

#### INNOVATIVE DESIGN. CLASSIC RESULTS.

# FINAL DRAINAGE REPORT ADDENDUM NO. 2 BENT GRASS RESIDENTIAL FILING NO. 1 FOR BENT GRASS EAST COMMERCIAL FILING NO. 3

Prepared for: LAND FIRST INC.

1378 PROMONTORY BLUFF VIEW COLORADO SPRINGS, CO 80921 Contact: Ron Waldthausen

Prepared by:
CLASSIC CONSULTING
619 N. CASCADE AVE., SUITE 200
COLORADO SPRINGS, CO 80903
(719) 785-0790

PCD File No. SP-20-010 Job no. 2177.64



### FINAL DRAINAGE REPORT ADDENDUM NO. 2 BENT GRASS RESIDENTIAL FILING NO. 1 FOR BENT GRASS EAST COMMERCIAL FILING NO. 3

#### **DRAINAGE REPORT STATEMENT**

#### **ENGINEER'S STATEMENT:**

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the County for drainage reports and said report is in conformity with the applicable master blad of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors, or only sions on my part in preparing this report.

Marc A. Whomon Colorado P. E. #37155

Date

#### **OWNER'S/DEVELOPER'S STATEMENT:**

I, the owner/developer, have read and will comply with all of the requirements specified in this drainage report and plan.

Business Name:	Land First Inc.
Title:	President
Address:	1378 Promontory Bluff View
	Colorado Springs, CO 80921

#### **EL PASO COUNTY:**

Filed in accordance with the requirements of the Drainage Criteria Manual, Volumes 1 and 2, El Paso County Engineering Criteria Manual and Land Development Code as amended.

Jennifer Irvine, P.E.
County Engineer, / ECM Administrator

Conditions:

APPROVED Engineering Department

11/02/2021 11:19:16 AM dsdnijkamp

EPC Planning & Community Development Department



## FINAL DRAINAGE REPORT ADDENDUM NO. 2 BENT GRASS RESIDENTIAL FILING NO. 1 FOR BENT GRASS EAST COMMERCIAL FILING NO. 3

#### **TABLE OF CONTENTS:**

PURPOSE	Page	1
GENERAL DESCRIPTION	Page	1
EXISTING/DEVELOPED DRAINAGE CONDITIONS	Page	1
DRAINAGE CRITERIA	Page	3
FLOODPLAIN STATEMENT	Page	5
DRAINAGE/BRIDGE FEES	Page	5
SUMMARY	Page	7
REFERENCES	Page	8

#### **APPENDICES**

**VICINITY MAP** 

SOILS MAP (S.C.S. SURVEY)

F.E.M.A. MAP

**CALCULATIONS** 

REFERENCE MATERIAL

DRAINAGE MAP



Page iii

## FINAL DRAINAGE REPORT ADDENDUM NO. 2 BENT GRASS RESIDENTIAL FILING NO. 1 FOR BENT GRASS EAST COMMERCIAL FILING NO. 3

#### **PURPOSE**

This portion of the Bent Grass East Commercial development was previously platted as Tract B within Bent Grass East Commercial Filing No. 2B. However, it was previously analyzed from a drainage standpoint and included in the Bent Grass Residential Filing No. 1 Final Drainage Report and latest Addendum filed in 2015. The previous drainage basins K, L and M1 encompass the proposed development and re-plat of Tract B. The purpose of this report is to confirm that the existing adjacent pond indeed accounted for this development and to better define the exact routing of the proposed storm sewer into the pond and associated concrete forebay design.

#### **GENERAL DESCRIPTION**

Tract B, Bent Grass East Commercial Filing No. 2B contains a total area of 219,877 SF (5.05 AC.), located in the county of El Paso within Section 1, Township 13 South, Range 65 West of the Sixth Principal Meridian, El Paso County, Colorado. The site is bounded on the north by Bent Grass Meadows Dr., on the east by Meridian Park Dr., on the west Bent Grass Residential Filing No. 1 and to the south by the existing detention pond within Tract A of the Bent Grass East Commercial development.

The average soil condition reflects Hydrologic Group "A" (Columbine gravelly sandy loam), as determined by the "Soil Survey of El Paso County Area," prepared by the Soil Conservation Service. (See Appendix) For the purposes of the hydrologic calculations within this report, the soil type A was utilized.

#### **EXISTING/DEVELOPED DRAINAGE CONDITIONS**

The entire proposed development area was previously overlot graded along with the adjacent developments. The revegetation consists of native grasses with slopes of 2%-4%. The entire property sheet flows in a southerly direction directly into the existing detention pond 2 just south of the property.



The proposed development plans to construct a private roadway in order to provide vehicular access to the 6 lots. This private road will connect to both Bent Grass Meadows Dr. to the north and Meridian Park Dr. to the east. High points are planned at each of these two connection points with a low point near the middle of the property. (See Developed Drainage Map in Appendix)

**Design Point 1 (Q**<sub>5</sub> = **4 cfs and Q**<sub>100</sub> = **8 cfs)** represents developed flows from Basin A (lots 2 and 3 and north half of the private road). These flows will be routed towards Design Point 1 where a private 5' Type R Sump Inlet will completely collect both the 5 and 100 yr. developed flows.

**Design Point 2 (Q**<sub>5</sub> = **1 cfs and Q**<sub>100</sub> = **3 cfs)** represents developed flows from Basin B (portion of lots 4 and 5 and south half of the private road). These flows will be routed towards Design Point 2 where a private 5' Type R Sump Inlet will completely collect both the 5 and 100 yr. developed flows.

Design Point 3 ( $Q_5 = 7$  cfs and  $Q_{100} = 13$  cfs) represents developed flows from Basin C (lots 4 and 6) and a portion of off-site Basin K (existing residential development to the west). These flows will be routed towards Design Point 3 where a private 24" RCP storm stub will collect both the 5 and 100 yr. developed flows. The individual site plans for each of these lots will show how curb and gutter will collect these developed flows and route them towards the provided 24" RCP private storm stub. These flows remain consistent with Basins L ( $Q_5 = 18$  cfs and  $Q_{100} = 35$  cfs) and K ( $Q_5 = 2$  cfs and  $Q_{100} = 4$  cfs) from the previous report. (See Appendix)

**Design Point 4 (Q**<sub>5</sub> = **11 cfs and Q**<sub>100</sub> = **22 cfs)** represents the total developed flows that will enter the existing pond at this location (Basins A, B, C and a portion of Basin K). A concrete forebay is proposed within the existing pond at this location with the following criteria: (See Appendix)



Per UD-BMP Spreadsheet – Concrete Forebay sizing

0.003 Ac-ft. or 131 SF min. Forebay with 12" high walls OR 88 SF min. with 18" high walls

4.5" wide notch at end of forebay

Basin E ( $Q_5$  = 0.3 cfs and  $Q_{100}$  = 1.0 cfs) represents developed flows from Basin E (landscape/setback area within lots 1, 2 and 3) that will continue to sheet flow in a northeasterly direction and directly into Bent Grass Meadows Dr. This minor developed flow was accounted for and remains consistent with the previously approved report. Also, per ECM I.7.1.C.1.a this basin of 0.3 ac. is not practical to be captured and will not drain towards the downstream control measures.

Basin D ( $Q_5$  = 3 cfs and  $Q_{100}$  = 6 cfs) represents developed flows from Basin D (lots 1 and a portion of 5 and a portion of the private road). These flows will continue to sheet flow directly into Meridian Park Dr. They then travel as curb and gutter flows to the existing sump inlet within the cul-de-sac and then directly into the existing pond. These flows were accounted for in the previously approved drainage report and remain consistent with Basin M1 ( $Q_5$  = 6 cfs and  $Q_{100}$  = 11 cfs) from the previous report. (See Appendix)

#### **DRAINAGE CRITERIA**

Hydrologic calculations were performed using the City of Colorado Springs/El Paso County Drainage Criteria Manual, as revised in November 1991 and October 1994 with County adopted Chapter 6 and Section 3.2.1 of Chapter 13 of the City of Colorado Springs/El Paso County Drainage Criteria Manual as revised in May 2014 along with the El Paso County Engineering Criteria Manual, updated October 2020. Individual on-site developed basin design used for detention/SWQ basin sizing, inlet sizing and storm system routing was calculated using the Rational Method. Runoff Coefficients are based on the imperviousness of the particular land



use and the hydrologic soil type in accordance with Table 6-6. The average rainfall intensity, by recurrence interval found in the Intensity-Duration-Frequency (IDF) curves in Figure 6-5. (See Appendix)

The City of Colorado Springs/El Paso County DCM requires the Four Step Process for receiving water protection that focuses on reducing runoff volumes, treating the water quality capture volume (WQCV), stabilizing drainage ways, and implementing long-term source controls. The Four Step Process pertains to management of smaller, frequently occurring storm events, as opposed to larger storms for which drainage and flood control infrastructure are sized. Implementation of these four steps helps to achieve storm water permit requirements.

This site adheres to this **Four Step Process** as follows:

- Employ Runoff Reduction Practices: Proposed urban commercial lot impervious areas
  (roof tops, parking lots, drive aisles, etc.) will to the extent possible, sheet flow across
  landscaped areas to slow runoff and increase time of concentration prior to being
  conveyed to the proposed private storm systems and stormwater quality facilities. This
  will minimize directly connected impervious areas within the project site.
- 2. **Stabilize Drainageways:** After developed flows utilize the runoff reduction practices through landscaped areas, developed flows will travel via curb and gutter and buried storm sewer systems. These collected flows are then routed directly to the existing stormwater quality facility adjacent to the site (Pond 2) that was originally constructed with Bent Grass Residential Filing No. 1.
- Provide Water Quality Capture Volume (WQCV): Runoff from this development will be treated through capture and slow release of the WQCV in the existing stormwater quality facility (Pond 2).



4. Consider need for Industrial and Commercial BMPs: No industrial uses are proposed

within this development. However, a site specific storm water quality and erosion

control plan and narrative will be submitted along with the grading and erosion control

plan. Details such as site specific sediment and erosion control construction BMP's as

well as temporary and permanent BMP's will be detailed in this plan and narrative to

protect receiving waters. BMP's will be constructed and maintained as the

development has been graded and erosion control methods employed.

**FLOODPLAIN STATEMENT** 

No portion of this site is located within a FEMA floodplain as determined by the Flood Insurance

Rate Map (F.I.R.M.) Map Number 08041C0553G, with effective date of December, 7 2018. (See

Appendix)

**DRAINAGE AND BRIDGE FEES** 

This site lies entirely within the Falcon Drainage Basin boundaries.

The fees are calculated using the following impervious acreage method approved by El Paso

County. Bent Grass East Commercial Filing No. 3 has a total area of 5.048 acres with a

commercial land use designation.

The percent imperviousness for this subdivision is calculated as follows:

**Fees for Commercial Land Use** 

(Per El Paso County Percent Impervious Chart: 95%)

 $5.048 \text{ Ac. } \times 95\% = 4.796 \text{ Impervious Ac.}$ 

The following calculations are based on the 2020 Falcon drainage/bridge fees:

#### **ESTIMATED FEES:**

#### **Bridge Fees**

\$ 4,232.00 x 4.796 Impervious Ac. = **\$ 20,296.67** 

**Drainage Fees** 

\$ 30,807.00 x 4.796 Impervious Ac. = **\$ 147,750.37** 

Per the ECM 3.10.4.a, this development requests a reduction of drainage fees based on the onsite detention pond 2 that was constructed as a part of the Bent Grass Residential Filing No. 1 development. This facility within the Falcon Drainage Basin seems to meet the following criteria for this reduction:

- Allowed only where regional system is not yet in place no downstream regional facility in place yet
- 2. The pond is less than 15 acre-feet in volume from the lowest outlet structure to the crest of the emergency spillway The existing pond 2 has a volume of 2.32 ac.-ft.
- 3. The on-site pond is not part of the regional plan (for approval ponds that are part of the regional plan, developers are given 100% credit) Pond 2 is not a part of the regional plan
- 4. The outlet of the pond must be designed to release at historic levels for all precipitation events from the 2 yr. storm to the 100 yr. storm. A smaller outlet may be required by the County if adequate downstream channel improvement are not in place to protect residents from the 2 yr. storm Pond 2 was designed as a full spectrum facility
- County approves design and construction County approved the design and construction of Pond 2 along with the Bent Grass Residential Filing No. 1 development
- 6. Landowners assume responsibility for maintenance Pond 2 is owned and maintained by the Bent Grass Metro. District



Per Bent Grass East Commercial Filing No. 2 Final Drainage Report – Dated Aug. 2014

Construction of Detention Pond 2 (Full Spectrum on-site Facility) = \$75,000 \*

50% credit was taken against drainage fees owed (See Appendix) = \$37,500 – 26,860.65

Credit remaining within the Falcon Basin = \$10,639.35

\*Developer to provide receipts for previous pond const. and apply for drainage reimbursement

in order to receive credit.

**TOTAL DRAINAGE FEES (after reduction):** 

**Drainage Fees** 

\$ 147,750.37 – 10,639.35

\$ 137,111.02 \*

**SUMMARY** 

The proposed grading plan, drainage patterns and quantities remain consistent with the previously approved final drainage report for Bent Grass Residential Filing No. 1 and associated addendum. The proposed development will not adversely impact surrounding properties.

PREPARED BY:

Classic Consulting Engineers & Surveyors, LLC

Marc A. Whorton, P.E.

Project Manager

mw/217764/Reports/217764FDR Addendum.doc



Page 7

#### REFERENCES

- 1. City of Colorado Springs/County of El Paso Drainage Criteria Manual as revised in November 1991 and October 1994 with County adopted Chapter 6 and Section 3.2.1 of Chapter 13 of the City of Colorado Springs/El Paso County Drainage Criteria Manual as revised in May 2014.
- 2. "Urban Storm Drainage Criteria Manual Volume 1, 2 & 3" Urban Drainage and Flood Control District, dated January 2016.
- 3. "Falcon Drainage Basin Planning Study Update," by Matrix Design Group, dated August 2013.
- 4. "Preliminary Drainage Report for Bent Grass East Commercial Phase 1 and Final Drainage Report for Bent Grass East Commercial Filing No. 1 Lot 1", by Classic Consulting, dated May 2013
- 5. "Final Drainage Report for Bent Grass East Commercial Filing No. 2", by Classic Consulting, dated May 2014.
- 6. "Final Drainage Report for Bent Grass Residential Filing No. 1", by Classic Consulting, Sept. 2014.
- 7. "Final Drainage Report Addendum for Bent Grass Residential Filing No. 1", by Classic Consulting, August 2015.

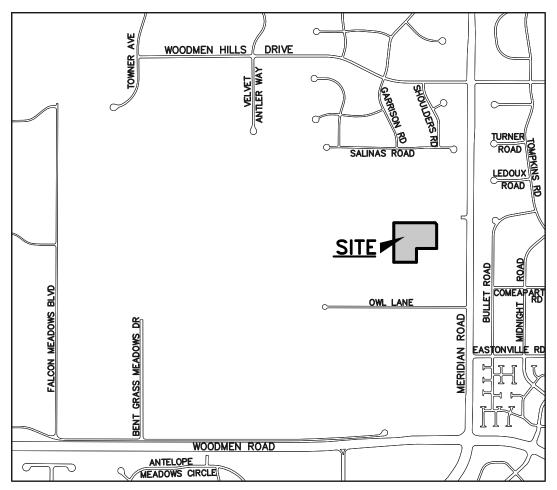


#### **APPENDIX**



**VICINITY MAP** 







### VICINITY MAP

N.T.S.

**SOILS MAP (S.C.S. SURVEY)** 





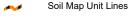
#### MAP LEGEND

#### Area of Interest (AOI)

Area of Interest (AOI)

#### Soils

Soil Map Unit Polygons



Soil Map Unit Points

#### Special Point Features

Blowout

Borrow Pit

Clay Spot

Closed Depression

Gravel Pit

Gravelly Spot

Landfill

Lava Flow

Marsh or swamp

Mine or Quarry

Miscellaneous Water

Perennial Water

Rock Outcrop

Saline Spot
Sandy Spot

Severely Eroded Spot

Sinkhole

Slide or Slip

#### \_\_..\_

Spoil Area

Stony Spot

Very Stony Spot

Wet Spot

Other

Special Line Features

#### Water Features

Δ

Streams and Canals

#### Transportation

Rails

Interstate Highways

US Routes

Major Roads

Local Roads

#### Background

Aerial Photography

#### MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24.000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service Web Soil Survey URL:

Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: El Paso County Area, Colorado Survey Area Data: Version 18, Jun 5, 2020

Soil map units are labeled (as space allows) for map scales 1:50.000 or larger.

Date(s) aerial images were photographed: Sep 11, 2018—Oct 20, 2018

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

### **Map Unit Legend**

	_		
Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
19	Columbine gravelly sandy loam, 0 to 3 percent slopes	22.5	100.0%
Totals for Area of Interest		22.5	100.0%

#### El Paso County Area, Colorado

#### 19—Columbine gravelly sandy loam, 0 to 3 percent slopes

#### **Map Unit Setting**

National map unit symbol: 367p Elevation: 6,500 to 7,300 feet

Mean annual precipitation: 14 to 16 inches
Mean annual air temperature: 46 to 50 degrees F

Frost-free period: 125 to 145 days

Farmland classification: Not prime farmland

#### **Map Unit Composition**

Columbine and similar soils: 97 percent

Minor components: 3 percent

Estimates are based on observations, descriptions, and transects of

the mapunit.

#### **Description of Columbine**

#### Setting

Landform: Fans, flood plains, fan terraces

Down-slope shape: Linear Across-slope shape: Linear Parent material: Alluvium

#### Typical profile

A - 0 to 14 inches: gravelly sandy loam
C - 14 to 60 inches: very gravelly loamy sand

#### **Properties and qualities**

Slope: 0 to 3 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Well drained Runoff class: Very low

Capacity of the most limiting layer to transmit water (Ksat): High to

very high (5.95 to 19.98 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water capacity: Very low (about 2.5 inches)

#### Interpretive groups

Land capability classification (irrigated): 4e Land capability classification (nonirrigated): 6e

Hydrologic Soil Group: A

Ecological site: R049XB215CO - Gravelly Foothill

Hydric soil rating: No

#### **Minor Components**

#### **Pleasant**

Percent of map unit: 1 percent



Landform: Depressions Hydric soil rating: Yes

#### Other soils

Percent of map unit: 1 percent Hydric soil rating: No

#### Fluvaquentic haplaquolls

Percent of map unit: 1 percent Landform: Swales Hydric soil rating: Yes

#### **Data Source Information**

Soil Survey Area: El Paso County Area, Colorado Survey Area Data: Version 18, Jun 5, 2020

F.E.M.A MAP



#### NOTES TO USERS

s map is for use in administrang the National Flood insurance Program. It doe necessarily identify, all areas subject to feoding, paracularly from local drainag urces of small size. The community map repository should be consulted to size updated or additional flood hazard information.

To obtain more detailed information in areas where Base Flood Elevations (BFEs) indier floodways have been determined users are encouraged to consult the Flood Profiles and Floodway Data and/or Summary of Soltwater Elevations tables contained within the Flood Insurance Study (FIS) report that accompanies this FIRM. Users should be aware that BFEs shown on the FIRM represent rounded whole-hoot treatment by the BFEs are intended for food nursence rating purposes only and should not be used as the sole source of flood elevation information. Accordingly, lock cleavation also presented in the FIS report should be subteed in conjunction with the FIRM for purposes of construction and/or floodplain management.

Coastal Base Flood Elevations shown on this map apply only lendward of 0.0 North American Vertical Datum of 1986 (NAVD88). Uses of this FIRM should be aware that coastal flood elevations are also provided in the Summary of Stillwate Elevations table in the Flood Insurance Study report for this principlion. Elevations thow in the Summary of Stillwater Elevations table should be used for construction and of floodpland management purposes when they are higher than the elevations shown on this FIRM.

countaries of the floodways were computed at cross sections and interpolate eitheren cross sections. The floodways were based on hydraulic considerations wit egged to requirements of the National Flood insurance Program Floodway within and other pertinent floodway data are provided in the Flood Insurance Study repore this juradiction.

he projection used in the preparation of this map was Universal Transvers-tercator (UTM) zone 13. The horizontal datum was NADBS, GRS80 spheroc Wiferences in datum, spherod, projection or UTM zones zones used in the reduction of FRMs for adjacent jurisdictions may result in shipfit positions of the projection of the

Junea most elevations in times most elevations must be compared to structure a junit elevations referenced to the same vertical datum. For information regard niversion between the National Geodetic Vertical Datum of 1929 and the No serican Vertical Datum of 1988, visit the National Geodetic Survey website 5/hwww.ngs.nosa.gow or contact the National Geodetic Survey at the follow-fress.

ional Geodetic Survey MC-3 #9202 15 East-West Highway Iver Spnng, MD 20910-3282

o obtain current elevation, description, and/or location information for bench mark hown on this map, please contact the Information Services Branch of the Nation Seodetic Survey at (301) 713-3242 or visit its website at http://www.ngs.noae.gov/.

ase Map information shown on this FIRM was provided in digital format by El Pass purity, Cotorado Springs Utildes, City of Fourhain, Bureau of Land Management thomal Coeano and Almospheric Administration, Univide States Geological Survey of Anderson Consulting Engineers. Inc. These data are current as of 2006

This map reflects more definited and up-to-date stream channel configurations an locotyplain definition than those shown on the previous FIRM for this jurisdiction file floopophars and floodways that were transferred from the previous FIRM may have been adjusted to conform to these new stream channel configurations. As a several channel configurations are selected from the previous FIRM may save been adjusted to conform to these new stream channel configurations. As a several channel configuration and the selected from the stream channel instances that differ from what is shown on this map. The profile baselines depicted in this map represent the hydraulic modeling baselines that match the flood profiles and Floodway Data Tables's deplicable, in the FIS report. As a result, the profile asselines may devalte agrificantly shown the new base map channel representation of may appear outside of the doodplain.

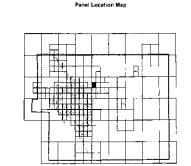
rporate limits shown on this map are based on the best data available at the time publication. Because changes due to annexations or de-annexations may have survice after this map was published, map users should contact appropriate immortly officials to venify current corporate limit locations.

Please refer to the separately printed Map Index for an overview map of the count howing the layout of map panels; community map repository addresses, and a staing of Communities table containing Nasional Flood Insurance Program dates to each community as well as a listing of the panels on which each community is

Contact FEMA Map Service Center (MSC) via the FEMA Map Information exchange (FMIX) 1-877-335-3627 bir information on available products associated with this FIRM. Available products may include previously issued Letters of Map Change, a Flood insurance Study Report, and/or option versions of this map. The MSC may see the content of the Map Change of th

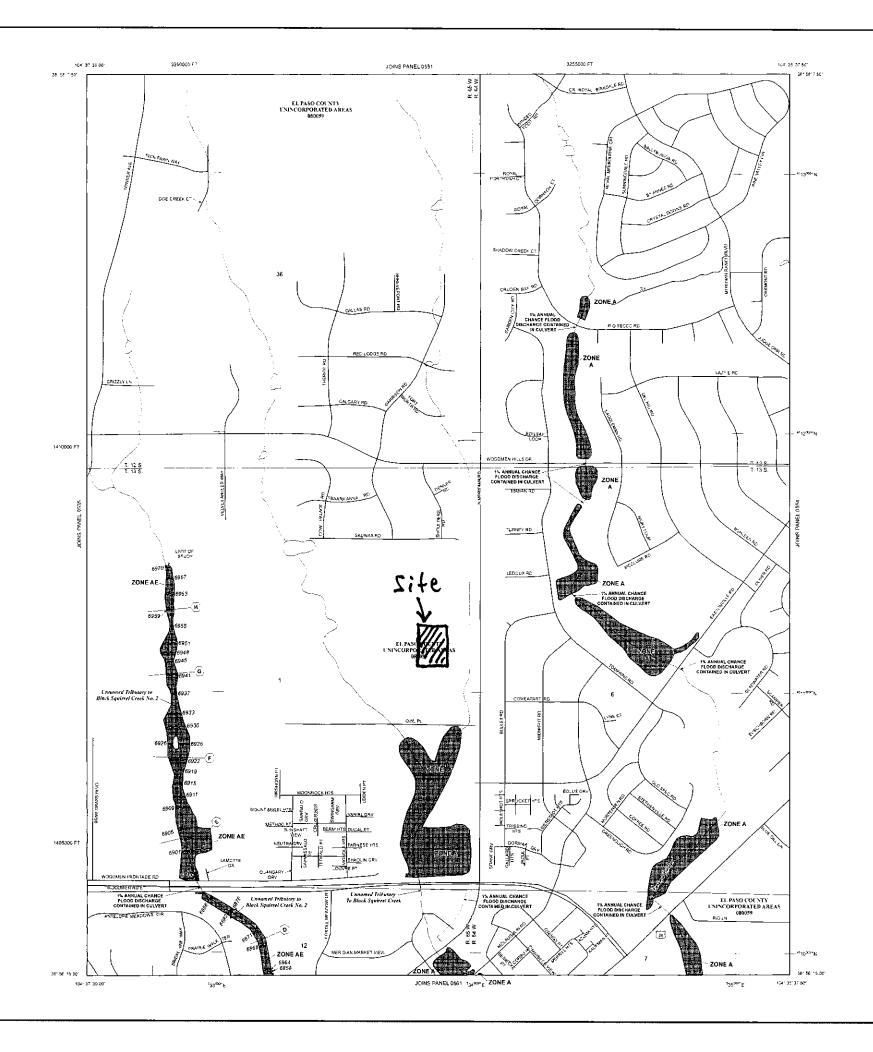
If you have questions about this map or questions concerning the National Floo Insurance Program in general, please call 1-877-FEMA MAP (1-877-336-2627) of visit the FEMA website at http://www.fema.gov/business/nfip

## OBSENTA REFER TO SECTION 3.3 OF THE EL PASC COUNTY FLOOD INSURANCE STU FOR STREAM BY STREAM VERTICAL DATUM CONVERSION INFORMATION



This Digital Flood Insurance Rate Map (DFIRM) was produced through a Cooperating Technical Pariner (CTP) agreement between the State of Colorado Water Conservation Board (CWCB) and the Federal Emergency Management Agency (FEMA).





#### LEGEND

SPECIA: FLOOD HAZARD AREAS (SFHAS) SUBJECT TO INUNDATION BY THE 1% ANNUAL CHANCE FLOOD

ZONE A No East Food Beratums determined.

ZONE AE Bose Flood Eevations determined.

ZONE AN Food decrits of 1 to 5 feet (us.eh) attest of pording), Base Flood Beratum determined.

Food depths of 1 to 3 feet (usually sheet flow on ploping terrain); average occurs occurs mean in a rear of attivial fain flooding, viscoluss also determined.

determined.

Social Rocci Agrand Area humenly protected from the 1% annual chance food by a food control system that was subsequently described. Zone At more that that the former food control system is being restared to provide protection from the 1% annual chance or greater food. Area to be protected from the annual chance flood by a federal flood protection system under construction no Base Flood Elevations

Coesta fluor zone with velocity hazard (wave action); no Base Ford Blevation; determined

Coasta Food zone with velocity hazard (wave action): Base Food Elevations determined:

FLOODWAY AREAS IN ZONE AE

The floodway is the channel of a stream plus any adjacent floodpain areas that must be vept firet of encreatment so that the 1% annual chance fixed can be camed without worldarful interesses in flood begins.

OTHER FLOOD AREAS

Areas of 0.2% article, chance flood, areas of 1% annual chance flood with average depths of less than 1 floot or with dramage areas less than 1 square milet and areas protected by leves from 1% and ual chance flood ZONE X

OTHER AREAS

Areas determined at the outside the 0.2% annual chance floods air. ZONE b. Areas in which food nazards are undetermined, but possible.

COASTAL BARRIER RESOURCES SYSTEM (CBRS) AREAS

OTHERWISE PROTECTED AREAS (OPAs)

CBRS areas and OPAs are normally located within or adjacent to Special Flood Hazert Areas Roodway boundary

Zone D Boundary

reanwood ARO bine 2980

 Boundary dividing Special Flood Hazard Areas of different Base Flood Elevations, flood depths or flood velocities Base Flood Everyation line and value: elevation in feet\* Base Flood Elevation value where unaform within zone, elevation in feet?

Erose seabor, noe

~~ 513 ~~

23 -----23 Transect line

Geographic cooldinates referenced to the horth America: Datum of 1963 (NAD 83) 47500-N 1000-meter Universal Transverse Mercator grid ticks. 2016;13

5000-foot grid tipes: Cookedo State Plane coordinate system central zone (FIPSZONE 0502). Lambert Conformal Conic Projection

Bench mark (see explanation in Notes to tise's section of this FIRM penel)

River Mae MAP REPOS TORIES
Refer to Map Repositories I stron Map Index

FFECTIVE DATE OF COUNTYVIDE FLOOD INSURANCE RATE VAP MARCH 17, 1997

EFFECTIVE DATE(S) OF REVISION S) TO THIS PANEL DECEMBER 7, 7018 to lydder colporate times to change Base Flood Bevisions and Special Short Hazard Areas, to broade max format it, add roads and read roams and to interpolate devices is also became the Max Revision.

For community map revision history prior to country at mapping, refer to the Community Map History Table Mosted in the Flood Insurance Study report for this pursolation.

To determine if flood insurance is evarable in the community, contact your insurance agent or call the hational Flood Insurance Program at 1-800-638-6620.

MAP SCALE 1" = 500" 250 0 500 1000 FEET

METERS 300

PR00

NAMINONAL FLOODINSURVANICE

PANEL 0553G

#### FIRM

FLOOD INSURANCE RATE MAP EL PASO COUNTY, COLORADO

AND INCORPORATED AREAS

PANEL 553 OF 1300

COMMONITY

(SEE MAP INDEX FOR FIRM PANEL LAYOU

NUMBER PANEL SUFFIX

DECEM ::ES (

Notice: This may was respected on 05:15:7070 Y. mark a corrector This version to be set for the course of the set of the course of the course



MAP NUMBER 08041C0553G

MAP REVISED DECEMBER 7, 2018

Federal Emergency Management Agency

#### **CALCULATIONS**



DB NAME: BENT GRASS EAST COMMERCIAL FILING NO. 3

JOB NAME: BENT GRA
JOB NUMBER: 2177.64
DATE: 11/04/20

CALCULATED BY: MAW

#### FINAL DRAINAGE REPORT ~ BASIN RUNOFF COEFFICIENT SUMMARY

		IMP	PERVIOUS A	REA / STREI	TS	LAND	SCAPE/UNI	DEVELOPED	AREAS	V	WEIGHTED			WEIGHTED C	A
BASIN	TOTAL AREA (AC)	AREA (AC)	C(2)	C(5)	C(100)	AREA (AC)	C(2)	C(5)	C(100)	C(2)	C(5)	C(100)	CA(2)	CA(5)	CA(100)
Α	1.4	1.10	0.89	0.90	0.96	0.30	0.02	0.08	0.35	0.70	0.72	0.83	0.99	1.01	1.16
В	0.4	0.30	0.89	0.90	0.96	0.10	0.02	0.08	0.35	0.67	0.70	0.81	0.27	0.28	0.32
С	2.0	1.60	0.89	0.90	0.96	0.40	0.02	0.08	0.35	0.72	0.74	0.84	1.43	1.47	1.68
D	0.9	0.75	0.89	0.90	0.96	0.15	0.02	0.08	0.35	0.75	0.76	0.86	0.67	0.69	0.77
Е	0.3	0.05	0.89	0.90	0.96	0.25	0.02	0.08	0.35	0.17	0.22	0.45	0.05	0.07	0.14
K	1.0	0.35	0.89	0.90	0.96	0.65	0.02	0.08	0.35	0.32	0.37	0.56	0.32	0.37	0.56

JOB NAME: BENT GRASS EAST COMMERCIAL FILING NO. 3

JOB NUMBER: 2177.64

DATE: 11/04/20
CALC'D BY: MAW

 $t_i = \frac{0.395 (1.1 - C_5) \sqrt{L}}{S^{0.33}} \qquad \qquad \mathcal{V} = C_v S_w^{-0.5} \qquad \text{Tc=L/V}$ 

Table 6-7. Conveyance Coefficient, Cv

Type of Land Surface	$C_v$
Heavy meadow	2.5
Tillage/field L	5
Riprap (not buried)* $I_c = \frac{180}{180}$	6.5
Short pasture and lawns	7
Nearly bare ground	10
Grassed waterway	15
Paved areas and shallow paved swales	20

For buried riprap, select C<sub>v</sub> value based on type of vegetative cover.

#### FINAL DRAINAGE REPORT ~ BASIN RUNOFF SUMMARY

			WEIGHTE	)		OVER	LAND		STRE	ET / CH	IANNEL	FLOW	Tc	IN	NTENSIT	Υ	тот	AL FLO	)WS
BASIN	TOTAL AREA (AC)	CA(2)	CA(5)	CA(100)	C(5)	Length (ft)	Height (ft)	Tc (min)	Length (ft)	Slope (%)	Velocity (fps)	Tc (min)	TOTAL (min)	l(2) (in/hr)	l(5) (in/hr)	I(100) (in/hr)	Q(2) (cfs)	Q(5) (cfs)	Q(100) (cfs)
А	1.4	0.99	1.01	1.16	0.08	30	2	5.4	250	2.0%	1.0	4.2	9.6	3.34	4.19	7.03	3	4	8
В	0.4	0.27	0.28	0.32	0.08	10	0.2	4.6	100	1.5%	0.9	1.9	6.6	3.79	4.76	7.99	1	1	3
С	2.0	1.43	1.47	1.68	0.08	30	1.5	5.9	400	2.0%	1.0	6.7	12.7	3.01	3.77	6.34	4	6	11
D	0.9	0.67	0.69	0.77	0.08	10	0.2	4.6	200	2.0%	1.4	2.4	7.0	3.72	4.67	7.83	2	3	6
Е	0.3	0.05	0.07	0.14	0.08	25	0.5	7.3					7.3	3.67	4.60	7.72	0.2	0.3	1.0
K	1.0	0.32	0.37	0.56	0.08	65	3	9.0					9.0	3.43	4.29	7.21	1	2	4

JOB NAME: BENT GRASS EAST COMMERCIAL FILING NO. 3

JOB NUMBER: 2177.64

DATE: 11/04/20

CALCULATED BY:  $\overline{MAW}$ 

#### FINAL DRAINAGE REPORT ~ SURFACE ROUTING SUMMARY

					Intensity		Fle	ow	
Design Point(s)	Contributing Basins	Equivalent CA(5)	Equivalent CA(100)	Maximum Tc	I(5)	I(100)	Q(5)	Q(100)	Outfall / Inlet Size
1	А	1.01	1.16	9.6	4.19	7.03	4	8	5' Type R Sump Inlet
2	В	0.28	0.32	6.6	4.76	7.99	1	3	5' Type R Sump Inlet
3	C, 70% K	1.73	2.07	12.7	3.77	6.34	7	13	24" RCP Stub
4	A, B, C, 70% K	3.02	3.55	12.8	3.76	6.32	11	22	Concrete Forebay

#### Version 4.05 Released March 2017

#### ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)
BENT GRASS EAST COMMERCIAL FILING NO. 3
DP1

Project: Inlet ID:

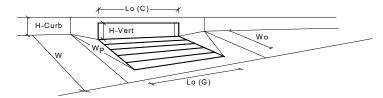
Tv STREET

#### Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb T<sub>BACK</sub> = 7.0 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) $S_{\text{BACK}}$ ft/ft 0.020 Manning's Roughness Behind Curb (typically between 0.012 and 0.020) 0.020 Height of Curb at Gutter Flow Line H<sub>CURB</sub> : 6.00 inches Distance from Curb Face to Street Crown T<sub>CROWN</sub> 14.0 Gutter Width w : 2.00 Street Transverse Slope S<sub>X</sub> = 0.020 ft/ft S<sub>W</sub> Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) ft/ft 0.083 Street Longitudinal Slope - Enter 0 for sump condition So 0.000 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) n<sub>STREET</sub> = 0.016 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm 14.0 14.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm 6.0 12.0 Check boxes are not applicable in SUMP conditions MINOR STORM Allowable Capacity is based on Depth Criterion Major Storm Minor Storm MAJOR STORM Allowable Capacity is based on Depth Criterion SUMP SUMP cfs

217764 UD-Inlet v4.05.xlsm, DP1 11/4/2020, 11:39 AM

#### **INLET IN A SUMP OR SAG LOCATION**

Version 4.05 Released March 2017



Design Information (Input) CDOT Type R Curb Opening   ■		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a <sub>local</sub> =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	6.0	12.0	inches
Grate Information		MINOR	MAJOR	Override Depths
Length of a Unit Grate	L <sub>0</sub> (G) =	N/A	N/A	feet
Width of a Unit Grate	W <sub>o</sub> =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A <sub>ratio</sub> =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	C <sub>f</sub> (G) =	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C <sub>w</sub> (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	C <sub>o</sub> (G) =	N/A	N/A	
Curb Opening Information	_	MINOR	MAJOR	
Length of a Unit Curb Opening	L <sub>o</sub> (C) =	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H <sub>vert</sub> =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H <sub>throat</sub> =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W <sub>p</sub> =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	C <sub>w</sub> (C) =	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	C <sub>o</sub> (C) =	0.67	0.67	]
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d <sub>Grate</sub> =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d <sub>Curb</sub> =	0.33	0.83	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF <sub>Combination</sub> =	0.77	1.00	
Curb Opening Performance Reduction Factor for Long Inlets	RF <sub>Curb</sub> =	1.00	1.00	
Grated Inlet Performance Reduction Factor for Long Inlets	RF <sub>Grate</sub> =	N/A	N/A	]
		MINOR	MAJOR	_
Total Inlet Interception Capacity (assumes clogged condition)	Q <sub>a</sub> =	5.4	12.3	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	4.0	8.0	cfs

217764 UD-Inlet\_v4.05.xlsm, DP1 11/4/2020, 11:39 AM

#### Version 4.05 Released March 2017

#### ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)
BENT GRASS EAST COMMERCIAL FILING NO. 3
DP2

Project: Inlet ID:

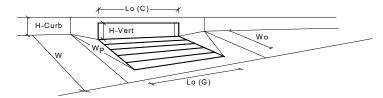
Tv STREET

#### Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb T<sub>BACK</sub> = 7.0 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) $S_{\text{BACK}}$ ft/ft 0.020 Manning's Roughness Behind Curb (typically between 0.012 and 0.020) 0.020 Height of Curb at Gutter Flow Line H<sub>CURB</sub> : 6.00 inches Distance from Curb Face to Street Crown T<sub>CROWN</sub> 14.0 Gutter Width w : 2.00 Street Transverse Slope S<sub>X</sub> = 0.020 ft/ft S<sub>W</sub> Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) ft/ft 0.083 Street Longitudinal Slope - Enter 0 for sump condition So 0.000 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) n<sub>STREET</sub> = 0.016 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm 14.0 14.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm 6.0 12.0 Check boxes are not applicable in SUMP conditions MINOR STORM Allowable Capacity is based on Depth Criterion Major Storm Minor Storm MAJOR STORM Allowable Capacity is based on Depth Criterion SUMP SUMP cfs

217764 UD-Inlet v4.05.xlsm, DP2 11/4/2020, 11:40 AM

#### **INLET IN A SUMP OR SAG LOCATION**

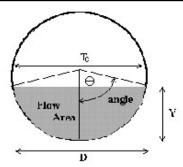
Version 4.05 Released March 2017



Design Information (Input)  CDOT Type R Curb Opening		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a <sub>local</sub> =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	6.0	12.0	inches
Grate Information		MINOR	MAJOR	Override Depths
Length of a Unit Grate	L <sub>0</sub> (G) =	N/A	N/A	feet
Width of a Unit Grate	W <sub>o</sub> =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A <sub>ratio</sub> =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	C <sub>f</sub> (G) =	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C <sub>w</sub> (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	C <sub>o</sub> (G) =	N/A	N/A	
Curb Opening Information	_	MINOR	MAJOR	_
Length of a Unit Curb Opening	L <sub>o</sub> (C) =	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H <sub>vert</sub> =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H <sub>throat</sub> =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W <sub>p</sub> =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	C <sub>w</sub> (C) =	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	C <sub>o</sub> (C) =	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d <sub>Grate</sub> =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d <sub>Curb</sub> =	0.33	0.83	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF <sub>Combination</sub> =	0.77	1.00	
Curb Opening Performance Reduction Factor for Long Inlets	RF <sub>Curb</sub> =	1.00	1.00	
Grated Inlet Performance Reduction Factor for Long Inlets	RF <sub>Grate</sub> =	N/A	N/A	
		MINOR	MAJOR	_
Total Inlet Interception Capacity (assumes clogged condition)	<b>Q</b> <sub>a</sub> =	5.4	12.3	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	1.0	3.0	cfs

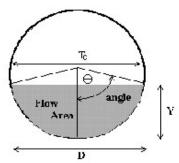
217764 UD-Inlet\_v4.05.xlsm, DP2 11/4/2020, 11:40 AM

## Project: BENT GRASS EAST COMMERCIAL FILING NO. 3 Pipe ID: 24" RCP (DP-1)



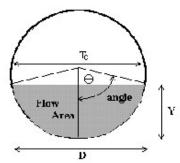
Design Information (Input)Pipe Invert SlopeSo = 0.0100 ft/ftPipe Manning's n-valuen = 0.0130 inchesPipe DiameterD = 24.00 inchesDesign dischargeQ = 8.00 cfsFull-Flow Capacity (Calculated)Full-flow areaAf = 3.14 sq ftFull-flow wetted perimeterPf = 6.28 ftHalf Central AngleTheta = 3.14 radiansFull-flow capacityQf = 22.68 cfsCalculation of Normal Flow ConditionHalf Central Angle (0 <theta<3.14)< td="">Theta = 1.39 radiansFlow areaAn = 1.21 sq ftTop widthTn = 1.97 ftWetted perimeterPn = 2.78 ftFlow depthYn = 0.82 ftFlow depthYn = 6.59 fpsDischargeQn = 8.00 cfsPercent of Full FlowFlow = 35.3% of full flowNormal Depth Froude NumberFr = 1.48 supercriticalCalculation of Critical Flow ConditionHalf Central Angle (0<theta-c<3.14)< td="">Theta-c = 1.58 radians</theta-c<3.14)<></theta<3.14)<>	Danian Information (Innat)			
Pipe Manning's n-value Pipe Diameter Design discharge  Q = 8.00 cfs  Full-Flow Capacity (Calculated) Full-flow area Full-flow wetted perimeter Half Central Angle Full-flow capacity Calculation of Normal Flow Condition Half Central Angle (0 <theta<3.14) af="3.14" area="" c<="" capacity="" cfs="" d="24.00" depth="" discharge="" flow="" ft="" full-flow="" inches="" manning's="" n-value="" perimeter="" pn="1.27" pripe="" radians="" sq="" td="" theta="1.39" tn="1.97" top="" velocity="" wetted="" width=""><td><del>-</del></td><td></td><td></td><td><b>T</b>a. (5</td></theta<3.14)>	<del>-</del>			<b>T</b> a. (5
Pipe Diameter Design discharge $ \begin{array}{c} D = & 24.00 \\ Q = & 8.00 \end{array}                                 $	•			ft/ft
Design discharge $Q = 8.00   cfs$ $\overline{Full-Flow Capacity (Calculated)}$ Full-flow area $Af = 3.14   sq ft$ Full-flow wetted perimeter $Pf = 6.28   ft$ Half Central Angle $Theta = 3.14   radians$ Full-flow capacity $Qf = 22.68   cfs$ $\overline{Calculation of Normal Flow Condition}$ Half Central Angle $(0 < Theta < 3.14)$ $Theta = 1.39   radians$ Flow area $An = 1.21   sq ft$ Top width $Tn = 1.97   ft$ Wetted perimeter $Pn = 2.78   ft$ Flow depth $Yn = 0.82   ft$ Flow velocity $Vn = 6.59   fps$ Discharge $Qn = 8.00   cfs$ Percent of Full Flow $Plow = 35.3\%   of full flow$ Normal Depth Froude Number $Fr_n = 1.48   supercritical$ $\overline{Calculation of Critical Flow Condition}$ Half Central Angle $(0 < Theta < < 3.14)$ $Theta = 3.14   radians$	•	• • • • • • • • • • • • • • • • • • • •		
	•	D =		
Full-flow area $ Af = 3.14                                   $	Design discharge	Q =	8.00	cfs
Full-flow area $ Af = 3.14                                   $				
Full-flow wetted perimeter $ Pf = 6.28 \\ Half Central Angle \\ Full-flow capacity \\ Qf = 22.68 \\ Cfs \\ \hline                                  $				_
Half Central Angle Theta = $3.14$ radians Calculation of Normal Flow Condition  Half Central Angle (0 <theta<3.14) theta="&lt;math">1.39 radians  Flow area An = <math>1.21</math> sq ft  Top width Tn = <math>1.97</math> ft  Wetted perimeter Pn = <math>2.78</math> ft  Flow depth Yn = <math>0.82</math> ft  Flow velocity Vn = <math>6.59</math> fps  Discharge Qn = <math>8.00</math> cfs  Percent of Full Flow Normal Depth Froude Number Fr<sub>n</sub> = <math>1.48</math> supercritical  Calculation of Critical Flow Condition  Half Central Angle (0<theta-c<3.14) theta-c="&lt;math">1.58 radians</theta-c<3.14)></theta<3.14)>	Full-flow area			sq ft
Full-flow capacity $Qf =                                  $	Full-flow wetted perimeter	Pf =	6.28	ft
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	Half Central Angle	Theta =	3.14	radians
Half Central Angle (0 <theta<3.14) (0<theta-c<3.14)="" an="1.21" angle="" area="" calculation="" central="" condition="" critical="" depth="" discharge="" flow="" froude="" ft="" full="" half="" normal="" number="" of="" percent="" perimeter="" radians="" radians<="" sq="" td="" theta="1.39" tn="1.97" top="" velocity="" wetted="" width=""><td>Full-flow capacity</td><td>Qf =</td><td>22.68</td><td>cfs</td></theta<3.14)>	Full-flow capacity	Qf =	22.68	cfs
Half Central Angle (0 <theta<3.14) (0<theta-c<3.14)="" an="1.21" angle="" area="" calculation="" central="" condition="" critical="" depth="" discharge="" flow="" froude="" ft="" full="" half="" normal="" number="" of="" percent="" perimeter="" radians="" radians<="" sq="" td="" theta="1.39" tn="1.97" top="" velocity="" wetted="" width=""><td></td><td></td><td></td><td></td></theta<3.14)>				
Flow area $An = 1.21 \qquad \text{sq ft}$ Top width $Tn = 1.97 \qquad \text{ft}$ Wetted perimeter $Pn = 2.78 \qquad \text{ft}$ Flow depth $Yn = 0.82 \qquad \text{ft}$ Flow velocity $Vn = 6.59 \qquad \text{fps}$ Discharge $Qn = 8.00 \qquad \text{cfs}$ Percent of Full Flow $Plow = 35.3\% \qquad \text{of full flow}$ Normal Depth Froude Number $Pr_n = 1.48 \qquad \text{supercritical}$ Calculation of Critical Flow Condition $Pr_n = 1.58 \qquad \text{radians}$	Calculation of Normal Flow Condition			_
Top width $ Tn = 1.97                                   $	5 (	Theta =		radians
$\begin{array}{llllllllllllllllllllllllllllllllllll$	Flow area	An =	1.21	sq ft
Flow depth $ Yn = 0.82                                   $	Top width	Tn =	1.97	
Flow velocity $ Vn = 6.59 \\ Discharge \\ Percent of Full Flow \\ Normal Depth Froude Number \\ Fr_n = 1.48 \\ Calculation of Critical Flow Condition \\ Half Central Angle (0$	Wetted perimeter	Pn =	2.78	ft
Discharge $\begin{array}{cccccccccccccccccccccccccccccccccccc$	Flow depth	Yn =	0.82	ft
Percent of Full Flow Flow = $35.3\%$ of full flow Normal Depth Froude Number Fr $_n$ = $1.48$ supercritical Calculation of Critical Flow Condition Half Central Angle (0 <theta-c<3.14) theta-c="&lt;math">1.58 radians</theta-c<3.14)>	Flow velocity	Vn =	6.59	fps
Normal Depth Froude Number $Fr_{n} = \frac{1.48}{\text{Supercritical}}$ Supercritical $\frac{\text{Calculation of Critical Flow Condition}}{\text{Half Central Angle (0 Theta-c = \frac{1.58}{\text{radians}} radians$	Discharge	Qn =	8.00	cfs
Calculation of Critical Flow Condition  Half Central Angle (0 <theta-c<3.14) radians<="" td="" theta-c="1.58"><td>Percent of Full Flow</td><td>Flow =</td><td>35.3%</td><td>of full flow</td></theta-c<3.14)>	Percent of Full Flow	Flow =	35.3%	of full flow
Half Central Angle (0 <theta-c<3.14) radians<="" td="" theta-c="1.58"><td>Normal Depth Froude Number</td><td>Fr<sub>n</sub> =</td><td>1.48</td><td>supercritical</td></theta-c<3.14)>	Normal Depth Froude Number	Fr <sub>n</sub> =	1.48	supercritical
Half Central Angle (0 <theta-c<3.14) radians<="" td="" theta-c="1.58"><td></td><td></td><td></td><td><del>-</del></td></theta-c<3.14)>				<del>-</del>
	Calculation of Critical Flow Condition			
	Half Central Angle (0 <theta-c<3.14)< td=""><td>Theta-c =</td><td>1.58</td><td>radians</td></theta-c<3.14)<>	Theta-c =	1.58	radians
Critical flow area $Ac = $   1.58   sq ft	Critical flow area	Ac =	1.58	sq ft
Critical top width $Tc = 2.00$ ft	Critical top width	Tc =	2.00	ft
Critical flow depth Yc = 1.01 ft	Critical flow depth	Yc =	1.01	ft
Critical flow velocity $Vc = 5.05$ fps	Critical flow velocity	Vc =	5.05	fps
Critical Depth Froude Number Fr <sub>c</sub> = 1.00		Fr <sub>c</sub> =	1.00	
		· <u></u>		<b>-</b>

## CIRCULAR CONDUIT FLOW (Normal & Critical Depth Computation) MHFD-Culvert, Version 4.00 (May 2020) Project: BENT GRASS EAST COMMERCIAL FILING NO. 3 Pipe ID: 24" RCP (DP-1 & DP-2)



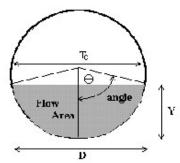
Design Information (Input)			_
Pipe Invert Slope	So =	0.0100	ft/ft
Pipe Manning's n-value	n =	0.0130	
Pipe Diameter	D =	24.00	inches
Design discharge	Q =	10.00	cfs
Full-Flow Capacity (Calculated)			
Full-flow area	Af =	3.14	sq ft
Full-flow wetted perimeter	Pf =	6.28	ft
Half Central Angle	Theta =	3.14	radians
Full-flow capacity	Qf =	22.68	cfs
Calculation of Normal Flow Condition			
Half Central Angle (0 <theta<3.14)< td=""><td>Theta =</td><td>1.50</td><td>radians</td></theta<3.14)<>	Theta =	1.50	radians
Flow area	An =	1.43	sq ft
Top width	Tn =	2.00	ft
Wetted perimeter	Pn =	3.00	ft
Flow depth	Yn =	0.93	ft
Flow velocity	Vn =	6.99	fps
Discharge	Qn =	10.00	cfs
Percent of Full Flow	Flow =	44.1%	of full flow
Normal Depth Froude Number	Fr <sub>n</sub> =	1.46	supercritical
<u>Calculation of Critical Flow Condition</u>			<b>–</b>
Half Central Angle (0 <theta-c<3.14)< td=""><td>Theta-c =</td><td>1.70</td><td>radians</td></theta-c<3.14)<>	Theta-c =	1.70	radians
Critical flow area	Ac =	1.83	sq ft
Critical top width	Tc =	1.98	ft
Critical flow depth	Yc =	1.13	ft
Critical flow velocity	Vc =	5.46	fps
Critical Depth Froude Number	Fr <sub>c</sub> =	1.00	

## Project: BENT GRASS EAST COMMERCIAL FILING NO. 3 Pipe ID: 24" RCP (DP-3)



Design Information (Input)			
Pipe Invert Slope	So =	0.0100	ft/ft
Pipe Manning's n-value	n =	0.0130	
Pipe Diameter	D =	24.00	inches
Design discharge	Q =	13.00	cfs
Full-Flow Capacity (Calculated)		2.11	¬ ,
Full-flow area	Af =	3.14	sq ft
Full-flow wetted perimeter	Pf =	6.28	ft
Half Central Angle	Theta =	3.14	radians
Full-flow capacity	Qf =	22.68	cfs
Calculation of Normal Flow Condition			
Half Central Angle (0 <theta<3.14)< td=""><td>Theta =</td><td>1.66</td><td>radians</td></theta<3.14)<>	Theta =	1.66	radians
Flow area	An =	1.74	sq ft
Top width	Tn =	1.99	⊢ <sub>ft</sub> '
Wetted perimeter	Pn =	3.31	H <sub>ft</sub>
Flow depth	Yn =	1.09	T <sub>ft</sub>
Flow velocity	Vn =	7.47	fps
Discharge	On =	13.00	cfs
Percent of Full Flow	Flow =	57.3%	of full flow
Normal Depth Froude Number	Fr <sub>n</sub> =	1.41	supercritical
Calculation of Critical Flow Condition			
Calculation of Critical Flow Condition	Thota a -	1 07	radians
Half Central Angle (0 <theta-c<3.14) area<="" critical="" flow="" td=""><td>Theta-c = Ac =</td><td>1.87 2.16</td><td></td></theta-c<3.14)>	Theta-c = Ac =	1.87 2.16	
	· · · · -		sq ft ⊕
Critical top width	Tc = Yc =	1.91 1.30	ft ft
Critical flow depth			<b>⊣</b> ''
Critical flow velocity	Vc =	6.03	fps
Critical Depth Froude Number	$Fr_c = $	1.00	

## CIRCULAR CONDUIT FLOW (Normal & Critical Depth Computation) MHFD-Culvert, Version 4.00 (May 2020) Project: BENT GRASS EAST COMMERCIAL FILING NO. 3 Pipe ID: 30" RCP (DP-4)

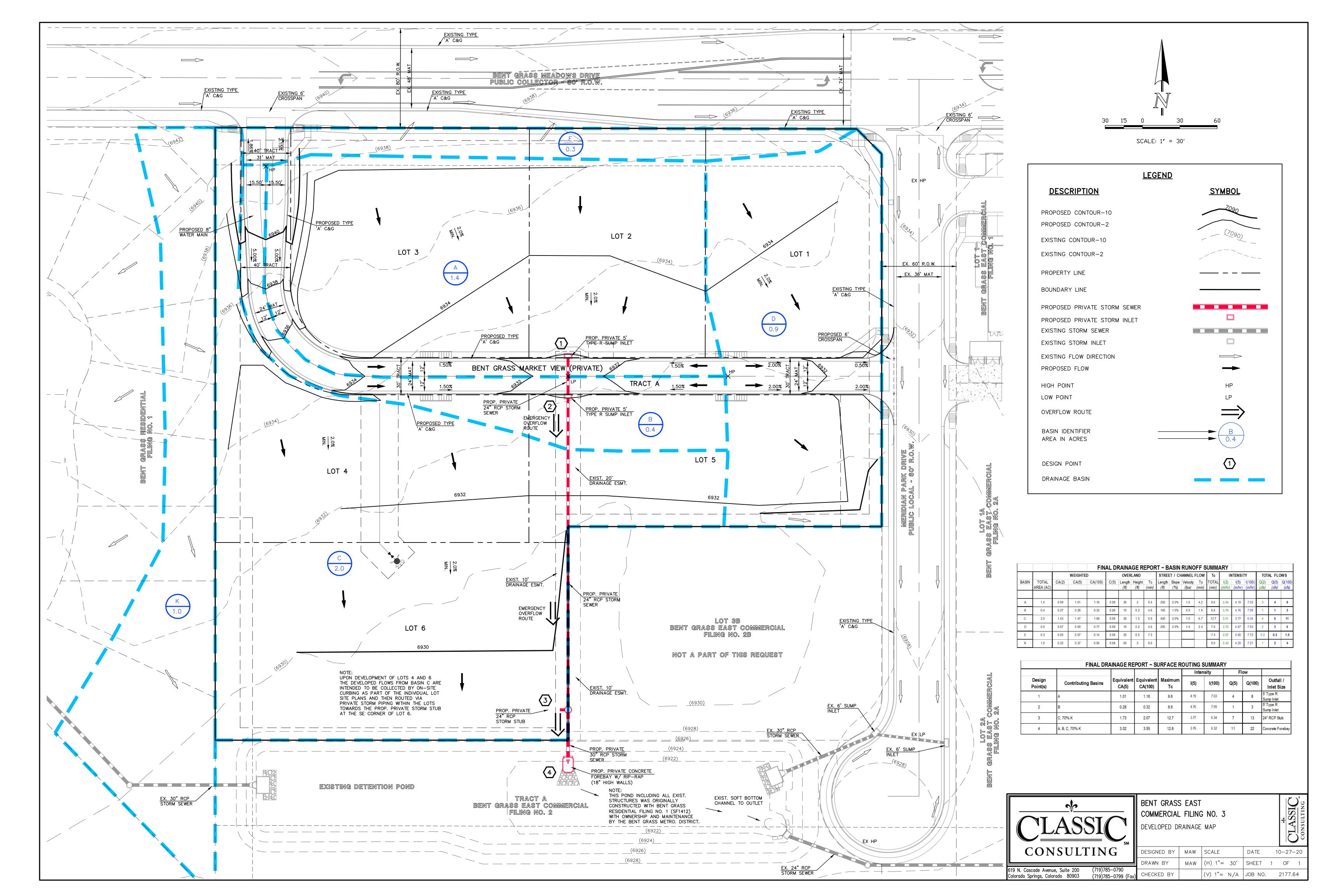


Design Information (Input)			_
Pipe Invert Slope	So =	0.0100	ft/ft
Pipe Manning's n-value	n =	0.0130	
Pipe Diameter	D =	30.00	inches
Design discharge	Q =	22.00	cfs
L Full-Flow Capacity (Calculated)			
Full-flow area	Af =	4.91	sq ft
Full-flow wetted perimeter	Pf =	7.85	H <sub>ff</sub>
Half Central Angle	Theta =	3.14	radians
Full-flow capacity	Of =	41.13	cfs
l dir now capacity	٠٠ –	11.13	
Calculation of Normal Flow Condition			
Half Central Angle (0 <theta<3.14)< td=""><td>Theta =</td><td>1.61</td><td>radians</td></theta<3.14)<>	Theta =	1.61	radians
Flow area	An =	2.58	sq ft
Top width	Tn =	2.50	ft
Wetted perimeter	Pn =	4.03	T <sub>ft</sub>
Flow depth	Yn =	1.30	ft
Flow velocity	Vn =	8.52	fps
Discharge	Qn =	22.00	cfs
Percent of Full Flow	Flow =	53.5%	of full flow
Normal Depth Froude Number	Fr <sub>n</sub> =	1.48	supercritical
Calculation of Critical Flow Condition			
Half Central Angle (0 <theta-c<3.14)< td=""><td>Theta-c =</td><td>1.85</td><td>radians</td></theta-c<3.14)<>	Theta-c =	1.85	radians
Critical flow area	Ac =	3.31	sq ft
Critical top width	Tc =	2.40	H <sub>ft</sub>
Critical flow depth	Yc =	1.59	ft
Critical flow velocity	Vc =	6.66	fps
Critical Depth Froude Number	Fr <sub>c</sub> =	1.00	

Design Procedure Form: Extended Detention Basin (EDB)				
UD-BMP (Version 3.07, March 2018)  Sheet 1 of 3				
Designer:	Marc A. Whorton, P.E.			
Company:	Classic Consulting			
Date: Project:	November 4, 2020  Bent Grass East Commercial Filing No. 3			
Location:	Exist. Pond - Proposed Forebay for Commercial Development			
Location.				
Basin Storage V	olume			
A) Effective Imperviousness of Tributary Area, I <sub>a</sub>		I <sub>a</sub> = 90.0 %		
B) Tributary Are	a's Imperviousness Ratio (i = I <sub>a</sub> / 100 )	i = 0.900		
C) Contributing	Watershed Area	Area = 4.500 ac		
D) For Watersh Runoff Prod	eds Outside of the Denver Region, Depth of Average ucing Storm	d <sub>6</sub> = 0.42 in		
E) Design Cond (Select EUR)	ept / when also designing for flood control)	Choose One  Water Quality Capture Volume (WQCV)  Excess Urban Runoff Volume (EURV)		
	ne (WQCV) Based on 40-hour Drain Time .0 * (0.91 * i² - 1.19 * i² + 0.78 * i) / 12 * Area)	V <sub>DESIGN</sub> = ac-ft		
Water Quali	eds Outside of the Denver Region, y Capture Volume (WQCV) Design Volume $(\text{WQCV})$ Design Volume $(\text{d}_6^*(\text{V}_{\text{DESiGN}}/0.43))$	V <sub>DESIGN OTHER</sub> = 0.147 ac-ft		
	f Water Quality Capture Volume (WQCV) Design Volume ferent WQCV Design Volume is desired)	V <sub>DESIGN USER</sub> = ac-ft		
i) Percenta ii) Percenta	ogic Soil Groups of Tributary Watershed ge of Watershed consisting of Type A Soils ge of Watershed consisting of Type B Soils age of Watershed consisting of Type C/D Soils	HSG <sub>A</sub> = 0 % HSG <sub>B</sub> = 100 % HSG <sub>C/D</sub> = 0 %		
For HSG A: For HSG B:	n Runoff Volume (EURV) Design Volume EURV <sub>A</sub> = $1.68 \times i^{1.28}$ EURV <sub>B</sub> = $1.36 \times i^{1.08}$ D: EURV <sub>CID</sub> = $1.20 \times i^{1.08}$	EURV <sub>DESIGN</sub> = 0.455 ac-f t		
K) User Input of	Excess Urban Runoff Volume (EURV) Design Volume ferent EURV Design Volume is desired)	EURV <sub>DESIGN USER</sub> = ac-f t		
	ength to Width Ratio o width ratio of at least 2:1 will improve TSS reduction.)	L:W= 2.0 :1		
Basin Side Slop	es			
A) Basin Maxim (Horizontal d	num Side Slopes listance per unit vertical, 4:1 or flatter preferred)	Z = 4.00 ft / ft		
4. Inlet				
A) Describe me inflow location	ans of providing energy dissipation at concentrated ons:			
5. Forebay				
A) Minimum Fo	rebay Volume = 2% of the WQCV)	V <sub>FMIN</sub> = 0.003 ac-ft		
B) Actual Foreb		V <sub>F</sub> = 0.003 ac-ft		
C) Forebay Dep		D <sub>F</sub> = 18.0 in		
D) Forebay Disc		<u>10.0</u> j		
	ed 100-year Peak Discharge	Q <sub>100</sub> = 22.00 cfs		
	Discharge Design Flow	Q <sub>F</sub> = 0.44 cfs		
E) Forebay Disc		Choose One		
F) Discharge Pi	pe Size (minimum 8-inches)	Calculated D <sub>P</sub> = in		
G) Rectangular	Notch Width	Calculated W <sub>N</sub> = 4.5 in		

**DEVELOPED DRAINAGE MAP** 





N:\217764\REPORTS\FDR Addendum\217764DM.dwg, 5/6/2021 11:24:04 AM, 1:

## PREVIOUS DRAINAGE MAP (BENT GRASS RESIDENTIAL FILING NO. 1)



6385 Corporate Drive, Suite 101

Colorado Springs, Colorado 80919

(V) 1"= N/A JOB NO. 2430.00

CHECKED BY

(719)785-0799 (Fax)



### Innovative Design. Classic Results.

SP149

#### FINAL DRAINAGE REPORT FOR BENT GRASS EAST COMMERCIAL FILING NO. 2

MAY 2014 REVISED JULY 2014

RETURN TO
ENC, INEEPING
LIEPARY

Prepared for:

LAND FIRST, INC.
154 DEL ORO CIRCLE
COLORADO SPRINGS, CO 80919
Contact: Ron Waldthasuen

Prepared by:

CLASSIC CONSULTING ENGINEERS & SURVEYORS, LLC
6385 CORPORATE DRIVE, SUITE 101

COLORADO SPRINGS, CO 80919

(719) 785-0790

defeived version

AUG 2 0 2014 2

Job no. 2177.53



#### FINAL DRAINAGE REPORT FOR BENT GRASS EAST COMMERCIAL FILING NO. 2

#### DRAINAGE REPORT STATEMENT

#### **ENGINEER'S STATEMENT:**

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the Drainage Criteria Manual for the City of Colorado Springs and El Paso County. I accept responsibility for any liability, caused by any negligent acts, errors, or omissions on my part in preparing this report.

Marc A. Whorton Colorado Par 37155

Date

#### **DEVELOPER'S STATEMENT:**

I, the developer, have read and will comply with all of the requirements specified in this drainage report and plan.

Business Name:

Land First, Inc.

Title:

Address:

154 Del Oro Circle

Colorado Springs, CO 80919

EL PASO COUNTY:

Filed in accordance with Section 51.1 of the El Paso Land Development Code, as amended.

For El Paso County Engineer/Director

<u>g-24-14</u> Date

Conditions:

The following calculations are based on the 2014 drainage/bridge fees:

**Bridge Fees** 

\$3,115 x 3.31 Impervious Ac.

**\$ 10,310.65** 

Drainage Fees

\$8,115 x 3.31 Impervious Ac.

\$ 26,860.65

Fee Reduction (50% reasonable const. costs for detention facility)

Detention Pond 2 (Full Spectrum on-site facility)

 $75,000 \times 50\% = 37,500.00$ 

(See FAE for Pond estimate)

**Drainage Fee Total** \$26,860.65 - \$37,500.00

N/A

**Bridge Fee Total** 

**\$10,310.65** 

#### SUMMARY

All detention facilities have been designed to release at or below historic rates. The proposed development will not adversely impact surrounding developments.

PREPARED BY:

Classic Consulting Engineers & Surveyors, LLC

Marc A. Whorton, P.E. Project Manager

mw/217753/Reports/217753FDR.doc

