Preliminary & Final Drainage Report  $_{for}$ 

# Rex Road

through Falcon Regional Park



EL PASO COUNTY, COLORADO

May 2023

Prepared For:

# GTL DEVELOPMENT, INC. P.O. Box 80036 San Diego, CA 92138

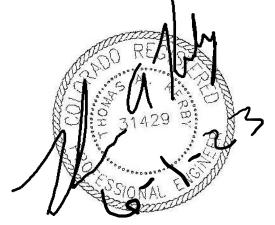
Prepared By: Tech Contractors 11910 Tourmaline Dr., Ste 130 Falcon, CO 80831 719.495.7444

PCD Project No. CDR236

# CERTIFICATIONS

# Design Engineer's Statement:

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the County for drainage reports and said report is in conformity with the applicable master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.



Thomas A. Kerby, P.E. #31429

# **Owner/Developer's Statement:**

I, the owner/developer have read and will comply with all of the requirements specified in this drainage report and plan.

íce D Raul Guzman, V

<u>6/5/2023</u>

# GTL Development, ine P.O. Box 80036 San Diego, CA 92138

# El Paso County:

Filed in accordance with the requirements of the Drainage Criteria Manual, Volumes 1 & 2, El Paso County Engineering Criteria Manual and Land Development Code as amended.

Joshua Palmer, P.E.
County Engineer / ECM Administrator

Date

# **Rex Road Preliminary/Final Drainage Report**

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# EXECUTIVE SUMMARY

The purpose of the following Preliminary/Final Drainage Report (PDR/FDR) is to present the changes to the drainage patterns as a result of constructing the extension of Rex Road through Falcon Regional Park from Meridian Ranch to Eastonville Road. Runoff quantities and proposed facilities have been calculated using the current City of Colorado Springs/El Paso County Drainage Criteria Manual (DCM) (1994 version) and portions of the City of Colorado Springs Drainage Criteria Manual, Volume 1 (DCM-1) ((2014 version) as amended by the El Paso County Engineering Criteria Manual (ECM).

This report based on the current version of the Meridian Ranch Sketch Plan amendment as adopted by the El Paso County Board of Commissioners on August 5, 2021. Hydrologic calculations follow method outlined in Chapter 6 of the 2014 version of the City of Colorado Springs Drainage Criteria Manual (COSDCM) as adopted by the El Paso County Board of County Commissioners by Resolution 15-042. Chapter 6 addresses the hydrologic calculation methods and includes an updated hydrograph to be used with storm drainage runoff. The Board adopted by the same resolution, Section 3.2.1 of Chapter 13 of the COSDCM referencing Full Spectrum Detention; the concept "provides better control of the full range of runoff rates that pass through detention facilities than the convention multi-stage concept. This section of the COSDCM identifies the necessity to provide full spectrum detention but does not prescribe a methodology to reach such the detention requirements. This report includes hydrologic models from HEC-HMS for the historic, interim and future conditions for the 2-yr, 5-yr, 10-yr, 25-yr, 50-yr, and 100-yr design storm frequencies. The interim and the future conditions include the existing detention facilities sized and modeled such that "frequent and infrequent inflows are released at rates approximating undeveloped conditions."

The Rex Road extension is approximately <sup>1</sup>/<sub>4</sub> mile long between Meridian Ranch on the west and Eastonville Road on the east, is approximately 4.2 acres and is located within the Falcon Regional Park in Section 21, Township 12 South, Range 64 West of the 6<sup>th</sup> Principal Meridian. It is approximately 12 miles northeast of the city of Colorado Springs, 2.5 miles north of the unincorporated town of Falcon.

This segment of Rex Road is located within Gieck Ranch Drainage Basin. The Gieck Ranch Basin has been studied, but has not received final approval from El Paso County.

Based on the aforementioned design parameters the construction of the project will not adversely affect downstream properties.

# **INTRODUCTION**

# Purpose

The purpose of the following Preliminary/Final Drainage Report (PDR/FDR) is to present proposed changes to the drainage patterns as a result of the construction of Rex Road. The report outlines and compares the calculated post construction flows with those of allowable exiting runoff discharge.

# Scope

The scope of this report includes:

- Location and description of the proposed development stating the proposed land use, density, acreage and adjacent features to the site.
- Calculations for design peak flows from all off-site tributary drainage areas.
- Calculations for design peak flows within the proposed project area for all drainage areas.
- Discussion of major drainage facilities required as a result of the development.
- Discussion and analysis of existing and proposed facilities.

Runoff quantities and proposed facilities have been calculated using the current City of Colorado Springs/El Paso County Drainage Criteria Manual (DCM) (1994 version) and those portions of the City of Colorado Springs Drainage Criteria Manual, Volume 1 (DCM-1) ((2014 version) adopted by Resolution 15-042 of the El Paso County Board of County Commissioners as amended by the El Paso County Engineering Criteria Manual (ECM).

# Background

On November 16, 2000 the El Paso County Board of County Commissioners approved the rezoning of the Meridian Ranch project (PUD-00-010) from A-35 to PUD with several conditions. Condition number seven stated in part that "drainage plans shall release and/or retain at approximately eighty percent (80%) of historic rates." At the time of the initial approvals there were no drainage improvements downstream of the Meridian Ranch project and the existing natural channels were shallow and undefined.

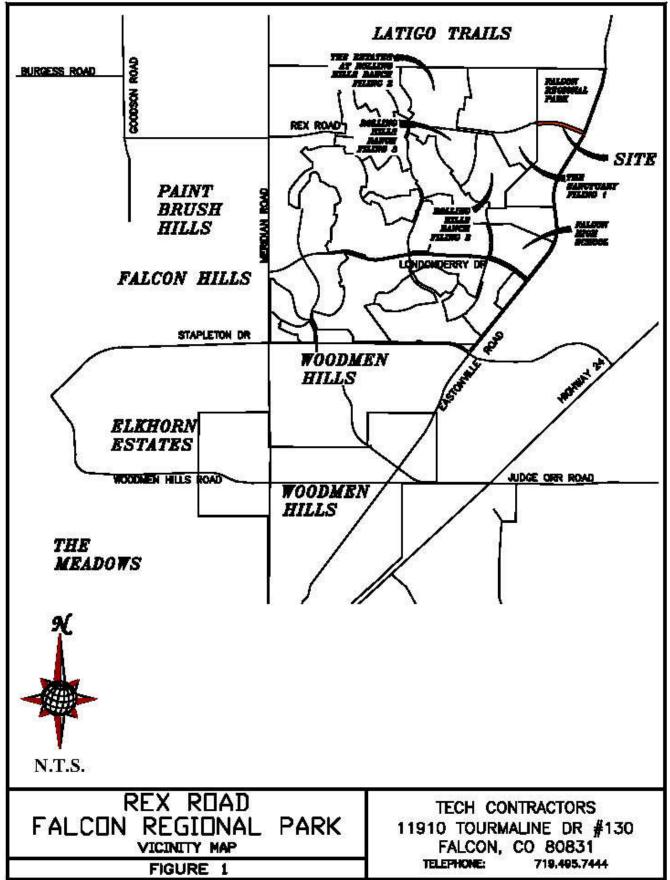
The Sketch Plan Amendment (SKP-21-003) was processed and approved in 2021 by the El Paso County Board of County Commissioners by Resolution 21-332 for Meridian Ranch. The resolution eliminated the required restriction of 80% of historic peak flow rates mentioned above. The drainage patterns proposed with this project will cause peak flow rates to approximate the historic peak flow rates as per the current El Paso County stormwater requirements.

No development has occurred downstream of Eastonville Road, however the approved Meridian Ranch MDDP and this report indicate the Eastonville Road culvert crossing located downstream of this project does not provide enough capacity for the historic flow rates. It is anticipated that this culvert will be replaced with the Eastonville Road construction proposed by El Paso County.

Current calculations show the future design discharge flow rates across Eastonville Road to be below historic flow rates at full buildout for the full spectrum of design storms.

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Figure 1: Vicinity Map



# EXISTING CONDITIONS

# **General** Location

The Rex Road extension project is approximately <sup>1</sup>/<sub>4</sub> mile long located between Meridian Ranch on the west and Eastonville Road on the east, is approximately 4.2 acres and is located in Section 21, Township 12 South, Range 64 West of the 6<sup>th</sup> Principal Meridian. It is approximately 12 miles northeast of the city of Colorado Springs, 2.5 miles north of the unincorporated town of Falcon, and immediately north of the Woodmen Hills development.

# Land Use

Historically, ranching dominated the area surrounding Meridian Ranch; however, currently urbanization has occurred in the general vicinity. Most notably, urbanization is occurring to the north with Latigo Trails, to the south and west the Meridian Ranch Subdivisions, and to the east in Grandview Reserve. The current and proposed land use surrounding the project is open space/ regional park. There are no existing utilities except buried electrical feed owned by Mountain View Electric.

A shallow swale traverses the site from northwest to southeast providing drainage for areas north of the project and carries the flow way from the site toward Eastonville Road.

# Climate

Mild summers and winter, light precipitation; high evaporation and moderately high wind velocities characterize the climate of the study area. The average annual monthly temperature is 48.4 F with an average monthly low of 30.3 F in the winter and an average monthly high of 68.1 F in the summer. Two years in ten will have maximum temperature higher than 98 F and a minimum temperature lower than -16 F. Precipitation averages 15.73" annually, with 80% of this occurring during the months of April through September. The average annual Class A pan evaporation is 45 inches. (Soil Survey of El Paso County Area, Colorado).

# Topography and Floodplains

The topography of the site is typical of a high desert, short prairie grass (approximately 60% vegetative cover) with relatively flat slopes generally ranging from 2% to 4%. The project site drains generally from the northwest to southeast and is tributary to the Black Squirrel Creek. There are no trees or brush located on the project site.

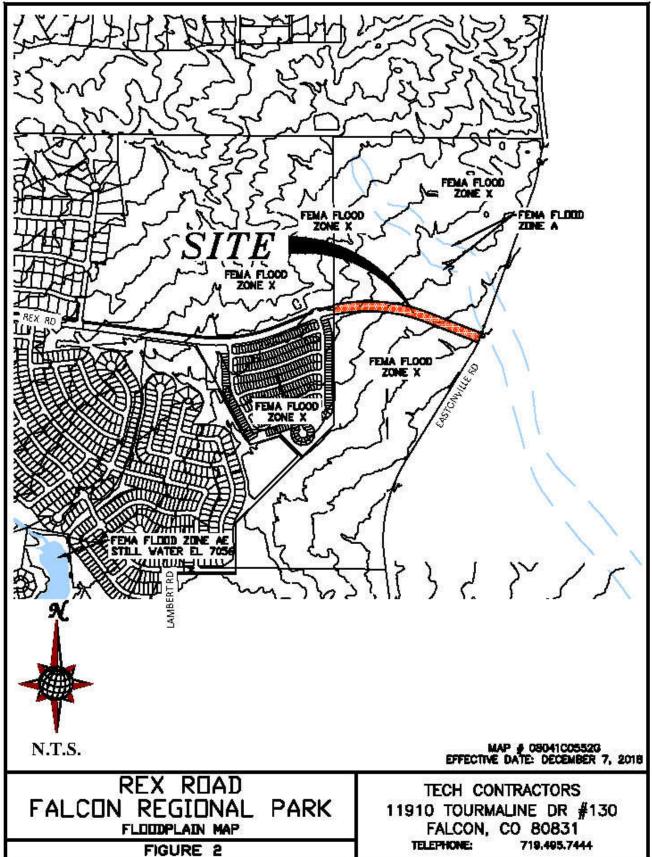
The Flood Insurance Rate Maps (FIRM No. 08041C0552G dated 12/07/2018) indicates that the project is outside of any designated flood plain. Please see Figure 2: The Sanctuary Federal Emergency Management Agency (FEMA) Floodplain Map.

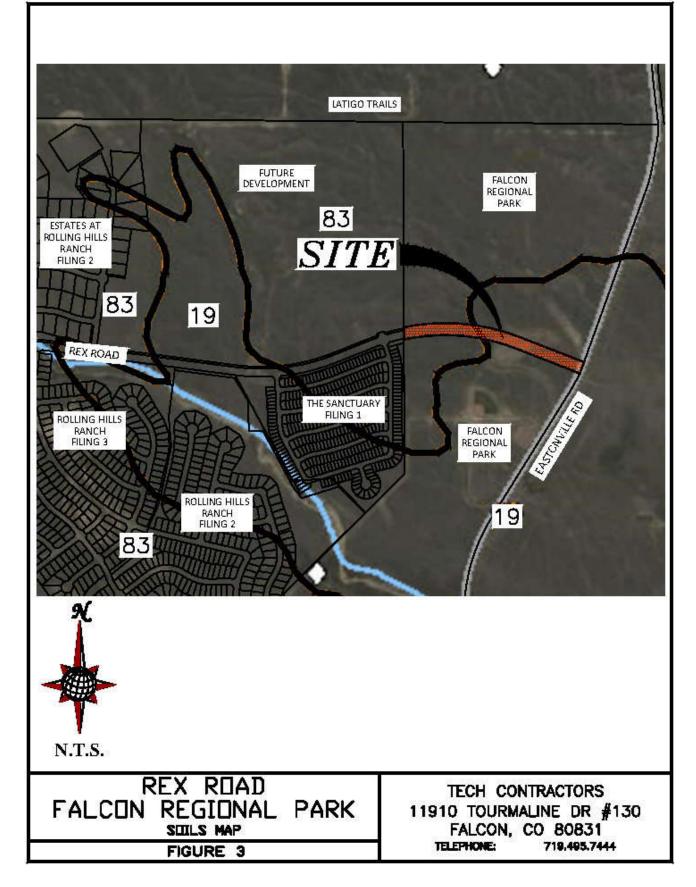
# Geology

The National Resources Conservation Service (NRCS) soil survey records indicate that the service area is predominately covered by soils classified in the Columbine (3.0 ac.) and Stapleton series (2.1 ac.). These series are categorized in the Hydrological Soil Groups A & B.

The Stapleton (83) sandy loam is a deep, non-calcareous, well-drained soil formed in alluvium derived from arkosic bedrock on uplands. Permeability of this soil is rapid. Available water

Figure 2: FEMA Floodplain Map





capacity is moderate, surface runoff is slow, and the hazard of erosion and soil blowing is moderate. The Stapleton series is categorized as a Hydrological Soil Group B.

This soil is used mainly for grazing livestock, for wildlife habitat and for home sites. The main limitation of this soil for urban development is a hazard of flooding in some areas.

This soil is suited to habitat for open land and rangeland wildlife. The main limitation of this soil for urban development is frost-action potential.

Typically, these soils are well-drained, gravelly sandy loams that form on alluvial terraces and fans and exhibit high permeability and low available water capacity with depth to bedrock greater than 6 feet.

The Columbine (19) gravelly sandy loam is a deep, well-drained to excessively drained soil formed in coarse textured material on alluvial terraces, fans and flood plains. Permeability of this soil is very rapid. Available water capacity is low to moderate, surface runoff is slow, and the hazard of erosion is slight to moderate. The Columbine series is categorized as a Hydrological Soil Group A.

This soil is used mainly for grazing livestock, for wildlife habitat and for home sites. The main limitation of this soil for urban development is a hazard of flooding in some areas.

Note: (#) indicates Soil Conservation Survey soil classification number. See Figure 3 the Sanctuary Filing 1 – Soils Map.

# Natural Hazards Analysis

Natural hazards analysis indicates that no unusual surface or subsurface hazards are located near the vicinity. However, because the soils are cohesionless, sloughing of steep banks during drilling and/or excavation could occur. By citing improvements in a manner that provides an opportunity to lay the banks of excavations back at a 1:1 slope during construction, the problems associated with sloughing soils can be minimized.

# DRAINAGE BASINS AND SUB-BASINS

The site is near the top of the Gieck Ranch Drainage Basin and accepts flow from areas north of the extension of Rex Road within undeveloped areas of Meridian Ranch and portions of the Latigo development.

Two different scenarios were analyzed for the drainage conditions for the project.

The first scenario analyzes the historic conditions for the area. This condition has project site and tributary area in the pre-development state; where the tributary and downstream areas were modeled in its undeveloped, undisturbed condition, alternatively called the historic condition.

The second scenario is the proposed conditions scenario and it consists of the current existing conditions for the tributary areas whether developed or undeveloped/historic with the addition of the Rex Road extension in the proposed developed condition. The current existing

conditions assume all approved projects tributary to the project are at full buildout. This condition was analyzed to ensure that the historic flow rates are approximated at the culverts crossing Eastonville Road.

The future final scenario has not been included with this report as the future design of the remainder of Rex Road is to be designed by others. No design specifics have been made available for the future intersection of Rex Road and Eastonville Road. The future build out conditions for the areas tributary and downstream of the project could not be modeled accurately to ensure the storm drain peak flow rate and design at the Eastonville Rd crossing locations downstream of this project approximate the peak historic flow rates.

# DRAINAGE DESIGN CRITERIA

# SCS Hydrograph Procedure

The US Army Corp of Engineers HEC-HMS computer program was used to model the Soil Conservation Service (SCS) Hydrograph procedure to determine final design parameters for the major drainage facilities within the project. Onsite basin areas were calculated using aerial topography of the site and approved final design data. Times of concentration were estimated using the SCS procedures described in the DCM. Based upon the hydrologic soil type, the natural conditions found in the basins and the runoff curve numbers (CN) chart from Table 6-10 of the City of Colorado Springs DCM for Antecedent Runoff Condition II (ARC II), the following CN values were used for the given conditions.

Table 1:	SCS	Runoff	Curve	Numbers
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Condition	CN*	School	80
Residential Lots (5 acre)	63	Parks/Open Space	62
Residential Lots (2.5 acre)	66	Commercial	85
Residential Lots (1 acre)	68	Roadways	98
Residential Lots (1/2 acre)	70	Graded	67
Residential Lots (1/3 acre)	72	Golf Course	62
Residential Lots (1/4 acre)	75	Latigo Undeveloped	65
Residential Lots (1/5 acre)	78	Undeveloped	61
Residential Lots (1/6 acre)	80	-	

\*Curve Numbers were interpolated and based on amount of impervious area per lot. The 24 hour storm precipitation values were selected from the NOAA Atlas 14, Volume 8, Version 2 for the Meridian Ranch location (Latitude 38.9783°, Longitude -104.5842°, Elevation 7054 ft). These numbers along with SCS information were used as input to the U.S. Army Corp of Engineers HEC-HMS computer model to determine design runoffs. See the table for all the design storm events in Appendix A. These numbers along with SCS information were used as input to the U.S. Army Corp of Engineers HEC-HMS computer model to determine design runoffs.

# Full Spectrum Design

No detention facilities are proposed with this project. Areas tributary that are located within Meridian Ranch have been graded such that the runoff is conveyed away from and around the Falcon Regional Park. Water quality for the proposed roadway improvements will be achieved by directing the surface flow from the roadway platform to existing natural swales south of Rex Rd. and directed toward a proposed bioretention basin.

# DRAINAGE CALCULATIONS

Provide the EDARP Filing number for reference.

# SCS General Overview

The project is located within the Gieck Ranch Drainage Basin; storm water runoff will be conveyed overland across the Regional Park natural swales or carried by proposed curb and gutter in a southeasterly direction towards existing Eastonville Road.

The bulk of historic overland flows from within Meridian Ranch have been directed away from the Falcon Regional Park to be kept within Meridian Ranch and conveyed to the existing Pond G detention facility. See approved preliminary and final drainage reports associated with the Rolling Hills Ranch and the Sanctuary Filing 1 final plats and the Rolling Hills Ranch North Grading for more information regarding drainage within Meridian Ranch. The remaining mostly undeveloped flows from Latigo Trails, undeveloped Meridian Ranch Open Space and the Falcon Regional Park will continue within the natural grass lined swales approximately matching the historic flows for the full spectrum of design storms.

Figure 4: Rex Road SCS Calculations – Historic Conditions Map and Figure 5: Rex Road SCS Calculations – Proposed Conditions Map depict the historic and proposed general drainage patterns through the Regional Park across and under Rex Road toward Eastonville Road..

The purpose of this report is to show that the construction of Rex Road will not adversely impact the existing drainage facilities adjacent to and downstream of the proposed Rex Road construction.

# SCS Calculations

# Historic Drainage - SCS Calculation Method

Following is a tabulation of the surface drainage characteristics under Existing Conditions using the SCS calculation method. Please refer to Figure 4 - Rex Road SCS Calculations - Historic Basin Map.

	HISTORIC SCS (Full Spectrum)								
HYDROLOGIC ELEMENT	Drainage Area (SQ. Ml.)	Peak Discharge Q100 (CFS)	Peak Discharge Q50 (CFS)	Peak Discharge Q10 (CFS)	Peak Discharge Q5 (CFS)	Peak Discharge Q2 (CFS)			
HG14	0.2297	79	52	12	4.7	0.8			
HG13	0.1053	38	25	5.8	2.2	0.4			
G14	0.1053	38	25	5.8	2.2	0.4			
G14-G16	0.1053	37	25	5.8	2.2	0.4			
G16	0.3350	116	77	18	6.8	1.2			

 Table 2: Historic Drainage Basins – SCS

The project site drains generally from the northwest to southeast with relatively flat slopes generally ranging from 2% to 4%.

# Proposed Drainage - SCS Calculation Method

Following is a tabulation of the surface drainage characteristics for the proposed conditions using the SCS calculation method. Please refer to Figure 5 - Rex Road SCS Calculations - Proposed Basins Map

PROPOSED SCS (Full Spectrum)								
HYDROLOGIC ELEMENT	Drainage Area (SQ. Ml.)	Peak Discharge Q100 (CFS)	Peak Discharge Q50 (CFS)	Peak Discharge Q10 (CFS)	Peak Discharge Q5 (CFS)	Peak Discharge Q2 (CFS)		
OS09b	0.0435	22	14	3.2	1.1	0.2		
OS09b-G14	0.0435	22	14	3.2	1.1	0.2		
FG34	0.0275	20	13	3.3	1.3	0.2		
G14	0.0710	38	25	5.5	2.0	0.3		
G14-G15	0.0710	37	24	5.5	2.0	0.3		
FG35	0.0292	25	18	5.5	2.4	0.5		
G15	0.1002	55	36	8.0	3.0	0.6		
G15-G16	0.1002	54	35	8.0	3.0	0.6		
FG37	0.0754	46	31	7.3	2.7	0.4		
FG36	0.0295	19	13	3.9	1.8	0.4		
G15a	0.0295	19	13	3.9	1.8	0.4		
G15a-G16	0.0295	19	13	3.8	1.7	0.4		
G16	0.2051	114	74	16	6.5	1.2		

 Table 3: Future Drainage Basins-SCS

# Rational Calculations

The Rational Hydrologic Calculation Method was used to estimate the total runoff from the 5year and the 100-year design storm and thus establish the storm drainage system design for facilities with less than 100 acres if tributary area. Using the rational calculation methodology outlined in the Hydrology Section (Ch 6) of the COSDCM coupled with the El Paso County EPCDCM an effective drainage design for the Rex Road construction has been designed. The storm drainage facilities have been designed such that the minor storm will be conveyed such that the street flow does not overtop the curbs. The culvert undercrossing has been designed such that the major storm will be safely conveyed downstream under Rex Road.

The site is located within the Gieck Ranch Drainage Basin. The storm drain runoff will be collected by natural swales and conveyed southeasterly toward Eastonville Road and away from the project without damaging adjacent property.

# Rational Narrative

The following is a detailed narrative of the proposed storm drainage runoff tributary to Rex Road (see Figure 6 for more information). These storm drainage analysis meets the requirements as found in the El Paso County Engineering Criteria Manual I.7.1.C.5. (ECM) for storm water quality and discharge into Waters of the State. Discharge points are located on the south side of Rex Road (DP15 & DP15a).

- Basin OS9b (28 acres,  $Q_5$ = 5.0 CFS,  $Q_{100}$  = 34 CFS) contains off-site area north of Meridian Ranch within the future Latigo Trails subdivision entering Meridian Ranch via existing natural swale at Design Point 1. The surface runoff is collected into natural drainage swales and ultimately directed southerly through Meridian Ranch Basin FG34 to DP G14.
- Basin FG34 (18 acres,  $Q_5$ = 4.7 CFS,  $Q_{100}$  = 25 CFS) contains open space area within the future Rolling Hills Ranch North subdivision entering the Falcon Regional Park via a natural swale at Design Point G14. The surface runoff is collected into natural drainage swales and ultimately directed southerly to the Falcon Regional Park. The flow ( $Q_5$ = 7.5 CFS,  $Q_{100}$  = 46 CFS) is conveyed downstream via a natural swale to a proposed culvert at Rex Road (DP G15.1).
- Basin FG35a (14 acres,  $Q_5$ = 4.5 CFS,  $Q_{100}$  = 23 CFS) contains area within the Falcon Regional Park north of Rex Road. The surface runoff will sheet flow toward natural swales and is directed toward a proposed 36" RCP culvert under Rex Road located at DP G15.1. The total flow at the culvert ( $Q_5$ = 8.0 CFS,  $Q_{100}$  = 47 CFS) is conveyed downstream via a 36" RCP where the culvert flow is combined with runoff from Basin FG35b at Inlet I01.
- Basin FG35b (4.9 acres,  $Q_5 = 6.3$  CFS,  $Q_{100} = 17$  CFS) contains area north of Rex Rd and portions of Rex Road east of Meridian Ranch and west of the above mentioned 36" RCP culvert crossing. The surface runoff will sheet flow off the surrounding areas onto Rex Road and the flow will be directed to a proposed flow-by inlet (Inlet I01) and combined with the flow in the 36" RCP culvert. Most of the flow is captured ( $Q_5 = 5.2$ CFS,  $Q_{100} = 12$  CFS) with the remaining flow ( $Q_5 = 1.2$  CFS,  $Q_{100} = 5.3$  CFS) continuing downstream to Design Point G15a. The combined flow in the 30" RCP ( $Q_5 = 4.9$  CFS,  $Q_{100} = 23$  CFS) from Basin FG36a will continue downstream along a natural channel through Basin FG37.
- Basin FG36a (18 acres,  $Q_5=5.3$  CFS,  $Q_{100}=26$  CFS) contains Regional Park area north of Rex Road within the Falcon Regional Park west of Eastonville Road. The surface runoff flows to a natural swale toward a proposed 30" RCP culvert near the intersection of Rex Rd with Eastonville Rd. The culvert flow is conveyed downstream to DP15a.
- Basin FG36c (2.8 acres,  $Q_5=3.3$  CFS,  $Q_{100}=8.0$  CFS) contains area north of Rex Road within the Falcon Regional Park west of Eastonville Road. The surface runoff sheet flows onto Rex Rd. The surface runoff is combined with the by-pass flow from Inlet I01 and is carried eastward toward the intersection of Rex Rd with Eastonville Rd. Near the intersection the flow ( $Q_5=4.2$  CFS,  $Q_{100}=12$  CFS) is directed southerly via a down drain to DP15a where it is combined with the culvert flow from FG36a. The total flow ( $Q_5=8.0$  CFS,  $Q_{100}=32$  CFS) is directed to DP16a.
- Basin FG37 (48 acres,  $Q_5 = 10$  CFS,  $Q_{100} = 62$  CFS) contains area within the Falcon Regional Park south of Rex Rd. The surface flow from the area combines with the

runoff from the Rex Rd culvert crossings and is directed to the Eastonville Rd culvert crossing located at DP G16 ( $Q_5$ = 15 CFS,  $Q_{100}$  = 78 CFS).

# **DETENTION POND**

There are no existing or proposed detention ponds associated with this project. Any necessary water quality as a result of the construction of the extension of Rex Road through the Falcon Regional Park is provided via the drainage swales within the regional park.

DRAINAGE FEES Update once water quality design is finalized per the 6/6/23 coordination meeting.

The proposed project falls in the Gieck Ranch Drainage Basin and there are no drainage or bridge fees associated with the Gieck Ranch Drainage Basin and this is not a final plat.

The following is the imperviousness calculation:

	Acres	Assumed Imperviousness	Impervious Acres			
Open Space Right-of-way Residential Lots Total	0.0 4.2 0.0 4.2	3% 90% 65%	0.0 4.6 0.0 3.8=90% imperv.			
GIECK RANCH FEES: Drainage Fees: There are no drainage fees for this basin.						
Bridge I	Fees:	There are no bridge fees	for this basin.			

# **CONCLUSION**

The rational and SCS based hydrologic calculation methods were used to estimate the historic and developed runoff values to determine the impact of this extension of Rex Road on surrounding property. The resulting calculations were used to estimate the hydraulic impact on the existing natural drainage swales and proposed facilities.. Based on the aforementioned design parameters the extension of Rex Road will not adversely affect downstream properties as the resultant developed flow rates for the various design storms fall below the historic flow rates of the same storms.

Below is a comparison of various flow rates at key design points:

MERIDIAN RANCH DISCHARGE KEY DESIGN POINTS								
Proposed Conditions SCS Calculations		Peak Discharge Q100 (CFS)	Peak Discharge <sup>Q50</sup> (CFS)	Peak Discharge Q10 (CFS)	Peak Discharge <sup>Q5</sup> (CFS)	Peak Discharge Q2 (CFS)		
G14 - DISCHARGE POINT	Historic	38	25	5.8	2.2	0.4		
TO REGIONAL PARK	Proposed	38	25	5.5	2.0	0.3		
(G07 - HISTORIC)	% of Historic	100%	100%	95%	89%	85%		
	Historic	116	77	18	6.8	1.2		
G16 - EASTONVILLE RD <sup>1</sup> DOWNSTREAM OF REX RD	Proposed	114	74	16	6.5	1.2		
	% of Historic	98%	97%	89%	95%	99%		

<sup>1</sup> Flow rate at Eastonville Rd. listed for reference only

# EROSION CONTROL DESIGN

# **General Concept**

Historically, erosion on this property has been held to a minimum by a variety of natural features and agricultural practices including:

- Substantial prairie grass growth
- Construction of drainage arresting berms
- Construction of multiple stock ponds along drainage courses

During construction, best management practices (BMP) for erosion control will be employed based on El Paso County Criteria. BMP's will be utilized as deemed necessary by the contractor and/or engineer and are not limited to the measures shown on the construction drawing set. The contractor shall minimize the amount of area disturbed during all construction activities.

In general the following shall be applied in developing the sequence of major activities:

- Install down-slope and side-slope perimeter BMP's before the land disturbing activity occurs.
- Do not disturb an area until it is necessary for the construction activity to proceed
- Cover or stabilize as soon as possible.
- Time the construction activities to reduce the impacts from seasonal climatic changes or weather events.
- The construction of filtration BMP's should wait until the end of the construction project when upstream drainage areas have been stabilized.
- Do not remove the temporary perimeter controls until after all upstream areas are stabilized.

# Four Step Process

The following four step process is recommended for selecting structural BMP's in developing urban areas:

# **Step 1: Quantify Runoff Reduction**

The intent of this approach is to avoid the direct connection of impervious areas to the storm drain and instead, guide runoff from pavement and roofs to vegetated areas such as grass buffers and grass swales in a manner that maintains sheet flow conditions. The soil type in the vicinity of this project is conducive to infiltration.

This project is located within the Falcon Regional Park with minimal hardscape surfaces proposed. The project will include a standard right-of-way, half-width pavement section and sidewalk along the south side. Run-off from the street will be directed to adjacent grass lined swales and buffers to carry the stormwater downstream. The grass lined swales will reduce the need for larger water quality basins and provide some form of runoff reduction.

# Step 2: Stabilize Drainageways

The existing natural drainage swales traversing the area and located adjacent to the project will remain primarily in its natural state with a wide flat bottom and gentle slope reducing the velocity of the concentrated flow traveling along the drainageway.

# Step 3: Provide Water Quality Capture Volume (WQCV)

Bioretention is proposed near the southeast terminus of the project providing the necessary WQCV for the project minus the credits from runoff reduction.

# Step 4: Consider Need for Industrial and Commercial BMP's

This project is neither industrial nor commercial and therefore this section does not apply.

See Appendix D for more information.

# **Detention** Pond

There is no proposed detention pond associated with this project.

# Silt Fence and/or Straw Wattles

Straw Wattles or silt fence will be placed along downstream limits of disturbed areas. This will prevent suspended sediment from leaving the site during infrastructure construction. Silt fencing is to remain in place until vegetation is reestablished.

# Straw Wattles and/or Erosion Bales

Straw wattles or erosion bales will be placed ten (10) feet from the upstream end of all culverts during construction to prevent culverts from filling with sediment. Erosion wattles/bales will remain in place until vegetation is reestablished. Erosion checks will be used in disturbed drainage swales where the slopes are greater than 1 percent in order to reduce flow velocities until vegetation is reestablished.

# Miscellaneous

Best erosion control practices will be utilized as deemed necessary by the Contractor or Engineer and are not limited to the measures described above.

# <u>REFERENCES</u>

- 1. "City of Colorado Springs/El Paso County Drainage Criteria Manual" September 1987, Revised November 1991, Revised October 1994.
- 2. Chapter 6, Hydrology and Chapter 11, Storage, Section 3.2.1 of the "City of Colorado Springs Drainage Criteria Manual" May 2014.
- 3. "Volume 2, El Paso County/City of Colorado Springs Drainage Criteria Manual-Stormwater Quality Policies, Procedures and Best Management Practices" November 1, 2002.
- 4. Flood Insurance Rate Study for El Paso County, Colorado and Incorporated Areas. Federal Emergency Management Agency, Revised March 17, 1997.
- 5. Soils Survey of El Paso County area, Natural Resources Conservation Services of Colorado.
- 6. Master Development Drainage Plan Meridian Ranch. August 2000. Prepared by URS Corp.
- 7. Revision to Master Development Drainage Plan Meridian Ranch. July 2021. Prepared by Tech Contractors.
- 8. Master Development Drainage Plan Latigo Trails. October 2001. Prepared by URS Corp.
- 9. Final Drainage Report for The Sanctuary Filing 1 at Meridian Ranch. August 2022. Prepared by Tech Contractors.

# **Appendices**

Appendix A - HEC-HMS Data

# Input Data Rex Road - Regional Park

BASIN	AR	EA	CURVE	LAG TIME
	(acre)	(mi <sup>2</sup> ) NO.		(min)
	Н	ISTORIO	C	
HG13	67	0.1053	61.0	43.0
HG14	147 0.2297		61.0	45.1
	PF	ROPOSE	ED	
OS09b	28	0.0435	61.0	25.1
FG34	18	0.0275	62.7	16.8
FG35	19	0.0292	65.3	15.0
FG36	19	0.0295	65.1	25.8
FG37	48	0.0754	62.1	21.0

# COMPOSITE 'C' FACTORS

PROJECT:		Rex Ro		Date	5/16/2	023		
DACINI		AREA (AC.)					COMPOSITE	
BASIN DESIGNATION	UNDEV 61	5 DU/AC 78	STREETS 98	OPEN SPACE PARKS/GC 62	TOTAL	AREA (MI <sup>2</sup> )	'C' FACTOR	PERCENT IMPERV.
			HIS	TORIC				
HG13	67				67	0.1053	61.0	0.0%
HG14	147				147	0.2297	61.0	0.0%
						0.3350	Composite	0.0%
TOTALS	214	0	0	0	214			
			PRO	POSED				
OS09b	28				28	0.0435	61.0	0.0%
FG34	16	1.8			18	0.0275	62.7	4.4%
FG35	14	1.6	1.4	1.2	19	0.0292	65.3	11.3%
FG36	16		2.1	0.5	19	0.0295	65.1	11.2%
FG37	15		0.5	33	48	0.0754	62.1	2.4%
						0.2051	Composite:	4.7%
	89	3	4	34	131			

# LAG TIMES

#### SCS Calculations

# PROJECT: Rex Road - Regional Park

DATE:

6/2/2023

						LAG	TIMES								
SU	BBASIN	DATA		INITIA	L/OVER	LAND TIME (	T <sub>i</sub> )		TRAVEL TIME (T <sub>t</sub> )				TOTAL		
BASIN DESIGNATION	P <sub>2</sub>	AREA (SQ MI)	LENGTH (FT)	ΔН	SLOP E %	OVERLAND CONVEYANC E TYPE	n	T <sub>i</sub> (Min.)*	LENGTH (FT)	ΔН	TRAVEL CONVEYANC E TYPE	VEL. (FPS)	T <sub>t</sub> (Min.)**	T <sub>i</sub> +T <sub>t</sub> (Min.)	FINAL T <sub>lag</sub> (min)
HISTORIC															
HG13	1.88	0.105	745	27.0	3.6%	GP	0.15	50.2	3225	90	G	2.5	21.5	71.7	43.0
HG14	1.88	0.230	550	14.0	2.5%	GP	0.15	45.4	3650	68	G	2.0	29.7	75.1	45.1
						PROF	POSED								
OS09b	1.88	0.071	495	30.0	6.1%	GP	0.15	29.5	1725	42	G	2.3	12.3	41.8	25.1
FG34	1.88	0.028	200	12.0	6.0%	GP	0.15	14.3	2045	56	G	2.5	13.7	28.1	16.8
FG35	1.88	0.029	165	7.0	4.2%	GP	0.15	14.1	1450	32	G	2.2	10.8	25.0	15.0
FG36	1.88	0.030	305	7.0	2.3%	GP	0.15	29.5	1770	38	G	2.2	13.4	42.9	25.8
FG37	1.88	0.075	305	15.0	4.9%	GP	0.15	21.8	1780	40	G	2.2	13.2	35.0	21.0

TYPE OF SURFACE		n
SMOOTH SURFACES (conc, asph, gravel, bare soil, etc)	S	0.0110
FALLOW (no cover)	F	0.0500
CULTIVATED SOILS (<20% cover)	CL	0.0600
CULTIVATED SOILS (>20% cover)	CG	0.1700
GRASS (Short prairie grass)	GP	0.1500
GRASS (Dense grass)	GD	0.2400
GRASS (Bermuda grass)	GB	0.4100
RANGE (Natural)	R	0.1300
WOODS (Light Underbrush)	WL	0.4000
WOODS (Dense Underbrush)	WD	0.8000

1101 <del>03</del>	* $T_i = 0.42 (n \bullet L)^{0.8} / (P_2)^{0.5} \bullet S^{0.4}$
	** T <sub>t</sub> = L/60∙V (min)

TYPE OF SURFACE				
HEAVYMEADOW	Н			
TILLAGE/FIELD	Т			
RIPRAP (not buried)	R			
SHORT PASTURE AND LAV	L			
NEARLY BARE GROUND	В			
GRASSED WATERWAY	G			
NATURAL SANDY CHANNE	Ν			
PAVED AREAS	Р			



NOAA Atlas 14, Volume 8, Version 2 Location name: Peyton, Colorado, USA\* Latitude: 38,9783°, Longitude: -104,5842° Elevation: 7054.14 ft\*\* \* source: ESRI Maps \*\* source: USGS



#### POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Deborah Martin, Sandra Pavlovic, Ishani Roy, Michael St. Laurent, Carl Trypaluk, Dale Unruh, Michael Yekta, Geoffery Bonnin

NOAA, National Weather Service, Silver Spring, Maryland

PF tabular PF oraphical Maps & aerials

# PF tabular

Duration		Average recurrence interval (years)											
Duration	1	2	5	10	25	50	100	200	500	1000			
5-min	0.239	0.291	0.381	0.460	<b>0.576</b>	0.670	0.770	0.875	<b>1.02</b>	1.14			
	(0.190-0.301)	(0.232-0.367)	(0.302-0.482)	(0.363-0.585)	(0.442-0.764)	(0.501-0.899)	(0.556-1.06)	(0.606-1.23)	(0.680-1.48)	(0.737-1.66			
10-min	0.349	0.426	0.558	0.674	0.843	0.982	1.13	1.28	1.50	1.67			
	(0.278-0.441)	(0.339-0.538)	(0.443-0.706)	(0.532-0.857)	(0.647-1.12)	(0.734-1.32)	(0.814-1.55)	(0.888-1.80)	(0.996-2.16)	(1.08-2.44)			
15-min	0.426	0.519	0.680	0.822	<b>1.03</b>	<b>1.20</b>	1.37	<b>1.56</b>	1.82	2.03			
	(0.340-0.538)	(0.413-0.656)	(0.540-0.861)	(0.648-1.04)	(0.789-1.36)	(0.895-1.61)	(0.993-1.89)	(1.08-2.20)	(1.22-2.64)	(1.31-2.97			
30-min	0.608	0.741	0.969	1.17	1.46	1.70	1.95	<b>2.21</b>	2.58	2.87			
	(0.485-0.768)	(0.590-0.936)	(0.769-1.23)	(0.923-1.49)	(1.12-1.94)	(1.27-2.28)	(1.41-2.68)	(1.53-3.12)	(1.72-3.73)	(1.86-4.20			
60-min	0.778 (0.620-0.982)	0.934	1.21 (0.962-1.54)	1.47 (1.16-1.86)	1.84 (1.42-2.46)	2.16 (1.62-2.91)	2.50 (1.81-3.44)	2.87 (1.99-4.05)	3.38 (2.26-4.91)	3.80 (2.46-5.56			
2-hr	0.948	1.13	<b>1.46</b>	<b>1.76</b>	2.23	2.62	3.05	<b>3.52</b>	4.19	4.73			
	(0.762-1.19)	(0.905-1.41)	(1.16-1.83)	(1.40-2.22)	(1.73-2.96)	(1.99-3.51)	(2.23-4.18)	(2.47-4.95)	(2.82-6.04)	(3.09-6.87			
3-hr	1.04	1.22	1,57	<b>1,90</b>	<b>2.41</b>	2.86	3.35	<b>3.90</b>	4.68	5.33			
	(0.839.1.29)	(0.986 1.52)	(1,26-1,96)	(1,51-2,38)	(1.90-3.21)	(2.18-3.83)	(2.47-4.59)	(2.75-5.47)	(3.18-6.75)	(3.50-7.71			
6-hr	<b>1.21</b>	<b>1.40</b>	1.78	2.16	2.76	<b>3.29</b>	3,88	<b>4,53</b>	<b>5.49</b>	6.29			
	(0.980-1.49)	(1.14-1.73)	(1.44-2.21)	(1.74-2.68)	(2.19-3.65)	(2.53-4.38)	(2.88-5.28)	(3.23-6.34)	(3.76-7.88)	(4.17-9.04			
12-hr	1.39	<b>1,62</b>	<b>2,06</b>	2,48	<b>3.16</b>	3,76	4,42	5,15	6,22	7,10			
	(1.14-1.70)	(1.33-1.98)	(1.68-2.53)	(2.02-3.06)	(2.53-4.14)	(2.92-4.96)	(3.31-5.97)	(3.70-7.14)	(4.30-8.85)	(4.75-10.1			
24-hr	<b>1.61</b>	1.88	<b>2.39</b>	<b>2.88</b>	<b>3.63</b>	4.27	4.98	5.75	6.87	7.79			
	(1.33-1.95)	(1.55-2.29)	(1.97-2.92)	(2.35-3.52)	(2.91-4.69)	(3.34-5.58)	(3.75-6.66)	(4.17-7.90)	(4.78-9.70)	(5.25-11.1)			
2-day	1.86	2.19	2.79	3.33	4.15	4.85	5.59	6.40	7.55	8.49			
	(1.55-2.24)	(1.83-2.64)	(2.31-3.36)	(2.75-4.04)	(3.35-5.30)	(3.81-6.25)	(4.25-7.39)	(4.67-8.70)	(5.30-10.6)	(5.77-12.0			
3-day	<b>2.04</b>	<b>2.41</b>	<b>3.05</b>	3.63	<b>4.51</b>	5.24	6.03	6.87	8.07	9.04			
	(1.71-2.45)	(2.01-2.88)	(2.54-3.66)	(3.01-4.38)	(3.65-5.71)	(4.14-6.72)	(4.59-7.92)	(5.03-9.29)	(5.69-11.2)	(6.18-12.7			
4-day	<b>2.20</b> (1.85-2.62)	2.58 (2.16-3.08)	<b>3.25</b> (2.72-3.89)	3.86 (3.21-4.63)	<b>4.77</b> (3.87-6.01)	5.53 (4.38-7.06)	6.34 (4.85-8.31)	7.22 (5.31-9.73)	8.46 (5.98-11.7)	9.46 (6.50-13.2			
7 <b>-</b> day	2.60 (2.20-3.08)	<b>3.00</b> (2.54-3.56)	<b>3.71</b> (3.13-4.41)	4.36 (3.65-5.20)	5.33 (4.36-6.67)	6.14 (4.89-7.78)	7.00 (5.40-9.11)	7.93 (5.87-10.6)	9.26 (6.59-12.8)	<b>10.3</b> (7.14-14.4			
10-day	<b>2.96</b> (2.51-3.48)	3.39 (2.88-4.00)	4.16 (3.52-4.92)	4.85 (4.08-5.76)	5.88 (4.82-7.31)	6.73 (5.38-8.48)	7.63 (5.91-9.88)	8.61 (6.39-11.5)	<b>9.97</b> (7.13-13.7)	<b>11.1</b> (7.70-15.4			
20-day	<b>3.95</b> (3.38-4.61)	<b>4.55</b> (3.89-5.32)	<b>5.57</b> (4.75-6.52)	<b>6.44</b> (5.46-7.58)	<b>7.68</b> (6.32-9.39)	8.67 (6.97-10.8)	9.69 (7.54-12.4)	<b>10.8</b> (8.04-14.1)	<b>12.2</b> (8.79-16.6)	<b>13.3</b> (9.36-18.4			
30-day	<b>4.75</b> (4.09-5.51)	5.49 (4.72-6.38)	<b>6.70</b> (5.74-7.81)	7.72 (6.58-9.04)	9.12 (7.52-11.1)	<b>10.2</b> (8.24-12.6)	<b>11.3</b> (8.83-14.3)	<b>12.4</b> (9.32-16.2)	<b>13.9</b> (10.1-18.7)	<b>15.0</b> (10.6-20.6)			
45-day	5.73 (4.96-6.62)	6.62 (5.72-7.65)	8.05 (6.93-9.33)	9.21 (7.89-10.7)	<b>10.8</b> (8.91-12.9)	<b>12.0</b> (9.68-14.6)	<b>13.1</b> (10.3-16.5)	<b>14.3</b> (10.7-18.5)	15.8 (11.4-21.1)	<b>16.9</b> (12.0-23.0			
60-day	6.56 (5.70-7.55)	7.55 (6.55-8.69)	9,12 (7,88-10,5)	<b>10.4</b> (8.92-12.0)	<b>12.1</b> (9.98-14.4)	13.3 (10.8-16.1)	<b>14.5</b> (11.4-18.1)	15.6 (11.8-20.2)	<b>17.1</b> (12,5-22,8)	<b>18.2</b> (12.9-24.8			

<sup>1</sup> Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values. Please refer to NOAA Atlas 14 document for more information.

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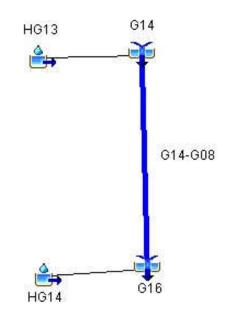
# HISTORIC CHARTS

HISTORIC SCS (100-YEAR)						
HYDROLOGIC ELEMENT	DRAINAGE AREA (SQ. MI.)	DISCHARGE PEAK Q100 (CFS)	TIME OF PEAK	TOTAL VOLUME Q100 (AC. FT.)		
HG14	0.2297	79	01Jul2015, 12:42	16		
HG13	0.1053	38	01Jul2015, 12:42	7.4		
G14	0.1053	38	01Jul2015, 12:42	7.4		
G14-G16	0.1053	37	01Jul2015, 12:48	7.3		
G16	0.3350	116	01Jul2015, 12:48	23		

HISTORIC SCS (50-YEAR)							
HYDROLOGIC ELEMENT	drainage Area (Sq. mi.)	DISCHARGE PEAK Q50 (CFS)	TIME OF PEAK	TOTAL VOLUME Q50 (AC. FT.)			
				-			
HG14	0.2297	52	01Jul2015, 12:48	11			
HG13	0.1053	25	01Jul2015, 12:42	5.2			
G14	0.1053	25	01Jul2015, 12:42	5.2			
G14-G16	0.1053	25	01Jul2015, 12:48	5.1			
G16	0.3350	77	01Jul2015, 12:48	16			

	HISTORIC SCS (10-YEAR)						
HYDROLOGIC ELEMENT	DRAINAGE AREA (SQ. MI.)	DISCHARGE PEAK Q10 (CFS)	TIME OF PEAK	TOTAL VOLUME Q10 (AC. FT.)			
HG14	0.2297	12	01Jul2015, 12:54	3.7			
HG13	0.1053	5.8	01Jul2015, 12:54	1.7			
G14	0.1053	5.8	01Jul2015, 12:54	1.7			
G14-G16	0.1053	5.8	01Jul2015, 13:00	1.7			
G16	0.3350	18	01Jul2015, 13:00	5.4			

# HISTORIC CONDITIONS



HISTORIC SCS (5-YEAR)							
HYDROLOGIC ELEMENT	Drainage Area (Sq. mi.)	DISCHARGE PEAK Q5 (CFS)	TIME OF PEAK	TOTAL VOLUME Q5 (AC. FT.)			
HG14	0.2297	4.7	01Jul2015, 13:06	1.9			
HG13	0.1053	2.2	01Jul2015, 13:00	0.9			
G14	0.1053	2.2	01Jul2015, 13:00	0.9			
G14-G16	0.1053	2.2	01Jul2015, 13:18	0.9			
G16	0.3350	6.8	01Jul2015, 13:12	2.8			

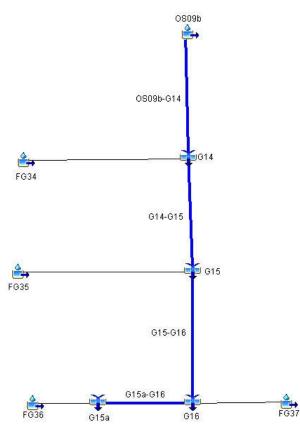
HISTORIC SCS (2-YEAR)						
HYDROLOGIC ELEMENT	DRAINAGE AREA (SQ. MI.)	DISCHARGE PEAK Q2 (CFS)	TIME OF PEAK	TOTAL VOLUME Q2 (AC. FT.)		
				-		
HG14	0.2297	0.8	01Jul2015, 14:18	0.6		
HG13	0.1053	0.4	01Jul2015, 14:12	0.3		
G14	0.1053	0.4	01Jul2015, 14:12	0.3		
G14-G16	0.1053	0.4	01Jul2015, 14:36	0.3		
G16	0.3350	1.2	01Jul2015, 14:24	0.8		

FUTURE	CHARTHS
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	PROPOSED SCS (100-YEAR)						
HYDROLOGIC ELEMENT	DRAINAGE AREA (SQ. MI.)	PEAK DISCHARGE Q100 (CFS)	TIME OF PEAK	TOTAL VOLUME Q100 (AC. FT.)			
OS09b	0.0435	22	01Jul2015, 12:18	3.1			
OS09b-G14	0.0435	22	01Jul2015, 12:24	3.1			
FG34	0.0275	20	01Jul2015, 12:12	2.1			
G14	0.0710	38	01Jul2015, 12:18	5.2			
G14-G15	0.0710	37	01Jul2015, 12:24	5.1			
FG35	0.0292	25	01Jul2015, 12:12	2.5			
G15	0.1002	55	01Jul2015, 12:18	7.7			
G15-G16	0.1002	54	01Jul2015, 12:24	7.5			
FG37	0.0754	46	01Jul2015, 12:18	5.6			
FG36	0.0295	19	01Jul2015, 12:18	2.5			
G15a	0.0295	19	01Jul2015, 12:18	2.5			
G15a-G16	0.0295	19	01Jul2015, 12:24	2.5			
G16	0.2051	114	01Jul2015, 12:24	16			

PROPOSED SCS (50-YEAR)													
HYDROLOGIC ELEMENT	DRAINAGE AREA (SQ. MI.)	PEAK DISCHARGE Q50 (CFS)	TIME OF PEAK	TOTAL VOLUME Q50 (AC. FT.)									
OS09b	0.0435	14	01Jul2015, 12:24	2.2									
OS09b-G14	0.0435	14	01Jul2015, 12:24	2.1									
FG34	0.0275	13	01Jul2015, 12:12	1.5									
G14	0.0710	25	01Jul2015, 12:18	3.7									
G14-G15	0.0710	24	01Jul2015, 12:24	3.6									
FG35	0.0292	18	01Jul2015, 12:12	1.9									
G15	0.1002	36	01Jul2015, 12:18	5.5									
G15-G16	0.1002	35	01Jul2015, 12:30	5.4									
FG37	0.0754	31	01Jul2015, 12:18	4.0									
FG36	0.0295	13	01Jul2015, 12:24	1.8									
G15a	0.0295	13	01Jul2015, 12:24	1.8									
G15a-G16	0.0295	13	01Jul2015, 12:30	1.8									
G16	0.2051	74	01Jul2015, 12:24	11									

# GIECK FUTURE CONDITIONS



	PRO	POSED SCS (1	0-YEAR)	
HYDROLOGIC ELEMENT	DRAINAGE AREA (SQ. MI.)	PEAK DISCHARGE Q10 (CFS)	TIME OF PEAK	TOTAL VOLUME Q10 (AC. FT.)
OS09b	0.1313	11.6	01Jul2015, 12:18	2.2
OS09b-G14	0.1313	11.6	01Jul2015, 12:18	2.2
FG34	0.1313	11.4	01Jul2015, 12:24	2.1
G14	0.0578	5.6	01Jul2015, 12:12	1.0
G14-G15	0.0578	5.5	01Jul2015, 12:18	1.0
FG35	0.0538	7.0	01Jul2015, 12:36	1.4
G15	0.0538	7.0	01Jul2015, 12:36	1.4
G15-G16	0.1116	11.0	01Jul2015, 12:24	2.3
FG37	0.1116	10.9	01Jul2015, 12:30	2.3
FG36	0.0391	6.4	01Jul2015, 12:12	0.9
G15a	0.2820	27.2	01Jul2015, 12:24	5.4
G15a-G16	0.2820	27.1	01Jul2015, 12:30	5.3
G16	0.2820	27	01Jul2015, 12:30	5.3

	PRC	POSED SCS (5	5-YEAR)	
HYDROLOGIC ELEMENT	DRAINAGE AREA (SQ. MI.)	PEAK DISCHARGE Q5 (CFS)	TIME OF PEAK	TOTAL VOLUME Q5 (AC. FT.)
OS09b	0.0435	1.1	01Jul2015, 12:36	0.4
OS09b-G14	0.0435	1.1	01Jul2015, 12:42	0.4
FG34	0.0275	1.3	01Jul2015, 12:18	0.3
G14	0.0710	2.0	01Jul2015, 12:36	0.7
G14-G15	0.0710	2.0	01Jul2015, 12:54	0.6
FG35	0.0292	2.4	01Jul2015, 12:12	0.4
G15	0.1002	3.0	01Jul2015, 12:48	1.0
G15-G16	0.1002	3.0	01Jul2015, 13:06	1.0
FG37	0.0754	2.7	01Jul2015, 12:24	0.7
FG36	0.0295	1.8	01Jul2015, 12:30	0.4
G15a	0.0295	1.8	01Jul2015, 12:30	0.4
G15a-G16	0.0295	1.7	01Jul2015, 12:36	0.4
G16	0.2051	6.5	01Jul2015, 12:36	2.1

	PRC	POSED SCS (2	2-YEAR)	
HYDROLOGIC ELEMENT	DRAINAGE AREA (SQ. MI.)	PEAK DISCHARGE Q2 (CFS)	TIME OF PEAK	TOTAL VOLUME Q2 (AC. FT.)
OS09b	0.0435	0.2	01Jul2015, 13:42	0.1
OS09b-G14	0.0435	0.2	01Jul2015, 14:00	0.1
FG34	0.0275	0.2	01Jul2015, 13:00	0.1
G14	0.0710	0.3	01Jul2015, 13:36	0.2
G14-G15	0.0710	0.3	01Jul2015, 14:06	0.2
FG35	0.0292	0.5	01Jul2015, 12:24	0.2
G15	0.1002	0.6	01Jul2015, 13:48	0.4
G15-G16	0.1002	0.6	01Jul2015, 14:24	0.3
FG37	0.0754	0.4	01Jul2015, 13:12	0.2
FG36	0.0295	0.4	01Jul2015, 12:48	0.2
G15a	0.0295	0.4	01Jul2015, 12:48	0.2
G15a-G16	0.0295	0.4	01Jul2015, 13:00	0.2
G16	0.2051	1.2	01Jul2015, 13:00	0.7

Appendix B – Rational Calculations

Land Use or Surface	Percent						Runoff Co	efficients					
Characteristics	Impervious	2-y	ear	5-y	ear	10-1	year	25-	/ear	50-1	year	100-	year
		HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D
Business													
Commercial Areas	95	0.79	0.80	0.81	0.82	0.83	0.84	0.85	0.87	0.87	0.88	0.88	0.89
Neighborhood Areas	70	0.45	0.49	0.49	0.53	0.53	0.57	0.58	0.62	0.60	0.65	0.62	0.68
Residential													
1/8 Acre or less	65	0.41	0.45	0.45	0.49	0.49	0.54	0.54	0.59	0.57	0.62	0.59	0.65
1/4 Acre	40	0.23	0.28	0.30	0.35	0.36	0.42	0.42	0.50	0.46	0.54	0.50	0.58
1/3 Acre	30	0.18	0.22	0.25	0.30	0.32	0.38	0.39	0.47	0.43	0.52	0.47	0.57
1/2 Acre	25	0.15	0.20	0.22	0.28	0.30	0.36	0.37	0.46	0.41	0.51	0.46	0.56
1 Acre	20	0.12	0.17	0.20	0.26	0.27	0.34	0.35	0.44	0.40	0.50	0.44	0.55
Industrial													
Light Areas	80	0.57	0.60	0.59	0.63	0.63	0.66	0.66	0.70	0.68	0.72	0.70	0.74
Heavy Areas	90	0.71	0.73	0.73	0.75	0.75	0.77	0.78	0.80	0.80	0.82	0.81	0.83
Parks and Cemeteries	7	0.05	0.09	0.12	0.19	0.20	0.29	0.30	0.40	0.34	0.46	0.39	0.52
Playgrounds	13	0.07	0.13	0.16	0.23	0.24	0.31	0.32	0.42	0.37	0.48	0.41	0.54
Railroad Yard Areas	40	0.23	0.28	0.30	0.35	0.36	0.42	0.42	0.50	0.46	0.54	0.50	0.58
Undeveloped Areas													
Historic Flow Analysis Greenbelts, Agriculture	2	0.03	0.05	0.09	0.16	0.17	0.26	0.26	0.38	0.31	0.45	0.36	0.51
Pasture/Meadow	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50
Forest	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50
Exposed Rock	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Offsite Flow Analysis (when landuse is undefined)	45	0.26	0.31	0.32	0.37	0.38	0.44	0.44	0.51	0.48	0.55	0.51	0.59
Streets			1										
Paved	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Gravel	80	0.57	0.60	0.59	0.63	0.63	0.66	0.66	0.70	0.68	0.72	0.70	0.74
Drive and Walks	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Roofs	90	0.71	0.73	0.73	0.75	0.75	0.77	0.78	0.80	0.80	0.82	0.81	0.83
Lawns	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50

# Table 6-6. Runoff Coefficients for Rational Method (Source: UDFCD 2001)

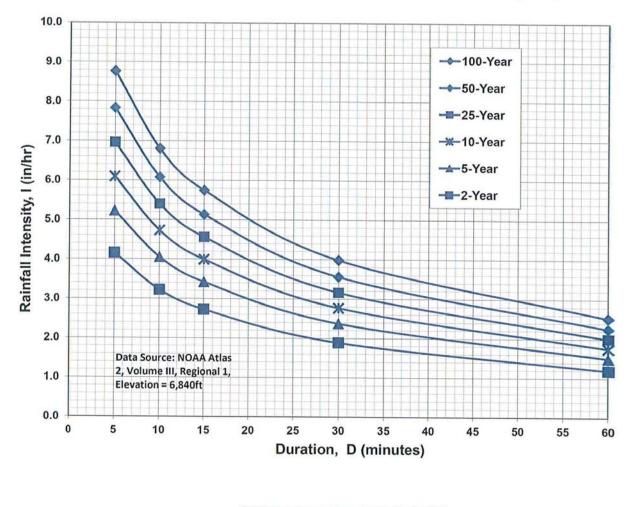


Figure 6-5. Colorado Springs Rainfall Intensity Duration Frequency

<b>IDF</b> Equations
$I_{100} = -2.52 \ln(D) + 12.735$
$I_{50} = -2.25 \ln(D) + 11.375$
$I_{25} = -2.00 \ln(D) + 10.111$
$I_{10} = -1.75 \ln(D) + 8.847$
$I_5 = -1.50 \ln(D) + 7.583$
$I_2 = -1.19 \ln(D) + 6.035$
Note: Values calculated by equations may not precisely duplicate values read from figure.

			<u>CO</u>	MPOSI	E'C'FAC	TORS								
PROJECT:	Rex Ro		6/2/2023											
			ARE	EA (AC.)			COM	MPOSITE FAC	TOR					
BASIN DESIGNATION	UNDEV	5 DU/AC	GRAVEL	STREETS	OPEN SPACE PARKS/GC LAWNS	TOTAL	2-year	5-year	100-year	Percent Imperviou				
	PROPOSED													
OS09b	28		28	0.03	0.09	0.36	0.0%							
FG34	16	1.8				18	0.06	0.12	0.38	4.4%				
FG35a	11	1.6			0.7	14	0.07	0.13	0.38	5.2%				
FG35b	3.0			1.4	0.5	4.9	0.27	0.33	0.53	28.0%				
FG36a	16		0.3	0.8		18	0.08	0.13	0.39	5.9%				
FG36c	1.3			1.0	0.5	2.8	0.34	0.40	0.58	35.4%				
FG37	48		48	0.03	0.09	0.36	0.5%							
TOTAL	124	3.4	0.3	3.4	1.7	133	0.06	0.12	0.38	3.9%				

#### TIME OF CONCENTRATION

# PROJECT: Rex Road - Regional Park

DATE: 6/2/2023

					TIME	OF CON		TION						
SUBBAS	SIN DA	TA	INIT./0	OVERLAN	ND TIME	(T <sub>i</sub> )			TRA\	/EL TIM	E (T <sub>t</sub> )			TOTA L
BASIN DESIGNATIO N	C <sub>5</sub>	AREA (AC)	LENGTH (FT) ΔΗ		SLOP E %	Ti (Min.)*	LENGTH (FT)	ΔН	SLOP E %	CONVI TYPE	EYANC COEF	VEL. (FPS)	Tt (Min.)* *	Ti+Tt (Min.)
OS09b	0.09	28	495	29.0	5.9%	22.9	1725	41	2.4%	В	10	1.5	18.6	41.5
FG34	0.12	18	200	12.0	6.0%	14.0	2045	56	2.7%	В	10	1.7	20.6	34.6
FG35a	0.13	14	165	7.0	4.2%	14.1	1305	31	2.4%	В	10	1.5	14.1	28.3
FG35b	0.33	4.9	125	8.0	6.4%	8.5	770	27	3.5%	Р	20	3.7	3.4	11.9
FG36a	0.13	18	305	7.0	2.3%	23.4	1690	41	2.4%	G	15	2.3	12.1	35.5
FG36c	0.40	2.8	270	7.5	2.8%	15.0	1275	30	2.4%	Р	20	3.1	6.9	21.9
FG37	0.09	48	305	15.0	4.9%	18.9	1780	40	2.2%	В	10	1.5	19.8	38.7

Notes	* Ti = * Ti = 0.3	395 (1.1-C5)L <sup>0.5</sup>
		S <sup>0.33</sup>
	$V = C_V S_W^{0.5}$	** Tt = L x V

TYPE OF SURFACE		Cv
HEAVYMEADOW	Н	2.5
TILLAGE/FIELD	т	5
RIPRAP (not buried)	R	6.5
SHORT PASTURE AND LAWN	L	7
NEARLY BARE GROUND	В	10
GRASSED WATERWAY	G	15
PAVED AREAS	Р	20

#### STORM DRAINAGE SYSTEM DESIGN (RATIONAL METHOD PROCEDURE) SURFACE ROUTING

PRO	IECT:	ECT: Rex Road - Regional Park																								Date: 6/2/2023						
							D	IRECT R	UNOFF							Т	OTAL I	RUNOFF	-									OVERL	AND TRA	VEL TI	ME	
OINT				I	l (in./h	r.)		COEFF.		CA Q (cfs)						I	(in./ hr.	)		CA			Q (cfs)		Z	Щ	F				τ	
DESIGN POI	BASIN	AREA (AC)	Tc (Min.)	(2 YR)	(5 YR)	(100 YR)	(2 YR)	(5 YR)	(100 YR)	(2 YR)	(5 YR)	(100 YR)	(2 YR)	(5 YR)	(100 YR)	Sum Tc (min.)	(2 YR)	(5 YR)	(100 YR)	(2 YR)	(5 YR)	(100 YR)	(2 YR)	(5 YR)	(100 YR)	DESTINATION	CONVEYANCE TYPE	COEFFICIEN <sup>-</sup> Cv	% 3401S	VEL. (FPS)	LENGTH (FT	TRAVEL TIME '
		PROPOSED																														
DP1	0S09b	28	41.5	1.60	1.99	3.35	0.03	0.09	0.36	0.83	2.50	10.0	1.3	5.0	34								1.3	5.0	34	G14	В	10.0	2.16%	1.5	950	10.8
G14	FG34	18	34.6	1.82	2.27	3.80	0.06	0.12	0.38	1.05	2.06	6.65	1.9	4.7	25	52.3	1.33		2.76		4.56	16.7	2.5	7.5		G15.1	В	10.0	2.28%	1.5	1360	15.0
G15.1	FG35a	14	28.3	2.06	2.57	4.32	0.07	0.13	0.38	0.91	1.76	5.27	1.9	4.5	23	67.3	1.03	1.27	2.13	2.80	6.32	21.9	2.9	8.0		I01						
I01	FG35b	4.9	11.9	3.09	3.87	6.49	0.27	0.33	0.53	1.35	1.64	2.63	4.2	6.3	17								4.2	6.3	17	G15a	Р	20.0	1.38%	2.3	60	0.4
G15a1	FG36a	18	35.5	1.79	2.23	3.74	0.08	0.13	0.39	1.36	2.37	6.91	2.4	5.3	26								2.4	5.3		G15a	Р	20.0	1.00%	2.0	85	0.7
	FG36c	2.8	21.9	2.36	2.95	4.96	0.34	0.40	0.58	0.95	1.12	1.62	2.2	3.3	8.0	21.9	2.36		4.96			2.43	2.6	4.2								
G15a																36.2	1.76	2.20	3.69		3.79	9.34	4.4	8.3	-	G16a	G	15.0	2.02%	2.1	420	3.3
G15																67.5	1.02	-	2.12	3.98	7.66	23.7	4.1	9.7		G16a	G	15.0	2.25%	2.3	1150	8.5
G16a																76.1	0.88	1.09	1.82	6.45	11.4	33.1	5.7	12	60	G16a	G	15.0	0.91%	1.4	715	8.3
G16	FG37	48	38.7	1.68	2.10	3.52	0.03	0.09	0.36	1.65	4.54	17.51	2.8	10	62	84.4	0.76	0.93	1.56	8.11	16.0	50.6	6.1	15	79							

# STORM DRAINAGE SYSTEM DESIGN INLET CALCULATIONS

### PROJECT: Rex Road - Regional Park

									Q <sub>⊺otal</sub>		Q <sub>Capture</sub>					QFlo	w-by		DEPTH	H(max)	SPR	EAD
DP	BASIN	Inlet size L(i)	Proposed or Existing	INLET TYPE	OROSS SLOPE	STREET SLOPE	T <sub>c</sub>	Q2 (cfs)	Q₅ (cfs)	Q <sub>100</sub> (cfs)	Q₅ (cfs)	Q <sub>100</sub> (cfs)		CA <sub>eqv.</sub> (100-yr)	Q₅ (cfs)	Q <sub>100</sub> (cfs)		CA <sub>eqv.</sub> (100-yr)	Q₅ (ft)	Q <sub>100</sub> (ft)	Q₅ (ft)	Q <sub>100</sub> (ft)
I01	FG35b	20	PROP	FLOW-BY	2.0%	1.0%	11.9	4.2	6.3	17	5.2	12	1.34	1.82	1.2	5.3	0.30	0.81	0.37	0.50	14.4	20.9

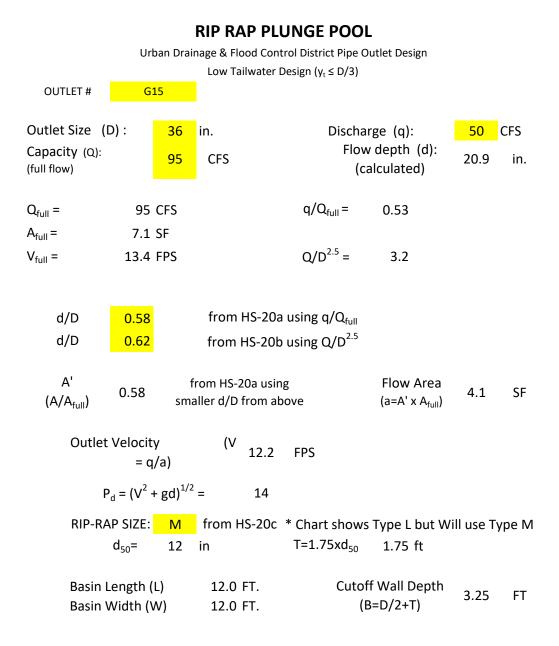
Date: 12/22/2022

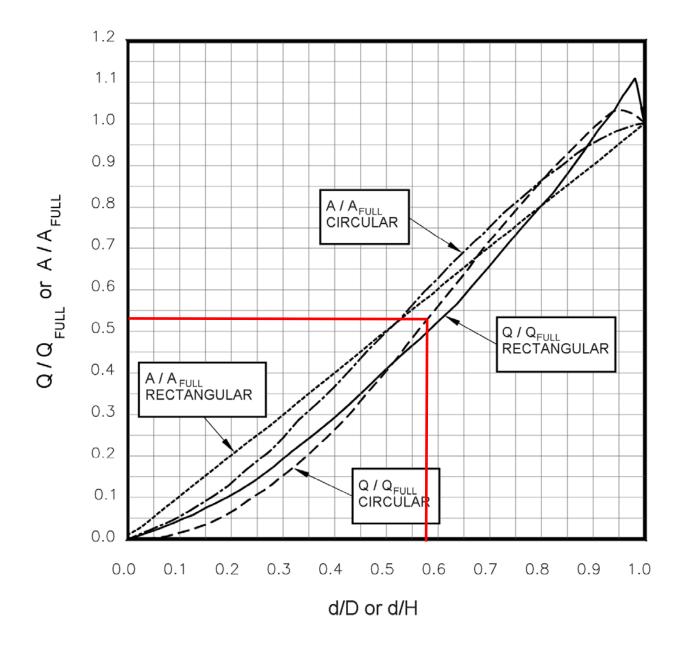
# STORM DRAINAGE SYSTEM DESIGN

HYDRAULICS

PROJECT:		Rex Road - Regional Park															Date:	6/2/2023		
Label	Upstrm Node	Dnstrm Node	Intlet CA (acres)	Inlet Tc (min)	Inlet Flow (ft³/s)	System CA (acres)	System Flow Time (min)	System Intensity (in/hr)	Length (ft)	Section Size (in)	Slope (%)	Capacity (Full Flow) (ft³/s)	System Flow (ft³/s)	Velocity (Ave) (ft/s)		Hydraulic Grade Line (Upstrm) (ft)	Invert		Hydraulic Grade Line (Dnstrm) (ft)	Invert (Dnstrm) (ft)
P01	G15.1	101	21.93	67.3	47	21.93	67.3	2.13	80.5	36	1.20%	73	47	11	7035.22	7034.5	7032.22	7037.27	7033.6	7031.25
P02	101	G15	1.82	11.9	12	23.75	67.4	2.12	60.3	36	1.18%	72	51	11	7037.27	7033.6	7031.25	7035.00	7032.5	7030.54

Appendix C – Culvert and Outlet Protection Design







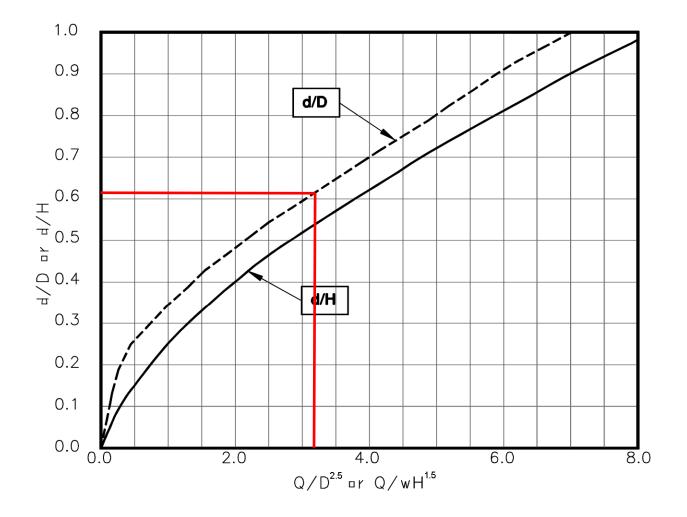


Figure HS-20b—Low Tailwater Riprap Basins for Storm Sewer Pipe Outlets— Brink Depth for Horizontal Pipe Outlets

(Stevens and Urbonas 1996)

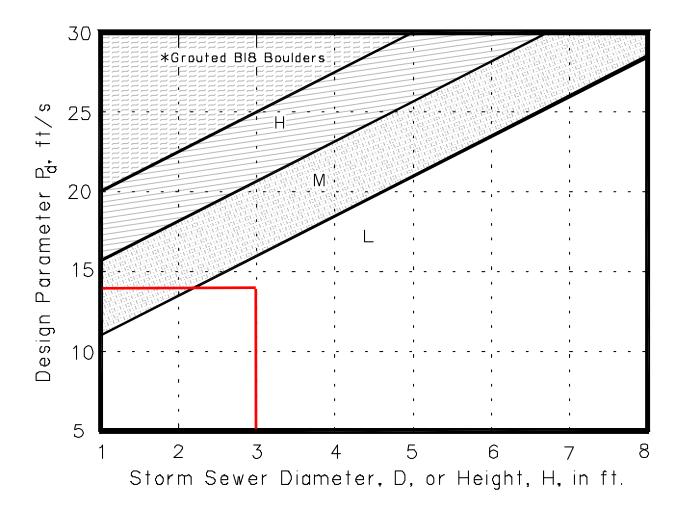
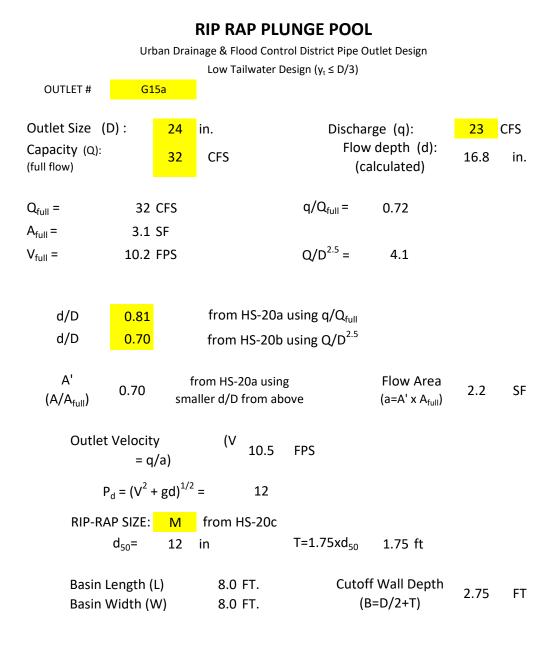
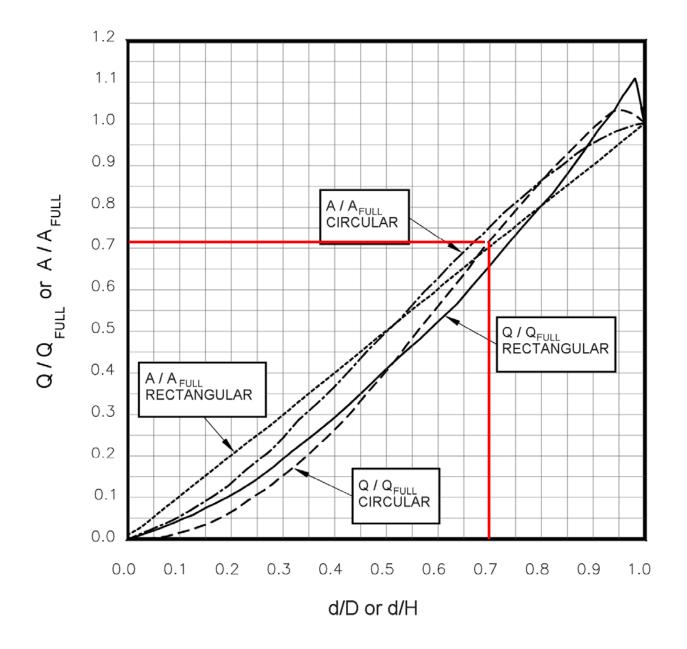


Figure HS-20c—Low Tailwater Riprap Basins for Storm Sewer Pipe Outlets— Riprap Selection Chart for Low Tailwater Basin at Pipe Outlet (Stevens and Urbonas 1996)







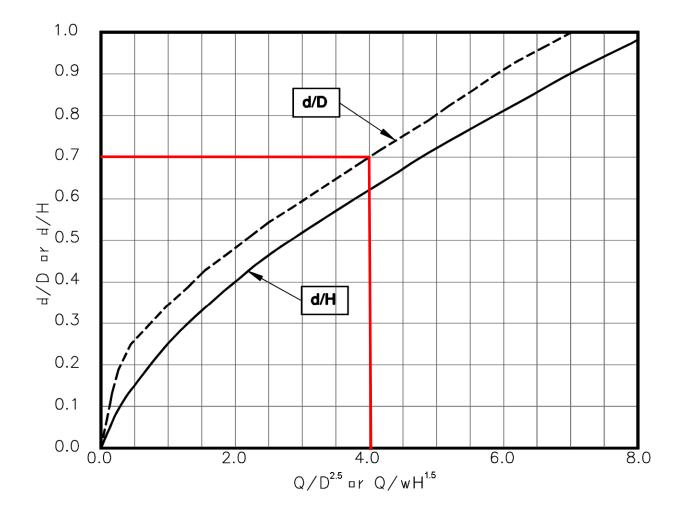


Figure HS-20b—Low Tailwater Riprap Basins for Storm Sewer Pipe Outlets— Brink Depth for Horizontal Pipe Outlets

(Stevens and Urbonas 1996)

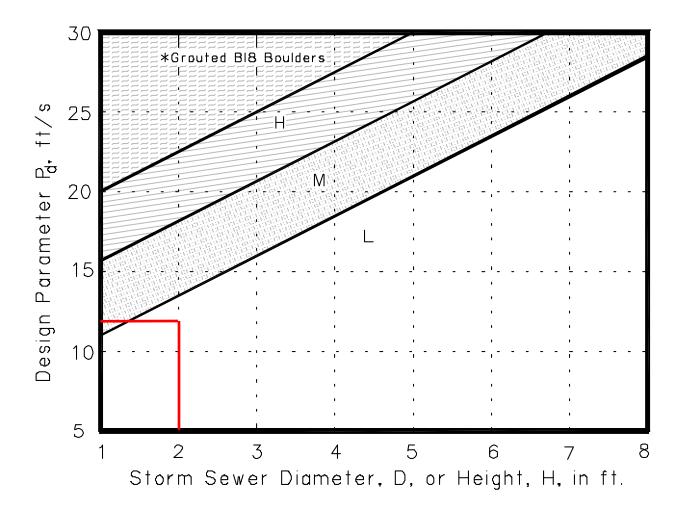


Figure HS-20c—Low Tailwater Riprap Basins for Storm Sewer Pipe Outlets— Riprap Selection Chart for Low Tailwater Basin at Pipe Outlet (Stevens and Urbonas 1996)

#### Appendix D – Water Quality Analysis

Update per 6/6/23 WQ coordination meeting

Appendix I Stormwater Quality Policy and Procedures-revisions

#### **I.7. Post-Construction Stormwater Management**

The Rex Road project will achieve water quality primarily with a Bioretention Basin located near the southwest corner of the future intersection of Rex Rd with Eastonville Road. The size of the basin was calculated to be just over 600 cu. ft.

The road platform consists of three basins, the first basin (FG35b), located at the western portions of the project will not require water quality treatment by Section I.7.1.C.1 as outlined below. The area comprises approximately 1.4 ac. of impervious area tributary to a flow-by inlet (I01), the inlet captures approximately 2/3 of the flow equating to approximately 1 acre of tributary area downstream of the inlet into a natural channel. By the exception listed, up to 20%, not exceeding 1 acre can be released without water quality when the County has determined that it is not practicable to capture the runoff prior to control measures.

#### I.7.1.C.1 Water Quality Capture Volume (WQCV) Standard.

100% of the applicable development site is captured, except the County may exclude up to 20 percent, not to exceed 1 acre of the applicable development site area when the County has determined that it is not practicable to capture runoff from portions of the site that will not drain towards control measures.

Of the total surface runoff from this area, approximately two-thirds of the total runoff is captured by the inlet and combined with the upstream tributary area. This basin area is approximately 8% of the total upstream tributary area. (4.9 ac v. 59 ac.).

The second basin consists of 18 acres (FG36a) that is north of Rex Rd and the northern half of the paved section. The runoff from the roadway platform will cross over a grass buffer and grass swale prior to combining with the remaining undeveloped flow. Runoff reduction calculations are included in the following pages. The unconnected impervious area (pavement, 15,600 sf) will flow across the grass buffer and swale (18,990 sf) resulting in a 100% WQCV reduction.

The third basin consists of 2.8 acres (FG36c) that is north of Rex Rd and the northern half of the paved section. The runoff from the roadway platform will cross over a grass buffer and grass swale prior to combining with the remaining undeveloped flow. Runoff reduction calculations are included in the following pages. The unconnected impervious area (pavement, 23,660 sf) will flow across the grass buffer and swale (5,230 sf) resulting in a 51% WQCV reduction, the remaining untreated WQCV is 483 CF. Bioretention will be used to treat and account for the remaining water quality needs.

The bioretention calculation resulted in the basin geometry having a 900 SF flat bottom, 8" of depth for a volume of 607 CF. The basin will be placed near the southwest corner of the future intersection of Rex Rd and Eastonville Rd,

See the exhibit on the following page for impacted areas, calculations, and more information. See Fig. 7 for drainage flow patterns and general drainage areas for the areas in question.

#### Update per 6/6/23 WQ coordination meeting

			Desiç	gn Procedu	re Form: I	Runoff Red	luction					
UD-BMP (Version 3.07, March 2018)										Sheet 1 of 1		
-	-	Thomas A Kerby, PE								_		
	Tech Contrac	tors									-	
	May 30, 2023										-	
		ension at Falc	on Regional F	Park							_	
Location:	Falcon, CO										-	
SITE INFORMATION (Use	er Input in Bl	ue Cells)										
OTE IN ORIGINATION (USE		Rainfall Depth	0.60	inches								
Depth of Average Ru			0.43		/atersheds O	utside of the D	enver Regior	n, Figure 3-1 i	n USDCM Vo	l. 3)		
Area Type	UIA:RPA	SPA										
Area ID	FG36a1	FG36a2										
Downstream Design Point ID	G15a1	G15a1										
Downstream BMP Type	None	None										
DCIA (ft <sup>2</sup> )												
UIA (ft <sup>2</sup> )	15,600											
RPA (ft <sup>2</sup> )	18,990											
SPA (ft <sup>2</sup> )		731,325										
HSG A (%)	0%	0%										
HSG B (%)	100%	100%		ļ								
HSG C/D (%)	0%	0%										
Average Slope of RPA (ft/ft)	0.020											
UIA:RPA Interface Width (ft)	250.00											
CALCULATED RUNOFF	RESULTS											
Area ID	FG36a1	FG36a2		r								
UIA:RPA Area (ft <sup>2</sup> )	34,590											
L / W Ratio	0.55											
UIA / Area	0.4510											
Runoff (in)	0.00	0.00										
Runoff (ft <sup>3</sup> )	0	0										
Runoff Reduction (ft <sup>3</sup> )	650	36566										
CALCULATED WQCV RE					1	1	1	1	1	1		
Area ID	FG36a1	FG36a2										
WQCV (ft <sup>3</sup> )	650 650	0										
WQCV Reduction (ft <sup>3</sup> ) WQCV Reduction (%)	100%	0%										
Untreated WQCV (ft <sup>3</sup> )	0	0 /0										
		, , , , , , , , , , , , , , , , , , ,		1	1	1	1	1	1	1	1	
CALCULATED DESIGN P		LTS (sums re	sults from a	ll columns w	ith the same	Downstream	n Design Poir	nt ID)				
Downstream Design Point ID												
DCIA (ft <sup>2</sup> )	0											
UIA (ft <sup>2</sup> )	15,600											
RPA (ft <sup>2</sup> )	18,990											
SPA (ft <sup>2</sup> )	731,325											
Total Area (ft <sup>2</sup> )	765,915			<u> </u>								└────┤│
Total Impervious Area (ft <sup>2</sup> )	15,600											┝────┤ ┃
WQCV (ft <sup>3</sup> )												┝────┤ ┃
WQCV Reduction (ft <sup>3</sup> ) WQCV Reduction (%)	650 100%			<u> </u>								├────┤ ┃
Untreated WQCV (ft <sup>3</sup> )												┝────┤ ┃
	5	I	<u> </u>	L	I	I	I	I	I	I	1	
CALCULATED SITE RES	ULTS (sums	results from	all columns	in workshee	et)							
Total Area (ft <sup>2</sup> )					-							
Total Impervious Area (ft <sup>2</sup> )	15,600	1										
WQCV (ft <sup>3</sup> )	650											
WQCV Reduction (ft <sup>3</sup> )	650											
WQCV Reduction (%)	100%											
Untreated WQCV (ft <sup>3</sup> )	0	]										

			Desi		ersion 3.07, Ma	Runoff Red						Sheet 1 of 1
Designer:	Thomas A Ke	rby, PE		OD-BIVIP (Ve	ersion 3.07, Ivia	rch 2018)						Sheet 1 of 1
-		ch Contractors										
	May 30, 2023											
		ension at Falco	on Regional I	Park								
-	Rex Road Extension at Falcon Regional Park Falcon, CO											
Location.												
SITE INFORMATION (Use			0.00	]:								
Depth of Average Ru		Rainfall Depth g Storm, d <sub>6</sub> =	0.60	inches inches (for V	/atersheds O	utside of the D	enver Region	n, Figure 3-1 i	n USDCM Vo	l. 3)		
Area Type	UIA:RPA	SPA										
Area ID	FG36c1	FG36c2										
Downstream Design Point ID	G15a	G15a										
Downstream BMP Type	None	None										
DCIA (ft <sup>2</sup> )												
UIA (ft <sup>2</sup> )	23,660											
RPA (ft <sup>2</sup> )	5,230											
SPA (ft <sup>2</sup> )		98,200										
HSG A (%)	0%	0%										
HSG B (%)	100%	100%										
HSG C/D (%)	0%	0%										
Average Slope of RPA (ft/ft)	0.020											
UIA:RPA Interface Width (ft)	250.00											
		· ·										
CALCULATED RUNOFF		г.			1							
Area ID	FG36c1	FG36c2										
UIA:RPA Area (ft <sup>2</sup> )	28,890											
L / W Ratio	0.46											
UIA / Area	0.8190											
Runoff (in)	0.20	0.00										
Runoff (ft <sup>3</sup> )	483	0										
Runoff Reduction (ft <sup>3</sup> )	503	4910										
CALCULATED WQCV RE	SULTS											
Area ID	FG36c1	FG36c2										
WQCV (ft <sup>3</sup> )	986	0										
WQCV Reduction (ft <sup>3</sup> )	503	0										
WQCV Reduction (%)	51%	0%										
Untreated WQCV (ft3)	483	0										
CALCULATED DESIGN P	OINT RESUL	_TS (sums res	sults from a	ll columns w	ith the same	Downstream	n Design Poi	nt ID)				
Downstream Design Point ID	G15a											
DCIA (ft <sup>2</sup> )	0											
UIA (ft <sup>2</sup> )	23,660			1								
RPA (ft <sup>2</sup> )	5,230	l l		1								
SPA (ft <sup>2</sup> )	98,200	i t		1								
Total Area (ft <sup>2</sup> )	127,090	<u>├</u>		1	1							
Total Impervious Area (ft <sup>2</sup> )	23,660											
• • • • • • •				-								
WQCV (ft <sup>3</sup> ) WQCV Reduction (ft <sup>3</sup> )	986	├										
· · ·	503	├										
WQCV Reduction (%)	51%	<b>├</b> ────┤		<u>├</u> ───			L				L	ļ
Untreated WQCV (ft <sup>3</sup> )	483	I I		L	l	L	l	L	L	L	l	L
CALCULATED SITE RES		results from a	all columns	in workshee	et)							
Total Area (ft <sup>2</sup> )	127,090											
Total Impervious Area (ft <sup>2</sup> )	23,660											
WQCV (ft <sup>3</sup> )	986											
WQCV Reduction (ft <sup>3</sup> )	503											
WQCV Reduction (%)	51%											
Untreated WQCV (ft <sup>3</sup> )	483											
		-										

	Design Procedure	e Form: Rain Garden (RG)	
Designer:	UD-BMP	(Version 3.07, March 2018)	Sheet 1 of 2
Company: Date:	May 30, 2023		
Project:			
Location:		1	
1. Basin Sto	rage Volume		
	re Imperviousness of Tributary Area, I <sub>a</sub> if all paved and roofed areas upstream of rain garden)	l <sub>a</sub> = <u>35.4</u> %	
B) Tributa	ary Area's Imperviousness Ratio (i = I <sub>a</sub> /100)	i = 0.354	
	Quality Capture Volume (WQCV) for a 12-hour Drain Time CV= 0.8 * (0.91* i <sup>3</sup> - 1.19 * i <sup>2</sup> + 0.78 * i)	WQCV = 0.13 watershe	ed inches
D) Contri	buting Watershed Area (including rain garden area)	Area = <u>127,090</u> sq ft	
	Quality Capture Volume (WQCV) Design Volume (WQCV / 12) * Area	V <sub>WQCV</sub> =cu ft	
	atersheds Outside of the Denver Region, Depth of ge Runoff Producing Storm	d <sub>6</sub> = 0.60 in	
	atersheds Outside of the Denver Region, Quality Capture Volume (WQCV) Design Volume	V <sub>WQCV OTHER</sub> =cu ft	
	nput of Water Quality Capture Volume (WQCV) Design Volume f a different WQCV Design Volume is desired)	V <sub>WQCV USER</sub> = 483 cu ft	
2. Basin Geo	ometry		
A) WQCV	Depth (12-inch maximum)	D <sub>WQCV</sub> = 8 in	
	arden Side Slopes (Z = 4 min., horiz. dist per unit vertical) " if rain garden has vertical walls)	Z = 4.00 ft / ft	
C) Mimim	um Flat Surface Area	A <sub>Min</sub> = 900 sq ft	
D) Actual	Flat Surface Area	A <sub>Actual</sub> = 900 sq ft	
E) Area a	t Design Depth (Top Surface Area)	A <sub>Top</sub> = <u>920</u> sq ft	
,	arden Total Volume A <sub>Top</sub> + A <sub>Actual</sub> ) / 2) * Depth)	V <sub>T</sub> = <u>607</u> cu ft	
3. Growing N	<i>I</i> ledia	Choose One 18" Rain Garden Gro	owing Media
		Other (Explain):	
4. Underdrai	n System	Choose One	
A) Are un	derdrains provided?	YES     NO	
B) Underc	Irain system orifice diameter for 12 hour drain time		
	i) Distance From Lowest Elevation of the Storage Volume to the Center of the Orifice	y = N/A ft	
	ii) Volume to Drain in 12 Hours	Vol <sub>12</sub> = <u>N/A</u> cu ft	
	iii) Orifice Diameter, 3/8" Minimum	D <sub>o</sub> = <u>N/A</u> in	

Design Procedu	ure Form: Rain Garden (RG)
Designer: Company: Date: May 30, 2023 Project: Location:	Sheet 2 of
<ol> <li>Impermeable Geomembrane Liner and Geotextile Separator Fabric</li> <li>A) Is an impermeable liner provided due to proximity of structures or groundwater contamination?</li> </ol>	Choose One YES NO
6. Inlet / Outlet Control A) Inlet Control	Choose One Sheet Flow- No Energy Dissipation Required Concentrated Flow- Energy Dissipation Provided
7. Vegetation	Choose One Seed (Plan for frequent weed control) Plantings Sand Grown or Other High Infiltration Sod
<ul><li>8. Irrigation</li><li>A) Will the rain garden be irrigated?</li></ul>	Choose One VES NO
Notes:	

**Appendix E – HEC-RAS: Natural Drainage Course Hydraulics** 

The main natural drainage course was analyzed using HEC-RAS from the beginning of construction to the end of construction. The proposed swale has 4:1 side slopes and a 10 foot bottom width. A Mannings N-value of 0.35 was selected for the main channel flow with the overbank having a slightly higher value of 0.45 signifying weedy overgrowth. A Mannings N-value of 0.78 was used for the rip-rap areas.

Cross sections were created at the beginning, end, at grade breaks and the culvert crossing. Interpolated sections were added as needed. A normal depth was selected for the reach boundary conditions upstream and downstream. This could create an artificially high velocity at the beginning of the study zone and an artificially low velocity at the downstream end. The flow velocities were all below the 7-fps maximum desired for the blanket material as specified by the manufacturer.

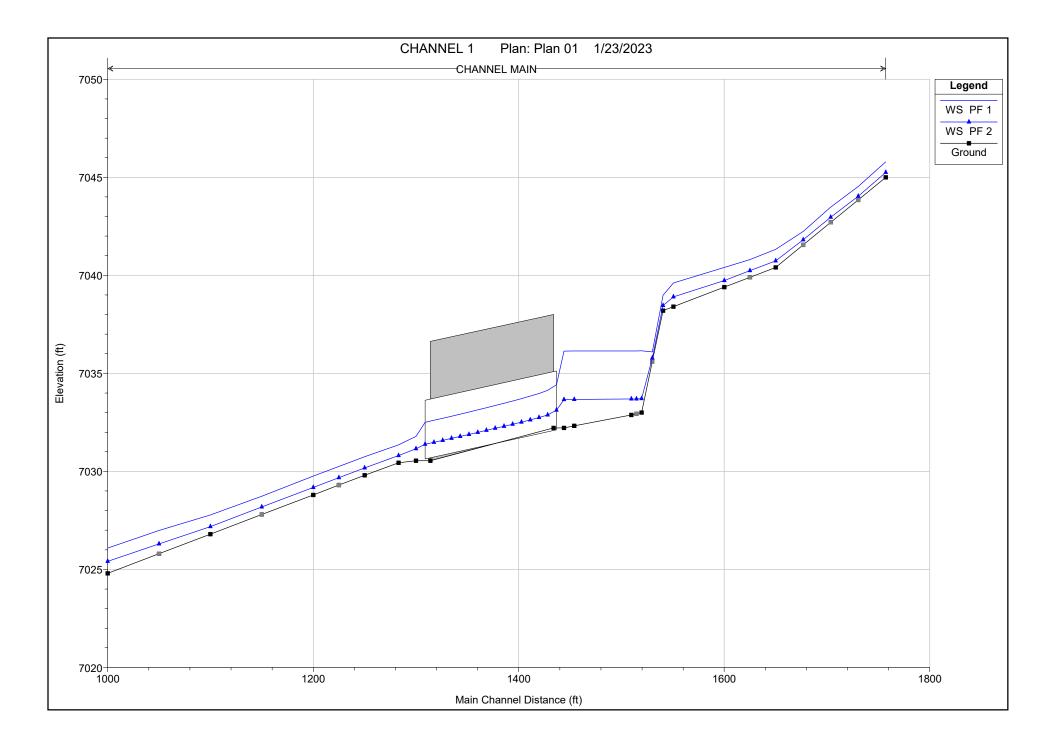
The Rational Calculation method was used for the channel and culvert analysis since the tributary area is less than 100-acres. Furthermore, the increase of flow was placed at the entrance to the culvert since HEC-RAS does not model the flow regime changes in the middle of a culvert. The flow regime change was modeled using the StormCAD software found in the Rational Calculation Appendix B.

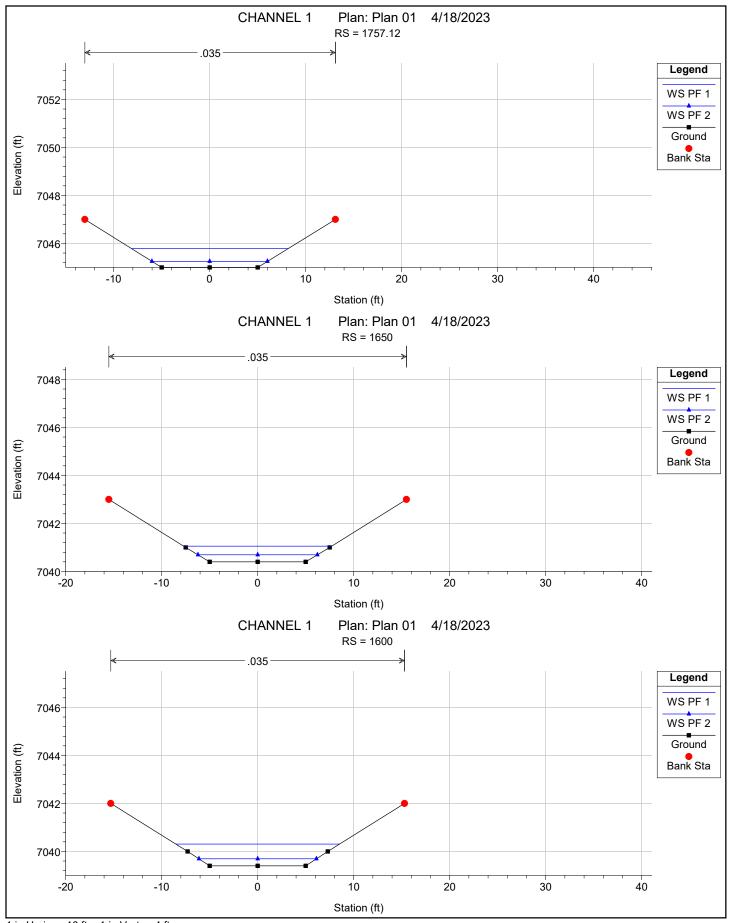
River Sta	Profile	Q Total	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope	Vel Chnl	Flow Area	Top Width	Froude # Chl
		(cfs)	(ft)	(ft)	(ft)	(ft)	(ft/ft)	(ft/s)	(sq ft)	(ft)	
1757.12	Q <sub>100</sub>	47	7045.0	7045.8	7045.8	7046.1	0.0212	4.5	10.4	16.3	1.0
1730.34*	Q <sub>100</sub>	47	7043.9	7044.4	7044.6	7045.2	0.0746	6.9	6.8	14.5	1.8
1703.56*	Q <sub>100</sub>	47	7042.7	7043.4	7043.5	7043.8	0.0346	5.4	8.8	15.6	1.3
1676.78*	Q <sub>100</sub>	47	7041.6	7042.2	7042.3	7042.8	0.0538	6.2	7.6	15	1.5
1650	Q <sub>100</sub>	47	7040.4	7041.1	7041.2	7041.6	0.0412	5.7	8.3	15.4	1.4
1625.00*	Q <sub>100</sub>	47	7039.9	7040.7	7040.7	7041.0	0.0214	4.5	10.3	16.3	1.0
1600	Q <sub>100</sub>	47	7039.4	7040.3	7040.2	7040.5	0.013	3.8	12.2	17.1	0.8
1550.5	Q <sub>100</sub>	47	7038.4	7039.6		7039.7	0.0198	2.6	17.9	19.7	0.5
1540.5	Q <sub>100</sub>	47	7038.2	7039.0	7039.0	7039.3	0.1072	4.6	10.3	16.3	1.0
1530.08*	Q <sub>100</sub>	47	7035.6	7036.1	7036.4	7037.1	0.5528	8.0	5.9	13.8	2.2
1519.65	Q <sub>100</sub>	47	7033.0	7036.1	7033.8	7036.2	0.0003	0.7	69.0	34.4	0.1
1514.65*	Q <sub>100</sub>	47	7032.9	7036.1		7036.2	0.0001	0.8	70.8	34.7	0.1
1509.65	Q <sub>100</sub>	47	7032.9	7036.1		7036.2	0.0001	0.8	72.6	35.1	0.1
1454	Q <sub>100</sub>	47	7032.3	7036.1		7036.1	0.0001	0.5	96.5	40.3	0.0
1444	Q <sub>100</sub>	50	7032.2	7036.1	7033.4	7036.1	0.0002	0.7	72.8	34.4	0.1
1436.75	Culvert	50									
1300	Q <sub>100</sub>	50	7030.5	7031.8	7031.5	7032.0	0.0309	3.6	14.2	16.5	0.6
1283	Q <sub>100</sub>	50	7030.4	7031.2	7031.2	7031.6	0.0176	4.6	11.1	16.5	0.9
1250	Q <sub>100</sub>	50	7029.8	7030.6	7030.6	7030.9	0.0196	4.5	11.1	16.7	1.0
1225.00*	Q <sub>100</sub>	50	7029.3	7030.1	7030.1	7030.4	0.0199	4.5	11.1	16.6	1.0
1200	Q <sub>100</sub>	50	7028.8	7029.6	7029.6	7029.9	0.0199	4.5	11.1	16.6	1.0
1150.00*	Q <sub>100</sub>	50	7027.8	7028.6	7028.6	7028.9	0.0204	4.6	11	16.6	1.0
1100	Q <sub>100</sub>	50	7026.8	7027.6	7027.6	7027.9	0.0195	4.5	11.1	16.7	1.0
1050.00*	Q <sub>100</sub>	50	7025.8	7026.9		7027.1	0.0137	4.0	12.4	16.7	0.8
1000	Q <sub>100</sub>	50	7024.8	7026.0	7025.9	7026.3	0.0199	4.7	10.7	15.3	1.0

See the charts, cross sections and profile below for more information.

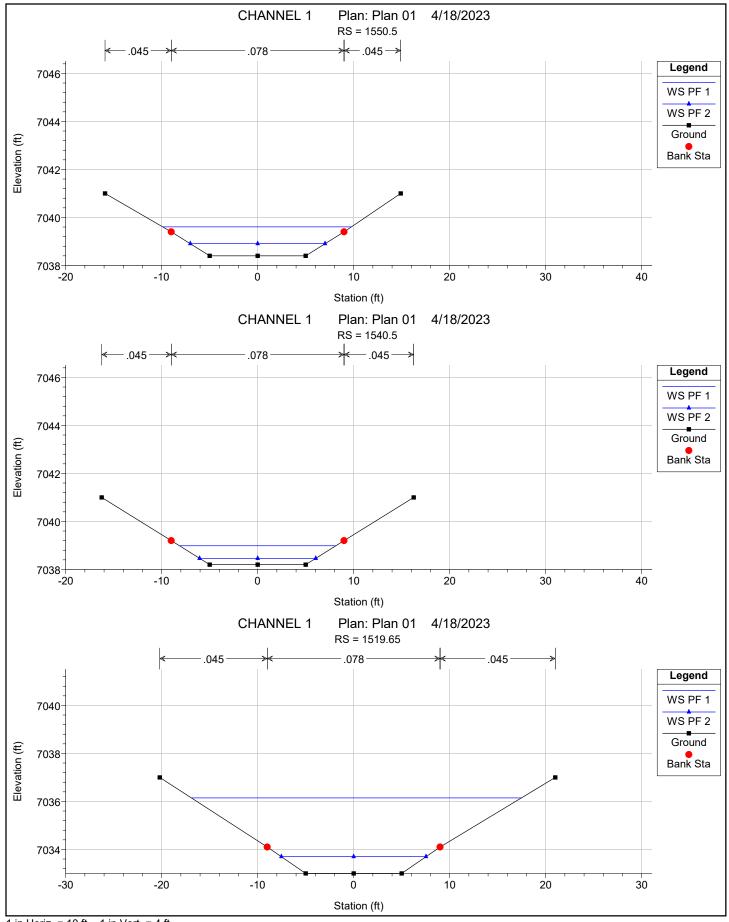
River Sta	Profile	Q Total	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope	Vel Chnl	Flow Area	Top Width	Froude # Chl
		(cfs)	(ft)	(ft)	(ft)	(ft)	(ft/ft)	(ft/s)	(sq ft)	(ft)	
1757.12	$Q_{\scriptscriptstyle{5}}$	8	7045.0	7045.3	7045.3	7045.4	0.0324	2.9	2.8	12.0	1.1
1730.34*	$Q_{\scriptscriptstyle{5}}$	8	7043.9	7044.1	7044.1	7044.3	0.0655	3.6	2.2	11.7	1.4
1703.56*	$Q_{\scriptscriptstyle{5}}$	8	7042.7	7042.9	7043.0	7043.1	0.0341	2.9	2.7	12.0	1.1
1676.78*	$Q_{\scriptscriptstyle{5}}$	8	7041.6	7041.8	7041.8	7042.0	0.0614	3.5	2.3	11.7	1.4
1650	$Q_{_{5}}$	8	7040.4	7040.7	7040.7	7040.8	0.0196	2.4	3.3	12.4	0.8
1625.00*	$Q_{\scriptscriptstyle{5}}$	8	7039.9	7040.2		7040.3	0.0204	2.5	3.2	12.3	0.9
1600	$Q_{\scriptscriptstyle{5}}$	8	7039.4	7039.7		7039.8	0.0196	2.5	3.3	12.2	0.8
1550.5	$Q_{\scriptscriptstyle{5}}$	8	7038.4	7038.9		7038.9	0.0148	1.3	6.1	14.0	0.4
1540.5	$Q_{\scriptscriptstyle{5}}$	8	7038.2	7038.5	7038.5	7038.6	0.1441	2.8	2.9	12.1	1.0
1530.08*	$Q_{\scriptscriptstyle{5}}$	8	7035.6	7035.8	7035.9	7036.0	0.4879	4.1	2.0	11.4	1.7
1519.65	$Q_{\scriptscriptstyle{5}}$	8	7033.0	7033.7	7033.3	7033.7	0.0048	0.9	8.8	15.1	0.2
1514.65*	$Q_{\scriptscriptstyle{5}}$	8	7032.9	7033.7		7033.7	0.0007	0.8	9.6	15.4	0.2
1509.65	$Q_{\scriptscriptstyle{5}}$	8	7032.9	7033.7		7033.7	0.0006	0.8	10.4	15.8	0.2
1454	$Q_{\scriptscriptstyle{5}}$	8	7032.3	7033.7		7033.7	0.0003	0.4	21.3	20.6	0.1
1444	$Q_{\scriptscriptstyle{5}}$	10	7032.2	7033.7	7032.6	7033.7	0.0013	0.8	13.1	13.8	0.1
1436.75	Culvert	10									
1300	$Q_{\scriptscriptstyle{5}}$	10	7030.5	7031.1		7031.2	0.0229	1.8	5.5	11.5	0.5
1283	$Q_{\scriptscriptstyle{5}}$	10	7030.4	7030.8		7030.9	0.0174	2.5	4.0	13.5	0.8
1250	$Q_{5}$	10	7029.8	7030.1	7030.1	7030.2	0.0206	2.7	3.7	12.7	0.9
1225.00*	$Q_{\scriptscriptstyle{5}}$	10	7029.3	7029.6		7029.7	0.0189	2.6	3.8	12.7	0.8
1200	$Q_{5}$	10	7028.8	7029.1	7029.1	7029.2	0.0211	2.7	3.7	12.6	0.9
1150.00*	$Q_{5}$	10	7027.8	7028.1	7028.1	7028.2	0.0189	2.6	3.8	12.7	0.8
1100	$Q_{5}$	10	7026.8	7027.1	7027.1	7027.2	0.0214	2.7	3.7	12.6	0.9
1050.00*	$Q_{5}$	10	7025.8	7026.2	7026.2	7026.3	0.0151	2.6	3.8	10.7	0.8
1000	$Q_5$	10	7024.8	7025.3	7025.3	7025.5	0.0199	3.0	3.3	8.9	0.9
River Sta	Profile	Q Culv		W.S. US.	Delta WS	E.G. US.	E.G. IC	E.G. OC	Culv Vel	Culv Vel DS	

River Sta	Profile	Q Culv	NIS IIS	Delta WS	FGUS	E.G. IC	E.G. OC	Culv Vel	Culv Vel
Triver Sta	FIUME	Q Cuiv	W.S. 05.	Della WS	L.G. 03.	L.G. IC	L.G. 00	US	DS
		(cfs)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft/s)	(ft/s)
1436.75	5 PF 1	50	7036.1	4.4	7036.1	7036.1	7036.1	8.6	10.8
Culvert #1	PF 2	10	7033.7	2.5	7033.7	7033.5	7033.7	4.8	7.2

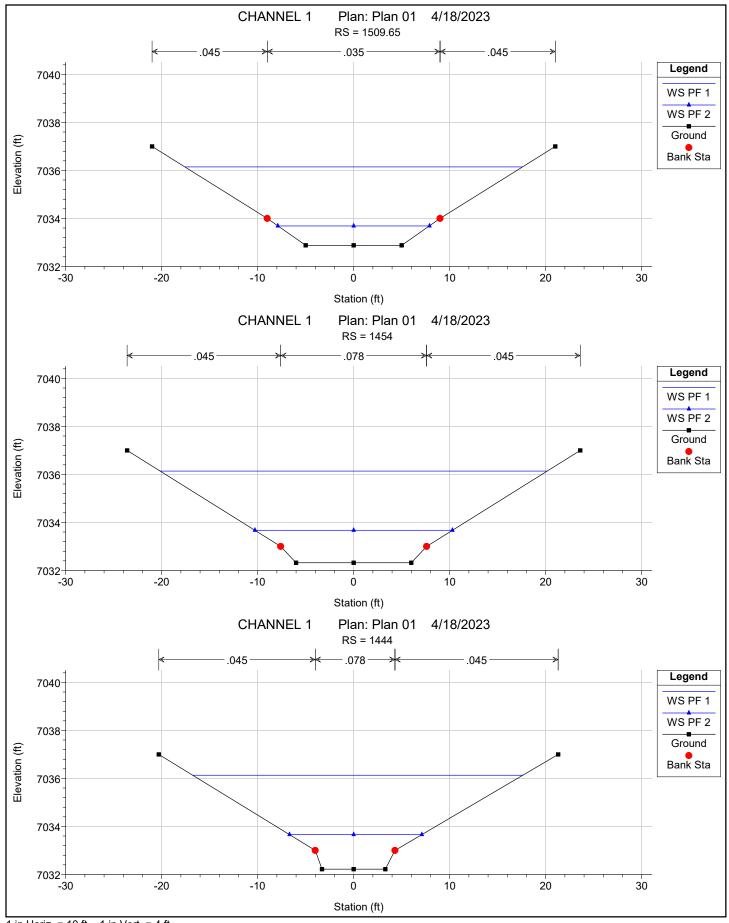




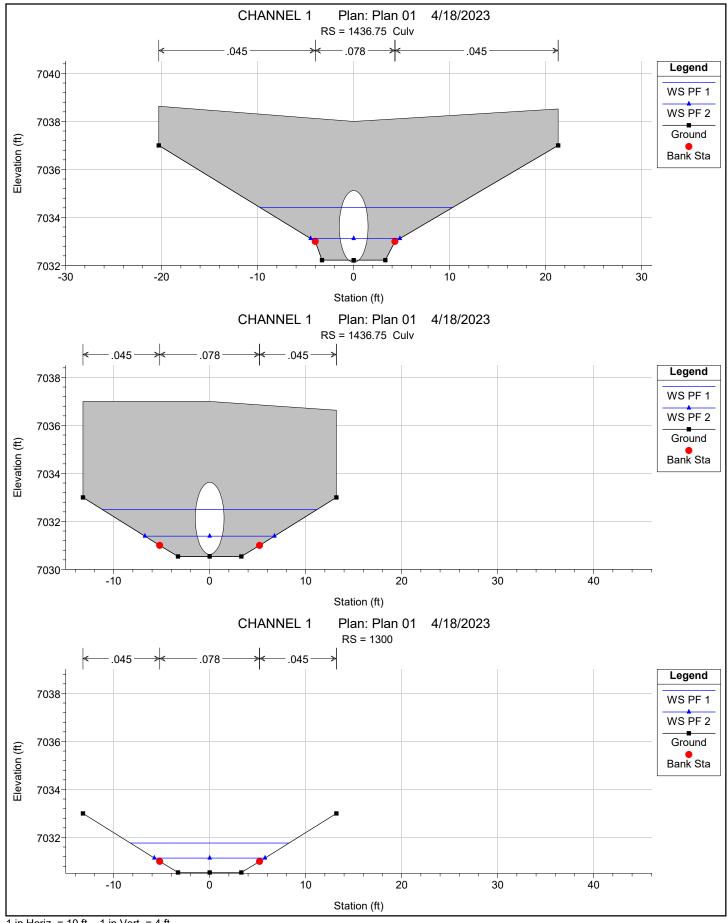
<sup>1</sup> in Horiz. = 10 ft 1 in Vert. = 4 ft



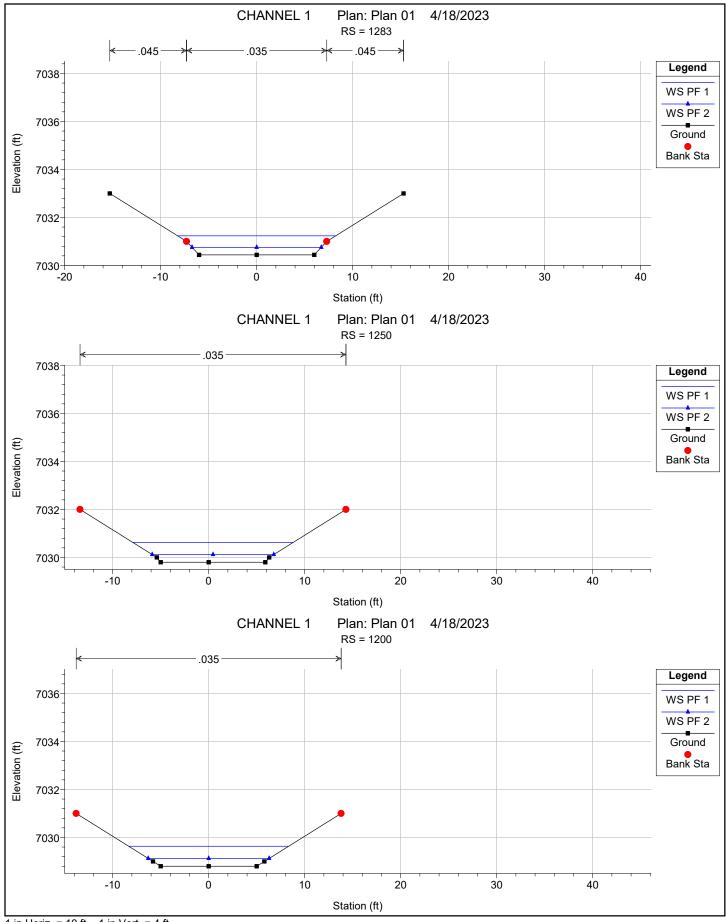
1 in Horiz. = 10 ft 1 in Vert. = 4 ft

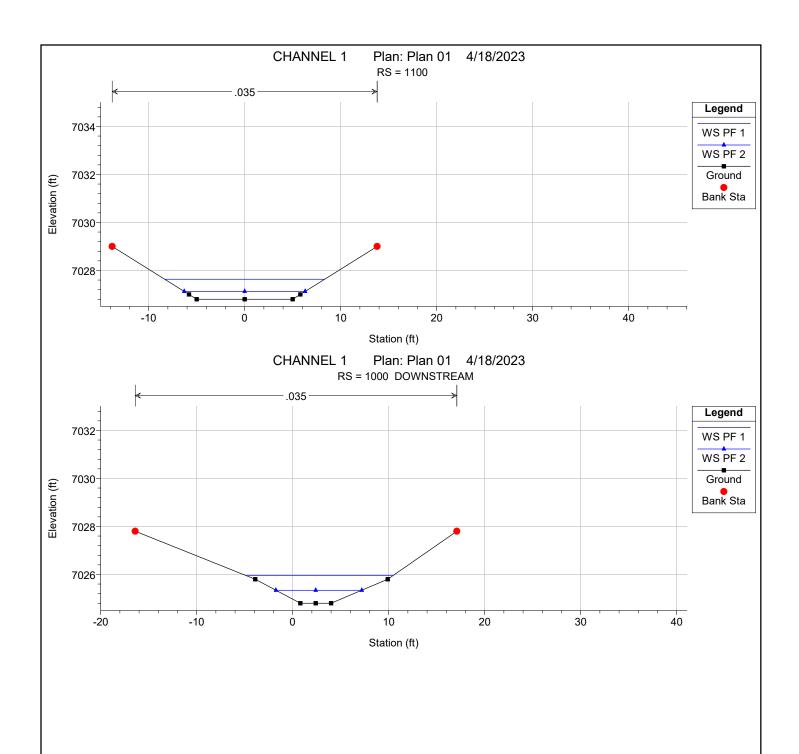


<sup>1</sup> in Horiz. = 10 ft 1 in Vert. = 4 ft



1 in Horiz. = 10 ft 1 in Vert. = 4 ft





Appendix F – Soil Resource Report



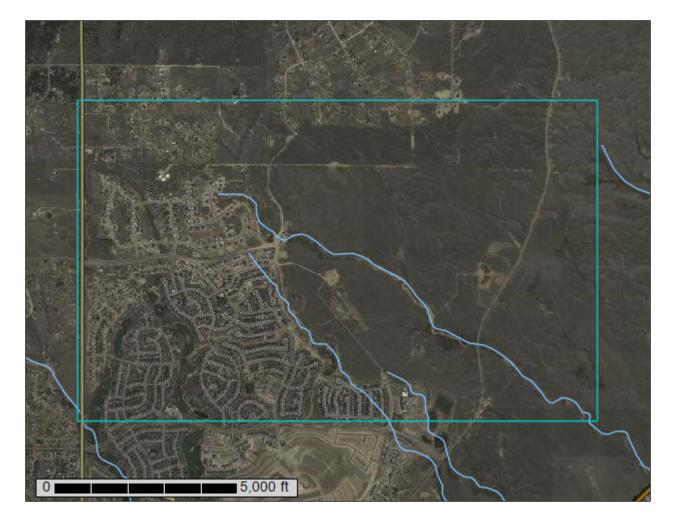
United States Department of Agriculture

Natural Resources Conservation

Service

A product of the National Cooperative Soil Survey, a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local participants

# Custom Soil Resource Report for El Paso County Area, Colorado



### Preface

Soil surveys contain information that affects land use planning in survey areas. They highlight soil limitations that affect various land uses and provide information about the properties of the soils in the survey areas. Soil surveys are designed for many different users, including farmers, ranchers, foresters, agronomists, urban planners, community officials, engineers, developers, builders, and home buyers. Also, conservationists, teachers, students, and specialists in recreation, waste disposal, and pollution control can use the surveys to help them understand, protect, or enhance the environment.

Various land use regulations of Federal, State, and local governments may impose special restrictions on land use or land treatment. Soil surveys identify soil properties that are used in making various land use or land treatment decisions. The information is intended to help the land users identify and reduce the effects of soil limitations on various land uses. The landowner or user is responsible for identifying and complying with existing laws and regulations.

Although soil survey information can be used for general farm, local, and wider area planning, onsite investigation is needed to supplement this information in some cases. Examples include soil quality assessments (http://www.nrcs.usda.gov/wps/portal/nrcs/main/soils/health/) and certain conservation and engineering applications. For more detailed information, contact your local USDA Service Center (https://offices.sc.egov.usda.gov/locator/app?agency=nrcs) or your NRCS State Soil Scientist (http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/contactus/? cid=nrcs142p2\_053951).

Great differences in soil properties can occur within short distances. Some soils are seasonally wet or subject to flooding. Some are too unstable to be used as a foundation for buildings or roads. Clayey or wet soils are poorly suited to use as septic tank absorption fields. A high water table makes a soil poorly suited to basements or underground installations.

The National Cooperative Soil Survey is a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local agencies. The Natural Resources Conservation Service (NRCS) has leadership for the Federal part of the National Cooperative Soil Survey.

Information about soils is updated periodically. Updated information is available through the NRCS Web Soil Survey, the site for official soil survey information.

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## **How Soil Surveys Are Made**

Soil surveys are made to provide information about the soils and miscellaneous areas in a specific area. They include a description of the soils and miscellaneous areas and their location on the landscape and tables that show soil properties and limitations affecting various uses. Soil scientists observed the steepness, length, and shape of the slopes; the general pattern of drainage; the kinds of crops and native plants; and the kinds of bedrock. They observed and described many soil profiles. A soil profile is the sequence of natural layers, or horizons, in a soil. The profile extends from the surface down into the unconsolidated material in which the soil formed or from the surface down to bedrock. The unconsolidated material is devoid of roots and other living organisms and has not been changed by other biological activity.

Currently, soils are mapped according to the boundaries of major land resource areas (MLRAs). MLRAs are geographically associated land resource units that share common characteristics related to physiography, geology, climate, water resources, soils, biological resources, and land uses (USDA, 2006). Soil survey areas typically consist of parts of one or more MLRA.

The soils and miscellaneous areas in a survey area occur in an orderly pattern that is related to the geology, landforms, relief, climate, and natural vegetation of the area. Each kind of soil and miscellaneous area is associated with a particular kind of landform or with a segment of the landform. By observing the soils and miscellaneous areas in the survey area and relating their position to specific segments of the landform, a soil scientist develops a concept, or model, of how they were formed. Thus, during mapping, this model enables the soil scientist to predict with a considerable degree of accuracy the kind of soil or miscellaneous area at a specific location on the landscape.

Commonly, individual soils on the landscape merge into one another as their characteristics gradually change. To construct an accurate soil map, however, soil scientists must determine the boundaries between the soils. They can observe only a limited number of soil profiles. Nevertheless, these observations, supplemented by an understanding of the soil-vegetation-landscape relationship, are sufficient to verify predictions of the kinds of soil in an area and to determine the boundaries.

Soil scientists recorded the characteristics of the soil profiles that they studied. They noted soil color, texture, size and shape of soil aggregates, kind and amount of rock fragments, distribution of plant roots, reaction, and other features that enable them to identify soils. After describing the soils in the survey area and determining their properties, the soil scientists assigned the soils to taxonomic classes (units). Taxonomic classes are concepts. Each taxonomic class has a set of soil characteristics with precisely defined limits. The classes are used as a basis for comparison to classify soils systematically. Soil taxonomy, the system of taxonomic classification used in the United States, is based mainly on the kind and character of soil properties and the arrangement of horizons within the profile. After the soil

scientists classified and named the soils in the survey area, they compared the individual soils with similar soils in the same taxonomic class in other areas so that they could confirm data and assemble additional data based on experience and research.

The objective of soil mapping is not to delineate pure map unit components; the objective is to separate the landscape into landforms or landform segments that have similar use and management requirements. Each map unit is defined by a unique combination of soil components and/or miscellaneous areas in predictable proportions. Some components may be highly contrasting to the other components of the map unit. The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The delineation of such landforms and landform segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, onsite investigation is needed to define and locate the soils and miscellaneous areas.

Soil scientists make many field observations in the process of producing a soil map. The frequency of observation is dependent upon several factors, including scale of mapping, intensity of mapping, design of map units, complexity of the landscape, and experience of the soil scientist. Observations are made to test and refine the soil-landscape model and predictions and to verify the classification of the soils at specific locations. Once the soil-landscape model is refined, a significantly smaller number of measurements of individual soil properties are made and recorded. These measurements may include field measurements, such as those for color, depth to bedrock, and texture, and laboratory measurements, such as those for content of sand, silt, clay, salt, and other components. Properties of each soil typically vary from one point to another across the landscape.

Observations for map unit components are aggregated to develop ranges of characteristics for the components. The aggregated values are presented. Direct measurements do not exist for every property presented for every map unit component. Values for some properties are estimated from combinations of other properties.

While a soil survey is in progress, samples of some of the soils in the area generally are collected for laboratory analyses and for engineering tests. Soil scientists interpret the data from these analyses and tests as well as the field-observed characteristics and the soil properties to determine the expected behavior of the soils under different uses. Interpretations for all of the soils are field tested through observation of the soils in different uses and under different levels of management. Some interpretations are modified to fit local conditions, and some new interpretations are developed to meet local needs. Data are assembled from other sources, such as research information, production records, and field experience of specialists. For example, data on crop yields under defined levels of management are assembled from farm records and from field or plot experiments on the same kinds of soil.

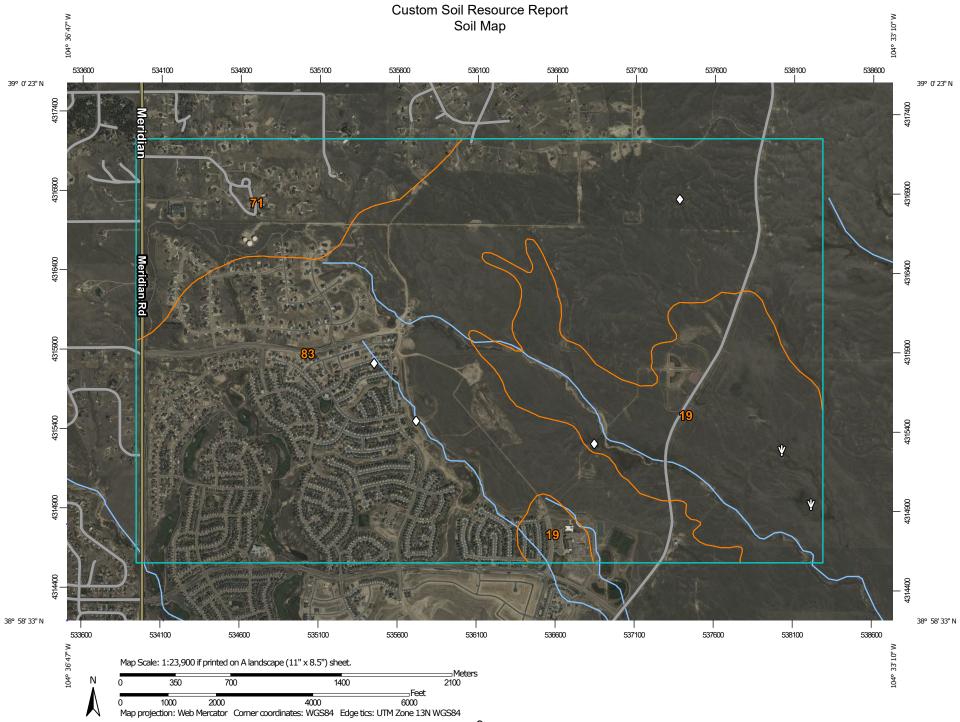
Predictions about soil behavior are based not only on soil properties but also on such variables as climate and biological activity. Soil conditions are predictable over long periods of time, but they are not predictable from year to year. For example, soil scientists can predict with a fairly high degree of accuracy that a given soil will have a high water table within certain depths in most years, but they cannot predict that a high water table will always be at a specific level in the soil on a specific date.

After soil scientists located and identified the significant natural bodies of soil in the survey area, they drew the boundaries of these bodies on aerial photographs and

identified each as a specific map unit. Aerial photographs show trees, buildings, fields, roads, and rivers, all of which help in locating boundaries accurately.

# Soil Map

The soil map section includes the soil map for the defined area of interest, a list of soil map units on the map and extent of each map unit, and cartographic symbols displayed on the map. Also presented are various metadata about data used to produce the map, and a description of each soil map unit.



MAP	LEGEND	MAP INFORMATION
Area of Interest (AOI) Area of Interest (AOI)	<ul><li>Spoil Area</li><li>Stony Spot</li></ul>	The soil surveys that comprise your AOI were mapp 1:24,000.
Soils Soil Map Unit Polygons Soil Map Unit Lines	s 🕅 Very Stony Spot	Please rely on the bar scale on each map sheet for n measurements.
Soil Map Unit Points	<ul><li>△ Other</li><li>✓ Special Line Features</li></ul>	Source of Map: Natural Resources Conservation S Web Soil Survey URL: Coordinate System: Web Mercator (EPSG:3857)
<ul> <li>Blowout</li> <li>Borrow Pit</li> <li>Clay Spot</li> <li>Closed Depression</li> </ul>	Water Features Streams and Canals Transportation HIT Rails	Maps from the Web Soil Survey are based on the W projection, which preserves direction and shape but distance and area. A projection that preserves area, Albers equal-area conic projection, should be used i accurate calculations of distance or area are require
Gravel Pit Gravelly Spot	<ul> <li>Interstate Highways</li> <li>US Routes</li> <li>Major Roads</li> </ul>	This product is generated from the USDA-NRCS cer of the version date(s) listed below.
<ul> <li>Landfill</li> <li>Lava Flow</li> <li>Marsh or swamp</li> </ul>	Local Roads  Background  Aerial Photography	Soil Survey Area: El Paso County Area, Colorado Survey Area Data: Version 19, Aug 31, 2021 Soil map units are labeled (as space allows) for map
<ul> <li>Mine or Quarry</li> <li>Miscellaneous Water</li> <li>Perennial Water</li> </ul>		1:50,000 or larger. Date(s) aerial images were photographed: Sep 11, 20, 2018
<ul> <li>Rock Outcrop</li> <li>Saline Spot</li> <li>Sandy Spot</li> </ul>		The orthophoto or other base map on which the soil compiled and digitized probably differs from the back imagery displayed on these maps. As a result, some
<ul> <li>Severely Eroded Spot</li> <li>Sinkhole</li> </ul>		shifting of map unit boundaries may be evident.
Slide or Slip		

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ap scales

11, 2018—Oct

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### **Map Unit Legend**

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
19	Columbine gravelly sandy loam, 0 to 3 percent slopes	575.5	20.0%
71	Pring coarse sandy loam, 3 to 8 percent slopes	339.8	11.8%
83	Stapleton sandy loam, 3 to 8 percent slopes	1,964.3	68.2%
Totals for Area of Interest		2,879.9	100.0%

#### **Map Unit Descriptions**

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or

landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An *association* is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

### El Paso County Area, Colorado

### 19—Columbine gravelly sandy loam, 0 to 3 percent slopes

### **Map Unit Setting**

National map unit symbol: 367p Elevation: 6,500 to 7,300 feet Mean annual precipitation: 14 to 16 inches Mean annual air temperature: 46 to 50 degrees F Frost-free period: 125 to 145 days Farmland classification: Not prime farmland

### **Map Unit Composition**

Columbine and similar soils: 97 percent Minor components: 3 percent Estimates are based on observations, descriptions, and transects of the mapunit.

### **Description of Columbine**

### Setting

Landform: Flood plains, fan terraces, fans Down-slope shape: Linear Across-slope shape: Linear Parent material: Alluvium

### **Typical profile**

*A - 0 to 14 inches:* gravelly sandy loam *C - 14 to 60 inches:* very gravelly loamy sand

### **Properties and qualities**

Slope: 0 to 3 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Well drained
Runoff class: Very low
Capacity of the most limiting layer to transmit water (Ksat): High to very high (5.95 to 19.98 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Available water supply, 0 to 60 inches: Very low (about 2.5 inches)

### Interpretive groups

Land capability classification (irrigated): 4e Land capability classification (nonirrigated): 6e Hydrologic Soil Group: A Ecological site: R049XY214CO - Gravelly Foothill Hydric soil rating: No

### **Minor Components**

### Fluvaquentic haplaquolls

Percent of map unit: 1 percent Landform: Swales Hydric soil rating: Yes

### Other soils

Percent of map unit: 1 percent Hydric soil rating: No

### Pleasant

Percent of map unit: 1 percent Landform: Depressions Hydric soil rating: Yes

### 71—Pring coarse sandy loam, 3 to 8 percent slopes

### Map Unit Setting

National map unit symbol: 369k Elevation: 6,800 to 7,600 feet Farmland classification: Not prime farmland

### Map Unit Composition

*Pring and similar soils:* 85 percent *Estimates are based on observations, descriptions, and transects of the mapunit.* 

### **Description of Pring**

### Setting

Landform: Hills Landform position (three-dimensional): Side slope Down-slope shape: Linear Across-slope shape: Linear Parent material: Arkosic alluvium derived from sedimentary rock

### **Typical profile**

A - 0 to 14 inches: coarse sandy loam C - 14 to 60 inches: gravelly sandy loam

### **Properties and qualities**

Slope: 3 to 8 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Well drained
Runoff class: Low
Capacity of the most limiting layer to transmit water (Ksat): High (2.00 to 6.00 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Available water supply, 0 to 60 inches: Low (about 6.0 inches)

### Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 3e Hydrologic Soil Group: B Ecological site: R048AY222CO - Loamy Park Hydric soil rating: No

### **Minor Components**

### Pleasant

Percent of map unit: Landform: Depressions Hydric soil rating: Yes

### Other soils

Percent of map unit: Hydric soil rating: No

### 83—Stapleton sandy loam, 3 to 8 percent slopes

### Map Unit Setting

National map unit symbol: 369z Elevation: 6,500 to 7,300 feet Mean annual precipitation: 14 to 16 inches Mean annual air temperature: 46 to 48 degrees F Frost-free period: 125 to 145 days Farmland classification: Not prime farmland

### Map Unit Composition

Stapleton and similar soils: 97 percent Minor components: 3 percent Estimates are based on observations, descriptions, and transects of the mapunit.

### **Description of Stapleton**

### Setting

Landform: Hills Landform position (three-dimensional): Side slope Down-slope shape: Linear Across-slope shape: Linear Parent material: Sandy alluvium derived from arkose

### **Typical profile**

A - 0 to 11 inches: sandy loam Bw - 11 to 17 inches: gravelly sandy loam C - 17 to 60 inches: gravelly loamy sand

### **Properties and qualities**

Slope: 3 to 8 percent Depth to restrictive feature: More than 80 inches Drainage class: Well drained Runoff class: Low Capacity of the most limiting layer to transmit water (Ksat): High (2.00 to 6.00 in/hr) Depth to water table: More than 80 inches Frequency of flooding: None Frequency of ponding: None Available water supply, 0 to 60 inches: Low (about 4.7 inches)

### Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 3e Hydrologic Soil Group: B Ecological site: R049XY214CO - Gravelly Foothill Hydric soil rating: No

### **Minor Components**

### Fluvaquentic haplaquolls

Percent of map unit: 1 percent Landform: Swales Hydric soil rating: Yes

### Other soils

Percent of map unit: 1 percent Hydric soil rating: No

### Pleasant

Percent of map unit: 1 percent Landform: Depressions Hydric soil rating: Yes

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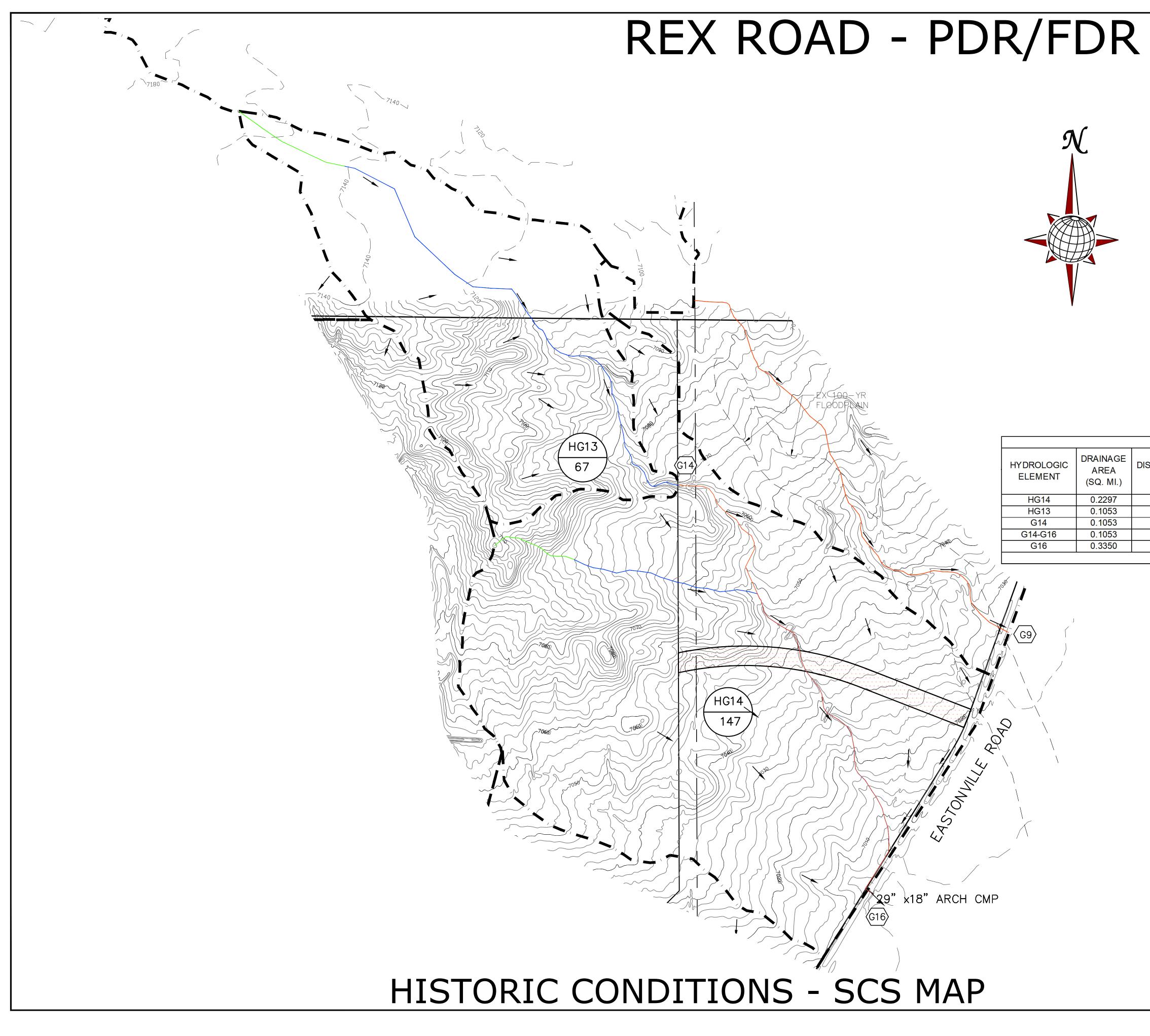
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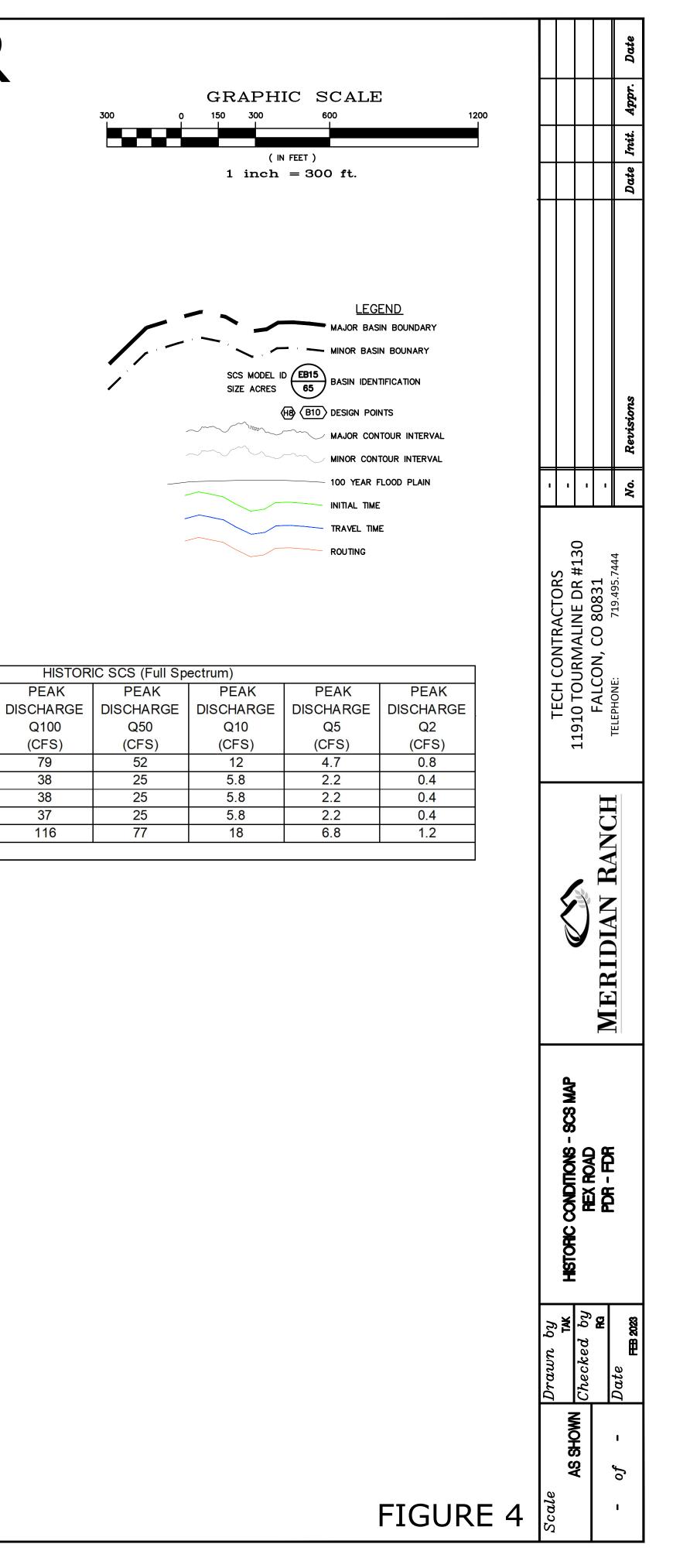
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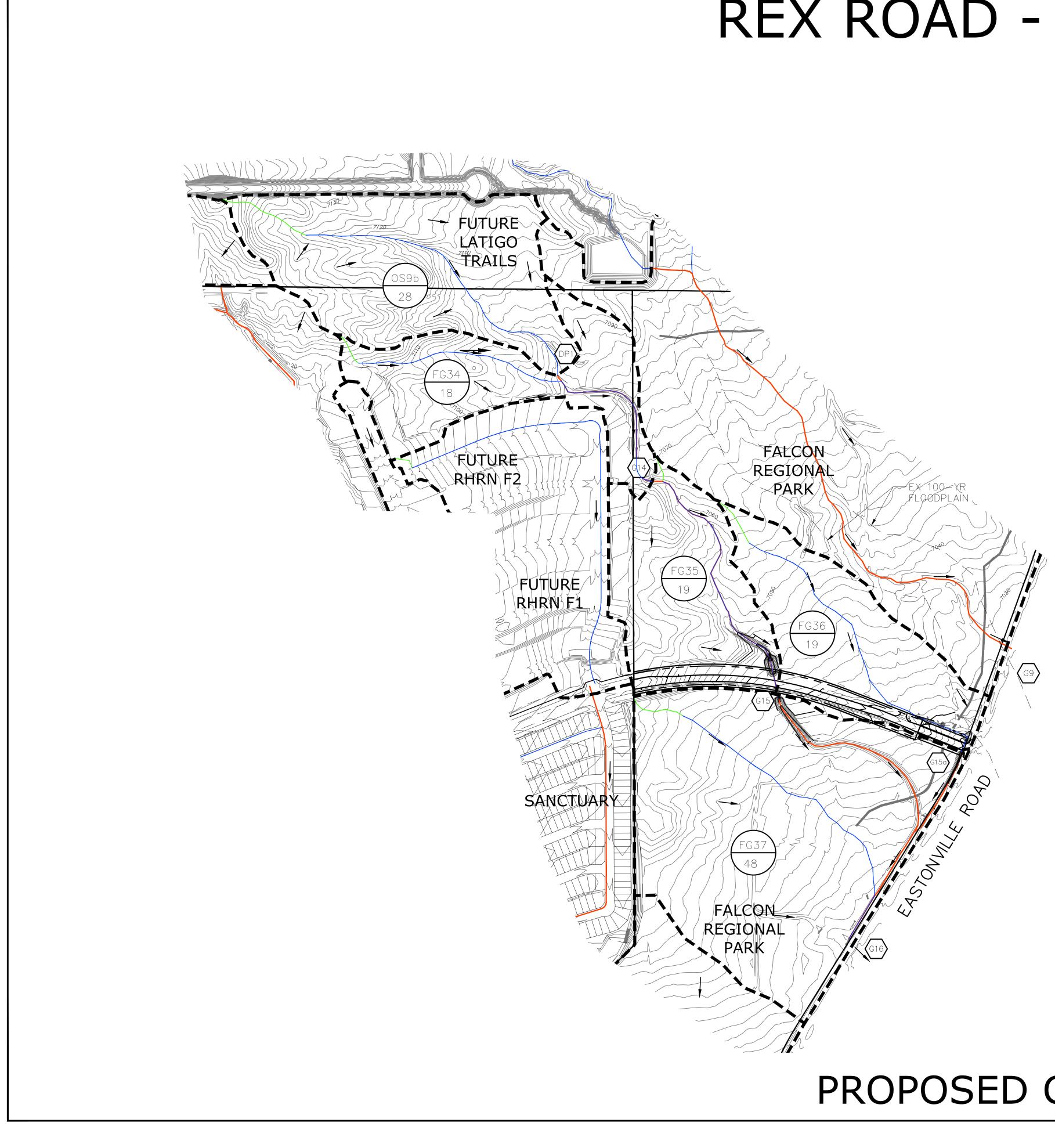
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Appendix G – Drainage Maps



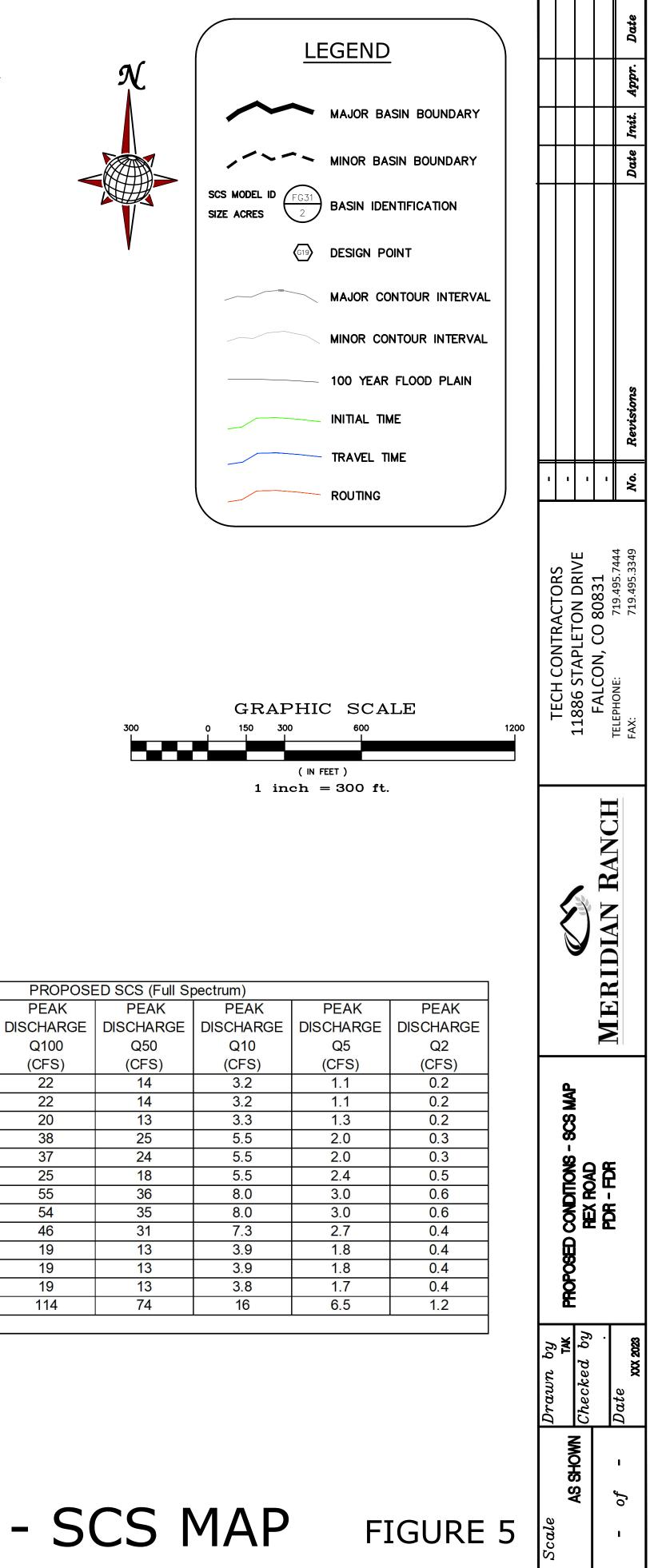


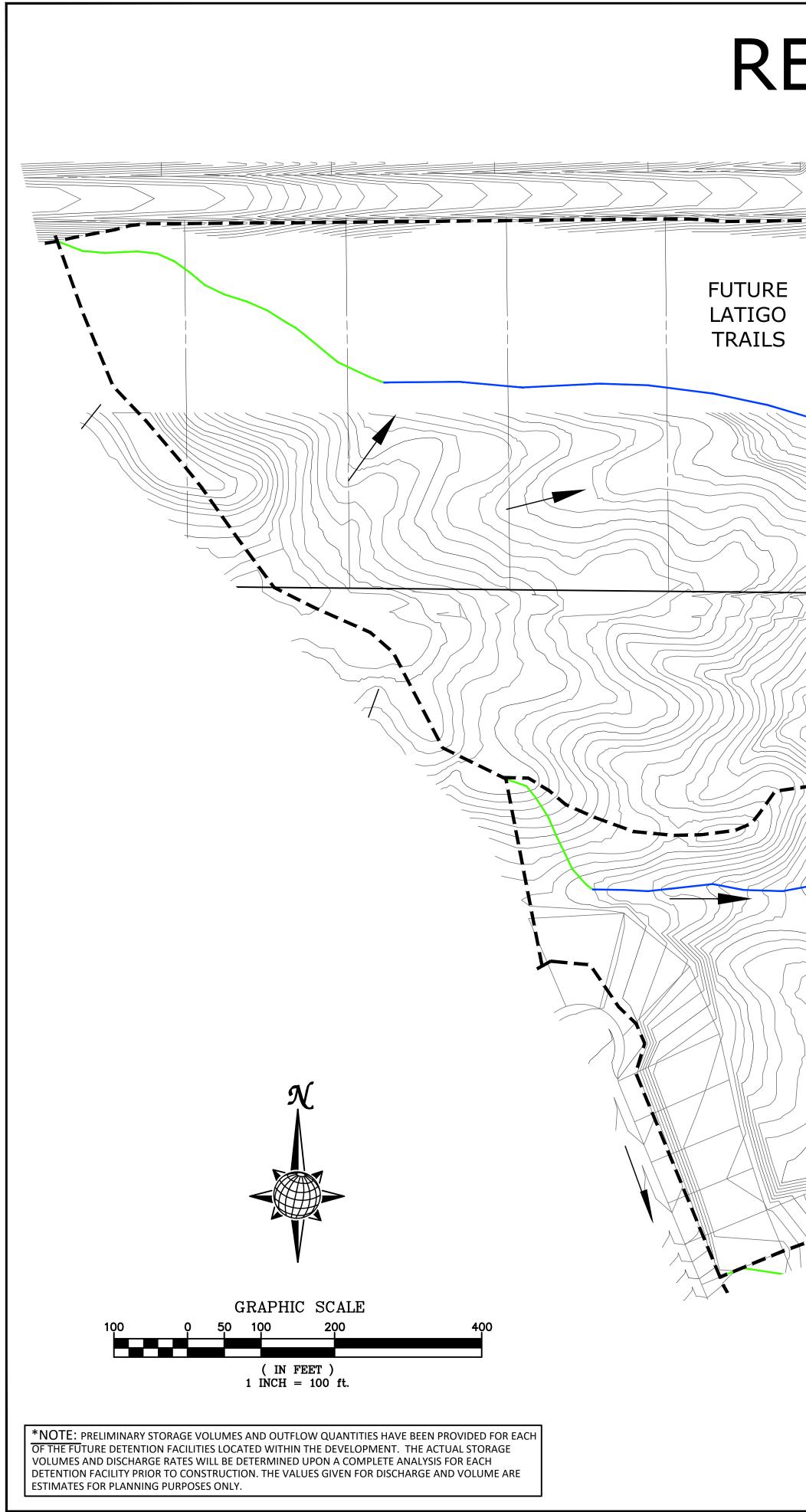


## REX ROAD - PDR/FDR

HYDROLOGIC ELEMENT	DRAINAGE AREA (SQ. MI.)	
OS09b	0.0435	
OS09b-G14	0.0435	
FG34	0.0275	
G14	0.0710	
G14-G15	0.0710	
FG35	0.0292	
G15	0.1002	
G15-G16	0.1002	
FG37	0.0754	
FG36	0.0295	
G15a	0.0295	
G15a-G16	0.0295	
G16	0.2051	
G16	0.2051	

### PROPOSED CONDITIONS - SCS MAP

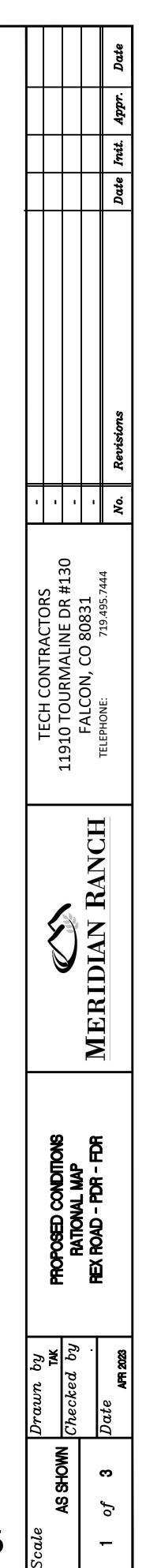


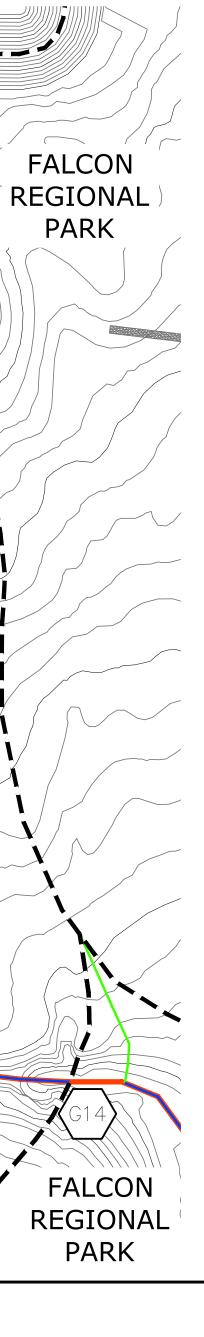


# RATIONAL MAP

	DP	BASIN	AREA
			(AC)
	DP1	OS09b	28
	G14	FG34	18
	G15.1	FG35a	14
	101	FG35b	4.9
	C15-1	5020	10
	G15a1	FG36a	16
	G15a	FG36c	3
	G15a G15		
	G15 G16a		
	0108		
	G16	FG37	48
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OS09b			
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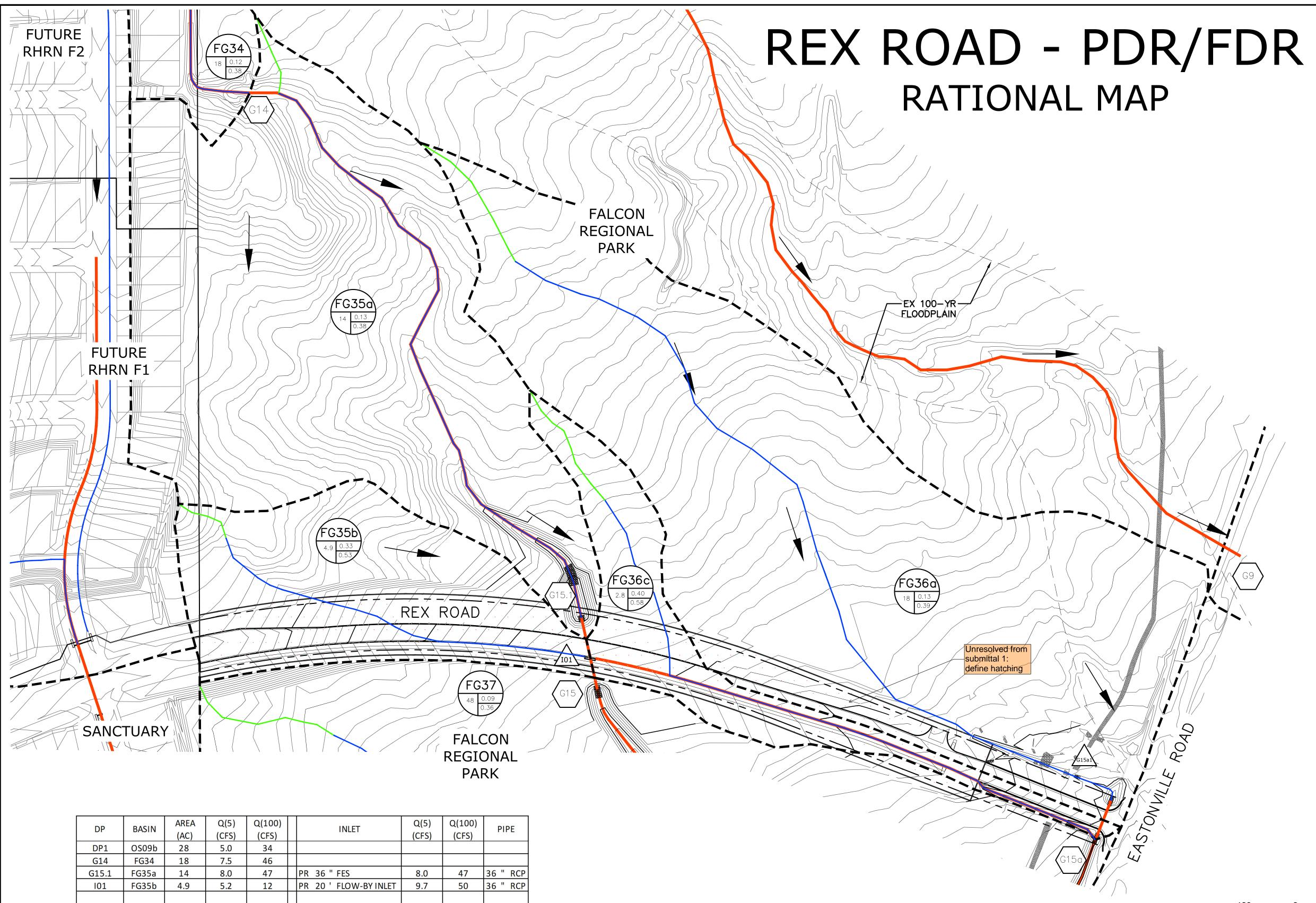
Q(5)	Q(100)	INLET	Q(5)	Q(100)	PIPE
(CFS)	(CFS)		(CFS)	(CFS)	
5.0	34				
7.5	46				
8.0	47	PR 36 " FES	8.0	47	36 " RCP
5.2	12	PR 20 ' FLOW-BY INLET	9.7	50	36 " RCP
4.9	23	PR 24 " FES	4.9	23	24 " RCP
4.2	12	PR GRASS SWALE	4.2	12	
8.0	32	PR GRASS SWALE	8.0	32	
9.7	50	PR GRASS SWALE	9.7	50	
12	59	PR GRASS SWALE	12	59	
15	78	EX REX ROAD CULVERT	15	78	
-		 -			



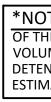


I	DEX MAP N.T.S.
	BASIN DESIGNATION
GO1 2.7 0.40 0.55 BASIN AREA IN ACRES	SUB-WATERSHED DESIGNATION MINOR/MAJOR STORM COEFFICIENT
61	DESIGN POINT DESIGNATION
	MAJOR BASIN BOUNDARY
	SUB-BASIN BOUNDARY
——6130— —	EXISTING CONTOUR
6130	PROPOSED COUNTOUR
0	PROPOSED STORM SEWER
	INITIAL OVERLAND TIME (TI)
	TRAVEL TIME (Tt)
	OVERLAND TIME (To)





DP	BASIN	AREA (AC)	Q(5) (CFS)	Q(100) (CFS)	INLET	Q(5) (CFS)	Q(100) (CFS)	PIPE
DP1	OS09b	28	5.0	34				
G14	FG34	18	7.5	46				
G15.1	FG35a	14	<mark>8.0</mark>	47	PR 36 " FES	8.0	47	36 " RCP
101	FG35b	4.9	5.2	12	PR 20 ' FLOW-BY INLET	9.7	50	36 " RCP
G15a1	FG36a	18	5.3	26	PR 24 " FES	5.3	26	24 " RCP
G15a	FG36c	3	4.2	12	PR GRASS SWALE	4.2	12	
G15a			8.3	34	PR GRASS SWALE	8.3	34	
G15			9.7	50	PR GRASS SWALE	9.7	50	
G16a			12	60	PR GRASS SWALE	12	60	
G16	FG37	48	15	79	EX REX ROAD CULVERT	15	79	



G9

_1	NDEX MAP
	N.T.S.
GO1	- BASIN DESIGNATION
2.7 0.40	SUB-WATERSHED DESIGNATION
BASIN ARE IN ACRES	STORM COEFFICIENT
61	DESIGN POINT DESIGNATION
	MAJOR BASIN BOUNDARY
	SUB-BASIN BOUNDARY
	- EXISTING CONTOUR
6130	- PROPOSED COUNTOUR
0	PROPOSED STORM SEWER
	- INITIAL OVERLAND TIME (TI)
	— TRAVEL TIME (Tt)
	- OVERLAND TIME (To)

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GRAPHIC SCALE 200 ( IN FEET ) 1 INCH = 100 ft.

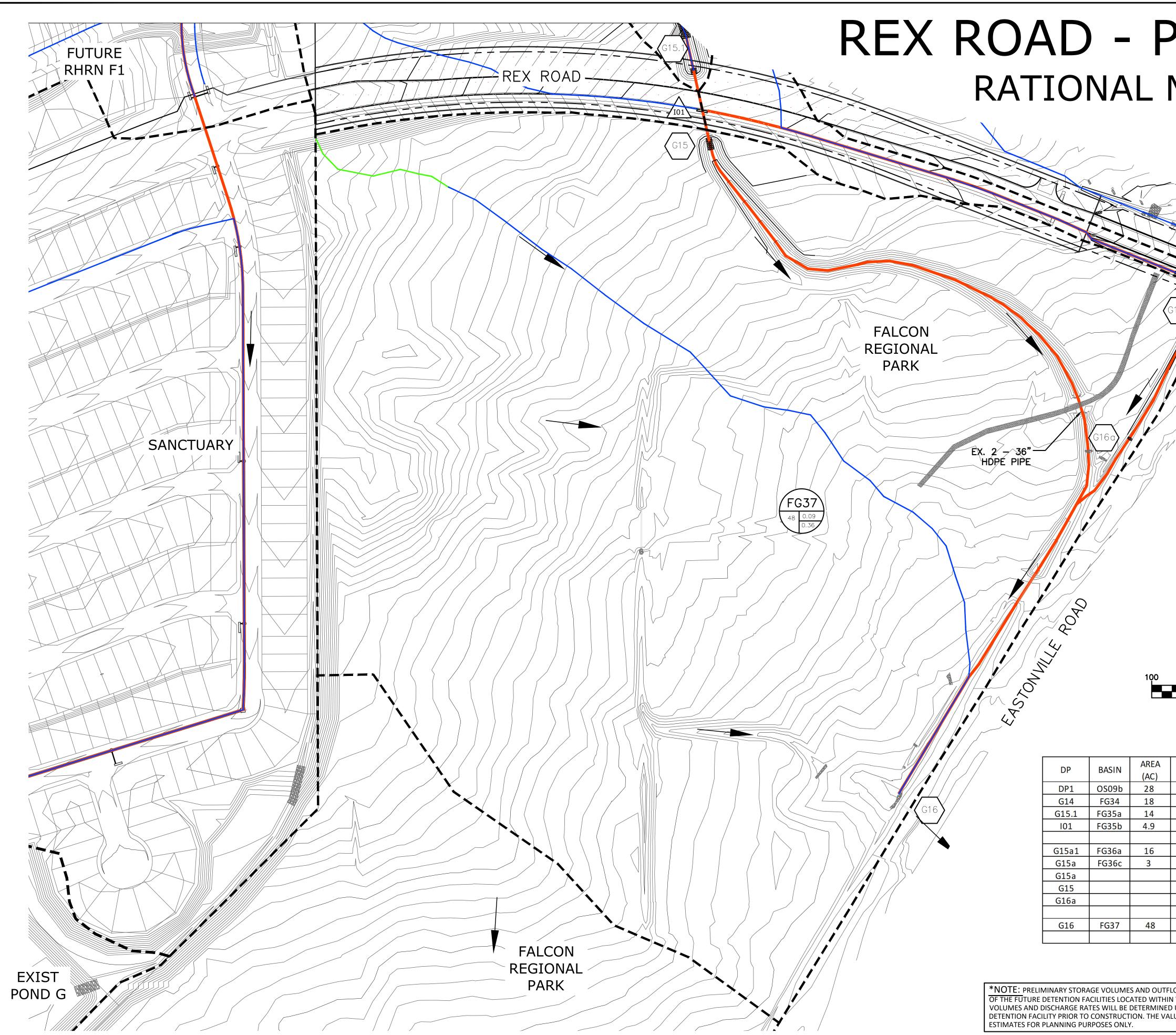
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FIGURE 6

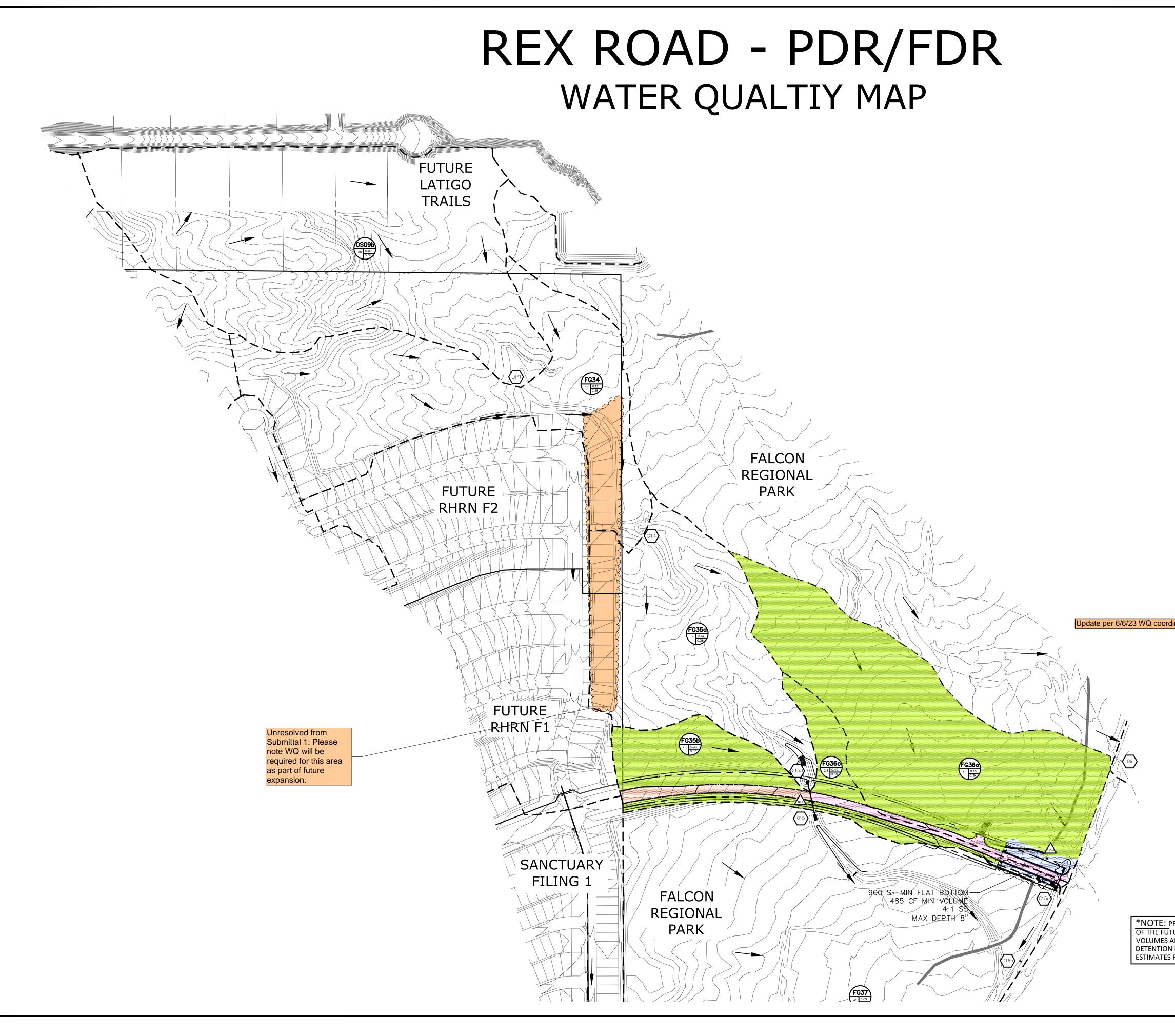
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Q(5) CFS) 5.0 7.5 8.0	50 10 1 J Q(100) (CFS) 34	00 200 ( IN FEET ) INCH = 100 ft.	Q(5)	Q(100)	PIPE 36 " RCP 36 " RCP	IOPOSED CONDITIONS	
Q(5) CFS) 5.0 7.5 8.0 5.2	50 10 1 1 Q(100) (CFS) 34 46 47 12	00 200 ( IN FEET ) INCH = 100 ft. INLET PR 36 " FES PR 20 ' FLOW-BY INLET	Q(5) (CFS) 8.0 9.7	Q(100) (CFS) 47 50	36 " RCP 36 " RCP	PROPOSED CONDITIONS	
Q(5) CFS) 5.0 7.5 3.0 5.2 4.9 4.2	50 10 1 J Q(100) (CFS) 34 46 47 12 23 12	200         ( IN FEET )         INCH = 100 ft.         INLET         PR 36 " FES         PR 20 ' FLOW-BY INLET         PR 24 " FES         PR GRASS SWALE	Q(5) (CFS) 8.0 9.7 4.9 4.2	Q(100) (CFS) 47 50 23 12	36 " RCP	PROPOSED CONDITIONS	
2(5) 5.0 7.5 3.0 5.2 4.9 4.2 3.0 9.7	50 10 1 1 Q(100) (CFS) 34 46 47 12 23 12 32 50	200         ( IN FEET )         INCH = 100 ft.         INLET         PR 36 " FES         PR 20 ' FLOW-BY INLET         PR 24 " FES         PR GRASS SWALE         PR GRASS SWALE         PR GRASS SWALE         PR GRASS SWALE	Q(5) (CFS) 8.0 9.7 4.9 4.2 8.0 9.7	Q(100) (CFS) 47 50 23 12 32 50	36 " RCP 36 " RCP		- RATIONAL MAP REX ROAD - PDR - FDR
Q(5) CFS) 5.0 7.5 3.0 5.2 4.9 4.2 3.0 9.7 12	50 10 1 1 Q(100) (CFS) 34 46 47 12 23 12 32	200         ( IN FEET )         INCH = 100 ft.         INLET         PR 36 " FES         PR 20 ' FLOW-BY INLET         PR 24 " FES         PR GRASS SWALE         PR GRASS SWALE	Q(5) (CFS) 8.0 9.7 4.9 4.2 8.0	Q(100) (CFS) 47 50 23 12 32	36 " RCP 36 " RCP	by TAK	oy     RATIONAL MAP       .     .    .
Q(5) 5.0 7.5 8.0 5.2 4.9 4.2 8.0 9.7 12 15	50 10 1 J Q(100) (CFS) 34 46 47 12 23 12 32 50 59 9	200       200         ( IN FEET )       INCH = 100 ft.         INCH = 100 ft.       INLET         PR 36 " FES       PR 20 ' FLOW-BY INLET         PR 20 ' FLOW-BY INLET       PR GRASS SWALE         PR GRASS SWALE       PR GRASS SWALE         PR GRASS SWALE       PR GRASS SWALE         PR GRASS SWALE       PR GRASS SWALE	Q(5) (CFS) 8.0 9.7 4.9 4.2 8.0 9.7 12	Q(100) (CFS) 47 50 23 12 32 50 59 59	36 " RCP 36 " RCP	by TAK	Unecked by RATIONAL MAP Date



					e
INDEX MAP N.T.S.					Date
G01 BASIN DESIGNATION					Appr.
2.7 0.40 0.55 SUB-WATERSHED DESIGNATION MINOR/MAJOR STORM COEFFICIENT	$\vdash$				Init.
BASIN AREA IN ACRES					
DESIGN POINT DESIGNATION					Date
MAJOR BASIN BOUNDARY					
6130 PROPOSED COUNTOUR					
□					
SEPARATE PERVIOUS AREA (SPA)					su
RECEIVING PERVIOUS AREA (RPA)					Revisions
DIRECT CONNECTED IMPERVIOUS AREA (DCIA)	•	ı	I	ı	No.
UNCONNECTED IMPERVIOUS AREA (UIA)			130	2	ţ
dination meeting				MERIDIAN RANCH	
GRAPHIC SCALE		WATER OUALITY CAPTURE VOLUME	BASINS MAP	REX ROAD - PDR - FDR	
( IN FEET ) 1 INCH = 200 ft.	n by	TAK	ked by		<b>JUNE</b> 2023
PRELIMINARY STORAGE VOLUMES AND OUTFLOW QUANTITIES HAVE BEEN PROVIDED FOR EACH TURE DETENTION FACILITIES LOCATED WITHIN THE DEVELOPMENT. THE ACTUAL STORAGE	Drawn		Checked		-
AND DISCHARGE RATES WILL BE DETERMINED UPON A COMPLETE ANALYSIS FOR EACH N FACILITY PRIOR TO CONSTRUCTION. THE VALUES GIVEN FOR DISCHARGE AND VOLUME ARE S FOR PLANNING PURPOSES ONLY.		NO CHOMN			o) o
FIGURE 7	Scale			-	_