



**Eastonville Road – Londonderry Dr. to Rex Rd.  
Segment 2 Improvements  
Stationing 47+00.00 – 79+31.62**

**Final Drainage Report**

August 2024

HR Green Project No: 201662.08

**Prepared For:**

D.R. Horton

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**Prepared By:**

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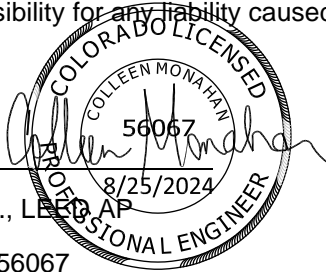
(719) 394-2433

EDARP Filing No:

CDR2321

## Engineer's Statement:

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the County for drainage reports and said report is in conformity with the applicable master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.



\_\_\_\_\_  
Colleen Monahan, P.E., LEED AP Date

State of Colorado No. 56067

For and on behalf of HR Green Development, LLC

## Owner/Developer's Statement:

I, the developer, have read and will comply with all of the requirements specified in this drainage report and plan.

By: \_\_\_\_\_

Authorized Signature

\_\_\_\_\_ Date

Address: D.R. Horton  
9555 S. Kingston Court  
Englewood, CO

## El Paso County Statement

Filed in accordance with the requirements of the Drainage Criteria Manual, Volumes 1 and 2, El Paso County Engineering Criteria Manual and Land Development code, as amended.

\_\_\_\_\_  
Joshua Palmer, P.E.

\_\_\_\_\_ Date

County Engineer/ECM Administrator

Conditions:

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## I. General Purpose, Location and Description

### a. Purpose

The purpose of this Final Drainage Report (FDR) for Eastonville Road Segment 2 Improvements is to describe the onsite and offsite drainage patterns, size drainage infrastructure to safely capture and convey developed runoff to water quality and detention facilities, and to safely route detained stormwater to adequate outfalls. This drainage report will detail the improvements of Eastonville Road from Londonderry Dr. to Rex Road for Segment 2. Stations 47+00.00 to 79+32.00 contain the Segment 2 Improvements for the Eastonville Road from Londonderry Drive to Rex Road for the portion of the project north of Grandview Filing No. 1. The project is all one project, however, the plan set has been broken into two segments to align with the Grandview Reserve Filings. A separate FDR describes Segment 1 of the project.

### b. Location

Eastonville Road from Londonderry Dr. to Rex Road, referred to as 'the site' herein, is an existing 26' wide treated gravel road in El Paso County, Colorado. Per field inspection the existing pavement is not full depth, and therefore described as 'temporary' for the purpose of this report. The site lies in the existing 60' wide El Paso County Right-of-Way within Sections 21 and 28, Township 12 South, Range 64 West of the 6<sup>th</sup> Principal Meridian, in El Paso County, State of Colorado.

The site is bound by undeveloped land to the east and west that has historically been used as ranching lands. Falcon Regional Park, which contains ballparks and parking, and Falcon High School also border the site to the west. All lands to the east and west of the site are unplatted. A vicinity map is presented in Appendix A.

### c. Description of Property

The site is approximately 0.69 miles (2.17 acres) of existing treated gravel roadway north of Londonderry Dr. and south of Rex Road. Per field inspection the existing pavement is not full depth, and therefore described as 'temporary' for the purpose of this report. The existing treated gravel width for the length of the project is 26' wide. There are 4' wide gravel shoulders and native landscaped swales are located on both sides of the roadway. Offsite stormwater is bypassed under the road through a series of existing culverts. See Appendix A for an existing conditions photo.

The existing roadway has slopes ranging from 0.3% up to about 4%. The general topography of the surrounding area is typical of high desert, short prairie grass with gently rolling hillside with slopes ranging from 2% to 4%. The project site drains generally from the west to the east and is tributary to Black Squirrel Creek.

Per a NRCS soil survey, the site is made up of Type A Columbine gravelly sandy loam, Type A Blakeland loamy sand and Type B Stapleton sandy loam. The NRCS soil survey is presented in Appendix A.

Gieck Ranch Tributary #1 (Channel A) is the only drainageway that traverses the site in the west to east direction through an existing culvert under Eastonville Road. The channel is a mapped wetland and a wetland permit will be required for a part of this Eastonville Road improvement project. Channel A is not within a FEMA floodplain.

Gieck Ranch Tributary #2 is located on the north end of the project site and will not be impacted by this project. There are no known irrigation facilities in the area.



Existing utilities include an underground gas line that runs under Eastonville road through the Grandview reserve property south of the segment 2 improvements, an existing raw water line that follows the west side of Eastonville north of Falcon Regional Park, and an existing aboveground electrical line along the western side of Eastonville Road. An existing drainage map with these facilities is presented in Appendix F.

**d. Floodplain Statement**

Based on FEMA Firm map 08041C0552G December 7, 2018, the site is not located in any FEMA designated floodplain. See FEMA Firm Map in Appendix A. There is a Zone A floodplain north of the site and a Zone AE south of the site, both of which will not be altered with the associated Eastonville Road improvements.

## II. Drainage Design Criteria

**a. Drainage Criteria**

Hydrologic data and calculations were performed using Drainage Criteria Manual Volume 1 of El Paso County (EPCDCM), with County adopted Chapter 6 and Section 3.2.1 of Chapter 13 of the City of Colorado Springs Drainage Criteria Manual (CCSDCM), May 2014 revised January 2021.

Onsite drainage improvements are designed for the 5-year storm (minor event) and 100-year storm (major event) using rainfall values from the NOAA Atlas 14 Point Precipitation Frequency Data Server. Runoff was calculated per CCSDCM Section 6.3.0 - Rational Method. Private, full spectrum pond design was completed using the latest version of Mile High Flood District’s (MHFD) UD-Detention per CCSDCM Section 13.3.2.1 – Private, full spectrum Detention. The detention pond allowable release rate will be limited to less than historic rates.

Rainfall Depths per NOAA Atlas 14		
Return Period (yr)	5	100
1-hr Rainfall Depth (in)	1.21	2.49

Inlet sizing was performed per the methods described in EPCDCM Section III Chapter 7 – Street Drainage and Storm Water Inlets. Storm sewer sizing was performed per the methods described in EPCDCM Section III Chapter 8 – Storm Drains and Appurtenances.

## III. Drainage Basins and Subbasins

**a. Major Basin Description**

The site is located within the Gieck Ranch Drainage Basin. The site’s drainage characteristics were previously studied in the following reports:

1. “Gieck Ranch Drainage Basin Planning Study” prepared by Drexel, Barrel & Co, February 2010.
2. “Master Development Drainage Plan Meridian Ranch” prepared by Tech Contractors, July 2021.
3. “Final Drainage Report for The Sanctuary Filing 1 at Meridian Ranch” by Tech Contractors, August 2022.

Gieck Ranch Drainage Basin is a 22.05 square mile watershed located in El Paso County, Colorado. Gieck Ranch Drainage Basin is tributary to Black Squirrel Creek which drains to the Arkansas River. The majority of the basin is undeveloped and is rolling range land typical of Colorado’s semi-arid climates. It should be noted that the Gieck Ranch DBPS has not been approved at the time of this report.

The Meridian Ranch MDDP and The Final Drainage Report for The Sanctuary Filing 1 at Meridian Ranch indicate that the Eastonville Road culvert crossing at the Gieck Ranch Tributary #1, within the project boundary, does not provide enough capacity for the historic flow rates. This culvert will be upgraded as part of this project.

Within the Gieck Ranch Drainage Basin, ranching has historically been the predominant land use, with rolling topography between 2%-4% slopes. Recently urbanization is occurring within the drainage basin, most notably for this project are Meridian Ranch and Latigo Trails Developments. Both are single family residential neighborhoods located upstream to the west and northwest of the Eastonville Segment 2 Improvements project site.

## **b. Existing Subbasin Description**

Eastonville Road Segment 2 (the site) accepts flows from areas to the west and northwest of the site, including portions of Meridian Ranch and Latigo Trails Development. The flows and design points used in the following descriptions are taken from the approved Meridian Ranch MDDP and The Final Drainage Report for The Sanctuary Filing 1 at Meridian Ranch provides the detailed analysis of the pond releases and flows as they outfall from those developments upstream of this Eastonville Road site. For the purpose of this report, full buildout of the Meridian Ranch development was assumed; hence the developed peak flow rates from the “future buildout conditions” for the entirety of Meridian Ranch were used to evaluate the existing conditions below.

Basin EX1 (The Sanctuary Filing 1 FG-38) is 85.16 acres of undeveloped area and treated gravel area to the crown of Eastonville Road roadway. Stormwater from this basin combines with flows from Latigo Trails South Pond (The Sanctuary Filing 1 G-17) is conveyed overland to DP1 for a total area of 321.5 acres (The Sanctuary Filing 1 G18). Flows at DP1 ( $Q_5 = 28.3$  cfs  $Q_{100} = 365.2$  cfs) are conveyed across Eastonville Road in an existing 24" CMP culvert and discharges to Gieck Ranch Tributary #2 (Channel B). This basin is located upstream of the Eastonville project and is presented here to show where flows go that are upstream of the project site. The Eastonville project will have no impact on this basin.

Basin EX2 (The Sanctuary Filing 1 FG36) is 18.88 acres undeveloped area, parking lot, and treated gravel to the crown of Eastonville Road roadway. Stormwater from this basin is conveyed overland to DP2 (The Sanctuary Filing 1 FG36). Flows at DP2 ( $Q_5 = 1.7$  cfs  $Q_{100} = 18.8$  cfs) are conveyed southerly across Rex Road in an existing 24" RCP culvert and discharges to Basin EX3.

Basin EX3 is 51.06 acres of undeveloped area and the Falcon Regional Park ball fields and treated gravel to the crown of Eastonville Road roadway. Stormwater from this basin combines with flows from The Sanctuary Filing 1 Design Point G15 via an existing roadside swale where it then combines with DP2 flows. Flows travel to DP3 for a total area of 131.3 acres (The Sanctuary Filing 1 Design Point G16) where they are conveyed across Eastonville Road in an existing 24" CMP culvert ( $Q_5 = 6.1$  cfs  $Q_{100} = 112.1$  cfs).

Basin EX4 is 62.87 acres of undeveloped area and treated gravel to the crown of Eastonville Road roadway. Stormwater from this basin combines with flows from The Sanctuary Filing 1 Design Point G12 (Meridian Ranch Pond G) to Gieck Ranch Tributary #1 and an existing roadside swale to DP 4 for a total area of 832.7 acres (The Sanctuary Filing 1 Design Point G06) ( $Q_5 = 22.4$  cfs  $Q_{100} = 491$  cfs). Flows at DP4 are conveyed across Eastonville Road in an existing 18" CMP culvert and discharges to Gieck Ranch Tributary #1 (Channel A).

Basin EX5 is 12.19 acres of undeveloped area and a future church property on the east side of the Eastonville Roadway. Stormwater from this basin sheet flows east directly to the Gieck Ranch Tributary #1 at DP13.1 ( $Q_5 = 2.7$  cfs  $Q_{100} = 18.0$  cfs).

Basin EX6 is 0.61 acres of undeveloped area on the future church property on the east side of the Eastonville Roadway. Stormwater from this basin flows south via an existing drainage channel south to DP O3.1 ( $Q_5 = 0.1$  cfs  $Q_{100} = 0.9$  cfs). Ultimately draining east to the Gieck Ranch Tributary #1.

Basin EX7 is 1.90 acres of undeveloped area on the east side of the Eastonville Roadway. Stormwater from this basin flows south via an existing drainage channel south to DP O3 ( $Q_5 = 0.4$  cfs  $Q_{100} = 2.5$  cfs). Ultimately draining east to the Gieck Ranch Tributary #1 combined with flows from DP G16 from the Sanctuary Filing 1.

Basin EX8 is 2.86 acres of undeveloped area on the east side of the Eastonville Roadway. Stormwater from this basin flows south via an existing drainage channel south to DP O3 ( $Q_5 = 0.6$  cfs  $Q_{100} = 4.0$  cfs). Ultimately draining east to the Gieck Ranch Tributary #1 combined with flows from DP G06 from the Sanctuary Filing 1.

### **c. Proposed Subbasin Description**

#### **Description of Proposed Project**

The proposed project includes improvements to Eastonville Road from Londonderry Drive to Rex Road. As described above, the current condition of the existing roadway in this area consists of 26' wide treated gravel roadway with 4' wide sand shoulders and weedy swales located on both sides of the roadway. Offsite stormwater is bypassed under the road through a series of existing culverts.

The proposed improvements from Rex Road south to the southern property line of the proposed Grandview Reserve Filing 1 include removal of the 26' wide treated gravel and replacing the road with a Modified Urban Minor Arterial Roadway Cross-Section consisting of 48' pavement and Type A EPC curb (53' back of curb to back of curb). This includes Basins EA1-EA11.

Refer to the Eastonville Road Segment 1 improvements FDR for subbasin information and calculations south of subbasins EA10 & EA11.

#### **Eastonville Road Basins**

Basin EA1 is 0.22 acres of proposed roadway (Modified Urban Minor Arterial Roadway Cross-Section). Stormwater ( $Q_5 = 0.7$  cfs  $Q_{100} = 1.3$  cfs) is conveyed in curb and gutter to DP2. Flows at DP2 are captured in a 5' Type R sump inlet (Public) and piped to Pond C, a private full spectrum sand filter basin. Basin EA1 will be detained by the Pond C Sand Filter.

Basin EA2 is 0.25 acres of proposed roadway (Modified Urban Minor Arterial Roadway Cross-Section). Stormwater ( $Q_5 = 0.8$  cfs  $Q_{100} = 1.5$  cfs) is conveyed in curb and gutter to DP3. Flows at DP3 are captured in a 5' Type R sump inlet (Public) and piped to Pond C. Basin EA2 will be detained by the Pond C Sand Filter.

Basin EA3 is 0.20 acres of proposed roadway (Modified Urban Minor Arterial Roadway Cross-Section). Stormwater ( $Q_5 = 0.7$  cfs  $Q_{100} = 1.4$  cfs) is conveyed in curb and gutter to DP5. Flows at DP5 are captured in a 10' Type R sump inlet (Public) and piped to DP9. Basin EA3 will not be detained per the Meridian Ranch MDDP as this basin has been over-detained within Meridian Ranch.

Basin EA4 is 0.17 acres of proposed roadway (Modified Urban Minor Arterial Roadway Cross-Section). Stormwater ( $Q_5 = 0.5$  cfs  $Q_{100} = 1.1$  cfs) is conveyed in curb and gutter to DP6. Flows at DP6 are captured in

a 5' Type R sump inlet (Public) and piped to DP9. Basin EA4 will not be detained per the Meridian Ranch MDDP as this basin has been over-detained within Meridian Ranch.

Basin EA5 is 0.16 acres of undeveloped area and includes the Pond C Sand Filter. Stormwater ( $Q_5 = 0.1$  cfs  $Q_{100} = 0.4$  cfs) is flows directly into the Pond C Sand Filter.

Basin EA6 is 0.70 acres of undeveloped area that will be future roadway (Rex Road) once the Grandview Filing 1 development is constructed. Stormwater ( $Q_5 = 3.1$  cfs  $Q_{100} = 5.5$  cfs) is conveyed in a swale to DP10: Temporary Sediment Basin #1 (TSB #1). TSB #1 has been sized for the paved area of the roundabout and the future paved area of Rex Road within Basin EA6. The swale will be removed with the construction of Rex Road curb and gutter. Basin EA6 will be detained in TSB #1.

Basin EA7 is 0.65 acres of undeveloped area that will be future roadway (Rex Road) once the Grandview Filing 1 development is constructed. Stormwater ( $Q_5 = 2.5$  cfs  $Q_{100} = 4.7$  cfs) is conveyed in a swale to DP10: Temporary Sediment Basin #1 (TSB #1). TSB #1 has been sized for the paved area of the roundabout and the future paved area of Rex Road within Basin EA7. The swale will be removed with the construction of Rex Road curb and gutter. Basin EA7 will be detained in TSB #1.

Basin EA8 is 2.08 acres of proposed roadway (Modified Urban Minor Arterial Roadway Cross-Section). Stormwater ( $Q_5 = 5.0$  cfs  $Q_{100} = 9.0$  cfs) is conveyed in curb and gutter to DP14. Flows at DP14 are captured in a 10' Type R sump inlet (Public) and piped to Pond B. Basin EA8 will be detained Pond B Full Spectrum Detention Basin.

Basin EA9 is 2.99 acres of proposed roadway (Modified Urban Minor Arterial Roadway Cross-Section). Stormwater ( $Q_5 = 4.6$  cfs  $Q_{100} = 9.5$  cfs) is conveyed in curb and gutter to DP15. Flows at DP15 are captured in a 10' Type R sump inlet (Public) and piped to Pond B. Basin EA9 will be detained Pond B Full Spectrum Detention Basin.

Basin EA10 is 0.12 acres of proposed roadway (Modified Urban Minor Arterial Roadway Cross-Section). Stormwater ( $Q_5 = 0.6$  cfs  $Q_{100} = 1.1$  cfs) is conveyed in curb and gutter to DP16.1 Flows from DP16.1 drain south and captured in a 10' Type R sump inlet (Public) and piped to Pond B. This inlet design is in the Eastonville Road Segment 1 FDR. Basin EA10 will be detained Pond B Full Spectrum Detention Basin which is detailed in the Eastonville Road Segment 1 FDR.

Basin EA11 is 0.19 acres of proposed roadway (Modified Urban Minor Arterial Roadway Cross-Section). Stormwater ( $Q_5 = 0.5$  cfs  $Q_{100} = 1.0$  cfs) is conveyed in curb and gutter to DP17.1. Flows from DP17.1 drain south and captured in a 10' Type R sump inlet (Public) and piped to Pond B. This inlet design is in the Eastonville Road Segment 1 FDR. Basin EA10 will be detained Pond B Full Spectrum Detention Basin which is detailed in the Eastonville Road Segment 1 FDR.

Basin EA12 is 0.34 acres of landscaping east of the Eastonville Roadway. Stormwater ( $Q_5 = 0.1$  cfs  $Q_{100} = 1.0$  cfs) is conveyed south to DP O4. Flows at DP O4 combine with DP G06 per the Sanctuary Filing 1 Report. This design point then drains east offsite in the Geick Ranch Tributary #1.

Basin EA13 is 0.45 acres of Eastonville Roadway at the Dawlish Dr roundabout. Stormwater ( $Q_5 = 1.4$  cfs  $Q_{100} = 2.8$  cfs) is conveyed east to DP O4.1. Flows to DP O4.1 will be detained and treated as a part of the Grandview Reserve development. This design point then drains southeast offsite in the Geick Ranch Tributary #1.

Basin EA14 is 1.48 acres of landscaping and concrete/gravel trail on the east side of Eastonville Rd. Stormwater ( $Q_5 = 1.2$  cfs  $Q_{100} = 3.8$  cfs) is conveyed southeast to DP O4.2. Flows to DP O4.2 will be detained

and treated as a part of the Grandview Reserve development. This design point then drains southeast offsite in the Geick Ranch Tributary #1.

Basin EA15 is 0.76 acres of landscaping and concrete/gravel trail on the east side of Eastonville Rd. Stormwater ( $Q_5 = 0.7$  cfs  $Q_{100} = 2.1$  cfs) is conveyed southeast to DP O3. Flows to DP O3 combine with flows from the Sanctuary Filing 1 FDR design point G16. Flows to DP O3 will be detained and treated as a part of the Grandview Reserve development. This design point then drains southeast offsite in the Geick Ranch Tributary #1.

Basin EA16 is 1.18 acres of landscaping on the east side of Eastonville Rd and south of the church property. Stormwater ( $Q_5 = 0.3$  cfs  $Q_{100} = 2.5$  cfs) is conveyed southeast to DP 13.1. Flows to DP 13.1 will be detained and treated as a part of the Grandview Reserve development. This design point then drains southeast offsite in the Geick Ranch Tributary #2.

Basin EA17 is 0.30 acres of landscaping on the east side of Eastonville Rd and south of the church property. Stormwater ( $Q_5 = 0.1$  cfs  $Q_{100} = 0.7$  cfs) is conveyed southeast to DP 10.1. This design point drains southeast offsite in the Geick Ranch Tributary #2.

### **Offsite Basins**

Basin OS1 (EX1) is 85.16 acres of undeveloped area. Stormwater from this basin combines with flows from Latigo Trails South Pond (The Sanctuary Filing 1 G-17) is conveyed overland to DP1 (The Sanctuary Filing 1 G18). Flows at DP1 ( $Q_5 = 28.3$  cfs  $Q_{100} = 365.2$  cfs) are conveyed across Eastonville Road in an existing 24" CMP culvert and discharges to Geick Ranch Tributary #2 (Channel B). This basin is located upstream of the Eastonville project and is presented here to show where flows go that are upstream of the project site. The Eastonville project will have no impact on this basin.

Basin OS2 is 15.03 acres of undeveloped land and parking area north of Rex Road and contains a portion of Rex Road ( $Q_5 = 4.2$  cfs  $Q_{100} = 21.6$  cfs). Stormwater is conveyed to DP7 and is captured in a proposed 24" RCP culvert and piped south across Rex Road. No development associated with Eastonville Road will occur in Basin OS2.

Basin OS3 is 1.00 acre of undeveloped land ( $Q_5 = 0.2$  cfs  $Q_{100} = 1.2$  cfs) along the western edge of Eastonville Road. Stormwater is conveyed to DP8 and is captured in a proposed 18" RCP culvert and piped south across Rex Road. No development associated with Eastonville Road will occur in Basin OS3.

Basin OS4 is 9.60 acres of undeveloped land ( $Q_5 = 4.8$  cfs  $Q_{100} = 21.6$  cfs) along the western edge of Eastonville Road. Stormwater is conveyed to DP11 in a roadside swale where it combines with Meridian Ranch DP G15 flows ( $Q_5 = 8$  cfs  $Q_{100} = 54.0$  cfs) before being captured in a proposed 24" RCP culvert and piped to DP11.1. The combined flows as it reaches DP11 is  $Q_5 = 7.5$  cfs  $Q_{100} = 44$  cfs.

Basin OS5 is 40.26 acres of undeveloped land and Falcon Regional Park along the western edge of Eastonville Road. Stormwater is conveyed to DP3 where per the Sanctuary Filing 1 FDR the total flow is 112.2.1 cfs to a proposed 48" RCP culvert and piped to Channel B.

Basin OS6 is 60.83 acres of undeveloped land along the western edge of Eastonville Road. Basin OS6 flows are adapted directly from the approved The Sanctuary Filing 1 FDR. Stormwater is conveyed to DP16 in a roadside swale where it combines with Meridian Ranch DP G12 flows before being conveyed across

Eastonville Road in dual 10' x 3.5' RCBC to Channel A. The combined flows at DP16 (EX4) are  $Q_5 = 22.4$  cfs  
 $Q_{100} = 491$  cfs.

Basin OS7 is future outflow of 11.29 acres of a future stormwater detention pond outflow developed land that will be detained to meet existing conditions ( $Q_5 = 3.9$  cfs  $Q_{100} = 24.6$  cfs) in the southeast corner of Eastonville Road and Rex Road. From there, stormwater is piped to Channel B.

## IV. Drainage Facility Design

### a. General Concept

The proposed improvements from Rex Road south to the southern property line of the proposed Grandview Reserve Filing 1 include removal of the 26' wide treated gravel and replacing the road with a Modified Urban Minor Arterial Roadway Cross-Section consisting of 48' pavement and Type A EPC curb (53' back of curb to back of curb). Inlets will be placed at low points and roundabout entrances. Stormwater from this roadway will be piped to either a full spectrum detention pond, sand filter or temporary sediment basin. All ponds and water quality features will discharge at less than historic rates.

### b. Water Quality & Detention

#### **Pond C (Sand Filter)**

Water quality and stormwater detention for Basins EA1, 2, & 5 is provided in Sand Filter Basin C. SFB C is a public, full spectrum sand filter basin within the Grandview Reserve property to be developed in the future. In Pond C, a total of 0.63 from the proposed project acres at 54% composite imperviousness will be detained. The minimum required acreage of treatment is 0.63 acres. The WQCV is 0.009 ac-ft, the EURV is 0.037 ac-ft, and the 100-year detention volume is 0.062 ac-ft. The WQCV, EURV and 100-year storms are released in 12, 41 and 44 hours, respectively. A 10' access and maintenance road is provided to the bottom of the pond to facilitate maintenance of the pond facilities. A 12' emergency overflow spillway is provided that conveys the developed, peak 100-yr flow rate with 1.0' of freeboard south. SFB C outfalls towards the future Channel B improvements at historic runoff rates. Runoff from Pond C will follow historic drainage patterns and not exceed historic flow rates.

#### **Extended Detention Basin B (Full Spectrum EDB)**

Water quality and detention for Basins EA6 – EA8 per the segment 1 FDR and EA9-10 per the segment 2 FDR is provided in Extended Detention Basin B; a public county owned, full spectrum extended detention basin within Filing No. 1 of Grandview Reserve within a proposed drainage easement. A total of 9.02 acres of disturbed area from the proposed project at 67% composite imperviousness will be treated and detained by EDB B for the ultimately developed Eastonville Road Improvements. Ultimate conditions include fully built sections of Eastonville Road from Londonderry Road to Rex Road and is anticipated for Spring 2025. Ultimate condition pond sizing calculations have also been provided in the Appendix of this report. The ultimate conditions WQCV is 0.197 ac-ft, the EURV is 0.756 ac-ft, and the 100-year detention volume is 1.119 ac-ft. The WQCV, EURV and 100-year storms are released in 40, 70 and 73 hours, respectively. A forebay is located at the outfall into the pond and a 40" trickle channel conveys flow towards the outlet structure. A 15' access and maintenance road is provided to the bottom of the pond to facilitate maintenance of the pond facilities. A 15.5' emergency overflow spillway is provided that conveys the developed, peak 100-yr flow rate with 1.0' of freeboard towards Gieck Ranch Tributary #1. EDB B outfalls towards DP8 at historic runoff rates. Runoff from DP8 will follow historic drainage patterns and not exceed historic flow rates.



### c. Inspection and Maintenance

After completion of construction and upon the Board of County Commissioners acceptance, it is anticipated that all drainage facilities within the public Right-of-Way are to be owned and maintained by El Paso County.

All public detention ponds are to be owned and maintained by El Paso County, once established, unless an agreement is reached stating otherwise. Maintenance access for all full spectrum detention facilities will be provided from public Right-of-Way. Maintenance access for the drainageways will be provided through the proposed tracts.

## V. Wetlands Mitigation

There is an existing wetland in Gieck Ranch Tributary #1 (Channel A). The wetland is contained entirely within the channel and is classified as jurisdictional. A Nationwide Wetland Permit will be applied for due to the disturbed area at the Dawlish Roundabout. Wetlands maintenance will be the responsibility of the DISTRICT.

## VI. Four Step Method to Minimize Adverse Impacts of Urbanization

Step 1 – Reducing Runoff Volumes: Low impact development (LID) practices are utilized to reduce runoff at the source. In general, stormwater discharges are routed across pervious areas prior to capture in storm sewer. This practice promotes infiltration and reduces peak runoff rates. The Impervious Reduction Factor (IRF) method was used and is presented in Appendix D.

Step 2 – Treat and slowly release the WQCV: This step utilizes full spectrum water quality and detention to capture the WQCV and slowly release runoff from the site. Onsite full spectrum detention pond provides water quality treatment for the site. The WQCV is released over a period of at least 12 hours for SFBs and 40 hours for EDBs while the EURV is released over a period of 40-44 hours for SFBs and 68 - 72 hours for EDBs as recommended by the MHFD.

Step 3 – Stabilize stream channels: This step establishes practices to stabilize drainageways and provide scour protection at stormwater outfalls. Erosion protection is provided at all concentrated stormwater discharge points in the form of riprap pads.

Step 4 – Consider the need for source controls: No industrial or commercial uses are proposed within this development and therefore no source controls are proposed.

## VII. Drainage and Bridge Fees

Gieck Ranch drainage basin has not been established as a fee basin within El Paso County. Therefore, no drainage basin fees are due at time of platting.

## VIII. Opinion of Probable Cost

An engineer's opinion of probable cost has been provided below for public and private drainage infrastructure improvements. This includes cost estimates for the public full spectrum sand filter basin C. All required stormwater infrastructure will be installed per El Paso County Requirements.

Public Infrastructure Cost Estimate			
Line Item	Quantity	Unit Price	Cost
18" Reinforced Concrete Pipe	290	\$76 LF	\$22,040
24" Reinforced Concrete Pipe	904	\$114 LF	\$103,056
48" Reinforced Concrete Pipe	1678	\$187 LF	\$313,786
18" CDOT FES	1	\$500 EA	\$500
24" CDOT FES	3	\$684 EA	\$2,052
48" CDOT FES	2	\$912 EA	\$1,824
6' DIA Storm Manhole	12	\$7,734 EA	\$92,808
CDOT Type D Inlet	1	\$6,931 EA	\$6,931
10' CDOT Type R Inlet	6	\$6,703 EA	\$40,218
Rip Rap, d50 size from 6"-24"	2	\$97 Tons	\$194
3' x 10' Concrete Box Culvert w/ Wingwalls	110	\$400 Tons	\$44,000
10% Contingency			\$62,741
<b>TOTAL:</b>			<b>\$690,150</b>

Public SFB C Cost Estimate			
Line Item	Quantity	Unit Price	Cost
Rip Rap, d50 size from 6"-24" (Inflow)	1.5	\$97 Tons	\$146
Sand Filter Media	44	\$100 /CY	\$4,400
4" Perforated PVC Underdrain	10	\$10 /LF	\$100
12" ABC Maintenance Access	19	\$40 /CY	\$760
Outlet Structure w/ Orifice Plate	1	\$5,000 EA	\$5,000
Rip Rap, d50 size from 6"-24" (Spillway)	19.5	\$97 Tons	\$1,892
18" RCP Outlet Pipe	180	\$60 /LF	\$10,800
18" RCP FES	1	\$350 EA	\$350
10% Contingency			\$2,345
<b>TOTAL:</b>			<b>\$25,792</b>

## IX. Hydraulic Grade Line Analysis

Hydraulic grade line analysis and final pipe sizes have been sized and calculations are provided in Appendix C. All proposed storm sewer will be designed in accordance with El Paso County Drainage Criteria Manuals.

## X. Summary

Eastonville Road lies within the Gieck Ranch Drainage Basin. Water quality and detention for the site is provided in full spectrum water quality and detention ponds, sand filters and temporary sediment basins. There is one major drainageway that traverses the site: Gieck Ranch Tributary 1. The water quality and



detention features ponds will be maintained by the Grandview Reserve Metropolitan District No. 2 (DISTRICT). All drainage facilities were sized per the El Paso County Drainage Criteria Manuals.

The development of this project will not adversely affect downstream properties.

## XI. Drawings

Please refer to the appendices for vicinity and drainage basin maps.

## XII. References

1. City of Colorado Springs – Drainage Criteria Manual, May 2014, Revised January 2021.
2. Drainage Criteria Manual of El Paso, Colorado, October 2018.
3. Urban Storm Drainage Criteria Manual, Urban Drainage Flood Control District, January 2018.
4. “Gieck Ranch Drainage Basin Planning Study” prepared by Drexel, Barrel & Co, February 2010.
5. “Master Development Drainage Plan Meridian Ranch” prepared by Tech Contractors, July 2021.
6. “The Sanctuary Filing 1 at Meridian Ranch” prepared by Tech Contactors, August 2022.

## **APPENDIX A – VICINITY MAP, PHOTOS, SOIL MAP, FEMA MAP**





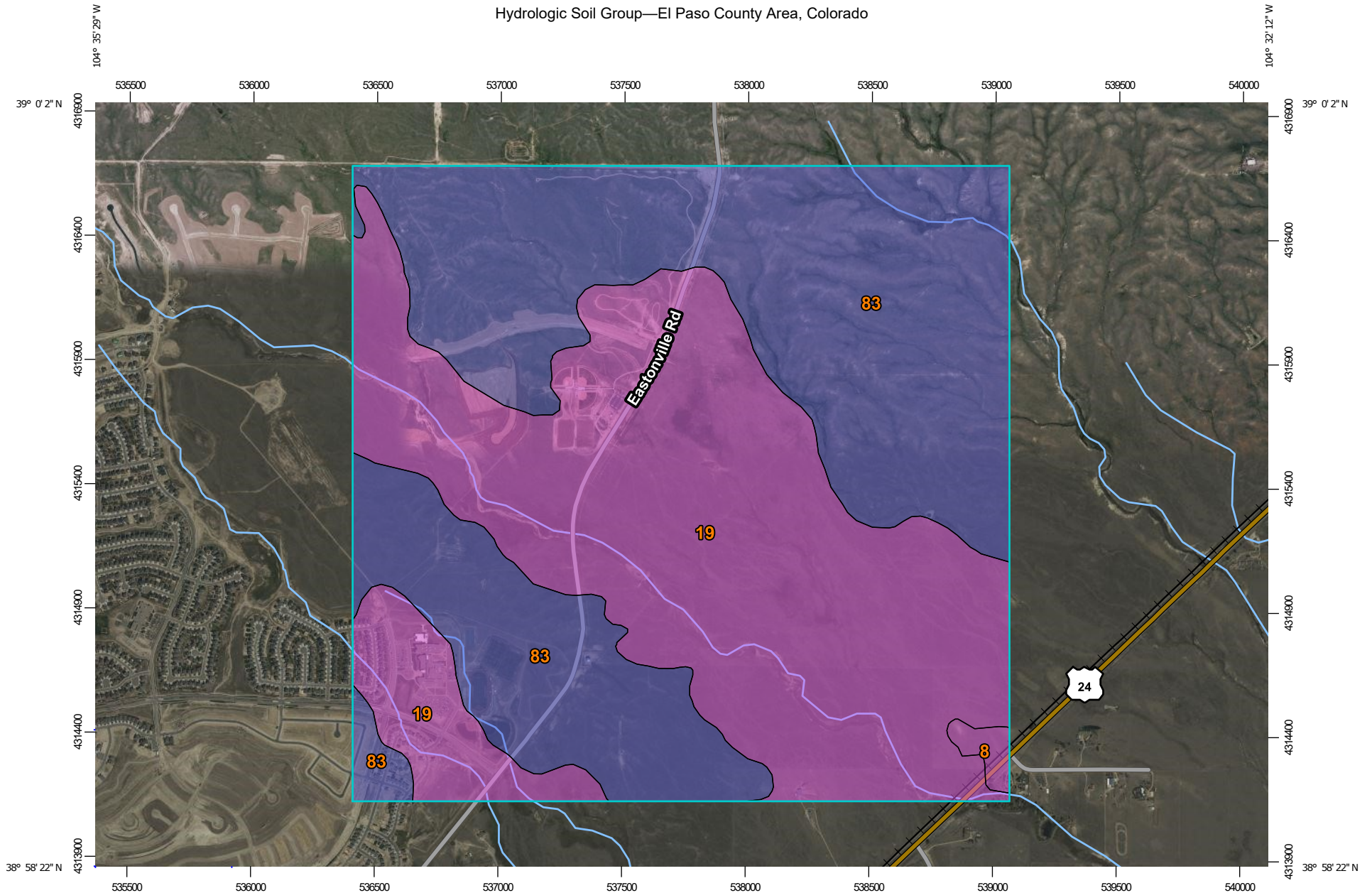


Photo - at Londonderry and Eastonville looking north

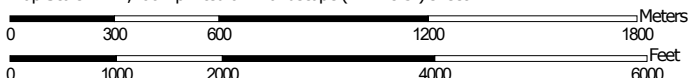




Hydrologic Soil Group—El Paso County Area, Colorado



Map Scale: 1:21,700 if printed on A landscape (11" x 8.5") sheet.




Map projection: Web Mercator Corner coordinates: WGS84 Edge tics: UTM Zone 13N WGS84



### MAP LEGEND

**Area of Interest (AOI)**









 Area of Interest (AOI)

**Soils**

**Soil Rating Polygons**





-  A
-  A/D
-  B
-  B/D
-  C
-  C/D
-  D
-  Not rated or not available

**Soil Rating Lines**

-  A
-  A/D
-  B
-  B/D
-  C
-  C/D
-  D
-  Not rated or not available

**Soil Rating Points**






-  A
-  A/D
-  B
-  B/D

-  C
-  C/D
-  D
-  Not rated or not available


**Water Features**

 Streams and Canals

**Transportation**

-  Rails
-  Interstate Highways
-  US Routes
-  Major Roads
-  Local Roads

**Background**

 Aerial Photography

### MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24,000.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service  
 Web Soil Survey URL:  
 Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: El Paso County Area, Colorado  
 Survey Area Data: Version 19, Aug 31, 2021

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Sep 11, 2018—Jun 12, 2021

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

## Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
8	Blakeland loamy sand, 1 to 9 percent slopes	A	10.4	0.6%
19	Columbine gravelly sandy loam, 0 to 3 percent slopes	A	839.5	49.8%
83	Stapleton sandy loam, 3 to 8 percent slopes	B	835.7	49.6%
<b>Totals for Area of Interest</b>			<b>1,685.6</b>	<b>100.0%</b>

### Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

## Rating Options

*Aggregation Method:* Dominant Condition

*Component Percent Cutoff:* None Specified

*Tie-break Rule:* Higher







**NOAA Atlas 14, Volume 8, Version 2**  
**Location name: Elbert, Colorado, USA\***  
**Latitude: 38.9796°, Longitude: -104.5696°**  
**Elevation: 6996 ft\*\***



\* source: ESRI Maps  
 \*\* source: USGS

**POINT PRECIPITATION FREQUENCY ESTIMATES**

Sanja Perica, Deborah Martin, Sandra Pavlovic, Ishani Roy, Michael St. Laurent, Carl Trypaluk, Dale Unruh, Michael Yekta, Geoffrey Bonnin

NOAA, National Weather Service, Silver Spring, Maryland

[PF tabular](#) | [PF graphical](#) | [Maps & aerals](#)

**PF tabular**

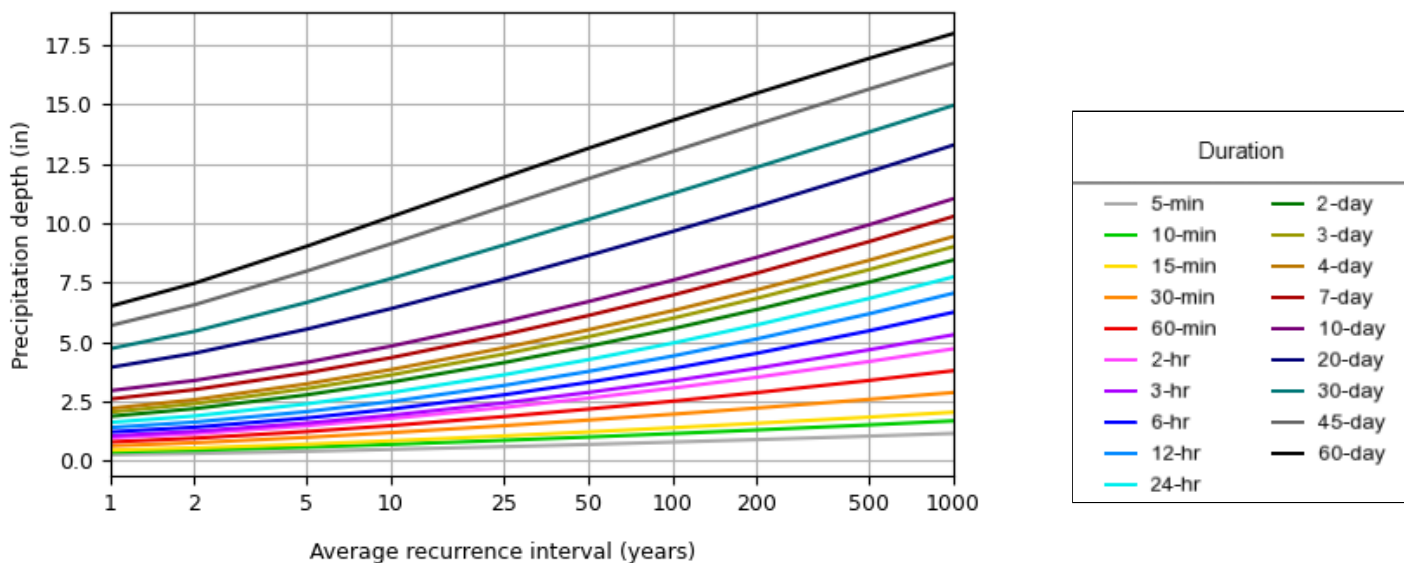
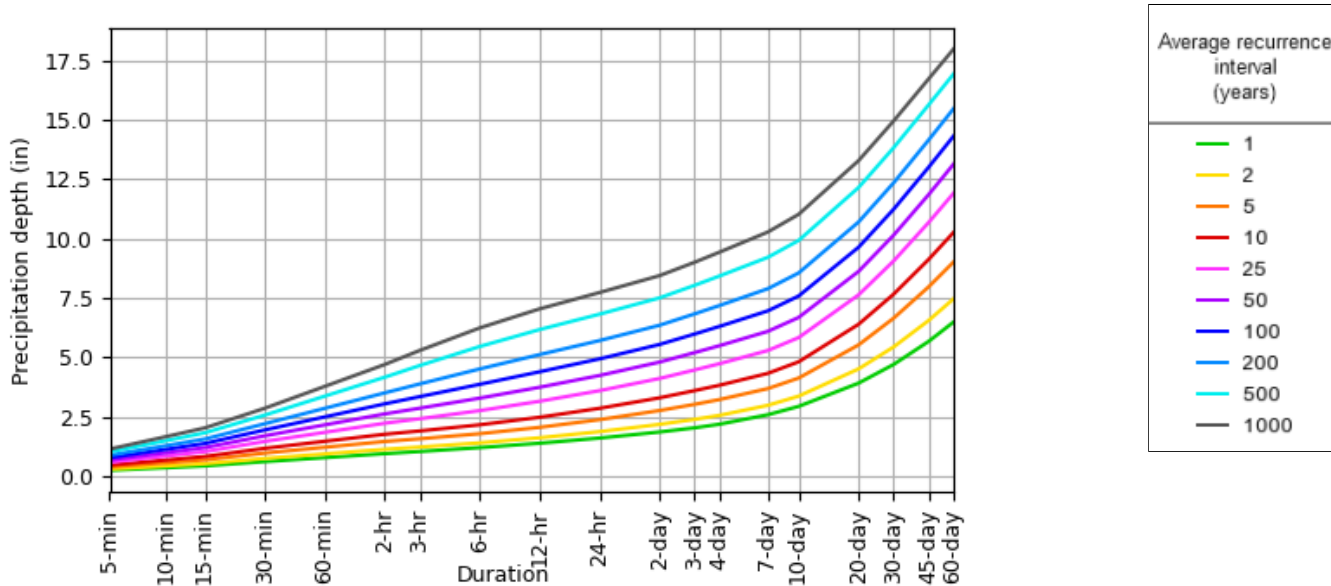
<b>PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches)<sup>1</sup></b>										
<b>Duration</b>	<b>Average recurrence interval (years)</b>									
	<b>1</b>	<b>2</b>	<b>5</b>	<b>10</b>	<b>25</b>	<b>50</b>	<b>100</b>	<b>200</b>	<b>500</b>	<b>1000</b>
<b>5-min</b>	<b>0.239</b> (0.189-0.303)	<b>0.291</b> (0.231-0.370)	<b>0.381</b> (0.301-0.486)	<b>0.461</b> (0.361-0.589)	<b>0.576</b> (0.440-0.768)	<b>0.671</b> (0.499-0.904)	<b>0.770</b> (0.554-1.06)	<b>0.875</b> (0.604-1.24)	<b>1.02</b> (0.678-1.48)	<b>1.14</b> (0.733-1.67)
<b>10-min</b>	<b>0.350</b> (0.277-0.444)	<b>0.426</b> (0.338-0.542)	<b>0.558</b> (0.441-0.711)	<b>0.674</b> (0.529-0.863)	<b>0.844</b> (0.644-1.12)	<b>0.982</b> (0.731-1.32)	<b>1.13</b> (0.811-1.56)	<b>1.28</b> (0.884-1.81)	<b>1.49</b> (0.992-2.17)	<b>1.66</b> (1.07-2.44)
<b>15-min</b>	<b>0.426</b> (0.338-0.541)	<b>0.520</b> (0.412-0.660)	<b>0.681</b> (0.537-0.867)	<b>0.823</b> (0.645-1.05)	<b>1.03</b> (0.785-1.37)	<b>1.20</b> (0.891-1.62)	<b>1.37</b> (0.988-1.90)	<b>1.56</b> (1.08-2.21)	<b>1.82</b> (1.21-2.65)	<b>2.03</b> (1.31-2.98)
<b>30-min</b>	<b>0.608</b> (0.482-0.771)	<b>0.740</b> (0.586-0.940)	<b>0.968</b> (0.764-1.23)	<b>1.17</b> (0.916-1.49)	<b>1.46</b> (1.11-1.94)	<b>1.70</b> (1.26-2.28)	<b>1.94</b> (1.40-2.68)	<b>2.20</b> (1.52-3.12)	<b>2.57</b> (1.71-3.73)	<b>2.86</b> (1.84-4.19)
<b>60-min</b>	<b>0.775</b> (0.615-0.984)	<b>0.933</b> (0.739-1.18)	<b>1.21</b> (0.956-1.54)	<b>1.46</b> (1.15-1.87)	<b>1.84</b> (1.41-2.47)	<b>2.16</b> (1.61-2.92)	<b>2.49</b> (1.80-3.45)	<b>2.85</b> (1.97-4.05)	<b>3.37</b> (2.24-4.90)	<b>3.78</b> (2.44-5.54)
<b>2-hr</b>	<b>0.943</b> (0.754-1.19)	<b>1.12</b> (0.898-1.42)	<b>1.46</b> (1.16-1.84)	<b>1.76</b> (1.39-2.23)	<b>2.22</b> (1.72-2.97)	<b>2.62</b> (1.97-3.52)	<b>3.04</b> (2.21-4.19)	<b>3.50</b> (2.45-4.95)	<b>4.16</b> (2.80-6.03)	<b>4.70</b> (3.06-6.85)
<b>3-hr</b>	<b>1.03</b> (0.829-1.29)	<b>1.22</b> (0.978-1.53)	<b>1.57</b> (1.25-1.97)	<b>1.90</b> (1.51-2.40)	<b>2.41</b> (1.88-3.22)	<b>2.86</b> (2.17-3.84)	<b>3.34</b> (2.45-4.60)	<b>3.88</b> (2.73-5.48)	<b>4.66</b> (3.15-6.74)	<b>5.29</b> (3.46-7.69)
<b>6-hr</b>	<b>1.20</b> (0.968-1.48)	<b>1.40</b> (1.13-1.74)	<b>1.78</b> (1.44-2.22)	<b>2.16</b> (1.73-2.70)	<b>2.76</b> (2.18-3.66)	<b>3.28</b> (2.52-4.39)	<b>3.86</b> (2.86-5.29)	<b>4.51</b> (3.20-6.34)	<b>5.46</b> (3.73-7.86)	<b>6.24</b> (4.12-9.01)
<b>12-hr</b>	<b>1.38</b> (1.13-1.70)	<b>1.61</b> (1.31-1.98)	<b>2.05</b> (1.66-2.53)	<b>2.48</b> (2.00-3.07)	<b>3.15</b> (2.51-4.15)	<b>3.74</b> (2.89-4.96)	<b>4.39</b> (3.28-5.96)	<b>5.12</b> (3.66-7.13)	<b>6.17</b> (4.25-8.82)	<b>7.04</b> (4.69-10.1)
<b>24-hr</b>	<b>1.60</b> (1.31-1.95)	<b>1.87</b> (1.54-2.28)	<b>2.38</b> (1.94-2.91)	<b>2.85</b> (2.32-3.51)	<b>3.60</b> (2.88-4.67)	<b>4.24</b> (3.29-5.56)	<b>4.94</b> (3.71-6.63)	<b>5.71</b> (4.12-7.87)	<b>6.82</b> (4.73-9.66)	<b>7.73</b> (5.20-11.0)
<b>2-day</b>	<b>1.85</b> (1.54-2.24)	<b>2.18</b> (1.80-2.63)	<b>2.76</b> (2.28-3.34)	<b>3.29</b> (2.70-4.01)	<b>4.11</b> (3.30-5.27)	<b>4.80</b> (3.76-6.22)	<b>5.54</b> (4.19-7.36)	<b>6.35</b> (4.62-8.68)	<b>7.50</b> (5.25-10.5)	<b>8.44</b> (5.73-11.9)
<b>3-day</b>	<b>2.03</b> (1.69-2.44)	<b>2.39</b> (1.98-2.87)	<b>3.02</b> (2.50-3.64)	<b>3.60</b> (2.97-4.36)	<b>4.47</b> (3.60-5.69)	<b>5.20</b> (4.08-6.70)	<b>5.98</b> (4.55-7.90)	<b>6.83</b> (4.99-9.28)	<b>8.03</b> (5.65-11.2)	<b>9.00</b> (6.15-12.7)
<b>4-day</b>	<b>2.18</b> (1.82-2.61)	<b>2.56</b> (2.13-3.06)	<b>3.22</b> (2.68-3.87)	<b>3.82</b> (3.16-4.62)	<b>4.73</b> (3.83-6.00)	<b>5.49</b> (4.33-7.04)	<b>6.30</b> (4.81-8.30)	<b>7.18</b> (5.26-9.72)	<b>8.43</b> (5.94-11.7)	<b>9.43</b> (6.46-13.3)
<b>7-day</b>	<b>2.58</b> (2.17-3.07)	<b>2.98</b> (2.50-3.54)	<b>3.68</b> (3.08-4.39)	<b>4.32</b> (3.60-5.18)	<b>5.29</b> (4.30-6.65)	<b>6.09</b> (4.84-7.76)	<b>6.96</b> (5.34-9.09)	<b>7.89</b> (5.82-10.6)	<b>9.21</b> (6.55-12.8)	<b>10.3</b> (7.10-14.4)
<b>10-day</b>	<b>2.93</b> (2.48-3.47)	<b>3.36</b> (2.84-3.98)	<b>4.13</b> (3.47-4.90)	<b>4.81</b> (4.02-5.74)	<b>5.83</b> (4.76-7.28)	<b>6.68</b> (5.32-8.45)	<b>7.58</b> (5.85-9.86)	<b>8.55</b> (6.34-11.4)	<b>9.92</b> (7.08-13.7)	<b>11.0</b> (7.65-15.4)
<b>20-day</b>	<b>3.91</b> (3.33-4.58)	<b>4.51</b> (3.84-5.29)	<b>5.52</b> (4.68-6.50)	<b>6.39</b> (5.39-7.55)	<b>7.63</b> (6.25-9.37)	<b>8.62</b> (6.90-10.8)	<b>9.64</b> (7.47-12.4)	<b>10.7</b> (7.98-14.1)	<b>12.2</b> (8.74-16.6)	<b>13.3</b> (9.31-18.4)
<b>30-day</b>	<b>4.70</b> (4.02-5.47)	<b>5.44</b> (4.65-6.34)	<b>6.65</b> (5.66-7.78)	<b>7.66</b> (6.49-9.00)	<b>9.06</b> (7.44-11.0)	<b>10.1</b> (8.15-12.5)	<b>11.2</b> (8.74-14.3)	<b>12.3</b> (9.24-16.2)	<b>13.8</b> (9.98-18.7)	<b>15.0</b> (10.5-20.6)
<b>45-day</b>	<b>5.67</b> (4.88-6.57)	<b>6.55</b> (5.63-7.60)	<b>7.97</b> (6.82-9.27)	<b>9.12</b> (7.77-10.7)	<b>10.7</b> (8.79-12.9)	<b>11.9</b> (9.56-14.5)	<b>13.0</b> (10.2-16.4)	<b>14.2</b> (10.6-18.4)	<b>15.6</b> (11.3-21.0)	<b>16.7</b> (11.9-23.0)
<b>60-day</b>	<b>6.48</b> (5.60-7.48)	<b>7.46</b> (6.43-8.62)	<b>9.01</b> (7.74-10.4)	<b>10.3</b> (8.77-11.9)	<b>11.9</b> (9.82-14.3)	<b>13.1</b> (10.6-16.0)	<b>14.3</b> (11.2-18.0)	<b>15.5</b> (11.7-20.0)	<b>16.9</b> (12.3-22.6)	<b>18.0</b> (12.8-24.6)

<sup>1</sup> Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS). Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values. Please refer to NOAA Atlas 14 document for more information.

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**PF graphical**

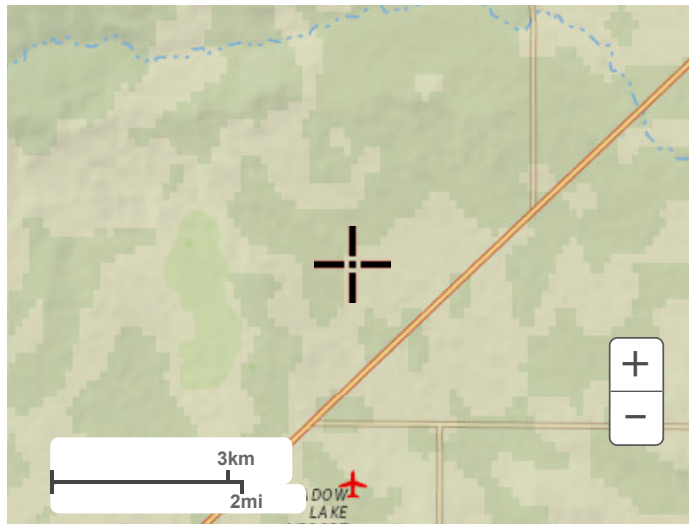
PDS-based depth-duration-frequency (DDF) curves  
 Latitude: 38.9796°, Longitude: -104.5696°



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**Maps & aerials**

**Small scale terrain**



Large scale terrain

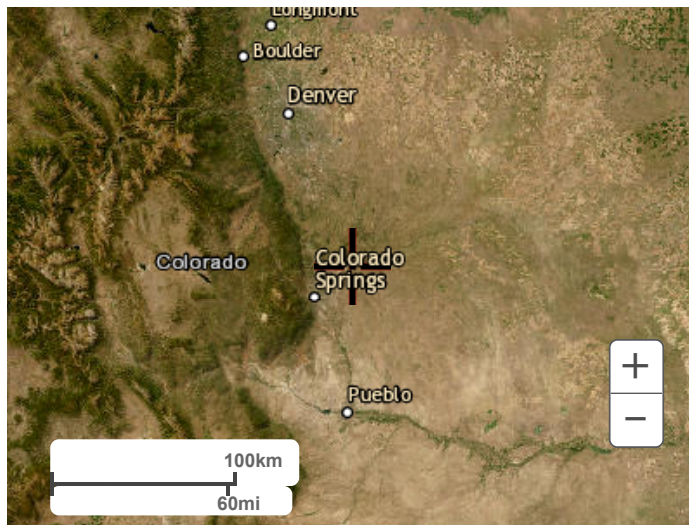


Large scale map



Large scale aerial





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[US Department of Commerce](#)  
[National Oceanic and Atmospheric Administration](#)  
[National Weather Service](#)  
[National Water Center](#)  
1325 East West Highway  
Silver Spring, MD 20910  
Questions?: [HDSC.Questions@noaa.gov](mailto:HDSC.Questions@noaa.gov)

[Disclaimer](#)

## **APPENDIX B – HYDROLOGIC CALCULATIONS**



<b>EASTONVILLE ROAD</b>	<b>Calc'd by:</b>	<b>SPC</b>
<b>EXISTING CONDITIONS</b>	<b>Checked by:</b>	<b>CM</b>
<b>EL PASO COUNTY, CO</b>	<b>Date:</b>	<b>8/28/2024</b>

SUMMARY RUNOFF TABLE				
BASIN	AREA (ac)	% IMPERVIOUS	Q <sub>5</sub> (cfs)	Q <sub>100</sub> (cfs)
G18*	321.53	-	28.3	365.2
FG36*	18.88	-	1.7	18.8
G16*	131.26	-	6.1	112.1
G06*	832.70	-	22.4	491.0
EX5	12.19	2	2.7	18.0
EX6	0.61	2	0.1	0.9
EX7	1.90	2	0.4	2.5
EX8	2.86	2	0.6	4.0

DESIGN POINT SUMMARY TABLE			
DESIGN POINT	CONTRIBUTING BASINS	ΣQ <sub>5</sub> (cfs)	ΣQ <sub>100</sub> (cfs)
1	G18*	28.3	365.2
2	FG36*	1.7	18.8
3	G16*	6.1	112.1
4	G06*	22.4	491.0
O3	EX7	6.5	114.6
O3.1	EX7	0.1	0.9
O4	EX7	23.0	495.0
13.1	EX7	2.7	18.0

\* AREA AND Q TAKEN FROM THE SANCTUARY FILING 1 FDR



**EASTONVILLE ROAD**

**EXISTING CONDITIONS**

**EL PASO COUNTY, CO**

**Calc'd by:**

**SPC**

**Checked by:**

**CM**

**Date:**


**8/28/2024**

**COMPOSITE 'C' FACTORS**

BASIN	UNDEVELOPED	WALKS & DRIVES	SINGLE FAMILY	TOTAL	SOIL TYPE	UNDEVELOPED			WALKS & DRIVES			SINGLE FAMILY			COMPOSITE IMPERVIOUSNESS & C			
	ACRES					%I	C <sub>5</sub>	C <sub>100</sub>	%I	C <sub>5</sub>	C <sub>100</sub>	%I	C <sub>5</sub>	C <sub>100</sub>	%I	C <sub>5</sub>	C <sub>100</sub>	
EX1 - EX4*																		
EX5	12.19	0.00	0.00	12.19	A/B	2	0.09	0.36	100	0.90	0.96	65	0.73	0.81	2	0.09	0.36	
EX6	0.61	0.00	0.00	0.61	A/B	2	0.09	0.36	100	0.90	0.96	65	0.73	0.81	2	0.09	0.36	
EX7	1.90	0.00	0.00	1.90	A/B	2	0.09	0.36	100	0.90	0.96	65	0.73	0.81	2	0.09	0.36	
EX8	2.86	0.00	0.00	2.86	A/B	2	0.09	0.36	100	0.90	0.96	65	0.73	0.81	2	0.09	0.36	

\* FLOWS TO DESIGN POINTS 1-4 WERE TAKEN FROM "THE SANCTUARY FILING 1 FDR" SO C WAS NOT CALCULATED FOR CONTRIBUTING AREAS EX1 - EX4



	<b>EASTONVILLE ROAD</b>	<b>Calc'd by:</b>	<b>SPC</b>
	<b>EXISTING CONDITIONS</b>	<b>Checked by:</b>	<b>CM</b>
	<b>EL PASO COUNTY, CO</b>	<b>Date:</b>	<b>8/28/2024</b>

**TIME OF CONCENTRATION**

BASIN DATA			OVERLAND TIME (T <sub>i</sub> )			TRAVEL TIME (T <sub>t</sub> )					TOTAL
DESIGNATION	C <sub>s</sub>	AREA (ac)	LENGTH (ft)	SLOPE %	t <sub>i</sub> (min)	C <sub>v</sub>	LENGTH (ft)	SLOPE %	V (ft/s)	t <sub>t</sub> (min)	t <sub>c</sub> (min)
EX1-EX4*											
EX5	0.09	12.19	300	2.8	22.8	10	835	3.0	1.7	8.0	30.8
EX6	0.09	0.61	180	1.3	22.8	10	411	1.6	1.3	5.4	28.2
EX7	0.09	1.90	116	1.5	17.4	10	1137	1.0	1.0	19.0	36.4
EX8	0.09	2.86	60	1.4	12.8	10	1302	1.1	1.0	20.7	33.5

\* FLOWS TO THESE DESIGN POINTS WERE TAKEN FROM "THE SANCTUARY FILING 1 FDR" SO TC WAS NOT CALCULATED FOR CONTRIBUTING AREAS EX1 - EX4

**FORMULAS:**

$$t_i = \frac{0.395(1.1 - C_s)\sqrt{L}}{S^{0.33}} \quad V = C_v S_w^{0.5}$$

**Table 6-7. Conveyance Coefficient, C<sub>v</sub>**

Type of Land Surface	C <sub>v</sub>
Heavy meadow	2.5
Tillage/field	5
Riprap (not buried)*	6.5
Short pasture and lawns	7
Nearly bare ground	10
Grassed waterway	15
Paved areas and shallow paved swales	20

\* For buried riprap, select C<sub>v</sub> value based on type of vegetative cover.



**EASTONVILLE ROAD**  
**EXISTING CONDITIONS**  
**DESIGN STORM: 5-YEAR**

Calc'd by:

SPC

Checked by:

CM

Date:

8/28/2024

STREET	DESIGN POINT	BASIN ID	DIRECT RUNOFF					TOTAL RUNOFF				STREET			PIPE			TRAVEL TIME			REMARKS		
			AREA (ac)	C <sub>s</sub>	t <sub>c</sub> (min)	C <sub>s</sub> *A (ac)	I (in./hr.)	Q (cfs)	t <sub>c</sub> (min)	C <sub>s</sub> *A (ac)	I (in./hr.)	Q (cfs)	Q <sub>street</sub> (cfs)	C <sub>s</sub> *A (ac)	SLOPE %	Q <sub>PIPE</sub> (cfs)	C <sub>s</sub> *A (ac)	SLOPE %	PIPE SIZE (in)	LENGTH (FT)		VEL. (FPS)	TRAVEL TIME (min)
	1	G18*	321.53							28.3													DP 1 CAPTURED IN GIECK RANCH TRIB #2 (CHANNEL B)
	2	FG36*	18.88							1.7													DP 2 CAPTURED IN 24" RCP CULVERT, PIPED TO BASIN EX3
	* AREA AND Q TAKEN FROM THE SANCTUARY FILING 1 FDR																						
	3	G16*	131.26							6.1													BASIN EX2, DP2 & DPG15 (SANCTUARY FDR Q5=3 CFS) CAPTURED IN 24" CMP CULVERT, PIPED ACROSS EASTONVILLE ROAD
	4	G06*	832.70							22.4													BASIN EX4 & DPG12 (SANCTUARY FDR Q5 = 21 CFS) CAPTURED IN 18" CMP CULVERT, PIPED ACROSS EASTONVILLE ROAD TO GIECK RANCH TRIB #1 (CHANNEL A)
																							* AREA AND Q TAKEN FROM THE SANCTUARY FILING 1 FDR
	O3	EX7	1.90	0.09	36.4	0.17	2.19	0.4		6.5													* TOTAL FLOW INCLUDES Q TAKEN FROM DP3 FROM THE SANCTUARY FILING 1 FDR
	O3.1	EX6	0.61	0.09	28.2	0.05	2.58	0.1		0.1													
	O4	EX8	2.86	0.09	33.5	0.26	2.32	0.6		23.0													* TOTAL FLOW INCLUDES Q TAKEN FROM DP4 FROM THE SANCTUARY FILING 1 FDR
	13.1	EX5	12.19	0.09	30.8	1.10	2.44	2.7		2.7													



**EASTONVILLE ROAD**  
**EXISTING CONDITIONS**  
**DESIGN STORM: 100-YEAR**

Calc'd by: **SCP**  
 Checked by: **CM**  
 Date: **8/28/2024**

STREET	DESIGN POINT	BASIN ID	DIRECT RUNOFF					TOTAL RUNOFF				STREET			PIPE			TRAVEL TIME			REMARKS		
			AREA (ac)	C <sub>100</sub>	t <sub>c</sub> (min)	C <sub>100</sub> *A (ac)	f (in./hr.)	Q (cfs)	t <sub>c</sub> (min)	C <sub>100</sub> *A (ac)	f (in./hr.)	Q (cfs)	Q <sub>street</sub> (cfs)	C <sub>100</sub> *A (ac)	SLOPE %	Q <sub>PIPE</sub> (cfs)	C <sub>100</sub> *A (ac)	SLOPE %	PIPE SIZE (ft)	LENGTH (ft)		VEL. (ft/s)	TRAVEL TIME (min)
	1	G18*	321.53							365.2													DP 1 CAPTURED IN GIECK RANCH TRIB #2 (CHANNEL B)
	2	FG36*	18.88							18.8													DP 2 CAPTURED IN 24" RCP CULVERT, PIPED TO BASIN EX3
	* AREA AND Q TAKEN FROM THE SANCTUARY FILING 1 FDR																						
	3	G16*	131.26							112.1													BASIN EX2, DP2 & DPG15 (SANCTUARY FDR Q5=3 CFS) CAPTURED IN 24" CMP CULVERT, PIPED ACROSS EASTONVILLE ROAD
	4	G06*	832.70							491.0													BASIN EX4 & DPG12 (SANCTUARY FDR Q5 = 21 CFS) CAPTURED IN 18" CMP CULVERT, PIPED ACROSS EASTONVILLE ROAD TO GIECK RANCH TRIB #1 (CHANNEL A)
																							* AREA AND Q TAKEN FROM THE SANCTUARY FILING 1 FDR
	O3	EX7	1.90	0.36	36.4	0.68	3.68	2.5		114.6													* TOTAL FLOW INCLUDES Q TAKEN FROM DP3 FROM THE SANCTUARY FILING 1 FDR
	O3.1	EX6	0.61	0.36	28.2	0.22	4.32	0.9		0.9													
	O4	EX8	2.86	0.36	33.5	1.03	3.89	4.0		495.0													* TOTAL FLOW INCLUDES Q TAKEN FROM DP4 FROM THE SANCTUARY FILING 1 FDR
	13.1	EX5	12.19	0.36	30.8	4.39	4.10	18.0		18.0													



**EASTONVILLE ROAD SEG 2**  
**PROPOSED CONDITIONS**  
**EL PASO COUNTY, CO**

**Calc'd by:** SPC  
**Checked by:** CM  
**Date:** 8/28/2024

SUMMARY RUNOFF TABLE				
BASIN	AREA (ac)	% IMPERVIOUS	Q <sub>5</sub> (cfs)	Q <sub>100</sub> (cfs)
EA1	0.22	73	0.8	1.5
EA2	0.25	72	0.9	1.7
EA3	0.20	70	0.7	1.3
EA4	0.17	65	0.5	1.1
EA5	0.16	0	0.1	0.4
EA6	0.25	76	0.8	1.4
EA7	0.20	50	0.4	1.0
EA8	2.08	99	5.2	8.8
EA9	3.14	60	5.0	10.6
EA10	0.16	75	0.6	1.1
EA11	0.15	67	0.5	1.0
EA12	0.34	0	0.1	1.0
EA13	0.45	73	1.4	2.8
EA14	1.48	21	1.2	3.8
EA15	0.76	24	0.7	2.1
EA16	1.18	0	0.3	2.5
EA17	0.30	0	0.1	0.7
*G18	321.53	-	28.3	365.2
*FG36	18.88	-	1.7	18.8
OS3	1.00	2	0.3	2.2
OS4	9.60	9	4.8	21.6
*G16	131.26	-	6.1	112.1
*G06	832.70	-	22.4	491.0
OS7	11.29	3	3.9	24.6

\* AREA AND Q TAKEN FROM THE SANCTUARY FILING 1 FDR

DESIGN POINT SUMMARY TABLE			
DESIGN POINT	CONTRIBUTING BASINS	ΣQ <sub>5</sub> (cfs)	ΣQ <sub>100</sub> (cfs)
1	G18	28.3	365.2
2	FG36	1.7	18.8
2.1	EA1	0.8	1.5
3	G16	6.1	112.1
3.1	EA2, DP2.1	1.6	3.2
4	G06	22.4	491.0
4.1	EA5, DP3.1	1.7	3.4
5	EA3	0.7	1.3
6	DP5, EA4	1.2	2.4
6.1	DP6, DP8	2.9	22.4
7	OS3	0.3	2.2
8	DP2, DP7	2.0	21.0
9	DP6.1	2.9	22.4
10	EA6, EA7	1.2	2.3
11	OS4, DP9	7.5	44.0
12	OS7	3.9	24.6
13	DP11.1, DP12	10.0	180.6
14	EA8	5.2	8.8
15	EA9	5.0	10.6
15.1	DP14, DP15	10.2	19.3
16.1	EA10	0.6	1.1
17.1	EA11	0.5	1.0
O3	EA15	0.7	2.1
O3.1	-	0.0	0.0
O4	EA12, DP4	22.5	492.0
O4.1	EA13	1.4	2.8
O4.2	EA14	1.2	3.8
10.1	EA17	0.1	0.7
11.1	DP3, DP11	13.6	156.1
13.1	EA16, DP13	0.3	183.1



**EASTONVILLE ROAD SEG 2**  
**PROPOSED CONDITIONS**  
 EL PASO COUNTY, CO

**Calc'd by:** SPC  
**Checked by:** CM  
**Date:** 11/27/2023

**SOIL TYPE: HSG A&B**

**COMPOSITE 'C' FACTORS**

BASIN	LAND USE TYPE															TOTAL ACRES	COMPOSITE IMPERVIOUSNESS & C FACTOR		
	Paved			Historic Flow Analysis-- Greenbelts, Agriculture			Lawns			Gravel			Drive and Walks				%I	C <sub>5</sub>	C <sub>100</sub>
	%I	C <sub>5</sub>	C <sub>100</sub>	%I	C <sub>5</sub>	C <sub>100</sub>	%I	C <sub>5</sub>	C <sub>100</sub>	%I	C <sub>5</sub>	C <sub>100</sub>	%I	C <sub>5</sub>	C <sub>100</sub>				
	100	0.90	0.96	2	0.09	0.36	0	0.08	0.35	80	0.59	0.70	100	0.90	0.96				
ACRES			ACRES			ACRES			ACRES			ACRES							
EA1	0.16						0.06									0.22	73	0.68	0.79
EA2	0.18						0.07									0.25	72	0.67	0.79
EA3	0.14						0.06									0.20	70	0.65	0.78
EA4	0.11						0.06									0.17	65	0.61	0.74
EA5	0.00						0.16									0.16	0	0.08	0.35
EA6	0.19						0.06									0.25	76	0.71	0.82
EA7	0.10						0.10									0.20	50	0.49	0.65
EA8	2.06						0.02									2.08	99	0.89	0.95
EA9	1.88						1.26									3.14	60	0.57	0.72
EA10	0.12						0.04									0.16	75	0.70	0.81
EA11	0.10						0.05									0.15	67	0.63	0.76
EA12							0.34									0.34	0	0.08	0.35
EA13	0.33						0.12									0.45	73	0.68	0.80
EA14							1.16			0.07			0.25			1.48	21	0.24	0.47
EA15							0.57			0.04			0.15			0.76	24	0.27	0.49
EA16							1.18									1.18	0	0.08	0.35
EA17							0.30									0.30	0	0.08	0.35
G18																321.53			
FG36																18.88			
OS3				1.00												1.00	2	0.09	0.36
OS4	0.70			8.90												9.60	9	0.15	0.40
OS5				40.26												40.26	2	0.09	0.36
G16																131.26			
G06																832.70			
OS7				11.16						0.03			0.10			11.29	3	0.10	0.37
SFB C	0.34			0.00			0.29									0.63	54		

### COMPOSITE 'C' FACTORS

<b>BASIN</b>	<b>LAND USE TYPE</b>															<b>TOTAL</b>	<b>COMPOSITE IMPERVIOUSNESS &amp; C FACTOR</b>		
	<b>Paved</b>			<b>Historic Flow Analysis-- Greenbelts, Agriculture</b>			<b>Lawns</b>			<b>Gravel</b>			<b>Drive and Walks</b>						
	%I	C <sub>5</sub>	C <sub>100</sub>	%I	C <sub>5</sub>	C <sub>100</sub>	%I	C <sub>5</sub>	C <sub>100</sub>	%I	C <sub>5</sub>	C <sub>100</sub>	%I	C <sub>5</sub>	C <sub>100</sub>				
	100	0.90	0.96	2	0.09	0.36	0	0.08	0.35	80	0.59	0.70	100	0.90	0.96				
<b>ACRES</b>			<b>ACRES</b>			<b>ACRES</b>			<b>ACRES</b>			<b>ACRES</b>			<b>ACRES</b>	%I	C <sub>5</sub>	C <sub>100</sub>	
EDB B	5.92			0.00			2.99			0.09			0.01			9.02	67		



**EASTONVILLE ROAD SEG 2**

**PROPOSED CONDITIONS**

**EL PASO COUNTY, CO**

**Calc'd by:**

**SPC**

**Checked by:**

**CM**

**Date:**

**8/28/2024**

**TIME OF CONCENTRATION**


BASIN DATA			OVERLAND TIME (T <sub>i</sub> )			TRAVEL TIME (T <sub>t</sub> )					TOTAL
DESIGNATION	C <sub>s</sub>	AREA (ac)	LENGTH (ft)	SLOPE %	t <sub>i</sub> (min)	C <sub>v</sub>	LENGTH (ft)	SLOPE %	V (ft/s)	t <sub>t</sub> (min)	t <sub>c</sub> (min)
EA1	0.68	0.22	34	2.0	3.6	20	137	1.4	2.4	1.0	5.0
EA2	0.67	0.25	34	2.0	3.6	20	60	1.4	2.4	0.4	5.0
EA3	0.65	0.20	34	2.0	3.8	20	126	1.4	2.4	0.9	5.0
EA4	0.61	0.17	34	2.0	4.2	20	126	3.8	3.9	0.5	5.0
EA5	0.08	0.16	20	2.0	6.6	20	20	33.0	11.5	0.0	6.7
EA6	0.71	0.25	26	2.0	2.9	20	630	1.7	2.6	4.0	7.0
EA7	0.49	0.20	24	2.0	4.4	20	630	1.7	2.6	4.0	8.4
EA8	0.89	2.08	26	2.0	1.5	20	2500	0.7	1.7	24.9	26.4
EA9	0.57	3.14	26	2.0	3.9	20	2500	0.7	1.7	24.9	28.8
EA10	0.70	0.16	26	2.0	3.0	20	157	0.6	1.5	1.7	5.0
EA11	0.63	0.15	26	2.0	3.5	20	157	0.6	1.5	1.7	5.2
EA12	0.08	0.34	30	25.0	3.5	10	0	0.0	0.0	0.0	5.0
EA13	0.68	0.45	76	2.0	5.3	10	115	2.0	1.4	1.4	6.7
EA14	0.24	1.48	50	10.0	5.2	10	1300	1.1	1.0	20.7	25.8
EA15	0.27	0.76	50	10.0	5.0	10	1137	1.0	1.0	19.0	24.0
EA16	0.08	1.18	300	3.0	22.5	10	500	3.0	1.7	4.8	27.3
EA17	0.08	0.30	89	5.0	10.3	10	0	0.0	0.0	0.0	10.3
G18											
FG36											
OS3	0.09	1.00	220	2.1	21.4	10	345	2.3	1.5	3.8	25.2
OS4	0.15	9.60	153	3.1	14.8	10	1124	2.5	1.6	11.8	26.6
OS5	0.09	40.26	300	2.7	23.0	10	1400	2.7	1.6	14.2	37.2
G16											
G06											
OS7	0.10	11.29	200	11.6	11.5	10	675	3.4	1.8	6.1	17.6

**FORMULAS:**

$$t_i = \frac{0.395(1.1 - C_s)\sqrt{L}}{S^{0.33}} \quad V = C_v S_w^{0.5}$$

**Table 6-7. Conveyance Coefficient, C<sub>v</sub>**

Type of Land Surface	C <sub>v</sub>
Heavy meadow	2.5
Tillage/field	5

	<b>EASTONVILLE ROAD SEG 2</b>	<b>Calc'd by:</b>	<b>SPC</b>
	<b>PROPOSED CONDITIONS</b>	<b>Checked by:</b>	<b>CM</b>
	<b>EL PASO COUNTY, CO</b>	<b>Date:</b>	<b>8/28/2024</b>

**TIME OF CONCENTRATION**

BASIN DATA			OVERLAND TIME ( $T_i$ )			TRAVEL TIME ( $T_t$ )					TOTAL
DESIGNATION	$C_5$	AREA (ac)	LENGTH (ft)	SLOPE %	$t_i$ (min)	$C_v$	LENGTH (ft)	SLOPE %	V (ft/s)	$t_t$ (min)	$t_c$ (min)

Riprap (not buried)*	6.5
Short pasture and lawns	7
Nearly bare ground	10
Grassed waterway	15
Paved areas and shallow paved swales	20

\*For buried riprap, select  $C_v$  value based on type of vegetative cover.





**EASTONVILLE ROAD SEG 2**

**PROPOSED CONDITIONS**

**DESIGN STORM: 5-YEAR**

Calc'd by:

SPC

Checked by:

CM

Date:

8/28/2024

STREET	DESIGN POINT	BASIN ID	DIRECT RUNOFF				TOTAL RUNOFF				STREET			PIPE			TRAVEL TIME			REMARKS			
			AREA (ac)	C <sub>s</sub>	t <sub>c</sub> (min)	C <sub>s</sub> *A (ac)	I (in./hr.)	Q (cfs)	t <sub>c</sub> (min)	C <sub>s</sub> *A (ac)	I (in./hr.)	Q (cfs)	Q <sub>street</sub> (cfs)	C <sub>s</sub> *A (ac)	SLOPE %	Q <sub>PIPE</sub> (cfs)	C <sub>s</sub> *A (ac)	SLOPE %	PIPE SIZE (ft)		LENGTH (FT)	VEL. (FPS)	TRAVEL TIME (min)
	1	G18	321.53							28.3													
	2	FG36	18.88							1.7													
	2.1	EA1	0.22	0.68	5.0	0.15	5.17	0.8	5.0	0.15	5.17	0.8		0.8	0.15	1.0	1.5	56	5.9	0.16		BASIN EA1 CAPTURED IN 5' TYPE R INLET @ DP2, PIPE TO DP3.1	
	3	G16								6.1													
	3.1	EA2	0.25	0.67	5.0	0.17	5.17	0.9	5.0	0.32	5.17	1.6		1.6	0.32	5.1	1.5	34	13.4	0.04		BASIN EA2 CAPTURED IN 5' TYPE R INLET @ DP3, PIPE TO DP3.1	
	4	G06								22.4													
	4.1	EA5	0.16	0.08	6.7	0.01	4.74	0.1	6.7	0.33	5.17	1.7											COMBINED DP2.1 & DP3.1 @ DP3.1, PIPE TO DP4 (POND A)
	5	EA3	0.20	0.65	5.0	0.13	5.17	0.7	5.0	0.13	5.17	0.7		0.7	0.13	0.5	1.3	48	3.7	0.21		BASIN EA3 CAPTURED IN 5' TYPE R INLET @ DP5, PIPE TO DP6.1	
	6	EA4	0.17	0.61	5.0	0.10	5.17	0.5	5.2	0.23	5.11	1.2		1.2	0.23	2.4	1.3	43	8.1	0.09		BASIN EA4 CAPTURED IN 5' TYPE R INLET @ DP6, PIPE TO DP6.1	
	6.1								13.2	0.32	3.71	2.9		2.9	0.32	1.0	2.0	61	7.2	0.14		DP6 & DP8 FLOW @ DP6.1, PIPE TO DP9	
	7	OS3	1.00	0.09	13.1	0.09	3.72	0.3	13.1	0.09	3.72	0.3		0.3	0.09	0.8	2.0	43	6.4	0.11		BASIN OS3 CAPTURED IN 15" FES, PIPE TO DP8	
	8	OS3	1.00	0.09	13.1	0.09	3.72	0.3	13.1	0.09	3.72	2.0		2.0	0.09	1.5	1.3	38	6.4	0.10		DP2 & DP7 FLOW @ DP8, PIPE TO DP9	
	9								13.2	0.32	3.71	2.9	2.9	0.32	2.1			615	2.9	3.56		DP6.1 @ DP9, DISCHARGE TO ROADSIDE SWALE TO DP11	
	10	EA6	0.25	0.71	7.0	0.18	4.67	0.8	8.4	0.28	4.39	1.2											BASIN EA6 & EA7 @ DP10 (TEMPORARY SEDIMENT BASIN #1)
		EA7	0.20	0.49	8.4	0.10	4.39	0.4															
	11	OS4	9.60	0.15	17.1	1.43	3.32	4.8	17.1	1.76	3.32	7.5		7.5	1.76	2.0	2.0	85	10.2	0.14		BASIN OS4, DP9.1 CAPTURED & MERIDIAN RANCH DPG15 (3 CFS) IN TYPE D INLET AT DP11	
	12	OS7	11.29	0.10	14.9	1.12	3.53	3.9	14.9	1.12	3.53	3.9		3.9	1.12	1.0	1.5	28	5.9	0.08		BASIN OS7 CAPTURED @ DP12 IN TYPE C INLET, PIPE TO DP13	
	13								14.9	1.12	3.53	10.0											COMBINED DP3 & DP12, PIPE TO CHANNEL B
	14	EA8	2.08	0.89	24.0	1.86	2.81	5.2	24.0	1.86	2.81	5.2		5.2	1.86	7.0	1.5	8	15.7	0.01		BASIN EA8 CAPTURED IN 10' TYPE R SUMP @ DP14, PIPE TO DP15.1	
	15	EA9	3.14	0.57	24.0	1.79	2.81	5.0	24.0	1.79	2.81	5.0		5.0	1.79	1.8	1.5	54	7.9	0.11		BASIN EA8 CAPTURED IN 10' TYPE R SUMP @ DP15, PIPE TO DP15.1	
	15.1								24.1	3.65	2.81	10.2											COMBINED DP14 & DP15, PIPE TO DP18 OF THE EASTONVILLE ROAD SEGMENT 1 FDR
	16.1	EA10	0.16	0.70	5.0	0.11	5.17	0.6	5.0	0.11	5.17	0.6											BASIN EA10 CONVEYED VIA CURB & GUTTER TO 10' TYPE R INLET. INLET DESIGN IS PROVIDED IN THE EASTONVILLE ROAD SEGMENT 1 FDR
	17.1	EA11	0.15	0.63	5.2	0.09	5.11	0.5	5.2	0.09	5.11	0.5											BASIN EA11 CONVEYED VIA CURB & GUTTER TO 10' TYPE R INLET. INLET DESIGN IS PROVIDED IN THE EASTONVILLE ROAD SEGMENT 1 FDR
	O3	EA15	0.76	0.27	16.6	0.21	3.37	0.7	16.6	0.21	3.37	0.7											
	O3.1	NA										0.0											
	O4	EA12	0.34	0.08	5.0	0.03	5.17	0.1				22.5											
	O4.1	EA13	0.45	0.68	6.7	0.30	4.73	1.4	6.7	0.30	4.73	1.4											



**EASTONVILLE ROAD SEG 2**

Calc'd by:

SPC

**PROPOSED CONDITIONS**

Checked by:

CM

**DESIGN STORM: 5-YEAR**

Date:

8/28/2024

STREET	DESIGN POINT	BASIN ID	DIRECT RUNOFF					TOTAL RUNOFF				STREET			PIPE			TRAVEL TIME			REMARKS		
			AREA (ac)	C <sub>s</sub>	t <sub>c</sub> (min)	C <sub>s</sub> *A (ac)	I (in./hr.)	Q (cfs)	t <sub>c</sub> (min)	C <sub>s</sub> *A (ac)	I (in./hr.)	Q (cfs)	Q <sub>street</sub> (cfs)	C <sub>s</sub> *A (ac)	SLOPE %	Q <sub>PIPE</sub> (cfs)	C <sub>s</sub> *A (ac)	SLOPE %	PIPE SIZE (ft)	LENGTH (FT)		VEL. (FPS)	TRAVEL TIME (min)
	O4.2	EA14	1.48	0.24	17.5	0.36	3.29	1.2	17.5	0.36	3.29	1.2											
	10.1	EA17	0.30	0.08	10.3	0.02	4.08	0.1	10.3	0.02	4.08	0.1											
	11.1											13.6											
	13.1	EA16	1.18	0.08	14.4	0.09	3.58	0.3	14.4	0.09	3.58	0.3											



**EASTONVILLE ROAD SEG 2**  
**PROPOSED CONDITIONS**  
**DESIGN STORM: 100-YEAR**

Calc'd by:

SPC

Checked by:

CM

Date:

8/28/2024

STREET	DESIGN POINT	BASIN ID	DIRECT RUNOFF					TOTAL RUNOFF					STREET			PIPE			TRAVEL TIME			REMARKS			
			AREA (ac)	C <sub>100</sub>	t <sub>c</sub> (min)	C <sub>100</sub> *A (ac)	I (in./hr.)	Q (cfs)	t <sub>c</sub> (min)	C <sub>100</sub> *A (ac)	I (in./hr.)	Q (cfs)	Q <sub>street</sub> (cfs)	C <sub>100</sub> *A (ac)	SLOPE %	Q <sub>PIPE</sub> (cfs)	C <sub>100</sub> *A (ac)	SLOPE %	PIPE SIZE (ft)	LENGTH (ft)	VEL. (ft/s)		TRAVEL TIME (min)		
	1	G18								365.2															
	2	FG36								18.8															
	2.1	EA1	0.22	0.79	5.0	0.17	8.68	1.5	5.0	0.17	8.68	1.5		1.5	0.17	1.0	1.5	56	5.9	0.16				BASIN EA1 CAPTURED IN 5' TYPE R INLET @ DP2, PIPE TO DP3.1	
	3	G16								112.1				112.1	0.00	5.1	1.5	34	13.4	0.04					
	3.1	EA2	0.25	0.79	5.0	0.20	8.68	1.7	5.0	0.37	8.66	3.2												BASIN EA2 CAPTURED IN 5' TYPE R INLET @ DP3, PIPE TO DP3.1	
	4	G06								491.0				491.0	0.00	0.5	1.3	48	3.7	0.21					
	4.1	EA5	0.16	0.35	6.7	0.06	7.95	0.4	6.7	0.43	7.95	3.4		3.4	0.43	2.4	1.3	43	8.1	0.09				COMBINED DP2.1 & DP3.1 @ DP3.1, PIPE TO DP4 (POND A)	
	5	EA3	0.20	0.78	5.0	0.16	8.68	1.3	5.0	0.16	8.68	1.3		1.3	0.16	1.0	2.0	61	7.2	0.14				BASIN EA3 CAPTURED IN 5' TYPE R INLET @ DP5, PIPE TO DP6.1	
	6	EA4	0.17	0.74	5.0	0.13	8.68	1.1	5.1	0.28	8.61	2.4		2.4	0.28	0.8	2.0	43	6.4	0.11				BASIN EA4 CAPTURED IN 5' TYPE R INLET @ DP6, PIPE TO DP6.1	
	6.1								16.7	0.64	5.64	22.4		22.4	0.64	1.5	1.3	38	6.4	0.10				DP6 & DP8 FLOW @ DP6.1, PIPE TO DP9	
	7	OS3	1.00	0.36	13.1	0.36	6.24	2.2	13.1	0.36	6.24	2.2		2.2	0.36	1.0	2.0	56	7.2	0.13				BASIN OS3 CAPTURED IN 15' FES, PIPE TO DP8	
	8	OS3	1.00	0.36	13.1	0.36	6.24	2.2	13.1	0.36	6.24	21.0	21.0	0.36	2.1			615	2.9	3.56				DP2 & DP7 FLOW @ DP8, PIPE TO DP9	
	9								16.8	0.64	5.63	22.4												DP6.1 @ DP9, DISCHARGE TO ROADSIDE SWALE TO DP11	
	10	EA6	0.25	0.71	7.0	0.18	7.85	1.4	8.4	0.31	7.37	2.3												BASIN EA6 & EA7 @ DP10 (TEMPORARY SEDIMENT BASIN #1)	
		EA7	0.20	0.65	8.4	0.13	7.37	1.0					0.0	0.00	0.5			530	1.4	6.25					
	11	OS4	9.60	0.40	17.1	3.88	5.58	21.6	17.1	4.52	5.58	44.0		44.0	4.52	1.0	4.0	1500	11.4	2.19				BASIN OS4, DP9.1 CAPTURED & MERIDIAN RANCH DPG15 (3 CFS) IN 30" FES @ DP11, SWALE TO DP3	
	12	OS7	11.29	0.37	14.9	4.14	5.93	24.6	14.9	4.14	5.93	24.6		24.6	4.14	1.0	1.5	28	5.9	0.08				BASIN OS7 CAPTURED @ DP12 IN TYPE C INLET, PIPE TO DP13	
	13								14.9	4.14	5.92	180.6												COMBINED DP3 & DP12, PIPE TO CHANNEL B	
	14	EA8	2.08	0.89	24.0	1.86	4.72	8.8	24.0	1.86	4.72	8.8		8.8	1.86	7.0	1.5	8	15.7	0.01				BASIN EA8 CAPTURED IN 10' TYPE R SUMP @ DP14, PIPE TO DP15.1	
	15	EA9	3.14	0.72	24.0	2.25	4.72	10.6	24.0	2.25	4.72	10.6		10.6	2.25	1.8	1.5	54	7.9	0.11				BASIN EA8 CAPTURED IN 10' TYPE R SUMP @ DP15, PIPE TO DP15.1	
	15.1								24.1	4.10	4.71	19.3												COMBINED DP14 & DP15, PIPE TO DP18 OF THE EASTONVILLE ROAD SEGMENT 1 FDR	
	16.1	EA10	0.16	0.81	5.0	0.13	8.68	1.1	5.0	0.13	8.68	1.1												BASIN EA10 CONVEYED VIA CURB & GUTTER TO 10' TYPE R INLET. INLET DESIGN IS PROVIDED IN THE EASTONVILLE ROAD SEGMENT 1 FDR	
	17.1	EA11	0.15	0.76	5.2	0.11	8.58	1.0	5.2	0.11	8.58	1.0												BASIN EA11 CONVEYED VIA CURB & GUTTER TO 10' TYPE R INLET. INLET DESIGN IS PROVIDED IN THE EASTONVILLE ROAD SEGMENT 1 FDR	
	O3	EA15	0.76	0.49	16.6	0.37	5.66	2.1	16.6	0.37	5.66	2.1												TOTAL FLOW OFFSITE AT DP O3	
	O3.1	NA										0.0													
	O4	EA12	0.34	0.35	5.0	0.12	8.68	1.0				492.0												TOTAL FLOW OFFSITE AT DP4	
	O4.1	EA13	0.45	0.80	6.7	0.36	7.95	2.8	6.7	0.36	7.95	2.8												TOTAL FLOW OFFSITE AT DP4.1	
	O4.2	EA14	1.48	0.47	17.5	0.69	5.52	3.8	17.5	0.69	5.52	3.8												TOTAL FLOW OFFSITE AT DP4.2	
	10.1	EA17	0.30	0.35	10.3	0.11	6.85	0.7	10.3	0.11	6.85	0.7												TOTAL FLOW OFFSITE AT DP10.1	



**EASTONVILLE ROAD SEG 2**

Calc'd by:

SPC

**PROPOSED CONDITIONS**

Checked by:

CM

**DESIGN STORM: 100-YEAR**

Date:

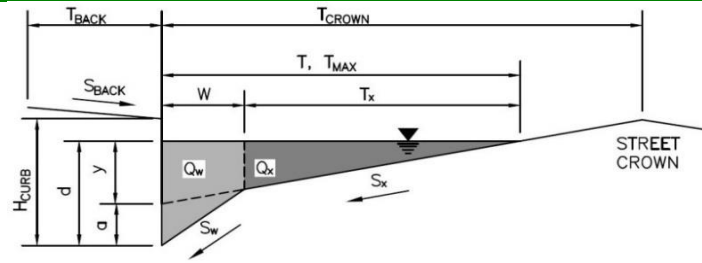
8/28/2024

			DIRECT RUNOFF					TOTAL RUNOFF				STREET			PIPE			TRAVEL TIME			REMARKS		
STREET	DESIGN POINT	BASIN ID	AREA (ac)	C <sub>100</sub>	t <sub>c</sub> (min)	C <sub>100</sub> *A (ac)	I (in./hr.)	Q (cfs)	t <sub>c</sub> (min)	C <sub>100</sub> *A (ac)	I (in./hr.)	Q (cfs)	Q <sub>street</sub> (cfs)	C <sub>100</sub> *A (ac)	SLOPE %	Q <sub>PIPE</sub> (cfs)	C <sub>100</sub> *A (ac)	SLOPE %	PIPE SIZE (ft)	LENGTH (ft)	VEL. (ft/s)	TRAVEL TIME (min)	
	11.1											156.1											TOTAL FLOW TO DP 11.1
	13.1	EA16	1.18	0.35	14.4	0.41	6.01	2.5	14.4	0.41	6.01	183.1											TOTAL FLOW OFFSITE AT DP 13.1

## APPENDIX C – HYDRAULIC CALCULATIONS

**ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)**  
 (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

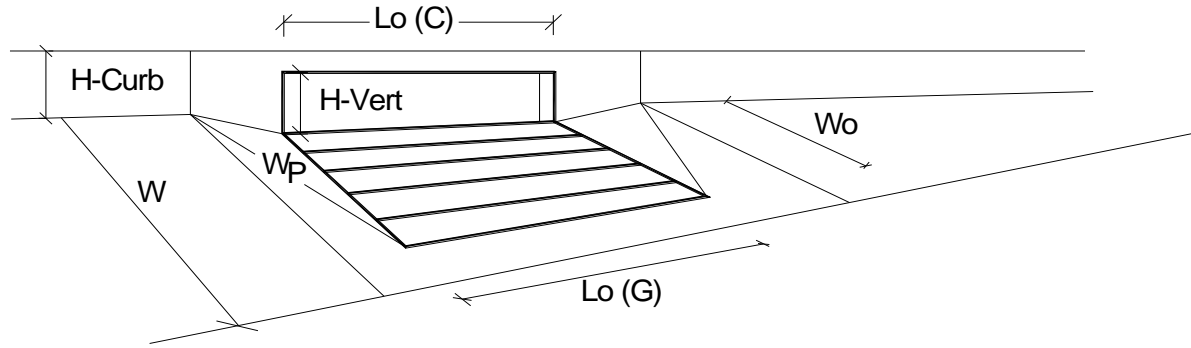
Project: Eastonville Road  
 Inlet ID: DP2.1



<b>Gutter Geometry:</b>	
Maximum Allowable Width for Spread Behind Curb	$T_{BACK} = 12.0$ ft
Side Slope Behind Curb (leave blank for no conveyance credit behind curb)	$S_{BACK} = 0.020$ ft/ft
Manning's Roughness Behind Curb (typically between 0.012 and 0.020)	$n_{BACK} = 0.020$
Height of Curb at Gutter Flow Line	$H_{CURB} = 6.00$ inches
Distance from Curb Face to Street Crown	$T_{CROWN} = 24.0$ ft
Gutter Width	$W = 2.00$ ft
Street Transverse Slope	$S_x = 0.020$ ft/ft
Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)	$S_w = 0.083$ ft/ft
Street Longitudinal Slope - Enter 0 for sump condition	$S_o = 0.000$ ft/ft
Manning's Roughness for Street Section (typically between 0.012 and 0.020)	$n_{STREET} = 0.016$
Max. Allowable Spread for Minor & Major Storm	$T_{MAX} = \begin{matrix} \text{Minor Storm} & \text{Major Storm} \\ 24.0 & 24.0 \end{matrix}$ ft
Max. Allowable Depth at Gutter Flowline for Minor & Major Storm	$d_{MAX} = \begin{matrix} \text{Minor Storm} & \text{Major Storm} \\ 5.9 & 8.8 \end{matrix}$ inches
Check boxes are not applicable in SUMP conditions	<input type="checkbox"/> <input type="checkbox"/>
<a href="#">MINOR STORM Allowable Capacity is based on Depth Criterion</a>	
<a href="#">MAJOR STORM Allowable Capacity is based on Depth Criterion</a>	
	$Q_{allow} = \begin{matrix} \text{Minor Storm} & \text{Major Storm} \\ \text{SUMP} & \text{SUMP} \end{matrix}$ cfs

# INLET IN A SUMP OR SAG LOCATION

MHFD-Inlet, Version 5.01 (April 2021)



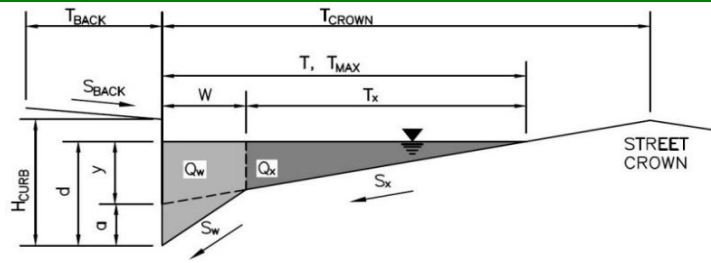
<div style="border: 1px solid black; display: inline-block; padding: 2px;">CDOT Type R Curb Opening</div>			
<b>Design Information (Input)</b>			
Type of Inlet	Type = <b>CDOT Type R Curb Opening</b>		
Local Depression (additional to continuous gutter depression 'a' from above)	$a_{local} =$	<b>3.00</b>	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	<b>1</b>	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	<b>5.9</b>	<input type="checkbox"/> Override Depths
<b>Grate Information</b>			
Length of a Unit Grate	$L_o(G) =$	<b>N/A</b>	feet
Width of a Unit Grate	$W_o =$	<b>N/A</b>	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	$A_{ratio} =$	<b>N/A</b>	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_f(G) =$	<b>N/A</b>	
Grate Weir Coefficient (typical value 2.15 - 3.60)	$C_w(G) =$	<b>N/A</b>	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	$C_o(G) =$	<b>N/A</b>	
<b>Curb Opening Information</b>			
Length of a Unit Curb Opening	$L_o(C) =$	<b>5.00</b>	feet
Height of Vertical Curb Opening in Inches	$H_{vert} =$	<b>6.00</b>	inches
Height of Curb Orifice Throat in Inches	$H_{throat} =$	<b>6.00</b>	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	<b>63.40</b>	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	$W_p =$	<b>2.00</b>	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_f(C) =$	<b>0.10</b>	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$	<b>3.60</b>	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_o(C) =$	<b>0.67</b>	
<b>Low Head Performance Reduction (Calculated)</b>			
Depth for Grate Midwidth	$d_{Grate} =$	<b>N/A</b>	ft
Depth for Curb Opening Weir Equation	$d_{Curb} =$	<b>0.32</b>	ft
Combination Inlet Performance Reduction Factor for Long Inlets	$RF_{Combination} =$	<b>0.75</b>	
Curb Opening Performance Reduction Factor for Long Inlets	$RF_{Curb} =$	<b>1.00</b>	
Grated Inlet Performance Reduction Factor for Long Inlets	$RF_{Grate} =$	<b>N/A</b>	
Total Inlet Interception Capacity (assumes clogged condition)	$Q_a =$	<b>5.1</b>	<b>cfs</b>
<b>Inlet Capacity IS GOOD for Minor and Major Storms(&gt;Q PEAK)</b>	$Q_{PEAK\ REQUIRED} =$	<b>0.8</b>	<b>cfs</b>



## ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

**Project:** Eastonville Road  
**Inlet ID:** DP3.1



**Gutter Geometry:**

Maximum Allowable Width for Spread Behind Curb  
 Side Slope Behind Curb (leave blank for no conveyance credit behind curb)  
 Manning's Roughness Behind Curb (typically between 0.012 and 0.020)  
 Height of Curb at Gutter Flow Line  
 Distance from Curb Face to Street Crown  
 Gutter Width  
 Street Transverse Slope  
 Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)  
 Street Longitudinal Slope - Enter 0 for sump condition  
 Manning's Roughness for Street Section (typically between 0.012 and 0.020)

$T_{BACK} = 11.0$  ft  
 $S_{BACK} = 0.020$  ft/ft  
 $n_{BACK} = 0.020$

$H_{CURB} = 6.00$  inches  
 $T_{CROWN} = 24.0$  ft  
 $W = 2.00$  ft  
 $S_X = 0.020$  ft/ft  
 $S_W = 0.083$  ft/ft  
 $S_O = 0.000$  ft/ft  
 $n_{STREET} = 0.016$

Max. Allowable Spread for Minor & Major Storm  
 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm  
 Check boxes are not applicable in SUMP conditions

	Minor Storm	Major Storm	
$T_{MAX} =$	24.0	24.0	ft
$d_{MAX} =$	5.9	8.8	inches
	<input type="checkbox"/>	<input type="checkbox"/>	

MINOR STORM Allowable Capacity is based on Depth Criterion  
 MAJOR STORM Allowable Capacity is based on Depth Criterion

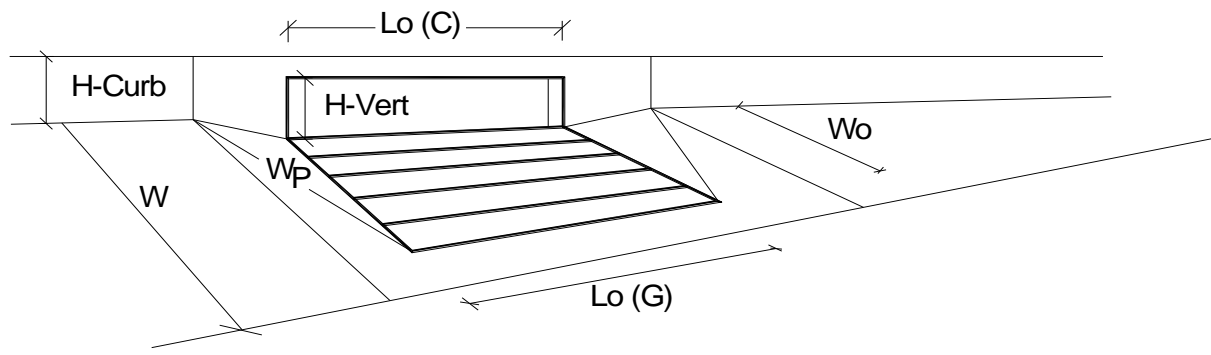
$Q_{allow} =$ 

Minor Storm	Major Storm
<b>SUMP</b>	<b>SUMP</b>

 cfs

# INLET IN A SUMP OR SAG LOCATION

*MHFD-Inlet, Version 5.01 (April 2021)*

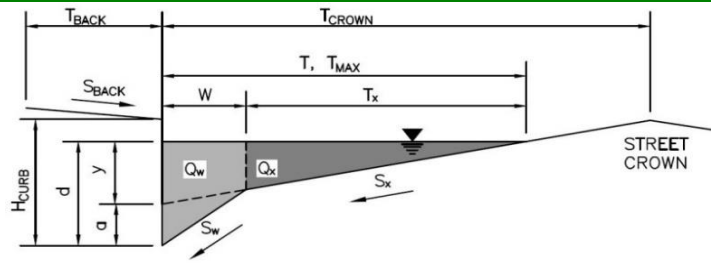


Design Information (Input)		CDOT Type R Curb Opening	
Type of Inlet		MINOR	MAJOR
Local Depression (additional to continuous gutter depression 'a' from above)		CDOT Type R Curb Opening	
Number of Unit Inlets (Grate or Curb Opening)		3.00	3.00
Water Depth at Flowline (outside of local depression)		1	1
<u>Grate Information</u>		<input type="checkbox"/> Override Depths	
Length of a Unit Grate		5.9	7.3
Width of a Unit Grate		N/A	N/A
Area Opening Ratio for a Grate (typical values 0.15-0.90)		N/A	N/A
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)		N/A	N/A
Grate Weir Coefficient (typical value 2.15 - 3.60)		N/A	N/A
Grate Orifice Coefficient (typical value 0.60 - 0.80)		N/A	N/A
<u>Curb Opening Information</u>		MINOR	MAJOR
Length of a Unit Curb Opening		5.00	5.00
Height of Vertical Curb Opening in Inches		6.00	6.00
Height of Curb Orifice Throat in Inches		6.00	6.00
Angle of Throat (see USDCM Figure ST-5)		63.40	63.40
Side Width for Depression Pan (typically the gutter width of 2 feet)		2.00	2.00
Clogging Factor for a Single Curb Opening (typical value 0.10)		0.10	0.10
Curb Opening Weir Coefficient (typical value 2.3-3.7)		3.60	3.60
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)		0.67	0.67
<u>Low Head Performance Reduction (Calculated)</u>		MINOR	MAJOR
Depth for Grate Midwidth		N/A	N/A
Depth for Curb Opening Weir Equation		0.32	0.44
Combination Inlet Performance Reduction Factor for Long Inlets		0.75	0.93
Curb Opening Performance Reduction Factor for Long Inlets		1.00	1.00
Grated Inlet Performance Reduction Factor for Long Inlets		N/A	N/A
Total Inlet Interception Capacity (assumes clogged condition)		MINOR	MAJOR
<b>Inlet Capacity IS GOOD for Minor and Major Storms(&gt;Q PEAK)</b>		5.1	8.1
		0.9	1.7

## ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

**Project:** Eastonville Road  
**Inlet ID:** DP5



**Gutter Geometry:**

Maximum Allowable Width for Spread Behind Curb  
 Side Slope Behind Curb (leave blank for no conveyance credit behind curb)  
 Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

$T_{BACK} = 11.0$  ft  
 $S_{BACK} = 0.020$  ft/ft  
 $n_{BACK} = 0.020$

Height of Curb at Gutter Flow Line  
 Distance from Curb Face to Street Crown  
 Gutter Width  
 Street Transverse Slope  
 Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)  
 Street Longitudinal Slope - Enter 0 for sump condition  
 Manning's Roughness for Street Section (typically between 0.012 and 0.020)

$H_{CURB} = 6.00$  inches  
 $T_{CROWN} = 24.0$  ft  
 $W = 2.00$  ft  
 $S_x = 0.020$  ft/ft  
 $S_w = 0.083$  ft/ft  
 $S_o = 0.000$  ft/ft  
 $n_{STREET} = 0.016$

Max. Allowable Spread for Minor & Major Storm  
 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm  
 Check boxes are not applicable in SUMP conditions

	Minor Storm	Major Storm	
$T_{MAX} =$	24.0	24.0	ft
$d_{MAX} =$	5.9	8.8	inches
	<input type="checkbox"/>	<input type="checkbox"/>	

MINOR STORM Allowable Capacity is based on Depth Criterion  
 MAJOR STORM Allowable Capacity is based on Depth Criterion

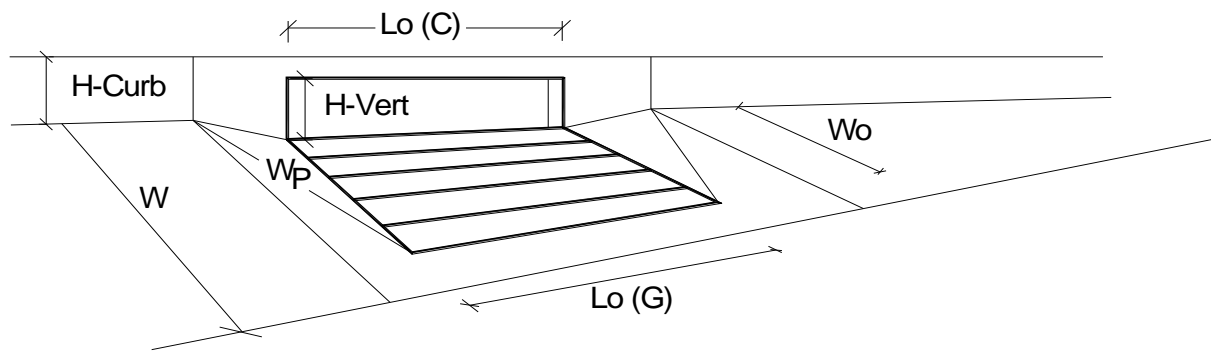
$Q_{allow} =$ 

Minor Storm	Major Storm
<b>SUMP</b>	<b>SUMP</b>

 cfs

# INLET IN A SUMP OR SAG LOCATION

MHFD-Inlet, Version 5.01 (April 2021)

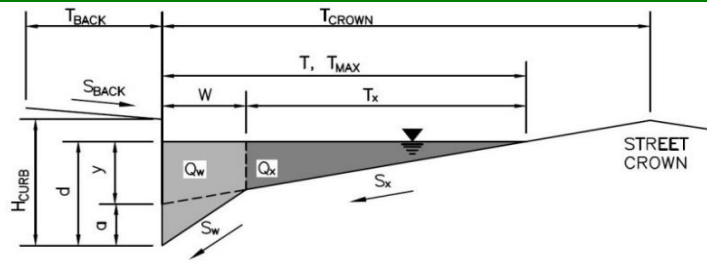


Design Information (Input)		CDOT Type R Curb Opening	
Type of Inlet		MINOR	MAJOR
Local Depression (additional to continuous gutter depression 'a' from above)		CDOT Type R Curb Opening	
Number of Unit Inlets (Grate or Curb Opening)		3.00	3.00
Water Depth at Flowline (outside of local depression)		1	1
<b>Grate Information</b>		<input type="checkbox"/> Override Depths	
Length of a Unit Grate		5.9	7.3
Width of a Unit Grate		N/A	N/A
Area Opening Ratio for a Grate (typical values 0.15-0.90)		N/A	N/A
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)		N/A	N/A
Grate Weir Coefficient (typical value 2.15 - 3.60)		N/A	N/A
Grate Orifice Coefficient (typical value 0.60 - 0.80)		N/A	N/A
<b>Curb Opening Information</b>		MINOR	MAJOR
Length of a Unit Curb Opening		5.00	5.00
Height of Vertical Curb Opening in Inches		6.00	6.00
Height of Curb Orifice Throat in Inches		6.00	6.00
Angle of Throat (see USDCM Figure ST-5)		63.40	63.40
Side Width for Depression Pan (typically the gutter width of 2 feet)		2.00	2.00
Clogging Factor for a Single Curb Opening (typical value 0.10)		0.10	0.10
Curb Opening Weir Coefficient (typical value 2.3-3.7)		3.60	3.60
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)		0.67	0.67
<b>Low Head Performance Reduction (Calculated)</b>		MINOR	MAJOR
Depth for Grate Midwidth		N/A	N/A
Depth for Curb Opening Weir Equation		0.32	0.44
Combination Inlet Performance Reduction Factor for Long Inlets		0.75	0.93
Curb Opening Performance Reduction Factor for Long Inlets		1.00	1.00
Grated Inlet Performance Reduction Factor for Long Inlets		N/A	N/A
Total Inlet Interception Capacity (assumes clogged condition)		5.1	8.1
<b>Inlet Capacity IS GOOD for Minor and Major Storms(&gt;Q PEAK)</b>		0.7	1.3

## ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

**Project:** Eastonville Road  
**Inlet ID:** DP6



**Gutter Geometry:**

Maximum Allowable Width for Spread Behind Curb  
 Side Slope Behind Curb (leave blank for no conveyance credit behind curb)  
 Manning's Roughness Behind Curb (typically between 0.012 and 0.020)  
 Height of Curb at Gutter Flow Line  
 Distance from Curb Face to Street Crown  
 Gutter Width  
 Street Transverse Slope  
 Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)  
 Street Longitudinal Slope - Enter 0 for sump condition  
 Manning's Roughness for Street Section (typically between 0.012 and 0.020)

$T_{BACK} =$   ft  
 $S_{BACK} =$   ft/ft  
 $n_{BACK} =$

$H_{CURB} =$   inches  
 $T_{CROWN} =$   ft  
 $W =$   ft  
 $S_x =$   ft/ft  
 $S_w =$   ft/ft  
 $S_o =$   ft/ft  
 $n_{STREET} =$

Max. Allowable Spread for Minor & Major Storm  
 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm  
 Check boxes are not applicable in SUMP conditions

	Minor Storm	Major Storm	
$T_{MAX} =$	<input type="text" value="24.0"/>	<input type="text" value="24.0"/>	ft
$d_{MAX} =$	<input type="text" value="3.5"/>	<input type="text" value="3.5"/>	inches
	<input type="checkbox"/>	<input type="checkbox"/>	

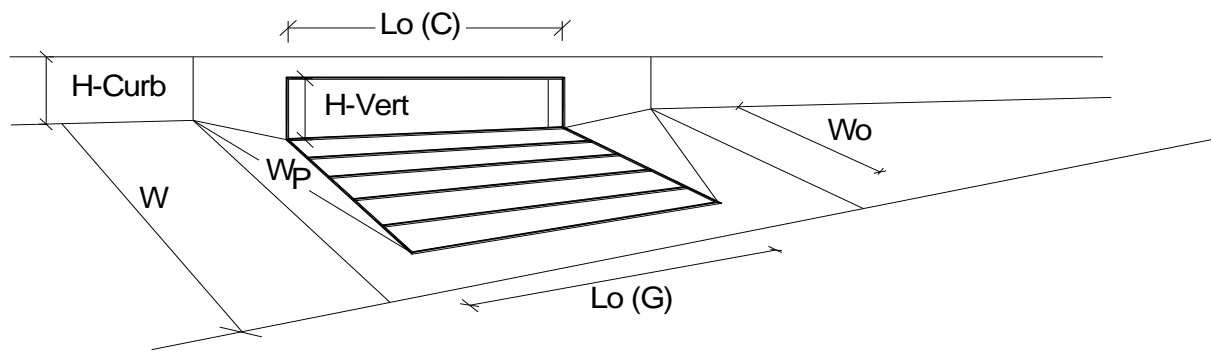
MINOR STORM Allowable Capacity is based on Depth Criterion  
 MAJOR STORM Allowable Capacity is based on Depth Criterion

$Q_{allow} =$ 

Minor Storm	Major Storm	
<input type="text" value="SUMP"/>	<input type="text" value="SUMP"/>	cfs

# INLET IN A SUMP OR SAG LOCATION

MHFD-Inlet, Version 5.01 (April 2021)

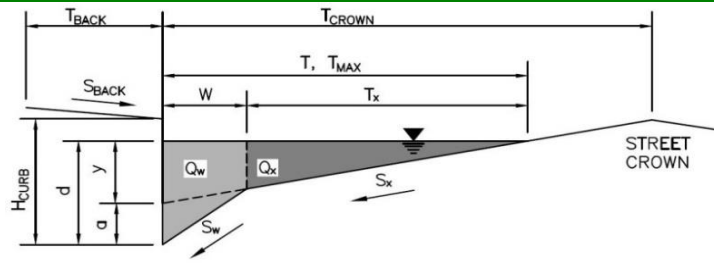


Design Information (Input)		CDOT Type R Curb Opening	
Type of Inlet		MINOR	MAJOR
Local Depression (additional to continuous gutter depression 'a' from above)		CDOT Type R Curb Opening	
Number of Unit Inlets (Grate or Curb Opening)		3.00	3.00
Water Depth at Flowline (outside of local depression)		1	1
<b>Grate Information</b>		<input type="checkbox"/> Override Depths	
Length of a Unit Grate		3.5	3.5
Width of a Unit Grate		N/A	N/A
Area Opening Ratio for a Grate (typical values 0.15-0.90)		N/A	N/A
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)		N/A	N/A
Grate Weir Coefficient (typical value 2.15 - 3.60)		N/A	N/A
Grate Orifice Coefficient (typical value 0.60 - 0.80)		N/A	N/A
<b>Curb Opening Information</b>		MINOR	MAJOR
Length of a Unit Curb Opening		5.00	5.00
Height of Vertical Curb Opening in Inches		6.00	6.00
Height of Curb Orifice Throat in Inches		6.00	6.00
Angle of Throat (see USDCM Figure ST-5)		63.40	63.40
Side Width for Depression Pan (typically the gutter width of 2 feet)		2.00	2.00
Clogging Factor for a Single Curb Opening (typical value 0.10)		0.10	0.10
Curb Opening Weir Coefficient (typical value 2.3-3.7)		3.60	3.60
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)		0.67	0.67
<b>Low Head Performance Reduction (Calculated)</b>		MINOR	MAJOR
Depth for Grate Midwidth		N/A	N/A
Depth for Curb Opening Weir Equation		0.13	0.13
Combination Inlet Performance Reduction Factor for Long Inlets		0.45	0.45
Curb Opening Performance Reduction Factor for Long Inlets		0.99	0.99
Grated Inlet Performance Reduction Factor for Long Inlets		N/A	N/A
Total Inlet Interception Capacity (assumes clogged condition)		MINOR	MAJOR
<b>Inlet Capacity IS GOOD for Minor and Major Storms(&gt;Q PEAK)</b>		1.2	1.2
		Q PEAK REQUIRED =	0.5
			1.1
			cfs
			cfs

## ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

**Project:** Eastonville Road  
**Inlet ID:** DP14



**Gutter Geometry:**

Maximum Allowable Width for Spread Behind Curb  
 Side Slope Behind Curb (leave blank for no conveyance credit behind curb)  
 Manning's Roughness Behind Curb (typically between 0.012 and 0.020)  
 Height of Curb at Gutter Flow Line  
 Distance from Curb Face to Street Crown  
 Gutter Width  
 Street Transverse Slope  
 Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)  
 Street Longitudinal Slope - Enter 0 for sump condition  
 Manning's Roughness for Street Section (typically between 0.012 and 0.020)

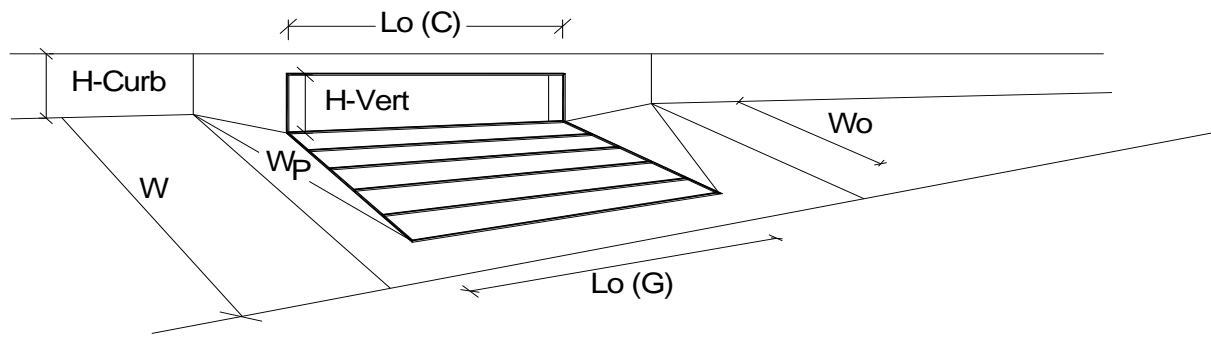
$T_{BACK}$	8.0	ft
$S_{BACK}$	0.020	ft/ft
$n_{BACK}$	0.020	
$H_{CURB}$	6.00	inches
$T_{CROWN}$	26.0	ft
$W$	2.00	ft
$S_x$	0.020	ft/ft
$S_w$	0.083	ft/ft
$S_o$	0.000	ft/ft
$n_{STREET}$	0.016	
	Minor Storm	Major Storm
$T_{MAX}$	26.0	26.0
$d_{MAX}$	5.9	8.8
	<input type="checkbox"/>	<input type="checkbox"/>
	Minor Storm	Major Storm
$Q_{allow}$	<b>SUMP</b>	<b>SUMP</b>
	cfs	

Max. Allowable Spread for Minor & Major Storm  
 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm  
 Check boxes are not applicable in SUMP conditions

MINOR STORM Allowable Capacity is based on Depth Criterion  
 MAJOR STORM Allowable Capacity is based on Depth Criterion

# INLET IN A SUMP OR SAG LOCATION

*MHFD-Inlet, Version 5.01 (April 2021)*



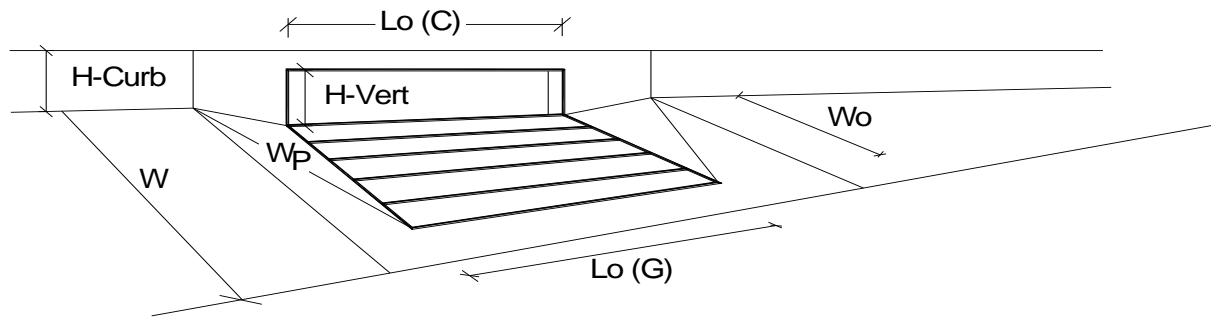
Design Information (Input)		CDOT Type R Curb Opening	
Type of Inlet		MINOR	MAJOR
Local Depression (additional to continuous gutter depression 'a' from above)		CDOT Type R Curb Opening	
Number of Unit Inlets (Grate or Curb Opening)		3.00	3.00
Water Depth at Flowline (outside of local depression)		2	2
<b>Grate Information</b>		<input type="checkbox"/> Override Depths	
Length of a Unit Grate		5.9	7.8
Width of a Unit Grate		N/A	N/A
Area Opening Ratio for a Grate (typical values 0.15-0.90)		N/A	N/A
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)		N/A	N/A
Grate Weir Coefficient (typical value 2.15 - 3.60)		N/A	N/A
Grate Orifice Coefficient (typical value 0.60 - 0.80)		N/A	N/A
<b>Curb Opening Information</b>		MINOR	MAJOR
Length of a Unit Curb Opening		5.00	5.00
Height of Vertical Curb Opening in Inches		6.00	6.00
Height of Curb Orifice Throat in Inches		6.00	6.00
Angle of Throat (see USDCM Figure ST-5)		63.40	63.40
Side Width for Depression Pan (typically the gutter width of 2 feet)		2.00	2.00
Clogging Factor for a Single Curb Opening (typical value 0.10)		0.10	0.10
Curb Opening Weir Coefficient (typical value 2.3-3.7)		3.60	3.60
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)		0.67	0.67
<b>Low Head Performance Reduction (Calculated)</b>		MINOR	MAJOR
Depth for Grate Midwidth		N/A	N/A
Depth for Curb Opening Weir Equation		0.32	0.48
Combination Inlet Performance Reduction Factor for Long Inlets		0.55	0.73
Curb Opening Performance Reduction Factor for Long Inlets		0.93	1.00
Grated Inlet Performance Reduction Factor for Long Inlets		N/A	N/A
Total Inlet Interception Capacity (assumes clogged condition)		MINOR	MAJOR
<b>Inlet Capacity IS GOOD for Minor and Major Storms(&gt;Q PEAK)</b>		9.9	18.6
		5.2	8.8





# INLET IN A SUMP OR SAG LOCATION

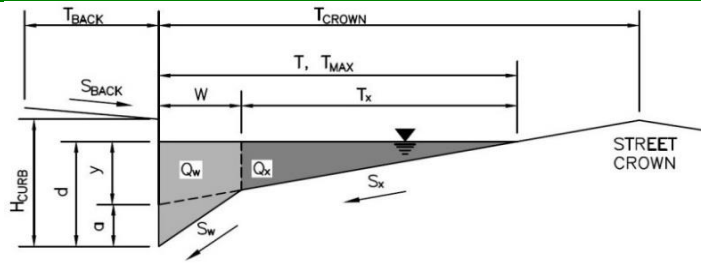
MHFD-Inlet, Version 5.01 (April 2021)



Design Information (Input)		CDOT Type R Curb Opening	
Type of Inlet		MINOR	MAJOR
Local Depression (additional to continuous gutter depression 'a' from above)		CDOT Type R Curb Opening	
Number of Unit Inlets (Grate or Curb Opening)		3.00	3.00
Water Depth at Flowline (outside of local depression)		2	2
<b>Grate Information</b>		<input type="checkbox"/> Override Depths	
Length of a Unit Grate		5.9	7.8
Width of a Unit Grate		N/A	N/A
Area Opening Ratio for a Grate (typical values 0.15-0.90)		N/A	N/A
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)		N/A	N/A
Grate Weir Coefficient (typical value 2.15 - 3.60)		N/A	N/A
Grate Orifice Coefficient (typical value 0.60 - 0.80)		N/A	N/A
<b>Curb Opening Information</b>		MINOR	MAJOR
Length of a Unit Curb Opening		5.00	5.00
Height of Vertical Curb Opening in Inches		6.00	6.00
Height of Curb Orifice Throat in Inches		6.00	6.00
Angle of Throat (see USDCM Figure ST-5)		63.40	63.40
Side Width for Depression Pan (typically the gutter width of 2 feet)		2.00	2.00
Clogging Factor for a Single Curb Opening (typical value 0.10)		0.10	0.10
Curb Opening Weir Coefficient (typical value 2.3-3.7)		3.60	3.60
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)		0.67	0.67
<b>Low Head Performance Reduction (Calculated)</b>		MINOR	MAJOR
Depth for Grate Midwidth		N/A	N/A
Depth for Curb Opening Weir Equation		0.32	0.48
Combination Inlet Performance Reduction Factor for Long Inlets		0.55	0.73
Curb Opening Performance Reduction Factor for Long Inlets		0.93	1.00
Grated Inlet Performance Reduction Factor for Long Inlets		N/A	N/A
Total Inlet Interception Capacity (assumes clogged condition)		9.9	18.6
<b>Inlet Capacity IS GOOD for Minor and Major Storms(&gt;Q PEAK)</b>		5.0	10.6

**ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)**  
 (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: Eastonville Road  
 Inlet ID: Street Capacity (DP14)

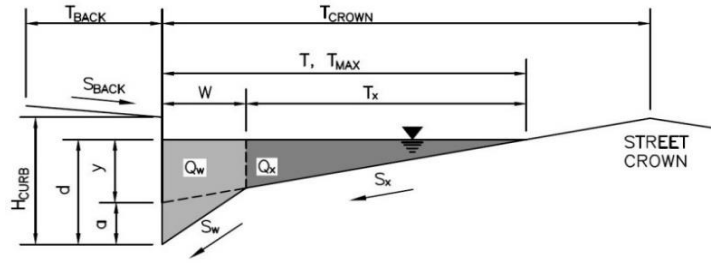


<b>Gutter Geometry:</b>	
Maximum Allowable Width for Spread Behind Curb	$T_{BACK} = 2.0$ ft
Side Slope Behind Curb (leave blank for no conveyance credit behind curb)	$S_{BACK} = 0.020$ ft/ft
Manning's Roughness Behind Curb (typically between 0.012 and 0.020)	$n_{BACK} = 0.015$
Height of Curb at Gutter Flow Line	$H_{CURB} = 6.00$ inches
Distance from Curb Face to Street Crown	$T_{CROWN} = 26.0$ ft
Gutter Width	$W = 2.00$ ft
Street Transverse Slope	$S_x = 0.020$ ft/ft
Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)	$S_w = 0.083$ ft/ft
Street Longitudinal Slope - Enter 0 for sump condition	$S_o = 0.005$ ft/ft
Manning's Roughness for Street Section (typically between 0.012 and 0.020)	$n_{STREET} = 0.012$
Max. Allowable Spread for Minor & Major Storm	$T_{MAX} = \begin{matrix} \text{Minor Storm} & \text{Major Storm} \\ 26.0 & 26.0 \end{matrix}$ ft
Max. Allowable Depth at Gutter Flowline for Minor & Major Storm	$d_{MAX} = \begin{matrix} \text{Minor Storm} & \text{Major Storm} \\ 5.9 & 8.8 \end{matrix}$ inches
Allow Flow Depth at Street Crown (check box for yes, leave blank for no)	<input type="checkbox"/> <input type="checkbox"/>
MINOR STORM Allowable Capacity is based on Depth Criterion	
MAJOR STORM Allowable Capacity is based on Spread Criterion	
<b>Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'</b>	
<b>Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'</b>	
	$Q_{allow} = \begin{matrix} \text{Minor Storm} & \text{Major Storm} \\ 12.3 & 30.5 \end{matrix}$ cfs

## ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

**Project:** Eastonville Road  
**Inlet ID:** Street Capacity (DP15)



**Gutter Geometry:**

Maximum Allowable Width for Spread Behind Curb  
 Side Slope Behind Curb (leave blank for no conveyance credit behind curb)  
 Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

$T_{BACK} = 8.0$  ft  
 $S_{BACK} = 0.020$  ft/ft  
 $n_{BACK} = 0.015$

Height of Curb at Gutter Flow Line  
 Distance from Curb Face to Street Crown  
 Gutter Width  
 Street Transverse Slope  
 Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)  
 Street Longitudinal Slope - Enter 0 for sump condition  
 Manning's Roughness for Street Section (typically between 0.012 and 0.020)

$H_{CURB} = 6.00$  inches  
 $T_{CROWN} = 26.0$  ft  
 $W = 2.00$  ft  
 $S_X = 0.020$  ft/ft  
 $S_W = 0.083$  ft/ft  
 $S_O = 0.005$  ft/ft  
 $n_{STREET} = 0.012$

Max. Allowable Spread for Minor & Major Storm  
 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm  
 Allow Flow Depth at Street Crown (check box for yes, leave blank for no)

	Minor Storm	Major Storm	
$T_{MAX} =$	26.0	26.0	ft
$d_{MAX} =$	5.9	8.8	inches
	<input type="checkbox"/>	<input type="checkbox"/>	

MINOR STORM Allowable Capacity is based on Depth Criterion  
 MAJOR STORM Allowable Capacity is based on Spread Criterion

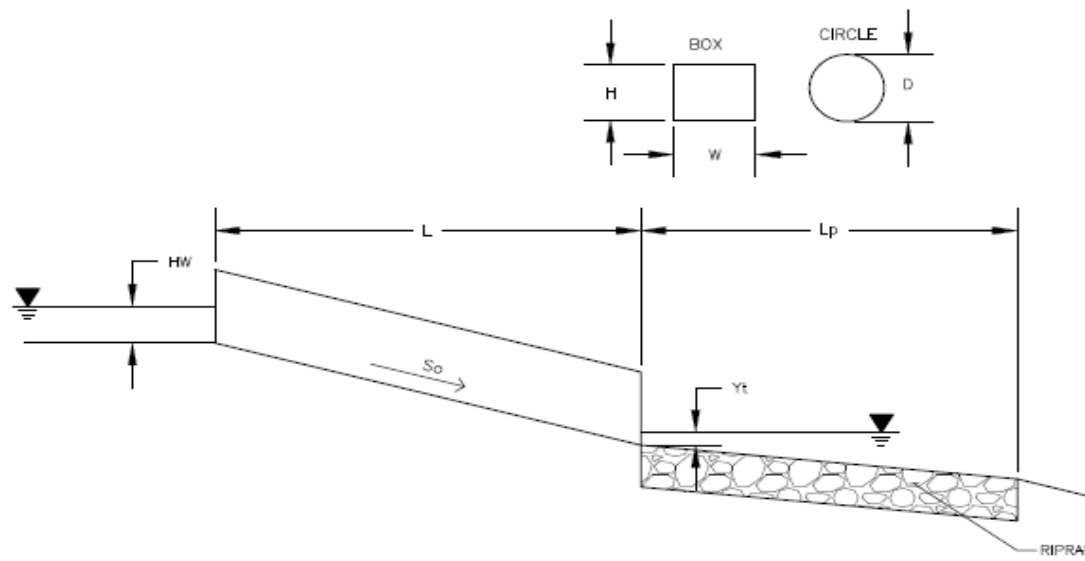
	Minor Storm	Major Storm	
$Q_{allow} =$	12.3	30.9	cfs

**Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'**  
**Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'**

# DETERMINATION OF CULVERT HEADWATER AND OUTLET PROTECTION

*MHFD-Culvert, Version 4.00 (May 2020)*

**Project:** \_\_\_\_\_  
**ID:** \_\_\_\_\_



**Soil Type:**  
 Choose One:  
 Sandy  
 Non-Sandy

**Supercritical Flow! Using Adjusted Rise to calculate protection type.**

Design Information:	
Design Discharge	Q = <input type="text" value="491"/> cfs
<b>Circular Culvert:</b>	
Barrel Diameter in Inches	D = <input type="text"/> inches
Inlet Edge Type (Choose from pull-down list)	
<b>OR:</b>	
<b>Box Culvert:</b>	
Barrel Height (Rise) in Feet	H (Rise) = <input type="text" value="3"/> ft
Barrel Width (Span) in Feet	W (Span) = <input type="text" value="10"/> ft
Inlet Edge Type (Choose from pull-down list)	1:1 Bevel w/ 45 deg. Flared Wingwall
Number of Barrels	# Barrels = <input type="text" value="2"/>
Inlet Elevation	Elev IN = <input type="text" value="100"/> ft
Outlet Elevation <b>OR</b> Slope	So = <input type="text" value="0.015"/> ft/ft
Culvert Length	L = <input type="text" value="116.5"/> ft
Manning's Roughness	n = <input type="text" value="0.012"/>
Bend Loss Coefficient	k <sub>b</sub> = <input type="text" value="0"/>
Exit Loss Coefficient	k <sub>x</sub> = <input type="text" value="1"/>
Tailwater Surface Elevation	Y <sub>t</sub> Elevation = <input type="text"/>
Max Allowable Channel Velocity	V = <input type="text" value="7"/> ft/s

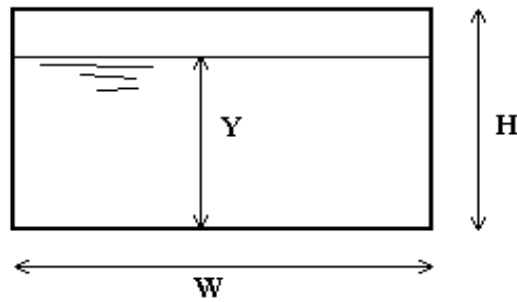
Calculated Results:	
Culvert Cross Sectional Area Available	A = <input type="text" value="30.00"/> ft <sup>2</sup>
Culvert Normal Depth	Y <sub>n</sub> = <input type="text" value="1.48"/> ft
Culvert Critical Depth	Y <sub>c</sub> = <input type="text" value="2.65"/> ft
Froude Number	Fr = <input type="text" value="2.41"/> <b>Supercritical!</b>
Entrance Loss Coefficient	k <sub>e</sub> = <input type="text" value="0.50"/>
Friction Loss Coefficient	k <sub>f</sub> = <input type="text" value="0.40"/>
Sum of All Loss Coefficients	k <sub>s</sub> = <input type="text" value="1.90"/> ft
<b>Headwater:</b>	
Inlet Control Headwater	HW <sub>I</sub> = <input type="text" value="4.57"/> ft
Outlet Control Headwater	HW <sub>O</sub> = <input type="text" value="3.06"/> ft
<b>Design Headwater Elevation</b>	<b>HW = <input type="text" value="104.57"/> ft</b>
<b>Headwater/Diameter <u>OR</u> Headwater/Rise Ratio</b>	<b>HW/H = <input type="text" value="1.52"/> <b>HW/H &gt; 1.5!</b></b>
<b>Outlet Protection:</b>	
Flow/(Span * Rise <sup>1.5</sup> )	Q/WH <sup>1.5</sup> = <input type="text" value="4.72"/> ft <sup>0.5</sup> /s
Tailwater Surface Height	Y <sub>t</sub> = <input type="text" value="1.20"/> ft
Tailwater/Rise	Y <sub>t</sub> /H = <input type="text" value="0.40"/>
Expansion Factor	1/(2*tan(θ)) = <input type="text" value="1.85"/>
Flow Area at Max Channel Velocity	A <sub>t</sub> = <input type="text" value="70.14"/> ft <sup>2</sup>
Width of Equivalent Conduit for Multiple Barrels	W <sub>eq</sub> = <input type="text" value="20.00"/> ft
<b>Length of Riprap Protection</b>	<b>L<sub>p</sub> = <input type="text" value="30"/> ft</b>
<b>Width of Riprap Protection at Downstream End</b>	<b>T = <input type="text" value="37"/> ft</b>
Adjusted Rise for Supercritical Flow	H <sub>a</sub> = <input type="text" value="2.24"/> ft
Minimum Theoretical Riprap Size	d <sub>50</sub> min = <input type="text" value="5"/> in
Nominal Riprap Size	d <sub>50</sub> nominal = <input type="text" value="6"/> in
<b>MHFD Riprap Type</b>	<b>Type = <input type="text" value="VL"/></b>

# BOX CONDUIT FLOW (Normal & Critical Depth Computation)

MHFD-Culvert, Version 4.00 (May 2020)

Project: **Eastonville Road Segment 2**

Box ID: **Geick Ranch Tributary 1 Box Culvert**

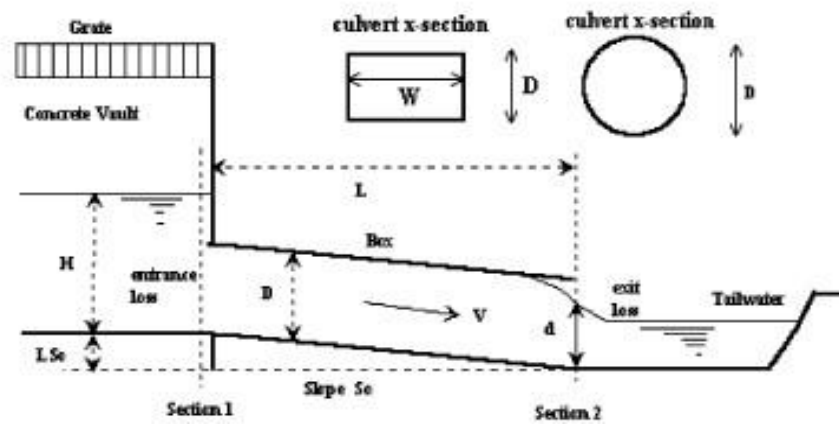


<u>Design Information (Input)</u>	
Box conduit invert slope	So = 0.0150 ft/ft
Box Manning's n-value	n = 0.0120
Box Width	W = 10.00 ft
Box Height	H = 3.00 ft
Design discharge	Q = 491.00 cfs
<u>Full-flow capacity (Calculated)</u>	
Full-flow area	Af = 30.00 sq ft
Full-flow wetted perimeter	Pf = 26.00 ft
Full-flow capacity	Qf = 501.88 cfs
<u>Calculations of Normal Flow Condition</u>	
Normal flow depth (<H)	Yn = 2.36 ft
Flow area	An = 23.58 sq ft
Wetted perimeter	Pn = 14.72 ft
Flow velocity	Vn = 20.82 fps
Discharge	Qn = 491.02 cfs
Percent of Full Flow	Flow = 97.8% of full flow
Normal Depth Froude Number	Fr <sub>n</sub> = 2.39 supercritical
<u>Calculation of Critical Flow Condition</u>	
Critical flow depth	Yc = 3.00 ft
Critical flow area	Ac = 30.00 sq ft
Critical flow velocity	Vc = 16.37 fps
Critical Depth Froude Number	Fr <sub>c</sub> = 1.67

# CULVERT SIZING (INLET vs. OUTLET CONTROL WITH TAILWATER EFFECTS)

MHFD-Culvert, Version 4.00 (May 2020)

**Project: EASTONVILLE ROAD**  
**ID: DP8**



**Design Information (Input):**

Circular Culvert: Barrel Diameter in Inches D =   
 Inlet Edge Type (Choose from pull-down list)

**OR:**

Box Culvert: Barrel Height (Rise) in Feet H (Rise) =  ft  
 Barrel Width (Span) in Feet W (Span) =  ft  
 Inlet Edge Type (Choose from pull-down list) 1:1 Bevel w/ 45 deg. Flared Wingwall

Number of Barrels # Barrels =   
 Inlet Elevation at Culvert Invert Elev IN =  ft  
 Outlet Elevation **OR** Slope So =  ft/ft  
 Culvert Length L =  ft  
 Manning's Roughness n =   
 Bend Loss Coefficient K<sub>b</sub> =   
 Exit Loss Coefficient K<sub>x</sub> =

**Design Information (calculated):**

Entrance Loss Coefficient K<sub>e</sub> =   
 Friction Loss Coefficient K<sub>f</sub> =   
 Sum of All Loss Coefficients K<sub>s</sub> =   
 Minimum Energy Condition Coefficient KE<sub>low</sub> =   
 Orifice Inlet Condition Coefficient C<sub>d</sub> =

**Calculations of Culvert Capacity (output):**

Backwater calculations required to obtain Outlet Control Flowrate when H<sub>wo</sub> < 0.75 \* Culvert Rise

Headwater Surface Elevation (ft)	Tailwater Surface Elevation (ft)	Inlet Control Equation Used	Inlet Control Flowrate (cfs)	Outlet Control Flowrate (cfs)	Controlling Culvert Flowrate (cfs)	Flow Control Used
100.00		No Flow (WS < inlet)	0.00	0.00	<b>0.00</b>	N/A
100.25		Min. Energy. Eqn.	7.74	#N/A	#N/A	#N/A
100.50		Min. Energy. Eqn.	21.82	#N/A	#N/A	#N/A
100.75		Min. Energy. Eqn.	40.04	#N/A	#N/A	#N/A
101.00		Min. Energy. Eqn.	61.66	#N/A	#N/A	#N/A
101.25		Min. Energy. Eqn.	86.22	#N/A	#N/A	#N/A
101.50		Min. Energy. Eqn.	113.26	#N/A	#N/A	#N/A
101.75		Regression Eqn.	141.06	#N/A	#N/A	#N/A
102.00		Regression Eqn.	170.46	#N/A	#N/A	#N/A
102.25		Regression Eqn.	201.26	403.16	<b>201.26</b>	INLET
102.50		Regression Eqn.	233.22	431.72	<b>233.22</b>	INLET
102.75		Regression Eqn.	265.78	458.99	<b>265.78</b>	INLET
103.00		Regression Eqn.	298.68	485.11	<b>298.68</b>	INLET
103.25		Regression Eqn.	331.42	510.21	<b>331.42</b>	INLET
103.50		Regression Eqn.	363.62	534.39	<b>363.62</b>	INLET
103.75		Regression Eqn.	395.04	557.76	<b>395.04</b>	INLET
104.00		Regression Eqn.	425.50	580.38	<b>425.50</b>	INLET
104.25		Regression Eqn.	454.90	604.46	<b>454.90</b>	INLET
104.50		Regression Eqn.	483.22	629.17	<b>483.22</b>	INLET
104.75		Regression Eqn.	510.44	652.94	<b>510.44</b>	INLET
105.00		Regression Eqn.	536.62	675.87	<b>536.62</b>	INLET
105.25		Regression Eqn.	561.84	698.05	<b>561.84</b>	INLET
105.50		Regression Eqn.	586.16	719.54	<b>586.16</b>	INLET
105.75		Regression Eqn.	609.62	740.41	<b>609.62</b>	INLET
106.00		Regression Eqn.	632.28	760.72	<b>632.28</b>	INLET
106.25		Regression Eqn.	654.22	780.49	<b>654.22</b>	INLET
106.50		Regression Eqn.	675.50	799.77	<b>675.50</b>	INLET
106.75		Regression Eqn.	696.22	818.60	<b>696.22</b>	INLET
107.00		Regression Eqn.	716.24	837.01	<b>716.24</b>	INLET
107.25		Regression Eqn.	735.82	855.02	<b>735.82</b>	INLET

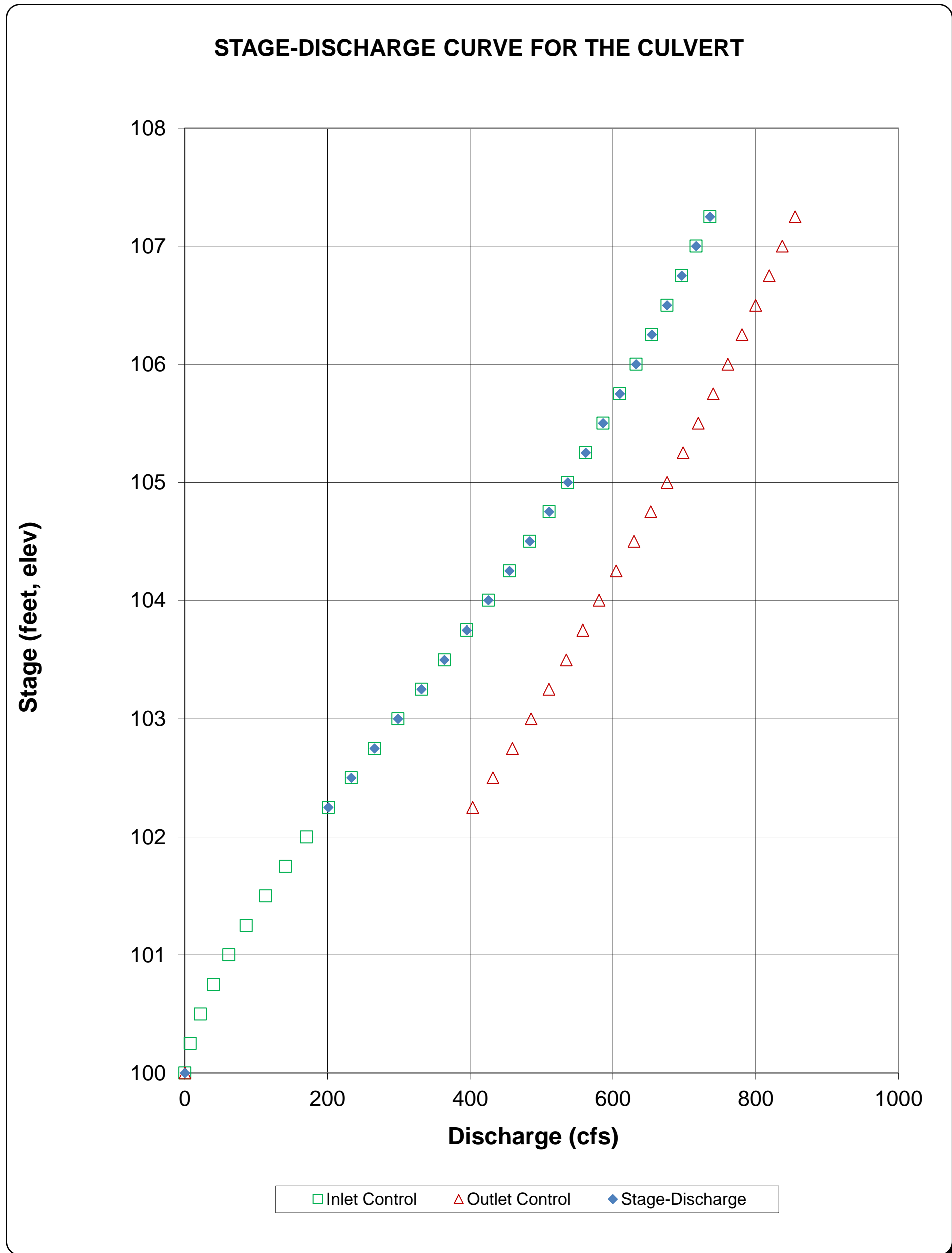
Processing Time: **00.20 Seconds**

# CULVERT SIZING (INLET vs. OUTLET CONTROL WITH TAILWATER EFFECTS)

MHFD-Culvert, Version 4.00 (May 2020)

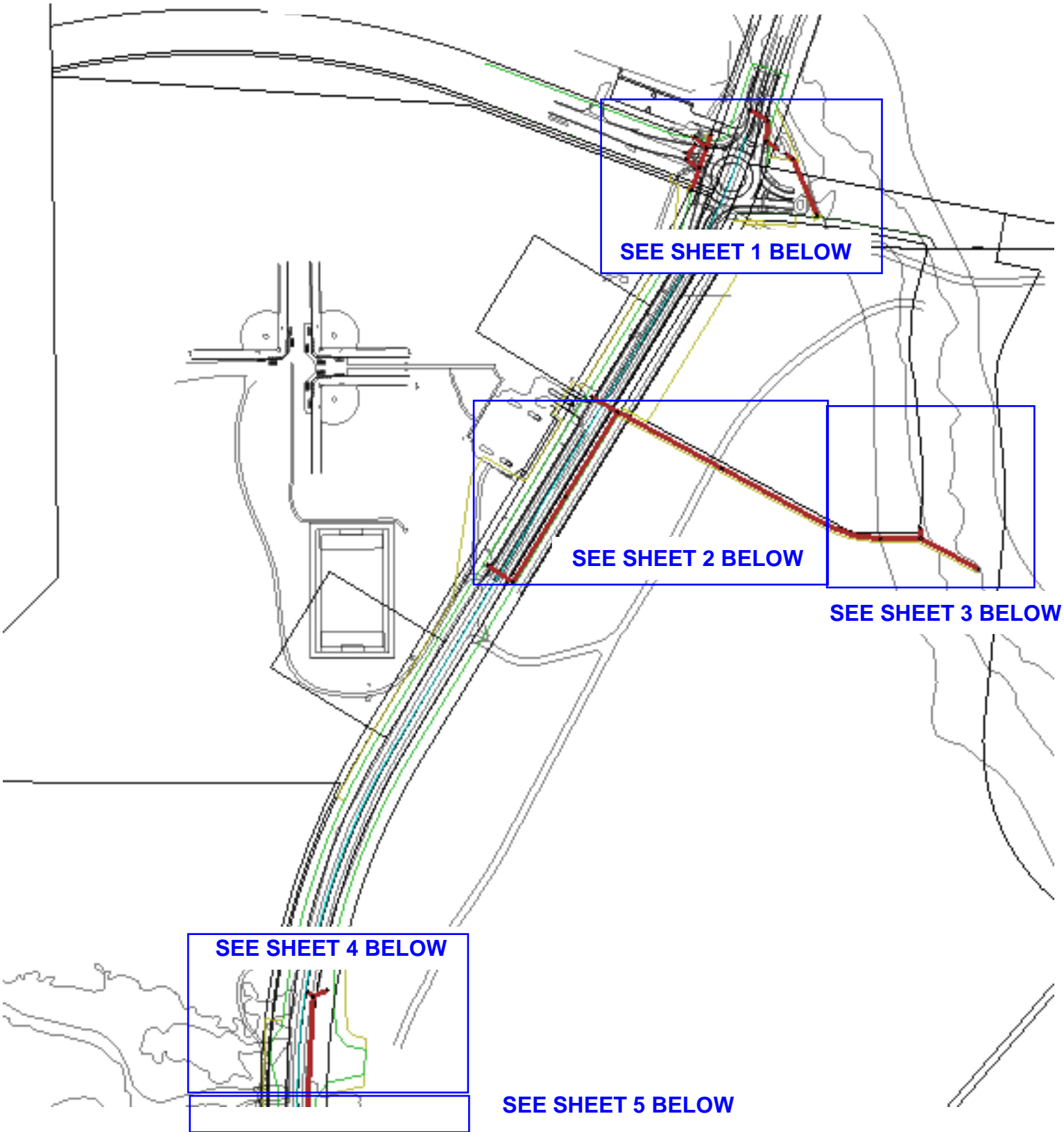
Project: EASTONVILLE ROAD

ID: DP8

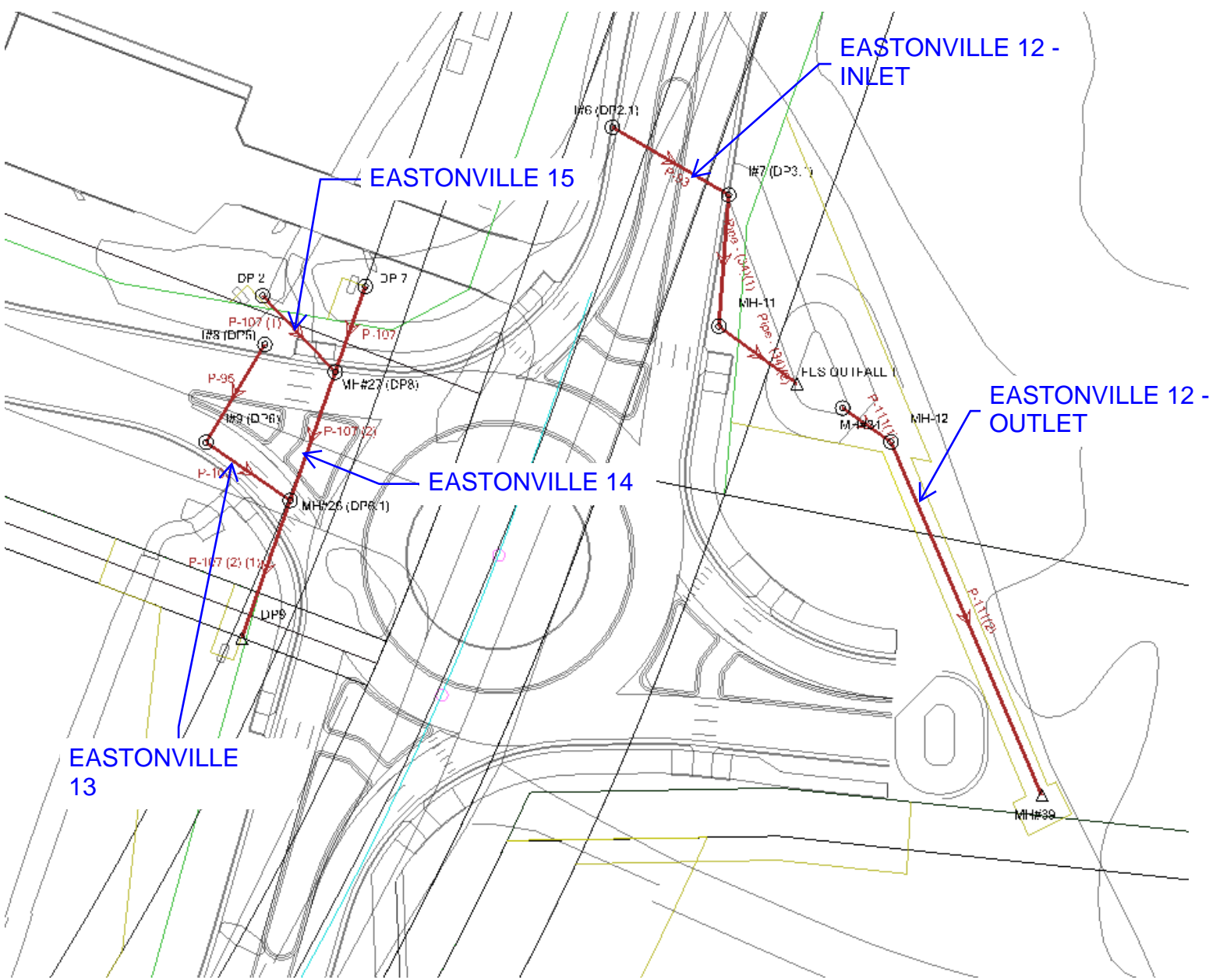


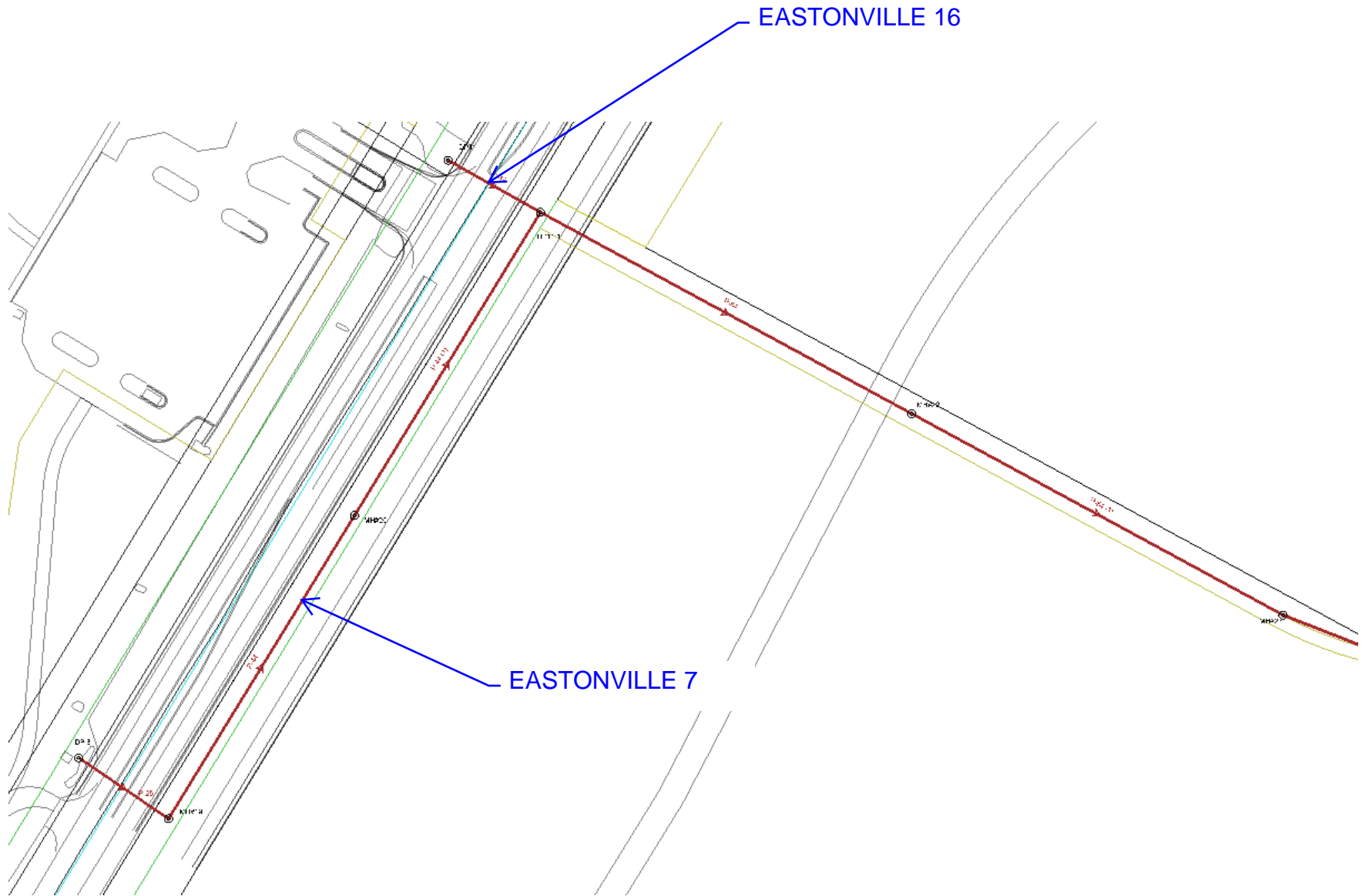


# STORMCAD NETWORK LAYOUT: SEGMENT 2



**MATCHLINE REFER TO SEGMENT 2 FDR**



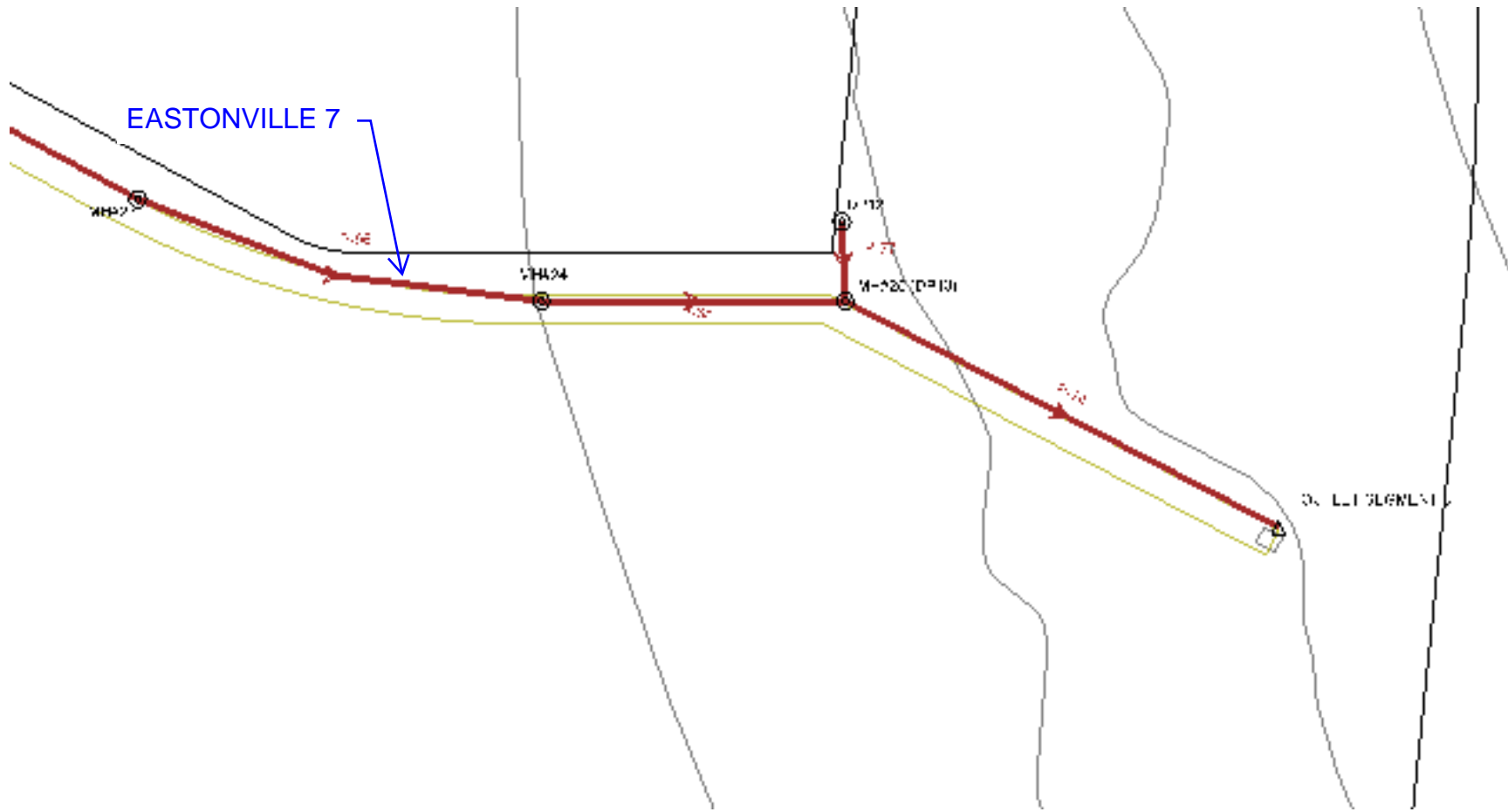


EASTONVILLE 16

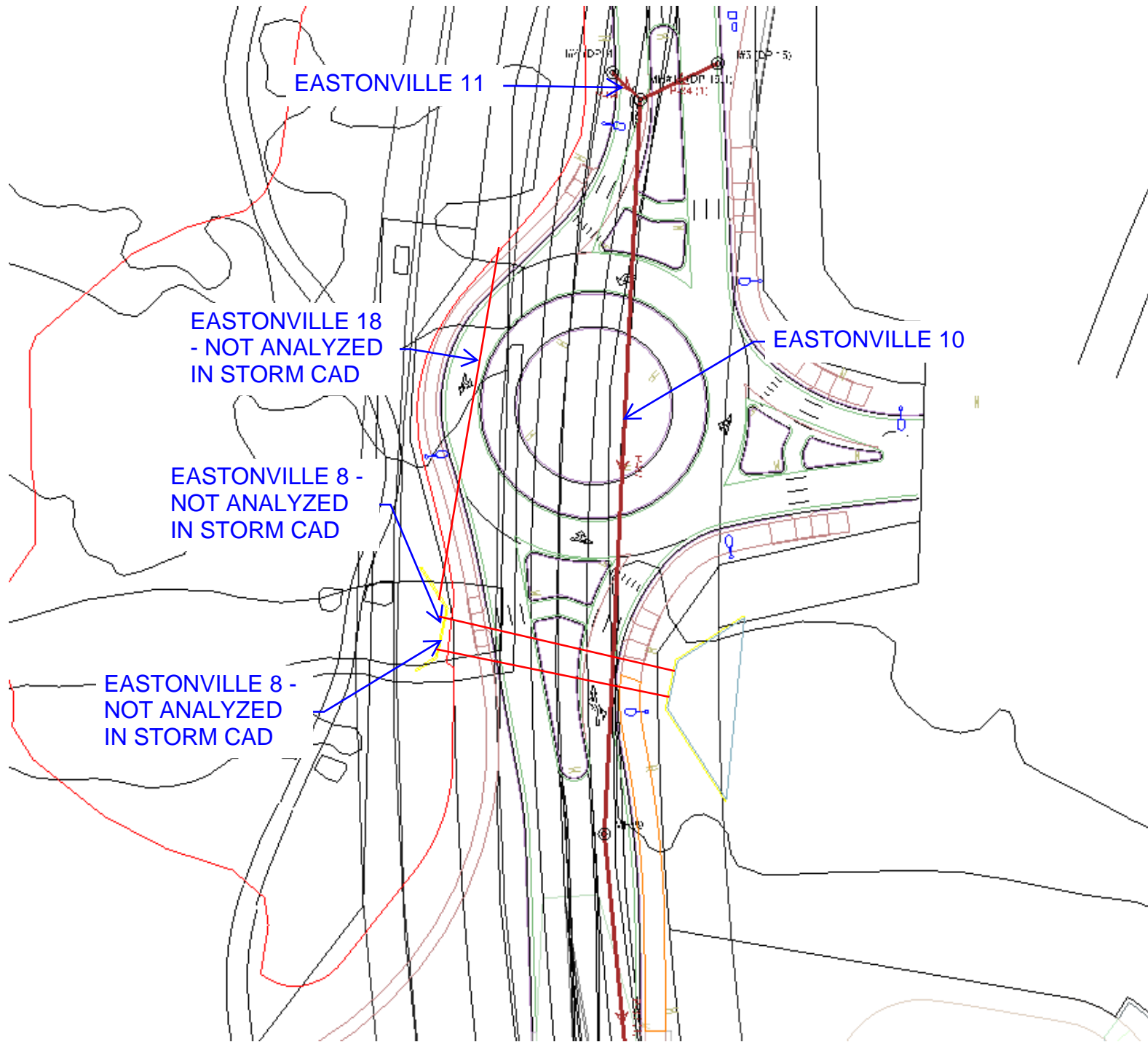
EASTONVILLE 7

MATCHLINE SEE SHEET 3

MATCHLINE SEE SHEET 2



SHEET 3



EASTONVILLE 10

EASTONVILLE 10  
(REFER TO SEGMENT  
1 FDR FOR  
UPSTREAM CALCS)

REFER TO  
SEGMENT 1 FDR  
FOR CALCS

REFER TO  
SEGMENT 1 FDR  
FOR CALCS

# 100 YEAR TAILWATER CONDITION: PIPE SUMMARY TABLE

	Start Node	Invert (Start) (ft)	Stop Node	Invert (Stop) (ft)	Length (User Defined) (ft)	Slope (Calculated) (ft/ft)	Diameter (in)	Manning's n	Flow (cfs)	Velocity (ft/s)	Capacity (Full Flow) (cfs)	Flow / Capacity (Design) (%)	Hydraulic Grade Line (In) (ft)	Hydraulic Grade Line (Out) (ft)
131: P-107 (2)	MH#26 (DP6.1)	7,020.50	DP9	7,019.00	60.7	0.025	24.0	0.013	22.40	11.97	35.57	63.0	7,022.19	7,020.22
132: P-103	I#9 (DP6)	7,023.00	MH#26 (DP6.1)	7,022.00	42.7	0.023	18.0	0.013	2.40	6.54	16.08	14.9	7,023.89	7,023.91
133: P-107 (2)	MH#27 (DP8)	7,021.00	MH#26 (DP6.1)	7,020.50	56.6	0.009	24.0	0.013	21.00	6.68	21.26	98.8	7,024.40	7,023.91
134: P-107	DP 7	7,023.01	MH#27 (DP8)	7,021.75	37.8	0.033	15.0	0.013	2.20	1.79	11.81	18.6	7,025.07	7,025.03
135: P-107 (1)	MH#27 (DP8)	7,021.00	DP 2	7,021.26	43.9	-0.006	24.0	0.013	18.80	5.98	17.41	108.0	7,025.33	7,025.03
136: P-95	I#8 (DP5)	7,024.00	I#9 (DP6)	7,023.00	47.5	0.021	18.0	0.013	1.30	5.26	15.24	8.5	7,024.43	7,023.94
137: P-93	I#6 (DP2.1)	7,022.34	I#7 (DP3.1)	7,021.78	55.9	0.010	18.0	0.013	1.50	4.22	10.51	14.3	7,022.80	7,022.73
140: P-44 (1)	MH#20	7,001.18	DP11.1	6,998.52	266.5	0.010	48.0	0.013	112.10	8.92	143.63	78.0	7,005.57	7,003.94
141: P-64	DP11.1	6,998.52	MH#22	6,995.26	316.5	0.010	48.0	0.013	112.10	12.80	145.88	76.8	7,001.72	6,997.89
142: P-44	MH#19	7,003.94	MH#20	7,001.28	266.5	0.010	48.0	0.013	112.10	12.64	143.63	78.0	7,007.14	7,005.63
143: P-26	DP 3	7,005.01	MH#19	7,004.04	81.5	0.012	48.0	0.013	112.10	8.92	156.73	71.5	7,009.86	7,009.36
144: P-64 (1)	MH#22	6,995.15	MH#23	6,988.82	316.6	0.020	48.0	0.013	112.10	16.57	203.15	55.2	6,998.35	6,995.32
145: P-87	MH#10 (DP 1...	6,993.41	MH#9	6,989.86	350.8	0.010	24.0	0.013	17.20	7.96	22.76	75.6	6,994.91	6,991.16
146: P-87 (1)	MH#9	6,989.76	MH#8	6,986.86	193.5	0.015	24.0	0.013	17.20	9.29	27.70	62.1	6,991.26	6,989.59
147: P-84	I#4 (DP14)	6,994.25	MH#10 (DP 1...	6,993.91	15.1	0.023	18.0	0.013	8.80	9.17	15.77	55.8	6,995.40	6,995.28
148: P-84 (1)	I#5 (DP 15)	6,994.74	MH#10 (DP 1...	6,993.91	39.7	0.021	18.0	0.013	10.40	9.25	15.18	68.5	6,995.98	6,995.28
149: P-66	MH#23	6,988.82	MH#24	6,988.00	149.0	0.006	48.0	0.013	112.10	8.92	106.64	105.1	6,995.26	6,994.35
150: P-68	MH#24	6,988.00	MH#25 (DP13)	6,987.50	107.8	0.005	48.0	0.013	112.10	8.92	97.84	114.6	6,994.29	6,993.63
151: P-77	DP12	6,990.32	MH#25 (DP13)	6,989.50	28.1	0.029	24.0	0.013	24.60	7.83	38.62	63.7	6,993.96	6,993.63
152: P-74	MH#25 (DP13)	6,987.50	OUTLET SEG...	6,986.67	173.3	0.005	48.0	0.013	136.60	10.87	99.34	137.5	6,991.98	6,990.15
225: P-42	DP11	7,001.22	DP11.1	6,999.51	85.7	0.020	24.0	0.013	44.00	14.01	31.96	137.7	7,007.19	7,003.94
227: Pipe - (34	I#7 (DP3.1)	7,021.78	MH-11	7,021.41	41.5	0.009	18.0	0.013	3.20	5.00	9.92	32.3	7,022.72	7,022.73
228: Pipe - (34	MH-11	7,021.21	FES OUTFALL 1	7,021.00	42.5	0.005	18.0	0.013	3.20	1.81	7.38	43.3	7,022.73	7,022.69
230: P-111(1)	MH#34	7,018.67	MH-12	7,018.57	20.4	0.005	18.0	0.013	0.80	2.73	7.35	10.9	7,019.00	7,018.90
231: P-111(2)	MH-12	7,018.37	MH#39	7,016.77	158.3	0.010	18.0	0.013	0.80	3.52	10.56	7.6	7,018.70	7,017.05

**NOTE: EASTONVILLE 12 - INLET & EASTONVILLE 10 SEGMENTS  
HAVE BEEN ANALYZED IN THE FREE OUTFALL CONDITION BELOW  
TO MEET CAPACITY & VELOCITY REQUIREMENTS. SEGMENT 1  
PIPES & STRUCTURES NOT INCLUDED IN TABLE, REFER TO  
SEGMENT 1 FDR.**

## 100 YEAR TAILWATER CONDITION: STRUCTURE SUMMARY TABLE

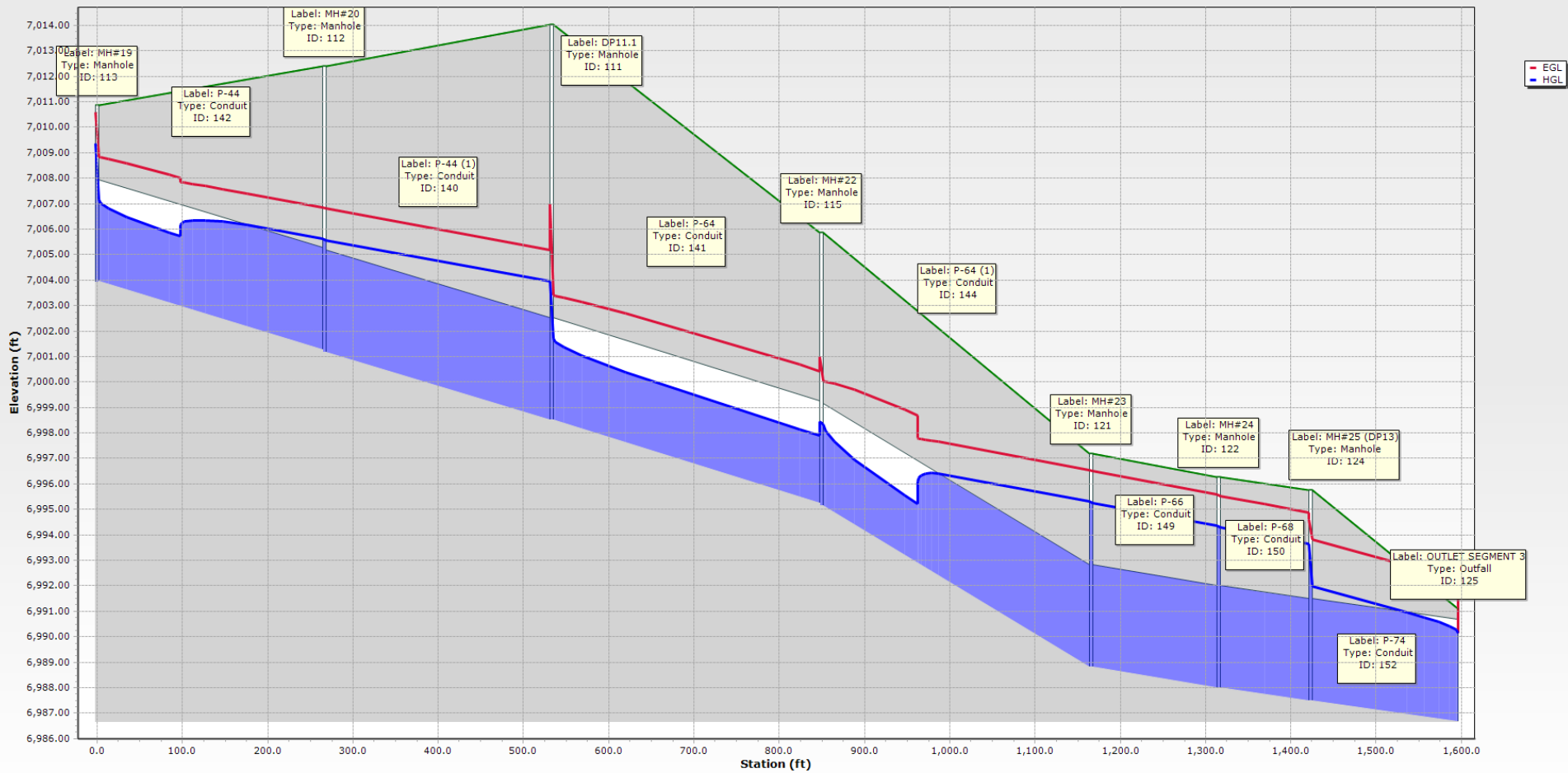
	Elevation (Ground) (ft)	Elevation (Rim) (ft)	Elevation (Invert in 1) (ft)	Flow (Total Out) (cfs)	Hydraulic Grade Line (Out) (ft)	Headloss Method	Hydraulic Grade Line (In) (ft)	Notes
98: MH#26 (D	7,027.15	7,027.15	7,022.00	22.40	7,022.19	Standard	7,023.91	STORM MH
99: MH#27 (D	7,027.09	7,027.09	7,021.75	21.00	7,024.40	Standard	7,025.03	STORM MH
100: I#9 (DP6)	7,027.04	7,027.04	7,023.00	2.40	7,023.89	Standard	7,023.94	CDOT Type-R
101: I#8 (DP5)	7,026.63	7,026.63	(N/A)	1.30	7,024.43	Standard	7,024.66	CDOT Type-R
102: I#7 (DP3.	7,026.51	7,026.51	7,021.78	3.20	7,022.72	Standard	7,022.73	CDOT Type-R
103: I#6 (DP2.	7,026.38	7,026.38	(N/A)	1.50	7,022.80	Standard	7,023.05	CDOT Type-R
106: MH#34	7,025.00	7,025.00	(N/A)	0.80	7,019.00	Standard	7,019.06	CDOT Type-C
111: DP11.1	7,014.03	7,014.03	6,998.52	112.10	7,001.72	Standard	7,003.94	STORM MH
112: MH#20	7,012.41	7,012.41	7,001.28	112.10	7,005.57	Standard	7,005.63	STORM MH
113: MH#19	7,010.85	7,010.85	7,004.04	112.10	7,007.14	Standard	7,009.36	STORM MH
115: MH#22	7,005.85	7,005.85	6,995.26	112.10	6,998.35	Standard	6,998.44	STORM MH
116: MH#9	7,000.92	7,000.92	6,989.86	17.20	6,991.26	Standard	6,991.29	STORM MH
117: I#4 (DP1	7,000.75	7,000.75	(N/A)	8.80	6,995.40	Standard	6,996.25	CDOT Type-R
118: MH#10 (	7,000.75	7,000.75	6,993.91	17.20	6,994.91	Standard	6,995.28	STORM MH
119: I#5 (DP 1	7,000.94	7,000.94	(N/A)	10.40	6,995.98	Standard	6,997.01	CDOT Type-R
121: MH#23	6,997.20	6,997.20	6,988.82	112.10	6,995.26	Standard	6,995.32	STORM MH
122: MH#24	6,996.25	6,996.25	6,988.00	112.10	6,994.29	Standard	6,994.35	STORM MH
123: DP12	6,996.40	6,996.40	(N/A)	24.60	6,993.96	Standard	6,995.39	CDOT Type-C
124: MH#25 (	6,995.75	6,995.75	6,987.50	136.60	6,991.98	Standard	6,993.63	STORM MH
192: DP 7	7,024.45	7,024.45	(N/A)	2.20	7,024.45	Standard	7,024.52	CDOT FES
193: DP 2	7,024.26	7,024.26	(N/A)	18.80	7,024.26	Standard	7,025.10	CDOT FES
194: DP 3	7,009.43	7,009.43	(N/A)	112.10	7,009.43	Standard	7,011.29	CDOT FES
224: DP11	7,010.95	7,010.95	(N/A)	44.00	7,007.19	Absolute	7,007.19	CDOT TYPE D INLET
226: MH-11	7,026.84	7,026.84	7,021.41	3.20	7,022.73	Absolute	7,022.73	
229: MH-12	7,024.52	7,024.52	7,018.57	0.80	7,018.70	Absolute	7,018.70	

	Elevation (Ground) (ft)	Elevation (Invert) (ft)	Boundary Condition Type	Elevation (User Defined Tailwater) (ft)	Hydraulic Grade (ft)	Flow (Total Out) (cfs)	Notes
107: DP9	7,022.74	7,019.00	Free Outfall		7,020.22	22.40	CDOT FES
108: FES OUTF	7,022.50	7,021.00	User Defined Tailwater	7,022.69	7,022.69	3.20	CDOT FES
110: MH#39	7,018.27	7,016.77	Free Outfall		7,017.05	0.80	CDOT FES
125: OUTLET S	6,991.09	6,986.67	Free Outfall		6,990.15	136.60	CDOT FES

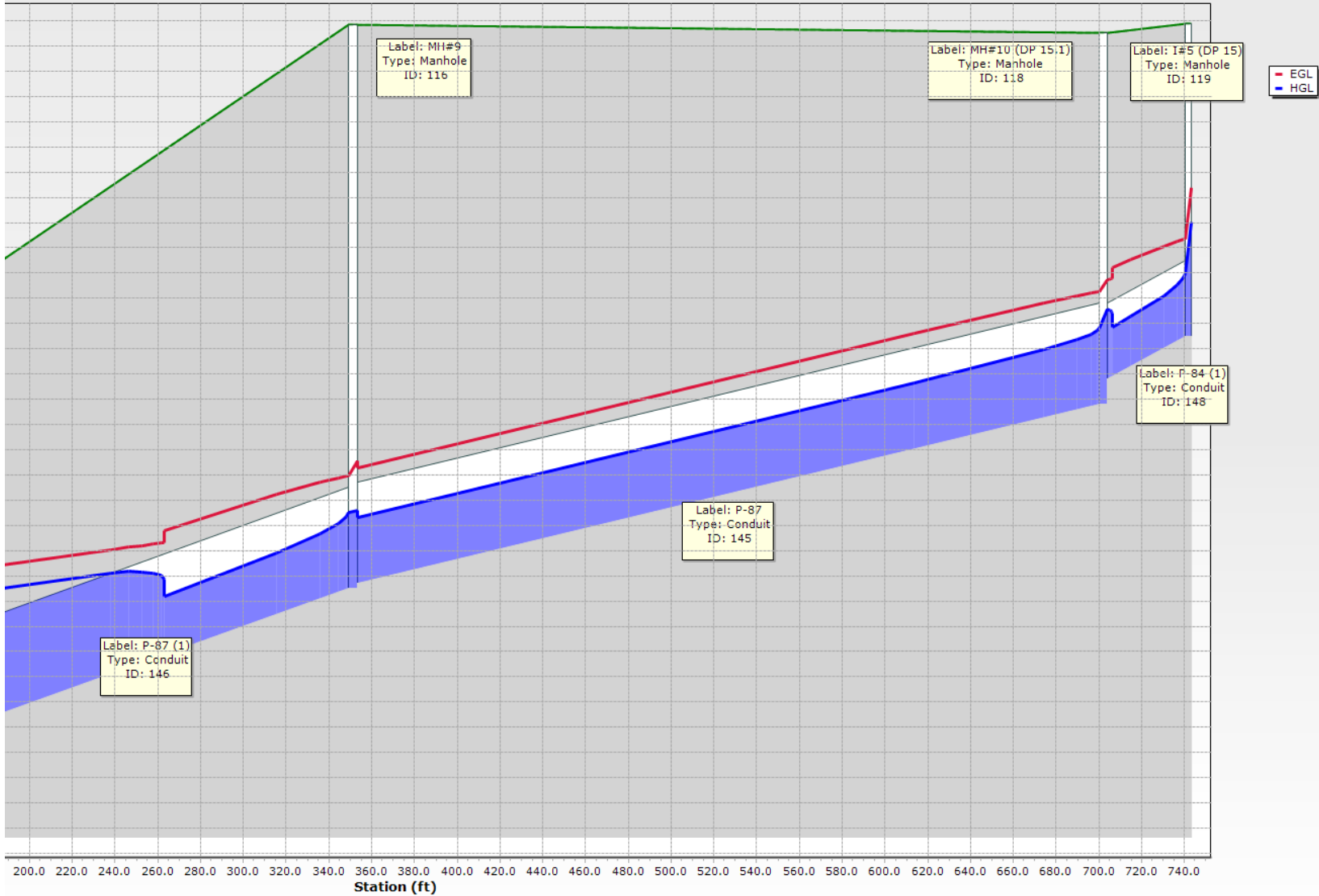
**NOTE: EASTONVILLE 12 - INLET & EASTONVILLE 10 SEGMENTS HAVE BEEN ANALYZED IN THE FREE OUTFALL CONDITION BELOW TO MEET CAPACITY & VELOCITY REQUIREMENTS. SEGMENT 1 PIPES & STRUCTURES NOT INCLUDED IN TABLE, REFER TO SEGMENT 1 FDR.**



EASTONVILLE 7 - 100-YR TAILWATER CONDITION

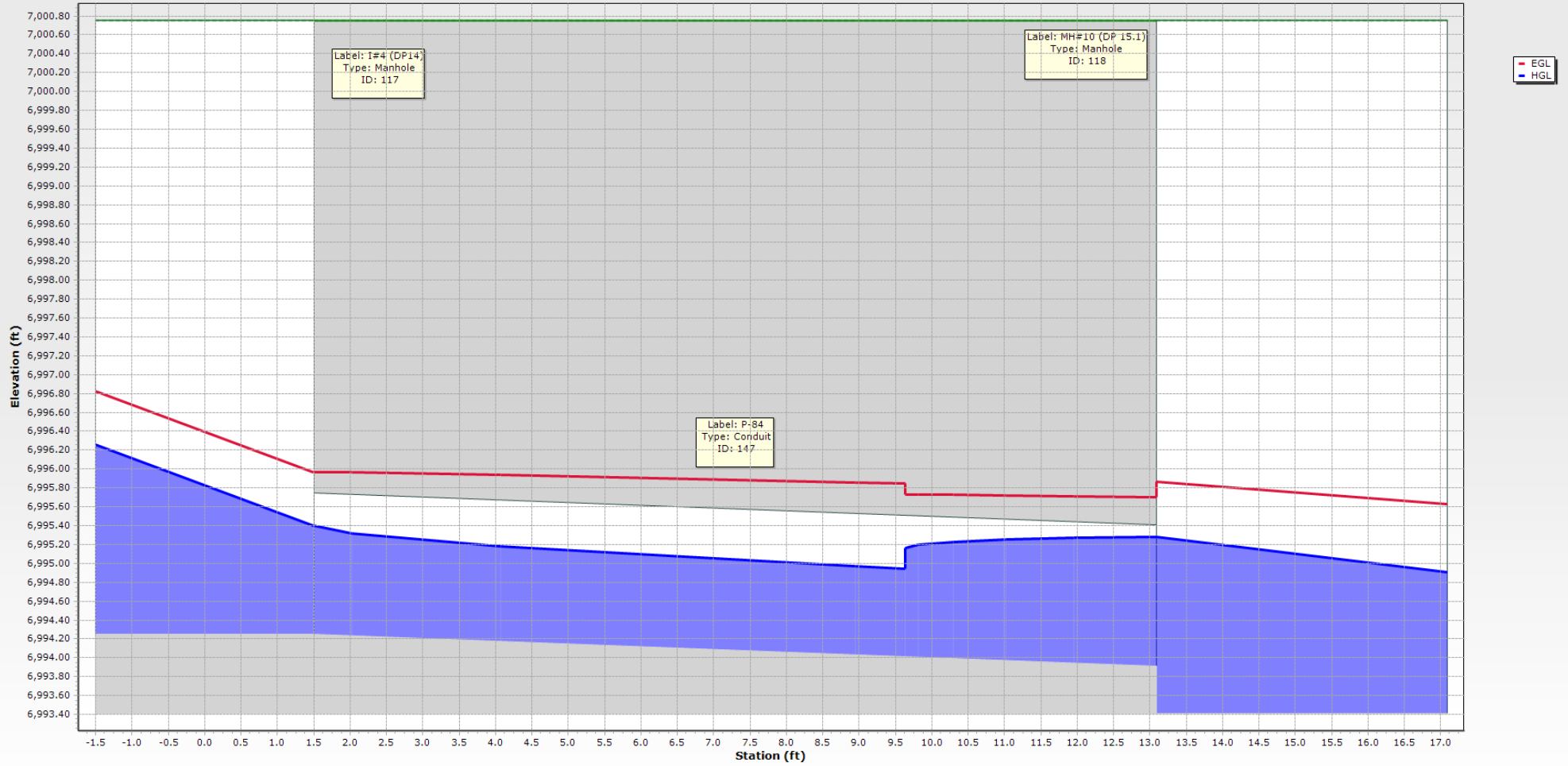


# EASTONVILLE 10 - 100-YR TAILWATER CONDITION

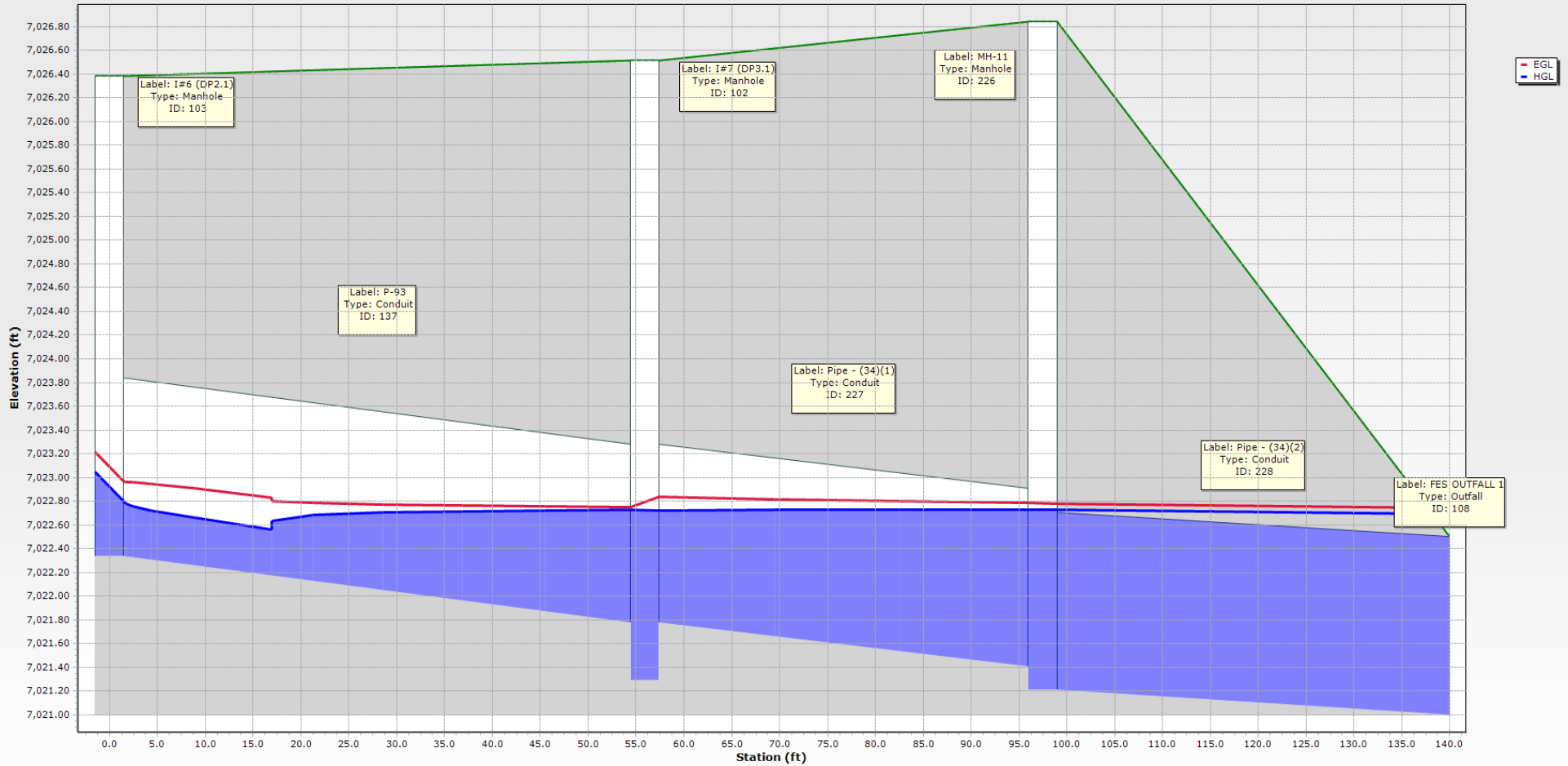


**NOTE: THIS SEGMENT HAS BEEN ANALYZED IN THE FREE  
OUTFALL CONDITION BLEW TO MEET CAPACITY & VELOCITY  
REQUIREMENTS**

### EASTONVILLE 11 - 100-YR TAILWATER CONDITION

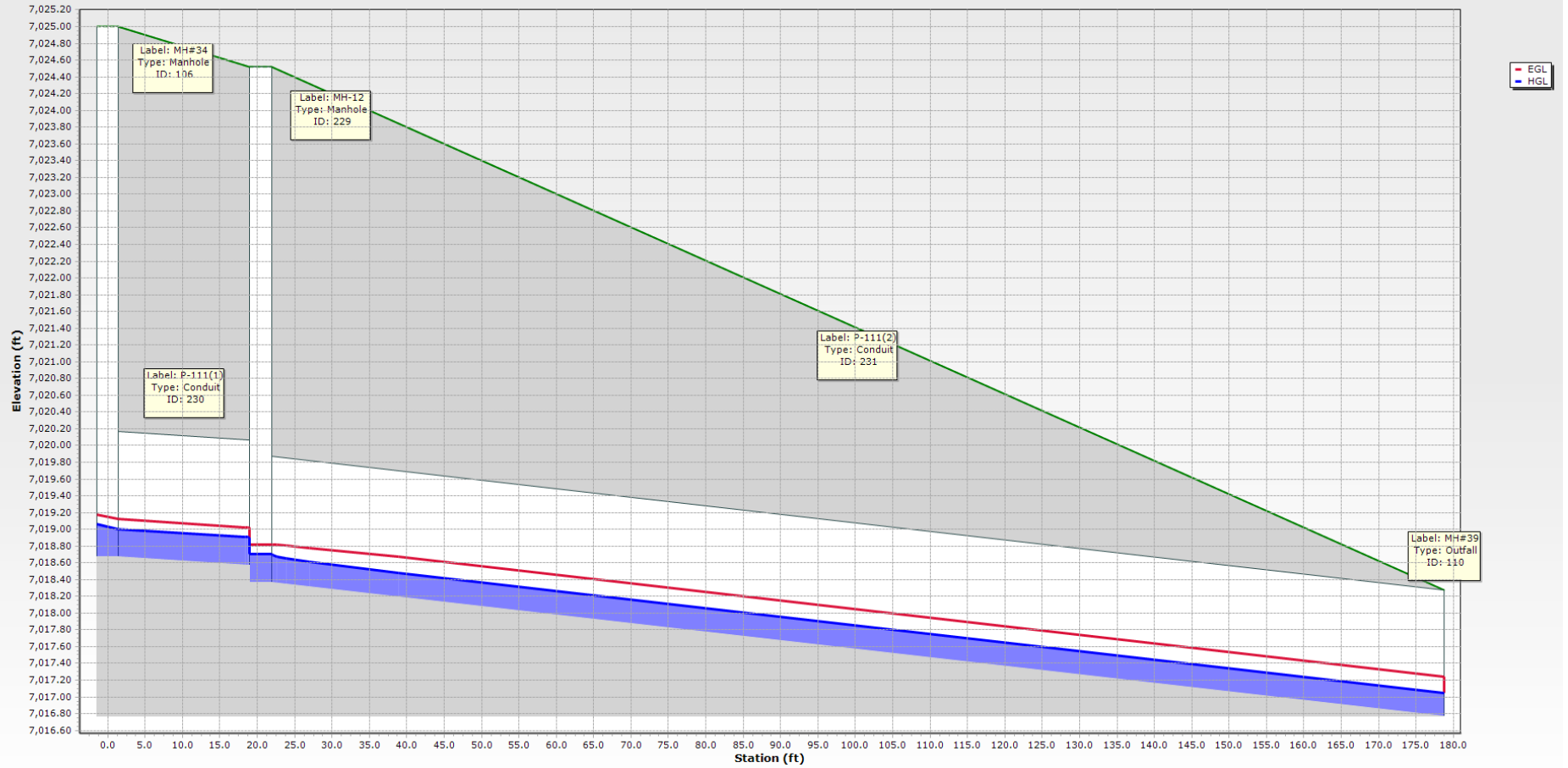


EASTONVILLE 12 INLET - 100-YR TAILWATER CONDITION

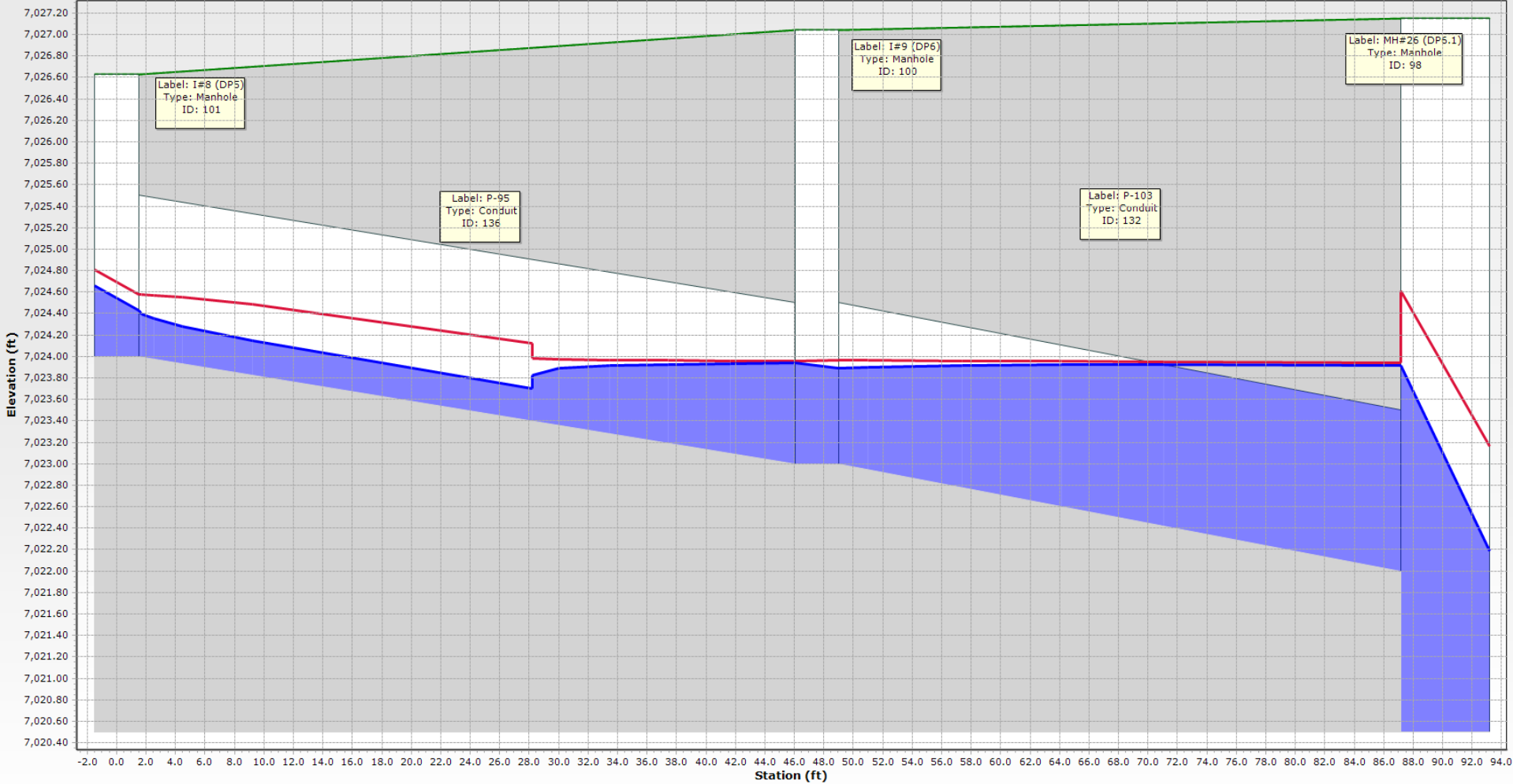


**NOTE: THIS SEGMENT HAS BEEN ANALYZED IN THE FREE OUTFALL CONDITION BLEW TO MEET CAPACITY & VELOCITY REQUIREMENTS**

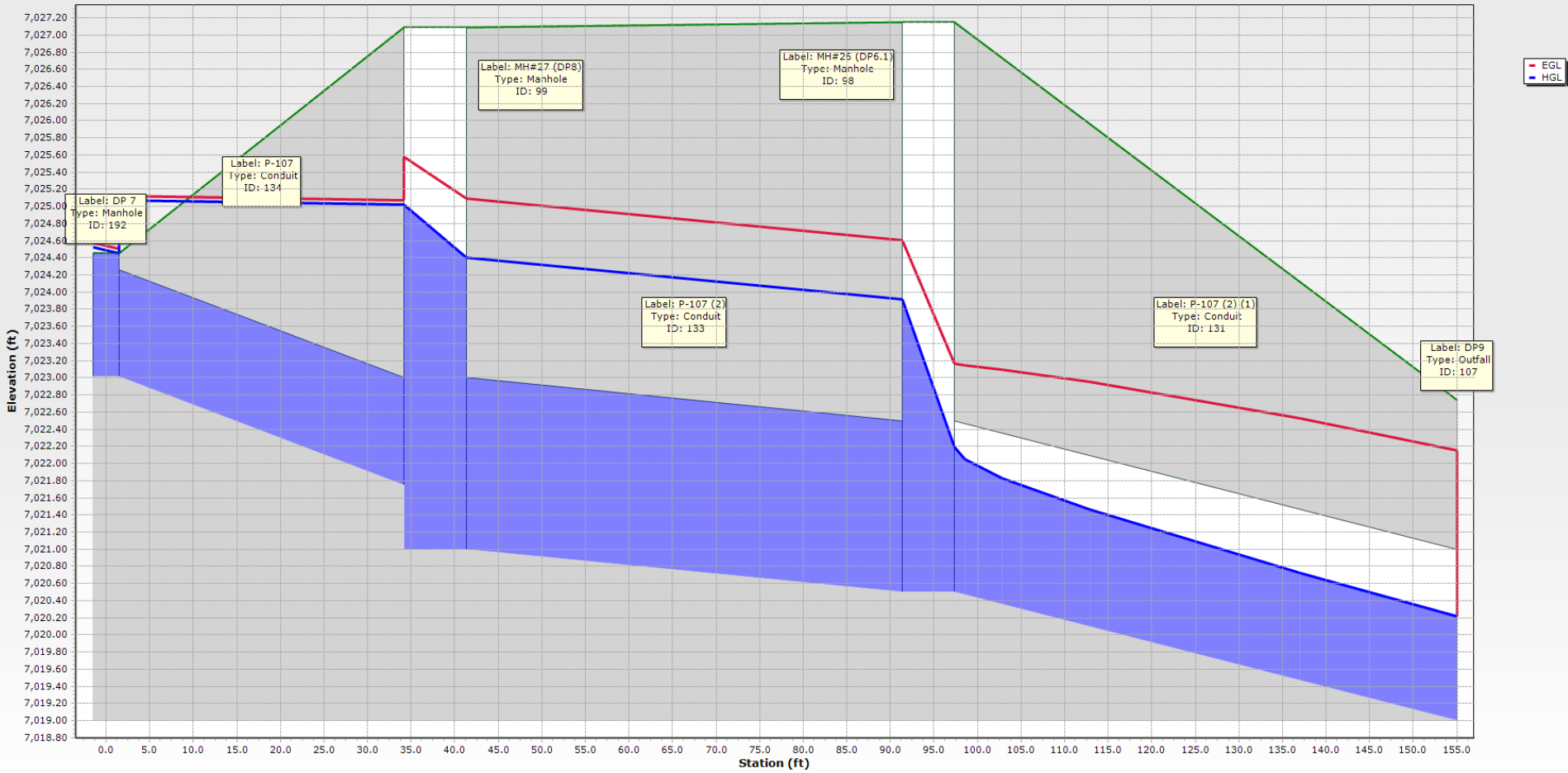
### EASTONVILLE 12 OUTLET - 100-YR TAILWATER CONDITION



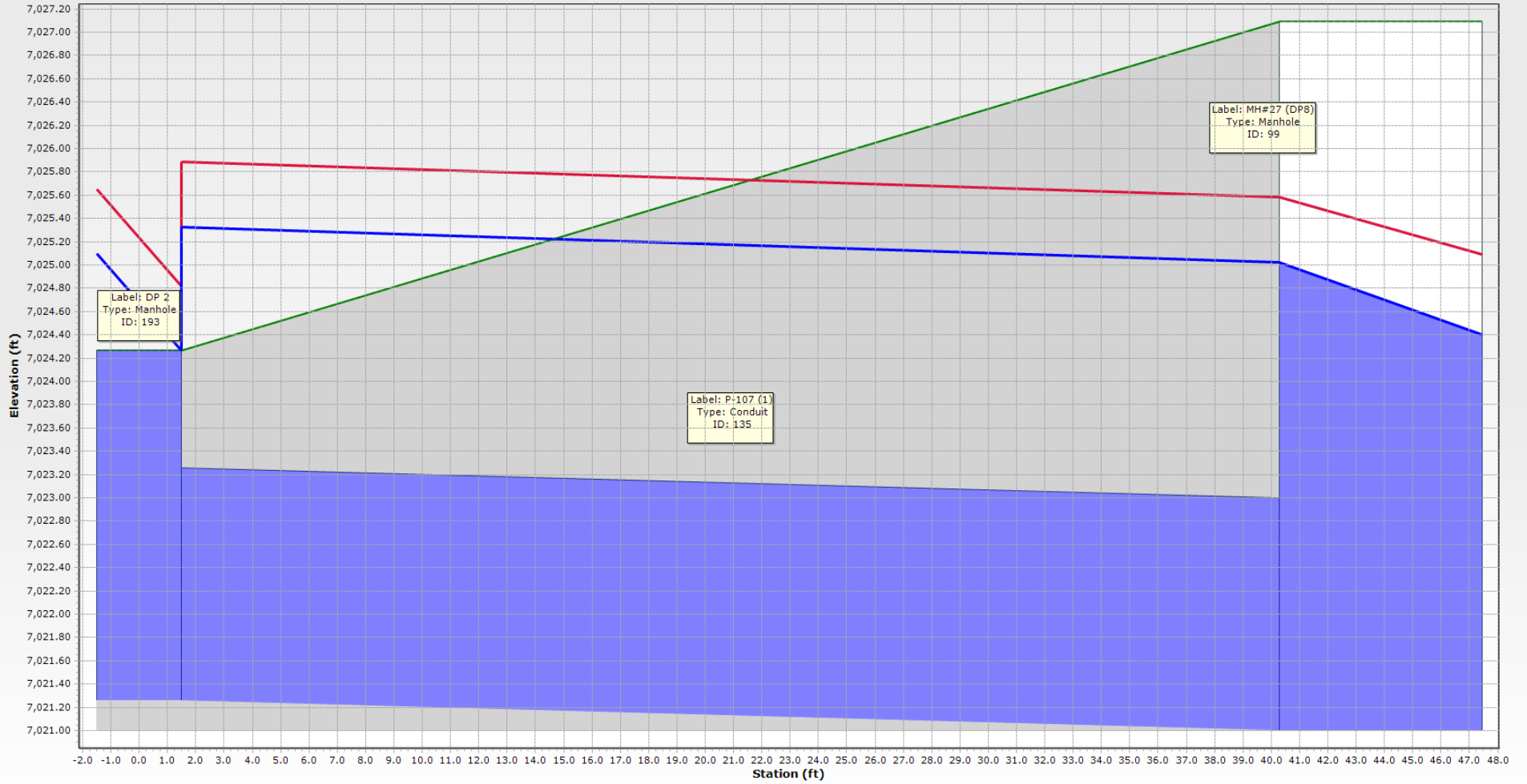
EASTONVILLE 13 - 100-YR TAILWATER CONDITION



**EASTONVILLE 14 - 100-YR TAILWATER CONDITION**

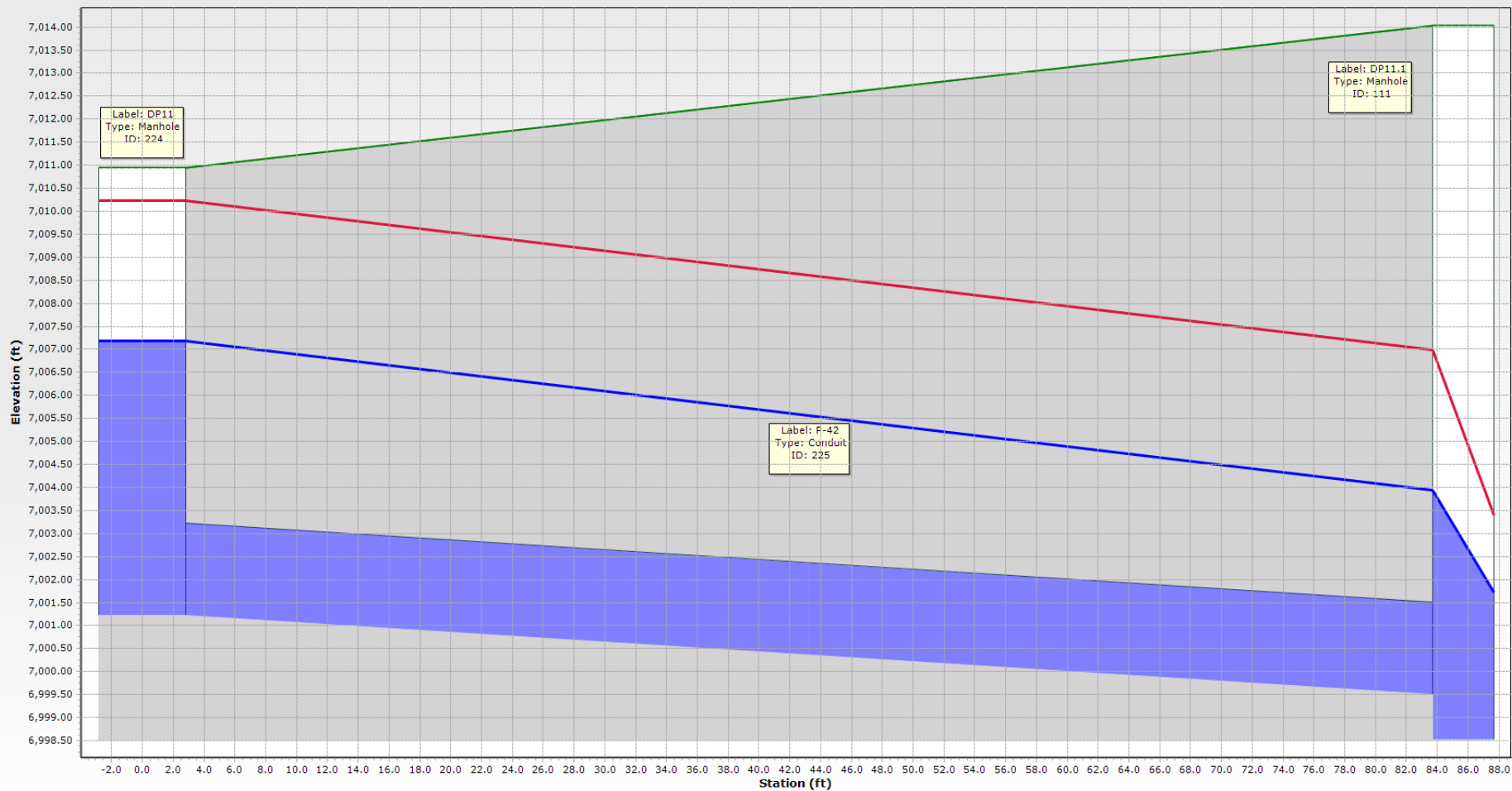


### EASTONVILLE 15 - 100-YR TAILWATER CONDITION





### EASTONVILLE 16 - 100-YR TAILWATER CONDITION



## 5 YEAR TAILWATER CONDITION: PIPE SUMMARY TABLE

	Start Node	Invert (Start) (ft)	Stop Node	Invert (Stop) (ft)	Length (User Defined) (ft)	Slope (Calculated) (ft/ft)	Diameter (in)	Manning's n	Flow (cfs)	Velocity (ft/s)	Capacity (Full Flow) (cfs)	Flow / Capacity (Design) (%)	Hydraulic Grade Line (In) (ft)	Hydraulic Grade Line (Out) (ft)
131: P-107 (2)	MH#26 (DP6.1)	7,020.50	DP9	7,019.00	60.7	0.025	24.0	0.013	2.90	6.82	35.57	8.2	7,021.09	7,019.39
132: P-103	I#9 (DP6)	7,023.00	MH#26 (DP6.1)	7,022.00	42.7	0.023	18.0	0.013	1.20	5.34	16.08	7.5	7,023.41	7,022.28
133: P-107 (2)	MH#27 (DP8)	7,021.00	MH#26 (DP6.1)	7,020.50	56.6	0.009	24.0	0.013	2.00	4.25	21.26	9.4	7,021.49	7,021.47
134: P-107	DP 7	7,023.01	MH#27 (DP8)	7,021.75	37.8	0.033	15.0	0.013	0.30	4.09	11.81	2.5	7,023.22	7,021.89
135: P-107 (1)	MH#27 (DP8)	7,021.00	DP 2	7,021.26	43.9	-0.006	24.0	0.013	1.70	3.52	17.41	9.8	7,021.71	7,021.65
136: P-95	I#8 (DP5)	7,024.00	I#9 (DP6)	7,023.00	47.5	0.021	18.0	0.013	0.70	4.38	15.24	4.6	7,024.31	7,023.50
137: P-93	I#6 (DP2.1)	7,022.34	I#7 (DP3.1)	7,021.78	55.9	0.010	18.0	0.013	0.80	3.51	10.51	7.6	7,022.67	7,022.26
140: P-44 (1)	MH#20	7,001.18	DP11.1	6,998.52	266.5	0.010	48.0	0.013	6.10	5.68	143.63	4.2	7,001.90	6,999.57
141: P-64	DP11.1	6,998.52	MH#22	6,995.26	316.5	0.010	48.0	0.013	6.10	5.74	145.88	4.2	6,999.24	6,995.82
142: P-44	MH#19	7,003.94	MH#20	7,001.28	266.5	0.010	48.0	0.013	6.10	5.68	143.63	4.2	7,004.66	7,001.84
143: P-26	DP 3	7,005.01	MH#19	7,004.04	81.5	0.012	48.0	0.013	6.10	6.03	156.73	3.9	7,005.73	7,004.99
144: P-64 (1)	MH#22	6,995.15	MH#23	6,988.82	316.6	0.020	48.0	0.013	6.10	7.23	203.15	3.0	6,995.87	6,989.55
145: P-87	MH#10 (DP 1...)	6,993.41	MH#9	6,989.86	350.8	0.010	24.0	0.013	10.20	7.04	22.76	44.8	6,994.55	6,990.80
146: P-87 (1)	MH#9	6,989.76	MH#8	6,986.86	193.5	0.015	24.0	0.013	10.20	8.15	27.70	36.8	6,990.90	6,988.20
147: P-84	I#4 (DP14)	6,994.25	MH#10 (DP 1...)	6,993.91	15.1	0.023	18.0	0.013	5.20	8.00	15.77	33.0	6,995.13	6,994.80
148: P-84 (1)	I#5 (DP 15)	6,994.74	MH#10 (DP 1...)	6,993.91	39.7	0.021	18.0	0.013	5.00	7.70	15.18	32.9	6,995.60	6,994.80
149: P-66	MH#23	6,988.82	MH#24	6,988.00	149.0	0.006	48.0	0.013	6.10	4.60	106.64	5.7	6,989.54	6,988.73
150: P-68	MH#24	6,988.00	MH#25 (DP13)	6,987.50	107.8	0.005	48.0	0.013	6.10	4.33	97.84	6.2	6,988.72	6,988.71
151: P-77	DP12	6,990.32	MH#25 (DP13)	6,989.50	28.1	0.029	24.0	0.013	3.90	7.89	38.62	10.1	6,991.01	6,989.95
152: P-74	MH#25 (DP13)	6,987.50	OUTLET SEG...	6,986.67	173.3	0.005	48.0	0.013	10.00	5.07	99.34	10.1	6,988.42	6,988.30
225: P-42	DP11	7,001.22	DP11.1	6,999.51	85.7	0.020	24.0	0.013	7.50	8.31	31.96	23.5	7,002.19	7,000.17
227: Pipe - (34	I#7 (DP3.1)	7,021.78	MH-11	7,021.41	41.5	0.009	18.0	0.013	1.60	4.12	9.92	16.1	7,022.25	7,022.16
228: Pipe - (34	MH-11	7,021.21	FES OUTFALL 1	7,021.00	42.5	0.005	18.0	0.013	1.60	3.34	7.38	21.7	7,022.16	7,022.16
230: P-111(1)	MH#34	7,018.67	MH-12	7,018.57	20.4	0.005	18.0	0.013	0.10	1.46	7.35	1.4	7,018.79	7,018.70
231: P-111(2)	MH-12	7,018.37	MH#39	7,016.77	158.3	0.010	18.0	0.013	0.80	3.52	10.56	7.6	7,018.70	7,017.05

**NOTE: EASTONVILLE 12 - INLET, EASTONVILLE 10, & EASTONVILLE 11 SEGMENTS HAVE BEEN ANALYZED IN THE FREE OUTFALL CONDITION BELOW TO MEET CAPACITY & VELOCITY REQUIREMENTS. SEGMENT 1 PIPES & STRUCTURES INCLUDED IN TABLE, REFER TO FDR FOR COMPLETE ANALYSIS.**

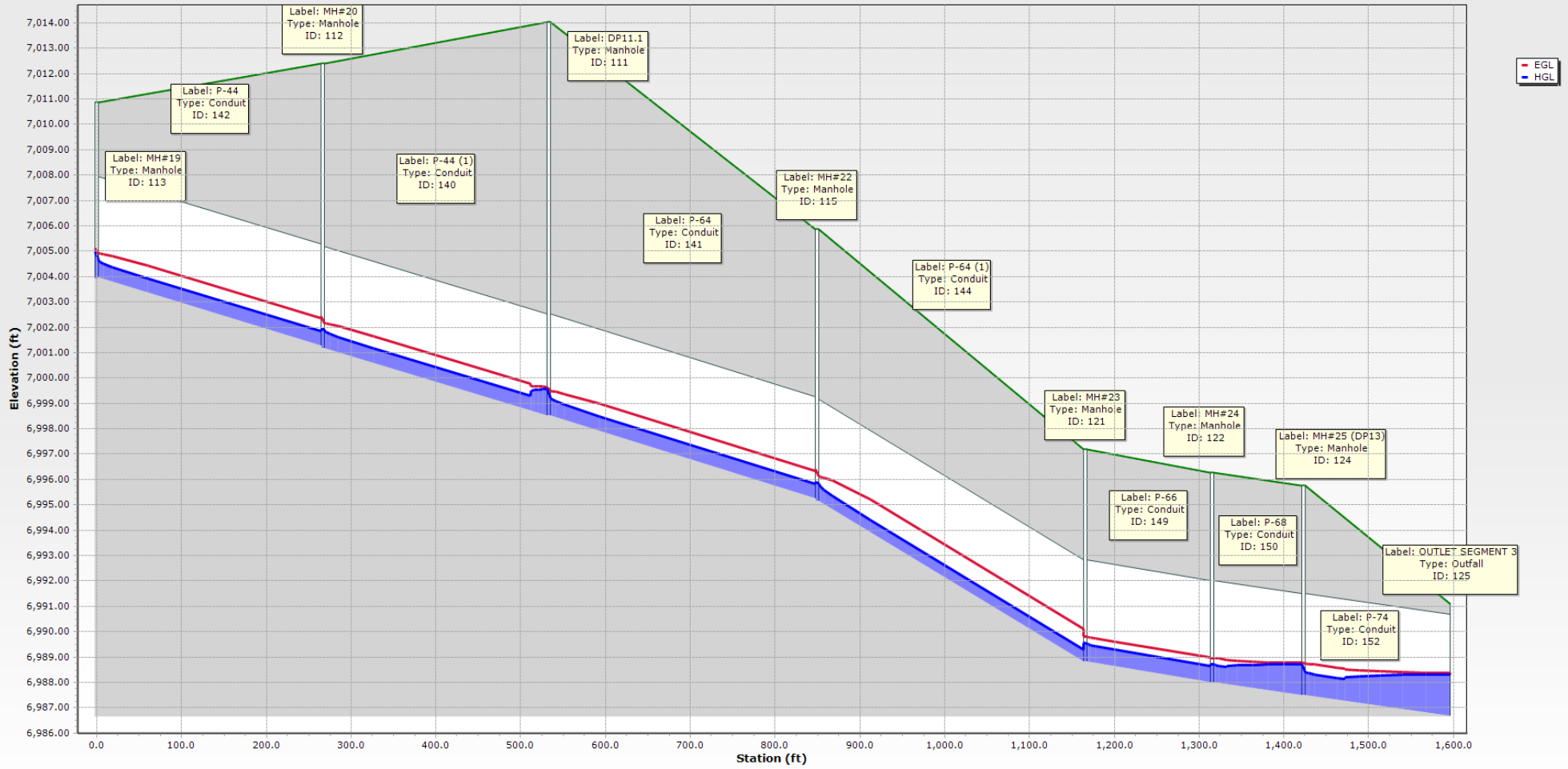
## 5 YEAR TAILWATER CONDITION: STRUCTURE SUMMARY TABLE

	Elevation (Ground) (ft)	Elevation (Rim) (ft)	Elevation (Invert in 1) (ft)	Flow (Total Out) (cfs)	Hydraulic Grade Line (Out) (ft)	Headloss Method	Hydraulic Grade Line (In) (ft)	Notes
98: MH#26 (D	7,027.15	7,027.15	7,022.00	2.90	7,021.09	Standard	7,021.47	STORM MH
99: MH#27 (D	7,027.09	7,027.09	7,021.75	2.00	7,021.49	Standard	7,021.65	STORM MH
100: I#9 (DP6)	7,027.04	7,027.04	7,023.00	1.20	7,023.41	Standard	7,023.50	CDOT Type-R
101: I#8 (DP5)	7,026.63	7,026.63	(N/A)	0.70	7,024.31	Standard	7,024.47	CDOT Type-R
102: I#7 (DP3.	7,026.51	7,026.51	7,021.78	1.60	7,022.25	Standard	7,022.26	CDOT Type-R
103: I#6 (DP2.	7,026.38	7,026.38	(N/A)	0.80	7,022.67	Standard	7,022.85	CDOT Type-R
106: MH#34	7,025.00	7,025.00	(N/A)	0.10	7,018.79	Standard	7,018.81	CDOT Type-C
111: DP11.1	7,014.03	7,014.03	6,998.52	6.10	6,999.24	Standard	6,999.57	STORM MH
112: MH#20	7,012.41	7,012.41	7,001.28	6.10	7,001.90	Standard	7,001.91	STORM MH
113: MH#19	7,010.85	7,010.85	7,004.04	6.10	7,004.66	Standard	7,004.99	STORM MH
115: MH#22	7,005.85	7,005.85	6,995.26	6.10	6,995.87	Standard	6,995.88	STORM MH
116: MH#9	7,000.92	7,000.92	6,989.86	10.20	6,990.90	Standard	6,990.93	STORM MH
117: I#4 (DP1	7,000.75	7,000.75	(N/A)	5.20	6,995.13	Standard	6,995.67	CDOT Type-R
118: MH#10 (	7,000.75	7,000.75	6,993.91	10.20	6,994.55	Standard	6,994.80	STORM MH
119: I#5 (DP 1	7,000.94	7,000.94	(N/A)	5.00	6,995.60	Standard	6,996.13	CDOT Type-R
121: MH#23	6,997.20	6,997.20	6,988.82	6.10	6,989.54	Standard	6,989.55	STORM MH
122: MH#24	6,996.25	6,996.25	6,988.00	6.10	6,988.72	Standard	6,988.73	STORM MH
123: DP12	6,996.40	6,996.40	(N/A)	3.90	6,991.01	Standard	6,991.39	CDOT Type-C
124: MH#25 (	6,995.75	6,995.75	6,987.50	10.00	6,988.42	Standard	6,988.71	STORM MH
192: DP 7	7,024.45	7,024.45	(N/A)	0.30	7,023.22	Standard	7,023.33	CDOT FES
193: DP 2	7,024.26	7,024.26	(N/A)	1.70	7,021.71	Standard	7,021.95	CDOT FES
194: DP 3	7,009.43	7,009.43	(N/A)	6.10	7,005.73	Standard	7,006.10	CDOT FES
224: DP11	7,010.95	7,010.95	(N/A)	7.50	7,002.19	Absolute	7,002.19	CDOT TYPE D INLET
226: MH-11	7,026.84	7,026.84	7,021.41	1.60	7,022.16	Absolute	7,022.16	
229: MH-12	7,024.52	7,024.52	7,018.57	0.80	7,018.70	Absolute	7,018.70	

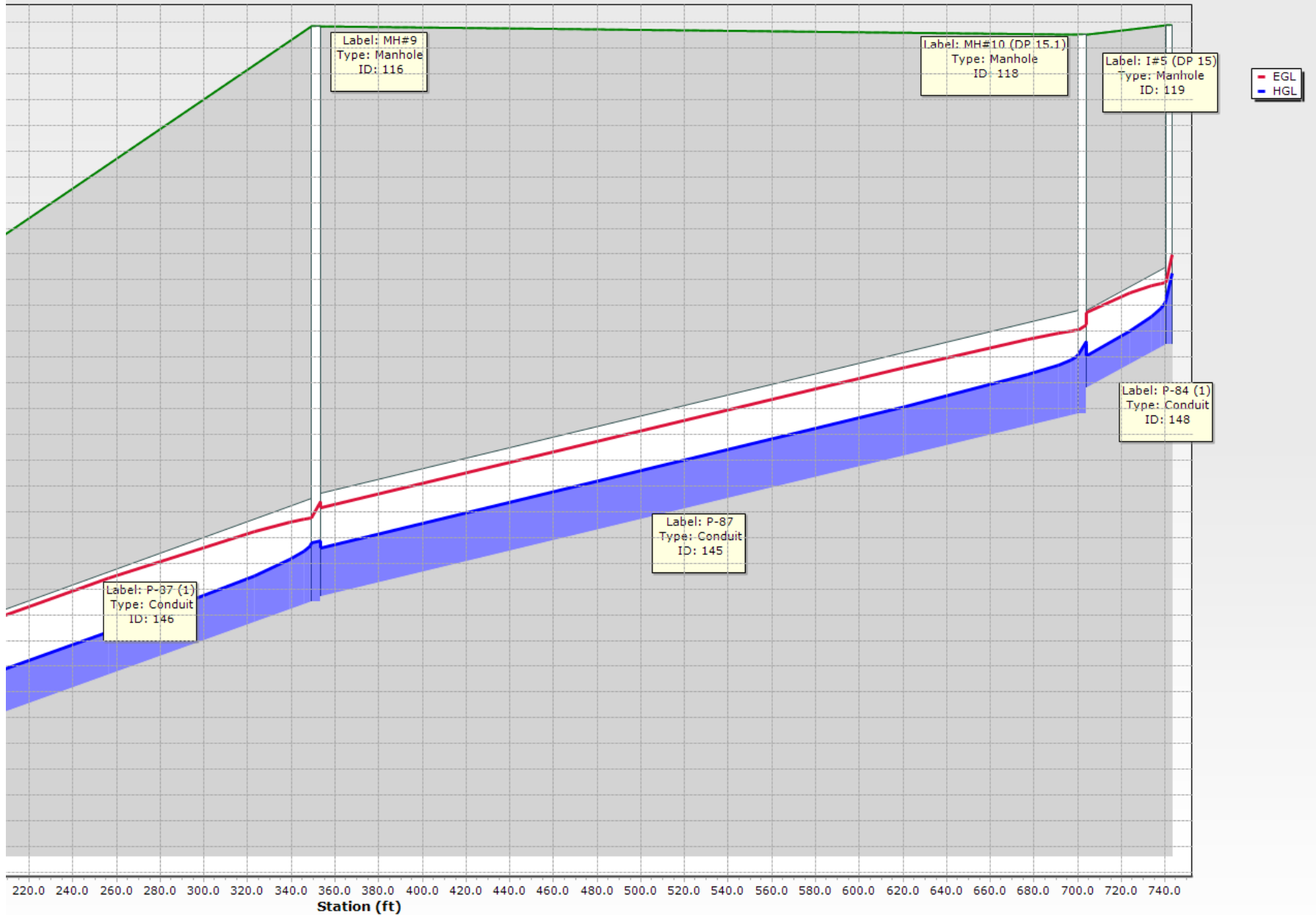
	Elevation (Ground) (ft)	Elevation (Invert) (ft)	Boundary Condition Type	Elevation (User Defined Tailwater) (ft)	Hydraulic Grade (ft)	Flow (Total Out) (cfs)	Notes
107: DP9	7,022.74	7,019.00	Free Outfall		7,019.39	2.90	CDOT FES
108: FES OUTF	7,022.50	7,021.00	User Defined Tailwater	7,022.16	7,022.16	1.60	CDOT FES
110: MH#39	7,018.27	7,016.77	Free Outfall		7,017.05	0.80	CDOT FES
125: OUTLET S	6,991.09	6,986.67	User Defined Tailwater	6,988.30	6,988.30	10.00	CDOT FES

**NOTE: EASTONVILLE 12 - INLET & EASTONVILLE 10 SEGMENTS HAVE BEEN ANALYZED IN THE FREE OUTFALL CONDITION BELOW TO MEET CAPACITY & VELOCITY REQUIREMENTS. SEGMENT 1 PIPES & STRUCTURES NOT INCLUDED IN TABLE, REFER TO SEGMENT 1 FDR.**

### EASTONVILLE 7 - 5-YR TAILWATER CONDITION

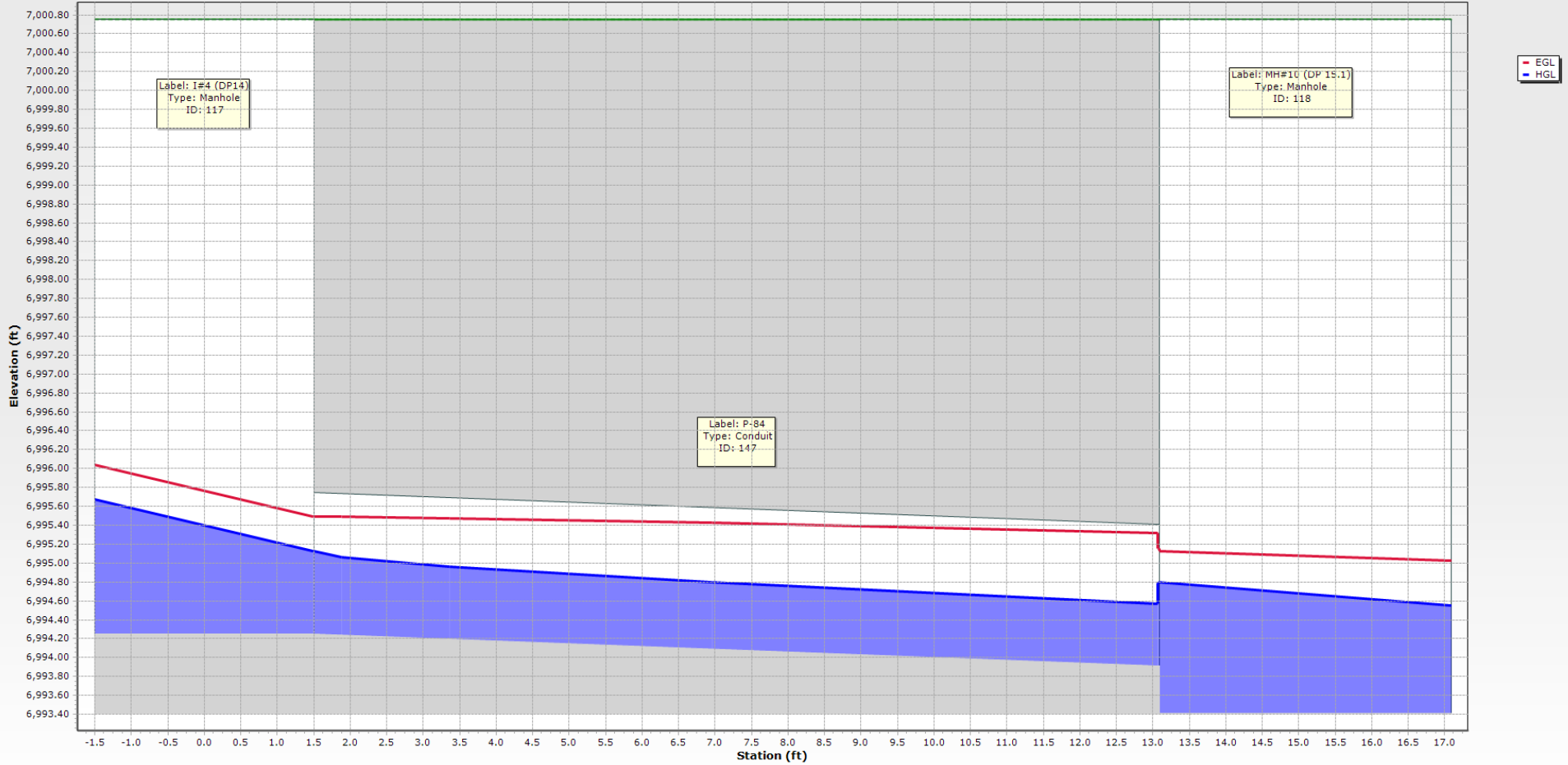


# EASTONVILLE 10 - 5-YR TAILWATER CONDITION

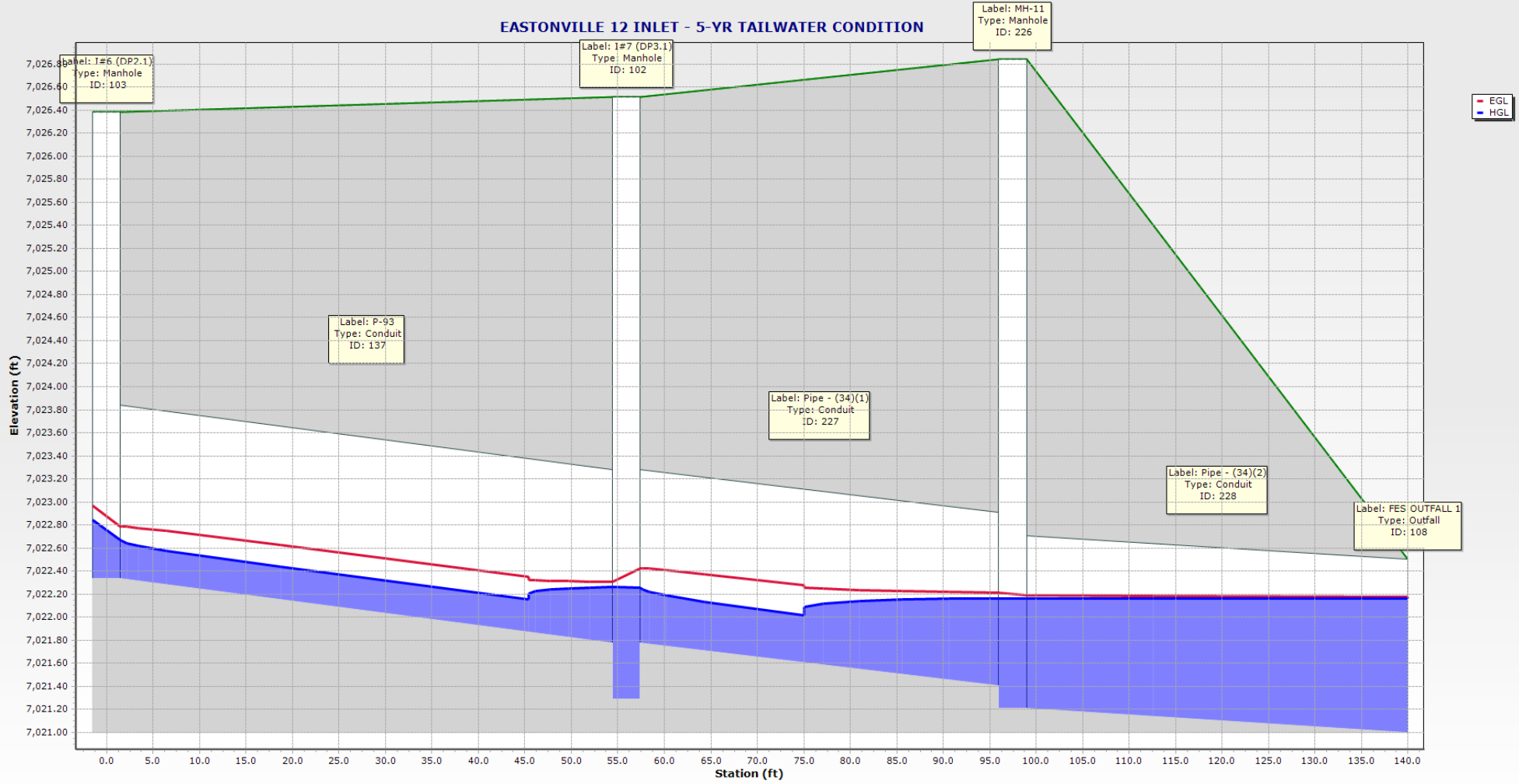


**NOTE: THIS SEGMENT HAS BEEN ANALYZED IN THE FREE  
OUTFALL CONDITION BLEW TO MEET CAPACITY & VELOCITY  
REQUIREMENTS**

### EASTONVILLE 11 - 5-YR TAILWATER CONDITION

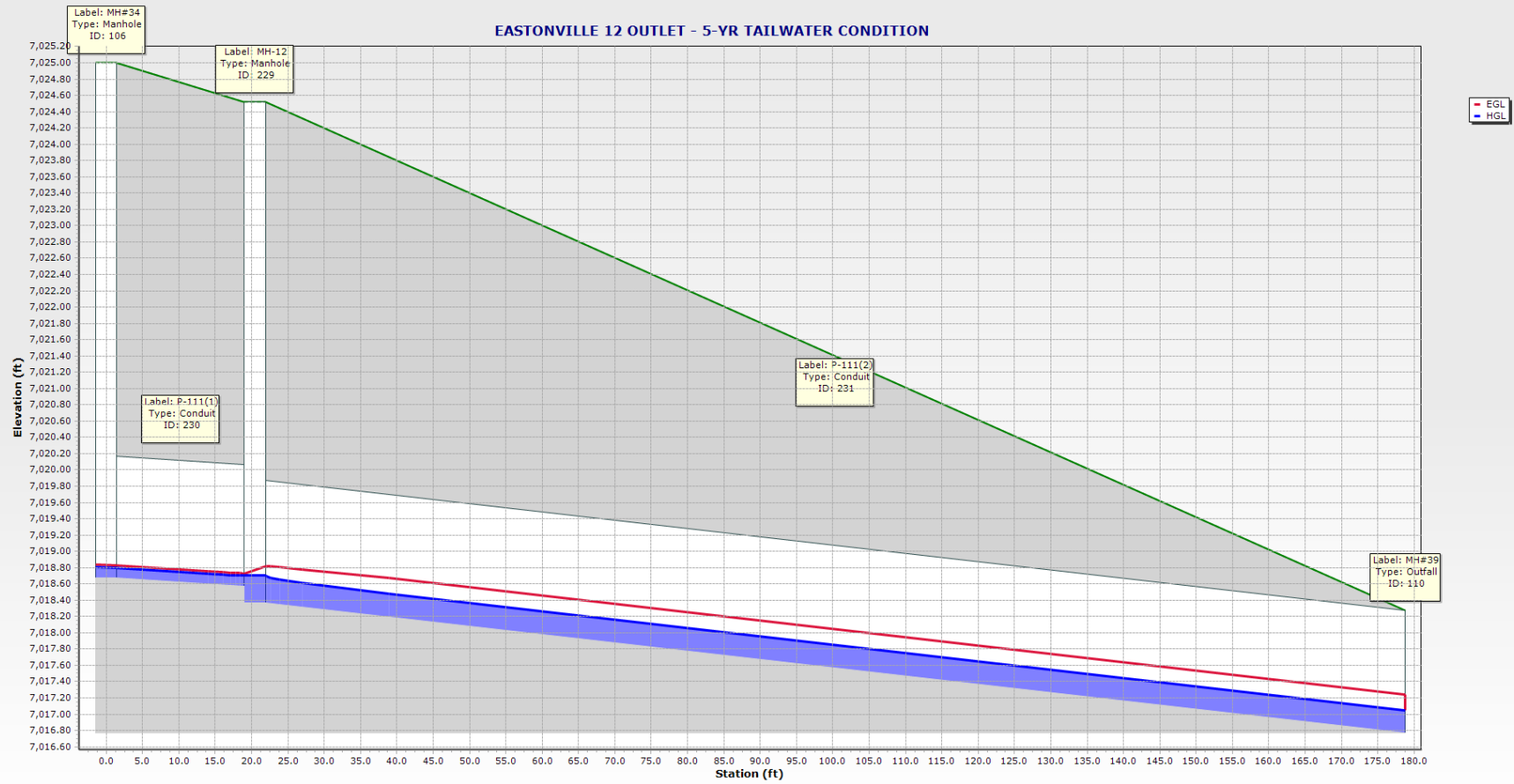


### EASTONVILLE 12 INLET - 5-YR TAILWATER CONDITION



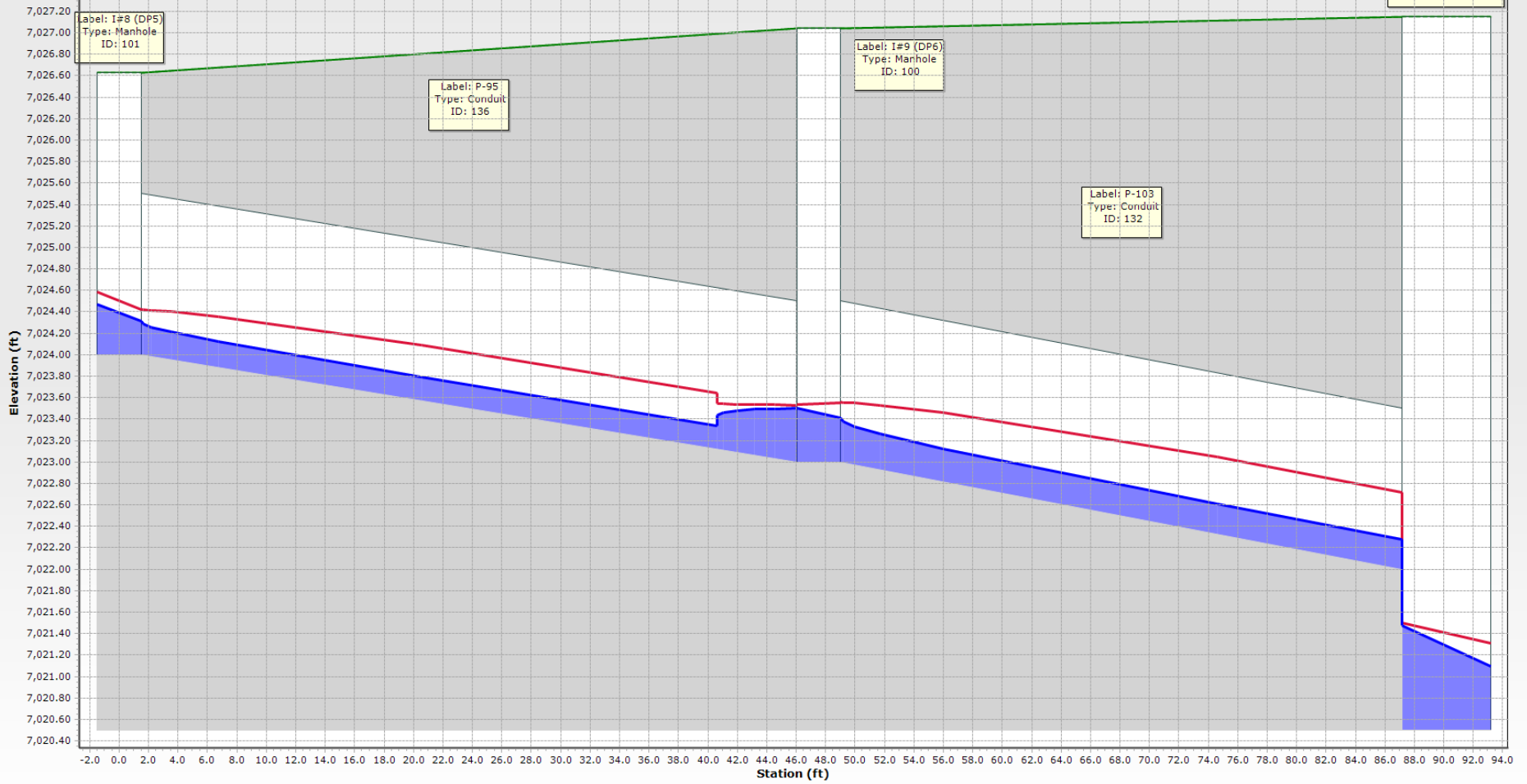
**NOTE: THIS SEGMENT HAS BEEN ANALYZED IN THE FREE  
OUTFALL CONDITION BLEW TO MEET CAPACITY & VELOCITY  
REQUIREMENTS**

### EASTONVILLE 12 OUTLET - 5-YR TAILWATER CONDITION

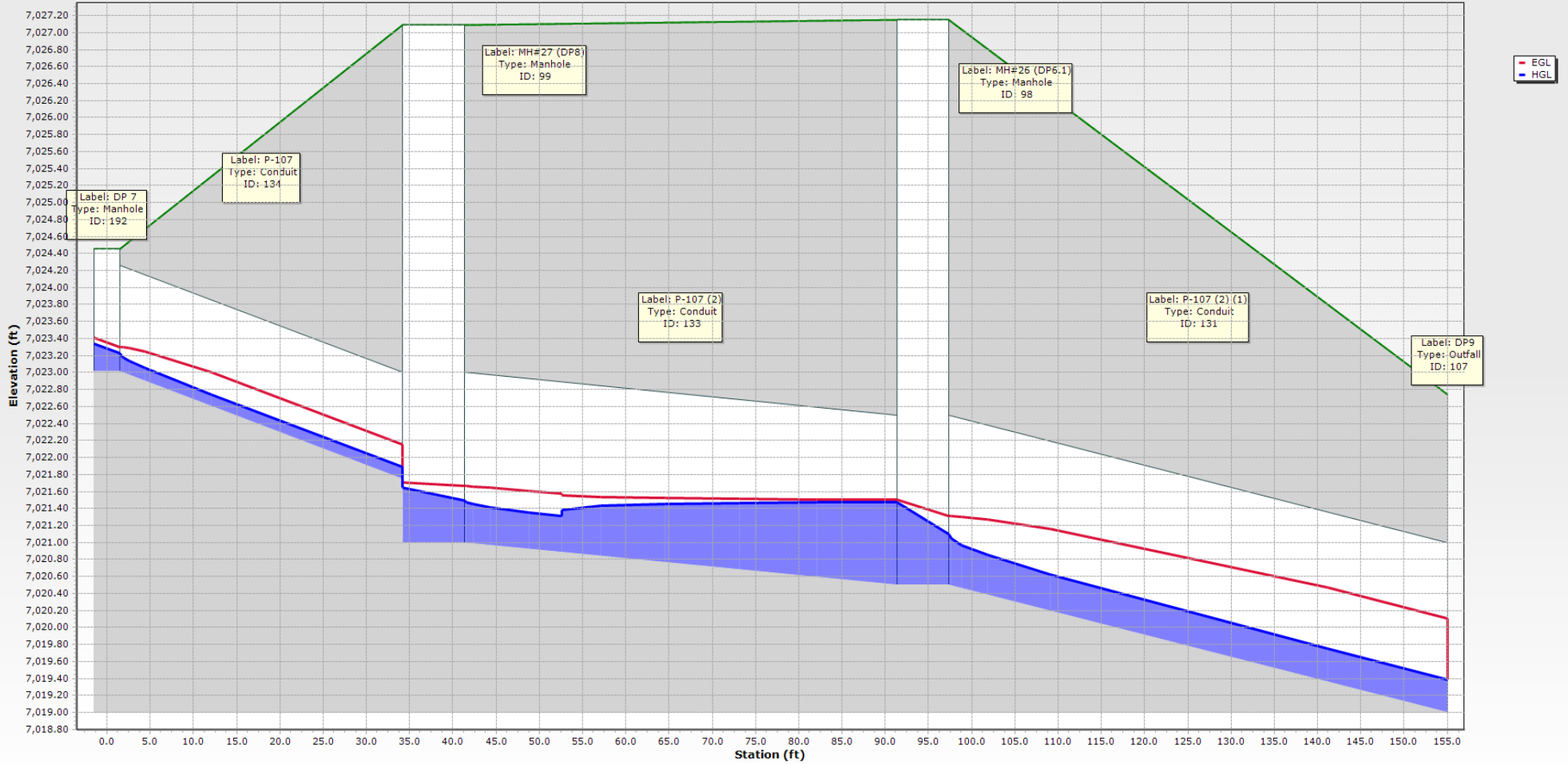




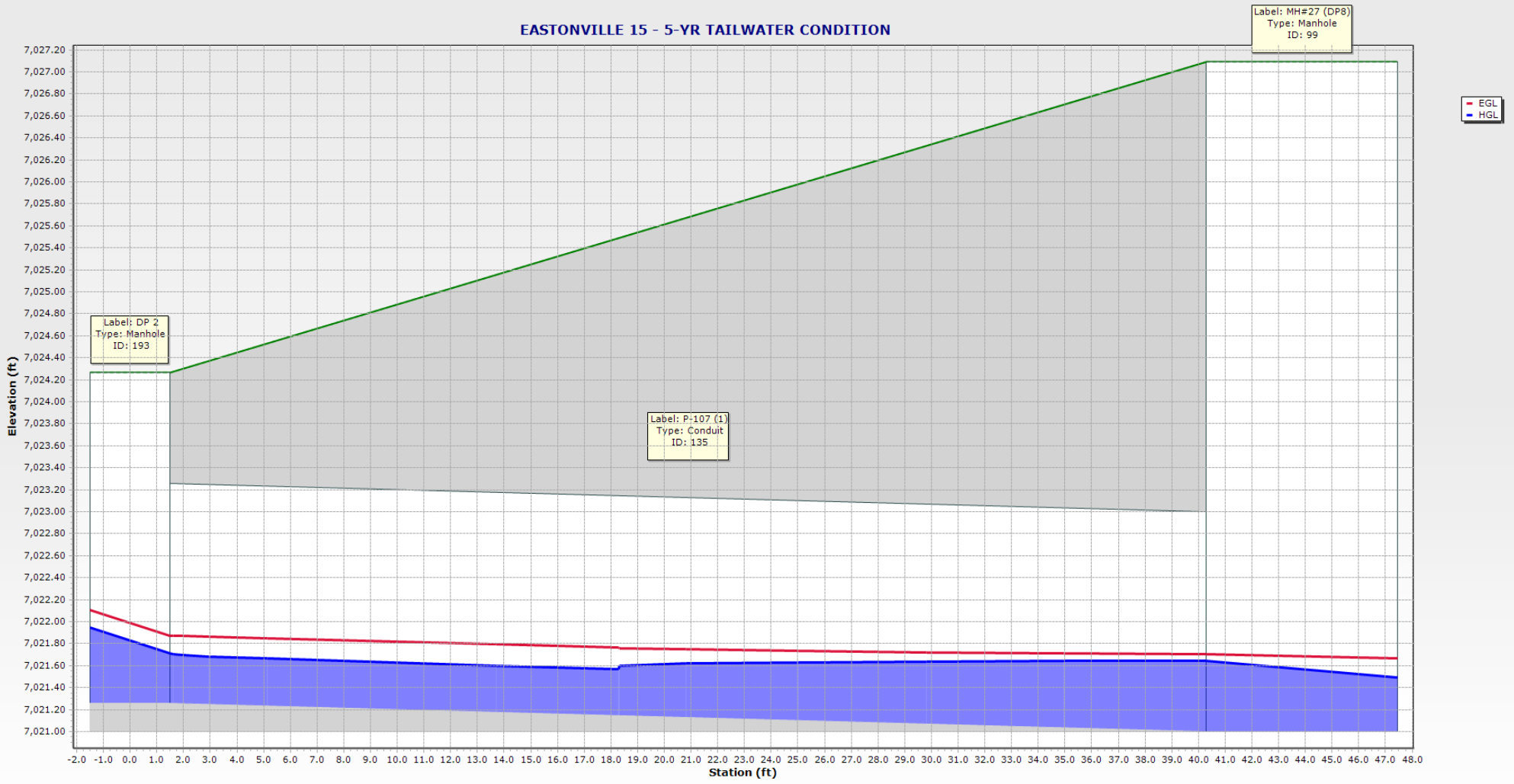
### EASTONVILLE 13 - 5-YR TAILWATER CONDITION



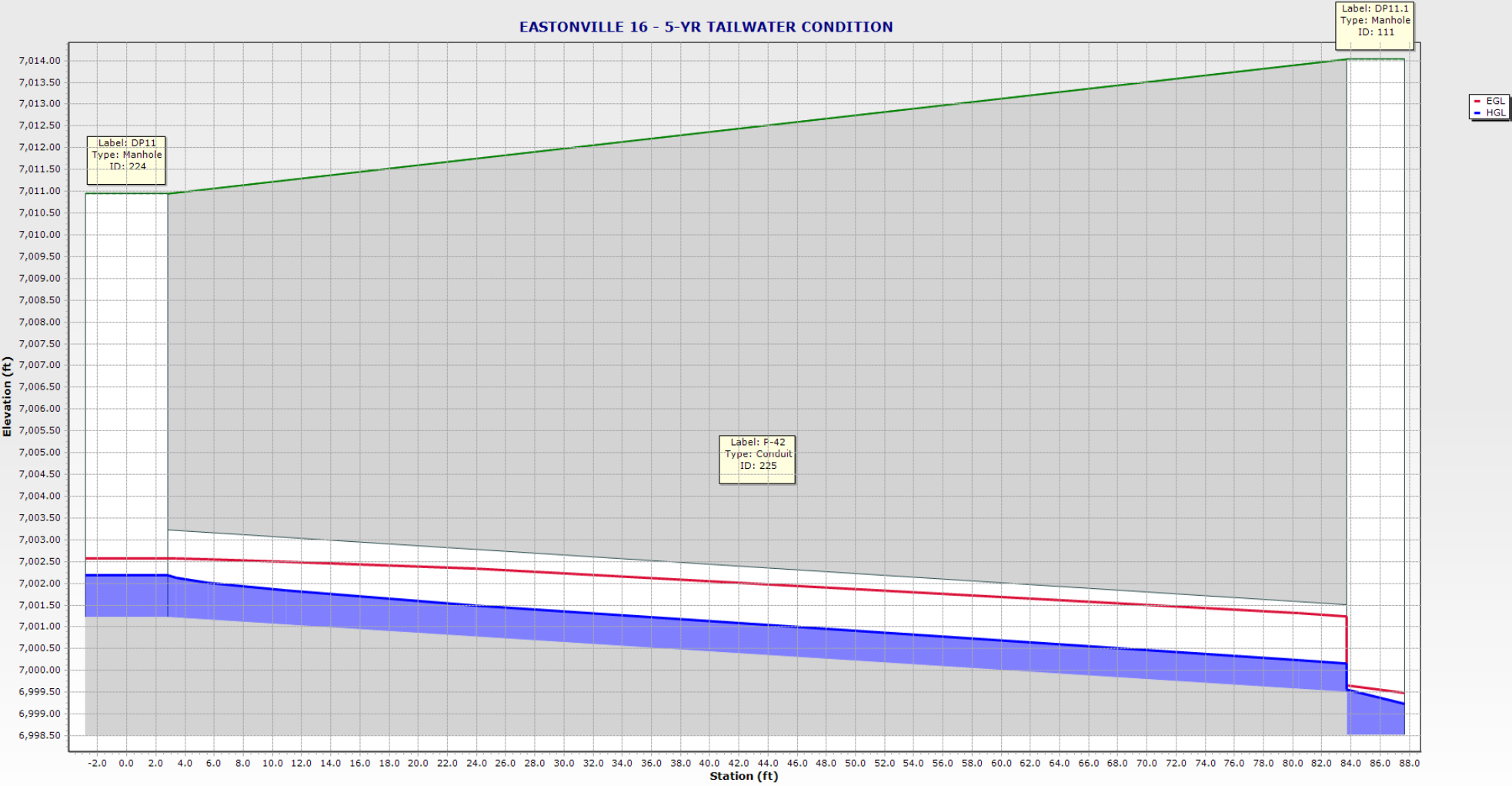
### EASTONVILLE 14 - 5-YR TAILWATER CONDITION



### EASTONVILLE 15 - 5-YR TAILWATER CONDITION



EASTONVILLE 16 - 5-YR TAILWATER CONDITION



# 100 YEAR FREE OUTFALL CONDITION: PIPE SUMMARY TABLE

	Start Node	Invert (Start) (ft)	Stop Node	Invert (Stop) (ft)	Length (User Defined) (ft)	Slope (Calculated) (ft/ft)	Diameter (in)	Manning's n	Flow (cfs)	Velocity (ft/s)	Capacity (Full Flow) (cfs)	Flow / Capacity (Design) (%)	Hydraulic Grade Line (In) (ft)	Hydraulic Grade Line (Out) (ft)
131: P-107 (2)	MH#26 (DP6.1)	7,020.50	DP9	7,019.00	60.7	0.025	24.0	0.013	22.40	11.97	35.57	63.0	7,022.19	7,020.22
132: P-103	I#9 (DP6)	7,023.00	MH#26 (DP6.1)	7,022.00	42.7	0.023	18.0	0.013	2.40	6.54	16.08	14.9	7,023.89	7,023.91
133: P-107 (2)	MH#27 (DP8)	7,021.00	MH#26 (DP6.1)	7,020.50	56.6	0.009	24.0	0.013	21.00	6.68	21.26	98.8	7,024.40	7,023.91
134: P-107	DP 7	7,023.01	MH#27 (DP8)	7,021.75	37.8	0.033	15.0	0.013	2.20	1.79	11.81	18.6	7,025.07	7,025.03
135: P-107 (1)	MH#27 (DP8)	7,021.00	DP 2	7,021.26	43.9	-0.006	24.0	0.013	18.80	5.98	17.41	108.0	7,025.33	7,025.03
136: P-95	I#8 (DP5)	7,024.00	I#9 (DP6)	7,023.00	47.5	0.021	18.0	0.013	1.30	5.26	15.24	8.5	7,024.43	7,023.94
137: P-93	I#6 (DP2.1)	7,022.34	I#7 (DP3.1)	7,021.78	55.9	0.010	18.0	0.013	1.50	4.22	10.51	14.3	7,022.80	7,022.47
140: P-44 (1)	MH#20	7,001.18	DP11.1	6,998.52	266.5	0.010	48.0	0.013	112.10	8.92	143.63	78.0	7,005.57	7,003.94
141: P-64	DP11.1	6,998.52	MH#22	6,995.26	316.5	0.010	48.0	0.013	112.10	12.80	145.88	76.8	7,001.72	6,997.89
142: P-44	MH#19	7,003.94	MH#20	7,001.28	266.5	0.010	48.0	0.013	112.10	12.64	143.63	78.0	7,007.14	7,005.63
143: P-26	DP 3	7,005.01	MH#19	7,004.04	81.5	0.012	48.0	0.013	112.10	8.92	156.73	71.5	7,009.86	7,009.36
144: P-64 (1)	MH#22	6,995.15	MH#23	6,988.82	316.6	0.020	48.0	0.013	112.10	16.57	203.15	55.2	6,998.35	6,995.32
145: P-87	MH#10 (DP 1...)	6,993.41	MH#9	6,989.86	350.8	0.010	24.0	0.013	17.20	7.96	22.76	75.6	6,994.91	6,991.16
146: P-87 (1)	MH#9	6,989.76	MH#8	6,986.86	193.5	0.015	24.0	0.013	17.20	9.29	27.70	62.1	6,991.26	6,988.76
147: P-84	I#4 (DP14)	6,994.25	MH#10 (DP 1...)	6,993.91	15.1	0.023	18.0	0.013	8.80	9.17	15.77	55.8	6,995.40	6,995.28
148: P-84 (1)	I#5 (DP 15)	6,994.74	MH#10 (DP 1...)	6,993.91	39.7	0.021	18.0	0.013	10.40	9.25	15.18	68.5	6,995.98	6,995.28
149: P-66	MH#23	6,988.82	MH#24	6,988.00	149.0	0.006	48.0	0.013	112.10	8.92	106.64	105.1	6,995.26	6,994.35
150: P-68	MH#24	6,988.00	MH#25 (DP13)	6,987.50	107.8	0.005	48.0	0.013	112.10	8.92	97.84	114.6	6,994.29	6,993.63
151: P-77	DP12	6,990.32	MH#25 (DP13)	6,989.50	28.1	0.029	24.0	0.013	24.60	7.83	38.62	63.7	6,993.96	6,993.63
152: P-74	MH#25 (DP13)	6,987.50	OUTLET SEG...	6,986.67	173.3	0.005	48.0	0.013	136.60	10.87	99.34	137.5	6,991.98	6,990.15
225: P-42	DP11	7,001.22	DP11.1	6,999.51	85.7	0.020	24.0	0.013	44.00	14.01	31.96	137.7	7,007.19	7,003.94
227: Pipe - (34	I#7 (DP3.1)	7,021.78	MH-11	7,021.41	41.5	0.009	18.0	0.013	3.20	5.00	9.92	32.3	7,022.46	7,022.00
228: Pipe - (34	MH-11	7,021.21	FES OUTFALL 1	7,021.00	42.5	0.005	18.0	0.013	3.20	4.03	7.38	43.3	7,021.90	7,021.68
230: P-111(1)	MH#34	7,018.67	MH-12	7,018.57	20.4	0.005	18.0	0.013	0.80	2.73	7.35	10.9	7,019.00	7,018.90
231: P-111(2)	MH-12	7,018.37	MH#39	7,016.77	158.3	0.010	18.0	0.013	0.80	3.52	10.56	7.6	7,018.70	7,017.05

**NOTE: SEE PROFILES BELOW FOR PIPES STUDIED WITH THIS ANALYSIS**

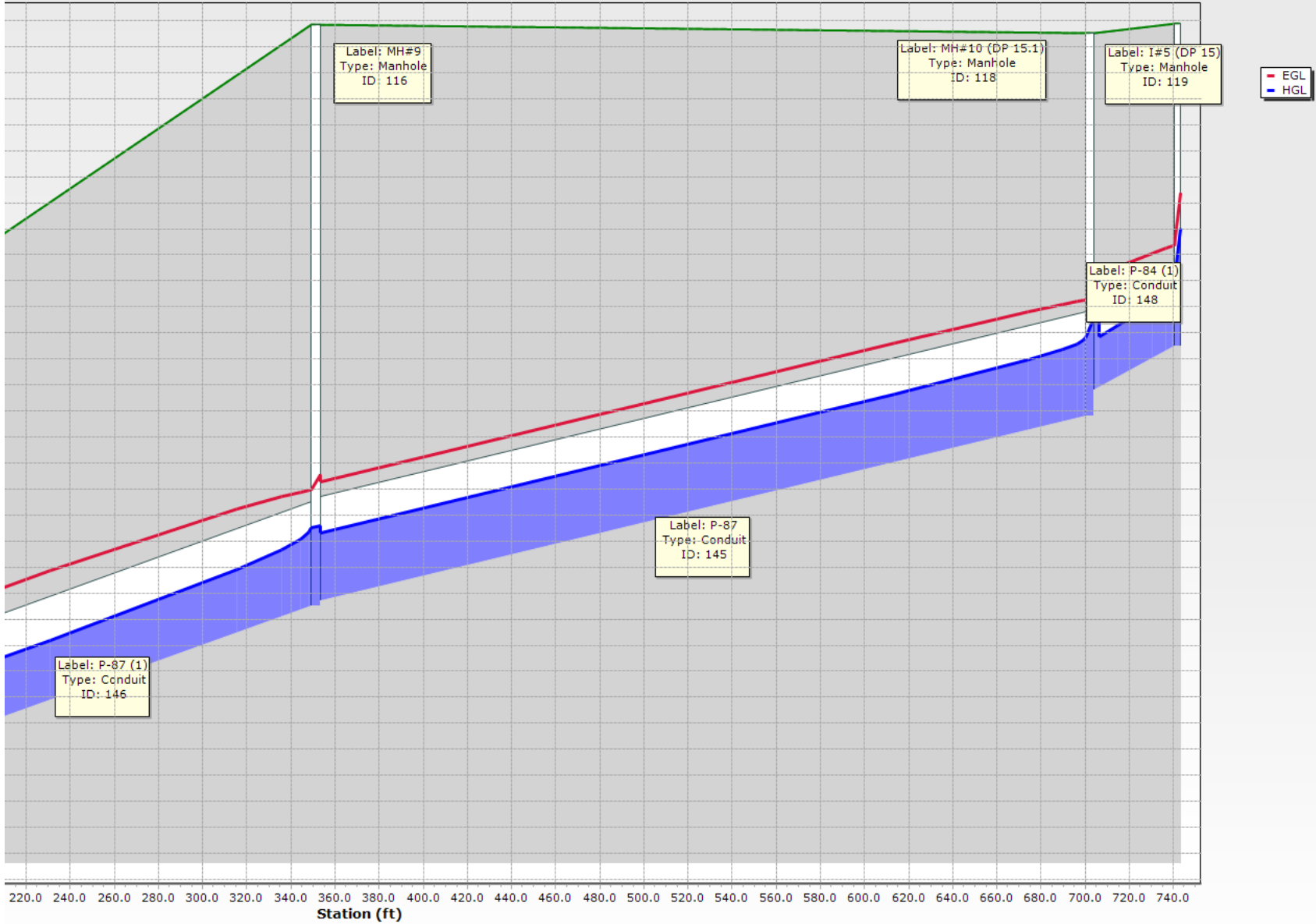
# 100 YEAR FREE OUTFALL CONDITION: STRUCTURE SUMMARY TABLE

	Elevation (Ground) (ft)	Elevation (Rim) (ft)	Elevation (Invert in 1) (ft)	Flow (Total Out) (cfs)	Hydraulic Grade Line (Out) (ft)	Headloss Method	Hydraulic Grade Line (In) (ft)	Notes
98: MH#26 (D	7,027.15	7,027.15	7,022.00	22.40	7,022.19	Standard	7,023.91	STORM MH
99: MH#27 (D	7,027.09	7,027.09	7,021.75	21.00	7,024.40	Standard	7,025.03	STORM MH
100: I#9 (DP6)	7,027.04	7,027.04	7,023.00	2.40	7,023.89	Standard	7,023.94	CDOT Type-R
101: I#8 (DP5)	7,026.63	7,026.63	(N/A)	1.30	7,024.43	Standard	7,024.66	CDOT Type-R
102: I#7 (DP3.	7,026.51	7,026.51	7,021.78	3.20	7,022.46	Standard	7,022.47	CDOT Type-R
103: I#6 (DP2.	7,026.38	7,026.38	(N/A)	1.50	7,022.80	Standard	7,023.05	CDOT Type-R
106: MH#34	7,025.00	7,025.00	(N/A)	0.80	7,019.00	Standard	7,019.06	CDOT Type-C
111: DP11.1	7,014.03	7,014.03	6,998.52	112.10	7,001.72	Standard	7,003.94	STORM MH
112: MH#20	7,012.41	7,012.41	7,001.28	112.10	7,005.57	Standard	7,005.63	STORM MH
113: MH#19	7,010.85	7,010.85	7,004.04	112.10	7,007.14	Standard	7,009.36	STORM MH
115: MH#22	7,005.85	7,005.85	6,995.26	112.10	6,998.35	Standard	6,998.44	STORM MH
116: MH#9	7,000.92	7,000.92	6,989.86	17.20	6,991.26	Standard	6,991.29	STORM MH
117: I#4 (DP1	7,000.75	7,000.75	(N/A)	8.80	6,995.40	Standard	6,996.25	CDOT Type-R
118: MH#10 (	7,000.75	7,000.75	6,993.91	17.20	6,994.91	Standard	6,995.28	STORM MH
119: I#5 (DP 1	7,000.94	7,000.94	(N/A)	10.40	6,995.98	Standard	6,997.01	CDOT Type-R
121: MH#23	6,997.20	6,997.20	6,988.82	112.10	6,995.26	Standard	6,995.32	STORM MH
122: MH#24	6,996.25	6,996.25	6,988.00	112.10	6,994.29	Standard	6,994.35	STORM MH
123: DP12	6,996.40	6,996.40	(N/A)	24.60	6,993.96	Standard	6,995.39	CDOT Type-C
124: MH#25 (	6,995.75	6,995.75	6,987.50	136.60	6,991.98	Standard	6,993.63	STORM MH
192: DP 7	7,024.45	7,024.45	(N/A)	2.20	7,024.45	Standard	7,024.52	CDOT FES
193: DP 2	7,024.26	7,024.26	(N/A)	18.80	7,024.26	Standard	7,025.10	CDOT FES
194: DP 3	7,009.43	7,009.43	(N/A)	112.10	7,009.43	Standard	7,011.29	CDOT FES
224: DP11	7,010.95	7,010.95	(N/A)	44.00	7,007.19	Absolute	7,007.19	CDOT TYPE D INLET
226: MH-11	7,026.84	7,026.84	7,021.41	3.20	7,021.90	Absolute	7,021.90	
229: MH-12	7,024.52	7,024.52	7,018.57	0.80	7,018.70	Absolute	7,018.70	

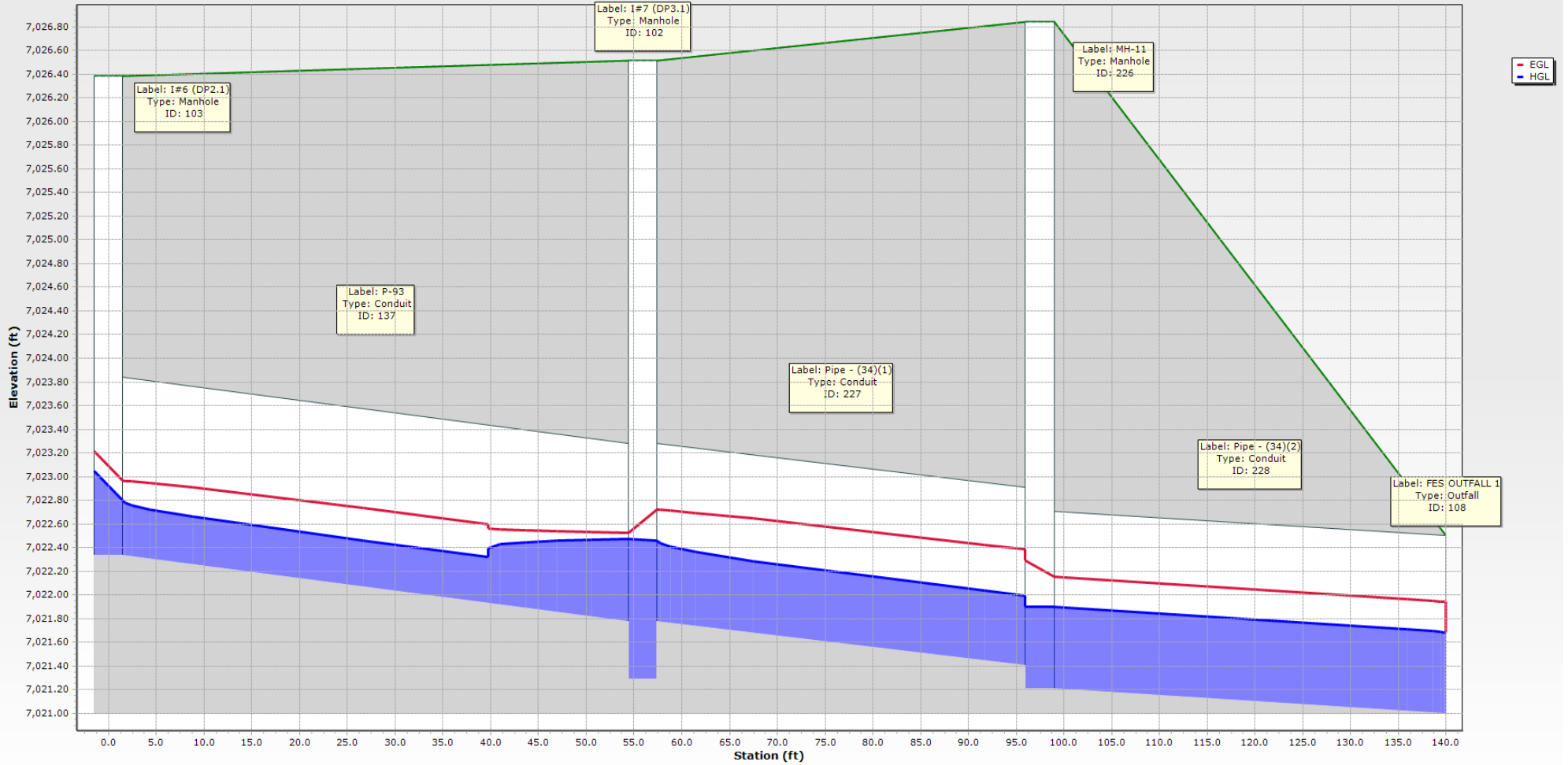
	Elevation (Ground) (ft)	Elevation (Invert) (ft)	Boundary Condition Type	Elevation (User Defined Tailwater) (ft)	Hydraulic Grade (ft)	Flow (Total Out) (cfs)	Notes
107: DP9	7,022.74	7,019.00	Free Outfall		7,020.22	22.40	CDOT FES
108: FES OUTF	7,022.50	7,021.00	Free Outfall		7,021.68	3.20	CDOT FES
110: MH#39	7,018.27	7,016.77	Free Outfall		7,017.05	0.80	CDOT FES
125: OUTLET S	6,991.09	6,986.67	Free Outfall		6,990.15	136.60	CDOT FES

**NOTE: SEE PROFILES BELOW FOR PIPES STUDIED WITH THIS ANALYSIS**

# EASTONVILLE 10 - 100-YR FREE OUTFALL CONDITION



### EASTONVILLE 12 INLET - 100-YR FREE OUTFALL CONDITION





## 5 YEAR FREE OUTFALL CONDITION: PIPE SUMMARY TABLE

	Start Node	Invert (Start) (ft)	Stop Node	Invert (Stop) (ft)	Length (User Defined) (ft)	Slope (Calculated) (ft/ft)	Diameter (in)	Manning's n	Flow (cfs)	Velocity (ft/s)	Capacity (Full Flow) (cfs)	Flow / Capacity (Design) (%)	Hydraulic Grade Line (In) (ft)	Hydraulic Grade Line (Out) (ft)
131: P-107 (2)	MH#26 (DP6.1)	7,020.50	DP9	7,019.00	60.7	0.025	24.0	0.013	2.90	6.82	35.57	8.2	7,021.09	7,019.39
132: P-103	I#9 (DP6)	7,023.00	MH#26 (DP6.1)	7,022.00	42.7	0.023	18.0	0.013	1.20	5.34	16.08	7.5	7,023.41	7,022.28
133: P-107 (2)	MH#27 (DP8)	7,021.00	MH#26 (DP6.1)	7,020.50	56.6	0.009	24.0	0.013	2.00	4.25	21.26	9.4	7,021.49	7,021.47
134: P-107	DP 7	7,023.01	MH#27 (DP8)	7,021.75	37.8	0.033	15.0	0.013	0.30	4.09	11.81	2.5	7,023.22	7,021.89
135: P-107 (1)	MH#27 (DP8)	7,021.00	DP 2	7,021.26	43.9	-0.006	24.0	0.013	1.70	3.52	17.41	9.8	7,021.71	7,021.65
136: P-95	I#8 (DP5)	7,024.00	I#9 (DP6)	7,023.00	47.5	0.021	18.0	0.013	0.70	4.38	15.24	4.6	7,024.31	7,023.50
137: P-93	I#6 (DP2.1)	7,022.34	I#7 (DP3.1)	7,021.78	55.9	0.010	18.0	0.013	0.80	3.51	10.51	7.6	7,022.67	7,022.26
140: P-44 (1)	MH#20	7,001.18	DP11.1	6,998.52	266.5	0.010	48.0	0.013	6.10	5.68	143.63	4.2	7,001.90	6,999.57
141: P-64	DP11.1	6,998.52	MH#22	6,995.26	316.5	0.010	48.0	0.013	6.10	5.74	145.88	4.2	6,999.24	6,995.82
142: P-44	MH#19	7,003.94	MH#20	7,001.28	266.5	0.010	48.0	0.013	6.10	5.68	143.63	4.2	7,004.66	7,001.84
143: P-26	DP 3	7,005.01	MH#19	7,004.04	81.5	0.012	48.0	0.013	6.10	6.03	156.73	3.9	7,005.73	7,004.99
144: P-64 (1)	MH#22	6,995.15	MH#23	6,988.82	316.6	0.020	48.0	0.013	6.10	7.23	203.15	3.0	6,995.87	6,989.55
145: P-87	MH#10 (DP 1...)	6,993.41	MH#9	6,989.86	350.8	0.010	24.0	0.013	10.20	7.04	22.76	44.8	6,994.55	6,990.80
146: P-87 (1)	MH#9	6,989.76	MH#8	6,986.86	193.5	0.015	24.0	0.013	10.20	8.15	27.70	36.8	6,990.90	6,988.20
147: P-84	I#4 (DP14)	6,994.25	MH#10 (DP 1...)	6,993.91	15.1	0.023	18.0	0.013	5.20	8.00	15.77	33.0	6,995.13	6,994.80
148: P-84 (1)	I#5 (DP 15)	6,994.74	MH#10 (DP 1...)	6,993.91	39.7	0.021	18.0	0.013	5.00	7.70	15.18	32.9	6,995.60	6,994.80
149: P-66	MH#23	6,988.82	MH#24	6,988.00	149.0	0.006	48.0	0.013	6.10	4.60	106.64	5.7	6,989.54	6,988.73
150: P-68	MH#24	6,988.00	MH#25 (DP13)	6,987.50	107.8	0.005	48.0	0.013	6.10	4.33	97.84	6.2	6,988.72	6,988.71
151: P-77	DP12	6,990.32	MH#25 (DP13)	6,989.50	28.1	0.029	24.0	0.013	3.90	7.89	38.62	10.1	6,991.01	6,989.95
152: P-74	MH#25 (DP13)	6,987.50	OUTLET SEG...	6,986.67	173.3	0.005	48.0	0.013	10.00	5.07	99.34	10.1	6,988.42	6,988.30
225: P-42	DP11	7,001.22	DP11.1	6,999.51	85.7	0.020	24.0	0.013	7.50	8.31	31.96	23.5	7,002.19	7,000.17
227: Pipe - (34)	I#7 (DP3.1)	7,021.78	MH-11	7,021.41	41.5	0.009	18.0	0.013	1.60	4.12	9.92	16.1	7,022.25	7,021.82
228: Pipe - (34)	MH-11	7,021.21	FES OUTFALL 1	7,021.00	42.5	0.005	18.0	0.013	1.60	3.34	7.38	21.7	7,021.69	7,021.47
230: P-111(1)	MH#34	7,018.67	MH-12	7,018.57	20.4	0.005	18.0	0.013	0.10	1.46	7.35	1.4	7,018.79	7,018.70
231: P-111(2)	MH-12	7,018.37	MH#39	7,016.77	158.3	0.010	18.0	0.013	0.80	3.52	10.56	7.6	7,018.70	7,017.05

**NOTE: SEE PROFILES BELOW FOR PIPES STUDIED WITH THIS ANALYSIS**

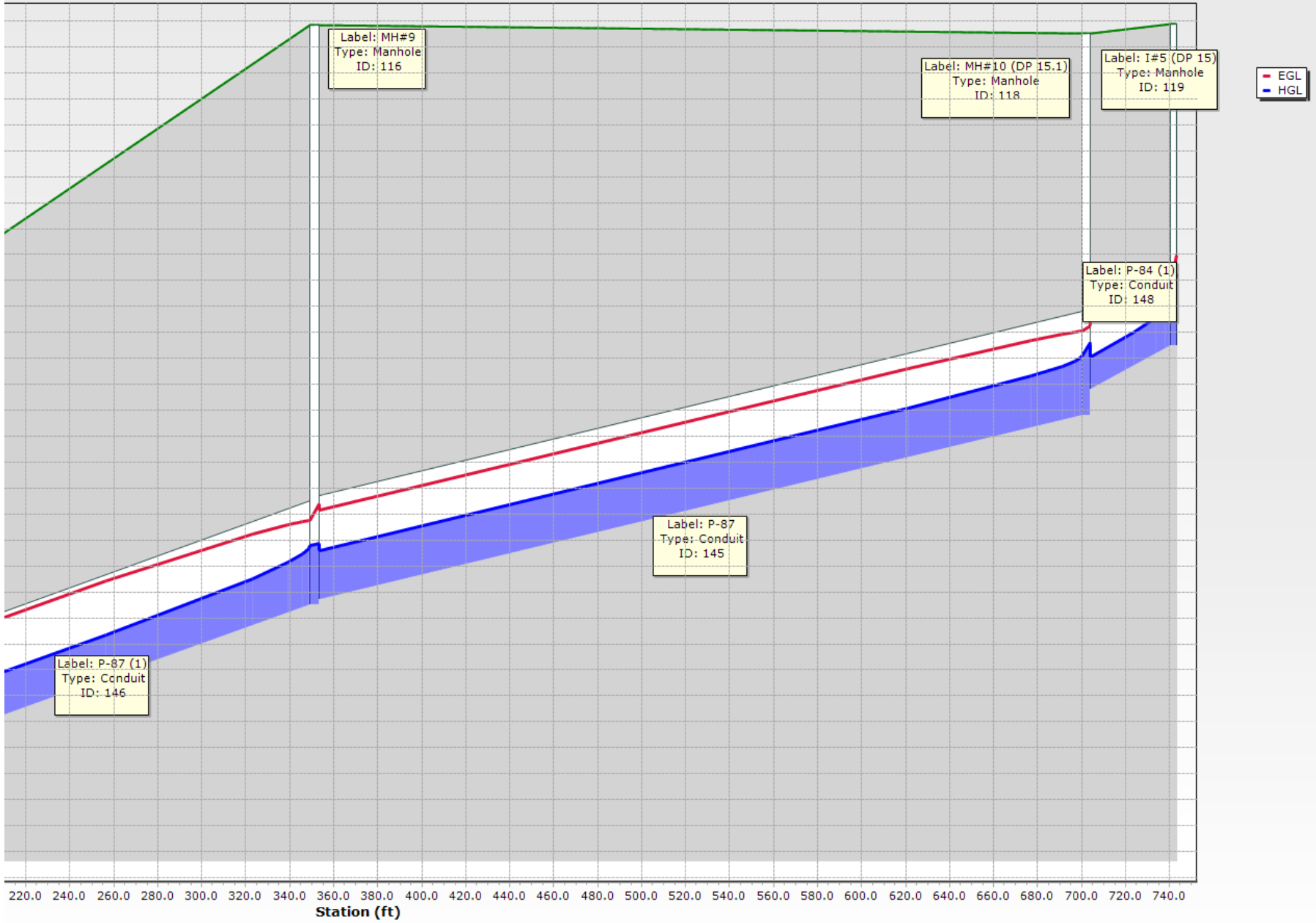
## 5 YEAR FREE OUTFALL CONDITION: STRUCTURE SUMMARY TABLE

	Elevation (Ground) (ft)	Elevation (Rim) (ft)	Elevation (Invert in 1) (ft)	Flow (Total Out) (cfs)	Hydraulic Grade Line (Out) (ft)	Headloss Method	Hydraulic Grade Line (In) (ft)	Notes
98: MH#26 (D	7,027.15	7,027.15	7,022.00	2.90	7,021.09	Standard	7,021.47	STORM MH
99: MH#27 (D	7,027.09	7,027.09	7,021.75	2.00	7,021.49	Standard	7,021.65	STORM MH
100: I#9 (DP6)	7,027.04	7,027.04	7,023.00	1.20	7,023.41	Standard	7,023.50	CDOT Type-R
101: I#8 (DP5)	7,026.63	7,026.63	(N/A)	0.70	7,024.31	Standard	7,024.47	CDOT Type-R
102: I#7 (DP3.	7,026.51	7,026.51	7,021.78	1.60	7,022.25	Standard	7,022.26	CDOT Type-R
103: I#6 (DP2.	7,026.38	7,026.38	(N/A)	0.80	7,022.67	Standard	7,022.85	CDOT Type-R
106: MH#34	7,025.00	7,025.00	(N/A)	0.10	7,018.79	Standard	7,018.81	CDOT Type-C
111: DP11.1	7,014.03	7,014.03	6,998.52	6.10	6,999.24	Standard	6,999.57	STORM MH
112: MH#20	7,012.41	7,012.41	7,001.28	6.10	7,001.90	Standard	7,001.91	STORM MH
113: MH#19	7,010.85	7,010.85	7,004.04	6.10	7,004.66	Standard	7,004.99	STORM MH
115: MH#22	7,005.85	7,005.85	6,995.26	6.10	6,995.87	Standard	6,995.88	STORM MH
116: MH#9	7,000.92	7,000.92	6,989.86	10.20	6,990.90	Standard	6,990.93	STORM MH
117: I#4 (DP1	7,000.75	7,000.75	(N/A)	5.20	6,995.13	Standard	6,995.67	CDOT Type-R
118: MH#10 (	7,000.75	7,000.75	6,993.91	10.20	6,994.55	Standard	6,994.80	STORM MH
119: I#5 (DP 1	7,000.94	7,000.94	(N/A)	5.00	6,995.60	Standard	6,996.13	CDOT Type-R
121: MH#23	6,997.20	6,997.20	6,988.82	6.10	6,989.54	Standard	6,989.55	STORM MH
122: MH#24	6,996.25	6,996.25	6,988.00	6.10	6,988.72	Standard	6,988.73	STORM MH
123: DP12	6,996.40	6,996.40	(N/A)	3.90	6,991.01	Standard	6,991.39	CDOT Type-C
124: MH#25 (	6,995.75	6,995.75	6,987.50	10.00	6,988.42	Standard	6,988.71	STORM MH
192: DP 7	7,024.45	7,024.45	(N/A)	0.30	7,023.22	Standard	7,023.33	CDOT FES
193: DP 2	7,024.26	7,024.26	(N/A)	1.70	7,021.71	Standard	7,021.95	CDOT FES
194: DP 3	7,009.43	7,009.43	(N/A)	6.10	7,005.73	Standard	7,006.10	CDOT FES
224: DP11	7,010.95	7,010.95	(N/A)	7.50	7,002.19	Absolute	7,002.19	CDOT TYPE D INLET
226: MH-11	7,026.84	7,026.84	7,021.41	1.60	7,021.69	Absolute	7,021.69	
229: MH-12	7,024.52	7,024.52	7,018.57	0.80	7,018.70	Absolute	7,018.70	

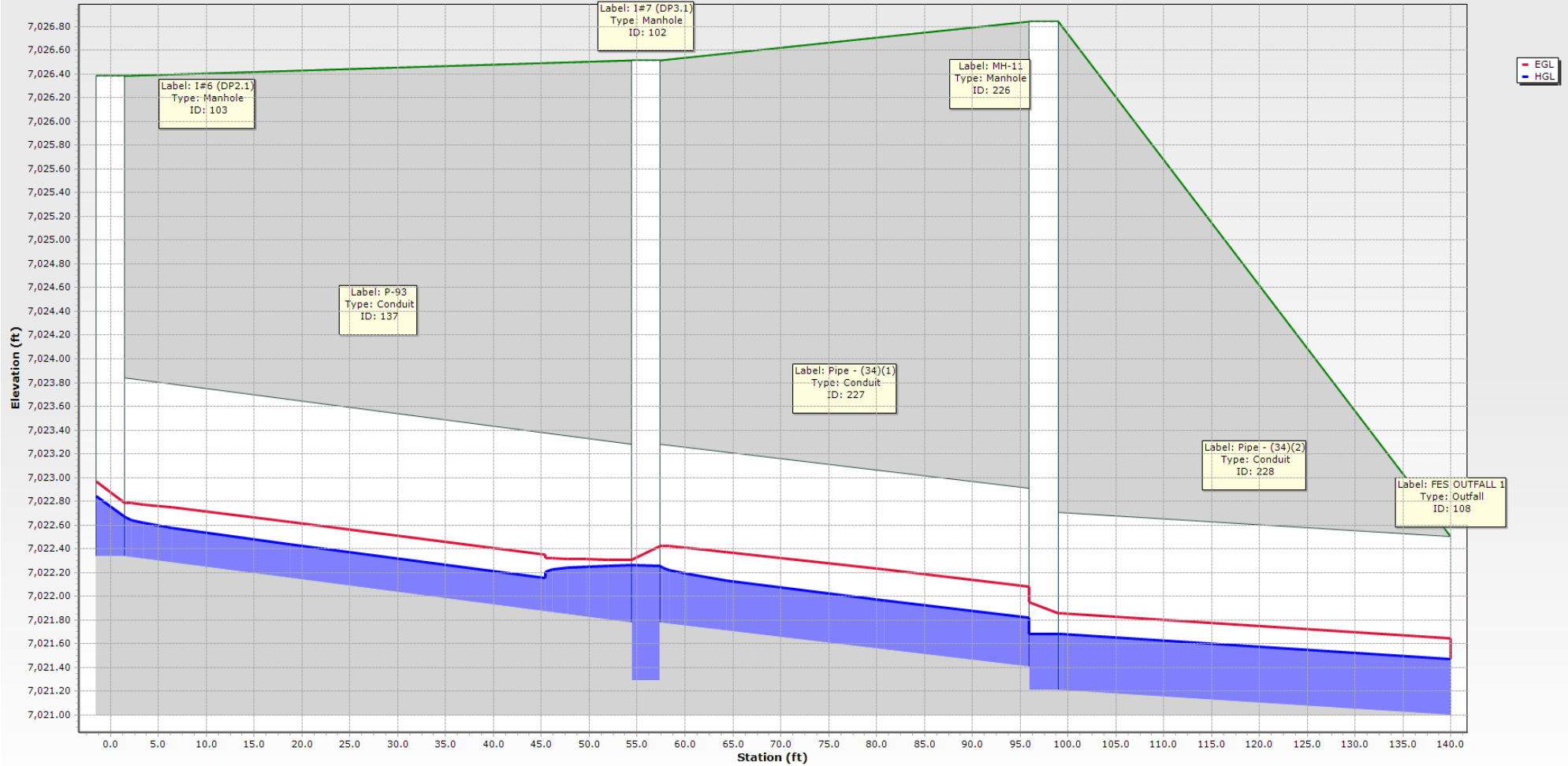
	Elevation (Ground) (ft)	Elevation (Invert) (ft)	Boundary Condition Type	Elevation (User Defined Tailwater) (ft)	Hydraulic Grade (ft)	Flow (Total Out) (cfs)	Notes
107: DP9	7,022.74	7,019.00	Free Outfall		7,019.39	2.90	CDOT FES
108: FES OUTF	7,022.50	7,021.00	Free Outfall		7,021.47	1.60	CDOT FES
110: MH#39	7,018.27	7,016.77	Free Outfall		7,017.05	0.80	CDOT FES
125: OUTLET S	6,991.09	6,986.67	User Defined Tailwater	6,988.30	6,988.30	10.00	CDOT FES

**NOTE: SEE PROFILES BELOW FOR PIPES STUDIED WITH THIS ANALYSIS**

# EASTONVILLE 10 - 5-YR FREE OUTFALL CONDITION



### EASTONVILLE 12 INLET - 5-YR FREE OUTFALL CONDITION



# Channel Report

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Wednesday, Aug 28 2024

## DP3 SWALE

### Trapezoidal

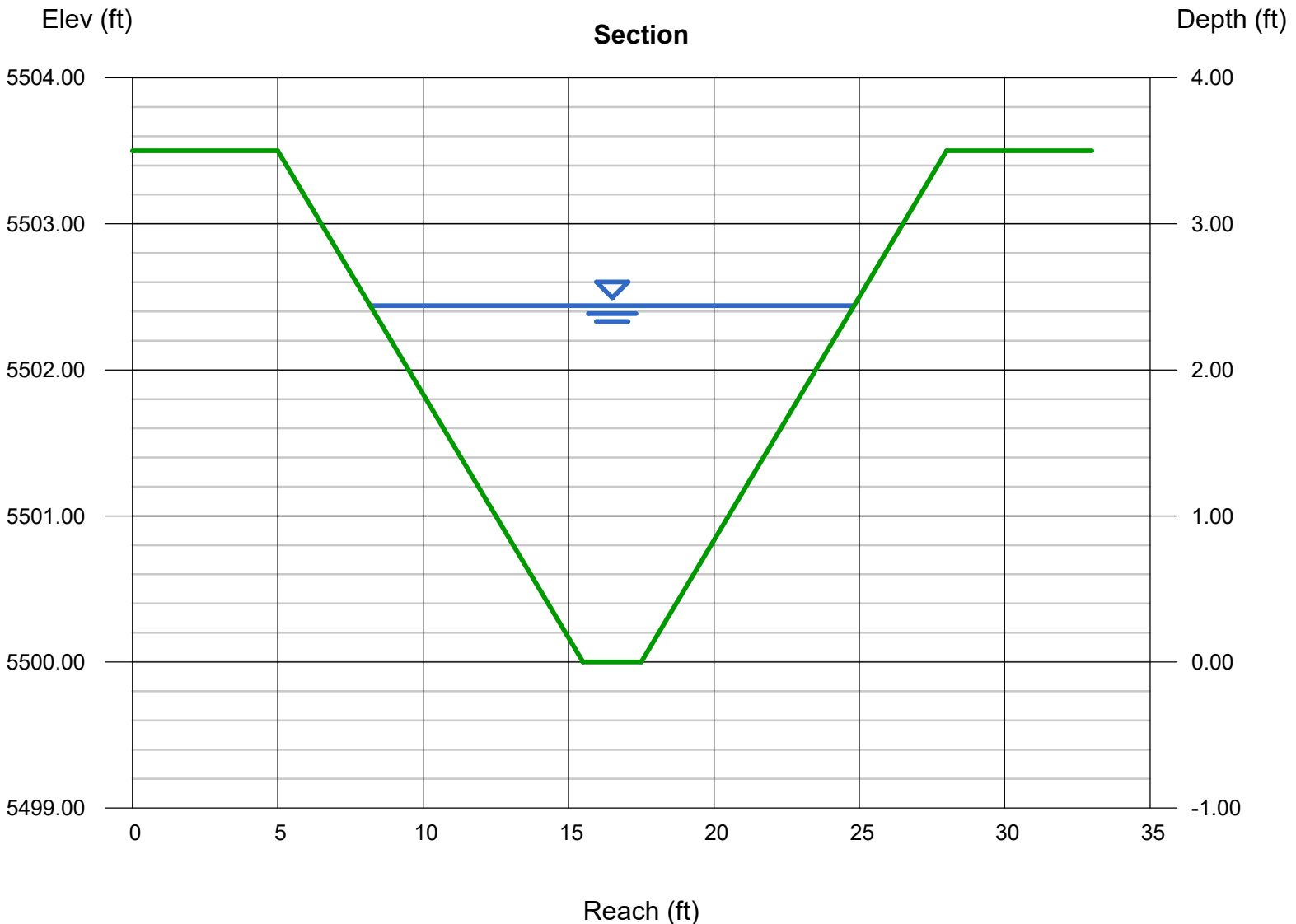
Bottom Width (ft) = 2.00  
Side Slopes (z:1) = 3.00, 3.00  
Total Depth (ft) = 3.50  
Invert Elev (ft) = 5500.00  
Slope (%) = 0.70  
N-Value = 0.030

### Highlighted

Depth (ft) = 2.44  
Q (cfs) = 112.00  
Area (sqft) = 22.74  
Velocity (ft/s) = 4.93  
Wetted Perim (ft) = 17.43  
Crit Depth, Yc (ft) = 2.14  
Top Width (ft) = 16.64  
EGL (ft) = 2.82

### Calculations

Compute by: Known Q  
Known Q (cfs) = 112.00



# Channel Report

## DP4 SWALE

### Trapezoidal

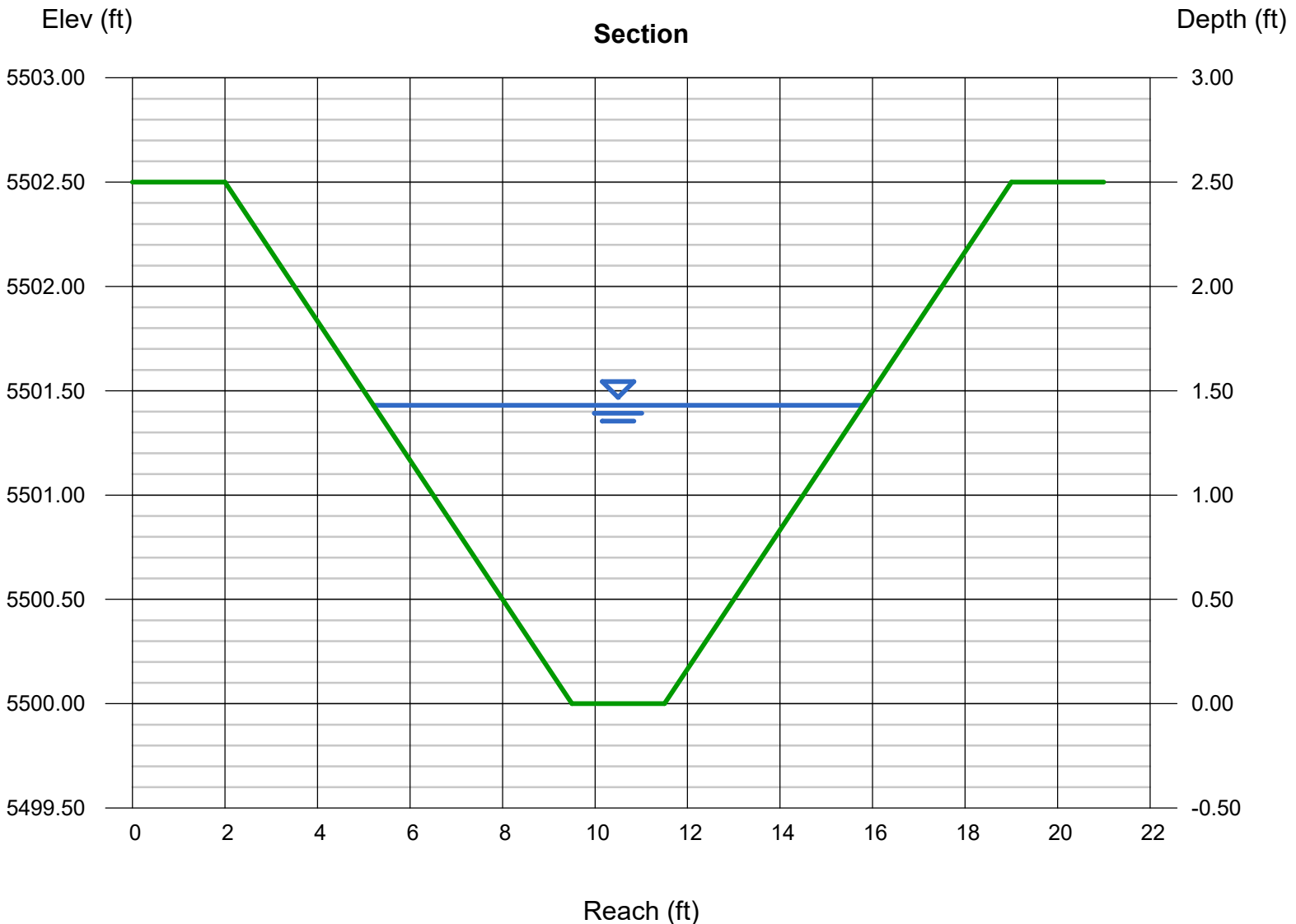
Bottom Width (ft) = 2.00  
Side Slopes (z:1) = 3.00, 3.00  
Total Depth (ft) = 2.50  
Invert Elev (ft) = 5500.00  
Slope (%) = 1.00  
N-Value = 0.030

### Highlighted

Depth (ft) = 1.43  
Q (cfs) = 38.60  
Area (sqft) = 8.99  
Velocity (ft/s) = 4.29  
Wetted Perim (ft) = 11.04  
Crit Depth, Yc (ft) = 1.31  
Top Width (ft) = 10.58  
EGL (ft) = 1.72

### Calculations

Compute by: Known Q  
Known Q (cfs) = 38.60





# Channel Report

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Wednesday, Aug 28 2024

## DP9 SWALE

### Trapezoidal

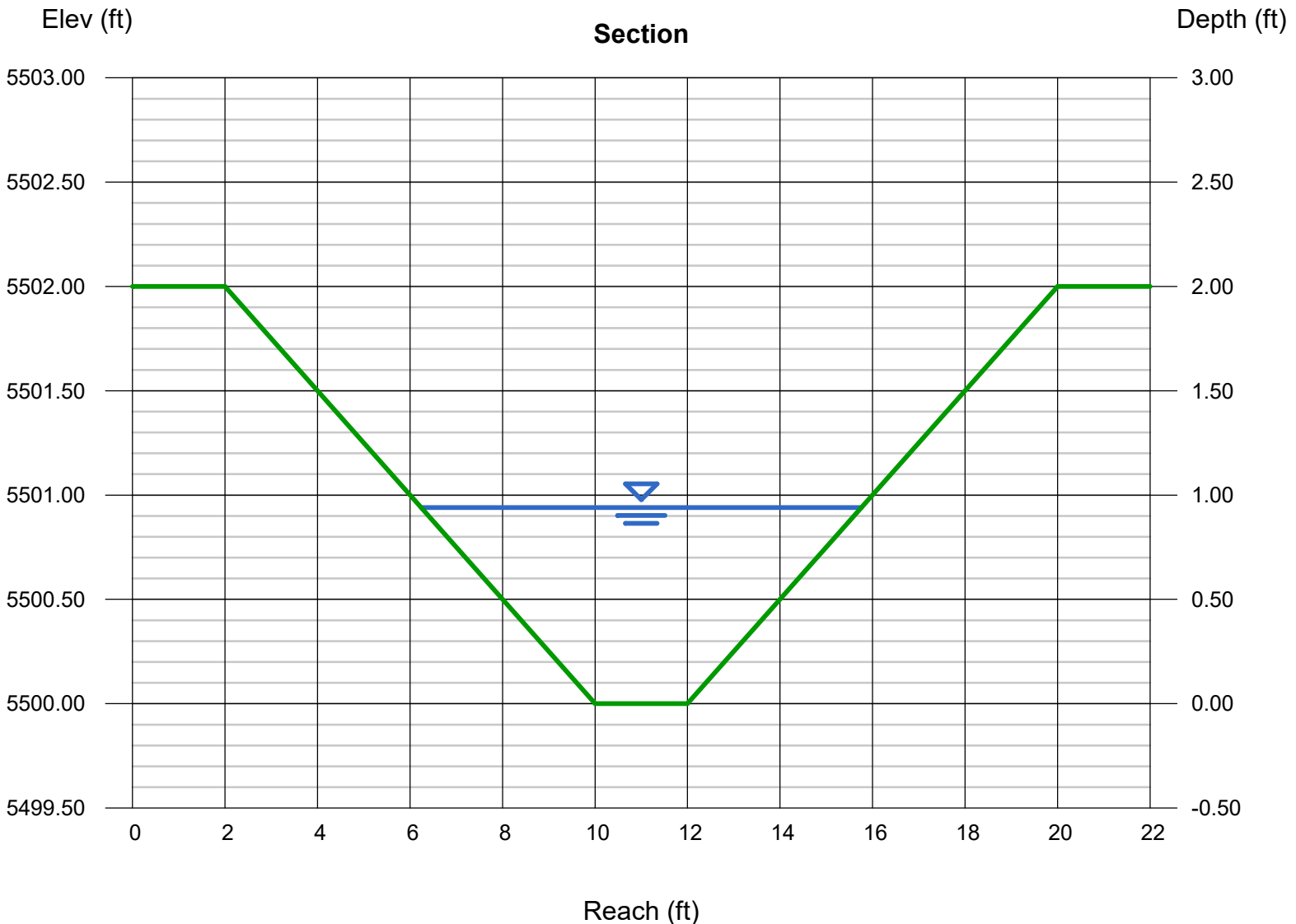
Bottom Width (ft) = 2.00  
Side Slopes (z:1) = 4.00, 4.00  
Total Depth (ft) = 2.00  
Invert Elev (ft) = 5500.00  
Slope (%) = 1.60  
N-Value = 0.030

### Highlighted

Depth (ft) = 0.94  
Q (cfs) = 22.40  
Area (sqft) = 5.41  
Velocity (ft/s) = 4.14  
Wetted Perim (ft) = 9.75  
Crit Depth, Yc (ft) = 0.93  
Top Width (ft) = 9.52  
EGL (ft) = 1.21

### Calculations

Compute by: Known Q  
Known Q (cfs) = 22.40



# Channel Report

## DP11 SWALE

### Trapezoidal

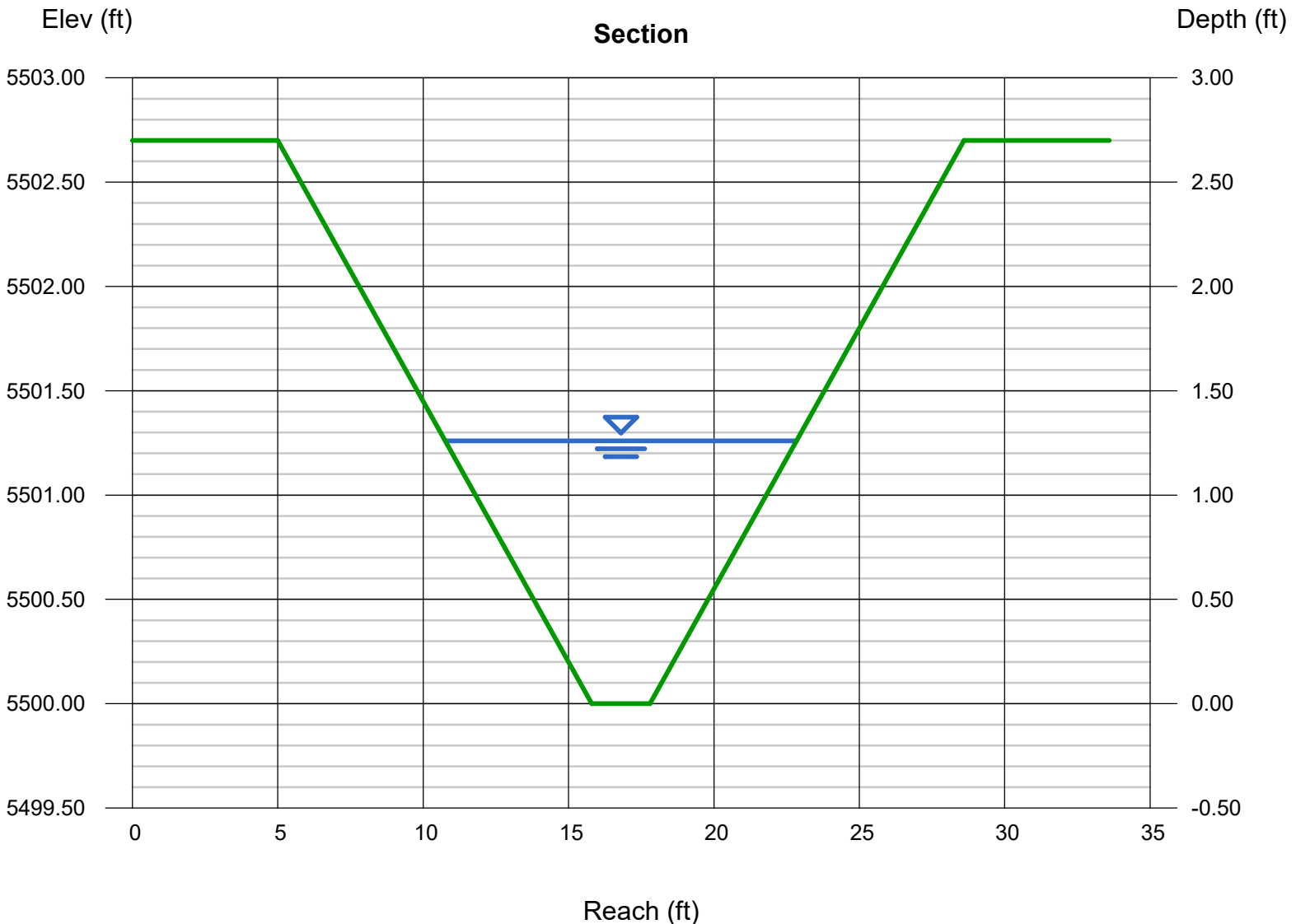
Bottom Width (ft) = 2.00  
Side Slopes (z:1) = 4.00, 4.00  
Total Depth (ft) = 2.70  
Invert Elev (ft) = 5500.00  
Slope (%) = 1.60  
N-Value = 0.030

### Highlighted

Depth (ft) = 1.26  
Q (cfs) = 44.00  
Area (sqft) = 8.87  
Velocity (ft/s) = 4.96  
Wetted Perim (ft) = 12.39  
Crit Depth, Yc (ft) = 1.28  
Top Width (ft) = 12.08  
EGL (ft) = 1.64

### Calculations

Compute by: Known Q  
Known Q (cfs) = 44.00





<b>EASTONVILLE RD SEG 2</b>	<b>Calc'd by:</b>	<b>SPC</b>
<b>201662.08</b>	<b>Checked by:</b>	<b>CM</b>
<b>DP4.1 (SFB C INLET)</b>	<b>Date:</b>	<b>8/28/2024</b>

Input Parameters	
Flow (Q)	3.4 cfs
Tailwater depth (Y <sub>t</sub> )	0.60 ft
Conduit Diameter (D <sub>c</sub> )	18 in
Expansion Factor (per Fig. 9-35)	6.5
Soil Type	Non-Cohesive Soils

Calculated Parameters	
Froude Parameter (Q/D <sup>2.5</sup> )	1.23
D <sub>50</sub> =	1.53 in
UDFCD Riprap Type =	Type VL
Design D <sub>50</sub> =	6 in
Minimum Mantle Thickness =	12 in
Minimum Length of Apron =	4.50 ft

Calculated D<sub>50</sub> for riprap was calculated using Equation 9-16 in the USDCM Vol 2.

$$d_{50} = \frac{0.023Q}{Y_t^{1.2} D_c^{0.3}}$$

Calculated minimum length of apron was calculated using Equations 9-11 and 9-12 in the USDCM Vol. 2

$$L_p = \left( \frac{1}{2 \tan \theta} \right) \left( \frac{A_t}{Y_t} - W \right) \quad \text{Equation 9-11} \quad A_t = \frac{Q}{V} \quad \text{Equation 9-12}$$

- Where:
- L<sub>p</sub> = length of protection (ft)
  - W = width of the conduit (ft, use diameter for circular conduits)
  - Y<sub>t</sub> = tailwater depth (ft)
  - θ = the expansion angle of the culvert flow
  - Q = design discharge (cfs)
  - V = the allowable non-eroding velocity in the downstream channel (ft/sec)
  - A<sub>t</sub> = required area of flow at allowable velocity (ft<sup>2</sup>)

- Note:
- <sup>1</sup> Calculations follow criteria in the USDCM Vol.2 Chapter 9
  - <sup>2</sup> Calculations assume a circular culvert
  - <sup>3</sup> This spreadsheet assumes y<sub>t</sub>/D<sub>c</sub>=0.4 in cases where y<sub>t</sub> is unknown or a hydraulic jump is suspected downstream of the outlet.
  - <sup>4</sup> Per the USDCM Vol.2 in no case should L<sub>p</sub> be less than 3D, nor does L<sub>p</sub> need to be greater than 10D whenever the Froude parameter is less than 6.0. whenever the Froude parameter is greater than 6, increase the maximum L<sub>p</sub> required by 1/4 D<sub>c</sub> for each whole number by which the Froude parameter is greater than 6



<b>EASTONVILLE RD SEG 2</b>	<b>Calc'd by:</b>	<b>SPC</b>
<b>201662.08</b>	<b>Checked by:</b>	<b>CM</b>
<b>DP9 (24" RCP CULVERT OUTLET)</b>	<b>Date:</b>	<b>8/28/2024</b>

Input Parameters	
Flow (Q)	22.4 cfs
Tailwater depth (Y <sub>t</sub> )	0.80 ft
Conduit Diameter (D <sub>c</sub> )	24 in
Expansion Factor (per Fig. 9-35)	3.5
Soil Type	Non-Cohesive Soils

Calculated Parameters	
Froude Parameter (Q/D <sup>2.5</sup> )	3.96
D <sub>50</sub> =	6.56 in
UDFCD Riprap Type =	Type L
Design D <sub>50</sub> =	9 in
Minimum Mantle Thickness =	18 in
Minimum Length of Apron =	12.60 ft

Calculated D<sub>50</sub> for riprap was calculated using Equation 9-16 in the USDCM Vol 2.

$$d_{50} = \frac{0.023Q}{Y_t^{1.2} D_c^{0.3}}$$

Calculated minimum length of apron was calculated using Equations 9-11 and 9-12 in the USDCM Vol. 2

$$L_p = \left( \frac{1}{2 \tan \theta} \right) \left( \frac{A_t}{Y_t} - W \right)$$

Equation 9-11

$$A_t = \frac{Q}{V}$$

Equation 9-12

Where:

- L<sub>p</sub> = length of protection (ft)
- W = width of the conduit (ft, use diameter for circular conduits)
- Y<sub>t</sub> = tailwater depth (ft)
- θ = the expansion angle of the culvert flow

Where:

- Q = design discharge (cfs)
- V = the allowable non-eroding velocity in the downstream channel (ft/sec)
- A<sub>t</sub> = required area of flow at allowable velocity (ft<sup>2</sup>)

Note:

- <sup>1</sup> Calculations follow criteria in the USDCM Vol.2 Chapter 9
- <sup>2</sup> Calculations assume a circular culvert
- <sup>3</sup> This spreadsheet assumes y<sub>t</sub>/D<sub>c</sub>=0.4 in cases where y<sub>t</sub> is unknown or a hydraulic jump is suspected downstream of the outlet.
- <sup>4</sup> Per the USDCM Vol.2 in no case should L<sub>p</sub> be less than 3D, nor does L<sub>p</sub> need to be greater than 10D whenever the Froude parameter is less than 6.0. whenever the Froude parameter is greater than 6, increase the maximum L<sub>p</sub> required by 1/4 D<sub>c</sub> for each whole number by which the Froude parameter is greater than 6



<b>EASTONVILLE RD SEG 2</b>	<b>Calc'd by:</b>	<b>SPC</b>
<b>201662.08</b>	<b>Checked by:</b>	<b>CM</b>
<b>DP10 (SFB C OUTLET)</b>	<b>Date:</b>	<b>8/28/2024</b>

Input Parameters	
Flow (Q)	2.3 cfs
Tailwater depth (Y <sub>t</sub> )	0.60 ft
Conduit Diameter (D <sub>c</sub> )	18 in
Expansion Factor (per Fig. 9-35)	6.5
Soil Type	Non-Cohesive Soils

Calculated Parameters	
Froude Parameter (Q/D <sup>2.5</sup> )	0.83
D <sub>50</sub> =	1.04 in
UDFCD Riprap Type =	Type VL
Design D <sub>50</sub> =	6 in
Minimum Mantle Thickness =	12 in
Minimum Length of Apron =	4.50 ft

Calculated D<sub>50</sub> for riprap was calculated using Equation 9-16 in the USDCM Vol 2.

$$d_{50} = \frac{0.023Q}{Y_t^{1.2} D_c^{0.3}}$$

Calculated minimum length of apron was calculated using Equations 9-11 and 9-12 in the USDCM Vol. 2

$$L_p = \left( \frac{1}{2 \tan \theta} \right) \left( \frac{A_r}{Y_t} - W \right) \quad \text{Equation 9-11} \quad A_r = \frac{Q}{V} \quad \text{Equation 9-12}$$

- Where:
- L<sub>p</sub> = length of protection (ft)
  - W = width of the conduit (ft, use diameter for circular conduits)
  - Y<sub>t</sub> = tailwater depth (ft)
  - θ = the expansion angle of the culvert flow
  - Q = design discharge (cfs)
  - V = the allowable non-eroding velocity in the downstream channel (ft/sec)
  - A<sub>r</sub> = required area of flow at allowable velocity (ft<sup>2</sup>)

- Note:
- <sup>1</sup> Calculations follow criteria in the USDCM Vol.2 Chapter 9
  - <sup>2</sup> Calculations assume a circular culvert
  - <sup>3</sup> This spreadsheet assumes y<sub>t</sub>/D<sub>c</sub>=0.4 in cases where y<sub>t</sub> is unknown or a hydraulic jump is suspected downstream of the outlet.
  - <sup>4</sup> Per the USDCM Vol.2 in no case should L<sub>p</sub> be less than 3D, nor does L<sub>p</sub> need to be greater than 10D whenever the Froude parameter is less than 6.0. whenever the Froude parameter is greater than 6, increase the maximum L<sub>p</sub> required by 1/4 D<sub>c</sub> for each whole number by which the Froude parameter is greater than 6



**EASTONVILLE RD SEG 1**

**Calc'd by:**

**SPC**

**201662.08**

**Checked by:**

**CM**

**DP13.1**

**Date:**

**8/28/2024**

Input Parameters	
Flow (Q)	183.1 cfs
Tailwater depth (Y <sub>t</sub> )	1.60 ft
Conduit Diameter (D <sub>c</sub> )	48 in
Expansion Factor (per Fig. 9-35)	2
Soil Type	Non-Cohesive Soils

Calculated Parameters	
Froude Parameter (Q/D <sup>2.5</sup> )	5.72
D <sub>50</sub> =	18.97 in
UDFCD Riprap Type =	Type VH
Design D <sub>50</sub> =	24 in
Minimum Mantle Thickness =	48 in
Minimum Length of Apron =	37.78 ft

Calculated D<sub>50</sub> for riprap was calculated using Equation 9-16 in the USDCM Vol 2.

$$d_{50} = \frac{0.023Q}{Y_t^{1.2} D_c^{0.3}}$$

Calculated minimum length of apron was calculated using Equations 9-11 and 9-12 in the USDCM Vol. 2

$$L_p = \left( \frac{1}{2 \tan \theta} \right) \left( \frac{A_t}{Y_t} - W \right)$$

Equation 9-11

$$A_t = \frac{Q}{V}$$

Equation 9-12

Where:

L<sub>p</sub> = length of protection (ft)

W = width of the conduit (ft, use diameter for circular conduits)

Y<sub>t</sub> = tailwater depth (ft)

θ = the expansion angle of the culvert flow

Where:

Q = design discharge (cfs)

V = the allowable non-eroding velocity in the downstream channel (ft/sec)

A<sub>t</sub> = required area of flow at allowable velocity (ft<sup>2</sup>)

Note:

<sup>1</sup> Calculations follow criteria in the USDCM Vol.2 Chapter 9

<sup>2</sup> Calculations assume a circular culvert

<sup>3</sup> This spreadsheet assumes y<sub>t</sub>/D<sub>c</sub>=0.4 in cases where y<sub>t</sub> is unknown or a hydraulic jump is suspected downstream of the outlet.

<sup>4</sup> Per the USDCM Vol.2 in no case should L<sub>p</sub> be less than 3D, nor does L<sub>p</sub> need to be greater than 10D whenever the Froude parameter is less than 6.0. whenever the Froude parameter is greater than 6, increase the maximum L<sub>p</sub> required by 1/4 D<sub>c</sub> for each whole number by which the Froude parameter is greater than 6



Riprap Sizing - Spillway				
q (cfs/ft)	S (ft/ft)	C <sub>f</sub>	n	D <sub>50</sub> min. (in)
0.16	0.02	3	0.025	0.76

SFB-C

**Type VL Riprap (D<sub>50</sub> = 6") will be utilized for the spillway protection**

$$D_{50} = 5.23 S^{0.43} (1.35 C_f q)^{0.56}$$

Equation 13-9

Where:

- $D_{50}$  = median rock size (in)
- $S$  = longitudinal slope (ft/ft)
- $C_f$  = concentration factor (1.0 to 3.0)
- $q$  = unit discharge (cfs/ft)

When:

- $\eta$  (porosity) = 0.0 (i.e., for buried soil riprap)

## **APPENDIX D – WATER QUALITY & DETENTION**

## Design Procedure Form: Sand Filter (SF)

UD-BMP (Version 3.07, March 2018)

Sheet 1 of 2

**Designer:** SPC  
**Company:** HR Green  
**Date:** August 28, 2024  
**Project:** Eastonville Road - Segment 2 Improvements  
**Location:** El Paso County, CO

<p>1. Basin Storage Volume</p> <p>A) Effective Imperviousness of Tributary Area, <math>I_a</math> (100% if all paved and roofed areas upstream of sand filter)</p> <p>B) Tributary Area's Imperviousness Ratio (<math>i = I_a/100</math>)</p> <p>C) Water Quality Capture Volume (WQCV) Based on 12-hour Drain Time <math>WQCV = 0.8 * (0.91 * i^3 - 1.19 * i^2 + 0.78 * i)</math></p> <p>D) Contributing Watershed Area (including sand filter area)</p> <p>E) Water Quality Capture Volume (WQCV) Design Volume <math>V_{WQCV} = WQCV / 12 * Area</math></p> <p>F) For Watersheds Outside of the Denver Region, Depth of Average Runoff Producing Storm</p> <p>G) For Watersheds Outside of the Denver Region, Water Quality Capture Volume (WQCV) Design Volume</p> <p>H) User Input of Water Quality Capture Volume (WQCV) Design Volume (Only if a different WQCV Design Volume is desired)</p>	<p><math>I_a = </math> <input style="width: 50px;" type="text" value="54.0"/> %</p> <p><math>i = </math> <input style="width: 50px;" type="text" value="0.540"/></p> <p>WQCV = <input style="width: 50px;" type="text" value="0.17"/> watershed inches</p> <p>Area = <input style="width: 50px;" type="text" value="27,443"/> sq ft</p> <p><math>V_{WQCV} = </math> <input style="width: 50px;" type="text" value="398"/> cu ft</p> <p><math>d_e = </math> <input style="width: 50px;" type="text" value=""/></p> <p><math>V_{WQCV OTHER} = </math> <input style="width: 50px;" type="text" value=""/> cu ft</p> <p><math>V_{WQCV USER} = </math> <input style="width: 50px;" type="text" value=""/> cu ft</p>
<p>2. Basin Geometry</p> <p>A) WQCV Depth</p> <p>B) Sand Filter Side Slopes (Horizontal distance per unit vertical, 4:1 or flatter preferred). Use "0" if sand filter has vertical walls.</p> <p>C) Minimum Filter Area (Flat Surface Area)</p> <p>D) Actual Filter Area</p> <p>E) Volume Provided</p>	<p><math>D_{WQCV} = </math> <input style="width: 50px;" type="text" value="1.0"/> ft</p> <p><math>Z = </math> <input style="width: 50px;" type="text" value="4.00"/> ft / ft</p> <p><math>A_{Min} = </math> <input style="width: 50px;" type="text" value="185"/> sq ft</p> <p><math>A_{Actual} = </math> <input style="width: 50px;" type="text" value="200"/> sq ft</p> <p><math>V_T = </math> <input style="width: 50px;" type="text" value="4288"/> cu ft</p>
<p>3. Filter Material</p>	<div style="border: 1px solid black; padding: 5px;"> <p>Choose One _____</p> <p><input checked="" type="radio"/> 18" CDOT Class B or C Filter Material</p> <p><input type="radio"/> Other (Explain):</p> <p>_____</p> <p>_____</p> </div>
<p>4. Underdrain System</p> <p>A) Are underdrains provided?</p> <p>B) Underdrain system orifice diameter for 12 hour drain time</p> <p style="margin-left: 20px;">i) Distance From Lowest Elevation of the Storage Volume to the Center of the Orifice</p> <p style="margin-left: 20px;">ii) Volume to Drain in 12 Hours</p> <p style="margin-left: 20px;">iii) Orifice Diameter, 3/8" Minimum</p>	<div style="border: 1px solid black; padding: 5px;"> <p>Choose One _____</p> <p><input checked="" type="radio"/> YES</p> <p><input type="radio"/> NO</p> </div> <p><math>y = </math> <input style="width: 50px;" type="text" value="2.0"/> ft</p> <p><math>Vol_{12} = </math> <input style="width: 50px;" type="text" value="398"/> cu ft</p> <p><math>D_o = </math> <input style="width: 50px;" type="text" value="7/16"/> in</p>

Design Procedure Form: Sand Filter (SF)

Sheet 2 of 2

Designer: SPC  
Company: HR Green  
Date: August 28, 2024  
Project: Eastonville Road - Segment 2 Improvements  
Location: El Paso County, CO

5. Impermeable Geomembrane Liner and Geotextile Separator Fabric

A) Is an impermeable liner provided due to proximity of structures or groundwater contamination?

Choose One

YES     NO

6. Inlet / Outlet Works

A) Describe the type of energy dissipation at inlet points and means of conveying flows in excess of the WQCV through the outlet

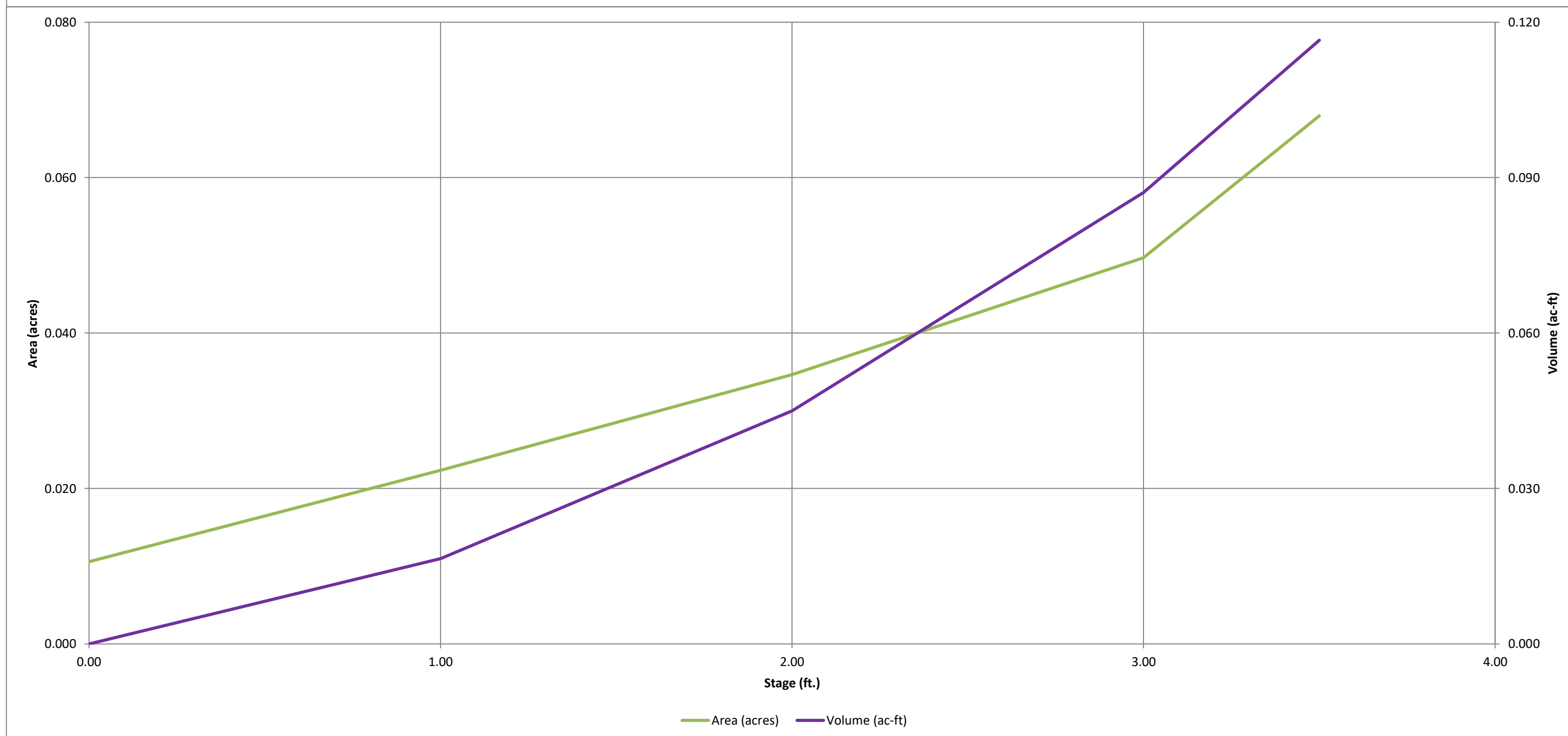
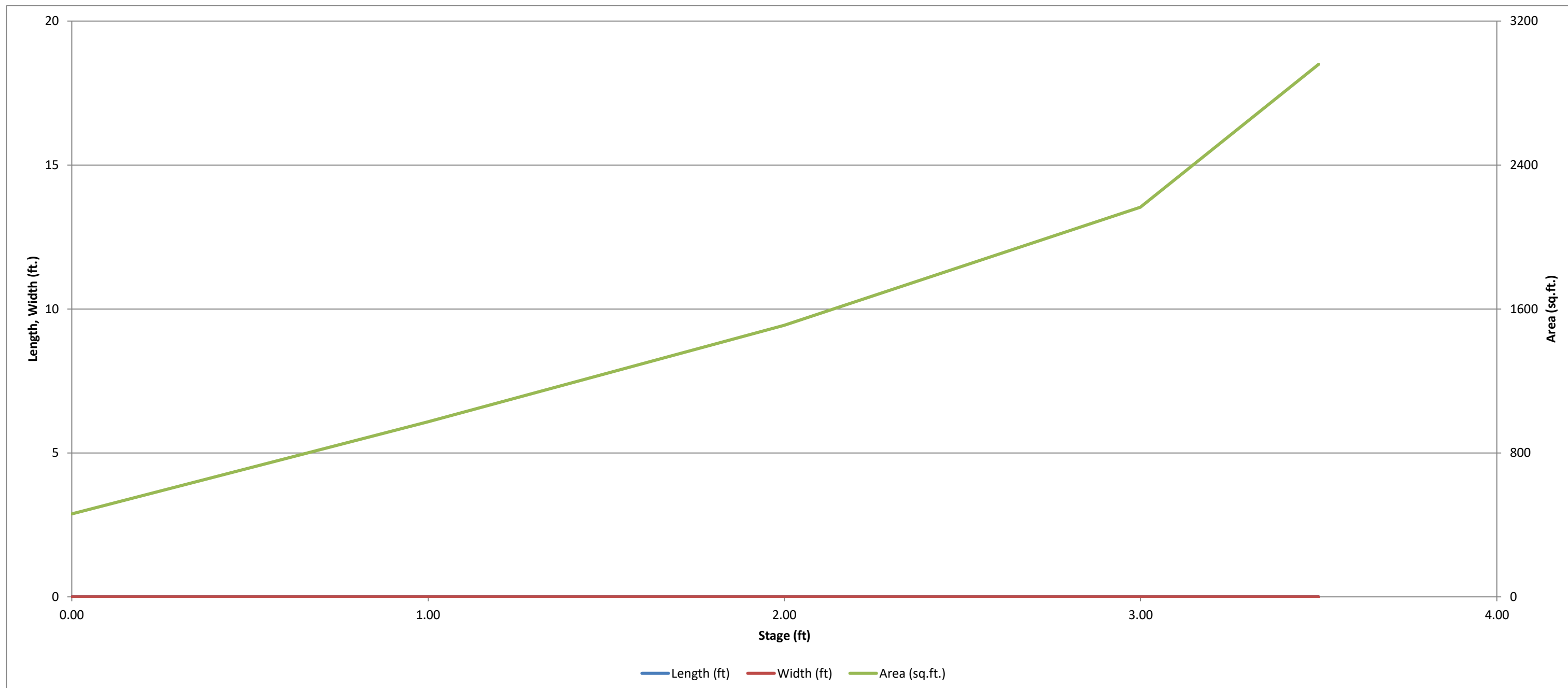
Engery dissapation at inlet points provided via riprap, and means of conveying flows in excess of the WQCV through the outlet is via the modified type 'C' inlet outlet structure grate, and a restricted outlet pipe.

Notes: \_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_



# DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.05 (January 2022)



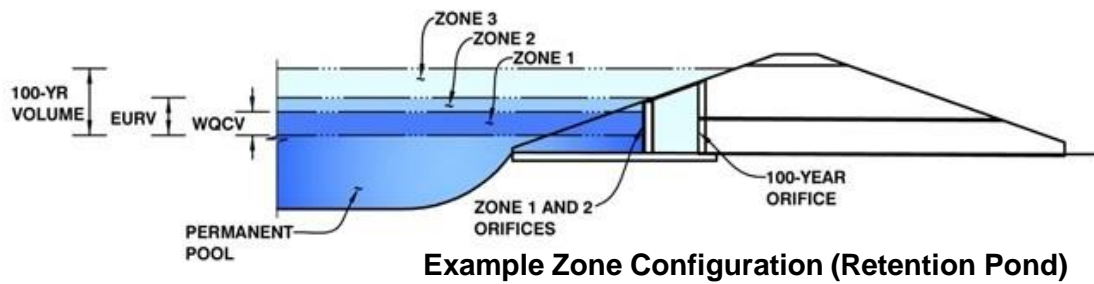


# DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.05 (January 2022)

**Project: Eastonville Road**

**Basin ID: POND C**



	Estimated Stage (ft)	Estimated Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	0.64	0.009	Filtration Media
Zone 2 (EURV)	1.75	0.027	Filtration Media
Zone 3 (100-year)	2.44	0.025	Weir&Pipe (Restrict)
<b>Total (all zones)</b>		<b>0.062</b>	

**User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)**

Underdrain Orifice Invert Depth =	1.98	ft (distance below the filtration media surface)
Underdrain Orifice Diameter =	0.48	inches

**Calculated Parameters for Underdrain**

Underdrain Orifice Area =	0.0	ft <sup>2</sup>
Underdrain Orifice Centroid =	0.02	feet

**User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)**

Centroid of Lowest Orifice =	N/A	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Orifice Plate =	N/A	ft (relative to basin bottom at Stage = 0 ft)
Orifice Plate: Orifice Vertical Spacing =	N/A	inches
Orifice Plate: Orifice Area per Row =	N/A	sq. inches

**Calculated Parameters for Plate**

WQ Orifice Area per Row =	N/A	ft <sup>2</sup>
Elliptical Half-Width =	N/A	feet
Elliptical Slot Centroid =	N/A	feet
Elliptical Slot Area =	N/A	ft <sup>2</sup>

**User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)**

	Row 1 (optional)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Orifice Area (sq. inches)	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Orifice Area (sq. inches)	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A

**User Input: Vertical Orifice (Circular or Rectangular)**

	Not Selected	Not Selected	
Invert of Vertical Orifice =	N/A	N/A	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Vertical Orifice =	N/A	N/A	ft (relative to basin bottom at Stage = 0 ft)
Vertical Orifice Diameter =	N/A	N/A	inches

**Calculated Parameters for Vertical Orifice**

	Not Selected	Not Selected	
Vertical Orifice Area =	N/A	N/A	ft <sup>2</sup>
Vertical Orifice Centroid =	N/A	N/A	feet

**User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir and No Outlet Pipe)**

**Calculated Parameters for Overflow Weir**

	Zone 3 Weir	Not Selected		Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, H <sub>o</sub> =	1.85	N/A	ft (relative to basin bottom at Stage = 0 ft)	1.85	N/A	feet
Overflow Weir Front Edge Length =	3.00	N/A	feet	3.00	N/A	feet
Overflow Weir Grate Slope =	0.00	N/A	H:V	0.00	N/A	
Horiz. Length of Weir Sides =	3.00	N/A	feet	3.00	N/A	feet
Overflow Grate Type =	Type C Grate	N/A		Type C Grate	N/A	
Debris Clogging % =	50%	N/A	%	50%	N/A	%
Height of Grate Upper Edge, H <sub>g</sub> =	1.85	N/A	feet	1.85	N/A	feet
Overflow Weir Slope Length =	3.00	N/A	feet	3.00	N/A	feet
Grate Open Area / 100-yr Orifice Area =	72.80	N/A		72.80	N/A	
Overflow Grate Open Area w/o Debris =	6.26	N/A	ft <sup>2</sup>	6.26	N/A	ft <sup>2</sup>
Overflow Grate Open Area w/ Debris =	3.13	N/A	ft <sup>2</sup>	3.13	N/A	ft <sup>2</sup>

**User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)**

**Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate**

	Zone 3 Restrictor	Not Selected		Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	2.00	N/A	ft (distance below basin bottom at Stage = 0 ft)	2.00	N/A	ft <sup>2</sup>
Outlet Pipe Diameter =	12.00	N/A	inches	12.00	N/A	feet
Restrictor Plate Height Above Pipe Invert =	2.00	N/A	inches	2.00	N/A	radians
Outlet Orifice Area =	0.09	N/A	ft <sup>2</sup>	0.09	N/A	ft <sup>2</sup>
Outlet Orifice Centroid =	0.10	N/A	feet	0.10	N/A	feet
Half-Central Angle of Restrictor Plate on Pipe =	0.84	N/A	radians	0.84	N/A	radians

**User Input: Emergency Spillway (Rectangular or Trapezoidal)**

**Calculated Parameters for Spillway**

Spillway Invert Stage =	2.86	ft (relative to basin bottom at Stage = 0 ft)	Spillway Design Flow Depth =	0.14	feet
Spillway Crest Length =	12.00	feet	Stage at Top of Freeboard =	4.00	feet
Spillway End Slopes =	4.00	H:V	Basin Area at Top of Freeboard =	0.07	acres
Freeboard above Max Water Surface =	1.00	feet	Basin Volume at Top of Freeboard =	0.12	acre-ft

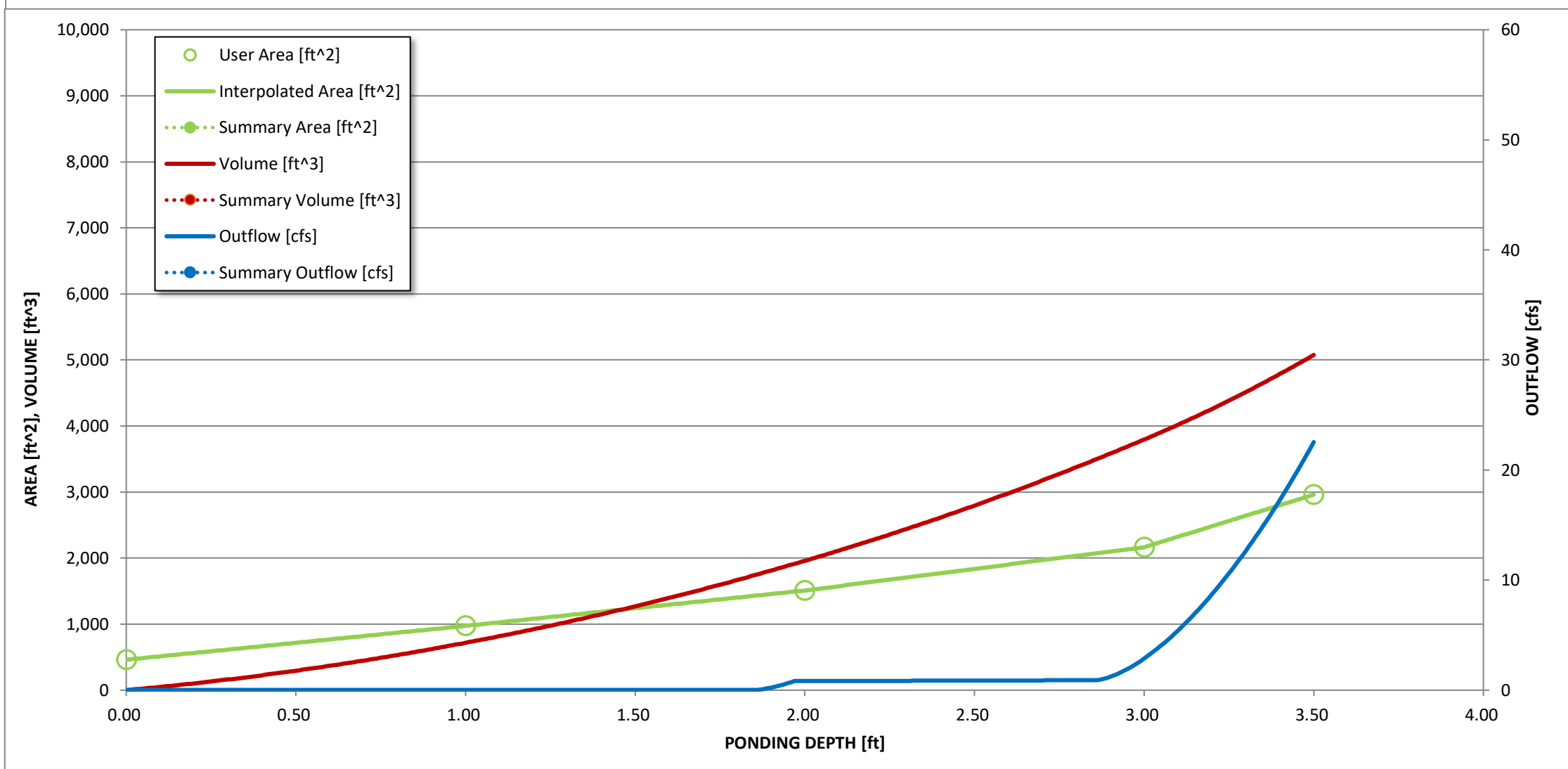
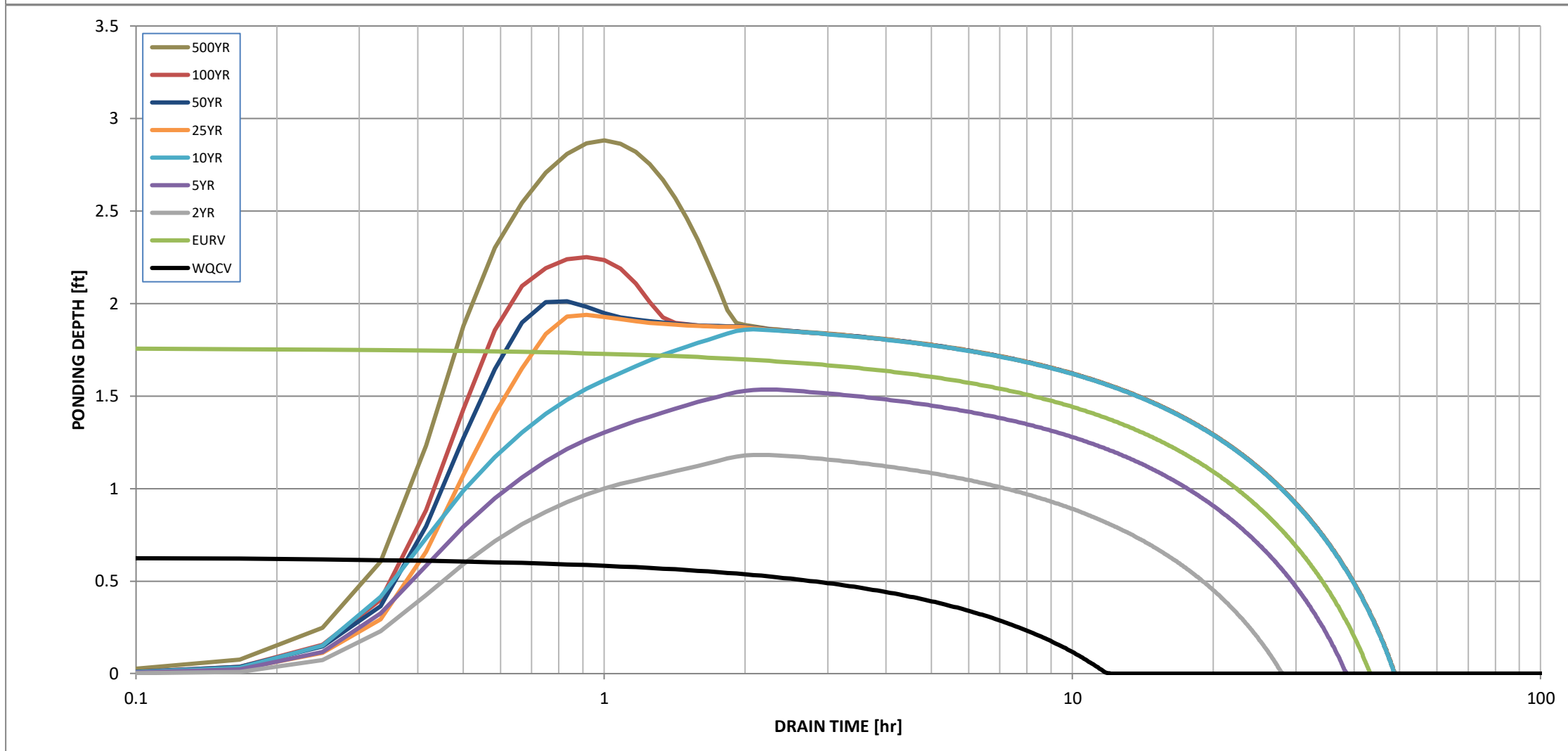
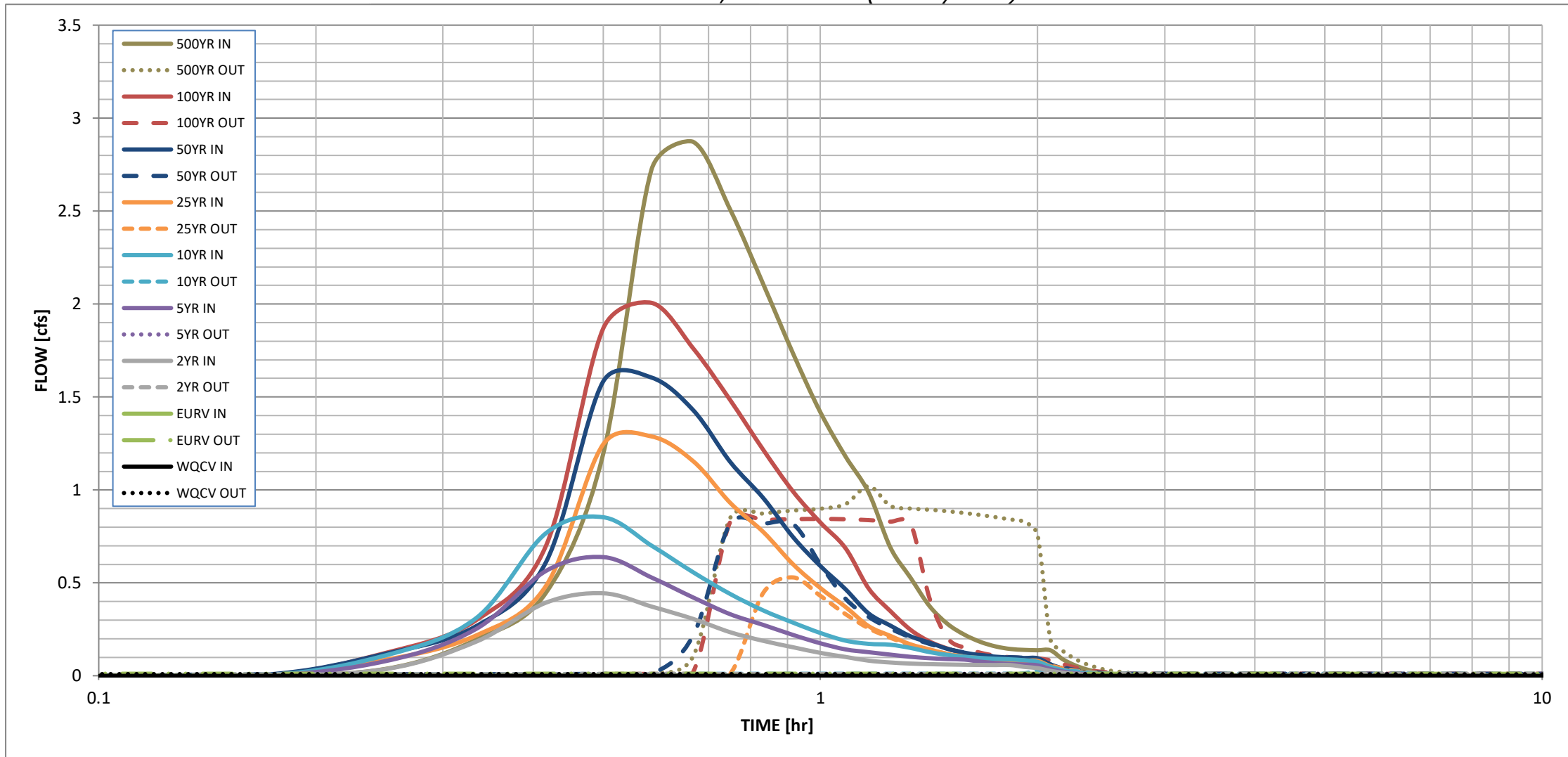
**Routed Hydrograph Results**

The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).

	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =	N/A	N/A	0.93	1.21	1.46	1.84	2.16	2.49	3.37
One-Hour Rainfall Depth (in) =	0.009	0.037	0.023	0.032	0.043	0.063	0.079	0.097	0.142
CUHP Runoff Volume (acre-ft) =	N/A	N/A	0.023	0.032	0.043	0.063	0.079	0.097	0.142
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	0.0	0.1	0.2	0.5	0.8	1.0	1.6
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A	0.01	0.12	0.32	0.87	1.20	1.59	2.49
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A	0.4	0.6	0.9	1.3	1.6	2.0	2.9
Predevelopment Unit Peak Flow, q (cfs/acre) =	0.0	0.0	0.0	0.0	0.0	0.5	0.8	0.8	1.0
Peak Inflow Q (cfs) =	N/A	N/A	N/A	0.1	0.2	1.0	1.1	0.8	0.6
Peak Outflow Q (cfs) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Ratio Peak Outflow to Predevelopment Q =	Filtration Media	Filtration Media	Filtration Media	Filtration Media	Overflow Weir 1	Overflow Weir 1	Outlet Plate 1	Outlet Plate 1	Spillway
Structure Controlling Flow =	N/A	N/A	N/A	N/A	0.0	0.1	0.1	0.1	0.1
Max Velocity through Gate 1 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Max Velocity through Gate 2 (fps) =	12	42	27	37	47	46	46	45	43
Time to Drain 97% of Inflow Volume (hours) =	12	43	28	38	48	48	48	47	47
Time to Drain 99% of Inflow Volume (hours) =	0.64	1.77	1.18	1.54	1.86	1.94	2.01	2.25	2.88
Maximum Ponding Depth (ft) =	0.02	0.03	0.02	0.03	0.03	0.03	0.03	0.04	0.05
Area at Maximum Ponding Depth (acres) =	0.009	0.037	0.021	0.030	0.040	0.043	0.045	0.054	0.081
Maximum Volume Stored (acre-ft) =									

# DETENTION BASIN OUTLET STRUCTURE DESIGN

*MHFD-Detention, Version 4.05 (January 2022)*



S-A-V-D Chart Axis Override	X-axis	Left Y-Axis	Right Y-Axis
minimum bound			
maximum bound			

# DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename: \_\_\_\_\_

## Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

Time Interval	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.04
	0:15:00	0.00	0.00	0.04	0.08	0.11	0.09	0.12	0.12	0.19
	0:20:00	0.00	0.00	0.18	0.25	0.31	0.22	0.27	0.30	0.45
	0:25:00	0.00	0.00	0.39	0.56	0.77	0.48	0.61	0.70	1.19
	0:30:00	0.00	0.00	0.44	0.64	0.85	1.25	1.58	1.87	2.72
	0:35:00	0.00	0.00	0.37	0.53	0.70	1.29	1.60	2.01	2.87
	0:40:00	0.00	0.00	0.31	0.42	0.56	1.15	1.43	1.76	2.51
	0:45:00	0.00	0.00	0.23	0.33	0.44	0.93	1.15	1.48	2.11
	0:50:00	0.00	0.00	0.19	0.27	0.35	0.77	0.96	1.22	1.73
	0:55:00	0.00	0.00	0.15	0.22	0.29	0.60	0.75	0.99	1.42
	1:00:00	0.00	0.00	0.12	0.18	0.23	0.47	0.59	0.83	1.18
	1:05:00	0.00	0.00	0.10	0.14	0.19	0.37	0.47	0.69	0.99
	1:10:00	0.00	0.00	0.08	0.13	0.17	0.27	0.34	0.47	0.69
	1:15:00	0.00	0.00	0.07	0.11	0.17	0.22	0.27	0.35	0.53
	1:20:00	0.00	0.00	0.07	0.10	0.15	0.17	0.21	0.25	0.38
	1:25:00	0.00	0.00	0.06	0.10	0.13	0.14	0.18	0.19	0.28
	1:30:00	0.00	0.00	0.06	0.09	0.11	0.12	0.15	0.15	0.22
	1:35:00	0.00	0.00	0.06	0.09	0.10	0.10	0.12	0.12	0.18
	1:40:00	0.00	0.00	0.06	0.08	0.10	0.09	0.11	0.11	0.16
	1:45:00	0.00	0.00	0.06	0.07	0.09	0.09	0.10	0.10	0.14
	1:50:00	0.00	0.00	0.06	0.06	0.09	0.08	0.10	0.09	0.14
	1:55:00	0.00	0.00	0.05	0.06	0.08	0.08	0.10	0.09	0.14
	2:00:00	0.00	0.00	0.04	0.06	0.08	0.08	0.10	0.09	0.14
	2:05:00	0.00	0.00	0.03	0.04	0.05	0.05	0.06	0.06	0.09
	2:10:00	0.00	0.00	0.02	0.02	0.03	0.03	0.04	0.04	0.06
	2:15:00	0.00	0.00	0.01	0.01	0.02	0.02	0.03	0.02	0.04
	2:20:00	0.00	0.00	0.01	0.01	0.01	0.01	0.02	0.01	0.02
	2:25:00	0.00	0.00	0.00	0.01	0.01	0.01	0.01	0.01	0.01
	2:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.01
	2:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
5:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	



## Design Procedure Form: Extended Detention Basin (EDB)

UD-BMP (Version 3.07, March 2018)

Sheet 1 of 3

**Designer:** SPC  
**Company:** HR Green  
**Date:** August 23, 2024  
**Project:** Eastonville Road - Segment 1 Improvements EDB B ULTIMATE CONDITIONS  
**Location:** EL PASO COUNTY, CO

<p>1. Basin Storage Volume</p> <p>A) Effective Imperviousness of Tributary Area, <math>I_a</math></p> <p>B) Tributary Area's Imperviousness Ratio (<math>i = I_a / 100</math>)</p> <p>C) Contributing Watershed Area</p> <p>D) For Watersheds Outside of the Denver Region, Depth of Average Runoff Producing Storm</p> <p>E) Design Concept (Select EURV when also designing for flood control)</p> <p>F) Design Volume (WQCV) Based on 40-hour Drain Time (<math>V_{DESIGN} = (1.0 * (0.91 * i^3 - 1.19 * i^2 + 0.78 * i) / 12 * Area)</math>)</p> <p>G) For Watersheds Outside of the Denver Region, Water Quality Capture Volume (WQCV) Design Volume (<math>V_{WQCV\ OTHER} = (d_6 * (V_{DESIGN} / 0.43))</math>)</p> <p>H) User Input of Water Quality Capture Volume (WQCV) Design Volume (Only if a different WQCV Design Volume is desired)</p> <p>I) NRCS Hydrologic Soil Groups of Tributary Watershed              i) Percentage of Watershed consisting of Type A Soils              ii) Percentage of Watershed consisting of Type B Soils              iii) Percentage of Watershed consisting of Type C/D Soils</p> <p>J) Excess Urban Runoff Volume (EURV) Design Volume              For HSG A: <math>EURV_A = 1.68 * i^{1.28}</math>              For HSG B: <math>EURV_B = 1.36 * i^{1.08}</math>              For HSG C/D: <math>EURV_{C/D} = 1.20 * i^{1.08}</math></p> <p>K) User Input of Excess Urban Runoff Volume (EURV) Design Volume (Only if a different EURV Design Volume is desired)</p>	<p><math>I_a = </math> <input type="text" value="67.0"/> %</p> <p><math>i = </math> <input type="text" value="0.670"/></p> <p>Area = <input type="text" value="9.020"/> ac</p> <p><math>d_6 = </math> <input type="text" value="0.42"/> in</p> <div style="border: 1px solid black; padding: 5px; margin: 5px 0;"> <p>Choose One</p> <p><input type="radio"/> Water Quality Capture Volume (WQCV)</p> <p><input checked="" type="radio"/> Excess Urban Runoff Volume (EURV)</p> </div> <p><math>V_{DESIGN} = </math> <input type="text"/> ac-ft</p> <p><math>V_{DESIGN\ OTHER} = </math> <input type="text" value="0.192"/> ac-ft</p> <p><math>V_{DESIGN\ USER} = </math> <input type="text"/> ac-ft</p> <p><math>HSG_A = </math> <input type="text" value="100"/> %  <math>HSG_B = </math> <input type="text" value="0"/> %  <math>HSG_{C/D} = </math> <input type="text" value="0"/> %</p> <p><math>EURV_{DESIGN} = </math> <input type="text" value="0.756"/> ac-ft</p> <p><math>EURV_{DESIGN\ USER} = </math> <input type="text"/> ac-ft</p>
<p>2. Basin Shape: Length to Width Ratio (A basin length to width ratio of at least 2:1 will improve TSS reduction.)</p>	<p><math>L : W = </math> <input type="text" value="2.0"/> : 1</p>
<p>3. Basin Side Slopes</p> <p>A) Basin Maximum Side Slopes (Horizontal distance per unit vertical, 4:1 or flatter preferred)</p>	<p><math>Z = </math> <input type="text" value="4.00"/> ft / ft</p>
<p>4. Inlet</p> <p>A) Describe means of providing energy dissipation at concentrated inflow locations:</p>	<p>_____</p> <p>_____</p> <p>_____</p>
<p>5. Forebay</p> <p>A) Minimum Forebay Volume (<math>V_{MIN} = </math> <input type="text" value="3%"/> of the WQCV)</p> <p>B) Actual Forebay Volume</p> <p>C) Forebay Depth (<math>D_F = </math> <input type="text" value="18"/> inch maximum)</p> <p>D) Forebay Discharge              i) Undetained 100-year Peak Discharge              ii) Forebay Discharge Design Flow (<math>Q_F = 0.02 * Q_{100}</math>)</p> <p>E) Forebay Discharge Design</p> <p>F) Discharge Pipe Size (minimum 8-inches)</p> <p>G) Rectangular Notch Width</p>	<p><math>V_{MIN} = </math> <input type="text" value="0.006"/> ac-ft</p> <p><math>V_F = </math> <input type="text" value="0.006"/> ac-ft</p> <p><math>D_F = </math> <input type="text" value="15.0"/> in</p> <p><math>Q_{100} = </math> <input type="text" value="26.00"/> cfs</p> <p><math>Q_F = </math> <input type="text" value="0.52"/> cfs</p> <div style="border: 1px solid black; padding: 5px; margin: 5px 0;"> <p>Choose One</p> <p><input type="radio"/> Berm With Pipe</p> <p><input checked="" type="radio"/> Wall with Rect. Notch</p> <p><input type="radio"/> Wall with V-Notch Weir</p> </div> <p style="color: blue; font-weight: bold;">Flow too small for berm w/ pipe</p> <p>Calculated <math>D_P = </math> <input type="text"/> in</p> <p>Calculated <math>W_N = </math> <input type="text" value="4.3"/> in</p>





**Design Procedure Form: Extended Detention Basin (EDB)**

**Designer:** SPC  
**Company:** HR Green  
**Date:** August 23, 2024  
**Project:** Eastonville Road - Segment 1 Improvements EDB B ULTIMATE CONDITIONS  
**Location:** EL PASO COUNTY, CO

<p>6. Trickle Channel</p> <p>A) Type of Trickle Channel</p> <p>F) Slope of Trickle Channel</p>	<div style="border: 1px solid black; padding: 5px; margin-bottom: 10px;">             Choose One  <input checked="" type="radio"/> Concrete  <input type="radio"/> Soft Bottom         </div> <p>S = <input type="text" value="0.0050"/> ft / ft</p>
<p>7. Micropool and Outlet Structure</p> <p>A) Depth of Micropool (2.5-feet minimum)</p> <p>B) Surface Area of Micropool (10 ft<sup>2</sup> minimum)</p> <p>C) Outlet Type</p> <p>D) Smallest Dimension of Orifice Opening Based on Hydrograph Routing (Use UD-Detention)</p> <p>E) Total Outlet Area</p>	<p>D<sub>M</sub> = <input type="text" value="2.5"/> ft</p> <p>A<sub>M</sub> = <input type="text" value="10"/> sq ft</p> <div style="border: 1px solid black; padding: 5px; margin-bottom: 10px;">             Choose One  <input checked="" type="radio"/> Orifice Plate  <input type="radio"/> Other (Describe):         </div> <hr/> <hr/> <p>D<sub>orifice</sub> = <input type="text" value="1.00"/> inches</p> <p>A<sub>ot</sub> = <input type="text" value="5.50"/> square inches</p>
<p>8. Initial Surcharge Volume</p> <p>A) Depth of Initial Surcharge Volume (Minimum recommended depth is 4 inches)</p> <p>B) Minimum Initial Surcharge Volume (Minimum volume of 0.3% of the WQCV)</p> <p>C) Initial Surcharge Provided Above Micropool</p>	<p>D<sub>IS</sub> = <input type="text" value="4"/> in</p> <p>V<sub>IS</sub> = <input type="text" value="25"/> cu ft</p> <p>V<sub>s</sub> = <input type="text" value="3.3"/> cu ft</p>
<p>9. Trash Rack</p> <p>A) Water Quality Screen Open Area: <math>A_t = A_{ot} * 38.5 * (e^{-0.095D})</math></p> <p>B) Type of Screen (If specifying an alternative to the materials recommended in the USDCM, indicate "other" and enter the ratio of the total open are to the total screen are for the material specified.)</p> <p style="text-align: right;">Other (Y/N): <input type="text" value="N"/></p> <p>C) Ratio of Total Open Area to Total Area (only for type 'Other')</p> <p>D) Total Water Quality Screen Area (based on screen type)</p> <p>E) Depth of Design Volume (EURV or WQCV) (Based on design concept chosen under 1E)</p> <p>F) Height of Water Quality Screen (H<sub>TR</sub>)</p> <p>G) Width of Water Quality Screen Opening (W<sub>opening</sub>) (Minimum of 12 inches is recommended)</p>	<p>A<sub>t</sub> = <input type="text" value="193"/> square inches</p> <div style="border: 1px solid black; padding: 2px; margin-bottom: 5px; width: fit-content;">             S.S. Well Screen with 60% Open Area         </div> <hr/> <hr/> <p>User Ratio = <input type="text"/></p> <p>A<sub>total</sub> = <input type="text" value="321"/> sq. in.</p> <p>H = <input type="text" value="5.05"/> feet</p> <p>H<sub>TR</sub> = <input type="text" value="88.6"/> inches</p> <p>W<sub>opening</sub> = <input type="text" value="12.0"/> inches <span style="color: red; font-weight: bold;">VALUE LESS THAN RECOMMENDED MIN. WIDTH. WIDTH HAS BEEN SET TO 12 INCHES.</span></p>

Design Procedure Form: Extended Detention Basin (EDB)

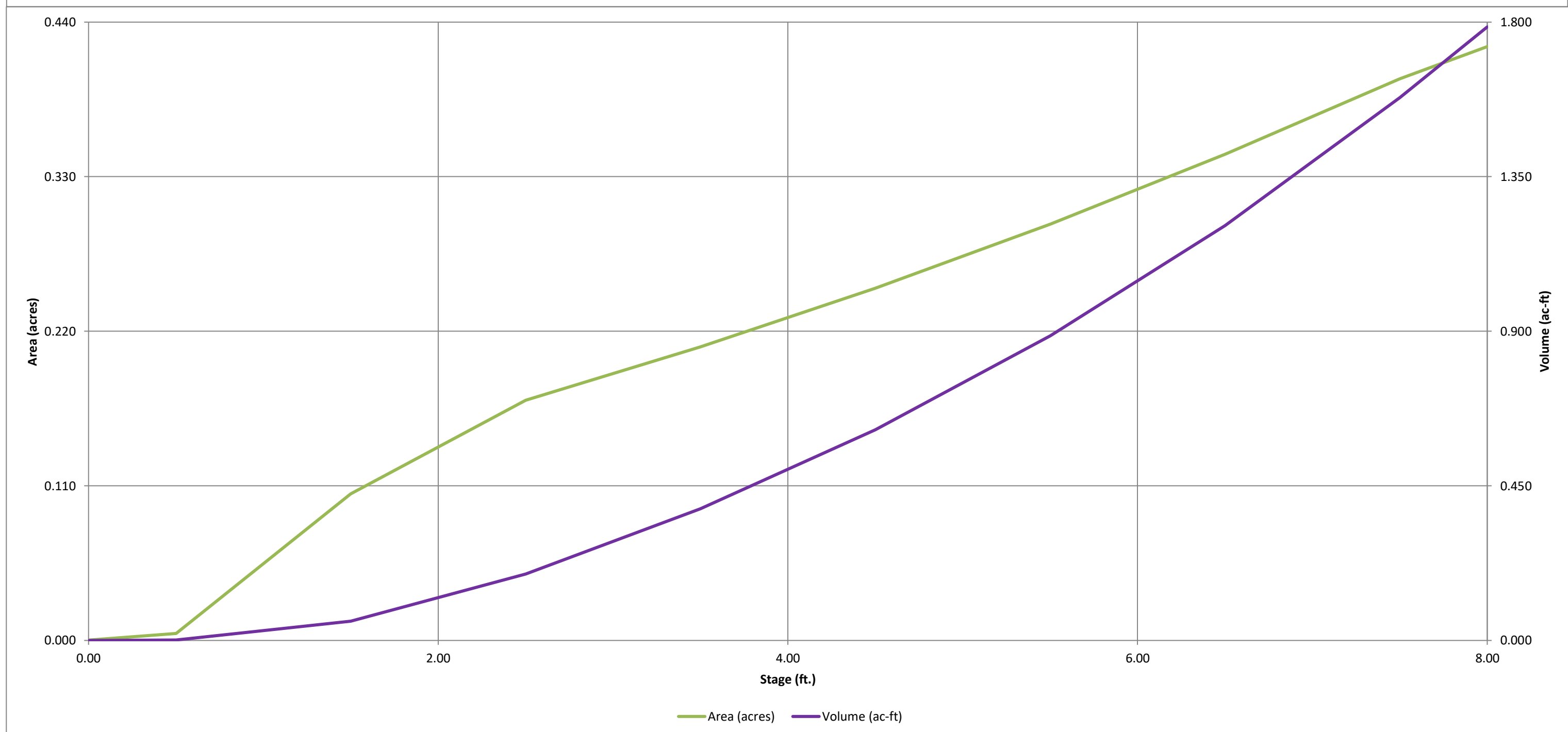
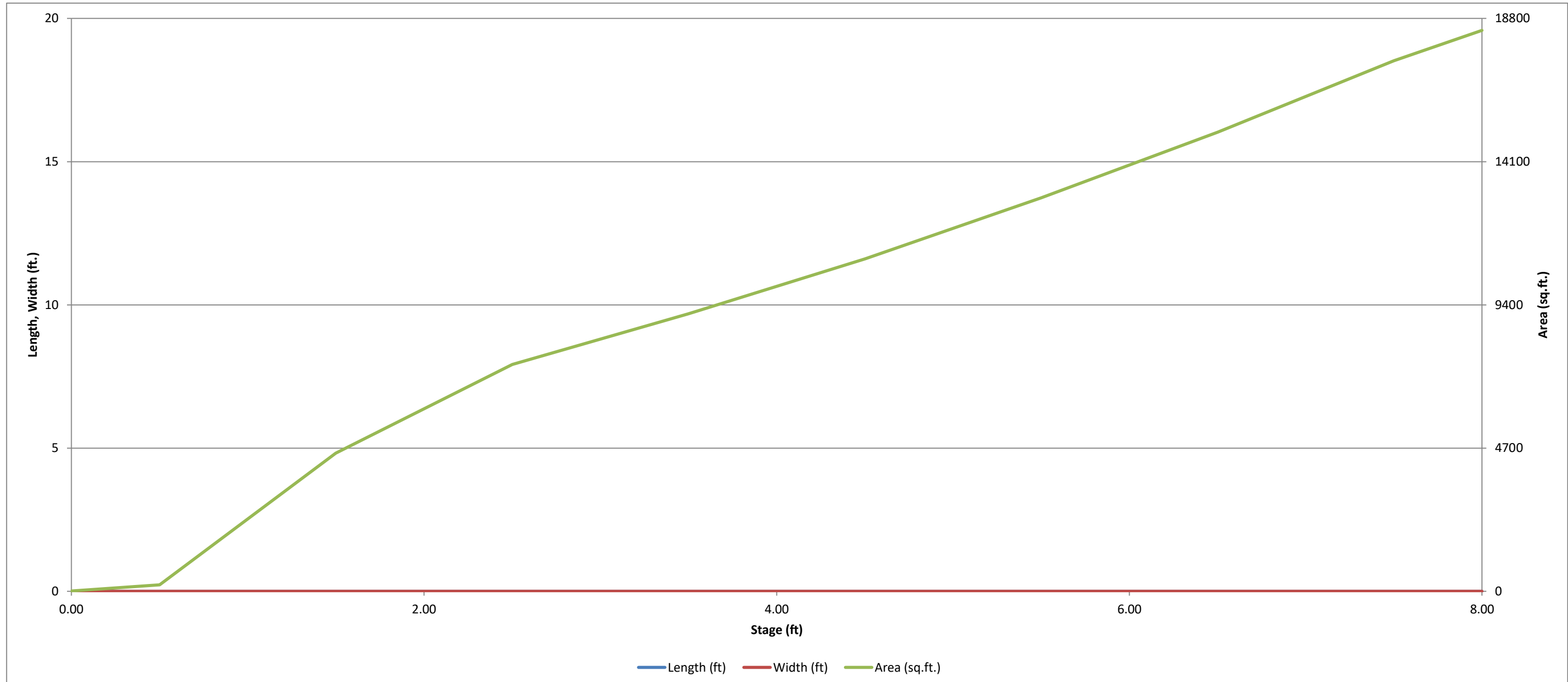
Designer: SPC  
Company: HR Green  
Date: August 23, 2024  
Project: Eastonville Road - Segment 1 Improvements EDB B ULTIMATE CONDITIONS  
Location: EL PASO COUNTY, CO

<p>10. Overflow Embankment</p> <p>A) Describe embankment protection for 100-year and greater overtopping:</p> <p>B) Slope of Overflow Embankment (Horizontal distance per unit vertical, 4:1 or flatter preferred)</p>	<p>_____</p> <p>_____</p> <p>_____</p> <p>Ze = <input type="text" value="4.00"/> ft / ft</p>
<p>11. Vegetation</p>	<p>Choose One</p> <p><input type="radio"/> Irrigated</p> <p><input checked="" type="radio"/> Not Irrigated</p>
<p>12. Access</p> <p>A) Describe Sediment Removal Procedures</p>	<p>_____</p> <p>_____</p> <p>_____</p> <p>_____</p> <p>_____</p>
<p>Notes: _____</p> <p>_____</p> <p>_____</p>	



# DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.05 (January 2022)

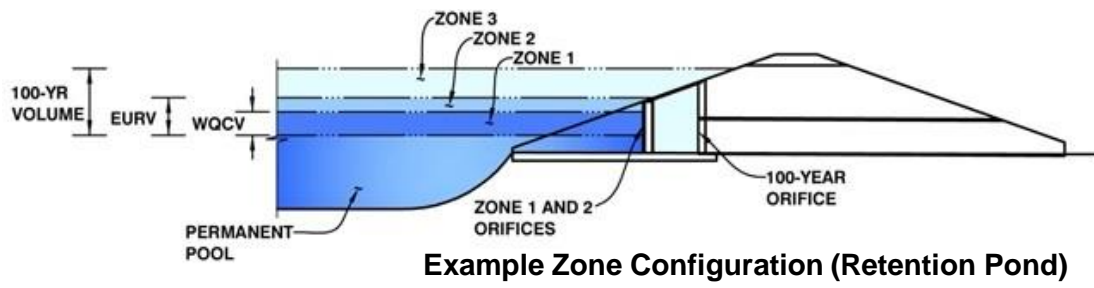


# DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.05 (January 2022)

**Project: Eastonville Road**

**Basin ID: POND B: Ultimate Conditions (INCLUDES SEGMENT 2 FLOW) [BASINS EA6 - EA10]**



	Estimated Stage (ft)	Estimated Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	2.53	0.197	Orifice Plate
Zone 2 (EURV)	5.05	0.559	Circular Orifice
Zone 3 (100-year)	6.25	0.363	Weir&Pipe (Restrict)
<b>Total (all zones)</b>		<b>1.119</b>	

**User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)**

Underdrain Orifice Invert Depth =	N/A	ft (distance below the filtration media surface)
Underdrain Orifice Diameter =	N/A	inches

**Calculated Parameters for Underdrain**

Underdrain Orifice Area =	N/A	ft <sup>2</sup>
Underdrain Orifice Centroid =	N/A	feet

**User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)**

Centroid of Lowest Orifice =	0.00	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Orifice Plate =	2.53	ft (relative to basin bottom at Stage = 0 ft)
Orifice Plate: Orifice Vertical Spacing =	N/A	inches
Orifice Plate: Orifice Area per Row =	0.79	sq. inches (diameter = 1 inch)

**Calculated Parameters for Plate**

WQ Orifice Area per Row =	5.451E-03	ft <sup>2</sup>
Elliptical Half-Width =	N/A	feet
Elliptical Slot Centroid =	N/A	feet
Elliptical Slot Area =	N/A	ft <sup>2</sup>

**User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)**

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	0.87	1.73					
Orifice Area (sq. inches)	0.79	0.79	0.79					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

**User Input: Vertical Orifice (Circular or Rectangular)**

	Zone 2 Circular	Not Selected	
Invert of Vertical Orifice =	2.55	N/A	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Vertical Orifice =	5.18	N/A	ft (relative to basin bottom at Stage = 0 ft)
Vertical Orifice Diameter =	1.75	N/A	inches

**Calculated Parameters for Vertical Orifice**

	Zone 2 Circular	Not Selected	
Vertical Orifice Area =	0.02	N/A	ft <sup>2</sup>
Vertical Orifice Centroid =	0.07	N/A	feet

**User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir and No Outlet Pipe)**

	Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, H <sub>o</sub> =	5.20	N/A	ft (relative to basin bottom at Stage = 0 ft)
Overflow Weir Front Edge Length =	3.00	N/A	feet
Overflow Weir Grate Slope =	0.00	N/A	H:V
Horiz. Length of Weir Sides =	3.00	N/A	feet
Overflow Grate Type =	Type C Grate	N/A	
Debris Clogging % =	50%	N/A	%

**Calculated Parameters for Overflow Weir**

	Zone 3 Weir	Not Selected	
Height of Grate Upper Edge, H <sub>g</sub> =	5.20	N/A	feet
Overflow Weir Slope Length =	3.00	N/A	feet
Grate Open Area / 100-yr Orifice Area =	25.92	N/A	
Overflow Grate Open Area w/o Debris =	6.26	N/A	ft <sup>2</sup>
Overflow Grate Open Area w/ Debris =	3.13	N/A	ft <sup>2</sup>

**User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)**

	Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	0.25	N/A	ft (distance below basin bottom at Stage = 0 ft)
Outlet Pipe Diameter =	18.00	N/A	inches
Restrictor Plate Height Above Pipe Invert =	3.50		inches

**Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate**

	Zone 3 Restrictor	Not Selected	
Outlet Orifice Area =	0.24	N/A	ft <sup>2</sup>
Outlet Orifice Centroid =	0.17	N/A	feet
Half-Central Angle of Restrictor Plate on Pipe =	0.91	N/A	radians

**User Input: Emergency Spillway (Rectangular or Trapezoidal)**

Spillway Invert Stage =	6.50	ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length =	15.50	feet
Spillway End Slopes =	4.00	H:V
Freeboard above Max Water Surface =	1.00	feet

**Calculated Parameters for Spillway**

Spillway Design Flow Depth =	0.50	feet
Stage at Top of Freeboard =	8.00	feet
Basin Area at Top of Freeboard =	0.42	acres
Basin Volume at Top of Freeboard =	1.79	acre-ft

**Routed Hydrograph Results**

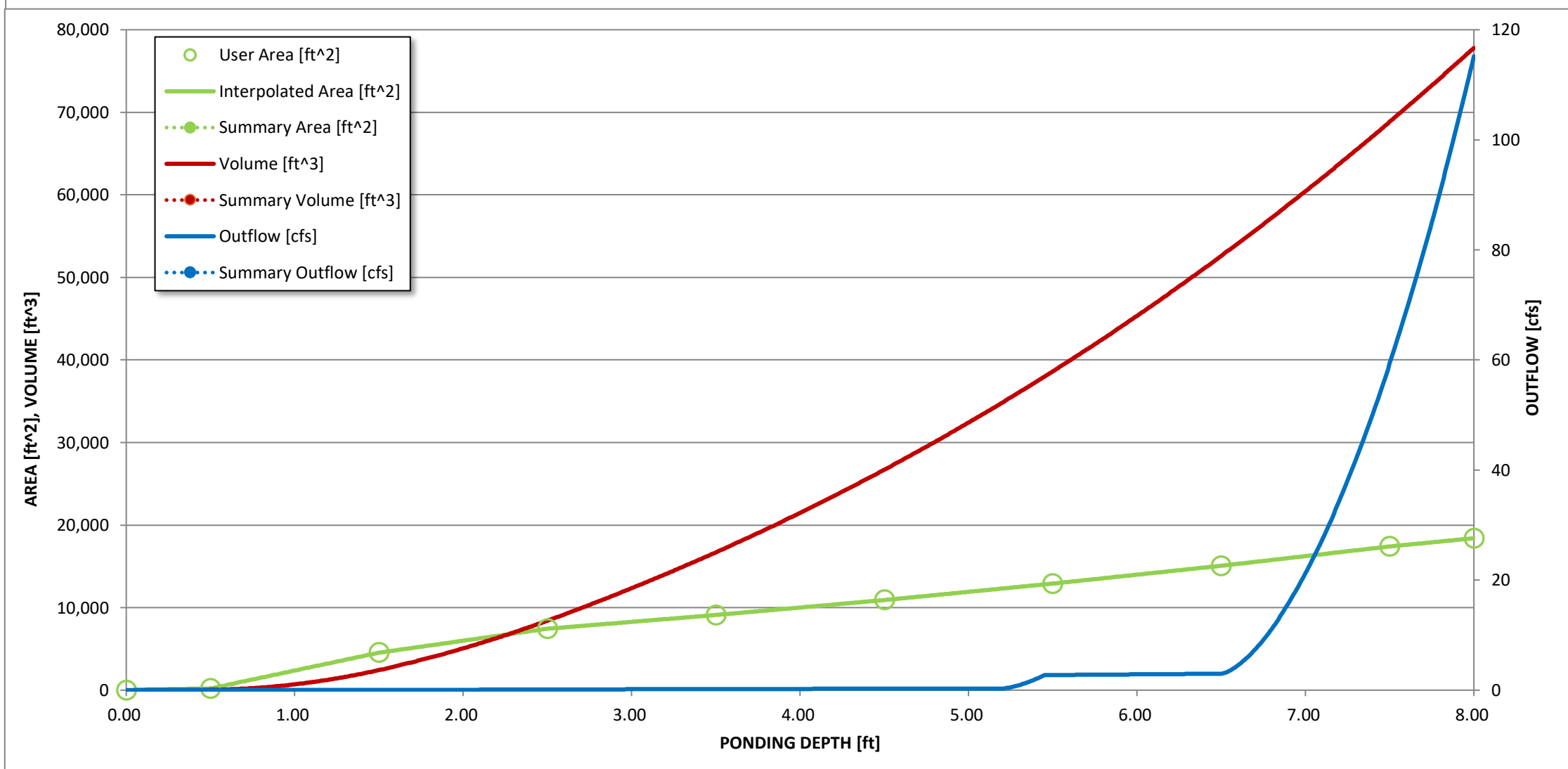
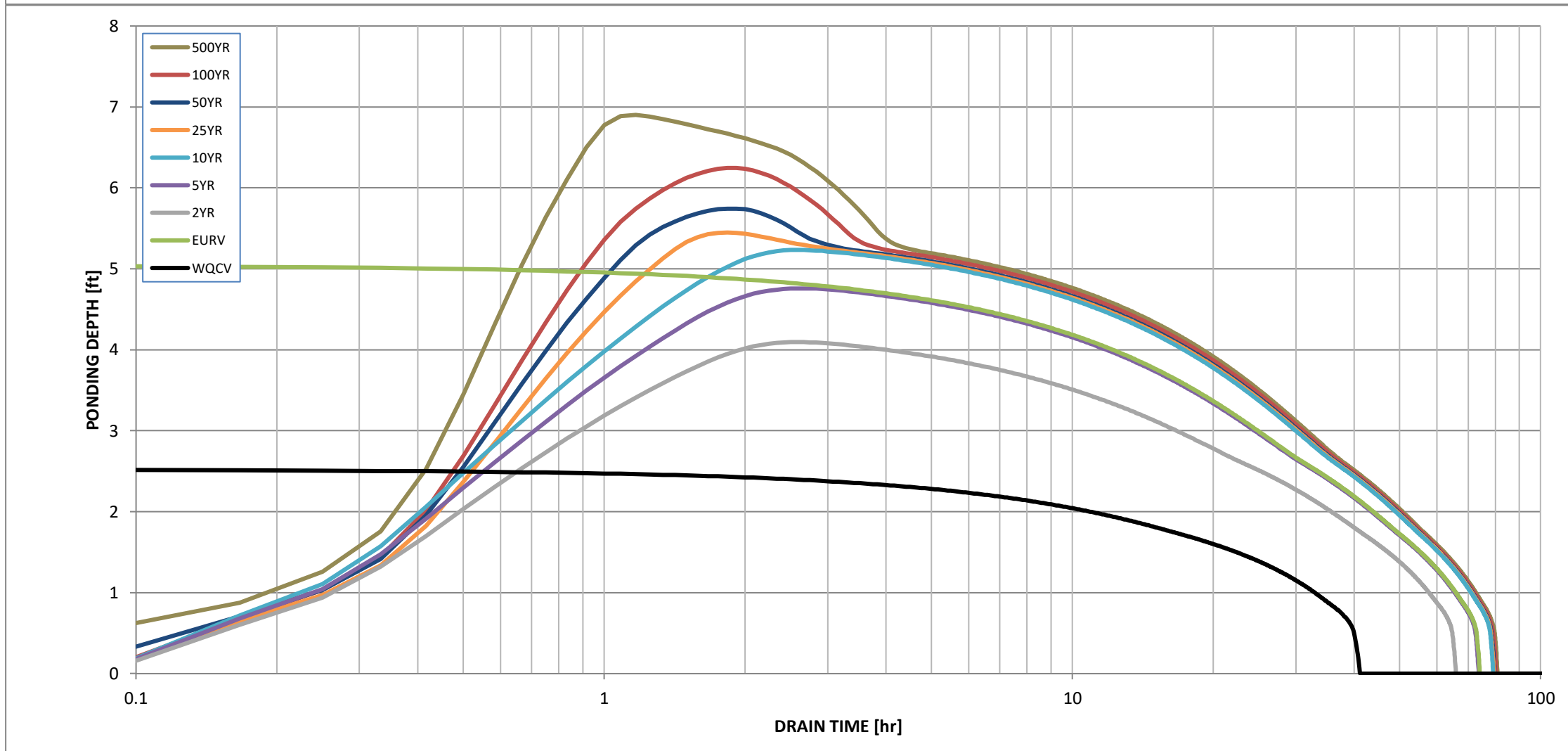
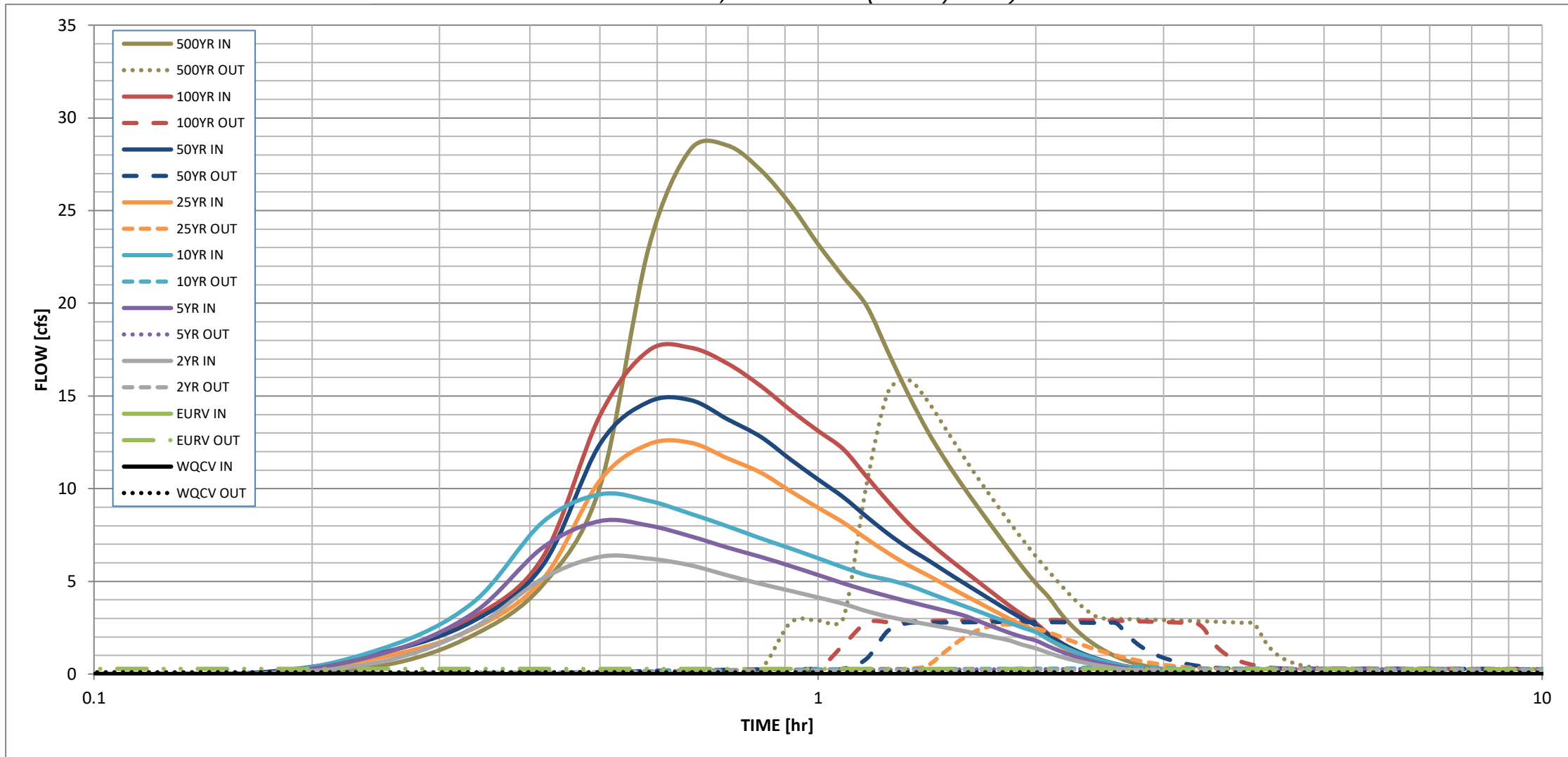
*The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).*

	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =									
One-Hour Rainfall Depth (in) =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52	3.68
CUHP Runoff Volume (acre-ft) =	0.197	0.756	0.556	0.728	0.866	1.043	1.217	1.427	2.302
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	0.556	0.728	0.866	1.043	1.217	1.427	2.302
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A	0.0	0.1	0.1	1.0	2.0	3.3	8.8
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A							
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.00	0.01	0.01	0.11	0.22	0.36	0.97
Peak Inflow Q (cfs) =	N/A	N/A	6.3	8.3	9.7	12.5	14.8	17.6	28.5
Peak Outflow Q (cfs) =	0.1	0.3	0.2	0.3	0.4	2.7	2.8	2.9	15.9
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	3.6	3.9	2.7	1.4	0.9	1.8
Structure Controlling Flow =	Plate	Vertical Orifice 1	Vertical Orifice 1	Vertical Orifice 1	Overflow Weir 1	Outlet Plate 1	Outlet Plate 1	Outlet Plate 1	Spillway
Max Velocity through Gate 1 (fps) =	N/A	N/A	N/A	N/A	0.0	0.4	0.4	0.4	0.4
Max Velocity through Gate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	37	64	58	64	68	67	66	65	59
Time to Drain 99% of Inflow Volume (hours) =	<b>40</b>	70	62	69	74	74	73	73	71
Maximum Ponding Depth (ft) =	2.53	5.05	4.09	4.76	5.23	5.45	5.74	6.25	6.90
Area at Maximum Ponding Depth (acres) =	0.17	0.28	0.23	0.26	0.28	0.29	0.31	0.33	0.37
Maximum Volume Stored (acre-ft) =	0.198	0.758	0.514	0.677	0.808	0.869	0.959	1.119	1.350



# DETENTION BASIN OUTLET STRUCTURE DESIGN

*MHFD-Detention, Version 4.05 (January 2022)*



S-A-V-D Chart Axis Override	X-axis	Left Y-Axis	Right Y-Axis
minimum bound			
maximum bound			

# DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename: \_\_\_\_\_

## Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

Time Interval	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.08	0.01	0.46
	0:15:00	0.00	0.00	0.68	1.11	1.37	0.92	1.16	1.13	2.08
	0:20:00	0.00	0.00	2.48	3.26	3.84	2.43	2.84	3.03	4.80
	0:25:00	0.00	0.00	5.15	6.82	8.20	5.12	5.86	6.29	10.12
	0:30:00	0.00	0.00	6.32	8.25	9.69	10.45	12.41	13.96	22.97
	0:35:00	0.00	0.00	6.23	8.02	9.35	12.39	14.68	17.45	28.30
	0:40:00	0.00	0.00	5.87	7.44	8.65	12.48	14.78	17.61	28.51
	0:45:00	0.00	0.00	5.33	6.82	7.97	11.64	13.74	16.75	27.19
	0:50:00	0.00	0.00	4.87	6.32	7.32	10.87	12.80	15.54	25.32
	0:55:00	0.00	0.00	4.49	5.83	6.77	9.86	11.57	14.23	23.19
	1:00:00	0.00	0.00	4.13	5.35	6.25	8.98	10.50	13.12	21.43
	1:05:00	0.00	0.00	3.79	4.90	5.76	8.18	9.55	12.14	19.87
	1:10:00	0.00	0.00	3.40	4.52	5.34	7.30	8.50	10.66	17.36
	1:15:00	0.00	0.00	3.10	4.20	5.08	6.53	7.56	9.30	15.07
	1:20:00	0.00	0.00	2.88	3.91	4.79	5.87	6.79	8.12	13.12
	1:25:00	0.00	0.00	2.68	3.65	4.40	5.34	6.16	7.17	11.53
	1:30:00	0.00	0.00	2.51	3.42	4.04	4.80	5.54	6.36	10.17
	1:35:00	0.00	0.00	2.33	3.18	3.70	4.31	4.96	5.64	8.95
	1:40:00	0.00	0.00	2.16	2.86	3.38	3.85	4.42	4.97	7.82
	1:45:00	0.00	0.00	1.99	2.54	3.07	3.42	3.91	4.32	6.75
	1:50:00	0.00	0.00	1.83	2.24	2.78	3.01	3.43	3.73	5.77
	1:55:00	0.00	0.00	1.58	2.00	2.51	2.64	2.99	3.20	4.89
	2:00:00	0.00	0.00	1.39	1.81	2.26	2.33	2.63	2.74	4.14
	2:05:00	0.00	0.00	1.14	1.49	1.87	1.86	2.10	2.16	3.25
	2:10:00	0.00	0.00	0.93	1.22	1.53	1.49	1.67	1.70	2.55
	2:15:00	0.00	0.00	0.76	0.99	1.25	1.19	1.34	1.34	2.00
	2:20:00	0.00	0.00	0.61	0.80	1.02	0.95	1.07	1.05	1.56
	2:25:00	0.00	0.00	0.50	0.65	0.82	0.76	0.86	0.83	1.22
	2:30:00	0.00	0.00	0.40	0.52	0.66	0.61	0.68	0.65	0.94
	2:35:00	0.00	0.00	0.32	0.41	0.52	0.48	0.54	0.50	0.72
	2:40:00	0.00	0.00	0.25	0.32	0.40	0.37	0.42	0.39	0.56
	2:45:00	0.00	0.00	0.20	0.25	0.32	0.29	0.32	0.30	0.44
	2:50:00	0.00	0.00	0.16	0.20	0.25	0.23	0.26	0.24	0.35
	2:55:00	0.00	0.00	0.12	0.15	0.19	0.18	0.20	0.19	0.27
	3:00:00	0.00	0.00	0.09	0.11	0.14	0.14	0.15	0.14	0.21
	3:05:00	0.00	0.00	0.06	0.08	0.10	0.10	0.11	0.10	0.15
	3:10:00	0.00	0.00	0.04	0.05	0.07	0.07	0.07	0.07	0.10
	3:15:00	0.00	0.00	0.02	0.03	0.04	0.04	0.05	0.04	0.06
	3:20:00	0.00	0.00	0.01	0.02	0.02	0.02	0.02	0.02	0.03
	3:25:00	0.00	0.00	0.00	0.01	0.01	0.01	0.01	0.01	0.01
	3:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
4:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
4:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
4:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
4:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
4:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
4:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
4:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
4:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
4:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
5:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
5:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	



## **APPENDIX E – REFERENCE MATERIAL**

Final Drainage Report  
for  
**The Sanctuary Filing 1**  
at  
**Meridian Ranch**



**MERIDIAN RANCH**

A GOLF & RECREATIONAL COMMUNITY

EL PASO COUNTY, COLORADO

August 2022

Prepared For:

**GTL DEVELOPMENT, INC.**  
**P.O. Box 80036**  
**San Diego, CA 92138**

Prepared By:

Tech Contractors  
11910 Tourmaline Dr., Ste 130  
Falcon, CO 80831  
719.495.7444

PCD Project No. SF22-020

## Future Drainage - SCS Calculation Method

Following is a tabulation of the surface drainage characteristics for the future conditions using the SCS calculation method. Please refer to Figure 6 - Meridian Ranch SCS Calculations – Future Basins Map

**Table 5: Future Drainage Basins-SCS**

FUTURE SCS (Full Spectrum)						
	DRAINAGE AREA (SQ. MI.)	PEAK DISCHARGE Q100 (CFS)	PEAK DISCHARGE Q50 (CFS)	PEAK DISCHARGE Q10 (CFS)	PEAK DISCHARGE Q5 (CFS)	PEAK DISCHARGE Q2 (CFS)
OS06	0.1313	80	52	12	3.8	0.5
G1a	0.1313	80	52	12	3.8	0.5
G1a-G2	0.1313	79	52	11	3.7	0.5
OS05	0.0578	39	26	5.6	1.8	0.2
OS05-G1	0.0578	39	25	5.5	1.7	0.2
FG01	0.0538	31	22	7.0	3.4	0.9
FG01-G1	0.0538	31	22	7.0	3.4	0.9
G1	0.1116	61	41	11	4.9	1.1
G1-G2	0.1116	61	41	11	4.8	1.1
FG02	0.0391	32	22	6.4	2.7	0.5
G2	0.2820	167	112	27	10	1.9
G2-G3	0.2820	163	108	27	10	1.9
FG03	0.0203	24	17	5.9	3.0	0.8
FG04	0.0172	22	16	5.8	3.1	0.9
G3	0.3195	185	123	31	12	2.4
FG06	0.0675	56	40	12	5.8	1.3
FG05	0.0580	45	33	12	6.7	2.4
OS07ab	0.0170	12	7.9	1.8	0.5	0.07
OS07ab-POND F	0.0170	12	7.6	1.7	0.5	0.07
POND F IN	0.4620	293	200	54	23	5.1
POND F	0.4620	178	121	16	8.0	2.1
POND F-G7	0.4620	177	120	16	8.0	2.1
OS07c	0.0296	19	12	2.7	0.9	0.12
OS07c-G4	0.0296	19	12	2.6	0.9	0.12
FG21a	0.0095	5.9	4.0	1.0	0.4	0.06
G4	0.0391	25	16	3.6	1.2	0.2
G4-G7	0.0391	24	16	3.5	1.2	0.2
FG21b	0.0150	21	16	6.5	3.9	1.7
G7	0.5161	194	131	18	8.9	2.3
G7-G8	0.5161	194	131	18	8.9	2.3
FG22	0.1354	121	88	32	17	5.4
OS08a	0.0251	16	11	2.3	0.7	0.10
OS08-G8	0.0251	16	10	2.3	0.7	0.10
FG23a	0.0216	21	15	5.2	2.7	0.8
OS07d	0.0034	2.5	1.6	0.4	0.11	0.01
OS07d-G8	0.0034	2.4	1.6	0.3	0.11	0.01
G8	0.7016	279	178	46	24	7.7
G8-G10	0.7016	278	177	45	24	7.6
FG24b	0.0589	76	57	24	15	6.5
FG24a	0.0348	24	16	4.5	2.0	0.4
OS08b	0.0165	9.5	6.3	1.4	0.5	0.07
OS08b-G9a	0.0165	9.4	6.0	1.4	0.5	0.07
OS09a	0.0093	5.3	3.5	0.8	0.3	0.04
OS09a-G9a	0.0093	5.2	3.4	0.7	0.3	0.04
G9a	0.1195	97	71	28	16	6.7

FUTURE SCS (Full Spectrum)						
	DRAINAGE AREA (SQ. MI.)	PEAK DISCHARGE Q100 (CFS)	PEAK DISCHARGE Q50 (CFS)	PEAK DISCHARGE Q10 (CFS)	PEAK DISCHARGE Q5 (CFS)	PEAK DISCHARGE Q2 (CFS)
G9a-G9b	0.1195	96	70	27	16	6.6
FG24c	0.0291	40	30	13	8.4	4.0
FG24d	0.0262	39	30	14	8.7	4.4
G9b	0.1748	170	127	53	32	14
REX RD WQCV	0.1748	158	125	51	31	14
G9b-G10	0.1748	158	123	50	31	13
FG23b	0.0236	17	11	2.7	0.9	0.13
G10	0.9000	390	263	90	46	15
G10-G11	0.9000	389	254	85	44	15
FG23c	0.0109	11	7.6	2.2	1.0	0.2
G11	0.9109	393	258	86	44	15
FG25	0.1084	111	84	36	22	9.9
FG28	0.0184	15	10	3.0	1.2	0.2
POND G IN-WEST	1.0377	503	350	122	63	22
FG27	0.0679	98	79	42	30	18
FG26	0.0570	65	50	24	16	8.2
G13	0.0570	65	50	24	16	8.2
G13-POND G	0.0570	64	50	24	16	8.1
POND G IN-EAST	0.1249	160	127	64	44	25
POND G	1.1626	450	293	52	21	5.3
G12	1.1626	450	293	52	21	5.3
G12-G06	1.1626	449	293	52	21	5.3
FG29	0.0983	60	39	8.9	2.9	0.4
FG32	0.0402	51	40	20	14	7.5
FG32-G06	0.0402	50	40	19	13	7.4
G06	1.3011	491	317	57	22	7.5

***Rational Calculations***

The Rational Hydrologic Calculation Method was used to estimate the total runoff from the 5-year and the 100-year design storm and thus establish the storm drainage system design. Using the rational calculation methodology outlined in the Hydrology Section (Ch 6) of the COSDCM coupled with the El Paso County EPCDCM an effective storm drainage design for the Sanctuary Filing 1 has been designed. The storm drainage facilities have been designed such that the minor storm will be captured by the inlets and conveyed by the storm drain pipes such that the street flow does not overtop the curbs. The storm drainage facility has been designed such that the major storm will be captured by the inlets and conveyed by the storm drain pipes such that the street flow does not exceed the right-of-way widths for residential streets and the hydraulic grade line will be less than one foot below the surface.

The site is located within the Gieck Ranch Drainage Basin. The storm drain runoff will be collected by a series of inlets and storm drain pipe then conveyed through the project and discharge directly into the existing Pond G that is properly sized to safely convey the storm water flows away from the project without damaging adjacent property.

***Rational Narrative***

The following is a detailed narrative of the storm drainage system located in the Sanctuary Filing 1. These storm drainage systems meet the requirements of as found in the El Paso

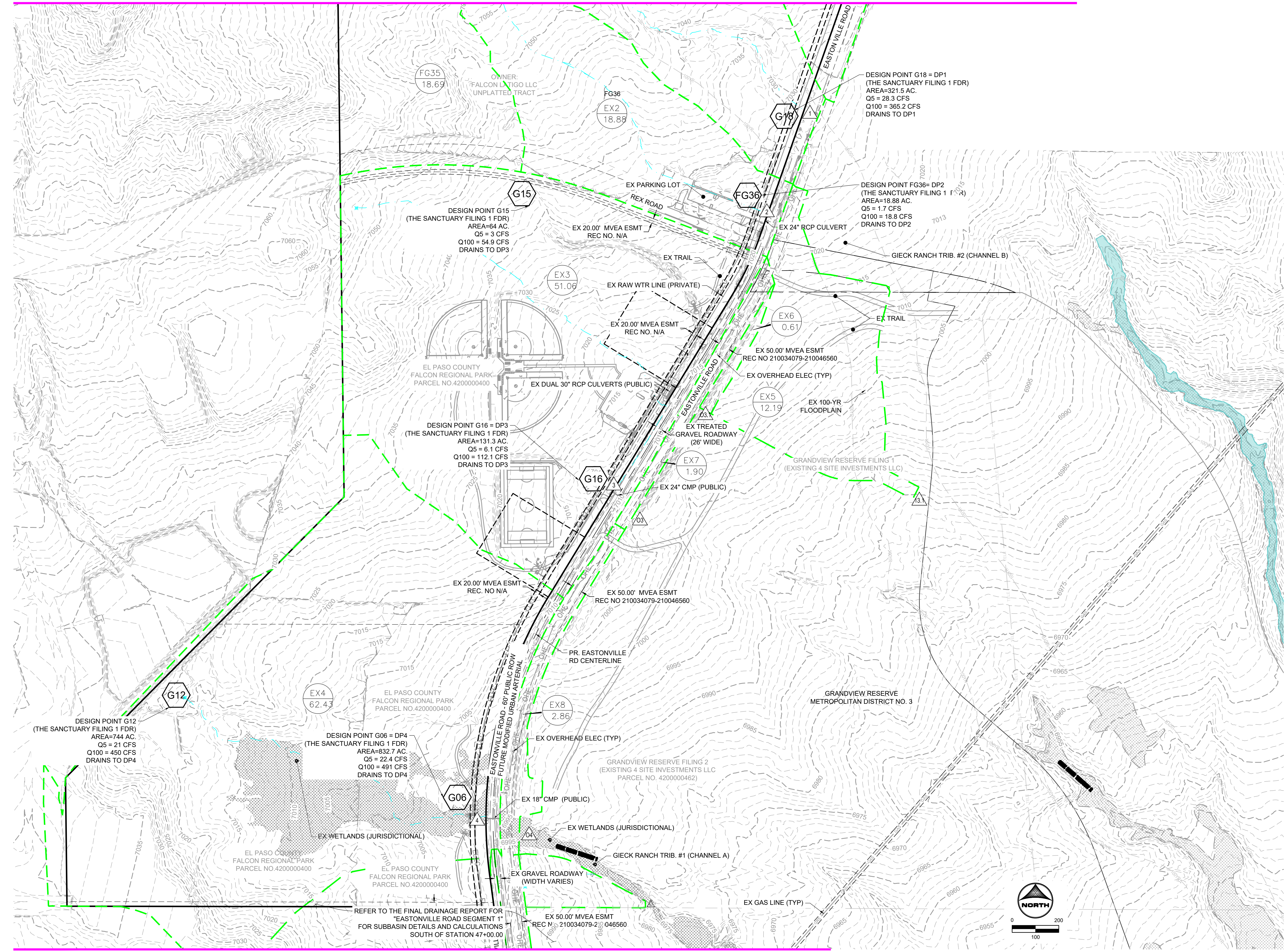






## **APPENDIX F – DRAINAGE MAPS**





**LEGEND:**

- EXISTING MAJOR CONTOUR: --- 5250 ---
- EXISTING MINOR CONTOUR: --- ---
- EX STORM SEWER: ————
- EX DRAINAGE SWALE: ————
- EX PROPERTY LINE: ————
- EXISTING FLOW DIRECTION: ←
- PROPOSED DRAINAGE BASIN: - - - -
- DESIGN POINT: ▲
- PROPOSED BASIN LABEL: (NAME / AREA)
- DESIGN POINT PER THE SANCTUARY FILING 1 FDR: GXX

**SUMMARY RUNOFF TABLE**

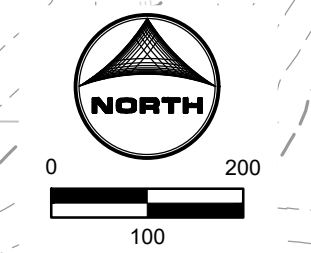
BASIN	AREA (ac)	% IMPERVIOUS	Q <sub>s</sub> (cfs)	Q <sub>100</sub> (cfs)
G18*	321.53	-	28.3	365.2
FG36*	18.88	-	1.7	18.8
G16*	131.26	-	6.1	112.1
G06*	832.70	-	22.4	491.0
EX5	12.19	2	2.7	18.0
EX6	0.61	2	0.1	0.9
EX7	1.90	2	0.4	2.5
EX8	2.86	2	0.6	4.0

\* AREA AND Q TAKEN FROM THE SANCTUARY FILING 1 FDR

**DESIGN POINT SUMMARY TABLE**

DESIGN POINT	CONTRIBUTING BASINS	ΣQ <sub>s</sub> (cfs)	ΣQ <sub>100</sub> (cfs)
1	G18*	28.3	365.2
2	FG36*	1.7	18.8
3	G16*	6.1	112.1
4	G06*	22.4	491.0
O3	EX7	6.5	114.6
O3.1	EX7	0.1	0.9
O4	EX7	23.0	495.0
13.1	EX7	2.7	18.0

\* AREA AND Q TAKEN FROM THE SANCTUARY FILING 1 FDR



REFER TO EASTONVILLE ROAD SEGMENT 1 FDR

DRAWN BY: SPC JOB DATE: 8/28/2024  
 APPROVED: CM JOB NUMBER: 201662.08  
 CAD DATE: 8/28/2024  
 CAD FILE: J:\2020\201662\CAD\Drawings\Eastonville\_Road\_662.08\Drainage\201662.08\_FDR\_map\_ex\_Seg1

NO.	DATE	BY	REVISION DESCRIPTION

HR GREEN - COLORADO SPRINGS  
 1975 RESEARCH PKWY SUITE 230  
 COLORADO SPRINGS CO 80920  
 PHONE: 719.300.4140  
 FAX: 713.965.0044

EASTONVILLE ROAD  
 D.R. HORTON  
 EL PASO COUNTY, CO



EXISTING CONDITIONS - DRAINAGE MAP  
 SHEET DRN 1

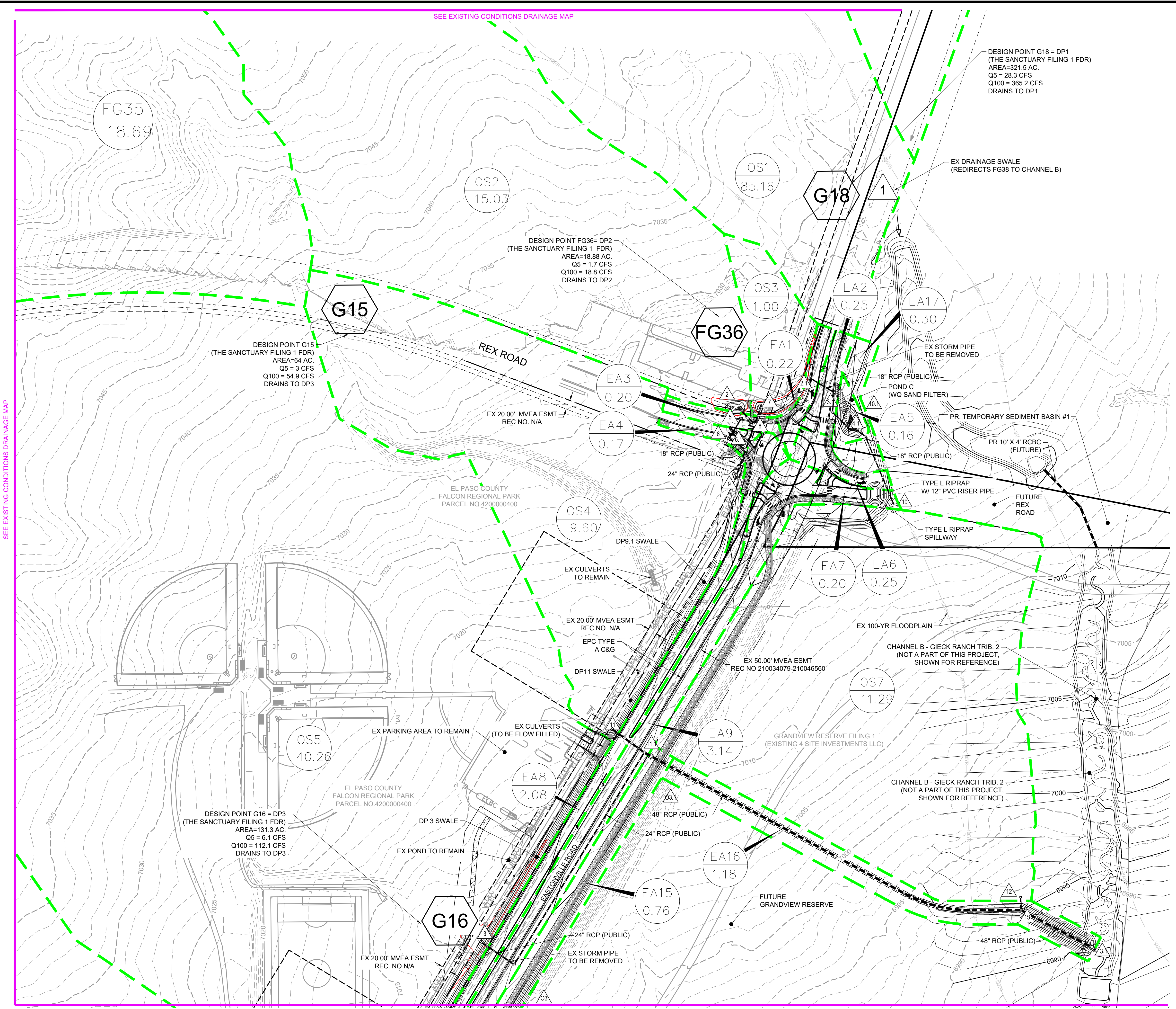












**LEGEND:**

- PROPOSED MAJOR CONTOUR — 5250 —
- PROPOSED MINOR CONTOUR - - - 5250 - - -
- EXISTING MAJOR CONTOUR — 5250 —
- EXISTING MINOR CONTOUR - - - 5250 - - -
- PROPOSED STORM SEWER ———
- PROPOSED DRAINAGE SWALE ———
- PROPERTY LINE ———
- PROPOSED FLOW DIRECTION ———
- EXISTING FLOW DIRECTION ———
- PROPOSED DRAINAGE BASIN ———
- DESIGN POINT ———
- PROPOSED BASIN LABEL ———
- PRELIMINARY 100-YR FLOODPLAIN ———
- WETLANDS ———
- DESIGN POINT PER MERIDIAN RANCH ———

**SUMMARY RUNOFF TABLE**

BASIN	AREA (ac)	% IMPERVIOUS	Q5 (cfs)	Q100 (cfs)
EA1	0.22	73	0.8	1.5
EA2	0.25	72	0.9	1.7
EA3	0.20	70	0.7	1.3
EA4	0.17	65	0.5	1.1
EA5	0.16	0	0.1	0.4
EA6	0.25	76	0.8	1.4
EA7	0.20	50	0.4	1.0
EA8	2.08	99	5.2	8.8
EA9	3.14	60	5.0	10.6
EA10	0.16	75	0.6	1.1
EA11	0.15	67	0.5	1.0
EA12	0.34	0	0.1	1.0
EA13	0.45	73	1.4	2.8
EA14	1.48	21	1.2	3.8
EA15	0.76	24	0.7	2.1
EA16	1.18	0	0.3	2.5
EA17	0.30	0	0.1	0.7
*G18	321.53	-	28.3	365.2
*FG36	18.88	-	1.7	18.8
OS3	1.00	2	0.3	2.2
OS4	9.60	9	4.8	21.6
*G16	131.26	-	6.1	112.1
*G06	832.70	-	22.4	491.0
OS7	11.29	3	3.9	24.6

\*AREA AND Q TAKEN FROM THE SANCTUARY FILING 1 FDR

**DESIGN POINT SUMMARY TABLE**

DESIGN POINT	CONTRIBUTING BASINS	Q5 (cfs)	Q100 (cfs)
1	G18	28.3	365.2
2	FG36	1.7	18.8
2.1	EA1	0.8	1.5
3	G16	6.1	112.1
3.1	EA2, DP2.1	1.6	3.2
4	G06	22.4	491.0
4.1	EA5, DP3.1	1.7	3.4
5	EA3	0.7	1.3
6	DP5, EA4	1.2	2.4
6.1	DP6, DP8	2.9	22.4
7	OS3	0.3	2.2
8	DP2, DP7	2.0	21.0
9	DP6.1	2.9	22.4
10	EA6, EA7	1.2	2.3
11	OS4, DP9	7.5	44.0
12	OS7	3.9	24.6
13	DP11.1, DP12	10.0	180.6
14	EA8	5.2	8.8
15	EA9	5.0	10.6
15.1	DP14, DP15	10.2	19.3
16.1	EA10	0.6	1.1
17.1	EA11	0.5	1.0
O3	EA15	0.7	2.1
O3.1	-	0.0	0.0
O4	EA12, DP4	22.5	492.0
O4.1	EA13	1.4	2.8
O4.2	EA14	1.2	3.8
10.1	EA17	0.1	0.7
11.1	DP3, DP11	13.6	156.1
13.1	EA16, DP13	0.3	183.1

DRAWN BY: SPC JOB DATE: 8/28/2024  
 APPROVED: CM JOB NUMBER: 201662.08  
 CAD DATE: 8/28/2024  
 CAD FILE: J:\2020\201662\CAD\DWG\C\Eastonville\_Road\_662.08\Drainage\201662.08\_FDR\_map\_Seg2.dwg

NO.	DATE	BY	REVISION DESCRIPTION

**HRGreen**  
 HR GREEN - COLORADO SPRINGS  
 1975 RESEARCH PKWY SUITE 230  
 COLORADO SPRINGS CO 80920  
 PHONE: 719.300.4140  
 FAX: 713.965.0044

EASTONVILLE ROAD  
 D.R. HORTON  
 EL PASO COUNTY, CO



PROPOSED CONDITIONS - DRAINAGE MAP  
 SHEET DRN 2