

PAVEMENT DESIGN REPORT VOLLMER ROAD NORTH EL PASO COUNTY, COLORADO

Prepared for:

Classic Communities 2138 Flying Horse Club North Colorado Springs, Colorado 80921

Attn: Austin Lenz

December 22, 2023 Revised – March 6, 2024

Respectfully Submitted,

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ENTECH ENGINEERING, INC.

Stuart Wood Geologist Reviewed by:

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Joseph C. Goode III, P.E. Sr. Engineer

SW:JCG/

Entech Job No. 231519



Table of Contents

1	Introduction	1										
2	Project and Site Description	1										
3	Subsurface Explorations and Laboratory Testing											
	3.1 Subsurface Exploration Program	1										
	3.2 Geotechnical Index and Engineering Property Testing	2										
4	Subgrade Conditions	2										
	4.1 Subsurface Conditions	3										
	4.2 Groundwater											
5	Pavement Design Recommendations	3										
	5.1 Subgrade Conditions	3										
	5.2 Swell Mitigation	4										
	5.3 Traffic Loading	4										
	5.4 Pavement Design	4										
6	Construction Recommendations	5										
	6.1 Earthwork Recommendations for Pavement Subgrade	5										
	6.1.1 Overexcavation											
	6.1.2 Subgrade Preparation – Aggregate Base Course Alternatives	6										
	6.1.3 Cement-treated Subgrade	6										
	6.1.4 Fill Placement and Compaction	7										
	6.2 Aggregate Base Course	7										
	6.3 Concrete Degradation Due to Sulfate Attack	7										
	6.4 Construction Observation	8										
7	Closure	8										

Figures

Figure 1: Vicinity Map
Figure 2: Site and Exploration Plan

List of Appendices

Appendix A: Test Boring Logs Appendix B: Laboratory Test Results Appendix C: Pavement Design Calculations



1 Introduction

Entech Engineering, Inc. (Entech) completed a subsurface exploration program, laboratory testing, and pavement design recommendations for a segment of Vollmer Road in northern El Paso County, Colorado. This report describes the subsurface exploration program conducted for the proposed roadway improvements and provides pavement section alternatives and construction recommendations. Entech participated in this project as a subconsultant to Classic Communities. The contents of this report, including the pavement design recommendations, are subject to the limitations and assumptions presented in Section 7.

This revised report supersedes previous versions of the report.

2 Project and Site Description

The proposed improvements to Vollmer Road consist of approximately 1 mile of roadway widening and improvements from approximately 500 feet northeast of Glider Loop to Poco Road (Figure 1). Improvements will include widening of the existing roadway and a new pavement section. The extent of the improvements will include a 2-inch mill and overlay to tie in with the existing roadway.

The existing topography along Vollmer Road includes vacant pasture land and land being developed for future residential lots. The roadway is currently paved with asphalt and is without curbs and gutters. We understand that the proposed roadway surface will remain asphalt. Based on the development plans the improvements include two travel lanes in each direction, a striped median, and curb and gutter installation. Vollmer Road will be designated as an urban minor arterial.

3 Subsurface Explorations and Laboratory Testing

3.1 Subsurface Exploration Program

Subsurface conditions at the project site were explored by 11 test borings, designated TB-1 through TB-11, drilled on November 1, 2023. The locations of the test borings are shown on the Site and Exploration Plan (Figure 2). The borings were drilled to depths of 5 to 10 feet below the existing ground surface (bgs). The drilling was performed using a truck-mounted, continuous flight auger drill rig supplied and operated by Entech. Descriptive boring logs providing the lithologies



of the subsurface conditions encountered during drilling are presented in Appendix A. Groundwater levels were measured in each open borehole at the conclusion of drilling.

Soil and bedrock samples were obtained from the borings utilizing the Standard Penetration Test (ASTM D1586) using a split-barrel California sampler. Results of the Standard Penetration Test (SPT) are included on the boring logs in terms of N-values expressed in blows per foot (bpf). Soil and bedrock samples recovered from the borings were visually classified and recorded on the boring logs. The soil classifications were later verified utilizing laboratory testing and grouped by soil type. The soil type numbers are included on the boring logs. It should be understood that the soil descriptions shown on the boring logs may vary between boring locations and sample depths. It should also be noted that the lines of stratigraphic separation shown on the boring logs represent approximate boundaries between soil types and the actual stratigraphic transitions may be more gradual or variable with location.

3.2 Geotechnical Index and Engineering Property Testing

Water content testing (ASTM D2216) was performed on the samples recovered from the borings, and the results are shown on the boring logs. Grain-Size Analysis (ASTM D422) and Atterberg Limits testing (ASTM D4318) were performed on selected samples to assist in classifying the materials encountered in the borings.

For pavement design, a modified proctor (ASTM D1557) and California Bearing Ratio (CBR) test (ASTM D1883) were completed. Soluble sulfate testing was performed on select soil samples to evaluate the potential for below-grade degradation of concrete due to sulfate attack. The laboratory testing results are presented in Appendix B and summarized in Table B-1.

Strength testing was performed on two sets of soil/cement composite samples. Testing was performed on soil samples prepared with 2% and 4% Portland Cement Type 1/2. A compression strength of 160 pounds per square inch (psi) is recommended for cement-stabilized subgrade. The 5-day average strength value of the 2% mix was 206 psi. The 5-day average strength value of the 4% mix was 233 psi. A 4% mix is recommended based on the laboratory test results. A summary of the testing results is attached in Appendix B, Table B-2.

4 Subgrade Conditions

Two primary soil types and one bedrock type were encountered in the test borings drilled for the subsurface investigation. Each soil type was classified in accordance with the Unified Soil



Classification System (USCS) and the American Association of State Highway and Transportation Officials (AASHTO) soil classification system using the laboratory testing results and the observations made during drilling.

4.1 Subsurface Conditions

Subsurface conditions along the proposed roadways consisted of loose to dense silty to clayey sand fill and sand with silt or clay fill (Soil Type 1), native medium dense to dense silty sand to sand with silt (Soil Type 2). Very weak to extremely weak, moderately to highly weathered sandstone was encountered at depths of 4 to 7 feet bgs in five of the test borings. When classified as a soil, the sandstone classified as very dense, silty sand to sand with silt (Soil Type 3). The test borings were drilled through 3 to 7 inches of existing hot mix asphalt (HMA) and 1 to 3 inches of aggregate base course (ABC). Soil types and corresponding AASHTO soil classifications are listed as follows:

- Soil Type 1: A-2-4, A-1-b, A-2-6, and A-6 (used for CBR testing and pavement design)
- Soil Type 2: A-2-4 and A-1-b
- Soil Type 3: A-1-b

Laboratory test results are presented in Appendix B and are summarized in Table B-1.

4.2 Groundwater

Groundwater was not encountered in the test borings. Groundwater fluctuations are possible and will depend on seasonal variations, local precipitation, runoff, and other factors. We do not anticipate groundwater to affect the proposed roadway construction.

5 Pavement Design Recommendations

Pavement design recommendations were made in accordance with the *El Paso County Engineering Criteria Manual*.

5.1 Subgrade Conditions

California Bearing Ratio (CBR) testing was performed on a representative sample of the subgrade clayey sand fill (Soil Type 1, A-2-4) from TB-7 to determine the support characteristic of the subgrade soils for the roadway section. The results of the CBR testing are presented in Appendix B and summarized in Exhibit 1.



Exhibit 1: Subsurface Laboratory Testing Summary

Design Parameter	Value
Soil Type	1 - Clayey Sand Fill
CBR at 95%	53.27
Design CBR	10
Liquid Limit	26
Plasticity Index	10
Percent Passing 200	27.5
AASHTO Classification	A-2-4
Unified Soils Classification	SC

5.2 Swell Mitigation

El Paso County recommendations require swell mitigation of expansive soils criteria for soils with swell testing results greater than 2% under a 150 pounds per square foot (psf) surcharge. Based on the granular nature of the site materials encountered, mitigation for expansive soils is not required. Localized areas of higher clay contents such as the A-6 material encountered in boring TB-11 may be encountered during subgrade preparation. Overexcavation of cohesive soils is recommended to provide proper subgrade support as discussed in Section 6.1.1.

5.3 Traffic Loading

Traffic data is not available for the Vollmer Road widening alignment; however, the roadway is classified as an urban minor arterial. *The El Paso County Engineering Criteria Manual, Table D-2, Minimum Pavement Sections*, provides default 18-kip equivalent single axle loading (ESAL) based street classifications. For design, a default ESAL value of 1,971,000 was used for the urban minor arterial designation.

5.4 Pavement Design

The pavement sections were determined utilizing the *El Paso County Engineering Criteria Manual*, *Appendix D, Pavement Design Criteria and Report*, the CBR testing, and default ESAL values. Design parameters used in the pavement analysis are presented in Exhibit 2.



Exhibit 2: Pavement Design Parameters

Design Parameter	Value
Reliability	85%
Standard Deviation	0.45
Serviceability Loss (∆ psi)	2.0
Design CBR	10.0
Resilient Modulus	15,000 psi
Structural Coefficients	
Hot Mix Asphalt	0.44
Cement Treated Subgrade	0.11

Pavement sections recommended for roads are summarized in Exhibit 3. The pavement design calculations are presented in Appendix C.

Exhibit 3: Recommended Pavement Sections

Pavement Area	Roadway Designation	Design ESAL	Alternative ¹
Vollmer Road	Urban Minor	1,971,000	1. 5.0 inches HMA over 8.0 inches ABC
(North)	Arterial	1,971,000	2. 5.0 inches HMA over 10.0 inches CTS

ABC = Aggregate Base Course; CTS = cement-treated subgrade; ESAL = equivalent single axle loads; HMA = Hot Mix Asphalt

Notes:

1. All pavement alternatives meet the minimum sections required per *El Paso County Pavement Design Criteria, Table D-2, Minimum Pavement Sections.*

6 Construction Recommendations

Pavement design recommendations provided herein are contingent on good construction practices, and poor construction techniques may result in poor performance. Our analyses assumed that this project will be constructed according to the *El Paso County Engineering Criteria Manual* and the *Pikes Peak Region Asphalt Paving Specifications*.

6.1 Earthwork Recommendations for Pavement Subgrade

Proper subgrade preparation is required for adequate pavement performance. Paving areas should be cleared of all deleterious materials including but not limited to existing pavements, utility poles, and fence poles. Surface vegetation, if any, should be removed by stripping, with the depth to be field determined.



6.1.1 Overexcavation

Where encountered, cohesive soils (AASHTO A-6, TB-11) should be removed to a depth 18 inches and replaced with granular fill (Section 6.1.4) to provide uniform subgrade support. The extent of any cohesive material overexcavation should be field determined.

6.1.2 Subgrade Preparation – Aggregate Base Course Alternatives

If pavement section alternatives are selected utilizing aggregate base course (ABC), the final subgrade surface should be scarified to a depth of 12 inches, moisture conditioned within +/-2% over the optimum water content, and recompacted to 95% of its maximum Modified Proctor dry density, ASTM D1557.

Any A-6 material identified during scarification should be removed to a depth of 18 inches and be replaced with granular fill as discussed in Section 6.1.1.

The compacted surface below pavements should be proof-rolled with a fully loaded, tandem-axle, 10-yard dump truck or equivalent. Any areas that are delineated to be soft, loose, or yielding during proof-rolling should be removed and reconditioned or replaced.

6.1.3 Cement-treated Subgrade

For pavement section alternatives utilizing cement-treated subgrade (CTS), the subgrade shall be stabilized prior to placement of the asphalt by the addition of cement to a depth of 10 inches. The amount of cement applied shall be a minimum of 4% (by weight) of the subgrade's maximum dry density as determined by the Modified Proctor Test (ASTM D1557) for granular soils or by the Standard Proctor Test (ASTM D698) for cohesive soils. The cement should be spread evenly on the subgrade surface and be thoroughly mixed into the subgrade over a 10-inch depth, as specified, such that a uniform blend of soil and cement is achieved. Prior to application or mixing of the cement, the upper 10 inches of subgrade should be thoroughly moisture conditioned to the soil's optimum water content or as much as 2% more than the optimum water content as necessary to provide a compactable soil condition. Densification of the cement-stabilized subgrade should be completed to obtain a compaction of at least 95% of the subgrade maximum dry density as determined by the Modified Proctor Test (ASTM D1557) or by the Standard Proctor Test (ASTM D698). Satisfactory compaction of the subgrade shall occur within 90 minutes from the time of mixing the cement into the subgrade.

The following conditions shall be observed as part of the subgrade stabilization:



- Type I/II or Type 1L cement as supplied; a local supplier shall be used. All cement used for stabilization should come from the same source. If cement sources are changed, a new laboratory mix design should be completed.
- Moisture conditioning of the subgrade and/or mixing of the cement into the subgrade shall not
 occur when soil temperatures are below 40 degrees F. Cement-treated subgrades should be
 maintained at a temperature of 40 degrees F or greater until the subgrade has been
 compacted as required.
- Cement placement, cement mixing, and compaction of the cement-treated subgrade should be observed by a qualified geotechnical engineer. The geotechnical engineer should complete in-situ compaction tests and construct representative compacted specimens of the treated subgrade material for subsequent laboratory quality assurance testing.

Pending the results of the field density testing, microfracturing of the stabilized subgrade may be required. Soil strengths in excess of 275 psi require microfracturing.

6.1.4 Fill Placement and Compaction

Granular fill placed as part of the pavement subgrade shall consist of non-expansive, granular soil, free of organic matter, unsuitable materials, debris, and cobbles greater than 3 inches in diameter. Additionally, any granular fill placed as part of the roadway subgrade should have a minimum CBR of 10. All granular fill placed within the pavement subgrade should be compacted to a minimum of 95% of its maximum Modified Proctor Dry Density (ASTM D1557) at +/-2% of optimum moisture content. Fill material should be placed in horizontal lifts such that each finished lift has a compacted thickness of 6 inches or less. Entech should approve any imported fill to be used within the pavement subgrade area prior to delivery to the site.

6.2 Aggregate Base Course

ABC materials shall conform to the *El Paso County Standard Specifications Manual, Table D-6, Aggregate Base Course Materials.* ABC materials should be compacted to a minimum of 95% of its maximum Modified Proctor Dry Density (ASTM D1557) at +/-2% of optimum moisture content

6.3 Concrete Degradation Due to Sulfate Attack

Sulfate solubility testing was conducted on several samples recovered from the test borings to evaluate the potential for sulfate attack on concrete. The test results indicated less than 0.01%



soluble sulfate (by weight). The test results indicate the sulfate component of the in-place soils presents a negligible exposure threat to concrete placed below the site grade.

Type II or Type 1L cement is recommended for concrete on the site. To further avoid concrete degradation during construction, it is recommended that concrete not be placed on frozen or wet ground. Care should be taken to prevent the accumulation or ponding of water in the foundation excavation prior to the placement of concrete. If standing water is present in the foundation excavation, it should be removed by ditching to sumps and pumping the water away from the foundation area prior to concrete placement. If concrete is placed during periods of cold temperatures, the concrete must be kept from freezing. This may require covering the concrete with insulated blankets and adding heat to prohibit freezing.

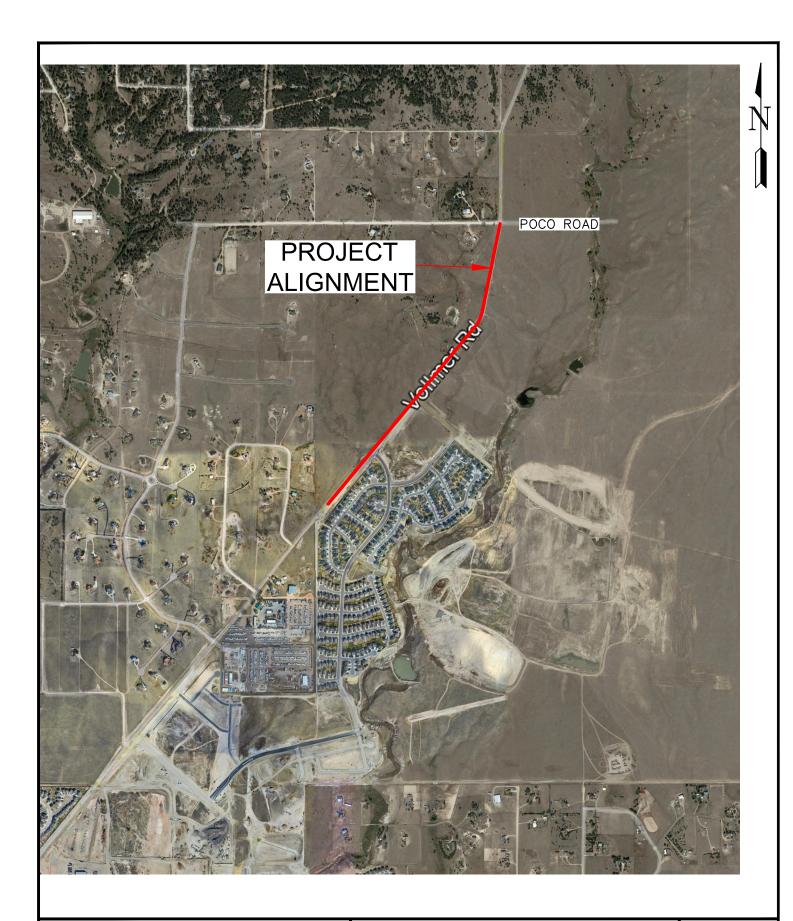
6.4 Construction Observation

Subgrade preparation for pavement structures should be observed by Entech in order to verify that (1) no anomalies are present, (2) materials similar to those described in this report have been encountered or placed, and (3) no soft spots, expansive or organic soil, or debris are present in the pavement subgrade prior to paving.

7 Closure

The subsurface investigation, geotechnical evaluation, and recommendations presented in this report are intended for use by Classic Communities with application to the Vollmer Road North paving project in El Paso County, Colorado. In conducting the subsurface exploration program, laboratory testing, engineering evaluation, and reporting, Entech Engineering, Inc. endeavored to work in accordance with generally accepted professional geotechnical and geologic practices and principles consistent with the level of care and skill ordinarily exercised by members of the geotechnical profession currently practicing in the same locality and under similar conditions. No other warranty, expressed or implied, is made. During final design and/or construction, if conditions are encountered that appear different from those described in this report, Entech Engineering, Inc. requests to be notified so that the evaluation and recommendations presented herein can be reviewed and modified as appropriate.

If there are any questions regarding the information provided herein, or if Entech Engineering, Inc. can be of further assistance, please do not hesitate to contact us.



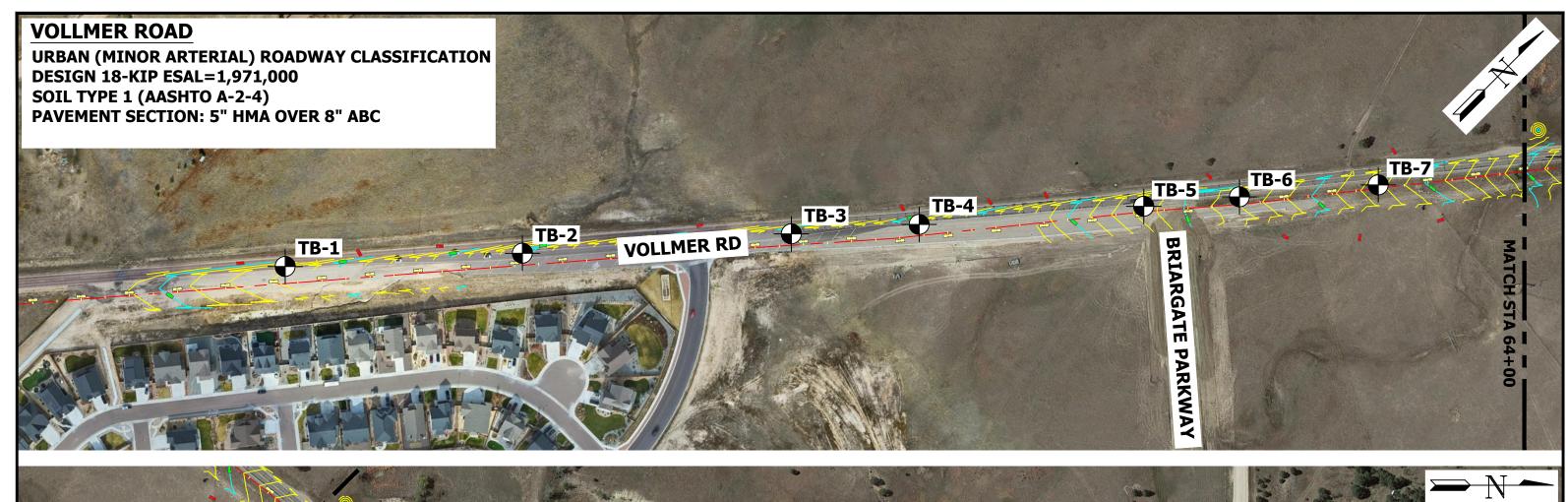


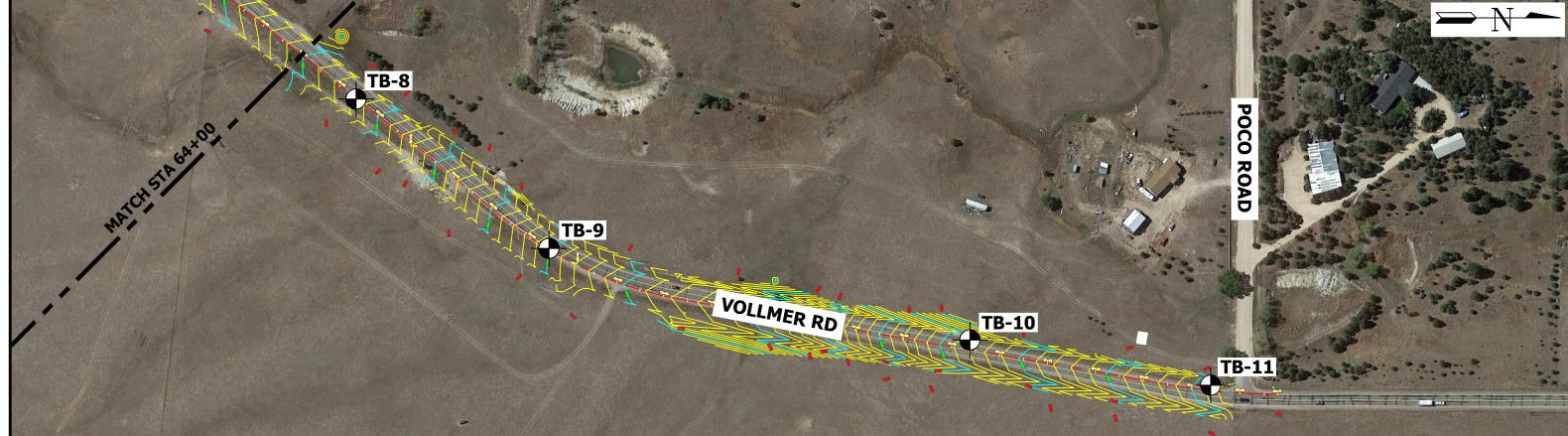
VICINITY MAP

VOLLMER ROAD NORTH CLASSIC COMMUNITIES

JOB NO. 231519

FIG. 1





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TB- APPROXIMATE TEST BORING LOCATION AND NUMBER



SITE AND EXPLORATION PLAN

VOLLMER ROAD NORTH CLASSIC COMMUNITIES

JOB NO. 231519

FIG. 2



APPENDIX A: Test Boring Logs

TEST BORING 1 DATE DRILLED 11/1/202	3						TEST BORING DATE DRILLED 11/1/202	2					
REMARKS	Ĭ						REMARKS	Ť					
DRY TO 10', 11/1/23	Depth (ft)	Symbol	Samples	Blows per foot	Watercontent %	Soil Type	DRY TO 5', 11/1/23	Depth (ft)	Symbol	Samples	Blows per foot	Watercontent %	Soil Type
3" ASPHALT, 2" BASE COURSE	_			21	4.3	1	3" ASPHALT, 2" BASE COURSE		11		15	6.0	1
FILL 0-6', SAND, WITH SILT, BROWN, MEDIUM DENSE, MOIST	-	 		21	4.3		FILL 0-5', SAND, WITH SILT TO SILTY, BROWN, MEDIUM DENSE		┪┋╢		15	0.0	'
BROWN, MEDIOW BENGE, MOIST	5_			11	5.9	1	to LOOSE, MOIST	5_			8	7.8	1
SANDSTONE, VERY WEAK, TAN, MODERATELY WEATHERED (SAND, WITH SILT, VERY DENSE, MOIST)	10			<u>50</u> 6"	6.8	3		10					



TEST BORING 3							TEST BORING 4					
DATE DRILLED 11/1/202 REMARKS	3 	Ī	Т				DATE DRILLED 11/1/202 REMARKS	3	1 1	I	1	_
DRY TO 5', 11/1/23	Depth (ft)	Symbol	Samples	Blows per foot	Watercontent %	Soil Type	DRY TO 10', 11/1/23	Depth (ft)	Symbol	Blows per foot	Watercontent %	Soil Type
5" ASPHALT, 1" BASE COURSE FILL 0-5', SAND, SILTY, BROWN, DENSE to LOOSE, MOIST	-[.			31	8.6	1	5" ASPHALT, 2" BASE COURSE FILL 0-4', SAND, SILTY, BROWN, MEDIUM DENSE, MOIST	- -		25	9.4	1
	5			7	8.0	1	SAND, SILTY, GRAY, MEDIUM DENSE, MOIST SANDSTONE, EXTREMELY WEAK, TAN, MODERATELY WEATHERED (SAND, WITH SILT, VERY DENSE,	5		10	10.8	2
	10 -						MOIST)	10		8"	11.7	3
	15							20_				



REMARKS (1) 10 10 10 10 10 10 10	TEST BORING DATE DRILLED 11/1/20	5 23				TEST BORING 6 DATE DRILLED 11/1/2023
15 <u>15 </u>	REMARKS DRY TO 5', 11/1/23 7" ASPHALT, 1" BASE COURSE FILL 0-5', SAND, SILTY TO CLAYEY, BROWN, DENSE to MEDIUM	15 To Depth (ft)	36	7.6	1	REMARKS (i) I to June and Line and Lin



TEST BORING 7							TEST BORING 8	.				
DATE DRILLED 11/1/2023	3						DATE DRILLED 11/1/202	3				
REMARKS					%		REMARKS				_0	
				oot	int %					too	Watercontent %	
	ft)		S	er f	onte	e Se		£)		Serf	onte	9e
	Depth (ft)	Symbol	Samples	Blows per foot	Watercontent	Soil Type		Depth (ft)	Symbol	Samples Blows per foot	terc	Soil Type
DRY TO 10', 11/1/23	Dep	Syr	Sar	Blo	Wa	Soil	DRY TO 5', 11/1/23	Dep	Syr	Sar Blo	Wa	Soil
6" ASPHALT, 3" BASE COURSE	_	11		19	6.0	1	6" ASPHALT, 3" BASE COURSE	_	11	23	3 5.2	1
FILL 0-6', SAND, WITH SILT TO CLAY, MEDIUM DENSE, MOIST	-	$ \cdot $		19	0.0	'	FILL 0-5', SAND, WITH SILT, BROWN, MEDIUM DENSE, MOIST	-	╽ ┞╢╏) 3.2	1
										╝		
	5_			15	11.5	1		5_	1 1	18	4.3	1
SANDSTONE, VERY WEAK, TAN,	-							-				
MODERATELY WEATHERED												
(SAND, WITH SILT, VERY DENSE,	10			<u>50</u>	13.1	3		10				
	_	: : :		<u>7"</u>	10.1	ľ		· · · -				
								-				
	_							-				
	15							15	1			
								_				
								-				
	-							-				
	20							20				



VOLLMER ROAD NORTH CLASSIC COMMUNITIES

JOB NO. 231519

FIG. A-4

TEST BORING 9 DATE DRILLED 11/1/202							TEST BORING 10 DATE DRILLED 11/1/202						
REMARKS DRY TO 5', 11/1/23	Depth (ft)	Symbol	Samples	Blows per foot	Watercontent %	Soil Type	REMARKS DRY TO 10', 11/1/23	Depth (ft)	Symbol	Samples	Blows per foot	Watercontent %	Soil Type
6" ASPHALT, 3" BASE COURSE FILL 0-4', SAND, SILTY, BROWN, MEDIUM DENSE, MOIST	-			11	12.8	1	6" ASPHALT, 3" BASE COURSE FILL 0-4', SAND, CLAYEY, BROWN, MEDIUM DENSE, MOIST	-	\.\.\		13	10.2	1
SAND, SILTY, TAN, MEDIUM DENSE, MOIST	5	<u> </u>		27	7.9	2	SAND, WITH SILT, TAN, DENSE, MOIST SANDSTONE, VERY WEAK, TAN, MODERATELY WEATHERED (SAND, WITH SILT, VERY DENSE,	5			44	6.4	2
	10	ı					(SAND, WITH SILI, VERT DENSE,	10			<u>50</u> 7"	9.8	3
	15	ı						15					
	20	ı						20					



VOLLMER ROAD NORTH CLASSIC COMMUNITIES

JOB NO. 231519

FIG. A-5

TEST BORING 11 11/1/2023 DATE DRILLED REMARKS Watercontent % Blows per foot Soil Type Symbol DRY TO 5', 11/1/23 6" ASPHALT, 3" BASE COURSE FILL 0-5', SAND, CLAYEY, BROWN, 7.3 1 11 MEDIUM, MOIST 5 20 6.3 1 10 15





APPENDIX B: Laboratory Test Results



TABLE B-1 SUMMARY OF LABORATORY TEST RESULTS

	1		1				1				
SOIL TYPE	TEST BORING NO.	DEPTH (FT)	PASSING NO. 200 SIEVE (%)	MOISTURE (%)	LIQUID LIMIT	PLASTIC LIMIT	PLASTIC INDEX	SULFATE (WT %)	AASHTO CLASS.	USCS	SOIL DESCRIPTION
1, CBR	7	0-3	27.5	8.7	26	16	10		A-2-4	SC	FILL, SAND, CLAYEY
1	1	1-2	10.7	4.4	NV	NP	NP		A-1-b	SM	FILL, SAND, WITH SILT
1	2	1-2	11.6	6.2	NV	NP	NP		A-1-b	SM	FILL, SAND, WITH SILT
1	3	1-2	29.3	9.7	NV	NP	NP	<0.01	A-2-4	SM	FILL, SAND, SILTY
1	4	1-2	30.4	11.3	NV	NP	NP		A-2-4	SM	FILL, SAND, SILTY
1	5	1-2	14.0	7.7	NV	NP	NP		A-1-b	SM	FILL, SAND, SILTY
1	6	1-2	30.2	15.2	NV	NP	NP	<0.01	A-2-4	SM	FILL, SAND, SILTY
1	7	1-2	9.3	6.8					A-2-6	SC	FILL, SAND, WITH CLAY
1	8	1-2	11.7	5.1	NV	NP	NP		A-1-b	SW-SM	FILL, SAND, WITH SILT
1	9	1-2	29.9	13.0	NV	NP	NP		A-2-4	SM	FILL, SAND, SILTY
1	10	1-2	31.9	11.6	29	21	8	<0.01	A-2-4	SC	FILL, SAND, CLAYEY
1	11	1-2	36.7	15.5	35	21	14		A-6	SC	FILL, SAND, CLAYEY
1	1	0-3	24.5	6.8					A-2-4	SM	FILL, SAND, SILTY
2	9	5	29.2	10.0	NV	NP	NP		A-2-4	SM	SAND, SILTY
2	10	5	9.3	6.8	NV	NP	NP		A-1-b	SW-SM	SAND, WITH SILT
3	1	10	10.3	8.1	NV	NP	NP	<0.01	A-1-b	SW-SM	SANDSTONE (SAND, WITH SILT)
3	4	10	10.0	14.3	NV	NP	NP		A-1-b	SW-SM	SANDSTONE (SAND, WITH SILT)
3	6	5	12.3	12.8	NV	NP	NP	<0.01	A-1-b	SM	SANDSTONE (SAND, SILTY)
3	7	10	9.5	12.6	NV	NP	NP	<0.01	A-1-b	SW-SM	SANDSTONE (SAND, WITH SILT)
3	10	10	9.7	10.2	NV	NP	NP	<0.01	A-1-b	SW-SM	SANDSTONE (SAND, WITH SILT)

Project: Vollmer Road North Client: Classic Communities Job No: 231519



TABLE B-2 SUMMARY OF CTS TEST RESULTS

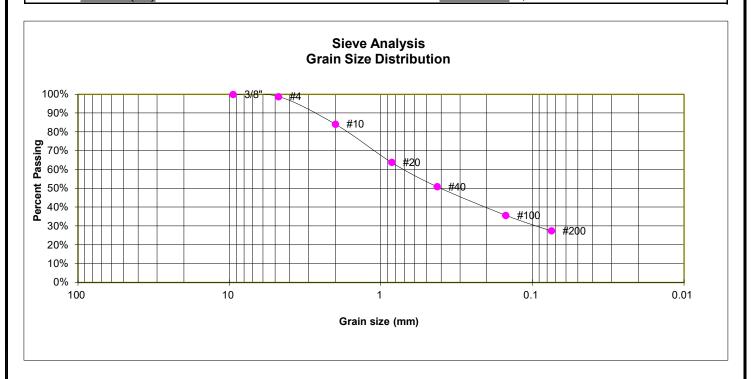
FIELD SAMPLE ID SOIL ADDITIVE CURING METHOD

SAND, SILTY
TYPE I/II CEMENT
100° HUMIDIFIED OVEN

ADDITIVE %	WATER %	DENSITY (dry)	AGE (days)	STRENGTH (psi)
2	7.0	122.9	5	197
2	7.0	122.7	5	207
2	7.0	122.6	5	214
			AVERAGE:	206
4	7.0	122.8	5	231
4	7.0	122.5	5	226
4	7.0	122.6	5	242
			AVERAGE:	233

Project: Vollmer Road North Client:: Classic Communities Job No: 231519 TEST BORING 7
DEPTH (FT) 0-3

SOIL DESCRIPTION FILL, SAND, CLAYEY SOIL TYPE 1, CBR



GRAIN SIZE ANALYSIS

U.S.	Percent
Sieve #	<u>Finer</u>
3"	
1 1/2"	
3/4"	
1/2"	
3/8"	100.0%
4	98.8%
10	84.2%
20	63.8%
40	50.9%
100	35.7%
200	27.5%

SOIL CLASSIFICATION

USCS CLASSIFICATION: SC
AASHTO CLASSIFICATION: A-2-4
AASHTO GROUP INDEX: 0

ATTERBERG LIMITS

Plastic Limit	16
Liquid Limit	26
Plastic Index	10

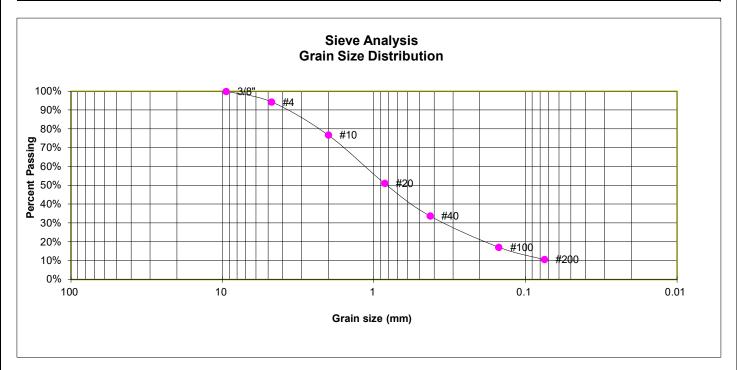


LABORATORY TEST RESULTS

VOLLMER ROAD NORTH CLASSIC COMMUNITIES

JOB NO. 231519

TEST BORING1SOIL DESCRIPTION FILL, SAND, WITH SILTDEPTH (FT)1-2SOIL TYPE 1



GRAIN SIZE ANALYSIS

U.S.	Percent
Sieve #	<u>Finer</u>
3"	
1 1/2"	
3/4"	
1/2"	
3/8"	100.0%
4	94.4%
10	76.7%
20	51.1%
40	33.7%
100	17.2%
200	10.7%

SOIL CLASSIFICATION

USCS CLASSIFICATION: SM
AASHTO CLASSIFICATION: A-1-b
AASHTO GROUP INDEX: 0

ATTERBERG LIMITS

Plastic Limit	NP
Liquid Limit	NV
Plastic Index	NP

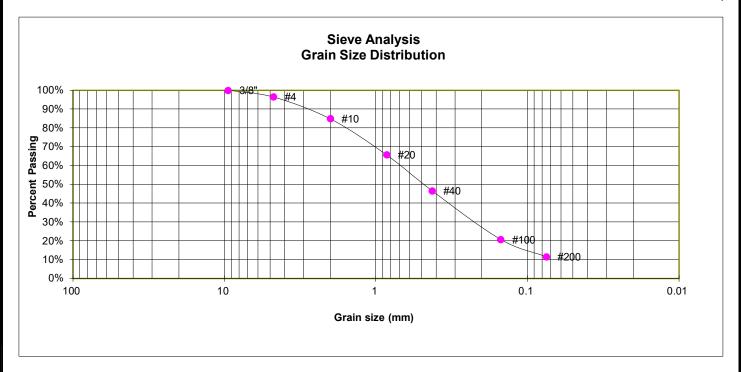


LABORATORY TEST RESULTS

VOLLMER ROAD NORTH CLASSIC COMMUNITIES

JOB NO. 231519

TEST BORING2SOIL DESCRIPTION FILL, SAND, WITH SILTDEPTH (FT)1-2SOIL TYPE 1



GRAIN SIZE ANALYSIS

U.S.	Percent
Sieve #	<u>Finer</u>
3"	
1 1/2"	
3/4"	
1/2"	
3/8"	100.0%
4	96.5%
10	84.9%
20	65.7%
40	46.5%
100	20.7%
200	11.6%

SOIL CLASSIFICATION

USCS CLASSIFICATION: SM
AASHTO CLASSIFICATION: A-1-b
AASHTO GROUP INDEX: 0

ATTERBERG LIMITS

Plastic Limit	NP
Liquid Limit	NV
Plastic Index	NP

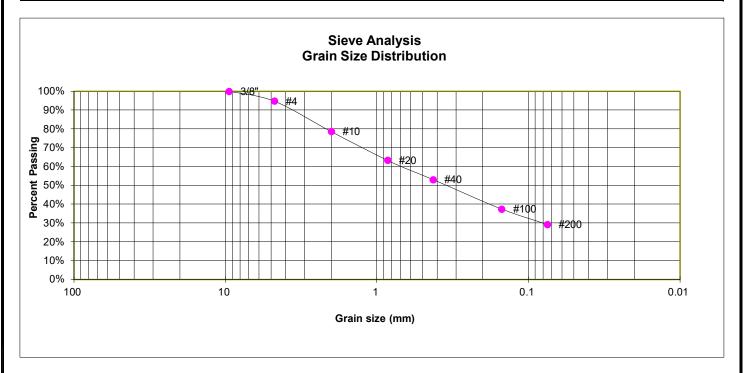


LABORATORY TEST RESULTS

VOLLMER ROAD NORTH CLASSIC COMMUNITIES

JOB NO. 231519

TEST BORING3SOIL DESCRIPTION FILL, SAND, SILTYDEPTH (FT)1-2SOIL TYPE 1



GRAIN SIZE ANALYSIS

U.S.	Percent
Sieve #	<u>Finer</u>
3"	
1 1/2"	
3/4"	
1/2"	
3/8"	100.0%
4	94.8%
10	78.6%
20	63.4%
40	53.1%
100	37.4%
200	29.3%

SOIL CLASSIFICATION

USCS CLASSIFICATION: SM
AASHTO CLASSIFICATION: A-2-4
AASHTO GROUP INDEX: 0

ATTERBERG LIMITS

Plastic Limit	NP
Liquid Limit	NV
Plastic Index	NP

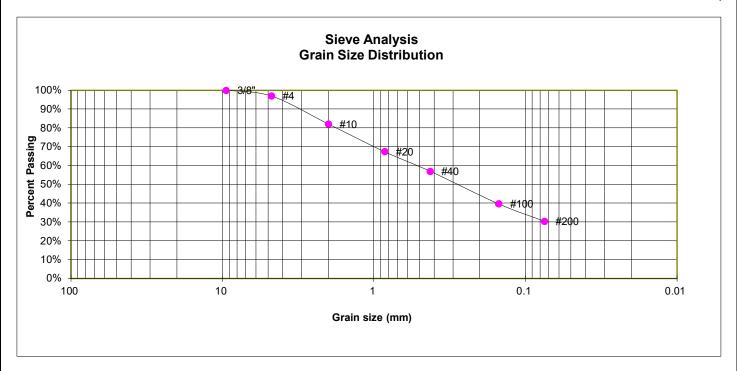


LABORATORY TEST RESULTS

VOLLMER ROAD NORTH CLASSIC COMMUNITIES

JOB NO. 231519

TEST BORING4SOIL DESCRIPTION
SOIL TYPEFILL, SAND, SILTYDEPTH (FT)1-2SOIL TYPE1



GRAIN SIZE ANALYSIS

U.S.	Percent
Sieve #	<u>Finer</u>
3"	
1 1/2"	
3/4"	
1/2"	
3/8"	100.0%
4	97.0%
10	82.1%
20	67.4%
40	57.0%
100	39.7%
200	30.4%

SOIL CLASSIFICATION

USCS CLASSIFICATION: SM
AASHTO CLASSIFICATION: A-2-4
AASHTO GROUP INDEX: 0

ATTERBERG LIMITS

Plastic Limit	NP
Liquid Limit	NV
Plastic Index	NP

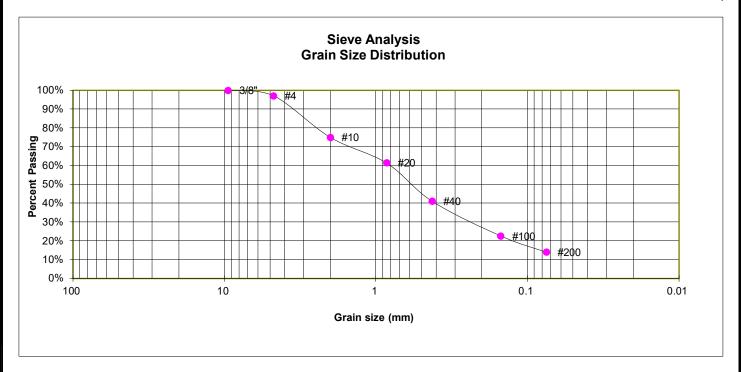


LABORATORY TEST RESULTS

VOLLMER ROAD NORTH CLASSIC COMMUNITIES

JOB NO. 231519

TEST BORING5SOIL DESCRIPTION
SOIL TYPEFILL, SAND, SILTYDEPTH (FT)1-2SOIL TYPE1



GRAIN SIZE ANALYSIS

U.S.	Percent
Sieve #	<u>Finer</u>
3"	
1 1/2"	
3/4"	
1/2"	
3/8"	100.0%
4	97.1%
10	75.0%
20	61.4%
40	41.0%
100	22.6%
200	14.0%

SOIL CLASSIFICATION

USCS CLASSIFICATION: SM
AASHTO CLASSIFICATION: A-1-b
AASHTO GROUP INDEX: 0

ATTERBERG LIMITS

Plastic Limit	NP
Liquid Limit	NV
Plastic Index	NP

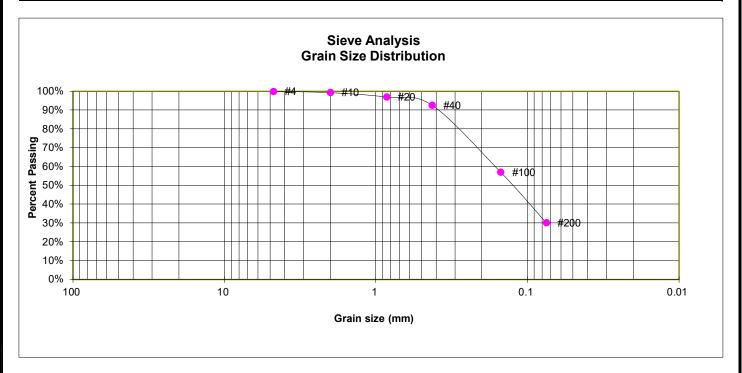


LABORATORY TEST RESULTS

VOLLMER ROAD NORTH CLASSIC COMMUNITIES

JOB NO. 231519

TEST BORING6SOIL DESCRIPTION
SOIL TYPEFILL, SAND, SILTYDEPTH (FT)1-2SOIL TYPE1



GRAIN SIZE ANALYSIS

U.S.	Percent
Sieve #	<u>Finer</u>
3"	
1 1/2"	
3/4"	
1/2"	
3/8"	
4	100.0%
10	99.3%
20	97.0%
40	92.6%
100	57.0%
200	30.2%

SOIL CLASSIFICATION

USCS CLASSIFICATION: SM
AASHTO CLASSIFICATION: A-2-4
AASHTO GROUP INDEX: 0

ATTERBERG LIMITS

Plastic Limit	NP
Liquid Limit	NV
Plastic Index	NP

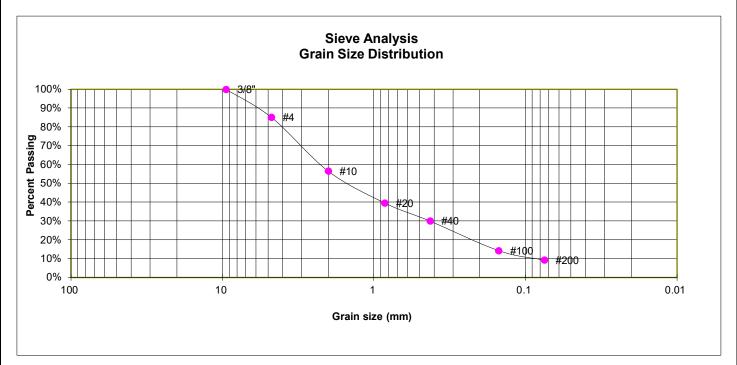


LABORATORY TEST RESULTS

VOLLMER ROAD NORTH CLASSIC COMMUNITIES

JOB NO. 231519





GRAIN SIZE ANALYSIS

U.S.	Percent
Sieve #	<u>Finer</u>
3"	
1 1/2"	
3/4"	
1/2"	
3/8"	100.0%
4	85.1%
10	56.5%
20	39.6%
40	30.0%
100	14.2%
200	9.3%

SOIL CLASSIFICATION

USCS CLASSIFICATION: SC AASHTO CLASSIFICATION: A-2-6 AASHTO GROUP INDEX: 0

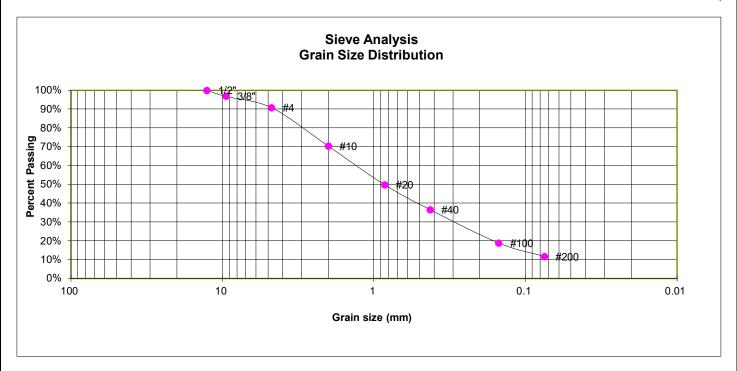


LABORATORY TEST RESULTS

VOLLMER ROAD NORTH CLASSIC COMMUNITIES

JOB NO. 231519

TEST BORING8SOIL DESCRIPTION
SOIL TYPEFILL, SAND, WITH SILTDEPTH (FT)1-2SOIL TYPE1



GRAIN SIZE ANALYSIS

U.S.	Percent
Sieve #	<u>Finer</u>
3"	
1 1/2"	
3/4"	
1/2"	100.0%
3/8"	96.8%
4	90.7%
10	70.4%
20	49.8%
40	36.6%
100	18.9%
200	11.7%

SOIL CLASSIFICATION

USCS CLASSIFICATION: SW-SM
AASHTO CLASSIFICATION: A-1-b
AASHTO GROUP INDEX: 0

ATTERBERG LIMITS

Plastic Limit	NP
Liquid Limit	NV
Plastic Index	NP

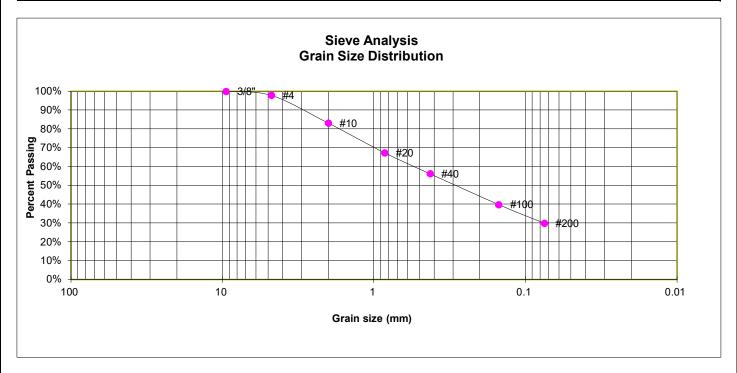


LABORATORY TEST RESULTS

VOLLMER ROAD NORTH CLASSIC COMMUNITIES

JOB NO. 231519

TEST BORING9SOIL DESCRIPTIONFILL, SAND, SILTYDEPTH (FT)1-2SOIL TYPE1



GRAIN SIZE ANALYSIS

U.S.	Percent
Sieve #	<u>Finer</u>
3"	
1 1/2"	
3/4"	
1/2"	
3/8"	100.0%
4	97.9%
10	83.1%
20	67.4%
40	56.2%
100	39.8%
200	29.9%

SOIL CLASSIFICATION

USCS CLASSIFICATION: SM
AASHTO CLASSIFICATION: A-2-4
AASHTO GROUP INDEX: 0

ATTERBERG LIMITS

Plastic Limit	NP
Liquid Limit	NV
Plastic Index	NP



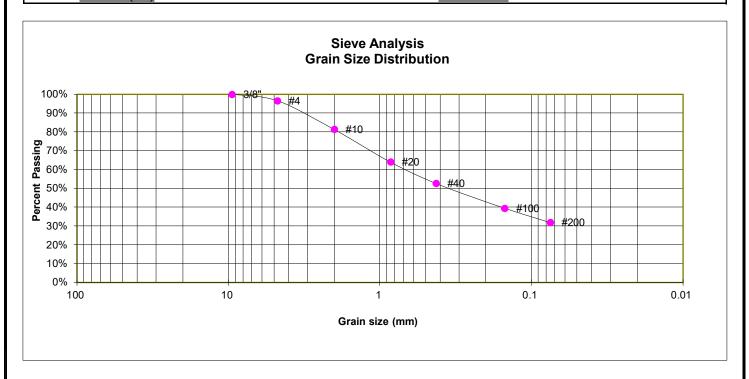
LABORATORY TEST RESULTS

VOLLMER ROAD NORTH CLASSIC COMMUNITIES

JOB NO. 231519

TEST BORING 10 DEPTH (FT) 1-2

SOIL DESCRIPTION FILL, SAND, CLAYEY SOIL TYPE 1



GRAIN SIZE ANALYSIS

U.S.	Percent
Sieve #	<u>Finer</u>
3"	
1 1/2"	
3/4"	
1/2"	
3/8"	100.0%
4	96.5%
10	81.4%
20	64.0%
40	52.7%
100	39.5%
200	31.9%

SOIL CLASSIFICATION

USCS CLASSIFICATION: SC AASHTO CLASSIFICATION: A-2-4 AASHTO GROUP INDEX: 0

ATTERBERG LIMITS

Plastic Limit	21
Liquid Limit	29
Plastic Index	8



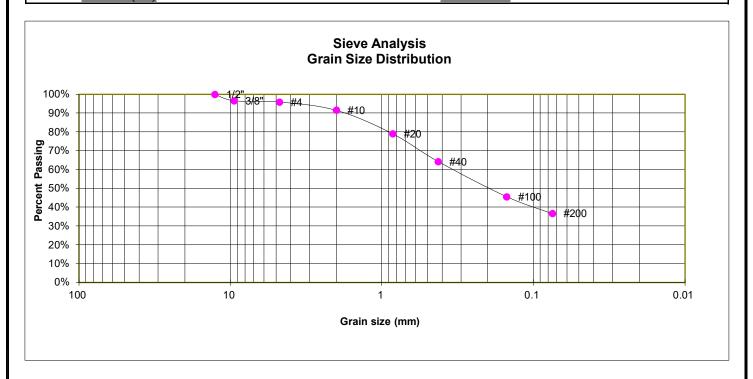
LABORATORY TEST RESULTS

VOLLMER ROAD NORTH CLASSIC COMMUNITIES

JOB NO. 231519

TEST BORING 11 DEPTH (FT) 1-2

SOIL DESCRIPTION FILL, SAND, CLAYEY SOIL TYPE 1



GRAIN SIZE ANALYSIS

U.S.	Percent
Sieve #	<u>Finer</u>
3"	
1 1/2"	
3/4"	
1/2"	100.0%
3/8"	96.6%
4	95.9%
10	91.6%
20	79.1%
40	64.3%
100	45.6%
200	36.7%

SOIL CLASSIFICATION

USCS CLASSIFICATION: SC AASHTO CLASSIFICATION: A-6 AASHTO GROUP INDEX: 1

ATTERBERG LIMITS

Plastic Limit 21 Liquid Limit 35 Plastic Index 14

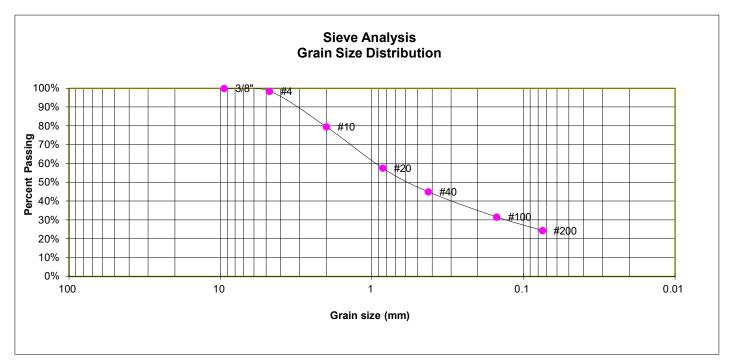


LABORATORY TEST RESULTS

VOLLMER ROAD NORTH CLASSIC COMMUNITIES

JOB NO. 231519





GRAIN SIZE ANALYSIS

U.S.	Percent
Sieve #	<u>Finer</u>
3"	
1 1/2"	
3/4"	
1/2"	
3/8"	100.0%
4	98.4%
10	79.6%
20	57.7%
40	45.0%
100	31.7%
200	24.5%

SOIL CLASSIFICATION

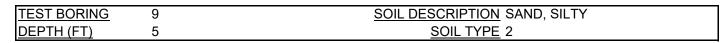
USCS CLASSIFICATION: SM AASHTO CLASSIFICATION: A-2-4

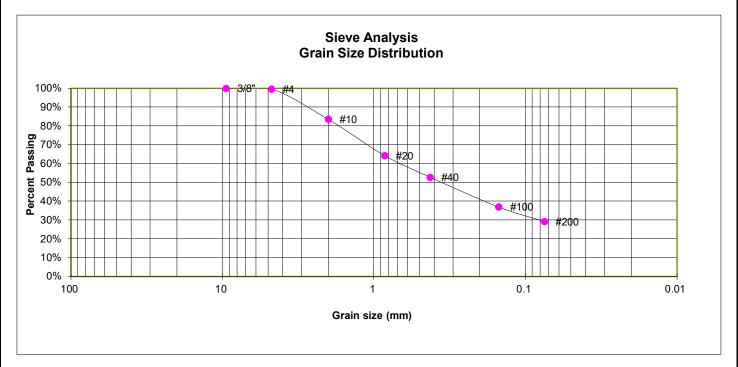


LABORATORY TEST RESULTS

VOLLMER ROAD NORTH CLASSIC COMMUNITIES

JOB NO. 231519





GRAIN SIZE ANALYSIS

U.S.	Percent
Sieve #	<u>Finer</u>
3"	
1 1/2"	
3/4"	
1/2"	
3/8"	100.0%
4	99.6%
10	83.6%
20	64.3%
40	52.7%
100	37.0%
200	29.2%

SOIL CLASSIFICATION

USCS CLASSIFICATION: SM
AASHTO CLASSIFICATION: A-2-4
AASHTO GROUP INDEX: 0

ATTERBERG LIMITS

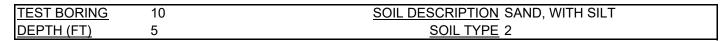
Plastic Limit	NP
Liquid Limit	NV
Plastic Index	NP

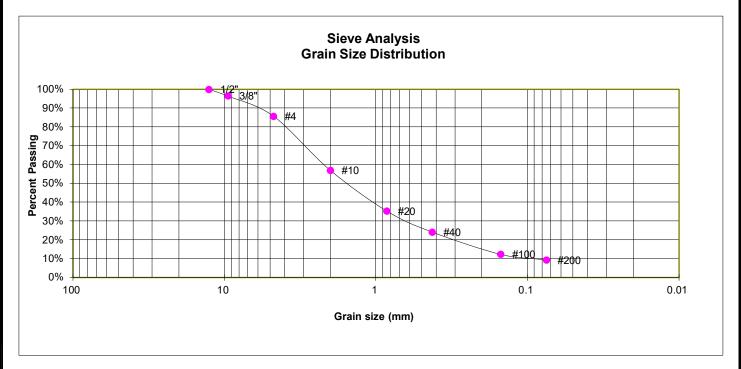


LABORATORY TEST RESULTS

VOLLMER ROAD NORTH CLASSIC COMMUNITIES

JOB NO. 231519





GRAIN SIZE ANALYSIS

U.S.	Percent
Sieve #	<u>Finer</u>
3"	
1 1/2"	
3/4"	
1/2"	100.0%
3/8"	96.5%
4	85.7%
10	57.0%
20	35.4%
40	24.1%
100	12.4%
200	9.3%

SOIL CLASSIFICATION

USCS CLASSIFICATION: SW-SM
AASHTO CLASSIFICATION: A-1-b
AASHTO GROUP INDEX: 0

ATTERBERG LIMITS

Plastic Limit	NP
Liquid Limit	NV
Plastic Index	NP

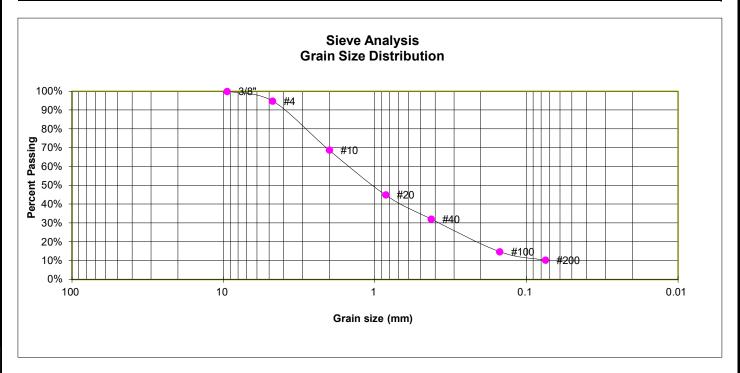


LABORATORY TEST RESULTS

VOLLMER ROAD NORTH CLASSIC COMMUNITIES

JOB NO. 231519

TEST BORING1SOIL DESCRIPTION SANDSTONE (SAND, WITH SILT)DEPTH (FT)10SOIL TYPE 3



GRAIN SIZE ANALYSIS

U.S.	Percent
Sieve #	<u>Finer</u>
3"	
1 1/2"	
3/4"	
1/2"	
3/8"	100.0%
4	94.8%
10	68.8%
20	44.9%
40	32.1%
100	14.8%
200	10.3%

SOIL CLASSIFICATION

USCS CLASSIFICATION: SW-SM
AASHTO CLASSIFICATION: A-1-b
AASHTO GROUP INDEX: 0

ATTERBERG LIMITS

Plastic Limit	NP
Liquid Limit	NV
Plastic Index	NP

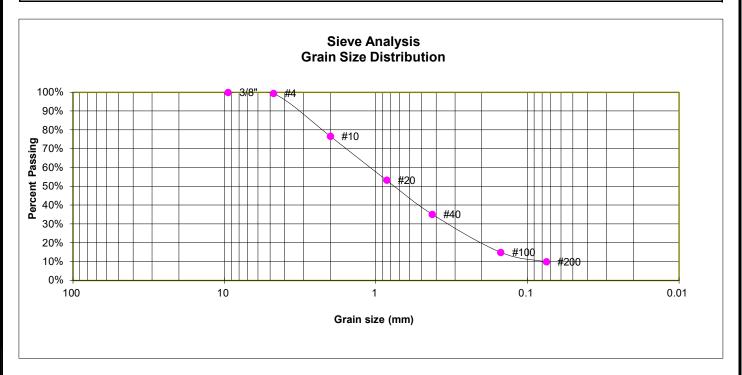


LABORATORY TEST RESULTS

VOLLMER ROAD NORTH CLASSIC COMMUNITIES

JOB NO. 231519

TEST BORING4SOIL DESCRIPTION SANDSTONE (SAND, WITH SILT)DEPTH (FT)10SOIL TYPE 3



GRAIN SIZE ANALYSIS

U.S.	Percent
Sieve #	<u>Finer</u>
3"	
1 1/2"	
3/4"	
1/2"	
3/8"	100.0%
4	99.4%
10	76.6%
20	53.3%
40	35.2%
100	14.9%
200	10.0%

SOIL CLASSIFICATION

USCS CLASSIFICATION: SW-SM
AASHTO CLASSIFICATION: A-1-b
AASHTO GROUP INDEX: 0

ATTERBERG LIMITS

Plastic Limit	NP
Liquid Limit	NV
Plastic Index	NP

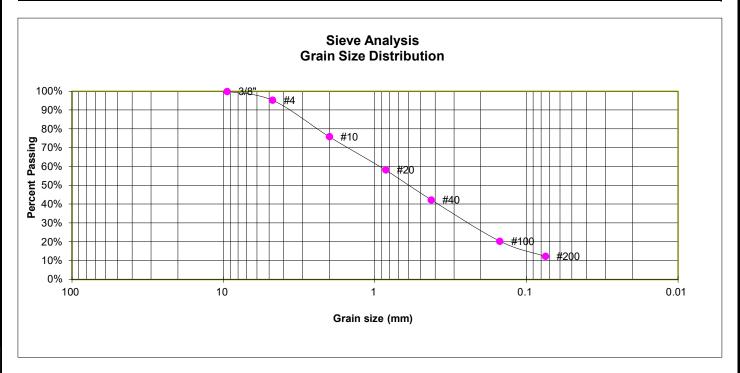


LABORATORY TEST RESULTS

VOLLMER ROAD NORTH CLASSIC COMMUNITIES

JOB NO. 231519

TEST BORING
DEPTH (FT)6SOIL DESCRIPTION
SOIL TYPE
3SANDSTONE (SAND, SILTY)



GRAIN SIZE ANALYSIS

U.S.	Percent
Sieve #	<u>Finer</u>
3"	
1 1/2"	
3/4"	
1/2"	
3/8"	100.0%
4	95.3%
10	75.9%
20	58.3%
40	42.4%
100	20.4%
200	12.3%

SOIL CLASSIFICATION

USCS CLASSIFICATION: SM
AASHTO CLASSIFICATION: A-1-b
AASHTO GROUP INDEX: 0

ATTERBERG LIMITS

Plastic Limit	NP
Liquid Limit	NV
Plastic Index	NP

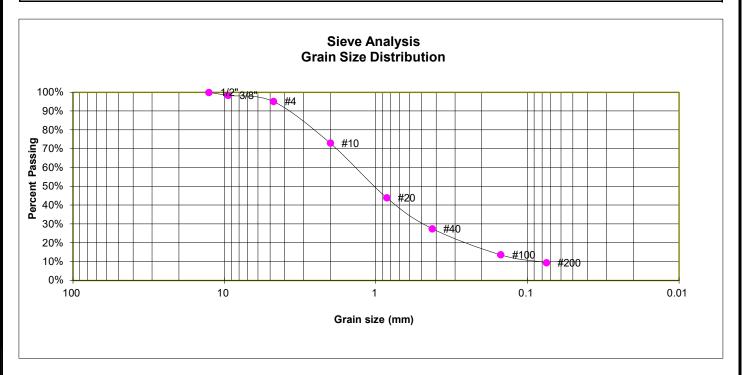


LABORATORY TEST RESULTS

VOLLMER ROAD NORTH CLASSIC COMMUNITIES

JOB NO. 231519

TEST BORING7SOIL DESCRIPTION SANDSTONE (SAND, WITH SILT)DEPTH (FT)10SOIL TYPE 3



GRAIN SIZE ANALYSIS

U.S.	Percent
Sieve #	<u>Finer</u>
3"	
1 1/2"	
3/4"	
1/2"	100.0%
3/8"	98.4%
4	95.1%
10	73.0%
20	44.0%
40	27.5%
100	13.7%
200	9.5%

SOIL CLASSIFICATION

USCS CLASSIFICATION: SW-SM
AASHTO CLASSIFICATION: A-1-b
AASHTO GROUP INDEX: 0

ATTERBERG LIMITS

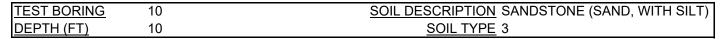
Plastic Limit	NP
Liquid Limit	NV
Plastic Index	NP



LABORATORY TEST RESULTS

VOLLMER ROAD NORTH CLASSIC COMMUNITIES

JOB NO. 231519





GRAIN SIZE ANALYSIS

U.S.	Percent
Sieve #	<u>Finer</u>
3"	
1 1/2"	
3/4"	
1/2"	
3/8"	100.0%
4	91.5%
10	62.2%
20	36.2%
40	24.6%
100	13.2%
200	9.7%

SOIL CLASSIFICATION

USCS CLASSIFICATION: SW-SM
AASHTO CLASSIFICATION: A-1-b
AASHTO GROUP INDEX: 0

ATTERBERG LIMITS

Plastic Limit	NP
Liquid Limit	NV
Plastic Index	NP



LABORATORY TEST RESULTS

VOLLMER ROAD NORTH CLASSIC COMMUNITIES

JOB NO. 231519

SAMPLE LOCATION TB-7 @ 0-3'

SOIL DESCRIPTION FILL, SAND, CLAYEY, BROWN SOIL TYPE 1

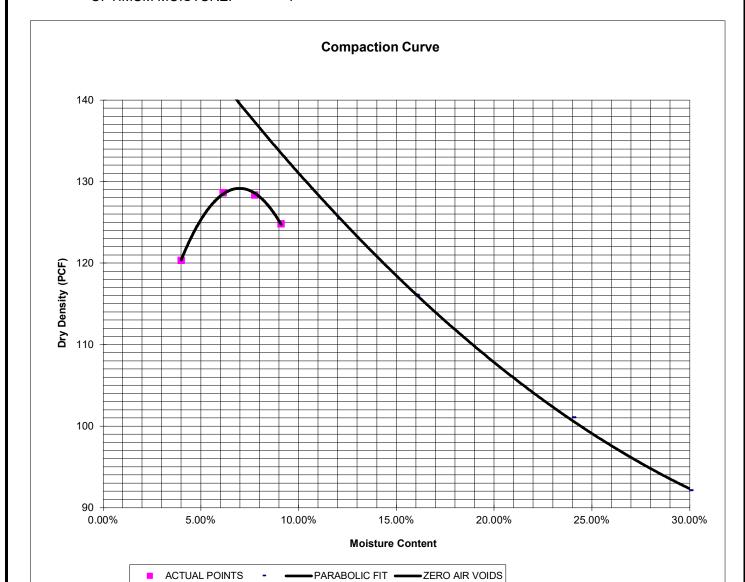
PROCTOR DATA

IDENTIFICATION: SC PROCTOR TEST #: 1

TEST BY: DK

TEST DESIGNATION: ASTM-1557-A MAXIMUM DRY DENSITY (PCF): 129.1

OPTIMUM MOISTURE: 7





LABORATORY TEST RESULTS

VOLLMER ROAD NORTH CLASSIC COMMUNITIES

JOB NO. 231519

SOIL DESCRIPTION FILL, SAND, CLAYEY, BROWN SOIL TYPE 1

CBR TEST LOAD DATA

Piston Diameter (cm): 4.958 Piston Area (in²): 2.993

	10 BLOWS		25 BLOWS		56 BLOWS	
Penetration	Mold # 1		Mold # 2		Mold # 3	
Depth	Load	Stress	Load	Stress	Load	Stress
(inches)	(lbs)	(psi)	(lbs)	(psi)	(lbs)	(psi)
0.000	0	0.00	0	0.00	0	0.00
0.025	151	50.46	208	69.51	306	102.26
0.050	309	103.26	450	150.38	796	266.00
0.075	490	163.74	723	241.60	1389	464.16
0.100	681	227.57	1051	351.21	2133	712.78
0.125	851	284.38	1329	444.11	2682	896.24
0.150	1006	336.17	1578	527.32	3310	1106.10
0.175	1137	379.95	1811	605.18	3620	1209.69
0.200	1251	418.04	2048	684.38	4190	1400.16
0.300	1703	569.09	2998	1001.83	5230	1747.70
0.400	1881	628.57	3506	1171.59	6000	2005.01
0.500	2053	686.05	3989	1333.00		

MOISTURE AND DENSITY DATA

	Mold # 1	Mold # 2	Mold # 3
Can #	341	117	352
Wt. Can	7.39	9.52	6.98
Wt. Can+Wet	176.67	231.7	235.23
Wt. Can+Dry	158.2	210.95	216.49
Wt. H20	18.47	20.75	18.74
Wt. Dry Soil	150.81	201.43	209.51
Moisture Content	12.25%	10.30%	8.94%
Wet Density (PCF)	123.7	127.8	134.6
Dry Density (PCF)	115.6	119.5	125.8
% Compaction	90%	93%	97%
CBR	22.76	35.12	71.28

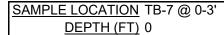
PROCTOR DATA

Maximum Dry Density (pcf) 129.1
Optimum Moisture 7
90% of Max. Dry Density (pcf) 116.2
95% of Max. Dry Density (pcf) 122.6

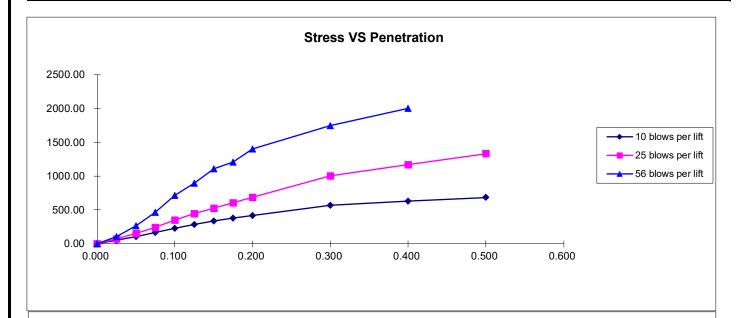
CBR at 90% of Max. Density = 24.56	~ R VALUE 71
CBR at 95% of Max. Density = 53.27	~ R VALUE 76

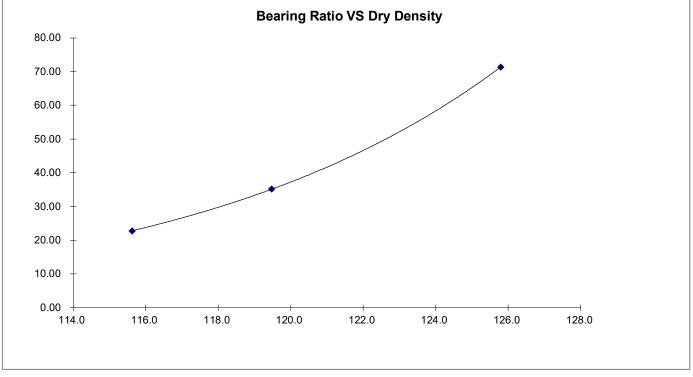


LABORATORY TEST RESULTS



SOIL DESCRIPTION FILL, SAND, CLAYEY, BROWN SOIL TYPE 1







LABORATORY TEST RESULTS

VOLLMER ROAD NORTH CLASSIC COMMUNITIES

JOB NO. 231519



APPENDIX C: Pavement Design Calculations



FLEXIBLE PAVEMENT DESIGN

PROJECT DATA

Project Location Vollmer Road North

Job Number: 231519

Note: Analysis follows design procedures from 1993 AASHTO Guide for Design of Pavement

Structures and Appendix D of the El Paso County Pavement Design Criteria and Report

DESIGN DATA

 $ESAL(W_{18}) =$ Equivalent (18-kip) Single Axle Load Applications (ESAL): 1,971,000 CBR =10 Design CBR Standard Deviation $S_0 =$ 0.45 Loss in Serviceability $\Delta psi =$ 2.0 Reliability = 85 Reliability Reliability (z-statistic) $Z_R =$ -1.04 Soil Resilient Modulus 15,000 psi

Required Structural Number (SN):

SN = 2.80

DESIGN EQUATIONS

Resilient Modulus

If using CBR: If using R-Value:

 $M_R = (CBR) \times 1,500$ $M_R = 10^{[(S_1 + 18.72)/6.24]} \text{ where } S_1 = [(R\text{-value - 5})/11.29] + 3$

Required Structural Number Solves nomograph shown in Figure D-1

$$\log_{10}W_{18} = Z_{R}^{*} S_{O} + 9.36^{*}\log_{10}(SN+1) - 0.20 + \frac{\log_{10}\left[\frac{\Delta PSI}{4.2 - 1.5}\right]}{0.40 + \frac{1094}{(SN+1)^{5.19}}} + 2.32^{*}\log_{10}M_{R}^{-} 8.07$$

Pavement Section Thickness

 $SN^* = C_1D_1 + C_2D_2$ where: $C_1 = Strength Coefficient - HMA$

 C_2 = Strength Coefficient - ABC

 D_1 = Depth of HMA (inches)

 D_2 = Depth of ABC (inches)

RECOMMENED THICKNESSES

Layer	Material	Coefficient	Thickness (D* _i)		SN* _i	SN
1	HMA	$C_1 = 0.44$	5.0	inches	2.200	
2	ABC	$C_2 = 0.11$	8.0	inches	0.880	ı
				SN* =	3.080	2.80

Pavement SN > Required SN, Design is Acceptable



FLEXIBLE PAVEMENT DESIGN

PROJECT DATA

Project Location Vollmer Road North

Job Number: 231519

Note: Analysis follows design procedures from 1993 AASHTO Guide for Design of Pavement

Structures and Appendix D of the El Paso County Pavement Design Criteria and Report

DESIGN DATA

 $ESAL(W_{18}) =$ Equivalent (18-kip) Single Axle Load Applications (ESAL): 1,971,000 CBR =10 Design CBR Standard Deviation $S_0 =$ 0.45 Loss in Serviceability $\Delta psi =$ 2.0 Reliability = 85 Reliability Reliability (z-statistic) $Z_R =$ -1.04 Soil Resilient Modulus 15,000 psi

Required Structural Number (SN): SN = 2.80

DESIGN EQUATIONS

Resilient Modulus

If using CBR: If using R-Value:

 $M_R = (CBR) \times 1,500$ $M_R = 10^{[(S_1 + 18.72)/6.24]} \text{ where } S_1 = [(R\text{-value - 5})/11.29] + 3$

Required Structural Number Solves nomograph shown in Figure D-1

$$\log_{10}W_{18} = Z_{R}^{*} S_{O} + 9.36^{*}\log_{10}(SN+1) - 0.20 + \frac{\log_{10}\left[\frac{\Delta PSI}{4.2 - 1.5}\right]}{0.40 + \frac{1094}{(SN+1)^{5.19}}} + 2.32^{*}\log_{10}M_{R} - 8.07$$

Pavement Section Thickness

 $SN^* = C_1D_1 + C_2D_2$ where: $C_1 = Strength Coefficient - HMA$

 C_2 = Strength Coefficient - CTS

 $D_1 = Depth of HMA (inches)$

 D_2 = Depth of CTS (inches)

RECOMMENED THICKNESSES

Layer	Material	Coefficient	Thickness (D* _i)		SN* _i	SN
1	HMA	$C_1 = 0.44$	5.0	inches	2.200	
2	CTS	$C_2 = 0.11$	10.0	inches	1.100	-
				SN* =	3 300	2.80

Pavement SN > Required SN, Design is Acceptable