

**FINAL DRAINAGE REPORT  
FOR  
LOT 5 OF CLEARWAY FILING NO. 2  
EL PASO COUNTY, COLORADO**

JUNE 2022

Prepared for:  
**WIENUT HOME SERVICES**  
6395 E Platte Ave.  
Colorado Springs, CO 80915  
(719)-227-0500

Prepared by:



212 N. Wahsatch, Suite 305  
Colorado Springs, CO 80903  
(719) 955-5485

Project #44-042

PCD Project No. SF-XX-XXX

**FINAL DRAINAGE REPORT FOR  
LOT 5 OF CLEARWAY FILING NO. 2**

**DRAINAGE PLAN STATEMENTS**

**ENGINEERS STATEMENT**

The attached drainage plan and report was prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the County for drainage reports and said report is in conformity with the applicable master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omission on my part in preparing this report.

\_\_\_\_\_  
Virgil A. Sanchez, P.E. #37160  
For and on Behalf of M&S Civil Consultants, Inc

**DEVELOPER'S STATEMENT**

I, the developer have read and will comply with all the requirements specified in this drainage report and plan.

BY: \_\_\_\_\_

TITLE: \_\_\_\_\_

DATE: \_\_\_\_\_

ADDRESS: Wirenut Home Services  
6395 E. Platte Ave.  
Colorado Springs, CO 80915

**EL PASO COUNTY'S STATEMENT**

Filed in accordance with the requirements of El Paso County Land Development Code, Drainage Criteria Manual Volumes 1 and 2, and the Engineering Manual, as amended.

BY: \_\_\_\_\_  
Jennifer Irvine, P.E.  
County Engineer

DATE: \_\_\_\_\_

**CONDITIONS:**

**FINAL DRAINAGE REPORT FOR  
LOT 5 OF CLEARWAY FILING NO. 2**

**TABLE OF CONTENTS**

PURPOSE	4
GENERAL LOCATION AND DESCRIPTION	4
SOILS	4
HYDROLOGIC CALCULATIONS	5
HYDRAULIC CALCULATIONS	5
FLOODPLAIN STATEMENT	5
DRAINAGE CRITERIA	5
FOUR STEP PROCESS	5
EXISTING DRAINAGE CONDITIONS	6
PROPOSED DRAINAGE CONDITIONS	7
WATER QUALITY PROVISIONS AND MAINTENANCE	11
EROSION CONTROL	12
CONSTRUCTION COST OPINION	12
DRAINAGE AND BRIDGE FEES	13
SUMMARY	13
REFERENCES	14

**APPENDIX**

Vicinity Map  
Soils Map  
FIRM Panel  
Hydrologic Calculations  
Hydraulic Calculations / FSD Pond & WQCV Calculations  
Background  
Grading Erosion Control Plan  
Existing/Proposed Drainage Map

# **FINAL DRAINAGE REPORT FOR LOT 5 OF CLEARWAY FILING NO. 2**

## **PURPOSE**

This document is intended to serve as the Final Drainage Report for the Lot 5 of Clearway Filing No. 2. The purpose of this document is to identify and analyze the on and offsite drainage patterns and to ensure that post development runoff is routed through the site safely and in a manner that satisfies the requirements set forth by the El Paso County Drainage Criteria Manual. The development plan for Lot 5 will consist of asphalt parking lots, an office/warehouse building, asphalt storage, lighting, utility infrastructure, and landscaping. A Sand Filter Basin (Pond 1) is proposed to provide on-site water quality and detention. The parcel is zoned "CS CAD-O" and the proposed use is permissible within the commercial zoning criteria.

## **GENERAL LOCATION AND DESCRIPTION**

Lot 5 of Clearway Filing No. 2 is located in the north quarter of Section 18, Township 14 South, Range 65 West of the 6th P.M. in El Paso County, Colorado. The parcel is bound to the north by existing commercial buildings approximately 6 feet from the northern boundary, and the East Fork Sand Creek Sub-tributary to the south and to the east by Cherokee Metropolitan District property, and to the west by City of Colorado Springs property and northwest by The Wrangler Mobile Home Park. As shown on the enclosed FIRM panel, a channel known as the East Fork of Sand Creek Sub-tributary flows from north to south approximately 15 feet from the eastern boundary of the site. The site is located within the greater Sand Creek Drainage Basin and is tributary to the Sand Creek Channel via the East Fork Sand Creek Sub-Tributary. A vicinity map showing the location of the proposed development has been provided in the appendix of this report.

The proposed development and improvements will be constructed on approximately 1.00 acres of the 2.97-acre parcel. The site is currently zoned "CS CAD-O" which is associated with commercial development. In the existing condition, both the parcel and offsite contributing watershed lands are sparsely vegetated, with ground cover consisting primarily of native grasses ranging in density from moderate to good. The proposed development will consist of an asphalt parking area with an office/warehouse building, crushed asphalt storage area, lighting, landscaping, and an access road. Slopes across the development typically range between 2% to 7%. Offsite flows reaching development are contributed in part from areas of The Wrangler Mobile Home Park and the City of Colorado Springs property along the western boundary, from platted commercial property to the north and northeast. Flows produced within the development will be collected by proposed storm sewer improvements, swales, a riprap rundown, and will be routed to a proposed Sand Filter Basin (Pond 1) located at the southern boundary of the development.

## **SOILS**

Soils for this project are delineated by the map in the appendix as Ellicott Loamy Coarse Sand (28) on the southeast corner of the property and Blakeland Loamy Sandy (8) throughout the majority of the property, both of which are characterized as Hydrologic Soil Types "A". Soils in the study area are shown as mapped by Soil Conservation Service in the "Soils Survey of El Paso County Area".



## **HYDROLOGIC CALCULATIONS**

Hydrologic calculations were performed using the El Paso County and City of Colorado Springs Storm Drainage Design Criteria manual and where applicable the Urban Storm Drainage Criteria Manual. The Rational Method was used to estimate stormwater runoff anticipated from design storms with 5-year and 100-year recurrence intervals.

## **HYDRAULIC CALCULATIONS**

Hydraulic calculations were estimated using the Manning's Formula and the methods described in the El Paso County and City of Colorado Springs Storm Drainage Design Criteria manual. The relevant data sheets are included in the appendix of this report.

## **FLOODPLAIN STATEMENT**

A portion of the site lies within the 100 year floodplain according to the Federal Emergency Management Agency (FEMA) Flood Insurance Rate Map (FIRM) Panel No. 08041C0543 F, effective date March 17, 1997 and the more recent FIRM Panel No. 08041C0754 G, effective date December 7, 2018. Base Flood Elevation (BFE) lines from FIRM Panel No. 08041C0754 G (NGVD29) are used for hydraulic calculations, drainage maps, and a discussion within this report. No development is anticipated to occur within the floodplain located at the northwest corner of the site. See Proposed Drainage Map and the FIRM Panels located in the appendix of this report for details. Tract A is provided on the plat for the portion of the lot encumbered by the floodplain. The Floodplain application and Floodplain permit are included in this report, in the Floodplain Map section in the appendix. No portions of the developed lots are within the 100 year flood zone. Additional work will be at the discretion of the local floodplain administrator in accordance with FEMA policy.

## **DRAINAGE CRITERIA**

This drainage analysis has been prepared in accordance with the current El Paso County Drainage Criteria Manual and where applicable the City of Colorado Springs DCM Volume 1 dated May 2014 effective January 2015. Hydrologic calculations were performed to determine runoff quantities for the 5-year and 100-year frequency storms for developed conditions using the Rational Method as required for basins having areas less than 130 acres (in accordance with Chapter 6 of the City of Colorado Springs DCM Volume 1). Full spectrum detention facilities have been designed in accordance with Section 3.2.1. of Chapter 13 of the City of Colorado Springs DCM Volume 1, dated May 2014, effective January 31, 2015 and Urban Drainage and Flood Control District Manuals dated January 2016.

## **FOUR STEP PROCESS**

**Step 1: Employ Runoff Reduction Practices.** – Approximately 0.5 acres of the proposed, 2.97 acre development is being set aside for a Sand Filter Basin. Whenever possible, runoff produced within developed areas containing impervious surfaces will be routed through landscaped areas or earthen swales (grass-lined where slope exceeds 2%) to minimize direct connection of impervious surfaces.

**Step 2: Stabilize drainage ways** –The Lot 5 at Clearway Filing No. 2 site, proposes a Full Spectrum Detention (FSD) Pond to control developed runoff that is discharging to the East Fork Sand Creek

Sub-Tributary located at southeastern boundary of the subject site. The FSD outlet structure has been designed to drain the water quality event storm in 40 hours, while reducing the 100 year peak discharge to approximately 90% of the predevelopment conditions. The development of this site is not anticipated to have negative effects on downstream drainageways. The existing channel embankment has been stabilized at the FSD pond's emergency spillway and where the outlet pipe from the pond enters the channel. The existing channel is to remain, and no improvements are necessary for this reach of the channel (See "Referenced Reports" in the Appendix).

**Step 3: Provide water quality capture volume.** – A Full Spectrum Detention Pond is proposed to reduce peak discharge rates and provide water quality treatment. The WQCV will be released over a 40 hour period while larger event storms will be released in periods of times between 64-80 hours.

**Step 4: Consider Need for Industrial and Commercial BMP's** – This submittal provides a final grading and erosion control plans with BMPs in place. The proposed project will use silt fence, inlet protection, straw bales, a vehicle tracking control pad, and concrete washout area, mulching and reseeding to mitigate the potential for erosion across the site. DL Holdings, LLC shall be responsible for existing and potentially necessary the BMPs for the site including staging, storage and stockpile areas as determined by the contractor. Individual lot owners will be responsible for additional permanent BMPs if necessary because of site uses.

## EXISTING DRAINAGE CONDITIONS

Lot 5 of Clearway Filing No. 2 site consists of 2.97 acres situated north and west of the East Fork Sub-tributary of Sand Creek. There are no existing structures within the site. In accordance with El Paso County's Engineering Criteria Manual (ECM) and Drainage Criteria Manual's (DCM Vol. 1 & 2), an existing conditions hydrologic analysis was performed to determine existing flow quantities entering and exiting the subject site so a comparison to post development discharge rates could be made. As shown on the enclosed Existing Drainage Map (located in the appendix of this report) the existing site terrain within the parcel generally slopes from north to south at grades that vary between 2% to 15%. An existing 6-8" concrete retaining wall lies approximately 6-12 feet from the northern boundary of the site and protects a portion of the site from erosion effects from the offsite, commercial area runoff from the north. The East Fork Sand Creek Sub-Tributary continues from north to south approximately 10 feet from the eastern boundary of the site. It was observed that existing channel banks appear to be stable with established vegetation and minimal scour. The existing channel is to remain, and no improvements have been determined to be necessary for this reach of the channel (See "Background" in the Appendix). An overlay of the 100 yr floodplain (Zone AE) is shown on the Floodplain Map in the appendix, of which 0.28 acres overlaps the southeast corner of the site. Refer to the enclosed Existing Drainage Map in the appendix for visual representation of the detailed, existing drainage patterns discussed below.

## Detailed Drainage Discussion

**Design Point 1 ((DP1),** Q5 = 7.3 cfs, Q100 = 14.0 cfs) receives runoff produced by **Basin D** (Q5 = 7.3 cfs, Q100 = 14.0 cfs), which consists of commercial, gravel and native grass covered platted land located along the northeast parcel property boundary. Runoff produced by **Basin D** is conveyed as sheet flow and earthen swale to the east towards **Design Point 1**. These flows will be routed via a retaining wall to **Design Point 2**.

**Design Point 2 ((DP2),** Q5 = 22.5 cfs, Q100 = 42.3 cfs) receives runoff produced by **Basin B** (Q5 = 8.9 cfs, Q100 = 16.6 cfs), **Basin C** (Q5 = 8.3 cfs, Q100 = 15.4 cfs) and **DP 1**. These basins consist of platted commercial lots and a 30 foot street for ingress/egress. Flows produced by **DP1** join with flows from **Basin C** and are conveyed by a retaining wall along the south border of **Basin C**. Runoff produced by **Basins B and Basin C** is conveyed as sheet flow towards **Design Point 2**. Runoff from **Design Point 2** continues southeast towards **Basin F**.

**Design Point 3 ((DP3),** Q5 = 22.8 cfs, Q100 = 44.6 cfs) receives runoff produced by **DP 2** and **Basin F** (Q5 = 0.3 cfs, Q100 = 2.5 cfs), which consists of native grass covered platted land located northeastern portion of the property. Runoff from these basins is conveyed as sheet flow to the southeast and is released on the southeast boundary of **Basin F** and routed southeast towards **Design Point 3**. This runoff outfalls into the East Fork Sand Creek Sub-Tributary.

**Design Point 4 ((DP4),** Q5 = 9.3 cfs, Q100 = 27.0 cfs) receives runoff produced by **Basin A** (Q5 = 9.3 cfs, Q100 = 27.0 cfs), which consist of developed gravel and un-developed native grass covered platted land located along the west portion of the property boundary. Runoff produced by **Basin A** is conveyed as sheet flow to the southeast towards **DP 4** on the west portion of the property boundary. Runoff from **DP 4** continues southeast towards **Basin E**.

**Design Point 5 ((DP5),** Q5 = 9.6 cfs, Q100 = 28.9 cfs) receives runoff produced by **DP 4** and **Basin E** (Q5 = 0.3 cfs, Q100 = 2.3 cfs), which consists of native grass covered platted land located at the west portion of the property boundary. Runoff from **DP 4** and **Basin E** is conveyed as sheet flow to the south and southwest and is captured by an existing swale on the western property boundary, then routed southeast towards **DP 5**. This runoff outfalls into the existing channel shared by **Basin G**, which drains southeast to the East Fork Sand Creek Sub-Tributary.

**Design Point 6 ((DP6),** Q5 = 31.0 cfs, Q100 = 72.3 cfs) receives runoff produced by **DP 3, DP 5** and **Basin G** (Q5 = 0.3 cfs, Q100 = 2.5 cfs), which consists of native grass covered platted land located at the southeast portion of the property. Runoff from **DP 3, DP 5** and **Basin G** is conveyed as sheet flow to the southeast and is captured by an existing channel along the southern portion of the property boundary, then is routed east towards **DP 6**. This runoff outfalls southeast to the East Fork Sand Creek Sub-Tributary. The cumulative runoff values are from the onsite flows and do not include the East Fork Sand Creek Sub-Tributary upstream flows. The values provided by FEMA for Sand Creek East Fork Sub-Tributary at confluence with Sand Creek East Fork is 1970 cfs for the 100 year event.

## **PROPOSED DRAINAGE CHARACTERISTICS**

The proposed development and improvements will be constructed on approximately 3.05 acres. The majority of the site has been accounted for as a storage yard and the remaining northern portion identified as Tract C being considered as pastureland/undeveloped is shown on the Proposed Drainage Map. Refer to the Proposed Drainage Map and hydraulic calculations un the Appendix for weighted runoff coefficients of the site. Proposed drainage patterns generally remain consistent with those in the existing condition with surface runoff traveling north to south. A swale is proposed on the western boundary of the site to capture and route offsite runoff south to the Sand Creek East Fork Subtributary. Storm sewer and inlets is proposed, on the north and eastern edge of the site, to capture and route offsite runoff south to the Sand Creek East Fork Subtributary. The onsite runoff, is conveyed via storm sewer and inlets to the proposed FSD pond. The runoff reaching the pond will be detained and discharged via a staged outlet structure and

proposed 24" RCP storm system to the East Fork Sand Creek Sub-Tributary below historic rates. The outfall into the East Fork Sand Creek Sub-Tributary channel is armored with a proposed riprap pad and is grading away from main flows within the channel. Type M riprap protection is also proposed to stabilize the emergency spillway bank and all proposed grading around the outfall. Refer to the Proposed Drainage Map in the appendix for an illustration of the proposed site drainage patterns. All storm sewer, drainage structure and pond are private, and shall be maintained by owner. A detailed description of the proposed drainage characteristics follows:

### **Detailed Drainage Discussion**

#### **Design Point 1: ((DP1), Q5 = 6.8 cfs, Q100 = 12.7 cfs)**

**DP1** consists of 2.30 acres of offsite **Basin B** (Q5 = 6.8 cfs, Q100 = 12.7 cfs). Surface runoff from the existing neighboring Clearway Industrial Park (parking lot, gravel lot, building) within this basin generally flows from north to south as sheet flow and is routed via curb and gutter to a modified triple Denver Type 16 inlet with a mountable grate configuration (**INLET 1**: Q5 = 4.3 cfs, Q100 = 6.6 cfs). The intercepted flows are conveyed east through an 18" PP **Pipe Run 1** (Q5 = 4.3 cfs, Q100 = 6.6 cfs) until they combine with flows from **DP2**. Uncaptured runoff from this design point is conveyed as flow-by, **FB DP1** (Q5 = 2.5 cfs, Q100 = 6.1 cfs) towards **DP2**.

#### **Design Point 2 ((DP2), Q5 = 7.1 cfs, Q100 = 13.2 cfs)**

**DP2** consists of 2.40 acres of offsite **Basin C** (Q5 = 7.1 cfs, Q100 = 13.2 cfs). Runoff from the existing neighboring Clearway Industrial Park (parking lot, gravel lot, building) within this basin travels as sheet flow north to south and is routed via curb and gutter a modified triple Denver Type 16 inlet with a mountable grate configuration (**INLET 2**: Q5 = 4.5 cfs, Q100 = 6.8 cfs) at **DP2**. The intercepted flow combines with flows from **PR1** and are conveyed south through 24" PP **Pipe Run 2** (Q5 = 5.9 cfs, Q100 = 9.7 cfs) to **DP4**. Uncaptured runoff from this design point is conveyed as flow-by, **FB DP2** (Q5 = 2.6 cfs, Q100 = 6.4 cfs) towards **DP4**.

#### **Design Point 3 ((DP3), Q5 = 2.7 cfs, Q100 = 6.4 cfs)**

**DP3** consists of 0.02 acre, offsite **Basin F** (Q5 = 0.1 cfs, Q100 = 0.2 cfs) and **FB DP1**. Runoff from the existing neighboring Clearway Industrial Park (parking lot, gravel lot) within offsite **Basin F** travels as sheet flow south and is routed via curb and gutter a modified triple Denver Type 16 inlet with a mountable grate configuration (**INLET 3**: Q5 = 2.2 cfs, Q100 = 4.1 cfs) at **DP3**. The intercepted flows are routed east through 15" **Pipe Run 3** (Q5 = 2.2 cfs, Q100 = 4.1 cfs) to **DP5**. Uncaptured runoff from this design point is conveyed east as flow-by, **FB DP3** (Q5 = 0.5 cfs, Q100 = 2.3 cfs) to **DP5**.

#### **Design Point 4 ((DP4), Q5 = 1.2 cfs, Q100 = 3.4 cfs)**

**DP4** consists of 0.04 acre, offsite **Basin G** (Q5 = 0.2 cfs, Q100 = 0.4 cfs) and **FB DP2**. Runoff from the existing neighboring Clearway Industrial Park (parking lot, gravel lot, building) within this basin travels as sheet flow north to south and is routed via curb and gutter a modified triple Denver Type 16 inlet with a mountable grate configuration (**INLET 4**: Q5 = 1.0 cfs, Q100 = 2.6 cfs) at **DP4**. The intercepted flow combines with flow from **PR2** and **PR3** and is conveyed south through a 24" **Pipe Run 4** (Q5 = 9.1 cfs, Q100 = 16.4 cfs) to **DP5**. Uncaptured runoff from this design point is conveyed east as flow-by, **FB DP4** (Q5 = 0.2 cfs, Q100 = 0.8 cfs) towards **DP5**.

#### **Design Point 5 ((DP5), Q5 = 4.1 cfs, Q100 = 9.7 cfs)**

**DP5** consists of 0.95 acre, offsite **Basin E** ( $Q_5 = 3.3$  cfs,  $Q_{100} = 6.1$  cfs), **FB DP3** and **FB DP4**. All runoff from the existing neighboring Clearway Industrial Park (parking lot, gravel lot, building) within this basin travels southeast as sheet flow and is routed via curb and gutter a modified triple sump Denver Type 16 inlet with a mountable grate configuration (**INLET 5**:  $Q_5 = 4.1$  cfs,  $Q_{100} = 9.7$  cfs) at **DP5**. The intercepted flows combines with flow from **PR4** and is conveyed southeast through 30" PP **Pipe Run 5** ( $Q_5 = 12.7$  cfs,  $Q_{100} = 30.5$  cfs) to **DP6**.

**Design Point 6 ((DP6),  $Q_5 = 7.5$  cfs,  $Q_{100} = 14.4$  cfs)**

**DP6** consists of 3.18 acre, offsite **Basin D** ( $Q_5 = 7.5$  cfs,  $Q_{100} = 14.4$  cfs). All runoff from the existing neighboring Clearway Industrial Park (parking lot, gravel lot, building) within this basin travels south as sheet flow to a natural swale and is fully captured via proposed Type D sump inlet (**INLET 6**) ( $Q_5 = 7.5$  cfs,  $Q_{100} = 14.4$  cfs) at the design point. These flows are conveyed south through 24" PP **Pipe Run 6** ( $Q_5 = 7.5$  cfs,  $Q_{100} = 14.4$  cfs) and combine with flows from **PR5** at a manhole. The combined flows continue south through a 36" PP **Pipe Run 7 & Pipe Run 8** ( $Q_5 = 18.8$  cfs,  $Q_{100} = 41.4$  cfs) to a manhole at the end of **PR8**.

**Design Point 7 ((DP7),  $Q_5 = 0.8$  cfs,  $Q_{100} = 1.5$  cfs)**

**DP7** consists of 0.19 acre, onsite **Basin I** ( $Q_5 = 0.8$  cfs,  $Q_{100} = 1.5$  cfs). Developed runoff from this basin (parking lot) is conveyed as sheet flow to a low point of the parking lot where a Nyloplast 24" grate inlet (**INLET 7**) intercepts the flows and conveys them west through 12" PP **Pipe Run 23** ( $Q_5 = 0.8$  cfs,  $Q_{100} = 1.5$  cfs). Intercepted runoff is routed to **DP8**.

**Design Point 8 ((DP8),  $Q_5 = 1.3$  cfs,  $Q_{100} = 2.4$  cfs)**

**DP8** consists of 0.33 acre, onsite **Basin H** ( $Q_5 = 1.3$  cfs,  $Q_{100} = 2.4$  cfs). Developed runoff from this basin, parking lot, is fully conveyed as sheet flow to a low point of the parking lot, where a proposed modified single sump Denver Type 16 inlet shall be constructed. The flows entering the inlet will combine with flows from **PR23** and will be directed southwest through 15" PP **Pipe Run 24** ( $Q_5 = 2.0$  cfs,  $Q_{100} = 3.8$  cfs), until the flows combine with roof drain flows from 0.20 acre **Basin K** ( $Q_5 = 0.7$  cfs,  $Q_{100} = 1.4$  cfs).

See below for detailed discussion of proportioned flow approximations from 0.20 acre **Basin K** ( $Q_5 = 0.7$  cfs,  $Q_{100} = 1.4$  cfs) and how they enter the storm system main between **Pipe Runs 24 to 34**.

**Roof Drain Detailed Discussion: Basin K**

The area of the eastern side of the commercial building roof (**Basin K**) was divided into sections and the area of the sections with respect to the area of **Basin K**, determined the portion of runoff to each roof drain. A 6" PP **Pipe Run 25** ( $Q_5 = 0.1$  cfs,  $Q_{100} = 0.2$  cfs) conveys runoff from ~14.3% of the basin to the east, until these flows merge with flows from **PR24** and are conveyed through 15" PP **Pipe Run 26** ( $Q_5 = 2.2$  cfs,  $Q_{100} = 4.1$  cfs) and flow south. A 6" PP **Pipe Run 27** ( $Q_5 = 0.2$  cfs,  $Q_{100} = 0.3$  cfs) conveys runoff from 21.4% of **Basin K** to the east, until these flows merge with flows from **PR26** and are conveyed through 15" PP **Pipe Run 28** ( $Q_5 = 2.3$  cfs,  $Q_{100} = 4.4$  cfs). A 6" PP **Pipe Run 29** ( $Q_5 = 0.2$  cfs,  $Q_{100} = 0.3$  cfs) conveys runoff from 21.4% of **Basin K** to the east, until these flows merge with flows from **PR28** and are conveyed through 18" PP **Pipe Run 30** ( $Q_5 = 2.5$  cfs,  $Q_{100} = 4.7$  cfs). A 6" PP **Pipe Run 31** ( $Q_5 = 0.2$  cfs,  $Q_{100} = 0.3$  cfs) conveys runoff from 21.4% of **Basin K** to the east, until these flows merge with flows from **PR30** and are conveyed through 18" PP **Pipe Run 32** ( $Q_5 = 2.7$  cfs,  $Q_{100} = 5.1$  cfs). A 6" PP **Pipe Run 33** ( $Q_5 = 0.1$  cfs,  $Q_{100} = 0.2$  cfs) conveys runoff from 14.3% of **Basin K** to the east, until these

flows merge with flows from **PR32** and are conveyed through 18" PP **Pipe Run 34** ( $Q_5 = 2.8$  cfs,  $Q_{100} = 5.2$  cfs). Flows from **PR34** are routed to a manhole at the end of **PR34**.

**Design Point 9 ((DP9),  $Q_5 = 1.0$  cfs,  $Q_{100} = 1.9$  cfs)**

**DP9** consists of 0.25 acre, onsite **Basin O** ( $Q_5 = 1.0$  cfs,  $Q_{100} = 1.9$  cfs). Developed runoff from this basin, crushed asphalt lot, is conveyed as sheet flow to a low point of the parking lot at the south boundary of the basin, where a proposed Nyloplast 24" grate inlet shall be constructed. These flows shall then travel southwest through 12" PP **Pipe Run 36** ( $Q_5 = 1.0$  cfs,  $Q_{100} = 1.9$  cfs) to **DP10**.

**Design Point 10 ((DP10),  $Q_5 = 1.8$  cfs,  $Q_{100} = 3.3$  cfs)**

**DP10** consists of 0.40 acre, onsite **Basin N** ( $Q_5 = 1.8$  cfs,  $Q_{100} = 3.3$  cfs). Developed runoff from this basin, crushed asphalt lot, is fully conveyed as sheet flow to a low point of the parking lot at the east boundary of the basin, where a proposed Nyloplast 2'x2' steel bar inlet shall be constructed. These flows will combine with flows from **PR36** and travel southwest through 18" PP **Pipe Run 37 & 18" RCP Pipe Run 38** ( $Q_5 = 2.8$  cfs,  $Q_{100} = 5.2$  cfs) to a low tailwater riprap basin in the Sand Filter Basin at **DP13**.

See below for detailed discussion of proportioned flow approximations from 0.21 acre **Basin J** ( $Q_5 = 0.8$  cfs,  $Q_{100} = 1.5$  cfs) and how they enter the storm system main between **Pipe Runs 9 to 20**.

**Roof Drain Detailed Discussion: Basin J**

The area of the western side of the roof (**Basin J**) was divided into sections and the area of the sections with respect to the area of **Basin J**, determined the portion of runoff to each roof drain. A 6" PP **Pipe Run 9** ( $Q_5 = 0.1$  cfs,  $Q_{100} = 0.2$  cfs) conveys runoff from 13.3% of the basin to the west, then the flows travel south via a 6" PP **PR10** ( $Q_5 = 0.1$  cfs,  $Q_{100} = 0.2$  cfs), until they combine with flow from **PR11**. A 6" PP **Pipe Run 11** ( $Q_5 = 0.2$  cfs,  $Q_{100} = 0.4$  cfs) conveys runoff from 26.7% of **Basin J** to the west, until these flows merge with flows from **PR10** and are conveyed south through a 8" PP **Pipe Run 12** ( $Q_5 = 0.3$  cfs,  $Q_{100} = 0.6$  cfs). Approximately 10% of **Basin J** is paved in asphalt and an area drain fully conveys the flow from this portion south through a 8" PP **PR13** ( $Q_5 = 0.5$  cfs,  $Q_{100} = 1.0$  cfs). A 6" PP **Pipe Run 14** ( $Q_5 = 0.0$  cfs,  $Q_{100} = 0.1$  cfs) conveys runoff from 7.7%% of **Basin J** to the west, until these flows merge with flows from **PR13** and are conveyed through a 12" PP **Pipe Run 15** ( $Q_5 = 0.6$  cfs,  $Q_{100} = 1.1$  cfs). A 6" PP **Pipe Run 16** ( $Q_5 = 0.1$  cfs,  $Q_{100} = 0.3$  cfs) conveys runoff from 20% of **Basin J** to the west, until these flows merge with flows from **PR15** and are conveyed through a 12" PP **Pipe Run 17** ( $Q_5 = 0.7$  cfs,  $Q_{100} = 1.3$  cfs). A 6" PP **Pipe Run 18** ( $Q_5 = 0.1$  cfs,  $Q_{100} = 0.1$  cfs) conveys runoff from 7.7% of **Basin J** to the west, until these flows merge with flows from **PR17** and are conveyed south through a 12" PP **Pipe Run 19 & Pipe Run 20** ( $Q_5 = 0.8$  cfs,  $Q_{100} = 1.5$  cfs) to **DP 11**.

**Design Point 11 ((DP11),  $Q_5 = 0.9$  cfs,  $Q_{100} = 1.5$  cfs)**

**DP11** consists of 0.19 acre, onsite **Basin L** ( $Q_5 = 0.9$  cfs,  $Q_{100} = 1.5$  cfs). Developed runoff from this basin, crushed asphalt lot, is conveyed as sheet flow to a low point of the parking lot at the southwest boundary of the basin, where a proposed Nyloplast 24" grate inlet shall be constructed. Flows conveyed by the inlet at **DP11**, will combine with flows from **Basin J** and be conveyed east through 15" PP **Pipe Run 21** ( $Q_5 = 1.6$  cfs,  $Q_{100} = 3.0$  cfs) to **DP12**.

**Design Point 12 ((DP12),  $Q_5 = 0.6$  cfs,  $Q_{100} = 1.1$  cfs)**

**DP12** consists of 0.13 acre, onsite **Basin M** ( $Q_5 = 0.6$  cfs,  $Q_{100} = 1.1$  cfs). Developed runoff from this basin, crushed asphalt lot, is fully conveyed as sheet flow to a low point of the parking lot at the southeast boundary of the basin, where a proposed Nyloplast 24" grate inlet shall be constructed. Flows conveyed by

the inlet at **DP12** will combine with flows from **PR 21** and be conveyed northeast through a 15" PP **Pipe Run 22** ( $Q_5 = 2.3$  cfs,  $Q_{100} = 4.1$  cfs). Flows from **PR22** combine with flows from **PR34** and are routed via a 24" RCP **Pipe Run 35** ( $Q_5 = 5.0$  cfs,  $Q_{100} = 9.3$  cfs) to a low tailwater riprap basin in the Sand Filter Basin at **DP13**.

**Design Point 13 ((DP13),  $Q_5 = 6.7$  cfs,  $Q_{100} = 12.8$  cfs)**

**DP13** consists of 0.23 acre, onsite **Basin Q** ( $Q_5 = 0.1$  cfs,  $Q_{100} = 0.6$  cfs). Developed runoff from this basin is conveyed to an onsite sand filter basin **Pond 1**. **Pond 1** receives flows from **PR35** ( $Q_5 = 5.0$  cfs,  $Q_{100} = 9.3$  cfs), **PR38** ( $Q_5 = 2.8$  cfs,  $Q_{100} = 5.2$  cfs), and **Basin Q** ( $Q_5 = 0.1$  cfs,  $Q_{100} = 0.6$  cfs). Release rates from **Pond 1** are routed south via an 18" RCP **Pipe Run 39** ( $Q_5 = 0.3$  cfs,  $Q_{100} = 0.3$  cfs), where the flows combine with flows from **PR8** to a 36" RCP **PR40** ( $Q_5 = 19.1$  cfs,  $Q_{100} = 41.7$  cfs) to a low tailwater riprap basin in East Fork Sand Creek Subtributary at **DP16**. See Water Quality Provision for **Pond 1** information.

**Design Point 14 ((DP14),  $Q_5 = 9.4$  cfs,  $Q_{100} = 27.5$  cfs)**

**DP 14** consists of 9.92 acre of offsite **Basin A** ( $Q_5 = 9.3$  cfs,  $Q_{100} = 27.0$  cfs) and onsite undeveloped 0.22 acre **Basin R** ( $Q_5 = 0.1$  cfs,  $Q_{100} = 0.5$  cfs). Runoff from these basins is fully conveyed to a low point on the southeast boundary of **Basin R**. These flows are captured by a proposed Type D sump inlet. These flows are conveyed via by a 30" RCP **Pipe Run 41** ( $Q_5 = 9.4$  cfs,  $Q_{100} = 27.5$  cfs) to a low tailwater riprap basin in East Fork Sand Creek Subtributary at **DP16**.

**Design Point 15 ((DP15),  $Q_5 = 0.1$  cfs,  $Q_{100} = 0.7$  cfs)**

**DP16** consists of 0.26 acre, onsite **Basin P** ( $Q_5 = 0.1$  cfs,  $Q_{100} = 0.7$  cfs). The runoff from this basin flows to the east boundary of the site and then south toward the East Fork Sand Creek Subtributary at **DP16**.

**Design Point 16 (DP16), ( $Q_5 = 28.8$  cfs,  $Q_{100} = 71.5$  cfs)**

**DP16** consists of 0.55 acre, onsite **Basin S** ( $Q_5 = 0.2$  cfs,  $Q_{100} = 1.6$  cfs). **DP16** receives flows from **Basin S** ( $Q_5 = 0.2$  cfs,  $Q_{100} = 1.6$  cfs), **PR40** ( $Q_5 = 19.1$  cfs,  $Q_{100} = 41.7$  cfs), **PR41** ( $Q_5 = 9.4$  cfs,  $Q_{100} = 27.5$  cfs), and **DP15** ( $Q_5 = 0.1$  cfs,  $Q_{100} = 0.7$  cfs). The cumulative flows at **DP16** ( $Q_5 = 28.8$  cfs,  $Q_{100} = 71.5$  cfs) are less than the flows in the existing condition **EX DP6** ( $Q_5 = 31.0$  cfs,  $Q_{100} = 72.3$  cfs). The site will not adversely affect adjacent or downstream properties.

## **WATER QUALITY PROVISIONS AND MAINTENANCE**

A Sand Filter Detention Pond is being proposed for this site to address water quality from 2.11 acres at 85.2% imperviousness. The pond has been sized utilizing MHFD-Detention v4.05 and UD-BMP v3.07 from Urban Drainage and Flood Control District (UDFCD). The pond is not expected to carry future additional flows other than from this project. The pond is being constructed with an outlet control structure which limits the release rate of the pond through the use of weirs and an 18" RCP outlet pipe. The pond has been sized to store the WCQV, EURV, and the flood control volumes for the 2, 5, 10, 25, 50 and 100 year storm events. The WQCV will be slowly released over 12 hours. The maximum WQCV storage volume is 0.051 acre-feet. An overflow emergency spillway is proposed along the northwest embankment to safely convey flows to the existing East Fork Sand Creek Subtributary in the event of outlet clogging. The emergency overflow spillway will be at an elevation of 6254.76 feet and will have a length of 22.0 feet, and a spillway design flow depth of approx. 0.23 feet across the crest (passing 12.8 cfs) should the outlet become clogged. The top of the proposed embankment will need to be constructed at approximately 6256.0 to provide one foot of freeboard. See Proposed Drainage Map in the appendix of this report. The

following table provided below summarizes the peak inflows, outflows, storage volumes and water surface elevations for the water quality, 5 year, EURV and 100 year event storms.

<b>WQCV Pond 1</b>	<b>WQCV</b>	<b>EURV</b>	<b>5 Year</b>	<b>100 Year</b>
Maximum Volume Stored (acre-ft)	0.051	0.242	0.170	0.323
Maximum WS Elevation	6252.28	6254.15	6253.55	6254.75
Peak Inflow (cfs)	N/A	N/A	5.4	10.7
Peak Outflow (cfs)	0.1	0.3	0.3	0.3

The proposed pond will be private and shall be maintained by the property owner. Access shall be granted to the owner and El Paso County for access and maintenance of the private WQCV facility. A private maintenance agreement document shall accompany this report on the next submittal.

## **EROSION CONTROL**

It is the policy of the El Paso County that we submit a grading and erosion control plan with the drainage report. Proposed silt fence, vehicle traffic control, and concrete washout area are proposed as erosion control measures. The costs for these measures have been provided on the Grading and Erosion Control plan.

## **CONSTRUCTION COST OPINION**

Private Drainage Facilities (**NON-Reimbursable**):

<b>Item</b>	<b>Description</b>	<b>Quantity</b>	<b>Unit Cost</b>	<b>Cost</b>
<b>1.</b>	6" PP	181 LF	\$25 /LF	\$4,525.00
<b>2.</b>	8" PP	17 LF	\$35 /LF	\$595.00
<b>3.</b>	12" PP	276 LF	\$45 /LF	\$12,420.00
<b>4.</b>	15" PP	312 LF	\$55 /LF	\$17,160.00
<b>5.</b>	18" PP	238 LF	\$68 /LF	\$16,184.00
<b>6.</b>	24" PP	65 LF	\$81 /LF	\$5,265.00
<b>7.</b>	30" PP	130 LF	\$125 /LF	\$16,250.00
<b>8.</b>	36" PP	357 LF	\$150 /LF	\$53,550.00
<b>9.</b>	18" RCP	55 LF	\$78 /LF	\$4,290.00
<b>10.</b>	24" RCP	27 LF	\$104 /LF	\$2,808.00
<b>11.</b>	30" RCP	70 LF	\$130 /LF	\$9,100.00
<b>12.</b>	36" RCP	32 LF	\$155 /LF	\$4,960.00
<b>13.</b>	18" FES RCP	1 EA	\$923 /EA	\$923.00
<b>14.</b>	24" FES RCP	1 EA	\$1046 /EA	\$1,046.00
<b>15.</b>	30" FES RCP	1 EA	\$1292 /EA	\$1292.00
<b>16.</b>	36" FES RCP	1 EA	\$1845 /EA	\$1845.00
<b>17.</b>	Triple Type 16 Inlet	5 EA	\$11,900 /EA	\$59,500.00
<b>18.</b>	Single Type 16 Inlet	1 EA	\$5900 /EA	\$5,900.00
<b>19.</b>	Type D Inlet	2 EA	\$4800 /EA	\$9,600.00



<b>20.</b>	24" Grate and Drain Basin	4	EA	\$2930	/EA	\$11,720.00
<b>21.</b>	2'x2' Steel Grate and Drain Basin	1	EA	\$2930	/EA	\$2,930.00
<b>22.</b>	Manhole	6	EA	\$6500	/EA	\$39,000.00
<b>23.</b>	Type M riprap, 2' deep Low Tailwater	60	CY	\$65	/CY	\$3,900.00
	FSD Pond (Including Outlet Struct, Spillway Cutoff Wall, Riprap, Signs, Sand Filter Media, Erosion Blanket)	1	LS	\$17,408	/LS	\$17,408.00
<b>Total \$</b>						<b>\$302,171.00</b>
<b>5% Contingency</b>						<b>\$15,108.55</b>
<b>10% Engineering</b>						<b>\$30,217.10</b>
<b>Total\$</b>						<b>\$347,496.65</b>

M & S Civil Consultants, Inc. (M & S) cannot and does not guarantee the construction cost will not vary from these opinions of probable costs. These opinions represent our best judgment as design professionals familiar with the construction industry and this development in particular. The above and below is only an estimate of the facility cost and drainage basin fee amounts in 2022.

#### **DRAINAGE & BRIDGE FEES – CLEARWAY FILING NO. 2, LOT 5**

Fees not required as this Filing was previously platted.

#### **SUMMARY**

Per this final drainage report, the proposed drainage facilities recommended within this report will adequately convey, detain and route runoff from the planned development to the East Fork Sand Creek Sub-Tributary drainage way at peak flow rates which are below existing with no negative impacts on surrounding developments. All drainage facilities described herein and shown on the included Proposed Drainage Map (See Appendix), this final Drainage Report and site construction documents are submitted for simultaneous review. Care will be taken to accommodate overland emergency flow routes on site and temporary drainage conditions. The development of the Clearway Filing No. 2, Lot 5 site will not adversely affect adjacent or downstream properties.

## **REFERENCES**

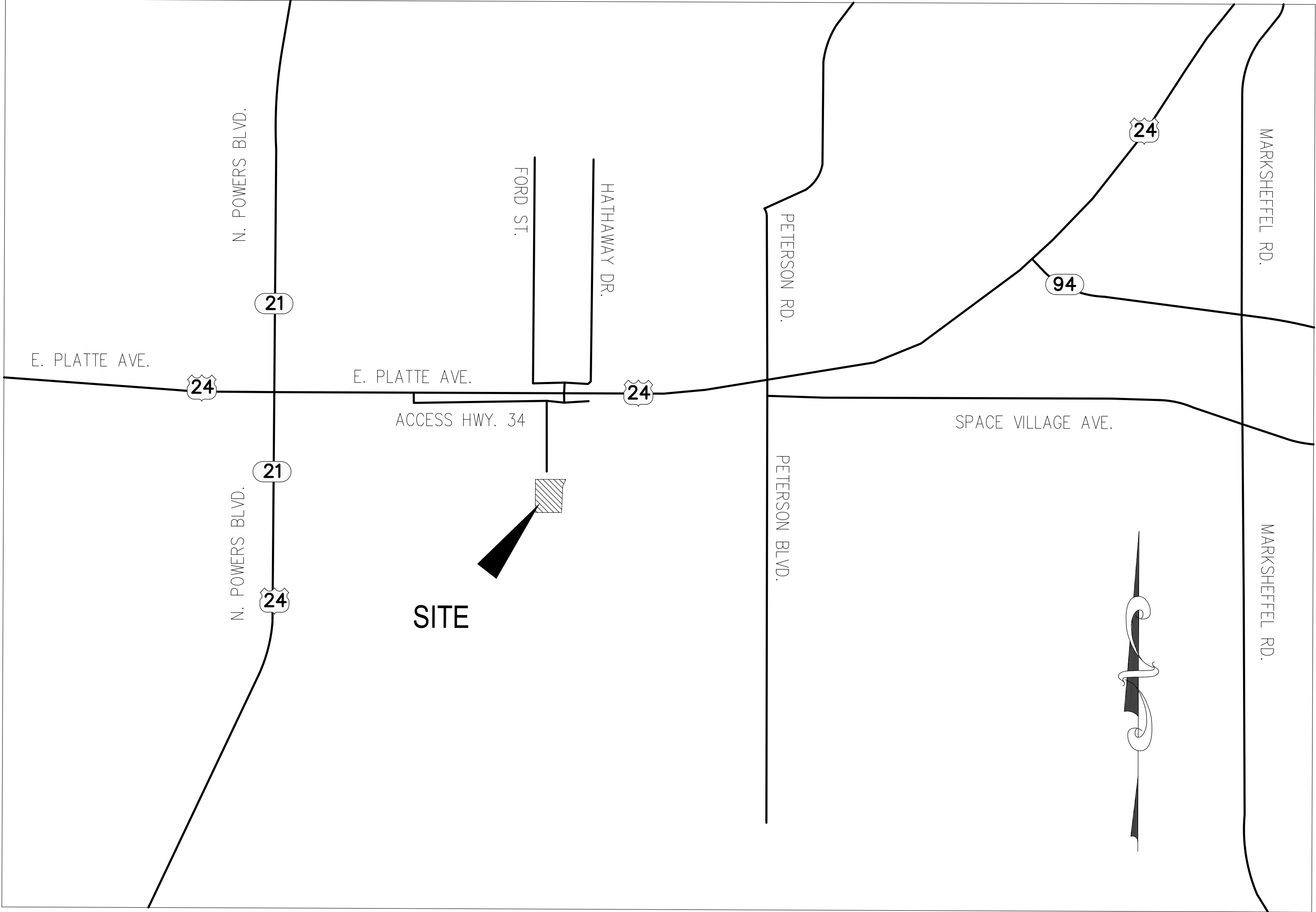
- 1.) "El Paso County and City of Colorado Springs Drainage Criteria Manuals".
- 2.) "Urban Storm Drainage Criteria Manual"
- 3.) SCS Soils Map for El Paso County.
- 4.) Flood Insurance Rate Map (FIRM), Federal Emergency Management Agency (Map No. 08041C0543F), Effective date March 17, 1997.
- 5.) Flood Insurance Rate Map (FIRM), Federal Emergency Management Agency (Map No. 08041C0754G), Effective date December 7, 2018.
- 7.) "Sand Creek Drainage Basin Planning Study, Preliminary Design Report", Revised March 1996, by Kiowa Engineering Corporation.

## **APPENDIX**

## **VICINITY MAP**

# VICINITY MAP

N.T.S.



REVISIONS:		BY: DESCRIPTION:		APP'D. BY:		DATE:	
NO.	DATE:	BY:	DESCRIPTION:	APP'D. BY:	DATE:		

THE ENGINEER PREPARING THESE PLANS WILL NOT BE RESPONSIBLE, OR LIABLE FOR, UNAUTHORIZED CHANGES TO OR USES OF THESE PLANS. ALL CHANGES TO THE PLANS MUST BE IN WRITING AND MUST BE APPROVED BY THE PREPARER OF THESE PLANS.

CAUTION

VIRGIL A. SANCHEZ, COLORADO, P.E. NO. 37160

FOR AND ON BEHALF OF MAS CIVIL CONSULTANTS, INC.

212 N. WAHATCH AVE., STE 305  
COLORADO SPRINGS, CO 80903  
PHONE: 719.555.5485

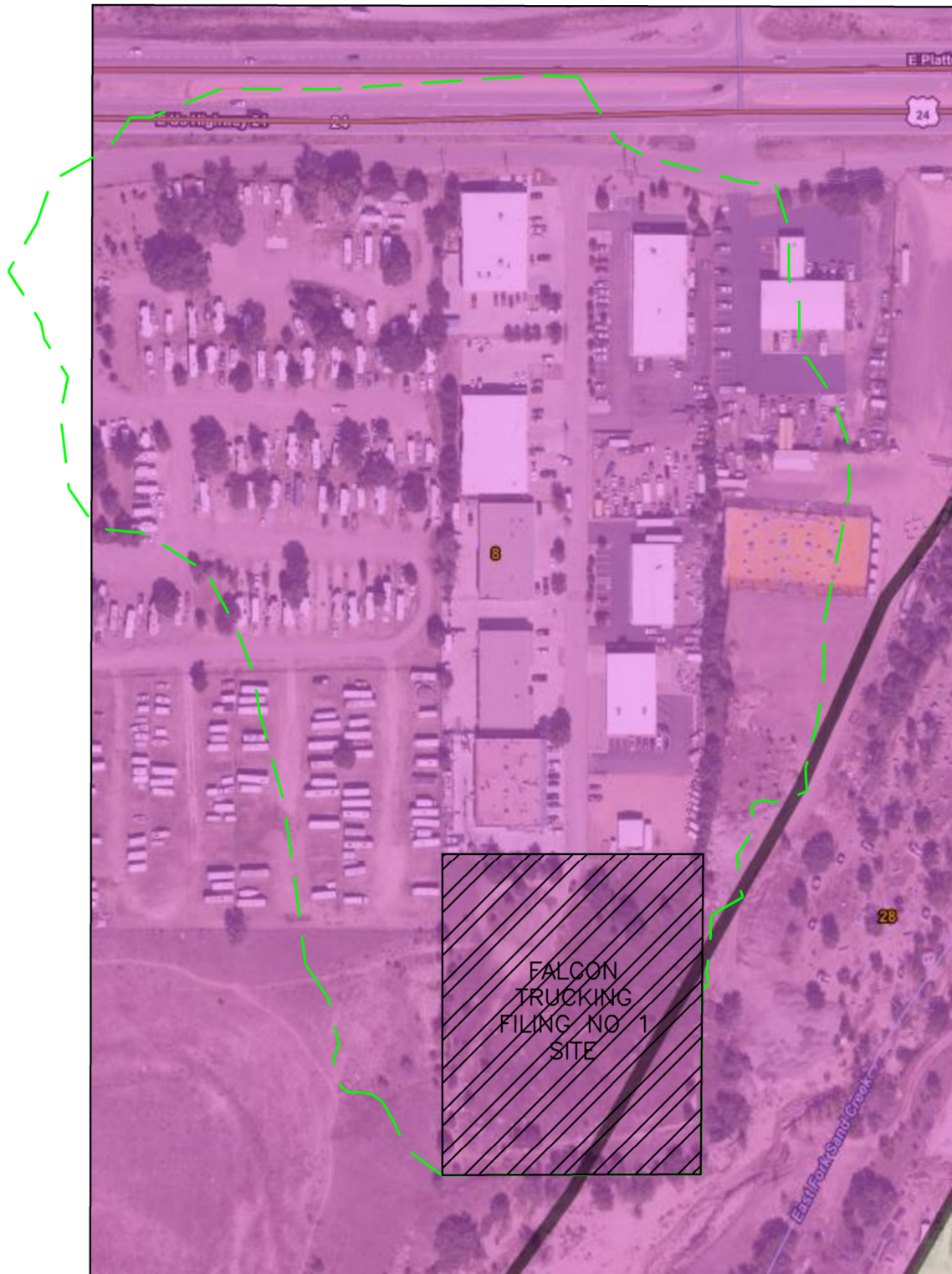
**CIVIL CONSULTANTS, INC.**

CLEARWAY FILING NO. 2, LOT 5			
VICINITY MAP			
PROJECT NO. 44-042		SCALE:	DATE:
DESIGNED BY: TAU		HORIZONTAL: N/A	05-20-2022
DRAWN BY: TAU		VERTICAL: N/A	
CHECKED BY: WAS			SHEET 1 OF 1
			VIC01

## **SOILS MAP**



NOT TO SCALE



Summary by Map Unit — El Paso County Area, Colorado (C0625)		
Map unit symbol	Map unit name	Rating
8	Blakeland loamy sand, 1 to 9 percent slopes	A
28	Ellicott loamy coarse sand, 0 to 5 percent slopes	A
111	Water	

FALCON TRUCKING  
FILING NO. 1  
SOILS MAP



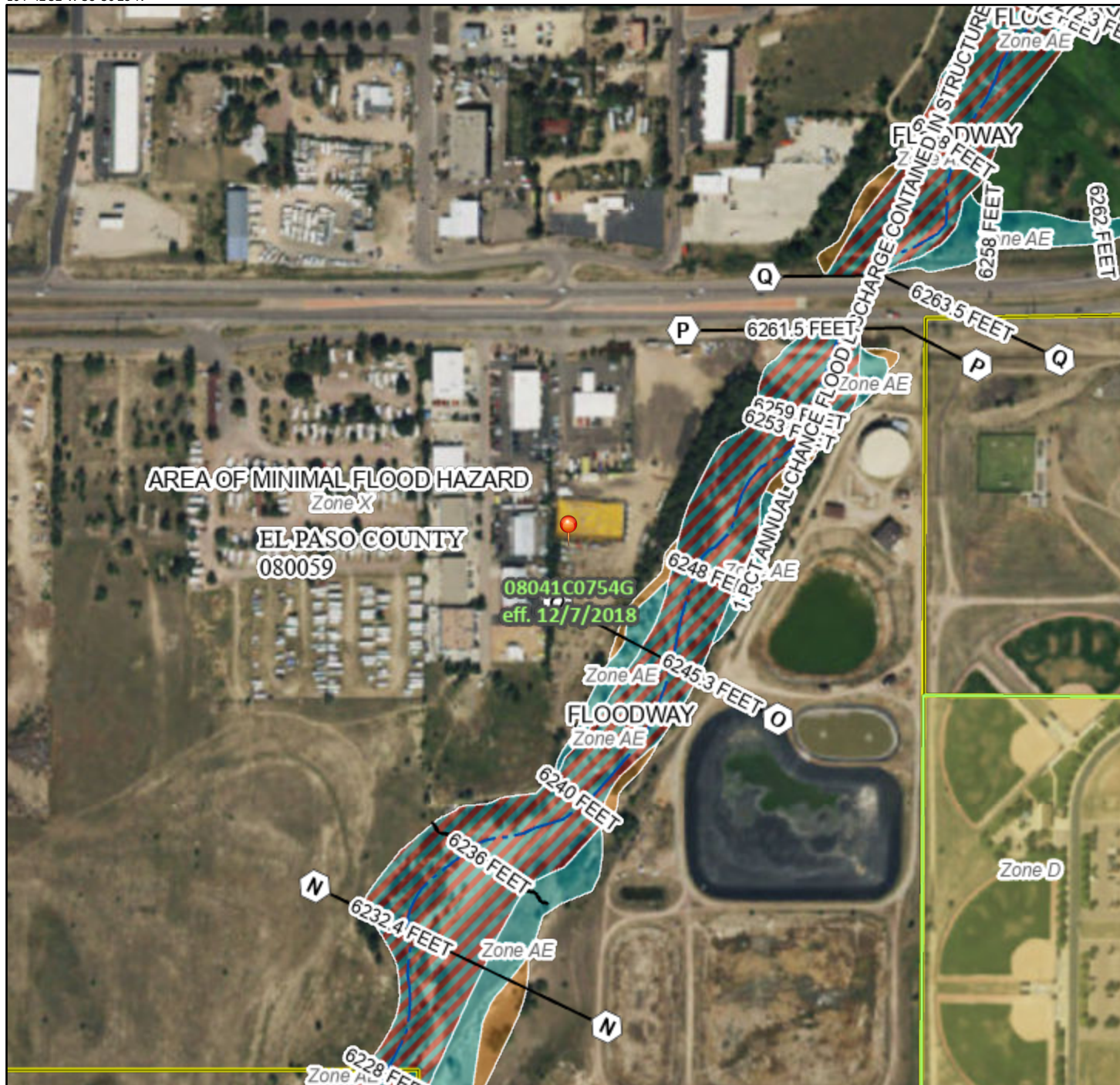
## **FIRM PANEL**



# National Flood Hazard Layer FIRMette



104°42'52"W 38°50'28"N



0 250 500 1,000 1,500 2,000 Feet 1:6,000

Basemap: USGS National Map: Orthoimagery: Data refreshed October, 2020

## Legend

SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT

SPECIAL FLOOD HAZARD AREAS		Without Base Flood Elevation (BFE) Zone A, V, A99
		With BFE or Depth Zone AE, AO, AH, VE, AR
		Regulatory Floodway
OTHER AREAS OF FLOOD HAZARD		0.2% Annual Chance Flood Hazard, Areas of 1% annual chance flood with average depth less than one foot or with drainage areas of less than one square mile Zone X
		Future Conditions 1% Annual Chance Flood Hazard Zone X
		Area with Reduced Flood Risk due to Levee. See Notes. Zone X
		Area with Flood Risk due to Levee Zone D
OTHER AREAS		NO SCREEN Area of Minimal Flood Hazard Zone X
		Effective LOMRs
GENERAL STRUCTURES		Area of Undetermined Flood Hazard Zone D
		Channel, Culvert, or Storm Sewer
		Levee, Dike, or Floodwall
OTHER FEATURES		20.2 Cross Sections with 1% Annual Chance Water Surface Elevation
		17.5
		Coastal Transect
		Base Flood Elevation Line (BFE)
		Limit of Study
		Jurisdiction Boundary
MAP PANELS		Coastal Transect Baseline
		Profile Baseline
		Hydrographic Feature
		Digital Data Available
		No Digital Data Available
		Unmapped



The pin displayed on the map is an approximate point selected by the user and does not represent an authoritative property location.

This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The basemap shown complies with FEMA's basemap accuracy standards

The flood hazard information is derived directly from the authoritative NFHL web services provided by FEMA. This map was exported on 5/16/2022 at 9:02 AM and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or become superseded by new data over time.

This map image is void if the one or more of the following map elements do not appear: basemap imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for unmapped and unmodernized areas cannot be used for regulatory purposes.

## **HYDROLOGIC CALCULATIONS**

***CLEARWAY NO.2, LOT 5 (WIRENUT)***  
***EXISTING CONDITIONS DRAINAGE CALCULATIONS***  
***(Area Runoff Coefficient Summary)***

			<i>STREETS/DEVELOPED</i>			<i>DEVELOPED LOTS</i>			<i>UNDEVELOPED/LANDSCAPE</i>			<i>RUNOFF COEFFICIENT</i>	
<b>BASIN</b>	<b>TOTAL AREA (SF)</b>	<b>TOTAL AREA (Acres)</b>	<b>AREA (Acres)</b>	<b>C<sub>5</sub></b>	<b>C<sub>100</sub></b>	<b>AREA (Acres)</b>	<b>C<sub>5</sub></b>	<b>C<sub>100</sub></b>	<b>AREA (Acres)</b>	<b>C<sub>5</sub></b>	<b>C<sub>100</sub></b>	<b>C<sub>5</sub></b>	<b>C<sub>100</sub></b>
<i>A</i>	<i>431946.186</i>	<i>9.92</i>	<i>0.00</i>	<i>0.90</i>	<i>0.96</i>	<i>9.13</i>	<i>0.30</i>	<i>0.50</i>	<i>0.78</i>	<i>0.08</i>	<i>0.35</i>	<i>0.28</i>	<i>0.49</i>
<i>B</i>	<i>133523.312</i>	<i>3.07</i>	<i>0.00</i>	<i>0.90</i>	<i>0.96</i>	<i>3.07</i>	<i>0.73</i>	<i>0.81</i>	<i>0.00</i>	<i>0.08</i>	<i>0.35</i>	<i>0.73</i>	<i>0.81</i>
<i>C</i>	<i>119110.0794</i>	<i>2.73</i>	<i>0.00</i>	<i>0.90</i>	<i>0.96</i>	<i>2.73</i>	<i>0.73</i>	<i>0.81</i>	<i>0.00</i>	<i>0.08</i>	<i>0.35</i>	<i>0.73</i>	<i>0.81</i>
<i>D</i>	<i>134064.3175</i>	<i>3.08</i>	<i>1.44</i>	<i>0.73</i>	<i>0.81</i>	<i>1.63</i>	<i>0.59</i>	<i>0.70</i>	<i>0.00</i>	<i>0.08</i>	<i>0.35</i>	<i>0.66</i>	<i>0.75</i>
<i>E</i>	<i>42111.756</i>	<i>0.97</i>	<i>0.00</i>	<i>0.90</i>	<i>0.96</i>	<i>0.00</i>	<i>0.08</i>	<i>0.35</i>	<i>0.97</i>	<i>0.08</i>	<i>0.35</i>	<i>0.08</i>	<i>0.35</i>
<i>F</i>	<i>46802.057</i>	<i>1.07</i>	<i>0.00</i>	<i>0.90</i>	<i>0.96</i>	<i>0.00</i>	<i>0.08</i>	<i>0.35</i>	<i>1.07</i>	<i>0.08</i>	<i>0.35</i>	<i>0.08</i>	<i>0.35</i>
<i>G</i>	<i>47704.938</i>	<i>1.10</i>	<i>0.00</i>	<i>0.90</i>	<i>0.96</i>	<i>0.00</i>	<i>0.08</i>	<i>0.35</i>	<i>1.10</i>	<i>0.08</i>	<i>0.35</i>	<i>0.08</i>	<i>0.35</i>

***CLEARWAY NO.2, LOT 5 (WIRENUT)***  
***EXISTING CONDITIONS DRAINAGE CALCULATIONS***  
***(Area Drainage Summary)***

From Area Runoff Coefficient Summary				OVERLAND				STREET / CHANNEL FLOW				Time of Travel (T <sub>i</sub> )		INTENSITY *		TOTAL FLOWS	
BASIN	AREA TOTAL (Acres)	C <sub>5</sub>	C <sub>100</sub>	C <sub>5</sub>	Length (ft)	Height (ft)	T <sub>C</sub> (min)	Length (ft)	Slope (%)	Velocity (fps)	T <sub>i</sub> (min)	TOTAL (min)	CHECK (min)	I <sub>5</sub> (in/hr)	I <sub>100</sub> (in/hr)	Q <sub>5</sub> (c.f.s.)	Q <sub>100</sub> (c.f.s.)
		From DCM Table 5-1															
A	9.92	0.28	0.49	0.28	100	2	11.7	1174	0.5%	0.7	27.4	39.1	17.1	3.3	5.6	9.3	27.0
B	3.07	0.73	0.81	0.73	100	2	5.3	775	1.3%	2.3	5.7	11.0	14.9	4.0	6.7	8.9	16.6
C	2.73	0.73	0.81	0.73	100	2	5.3	675	1.5%	2.4	4.6	9.9	14.3	4.1	6.9	8.3	15.4
D	3.08	0.66	0.75	0.66	100	2	6.4	673	1.9%	1.4	8.1	14.5	14.3	3.6	6.0	7.3	14.0
E	0.97	0.08	0.35	0.08	50	2	8.2	298	8.4%	2.0	2.4	10.7	11.9	4.0	6.8	0.3	2.3
F	1.07	0.08	0.35	0.08	100	2	14.7	138	6.5%	1.8	1.3	15.9	11.3	3.9	6.6	0.3	2.5
G	1.10	0.08	0.35	0.08	100	1	18.4	169	14.8%	2.7	1.0	19.5	11.5	3.9	6.6	0.3	2.5

\* Intensity equations assume a minimum travel time of 5 minutes.

Calculated by: TAU  
Date: 3/31/2022  
Checked by: VAS

***CLEARWAY NO.2, LOT 5 (WIRENUT)***  
***EXISTING CONDITIONS DRAINAGE CALCULATIONS***  
***(Basin Routing Summary)***

<i>From Area Runoff Coefficient Summary</i>				<b>OVERLAND</b>				<b>PIPE / CHANNEL FLOW</b>				<b>Time of Travel (T<sub>t</sub>)</b>	<b>INTENSITY *</b>		<b>TOTAL FLOWS</b>		<b>COMMENTS</b>
DESIGN POINT	CONTRIBUTING BASINS	CA <sub>5</sub>	CA <sub>100</sub>	C <sub>5</sub>	Length (ft)	Height (ft)	T <sub>c</sub> (min)	Length (ft)	Slope (%)	Velocity (fps)	T <sub>t</sub> (min)	TOTAL (min)	I <sub>5</sub> (in/hr)	I <sub>100</sub> (in/hr)	Q <sub>5</sub> (c.f.s.)	Q <sub>100</sub> (c.f.s.)	
1	D	2.02	2.31									14.3	3.6	6.0	7.3	14.0	conveyed by sheet flow and swale
				use D BASIN T <sub>c</sub>													
2	DP1, B, C	6.25	7.01									14.3	3.6	6.0	22.5	42.3	conveyed by private street c&g
				use DP1 T <sub>c</sub>													
3	DP2, F	6.34	7.39									14.3	3.6	6.0	22.8	44.6	conveyed by swale to East Fork Sand Creek
				use DP2 T <sub>c</sub>													
4	A	2.80	4.84									17.1	3.3	5.6	9.3	27.0	conveyed to Lot 5
				use A BASIN T <sub>c</sub>													
5	DP4, E	2.88	5.18									17.1	3.3	5.6	9.6	28.9	conveyed to East Fork Sand Creek
				use DP4 T <sub>c</sub>													
6	G, DP3, DP5	9.30	12.95									17.1	3.3	5.6	31.0	72.3	conveyed to East Fork Sand Creek
				use DP5 T <sub>c</sub>													

<i>Weighted Percent Imperviousness of WQ Pond 1</i>				
<i>Contributing Basins</i>	<i>Area (Acres)</i>	<i>C<sub>s</sub></i>	<i>Impervious % (I)</i>	<i>(Acres)*(I)</i>
<b>Column1</b>	<b>Column2</b>	<b>Column3</b>	<b>Column4</b>	<b>Column5</b>
H	0.33	0.75	91	29.71
I	0.19	0.80	94	17.73
J	0.21	0.74	91	18.70
K	0.20	0.73	90	17.56
L	0.18	0.90	100	18.43
M	0.13	0.90	100	13.32
N	0.40	0.90	100	39.72
O	0.25	0.78	93	22.90
Q	0.23	0.08	7	1.63
<i>Totals</i>	<b>2.11</b>			<b>179.70</b>
<i>Imperviousness of WQ Pond 1</i>	<b>85.2</b>			

**CLEARWAY NO.2, LOT 5**  
**PROPOSED CONDITIONS DRAINAGE CALCULATIONS**  
**(Area Runoff Coefficient Summary)**

			<i>STREETS/DEVELOPED</i>			<i>DEVELOPED LOTS</i>			<i>UNDEVELOPED/LANDSCAPE</i>			<i>RUNOFF COEFFICIENT</i>	
BASIN	TOTAL AREA (SF)	TOTAL AREA (Acres)	AREA (Acres)	C <sub>5</sub>	C <sub>100</sub>	AREA (Acres)	C <sub>5</sub>	C <sub>100</sub>	AREA (Acres)	C <sub>5</sub>	C <sub>100</sub>	C <sub>5</sub>	C <sub>100</sub>
<i>A</i>	431957.157	9.92	0.00	0.90	0.96	9.13	0.30	0.50	0.78	0.08	0.35	0.28	0.49
<i>B</i>	100360.697	2.30	0.00	0.90	0.96	2.30	0.73	0.81	0.00	0.08	0.35	0.73	0.81
<i>C</i>	104496.823	2.40	0.00	0.90	0.96	2.40	0.73	0.81	0.00	0.08	0.35	0.73	0.81
<i>D</i>	138334.367	3.18	1.54	0.73	0.81	1.63	0.59	0.70	0.00	0.08	0.35	0.66	0.75
<i>E</i>	41339.688	0.95	0.00	0.90	0.96	0.95	0.73	0.81	0.00	0.08	0.35	0.73	0.81
<i>F</i>	985.639	0.02	0.02	0.90	0.96	0.00	0.73	0.81	0.00	0.08	0.35	0.90	0.96
<i>G</i>	1858.029	0.04	0.04	0.90	0.96	0.00	0.73	0.81	0.00	0.08	0.35	0.90	0.96
<i>H</i>	14220.85	0.33	0.27	0.90	0.96	0.00	0.73	0.81	0.06	0.08	0.35	0.75	0.85
<i>I</i>	8213.984	0.19	0.17	0.90	0.96	0.00	0.73	0.81	0.02	0.08	0.35	0.80	0.89
<i>J</i>	8949.66	0.21	0.01	0.90	0.96	0.20	0.73	0.81	0.00	0.08	0.35	0.74	0.82
<i>K</i>	8500	0.20	0.00	0.90	0.96	0.20	0.73	0.81	0.00	0.08	0.35	0.73	0.81
<i>L</i>	8030.038	0.18	0.18	0.90	0.96	0.00	0.73	0.81	0.00	0.08	0.35	0.90	0.96
<i>M</i>	5803.105	0.13	0.13	0.90	0.96	0.00	0.73	0.81	0.00	0.08	0.35	0.90	0.96
<i>N</i>	17303.404	0.40	0.40	0.90	0.96	0.00	0.73	0.81	0.00	0.08	0.35	0.90	0.96
<i>O</i>	10726.014	0.25	0.21	0.90	0.96	0.00	0.73	0.81	0.03	0.08	0.35	0.78	0.87
<i>P</i>	11364.603	0.26	0.00	0.90	0.96	0.00	0.12	0.39	0.26	0.12	0.39	0.12	0.39
<i>Q</i>	10112.778	0.23	0.00	0.90	0.96	0.00	0.12	0.39	0.23	0.08	0.35	0.08	0.35
<i>R</i>	9732.156	0.22	0.00	0.90	0.96	0.00	0.08	0.35	0.22	0.08	0.35	0.08	0.35
<i>S</i>	23948.368	0.55	0.00	0.90	0.96	0.00	0.08	0.35	0.55	0.08	0.35	0.08	0.35



**CLEARWAY NO.2, LOT 5**  
**PROPOSED CONDITIONS DRAINAGE CALCULATIONS**  
**(Area Drainage Summary)**

From Area Runoff Coefficient Summary				OVERLAND				STREET / CHANNEL FLOW				Time of Travel (T <sub>t</sub> )		INTENSITY *		TOTAL FLOWS	
BASIN	AREA TOTAL (Acres)	C <sub>5</sub>	C <sub>100</sub>	C <sub>5</sub>	Length (ft)	Height (ft)	T <sub>C</sub> (min)	Length (ft)	Slope (%)	Velocity (fps)	T <sub>t</sub> (min)	TOTAL (min)	CHECK (min)	I <sub>5</sub> (in/hr)	I <sub>100</sub> (in/hr)	Q <sub>5</sub> (c.f.s.)	Q <sub>100</sub> (c.f.s.)
		From DCM Table 5-1															
A	9.92	0.28	0.49	0.28	100	2	11.7	1174	0.5%	0.7	27.4	39.1	17.1	3.3	5.6	9.3	27.0
B	2.30	0.73	0.81	0.73	100	2	5.3	674	1.2%	2.2	5.2	10.5	14.3	4.1	6.8	6.8	12.7
C	2.40	0.73	0.81	0.73	100	2	5.3	735	1.4%	2.3	5.3	10.6	14.6	4.0	6.8	7.1	13.2
D	3.18	0.66	0.75	0.66	100	2	6.3	685	1.9%	1.4	8.3	14.6	14.4	3.6	6.0	7.5	14.4
E	0.95	0.73	0.81	0.73	50	1	3.8	390	1.3%	2.3	2.9	6.6	12.4	4.7	8.0	3.3	6.1
F	0.02	0.90	0.96	0.90	25	1	1.1	17	1.5%	2.4	0.1	5.0	10.2	5.2	8.7	0.1	0.2
G	0.04	0.90	0.96	0.90	25	1	1.1	90	1.7%	2.6	0.6	5.0	10.6	5.2	8.7	0.2	0.4
H	0.33	0.75	0.85	0.75	50	1	3.6	127	0.8%	1.8	1.2	5.0	11.0	5.2	8.7	1.3	2.4
I	0.19	0.80	0.89	0.80	50	1	3.0	51	2.0%	2.8	0.3	5.0	10.6	5.2	8.7	0.8	1.5
J	0.21	0.74	0.82	0.74	50	1	3.7	86	1.2%	2.2	0.7	5.0	10.8	5.2	8.7	0.8	1.5
K	0.20	0.73	0.81	0.73	50	1	3.8	86	1.2%	2.2	0.7	5.0	10.8	5.2	8.7	0.7	1.4
L	0.18	0.90	0.96	0.90	50	1	2.0	64	2.0%	2.8	0.4	5.0	10.6	5.2	8.7	0.9	1.5
M	0.13	0.90	0.96	0.90	50	1	2.0	62	2.0%	2.8	0.4	5.0	10.6	5.2	8.7	0.6	1.1
N	0.40	0.90	0.96	0.90	50	1	2.0	123	2.4%	3.1	0.7	5.0	11.0	5.2	8.7	1.8	3.3
O	0.25	0.78	0.87	0.78	50	1	3.2	130	1.5%	2.4	0.9	5.0	11.0	5.2	8.7	1.0	1.9
P	0.26	0.12	0.39	0.12	50	2	7.9	159	5.0%	1.6	1.7	9.6	11.2	4.2	7.0	0.1	0.7
Q	0.23	0.08	0.35	0.08	50	4	6.6	140	2.9%	1.2	2.0	8.5	11.1	4.4	7.3	0.1	0.6
R	0.22	0.08	0.35	0.08	25	2	4.6	356	2.8%	1.2	5.1	9.7	12.1	4.2	7.0	0.1	0.5
S	0.55	0.08	0.35	0.08	50	8	5.2	115	15.7%	2.8	0.7	5.9	10.9	4.9	8.3	0.2	1.6

\* Intensity equations assume a minimum travel time of 5 minutes.

Calculated by: TAU  
Date: 4/4/2022  
Checked by: VAS



***CLEARWAY NO.2, LOT 5***  
***PROPOSED CONDITIONS DRAINAGE CALCULATIONS***  
***(Basin Routing Summary)***

<i>From Area Runoff Coefficient Summary</i>				<b>OVERLAND</b>				<b>PIPE / CHANNEL FLOW</b>				<b>Time of Travel (T<sub>t</sub>)</b>	<b>INTENSITY *</b>		<b>TOTAL FLOWS</b>		<b>COMMENTS</b>
<b>DESIGN POINT</b>	<b>CONTRIBUTING BASINS</b>	<b>CA<sub>5</sub></b>	<b>CA<sub>100</sub></b>	<b>C<sub>5</sub></b>	<b>Length (ft)</b>	<b>Height (ft)</b>	<b>T<sub>c</sub> (min)</b>	<b>Length (ft)</b>	<b>Slope (%)</b>	<b>Velocity (fps)</b>	<b>T<sub>t</sub> (min)</b>	<b>TOTAL (min)</b>	<b>I<sub>5</sub> (in/hr)</b>	<b>I<sub>100</sub> (in/hr)</b>	<b>Q<sub>5</sub> (c.f.s.)</b>	<b>Q<sub>100</sub> (c.f.s.)</b>	
<b>1</b>	<b>B</b>	1.68	1.87									10.5	4.1	6.8	<b>6.8</b>	<b>12.7</b>	Mod Triple Denver Type 16 Grate Inlet
				Basin B Tc Used													
<b>2</b>	<b>C</b>	1.75	1.94									10.6	4.0	6.8	<b>7.1</b>	<b>13.2</b>	Mod Triple Denver Type 16 Grate Inlet
				Basin C Tc Used													
<b>3</b>	<b>FB1, F</b>	0.67	0.93									10.5	4.1	6.8	<b>2.7</b>	<b>6.4</b>	Mod Triple Denver Type 16 Grate Inlet
				Basin B Tc Used													
<b>4</b>	<b>FB2, G</b>	0.29	0.50									10.6	4.0	6.8	<b>1.2</b>	<b>3.4</b>	Mod Triple Denver Type 16 Grate Inlet
				Basin C Tc Used													
<b>5</b>	<b>FB3, FB4, E</b>	0.86	1.22									6.6	4.7	8.0	<b>4.1</b>	<b>9.7</b>	Mod Triple Denver Type 16 Grate Inlet
				Basin E Tc Used													
<b>6</b>	<b>D</b>	2.09	2.39									14.4	3.6	6.0	<b>7.5</b>	<b>14.4</b>	CDOT Type D Grate Inlet
				Basin D Tc Used													
<b>7</b>	<b>I</b>	0.15	0.17									5.0	5.2	8.7	<b>0.8</b>	<b>1.5</b>	Nyloplast 24" Grate Inlet
				Basin I Tc Used													
<b>8</b>	<b>H</b>	0.24	0.28									5.0	5.2	8.7	<b>1.3</b>	<b>2.4</b>	Mod Single Denver Type 16 Grate Inlet
				Basin H Tc Used													
<b>9</b>	<b>O</b>	0.19	0.22									5.0	5.2	8.7	<b>1.0</b>	<b>1.9</b>	Nyloplast 24" Grate Inlet
				Basin O Tc Used													
<b>10</b>	<b>N</b>	0.36	0.38									5.0	5.2	8.7	<b>1.8</b>	<b>3.3</b>	Nyloplast 2'X2' Steel Bar Inlet
				Basin N Tc Used													
<b>11</b>	<b>L</b>	0.17	0.18									5.0	5.2	8.7	<b>0.9</b>	<b>1.5</b>	Nyloplast 24" Grate Inlet
				Basin L Tc Used													
<b>12</b>	<b>M</b>	0.12	0.13									5.0	5.2	8.7	<b>0.6</b>	<b>1.1</b>	Nyloplast 24" Grate Inlet
				Basin M Tc Used													
<b>13</b>	<b>Q, PR35, PR38</b>	1.54	1.75									8.5	4.4	7.3	<b>6.7</b>	<b>12.8</b>	FSD POND
				Basin Q Tc Used													
<b>14</b>	<b>A, R</b>	2.82	4.92									17.1	3.3	5.6	<b>9.4</b>	<b>27.5</b>	CDOT Type D Grate Inlet
				Basin A Tc Used													

**CLEARWAY NO.2, LOT 5**  
**PROPOSED CONDITIONS DRAINAGE CALCULATIONS**  
**(Basin Routing Summary)**

From Area Runoff Coefficient Summary				OVERLAND				PIPE / CHANNEL FLOW				Time of Travel (T <sub>t</sub> )	INTENSITY *		TOTAL FLOWS		COMMENTS
DESIGN POINT	CONTRIBUTING BASINS	CA <sub>5</sub>	CA <sub>100</sub>	C <sub>5</sub>	Length (ft)	Height (ft)	T <sub>c</sub> (min)	Length (ft)	Slope (%)	Velocity (fps)	T <sub>t</sub> (min)	TOTAL (min)	I <sub>5</sub> (in/hr)	I <sub>100</sub> (in/hr)	Q <sub>5</sub> (c.f.s.)	Q <sub>100</sub> (c.f.s.)	
15	p	0.03	0.10									9.6	4.2	7.0	0.1	0.7	SWALE CONVEYS FLOW TO EAST FORK SAND CREEK
				Basin P Tc Used													
16	S, DP15, PR40, PR41														28.8	71.5	EAST FORK SAND CREEK
				Basin S Tc Used													

***CLEARWAY NO.2, LOT 5***  
***PROPOSED CONDITIONS DRAINAGE CALCULATIONS***  
***(Storm Sewer Routing Summary)***

<b><i>PIPE RUN</i></b>	<b><i>Contributing Pipes/Design Points</i></b>	<b><i>Equivalent CA<sub>5</sub></i></b>	<b><i>Equivalent CA<sub>100</sub></i></b>	<b><i>Maximum T<sub>c</sub></i></b>	<b><i>Intensity*</i></b>		<b><i>Flow</i></b>	
					<b><i>I<sub>5</sub></i></b>	<b><i>I<sub>100</sub></i></b>	<b><i>Q<sub>5</sub></i></b>	<b><i>Q<sub>100</sub></i></b>
<b><i>1</i></b>	<b><i>DP1</i></b>	1.03	0.95	10.5	4.1	6.8	<b><i>4.3</i></b>	<b><i>6.6</i></b>
<b><i>2</i></b>	<b><i>PR1, DP2</i></b>	1.45	1.43	10.6	4.0	6.8	<b><i>5.9</i></b>	<b><i>9.7</i></b>
<b><i>3</i></b>	<b><i>DP3</i></b>	0.52	0.60	10.5	4.1	6.8	<b><i>2.1</i></b>	<b><i>4.1</i></b>
<b><i>4</i></b>	<b><i>PR2, PR3, DP4</i></b>	2.24	2.41	10.6	4.0	6.8	<b><i>9.1</i></b>	<b><i>16.4</i></b>
<b><i>5</i></b>	<b><i>PR4, DP5</i></b>	3.14	4.48	10.6	4.0	6.8	<b><i>12.7</i></b>	<b><i>30.5</i></b>
<b><i>6</i></b>	<b><i>DP6</i></b>	2.09	2.39	14.4	3.6	6.0	<b><i>7.5</i></b>	<b><i>14.4</i></b>
<b><i>7</i></b>	<b><i>PR5, PR6</i></b>	5.23	6.88	14.4	3.6	6.0	<b><i>18.8</i></b>	<b><i>41.4</i></b>
<b><i>8</i></b>	<b><i>PR7</i></b>	5.23	6.88	14.4	3.6	6.0	<b><i>18.8</i></b>	<b><i>41.4</i></b>
<b><i>9</i></b>	<b><i>.02 ACRE BASIN J</i></b>	0.02	0.02	5.0	5.2	8.7	<b><i>0.1</i></b>	<b><i>0.2</i></b>
<b><i>10</i></b>	<b><i>PR9</i></b>	0.02	0.02	5.0	5.2	8.7	<b><i>0.1</i></b>	<b><i>0.2</i></b>
<b><i>11</i></b>	<b><i>.06 ACRE BASIN J</i></b>	0.04	0.05	5.0	5.2	8.7	<b><i>0.2</i></b>	<b><i>0.4</i></b>
<b><i>12</i></b>	<b><i>PR10, PR11</i></b>	0.06	0.07	5.0	5.2	8.7	<b><i>0.3</i></b>	<b><i>0.6</i></b>
<b><i>13</i></b>	<b><i>PR12, .06 ACRE BASIN J</i></b>	0.10	0.12	5.0	5.2	8.7	<b><i>0.5</i></b>	<b><i>1.0</i></b>
<b><i>14</i></b>	<b><i>.01 ACRE BASIN J</i></b>	0.01	0.01	5.0	5.2	8.7	<b><i>0.0</i></b>	<b><i>0.1</i></b>
<b><i>15</i></b>	<b><i>PR13, PR14</i></b>	0.11	0.12	5.0	5.2	8.7	<b><i>0.6</i></b>	<b><i>1.1</i></b>
<b><i>16</i></b>	<b><i>.04 ACRE BASIN J</i></b>	0.03	0.03	5.0	5.2	8.7	<b><i>0.1</i></b>	<b><i>0.3</i></b>
<b><i>17</i></b>	<b><i>PR15, PR16</i></b>	0.14	0.15	5.0	5.2	8.7	<b><i>0.7</i></b>	<b><i>1.3</i></b>
<b><i>18</i></b>	<b><i>.02 ACRE BASIN J</i></b>	0.01	0.01	5.0	5.2	8.7	<b><i>0.1</i></b>	<b><i>0.1</i></b>

***CLEARWAY NO.2, LOT 5***  
***PROPOSED CONDITIONS DRAINAGE CALCULATIONS***  
***(Storm Sewer Routing Summary)***

<b><i>PIPE RUN</i></b>	<b><i>Contributing Pipes/Design Points</i></b>	<b><i>Equivalent CA<sub>5</sub></i></b>	<b><i>Equivalent CA<sub>100</sub></i></b>	<b><i>Maximum T<sub>c</sub></i></b>	<b><i>Intensity*</i></b>		<b><i>Flow</i></b>	
					<b><i>I<sub>5</sub></i></b>	<b><i>I<sub>100</sub></i></b>	<b><i>Q<sub>5</sub></i></b>	<b><i>Q<sub>100</sub></i></b>
<b><i>19</i></b>	<b><i>PR17, PR18</i></b>	0.15	0.17	5.0	5.2	8.7	<b><i>0.8</i></b>	<b><i>1.5</i></b>
<b><i>20</i></b>	<b><i>PR19</i></b>	0.15	0.17	5.0	5.2	8.7	<b><i>0.8</i></b>	<b><i>1.5</i></b>
<b><i>21</i></b>	<b><i>PR20, DP11</i></b>	0.32	0.34	5.0	5.2	8.7	<b><i>1.6</i></b>	<b><i>3.0</i></b>
<b><i>22</i></b>	<b><i>PR21, DP12</i></b>	0.44	0.47	5.0	5.2	8.7	<b><i>2.3</i></b>	<b><i>4.1</i></b>
<b><i>23</i></b>	<b><i>DP7</i></b>	0.15	0.17	5.0	5.2	8.7	<b><i>0.8</i></b>	<b><i>1.5</i></b>
<b><i>24</i></b>	<b><i>PR23, DP8</i></b>	0.40	0.44	5.0	5.2	8.7	<b><i>2.0</i></b>	<b><i>3.8</i></b>
<b><i>25</i></b>	<b><i>.03 ACRE BASIN K</i></b>	0.02	0.03	5.0	5.2	8.7	<b><i>0.1</i></b>	<b><i>0.2</i></b>
<b><i>26</i></b>	<b><i>PR24, PR25</i></b>	0.42	0.47	5.0	5.2	8.7	<b><i>2.2</i></b>	<b><i>4.1</i></b>
<b><i>27</i></b>	<b><i>.05 ACRE BASIN K</i></b>	0.03	0.04	5.0	5.2	8.7	<b><i>0.2</i></b>	<b><i>0.3</i></b>
<b><i>28</i></b>	<b><i>PR26, PR27</i></b>	0.45	0.51	5.0	5.2	8.7	<b><i>2.3</i></b>	<b><i>4.4</i></b>
<b><i>29</i></b>	<b><i>.05 ACRE BASIN K</i></b>	0.03	0.04	5.0	5.2	8.7	<b><i>0.2</i></b>	<b><i>0.3</i></b>
<b><i>30</i></b>	<b><i>PR28, PR29</i></b>	0.49	0.54	5.0	5.2	8.7	<b><i>2.5</i></b>	<b><i>4.7</i></b>
<b><i>31</i></b>	<b><i>.05 ACRE BASIN K</i></b>	0.04	0.04	5.0	5.2	8.7	<b><i>0.2</i></b>	<b><i>0.3</i></b>
<b><i>32</i></b>	<b><i>PR30, PR31</i></b>	0.52	0.58	5.0	5.2	8.7	<b><i>2.7</i></b>	<b><i>5.1</i></b>
<b><i>33</i></b>	<b><i>.02 ACRE BASIN K</i></b>	0.02	0.02	5.0	5.2	8.7	<b><i>0.1</i></b>	<b><i>0.2</i></b>
<b><i>34</i></b>	<b><i>PR32, PR33</i></b>	0.54	0.60	5.0	5.2	8.7	<b><i>2.8</i></b>	<b><i>5.2</i></b>
<b><i>35</i></b>	<b><i>PR22, PR34</i></b>	0.98	1.07	5.0	5.2	8.7	<b><i>5.0</i></b>	<b><i>9.3</i></b>
<b><i>36</i></b>	<b><i>DP9</i></b>	0.19	0.22	5.0	5.2	8.7	<b><i>1.0</i></b>	<b><i>1.9</i></b>

***CLEARWAY NO.2, LOT 5***  
***PROPOSED CONDITIONS DRAINAGE CALCULATIONS***  
***(Storm Sewer Routing Summary)***

<b><i>PIPE RUN</i></b>	<b><i>Contributing Pipes/Design Points</i></b>	<b><i>Equivalent CA<sub>5</sub></i></b>	<b><i>Equivalent CA<sub>100</sub></i></b>	<b><i>Maximum T<sub>c</sub></i></b>	<b><i>Intensity*</i></b>		<b><i>Flow</i></b>	
					<b><i>I<sub>5</sub></i></b>	<b><i>I<sub>100</sub></i></b>	<b><i>Q<sub>5</sub></i></b>	<b><i>Q<sub>100</sub></i></b>
<b><i>37</i></b>	<b><i>PR36, DP10</i></b>	0.55	0.60	5.0	5.2	8.7	<b><i>2.8</i></b>	<b><i>5.2</i></b>
<b><i>38</i></b>	<b><i>PR37</i></b>	0.55	0.60	5.0	5.2	8.7	<b><i>2.8</i></b>	<b><i>5.2</i></b>
<b><i>39</i></b>	<b><i>FSD POND RELEASE</i></b>						<b><i>0.3</i></b>	<b><i>0.3</i></b>
<b><i>40</i></b>	<b><i>PR8, PR39</i></b>						<b><i>19.1</i></b>	<b><i>41.7</i></b>
<b><i>41</i></b>	<b><i>DP14</i></b>	2.82	4.92	17.1	3.3	5.6	<b><i>9.4</i></b>	<b><i>27.5</i></b>

\* Intensity equations assume a minimum travel time of 5 minutes.

DP - Design Point

EX - Existing Design Point

FB- Flow By from Design Point

INT- Intercepted Flow from Design Point

Calculated by: TAU

Date: 4/4/2022

Checked by: VAS

## **HYDRAULIC CALCULATIONS / FSD POND CALCULATIONS**

# Design Procedure Form: Sand Filter (SF)

UD-BMP (Version 3.07, March 2018)

Sheet 1 of 2

Designer: Darin Moffett  
 Company: M&S Civil Consultants  
 Date: June 3, 2022  
 Project: Clearway No.2, Lot 5 - WireNut  
 Location: \_\_\_\_\_

## 1. Basin Storage Volume

- A) Effective Imperviousness of Tributary Area,  $I_e$   
 (100% if all paved and roofed areas upstream of sand filter)
- B) Tributary Area's Imperviousness Ratio ( $i = I_e/100$ )
- C) Water Quality Capture Volume (WQCV) Based on 12-hour Drain Time  
 $WQCV = 0.8 * (0.91 * i^3 - 1.19 * i^2 + 0.78 * i)$
- D) Contributing Watershed Area (including sand filter area)
- E) Water Quality Capture Volume (WQCV) Design Volume  
 $V_{WQCV} = WQCV / 12 * \text{Area}$
- F) For Watersheds Outside of the Denver Region, Depth of Average Runoff Producing Storm
- G) For Watersheds Outside of the Denver Region, Water Quality Capture Volume (WQCV) Design Volume
- H) User Input of Water Quality Capture Volume (WQCV) Design Volume  
 (Only if a different WQCV Design Volume is desired)

$I_e = 85.2$  %

$i = 0.852$

WQCV = 0.29 watershed inches

Area = 103,237 sq ft

$V_{WQCV} =$  cu ft

$d_e = 0.50$  in

$V_{WQCV \text{ OTHER}} =$  cu ft

$V_{WQCV \text{ USER}} = 2,222$  cu ft

## 2. Basin Geometry

- A) WQCV Depth
- B) Sand Filter Side Slopes (Horizontal distance per unit vertical, 4:1 or flatter preferred). Use "0" if sand filter has vertical walls.
- C) Minimum Filter Area (Flat Surface Area)
- D) Actual Filter Area
- E) Volume Provided

$D_{WQCV} = 0.8$  ft

$Z = 4.00$  ft / ft

$A_{Min} = 1099$  sq ft

$A_{Actual} = 2331$  sq ft

$V_T =$  cu ft

## 3. Filter Material

- Choose One
- ☒ 18" CDOT Class B or C Filter Material
- ☐ Other (Explain):

## 4. Underdrain System

- A) Are underdrains provided?
- B) Underdrain system orifice diameter for 12 hour drain time
- i) Distance From Lowest Elevation of the Storage Volume to the Center of the Orifice
- ii) Volume to Drain in 12 Hours
- iii) Orifice Diameter, 3/8" Minimum

- Choose One
- ☒ YES
- ☐ NO

$y = 2.4$  ft

$Vol_{12} = 2,222$  cu ft

$D_o = 1 \frac{1}{16}$  in

# Design Procedure Form: Sand Filter (SF)

Sheet 2 of 2

Designer: Darin Moffett  
 Company: M&S Civil Consultants  
 Date: June 3, 2022  
 Project: Clearway No.2, Lot 5 - WireNut  
 Location: \_\_\_\_\_

## 5. Impermeable Geomembrane Liner and Geotextile Separator Fabric

A) Is an impermeable liner provided due to proximity of structures or groundwater contamination?

Choose One

☐ YES ☒ NO

## 6. Inlet / Outlet Works

A) Describe the type of energy dissipation at inlet points and means of conveying flows in excess of the WQCV through the outlet

A riprap stilling basin is provided at the inlet point

Flows in excess of the WQCV are conveyed via a rectangular slot in the outlet box wall and enter the top of the box and discharge out via an restricted 18rcp

Notes: \_\_\_\_\_

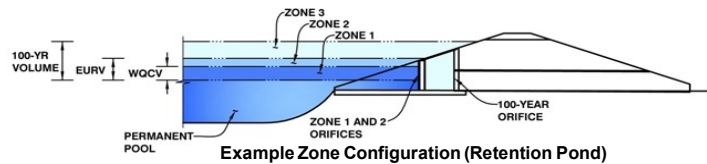


## DETENTION BASIN STAGE-STORAGE TABLE BUILDER

*MHFD-Detention, Version 4.05 (January 2022)*

**Project: Clearway No. 2, Lot 5 (WireNut)**

**Basin ID: Pond 1**



### Watershed Information

Selected BMP Type =	<b>SF</b>	
Watershed Area =	2.11	acres
Watershed Length =	335	ft
Watershed Length to Centroid =	165	ft
Watershed Slope =	0.020	ft/ft
Watershed Imperviousness =	85.20%	percent
Percentage Hydrologic Soil Group A =	100.0%	percent
Percentage Hydrologic Soil Group B =	0.0%	percent
Percentage Hydrologic Soil Groups C/D =	0.0%	percent
Target WQCV Drain Time =	12.0	hours
Location for 1-hr Rainfall Depths =	User Input	

After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

Water Quality Capture Volume (WQCV) =	0.051	acre-feet
Excess Urban Runoff Volume (EURV) =	0.241	acre-feet
2-yr Runoff Volume (P1 = 1.19 in.) =	0.158	acre-feet
5-yr Runoff Volume (P1 = 1.5 in.) =	0.204	acre-feet
10-yr Runoff Volume (P1 = 1.75 in.) =	0.241	acre-feet
25-yr Runoff Volume (P1 = 2 in.) =	0.283	acre-feet
50-yr Runoff Volume (P1 = 2.25 in.) =	0.323	acre-feet
100-yr Runoff Volume (P1 = 2.52 in.) =	0.370	acre-feet
500-yr Runoff Volume (P1 = 3.14 in.) =	0.474	acre-feet
Approximate 2-yr Detention Volume =	0.158	acre-feet
Approximate 5-yr Detention Volume =	0.206	acre-feet
Approximate 10-yr Detention Volume =	0.245	acre-feet
Approximate 25-yr Detention Volume =	0.290	acre-feet
Approximate 50-yr Detention Volume =	0.316	acre-feet
Approximate 100-yr Detention Volume =	0.339	acre-feet

### Define Zones and Basin Geometry

Zone 1 Volume (WQCV)	=	0.051	acre-feet
Zone 2 Volume (EURV - Zone 1)	=	0.190	acre-feet
Zone 3 Volume (100-year - Zones 1 & 2)	=	0.098	acre-feet
Total Detention Basin Volume	=	0.339	acre-feet
Initial Surge Volume (ISV)	=	user	ft <sup>3</sup>
Initial Surge Depth (ISD)	=	user	ft
Total Available Detention Depth ( $H_{total}$ )	=	user	ft
Depth of Trickle Channel ( $H_{TC}$ )	=	user	ft
Slope of Trickle Channel ( $S_{TC}$ )	=	user	ft/ft
Slopes of Main Basin Sides ( $S_{main}$ )	=	user	H:V
Basin Length-to-Width Ratio ( $R_L/W$ )	=	user	

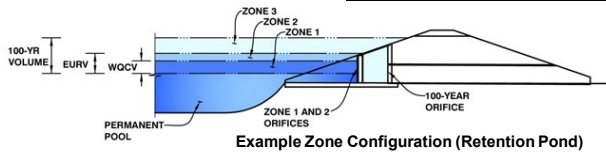
[illegible]

# DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.05 (January 2022)

Project: Clearway No. 2, Lot 5 (WireNut)

Basin ID: Pond 1



Example Zone Configuration (Retention Pond)

	Estimated Stage (ft)	Estimated Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	0.79	0.051	Filtration Media
Zone 2 (EURV)	2.65	0.190	Circular Orifice
Zone 3 (100-year)	3.36	0.098	Weir&Pipe (Restrict)
Total (all zones)		0.339	

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth = 2.40 ft (distance below the filtration media surface)  
Underdrain Orifice Diameter = 1.08 inches

Calculated Parameters for Underdrain  
Underdrain Orifice Area = 0.0 ft<sup>2</sup>  
Underdrain Orifice Centroid = 0.05 feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Centroid of Lowest Orifice = N/A ft (relative to basin bottom at Stage = 0 ft)  
Depth at top of Zone using Orifice Plate = N/A ft (relative to basin bottom at Stage = 0 ft)  
Orifice Plate: Orifice Vertical Spacing = N/A inches  
Orifice Plate: Orifice Area per Row = N/A sq. inches

Calculated Parameters for Plate  
WQ Orifice Area per Row = N/A ft<sup>2</sup>  
Elliptical Half-Width = N/A feet  
Elliptical Slot Centroid = N/A feet  
Elliptical Slot Area = N/A ft<sup>2</sup>

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (optional)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Orifice Area (sq. inches)	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Orifice Area (sq. inches)	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A

User Input: Vertical Orifice (Circular or Rectangular)

Invert of Vertical Orifice = 0.79 ft (relative to basin bottom at Stage = 0 ft)  
Depth at top of Zone using Vertical Orifice = 2.65 ft (relative to basin bottom at Stage = 0 ft)  
Vertical Orifice Diameter = 2.59 inches

Calculated Parameters for Vertical Orif  
Zone 2 Circular Not Selected  
Vertical Orifice Area = 0.04 ft<sup>2</sup>  
Vertical Orifice Centroid = 0.11 ft

User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir and No Outlet Pipe)

Zone 3 Weir Not Selected  
Overflow Weir Front Edge Height, H<sub>o</sub> = 2.65 ft (relative to basin bottom at Stage = 0 ft)  
Overflow Weir Front Edge Length = 2.91 feet  
Overflow Weir Grate Slope = 0.00 H:V  
Horiz. Length of Weir Sides = 2.91 feet  
Overflow Grate Type = Close Mesh Grate  
Debris Clogging % = 50%

Calculated Parameters for Overflow W  
Zone 3 Weir Not Selected  
Height of Grate Upper Edge, H<sub>u</sub> = 2.65 ft  
Overflow Weir Slope Length = 2.91 feet  
Grate Open Area / 100-yr Orifice Area = N/A  
Overflow Grate Open Area w/o Debris = N/A  
Overflow Grate Open Area w/ Debris = N/A

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

Zone 3 Restrictor Not Selected  
Depth to Invert of Outlet Pipe = 3.00 ft (distance below basin bottom at Stage = 0 ft)  
Outlet Pipe Diameter = 18.00 inches  
Restrictor Plate Height Above Pipe Invert = 2.75 inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Pl  
Zone 3 Restrictor Not Selected  
Outlet Orifice Area = 0.17 ft<sup>2</sup>  
Outlet Orifice Centroid = 0.14 ft  
Half-Central Angle of Restrictor Plate on Pipe = 0.80

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage = 3.26 ft (relative to basin bottom at Stage = 0 ft)  
Spillway Crest Length = 22.00 feet  
Spillway End Slopes = 4.00 H:V  
Freeboard above Max Water Surface = 1.00 feet

Calculated Parameters for Spillway  
Spillway Design Flow Depth = 0.23 feet  
Stage at Top of Freeboard = 4.49 feet  
Basin Area at Top of Freeboard = 0.18 acres  
Basin Volume at Top of Freeboard = 0.53 acre-ft

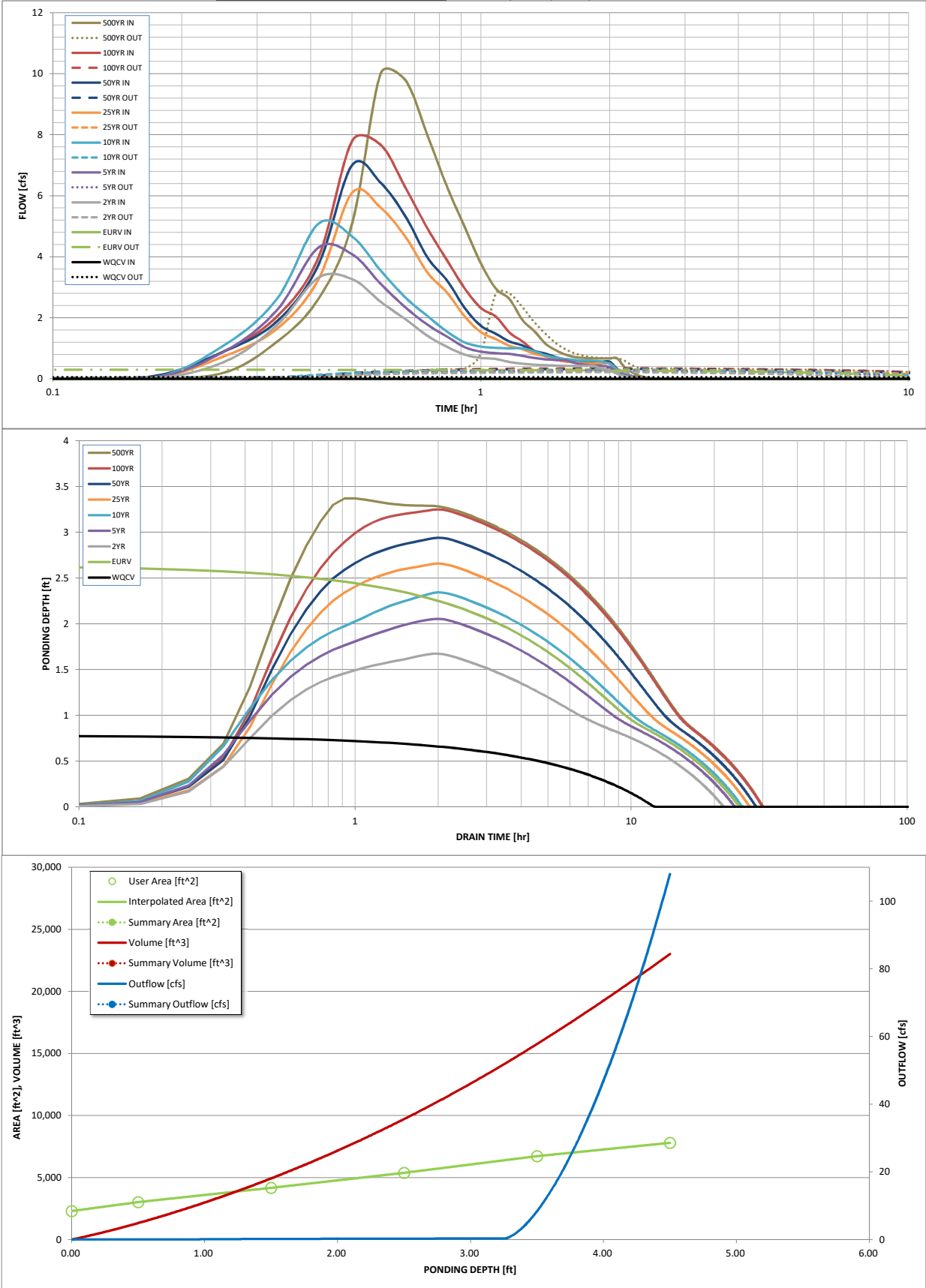
## Routed Hydrograph Results

The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through A)

	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year
Design Storm Return Period =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52
One-Hour Rainfall Depth (in) =	N/A	N/A	0.158	0.204	0.241	0.283	0.323	0.370
CUHP Runoff Volume (acre-ft) =	N/A	N/A	0.158	0.204	0.241	0.283	0.323	0.370
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	0.0	0.0	0.1	0.5	1.0	1.6
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A	0.01	0.02	0.03	0.24	0.45	0.74
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A	0.01	0.02	0.03	0.24	0.45	0.74
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	3.3	4.3	5.1	6.1	7.0	7.8
Peak Inflow Q (cfs) =	N/A	N/A	0.2	0.3	0.3	0.3	0.3	0.3
Peak Outflow Q (cfs) =	N/A	N/A	N/A	6.3	5.0	0.6	0.3	0.2
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	6.3	5.0	0.6	0.3	0.2
Structure Controlling Flow =	Filtration Media	Vertical Orifice 1	Vertical Orifice 1	Vertical Orifice 1	Vertical Orifice 1	Vertical Orifice 1	Vertical Orifice 1	Vertical Orifice 1
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	12	23	21	22	24	25	26	27
Time to Drain 99% of Inflow Volume (hours) =	12	24	21	23	25	26	28	29
Maximum Ponding Depth (ft) =	0.78	2.65	1.67	2.05	2.34	2.66	2.94	3.25
Area at Maximum Ponding Depth (acres) =	0.08	0.13	0.10	0.11	0.12	0.13	0.14	0.15
Maximum Volume Stored (acre-ft) =	0.051	0.242	0.130	0.170	0.203	0.242	0.280	0.323

DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-*Detention*, Version 4.05 (January 2022)



S-A-V-D Chart Axis Override	X-axis	Left Y-Axis	Right Y-Axis
minimum bound			
maximum bound			

# DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename: \_\_\_\_\_

## Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.06	0.01	0.19
	0:15:00	0.00	0.00	0.54	0.88	1.09	0.73	0.89	0.88	1.21
	0:20:00	0.00	0.00	1.75	2.24	2.61	1.63	1.88	2.04	2.61
	0:25:00	0.00	0.00	3.31	4.30	5.08	3.24	3.73	3.97	5.09
	0:30:00	0.00	0.00	3.27	4.08	4.67	6.09	7.00	7.80	10.01
	0:35:00	0.00	0.00	2.52	3.11	3.55	5.60	6.42	7.67	9.78
	0:40:00	0.00	0.00	1.95	2.34	2.66	4.64	5.32	6.26	7.99
	0:45:00	0.00	0.00	1.41	1.77	2.06	3.48	3.98	4.93	6.30
	0:50:00	0.00	0.00	1.05	1.38	1.55	2.82	3.22	3.89	4.98
	0:55:00	0.00	0.00	0.79	1.03	1.19	2.04	2.32	2.96	3.78
	1:00:00	0.00	0.00	0.68	0.89	1.06	1.53	1.74	2.32	2.96
	1:05:00	0.00	0.00	0.65	0.84	1.02	1.30	1.48	2.04	2.61
	1:10:00	0.00	0.00	0.55	0.82	1.00	1.08	1.22	1.52	1.93
	1:15:00	0.00	0.00	0.49	0.75	1.00	0.97	1.09	1.23	1.56
	1:20:00	0.00	0.00	0.46	0.68	0.90	0.81	0.92	0.91	1.15
	1:25:00	0.00	0.00	0.44	0.64	0.77	0.74	0.83	0.74	0.93
	1:30:00	0.00	0.00	0.43	0.61	0.69	0.63	0.70	0.63	0.79
	1:35:00	0.00	0.00	0.42	0.60	0.64	0.56	0.63	0.57	0.71
	1:40:00	0.00	0.00	0.42	0.51	0.61	0.53	0.59	0.55	0.68
	1:45:00	0.00	0.00	0.42	0.46	0.60	0.51	0.57	0.54	0.67
	1:50:00	0.00	0.00	0.42	0.43	0.59	0.50	0.56	0.54	0.67
	1:55:00	0.00	0.00	0.33	0.42	0.56	0.50	0.56	0.54	0.67
	2:00:00	0.00	0.00	0.28	0.38	0.50	0.50	0.56	0.54	0.67
	2:05:00	0.00	0.00	0.16	0.22	0.28	0.29	0.32	0.31	0.38
	2:10:00	0.00	0.00	0.09	0.12	0.16	0.16	0.18	0.18	0.22
	2:15:00	0.00	0.00	0.04	0.06	0.08	0.09	0.10	0.09	0.12
	2:20:00	0.00	0.00	0.02	0.03	0.04	0.04	0.05	0.05	0.06
	2:25:00	0.00	0.00	0.01	0.01	0.01	0.02	0.02	0.02	0.02
	2:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

## INLET MANAGEMENT

Worksheet Protected

INLET NAME	Inlet 1	Inlet 2	Inlet 3	Inlet 4	Inlet 5	Inlet 6	Inlet 8	Inlet 14
Site Type (Urban or Rural)	URBAN	URBAN	URBAN	URBAN	URBAN	URBAN	URBAN	URBAN
Inlet Application (Street or Area)	STREET	STREET	STREET	STREET	STREET	AREA	STREET	AREA
Hydraulic Condition	On Grade	On Grade	On Grade	On Grade	In Sump	Swale	In Sump	Swale
Inlet Type	Denver No. 16 Valley Grate	Denver No. 16 Valley Grate	Denver No. 16 Valley Grate	Denver No. 16 Valley Grate	Denver No. 16 Valley Grate	CDOT Type D (In Series & Depressed)	Denver No. 16 Valley Grate	CDOT Type D (In Series & Depressed)

## USER-DEFINED INPUT

User-Defined Design Flows								
Minor $Q_{down}$ (cfs)	6.8	7.1	2.7	1.2	4.1	7.5	1.3	9.4
Major $Q_{down}$ (cfs)	12.7	13.2	6.4	3.4	9.7	14.4	2.4	27.5
Bypass (Carry-Over) Flow from Upstream								
Receive Bypass Flow from:	No Bypass Flow Received	No Bypass Flow Received	No Bypass Flow Received	No Bypass Flow Received	No Bypass Flow Received	No Bypass Flow Received	No Bypass Flow Received	No Bypass Flow Received
Minor Bypass Flow Received, $Q_b$ (cfs)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Major Bypass Flow Received, $Q_b$ (cfs)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Watershed Characteristics								
Subcatchment Area (acres)								
Percent Impervious								
NRCS Soil Type								
Watershed Profile								
Overland Slope (ft/ft)								
Overland Length (ft)								
Channel Slope (ft/ft)								
Channel Length (ft)								
Minor Storm Rainfall Input								
Design Storm Return Period, $T_r$ (years)								
One-Hour Precipitation, $P_1$ (inches)								
Major Storm Rainfall Input								
Design Storm Return Period, $T_r$ (years)								
One-Hour Precipitation, $P_1$ (inches)								

## CALCULATED OUTPUT

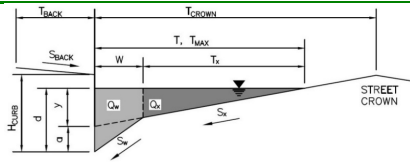
Minor Total Design Peak Flow, $Q$ (cfs)	6.8	7.1	2.7	1.2	4.1	7.5	1.3	9.4
Major Total Design Peak Flow, $Q$ (cfs)	12.7	13.2	6.4	3.4	9.7	14.4	2.4	27.5
Minor Flow Bypassed Downstream, $Q_b$ (cfs)	2.5	2.6	0.5	0.2	N/A	0.0	N/A	0.0
Major Flow Bypassed Downstream, $Q_b$ (cfs)	6.1	6.4	2.3	0.8	N/A	0.0	N/A	0.0

**ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)**

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: WireNut

Inlet ID: Inlet 1

**Gutter Geometry:**

Maximum Allowable Width for Spread Behind Curb

Side Slope Behind Curb (leave blank for no conveyance credit behind curb)

Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

Height of Curb at Gutter Flow Line

Distance from Curb Face to Street Crown

Gutter Width

Street Transverse Slope

Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)

Street Longitudinal Slope - Enter 0 for sump condition

Manning's Roughness for Street Section (typically between 0.012 and 0.020)

$T_{BACK} =$	5.0	ft
$S_{BACK} =$	0.020	ft/ft
$n_{BACK} =$	0.015	

$H_{CURB} =$	6.00	inches
$T_{CROWN} =$	15.3	ft
$W =$	2.50	ft
$S_x =$	0.022	ft/ft
$S_w =$	0.083	ft/ft
$S_o =$	0.020	ft/ft
$n_{STREET} =$	0.015	

Max. Allowable Spread for Minor &amp; Major Storm

Max. Allowable Depth at Gutter Flowline for Minor &amp; Major Storm

Allow Flow Depth at Street Crown (check box for yes, leave blank for no)

	Minor Storm	Major Storm	
$T_{MAX} =$	14.8	15.3	ft
$d_{MAX} =$	4.7	6.0	inches
	<input type="checkbox"/>	<input checked="" type="checkbox"/>	

MINOR STORM Allowable Capacity is based on Depth Criterion

MAJOR STORM Allowable Capacity is based on Depth Criterion

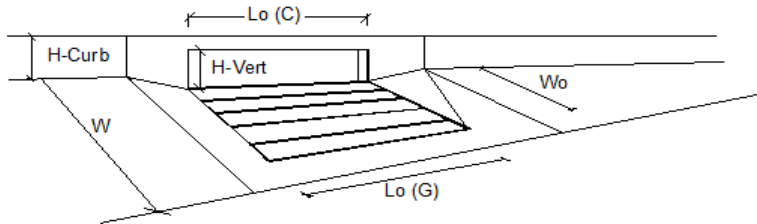
	Minor Storm	Major Storm	
$Q_{allow} =$	7.2	14.0	cfs

Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

# INLET ON A CONTINUOUS GRADE

MHFD-Inlet, Version 5.01 (April 2021)



Warning 1  
Warning 1

Design Information (Input)		MINOR		MAJOR	
Type of Inlet	Denver No. 16 Valley Grate	Type =	Denver No. 16 Valley Grate		
Local Depression (additional to continuous gutter depression 'a')		$a_{LOCAL}$ =	2.0	2.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)		$N_o$ =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)		$L_o$ =	10.92	10.92	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)		$W_o$ =	2.50	2.50	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)		$C_r-G$ =	0.50	0.50	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)		$C_r-C$ =	N/A	N/A	
<b>Street Hydraulics: OK - Q &lt; Allowable Street Capacity</b>					
Design Discharge for Half of Street (from Inlet Management)		$Q_o$ =	6.8	12.7	cfs
Water Spread Width		$T$ =	10.7	14.2	ft
Water Depth at Flowline (outside of local depression)		$d$ =	4.6	5.5	inches
Water Depth at Street Crown (or at $T_{MAX}$ )		$d_{CROWN}$ =	0.0	0.0	inches
Ratio of Gutter Flow to Design Flow		$E_o$ =	0.643	0.507	
Discharge outside the Gutter Section W, carried in Section $T_x$		$Q_x$ =	2.4	6.3	cfs
Discharge within the Gutter Section W		$Q_w$ =	4.4	6.4	cfs
Discharge Behind the Curb Face		$Q_{BACK}$ =	0.0	0.0	cfs
Flow Area within the Gutter Section W		$A_w$ =	0.71	0.89	sq ft
Velocity within the Gutter Section W		$V_w$ =	6.2	7.2	fps
Water Depth for Design Condition		$d_{LOCAL}$ =	6.6	7.5	inches
<b>Grate Analysis (Calculated)</b>					
Total Length of Inlet Grate Opening		$L$ =	10.92	10.92	ft
Ratio of Grate Flow to Design Flow		$E_{o-GRATE}$ =	0.642	0.507	
<b>Under No-Clogging Condition</b>					
Minimum Velocity Where Grate Splash-Over Begins		$V_o$ =	3.98	3.98	fps
Interception Rate of Frontal Flow		$R_f$ =	0.93	0.88	
Interception Rate of Side Flow		$R_s$ =	0.68	0.63	
Interception Capacity		$Q_i$ =	5.7	9.6	cfs
<b>Under Clogging Condition</b>					
Clogging Coefficient for Multiple-unit Grate Inlet		GrateCoef =	1.00	1.00	
Clogging Factor for Multiple-unit Grate Inlet		GrateClog =	0.50	0.50	
Effective (unclogged) Length of Multiple-unit Grate Inlet		$L_e$ =	5.46	5.46	ft
Minimum Velocity Where Grate Splash-Over Begins		$V_o$ =	2.73	2.73	fps
Interception Rate of Frontal Flow		$R_f$ =	0.82	0.76	
Interception Rate of Side Flow		$R_s$ =	0.30	0.26	
Actual Interception Capacity		$Q_a$ =	4.3	6.6	cfs
Carry-Over Flow = $Q_o - Q_a$ (to be applied to curb opening or next d/s inlet)		$Q_b$ =	2.5	6.1	cfs
<b>Curb or Slotted Inlet Opening Analysis (Calculated)</b>					
Equivalent Slope $S_e$ (based on grate carry-over)		$S_e$ =	N/A	N/A	ft/ft
Required Length $L_T$ to Have 100% Interception		$L_T$ =	N/A	N/A	ft
<b>Under No-Clogging Condition</b>					
Effective Length of Curb Opening or Slotted Inlet (minimum of $L$ , $L_T$ )		$L$ =	N/A	N/A	ft
Interception Capacity		$Q_i$ =	N/A	N/A	cfs
<b>Under Clogging Condition</b>					
Clogging Coefficient		CurbCoef =	N/A	N/A	
Clogging Factor for Multiple-unit Curb Opening or Slotted Inlet		CurbClog =	N/A	N/A	
Effective (Unclogged) Length		$L_e$ =	N/A	N/A	ft
Actual Interception Capacity		$Q_a$ =	N/A	N/A	cfs
Carry-Over Flow = $Q_o - Q_a$		$Q_b$ =	N/A	N/A	cfs
<b>Summary</b>					
Total Inlet Interception Capacity		$Q$ =	4.3	6.6	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)		$Q_b$ =	2.5	6.1	cfs
Capture Percentage = $Q_o/Q_a$		C% =	64	52	%

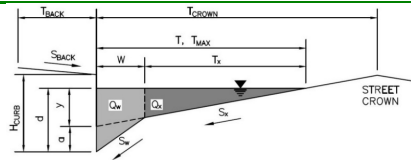
Warning 1: Dimension entered is not a typical dimension for inlet type specified.

**ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)**

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: WireNut

Inlet ID: Inlet 2

**Gutter Geometry:**

Maximum Allowable Width for Spread Behind Curb

Side Slope Behind Curb (leave blank for no conveyance credit behind curb)

Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

Height of Curb at Gutter Flow Line

Distance from Curb Face to Street Crown

Gutter Width

Street Transverse Slope

Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)

Street Longitudinal Slope - Enter 0 for sump condition

Manning's Roughness for Street Section (typically between 0.012 and 0.020)

$T_{BACK} =$	5.0	ft
$S_{BACK} =$	0.020	ft/ft
$n_{BACK} =$	0.015	

$H_{CURB} =$	6.00	inches
$T_{CROWN} =$	15.3	ft
$W =$	2.50	ft
$S_x =$	0.024	ft/ft
$S_w =$	0.083	ft/ft
$S_o =$	0.020	ft/ft
$n_{STREET} =$	0.015	

Max. Allowable Spread for Minor &amp; Major Storm

Max. Allowable Depth at Gutter Flowline for Minor &amp; Major Storm

Allow Flow Depth at Street Crown (check box for yes, leave blank for no)

	Minor Storm	Major Storm	
$T_{MAX} =$	14.8	15.3	ft
$d_{MAX} =$	4.8	6.0	inches
	<input type="checkbox"/>	<input checked="" type="checkbox"/>	

MINOR STORM Allowable Capacity is based on Depth Criterion

MAJOR STORM Allowable Capacity is based on Depth Criterion

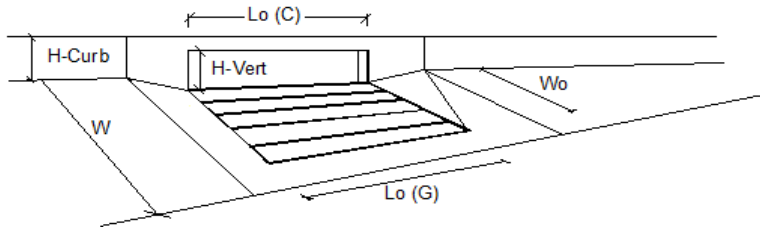
	Minor Storm	Major Storm	
$Q_{allow} =$	7.5	13.4	cfs

**Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'****Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'**



# INLET ON A CONTINUOUS GRADE

MHFD-Inlet, Version 5.01 (April 2021)



Design Information (Input)		MINOR		MAJOR	
Type of Inlet	Denver No. 16 Valley Grate	Type =	Denver No. 16 Valley Grate		
Local Depression (additional to continuous gutter depression 'a')		$a_{LOCAL} =$	2.0	2.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)		$N_o =$	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)		$L_o =$	10.92	10.92	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)		$W_o =$	2.50	2.50	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)		$C_r-G =$	0.50	0.50	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)		$C_r-C =$	N/A	N/A	
<b>Street Hydraulics: OK - Q &lt; Allowable Street Capacity</b>		MINOR		MAJOR	
Total Inlet Interception Capacity		$Q =$	4.5	6.8	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)		$Q_o =$	2.6	6.4	cfs
Capture Percentage = $Q_i/Q_o =$		$C\% =$	63	52	%

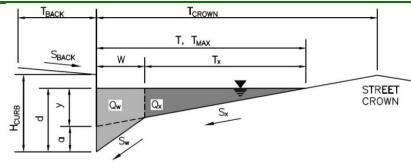
Warning 1: Dimension entered is not a typical dimension for inlet type specified.

**ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)**

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: WireNut

Inlet ID: Inlet 3

**Gutter Geometry:**

Maximum Allowable Width for Spread Behind Curb

Side Slope Behind Curb (leave blank for no conveyance credit behind curb)

Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

Height of Curb at Gutter Flow Line

Distance from Curb Face to Street Crown

Gutter Width

Street Transverse Slope

Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)

Street Longitudinal Slope - Enter 0 for sump condition

Manning's Roughness for Street Section (typically between 0.012 and 0.020)

$T_{BACK} =$	5.0	ft
$S_{BACK} =$	0.020	ft/ft
$n_{BACK} =$	0.015	

$H_{CURB} =$	6.00	inches
$T_{CROWN} =$	15.3	ft
$W =$	2.50	ft
$S_x =$	0.022	ft/ft
$S_w =$	0.083	ft/ft
$S_o =$	0.020	ft/ft
$n_{STREET} =$	0.015	

Max. Allowable Spread for Minor &amp; Major Storm

Max. Allowable Depth at Gutter Flowline for Minor &amp; Major Storm

Allow Flow Depth at Street Crown (check box for yes, leave blank for no)

	Minor Storm	Major Storm	
$T_{MAX} =$	14.8	15.3	ft
$d_{MAX} =$	4.1	6.0	inches
	<input type="checkbox"/>	<input checked="" type="checkbox"/>	

MINOR STORM Allowable Capacity is based on Depth Criterion

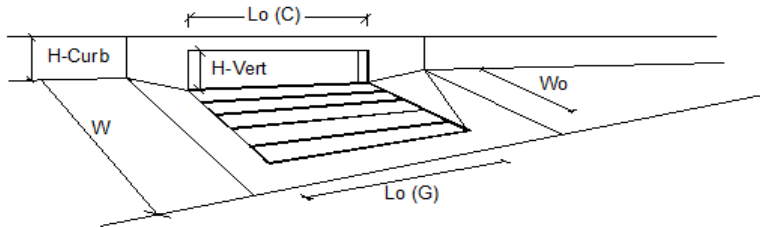
MAJOR STORM Allowable Capacity is based on Depth Criterion

	Minor Storm	Major Storm	
$Q_{allow} =$	4.5	14.0	cfs

**Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'****Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'**

# INLET ON A CONTINUOUS GRADE

MHFD-Inlet, Version 5.01 (April 2021)



Design Information (Input)		MINOR		MAJOR	
Type of Inlet	Denver No. 16 Valley Gate	Type =	Denver No. 16 Valley Gate		
Local Depression (additional to continuous gutter depression 'a')		$a_{LOCAL} =$	2.0	2.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)		$N_o =$	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)		$L_o =$	10.92	10.92	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)		$W_o =$	2.50	2.50	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)		$C_r-G =$	0.50	0.50	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)		$C_r-C =$	N/A	N/A	
<b>Street Hydraulics: OK - Q &lt; Allowable Street Capacity</b>		MINOR		MAJOR	
Total Inlet Interception Capacity		$Q =$	2.2	4.1	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)		$Q_o =$	0.5	2.3	cfs
Capture Percentage = $Q_o/Q_o =$		$C\% =$	80	65	%

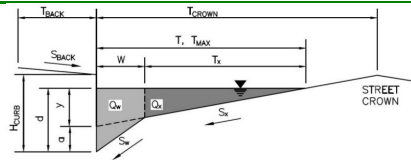
Warning 1: Dimension entered is not a typical dimension for inlet type specified.

**ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)**

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: WireNut

Inlet ID: Inlet 4

**Gutter Geometry:**

Maximum Allowable Width for Spread Behind Curb

Side Slope Behind Curb (leave blank for no conveyance credit behind curb)

Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

Height of Curb at Gutter Flow Line

Distance from Curb Face to Street Crown

Gutter Width

Street Transverse Slope

Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)

Street Longitudinal Slope - Enter 0 for sump condition

Manning's Roughness for Street Section (typically between 0.012 and 0.020)

$T_{BACK} =$	5.0	ft
$S_{BACK} =$	0.020	ft/ft
$n_{BACK} =$	0.015	

$H_{CURB} =$	6.00	inches
$T_{CROWN} =$	15.3	ft
$W =$	2.50	ft
$S_x =$	0.024	ft/ft
$S_y =$	0.083	ft/ft
$S_o =$	0.020	ft/ft
$n_{STREET} =$	0.015	

Max. Allowable Spread for Minor &amp; Major Storm

Max. Allowable Depth at Gutter Flowline for Minor &amp; Major Storm

Allow Flow Depth at Street Crown (check box for yes, leave blank for no)

	Minor Storm	Major Storm	
$T_{MAX} =$	14.8	15.3	ft
$d_{MAX} =$	4.1	6.0	inches
	<input type="checkbox"/>	<input checked="" type="checkbox"/>	

MINOR STORM Allowable Capacity is based on Depth Criterion

MAJOR STORM Allowable Capacity is based on Depth Criterion

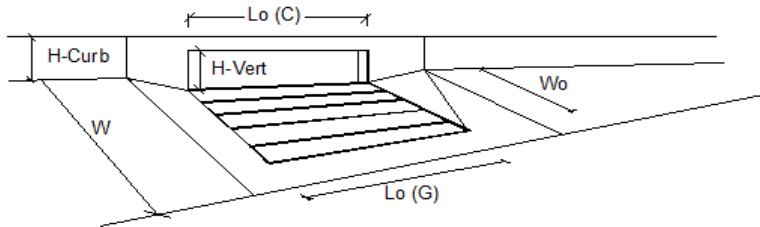
	Minor Storm	Major Storm	
$Q_{allow} =$	4.4	13.4	cfs

Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

# INLET ON A CONTINUOUS GRADE

MHFD-Inlet, Version 5.01 (April 2021)



Design Information (Input)		MINOR		MAJOR	
Type of Inlet	Denver No. 16 Valley Gate	Type =	Denver No. 16 Valley Gate		
Local Depression (additional to continuous gutter depression 'a')		$a_{LOCAL} =$	2.0	2.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)		$N_o =$	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)		$L_o =$	10.92	10.92	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)		$W_o =$	2.50	2.50	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)		$C_r-G =$	0.50	0.50	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)		$C_r-C =$	N/A	N/A	
<b>Street Hydraulics: OK - Q &lt; Allowable Street Capacity</b>		MINOR		MAJOR	
Total Inlet Interception Capacity		$Q =$	1.0	2.6	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)		$Q_o =$	0.2	0.8	cfs
Capture Percentage = $Q_i/Q_o =$		$C\% =$	85	77	%

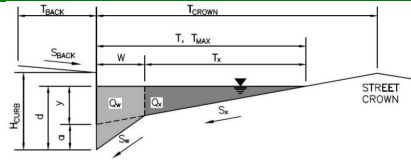
Warning 1: Dimension entered is not a typical dimension for inlet type specified.

**ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)**

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: WireNut

Inlet ID: Inlet 5

**Gutter Geometry:**

Maximum Allowable Width for Spread Behind Curb

Side Slope Behind Curb (leave blank for no conveyance credit behind curb)

Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

Height of Curb at Gutter Flow Line

Distance from Curb Face to Street Crown

Gutter Width

Street Transverse Slope

Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)

Street Longitudinal Slope - Enter 0 for sump condition

Manning's Roughness for Street Section (typically between 0.012 and 0.020)

Max. Allowable Spread for Minor &amp; Major Storm

Max. Allowable Depth at Gutter Flowline for Minor &amp; Major Storm

Check boxes are not applicable in SUMP conditions

MINOR STORM Allowable Capacity is based on Depth Criterion

MAJOR STORM Allowable Capacity is based on Depth Criterion

$T_{BACK}$	=	5.0	ft
$S_{BACK}$	=	0.020	ft/ft
$n_{BACK}$	=	0.015	

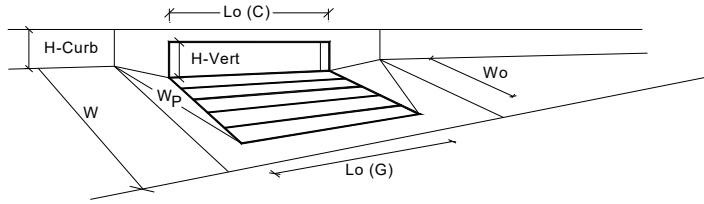
$H_{CURB}$	=	6.00	inches
$T_{CROWN}$	=	15.3	ft
$W$	=	2.50	ft
$S_x$	=	0.024	ft/ft
$S_w$	=	0.083	ft/ft
$S_o$	=	0.000	ft/ft
$n_{STREET}$	=	0.015	

	Minor Storm	Major Storm	
$T_{MAX}$	14.8	15.3	ft
$d_{MAX}$	6.0	8.0	inches
	<input type="checkbox"/>	<input type="checkbox"/>	

	Minor Storm	Major Storm	
$Q_{allow}$	SUMP	SUMP	cfs

# INLET IN A SUMP OR SAG LOCATION

MHFD-Inlet, Version 5.01 (April 2021)



**Warning 1**

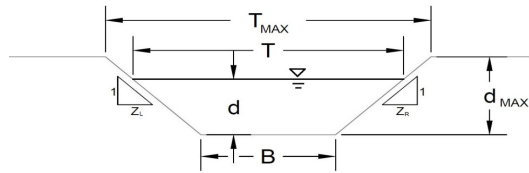
Design Information (Input)		MINOR		MAJOR	
Type of Inlet	Denver No. 16 Valley Grate	Type =	Denver No. 16 Valley Grate		
Local Depression (additional to continuous gutter depression 'a' from above)		$a_{local}$ =	2.00	2.00	inches
Number of Unit Inlets (Grate or Curb Opening)		No =	1	1	
Water Depth at Flowline (outside of local depression)		Ponding Depth =	6.1	8.6	inches
<b>Grate Information</b>			MINOR	MAJOR	<input checked="" type="checkbox"/> Override Depths
Length of a Unit Grate		$L_o (G)$ =	10.92	10.92	feet
Width of a Unit Grate		$W_o$ =	2.50	2.50	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)		$A_{ratio}$ =	0.31	0.31	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)		$C_f (G)$ =	0.50	0.50	
Grate Weir Coefficient (typical value 2.15 - 3.60)		$C_w (G)$ =	3.60	3.60	
Grate Orifice Coefficient (typical value 0.60 - 0.80)		$C_o (G)$ =	0.60	0.60	
<b>Curb Opening Information</b>			MINOR	MAJOR	
Length of a Unit Curb Opening		$L_o (C)$ =	N/A	N/A	feet
Height of Vertical Curb Opening in Inches		$H_{vert}$ =	N/A	N/A	inches
Height of Curb Orifice Throat in Inches		$H_{throat}$ =	N/A	N/A	inches
Angle of Throat (see USDCM Figure ST-5)		Theta =	N/A	N/A	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)		$W_p$ =	N/A	N/A	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)		$C_f (C)$ =	N/A	N/A	
Curb Opening Weir Coefficient (typical value 2.3-3.7)		$C_w (C)$ =	N/A	N/A	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)		$C_o (C)$ =	N/A	N/A	
<b>Low Head Performance Reduction (Calculated)</b>			MINOR	MAJOR	
Depth for Grate Midwidth		$d_{Grate}$ =	0.488	0.696	ft
Depth for Curb Opening Weir Equation		$d_{Curb}$ =	N/A	N/A	ft
Combination Inlet Performance Reduction Factor for Long Inlets		$RF_{Combination}$ =	N/A	N/A	
Curb Opening Performance Reduction Factor for Long Inlets		$RF_{Curb}$ =	N/A	N/A	
Grated Inlet Performance Reduction Factor for Long Inlets		$RF_{Grate}$ =	0.58	0.81	
Total Inlet Interception Capacity (assumes clogged condition)			MINOR	MAJOR	
<b>Inlet Capacity IS GOOD for Minor and Major Storms(&gt;Q PEAK)</b>		$Q_a$ =	4.1	9.9	cfs
		$Q_{PEAK REQUIRED}$ =	4.1	9.7	cfs

**Warning 1: Dimension entered is not a typical dimension for inlet type specified.**

MHFD-Inlet, Version 5.01 (April 2021)

## AREA INLET IN A SWALE

WireNut  
Inlet 6



This worksheet uses the NRCS vegetal retardance method to determine Manning's n.

For more information see Section 7.2.3 of the USDCM.

### Analysis of Trapezoidal Grass-Lined Channel Using SCS Method

NRCS Vegetal Retardance (A, B, C, D, or E)

Manning's n (Leave cell D16 blank to manually enter an n value)

Channel Invert Slope

Bottom Width

Left Side Slope

Right Side Slope

Check one of the following soil types:

Soil Type:	Max. Velocity ( $V_{MAX}$ )	Max Froude No. ( $F_{MAX}$ )
Non-Cohesive	5.0 fps	0.60
Cohesive	7.0 fps	0.80
Paved	N/A	N/A

A, B, C, D, or E =

C
see details below
$S_0 = 0.0200$ ft/ft
$B = 3.00$ ft
$Z1 = 3.00$ ft/ft
$Z2 = 3.00$ ft/ft

Choose One:

- ☐ Non-Cohesive  
☒ Cohesive  
☐ Paved

Maximum Allowable Top Width of Channel for Minor & Major Storm

Maximum Allowable Water Depth in Channel for Minor & Major Storm

	Minor Storm	Major Storm	
$T_{MAX} =$	13.00	13.00	ft
$d_{MAX} =$	1.10	1.30	ft

### Allowable Channel Capacity Based On Channel Geometry

MINOR STORM Allowable Capacity is based on Depth Criterion

MAJOR STORM Allowable Capacity is based on Depth Criterion

	Minor Storm	Major Storm	
$Q_{allow} =$	20.9	35.8	cfs
$d_{allow} =$	1.10	1.30	ft

### Water Depth in Channel Based On Design Peak Flow

Design Peak Flow

Water Depth

$Q_o =$	7.5	14.4	cfs
$d =$	0.84	1.00	ft

Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'



MHFD-Inlet, Version 5.01 (April 2021)

## AREA INLET IN A SWALE

WireNut  
Inlet 6

### Inlet Design Information (Input)

Type of Inlet

CDOT Type D (In Series & Depressed)

Inlet Type = CDOT Type D (In Series & Depressed)

Angle of Inclined Gate (must be  $\leq 30$  degrees)

Width of Gate

Length of Gate

Open Area Ratio

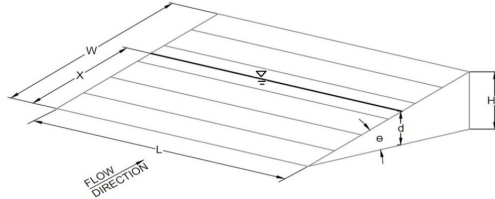
Height of Inclined Gate

Clogging Factor

Grate Discharge Coefficient

Orifice Coefficient

Weir Coefficient



$\theta =$  0.00 degrees

W = 3.00 ft

L = 6.00 ft

A<sub>RATIO</sub> = 0.70

H<sub>B</sub> = 0.00 ft

C<sub>f</sub> = 0.38

C<sub>d</sub> = 0.72

C<sub>o</sub> = 0.48

C<sub>w</sub> = 1.53

Water Depth at Inlet (for depressed inlets, 1 foot is added for depression)

Total Inlet Interception Capacity (assumes clogged condition)

Bypassed Flow

Capture Percentage =  $Q_a/Q_o$

	MINOR	MAJOR	
d =	1.84	2.00	
Q <sub>a</sub> =	40.9	42.6	cfs
Q <sub>b</sub> =	0.0	0.0	cfs
C% =	100	100	%

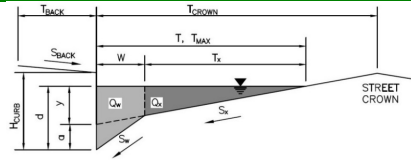
**Warning 01: Sideslope steepness exceeds USDCM Volume I recommendation.**

**ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)**

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: WireNut

Inlet ID: Inlet 8

**Gutter Geometry:**

Maximum Allowable Width for Spread Behind Curb

Side Slope Behind Curb (leave blank for no conveyance credit behind curb)

Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

Height of Curb at Gutter Flow Line

Distance from Curb Face to Street Crown

Gutter Width

Street Transverse Slope

Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)

Street Longitudinal Slope - Enter 0 for sump condition

Manning's Roughness for Street Section (typically between 0.012 and 0.020)

Max. Allowable Spread for Minor &amp; Major Storm

Max. Allowable Depth at Gutter Flowline for Minor &amp; Major Storm

Check boxes are not applicable in SUMP conditions

MINOR STORM Allowable Capacity is based on Depth Criterion

MAJOR STORM Allowable Capacity is based on Depth Criterion

$T_{BACK}$	=	5.0	ft
$S_{BACK}$	=	0.020	ft/ft
$n_{BACK}$	=	0.015	

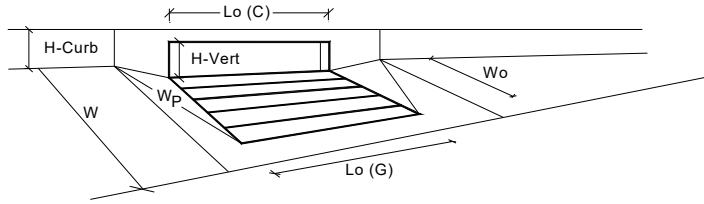
$H_{CURB}$	=	6.00	inches
$T_{CROWN}$	=	15.3	ft
$W$	=	2.50	ft
$S_x$	=	0.022	ft/ft
$S_w$	=	0.083	ft/ft
$S_o$	=	0.000	ft/ft
$n_{STREET}$	=	0.015	

	Minor Storm	Major Storm	
$T_{MAX}$	14.8	15.3	ft
$d_{MAX}$	4.2	6.0	inches
	<input type="checkbox"/>	<input type="checkbox"/>	

	Minor Storm	Major Storm	
$Q_{allow}$	SUMP	SUMP	cfs

# INLET IN A SUMP OR SAG LOCATION

MHFD-Inlet, Version 5.01 (April 2021)



Warning 1

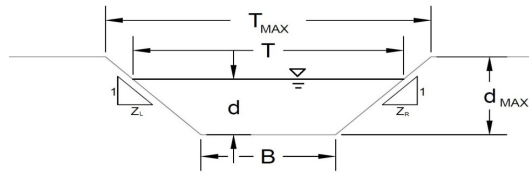
Design Information (Input)		MINOR		MAJOR	
Type of Inlet	Denver No. 16 Valley Grate	Type =	Denver No. 16 Valley Grate		
Local Depression (additional to continuous gutter depression 'a' from above)		$a_{local}$ =	2.00	2.00	inches
Number of Unit Inlets (Grate or Curb Opening)		No =	1	1	
Water Depth at Flowline (outside of local depression)		Ponding Depth =	4.2	5.9	inches
<b>Grate Information</b>			MINOR	MAJOR	<input type="checkbox"/> Override Depths
Length of a Unit Grate		$L_o (G)$ =	3.64	3.64	feet
Width of a Unit Grate		$W_o$ =	2.50	2.50	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)		$A_{ratio}$ =	0.31	0.31	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)		$C_f (G)$ =	0.50	0.50	
Grate Weir Coefficient (typical value 2.15 - 3.60)		$C_w (G)$ =	3.60	3.60	
Grate Orifice Coefficient (typical value 0.60 - 0.80)		$C_o (G)$ =	0.60	0.60	
<b>Curb Opening Information</b>			MINOR	MAJOR	
Length of a Unit Curb Opening		$L_o (C)$ =	N/A	N/A	feet
Height of Vertical Curb Opening in Inches		$H_{vert}$ =	N/A	N/A	inches
Height of Curb Orifice Throat in Inches		$H_{throat}$ =	N/A	N/A	inches
Angle of Throat (see USDCM Figure ST-5)		Theta =	N/A	N/A	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)		$W_p$ =	N/A	N/A	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)		$C_f (C)$ =	N/A	N/A	
Curb Opening Weir Coefficient (typical value 2.3-3.7)		$C_w (C)$ =	N/A	N/A	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)		$C_o (C)$ =	N/A	N/A	
<b>Low Head Performance Reduction (Calculated)</b>			MINOR	MAJOR	
Depth for Grate Midwidth		$d_{Grate}$ =	0.330	0.469	ft
Depth for Curb Opening Weir Equation		$d_{Curb}$ =	N/A	N/A	ft
Combination Inlet Performance Reduction Factor for Long Inlets		$RF_{Combination}$ =	N/A	N/A	
Curb Opening Performance Reduction Factor for Long Inlets		$RF_{Curb}$ =	N/A	N/A	
Grated Inlet Performance Reduction Factor for Long Inlets		$RF_{Grate}$ =	0.61	0.86	
Total Inlet Interception Capacity (assumes clogged condition)			MINOR	MAJOR	
<b>Inlet Capacity IS GOOD for Minor and Major Storms(&gt;Q PEAK)</b>		$Q_a$ =	1.3	3.1	cfs
		$Q_{PEAK REQUIRED}$ =	1.3	2.4	cfs

Warning 1: Dimension entered is not a typical dimension for inlet type specified.

MHFD-Inlet, Version 5.01 (April 2021)

## AREA INLET IN A SWALE

WireNut  
Inlet 14



This worksheet uses the NRCS vegetal retardance method to determine Manning's n.

For more information see Section 7.2.3 of the USDCM.

### Analysis of Trapezoidal Grass-Lined Channel Using SCS Method

NRCS Vegetal Retardance (A, B, C, D, or E)

Manning's n (Leave cell D16 blank to manually enter an n value)

Channel Invert Slope

Bottom Width

Left Side Slope

Right Side Slope

Check one of the following soil types:

Soil Type:	Max. Velocity ( $V_{MAX}$ )	Max Froude No. ( $F_{MAX}$ )
Non-Cohesive	5.0 fps	0.60
Cohesive	7.0 fps	0.80
Paved	N/A	N/A

A, B, C, D, or E =

C
see details below
$S_0 = 0.0200$ ft/ft
$B = 0.00$ ft
$Z_1 = 3.00$ ft/ft
$Z_2 = 3.00$ ft/ft

Choose One:

- ☐ Non-Cohesive  
☐ Cohesive  
☐ Paved

Maximum Allowable Top Width of Channel for Minor & Major Storm

Maximum Allowable Water Depth in Channel for Minor & Major Storm

	Minor Storm	Major Storm	
$T_{MAX} =$	14.00	16.00	ft
$d_{MAX} =$	1.30	1.60	ft

### Allowable Channel Capacity Based On Channel Geometry

MINOR STORM Allowable Capacity is based on Depth Criterion

MAJOR STORM Allowable Capacity is based on Depth Criterion

	Minor Storm	Major Storm	
$Q_{allow} =$	10.6	27.7	cfs
$d_{allow} =$	1.30	1.60	ft

### Water Depth in Channel Based On Design Peak Flow

Design Peak Flow

Water Depth

$Q_o =$	9.4	27.5	cfs
$d =$	1.27	1.60	ft

Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

MHFD-Inlet, Version 5.01 (April 2021)

## AREA INLET IN A SWALE

**WireNut**  
**Inlet 14**

### Inlet Design Information (Input)

Type of Inlet

CDOT Type D (In Series & Depressed)

Inlet Type = CDOT Type D (In Series & Depressed)

Angle of Inclined Grate (must be  $\leq 30$  degrees)

Width of Grate

Length of Grate

Open Area Ratio

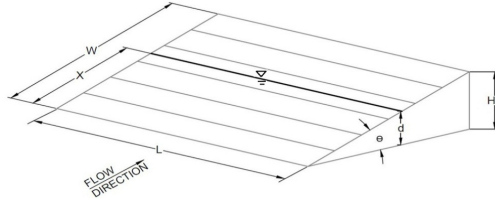
Height of Inclined Grate

Clogging Factor

Grate Discharge Coefficient

Orifice Coefficient

Weir Coefficient



$\theta = 0.00$  degrees

$W = 3.00$  ft

$L = 6.00$  ft

$A_{RATIO} = 0.70$

$H_b = 0.00$  ft

$C_f = 0.38$

$C_d = 0.72$

$C_o = 0.48$

$C_w = 1.53$

Water Depth at Inlet (for depressed inlets, 1 foot is added for depression)

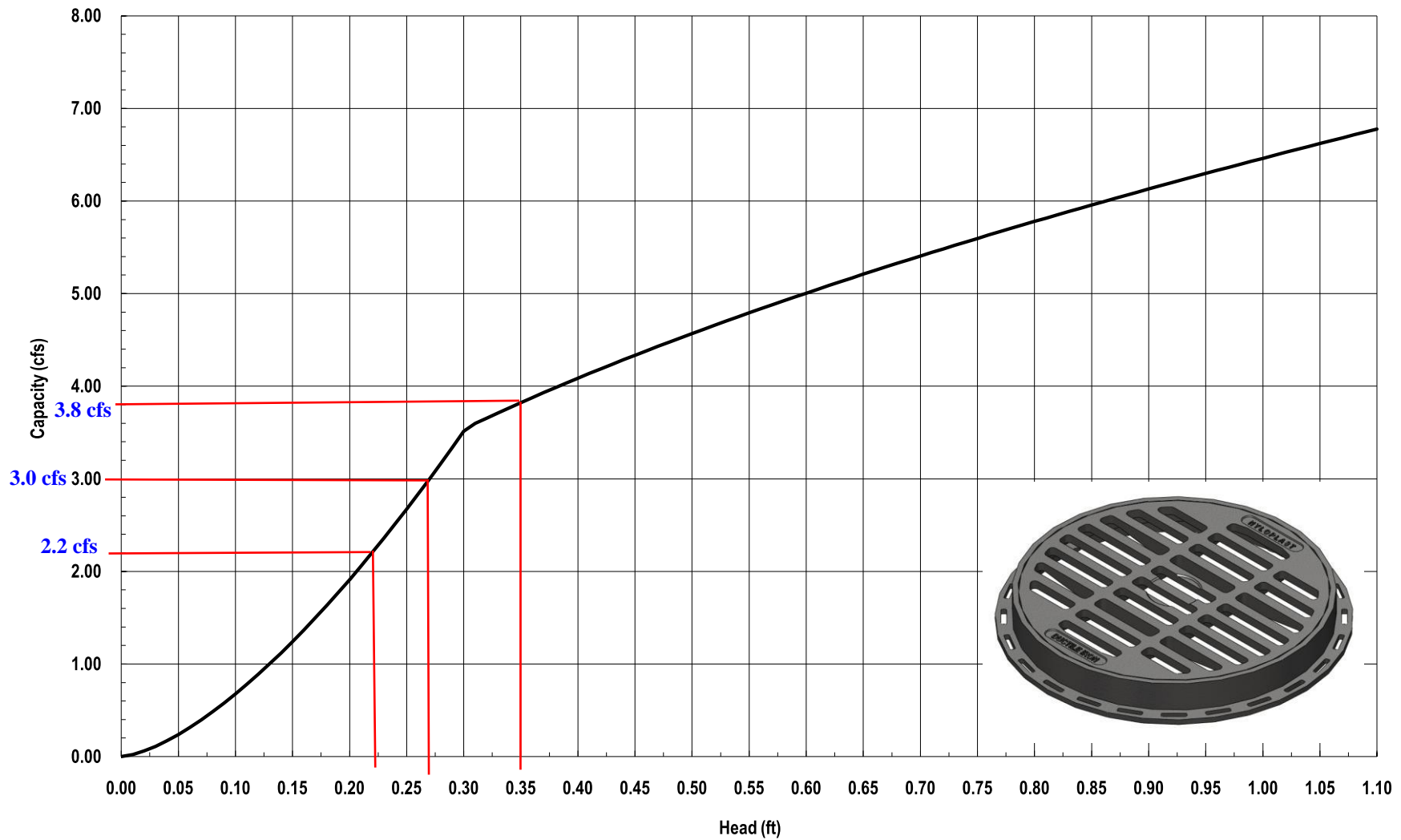
Total Inlet Interception Capacity (assumes clogged condition)

Bypassed Flow

Capture Percentage =  $Q_a/Q_o$

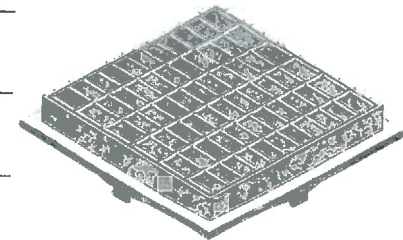
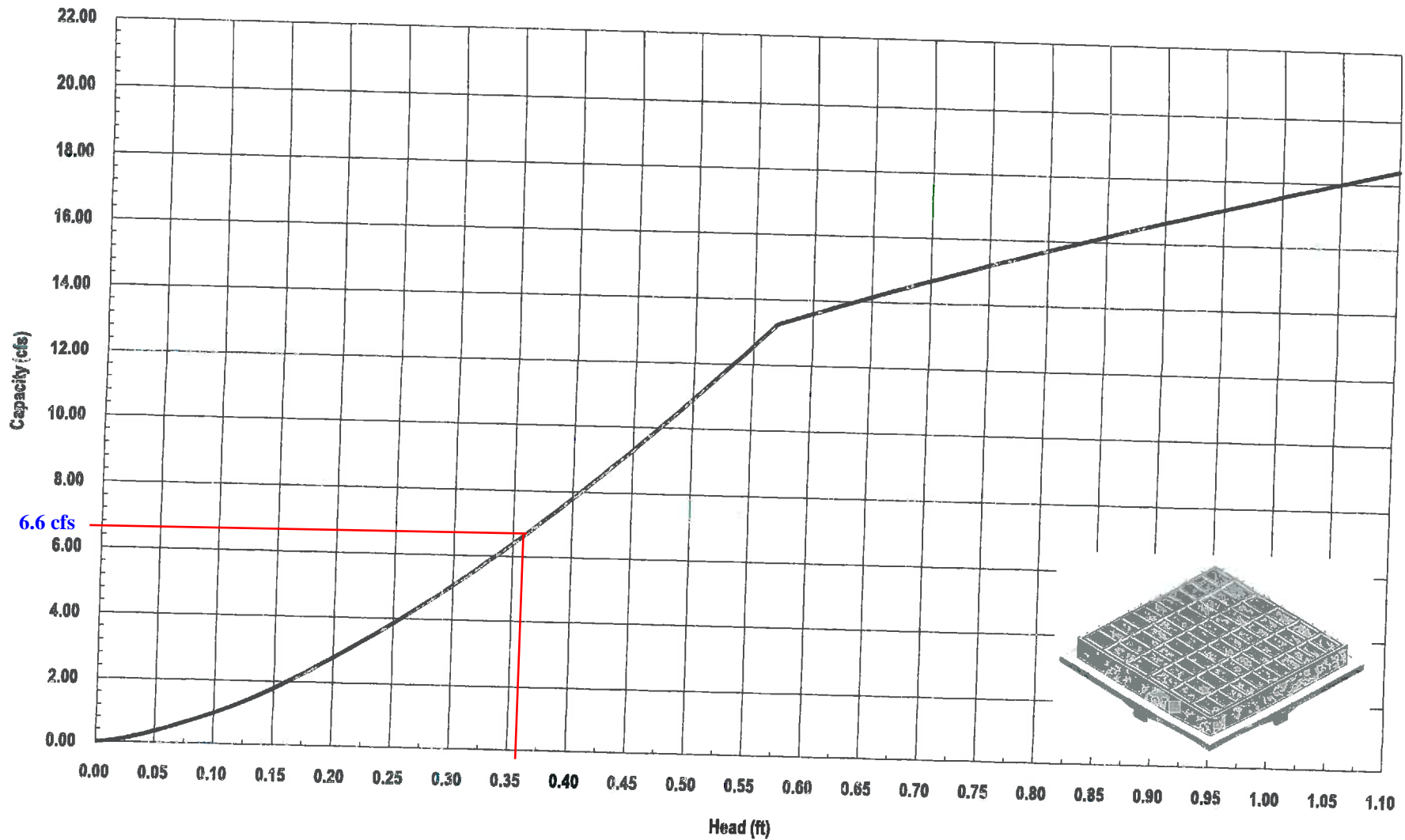
	MINOR	MAJOR	
$d =$	2.27	2.60	
$Q_a =$	45.4	48.6	cfs
$Q_b =$	0.0	0.0	cfs
$C\% =$	100	100	%

Nyloplast 24" Standard Grate Inlet Capacity Chart



**DP7=  $Q_{100}=1.5$  cfs 50% BLOCKAGE = 3.0 cfs**  
**DP9=  $Q_{100}=1.9$  cfs 50% BLOCKAGE = 3.8 cfs**  
**DP11= $Q_{100}=1.5$  cfs 50% BLOCKAGE = 3.0 cfs**  
**DP12= $Q_{100}=1.1$  cfs 50% BLOCKAGE = 2.2 cfs**

Nyloplast 2' x 2' Steel Bar / MAG Grate Inlet Capacity Chart



DP10= Q<sub>100</sub>=3.3 cfs 50% BLOCKAGE = 6.6 cfs



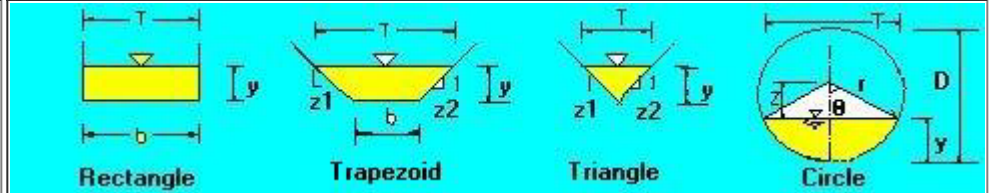
**Nyloplast**

3130 Verona Avenue • Buford, GA 30518  
 (866) 888-8479 / (770) 932-2443 • Fax: (770) 932-2490  
 © Nyloplast Inlet Capacity Charts June 2012

# The open channel flow calculator

Select Channel Type:

Triangle ▼



Velocity(V)&Discharge(Q) ▼

Select unit system: Feet(ft) ▼

Channel slope: .02  
ft/ft

Water depth(y): 1.25 ft

Bottom W(b) 0  
ft

Flow velocity 5.9328  
ft/s

LeftSlope (Z1): 3 to 1 (H:V)

RightSlope (Z2): 3  
to 1 (H:V)

Flow discharge 27.8101  
ft<sup>3</sup>/s

Input n value 0.025 or select n

Calculate!

Status: Calculation finished

Reset

Wetted perimeter 7.91  
ft

Flow area 4.69 ft<sup>2</sup>

Top width(T) 7.5  
ft

Specific energy 1.8  
ft

Froude number 1.32

Flow status  
Supercritical flow

Critical depth 1.4  
ft

Critical slope 0.0109 ft/ft

Velocity head 0.55  
ft

Copyright 2000 Dr. Xing Fang, Department of Civil Engineering, Lamar University.

DP14~Q<sub>100</sub>=27.5 cfs



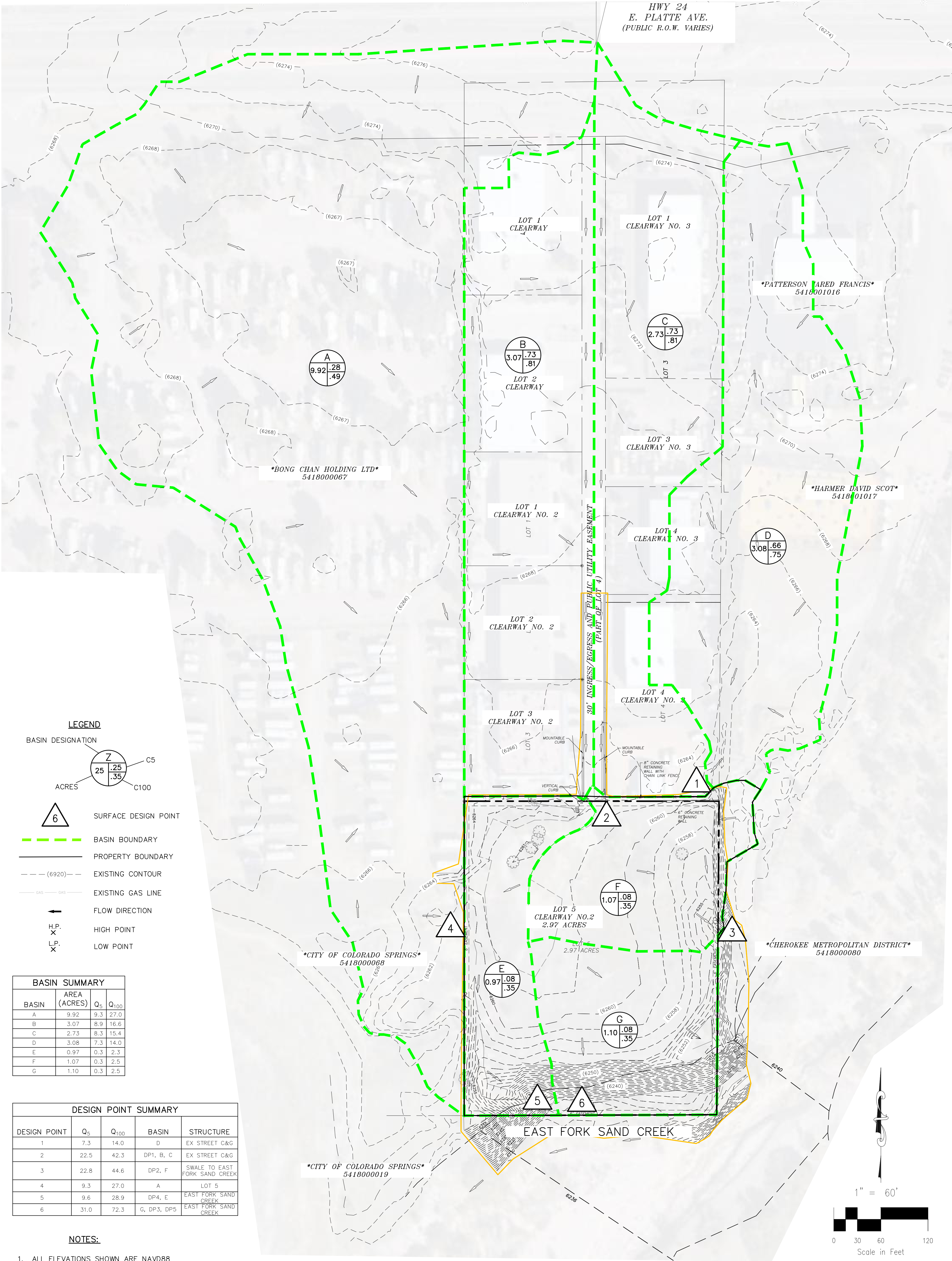
## **EXISTING AND PROPOSED DRAINAGE MAPS**

CLEARWAY NO. 2, LOT 5 (WIRENUT)

CITY OF COLORADO SPRINGS, STATE OF COLORADO

EXISTING DRAINAGE MAP

JUNE 2022



LEGEND

BASIN DESIGNATION

Z

25

.25

.35

C5

C100

ACRES

6

6

SURFACE DESIGN POINT

6

6

BASIN BOUNDARY

6

6

PROPERTY BOUNDARY

6

6

EXISTING CONTOUR

6

6

EXISTING GAS LINE

6

6

FLOW DIRECTION

6

6

HIGH POINT

6

6

LOW POINT

6

6

BASIN SUMMARY			
BASIN	AREA (ACRES)	Q <sub>5</sub>	Q <sub>100</sub>
A	9.92	9.3	27.0
B	3.07	8.9	16.6
C	2.73	8.3	15.4
D	3.08	7.3	14.0
E	0.97	0.3	2.3
F	1.07	0.3	2.5
G	1.10	0.3	2.5

DESIGN POINT SUMMARY				
DESIGN POINT	Q <sub>5</sub>	Q <sub>100</sub>	BASIN	STRUCTURE
1	7.3	14.0	D	EX STREET C&G
2	22.5	42.3	DP1, B, C	EX STREET C&G
3	22.8	44.6	DP2, F	SWALE TO EAST FORK SAND CREEK
4	9.3	27.0	A	LOT 5
5	9.6	28.9	DP4, E	EAST FORK SAND CREEK
6	31.0	72.3	G, DP3, DP5	EAST FORK SAND CREEK

- NOTES:
1. ALL ELEVATIONS SHOWN ARE NAVD88

2. ALL RUNOFF IS TRIBUTARY TO THE EAST FORK SAND CREEK DRAINAGE BASIN

VIRGIL A. SANCHEZ, COLORADO P.E. NO. 37160

FOR AND ON BEHALF OF  
M&S CIVIL CONSULTANTS, INC.



212 N. WAHSATCH AVE., STE 305  
COLORADO SPRINGS, CO 80903  
PHONE: 719.955.5485

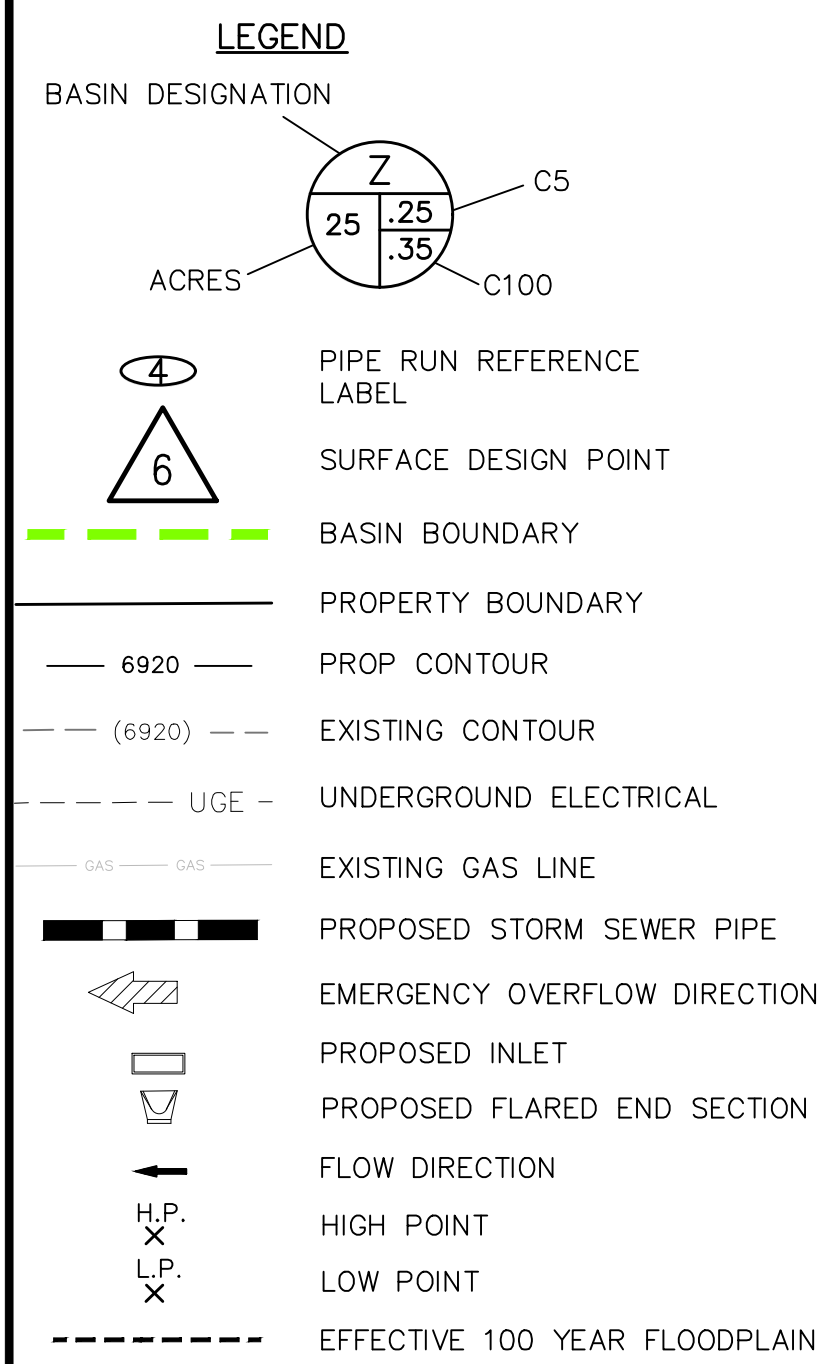
CLEARWAY NO. 2, LOT 5

EXISTING DRAINAGE MAP

PROJECT NO. 44-042	SCALE: HORIZONTAL: 1"=60' VERTICAL: N/A	DATE: 06/02/2022	SHEET 1 OF 1	EDM
DESIGNED BY: TAU DRAWN BY: DLM CHECKED BY: VAS				



CLEARWAY NO. 2, LOT 5 (WIRENUT)  
CITY OF COLORADO SPRINGS, STATE OF COLORADO  
PROPOSED DRAINAGE MAP  
JUNE 2022



DESIGN POINT SUMMARY				
DESIGN POINT	Q <sub>5</sub>	Q <sub>100</sub>	BASIN	STRUCTURE
1	6.8	12.7	B	MOD TRIPLE DENVER TYPE 16 INLET
2	7.1	13.2	C	MOD TRIPLE DENVER TYPE 16 INLET
3	2.7	6.4	FB1, F	MOD TRIPLE DENVER TYPE 16 INLET
4	1.2	3.4	FB2, G	MOD TRIPLE DENVER TYPE 16 INLET
5	4.1	9.7	FB3, FB4, E	MOD TRIPLE DENVER TYPE 16 INLET
6	7.5	14.4	D	CDOT TYPE D GRATE INLET
7	0.8	1.5	I	NYLOPLAST 24" GRATE INLET
8	1.3	2.4	H	MOD SINGLE DENVER TYPE 16 INLET
9	1.0	1.9	O	NYLOPLAST 24" GRATE INLET
10	1.8	3.3	N	NYLOPLAST 2'x2' STEEL BAR INLET
11	0.9	1.5	L	NYLOPLAST 24" GRATE INLET
12	0.6	1.1	M	NYLOPLAST 24" GRATE INLET
13	6.7	12.8	Q	FSD POND
14	9.4	27.5	A, R	CDOT TYPE D GRATE INLET
15	0.1	0.7	P	SWALE CONVEYS FLOW TO EAST FORK SAND CREEK
16	28.8	71.5	S, DP15, PR40, PR41	EAST FORK SAND CREEK

BASIN SUMMARY				
BASIN	AREA (ACRES)	Q <sub>5</sub>	Q <sub>100</sub>	
A	9.92	9.3	27.0	
B	2.30	6.8	12.7	
C	2.40	7.1	13.2	
D	3.18	7.5	14.4	
E	0.95	3.3	6.1	
F	0.02	0.1	0.2	
G	0.04	0.2	0.4	
H	0.33	1.3	2.4	
I	0.19	0.8	1.5	
J	0.21	0.8	1.5	
K	0.20	0.7	1.4	
L	0.18	0.9	1.5	
M	0.13	0.6	1.1	
N	0.40	1.8	3.3	
O	0.25	1.0	1.9	
P	0.26	0.1	0.7	
Q	0.23	0.1	0.6	
R	0.22	0.1	0.5	
S	0.55	0.4	3.2	

1" = 30'

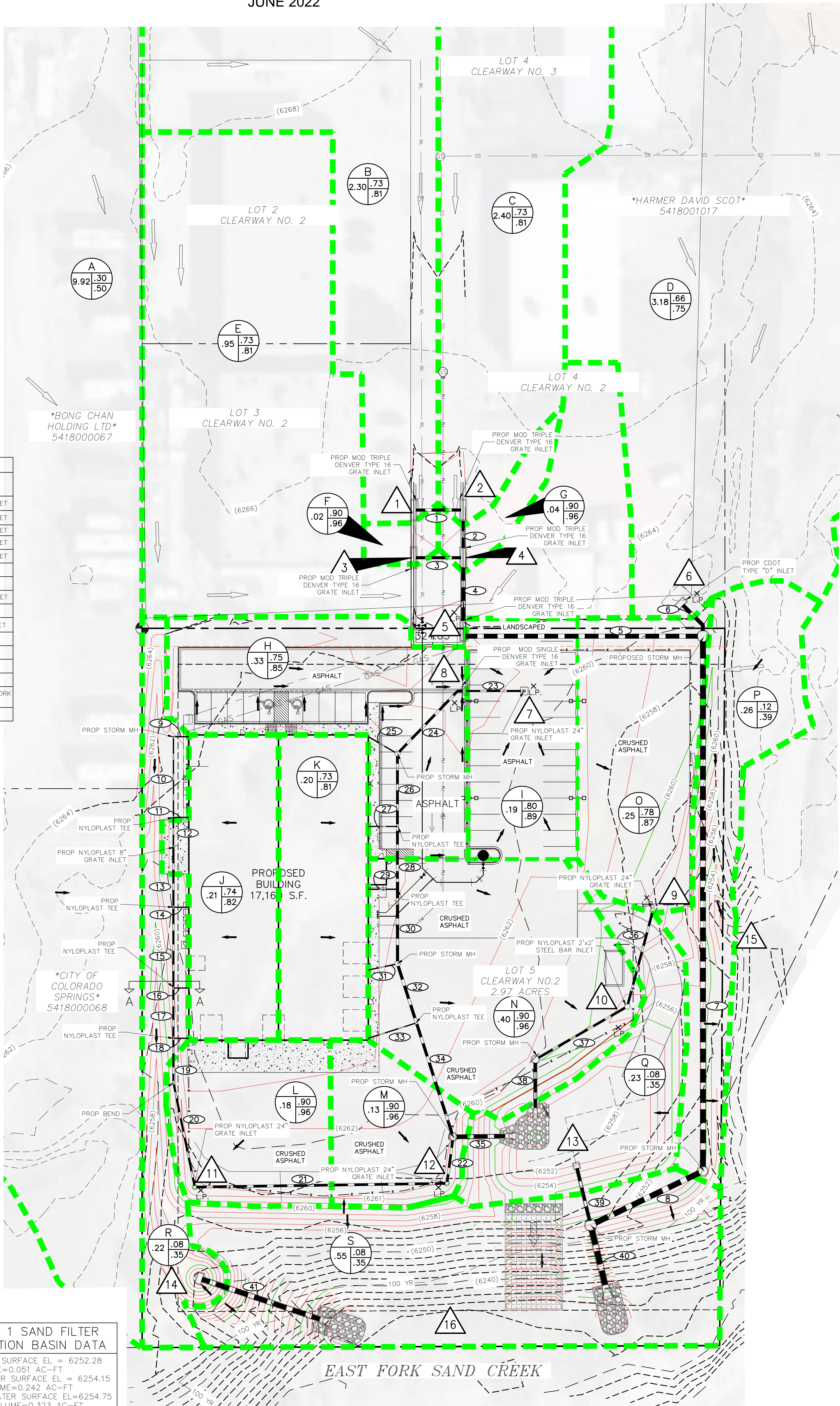
Scale in Feet

STORM SEWER SUMMARY				
PIPE RUN	Q <sub>5</sub>	Q <sub>100</sub>	PIPE SIZE	CONTRIBUTING PIPES/DESIGN POINTS
1	4.2	6.6	18" PP	DP1
2	5.9	9.7	24" PP	PR1, DP2
3	2.1	4.1	15" PP	DP3
4	9.1	16.4	24" PP	PR2, PR3, DP4
5	12.7	30.5	30" PP	PR4, DP5
6	7.5	14.4	24" PP	DP6
7	18.8	41.4	36" PP	PR5, PR6
8	18.8	41.4	36" PP	PR7
9	0.1	0.2	6" PP	.02 ACRE BASIN J
10	0.1	0.2	6" PP	PR9
11	0.2	0.4	6" PP	.06 ACRE BASIN J
12	0.3	0.6	8" PP	PR10, PR11
13	0.5	1.0	12" PP	PR12, .06 ACRE BASIN J
14	0.0	0.1	6" PP	.01 ACRE BASIN J
15	0.6	1.1	12" PP	PR13, PR14
16	0.1	0.3	6" PP	.04 ACRE BASIN J
17	0.7	1.3	12" PP	PR15, PR16
18	0.1	0.1	6" PP	.02 ACRE BASIN J
19	0.8	1.5	12" PP	PR17, PR18
20	0.8	1.5	12" PP	PR19
21	1.6	3.0	15" PP	PR20, DP11
22	2.3	4.1	15" PP	PR21, DP12
23	0.8	1.5	12" PP	DP7
24	2.0	3.8	15" PP	PR23, DP8
25	0.1	0.2	6" PP	.03 ACRE BASIN K
26	2.2	4.1	15" PP	PR24, PR25
27	0.2	0.3	6" PP	.05 ACRE BASIN K
28	2.3	4.4	15" PP	PR26, PR27
29	0.2	0.3	6" PP	.05 ACRE BASIN K
30	2.5	4.7	18" PP	PR28, PR29
31	0.2	0.3	6" PP	.05 ACRE BASIN K
32	2.7	5.1	18" PP	PR30, PR31
33	0.1	0.2	6" PP	.02 ACRE BASIN K
34	2.8	5.2	18" PP	PR32, PR33
35	5.0	9.3	24" RCP	PR22, PR34
36	1.0	1.9	12" PP	DP9
37	2.8	5.2	18" PP	PR36, DP10
38	2.8	5.2	18" RCP	PR37
39	0.3	0.3	18" RCP	FSD POND RELEASE
40	19.1	41.7	36" RCP	PR8, PR39
41	9.4	27.5	30" RCP	DP14

POND 1 SAND FILTER DETENTION BASIN DATA	
WQ WATER SURFACE EL =	6252.28
WQ VOLUME=	0.051 AC-FT
EURV WATER SURFACE EL =	6254.15
EURV VOLUME=	0.242 AC-FT
100-YR WATER SURFACE EL=	6254.75
100-YR VOLUME=	0.323 AC-FT
SPILLWAY CREST EL=	6254.76
TOP OF EMBANKMENT EL=	6256.00
RATIONAL 100-YR INFLOW=	12.8 CFS
MHFD 100-YR INFLOW =	7.8 CFS
MHFD 100-YR RELEASE =	0.2 CFS

NOTES

1. REFER TO EXISTING DRAINAGE MAP FOR BASINS A, B, C, AND D.



VIRGIL A. SANCHEZ, COLORADO P.E. NO. 37160

FOR AND ON  
BEHALF OF  
M&S CIVIL  
CONSULTANTS,  
INC.



212 N. WAHSATCH AVE, STE 305  
COLORADO SPRINGS, CO 80903  
PHONE: 719.955.5485

CLEARWAY NO. 2, LOT 5  
PROPOSED DRAINAGE MAP

PROJECT NO. 44-042  
DESIGNED BY: DLM  
DRAWN BY: TAU  
CHECKED BY: VAS

SCALE:  
HORIZONTAL:  
1"=30'  
VERTICAL:  
N/A

DATE: 06/02/2022

SHEET 1 OF 1

PDM