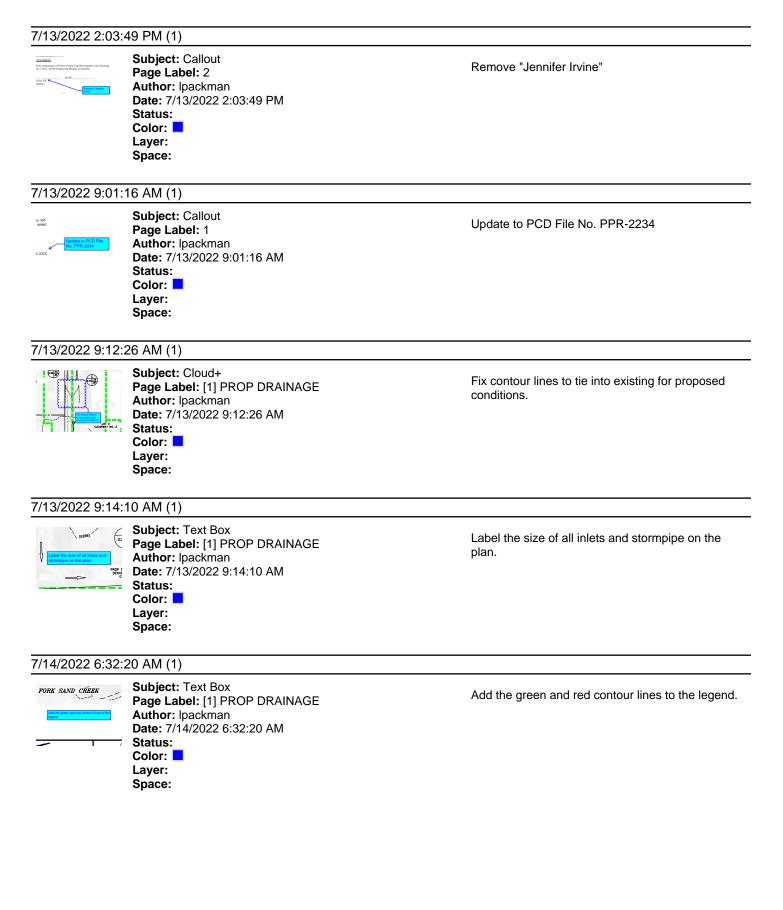
Drainage Report Final_V1.pdf Markup Summary



7/18/2022 1:01:39 PM (1)



Subject: Callout Page Label: [1] EXIST DRAINAGE Author: Daniel Torres Date: 7/18/2022 1:01:39 PM Status: Color: Layer:

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Space:



Subject: Highlight Page Label: [1] EXIST DRAINAGE Author: Daniel Torres Date: 7/18/2022 1:10:23 PM Status: Color: Layer: Space:

7/18/2022 1:10:43 PM (1)



Subject: Highlight Page Label: [1] PROP DRAINAGE Author: Daniel Torres Date: 7/18/2022 1:10:43 PM Status: Color: Layer: Space:

7/18/2022 1:10:50 PM (1)

CLEARWAY NO. 2, LOT PROPOSED DRAINAGE N NO. 44-582 SOLE: NORECORD.

Subject: Highlight Page Label: [1] PROP DRAINAGE Author: Daniel Torres Date: 7/18/2022 1:10:50 PM Status: Color: Layer: Space:

7/18/2022 1:11:53 PM (1)

stant vicks user (normal), the ast Fork Sub-Tributary at 2.97 identified above proximately 3.05 acres. The upged Drainage Map. Refer to Subject: Callout Page Label: 7 Author: Daniel Torres Date: 7/18/2022 1:11:53 PM Status: Color: Layer: Space:

7/18/2022 1:12:46 PM (1)



Subject: Highlight Page Label: 7 Author: Daniel Torres Date: 7/18/2022 1:12:46 PM Status: Color: Layer: Space: CLEARWAY NO.

2.97 identified above

The proposed development and improvements will be constructed on approximately 3.05 acres. The majority of the site has been accounted for as a storage yard and the remaining northern portion identified as Tract C being considered as

pastureland/undeveloped is shown on the Proposed Drainage Map.

?

7/18/2022 1:13:36 PM (1)



Subject: Callout Page Label: 7 Author: Daniel Torres Date: 7/18/2022 1:13:36 PM Status: Color: Layer: Space:

7/18/2022 1:17:08 PM (1)



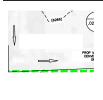
Subject: Callout Page Label: 8 Author: Daniel Torres Date: 7/18/2022 1:17:08 PM Status: Color: Layer: Space:

7/18/2022 1:21:21 PM (1)



Subject: Cloud+ Page Label: [1] PROP DRAINAGE Author: Daniel Torres Date: 7/18/2022 1:21:21 PM Status: Color: Layer: Space:

7/18/2022 1:30:51 PM (1)



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7/18/2022 1:32:08 PM (1)



Subject: Callout Page Label: [1] PROP DRAINAGE Author: Daniel Torres Date: 7/18/2022 1:32:08 PM Status: Color: Layer: Space:

7/18/2022 1:36:39 PM (1)



Subject: Callout Page Label: 8 Author: Daniel Torres Date: 7/18/2022 1:36:39 PM Status: Color: Layer: Space: please clarify/revise this statement. The majority of the site is a building and parking lot area.

does not match the drainage plan. Revise accordingly.

The site plan identifies this area as an asphalt parking lot. Revise your design accordingly.

the 100yr floodplain line type does not match the legend. Please revise

shouldn't this be DP3?

7/18/2022 1:47:00 PM (1)



Subject: Callout Page Label: 8 Author: Daniel Torres Date: 7/18/2022 1:47:00 PM Status: Color: Layer: Space:

7/18/2022 1:51:45 PM (1)



Subject: Callout Page Label: [1] EXIST DRAINAGE Author: Daniel Torres Date: 7/18/2022 1:51:45 PM Status: Color: Layer: Space:

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7/18/2022 10:10:35 AM (1)

d just indicate County gineer/ECM ministrator Subject: Text Box Page Label: 2 Author: Daniel Torres Date: 7/18/2022 10:10:35 AM Status: Color: Layer: Space:

7/18/2022 10:36:45 AM (1)



Subject: Callout Page Label: 4 Author: Daniel Torres Date: 7/18/2022 10:36:45 AM Status: Color: Layer: Space: please identify in the narrative how flow from Basin B is conveyed to the east on the southerly boundary of lot 3

south

does not appear to account for DP2 flow by. Revise.

and just indicate County Engineer/ECM Administrator

There is more than 1 acre of development proposed. Revise accordingly

7/18/2022 10:42:02 AM (1)



Subject: Image Page Label: 5 Author: Daniel Torres Date: 7/18/2022 10:42:02 AM Status: Color: Layer: Space:

7/18/2022 10:42:06 AM (1)



Subject: Callout Page Label: 5 Author: Daniel Torres Date: 7/18/2022 10:42:06 AM Status: Color: Layer: Space:

7/18/2022 10:43:28 AM (1)

inimize direct connectio rway Filing No. 2 site, off that is discharging to

Subject: Highlight Page Label: 5 Author: Daniel Torres Date: 7/18/2022 10:43:28 AM Status: Color: Color: Color: Space:

7/18/2022 10:43:38 AM (1)

LOCATION AND D arway Filing No. 2 is k the 6th P.M. in El Pas buildings approximate! Status: Color: Layer: Space:

7/18/2022 10:43:42 AM (1)

Subject: Highlight Page Label: 4 Author: Daniel Torres Date: 7/18/2022 10:43:42 AM Status: Color: Layer: Space:

7/18/2022 10:43:45 AM (1)

arwa<mark>y Filing No. 2.</mark> tterns and to ensure r that satisfies the Subject: Highlight Page Label: 4 Author: Daniel Torres Date: 7/18/2022 10:43:45 AM Status: Color: Color: Color: Color: Space:

7/18/2022 10:45:19 AM (1)

DRAINAGE CONDIT arway Filing No. 2 site Sand Creek. There are gineering Criteria Man Subject: Highlight Page Label: 6 Author: Daniel Torres Date: 7/18/2022 10:45:19 AM Status: Color: Layer: Space: tract A is not identified on the plat for lot 5. Tract A is part of the adjacent easterly subdivision. A floodplain area is identified on the plat. Revise the text accordingly.

Filing No. 2

y Filing No. 2

FILING NO. 2

y Filing No. 2.

y Filing No. 2

7/18/2022 10:51:37 AM (1)



Subject: Highlight Page Label: [1] EXIST DRAINAGE Author: Daniel Torres Date: 7/18/2022 10:51:37 AM Status: Color: Layer: Space:

7/18/2022 11:04:45 AM (1)



Subject: Callout Page Label: [1] EXIST DRAINAGE Author: Daniel Torres Date: 7/18/2022 11:04:45 AM Status: Color: Layer: Space:

7/18/2022 11:17:58 AM (1)

east and is captured by an existing ted east towards **DP 6**. This runof lative ranoff values are from the o tary upstram flows. The values p uence with sand Creek East Fork i west? **POSED DRAINAGE CHARAC** Subject: Callout Page Label: 7 Author: Daniel Torres Date: 7/18/2022 11:17:58 AM Status: Color: Layer: Space:

provide contour labels

west?

7/18/2022 2:11:06 PM (1)

Subject: Callout Page Label: 10 Author: Daniel Torres Date: 7/18/2022 2:11:06 PM Status: Color: Layer: Space:

7/18/2022 3:01:50 PM (1)

 A
 5.4
 10.7

 J
 0.4
 0.3

 or for private WOCV facility. A
 mainterance

 and the set submitting
 agreement has been provided. Please provided. Please provided. Please induct stars are proveded. sensitie in the Gauling and Erssion Council

= 1.8 cfs, Q 100 -

Subject: Callout Page Label: 12 Author: Daniel Torres Date: 7/18/2022 3:01:50 PM Status: Color: Layer: Space:

the site plan indicates this basin as a asphalt

parking lot. Revise accordingly.

maintenance agreement has been provided. Please revise

7/18/2022 3:02:02 PM (1)

vy the property owner. Access enance of the private WQCV fa eport on the next submittal. Subject: Highlight Page Label: 12 Author: Daniel Torres Date: 7/18/2022 3:02:02 PM Status: Color: Layer: Space:

on the next submittal

7/18/2022 3:04:38 PM (1)



Subject: Callout Page Label: 4 Author: Daniel Torres Date: 7/18/2022 3:04:38 PM Status: Color: Layer: Space:

7/18/2022 3:04:48 PM (1)

.GE REPORT ¹ AY <mark>FILING NO. 2</mark> Y, COLORADO	Subject: Highlight Page Label: 1 Author: Daniel Torres Date: 7/18/2022 3:04:48 PM Status: Color: Layer:
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Subject: Callout Page Label: 6 Author: Daniel Torres Date: 7/18/2022 3:26:18 PM Status: Color: Laver: Space:

7/18/2022 3:26:41 PM (1)

Subject: Callout Page Label: 7 Author: Daniel Torres Date: 7/18/2022 3:26:41 PM Status: Color: Layer: Space:

7/18/2022 3:36:56 PM (1)



Subject: Text Box Page Label: 5 Author: Daniel Torres Date: 7/18/2022 3:36:56 PM Status: Color: Layer: Space:

7/18/2022 3:37:56 PM (1)



Subject: Callout Page Label: 13 Author: Daniel Torres Date: 7/18/2022 3:37:56 PM Status: Color: Laver: Space:

Lot 5 does not appear to be part of the plat (10231) for filing 2 as that plat was for lot 4. Legal description indicates Lot5 Clearway. Please verify and revise accordingly.

FILING NO. 2

100% of the site shall be captured per ECM I.7.1.C.1. Basins R,S,and a disturbed portion of P are not being captured by the pond. Identify exclusions in Appendix I that may apply for these basins.

is there a channel/swale on the easterly boundary at DP3 that conveys DP3 flows to the south and then to the west? Please clarify in the narrative how DP3 flows are conveyed to DP6.

The sand creek DBPS identified improvements to Sand Creek channel. It appears that clearway subdivision may have completed channel related improvements. Please provide background/discussion on these improvements. I have provided the EDARP file number for clearway subdivision for your use (SF96017).

Please also identify that fees are not collected with site development plan applications.

7/18/2022 3:38:46 PM (1)

a fee amounts in 2022.	Subject: Highlight Page Label: 13
₹WA <mark>Y FILING NO. 2</mark> , LO	Author: Daniel Torres
y platted.	Date: 7/18/2022 3:38:46 PM
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7/18/2022 3:38:52 PM (1)

site construction docume verland emergency flow r arway Filing No. 2, Loi Date: Statu Color

Subject: Highlight Page Label: 13 Author: Daniel Torres Date: 7/18/2022 3:38:52 PM Status: Color: Layer: Space:

7/18/2022 3:54:01 PM (1)



Subject: Callout Page Label: 29 Author: Daniel Torres Date: 7/18/2022 3:54:01 PM Status: Color: Layer: Space:

7/18/2022 3:58:26 PM (1)

Subject: Cloud+ Page Label: 41 Author: Daniel Torres Date: 7/18/2022 3:58:26 PM Status: Color: Layer: Space:

7/18/2022 3:58:54 PM (1)



Subject: Callout Page Label: 8 Author: Daniel Torres Date: 7/18/2022 3:58:54 PM Status: Color: Layer: Space:

Y FILING NO. 2

y Filing No. 2

Does not appear to account for the bypass flows from DP2. Revise accordingly

Please see comments regarding the bypass flows that are conveyed to this inlet and revise accordingly.

Please include flow-by from DP2 that isn't captured by inlet 4 and update the design accordingly at DP5 as it does not appear to be accounted for.

7/18/2022 4:14:18 PM (1)



Subject: Callout Page Label: [1] PROP DRAINAGE Author: Daniel Torres Date: 7/18/2022 4:14:18 PM Status: Color: Layer: Space:

analyze and identify the protection needed at this proposed channel.

Additionally, an easement should be provided for the proposed channel. Please reflect this on the GEC and site plan.

7/18/2022 4:19:39 PM (1)



Subject: Callout Page Label: [1] PROP DRAINAGE Author: Daniel Torres Date: 7/18/2022 4:19:39 PM Status: Color:

Layer: Space:

7/18/2022 4:20:08 PM (1)



Subject: Callout Page Label: [1] PROP DRAINAGE Author: Daniel Torres Date: 7/18/2022 4:20:08 PM Status: Color: Layer: Space:

7/18/2022 4:23:24 PM (1)



Subject: Callout Page Label: [1] PROP DRAINAGE Author: Daniel Torres Date: 7/18/2022 4:23:24 PM Status: Color: Layer: Space:

7/18/2022 4:34:12 PM (1)

is to remain, and no improvements ha ce "Background" in the Appendix). An ov plain Map in the appendix, of which 0.2 losed Existing Dringage Map in the appe terns discussed below. ase provi eives runoff produced by Basin D (Q5 =

Subject: Callout Page Label: 6 Author: Daniel Torres Date: 7/18/2022 4:34:12 PM Status: Color: Layer: Space:

7/18/2022 4:47:19 PM (1)



Subject: Text Box Page Label: 4 Author: Daniel Torres Date: 7/18/2022 4:47:19 PM Status: Color: Layer: Space:

Please provide discussion/background on the File No. SF96017, VR97018, PPR02019.

7/19/2022 6:43:13 AM (1)



Subject: Callout Page Label: 38 Author: Daniel Torres Date: 7/19/2022 6:43:13 AM Status: Color: Laver: Space:

please tie the proposed contours with existing. typical throughout the plan

please label the proposed stilling basins with proposed specifications throughout the plans and provide design analysis

please provide

previous drainage studies for the site. See PCD

does not appear to match the plans. revise accordingly

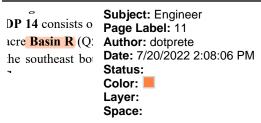
label the spillway and protection and provide design analysis of the spillway conveying the undetained rational flow and the protection down the embankment

7/20/2022 1:47:58 PM (1)

Design P DP16 control to the ease	Subject: Engineer Page Label: 11 Author: dotprete Date: 7/20/2022 1:47:58 PM Status: Color: Layer: Space:	DP16
7/20/2022 1:48:0	08 PM (1)	
basin in East Fork San DP15 Design Point 15 ((DP) DP16 consists of 0.26 to the cost houndary of	Subject: Engineer Page Label: 11 Author: dotprete Date: 7/20/2022 1:48:08 PM Status: Color: Layer: Space:	DP15
7/20/2022 1:48:2	25 PM (1)	
this basin flov y at DP16 .	Subject: Engineer Page Label: 11 Author: dotprete Date: 7/20/2022 1:48:25 PM Status: Color: Layer: Space:	DP16.
7/20/2022 2:05:	53 PM (1)	
= 0.1 cfs, Q100 = site Basin P (Q5 and then south t	Subject: Engineer Page Label: 11 Author: dotprete Date: 7/20/2022 2:05:53 PM Status: Color: Layer: Space:	Basin P
7/20/2022 2:07:0	02 PM (1)	
28.8 cfs, Q100 site Basin S (Q 1.6 cfs), PR40 ((Subject: Engineer Page Label: 11 Author: dotprete Date: 7/20/2022 2:07:02 PM Status: Color: Layer: Space:	Basin S
7/20/2022 2:08:0	01 PM (1)	
	Subject: Engineer Page Label: 11 Author: dotorete	Explain in the narrative how WQ is being addressed for these basins. Possible exclusions

Page Label: 11 Author: dotprete Date: 7/20/2022 2:08:01 PM Status: Color: ■ Layer: Space: Explain in the narrative how WQ is being addressed for these basins. Possible exclusions include I.7.1.B.7 (land disturbance to undeveloped land that will remain undeveloped) and/or I.7.1.C.1 (which allows for 20% not to exceed 1 acre of the applicable development site area to not be captured).

7/20/2022 2:08:06 PM (1)



7/20/2022 2:12:23 PM (1)



Subject: Engineer Page Label: [1] PROP DRAINAGE Author: dotprete Date: 7/20/2022 2:12:23 PM Status: Color: ■ Layer: Space:

7/20/2022 2:13:23 PM (1)



Subject: Engineer Page Label: 10 Author: dotprete Date: 7/20/2022 2:13:23 PM Status: Color: Layer: Space:

7/20/2022 2:13:49 PM (1)

See comment on Proposed barraye Map. 18" PP Fips Ba 34 (05 – 2.8 cfs, Q100 – of PEM. 100 – 1.9 fs). Developed runoff from this said of the parking for at the work boundary to extractional theory shall then true! Subject: Engineer Page Label: 10 Author: dotprete Date: 7/20/2022 2:13:49 PM Status: Color: ■ Layer: Space:

7/20/2022 3:45:48 PM (1)



Subject: Engineer Page Label: 38 Author: dotprete Date: 7/20/2022 3:45:48 PM Status: Color: ■ Layer: Space: Basin R

Proposed grades for Basin O do not seem to divert all stormwater to DP-9. Adjust contours so that all SW will drain to DP-9 for WQ treatment

is conveyed as sheet flow to a low point of the parking lot at the south boundary of the basin,

See comment on Proposed Drainage Map

this will cause clogging maintenance issues, consider adjusting restrictor plate height

FINAL DRAINAGE REPORT FOR LOT 5 OF CLEARWAY FILING NO. 2

EL PASO COUNTY, COLORADO

JUNE 2022

Prepared for: WIRENUT HOME SERVICES 6395 E Platte Ave. Colorado Springs, CO 80915 (719)-227-0500

Prepared by:



212 N. Wahsatch, Suite 305 Colorado Springs, CO 80903 (719) 955-5485

Project #44-042

Update to PCD File No. PPR-2234

PCD Project No. SF-XX-XXX

FINAL DRAINAGE REPORT FOR LOT 5 OF CLEARWAY FILING NO. 2

DRAINAGE PLAN STATEMENTS

ENGINEERS STATEMENT

The attached drainage plan and report was prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the County for drainage reports and said report is in conformity with the applicable master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omission on my part in preparing this report.

Virgil A. Sanchez, P.E. #37160 For and on Behalf of M&S Civil Consultants, Inc

DEVELOPER'S STATEMENT

I, the developer have read and will comply with all the requirements specified in this drainage report and plan.

BY:

TITLE:	
DATE:	

ADDRESS: Wirenut Home Services 6395 E. Platte Ave. Colorado Springs, CO 80915

EL PASO COUNTY'S STATEMENT

Filed in accordance with the requirements of El Paso County Land Development Code, Drainage Criteria Manual Volumes 1 and 2, and the Engineering Manual, as amended.

BY:	DATE:	
Jennifer Irvine, P.E. County Engineer		
<u>CONDITIONS:</u>	2	Remove "Jennifer Irvine"
		and just indicate County Engineer/ECM Administrator

FINAL DRAINAGE REPORT FOR LOT 5 OF CLEARWAY FILING NO. 2

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GENERAL LOCATION AND DESCRIPTION	4
SOILS	4
HYDROLOGIC CALCULATIONS	5
HYDRAULIC CALCULATIONS	5
FLOODPLAIN STATEMENT	5
DRAINAGE CRITERIA	5
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WATER QUALITY PROVISIONS AND MAINTENANCE	11
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APPENDIX

Vicinity Map Soils Map FIRM Panel Hydrologic Calculations Hydraulic Calculations / FSD Pond & WQCV Calculations Background Grading Erosion Control Plan Existing/Proposed Drainage Map Lot 5 does not appear to be part of the plat (10231) for filing 2 as that plat was for lot 4. Legal description indicates Lot5 Clearway. Please verify and revise accordingly.

FINAL DRAINAGE REPORT FOR LOT 5 OF CLEARWAY FILING NO. 2

This document is intended to serve as the Final Drainage Report for the Lot 5 of Clearway Filing No. 2. The purpose of this document is to identify and analyze the on and offsite drainage patterns and to ensure that post development runoff is routed through the site safely and in a manner that satisfies the requirements set forth by the El Paso County Drainage Criteria Manual. The development plan for Lot 5 will consist of asphalt parking lots, an office/warehouse building, asphalt storage, lighting, utility infrastructure, and landscaping. A Sand Filter Basin (Pond 1) is proposed to provide on-site water quality and detention. The parcel is zoned "CS CAD-O" and the proposed use is permissible within the There is more than 1 commercial zoning criteria.

GENERAL LOCATION AND DESCRIPTION

There is more than 1 acre of development proposed. Revise accordingly

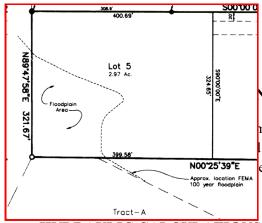
Lot 5 of Clearway Filing No. 2 is located in the north quarter of Section 18, Township 14 South, Range 65 West of the 6th P.M. in El Paso County, Colorado. The parcel is bound to the north by existing commercial buildings approximately 6 feet from the northern boundary, and the East Fork Sand Creek Sub-tributary to the south and to the east by Cherokee Metropolitan District property, and to the west by City of Colorado Springs property and northwest by The Wrangler Mobile Home Park. As shown on the enclosed FIRM panel, a channel known as the East Fork of Sand Creek Sub-tributary flows from north to south approximately 15 feet from the eastern boundary of the site. The site is located within the greater Sand Creek Drainage Basin and is tributary to the Sand Creek Channel via the East Fork Sand Creek Sub-Tributary. A vicinity map showing the location of the proposed development has been provided in the appendix of this report.

The proposed development and improvements will be constructed on approximately 1.00 acres of the 2.97-acre parcel. The site is currently zoned "CS CAD-O" which is associated with commercial development. In the existing condition, both the parcel and offsite contributing watershed lands are sparsely vegetated, with ground cover consisting primarily of native grasses ranging in density from moderate to good. The proposed development will consist of an asphalt parking area with an office/warehouse building, crushed asphalt storage area, lighting, landscaping, and an access road. Slopes across the development typically range between 2% to 7%. Offsite flows reaching development are contributed in part from areas of The Wrangler Mobile Home Park and the City of Colorado Springs property along the western boundary, from platted commercial property to the north and northeast. Flows produced within the development will be collected by proposed storm sewer improvements, swales, a riprap rundown, and will be routed to a proposed Sand Filter Basin (Pond 1) located at the southern boundary of the development.

SOILS

Please provide discussion/background on the previous drainage studies for the site. See PCD File No. SF96017, VR97018, **PPR02019.**

Soils for this project are delineated by the map in the appendix as Ellicott Loamy Coarse Sand (28) on the southeast corner of the property and Blakeland Loamy Sandy (8) throughout the majority of the property, both of which are characterized as Hydrologic Soil Types "A". Soils in the study area are shown as mapped by Soil Conservation Service in the "Soils Survey of El Paso County Area".



tract A is not identified on the plat for lot 5. Tract A is part of the adjacent easterly subdivision. A floodplain area is identified on the plat. Revise the text accordingly.

ned using the El Paso County and City of Colorado Springs Storm where applicable the Urban Storm Drainage Criteria Manual. The e stormwater runoff anticipated from design storms with 5-year and

HYDRAULIC CALCULATIONS

Hydraulic calculations were estimated using the Manning's Formula and the methods described in the El Paso County and City of Colorado Springs Storm Drainage Design Criteria manual. The relevant data sheets are included in the appendix of this report.

FLOODPLAIN STATEMENT

A portion of the site lies within the 100 year floodplain according to the Federal Emergency Management Agency (FEMA) Flood Insurance Rate Map (FIRM) Panel No. 08041C0543 F, effective date March 17, 1997 and the more recent FIRM Panel No. 08041C0754 G, effective date December 7, 2018. Base Flood Elevation (BFE) lines from FIRM Panel No. 08041C0754 G (NGVD29) are used for hydraulic calculations, drainage maps, and a discussion within this report. No development is anticipated to occur within the floodplain located at the northwest corner of the site. See Broposed Drainage Map and the FIRM Panels located in the appendix of this report for details. Tract A is provided on the plat for the portion of the lot encumbered by the floodplain. The Floodplain application and Floodplain permit are included in this report, in the Floodplain Map section in the appendix. No portions of the local floodplain located here within the 100 year flood zone. Additional work will be at the discretion of the local floodplain

administrator in accordance with FEMA policy.

DRAINAGE CRITERIA

This drainage analysis has been prepared in a Criteria Manual and where applicable the City effective January 2015. Hydrologic calculation

The sand creek DBPS identified improvements to Sand Creek channel. It appears that clearway subdivision may have completed channel related improvements. Please provide background/discussion on these improvements. I have provided the EDARP file number for clearway subdivision for your use (SF96017).

5-year and 100-year frequency storms for developed conditions using the Rational Method as required for basins having areas less than 130 acres (in accordance with Chapter 6 of the City of Colorado Springs DCM Volume 1). Full spectrum detention facilities have been designed in accordance with Section 3.2.1. of Chapter 13 of the City of Colorado Springs DCM Volume 1, dated May 2014, effective January 31, 2015 and Urban Drainage and Flood Control District Manuals dated January 2016.

FOUR STEP PROCESS

- Step 1: Employ Runoff Reduction Practices. Approximately 0.5 acres of the proposed, 2.97 acre development is being set aside for a Sand Filter Basin. Whenever possible, runoff produced within developed areas containing impervious surfaces will be routed through landscaped areas or earthen swales (grass-lined where slope exceeds 2%) to minimize direct connection of impervious surfaces.
- **Step 2: Stabilize drainage ways** –The Lot 5 at Clearway Filing No. 2 site, proposes a Full Spectrum Detention (FSD) Pond to control developed runoff that is discharging to the East Fork Sand Creek

Sub-Tributary located at southeastern boundary of the subject site. The FSD outlet structure has been designed to drain the water quality event storm in 40 hours, while reducing the 100 year peak discharge to approximately 90% of the predevelopment conditions. The development of this site is not anticipated to have negative effects on downstream drainageways. The existing channel embankment has been stabilized at the FSD pond's emergency spillway and where the outlet pipe from the pond enters the channel. The existing channel is to remain, and no improvements are necessary for this reach of the channel (See "Referenced Reports" in the Appendix).

- Step 3: Provide water quality capture volume. A Full Spectrum Detention Pond is proposed to reduce peak discharge rates and provide water quality treatment. The WQCV will be released over a 40 hour period while larger event storms will be released in periods of times between 64-80 hours.
- Step 4: Consider Need for Industrial and Commercial BMP's This submittal provides a final grading and erosion control plans with BMPs in place. The proposed project will use silt fence, inlet protection, straw bales, a vehicle tracking control pad, and concrete washout area, mulching and reseeding to mitigate the potential for erosion across the site. DL Holdings, LLC shall be responsible for existing and potentially necessary the BMPs for the site including staging, storage and stockpile areas as determined by the contractor. Individual lot owners will be responsible for ECM additional permanent BMPs if necessary because of site use of the site shall be captured per ECM

EXISTING DRAINAGE CONDITIONS

P are not being captured by the pond. Identify exclusions in Appendix I that may apply for these

Lot 5 of Clearway Filing No. 2 site consists of 2.97 acres situated north and west of the East Fork Subtributary of Sand Creek. There are no existing structures within the site. In accordance with El Paso County's Engineering Criteria Manual (ECM) and Drainage Criteria Manual's (DCM Vol. 1 & 2), an existing conditions hydrologic analysis was performed to determine existing flow quantities entering and exiting the subject site so a comparison to post development discharge rates could be made. As shown on the enclosed Existing Drainage Map (located in the appendix of this report) the existing site terrain within the parcel generally slopes from north to south at grades that vary between 2% to 15%. An existing 6-8" concrete retaining wall lies approximately 6-12 feet from the northern boundary of the site and protects a portion of the site from erosion effects from the offsite, commercial area runoff from the north. The East Fork Sand Creek Sub-Tributary continues from north to south approximately 10 feet from the eastern boundary of the site. It was observed that existing channel banks appear to be stable with established vegetation and minimal scour. The existing channel is to remain, and no improvements have been determined to be necessary for this reach of the channel (See "Background" in the Appendix). An overlay of the 100 yr floodplain (Zone AE) is shown on the Floodplain Map in the appendix, of which 0.28 acres overlaps the southeast corner of the site. Refer to the enclosed Existing Drainage Map in the appendix for visual representation of the detailed, existing drainage patterns discussed below.

Detailed Drainage Discussion

please provide

Design Point 1 ((DP1), Q5 = 7.3 cfs, Q100 = 14.0 cfs) receives runoff produced by **Basin D** (Q5 = 7.3 cfs, Q100 = 14.0 cfs), which consists of commercial, gravel and native grass covered platted land located along the northeast parcel property boundary. Runoff produced by **Basin D** is conveyed as sheet flow and earthen swale to the east towards **Design Point 1**. These flows will be routed via a retaining wall to **Design Point 2**.

is there a channel/swale on the easterly boundary at DP3 that conveys DP3 flows to the south and then to the west? Please

Design Point 2 ((**DP2**), Q5 = 22.5 cfs, Q100 = 42.3 cfs) receives runoff produced by **Basin B** (25 = 8.3 cfs, Q100 = 15.4 cfs) and **DP 1**. These basins consist of platted commercial lots and a 30 foot street for ingress/egress. Flows produced by **DP1** join with flows from **Basin C** and are conveyed by a retaining wall along the south border of **Basin C**. Runoff produced by **Basins B** and **Basin C** is conveyed as sheet flow towards **Design Point 2**. Runoff from **Design Point 2** continues southeast towards **Basin F**.

Design Point 3 ((**DP3**), Q5 = 22.8 cfs, Q100 = 44.6 cfs) receives runoff produced by **DP 2** and **Basin F** (Q5 = 0.3 cfs, Q100 = 2.5 cfs), which consists of native grass covered platted land located northeastern portion of the property. Runoff from these basins is conveyed as sheet flow to the southeast and is released on the southeast boundary of **Basin F** and routed southeast towards **Design Point 3**. This runoff outfalls into the East Fork Sand Creek Sub-Tributary.

Design Point 4 ((**DP4**), Q5 = 9.3 cfs, Q100 = 27.0 cfs) receives runoff produced by **Basin A** (Q5 = 9.3 cfs, Q100 = 27.0 cfs), which consist of developed gravel and un-developed native grass covered platted land located along the west portion of the property boundary. Runoff produced by **Basin A** is conveyed as sheet flow to the southeast towards **DP 4** on the west portion of the property boundary. Runoff from **DP 4** continues southeast towards **Basin E**.

Design Point 5 ((DP5), Q5 = 9.6 cfs, Q100 = 28.9 cfs) receives runoff produced by DP 4 and Basin E (Q5 = 0.3 cfs, Q100 = 2.3 cfs), which consists of native grass covered platted land located at the west portion of the property boundary. Runoff from DP 4 and Basin E is conveyed as sheet flow to the south and southwest and is captured by an existing swale on the western property boundary, then routed southeast towards DP 5. This runoff outfalls into the existing channel shared by Basin G, which drains southeast to the East Fork Sand Creek Sub-Tributary.

Design Point 6 ((**DP6**), Q5 = 31.0 cfs, Q100 = 72.3 cfs) receives runoff produced by **DP 3**, **DP 5** and **Basin G** (Q5 = 0.3 cfs, Q100 = 2.5 cfs), which consists of native grass covered platted land located at the southeast portion of the property. Runoff from **DP 3**, **DP 5** and **Basin G** is conveyed as sheet flow to the southeast and is captured by an existing channel along the southern portion of the property boundary, then is routed east towards **DP 6**. This runoff outfalls southeast to the East Fork Sand Creek Sub-Tributary. The cumulative runoff values are from the onsite flows and do not include the East Fork Sand Creek Sub-Tributary at confluence with Sand Creek East Fork is 1970 cfs for the 100 year event.

west?

PROPOSED DRAINAGE CHARACTERISTICS

2.97 identified above

The proposed development and improvements will be constructed on approximately 3.05 acres. The majority of the site has been accounted for as a storage yard and the remaining northern portion identified as Tract C being considered as pastureland/undeveloped is shown on the Proposed Drainage Map. Refer to the Proposed Drainage Map and hydraulic calculations un the Appendix for weighted runoff coefficients of the site. Proposed drainage patterns generally remain consistent with those in the existing condition with surface runoff traveling north to south. A swale is proposed on the western boundary of the site to capture and route offsite runoff south to the Sand Creek East Fork Subtributary. Storm sewer and inlets is proposed, on the north and eastern edge of the site, to capture and route offsite runoff south to the Sand Creek East Fork Subtributary. The onsite runoff, is conveyed via storm sewer and inlets to the proposed FSD pond. The runoff reaching the pond will be detained and discharged via a staged outlet structure and

please clarify/revise this statement. The majority of the site is a building and parking lot area.

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does not match the drainage – plan. Revise accordingly.

proposed 24° RCP storm system to the East Fork Sand Creek Sub-Tributary below historic rates. The outfall into the East Fork Sand Creek Sub-Tributary channel is armored with a proposed riprap pad and is grading away from main flows within the channel. Type M riprap protection is also proposed to stabilize the emergency spillway bank and all proposed grading around the outfall. Refer to the Proposed Drainage Map in the appendix for an illustration of the proposed site drainage patterns. All storm sewer, drainage structure and pond are private, and shall be maintained by owner. A detailed description of the proposed drainage characteristics follows:

Detailed Drainage Discussion

Design Point 1: ((DP1), Q5 = 6.8 cfs, Q100 = 12.7 cfs)

DP1 consists of 2.30 acres of offsite **Basin B** (Q5 = 6.8 cfs, Q100 = 12.7 cfs). Surface runoff from the existing neighboring Clearway Industrial Park (parking lot, gravel lot, building) within this basin generally flows from north to south as sheet flow and is routed via curb and gutter to a modified triple Denver Type 16 inlet with a mountable grate configuration (**INLET 1:** Q5 = 4.3 cfs, Q100 = 6.6 cfs). The intercepted flows are conveyed east through an 18" PP **Pipe Run 1** (Q5 = 4.3 cfs, Q100 = 6.6 cfs) until they combine with flows from **DP2**. Uncaptured runoff from this design point is conveyed as flow-by, **FB DP1** (Q5 = 2.5 cfs, Q100 = 6.1 cfs) towards **DP2**.

Design Point 2 ((DP2), Q5 = 7.1 cfs, Q100 = 13.2 cfs)

DP2 consists of 2.40 acres of offsite **Basin** C (Q5 = 7.1 cfs, Q100 = 13.2 cfs). Runoff from the existing neighboring Clearway Industrial Park (parking lot, gravel lot, building) within this basin travels as sheet flow north to south and is routed via curb and gutter a modified triple Denver Type 16 inlet with a mountable grate configuration (**INLET 2:** Q5 = 4.5 cfs, Q100 = 6.8 cfs) at **DP2**. The intercepted flow combines with flows from **PR1** and are conveyed south through 24" PP **Pipe Run 2** (Q5 = 5.9 cfs, Q100 = 9.7 cfs) to **DP4**. Uncaptured runoff from this design point is conveyed as flow-by, **FB DP2** (Q5 = 2.6 cfs, Q100 = 6.4 cfs towards **DP4**.

does not appear to - account for DP2 flow by. Revise.

Design Point 3 ((DP3), Q5 = 2.7 cfs, Q100 = 6.4/cfs)

DP3 consists of 0.02 acre, offsite **Basin F** (Q5 = 0.1 cfs, Q100 = 0.2 cfs) and **FB DP1** Runoff from the existing neighboring Clearway Industrial Park (parking lot, gravel lot) within offsite **Basin F** travels as sheet flow south and is routed via curb and gutter a modified triple Denver Type 16 inlet with a mountable grate configuration (**INLET 3**: Q5 = 2.2 cfs, Q100 = 4.1 cfs) at **DP3**. The intercepted flows are routed east through 15" **Pipe Run 3** (Q5 = 2.2 cfs, Q100 = 4.1 cfs) to **DP5**. Uncaptured runoff from this design point is conveyed east as flow-by, **FB DP3** (Q5 = 0.5 cfs, Q100 = 2.3 cfs) to **DP5**.

Design Point 4 ((DP4), Q5 = 1.2 cfs, Q100 = 3.4 cfs)

DP4 consists of 0.04 acre, offsite **Basin** G (Q5 = 0.2 cfs, Q100 = 0.4 cfs) and **FB DP2**. Runoff from the existing neighboring Clearway Industrial Park (parking lot, gravel lot, building) within this basin travels as sheet flow north to south and is routed via curb and gutter a modified triple Denver Type 16 inlet with a mountable grate configuration (**INLET 4**: Q5 = 1.0 cfs, Q100 = 2.6 cfs) at **DP4**. The intercepted flow combines with flow from **PR2** and **PR3** and is conveyed south through a 24" **Pipe Rnn 4** (Q5 = 9.1 cfs, Q100 = 16.4 cfs) to **DP5**. Uncaptured runoff from this design point is conveyed east as flow-by, **FB DP4** (Q5 = 0.2 cfs, Q100 = 0.8 cfs) towards **DP5**.

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Design Point 5 ((DP5), Q5 = 4.1 cfs, Q100 = 9.7 cfs)

Please include flow-by from DP2 that isn't captured by inlet 4 and update the design accordingly at DP5 as it does not appear to be accounted for. **DP5** consists of 0.95 acre, offsite **Basin E** (Q5 = 3.3 cfs, Q100 = 6.1 cfs), **FB DP3** and **FB DP4**. All runoff from the existing neighboring Clearway Industrial Park (parking lot, gravel lot, building) within this basin travels southeast as sheet flow and is routed via curb and gutter a modified triple sump Denver Type 16 inlet with a mountable grate configuration (**INLET 5:** Q5 = 4.1 cfs, Q100 = 9.7 cfs) at **DP5**. The intercepted flows combines with flow from **PR4** and is conveyed southeast through 30" PP **Pipe Run 5** (Q5 = 12.7 cfs, Q100 = 30.5 cfs) to **DP6**.

Design Point 6 ((DP6), Q5 = 7.5 cfs, Q100 = 14.4 cfs)

DP6 consists of 3.18 acre, offsite **Basin D** (Q5 = 7.5 cfs, Q100 = 14.4 cfs). All runoff from the existing neighboring Clearway Industrial Park (parking lot, gravel lot, building) within this basin travels south as sheet flow to a natural swale and is fully captured via proposed Type D sump inlet (INLET 6) (Q5 = 7.5 cfs, Q100 = 14.4 cfs) at the design point. These flows are conveyed south through 24" PP **Pipe Run 6** (Q5 = 7.5 cfs, Q100 = 14.4 cfs) and combine with flows from **PR5** at a manhole. The combined flows continue south through a 36" PP **Pipe Run 7 & Pipe Run 8** (Q5 = 18.8 cfs, Q100 = 41.4 cfs) to a manhole at the end of **PR8**.

Design Point 7 ((DP7), Q5 = 0.8 cfs, Q100 = 1.5 cfs)

DP7 consists of 0.19 acre, onsite **Basin I** (Q5 = 0.8 cfs, Q100 = 1.5 cfs). Developed runoff from this basin (parking lot) is conveyed as sheet flow to a low point of the parking lot where a Nyloplast 24" grate inlet (**INLET 7**) intercepts the flows and conveys them west through 12" PP **Pipe Run 23** (Q5 = 0.8 cfs, Q100 = 1.5 cfs). Intercepted runoff is routed to **DP8**.

Design Point 8 ((DP8), Q5 = 1.3 cfs, Q100 = 2.4 cfs)

DP8 consists of 0.33 acre, onsite **Basin H** (Q5 = 1.3 cfs, Q100 = 2.4 cfs). Developed runoff from this basin, parking lot, is fully conveyed as sheet flow to a low point of the parking lot, where a proposed modified single sump Denver Type 16 inlet shall be constructed. The flows entering the inlet will combine with flows from **PR23** and will be directed southwest through 15" PP **Pipe Run 24** (Q5 = 2.0 cfs, Q100 = 3.8 cfs), until the flows combine with roof drain flows from 0.20 acre **Basin K** (Q5 = 0.7 cfs, Q100 = 1.4 cfs).

See below for detailed discussion of proportioned flow approximations from 0.20 acre **Basin K** (Q5 = 0.7 cfs, Q100 = 1.4 cfs) and how they enter the storm system main between **Pipe Runs 24 to 34**.

Roof Drain Detailed Discussion: Basin K

The area of the eastern side of the commercial building roof (**Basin K**) was divided into sections and the area of the sections with respect to the area of **Basin K**, determined the portion of runoff to each roof drain. A 6" PP **Pipe Run 25** (Q5 = 0.1 cfs, Q100 = 0.2 cfs) conveys runoff from ~14.3% of the basin to the east, until these flows merge with flows from **PR24** and are conveyed through 15" PP **Pipe Run 26** (Q5 = 2.2 cfs, Q100 = 4.1 cfs) and flow south. A 6" PP **Pipe Run 27** (Q5 = 0.2 cfs, Q100 = 0.3 cfs) conveys runoff from 21.4% of **Basin K** to the east, until these flows merge with flows from **PR26** and are conveyed through 15" PP **Pipe Run 28** (Q5 = 2.3 cfs, Q100 = 4.4 cfs). A 6" PP **Pipe Run 29** (Q5 = 0.2 cfs, Q100 = 0.3 cfs) conveys runoff from 21.4% of **Basin K** to the east, until these flows merge with flows from **PR28** and are conveyed through 18" PP **Pipe Run 30** (Q5 = 2.5 cfs, Q100 = 4.7 cfs). A 6" PP **Pipe Run 31** (Q5 = 0.2 cfs, Q100 = 0.3 cfs) conveys runoff from 21.4% of **Basin K** to the east, until these flows merge with flows from **PR28** and are conveyed through 18" PP **Pipe Run 30** (Q5 = 2.5 cfs, Q100 = 4.7 cfs). A 6" PP **Pipe Run 31** (Q5 = 0.2 cfs, Q100 = 0.3 cfs) conveys runoff from 21.4% of **Basin K** to the east, until these flows merge with flows from **PR28** and are conveyed through 18" PP **Pipe Run 30** (Q5 = 2.5 cfs, Q100 = 4.7 cfs). A 6" PP **Pipe Run 31** (Q5 = 0.2 cfs, Q100 = 0.3 cfs) conveys runoff from 21.4% of **Basin K** to the east, until these flows merge with flows from **PR30** and are conveyed through 18" PP **Pipe Run 32** (Q5 = 2.7 cfs, Q100 = 5.1 cfs). A 6" PP **Pipe Run 33** (Q5 = 0.1 cfs, Q100 = 0.2 cfs) conveys runoff from 14.3% of **Basin K** to the east, until these

the site plan indicates this – basin as a asphalt parking lot. Revise accordingly.

See comment on Proposed Drainage Map

flows merge with flows from **PR32** and are conveyed through 18" PP **Pipe Run 34** (Q5 = 2.8 cfs, Q100 = 5.2 cfs). Flows from **PR34** are routed to a manhole at the end of **PR34**.

Design Point 9 ((**D**P9), Q5 = 1.0 cfs, Q100 = 1.9 cfs)

DP9 consists of 0.25 acre, onsite **Basin O** (Q5 = 1.0 cfs, Q100 = 1.9 cfs). Developed runoff from this basin, crushed asphalt lot, is conveyed as sheet flow to a low point of the parking lot at the south boundary of the basin, where a proposed Nyloplast 24" grate inlet shall be constructed. These flows shall then travel southwest through 12" PP **Pipe Run 36** (Q5 = 1.0 cfs, Q100 = 1.9 cfs) to **DP10**.

Design Point 10 ((DP10), Q5 = 1.8 cfs, Q100 = 3.3 cfs)

DP10 consists of 0.40 acre, onsite **Basin N** (Q5 = 1.8 cfs, Q100 = 3.3 cfs). Developed runoff from this basin, crushed asphalt lot, is fully conveyed as sheet flow to a low point of the parking lot at the east boundary of the basin, where a proposed Nyloplast 2'x2' steel bar inlet shall be constructed. These flows will combine with flows from **PR36** and travel southwest through 18" PP **Pipe Run 37 &** 18" RCP **Pipe Run 38** (Q5 = 2.8 cfs, Q100 = 5.2 cfs) to a low tailwater riprap basin in the Sand Filter Basin at **DP13**.

See below for detailed discussion of proportioned flow approximations from 0.21 acre **Basin J** (Q5 = 0.8 cfs, Q100 = 1.5 cfs) and how they enter the storm system main between **Pipe Runs 9 to 20**.

Roof Drain Detailed Discussion: Basin J

The area of the western side of the roof (**Basin J**) was divided into sections and the area of the sections with respect to the area of **Basin J**, determined the portion of runoff to each roof drain. A 6" PP **Pipe Run 9** (Q5 = 0.1 cfs, Q100 = 0.2 cfs) conveys runoff from 13.3% of the basin to the west, then the flows travel south via a 6" PP **PR10** (Q5 = 0.1 cfs, Q100 = 0.2 cfs), until they combine with flow from **PR11**. A 6" PP **Pipe Run 11** (Q5 = 0.2 cfs, Q100 = 0.4 cfs) conveys runoff from 26.7% of **Basin J** to the west, until these flows merge with flows from **PR10** and are conveyed south through a 8" PP **Pipe Run 12** (Q5 = 0.3 cfs, Q100 = 0.6 cfs). Approximately 10% of **Basin J** is paved in asphalt and an area drain fully conveys the flow from this portion south through a 8" PP **Pipe Run 13** (Q5 = 0.0 cfs, Q100 = 0.1 cfs) conveys runoff from 7.7%% of **Basin J** to the west, until these flows merge with flows from **PR13** and are conveyed through a 12" PP **Pipe Run 15** (Q5 = 0.6 cfs, Q100 = 1.1 cfs). A 6" PP **Pipe Run 16** (Q5 = 0.1 cfs, Q100 = 0.3 cfs) conveys runoff from 20% of **Basin J** to the west, until these flows merge with flows from **PR15** and are conveyed through a 12" PP **Pipe Run 17** (Q5 = 0.7 cfs, Q100 = 1.3 cfs). A 6" PP **Pipe Run 18** (Q5 = 0.1 cfs, Q100 = 0.3 cfs) conveys runoff from 20% of **Basin J** to the west, until these flows merge with flows from **PR15** and are conveyed through a 12" PP **Pipe Run 17** (Q5 = 0.7 cfs, Q100 = 1.3 cfs). A 6" PP **Pipe Run 18** (Q5 = 0.1 cfs, Q100 = 0.1 cfs) conveys runoff from 7.7% of **Basin J** to the west, until these flows merge with flows from **PR15** and are conveyed through a 12" PP **Pipe Run 17** (Q5 = 0.7 cfs, Q100 = 1.3 cfs). A 6" PP **Pipe Run 18** (Q5 = 0.1 cfs, Q100 = 0.1 cfs) conveys runoff from 7.7% of **Basin J** to the west, until these flows merge with flows from **PR15** and are conveyed through a 12" PP **Pipe Run 17** (Q5 = 0.7 cfs, Q100 = 1.3 cfs). A 6" PP **Pipe Run 18** (Q5 = 0.1 cfs, Q100 = 0.1 cfs) conveys runoff from 7.7% of **Basin J** to the west,

Design Point 11 ((DP11), Q5 = 0.9 cfs, Q100 = 1.5 cfs)

DP11 consists of 0.19 acre, onsite **Basin** L (Q5 = 0.9 cfs, Q100 = 1.5 cfs). Developed runoff from this basin, crushed asphalt lot, is conveyed as sheet flow to a low point of the parking lot at the southwest boundary of the basin, where a proposed Nyloplast 24" grate inlet shall be constructed. Flows conveyed by the inlet at **DP11**, will combine with flows from **Basin J** and be conveyed east through 15" PP **Pipe Run 21** (Q5 = 1.6 cfs, Q100 = 3.0 cfs) to **DP12**.

Design Point 12 ((DP12), Q5 = 0.6 cfs, Q100 = 1.1 cfs)

DP12 consists of 0.13 acre, onsite **Basin M** (Q5 = 0.6 cfs, Q100 = 1.1 cfs). Developed runoff from this basin, crushed asphalt lot, is fully conveyed as sheet flow to a low point of the parking lot at the southeast boundary of the basin, where a proposed Nyloplast 24" grate inlet shall be constructed. Flows conveyed by

Explain in the narrative how WQ is being addressed for these basins. Possible exclusions include I.7.1.B.7 (land disturbance to undeveloped land that will remain undeveloped) and/or I.7.1.C.1 (which allows for 20% not to exceed 1 acre of the applicable development site area to not be captured).

the inlet at DP12 will combine with flows from PR 21 and be conveyed northeast through a 15" PP Pipe **Run 22** (Q5 = 2.3 cfs, Q100 = 4.1 cfs). Flows from **PR22** combine with flows from **PR34** and are routed via a 24" RCP **Pipe Run 35** (O5 = 5.0 cfs, O100 = $9\sqrt{3}$ cfs/to a low tailwater riprap basin in the Sand Filter Basin at **DP13**.

Design Point 13 ((DP13), Q5 = 6.7 cfs, Q100 = 12.8 cfs)

DP13 consists of 0.23 acre, onsite **Basin** Q (Q5 = 0.1 kfs, Q100 = 0.6 cfs). Developed runoff from this basin is conveyed to an onsite sand filter basin Pond/1/ Pond 1 receives flows from PR35 (Q5 = 5.0 cfs, Q100 = 9.3 cfs), **PR38** (Q5 = 2.8 cfs, Q100 = 5.2 dfs), and **Basin Q** (Q5 = 0.1 cfs, Q100 = 0.6 cfs). Release rates from **Pond 1** are routed south via an /18/° RCP **Pipe Run 39** (Q5 = 0.3 cfs, Q100 = 0.3 cfs), where the flows combine with flows from **PR8** to a $\frac{3}{6}$ ° RCP **PR40** (Q5 = 19.1 cfs, Q100 = 41.7 cfs) to a low tailwater riprap basin in East Fork Sand Creek Subtributary at DP16. See Water Quality Provision for **Pond 1** information.

Design Point 14/((DP14), Q5 = 9.4 cfs, Q100 $\neq 27.5$ cfs)

DP 14 consists of 9.92 acre of offsite **Basin** A(Q5 = 9.3 cfs, Q100 = 27.0 cfs) and onsite undeveloped 0.22 acre **Basin** \mathbf{R} (Q5 = 0.1 cfs, Q100 = 0.5 cfs)/ Runoff from these basins is fully conveyed to a low point on the southeast boundary of **Basin R**. These/flows are captured by a proposed Type D sump inlet. These flows are conveyed via by a 30" RCP Pipe/Run/ 41 (Q5 = 9.4 cfs, Q100 = 27.5 cfs) to a low tailwater riprap basin in East Fork Sand Creek Subtributary at **DP16.**

Design Point 15 ((DP15), Q5 = 0.1 cfs, Q100 = 0.7 cfs) DP16 consists of 0.26 acre, onsite Basin P (Q5 = 0.1 cfs, Q100 = 0.7 cfs). The runoff from this basin flows to the east boundary of the site and then south toward the East Fork Sand Creek Subtributary at **DP16**.

Design Point 16 (DP16), (Q5 = 28.8 cfs, Q100 = 71.5 cfs)

DP16 consists of 0.55 acre, onsite **Basin S** (Q5 = 0.2 cfs, Q100 = 1.6 cfs). **DP16** receives flows from **Basin S** (Q5 = 0.2 cfs, Q100 = 1.6 cfs), **PR40** (Q5 = 19.1 cfs, Q100 = 41.7 cfs), **PR41** (Q5 = 9.4 cfs, Q100 = 27.5 cfs), and **DP15** (Q5 = 0.1 cfs, Q100 = 0.7 cfs). The cumulative flows at **DP16** (Q5 = 28.8 cfs, Q100 = 71.5 cfs) are less than the flows in the existing condition **EX DP6** (Q5 = 31.0 cfs, Q100 = 72.3 cfs). The site will not adversely affect adjacent or downstream properties.

WATER QUALITY PROVISIONS AND MAINTENANCE

A Sand Filter Detention Pond is being proposed for this site to address water quality from 2.11 acres at 85.2% imperviousness. The pond has been sized utilizing MHFD-Detention v4.05 and UD-BMP v3.07 from Urban Drainage and Flood Control District (UDFCD). The pond is not expected to carry future additional flows other than from this project. The pond is being constructed with an outlet control structure which limits the release rate of the pond through the use of weirs and an 18" RCP outlet pipe. The pond has been sized to store the WCQV, EURV, and the flood control volumes for the 2, 5, 10, 25, 50 and 100 year storm events. The WQCV will be slowly released over 12 hours. The maximum WQCV storage volume is 0.051 acre-feet. An overflow emergency spillway is proposed along the northwest embankment to safely convey flows to the existing East Fork Sand Creek Subtributary in the event of outlet clogging. The emergency overflow spillway will be at an elevation of 6254.76 feet and will have a length of 22.0 feet, and a spillway design flow depth of approx. 0.23 feet across the crest (passing 12.8 cfs) should the outlet become clogged. The top of the proposed embankment will need to be constructed at approximately 6256.0 to provide one foot of freeboard. See Proposed Drainage Map in the appendix of this report. The

WQCV Pond 1	WQCV	EURV	5 Year	100 Year
Maximum Volume Stored (acre-ft)	0.051	0.242	0.170	0.323
Maximum WS Elevation	6252.28	6254.15	6253.55	6254.75
Peak Inflow (cfs)	N/A	N/A	5.4	10.7
Peak Outflow (cfs)	0.1	0.3	0.3	0.3

following table provided below summarizes the peak inflows, outflows, storage volumes and water surface

elevations for the water quality, 5 year, EURV and 100 year event storms.

The proposed pond will be private and shall be maintained by the property owner. Access shall be granted to the owner and El Paso County for access and maintenance of the private WQCV facility. A private maintenance agreement document shall accompany this report on the next submittal.

EROSION CONTROL

maintenance agreement has been provided. Please

It is the policy of the El Paso County that we submit a grading and erosion control plan with the drainage report. Proposed silt fence, vehicle traffic control, and concrete washout area are proposed as erosion control measures. The costs for these measures have been provided on the Grading and Erosion Control plan.

CONSTRUCTION COST OPINION

Private Drainage Facilities (NON-Reimbursable):

Item	Description	Qua	ntity	Unit Co	ost	Cost
1.	6" PP	181	LF	\$25	/LF	\$4,525.00
2.	8" PP	17	LF	\$35	/LF	\$595.00
3.	12" PP	276	LF	\$45	/LF	\$12,420.00
4.	15" PP	312	LF	\$55	/LF	\$17,160.00
5.	18" PP	238	LF	\$68	/LF	\$16,184.00
6.	24" PP	65	LF	\$81	/LF	\$5,265.00
7.	30" PP	130	LF	\$125	/LF	\$16,250.00
8.	36" PP	357	LF	\$150	/LF	\$53,550.00
9.	18" RCP	55	LF	\$78	/LF	\$4,290.00
10.	24" RCP	27	LF	\$104	/LF	\$2,808.00
11.	30" RCP	70	LF	\$130	/LF	\$9,100.00
12.	36" RCP	32	LF	\$155	/LF	\$4,960.00
13.	18" FES RCP	1	EA	\$923	/EA	\$923.00
14.	24" FES RCP	1	EA	\$1046	/EA	\$1,046.00
15.	30" FES RCP	1	EA	\$1292	/EA	\$1292.00
16.	36" FES RCP	1	EA	\$1845	/EA	\$1845.00
17.	Triple Type 16 Inlet	5	EA	\$11,900	/EA	\$59,500.00
18.	Single Type 16 Inlet	1	EA	\$5900	/EA	\$5,900.00
19.	Type D Inlet	2	EA	\$4800	/EA	\$9,600.00

20.	24" Grate and Drain Basin	4	EA	\$2930	/EA		\$11,720.00
21.	2'x2' Steel Grate and Drain Basin	1	EA	\$2930	/EA		\$2,930.00
22.	Manhole	6	EA	\$6500	/EA		\$39,000.00
23.	Type M riprap, 2' deep Low Tailwater	60	CY	\$65	/CY		\$3,900.00
	FSD Pond (Inlcuding Outlet Struct, Spillway Cutoff Wall, Riprap, Signs, Sand Filter Media, Erosion Blanket)	1	LS	\$17,408	/LS		\$17,408.00
						Total \$	\$302,171.00
						5%	\$15,108.55
						Contingency	
						10%	\$30,217.10
						Engineering	
						Total\$	\$347,496.65

M & S Civil Consultants, Inc. (M & S) cannot and does not guarantee the construction cost will not vary from these opinions of probable costs. These opinions represent our best judgment as design professionals familiar with the construction industry and this development in particular. The above and below is only an estimate of the facility cost and drainage basin fee amounts in 2022.

DRAINAGE & BRIDGE FEES – CLEARWA	V FILINC NO 2 LOT 5
DRAMAGE & DRIDGE FEES - CLEARWA	

Fees not required as this Filing was previously platted.

Please also identify that fees are not collected with site development plan applications.

SUMMARY

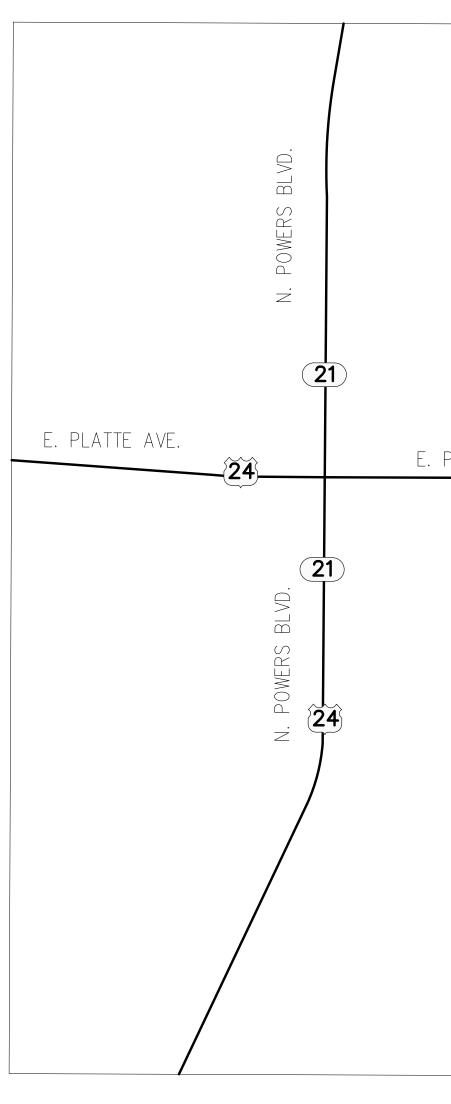
Per this final drainage report, the proposed drainage facilities recommended within this report will adequately convey, detain and route runoff from the planned development to the East Fork Sand Creek Sub-Tributary drainage way at peak flow rates which are below existing with no negative impacts on surrounding developments. All drainage facilities described herein and shown on the included Proposed Drainage Map (See Appendix), this final Drainage Report and site construction documents are submitted for simultaneous review. Care will be taken to accommodate overland emergency flow routes on site and temporary drainage conditions. The development of the Clearway Filing No. 2, Lot 5 site will not adversely affect adjacent or downstream properties.

REFERENCES

- 1.) "El Paso County and City of Colorado Springs Drainage Criteria Manuals".
- 2.) "Urban Storm Drainage Criteria Manual"
- 3.) SCS Soils Map for El Paso County.
- 4.) Flood Insurance Rate Map (FIRM), Federal Emergency Management Agency (Map No. 08041C0543F), Effective date March 17, 1997.
- 5.) Flood Insurance Rate Map (FIRM), Federal Emergency Management Agency (Map No. 08041C0754G), Effective date December 7, 2018.
- 7.) "Sand Creek Drainage Basin Planning Study, Preliminary Design Report", Revised March 1996, by Kiowa Engineering Corporation.

APPENDIX

VICINITY MAP



24 MARKSH 4EFFEL THAWA TER RD. 94 \bigcirc E. PLATTE AVE. 24-ACCESS HWY. 34 SPACE VILLAGE AVE. MAR IEFFEL SITE RD

VICINITY MAP N.T.S.

 REVISIONS	NIC.			VIRCH A SANC	ARCIL A SANCHEZ COLORADO D'E NO 37160	37160						
 NO. DV		BY: DESCRIPTION:	APRV'D. BY: DATE:					212 N. WAHSATCH AVE STE 305	CLEARW	AY FILING	CLEARWAY FILING NO. 2, LOT 5	Ŋ
				innester.	JALL.	FOR AND ON BEHALF OF		COLORADO SPRINGS, CO 80903 PHONE: 719.955.5485		VICINITY MAP	MAP	
				- All	37160 =	M&S UNIL CONSULTANTS,		<u>ı I</u>	PROJECT NO. 44-042	SCALE:	DATE: 05-20-2022	2
	ENGINEER PRE UTHORIZED CH ST BE IN WRITIN	THE ENGINEER PREPARING THESE PLANS WILL NOT BE RESPONSIBLE, OR LIABLE FOR, UNAUTHORIZED CHANGES TO OR USES OF THESE PLANS. ALL CHANGES TO THE PLANS MUST BE IN WRITING AND MUST BE APPROVED BY THE PREPARER OF THESE PLANS.	IBLE, OR LIABLE FOR, CHANGES TO THE PLAN ER OF THESE PLANS.		ESSIDNAL ENGINE	.) N	CIVIL CONSULTANTS, INC.		DESIGNED BY: TAU DRAWN BY: TAU CHECKED BY: VAS	HORIZONTAL: N/A VERTICAL: N/A	SHEET 1 OF 1	VIC01

SOILS MAP



Map unit symbol	Map unit name	Rating
8	Blakeland loamy sand, 1 to 9 percent slopes	A
28	Ellicott loamy coarse sand, 0 to 5 percent slopes	A
111	Water	

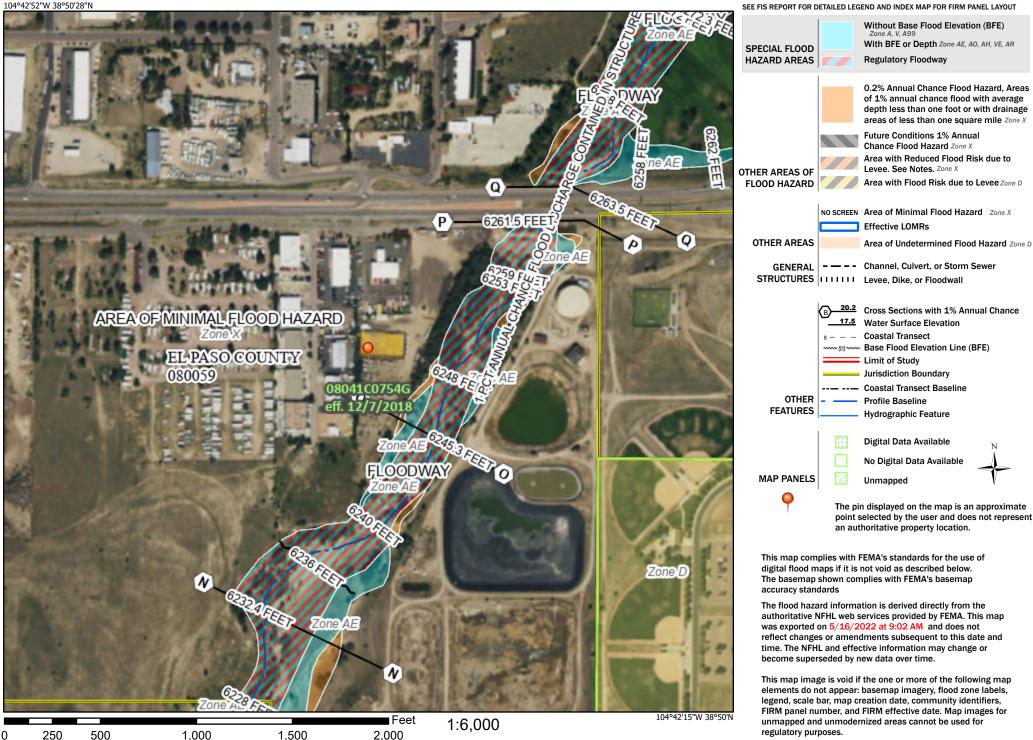


FIRM PANEL

National Flood Hazard Layer FIRMette



Legend



Basemap: USGS National Map: Orthoimagery: Data refreshed October, 2020

HYDROLOGIC CALCULATIONS

CLEARWAY NO.2, LOT 5 (WIRENUT) EXISTING CONDITIONS DRAINAGE CALCULATIONS (Area Runoff Coefficient Summary)

			STRE	ETS/DEVEI	LOPED	DE	VELOPED L	OTS	UNDEVI	ELOPED/LA	NDSCAPE	RUNOFF COEFFICIENT		
BASIN	TOTAL AREA (SF)	TOTAL AREA (Acres)	AREA (Acres)	C ₅	C ₁₀₀	AREA (Acres)	C ₅	C ₁₀₀	AREA (Acres)	C ₅	C ₁₀₀	C ₅	C ₁₀₀	
A	431946.186	9.92	0.00	0.90	0.96	9.13	0.30	0.50	0.78	0.08	0.35	0.28	0.49	
В	133523.312	3.07	0.00	0.90	0.96	3.07	0.73	0.81	0.00	0.08	0.35	0.73	0.81	
С	119110.0794	2.73	0.00	0.90	0.96	2.73	0.73	0.81	0.00	0.08	0.35	0.73	0.81	
D	134064.3175	3.08	1.44	0.73	0.81	1.63	0.59	0.70	0.00	0.08	0.35	0.66	0.75	
Ε	42111.756	0.97	0.00	0.90	0.96	0.00	0.08	0.35	0.97	0.08	0.35	0.08	0.35	
F	46802.057	1.07	0.00	0.90	0.96	0.00	0.08	0.35	1.07	0.08	0.35	0.08	0.35	
G	47704.938	1.10	0.00	0.90	0.96	0.00	0.08	0.35	1.10	0.08	0.35	0.08	0.35	

CLEARWAY NO.2, LOT 5 (WIRENUT) EXISTING CONDITIONS DRAINAGE CALCULATIONS (Area Drainage Summary)

From Area I	Runoff Coefficient Sum		S7	REET / CH	ANNEL FLO	DW	Time of T	ravel (T _t)	INTENSITY *		TOTAL FLOWS						
BASIN	AREA TOTAL	C ₅	C ₁₀₀	C ₅	Length	Height	T _C	Length	Slope	Velocity	T _t	TOTAL	СНЕСК	I ₅	I ₁₀₀	Q5	Q ₁₀₀
	(Acres)	From DC.	M Table 5-1		(ft)	(ft)	(min)	(ft)	(%)	(fps)	(min)	(min)	(min)	(in/hr)	(in/hr)	(c.f.s.)	(c.f.s.)
A	9.92	0.28	0.49	0.28	100	2	11.7	1174	0.5%	0.7	27.4	39.1	17.1	3.3	5.6	9.3	27.0
В	3.07	0.73	0.81	0.73	100	2	5.3	775	1.3%	2.3	5.7	11.0	14.9	4.0	6.7	8.9	16.6
С	2.73	0.73	0.81	0.73	100	2	5.3	675	1.5%	2.4	4.6	9.9	14.3	4.1	6.9	8.3	15.4
D	3.08	0.66	0.75	0.66	100	2	6.4	673	1.9%	1.4	8.1	14.5	14.3	3.6	6.0	7.3	14.0
Ε	0.97	0.08	0.35	0.08	50	2	8.2	298	8.4%	2.0	2.4	10.7	11.9	4.0	6.8	0.3	2.3
F	1.07	0.08	0.35	0.08	100	2	14.7	138	6.5%	1.8	1.3	15.9	11.3	3.9	6.6	0.3	2.5
G	1.10	0.08	0.35	0.08	100	1	18.4	169	14.8%	2.7	1.0	19.5	11.5	3.9	6.6	0.3	2.5

* Intensity equations assume a minimum travel time of 5 minutes.

Calculated by: TAU Date: 3/31/2022 Checked by: VAS

			EXI	IST		CON	NDI T		S DR	AIN	AGI	TRENUT) E CALCUI ury)		ION.	5		
		OVERLAND				PIPE / CHANNEL FLOW				Time of Travel (T ₁)	INTENSITY *		TOTAL FLOWS				
DESIGN POINT	CONTRIBUTING BASINS	CA ₅	CA ₁₀₀	C ₅	Length (ft)	Height (ft)	T _C (min)	Length (ft)	Slope (%)	Velocity (fps)	T _t (min)	TOTAL (min)	I ₅ (in/hr)	I ₁₀₀ (in/hr)	Q ₅ (c.f.s.)	Q ₁₀₀ (c.f.s.)	COMMENTS
1	D	2.02	2.31			BASIN Tc				<i></i>		14.3	3.6	6.0	7.3	14.0	conveyed by sheet flow and swale
2	DP1, B, C	6.25	7.01			DASILV TC						14.3	3.6	6.0	22.5	42.3	conveyed by private street c&g
3	DP2, F	6.34	7.39			e DP2 Tc						14.3	3.6	6.0	22.8	44.6	conveyed by swale to East Fork Sand Creek
4	Α	2.80	4.84			BASIN Tc						17.1	3.3	5.6	9.3	27.0	conveyed to Lot 5
5	DP4, E	2.88	5.18		use	e DP4 Tc						17.1	3.3	5.6	9.6	28.9	conveyed to East Fork Sand Creek
6	G, DP3, DP5	9.30	12.95		use	e DP5 Tc						17.1	3.3	5.6	31.0	72.3	conveyed to East Fork Sand Creek

	Weighted Percent I	mperviousness	of WQ Pond 1	
Contributing Basins	Area (Acres)	C 5	Impervious % (I)	(Acres)*(I)
Column1	Column2	Column3	Column4	Column5
Н	0.33	0.75	91	29.71
I	0.19	0.80	94	17.73
J	0.21	0.74	91	18.70
K	0.20	0.73	90	17.56
L	0.18	0.90	100	18.43
М	0.13	0.90	100	13.32
N	0.40	0.90	100	39.72
0	0.25	0.78	93	22.90
Q	0.23	0.08	7	1.63
Totals	2.11			179.70
Imperviousness of WQ Pond 1	85.2			

CLEARWAY NO.2, LOT 5 PROPOSED CONDITIONS DRAINAGE CALCULATIONS (Area Runoff Coefficient Summary)

			STRE	ETS/DEVEI	LOPED	DE	VELOPED L	OTS	UNDEVE	LOPED/LA	NDSCAPE	RUNOFF C	OEFFICIENT
BASIN	TOTAL AREA (SF)	TOTAL AREA (Acres)	AREA (Acres)	C ₅	C ₁₀₀	AREA (Acres)	C ₅	C ₁₀₀	AREA (Acres)	C ₅	C ₁₀₀	C ₅	C ₁₀₀
A	431957.157	9.92	0.00	0.90	0.96	9.13	0.30	0.50	0.78	0.08	0.35	0.28	0.49
В	100360.697	2.30	0.00	0.90	0.96	2.30	0.73	0.81	0.00	0.08	0.35	0.73	0.81
С	104496.823	2.40	0.00	0.90	0.96	2.40	0.73	0.81	0.00	0.08	0.35	0.73	0.81
D	138334.367	3.18	1.54	0.73	0.81	1.63	0.59	0.70	0.00	0.08	0.35	0.66	0.75
Ε	41339.688	0.95	0.00	0.90	0.96	0.95	0.73	0.81	0.00	0.08	0.35	0.73	0.81
F	985.639	0.02	0.02	0.90	0.96	0.00	0.73	0.81	0.00	0.08	0.35	0.90	0.96
G	1858.029	0.04	0.04	0.90	0.96	0.00	0.73	0.81	0.00	0.08	0.35	0.90	0.96
H	14220.85	0.33	0.27	0.90	0.96	0.00	0.73	0.81	0.06	0.08	0.35	0.75	0.85
Ι	8213.984	0.19	0.17	0.90	0.96	0.00	0.73	0.81	0.02	0.08	0.35	0.80	0.89
J	8949.66	0.21	0.01	0.90	0.96	0.20	0.73	0.81	0.00	0.08	0.35	0.74	0.82
K	8500	0.20	0.00	0.90	0.96	0.20	0.73	0.81	0.00	0.08	0.35	0.73	0.81
L	8030.038	0.18	0.18	0.90	0.96	0.00	0.73	0.81	0.00	0.08	0.35	0.90	0.96
М	5803.105	0.13	0.13	0.90	0.96	0.00	0.73	0.81	0.00	0.08	0.35	0.90	0.96
N	17303.404	0.40	0.40	0.90	0.96	0.00	0.73	0.81	0.00	0.08	0.35	0.90	0.96
0	10726.014	0.25	0.21	0.90	0.96	0.00	0.73	0.81	0.03	0.08	0.35	0.78	0.87
Р	11364.603	0.26	0.00	0.90	0.96	0.00	0.12	0.39	0.26	0.12	0.39	0.12	0.39
Q	10112.778	0.23	0.00	0.90	0.96	0.00	0.12	0.39	0.23	0.08	0.35	0.08	0.35
R	9732.156	0.22	0.00	0.90	0.96	0.00	0.08	0.35	0.22	0.08	0.35	0.08	0.35
S	23948.368	0.55	0.00	0.90	0.96	0.00	0.08	0.35	0.55	0.08	0.35	0.08	0.35

CLEARWAY NO.2, LOT 5 PROPOSED CONDITIONS DRAINAGE CALCULATIONS (Area Drainage Summary)

From Area Runoff	Coefficient Sumn	nary			OVERLA	1ND		ST	REET / CH	ANNEL FLO)W	Time of T	ravel (T _t)	INTEN	SITY *	TOTAL	FLOWS
BASIN	AREA TOTAL	C ₅	C ₁₀₀	C ₅	Length	Height	T _C	Length	Slope	Velocity	T _t	TOTAL	CHECK	I ₅	I ₁₀₀	Q5	Q ₁₀₀
	(Acres)	From DCM	A Table 5-1		(ft)	(ft)	(min)	(ft)	(%)	(fps)	(min)	(min)	(min)	(in/hr)	(in/hr)	(c.f.s.)	(c.f.s.)
A	9.92	0.28	0.49	0.28	100	2	11.7	1174	0.5%	0.7	27.4	39.1	17.1	3.3	5.6	9.3	27.0
В	2.30	0.73	0.81	0.73	100	2	5.3	674	1.2%	2.2	5.2	10.5	14.3	4.1	6.8	6.8	12.7
С	2.40	0.73	0.81	0.73	100	2	5.3	735	1.4%	2.3	5.3	10.6	14.6	4.0	6.8	7.1	13.2
D	3.18	0.66	0.75	0.66	100	2	6.3	685	1.9%	1.4	8.3	14.6	14.4	3.6	6.0	7.5	14.4
E	0.95	0.73	0.81	0.73	50	1	3.8	390	1.3%	2.3	2.9	6.6	12.4	4.7	8.0	3.3	6.1
F	0.02	0.90	0.96	0.90	25	1	1.1	17	1.5%	2.4	0.1	5.0	10.2	5.2	8.7	0.1	0.2
G	0.04	0.90	0.96	0.90	25	1	1.1	90	1.7%	2.6	0.6	5.0	10.6	5.2	8.7	0.2	0.4
Н	0.33	0.75	0.85	0.75	50	1	3.6	127	0.8%	1.8	1.2	5.0	11.0	5.2	8.7	1.3	2.4
Ι	0.19	0.80	0.89	0.80	50	1	3.0	51	2.0%	2.8	0.3	5.0	10.6	5.2	8.7	0.8	1.5
J	0.21	0.74	0.82	0.74	50	1	3.7	86	1.2%	2.2	0.7	5.0	10.8	5.2	8.7	0.8	1.5
K	0.20	0.73	0.81	0.73	50	1	3.8	86	1.2%	2.2	0.7	5.0	10.8	5.2	8.7	0.7	1.4
L	0.18	0.90	0.96	0.90	50	1	2.0	64	2.0%	2.8	0.4	5.0	10.6	5.2	8.7	0.9	1.5
М	0.13	0.90	0.96	0.90	50	1	2.0	62	2.0%	2.8	0.4	5.0	10.6	5.2	8.7	0.6	1.1
N	0.40	0.90	0.96	0.90	50	1	2.0	123	2.4%	3.1	0.7	5.0	11.0	5.2	8.7	1.8	3.3
0	0.25	0.78	0.87	0.78	50	1	3.2	130	1.5%	2.4	0.9	5.0	11.0	5.2	8.7	1.0	1.9
Р	0.26	0.12	0.39	0.12	50	2	7.9	159	5.0%	1.6	1.7	9.6	11.2	4.2	7.0	0.1	0.7
Q	0.23	0.08	0.35	0.08	50	4	6.6	140	2.9%	1.2	2.0	8.5	11.1	4.4	7.3	0.1	0.6
R	0.22	0.08	0.35	0.08	25	2	4.6	356	2.8%	1.2	5.1	9.7	12.1	4.2	7.0	0.1	0.5
S	0.55	0.08	0.35	0.08	50	8	5.2	115	15.7%	2.8	0.7	5.9	10.9	4.9	8.3	0.2	1.6

* Intensity equations assume a minimum travel time of 5 minutes.

Calculated by: <u>TAU</u> Date: <u>4/4/2022</u> Checked by: VAS

		j	PRO	P <i>O</i> ,	SED	CON	NDIT	ARWA IONS n Roi	S D K	AIN.	4 <i>G</i> 1	E CALCUL	ATI	ON.	S acc byp DP	count bass f 2. Re	
								-					8		-	cordin	igly
	From Area Runoff Coefficient Summary		L = :	-		ERLAND				NNEL FLO		Time of Travel (T_t)	INTEN	r	TOTAL	1	
DESIGN POINT	CONTRIBUTING BASINS	CA ₅	CA ₁₀₀	C ₅	Length (ft)	Height (ft)	T _C (min)	Length (ft)	Slope (%)	Velocity (fps)	T _t (min)	TOTAL (min)	I ₅ (in/hr)	I ₁₀₀ (in/hr)	Q ₅ (c.f.s.)	Q ₁₀₀ (c.f.s.)	COMMENTS
1	В	1.68	1.87			B Tc Used						10.5	4.1	6.8	6.8		Mel Triple Denver Type 16 Grate Inlet
2	С	1.75	1.94		Dusin							10.6	4.0	6.8	7.1	13.2	Nod Triple Denver Type 16 Grate Inlet
					Basin	C Tc Used											
3	FB1, F	0.67	0.93		Desir	B Tc Used						10.5	4.1	6.8	2.7	6.4	Mod Triple Denver Type 16 Grate Inlet
4	FB2, G	0.29	0.50									10.6	4.0	6.8	1.2	3.4	Mod Triple Denver Type 16 Grate Inlet
5	ED2 ED4 E	0.86	1.22		Basin	C Tc Used						6.6	47	80	4.1	9.4	Mod Triple Denver Type 16 Grate Inlet
5	FB3, FB4, E	0.86	1.22		Basin	E Tc Used		-				6.6	4.7	8.0	4.1	9.7	Mod Triple Denver Type 16 Grate Inlet
6	D	2.09	2.39									14.4	3.6	6.0	7.5	14.4	CDOT Type D Grate Inlet
7	I	0.15	0.17			n D Tc Used						5.0	5.2	8.7	0.8	1.5	Nyloplast 24" Grate Inlet
0	n	0.24	0.28		Basir	n I Tc Used	[5.0	5.2	07	1.2	24	Mal Cash Davis True 14 Cash Lilat
8	Н	0.24	0.28		Basin	H Tc Used		-				5.0	3.2	8.7	1.3	2.4	Mod Single Denver Type 16 Grate Inlet
9	0	0.19	0.22		Desig	O Tc Used						5.0	5.2	8.7	1.0	1.9	Nyloplast 24" Grate Inlet
10	N	0.36	0.38		Basin	O Te Osed						5.0	5.2	8.7	1.8	3.3	Nyloplast 2'X2' Steel Bar Inlet
					Basin	N Tc Used		-									
11	L	0.17	0.18		Bacin	L Tc Used						5.0	5.2	8.7	0.9	1.5	Nyloplast 24" Grate Inlet
12	М	0.12	0.13			M Tc Used						5.0	5.2	8.7	0.6	1.1	Nyloplast 24" Grate Inlet
13	Q, PR35, PR38	1.54	1.75									8.5	4.4	7.3	6.7	12.8	FSD POND
14	A, R	2.82	4.92		Basin	Q Tc Used						17.1	3.3	5.6	9.4	27.5	CDOT Type D Grate Inlet
					Basin	A Tc Used		-									

]	PRO	PO.	SED	CO	NDIT	IONS	S DR	O.2, AIN Sum	4 <i>GE</i>	E CALCUL	ATI	ONS	5		
	From Area Runoff Coefficient Summary	v			OVE	ERLAND		PIPE	E / CHA	NNEL FLO	W	Time of Travel (T_t)	INTEN	SITY *	TOTAL	FLOWS	
DESIGN POINT	CONTRIBUTING BASINS	CA ₅	CA100	C ₅	Length	Height	T _C	Length	Slope	Velocity	T _t	TOTAL	I ₅	I ₁₀₀	Q5	Q ₁₀₀	COMMENTS
				1	(ft)	(ft)	(min)	(ft)	(%)	(fps)	(min)	(min)	(in/hr)	(in/hr)	(c.f.s.)	(c.f.s.)	
15	р	0.03	0.10									9.6	4.2	7.0	0.1	0.7	SWALE CONVEYS FLOW TO
																	EAST FORK SAND CREEK
					Basin	P Tc Used											
16	S, DP15, PR40, PR41														28.8	71.5	EAST FORK SAND CREEK
					Basin	S Tc Used											

CLEARWAY NO.2, LOT 5 PROPOSED CONDITIONS DRAINAGE CALCULATIONS

(Storm Sewer Routing Summary)

					Inten	sity*	Fl	ow
PIPE RUN	Contributing Pipes/Design Points	Equivalent CA 5	Equivalent CA ₁₀₀	Maximum T _C	I_5	I 100	Q 5	Q 100
1	DP1	1.03	0.95	10.5	4.1	6.8	4.3	6.6
2	PR1, DP2	1.45	1.43	10.6	4.0	6.8	5.9	9 .7
3	DP3	0.52	0.60	10.5	4.1	6.8	2.1	4.1
4	PR2, PR3, DP4	2.24	2.41	10.6	4.0	6.8	9.1	16.4
5	PR4, DP5	3.14	4.48	10.6	4.0	6.8	12.7	30.5
6	DP6	2.09	2.39	14.4	3.6	6.0	7.5	14.4
7	PR5, PR6	5.23	6.88	14.4	3.6	6.0	18.8	41.4
8	PR7	5.23	6.88	14.4	3.6	6.0	18.8	41.4
9	.02 ACRE BASIN J	0.02	0.02	5.0	5.2	8.7	0.1	0.2
10	PR9	0.02	0.02	5.0	5.2	8.7	0.1	0.2
11	.06 ACRE BASIN J	0.04	0.05	5.0	5.2	8.7	0.2	0.4
12	PR10, PR11	0.06	0.07	5.0	5.2	8.7	0.3	0.6
13	PR12, .06 ACRE BASIN J	0.10	0.12	5.0	5.2	8.7	0.5	1.0
14	.01 ACRE BASIN J	0.01	0.01	5.0	5.2	8.7	0.0	0.1
15	PR13, PR14	0.11	0.12	5.0	5.2	8.7	0.6	1.1
16	.04 ACRE BASIN J	0.03	0.03	5.0	5.2	8.7	0.1	0.3
17	PR15, PR16	0.14	0.15	5.0	5.2	8.7	0.7	1.3
18	.02 ACRE BASIN J	0.01	0.01	5.0	5.2	8.7	0.1	0.1

CLEARWAY NO.2, LOT 5 PROPOSED CONDITIONS DRAINAGE CALCULATIONS

(Storm Sewer Routing Summary)

					Inten	sity*	Fl	ow
PIPE RUN	Contributing Pipes/Design Points	Equivalent CA 5	Equivalent CA ₁₀₀	Maximum T _C	<i>I</i> ₅	I ₁₀₀	Q 5	Q 100
19	PR17, PR18	0.15	0.17	5.0	5.2	8.7	0.8	1.5
20	PR19	0.15	0.17	5.0	5.2	8.7	0.8	1.5
21	PR20, DP11	0.32	0.34	5.0	5.2	8.7	1.6	3.0
22	PR21, DP12	0.44	0.47	5.0	5.2	8.7	2.3	4.1
23	DP7	0.15	0.17	5.0	5.2	8.7	0.8	1.5
24	PR23, DP8	0.40	0.44	5.0	5.2	8.7	2.0	3.8
25	.03 ACRE BASIN K	0.02	0.03	5.0	5.2	8.7	0.1	0.2
26	PR24, PR25	0.42	0.47	5.0	5.2	8.7	2.2	4.1
27	.05 ACRE BASIN K	0.03	0.04	5.0	5.2	8.7	0.2	0.3
28	PR26, PR27	0.45	0.51	5.0	5.2	8.7	2.3	4.4
29	.05 ACRE BASIN K	0.03	0.04	5.0	5.2	8.7	0.2	0.3
30	PR28, PR29	0.49	0.54	5.0	5.2	8.7	2.5	4.7
31	.05 ACRE BASIN K	0.04	0.04	5.0	5.2	8.7	0.2	0.3
32	PR30, PR31	0.52	0.58	5.0	5.2	8.7	2.7	5.1
33	.02 ACRE BASIN K	0.02	0.02	5.0	5.2	8.7	0.1	0.2
34	PR32, PR33	0.54	0.60	5.0	5.2	8.7	2.8	5.2
35	PR22, PR34	0.98	1.07	5.0	5.2	8.7	5.0	9.3
36	DP9	0.19	0.22	5.0	5.2	8.7	1.0	1.9

CLEARWAY NO.2, LOT 5 PROPOSED CONDITIONS DRAINAGE CALCULATIONS

(Storm Sewer Routing Summary)

					Inten	sity*	Fl	ow
PIPE RUN	Contributing Pipes/Design Points	Equivalent CA 5	Equivalent CA ₁₀₀	Maximum T _C	I_5	I 100	Q 5	Q 100
37	PR36, DP10	0.55	0.60	5.0	5.2	8.7	2.8	5.2
38	PR37	0.55	0.60	5.0	5.2	8.7	2.8	5.2
39	FSD POND RELEASE						0.3	0.3
40	PR8, PR39						19.1	41.7
41	DP14	2.82	4.92	17.1	3.3	5.6	9.4	27.5

* Intensity equations assume a minimum travel time of 5 minutes.

DP - Design Point

EX - Existing Design Point

FB- Flow By from Design Point INT- Intercepted Flow from Design Point Calculated by: TAU Date: 4/4/2022

Checked by: VAS

HYDRAULIC CALCULATIONS / FSD POND CALCULATIONS

	Design Procedure For	m: Sand Filter (SF)	
	UD-BMP (Version 3.0	7, March 2018)	Sheet 1 of 2
Designer:	Darin Moffett M&S Civil Consultants		
Company: Date:	June 3, 2022		
Project:	Clearway No.2, Lot 5 - WireNut		
Location:			
1. Basin Sto	rage Volume		
	ve Imperviousness of Tributary Area, ${\sf I}_{\sf a}$ if all paved and roofed areas upstream of sand filter)	I _a = <u>85.2</u> %	
B) Tributa	ary Area's Imperviousness Ratio (i = l _i /100)	i = 0.852	
	Quality Capture Volume (WQCV) Based on 12-hour Drain Time $V = 0.8$ * (0.91* i^3 - 1.19 * i^2 + 0.78 * i)	WQCV = 0.29 watershed incl	hes
D) Contri	ibuting Watershed Area (including sand filter area)	Area = 103,237 sq ft	
	Quality Capture Volume (WQCV) Design Volume _v = WQCV / 12 * Area	V _{WQCV} =cu ft	
	atersheds Outside of the Denver Region, Depth of ge Runoff Producing Storm	d ₆ = 0.50 in	
	/atersheds Outside of the Denver Region, r Quality Capture Volume (WQCV) Design Volume	V _{WQCV OTHER} =cu ft	
H) User I (Only i	Input of Water Quality Capture Volume (WQCV) Design Volume f a different WQCV Design Volume is desired)	V _{WQCV USER} = 2,222 cu ft	
2. Basin Geo	ometry		
A) WQCV	/ Depth	D _{WQCV} = 0.8 ft	
	-ilter Side Slopes (Horizontal distance per unit vertical, flatter preferred). Use "0" if sand filter has vertical walls.	Z = 4.00 ft / ft	
C) Minimu	um Filter Area (Flat Surface Area)	A _{Min} = 1099 sq ft	
D) Actual	Filter Area	A _{Actual} = 2331 sq ft	
E) Volume	e Provided	V _T =cu ft	
3. Filter Mate	erial	Choose One 18" CDOT Class B or C Filter Mater O Other (Explain):	rial
4. Underdrai	in System	Choose One	
A) Are un	derdrains provided?	● YES ○ NO	
B) Underg	drain system orifice diameter for 12 hour drain time		
	i) Distance From Lowest Elevation of the Storage Volume to the Center of the Orifice	y =ft	
	ii) Volume to Drain in 12 Hours	Vol ₁₂ = 2,222 cu ft	
	iii) Orifice Diameter, 3/8" Minimum	D _o = <u>1 1/16</u> in	

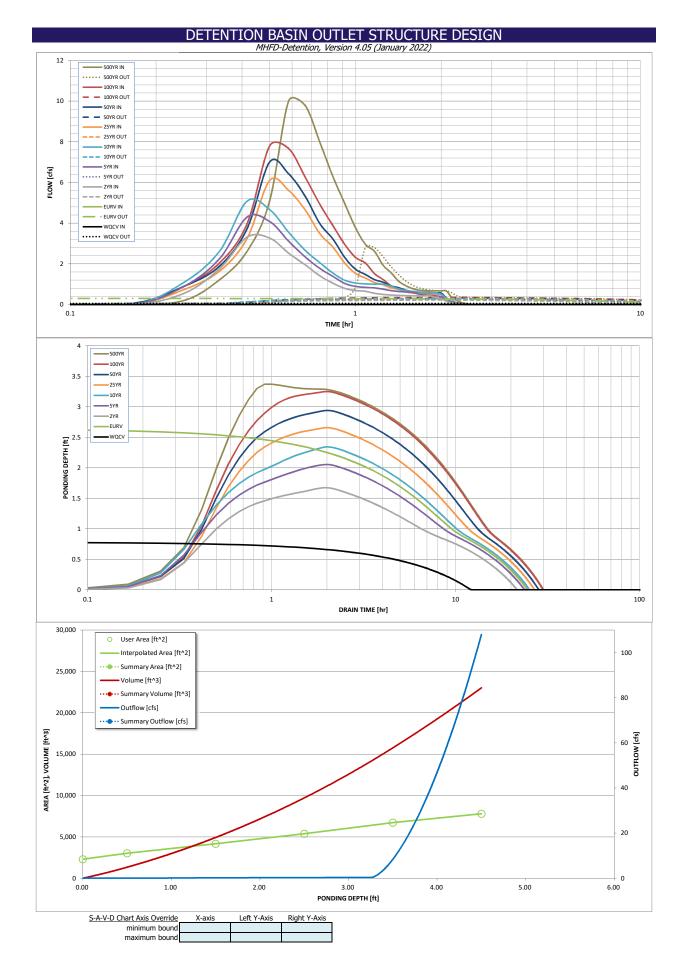
	Design Procedure For	m: Sand Filter (SF)	
			Sheet 2 of 2
Designer:	Darin Moffett M&S Civil Consultants		
Company: Date:	June 3, 2022		
Project:	Clearway No.2, Lot 5 - WireNut		
Location:			
A) Is an i	able Geomembrane Liner and Geotextile Separator Fabric mpermeable liner provided due to proximity actures or groundwater contamination?	Choose One	
	tlet Works ibe the type of energy dissipation at inlet points and means of ying flows in excess of the WQCV through the outlet	A riprap stilling basin is provided at the in Flows in excess of the WQCV are conve box wall and enter the top of the box and	yed via a retangular slot in the outlet box w
Notes:			

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.05 (January 2022)

Basin ID:	Pond 1	o. 2, Lot 5 (V												
	2													
	ONE 1													
		100-YE	AR		Depth Increment =		A							
PERMANENT ORIFIC	1 AND 2	ORIFIC	E		Deptil Increment -		Optional				Optional			T
POOL Example Zone	Configurati	on (Retentio	on Pond)		Stage - Storage	Stage	Override	Length	Width	Area (ft ²)	Override	Area	Volume	Volume
Watershed Information				6254 5	Description Media Surface	(ft) 	Stage (ft) 0.00	(ft) 	(ft) 		Area (ft ²) 2,300	(acre) 0.053	(ft ³)	(ac-ft)
Selected BMP Type =	SF	1		6251.5	Fieula Surface		0.50				3,023	0.069	1,331	0.031
Watershed Area =		20100					1.50						· ·	0.031
	2.11	acres									4,171	0.096	4,928	
Watershed Length =	335 165	ft ft					2.50 3.50				5,380	0.124	9,703	0.223
Watershed Length to Centroid = Watershed Slope =	0.020	ft/ft					4.50				6,724 7,797	0.134	15,755 23,016	0.528
Watershed Imperviousness =	85.20%	percent					1.50				7,737	0.179	25,010	0.520
Percentage Hydrologic Soil Group A =	100.0%	percent												
Percentage Hydrologic Soil Group B =	0.0%	percent												+
Percentage Hydrologic Soil Groups C/D =	0.0%	percent												+
Target WQCV Drain Time =	12.0	hours												+
Location for 1-hr Rainfall Depths =		nouro												-
	•	vainfall												-
After providing required inputs above incl depths, click 'Run CUHP' to generate runo														1
the embedded Colorado Urban Hydrog			Optional Use	er Overrides										+
Water Quality Capture Volume (WQCV) =	0.051	acre-feet		acre-feet										1
Excess Urban Runoff Volume (EURV) =	0.241	acre-feet		acre-feet										1
2-yr Runoff Volume (P1 = 1.19 in.) =	0.158	acre-feet	1.19	inches										
5-yr Runoff Volume (P1 = 1.5 in.) =	0.204	acre-feet	1.50	inches										
10-yr Runoff Volume (P1 = 1.75 in.) =	0.241	acre-feet	1.75	inches										
25-yr Runoff Volume (P1 = 2 in.) =	0.283	acre-feet	2.00	inches										
50-yr Runoff Volume (P1 = 2.25 in.) =	0.323	acre-feet	2.25	inches										
100-yr Runoff Volume (P1 = 2.52 in.) =	0.370	acre-feet	2.52	inches										
500-yr Runoff Volume (P1 = 3.14 in.) =	0.474	acre-feet		inches										
Approximate 2-yr Detention Volume =	0.158	acre-feet												1
Approximate 5-yr Detention Volume =	0.206	acre-feet												1
Approximate 10-yr Detention Volume =	0.245	acre-feet												
Approximate 25-yr Detention Volume =	0.290	acre-feet												
Approximate 50-yr Detention Volume =	0.316	acre-feet												
Approximate 100-yr Detention Volume =	0.339	acre-feet												
Define Zones and Basin Geometry														
Zone 1 Volume (WQCV) =	0.051	acre-feet												
Zone 2 Volume (EURV - Zone 1) =	0.190	acre-feet												
Zone 3 Volume (100-year - Zones 1 & 2) =	0.098	acre-feet												
Total Detention Basin Volume =	0.339	acre-feet												
Initial Surcharge Volume (ISV) =	user	ft ³												<u> </u>
Initial Surcharge Depth (ISD) =	user	ft												<u> </u>
Total Available Detention Depth $(H_{total}) =$	user	ft												
Depth of Trickle Channel $(H_{TC}) =$	user	ft												
Slope of Trickle Channel (S_{TC}) =	user	ft/ft												
Slopes of Main Basin Sides $(S_{main}) =$	user	H:V												<u> </u>
Basin Length-to-Width Ratio $(R_{I/W}) =$	user												1	1

		DE	TENTION	BASIN OUT	LET STRU	CTURE DE	SIGN		
	Project:	Clearway No. 2, Lo		IFD-Detention, Ver	rsion 4.05 (Januar)	/ 2022)			
	Basin ID:		in the second						
	ZONE 3 ZONE 2 ZONE 1	\frown			Estimated	Estimated			
100-YR VOLUME EURV	wacy				Stage (ft)	Volume (ac-ft)	Outlet Type	1	
	wacv			Zone 1 (WQCV)	0.79	0.051	Filtration Media		
	ZONE 1 AND 2	ORIFICE		Zone 2 (EURV) Zone 3 (100-year)	2.65 3.36	0.190	Circular Orifice Weir&Pipe (Restrict)	-	
		Configuration (Re	tention Pond)	Zone 5 (100-year)	Total (all zones)	0.098	weirapipe (Restrict)	1	
User Input: O	rifice at Underdrain Outlet (typically	v used to drain WQ	CV in a Filtration Bl	<u>MP)</u>		0.005	1	Calculated Paramet	ters for Underdrain
	Underdrain Orifice Invert Depth =			the filtration media	surface)		drain Orifice Area =		ft ²
	Underdrain Orifice Diameter =	1.08	inches			Underdrair	Orifice Centroid =	0.05	feet
User Input: (Drifice Plate with one or more orifice	es or Elliptical Slot \	Neir (typically used	to drain WQCV and	l/or EURV in a sedir	nentation BMP)		Calculated Paramet	ters for Plate
	Centroid of Lowest Orifice =			n bottom at Stage =			ice Area per Row =		ft²
	at top of Zone using Orifice Plate =			bottom at Stage =			ptical Half-Width =		feet
	ce Plate: Orifice Vertical Spacing = rifice Plate: Orifice Area per Row =	N/A N/A	inches sq. inches	does not a	appear to		ical Slot Centroid = Iliptical Slot Area =	N/A N/A	feet ft ²
0	nince hate. Onlince Area per Now -	11/1	sq. menes	match the	plans.			174	i c
				revise acc	ordinaly				
User Input: S	Stage and Total Area of Each Orifice	Row (numbered fr	rom lowest to high				Dow 6 (anti-anti-	Dow 7 (ti)	Dow 9 (cational)
	Stage of Orifice Centroid (ft)	Row 1 (optional) N/A	Row 2 (optional) N/A	Row 3 (optional) N/A	Row 4 (optional) N/A	Row 5 (optional) N/A	Row 6 (optional) N/A	Row 7 (optional) N/A	Row 8 (optional) N/A
	Orifice Area (sq. inches)	N/A N/A	N/A N/A	N/A N/A	N/A N/A	N/A N/A	N/A N/A	N/A N/A	N/A N/A
					·				
	Star - College College College	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
	Stage of Orifice Centroid (ft) Orifice Area (sq. inches)	N/A N/A	N/A N/A	N/A N/A	N/A N/A	N/A N/A	N/A N/A	N/A N/A	N/A N/A
	onnee Area (sq. menes)	in pro-		N/A	14/5	14/15	11/15	ing PA	N/A
User Input: \	/ertical Orifice (Circular or Rectangu			1				Calculated Paramet	
	Invert of Vertical Orifice =	Zone 2 Circular 0.79	Not Selected	ft (rolativo to bacin	bottom at Stago -	0.ft) \/a	tical Orifica Aroa -	Zone 2 Circular	Not Selected
Depth at t	top of Zone using Vertical Orifice =	2.65	N/A N/A	ft (relative to basin	bottom at Stage =	,	rtical Orifice Area = I Orifice Centroid =	0.04	N/A N/A
Deptil ut	Vertical Orifice Diameter =	2.59	N/A	inches	bottom ut Stuge -	vertica		0.11	14/7
				-					
User Input: (Overflow Weir (Dropbox with Flat or	Sloped Grate and	Outlet Pipe OR Rec	tangular/Trapezoida	al Weir and No Outl	et Pipe)		Calculated Paramet	ters for Overflow W
	(= - p		• • • • • • • • • • • • • • • • • • •						
		Zone 3 Weir	Not Selected					Zone 3 Weir	Not Selected
Over	flow Weir Front Edge Height, Ho =	2.65	N/A	ft (relative to basin b	oottom at Stage = 0 fl) Height of Grat	e Upper Edge, H _t =	2.65	N/A
(verflow Weir Front Edge Length =	2.65 2.91	N/A N/A	feet	-	Overflow W	/eir Slope Length =		N/A N/A
this will cause	Verflow Weir Front Edge Length = Overflow Weir Grate Slope =	2.65 2.91 0.00	N/A N/A N/A	feet H:V	G	Overflow W ate Open Area / 10	/eir Slope Length = 00-yr Orifice Area =	2.65	N/A N/A N/A
this will cause clogging	Verflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides =	2.65 2.91	N/A N/A N/A N/A	feet	Gi	Overflow W ate Open Area / 10 verflow Grate Open	/eir Slope Length =)0-yr Orifice Area = Area w/o Debris =	2.65	N/A N/A
this will cause	Verflow Weir Front Edge Length = Overflow Weir Grate Slope =	2.65 2.91 0.00	N/A N/A N/A	feet H:V	Gi	Overflow W ate Open Area / 10	/eir Slope Length =)0-yr Orifice Area = Area w/o Debris =	2.65	N/A N/A N/A N/A
this will cause clogging maintenance	Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % =	2.65 2.91 0.00 2.91 50%	N/A N/A N/A Close Mesh Grate N/A	feet H:V feet %	Gi	Overflow W rate Open Area / 10 verflow Grate Open Overflow Grate Ope	/eir Slope Length =)0-yr Orifice Area = Area w/o Debris = n Area w/ Debris =	2.65 2.91	N/A N/A N/A N/A N/A
this will cause clogging maintenance	Verflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type =	2.65 2.91 0.00 2.91 50% (Circular Orifice, Re	N/A N/A N/A Close Mesh Grate N/A estrictor Plate, or R	feet H:V feet %	Gi	Overflow W rate Open Area / 10 verflow Grate Open Overflow Grate Ope	/eir Slope Length =)0-yr Orifice Area = Area w/o Debris = n Area w/ Debris =	2.65 2.91 s for Outlet Pipe w/	N/A N/A N/A N/A N/A Flow Restriction Pla
this will cause clogging maintenance issues, consider adjustin gser Input: 0	Verflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = utlet Pipe w/ Flow Restriction Plate	2.65 2.91 0.00 2.91 50% (<u>Circular Orifice, Rr</u> Zone 3 Restrictor	N/A N/A N/A Close Mesh Grate N/A estrictor Plate, or R Not Selected	feet H:V feet % <u>ectangular Orifice)</u>	Gi	Overflow W rate Open Area / 10 verflow Grate Open Overflow Grate Ope	/eir Slope Length =)0-yr Orifice Area = Area w/o Debris = n Area w/ Debris = Iculated Parameter	2.65 2.91 s for Outlet Pipe w/ Zone 3 Restrictor	N/A N/A N/A N/A N/A Flow Restriction Pla Not Selected
this will cause clogging maintenance issues, consider adjustingser Input: C restrictor plate	Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % =	2.65 2.91 0.00 2.91 50% (Circular Orifice, Re	N/A N/A N/A Close Mesh Grate N/A estrictor Plate, or R	feet H:V feet %	Gi	Overflow W rate Open Area / 10 verflow Grate Open Overflow Grate Open <u>Ca</u> = 0 ft) O	/eir Slope Length =)0-yr Orifice Area = Area w/o Debris = n Area w/ Debris =	2.65 2.91 s for Outlet Pipe w/	N/A N/A N/A N/A N/A Flow Restriction Pla
this will cause clogging maintenance issues, consider adjustin gser Input: Q restrictor plate height	Verflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = <u>utlet Pipe w/ Flow Restriction Plate</u> Depth to Invert of Outlet Pipe =	2.65 2.91 0.00 2.91 50% (<u>Circular Orifice, R</u> Zone 3 Restrictor 3.00	N/A N/A N/A Close Mesh Grate N/A estrictor Plate, or R Not Selected N/A	feet H:V feet % ectangular Orifice) ft (distance below ba	Gi Or (Overflow W rate Open Area / 10 verflow Grate Open Overflow Grate Open <u>Ca</u> = 0 ft) O Outle	<pre>/eir Slope Length = 00-yr Orifice Area = Area w/o Debris = n Area w/ Debris = <u>alculated Parameter</u> utlet Orifice Area =</pre>	2.65 2.91 s for Outlet Pipe w/ Zone 3 Restrictor 0.17 0.14	N/A N/A N/A N/A N/A Flow Restriction Pla Not Selected N/A
this will cause clogging maintenance issues, consider adjustingser Input: C restrictor plate height	verflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = utlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = r Plate Height Above Pipe Invert =	2.65 2.91 0.00 2.91 50% (Circular Orifice, Re Zone 3 Restrictor 3.00 18.00 2.75	N/A N/A N/A Close Mesh Grate N/A estrictor Plate, or R Not Selected N/A	feet H:V feet % ectangular Orifice) ft (distance below ba inches	Gi Or (Overflow W rate Open Area / 10 verflow Grate Open Overflow Grate Open <u>Ca</u> = 0 ft) O Outle	<pre>/eir Slope Length = 00-yr Orifice Area = Area w/o Debris = n Area w/ Debris = <u>alculated Parameter</u> utlet Orifice Area = t Orifice Centroid =</pre>	2.65 2.91 s for Outlet Pipe w/ Zone 3 Restrictor 0.17 0.14 0.80	N/A N/A N/A N/A N/A Elow Restriction Pla N/A N/A N/A N/A N/A
this will cause clogging maintenance issues, consider adjustingser Input: C restrictor plate height	Verflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = utlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = r Plate Height Above Pipe Invert = mergency Spillway (Rectangular or	2.65 2.91 0.00 2.91 50% (Circular Orifice, Ra Zone 3 Restrictor 3.00 18.00 2.75 Trapezoidal)	N/A N/A N/A Close Mesh Grate N/A estrictor Plate, or R Not Selected N/A N/A	feet H:V feet 9% ft (distance below ba inches inches	Gi O' (tsin bottom at Stage = Half-Cent	Overflow W rate Open Area / 10 verflow Grate Open Overflow Grate Open Ca = 0 ft) O Outle tral Angle of Restric	<pre>/eir Slope Length = 00-yr Orifice Area = Area w/o Debris = n Area w/ Debris = liculated Parameter utlet Orifice Area = t Orifice Centroid = tor Plate on Pipe =</pre>	2.65 2.91 s for Outlet Pipe w/ Zone 3 Restrictor 0.17 0.14 0.80 Calculated Paramet	N/A N/A N/A N/A N/A Elow Restriction Pla N/A N/A N/A N/A N/A N/A Selected N/A N/A
this will cause clogging maintenance issues, consider adjustingser Input: C restrictor plate height	verflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = utlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = r Plate Height Above Pipe Invert =	2.65 2.91 0.00 2.91 50% (Circular Orifice, Re Zone 3 Restrictor 3.00 18.00 2.75 Trapezoidal) 3.26	N/A N/A N/A Close Mesh Grate N/A estrictor Plate, or R Not Selected N/A N/A	feet H:V feet % ectangular Orifice) ft (distance below ba inches	Gi O' (tsin bottom at Stage = Half-Cent	Overflow W rate Open Area / 10 verflow Grate Open Overflow Grate Open Ca = 0 ft) O Outle rral Angle of Restrict Spillway D	<pre>/eir Slope Length = 00-yr Orifice Area = Area w/o Debris = n Area w/ Debris = <u>alculated Parameter</u> utlet Orifice Area = t Orifice Centroid =</pre>	2.65 2.91 s for Outlet Pipe w/ Zone 3 Restrictor 0.17 0.14 0.80 Calculated Paramet	N/A N/A N/A N/A N/A Elow Restriction Pla N/A N/A N/A N/A N/A
this will cause clogging maintenance issues, consider adjustingser Input: C restrictor plate height	Verflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = utlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = r Plate Height Above Pipe Invert = mergency Spillway (Rectangular or Spillway Invert Stage=	2.65 2.91 0.00 2.91 50% (<u>Circular Orifice, Re</u> Zone 3 Restrictor 3.00 18.00 2.75 Trapezoidal) 3.26 22.00	N/A N/A N/A Close Mesh Grate N/A estrictor Plate, or R Not Selected N/A N/A N/A	feet H:V feet 9% ft (distance below ba inches inches	Gi O' (tsin bottom at Stage = Half-Cent	Overflow W rate Open Area / 10 verflow Grate Open Overflow Grate Open Ca ca = 0 ft) O Outle tral Angle of Restrict Spillway D Stage at	<pre>/eir Slope Length = /0-yr Orifice Area = /Area w/o Debris = n Area w/ Debris = // Deb</pre>	2.65 2.91 s for Outlet Pipe w/ Zone 3 Restrictor 0.17 0.14 0.80 <u>Calculated Paramet</u> 0.23 4.49	N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A
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this will cause clogging maintenance issues, consider adjustingser input: O restrictor plate height Restricto User Input: E Free Routed Hydr OPTIONAL O Predevel Ratic	verflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = utlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = r Plate Height Above Pipe Invert = mergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length = Spillway Crest Length = CUHP Runoff Volume (acre-ft) = CUHP Runoff Volume (acre-ft) = CUHP Predevelopment Peak Q (cfs) = veride Predevelopment Peak Q (cfs) = Peak Nufflow Q (cfs) = Peak Nufflow Q (cfs) = Peak Unflow Q (cfs) = Peak Outflow G (cfs) = Peak Outflow G (cfs) = Peak Outflow G (cfs) = Nax Velocity through Grate 1 (fps) = Max Velocity through Grate 2 (fps) =	2.65 2.91 0.00 2.91 50% (Circular Orifice, Re Zone 3 Restrictor 3.00 18.00 2.75 Trapezoidal) 3.26 22.00 4.00 1.00 The user can over WQCV N/A 0.051 N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A	N/A N/A N/A N/A N/A Close Mesh Grate N/A estrictor Plate, or R Not Selected N/A N/A N/A ft (relative to basin feet H:V feet ide the default CU EURV N/A 0.241 N/A	feet H:V feet 9% ectangular Orifice) ft (distance below ba inches inches inches n bottom at Stage = <u>4/P hydrographs and 2 Year</u> 1.19 0.158 0.058 0.01 3.3 0.2 N/A Vertical Orifice 1 N/A	Gi Or (asin bottom at Stage = Half-Cent 0 ft) 1.50 0.204 0.	Overflow W rate Open Area / 10 verflow Grate Open Overflow Grate Open Overflow Grate Open Car a of the open solution of the open solution of the open solution of the open solution of the open solution of the open solution open and the open and the open solution open and the open and the open and the open solution open and the open and	<pre>/eir Slope Length = 0-yr Orifice Area = Area w/o Debris = n Area w/ Debris = n Area w/ Debris = elculated Parameter utlet Orifice Area = t Orifice Centroid = tor Plate on Pipe = esign Flow Depth= Fop of Freeboard = Fop of Freeboard = Fop of Freeboard = Fop of Freeboard = Fop of Freeboard = Cop of Cop of Cop of Cop of Cop of Cop of Cop of Cop of Cop of Cop of Cop of Co</pre>	2.65 2.91 2.91 2.00 3 Restrictor 0.17 0.14 0.80 2.23 4.49 0.18 0.53 4.49 0.18 0.53 50 Year 2.25 0.323 0.323 1.0 50 Year 2.25 0.323 0.323 1.0 0.323 1.0 0.3 0.323 1.0 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0	N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A
this will cause clogging maintenance issues, consider adjustingser Input: O restrictor plate height Restrictor User Input: E Free Routed Hydr OPTIONAL O Predevel Ratio	verflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = utlet Pipe wir Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = r Plate Height Above Pipe Invert = mergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length = Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = board above Max Water Surface = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acreft) = Inflow Hydrograph Volume (acreft) = Inflow Hydrograph Volume (acreft) = Peak Inflow Q (cfs) = Peak Outflow to Predevelopment Q = Desidue Volume (acreft) = Peak Outflow to Predevelopment Q = Peak Outflow to Predevelopment Q = Structure Controlling Flow = Max Velocity through Grate 1 (fps) = Max Velocity through Grate 1 (fps) = Drain 97% of Inflow Volume (hours) =	2.65 2.91 0.00 2.91 50% Zone 3 Restrictor 3.00 18.00 2.75 Trapezoidal) 3.26 22.00 4.00 1.00 The user can overn WQCV N/A 0.051 N/A N/A N/A N/A N/A N/A N/A 12	N/A N/A N/A N/A Close Mesh Grate N/A estrictor Plate, or R Not Selected N/A N/A N/A fet (relative to basin feet H:V feet EURV N/A 0.241 N/A 0.241 N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A	feet H:V feet 9% ectangular Orifice) ft (distance below ba inches inches n bottom at Stage = 0.0158 0.122 0.1580 0.15800	Gi Or (asin bottom at Stage = Half-Cent Half-Cent 0 ft) 0 ft) 0 ft) 0.204 0.204 0.204 0.204 0.204 0.204 0.204 0.204 0.204 0.204 0.204 0.3 0.3 0.3 0.3 0.3 Vertical Orifice 1 N/A N/A 22	Overflow W rate Open Area / 10 verflow Grate Open Overflow Grate Open Overflow Grate Open Carlow Grate Open Carlow Grate Open Carlow Grate Open Carlow Grate Open Carlow Grate Open Carlow Grate Open Stage at Basin Area at Basin Volume at Basin Volume at Basin Volume at Carlow Grate Basin Volume at Carlow Grate Carlow	<pre>/eir Slope Length = 0-yr Orifice Area = Area w/o Debris = n Area w/ Debris = n Area w/ Debris = elculated Parameter utlet Orifice Area = t Orifice Centroid = tor Plate on Pipe = esign Flow Depth= Fop of Freeboard = Fop of Freeboard = Fop of Freeboard = Fop of Freeboard = Cop of Cop of C</pre>	2.65 2.91 2.91 2.00 3 Restrictor 0.17 0.14 0.80 2.25 0.23 4.49 0.18 0.53 2.25 0.323 0.323 1.0 50 Year 2.25 0.323 0.323 1.0 0.323 0.323 1.0 0.3 0.323 1.0 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0	N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A
this will cause clogging maintenance issues, consider adjustingser Input: O restrictor plate height Restricto User Input: E Free Routed Hydr OPTIONAL O Predevel Ratio	overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = utlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = r Plate Height Above Pipe Invert = mergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length = Spillway End Slopes = eboard above Max Water Surface = One-Hour Rainfall Depth (in) = CUHP Predevelopment Peak Q (cfs) = verride Predevelopment Peak Q (cfs) = peak Inflow Q (cfs) = Peak Outflow to Predevelopment Q = Structure Controlling Flow = Max Velocity through Grate 1 (fps) = Max Velocity through Grate 2 (fps) = Drain 99% of Inflow Volume (hours) = Drain 99% of Inflow Volume (hours) = Maximum Ponding Depth (ft) =	2.65 2.91 0.00 2.91 50% Zone 3 Restrictor 3.00 18.00 2.75 Trapezoidal) 3.26 22.00 4.00 1.00 7 <i>The user can overl</i> WQCV N/A 0.051 N/A 0.051 N/A N/A N/A N/A N/A N/A N/A N/A N/A 2.75	N/A N/A N/A N/A N/A Close Mesh Grate N/A estrictor Plate, or R Not Selected N/A N/A N/A ft (relative to basin feet H:V feet ride the default CU EURV N/A 0.241 N/A	feet H:V feet 9% ectangular Orifice) ft (distance below ba inches inches n bottom at Stage = 4/P hydrographs and 2 Year 1.19 0.158 0.0 0.01 0.158 0.0 0.01 0.2 N/A Vertical Orifice 1 N/A N/A 21 1.67	Gi Or (asin bottom at Stage a Half-Cent a Unit for the stage of the s	Overflow W rate Open Area / 10 verflow Grate Open Overflow Grate Open Overflow Grate Open Car a of the open source of the open car a open car open car a open car a open ca	<pre>/eir Slope Length = //eir Slope Length = //eix Slope Length = //eix Slope Length = //eix Slope Lenk - //eix Slope Lenk - /</pre>	2.65 2.91 2.91 2.000 3 Restrictor 0.17 0.14 0.80 2.23 4.49 0.18 0.53 2.25 0.323 1.0 50 Year 2.25 0.323 1.0 50 Year 2.25 0.323 1.0 50 7.0 7.0 50 7.0 7.0 50 7.0 50 7.0 50 7.0 50 7.0 50 7.0 7.0 50 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.	N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A
this will cause clogging maintenance issues, consider adjustingser Input: O restrictor plate height Restricto User Input: E Free Routed Hydr OPTIONAL O Predevel Ratio	overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = utlet Pipe W/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = r Plate Height Above Pipe Invert = mergency Spillway (Rectangular or Spillway Crest Length = Spillway Crest Length = Spillway Crest Length = Spillway Crest Length = One-Hour Rainfall Depth (in) = CUHP Ruooff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = Peak Inflow Q (cfs) = Peak Nutflow Q (cfs) = Peak Outflow to Predevelopment Peak Q (cfs) = Peak Outflow to Predevelopment Q = Structure Controlling Flow = Max Velocity through Grate 1 (fps) = Max Velocity through Grate 2 (fps) = Drain 97% of Inflow Volume (hours) =	2.65 2.91 0.00 2.91 50% Zone 3 Restrictor 3.00 18.00 2.75 Trapezoidal) 3.26 22.00 4.00 1.00 7 <i>The user can overn</i> WQCV N/A 0.051 N/A N/A N/A N/A N/A N/A N/A N/A 12 12 12	N/A N/A N/A N/A N/A Close Mesh Grate N/A estrictor Plate, or R Not Selected N/A N/A N/A ft (relative to basin feet H:V feet ride the default CU) EURV N/A 0.241 N/A	feet H:V feet 9% ectangular Orifice) ft (distance below ba inches inches n bottom at Stage = 0.01 0.158 0.058 0.01 0.01 3.3 0.2 N/A Vertical Orifice 1 N/A Vertical Orifice 1 N/A 21 21	Gi Ori esin bottom at Stage = Half-Cent 0 ft) 0 ft) 0 ft) 0.204 0.202 0.204 0.202 0.	Overflow W rate Open Area / 10 verflow Grate Open Overflow Grate Open Overflow Grate Open Carlow Grate Open (Carlow Grate Open	<pre>/eir Slope Length = 0-yr Orifice Area = Area w/o Debris = n Area w/ Debris = n Area w/ Debris = ilculated Parameter utlet Orifice Area = t Orifice Centroid = tor Plate on Pipe = esign Flow Depth= Top of Freeboard = Top of Freeboard = Fop of Freeboard = Fop of Freeboard = Cop of Freeboard = Co</pre>	2.65 2.91 2.91 2.00 3 Restrictor 0.17 0.14 0.80 2.23 4.49 0.18 0.53 2.25 0.323 1.0 50 Year 2.25 0.323 1.0 90 Year 2.25 0.323 1.0 90 Year 2.25 0.323 0.323 1.0 90 Year 2.25 0.323 0.323 1.0 90 Year 2.25 0.323 0.323 1.0 90 Year 2.25 0.323 1.0 90 Year 2.25 0.323 0.323 0.3 90 Year 2.25 0.323 0.323 1.0 90 Year 2.25 0.323 0.323 1.0 90 Year 2.25 0.323 0.3 90 Year 2.25 0.323 0.3 90 Year 2.25 0.323 0.32 0.3 90 Year 2.25 0.323 0.32 0.3 90 Year 2.25 0.323 0.323 0.3 90 Year 2.25 0.323 0.3 90 Year 2.25 0.323 0.3 90 Year 2.25 0.323 0.3 90 Year 2.25 0.323 0.3 90 Year 2.25 0.323 0.323 0.3 90 Year 2.25 0.323 0.323 0.3 90 Year 2.25 7.0 90 Year 2.26 2.28	N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A



DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename:

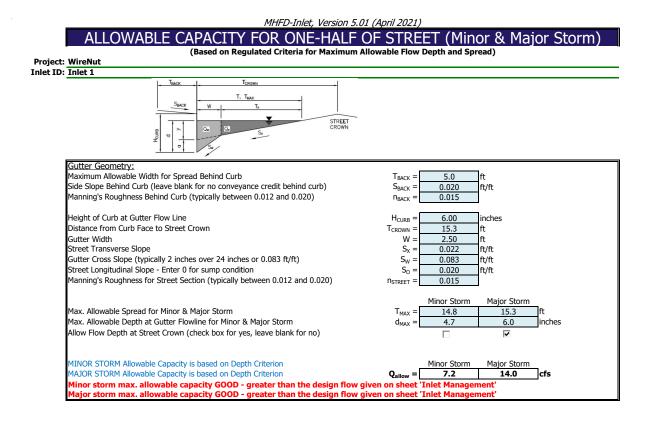
Inflow Hydrographs

	The user can o	verride the calcu	lated inflow hyd	rographs from th	nis workbook wit	h inflow hydrogr	aphs developed	in a separate pro	gram.	
	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.06	0.01	0.19
	0:15:00	0.00	0.00	0.54	0.88	1.09	0.73	0.89	0.88	1.21
	0:20:00	0.00	0.00	1.75	2.24	2.61	1.63	1.88	2.04	2.61
	0:25:00	0.00	0.00	3.31	4.30	5.08	3.24	3.73	3.97	5.09
	0:30:00	0.00	0.00	3.27	4.08	4.67	6.09	7.00	7.80	10.01
	0:35:00	0.00	0.00	2.52	3.11	3.55	5.60	6.42	7.67	9.78
	0:40:00	0.00	0.00	1.95	2.34	2.66	4.64	5.32	6.26	7.99
	0:45:00	0.00	0.00	1.41	1.77	2.06	3.48	3.98	4.93	6.30
	0:50:00	0.00	0.00	1.05	1.38	1.55	2.82	3.22	3.89	4.98
	0:55:00 1:00:00	0.00	0.00	0.79	1.03 0.89	1.19	2.04	2.32	2.96 2.32	3.78 2.96
	1:05:00	0.00	0.00	0.68	0.89	1.06	1.30	1.74	2.32	2.96
	1:10:00	0.00	0.00	0.55	0.82	1.02	1.08	1.48	1.52	1.93
	1:15:00	0.00	0.00	0.35	0.75	1.00	0.97	1.09	1.32	1.55
	1:20:00	0.00	0.00	0.46	0.68	0.90	0.81	0.92	0.91	1.15
	1:25:00	0.00	0.00	0.44	0.64	0.77	0.74	0.83	0.74	0.93
	1:30:00	0.00	0.00	0.43	0.61	0.69	0.63	0.70	0.63	0.79
	1:35:00	0.00	0.00	0.42	0.60	0.64	0.56	0.63	0.57	0.71
	1:40:00	0.00	0.00	0.42	0.51	0.61	0.53	0.59	0.55	0.68
	1:45:00	0.00	0.00	0.42	0.46	0.60	0.51	0.57	0.54	0.67
	1:50:00	0.00	0.00	0.42	0.43	0.59	0.50	0.56	0.54	0.67
	1:55:00	0.00	0.00	0.33	0.42	0.56	0.50	0.56	0.54	0.67
	2:00:00	0.00	0.00	0.28	0.38	0.50	0.50	0.56	0.54	0.67
	2:05:00	0.00	0.00	0.16	0.22	0.28	0.29	0.32	0.31	0.38
	2:10:00 2:15:00	0.00	0.00	0.09	0.12	0.16	0.16	0.18	0.18	0.22
	2:20:00	0.00	0.00	0.04	0.06	0.08	0.09	0.10	0.09	0.12
	2:25:00	0.00	0.00	0.02	0.03	0.04	0.04	0.03	0.03	0.08
	2:30:00	0.00	0.00	0.00	0.00	0.00	0.02	0.02	0.02	0.02
	2:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:20:00 3:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:10:00	0.00 0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:15:00 4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:40:00 4:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:00:00 5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:25:00 5:30:00	0.00 0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:50:00 5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

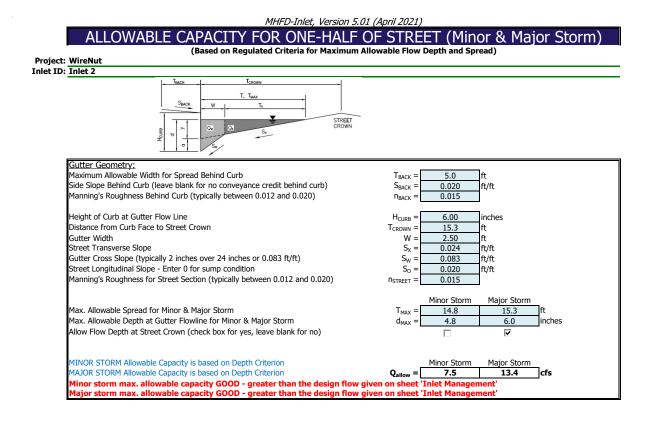
			Please see					
			comments re	egarding				
			the bypass f	lows that				
			are conveye	d to this				
MHFD-Inlet, Version 5.01 (April 2021) INLET MANAGEMENT			inlet and rev	rise				
Worksheet Protected			accordingly.	(YYYY			
INLET NAME	Inlet 1	Inlet 2	Inlet 3	Inlet 4	Inlet 5	Inlet 6	Inlet 8	Inlet 14
Site Type (Urban or Rural)	URBAN	URBAN	URBAN	URBAN	URBAN	URBAN	URBAN	URBAN
Inlet Application (Street or Area)	STREET	STREET	STREET	STREET	STREET	AREA	STREET	AREA
Hydraulic Condition	On Grade	On Grade	On Grade	On Grade	In Sump	Swale	In Sump	Swale
Inlet Type	Denver No. 16 Valley Grate	CDOT Type D (In Series & Depressed)	Denver No. 16 Valley Grate	CDOT Type D (In Series & Depressed				
ER-DEFINED INPUT					>			
User-Defined Design Flows								
finor Q _{Known} (cfs)	6.8	7.1	2.7	1.2	4.1	7.5	1.3	9.4
Major Q _{known} (cfs)	12.7	13.2	6.4	3.4	9.7	14.4	2.4	27.5
Bypass (Carry-Over) Flow from Upstream		- <u>i</u>			×			
Receive Bypass Flow from:	No Bypass Flow Received	No Bypass Flow Received	No Bypass Flow Received					
Minor Bypass Flow Received, Q _b (cfs)	0.0	0.0	0.0	0.0	0.0		0.0	0.0
Major Bypass Flow Received, Q _b (cfs)	0.0	0.0	0.0	0.0	0.0	<u> </u>	0.0	0.0
Watershed Characteristics)		
Subcatchment Area (acres)					\sim			
Percent Impervious								
NRCS Soil Type								
Watershed Profile								
Overland Slope (ft/ft)								
Overland Length (ft)								
Channel Slope (ft/ft)								
Channel Length (ft)								
Minor Storm Rainfall Input Design Storm Return Period, T _r (years)								
One-Hour Precipitation, P ₁ (inches)								
Maior Storm Rainfall Input								
major storm Kalntall Input								
Design Storm Return Period, T _r (years)								

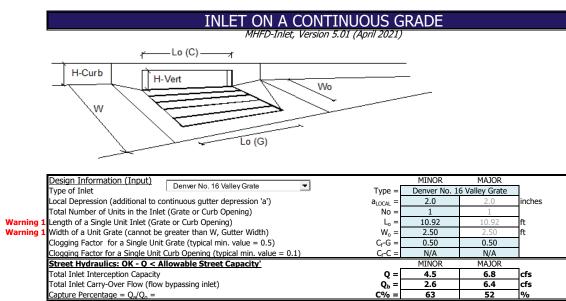
CALCULATED OUTPUT

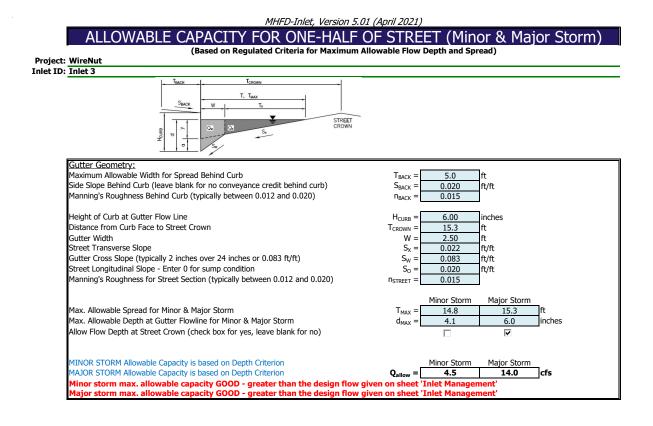
Minor Total Design Peak Flow, Q (cfs)	6.8	7.1	2.7	1.2	4.1	7.5	1.3	9.4
Major Total Design Peak Flow, Q (cfs)	12.7	13.2	6.4	3.4	9.7	14.4	2.4	27.5
Minor Flow Bypassed Downstream, Q _b (cfs)	2.5	2.6	0.5	0.2	N/A	0.0	N/A	0.0
Major Flow Bypassed Downstream, Q _b (cfs)	6.1	6.4	2.3	0.8	N/A	0.0	N/A	0.0

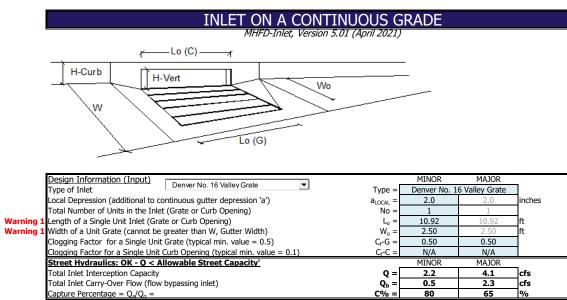


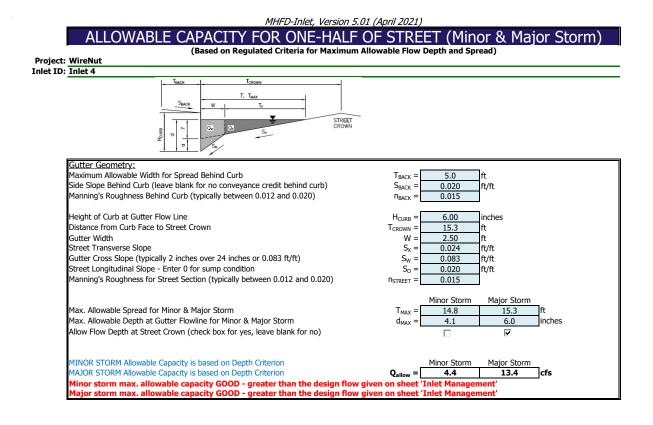
INLET ON A CONTI MHFD-Inlet, Version 5.	.01 (April 2021)	KADL		
1 (0)				
		-		
H-Curb H-Vert		_		
Lo (G)				
Design Information (Input) Denver No. 16 Valley Grate		MINOR	MAJOR	
Type of Inlet	Type =		6 Valley Grate	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	2.0	2.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening) ing 1 Length of a Single Unit Inlet (Grate or Curb Opening)	No = L _o =	1 10.92	10.92	ft
ning 1 Width of a Unit Grate (cannot be greater than W, Gutter Width)	W ₀ =	2.50	2.50	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	0.50	0.50	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	$C_{f}-C =$	N/A	N/A	
Street Hydraulics: OK - Q < Allowable Street Capacity	о Г	MINOR	MAJOR	٦.
Design Discharge for Half of Street (from <i>Inlet Management</i>) Water Spread Width	Q₀ = T =	6.8 10.7	12.7 14.2	cfs ft
Water Depth at Flowline (outside of local depression)	1 = d =	4.6	5.5	inches
Water Depth at Street Crown (or at T_{MAX})	d _{CROWN} =	0.0	0.0	inches
Ratio of Gutter Flow to Design Flow	E _o =	0.643	0.507	
Discharge outside the Gutter Section W, carried in Section T_{x}	Q _x =	2.4	6.3	cfs
Discharge within the Gutter Section W	Q _w =	4.4	6.4	cfs
Discharge Behind the Curb Face Flow Area within the Gutter Section W	$Q_{BACK} =$	0.0 0.71	0.0 0.89	cfs sq ft
Velocity within the Gutter Section W	A _W = V _W =	6.2	7.2	fps
Water Depth for Design Condition	d _{LOCAL} =	6.6	7.5	inches
Grate Analysis (Calculated)		MINOR	MAJOR	
Total Length of Inlet Grate Opening	L =	10.92	10.92	ft
Ratio of Grate Flow to Design Flow	$E_{o-GRATE} =$	0.642	0.507	
Under No-Clogging Condition Minimum Velocity Where Grate Splash-Over Begins	V _o =	MINOR 3.98	MAJOR 3.98	fps
Interception Rate of Frontal Flow	$R_{f} =$	0.93	0.88	ips
Interception Rate of Side Flow	$R_x =$	0.68	0.63	
Interception Capacity	Q _i =	5.7	9.6	cfs
Under Clogging Condition	F	MINOR	MAJOR	_
Clogging Coefficient for Multiple-unit Grate Inlet	GrateCoef = GrateClog =	1.00 0.50	1.00 0.50	
Clogging Factor for Multiple-unit Grate Inlet Effective (unclogged) Length of Multiple-unit Grate Inlet	$GrateClog = L_e =$	5.46	5.46	ft
Minimum Velocity Where Grate Splash-Over Begins	V _o =	2.73	2.73	fps
Interception Rate of Frontal Flow	R _f =	0.82	0.76	
Interception Rate of Side Flow	R _x =	0.30	0.26	4.
Actual Interception Capacity	Q _a =	4.3	6.6	cfs
Carry-Over Flow = Q_0 - Q_a (to be applied to curb opening or next d/s inlet) Curb or Slotted Inlet Opening Analysis (Calculated)	Q _b =	2.5 MINOR	6.1 MAJOR	cfs
<u>Curb or Slotted Inlet Opening Analysis (Calculated)</u> Equivalent Slope S _e (based on grate carry-over)	S _e =	N/A	MAJOR N/A	ft/ft
Required Length L_T to Have 100% Interception	L _T =	N/A	N/A	ft
Under No-Clogging Condition		MINOR	MAJOR	
Effective Length of Curb Opening or Slotted Inlet (minimum of L, L_T)	L =	N/A	N/A	ft
Interception Capacity	$Q_i =$	N/A	N/A	cfs
Under Clogging Condition Clogging Coefficient	CurbCoef =	MINOR N/A	MAJOR N/A	7
Clogging Factor for Multiple-unit Curb Opening or Slotted Inlet	CurbClog =	N/A N/A	N/A N/A	-
Effective (Unclogged) Length	$L_e =$	N/A	N/A	ft
Actual Interception Capacity	Q _a =	N/A	N/A	cfs
Carry-Over Flow = $Q_{b(GRATE)}$ - Q_a	Q _b =	N/A	N/A	cfs
Summary Total Inlet Interception Capacity	с Г	MINOR	MAJOR	
	Q =	4.3	6.6	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	$Q_b =$	2.5	6.1	cfs

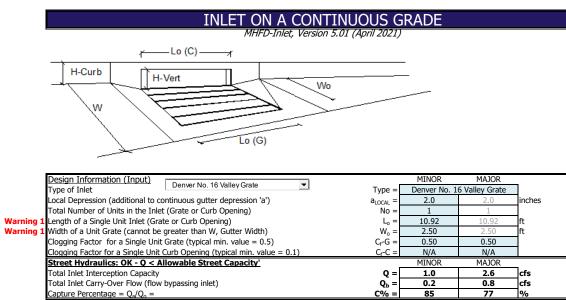


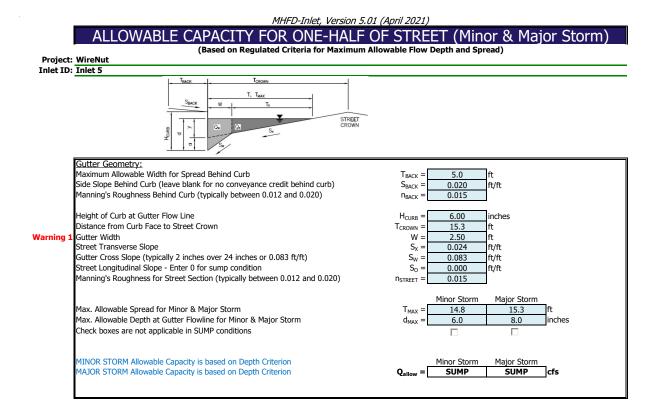




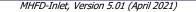


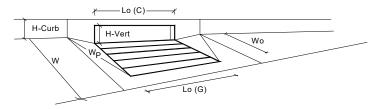






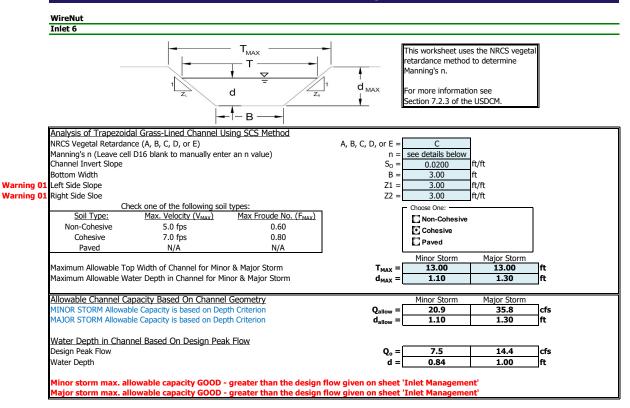
INLET IN A SUMP OR SAG LOCATION MHFD-Inlet, Version 5.01 (April 2021)



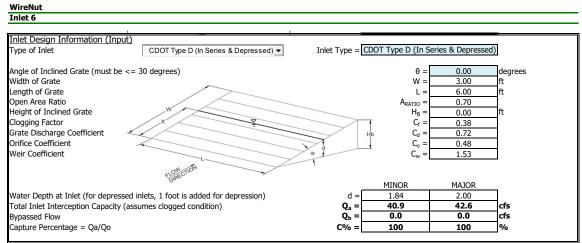


Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	Denver No. 1	6 Valley Grate	1
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	2.00	2.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	6.1	8.6	inches
Grate Information		MINOR	MAJOR	Verride Depths
Length of a Unit Grate	$L_{0}(G) =$	10.92	10.92	feet
arning 1 Width of a Unit Grate	W _o =	2.50	2.50	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	0.31	0.31	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_{f}(G) =$	0.50	0.50	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C _w (G) =	3.60	3.60]
Grate Orifice Coefficient (typical value 0.60 - 0.80)	$C_{o}(G) =$	0.60	0.60]
Curb Opening Information	_	MINOR	MAJOR	_
Length of a Unit Curb Opening	$L_{o}(C) =$	N/A	N/A	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	N/A	N/A	inches
Height of Curb Orifice Throat in Inches	H _{throat} =	N/A	N/A	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	N/A	N/A	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W _p =	N/A	N/A	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_{f}(C) =$	N/A	N/A	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$	N/A	N/A	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_{o}(C) =$	N/A	N/A]
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	0.488	0.696	ft
Depth for Curb Opening Weir Equation	d _{Curb} =	N/A	N/A	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	N/A	N/A	
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	N/A	N/A	
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	0.58	0.81	
	_	MINOD		
	o -□	MINOR 4.1	MAJOR 9.9	cfs
Total Inlet Interception Capacity (assumes clogged condition)	Q _a =	4.1 4.1	9.7	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK) Warning 1: Dimension entered is not a typical dimension for inlet type s	Q PEAK REQUIRED =	4.1	9.7	us

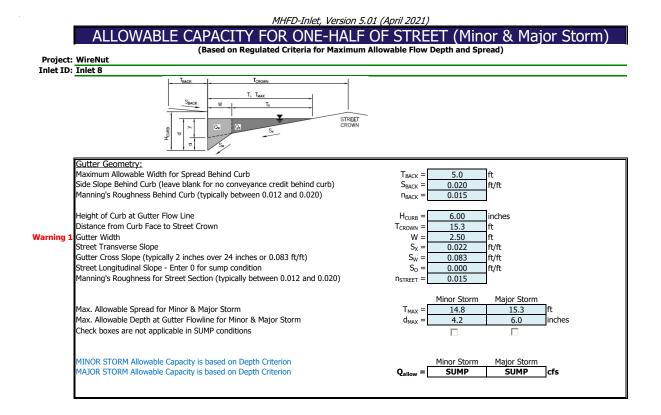
MHFD-Inlet, Version 5.01 (April 2021) AREA INLET IN A SWALE



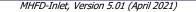
MHFD-Inlet, Version 5.01 (April 2021) AREA INLET IN A SWALE

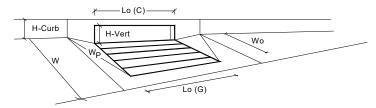


Warning 01: Sideslope steepness exceeds USDCM Volume I recommendation.



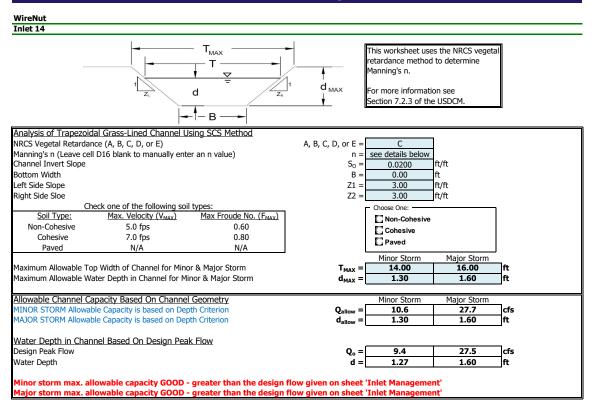
INLET IN A SUMP OR SAG LOCATION MHFD-Inlet, Version 5.01 (April 2021)





		MINOD	141300	
Design Information (Input) Two of Inlot		MINOR	MAJOR	
Type of filler	Type =		6 Valley Grate	
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	2.00	2.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	4.2	5.9	inches
Grate Information	_	MINOR	MAJOR	Override Depths
Length of a Unit Grate	$L_{o}(G) =$	3.64	3.64	feet
Warning 1 Width of a Unit Grate	W _o =	2.50	2.50	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	0.31	0.31	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_{f}(G) =$	0.50	0.50	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C_{w} (G) =	3.60	3.60	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	$C_{0}(G) =$	0.60	0.60	
Curb Opening Information	-	MINOR	MAJOR	
Length of a Unit Curb Opening	$L_{0}(C) =$	N/A	N/A	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	N/A	N/A	inches
Height of Curb Orifice Throat in Inches	H _{throat} =	N/A	N/A	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	N/A	N/A	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W _p =	N/A	N/A	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_f(C) =$	N/A	N/A	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_{w}(C) =$	N/A	N/A	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_{o}(C) =$	N/A	N/A	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	_
Depth for Grate Midwidth	d _{Grate} =	0.330	0.469	ft
Depth for Curb Opening Weir Equation	d _{Curb} =	N/A	N/A	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	N/A	N/A	
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	N/A	N/A	7
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	0.61	0.86	
	-	MINOR	MAJOR	-
Total Inlet Interception Capacity (assumes clogged condition)	Q _a =	1.3	3.1	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	$Q_{PEAK REQUIRED} =$	1.3	2.4	cfs
Warning 1: Dimension entered is not a typical dimension for inlet type	enocified			

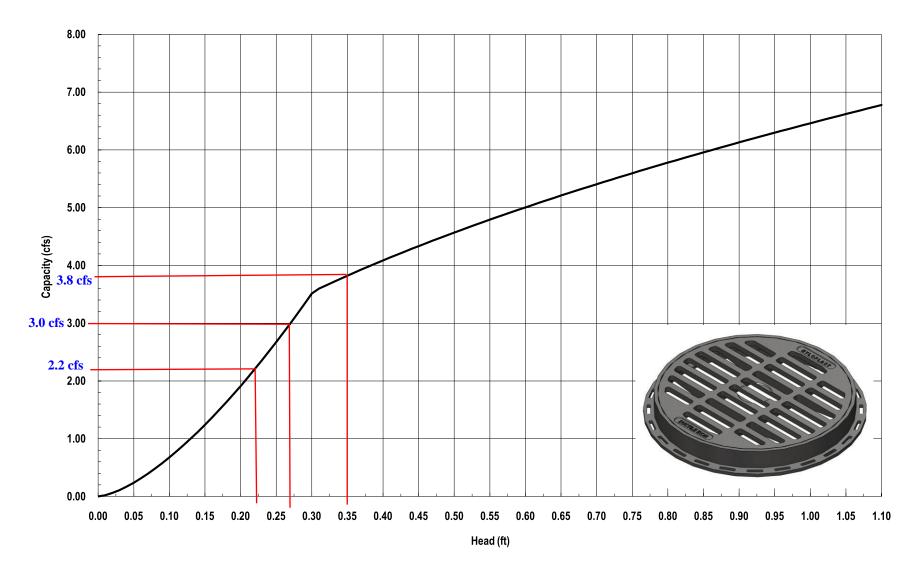
MHFD-Inlet, Version 5.01 (April 2021) AREA INLET IN A SWALE



MHFD-Inlet, Version 5.01 (April 2021) AREA INLET IN A SWALE

WireNut Inlet 14 Inlet Design Information (Input) Inlet Type = CDOT Type D (In Series & Depressed) CDOT Type D (In Series & Depressed) -Type of Inlet Angle of Inclined Grate (must be <= 30 degrees) Width of Grate θ= 0.00 degrees W = 3.00 ft Length of Grate L = 6.00 ft Open Area Ratio Height of Inclined Grate Clogging Factor Grate Discharge Coefficient Orifice Coefficient A_{RATIO} 0.70 H_B = C_f = 0.00 ft 0.38 C_d = 0.72 C_o 0.48 Weir Coefficient C_w 1.53 FLOW MINOR MAJOR Water Depth at Inlet (for depressed inlets, 1 foot is added for depression) Total Inlet Interception Capacity (assumes clogged condition) d 2.27 2.60 Q_a = 45.4 48.6 cfs Bypassed Flow Q_b 0.0 0.0 cfs Capture Percentage = Qa/Qo C% : 100 100 %

Nyloplast 24" Standard Grate Inlet Capacity Chart

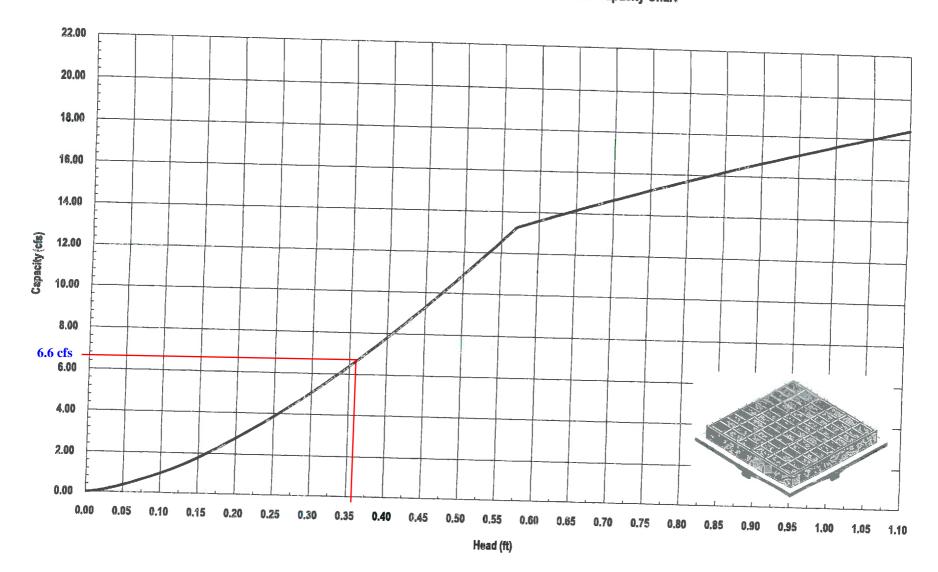


DP7= Q100=1.5 cfs 50% BLOCKAGE = 3.0 cfs DP9= Q100=1.9 cfs 50% BLOCKAGE = 3.8 cfs DP11=Q100=1.5 cfs 50% BLOCKAGE = 3.0 cfs DP12=Q100=1.1 cfs 50% BLOCKAGE = 2.2 cfs



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Nyloplast 2' x 2' Steel Bar / MAG Grate Inlet Capacity Chart



DP10= Q100**=3.3** cfs **50% BLOCKAGE = 6.6** cfs



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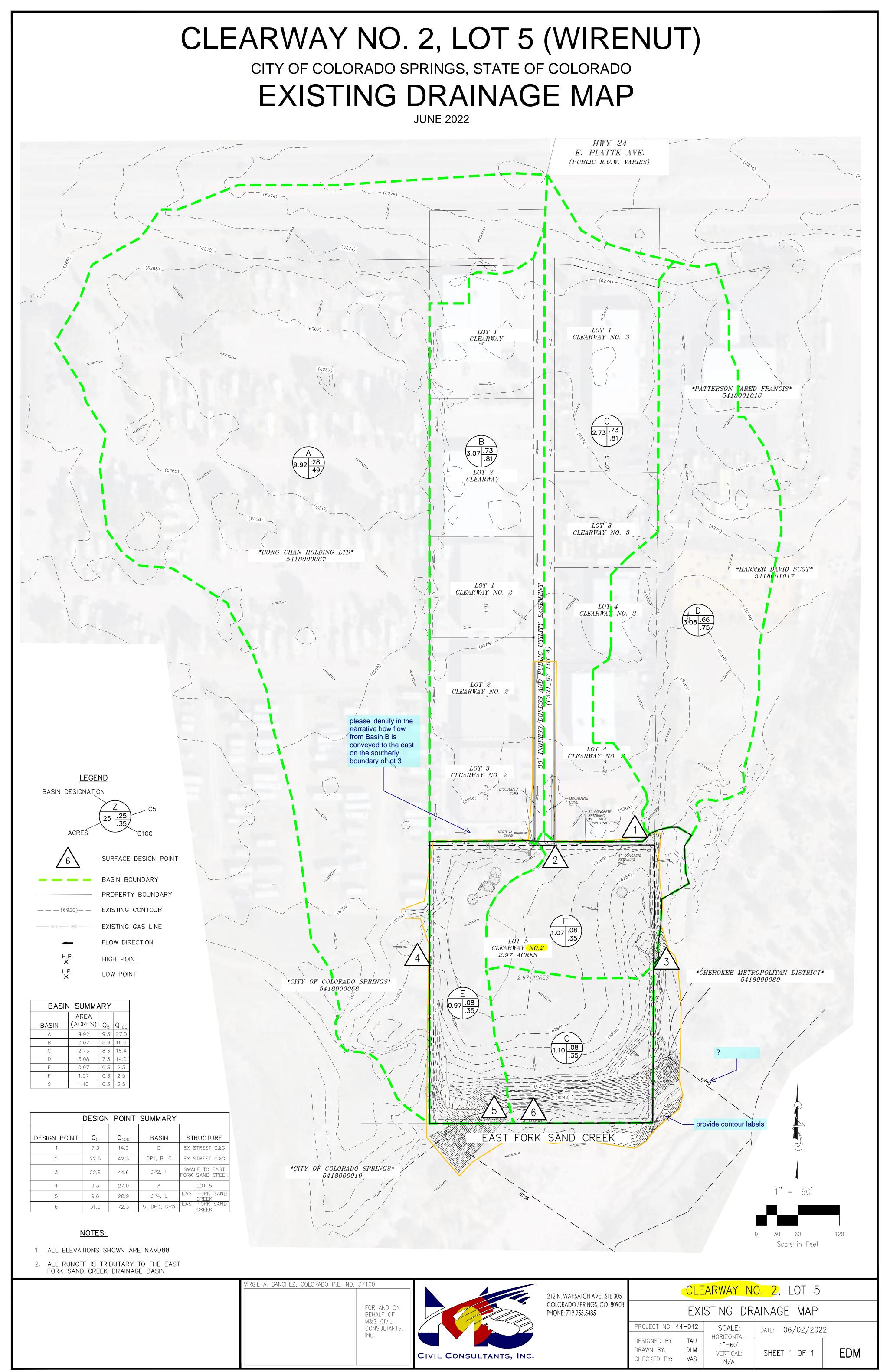
The open channel flow calculator							
Select Channel Type: Triangle ✓	$ \begin{array}{c c} \hline & & & & \\ \hline & & & $	$ \begin{array}{c} $					
Velocity(V)&Discharge(Q)	Select unit system: Feet(ft) V						
Channel slope: .02 ft/ft	Water depth(y): 1.25 ft	Bottom W(b) 0 ft					
Flow velocity 5.9328 ft/s	LeftSlope (Z1): 3 to 1 (H:V)	RightSlope (Z2): 3 to 1 (H:V)					
Flow discharge 27.8101 ft^3/s	Input n value 0.025 or select n						
Calculate!	Status: Calculation finished	Reset					
Wetted perimeter 7.91	Flow area 4.69 ft^2	Top width(T) 7.5 ft					
Specific energy 1.8 ft	Froude number 1.32	Flow status Supercritical flow					
Critical depth 1.4 ft	Critical slope 0.0109 ft/ft	Velocity head 0.55					

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DP14~Q100=27.5 cfs

EXISTING AND PROPOSED DRAINAGE MAPS

File: 0:\44042A—Wire Nut\Hammers\Drainage\Drainage Map\Existing Drainage Map.dwg Plotstamp: 6/1/2022 3:23 PM



File: 0:\44042A-Wire Nut\Hammers\Drainage\Drainage Map\Proposed Drainage Map.dwg Plotstamp: 6/3/2022 2:27 PM

