.70 0.90 | 5.5 | 0.6

 | 3 8.43
 | 5.3 | 6.1 | 1.21 | 8.19 | 9.9 |
 | | | | |
 | | | | | BASIN EA6 & EA7 @ DP10 (TEMPORARY SEDIMENT BASIN #1)
 |
| | EA7 | 0.65 0.80 | 6.1 | 0.5

 | 8 8 10
 | 18 | | | | | 0.0
 | 0.00 | 0.5 | | |
 | | 530 | 1.4 | 6.25 |
 |
| 11 | | 0.00 0.00 | 17.4 | 0.00

 |
 | , 4.0 | 17.1 | 4.52 | 5.58 | 44.0 |
 | | | 44.0 | 4.52 | 1.0
 | 4.0 | 1500 | 11.4 | 2.19 | BASIN OS4, DP9.1 CAPTURED & MERIDIAN RANCH DPG15 (3 CFS) IN 30" FES @ DP11, SWALE TO DP3
 |
| 12 | 004 | 9.00 0.40 | | 3.00

 |
 | 04.4 | 14.9 | 4.11 | 5.93 | 24.4 |
 | | | 24.4 | 4.11 | 1.0
 | 1.5 | 28 | 5.9 | 0.08 | BASIN OS7 CAPTURED @ DP12 IN TYPE C INLET, PIPE TO DP13
 |
| 13 | 057 | 11.42 0.36 | 14.9 | 9 4.1

 | 1 5.93
 | 3 24.4 | 14.9 | 4.11 | 5.92 | 515.3 |
 | | | | |
 | | | | | COMBINED DP3 & DP12, PIPE TO CHANNEL B
 |
| 14 | | | |

 |
 | | 24.0 | 1.86 | 4.72 | 8.8 |
 | | | 8.8 | 1.86 | 7.0
 | 1.5 | 8 | 15.7 | 0.01 | BASIN EA8 CAPTURED IN 10' TYPE R SUMP @ DP14, PIPE TO DP15.1
 |
| 15 | EA8 | 2.08 0.89 | 24.0 | 1.80

 | 6 4.72
 | 2 8.8 | 24.0 | 2.19 | 4.72 | 10.4 |
 | | | 10.4 | 2.19 | 1.8
 | 1.5 | 54 | 7.9 | 0.11 | BASIN EA8 CAPTURED IN 10' TYPE R SUMP @ DP15, PIPE TO DP15.1
 |
| 15.1 | EA9 | 2.99 0.73 | 24.0 | 2.19

 | 9 4.72
 | 2 10.4 | 24.1 | 4.05 | 4.71 | 19.1 |
 | | | | |
 | | | | + | COMBINED DP14 & DP15, PIPE TO DP18 OF THE EASTONVILLE ROAD SEGMENT 1 FDR
 |
| 16.1 | | | |

 |
 | | 5.0 | 0.13 | 8.68 | 1.1 |
 | | | | | <u> </u>
 | | | | | BASIN EA10 CONVEYED VIA CURB & GUTTER TO 10' TYPE R INLET. INLET DESIGN IS PROVIDED IN THE EASTONVILLE ROAD
 |
| | EA10 | 0.16 0.81 | 5.0 | 0.13

 | <mark>3</mark> 8.68
 | 1.1 | 0.0 | 5.10 | 5.00 | |
 | | | | |
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 |
| 17.1 | | 0.45 | E |

 | 1 0 50
 | | 5.2 | 0.11 | 8.58 | 1.0 |
 | | | | |
 | | | | | BASIN EA11 CONVEYED VIA CURB & GUTTER TO 10' TYPE R INLET. INLET DESIGN IS PROVIDED IN THE EASTONVILLE ROAD
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See comments on previous sheet



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APPENDIX C – HYDRAULIC CALCULATIONS

Provide design calculations for all proposed swales & ditches

Provide design calculations for riprap outlet protection at end of all culverts

Provide design calculations for culverts and storm systems

Provide analysis of any existing culverts that remain Including DP1 calculations for existing and needed culvert size







Design Information (Input)			MINOR	MAJOR	
Type of Inlet	CDOT Type R Curb Opening	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to o	ontinuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or 0	Curb Opening)	No =	1	1	
Water Depth at Flowline (outside	of local depression)	Ponding Depth =	5.9	7.3	inches
Grate Information		-	MINOR	MAJOR	Coverride Depths
Length of a Unit Grate		$L_{o}(G) =$	N/A	N/A	feet
Width of a Unit Grate		W _o =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grat	e (typical value 0.50 - 0.70)	$C_{f}(G) =$	N/A	N/A	
Grate Weir Coefficient (typical va	lue 2.15 - 3.60)	C_w (G) =	N/A	N/A	
Grate Orifice Coefficient (typical	value 0.60 - 0.80)	$C_o(G) =$	N/A	N/A	
Curb Opening Information			MINOR	MAJOR	_
Length of a Unit Curb Opening		$L_{o}(C) =$	5.00	5.00	feet
Height of Vertical Curb Opening	in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in I	inches	H _{throat} =	6.00	6.00	inches
Angle of Throat (see USDCM Figu	ure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (t	ypically the gutter width of 2 feet)	W _p =	2.00	2.00	feet
Clogging Factor for a Single Curb	Opening (typical value 0.10)	$C_{f}(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (t	ypical value 2.3-3.7)	$C_{w}(C) =$	3.60	3.60	
Curb Opening Orifice Coefficient	(typical value 0.60 - 0.70)	$C_{o}(C) =$	0.67	0.67	
		-			-
Low Head Performance Reduce	tion (Calculated)	_	MINOR	MAJOR	_
Depth for Grate Midwidth		d _{Grate} =	N/A	N/A	ft
Depth for Curb Opening Weir Eq	uation	d _{Curb} =	0.32	0.44	ft
Combination Inlet Performance F	Reduction Factor for Long Inlets	RF _{Combination} =	0.75	0.93	
Curb Opening Performance Redu	ction Factor for Long Inlets	RF _{Curb} =	1.00	1.00	
Grated Inlet Performance Reduct	ion Factor for Long Inlets	RF _{Grate} =	N/A	N/A	
		-			
		_	MINOR	MAJOR	_
Total Inlet Interception Capacity	(assumes clogged condition)	Q _a =	5.1	8.1	cfs
Inlet Canacity IS GOOD for M	linor and Major Storms(>O PEAK)	$Q_{PEAK PEOLITRED} =$	0.8	1.5	cfs







Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =			
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =			inches
Number of Unit Inlets (Grate or Curb Opening)	No =			
Water Depth at Flowline (outside of local depression)	Ponding Depth =			inches
Grate Information		MINOR	MAJOR	Override Depths
Length of a Unit Grate	$L_{0}(G) =$			feet
Width of a Unit Grate	W _o =			feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =			
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_{f}(G) =$			
Grate Weir Coefficient (typical value 2.15 - 3.60)	C_w (G) =			
Grate Orifice Coefficient (typical value 0.60 - 0.80)	$C_{0}(G) =$			
Curb Opening Information		MINOR	MAJOR	
Length of a Unit Curb Opening	$L_{o}(C) =$			feet
Height of Vertical Curb Opening in Inches	H _{vert} =			inches
Height of Curb Orifice Throat in Inches	H _{throat} =			inches
Angle of Throat (see USDCM Figure ST-5)	Theta =			degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W _p =			feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_{f}(C) =$			
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$			
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_{o}(C) =$			
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d _{Curb} =	N/A	N/A	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	N/A	N/A	
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	N/A	N/A	
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A	
		MINOP	MATOR	
Total Inlet Interception Capacity (assumes clogged condition)	0 =	PILINOK	INAUCK	cfs
rour meet merception capacity (assumes clogged condition)	$Q_{PEAK REQUIRED} =$			cfs







Design Information (Input)			MINOR	MAJOR	
Type of Inlet	CDOT Type R Curb Opening	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to o	ontinuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or 0	Curb Opening)	No =	1	1	
Water Depth at Flowline (outside	of local depression)	Ponding Depth =	5.9	7.3	inches
Grate Information		-	MINOR	MAJOR	C Override Depths
Length of a Unit Grate		$L_{o}(G) =$	N/A	N/A	feet
Width of a Unit Grate		W _o =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grat	e (typical value 0.50 - 0.70)	$C_{f}(G) =$	N/A	N/A	
Grate Weir Coefficient (typical va	lue 2.15 - 3.60)	C_w (G) =	N/A	N/A	
Grate Orifice Coefficient (typical	value 0.60 - 0.80)	$C_o(G) =$	N/A	N/A	
Curb Opening Information			MINOR	MAJOR	_
Length of a Unit Curb Opening		$L_{o}(C) =$	5.00	5.00	feet
Height of Vertical Curb Opening	in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in I	inches	H _{throat} =	6.00	6.00	inches
Angle of Throat (see USDCM Figu	ure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (t	ypically the gutter width of 2 feet)	W _p =	2.00	2.00	feet
Clogging Factor for a Single Curb	Opening (typical value 0.10)	$C_{f}(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (t	ypical value 2.3-3.7)	$C_w(C) =$	3.60	3.60	
Curb Opening Orifice Coefficient	(typical value 0.60 - 0.70)	$C_{o}(C) =$	0.67	0.67	
		-			-
Low Head Performance Reduce	tion (Calculated)	_	MINOR	MAJOR	_
Depth for Grate Midwidth		d _{Grate} =	N/A	N/A	ft
Depth for Curb Opening Weir Equ	uation	d _{Curb} =	0.32	0.44	ft
Combination Inlet Performance F	Reduction Factor for Long Inlets	RF _{Combination} =	0.75	0.93	
Curb Opening Performance Redu	ction Factor for Long Inlets	$RF_{Curb} =$	1.00	1.00	
Grated Inlet Performance Reduct	ion Factor for Long Inlets	RF _{Grate} =	N/A	N/A	
		-			
		_	MINOR	MAJOR	_
Total Inlet Interception Capacity	(assumes clogged condition)	Q _a =	5.1	8.1	cfs
Inlet Canacity IS GOOD for N	linor and Major Storms(>O PEAK)	$Q_{PEAK PEOLITRED} =$	0.7	1.4	cfs







Design Information (Input)		MINOR	MAJOR				
Type of Inlet	Type =	CDOT Type R	Curb Opening				
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches			
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1			n in the second s	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	3.5	3.5	inches			
Grate Information		MINOR	MAJOR	C Override De	pths	n in the second s	
Length of a Unit Grate	$L_{o}(G) =$	N/A	N/A	feet		n in the second s	
Width of a Unit Grate	W _o =	N/A	N/A	feet		n in the second s	
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A			n in the second s	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_{f}(G) =$	N/A	N/A				
Grate Weir Coefficient (typical value 2.15 - 3.60)	$C_{w}(G) =$	N/A	N/A			n in the second s	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	$C_o(G) =$	N/A	N/A			n in the second s	
Curb Opening Information		MINOR	MAJOR	_		n in the second s	
Length of a Unit Curb Opening	$L_{o}(C) =$	5.00	5.00	feet			
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches		n in the second s	
Height of Curb Orifice Throat in Inches	H _{throat} =	6.00	6.00	inches		n in the second s	
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees		n in the second s	
Side Width for Depression Pan (typically the gutter width of 2 feet)	W _p =	2.00	2.00	feet		n in the second s	
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_{f}(C) =$	0.10	0.10			n in the second s	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$	3.60	3.60			n in the second s	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_{o}(C) =$	0.67	0.67			1	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR			1	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	ft			
Depth for Curb Opening Weir Equation	d _{Curb} =	0.13	0.13	ft		n in the second s	
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	0.45	0.45			n in the second s	
Curb Opening Performance Reduction Factor for Long Inlets	$RF_{Curb} =$	0.99	0.99				
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A] [Per h	ydrology	/
		MINOR	MAJOR	5	prea	dsheet.	DP
Total Inlet Interception Capacity (assumes clogged condition)	Q _a =	1.2	1.2	Cfs /	2400		4
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	0.5	1.1 🧲	efs	J 100	01 2.4 C	JS.
					ntorc	ention c	ana
					merc	option c	ape

6 has acity is not adequate at this inlet







Design Information (Input)	-	MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	2	2	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	5.9	7.8	inches
Grate Information		MINOR	MAJOR	Override Depths
Length of a Unit Grate	$L_{o}(G) =$	N/A	N/A	feet
Width of a Unit Grate	W _o =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_{f}(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	$C_{w}(G) =$	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	$C_{0}(G) =$	N/A	N/A	
Curb Opening Information		MINOR	MAJOR	_
Length of a Unit Curb Opening	$L_o(C) =$	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H _{throat} =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W _p =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_{w}(C) =$	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_{o}(C) =$	0.67	0.67	
	-			-
Low Head Performance Reduction (Calculated)	_	MINOR	MAJOR	_
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d _{Curb} =	0.32	0.48	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	0.55	0.73	
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	0.93	1.00	
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A	
	-			_
		MINOR	MAJOR	
Total Inlet Interception Capacity (assumes clogged condition)	Q _a =	9.9	18.6	cfs
Inlet Canacity IS GOOD for Minor and Major Storms(>O PEAK)	$Q_{PEAK REQUIRED} =$	5.0	9.0	cfs







Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	2	2	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	5.9	7.8	inches
Grate Information		MINOR	MAJOR	Override Depths
Length of a Unit Grate	$L_{o}(G) =$	N/A	N/A	feet
Width of a Unit Grate	W _o =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_{f}(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	$C_{w}(G) =$	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	$C_o(G) =$	N/A	N/A	
Curb Opening Information		MINOR	MAJOR	_
Length of a Unit Curb Opening	$L_{o}(C) =$	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H _{throat} =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	$W_p =$	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_o(C) =$	0.67	0.67	
	-			-
Low Head Performance Reduction (Calculated)	_	MINOR	MAJOR	_
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d _{Curb} =	0.32	0.48	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	0.55	0.73	
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	0.93	1.00	
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A	
				_
	_	MINOR	MAJOR	_
Total Inlet Interception Capacity (assumes clogged condition)	Q _a =	9.9	18.6	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>O PEAK)	$Q_{PEAK REQUIRED} =$	4.6	9.5	cfs



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APPENDIX D – WATER QUALITY & DETENTION

Also provide for Pond E (PPRTA)

UDBMP (Vertion 307, March 2018) Sheet 1 of 1 Designer: SPC Company: IH & Green Date: Jamash 30, 2024 Project: Eactorville Road - Segment 2 Improvements < add: "SFB C" Location: El Pase County, CO 1 Basin Storage Volume A) Storage Indeptionance of Tobary Area, I. (100%) If all paved and roded areas upstream of and Titler; I, I = 54.0 "%. B) Tobary Area's Improvionances Rate (i = 1/100) I = 0.540 C) Water Outling (MCCV) Besign Outline WCCV = 0.177 vestersheel inches Vacco:		Design Procedu	ure Form: Sand Filter (SF)	
Unsigning in the Green Date: January 30, 2024 Project: Exaction: EI Pase County, CO 1. Basis Storage Volume A) Effective imperioduanes at thotary Asa, I. (1005 if all exact and code areas upstraam of state filter) 9) Trobusy Areas imperioduanes state (1 = 1/100) C) Water Oxality Capture Volume (VOCV) Design Volume Veccore 27.455 seq.1 B) Contributing Waterhed Area (NOCV) Design Volume Vaccore Vaccore 27.455 seq.1 F) For Vatershed Xe (NOCV) Design Volume Vaccore Vaccore 1. B) Sand The Side Stopes (Volume (NOCV) Design Volume Vaccore Vaccore 0. Video Value (NOCV) Design Volume Vaccore Video Value (NOCV) Design Volum	Decimary	UD-BMP (Ve	/ersion 3.07, March 2018)	Sheet 1 of 2
Determined Industry 30, 2024 Project: Eastonville Road-Segment 2 Improvements add: "SFB C" Location: IF Back Scarps Volume I. = 54.0 Al. Effective Improvements of Tribuary Area, I., (100%: # all saved and coded areas upstream of sand tiler) I. = 54.0 By Tribuary Area is imperviourness of Tribuary Area, I., (100%: # all saved and coded areas upstream of sand tiler) I. = 54.0 By Tribuary Area is imperviourness of Tribuary Area, I., (100%: # all saved and coded areas upstream of sand tiler) WCCV = 0.17 By Tribuary Area is imperviourness of Tribuary Area, I., (100%: # all saved and coded areas upstream of sand tiler) WCCV = 0.17 D) Contribuing Watershot Area (including sand filter and) H. = 54.0 F) For Watershota Outside of the Deriver Region. WCCV = 0.17 Water Outsity Capture Volume (VOCV) Design Volume Wcccv = 0.00 (i) Port Watershota Outside of the Deriver Region. Weccv = 0.01 Water Outsity Capture Volume (VOCV) Design Volume Veccv = 0.01 (i) Water Outsity Capture Volume (VOCV) Design Volume Veccv = 0.01 (i) Water Outsity Capture Volume (VOCV) Design Volume Veccv = 0.01 (ii) Water Outsity Capture Volume (VOCV) Design Volume Veccv = 0.01 (iii) Water Provided User (The Eristals Blance Area) Deriver Regio	Company:			
Project: Bastownite Road - Segment 2 Improvements (add: "SFB C") Leaterin: El Prace County, CO 1. Basin Storage Volume	Date:	January 30, 2024		
Lotation: El Pleas County, CO 1. Basin Storage Volume A Effective Imperviousness of Tributary Area, I, (100°): fl all pavel and coded areas spatients of and filee) 19. Tributary Areas Imperviousness Ratio (1 = 1/100) I = 0.540 (100°: fl all pavel and coded areas spatients of and filee) III: = 0.540 (100°: fl all pavel and coded areas spatients of and filee) III: = 0.540 (1): Water Could Cyclure Volume (WCCV) Based to 12-four Drain Time WCCV = 0.17 Water Could's County Cyclure Volume (WCCV) Bases to 12-four Drain Time WCCV = 0.17 (1): Water Could's County Cyclure Volume (WCCV) Design Volume WCCV = 0.17 Input a value since the site is outside of the Deriver Region. (1): Water Could's County Cyclure Volume (WCCV) Design Volume WCCV = 0.17 Input a value since the site is outside of the Deriver Region. (1): Water Could's County Volume (WCCV) Design Volume (Chy if a different WCCV) Design Volume (Chy if a different Medical Diverse Area) D _{NCOV} = 1.0 III (2): Mater Could Cyclure Volume (WCCV) Design Volume (Chy if a different MCCV) Design Volume (Chy if a different Medical Diverse Area) D _{NCOV} = 1.0 III (2): Mater Area (2): Storage Your Volume (WCCV) Design Volume (Chy if a different Medical Diverse Area) D _{NCOV} = 1.0 IIII (2): Volume Provi	Project:	Eastonville Road - Segment 2 Improvements	add: "SFB C"	
1. Basin Storage Volume A) Effective Imperviousness of Tributary Ares I, (100% if all paved and rooted areas upstream of sand filter) I = 540 % 8) Tributary Area Imperviousness Ratio (= 1/100) I = 0540 % C) Water Quality Capture Volume (WQCV) Based on 12-hour Drain Time WQCV = 0:17 mattershed inches WQCV = 0:17 mattershed inches VICU = 0:000 (VI = 12 + 0.0 % h) I = 0540 % WQCV = 0:17 mattershed inches D) Contributing Watershead Area (including sand filter area) I = 0.0 % I = 0.0 % E) Water Quality Capture Volume (WQCV) Design Volume Vaccov = 10 % I = 0.0 % I = 0.0 % Vaccov = 100 filt Vaccov = 0.0 % I = 0.0 % I = 0.0 % O) For Watershead Studied of the Derver Region, Water Volume (WQCV) Design Volume Vaccov = 0.0 % Vaccov = 0.0 % I = 0.0 % I) For Watershead Studied of the Derver Region, Water Volume (WQCV) Design Volume Vaccov = 0.0 % Vaccov = 0.0 % I = 0.0 % I) Water Quality Capture Volume (WQCV) Design Volume Vaccov = 1.0 % Vaccov = 0.0 % I = 0.0 % I) Water Mater Volume (WQCV) Design Volume Vaccov = 1.0 % Vaccov = 0.0 % I = 0.0 % I) Water Mater Volume (WQCV) Design Volume Vaccov = 1.0 % I = 0.0 % I = 0.0 % I) Water Outer (WQCV) Design Volume Vaccov = 1.0 % I = 0.0 % I = 0.0 % I =	Location:	El Paso County, CO		
1: Basin Storage Volume <pre></pre>				
A) Effective imperiodusces of Tributary Area, I, (100% if all paved areas upstream of sand filter) I, I, I, Status, Yaev, Simparviouness Rato (I = 1/100) B) Tributary Area Imperviouness Rato (I = 1/100) I, I = 0.540 C) Water Quality Capture Volume (WQCV) Design volume VOCV = 0.17 watershed inches WGCV = 0.17 watershed inches D) Contributing Watershed Area (including sand filter area) Area = 27.443 as ft Wincov = 308 out if splut a value since the value value since the value value since the splut avalue value va	1. Basin Stor	rage Volume		
B) Tributary Area's Imperviousness Ratio (i = 1/100) i = 0.540 C) Water Cuality Capture Volume (WCCV) Based on 12-hour Drain Time WCVCV = 0.17 vestenhed inches WCVC = 0.17 vestenhed inches D) Cortributy Water Cuality Capture Volume (WCV) Design Volume VocCV = 0.17 vestenhed inches WCVC = 0.17 vestenhed inches E) Water Cuality Capture Volume (WCV) Design Volume VocCV = 0.17 vestenhed inches WCV = 0.17 vestenhed inches F) For Watersheds Outside of the Derver Region, Depth of Average R word VocCV = 0.17 vestenhed inches VecCV = 0.17 vestenhed inches G) For Watersheds Outside of the Derver Region, Depth of Average R word VocCV Design Volume VecCV = 0.17 vestenhed inches H) User Input of Vater Cuality Capture Volume (WCV) Design Volume VecCV = 0.17 vestenhed inches H) User Input of Vater Cuality Capture Volume (WCV) Design Volume VeccV = 0.17 vestenhed inches H) User Input of Vater Cuality Capture Volume (WCV) Design Volume VeccV = 0.17 vestenhed inches J) Word V Depth VeccV = 0.17 vestenhed inches VeccV = 0.17 vestenhed inches A) WOCV Depth VeccV Design Volume VeccV = 0.17 vestenhed inches B) Sand Filter Xea (Hat States Area) VeccV = 0.17 vestenhed inches VeccV = 0.17 vestenhed inches J) Mountum Filter Area (Hat States Area) VeccV = 1.0 ft Z = 4.00 ft / ft J) Word V Depth VeccV = 1.0 f	A) Effectiv (100%	ve Imperviousness of Tributary Area, I _a if all paved and roofed areas upstream of sand filter)	$I_a = 54.0\%$	
C) Mater Outing Capture Volume (WOCV) Based on 12-hour Drain Time WOCV = 0.17 watershed inches WOCV = $0.8 + (0.91^{-1} + 1.19^{-1} + 0.08^{-1})$ Area = 27.443 sq ft D) Contributing Watershed Area (including stand filter area) Area = 27.443 sq ft E) Water Outing (Copture Volume (WOCV) Design Volume Volume Volume) FOR Watersheds Outside of the Deriver Region, Depth of Average R WOTV / 12 * Area Area = 27.443 sq ft F) For Watersheds Outside of the Deriver Region, Depth of Average R WOTP Outing (WOCV) Design Volume (WOCV) Desi	B) Tributa	ary Area's Imperviousness Ratio (i = $I_a/100$)	i = 0.540	
D) Contributing Watershed Area (including sand filter area) $Area = 27.443$ sq ft E) Water Quality Capture Volume (WQCV) Design Volume $V_{mocv} = 388$ ou ft P) For Watersheds Outside of the Derver Region. Depth of Average Runolf Producing Storm $V_{mocv} = 100$ ou ft G) For Watersheds Outside of the Derver Region. $V_{mocv} = 0$ ou ft H) User Input of Water Outsity Capture Volume (WQCV) Design Volume $V_{wazov=0} = 0$ ou ft H) User Input of Water Outsity Capture Volume (WQCV) Design Volume $V_{wazov=0} = 0$ ou ft J) Word Voludity Capture Volume (WQCV) Design Volume $V_{wazov=0} = 0$ ou ft J) Word Voludity Capture Volume (WQCV) Design Volume $V_{wazov=0} = 0$ ou ft J) Word Voludity Capture Volume (WQCV) Design Volume $V_{wazov=0} = 0$ ou ft J) Word Voludity Capture Volume (WQCV) Design Volume $V_{wazov=0} = 0$ ou ft J) Word Volume Volume VOLUME (WQCV) Design Volume $V_{wazov=0} = 0$ ou ft J) Word Volume Volume (WQCV) Design Volume $V_{wazov=0} = 0$ ou ft J) Word Volume Volume (WQCV) Design Volume $V_{wazov=0} = 0$ ou ft J) Word Volume IN Material $P_{wazov=0} = 0$ of ft J) Around Filter Area $A_{was=0} = 0$ of ft J) Around Filter Area $A_{was=0} = 0$ of ft J) Around Finderdains System $A_{was=0} $	C) Water WQC	Quality Capture Volume (WQCV) Based on 12-hour Drain Time $CV=0.8 * (0.91* i^3 - 1.19 * i^2 + 0.78 * i)$	WQCV = 0.17 watershed inches	
E) Water Outlik Capture Volume (WQCV) Design Volume Vmocy = 1000 mm states and states	D) Contril	buting Watershed Area (including sand filter area)	Area = 27,443 sq ft	
F) For Watersheds Outside of the Deriver Region, Depth of Average Runoff Producing Storm ds =	E) Water V _{wqc}	Quality Capture Volume (WQCV) Design Volume	V _{wqcv} = <u>398</u> cu ft Input a value since the site is outside of the	
G) For Watershelds Outside of the Denver Region. Water Quality Capture Volume (WQCV) Design Volume Vwdcvores = ou ft H) User Input of Water Quality Capture Volume (WQCV) Design Volume Vwdcvores = ou ft 2. Basin Geometry A) WQCV Depth B) Sand Filter Side Slopes (Horizontal distance per unit vertical, 4:1 or flatter preferred). Use '0' if sand filter has vertical walls. Z =	F) For Wa Avera	atersheds Outside of the Denver Region, Depth of ge Runoff Producing Storm	d ₆ = in Denver region.	
H) User Input of Water Quality Capture Volume (WQCV) Design Volume (QOV) design Volume is desired) $V_{VOCV USER} = $ $cu ft$ 2. Basin Geometry A) WQCV Depth $D_{WQCV} = 1.0$ ft $D_{WQCV} = 1.0$ ft B) Sand Filter Side Slopes (Horizontal distance per unit vertical, 4:1 or flatter preferred). Use '0' if sand filter has vertical wals. $D_{WQCV} = 1.0$ ft $Z = 4.00$ ft / ft C) Minimum Filter Area (Flat Surface Area) $A_{total} = 185$ sq ft $A_{total} = 200$ sq ft D) Actual Filter Area $A_{total} = 200$ sq ft $V_T = 4288$ cu ft 3. Filter Material $O O O O O O O O O O O O O O O O O O O $	G) For W Water	/atersheds Outside of the Denver Region, r Quality Capture Volume (WQCV) Design Volume	V _{WQCV OTHER} =cu ft	
2. Basin Geometry $D_{WOCV} = 1.0$ A) WQCV Depth $D_{WOCV} = 1.0$ B) Sand Filter Side Slopes (Horizontal distance per unit vertical, 4:1 of fatter preferred). Use '0' if sand filter has vertical walls. $Z = 4.00$ C) Minimum Filter Area (Flat Surface Area) $A_{Mn} = 185$ sq ftD) Actual Filter Area $A_{Actual} = 200$ sq ftE) Volume Provided $V_T = 4288$ cu ft3. Filter MaterialChoose One $I \otimes 18^\circ$ CDOT Class B or C Filter Material O Other (Explain):4. Underdrain System A) Are underdrains provided? $V = 2.0$ B) Underdrain system orifice diameter for 12 hour drain time Volume to Drain in 12 Hours $V = 2.0$ i) Dotance Form Lowest Elevation of the Storage Volume to Drain in 12 Hours $V = 398$ ii) Orflice Diameter, 3/8' Minimum $V = 398$ iii) Orflice Diameter, 3/8' Minimum $D_0 = 7/16$	H) User I (Only if	nput of Water Quality Capture Volume (WQCV) Design Volume f a different WQCV Design Volume is desired)	V _{WQCV USER} =cu ft	
A) WQCV Depth $D_{wacv} = 1.0$ ft B) Sand Filter Side Slopes (Horizontal distance per unit vertical, 4:1 or flatter preferred). Use "0" if sand filter has vertical walls. $Z = 4.00$ ft / ft C) Minimum Filter Area (Flat Surface Area) $A_{oftrat} = 185$ sq ft $A_{oftrat} = 200$ sq ft D) Actual Filter Area $A_{oftrat} = 200$ sq ft $V_T = 4228$ ou ft 3. Filter Material $V_T = 4228$ ou ft $V_T = 4228$ ou ft 4. Underdrain System A Are underdrains provided? B Orborse One B) Underdrain system onfice diameter for 12 hour drain time $Y = 2.0$ ft No i) Distance From Lowest Elevation of the Storage Volume to Drain in 12 Hours $V_{01_{1/2}} = 398$ ou ft $V_{01_{1/2}} = 398$ ou ft ii) Volume to Drain in 12 Hours $V_{01_{1/2}} = 398$ ou ft $D_{0} = 7/16$ in	2. Basin Geo	ometry		
B) Sand Filter Side Slopes (Horizontal distance per unit vertical, 4:1 or flatter preferred). Use "0" if sand filter has vertical walls. $Z = 4.00$ ft / ft C) Minimum Filter Area (Flat Surface Area) $A_{Min} = 185$ sq ft D) Actual Filter Area $A_{Actual} = 200$ sq ft E) Volume Provided $V_T = 4288$ cu ft 3. Filter Material Choose One I 3" CDOT Class B or C Filter Material Other (Explain): 4. Underdrain System A) Are underdrains provided? B) Underdrain system orifice diameter for 12 hour drain time I Choose One I 10" NO i) Distance From Lowest Elevation of the Storage Volume to the Center of the Orifice $y = 2.0$ ft ii) Volume to Drain in 12 Hours Volt12 = 398 cu ft iii) Orfice Diameter, 38" Minimum $D_0 = 7/16$ in	A) WQCV	/ Depth	$D_{WQCV} = 1.0$ ft	
C) Minimum Filter Area (Flat Surface Area) $A_{Min} = 185$ sq ftD) Actual Filter Area $A_{Actual} = 200$ sq ftE) Volume Provided $V_T = 4288$ cu ft3. Filter MaterialChoose One 	B) Sand F 4:1 or f	Filter Side Slopes (Horizontal distance per unit vertical, flatter preferred). Use "0" if sand filter has vertical walls.	Z = 4.00 ft / ft	
D) Actual Filter Area $A_{Actual} = 200$ sq ftE) Volume Provided $V_T = 4288$ cu ft3. Filter MaterialChoose One 	C) Minimu	um Filter Area (Flat Surface Area)	A _{Min} = <u>185</u> sq ft	
E) Volume Provided $V_T = 4228$ cu ft 3. Filter Material Choose One ③ 18" CDOT Class B or C Filter Material Other (Explain): ④ 14" CDOT Class B or C Filter Material Other (Explain): 4. Underdrain System Choose One A) Are underdrains provided? $Other (Explain)$: B) Underdrain system orifice diameter for 12 hour drain time $V r = 398$ i) Distance From Lowest Elevation of the Storage $y = 2.0$ Volume to the Center of the Orifice $Vol_{12} = 398$ ii) Volume to Drain in 12 Hours $D_0 = 7/16$ iii) Orifice Diameter, 3/8" Minimum $D_0 = 7/16$	D) Actual	Filter Area	A _{Actual} = 200 sq ft	
3. Filter Material Choose One (a) Is " CDOT Class B or C Filter Material Other (Explain): (b) Other (Explain): Choose One (c) Other (Explain): (c) Other (Explain): (c) Other (Explain): (c) Other	E) Volume	e Provided	$V_T = 4288$ cu ft	
4. Underdrain System A) Are underdrains provided? B) Underdrain system orifice diameter for 12 hour drain time i) Distance From Lowest Elevation of the Storage Volume to the Center of the Orifice ii) Volume to Drain in 12 Hours iii) Orifice Diameter, 3/8" Minimum	3. Filter Mate	erial	Choose One	
4. Underdrain System A) Are underdrains provided? B) Underdrain system orifice diameter for 12 hour drain time i) Distance From Lowest Elevation of the Storage Volume to the Center of the Orifice ii) Volume to Drain in 12 Hours iii) Orifice Diameter, 3/8" Minimum				
4. Underdrain SystemA) Are underdrains provided?B) Underdrain system orifice diameter for 12 hour drain timei) Distance From Lowest Elevation of the Storage Volume to the Center of the Orificeii) Volume to Drain in 12 Hoursiii) Orifice Diameter, 3/8" Minimum			Outer (Explain):	
4. Underdrain System A) Are underdrains provided? B) Underdrain system orifice diameter for 12 hour drain time i) Distance From Lowest Elevation of the Storage Volume to the Center of the Orifice ii) Volume to Drain in 12 Hours Vol12 = 398 cu ft Do = 7/16				
 4. Underdrain System A) Are underdrains provided? B) Underdrain system orifice diameter for 12 hour drain time i) Distance From Lowest Elevation of the Storage Volume to the Center of the Orifice ii) Volume to Drain in 12 Hours iii) Orifice Diameter, 3/8" Minimum 				
A) Are underdrains provided? \bigcirc YES \bigcirc NO B) Underdrain system orifice diameter for 12 hour drain time \bigcirc NO i) Distance From Lowest Elevation of the Storage Volume to the Center of the Orifice $y = 2.0$ ft $Vol_{12} = 398$ cu ft $D_0 = 7/16$ in	4. Underdrai	in System	Choose One	
B) Underdrain system orifice diameter for 12 hour drain time \bigcirc NO i) Distance From Lowest Elevation of the Storage $y = 2.0$ ft volume to the Center of the Orifice $\forall ol_{12} = 398$ cu ft iii) Orifice Diameter, 3/8" Minimum $D_0 = 7/16$ in	A) Are und	derdrains provided?	() YES	
B) Underdrain system or file diameter for 12 hour drain time $y = 2.0$ ft i) Distance From Lowest Elevation of the Storage $y = 2.0$ ft volume to the Center of the Orifice $Vol_{12} = 398$ cu ft ii) Orifice Diameter, 3/8" Minimum $D_0 = 7/16$ in			◯ NO	
i) Distance From Lowest Elevation of the Storage Volume to the Center of the Orifice $y = 2.0$ ftii) Volume to Drain in 12 Hours $Vol_{12} = 398$ cu ftiii) Orifice Diameter, 3/8" Minimum $D_0 = 7/16$ in	B) Underd	arain system orifice diameter for 12 hour drain time		
ii) Volume to Drain in 12 Hours $Vol_{12} = 398$ cu ftiii) Orifice Diameter, 3/8" Minimum $D_0 = 7/16$ in		 i) Distance From Lowest Elevation of the Storage Volume to the Center of the Orifice 	y = 2.0 ft	
iii) Orifice Diameter, 3/8" Minimum $D_0 = 7/16$ in		ii) Volume to Drain in 12 Hours	Vol ₁₂ = <u>398</u> cu ft	
		iii) Orifice Diameter, 3/8" Minimum	$D_0 = \boxed{7/16}$ in	

Shown as 0.47" on MHFD-Detention calcs below. Revise to remove discrepancy.

	Design Procedure Forr	m: Sand Filter (SF)	
	000		Sheet 2 of 2
Designer:			
Company:			
Date. Project:	Eastonville Road - Segment 2 Improvements		
Froject.	El Paso County, CO		
Location.			
5. Imperme A) Is an of stri	able Geomembrane Liner and Geotextile Separator Fabric impermeable liner provided due to proximity uctures or groundwater contamination?	Choose One	
6. Inlet / Ou A) Descr conve	tlet Works ribe the type of energy dissipation at inlet points and means of eying flows in excess of the WQCV through the outlet	Engery dissapation at inlet points provide of conveying flows in excess of the WQC modified type 'C' inlet outlet structure gra	ed via riprap, and means W through the outlet is via the te, and a restricted outlet pipe.
Notes:			

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.05 (January 2022)



Why is SFB C designed to drain in 12hrs but SFB A with Segment 1 is designed to drain in 40hrs. Consider revising for consistency. Either is fine per MHFD and EPC criteria.

5 ()		-
Initial Surcharge Depth (ISD) =	N/A	ft
Total Available Detention Depth $(H_{total}) =$	user	ft
Depth of Trickle Channel (H_{TC}) =	N/A	ft
Slope of Trickle Channel (S_{TC}) =	N/A	ft/ft
Slopes of Main Basin Sides (S_{main}) =	user	H:V
Basin Length-to-Width Ratio $(R_{L/W}) =$	user	
Initial Surcharge Area (A_{ISV}) =	user	ft ²
Surcharge Volume Length (L_{ISV}) =	user	ft

Initial Surcharge Area $(A_{ISV}) =$	user	ft-
Surcharge Volume Length (L_{ISV}) =	user	ft
Surcharge Volume Width (W_{ISV}) =	user	ft
Depth of Basin Floor (H_{FLOOR}) =	user	ft
Length of Basin Floor (L_{FLOOR}) =	user	ft
Width of Basin Floor (W_{FLOOR}) =	user	ft
Area of Basin Floor (A_{FLOOR}) =	user	ft²
Volume of Basin Floor (V_{FLOOR}) =	user	ft ³
Depth of Main Basin (H_{MAIN}) =	user	ft
Length of Main Basin (L_{MAIN}) =	user	ft
Width of Main Basin (W_{MAIN}) =	user	ft
Area of Main Basin $(A_{MAIN}) =$	user	ft²
Volume of Main Basin (V_{MAIN}) =	user	ft ³
Calculated Total Basin Volume (V_{total}) =	user	acre-feet





DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.05 (January 2022)







Shown as 7/16" (0.4375) on UD-BMP calcs above. Revise to remove

discrepancy.



Horiz. Length of Weir Sides = 3.00 N/A feet Type C Grate N/A Overflow Grate Type = 50% N/A Debris Clogging % = %

> Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate Zono 2 Destrictor Not Colected

3.13

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice) Zan a 2 Destrictor Not Colected

	Zone 3 Restrictor	Not Selected			Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	2.00	N/A	ft (distance below basin bottom at Stage = 0 ft)	Outlet Orifice Area =	0.10	N/A	ft ²
Outlet Pipe Diameter =	12.00	N/A	inches	Outlet Orifice Centroid =	0.11	N/A	feet
Restrictor Plate Height Above Pipe Invert =	2.20		inches Half-Central Angle	of Restrictor Plate on Pipe =	0.88	N/A	radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage=	2.86	ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length =	12.00	feet
Spillway End Slopes =	4.00	H:V
Freeboard above Max Water Surface =	1.00	feet

Calculated Parameters for Spillway

N/A

N/A

ft²

Spillway Design Flow Depth=	0.14	feet
Stage at Top of Freeboard =	4.00	feet
Basin Area at Top of Freeboard =	0.05	acres
Basin Volume at Top of Freeboard =	0.10	acre-ft

Overflow Grate Open Area w/o Debris =

Overflow Grate Open Area w/ Debris =

Routed Hydrograph Results	The user can over	ride the default CU	HP hydrographs an	d runoff volumes b	y entering new valu	les in the Inflow Hy	/drographs table (C	Columns W through	AF).
Design Storm Return Period =	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
One-Hour Rainfall Depth (in) =	N/A	N/A	0.93	1.21	1.46	1.84	2.16	2.49	3.37
CUHP Runoff Volume (acre-ft) =	0.009	0.037	0.023	0.032	0.043	0.063	0.079	0.097	0.142
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	0.023	0.032	0.043	0.063	0.079	0.097	0.142
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A	0.0	0.1	0.2	0.5	0.8	1.0	1.6
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A							
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.01	0.12	0.32	0.87	1.20	1.59	2.49
Peak Inflow Q (cfs) =	N/A	N/A	0.4	0.6	0.9	1.3	1.6	2.0	2.9
Peak Outflow Q (cfs) =	0.0	0.0	0.0	0.0	0.1	0.6	1.0	1.0	2.5
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	0.2	0.4	1.2	1.3	1.0	1.6
Structure Controlling Flow =	Filtration Media	Filtration Media	Filtration Media	Filtration Media	Overflow Weir 1	Overflow Weir 1	Outlet Plate 1	Outlet Plate 1	Spillway
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	N/A	0.0	0.1	0.2	0.2	0.2
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	11	40	26	36	44	43	42	42	40
Time to Drain 99% of Inflow Volume (hours) =	12	41	27	37	45	45	45	44	44
Maximum Ponding Depth (ft) =	1.06	2.46	1.77	2.20	2.52	2.60	2.65	2.85	2.97
Area at Maximum Ponding Depth (acres) =	0.01	0.03	0.02	0.02	0.03	0.03	0.03	0.03	0.04
Maximum Volume Stored (acre-ft) =	0.009	0.037	0.021	0.030	0.039	0.041	0.043	0.049	0.053



DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename:

Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5100 11111	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:15:00	0.00	0.00	0.04	0.08	0.11	0.09	0.12	0.12	0.19
	0:20:00	0.00	0.00	0.18	0.25	0.31	0.22	0.27	0.30	0.45
	0:25:00	0.00	0.00	0.39	0.56	0.77	0.48	0.61	0.70	1.19
	0:30:00	0.00	0.00	0.44	0.64	0.85	1.25	1.58	1.87	2.72
	0:35:00	0.00	0.00	0.37	0.53	0.70	1.29	1.60	2.01	2.87
	0:40:00	0.00	0.00	0.31	0.42	0.56	1.15	1.43	1.76	2.51
	0:45:00	0.00	0.00	0.23	0.33	0.44	0.93	1.15	1.48	2.11
	0:50:00	0.00	0.00	0.19	0.27	0.35	0.77	0.96	1.22	1.73
	0:55:00	0.00	0.00	0.15	0.22	0.29	0.60	0.75	0.99	1.42
	1:00:00	0.00	0.00	0.12	0.18	0.23	0.47	0.59	0.83	1.18
	1.05.00	0.00	0.00	0.10	0.14	0.19	0.37	0.47	0.69	0.99
	1:15:00	0.00	0.00	0.00	0.15	0.17	0.27	0.27	0.47	0.53
	1:20:00	0.00	0.00	0.07	0.10	0.15	0.17	0.21	0.25	0.38
	1:25:00	0.00	0.00	0.06	0.10	0.13	0.14	0.18	0.19	0.28
	1:30:00	0.00	0.00	0.06	0.09	0.11	0.12	0.15	0.15	0.22
	1:35:00	0.00	0.00	0.06	0.09	0.10	0.10	0.12	0.12	0.18
	1:40:00	0.00	0.00	0.06	0.08	0.10	0.09	0.11	0.11	0.16
	1:45:00	0.00	0.00	0.06	0.07	0.09	0.09	0.10	0.10	0.14
	1:50:00	0.00	0.00	0.06	0.06	0.09	0.08	0.10	0.09	0.14
	1:55:00	0.00	0.00	0.05	0.06	0.08	0.08	0.10	0.09	0.14
	2:00:00	0.00	0.00	0.04	0.06	0.08	0.08	0.10	0.09	0.14
	2:05:00	0.00	0.00	0.03	0.04	0.05	0.05	0.06	0.06	0.09
	2:10:00	0.00	0.00	0.02	0.02	0.03	0.03	0.04	0.04	0.06
	2.15.00	0.00	0.00	0.01	0.01	0.02	0.02	0.03	0.02	0.04
	2:25:00	0.00	0.00	0.01	0.01	0.01	0.01	0.02	0.01	0.02
	2:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.01
	2:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3.20.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3.23.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	<u>5:10:00</u>	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

DETENTION BASIN OUTLET STRUCTURE DESIGN MHFD-Detention, Version 4.05 (January 2022)

Summary Stage-Area-Volume-Discharge Relationships

The user can create a summary S-A-V-D by entering the desired stage increments and the remainder of the table will populate automatically. The user should graphically compare the summary S-A-V-D table to the full S-A-V-D table in the chart to confirm it captures all key transition points.

Stage - Storage Description	Stage	Area	Area	Volume	Volume	Total Outflow	
	[it]	[it]	[acres]	[it]		[CIS]	
							For best results, include the
							changes (e.g. ISV and Floor)
							from the S-A-V table on
							Sheet 'Basin'.
							Also include the inverte of all
							outlets (e.g. vertical orifice.
							overflow grate, and spillway,
							where applicable).



Eastonville Road Final Drainage Report Project No.: 201662.08

APPENDIX E – REFERENCE MATERIAL

Final Drainage Report for The Sanctuary Filing 1 at Meridian Ranch



EL PASO COUNTY, COLORADO

August 2022

Prepared For:

GTL DEVELOPMENT, INC. P.O. Box 80036 San Diego, CA 92138

Prepared By: Tech Contractors 11910 Tourmaline Dr., Ste 130 Falcon, CO 80831 719.495.7444

Highlight information on next few sheets which is being referenced in other portions of this report.

PCD Project No. SF22-020

Future Drainage - SCS Calculation Method

Following is a tabulation of the surface drainage characteristics for the future conditions using the SCS calculation method. Please refer to Figure 6 - Meridian Ranch SCS Calculations – Future Basins Map

Table 5: Future Drainage Basins-SCS

		FUTUR	E SCS (Full Spe	ctrum)		
		PEAK	PEAK	PEAK	PEAK	PEAK
		DISCHARGE	DISCHARGE	DISCHARGE	DISCHARGE	DISCHARGE
		Q100	Q50	Q10	Q5	Q2
		(CFS)	(CFS)	(CFS)	(CFS)	(CFS)
OS06	0.1313	80	52	12	3.8	0.5
G1a	0.1313	80	52	12	3.8	0.5
G1a-G2	0.1313	79	52	11	3.7	0.5
OS05	0.0578	39	26	5.6	1.8	0.2
OS05-G1	0.0578	39	25	5.5	1.7	0.2
FG01	0.0538	31	22	7.0	3.4	0.9
FG01-G1	0.0538	31	22	7.0	3.4	0.9
G1	0.1116	61	41	11	4.9	1.1
G1-G2	0.1116	61	41	11	4.8	1.1
FG02	0.0391	32	22	6.4	2.7	0.5
G2	0.2820	167	112	27	10	1.9
G2-G3	0.2820	163	108	27	10	1.9
FG03	0.0203	24	17	5.9	3.0	0.8
FG04	0.0172	22	16	5.8	3.1	0.9
G3	0.3195	185	123	31	12	2.4
FG06	0.0675	56	40	12	5.8	1.3
FG05	0.0580	45	33	12	6.7	2.4
OS07ab	0.0170	12	7.9	1.8	0.5	0.07
OS07ab-POND F	0.0170	12	7.6	1.7	0.5	0.07
POND F IN	0.4620	293	200	54	23	5.1
POND F	0.4620	178	121	16	8.0	2.1
POND F-G7	0.4620	177	120	16	8.0	2.1
OS07c	0.0296	19	12	2.7	0.9	0.12
OS07c-G4	0.0296	19	12	2.6	0.9	0.12
FG21a	0.0095	5.9	4.0	1.0	0.4	0.06
G4	0.0391	25	16	3.6	1.2	0.2
G4-G7	0.0391	24	16	3.5	1.2	0.2
FG21b	0.0150	21	16	6.5	3.9	1./
G7	0.5161	194	131	18	8.9	2.3
G7-G8	0.5161	194	131	18	8.9	2.3
FG22	0.1354	121	88	32	17	5.4
OS08a	0.0251	16	11	2.3	0.7	0.10
0508-68	0.0251	16	10	2.3	0.7	0.10
FG23a	0.0216	21	15	5.2	2.7	0.8
USU/d	0.0034	2.5	1.6	0.4	0.11	0.01
05070-68	0.0034	2.4	1.6	0.3	0.11	0.01
G8	0.7016	279	178	46	24	1.1
G8-G10	0.7016	278	1//	45	24	7.6
FG24D	0.0589	76	5/	24	15	0.5
C G 248	0.0348	24	10	4.5	2.0	0.4
	0.0165	9.5	0.3	1.4	0.5	0.07
CSUAD-GAA	0.0165	9.4	0.0	1.4	0.5	0.07
	0.0093	5.3	3.5	0.8	0.3	0.04
03098-098	0.0093	5.Z	3.4 74	0.7	0.3	0.04
098	0.1195	91	1	20	10	0.7

DRAINAGE AREA (SQ. MI.) PEAK DISCHARGE Q100 (CFS) PEAK DISCHARGE Q100 (CFS) PEAK DISCHARGE Q10 (CFS) PEAK DISCHARGE Q5 (CFS) PEAK DISCHARGE Q2 (CFS) G9a-G9b 0.1195 96 70 27 16 6.6 FG24c 0.0291 40 30 13 8.4 4.0 FG24d 0.0262 39 30 14 8.7 4.4 G9b 0.1748 170 127 53 32 14 REX RD WQCV 0.1748 158 123 50 31 13 FG23b 0.0236 17 11 2.7 0.9 0.13 G10 0.9000 390 263 90 46 15 G10-G11 0.9000 389 254 85 44 15 FG23c 0.0109 11 7.6 2.2 1.0 0.2 G11 0.9109 393 258 86 44 15 FG25 0.1084 111 <td< th=""><th colspan="6">FUTURE SCS (Full Spectrum)</th></td<>	FUTURE SCS (Full Spectrum)						
DRAINAGE AREA (SQ. MI.) DISCHARGE Q100 (CFS) DISCHARGE Q50 (CFS) DISCHARGE Q10 (CFS) DISCHARGE Q5 (CFS) DISCHARGE Q2 (CFS) DISCHARGE Q2 DISCHARGE			PEAK	PEAK	PEAK	PEAK	PEAK
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$			DISCHARGE	DISCHARGE	DISCHARGE	DISCHARGE	DISCHARGE
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$			Q100	Q50	Q10	Q5	Q2
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		(SQ. IVII.)	(CFS)	(CFS)	(CFS)	(CFS)	(CFS)
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	G9a-G9b	0.1195	96	70	27	16	6.6
FG24d 0.0262 39 30 14 8.7 4.4 G9b 0.1748 170 127 53 32 14 REX RD WQCV 0.1748 158 125 51 31 14 G9b-G10 0.1748 158 123 50 31 13 FG23b 0.0236 17 11 2.7 0.9 0.13 G10 0.9000 390 263 90 46 15 G10-G11 0.9000 389 254 85 44 15 FG23c 0.0109 11 7.6 2.2 1.0 0.2 G11 0.9109 393 258 86 44 15 FG25 0.1084 111 84 36 22 9.9 FG26 0.0184 15 10 3.0 1.2 0.2 POND G IN-WEST 1.0377 503 350 122 63 22 FG26 0.0570 65 50 24 16 8.2 <t< td=""><td>FG24c</td><td>0.0291</td><td>40</td><td>30</td><td>13</td><td>8.4</td><td>4.0</td></t<>	FG24c	0.0291	40	30	13	8.4	4.0
G9b 0.1748 170 127 53 32 14 REX RD WQCV 0.1748 158 125 51 31 14 G9b-G10 0.1748 158 123 50 31 13 FG23b 0.0236 17 11 2.7 0.9 0.13 G10 0.9000 390 263 90 46 15 G10-G11 0.9000 389 254 85 44 15 FG23c 0.0109 11 7.6 2.2 1.0 0.2 G11 0.9109 393 258 86 44 15 FG25 0.1084 111 84 36 22 9.9 FG28 0.0184 15 10 3.0 1.2 0.2 POND G IN-WEST 1.0377 503 350 122 63 22 FG27 0.0679 98 79 42 30 18	FG24d	0.0262	39	30	14	8.7	4.4
REX RD WQCV 0.1748 158 125 51 31 14 G9b-G10 0.1748 158 123 50 31 13 FG23b 0.0236 17 11 2.7 0.9 0.13 G10 0.9000 390 263 90 46 15 G10-G11 0.9000 389 254 85 44 15 FG23c 0.0109 11 7.6 2.2 1.0 0.2 G11 0.9109 393 258 86 44 15 FG25 0.1084 111 84 36 22 9.9 FG28 0.0184 15 10 3.0 1.2 0.2 POND G IN-WEST 1.0377 503 350 122 63 22 FG26 0.0570 65 50 24 16 8.1 POND G 0.570 64 50 24 16 8.1	G9b	0.1748	170	127	53	32	14
G9b-G10 0.1748 158 123 50 31 13 FG23b 0.0236 17 11 2.7 0.9 0.13 G10 0.9000 390 263 90 46 15 G10-G11 0.9000 389 254 85 44 15 FG23c 0.0109 11 7.6 2.2 1.0 0.2 G11 0.9109 393 258 86 44 15 FG25 0.1084 111 84 36 22 9.9 FG28 0.0184 15 10 3.0 1.2 0.2 POND G IN-WEST 1.0377 503 350 122 63 22 FG27 0.0679 98 79 42 30 18 FG26 0.0570 65 50 24 16 8.2 G13-POND G 0.0570 64 50 24 16 8.1	REX RD WQCV	0.1748	158	125	51	31	14
FG23b 0.0236 17 11 2.7 0.9 0.13 G10 0.9000 390 263 90 46 15 G10-G11 0.9000 389 254 85 44 15 FG23c 0.0109 11 7.6 2.2 1.0 0.2 G11 0.9109 393 258 86 44 15 FG23c 0.1084 111 84 36 22 9.9 FG25 0.1084 15 10 3.0 1.2 0.2 POND G IN-WEST 1.0377 503 350 122 63 22 FG27 0.0679 98 79 42 30 18 FG26 0.0570 65 50 24 16 8.2 G13 0.0570 64 50 24 16 8.1 POND G 0.426 450 293 52 21 5.3 G12 1.1626 450 293 52 21 5.3 G12	G9b-G10	0.1748	158	123	50	31	13
G10 0.9000 390 263 90 46 15 G10-G11 0.9000 389 254 85 44 15 FG23c 0.0109 11 7.6 2.2 1.0 0.2 G11 0.9109 393 258 86 44 15 FG25 0.1084 111 84 36 22 9.9 FG28 0.0184 15 10 3.0 1.2 0.2 POND G IN-WEST 1.0377 503 350 122 63 22 FG27 0.0679 98 79 42 30 18 FG26 0.0570 65 50 24 16 8.2 G13 0.0570 64 50 24 16 8.1 POND G 0.0570 64 52 21 5.3 53 G12 1.1626 450 293 52 21 5.3 53	FG23b	0.0236	17	11	2.7	0.9	0.13
G10-G110.9000389254854415FG23c0.0109117.62.21.00.2G110.9109393258864415FG250.10841118436229.9FG280.018415103.01.20.2POND G IN-WEST1.03775033501226322FG270.06799879423018FG260.0570655024168.2G130.0570655024168.2G13-POND G0.0570645024168.1POND G IN-EAST0.1249160127644425POND G1.162645029352215.3G121.162645029352215.3G12-G061.162644929352215.3FG290.098360398.92.90.4FG320.0402504019137.4G061.301149131757227.5	G10	0.9000	390	263	90	46	15
FG23c0.0109117.62.21.00.2G110.9109393258864415FG250.10841118436229.9FG280.018415103.01.20.2POND G IN-WEST1.03775033501226322FG270.06799879423018FG260.0570655024168.2G130.0570655024168.2G130.0570645024168.1POND G IN-EAST0.1249160127644425POND G1.162645029352215.3G121.162645029352215.3G12-G061.162644929352215.3FG290.098360398.92.90.4FG320.0402514020147.5FG32-G060.0402504019137.4G061.301149131757227.5	G10-G11	0.9000	389	254	85	44	15
G11 0.9109 393 258 86 44 15 FG25 0.1084 111 84 36 22 9.9 FG28 0.0184 15 10 3.0 1.2 0.2 POND G IN-WEST 1.0377 503 350 122 63 22 FG27 0.0679 98 79 42 30 18 FG26 0.0570 65 50 24 16 8.2 G13 0.0570 65 50 24 16 8.1 POND G IN-EAST 0.1249 160 127 64 44 25 G12 1.1626 450 293 52 21 5.3 G12 1.1626 450 293 52 21 5.3 G12-G06 1.1626 449 293 52 21 5.3 FG29 0.0983 60 39 8.9 2.9 0.4 <t< td=""><td>FG23c</td><td>0.0109</td><td>11</td><td>7.6</td><td>2.2</td><td>1.0</td><td>0.2</td></t<>	FG23c	0.0109	11	7.6	2.2	1.0	0.2
FG250.10841118436229.9FG280.018415103.01.20.2POND G IN-WEST1.03775033501226322FG270.06799879423018FG260.0570655024168.2G130.0570655024168.2G13-POND G0.0570645024168.1POND G IN-EAST0.1249160127644425POND G1.162645029352215.3G121.162645029352215.3G12-G061.162644929352215.3FG290.098360398.92.90.4FG320.0402514020147.5FG32-G060.0402504019137.4G061.301149131757227.5	G11	0.9109	393	258	86	44	15
FG280.018415103.01.20.2POND G IN-WEST1.03775033501226322FG270.06799879423018FG260.0570655024168.2G130.0570655024168.2G13-POND G0.0570645024168.1POND G IN-EAST0.1249160127644425POND G1.162645029352215.3G121.162645029352215.3G12-G061.162644929352215.3FG290.098360398.92.90.4FG320.0402514020147.5FG32-G060.0402504019137.4G061.301149131757227.5	FG25	0.1084	111	84	36	22	9.9
POND G IN-WEST1.03775033501226322FG270.06799879423018FG260.0570655024168.2G130.0570655024168.2G13-POND G0.0570645024168.1POND G IN-EAST0.1249160127644425G121.162645029352215.3G12-G061.162644929352215.3FG290.098360398.92.90.4FG320.0402514020147.5FG32-G060.0402504019137.4G061.301149131757227.5	FG28	0.0184	15	10	3.0	1.2	0.2
FG270.06799879423018FG260.0570655024168.2G130.0570655024168.2G13-POND G0.0570645024168.1POND G IN-EAST0.1249160127644425G121.162645029352215.3G121.162644929352215.3G12-G061.162644929352215.3FG290.098360398.92.90.4FG320.0402514020147.5FG32-G060.0402504019137.4G061.301149131757227.5	POND G IN-WEST	1.0377	503	350	122	63	22
FG260.0570655024168.2G130.0570655024168.2G13-POND G0.0570645024168.1POND G IN-EAST0.1249160127644425G121.162645029352215.3G121.162644929352215.3G12-G061.162644929352215.3FG290.098360398.92.90.4FG320.0402514020147.5FG32-G060.0402504019137.4G061.301149131757227.5	FG27	0.0679	98	79	42	30	18
G13 0.0570 65 50 24 16 8.2 G13-POND G 0.0570 64 50 24 16 8.1 POND G IN-EAST 0.1249 160 127 64 44 25 POND G 1.1626 450 293 52 21 5.3 G12 1.1626 450 293 52 21 5.3 G12 1.1626 449 293 52 21 5.3 G12-G06 1.1626 449 293 52 21 5.3 FG29 0.0983 60 39 8.9 2.9 0.4 FG32 0.0402 51 40 20 14 7.5 FG32-G06 0.0402 50 40 19 13 7.4 G06 1.3011 491 317 57 22 7.5	FG26	0.0570	65	50	24	16	8.2
G13-POND G 0.0570 64 50 24 16 8.1 POND G IN-EAST 0.1249 160 127 64 44 25 POND G 1.1626 450 293 52 21 5.3 G12 1.1626 450 293 52 21 5.3 G12-G06 1.1626 449 293 52 21 5.3 G12-G06 1.1626 449 293 52 21 5.3 FG29 0.0983 60 39 8.9 2.9 0.4 FG32 0.0402 51 40 20 14 7.5 FG32-G06 0.0402 50 40 19 13 7.4 G06 1.3011 491 317 57 22 7.5	G13	0.0570	65	50	24	16	8.2
POND G IN-EAST0.1249160127644425POND G1.162645029352215.3G121.162645029352215.3G12-G061.162644929352215.3FG290.098360398.92.90.4FG320.0402514020147.5FG32-G060.0402504019137.4G061.301149131757227.5	G13-POND G	0.0570	64	50	24	16	8.1
POND G1.162645029352215.3G121.162645029352215.3G12-G061.162644929352215.3FG290.098360398.92.90.4FG320.0402514020147.5FG32-G060.0402504019137.4G061.301149131757227.5	POND G IN-EAST	0.1249	160	127	64	44	25
G12 1.1626 450 293 52 21 5.3 G12-G06 1.1626 449 293 52 21 5.3 FG29 0.0983 60 39 8.9 2.9 0.4 FG32 0.0402 51 40 20 14 7.5 FG32-G06 0.0402 50 40 19 13 7.4 G06 1.3011 491 317 57 22 7.5	POND G	1.1626	450	293	52	21	5.3
G12-G06 1.1626 449 293 52 21 5.3 FG29 0.0983 60 39 8.9 2.9 0.4 FG32 0.0402 51 40 20 14 7.5 FG32-G06 0.0402 50 40 19 13 7.4 G06 1.3011 491 317 57 22 7.5	G12	1.1626	450	293	52	21	5.3
FG290.098360398.92.90.4FG320.0402514020147.5FG32-G060.0402504019137.4G061.301149131757227.5	G12-G06	1.1626	449	293	52	21	5.3
FG320.0402514020147.5FG32-G060.0402504019137.4G061.301149131757227.5	FG29	0.0983	60	39	8.9	2.9	0.4
FG32-G06 0.0402 50 40 19 13 7.4 G06 1.3011 491 317 57 22 7.5	FG32	0.0402	51	40	20	14	7.5
G06 1.3011 491 317 57 22 7.5	FG32-G06	0.0402	50	40	19	13	7.4
	G06	1.3011	491	317	57	22	7.5

Rational Calculations

The Rational Hydrologic Calculation Method was used to estimate the total runoff from the 5-year and the 100-year design storm and thus establish the storm drainage system design. Using the rational calculation methodology outlined in the Hydrology Section (Ch 6) of the COSDCM coupled with the El Paso County EPCDCM an effective storm drainage design for the Sanctuary Filing 1 has been designed. The storm drainage facilities have been designed such that the minor storm will be captured by the inlets and conveyed by the storm drain pipes such that the street flow does not overtop the curbs. The storm drainage facility has been designed such that the major storm will be captured by the inlets and conveyed by the storm drain pipes such that the street flow does not exceed the right-of-way widths for residential streets and the hydraulic grade line will be less than one foot below the surface.

The site is located within the Gieck Ranch Drainage Basin. The storm drain runoff will be collected by a series of inlets and storm drain pipe then conveyed through the project and discharge directly into the existing Pond G that is properly sized to safely convey the storm water flows away from the project without damaging adjacent property.

Rational Narrative

The following is a detailed narrative of the storm drainage system located in the Sanctuary Filing 1. These storm drainage systems meet the requirements of as found in the El Paso





Eastonville Road Final Drainage Report Project No.: 201662.08

APPENDIX F – DRAINAGE MAPS



LEGEND:

EXISTING MAJOR CONTOUR EXISTING MINOR CONTOUR EX STORM SEWER EX DRAINAGE SWALE EX PROPERTY LINE EXISTING FLOW DIRECTION PROPOSED DRAINAGE BASIN — — — 5250 [·] — — _ _ _ _____

13

DESIGN POINT

PROPOSED BASIN LABEL

- Add Basin and Design Point Summary Tables

- Label all existing easements (all maps)

- Text is hard to read, suggest making it a little larger

-Could not find Design Points G15, G18, FG36, or G16 in the Sanctuary FDR for comparison. Recommended highlighting them in the reference section.

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DESIGN POINT

PROPOSED BASIN LABEL

LEGEND:

PROPOSED MAJOR CONTOUR PROPOSED MINOR CONTOUR EXISTING MAJOR CONTOUR EXISTING MINOR CONTOUR PROPOSED STORM SEWER PROPOSED DRAINAGE SWALE PROPERTY LINE PROPOSED FLOW DIRECTION EXISTING FLOW DIRECTION PROPOSED DRAINAGE BASIN DESIGN POINT

PROPOSED BASIN LABEL

SUMMARY RUNOFF TABLE				
BASIN	AREA (ac)	% IMPERVIOUS	Q5 (cfs)	Q100 (cfs)
EA1	0.22	73	0.8	1.5
EA2	0.25	72	0.9	1.7
EA3	0.20	70	0.7	1.3
EA4	0.17	65	0.5	1.1
EA5	0.16	0	0.1	0.4
EA6	0.70	100	3.2	5.3
EA7	0.65	89	2.6	4.3
EA8	2.08	99	5.2	8.8
EA9	2.99	63	5.0	10.4
EA10	0.16	75	0.6	1.1
EA11	0.15	67	0.5	1.0
OS1	85.16	2	<mark>#NUM!</mark>	<mark>#NUM!</mark>
OS2	15.03	7	6.0	30.8
OS3	1.00	2	0.3	2.2
OS4	9.60	9	4.8	21.6
OS5	40.26	8	17.7	85.2
OS6	60.83	2	16.3	109.3
OS7	11.42	2	3.6	24.4

	DESIGN POINT SUMMARY TABLE				
	DESIGN POINT	CONTRIBUTING BASINS	SQ5 (cfs)	SQ100 (cfs)	
	1	OS1	0.0	<mark>0.0</mark>	
	2	EA1	0.8	1.5	
	3	EA2, DP2	1.6	3.2	
	4	EA5, DP3	1.7	3.4	
	5	EA3	0.7	1.3	
	6	EA4	1.2	2.4	
	6.1	DP6, DP8.1	7.0	<mark>34.0</mark>	
	7	OS2	<mark>6.0</mark>	<mark>30.8</mark>	
	8	OS3	0.3	<mark>2.2</mark>	
	7 8.1	DP7, DP8	6.3	32.6	
	9	DP6.1	7.0	<mark>33.8</mark>	
	10	EA6, EA7	5.6	9.5	
	11	OS4, DP9	<mark>10.5</mark>	<mark>49.8</mark>	
	12	OS5	<mark>23.1</mark>	<mark>110.5</mark>	
	13	OS7	<mark>3.6</mark>	24.4	
	13.1	DP12, DP13	24.6	122,4	
	14	EA8	5.2	8.8	
	15	EA9	5.0	10.4	
	15.1	DP14, DP15	10.2	19.1	
	16.1	EA10	0.6	1.1	
	17.1	EA11	0.5	1.0	
-	8.1	OS6	6.3	32.6	

in summary table

nclude all basins

nclude all design points as liste n hydrology spreadsheet

ch with hydrology spreadshe ase revise so table and Isheet match

D·R·HORTON^{*} America's Builder

SHEET DRN

EL PASO COUNTY, CO

LEGEND:

PROPOSED MAJOR CONTOUR PROPOSED MINOR CONTOUR EXISTING MAJOR CONTOUR EXISTING MINOR CONTOUR PROPOSED STORM SEWER PROPOSED DRAINAGE SWALE PROPERTY LINE PROPOSED FLOW DIRECTION EXISTING FLOW DIRECTION PROPOSED DRAINAGE BASIN DESIGN POINT

PROPOSED BASIN LABEL

SUMMARY RUNOFF TABLE				
BASIN	AREA (ac)	% IMPERVIOUS	Q5 (cfs)	Q100 (cfs)
EA1	0.22	73	0.8	1.5
EA2	0.25	72	0.9	1.7
EA3	0.20	70	0.7	1.3
EA4	0.17	65	0.5	1.1
EA5	0.16	0	0.1	0.4
EA6	0.70	100	3.2	5.3
EA7	0.65	89	2.6	4.3
EA8	2.08	99	5.2	8.8
EA9	2.99	63	5.0	10.4
EA10	0.16	75	0.6	1.1
EA11	0.15	67	0.5	1.0
OS1	85.16	2	#NUM!	#NUM!
OS2	15.03	7	6.0	30.8
OS3	1.00	2	0.3	2.2
OS4	9.60	9	4.8	21.6
OS5	40.26	8	17.7	85.2
OS6	60.83	2	16.3	109.3
OS7	11.42	2	3.6	24.4

DESIGN POINT SUMMARY TABLE				
DESIGN POINT	CONTRIBUTING BASINS	SQ5 (cfs)	SQ100 (cfs)	
1	OS1	0.0	0.0	
2	EA1	0.8	1.5	
3	EA2, DP2	1.6	3.2	
4	EA5, DP3	1.7	3.4	
5	EA3	0.7	1.3	
6	EA4	1.2	2.4	
6.1	DP6, DP8.1	7.0	34.0	
7	OS2	6.0	30.8	
8	OS3	0.3	2.2	
8.1	DP7, DP8	6.3	32.6	
9	DP6.1	7.0	33.8	
10	EA6, EA7	5.6	9.5	
11	OS4, DP9	10.5	49.8	
12	OS5	23.1	110.5	
13	OS7	3.6	24.4	
13.1	DP12, DP13	24.6	122.4	
14	EA8	5.2	8.8	
15	EA9	5.0	10.4	
15.1	DP14, DP15	10.2	19.1	
16.1	EA10	0.6	1.1	
17.1	EA11	0.5	1.0	
8.1	OS6	6.3	32.6	

Provide DP and show conveyance to drainageway

SHEET DRN

2