



## Preliminary Drainage Report

# Trinity Ranch El Paso County, Colorado

Prepared for:

**Terry Street**  
**8576 Via Gwynn Way**  
**Fair Oaks, CA 95528**

Prepared by:

**Kimley-Horn and Associates, Inc.**  
**2 North Nevada Avenue, Suite 900**  
**Colorado Springs, Colorado 80903**  
**(719) 453-0180**  
**Contact: Kevin Kofford, P.E.**

Project #: 096726003

PCD Filing No.: XXXX

SP268

Prepared: July 17, 2026

**Kimley»Horn**

## CERTIFICATION

### **DESIGN ENGINEER'S STATEMENT**

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the County for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparation of this report.

SIGNATURE (Affix Seal): \_\_\_\_\_  
Kevin Kofford, P.E. Date

### **OWNER/DEVELOPER'S STATEMENT**

I, the developer, have read and will comply with all of the requirements specified in this Drainage Report and Plan.

20165 Howle Street LLC  
Name of Developer

\_\_\_\_\_  
Authorized Signature Date

Terence Street  
Printed Name

Managing Partner  
Title

8576 Via Gwynn Way, Fair Oaks, CA 95528  
Address

### **EL PASO COUNTY**

Filed in accordance with the requirements of the Drainage Criteria Manual, Volumes 1 and 2, El Paso County Engineering Criteria Manual and Land Development Code as amended.

\_\_\_\_\_  
Joshua Palmer, P.E. Date  
County Engineer/ ECM Administrator

Conditions:

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## **INTRODUCTION**

### ***PURPOSE AND SCOPE OF STUDY***

The purpose of this Preliminary Drainage Report (PDR) is to document the drainage design in support of the proposed Trinity Ranch Estates subdivision ("the Project") on behalf of 20165 Howle Street LLC. The Project is located within the jurisdictional limits of El Paso County ("the County"). Therefore, the hydrologic and hydraulic design is based on the County's criteria which is described in further detail within the report.

### ***LOCATION***

The Project Site located along HWY 94 and east of Peyton HWY within El Paso County, Colorado on parcel 3400000455. More specifically, the site is a Portion of the Southeast corner of Section 9, Township 14 South, Range 63 West of the 6<sup>th</sup> PM, County of El Paso, State of Colorado. To the north, west, and south of the Project is agricultural and rural residential land zoned RR-5 and to the east is Antelope Park Ranchettes zoned RR-5 and Viewpoint Estates, zoned RR-2.5. A vicinity map has been provided in the **Appendix** of this report.

The Site is currently owned by 20165 Howle Street LLC and will be developed by 20165 Howle Street LLC.

### ***DESCRIPTION OF PROPERTY***

The entire Trinity Ranch Estates Project is approximately 137.9 acres consisting of vacant, undeveloped land with native vegetation and is classified as Agricultural Grazing Land to be subdivided into 35 total lots. Filing No.1 is approximately 56.79 acres, and consists of 17, 2.5 acre lots, proposed roadways and easements designated for stormwater treatment and detention and is located just east of Viewpoint Estates. Filing No. 2 is just north of Filing No. 1 and west of Antelope Park Ranchettes, approximately 51.51 acres, and consists of 18, 2.5 acre lots. The remaining 29.60 acres along HWY 94 is proposed to be rezoned as commercial. Vegetation within the site is characterized primarily by prairie grasses. The Site does not currently provide water quality or detention for the Project area.

The existing topography consists of slopes ranging from 1% to 9%. Flows in the existing conditions run off site into the existing CDOT roadside ditch along HWY 94. Majority of the site collects in the roadside ditch and is conveyed to two existing 30" CMP culverts that carry runoff underneath HWY 94, located to the east of the existing access point. Additionally a portion of the site runs further east and eventually collects into three existing 30" CMP culverts that convey runoff underneath HWY 94, located approximately 0.25-miles east of the SE corner of the Site. Runoff ultimately drains into Black Squirrel Creek.

### ***PROJECT CHARACTERISTICS***

Filing No. 1 development of this site will consist of 17, 2.5-acre residential lots with roadway improvements, roadway grading, two (2) full spectrum detention pond, roadside ditches, culverts, and drainage swales.

Filing No. 2 development of this site will consist of 18, 2.5-acre residential lots with roadway improvements, roadway grading, roadside ditches, culverts, and drainage swales.

The commercial development of this site will consist of 29.60 acres of low impact commercial development with roadway improvements, roadway grading, two full spectrum detention pond, roadside ditches, culverts, and drainage swales.

## **SOILS DATA**

According to NRCS soil mapping data, USCS Type A soils are the primary soil type within the Site. Type A soils described as having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission. Soils mapping information has been provided in the **Appendix**.

## **FLOODPLAIN STATEMENT**

The Site is located outside the 100-year floodplain and within Zone X (an area of minimal flood hazard) as noted on the FEMA FIRM Map No. 08041C0805G revised on December 7, 2018 (See **Appendix**).

## **DRAINAGE BASINS**

### **EXISTING SUB-BASIN DESCRIPTIONS**

Historically, runoff from the Site drains generally from upstream tributary areas toward downstream design points and ultimately contributes to larger off-site drainage systems. Slopes across the Site are variable and support a combination of overland and concentrated drainage patterns. Based on topography and drainage divides, the Site has been delineated into five (5) on-site sub-basins (EX-1 through EX-5) and four (4) off-site sub-basins (OF-1 through OF-4). The off-site basins are located primarily upstream of the Site and contribute flows that enter the on-site drainage system at defined design points.

Under existing conditions, runoff from the sub-basins is conveyed primarily as overland sheet flow in upland areas, transitioning to shallow concentrated flow and localized channelized flow along natural drainage paths. These natural drainage paths collect and convey stormwater through the Site in accordance with historic drainage patterns. The majority of on-site basins exhibit minimal development and low imperviousness, resulting in relatively low runoff rates and limited concentration of flow except near downstream design points.

#### **Sub-Basin EX-1**

Existing sub-basin EX-1 is approximately 16.42 acres and consists of undeveloped land with native vegetation and minimal impervious surfaces. Runoff developed within this basin generally occurs as overland sheet flow toward design point EX-1, with minor localized concentration in lower areas. Runoff from EX-1 flows offsite into vacant agricultural land. The weighted imperviousness of sub-basin EX-1 is 2.0%. The existing direct runoff from sub-basin EX-1 is 2.37 cfs for the 5-year event and 15.90 cfs for the 100-year event.

#### **Sub-Basin EX-2**

Existing sub-basin EX-2 is approximately 15.87 acres and consists of predominantly undeveloped land with low impervious cover. Runoff within this basin is conveyed primarily as overland sheet flow toward design point EX-2, with some shallow concentrated flow paths developing along natural drainage patterns. Runoff from EX-2 currently flows into subbasin EX-4 at design point

EX2. EX-2 ultimately collects at a double 30" RCP culvert that conveys runoff underneath HWY 94. The weighted imperviousness of sub-basin EX-2 is 2.0%. The existing direct runoff from sub-basin EX-2 is 2.36 cfs for the 5-year event and 15.85 cfs for the 100-year event.

#### **Sub-Basin EX-3**

Existing sub-basin EX-3 is approximately 17.35 acres and consists of native vegetation and undeveloped terrain. Runoff developed within this basin generally flows as sheet flow transitioning to shallow concentrated flow near the downstream design point EX-3. Runoff from EX-3 flows offsite into Antelope Park Ranchettes and is ultimately collected into a triple barrel 30" RCP culvert that conveys runoff underneath HWY 94. The weighted imperviousness of sub-basin EX-3 is 2.0%. The existing direct runoff from sub-basin EX-3 is 2.82 cfs for the 5-year event and 18.98 cfs for the 100-year event.

#### **Sub-Basin EX-4**

Existing sub-basin EX-4 is approximately 52.09 acres and represents the largest on-site basin. The basin consists of undeveloped terrain with natural drainage patterns. Runoff is conveyed as sheet flow over the majority of the basin, with increased concentration into shallow swales or natural low points approaching design point EX-4. EX-4 ultimately collects at a double 30" RCP culvert that conveys runoff underneath HWY 94. The weighted imperviousness of sub-basin EX-4 is 2.0%. The existing direct runoff from sub-basin EX-4 is 7.11 cfs for the 5-year event and 47.80 cfs for the 100-year event.

#### **Sub-Basin EX-5**

Existing sub-basin EX-5 is approximately 36.19 acres and consists of undeveloped land with native vegetation. Runoff within this basin generally occurs as overland sheet flow with limited concentrated flow paths, ultimately draining toward design point EX-5. EX-5 flows offsite either into Viewpoint Estates or into the existing roadside ditch along HWY 94. EX-5 ultimately collects into a triple barrel 30" RCP culvert that conveys runoff underneath HWY 94. The weighted imperviousness of sub-basin EX-5 is 2.0%. The existing direct runoff from sub-basin EX-5 is 5.74 cfs for the 5-year event and 38.56 cfs for the 100-year event.

#### **Sub-Basin OF-1**

Existing sub-basin OF-1 is approximately 204.29 acres and consists of a large off-site drainage area contributing flow to the project site. Runoff is conveyed primarily as sheet flow in upstream areas, transitioning to concentrated/channelized flow within natural drainageways approaching design point OF-1. OF-1 flows into EX-1 and follows the drainage patterns detailed in EX-1. The weighted imperviousness of sub-basin OF-1 is 3.72%. The existing direct runoff is 18.45 cfs (5-year) and 112.58 cfs (100-year).

#### **Sub-Basin OF-2**

Existing sub-basin OF-2 is approximately 290.54 acres and represents the largest contributing off-site basin. Runoff within this basin is conveyed as sheet flow over upstream portions, combining into well-defined concentrated flow paths as it approaches design point OF-2. OF-2 flows into EX-3 and follows the drainage patterns detailed in EX-3. The weighted imperviousness is 3.81%. The existing direct runoff is 25.46 cfs (5-year) and 154.64 cfs (100-year).

#### **Sub-Basin OF-3**

Existing sub-basin OF-3 is approximately 18.51 acres and consists of a smaller off-site tributary area. Runoff is primarily conveyed as overland sheet flow with limited concentration, draining toward design point OF-3. OF-3 flows into EX-2 and follows the drainage patterns detailed in

EX-2. The weighted imperviousness is 2.0%. The existing direct runoff is 3.41 cfs (5-year) and 22.92 cfs (100-year).

#### **Sub-Basin OF-4**

Existing sub-basin OF-4 is approximately 0.96 acres and consists of a very small off-site drainage area. Runoff occurs as localized sheet flow with minimal concentration toward design point OF-4. OF-4 flows into EX-4 and follows the drainage patterns detailed in EX-4. The weighted imperviousness is 2.0%. The existing direct runoff is 0.18 cfs (5-year) and 1.24 cfs (100-year).

#### **Sub-Basin OF-5**

Existing sub-basin OF-5 is approximately 6.21 acres and consists of the northern half of HWY 94 and the roadside ditch. Runoff sheet flows off of HWY 94 into the adjacent roadside ditch and is concentrated as it flows towards design point OF-5. As shown in the existing drainage map, design points OF-5 and EX-4 ultimately collect at the double 30" CMP culverts that convey runoff underneath HWY 94. The weighted imperviousness is 30.9%. The existing direct runoff is 3.01 cfs (5-year) and 8.56 cfs (100-year).

#### **Sub-Basin OF-6**

Existing sub-basin OF-6 is approximately 0.14 acres and consists of the off-site Golden Eagle Drive public right-of-way. Existing conditions consist of packed gravel. Runoff sheet flows southeast towards design point OF-6. The weighted imperviousness is 80.0%. The existing direct runoff is 0.34 cfs (5-year) and 0.67 cfs (100-year).

#### **Sub-Basin OP-1**

Existing sub-basin OP-1 is approximately 0.04 acres and consists of a very small off-site drainage area that includes the area that has been utilized to access the Site via HWY 94. Runoff occurs as localized sheet flow with minimal concentration toward design point OP-1. OP-1 flows into OF-5 and ultimately collects at design point OF-5. The weighted imperviousness is 41.0%. The existing direct runoff is 0.07 cfs (5-year) and 0.18 cfs (100-year).

### ***PROPOSED SUB-BASIN DESCRIPTIONS***

Under proposed conditions, stormwater runoff from the Site will generally maintain historic drainage patterns, with localized modifications resulting from the proposed development. Impervious percentages and runoff coefficients from the DCM for large lot residential and low impact commercial were utilized to calculate the 100-year detention volume. It should be noted that a blanket 65% imperviousness percentage was utilized for the proposed commercial area in all drainage calculations. The construction of roadways and associated grading will alter some existing flow paths; however, drainage infrastructure has been designed to convey runoff back to its historic flow regime or provide controlled discharge through proposed facilities. The Site has been delineated into multiple on-site sub-basins (PR-1 through PR-9) and off-site contributing basins (OF-1 through OF-4 and OP-1). The off-site basins represent upstream tributary areas that are not altered by the proposed development. No changes to upstream drainage patterns or hydrologic response are anticipated from these off-site areas, and they will continue to contribute flow to the Site consistent with existing conditions.

There are several drainage culverts proposed within the Site. Locations of the proposed culverts were chosen to ensure historic drainage patterns are maintained. Culvert sizing and the outlet protection analysis is included in this report. Outlet protection will be installed with the culverts as part of the early grading portion of this development. The detail is provided in the **Appendix** of

Typical comment: Verify if you are following Table 3-1. Typical Values of Percent Impervious of the ECM. The overall percentage is not necessary, You should document the impervious percentage on the lot itself.

Typical comment (please perform a global search and replace "historic rates" where possible with "pre-development rates").

this report.

The two proposed full spectrum extended detention basin (EDB) will be designed to release developed flows from the Site at less than or equal to historic rates prior to releasing to the existing roadside ditch along HWY 94. The full design of these full spectrum extended detention basins are provided will be provided in the Final Drainage Report. A low tailwater stilling basin, based on the design provided by Mile High Flood District (MHFD) Urban Drainage and Flood Control District Drainage Criteria Manuals (UDFCDCM) Volume 2, Figure 9-37, will be installed at the inlet locations of the proposed EDB. The design helps prevent scour and mitigates the concentrated flow, acting as a level spreader for concentrated flow in an existing drainageway. This is displayed and discussed in text and drainage maps. More detail regarding the proposed EDBs can be found in the detention basin section of this report.

I don't think this figure still part of the manual, please verify and provide the detail if you think otherwise.

#### Sub-Basin PR-1

Proposed sub-basin PR-1 is approximately 1.0 acre. Runoff occurs as sheet flow across developed areas, transitioning to concentrated flow toward design point PR-1. PR-1 ultimate flows offsite into undeveloped agricultural land. The proposed roadway within this sub-basin is part of the 1-acre disturb area exclusion detailed later in this report. The weighted imperviousness is 8.12%. The developed runoff is 4.05 cfs (5-year) and 21.02 cfs (100-year). Refer to the Appendix for the Proposed Conditions Drainage Map.

#### Sub-Basin PR-2

Proposed sub-basin PR-2 is approximately 9.55 acres. Proposed development in PR-2 consists of low density 2.5 acre lots, roadway, and roadside ditch. Runoff is conveyed as sheet flow from developed surfaces toward design point PR-2. Runoff is collected in the proposed 30" RCP culvert and conveyed into PR-4. The weighted imperviousness is 9.90%. The developed runoff is 2.98 cfs (5-year) and 14.38 cfs (100-year). Refer to the **Appendix** for the Proposed Conditions Drainage Map.

#### Sub-Basin PR-3

Proposed sub-basin PR-3 is approximately 17.72 acres. Runoff is conveyed as sheet flow transitioning to concentrated flow, ultimately routed to downstream conveyance features at design point PR-3. Runoff from PR-3 flows offsite into Antelope Park Ranchettes and is ultimately collected into a triple barrel 30" RCP culvert that conveys runoff underneath HWY 94. The proposed roadway disturbance in this subbasin is part of the 1-acre disturbance exclusion detailed later in this report. The weighted imperviousness is 8.90%. The developed runoff is 4.98 cfs (5-year) and 24.98 cfs (100-year). Refer to the **Appendix** for the Proposed Conditions Drainage Map.

#### Sub-Basin PR-4

Proposed sub-basin PR-4 is approximately 16.42 acres. Runoff occurs as sheet flow over developed surfaces, concentrating into defined conveyance paths or roadside ditch toward design point PR-4. Runoff is collected into the roadside ditch and conveyed towards double 30" RCP culverts and outfalls into PR-8. Runoff from PR-2 is confined to the roadside ditch as it is conveyed towards design point PR-4. The weighted imperviousness is 11.48%. The developed runoff is 5.99 cfs (5-year) and 27.20 cfs (100-yr). Refer to the **Appendix** for the Proposed Conditions Drainage Map.

#### Sub-Basin PR-5

Proposed sub-basin PR-5 is approximately 2.08 acres. Proposed development consists of low density 2.5 acre lots and roadway, runoff is quickly concentrated and routed through localized roadside ditch toward design point PR-5. Runoff is ultimately collected into a 24" RCP culvert and

outfalling into the roadside ditch in subbasin PR-8. The weighted imperviousness is 36.59%. The developed runoff is 2.00 cfs (5-year) and 5.39 cfs (100-year). Refer to the **Appendix** for the Proposed Conditions Drainage Map.

#### **Sub-Basin PR-6**

Proposed sub-basin PR-6 is approximately 17.78 acres. Proposed development consists of low density 2.5 acre lots and roadway. Runoff occurs as sheet flow transitioning to shallow concentrated flow with the proposed roadside ditch toward design point PR-6. Runoff is ultimately collected into a 16" RCP culvert and outfalls into subbasin PR-9. The weighted imperviousness is 10.34%. The developed runoff is 5.49 cfs (5-year) and 25.99 cfs (100-year). Refer to the **Appendix** for the Proposed Conditions Drainage Map.

#### **Sub-Basin PR-7**

Proposed sub-basin PR-7 is approximately 29.21 acres. Proposed development consists of low density 2.5 acre lots, low impact commercial area, and roadway. In the full development of this basin there will be rapidly concentrated runoff that flows toward design point PR-7. Runoff is ultimately collected into double 30" RCP culverts and outfall into the proposed EDB in PR-8. The weighted imperviousness is 42.16%. The developed runoff is 25.51 cfs (5-year) and 68.20 cfs (100-year). Refer to the **Appendix** for the Proposed Conditions Drainage Map.

#### **Sub-Basin PR-8**

Proposed sub-basin PR-8 is approximately 11.31 acres. Proposed development consists of low density 2.5 acre lots, low impact commercial area, roadway, and a full spectrum detention basin. Runoff is conveyed as concentrated flow due to high impervious cover, flowing efficiently toward design point PR-8. Runoff from subbasins OF-3, OF-4, PR-2, PR-4, PR-5, PR-7, and PR-8 ultimately collect into the proposed EDB. The total cumulative flow that collects into the EDB in the 100-yr event is 155.00 cfs. Runoff will be released at less than historic flows and outfall into the existing roadside ditch along HWY 94. Runoff is ultimately routed to the existing double 30" RCP culverts that convey flows underneath HWY 94. The weighted imperviousness is 47.62%. The developed runoff is 11.76 cfs (5-year) and 29.60 cfs (100-year). Refer to the **Appendix** for the Proposed Conditions Drainage Map.

#### **Sub-Basin PR-9**

Proposed sub-basin PR-9 is approximately 17.68 acres. Proposed development consists of low density 2.5 acre lots, low impact commercial area, roadway, and a full spectrum detention basin. Runoff is conveyed as concentrated flow due to high impervious cover, flowing efficiently toward design point PR-9. Runoff from subbasins PR-6 and PR-9 ultimately collect into the proposed EDB. The total cumulative flow that collects into the EDB in the 100-yr event is 61.78 cfs. Runoff will be released at less than historic flows and outfall into the existing roadside ditch along HWY 94. Runoff is ultimately routed to the existing triple 30" RCP culverts that convey flows underneath HWY 94. The weighted imperviousness is 40.68%. The developed runoff is 14.37 cfs (5-year) and 38.97 cfs (100-year). Refer to the **Appendix** for the Proposed Conditions Drainage Map.

#### **Sub-Basin OF-1**

Existing sub-basin OF-1 is approximately 204.29 acres and consists of a large off-site drainage area contributing flow to the project site. Runoff is conveyed primarily as sheet flow in upstream areas, transitioning to concentrated/channelized flow within natural drainageways approaching design point OF-1. OF-1 flows into PR-1 and follows the drainage patterns detailed in PR-1. The weighted imperviousness of sub-basin OF-1 is 3.72%. The existing direct runoff is 18.45 cfs (5-year) and 112.58 cfs (100-year).

#### **Sub-Basin OF-2**

Existing sub-basin OF-2 is approximately 290.54 acres and represents the largest contributing off-site basin. Runoff within this basin is conveyed as sheet flow over upstream portions, combining into well-defined concentrated flow paths as it approaches design point OF-2. OF-2 flows into PR-3 and follows the drainage patterns detailed in PR-3. The weighted imperviousness is 3.81%. The existing direct runoff is 25.46 cfs (5-year) and 154.64 cfs (100-year).

#### **Sub-Basin OF-3**

Existing sub-basin OF-3 is approximately 18.51 acres and consists of a smaller off-site tributary area. Runoff is primarily conveyed as overland sheet flow with limited concentration, draining toward design point OF-3. OF-3 flows into PR-2 and follows the drainage patterns detailed in PR-2. The weighted imperviousness is 2.0%. The existing direct runoff is 3.41 cfs (5-year) and 22.92 cfs (100-year).

#### **Sub-Basin OF-4**

Existing sub-basin OF-4 is approximately 0.96 acres and consists of a very small off-site drainage area. Runoff occurs as localized sheet flow with minimal concentration toward design point OF-4. OF-4 flows into PR-7 and follows the drainage patterns detailed in PR-7. The weighted imperviousness is 2.0%. The existing direct runoff is 0.18 cfs (5-year) and 1.24 cfs (100-year).

#### **Sub-Basin OF-5**

Existing sub-basin OF-5 is approximately 6.21 acres and consists of the northern half of HWY 94 and the roadside ditch. Runoff sheet flows off of HWY 94 into the adjacent roadside ditch and is concentrated as it flows towards design point OF-5. As shown in the proposed drainage map, design point OF-5 collects at the 18" RCP culvert that conveys flows underneath the Site access point and ultimately discharges at the double 30" CMP culverts that convey runoff underneath HWY 94. The weighted imperviousness is 30.9%. The existing direct runoff is 3.01 cfs (5-year) and 8.56 cfs (100-year).

#### **Sub-Basin OF-6**

Proposed sub-basin OF-6 is approximately 0.14 acres and consists of the off-site Golden Eagle Drive public right-of-way. Proposed conditions consist of proposed asphalt road and gravel shoulder. Runoff sheet flows southeast towards design point OF6. This entire basin is part of the proposed disturbed area exclusion. The weighted imperviousness is 84.9%. The proposed direct runoff is 0.42 cfs (5-year) and 0.81 cfs (100-year).

#### **Sub-Basin OP-1**

Proposed sub-basin OP-1 is approximately 0.04 acres and consists of a very small off-site drainage area that includes the area that is utilized to access the Site via HWY 94. Runoff occurs as localized sheet flow with minimal concentration toward design point OP-1. OP-1 flows into OF-5 and collects into the proposed 18" RCP culvert that conveys water underneath the proposed access point and ultimately discharges into the existing double 30" CMP culverts underneath HWY 94.. The weighted imperviousness is 46.0%. The existing direct runoff is 0.08 cfs (5-year) and 0.20 cfs (100-year).

#### Hwy 94 – Double 30” CMP Culverts

| Contributing Basins               | Controlling Structure                  | Existing 100-yr Flow (CFS) | Proposed 100-yr Flow (cfs) |
|-----------------------------------|----------------------------------------|----------------------------|----------------------------|
| OF3, OF4, PR2, PR4, PR5, PR7, PR8 | Full Spectrum Detention Pond           | 127.17                     | 29.6                       |
| OF5, OP1                          | 18” RCP Culvert with riprap protection | 8.74                       | 8.76                       |

Flows shown in the “Proposed 100-yr Flow (cfs)” are not final. Final flows to be determined in the Final Drainage report and will maintain flows to be less than historic.

#### DRAINAGE DESIGN

#### DEVELOPMENT C

Please provide a table that provides and compares the 5 - year and the 100 year for the pre-development and post-development flows for the project site and discuss the reductions or increases in flows to come to the conclusion that the post-development flows are lower than the pre-development flows.

The proposed storm facilities are designed to be in compliance with El Paso County “Drainage Criteria Manual (DCM)” dated October 2018 (“the MANUAL”), El Paso County “Engineering Criteria Manual” (“the Engineering Manual”), Chapter 6 and Section 3.2.1 of Chapter 13 of the City of Colorado Springs Drainage Criteria Manual dated May 2014 (“the Colorado Springs MANUAL”), and Mile High Flood District (MHFD), Urban Drainage and Flood Control District Drainage Criteria Manuals (UDFCDCM), (Volumes 1, 2 and 3), prepared by Wright-McLaughlin Engineers, June 2001, with latest revisions.

Site drainage is not significantly impacted by such constraints as utilities or existing development.

#### HYDROLOGIC CRITERIA

The 5-year and 100-year design storm events were used in determining rainfall and runoff for the proposed drainage system per chapter 6 of the CRITERIA. Table 6-2 of the CRITERIA is the source for rainfall data for the 5-year and 100-year design storm events. Design runoff was calculated using the Rational Method for developed conditions as established in the CRITERIA and MANUAL. Runoff coefficients for the proposed development were determined using Table 6-6 of the CRITERIA by calculating weighted impervious values for each specific site basin as outlined and shown in the Preliminary Drainage Report.

#### HYDRAULIC CRITERIA

Applicable design methods were utilized to analyze & size the proposed ponds, culverts, and existing drainage channels which includes the use of the UD-Detention spreadsheet, rational calculations spreadsheet, and FlowMaster, and UD-Culvert.

Proposed Drainage features on-site have been analyzed and sized for the following design storm events:

- Major Storm: 100-year Storm Event

The proposed drainage channels and proposed roadside ditches are designed to carry flows to the proposed EDB and water quality pond. Channel calculations and summary table have been provided in the **Appendix**. Proposed drainage easements have been proposed in locations where flow is being conveyed between properties.

Roadside ditches are provided along the proposed roadways to route flows to the proposed culverts. The roadside ditches are sized to convey the major event flow. The proposed roadside ditches comply with Table 6-1 of the EPC DCM V1. The roadside ditches have been designed to have an average depth of 3 feet, a v-ditch, and side slopes of 4:1. Roadside ditch calculations and summary table has been provided in the **Appendix**.

Culverts were sized to convey flows from the ditches and channels, underneath the sites paved roads. The proposed culverts range from 18" to 30" and have been designed to convey the 100-year storm event. Culvert calculations and summary table has been provided in the **Appendix**.

Calcs show the 25 yr passing through the spillway

### DETENTION

One full spectrum extended detention basin designed to detain the 100-year storm event and one basin designed to detain the 50-year storm but control release the 100-year storm event is proposed in order to maintain historic flows and water quality. Mile High Flood District UD-Detention Spreadsheet was utilized to design the pond outlet structures. The two basins are to be owned and maintained by the HOA. As most of the site is exempt from water quality per the large lot single family exclusion, the WQCV numbers provided represent the required volume to be treated from the proposed roadway improvements. The overridden WQCV value was determined using UD-Detention spreadsheets calculating from only the roadway improvements. The UD-Detention spreadsheets used to calculate WQCV have been included in the **Appendix**. Detailed information regarding the large lot single family exclusions and WQCV can be found in Step 2 of the Four-Step Process section below.

Detention must be provided for the 100-year storm event.

Detailed pond and outlet structure design can be found below. A pond summary table

| Pond | Contributing Basins               | Total Contributing Basin Area (Acre) | WQCV (Ac-ft) | Total Volume Required (Ac-ft) | Total Volume Provided (Ac-ft) | 100-YR Pond Outfall (CFS) |
|------|-----------------------------------|--------------------------------------|--------------|-------------------------------|-------------------------------|---------------------------|
| A    | OF3, OF4, PR2, PR4, PR5, PR7, PR8 | 88.04                                | 0.600        | 4.128                         | 4.405                         | 29.60                     |
| B    | PR6 & PR9                         | 38.38                                | 0.238        | 1.36                          | 1.387                         | 9.9                       |

### THE FOUR STEP PROCESS

The Project was designed in accordance with the four-step process to minimize adverse impacts of urbanization, as outlined in the El Paso County Engineering Manual for BMP selection as noted below:

**Step 1. Employ Runoff Reduction Practices** – The Project is proposing a low-density residential development that will be designed to minimize the impact to the current existing terrain. Per Section I.7.1B of Appendix I of the ECM, the single-family residences fall under the large lot exemption as the total impervious area is less than 10% of the area. Homes are typically placed in the center of the lot and provide long distances for infiltration across natural terrain. The Site's proposed paved roadways will increase the Site's impervious area; however, roadside ditches and channels will be constructed to slow down the runoff

Pond calcs use pcm identifiers pond 1/2, please revise for consistent naming throughout documents

velocity and reduce runoff peaks. The two proposed detention ponds will be used to capture stormwater, provide water quality treatment, and maintain flows discharging off site at or below historic levels.

I.6.B.5 now with  
appendix I update

**Step 2. Provide a Water Quality Capture Volume** – Permanent water quality measures and detention facilities will be necessary for the Project. Two (2) Full Spectrum Extended Detention Basins will treat the areas not excluded with either the Large Lot or 20% exclusion. Per ECM Appendix I Section 1.7.B.5: Large Lot Single Family exclusion, most of the proposed site will be excluded from water quality, lot imperviousness shall be limited to 10 percent or less. Per ECM Appendix I Section 1.7.C.1.a., 20% of the development site or less than 1 acre can be excluded from providing water quality. As mentioned, 0.94 acres (40886 sq ft) of impervious area will not be able to be treated which is less than 20% of the overall site.

Appendix I.6.3.A.1.a

**Step 3 Stabilize Drainageways**– Stabilizing proposed roadside ditches, and channels by designing them with slopes that control the flow rates. Placement of riprap upstream and downstream of culverts to help reduce erosion of the roadside ditches. Additionally, low tailwater stilling basins will be constructed in the place of traditional riprap outlet protection. The design helps prevent downstream scour and mitigates the concentrated flow, acting as a level spreader for concentrated flow in an existing drainageway.

**Step 4. Implement Site Specific and Other Source Control BMPs** – The erosion control construction BMPs of the Project were designed to reduce contamination. Source control BMPs include the use of vehicle tracking control, culvert protection, stockpile management, and stabilized staging areas.

## DRAINAGE FACILITY DESIGN

### GENERAL CONCEPT

The proposed drainage patterns will match the h full spectrum detention ponds are being proposed proposed development at less than or equal to historic rates.

The project is in the TELEPHONE EXCHANGE basin and the Basin Fee and the Bridge Fee are applicable; the Basin fee is \$15,323 and the Bridge fee is \$359 per impervious area.

### WQCV EXCLUSION AREAS

Areas within the site do not have water quality provided. Under the ECM's Appendix I. Section 1.7.C.A, 20% of the development site or less than 1 acre can be excluded from providing water quality. The combined exclusion areas for the Site sum to 0.96 acres (41,891 SQ FT). WQCV exclusion locations are provided in the **Appendix**.

## DRAINAGE FEES

### FEES

The Project is within the Ellicott Consolidated Drainage Basin (CHBS1200). As such, no drainage fees are due with this Project.

## SUMMARY

This report has been prepared in accordance with El Paso County stormwater criteria. It outlines the Site design for the 5-year and 100-year storm events drainage system. The drainage design presented within this report conforms to the criteria presented in the MANUAL. Additionally, as the proposed detention ponds release rates are to be designed less than historic rates, the Site

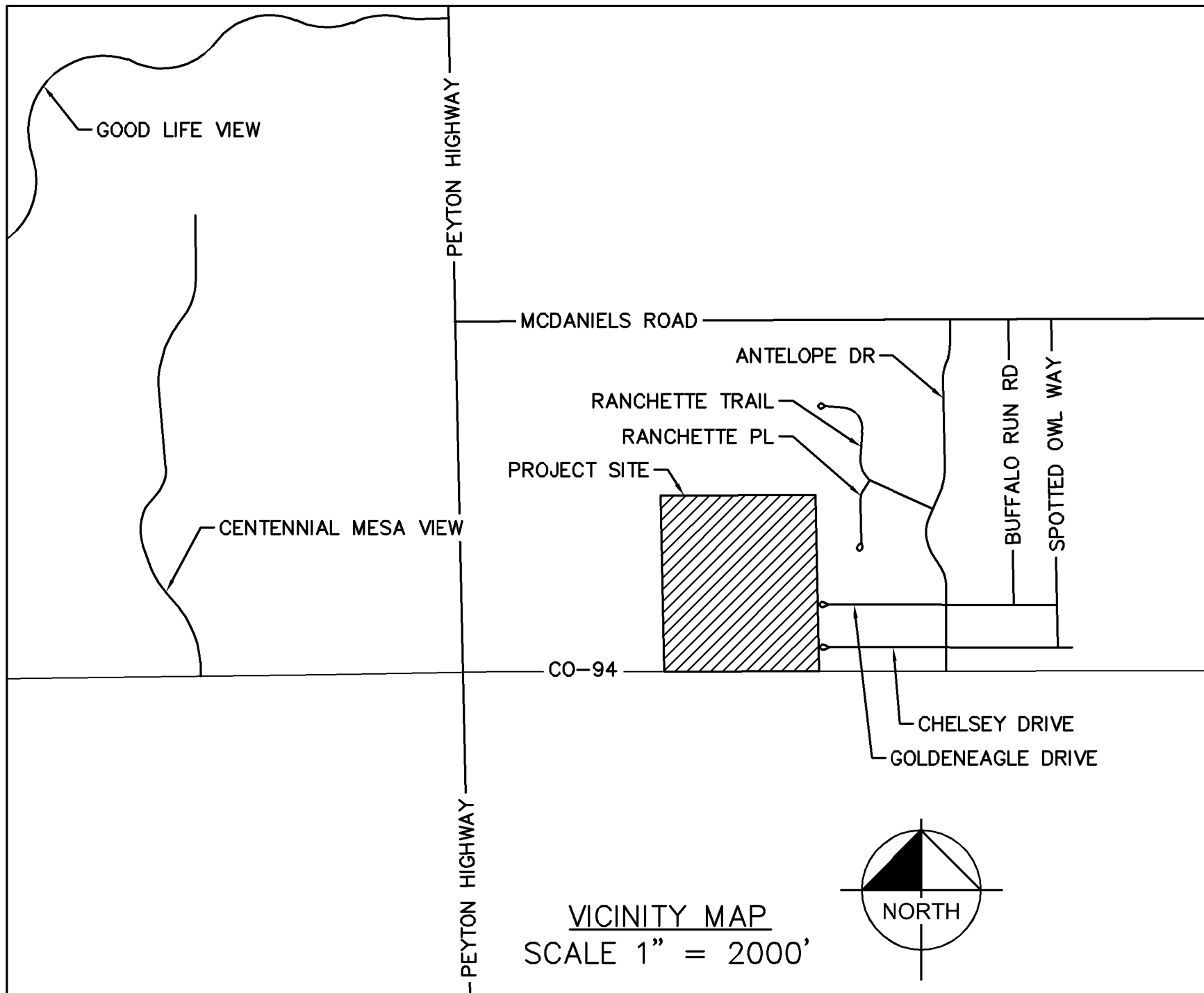
runoff and storm drain facilities will not adversely affect the downstream and surrounding developments.

## REFERENCES

1. El Paso County "Engineering Criteria Manual" Volumes 1 & 2, dated October 31, 2018
2. Natural Resources Conservation Service, Web Soil Survey, dated June 21, 2023.
3. Urban Drainage and Flood Control District Drainage Criteria Manuals (UDFCDCM), (Volumes 1, 2 and 3), prepared by Wright-McLaughlin Engineers, June 2001, with latest revisions.
4. Flood Insurance Rate Map, El Paso County, Colorado and Incorporated Areas, Map Number 08041C0805G, Effective Date December 7, 2018, prepared by the Federal Emergency Management Agency (FEMA).
5. Soils and Geology Study Trinity Ranch Estates – Filing No.1 by Entech Engineering, Inc., dated December 7, 2021.

## APPENDIX

***APPENDIX A: VICINITY MAP***



***APPENDIX B: FEMA MAP & SOILS REPORT***

**NOTES TO USERS**

This map is for use in administering the National Flood Insurance Program. It does not necessarily identify all areas subject to flooding, particularly from local drainage sources of small size. The **community map repository** should be consulted for possible updated or additional flood hazard information.

To obtain more detailed information in areas where **Base Flood Elevations (BFEs)** and/or **floodways** have been determined, users are encouraged to consult the Flood Profiles and Floodway Data and/or Summary of Stillwater Elevations tables contained within the Flood Insurance Study (FIS) report that accompanies this FIRM. Users should be aware that BFEs shown on the FIRM represent rounded whole-foot elevations. These BFEs are intended for flood insurance rating purposes only and should not be used as the sole source of flood elevation information. Accordingly, flood elevation data presented in the FIS report should be utilized in conjunction with the FIRM for purposes of construction and/or floodplain management.

**Coastal Base Flood Elevations** shown on this map apply only landward of 0.0' North American Vertical Datum of 1988 (NAVD88). Users of this FIRM should be aware that coastal flood elevations are also provided in the Summary of Stillwater Elevations table in the Flood Insurance Study report for this jurisdiction. Elevations shown in the Summary of Stillwater Elevations table should be used for construction and/or floodplain management purposes when they are higher than the elevations shown on this FIRM.

Boundaries of the **floodways** were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations with regard to requirements of the National Flood Insurance Program. Floodway widths and other pertinent floodway data are provided in the Flood Insurance Study report for this jurisdiction.

Certain areas not in Special Flood Hazard Areas may be protected by **flood control structures**. Refer to section 2.4 "Flood Protection Measures" of the Flood Insurance Study report for information on flood control structures for this jurisdiction.

The **projection** used in the preparation of this map was Universal Transverse Mercator (UTM) zone 13. The **horizontal datum** was NAD83, GRS80 spheroid. Differences in datum, spheroid, projection or UTM zones zones used in the production of FIRMs for adjacent jurisdictions may result in slight positional differences in map features across jurisdiction boundaries. These differences do not affect the accuracy of this FIRM.

Flood elevations on this map are referenced to the **North American Vertical Datum of 1988 (NAVD88)**. These flood elevations must be compared to structure and ground elevations referenced to the same **vertical datum**. For information regarding conversion between the National Geodetic Vertical Datum of 1929 and the North American Vertical Datum of 1988, visit the National Geodetic Survey website at <http://www.ngs.noaa.gov/> or contact the National Geodetic Survey at the following address:

NGS Information Services  
NOAA, NIMS12  
National Geodetic Survey  
SSMC-3, #9202  
1315 East-West Highway  
Silver Spring, MD 20910-3282

To obtain current elevation, description, and/or location information for **bench marks** shown on this map, please contact the Information Services Branch of the National Geodetic Survey at (301) 713-3242 or visit its website at <http://www.ngs.noaa.gov/>.

**Base Map** information shown on this FIRM was provided in digital format by El Paso County, Colorado Springs Utilities, and Anderson Consulting Engineers, Inc. These data are current as of 2008.

This map reflects more detailed and up-to-date **stream channel configurations and floodplain delineations** than those shown on the previous FIRM for this jurisdiction. The floodplains and floodways that were transferred from the previous FIRM may have been adjusted to conform to these new stream channel configurations. As a result, the Flood Profiles and Floodway Data tables in the Flood Insurance Study Report (which contains authoritative hydraulic data) may reflect stream channel distances that differ from what is shown on this map. The profile baselines depicted on this map represent the hydraulic modeling baselines that match the flood profiles and Floodway Data Tables if applicable, in the FIS report. As a result, the profile baselines may deviate significantly from the new base map channel representation and may appear outside of the floodplain.

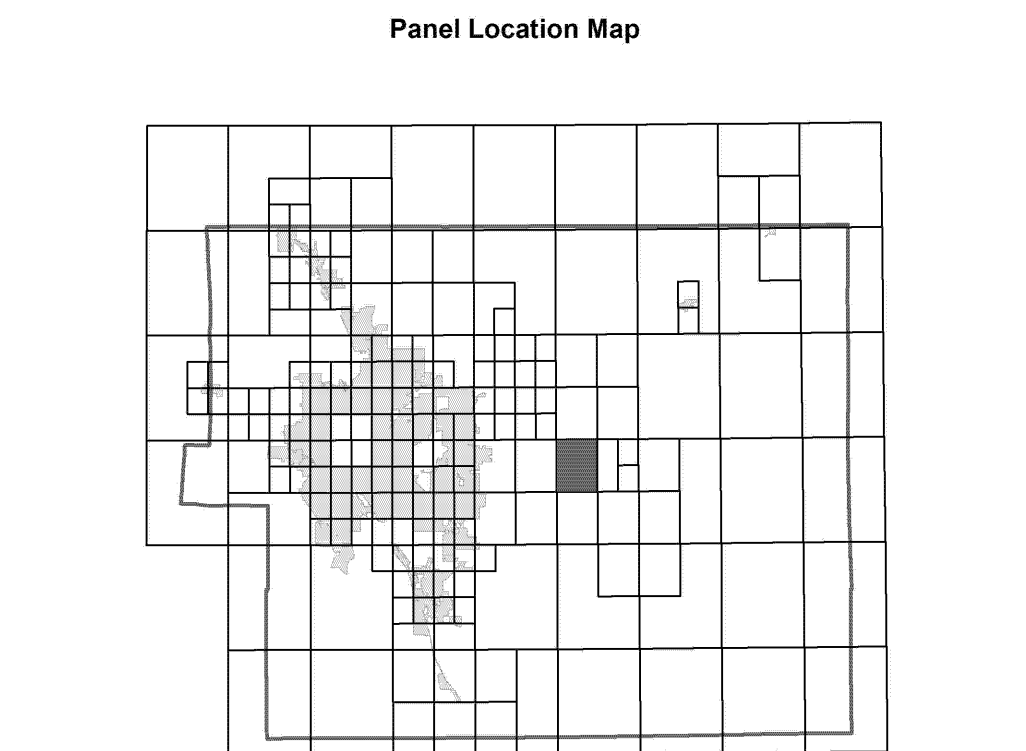
**Corporate limits** shown on this map are based on the best data available at the time of publication. Because changes due to annexations or de-annexations may have occurred after this map was published, map users should contact appropriate community officials to verify current corporate limit locations.

Please refer to the separately printed **Map Index** for an overview map of the county showing the layout of map panels; community map repository addresses; and a Listing of Communities table containing National Flood Insurance Program dates for each community as well as a listing of the panels on which each community is located.

Contact **FEMA Map Service Center (MSC)** via the FEMA Map Information eXchange (FIMX) 1-877-336-2627 for information on available products associated with this FIRM. Available products may include previously issued Letters of Map Change, a Flood Insurance Study Report, and/or digital versions of this map. The MSC may also be reached by Fax at 1-800-358-9620 and its website at <http://www.msc.fema.gov/>.

If you have **questions about this map** or questions concerning the National Flood Insurance Program in general, please call **1-877-FEMA MAP** (1-877-336-2627) or visit the FEMA website at <http://www.fema.gov/business/nfip>.

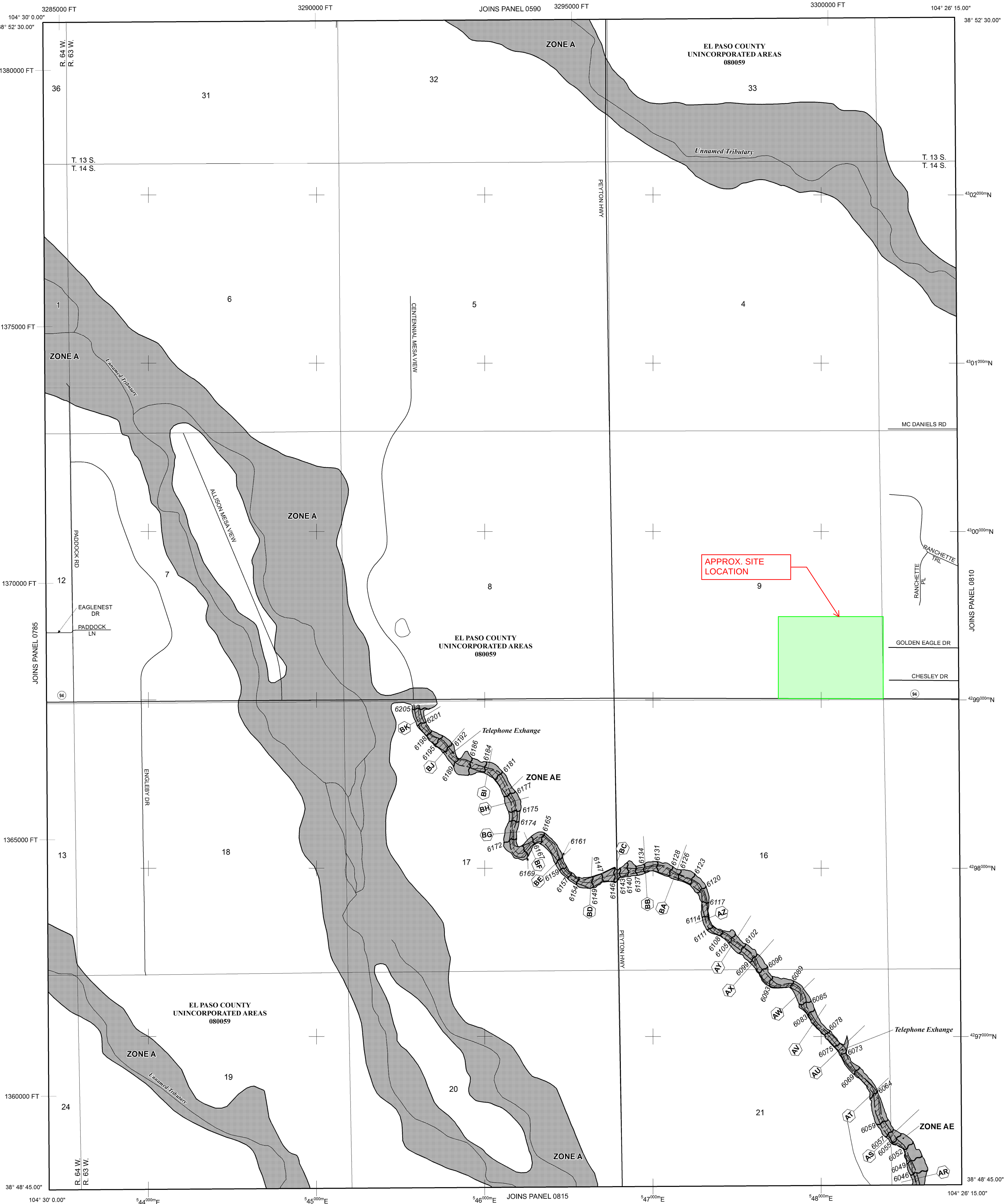
| El Paso County Vertical Datum Offset Table                                                                                  |                            |
|-----------------------------------------------------------------------------------------------------------------------------|----------------------------|
| Flooding Source                                                                                                             | Vertical Datum Offset (ft) |
| REFER TO SECTION 3.3 OF THE EL PASO COUNTY FLOOD INSURANCE STUDY FOR STREAM BY STREAM VERTICAL DATUM CONVERSION INFORMATION |                            |



This Digital Flood Insurance Rate Map (DFIRM) was produced through a Cooperating Technical Partner (CTP) agreement between the State of Colorado Water Conservation Board (CWCB) and the Federal Emergency Management Agency (FEMA).



Additional Flood Hazard information and resources are available from local communities and the Colorado Water Conservation Board.



**LEGEND**

**SPECIAL FLOOD HAZARD AREAS (SFHAS) SUBJECT TO INUNDATION BY THE 1% ANNUAL CHANCE FLOOD**

The 1% annual chance flood (100-year flood), also known as the base flood, is the flood that has a 1% chance of being equalled or exceeded in any given year. The Special Flood Hazard Area is the area subject to flooding by the 1% annual chance flood. Areas of Special Flood Hazard include Zones A, AE, AH, AO, AR, A99, V, and VE. The Base Flood Elevation is the water-surface elevation of the 1% annual chance flood.

**ZONE A** No Base Flood Elevations determined.  
**ZONE AE** Base Flood Elevations determined.  
**ZONE AH** Flood depths of 1 to 3 feet (usually areas of ponding); Base Flood Elevations determined.  
**ZONE AO** Flood depths of 1 to 3 feet (usually sheet flow on sloping terrain); average depths determined. For areas of alluvial fan flooding, velocities also determined.  
**ZONE AR** Special Flood Hazard Area Formerly protected from the 1% annual chance flood by a flood control system that was subsequently decertified. Zone AR indicates that the former flood control system is being restored to provide protection from the 1% annual chance or greater flood.  
**ZONE A99** Area to be protected from 1% annual chance flood by a Federal flood protection system under construction; no Base Flood Elevations determined.  
**ZONE V** Coastal flood zone with velocity hazard (wave action); no Base Flood Elevations determined.  
**ZONE VE** Coastal flood zone with velocity hazard (wave action); Base Flood Elevations determined.

**FLOODWAY AREAS IN ZONE AE**

The floodway is the channel of a stream plus any adjacent floodplain areas that must be kept free of encroachment so that the 1% annual chance flood can be carried without substantial increases in flood heights.

**OTHER FLOOD AREAS**

**ZONE X** Areas of 0.2% annual chance flood; areas of 1% annual chance flood with average depths of less than 1 foot or with drainage areas less than 1 square mile; and areas protected by levees from 1% annual chance flood.

**OTHER AREAS**

**ZONE X** Areas determined to be outside the 0.2% annual chance floodplain.  
**ZONE D** Areas in which flood hazards are undetermined, but possible.

**COASTAL BARRIER RESOURCES SYSTEM (CBRS) AREAS**

**OTHERWISE PROTECTED AREAS (OPAs)**

CBRS areas and OPAs are normally located within or adjacent to Special Flood Hazard Areas.

**Legend Symbols:**

- Floodplain boundary
- Floodway boundary
- Zone D Boundary
- CBRS and OPA boundary
- Boundary dividing Special Flood Hazard Areas of different Base Flood Elevations, flood depths or flood velocities.
- Base Flood Elevation line and value; elevation in feet\* (EL 987)
- Base Flood Elevation value where uniform within zone; elevation in feet\*

\* Referenced to the North American Vertical Datum of 1988 (NAVD 88)

**Legend Symbols:**

- Cross section line
- Transect line
- Geographic coordinates referenced to the North American Datum of 1983 (NAD 83)
- 1000-meter Universal Transverse Mercator grid ticks, zone 13
- 5000-foot grid ticks: Colorado State Plane coordinate system, central zone (FIPSZONE 0502), Lambert Conformal Conic Projection
- Bench mark (see explanation in Notes to Users section of this FIRM panel)
- River Mile

**MAP REPOSITORIES**

Refer to Map Repositories list on Map Index

**EFFECTIVE DATE OF COUNTYWIDE FLOOD INSURANCE RATE MAP**

**MARCH 17, 1997**

**EFFECTIVE DATE(S) OF REVISION(S) TO THIS PANEL**

**DECEMBER 7, 2018** - to update corporate limits, to change Base Flood Elevations and Special Flood Hazard Areas, to update map format, to add roads and road names, and to incorporate previously issued Letters of Map Revision.

For community map revision history prior to countywide mapping, refer to the Community Map History Table located in the Flood Insurance Study report for this jurisdiction.

To determine if flood insurance is available in this community, contact your insurance agent or call the National Flood Insurance Program at 1-800-638-6620.

**MAP SCALE 1" = 1000'**

**500 0 1000 2000 FEET**

**300 0 300 600 METERS**

**NFIP**

**PANEL 0805G**

**FIRM**

**FLOOD INSURANCE RATE MAP**

**EL PASO COUNTY, COLORADO AND INCORPORATED AREAS**

**PANEL 805 OF 1300**

(SEE MAP INDEX FOR FIRM PANEL LAYOUT)

**CONTAINS:**

| COMMUNITY      | NUMBER | PANEL | SUFFIX |
|----------------|--------|-------|--------|
| EL PASO COUNTY | 0805G  | 0805  | G      |

Notice to User: The Map Number shown below should be used when placing map orders. The Community Number shown above should be used on insurance applications for the subject community.

**MAP NUMBER**

**08041C0805G**

**MAP REVISED**

**DECEMBER 7, 2018**

**Federal Emergency Management Agency**



United States  
Department of  
Agriculture

**NRCS**

Natural  
Resources  
Conservation  
Service

A product of the National  
Cooperative Soil Survey,  
a joint effort of the United  
States Department of  
Agriculture and other  
Federal agencies, State  
agencies including the  
Agricultural Experiment  
Stations, and local  
participants

# Custom Soil Resource Report for **El Paso County Area, Colorado**



# Preface

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Soil surveys contain information that affects land use planning in survey areas. They highlight soil limitations that affect various land uses and provide information about the properties of the soils in the survey areas. Soil surveys are designed for many different users, including farmers, ranchers, foresters, agronomists, urban planners, community officials, engineers, developers, builders, and home buyers. Also, conservationists, teachers, students, and specialists in recreation, waste disposal, and pollution control can use the surveys to help them understand, protect, or enhance the environment.

Various land use regulations of Federal, State, and local governments may impose special restrictions on land use or land treatment. Soil surveys identify soil properties that are used in making various land use or land treatment decisions. The information is intended to help the land users identify and reduce the effects of soil limitations on various land uses. The landowner or user is responsible for identifying and complying with existing laws and regulations.

Although soil survey information can be used for general farm, local, and wider area planning, onsite investigation is needed to supplement this information in some cases. Examples include soil quality assessments (<http://www.nrcs.usda.gov/wps/portal/nrcs/main/soils/health/>) and certain conservation and engineering applications. For more detailed information, contact your local USDA Service Center (<https://offices.sc.egov.usda.gov/locator/app?agency=nrcs>) or your NRCS State Soil Scientist ([http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/contactus/?cid=nrcs142p2\\_053951](http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/contactus/?cid=nrcs142p2_053951)).

Great differences in soil properties can occur within short distances. Some soils are seasonally wet or subject to flooding. Some are too unstable to be used as a foundation for buildings or roads. Clayey or wet soils are poorly suited to use as septic tank absorption fields. A high water table makes a soil poorly suited to basements or underground installations.

The National Cooperative Soil Survey is a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local agencies. The Natural Resources Conservation Service (NRCS) has leadership for the Federal part of the National Cooperative Soil Survey.

Information about soils is updated periodically. Updated information is available through the NRCS Web Soil Survey, the site for official soil survey information.

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# How Soil Surveys Are Made

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Soil surveys are made to provide information about the soils and miscellaneous areas in a specific area. They include a description of the soils and miscellaneous areas and their location on the landscape and tables that show soil properties and limitations affecting various uses. Soil scientists observed the steepness, length, and shape of the slopes; the general pattern of drainage; the kinds of crops and native plants; and the kinds of bedrock. They observed and described many soil profiles. A soil profile is the sequence of natural layers, or horizons, in a soil. The profile extends from the surface down into the unconsolidated material in which the soil formed or from the surface down to bedrock. The unconsolidated material is devoid of roots and other living organisms and has not been changed by other biological activity.

Currently, soils are mapped according to the boundaries of major land resource areas (MLRAs). MLRAs are geographically associated land resource units that share common characteristics related to physiography, geology, climate, water resources, soils, biological resources, and land uses (USDA, 2006). Soil survey areas typically consist of parts of one or more MLRA.

The soils and miscellaneous areas in a survey area occur in an orderly pattern that is related to the geology, landforms, relief, climate, and natural vegetation of the area. Each kind of soil and miscellaneous area is associated with a particular kind of landform or with a segment of the landform. By observing the soils and miscellaneous areas in the survey area and relating their position to specific segments of the landform, a soil scientist develops a concept, or model, of how they were formed. Thus, during mapping, this model enables the soil scientist to predict with a considerable degree of accuracy the kind of soil or miscellaneous area at a specific location on the landscape.

Commonly, individual soils on the landscape merge into one another as their characteristics gradually change. To construct an accurate soil map, however, soil scientists must determine the boundaries between the soils. They can observe only a limited number of soil profiles. Nevertheless, these observations, supplemented by an understanding of the soil-vegetation-landscape relationship, are sufficient to verify predictions of the kinds of soil in an area and to determine the boundaries.

Soil scientists recorded the characteristics of the soil profiles that they studied. They noted soil color, texture, size and shape of soil aggregates, kind and amount of rock fragments, distribution of plant roots, reaction, and other features that enable them to identify soils. After describing the soils in the survey area and determining their properties, the soil scientists assigned the soils to taxonomic classes (units). Taxonomic classes are concepts. Each taxonomic class has a set of soil characteristics with precisely defined limits. The classes are used as a basis for comparison to classify soils systematically. Soil taxonomy, the system of taxonomic classification used in the United States, is based mainly on the kind and character of soil properties and the arrangement of horizons within the profile. After the soil

scientists classified and named the soils in the survey area, they compared the individual soils with similar soils in the same taxonomic class in other areas so that they could confirm data and assemble additional data based on experience and research.

The objective of soil mapping is not to delineate pure map unit components; the objective is to separate the landscape into landforms or landform segments that have similar use and management requirements. Each map unit is defined by a unique combination of soil components and/or miscellaneous areas in predictable proportions. Some components may be highly contrasting to the other components of the map unit. The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The delineation of such landforms and landform segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, onsite investigation is needed to define and locate the soils and miscellaneous areas.

Soil scientists make many field observations in the process of producing a soil map. The frequency of observation is dependent upon several factors, including scale of mapping, intensity of mapping, design of map units, complexity of the landscape, and experience of the soil scientist. Observations are made to test and refine the soil-landscape model and predictions and to verify the classification of the soils at specific locations. Once the soil-landscape model is refined, a significantly smaller number of measurements of individual soil properties are made and recorded. These measurements may include field measurements, such as those for color, depth to bedrock, and texture, and laboratory measurements, such as those for content of sand, silt, clay, salt, and other components. Properties of each soil typically vary from one point to another across the landscape.

Observations for map unit components are aggregated to develop ranges of characteristics for the components. The aggregated values are presented. Direct measurements do not exist for every property presented for every map unit component. Values for some properties are estimated from combinations of other properties.

While a soil survey is in progress, samples of some of the soils in the area generally are collected for laboratory analyses and for engineering tests. Soil scientists interpret the data from these analyses and tests as well as the field-observed characteristics and the soil properties to determine the expected behavior of the soils under different uses. Interpretations for all of the soils are field tested through observation of the soils in different uses and under different levels of management. Some interpretations are modified to fit local conditions, and some new interpretations are developed to meet local needs. Data are assembled from other sources, such as research information, production records, and field experience of specialists. For example, data on crop yields under defined levels of management are assembled from farm records and from field or plot experiments on the same kinds of soil.

Predictions about soil behavior are based not only on soil properties but also on such variables as climate and biological activity. Soil conditions are predictable over long periods of time, but they are not predictable from year to year. For example, soil scientists can predict with a fairly high degree of accuracy that a given soil will have a high water table within certain depths in most years, but they cannot predict that a high water table will always be at a specific level in the soil on a specific date.

After soil scientists located and identified the significant natural bodies of soil in the survey area, they drew the boundaries of these bodies on aerial photographs and

## Custom Soil Resource Report

identified each as a specific map unit. Aerial photographs show trees, buildings, fields, roads, and rivers, all of which help in locating boundaries accurately.

# Soil Map

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The soil map section includes the soil map for the defined area of interest, a list of soil map units on the map and extent of each map unit, and cartographic symbols displayed on the map. Also presented are various metadata about data used to produce the map, and a description of each soil map unit.

# Custom Soil Resource Report Soil Map



# Custom Soil Resource Report

## MAP LEGEND

### Area of Interest (AOI)

 Area of Interest (AOI)

### Soils

 Soil Map Unit Polygons

 Soil Map Unit Lines

 Soil Map Unit Points

### Special Point Features

 Blowout

 Borrow Pit

 Clay Spot

 Closed Depression

 Gravel Pit

 Gravelly Spot

 Landfill

 Lava Flow

 Marsh or swamp

 Mine or Quarry

 Miscellaneous Water

 Perennial Water

 Rock Outcrop

 Saline Spot

 Sandy Spot

 Severely Eroded Spot

 Sinkhole

 Slide or Slip

 Sodic Spot

 Spoil Area

 Stony Spot

 Very Stony Spot

 Wet Spot

 Other

 Special Line Features

### Water Features

 Streams and Canals

### Transportation

 Rails

 Interstate Highways

 US Routes

 Major Roads

 Local Roads

### Background

 Aerial Photography

## MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24,000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service

Web Soil Survey URL:

Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: El Paso County Area, Colorado

Survey Area Data: Version 23, Aug 29, 2025

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: May 27, 2024—Jul 28, 2024

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

## Map Unit Legend

| Map Unit Symbol                    | Map Unit Name                               | Acres in AOI | Percent of AOI |
|------------------------------------|---------------------------------------------|--------------|----------------|
| 8                                  | Blakeland loamy sand, 1 to 9 percent slopes | 17.6         | 12.4%          |
| 95                                 | Truckton loamy sand, 1 to 9 percent slopes  | 22.7         | 16.1%          |
| 96                                 | Truckton sandy loam, 0 to 3 percent slopes  | 35.0         | 24.8%          |
| 97                                 | Truckton sandy loam, 3 to 9 percent slopes  | 65.9         | 46.7%          |
| <b>Totals for Area of Interest</b> |                                             | <b>141.1</b> | <b>100.0%</b>  |

## Map Unit Descriptions

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

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The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An *association* is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

## El Paso County Area, Colorado

### 8—Blakeland loamy sand, 1 to 9 percent slopes

#### Map Unit Setting

*National map unit symbol:* 369v  
*Landscape:* Uplands  
*Elevation:* 4,600 to 5,800 feet  
*Mean annual precipitation:* 14 to 16 inches  
*Mean annual air temperature:* 46 to 48 degrees F  
*Frost-free period:* 125 to 145 days  
*Farmland classification:* Not prime farmland

#### Map Unit Composition

*Blakeland and similar soils:* 98 percent  
*Minor components:* 2 percent  
*Estimates are based on observations, descriptions, and transects of the mapunit.*

#### Description of Blakeland

##### Setting

*Landscape:* Uplands  
*Landform:* Flats, Hills  
*Landform position (three-dimensional):* Side slope, tal<sup>l</sup>  
*Down-slope shape:* Linear  
*Across-slope shape:* Linear  
*Parent material:* Alluvium derived from sedimentary rock and/or eolian deposits  
derived from sedimentary rock

##### Typical profile

*A - 0 to 11 inches:* loamy sand  
*AC - 11 to 27 inches:* loamy sand  
*C - 27 to 60 inches:* sand

##### Properties and qualities

*Slope:* 1 to 9 percent  
*Depth to restrictive feature:* More than 80 inches  
*Drainage class:* Somewhat excessively drained  
*Runoff class:* Low  
*Capacity of the most limiting layer to transmit water (Ksat):* High to very high (5.95 to 19.98 in/hr)  
*Depth to water table:* More than 80 inches  
*Frequency of flooding:* None  
*Frequency of ponding:* None  
*Calcium carbonate, maximum content:* 5 percent  
*Available water supply, 0 to 60 inches:* Low (about 4.5 inches)

##### Interpretive groups

*Land capability classification (irrigated):* 3e  
*Land capability classification (nonirrigated):* 6e  
*Hydrologic Soil Group:* A  
*Ecological site:* R049XB210CO - Sandy Foothill  
*Hydric soil rating:* No

**Minor Components**

**Other soils**

*Percent of map unit:* 1 percent

*Hydric soil rating:* No

**Pleasant**

*Percent of map unit:* 1 percent

*Landform:* Depressions

*Hydric soil rating:* Yes

**95—Truckton loamy sand, 1 to 9 percent slopes**

**Map Unit Setting**

*National map unit symbol:* 2yvrn

*Landscape:* Uplifted piedmonts

*Elevation:* 5,800 to 7,100 feet

*Mean annual precipitation:* 12 to 19 inches

*Mean annual air temperature:* 46 to 50 degrees F

*Frost-free period:* 90 to 155 days

*Farmland classification:* Not prime farmland

**Map Unit Composition**

*Truckton and similar soils:* 87 percent

*Minor components:* 13 percent

*Estimates are based on observations, descriptions, and transects of the mapunit.*

**Description of Truckton**

**Setting**

*Landscape:* Uplifted piedmonts

*Landform:* Interfluves, Fan remnants

*Down-slope shape:* Linear

*Across-slope shape:* Linear

*Parent material:* Wind re-worked alluvium derived from arkose

**Typical profile**

*A - 0 to 4 inches:* loamy sand

*Bt1 - 4 to 12 inches:* sandy loam

*Bt2 - 12 to 19 inches:* sandy loam

*C - 19 to 80 inches:* sandy loam

**Properties and qualities**

*Slope:* 1 to 9 percent

*Depth to restrictive feature:* More than 80 inches

*Drainage class:* Well drained

*Runoff class:* Low

*Capacity of the most limiting layer to transmit water (Ksat):* High (2.00 to 6.00 in/hr)

*Depth to water table:* More than 80 inches

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*Frequency of flooding:* None  
*Frequency of ponding:* None  
*Calcium carbonate, maximum content:* 1 percent  
*Maximum salinity:* Nonsaline to very slightly saline (0.1 to 2.0 mmhos/cm)  
*Available water supply, 0 to 60 inches:* Moderate (about 6.5 inches)

### Interpretive groups

*Land capability classification (irrigated):* 6e  
*Land capability classification (nonirrigated):* 6e  
*Hydrologic Soil Group:* A  
*Ecological site:* R049XB210CO - Sandy Foothill  
*Hydric soil rating:* No

### Minor Components

#### Blakeland

*Percent of map unit:* 5 percent  
*Landscape:* Uplifted piedmonts  
*Landform:* Interfluves, Low hills  
*Landform position (two-dimensional):* Summit, shoulder, backslope  
*Landform position (three-dimensional):* Crest, side slope  
*Down-slope shape:* Convex, linear  
*Across-slope shape:* Convex, linear  
*Ecological site:* R049XB210CO - Sandy Foothill  
*Hydric soil rating:* No

#### Bresser

*Percent of map unit:* 5 percent  
*Landscape:* Uplifted piedmonts  
*Landform:* Interfluves, Terraces  
*Landform position (three-dimensional):* Tread  
*Down-slope shape:* Linear  
*Across-slope shape:* Linear  
*Ecological site:* R049XB210CO - Sandy Foothill  
*Hydric soil rating:* No

#### Urban land

*Percent of map unit:* 2 percent  
*Landscape:* Uplifted piedmonts  
*Anthropogenic features:* Streets, parking lots, sidewalks, buildings, etc. of urban land, urban or suburban anthroscape  
*Hydric soil rating:* No

#### Ellicott, occasionally flooded

*Percent of map unit:* 1 percent  
*Landscape:* Uplifted piedmonts  
*Landform:* Flood plains, Drainageways  
*Down-slope shape:* Linear  
*Across-slope shape:* Concave, linear  
*Ecological site:* R067BY031CO - Sandy Bottomland  
*Hydric soil rating:* No

## 96—Truckton sandy loam, 0 to 3 percent slopes

### Map Unit Setting

*National map unit symbol:* 2yvr  
*Landscape:* Uplifted piedmonts  
*Elevation:* 5,400 to 7,000 feet  
*Mean annual precipitation:* 14 to 23 inches  
*Mean annual air temperature:* 45 to 52 degrees F  
*Frost-free period:* 90 to 155 days  
*Farmland classification:* Farmland of statewide importance

### Map Unit Composition

*Truckton and similar soils:* 85 percent  
*Minor components:* 15 percent  
*Estimates are based on observations, descriptions, and transects of the mapunit.*

### Description of Truckton

#### Setting

*Landscape:* Uplifted piedmonts  
*Landform:* Fan remnants, Interfluves  
*Down-slope shape:* Linear  
*Across-slope shape:* Linear  
*Parent material:* Wind re-worked alluvium derived from arkose

#### Typical profile

*A - 0 to 4 inches:* sandy loam  
*Bt1 - 4 to 12 inches:* sandy loam  
*Bt2 - 12 to 19 inches:* sandy loam  
*C - 19 to 80 inches:* sandy loam

#### Properties and qualities

*Slope:* 0 to 3 percent  
*Depth to restrictive feature:* More than 80 inches  
*Drainage class:* Well drained  
*Runoff class:* Very low  
*Capacity of the most limiting layer to transmit water (Ksat):* High (2.00 to 6.00 in/hr)  
*Depth to water table:* More than 80 inches  
*Frequency of flooding:* None  
*Frequency of ponding:* None  
*Calcium carbonate, maximum content:* 1 percent  
*Maximum salinity:* Nonsaline to very slightly saline (0.1 to 2.0 mmhos/cm)  
*Available water supply, 0 to 60 inches:* Moderate (about 6.6 inches)

#### Interpretive groups

*Land capability classification (irrigated):* 3e  
*Land capability classification (nonirrigated):* 4e  
*Hydrologic Soil Group:* A  
*Ecological site:* R049XB210CO - Sandy Foothill

*Hydric soil rating:* No

**Minor Components**

**Blakeland**

*Percent of map unit:* 5 percent  
*Landscape:* Uplifted piedmonts  
*Landform:* Low hills, Interfluves  
*Landform position (two-dimensional):* Shoulder, backslope, summit  
*Landform position (three-dimensional):* Side slope, crest  
*Down-slope shape:* Convex, linear  
*Across-slope shape:* Convex, linear  
*Ecological site:* R049XB210CO - Sandy Foothill  
*Hydric soil rating:* No

**Bresser**

*Percent of map unit:* 5 percent  
*Landscape:* Uplifted piedmonts  
*Landform:* Terraces, Interfluves  
*Landform position (three-dimensional):* Tread  
*Down-slope shape:* Linear  
*Across-slope shape:* Linear  
*Ecological site:* R049XB210CO - Sandy Foothill  
*Hydric soil rating:* No

**Pleasant, frequently ponded**

*Percent of map unit:* 2 percent  
*Landscape:* Uplifted piedmonts  
*Landform:* Closed depressions  
*Down-slope shape:* Concave, linear  
*Across-slope shape:* Concave  
*Ecological site:* R067BY010CO - Closed Depression  
*Hydric soil rating:* Yes

**Urban land**

*Percent of map unit:* 2 percent  
*Landscape:* Uplifted piedmonts  
*Anthropogenic features:* Streets, parking lots, sidewalks, buildings, etc. of urban land, urban or suburban anthroscape  
*Hydric soil rating:* No

**Ellicott, occasionally flooded**

*Percent of map unit:* 1 percent  
*Landscape:* Uplifted piedmonts  
*Landform:* Drainageways, Flood plains  
*Down-slope shape:* Linear  
*Across-slope shape:* Concave, linear  
*Ecological site:* R067BY031CO - Sandy Bottomland  
*Hydric soil rating:* No

## 97—Truckton sandy loam, 3 to 9 percent slopes

### Map Unit Setting

*National map unit symbol:* 2x0j2  
*Landscape:* Uplifted piedmonts  
*Elevation:* 5,300 to 6,850 feet  
*Mean annual precipitation:* 14 to 19 inches  
*Mean annual air temperature:* 48 to 52 degrees F  
*Frost-free period:* 85 to 155 days  
*Farmland classification:* Not prime farmland

### Map Unit Composition

*Truckton and similar soils:* 85 percent  
*Minor components:* 15 percent  
*Estimates are based on observations, descriptions, and transects of the mapunit.*

### Description of Truckton

#### Setting

*Landscape:* Uplifted piedmonts  
*Landform:* Backslopes of hillslopes, Sideslopes of interfluves  
*Landform position (two-dimensional):* Backslope  
*Landform position (three-dimensional):* Side slope  
*Down-slope shape:* Linear  
*Across-slope shape:* Linear  
*Parent material:* Re-worked alluvium derived from arkose

#### Typical profile

*A - 0 to 4 inches:* sandy loam  
*Bt1 - 4 to 12 inches:* sandy loam  
*Bt2 - 12 to 19 inches:* sandy loam  
*C - 19 to 80 inches:* sandy loam

#### Properties and qualities

*Slope:* 3 to 9 percent  
*Depth to restrictive feature:* More than 80 inches  
*Drainage class:* Well drained  
*Runoff class:* Low  
*Capacity of the most limiting layer to transmit water (Ksat):* High (2.00 to 6.00 in/hr)  
*Depth to water table:* More than 80 inches  
*Frequency of flooding:* None  
*Frequency of ponding:* None  
*Calcium carbonate, maximum content:* 1 percent  
*Maximum salinity:* Nonsaline (0.1 to 1.9 mmhos/cm)  
*Available water supply, 0 to 60 inches:* Moderate (about 6.6 inches)

#### Interpretive groups

*Land capability classification (irrigated):* 6e  
*Land capability classification (nonirrigated):* 6e

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*Hydrologic Soil Group:* A

*Ecological site:* R049XB210CO - Sandy Foothill

*Hydric soil rating:* No

### Minor Components

#### **Blakeland**

*Percent of map unit:* 8 percent

*Landscape:* Uplifted piedmonts

*Landform:* Shoulders and backslopes of hillslopes, Sideslopes and crests of interfluves

*Landform position (two-dimensional):* Shoulder, backslope, summit

*Landform position (three-dimensional):* Crest, side slope

*Down-slope shape:* Convex, linear

*Across-slope shape:* Convex, linear

*Ecological site:* R049XB210CO - Sandy Foothill

*Hydric soil rating:* No

#### **Bresser**

*Percent of map unit:* 7 percent

*Landscape:* Uplifted piedmonts

*Landform:* Toeslopes or footslopes of low hills, Baseslopes of interfluves

*Landform position (two-dimensional):* Footslope, toeslope

*Landform position (three-dimensional):* Base slope

*Down-slope shape:* Concave, linear

*Across-slope shape:* Concave, linear

*Ecological site:* R049XB210CO - Sandy Foothill

*Hydric soil rating:* No

# **Soil Information for All Uses**

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## **Soil Properties and Qualities**

The Soil Properties and Qualities section includes various soil properties and qualities displayed as thematic maps with a summary table for the soil map units in the selected area of interest. A single value or rating for each map unit is generated by aggregating the interpretive ratings of individual map unit components. This aggregation process is defined for each property or quality.

## **Soil Qualities and Features**

Soil qualities are behavior and performance attributes that are not directly measured, but are inferred from observations of dynamic conditions and from soil properties. Example soil qualities include natural drainage, and frost action. Soil features are attributes that are not directly part of the soil. Example soil features include slope and depth to restrictive layer. These features can greatly impact the use and management of the soil.

## **Hydrologic Soil Group**

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

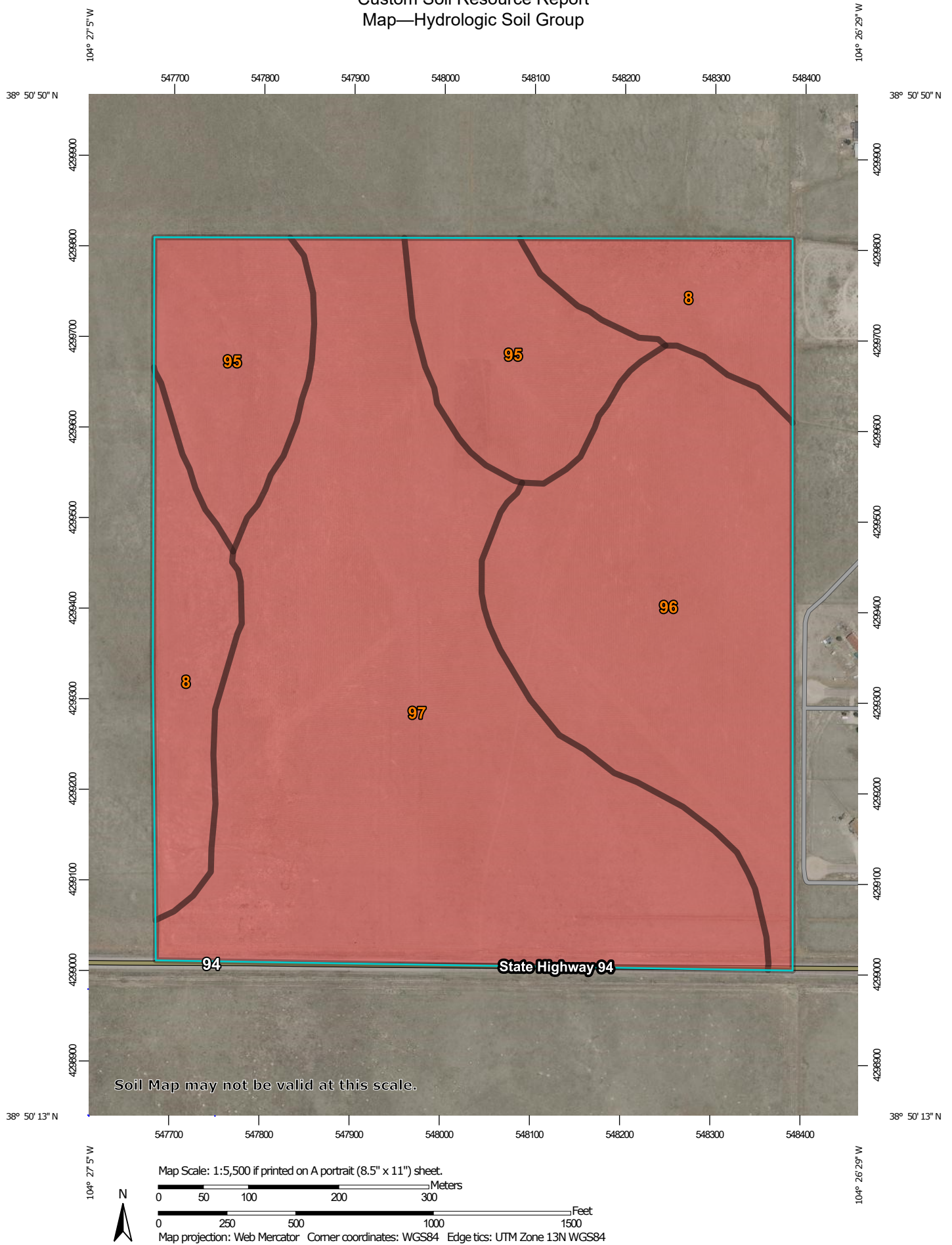
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Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

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Map—Hydrologic Soil Group



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### MAP LEGEND

#### Area of Interest (AOI)

 Area of Interest (AOI)

#### Soils

##### Soil Rating Polygons

 A  
 A/D  
 B  
 B/D  
 C  
 C/D  
 D  
 Not rated or not available

##### Soil Rating Lines

 A  
 A/D  
 B  
 B/D  
 C  
 C/D  
 D  
 Not rated or not available

##### Soil Rating Points

 A  
 A/D  
 B  
 B/D

 C  
 C/D  
 D  
 Not rated or not available

#### Water Features

 Streams and Canals

#### Transportation

 Rails  
 Interstate Highways  
 US Routes  
 Major Roads  
 Local Roads

#### Background

 Aerial Photography

### MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24,000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service  
Web Soil Survey URL:  
Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: El Paso County Area, Colorado  
Survey Area Data: Version 23, Aug 29, 2025

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: May 27, 2024—Jul 28, 2024

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

**Table—Hydrologic Soil Group**

| Map unit symbol                    | Map unit name                               | Rating | Acres in AOI | Percent of AOI |
|------------------------------------|---------------------------------------------|--------|--------------|----------------|
| 8                                  | Blakeland loamy sand, 1 to 9 percent slopes | A      | 17.6         | 12.4%          |
| 95                                 | Truckton loamy sand, 1 to 9 percent slopes  | A      | 22.7         | 16.1%          |
| 96                                 | Truckton sandy loam, 0 to 3 percent slopes  | A      | 35.0         | 24.8%          |
| 97                                 | Truckton sandy loam, 3 to 9 percent slopes  | A      | 65.9         | 46.7%          |
| <b>Totals for Area of Interest</b> |                                             |        | <b>141.1</b> | <b>100.0%</b>  |

**Rating Options—Hydrologic Soil Group***Aggregation Method: Dominant Condition**Component Percent Cutoff: None Specified**Tie-break Rule: Higher*

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***APPENDIX C: HYDROLOGY***

### EXISTING RATIONAL CALCULATIONS SUMMARY

| SUBCATCHMENT NAME | DESIGN POINT                             | TRIBUTARY AREA (AC) | IMPERVIOUSNESS (%) | PEAK FLOWS (CFS) |        |
|-------------------|------------------------------------------|---------------------|--------------------|------------------|--------|
|                   |                                          |                     |                    | Q5               | Q100   |
| EX-1              | EX-1                                     | 16.42               | 2.0%               | 2.37             | 15.90  |
| EX-2              | EX-2                                     | 15.87               | 2.0%               | 2.36             | 15.85  |
| EX-3              | EX-3                                     | 17.35               | 2.0%               | 2.82             | 18.98  |
| EX-4              | EX-4                                     | 52.09               | 2.0%               | 7.11             | 47.80  |
| EX-5              | EX-5                                     | 36.19               | 2.0%               | 5.74             | 38.56  |
| OF-1              | OF-1                                     | 204.29              | 3.7%               | 18.45            | 112.58 |
| OF-2              | OF-2                                     | 290.54              | 3.8%               | 25.46            | 154.64 |
| OF-3              | OF-3                                     | 18.51               | 2.0%               | 3.41             | 22.92  |
| OF-4              | OF-4                                     | 0.96                | 2.0%               | 0.19             | 1.25   |
| OP-1              | OP-1                                     | 0.04                | 41.0%              | 0.07             | 0.18   |
| OF-5              | OF-5                                     | 6.21                | 30.9%              | 3.01             | 8.56   |
| OF-6              | OF-6                                     | 0.14                | 80.0%              | 0.34             | 0.67   |
| CUMMULATIVE FLOWS |                                          |                     |                    |                  |        |
| DESIGN POINT      | BASINS                                   | TRIBUTARY AREA (AC) | IMPERV. (%)        | Q5               | Q100   |
| EX1               | EX-1, OF-1                               | 220.71              | 3.6%               | 19.77            | 121.43 |
| EX3               | OF-2, EX-3                               | 307.90              | 3.7%               | 26.80            | 163.68 |
| EX4               | EX-2, EX-4, EX-5, OF-3, OF-4, OF-5, OP-1 | 129.88              | 7.7%               | 15.08            | 127.17 |
| OF-6              | OF-6                                     | 0.14                | 80.0%              | 0.34             | 0.67   |
| TOTAL             |                                          | 658.62              | 4.5%               | 61.98            | 412.95 |

Calculation of Peak Runoff using Rational Method

Designer: DJS

Company: Kimley-Horn

Date: 7/29/2026

Project: Trinity Ranch Estates

Location: El Paso County, Colorado

MHFD-Rational, Version 3.00 (August 2025)

$t_i = \frac{0.395(1.1 - C_g)\sqrt{L_i}}{S^{0.33}}$

Computed  $t_c = t_i + t_t$

$t_t = \frac{L_t}{60K\sqrt{S_t}} = \frac{L_t}{60V_t}$

Regional  $t_c = (26 - 17i) + \frac{L_t}{60(14i + 9)\sqrt{S_t}}$

$t_{c \text{ minimum}} = 5 \text{ (urban)}$   
 $t_{c \text{ minimum}} = 10 \text{ (non-urban)}$

Selected  $t_c = \max(t_{\text{minimum}}, \min(\text{Computed } t_c, \text{Regional } t_c))$

Calculation of Peak Runoff using Rational Method

Select MHFD location for NOAA Atlas 14 Rainfall Depths from the pulldown list OR enter your own depths obtained from the NOAA website (click this link)

WQE2-yr5-yr10-yr25-yr50-yr100-yr500-yr

1-hour rainfall depth, P1 (in) =

0.601.191.501.752.002.252.522.91

a

b

c

Rainfall Intensity Equation Coefficients =

28.5010.000.786

$I(in/hr) = \frac{a + P_1}{(b + t_c)^c}$

$Q(cfs) = CIA$

Calculation of Peak Runoff using Rational Method

Provide input for area, soil type, and imperviousness on the Runoff Coeffts worksheet.

| Subcatchment Name | Area (ac) | NRCS Hydrologic Soil Group(s) | Imperviousness | Runoff Coefficient, C |      |       |       |       |        |        |                                          | Overland (Initial) Flow Time  |                               |                                            |                                         |                                             | Channelized (Travel) Flow Time |                               |                                               |                          |                                                   |                                            | Time of Concentration         |                               |                               |                                          | Rainfall Intensity, I (in/hr) |      |      |       |       |       |        |        | Peak Flow, Q (cfs) |      |       |       |       |        |        |        |
|-------------------|-----------|-------------------------------|----------------|-----------------------|------|-------|-------|-------|--------|--------|------------------------------------------|-------------------------------|-------------------------------|--------------------------------------------|-----------------------------------------|---------------------------------------------|--------------------------------|-------------------------------|-----------------------------------------------|--------------------------|---------------------------------------------------|--------------------------------------------|-------------------------------|-------------------------------|-------------------------------|------------------------------------------|-------------------------------|------|------|-------|-------|-------|--------|--------|--------------------|------|-------|-------|-------|--------|--------|--------|
|                   |           |                               |                | WQE & 2-yr            | 5-yr | 10-yr | 25-yr | 50-yr | 100-yr | 500-yr | Overland Flow Length L <sub>i</sub> (ft) | U/S Elevation (ft) (Optional) | D/S Elevation (ft) (Optional) | Overland Flow Slope S <sub>i</sub> (ft/ft) | Overland Flow Time t <sub>i</sub> (min) | Channelized Flow Length L <sub>i</sub> (ft) | U/S Elevation (ft) (Optional)  | D/S Elevation (ft) (Optional) | Channelized Flow Slope S <sub>i</sub> (ft/ft) | NRCS Conveyance Factor K | Channelized Flow Velocity V <sub>i</sub> (ft/sec) | Channelized Flow Time t <sub>i</sub> (min) | Computed t <sub>c</sub> (min) | Regional t <sub>c</sub> (min) | Selected t <sub>c</sub> (min) | (Optional) Override t <sub>c</sub> (min) | WQE                           | 2-yr | 5-yr | 10-yr | 25-yr | 50-yr | 100-yr | 500-yr | WQE                | 2-yr | 5-yr  | 10-yr | 25-yr | 50-yr  | 100-yr | 500-yr |
| EX-1              | 16.42     | A                             | 2.0%           | 0.03                  | 0.09 | 0.17  | 0.26  | 0.31  | 0.36   | 0.47   | 215.00                                   | 6176.50                       | 6173.49                       | 0.014                                      | 23.93                                   | 1614.41                                     |                                |                               | 0.010                                         | 2.5                      | 0.24                                              | 109.85                                     | 133.78                        | 55.25                         | 55.25                         |                                          | 0.64                          | 1.27 | 1.60 | 1.87  | 2.14  | 2.40  | 2.69   | 3.11   | 0.32               | 0.63 | 2.37  | 5.22  | 9.12  | 12.23  | 15.90  | 23.98  |
| EX-2              | 15.87     | A                             | 2.0%           | 0.03                  | 0.09 | 0.17  | 0.26  | 0.31  | 0.36   | 0.47   | 485.00                                   |                               |                               | 0.032                                      | 27.36                                   | 931.00                                      |                                | 0.004                         | 2.5                                           | 0.15                     | 100.69                                            | 128.04                                     | 52.78                         | 52.78                         |                               | 0.66                                     | 1.31                          | 1.65 | 1.93 | 2.20  | 2.48  | 2.77  | 3.20   | 0.31   | 0.62               | 2.36 | 5.20  | 9.08  | 12.19 | 15.85  | 23.89  |        |
| EX-3              | 17.35     | A                             | 2.0%           | 0.03                  | 0.09 | 0.17  | 0.26  | 0.31  | 0.36   | 0.47   | 500.00                                   | 6166.00                       | 6150.00                       | 0.032                                      | 27.78                                   | 1142.85                                     |                                | 6138.29                       | 0.010                                         | 2.5                      | 0.25                                              | 75.27                                      | 103.05                        | 45.94                         | 45.94                         |                                          | 0.72                          | 1.43 | 1.81 | 2.11  | 2.41  | 2.71  | 3.04   | 3.51   | 0.38               | 0.75 | 2.82  | 6.22  | 10.88 | 14.59  | 18.98  | 28.61  |
| EX-4              | 52.09     | A                             | 2.0%           | 0.03                  | 0.09 | 0.17  | 0.26  | 0.31  | 0.36   | 0.47   | 500.00                                   | 6166.75                       | 6149.75                       | 0.034                                      | 27.23                                   | 1872.26                                     | 6149.55                        | 6131.52                       | 0.010                                         | 2.5                      | 0.25                                              | 127.19                                     | 154.42                        | 59.93                         | 59.93                         |                                          | 0.61                          | 1.20 | 1.52 | 1.77  | 2.02  | 2.28  | 2.55   | 2.94   | 0.95               | 1.88 | 7.11  | 15.68 | 27.40 | 36.75  | 47.80  | 72.07  |
| EX-5              | 36.19     | A                             | 2.0%           | 0.03                  | 0.09 | 0.17  | 0.26  | 0.31  | 0.36   | 0.47   | 500.00                                   | 6173.18                       | 6165.18                       | 0.016                                      | 34.92                                   | 1747.00                                     | 6165.00                        | 6130.00                       | 0.020                                         | 2.5                      | 0.35                                              | 82.28                                      | 117.20                        | 47.83                         | 47.83                         |                                          | 0.70                          | 1.40 | 1.76 | 2.06  | 2.35  | 2.64  | 2.96   | 3.42   | 0.77               | 1.52 | 5.74  | 12.64 | 22.10 | 29.65  | 38.56  | 58.13  |
| OF-1              | 204.29    | A                             | 3.7%           | 0.04                  | 0.10 | 0.18  | 0.27  | 0.32  | 0.37   | 0.48   | 500.00                                   | 6292.32                       | 6279.32                       | 0.026                                      | 29.42                                   | 7140.85                                     | 6279.09                        | 6171.98                       | 0.015                                         | 2.5                      | 0.31                                              | 388.70                                     | 418.12                        | 127.43                        | 127.43                        |                                          | 0.36                          | 0.71 | 0.89 | 1.04  | 1.19  | 1.34  | 1.50   | 1.73   | 3.07               | 6.09 | 18.45 | 38.34 | 65.37 | 87.03  | 112.58 | 169.21 |
| OF-2              | 290.54    | A                             | 3.8%           | 0.04                  | 0.10 | 0.18  | 0.27  | 0.32  | 0.37   | 0.48   | 500.00                                   | 6286.17                       | 6260.17                       | 0.052                                      | 23.39                                   | 7341.73                                     | 6260.18                        | 6157.40                       | 0.014                                         | 2.5                      | 0.30                                              | 413.66                                     | 437.05                        | 133.82                        | 133.82                        |                                          | 0.34                          | 0.68 | 0.86 | 1.00  | 1.15  | 1.29  | 1.45   | 1.67   | 4.27               | 8.48 | 25.46 | 52.76 | 89.85 | 119.58 | 154.64 | 232.41 |
| OF-3              | 18.51     | A                             | 2.0%           | 0.03                  | 0.09 | 0.17  | 0.26  | 0.31  | 0.36   | 0.47   | 270.00                                   |                               |                               | 0.008                                      | 32.25                                   | 1086.50                                     |                                |                               | 0.026                                         | 2.5                      | 0.40                                              | 44.92                                      | 77.18                         | 37.76                         | 37.76                         |                                          | 0.82                          | 1.62 | 2.05 | 2.39  | 2.73  | 3.07  | 3.44   | 3.97   | 0.45               | 0.90 | 3.41  | 7.52  | 13.14 | 17.62  | 22.92  | 34.55  |
| OF-4              | 0.96      | A                             | 2.0%           | 0.03                  | 0.09 | 0.17  | 0.26  | 0.31  | 0.36   | 0.47   | 239.00                                   |                               |                               | 0.006                                      | 33.37                                   | 493.00                                      |                                |                               | 0.009                                         | 2.5                      | 0.24                                              | 34.64                                      | 68.01                         | 34.99                         | 34.99                         |                                          | 0.86                          | 1.70 | 2.15 | 2.50  | 2.86  | 3.22  | 3.60   | 4.16   | 0.02               | 0.05 | 0.19  | 0.41  | 0.71  | 0.96   | 1.25   | 1.88   |
| OF-1              | 0.04      | A                             | 41.0%          | 0.30                  | 0.34 | 0.40  | 0.46  | 0.50  | 0.53   | 0.57   | 16.00                                    |                               |                               | 0.020                                      | 4.37                                    | 30.00                                       |                                |                               | 0.010                                         | 20                       | 2.00                                              | 4.62                                       | 19.37                         | 5.00                          |                               | 2.04                                     | 4.04                          | 5.09 | 5.94 | 6.78  | 7.63  | 8.55  | 9.67   | 0.02   | 0.05               | 0.07 | 0.09  | 0.12  | 0.15  | 0.18   | 0.26   |        |
| OF-5              | 6.21      | A                             | 30.9%          | 0.25                  | 0.30 | 0.36  | 0.43  | 0.47  | 0.51   | 0.61   | 20.00                                    |                               |                               | 0.020                                      | 5.14                                    | 4444.00                                     |                                |                               | 0.010                                         | 15                       | 1.50                                              | 49.38                                      | 54.52                         | 76.32                         | 54.52                         |                                          | 0.65                          | 1.28 | 1.62 | 1.89  | 2.18  | 2.42  | 2.72   | 3.14   | 1.02               | 2.02 | 3.01  | 4.22  | 5.77  | 7.09   | 8.56   | 11.84  |
| OF-6              | 0.14      | A                             | 80.0%          | 0.57                  | 0.59 | 0.63  | 0.66  | 0.68  | 0.70   | 0.86   | 116.00                                   |                               |                               | 0.010                                      | 9.92                                    | 1.00                                        |                                |                               | 0.010                                         | 15                       | 1.50                                              | 0.01                                       | 9.93                          | 12.41                         | 9.93                          |                                          | 1.63                          | 3.23 | 4.07 | 4.75  | 5.43  | 6.10  | 6.84   | 7.89   | 0.13               | 0.26 | 0.34  | 0.42  | 0.50  | 0.58   | 0.67   | 0.95   |

Existing Rational Calcs\_Trinity Ranch, Rational Calcs

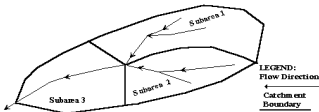
7/29/2026, 10:35 AM

Determination of Runoff Coefficients for Rational Method

MHFD-Rational, Version 3.00 (August 2025)

Designer: DJS  
Company: Kimley-Horn  
Date: 7/29/2026  
Project: Trinity Ranch Estates  
Location: El Paso County, Colorado

Cells of this color are for required user-input  
Cells of this color are for optional override values



| Provide subcatchment names on the Rational Calcs worksheet to open up the table below. |               |           |                            |                        |                             |                           |                                    |                       |      |       |       |       |        |        |             |                                           |       |       |       |        |        |  |  |          |
|----------------------------------------------------------------------------------------|---------------|-----------|----------------------------|------------------------|-----------------------------|---------------------------|------------------------------------|-----------------------|------|-------|-------|-------|--------|--------|-------------|-------------------------------------------|-------|-------|-------|--------|--------|--|--|----------|
| Subcatchment Name                                                                      | # of Subareas | Area (ac) | NRCS Hydrologic Soil Group | Percent Imperviousness |                             |                           |                                    | Runoff Coefficient, C |      |       |       |       |        |        |             | (Optional) Override Runoff Coefficient, C |       |       |       |        |        |  |  | Comments |
|                                                                                        |               |           |                            | Imperviousness Source  | Imperviousness Category     | Calculated Imperviousness | (Optional) Override Imperviousness | WQEI & 2-yr           | 5-yr | 10-yr | 25-yr | 50-yr | 100-yr | 500-yr | WQEI & 2-yr | 5-yr                                      | 10-yr | 25-yr | 50-yr | 100-yr | 500-yr |  |  |          |
| EX-1                                                                                   | 1             | 16.42     | A                          |                        |                             | 5.0%                      | 2.0%                               | 0.01                  | 0.01 | 0.01  | 0.01  | 0.04  | 0.13   | 0.27   | 0.03        | 0.09                                      | 0.17  | 0.26  | 0.31  | 0.36   | 0.47   |  |  |          |
|                                                                                        |               | 16.42     | A                          | Surface Type           | Historic Flow Analysis      | 5%                        | 2%                                 | 0.01                  | 0.01 | 0.01  | 0.01  | 0.04  | 0.13   | 0.27   | 0.03        | 0.09                                      | 0.17  | 0.26  | 0.31  | 0.36   | 0.47   |  |  |          |
| EX-2                                                                                   | 1             | 15.87     | A                          |                        |                             | 5.0%                      | 2.0%                               | 0.01                  | 0.01 | 0.01  | 0.01  | 0.04  | 0.13   | 0.27   | 0.03        | 0.09                                      | 0.17  | 0.26  | 0.31  | 0.36   | 0.47   |  |  |          |
|                                                                                        |               | 15.87     | A                          | Surface Type           | Historic Flow Analysis      | 5%                        | 2%                                 | 0.01                  | 0.01 | 0.01  | 0.01  | 0.04  | 0.13   | 0.27   | 0.03        | 0.09                                      | 0.17  | 0.26  | 0.31  | 0.36   | 0.47   |  |  |          |
| EX-3                                                                                   | 1             | 17.35     | A                          |                        |                             | 5.0%                      | 2.0%                               | 0.01                  | 0.01 | 0.01  | 0.01  | 0.04  | 0.13   | 0.27   | 0.03        | 0.09                                      | 0.17  | 0.26  | 0.31  | 0.36   | 0.47   |  |  |          |
|                                                                                        |               | 17.35     | A                          | Surface Type           | Historic Flow Analysis      | 5%                        | 2%                                 | 0.01                  | 0.01 | 0.01  | 0.01  | 0.04  | 0.13   | 0.27   | 0.03        | 0.09                                      | 0.17  | 0.26  | 0.31  | 0.36   | 0.47   |  |  |          |
| EX-4                                                                                   | 1             | 52.09     | A                          |                        |                             | 5.0%                      | 2.0%                               | 0.01                  | 0.01 | 0.01  | 0.01  | 0.04  | 0.13   | 0.27   | 0.03        | 0.09                                      | 0.17  | 0.26  | 0.31  | 0.36   | 0.47   |  |  |          |
|                                                                                        |               | 52.09     | A                          | Surface Type           | Historic Flow Analysis      | 5%                        | 2%                                 | 0.01                  | 0.01 | 0.01  | 0.01  | 0.04  | 0.13   | 0.27   | 0.03        | 0.09                                      | 0.17  | 0.26  | 0.31  | 0.36   | 0.47   |  |  |          |
| EX-5                                                                                   | 1             | 36.19     | A                          |                        |                             | 5.0%                      | 2.0%                               | 0.01                  | 0.01 | 0.01  | 0.01  | 0.04  | 0.13   | 0.27   | 0.03        | 0.09                                      | 0.17  | 0.26  | 0.31  | 0.36   | 0.47   |  |  |          |
|                                                                                        |               | 36.19     | A                          | Surface Type           | Historic Flow Analysis      | 5%                        | 2%                                 | 0.01                  | 0.01 | 0.01  | 0.01  | 0.04  | 0.13   | 0.27   | 0.03        | 0.09                                      | 0.17  | 0.26  | 0.31  | 0.36   | 0.47   |  |  |          |
| OF-1                                                                                   | 3             | 204.29    | A                          |                        |                             | 6.7%                      | 3.7%                               | 0.02                  | 0.02 | 0.02  | 0.03  | 0.06  | 0.14   | 0.28   | 0.04        | 0.10                                      | 0.18  | 0.27  | 0.32  | 0.37   | 0.48   |  |  |          |
|                                                                                        |               | 3.94      | A                          | Surface Type           | Gravel - High Traffic Areas | 80%                       |                                    | 0.63                  | 0.65 | 0.66  | 0.69  | 0.71  | 0.73   | 0.77   | 0.57        | 0.59                                      | 0.63  | 0.66  | 0.68  | 0.70   | 0.86   |  |  |          |
|                                                                                        |               | 0.51      | A                          | Surface Type           | Roofs                       | 95%                       | 90%                                | 0.73                  | 0.75 | 0.77  | 0.79  | 0.79  | 0.81   | 0.83   | 0.71        | 0.73                                      | 0.75  | 0.78  | 0.80  | 0.81   | 0.89   |  |  |          |
|                                                                                        |               | 199.84    | A                          | Surface Type           | Historic Flow Analysis      | 5%                        | 2%                                 | 0.01                  | 0.01 | 0.01  | 0.01  | 0.04  | 0.13   | 0.27   | 0.03        | 0.09                                      | 0.17  | 0.26  | 0.31  | 0.36   | 0.47   |  |  |          |
| OF-2                                                                                   | 3             | 290.54    | A                          |                        |                             | 6.8%                      | 3.8%                               | 0.02                  | 0.02 | 0.02  | 0.03  | 0.06  | 0.14   | 0.28   | 0.04        | 0.10                                      | 0.18  | 0.27  | 0.32  | 0.37   | 0.48   |  |  |          |
|                                                                                        |               | 6.01      | A                          | Surface Type           | Gravel - High Traffic Areas | 80%                       |                                    | 0.63                  | 0.65 | 0.66  | 0.69  | 0.71  | 0.73   | 0.77   | 0.57        | 0.59                                      | 0.63  | 0.66  | 0.68  | 0.70   | 0.86   |  |  |          |
|                                                                                        |               | 0.66      | A                          | Surface Type           | Roofs                       | 95%                       | 90%                                | 0.73                  | 0.75 | 0.77  | 0.79  | 0.79  | 0.81   | 0.83   | 0.71        | 0.73                                      | 0.75  | 0.78  | 0.80  | 0.81   | 0.89   |  |  |          |
|                                                                                        |               | 283.87    | A                          | Surface Type           | Historic Flow Analysis      | 5%                        | 2%                                 | 0.01                  | 0.01 | 0.01  | 0.01  | 0.04  | 0.13   | 0.27   | 0.03        | 0.09                                      | 0.17  | 0.26  | 0.31  | 0.36   | 0.47   |  |  |          |
| OF-3                                                                                   | 1             | 18.51     | A                          |                        |                             | 5.0%                      | 2.0%                               | 0.01                  | 0.01 | 0.01  | 0.01  | 0.04  | 0.13   | 0.27   | 0.03        | 0.09                                      | 0.17  | 0.26  | 0.31  | 0.36   | 0.47   |  |  |          |
|                                                                                        |               | 18.51     | A                          | Surface Type           | Historic Flow Analysis      | 5%                        | 2%                                 | 0.01                  | 0.01 | 0.01  | 0.01  | 0.04  | 0.13   | 0.27   | 0.03        | 0.09                                      | 0.17  | 0.26  | 0.31  | 0.36   | 0.47   |  |  |          |
| OF-4                                                                                   | 1             | 0.96      | A                          |                        |                             | 5.0%                      | 2.0%                               | 0.01                  | 0.01 | 0.01  | 0.01  | 0.04  | 0.13   | 0.27   | 0.03        | 0.09                                      | 0.17  | 0.26  | 0.31  | 0.36   | 0.47   |  |  |          |
|                                                                                        |               | 0.96      | A                          | Surface Type           | Historic Flow Analysis      | 5%                        | 2%                                 | 0.01                  | 0.01 | 0.01  | 0.01  | 0.04  | 0.13   | 0.27   | 0.03        | 0.09                                      | 0.17  | 0.26  | 0.31  | 0.36   | 0.47   |  |  |          |
| OP-1                                                                                   | 2             | 0.04      | A                          |                        |                             | 42.5%                     | 41.0%                              | 0.32                  | 0.33 | 0.34  | 0.35  | 0.38  | 0.43   | 0.52   | 0.30        | 0.34                                      | 0.40  | 0.46  | 0.50  | 0.53   | 0.67   |  |  |          |
|                                                                                        |               | 0.02      | A                          | Surface Type           | Gravel - High Traffic Areas | 80%                       |                                    | 0.63                  | 0.65 | 0.66  | 0.69  | 0.71  | 0.73   | 0.77   | 0.57        | 0.59                                      | 0.63  | 0.66  | 0.68  | 0.70   | 0.86   |  |  |          |
|                                                                                        |               | 0.02      | A                          | Surface Type           | Historic Flow Analysis      | 5%                        | 2%                                 | 0.01                  | 0.01 | 0.01  | 0.01  | 0.04  | 0.13   | 0.27   | 0.03        | 0.09                                      | 0.17  | 0.26  | 0.31  | 0.36   | 0.47   |  |  |          |
| OF-5                                                                                   | 2             | 6.21      | A                          |                        |                             | 34.6%                     | 30.9%                              | 0.24                  | 0.25 | 0.26  | 0.27  | 0.29  | 0.35   | 0.45   | 0.25        | 0.30                                      | 0.36  | 0.43  | 0.47  | 0.51   | 0.61   |  |  |          |
|                                                                                        |               | 2.04      | A                          | Surface Type           | Roadways and Paved Streets  | 95%                       | 90%                                | 0.73                  | 0.75 | 0.77  | 0.79  | 0.79  | 0.81   | 0.83   | 0.71        | 0.73                                      | 0.75  | 0.78  | 0.80  | 0.81   | 0.89   |  |  |          |
|                                                                                        |               | 4.17      | A                          | Surface Type           | Historic Flow Analysis      | 5%                        | 2%                                 | 0.01                  | 0.01 | 0.01  | 0.01  | 0.04  | 0.13   | 0.27   | 0.03        | 0.09                                      | 0.17  | 0.26  | 0.31  | 0.36   | 0.47   |  |  |          |
| OF-6                                                                                   | 1             | 0.14      | A                          |                        |                             | 80.0%                     | 80.0%                              | 0.63                  | 0.65 | 0.66  | 0.69  | 0.71  | 0.73   | 0.77   | 0.57        | 0.59                                      | 0.63  | 0.66  | 0.68  | 0.70   | 0.86   |  |  |          |
|                                                                                        |               | 0.14      | A                          | Surface Type           | Gravel - High Traffic Areas | 80%                       |                                    | 0.63                  | 0.65 | 0.66  | 0.69  | 0.71  | 0.73   | 0.77   | 0.57        | 0.59                                      | 0.63  | 0.66  | 0.68  | 0.70   | 0.86   |  |  |          |

Combined Peak Runoff Calculations for Inlets and Storm Drains

Designer: DJS

Company: Kimley-Horn

Date: 7/29/2026

Project: Trinity Ranch Estates

Location: El Paso County, Colorado

MHFD-Rational, Version 3.00 (August 2025)

5-yrDesign Storm Return Period (Note: this worksheet can only evaluate one design storm at a time)

Use 1 column (C, D, E) per row

Obtain Inlet Capacity from MHFD-Inlet (Optional)

| Design Point | # of Upstream Runoff Sources | Local Subcatchment Name | Upstream Surface Design Point | Upstream Pipe Design Point | Local Subcatchment Runoff |      |                      |               | Surface Runoff to Design Point |                      |                   |                      | Inlet Capacity / Bypass Flow |                      |                   | Total Runoff to Design Point |                      |                   |                    |
|--------------|------------------------------|-------------------------|-------------------------------|----------------------------|---------------------------|------|----------------------|---------------|--------------------------------|----------------------|-------------------|----------------------|------------------------------|----------------------|-------------------|------------------------------|----------------------|-------------------|--------------------|
|              |                              |                         |                               |                            | Area (ac)                 | C    | t <sub>c</sub> (min) | Local Q (cfs) | Σ(C*A) (acre)                  | t <sub>c</sub> (min) | Intensity (in/hr) | Surface Runoff (cfs) | (Optional) Inlet Name        | Inlet Capacity (cfs) | Bypass Flow (cfs) | Σ(C*A) (acre)                | t <sub>c</sub> (min) | Intensity (in/hr) | Total Runoff (cfs) |
| EX1          | 2                            |                         |                               |                            |                           |      |                      |               | 22.16                          | 127.43               | 0.89              | 19.77                |                              |                      | 19.77             | 22.16                        | 127.43               | 0.89              | 19.77              |
|              |                              | EX-1                    |                               |                            | 16.42                     | 0.09 | 55.25                | 2.37          | 1.48                           | 55.25                | 1.60              | 16.73                |                              |                      |                   | 1.48                         | 55.25                | 1.60              | 16.73              |
|              |                              | OF-1                    |                               |                            | 204.29                    | 0.10 | 127.43               | 18.45         | 20.68                          | 127.43               | 0.89              | 19.77                |                              |                      |                   | 20.68                        | 127.43               | 0.89              | 19.77              |
| EX4          | 6                            |                         |                               |                            |                           |      |                      |               | 9.13                           | 52.78                | 1.65              | 15.08                |                              |                      | 15.08             | 9.13                         | 52.78                | 1.65              | 15.08              |
|              |                              | OF-3                    |                               |                            | 18.51                     | 0.09 | 37.76                | 3.41          | 1.67                           | 37.76                | 2.05              | 14.40                |                              |                      |                   | 1.67                         | 37.76                | 2.05              | 14.40              |
|              |                              | EX-2                    |                               |                            | 15.87                     | 0.09 | 52.78                | 2.36          | 1.43                           | 52.78                | 1.65              | 15.08                |                              |                      |                   | 1.43                         | 52.78                | 1.65              | 15.08              |
|              |                              | EX-4                    |                               |                            | 52.09                     | 0.09 | 59.93                | 7.11          | 4.69                           | 59.93                | 1.52              | 14.79                |                              |                      |                   | 4.69                         | 59.93                | 1.52              | 14.79              |
|              |                              | OF-4                    |                               |                            | 0.96                      | 0.09 | 34.99                | 0.19          | 0.09                           | 34.99                | 2.15              | 14.00                |                              |                      |                   | 0.09                         | 34.99                | 2.15              | 14.00              |
|              |                              | OF-5                    |                               |                            | 6.21                      | 0.30 | 54.52                | 3.01          | 1.86                           | 54.52                | 1.62              | 15.07                |                              |                      |                   | 1.86                         | 54.52                | 1.62              | 15.07              |
|              |                              | OP-1                    |                               |                            | 0.04                      | 0.34 | 5.00                 | 0.07          | 0.01                           | 5.00                 | 5.09              | 4.80                 |                              |                      |                   | 0.01                         | 5.00                 | 5.09              | 4.80               |
| EX3          | 2                            |                         |                               |                            |                           |      |                      |               | 31.14                          | 133.82               | 0.86              | 26.80                |                              |                      | 26.80             | 31.14                        | 133.82               | 0.86              | 26.80              |
|              |                              | OF-2                    |                               |                            | 290.54                    | 0.10 | 133.82               | 25.46         | 29.58                          | 133.82               | 0.86              | 26.80                |                              |                      |                   | 29.58                        | 133.82               | 0.86              | 26.80              |
|              |                              | EX-3                    |                               |                            | 17.35                     | 0.09 | 45.94                | 2.82          | 1.56                           | 45.94                | 1.81              | 21.18                |                              |                      |                   | 1.56                         | 45.94                | 1.81              | 21.18              |
| EX5          | 1                            |                         |                               |                            |                           |      |                      |               | 3.26                           | 47.83                | 1.76              | 5.74                 |                              |                      | 5.74              | 3.26                         | 47.83                | 1.76              | 5.74               |
|              |                              | EX-5                    |                               |                            | 36.19                     | 0.09 | 47.83                | 5.74          | 3.26                           | 47.83                | 1.76              | 5.74                 |                              |                      |                   | 3.26                         | 47.83                | 1.76              | 5.74               |
|              |                              |                         |                               |                            |                           |      |                      |               |                                |                      |                   |                      |                              |                      |                   |                              |                      |                   |                    |
|              |                              |                         |                               |                            |                           |      |                      |               |                                |                      |                   |                      |                              |                      |                   |                              |                      |                   |                    |
|              |                              |                         |                               |                            |                           |      |                      |               |                                |                      |                   |                      |                              |                      |                   |                              |                      |                   |                    |
|              |                              |                         |                               |                            |                           |      |                      |               |                                |                      |                   |                      |                              |                      |                   |                              |                      |                   |                    |
|              |                              |                         |                               |                            |                           |      |                      |               |                                |                      |                   |                      |                              |                      |                   |                              |                      |                   |                    |

Combined Peak Runoff Calculations for Inlets and Storm Drains

Designer: DJS

Company: Kimley-Horn

Date: 7/29/2026

Project: Trinity Ranch Estates

Location: El Paso County, Colorado

MHFD-Rational, Version 3.00 (August 2025)

100-yr

Design Storm Return Period (Note: this worksheet can only evaluate one design storm at a time)

| Use 1 column (C, D, E) per row |                              |                         |                               |                            |                           |      |                      |               |                                | Obtain Inlet Capacity from MHFD-Inlet (Optional) |                   |                      |                              |                      |                   |                              |                      |                   |                    |
|--------------------------------|------------------------------|-------------------------|-------------------------------|----------------------------|---------------------------|------|----------------------|---------------|--------------------------------|--------------------------------------------------|-------------------|----------------------|------------------------------|----------------------|-------------------|------------------------------|----------------------|-------------------|--------------------|
| Design Point                   | # of Upstream Runoff Sources | Local Subcatchment Name | Upstream Surface Design Point | Upstream Pipe Design Point | Local Subcatchment Runoff |      |                      |               | Surface Runoff to Design Point |                                                  |                   |                      | Inlet Capacity / Bypass Flow |                      |                   | Total Runoff to Design Point |                      |                   |                    |
|                                |                              |                         |                               |                            | Area (ac)                 | C    | t <sub>c</sub> (min) | Local Q (cfs) | Σ(C*A) (acre)                  | t <sub>c</sub> (min)                             | Intensity (in/hr) | Surface Runoff (cfs) | (Optional) Inlet Name        | Inlet Capacity (cfs) | Bypass Flow (cfs) | Σ(C*A) (acre)                | t <sub>c</sub> (min) | Intensity (in/hr) | Total Runoff (cfs) |
| EX1                            | 2                            |                         |                               |                            |                           |      |                      |               | 81.02                          | 127.43                                           | 1.50              | 121.43               |                              |                      |                   |                              |                      |                   |                    |
|                                |                              | EX-1                    |                               |                            | 16.42                     | 0.36 | 55.25                | 15.90         | 5.91                           | 55.25                                            | 2.69              | 103.56               |                              |                      | 121.43            | 81.02                        | 127.43               | 1.50              | 121.43             |
|                                |                              | OF-1                    |                               |                            | 204.29                    | 0.37 | 127.43               | 112.58        | 75.11                          | 127.43                                           | 1.50              | 121.43               |                              |                      |                   | 5.91                         | 55.25                | 2.69              | 103.56             |
| EX4                            | 6                            |                         |                               |                            |                           |      |                      |               | 32.32                          | 52.78                                            | 2.77              | 89.65                |                              |                      | 89.65             | 32.32                        | 52.78                | 2.77              | 89.65              |
|                                |                              | OF-3                    |                               |                            | 18.51                     | 0.36 | 37.76                | 22.92         | 6.66                           | 37.76                                            | 3.44              | 86.40                |                              |                      |                   | 6.66                         | 37.76                | 3.44              | 86.40              |
|                                |                              | EX-2                    |                               |                            | 15.87                     | 0.36 | 52.78                | 15.85         | 5.71                           | 52.78                                            | 2.77              | 89.65                |                              |                      |                   | 5.71                         | 52.78                | 2.77              | 89.65              |
|                                |                              | EX-4                    |                               |                            | 52.09                     | 0.36 | 59.93                | 47.80         | 18.75                          | 59.93                                            | 2.55              | 88.32                |                              |                      |                   | 18.75                        | 59.93                | 2.55              | 88.32              |
|                                |                              | OF-4                    |                               |                            | 0.96                      | 0.36 | 34.99                | 1.25          | 0.35                           | 34.99                                            | 3.60              | 84.01                |                              |                      |                   | 0.35                         | 34.99                | 3.60              | 84.01              |
|                                |                              | OF-5                    |                               |                            | 6.21                      | 0.51 | 54.52                | 8.56          | 3.15                           | 54.52                                            | 2.72              | 89.50                |                              |                      |                   | 3.15                         | 54.52                | 2.72              | 89.50              |
|                                |                              | OP-1                    |                               |                            | 0.04                      | 0.53 | 5.00                 | 0.18          | 0.02                           | 5.00                                             | 8.55              | 28.62                |                              |                      |                   | 0.02                         | 5.00                 | 8.55              | 28.62              |
| EX3                            | 2                            |                         |                               |                            |                           |      |                      |               | 113.18                         | 133.82                                           | 1.45              | 163.68               |                              |                      | 163.68            | 113.18                       | 133.82               | 1.45              | 163.68             |
|                                |                              | OF-2                    |                               |                            | 290.54                    | 0.37 | 133.82               | 154.64        | 106.94                         | 133.82                                           | 1.45              | 163.68               |                              |                      |                   | 106.94                       | 133.82               | 1.45              | 163.68             |
|                                |                              | EX-3                    |                               |                            | 17.35                     | 0.36 | 45.94                | 18.98         | 6.25                           | 45.94                                            | 3.04              | 130.49               |                              |                      |                   | 6.25                         | 45.94                | 3.04              | 130.49             |
| EX5                            | 1                            |                         |                               |                            |                           |      |                      |               | 13.03                          | 47.83                                            | 2.96              | 38.56                |                              |                      | 38.56             | 13.03                        | 47.83                | 2.96              | 38.56              |
|                                |                              | EX-5                    |                               |                            | 36.19                     | 0.36 | 47.83                | 38.56         | 13.03                          | 47.83                                            | 2.96              | 38.56                |                              |                      |                   | 13.03                        | 47.83                | 2.96              | 38.56              |
|                                |                              |                         |                               |                            |                           |      |                      |               |                                |                                                  |                   |                      |                              |                      |                   |                              |                      |                   |                    |
|                                |                              |                         |                               |                            |                           |      |                      |               |                                |                                                  |                   |                      |                              |                      |                   |                              |                      |                   |                    |
|                                |                              |                         |                               |                            |                           |      |                      |               |                                |                                                  |                   |                      |                              |                      |                   |                              |                      |                   |                    |
|                                |                              |                         |                               |                            |                           |      |                      |               |                                |                                                  |                   |                      |                              |                      |                   |                              |                      |                   |                    |
|                                |                              |                         |                               |                            |                           |      |                      |               |                                |                                                  |                   |                      |                              |                      |                   |                              |                      |                   |                    |
|                                |                              |                         |                               |                            |                           |      |                      |               |                                |                                                  |                   |                      |                              |                      |                   |                              |                      |                   |                    |
|                                |                              |                         |                               |                            |                           |      |                      |               |                                |                                                  |                   |                      |                              |                      |                   |                              |                      |                   |                    |
|                                |                              |                         |                               |                            |                           |      |                      |               |                                |                                                  |                   |                      |                              |                      |                   |                              |                      |                   |                    |
|                                |                              |                         |                               |                            |                           |      |                      |               |                                |                                                  |                   |                      |                              |                      |                   |                              |                      |                   |                    |
|                                |                              |                         |                               |                            |                           |      |                      |               |                                |                                                  |                   |                      |                              |                      |                   |                              |                      |                   |                    |
|                                |                              |                         |                               |                            |                           |      |                      |               |                                |                                                  |                   |                      |                              |                      |                   |                              |                      |                   |                    |
|                                |                              |                         |                               |                            |                           |      |                      |               |                                |                                                  |                   |                      |                              |                      |                   |                              |                      |                   |                    |
|                                |                              |                         |                               |                            |                           |      |                      |               |                                |                                                  |                   |                      |                              |                      |                   |                              |                      |                   |                    |
|                                |                              |                         |                               |                            |                           |      |                      |               |                                |                                                  |                   |                      |                              |                      |                   |                              |                      |                   |                    |
|                                |                              |                         |                               |                            |                           |      |                      |               |                                |                                                  |                   |                      |                              |                      |                   |                              |                      |                   |                    |
|                                |                              |                         |                               |                            |                           |      |                      |               |                                |                                                  |                   |                      |                              |                      |                   |                              |                      |                   |                    |
|                                |                              |                         |                               |                            |                           |      |                      |               |                                |                                                  |                   |                      |                              |                      |                   |                              |                      |                   |                    |
|                                |                              |                         |                               |                            |                           |      |                      |               |                                |                                                  |                   |                      |                              |                      |                   |                              |                      |                   |                    |
|                                |                              |                         |                               |                            |                           |      |                      |               |                                |                                                  |                   |                      |                              |                      |                   |                              |                      |                   |                    |
|                                |                              |                         |                               |                            |                           |      |                      |               |                                |                                                  |                   |                      |                              |                      |                   |                              |                      |                   |                    |
|                                |                              |                         |                               |                            |                           |      |                      |               |                                |                                                  |                   |                      |                              |                      |                   |                              |                      |                   |                    |
|                                |                              |                         |                               |                            |                           |      |                      |               |                                |                                                  |                   |                      |                              |                      |                   |                              |                      |                   |                    |
|                                |                              |                         |                               |                            |                           |      |                      |               |                                |                                                  |                   |                      |                              |                      |                   |                              |                      |                   |                    |
|                                |                              |                         |                               |                            |                           |      |                      |               |                                |                                                  |                   |                      |                              |                      |                   |                              |                      |                   |                    |
|                                |                              |                         |                               |                            |                           |      |                      |               |                                |                                                  |                   |                      |                              |                      |                   |                              |                      |                   |                    |
|                                |                              |                         |                               |                            |                           |      |                      |               |                                |                                                  |                   |                      |                              |                      |                   |                              |                      |                   |                    |
|                                |                              |                         |                               |                            |                           |      |                      |               |                                |                                                  |                   |                      |                              |                      |                   |                              |                      |                   |                    |
|                                |                              |                         |                               |                            |                           |      |                      |               |                                |                                                  |                   |                      |                              |                      |                   |                              |                      |                   |                    |
|                                |                              |                         |                               |                            |                           |      |                      |               |                                |                                                  |                   |                      |                              |                      |                   |                              |                      |                   |                    |
|                                |                              |                         |                               |                            |                           |      |                      |               |                                |                                                  |                   |                      |                              |                      |                   |                              |                      |                   |                    |
|                                |                              |                         |                               |                            |                           |      |                      |               |                                |                                                  |                   |                      |                              |                      |                   |                              |                      |                   |                    |
|                                |                              |                         |                               |                            |                           |      |                      |               |                                |                                                  |                   |                      |                              |                      |                   |                              |                      |                   |                    |
|                                |                              |                         |                               |                            |                           |      |                      |               |                                |                                                  |                   |                      |                              |                      |                   |                              |                      |                   |                    |
|                                |                              |                         |                               |                            |                           |      |                      |               |                                |                                                  |                   |                      |                              |                      |                   |                              |                      |                   |                    |
|                                |                              |                         |                               |                            |                           |      |                      |               |                                |                                                  |                   |                      |                              |                      |                   |                              |                      |                   |                    |
|                                |                              |                         |                               |                            |                           |      |                      |               |                                |                                                  |                   |                      |                              |                      |                   |                              |                      |                   |                    |
|                                |                              |                         |                               |                            |                           |      |                      |               |                                |                                                  |                   |                      |                              |                      |                   |                              |                      |                   |                    |
|                                |                              |                         |                               |                            |                           |      |                      |               |                                |                                                  |                   |                      |                              |                      |                   |                              |                      |                   |                    |
|                                |                              |                         |                               |                            |                           |      |                      |               |                                |                                                  |                   |                      |                              |                      |                   |                              |                      |                   |                    |
|                                |                              |                         |                               |                            |                           |      |                      |               |                                |                                                  |                   |                      |                              |                      |                   |                              |                      |                   |                    |
|                                |                              |                         |                               |                            |                           |      |                      |               |                                |                                                  |                   |                      |                              |                      |                   |                              |                      |                   |                    |
|                                |                              |                         |                               |                            |                           |      |                      |               |                                |                                                  |                   |                      |                              |                      |                   |                              |                      |                   |                    |

**PROPOSED CONDITIONS**

Trinity Ranch

DATE: 7/10/2026

PROJECT NUMBER: 096726003

CALCULATED BY: DJS

CHECKED BY: KRK

**PROPOSED RATIONAL CALCULATIONS SUMMARY**

| SUBCATCHMENT NAME       | DESIGN POINT                    | BASIN AREA (AC)     | IMPERVIOUSNESS (%) | PEAK FLOWS (CFS) |        |
|-------------------------|---------------------------------|---------------------|--------------------|------------------|--------|
|                         |                                 |                     |                    | Q5               | Q100   |
| PR-1                    | PR-1                            | 16.17               | 8.1%               | 4.05             | 21.02  |
| PR-2                    | PR-2                            | 9.55                | 9.9%               | 2.98             | 14.38  |
| PR-3                    | PR-3                            | 17.72               | 8.9%               | 4.98             | 24.98  |
| PR-4                    | PR-4                            | 16.42               | 11.5%              | 5.99             | 27.20  |
| PR-5                    | PR-5                            | 2.08                | 36.6%              | 2.00             | 5.39   |
| PR-6                    | PR-6                            | 17.78               | 10.3%              | 5.49             | 25.99  |
| PR-7                    | PR-7                            | 29.21               | 42.2%              | 25.51            | 68.20  |
| PR-8                    | PR-8                            | 11.31               | 47.6%              | 11.76            | 29.60  |
| PR-9                    | PR-9                            | 17.68               | 40.7%              | 14.37            | 38.97  |
| OF-1                    | OF-1                            | 204.29              | 3.7%               | 18.45            | 112.58 |
| OF-2                    | OF-2                            | 290.54              | 3.8%               | 25.46            | 154.64 |
| OF-3                    | OF-3                            | 18.51               | 2.0%               | 3.41             | 22.92  |
| OF-4                    | OF-4                            | 0.96                | 2.0%               | 0.19             | 1.25   |
| OP-1                    | OP-1                            | 0.04                | 46.0%              | 0.08             | 0.20   |
| OF-5                    | OF-5                            | 6.21                | 30.9%              | 3.01             | 8.56   |
| OF-6                    | OF-6                            | 0.14                | 84.3%              | 0.42             | 0.81   |
| CUMMULATIVE FLOWS       |                                 |                     |                    |                  |        |
| DESIGN POINT            | BASINS                          | TRIBUTARY AREA (AC) | IMPERV. (%)        | Q5               | Q100   |
| PR1                     | PR1+OF1                         | 220.46              | 4.1%               | 20.30            | 122.16 |
| PR3                     | OF2+PR3                         | 308.26              | 4.1%               | 27.50            | 164.88 |
| PR8                     | OF3+OF4+PR2+PR4<br>+PR5+PR7+PR8 | 88.04               | 24.6%              | 49.08            | 155.00 |
| PR9                     | PR6+PR9                         | 35.46               | 25.5%              | 19.19            | 61.78  |
| OF5                     | OF5+OP1                         | 6.25                | 31.0%              | 3.04             | 8.63   |
| OF-6                    | OF-6                            | 0.14                | 84.3%              | 0.42             | 0.81   |
| TOTAL CUMMULATIVE FLOWS |                                 | 658.62              | 8.3%               | 119.53           | 513.26 |

Calculation of Peak Runoff using Rational Method

Designer: DJS  
Company: Kirby-Horn  
Date: 7/25/2025  
Project: Trinity Ranch  
Location: El Paso County, CO

MPFD-Rational, Version 3.00 (August 2025)  
Scale of this color arc for required user input.  
Scale of this color arc for optional override values.

$$t_t = \frac{0.395(L^{1.1} - C_t)L_t}{60K\sqrt{S_x}}$$

Computed  $t_c = t_t + t_r$

$$t_t = \frac{L_t}{60K\sqrt{S_x}} = \frac{L_t}{60\sqrt{S_x}}$$

Regional  $t_c = (25 - 17) + \frac{L_t}{60(141 + 9)\sqrt{S_x}}$

$$t_{c_{minimum}} = 5 \text{ (urban)}$$
$$t_{c_{minimum}} = 10 \text{ (non-urban)}$$

Selected  $t_c = \max(t_{c_{minimum}}, \min(\text{Computed } t_c, \text{Regional } t_c))$

Calculation of Peak Runoff using Rational Method

Select HEC-2 location for NOAA Atlas 14 Rainfall Coefficients from the pdf below (or enter your own coefficients obtained from the NOAA website (click this link)).  
1-hour rainfall depth, P1 (in) = 

WQFE 2-yr 5-yr 10-yr 25-yr 50-yr 100-yr 500-yr

0.69 1.13 1.59 1.75 2.60 3.25 3.53 3.91

Rainfall Intensity Equation Coefficients = 

a 28.56 b 10.00 c 0.786

$$I(in/hr) = \frac{a+b}{b + t_c^c}$$

$$Q(cfs) = CIA$$

Calculation of Peak Runoff using Rational Method

Provide input for area, soil type, and imperviousness on the Runoff Coeffs worksheet

| Subcatchment Name | Area (ac) | NRCS Hydrologic Soil Group(s) | Runoff Coefficient, C |      |       |       |       |        |        |                             | Overland (Initial) Flow Time |                              |                               |                                         |                                             |                              |                              |                                               | Channelized (Travel) Flow Time |                                                   |                                            |                               |                               |                               |                                          |      | Time of Concentration |      |       |       | Rainfall Intensity, I (in/hr) |        |        |      |       |       |       |       | Peak Flow, Q (cfs) |        |        |  |  |  |  |  |
|-------------------|-----------|-------------------------------|-----------------------|------|-------|-------|-------|--------|--------|-----------------------------|------------------------------|------------------------------|-------------------------------|-----------------------------------------|---------------------------------------------|------------------------------|------------------------------|-----------------------------------------------|--------------------------------|---------------------------------------------------|--------------------------------------------|-------------------------------|-------------------------------|-------------------------------|------------------------------------------|------|-----------------------|------|-------|-------|-------------------------------|--------|--------|------|-------|-------|-------|-------|--------------------|--------|--------|--|--|--|--|--|
|                   |           |                               | WQFE & 2-yr           | 5-yr | 10-yr | 25-yr | 50-yr | 100-yr | 500-yr | Overland Flow Length L (ft) | US Elevation (ft) (Optional) | DS Elevation (ft) (Optional) | Overland Flow Slope S (ft/ft) | Overland Flow Time T <sub>o</sub> (min) | Channelized Flow Length L <sub>c</sub> (ft) | US Elevation (ft) (Optional) | DS Elevation (ft) (Optional) | Channelized Flow Slope S <sub>c</sub> (ft/ft) | NRCS Conveyance Factor K       | Channelized Flow Velocity V <sub>c</sub> (ft/sec) | Channelized Flow Time T <sub>c</sub> (min) | Computed L <sub>t</sub> (min) | Regional L <sub>t</sub> (min) | Selected L <sub>t</sub> (min) | (Optional) Override L <sub>t</sub> (min) | WQFE | 2-yr                  | 5-yr | 10-yr | 25-yr | 50-yr                         | 100-yr | 500-yr | WQFE | 2-yr  | 5-yr  | 10-yr | 25-yr | 50-yr              | 100-yr | 500-yr |  |  |  |  |  |
| PR-1              | 16.17     | A                             | 8.1%                  | 0.06 | 0.13  | 0.21  | 0.24  | 0.29   | 0.40   | 0.31                        |                              |                              | 0.020                         | 31.21                                   | 1375.87                                     |                              |                              | 0.020                                         | 2.3                            | 0.36                                              | 64.88                                      | 96.10                         | 45.62                         | 45.62                         |                                          | 0.78 | 1.95                  | 1.99 | 2.28  | 2.61  | 2.93                          | 3.29   | 3.79   | 5.74 | 1.48  | 4.05  | 7.65  | 10.03 | 13.61              | 21.02  | 31.00  |  |  |  |  |  |
| PR-2              | 9.95      | A                             | 9.9%                  | 0.07 | 0.14  | 0.22  | 0.25  | 0.30   | 0.40   | 0.31                        |                              |                              | 0.030                         | 26.94                                   | 990.24                                      |                              |                              | 0.035                                         | 7                              | 0.49                                              | 13.14                                      | 40.08                         | 33.17                         | 33.17                         |                                          | 0.89 | 1.76                  | 2.22 | 2.59  | 2.96  | 3.32                          | 3.72   | 4.30   | 6.62 | 1.22  | 2.88  | 6.41  | 7.03  | 9.46               | 14.39  | 21.10  |  |  |  |  |  |
| PR-3              | 17.12     | A                             | 9.9%                  | 0.06 | 0.13  | 0.21  | 0.24  | 0.29   | 0.40   | 0.31                        |                              |                              | 0.015                         | 34.12                                   | 884.52                                      |                              |                              | 0.015                                         | 7                              | 0.86                                              | 17.20                                      | 51.32                         | 38.24                         | 38.24                         |                                          | 0.94 | 1.67                  | 2.10 | 2.45  | 2.80  | 3.15                          | 3.53   | 4.07   | 6.97 | 1.80  | 4.98  | 9.23  | 12.03 | 16.29              | 24.88  | 36.75  |  |  |  |  |  |
| PR-4              | 16.42     | A                             | 11.5%                 | 0.09 | 0.15  | 0.23  | 0.26  | 0.32   | 0.41   | 0.32                        |                              |                              | 0.030                         | 26.62                                   | 966.64                                      |                              |                              | 0.030                                         | 2.5                            | 0.43                                              | 21.81                                      | 48.43                         | 29.19                         | 29.19                         |                                          | 0.96 | 1.90                  | 2.39 | 2.79  | 3.19  | 3.59                          | 4.02   | 4.64   | 1.34 | 2.65  | 6.99  | 10.50 | 13.98 | 18.12              | 27.20  | 39.71  |  |  |  |  |  |
| PR-5              | 7.08      | A                             | 16.0%                 | 0.20 | 0.34  | 0.39  | 0.40  | 0.46   | 0.61   | 0.44                        |                              |                              | 0.020                         | 4.39                                    | 1224.91                                     |                              |                              | 0.016                                         | 10                             | 1.22                                              | 16.07                                      | 21.06                         | 31.06                         | 31.06                         |                                          | 1.15 | 2.29                  | 2.67 | 3.28  | 3.83  | 4.31                          | 4.80   | 6.07   | 0.66 | 1.34  | 2.00  | 2.79  | 3.96  | 4.16               | 5.39   | 7.41   |  |  |  |  |  |
| PR-6              | 17.78     | A                             | 10.3%                 | 0.08 | 0.14  | 0.22  | 0.25  | 0.30   | 0.41   | 0.32                        |                              |                              | 0.020                         | 28.51                                   | 968.52                                      |                              |                              | 0.020                                         | 2.5                            | 0.35                                              | 45.66                                      | 74.17                         | 35.17                         | 35.17                         |                                          | 0.86 | 1.70                  | 2.14 | 2.50  | 2.88  | 3.21                          | 3.59   | 4.15   | 1.16 | 2.31  | 5.49  | 9.85  | 12.78 | 17.18              | 26.99  | 38.09  |  |  |  |  |  |
| PR-7              | 29.21     | A                             | 42.2%                 | 0.27 | 0.32  | 0.38  | 0.42  | 0.46   | 0.51   | 0.40                        |                              |                              | 0.030                         | 21.82                                   | 731.32                                      |                              |                              | 0.030                                         | 15                             | 2.60                                              | 4.69                                       | 26.52                         | 23.55                         | 23.55                         |                                          | 1.08 | 2.14                  | 2.70 | 3.15  | 3.60  | 4.05                          | 4.54   | 5.24   | 8.57 | 17.03 | 25.51 | 34.89 | 44.24 | 54.24              | 68.20  | 91.15  |  |  |  |  |  |
| PR-8              | 11.31     | A                             | 27.6%                 | 0.31 | 0.36  | 0.41  | 0.45  | 0.49   | 0.54   | 0.52                        |                              |                              | 0.015                         | 26.15                                   | 530.80                                      |                              |                              | 0.040                                         | 15                             | 3.00                                              | 2.95                                       | 29.11                         | 25.73                         | 25.73                         |                                          | 1.15 | 2.35                  | 2.80 | 3.38  | 3.98  | 4.54                          | 4.86   | 5.82   | 4.07 | 8.07  | 11.76 | 15.71 | 19.95 | 24.03              | 29.60  | 36.13  |  |  |  |  |  |
| PR-9              | 17.69     | A                             | 40.7%                 | 0.26 | 0.32  | 0.37  | 0.41  | 0.45   | 0.51   | 0.59                        |                              |                              | 0.015                         | 27.66                                   | 880.89                                      |                              |                              | 0.022                                         | 15                             | 2.22                                              | 6.60                                       | 34.26                         | 25.82                         | 25.82                         |                                          | 1.03 | 2.04                  | 2.57 | 2.99  | 3.42  | 3.85                          | 4.31   | 4.98   | 8.80 | 9.52  | 14.37 | 19.77 | 25.05 | 30.79              | 38.97  | 52.28  |  |  |  |  |  |
| QF-1              | 204.26    | A                             | 3.7%                  | 0.04 | 0.10  | 0.16  | 0.22  | 0.26   | 0.32   | 0.48                        | 6292.32                      | 6279.32                      | 0.020                         | 28.40                                   | 1240.05                                     | 6279.03                      | 6171.06                      | 0.015                                         | 2.5                            | 6.21                                              | 288.70                                     | 418.14                        | 127.45                        | 127.45                        |                                          | 0.36 | 0.70                  | 0.99 | 1.24  | 1.19  | 1.24                          | 1.55   | 1.75   | 3.60 | 6.09  | 14.45 | 28.54 | 45.27 | 67.00              | 112.28 | 169.21 |  |  |  |  |  |
| QF-2              | 200.54    | A                             | 3.8%                  | 0.04 | 0.10  | 0.16  | 0.22  | 0.26   | 0.32   | 0.48                        | 6296.17                      | 6266.17                      | 0.020                         | 23.35                                   | 7341.73                                     | 6260.18                      | 6157.40                      | 0.014                                         | 2.5                            | 0.30                                              | 413.66                                     | 437.05                        | 133.82                        | 133.82                        |                                          | 0.34 | 0.65                  | 0.96 | 1.00  | 1.15  | 1.29                          | 1.46   | 1.67   | 4.27 | 6.48  | 25.46 | 42.76 | 69.85 | 116.59             | 154.64 | 232.41 |  |  |  |  |  |
| QF-3              | 18.51     | A                             | 2.0%                  | 0.03 | 0.09  | 0.17  | 0.26  | 0.31   | 0.36   | 0.47                        | 210.00                       |                              | 0.008                         | 32.25                                   | 1088.50                                     |                              |                              | 0.026                                         | 2.5                            | 0.40                                              | 44.82                                      | 77.18                         | 37.76                         | 37.76                         |                                          | 0.82 | 1.62                  | 2.05 | 2.59  | 2.73  | 3.07                          | 3.44   | 3.97   | 0.45 | 0.90  | 2.41  | 7.52  | 13.14 | 17.62              | 22.92  | 34.55  |  |  |  |  |  |
| QF-4              | 15.96     | A                             | 2.0%                  | 0.03 | 0.09  | 0.17  | 0.26  | 0.31   | 0.36   | 0.47                        | 238.00                       |                              | 0.008                         | 33.37                                   | 493.09                                      |                              |                              | 0.009                                         | 2.5                            | 0.24                                              | 84.64                                      | 68.01                         | 34.99                         | 34.99                         |                                          | 0.86 | 1.70                  | 2.15 | 2.50  | 2.88  | 3.22                          | 3.60   | 4.16   | 0.02 | 0.05  | 0.10  | 0.41  | 0.71  | 0.96               | 1.25   | 1.98   |  |  |  |  |  |
| QF-1              | 0.04      | A                             | 46.0%                 | 0.37 | 0.41  | 0.46  | 0.52  | 0.56   | 0.59   | 0.69                        | 16.00                        |                              | 0.020                         | 3.96                                    | 30.00                                       |                              |                              | 0.020                                         | 30                             | 2.90                                              | 0.25                                       | 4.21                          | 16.50                         | 5.00                          |                                          | 2.04 | 4.54                  | 5.09 | 5.94  | 6.78  | 7.63                          | 8.50   | 9.87   | 0.03 | 0.06  | 0.08  | 0.11  | 0.14  | 0.17               | 0.20   | 0.27   |  |  |  |  |  |
| QF-5              | 0.01      | A                             | 49.9%                 | 0.25 | 0.26  | 0.26  | 0.45  | 0.47   | 0.51   | 0.61                        | 40.00                        |                              | 0.020                         | 5.14                                    | 4444.00                                     |                              |                              | 0.020                                         | 15                             | 1.29                                              | 49.39                                      | 54.03                         | 76.35                         | 54.03                         |                                          | 0.65 | 1.29                  | 1.42 | 1.49  | 2.16  | 2.42                          | 2.77   | 3.14   | 1.00 | 0.60  | 1.01  | 1.25  | 1.77  | 1.69               | 8.50   | 11.84  |  |  |  |  |  |
| QF-6              | 0.14      | A                             | 84.3%                 | 0.63 | 0.65  | 0.68  | 0.71  | 0.73   | 0.75   | 0.87                        | 116.00                       |                              | 0.020                         | 6.95                                    | 1.00                                        |                              |                              | 0.010                                         | 20                             | 2.00                                              | 0.01                                       | 6.97                          | 11.68                         | 6.97                          |                                          | 1.85 | 3.65                  | 4.62 | 5.59  | 6.16  | 6.93                          | 7.76   | 8.96   | 0.16 | 0.32  | 0.42  | 0.51  | 0.61  | 0.71               | 0.81   | 1.00   |  |  |  |  |  |

Proposed Rational Calc., Trinity Ranch, Rational Calc.

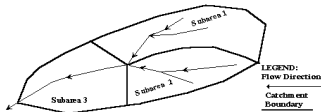
7/25/2025, 10:39 AM

Determination of Runoff Coefficients for Rational Method

MHFD-Rational, Version 3.00 (August 2025)

Designer: DJS  
Company: Kimley-Horn  
Date: 7/29/2026  
Project: Trinity Ranch  
Location: El Paso County, CO

Cells of this color are for required user-input  
Cells of this color are for optional override values



| Provide subcatchment names on the Rational Calcs worksheet to open up the table below. |               |           |                            |                        |                             |                           |                                    |                       |      |       |       |       |        |        |                                           |      |       |       |       |        |        |          |
|----------------------------------------------------------------------------------------|---------------|-----------|----------------------------|------------------------|-----------------------------|---------------------------|------------------------------------|-----------------------|------|-------|-------|-------|--------|--------|-------------------------------------------|------|-------|-------|-------|--------|--------|----------|
| Subcatchment Name                                                                      | # of Subareas | Area (ac) | NRCS Hydrologic Soil Group | Percent Imperviousness |                             |                           |                                    | Runoff Coefficient, C |      |       |       |       |        |        | (Optional) Override Runoff Coefficient, C |      |       |       |       |        |        | Comments |
|                                                                                        |               |           |                            | Imperviousness Source  | Imperviousness Category     | Calculated Imperviousness | (Optional) Override Imperviousness | WQFE & 2-yr           | 5-yr | 10-yr | 25-yr | 50-yr | 100-yr | 500-yr | WQFE & 2-yr                               | 5-yr | 10-yr | 25-yr | 50-yr | 100-yr | 500-yr |          |
| PR-1                                                                                   | 3             | 16.17     | A                          |                        |                             | 35.8 %                    | 8.1 %                              | 0.04                  | 0.04 | 0.04  | 0.05  | 0.09  | 0.17   | 0.31   | 0.06                                      | 0.13 | 0.21  | 0.24  | 0.29  | 0.40   | 0.51   |          |
|                                                                                        |               | 0.20      | A                          | Surface Type           | Roadways and Paved Streets  | 95%                       | 90%                                | 0.73                  | 0.75 | 0.77  | 0.79  | 0.79  | 0.81   | 0.83   | 0.71                                      | 0.73 | 0.75  | 0.78  | 0.80  | 0.81   | 0.89   |          |
|                                                                                        |               | 0.02      | A                          | Surface Type           | Gravel - High Traffic Areas | 80%                       |                                    | 0.63                  | 0.65 | 0.66  | 0.69  | 0.71  | 0.73   | 0.77   | 0.57                                      | 0.59 | 0.63  | 0.66  | 0.68  | 0.70   | 0.86   |          |
|                                                                                        |               | 15.95     | A                          | Land Use               | Single-Family - Rural       | 35%                       | 7%                                 | 0.03                  | 0.03 | 0.03  | 0.04  | 0.08  | 0.16   | 0.30   | 0.05                                      | 0.12 | 0.20  | 0.23  | 0.28  | 0.39   | 0.50   |          |
| PR-2                                                                                   | 3             | 9.55      | A                          |                        |                             | 37.1 %                    | 9.9 %                              | 0.05                  | 0.05 | 0.06  | 0.07  | 0.11  | 0.19   | 0.32   | 0.07                                      | 0.14 | 0.22  | 0.25  | 0.30  | 0.40   | 0.51   |          |
|                                                                                        |               | 0.29      | A                          | Surface Type           | Roadways and Paved Streets  | 95%                       | 90%                                | 0.73                  | 0.75 | 0.77  | 0.79  | 0.79  | 0.81   | 0.83   | 0.71                                      | 0.73 | 0.75  | 0.78  | 0.80  | 0.81   | 0.89   |          |
|                                                                                        |               | 0.05      | A                          | Surface Type           | Gravel - High Traffic Areas | 80%                       |                                    | 0.63                  | 0.65 | 0.66  | 0.69  | 0.71  | 0.73   | 0.77   | 0.57                                      | 0.59 | 0.63  | 0.66  | 0.68  | 0.70   | 0.86   |          |
|                                                                                        |               | 9.21      | A                          | Land Use               | Single-Family - Rural       | 35%                       | 7%                                 | 0.03                  | 0.03 | 0.03  | 0.04  | 0.08  | 0.16   | 0.30   | 0.05                                      | 0.12 | 0.20  | 0.23  | 0.28  | 0.39   | 0.50   |          |
| PR-3                                                                                   | 3             | 17.72     | A                          |                        |                             | 36.4 %                    | 8.9 %                              | 0.04                  | 0.05 | 0.05  | 0.06  | 0.10  | 0.18   | 0.31   | 0.06                                      | 0.13 | 0.21  | 0.24  | 0.29  | 0.40   | 0.51   |          |
|                                                                                        |               | 0.37      | A                          | Surface Type           | Roadways and Paved Streets  | 95%                       | 90%                                | 0.73                  | 0.75 | 0.77  | 0.79  | 0.79  | 0.81   | 0.83   | 0.71                                      | 0.73 | 0.75  | 0.78  | 0.80  | 0.81   | 0.89   |          |
|                                                                                        |               | 0.04      | A                          | Surface Type           | Gravel - High Traffic Areas | 80%                       |                                    | 0.63                  | 0.65 | 0.66  | 0.69  | 0.71  | 0.73   | 0.77   | 0.57                                      | 0.59 | 0.63  | 0.66  | 0.68  | 0.70   | 0.86   |          |
|                                                                                        |               | 17.31     | A                          | Land Use               | Single-Family - Rural       | 35%                       | 7%                                 | 0.03                  | 0.03 | 0.03  | 0.04  | 0.08  | 0.16   | 0.30   | 0.05                                      | 0.12 | 0.20  | 0.23  | 0.28  | 0.39   | 0.50   |          |
| PR-4                                                                                   | 3             | 16.42     | A                          |                        |                             | 38.2 %                    | 11.5 %                             | 0.06                  | 0.07 | 0.07  | 0.08  | 0.12  | 0.20   | 0.33   | 0.09                                      | 0.15 | 0.23  | 0.26  | 0.31  | 0.41   | 0.52   |          |
|                                                                                        |               | 0.78      | A                          | Surface Type           | Roadways and Paved Streets  | 95%                       | 90%                                | 0.73                  | 0.75 | 0.77  | 0.79  | 0.79  | 0.81   | 0.83   | 0.71                                      | 0.73 | 0.75  | 0.78  | 0.80  | 0.81   | 0.89   |          |
|                                                                                        |               | 0.12      | A                          | Surface Type           | Gravel - High Traffic Areas | 80%                       |                                    | 0.63                  | 0.65 | 0.66  | 0.69  | 0.71  | 0.73   | 0.77   | 0.57                                      | 0.59 | 0.63  | 0.66  | 0.68  | 0.70   | 0.86   |          |
|                                                                                        |               | 15.52     | A                          | Land Use               | Single-Family - Rural       | 35%                       | 7%                                 | 0.03                  | 0.03 | 0.03  | 0.04  | 0.08  | 0.16   | 0.30   | 0.05                                      | 0.12 | 0.20  | 0.23  | 0.28  | 0.39   | 0.50   |          |
| PR-5                                                                                   | 3             | 2.08      | A                          |                        |                             | 56.1 %                    | 36.6 %                             | 0.28                  | 0.29 | 0.29  | 0.31  | 0.34  | 0.40   | 0.49   | 0.28                                      | 0.34 | 0.39  | 0.42  | 0.46  | 0.54   | 0.64   |          |
|                                                                                        |               | 0.68      | A                          | Surface Type           | Roadways and Paved Streets  | 95%                       | 90%                                | 0.73                  | 0.75 | 0.77  | 0.79  | 0.79  | 0.81   | 0.83   | 0.71                                      | 0.73 | 0.75  | 0.78  | 0.80  | 0.81   | 0.89   |          |
|                                                                                        |               | 0.07      | A                          | Surface Type           | Gravel - High Traffic Areas | 80%                       |                                    | 0.63                  | 0.65 | 0.66  | 0.69  | 0.71  | 0.73   | 0.77   | 0.57                                      | 0.59 | 0.63  | 0.66  | 0.68  | 0.70   | 0.86   |          |
|                                                                                        |               | 1.33      | A                          | Land Use               | Single-Family - Rural       | 35%                       | 7%                                 | 0.03                  | 0.03 | 0.03  | 0.04  | 0.08  | 0.16   | 0.30   | 0.05                                      | 0.12 | 0.20  | 0.23  | 0.28  | 0.39   | 0.50   |          |
| PR-6                                                                                   | 3             | 17.78     | A                          |                        |                             | 37.4 %                    | 10.3 %                             | 0.05                  | 0.06 | 0.06  | 0.07  | 0.11  | 0.19   | 0.32   | 0.08                                      | 0.14 | 0.22  | 0.25  | 0.30  | 0.41   | 0.52   |          |
|                                                                                        |               | 0.68      | A                          | Surface Type           | Roadways and Paved Streets  | 95%                       | 90%                                | 0.73                  | 0.75 | 0.77  | 0.79  | 0.79  | 0.81   | 0.83   | 0.71                                      | 0.73 | 0.75  | 0.78  | 0.80  | 0.81   | 0.89   |          |
|                                                                                        |               | 0.04      | A                          | Surface Type           | Gravel - High Traffic Areas | 80%                       |                                    | 0.63                  | 0.65 | 0.66  | 0.69  | 0.71  | 0.73   | 0.77   | 0.57                                      | 0.59 | 0.63  | 0.66  | 0.68  | 0.70   | 0.86   |          |
|                                                                                        |               | 17.06     | A                          | Land Use               | Single-Family - Rural       | 35%                       | 7%                                 | 0.03                  | 0.03 | 0.03  | 0.04  | 0.08  | 0.16   | 0.30   | 0.05                                      | 0.12 | 0.20  | 0.23  | 0.28  | 0.39   | 0.50   |          |
| PR-7                                                                                   | 4             | 29.21     | A                          |                        |                             | 53.6 %                    | 42.2 %                             | 0.30                  | 0.31 | 0.33  | 0.35  | 0.39  | 0.44   | 0.53   | 0.27                                      | 0.32 | 0.38  | 0.42  | 0.46  | 0.51   | 0.60   |          |
|                                                                                        |               | 0.63      | A                          | Surface Type           | Roadways and Paved Streets  | 95%                       | 90%                                | 0.73                  | 0.75 | 0.77  | 0.79  | 0.79  | 0.81   | 0.83   | 0.71                                      | 0.73 | 0.75  | 0.78  | 0.80  | 0.81   | 0.89   |          |
|                                                                                        |               | 0.10      | A                          | Surface Type           | Gravel - High Traffic Areas | 80%                       |                                    | 0.63                  | 0.65 | 0.66  | 0.69  | 0.71  | 0.73   | 0.77   | 0.57                                      | 0.59 | 0.63  | 0.66  | 0.68  | 0.70   | 0.86   |          |
|                                                                                        |               | 11.80     | A                          | Land Use               | Single-Family - Rural       | 35%                       | 7%                                 | 0.03                  | 0.03 | 0.03  | 0.04  | 0.08  | 0.16   | 0.30   | 0.05                                      | 0.12 | 0.20  | 0.23  | 0.28  | 0.39   | 0.50   |          |
| PR-8                                                                                   | 4             | 16.68     | A                          | Land Use               | Commercial - Low Density    | 65%                       |                                    | 0.48                  | 0.50 | 0.51  | 0.54  | 0.58  | 0.62   | 0.67   | 0.41                                      | 0.45 | 0.49  | 0.54  | 0.57  | 0.59   | 0.65   |          |
|                                                                                        |               | 11.31     | A                          |                        |                             | 57.0 %                    | 47.6 %                             | 0.35                  | 0.36 | 0.37  | 0.40  | 0.43  | 0.48   | 0.56   | 0.31                                      | 0.36 | 0.41  | 0.45  | 0.49  | 0.54   | 0.62   |          |
|                                                                                        |               | 0.64      | A                          | Surface Type           | Roadways and Paved Streets  | 95%                       | 90%                                | 0.73                  | 0.75 | 0.77  | 0.79  | 0.79  | 0.81   | 0.83   | 0.71                                      | 0.73 | 0.75  | 0.78  | 0.80  | 0.81   | 0.89   |          |
|                                                                                        |               | 0.06      | A                          | Surface Type           | Gravel - High Traffic Areas | 80%                       |                                    | 0.63                  | 0.65 | 0.66  | 0.69  | 0.71  | 0.73   | 0.77   | 0.57                                      | 0.59 | 0.63  | 0.66  | 0.68  | 0.70   | 0.86   |          |
| PR-9                                                                                   | 4             | 3.68      | A                          | Land Use               | Single-Family - Rural       | 35%                       | 7%                                 | 0.03                  | 0.03 | 0.03  | 0.04  | 0.08  | 0.16   | 0.30   | 0.05                                      | 0.12 | 0.20  | 0.23  | 0.28  | 0.39   | 0.50   |          |
|                                                                                        |               | 6.93      | A                          | Land Use               | Commercial - Low Density    | 65%                       |                                    | 0.48                  | 0.50 | 0.51  | 0.54  | 0.58  | 0.62   | 0.67   | 0.41                                      | 0.45 | 0.49  | 0.54  | 0.57  | 0.59   | 0.65   |          |
|                                                                                        |               | 17.68     | A                          |                        |                             | 53.1 %                    | 40.7 %                             | 0.29                  | 0.30 | 0.31  | 0.34  | 0.37  | 0.43   | 0.52   | 0.26                                      | 0.32 | 0.37  | 0.41  | 0.45  | 0.51   | 0.59   |          |
|                                                                                        |               | 0.64      | A                          | Surface Type           | Roadways and Paved Streets  | 95%                       | 90%                                | 0.73                  | 0.75 | 0.77  | 0.79  | 0.79  | 0.81   | 0.83   | 0.71                                      | 0.73 | 0.75  | 0.78  | 0.80  | 0.81   | 0.89   |          |
| OF-1                                                                                   | 3             | 0.04      | A                          | Surface Type           | Gravel - High Traffic Areas | 80%                       |                                    | 0.63                  | 0.65 | 0.66  | 0.69  | 0.71  | 0.73   | 0.77   | 0.57                                      | 0.59 | 0.63  | 0.66  | 0.68  | 0.70   | 0.86   |          |
|                                                                                        |               | 3.94      | A                          | Surface Type           | Roofs                       | 95%                       | 90%                                | 0.73                  | 0.75 | 0.77  | 0.79  | 0.79  | 0.81   | 0.83   | 0.71                                      | 0.73 | 0.75  | 0.78  | 0.80  | 0.81   | 0.89   |          |
|                                                                                        |               | 0.51      | A                          | Surface Type           | Historic Flow Analysis      | 5%                        | 2%                                 | 0.01                  | 0.01 | 0.01  | 0.01  | 0.04  | 0.13   | 0.27   | 0.03                                      | 0.09 | 0.17  | 0.26  | 0.31  | 0.36   | 0.47   |          |
|                                                                                        |               | 199.84    | A                          |                        |                             | 6.8 %                     | 3.8 %                              | 0.02                  | 0.02 | 0.02  | 0.03  | 0.06  | 0.14   | 0.28   | 0.04                                      | 0.10 | 0.18  | 0.27  | 0.32  | 0.37   | 0.48   |          |
| OF-2                                                                                   | 3             | 290.54    | A                          |                        |                             | 80%                       |                                    | 0.63                  | 0.65 | 0.66  | 0.69  | 0.71  | 0.73   | 0.77   | 0.57                                      | 0.59 | 0.63  | 0.66  | 0.68  | 0.70   | 0.86   |          |
|                                                                                        |               | 6.01      | A                          | Surface Type           | Roofs                       | 95%                       | 90%                                | 0.73                  | 0.75 | 0.77  | 0.79  | 0.79  | 0.81   | 0.83   | 0.71                                      | 0.73 | 0.75  | 0.78  | 0.80  | 0.81   | 0.89   |          |
|                                                                                        |               | 0.66      | A                          | Surface Type           | Historic Flow Analysis      | 5%                        | 2%                                 | 0.01                  | 0.01 | 0.01  | 0.01  | 0.04  | 0.13   | 0.27   | 0.03                                      | 0.09 | 0.17  | 0.26  | 0.31  | 0.36   | 0.47   |          |
|                                                                                        |               | 283.87    | A                          |                        |                             | 5.0 %                     | 2.0 %                              | 0.01                  | 0.01 | 0.01  | 0.01  | 0.04  | 0.13   | 0.27   | 0.03                                      | 0.09 | 0.17  | 0.26  | 0.31  | 0.36   | 0.47   |          |
| OF-3                                                                                   | 1             | 18.51     | A                          |                        |                             | 5.0 %                     | 2.0 %                              | 0.01                  | 0.01 | 0.01  | 0.01  | 0.04  | 0.13   | 0.27   | 0.03                                      | 0.09 | 0.17  | 0.26  | 0.31  | 0.36   | 0.47   |          |
|                                                                                        |               | 0.96      | A                          | Surface Type           | Historic Flow Analysis      | 5%                        | 2%                                 | 0.01                  | 0.01 | 0.01  | 0.01  | 0.04  | 0.13   | 0.27   | 0.03                                      | 0.09 | 0.17  | 0.26  | 0.31  | 0.36   | 0.47   |          |
|                                                                                        |               | 0.96      | A                          |                        |                             | 5.0 %                     | 2.0 %                              | 0.01                  | 0.01 | 0.01  | 0.01  | 0.04  | 0.13   | 0.27   | 0.03                                      | 0.09 | 0.17  | 0.26  | 0.31  | 0.36   | 0.47   |          |
|                                                                                        |               | 0.04      | A                          | Surface Type           | Historic Flow Analysis      | 5%                        | 2%                                 | 0.01                  | 0.01 | 0.01  | 0.01  | 0.04  | 0.13   | 0.27   | 0.03                                      | 0.09 | 0.17  | 0.26  | 0.31  | 0.36   | 0.47   |          |
| OP-1                                                                                   | 2             | 0.02      | A                          |                        |                             | 50.0 %                    | 46.0 %                             | 0.37                  | 0.38 | 0.39  | 0.40  | 0.42  | 0.47   | 0.55   | 0.37                                      | 0.41 | 0.46  | 0.52  | 0.56  | 0.59   | 0.68   |          |
|                                                                                        |               | 0.02      | A                          | Surface Type           | Roadways and Paved Streets  | 95%                       | 90%                                | 0.73                  | 0.75 | 0.77  | 0.79  | 0.79  | 0.81   | 0.83   | 0.71                                      | 0.73 | 0.75  | 0.78  | 0.80  | 0.81   | 0.89   |          |
|                                                                                        |               | 0.02      | A                          | Surface Type           | Historic Flow Analysis      | 5%                        | 2%                                 | 0.01                  | 0.01 | 0.01  | 0.01  | 0.04  | 0.13   | 0.27   | 0.03                                      | 0.09 | 0.17  | 0.26  | 0.31  | 0.36   | 0.47   |          |
|                                                                                        |               | 6.21      | A                          |                        |                             | 34.6 %                    | 30.9 %                             | 0.24                  | 0.25 | 0.26  | 0.27  | 0.29  | 0.35   | 0.45   | 0.25                                      | 0.30 | 0.36  | 0.43  | 0.47  | 0.51   | 0.61   |          |
| OF-5                                                                                   | 2             | 2.04      | A                          | Surface Type           | Roadways and Paved Streets  | 95%                       | 90%                                | 0.73                  | 0.75 | 0.77  | 0.79  | 0.79  | 0.81   | 0.83   | 0.71                                      | 0.73 | 0.75  | 0.78  | 0.80  | 0.81   | 0.89   |          |
|                                                                                        |               | 4.17      | A                          | Surface Type           | Historic Flow Analysis      | 5%                        | 2%                                 | 0.01                  | 0.01 | 0.01  | 0.01  | 0.04  | 0.13   | 0.27   | 0.03                                      | 0.09 | 0.17  | 0.26  | 0.31  | 0.36   | 0.47   |          |
|                                                                                        |               | 0.14      | A                          |                        |                             | 86.4 %                    | 84.3 %                             | 0.67                  | 0.69 | 0.71  | 0.73  | 0.74  | 0.77   | 0.80   | 0.63                                      | 0.65 | 0.68  | 0.71  | 0.73  | 0.75   | 0.87   |          |
|                                                                                        |               | 0.06      | A                          | Surface Type           | Roadways and Paved Streets  | 95%                       | 90%                                | 0.73                  | 0.75 | 0.77  | 0.79  | 0.79  | 0.81   | 0.83   | 0.71                                      | 0.73 | 0.75  | 0.78  | 0.80  | 0.81   | 0.89   |          |
| OF-6                                                                                   | 2             | 0.08      | A                          | Surface Type           | Gravel - High Traffic Areas | 80%                       |                                    | 0.63                  | 0.65 | 0.66  | 0.69  | 0.71  | 0.73   | 0.77   | 0.57                                      | 0.59 | 0.63  | 0.66  | 0.68  | 0.70   | 0.86   |          |

Combined Peak Runoff Calculations for Inlets and Storm Drains

Designer: DJS

Company: Kimley-Horn

Date: 7/29/2026

Project: Trinity Ranch

Location: El Paso County, CO

MHFD-Rational, Version 3.00 (August 2025)

5-yrDesign Storm Return Period (Note: this worksheet can only evaluate one design storm at a time)

| Use 1 column (C, D, E) per row |                              |                         |                               |                            |                           |      |                      |               |                                | Obtain Inlet Capacity from MHFD-Inlet (Optional) |                   |                      |                              |                      |                   |                              |                      |                   |                    |
|--------------------------------|------------------------------|-------------------------|-------------------------------|----------------------------|---------------------------|------|----------------------|---------------|--------------------------------|--------------------------------------------------|-------------------|----------------------|------------------------------|----------------------|-------------------|------------------------------|----------------------|-------------------|--------------------|
| Design Point                   | # of Upstream Runoff Sources | Local Subcatchment Name | Upstream Surface Design Point | Upstream Pipe Design Point | Local Subcatchment Runoff |      |                      |               | Surface Runoff to Design Point |                                                  |                   |                      | Inlet Capacity / Bypass Flow |                      |                   | Total Runoff to Design Point |                      |                   |                    |
|                                |                              |                         |                               |                            | Area (ac)                 | C    | t <sub>c</sub> (min) | Local Q (cfs) | Σ(C*A) (acre)                  | t <sub>c</sub> (min)                             | Intensity (in/hr) | Surface Runoff (cfs) | (Optional) Inlet Name        | Inlet Capacity (cfs) | Bypass Flow (cfs) | Σ(C*A) (acre)                | t <sub>c</sub> (min) | Intensity (in/hr) | Total Runoff (cfs) |
| PR1                            | 2                            |                         |                               |                            | 204.29                    | 0.10 | 127.43               | 18.45         | 22.75                          | 127.43                                           | 0.89              | 20.30                |                              | 0.00                 | 20.30             | 22.75                        | 127.43               | 0.89              | 20.30              |
|                                |                              | OF-1                    |                               |                            |                           |      |                      |               | 20.68                          | 127.43                                           | 0.89              | 20.30                |                              |                      |                   | 20.68                        | 127.43               | 0.89              | 20.30              |
|                                |                              | PR-1                    |                               |                            | 16.17                     | 0.13 | 40.62                | 4.05          | 2.07                           | 40.62                                            | 1.96              | 16.95                |                              |                      |                   | 2.07                         | 40.62                | 1.96              | 16.95              |
| PR2                            | 2                            |                         |                               |                            |                           |      |                      |               | 2.81                           | 33.17                                            | 2.22              | 6.23                 | PR2                          | 36.20                | 0.00              | 2.81                         | 33.17                | 2.22              | 6.23               |
|                                |                              | OF-3                    |                               |                            | 18.51                     | 0.09 | 37.76                | 3.41          | 1.67                           | 37.76                                            | 2.05              | 6.17                 |                              |                      |                   | 1.67                         | 37.76                | 2.05              | 6.17               |
|                                |                              | PR-2                    |                               |                            | 9.55                      | 0.14 | 33.17                | 2.98          | 1.35                           | 33.17                                            | 2.22              | 6.23                 |                              |                      |                   | 1.35                         | 33.17                | 2.22              | 6.23               |
| PR4                            | 2                            |                         |                               |                            |                           |      |                      |               | 2.50                           | 29.19                                            | 2.39              | 5.99                 | PR4                          | 30.00                | 0.00              | 4.97                         | 29.19                | 2.39              | 11.88              |
|                                |                              | PR-4                    |                               |                            | 16.42                     | 0.15 | 29.19                | 5.99          | 2.50                           | 29.19                                            | 2.39              | 5.99                 |                              |                      |                   | 2.50                         | 29.19                | 2.39              | 11.88              |
|                                |                              |                         | PR2                           |                            |                           |      |                      |               |                                |                                                  |                   |                      |                              |                      |                   | 2.81                         | 33.29                | 2.21              | 11.75              |
| PR5                            | 1                            |                         |                               |                            |                           |      |                      |               | 0.70                           | 21.06                                            | 2.87              | 2.00                 | PR5                          | 10.00                | 0.00              | 0.70                         | 21.06                | 2.87              | 2.00               |
|                                |                              | PR-5                    |                               |                            | 2.08                      | 0.34 | 21.06                | 2.00          | 0.70                           | 21.06                                            | 2.87              | 2.00                 |                              |                      |                   | 0.70                         | 21.06                | 2.87              | 2.00               |
| PR6                            | 1                            |                         |                               |                            |                           |      |                      |               | 2.57                           | 35.17                                            | 2.14              | 5.49                 | PR6                          | 26.00                | 0.00              | 2.57                         | 35.17                | 2.14              | 5.49               |
|                                |                              | PR-6                    |                               |                            | 17.78                     | 0.14 | 35.17                | 5.49          | 2.57                           | 35.17                                            | 2.14              | 5.49                 |                              |                      |                   | 2.57                         | 35.17                | 2.14              | 5.49               |
| PR7                            | 1                            |                         |                               |                            |                           |      |                      |               | 9.44                           | 23.55                                            | 2.70              | 25.51                | PR7                          | 70.00                | 0.00              | 9.44                         | 23.55                | 2.70              | 25.51              |
|                                |                              | PR-7                    |                               |                            | 29.21                     | 0.32 | 23.55                | 25.51         | 9.44                           | 23.55                                            | 2.70              | 25.51                |                              |                      |                   | 9.44                         | 23.55                | 2.70              | 25.51              |
| PR8                            | 4                            |                         |                               |                            |                           |      |                      |               | 4.06                           | 20.73                                            | 2.90              | 11.76                |                              | 200.00               | 0.00              | 18.21                        | 23.66                | 2.70              | 49.08              |
|                                |                              | PR-8                    |                               |                            | 11.31                     | 0.36 | 20.73                | 11.76         | 4.06                           | 20.73                                            | 2.90              | 11.76                |                              |                      |                   | 4.06                         | 20.73                | 2.90              | 47.84              |
|                                |                              |                         | PR4                           |                            |                           |      |                      |               |                                |                                                  |                   |                      |                              |                      |                   | 4.97                         | 29.33                | 2.38              | 45.71              |
|                                |                              |                         | PR5                           |                            |                           |      |                      |               |                                |                                                  |                   |                      |                              |                      |                   | 0.70                         | 21.27                | 2.86              | 48.12              |
|                                |                              |                         | PR7                           |                            |                           |      |                      |               |                                |                                                  |                   |                      |                              |                      |                   | 9.44                         | 23.66                | 2.70              | 49.08              |
| PR9                            | 2                            |                         |                               |                            |                           |      |                      |               | 5.60                           | 25.82                                            | 2.57              | 14.37                |                              |                      | 14.37             | 7.48                         | 25.82                | 2.57              | 19.19              |
|                                |                              | PR-9                    |                               |                            | 17.68                     | 0.32 | 25.82                | 14.37         | 5.60                           | 25.82                                            | 2.57              | 14.37                |                              |                      |                   | 5.60                         | 25.82                | 2.57              | 19.19              |
|                                |                              |                         | PR6                           |                            |                           |      |                      |               |                                |                                                  |                   |                      |                              |                      |                   | 2.57                         | 35.30                | 2.13              | 17.43              |
| PR3                            | 2                            |                         |                               |                            |                           |      |                      |               | 31.95                          | 133.82                                           | 0.86              | 27.50                |                              |                      | 27.50             | 31.95                        | 133.82               | 0.86              | 27.50              |
|                                |                              | OF-2                    |                               |                            | 290.54                    | 0.10 | 133.82               | 25.46         | 29.58                          | 133.82                                           | 0.86              | 27.50                |                              |                      |                   | 29.58                        | 133.82               | 0.86              | 27.50              |
|                                |                              | PR-3                    |                               |                            | 17.72                     | 0.13 | 36.24                | 4.98          | 2.37                           | 36.24                                            | 2.10              | 21.80                |                              |                      |                   | 2.37                         | 36.24                | 2.10              | 21.80              |
| OF5                            | 2                            |                         |                               |                            |                           |      |                      |               | 1.88                           | 54.52                                            | 1.62              | 3.04                 | OF5                          | 10.00                | 0.00              | 1.88                         | 54.52                | 1.62              | 3.04               |
|                                |                              | OF-5                    |                               |                            | 6.21                      | 0.30 | 54.52                | 3.01          | 1.86                           | 54.52                                            | 1.62              | 3.04                 |                              |                      |                   | 1.86                         | 54.52                | 1.62              | 3.04               |
|                                |                              | OP-1                    |                               |                            | 0.04                      | 0.41 | 5.00                 | 0.08          | 0.02                           | 5.00                                             | 5.09              | 0.95                 |                              |                      |                   | 0.02                         | 5.00                 | 5.09              | 0.95               |
|                                |                              |                         |                               |                            |                           |      |                      |               |                                |                                                  |                   |                      |                              |                      |                   |                              |                      |                   |                    |

Combined Peak Runoff Calculations for Inlets and Storm Drains

Designer: DJS

Company: Kimley-Horn

Date: 7/29/2026

Project: Trinity Ranch

Location: El Paso County, CO

MHFD-Rational, Version 3.00 (August 2025)

100-yr

Design Storm Return Period (Note: this worksheet can only evaluate one design storm at a time)

| Use 1 column (C, D, E) per row |                              |                         |                               |                            |                           |      |                      |               |                                | Obtain Inlet Capacity from MHFD-Inlet (Optional) |                   |                      |                              |                      |                   |                              |                      |                   |                    |        |
|--------------------------------|------------------------------|-------------------------|-------------------------------|----------------------------|---------------------------|------|----------------------|---------------|--------------------------------|--------------------------------------------------|-------------------|----------------------|------------------------------|----------------------|-------------------|------------------------------|----------------------|-------------------|--------------------|--------|
| Design Point                   | # of Upstream Runoff Sources | Local Subcatchment Name | Upstream Surface Design Point | Upstream Pipe Design Point | Local Subcatchment Runoff |      |                      |               | Surface Runoff to Design Point |                                                  |                   |                      | Inlet Capacity / Bypass Flow |                      |                   | Total Runoff to Design Point |                      |                   |                    |        |
|                                |                              |                         |                               |                            | Area (ac)                 | C    | t <sub>c</sub> (min) | Local Q (cfs) | Σ(C*A) (acre)                  | t <sub>c</sub> (min)                             | Intensity (in/hr) | Surface Runoff (cfs) | (Optional) Inlet Name        | Inlet Capacity (cfs) | Bypass Flow (cfs) | Σ(C*A) (acre)                | t <sub>c</sub> (min) | Intensity (in/hr) | Total Runoff (cfs) |        |
| PR1                            | 2                            |                         |                               |                            |                           |      |                      |               | 81.51                          | 127.43                                           | 1.50              | 122.16               |                              |                      |                   |                              |                      |                   |                    |        |
|                                |                              | OF-1                    |                               |                            | 204.29                    | 0.37 | 127.43               | 112.58        | 75.11                          | 127.43                                           | 1.50              | 122.16               |                              |                      |                   |                              | 75.11                | 127.43            | 1.50               | 122.16 |
|                                |                              | PR-1                    |                               |                            | 16.17                     | 0.40 | 40.62                | 21.02         | 6.40                           | 40.62                                            | 3.29              | 99.70                |                              |                      |                   |                              | 6.40                 | 40.62             | 3.29               | 99.70  |
| PR2                            | 2                            |                         |                               |                            |                           |      |                      |               | 10.53                          | 37.76                                            | 3.44              | 36.20                | PR2                          | 36.20                | 0.00              |                              | 10.53                | 37.76             | 3.44               | 36.20  |
|                                |                              | OF-3                    |                               |                            | 18.51                     | 0.36 | 37.76                | 22.92         | 6.66                           | 37.76                                            | 3.44              | 36.20                |                              |                      |                   |                              | 6.66                 | 37.76             | 3.44               | 36.20  |
|                                |                              | PR-2                    |                               |                            | 9.55                      | 0.40 | 33.17                | 14.38         | 3.86                           | 33.17                                            | 3.72              | 36.18                |                              |                      |                   |                              | 3.86                 | 33.17             | 3.72               | 36.18  |
| PR4                            | 2                            |                         |                               |                            |                           |      |                      |               | 6.77                           | 29.19                                            | 4.02              | 27.20                | PR4                          | 30.00                | 0.00              |                              | 14.88                | 29.19             | 4.02               | 59.78  |
|                                |                              | PR-4                    |                               |                            | 16.42                     | 0.41 | 29.19                | 27.20         | 6.77                           | 29.19                                            | 4.02              | 27.20                |                              |                      |                   |                              | 6.77                 | 29.19             | 4.02               | 59.78  |
|                                |                              |                         |                               | PR2                        |                           |      |                      |               |                                |                                                  |                   |                      |                              |                      |                   |                              | 10.52                | 37.88             | 3.43               | 59.36  |
| PR5                            | 1                            |                         |                               |                            |                           |      |                      |               | 1.12                           | 21.06                                            | 4.82              | 5.39                 | PR5                          | 10.00                | 0.00              |                              | 1.12                 | 21.06             | 4.82               | 5.39   |
|                                |                              | PR-5                    |                               |                            | 2.08                      | 0.54 | 21.06                | 5.39          | 1.12                           | 21.06                                            | 4.82              | 5.39                 |                              |                      |                   |                              | 1.12                 | 21.06             | 4.82               | 5.39   |
| PR6                            | 1                            |                         |                               |                            |                           |      |                      |               | 7.23                           | 35.17                                            | 3.59              | 25.99                | PR6                          | 26.00                | 0.00              |                              | 7.23                 | 35.17             | 3.59               | 25.99  |
|                                |                              | PR-6                    |                               |                            | 17.78                     | 0.41 | 35.17                | 25.99         | 7.23                           | 35.17                                            | 3.59              | 25.99                |                              |                      |                   |                              | 7.23                 | 35.17             | 3.59               | 25.99  |
| PR7                            | 1                            |                         |                               |                            |                           |      |                      |               | 15.02                          | 23.55                                            | 4.54              | 68.20                | PR7                          | 70.00                | 0.00              |                              | 15.02                | 23.55             | 4.54               | 68.20  |
|                                |                              | PR-7                    |                               |                            | 29.21                     | 0.51 | 23.55                | 68.20         | 15.02                          | 23.55                                            | 4.54              | 68.20                |                              |                      |                   |                              | 15.02                | 23.55             | 4.54               | 68.20  |
| PR8                            | 4                            |                         |                               |                            |                           |      |                      |               | 6.08                           | 20.73                                            | 4.86              | 29.60                |                              | 200.00               | 0.00              |                              | 34.23                | 23.66             | 4.53               | 155.00 |
|                                |                              | PR-8                    |                               |                            | 11.31                     | 0.54 | 20.73                | 29.60         | 6.08                           | 20.73                                            | 4.86              | 29.60                |                              |                      |                   |                              | 6.08                 | 20.73             | 4.86               | 150.08 |
|                                |                              |                         |                               | PR4                        |                           |      |                      |               |                                |                                                  |                   |                      |                              |                      |                   |                              | 14.88                | 29.33             | 4.01               | 148.67 |
|                                |                              |                         |                               | PR5                        |                           |      |                      |               |                                |                                                  |                   |                      |                              |                      |                   |                              | 1.12                 | 21.27             | 4.80               | 151.15 |
|                                |                              |                         |                               | PR7                        |                           |      |                      |               |                                |                                                  |                   |                      |                              |                      |                   |                              | 15.02                | 23.66             | 4.53               | 155.00 |
| PR9                            | 2                            |                         |                               |                            |                           |      |                      |               | 9.04                           | 25.82                                            | 4.31              | 38.97                |                              |                      | 38.97             |                              | 14.33                | 25.82             | 4.31               | 61.78  |
|                                |                              | PR-9                    |                               |                            | 17.68                     | 0.51 | 25.82                | 38.97         | 9.04                           | 25.82                                            | 4.31              | 38.97                |                              |                      |                   |                              | 9.04                 | 25.82             | 4.31               | 61.78  |
|                                |                              |                         |                               | PR6                        |                           |      |                      |               |                                |                                                  |                   |                      |                              |                      |                   |                              | 7.23                 | 35.30             | 3.59               | 58.33  |
| PR3                            | 2                            |                         |                               |                            |                           |      |                      |               | 114.02                         | 133.82                                           | 1.45              | 164.88               |                              |                      | 164.88            |                              | 114.02               | 133.82            | 1.45               | 164.88 |
|                                |                              | OF-2                    |                               |                            | 290.54                    | 0.37 | 133.82               | 154.64        | 106.94                         | 133.82                                           | 1.45              | 164.88               |                              |                      |                   |                              | 106.94               | 133.82            | 1.45               | 164.88 |
|                                |                              | PR-3                    |                               |                            | 17.72                     | 0.40 | 36.24                | 24.98         | 7.08                           | 36.24                                            | 3.53              | 127.14               |                              |                      |                   |                              | 7.08                 | 36.24             | 3.53               | 127.14 |
| OF5                            | 2                            |                         |                               |                            |                           |      |                      |               | 3.18                           | 54.52                                            | 2.72              | 8.63                 | OF5                          | 10.00                | 0.00              |                              | 3.18                 | 54.52             | 2.72               | 8.63   |
|                                |                              | OF-5                    |                               |                            | 6.21                      | 0.51 | 54.52                | 8.56          | 3.15                           | 54.52                                            | 2.72              | 8.63                 |                              |                      |                   |                              | 3.15                 | 54.52             | 2.72               | 8.63   |
|                                |                              | OP-1                    |                               |                            | 0.04                      | 0.59 | 5.00                 | 0.20          | 0.02                           | 5.00                                             | 8.55              | 2.67                 |                              |                      |                   |                              | 0.02                 | 5.00              | 8.55               | 2.67   |

***APPENDIX D: HYDRUALICS***

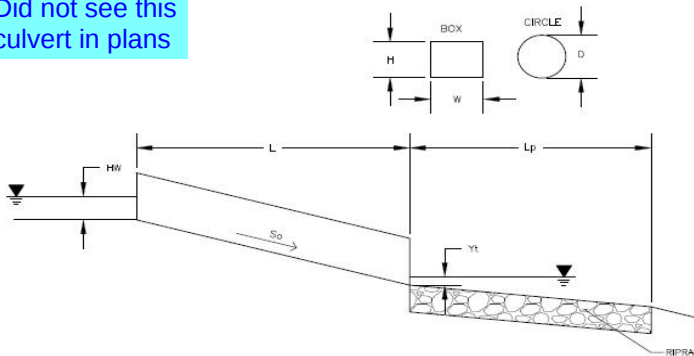
# DETERMINATION OF CULVERT HEADWATER AND OUTLET PROTECTION

MHFD-Culvert, Version 4.01 (April 2025)

Project: Trinity Ranch Estates - PDR

ID: P2

Did not see this  
culvert in plans



Soil Type:

Choose One:

☒ Sandy

☐ Non-Sandy

Supercritical Flow! Using Adjusted Diameter to calculate protection type.

## Design Information:

Design Discharge

Q = 36.2 cfs

Circular Culvert:

Barrel Diameter in Inches

D = 30 inches

Inlet Edge Type (Choose from pull-down list)

Beveled Edge (1:1)

OR:

Box Culvert:

Barrel Height (Rise) in Feet

H (Rise) =

Barrel Width (Span) in Feet

W (Span) =

Inlet Edge Type (Choose from pull-down list)

Number of Barrels

# Barrels = 1

Inlet Elevation

Elev IN = 6155 ft

Outlet Elevation OR Slope

So = 0.008 ft/ft

Culvert Length

L = 55 ft

Manning's Roughness

n = 0.013

Bend Loss Coefficient

k<sub>b</sub> = 0

Exit Loss Coefficient

k<sub>x</sub> = 1

Tailwater Surface Elevation

Y<sub>t</sub>, Elevation =

Max Allowable Channel Velocity

V = 5 ft/s

## Calculated Results:

Culvert Cross Sectional Area Available

A = 4.91 ft<sup>2</sup>

Culvert Normal Depth

Y<sub>n</sub> = 2.01 ft

Culvert Critical Depth

Y<sub>c</sub> = 2.04 ft

Froude Number

Fr = 1.03 Supercritical!

Entrance Loss Coefficient

k<sub>e</sub> = 0.20

Friction Loss Coefficient

k<sub>f</sub> = 0.50

Sum of All Loss Coefficients

k<sub>s</sub> = 1.70 ft

Headwater:

Inlet Control Headwater

HW<sub>i</sub> = 3.60 ft

Outlet Control Headwater

HW<sub>o</sub> = 3.27 ft

Design Headwater Elevation

HW = 6158.60 ft

Headwater / Diameter OR Headwater / Rise Ratio

HW / D = 1.44

Outlet Protection:

Flow / (Diameter<sup>2.5</sup>)

Q / D<sup>2.5</sup> = 3.66 ft<sup>0.5</sup>/s

Tailwater Surface Height

Y<sub>t</sub> = 1.00 ft

Tailwater / Diameter

Y<sub>t</sub> / D = 0.40

Expansion Factor

1 / (2 \* tan(Θ)) = 3.80

Flow Area at Max Channel Velocity

A<sub>t</sub> = 7.24 ft<sup>2</sup>

Width of Equivalent Conduit for Multiple Barrels

W<sub>eq</sub> = - ft

Length of Riprap Protection

L<sub>p</sub> = 19 ft

Width of Riprap Protection at Downstream End

T = 8 ft

Adjusted Diameter for Supercritical Flow

Da = 2.26 ft

Minimum Theoretical Riprap Size

d<sub>50</sub> min = 8 in

Nominal Riprap Size

d<sub>50</sub> nominal = 9 in

MHFD Riprap Type

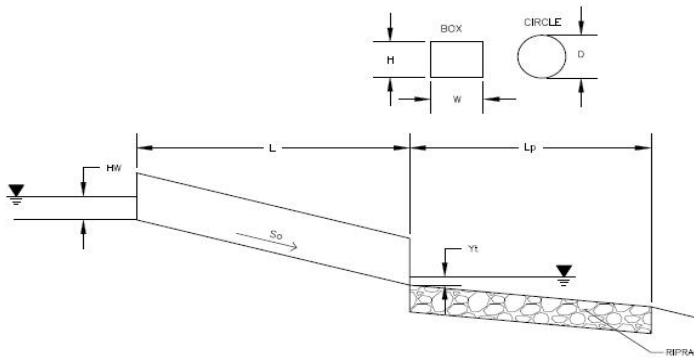
Type = L

# DETERMINATION OF CULVERT HEADWATER AND OUTLET PROTECTION

MHFD-Culvert, Version 4.01 (April 2025)

Project: Trinity Ranch Estates - PDR

ID: P4



Soil Type:

Choose One:

☐ Sandy

☒ Non-Sandy

## Design Information:

Design Discharge

Q = 59.78 cfs

Circular Culvert:

Barrel Diameter in Inches

D = 30 inches

Inlet Edge Type (Choose from pull-down list)

Beveled Edge (1:1)

OR:

Box Culvert:

Barrel Height (Rise) in Feet

H (Rise) = OR ft

Barrel Width (Span) in Feet

W (Span) = ft

Inlet Edge Type (Choose from pull-down list)

Number of Barrels

# Barrels = 2

Inlet Elevation

Elev IN = 6145.12 ft

Outlet Elevation OR Slope

So = 0.005 ft/ft

Culvert Length

L = 79 ft

Manning's Roughness

n = 0.013

Bend Loss Coefficient

k<sub>b</sub> = 0

Exit Loss Coefficient

k<sub>x</sub> = 1

Tailwater Surface Elevation

Y<sub>t</sub>, Elevation = ft

Max Allowable Channel Velocity

V = 7 ft/s

Information on these sheets does not seem to match with plan & profiles. Please verify and update as needed

## Calculated Results:

Culvert Cross Sectional Area Available

A = 4.91 ft<sup>2</sup>

Culvert Normal Depth

Y<sub>n</sub> = 2.12 ft

Culvert Critical Depth

Y<sub>c</sub> = 1.86 ft

Froude Number

Fr = 0.76

Entrance Loss Coefficient

k<sub>e</sub> = 0.20

Friction Loss Coefficient

k<sub>f</sub> = 0.72

Sum of All Loss Coefficients

k<sub>s</sub> = 1.92 ft

Headwater:

Inlet Control Headwater

HW<sub>i</sub> = 2.99 ft

Outlet Control Headwater

HW<sub>o</sub> = 2.89 ft

Design Headwater Elevation

HW = 6148.11 ft

Headwater / Diameter OR Headwater / Rise Ratio

HW / D = 1.20

Outlet Protection:

Flow / (Diameter<sup>2.5</sup>)

Q / D<sup>2.5</sup> = 3.02 ft<sup>0.5</sup>/s

Tailwater Surface Height

Y<sub>t</sub> = 1.00 ft

Tailwater / Diameter

Y<sub>t</sub> / D = 0.40

Expansion Factor

1 / (2 \* tan(Θ)) = 4.36

Flow Area at Max Channel Velocity

A<sub>t</sub> = 8.54 ft<sup>2</sup>

Width of Equivalent Conduit for Multiple Barrels

W<sub>eq</sub> = 5.00 ft

Length of Riprap Protection

L<sub>p</sub> = 16 ft

Width of Riprap Protection at Downstream End

T = 9 ft

Adjusted Diameter for Supercritical Flow

Da = - ft

Minimum Theoretical Riprap Size

d<sub>50</sub> min = 6 in

Nominal Riprap Size

d<sub>50</sub> nominal = 9 in

MHFD Riprap Type

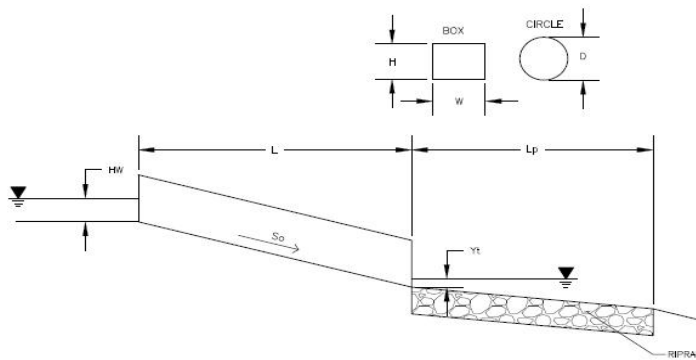
Type = L

# DETERMINATION OF CULVERT HEADWATER AND OUTLET PROTECTION

MHFD-Culvert, Version 4.01 (April 2025)

Project: Trinity Ranch Estates - PDR

ID: P5



Soil Type:

Choose One:

☐ Sandy

☒ Non-Sandy

## Design Information:

Design Discharge

Q = 5.39 cfs

Circular Culvert:

Barrel Diameter in Inches

D = 16 inches

Inlet Edge Type (Choose from pull-down list)

Beveled Edge (1:1)

OR:

Box Culvert:

Barrel Height (Rise) in Feet

H (Rise) = OR

Barrel Width (Span) in Feet

W (Span) =

Inlet Edge Type (Choose from pull-down list)

Number of Barrels

# Barrels = 1

Inlet Elevation

Elev IN = 6148 ft

Outlet Elevation OR Slope

So = 0.005 ft/ft

Culvert Length

L = 49 ft

Manning's Roughness

n = 0.013

Bend Loss Coefficient

k<sub>b</sub> = 0

Exit Loss Coefficient

k<sub>x</sub> = 1

Tailwater Surface Elevation

Y<sub>t</sub>, Elevation = ft

Max Allowable Channel Velocity

V = 7 ft/s

## Calculated Results:

Culvert Cross Sectional Area Available

A = 1.40 ft<sup>2</sup>

Culvert Normal Depth

Y<sub>n</sub> = 1.08 ft

Culvert Critical Depth

Y<sub>c</sub> = 0.93 ft

Froude Number

Fr = 0.73

Entrance Loss Coefficient

k<sub>e</sub> = 0.20

Friction Loss Coefficient

k<sub>f</sub> = 1.04

Sum of All Loss Coefficients

k<sub>s</sub> = 2.24 ft

Headwater:

Inlet Control Headwater

HW<sub>i</sub> = 1.42 ft

Outlet Control Headwater

HW<sub>o</sub> = 1.40 ft

Design Headwater Elevation

HW = 6149.42 ft

Headwater / Diameter OR Headwater / Rise Ratio

HW / D = 1.07

Outlet Protection:

Flow / (Diameter<sup>2.5</sup>)

Q / D<sup>2.5</sup> = 2.63 ft<sup>0.5</sup>/s

Tailwater Surface Height

Y<sub>t</sub> = 0.53 ft

Tailwater / Diameter

Y<sub>t</sub> / D = 0.40

Expansion Factor

1 / (2 \* tan(Θ)) = 4.89

Flow Area at Max Channel Velocity

A<sub>t</sub> = 0.77 ft<sup>2</sup>

Width of Equivalent Conduit for Multiple Barrels

W<sub>eq</sub> = - ft

Length of Riprap Protection

L<sub>p</sub> = 4 ft

Width of Riprap Protection at Downstream End

T = 3 ft

Adjusted Diameter for Supercritical Flow

Da = - ft

Minimum Theoretical Riprap Size

d<sub>50</sub> min = 3 in

Nominal Riprap Size

d<sub>50</sub> nominal = 6 in

MHFD Riprap Type

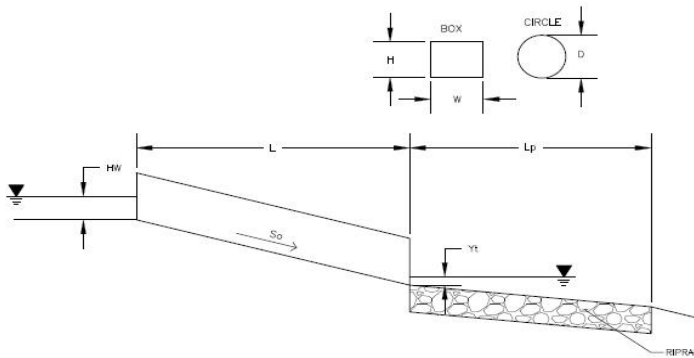
Type = VL

# DETERMINATION OF CULVERT HEADWATER AND OUTLET PROTECTION

MHFD-Culvert, Version 4.01 (April 2025)

Project: Trinity Ranch Estates - PDR

ID: P6



Soil Type:

Choose One:

☐ Sandy

☒ Non-Sandy

## Design Information:

Design Discharge

Q = 25.99 cfs

Circular Culvert:

Barrel Diameter in Inches

D = 30 inches

Inlet Edge Type (Choose from pull-down list)

Beveled Edge (1:1)

OR:

Box Culvert:

Barrel Height (Rise) in Feet

H (Rise) = OR

Barrel Width (Span) in Feet

W (Span) =

Inlet Edge Type (Choose from pull-down list)

Number of Barrels

# Barrels = 1

Inlet Elevation

Elev IN = 6133.3 ft

Outlet Elevation OR Slope

So = 0.005 ft/ft

Culvert Length

L = 49 ft

Manning's Roughness

n = 0.013

Bend Loss Coefficient

k<sub>b</sub> = 0

Exit Loss Coefficient

k<sub>x</sub> = 1

Tailwater Surface Elevation

Y<sub>t</sub>, Elevation = ft

Max Allowable Channel Velocity

V = 7 ft/s

## Calculated Results:

Culvert Cross Sectional Area Available

A = 4.91 ft<sup>2</sup>

Culvert Normal Depth

Y<sub>n</sub> = 1.84 ft

Culvert Critical Depth

Y<sub>c</sub> = 1.74 ft

Froude Number

Fr = 0.89

Entrance Loss Coefficient

k<sub>e</sub> = 0.20

Friction Loss Coefficient

k<sub>f</sub> = 0.45

Sum of All Loss Coefficients

k<sub>s</sub> = 1.65 ft

Headwater:

Inlet Control Headwater

HW<sub>i</sub> = 2.67 ft

Outlet Control Headwater

HW<sub>o</sub> = 2.59 ft

Design Headwater Elevation

HW = 6135.97 ft

Headwater / Diameter OR Headwater / Rise Ratio

HW / D = 1.07

Outlet Protection:

Flow / (Diameter<sup>2.5</sup>)

Q / D<sup>2.5</sup> = 2.63 ft<sup>0.5</sup>/s

Tailwater Surface Height

Y<sub>t</sub> = 1.00 ft

Tailwater / Diameter

Y<sub>t</sub> / D = 0.40

Expansion Factor

1 / (2 \* tan(Θ)) = 4.88

Flow Area at Max Channel Velocity

A<sub>t</sub> = 3.71 ft<sup>2</sup>

Width of Equivalent Conduit for Multiple Barrels

W<sub>eq</sub> = - ft

Length of Riprap Protection

L<sub>p</sub> = 8 ft

Width of Riprap Protection at Downstream End

T = 5 ft

Adjusted Diameter for Supercritical Flow

Da = - ft

Minimum Theoretical Riprap Size

d<sub>50</sub> min = 5 in

Nominal Riprap Size

d<sub>50</sub> nominal = 6 in

MHFD Riprap Type

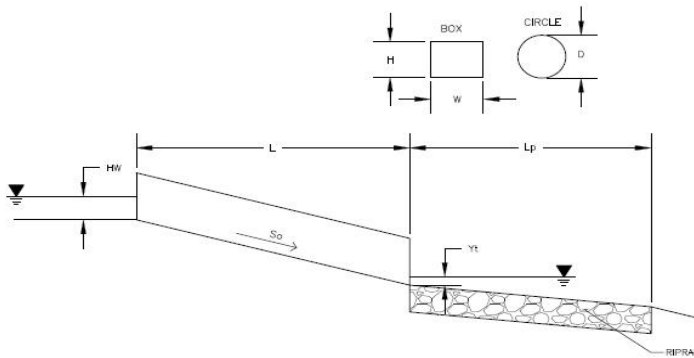
Type = VL

# DETERMINATION OF CULVERT HEADWATER AND OUTLET PROTECTION

MHFD-Culvert, Version 4.01 (April 2025)

Project: Trinity Ranch Estates - PDR

ID: P7



Soil Type:

Choose One:

☐ Sandy

☒ Non-Sandy

## Design Information:

Design Discharge

Q = 69.25 cfs

Circular Culvert:

Barrel Diameter in Inches

D = 30 inches

Inlet Edge Type (Choose from pull-down list)

Beveled Edge (1:1)

OR:

Box Culvert:

Barrel Height (Rise) in Feet

H (Rise) = OR

Barrel Width (Span) in Feet

W (Span) =

Inlet Edge Type (Choose from pull-down list)

Number of Barrels

# Barrels = 2

Inlet Elevation

Elev IN = 6132 ft

Outlet Elevation OR Slope

So = 0.005 ft/ft

Culvert Length

L = 60 ft

Manning's Roughness

n = 0.013

Bend Loss Coefficient

k<sub>b</sub> = 0

Exit Loss Coefficient

k<sub>x</sub> = 1

Tailwater Surface Elevation

Y<sub>t</sub>, Elevation =

Max Allowable Channel Velocity

V = 7 ft/s

## Calculated Results:

Culvert Cross Sectional Area Available

A = 4.91 ft<sup>2</sup>

Culvert Normal Depth

Y<sub>n</sub> = 2.50 ft

Culvert Critical Depth

Y<sub>c</sub> = 2.00 ft

Froude Number

Fr = - Pressure flow!

Entrance Loss Coefficient

k<sub>e</sub> = 0.20

Friction Loss Coefficient

k<sub>f</sub> = 0.55

Sum of All Loss Coefficients

k<sub>s</sub> = 1.75 ft

Headwater:

Inlet Control Headwater

HW<sub>i</sub> = 3.44 ft

Outlet Control Headwater

HW<sub>o</sub> = 3.30 ft

Design Headwater Elevation

HW = 6135.44 ft

Headwater / Diameter OR Headwater / Rise Ratio

HW / D = 1.37

Outlet Protection:

Flow / (Diameter<sup>2.5</sup>)

Q / D<sup>2.5</sup> = 3.50 ft<sup>0.5</sup>/s

Tailwater Surface Height

Y<sub>t</sub> = 1.00 ft

Tailwater / Diameter

Y<sub>t</sub> / D = 0.40

Expansion Factor

1 / (2 \* tan(Θ)) = 3.94

Flow Area at Max Channel Velocity

A<sub>t</sub> = 9.89 ft<sup>2</sup>

Width of Equivalent Conduit for Multiple Barrels

W<sub>eq</sub> = 5.00 ft

Length of Riprap Protection

L<sub>p</sub> = 20 ft

Width of Riprap Protection at Downstream End

T = 11 ft

Adjusted Diameter for Supercritical Flow

Da = - ft

Minimum Theoretical Riprap Size

d<sub>50</sub> min = 7 in

Nominal Riprap Size

d<sub>50</sub> nominal = 9 in

MHFD Riprap Type

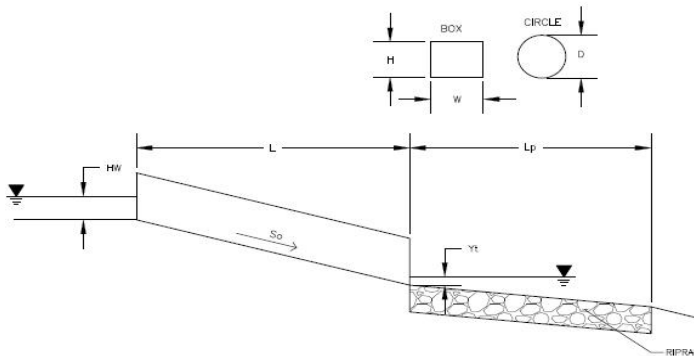
Type = L

# DETERMINATION OF CULVERT HEADWATER AND OUTLET PROTECTION

MHFD-Culvert, Version 4.01 (April 2025)

Project: Trinity Ranch - PDR

ID: Bypass Culvert - HWY 94 Ditch



Soil Type:

Choose One:

☒ Sandy

☐ Non-Sandy

Supercritical Flow! Using Adjusted Diameter to calculate protection type.

## Design Information:

Design Discharge

Q = 8.76 cfs

Circular Culvert:

Barrel Diameter in Inches

D = 18 inches

Inlet Edge Type (Choose from pull-down list)

Beveled Edge (1:1)

OR:

Box Culvert:

Barrel Height (Rise) in Feet

H (Rise) =

Barrel Width (Span) in Feet

W (Span) =

Inlet Edge Type (Choose from pull-down list)

Number of Barrels

# Barrels = 1

Inlet Elevation

Elev IN = 6132.7 ft

Outlet Elevation OR Slope

Elev OUT = 6132 ft

Culvert Length

L = 44 ft

Manning's Roughness

n = 0.013

Bend Loss Coefficient

k<sub>b</sub> = 0

Exit Loss Coefficient

k<sub>x</sub> = 1

Tailwater Surface Elevation

Y<sub>t</sub>, Elevation =

Max Allowable Channel Velocity

V = 7 ft/s

## Calculated Results:

Culvert Cross Sectional Area Available

A = 1.77 ft<sup>2</sup>

Culvert Normal Depth

Y<sub>n</sub> = 0.89 ft

Culvert Critical Depth

Y<sub>c</sub> = 1.15 ft

Froude Number

Fr = 1.64 Supercritical!

Entrance Loss Coefficient

k<sub>e</sub> = 0.20

Friction Loss Coefficient

k<sub>f</sub> = 0.80

Sum of All Loss Coefficients

k<sub>s</sub> = 2.00 ft

Headwater:

Inlet Control Headwater

HW<sub>i</sub> = 1.87 ft

Outlet Control Headwater

HW<sub>o</sub> = 1.38 ft

Design Headwater Elevation

HW = 6134.57 ft

Headwater / Diameter OR Headwater / Rise Ratio

HW / D = 1.24

Outlet Protection:

Flow / (Diameter<sup>2.5</sup>)

Q / D<sup>2.5</sup> = 3.18 ft<sup>0.5</sup>/s

Tailwater Surface Height

Y<sub>t</sub> = 0.60 ft

Tailwater / Diameter

Y<sub>t</sub> / D = 0.40

Expansion Factor

1 / (2 \* tan(θ)) = 4.22

Flow Area at Max Channel Velocity

A<sub>t</sub> = 1.25 ft<sup>2</sup>

Width of Equivalent Conduit for Multiple Barrels

W<sub>eq</sub> = - ft

Length of Riprap Protection

L<sub>p</sub> = 5 ft

Width of Riprap Protection at Downstream End

T = 3 ft

Adjusted Diameter for Supercritical Flow

Da = 1.19 ft

Minimum Theoretical Riprap Size

d<sub>50</sub> min = 4 in

Nominal Riprap Size

d<sub>50</sub> nominal = 6 in

MHFD Riprap Type

Type = VL

## Cross Section for Triangular Channel - 1

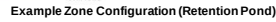
| Project Description   |              |
|-----------------------|--------------|
| Friction Method       | Manning      |
|                       | Formula      |
| Solve For             | Normal Depth |
| Input Data            |              |
| Roughness Coefficient | 0.030        |
| Channel Slope         | 0.002 ft/ft  |
| Normal Depth          | 11.8 in      |
| Left Side Slope       | 50.000 H:V   |
| Right Side Slope      | 4.000 H:V    |
| Discharge             | 36.00 cfs    |



V: 1  
H: 1

MHFD-Detention, Version 4.08 (April 2026)

Basin ID: Pond 1 (WQCV Override)

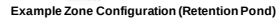


|                                               |   |                 |
|-----------------------------------------------|---|-----------------|
| Initial Surcharge Area ( $A_{SIV}$ )          | = | ft <sup>2</sup> |
| Surcharge Volume Length ( $L_{SV}$ )          | = | ft              |
| Surcharge Volume Width ( $W_{SV}$ )           | = | ft              |
| Depth of Basin Floor ( $H_{BLOOR}$ )          | = | ft              |
| Length of Basin Floor ( $L_{BLOOR}$ )         | = | ft              |
| Width of Basin Floor ( $W_{BLOOR}$ )          | = | ft              |
| Area of Basin Floor ( $A_{BLOOR}$ )           | = | ft <sup>2</sup> |
| Volume of Basin Floor ( $V_{BLOOR}$ )         | = | ft <sup>3</sup> |
| Depth of Main Basin ( $H_{MAIN}$ )            | = | ft              |
| Length of Main Basin ( $L_{MAIN}$ )           | = | ft              |
| Width of Main Basin ( $W_{MAIN}$ )            | = | ft              |
| Area of Main Basin ( $A_{MAIN}$ )             | = | ft <sup>2</sup> |
| Volume of Main Basin ( $V_{MAIN}$ )           | = | ft <sup>3</sup> |
| Calculated Total Basin Volume ( $V_{TOTAL}$ ) | = | acre-feet       |

## WQCV OVERRIDE

MHFD-Detention, Version 4.08 (April 2026)

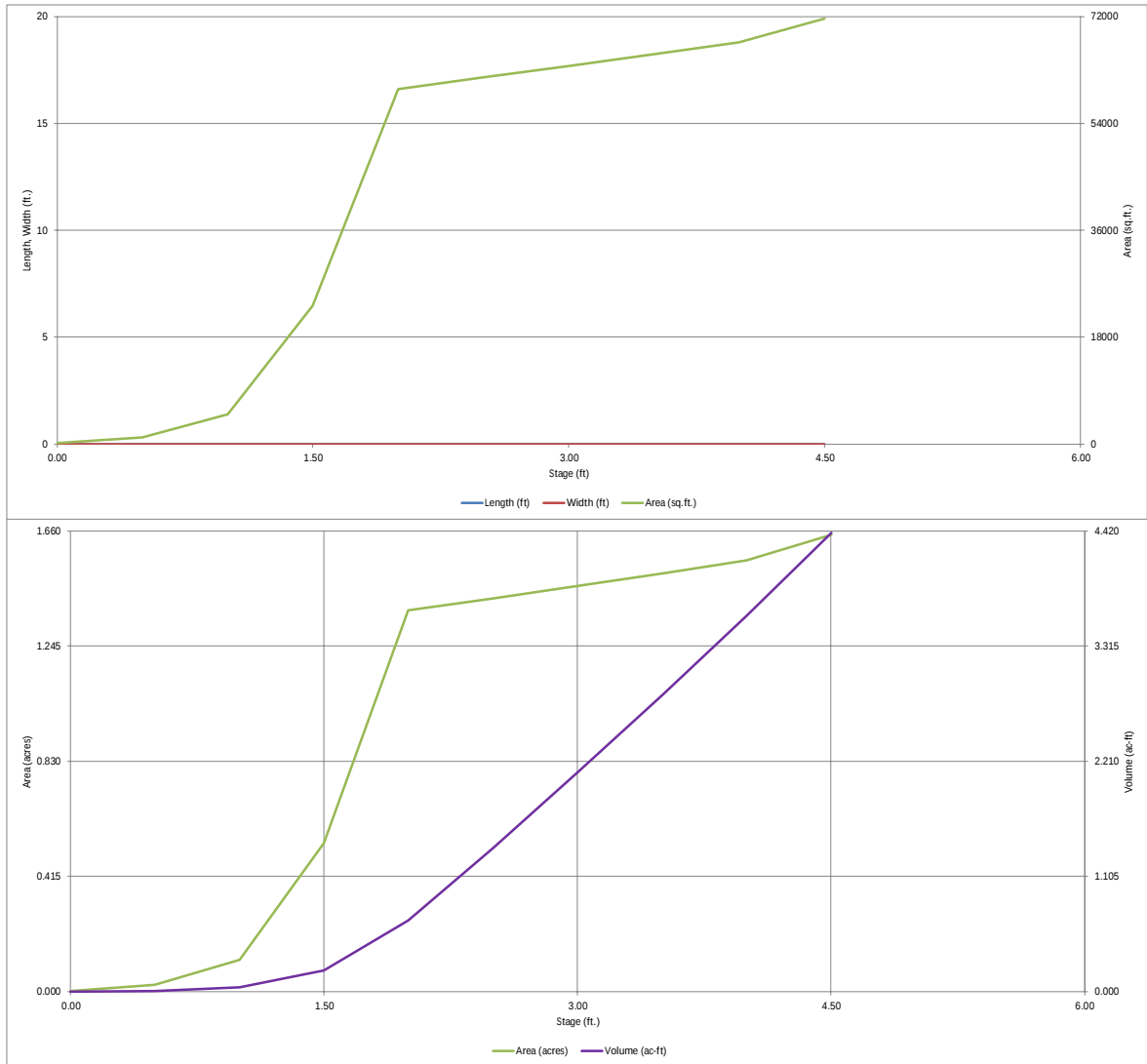
Basin ID: Pond 1 (Full Detention for Overall Buildout)



7/17/2026, 12:40 PM

# DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.08 (April 2026)

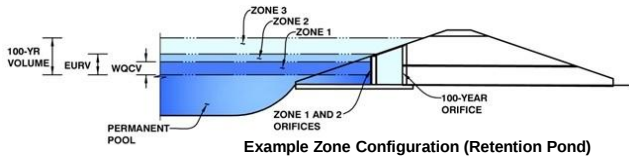


## DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.08 (April 2026)

Project: Trinity Ranch Estates - PDR

Basin ID: Pond 1 (Full Detention for Overall Buildout)



Example Zone Configuration (Retention Pond)

|                   | Estimated Stage (ft) | Estimated Volume (ac-ft) | Outlet Type          |
|-------------------|----------------------|--------------------------|----------------------|
| Zone 1 (WQCV)     | 1.94                 | 0.600                    | Orifice Plate        |
| Zone 2 (EURV)     | 2.97                 | 1.451                    | Orifice Plate        |
| Zone 3 (100-year) | 4.33                 | 2.077                    | Weir&Pipe (Restrict) |
| Total (all zones) |                      | 4.128                    |                      |

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration SCM)

Underdrain Orifice Invert Depth = N/A ft (distance below the filtration media surface)  
Underdrain Orifice Diameter = N/A inches

Calculated Parameters for Underdrain  
Underdrain Orifice Area = N/A ft<sup>2</sup>  
Underdrain Orifice Centroid = N/A feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation SCM)

Centroid of Lowest Orifice = 0.00 ft (relative to basin bottom at Stage = 0 ft)  
Depth at top of Zone using Orifice Plate = 2.97 ft (relative to basin bottom at Stage = 0 ft)  
Orifice Plate: Orifice Vertical Spacing = N/A inches  
Orifice Plate: Orifice Area per Row = N/A sq. inches

Calculated Parameters for Plate  
WQ Orifice Area per Row = N/A ft<sup>2</sup>  
Elliptical Half-Width = N/A feet  
Elliptical Slot Centroid = N/A feet  
Elliptical Slot Area = N/A ft<sup>2</sup>

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

|                                | Row 1 (required) | Row 2 (optional) | Row 3 (optional) | Row 4 (optional) | Row 5 (optional) | Row 6 (optional) | Row 7 (optional) | Row 8 (optional) |
|--------------------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|
| Stage of Orifice Centroid (ft) | 0.00             | 1.00             | 1.75             |                  |                  |                  |                  |                  |
| Orifice Area (sq. inches)      | 2.24             | 3.14             | 8.30             |                  |                  |                  |                  |                  |

|                                | Row 9 (optional) | Row 10 (optional) | Row 11 (optional) | Row 12 (optional) | Row 13 (optional) | Row 14 (optional) | Row 15 (optional) | Row 16 (optional) |
|--------------------------------|------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| Stage of Orifice Centroid (ft) |                  |                   |                   |                   |                   |                   |                   |                   |
| Orifice Area (sq. inches)      |                  |                   |                   |                   |                   |                   |                   |                   |

User Input: Vertical Orifice (Circular or Rectangular)

Invert of Vertical Orifice = N/A ft (relative to basin bottom at Stage = 0 ft)  
Depth at top of Zone using Vertical Orifice = N/A ft (relative to basin bottom at Stage = 0 ft)  
Vertical Orifice Diameter = N/A inches

Calculated Parameters for Vertical Orifice  
Vertical Orifice Area = N/A  
Vertical Orifice Centroid = N/A

User Input: Overflow Weir (Dropbox with Flat or Sloped Gate and Outlet Pipe OR Rectangular/Trapezoidal Weir and No Outlet Pipe)

Overflow Weir Front Edge Height, H<sub>o</sub> = 2.97 ft (relative to basin bottom at Stage = 0 ft)  
Overflow Weir Front Edge Length = 20.00 feet  
Overflow Weir Gate Slope = 4.00 H:V  
Horiz. Length of Weir Sides = 5.00 feet  
Overflow Gate Type = Type C Gate  
Debris Clogging % = 50%

Calculated Parameters for Overflow Weir  
Height of Gate Upper Edge, H<sub>t</sub> = 4.22  
Overflow Weir Slope Length = 5.15  
Gate Open Area / 100-yr Orifice Area = N/A  
Overflow Gate Open Area w/o Debris = 71.74  
Overflow Gate Open Area w/ Debris = 35.87

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

Depth to Invert of Outlet Pipe = 0.67 ft (distance below basin bottom at Stage = 0 ft)  
Outlet Pipe Diameter = 36.00 inches  
Restrictor Plate Height Above Pipe Invert = inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate  
Outlet Orifice Area = N/A  
Outlet Orifice Centroid = N/A  
Half-Central Angle of Restrictor Plate on Pipe = N/A

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage = 4.33 ft (relative to basin bottom at Stage = 0 ft)  
Spillway Crest Length = 30.00 feet  
Spillway End Slopes = 4.00 H:V  
Freeboard above Max Water Surface = 1.00 feet

Calculated Parameters for Spillway  
Spillway Design Flow Depth = 0.79 feet  
Stage at Top of Freeboard = 6.12 feet  
Basin Area at Top of Freeboard = 1.65 acres  
Basin Volume at Top of Freeboard = 4.41 acre-ft

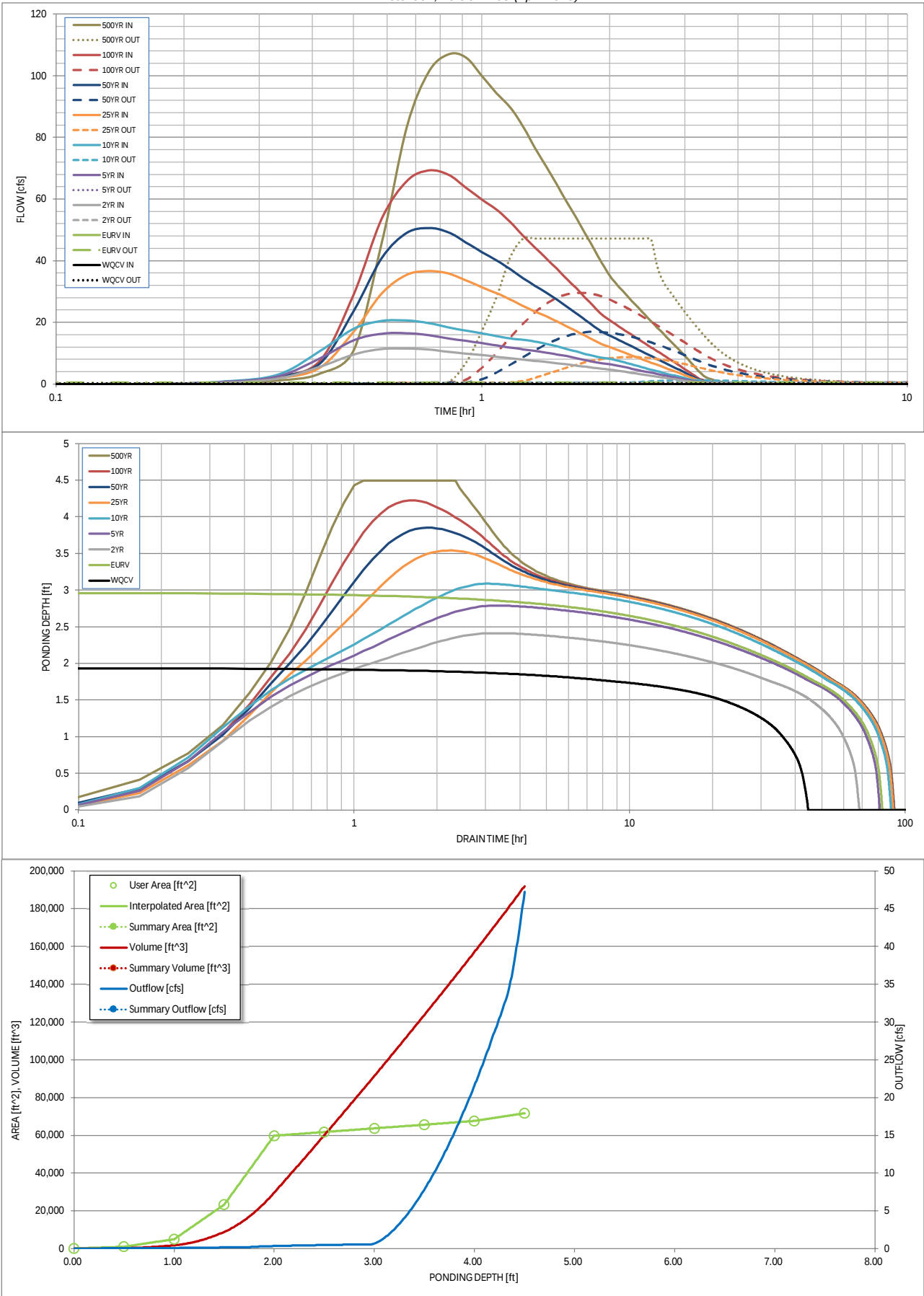
### Routed Hydrograph Results

The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).

|                                                 | WQCV  | EURV            | 2 Year | 5 Year | 10 Year         | 25 Year         | 50 Year         | 100 Year        |
|-------------------------------------------------|-------|-----------------|--------|--------|-----------------|-----------------|-----------------|-----------------|
| Design Storm Return Period =                    | N/A   | N/A             | 1.19   | 1.50   | 1.75            | 2.00            | 2.25            | 2.52            |
| One-Hour Rainfall Depth (in) =                  | N/A   | N/A             | 1.368  | 1.925  | 2.420           | 3.843           | 5.181           | 6.990           |
| CUHP Runoff Volume (acre-ft) =                  | 0.600 | 2.051           | 1.368  | 1.925  | 2.420           | 3.843           | 5.181           | 6.990           |
| Inflow Hydrograph Volume (acre-ft) =            | N/A   | N/A             | 1.368  | 1.925  | 2.420           | 3.843           | 5.181           | 6.990           |
| CUHP Predevelopment Peak Q (cfs) =              | N/A   | N/A             | 1.3    | 2.4    | 3.3             | 14.7            | 26.9            | 43.0            |
| OPTIONAL Override Predevelopment Peak Q (cfs) = | N/A   | N/A             |        |        |                 |                 |                 |                 |
| Predevelopment Unit Peak Flow, q (cfs/acre) =   | N/A   | N/A             | 0.01   | 0.03   | 0.04            | 0.17            | 0.31            | 0.49            |
| Peak Inflow Q (cfs) =                           | N/A   | N/A             | 11.6   | 16.5   | 20.7            | 36.7            | 50.7            | 69.3            |
| Peak Outflow Q (cfs) =                          | 0.3   | 0.6             | 0.5    | 0.5    | 1.3             | 8.8             | 17.0            | 29.6            |
| Ratio Peak Outflow to Predevelopment Q =        | N/A   | N/A             | N/A    | 0.2    | 0.4             | 0.6             | 0.6             | 0.7             |
| Structure Controlling Flow =                    | Plate | Overflow Weir 1 | Plate  | Plate  | Overflow Weir 1 | Overflow Weir 1 | Overflow Weir 1 | Overflow Weir 1 |
| Max Velocity through Gate 1 (fps) =             | N/A   | N/A             | N/A    | N/A    | 0.0             | 0.0             | 0.0             | 0.0             |
| Max Velocity through Gate 2 (fps) =             | N/A   | N/A             | N/A    | N/A    | N/A             | N/A             | N/A             | N/A             |
| Time to Drain 97% of Inflow Volume (hours) =    | 40    | 72              | 60     | 71     | 77              | 75              | 72              | 68              |
| Time to Drain 99% of Inflow Volume (hours) =    | 43    | 78              | 65     | 76     | 83              | 83              | 81              | 79              |
| Maximum Ponding Depth (ft) =                    | 1.94  | 2.97            | 2.42   | 2.79   | 3.09            | 3.54            | 3.85            | 4.23            |
| Area at Maximum Ponding Depth (acres) =         | 1.27  | 1.46            | 1.41   | 1.44   | 1.47            | 1.51            | 1.54            | 1.59            |
| Maximum Volume Stored (acre-ft) =               | 0.602 | 2.055           | 1.251  | 1.779  | 2.231           | 2.901           | 3.374           | 3.952           |

DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.08 (April 2026)



| S-A-V-D Chart Axis Override | X-axis | Left Y-Axis | Right Y-Axis |
|-----------------------------|--------|-------------|--------------|
| minimum bound               |        |             |              |
| maximum bound               |        |             |              |

# DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename: \_\_\_\_\_

## Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

| Time Interval | SOURCE  | CUHP       | CUHP       | CUHP         | CUHP         | CUHP          | CUHP          | CUHP          | CUHP           | CUHP           |
|---------------|---------|------------|------------|--------------|--------------|---------------|---------------|---------------|----------------|----------------|
|               | TIME    | WQCV [cfs] | EURV [cfs] | 2 Year [cfs] | 5 Year [cfs] | 10 Year [cfs] | 25 Year [cfs] | 50 Year [cfs] | 100 Year [cfs] | 500 Year [cfs] |
| 5.00 min      | 0:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 0:05:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 0:10:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.05          | 0.01           | 0.16           |
|               | 0:15:00 | 0.00       | 0.00       | 0.43         | 0.71         | 0.88          | 0.60          | 0.79          | 0.74           | 1.19           |
|               | 0:20:00 | 0.00       | 0.00       | 1.90         | 2.60         | 3.11          | 2.00          | 2.39          | 2.50           | 3.41           |
|               | 0:25:00 | 0.00       | 0.00       | 5.69         | 8.45         | 10.79         | 5.39          | 6.84          | 7.63           | 11.16          |
|               | 0:30:00 | 0.00       | 0.00       | 9.68         | 14.26        | 18.04         | 17.03         | 23.84         | 29.29          | 46.36          |
|               | 0:35:00 | 0.00       | 0.00       | 11.36        | 16.40        | 20.52         | 29.53         | 41.13         | 53.90          | 83.63          |
|               | 0:40:00 | 0.00       | 0.00       | 11.58        | 16.52        | 20.65         | 35.46         | 49.10         | 65.99          | 101.24         |
|               | 0:45:00 | 0.00       | 0.00       | 11.21        | 15.92        | 19.85         | 36.66         | 50.70         | 69.31          | 107.01         |
|               | 0:50:00 | 0.00       | 0.00       | 10.52        | 14.90        | 18.47         | 35.90         | 49.30         | 68.02          | 106.01         |
|               | 0:55:00 | 0.00       | 0.00       | 9.92         | 14.05        | 17.38         | 33.72         | 46.07         | 63.88          | 100.07         |
|               | 1:00:00 | 0.00       | 0.00       | 9.42         | 13.29        | 16.44         | 31.46         | 42.93         | 59.96          | 94.39          |
|               | 1:05:00 | 0.00       | 0.00       | 8.94         | 12.55        | 15.57         | 29.52         | 40.16         | 56.62          | 89.68          |
|               | 1:10:00 | 0.00       | 0.00       | 8.43         | 11.86        | 14.82         | 27.46         | 37.27         | 52.53          | 83.47          |
|               | 1:15:00 | 0.00       | 0.00       | 7.98         | 11.31        | 14.36         | 25.36         | 34.39         | 48.14          | 76.62          |
|               | 1:20:00 | 0.00       | 0.00       | 7.59         | 10.78        | 13.82         | 23.59         | 31.96         | 44.31          | 70.53          |
|               | 1:25:00 | 0.00       | 0.00       | 7.20         | 10.23        | 13.09         | 21.98         | 29.67         | 40.78          | 64.71          |
|               | 1:30:00 | 0.00       | 0.00       | 6.81         | 9.67         | 12.28         | 20.39         | 27.43         | 37.43          | 59.18          |
|               | 1:35:00 | 0.00       | 0.00       | 6.42         | 9.10         | 11.44         | 18.80         | 25.20         | 34.24          | 53.96          |
|               | 1:40:00 | 0.00       | 0.00       | 6.03         | 8.47         | 10.61         | 17.23         | 23.01         | 31.11          | 48.88          |
|               | 1:45:00 | 0.00       | 0.00       | 5.65         | 7.81         | 9.82          | 15.71         | 20.87         | 28.06          | 43.92          |
|               | 1:50:00 | 0.00       | 0.00       | 5.31         | 7.20         | 9.10          | 14.23         | 18.80         | 25.12          | 39.18          |
|               | 1:55:00 | 0.00       | 0.00       | 5.01         | 6.78         | 8.63          | 12.91         | 16.98         | 22.53          | 35.09          |
|               | 2:00:00 | 0.00       | 0.00       | 4.73         | 6.45         | 8.22          | 11.99         | 15.72         | 20.67          | 32.13          |
|               | 2:05:00 | 0.00       | 0.00       | 4.40         | 6.03         | 7.67          | 11.12         | 14.55         | 19.05          | 29.52          |
|               | 2:10:00 | 0.00       | 0.00       | 4.03         | 5.53         | 7.03          | 10.21         | 13.37         | 17.47          | 27.02          |
|               | 2:15:00 | 0.00       | 0.00       | 3.67         | 5.04         | 6.40          | 9.34          | 12.24         | 15.99          | 24.68          |
|               | 2:20:00 | 0.00       | 0.00       | 3.33         | 4.57         | 5.80          | 8.52          | 11.15         | 14.57          | 22.46          |
|               | 2:25:00 | 0.00       | 0.00       | 3.01         | 4.13         | 5.23          | 7.73          | 10.11         | 13.21          | 20.34          |
|               | 2:30:00 | 0.00       | 0.00       | 2.71         | 3.72         | 4.69          | 6.98          | 9.13          | 11.93          | 18.35          |
|               | 2:35:00 | 0.00       | 0.00       | 2.43         | 3.32         | 4.18          | 6.27          | 8.18          | 10.71          | 16.45          |
|               | 2:40:00 | 0.00       | 0.00       | 2.15         | 2.94         | 3.70          | 5.57          | 7.25          | 9.50           | 14.58          |
|               | 2:45:00 | 0.00       | 0.00       | 1.89         | 2.58         | 3.24          | 4.90          | 6.36          | 8.32           | 12.74          |
|               | 2:50:00 | 0.00       | 0.00       | 1.64         | 2.23         | 2.80          | 4.24          | 5.47          | 7.15           | 10.92          |
|               | 2:55:00 | 0.00       | 0.00       | 1.39         | 1.89         | 2.37          | 3.59          | 4.60          | 6.00           | 9.11           |
|               | 3:00:00 | 0.00       | 0.00       | 1.15         | 1.56         | 1.95          | 2.94          | 3.74          | 4.85           | 7.32           |
|               | 3:05:00 | 0.00       | 0.00       | 0.93         | 1.25         | 1.55          | 2.32          | 2.91          | 3.73           | 5.57           |
|               | 3:10:00 | 0.00       | 0.00       | 0.72         | 0.96         | 1.19          | 1.73          | 2.11          | 2.66           | 3.90           |
|               | 3:15:00 | 0.00       | 0.00       | 0.58         | 0.76         | 0.97          | 1.20          | 1.43          | 1.75           | 2.59           |
|               | 3:20:00 | 0.00       | 0.00       | 0.48         | 0.64         | 0.82          | 0.88          | 1.04          | 1.22           | 1.82           |
|               | 3:25:00 | 0.00       | 0.00       | 0.42         | 0.55         | 0.70          | 0.70          | 0.82          | 0.92           | 1.35           |
|               | 3:30:00 | 0.00       | 0.00       | 0.36         | 0.47         | 0.61          | 0.57          | 0.67          | 0.71           | 1.01           |
|               | 3:35:00 | 0.00       | 0.00       | 0.31         | 0.40         | 0.52          | 0.47          | 0.54          | 0.56           | 0.77           |
|               | 3:40:00 | 0.00       | 0.00       | 0.26         | 0.34         | 0.44          | 0.39          | 0.45          | 0.43           | 0.58           |
|               | 3:45:00 | 0.00       | 0.00       | 0.22         | 0.29         | 0.36          | 0.32          | 0.36          | 0.34           | 0.43           |
|               | 3:50:00 | 0.00       | 0.00       | 0.18         | 0.24         | 0.30          | 0.26          | 0.29          | 0.27           | 0.33           |
|               | 3:55:00 | 0.00       | 0.00       | 0.15         | 0.19         | 0.24          | 0.21          | 0.24          | 0.22           | 0.26           |
|               | 4:00:00 | 0.00       | 0.00       | 0.12         | 0.15         | 0.19          | 0.17          | 0.19          | 0.17           | 0.21           |
|               | 4:05:00 | 0.00       | 0.00       | 0.10         | 0.12         | 0.15          | 0.13          | 0.15          | 0.14           | 0.17           |
|               | 4:10:00 | 0.00       | 0.00       | 0.07         | 0.09         | 0.11          | 0.10          | 0.11          | 0.11           | 0.13           |
|               | 4:15:00 | 0.00       | 0.00       | 0.05         | 0.07         | 0.09          | 0.08          | 0.09          | 0.08           | 0.09           |
|               | 4:20:00 | 0.00       | 0.00       | 0.04         | 0.05         | 0.06          | 0.06          | 0.06          | 0.06           | 0.07           |
|               | 4:25:00 | 0.00       | 0.00       | 0.02         | 0.03         | 0.04          | 0.04          | 0.04          | 0.04           | 0.04           |
|               | 4:30:00 | 0.00       | 0.00       | 0.01         | 0.02         | 0.02          | 0.02          | 0.02          | 0.02           | 0.02           |
|               | 4:35:00 | 0.00       | 0.00       | 0.01         | 0.01         | 0.01          | 0.01          | 0.01          | 0.01           | 0.01           |
|               | 4:40:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:45:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:50:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:55:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:05:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:10:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:15:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:20:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:25:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:30:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:35:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:40:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:45:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:50:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:55:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 6:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |

## DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.08 (April 2026)

### Summary Stage-Area-Volume-Discharge Relationships

The user can create a summary S-A-V-D by entering the desired stage increments and the remainder of the table will populate automatically.

The user should graphically compare the summary S-A-V-D table to the full S-A-V-D table in the chart to confirm it captures all key transition points.

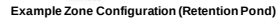
[illegible]

For best results, include the stages of all grade slope changes (e.g. ISV and Floor) from the S-A-V table on Sheet 'Basin'.

Also include the inverts of all outlets (e.g. vertical orifice, overflow grate, and spillway, where applicable).

*MHFD-Detention, Version 4.08 (April 2026)*

Basin ID: Pond 2 (WQCV Override)



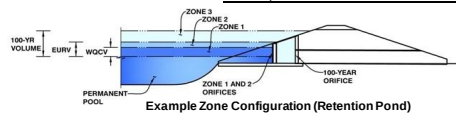
|                                               |   |                 |
|-----------------------------------------------|---|-----------------|
| Initial Surcharge Area ( $A_{SIV}$ )          | = | ft <sup>2</sup> |
| Surcharge Volume Length ( $L_{SV}$ )          | = | ft              |
| Surcharge Volume Width ( $W_{SV}$ )           | = | ft              |
| Depth of Basin Floor ( $H_{BLOOR}$ )          | = | ft              |
| Length of Basin Floor ( $L_{BLOOR}$ )         | = | ft              |
| Width of Basin Floor ( $W_{BLOOR}$ )          | = | ft              |
| Area of Basin Floor ( $A_{BLOOR}$ )           | = | ft <sup>2</sup> |
| Volume of Basin Floor ( $V_{BLOOR}$ )         | = | ft <sup>3</sup> |
| Depth of Main Basin ( $H_{MAIN}$ )            | = | ft              |
| Length of Main Basin ( $L_{MAIN}$ )           | = | ft              |
| Width of Main Basin ( $W_{MAIN}$ )            | = | ft              |
| Area of Main Basin ( $A_{MAIN}$ )             | = | ft <sup>2</sup> |
| Volume of Main Basin ( $V_{MAIN}$ )           | = | ft <sup>3</sup> |
| Calculated Total Basin Volume ( $V_{TOTAL}$ ) | = | acre-feet       |

|      |           |
|------|-----------|
|      | acre-feet |
|      | acre-feet |
| 1.19 | inches    |
| 1.50 | inches    |
| 1.75 | inches    |
| 2.00 | inches    |
| 2.25 | inches    |
| 2.52 | inches    |
|      | inches    |

7/17/2026, 12:30 PM

MHFD-Detention, Version 4.08 (April 2026)

Basin ID: Pond 2 (Full Detention for Overall Buildout)



|                                                |        |         |
|------------------------------------------------|--------|---------|
| Selected SCM Type =                            | EDB    |         |
| Watershed Area =                               | 35.46  | acres   |
| Watershed Length =                             | 2.280  | ft      |
| Watershed Length to Centroid =                 | 1.140  | ft      |
| Watershed Slope =                              | 0.020  | ft/ft   |
| Watershed Imperviousness =                     | 25.47% | percent |
| Percentage Hydrologic Soil Group A =           | 100.0% | percent |
| Percentage Hydrologic Soil Group B =           | 0.0%   | percent |
| Percentage Hydrologic Soil Groups C/D =        | 0.0%   | percent |
| Target WQCV Drain Time =                       | 40.0   | hours   |
| Location for 1-hr Rainfall Depths = User Input |        |         |

### Optional User Overrides

|                                        |       |           |       |           |
|----------------------------------------|-------|-----------|-------|-----------|
| Water Quality Capture Volume (WQCV) =  | 0.238 | acre-feet | 0.238 | acre-feet |
| Excess Urban Runoff Volume (EURV) =    | 0.662 | acre-feet |       | acre-feet |
| 2-yr Runoff Volume (P1 = 1.19 in.) =   | 0.579 | acre-feet | 1.19  | inches    |
| 5-yr Runoff Volume (P1 = 1.5 in.) =    | 0.812 | acre-feet | 1.50  | inches    |
| 10-yr Runoff Volume (P1 = 1.75 in.) =  | 1.016 | acre-feet | 1.75  | inches    |
| 25-yr Runoff Volume (P1 = 2 in.) =     | 1.593 | acre-feet | 2.00  | inches    |
| 50-yr Runoff Volume (P1 = 2.25 in.) =  | 2.134 | acre-feet | 2.25  | inches    |
| 100-yr Runoff Volume (P1 = 2.52 in.) = | 2.863 | acre-feet | 2.52  | inches    |
| 500-yr Runoff Volume (P1 = 3.14 in.) = | 4.445 | acre-feet |       | inches    |
| Approximate 2-yr Detention Volume =    | 0.538 | acre-feet |       |           |
| Approximate 5-yr Detention Volume =    | 0.721 | acre-feet |       |           |
| Approximate 10-yr Detention Volume =   | 0.908 | acre-feet |       |           |
| Approximate 25-yr Detention Volume =   | 1.159 | acre-feet |       |           |
| Approximate 50-yr Detention Volume =   | 1.360 | acre-feet |       |           |
| Approximate 100-yr Detention Volume =  | 1.712 | acre-feet |       |           |

|                                                   |       |                 |
|---------------------------------------------------|-------|-----------------|
| Zone 1 Volume (WQCV) =                            | 0.238 | acre-feet       |
| Zone 2 Volume (EURV - Zone 1) =                   | 0.624 | acre-feet       |
| Zone 3 Volume (50-year - Zones 1 & 2) =           | 0.498 | acre-feet       |
| Total Detention Basin Volume =                    | 1.360 | acre-feet       |
| Initial Surge Volume (ISV) =                      | USER  | ft <sup>3</sup> |
| Initial Surge Depth (ISD) =                       | USER  | ft              |
| Total Available Detention Depth ( $H_{total}$ ) = | USER  | ft              |
| Depth of Trickle Channel ( $H_{TC}$ ) =           | USER  | ft              |
| Slope of Trickle Channel ( $S_{TC}$ ) =           | USER  | ft/ft           |
| Slopes of Main Basin Sides ( $S_{main}$ ) =       | USER  | H:V             |
| Basin Length-to-Width Ratio ( $R_{L/W}$ ) =       | USER  |                 |

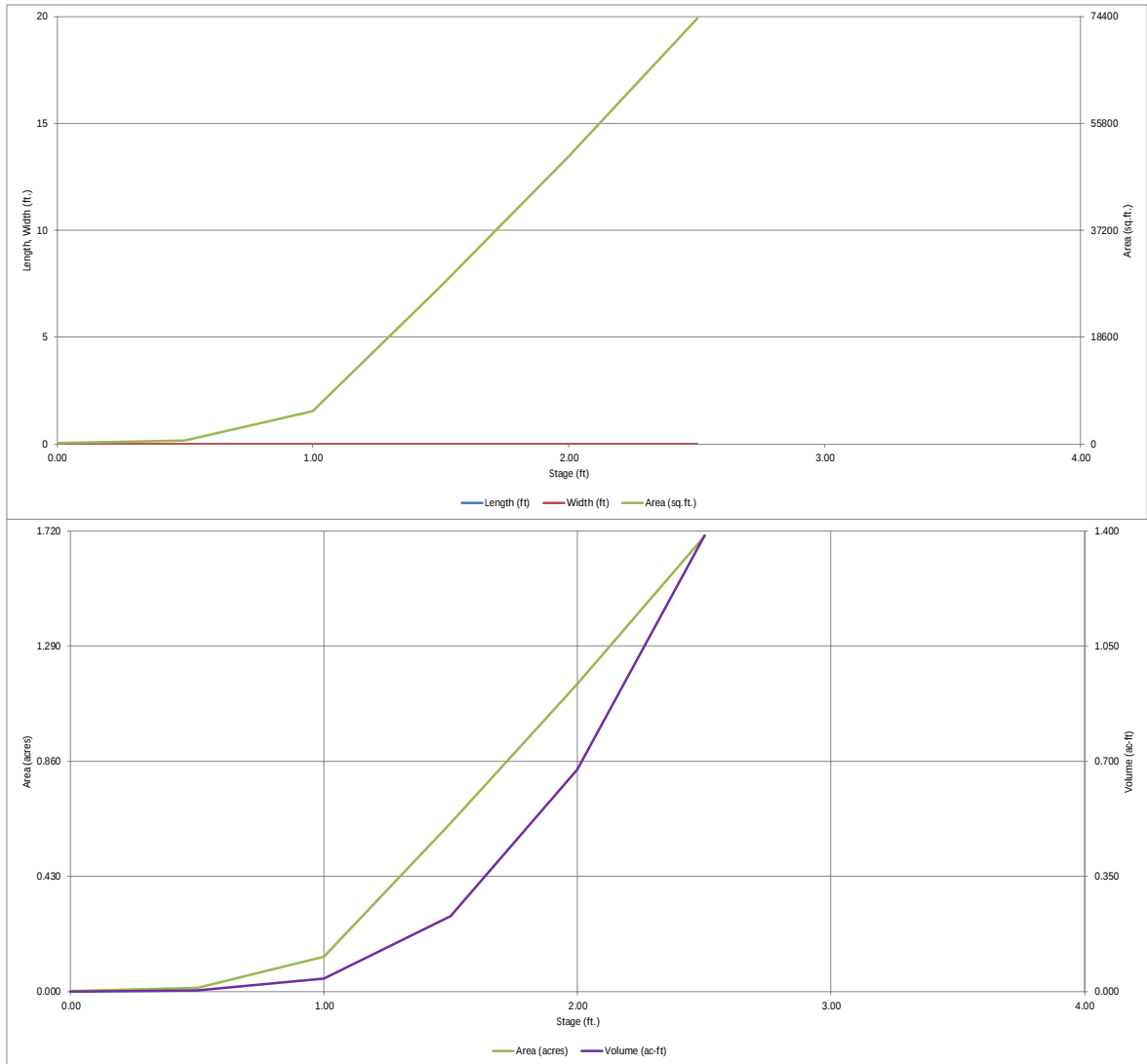
Total detention volume is less than 100-year volume.

|                                               |   |      |                 |
|-----------------------------------------------|---|------|-----------------|
| Initial Surcharge Area ( $A_{ISV}$ )          | = | user | ft <sup>2</sup> |
| Surcharge Volume Length ( $L_{SV}$ )          | = | user | ft              |
| Surcharge Volume Width ( $W_{SV}$ )           | = | user | ft              |
| Depth of Basin Floor ( $H_{FLOOR}$ )          | = | user | ft              |
| Length of Basin Floor ( $L_{FLOOR}$ )         | = | user | ft              |
| Width of Basin Floor ( $W_{FLOOR}$ )          | = | user | ft              |
| Area of Basin Floor ( $A_{FLOOR}$ )           | = | user | ft <sup>2</sup> |
| Volume of Basin Floor ( $V_{FLOOR}$ )         | = | user | ft <sup>3</sup> |
| Depth of Main Basin ( $H_{MAIN}$ )            | = | user | ft              |
| Length of Main Basin ( $L_{MAIN}$ )           | = | user | ft              |
| Width of Main Basin ( $W_{MAIN}$ )            | = | user | ft              |
| Area of Main Basin ( $A_{MAIN}$ )             | = | user | ft <sup>2</sup> |
| Volume of Main Basin ( $V_{MAIN}$ )           | = | user | ft <sup>3</sup> |
| Calculated Total Basin Volume ( $V_{TOTAL}$ ) | = | user | acre-feet       |

[illegible]

# DETENTION BASIN STAGE-STORAGE TABLE BUILDER

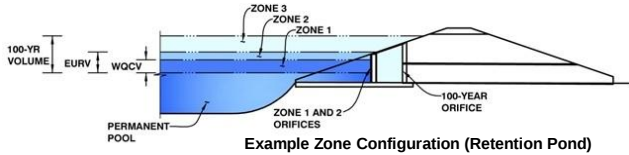
MHFD-Detention, Version 4.08 (April 2026)



## DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.08 (April 2026)

Project: Trinity Ranch Estates - PDR  
Basin ID: Pond 2 (Full Detention for Overall Buildout)



|                   | Estimated Stage (ft) | Estimated Volume (ac-ft) | Outlet Type    |
|-------------------|----------------------|--------------------------|----------------|
| Zone 1 (WQCV)     | 1.52                 | 0.238                    | Orifice Plate  |
| Zone 2 (EURV)     | 2.16                 | 0.624                    | Orifice Plate  |
| Zone 3 (50-year)  | 2.49                 | 0.498                    | Weir (No Pipe) |
| Total (all zones) |                      | 1.360                    |                |

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration SCM)

Underdrain Orifice Invert Depth = N/A ft (distance below the filtration media surface)  
Underdrain Orifice Diameter = N/A inches

Calculated Parameters for Underdrain  
Underdrain Orifice Area = N/A ft<sup>2</sup>  
Underdrain Orifice Centroid = N/A feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation SCM)

Centroid of Lowest Orifice = 0.00 ft (relative to basin bottom at Stage = 0 ft)  
Depth at top of Zone using Orifice Plate = 2.16 ft (relative to basin bottom at Stage = 0 ft)  
Orifice Plate: Orifice Vertical Spacing = N/A inches  
Orifice Plate: Orifice Area per Row = N/A sq. inches

Calculated Parameters for Plate  
WQ Orifice Area per Row = N/A ft<sup>2</sup>  
Elliptical Half-Width = N/A feet  
Elliptical Slot Centroid = N/A feet  
Elliptical Slot Area = N/A ft<sup>2</sup>

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

|                                | Row 1 (required) | Row 2 (optional) | Row 3 (optional) | Row 4 (optional) | Row 5 (optional) | Row 6 (optional) | Row 7 (optional) | Row 8 (optional) |
|--------------------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|
| Stage of Orifice Centroid (ft) | 0.00             | 0.85             | 1.50             |                  |                  |                  |                  |                  |
| Orifice Area (sq. inches)      | 0.69             | 3.14             | 4.91             |                  |                  |                  |                  |                  |

|                                | Row 9 (optional) | Row 10 (optional) | Row 11 (optional) | Row 12 (optional) | Row 13 (optional) | Row 14 (optional) | Row 15 (optional) | Row 16 (optional) |
|--------------------------------|------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| Stage of Orifice Centroid (ft) |                  |                   |                   |                   |                   |                   |                   |                   |
| Orifice Area (sq. inches)      |                  |                   |                   |                   |                   |                   |                   |                   |

User Input: Vertical Orifice (Circular or Rectangular)

Invert of Vertical Orifice = N/A ft (relative to basin bottom at Stage = 0 ft)  
Depth at top of Zone using Vertical Orifice = N/A ft (relative to basin bottom at Stage = 0 ft)  
Vertical Orifice Diameter = N/A inches

Calculated Parameters for Vertical Orifice  
Vertical Orifice Area = N/A  
Vertical Orifice Centroid = N/A

User Input: Overflow Weir (Dropbox with Flat or Sloped Gate and Outlet Pipe OR Rectangular/Trapezoidal Weir and No Outlet Pipe)

Overflow Weir Front Edge Height, H<sub>o</sub> = 2.16 ft (relative to basin bottom at Stage = 0 ft)  
Overflow Weir Bottom Length = 5.00 feet  
Overflow Weir Side Slopes = 4.00 H:V  
Horiz. Length of Weir Sides = N/A feet  
Overflow Gate Type = Type C Gate  
Debris Clogging % = 50%

Calculated Parameters for Overflow Weir  
Height of Gate Upper Edge, H<sub>1</sub> = N/A  
Overflow Weir Slope Length = N/A  
Gate Open Area / 100-yr Orifice Area = N/A  
Overflow Gate Open Area w/o Debris = N/A  
Overflow Gate Open Area w/ Debris = N/A

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

Depth to Invert of Outlet Pipe = N/A ft (distance below basin bottom at Stage = 0 ft)  
Circular Orifice Diameter = N/A inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate  
Outlet Orifice Area = N/A  
Outlet Orifice Centroid = N/A  
Half-Central Angle of Restrictor Plate on Pipe = N/A

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage = 2.25 ft (relative to basin bottom at Stage = 0 ft)  
Spillway Crest Length = 15.00 feet  
Spillway End Slopes = 4.00 H:V  
Freeboard above Max Water Surface = 0.50 feet  
Spillway position relative to Overflow Weir = Offset

Calculated Parameters for Spillway  
Spillway Design Flow Depth = 0.68 feet  
Stage at Top of Freeboard = 3.43 feet  
Basin Area at Top of Freeboard = 1.70 acres  
Basin Volume at Top of Freeboard = 1.39 acre-ft

### Routed Hydrograph Results

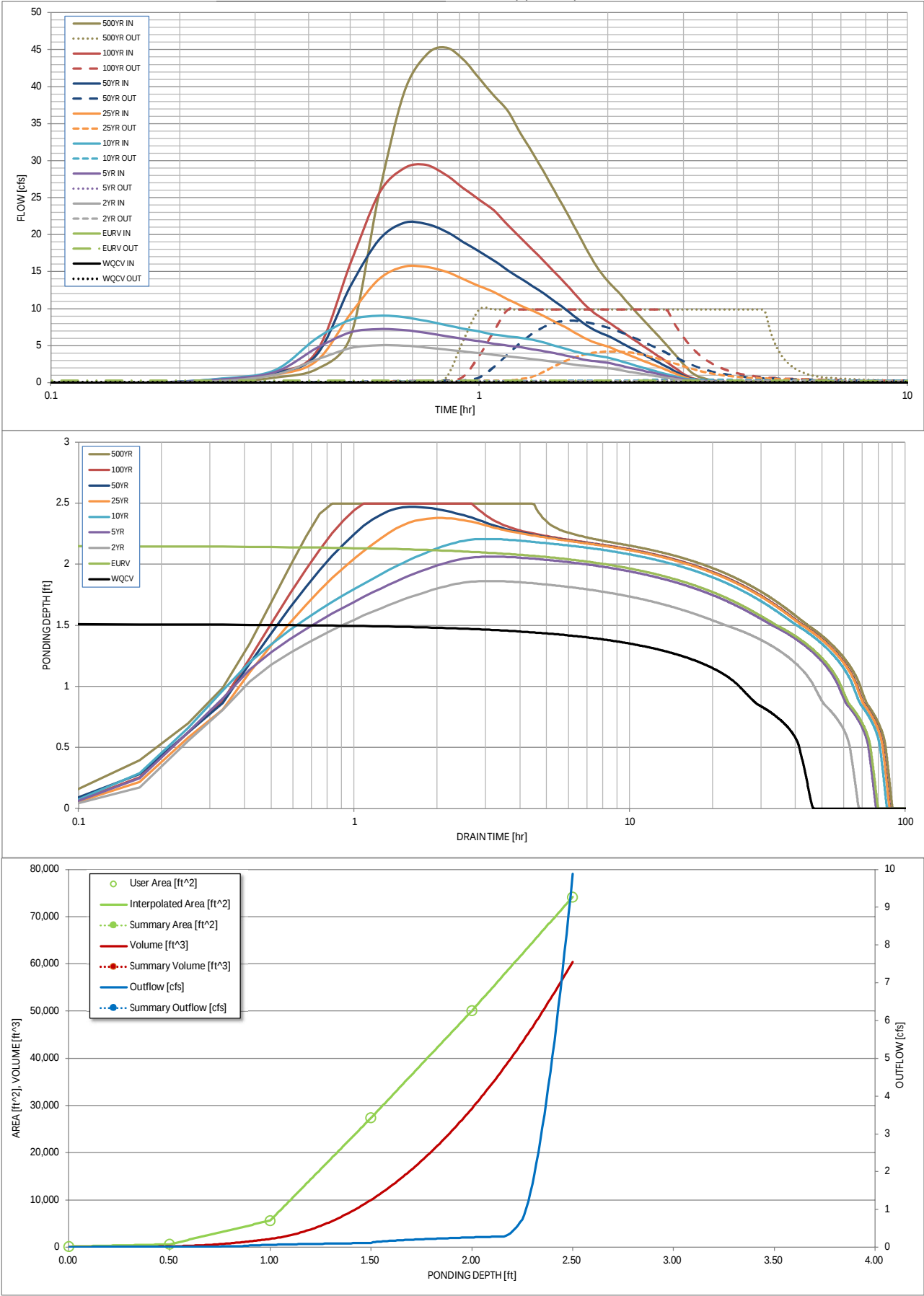
The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).

|                                               | WQCV  | EURV            | 2 Year | 5 Year | 10 Year         | 25 Year  | 50 Year  | 100 Year |
|-----------------------------------------------|-------|-----------------|--------|--------|-----------------|----------|----------|----------|
| Design Storm Return Period                    | N/A   | N/A             | 1.19   | 1.50   | 1.75            | 2.00     | 2.25     | 2.52     |
| One-Hour Rainfall Depth (in)                  | N/A   | N/A             | 1.19   | 1.50   | 1.75            | 2.00     | 2.25     | 2.52     |
| CUHP Runoff Volume (acre-ft)                  | 0.238 | 0.862           | 0.579  | 0.812  | 1.016           | 1.593    | 2.134    | 2.863    |
| Inflow Hydrograph Volume (acre-ft)            | N/A   | N/A             | 0.579  | 0.812  | 1.016           | 1.593    | 2.134    | 2.863    |
| CUHP Predevelopment Peak Q (cfs)              | N/A   | N/A             | 0.5    | 1.0    | 1.4             | 6.2      | 11.3     | 18.2     |
| OPTIONAL Override Predevelopment Peak Q (cfs) | N/A   | N/A             |        |        |                 |          |          |          |
| Predevelopment Unit Peak Flow, q (cfs/acre)   | N/A   | N/A             | 0.02   | 0.03   | 0.04            | 0.17     | 0.32     | 0.51     |
| Peak Inflow Q (cfs)                           | N/A   | N/A             | 5.1    | 7.3    | 9.1             | 15.7     | 21.6     | 29.4     |
| Peak Outflow Q (cfs)                          | 0.1   | 0.3             | 0.2    | 0.3    | 0.5             | 4.3      | 8.4      | 9.9      |
| Ratio Peak Outflow to Predevelopment Q        | N/A   | N/A             | N/A    | 0.3    | 0.3             | 0.7      | 0.7      | 0.5      |
| Structure Controlling Flow                    | Plate | Overflow Weir 1 | Plate  | Plate  | Overflow Weir 1 | Spillway | Spillway | N/A      |
| Max Velocity through Gate 1 (fps)             | N/A   | N/A             | N/A    | N/A    | N/A             | N/A      | N/A      | N/A      |
| Max Velocity through Gate 2 (fps)             | N/A   | N/A             | N/A    | N/A    | N/A             | N/A      | N/A      | N/A      |
| Time to Drain 97% of Inflow Volume (hours)    | 39    | 62              | 55     | 61     | 67              | 65       | 63       | 60       |
| Time to Drain 99% of Inflow Volume (hours)    | 43    | 72              | 62     | 71     | 77              | 76       | 73       | 70       |
| Maximum Ponding Depth (ft)                    | 1.52  | 2.16            | 1.86   | 2.06   | 2.21            | 2.38     | 2.47     | 2.50     |
| Area at Maximum Ponding Depth (acres)         | 0.65  | 1.33            | 1.00   | 1.22   | 1.37            | 1.57     | 1.67     | 1.70     |
| Maximum Volume Stored (acre-ft)               | 0.243 | 0.872           | 0.524  | 0.745  | 0.926           | 1.191    | 1.337    | 1.387    |

Note: Drainage report narrative states spillway will be activated with 50 yr storm not 25.

DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.08 (April 2026)



| S-A-V-D Chart Axis Override | X-axis | Left Y-Axis | Right Y-Axis |
|-----------------------------|--------|-------------|--------------|
| minimum bound               |        |             |              |
| maximum bound               |        |             |              |

# DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename: \_\_\_\_\_

## Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

|               | SOURCE  | CUHP       | CUHP       | CUHP         | CUHP         | CUHP          | CUHP          | CUHP          | CUHP           | CUHP           |
|---------------|---------|------------|------------|--------------|--------------|---------------|---------------|---------------|----------------|----------------|
| Time Interval | TIME    | WQCV [cfs] | EURV [cfs] | 2 Year [cfs] | 5 Year [cfs] | 10 Year [cfs] | 25 Year [cfs] | 50 Year [cfs] | 100 Year [cfs] | 500 Year [cfs] |
| 5.00 min      | 0:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 0:05:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 0:10:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.03          | 0.00           | 0.10           |
|               | 0:15:00 | 0.00       | 0.00       | 0.28         | 0.46         | 0.57          | 0.38          | 0.49          | 0.47           | 0.71           |
|               | 0:20:00 | 0.00       | 0.00       | 1.09         | 1.46         | 1.73          | 1.11          | 1.31          | 1.39           | 1.86           |
|               | 0:25:00 | 0.00       | 0.00       | 3.11         | 4.67         | 6.00          | 2.92          | 3.73          | 4.18           | 6.15           |
|               | 0:30:00 | 0.00       | 0.00       | 4.68         | 6.81         | 8.51          | 9.27          | 13.01         | 16.07          | 25.43          |
|               | 0:35:00 | 0.00       | 0.00       | 5.07         | 7.27         | 9.07          | 14.00         | 19.26         | 25.52          | 39.09          |
|               | 0:40:00 | 0.00       | 0.00       | 5.04         | 7.13         | 8.87          | 15.69         | 21.61         | 28.98          | 44.27          |
|               | 0:45:00 | 0.00       | 0.00       | 4.78         | 6.74         | 8.36          | 15.65         | 21.47         | 29.44          | 45.32          |
|               | 0:50:00 | 0.00       | 0.00       | 4.48         | 6.33         | 7.81          | 15.05         | 20.48         | 28.15          | 43.76          |
|               | 0:55:00 | 0.00       | 0.00       | 4.23         | 5.96         | 7.34          | 14.04         | 19.06         | 26.35          | 41.14          |
|               | 1:00:00 | 0.00       | 0.00       | 4.00         | 5.61         | 6.91          | 13.09         | 17.73         | 24.74          | 38.78          |
|               | 1:05:00 | 0.00       | 0.00       | 3.79         | 5.28         | 6.53          | 12.23         | 16.51         | 23.26          | 36.71          |
|               | 1:10:00 | 0.00       | 0.00       | 3.58         | 5.03         | 6.28          | 11.27         | 15.18         | 21.31          | 33.72          |
|               | 1:15:00 | 0.00       | 0.00       | 3.39         | 4.79         | 6.09          | 10.47         | 14.11         | 19.60          | 31.05          |
|               | 1:20:00 | 0.00       | 0.00       | 3.20         | 4.53         | 5.80          | 9.72          | 13.07         | 17.99          | 28.44          |
|               | 1:25:00 | 0.00       | 0.00       | 3.01         | 4.27         | 5.43          | 9.00          | 12.05         | 16.43          | 25.89          |
|               | 1:30:00 | 0.00       | 0.00       | 2.83         | 4.00         | 5.04          | 8.26          | 11.02         | 14.95          | 23.47          |
|               | 1:35:00 | 0.00       | 0.00       | 2.64         | 3.73         | 4.64          | 7.54          | 10.01         | 13.50          | 21.14          |
|               | 1:40:00 | 0.00       | 0.00       | 2.46         | 3.43         | 4.28          | 6.83          | 9.02          | 12.10          | 18.86          |
|               | 1:45:00 | 0.00       | 0.00       | 2.31         | 3.16         | 3.97          | 6.15          | 8.08          | 10.76          | 16.71          |
|               | 1:50:00 | 0.00       | 0.00       | 2.21         | 2.98         | 3.77          | 5.59          | 7.31          | 9.66           | 14.99          |
|               | 1:55:00 | 0.00       | 0.00       | 2.10         | 2.83         | 3.60          | 5.18          | 6.76          | 8.86           | 13.71          |
|               | 2:00:00 | 0.00       | 0.00       | 1.98         | 2.69         | 3.41          | 4.87          | 6.33          | 8.22           | 12.65          |
|               | 2:05:00 | 0.00       | 0.00       | 1.81         | 2.47         | 3.14          | 4.47          | 5.81          | 7.53           | 11.55          |
|               | 2:10:00 | 0.00       | 0.00       | 1.64         | 2.24         | 2.84          | 4.07          | 5.29          | 6.84           | 10.49          |
|               | 2:15:00 | 0.00       | 0.00       | 1.48         | 2.02         | 2.55          | 3.69          | 4.78          | 6.19           | 9.47           |
|               | 2:20:00 | 0.00       | 0.00       | 1.33         | 1.81         | 2.28          | 3.32          | 4.30          | 5.56           | 8.50           |
|               | 2:25:00 | 0.00       | 0.00       | 1.18         | 1.61         | 2.03          | 2.96          | 3.84          | 4.97           | 7.58           |
|               | 2:30:00 | 0.00       | 0.00       | 1.05         | 1.42         | 1.79          | 2.63          | 3.39          | 4.40           | 6.71           |
|               | 2:35:00 | 0.00       | 0.00       | 0.92         | 1.24         | 1.56          | 2.30          | 2.96          | 3.84           | 5.84           |
|               | 2:40:00 | 0.00       | 0.00       | 0.79         | 1.07         | 1.34          | 1.98          | 2.54          | 3.30           | 4.99           |
|               | 2:45:00 | 0.00       | 0.00       | 0.67         | 0.91         | 1.13          | 1.68          | 2.13          | 2.75           | 4.16           |
|               | 2:50:00 | 0.00       | 0.00       | 0.55         | 0.74         | 0.93          | 1.37          | 1.73          | 2.22           | 3.33           |
|               | 2:55:00 | 0.00       | 0.00       | 0.44         | 0.59         | 0.74          | 1.08          | 1.34          | 1.70           | 2.52           |
|               | 3:00:00 | 0.00       | 0.00       | 0.35         | 0.46         | 0.57          | 0.80          | 0.97          | 1.21           | 1.76           |
|               | 3:05:00 | 0.00       | 0.00       | 0.28         | 0.37         | 0.46          | 0.56          | 0.67          | 0.80           | 1.18           |
|               | 3:10:00 | 0.00       | 0.00       | 0.23         | 0.31         | 0.39          | 0.42          | 0.49          | 0.57           | 0.84           |
|               | 3:15:00 | 0.00       | 0.00       | 0.20         | 0.26         | 0.34          | 0.33          | 0.39          | 0.43           | 0.62           |
|               | 3:20:00 | 0.00       | 0.00       | 0.17         | 0.22         | 0.29          | 0.27          | 0.31          | 0.33           | 0.47           |
|               | 3:25:00 | 0.00       | 0.00       | 0.15         | 0.19         | 0.25          | 0.22          | 0.26          | 0.26           | 0.36           |
|               | 3:30:00 | 0.00       | 0.00       | 0.12         | 0.16         | 0.21          | 0.18          | 0.21          | 0.20           | 0.27           |
|               | 3:35:00 | 0.00       | 0.00       | 0.10         | 0.13         | 0.17          | 0.15          | 0.17          | 0.16           | 0.20           |
|               | 3:40:00 | 0.00       | 0.00       | 0.09         | 0.11         | 0.14          | 0.12          | 0.14          | 0.13           | 0.16           |
|               | 3:45:00 | 0.00       | 0.00       | 0.07         | 0.09         | 0.11          | 0.10          | 0.11          | 0.10           | 0.13           |
|               | 3:50:00 | 0.00       | 0.00       | 0.06         | 0.07         | 0.09          | 0.08          | 0.09          | 0.08           | 0.10           |
|               | 3:55:00 | 0.00       | 0.00       | 0.05         | 0.06         | 0.07          | 0.06          | 0.07          | 0.07           | 0.08           |
|               | 4:00:00 | 0.00       | 0.00       | 0.03         | 0.04         | 0.05          | 0.05          | 0.05          | 0.05           | 0.06           |
|               | 4:05:00 | 0.00       | 0.00       | 0.03         | 0.03         | 0.04          | 0.04          | 0.04          | 0.04           | 0.04           |
|               | 4:10:00 | 0.00       | 0.00       | 0.02         | 0.02         | 0.03          | 0.03          | 0.03          | 0.03           | 0.03           |
|               | 4:15:00 | 0.00       | 0.00       | 0.01         | 0.01         | 0.02          | 0.02          | 0.02          | 0.02           | 0.02           |
|               | 4:20:00 | 0.00       | 0.00       | 0.01         | 0.01         | 0.01          | 0.01          | 0.01          | 0.01           | 0.01           |
|               | 4:25:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.01          | 0.00          | 0.01          | 0.00           | 0.00           |
|               | 4:30:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:35:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:40:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:45:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:50:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:55:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:05:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:10:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:15:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:20:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:25:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:30:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:35:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:40:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:45:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:50:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:55:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 6:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |

## DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.08 (April 2026)

### Summary Stage-Area-Volume-Discharge Relationships

The user can create a summary S-A-V-D by entering the desired stage increments and the remainder of the table will populate automatically.

The user should graphically compare the summary S-A-V-D table to the full S-A-V-D table in the chart to confirm it captures all key transition points.

[illegible]

For best results, include the stages of all grade slope changes (e.g. ISV and Floor) from the S-A-V table on Sheet 'Basin'.

Also include the inverts of all outlets (e.g. vertical orifice, overflow grate, and spillway, where applicable).

***APPENDIX E: DRAINAGE MAPS***

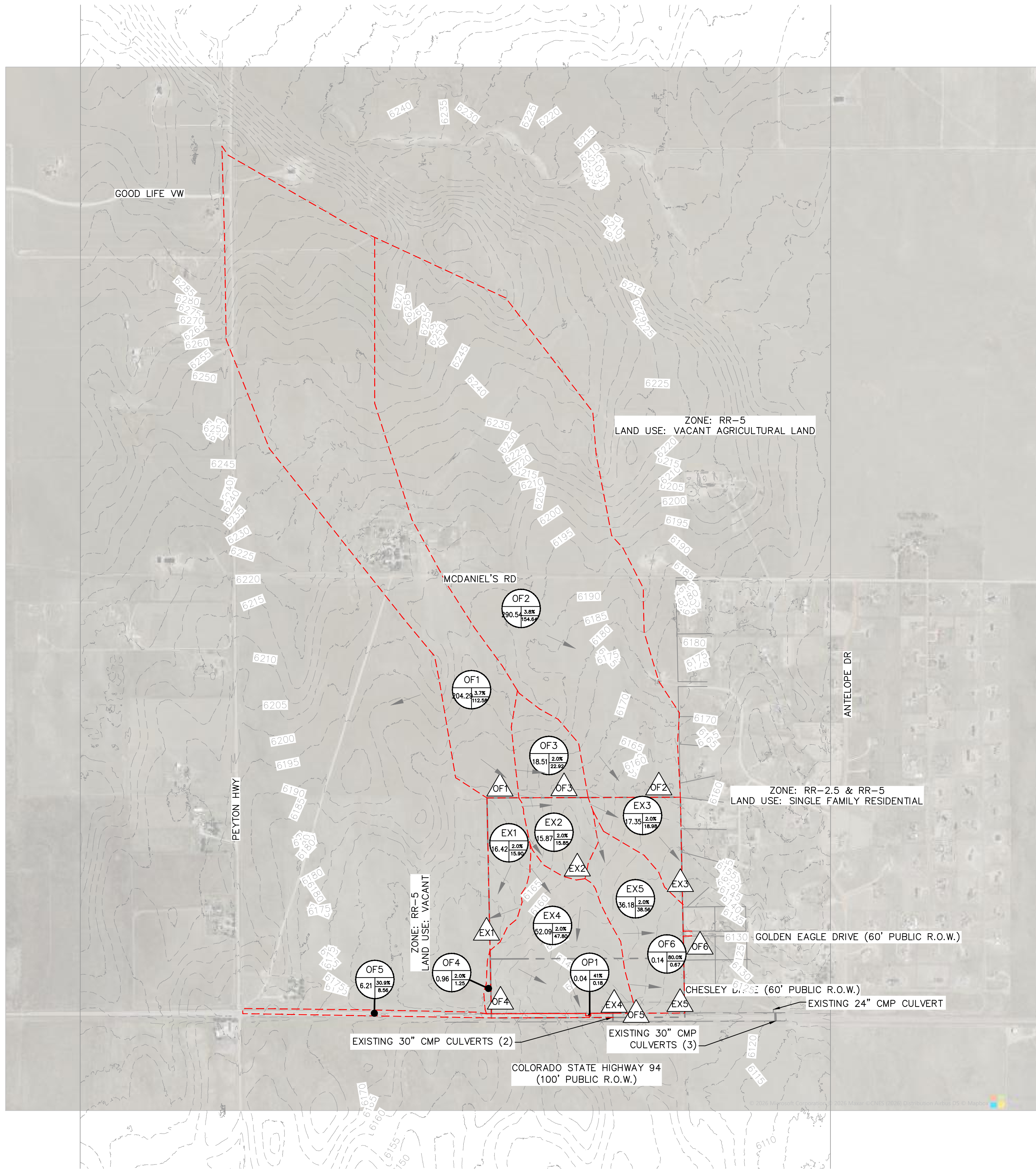
K:\COS\_Civil\096726003\_Trinity Ranch\CADD\Exhibits\2026-0415\_Drainage Maps\EX\_DM\_Extents.dwg Schwenke, DJ 7/31/2026 10:39 AM



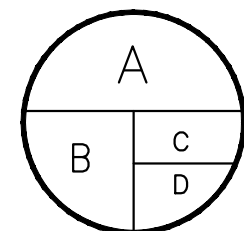
Know what's below.  
Call before you dig.



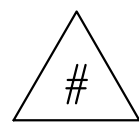
CALL UTILITY NOTIFICATION  
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1-800-922-1987  
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FOR THE MARKING OF UNDERGROUND  
MEMBER UTILITIES



#### LEGEND



A = BASIN DESIGNATION  
B = AREA (ACRES)  
C = BASIN IMPERVIOUSNESS  
D = 100YR DESIGN STORM RUNOFF (CFS)

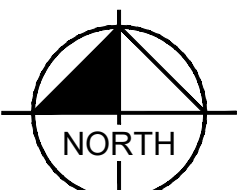


# = DESIGN POINT

EXISTING FLOW DIRECTION  
PROPERTY LINE  
EXISTING ADJACENT LOT LINE  
DRAINAGE BASIN BOUNDARY  
EXISTING MAJOR CONTOUR  
EXISTING MINOR CONTOUR

#### NOTE

\* SEE SHEET 2 - EXISTING DRAINAGE MAP FOR  
EXISTING RATIONAL CALCULATIONS SUMMARY TABLE.



GRAPHIC SCALE IN FEET  
0 100 200 400

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Colorado Springs, Colorado 80903 (719) 453-0180

DESIGNED BY: DJS  
DRAWN BY: MEO  
CHECKED BY: KRK  
DATE: 7/31/26

TRINITY RANCH  
EL PASO COUNTY, COLORADO  
PRELIMINARY PLAN  
EXISTING DRAINAGE MAP - FULL BASIN

PRELIMINARY  
FOR REVIEW ONLY  
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PROJECT NO.  
096726003

SHEET  
1

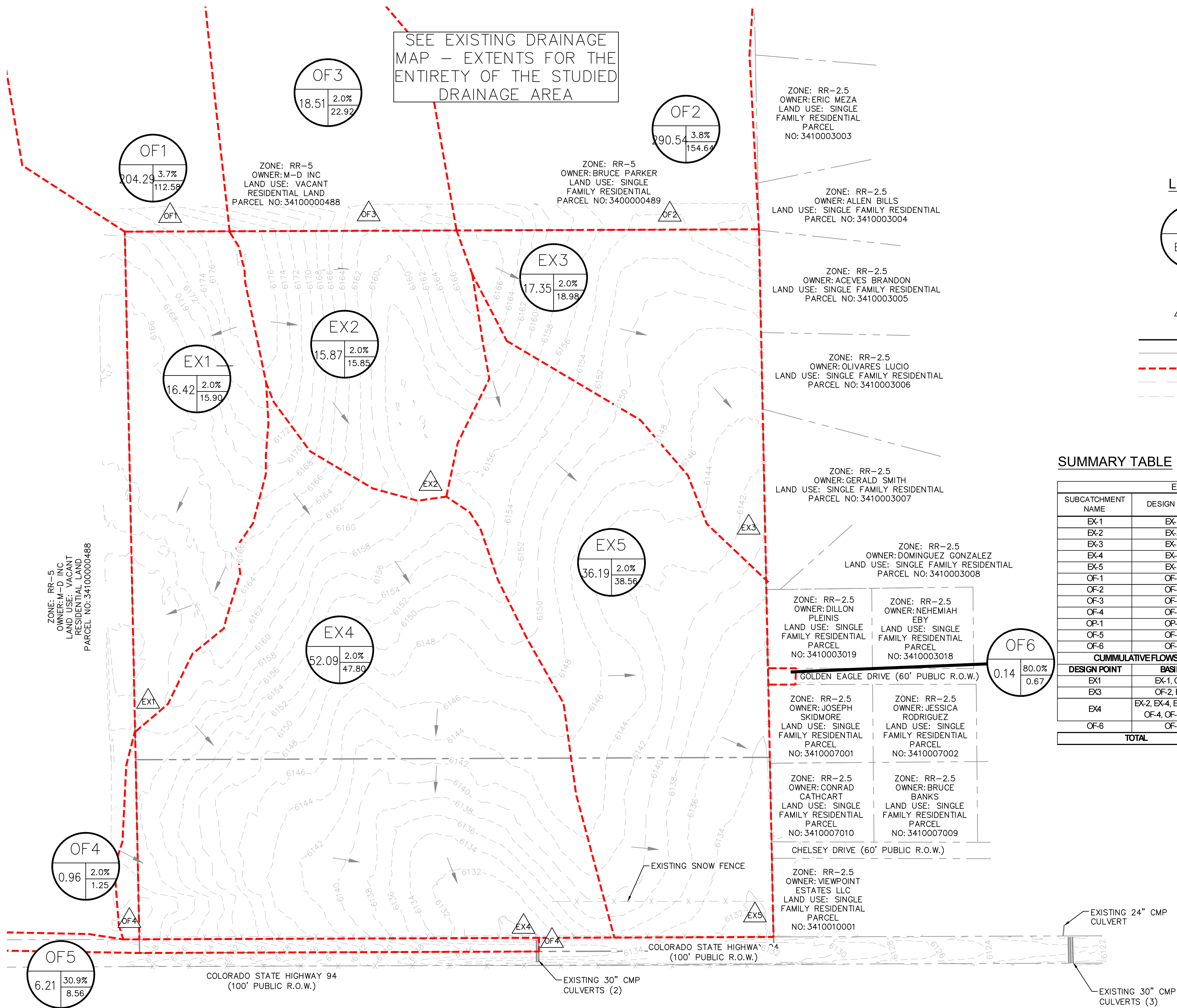
K:\COS\_Civil\096726003\_Trinity Ranch\CADD\Exhibits\2026-0415\_Drainage Maps\EX\_DM.dwg Schwenke, DJ 7/29/2026 11:17 AM



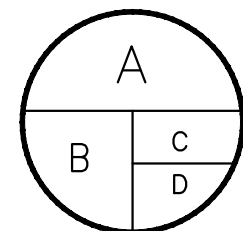
Know what's below.  
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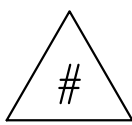
CALL UTILITY NOTIFICATION  
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#### LEGEND



A = BASIN DESIGNATION  
B = AREA (ACRES)  
C = BASIN IMPERVIOUSNESS  
D = 100YR DESIGN STORM RUNOFF (CFS)

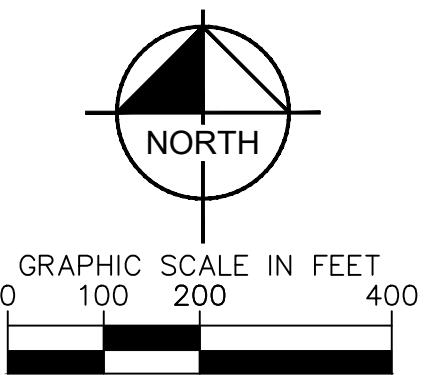


# = DESIGN POINT

EXISTING FLOW DIRECTION  
PROPERTY LINE  
EXISTING ADJACENT LOT LINE  
DRAINAGE BASIN BOUNDARY  
EXISTING MAJOR CONTOUR  
EXISTING MINOR CONTOUR

#### SUMMARY TABLE

| EXISTING RATIONAL CALCULATIONS SUMMARY |                                          |                     |                    |                  |        |
|----------------------------------------|------------------------------------------|---------------------|--------------------|------------------|--------|
| SUBCATCHMENT NAME                      | DESIGN POINT                             | TRIBUTARY AREA (AC) | IMPERVIOUSNESS (%) | PEAK FLOWS (CFS) |        |
|                                        |                                          |                     |                    | Q5               | Q100   |
| EX-1                                   | EX-1                                     | 16.42               | 2.0%               | 2.37             | 15.90  |
| EX-2                                   | EX-2                                     | 15.87               | 2.0%               | 2.36             | 15.85  |
| EX-3                                   | EX-3                                     | 17.35               | 2.0%               | 2.82             | 18.98  |
| EX-4                                   | EX-4                                     | 52.09               | 2.0%               | 7.11             | 47.80  |
| EX-5                                   | EX-5                                     | 36.19               | 2.0%               | 5.74             | 38.56  |
| OF-1                                   | OF-1                                     | 204.29              | 3.7%               | 18.45            | 112.58 |
| OF-2                                   | OF-2                                     | 290.54              | 3.8%               | 25.46            | 154.64 |
| OF-3                                   | OF-3                                     | 18.51               | 2.0%               | 3.41             | 22.92  |
| OF-4                                   | OF-4                                     | 0.96                | 2.0%               | 0.19             | 1.25   |
| OF-1                                   | OF-1                                     | 0.04                | 41.0%              | 0.07             | 0.18   |
| OF-5                                   | OF-5                                     | 6.21                | 30.9%              | 3.01             | 8.56   |
| OF-6                                   | OF-6                                     | 0.14                | 80.0%              | 0.34             | 0.67   |
| CUMULATIVE FLOWS                       |                                          |                     |                    |                  |        |
| DESIGN POINT                           | BASINS                                   | TRIBUTARY AREA (AC) | IMPERV. (%)        | Q5               | Q100   |
| EX1                                    | EX-1, OF-1                               | 220.71              | 3.6%               | 19.77            | 121.43 |
| EX3                                    | OF-2, EX-3                               | 307.90              | 3.7%               | 26.80            | 163.68 |
| EX4                                    | EX-2, EX-4, EX-5, OF-3, OF-4, OF-5, OF-1 | 129.88              | 7.7%               | 15.08            | 127.17 |
| OF-6                                   | OF-6                                     | 0.14                | 80.0%              | 0.34             | 0.67   |
| TOTAL                                  |                                          | 658.62              | 4.8%               | 61.98            | 412.95 |



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DRAWN BY: MEO  
CHECKED BY: KRK  
DATE: 7/29/26

TRINITY RANCH  
EL PASO COUNTY, COLORADO  
PRELIMINARY PLAN  
EXISTING DRAINAGE MAP

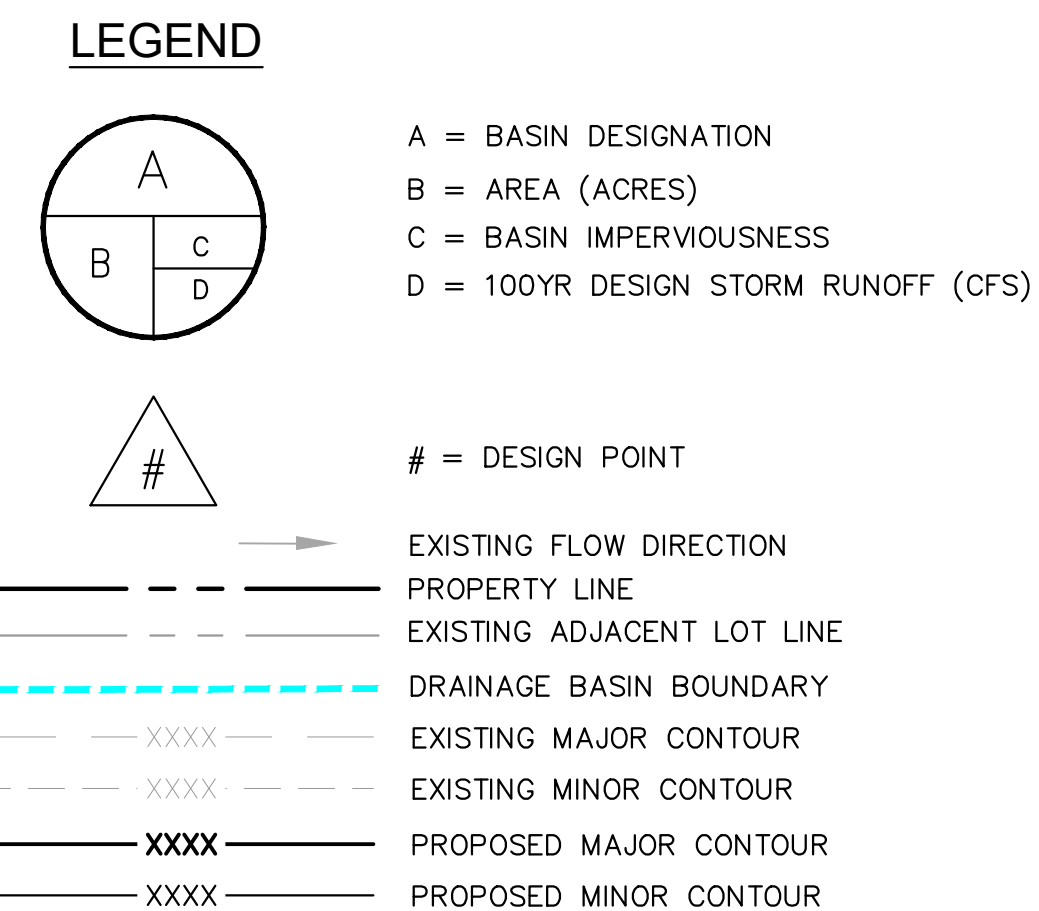
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SHEET

2

NO. BY DATE APPR



| PROPOSED RATIONAL CALCULATIONS SUMMARY |                             |                     |                    |                  |        |
|----------------------------------------|-----------------------------|---------------------|--------------------|------------------|--------|
| SUBCATCHMENT NAME                      | DESIGN POINT                | BASIN AREA (AC)     | IMPERVIOUSNESS (%) | PEAK FLOWS (CFS) |        |
|                                        |                             |                     |                    | Q5               | Q100   |
| PR-1                                   | PR-1                        | 16.17               | 8.1%               | 4.05             | 21.02  |
| PR-2                                   | PR-2                        | 9.55                | 9.9%               | 2.98             | 14.38  |
| PR-3                                   | PR-3                        | 17.72               | 8.9%               | 4.98             | 24.98  |
| PR-4                                   | PR-4                        | 16.42               | 11.5%              | 5.99             | 27.20  |
| PR-5                                   | PR-5                        | 2.08                | 36.6%              | 2.00             | 5.39   |
| PR-6                                   | PR-6                        | 17.78               | 10.3%              | 5.49             | 25.99  |
| PR-7                                   | PR-7                        | 29.21               | 42.2%              | 25.51            | 68.20  |
| PR-8                                   | PR-8                        | 11.31               | 47.6%              | 11.76            | 29.60  |
| PR-9                                   | PR-9                        | 17.68               | 40.7%              | 14.37            | 38.97  |
| OF-1                                   | OF-1                        | 204.29              | 3.7%               | 18.45            | 112.58 |
| OF-2                                   | OF-2                        | 290.54              | 3.8%               | 25.46            | 154.64 |
| OF-3                                   | OF-3                        | 18.51               | 2.0%               | 3.41             | 22.92  |
| OF-4                                   | OF-4                        | 0.96                | 2.0%               | 0.19             | 1.25   |
| OP-1                                   | OP-1                        | 0.04                | 46.0%              | 0.08             | 0.20   |
| OF-5                                   | OF-5                        | 6.21                | 30.9%              | 3.01             | 8.56   |
| OF-6                                   | OF-6                        | 0.14                | 84.3%              | 0.42             | 0.81   |
| CUMULATIVE FLOWS                       |                             |                     |                    |                  |        |
| DESIGN POINT                           | BASINS                      | TRIBUTARY AREA (AC) | IMPERV. (%)        | Q5               | Q100   |
| PR1                                    | PR1+OF1                     | 220.46              | 4.1%               | 20.30            | 122.16 |
| PR3                                    | OF2+PR3                     | 308.26              | 4.1%               | 27.50            | 164.88 |
| PR8                                    | OF3+OF4+PR2+PR4+PR5+PR7+PR8 | 88.04               | 24.6%              | 49.08            | 155.00 |
| PR9                                    | PR6+PR9                     | 35.46               | 25.5%              | 19.19            | 61.78  |
| OF5                                    | OF5+OP1                     | 6.25                | 31.0%              | 3.04             | 8.63   |
| OF-6                                   | OF-6                        | 0.14                | 84.3%              | 0.42             | 0.81   |
| TOTAL CUMULATIVE FLOWS                 |                             | 658.62              | 8.3%               | 119.53           | 513.26 |

TRINITY RANCH  
LAS PASE COUNTY, COLORADO  
PRELIMINARY PLAN  
PROPOSED DRAINAGE MAP

SHEET  
3

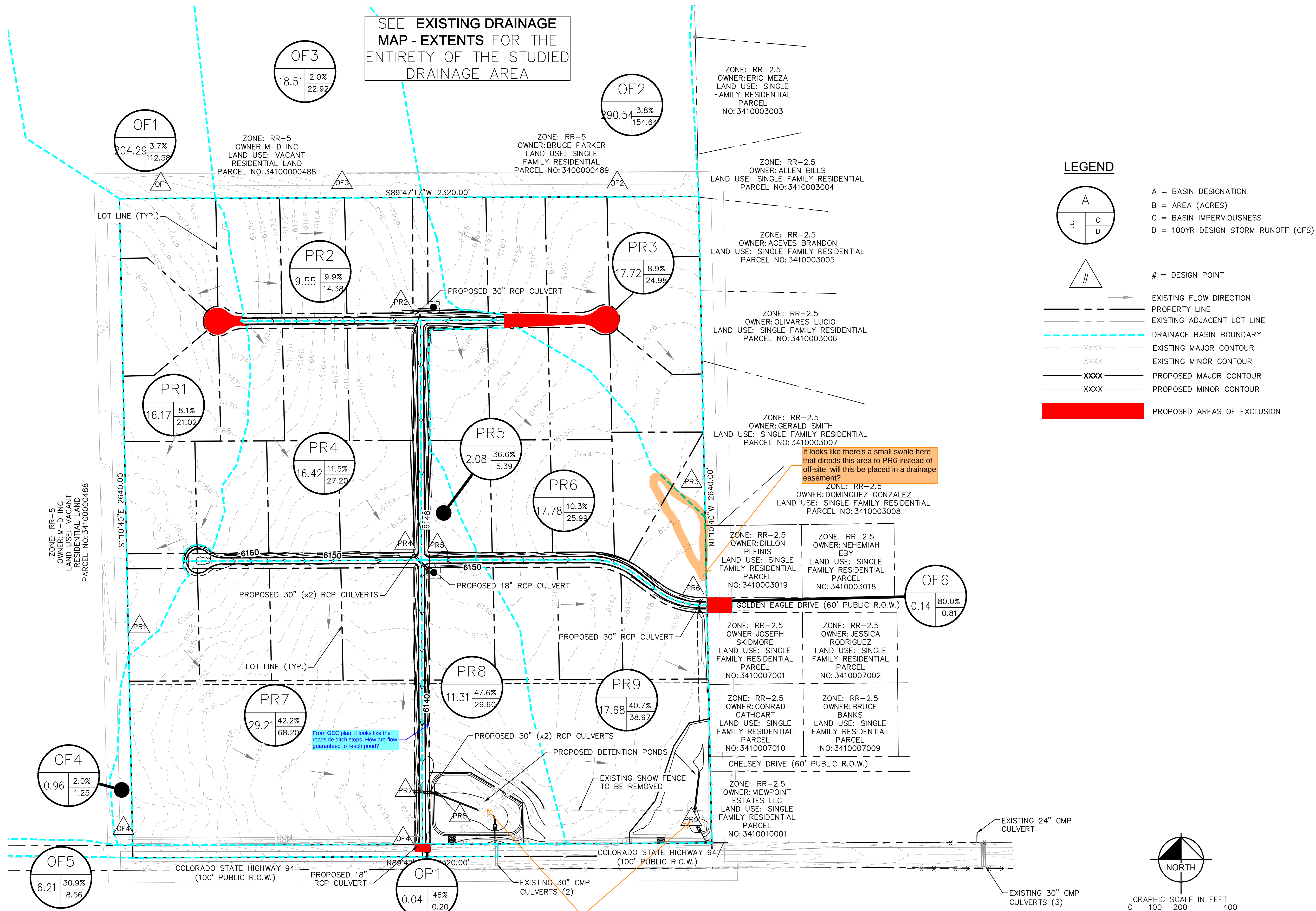
K:\COS\_Civil\096726003\_Trinity Ranch\CADD\Exhibits\2026-0415\_Drainage Maps\PR\_DM\_Exclusion.dwg Schwenke, DJ 7/29/2026 11:17 AM



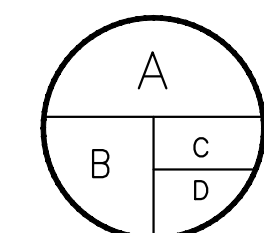
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LEGEND



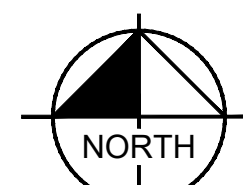
- A = BASIN DESIGNATION
- B = AREA (ACRES)
- C = BASIN IMPERVIOUSNESS
- D = 100YR DESIGN STORM RUNOFF (CFS)



# = DESIGN POINT

- EXISTING FLOW DIRECTION
- PROPERTY LINE
- EXISTING ADJACENT LOT LINE
- DRAINAGE BASIN BOUNDARY
- EXISTING MAJOR CONTOUR
- EXISTING MINOR CONTOUR
- PROPOSED MAJOR CONTOUR
- PROPOSED MINOR CONTOUR

PROPOSED AREAS OF EXCLUSION



GRAPHIC SCALE IN FEET  
0 100 200 400

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DESIGNED BY: DJS  
DRAWN BY: MEO  
CHECKED BY: KKK  
DATE: 7/29/26

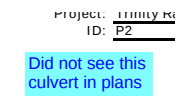
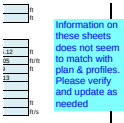
TRINITY RANCH  
EL PASO COUNTY, COLORADO  
PRELIMINARY PLAN  
PROPOSED EXCLUSION AREA MAP

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FOR REVIEW ONLY  
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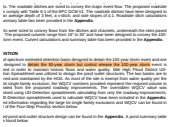
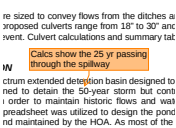
PROJECT NO.  
096726003  
SHEET  
4

# V1\_Drainage Report - Preliminary.pdf Markup Summary

## CDurham (3)

|                                                                                   |                                                                                                                                                                                                                                                                                                        |                                                                                                             |
|-----------------------------------------------------------------------------------|--------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-------------------------------------------------------------------------------------------------------------|
|  | <b>Subject:</b> Text Box<br><b>Page Label:</b> 57<br><b>Author:</b> CDurham<br><b>Date:</b> 9/3/2026 12:10:08 PM<br><b>Status:</b><br><b>Color:</b> <br><b>Layer:</b><br><b>Space:</b>                                | Did not see this culvert in plans                                                                           |
|  | <b>Subject:</b> Text Box<br><b>Page Label:</b> 58<br><b>Author:</b> CDurham<br><b>Date:</b> 9/3/2026 12:13:36 PM<br><b>Status:</b><br><b>Color:</b> <br><b>Layer:</b><br><b>Space:</b>                                | Information on these sheets does not seem to match with plan & profiles. Please verify and update as needed |
|  | <b>Subject:</b> Callout<br><b>Page Label:</b> [4] 4 PROPOSED EXCLUSION AREA MAP<br><b>Author:</b> CDurham<br><b>Date:</b> 9/3/2026 12:03:37 PM<br><b>Status:</b><br><b>Color:</b> <br><b>Layer:</b><br><b>Space:</b> | From GEC plan, it looks like the roadside ditch stops. How are flow guaranteed to reach pond?               |

## EPC Stormwater- Zachary (11)

|                                                                                     |                                                                                                                                                                                                                                                                                                         |                                                                                                   |
|-------------------------------------------------------------------------------------|---------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|---------------------------------------------------------------------------------------------------|
|  | <b>Subject:</b> SW - Textbox with Arrow<br><b>Page Label:</b> 12<br><b>Author:</b> EPC Stormwater- Zachary<br><b>Date:</b> 9/1/2026 3:00:07 PM<br><b>Status:</b><br><b>Color:</b> <br><b>Layer:</b><br><b>Space:</b> | Pond calcs use pcm identifiers pond 1/2, please revise for consistent naming throughout documents |
|  | <b>Subject:</b> SW - Highlight<br><b>Page Label:</b> 12<br><b>Author:</b> EPC Stormwater- Zachary<br><b>Date:</b> 9/1/2026 3:00:33 PM<br><b>Status:</b><br><b>Color:</b> <br><b>Layer:</b><br><b>Space:</b>          | detain the 50-year storm but control release the 100-year storm                                   |
|  | <b>Subject:</b> SW - Textbox with Arrow<br><b>Page Label:</b> 12<br><b>Author:</b> EPC Stormwater- Zachary<br><b>Date:</b> 9/1/2026 3:07:14 PM<br><b>Status:</b><br><b>Color:</b> <br><b>Layer:</b><br><b>Space:</b> | Calcs show the 25 yr passing through the spillway                                                 |

the two proposed detention I  
quality treatment, and maintain  
I.6.B.5 now with  
appendix I update  
ature Volume – Permanent v  
ary for the Project. Two (2) Fi  
s not excluded with either I  
on I.7.B.5: Large Lot Single f  
om water quality. In response

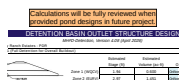
**Subject:** SW - Textbox with Arrow  
**Page Label:** 13  
**Author:** EPC Stormwater- Zachary  
**Date:** 9/1/2026 2:36:58 PM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

I.6.B.5 now with appendix I update



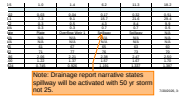
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**Page Label:** 13  
**Author:** EPC Stormwater- Zachary  
**Date:** 9/1/2026 2:40:32 PM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

Appendix I.6.3.A.1.a



**Subject:** SW - Textbox  
**Page Label:** 66  
**Author:** EPC Stormwater- Zachary  
**Date:** 9/1/2026 2:48:04 PM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

Calculations will be fully reviewed when provided pond designs in future project.



**Subject:** SW - Textbox with Arrow  
**Page Label:** 73  
**Author:** EPC Stormwater- Zachary  
**Date:** 9/1/2026 2:57:53 PM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

Note: Drainage report narrative states spillway will be activated with 50 yr storm not 25.

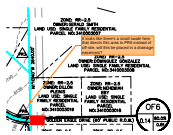


**Subject:** SW - Textbox  
**Page Label:** 73  
**Author:** EPC Stormwater- Zachary  
**Date:** 9/1/2026 2:49:26 PM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

Calculations will be fully reviewed when provided pond designs in future project.

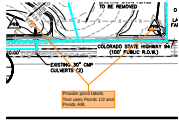


**Subject:** SW - Highlight  
**Page Label:** [4] 4 PROPOSED EXCLUSION AREA MAP  
**Author:** EPC Stormwater- Zachary  
**Date:** 9/1/2026 2:17:30 PM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**



**Subject:** SW - Textbox with Arrow  
**Page Label:** [4] 4 PROPOSED EXCLUSION AREA MAP  
**Author:** EPC Stormwater- Zachary  
**Date:** 9/1/2026 2:21:28 PM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

It looks like there's a small swale here that directs this area to PR6 instead of off-site, will this be placed in a drainage easement?



**Subject:** SW - Textbox with Arrow  
**Page Label:** [4] 4 PROPOSED EXCLUSION AREA MAP  
**Author:** EPC Stormwater- Zachary  
**Date:** 9/1/2026 2:59:12 PM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

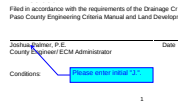
Provide pond labels. Text uses Ponds 1/2 and Ponds A/B.

## Jalal Saleh (8)



**Subject:** Cloud+  
**Page Label:** 1  
**Author:** Jalal Saleh  
**Date:** 9/2/2026 6:13:09 PM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

SP268



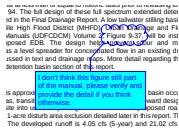
**Subject:** Callout  
**Page Label:** 2  
**Author:** Jalal Saleh  
**Date:** 9/2/2026 1:11:54 PM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

Please enter initial "J.".



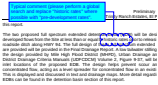
**Subject:** Cloud+  
**Page Label:** 7  
**Author:** Jalal Saleh  
**Date:** 9/3/2026 2:33:45 PM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

Typical comment: Verify if you are following Table 3-1. Typical Values of Percent Impervious of the ECM. The overall percentage is not necessary, You should document the impervious percentage on the lot itself.



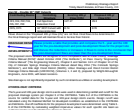
**Subject:** Cloud+  
**Page Label:** 8  
**Author:** Jalal Saleh  
**Date:** 9/2/2026 4:37:07 PM  
**Status:**  
**Color:** ■  
**Layer:**  
**Space:**

I don't think this figure still part of the manual, please verify and provide the detail if you think otherwise.



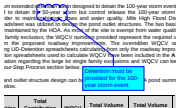
**Subject:** Cloud+  
**Page Label:** 8  
**Author:** Jalal Saleh  
**Date:** 9/2/2026 4:40:33 PM  
**Status:**  
**Color:**    
**Layer:**  
**Space:**

Typical comment (please perform a global search and replace "historic rates" where possible with "pre-development rates".



**Subject:** Callout  
**Page Label:** 11  
**Author:** Jalal Saleh  
**Date:** 9/3/2026 2:39:28 PM  
**Status:**  
**Color:**    
**Layer:**  
**Space:**

Please provide a table that provides and compares the 5 - year and the 100 year for the pre-development and post-development flows for the project site and discuss the reductions or increases in flows to come to the conclusion that the post-development flows are lower than the pre-development flows.



**Subject:** Cloud+  
**Page Label:** 12  
**Author:** Jalal Saleh  
**Date:** 9/2/2026 4:21:56 PM  
**Status:**  
**Color:**    
**Layer:**  
**Space:**

Detention must be provided for the 100- year storm event.



**Subject:** Cloud+  
**Page Label:** 13  
**Author:** Jalal Saleh  
**Date:** 9/2/2026 4:35:57 PM  
**Status:**  
**Color:**    
**Layer:**  
**Space:**

The project is in the TELEPHONE EXCHANGE basin and the Basin Fee and the Bridge Fee are applicable; the Basin fee is \$15,323 and the Bridge fee is \$359 per impervious area.