

### Flying Horse North – Phase 2 PUD Parcels 1-6 Preliminary Drainage Report

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January 2024

#### **Prepared For:**

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PCD File No. PUD-SP234



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## Engineer's Statement

This report and plan for the drainage design of the development, Flying Horse North, was prepared by me (or under my direct supervision) and is correct to the best of my knowledge and belief. Said report and plan has been prepared in accordance with the *El Paso County Drainage Criteria* Manual and is in conformity with the master plan of the drainage basin. I understand that El Paso County does not and will not assume liability for drainage facilities designed by others. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.

Richie Lyon, PE Date State of Colorado No. 53921 For and on behalf of HR Green Development, LLC

## **Developer's Statement**

I, the developer, have read and will comply with all of the requirements specified in this drainage report and plan.

Flying Horse Development, LLC

Drew Balsick Date

Vice President / Project Manager

Flying Horse Development, LLC 2138 Flying Horse Club Drive

Colorado Springs, CO 80921

# El Paso County:

Filed in accordance with the requirements of the El Paso County Land Development Code, Drainage Criteria Manual, Volumes 1 and 2 and the Engineering Criteria Manual, as amended.

Joshua Palmer, P.E.

Date

County Engineer/ECM Administrator



## I. General Purpose, Location and Description

#### **Purpose and Scope**

The Purpose of this Preliminary Drainage Report (PDR) is to identify specific solutions to drainage concerns on site and off-site resulting from the development of the subdivision to be platted as well as any drainage issues that exist prior to development. The PDR is to describe the onsite and offsite drainage patterns, quantify stormwater runoff and detention volumes, assess existing and proposed storm infrastructure as it relates to preliminary water quality and stormwater detention, describe areas tributary to the site and the planned storm water management for the Flying Horse North Parcels 1-6 development. Flying Horse North, (F.H.N.) Filing No. 1 combined Preliminary Drainage Report (PDR) and Final Drainage Report (FDR) was previously developed by Classic Consulting Engineers and Surveyors and included in Appendix F and a more recent Master Development Drainage Plan (MDDP) was prepared by HR Green Development, LLC. and was approved by the County in September of 2022, entitled *Flying Horse North Master Development Drainage Plan* latest revision date of September 9, 2022. A Final Drainage Report for Flying Horse North Filing No. 3 developed by HR Green Development, LLC. is currently in process with the County for a final plat application for Filing No. 3.

The items discussed in this report are preliminary in nature and final drainage calculations and design will be required in a future Final Drainage Report (FDR) as design development proceeds including delineation of sub-basins per roadway plan and profiles and overlot grading, design of public and private storm systems and outfalls, and final permanent control measure design. This PDR provides the drainage concept and guidance for future development of Flying Horse North Parcels 1-6 by analyzing the major basins, off-site stormwater runoff, water quality and full spectrum extended detention basins, and outfall locations to demonstrate compliance with drainage criteria and the Master Plan for the Flying Horse North subdivision. The extent of hydraulic analysis for this PDR is described further in its own section.

#### **Project Location and Description**

The Flying Horse North subdivision is in El Paso County. The larger subdivision development is bordered by Highway 83 to the west, Black Forest Road to the east, Cathedral Pines to the south, and High Forest Ranch to the north. The area contains approximately 1,473.6 acres within the whole Section 36, Township 11 South, Range 66 West of the Sixth Principal Meridian, and a portion of Section 30 and 31, Township 11 South, and Range 65 West of the Sixth Principal Meridian.

The Flying Horse North Parcels 1-6 area is the proposed PUD within the greater Flying Horse North subdivision that is approximately 747.27 acres that are currently unplatted parcels within the greater Flying Horse North subdivision. The subdivision is surrounded by the Flying Horse North Golf Course, the Cathedral Pines and Palmer Divide subdivisions to the south, residential subdivisions north of Hodgen Road such as Lesley Subdivision and High Plains Subdivision, and unplatted RR-5 zoned residential parcels to the northwest and east.

Review C1: A floodplain statement shall be provided indicating whether any portion of the development is in a designated floodplain as delineated on the current FEMA mapping.

Review C2: Unresolved. Please address the comment because a portion of site is within the floodplain.





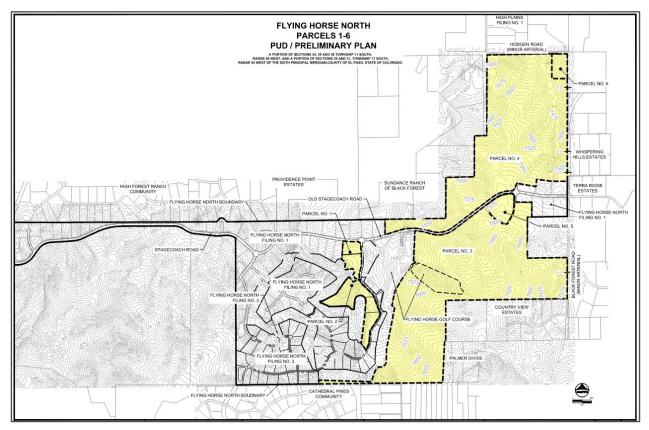


Figure 1: Site Map

A full sheet vicinity map is provided in Appendix A for a clear visual of Parcels 1 though 6 and adjacent developments.

This PDR will assess the drainage conditions for the 747.3 acres of onsite proposed PUD development, additional Flying Horse North acreage from other tributary filings and off-site tributary areas. The proposed PUD Preliminary Plan includes 796 proposed single-family residential units of various lot sizes. The PUD includes rural single-family estate lots of 2.5 and 5.0 acres, more dense single-family residential lots from 1/8-acre to 1/4-acre in size, commercial development, an 18-acre hotel and resort site with residential casitas, a 15-acre multifamily Flats area, open space and park areas, fitness center and a clubhouse.

The following table is a breakdown of the proposed land uses for the PUD Preliminary Plan Parcels 1-6, by Parcel.

Parcel No.	arcel No. Land Use(s)	
1	Commercial Golf Course Clubhouse	N/A
2	2 Commercial Hotel & Resort, Residential Casitas, Multi- Family Residential Flats	
3	3 Single-Family Residential	
4	Single-Family Residential	1.08
5	5 Community Recreation Center & Park	
6 Commercial		N/A

#### Table 1: Land Use by Parcel Number



The following table is a breakdown of the various proposed lot sizes for the single-family parcels within the PUD Preliminary Plan Parcels 1-6, by lot size:

Lot Size	Typical Minimum Dimensions	No. of Proposed Parcels	Total Area (ac.)
1/8-acre	75'x130'	123	45.2
1/4-acre	85'x130' ; 100'x130'	432 ; 94	130.33
1/3-acre	140'x130'	74	36.6
1/2-acre	160'x145'	43	51.4
1-acre	-	0	0.0
2.5-acre Rural	-	6	20.22
5.0-acre Rural	-	24	121.36
TOTALS		796	405.11

Table 2: Single-Family Lot Size Summary

Parcel 2 consists of the Commercial Hotel & Resort as well as the Casitas and multi-family Flats development areas. The anticipated number of hotel and casitas keys (units) is 225, and the preliminarily sited number of Flats is 50 units (6 units per building), totaling 275 units. This brings the total number of units for the entire PUD Preliminary Plan to 1,024. Excluding the hotel keys, the total amount of dwelling units comes out to 896, with 100 of those being responsible for the casitas and flats. The total weighted imperviousness of the PUD is approximately 27% for the fully developed conditions of all parcels.

### **Existing Conditions Description**

The existing ground cover consists of native grass and shrubbery with areas of barren pervious soil. The parcel 1 and 2 areas to the west where the proposed hotel resort, casitas, and flats are to be developed consist of the same native grass with areas of dense tree cover with pinyon pines, mostly in the areas adjacent to the golf course property. Slopes within this area generally range from 2 to 20 percent and flow west to east within East Cherry Creek Basin and east to west within Black Squirrel Creek Basin. These parcels are split by the Black Squirrel Creek and East Cherry Creek basin delineation line, with a majority of parcel 1 flowing east into East Cherry Creek. A majority of the area defined by parcel 2 flows west into Black Squirrel Creek. The remaining portion of parcel 2 that flows east into East Cherry Creek Basin is captured in an adjacent section of Allen Ranch Road that will be developed as F.H.N. Filing No. 3 is concurrently in review. The captured run-off is detained in F.H.N. Filing 3 pond A and ultimately released into an existing tertiary drainage swale located in a tract of the Flying Horse Golf Course. The natural vegetation has been documented by survey and aerial photography.

Parcels 3 through 6 are separated from the first two parcels by a stretch of golf course that runs south to north from the southern property border up to the existing Old Stagecoach Road. These parcels also consist of native grasses and shrubbery with areas of barren pervious soil. Slopes within this area generally range from 1 to 15 percent and generally flow from south to north. The natural vegetation has been documented by survey and aerial photography. Adjacent subdivisions in Palmer Divide and Country View Estates consist of 5 acre lots and make up a majority of the off-site flows. Flows from these off-site basins drain directly into existing drainage swales located in parcel no. 3. Black Forest Road which runs North to South along the eastern edge of parcels 3, 4, and 6, has 3 corrugated metal pipe culvert crossings that allow runoff to flow from east to west into parcel 4. Additionally, parcel no. 4 has 3 concrete culverts of varying size that



allow flows from parcel 3 to drain north into parcel 4, past the existing stretch of Old Stagecoach Road that separates the two aforementioned parcels.

All existing sub-basins within the site as well as existing off-site basins have associated design points, all of which are described in a further section. An existing drainage conditions map can be found within the appendix.

There are no existing major drainageways such as formal channels or water ways. There are existing natural tertiary swales and channels throughout the parcels that convey stormwater and are addressed in this PDR for the developed conditions. There are no existing stormwater facilities within the proposed PUD parcels. Adjacent filings that are developed such as the golf course, Filing No. 1, and the concurrent review of Filing No. 3 have public and private storm infrastructure such as storm sewer main, inlets, and detention basins. There are no existing irrigation facilities within the PUD parcels. There are existing irrigation facilities within the PUD parcels. There are existing irrigation facilities within the PUD parcels. There are existing irrigation facilities within the site are planned to be maintained to the maximum extent possible as a part of parkways and greenways with the development. These will continue to be used for conveyance of storm drainage flows.

The Franktown Parker Dam (080130) is located near the northwest corner of site. The dam is designated as a jurisdictional dam and has a low hazard class. It is located along East Cherry Creek. See Appendix A for characteristics and location of dam.

Drainageways of note including grass-lined swales and emergency overflow Tracts are described within this report with preliminary parameters to demonstrate compliance with swale design criteria and capacities.

The soils that existing within the PUD boundaries include the following:

- Brussett loam hydrologic soils group B.
- Elbeth sandy loam hydrologic soils group B.
- Kettle gravelly loamy sand hydrologic soils group B.
- Peyton sandy loam hydrologic soils group B.
- Peyton-Pring complex hydrologic soils group B.
- Pring coarse sandy loam hydrologic soils group B.

Per the NRCS web soil survey, the site is made up entirely of Type B soils. The ridge line between the Arkansas River and South Platte River Basins creates different soil environments for each. The portion of site that is within the Black Squirrel Drainage Basin, which includes Flying Horse Norse Filing No. 2 and No. 3, are predominately Elbeth sandy loam. The remaining filings are within the East Cherry Creek Basin which consists of Peyton sandy loam and Peyton-Pring complex. See Appendix A for the NRCS soil map.

The property for the PUD Parcels 1-6 do not consist of any existing utilities such as potable water main, wastewater main, natural gas facilities, or electric facilities. There are no encumbrances by utilities including platted easements that contain facilities for removal or relocation. Platted easements and other legal items are shown on the PUD Preliminary Plan set drawings.



## **II. Drainage Basins and Sub-Basins**

#### Drainage Basin Information

Flying Horse North is located within both the Black Squirrel Drainage Basin and East Cherry Creek Basin. Predominantly, the existing Filing No.1 and part of the proposed Filing No. 2 is located within the Black Squirrel Drainage Basin. This drainage basin encompasses 10.9 square miles of mostly forested area and generally slopes from east to west and outfalls into Monument Creek. Black Squirrel is a sub-basin of the Arkansas River. The remaining filings and part of Filing No. 2 is located within the East Cherry Creek Basin. There is not a current planning study of the drainage basin, but generally it slopes from southwest to northeast. The basin eventually flows into the South Platte River.

As the site generally lies at the top of each of the respective basins, minimal offsite flows are conveyed onto the site. The Black Squirrel Creek Drainage basin has no offsite flow come onto the site sans those flows generated as part of Filing 1 of F.H.N.. The development which is within the Black Squirrel Creek Drainage Basin is unchanged from the FDR shown in Filing 1.

#### **DBPS** Investigations

Flying Horse North is split by the Arkansas River Basin and South Platte Basin. Within each of those river basins, the site stretches across the Black Squirrel Basin and East Cherry Creek Drainage Basins.

The Black Squirrel Drainage Basin Planning Study (DBPS) Preliminary Design Report prepared by URS Corporation was reviewed to determine existing plans and constraints that would influence the design of the F.H.N. Development. The proposed plans for F.H.N. are in general conformance with the DBPS.

Flying Horse North Parcels 1-6 is located within a major portion of the East Cherry Creek Drainage Basin to the east of the larger F.H.N. subdivision and the west portion of the site is within the Black Squirrel Creek Drainage Basin. A MDDP developed by HR Green Development, LLC. that includes the proposed Parcels 1-6 area was approved by the County in September of 2022 and it is the intent of this PDR to follow the general drainage approach for this area where densities for the development will remain similar to the report.

For the portion of F.H.N. which lies within the East Cherry Creek Drainage Basin, a DBPS does not currently exist and the MDDP will comply with standard El Paso County regulations regarding drainage within this corridor.

#### **Compliance with DBPS**

This PDR is in general conformance with the guidelines outlined in the Black Squirrel DBPS and current drainage flows of the East Cherry Creek Basin. Flying Horse North will construct multiple full spectrum detention facilities to limit the effects of development and mimic natural flow patterns.

Existing downstream infrastructure is currently limited to the historic drainage channels and minimal downstream improvements exist. As such, the site follows the DBPS and restricts offsite flow rates to not exceed historic flow rates. The site's ultimate outfalls will generally be along the same historic tributaries. Although outfall rates will be at or below historic, the cumulative volume of runoff will increase and therefore downstream facilities may see an increase in the duration of flows. This may provide a net benefit to the downstream facilities by providing more water to assist with the sustenance of vegetation. However, it should be noted that increased volume may expedite potential erosion or channel movement.



## III. Hydrologic Analysis

#### **Existing Major Basin Descriptions**

**Design Point 1 (** $Q_5$ **=4.3 CFS, Q**<sub>100</sub>**=24.9 CFS)** represents flows from existing sub basin EX1. This basin is located within parcel 1 and is part of the East Cherry Creek Basin. Run-off from this sub-basin consists mostly of sheet flows that collect within a roadside ditch section on the west side of Allen Ranch Road. The swale flows from south to north to the round-about that intersects Allen Ranch Road and Old Stagecoach Road. From there the flows continue east within a roadside ditch section on the south side of Old Stagecoach Road where a 36" RCP culvert diverts flow north to detention pond 12 that has been developed as part of F.H.N. Filing No. 1.

**Design Point 2 (** $Q_5$ **=0.3 CFS, Q**<sub>100</sub>**=2.2 CFS)** represents flows from existing sub basin EX2. This basin is located within parcel 1 and is part of the Black Squirrel Creek Basin. Run-off from this sub-basin consists mostly of sheet flows that flow directly offsite into a tract within the F.H.N. Golf Course.

**Design Point 3 (** $Q_5$ **=0.6 CFS,**  $Q_{100}$ **=4.3 CFS)** represents flows from existing sub basin EX3. This basin is located within parcel 1 and is part of the Black Squirrel Creek Basin. Run-off from this sub-basin consists mostly of sheet flows that drain directly west offsite into a tract within the F.H.N. Golf Course.

**Design Point 4 (Q**<sub>5</sub>**=4.3 CFS, Q**<sub>100</sub>**=31.4 CFS)** represents flows from existing sub basin EX4. This basin is located within parcel 2 and is part of the Black Squirrel Creek Basin. Run-off from this sub-basin consists mostly of sheet flows that collect within an existing tertiary drainage swale. The swale flows east to west to the associated design point where the run-off drains directly off-site into tract K of the F.H.N. Golf Course.

**Design Point 5 (Q<sub>5</sub>=2.0 CFS, Q<sub>100</sub>=14.6 CFS)** represents flows from existing sub basin EX5. This basin is located within parcel 2 and is part of the Black Squirrel Creek Basin. Run-off from this sub-basin consist of sheet flows that drain west directly off-site into tract K of F.H.N. Golf Course.

**Design Point 5.1 (** $Q_5$ **= 1.8 CFS, Q**<sub>100</sub>**= 13.0 CFS)** represents flows from existing sub basin EX5.1. This basin is located within parcel 2 and is part of the East Cherry Creek Basin. Run-off from this sub-basin consists of sheet flows that drain east. Under the current conditions as of the date of this report, stormwater from this basin continues to drain east into the undeveloped portion of land that is a part of F.H.N. Filing No. 3 and eventually is captured within the **irrigation** pond located within tract L of the adjacent golf course. Under future conditions, once F.H.N. filing no. 3 has been constructed, flows from this basin will be collected within the EPC type A curb and gutter along Allen Ranch Road within F.H.N. Filing No. 3, of which is concurrently being reviewed. Flows collected within the existing curb and gutter are collected within 2 CDOT type R on-grade inlets sized 15' and 10'. Runoff not collected to F.H.N. Filing 3 pond A to be detained and released at historic rates into an existing tertiary drainage swale located within tract L of the Flying Horse Golf Course.

**Design Point 6 (** $Q_5$ **=3.9 CFS,**  $Q_{100}$ **=28.8 CFS)** represents flows from existing sub basin EX6. This basin is located within parcel 3 and is part of the East Cherry Creek Basin. Run-off from this sub-basin consists mostly of sheet flows that drain south off-site into Edmonds Subdivision.



**Design Point 7 (** $Q_5$ **=22.7 CFS, Q**<sub>100</sub>**=150.9 CFS)** represents flows from existing sub basin EX7 and off-site basin OS1. Basin OS1 flows into EX7 from the east at design point 26. This basin is located within parcel 3 and is part of the East Cherry Creek Basin. Run-off from this sub-basin consists mostly of sheet flows that collect within an existing tertiary drainage swale. The swale flows from east to west to the associated design point. This design point continues into off-site basin OS6, tract L of the Flying Horse Golf Course.

**Design Point 8 (Q<sub>5</sub>=23.2 CFS, Q<sub>100</sub>=144.5 CFS)** represents flows from existing sub basin EX8 and off-site basin OS2. Basin OS2 flows into EX8 from the east at design point 27. This basin is located within parcel 3 and is part of the East Cherry Creek Basin. Run-off from this sub-basin consists mostly of sheet flows that collect within an existing tertiary drainage swale. The swale flows from south-east to north-west, into off-site basin OS6, which represents tract L of the F.H.N. Golf Course.

**Design Point 9 (** $Q_5$ **=6.0 CFS, Q**<sub>100</sub>**=44.2 CFS)** represents flows from existing sub basin EX9. This basin is located within parcel 3 and is part of the East Cherry Creek Basin. Run-off from this sub-basin consists of sheet flows that drain north-west into off-site basin OS7 which represents tract M of the F.H.N. Golf Course.

**Design Point 10 (** $Q_5$ **=10.5 CFS, Q**<sub>100</sub>**=70.3 CFS)** represents flows from existing sub basin EX10 and offsite basin OS3. Basin OS3 flows into EX10 from the south at design point 28. This basin is located within parcel 3 and is part of the East Cherry Creek Basin. Run-off from this sub-basin consists mostly of sheet flows that collect within an existing tertiary drainage swale. The swale flows from south-east to north-west, into off-site basin OS7, which represents tract M of the F.H.N. Golf Course.

**Design Point 11 (** $Q_5$ **=42.5 CFS, Q**<sub>100</sub>**=235.3 CFS)** represents flows from existing sub basin EX11 and offsite basin OS4. Basin OS4 flows into EX11 from the south at design point 29. This basin is located within parcel 3 and is part of the East Cherry Creek Basin. Run-off from this sub-basin consists mostly of sheet flows that collect within an existing tertiary drainage swale. The swale flows from south to north-east to the associated design point.

**Design Point 12 (Q**<sub>5</sub>=6.8 CFS, Q<sub>100</sub>=49.6 CFS) represents flows from existing sub basin EX12. This basin is located within parcel 3 and is part of the East Cherry Creek Basin. Run-off from this sub-basin consists of sheet flows that drains east directly off site to the associated design point.

**Design Point 13 (** $Q_5$ **=5.4 CFS, Q**<sub>100</sub>**=39.8 CFS)** represents flows from existing sub basin EX13. This basin is located within a portion of parcel 3 and parcel 4 and is part of the East Cherry Creek Basin. Run-off from this sub-basin consists mostly of sheet flows that collect at an existing public storm culvert that runs from south to north through Old Stagecoach Road. Flows continue north into basin EX23.

**Design Point 14 (** $Q_5$ **=12.4 CFS, Q**<sub>100</sub>**=41.0 CFS)** represents flows from existing sub basin EX14 and a third of the runoff from basin OS9. This basin is located within a portion of parcel 3 and parcel 5 and is part of the East Cherry Creek Basin. Run-off from sub-basin EX14 consists of sheet flows that collect at an existing public storm culvert that runs from south to north through Old Stagecoach Road. Run-off from OS9 is led to the DP via roadside swales on Old Stagecoach Road. Flows continue north into basin EX21.

**Design Point 15 (** $Q_5$ **=30.7 CFS, Q**<sub>100</sub>**=175.3 CFS)** represents flows from existing sub basin EX15. This basin is located within parcel 3 and is part of the East Cherry Creek Basin. Run-off from sub-basin EX15 consists mostly of sheet flows that collect within an existing tertiary drainage swale. The swale flows from south to north to the associated design point where an existing public storm culvert that runs from south to north to the associated design point where an existing public storm culvert that runs from south to north to the associated design point where an existing public storm culvert that runs from south to north to the associated design point where an existing public storm culvert that runs from south to north to the associated design point where an existing public storm culvert that runs from south to north to the associated design point where an existing public storm culvert that runs from south to north to the associated design point where an existing public storm culvert that runs from south to north to the associated design point where an existing public storm culvert that runs from south to north to the associated design point where an existing public storm culvert that runs from south to north to the associated design point where an existing public storm culvert that runs from south to the associated design point where an existing public storm culvert that runs from south to public storm culvert that runs from s



north through Old Stagecoach Road carries flows to basin EX20. Run-off from basin OS9 is led to the DP via roadside swales on Old Stagecoach Road.

**Design Point 16 (** $Q_5$ **=2.3 CFS, Q**<sub>100</sub>**=16.6 CFS)** represents flows from existing sub basin EX16. This basin is located within parcel 3 and is part of the East Cherry Creek Basin. Run-off from this sub-basin consists of sheet flows that drain directly west into off-site basin OS7 which represents tract M of the F.H.N. Golf Course where an existing tertiary swale conveys flows north-west.

**Design Point 17 (** $Q_5$ **=4.4 CFS, Q**<sub>100</sub>**=32.3 CFS)** represents flows from existing sub basin EX17. This basin is located within parcel 3 and is part of the East Cherry Creek Basin. Run-off from this sub-basin consists of sheet flows that drain west directly into off-site basin OS6. Drainage from basin EX17 making its way into OS6 goes directly into the existing retention pond/water feature within off-site basin OS6.

**Design Point 18 (Q**<sub>5</sub>**=23.5 CFS, Q**<sub>100</sub>**=165.9 CFS)** represents run-off from off-site sub-basin OS7 in addition to run-off entering basin OS7 at design points 9, 10, and 16. This basin is located within parcel 3 and is part of the East Cherry Creek Basin. The associated sub-basin, OS7, is representative of tract M within the F.H.N. Golf Course and is actively in use. Within the tract there are several golf course features including fairways, greens, golf cart paths, a cart bridge over an existing natural drainage swale, and a retention pond. The retention pond has been designed with an overflow spillway at the west side of the pond/tract that releases water into the larger golf course water feature/retention pond that is in off-site sub-basin OS6 (tract L of F.H.N. Golf course). All drainage entering the tract will make its way down to the existing golf course retention pond via the existing tertiary drainage swale and will be released once the water surface elevation reaches a height that allows spillage to occur into the downstream pond in basin OS6.

**Design Point 19 (** $Q_5$ **=7.0 CFS, Q**<sub>100</sub>**=203.7 CFS)** represents flows from existing sub basins EX18 & EX19 as well as the release flow from the jurisdictional irrigation reservoir at design point 31. These basins are located within parcel 5 and are a part of the East Cherry Creek Basin. Run-off from this sub-basin consists mostly of sheet flows that are directed south-north and collect within an existing tertiary drainage swale. The minor (Q5=4.0 cfs) and major (182.0 cfs) flows that are released from the upstream irrigation reservoir are done so via a set of twin concrete box culverts (4'x10') that spill out into a 20' wide rock chute that leads down to a 2' deep plunge pool. Released flows are then directed into the existing natural drainage swale that flows off-site to the north.

**Design Point 20 (** $Q_5$ **= 34.9 CFS, Q**<sub>100</sub>**= 205.9 CFS)** represents flows from existing sub basin EX20 and design point 15. Design point 15 enters basin EX20 from the culvert outlet on the north side of Old Stagecoach Road. This basin is located within parcel 5 and is part of the East Cherry Creek Basin. Run-off from this sub-basin consists mostly of sheet flows that collect within an existing tertiary drainage swale. The swale flows from south to north to the associated design point which continues north off-site.

**Design Point 21 (** $Q_5$ **=26.6 CFS, Q**<sub>100</sub>**=144.9 CFS)** represents flows from existing sub basin EX21 and design point 14. Design point 14 enters basin EX21 from the culvert outlet on the north side of Old Stagecoach Road. This basin is located within parcel 5 and is part of the East Cherry Creek Basin. Run-off from this sub-basin consists mostly of sheet flows that collect within an existing tertiary drainage swale. The swale flows from south to north to the associated design point where the flows will continue north off-site.



**Design Point 22 (Q**<sub>5</sub>=6.7 CFS, Q<sub>100</sub>=49.3 CFS) represents flows from existing sub basin EX22. This basin is located within parcel 4 and is part of the East Cherry Creek Basin. Run-off from this sub-basin consists of sheet flows that drain north-west directly off-site.

**Design Point 23 (** $Q_5$ **=65.9 CFS, Q**<sub>100</sub>**=443.4 CFS)** represents flows from existing sub basin EX23 and design points 13 and 32. Design point 13 represents flows from basin EX13 and makes its way into basin EX23 via a culvert that runs under the eastern most round-about on Old Stagecoach Road. Design point 32 represent basin OS5 which enters the basin EX23 via a natural drainage swale from the south of basin EX23. Basin EX23 is located within parcel 4, contains the entirety of parcel 6, and is part of the East Cherry Creek Basin. Run-off from this sub-basin consists mostly of sheet flows that collect within multiple existing tertiary drainage swales. The swales flow from south to north to the associated design point and continue off-site.

**Design Point 24 (** $Q_5$ **=3.3 CFS, Q**<sub>100</sub>**=24.0 CFS)** represents flows from existing sub basin EX24. This basin is located within parcel 4 and is part of the East Cherry Creek Basin. Run-off from this sub-basin consists mostly of sheet flows that collect within an existing tertiary drainage swale. The swale flows from south to north to the associated design point where the flows exit the site.

**Design Point 25 (** $Q_5$ **=11.2 CFS, Q**<sub>100</sub>**=82.1 CFS)** represents flows from existing sub basin EX25. This basin is located within parcel 4 and is part of the East Cherry Creek Basin. Run-off from this sub-basin consists mostly of sheet flows that drain north-west directly off-site towards Hodgen Road. The swale flows from south to north to the associated design point.

**Design Point 26 (** $Q_5$ **=7.9 CFS, Q**<sub>100</sub>**=42.7 CFS)** represents flows from existing sub basin OS1. This basin is located just east of basin EX7 and is part of the East Cherry Creek Basin. Run-off from this sub-basin consists mostly of sheet flows that drain west towards the associated design point and enter the site via basin EX7. Flows that enter the site are then naturally collected within an existing tertiary drainage swale and continue to flow west.

**Design Point 27 (** $Q_5$ **=13.5 CFS, Q**<sub>100</sub>**=73.4 CFS)** represents flows from existing sub basin OS2. This basin is located just east of existing sub-basins EX7 and EX8 and is part of the East Cherry Creek Basin. This off-site basin contains a part of the Palmer Divide subdivision which is a cul-de-sac containing 5 acre lots. Run-off from this sub-basin consists mostly of sheet flows that flow west and collect within an existing tertiary drainage swale that begins at the associated design point. The flows continue west, combining with run-off from basin EX8.

**Design Point 28 (Q**<sub>5</sub>**=8.2 CFS, Q**<sub>100</sub>**=53.9 CFS)** represents flows from existing sub basin OS3. This basin is located east of basin EX9 and south of EX10 and is part of the East Cherry Creek Basin. Part of this basin lies within the Country View Estates subdivisions which consists of 5 acre lots. Run-off from this subbasin consists of sheet flows that collect within an existing tertiary drainage swale. The swale flows from south to north to the associated design point where it then enters the proposed site.

**Design Point 29 (Q**<sub>5</sub>**=28.8 CFS, Q**<sub>100</sub>**=134.6 CFS)** represents flows from existing sub basin OS4. This basin is located directly south of basin EX11 and is part of the East Cherry Creek Basin. The off-site basin is comprised entirely of the Country View Estates Subdivision which contains 5 acre lots. Run-off from this sub-basin consists mostly of sheet flows that collect within an existing tertiary drainage swale. The swale flows from south to north to the associated design point where is enters the site through basin EX11.



**Design Point 30** ( $Q_5$ =3.8 CFS,  $Q_{100}$ =4.4 CFS) represents flows from existing off-site sub-basin OS8. This basin is located directly east of basin EX5.1 and is part of the East Cherry Creek Basin. This basin contains existing storm infrastructure that had been constructed during the F.H.N. Filing 3 development. Infrastructure includes 2 on-grade storm inlets, 2 sump inlets, and a full spectrum detention pond. The detention pond releases flows at historic rates which are reflected in the design points flow rates. Detained stormwater is released from the pond into the existing tertiary drainage swale located in off-site basin OS7.

**Design Point 31 (** $Q_5$ **=102.7 CFS, Q**<sub>100</sub>**=624.8 CFS)** represents flows from existing sub basin OS6 as well as run-off from design points 7, 8, 17, 18, and 30. Basin OS6 is representative of a majority of tract L within F.H.N. Golf Course and is part of the East Cherry Creek Basin. This tract contains several golf course features as well as the irrigation reservoir. Flows entering this reservoir are retained and released at historic rates as shown with the flows associated with this design point. Stormwater exiting the reservoir does so through a small jurisdictional dam where twin concrete box culverts sized 4' x 10' allow water to pass under the roadway (Old Stagecoach Road) and into a 20' wide rock chute. The rock chute then releases water into an existing natural drainage swale that continues north, off-site. Calculated flows for this design point have been overridden by design flows from Classic Consulting's approved JD design report to provide a more accurate depiction of existing flows exiting the reservoir.

**Design Point 32 (** $Q_5$ **=16.2 CFS, Q**<sub>100</sub>**=78.3 CFS)** represents flows from existing off-site sub-basin OS5. This basin is located directly east of basin EX13 and is part of the East Cherry Creek Basin. This basin contains a portion of F.H.N. Filing 1 development which includes several lots and a culvert that allows flows to pass underneath Old Stagecoach Road. Flows exiting the subbasin do so at the northern end of the subbasin which enter an existing natural drainage swale and flow into basin EX23.

There are offsite drainage basins that are conveyed onto or through the site on the southwestern portion. There are also offsite basins shown that are central to the greater PUD that represent the existing F.H.N. Golf Course areas. These basins are generally conveyed through the development via natural drainage ways or overland sheet flow. The proposed PUD is to either continue conveyance of these offsite basins are described below in detail for comparison to developed conditions in a later section.

- **Basin OS1** is approximately 19.0 acres and is located offsite to the south of parcel no. 3, adjacent and upstream to Basin EX7. The offsite basin was analyzed in the MDDP as Basin A and categorized as all open space with native weeds/grasses. In this report, basin OS1 has been analyzed as majority existing 5-acre residential lots with a portion of the basin remaining as open space. Existing developments within this basin are from the Edmonds Subdivision and Palmer Divide subdivision. Both subdivisions consist largely of 5 acre lots that did not require detention at their time of approval. Flows entering the proposed site are routed via overland sheet flow and eventually collect within existing drainage swales located on-site. The basin has a composite imperviousness of 5.2% and the 5-year minor storm event and the 100-year major storm event are 7.7 cfs and 40.8 cfs, respectively.
- **Basin OS2** is approximately 36.4 acres and is located offsite to the southeast of parcel no. 3, adjacent and upstream to Basin EX8. The offsite basin was analyzed in the MDDP as Basin C and categorized as all open space with native weeds/grasses. In this report, basin OS2 has been analyzed as majority existing 5 acre residential with a portion of the basin remaining as open space. Existing developments within this basin are a part of the adjacent Palmer Divide subdivision. Run-



off coming from the mentioned subdivision did not require any detention at the time of approval. This off-site stormwater makes it way on-site via overland sheet flow that collects within an existing drainage swale, beginning at the property line. The basin has a composite imperviousness of 5.1% and the runoff rates for the 5-year minor storm event and the 100-year major storm event are 13.1 cfs and 69.9 cfs, respectively.

- Basin OS3 is approximately 25.25 acres and is located offsite to the southeast of parcel no. 3, adjacent and upstream to Basin EX10. The offsite basin was analyzed in the MDDP as Basin F and categorized as all open space with native weeds/grasses. In this report, basin OS3 has been analyzed as majority existing open space with native weeds/grasses and a portion of the basin now categorized as existing 5 acre residential. Existing developments within this basin are a part of the adjacent Country View Estates subdivision. Run-off entering the proposed site from the mentioned subdivision did not require any detention at the time of approval. This off-site stormwater makes it way on-site via overland sheet flow that collects within an existing drainage swale, beginning at the property line. The basin has a composite imperviousness of 3.0% and the runoff rates for the 5-year minor storm event and the 100-year major storm event are 8.2 cfs and 53.9 cfs, respectively.
- Basin OS4 is approximately 72.3 acres and is located offsite to the southeast of parcel no. 3, adjacent and upstream to Basin EX11. The offsite basin was analyzed in the MDDP as Basin Q and categorized as all open space with native weeds/grasses. In this report, basin OS4 has been analyzed as entirely existing 5 acre residential. Existing developments within this basin are a part of the adjacent Country View Estates subdivision. Run-off entering the proposed site from the mentioned subdivision did not require any detention at the time of approval. This off-site stormwater makes it way on-site via overland sheet flow that collects within an existing 18" HDPE culvert to cross under a gravel driveway that borders the north side of Country View Estates. The flows exit the culvert and enter an existing natural drainage swale that travels into parcel no. 3 of the proposed site. The basin has a composite imperviousness of 7.0% and the runoff rates for the 5-year minor storm event and the 100-year major storm event are 28.8 cfs and 134.6 cfs, respectively.
- **Basin OS5** is approximately 41.2 acres and is located offsite to the east of parcel no. 3 and south of parcel no. 4, adjacent and upstream to basin EX23. The offsite basin was analyzed in the MDDP as Basin V and categorized as mostly 5-acre residential with the rest of the area as open space, and this categorization remains in this report. Existing developments within this basin are 5-acre residential that have been developed as a part of F.H.N. Filing No. 1. Flows from the south of this subbasin are sheet flows that pass through a culvert that runs underneath Old Stagecoach Road and continue north into an existing drainage swale. This swale continues north and enters parcel no. 4, basin EX23, from the southern edge. The basin has a composite imperviousness of 6.5% and the runoff rates for the 5-year minor storm event and the 100-year major storm event are 16.2 cfs and 78.3 cfs, respectively.
- Basin OS6 is approximately 83.6 acres and is located west of parcel no. 3. The offsite basin was analyzed in the MDDP as part of Basin E and categorized as all open space which remains as the categorization within this report. Existing developments within this basin are a part of the adjacent F.H.N. North Golf Course and consist of golf course infrastructure/features. Run-off coming from and making its way into the golf course tract collect within the existing irrigation reservoir. Water released from the reservoir is done so through the small jurisdiction dam via twin 4'x10' concrete box culverts that allows the released waters to pass underneath Old Stagecoach Road, into a rock



chute, and finally into an existing natural drainage swale that flows north off-site. The basin has a composite imperviousness of 2.0% and the discharge rates, from the reservoir, for the 5-year minor storm event and the 100-year major storm event are 12.0 cfs and 124.0 cfs, respectively.

- **Basin OS7** is approximately 20.1 acres and is located within the western half of parcel no. 3, adjacent and downstream to Basins EX9, EX10, and EX16. The offsite basin was analyzed in the MDDP as Basin G and categorized as all open space with native weeds/grasses and remains as this categorization within this report. Existing developments within this basin are a part of the adjacent F.H.N. Golf Course and consist of golf course infrastructure/features. Run-off coming from and making its way into the golf course tract collect within a retention pond/water feature. Water released from the pond is directed into the downstream irrigation reservoir. The basin has a composite imperviousness of 2.0% and the runoff rates for the 5-year minor storm event and the 100-year major storm event are 4.7 cfs and 34.9 cfs, respectively.
- **Basin OS8** is approximately 8.0 acres and is located east of parcel no. 2, adjacent and downstream to Basin EX5.1. The offsite basin was analyzed in the MDDP as a part of Basin E and categorized as all open space with native weeds/grasses. This basin is a part of F.H.N. Filing No. 3 and contains a part of Allen Ranch Road as well as an existing full spectrum detention pond. Run-off coming from and making its way into this basin, from basin EX5.1, is collected with the 4 type-R inlets along Allen Ranch Road that direct the stormwater into the detention pond which is then released at historic rates into the existing adjacent F.H.N. Golf Course tract. The basin has a composite imperviousness of 58.1% and the runoff rates for the 5-year minor storm event and the 100-year major storm event are 3.8 cfs and 4.4 cfs, respectively.
- Basin OS9 is approximately 9.4 acres and is located in between parcels 3 and 4. The offsite basin was analyzed in the MDDP as a part of several basins, but now represents the area of Old Stagecoach Road that splits F.H.N. parcels 3 and 4. Because of this, this basin is categorized as mostly paved surface. This was developed as a part of F.H.N. Filing No. 1 and several pieces of stormwater infrastructure, all of which are culverts, allow flow from the south to cross underneath the road and continue north. Runoff from Old Stagecoach Road is captured in roadside swales and discharged into the culverts at design points 14 and 15, with the remaining flows discharging into the irrigation reservoir in offsite basin OS6. The basin has a c There are no exemptions for

and the runoff rates for the 5-year minor storm event and the 1 cfs and 50.6 cfs, respectively.

There are no exemptions for detention in the criteria. Please revise the statement and see comments on the drainage plan.

#### **Proposed Major Basin Descriptions**

This PDR discusses the hydrology of the larger basins that correspondence to the hydrology of the larger basins that correspondence to the developed and disturbed basin areas. Any basin areas that drain directly offsite will consist of grass buffers that provide 100 percent runoff reduction and/or are exempt from detention requirements. An exhibit showing what areas throughout all parcels of the development that will be exempt from detention requirements will be shown in appendix F. All basins that are stated to have 100% run-off reduction from water quality are supported with UDBMP spreadsheet calculations that can be found in appendix D. These calculations represent "worst case scenarios" for percent imperviousness of 2.5 acres lots and larger and ensure that these large lots still receive runoff reduction. The major basins yield overall minor and major storm event runoff rates calculated by the Rational Method that are to be captured in the public roadways with public storm sewer inlets and routed to their respective detention facility via public and private storm pipes. A





combination of inlet sump locations, on-grade inlets, and grass lined swales are to be utilized for capture and conveyance. Design details such as specified inlet types and sizes, pipe sizing and hydraulic grade line analysis, and roadway capacities are to be presented in a future FDR in which sub-basins are delineated and additional design points where runoff is captured within major basins are presented. The PDR delineates the major basin throughout the development and provides preliminary sizing for proposed permanent control measures only Below are the major basins within the PUD ributary area size, location, land use makeup, downstream design point and permanent control measure, as well as minor and major storr Review C2: Unresolvedtidt appears that table 41d PDR level of design is more clearly explaine section 6.d does not compare historical funofff with mentioned for each basin. Emergency over further section of the report.

- Basin A is approximately 74.1 acres located to the south of the PUD within Parcel No. 3 and is east of the existing F.H.N. Golf Course. The basin consists of ½-acre sized single-family residential lots with a network of paved roadways within the 60' local urban rights-of-way. The basin contains a large area of open space tract including Detention Pond A, Design Point 3. The basin has a composite imperviousness of 15.0% and the runoff rates for the 5-year minor storm event and the 100-year major storm event are 38.9 cfs and 161.6 cfs, respectively.
- Basin A1 is approximately 12.6 acres located to the south of the PUD within Parcel No. 3 and the east onsite area downstream of offsite basin OS1. The basin consists of 5.0-acre estate single-family residential lots that include mostly pervious lawn area, and the basin includes an existing tertiary channel that is intended to be undisturbed and flow through the PUD via a public culvert pipe crossing at **Design Point 4.** This design point will also convey the upstream Basin OS2, and ultimately drain to the existing Golf Course Trrigation Pond, **Design Point 6**, where the basin will receive detention. Refer to table 4 in section 6.d of this report for supporting calculations that prove that the irrigation pond will not receive more major stormwater flow than historical conditions. The basin has a composite imperviousness of 7.0% and the runoff rates for the 5-year minor storm event and the 100-year major storm event are 6.0 cfs and 29.0 cfs, respectively.
- **Basin A2** is approximately 6.5 acres located to the south of the PUD within Parcel No. 3 and is east of the existing Flying Horse North Golf Course. The basin consists of the rear of ½-acre sized single-family residential lots that include mostly pervious lawn area and the majority of the basin includes an existing tertiary channel that is intended to be undisturbed and flow through the PUD via a public culvert pipe crossing at **Design Point 5** conveying the upstream Basin OS2, ultimately to the existing F.H.N. Golf Course Irrigation Pond, **Design Point 6**, where basin A2 will receive storage detention. Refer to table 4 in section 6.d of this report for supporting calculations that prove that the irrigation pond will not receive more major stormwater flow than historical conditions. The basin has a composite imperviousness of 13.1% and the runoff rates for the 5-year minor storm event and the 100-year major storm event are 3.4 cfs and 15.3 cfs, respectively.
- **Basin B** is approximately 32.7 acres and is located north of Basin A, within the south half of the PUD in Parcel No. 3 and is east of the existing golf course. The basin consists of 1/2-acre and 1/3-acre sized single-family residential lots with a network of paved roadways within the 60' local urban rights-of-way. The basin contains an area of open space tract to its south and tract area to the north for Detention Pond B, **Design Point 7**. The basin has a composite imperviousness of 24.1% and



the runoff rates for the 5-year minor storm event and the 100-year major storm event are 24.6 cfs and 86.1 cfs, respectively.

- Basin C is approximately 121.0 acres and is located northeast of Basin OS7 and west of Basin D, within the south half and central areas of the PUD in Parcel No. 3. The basin consists of a mix of land uses consisting of ½-acre and ¼ -acre sized single-family residential lots with paved roadways within the 60' local urban rights-of-way and the extension of Old Stagecoach Road. The basin contains a large area of open space tract central to the basin including designated Park Space. This open space area consists of existing tertiary swales to remain undisturbed. These swales convey stormwater runoff to an existing public 48" RCP culvert pipe (Design Point 10) that crosses Old Stagecoach Road that will now outfall to Detention Pond C, Design Point 11. Proposed flows leading to the existing RCP culvert will be analyzed further in the FDR. The basin has a composite imperviousness of 31.6% and the runoff rates for the 5-year minor storm event and the 100-year major storm event are 81.4 cfs and 251.4 cfs, respectively.
- Basin D is approximately 86.2 acres and is located east of Basin C within the southeast of the PUD in Parcel No. 3. The basin consists of ¼ -acre, 1/8-acre (0.2-acres), and 5-acre estate single-family residential lots with paved roadways within the 60' local urban rights-of-way. The basin contains open space at the filing boundary to the east which includes Detention Pond D, Design Point 13. The basin has a composite imperviousness of 26.8% and the runoff rates for the 5-year minor storm event and the 100-year major storm event are 54.8 cfs and 177.1 cfs, respectively.
- **Basin E** is approximately 52.4 acres and is located northeast of Basin C and north of Basin D and is within the central north half of the of the PUD and is a part of Parcel No. 3 and No. 5 which is the dedicated future amenities and recreation/gym facility parcel. The basin consists of ¼ -acre single-family residential lots with paved roadways within the 60' local urban rights-of-way and the extension of Old Stagecoach Road. Parcel No. 5 is assumed at 75% future commercial land use area. The basin drains due northwest and is tributary to Detention Pond E, **Design Point 15**. Within the basin is a culvert pipe that is to cross Old Stagecoach Road, **Design Point 14**. Sub-basins within Basin E are to be delineated in a future FDR to size the culvert pipe crossing. The future commercial amenities center area within Parcel No. 5 is assumed to drain directly to the public storm system that outfalls to Detention Pond E. The basin has a composite imperviousness of 43.7% and the runoff rates for the 5-year minor storm event and the 100-year major storm event are 67.7 cfs and 171.0 cfs, respectively.
- Basin F is a large area of the northern portion of the PUD totaling approximately 197.5 acres and is located northeast of Basin E and east of Basin G and extends to the north and northeast filing boundary within Parcel No. 4 and Parcel No. 6 which is the commercial lot at the northeast of the PUD. The basin consists of a mix of 1/8-acre, ¼ -acre and 2.5-acre single-family residential lots with paved roadways within the 60' local urban rights-of-way and a short extension of Old Stagecoach Road to a roundabout connection to the local and collector roadways. The basin contains a large area of open space tract area to the east of the filing as a buffer from surrounding subdivision. This tract consists of existing natural tertiary channels and swales that drain due north. Portions of these tertiary swales will be re-graded to ensure proper bury depth of public sanitary sewer crossings from the Parcel's south residential blocks to the north area. There are interior tract areas of open space and a designated Park Area to the north central portion of the basin. The very northeast corner of the basin and filing contains a future commercial development parcel of

Review C1: Please address whether the development has or will obtain the necessary downstream easements to accept the developed flows of this basin as the development of these lots will increase historic flows and they are not being mitigated as required. Analysis of the downstream will be required with the FDR.

Review C2: Unresolved. It appears that section 6.c does not include information about the effect on downstream from storm water release points at basin H. Additionally, Appendix D shows that 100% of the WQCV is captured but does not address detention of flows from this area. Please identify how the increase in flows from these basins will be mitigated. rth Phase 2 Parcels 1-6 ninary Drainage Report Project No.: 211030

ention Pond F, off rates for the and 366.3 cfs,

g, west of Basin re single-family

residential lots with paved roadways within the 60' local urban rights-of-way and the connection to Hodgen Road. The basin contains a large area of open space tract at the north boundary of the site which contains Detention Pond G, **Design Point 18**. Additionally, the tract provides an emergency spillway overland path to the pond. The basin drains due north and northwest to the proposed pond. The basin has a composite imperviousness of 16.4% and the runoff rates for the 5-year minor storm event and the 100-year major storm event are 16.4 cfs and 68.4 cfs, respectively.

- Basin H is approximately 74.0 acres and is located onsite at the east filing boundary on the north half of the filing, adjacent to Basins C, E, F and G within Parcel No. 4. The basin consists of 5-acre rural single-family residential estate lots to act as buffers to the urban areas of the development. The developed areas within this basin are large estate lots that have sufficient undeveloped open space downstream for grass buffers that provide 100 percent runoff reduction and therefore do not have to be captured and detained onsite, as per the PBMP applicability item part II.E, which classifies lots greater than 2.5 acres with less than 10% imperviousness. Additionally, run-off reduction supporting calculations can be found in appendix D and an exhibit can be found in appendix F showing areas that do not require detention. The basin has a composite imperviousness of 7.0% and the runoff rates for the 5-year minor storm event and the 100-year major storm event are 37.6 cfs and 180.4 cfs, respectively. Design Point 19 represents the respective downstream outfall areas at the filing border with offsite adjacent properties for the rural lots that drain directly offsite. See section 6.c of this report for more information about the effect on downstream properties from stormwater release points.
- **Basin I** is approximately 7.1 acres and is in the northwest portion of Parcel No. 3, adjacent to Filing No. 1, west of Basin C and north of Basin OS7. The basin consists of ½-acre and 1/3-acre residential lots and a Tract at the northern cul-de-sac. The basin drains to a sump inlet (**Design Point 20**) at the northern cul-de-sac which is to outfall to the existing golf course Irrigation Pond/Reservoir (**Design Point 6**) matching the historical drainage pattern of this basin. Historical flows from this basin are lower than the proposed flows to the irrigation pond. However, total overall flowrates leading to the irrigation pond are to be reduced in proposed conditions. Because the total flows leading the existing irrigation pond will be lower for the proposed conditions as compared to historical values, the flows exiting basin I can be discharged into the existing irrigation pond. Refer to section 6.d of this report for supporting calculations. The basin has a composite imperviousness of 26.4% and the runoff rates for the 5-year minor storm event and the 100-year major storm event are 6.1 cfs and 20.7 cfs, respectively.
- **Basin J** is approximately 15.8 acres and is in the west area of the PUD in Parcel No. 1, adjacent to F.H.N. Filing No. 1. The basin consists of the proposed permanent golf course clubhouse development with parking lot. The basin drains due north toward Old Stagecoach Road and west into Pond J, **Design Point 21**. The basin has a composite imperviousness of 86.1% which



conservatively includes an assumed 95% imperviousness for most of the developed commercial parcel and 1.5 acre of pond open space. The runoff rates for the 5-year minor storm event and the 100-year major storm event are 59.8 cfs and 112.4 cfs, respectively.

- **Basin K** is approximately 18.0 acres and is in the west commercial and flats area of Parcel No. 2, adjacent to Filing Nos. 1 and 3. The basin consists of the hotel and resort complex with paved parking areas and various amenities buildings in addition to the main hotel and event center building as well as a casitas residential development with paved access roadways. The basin drains due west to proposed Detention Pond K, **Design Point 22** which outfalls due west through the existing golf course and F.H.N. Filing No. 1. The basin has a composite imperviousness of 86.0% which conservatively includes an assumed 95% imperviousness for most of the developed commercial and residential parcel and 1.75 acre of pond open space area. The runoff rates for the 5-year minor storm event and the 100-year major storm event are 64.4 cfs and 121.2 cfs, respectively.
- Basin L is approximately 7.1 acres and is in the west commercial and flats area in Parcel No. 2, adjacent to Filing Nos. 1 and 3. The basin consists of the Flats which includes the buildings, access drives, and landscaping that are conceptual at this point. Assumed imperviousness for this basin is 40% open space landscaped area and 60% roof and pavement. The basin drains due west through the existing F.H.N. Golf Course and is tributary to existing Pond 8 in Filing No. 1. In the final design of this basin, it will be demonstrated that Pond 8 has sufficient capacity for the contributing flow and that the pond will continue to function as intended and without maintenance deficiencies. This tributary basin was discussed in the 2018 Classic Consulting PDR/FDR and the 2023 F.H.N. Filing No. 3 FDR by HR Green Development, LLC. The basin has a composite imperviousness of 57.8% and the runoff rates for the 5-year minor storm event and the 100-year major storm event are 19.0 cfs and 41.1 cfs, respectively. Design Point 23 represents the basin's west outfall location at the golf course from the flats area. The adjacent development to the east is a part of Filing No. 3 and is described in the Filing No. 3 FDR to be detained in Pond A of Filing No. 3 located adjacent to the golf course.

#### plan

Basin M is approximately 5.0 acres and is in the west commercial and flats area in Parcel No. 2, adjacent to Filing Nos. 1 and 3. The basin consists of the Flats wike view @2 the buildings, access drives, and landscaping that are conceptual at this point. Assurb in resolved is the basin is 40% open space landscaped area and 60% roof and pavertabel promote imperviousness of 57.8% and the runoff rates for the 5-year miproprose deditionate to F.H.N. Filing No. 3, which is being reviewed concurrently, into a section of Allen Ranch Road that contains several pieces of drainage infrastructure including 4 CDOT Type-R inlets. Stormwater that exits the basin is captured within those inlets and then piped down to full spectrum detention pond A, a part of F.H.N. Filing No. 3, which will release flows at historic rates. Flows released from the pond eventually end up in the irrigation reservoir that has been developed as part of F.H.N. Filing No. 1. This portion of Allen Ranch Road and the detention pond have been assessed for fully developed conditions of the Flats area as part of the F.H.N. Filing No. 3 FDR.

The following are the Offsite Basins that the upstream tributary areas that drain to and through the proposed PUD that will require collection and conveyance to downstream permanent control measures or routing around or through the development. The offsite basins are described as undeveloped open space



consisting of their native grasses and weeds with sparse areas of barren pervious soils per the NRCS Soils Maps included in the Appendix. Any future development of these upstream adjacent properties are to require onsite water quality and detention and any stormwater release to and through the Flying Horse North subdivision will be restricted to be at or less than historical rates and via overland sheet flow. There are also offsite basins that represent the existing F.H.N. Golf Course areas, as relevant to this PUD.

- Basin OS1 is approximately 19.0 acres and is located offsite to the southeast of the filing, adjacent and upstream to Basin A. The offsite basin was analyzed in the MDDP as Basin A and remains as its existing undeveloped open space with native grasses and weeds. There are no developments within this major offsite basin and any future development of the area will require onsite water quality and detention. The offsite basin is tributary to onsite Detention Pond A / Design Point 3. Detention Pond A outfalls to the existing golf course at or below historical stormwater runoff rates and drains to the existing Golf Course Irrigation Pond (Design Point 6). The offsite basin is routed via overland sheet flow to the roadway in the PUD and is to cross and outfall into undisturbed open space in Basin A via public culvert pipes sited at Design Points 1 and 2. The basin is to be split into two sub-basins to assess each culvert pipe design in a future FDR. The basin has a composite imperviousness of 2.0% and the runoff rates for the 5-year minor storm event and the 100-year major storm event are 5.6 cfs and 41.3 cfs, respectively.
- Basin OS2 is approximately 36.4 acres and is adjacent and upstream of Basin A1. The offsite basin was analyzed in the MDDP as Basin B and remains as its existing undeveloped open space with native grasses and weeds. There are no developments within this major offsite portion of the basin and there is a small area of 5-acre development within the Site where the existing tertiary channel crossing through the development. Any future development of the off-site area will require onsite water quality and detention to release at historical rates as it passes through the F.H.N. PUD. The offsite basin is tributary to the existing Irrigation Pond (Design Point 6) that was built as a part of the F.H.N. Golf Course development. The offsite basin is routed via overland sheet flow and is conveyed through the PUD via public culvert pipes (Design Point 4) through the PUD roadways and through the existing tertiary channel in Basin A2. The basin has a composite imperviousness of 2.0% and the runoff rates for the 5-year minor storm event and the 100-year major storm event are 9.2 cfs and 67.9 cfs, respectively.
- Basin OS3 is approximately 25.3 acres and is located offsite to the southeast of the filing, adjacent and upstream to Basin BB. The offsite basin was analyzed in the MDDP as Basin C and remains as its existing undeveloped open space with native grasses and weeds. There are no developments within this major offsite basin and any future development of the area will require onsite water quality and detention. The offsite basin overland sheet flows to the roadway at the south portion of Basin BB and C and is conveyed directly to the open space existing F.H.N. Golf Course area in Basin BB via a public culvert pipe (Design Point 8) and is directed offsite, ultimately to the existing Irrigation Pond at the Golf Course (Design Point 6). The basin has a composite imperviousness of 2.0% and the runoff rates for the 5-year minor storm event and the 100-year major storm event are 6.8 cfs and 49.9 cfs, respectively.
- **Basin OS4** is approximately 72.3 acres and is located offsite to the southeast of the filing, adjacent and upstream to Basin D. The offsite basin was analyzed in the MDDP as Basin D and remains as its existing undeveloped open space with native grasses and weeds. There are no developments within this major offsite basin and any future development of the area will require onsite water





quality and detention. The basin drains onto the PUD site via overland flow until it is channelized in a tertiary swale at **Design Point** 12. The offsite basin is tributary to onsite Detention Pond D / **Design Point 13**. The offsite basin is routed via overland sheet flow and is channelized through onsite Basin F via existing natural channels. The basin has a composite imperviousness of 2.0% and the runoff rates for the 5-year minor storm event and the 100-year major storm event are 18.3 cfs and 134.5 cfs, respectively.

- Basin OS5 is approximately 41.2 acres and is located offsite central east boundary of the filing, adjacent to Basin E and upstream to Basin F. The offsite basin was analyzed in the MDDP as Basins V2, U, W, and X3 and remains as existing 2.5 acre lots and partion open space with native weeds and grasses. The existing developments within this site will receive detention as a part of the development of parcel no. 4 of this PUD. The offsite basin is tributary to onsite Detention Pond F / Design Point 17. The offsite basin is routed via overland sheet flow and is channelized through onsite Basin F via existing natural channels on the east side of parcel no. 4, entering the Site at Design Point 16 where proposed estate lots are sited. It is expected that driveway culvert pipes for these estate lots will be required to convey the upstream off-site stormwater runoff. The basin has a composite imperviousness of 2.0% and the runoff rates for the 5-year minor storm event and the 100-year major storm event are 15.9 cfs and 78.8 cfs, respectively.
- Basin OS6 is approximately 95.0 acres and represents the existing F.H.N. Golf Course area between the west Parcels 1 and 2, Filing No. 1, and Filing No. 3 and the east PUD residential areas for Parcels 3-6. The existing golf course area includes areas of pervious grassed surfaces for the golf course, and rear of residential lots of various lot sizes that drain through the course. This basin includes the existing Irrigation Pond/Reservoir, **Design Point 6** that is the ultimate drainage control measure for many basins and pond outfalls within the PUD. The offsite basin was analyzed in the MDDP as Basin E and most of the basin remains as the existing golf course development with the addition of some rear of developed PUD lots adjacent to Basins A, B, I, and Filing No. 1 and 3 estate lots. The basin has been reduced in size from the MDDP as the PUD development of Basins A, B, and I will capture stormwater runoff where historic conditions have areas within these basins that flow directly to the Irrigation Reservoir. In cases where the back half of a proposed lot will be directed to flow into basin OS6, the lot will be provided detention via the irrigation pond within basin OS6. The offsite basin is routed via overland sheet flow and is channelized through grass-lined swales along its east edge adjacent to Basins A and B. The basin has a composite imperviousness of 4.6% and the runoff rates for the 5-year minor storm event and the 100-year major storm event are 23.0 cfs and 143.5 cfs, respectively.
- Basin OS7 is approximately 28.2 acres and is located north of Basin B and southwest of Basin C, within the south half of the PUD in Parcel No. 3 and is comprised of existing golf course area that is not to be disturbed. The basin includes some onsite area (7.6 ac.) of developed single-family residential lots which are the rear half of the lots backing up to the existing golf course. The basin flows directly offsite at Design Point 9 and has 100 percent runoff reduction via the grass buffer in the existing Golf Course and ultimately drains to the existing Irrigation Pond/Reservoir (Design Point 6). The basin has a composite imperviousness of 8.2% and the runoff rates for the 5-year minor storm event and the 100-year major storm event are 10.6 cfs and 57.7 cfs, respectively. The basin is all open space and has 100 percent water quality runoff reduction via a grass buffer and is directed offsite.



• **Basin OS8** is approximately 8.0 acres and is located east of parcel no. 2, adjacent and downstream to Basin M. The offsite basin was analyzed in the MDDP as a part of Basin E and categorized as all open space with native weeds/grasses. This basin is a part of F.H.N. Filing No. 3 and contains a part of Allen Ranch Road as well as an existing full spectrum detention pond. Run-off coming from and making its way into this basin, from basin M, is collected with the 4 type-R inlets along Allen Ranch Road that direct the stormwater into the detention pond which is then released at historic rates into the existing adjacent F.H.N. Golf Course tract. The basin has a composite imperviousness of 58.1% and the runoff rates for the 5-year minor storm event and the 100-year major storm event are 3.8 cfs and 4.4 cfs, respectively.

The above-mentioned basins are large planning area basins and as the Final Drainage Report is developed for the filing, additional analysis and calculations will be required to assess proposed storm sewer conveyance, roadway and inlet capacities, capacities and routing of natural and proposed channels and swales, and detention pond infrastructure.

## IV. Drainage Design Criteria

#### a. Development Criteria Reference

The following criteria manuals and reports were used as reference material for the preparation of this PDR and its hydrologic and hydraulic design parameters.

- NOAA Atlas 14
- NRCS Soil Survey for El Paso County Area, Colorado
- El Paso County Assessor Property Records
- El Paso County Drainage Criteria Manual, 2014
- City of Colorado Springs Drainage Criteria Manual, May 2014
- Urban Storm Drainage Criteria Manual, Urban Drainage Flood Control District, January 2018

The following reports were used as reference documents for surrounding developments and the major drainage basin that the proposed PUD lies within.

- Preliminary Drainage Report for Flying Horse North Preliminary Plan and Final Drainage Report for Flying Horse North Filing No. 1, Classic Consulting Engineers and Surveyors, November 2017
- Flying Horse North Filing No. 3 Final Drainage Report prepared by HR Green Development, LLC.
   latest revision August 2023
- Flying Horse North Master Development Drainage Plan, HR Green Development, LLC., September 2022
- Flying Horse North Irrigation Reservoir Embankment Design Report, Classic Consulting Engineers and Surveyors, August 2018
- Black Squirrel Drainage Basin Planning Study (DBPS), URS Consultants, January 1989

#### b. Hydrologic Criteria

Design rainfall was determined utilizing Table 6-2 from the City of Colorado Springs Drainage Criteria Manual to determine the 5-year and 100-year rainfall values for the 1-hour events. The 1-hour rainfall depths are 1.5 and 2.52 in/hr respectively. The Rational Method is used for stormwater runoff calculations.

Composite percent impervious calculations were completed for each subbasin based on the density of lots and can be found in Appendix B. The El Paso County Drainage Criteria Manual Table 5-1 was used for



reference when correlating land use to percent impervious values and located in Appendix F. Impervious values for 5-Acre Rural Lots, 2.5-Acre Rural Lots, 1/2-acre, 1/3-acre, 1/4-acre, 1/8-acre single family residential lots and Commercial Lots have impervious values of 7%, 11%, 25%, 30%, 40%, 65%, 95%, respectively. Open space, lawn, and golf course areas have 2% impervious values. Rainfall intensity and peak runoff calculations are provided in Appendix B.

Basins are routed to their respective design points and detention ponds as shown on the Hydrology Maps in Appendix F. Calculations performed in the Mile High Flood District BMP and Detention spreadsheets are used to determine pond storage sizing and detention discharge release rates at the preliminary design level.

#### c. Applicable Criteria and Standards

Per the DBPS and El Paso County Criteria Manual, flows from the proposed site will be limited to historic flows to maintain the stability of the existing channels within the drainage basins. The master plan follows the Drainage Criteria Manual for El Paso County which refers to the City of Colorado Springs Drainage Criteria Manuals as amended. Criteria within the County and City manuals refer to the Mile High Flood District manuals, particularly for extended detention basin design and runoff reduction calculations which are utilized in this report.

### V. Hydraulic Analysis

#### **Major Drainageways**

There are no major drainage ways that exist within the PUD development; however, natural tertiary tributaries are within the site currently and function to convey flows to unnamed tributaries of the East Cherry Creek and Black Squirrel Creek. Open spaces including tracts and park areas have natural drainageways that will remain undisturbed and are assessed within this report for capacity and stabilization. This PDR does not include hydraulic analysis for the storm systems to be designed as a part a future FDR, however, there are preliminary design points with storm pipes such as culvert crossings, tract drainageways, and other conveyances that are included in the hydraulic analysis of this PDR.

Hydraulic analysis is provided in this PDR for the following:

- Locations where upstream off-site basins will cross roadways in the development and culverts are sited.
- Natural channels both onsite and offsite that will either be undisturbed or graded into an engineered channel.
- Locations where existing culvert storm infrastructure will be used to convey newly proposed flows underneath Old Stagecoach Road.

## VI. Drainage Facility Design

#### a. General Concept

For the PUD Preliminary Plan to be in compliance with off-site runoff requirements, the developed conditions require conveyance of upstream off-site areas through or around the developed areas. The off-site tributary basins are to be captured and conveyed within the major basins of the developed PUD parcels and routed to downstream design points that are full spectrum detention basins. This PDR includes preliminary hydraulic design for the conveyance of off-site stormwater runoff but does not include detailed



analysis of proposed storm systems within the major basins. It is anticipated that developed rights-of-way will include public stormwater infrastructure including inlets that will capture stormwater runoff and convey the runoff downstream via storm main to their respective detention basins. Off-site areas that drain directly onto the developed areas are to be captured either by culvert pipes or drainage swales and conveyed to storm sewer systems that ultimately outfall to detention basins.

The content included in this PDR to demonstrate drainage facility design at the preliminary level include hydrology design calculations including the Rational Method tabulations for determining major basin composite coefficients, imperviousness, time of concentration, rainfall intensity, and peak runoff rates for minor and major storm events; MHFD Detention and BMP tabulations for basin stage-storage and detention discharge rates; tables and figures from the El Paso County Drainage Criteria Manual for Land Use Coefficients and Percent Imperviousness; tables and figures from the City of Colorado Springs Drainage Criteria Manuals Volumes 1 and 2 for roadway stormwater capacity; and hydrology maps for the predevelopment and developed conditions of the PUD to show major basin delineations, acreage of tributary areas, and design point routing.

#### b. Specific Details

This PDR includes Appendix F hydrology/drainage maps showing the major basin tributary areas associated with the PUD development for both the pre-developed and developed conditions. The appendix calculations and drainage maps include tables summarizing the stormwater peak runoff rates fo the minor (5-year) and major (100-year) events. The maps and calculations include off-site tributary areas entering the PUD parcels and the outfall locations for pond outlet pipes and any basins with direct runoff exiting the PUD parcels to off-site downstream locations.

The approach to accommodate drainage impacts on existing or proposed improvements includes the delineation of major basins at the PDR level to determine the required location and sizing of full spectrum detention basins to provide water quality and detention and release stormwater downstream at or below historical rates. The general concept for future delineated sub-basins and a storm system design to be presented in a future FDR includes public and private storm inlets and pipes that will collect and convey off-site and on-site stormwater runoff within roadways that ultimately outfall to detention ponds. A future FDR will include storm system design based on roadway capacity, inlet capacity, and hydraulic grade lines. The PDR summarizes the major basin areas and provides preliminary calculations for each major basin and their downstream control measures.

The proposed water quality and full spectrum detention basins are preliminarily sized in this PDR for the purpose of siting, and the outlet structures and orifice plate design are to be designed for release rates at or below historical rates in a future FDR. Pond designs are also preliminarily shown on the developed conditions drainage map including the required stormwater infrastructure for extended detention basins including concrete forebays, concrete trickle channels, concrete micropools and outlet structures with orifice plates and/or outlet pipe restrictor plates, emergency spillways with weirs, maintenance pathways, outlet pipes.

The drainage impact of site constraints such as streets, utilities, existing and proposed structures are mitigated by following typical sections for right-of-way improvements per the County Engineering Criteria Manual. The majority of the PUD parcels include urban local and urban collector roadways with standard alignments for storm sewer, water main, and sanitary sewer. A future FDR is to include sited storm sewer



alignments and inlet locations with consideration for vertical clearances of utility crossings. There are no existing structures or utilities currently in conflict with the preliminary storm design.

There are no known environmental features or issues applicable to the drainage facility design of the PUD.

Maintenance access is required by the County for the perpetual access and maintenance of stormwater facilities. The PDR level of design presented in this report and its maps shows that each detention facility will require a standard maintenance pathway from the public rights-of-way to access all pond infrastructure including forebays and outlet structures. Access to drainage facilities are to include a pathway from the public rights-of-way or a pathway within an access easement.

#### c. Detention Pond Preliminary Design Summary

The following table summarizes the full spectrum detention ponds sited for the PUD Preliminary Plan. The ponds are designed for WQCV, EURV, and 100-year storage volumes. Preliminary design has been done for the outlet structures to release at or below historical rates.

Pond Name	Preliminary Bottom Elev. (ft)	Preliminary Top of Pond Elev. (ft)	WQCV (ac-ft)	EURV (ac-ft)	100-Year (ac-ft)	Total Required Volume (ac-ft)	Total Preliminary Design Volume * (ac-ft)
Pond A	7562.00	7572.00	0.618	0.476	2.699	3.793	10.504
Pond B	7552.00	7558.00	0.359	0.436	1.110	1.904	2.780
Pond C	7526.00	7534.00	1.577	2.364	4.361	8.302	12.062
Pond D	7530.00	7538.00	1.264	1.127	4.863	7.254	9.082
Pond E	7550.00	7557.00	0.828	1.594	2.032	4.454	6.316
Pond F	7438.00	7446.00	1.768	1.484	7.158	10.409	15.680
Pond G	7442.00	7447.00	0.227	0.210	0.849	1.287	3.045
Pond J	7583.00	7591.00	0.487	1.031	0.751	2.270	2.985
Pond K	7501.00	7511.00	0.554	1.174	0.856	2.584	3.436

Table	3:	Preliminary	Pond	Design	Information
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\* Total basin volumes include the required 1' of freeboard to top of pond.

The following descriptions of each detention pond are provided to describe outfall locations, emergency spillway routing, and ultimate outfall locations downstream. All pond embankments have been designed to be no greater than 10 feet in height, therefore there are no proposed jurisdictional dams.

Pond outlet locations have been strategically selected and designed to reduce the impact on downstream properties/conditions. Additionally, pond outfalls will have rip-rap to provide energy dissipation which will be analyzed in the future FDR. In the subsequent pond de This should be OS8 locations will be described and This should be DP3 is will be explained.

**Pond A (Design Point 1)** provides water quality and full-spectrum detention for tributary basins A and OS1. This extended detention basin outfalls due west into Basin OB6, the existing F.H.N. Golf Course, under the adjacent western roadway. The golf course has an existing grass-lined swale that drains due north to its existing Irrigation Pond/Reservoir that was designed and constructed as a part of Filing No. 1. Analysis of this existing pond is included in this report to demonstrate compliance for upstream stormwater detention and ponds in-series. The emergency spillway of this pond is to consist of a rip-rap weir designed for the peak inflow to the pond and is to be directed west toward the Tract located across the street so that emergency stormwater overflow is ultimately directed toward the golf course. Detained stormwater is released in Tract E which then allows flows to enter into an existing swale located in tract L of the Flying



Horse Golf Course. Flows travel to the existing irrigation pond and ultimately travel north to be captured in a roadside swale along Hodgen Road.

**Pond B (Design Point 7)** provides water quality and full-spectrum detention for tributary basin B. This extended detention basin outfalls due north into Basin OS6, the existing F.H.N. Golf Course, under the existing maintenance and golf car path to its north. The golf course has an existing grass-lined swale that drains due north to its existing Irrigation Pond/Reservoir that was designed and constructed as a part of Filing No. 1. Analysis of this existing pond is included in this report to demonstrate compliance for upstream stormwater detention and ponds in-series. The emergency spillway of this pond is to consist of a rip-rap weir designed for the peak inflow to the pond and is to be directed northwest toward the existing golf course swale. Detained stormwater is released in Tract M of the Flying Horse Golf Course and enters an existing swale which travels to Tract L of the golf course. Flows travel to the existing irrigation pond and ultimately travel north to be captured in a roadside swale along Hodgen Road.

**Pond C (Design Point 11)** provides water quality and full-spectrum detention for tributary basin C. This extended detention basin outfalls due north directly offsite. The emergency spillway of this pond is to consist of a rip-rap weir designed for the peak inflow to the pond and is to be directed northwest, directly offsite. Detained stormwater is released into the headwaters of an existing swale directly north-west of the pond. Flows travel north, off-site, and ultimately are captured in a roadside swale along Hodgen Road.

**Pond D (Design Point 13)** provides water quality and full-spectrum detention for tributary basin D. This extended detention basin outfalls due north directly offsite. The emergency spillway of this pond consists of a rip-rap weir designed for the peak inflow to the pond and is to be directed northwest, directly offsite. Detained stormwater is released east into a roadside swale along Black Forest Road. Flows ultimately travel north to an unnamed tributary.

**Pond E (Design Point 15)** provides water quality and full-spectrum detention for tributary basin E which includes the future amenities center with gym/recreation building(s) that has assumed imperviousness described in the proposed basins section. This extended detention basin outfalls due northwest directly offsite into an existing swale that travels north and ultimately is collected in a roadside swale along Hodgen Road. The emergency spillway of this pond is to consist of a rip-rap weir designed for the peak inflow to the pond and is to be directed northwest, directly offsite.

**Pond F (Design Point 17)** provides water quality and full-spectrum detention for tributary basin F and OS5. This extended detention basin outfalls due north toward Hodgens Road where an existing culvert pipe crosses to the north side of the roadway and is directed offsite. The emergency spillway of this pond is to consist of a rip-rap weir designed for the peak inflow to the pond and is to be directed north, following the same drainage pattern as the outlet pipe.

**Pond G (Design Point 15)** provides water quality and full-spectrum detention for tributary basin G. This extended detention basin outfalls due north toward Hodgens Road where an existing culvert pipe crosses to the north side of the roadway and is directed offsite. The emergency spillway of this pond is to consist of a rip-rap weir designed for the peak inflow to the pond and is to be directed north, following the same drainage pattern as the outlet pipe.



**Pond J (Design Point 18)** provides water quality and full-spectrum detention for tributary basin J which is Parcel No. 1, the future commercial golf course club house with parking. Assumed imperviousness and land uses for the parcel are described in the proposed basins section. This extended detention basin outfalls due north to the roadside swale of Old Stagecoach Road which drains due west to an existing culvert pipe crosses to the north side of the roadway and is directed to an existing detention pond that was constructed as a part of Filing No. 1. This pond was designed to detain the runoff from this Parcel as 2.5 acre lots. On-site detention of the commercial development will reduce the runoff form this area to historic rates. The emergency spillway of this pond is to consist of a rip-rap weir designed for the peak inflow to the pond and is to be directed northwest, following the same drainage pattern as the outlet pipe.

**Pond K (Design Point 19)** provides water quality and full-spectrum detention for tributary basin K which is part of Parcel No. 2 area that is for the future commercial hotel and resort with parking and residential casitas development. Assumed imperviousness and land uses for the parcel are described in the proposed basins section. This extended detention basin outfalls due west directly to Filing No. 1. The downstream existing Pond 8, which was constructed as a part of Filing No. 1, accounted for runoff from this basin as existing undeveloped area. In the final design of this pond, it will be demonstrated that Pond 8 has sufficient capacity for the contributing flow being released from this pond, and that Pond 8 will continue to function as intended and without maintenance deficiencies. On-site detention of the commercial development will reduce the runoff from this area to historic rates, matching that of the assumed runoff rates for Filing No. 1. The emergency spillway of this pond is to consist of a rip-rap weir designed for the peak inflow to the pond and is to be directed west, following the same drainage pattern as the outlet pipe.

d. Existing Tract L Irrigation Pond & Reservoir, Filing No. 1



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Per the Flying Horse North Irrigation Reservoir Embankment Design Report, the Existing Tract L Irrigation Pond and Reservoir acts as an irrigation reservoir and detention pond for the golf course and surrounding tributary area as seen in Figure 2.



Figure 2: Existing Tract L Irrigation Pond and Reservoir

The full proposed drainage map is provided in Appendix F. The Flying Horse North Irrigation Design Report can be found in Appendix E.

The development of Parcels 1-6 results in an increase in land density from 2 acre lots to ½ acre residential lots upstream of the irrigation pond. To reduce runoff to historic rates, detention ponds will be added upstream of the reservoir. The table below shows the existing and proposed runoff rates of each basin tributary to the irrigation pond through Tract L.

Table 4: Preliminary	Existing	and	Proposed	Runoff	Rates
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	Existing Condi	tions	Proposed Conditions <sup>1</sup>			
Design Point	Contributing Basins	0 100 1001		Contributing Basins	100 Year Runoff Rate (cfs)	
17	EX17	32.3	25 <sup>1</sup>	OS8	10.5	
18	OS5, DP9, 16, 10	165.9	3 <sup>2</sup>	A, OS1	43.1	
8	EX8 & DP27	144.5	5	A2, A1, OS2	117.4	
7	EX7 & DP26	150.9	7 <sup>3</sup>	В	22.8	
30	OS8	4.4	9	OS7, OS3	124.7	
	OS6	110.0	20	I OS6	15.7 161.12	
	Total	608	Тс	otal <sup>4</sup>	459.3	





All proposed runoff rates are from the CUHP model
 DP 25 100-year runoff rate is FHN Filing No. 3 Pond A's peak discharge rate
 DP3 100-year runoff rate is proposed Pond A's peak discharge rate
 DP7 100-year runoff rate is proposed Pond B's discharge rate
 d from total inflow into irritation pond per SWMM and accounts for timing of peak runoff rates from

4. Value derived from total inflow into irrigation pond per SWMM and accounts for timing of peak runoff rates from basins.

The proposed conditions were modeled in EPA SWMM to ensure the ponds in series meet compliance with Senate Bill 15-212 for drain times and evaluate the storage capacity and outlet structure of the existing irrigation pond. Per the Flying Horse North Irrigation Reservoir Embankment Report, the existing irrigation pond was designed to hold an inflow runoff rate of 609 cfs. The peak has been reduced to 460 cfs. The table below shows the existing and proposed parameters of the irrigation pond.

	North Irrigation Reservoir Design Report Design Values	Proposed Irrigation Pond Design Values
Total Design Inflows (cfs)	609	460
100-Year WSE (ft)	7534.23	7534.98
Peak Discharge (ft)	182	206

Table 5: Irrigation Pond Design Value Comparison

Please note that different hydrologic and hydraulic methods were used when modeling the pond. The FHN Irrigation Reservoir Embankment Design Report uses the SCS Curve Number Method and Pond Pack to design the pond. This differs from the CUHP/ EPA SWMM Modeling approach and will result in different values. CUHP utilizes 1-hr rainfall depths whereas Pond Pack uses 24-hr rainfall depths.

Per discussions with El Paso County, EPA SWMM is an acceptable method to model the pond. The lower peak but higher volume of runoff is a result of the use of the different rainfall depths and methodology. Furthermore, the County has agreed that retrofits will not be required.

Per the model, all pond drain times do not exceed 120 hours and are within compliance for events greater than the 5-year storms outlined in Senate Bill 15-212.

All SWMM results and supporting information is located in Appendix C.

### VII. 4-Step Process

In accordance with the Engineering Criteria Manual I.7.2.A and DCM V2, this site has implemented the four-step process to minimize adverse impacts of urbanization. The four-step process includes reducing runoff volumes, stabilizing drainageways, treating the water quality capture volume, and considering the need for Industrial Commercial BMPs. The PDR stage of design for the 4-step process is conceptual in nature and is to be more specifically described within a future FDR when storm system routing at the subbasin level is available.

Step 1 – Reducing Runoff Volumes: The development of the project site includes a variety of land uses including open and vegetated areas interspersed to help disconnect imperious areas and reduce runoff volumes. Single-family residential lots are standardized to include side yard swales that roof runoff drain to via downspouts. Runoff reduction is provided within side yard swales for each lot.





Step 2 – Stabilize Drainageways: Altered drainage ways will be designed in a manner that provides water quality benefits through infiltration and the removal of pollutants via phytoremediation. Vegetation will also be selected to stabilize the drainage ways by reducing the velocity of flows and decreasing any scour. Should the final drainage ways require, grade control structures may be implemented to further reduce flow velocities and protect against erosion. These improvements will help stabilize drainageways.

Step 3 – Provide WQCV: Runoff from this development is treated through capture and slow release of the WQCV via detention ponds that are designed per current El Paso County DCM V2.

Step 4 – Consider the need for Industrial and Commercial BMP's: A site specific storm water quality and erosion control plan and narrative will be prepared with subsequent land use approvals prepared in conjunction with the report prior to any construction. Site specific temporary source control BMPs as well as permanent BMPs are detailed in this plan and narrative. Guidelines detailed in the El Paso DCM V2 4.2 pertaining to the covering and storage handline and spill containment and control shall be followed as necessary.

### VIII. Drawings

Please refer to the appendices for vicinity maps and drainage basin maps.

The drainage maps identify drainage flows entering and leaving the development and general drainage patterns. The maps identify any major construction such as existing and proposed detention facilities, culverts, and preliminarily sited storm sewer infrastructure. The Drainage plans delineate all subbasins and proposed initial and major facilities as well as a provide a summary of all initial and major flow rates at design points. All floodplains effecting the site are shown.

### IX. Summary

Flying Horse North is a large master planned community consisting of various densities of dwelling units to include single family homes, multifamily homes, parks, institutional sites, and commercial areas. Due to development, increased runoff will occur. To mitigate downstream impacts, full spectrum detention facilities will be built to reduce the runoff rate to be at or below historic levels. These detention facilities will provide water quality enhancements to account for the increased urbanization of the upstream catchment areas. The ponds are preliminarily sized to ensure that the 5-year and 100-year release rates are equal to or less than the historic rates.

Additional analysis will be required and completed to review the hydraulics of the proposed major drainage channels and sub-basins to be included in a future submittal of an FDR. The proposed design, as described in this report, is not anticipated to cause any adverse impact to downstream properties. Implementation of the four-step process above and any additional measures that are within reason to disconnect impervious areas and increase infiltration should be pursued within a future FDR.

This PDR includes major basin analysis and provides descriptions and calculations for best management practices for stormwater collection and conveyance at the preliminary design stage.

Review C1: Please address the floodplain at the Northwest corner of the site and the requirement to demonstrate baseflood elevations(CLOMR/LOMR) with the final plat application. Review C2: Unresolved. Please address the above comment. Verify with FEMA as the

section within the development may be Zone AE.



### X. References

Mile High Flood District Urban Drainage Criteria Manuals, Volumes 1-3 NOAA Atlas 14 NRCS Soil Survey for El Paso County Area, Colorado FEMA FIRM 08041C0305G and FIRM 08041C0315G (eff. 12/7/2018) El Paso County Assessor Property Records El Paso County – Drainage Criteria Manual, 2014 City of Colorado Springs – Drainage Criteria Manual, May 2014 Urban Storm Drainage Criteria Manual, Urban Drainage Flood Control District, January 2018 Preliminary Drainage Report for Flying Horse North Preliminary Plan and Final Drainage Report for Flying Horse North Filing No. 1, Classic Consulting Engineers and Surveyors, November 2017 Flying Horse North Filing No. 3 Final Drainage Report prepared by HR Green Development, LLC. – latest revision August 2023 Flying Horse North Master Development Drainage Plan, HR Green Development, LLC., September 2022

Flying Horse North Irrigation Reservoir Embankment Design Report, Classic Consulting Engineers and Surveyors, August 2018

Black Squirrel Drainage Basin Planning Study (DBPS), URS Consultants, January 1989

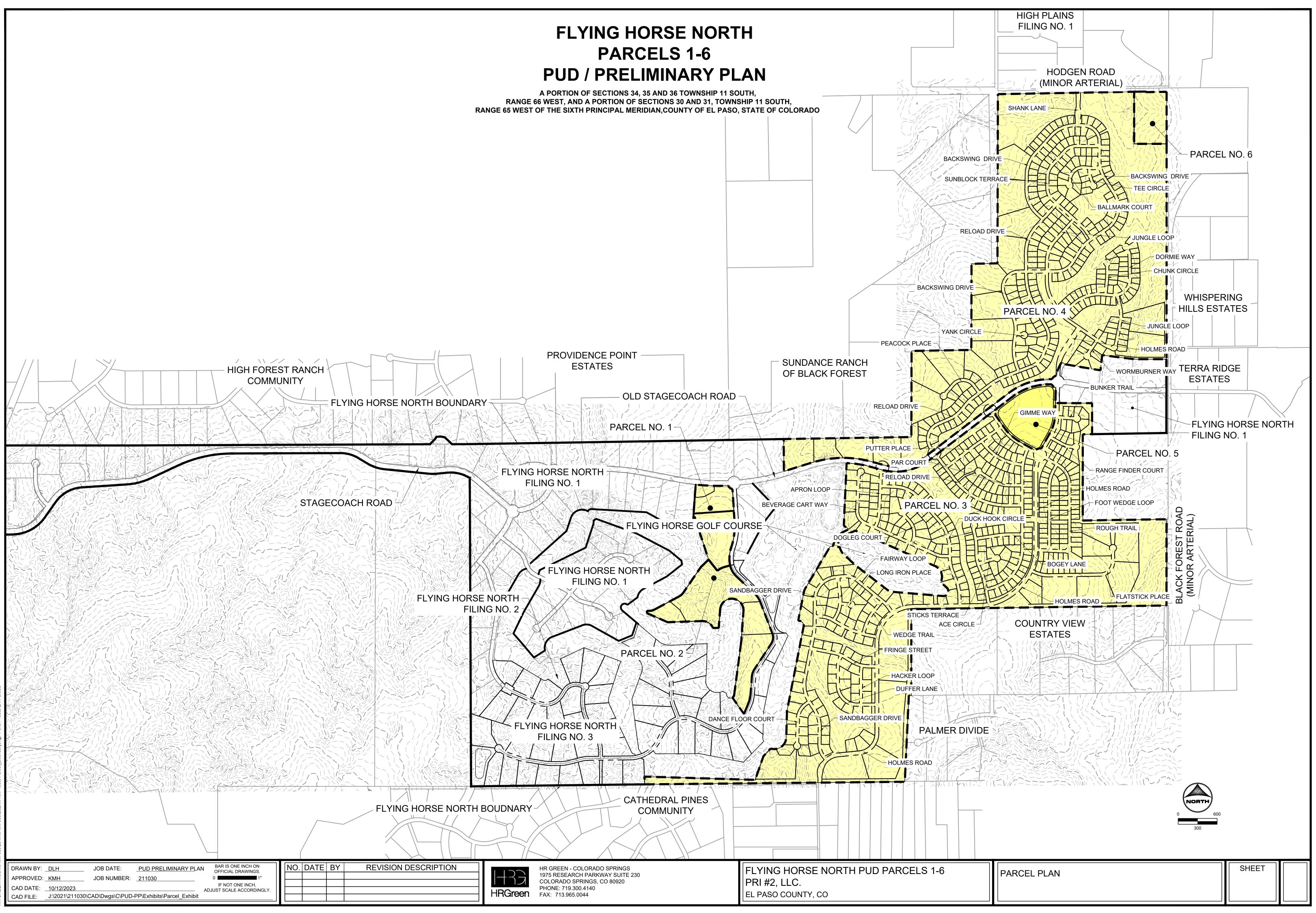


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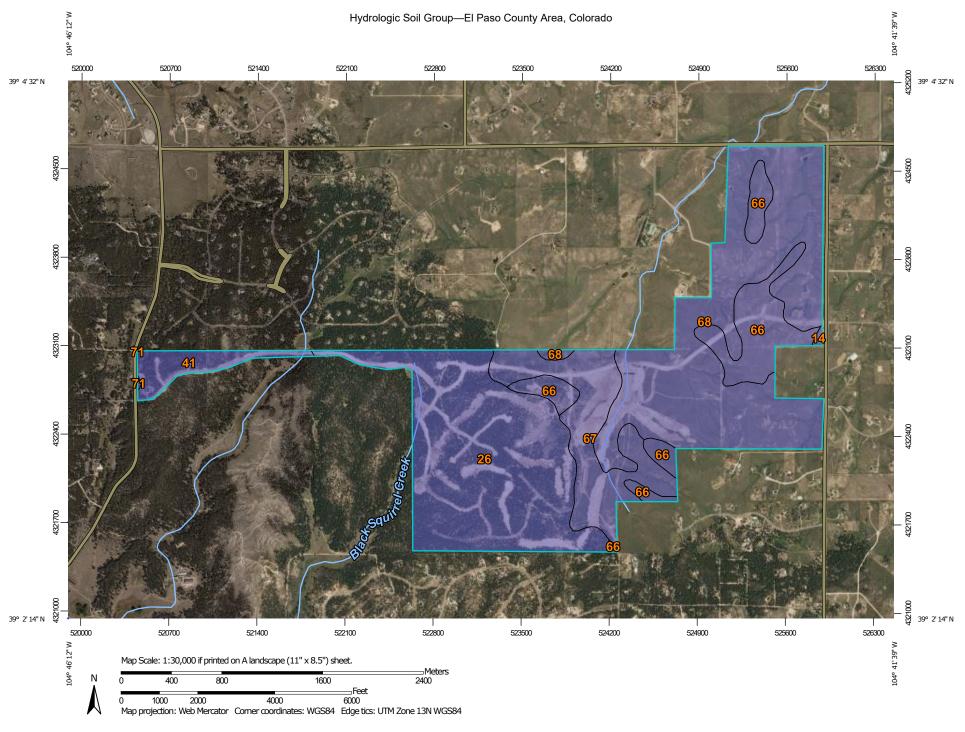
Appendix A:

Vicinity Map, NRCS Soils Map, and FEMA Floodplain Map

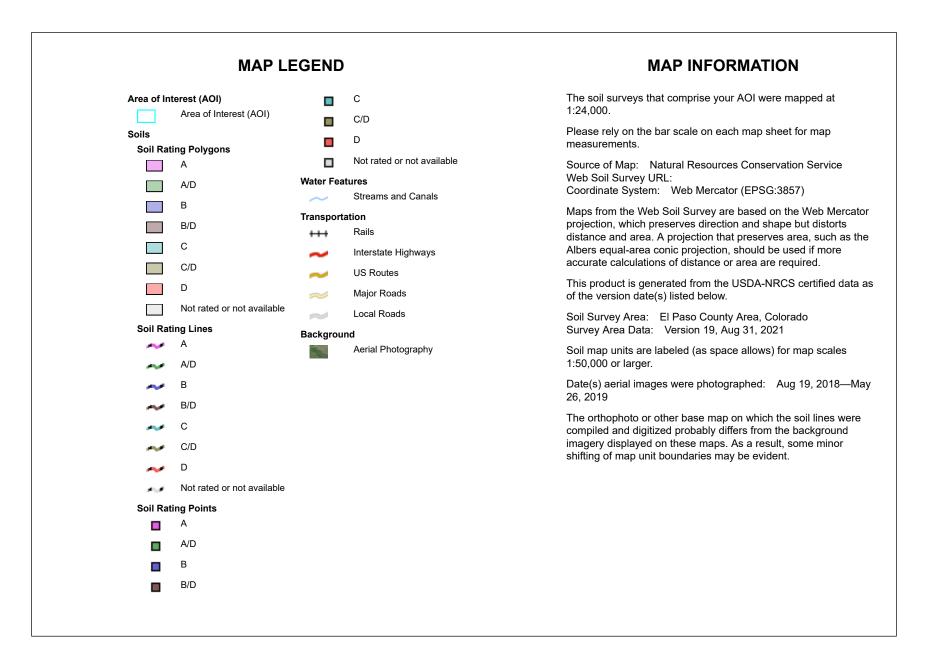




l Xrefs: xc-row-030.201; xc-row-030.202; xv-row-1030; Parcel\_Boundary; xgt-1-dh01-1C



USDA Natural Resources Conservation Service Web Soil Survey National Cooperative Soil Survey



# Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
14	Brussett loam, 1 to 3 percent slopes	В	1.9	0.1%
26	Elbeth sandy loam, 8 to 15 percent slopes	В	474.2	33.7%
41	Kettle gravelly loamy sand, 8 to 40 percent slopes	В	53.4	3.8%
66	Peyton sandy loam, 1 to 5 percent slopes	В	160.9	11.4%
67	Peyton sandy loam, 5 to 9 percent slopes	В	182.8	13.0%
68	Peyton-Pring complex, 3 to 8 percent slopes	В	533.4	37.9%
71	Pring coarse sandy loam, 3 to 8 percent slopes	В	0.6	0.0%
Totals for Area of Inter	rest		1,407.3	100.0%

## Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

## **Rating Options**

Aggregation Method: Dominant Condition Component Percent Cutoff: None Specified Tie-break Rule: Higher

#### NOTES TO USERS

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Certain areas not in Special Flood Hazard Areas may be protected by **flood contro** structures. Refer to section 2.4 "Flood Protection Measures" of the Flood Insurano Study report for information on flood control structures for this jurisdiction.

The projection used in the preparation of this map was Universal Transverse Mercario (UTM) zone 13. The horizontal datum was HADB3, GR580 spherol. production of PTMB for adjacent spiraticitors may result in sight positional differences in map features across juridiciton boundaries. These differences do not affect the accuracy of this FIRM.

Flood elevations on this map are referenced to the North American Vertical Datus of 1988 (NAVD83). These flood elevations must be compared to structure an ground elevations referenced to the same vertical datum. To information regarding conversion between the National Geodetic Vertical Datum of 1929 and the North American Vertical Datum of 1989, vertical tatum. To is the North American Vertical Datum of 1989, vertical datum. To advect the National Sections and the National Geodetic Survey satisfies and advections.

NGS Information Services NOAA, N/NGS12 NOAA, N/NGS12 National Geodetic Survey SSMC-3, #9202 1315 East-West Highway Silver Spring, MD 20910-3282

o obtain current elevation, description, and/or location information for **bench ma** hown on this map, please contact the Information Services Branch of the Natio Seodetic Survey at (301) 713-3242 or visit its website at http://www.ngs.noaa.gov/.

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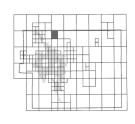
Please refer to the separately printed Map Index for an overview map of the county showing the layout of map panels, community map repository addresses; and a Listing of Communities table containing National Flood Insurance Program dates for each community as well as a listing of the panels on which each community is lorated.

Contact FEMA Map Service Center (MSC) via the FEMA Map Information eXchange (FMIX) 1477-358-5527 for information on available products associated with hite Flood Insurance Suby Report, and/or digital versions of the map. The MSC may also be reached by Fax at 1400-358-9620 and its website at http://www.msc.fema.gov/.

f you have questions about this map or questions concerning the National Floor insurance Program in general, please call 1-877-FEMA MAP (1-877-336-2627) or dit the FEMA website at http://www.fema.org/business/nfin

El Paso County Vertical Datu	n Offset Table
Flooding Source	Vertical Datum Offset (ft)
REFER TO SECTION 3.3 OF THE EL PASO COUN FOR STREAM BY STREAM VERTICAL DATUM	





This Digital Flood Insurance Rate Map (DFIRM) was produced through a Cooperating Technical Partner (CTP) agreement between the State of Colorado Water Conservation Board (CWCB) and the Federal Emergency Management Agency (FEMA).

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3230000 FT 104° 45' 0.00' 3215000 FT 3220000 FT JOINS PANEL 0100 3225000 FT 4° 41' 15.00" 39" 7" 30.00 39" 7" 30.00" 66 W. 65 W. COOPER GRV 2 CZ OND! IN RORP PHOEBE ORN 1470000 F ++GAMBLER WR DEFERSE TRL ZONE A Iron Gulch MEADOWPINE ECHO RANCH HTS +7 4329<sup>300</sup>"N 8 1465000 FT 11 12 East Cherry Creek ~ +4328000mN EL PASO COUNTY UNINCORPORATED AREAS 080059 ZONE A 1460000 F ZONE 13 14 +18 £ PALEO 17 CLOVI WAY ZONE PAGO NAY +ROPERS PT 0,73 1455000 F 4 ZONE AE -/ OTA WAY 19  $\langle \mathbf{r} \rangle$ ZONE AE 23 24 20 7389 Tributary to East Cherry Creek (F) 1398 - 7406 (\* 7401 - 741 7405 - 7409 (\* MOUNTAIN SHADOW VIEW 7410 + +ŝ East Cherry Creek ZONE AE KK0278 HODGEN R LIMIT OF STUDY  $\bigcirc$ RIDGE PORT CT TINCE East Cherr Creek 26 1450000 FT 25 29 ALPACA HT 39" 3" 45.00 39" 3' 45.00" 24000 E JOINS PANEL 0315 520<sup>0000</sup>E 104" 41" 15.00" 25000 104" 45" 0.00 02200mg NOTE: MAP AREA SHOWN ON THIS PANEL IS LOCATED WITHIN TOWNSHIP 11 SOUTH, RANGE 65 WEST AND TOWNSHIP 11 SOUTH, RANGE 66 WEST

LEGEND SPECIAL FLOOD HAZARD AREAS (SFHAS) SUBJECT TO INUNDATION BY THE 1% ANNUAL CHANCE FLOOD The 1% annual chance flood (100-year flood), also known as the base flood, is the flood that has a 1% chance of being equaled or exceeded in any given year. The Special Flood heard Area is the area subject to flooding by the 1% armusi chance flood. Areas of Special Flood Heard include Zones A, AE, AH, AD, AR, A99, V, and VE. The Base Flood Elevation is the water-sufficient levation of the 1% armusic hance flood. No Base Rood Elevations determined. Base Rood Elevations determined. Rood depths of 1 to 3 feet (usually areas of ponding); Base Rood Elevation determined. ZONE A ZONE AE ZONE AH ZONE AO Flood depths of 1 to 3 feet (usually sheet flow on sloping terrain); average depths determined. For areas of alluvial fan flooding, velocities also determined. Special Rood Hazard Area Formerly protected from the 1% annual chance flood by a flood control system that was subsequently decertified. Zone AR indicates that the former flood control system is being restored to provide protection from the 1% annual chance or greater flood. ZONE AR Area to be protected from 1% annual chance flood by a Federal flood protection system under construction; no Base Flood Elevations determined. ZONE A99 ZONE V Coastal flood zone with velocity hazard (wave action); no Base Flood Bevations determined. ZONE VE Coastal flood zone with velocity hazard (wave action); Base Flood Elevations determined //// FLOODWAY AREAS IN ZONE AE The floodway is the channel of a stream plus any adjacent floodplain areas that must be kept free of encroachment so that the 1% annual chance flood can be carried without substantial increases in flood beinbts. OTHER FLOOD AREAS Areas of 0.2% annual chance flood; areas of 1% annual chance flood with average depths of less than 1 foot or with drainage areas less than 1 square mile; and areas protected by levees from 1% annual chance flood. ZONE X OTHER AREAS ZONE X Areas determined to be outside the 0.2% annual chance floodplai Areas in which flood hazards are undetermined, but possible. ZONE D COASTAL BARRIER RESOURCES SYSTEM (CBRS) AREAS OTHERWISE PROTECTED AREAS (OPAs) OPAs are normally located within or adjacent to Spe Floodplain boundary Floodway boundary Zone D Boundary ..... CBRS and ORA boundar • Boundary dividing Special Flood Hazard Areas of diffe Flood Elevations, flood depths or flood velocities. ~~ 512 ~~ Base Flood Elevation line and value: elevation in feet\* Base Flood Elevation value where uniform within zone; elevation in feet\* (EL 987) an Vertical Datum of 1958 (NAVD 88) Cross section line 23-----23 Transect line Geographic coordinates referenced to the North American Datum of 1983 (NAD 83) 97° 07' 30.00" 32° 22' 30.00" 1000-meter Universal Transverse Mercator grid ticks, zone 13 4275000mN 6000000 FT 5000-foot grid ticks: Colorado State Plane system, central zone (FIPSZONE 0502), Lambert Conformal Conic Projection DX5510 Bench mark (see explanation in Notes to User this FIRM panel) M1.5 River Mile MAP REPOSITORIES Refer to Map Repositories list on Map Index EFFECTIVE DATE OF COUNTYWIDE FLOOD INSURANCE RATE MAP MARCH 17, 1997 EFFECTIVE DATE(S) OF REVISION(S) TO THIS PANEL DECEMBER 7, 2018 - to update corporate limits, to change Base Flood Ele Special Flood Hazard Areas, to update map format, to add roads and road n incorporate providualy issued. Letters of Max Revision. For community map revision history prior to countywide mapping, refer to the Comm Map History Table located in the Flood Insurance Study report for this jurisdiction. To determine if flood insurance is available in this community, contact your insurance agent or call the National Flood Insurance Program at 1-800-638-6620. MAP SCALE 1" = 1000' 2000 500 0 1000 HHH H NFIP PANEL 0305G MAVA FIRM FLOOD INSURANCE RATE MAP T EL PASO COUNTY, NPARTONPAL FLOVOD HINKULANNO ETRO COLORADO AND INCORPORATED AREAS PANEL 305 OF 1300 (SEE MAP INDEX FOR FIRM PANEL LAYOUT) CONTAINS: NUMBER PANEL SUFFIX COMMUNITY 080059 0305 te Map Number shown below should be use orders: the Community Number shown used on insurance applications for the subject MAP NUMBER 08041C0305G 1

MAP REVISED

DECEMBER 7, 2018 Federal Emergency Management Agency

#### NOTES TO USERS

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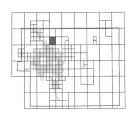
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El Paso County Vertical Datum	Offset Table
Flooding Source	Vertical Datum Offset (ft)
REFER TO SECTION 3.3 OF THE EL PASO COUNTY FOR STREAM BY STREAM VERTICAL DATUM CO	

Panel Location Map



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104" 45" 0.00" 3215000 ET 3220000 FT JOINS PANEL 0305 3225000 FT 3230000 FT 104" 41' 15.00" 9" 3" 45.00 39" 3" 45.0 SIESTA GRV 66 W. 65 W. MONTY PL EL PASO COUNTY UNINCORPORATED AREAS SECLUDED CREEK CO 30 29 26 25 ERRA RIDGE CIR OPEN 1445000 FT 32 COUNTRY LISTATES LN 4322000mN OHT D T. 11 S. T. 12 S. T. 11 S. T. 12 S. WILLHAVEN PL 1440000 FT 4321000WN HOLMES LN COOLWELL DR 5 2 6 PIEDRA VISTA ST JICARILLA DR EL PASO COUNTY UNINCORPORATED AREAS 080059 SCHWENCKS PL ELEMENTARY DR +ZONE D BOUNDARY COINCIDENT WITH FOREST BOUNDARY ANITA ST 1435000 F ZONE AE 7299 7293 AS 7288 730 ADYS LIMIT O ZONE D E NATIONAL HIGHLINE PI 20 PINERY DR PIKE NATIONAL FOREST 12 UMMINGBIRD LN 11 ZONE AE 7310 7316 7321 4319000mN ZONE AE DARR CH To TRAPPE PASS TI WHITE FIR LN BLACK FOREST AL. ZONE AF 1430000 FT 418000m TERRELL LN 13 17 SHADY UN ZONE AE INIPER DR LEPRECHAUN 9 EL PASO COUNTY UNINCORPORATED AREAS 080059  $\langle z \rangle$ ZONE AE HILLS , BURROWS RD LUPINE 18 4317000mN XXX sisi Kettle Creek ۲ \$ 53 All a e e 39" 0' 0.00 39" 0' 0.00" JOINS PANEL 0527 526 104" 41" 15 00" JOINS PANEL 0526 23 "24"""E "25"00"E

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Federal Emergency Management Agency



Flying Horse North Phase 2 Parcels 1-6 Preliminary Drainage Report Project No.: 211030

Appendix B:

Hydrologic Calculations



#### FLYING HORSE NORTH - PARCELS 1-6

**EXISTING CONDITIONS** 

HRGreen EL PASO COUNTY, COLORADO

	SUMM	ARY RU	NOFF	TABLE		
BASIN	AREA (ac)	% IMP.	C <sub>5</sub>	C <sub>100</sub>	Q <sub>5</sub> (cfs)	Q <sub>100</sub> (cfs)
EX1	12.4	4.2	0.11	0.37	4.3	24.9
EX2	0.8	2.0	0.08	0.35	0.3	2.2
EX3	1.5	2.0	0.08	0.35	0.6	4.3
EX4	16.5	2.0	0.08	0.35	4.3	31.4
EX5	6.4	2.0	0.08	0.35	2.0	14.6
EX5.1	7.4	2.0	0.08	0.35	1.8	13.0
EX6	13.7	2.0	0.08	0.35	3.9	28.8
EX7	64.7	2.0	0.08	0.35	14.7	108.1
EX8	41.6	2.0	0.08	0.35	9.7	71.1
EX9	21.7	2.0	0.08	0.35	6.0	44.2
EX10	7.6	2.0	0.08	0.35	2.2	16.4
EX11	55.3	2.0	0.08	0.35	13.7	100.7
EX12	27.5	2.0	0.08	0.35	6.8	49.6
EX13	20.0	2.0	0.08	0.35	5.4	39.8
EX14	12.2	2.0	0.08	0.35	3.3	24.2
EX15	90.1	2.0	0.08	0.35	21.6	158.5
EX16	8.0	2.0	0.08	0.35	2.3	16.6
EX17	15.6	2.0	0.08	0.35	4.4	32.3
EX18	5.4	2.0	0.08	0.35	1.4	10.4
EX19	5.4	2.0	0.08	0.35	1.5	11.3
EX20	14.9	2.0	0.08	0.35	4.2	30.5
EX21	48.4	2.0	0.08	0.35	14.1	103.8
EX22	24.6	2.0	0.08	0.35	6.7	49.3
EX23	164.4	2.0	0.08	0.35	44.3	325.4
EX24	17.3	2.0	0.08	0.35	3.3	24.0
EX25	42.7	2.0	0.08	0.35	11.2	82.1
OS1	19.0	5.1	0.12	0.37	7.9	42.7
OS2	36.4	5.0	0.12	0.37	13.5	73.4
OS3	25.3	3.0	0.09	0.36	8.2	53.9
OS4	72.3	7.0	0.14	0.39	28.8	134.6
OS5	41.2	6.5	0.13	0.39	16.2	78.3
OS6	83.6	2.5	0.09	0.35	16.0	110.0
OS7	20.1	2.0	0.08	0.35	4.7	34.9
OS8	8.0	58.1	0.55	0.70	3.8	4.4
OS9	9.4	90.2	0.82	0.90	27.4	50.6
TOTAL ONSITE	746.0	2.04%	0.08	0.35	193.9	1417.2
TOTAL OFFSITE	315.2	8.54%	0.14	0.40	126.6	582.8
TOTAL	1061.2	3.97%	0.10	0.36	320.5	2000.0

#### Calc'd by:

Checked by:

Date:

RDL

1/8/2024

DLH

	DESIGN	POINT	SUMMAF	RY TABLE	
DESIGN POINT	CONTRIBUTING BASINS	$\Sigma Q_5$ (cfs)	$\Sigma Q_{100}$ (cfs)	Tributary Area (ac.)	Weighted % Impervious
1	EX1	4.3	24.9	12.4	4.23
2	EX2	0.3	2.2	0.8	2.00
3	EX3	0.6	4.3	1.5	2.00
4	EX4	4.3	31.4	16.5	2.00
5	EX5	2.0	14.6	6.4	2.00
5.1	EX5.1	1.8	13.0	7.4	2.00
6	EX6	3.9	28.8	13.7	2.00
7	EX7 & DP26	22.7	150.9	83.6	2.70
8	EX8 & DP27	23.2	144.5	78.0	3.39
9	EX9	6.0	44.2	21.7	2.00
10	EX10 & DP28	10.5	70.3	32.9	2.76
11	EX11 & DP29	42.5	235.3	127.6	4.83
12	EX12	6.8	49.6	27.5	2.00
13	EX13	5.4	39.8	20.0	2.00
14	EX14 & 1/3RD OS9	12.4	41.0	15.3	20.02
15	EX15 & 1/3RD OS9	30.7	175.3	93.3	4.96
16	EX16	2.3	16.6	8.0	2.00
17	EX17	4.4	32.3	15.6	2.00
18	OS5, DP9, 16, 10	23.5	165.9	82.6	1.39
19	EX18, EX19, DP31	7.0	203.7	374.2	3.57
20	EX20 & DP15	34.9	205.9	108.2	1.94
21	EX21 & DP14	26.6	144.9	63.8	1.90
22	EX22	6.7	49.3	24.6	2.00
23	EX23, DP13 &32	65.9	443.4	184.4	2.00
24	EX24	3.3	24.0	17.3	2.00
25	EX25	11.2	82.1	42.7	2.00
26	OS1	7.9	42.7	19.0	5.06
27	OS2	13.5	73.4	36.4	4.99
28	OS3	8.2	53.9	25.3	2.99
29	OS4	28.8	134.6	72.3	7.00
30	OS8	3.8	4.4	20.1	2.00
31	OS6, DP7, 8, 17, 18, 30	102.7	624.8	363.5	3.61
32	OS5	16.2	78.3	41.2	6.47
	TOTAL	320.5	2000.0	1061.2	3.97%

		RSE NORTH -	PARCELS 1	-6									'd by: cked		DLH	
	EXISTING C	ONDITIONS											v:		RDL	
HRGreen	EL PASO COUNT	Y, COLORADO											ate		1/8/2024	
	•			СОМРО	SITE 'C' F	АСТ	ORS					<u>.</u>				
	OPEN SPACE /	<b>RESIDENTIAL (5</b>	ROADWAY /	TOTAL		OPE	N SPA	ACE /	RES	IDENTIAL (5	RC	DADWA	<b>Y</b> /	_	OMPOSIT	
BASIN	LAWN	AC LOT)	PAVEMENT		SOIL TYPE		LAWN	1		AC LOT)		VEME		IMPER	VIOUSNE	
		ACRES				%	<b>C</b> <sub>5</sub>	<b>C</b> <sub>100</sub>	%I	C <sub>5</sub> C <sub>100</sub>	%	<b>C</b> <sub>5</sub>	<b>C</b> <sub>100</sub>	%	<b>C</b> <sub>5</sub>	<b>C</b> <sub>100</sub>
EX1	6.84	5.52	0.00	12.36	В	2	0.08	0.35	7	0.14 0.39	100	0.90	0.96	4.2	0.11	0.37
EX2	0.80	0.00	0.00	0.80	В	2	0.08	0.35	7	0.14 0.39	100	0.90	0.96	2.0	0.08	0.35
EX3	1.48	0.00	0.00	1.48	В	2	0.08	0.35	7	0.14 0.39	100	0.90	0.96	2.0	0.08	0.35
EX4	16.53	0.00	0.00	16.53	В	2	0.08	0.35	7	0.14 0.39	100	0.90	0.96	2.0	0.08	0.35
EX5	6.36	0.00	0.00	6.36	В	2	0.08	0.35	7	0.14 0.39	100	0.90	0.96	2.0	0.08	0.35
EX5.1	7.37	0.00	0.00	7.37	В	2	0.08	0.35	7	0.14 0.39	100	0.90	0.96	2.0	0.08	0.35
EX6	13.74	0.00	0.00	13.74	В	2	0.08	0.35	7	0.14 0.39	100	0.90	0.96	2.0	0.08	0.35
EX7	64.65	0.00	0.00	64.65	В	2	0.08	0.35	7	0.14 0.39	100	0.90	0.96	2.0	0.08	0.35
EX8	41.56	0.00	0.00	41.56	В	2	0.08	0.35	7	0.14 0.39	100	0.90	0.96	2.0	0.08	0.35
EX9	21.68	0.00	0.00	21.68	В	2	0.08	0.35	7	0.14 0.39	100	0.90	0.96	2.0	0.08	0.35
EX10	7.62	0.00	0.00	7.62	В	2	0.08	0.35	7	0.14 0.39	100	0.90	0.96	2.0	0.08	0.35
EX11	55.34	0.00	0.00	55.34	В	2	0.08	0.35	7	0.14 0.39	100	0.90	0.96	2.0	0.08	0.35
EX12	27.47	0.00	0.00	27.47	В	2	0.08	0.35	7	0.14 0.39	100	0.90	0.96	2.0	0.08	0.35
EX13	19.98	0.00	0.00	19.98	В	2	0.08	0.35	7	0.14 0.39	100	0.90	0.96	2.0	0.08	0.35
EX14	12.20	0.00	0.00	12.20	В	2	0.08	0.35	7	0.14 0.39	100	0.90	0.96	2.0	0.08	0.35
EX15	90.14	0.00	0.00	90.14	В	2	0.08	0.35	7	0.14 0.39	100	0.90	0.96	2.0	0.08	0.35
EX16	8.02	0.00	0.00	8.02	В	2	0.08	0.35	7	0.14 0.39	100	0.90	0.96	2.0	0.08	0.35
EX17	15.59	0.00	0.00	15.59	B	2	0.08	0.35	7	0.14 0.39	100	0.90	0.96	2.0	0.08	0.35
EX18	5.35 5.35	0.00	0.00	5.35	B	2	0.08	0.35	7	0.14 0.39	100 100	0.90	0.96	2.0 2.0	0.08	0.35
EX19 EX20	14.89	0.00	0.00	5.35 14.89	B	2	0.08	0.35	7	0.14 0.39	100	0.90	0.96	2.0	0.08	0.35
EX20	48.43	0.00	0.00		B	2	0.08	0.35	7	0.14 0.39	100	0.90	0.90	2.0	0.08	0.35
				48.43						_				-		
EX22	24.63	0.00	0.00	24.63	В	2	0.08	0.35	7	0.14 0.39	100	0.90	0.96	2.0	0.08	0.35
EX23	164.44	0.00	0.00	164.44	В	2	0.08	0.35	7	0.14 0.39	100	0.90	0.96	2.0	0.08	0.35
EX24	17.27	0.00	0.00	17.27	В	2	0.08	0.35	7	0.14 0.39	100	0.90	0.96	2.0	0.08	0.35
EX25	42.71	0.00	0.00	42.71	В	2	0.08	0.35	7	0.14 0.39	100	0.90	0.96	2.0	0.08	0.35
OS1	7.36	11.63	0.00	18.99	В	2	0.08	0.35	7	0.14 0.39	100	0.90	0.96	5.1	0.12	0.37
OS2	14.65	21.74	0.00	36.39	B	2	0.08	0.35	7	0.14 0.39	100	0.90	0.96	5.0	0.12	0.37
OS3	20.25	5.00 72.29	0.00	25.25	B	2	0.08	0.35	7	0.14 0.39	100 100	0.90	0.96	3.0 7.0	0.09	0.36
OS4 OS5	0.00 4.37	36.87	0.00	72.29	B	2	0.08	0.35	7	0.14 0.39	100	0.90	0.96	7.0 6.5	0.14	0.39 0.39
055 057	20.07	0.00	0.00	20.07	B	2	0.08	0.35	7	0.14 0.39	100	0.90	0.96	0.5 2.0	0.13	0.39
037 0S8	3.42	0.00	4.58	8.00	B	2	0.08	0.35	7	0.14 0.39	100	0.90	0.96	2.0 58.1	0.08	0.35
038 0S6	74.56	9.00	4.58	83.56	B	2	0.08	0.35	7	0.14 0.39	100	0.90	0.96	2.5	0.55	0.70
030 0S9	0.94	0.00	8.46	9.40	B	2	0.08	0.35	7	0.14 0.39	100	0.90	0.90	90.2	0.09	0.35
TOTAL ONSITE	740.44	5.52	0.00	745.96		2	0.08	0.35	7	0.14 0.39	100	0.90	0.96	2.04	0.02	0.35
						2	0.08	0.35	7	0.14 0.39	100	0.90	0.96	2.04 8.54	0.08	0.35
TOTAL OFFSITE	145.62	156.53	13.04	315.19												
GRAND TOTAL	886.06	162.05	13.04	1061.15		2	0.08	0.35	7	0.14 0.39	100	0.90	0.96	3.97	0.10	0.36

	EXIST	ING CO	ONDITIO	NS						Check	ed by:	R	DL
HRGreen	EL PAS	O COUNT	TY, COLOF	RADO						Date:		1/8/:	2024
						OF CON	CENTRAT	ION					
BAS	IN DATA		OVER	LAND TIM	E (T,)		TRAV	EL TIME (	$T_t$		TOTAL	tc=(L/180)+10	Design to
DESIGNATION	C <sub>5</sub>	AREA (ac)	LENGTH (ft)	SLOPE %	t <sub>i</sub> (min)	Cv	LENGTH (ft)	SLOPE %	V (ft/s)	t <sub>t</sub> (min)	$t_c$ (min)	tc max	tc design (min,
EX1	0.11	12.36	300	2.2	24.3	7	1100	2.3	1.1	17.3	41.5	17.8	17.8
EX2	0.08	0.80	100	21.0	6.8	7	100	20.0	3.1	0.5	7.3	11.1	7.3
EX3	0.08	1.48	25	5.0	5.5	7	25	5.0	1.6	0.3	5.7	10.3	5.7
EX4	0.08	16.53	300	10.3	14.9	7	1180	5.9	1.7	11.6	26.5	18.2	18.2
EX5	0.08	6.36	200	16.0	10.5	7	200	16.0	2.8	1.2	11.7	12.2	11.7
EX5.1	0.08	7.37	270	6.7	16.3	7	1770	2.0	1.0	29.8	46.1	21.3	21.3
EX6	0.08	13.74	300	13.8	13.5	7	510	7.8	2.0	4.3	17.9	14.5	14.5
EX7	0.08	64.65	300	5.0	18.9	7	2130	2.0	1.0	35.9	54.8	23.5	23.5
EX8	0.08	41.56	300	8.0	16.2	7	1950	2.5	1.1	29.4	45.6	22.5	22.5
EX9	0.08	21.68	300	3.0	22.5	7	700	4.0	1.4	8.3	30.8	15.6	15.6
EX10	0.08	7.62	300	6.4	17.4	7	370	3.6	1.3	4.6	22.1	13.7	13.7
EX11	0.08	55.34	300	6.6	17.3	7	1480	2.2	1.0	23.8	41.0	19.9	19.9
EX12	0.08	27.47	300	7.1	16.9	7	1540	4.9	1.5	16.6	33.4	20.2	20.2
EX13	0.08	19.98	300	3.4	21.5	7	850	3.3	1.3	11.1	32.7	16.4	16.4
EX14	0.08	12.20	300	5.1	18.8	7	880	4.9	1.5	9.5	28.3	16.6	16.6
EX15	0.08	90.14	300	11.1	14.5	7	1740	5.5	1.6	17.7	32.2	21.3	21.3
EX16	0.08	8.02	300	5.7	18.1	7	600	5.3	1.6	6.2	24.3	15.0	15.0
EX17	0.08	15.59	300	6.9	17.0	7	980	5.7	1.6	6.2	23.2	15.0	15.0
EX18	0.08	5.35	300	7.0	16.9	7	480	4.7	1.7	9.8	26.7	17.1	17.1
EX19	0.08	5.35	300	5.0	18.9	7	660	5.3	1.5	5.3	24.2	14.3	14.3
EX20	0.08	14.89	300	6.1	17.7	7	380	3.9	1.6	6.8	24.6	15.3	15.3
EX21	0.08	48.43	300	7.0	16.9	7	820	4.6	1.4	4.6	21.5	13.8	13.8
EX22	0.08	24.63	300	8.3	16.0	7	890	4.0	1.5	9.1	25.1	16.2	16.2
EX23	0.08	164.44	300	4.5	19.6	7	3730	3.0	1.4	10.6	30.2	16.6	16.6
EX24	0.08	17.27	300	9.2	15.5	7	1090	3.8	1.2	51.3	66.7	32.4	32.4
EX25	0.08	42.71	300	9.2	15.5	7	1200	3.9	1.4	13.3	28.8	17.7	17.7
OS1	0.12	18.99	300	5.5	17.7	7	500	6.6	1.8	4.6	22.3	14.4	14.4
OS2	0.12	36.39	300	5.8	17.4	7	1213	4.9	1.5	13.0	30.4	18.4	18.4
OS3	0.09	25.25	300	5.7	17.9	7	540	7.3	1.9	4.8	22.7	14.7	14.7
OS4	0.14	72.29	300	6.1	16.7	7	2140	4.0	1.4	25.5	42.2	23.6	23.6
OS5	0.13	41.24	300	5.0	17.9	7	1900	5.0	1.6	20.2	38.2	22.2	22.2
OS7	0.08	20.07	280	9.0	15.0	15	1850	2.8	2.5	12.3	27.3	21.8	21.8
OS8	0.55	8.00	OVERR	IDDEN		20	OVERR	IDDEN	0.0				
OS6	0.09	83.56	300	7.0	16.8	15	4350	3.0	2.6	27.9	44.7	35.8	35.8
OS9	0.82	9.40	15	2	1.6	15	1650	2	2.1	13.0	14.6	19.3	14.6

$$t_i = \frac{0.395(1.1 - C_5)\sqrt{L}}{S^{0.33}} \qquad \qquad V = C_v S_w^{0.5}$$

	Type of Land Surface	$C_{\nu}$
	Heavy meadow	2.5
	Tillage/field	5
-	Riprap (not buried)*	6.5
	Short pasture and lawns	7
	Nearly bare ground	10
	Grassed waterway	15
	Paved areas and shallow paved swales	20

 Paved areas and shallow paved swales
 20

 \* For buried riprap, select C<sub>v</sub> value based on type of vegetative cover.

			FLYI	NG H	IOR	SE NC	)RTH -	PAR	CELS	5 1-6											Calc	'd by:	DLH
			EXIST	<b>FING</b>	CONI	DITION	IS														Chec	ked by:	RDL
	I.		DESIC	GN ST	ORM	l: 5-YE	EAR														Da	nte:	1/8/2024
HR	Gre	en																3.20	60761	143			
				D	DIRECT	T RUNG	DFF		т	OTAL	RUNO	F	0\	/ERLA	ND		PI	PE		TR	AVEL .	ГІМЕ	REMARKS
																						(min	
STREET	DESIGN POINT	BASIN ID	AREA (ac)	C <sub>5</sub>	t <sub>e</sub> (min)	C <sub>5</sub> *A (ac)	/ (in./ hr.)	Q (cfs)	t <sub>e</sub> (min)	C <sub>5</sub> *A (ac)	/ (in./ hr.)	Q (cfs)	Q <sub>street</sub> (cfs)	C <sub>5</sub> *A (ac)	SLOPE %	Q <sub>PIPE</sub> (cfs)	C <sub>5</sub> *A (ac)	SLOPE %	PIPE SIZE (FT)	LENGTH (FT)	VEL. (FPS)	TRAVEL TIME (r	
	1	EX1	12.36	0.11		1.32	3.27	4.3															DRAINS EAST INTO ALLEN RANCH ROAD
	1	EAT	12.30	0.11	17.0	1.32	3.21	4.3															DRAINS EAST INTO ALLEN RANOF ROAD
	2	EX2	0.80	0.08	7.3	0.06	4.60	0.3															DRAINS WEST OFF INTO GOLF COURSE TRACT
	3	EX3	1.48	0.08	5.7	0.12	4.96	0.6															DRAINS SOUTH WEST INTO EX4
	4	EX4	16.53	0.08	18.2	1.32	3.23	4.3															DRAINS SOUTH WEST INTO FLYING HORSE GOLF COURSE TRACT
	_																						
	5	EX5	6.36	0.08	11.7	0.51	3.90	2.0															DRAINS WEST INTO FLYING HORSE GOLF COURSE
	5.1	EX5.1	7.37	0.08	21.3	0.59	2.99	1.8															BASIN DRAINS EAST INTO ALLEN RANCH ROAD
	6	EX6	13.74	0.08	14.5	1.10	3.57	3.9															DRAINS SOUTH WEST OFFSITE INTO EDMONDS SUBDIVISION
	7	EX7	64.65	0.08	23.5	5.17	2.85	14.7		7.39		22.7											BASIN & OS1 COLLECT INTO EX. TERTIARY DRAINAGE SWALE, FLOWS TO NORTHWEST TO DP7
	8	EX8	41.56	0.08	22.5	3.32	2.91	9.7		7.54		23.2											BASIN & OS2 COLLECT INTO EX. TERTIARY DRAINAGE SWALE, FLOWS TO NORTHWEST TO DP8
												20.2											
	9	EX9	21.68	0.08	15.6	1.73	3.47	6.0															DRAINS NORTH WEST INTO OS7
	10	EX10	7.62	0.08	13.7	0.61	3.65	2.2		2.93		10.5											EX10 & OS3 COLLECT INTO EX NATURAL DRAINAGE SWALE AND INTO OS7
	11	EX11	55.34	0.08	19.9	4.43	3.10	13.7		14.55		42.5											SHEET FLOWS EAST INTO BLACK FOREST ROAD
	12	EX12	27.47	0.08	20.2	2.20	3.07	6.8															SHEET FLOWS EAST OFFSITE
	13	EX13	19.98	0.08			3.39																SHEET FLOWS NORTH-EAST INTO CULVERT AT DP13
	14	EX14	12.20	0.08	16.6	0.98	3.37	3.3		3.54		12.4								<u> </u>	+		SHEET FLOWS NORTH INTO CULVERT AT DP14 + ONE THIRD OF FLOWS FROM OS9 SHEET FLOWS AND COLLECTS INTO NATURAL DRAINAGE SWALE, FLOWS NORTH TO CULVERT @ DP15
	15	EX15	90.14	0.08	21.3	7.21	2.99	21.6		9.77		30.7											+ ONE THRID OF FLOWS FROM OS9

	1	/	FLYI	NG H	HORS	SE NO	DRTH -	PAR	CEL	s 1-6											Cal	c'd by:	DLH
_	+⊰·	$\rightarrow$	EXIS	TING	CON	οιτιο	NS														Chec	ked by	RDL
	I I.		DESI	GN ST	TORM	: 5-Y	EAR														D	ate:	1/8/2024
HF	Gre	en																					
																		3.26	660761	143			
				0	DIRECT	RUN	OFF		т	OTAL	RUNOF	F	0\	ERLA	ND		PI	PE		TR	RAVEL	TIME	REMARKS
STREET	DESIGN POINT	BASIN ID	AREA (ac)	c,	t <sub>e</sub> (min)	C <sub>5</sub> *A (ac)	/ (in./ hr.)	Q (cfs)	t <sub>e</sub> (min)	C <sub>5</sub> *A (ac)	/ (in./ hr.)	Q (cfs)	Q <sub>street</sub> (cfs)	C <sub>5</sub> *A (ac)	% JAONS	Q <sub>PIPE</sub> (cfs)	C <sub>5</sub> *A (ac)	% SLOPE %	PIPE SIZE (FT)	LENGTH (FT)	VEL. (FPS)	TRAVEL TIME (mir	
	16	EX16	8.02	0.08	15.0	0.64	3.52	2.3															SHEET FLOWS SOUTH-WEST INTO OS7
	17	EX17	15.59	0.08	15.0	1.25	3.52	4.4															SHEET FLOWS WEST INTO OS6
	18									6.91		23.5											DP IS CUMULATIVE OF DP9, 16, 10 AND OS7
		EX18	5.35	0.08	17.1	0.43	3.32	1.4															SHEET FLOWS EAST INTO EX NATURAL DRAINAGE SWALE THAT FLOWS NORTH OFF-SITE
		EATO	5.55	0.08	17.1	0.43	3.32	1.4															Sheet FLOWS EAST INTO EX NATURAL DRAINAGE SWALE THAT FLOWS NORTH OFF-SITE
		EX19	5.35	0.08	14.3	0.43	3.59	1.5															SHEET FLOWS WEST INTO EX NATURAL DRAINAGE SWALE THAT FLOWS NORTH OFF-SITE
	19									35.56		7.0											DP19 HAS BEEN OVERRIDDEN TO SHOW RELEASE FLOWS FROM THE JD DESIGN + EX18 AND EX19
	20	EX20	14.89	0.08	15.3	1.19	3.49	4.2		10.97		34.9											SHEEET FLOWS COLLECT INTO NATURAL DRAINAGE SWALE AT DP20
	21	EX21	48.43	0.08	13.8	3.87	3.65	i 14.1		7.41		26.6											SHEET FLOWS COLLECT INTO NATURAL DRAINAGE SWALE , FLOWS NORTH OFF-SITE
	22	EX22	24.63	0.08	16.2	1.97	3.40	6.7															SHEET FLOWS NORTH WEST OFF-SITE
																				1			
	23	EX23	164.44	0.08	16.6	13.16	3.37	44.3		20.27		65.9										_	SHEET FLOWS COLLECT INTO MULTIPLE NATURAL SWALES THAT FLOW NORTH TO HODGEN ROAD
	24	EX24	17.27	0.08	32.4	1.38	2.37	3.3															FLOWS NORTH TO HODGEN ROAD
	25	EX25	42.71	0.08	17.7	3.42	3.27	11.2															FLOWS NORTH-WEST OFF-SITE TO HODGEN ROAD
	25	EAZS	42.71	0.08	17.7	3.42	3.21	11.2															
	26	OS1	18.99	0.12	14.4	2.22	3.58	7.9															FLOWS NORTH-WEST INTO SITE AT DP26 INTO EX7
	27	OS2	36.39	0.12	18.4	4.22	3.21	13.5															FLOWS NORTH-WEST INTO SITE AT DP27 INTO EX8
	20	082	25.05	0.00	14.7	2.22	2 55																FLOWS NORTH INTO SITE AT DP28 INTO EX10
	28	OS3	25.25	0.09	14.7	2.32	3.55														+	+	
	29	OS4	72.29	0.14	23.6	10.12	2.84	28.8												<b> </b>			FLOWS NORTH-EAST TO DP29 AND INTO EX11
	32	OS5	41.24	0.13	22.2	5.51	2.93	16.2															FLOWS NORTH, THROUGH EX CULVERT UNDER O.S.R. INTO EX23
		OS7	20.07	0.08	21.8	1.61	2.96	4.7															SHEET FLOWS INTO EX SWALE THROUGH GOLF COURSE. COMBINED FLOWS IN DP18
	1																			I		1	OS6 IS ENTIRELY CAPTURED WITHIN AN EXISTING POND IN FHN FILING 3
	30	OS8	8.00	0.55		4.40						3.8									-	+	RELEASED AT HISTORIC RATES AS CALCULATED IN F.H.N. FILING 3 SHEET FLOWS INTO MULTIPLE EX SWALES IN GOLF COURSE, LEADS DOWN TO
		OS6	83.56	0.09	35.8	7.22	2.21	16.0		9.79		25.1											IRRIGATION RESERVOIR
	24									24.74		100 7											DP31 REPRESENTS RELEASE FROM IRRIGATIONAL RESERVIOR (OVERRIDDEN BY DESIGN RELEASE)
	31									34.71		102.7										+	CUMULATIVE OF BASIN OS6, OS9, AND DP7, 8, 17, 18, 30 RUNOFF FROM OLD STAGECOACH ROAD HAS BEEN SPLIT INTO THIRDS FOR SIMPLICITY
		OS9	9.40	0.82	14.6	7.69	3.57	27.4															ENTERING DP14, DP15, AND OS6



	FLYING HORSE NORTH - PARCELS 1-6			Calc'd by:	DLH
	EXISTING CONDITIONS			Checked by	RDL
	DESIGN STORM: 100-YEAR			Date:	1/8/2024
en					
	DIRECT RUNOFF TOTAL RUNOFF	OVERLAND	PIPE 1	RAVEL TIME	REMARKS

STREET	DESIGN PONT	BASIN ID	AREA (ac)	C100	t <sub>c</sub> (min)	C <sub>100</sub> *A (ac)	/ (in./ hr.)	Q (cfs)	t <sub>e</sub> (min)	C <sub>100</sub> *A (ac)	/ (in./ hr.)	Q (cfs)	Q <sub>street</sub> (cfs)	C <sub>100</sub> *A (ac)	SLOPE %	Q <sub>PIPE</sub> (cfs)	C <sub>100</sub> *A (ac)	% adone	PIPE SIZE (ft)	LENGTH (ft)	VEL. (ft/s)	TRAVEL TIME (mi	
			40.00			4.55	- 10																
	1	EX1	12.36	0.37	17.8	4.55	5.48	24.9															DRAINS EAST INTO ALLEN RANCH ROAD
	2	EX2	0.80	0.35	7.3	0.28	7.72	2.2															DRAINS WEST OFF INTO GOLF COURSE TRACT
	3	EX3	1.48	0.35	5.7	0.52	8.33	4.3															DRAINS SOUTH WEST INTO EX4
	4	EX4	16.53	0.35	18.2	5.79	5.42	31.4	-														DRAINS SOUTH WEST INTO FLYING HORSE GOLF COURSE TRACT
	4	E/\4	10.55	0.35	10.2	5.79	0.42	31.4															DRAINS SOUTH WEST INTO FETING HORSE GOLF COURSE TRACT
	5	EX5	6.36	0.35	11.7	2.23	6.54	14.6															DRAINS WEST INTO FLYING HORSE GOLF COURSE
	5.1	EX5.1	7.37	0.35	21.3	2.58	5.02	13.0	)														BASIN DRAINS EAST INTO ALLEN RANCH ROAD
	6	EX6	13.74	0.35	14.5	4.81	6.00	28.8	-														DRAINS SOUTH WEST OFFSITE INTO EDMONDS SUBDIVISION
	0	EVO	13.74	0.35	14.0	4.01	0.00	20.0	, 														DRAINS SOUTH WEST OFFSTE INTO EDMONDS SUBDIVISION
	7	EX7	64.65	0.35	23.5	22.63	4.78	108.1	1	29.74		150.9											BASIN & OS1 COLLECT INTO EX. TERTIARY DRAINAGE SWALE, FLOWS TO NORTHWEST TO DP7
	8	EX8	41.56	0.35	22.5	14.55	4.89	71.1		28.15		144.5											BASIN & OS2 COLLECT INTO EX. TERTIARY DRAINAGE SWALE, FLOWS TO NORTHWEST TO DP8
	9	EX9	21.68	0.35	15.6	7.59	5.82	44.2															DRAINS NORTH WEST INTO OS7
	10	EX10	7.62	0.35	13.7	2.67	6.14	16.4		11.70		70.3											EX10 & OS3 COLLECT INTO EX NATURAL DRAINAGE SWALE AND INTO OS7
		2,410	1.02	0.00	10.1	2.07	0.11					10.0											
	11	EX11	55.34	0.35	19.9	19.37	5.20	100.7	-	47.56		235.3											SHEET FLOWS EAST INTO BLACK FOREST ROAD
	10	51/10	07.17	0.05		0.04	5.40	40.0															
	12	EX12	27.47	0.35	20.2	9.61	5.16	49.6															SHEET FLOWS EAST OFFSITE
	13	EX13	19.98	0.35	16.4	6.99	5.69	39.8															SHEET FLOWS NORTH-EAST INTO CULVERT AT DP13
	14	EX14	12.20	0.35	16.6	4.27	5.66	24.2	-	7.09		41.0											SHEET FLOWS NORTH INTO CULVERT AT DP14 + ONE THIRD OF FLOWS FROM OS9
	45		90.14	0.35	21.3	24 55	5.02	158.5	-	24.27		175.3											SHEET FLOWS AND COLLECTS INTO NATURAL DRAINAGE SWALE, FLOWS NORTH TO CULVERT @ DP15 + ONE THRID OF FLOWS FROM OS9
	15	EX15	90.14	0.35	21.3	31.55	5.02	156.5		34.37		1/5.3											
	16	EX16	8.02	0.35	15.0	2.81	5.91	16.6															SHEET FLOWS SOUTH-WEST INTO OS7



	FLY	ING F	IORS	E NO	ORTH -	PAR	CELS	s 1-6								Calc'd	l by:	DLH
<u> </u>	EXIS.	TING	COND	ΙΤΙΟΙ	NS											Checke	ed by:	RDL
$\checkmark$	DESI	GN ST	ORM	: 100	-YEAR											Date	e:	1/8/2024
en																		
- · ·																		
		D	IRECT	RUNG	DFF		т		UNOF	F	OVE	RLAND	PI	PE	TRA	VEL TI	ME	REMARKS

STREET	DESIGN PONT	BASIN ID	AREA (ac)	C100	t <sub>e</sub> (min)	C <sub>100</sub> *A (ac)	/ (in./ hr.)	Q (cfs)	ť <sub>c</sub> (min)	C <sub>100</sub> *A (ac)	/ (in./ hr.)	Q (cfs)	Q <sub>street</sub> (cfs)	C <sub>100</sub> *A (ac)	SLOPE %	Q <sub>PIPE</sub> (cfs)	C <sub>100</sub> *A (ac)	SLOPE %	PIPE SIZE (ft)	LENGTH (ft)	VEL. (ft/s)	TRAVEL TIME (	
	17	EX17	15.59	0.35	15.0	5.46	5.91	32.3	-														SHEET FLOWS WEST INTO OS6
	17		10.00	0.00	15.0	3.40	5.5	52.5															
	18									29.12		165.9											DP IS CUMULATIVE OF DP9, 16, 10 AND OS7
		EX18	5.35	0.35	17.1	1.87	5.58	3 10.4															SHEET FLOWS EAST INTO EX NATURAL DRAINAGE SWALE THAT FLOWS NORTH OFF-SITE
		EX19	5.35	0.35	14.3	1.87	6.03	3 11.3	-														SHEET FLOWS WEST INTO EX NATURAL DRAINAGE SWALE THAT FLOWS NORTH OFF-SITE
		EVIA	0.00	0.35	14.3	1.07	0.03	5 11.3										-					SHEET FLOWS WEST INTO EX NATURAL DRAINAGE SWALE THAT FLOWS NORTH OFF-SITE
	19									131.42		203.7											DP19 HAS BEEN OVERRIDDEN TO SHOW RELEASE FLOWS FROM THE JD DESIGN + EX18 AND EX19
	20	EX20	14.89	0.35	15.3	5.21	5.86	30.5	-	39.58		205.9											SHEEET FLOWS COLLECT INTO NATURAL DRAINAGE SWALE AT DP20
	20	EX20	14.69	0.35	15.3	5.21	5.60	5 30.5		39.56		205.9						-					SHEELT FLOWS COLLECT INTO NATURAL DRAINAGE SWALE AT DF20
	21	EX21	48.43	0.35	13.8	16.95	6.12	2 103.8		24.04		144.9											SHEET FLOWS COLLECT INTO NATURAL DRAINAGE SWALE , FLOWS NORTH OFF-SITE
	22	EX22	24.63	0.35	16.2	8.62	5.71	49.3															SHEET FLOWS NORTH WEST OFF-SITE
	00	EVOO	404.44	0.05	40.0	57.55	5.00	005.4	-	00.40		440.4											SHEET FLOWS COLLECT INTO MULTIPLE NATURAL SWALES THAT FLOW NORTH TO HODGEN ROAD
	23	EX23	164.44	0.35	16.6	57.55	5.65	325.4		80.46		443.4								-			SHEET FLOWS COLLECT INTO MULTIPLE NATURAL SWALES THAT FLOW NORTH TO HODGEN ROAD
	24	EX24	17.27	0.35	32.4	6.04	3.97	24.0															FLOWS NORTH TO HODGEN ROAD
	25	EX25	42.71	0.35	17.7	14.95	5.49	82.1															FLOWS NORTH-WEST OFF-SITE TO HODGEN ROAD
									_														
	26	OS1	18.99	0.37	14.4	7.11	6.01	42.7															FLOWS NORTH-WEST INTO SITE AT DP26 INTO EX7
	27	OS2	36.39	0.37	18.4	13.61	5.40	73.4	-														FLOWS NORTH-WEST INTO SITE AT DP27 INTO EX8
	21	032	30.39	0.37	10.4	13.01	0.40	73.4															PLOWS NORTH-WEST INTO SITE AT DF27 INTO EA6
	28	OS3	25.25	0.36	14.7	9.04	5.97	53.9															FLOWS NORTH INTO SITE AT DP28 INTO EX10
	29	OS4	72.29	0.39	23.6	28.19	4.77	7 134.6															FLOWS NORTH-EAST TO DP29 AND INTO EX11
	32	OS5	41.24	0.39	22.2	15.91	4.92	2 78.3															FLOWS NORTH, THROUGH EX CULVERT UNDER O.S.R. INTO EX23
		OS7	20.07	0.35	21.8	7.02	4.96	6 34.9													1		SHEET FLOWS INTO EX SWALE THROUGH GOLF COURSE. COMBINED FLOWS IN DP18
																						1	OS6 IS ENTIRELY CAPTURED WITHIN AN EXISTING POND IN FHN FILING 3
	30	OS8	8.00	0.70		5.59						4.4											RELEASED AT HISTORIC RATES AS CALCULATED IN F.H.N. FILING 3
																							SHEET FLOWS INTO MULTIPLE EX SWALES IN GOLF COURSE, LEADS DOWN TO
		OS6	83.56	0.35	35.8	29.61	3.72	2 110.0		32.42		126.9							I	I			IRRIGATION RESERVOIR
	24								-	107.07		604.0											DP31 REPRESENTS RELEASE FROM IRRIGATIONAL RESERVIOR (OVERRIDDEN BY DESIGN RELEASE)
	31	<u> </u>								127.67		624.8											CUMULATIVE OF BASIN OS6, OS9, AND DP7, 8, 17, 18, 30 RUNOFF FROM OLD STAGECOACH ROAD HAS BEEN SPLIT INTO THIRDS FOR SIMPLICITY
		OS9	9.40	0.90	14.6	8.45	5.99	9 50.6															ENTERING DP14, DP15, AND OS6
	1	039	9.40	0.90	14.0	0.45	0.98	50.0					1						1		1	1	

HRGreen EL PASO COUNTY, COLORADO

	SUMM	ARY RU	NOFF	TABLE	E									
BASIN	AREA (ac)	% IMP.	$C_5$	C <sub>100</sub>	Q <sub>5</sub> (cfs)	Q <sub>100</sub> (cfs)								
А	74.1	15.0	0.17	0.42	38.9	161.6								
A1	12.6	7.0	0.14	0.39	6.0	29.0								
A2	6.5	13.1	0.15	0.40	3.4	15.3								
В	32.7	24.1	0.22	0.45	24.6	86.1								
С	121.0	31.6	0.26	0.47	81.4	251.4								
D 86.2 26.8 0.23 0.45 54.8 177.1														
E	52.4	43.7	0.37	0.55	67.7	171.0								
F	197.5	15.7	0.19	0.43	95.9	366.3								
G	27.3	16.4	0.16	0.41	16.4	68.4								
Н	74.0	7.0	0.14	0.39	37.6	180.4								
I	7.1	26.4	0.23	0.46	6.1	20.7								
J	15.8	86.1	0.74	0.83	59.8	112.4								
K	18.0	86.0	0.74	0.83	64.4	121.2								
L	7.1	57.8	0.52	0.67	19.0	41.1								
М	5.0	57.8	0.52	0.67	9.9	21.3								
OS1	19.0	2.0	0.08	0.35	5.6	41.3								
OS2	36.4	2.0	0.08	0.35	9.2	67.9								
OS3	25.3	2.0	0.08	0.35	6.8	49.9								
OS4	72.3	2.0	0.08	0.35	18.3	134.5								
OS5	41.2	6.5	0.13	0.39	15.9	78.8								
OS6	93.6	4.5	0.10	0.36	23.0	143.5								
OS7	28.2	8.2	0.12	0.38	10.6	57.7								
OS8	8.0	58.1	0.50	0.65	3.8	4.4								
TOTAL ONSITE	747.3	24.6%	0.24	0.46	585.8	1823.4								
TOTAL OFFSITE	313.9	5.4%	0.11	0.38	93.3	577.8								
TOTAL	1061.2	18.9%	0.20	0.44	679.1	2401.2								
	*Includes some	on-site area that a	re rear of B, G,	or W/O lot types										

	CUMULATIVE DESIG	N POIN	T SUMM	ARY TABLE	E
DESIGN POINT	CONTRIBUTING BASINS	$\Sigma Q_5$ (cfs)	ΣQ <sub>100</sub> (cfs)	Tributary Area (ac.)	Weighted % Impervious
1	A, OS1 (portions)	14.5	69.1	31.7	11.1%
2	A, OS1 (portions)	14.5	69.1	31.7	11.1%
3	A, OS1	44.5	202.8	93.1	12.3%
4	A1, OS2	15.3	96.9	49.0	3.3%
5	A1, A2, OS2	18.7	112.2	55.5	4.4%
6	A1, A2, I, OS2, OS3, OS6, OS7 + Outlet Q's of A, B, Pond A (Fil. 3)	72.1	459.3	217.7	5.4%
7	В	24.6	86.1	32.7	24.1%
8	OS3	6.8	49.9	25.3	2.0%
9	OS3, OS7	17.4	107.6	53.5	4.7%
10	С	81.4	251.4	121.0	31.6%
11	С	81.4	251.4	121.0	31.6%
12	OS4	18.3	134.5	72.3	2.0%
13	D, OS4	73.1	311.6	158.5	15.5%
14	E (portion)	33.8	85.5	26.2	43.7%
15	E	67.7	171.0	52.4	43.7%
16	OS5	15.9	78.8	41.2	6.5%
17	F, OS5	111.8	445.1	238.7	14.1%
18	G	16.4	68.4	27.3	16.4%
19	Н	37.6	180.4	74.0	7.0%
20		6.1	20.7	7.1	26.4%
21	J	59.8	112.4	15.8	86.1%
22	К	64.4	121.2	18.0	86.0%
23	L	19.0	41.1	7.1	57.8%
24	М	9.9	21.3	5.0	57.8%
25	OS8	3.8	4.4	8.0	58.1%
	*FINAL Q5 AND 100 OF DESIGN POINT 6 WILL REC	QUIRE DETERMIN	ATION OF OUTLET P	EAK FLOWS AS DESIGN	ED IN FUTURE FDR
	*PRELIMINARY OUTLET STRUCTURE CALCS AND R	ELEASE RATES A	RE INCLUDED IN TH	IS REPORT, SEE POND A	AND POND B CALCS

<u>Calc'd by:</u>	DLH
<u>Checked by:</u>	RDL
<u>Date:</u>	10/30/2023

#### FLYING HORSE NORTH PARCELS 1-6

<u>Calc'd by:</u> DLH Checked by: RDL

1433 PROPOSED CONDITIONS

DASO COUNTY COLODADO

HRGreen	EL PASO COUNT	Y, COLORADO				Date	10/19/2023																								
									CON	MPOSIT	E 'C' FAG	CTORS																			
	OPEN SPACE /	COMMERCIAL	ROADWAY /	RESIDENTIAL	RESIDENTIAL	RESIDENTIAL	RESIDENTIAL	RESIDENTIAL	RESIDENTIAL	TOTAL		OPEN SP	ACE /	COMM	ERCIAL	ROAD	WAY /	RES	SIDENTIA	L RESID	DENTIA	L RESID	ENTIA	RESIDE		SIDENT	AL RE	SIDENTIAL		OMPOSIT	
BASIN	LAWN	COMMERCIAL	PAVEMENT	(5 AC LOT)	(2.5 AC LOT)	(1/2-AC LOT)	(1/3-AC LOT)	(1/4-AC LOT)	(1/8-AC LOT)	TOTAL	SOIL TYPE	LAW	N	COMIN	ERGIAL	PAVE		(5	AC LOT)	(2.5	AC LOT)	) L (1/	2-AC	(1/3-AC	LOT) (1	/4-AC LO	T) (1/	8-AC LOT)		VIOUSNE	55 & C
					ACRES							%I C <sub>t</sub>	C10	∞ %I C	5 C <sub>100</sub>	%I	C5 C1	100 %I	C <sub>5</sub> C <sub>1</sub>	" %I C	5* C100	,* %I C	5 C <sub>100</sub>	%I C <sub>5</sub>	C <sub>100</sub> %	I C₅ C	100 %1	C <sub>5</sub> C <sub>100</sub>	%I	C <sub>5</sub>	C <sub>100</sub>
A	12.50			27.35		27.15	7.11			74.11	В	2 0.0	8 0.35	5 95 0.8	0.88	100 0	.90 0.9	96 7	0.14 0.3	9 11 0	.17 0.42	2 25 0.2			0.47 40	0.30 0	.50 65	0.45 0.59	15.0	0.17	0.42
A1				12.58						12.58	В	2 0.0	8 0.35	5 95 0.8	0.88	100 0	.90 0.9	96 7	0.14 0.3		.17 0.42			30 0.25		0.30 0		0.45 0.59		0.14	0.39
A2	3.95						2.58			6.53	В	2 0.0	8 0.35	5 95 0.8	0.88	100 0	.90 0.9	96 7	0.14 0.3	9 11 0	.17 0.42	2 25 0.2	2 0.46		0.47 40	0.30 0	.50 65	0.45 0.59		0.15	0.40
В	1.70			3.25		14.20	13.54			32.69	В	2 0.0	8 0.35	5 95 0.8	0.88	100 0	.81 0.8	88 7	0.14 0.3	9 11 0	.17 0.42	2 25 0.2	2 0.46	30 0.25	0.47 40	0.30 0	.50 65	0.45 0.59		0.22	0.45
С	29.76		3.56			6.47		81.24		121.03	В	2 0.0	8 0.35	5 95 0.8	0.88	100 0	.81 0.8	88 7	0.14 0.3	9 11 0	.17 0.42		2 0.46	30 0.25		0.30 0		0.45 0.59		0.26	0.47
D	24.04			29.10				3.58	29.44	86.16	В	2 0.0		5 95 0.8	0.88	100 0	.81 0.8	88 7	0.14 0.3		.17 0.42				0.47 40			0.45 0.59		0.23	0.45
E	14.30	11.04	2.15					24.87		52.36	В	2 0.0	8 0.35	5 95 0.8	0.88	100 0	.81 0.8	88 7	0.14 0.3		.17 0.42			30 0.25		0.30 0		0.45 0.59		0.37	0.55
F	76.45	9.18			96.02				15.80	197.45	В	2 0.0	8 0.35	5 95 0.8	0.88	100 0	.81 0.8		0.14 0.3	0 11 0	.17 0.42			30 0.25		0.00 0		0.40 0.00		0.19	0.43
G	16.98							10.32		27.30	В	2 0.0	8 0.35	5 95 0.8	0.88	100 0	.81 0.8	88 7	0.14 0.3	9 11 0	.17 0.42	2 25 0.2	2 0.46	30 0.25	0.47 40	0.30 0	.50 65	0.45 0.59		0.16	0.41
Н				74.02						74.02	В	2 0.0	8 0.35	5 95 0.8	0.88	100 0	.81 0.8	88 7	0.14 0.3	9 11 0	.17 0.42	2 25 0.2	2 0.46	30 0.25	0.47 40	0.30 0	.50 65	0.45 0.59		0.14	0.39
I	0.56					2.06	4.51			7.13	В	2 0.0	0.00	5 95 0.8	0.88	100 0	.81 0.8	88 7	0.14 0.3	-	.17 0.42			30 0.25				0.45 0.59		0.23	0.46
J	1.50	14.26								15.76	В	2 0.0	8 0.35	5 95 0.8	0.88	100 0	.81 0.8	88 7	0.14 0.3		.17 0.42			30 0.25			.50 65	0.45 0.59		0.74	0.83
K	1.75	16.25								18.00	В	2 0.0	8 0.35	5 95 0.8	0.88	100 0	.81 0.8	88 7	0.14 0.3		.17 0.42			30 0.25		0.30 0	.50 65	0.45 0.59		0.74	0.83
L	2.84	4.25								7.09	В	2 0.0	8 0.35	5 95 0.8	0.88	100 0	.81 0.8		0.14 0.3						0.47 40			0.45 0.59		0.52	
M	1.99	2.98								4.97	В	2 0.0	8 0.35	5 95 0.8	0.88	100 0	.81 0.8	88 7	0.14 0.3	9 13 0	.17 0.42		2 0.46	30 0.25	0.47 40	0.30 0	.50 65	0.45 0.59		0.52	0.67
OS1	18.99									18.99	В	2 0.0	8 0.35	5 95 0.8	0.88	100 0	.81 0.8	88 7	0.14 0.3	9 11 0	.17 0.42		2 0.46	30 0.25	0.47 40	0.30 0	.50 65	0.45 0.59		0.08	0.35
OS2	36.39									36.39	В	2 0.0	8 0.35	5 95 0.8	0.88	100 0	.81 0.8	88 7	0.14 0.3		.17 0.42			30 0.25				0.45 0.59		0.08	0.35
OS3	25.25									25.25	В	2 0.0	8 0.35	5 95 0.8	0.88	100 0	.81 0.8	88 7	0.14 0.3		.17 0.42			30 0.25		0.30 0		0.45 0.59		0.08	0.35
OS4	72.29									72.29	В	2 0.0	8 0.35	5 95 0.8	0.88	100 0	.81 0.8	88 7	0.14 0.3		.17 0.42			30 0.25		0.30 0		0.45 0.59		0.08	0.35
OS5	4.37			36.87						41.24	В	2 0.0	8 0.35	5 95 0.8	0.88	100 0	.81 0.8	88 7	0.14 0.3						0.47 40		.50 65	0.45 0.59		0.13	
OS6	79.28				6.59	7.76				93.63	В	2 0.0	8 0.35	5 95 0.8	0.88	100 0	.81 0.8	88 7	0.14 0.3	9 11 0	.17 0.42	2 25 0.2	2 0.46	30 0.25		0.30 0	.50 65	0.45 0.59		0.10	0.36
OS7	20.65					7.57				28.22	В	2 0.0	8 0.35	5 95 0.8	0.88	100 0	.81 0.8	88 7	0.14 0.3	9 11 0	.17 0.42		2 0.46	30 0.25		0.30 0	.50 65	0.45 0.59	-	0.12	0.38
OS8	3.42		4.58							8.00	В	2 0.0	8 0.35	5 95 0.8	0.88	100 0	.81 0.8	88 7	0.14 0.3	9 12 0	.17 0.42	2 25 0.2	2 0.46	30 0.25	0.47 40	0.30 0	.50 65	0.45 0.59	58.1	0.50	0.65
TOTAL ONSITE	195.88	57.97	5.71	146.30	96.02	57.45	27.74	120.01	45.24	744.75		2 0.08	3 0.35	5 95 0.8	1 0.88	100 0.	.81 0.8	38 7	0.14 0.3	9 11 0.	.17 0.42	2 25 0.2	2 0.46	30 0.25	0.47 40	0.30 0.	50 65	0.45 0.59	24.9	0.24	0.47
TOTAL OFFSITE	253.07	0.00	4.58	36.87	6.59	7.76	0.00	0.00	0.00	316.44		2 0.08	3 0.35	5 95 0.8	1 0.88	100 0.	.81 0.8	38 7	0.14 0.3	9 11 0.	.17 0.42	2 25 0.2	2 0.46	30 0.25	0.47 40	0.30 0.	50 65	0.45 0.59	4.7	0.10	0.36
GRAND TOTAL	448.95	57.97	10.29	183.17	102.61	65.21	27.74	120.01	45.24	1061.19		2 0.08	3 0.35	5 95 0.8	1 0.88	100 0.	.81 0.8	38 7	0.14 0.3	9 11 0.	.17 0.42	2 25 0.2	2 0.46	30 0.25	0.47 40	0.30 0.	50 65	0.45 0.59	18.9	0.20	0.44
	NOTES																														

NOTES: \* The areas highlighted in OS6 & OS7 is on-site tributary area. These figures are included in the on-site area total and excluded from the offsite area total.

## **FLYING HORSE NORTH PARCELS 1-6**

# HROPOSED CONDITIONS

# HRGreen EL PASO COUNTY, COLORADO

					TIME	OF CON	CENTRAT	ION					
BAS	IN DATA		OVERI	AND TIM	E (T <sub>i</sub> )		TRAV	EL TIME ('	$T_t$		TOTAL	tc=(L/180)+10	Design tc
DESIGNATION	C <sub>5</sub>	AREA (ac)	LENGTH (ft)	SLOPE %	t <sub>i</sub> (min)	C <sub>V</sub>	LENGTH (ft)	SLOPE %	V (ft/s)	t <sub>t</sub> (min)	t <sub>c</sub> (min)	tc max	tc design (min)
А	0.17	74.11	100	4.0	10.8	20	1650	2.0	2.8	9.7	20.5	19.7	19.7
A1	0.14	12.58	100	3.0	12.2	7	850	3.0	1.2	11.7	23.9	15.3	15.3
A2	0.15	6.53	100	3.0	12.1	7	800	3.0	1.2	11.0	23.1	15.0	15.0
В	0.22	32.69	100	4.0	10.2	20	1265	4.0	4.0	5.3	15.5	17.6	15.5
С	0.26	121.03	100	1.0	15.5	20	3020	1.0	2.0	25.2	40.6	27.3	27.3
D	0.23	86.16	100	2.0	12.6	20	2750	2.5	3.2	14.5	27.1	25.8	25.8
E	0.37	52.36	100	5.0	7.8	20	1750	4.0	4.0	7.3	15.1	20.3	15.1
F	0.19	197.45	100	4.0	10.5	20	3600	3.0	3.5	17.3	27.9	30.6	27.9
G	0.16	27.30	100	25.0	5.9	20	1600	3.0	3.5	7.7	13.6	19.4	13.6
Н	0.14	74.02	100	5.0	10.3	7	500	5.0	1.6	5.3	15.6	13.3	13.3
	0.23	7.13	100	5.0	9.3	20	900	5.0	4.5	3.4	12.7	15.6	12.7
J	0.74	15.76	100	5.0	3.9	20	350	5.0	4.5	1.3	5.2	12.5	5.2
K	0.74	18.00	100	10.0	3.1	20	1000	7.0	5.3	3.1	6.2	16.1	6.2
L	0.52	7.09	100	25.0	3.6	20	250	12.0	6.9	0.6	5.0	11.9	5.0
М	0.52	4.97	100	5.5	6.0	20	1050	2.0	2.8	6.2	12.2	16.4	12.2
OS1	0.08	18.99	300	7.0	16.9	10	300	7.0	2.6	1.9	18.8	13.3	13.3
OS2	0.08	36.39	300	4.0	20.4	10	1300	4.0	2.0	10.8	31.2	18.9	18.9
OS3	0.08	25.25	300	6.0	17.8	10	900	6.0	2.4	6.1	23.9	16.7	16.7
OS4	0.08	72.29	300	7.0	16.9	10	1320	6.0	2.4	9.0	25.9	19.0	19.0
OS5	0.13	41.24	300	5.0	18.0	10	1900	5.0	2.2	14.2	32.2	22.2	22.2
OS6	0.10	93.63	100	2.5	13.5	15	3400	2.5	2.4	23.9	37.4	29.4	29.4
OS7	0.12	28.22	100	5.0	10.5	15	1600	5.0	3.4	8.0	18.5	19.4	18.5
OS8	0.50	8.00	OVERR	IDEN	#VALUE!	20	OVERF	RIDEN	0.0	######	#VALUE!	#VALUE!	#VALUE!

FORMULAS:

$$t_i = \frac{0.395(1.1 - C_5)\sqrt{L}}{S^{0.33}}$$

 $V = C_v S_w^{0.5}$ 

$$V = C_v S_w^{0.5}$$

Table 6-7. Conveyance Coefficient,  $C_{\nu}$ 

Type of Land Surface	$C_{\nu}$
Heavy meadow	2.5
Tillage/field	5
Riprap (not buried)*	6.5
Short pasture and lawns	7
Nearly bare ground	10
Grassed waterway	15
Paved areas and shallow paved swales	20

For buried riprap, select  $C_v$  value based on type of vegetative cover.

Calc'd by: DLH

Checked by: RDL

#### Date: 10/19/2023



<u>Calc'd by:</u> DLH

Checked by: RDL

Date: 10/19/2023

DESIGN STORM: 5-YEAR

		_		Ι	DIRECT	r Rung	OFF		то	TAL R	UNO	FF	0\	/ERLAN	ID		PI	PE		TI	RAVEL 1	ГІМЕ	
DESIGN POINT(S)	ULTIMATEDESIGN PONT	BASIN ID	AREA (ac)	C5	t <sub>c</sub> (min)	C₅*A (ac)	/ (in./ hr.)	Q (cfs)	ł <sub>c</sub> (min)	C <sub>5</sub> *A (ac)	/ (in./ hr.)	Q (cfs)	Q <sub>street</sub> (cfs)	C₅*A (ac)	SLOPE %	Q <sub>PIPE</sub> (cfs)	C₅*A (ac)	SLOPE %	PIPE SIZE (FT)	LENGTH (FT)	VEL. (FPS)	TRAVEL TIME (min)	
1, 2, 3	3	А	74.11	0.17	19.7	12.51	3.11	38.9															D
4	6	A1	12.58	0.14	15.3	1.73	3.49																DIRECTLY DRAINS OFFSITE,
5, 6	6	A2	6.53	0.15	15.0	0.96	3.52	3.4															DIRECTLY DRAINS OFFSITE,
7	7	в	32.69	0.22	15.5	7.09	3.47	24.6															D
10, 11	11	С	121.03	0.26	27.3	31.06	2.62	81.4															
13	13	D	86.16	0.23	25.8	20.24																	DE
14, 15	15	E		0.37																			
17	17	F	197.45																				
18	18	G	27.30																				
19	19	н	74.02																				DIRECT
6, 20	6	Ι	7.13																				

#### REMARKS

DETENTION IN POND A, OUTLETS TO EX. FIL. NO. 1 POND 13

E, CONVEYS OFFSITE FLOW THROUGH THE DEVELOPMENT. ULTIMATELY OUTFALLS TO EX. FIL. NO. 1 POND 13.

E, CONVEYS OFFSITE FLOW THROUGH THE DEVELOPMENT. ULTIMATELY OUTFALLS TO EX. FIL. NO. 1 POND 13.

DETENTION IN POND B, OUTLETS TO EX. FIL. NO. 1 POND 13

DETENTION IN POND C. OUTLETS OFFSITE DUE NORTH.

DETENTION IN POND D. OUTLETS OFFSITE DUE NORTHWEST.

DETENTION IN POND E. OUTLETS OFFSITE DUE NORTH.

DETENTION IN POND F. OUTLETS ONSITE DUE NORTH.

DETENTION IN POND G. OUTLETS ONSITE DUE NORTH.

CTLY DRAINS OFFSITE. RUNOFF REDUCTION VIA GRASS BUFFERS.

DIRECTLY DRAINS OFFSITE TO EX. FIL. NO. 1 POND 13



<u>Calc'd by:</u> DLH

Checked by: RDL

Date: 10/19/2023

DESIGN STORM: 5-YEAR

		_		I	DIRECT	RUN	OFF		то	TAL R	UNO	FF	0\	/ERLAN	ND		PI	PE		TI	RAVEL '	ТІМЕ	
DESIGN POINT(S)	ULTIMATEDESIGN Pont	BASIN ID	AREA (ac)	c°	t <sub>c</sub> (min)	C₅*A (ac)	/ (in./ hr.)	Q (cfs)	ł <sub>c</sub> (min)	C₅*A (ac)	/ (in./ hr.)	Q (cfs)	Q <sub>street</sub> (cfs)	C <sub>5</sub> *A (ac)	SLOPE %	Q <sub>PIPE</sub> (cfs)	C₅*A (ac)	SLOPE %	PIPE SIZE (FT)	LENGTH (FT)	VEL. (FPS)	TRAVEL TIME (min)	
21	21	J	15.76	0.74	5.2	11.67	5.12	59.8															
22, Pond 8 (Fil. 1)	22	к	18.00	0.74	6.2	13.30	4.84	64.4															DETENTION IN POND K
23, Pond 8 (Fil. 1)	23	L	7.09																				DRAINS OF
24	6	М	4.97	0.52															1				DRAINS INTO
1, 2, 3	3	OS1	18.99	0.08																			DRAINS THROU
4, 5, 6	6	OS2	36.39																				DRAINS THROUGH
6, 8, 9	6	083	25.25																				DRAINS THRO
12, 13	13	033 0S4	72.29																				
16, 17	17	OS5	41.24																				
6	6	OS6	93.63																				
6, 9	6	OS7	28.22	0.12	18.5	3.32	3.21	10.6															
25	6	OS8	8.00	0.50		3.98						3.8											F.H.N. FILIN

#### REMARKS

DETENTION IN POND J. OUTLETS OFFSITE DUE WEST.

D K. OUTLETS OFFSITE DUE WEST. ULTIMATELY DRAINS TO EX. FIL. NO. 1 POND 8.

OFFSITE TO GOLF COURSE AND ULTIMATLEY TO EX. FIL. NO. 1 POND 8.

ITO ADJACENT ALLEN RANCH ROAD AND INTO F.H.N. FILING NO. 3 POND

DUGH TO BASIN A. TWO CULVERT PIPE LOCATIONS TO CROSS ROADWAYS.

GH TO BASINS A1 AND A2. ULTIMATELY OUTFALLS TO EX. FIL. NO. 1 POND 13.

ROUGH TO BASIN OS7. ULTIMATELY OUTFALLS TO EX. FIL. NO. 1 POND 13.

DRAINS THROUGH TO BASIN D. DETENTION IN POND D.

DRAINS THROUGH TO BASIN F. DETENTION IN POND F.

DIRECTLY DRAINS TO EX. FIL. NO. 1 POND 13

DIRECTLY DRAINS TO EX. FIL. NO. 1 POND 13

LING NO. 3 POND DRAINS DIRECTLY DRAINS TO EX. FIL. NO. 1 POND 13



<u>Calc'd by:</u> DLH

<u>Checked by:</u> RDL

<u>Date:</u> 10/19/2023

DESIGN STORM: 100-YEAR

ľ			_		C	DIRECT	RUN	OFF			TOTAL R	UNOFF	•	0\	/ERLAN	ND		PI	PE		TF	RAVEL	TIME	
	DESIGN POINT(S)	ULTIMATEDESIGN Pont	DI NISVA	AREA (ac)	C <sub>100</sub>	t <sub>c</sub> (min)	C <sub>100</sub> *A (ac)	/ (in./ hr.)	Q (cfs)	t <sub>c</sub> (min)	C <sub>100</sub> *A (ac)	/ (in./ hr.)	Q (cfs)	Q <sub>street</sub> (cfs)	C <sub>100</sub> *A (ac)	SLOPE %	Q <sub>PIPE</sub> (cfs)	C <sub>100</sub> *A (ac)	SLOPE %	PIPE SIZE (ft)	LENGTH (ft)	VEL. (ft/s)	TRAVEL TIME (min)	
	1, 2, 3	3	А	74.11	0.42	19.7	30.95	5.22	161.6															
ľ	4	6	A1	12.58																				DIRECTLY DRAIN
Ī	5, 6	6	A2	6.53	0.40	15.0	2.60	5.91	15.3															DIRECTLY DRAIN
I	7	7	В	32.69	0.45	15.5	14.77	5.83	86.1															
	10, 11	11	С	121.03	0.47	27.3	57.15	4.40	251.4															
	13	13	D	86.16	0.45	25.8	39.00	4.54	177.1															
	14, 15	15	Е	52.36					171.0															
	17	17	F	197.45	0.43	27.9			366.3															
	18	18	G	27.30	0.41	13.6	11.10	6.16	68.4															
	19	19	Н	74.02																				DIF
	6, 20	6	I	7.13																				

#### REMARKS

DETENTION IN POND A, OUTLETS TO EX. FIL. NO. 1 POND 13

AINS OFFSITE, CONVEYS OFFSITE FLOW THROUGH THE DEVELOPMENT. ULTIMATELY OUTFALLS TO EX. FIL. NO. 1 POND 13.

AINS OFFSITE, CONVEYS OFFSITE FLOW THROUGH THE DEVELOPMENT. ULTIMATELY OUTFALLS TO EX. FIL. NO. 1 POND 13.

DETENTION IN POND B, OUTLETS TO EX. FIL. NO. 1 POND 13

DETENTION IN POND C. OUTLETS OFFSITE DUE NORTH.

DETENTION IN POND D. OUTLETS OFFSITE DUE NORTHWEST.

DETENTION IN POND E. OUTLETS OFFSITE DUE NORTH.

DETENTION IN POND F. OUTLETS ONSITE DUE NORTH.

DETENTION IN POND G. OUTLETS ONSITE DUE NORTH.

DIRECTLY DRAINS OFFSITE. RUNOFF REDUCTION VIA GRASS BUFFERS.

DIRECTLY DRAINS OFFSITE TO EX. FIL. NO. 1 POND 13



<u>Calc'd by:</u> DLH

<u>Checked by:</u> RDL

<u>Date:</u> 10/19/2023

DESIGN STORM: 100-YEAR

		_		0	DIRECT	RUNG	OFF			TOTAL R	UNOFF		0	VERLAN	ND		PI	PE		TF	RAVEL	TIME	
DESIGN POINT(S)	ULTIMATEDESIGN PONT	BASIN ID	AREA (ac)	C <sub>100</sub>	t <sub>c</sub> (min)	C <sub>100</sub> *A (ac)	/ (in./ hr.)	Q (cfs)	t <sub>c</sub> (min)	C <sub>100</sub> *A (ac)	/ (in./ hr.)	Q (cfs)	Q <sub>street</sub> (cfs)	C <sub>100</sub> *A (ac)	SLOPE %	Q <sub>PIPE</sub> (cfs)	C <sub>100</sub> *A (ac)	SLOPE %	PIPE SIZE (ft)	LENGTH (ft)	VEL. (ft/s)	TRAVEL TIME (min)	
21	21	J	15.76	0.83	5.2	13.07	8.60	112.4															
22, Pond 8 (Fil. 1)	22	к	18.00	0.83	6.2	14.91	8.13	121.2															DETENTION IN P
23, Pond 8 (Fil. 1)	23	L	7.09	0.67	5.0	4.74	8.68	41.1															DRAIN
24	6	М	4.97	0.67	12.2	3.32	6.42	21.3															DRAINS
1, 2, 3	3	OS1	18.99	0.35	13.3	6.65	6.21	41.3															DRAINS TH
4, 5, 6	6	OS2	36.39	0.35	18.9	12.74	5.33	67.9															DRAINS THRO
6, 8, 9	6	OS3	25.25	0.35	16.7	8.84	5.65	49.9															DRAINS T
12, 13	13	OS4	72.29	0.35	19.0	25.30	5.32	134.5															
16, 17	17	OS5	41.24	0.39	22.2	16.01	4.92	78.8															
6	6	OS6	93.63	0.36	29.4	34.07	4.21	143.5															
6, 9	6	OS7	28.22			10.71																	
25	6	OS8	8.00			5.23						4.4											F.H.N.

#### REMARKS

DETENTION IN POND J. OUTLETS OFFSITE DUE WEST.

POND K. OUTLETS OFFSITE DUE WEST. ULTIMATELY DRAINS TO EX. FIL. NO. 1 POND 8

INS OFFSITE TO GOLF COURSE AND ULTIMATLEY TO EX. FIL. NO. 1 POND 8.

NS INTO ADJACENT ALLEN RANCH ROAD AND INTO F.H.N. FILING NO. 3 POND

THROUGH TO BASIN A. TWO CULVERT PIPE LOCATIONS TO CROSS ROADWAYS.

ROUGH TO BASINS A1 AND A2. ULTIMATELY OUTFALLS TO EX. FIL. NO. 1 POND 13.

THROUGH TO BASIN OS7. ULTIMATELY OUTFALLS TO EX. FIL. NO. 1 POND 13.

DRAINS THROUGH TO BASIN D. DETENTION IN POND D.

DRAINS THROUGH TO BASIN F. DETENTION IN POND F.

DIRECTLY DRAINS TO EX. FIL. NO. 1 POND 13

DIRECTLY DRAINS TO EX. FIL. NO. 1 POND 13

N. FILING NO. 3 POND DRAINS DIRECTLY DRAINS TO EX. FIL. NO. 1 POND 13



Flying Horse North Phase 2 Parcels 1-6 Preliminary Drainage Report Project No.: 211030

Appendix C:

Hydraulic Calculations

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Tuesday, Oct 10 2023

= 0.22

#### Section A-A OFF-SITE CHANNEL: 5-YR

#### Trapezoidal

= 50.00
= 89.00, 8.00
= 2.00
= 1.00
= 2.70
= 0.035

#### Calculations

Compute by:	Known Q
Known Q (cfs)	= 18.30

# CHANNEL LOCATION: WITHIN BASIN OS4

# HighlightedDepth (ft)= 0.17Q (cfs)= 18.30Area (sqft)= 9.90Velocity (ft/s)= 1.85Wetted Perim (ft)= 66.50Crit Depth, Yc (ft)= 0.16Top Width (ft)= 66.49

EGL (ft)

Elev (ft) Depth (ft) Section 4.00 -- 3.00 3.50 -- 2.50 3.00 -- 2.00 2.50 -- 1.50 2.00 -- 1.00 1.50 -- 0.50 1.00 -- 0.00 0.50 -0.50 0 50 100 150 200 250 300 350

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Tuesday, Oct 10 2023

#### Section A-A OFF-SITE CHANNEL: 100-YR

#### Trapezoidal

Bottom Width (ft)	= 50.00
Side Slopes (z:1)	= 89.00, 8.00
Total Depth (ft)	= 2.00
Invert Elev (ft)	= 1.00
Slope (%)	= 2.70
N-Value	= 0.035

#### Calculations

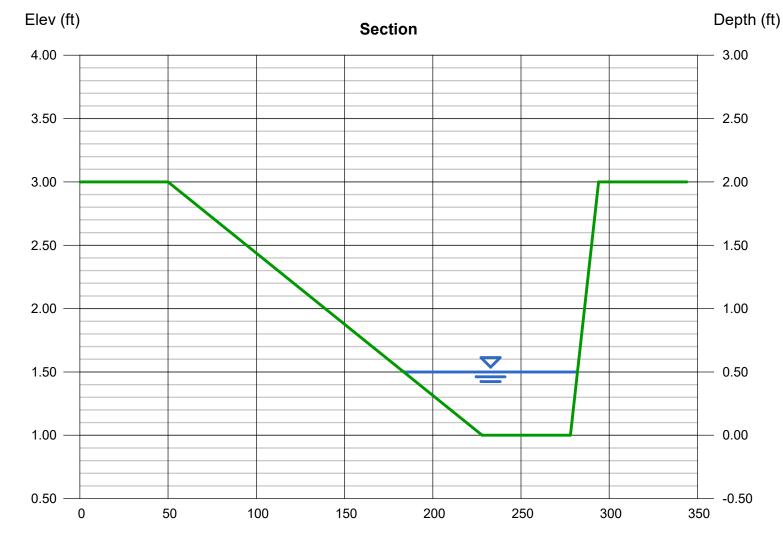
Compute by: Known Q Known Q (cfs) = 134.50

#### CHANNEL LOCATION: WITHIN BASIN OS4

#### Highlighted

Depth (ft)	= 0.50
Q (cfs)	= 134.50
Area (sqft)	= 37.12
Velocity (ft/s)	= 3.62
Wetted Perim (ft)	= 98.53
Crit Depth, Yc (ft)	= 0.52
Top Width (ft)	= 98.50
EGL (ft)	= 0.70

Recommended BMP: North American Green Rollmax Permanent Turf Reinforcement Mat P300 (or equiv.) Permissible Velocity (ft/s) = 9.0 Permissible Shear Stress (lb/ft^2) = 3.0



Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Q

Monday, Oct 9 2023

#### Section B-B OFF-SITE CHANNEL: 5-YR

#### Triangular

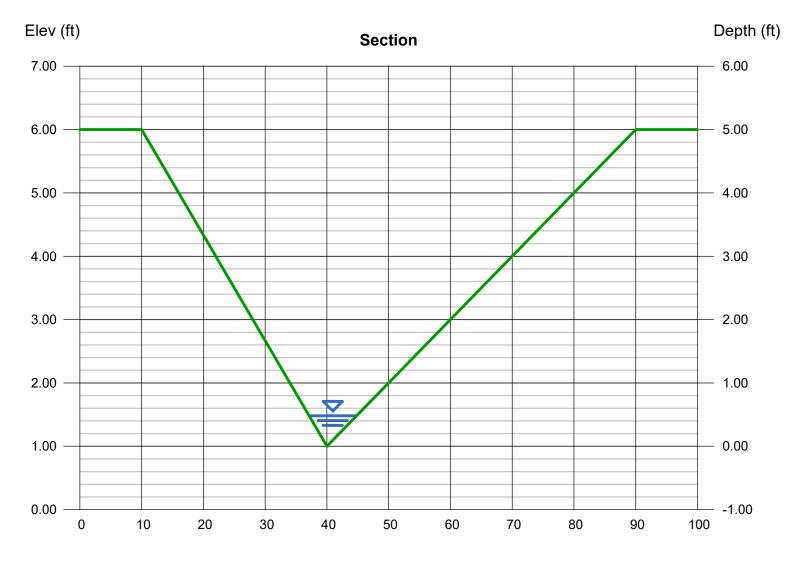
Side Slopes (z:1)	= 6.00, 10.00
Total Depth (ft)	= 5.00
Invert Elev (ft)	= 1.00
Slope (%)	= 5.70
N-Value	= 0.035

#### Calculations

Compute by:	Known
Known Q (cfs)	= 6.80

CHANNEL LOCATION: WITHIN BASIN OS3

=	0.48
=	6.800
=	1.84
=	3.69
=	7.74
=	0.54
=	7.68
=	0.69



Reach (ft)

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Monday, Oct 9 2023

#### Section B-B OFF-SITE CHANNEL: 100-YR

#### Triangular

Side Slopes (z:1)	= 6.00, 10.00
Total Depth (ft)	= 5.00
Invert Elev (ft)	= 1.00
Slope (%)	= 5.70
N-Value	= 0.035

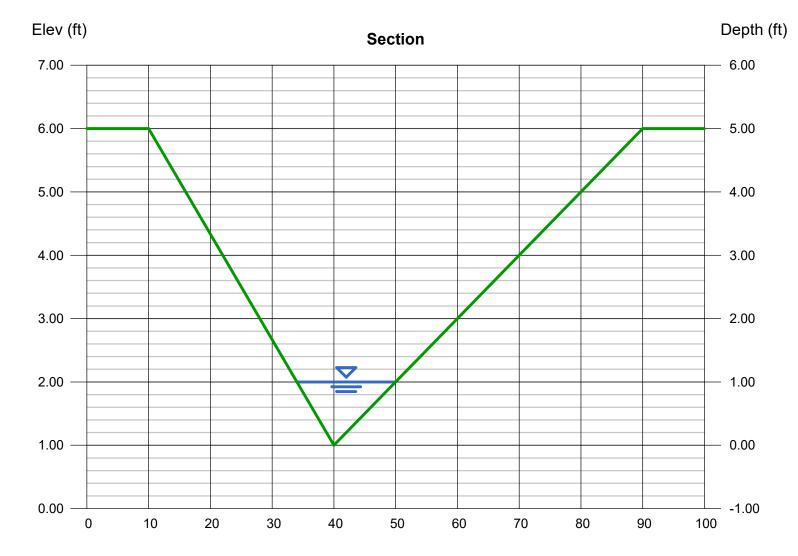
#### Calculations

Compute by:Known QKnown Q (cfs)= 49.90

#### CHANNEL LOCATION: WITHIN BASIN OS3

Highlighted	
Depth (ft)	= 1.00
Q (cfs)	= 49.90
Area (sqft)	= 8.00
Velocity (ft/s)	= 6.24
Wetted Perim (ft)	= 16.13
Crit Depth, Yc (ft)	= 1.20
Top Width (ft)	= 16.00
EGL (ft)	= 1.60

Recommended BMP: Rollmax Permanent Turf Reinforcement Mat TMAX (or equiv.) Permissible Velocity (ft/s) = 25.0 Permissible Shear Stress (lb/ft^2) = 15.0



Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Tuesday, Oct 10 2023

## Section C-C OFF-SITE CHANNEL: 5-YR

Trapezoidal
-------------

Bottom Width (ft)	= 23.00
Side Slopes (z:1)	= 39.00, 10.00
Total Depth (ft)	= 1.20
Invert Elev (ft)	= 1.00
Slope (%)	= 6.60
N-Value	= 0.035

#### Calculations

Compute by:	Known Q
Known Q (cfs)	= 9.20

# CHANNEL LOCATION: WITHIN BASIN OS2

Elev (ft)	Section	Depth (f
3.00		2.00
2.50		1.50
2.00		1.00
2.00		1.00
1.50		0.50
1.00		0.00
0.50 0 10		-0.50

#### Highlighted

Depth (ft)	=	0.14
Q (cfs)	=	9.200
Area (sqft)	=	3.70
Velocity (ft/s)	=	2.49
Wetted Perim (ft)	=	29.87
Crit Depth, Yc (ft)	=	0.17
Top Width (ft)	=	29.86
EGL (ft)	=	0.24

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Tuesday, Oct 10 2023

#### Section C-C OFF-SITE CHANNEL: 100-YR

#### Trapezoidal

Bottom Width (ft)	= 23.00
Side Slopes (z:1)	= 39.00, 10.00
Total Depth (ft)	= 1.20
Invert Elev (ft)	= 1.00
Slope (%)	= 6.60
N-Value	= 0.035

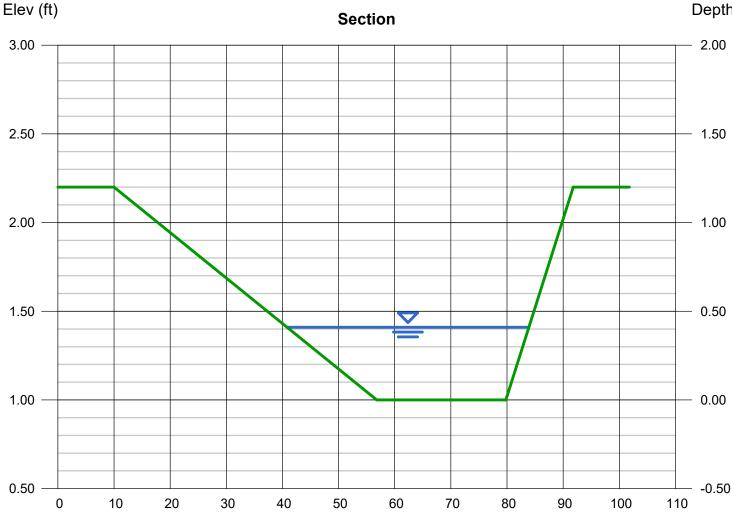
#### Calculations

Compute by: Known Q Known Q (cfs) = 67.90

#### CHANNEL LOCATION: WITHIN BASIN OS2

Highlighted		
Depth (ft)	=	0.41
Q (cfs)	=	67.90
Area (sqft)	=	13.55
Velocity (ft/s)	=	5.01
Wetted Perim (ft)	=	43.12
Crit Depth, Yc (ft)	=	0.54
Top Width (ft)	=	43.09
EGL (ft)	=	0.80

Recommended BMP: North American Green Rollmax Permanent Turf Reinforcement Mat P300 (or equiv.) Permissible Velocity (ft/s) = 9.0 Permissible Shear Stress ( $lb/ft^{2}$ ) = 3.0



Depth (ft)

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Tuesday, Oct 10 2023

#### Section D-D ON-SITE CHANNEL: 5-YR

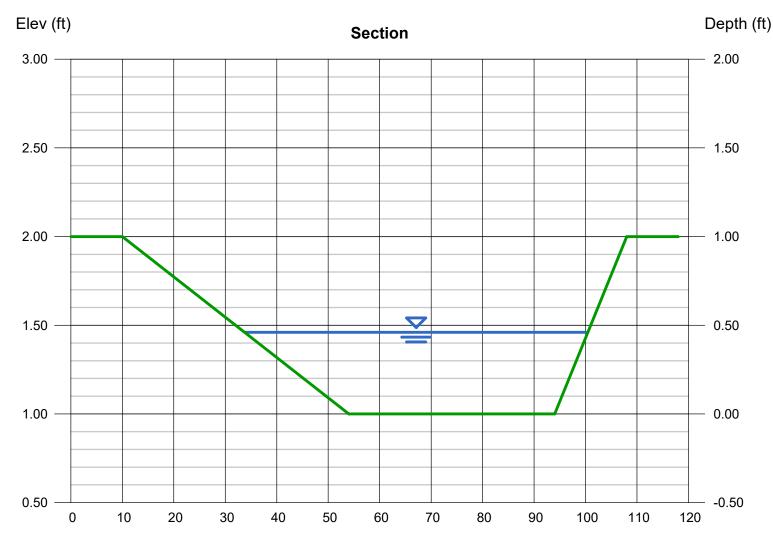
Trapezoidal	
Bottom Width (ft)	= 40.00
Side Slopes (z:1)	= 44.00, 14.00
Total Depth (ft)	= 1.00
Invert Elev (ft)	= 1.00
Slope (%)	= 2.50
N-Value	= 0.035

#### Calculations

Compute by:	Known Q
Known Q (cfs)	= 81.40

# CHANNEL LOCATION: WITHIN BASIN C

#### Highlighted Depth (ft) = 0.46 Q (cfs) = 81.40 Area (sqft) = 24.54 Velocity (ft/s) = 3.32 Wetted Perim (ft) = 66.70 Crit Depth, Yc (ft) = 0.46 Top Width (ft) = 66.68 EGL (ft) = 0.63



Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

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#### Section D-D ON-SITE CHANNEL: 100-YR

#### Trapezoidal

Bottom Width (ft)	= 40.00
Side Slopes (z:1)	= 44.00, 14.00
Total Depth (ft)	= 1.00
Invert Elev (ft)	= 1.00
Slope (%)	= 2.50
N-Value	= 0.035

#### Calculations

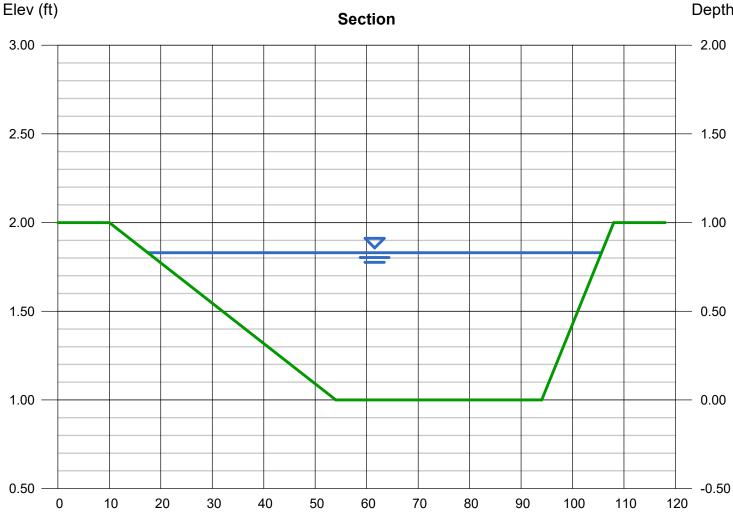
Compute by: Known Q Known Q (cfs) = 251.40

#### CHANNEL LOCATION: WITHIN BASIN C

## Highlighted

J J	
Depth (ft)	= 0.83
Q (cfs)	= 251.40
Area (sqft)	= 53.18
Velocity (ft/s)	= 4.73
Wetted Perim (ft)	= 88.18
Crit Depth, Yc (ft)	= 0.87
Top Width (ft)	= 88.14
EGL (ft)	= 1.18

Recommended BMP: North American Green **Rollmax Permanent Turf Reinforcement Mat** P300 (or equiv.) Permissible Velocity (ft/s) = 9.0 Permissible Shear Stress (lb/ft^2) = 3.0



Depth (ft)

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Tuesday, Oct 10 2023

#### Section E-E ON-SITE CHANNEL: 5-YR

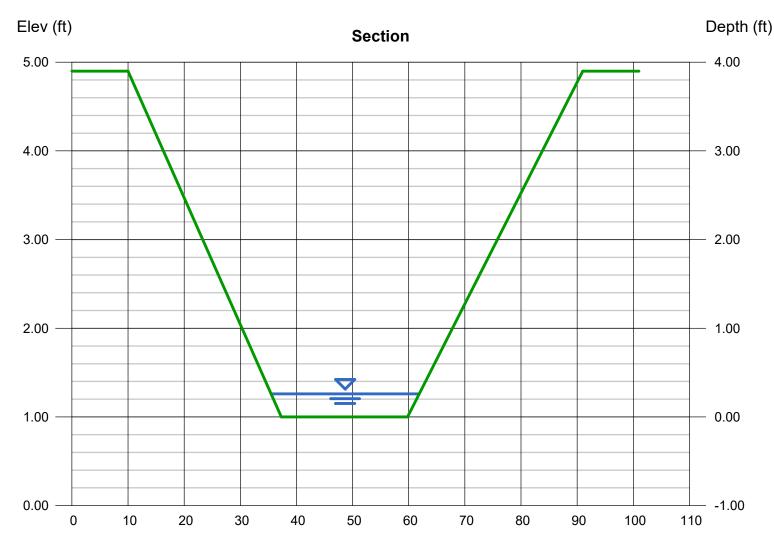
Trapezoidal	
Bottom Width (ft)	= 22.50
Side Slopes (z:1)	= 7.00, 8.00
Total Depth (ft)	= 3.90
Invert Elev (ft)	= 1.00
Slope (%)	= 2.10
N-Value	= 0.035

#### Calculations

Compute by: Known Q Known Q (cfs) = 14.50

CHANNEL LOCATION: WITHIN BASIN A

#### Highlighted Depth (ft) = 0.26 Q (cfs) = 14.50 Area (sqft) = 6.36 Velocity (ft/s) = 2.28 Wetted Perim (ft) = 26.43 Crit Depth, Yc (ft) = 0.23Top Width (ft) = 26.40 EGL (ft) = 0.34



Reach (ft)

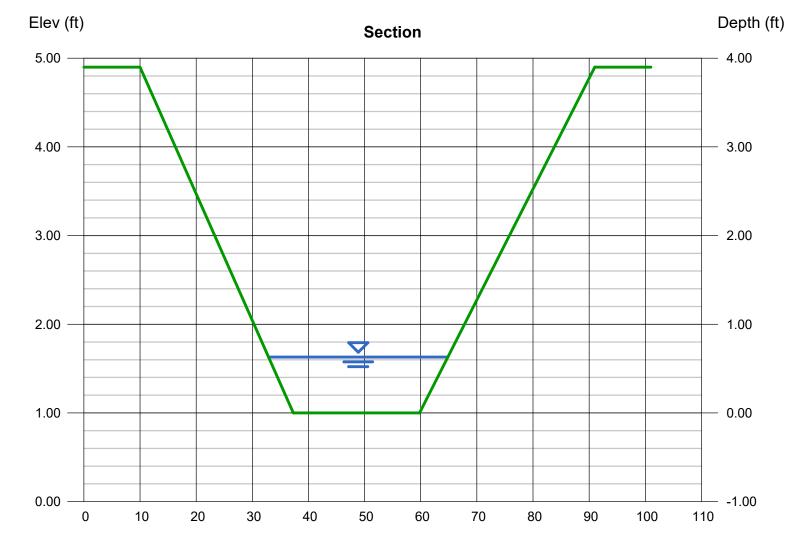
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Tuesday, Oct 10 2023

#### Section E-E ON-SITE CHANNEL: 100-YR

#### Trapezoidal Highlighted Bottom Width (ft) = 22.50 Depth (ft) = 0.63 Side Slopes (z:1) = 7.00, 8.00Q (cfs) = 69.10 Total Depth (ft) Area (sqft) = 3.90= 17.15Velocity (ft/s) Invert Elev (ft) = 1.00 = 4.03 Slope (%) = 2.10 Wetted Perim (ft) = 32.03 N-Value Crit Depth, Yc (ft) = 0.035= 0.62 Top Width (ft) = 31.95EGL (ft) Calculations = 0.88Compute by: Known Q = 69.10 Known Q (cfs) **Recommended BMP:** North American Green CHANNEL LOCATION: **Rollmax Permanent Turf Reinforcement Mat** WITHIN BASIN A P300 (or equiv.) Permissible Velocity (ft/s) = 9.0

Permissible Shear Stress ( $lb/ft^2$ ) = 3.0



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#### Section F-F ON-SITE CHANNEL: 5-YR

#### Triangular

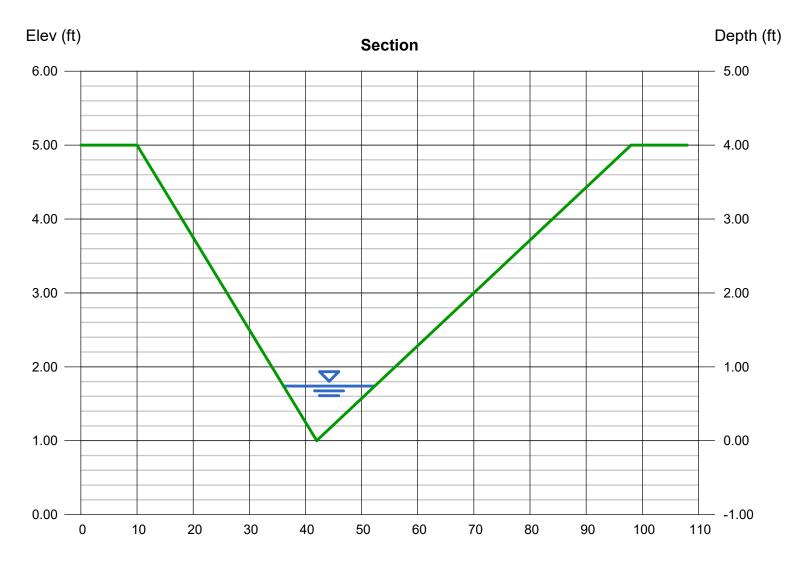
Side Slopes (z:1)	= 8.00, 14.00
Total Depth (ft)	= 4.00
Invert Elev (ft)	= 1.00
Slope (%)	= 2.10
N-Value	= 0.035

#### Calculations

Compute by:	Known Q
Known Q (cfs)	= 18.70

CHANNEL LOCATION: WITHIN BASIN A2

Highlighted		
Depth (ft)	=	0.74
Q (cfs)	=	18.70
Area (sqft)	=	6.02
Velocity (ft/s)	=	3.10
Wetted Perim (ft)	=	16.35
Crit Depth, Yc (ft)	=	0.71
Top Width (ft)	=	16.28
EGL (ft)	=	0.89



Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Tuesday, Oct 10 2023

#### Section F-F ON-SITE CHANNEL: 100-YR

#### Triangular

Side Šlopes (z:1)	= 8.00, 14.00
Total Depth (ft)	= 4.00
Invert Elev (ft)	= 1.00
Slope (%)	= 2.10
N-Value	= 0.035

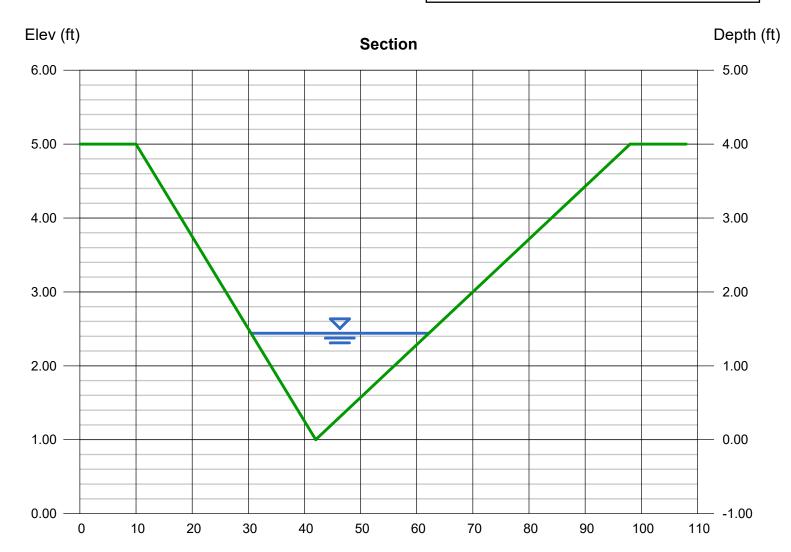
#### Calculations

Compute by:	Known Q
Known Q (cfs)	= 112.20
CHANNEL LOCATION:	

WITHIN BASIN A2

Highlighted		
Depth (ft)	=	1.44
Q (cfs)	=	112.20
Area (sqft)	=	22.81
Velocity (ft/s)	=	4.92
Wetted Perim (ft)	=	31.82
Crit Depth, Yc (ft)	=	1.46
Top Width (ft)	=	31.68
EGL (ft)	=	1.82

Recommended BMP: North American Green Rollmax Permanent Turf Reinforcement Mat P300 (or equiv.) Permissible Velocity (ft/s) = 9.0 Permissible Shear Stress (lb/ft^2) = 3.0



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#### Section G-G ON-SITE CHANNEL: 5-YR

#### Trapezoidal

Bottom Width (ft)	= 22.50
Side Slopes (z:1)	= 6.00, 21.00
Total Depth (ft)	= 4.00
Invert Elev (ft)	= 1.00
Slope (%)	= 5.30
N-Value	= 0.035

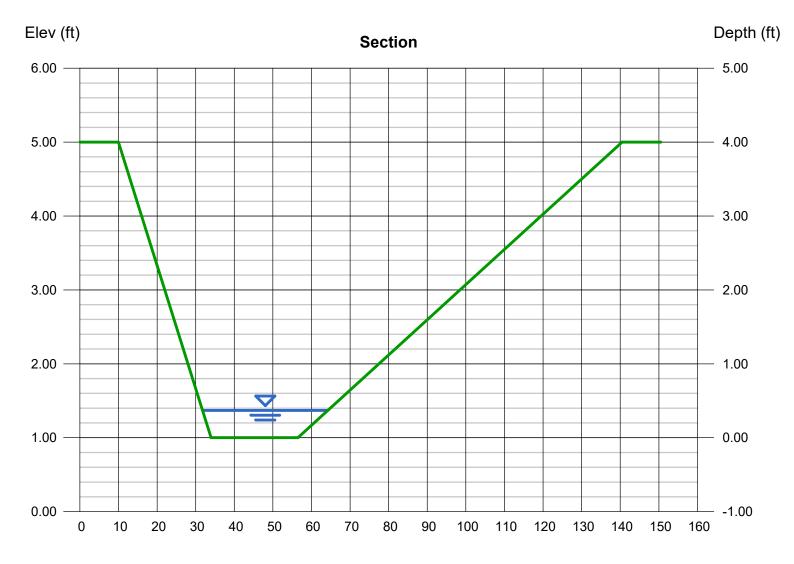
#### Calculations

Compute by:	Known Q
Known Q (cfs	) = 44.30

CHANNEL LOCATION: WITHIN BASIN F

# HighlightedDepth (ft)= 0.37Q (cfs)= 44.30Area (sqft)= 10.17

Velocity (ft/s)	= 4.35
Wetted Perim (ft)	= 32.53
Crit Depth, Yc (ft)	= 0.45
Top Width (ft)	= 32.49
EGL (ft)	= 0.66



Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Tuesday, Oct 10 2023

1.08

325.40

40.05

#### Section G-G ON-SITE CHANNEL: 100-YR

#### Trapezoidal

Bottom Width (ft)	= 22.50
Side Slopes (z:1)	= 6.00, 21.00
Total Depth (ft)	= 4.00
Invert Elev (ft)	= 1.00
Slope (%)	= 5.30
N-Value	= 0.035

#### Calculations

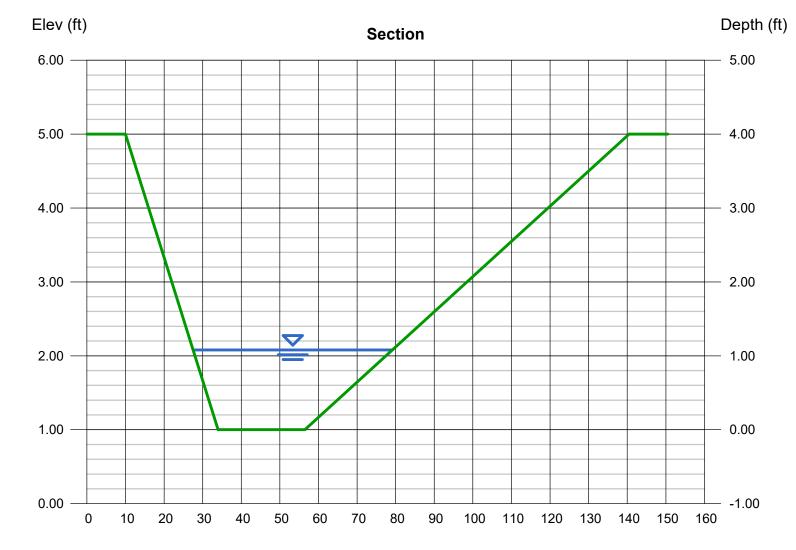
Compute by: Known Q = 325.40 Known Q (cfs)

#### CHANNEL LOCATION: WITHIN BASIN F

Highlighted	
Depth (ft)	=
Q (cfs)	=
Area (sqft)	=
Velocity (ft/s)	=

Velocity (ft/s)	= 8.13
Wetted Perim (ft)	= 51.78
Crit Depth, Yc (ft)	= 1.41
Top Width (ft)	= 51.66
EGL (ft)	= 2.11

Recommended BMP: Rollmax Permanent Turf Reinforcement Mat TMAX (or equiv.) Permissible Velocity (ft/s) = 25.0 Permissible Shear Stress (lb/ft^2) = 15.0



FRO	UDE NUMBI	ER CALCULATIONS	CALCULATED BY:	DLH	DATE:	10/10/2023
PF	ROJECT: 211	030 Parcels 1-6	CHECKED BY:	RL		
		Froude Nur	nber Calculations: 1	.00-YR		
		Gravitational		X-Sectional		
Section	Velocity	Constant	Hydraulic depth	Area	top Width	Froude #
-	ft/s	ft/s^2	ft	ft^2	ft	N/A
A-A	3.62	32.17	0.38	37.12	98.50	1.04
B-B	6.24	32.17	0.50	8.00	16.00	1.56
C-C	5.01	32.17	0.31	13.55	43.09	1.58
D-D	4.73	32.17	0.60	53.18	88.14	1.07
E-E	4.03	32.17	0.54	17.15	31.95	0.97
F-F	4.92	32.17	0.72	22.81	31.68	1.02
G-G	8.13	32.17	0.78	40.05	51.66	1.63

	Shear Stress Calculations: 100-YR					
Section	Unit Weight of Water	Depth of flow	Slope	Shear Stress		
-	lb/ft^3	ft	ft/ft	lb/ft^2		
A-A	62.43	0.50	0.03	0.84		
B-B	62.43	1.00	0.057	3.56		
C-C	62.43	0.41	0.066	1.69		
D-D	62.43	1.00	0.025	1.56		
E-E	62.43	0.63	0.021	0.83		
F-F	62.43	1.44	0.021	1.89		
G-G	62.43	1.08	0.053	3.57		

Channel Lining Determination						
Calculated Values		P300 Max Values				
Section	Shear Stress	Velocity	Shear Stress	Velocity	Lining Required	
A-A	0.84	3.62	3	9	P300	
B-B	3.56	6.24	3	9	TMAX	
C-C	1.69	5.01	3	9	P300	
D-D	1.56	4.73	3	9	P300	
E-E	0.83	4.03	3	9	P300	
F-F	1.89	4.92	3	9	P300	
G-G	3.57	8.13	3	9	TMAX	

# **Culvert Report**

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

#### **CULVERT-01**

Invert Elev Dn (ft) Pipe Length (ft)	= 7581.40 = 272.80	Calculations Qmin (cfs)	= 6.80
Slope (%)	= 3.92	Qmax (cfs)	= 49.90
Invert Elev Up (ft)	= 7592.09	Tailwater Elev (ft)	= (dc+D)
Rise (in)	= 48.0		,
Shape	= Circular	Highlighted	
Span (in)	= 48.0	Qtotal (cfs)	= 49.80
No. Barrels	= 1	Qpipe (cfs)	= 49.80
n-Value	= 0.012	Qovertop (cfs)	= 0.00
Culvert Type	= Circular Concrete	Veloc Dn (ft/s)	= 4.83
Culvert Entrance	= Square edge w/headwall (C)	Veloc Up (ft/s)	= 7.38
Coeff. K,M,c,Y,k	= 0.0098, 2, 0.0398, 0.67, 0.5	HGL Dn (ft)	= 7584.4
		HGL Up (ft)	= 7594.2
Embankment		Hw Elev (ft)	= 7595.1

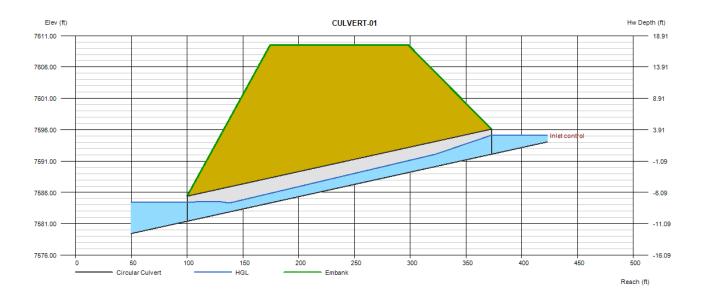
Top Elevation (ft)
Top Width (ft)
Crest Width (ft)

= 7609.50 = 124.00 = 100.00

CULVERT LOCATION: PARCEL 3, **BASIN B, CROSSING HOLMES ROAD, DESIGN POINT 8** 

Qmin (cfs)	= 6.80
Qmax (cfs)	= 49.90
Tailwater Elev (ft)	= (dc+D)/2

Qtotal (cfs)	= 49.80
Qpipe (cfs)	= 49.80
Qovertop (cfs)	= 0.00
Veloc Dn (ft/s)	= 4.83
Veloc Up (ft/s)	= 7.38
HGL Dn (ft)	= 7584.46
HGL Up (ft)	= 7594.21
Hw Elev (ft)	= 7595.13
Hw/D (ft)	= 0.76
Flow Regime	= Inlet Control



Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

# Culvert-02

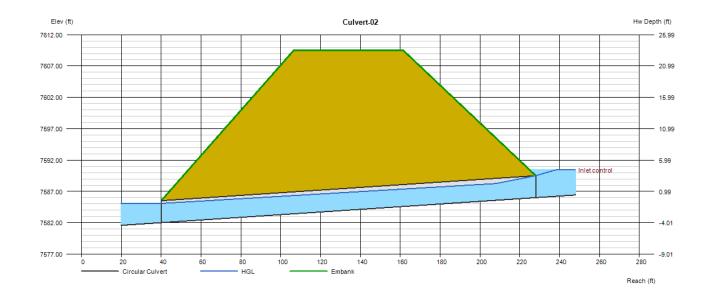
Invert Elev Dn (ft)	= 7582.02	Calculations	
Pipe Length (ft)	= 188.00	Qmin (cfs)	= 1
Slope (%)	= 2.12	Qmax (cfs)	= 7
Invert Elev Up (ft)	= 7586.01	Tailwater Élev (ft)	= (
Rise (in)	= 42.0		
Shape	= Circular	Highlighted	
Span (in)	= 42.0	Qtotal (cfs)	= 7
No. Barrels	= 1	Qpipe (cfs)	= 7
n-Value	= 0.012	Qovertop (cfs)	= 0
Culvert Type	<ul> <li>Circular Concrete</li> </ul>	Veloc Dn (ft/s)	= 7
Culvert Entrance	= Square edge w/headwall (C)	Veloc Up (ft/s)	= 9
Coeff. K,M,c,Y,k	= 0.0098, 2, 0.0398, 0.67, 0.5	HGL Dn (ft)	= 7
		HGL Up (ft)	= 7
			_

# Embankment

Top Elevation (ft) = 7609.50 Top Width (ft) = 55.00 Crest Width (ft) = 100.00 CULVERT LOCATION: PARCEL 3, **BASIN A1-A2, CROSSING** HOLMES ROAD, DESIGN POINT 4

Qmin (cfs)	= 10.00
Qmax (cfs)	= 70.00
Tailwater Elev (ft)	= (dc+D)/2

inginginoa	
Qtotal (cfs)	= 70.00
Qpipe (cfs)	= 70.00
Qovertop (cfs)	= 0.00
Veloc Dn (ft/s)	= 7.85
Veloc Up (ft/s)	= 9.06
HGL Dn (ft)	= 7585.08
HGL Up (ft)	= 7588.63
Hw Elev (ft)	= 7590.42
Hw/D (ft)	= 1.26
Flow Regime	= Inlet Control



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# **CULVERT-03**

Invert Elev Dn (ft) Pipe Length (ft)	= 7601.62 = 167.11	Calculations Qmin (cfs)	= ;
Slope (%)	= 2.94	Qmax (cfs)	= -
Invert Elev Up (ft)	= 7606.53	Tailwater Elev (ft)	=
Rise (in)	= 48.0		
Shape	= Circular	Highlighted	
Span (in)	= 48.0	Qtotal (cfs)	= ;
No. Barrels	= 1	Qpipe (cfs)	= ;
n-Value	= 0.012	Qovertop (cfs)	= (
Culvert Type	<ul> <li>Circular Concrete</li> </ul>	Veloc Dn (ft/s)	= (
Culvert Entrance	= Square edge w/headwall (C)	Veloc Up (ft/s)	= ;
Coeff. K,M,c,Y,k	= 0.0098, 2, 0.0398, 0.67, 0.5	HGL Dn (ft)	= '
		HGL Up (ft)	= '

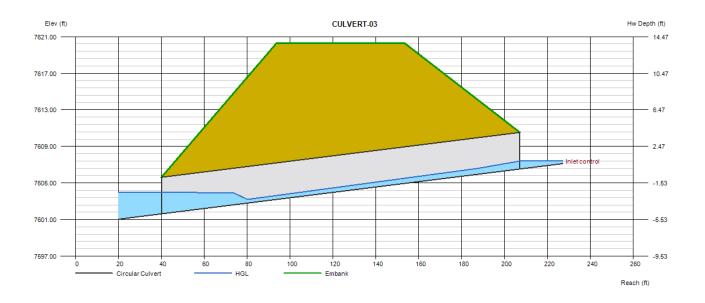
# Embankment

Top Elevation (ft) = 7620.26 Top Width (ft) = 60.00 Crest Width (ft) = 100.00 CULVERT LOCATION: PARCEL 3, **BASIN A, CROSSING HOLMES ROAD, DESIGN POINT 2** 

### Monday, Oct 9 2023

Qmin (cfs)	= 5.60
Qmax (cfs)	= 41.30
Tailwater Elev (ft)	= (dc+D)/2

00	
Qtotal (cfs)	= 5.60
Qpipe (cfs)	= 5.60
Qovertop (cfs)	= 0.00
Veloc Dn (ft/s)	= 0.73
Veloc Up (ft/s)	= 3.92
HGL Dn (ft)	= 7603.96
HGL Up (ft)	= 7607.21
Hw Elev (ft)	= 7607.40
Hw/D (ft)	= 0.22
Flow Regime	= Inlet Control



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# **CULVERT-04**

Invert Elev Dn (ft) Pipe Length (ft) Slope (%) Invert Elev Up (ft)	= 7596.23 = 183.00 = 2.82 = 7601.39	<b>Calculations</b> Qmin (cfs) Qmax (cfs) Tailwater Elev (ft)
Rise (in)	= 36.0	
Shape	= Circular	Highlighted
Span (in)	= 36.0	Qtotal (cfs)
No. Barrels	= 1	Qpipe (cfs)
n-Value	= 0.012	Qovertop (cfs)
Culvert Type	= Circular Concrete	Veloc Dn (ft/s)
Culvert Entrance	= Square edge w/headwall (C)	Veloc Up (ft/s)
Coeff. K,M,c,Y,k	= 0.0098, 2, 0.0398, 0.67, 0.5	HGL Dn (ft)
		HGL Up (ft)

# Embankment

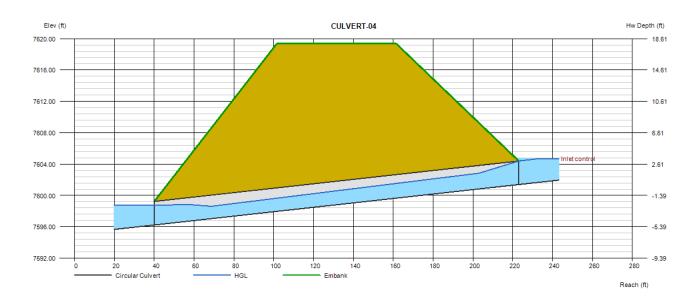
Top Elevation (ft) Top Width (ft) Crest Width (ft)

= 7619.36 = 60.00 = 50.00

CULVERT LOCATION: PARCEL 3, **BASIN A, CROSSING HOLMES ROAD, DESIGN POINT 1** 

Qmin (cfs)	= 5.60
Qmax (cfs)	= 41.30
Tailwater Elev (ft)	= (dc+D)/2

inginginea		
Qtotal (cfs)	=	40.60
Qpipe (cfs)	=	40.60
Qovertop (cfs)	=	0.00
Veloc Dn (ft/s)	=	6.37
Veloc Up (ft/s)	=	7.79
HGL Dn (ft)	=	7598.77
HGL Up (ft)	=	7603.46
Hw Elev (ft)	=	7604.69
Hw/D (ft)	=	1.10
Flow Regime	=	Inlet Control



Tuesday, Oct 10 2023

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

# **EX-CULVERT-01**

Invert Elev Dn (ft)	= 7532.00	Calculations
Pipe Length (ft)	= 89.39	Qmin (cfs)
Slope (%)	= 3.36	Qmax (cfs)
Invert Elev Up (ft)	= 7535.00	Tailwater Élev (ft)
Rise (in)	= 48.0	. ,
Shape	= Circular	Highlighted
Span (in)	= 48.0	Qtotal (cfs)
No. Barrels	= 1	Qpipe (cfs)
n-Value	= 0.012	Qovertop (cfs)
Culvert Type	= Circular Concrete	Veloc Dn (ft/s)
Culvert Entrance	= Square edge w/headwall (C)	Veloc Up (ft/s)
Coeff. K,M,c,Y,k	= 0.0098, 2, 0.0398, 0.67, 0.5	HGL Dn (ft)
		HGL Up (ft)

# Embankment

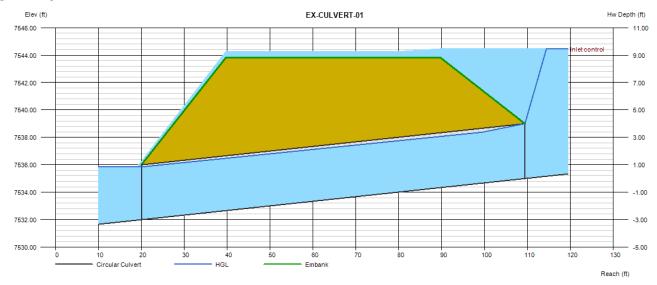
Top Elevation (ft) Top Width (ft) Crest Width (ft)

=	7543.82
=	50.00
=	50.00

CULVERT LOCATION: PARCEL 3-4, BASIN C, CROSSING OLD STAGECOACH ROAD, DESIGN POINT 10

Qmin (cfs)	= 81.40
Qmax (cfs)	= 251.40
Tailwater Elev (ft)	= (dc+D)/2

	giitoa		
Qtotal	(cfs)	=	241.40
Qpipe	(cfs)	=	164.69
Qover	top (cfs)	=	76.71
Veloc	Dn (ft/s)	=	13.27
Veloc	Up (ft/s)	=	13.58
HGL D	Dn (ft)	=	7535.85
HGL L	Jp (ft)	=	7538.70
Hw Ele	ev (ft)	=	7544.45
Hw/D	(ft)	=	2.36
Flow F	Regime	=	Inlet Control



FLOW TO DP10 OVERTOPS OLD STAGECOACH ROAD UNDER SINGLE PIPE ANALYSIS, FUTURE FDR TO DELINEATE SUBBASINS AND REDUCE FLOW TO EXISTING **CULVERT PIPE** 

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

# **EX-CULVERT-02**

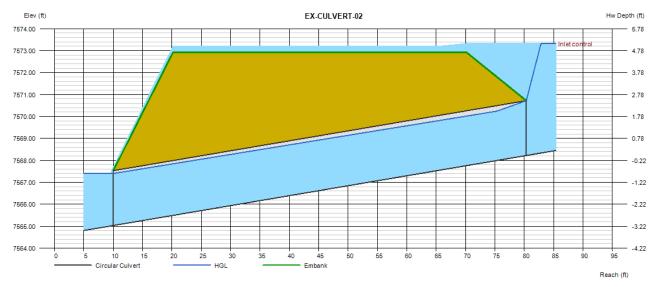
Invert Elev Dn (ft)	= 7565.03 = 70.24	Calculations
Pipe Length (ft)	= 70.34	Qmin (cfs)
Slope (%)	= 4.54	Qmax (cfs)
Invert Elev Up (ft)	= 7568.22	Tailwater Elev (ft)
Rise (in)	= 30.0	
Shape	= Circular	Highlighted
Span (in)	= 30.0	Qtotal (cfs)
No. Barrels	= 1	Qpipe (cfs)
n-Value	= 0.012	Qovertop (cfs)
Culvert Type	= Circular Concrete	Veloc Dn (ft/s)
Culvert Entrance	= Square edge w/headwall (C)	Veloc Up (ft/s)
Coeff. K,M,c,Y,k	= 0.0098, 2, 0.0398, 0.67, 0.5	HGL Dn (ft)
		HGL Un (ft)

# Embankment

Top Elevation (ft)= 7572.92Top Width (ft)= 50.00Crest Width (ft)= 50.00CULVERT LOCATION: PARCEL 5-4,BASIN E, CROSSING OLDSTAGECOACH ROAD, DESIGNPOINT 14

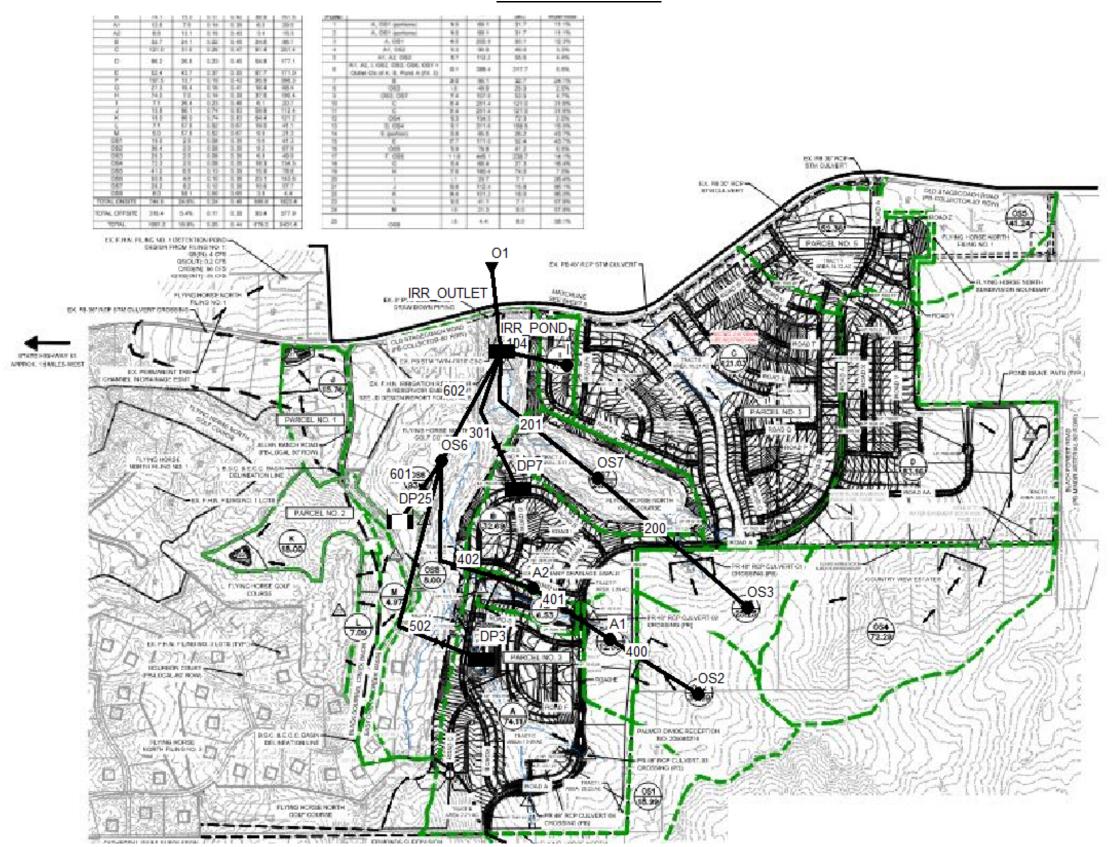
Qmin (cfs)	= 33.80
Qmax (cfs)	= 85.50
Tailwater Elev (ft)	= (dc+D)/2

inginginoa		
Qtotal (cfs)	=	83.80
Qpipe (cfs)	=	45.88
Qovertop (cfs)	=	37.92
Veloc Dn (ft/s)	=	9.54
Veloc Up (ft/s)	=	9.90
HGL Dn (ft)	=	7567.40
HGL Up (ft)	=	7570.46
Hw Elev (ft)	=	7573.32
Hw/D (ft)	=	2.04
Flow Regime	=	Inlet Control



FLOW TO DP14 OVERTOPS OLD STAGECOACH ROAD UNDER SINGLE PIPE ANALYSIS, FUTURE FDR TO DELINEATE SUBBASINS AND REDUCE FLOW TO EXISTING CULVERT PIPE

# SWMM Model Schematic



EPA STORM WATER MANAGEMENT MODEL - VERSION 5.1 (Build 5.1.012) \_\_\_\_\_ NOTE: The summary statistics displayed in this report are based on results found at every computational time step, not just on results from each reporting time step. \*\*\*\*\* Analysis Options \*\*\*\*\* Flow Units ..... CFS Process Models: Rainfall/Runoff ..... NO RDII ..... NO Snowmelt ..... NO Groundwater ..... NO Flow Routing ..... YES Ponding Allowed ..... NO Water Quality ..... NO Flow Routing Method ..... KINWAVE Starting Date ..... 01/01/2005 00:00:00 Ending Date ..... 01/04/2005 00:00:00 Antecedent Dry Days ..... 0.0 Report Time Step ..... 00:05:00 Routing Time Step ..... 30.00 sec \*\*\*\*\*\* Volume Volume acre-feet 10^6 gal Flow Routing Continuity \*\*\*\*\*\* \_ D 900 W 00 G 00 R 00 E '99

Day Westher Inflow	0,000	0 000
Dry Weather Inflow	0.000	0.000
Wet Weather Inflow	0.000	0.000
Groundwater Inflow	0.000	0.000
RDII Inflow	0.000	0.000
External Inflow	63.827	20.799
External Outflow	63.465	20.681
Flooding Loss	0.000	0.000
Evaporation Loss	0.000	0.000
Exfiltration Loss	0.000	0.000
Initial Stored Volume	0.000	0.000
Final Stored Volume	0.368	0.120
Continuity Error (%)	-0.009	

#### \*\*\*\*\*

Highest Flow Instability Indexes

### \*\*\*\*\*\*

Routing Time Step Summary *********			
Minimum Time Step	:	30.00	sec
Average Time Step	:	30.00	sec
Maximum Time Step	:	30.00	sec
Percent in Steady State	:	0.00	
Average Iterations per Step	:	1.00	
Percent Not Converging	:	0.00	

\*\*\*\*\*\*

Node Depth Summary \*\*\*\*\*\*\*\*\*

Node	Туре	Average Depth Feet	Maximum Depth Feet	Maximum HGL Feet	0ccu	of Max rrence hr:min	Reported Max Depth Feet
052	JUNCTION	0.01	0.62	7643.62	0	00:40	0.62
0S3	JUNCTION	0.02	0.68	7650.68	0	00:40	0.68
A1	JUNCTION	0.01	0.61	7613.61	0	00:48	0.61
A2	JUNCTION	0.04	1.32	7571.32	0	00:48	1.32
0S7	JUNCTION	0.02	0.68	7555.68	0	00:41	0.68
I	JUNCTION	0.00	0.00	7558.00	0	00:00	0.00
0S6	JUNCTION	0.04	1.32	7553.32	0	00:49	1.32
01	OUTFALL	0.00	0.00	7511.00	0	00:00	0.00
IRR_POND	STORAGE	0.44	3.98	7534.98	0	02:04	3.98
DP25	STORAGE	3.26	8.18	7567.18	0	01:27	8.18
DP3	STORAGE	3.00	8.70	7571.70	0	01:30	8.70
DP7	STORAGE	0.14	5.18	7557.18	0	01:24	5.18

\*\*\*\*\*\*

Node Inflow Summary \*\*\*\*\*\*\*\*\*

Volume Node gal	Error Percent	Туре	CFS	CFS	days	hr:min	10^6 gal	10^6
052		JUNCTION	82.92	82.92	0	00:40	2.5	
2.5	0.000							
0S3		JUNCTION	65.20	65.20	0	00:40	1.73	
1.73	-0.000							
A1		JUNCTION	27.93	108.39	0	00:47	0.863	
3.38	0.000							
A2		JUNCTION	9.10	117.37	0	00:48	0.45	
3.83	0.000		50 50	124 65	•	00.11	1 0 4	
0S7 3.67	0.000	JUNCTION	59.52	124.65	0	00:41	1.94	
J.67 I	0.000	JUNCTION	15.72	15.72	0	00:40	0.488	
0.488	0.000	JUNCTION	13.72	17.72	U	00.40	0.488	
0.400 0S6	0.000	JUNCTION	161.12	313.79	0	00:56	6.45	
15.1	0.000			0_0000	· ·		01.0	
01		OUTFALL	0.00	206.37	0	02:04	0	
20.7	0.000							
IRR_P	POND	STORAGE	0.00	459.33	0	00:52	0	
20.7	0.060							
DP25		STORAGE	63.88	63.88	0	00:35	1.18	
1.18	0.068				_			
DP3	0.050	STORAGE	187.41	187.41	0	00:40	3.75	
3.75	0.052	CTODACE		C 4 05	0	00.40	1 4 4	
DP7 1.44	0.006	STORAGE	64.85	64.85	0	00:40	1.44	
1.44	0.000							

\*\*\*\*\*

Node Flooding Summary \*\*\*\*\*\*\*\*\*\*

No nodes were flooded.

Average Avg Evap Exfil Maximum Max Time of Max Maximum Volume Pcnt Pcnt Pcnt Volume Pcnt Occurrence Outflow

Stora hr:min	ge Unit CFS	1000 ft3	Full	Loss	Loss	1000 ft3	Fu	11 da	ays
IRR_P	OND	144.161	2	0	0	1374.169		21	0
02:03	206.37								
DP25		23.148	12	0	0	130.463		69	0
01:27	10.46	50.026	10	0	0	250,000		70	•
DP3 01:29	43.10	59.026	13	0	0	359.899		79	0
DP7	45.10	2.228	1	0	0	97.286		37	0
01:23	22.75		-	Ū	·			•	·
	**************************************								
	*****************								
		Elow	Avg			Total			
			Flow						
Outfa	ll Node		CFS			.0^6 gal			
01		99.72	10.70	206.	37 	20.679			
Syste	m	99.72	10.70	206.	37	20.679			
****	*****								
	Flow Summary ***********								
			Maximum				Max/		
Link		Type	Flow  CFS		rrence hr:min	Veloc  ft/sec	Full Flow	Full Depth	
L111K		Туре		uays					
400		CONDUIT	81.34	0	00:48	3.52	0.26	0.51	
200		CONDUIT	65.16	0	00:41	20.26	0.00	0.14	
401		CONDUIT	108.37	0	00:48	6.88	0.15	0.38	
104		DUMMY	15.72	0	00:40	<b>C</b> 10	0 05	0.00	
402			117.32	0	00:49	6.10	0.05	0.33	
201			124.65	0	00:41				
602			313.79	0	00:56				
	UTLET		206.37	0	02:04 01:27				
601 301		dummy Dummy	10.46 22.75	0 0	01:27 01:24				
501			43.10	0	01:24				
502			42.10	0	01.00				

\*\*\*\*\*\*

No conduits were surcharged.

Analysis begun on: Wed Oct 18 09:07:08 2023 Analysis ended on: Wed Oct 18 09:07:08 2023 Total elapsed time: < 1 sec

			Unit	t Hydrograp	oh Paramet	Excess Precip.		Storm Hydrograph							
Catchment Name/ID	ст	Ср	W50 (min.)	W50 Before Peak	W75 (min.)	W75 Before Peak	Time to Peak (min.)	Peak (cfs)	Volume (c.f)	Excess (inches)	Excess (c.f.)	Time to Peak (min.)	Peak Flow (cfs)	Total Volume (c.f.)	Runoff per Unit Area (cfs/acre)
OS3	0.156	0.109	22.8	3.40	11.8	2.40	5.7	52	91,839	2.54	233,060	40.0	65	230,694	2.58
OS7	0.133	0.099	31.1	3.87	16.2	2.73	6.4	42	102,366	2.55	260,801	40.0	60	259,724	2.11
OS6	0.146	0.185	43.4	7.65	22.6	5.41	12.8	101	339,768	2.54	863,660	50.0	161	862,778	1.72
A1	0.137	0.071	28.8	3.07	15.0	2.17	5.1	21	45,738	2.55	116,439	40.0	28	115,392	2.22
A2	0.121	0.048	56.2	3.56	29.2	2.52	5.9	5	23 <i>,</i> 595	2.56	60,301	50.0	9	60,162	1.40
I	0.103	0.050	28.9	2.60	15.0	1.84	4.3	12	25,773	2.58	66,421	40.0	16	65,254	2.21
OS2	0.156	0.128	28.1	4.26	14.6	3.01	7.1	61	132,132	2.54	335,312	40.0	83	334,189	2.28

Summary of Unit Hydrograph Parameters Used By Program and Calculated Results (Version 2.0.1)

### Summary of CUHP Input Parameters (Version 2.0.1)

								Depression Storage Horton's Infiltration Parameter					DCIA			
Catchment Name/ID	SWMM Node/ID	Raingage Name/ID	Area (sq.mi.)	Dist. to Centroid (miles)	Length (miles)	Slope (ft./ft.)	Percent Imperv.	Pervious (inches)	Imperv. (inches)	Initial Rate (in./hr.)	Final Rate (in.hr.)	Decay Coeff. (1/sec.)	DCIA Level	Dir. Con'ct Imperv. Fraction	Receiv. Perv. Fraction	Percent Eff. Imperv.
OS3	OS3	100-YR	0.040	0.114	0.227	0.060	2.0	0.35	0.08	4.50	0.00	0.6000	0.00	0.04	0.02	2.00
OS7	OS7	100-YR	0.044	0.161	0.322	0.050	8.2	0.35	0.08	4.50	0.00	0.6000	0.00	0.16	0.08	8.20
OS6	OS6	100-YR	0.146	0.331	0.663	0.025	4.6	0.35	0.08	4.50	0.00	0.6000	0.00	0.09	0.05	4.60
A1	A1	100-YR	0.020	0.080	0.180	0.025	7.0	0.35	0.08	4.50	0.00	0.6000	0.00	0.14	0.07	7.00
A2	A2	100-YR	0.010	0.142	0.259	0.030	13.1	0.35	0.08	4.50	0.00	0.6000	0.00	0.26	0.11	13.10
Ι	I	100-YR	0.011	0.095	0.189	0.050	26.4	0.35	0.08	4.50	0.00	0.6000	0.00	0.53	0.16	26.40
OS2	OS2	100-YR	0.057	0.152	0.303	0.040	2.0	0.35	0.08	4.50	0.00	0.6000	0.00	0.04	0.02	2.00

# Printouts for Storm Hydrographs

flow in cfs

	flow in cfs						
time in minutes	33	7	90				5
tin	033	2SO	950	A1	A2	-	052
5	0.00	0.00	0.00	0.00	0.00	0.00	0.00
10	0.00	0.01	0.01	0.00	0.00	0.04	0.00
15	0.01	0.07	0.03	0.03	0.02	0.21	0.01
20	2.47	2.61	2.77	1.28	0.42	1.34	2.58
25	20.38	16.62	22.60	8.44	2.26	5.27	21.69
30	51.43	41.94	69.84	20.91	5.58	12.09	57.24
35	64.50	55.54	117.60	26.66	7.45	15.12	77.49
40	65.20	59.52	145.40	27.93	8.37	15.72	82.92
45	62.58	59.24	158.13	27.51	8.89	15.46	81.76
50	58.69	57.59	161.12	26.46	9.10	14.86	78.51
55	54.44	54.87	158.30	25.01	9.06	14.03	74.06
60	50.49	52.39	154.79	23.84	8.99	13.37	70.32
65	46.63	50.48	151.16	22.84	8.95	12.79	67.10
70	40.80	46.75	145.04	20.81	8.65	11.63	61.26
75	36.28	42.83	137.43	18.77	8.32	10.50	54.98
80	31.82	38.21	129.54	16.54	7.90	9.26	48.34
85	27.89	34.03	121.14	14.76	7.50	8.27	43.08
90	24.51	30.68	112.90	13.37	7.16	7.49	38.89
95	21.41	28.11	105.10	12.22	6.84	6.85	35.41
100	18.51	25.95	97.48	11.19	6.54	6.27	32.30
105	15.80	24.02	90.14	10.26	6.26	5.74	29.45
110	13.58	22.24	83.47	9.37	5.98	5.25	26.76
115	12.08	20.56	78.19	8.54	5.70	4.77	24.20
120	11.15	18.97	74.07	7.74	5.42	4.32	21.78
125	8.95	16.28	69.09	6.35	4.99	3.55	17.83
130	6.98	13.55	63.09	5.03	4.56	2.81	14.02
135	5.44 4.21	10.96	57.15	3.93	4.17	2.20	11.02
140		8.68	51.50	3.14	3.84	1.75	8.81
145	3.26	6.83	46.26	2.52	3.55	1.41	7.04
150 155	2.51 1.93	5.47 4.42	41.53	2.02	3.30	1.13	5.63 4.47
160	1.93	3.54	37.07	1.61 1.27	3.07	0.90	3.51
165	1.48	2.83	32.83 28.78	1.27	2.85 2.65	0.71 0.56	2.74
170	0.88	2.24	24.87	0.79	2.46	0.30	2.17
175	0.64	1.78	24.87	0.64	2.40	0.36	1.75
180	0.43	1.43	17.30	0.51	2.11	0.29	1.40
185	0.43	1.43	13.75	0.31	1.95	0.23	1.40
190	0.27	0.94	10.79	0.41	1.79	0.23	0.84
195	0.15	0.75	8.68	0.32	1.64	0.13	0.61
200	0.00	0.57	7.09	0.17	1.48	0.10	0.42
205	0.00	0.42	5.83	0.11	1.33	0.06	0.26
210	0.00	0.30	4.81	0.07	1.19	0.04	0.14
215	0.00	0.19	3.95	0.03	1.04	0.02	0.06
220	0.00	0.11	3.22	0.01	0.90	0.01	0.01
225	0.00	0.05		0.00	0.76	0.00	0.00
230	0.00	0.01	2.14	0.00	0.63	0.00	0.00
235	0.00	0.00	1.73	0.00	0.51	0.00	0.00
240	0.00	0.00	1.38	0.00	0.40	0.00	0.00
225 230 235	0.00 0.00 0.00	0.05 0.01 0.00	2.61 2.14 1.73	0.00 0.00 0.00	0.76 0.63 0.51	0.00 0.00 0.00	0.00 0.00 0.00

245	0.00	0.00	1.07	0.00	0.33	0.00	0.00
250	0.00	0.00	0.80	0.00	0.27	0.00	0.00
255	0.00	0.00	0.57	0.00	0.23	0.00	0.00
260	0.00	0.00	0.37	0.00	0.19	0.00	0.00
265	0.00	0.00	0.22	0.00	0.15	0.00	0.00
270	0.00	0.00	0.11	0.00	0.12	0.00	0.00
275	0.00	0.00	0.03	0.00	0.10	0.00	0.00
280	0.00	0.00	0.00	0.00	0.08	0.00	0.00
285	0.00	0.00	0.00	0.00	0.07	0.00	0.00
290	0.00	0.00	0.00	0.00	0.05	0.00	0.00
295	0.00	0.00	0.00	0.00	0.04	0.00	0.00
300	0.00	0.00	0.00	0.00	0.03	0.00	0.00
305	0.00	0.00	0.00	0.00	0.02	0.00	0.00
310	0.00	0.00	0.00	0.00	0.01	0.00	0.00
315	0.00	0.00	0.00	0.00	0.01	0.00	0.00
320	0.00	0.00	0.00	0.00	0.00	0.00	0.00
325	0.00	0.00	0.00	0.00	0.00	0.00	0.00
330	0.00	0.00	0.00	0.00	0.00	0.00	0.00

# Printouts for Unit Hydrographs

flow in cfs

flow in cfs							
م time in minutes	3	7	9				2
tir	033	USO	950	A1	A2	-	052
5	51.09	39.50	49.24	20.51	5.23	11.52	53.35
10	49.36	41.72	94.61	19.77	5.39	10.99	59.82
15	39.36	38.17	100.74	17.46	5.26	9.64	53.72
20	32.65	31.77	96.65	14.56	5.04	8.10	43.95
25	26.09	27.93	88.26	12.57	4.73	7.00	37.74
30	22.25	24.08	75.74	10.59	4.32	5.90	31.53
35	18.43	20.65	68.93	9.28	3.94	5.19	27.43
40	14.60	18.38	62.12	8.10	3.68	4.53	23.81
45	10.78	16.12	55.31	6.92	3.42	3.87	20.19
50	9.26	13.86	49.38	5.75	3.16	3.22	16.58
55	7.99	11.59	45.46	4.57	2.90	2.56	12.96
60	6.72	9.33	41.53	3.87	2.67	2.17	11.22
65	5.44	8.02	37.60	3.47	2.51	1.95	10.01
70	4.17	7.26	33.67	3.08	2.35	1.74	8.80
75	2.89	6.51	29.75	2.69	2.19	1.52	7.60
80	1.62	5.75	25.82	2.30	2.04	1.30	6.39
85	0.34	5.00	21.89	1.90	1.88	1.08	5.18
90	0.00	4.25	19.48	1.51	1.72	0.86	3.98
95		3.49	18.17	1.12	1.56	0.64	2.77
100		2.74	16.86	0.73	1.41	0.42	1.57
105		1.98	15.55	0.33	1.25	0.20	0.36
110		1.23	14.24	0.00	1.09	0.00	0.00
115		0.47	12.93		1.03		
120		0.00	11.62		0.98		
125			10.31		0.93		
130			9.00		0.88		
135			7.70		0.82		
140			6.39		0.77		
145			5.08		0.72		
150			3.77		0.67		
155			2.46		0.61		
160			1.15		0.56		
165			0.00		0.51		
170					0.46		
175					0.41		
180					0.35		
185					0.30		
190					0.25		
195					0.20		
200					0.14		
205					0.09		
210					0.04		
215					0.00		



Flying Horse North Phase 2 Parcels 1-6 Preliminary Drainage Report Project No.: 211030

Appendix D:

Water Quality & Detention Basin Calculations

Stage (ft)

Override

Stage (ft)

MHFD-Detention, Version 4.06 (July 2022)

#### Project: FLYING HORSE NORTH PUD PRELIMINARY PLAN Basin ID: BASINS: A, OS1 ; DESIGN POINT 3

	ZONE 3 ZONE 2 ZONE 1	
PERMANENT		100-YEAR ORIFICE
PERMANENT		ORIFICE

Depth Increment = Stage - Storage Description Example Zone Configuration (Retention Pond)

### Watershed Information

Selected BMP Type =	EDB				
Watershed Area =	93.10	acres			
Watershed Length =	2,250	ft			
Watershed Length to Centroid =	800	ft			
Watershed Slope =	0.040	ft/ft			
Watershed Imperviousness =	12.30%	percent			
Percentage Hydrologic Soil Group A =	0.0%	percent			
Percentage Hydrologic Soil Group B =	100.0%	percent			
Percentage Hydrologic Soil Groups C/D =	0.0%	percent			
Target WQCV Drain Time =	40.0	hours			
Location for 1-hr Rainfall Depths = User Input					

# After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

the embedded Colorado Urban Hydrograph Procedure.						
Water Quality Capture Volume (WQCV) =	0.618	acre-feet				
Excess Urban Runoff Volume (EURV) =	1.094	acre-feet				
2-yr Runoff Volume (P1 = 1.19 in.) =	1.411	acre-feet				
5-yr Runoff Volume (P1 = 1.5 in.) =	2.948	acre-feet				
10-yr Runoff Volume (P1 = 1.75 in.) =	4.463	acre-feet				
25-yr Runoff Volume (P1 = 2 in.) =	7.102	acre-feet				
50-yr Runoff Volume (P1 = 2.25 in.) =	8.925	acre-feet				
100-yr Runoff Volume (P1 = 2.52 in.) =	11.525	acre-feet				
500-yr Runoff Volume (P1 = 3.14 in.) =	16.296	acre-feet				
Approximate 2-yr Detention Volume =	0.714	acre-feet				
Approximate 5-yr Detention Volume =	1.100	acre-feet				
Approximate 10-yr Detention Volume =	2.097	acre-feet				
Approximate 25-yr Detention Volume =	2.828	acre-feet				
Approximate 50-yr Detention Volume =	2.973	acre-feet				
Approximate 100-yr Detention Volume =	3.793	acre-feet				

### Define Zones and Basin Geometry

Define Zones and Basin Geometry		
Zone 1 Volume (WQCV) =	0.618	acre-feet
Zone 2 Volume (EURV - Zone 1) =	0.476	acre-feet
Zone 3 Volume (100-year - Zones 1 & 2) =	2.699	acre-feet
Total Detention Basin Volume =	3.793	acre-feet
Initial Surcharge Volume (ISV) =	user	ft <sup>3</sup>
Initial Surcharge Depth (ISD) =	user	ft
Total Available Detention Depth (H <sub>total</sub> ) =	user	ft
Depth of Trickle Channel (H <sub>TC</sub> ) =	user	ft
Slope of Trickle Channel (STC) =	user	ft/ft
Slopes of Main Basin Sides (S <sub>main</sub> ) =	user	H:V
Basin Length-to-Width Ratio (R <sub>L/W</sub> ) =	user	

### Initial Surcharge Area (A<sub>ISV</sub>) = user ft<sup>2</sup> ft ft ft ft² ft³ ft ft ft ft 2 ft <sup>3</sup>

	7562	Top of Micropool		0.00	-		-	0	0.000	(10)	(de le)
				1.00				8,622	0.198	4,311	0.099
	F			2.00	-			24,877	0.571	21,060	0.483
	F			3.00				37,363	0.858	52,180	1.198
	F			4.00				42,000	0.964	91,862	2.109
				5.00				47,874	1.099	136,799	3.140
				6.00	-		-	54,892	1.260	188,182	4.320
			1	7.00	-	1	-	62,293	1.430	246,774	5.665
				8.00	-		-	67,350	1.546	311,596	7.153
				9.00	-		-	73,250	1.682	381,896	8.767
	-	TOP: 7572		10.00				78,100	1.793	457,571	10.504
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Optional User Overri	des				-		-				
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1.50 inches					-		-				
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Width (ft)

Length (ft)

Area (ft<sup>2</sup>)

Override

Area (ft<sup>2</sup>)

Area (acre)

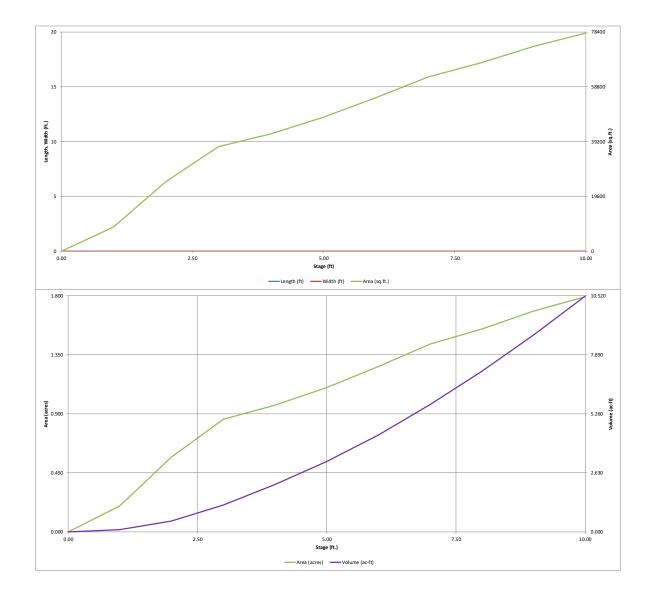
Volume (ft<sup>3</sup>)

Volume (ac-ft)

Total Ba

Surcharge Volume Length $(L_{ISV}) =$	user ft
Surcharge Volume Width $(W_{ISV}) =$	user ft
Depth of Basin Floor $(H_{FLOOR}) =$	user ft
Length of Basin Floor $(L_{FLOOR}) =$	user ft
Width of Basin Floor $(W_{FLOOR}) =$	user ft
Area of Basin Floor (A <sub>FLOOR</sub> ) =	user ft <sup>2</sup>
Volume of Basin Floor (V <sub>FLOOR</sub> ) =	user ft 3
Depth of Main Basin $(H_{MAIN}) =$	user ft
Length of Main Basin $(L_{MAIN}) =$	user ft
Width of Main Basin ( $W_{MAIN}$ ) =	user ft
Area of Main Basin $(A_{MAIN}) =$	user ft <sup>2</sup>
Volume of Main Basin ( $V_{MAIN}$ ) =	user ft 3
Calculated Total Basin Volume ( $V_{total}$ ) =	user acre-feet

MHFD-Detention, Version 4.06 (July 2022)



	D	TENTION	BASIN OUT	LET STRU	CTURE DE	SIGN		
		٨	MHFD-Detention, V			01011		
-	BASINS: A, OS1 ;	ORTH PUD PRELIM	INARY PLAN					
ZONE 3 ZONE 2				Estimated	Estimated			
				Stage (ft)	Volume (ac-ft)	Outlet Type		
			Zone 1 (WQCV)	2.23	0.618	Orifice Plate	1	
	100-YEAR ORIFICE		Zone 2 (EURV)	2.88	0.476	Orifice Plate		
PERMANENT ORIFICES			Zone 3 (100-year)	5.58	2.699	Weir&Pipe (Restrict)	1	
POOL Example Zone	Configuration (Re	etention Pond)		Total (all zones)	3.793		-	
User Input: Orifice at Underdrain Outlet (typical							Calculated Parame	
Underdrain Orifice Invert Depth = Underdrain Orifice Diameter =	N/A N/A		the filtration media	surface)		drain Orifice Area = n Orifice Centroid =	N/A N/A	ft <sup>2</sup>
	N/A	inches			Underdran		N/A	feet
User Input: Orifice Plate with one or more orific	es or Elliptical Slot	Weir (typically used	to drain WQCV and	l/or EURV in a sedir	mentation BMP)		Calculated Parame	ters for Plate
Centroid of Lowest Orifice =	0.00	ft (relative to basin	n bottom at Stage =	= 0 ft)	WQ Orif	ice Area per Row =	2.778E-02	ft²
Depth at top of Zone using Orifice Plate =	3.00		n bottom at Stage =	= 0 ft)		iptical Half-Width =	N/A	feet
Orifice Plate: Orifice Vertical Spacing =	N/A	inches				tical Slot Centroid =	N/A	feet
Orifice Plate: Orifice Area per Row =	4.00	sq. inches (use rec	ctangular openings)		E	Elliptical Slot Area =	N/A	ft <sup>2</sup>
User Input: Stage and Total Area of Each Orific	e Row (numbered f	rom lowest to highe	<u>est)</u>					
	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)		1.50	2.50					
Orifice Area (sq. inches)	4.00	4.00	4.00					
	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								(optional)
Orifice Area (sq. inches)								
	<u> </u>							
User Input: Vertical Orifice (Circular or Rectang	ular) Not Selected	Not Selected	7				Calculated Parame Not Selected	ters for Vertical Or Not Selected
Invert of Vertical Orifice =	Not Selected	Not Selected	ft (relative to basin	n bottom at Stage =	0ft) Ve	rtical Orifice Area =	NOL Selected	N/A
Depth at top of Zone using Vertical Orifice =		N/A		bottom at Stage =		al Orifice Centroid =	N/A	N/A
Vertical Orifice Diameter =		N/A	inches	5	,			• • •
			_					
	. Claused Custa and				-t Dia -)			have fam Ourseffam )
User Input: Overflow Weir (Dropbox with Flat o	Zone 3 Weir	Not Selected	tangular/ i rapezoida	al weir and No Outle	et Pipe)		Calculated Parame Zone 3 Weir	Not Selected
Overflow Weir Front Edge Height, Ho =		N/A	ft (relative to basin b	oottom at Stage = 0 fl	t) Height of Grat	e Upper Edge, H <sub>t</sub> =		N/A
Overflow Weir Front Edge Length =		N/A	feet	5	-	Veir Slope Length =	6.32	N/A
Overflow Weir Grate Slope =	3.00	N/A	H:V	Gi	rate Open Area / 10	00-vr Orifice Area =	0.45	
Horiz. Length of Weir Sides =	6.00	N/A	feet		•		8.45	N/A
Overflow Grate Type =	Type C Grate		IEEL		verflow Grate Open	Area w/o Debris =	26.41	N/A
Debris Clogging 70 -								
	50%	N/A N/A	%		•	Area w/o Debris =		N/A
		N/A	%		Dverflow Grate Ope	a Area w/o Debris = en Area w/ Debris =	26.41 13.21	N/A N/A
		N/A	%		Dverflow Grate Ope	a Area w/o Debris = en Area w/ Debris =	26.41	N/A N/A
	e (Circular Orifice, R	N/A estrictor Plate, or R	ectangular Orifice)		Dverflow Grate Ope <u>Ca</u>	a Area w/o Debris = en Area w/ Debris =	26.41 13.21	N/A N/A Flow Restriction F
User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter =	e <u>(Circular Orifice, R</u> Zone 3 Restrictor 0.50 24.00	N/A estrictor Plate, or R Not Selected	% ectangular Orifice) ft (distance below ba inches	( asin bottom at Stage =	Overflow Grate Ope <u>Ca</u> = 0 ft) C Outle	a Area w/o Debris = en Area w/ Debris = alculated Parameter putlet Orifice Area = et Orifice Centroid =	26.41 13.21 rs for Outlet Pipe w/ Zone 3 Restrictor 3.13 1.00	N/A N/A Flow Restriction F Not Selected N/A N/A
User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe =	e <u>(Circular Orifice, R</u> Zone 3 Restrictor 0.50 24.00	N/A estrictor Plate, or R Not Selected N/A	% ectangular Orifice) ft (distance below ba	( asin bottom at Stage =	Dverflow Grate Ope	a Area w/o Debris = en Area w/ Debris = alculated Parameter putlet Orifice Area = et Orifice Centroid =	26.41 13.21 s for Outlet Pipe w/ Zone 3 Restrictor 3.13	N/A N/A Flow Restriction F Not Selected N/A
User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert =	e (Circular Orifice, R Zone 3 Restrictor 0.50 24.00 23.50	N/A estrictor Plate, or R Not Selected N/A	% ectangular Orifice) ft (distance below ba inches	( asin bottom at Stage =	Overflow Grate Ope <u>Ca</u> = 0 ft) C Outle	a Area w/o Debris = en Area w/ Debris = alculated Parameter putlet Orifice Area = et Orifice Centroid =	26.41 13.21 rs for Outlet Pipe w/ Zone 3 Restrictor 3.13 1.00	N/A N/A Flow Restriction F Not Selected N/A N/A N/A
User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert =	e (Circular Orifice, R Zone 3 Restrictor 0.50 24.00 23.50 <u>Trapezoidal</u> )	N/A estrictor Plate, or R Not Selected N/A N/A	% ectangular Orifice) ft (distance below ba inches	( asin bottom at Stage = Half-Cent	Overflow Grate Ope <u>Cr</u> = 0 ft) O Outle tral Angle of Restric	a Area w/o Debris = en Area w/ Debris = alculated Parameter putlet Orifice Area = et Orifice Centroid =	26.41     13.21     S for Outlet Pipe w/     Zone 3 Restrictor     3.13     1.00     2.85 <u>Calculated Parame</u>	N/A N/A Flow Restriction F Not Selected N/A N/A N/A
User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or	e (Circular Orifice, R Zone 3 Restrictor 0.50 24.00 23.50 <u>Trapezoidal</u> )	N/A estrictor Plate, or R Not Selected N/A N/A ft (relative to basin feet	% ectangular Orifice) ft (distance below ba inches inches	( asin bottom at Stage = Half-Cent	Dverflow Grate Ope <u>Ca</u> = 0 ft) C Outle tral Angle of Restric Spillway E Stage at	a Area w/o Debris = en Area w/ Debris = alculated Parameter butlet Orifice Area = tt Orifice Centroid = ctor Plate on Pipe = Design Flow Depth= Top of Freeboard =	s for Outlet Pipe w/ Zone 3 Restrictor 3.13 1.00 2.85 <u>Calculated Parame</u> 1.10 11.10	N/A N/A Flow Restriction F Not Selected N/A N/A N/A ters for Spillway
User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length = Spillway End Slopes =	e (Circular Orifice, R Zone 3 Restrictor 0.50 24.00 23.50 Trapezoidal) 9.00 50.00 4.00	N/A estrictor Plate, or R Not Selected N/A N/A ft (relative to basir feet H:V	% ectangular Orifice) ft (distance below ba inches inches	( asin bottom at Stage = Half-Cent	Overflow Grate Ope <u>Ci</u> = 0 ft) C Outle tral Angle of Restric Spillway E Stage at Basin Area at	n Area w/o Debris = en Area w/ Debris = alculated Parameter Dutlet Orifice Area = et Orifice Centroid = ctor Plate on Pipe = Design Flow Depth= Top of Freeboard = Top of Freeboard =	26.41           13.21           s for Outlet Pipe w/           Zone 3 Restrictor           3.13           1.00           2.85           Calculated Parame           1.10           1.79	N/A N/A N/A N/A N/A N/A N/A ters for Spillway feet feet acres
User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length =	e (Circular Orifice, R Zone 3 Restrictor 0.50 24.00 23.50 Trapezoidal) 9.00 50.00 4.00	N/A estrictor Plate, or R Not Selected N/A N/A ft (relative to basin feet	% ectangular Orifice) ft (distance below ba inches inches	( asin bottom at Stage = Half-Cent	Overflow Grate Ope <u>Ci</u> = 0 ft) C Outle tral Angle of Restric Spillway E Stage at Basin Area at	a Area w/o Debris = en Area w/ Debris = alculated Parameter butlet Orifice Area = tt Orifice Centroid = ctor Plate on Pipe = Design Flow Depth= Top of Freeboard =	s for Outlet Pipe w/ Zone 3 Restrictor 3.13 1.00 2.85 <u>Calculated Parame</u> 1.10 11.10	N/A N/A N/A N/A N/A N/A N/A ters for Spillway feet feet
User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface =	e (Circular Orifice, R Zone 3 Restrictor 0.50 24.00 23.50 Trapezoidal) 9.00 50.00 4.00 1.00	N/A estrictor Plate, or R Not Selected N/A N/A ft (relative to basir feet H:V feet	% ectangular Orifice) ft (distance below ba inches inches n bottom at Stage =	( asin bottom at Stage = Half-Cent = 0 ft)	Overflow Grate Ope (Carried Control (Carried C	a Area w/o Debris = en Area w/ Debris = alculated Parameter butlet Orifice Area = tt Orifice Centroid = ttor Plate on Pipe = Design Flow Depth= Top of Freeboard = Top of Freeboard = Top of Freeboard =	26.41           13.21           's for Outlet Pipe W/           Zone 3 Restrictor           3.13           1.00           2.85           Calculated Parame           1.10           1.10           1.10           1.50	N/A N/A N/A Not Selected N/A N/A N/A ters for Spillway feet feet acres acre-ft
User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Routed Hydrograph Results	Circular Orifice, R           Zone 3 Restrictor           0.50           24.00           23.50   Trapezoidal)           9.00           50.00           4.00           1.00   The user can over	N/A estrictor Plate, or R Not Selected N/A N/A ft (relative to basin feet H:V feet ride the default CUI	% ectangular Orifice) ft (distance below ba inches inches n bottom at Stage =	( asin bottom at Stage - Half-Cent = 0 ft)	Dverflow Grate Ope <u>Ca</u> = 0 ft) O Uutle tral Angle of Restrict Spillway D Stage at Basin Area at Basin Volume at <u>entering new value</u>	Area w/o Debris = en Area w/ Debris = alculated Parameter butlet Orifice Area = to Orifice Centroid = tor Plate on Pipe = Design Flow Depth= Top of Freeboard = Top of Freeboard = Top of Freeboard = es in the Inflow Hyp	26.41           13.21           s for Outlet Pipe w/           Zone 3 Restrictor           3.13           1.00           2.85           Calculated Parame           1.10           1.79           10.50	N/A N/A N/A N/A N/A N/A N/A ters for Spillway feet feet acres acre-ft
User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Routed Hydrograph Results Design Storm Return Period =	Circular Orifice, R           Zone 3 Restrictor           0.50           24.00           23.50           Trapezoidal)           9.00           50.00           4.00           1.00	N/A estrictor Plate, or R Not Selected N/A N/A ft (relative to basin feet H:V feet H:V feet EURV	% ectangular Orifice) ft (distance below ba inches inches n bottom at Stage = <u>HP hydrographs and</u> 2 Year	( asin bottom at Stage = Half-Cent - 0 ft) <u>f <i>runoff volumes by</i> 5 Year</u>	Dverflow Grate Ope Ca a 0 ft) C Outle tral Angle of Restric Spillway I Stage at Basin Area at Basin Volume at entering new valuu 10 Year	A Area w/o Debris = en Area w/ Debris = alculated Parameter Dutlet Orifice Area = et Orifice Centroid = ctor Plate on Pipe = Design Flow Depth= Top of Freeboard = Top of Freeboard = Top of Freeboard = es in the Inflow Hyy 25 Year	26.41           13.21           s for Outlet Pipe w/           Zone 3 Restrictor           3.13           1.00           2.85           Calculated Parame           1.10           1.79           10.50	N/A N/A N/A N/A N/A N/A N/A ters for Spillway feet feet acres acre-ft 100 Year
User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length = Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Routed Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre.t) =	e (Circular Orifice, R Zone 3 Restrictor 0.50 24.00 23.50 Trapezoidal) 9.00 50.00 4.00 1.00 The user can over WQCV N/A 0.618	N/A estrictor Plate, or R Not Selected N/A N/A ft (relative to basir feet H:V feet ride the default CUI EURV N/A 1.094	% ectangular Orifice) ft (distance below ba inches inches h bottom at Stage = <u>HP hydrographs and</u> <u>2 Year</u> 1.19 1.411	( asin bottom at Stage = Half-Cent = 0 ft) <u>1 runoff volumes by</u> <u>5 Year</u> 1.50 2.948	Dverflow Grate Ope <u>Cr</u> = 0 ft) C Outle tral Angle of Restric Spillway D Stage at Basin Area at Basin Volume at <u>entering new value</u> 1.75 4.463	Area w/o Debris = en Area w/ Debris = alculated Parameter butlet Orifice Area = tt Orifice Centroid = ttor Plate on Pipe = Design Flow Depth= Top of Freeboard = Top of Freeboard = Top of Freeboard = Top of Freeboard = 20 of Treeboard = 20 of Tree	26.41           13.21           s for Outlet Pipe w/           Zone 3 Restrictor           3.13           1.00           2.85           Calculated Parame           1.10           11.10           1.79           10.50           drographs table (Cool           50 Year           2.25           8.925	N/A N/A N/A N/A N/A N/A N/A ters for Spillway feet feet acres acre-ft 100 Year 2.52 11.525
User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Routed Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) =	Circular Orifice, R           Zone 3 Restrictor           0.50           24.00           23.50             Trapezoidal)           9.00           50.00           4.00           1.00             The user can over           WQCV           N/A           0.618           N/A	N/A estrictor Plate, or R Not Selected N/A N/A ft (relative to basin feet H:V feet H:V feet Feet Feet N/A N/A N/A	% ectangular Orifice) ft (distance below ba inches inches n bottom at Stage = <u>HP hydrographs and</u> 2 Year 1.19 1.411 1.411	( asin bottom at Stage = Half-Cent = 0 ft) 5 Year 1.50 2.948 2.948	Dverflow Grate Ope Crack = 0 ft) C Outle tral Angle of Restrict Spillway E Stage at Basin Area at Basin Volume at <u>entering new value</u> 1.75 <u>4.463</u> <u>4.463</u>	A Area w/o Debris = en Area w/ Debris = alculated Parameter butlet Orifice Area = the Orifice Centroid = thor Plate on Pipe = tor Plate on Pipe = top of Freeboard = Top of Freeboard = Top of Freeboard = Top of Freeboard = <u>es in the Inflow Hyr</u> <u>25 Year</u> 2.00 7.102 7.102	26.41           13.21           2one 3 Restrictor           3.13           1.00           2.85           Calculated Parame           1.10           1.10           1.10           1.10           2.85           Calculated Parame           1.10           2.85           8.925           8.925           8.925	N/A N/A N/A N/A N/A N/A N/A N/A ters for Spillway feet feet acres acre-ft 100 Year 2.52 11.525 11.525
User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length = Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Routed Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) =	e (Circular Orifice, R Zone 3 Restrictor 0.50 24.00 23.50 Trapezoidal) 9.00 50.00 4.00 1.00 The user can over WQCV N/A 0.618	N/A estrictor Plate, or R Not Selected N/A N/A ft (relative to basir feet H:V feet ride the default CUI EURV N/A 1.094	% ectangular Orifice) ft (distance below ba inches inches h bottom at Stage = <u>HP hydrographs and</u> <u>2 Year</u> 1.19 1.411	( asin bottom at Stage = Half-Cent = 0 ft) <u>1 runoff volumes by</u> <u>5 Year</u> 1.50 2.948	Dverflow Grate Ope <u>Cr</u> = 0 ft) C Outle tral Angle of Restric Spillway D Stage at Basin Area at Basin Volume at <u>entering new value</u> 1.75 4.463	Area w/o Debris = en Area w/ Debris = alculated Parameter butlet Orifice Area = tt Orifice Centroid = ttor Plate on Pipe = Design Flow Depth= Top of Freeboard = Top of Freeboard = Top of Freeboard = Top of Freeboard = 20 of Treeboard = 20 of Tree	26.41           13.21           s for Outlet Pipe w/           Zone 3 Restrictor           3.13           1.00           2.85           Calculated Parame           1.10           11.10           1.79           10.50           drographs table (Cool           50 Year           2.25           8.925	N/A N/A N/A N/A N/A N/A N/A ters for Spillway feet feet feet acres acre-ft 100 Year 2.52 11.525
User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length = Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Routed Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = CUHP Predevelopment Peak Q (cfs) = OPTIONAL Override Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, q (cfs/acre) =	E (Circular Orifice, R           Zone 3 Restrictor           0.50           24.00           23.50             Trapezoidal)           9.00           50.00           4.00           1.00             The user can over           WQCV           N/A           N/A           N/A           N/A           N/A	N/A estrictor Plate, or R Not Selected N/A N/A It (relative to basir feet H:V feet Feet Fiet Fiet N/A N/A N/A N/A N/A N/A	% ectangular Orifice) ft (distance below ba inches inches h bottom at Stage = HP hydrographs and 2 Year 1.19 1.411 1.411 1.5.8 0.17	( asin bottom at Stage = Half-Cent = 0 ft) 5 Year 1.50 2.948 2.948 2.948 43.9 0.47	Dverflow Grate Ope Car a 0 ft) C Car Car Car Car Car Car Car Ca	A Area w/o Debris = en Area w/ Debris = alculated Parameter Dutlet Orifice Area = tt Orifice Centroid = ttor Plate on Pipe = Design Flow Depth= Top of Freeboard = Top of Freeboard = Top of Freeboard = Top of Freeboard = <u>es in the Inflow Hy</u> <u>25 Year</u> 2.00 7.102 7.102 113.0 1.21	26.41           13.21           2 for Outlet Pipe W/           Zone 3 Restrictor           3.13           1.00           2.85           Calculated Parame           1.10           1.79           10.50           Chographs table (Co           50 Year           2.25           8.925           8.925           141.5           1.52	N/A N/A N/A N/A N/A N/A N/A N/A N/A ters for Spillway feet feet acres acre-ft 100 Year 2.52 11.525 11.525 11.525 11.525
User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Routed Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = CUHP Predevelopment Peak Q (cfs) = OPTIONAL Override Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, q (cfs/acr) = Peak Inflow Q (cfs) =	2 (Circular Orifice, R Zone 3 Restrictor 0.50 24.00 23.50 Trapezoidal) 9.00 50.00 4.00 1.00 The user can over WQCV N/A 0.618 N/A N/A N/A N/A N/A	N/A estrictor Plate, or R N/A N/A N/A ft (relative to basin feet H:V feet ride the default CU/I EURV N/A 1.094 N/A	% ectangular Orifice) ft (distance below ba inches inches inches n bottom at Stage = HP hydrographs and 2 Year 1.19 1.411 1.411 1.5.8 0.17 2.7.2	( asin bottom at Stage = Half-Cent - 0 ft) - 0	Dverflow Grate Ope Ca = 0 ft) C Outle tral Angle of Restric Spillway I Stage at Basin Area at Basin Area at Basin Area at entering new valuu 10 Year 1.75 4.463 4.463 65.0 0.70 76.6	A Area w/o Debris = en Area w/ Debris = alculated Parameter butlet Orifice Area = the Orifice Centroid = the Orifice Centroid = the Plate on Pipe = Design Flow Depth= Top of Freeboard = Top of Freeboard = Top of Freeboard = Top of Freeboard = Cop of Freeboard = Top of Freeboard = Cop of Treeboard	26.41           13.21           2 for Outlet Pipe w/           Zone 3 Restrictor           3.13           1.00           2.85           Calculated Parame           1.10           1.79           10.50           Chographs table (Color           50 Year           2.25           8.925           141.5           1.52           151.6	N/A N/A N/A N/A N/A N/A N/A N/A ters for Spillway feet feet acres acre-ft 100 Year 2.52 11.525 11.525 11.525 11.525 11.525
User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length = Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Routed Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = CUHP Runoff Volume (acre-ft) = CUHP Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, q (cfs/acre) = Peak Inflow Q (cfs) = Peak Inflow Q (cfs) = Ratio Peak Outflow to Predevelopment Q = Ratio Peak Outflow to Predevelopment Q	e (Circular Orifice, R Zone 3 Restrictor 0.50 24.00 23.50 Trapezoidal) 9.00 50.00 4.00 1.00 The user can over WQCV N/A 0.618 N/A N/A N/A N/A 0.3 N/A	N/A estrictor Plate, or R Not Selected N/A N/A N/A ft (relative to basir feet H:V feet Fide the default CUI EURV N/A N/A N/A N/A N/A N/A N/A N/A	% ectangular Orifice) ft (distance below ba inches n bottom at Stage = HP hydrographs and 2 Year 1.19 1.411 1.411 1.411 1.5.8 0.17 2.7.2 0.5 N/A	asin bottom at Stage = Half-Cent = 0 ft)	Overflow Grate Ope         Ci           Ca         Ci         Ci           = 0 ft)         C         Outle           tral Angle of Restrict         Spillway D         Stage at           Stage at         Basin Area at         Basin Volume at           10 Year         1.75         4.463           4.463         65.0         0.70           76.6         9.9         0.2	A Area w/o Debris = en Area w/ Debris = alculated Parameter butlet Orifice Area = tt Orifice Centroid = ttor Plate on Pipe = Design Flow Depth= Top of Freeboard = Top of Freeboard = Top of Freeboard = Top of Freeboard = Cop of Freeboard = 2.00 7.102 7.102 7.102 113.0 1.21 123.4 2.8.3 0.3	26.41           13.21           2 for Outlet Pipe W/           Zone 3 Restrictor           3.13           1.00           2.85           Calculated Parame           1.10           1.79           10.50           drographs table (Cool           50 Year           2.25           8.925           141.5           1.52           151.6           39.7           0.3	N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A
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User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length = Spillway Crest Length = Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Routed Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = CUHP Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, q (cfs/acre) = Peak Inflow Q (cfs) = Peak Inflow Q (cfs) = Ratio Peak Outflow to Predevelopment Q = Peak Inflow Q (cfs) = Ratio Peak Outflow to Predevelopment Q = Peak Inflow Q (cfs) = Ratio Peak Outflow to Predevelopment Q = Peak Inflow Q (cfs) = Peak Outflow Q (cfs) = Peak Outflow Q (cfs) = Peak Outflow Q (cfs) = Peak Outflow Redevelopment Q = Peak Outflow Redevelopment Q = Peak Outflow Redevelopment Q = Peak Dutflow Q (cfs) = Peak Outflow Redevelopment Q = Peak Dutflow Redevelopment Q = Peak Dutflow Redevelopment Q = Peak Outflow Redevelopment Q = Peak Dutflow Redevelopment Q = Peak Dutflow Redevelopment Q = Peak Dutflow Redvelopment Peak Q = Peak Dutflow Redvelopment	e (Circular Orifice, R Zone 3 Restrictor 0.50 24.00 23.50 Trapezoidal) 9.00 50.00 4.00 1.00 The user can over WQCV N/A 0.618 N/A N/A N/A N/A 0.3 N/A	N/A estrictor Plate, or R Not Selected N/A N/A N/A ft (relative to basir feet H:V feet Fide the default CUI EURV N/A N/A N/A N/A N/A N/A N/A N/A	% ectangular Orifice) ft (distance below ba inches n bottom at Stage = HP hydrographs and 2 Year 1.19 1.411 1.411 1.411 1.5.8 0.17 2.7.2 0.5 N/A	asin bottom at Stage = Half-Cent = 0 ft)	Overflow Grate Ope         Ci           Ca         Ci         Ci           = 0 ft)         C         Outle           tral Angle of Restrict         Spillway D         Stage at           Stage at         Basin Area at         Basin Volume at           10 Year         1.75         4.463           4.463         65.0         0.70           76.6         9.9         0.2	A Area w/o Debris = en Area w/ Debris = alculated Parameter butlet Orifice Area = tt Orifice Centroid = ttor Plate on Pipe = Design Flow Depth= Top of Freeboard = Top of Freeboard = Top of Freeboard = Top of Freeboard = Cop of Freeboard = 2.00 7.102 7.102 7.102 113.0 1.21 123.4 2.8.3 0.3	26.41           13.21           2 for Outlet Pipe W/           Zone 3 Restrictor           3.13           1.00           2.85           Calculated Parame           1.10           1.79           10.50           drographs table (Cool           50 Year           2.25           8.925           141.5           1.52           151.6           39.7           0.3	N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A
User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length = Spillway Crest Length = Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Routed Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = UHP Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Nov, q (cfs/acre) = Peak Inflow Q (cfs) = Peak Inflow Q (cfs) = Ratio Peak Outflow to Predevelopment 2 (fps) = Max Velocity through Grate 1 (fps) = Max Velocity through Grate 2 (fps) = Time to Drain 97% of Inflow Volume (hours) =	e (Circular Orifice, R Zone 3 Restrictor 0.50 24.00 23.50 Trapezoidal) 9.00 50.00 4.00 1.00 The user can over WQCV N/A 0.618 N/A N/A N/A N/A 0.3 N/A Plate N/A N/A 38	N/A estrictor Plate, or R Not Selected N/A N/A N/A ft (relative to basir feet H:V feet Fide the default CU/ N/A N/A N/A N/A N/A N/A N/A N/	% ectangular Orifice) ft (distance below ba inches inches inches n bottom at Stage = HP hydrographs and 2 Year 1.19 1.411 1.411 1.5.8 0.17 2.7.2 0.5 N/A Plate N/A Plate N/A S8	asin bottom at Stage = Half-Cent = 0 ft) = 0 ft) = 0 ft) = 0 ft) = 0 ft = 0 ft	Dverflow Grate Ope Ca = 0 ft) C Uutle tral Angle of Restrict Spillway I Stage at Basin Area at Basin Volume at entering new value 10 Year 1.75 4.463 4.463 65.0 0.70 76.6 9.9 0.2 Overflow Weir I 0.3 N/A 74	Area w/o Debris = en Area w/ Debris = alculated Parameter Dutlet Orifice Area = tt Orifice Centroid = ttor Plate on Pipe = Design Flow Depth= Top of Freeboard = Top of Freeboard = Top of Freeboard = Top of Freeboard = Cop of Cop o	26.41           13.21           2 for Outlet Pipe W/           Zone 3 Restrictor           3.13           1.00           2.85           Calculated Parame           1.10           1.10           1.10           1.79           10.50           Carographs table (Co           50 Year           2.25           8.925           8.925           141.5           1.52           151.6           39.7           0.3           Outlet Plate 1           1.5           N/A           65	N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A
User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Routed Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-t) = CUHP Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, q (cfs/acre) = Peak Inflow Q (cfs) = Peak Inflow Q (cfs) = Ratio Peak Outflow to Predevelopment Q Structure Controlling Flow = Max Velocity through Grate 1 (fps) = Max Velocity through Grate 1 (fps) = Time to Drain 97% of Inflow Volume (hours) = Time to Drain 97% of Inflow Volume (hours)	e (Circular Orifice, R Zone 3 Restrictor 0.50 24.00 23.50 Trapezoidal) 9.00 50.00 4.00 1.00 7 <i>The user can over</i> WQCV N/A 0.618 N/A 0.618 N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A	N/A estrictor Plate, or R N/A N/A N/A ft (relative to basin feet H:V feet ride the default CU/I EURV N/A 1.094 N/A	% ectangular Orifice) ft (distance below ba inches inches n bottom at Stage = HP hydrographs and 2 Year 1.19 1.411 1.411 1.411 1.5.8 0.17 2.7.2 0.5 N/A Plate N/A N/A N/A S8 62	asin bottom at Stage = Half-Cent - 0 ft) - 0 ft) - 1.50 - 2.948 - 2.948 - 43.9 	Dverflow Grate Ope Ca Ca Ca Ca Ca Ca Ca Ca Ca Ca	Area w/o Debris = en Area w/ Debris = alculated Parameter butlet Orifice Area = the Orifice Centroid = the Orifice Centroid = the Plate on Pipe = Design Flow Depth= Top of Freeboard = Top of Freeboard = Top of Freeboard = Top of Freeboard = Top of Freeboard = Cop of Treeboard =	26.41           13.21           2 for Outlet Pipe w/           Zone 3 Restrictor           3.13           1.00           2.85           Calculated Parame           1.10           1.79           10.50           Crographs table (Co           50 Year           2.25           8.925           141.5           1.52           1.51.6           39.7           0.3           Outlet Plate 1           1.5           N/A           65           80	N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A
User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length = Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Routed Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = UHP Predevelopment Peak Q (cfs) = Predevelopment Unit Peak NQ (cfs) = Predevelopment Unit Peak NQ (cfs) = Peak Inflow Q (cfs) = Peak Inflow Q (cfs) = Ratio Peak Outflow to Predevelopment 2 (fps) = Max Velocity through Grate 1 (fps) = Max Velocity through Grate 1 (fps) = Time to Drain 97% of Inflow Volume (hours) =	e (Circular Orifice, R Zone 3 Restrictor 0.50 24.00 23.50 Trapezoidal) 9.00 50.00 4.00 1.00 The user can over WQCV N/A 0.618 N/A N/A N/A N/A 0.3 N/A Plate N/A N/A 38	N/A estrictor Plate, or R Not Selected N/A N/A N/A ft (relative to basir feet H:V feet Fide the default CU/ N/A N/A N/A N/A N/A N/A N/A N/	% ectangular Orifice) ft (distance below ba inches inches inches n bottom at Stage = HP hydrographs and 2 Year 1.19 1.411 1.411 1.5.8 0.17 2.7.2 0.5 N/A Plate N/A Plate N/A S8	asin bottom at Stage = Half-Cent = 0 ft) = 0 ft) = 0 ft) = 0 ft) = 0 ft = 0 ft	Dverflow Grate Ope Ca = 0 ft) C Uutle tral Angle of Restrict Spillway I Stage at Basin Area at Basin Volume at entering new value 10 Year 1.75 4.463 4.463 65.0 0.70 76.6 9.9 0.2 Overflow Weir I 0.3 N/A 74	Area w/o Debris = en Area w/ Debris = alculated Parameter Dutlet Orifice Area = tt Orifice Centroid = ttor Plate on Pipe = Design Flow Depth= Top of Freeboard = Top of Freeboard = Top of Freeboard = Top of Freeboard = Cop of Cop o	26.41           13.21           2 for Outlet Pipe W/           Zone 3 Restrictor           3.13           1.00           2.85           Calculated Parame           1.10           1.10           1.10           1.79           10.50           Carographs table (Co           50 Year           2.25           8.925           8.925           141.5           1.52           151.6           39.7           0.3           Outlet Plate 1           1.5           N/A           65	N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A

Stage (ft)

MHFD-Detention, Version 4.06 (July 2022)

#### Project: FLYING HORSE NORTH PUD PRELIMINARY PLAN Basin ID: BASINS: B ; DESIGN POINT 7

100-YR VOLUME EURV	ZONE 3 ZONE 2 ZONE 1
	PERMANENT CONFICE ORIFICE ORIFICE

Depth Increment = Stage - Storage Description Example Zone Configuration (Retention Pond)

Optional User Overrid

1.19 inches 
 1.50
 inches

 1.75
 inches

 2.00
 inches
 2.25 inches 2.52 inches inches

7552 Top of Micropool

#### Watershed Information

Selected BMP Type =	EDB				
Watershed Area =	32.69	acres			
Watershed Length =	1,500	ft			
Watershed Length to Centroid =	650	ft			
Watershed Slope =	0.040	ft/ft			
Watershed Imperviousness =	24.10%	percent			
Percentage Hydrologic Soil Group A =	0.0%	percent			
Percentage Hydrologic Soil Group B =	100.0%	percent			
Percentage Hydrologic Soil Groups C/D =	0.0%	percent			
Target WQCV Drain Time =	40.0	hours			
Location for 1-hr Rainfall Depths = User Input					

# After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

the embedded Colorado Orban Hydro	igraph Procedu	re.
Water Quality Capture Volume (WQCV) =	0.359	acre-feet
Excess Urban Runoff Volume (EURV) =	0.794	acre-feet
2-yr Runoff Volume (P1 = 1.19 in.) =	0.830	acre-feet
5-yr Runoff Volume (P1 = 1.5 in.) =	1.433	acre-feet
10-yr Runoff Volume (P1 = 1.75 in.) =	1.999	acre-feet
25-yr Runoff Volume (P1 = 2 in.) =	2.889	acre-feet
50-yr Runoff Volume (P1 = 2.25 in.) =	3.542	acre-feet
100-yr Runoff Volume (P1 = 2.52 in.) =	4.433	acre-feet
500-yr Runoff Volume (P1 = 3.14 in.) =	6.124	acre-feet
Approximate 2-yr Detention Volume =	0.556	acre-feet
Approximate 5-yr Detention Volume =	0.810	acre-feet
Approximate 10-yr Detention Volume =	1.244	acre-feet
Approximate 25-yr Detention Volume =	1.493	acre-feet
Approximate 50-yr Detention Volume =	1.576	acre-feet
Approximate 100-yr Detention Volume =	1.904	acre-feet

### Define Zones and Basin Geometry

Zone 1 Volume (WQCV) =	0.359	acre-feet
Zone 2 Volume (EURV - Zone 1) =	0.436	acre-feet
Zone 3 Volume (100-year - Zones 1 & 2) =	1.110	acre-feet
Total Detention Basin Volume =	1.904	acre-feet
Initial Surcharge Volume (ISV) =	user	ft <sup>3</sup>
Initial Surcharge Depth (ISD) =	user	ft
Total Available Detention Depth (H <sub>total</sub> ) =	user	ft
Depth of Trickle Channel (H <sub>TC</sub> ) =	user	ft
Slope of Trickle Channel (S <sub>TC</sub> ) =	user	ft/ft
Slopes of Main Basin Sides (S <sub>main</sub> ) =	user	H:V
Basin Length-to-Width Ratio (R <sub>L/W</sub> ) =	user	

#### ٦<sub>ft</sub> : Initial Surcharge Area (A<sub>ISV</sub>) = user Surcharge Volume Length (LISV) = user ft Surcharge Volume Width $(W_{ISV}) =$ user Depth of Basin Floor (H<sub>FLOOR</sub>) = user Length of Basin Floor (L<sub>FLOOR</sub>) = user Width of Basin Floor ( $W_{FLOOR}$ ) = user Area of Basin Floor (A<sub>FLOOR</sub>) = user Volume of Basin Floor (V<sub>FLOOR</sub>) = user Depth of Main Basin $(H_{MAIN}) =$ user Length of Main Basin (LMAIN) = user Width of Main Basin ( $W_{MAIN}$ ) = user Area of Main Basin ( $A_{MAIN}$ ) = Volume of Main Basin ( $V_{MAIN}$ ) = user Ĥ user acre-fee Calculated Total Basin Volume (V<sub>total</sub>) = user

		1.00	-	 	12,035	0.276	6,017	0.138
		 2.00		 	19,768	0.454	21,919	0.503
				 	22,182			
		 3.00				0.509	42,894	0.985
		 4.00		 	24,710	0.567	66,340	1.523
		 5.00		 	27,347	0.628	92,368	2.120
	TOP:7558	 6.00		 -	30,105	0.691	121,094	2.780
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er Overrides				 -				
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Area (acre)

0.000

Area

(ft<sup>2</sup>)

Area (ft<sup>2</sup>)

0

Width

(ft)

Length

(ft)

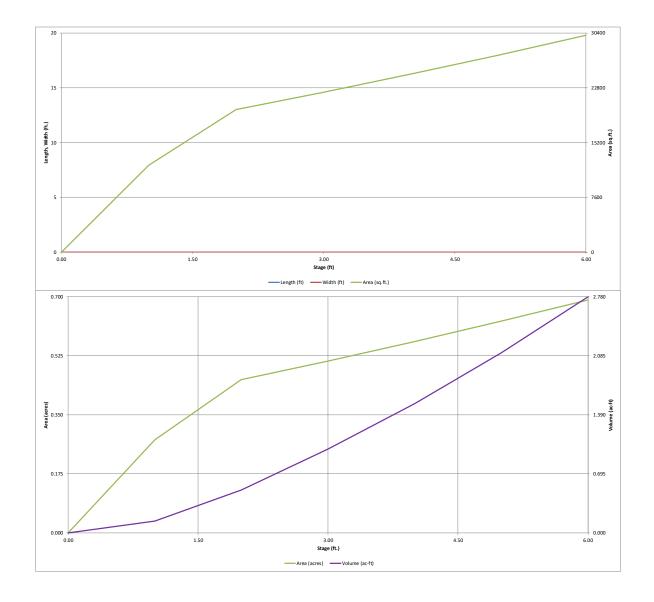
Stage (ft)

0.00

Volume (ft<sup>3</sup>)

Volume (ac-ft)

MHFD-Detention, Version 4.06 (July 2022)



	טע	ELENTION	BASIN UU	ILEI SIKU	CTURE DE	SIGN				
DETENTION BASIN OUTLET STRUCTURE DESIGN MHFD-Detention, Version 4.06 (July 2022) Project: FLYING HORSE NORTH PUD PRELIMINARY PLAN										
-	BASINS: B ; DESI									
ZONE 3				Estimated	Estimated					
100-YR				Stage (ft)	Volume (ac-ft)	Outlet Type				
VOLUME EURV WOCV			Zone 1 (WQCV)	1.66	0.359	Orifice Plate	1			
	100-YEAR		Zone 2 (EURV)	2.62	0.436	Orifice Plate				
ZONE 1 AND 2 ORIFICES	ORIFICE		Zone 3 (100-year)	4.65	1.110	Weir&Pipe (Restrict)	<u>,</u>			
	Configuration (Re	etention Pond)	2011C 5 (100 year)	Total (all zones)	1.904	Weirdripe (Restrict)				
User Input: Orifice at Underdrain Outlet (typically	used to drain WC	CV in a Filtration BN	MP)		1.504	1	Calculated Parame	ters for Underdra		
Underdrain Orifice Invert Depth =	N/A		the filtration media	surface)	Under	drain Orifice Area =		ft <sup>2</sup>		
Underdrain Orifice Diameter =	N/A	inches		bundeey		n Orifice Centroid =	N/A	feet		
	,						,	1		
User Input: Orifice Plate with one or more orifice	es or Elliptical Slot	Weir (typically used	to drain WQCV and	l/or EURV in a sedii	mentation BMP)		Calculated Parame	ters for Plate		
Centroid of Lowest Orifice =	0.00	ft (relative to basin	n bottom at Stage =	= 0 ft)	WQ Orif	ice Area per Row =	N/A	ft <sup>2</sup>		
Depth at top of Zone using Orifice Plate =	3.50	ft (relative to basin	n bottom at Stage =	= 0 ft)	Ell	iptical Half-Width =	N/A	feet		
Orifice Plate: Orifice Vertical Spacing =	N/A	inches			Ellipt	ical Slot Centroid =	N/A	feet		
Orifice Plate: Orifice Area per Row =	N/A	sq. inches			E	Elliptical Slot Area =	N/A	ft <sup>2</sup>		
User Input: Stage and Total Area of Each Orifice		-		D. 44	D. 54	D. 64		D. 01.11		
	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional		
Stage of Orifice Centroid (ft)	0.00	1.50	2.50							
Orifice Area (sq. inches)	3.25	3.25	6.00							
1	Row 9 (optional)	Row 10 (optional)	Pow 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optiona		
Stage of Orifice Centroid (ft)	Kow 9 (opuolidi)	Now to (optional)	Row 11 (optional)	(optional)	(optional)	(optional)	Row 13 (optional)			
Orifice Area (sq. inches)							1			
Office Area (sq. increas)										
Iser Input: Vertical Orifice (Circular or Rectangu	ılar)						Calculated Parame	ters for Vertical		
	Not Selected	Not Selected	1				Not Selected	Not Selected		
Invert of Vertical Orifice =	N/A	N/A	ft (relative to basir	bottom at Stage =	= 0 ft) Ve	rtical Orifice Area =	N/A	N/A		
Depth at top of Zone using Vertical Orifice =	N/A	N/A	ft (relative to basir	bottom at Stage =	= 0 ft) Vertica	I Orifice Centroid =	N/A	N/A		
Vertical Orifice Diameter =	N/A	N/A	inches							
			_							
Jser Input: Overflow Weir (Dropbox with Flat or	Sloped Grate and	Outlet Pipe OR Rec	tangular/Trapezoida	al Weir and No Outl	et Pipe)		Calculated Parame	ters for Overflow		
Jser Input: Overflow Weir (Dropbox with Flat or	Sloped Grate and Zone 3 Weir	Outlet Pipe OR Rec Not Selected	tangular/Trapezoida	al Weir and No Outl	et Pipe)		Calculated Parame	ters for Overflow Not Selected		
Jser Input: Overflow Weir (Dropbox with Flat or Overflow Weir Front Edge Height, Ho =				al Weir and No Outl		e Upper Edge, $H_t$ =	Zone 3 Weir			
	Zone 3 Weir	Not Selected			t) Height of Grat	e Upper Edge, H <sub>t</sub> = /eir Slope Length =	Zone 3 Weir 4.00	Not Selected		
	Zone 3 Weir 4.00	Not Selected N/A	ft (relative to basin b	pottom at Stage = 0 f	t) Height of Grat	/eir Slope Length =	Zone 3 Weir 4.00 6.00	Not Selected N/A		
Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length =	Zone 3 Weir 4.00 6.00	Not Selected N/A N/A	ft (relative to basin t feet	pottom at Stage = 0 f G	t) Height of Grat Overflow W	/eir Slope Length = 00-yr Orifice Area =	Zone 3 Weir 4.00 6.00 9.91	Not Selected N/A N/A		
Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope =	Zone 3 Weir 4.00 6.00 0.00	Not Selected N/A N/A N/A	ft (relative to basin t feet H:V	oottom at Stage = 0 f G O	t) Height of Grat Overflow W rate Open Area / 10	/eir Slope Length = 00-yr Orifice Area = Area w/o Debris =	Zone 3 Weir 4.00 6.00 9.91 25.06	Not Selected N/A N/A N/A		
Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides =	Zone 3 Weir 4.00 6.00 0.00 6.00	Not Selected N/A N/A N/A N/A	ft (relative to basin t feet H:V	oottom at Stage = 0 f G O	t) Height of Grat Overflow W rate Open Area / 10 verflow Grate Open	/eir Slope Length = 00-yr Orifice Area = Area w/o Debris =	Zone 3 Weir 4.00 6.00 9.91 25.06	Not Selected N/A N/A N/A N/A		
Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % =	Zone 3 Weir 4.00 6.00 0.00 6.00 Type C Grate 50%	Not Selected N/A N/A N/A N/A N/A N/A	ft (relative to basin t feet H:V feet %	oottom at Stage = 0 f G O	t) Height of Grat Overflow W rate Open Area / 10 verflow Grate Open Overflow Grate Ope	Veir Slope Length = 00-yr Orifice Area = Area w/o Debris = en Area w/ Debris =	Zone 3 Weir 4.00 6.00 9.91 25.06 12.53	Not Selected N/A N/A N/A N/A N/A		
Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % =	Zone 3 Weir 4.00 6.00 0.00 6.00 Type C Grate 50% (Circular Orifice, R	Not Selected N/A N/A N/A N/A N/A estrictor Plate, or R	ft (relative to basin t feet H:V feet %	oottom at Stage = 0 f G O	t) Height of Grat Overflow W rate Open Area / 10 verflow Grate Open Overflow Grate Ope	Veir Slope Length = 00-yr Orifice Area = Area w/o Debris = en Area w/ Debris =	Zone 3 Weir 4.00 6.00 9.91 25.06 12.53 rs for Outlet Pipe w/	Not Selected N/A N/A N/A N/A N/A Flow Restriction		
Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = Jser Input: Outlet Pipe w/ Flow Restriction Plate	Zone 3 Weir 4.00 6.00 0.00 6.00 Type C Grate 50% ( <u>Circular Orifice, R</u> Zone 3 Restrictor	Not Selected N/A N/A N/A N/A N/A estrictor Plate, or R Not Selected	ft (relative to basin t feet H:V feet % ectangular Orifice)	bottom at Stage = 0 f G O (	t) Height of Grat Overflow W rate Open Area / I verflow Grate Open Overflow Grate Open Overflow Grate Ope	/eir Slope Length = )0-yr Orifice Area = Area w/o Debris = In Area w/ Debris = alculated Parameter	Zone 3 Weir           4.00           6.00           9.91           25.06           12.53   rs for Outlet Pipe w/	Not Selected N/A N/A N/A N/A N/A Flow Restriction Not Selected		
Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = Jser Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe =	Zone 3 Weir 4.00 6.00 0.00 6.00 Type C Grate 50% ( <u>Circular Orifice, R</u> Zone 3 Restrictor 0.50	Not Selected N/A N/A N/A N/A N/A N/A estrictor Plate, or R Not Selected N/A	ft (relative to basin t feet H:V feet % ectangular Orifice)	oottom at Stage = 0 f G O	t) Height of Grat Overflow W rate Open Area / 10 verflow Grate Open Overflow Grate Open <u>Ca</u> = 0 ft) O	Veir Slope Length = 00-yr Orifice Area = Area w/o Debris = in Area w/ Debris = alculated Parameter Nutlet Orifice Area =	Zone 3 Weir           4.00           6.00           9.91           25.06           12.53   rs for Outlet Pipe www. Zone 3 Restrictor 2.53	Not Selected N/A N/A N/A N/A N/A Flow Restriction Not Selected N/A		
Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = Jser Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter =	Zone 3 Weir 4.00 6.00 0.00 6.00 Type C Grate 50% ( <u>Circular Orifice, R</u> Zone 3 Restrictor 0.50 24.00	Not Selected N/A N/A N/A N/A N/A estrictor Plate, or R Not Selected	ft (relative to basin t feet H:V feet % ectangular Orifice) ft (distance below ba inches	bottom at Stage = 0 f G O ( asin bottom at Stage	t) Height of Grat Overflow W rate Open Area / 10 verflow Grate Open Overflow Grate Open <u>Ca</u> = 0 ft) 0 Outle	Veir Slope Length = 00-yr Orifice Area = Area w/o Debris = in Area w/ Debris = alculated Parameter utlet Orifice Area = t Orifice Centroid =	Zone 3 Weir           4.00           6.00           9.91           25.06           12.53   rs for Outlet Pipe www. Zone 3 Restrictor 2.53 0.83	Not Selected N/A N/A N/A N/A N/A Flow Restriction Not Selected N/A N/A		
Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe =	Zone 3 Weir 4.00 6.00 0.00 6.00 Type C Grate 50% ( <u>Circular Orifice, R</u> Zone 3 Restrictor 0.50	Not Selected N/A N/A N/A N/A N/A N/A estrictor Plate, or R Not Selected N/A	ft (relative to basin t feet H:V feet % ectangular Orifice) ft (distance below ba	bottom at Stage = 0 f G O ( asin bottom at Stage	t) Height of Grat Overflow W rate Open Area / 10 verflow Grate Open Overflow Grate Open <u>Ca</u> = 0 ft) O	Veir Slope Length = 00-yr Orifice Area = Area w/o Debris = in Area w/ Debris = alculated Parameter utlet Orifice Area = t Orifice Centroid =	Zone 3 Weir           4.00           6.00           9.91           25.06           12.53   rs for Outlet Pipe www. Zone 3 Restrictor 2.53 0.83	Not Selected N/A N/A N/A N/A N/A Flow Restriction Not Selected N/A		
Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = Jser Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert =	Zone 3 Weir 4.00 6.00 0.00 6.00 Type C Grate 50% ( <u>Circular Orifice, R</u> Zone 3 Restrictor 0.50 24.00 18.00	Not Selected N/A N/A N/A N/A N/A N/A estrictor Plate, or R Not Selected N/A	ft (relative to basin t feet H:V feet % ectangular Orifice) ft (distance below ba inches	bottom at Stage = 0 f G O ( asin bottom at Stage	t) Height of Grat Overflow W rate Open Area / 10 verflow Grate Open Overflow Grate Open <u>Ca</u> = 0 ft) 0 Outle	Veir Slope Length = 00-yr Orifice Area = Area w/o Debris = in Area w/ Debris = alculated Parameter utlet Orifice Area = t Orifice Centroid =	Zone 3 Weir           4.00           6.00           9.91           25.06           12.53   rs for Outlet Pipe www. Zone 3 Restrictor           2.53           2.53	Not Selected N/A N/A N/A N/A N/A Flow Restriction Not Selected N/A N/A N/A		
Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = Jser Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = Jser Input: Emergency Spillway (Rectangular or	Zone 3 Weir 4.00 6.00 0.00 Type C Grate 50% (Circular Orifice, R Zone 3 Restrictor 0.50 24.00 18.00	Not Selected N/A N/A N/A N/A N/A N/A N/A estrictor Plate, or R Not Selected N/A N/A	ft (relative to basin t feet H:V feet % <u>ectangular Orifice)</u> ft (distance below ba inches inches	bottom at Stage = 0 f G O ( asin bottom at Stage Half-Cen	t) Height of Grat Overflow V rate Open Area / 10 verflow Grate Open Overflow Grate Open Cerflow Grate Ope <u>Ce</u> = 0 ft) O Outle tral Angle of Restric	Veir Slope Length = 00-yr Orifice Area = Area w/o Debris = an Area w/ Debris = alculated Parameter alculated Parameter utlet Orifice Area = t Orifice Centroid = ctor Plate on Pipe =	Zone 3 Weir           4.00           6.00           9.91           25.06           12.53   rs for Outlet Pipe w/ Zone 3 Restrictor           2.53           0.83           0.83           2.09	Not Selected N/A N/A N/A N/A N/A Flow Restriction Not Selected N/A N/A N/A N/A		
Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = Jser Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = Jser Input: Emergency Spillway (Rectangular or Spillway Invert Stage=	Zone 3 Weir 4.00 6.00 0.00 6.00 Type C Grate 50% (Circular Orifice, R Zone 3 Restrictor 0.50 24.00 18.00 Trapezoidal) 6.00	Not Selected N/A N/A N/A N/A N/A N/A N/A estrictor Plate, or R Not Selected N/A N/A	ft (relative to basin t feet H:V feet % ectangular Orifice) ft (distance below ba inches	bottom at Stage = 0 f G O ( asin bottom at Stage Half-Cen	t) Height of Grat Overflow V rate Open Area / 10 verflow Grate Open Overflow Grate Open Cerflow Grate Ope <u>Ce</u> = 0 ft) O Outle tral Angle of Restric Spillway D	Veir Slope Length = 00-yr Orifice Area = Area w/o Debris = an Area w/ Debris = alculated Parameter butlet Orifice Area = t Orifice Centroid = ttor Plate on Pipe = Design Flow Depth=	Zone 3 Weir           4.00           6.00           9.91           25.06           12.53           rs for Outlet Pipe w/           Zone 3 Restrictor           2.53           0.83           2.09           Calculated Parame           0.55	Not Selected N/A N/A N/A N/A N/A Flow Restriction Not Selected N/A N/A N/A N/A ters for Spillway feet		
Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = Jser Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = Jser Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length =	Zone 3 Weir 4.00 6.00 0.00 6.00 Type C Grate 50% (Circular Orifice, R Zone 3 Restrictor 0.50 24.00 18.00 Trapezoidal) 6.00 50.00	Not Selected N/A N/A N/A N/A N/A N/A N/A N/A estrictor Plate, or R Not Selected N/A N/A ft (relative to basin feet	ft (relative to basin t feet H:V feet % <u>ectangular Orifice)</u> ft (distance below ba inches inches	bottom at Stage = 0 f G O ( asin bottom at Stage Half-Cen	t) Height of Grat Overflow W rate Open Area / I verflow Grate Open Overflow Grate Open Overflow Grate Ope <u>Ca</u> = 0 ft) O Uutle tral Angle of Restric Spillway D Stage at	Veir Slope Length = 00-yr Orifice Area = Area w/o Debris = an Area w/ Debris = alculated Parameter Nutlet Orifice Area = t Orifice Centroid = ctor Plate on Pipe = Design Flow Depth= Top of Freeboard =	Zone 3 Weir           4.00           6.00           9.91           25.06           12.53   rs for Outlet Pipe w/ Zone 3 Restrictor           2.53           0.83           2.09           Calculated Parame           0.55           7.55	Not Selected N/A N/A N/A N/A N/A Flow Restriction Not Selected N/A N/A N/A N/A ters for Spillway feet feet		
Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length = Spillway End Slopes =	Zone 3 Weir 4.00 6.00 0.00 6.00 Type C Grate 50% (Circular Orifice, R Zone 3 Restrictor 0.50 24.00 18.00 Trapezoidal) 6.00 50.00 4.00	Not Selected N/A N/A N/A N/A N/A N/A estrictor Plate, or R Not Selected N/A N/A ft (relative to basir feet H:V	ft (relative to basin t feet H:V feet % <u>ectangular Orifice)</u> ft (distance below ba inches inches	bottom at Stage = 0 f G O ( asin bottom at Stage Half-Cen	t) Height of Grat Overflow W rate Open Area / 10 verflow Grate Open Overflow Grate Open Car Car Car Car Car Car Car Car Car Car	Veir Slope Length = 00-yr Orifice Area = Area w/o Debris = an Area w/ Debris = alculated Parameter Nutlet Orifice Area = t Orifice Centroid = tor Plate on Pipe = Design Flow Depth= Top of Freeboard = Top of Freeboard =	Zone 3 Weir           4.00           6.00           9.91           25.06           12.53   rs for Outlet Pipe w// Zone 3 Restrictor           Zone 3 Restrictor           2.53           0.83           2.09           Calculated Parame           0.55           7.55           0.69	Not Selected N/A N/A N/A N/A N/A Flow Restriction Not Selected N/A N/A N/A N/A ters for Spillway feet feet acres		
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Stage (ft)

MHFD-Detention, Version 4.06 (July 2022)

#### Project: FLYING HORSE NORTH PUD PRELIMINARY PLAN Basin ID: BASINS: C ; DESIGN POINT 11

100-YR VOLUME EURV	ZONE 2 ZONE 2 ZONE 1	-
	ZONE 1 AND 2 ORIFICE PERMANENT ORIFICES POOL Strength of the Construction of the Const	

 $\geq$ Depth Increment = Stage - Storage Description Example Zone Configuration (Retention Pond)

7526

Top of Micropool

#### Watershed Information

Selected BMP Type =	EDB				
Watershed Area =	121.00	acres			
Watershed Length =	2,500	ft			
Watershed Length to Centroid =	1,250	ft			
Watershed Slope =	0.010	ft/ft			
Watershed Imperviousness =	31.60%	percent			
Percentage Hydrologic Soil Group A =	0.0%	percent			
Percentage Hydrologic Soil Group B =	100.0%	percent			
Percentage Hydrologic Soil Groups C/D =	0.0%	percent			
Target WQCV Drain Time =	40.0	hours			
Location for 1-hr Rainfall Depths = User Input					

# After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

the embedded colorado orban hydro	graph Floceuc	ile.
Water Quality Capture Volume (WQCV) =	1.577	acre-feet
Excess Urban Runoff Volume (EURV) =	3.940	acre-feet
2-yr Runoff Volume (P1 = 1.19 in.) =	3.965	acre-feet
5-yr Runoff Volume (P1 = 1.5 in.) =	6.340	acre-feet
10-yr Runoff Volume (P1 = 1.75 in.) =	8.517	acre-feet
25-yr Runoff Volume (P1 = 2 in.) =	11.776	acre-feet
50-yr Runoff Volume (P1 = 2.25 in.) =	14.262	acre-feet
100-yr Runoff Volume (P1 = 2.52 in.) =	17.560	acre-feet
500-yr Runoff Volume (P1 = 3.14 in.) =	23.960	acre-feet
Approximate 2-yr Detention Volume =	2.834	acre-feet
Approximate 5-yr Detention Volume =	4.038	acre-feet
Approximate 10-yr Detention Volume =	5.823	acre-feet
Approximate 25-yr Detention Volume =	6.705	acre-feet
Approximate 50-yr Detention Volume =	7.060	acre-feet
Approximate 100-yr Detention Volume =	8.302	acre-feet

### Define Zones and Basin Geometry

Define Zones and Basin Geometry		
Zone 1 Volume (WQCV) =	1.577	acre-feet
Zone 2 Volume (EURV - Zone 1) =	2.364	acre-feet
Zone 3 Volume (100-year - Zones 1 & 2) =	4.361	acre-feet
Total Detention Basin Volume =	8.302	acre-feet
Initial Surcharge Volume (ISV) =	user	ft <sup>3</sup>
Initial Surcharge Depth (ISD) =	user	ft
Total Available Detention Depth (H <sub>total</sub> ) =	user	ft
Depth of Trickle Channel (H <sub>TC</sub> ) =	user	ft
Slope of Trickle Channel (STC) =	user	ft/ft
Slopes of Main Basin Sides (S <sub>main</sub> ) =	user	H:V
Basin Length-to-Width Ratio (R <sub>L/W</sub> ) =	user	

#### ft ² Initial Surcharge Area (A<sub>ISV</sub>) = user Surcharge Volume Length (LISV) = user ft Surcharge Volume Width $(W_{ISV}) =$ user Depth of Basin Floor (H<sub>FLOOR</sub>) = user Length of Basin Floor (L<sub>FLOOR</sub>) = user Width of Basin Floor ( $W_{FLOOR}$ ) = user Area of Basin Floor (A<sub>FLOOR</sub>) = user Volume of Basin Floor (V<sub>FLOOR</sub>) = user Depth of Main Basin $(H_{MAIN})$ = user Length of Main Basin (LMAIN) = user Width of Main Basin ( $W_{MAIN}$ ) = user Area of Main Basin $(A_{MAIN}) =$ Volume of Main Basin $(V_{MAIN}) =$ user Ĥ user Calculated Total Basin Volume (V<sub>total</sub>) = user

				1.00				9,667	0.222	4,833	0.111
				2.00				37,002	0.849	28,168	0.647
				3.00	-	-	-	70,876	1.627	82,106	1.885
				4.00				82,455	1.893	158,772	3.645
		7531		5.00				86,963	1.996	243,481	5.590
				6.00				91,578	2.102	332,751	7.639
			-	7.00	-		-	96,300	2.211	426,690	9.795
		TOP: 7534		8.00				101,130	2.322	525,405	12.062
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Optional Use	7										
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Area (ft<sup>2</sup>)

Width

(ft)

Length (ft)

Stage (ft)

0.00

1.00

Area (acre)

0.000

0.222

rea (ft<sup>2</sup>

0

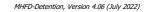
9,667

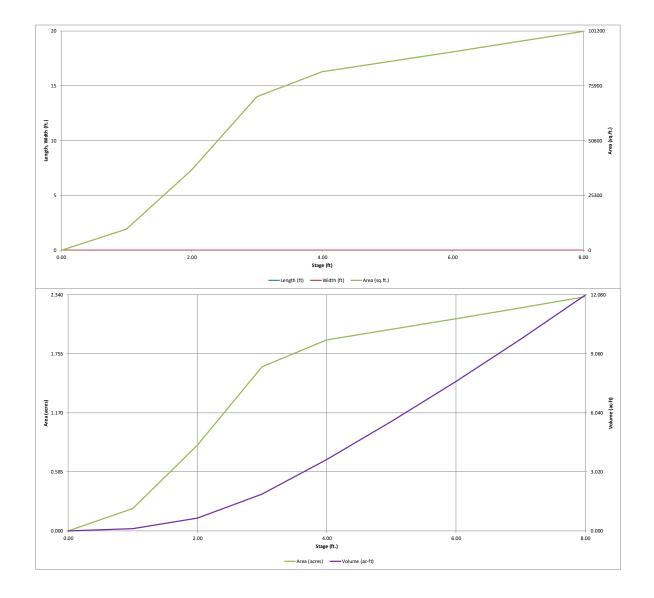
Volume (ft <sup>3</sup>)

4,833

Volume (ac-ft)

0.111



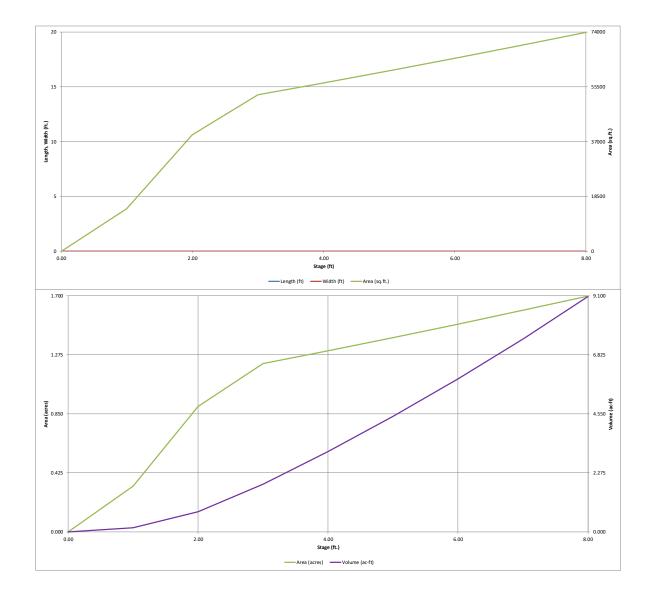


MHFD-Detention, Version 4.06 (July 2022)

#### Project: FLYING HORSE NORTH PUD PRELIMINARY PLAN Basin ID: BASINS: D, OS4 ; DESIGN POINT 13

	BASINS: D,	OS4 ; DES	IGN POINT 1	3										
ZONE 3	2 ONE 1	_	_											
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	1 AND 2	ORIFIC	CE		Depth Increment =		ft Optional		1		Ontional			
POOL Example Zone		tion (Rete	ntion Pond)		Stage - Storage	Stage	Override	Length	Width	Area	Override	Area	Volume	Volume
Websuch and Teffermentian					Description	(ft)	Stage (ft) 0.00	(ft)	(ft)	(ft <sup>2</sup> )	Area (ft <sup>2</sup> )	(acre) 0.000	(ft 3)	(ac-ft)
Watershed Information	500	1		7530	Top of Micropool						0		2442	0.454
Selected BMP Type =	EDB	_	Note: L / W				1.00				14,296	0.328	7,147	0.164
Watershed Area =	158.50	acres	L / W Ratio	= 0.73			2.00				39,265	0.901	33,928	0.779
Watershed Length = Watershed Length to Centroid =	2,250	π ft					3.00 4.00				52,784 56,790	1.212	79,952 134,739	1.835 3.093
Watershed Eength to Centrold = Watershed Slope =	0.025	ft/ft					5.00				60,908	1.398	193,588	4.444
Watershed Imperviousness =	15.50%	percent					6.00				65,138	1.495	256,611	5.891
Percentage Hydrologic Soil Group A =	0.0%	percent					7.00				69,479	1.595	323,920	7.436
Percentage Hydrologic Soil Group B =	100.0%	percent			TOP:7538	-	8.00			-	73,933	1.697	395,626	9.082
Percentage Hydrologic Soil Groups C/D =	0.0%	percent												
Target WQCV Drain Time =	40.0	hours												
Location for 1-hr Rainfall Depths =														
After providing required inputs above in depths, click 'Run CUHP' to generate run	cluding 1-hour	rainfall								-				
the embedded Colorado Urban Hydro			Optional Use	r Overrides				-		-				
Water Quality Capture Volume (WQCV) =	1.264	acre-feet	optional obc	acre-feet										
Excess Urban Runoff Volume (EURV) =	2.391	acre-feet		acre-feet										
2-yr Runoff Volume (P1 = 1.19 in.) =	2.840	acre-feet	1.19	inches										
5-yr Runoff Volume (P1 = 1.5 in.) =	5.559	acre-feet	1.50	inches		-								
10-yr Runoff Volume (P1 = 1.75 in.) =	8.198	acre-feet	1.75	inches										
25-yr Runoff Volume (P1 = 2 in.) =	12.663	acre-feet	2.00	inches										
50-yr Runoff Volume (P1 = 2.25 in.) =	15.793	acre-feet	2.25	inches						-				
100-yr Runoff Volume (P1 = 2.52 in.) =	20.207	acre-feet	2.52	inches										
500-yr Runoff Volume (P1 = 3.14 in.) = Approximate 2-yr Detention Volume =	28.375	acre-feet		inches										
Approximate 2 yr Detention Volume =	2.416	acre-feet												
Approximate 10-yr Detention Volume =	4.232	acre-feet												
Approximate 25-yr Detention Volume =	5.479	acre-feet												
Approximate 50-yr Detention Volume =	5.780	acre-feet												
Approximate 100-yr Detention Volume =	7.254	acre-feet												
		-								-				
Define Zones and Basin Geometry	1	7												
Zone 1 Volume (WQCV) =	1.264	acre-feet						-		-				
Zone 2 Volume (EURV - Zone 1) =	1.127	acre-feet												
Zone 3 Volume (100-year - Zones 1 & 2) =	4.863 7.254	acre-feet acre-feet												
Total Detention Basin Volume = Initial Surcharge Volume (ISV) =	User	ft <sup>3</sup>						-		-				
Initial Surcharge Depth (ISD) =	user	ft						-		-				
Total Available Detention Depth (H <sub>total</sub> ) =	user	ft												
Depth of Trickle Channel (H <sub>TC</sub> ) =	user	ft												
Slope of Trickle Channel (STC) =	user	ft/ft												
Slopes of Main Basin Sides (Smain) =	user	H:V												
Basin Length-to-Width Ratio $(R_{L/W}) =$	user							-						
		-												
Initial Surcharge Area (A <sub>ISV</sub> ) =	user	ft 2												
Surcharge Volume Length $(L_{ISV}) =$	user	ft												
Surcharge Volume Width (W <sub>ISV</sub> ) = Depth of Basin Floor (H <sub>FLOOR</sub> ) =	user	ft ft												
Length of Basin Floor ( $L_{FLOOR}$ ) =	user	ft						-		-				
Width of Basin Floor (W <sub>FLOOR</sub> ) =	user	ft												
Area of Basin Floor (A <sub>FLOOR</sub> ) =	user	ft <sup>2</sup>												
Volume of Basin Floor (V <sub>FLOOR</sub> ) =	user	ft <sup>3</sup>												
Depth of Main Basin $(H_{MAIN}) =$	user	ft												
Length of Main Basin ( $L_{MAIN}$ ) =	user	ft						-						
Width of Main Basin (W <sub>MAIN</sub> ) =	user	ft					L			-				
Area of Main Basin (A <sub>MAIN</sub> ) =	user	ft <sup>2</sup>												
Volume of Main Basin (V <sub>MAIN</sub> ) =	user	ft '												
Calculated Total Basin Volume ( $V_{total}$ ) =	user	acre-feet												
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MHFD-Detention, Version 4.06 (July 2022)



Stage (ft)

Override Stage (ft)

0.00

1.00

2.00

Depth Increment =

Stage - Storage Description

7550 Top of Micropool

MHFD-Detention, Version 4.06 (July 2022)

Optional User Override acre-fee acre-fee

1.19 inches

1.50 inches 1.75 inches 2.00 inches 2.25 inches 2.52 inches inches

#### Project: FLYING HORSE NORTH PUD PRELIMINARY PLAN Basin ID: BASIN: E ; DESIGN POINT 15

POOL Example Zone Configuration (Retention Pond)

### Watershed Info

itersned information		
Selected BMP Type =	EDB	
Watershed Area =	52.40	acres
Watershed Length =	1,700	ft
Watershed Length to Centroid =	650	ft
Watershed Slope =	0.050	ft/ft
Watershed Imperviousness =	43.70%	percent
Percentage Hydrologic Soil Group A =	0.0%	percent
Percentage Hydrologic Soil Group B =	100.0%	percent
Percentage Hydrologic Soil Groups C/D =	0.0%	percent
Target WQCV Drain Time =	40.0	hours
Location for 1-hr Rainfall Depths =	User Input	

# After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

the embedded Colorado Orban Hydro	igraph Procedu	ire.
Water Quality Capture Volume (WQCV) =	0.828	acre-feet
Excess Urban Runoff Volume (EURV) =	2.422	acre-feet
2-yr Runoff Volume (P1 = 1.19 in.) =	2.287	acre-feet
5-yr Runoff Volume (P1 = 1.5 in.) =	3.360	acre-feet
10-yr Runoff Volume (P1 = 1.75 in.) =	4.316	acre-feet
25-yr Runoff Volume (P1 = 2 in.) =	5.656	acre-feet
50-yr Runoff Volume (P1 = 2.25 in.) =	6.714	acre-feet
100-yr Runoff Volume (P1 = 2.52 in.) =	8.081	acre-feet
500-yr Runoff Volume (P1 = 3.14 in.) =	10.820	acre-feet
Approximate 2-yr Detention Volume =	1.802	acre-feet
Approximate 5-yr Detention Volume =	2.498	acre-feet
Approximate 10-yr Detention Volume =	3.384	acre-feet
Approximate 25-yr Detention Volume =	3.748	acre-feet
Approximate 50-yr Detention Volume =	3.928	acre-feet
Approximate 100-yr Detention Volume =	4.454	acre-feet

### Define Zones and Basin Geometry

Jenne Zones and Basin Geometry		
Zone 1 Volume (WQCV) =	0.828	acre-feet
Zone 2 Volume (EURV - Zone 1) =	1.594	acre-feet
Zone 3 Volume (100-year - Zones 1 & 2) =	2.032	acre-feet
Total Detention Basin Volume =	4.454	acre-feet
Initial Surcharge Volume (ISV) =	user	ft <sup>3</sup>
Initial Surcharge Depth (ISD) =	user	ft
Total Available Detention Depth (H <sub>total</sub> ) =	user	ft
Depth of Trickle Channel (H <sub>TC</sub> ) =	user	ft
Slope of Trickle Channel (STC) =	user	ft/ft
Slopes of Main Basin Sides (S <sub>main</sub> ) =	user	H:V
Basin Length-to-Width Ratio (R <sub>L/W</sub> ) =	user	

#### ft ² Initial Surcharge Area (AISV) = user Surcharge Volume Length (LISV) = user ft Surcharge Volume Width $(W_{ISV}) =$ user Depth of Basin Floor (H<sub>FLOOR</sub>) = user Length of Basin Floor (L<sub>FLOOR</sub>) = user Width of Basin Floor ( $W_{FLOOR}$ ) = user Area of Basin Floor (A<sub>FLOOR</sub>) = user Volume of Basin Floor (V<sub>FLOOR</sub>) = user Depth of Main Basin $(H_{MAIN}) =$ user Length of Main Basin (LMAIN) = user Width of Main Basin ( $W_{MAIN}$ ) = user Area of Main Basin $(A_{MAIN}) =$ Volume of Main Basin $(V_{MAIN}) =$ user Ĥ user Calculated Total Basin Volume (V<sub>total</sub>) = user acre-fe

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- L			3.00				34,450	0.791	45,979	1.056
- [			4.00				47,390	1.088	86,899	1.995
H										
			5.00	-		-	59,670	1.370	140,429	3.224
			6.00				68,780	1.579	204,654	4.698
Γ	TOP:7557		7.00				72,120	1.656	275,104	6.316
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Area (acre)

0.000

0.169

0.491

Area (ft<sup>2</sup>)

0

7,378

21,376

Area

(ft<sup>2</sup>)

Width

(ft)

Length

(ft)

Volume (ft <sup>3</sup>)

3,689

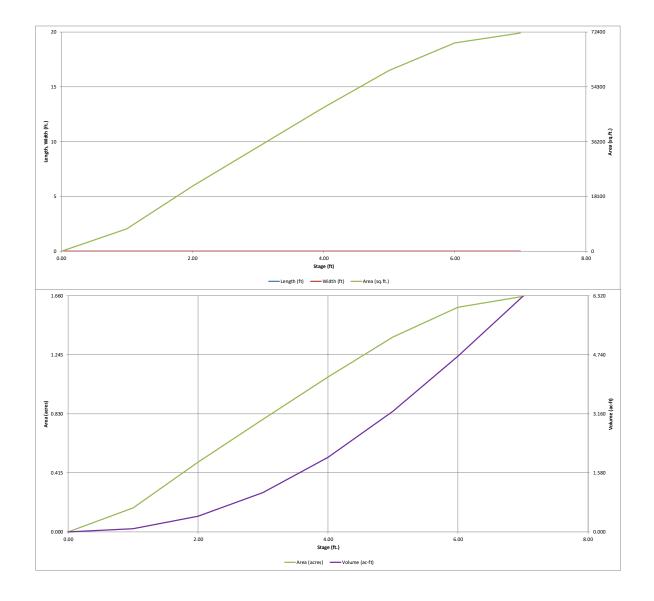
18,066

Volume (ac-ft)

0.085

0.415

MHFD-Detention, Version 4.06 (July 2022)



Stage (ft)

Depth Increment =

Stage - Storage Description

7438 Top of Micropool

MHFD-Detention, Version 4.06 (July 2022)

Optional User Overrid

1.19 inches 1.50 inches 1.75 inches 2.00 inches 2.25 inches 2.52 inches inches

#### Project: FLYING HORSE NORTH PUD PRELIMINARY PLAN Basin ID: BASINS: F. OS5 : DESIGN POINT 17

POOL Example Zone Configuration (Retention Pond)

#### Watershed Information

itersned information		
Selected BMP Type =	EDB	
Watershed Area =	238.70	acres
Watershed Length =	5,000	ft
Watershed Length to Centroid =	1,200	ft
Watershed Slope =	0.040	ft/ft
Watershed Imperviousness =	14.10%	percent
Percentage Hydrologic Soil Group A =	0.0%	percent
Percentage Hydrologic Soil Group B =	100.0%	percent
Percentage Hydrologic Soil Groups C/D =	0.0%	percent
Target WQCV Drain Time =	40.0	hours
Location for 1-hr Rainfall Depths =	User Input	

# After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

the embedded Colorado Orban Hydro	igraph Procedu	re.
Water Quality Capture Volume (WQCV) =	1.768	acre-feet
Excess Urban Runoff Volume (EURV) =	3.252	acre-feet
2-yr Runoff Volume (P1 = 1.19 in.) =	4.000	acre-feet
5-yr Runoff Volume (P1 = 1.5 in.) =	8.042	acre-feet
10-yr Runoff Volume (P1 = 1.75 in.) =	11.991	acre-feet
25-yr Runoff Volume (P1 = 2 in.) =	18.755	acre-feet
50-yr Runoff Volume (P1 = 2.25 in.) =	23.467	acre-feet
100-yr Runoff Volume (P1 = 2.52 in.) =	30.144	acre-feet
500-yr Runoff Volume (P1 = 3.14 in.) =	42.456	acre-feet
Approximate 2-yr Detention Volume =	2.151	acre-feet
Approximate 5-yr Detention Volume =	3.279	acre-feet
Approximate 10-yr Detention Volume =	5.936	acre-feet
Approximate 25-yr Detention Volume =	7.816	acre-feet
Approximate 50-yr Detention Volume =	8.236	acre-feet
Approximate 100-yr Detention Volume =	10.409	acre-feet

### Define Zones and Basin Geometry

Zone 1 Volume (WQCV) =	1.768	acre-feet
Zone 2 Volume (EURV - Zone 1) =	1.484	acre-feet
Zone 3 Volume (100-year - Zones 1 & 2) =	7.158	acre-feet
Total Detention Basin Volume =	10.409	acre-feet
Initial Surcharge Volume (ISV) =	user	ft <sup>3</sup>
Initial Surcharge Depth (ISD) =	user	ft
Total Available Detention Depth (H <sub>total</sub> ) =	user	ft
Depth of Trickle Channel (H <sub>TC</sub> ) =	user	ft
Slope of Trickle Channel (STC) =	user	ft/ft
Slopes of Main Basin Sides (Smain) =	user	H:V
Basin Length-to-Width Ratio (R <sub>L/W</sub> ) =	user	

#### ٦<sub>ft</sub> : Initial Surcharge Area (A<sub>ISV</sub>) = user Surcharge Volume Length (LISV) = user Surcharge Volume Width (W<sub>ISV</sub>) = user Depth of Basin Floor (H<sub>FLOOR</sub>) = user Length of Basin Floor (L<sub>FLOOR</sub>) = user Width of Basin Floor ( $W_{FLOOR}$ ) = user Area of Basin Floor (A<sub>FLOOR</sub>) = user Volume of Basin Floor (V<sub>FLOOR</sub>) = user Depth of Main Basin $(H_{MAIN}) =$ user Length of Main Basin (LMAIN) = user Width of Main Basin ( $W_{MAIN}$ ) = user Area of Main Basin $(A_{MAIN}) =$ Volume of Main Basin $(V_{MAIN}) =$ user Ĥ user Calculated Total Basin Volume (V<sub>total</sub>) = user acre-fe

			1.00	-		-	13,590	0.312	6,795	0.156
			2.00				46,610	1.070	36,894	0.847
			3.00			-	78,060	1.792	99,229	2.278
			4.00	-		-	104,890	2.408	190,704	4.378
	7443		5.00				116,640	2.678	301,469	6.921
			6.00	-		-	123,550	2.836	421,564	9.678
			7.00				130,667	3.000	548,673	12.596
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Volume (ft <sup>3</sup>)

6,795 0.156

Volume (ac-ft)

Area

(acre)

0.000

Area (ft<sup>2</sup>)

0

13,590 0.312

Area

(ft<sup>2</sup>)

Width

(ft)

Length

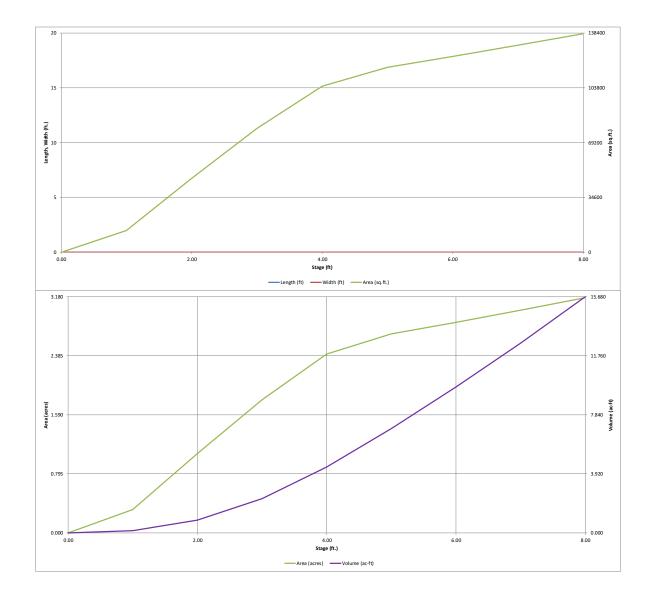
(ft)

Stage (ft)

0.00

1.00





Stage (ft)

Depth Increment = Stage - Storage Description

7442 Top of Micropool

#### Project: FLYING HORSE NORTH PUD PRELIMINARY PLAN Basin ID: BASIN G ; DESIGN POINT 18

POOL Example Zone Configuration (Retention Pond)

### Watershed Information

itersneu information		
Selected BMP Type =	EDB	
Watershed Area =	27.30	acres
Watershed Length =	1,650	ft
Watershed Length to Centroid =	800	ft
Watershed Slope =	0.030	ft/ft
Watershed Imperviousness =	16.40%	percent
Percentage Hydrologic Soil Group A =	0.0%	percent
Percentage Hydrologic Soil Group B =	100.0%	percent
Percentage Hydrologic Soil Groups C/D =	0.0%	percent
Target WQCV Drain Time =	40.0	hours
Location for 1-hr Rainfall Depths =	User Input	

# After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

the embedded Colorado Orban Hydro	igraph Procedu	ire.
Water Quality Capture Volume (WQCV) =	0.227	acre-feet
Excess Urban Runoff Volume (EURV) =	0.438	acre-feet
2-yr Runoff Volume (P1 = 1.19 in.) =	0.511	acre-feet
5-yr Runoff Volume (P1 = 1.5 in.) =	0.984	acre-feet
10-yr Runoff Volume (P1 = 1.75 in.) =	1.441	acre-feet
25-yr Runoff Volume (P1 = 2 in.) =	2.209	acre-feet
50-yr Runoff Volume (P1 = 2.25 in.) =	2.749	acre-feet
100-yr Runoff Volume (P1 = 2.52 in.) =	3.509	acre-feet
500-yr Runoff Volume (P1 = 3.14 in.) =	4.918	acre-feet
Approximate 2-yr Detention Volume =	0.294	acre-feet
Approximate 5-yr Detention Volume =	0.443	acre-feet
Approximate 10-yr Detention Volume =	0.761	acre-feet
Approximate 25-yr Detention Volume =	0.976	acre-feet
Approximate 50-yr Detention Volume =	1.030	acre-feet
Approximate 100-yr Detention Volume =	1.287	acre-feet

### Define Zones and Basin Geometry

Zone 3

Zone 1 Volume (WQCV) =	0.227	acre-feet
Zone 2 Volume (EURV - Zone 1) =	0.210	acre-feet
Zone 3 Volume (100-year - Zones 1 & 2) =	0.849	acre-feet
Total Detention Basin Volume =	1.287	acre-feet
Initial Surcharge Volume (ISV) =	user	ft <sup>3</sup>
Initial Surcharge Depth (ISD) =	user	ft
Total Available Detention Depth (H <sub>total</sub> ) =	user	ft
Depth of Trickle Channel $(H_{TC}) =$	user	ft
Slope of Trickle Channel (STC) =	user	ft/ft
Slopes of Main Basin Sides (Smain) =	user	H:V
Basin Length-to-Width Ratio (R <sub>L/W</sub> ) =	user	

#### ٦<sub>ft</sub> : Initial Surcharge Area (A<sub>ISV</sub>) = user Surcharge Volume Length (LISV) = user ft Surcharge Volume Width (W<sub>ISV</sub>) = user Depth of Basin Floor (H<sub>FLOOR</sub>) = user Length of Basin Floor (L<sub>FLOOR</sub>) = user Width of Basin Floor ( $W_{FLOOR}$ ) = user Area of Basin Floor (A<sub>FLOOR</sub>) = user Volume of Basin Floor (V<sub>FLOOR</sub>) = user Depth of Main Basin $(H_{MAIN}) =$ user Length of Main Basin (LMAIN) = user Width of Main Basin ( $W_{MAIN}$ ) = user user Ĥ

	7442	Top of Micropool		0.00				0	0.000		
				1.00				9,180	0.211	4,590	0.105
				2.00				25,856	0.594	22,108	0.508
				3.00				34,590	0.794	52,331	1.201
				4.00				40,046	0.919	89,649	2.058
		TOP:7447		5.00				45,920	1.054	132,632	3.045
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Area (acre)

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Area

(ft<sup>2</sup>)

Area (ft<sup>2</sup>

0

Width

(ft)

Length

(ft)

Stage (ft)

0.00

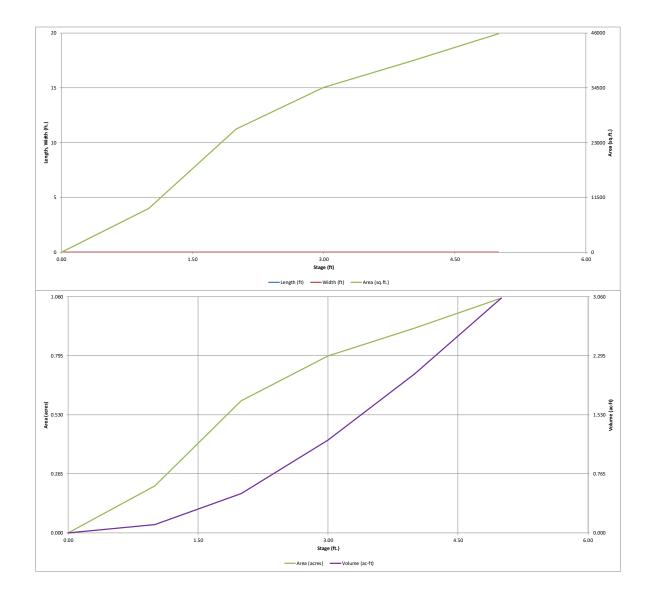
Volume (ft <sup>3</sup>)

Volume (ac-ft)

# er er er er er ft ft ft/ft H:V er

Area of Main Basin ( $A_{MAIN}$ ) = Volume of Main Basin ( $V_{MAIN}$ ) = user Calculated Total Basin Volume (V<sub>total</sub>) = user

MHFD-Detention, Version 4.06 (July 2022)



Depth Increment =

MHFD-Detention, Version 4.06 (July 2022)

#### Project: FLYING HORSE NORTH PUD PRELIMINARY PLAN Basin ID: BASIN J ; DESIGN POINT 21

POOL Example Zone Configuration (Potention Bond)

Example Zone Configuration (Retention Pond)

### Watershed Information

Selected BMP Type =	EDB	
Watershed Area =	15.80	acres
Watershed Length =	1,150	ft
Watershed Length to Centroid =	350	ft
Watershed Slope =	0.040	ft/ft
Watershed Imperviousness =	86.10%	percent
Percentage Hydrologic Soil Group A =	0.0%	percent
Percentage Hydrologic Soil Group B =	100.0%	percent
Percentage Hydrologic Soil Groups C/D =	0.0%	percent
Target WQCV Drain Time =	40.0	hours
Location for 1-hr Rainfall Depths =	User Input	

# After providing required inputs above including 1-depths, click 'Run CUHP' to generate runoff hydrog the embedded Colorado Urban Hydrograph Pro

the embedded Colorado Orban Hydro	graph Procedu	re.
Water Quality Capture Volume (WQCV) =	0.487	acre-feet
Excess Urban Runoff Volume (EURV) =	1.519	acre-feet
2-yr Runoff Volume (P1 = 1.19 in.) =	1.272	acre-feet
5-yr Runoff Volume (P1 = 1.5 in.) =	1.665	acre-feet
10-yr Runoff Volume (P1 = 1.75 in.) =	1.988	acre-feet
25-yr Runoff Volume (P1 = 2 in.) =	2.332	acre-feet
50-yr Runoff Volume (P1 = 2.25 in.) =	2.662	acre-feet
100-yr Runoff Volume (P1 = 2.52 in.) =	3.031	acre-feet
500-yr Runoff Volume (P1 = 3.14 in.) =	3.854	acre-feet
Approximate 2-yr Detention Volume =	1.213	acre-feet
Approximate 5-yr Detention Volume =	1.588	acre-feet
Approximate 10-yr Detention Volume =	1.955	acre-feet
Approximate 25-yr Detention Volume =	2.094	acre-feet
Approximate 50-yr Detention Volume =	2.174	acre-feet
Approximate 100-yr Detention Volume =	2.270	acre-feet

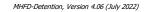
#### Define Zones and Basin Geometry

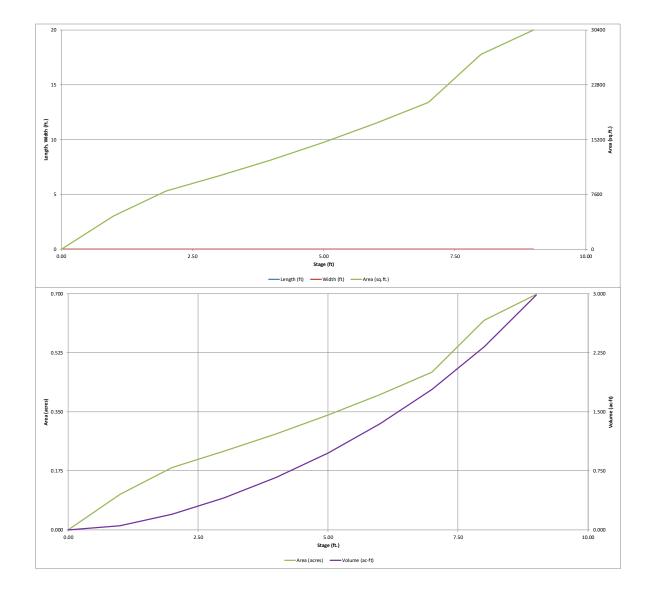
0.4	Zone 1 Volume (WQCV) =
1.0	Zone 2 Volume (EURV - Zone 1) =
0.7	Zone 3 Volume (100-year - Zones 1 & 2) =
2.2	Total Detention Basin Volume =
USE	Initial Surcharge Volume (ISV) =
USE	Initial Surcharge Depth (ISD) =
USE	Total Available Detention Depth (H <sub>total</sub> ) =
USE	Depth of Trickle Channel (H <sub>TC</sub> ) =
USE	Slope of Trickle Channel (S <sub>TC</sub> ) =
USE	Slopes of Main Basin Sides (Smain) =
USE	Basin Length-to-Width Ratio (R <sub>L/W</sub> ) =

#### Initial Surcharge Area (A<sub>ISV</sub>) = use Surcharge Volume Length (LISV) = use use use user user Width of Basin Floor ( $W_{FLOOR}$ ) = Area of Basin Floor ( $A_{FLOOR}$ ) = use Volume of Basin Floor (V<sub>FLOOR</sub>) = $Depth of Main Basin (H_{MAIN}) = \\ Length of Main Basin (L_{MAIN}) = \\ Width of Main Basin (W_{MAIN}) = \\ Width of W_{MAIN} = \\ Width of W_{MAIN} = \\ Width of W_{MAIN} = \\ Width of W_{MAIN} = \\ Width of W_{MAIN} = \\ Width of W_{MAIN} = \\ Width of W_{MAIN} = \\ Width of W_{MAIN} = \\ Width of W_{MAIN} = \\ Width of W_{MAIN} = \\ Width of W_{MAIN} = \\ Width of W_{MAIN} = \\ W W_{MAI$ use use use Area of Main Basin (A<sub>MAIN</sub>) = Volume of Main Basin (V<sub>MAIN</sub>) = use use

Location for 1-hr Rainiali Depths = User Input						
After providing required inputs above including 1-hour ra	ainfall				-	
depths, click 'Run CUHP' to generate runoff hydrographs						
the embedded Colorado Urban Hydrograph Procedure	e. 0	ptional Use	r Overrides			
Water Quality Capture Volume (WQCV) = 0.487 a	acre-feet		acre-feet			
	acre-feet		acre-feet			
	acre-feet	1.19	inches			
	acre-feet	1.50	inches			
	acre-feet	1.75	inches		-	
	acre-feet	2.00	inches			
			ł			
, , ,	acre-feet	2.25	inches			
	acre-feet	2.52	inches		-	
, , ,	acre-feet		inches			
	acre-feet					
	acre-feet					
Approximate 10-yr Detention Volume = 1.955 a	acre-feet					
Approximate 25-yr Detention Volume = 2.094 a	acre-feet					
Approximate 50-yr Detention Volume = 2.174 a	acre-feet					
Approximate 100-yr Detention Volume = 2.270 a	acre-feet					
fine Zones and Basin Geometry						
Zone 1 Volume (WQCV) = 0.487 a	acre-feet					
Zone 2 Volume (EURV - Zone 1) = 1.031 a	acre-feet					
Zone 3 Volume (100-year - Zones 1 & 2) = 0.751 a	acre-feet					
	acre-feet					
Initial Surcharge Volume (ISV) = user f	t <sup>3</sup>					
Initial Surcharge Depth (ISD) = user fi						
Total Available Detention Depth (H <sub>total</sub> ) = user fi						
Depth of Trickle Channel (H <sub>TC</sub> ) = user ff						
	t/ft					
	H:V					
Basin Length-to-Width Ratio (R <sub>L/W</sub> ) = user						
basin cengar to wider ratio (rt/w) =						
Initial Surcharge Area (A <sub>ISV</sub> ) = user fi	t²					
Surcharge Volume Length (L <sub>ISV</sub> ) = user ff						
Surcharge Volume Width (W <sub>ISV</sub> ) = user ff						
Depth of Basin Floor (H <sub>FLOOR</sub> ) = user fl						
Length of Basin Floor $(L_{FLOOR}) =$ user fl						
Width of Basin Floor (W <sub>FLOOR</sub> ) = user fl	-					
	t²					
	t³					
Depth of Main Basin (H <sub>MAIN</sub> ) = user fl						
Length of Main Basin (L <sub>MAIN</sub> ) = user f	t					
Width of Main Basin (W <sub>MAIN</sub> ) = user fl						
( Ibuly	t²				-	
Volume of Main Basin (V <sub>MAIN</sub> ) = user fi	t³					
Calculated Total Basin Volume (V <sub>total</sub> ) = user a	acre-feet					
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	Depth Increment =		ft			r	Orthogod			
	Stage - Storage	Stage	Optional Override	Length	Width	Area	Optional Override	Area	Volume	Volume
	Description	(ft)	Stage (ft)	(ft)	(ft)	(ft <sup>2</sup> )	Area (ft <sup>2</sup> )	(acre)	(ft <sup>3</sup> )	(ac-ft)
583	Top of Micropool		0.00	-			0	0.000		
			1.00	-			4,576	0.105	2,288	0.053
			2.00	-			8,060	0.185	8,606	0.198
			3.00	-			10,142	0.233	17,707	0.406
			4.00				12,370	0.284	28,963	0.665
			5.00				14,814	0.340	42,555	0.977
			6.00				17,475	0.401	58,699	1.348
			7.00	-			20,351	0.467	77,612	1.782
			8.00	-			27,036	0.621	101,306	2.326
-	TOP:7592		9.00	-	-	-	30,400	0.698	130,024	2.985
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Stage (ft)

Project: FLYING HORSE NORTH PUD PRELIMINARY PLAN Basin ID: BASIN K ; DESIGN POINT 22

100-YR VOLUME EURV	
	PERMANENT ORIFICE ORIFICES

Depth Increment = Stage - Storage Description Example Zone Configuration (Retention Pond)

7501 Top of Micropool

#### Watershed Information

Selected BMP Type =	EDB	
Watershed Area =	18.00	acres
Watershed Length =	1,400	ft
Watershed Length to Centroid =	500	ft
Watershed Slope =	0.060	ft/ft
Watershed Imperviousness =	86.00%	percent
Percentage Hydrologic Soil Group A =	0.0%	percent
Percentage Hydrologic Soil Group B =	100.0%	percent
Percentage Hydrologic Soil Groups C/D =	0.0%	percent
Target WQCV Drain Time =	40.0	hours
Location for 1-hr Rainfall Depths =	User Input	

# After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

the embedded colorado orban hydro	graph Floceuu	ile.
Water Quality Capture Volume (WQCV) =	0.554	acre-feet
Excess Urban Runoff Volume (EURV) =	1.728	acre-feet
2-yr Runoff Volume (P1 = 1.19 in.) =	1.470	acre-feet
5-yr Runoff Volume (P1 = 1.5 in.) =	1.925	acre-feet
10-yr Runoff Volume (P1 = 1.75 in.) =	2.299	acre-feet
25-yr Runoff Volume (P1 = 2 in.) =	2.697	acre-feet
50-yr Runoff Volume (P1 = 2.25 in.) =	3.079	acre-feet
100-yr Runoff Volume (P1 = 2.52 in.) =	3.507	acre-feet
500-yr Runoff Volume (P1 = 3.14 in.) =	4.460	acre-feet
Approximate 2-yr Detention Volume =	1.380	acre-feet
Approximate 5-yr Detention Volume =	1.807	acre-feet
Approximate 10-yr Detention Volume =	2.225	acre-feet
Approximate 25-yr Detention Volume =	2.383	acre-feet
Approximate 50-yr Detention Volume =	2.474	acre-feet
Approximate 100-yr Detention Volume =	2.584	acre-feet

### Define Zones and Basin Geometry

Define Zones and Basin Geometry		
Zone 1 Volume (WQCV) =	0.554	acre-feet
Zone 2 Volume (EURV - Zone 1) =	1.174	acre-feet
Zone 3 Volume (100-year - Zones 1 & 2) =	0.856	acre-feet
Total Detention Basin Volume =	2.584	acre-feet
Initial Surcharge Volume (ISV) =	user	ft <sup>3</sup>
Initial Surcharge Depth (ISD) =	user	ft
Total Available Detention Depth (H <sub>total</sub> ) =	user	ft
Depth of Trickle Channel (H <sub>TC</sub> ) =	user	ft
Slope of Trickle Channel (S <sub>TC</sub> ) =	user	ft/ft
Slopes of Main Basin Sides (S <sub>main</sub> ) =	user	H:V
Basin Length-to-Width Ratio (R <sub>L/W</sub> ) =	user	

#### ft i Initial Surcharge Area (A<sub>ISV</sub>) = user Surcharge Volume Length (LISV) = user ft Surcharge Volume Width (W<sub>ISV</sub>) = user Depth of Basin Floor (H<sub>FLOOR</sub>) = user Length of Basin Floor (L<sub>FLOOR</sub>) = user Width of Basin Floor ( $W_{FLOOR}$ ) = user Area of Basin Floor (A<sub>FLOOR</sub>) = user Volume of Basin Floor (V<sub>FLOOR</sub>) = user Depth of Main Basin $(H_{MAIN}) =$ Length of Main Basin $(L_{MAIN}) =$ user user Width of Main Basin ( $W_{MAIN}$ ) = user Area of Main Basin ( $A_{MAIN}$ ) = Volume of Main Basin ( $V_{MAIN}$ ) = user ff ft user acre-fee Calculated Total Basin Volume (V<sub>total</sub>) = user

		 1.00				8,296	0.190	4,148	0.095
		 2.00				10,427	0.239	13,509	0.310
		 3.00				11,897	0.273	24,671	0.566
		 4.00				13,449	0.309	37,344	0.857
		 5.00				15,082	0.346	51,610	1.185
		 6.00	-		-	16,797	0.346	67,549	1.165
		 7.00	-		-	18,594	0.366	85,245	1.957
		 8.00	-		-	20,473	0.427	65,245 104,778	2.405
			-		-	20,473			
	700 7544	9.00					0.515	126,231	2.898
	TOP:7511	 10.00				24,475	0.562	149,685	3.436
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Area (acre)

0.000

Area

(ft<sup>2</sup>)

Area (ft<sup>2</sup>)

0

8,296 0.190

Width

(ft)

Length

ride (ft)

Stage (ft)

0.00

1.00

Volume (ft<sup>3</sup>)

4,148 0.095

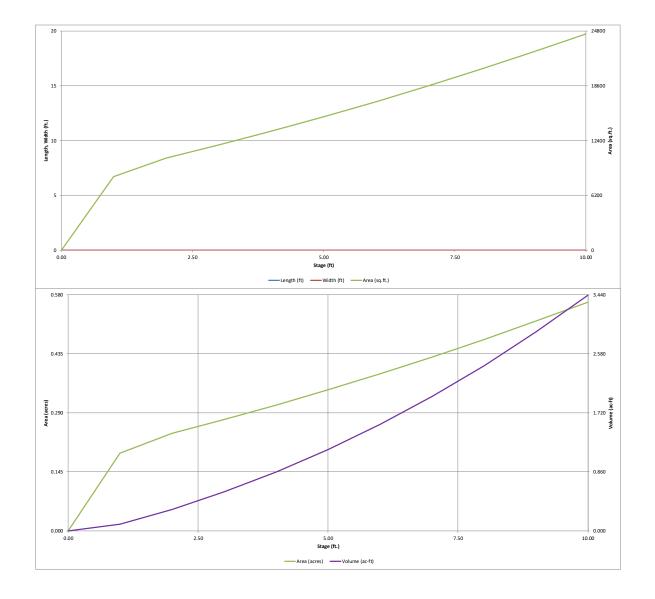
Volume (ac-ft)

# Optional User Overrid acre-fee

1.19 inches 1.50 inches 1.75 inches 2.00 inches 2.25 inches 2.52 inches inches

#### DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.06 (July 2022)



			Desig	gn Procedu	ire Form:	Runoff Red	luction					
				UD-BMP (Ve	ersion 3.07, Ma	irch 2018)						Sheet 1 of 1
Designer:	DLH										_	
	HR GREEN										_	
Date:	January 15, 2										-	
Project:	FLYING HOR	SE NORTH PUD									-	
Location:											-	
SITE INFORMATION (Use		lue Cells) Rainfall Depth	0.60	inches								
Depth of Average Ru			0.43		Vatersheds O	utside of the D	Denver Regio	n, Figure 3-1	in USDCM Vo	l. 3)		
Area Type												
Area ID	2.5AC+											
Downstream Design Point ID	OS	<b>├</b> ───										
Downstream BMP Type	None											
DCIA (ft <sup>2</sup> )	40,000											
UIA (ft <sup>2</sup> )	40,000	ł – – ł				-			-			
RPA (ft <sup>2</sup> ) SPA (ft <sup>2</sup> )	40,000	-										
HSG A (%)	0%											
HSG B (%)	100%											
HSG C/D (%)	0%	1										
Average Slope of RPA (ft/ft)	0.330											
UIA:RPA Interface Width (ft)	75.00											
.,												
CALCULATED RUNOFF	RESULTS											
Area ID	2.5AC+											
UIA:RPA Area (ft <sup>2</sup> )	80,000											
L / W Ratio	14.22											
UIA / Area	0.5000	<b>├</b> ───┤										
Runoff (in)	0.00											
Runoff (ft <sup>3</sup> ) Runoff Reduction (ft <sup>3</sup> )	1667	ł ł										
	1007	I										
CALCULATED WQCV RE	SULTS											
Area ID												
WQCV (ft <sup>3</sup> )	1667											
WQCV Reduction (ft <sup>3</sup> )	1667											
WQCV Reduction (%)	100%											
Untreated WQCV (ft <sup>3</sup> )	0											
CALCULATED DESIGN F		LTS (sums res	ults from a	II columns w	ith the same	Downstream	n Design Poi	nt ID)	1		1	
Downstream Design Point ID		<b>├</b> ───┤										
DCIA (ft <sup>2</sup> )	0											
UIA (ft <sup>2</sup> )	40,000	ł – – ł							-			
RPA (ft <sup>2</sup> ) SPA (ft <sup>2</sup> )	40,000 0								1			
Total Area (ft <sup>2</sup> )	80,000											
Total Impervious Area (ft <sup>2</sup> )	40,000	1 1										
WQCV (ft <sup>3</sup> )												
WQCV Reduction (ft <sup>3</sup> )												
WQCV Reduction (%)	100%	1										
Untreated WQCV (ft <sup>3</sup> )												
. ,												
CALCULATED SITE RES		results from a	all columns	in workshee	et)							
Total Area (ft <sup>2</sup> )	80,000			NC	DTE: TH	E PRESE	ENTED I	JDBMP	CALCUL	ATIONS	SHOW	N HERE
Total Impervious Area (ft <sup>2</sup> )	40,000	1							SCENAR			
WQCV (ft <sup>3</sup> )	1,667	1							GREATE			DES
WQCV Reduction (ft <sup>3</sup> )		4										
WQCV Reduction (%)	100%	4							D IMPEF			
Untreated WQCV (ft <sup>3</sup> )	0	J							OTAL W	QCV RE		JN OF
				10	0% IS S	TILL ACH	HEIVED.					

Large lot (2.5 acres & greater) SFD are excluded from water quality per exclusion I.7.2XXXX. This exclusion does not include detention requirements. Please identify how increase in flows from the developed areas will be mitigated if not being conveyed to a full spectrum detention ponds



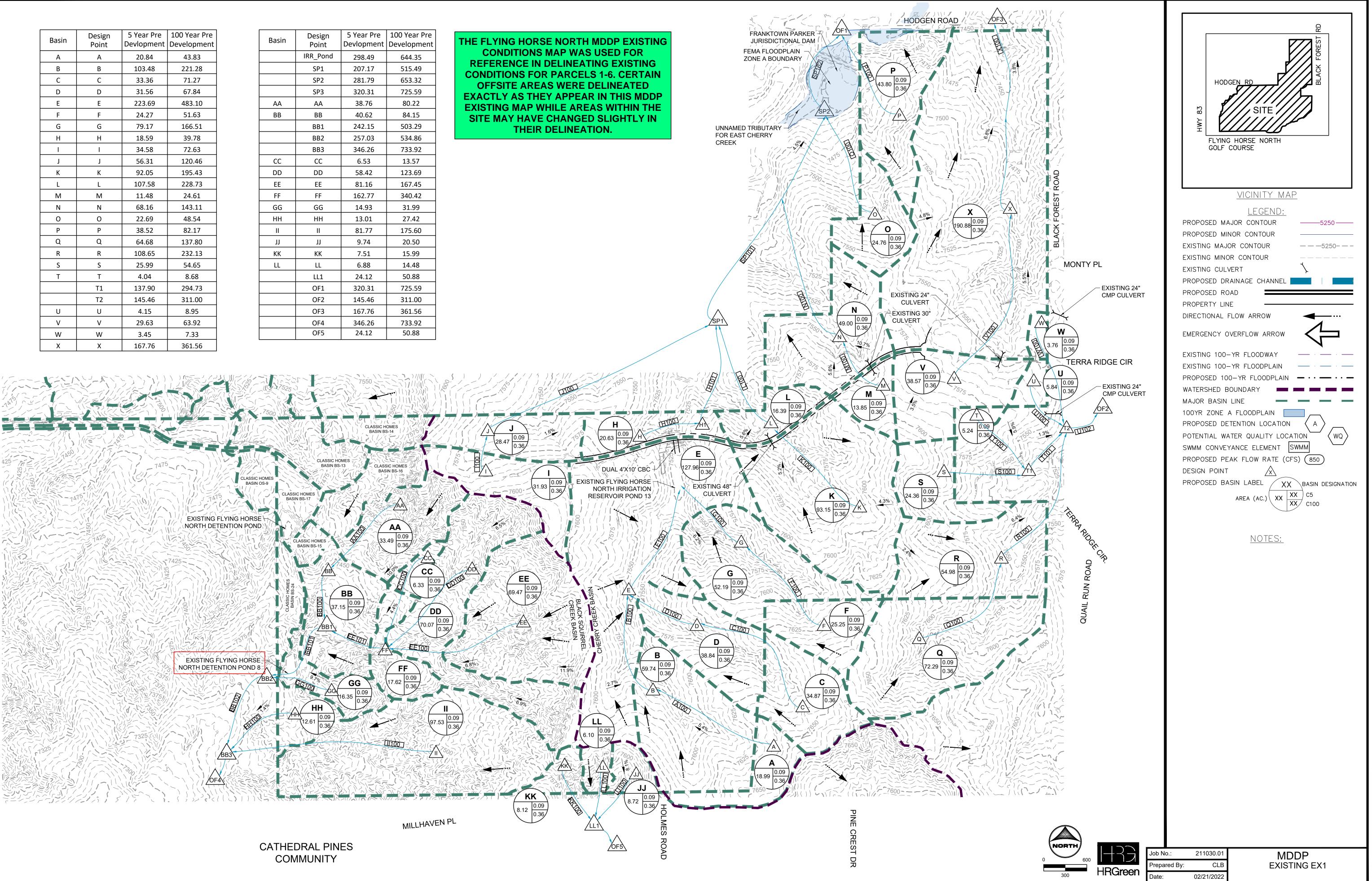
Flying Horse North Phase 2 Parcels 1-6 Preliminary Drainage Report Project No.: 211030

Appendix E:

Reference Report Excerpts and Materials

Basin	Design Point	5 Year Pre Devlopment	100 Year Pre Development
А	А	20.84	43.83
В	В	103.48	221.28
С	С	33.36	71.27
D	D	31.56	67.84
E	E	223.69	483.10
F	F	24.27	51.63
G	G	79.17	166.51
Н	Н	18.59	39.78
I	I	34.58	72.63
J	J	56.31	120.46
К	К	92.05	195.43
L	L	107.58	228.73
М	М	11.48	24.61
N	N	68.16	143.11
0	0	22.69	48.54
Р	Р	38.52	82.17
Q	Q	64.68	137.80
R	R	108.65	232.13
S	S	25.99	54.65
Т	Т	4.04	8.68
	T1	137.90	294.73
	T2	145.46	311.00
U	U	4.15	8.95
V	V	29.63	63.92
W	W	3.45	7.33
Х	Х	167.76	361.56

Basin	Design	5 Year Pre	100 Year Pre
Dasin	Point	Devlopment	Development
	IRR_Pond	298.49	644.35
	SP1	207.17	515.49
	SP2	281.79	653.32
	SP3	320.31	725.59
AA	AA	38.76	80.22
BB	BB	40.62	84.15
	BB1	242.15	503.29
	BB2	257.03	534.86
	BB3	346.26	733.92
СС	СС	6.53	13.57
DD	DD	58.42	123.69
EE	EE	81.16	167.45
FF	FF	162.77	340.42
GG	GG	14.93	31.99
НН	НН	13.01	27.42
Π	II	81.77	175.60
IJ	JJ	9.74	20.50
КК	КК	7.51	15.99
LL	LL	6.88	14.48
	LL1	24.12	50.88
	OF1	320.31	725.59
	OF2	145.46	311.00
	OF3	167.76	361.56
	OF4	346.26	733.92
	OF5	24.12	50.88





INNOVATIVE DESIGN. CLASSIC RESULTS.

### **FLYING HORSE NORTH**

## **IRRIGATION RESERVOIR EMBANKMENT**

### **DESIGN REPORT**

# DAMID: 080459 Construction File No.: C-2085

AUGUST 2018

**THIS REPORT WAS** USED FOR REFERENCE IN THE SWMM **CALCULATIONS AS** WELL AS THE **CALLOUT OF EXISTING INFRASTRUCTURE IN** THE EX AND PR **DRAINAGE MAPS. THE FOLLOWING PAGES** THAT ARE APART OF THIS DESIGN REPORT WILL HAVE OUTLINES **AND HIGHLIGHTED TEXT THAT WERE** SPECIFICALLY USED **DURING THE** PREPERATION OF THIS PDR.

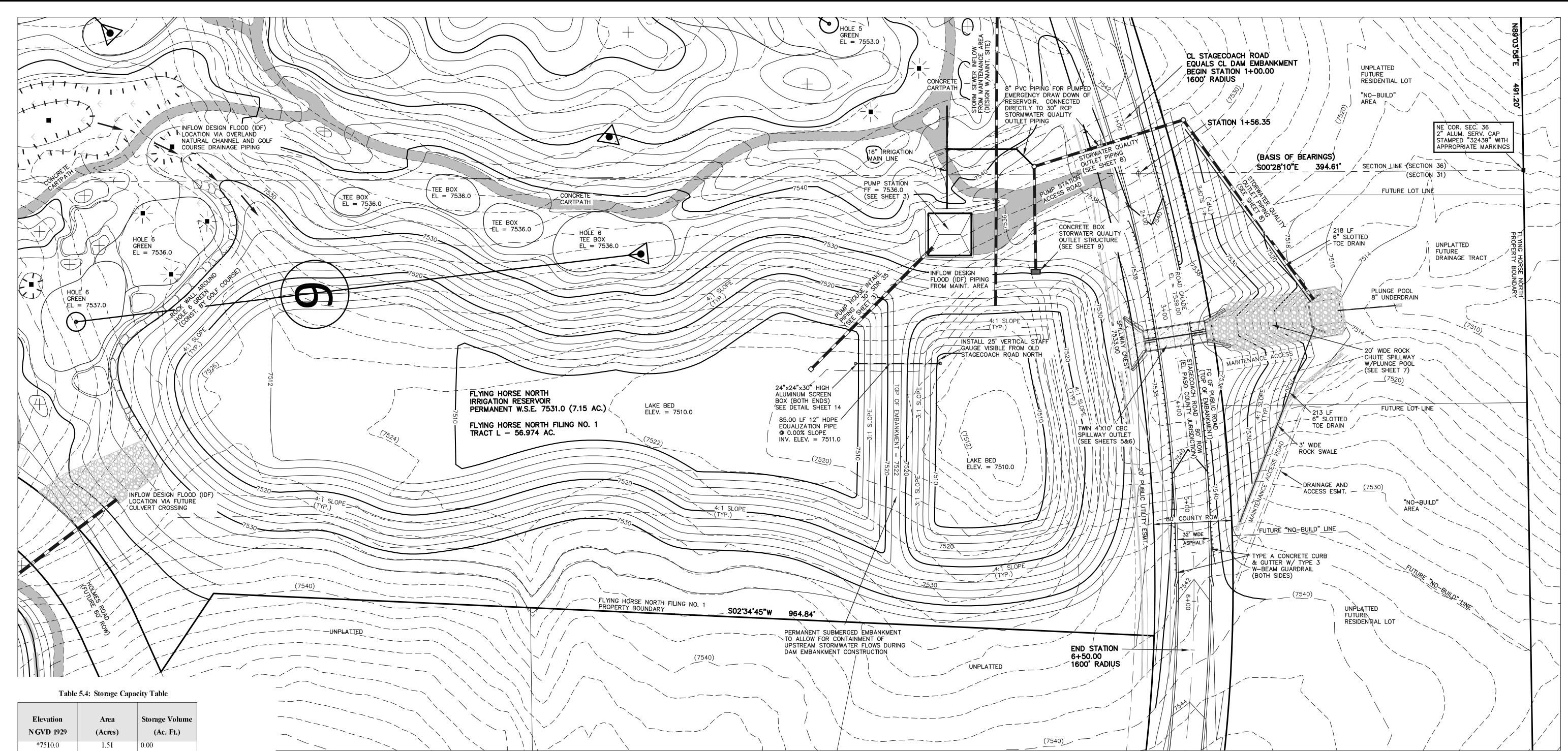
Prepared for: **PRI #2 LLC** 6385 CORPORATE DRIVE SUITE 200 COLORADO SPRINGS CO 80919 (719) 592-9333

Prepared by: CLASSIC CONSULTING ENGINEERS & SURVEYORS 619 N. CASCADE AVE SUITE 200 COLORADO SPRINGS CO 80903 (719) 785-0790

> Job no. 1096.11 PCD File No. SF-18-001



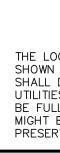
619 N. Cascade Ave, Suite 200 | Colorado Springs, CO 80903 | (719) 785-0790



Elevation N GVD 1929	Area (Acres)	Storage Volume (Ac. Ft.)
*7510.0	1.51	0.00
*7511.0	1.99	1.74
*7512.0	2.52	3.99
*7513.0	2.85	6.68
*7514.0	3.05	9.63
*7515.0	3.26	12.78
7516.0	3.48	16.15
7517.0	3.70	19.74
7518.0	3.93	23.56
7519.0	4.16	27.60
7520.0	4.40	31.88
7521.0	4.64	36.40
7522.0	4.88	41.16
7523.0	5.14	46.17
7524.0	5.36	51.42
7525.0	5.59	56.89
7526.0	5.84	62.61
7527.0	6.08	68.57
7528.0	6.33	74.77
7529.0	6.57	81.22
7530.0	6.81	87.91
7531.0	7.15	94.89
7532.0	7.52	102.22
7533.0	7.83	109.90
7534.0	8.37	118.00
7535.0	8.77	126.57
7536.0	9.17	135.53

# \*Indicates dead storage below pumping ability

	Discharge (cfs)	Discharge (cfs)	Discharge (cfs)
Elevation	(SWQ Outlet Box)	(Twin CBC Spillway)	(Total)
7531.0	0.0	0.0	0.0
7532.0	13.89	0.0	13.89
7533.0	27.77	0.0	27.77
7534.0	51.31	49.05	100.36
7535.0	69.52	138.56	208.08
7536.0	74.61	254.72	329.33
Permanent V	VSE = 7531.0		



# NOTES:

1. TOPOGRAPHIC BASE MAPPING PRODUCED FROM AERIAL PHOTOGRAPHY PROVIDED BY NORTH AMERICAN MAPPING IN 2009. HORIZONTAL CONTROL IS BASED ON LOCAL CALIBRATION TIED TO SECTION CORNER AND VERTICAL CONTROL IS BASED ON NGVD 1929 DATUM.

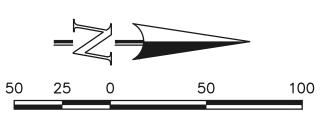
### 2. **PERMANENT WSE = 7531.0**

3. RESERVOIR LINER INSTALLED UP TO ELEVATION 7534.0

48 HOURS BEFORE YOU DIG, CALL UTILITY LOCATORS	NO.	REVISION	DATE	REVIEW:
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UTILITY NOTIFICATION CENTER OF COLORADO	2	REVISED PER COUNTY COMMENTS	7-31-18	CLASSIC CONSULTING ENGINEERS
IT'S THE LAW				
DCATIONS OF EXISTING UNDERGROUND UTILITIES ARE				
DETERMINE THE EXACT LOCATION OF ALL EXISTING ES BEFORE COMMENCING WORK, THE CONTRACTOR SHALL				
LLY RESPONSIBLE FOR ANY AND ALL DAMAGES WHICH				
BE CAUSED BY HIS FAILURE TO EXACTLY LOCATE AND RVE ANY AND ALL UNDERGROUND UTILITIES.				MARC A. WHORTON, COLORADO
		·		

# STAFF GAUGE DETAILS:

- 1. 12"X25'X1/2" PVC
- 2. LASER CUT ACRYLIC NUMBERS AND HATCH MARKS LIQUID WELDED TO PVC ON 1 FT. INCREMENTS
- 3. MOUNTED ON ALUMINUM FRAME WITH CROSS BRACKETS ANCHORED INTO SLOPE
- 4. BASE FASTENED TO 12" PIPE
- 5. ELEVATION DISPLAY RANGE: 7512-7535



SCALE: 1'' = 50'

# **FIGURE 1.3**

STATE ENGINEER'S CONSTRUCTION FILE NUMBER: C-2085



#### SECTION 4: RESERVOIR AND DAM

#### 4.1 DESIGN CRITERIA

The proposed dam for the Flying Horse North Irrigation Reservoir was designed in accordance with Rule 5 of the State of Colorado Rules and Regulations for Dam Safety and Dam Construction, dated January 2007.

#### 4.2 **RESERVOIR**

This watershed will contain development of a private golf course (currently under construction) including an outdoor golf maintenance facility, along with 2.5 ac. rural residential lot development accessed by rural County paved roadways. As such, the irrigation reservoir will also be designed with a separate stormwater detention and SWQ component per El Paso County criteria. This separate structure will be in the form of a concrete outlet box with an orifice plate and 30" RCP outlet allowing the release of the smaller storm events to meet the standards as specified per this criteria and the County's MS4 permit with the State. This SWQ release through the 30" RCP will be constructed outside of the reservoir embankment. The specific location of this reservoir is within a portion of Section 36, township 11 south, range 66 west of the sixth principal meridian, and a portion of Section 31 township 11 south, range 65 west of the sixth principal meridian, El Paso County Colorado. (See Figure 1.3)

The reservoir has a surface area at its permanent WSE (Elev. 7531.0) of 7.0 acres with a storage volume of 94.9 acre feet. The maximum depth at this elevation is 21 feet with the lake bed at 7510. The reservoir will have a liner constructed of a flexible membrane. This liner will be laid up to a maximum elevation of 7534. The reservoir is supplied by water from a well located on the Clubhouse site within the development approximately 1/4 mile west of the reservoir. The level in the reservoir is controlled by the two outlet structures. The Detention/SWQ structure will facilitate the State required 72 hr. drain time for the smaller stormwater events and help maintain the permanent water level while the twin box culvert spillway will allow for the County required 100 yr. detention release of the major stormwater events. The total storage capacity table is found in Section 5, Table 5.4.

#### 4.3 DAM EMBANKMENT

The dam embankment for this reservoir will be constructed within the County owned and maintained Old Stagecoach Road (80' ROW - Collector). The subdivision Improvement Agreement (SIA) as required by El



Paso County for this subdivision, will be recorded along with the Final Plat and specify ownership and maintenance responsibilities related to the embankment and associated drainage structures. The crest of the embankment, which will be the finished grade of asphalt for the roadway is at elevation 7539.0 at the lowest point. The regulatory height from the twin box culvert emergency spillway invert to the native channel grade equals 23.0°. The length of the embankment measured from the toe of slopes on each side is approximately 450°. Both the upstream and downstream slopes of the embankment will be constructed at no greater than a 4:1 slope. The roadway will have a typical 2% crown with an asphalt width of 32.0° with El Paso County Type A concrete curb and gutter on both sides and then 6:1 maximum to edge of ROW with a County required clear zone of 14.0°. The twin box culvert emergency spillway structure is outside this clear zone. El Paso County will also require CDOT Type 3 W-Beam guardrail along both sides of the embankment. The embankment itself will be constructed of local material found on-site and tested by the Geotech. According to the State of Colorado Rules and Regulations for Dam Safety and Dam Construction, Rule 4.2.5.4, this facility is considered a "Small Jurisdictional Dam" given the jurisdictional height greater than 20 feet but less than 50 feet and a capacity greater than 100 acre-feet.

#### 4.4 SPILLWAY AND OUTLET WORKS

This facility will be designed with two separate outlet structures. One will facilitate the State/County required detention/SWQ component of the facility while the other will allow for the 100 yr. stormwater event and emergency flow situations. A low level outlet will be built into the pump station design allowing for an emergency drawdown of the reservoir to be with connection to the SWQ outlet piping.

#### Detention / SWQ Outlet

Per the County's MS4 permit with the State, this development is required to provide detention and stormwater quality within this reservoir facility. The design for this is being handled by a separate concrete outlet box constructed outside the formal dam embankment. This structure is a 4'x8' concrete box with a steel flow control plate and protective well screen located on the front. The control plate is designed with three rectangular holes to facilitate the State required drain times. The first hole is located at elevation 7531.0 with the top of box at elevation 7533.0. The top of box will be constructed with a grate to allow flows to enter the box as well. A 30" RCP outlet pipe will allow for the release of all the flows entering the box structure. The design of this structure meets all State and County requirements for both EURV and



WQCV. The 30" RCP outlet piping will be routed around the dam embankment and into the rock chute and plunge pool at the base of the emergency spillway.

#### Spillway Outlet

Given that the embankment for this reservoir will be a County roadway, the conventional emergency spillway channel design at the crest of the embankment was not appropriate. But rather a concrete box culvert spillway design under the roadway to allow for both the major stormwater events and emergency release has been employed. Twin 4'x10' concrete box culverts (CBC) will facilitate the required releases. The crest of the spillway will be constructed at elevation 7533.0 where the release will then travel under the roadway and into a 20' wide rock chute. The rock chute will have a 4:1 slope with 3:1 side slopes and a total drop of 18.0' into a 2.0' deep plunge pool. The following roughness coefficients were used: CBCs 0.013 and Rock Chute 0.035. The rip-rap thickness will be 56'' with a gradation specified by the Geotech. (See Design Plans) The spillway CBCs and Rock Chute have been designed to accommodate both the 100 yr. release of 182 cfs with a headwater depth ratio (Hw/D) of 0.54 and the total basin inflow of 609 cfs with a (Hw/D) of 1.31. This design is within the maximum County criteria of (Hw/D) of 1.40. The freeboard design is as follows: 100 Yr. = 4.39' and 500 Yr. = 3.03'. The velocity at inlet of chute = 15.6 fps and velocity at outlet of chute = 6.99 fps, both at normal depth. 1.76' of Freeboard is included in chute design.

### Low Level Outlet

This reservoir will not be designed with a formal low level outlet given the nature of the facility and the ability for the pump station to facilitate the draining of the reservoir for embankment inspection or emergency purposes. Thus, directly off of the 16" irrigation main just outside the pump station, a 16"x8" tee with gate valves and a 8" drain line will be installed to allow for the pumped release and draining of the reservoir. This 8" drain line will then connect directly to the 30" RCP storm system via a Type II concrete storm manhole constructed as a part of the release of the Detention/SWQ component as required by El Paso County. This 30" storm system then daylights into the base of the rock chute and plunge pool on the backside of the embankment. The 8" drain line @ 110 psi is expected to release 800-1200 GPM. However, using the maximum pump station capacity of 2,250 GPM while opening system drain valves and irrigation heads, the drain time is as follows: As mentioned earlier, the pumps will allow for release down to an elevation of 7515.67. Based on the permanent WSE of 7531, this equates to a total of approximately 26 million gallons (MG) to be drained. The total drain time is estimated at approximately 8 days.



**Hazard Classification**" as described in section 5.6 of this report the Inflow Design Flood Requirements (IDF) as found in Rule 5.9.1, Table 5.1 utilize the (NOAA 14 – 24 Hr. duration) 100 Yr. storm event. The UD-Detention v3.07 spreadsheet (Per Urban Drainage Vol. 3) will also be utilized in the final design of the Detention and SWQ aspects of this facility. This spreadsheet uses 1 Hr. precipitation depths. See Table 5.1 for precipitation depth comparison. Please note that the higher precipitation amounts have been used for each return period.

Return Period	1-Hr. Depth (City/County)	1-Hr. Depth (NOAA 14)	24-Hr. Depth (City/County)	24-Hr. Depth (NOAA 14)
2	1.19	0.92	2.10	1.93
5	1.50	1.20	2.70	2.44
50	2.25	2.15	4.20	4.33
100	2.52	2.49	4.60	5.04

Table 5.1: Precipitation Depth Comparison

#### 5.2 WATER RIGHTS

Based on the water decree filed October 6, 2017 (See Appendix), PRI #2, LLC has the water rights to pump and store in the on-site Flying Horse North reservoir. PRI #2, LLC has a lease from the State Land Board for the following water rights: 515 AF in the Dawson, 577 AF in the Denver, 239 AF in the Arapahoe and 182 AF in the Laramie Fox Hills. The Arapahoe and Laramie Fox Hills are both deemed non-tributary reservoirs. The Flying Horse North Golf Course will take an average of 200 AF per year from their Arapahoe well that will be pumped into the reservoir. Evaporative loss is not an issue when pumping from a non-tributary source. Upon termination of the State Land Board Lease in 2048, all water rights revert automatically back to PRI #2, LLC who will own them in perpetuity.



#### 5.3 WATERSHED CHARACTERISTICS

The watershed of the irrigation reservoir includes a total area of 366.8 acres within the East Cherry Creek drainage basin and just north of the Palmer Divide. A portion of this area is outside the Flying Horse North development as shown in basins OS-12, OS-13 and OS-14. These basins are both currently undeveloped and developed as County zoned RR-5 (5 ac. rural residential). All the on-site basins are zoned PUD for either 2.5 ac. rural residential or golf course/open space. (See Tables 5.2 and 5.3 for sub-basin CN values and associated Tc times) Nearly the entire watershed is outside of the black forest tree line and mainly consists of prairie grasses with grades ranging from 2%-20% with three major natural ravines that drain in a northwesterly direction directly towards the planned irrigation reservoir. The golf course layout aides in the natural conveyance of the majority of the stormwater flows to the reservoir. The storage capacity table for the reservoir is listed in Table 5.4.

		Table	5.2: Sub-basin	n CN Values		
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	01					
	CN	VALUES -	DEVELOP	ED COND	TIONS	
BASIN	BASIN	GOLF C	OURSE (B)	2 AC. RES	SIDENTIAL (B)	COMPOSITE
(label)	AREA					CN
	(Ac)	CN	AREA	CN	AREA	
			(Ac.)		(Ac.)	
CC-1	22.3	61	0.0	65	22.3	65.0
CC-2	36.4	61	0.0	65	36.4	65.0
CC-3	51.9	61	19.1	65	32.8	63.5
CC-4A	108.2	61	63.2	65	45.0	62.7
CC-4B	17.0	61	5.5	65	11.5	63.7
OS-12	67.7	61	0.0	65	67.7	65.0
OS-13	36.9	61	0.0	65	36.9	65.0
05-15		61	0.0	65	26.4	65.0



			TIMEC	OF CONC	ENTRATIO	ON DEVE	LOPED			
	COMPOSITE		OVERLAND		STREET / C	HANNEL FL	OW(DCM Vo	l. 1 Fig. 6-25)	Tc	Тс
BASIN	Cn	Length	Height	Тс	Length	Slope	Velocity	Tc	TOTAL	LAG (0.6tc)
		(ft)	(ft)	(hr)	(ft)	(%)	(fps)	(hr)	(hr)	(hr)
CC-1	65.0	300	10	0.40	900	2.0%	1.8	0.14	0.53	0.32
CC-2	65.0	300	10	0.40	1700	2.0%	1.8	0.26	0.66	0.39
CC-3	63.5	300	14	0.35	900	2.5%	2.4	0.10	0.45	0.27
CC-4A	62.7	300	14	0.35	2900	2.0%	2.1	0.38	0.73	0.44
CC-4B	63.7	300	12	0.37	900	3.0%	2.5	0.10	0.47	0.28
OS-12	65.0	300	14	0.35	1500	3.0%	2.5	0.17	0.51	0.31
OS-13	65.0	300	16	0.33	900	3.0%	2.5	0.10	0.43	0.26
OS-14	65.0	300	14	0.35	600	3.5%	2.7	0.06	0.41	0.24

Table 5.3: Sub-basin Time of Concentration

 Table 5.4: Storage Capacity Table

Elevation	Area	Storage Volume
NGVD 1929	(Acres)	(Ac. Ft.)
*7510.0	1.51	0.00
*7511.0	1.99	1.74
*7512.0	2.52	3.99
*7513.0	2.85	6.68
*7514.0	3.05	9.63
*7515.0	3.26	12.78
7516.0	3.48	16.15
7517.0	3.70	19.74
7518.0	3.93	23.56
7519.0	4.16	27.60
7520.0	4.40	31.88
7521.0	4.64	36.40
7522.0	4.88	41.16



7523.0	5.14	46.17
7524.0	5.36	51.42
7525.0	5.59	56.89
7526.0	5.84	62.61
7527.0	6.08	68.57
7528.0	6.33	74.77
7529.0	6.57	81.22
7530.0	6.81	87.91
7531.0	7.15	94.89
7532.0	7.52	102.22
7533.0	7.83	109.90
7534.0	8.37	118.00
7535.0	8.77	126.57
7536.0	9.17	135.53

\*Indicates dead storage below pumping ability

#### 5.4 HYDROLOGIC MODEL

The PondPack model produced peak discharges for the 2-yr, 5-yr, 50-yr and 100-yr storm events assuming a permanent pool elevation of 7531.0. Reference Appendix B for specific hydrologic model results. Table 5.5 below shows the results of these storm events upon the irrigation reservoir.

			Total
Storm Event	Peak Inflow	Max. WSE	Discharge
	(cfs)	(ft.)	(cfs)
2-yr (City/County)	48	7531.40	6
5-yr (City/County)	119	7531.87	12
50-yr (NOAA 14)	431	7533.58	64
100-yr (NOAA 14)	609	7534.23	124

Table 5.5: Inflow Design Flood (IDF) Summary Table



#### 5.5 HYDRAULIC MODEL

Both the SWQ Outlet and the CBC Spillway were modeled using both PondPack (24-hr. precipitation) and the Urban Drainage UD Detention Spreadsheet (1-hr precipitation) as required by County design criteria. Table 5.6 below shows the results of the PondPack model. Reference Appendix B for the UD Detention – Retention Pond Spreadsheet results. As this facility is required to meet both detention and SWQ criteria, the following is applicable to these design components:

Required WQCV =	1.36 ac-ft.	Provided WQCV =	15.01 ac-ft.
Required EURV =	2.83 ac-ft.	Provided EURV =	15.01 ac-ft.
Required 100-yr. =	12.42 ac-ft.	Provided 100-yr =	27.35 ac-ft.

	Discharge (cfs)	Discharge (cfs)	Discharge (cfs)
Elevation	(SWQ Outlet Box)	(Twin CBC Spillway)	(Total)
7531.0	0.0	0.0	0.0
7532.0	13.89	0.0	13.89
7533.0	27.77	0.0	27.77
7534.0	51.31	49.05	100.36
7535.0	69.52	138.56	208.08
7536.0	74.61	254.72	329.33

 Table 5.6:
 Reservoir Discharge Table

Permanent WSE = 7531.0

Top of SWQ Outlet box = 7533.0

Spillway elevation = 7533.0

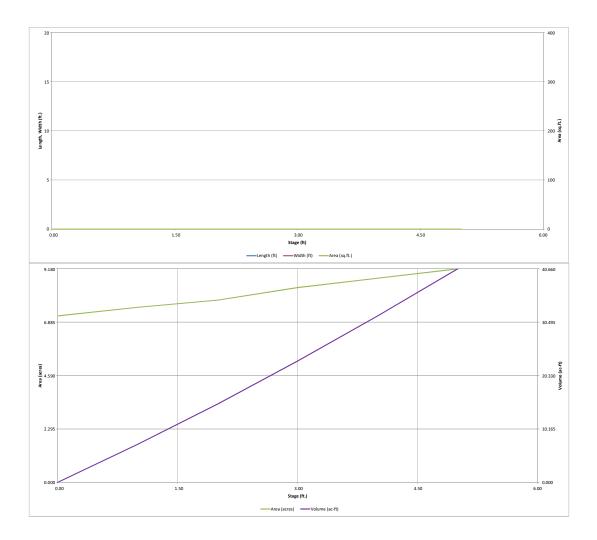
The twin 4'x10' CBC Spillway design has the following results:

100-yr storm release = $182  cfs$	Hw/D = 0.54
Emergency release – Max. basin IDF = $609 \text{ cfs}$	Hw/D = 1.31
County Criteria (max.)	Hw/D = 1.40

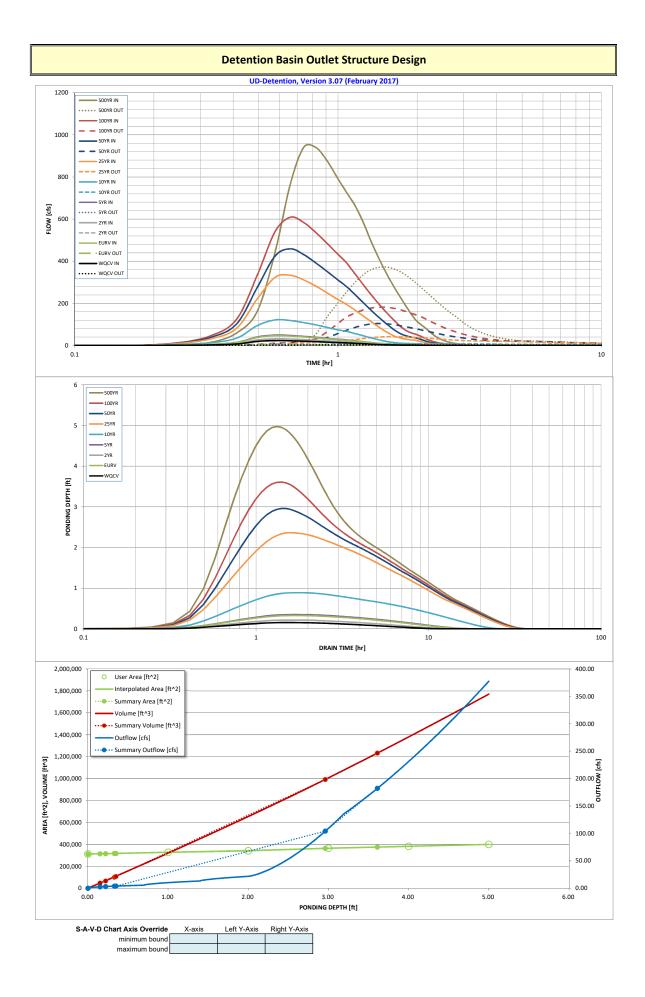


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UD-Detention, Version 3.07 (February 2017)



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-	Flying Horse North Golf Course Irrigat		- 13)						
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			Zone 1 (WQCV)	0.20	1.395	Orifice Plate			
ZONE 1 AND 2	100-YEA	R	Zone 2 (EURV)	0.40	1.424	Orifice Plate			
PERMANENT ORIFICES		tention Dand)	:one 3 (100-year)	1.67	9.598	Weir&Pipe (Restrict)			
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ser Input: Orifice Plate with one or more orifices		r (typically used to d	rain WQCV and/or EL	JRV in a sedimentati	ion BMP)	Calcu	lated Parameters for	1	
Invert of Lowest Orifice =	0.00		bottom at Stage = 0 ft			rifice Area per Row =	1.354E+00	ft <sup>2</sup>	
Depth at top of Zone using Orifice Plate = Orifice Plate: Orifice Vertical Spacing =	2.00	ft (relative to basin I inches	bottom at Stage = 0 ft	t)		lliptical Half-Width = ptical Slot Centroid =	N/A N/A	feet feet	
Orifice Plate: Orifice Area per Row =	195.00	sq. inches (use recta	ingular openings)		EIII	Elliptical Slot Area =	N/A N/A	ft <sup>2</sup>	
		1	0.00					]	
er Input: Stage and Total Area of Each Orifice	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)	]
Stage of Orifice Centroid (ft)		0.70	1.40						
Orifice Area (sq. inches)	195.00	195.00	195.00						
	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)	1
Stage of Orifice Centroid (ft)									1
Orifice Area (sq. inches)									
Developments Martinel 6-10. Com	ular or Peatrice 1					6-1- 1-7 ·	Dorometers for M	ical Orifica	
User Input: Vertical Orifice (Circ	Not Selected	Not Selected	1			Calculated	Parameters for Vert Not Selected	Not Selected	1
Invert of Vertical Orifice =	N/A	N/A	ft (relative to basin b	oottom at Stage = 0 f	t) V	ertical Orifice Area =	N/A	N/A	ft <sup>2</sup>
Depth at top of Zone using Vertical Orifice =	N/A	N/A	ft (relative to basin b	oottom at Stage = 0 f	t) Vertio	al Orifice Centroid =	N/A	N/A	feet
Vertical Orifice Diameter =	N/A	N/A	inches						
User Input: Overflow Weir (Dropbox) and G	rate (Flat or Sloped)					Calculated	Parameters for Ove	rflow Weir	
	Zone 3 Weir	Not Selected	]				Zone 3 Weir	Not Selected	]
Overflow Weir Front Edge Height, Ho =	2.00	N/A	ft (relative to basin bo	ttom at Stage = 0 ft)		ate Upper Edge, H <sub>t</sub> =	3.00	N/A	feet
Overflow Weir Front Edge Length =	8.00	N/A	feet			Weir Slope Length =	4.12	N/A	feet
Overflow Weir Slope = Horiz. Length of Weir Sides =	4.00	N/A N/A	H:V (enter zero for fl feet	al grate)		100-yr Orifice Area = en Area w/o Debris =	5.04 24.74	N/A N/A	should be $\geq 4$ ft <sup>2</sup>
Overflow Grate Open Area % =	75%	N/A	%, grate open area/t	total area	-	pen Area w/ Debris =	12.37	N/A	ft <sup>2</sup>
Debris Clogging % =	50%	N/A	%						-
ser Input: Outlet Pipe w/ Flow Restriction Plate (C	Zone 3 Restrictor	Not Selected	ngular Orifice)		C C	alculated Parameter	s for Outlet Pipe w/ Zone 3 Restrictor	Flow Restriction Pla Not Selected	lte T
Depth to Invert of Outlet Pipe =	4.00	N/A	ft (distance below bas	in bottom at Stage = 0	ft)	Outlet Orifice Area =	4.91	N/A	ft <sup>2</sup>
Outlet Pipe Diameter =		N/A	inches			let Orifice Centroid =	1.25	N/A	feet
Restrictor Plate Height Above Pipe Invert =	30.00		inches	Half-0	Central Angle of Rest	rictor Plate on Pipe =	3.14	N/A	radians
User Input: Emergency Spillway (Rectang Spillway Invert Stage=		ft (relative to basin l	bottom at Stage = 0 ft	-)	Spillway	Design Flow Depth=	ted Parameters for S 4.13	feet	
Spillway Crest Length =	20.00	feet		-)		t Top of Freeboard =	7.13	feet	
Spillway End Slopes =	0.00	H:V			Basin Area a	t Top of Freeboard =	9.17	acres	
	1.00	feet							
Freeboard above Max Water Surface =	1.00								
Freeboard above Max Water Surface = Routed Hydrograph Results								100 Vees	500 Year
Routed Hydrograph Results Design Storm Return Period =	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	
<b>Routed Hydrograph Results</b> Design Storm Return Period = One-Hour Rainfall Depth (in) =	<u>WQCV</u> 0.53	1.07	1.19	1.50	1.75	2.00	2.25	2.52	3.39
Routed Hydrograph Results Design Storm Return Period =	WQCV								3.39 68.375
Routed Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = Calculated Runoff Volume (acre-ft) = OPTIONAL Override Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) =	WQCV 0.53 1.395 1.395	1.07 2.819 2.819	1.19 1.903 1.902	1.50 3.006 3.006	1.75 7.525 7.522	2.00 21.442 21.445	2.25 30.109 30.113	2.52 41.427 41.428	68.375 68.385
Routed Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = Calculated Runoff Volume (acre-ft) = OPTIONAL Override Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = Predevelopment Unit Peak Flow, q (cfs/acre) =	WQCV 0.53 1.395 1.395 0.00	1.07 2.819 2.819 0.00	1.19 1.903 1.902 0.01	1.50 3.006 3.006 0.02	1.75 7.525 7.522 0.20	2.00 21.442 21.445 0.67	2.25 30.109 30.113 0.93	2.52 41.427 41.428 1.25	68.375 68.385 2.00
Routed Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = Calculated Runoff Volume (acre-ft) = OPTIONAL Override Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) =	WQCV 0.53 1.395 1.395	1.07 2.819 2.819	1.19 1.903 1.902	1.50 3.006 3.006	1.75 7.525 7.522	2.00 21.442 21.445	2.25 30.109 30.113	2.52 41.427 41.428	68.375 68.385
Routed Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = Calculated Runoff Volume (acre-ft) = OPTIONAL Override Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = Predevelopment Unit Peak Riow, q (cfs/acre) = Predevelopment Peak Q (cfs) = Peak Inflow Q (cfs) = Peak Outflow Q (cfs) =	WQCV 0.53 1.395 1.395 0.00 0.0 23.2 2.6	1.07 2.819 2.819 0.00 0.0 46.4 3.7	1.19 1.903 0.01 4.5 31.5 3.0	1.50 3.006 0.02 7.8 49.5 3.9	1.75 7.525 7.522 0.20 75.1 121.4 9.0	2.00 21.442 21.445 0.67 247.4 333.1 41.5	2.25 30.109 	2.52 41.427 41.428 1.25 460.1 608.8 182.0	68.375 68.385 2.00 734.0 941.9 373.2
Routed Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = Calculated Runoff Volume (acre-ft) = OPTIONAL Override Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = Predevelopment Unit Peak Row, q (cfs/acre) = Predevelopment Peak Q (cfs) = Peak Inflow Q (cfs) = Peak Outflow Q (cfs) = Ratio Peak Outflow to Predevelopment Q =	WQCV 0.53 1.395 0.00 23.2 2.6 N/A	1.07 2.819 2.819 0.00 0.0 46.4 3.7 N/A	1.19 1.903 0.01 4.5 31.5 3.0 N/A	1.50 3.006 3.006 0.02 7.8 49.5 3.9 0.5	1.75 7.525 7.522 0.20 75.1 121.4 9.0 0.1	2.00 21.442 21.445 0.67 247.4 333.1 41.5 0.2	2.25 30.109 30.113 0.93 342.3 458.5 103.9 0.3	2.52 41.427 41.428 1.25 460.1 608.8 182.0 0.4	68.375 68.385 2.00 734.0 941.9 373.2 0.5
Routed Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = Calculated Runoff Volume (acre-ft) = OPTIONAL Override Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = Predevelopment Unit Peak Flow, q (cfs/acre) = Predevelopment Peak Q (cfs) = Peak Inflow Q (cfs) = Peak Outflow Q (cfs) =	WQCV 0.53 1.395 1.395 0.00 0.0 23.2 2.6	1.07 2.819 2.819 0.00 0.0 46.4 3.7	1.19 1.903 0.01 4.5 31.5 3.0	1.50 3.006 3.006 0.02 7.8 49.5 3.9	1.75 7.525 7.522 0.20 75.1 121.4 9.0	2.00 21.442 21.445 0.67 247.4 333.1 41.5	2.25 30.109 	2.52 41.427 41.428 1.25 460.1 608.8 182.0	68.375 68.385 2.00 734.0 941.9 373.2 0.5
Routed Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = Calculated Runoff Volume (acre-ft) = OPTIONAL Override Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = Predevelopment Unit Peak Flow, q (cfs/acre) = Predevelopment Peak (cfs/s) Peak Inflow Q (cfs) = Peak Outflow Q (cfs) = Ratio Peak Outflow to Predevelopment Q = Structure Controlling Flow = Max Velocity through Grate 1 (fps) = Max Velocity through Grate 2 (fps) =	WQCV 0.53 1.395 0.00 0.0 23.2 2.6 N/A Plate N/A N/A	1.07 2.819 2.819 0.00 46.4 3.7 N/A Plate N/A N/A	1.19 1.903 0.01 4.5 31.5 3.0 N/A Plate N/A N/A	1.50 3.006 0.02 7.8 49.5 3.9 0.5 Plate N/A N/A	1.75 7.525 0.20 75.1 121.4 9.0 0.1 Plate N/A N/A	2.00 21.442 21.445 0.67 247.4 333.1 41.5 0.2 Spillway 0.1 N/A	2.25 30.109 30.113 0.93 342.3 458.5 103.9 0.3 Spillway 0.7 N/A	2.52 41.427 41.428 1.25 460.1 608.8 182.0 0.4 Spillway 1.1 N/A	68.375 68.385 2.00 734.0 941.9 373.2 0.5 Spillway 1.0 N/A
Routed Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = Calculated Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = Predevelopment Unit Peak Flow, q (cfs/acre) = Predevelopment Peak Q (cfs) = Peak Inflow Q (cfs) = Peak Outflow Q (cfs) = Ratio Peak Outflow to Predevelopment Q = Structure Controlling Flow = Max Velocity through Grate 1 (fps) = Max Velocity through Grate 2 (fps) = Time to Drain 97% of Inflow Volume (hours) =	WQCV           0.53           1.395           0.00           0.01           23.2           2.6           N/A           Plate           N/A           11	1.07 2.819 0.00 0.0 46.4 3.7 N/A Plate N/A N/A 15	1.19 1.903 0.01 4.5 31.5 3.0 N/A Plate N/A N/A N/A 12	1.50 3.006 0.02 7.8 49.5 3.9 0.5 Plate N/A N/A 15	1.75 7.525 7.522 0.20 75.1 121.4 9.0 0.1 Plate N/A N/A 22	2.00 21.442 21.445 0.67 247.4 333.1 41.5 0.2 Spillway 0.1 N/A 27	2.25 30.109 30.113 0.93 342.3 458.5 103.9 0.3 Spillway 0.7 N/A 27	2.52 41.427 41.428 1.25 460.1 608.8 182.0 0.4 Spillway 1.1 N/A 25	68.375 68.385 2.00 734.0 941.9 373.2 0.5 Spillway 1.0 N/A 23
Routed Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = Calculated Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = Predevelopment Unit Peak Flow, q (cfs/acre) = Predevelopment Peak Q (cfs) = Peak Inflow Q (cfs) = Peak Outflow Q (cfs) = Ratio Peak Outflow to Predevelopment Q = Structure Controlling Flow = Max Velocity through Grate 1 (fps) = Max Velocity through Grate 2 (fps) = Time to Drain 97% of Inflow Volume (hours) = Time to Drain 99% of Inflow Volume (hours) =	WQCV           0.53           1.395           0.00           0.01           23.2           2.6           N/A           Plate           N/A           11           12	1.07 2.819 0.00 0.0 46.4 3.7 N/A Plate N/A N/A 15 16	1.19 1.903 0.01 4.5 31.5 3.0 N/A Plate N/A N/A 12 14	1.50 3.006 0.02 7.8 49.5 3.9 0.5 Plate N/A N/A 15 16	1.75 7.525 0.20 75.1 121.4 9.0 0.1 Plate N/A N/A 22 24	2.00 21.442 21.445 0.67 247.4 333.1 41.5 0.2 Spillway 0.1 N/A 27 31	2.25 30.109 30.113 0.93 342.3 4458.5 103.9 0.3 Spillway 0.7 N/A 27 31	2.52 41.427 41.428 1.25 460.1 608.8 182.0 0.4 Spillway 1.1 N/A 25 30	68.375 68.385 2.00 734.0 941.9 373.2 0.5 Spillway 1.0 N/A 23 29
Routed Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = Calculated Runoff Volume (acre-ft) = OPTIONAL Override Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = Predevelopment Unit Peak Riow, q (cfs/acre) = Predevelopment Peak Q (cfs) = Peak Inflow Q (cfs) = Peak Nutflow Q (cfs) = Ratio Peak Outflow to Predevelopment Q = Structure Controlling Flow = Max Velocity through Grate 1 (fps) = Max Velocity through Grate 2 (fps) = Time to Drain 97% of Inflow Volume (hours) =	WQCV           0.53           1.395           0.00           0.01           23.2           2.6           N/A           Plate           N/A           11	1.07 2.819 0.00 0.0 46.4 3.7 N/A Plate N/A N/A 15	1.19 1.903 0.01 4.5 31.5 3.0 N/A Plate N/A N/A N/A 12	1.50 3.006 0.02 7.8 49.5 3.9 0.5 Plate N/A N/A 15	1.75 7.525 7.522 0.20 75.1 121.4 9.0 0.1 Plate N/A N/A 22	2.00 21.442 21.445 0.67 247.4 333.1 41.5 0.2 Spillway 0.1 N/A 27	2.25 30.109 30.113 0.93 342.3 458.5 103.9 0.3 Spillway 0.7 N/A 27	2.52 41.427 41.428 1.25 460.1 608.8 182.0 0.4 Spillway 1.1 N/A 25	68.375 68.385 2.00 734.0 941.9 373.2 0.5 Spillway 1.0 N/A 23



#### **Detention Basin Outlet Structure Design**

Outflow Hydrograph Workbook Filename:

	Storm Inflow H				n 3.07 (Februa					
ſ		WORKBOOK	WORKBOOK	WORKBOOK	WORKBOOK	WORKBOOK		ed in a separate	-	WORKBOOK
Time Interval	SOURCE						WORKBOOK	WORKBOOK	WORKBOOK	WORKBOOK
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
4.95 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:04:57	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Hydrograph	0:09:54	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Constant 1.010	0:14:51 0:19:48	2.74	1.97 5.42	1.36 3.70	2.10	4.69 13.49	9.77 31.71	11.39 39.07	12.89 46.76	15.10 59.45
1.010	0:24:45	7.04	5.42 13.91	9.51	14.80	34.64	82.12	102.73	124.75	164.90
	0:29:42	19.32	38.17	26.10	40.61	94.81	223.20	277.98	336.63	444.01
	0:34:39	23.19	46.42	31.50	49.46	121.39	323.47	425.12	541.27	768.07
	0:39:36	22.19	44.52	30.16	47.44	118.28	333.14	458.54	608.77	941.94
	0:44:33	20.20	40.51	27.45	43.17	108.29	310.79	431.04	582.87	939.56
	0:49:30	18.10	36.44	24.64	38.84	97.66	281.42	390.98	535.69	878.35
	0:54:27	15.70	31.77	21.42	33.89	85.81	250.82	352.31	485.61	800.60
	0:59:24	13.65	27.68	18.60	29.53	75.09	221.36	315.01	438.24	731.15
	1:04:21	12.38	25.04	16.87	26.71	67.46	196.13	281.72	395.12	668.65
	1:09:18	10.29	20.92	14.06 11.59	22.33	56.98	169.57	244.05	343.20	594.66
	1:14:15	8.46 6.60	17.30 13.63	9.08	18.47 14.56	47.35 37.87	142.96 117.65	207.70 173.58	294.13 249.28	509.61 435.39
	1:24:09	4.99	10.46	6.92	14.56	29.48	94.26	1/5.58	249.28	372.25
	1:29:06	3.64	7.75	5.08	8.30	22.24	74.08	115.60	173.54	316.50
	1:34:03	2.78	5.85	3.86	6.26	16.51	56.37	91.58	142.20	268.83
	1:39:00	2.28	4.73	3.14	5.06	13.16	42.77	70.68	113.81	225.24
	1:43:57	1.92	3.99	2.65	4.26	11.04	34.92	55.08	89.03	185.28
	1:48:54	1.68	3.48	2.32	3.72	9.57	29.75	45.79	70.94	149.07
	1:53:51	1.51	3.12	2.08	3.33	8.53	26.20	39.69	59.85	118.87
	1:58:48	1.39	2.86	1.91	3.05	7.79	23.63	35.39	52.61	99.74
	2:03:45	1.02	2.12	1.41	2.26	5.92	18.97	28.99	43.64	83.33
	2:13:39	0.75	1.54 1.13	1.03 0.76	1.64	4.27 3.17	13.83 10.12	21.64 15.73	33.32 24.54	65.70 49.44
	2:18:36	0.41	0.84	0.56	0.90	2.35	7.55	11.63	18.13	37.08
	2:23:33	0.29	0.61	0.41	0.66	1.73	5.63	8.83	13.58	27.60
	2:28:30	0.21	0.44	0.29	0.47	1.25	4.16	6.61	10.30	20.70
	2:33:27	0.15	0.32	0.21	0.34	0.91	3.03	4.92	7.75	15.78
	2:38:24	0.10	0.22	0.14	0.24	0.64	2.25	3.67	5.84	11.98
	2:43:21	0.06	0.14	0.09	0.15	0.42	1.58	2.71	4.47	9.20
	2:48:18	0.03	0.08	0.05	0.08	0.25	1.03	1.90	3.30	7.18
	2:53:15	0.01	0.03	0.02	0.04	0.12	0.60	1.23	2.30	5.41
	2:58:12 3:03:09	0.00	0.01	0.00	0.01	0.04	0.28	0.71	1.49	3.89
	3:08:06	0.00	0.00	0.00	0.00	0.00	0.08	0.33	0.85	2.62
	3:13:03	0.00	0.00	0.00	0.00	0.00	0.00	0.09	0.39	0.83
	3:18:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.30
	3:22:57	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.03
	3:27:54	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:32:51	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:37:48	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:42:45	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:47:42	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:52:39 3:57:36	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:02:33	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:07:30	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:12:27	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ĺ	4:17:24	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:22:21	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:27:18 4:32:15	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:37:12	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:42:09	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:47:06	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:52:03 4:57:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:01:57	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:06:54	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ļ	5:11:51	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:16:48	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:21:45 5:26:42	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:26:42	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:36:36	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
[	5:41:33	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:46:30	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:51:27 5:56:24	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
l	5:50:24	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

#### **Detention Basin Outlet Structure Design**

UD-Detention, Version 3.07 (February 2017)

Summary Stage-Area-Volume-Discharge Relationships

The user can create a summary S-A-V-D by entering the desired stage increments and the remainder of the table will populate automatically.

The user should graphically compare the summary S-A-V-D table to the full S-A-V-D table in the chart to confirm it captures all key transition points.

Stage - Storage Description	Stage [ft]	Area [ft^2]	[acres]	[ft^3]	[ac-ft]	Outflow [cfs]	
PERMANENT WSE	0.00	311,545	7.152	0	0.000	0.00	For best results, include
WQCV	0.15	313,949	7.207	46,912	1.077	2.53	stages of all grade slope
2 YR. WSE	0.13	314,910	7.229	65,778	1.510	2.99	changes (e.g. ISV and Fl
EURV	0.33	316,673	7.270	100,515	2.308	3.69	from the S-A-V table on
5 YR. WSE	0.35	316,994	7.277	106,852	2.453	3.80	Sheet 'Basin'.
50 YR. WSE	2.96	363,656	8.348	992,161	22.777	104.11	Also include the inverts
100 YR. WSE	3.61	375,226	8.614	1,232,372	28.291	182.18	outlets (e.g. vertical ori
							overflow grate, and spil
							where applicable).
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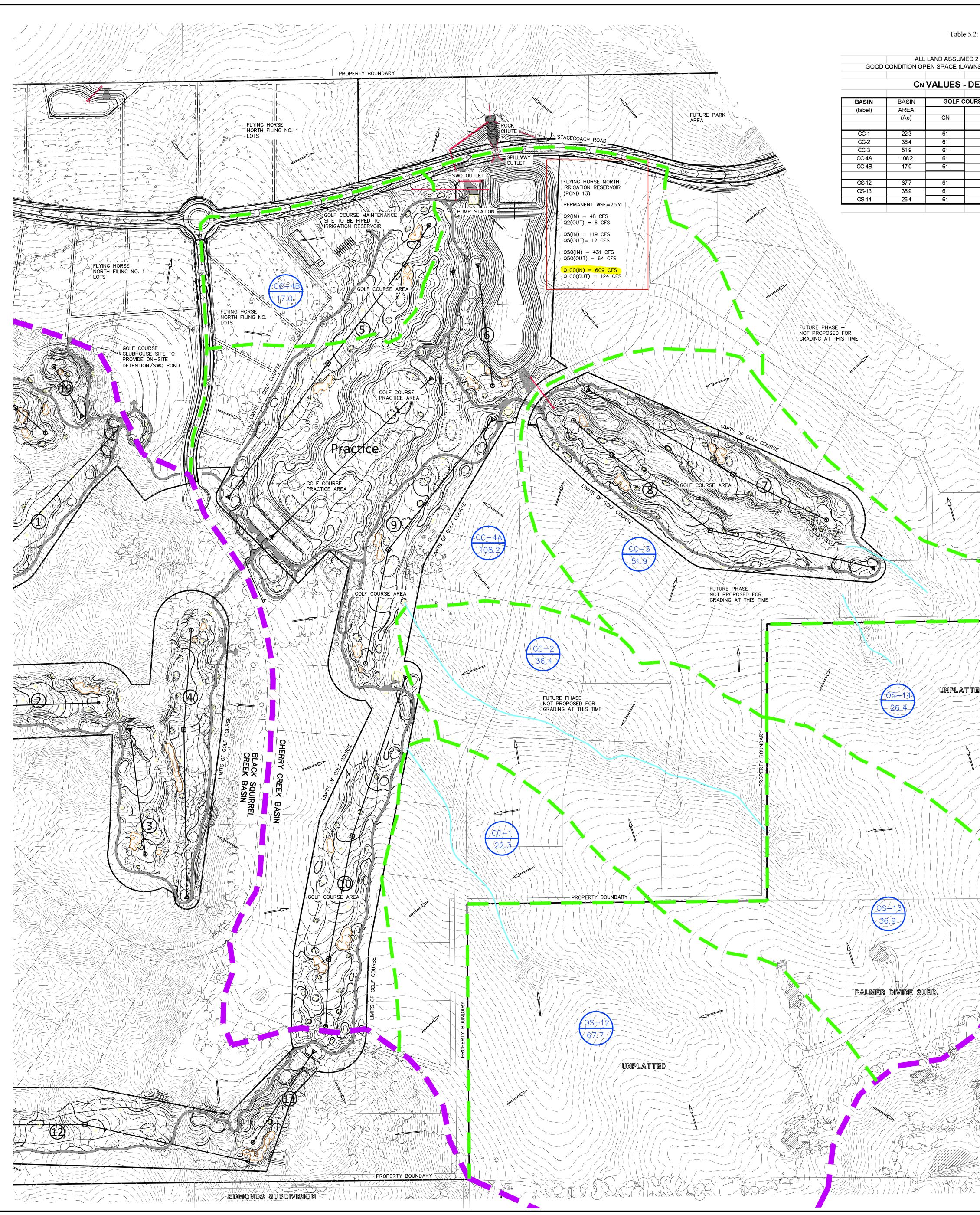


Table 5.2: Sub-basin CN Values

## ALL LAND ASSUMED 2 ACRE RESIDENTIAL LOTS OR GOOD CONDITION OPEN SPACE (LAWNS, PARKS GOLF COURSES, CEMETARIES ETC.)

**CN VALUES - DEVELOPED CONDITIONS** 

DURSE (B)	2 AC. RE	SIDENTIAL (B)	COMPOSITE
			C <sub>N</sub>
AREA	CN	AREA	
(Ac.)		(Ac.)	
0.0	65	22.3	65.0
0.0	65	36.4	65.0
19.1	65	32.8	63.5
63.2	65	45.0	62.7
5.5	65	11.5	63.7
0.0	65	67.7	65.0
0.0	65	36.9	65.0
0.0	65	26.4	65.0

# Table 5.3 Sub-basin Time of Concentration

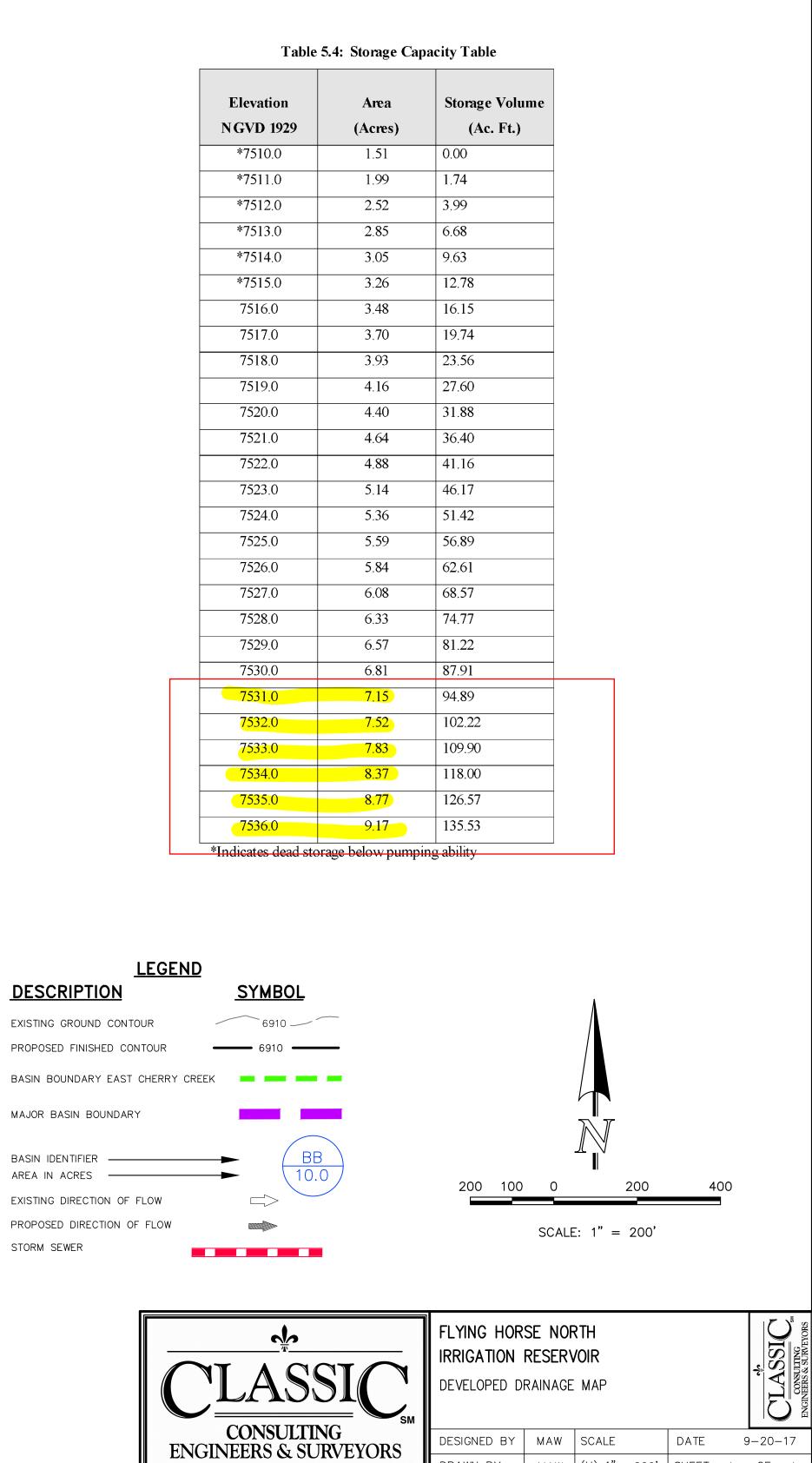
			TIME	OF CONC	ENTRATIC	ON DEVE	LOPED			
	COMPOSITE		OVERLAND		STREET / C	HANNEL FLO	OW(DCM Vo	l. 1 Fig. 6-25)	Tc	Tc
BASIN	Cn	Length	Height	Tc	Length	Slope	Veloaity	Тс	TOTAL	LAG(0.6tc)
		(ft)	(ft)	(hr)	(ft)	(%)	(fps)	(hr)	(hr)	(hr)
CC-1	65.0	300	10	0.40	900	2.0%	1.8	0.14	0.53	0.32
CC-2	65.0	300	10	0.40	1700	2.0%	1.8	0.26	0.66	0.39
CC-3	63.5	300	14	0.35	900	2.5%	2.4	0.10	0.45	0.27
CC-4A	62.7	300	14	0.35	2900	2.0%	2.1	0.38	0.73	0.44
CC-4B	63.7	300	12	0.37	900	3.0%	2.5	0.10	0.47	0.28
OS-12	65.0	300	14	0.35	1500	3.0%	2.5	0.17	0.51	0.31
OS-13	65.0	300	16	0.33	900	3.0%	2.5	0.10	0.43	0.26
OS-14	65.0	300	14	0.35	600	3.5%	2.7	0.06	0.41	0.24

			Total
Storm Event	Peak Inflow	Max. WSE	Discharge
	(cfs)	(ft.)	(cfs)
2-yr (City/ County)	48	7531.40	6
5-yr (City/ County)	119	7531.87	12
50-yr (NOAA 14)	431	7533.58	64
100-yr (NOAA 14)	609	7534.23	124

	2000 000000000000000000000000000000000

	Discharge (cfs)	Discharge (cfs)	Discharge (c
Elevation	(SWQ Outlet Box)	(Twin CBC Spillway)	(Total)
7531.0	0.0	0.0	0.0
7532.0	13.89	0.0	13.89
7533.0	27.77	0.0	27.77
7534.0	51.31	49.05	100.36
7535.0	69.52	138.56	208.08
7536.0	74.61	254.72	329.33
Permanent W	VSE = 7531.0		

Elevation	Area	Storag
NGVD 1929	(Acres)	(A
*7510.0	1.51	0.00
*7511.0	1.99	1.74
*7512.0	2.52	3.99
*7513.0	2.85	6.68
*7514.0	3.05	9.63
*7515.0	3.26	12.78
7516.0	3.48	16.15
7517.0	3.70	19.74
7518.0	3.93	23.56
7519.0	4.16	27.60
7520.0	4.40	31.88
7521.0	4.64	36.40
7522.0	4.88	41.16
7523.0	5.14	46.17
7524.0	5.36	51.42
7525.0	5.59	56.89
7526.0	5.84	62.61
7527.0	6.08	68.57
7528.0	6.33	74.77
7529.0	6.57	81.22
7530.0	6.81	87.91
7531.0	7,15	94.89
7532.0	7.52	102.22
7533.0	7.83	109.90
7534.0	8.37	118.00
7535.0	8.77	126.57
7536.0	9.17	135.53
1550.0	2.17	155.55



DRAWN BY         MAW         (H) 1"= 200'         SHEET         1         OF         1           619 N. Cascade Avenue, Suite 200 Colorado Springs, Colorado 80903         (719)785-0799 (719)785-0799 (Fax)         CHECKED BY         (V) 1"= N/A         JOB NO.         1096.11		CONSULTI ENGINEERS & SU	DESIGNED BY	MAW	SCALE	DATE	9-20-17
	ļ		DRAWN BY	MAW	(H) 1"= 200'	SHEET 1	OF 1
			CHECKED BY		(V) 1"= N/A	JOB NO.	1096.11



# Flying Horse North Filing No. 3 Final Drainage Report

July 27, 2023

#### **Prepared For:**

Mr. Drew Balsick Vice President / Project Manager Flying Horse Development, LLC 2138 Flying Horse Club Drive Colorado Springs, CO 80921 (719) 785-3237

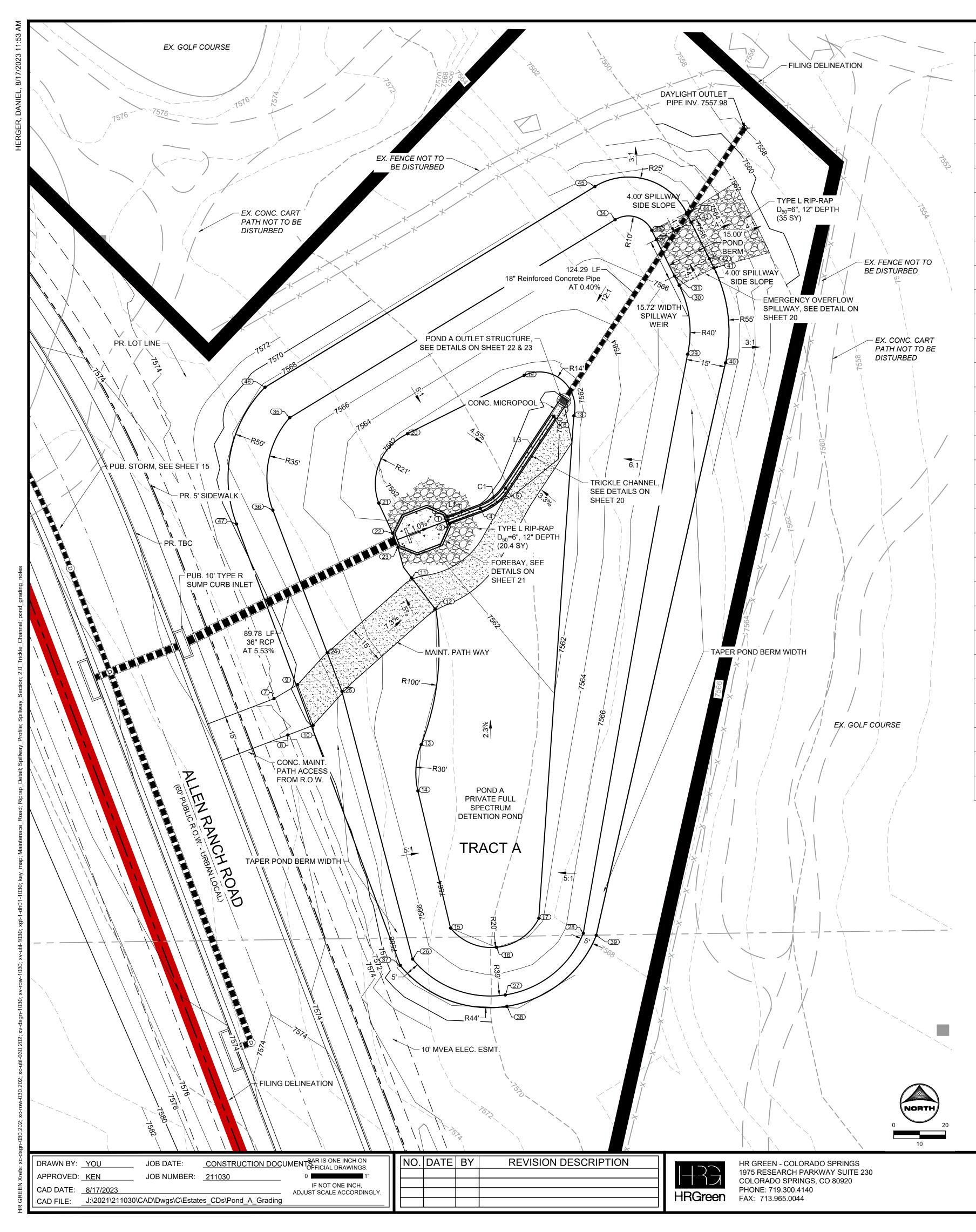
#### **Prepared By:**

HR Green Development, LLC Contact: Richie Lyon, PE Richie.Lyon@hrgreen.com 719-318-0871

PCD File No. SF-XXXX

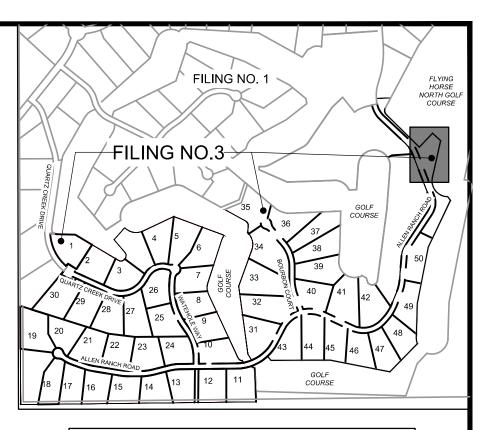
THE FLYING HORSE **FILING NO. 3 FDR CONTAINS A SECTION OF ALLEN RANCH ROAD** AS WELL AS A **DETENTION POND THAT** ARE TO BE USED IN THE **CAPTURE AND DETENTION OF BASINS EX5.1 AND M, EXISTING** AND PROPOSED, LOCATED WITHIN **PARCEL NO. 2 OF THIS** PDR. THE FDR HAS **INCLUDED THESE BASINS INTO THE DESIGN OF ITS PROPOSED STORM** INFRASTRUCTURE.

> HRGREEN.COM



	POINT T			] [	PC	DINT TABLE	
No.	DESC.	NORTHING & EASTING	ELEV	No.	DESC.	NORTHING & EASTING	ELEV
1	TC FLOWLINE	N: 444526.79 E: 222290.46	7559.59	31	SPILLWAY WEIR INV.	N: 444621.06 E: 222377.98	7566.50
2	ТВС	N: 444528.27 E: 222290.12	7560.17	32	SPILLWAY WEIR INV.	N: 444635.13 E: 222370.96	7566.50
3	ТВС	N: 444525.45 E: 222291.16	7560.17	33	ТОР	N: 444638.71 E: 222369.17	7567.50
4	TC FLOWLINE	N: 444531.40 E: 222303.06	7559.46	34	ТОР	N: 444642.78 E: 222355.03	7567.50
5	TC FLOWLINE	N: 444539.14 E: 222312.88	7559.33	35	ТОР	N: 444566.42 E: 222229.50	7567.50
6	TC FLOWLINE	N: 444566.88 E: 222331.26	7559.00	36	ТОР	N: 444530.71 E: 222222.96	7567.50
7	MAINT. RD. EDGE	N: 444457.98 E: 222223.41	7570.90	37	TOP	N: 444355.04 E: 222272.11	7567.50
8	MAINT. RD. EDGE	N: 444443.96 E: 222228.75	7571.06	38	ТОР	N: 444339.28 E: 222313.25	7567.82
9	MAINT. RD. EDGE	N: 444463.39 E: 222232.50	7569.66	39	ТОР	N: 444366.66 E: 222347.77	7567.50
10	MAINT. RD. EDGE	N: 444447.66 E: 222238.48	7569.82	40	ТОР	N: 444587.56 E: 222397.64	7567.50
11	MAINT. RD. EDGE / BOP	N: 444504.59 E: 222276.51	7564.00	41	ТОР	N: 444624.19 E: 222393.19	7567.50
12	MAINT. RD. EDGE / BOP	N: 444492.60 E: 222285.61	7564.00	42	SPILLWAY WEIR INV.	N: 444627.76 E: 222391.40	7566.50
13	BOP	N: 444440.25 E: 222280.19	7564.00	43	SPILLWAY WEIR INV.	N: 444641.83 E: 222384.38	7566.50
14	BOP	N: 444422.39 E: 222278.94	7564.00	44	ТОР	N: 444645.41 E: 222382.59	7567.50
15	BOP	N: 444369.45 E: 222291.52	7564.00	45	ТОР	N: 444655.60 E: 222347.23	7567.50
16	BOP HP	N: 444362.04 E: 222309.25	7564.00	46	ТОР	N: 444578.17 E: 222219.95	7567.50
17	BOP	N: 444373.24 E: 222325.60	7563.62	47	ТОР	N: 444525.36 E: 222208.95	7569.66
18	BOP	N: 444567.11 E: 222339.11	7561.50				
19	BOP	N: 444582.71 E: 222319.90	7561.50				
20	BOP	N: 444560.21 E: 222274.90	7561.63				
21	BOP	N: 444533.46 E: 222263.80	7562.25				
22	BOP / TOP OF FOREBAY WALL	N: 444521.77 E: 222269.18	7565.33				
23	BOP / TOP OF FOREBAY WALL	N: 444516.38 E: 222271.24	7565.33				
24	TOP / MAINT. RD. EDGE	N: 444475.69 E: 222243.95	7567.50				
25	TOP / MAINT. RD. EDGE	N: 444460.75 E: 222249.64	7567.50				
26	ТОР	N: 444357.48 E: 222276.86	7567.50				
27	ТОР	N: 444343.67 E: 222312.66	7567.50				
28	ТОР	N: 444367.45 E: 222342.78	7567.50				
29	ТОР	N: 444590.85 E: 222383.01	7567.50				
30	ТОР	N: 444617.49 E: 222379.77	7567.50				

FLYING HORSE NORTH FILING 3 FLYING HORSE NORTH, LLC EL PASO COUNTY, CO



	Line Table								
	Line	#	Length		Dir	rection	Centerline/Flowline	Э	
	L1		13.42		N 69°	°56'16" E	Centerline		
	L3		33.28		33.28 N 33°31'34" E		Centerline		
					Curv	ve Table	_		
Cur	ve #	Le	ength	R	adius	Delta	Centerline/Flow	line	
0	C1	1	2.71	2	20.00 36°24'43" Flowline				

POND GRADING NOTES:

1.	TWO SIGNS OF MINIMUM 3 SQ. FT. AREA, SHALL BE INSTALLED AROUND THE POND
	PERIMETER. THE SIGNS WILL BE CONSTRUCTED OF A DURABLE MATERIAL SUCH
	AS METAL OR PLASTIC AND HAVE RED LETTERING ON A WHITE BACKGROUND
	STATING, "WARNING- THIS AREA IS A STORMWATER FACILITY AND IS SUBJECT TO

PERIODIC FLOODING. 2. SEE LANDSCAPE PLAN FOR RE-SEEDING AREAS ASSOCIATED WITH PERMANENT CONTROL MEASURE IMPROVEMENTS.

3. SEE GRADING & EROSION CONTROL PLANS FOR ANY EXISTING VEGETATION IN THE AREA. CLEARING AND GRUBBING WILL OCCUR PRIOR TO POND CONSTRUCTION AND THEREFORE, NO EXISTING VEGETATION WILL BE PRESENT. 4. ALL RIPRAP MUST BE INSTALLED PER DETAIL ON NEXT PAGE.

POND A GRADING PLAN

DRAINAGE DETAILS

ABBREVIATIONS:

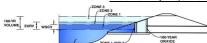
B.O.P ~ BOTTOM OF POND T.O.P. ~ TOP OF POND T.C. ~TRICKLE CHANNEL T.B.C~ TOP BACK OF CURB C.L.~ CENTERLINE E.O.G~ EDGE OF GRADING S.W ~ SPILLWAY

SHEET	
PND	19

#### DETENTION BASIN STAGE-STORAGE TABLE BUILDER

#### Project: FLYING HORSE NORTH FILING NO. 3 Basin ID: DESIGN POINT 2 (FLATS/CONDO AREA)

acre-feet



ZONE 1 AND 2 ORIFICES Example Zone Configuration (Retention Pond) PERMA

#### Watershed Information

Selected BMP Type =	EDB	
Watershed Area =	25.30	acres
Watershed Length =	1,800	ft
Watershed Length to Centroid =	400	ft
Watershed Slope =	0.050	ft/ft
Watershed Imperviousness =	32.24%	percent
Percentage Hydrologic Soil Group A =	0.0%	percent
Percentage Hydrologic Soil Group B =	100.0%	percent
Percentage Hydrologic Soil Groups C/D =	0.0%	percent
Target WQCV Drain Time =	40.0	hours
Location for 1-hr Rainfall Depths =	User Input	

# After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

the embedded Colorado Urban Hydro	graph Procedu	re.
Water Quality Capture Volume (WQCV) =	0.334	acre-feet
Excess Urban Runoff Volume (EURV) =	0.842	acre-feet
2-yr Runoff Volume (P1 = 1.19 in.) =	0.828	acre-feet
5-yr Runoff Volume (P1 = 1.5 in.) =	1.315	acre-feet
10-yr Runoff Volume (P1 = 1.75 in.) =	1.762	acre-feet
25-yr Runoff Volume (P1 = 2 in.) =	2.426	acre-feet
50-yr Runoff Volume (P1 = 2.25 in.) =	2.934	acre-feet
100-yr Runoff Volume (P1 = 2.52 in.) =	3.607	acre-feet
500-yr Runoff Volume (P1 = 3.14 in.) =	4.918	acre-feet
Approximate 2-yr Detention Volume =	0.607	acre-feet
Approximate 5-yr Detention Volume =	0.863	acre-feet
Approximate 10-yr Detention Volume =	1.239	acre-feet
Approximate 25-yr Detention Volume =	1.423	acre-feet
Approximate 50-yr Detention Volume =	1.498	acre-feet
Approximate 100-yr Detention Volume =	1.758	acre-feet

#### Define Zones and Basin Geometry

Zone 1 Volume (WQCV) =	0.334	acre-feet
Zone 2 Volume (EURV - Zone 1) =	0.508	acre-feet
Zone 3 Volume (100-year - Zones 1 & 2) =	0.916	acre-feet
Total Detention Basin Volume =	1.758	acre-feet
Initial Surcharge Volume (ISV) =	user	ft <sup>3</sup>
Initial Surcharge Depth (ISD) =	user	ft
Total Available Detention Depth (H <sub>total</sub> ) =	user	ft
Depth of Trickle Channel (H <sub>TC</sub> ) =	user	ft
Slope of Trickle Channel (S <sub>TC</sub> ) =	user	ft/ft
Slopes of Main Basin Sides (S <sub>main</sub> ) =	user	H:V
Basin Length-to-Width Ratio (R <sub>L/W</sub> ) =	user	
Initial Europarao Area (A) =	ucor	<b>⊕</b> 2

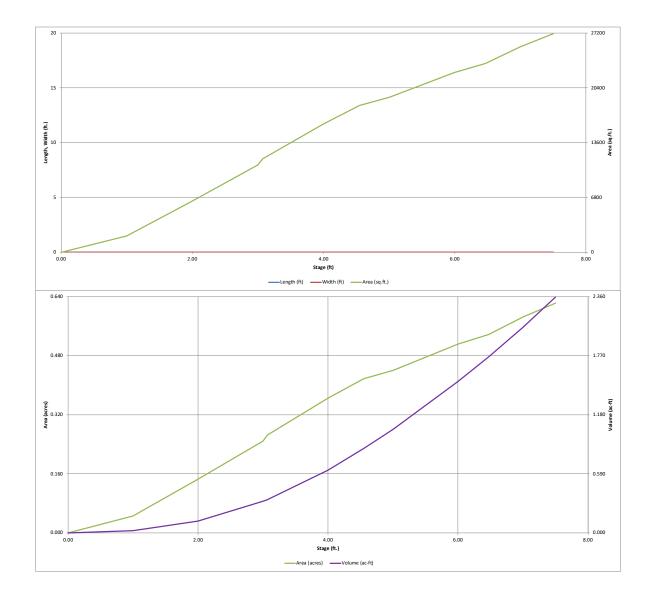
Initial Surcharge Area $(A_{ISV}) =$	user	ft '
Surcharge Volume Length $(L_{ISV}) =$	user	ft
Surcharge Volume Width (W <sub>ISV</sub> ) =	user	ft
Depth of Basin Floor $(H_{FLOOR}) =$	user	ft
Length of Basin Floor $(L_{FLOOR}) =$	user	ft
Width of Basin Floor ( $W_{FLOOR}$ ) =	user	ft
Area of Basin Floor $(A_{FLOOR}) =$	user	ft²
Volume of Basin Floor ( $V_{FLOOR}$ ) =	user	ft <sup>3</sup>
Depth of Main Basin $(H_{MAIN}) =$	user	ft
Length of Main Basin $(L_{MAIN}) =$	user	ft
Width of Main Basin ( $W_{MAIN}$ ) =	user	ft
Area of Main Basin (A <sub>MAIN</sub> ) =	user	ft <sup>2</sup>
Volume of Main Basin (V <sub>MAIN</sub> ) =	user	ft <sup>3</sup>

Calculated Total Basin Volume (V<sub>total</sub>) = user acre-feet

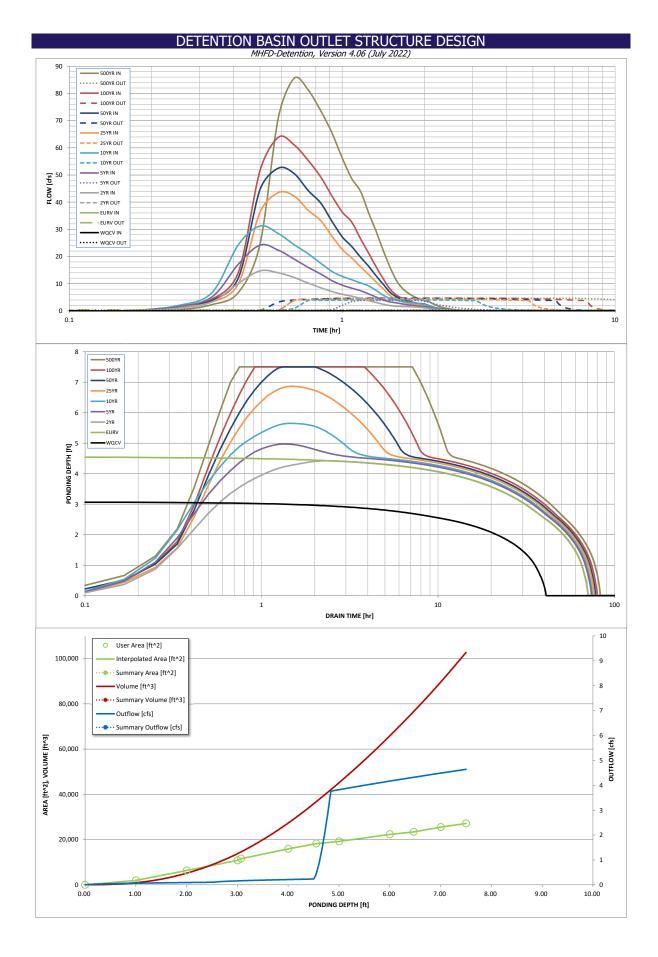
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	on Pond)		Override			Override			
			Stage (ft)					(ft )	(ac-ft)
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		7560	 1.00	 		1,991	0.046	995	0.023
		7561	 2.00	 		6,349	0.146	5,165	0.119
				 		10.825			
198110									
							0.440	45,093	1.035
		7565	 6.00	 		22,288	0.512	65,830	1.511
		100-YR: 7565.47	 6.47	 		23,400	0.537	76,566	1.758
				 				89.526	
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#### DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.06 (July 2022)



	DE	TENTION I	BASIN OUT	<b>FLET STRU</b>	CTURE DE	SIGN			
	FLYING HORSE N	M. DRTH FILING NO. 3	HFD-Detention, V 3	ersion 4.06 (July					
Basin ID:	DESIGN POINT 2	FLATS/CONDO AR	EA)						
ZONE 2 ZONE 1				Estimated	Estimated	0.41-4.75.00.0			
			7 4 4 4 4 6 6 6	Stage (ft)	Volume (ac-ft)	Outlet Type	1		
TT Mach			Zone 1 (WQCV)	3.08	0.334	Orifice Plate			
ZONE 1 AND 2	100-YEAR ORIFICE		Zone 2 (EURV)	-	0.508	Orifice Plate			
PERMANENT ORIFICES POOL Example Zone	Configuration (R		Zone 3 (100-year)	6.48	0.916	Weir&Pipe (Restrict)			
•	• •	,		Total (all zones)	1.758				
User Input: Orifice at Underdrain Outlet (typical		-	,	<i>c</i> .				eters for Underdrain	<u>l</u>
Underdrain Orifice Invert Depth = Underdrain Orifice Diameter =	N/A N/A	inches	the filtration media	i surrace)		drain Orifice Area = n Orifice Centroid =	N/A N/A	ft <sup>2</sup> feet	
User Input: Orifice Plate with one or more orific			-				Calculated Parame		
Centroid of Lowest Orifice =	0.00		h bottom at Stage =		-	ice Area per Row =	1.389E-02	ft <sup>2</sup>	
Depth at top of Zone using Orifice Plate =	4.00		h bottom at Stage =	= 0 ft)		iptical Half-Width =	N/A	feet	
Orifice Plate: Orifice Vertical Spacing =	N/A 2.00	inches	ar = 1.0/16 inchos	<b>`</b>		ical Slot Centroid =	N/A N/A	feet ft <sup>2</sup>	
Orifice Plate: Orifice Area per Row =	2.00	sq. incries (diamet	er = 1-9/16 inches	)	E	Elliptical Slot Area =	IN/A	lit.	
User Input: Stage and Total Area of Each Orific	e Row (numbered	from lowest to high	nest)						
	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)	
Stage of Orifice Centroid (ft)	0.00	2.55	· · ·				· · · · · · · · · · · · · · · · · · ·		
Orifice Area (sq. inches)	2.00	2.00							
									l
	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)	
Stage of Orifice Centroid (ft)									
Orifice Area (sq. inches)					<u> </u>				
User Input: Vertical Orifice (Circular or Rectang	udes)						Calculated Davam	tors for Vortical Or	fiee
User Input: Vertical Office (Circular of Rectang	Not Selected	Not Selected						eters for Vertical Ori	lince
Invert of Vertical Orifice =	N/A	N/A	ft (relative to bacir	n bottom at Stage =	-0ft) Ve	rtical Orifice Area =	Not Selected N/A	Not Selected N/A	ft <sup>2</sup>
Depth at top of Zone using Vertical Orifice =	N/A	N/A N/A		n bottom at Stage =	,	I Orifice Centroid =	N/A		feet
Vertical Orifice Diameter =	N/A	N/A	inches	- Doctom at Stage -	- ore) vertica		11/1	N/A	
User Input: Overflow Weir (Dropbox with Flat c	or Sloped Grate and	l Outlet Pipe OR Re	ctangular/Trapezoi	idal Weir and No O	utlet Pipe)		Calculated Parame	eters for Overflow W	Veir
	Zone 3 Weir	Not Selected					Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	4.50	N/A		bottom at Stage = 0			4.50	N/A	feet
Overflow Weir Front Edge Length =	3.00	N/A	feet			/eir Slope Length =	2.50	N/A	feet
Overflow Weir Grate Slope =	0.00	N/A	H:V			00-yr Orifice Area =	15.11	N/A	2
Horiz. Length of Weir Sides =	2.50	N/A	feet		•	Area w/o Debris =	5.22	N/A	ft <sup>2</sup>
Overflow Grate Type =	Type C Grate 50%	N/A	0/	0	verflow Grate Ope	n Area w/ Debris =	2.61	N/A	ft <sup>2</sup>
Debris Clogging % =	50%	N/A	%						
User Input: Outlet Pipe w/ Flow Restriction Plate	e (Circular Orifice, I	Restrictor Plate, or	Rectangular Orifice	2)					
F	Zone 3 Restrictor	Not Selected			Ca	lculated Parameters	s for Outlet Pipe w	Flow Restriction Pl	ate
Depth to Invert of Outlet Pipe =	0.50				<u>Ca</u>	Iculated Parameters	s for Outlet Pipe w Zone 3 Restrictor	/ Flow Restriction Pl Not Selected	<u>ate</u>
Outlet Pipe Diameter =		IN/A	ft (distance below ba	asin bottom at Stage		ulculated Parameters		Not Selected	<u>ate</u> ft <sup>2</sup>
	18.00	N/A N/A	ft (distance below ba inches	asin bottom at Stage	= 0 ft) O		Zone 3 Restrictor	Not Selected	
Restrictor Plate Height Above Pipe Invert =	18.00 4.50			5	= 0 ft) Outlet	utlet Orifice Area =	Zone 3 Restrictor 0.35	Not Selected N/A	ft²
Restrictor Plate Height Above Pipe Invert =	4.50		inches	5	= 0 ft) Outlet	utlet Orifice Area = t Orifice Centroid =	Zone 3 Restrictor 0.35 0.22 1.05	Not Selected N/A N/A N/A	ft <sup>2</sup> feet
Restrictor Plate Height Above Pipe Invert =	4.50 Trapezoidal)	N/A	inches inches	Half-Cent	= 0 ft) Ou Outlet ral Angle of Restric	utlet Orifice Area = t Orifice Centroid = ctor Plate on Pipe =	Zone 3 Restrictor 0.35 0.22 1.05 Calculated Parame	Not Selected N/A N/A N/A eters for Spillway	ft <sup>2</sup> feet
Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage=	4.50 • <u>Trapezoidal)</u> 8.00	N/A ft (relative to basir	inches	Half-Cent	= 0 ft) Ou Outlet ral Angle of Restric Spillway D	utlet Orifice Area = t Orifice Centroid = tor Plate on Pipe = Design Flow Depth=	Zone 3 Restrictor 0.35 0.22 1.05 Calculated Parame 0.81	Not Selected N/A N/A N/A eters for Spillway feet	ft <sup>2</sup> feet
Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length =	4.50 <u>Trapezoidal)</u> 8.00 23.72	N/A ft (relative to basir feet	inches inches	Half-Cent	= 0 ft) Oi Outler ral Angle of Restric Spillway D Stage at T	utlet Orifice Area = t Orifice Centroid = tor Plate on Pipe = Design Flow Depth= Top of Freeboard =	Zone 3 Restrictor 0.35 0.22 1.05 Calculated Parame 0.81 9.81	Not Selected N/A N/A N/A eters for Spillway feet feet	ft <sup>2</sup> feet
Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length = Spillway End Slopes =	4.50 <u>Trapezoidal)</u> 8.00 23.72 4.00	N/A ft (relative to basir feet H:V	inches inches	Half-Cent	= 0 ft) O Outlet ral Angle of Restric Spillway D Stage at T Basin Area at T	utlet Orifice Area = t Orifice Centroid = tor Plate on Pipe = Design Flow Depth= Top of Freeboard = Fop of Freeboard =	Zone 3 Restrictor 0.35 0.22 1.05 <u>Calculated Parame</u> 0.81 9.81 0.62	Not Selected N/A N/A N/A eters for Spillway feet feet acres	ft <sup>2</sup> feet
Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length =	4.50 <u>Trapezoidal)</u> 8.00 23.72	N/A ft (relative to basir feet	inches inches	Half-Cent	= 0 ft) O Outlet ral Angle of Restric Spillway D Stage at T Basin Area at T	utlet Orifice Area = t Orifice Centroid = tor Plate on Pipe = Design Flow Depth= Top of Freeboard =	Zone 3 Restrictor 0.35 0.22 1.05 Calculated Parame 0.81 9.81	Not Selected N/A N/A N/A eters for Spillway feet feet	ft <sup>2</sup> feet
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Restrictor Plate Height Above Pipe Invert = <u>User Input: Emergency Spillway (Rectangular or</u> Spillway Invert Stage= Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface =	4.50 Trapezoidal) 8.00 23.72 4.00 1.00	N/A ft (relative to basir feet H:V feet	inches inches hottom at Stage =	Half-Centr = 0 ft) <i>Id runoff volumes b</i> 5 Year	= 0 ft) O Outlet ral Angle of Restric Spillway D Stage at T Basin Area at T Basin Volume at T	utlet Orifice Area = t Orifice Centroid = tor Plate on Pipe = Design Flow Depth= Top of Freeboard = Top of Freeboard = Top of Freeboard = <u>Uses in the Inflow H</u> 25 Year	Zone 3 Restrictor 0.35 0.22 1.05 <u>Calculated Parame</u> 0.81 9.81 0.62 2.36 <u>vdrographs table (r</u> 50 Year	Not Selected N/A N/A N/A N/A eters for Spillway feet feet acres acre-ft Columns W through 100 Year	ft <sup>2</sup> feet radians <i>AF)</i> .
Restrictor Plate Height Above Pipe Invert = <u>User Input: Emergency Spillway (Rectangular or</u> Spillway Invert Stage= Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = <u>Routed Hydrograph Results</u> Design Storm Return Period = One-Hour Rainfall Depth (in) =	4.50 <u>Trapezoidal)</u> 8.00 23.72 4.00 1.00 The user can over WQCV N/A	N/A ft (relative to basir feet H:V feet ride the default CU EURV N/A	inches inches n bottom at Stage = <u>HP hydrographs an</u> <u>2 Year</u> 1.19	Half-Centr = 0 ft) dr <i>runoff volumes b</i> 5 Year 1.50	= 0 ft) Or Outlet ral Angle of Restric Spillway D Stage at T Basin Area at T Basin Volume at T ov entering new val 10 Year 1.75	utlet Orifice Area = t Orifice Centroid = tor Plate on Pipe = Design Flow Depth= Top of Freeboard = Top of Freeboard = Top of Freeboard = <u>Lues in the Inflow H</u> <u>25 Year</u> 2.00	Zone 3 Restrictor 0.35 0.22 1.05 <u>Calculated Parame</u> 0.81 0.62 2.36 <u>vdrographs table (r</u> <u>50 Year</u> 2.25	Not Selected N/A N/A N/A eters for Spillway feet feet acres acre-ft Columns W through 100 Year 2.52	ft <sup>2</sup> feet radians <u>AF).</u> <u>500 Year</u> <u>3.14</u>
Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Routed Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) =	4.50 <u>Trapezoidal)</u> 8.00 23.72 4.00 1.00 <i>The user can over</i> WQCV N/A 0.334	N/A ft (relative to basir feet H:V feet ride the default CU EURV N/A 0.842	inches inches h bottom at Stage = HP hydrographs an 2 Year 1.19 0.828	Half-Centr = 0 ft) <u>0 runoff volumes b</u> <u>5 Year</u> <u>1.50</u> <u>1.315</u>	= 0 ft) Or Outlet ral Angle of Restric Spillway D Stage at T Basin Area at T Basin Volume at T Basin Volume at T Or entering new Val 10 Year 1.75 1.762	utlet Orifice Area = t Orifice Centroid = ctor Plate on Pipe = Design Flow Depth= Top of Freeboard = Top of Freeboard = Top of Freeboard = <u>Uses in the Inflow H</u> <u>2.5 Year</u> <u>2.00</u>	Zone 3 Restrictor 0.35 0.22 1.05 <u>Calculated Parame</u> 0.81 9.81 0.62 2.36 <u>vdrographs table (1</u> 50 Year 2.25 2.934	Not Selected N/A N/A N/A N/A eters for Spillway feet feet acres acre-ft Columns W through 100 Year 2.52 3.607	ft <sup>2</sup> feet radians 500 Year <u>3.14</u> 4.918
Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Routed Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) =	4.50 <u>Trapezoidal</u> ) 8.00 23.72 4.00 1.00 <i>The user can over</i> WQCV N/A 0.334 N/A	N/A ft (relative to basir feet H:V feet EURV N/A 0.842 N/A	inches inches n bottom at Stage = HP hydrographs am 2 Year 1.19 0.828 0.828	Half-Centr = 0 ft) 5 Year 1.50 1.315 1.315	= 0 ft) Or Outlet ral Angle of Restric Spillway D Stage at T Basin Area at T Basin Volume at T Basin Volume at T Dy entering new val 1.75 1.762 1.762	utlet Orifice Area = t Orifice Centroid = tor Plate on Pipe = Design Flow Depth= Top of Freeboard = Top of Freeboard = Top of Freeboard = <u>Uses in the Inflow H</u> 25 Year 2.00 2.426 2.426	Zone 3 Restrictor 0.35 0.22 1.05 <u>Calculated Parame</u> 0.81 9.81 0.62 2.36 <u>vdrographs table (v</u> <u>50 Year</u> 2.25 2.934 2.934	Not Selected N/A N/A N/A N/A eters for Spillway feet feet acres acre-ft Columns W through 100 Year 2.52 3.607 3.607	AF). 500 Year 3.14 4.918
Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Routed Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = CUHP Predevelopment Peak Q (cfs) = OPTIONAL Override Predevelopment Peak Q (cfs) =	4.50 <u>Trapezoidal)</u> 8.00 23.72 4.00 1.00 <i>The user can over</i> WQCV N/A 0.334	N/A ft (relative to basir feet H:V feet ride the default CU EURV N/A 0.842	inches inches h bottom at Stage = HP hydrographs an 2 Year 1.19 0.828 0.828 4.0	Half-Centr = 0 ft) 5 Year 1.50 1.315 1.315 1.315	= 0 ft) Ou Outlet ral Angle of Restric Spillway D Stage at T Basin Area at T Basin Volume at T Basin Volume at T 0 yentering new val 10 Year 1.75 1.762 1.762 1.762 1.762	utlet Orifice Area = t Orifice Centroid = ctor Plate on Pipe = Design Flow Depth= Top of Freeboard = Top of Freeboard = Top of Freeboard = <u>Uses in the Inflow H</u> <u>2.5 Year</u> <u>2.00</u>	Zone 3 Restrictor 0.35 0.22 1.05 <u>Calculated Parame</u> 0.81 9.81 0.62 2.36 <u>vdrographs table (0</u> <u>50 Year</u> 2.25 2.934 2.934 3.5.4	Not Selected N/A N/A N/A N/A eters for Spillway feet feet acres acre-ft Columns W through 100 Year 2.52 3.607 3.607 44.3	AF).           500 Year           3.14           4.918           61.5
Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Routed Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = UHP Predevelopment Peak Q (cfs) = OPTIONAL Override Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, q (cfs/acre) =	4.50 <u>Trapezoidal)</u> 8.00 23.72 4.00 1.00 <i>The user can over</i> WQCV N/A 0.334 N/A N/A N/A N/A	N/A ft (relative to basir feet H:V feet <u>EURV</u> N/A N/A N/A N/A N/A	Inches Inches In bottom at Stage = HP hydrographs an 2 Year 1.19 0.828 0.828 4.0 0.16	Half-Centr = 0 ft) = 0 ft) = 5 Year 1.50 1.315 1.315 1.315 1.315 1.315 1.315 1.315	= 0 ft) Ou Outlet ral Angle of Restric Spillway D Stage at T Basin Area at T Basin Volume at T Basin Volume at T 1.75 1.762 1.762 1.762 1.762 1.762	utlet Orifice Area = t Orifice Centroid = ctor Plate on Pipe = Design Flow Depth= Top of Freeboard = Top of Freeboard = Top of Freeboard = 2.00 2.426 2.426 2.426 2.426 2.426 2.426 1.12	Zone 3 Restrictor 0.35 0.22 1.05 <u>Calculated Parame</u> 0.81 9.81 0.62 2.36 <u>Vdrographs table (0</u> 50 Year 2.25 2.934 2.934 3.5.4 1.40	Not Selected N/A N/A N/A N/A eters for Spillway feet feet acres acre-ft Columns W through 100 Year 2.52 3.607 3.607 44.3 1.75	AF). 500 Year 3.14 4.918 4.918 61.5 2.43
Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Routed Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (are: ft) = UHP Predevelopment Peak Q (cfs) = CUHP Predevelopment Peak Q (cfs) = Predevelopment Unit Peak How, q (cfs/are) = Peak Inflow Q (cfs) = Peak Inflow Q (cfs) =	4.50 <u>Trapezoidal)</u> 8.00 23.72 4.00 1.00 The user can over WQCV N/A 0.334 N/A N/A N/A N/A N/A N/A	N/A ft (relative to basin feet H:V feet <u>Fide the default CU</u> N/A N/A N/A N/A N/A N/A N/A N/A	inches inches n bottom at Stage = <u>HIP hydrographs am</u> <u>2 Year</u> <u>1.19</u> <u>0.828</u> <u>4.0</u> <u>0.16</u> <u>14.7</u>	Half-Centr = 0 ft) d runoff volumes b 5 Year 1.50 1.315 1.315 10.9 0.43 24.2	= 0 ft) Or Outlet ral Angle of Restric Spillway D Stage at T Basin Area at T Basin Volume at T Basin Volume at T 1.75 1.762 1.762 1.762 1.61 0.64 31.2	utlet Orifice Area = t Orifice Centroid = tor Plate on Pipe = Design Flow Depth= Top of Freeboard = Top of Freeboard = Top of Freeboard = <u>1000 freeboard =</u> 2.00 2.426 2.426 2.426 2.426 2.426 2.426 2.43 1.12 4.3.5	Zone 3 Restrictor 0.35 0.22 1.05 <u>Calculated Parame</u> 0.81 9.81 0.62 2.36 <u>vdrographs table (0</u> 50 Year 2.25 2.934 35.4 <u>1.40</u> 52.5	Not Selected N/A N/A N/A N/A eters for Spillway feet feet acres acre-ft Columns W through 100 Year 2.52 3.607 3.607 44.3 1.75 63.9	AF).           500 Year           3.14           4.918           61.5           2.43           85.5
Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Routed Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = UHP Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, q (cfs)acre) = Peak Notflow Q (cfs) = Peak Outflow Q (cfs) = Peak Outflow Q (cfs) = Peak Notflow Q (cfs)	4.50 Trapezoidal) 8.00 23.72 4.00 1.00 The user can over WQCV N/A 0.334 N/A N/A N/A N/A N/A N/A 0.2	N/A ft (relative to basin feet H:V feet ride the default CU N/A N/A N/A N/A N/A N/A N/A N/A 0.4	Inches Inches In bottom at Stage = HP hydrographs an 2 Year 1.19 0.828 0.828 4.0 0.16 14.7 0.2	Half-Centr = 0 ft) d runoff volumes b 5 Year 1.50 1.315 1.315 1.315 1.315 1.0.9 0.43 24.2 3.8	= 0 ft) Or Outlet ral Angle of Restric Spillway D Stage at T Basin Area at T Basin Volume at T Basin Volume at T Over 1.75 1.762 1.775 1.762 1.775 1.762 1.775 1.762 1.775 1.762 1.775 1.762 1.775 1.762 1.775 1.762 1.775 1.762 1.775 1.762 1.775 1.762 1.775 1.762 1.775 1.762 1.775 1.762 1.752 1.762 1.775 1.762 1.752 1.762 1.752 1.762 1.752 1.762 1.752 1.762 1.752 1.762 1.752 1.762 1.752 1.762 1.752 1.762 1.762 1.762 1.762 1.762 1.762 1.762 1.762 1.762 1.762 1.762 1.762 1.762 1.762 1.762 1.762	utlet Orifice Area = t Orifice Centroid = ctor Plate on Pipe = Design Flow Depth= Top of Freeboard = Top of Freeboard = Top of Freeboard = 25 Year 2.00 2.426 2.426 2.426 2.426 1.12 1.12 4.3.5 4.4	Zone 3 Restrictor 0.35 0.22 1.05 Calculated Parame 0.81 9.81 0.62 2.36 vdrographs table (C 50 Year 2.25 2.934 2.934 3.5.4 - 1.40 52.5 4.6	Not Selected N/A N/A N/A N/A eters for Spillway feet feet acres acre-ft Columns W through 100 Year 2.52 3.607 3.607 3.607 44.3 - - - - - - - - - - - - - - - - - - -	AF).           500 Year           3.14           4.918           61.5           2.43           85.5           4.6
Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Routed Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (are: ft) = UHP Predevelopment Peak Q (cfs) = CUHP Predevelopment Peak Q (cfs) = Predevelopment Unit Peak How, q (cfs/are) = Peak Inflow Q (cfs) = Peak Inflow Q (cfs) =	4.50 <u>Trapezoidal)</u> 8.00 23.72 4.00 1.00 The user can over WQCV N/A 0.334 N/A N/A N/A N/A N/A N/A	N/A ft (relative to basin feet H:V feet <u>Fide the default CU</u> N/A N/A N/A N/A N/A N/A N/A N/A	inches inches n bottom at Stage = <u>HIP hydrographs am</u> <u>2 Year</u> <u>1.19</u> <u>0.828</u> <u>4.0</u> <u>0.16</u> <u>14.7</u>	Half-Centr = 0 ft) d runoff volumes b 5 Year 1.50 1.315 1.315 10.9 0.43 24.2	= 0 ft) Or Outlet ral Angle of Restric Spillway D Stage at T Basin Area at T Basin Volume at T Basin Volume at T 1.75 1.762 1.762 1.762 1.61 0.64 31.2	utlet Orifice Area = t Orifice Centroid = tor Plate on Pipe = Design Flow Depth= Top of Freeboard = Top of Freeboard = Top of Freeboard = <u>1000 freeboard =</u> 2.00 2.426 2.426 2.426 2.426 2.426 2.426 2.43 1.12 4.3.5	Zone 3 Restrictor 0.35 0.22 1.05 <u>Calculated Parame</u> 0.81 9.81 0.62 2.36 <u>vdrographs table (0</u> 50 Year 2.25 2.934 35.4 <u>1.40</u> 52.5	Not Selected N/A N/A N/A N/A eters for Spillway feet feet acres acre-ft Columns W through 100 Year 2.52 3.607 3.607 44.3 1.75 63.9	AF).           500 Year           3.14           4.918           61.5           2.43           85.5
Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Routed Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = OHPTIONAL Override Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, q (cfs) = Peak Inflow Q (cfs) = Peak Outflow to Predevelopment Q = Structure Controlling Flow = Max Velocity through Grate 1 (fps) =	4.50 Trapezoidal) 8.00 23.72 4.00 1.00 The user can over WQCV N/A 0.334 N/A N/A N/A N/A N/A N/A N/A N/A	N/A ft (relative to basin feet H:V feet CURV N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A	Inches Inches In bottom at Stage = Network Stage Inches In	Half-Centr = 0 ft) = 0 ft) = 5 Year 1.50 1.315 1.315 10.9 = 0.43 24.2 3.8 0.4 0.43 24.2 3.8 0.4 0.4 0.4 0.4 0.7	= 0 ft) Ou Outlet ral Angle of Restric Spillway D Stage at 1 Basin Area at 1 Basin Volume at 1 Basin Volume at 1 1.75 1.762 1.762 1.762 1.6.1 0.64 31.2 4.1 0.3 Outlet Plate 1 0.7	utlet Orifice Area = t Orifice Centroid = tor Plate on Pipe = Cop of Freeboard = Top of Freeboard = Top of Freeboard = Cop of Freeboard = 2.426	Zone 3 Restrictor 0.35 0.22 1.05 <u>Calculated Parame</u> 0.81 9.81 0.62 2.36 <u>vdrographs table (0</u> 50 Year 2.25 2.934 35.4 <u>1.40</u> 52.5 4.6 0.1 N/A 0.8	Not Selected N/A N/A N/A N/A eters for Spillway feet feet acres acre-ft Columns W through 100 Year 2.52 3.607 3.607 3.607 44.3 0.1 0.1 N/A 0.8	AF).           500 Year           3.14           4.918           61.5           2.43           85.5           4.6           0.1           N/A           0.8
Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = One-Hour Rainfail Depth (in) = CUHP Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = CUHP Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, q (cfs/acre) = Peak Unflow Q (cfs) = Peak Inflow Q (cfs) = Ratio Peak Outflow to Predevelopment Q = Structure Controlling Flow = Max Velocity through Grate 1 (fps) = Max Velocity through Grate 1 (fps) =	4.50 Trapezoidal) 8.00 23.72 4.00 1.00 The user can over WQCV N/A 0.334 N/A N/A N/A N/A N/A N/A N/A N/A	N/A ft (relative to basin feet H:V feet ride the default CU EURV N/A 0.842 N/A N/A N/A N/A N/A N/A O.4 N/A O.4 N/A O.4 N/A O.4 N/A	Inches Inches In bottom at Stage = HP hydrographs an 2 Year 1.19 0.828 0.828 4.0 0.16 14.7 0.2 N/A Plate N/A N/A	Half-Centr = 0 ft) d runoff volumes b 5 Year 1.50 1.315 1.31	= 0 ft) Or Outlet ral Angle of Restrict Spillway D Stage at T Basin Area at T Basin Volume at T Basin Volume at T Or <i>entering new val</i> 10 Year 1.75 1.762 1.775 1.762 1.762 1.762 1.775 1.762 1.775 1.762 1.775 1.762 1.775 1.762 1.775 1.762 1.775 1.762 1.775 1.775 1.762 1.775 1.762 1.775 1	utlet Orifice Area = t Orifice Centroid = ctor Plate on Pipe = Cop of Freeboard = Top of Freeboard = Top of Freeboard = Cop of	Zone 3 Restrictor 0.35 0.22 1.05 Calculated Parame 0.81 9.81 0.62 2.36 Vdrographs table (1 50 Year 2.25 2.934 2.934 2.934 35.4 1.40 52.5 4.6 0.1 N/A 0.8 N/A	Not Selected           N/A           N/A           N/A           N/A           N/A           eters for Spillway           feet           feet           acres           acre-ft           Columns W through           100 Year           2.52           3.607           3.607           3.607           44.3           1.75           63.9           4.6           0.1           N/A	AF).           500 Year           3.14           4.918           61.5           2.43           85.5           4.6           0.1           N/A
Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length = Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface =  Routed Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = CUHP Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, q (cfs/acre) = Peak Inflow Q (cfs) = Peak Outflow to Predevelopment Q (cfs) = Peak Outflow Q (cfs) = Ratio Peak Outflow to Predevelopment Q = Structure Controlling Flow = Max Velocity through Grate 1 (fps) = Max Velocity through Grate 2 (fps) = Time to Drain 97% of Inflow Volume (hours) =	4.50 Trapezoidal) 8.00 23.72 4.00 1.00 The user can over WQCV N/A 0.334 N/A N/A N/A N/A N/A N/A N/A N/A	N/A ft (relative to basin feet H:V feet EURV N/A 0.842 N/A N/A N/A N/A N/A 0.4 N/A 0.4 N/A 0.4 N/A 0.4 N/A 65	Inches Inches In bottom at Stage = HP hydrographs an 2 Year 1.19 0.828 0.828 4.0 0.16 14.7 0.2 N/A Plate N/A N/A 65	Half-Centr = 0 ft) = 0 ft) = 5 Year 1.50 1.315 1.316 1.315 1	= 0 ft) Ou Outlet ral Angle of Restrict Spillway D Stage at T Basin Area at T Basin Volume at T Basin Volume at T 1.75 1.762 1.775 1.762 1.762 1.775 1.762 1.762 1.775 1.776 1.775 1.776 1.775 1.776 1.775 1.776 1.775 1.776 1.775 1.776 1.776 1.775 1.776 1.776 1.775 1.776 1.776 1.775 1.776 1.776 1.776 1.776 1.775 1.776 1.776 1.775 1.776 1.776 1.775 1.776 1.775 1.776 1.775 1.776 1.775 1.776 1.775 1.776 1.775 1.776 1.775 1.776 1.775 1.776 1.775 1.776 1.775 1.777 1.775 1.776 1.775 1.776 1.775 1.776 1.775 1.776 1.775 1.776 1.775 1.776 1.775 1.776 1.775 1.776 1.775 1.776 1.775 1.777 1.775 1.777 1.777 1.777 1.777 1.777 1.777 1.777 1.777 1.777 1.777 1.777 1.777 1.777 1.7777 1.7777 1.77777 1.77777777	utlet Orifice Area = t Orifice Centroid = ctor Plate on Pipe = Cop of Freeboard = Top of Freeboard = Top of Freeboard = Cop of Freeboard = 2.00 2.426 3.44 0.2 0.0 0.2 0.0 0.4 0.2 0.0 0.4 0.2 0.0 0.4 0.2 0.0 0.4 0.2 0.0 0.4 0.2 0.0 0.4 0.6 0 0.4 0.6 0 0.4 0.6 0 0.4 0.6 0 0.4 0.6 0 0.4 0.6 0 0.4 0.6 0 0.4 0.6 0 0.4 0.6 0 0.4 0.6 0 0.4 0.6 0.6 0 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0	Zone 3 Restrictor 0.35 0.22 1.05 <u>Calculated Parame</u> 0.81 9.81 0.62 2.36 <u>Vdrographs table (0</u> 50 Year 2.25 2.934 2.934 35.4 1.40 52.5 4.6 0.1 N/A 0.8 N/A 63	Not Selected           N/A           N/A           N/A           N/A           N/A           eters for Spillway           feet           feet           acres           acre-ft           100 Year           2.52           3.607           3.607           44.3           1.75           63.9           4.6           0.1           N/A           0.8           N/A	AF). 500 Year 3.14 4.918 4.918 61.5 2.43 85.5 4.6 0.1 N/A 0.8 N/A 60
Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Routed Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = UHP Predevelopment Peak Q (cfs) = OPTIONAL Override Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, q (cfs)= Predevelopment Unit Peak Inflow Q (cfs) = Peak Inflow Q (cfs) = Peak Outflow to Predevelopment Q = Structure Controlling Flow = Max Velocity through Grate 1 (fps) = Max Velocity through Grate 1 (fps) = Time to Drain 97% of Inflow Volume (hours) = Time to Drain 97% of Inflow Volume (hours) =	4.50 Trapezoidal) 8.00 23.72 4.00 1.00 The user can over WQCV N/A 0.334 N/A N/A N/A N/A N/A N/A N/A N/A	N/A ft (relative to basin feet H:V feet EURV N/A 0.842 N/A N/A N/A N/A N/A N/A N/A Overflow Weir 1 0.04 N/A Overflow Weir 1 0.04 N/A 65 65	Inches Inches In bottom at Stage = Definition of the stage Definition of the s	Half-Centr = 0 ft) = 0 ft) = 0 ft) = 0 ft =	= 0 ft) Or Outlet ral Angle of Restrict Spillway D Stage at T Basin Area at T Basin Volume at T Basin Volume at T 1.752 1.762 1.762 1.762 1.762 1.762 1.762 1.762 1.762 1.762 1.762 1.762 1.762 1.762 1.762 1.762 1.77 0.044 31.2 4.1 0.3 Outlet Plate 1 0.7 N/A 0.7 N/A 0.7	utlet Orifice Area = t Orifice Centroid = tor Plate on Pipe = Top of Freeboard = Top of Freeboard = Top of Freeboard = Top of Freeboard = 2.00 2.426 2.427 3.5 4.4 0.2 0.0 0.12 1.12 1.12 1.12 1.03 1.12 1.03 1.12 1.03 1.12 1.03 1.12 1.03 1.12 1.03 1.12 1.03 1.12 1.03 1.12 1.03 1.12 1.03 1.12 1.03 1.12 1.03 1.12 1.03 1.12 1.03 1.12 1.03 1.12 1.03 1.12 1.03 1.12 1.03 1.03 1.03 1.03 1.03 1.03 1.03 1.03	Zone 3 Restrictor 0.35 0.22 1.05 <u>Calculated Parame</u> 0.81 9.81 0.62 2.36 <u>Vdrographs table (v</u> 50 Year 2.25 2.934 2.934 35.4 <u>1.40</u> 52.5 4.6 0.1 N/A 0.8 N/A 63 71	Not Selected           N/A           N/A           N/A           N/A           N/A           N/A           N/A           N/A           Sters for Spillway           feet           feet           acres           acre-ft           2.52           3.607           3.607           44.3           1.75           63.9           4.6           0.1           N/A           0.8           N/A           62           72	AF). 500 Year 3.14 4.918 61.5 2.43 85.5 4.6 0.1 N/A 0.8 N/A 60 73
Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length = Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Routed Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = CUHP Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, q (cfs/acre) = Peak Inflow Q (cfs) = Peak Inflow Q (cfs) = Peak Outflow to Predevelopment Q = Structure Controlling Flow = Max Velocity through Grate 1 (fps) = Max Velocity through Grate 2 (fos) = Time to Drain 97% of Inflow Volume (hours) =	4.50 Trapezoidal) 8.00 23.72 4.00 1.00 The user can over WQCV N/A 0.334 N/A N/A N/A N/A N/A N/A N/A N/A	N/A ft (relative to basin feet H:V feet EURV N/A 0.842 N/A N/A N/A N/A N/A 0.4 N/A 0.4 N/A 0.4 N/A 0.4 N/A 65	Inches Inches In bottom at Stage = HP hydrographs an 2 Year 1.19 0.828 0.828 4.0 0.16 14.7 0.2 N/A Plate N/A N/A 65	Half-Centr = 0 ft) = 0 ft) = 5 Year 1.50 1.315 1.316 1.315 1	= 0 ft) Ou Outlet ral Angle of Restrict Spillway D Stage at T Basin Area at T Basin Volume at T Basin Volume at T 1.75 1.762 1.775 1.762 1.762 1.775 1.762 1.762 1.775 1.776 1.775 1.776 1.775 1.776 1.775 1.776 1.775 1.776 1.775 1.776 1.776 1.775 1.776 1.776 1.775 1.776 1.776 1.775 1.776 1.776 1.776 1.776 1.775 1.776 1.776 1.775 1.776 1.776 1.775 1.776 1.775 1.776 1.775 1.776 1.775 1.776 1.775 1.776 1.775 1.776 1.775 1.776 1.775 1.776 1.775 1.776 1.775 1.777 1.775 1.776 1.775 1.776 1.775 1.776 1.775 1.776 1.775 1.776 1.775 1.776 1.775 1.776 1.775 1.776 1.775 1.776 1.775 1.777 1.775 1.777 1.777 1.777 1.777 1.777 1.777 1.777 1.777 1.777 1.777 1.777 1.777 1.777 1.7777 1.7777 1.77777 1.77777777	utlet Orifice Area = t Orifice Centroid = ctor Plate on Pipe = Cop of Freeboard = Top of Freeboard = Top of Freeboard = Cop of Freeboard = 2.00 2.426 3.44 0.2 0.0 0.2 0.0 0.4 0.2 0.0 0.4 0.2 0.0 0.4 0.2 0.0 0.4 0.2 0.0 0.4 0.2 0.0 0.4 0.6 0 0.4 0.6 0 0.4 0.6 0 0.4 0.6 0 0.4 0.6 0 0.4 0.6 0 0.4 0.6 0 0.4 0.6 0 0.4 0.6 0 0.4 0.6 0 0.4 0.6 0.6 0 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0	Zone 3 Restrictor 0.35 0.22 1.05 <u>Calculated Parame</u> 0.81 9.81 0.62 2.36 <u>Vdrographs table (0</u> 50 Year 2.25 2.934 2.934 35.4 1.40 52.5 4.6 0.1 N/A 0.8 N/A 63	Not Selected           N/A           N/A           N/A           N/A           N/A           eters for Spillway           feet           feet           acres           acre-ft           100 Year           2.52           3.607           3.607           44.3           1.75           63.9           4.6           0.1           N/A           0.8           N/A	AF). 500 Year 3.14 4.918 4.918 61.5 2.43 85.5 4.6 0.1 N/A 0.8 N/A 60



### DETENTION BASIN OUTLET STRUCTURE DESIGN

	The user can o	verride the calc	lated inflow by	drographs from	this workhook	with inflow hydro	ographs develor	oed in a separate	program.	
	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
ime Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [c
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.11	0.01	0.35
	0:15:00	0.00	0.00	0.94	1.55	1.93	1.30	1.63	1.60	2.30
	0:20:00	0.00	0.00	3.31 10.10	5.09 17.17	6.71 24.32	3.28 10.02	3.83 12.14	4.27 14.18	6.78 24.52
	0:30:00	0.00	0.00	10.10	24.19	31.21	36.23	44.60	51.55	71.06
	0:35:00	0.00	0.00	14.02	22.32	28.42	43.51	52.50	63.88	85.54
	0:40:00	0.00	0.00	12.28	19.07	24.39	42.25	50.54	61.11	81.34
	0:45:00	0.00	0.00	10.21	16.02	21.02	37.05	44.30	55.38	73.68
	0:50:00	0.00	0.00	8.54	13.61	17.56	33.24	39.74	49.35	65.56
	0:55:00 1:00:00	0.00	0.00	7.10	11.14	14.54	27.55	33.02	42.33	56.29
	1:05:00	0.00	0.00	6.09 5.42	9.46 8.36	12.70 11.44	22.63 19.54	27.28 23.70	36.39 32.74	48.75 44.02
	1:10:00	0.00	0.00	4.56	7.40	10.29	16.23	19.78	26.60	36.09
	1:15:00	0.00	0.00	3.78	6.26	9.17	13.39	16.39	21.23	29.15
	1:20:00	0.00	0.00	3.06	5.04	7.49	10.53	12.85	16.11	22.03
	1:25:00	0.00	0.00	2.43	3.98	5.69	8.02	9.72	11.67	15.91
	1:30:00	0.00	0.00	1.95	3.27	4.54	5.61	6.78	7.95	11.07
	1:35:00 1:40:00	0.00	0.00	1.69 1.58	2.93 2.50	3.89 3.46	4.16 3.30	5.11 4.09	5.78 4.51	8.20 6.45
	1:45:00	0.00	0.00	1.58	2.50	3.46	2.76	3.43	3.62	5.22
	1:50:00	0.00	0.00	1.48	1.95	2.95	2.39	2.98	3.00	4.37
	1:55:00	0.00	0.00	1.29	1.77	2.70	2.16	2.70	2.58	3.77
	2:00:00	0.00	0.00	1.13	1.60	2.33	2.00	2.50	2.28	3.35
	2:05:00	0.00	0.00	0.86	1.20	1.74	1.48	1.85	1.64	2.41
	2:10:00	0.00	0.00	0.64	0.88	1.26	1.08	1.34	1.19	1.74
	2:15:00 2:20:00	0.00	0.00	0.48	0.65	0.90	0.78	0.97	0.87	1.26 0.93
	2:25:00	0.00	0.00	0.35	0.47	0.65	0.57	0.70	0.64	0.93
	2:30:00	0.00	0.00	0.18	0.23	0.33	0.29	0.35	0.32	0.47
	2:35:00	0.00	0.00	0.13	0.16	0.23	0.20	0.25	0.23	0.33
	2:40:00	0.00	0.00	0.08	0.10	0.15	0.14	0.17	0.15	0.22
	2:45:00	0.00	0.00	0.05	0.06	0.09	0.08	0.10	0.09	0.13
	2:50:00	0.00	0.00	0.02	0.03	0.04	0.04	0.05	0.05	0.06
	2:55:00 3:00:00	0.00	0.00	0.01	0.01	0.01	0.02	0.02	0.01	0.02
	3:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:35:00 3:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:10:00 4:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:30:00 4:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:50:00 4:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:10:00 5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:30:00 5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:50:00 5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

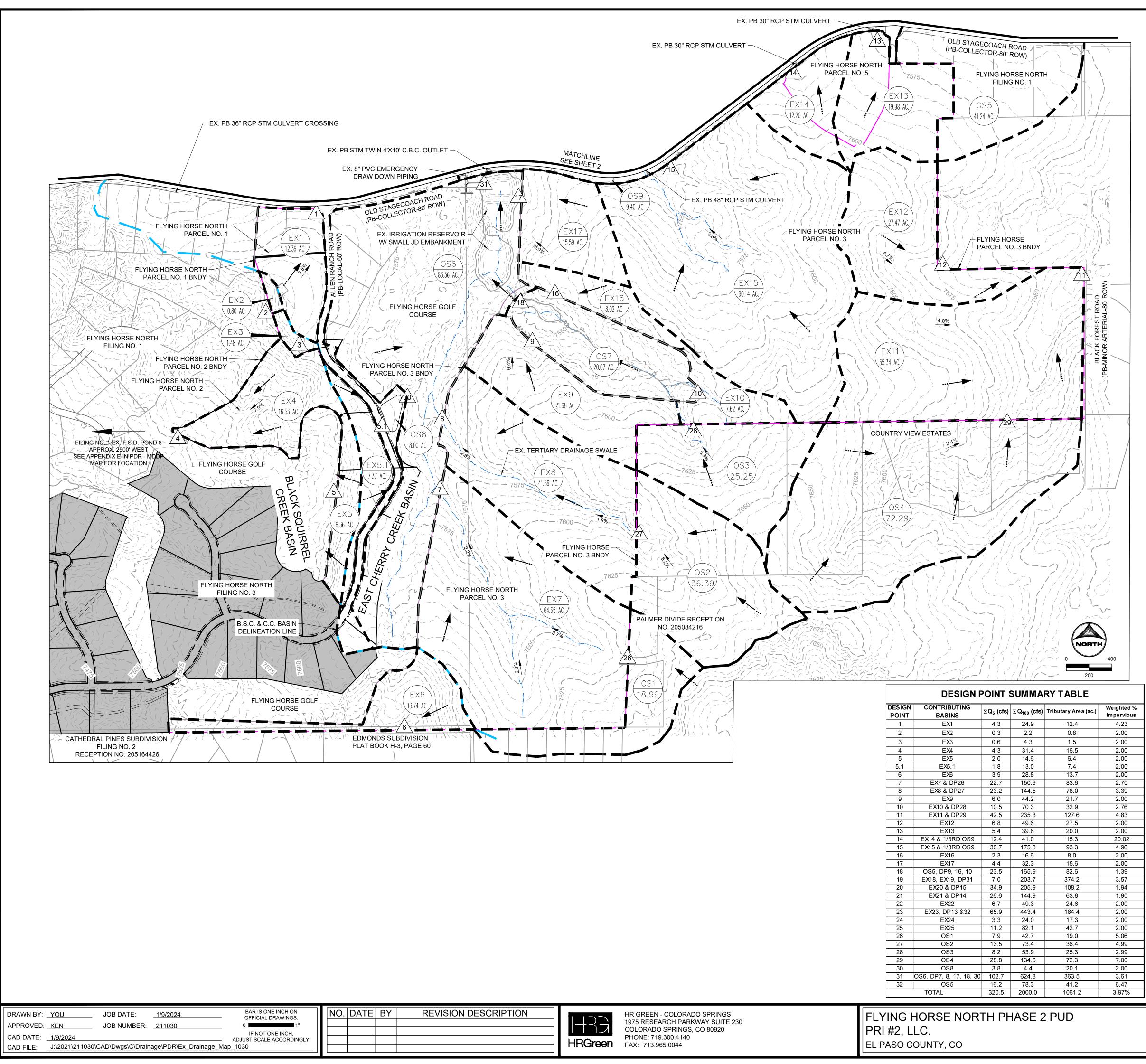


Flying Horse North Phase 2 Parcels 1-6 Preliminary Drainage Report Project No.: 211030

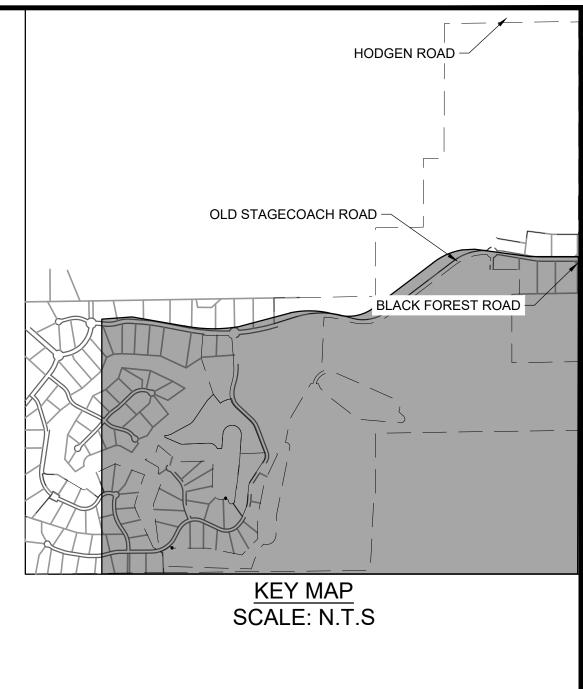
Appendix F:

Drainage Maps





RY TABLE				
Tributary Area (ac.)	Weighted % Impervious			
12.4	4.23			
0.8	2.00			
1.5	2.00			
16.5	2.00			
6.4	2.00			
7.4	2.00			
13.7	2.00			
83.6	2.70			
78.0	3.39			
21.7	2.00			
32.9	2.76			
127.6	4.83			
27.5	2.00			
20.0	2.00			
15.3	20.02			
93.3	4.96			
8.0	2.00			
15.6	2.00			
82.6	1.39			
374.2	3.57			
108.2	1.94			
63.8	1.90			
24.6	2.00			
184.4	2.00			
17.3	2.00			
42.7	2.00			
19.0	5.06			
36.4	4.99			
25.3	2.99			
72.3	7.00			
20.1	2.00			
363.5	3.61			
41.2	6.47			
1061.2	3.97%			



-----

X

BASIN DESIGNATION

AREA (AC.)

11

1.25

# LEGEND

EXISTING MAJOR CONTOUR **EXISTING MINOR CONTOUR** EXISTING TERTIARY DRAINAGE WAY **EXISTING STORM INFRASTRUCTURE** PROPOSED PARCEL BOUNDARY **BASIN BOUNDARY B.S.C. - C.C. BASIN DELINEATION** 

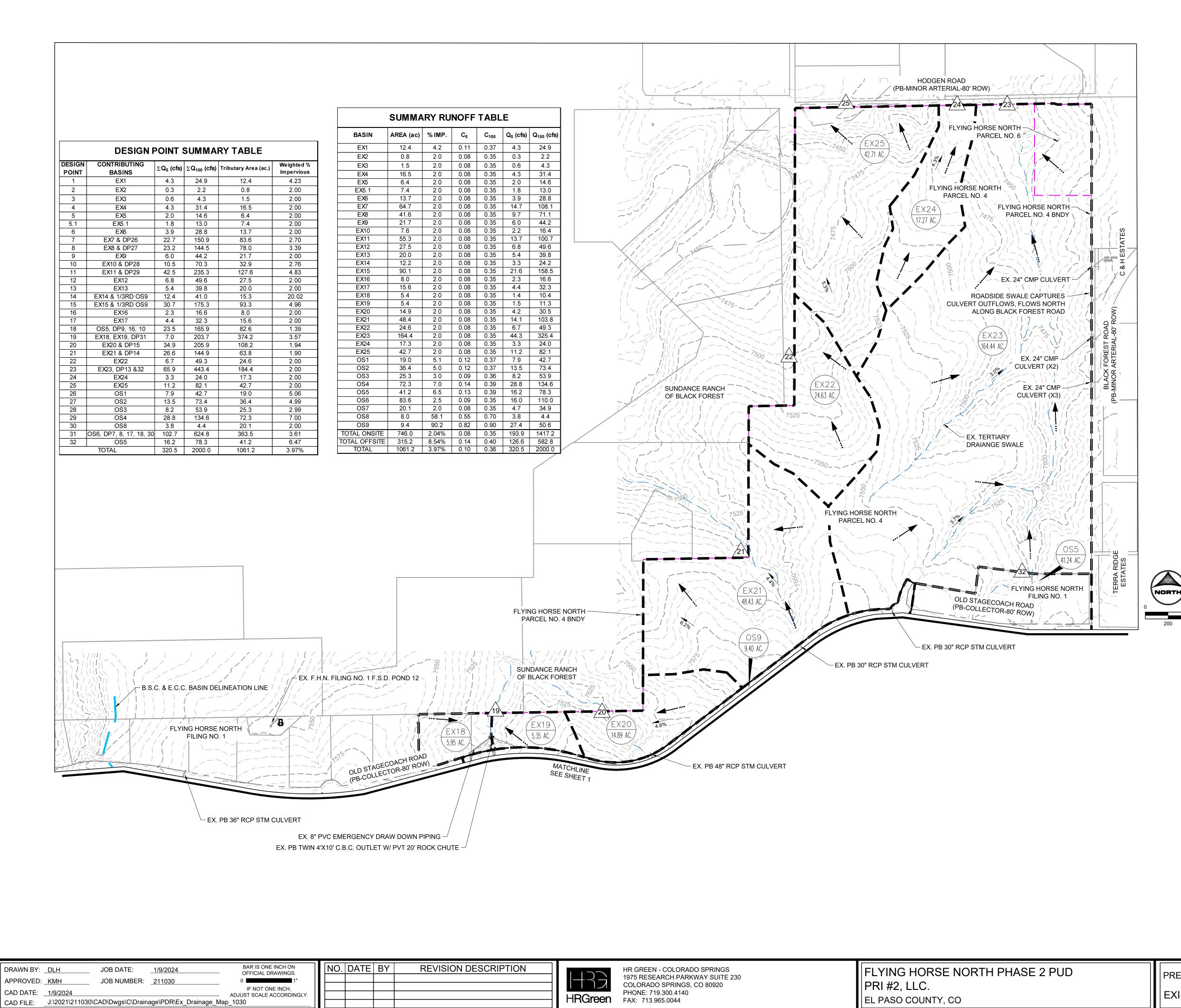
**EXISTING FLOW DIRECTION DESIGN POINT** 

EXISTING BASIN LABEL

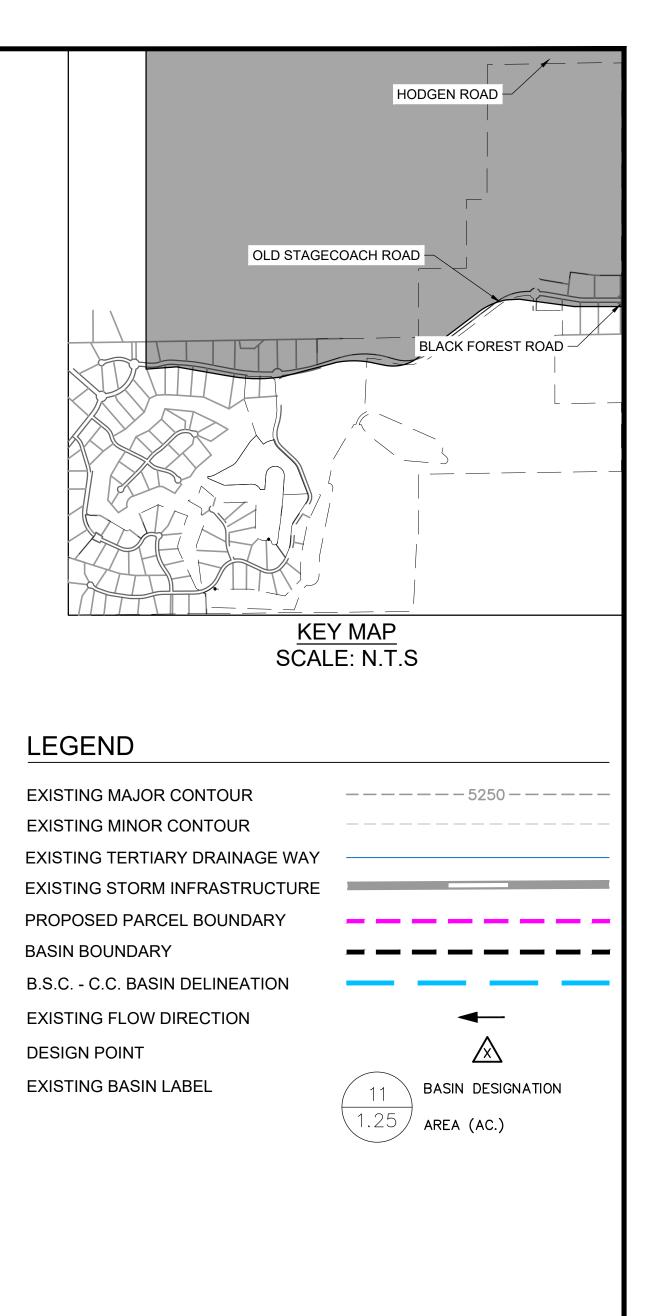
SUMMARY RUNOFF TABLE						
BASIN	AREA (ac)	% IMP.	C <sub>5</sub>	C <sub>100</sub>	Q <sub>5</sub> (cfs)	Q <sub>100</sub> (cfs)
EX1	12.4	4.2	0.11	0.37	4.3	24.9
EX2	0.8	2.0	0.08	0.35	0.3	2.2
EX3	1.5	2.0	0.08	0.35	0.6	4.3
EX4	16.5	2.0	0.08	0.35	4.3	31.4
EX5	6.4	2.0	0.08	0.35	2.0	14.6
EX5.1	7.4	2.0	0.08	0.35	1.8	13.0
EX6	13.7	2.0	0.08	0.35	3.9	28.8
EX7	64.7	2.0	0.08	0.35	14.7	108.1
EX8	41.6	2.0	0.08	0.35	9.7	71.1
EX9	21.7	2.0	0.08	0.35	6.0	44.2
EX10	7.6	2.0	0.08	0.35	2.2	16.4
EX11	55.3	2.0	0.08	0.35	13.7	100.7
EX12	27.5	2.0	0.08	0.35	6.8	49.6
EX13	20.0	2.0	0.08	0.35	5.4	39.8
EX14	12.2	2.0	0.08	0.35	3.3	24.2
EX15	90.1	2.0	0.08	0.35	21.6	158.5
EX16	8.0	2.0	0.08	0.35	2.3	16.6
EX17	15.6	2.0	0.08	0.35	4.4	32.3
EX18	5.4	2.0	0.08	0.35	1.4	10.4
EX19	5.4	2.0	0.08	0.35	1.5	11.3
EX20	14.9	2.0	0.08	0.35	4.2	30.5
EX21	48.4	2.0	0.08	0.35	14.1	103.8
EX22	24.6	2.0	0.08	0.35	6.7	49.3
EX23	164.4	2.0	0.08	0.35	44.3	325.4
EX24	17.3	2.0	0.08	0.35	3.3	24.0
EX25	42.7	2.0	0.08	0.35	11.2	82.1
OS1	19.0	5.1	0.12	0.37	7.9	42.7
OS2	36.4	5.0	0.12	0.37	13.5	73.4
OS3	25.3	3.0	0.09	0.36	8.2	53.9
OS4	72.3	7.0	0.14	0.39	28.8	134.6
OS5	41.2	6.5	0.13	0.39	16.2	78.3
OS6	83.6	2.5	0.09	0.35	16.0	110.0
OS7	20.1	2.0	0.08	0.35	4.7	34.9
OS8	8.0	58.1	0.55	0.70	3.8	4.4
OS9	9.4	90.2	0.82	0.90	27.4	50.6
TOTAL ONSITE	746.0	2.04%	0.08	0.35	193.9	1417.2
TOTAL OFFSITE	315.2	8.54%	0.14	0.40	126.6	582.8
TOTAL	1061.2	3.97%	0.10	0.36	320.5	2000.0

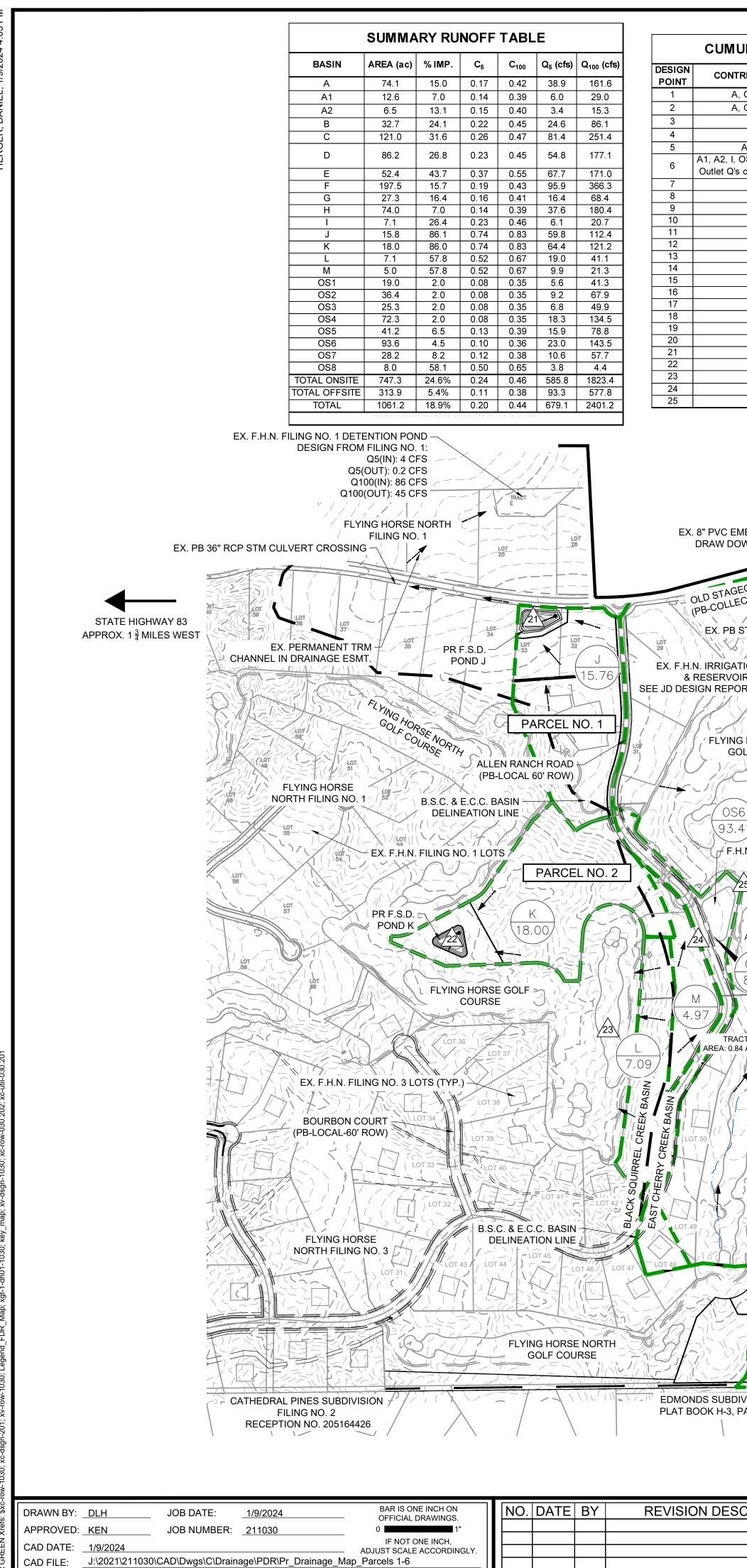
PCD FILE NO.: PUDSP234

SHEET ΕX



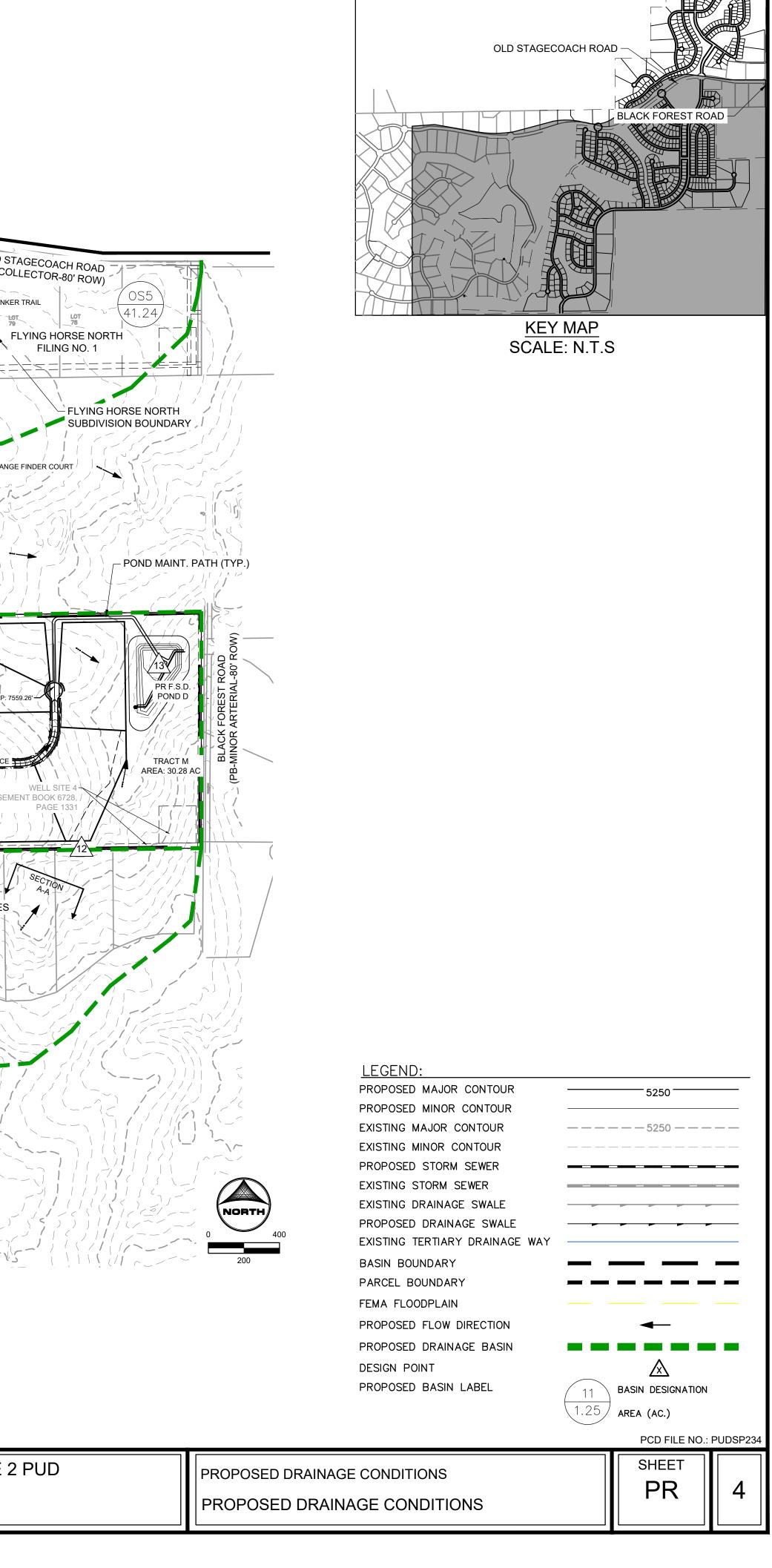
				PCD FILE NO.: P	PUDSP
CRIPTION	HR GREEN - COLORADO SPRINGS 1975 RESEARCH PARKWAY SUITE 230 COLORADO SPRINGS, CO 80920 PHONE: 719.300.4140 FAX: 713.965.0044	FLYING HORSE NORTH PHASE 2 PUD PRI #2, LLC. EL PASO COUNTY, CO	PRELIMINARY DRAINAGE REPORT EXISTING CONDITIONS	SHEET EX	2





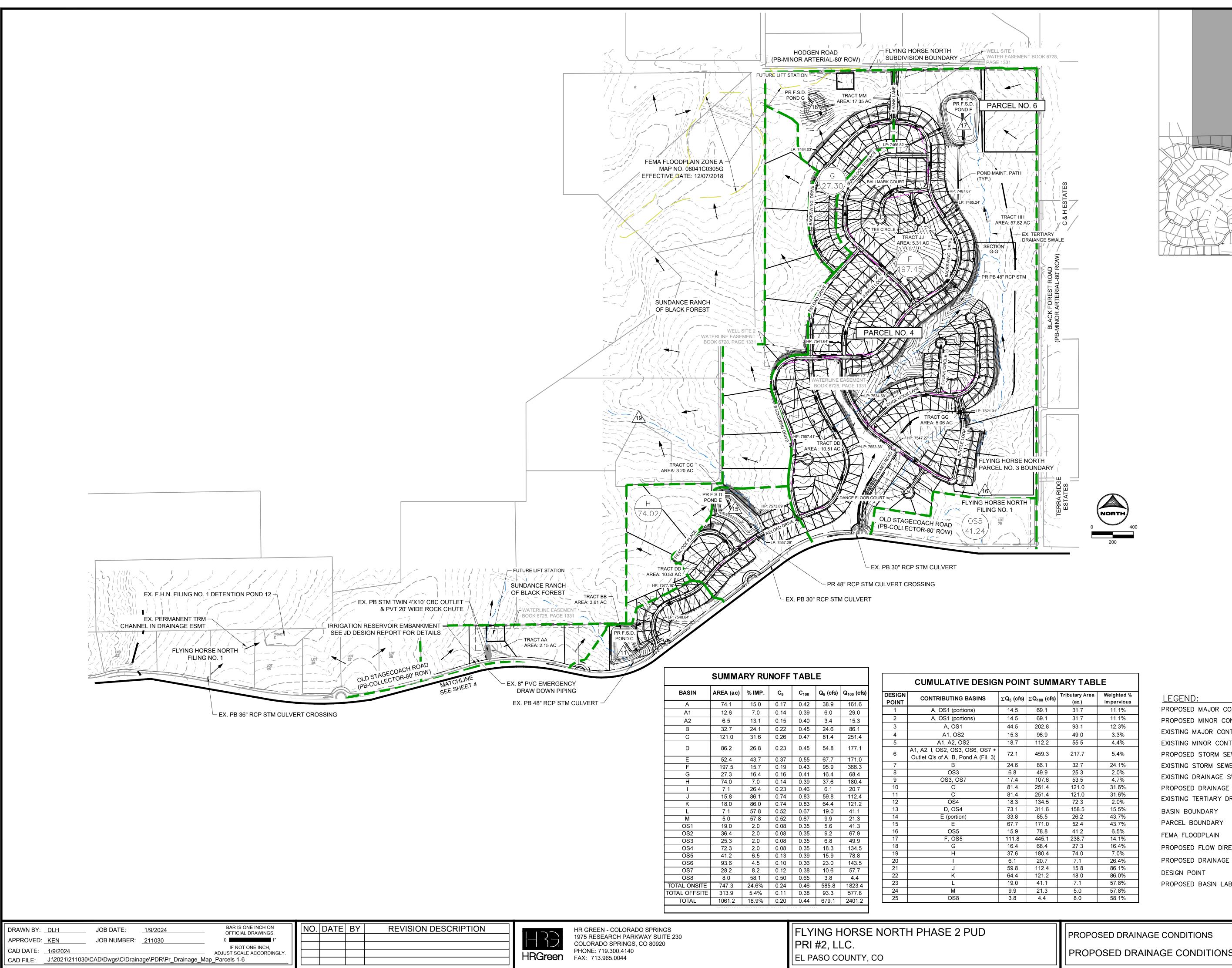
JMULATIVE DESIG						
		$\Sigma \mathbf{Q}_{100}$ (CTS)	Tributary Area (ac.)	Impervious		
A, OS1 (portions) A, OS1 (portions)	14.5 14.5	69.1 69.1	31.7 31.7	11.1% 11.1%		
A, OS1 A1, OS2	44.5 15.3	202.8 96.9	93.1 49.0	12.3% 3.3%		
A1, A2, OS2 2, I, OS2, OS3, OS6, OS7 +	18.7 72.1	112.2 459.3	55.5 217.7	4.4% 5.4%		
et Q's of A, B, Pond A (Fil. 3) B	24.6	86.1	32.7	24.1%		
OS3 OS3, OS7 C	6.8 17.4 81.4	49.9 107.6 251.4	25.3 53.5 121.0	2.0% 4.7% 31.6%		
C OS4	81.4 18.3	251.4 251.4 134.5	121.0 121.0 72.3	31.6% 2.0%		
D, OS4 E (portion)	73.1 33.8	311.6 85.5	158.5 26.2	15.5% 43.7%		
E OS5	67.7 15.9	171.0 78.8	52.4 41.2	43.7% 6.5%		
F, OS5 G	111.8 16.4	445.1 68.4	238.7 27.3	14.1% 16.4%		3 30" RCP – CULVERT
H I J	37.6 6.1 59.8	180.4 20.7 112.4	74.0 7.1 15.8	7.0% 26.4% 86.1%	EX. PB 30" RCP —	
	64.4 19.0	112.4 121.2 41.1	18.0 7.1	86.0% 57.8%	STM CULVERT	OLD STA
M OS8	9.9 3.8	21.3 4.4	5.0	57.8% 58.1%		
						52.36
					PAR	CEL NO. 5
			EX. PB 48" R	CP STM CULVE		
					PLACE HP: 7593.26	
			MATCHLINE SEE SHEET	E	PUTER PLACE CHAME HP: 7593.26	HP: 7604.15
V DOWN PIPING	V-A			5		
TAGECOACH ROAD						HP: 7610.81' HP: 7610.81'
TAGECOACH ROAD DLLECTOR-80' ROW)					PAR COURT	
PB STM TWIN 4'X10' CBC -			7.13		таст т 121.03	
				LP: 7560		
RVOIR EMBANKMENT				KHS		
1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1				HE	PARCEL NO. 3	LP: 7584.84'
YING HORSE NORTH		9		GRAND SLAM CIRCLE	HP: 7592.41"	LP: 7599.91' LP: 7606.05' LP: 7603.69'
GOLF COURSE		R-A		CIRCLE	ACE CIRCLE	
	PR F.S POND		ACT K EA: 3.17 AC			LP: 7559
OS6	7			OS7		83.16
93.41 F.H.N. FILING 3 POND A	7563.61		Sa Charles	28.22		WATERLINE EASEMENT
			CGEP C		HORSE NORTH F COURSE	
	B 32.69		LONG IRON PLA		LP: 7607.10'- HP: 7608.20'-	
			A A		HOLMES ROAD	
TRACT H AREA: 0.95 AC		HP: 7604.			7598.91' SECTION PR 48" RCP CULVERT-01, SUI	FLYING HORSE NORTH BDIVISION BOUNDARY
		EX. TER	LIARY DRAIN	AGE SWALE	CROSSING (PB)	COUNTRY VIEW ESTATES
HP: 7578.54	No to		R WAY	AREA: 3.89 AC		
				HP: 7611.36	$\frac{OS3}{25.25}$	
TRACT E A: 0.84 AC P: 7576.03	RINGE STREE		: 7607.75'		PR 48" RCP CULVERT-02 CROSSING (PB)	OS4
L / L / L / T T P P F	S.D.			A1 (12.58)		72.29
	F			7610.28'		
				HACKER LÓOP		
1-11	E-E.				OS2 36.39	
	74	1			PALMER DIVIDE RECEPTION	
	AR	TRACT C EA: 13.06 AC			NO. 205084216	
	ANDBAG	HP: 761	7622.06	25	- PR 48" RCP CULVERT-03 - CROSSING (PB)	
	GER DR		Z MK			
			AREA: 3	0.28 AC	OS1 17 11 11 11 11 11 11 11 11 11 11 11 11	
TRACT B AREA: 7.71 AC	HP 7	632.93'	R 48" RCP CI	JLVERT-04		
			ROSSING (P	B) _ /		
UBDIVISION 1-3, PAGE 60			YING HORSE BDIVISION B			

RIPTION		HR GREEN - COLORADO SPRINGS 1975 RESEARCH PARKWAY SUITE 230	FLYING HORSE NORTH PHASE
	HRGreen	PHONE: 719.300.4140	
		FAX: 713.965.0044	EL PASO COUNTY, CO



HODGEN ROAD





/E DESIGN POINT SUMMARY TABLE					
G BASINS	$\Sigma Q_5$ (cfs)	$\Sigma Q_{100}$ (cfs)	Tributary Area (ac.)	Weighted % Impervious	
rtions)	14.5	69.1	31.7	11.1%	
rtions)	14.5	69.1	31.7	11.1%	
1	44.5	202.8	93.1	12.3%	
52	15.3	96.9	49.0	3.3%	
DS2	18.7	112.2	55.5	4.4%	
3, OS6, OS7 + Pond A (Fil. 3)	72.1	459.3	217.7	5.4%	
	24.6	86.1	32.7	24.1%	
	6.8	49.9	25.3	2.0%	
S7	17.4	107.6	53.5	4.7%	
	81.4	251.4	121.0	31.6%	
	81.4	251.4	121.0	31.6%	
	18.3	134.5	72.3	2.0%	
4	73.1	311.6	158.5	15.5%	
on)	33.8	85.5	26.2	43.7%	
	67.7	171.0	52.4	43.7%	
	15.9	78.8	41.2	6.5%	
5	111.8	445.1	238.7	14.1%	
	16.4	68.4	27.3	16.4%	
	37.6	180.4	74.0	7.0%	
	6.1	20.7	7.1	26.4%	
	59.8	112.4	15.8	86.1%	
	64.4	121.2	18.0	86.0%	
	19.0	41.1	7.1	57.8%	
	9.9	21.3	5.0	57.8%	
	3.8	4.4	8.0	58.1%	

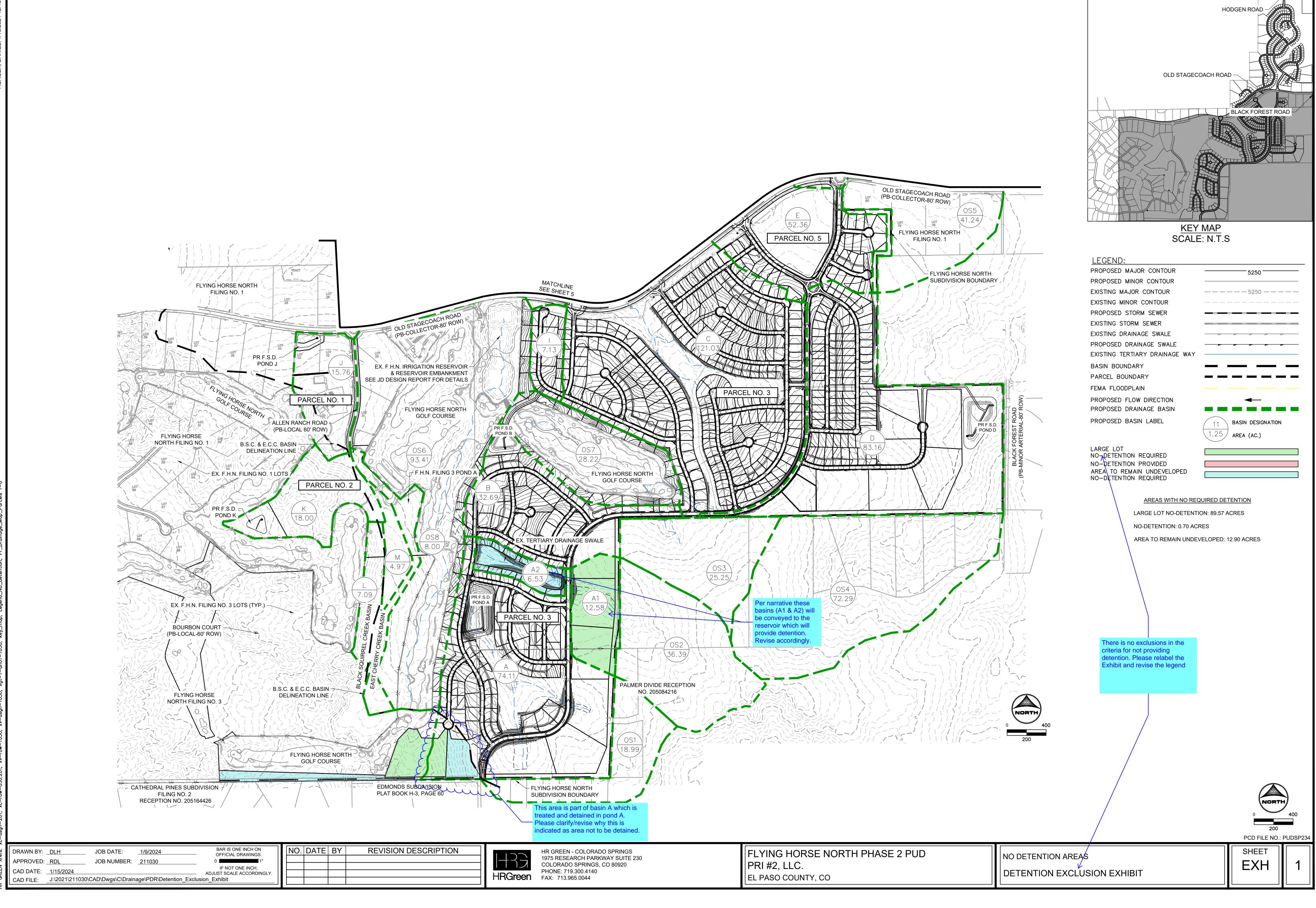
ghted % ervious	LEGEND:			
1.1%	PROPOSED MAJOR CONTOUR		5250	
1.1%	PROPOSED MINOR CONTOUR			
2.3%	EXISTING MAJOR CONTOUR		5250	
3.3%			5250	
4.4%	EXISTING MINOR CONTOUR			
5.4%	PROPOSED STORM SEWER			
4.1%	EXISTING STORM SEWER			_
2.0% 4.7%	EXISTING DRAINAGE SWALE			
4.7% 1.6%	PROPOSED DRAINAGE SWALE			
1.6%				
2.0%	EXISTING TERTIARY DRAINAGE WAY			
5.5%	BASIN BOUNDARY			
3.7%	PARCEL BOUNDARY	_		
3.7% 6.5%	TARGEL BOONDART			
4.1%	FEMA FLOODPLAIN			
6.4%	PROPOSED FLOW DIRECTION		◄	
7.0% 6.4%	PROPOSED DRAINAGE BASIN	-		
6.1% 6.0%	DESIGN POINT		$\wedge$	
7.8%	PROPOSED BASIN LABEL		BASIN DESIGNATION	
7.8%		$\begin{pmatrix} 11 \end{pmatrix}$	BASIN BESIGNATION	
8.1%		1.25	AREA (AC.)	
			PCD FILE NO.:	PUDSP234
			SHEET	
DRAINA	GE CONDITIONS			
D DRAI	NAGE CONDITIONS		PR	5

HODGEN ROAD

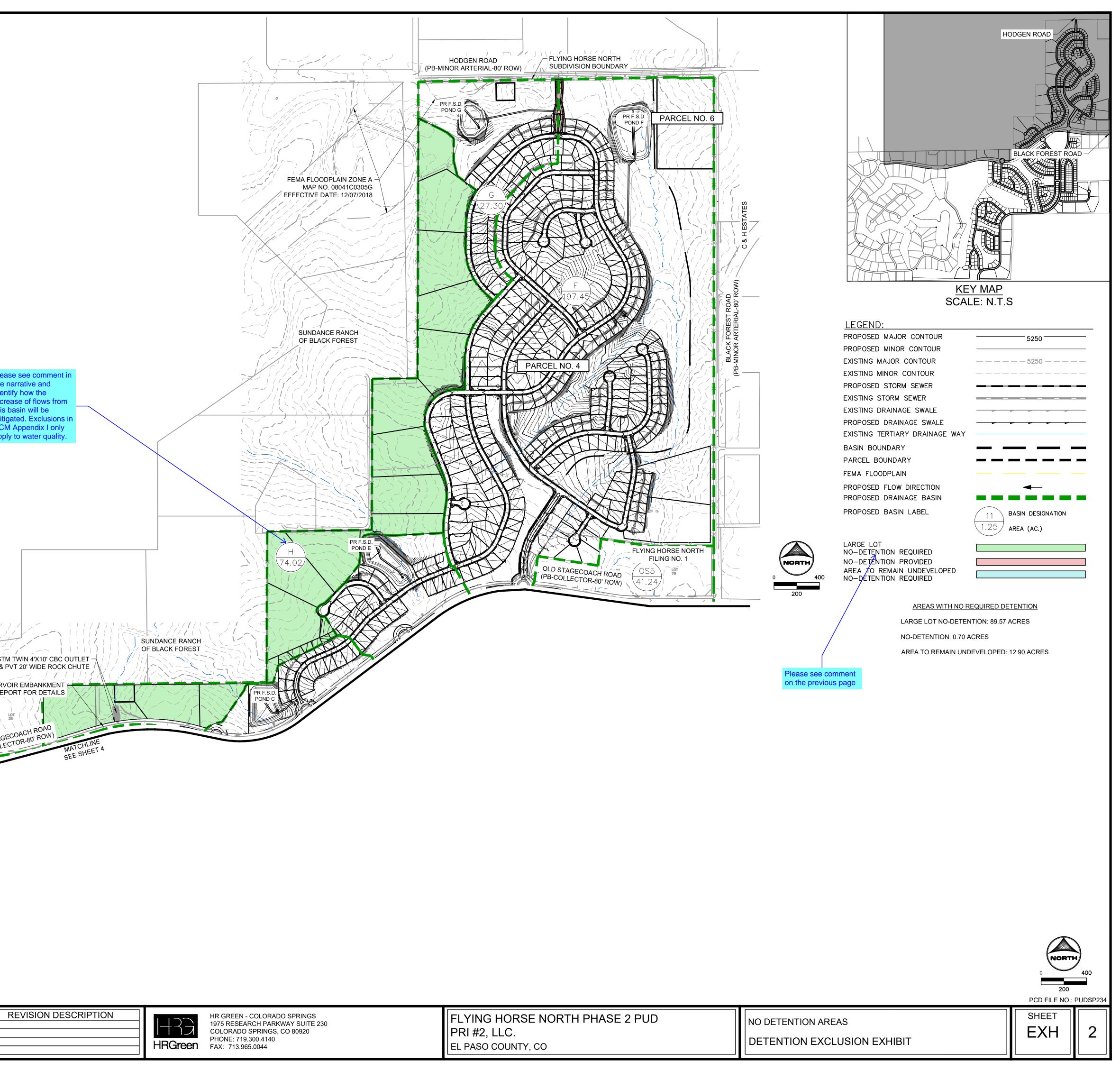
BLACK FOREST ROAD -

OLD STAGECOACH ROAD

KEY MAP SCALE: N.T.S







COLORADO SPRINGS, CO 80920 PHONE: 719.300.4140	ELYING HORSE NORTH PHASE 2 PUE PRI #2, LLC. EL PASO COUNTY, CO
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