



Flying Horse North – Phase 2 PUD Parcels 1-6 Preliminary Drainage Report

January 2024

Prepared For:

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Engineer's Statement

This report and plan for the drainage design of the development, Flying Horse North, was prepared by me (or under my direct supervision) and is correct to the best of my knowledge and belief. Said report and plan has been prepared in accordance with the *El Paso County Drainage Criteria* Manual and is in conformity with the master plan of the drainage basin. I understand that El Paso County does not and will not assume liability for drainage facilities designed by others. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.

Richie Lyon, PE	Date	
State of Colorado No.	53921	
For and on behalf of H	HR Green Development, LLC	
Developer's	Statement	
I, the developer, have	read and will comply with al	of the requirements specified in this drainage report and pla
Flying Horse Develop	ment, LLC	
Drew Balsick	 Date	
Vice President / Proje		
Flying Horse Develop		
Colorado Springs, CO	80921	
El Paso Co	unty:	
	rith the requirements of the End 2 and the Engineering Cri	Paso County Land Development Code, Drainage Criteria ria Manual, as amended.
Joshua Palmer, P.E.		Date
County Engineer/ECM	/I Administrator	



I. General Purpose, Location and Description

Purpose and Scope

The Purpose of this Preliminary Drainage Report (PDR) is to identify specific solutions to drainage concerns on site and off-site resulting from the development of the subdivision to be platted as well as any drainage issues that exist prior to development. The PDR is to describe the onsite and offsite drainage patterns, quantify stormwater runoff and detention volumes, assess existing and proposed storm infrastructure as it relates to preliminary water quality and stormwater detention, describe areas tributary to the site and the planned storm water management for the Flying Horse North Parcels 1-6 development. Flying Horse North, (F.H.N.) Filing No. 1 combined Preliminary Drainage Report (PDR) and Final Drainage Report (FDR) was previously developed by Classic Consulting Engineers and Surveyors and included in Appendix F and a more recent Master Development Drainage Plan (MDDP) was prepared by HR Green Development, LLC. and was approved by the County in September of 2022, entitled *Flying Horse North Master Development Drainage Plan* latest revision date of September 9, 2022. A Final Drainage Report for Flying Horse North Filing No. 3 developed by HR Green Development, LLC. is currently in process with the County for a final plat application for Filing No. 3.

The items discussed in this report are preliminary in nature and final drainage calculations and design will be required in a future Final Drainage Report (FDR) as design development proceeds including delineation of sub-basins per roadway plan and profiles and overlot grading, design of public and private storm systems and outfalls, and final permanent control measure design. This PDR provides the drainage concept and guidance for future development of Flying Horse North Parcels 1-6 by analyzing the major basins, off-site stormwater runoff, water quality and full spectrum extended detention basins, and outfall locations to demonstrate compliance with drainage criteria and the Master Plan for the Flying Horse North subdivision. The extent of hydraulic analysis for this PDR is described further in its own section.

Project Location and Description

The Flying Horse North subdivision is in El Paso County. The larger subdivision development is bordered by Highway 83 to the west, Black Forest Road to the east, Cathedral Pines to the south, and High Forest Ranch to the north. The area contains approximately 1,473.6 acres within the whole Section 36, Township 11 South, Range 66 West of the Sixth Principal Meridian, and a portion of Section 30 and 31, Township 11 South, and Range 65 West of the Sixth Principal Meridian.

The Flying Horse North Parcels 1-6 area is the proposed PUD within the greater Flying Horse North subdivision that is approximately 747.27 acres that are currently unplatted parcels within the greater Flying Horse North subdivision. The subdivision is surrounded by the Flying Horse North Golf Course, the Cathedral Pines and Palmer Divide subdivisions to the south, residential subdivisions north of Hodgen Road such as Lesley Subdivision and High Plains Subdivision, and unplatted RR-5 zoned residential parcels to the northwest and east.

Review C1: A floodplain statement shall be provided indicating whether any portion of the development is in a designated floodplain as delineated on the current FEMA mapping.

Review C2: Unresolved. Please address the comment because a portion of site is within the floodplain.



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4

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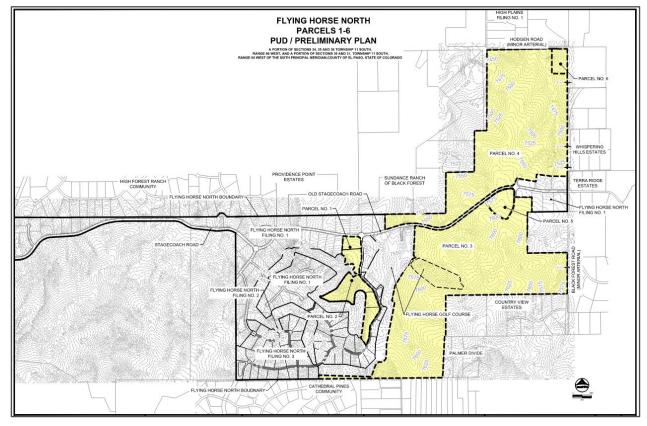


Figure 1: Site Map

A full sheet vicinity map is provided in Appendix A for a clear visual of Parcels 1 though 6 and adjacent developments.

This PDR will assess the drainage conditions for the 747.3 acres of onsite proposed PUD development, additional Flying Horse North acreage from other tributary filings and off-site tributary areas. The proposed PUD Preliminary Plan includes 796 proposed single-family residential units of various lot sizes. The PUD includes rural single-family estate lots of 2.5 and 5.0 acres, more dense single-family residential lots from 1/8-acre to 1/4-acre in size, commercial development, an 18-acre hotel and resort site with residential casitas, a 15-acre multifamily Flats area, open space and park areas, fitness center and a clubhouse.

The following table is a breakdown of the proposed land uses for the PUD Preliminary Plan Parcels 1-6, by Parcel.

PROPOSED Parcel No. Land Use(s) DU/AC Commercial Golf Course Clubhouse 1 N/A 2 Commercial Hotel & Resort, Residential Casitas, Multi-

Table 1: Land Use by Parcel Number



The following table is a breakdown of the various proposed lot sizes for the single-family parcels within the PUD Preliminary Plan Parcels 1-6, by lot size:

	O	,	
Lot Size	Typical Minimum Dimensions	No. of Proposed Parcels	Total Area (ac.)
1/8-acre	75'x130'	123	45.2
1/4-acre	85'x130' ; 100'x130'	432 ; 94	130.33
1/3-acre	140'x130'	74	36.6
1/2-acre	160'x145'	43	51.4
1-acre	-	0	0.0
2.5-acre Rural	-	6	20.22
5.0-acre Rural	-	24	121.36
TOTALS		796	405 11

Table 2: Single-Family Lot Size Summary

Parcel 2 consists of the Commercial Hotel & Resort as well as the Casitas and multi-family Flats development areas. The anticipated number of hotel and casitas keys (units) is 225, and the preliminarily sited number of Flats is 50 units (6 units per building), totaling 275 units. This brings the total number of units for the entire PUD Preliminary Plan to 1,024. Excluding the hotel keys, the total amount of dwelling units comes out to 896, with 100 of those being responsible for the casitas and flats. The total weighted imperviousness of the PUD is approximately 27% for the fully developed conditions of all parcels.

Existing Conditions Description

The existing ground cover consists of native grass and shrubbery with areas of barren pervious soil. The parcel 1 and 2 areas to the west where the proposed hotel resort, casitas, and flats are to be developed consist of the same native grass with areas of dense tree cover with pinyon pines, mostly in the areas adjacent to the golf course property. Slopes within this area generally range from 2 to 20 percent and flow west to east within East Cherry Creek Basin and east to west within Black Squirrel Creek Basin. These parcels are split by the Black Squirrel Creek and East Cherry Creek basin delineation line, with a majority of parcel 1 flowing east into East Cherry Creek. A majority of the area defined by parcel 2 flows west into Black Squirrel Creek. The remaining portion of parcel 2 that flows east into East Cherry Creek Basin is captured in an adjacent section of Allen Ranch Road that will be developed as F.H.N. Filing No. 3 is concurrently in review. The captured run-off is detained in F.H.N. Filing 3 pond A and ultimately released into an existing tertiary drainage swale located in a tract of the Flying Horse Golf Course. The natural vegetation has been documented by survey and aerial photography.

Parcels 3 through 6 are separated from the first two parcels by a stretch of golf course that runs south to north from the southern property border up to the existing Old Stagecoach Road. These parcels also consist of native grasses and shrubbery with areas of barren pervious soil. Slopes within this area generally range from 1 to 15 percent and generally flow from south to north. The natural vegetation has been documented by survey and aerial photography. Adjacent subdivisions in Palmer Divide and Country View Estates consist of 5 acre lots and make up a majority of the off-site flows. Flows from these off-site basins drain directly into existing drainage swales located in parcel no. 3. Black Forest Road which runs North to South along the eastern edge of parcels 3, 4, and 6, has 3 corrugated metal pipe culvert crossings that allow runoff to flow from east to west into parcel 4. Additionally, parcel no. 4 has 3 concrete culverts of varying size that





allow flows from parcel 3 to drain north into parcel 4, past the existing stretch of Old Stagecoach Road that separates the two aforementioned parcels.

All existing sub-basins within the site as well as existing off-site basins have associated design points, all of which are described in a further section. An existing drainage conditions map can be found within the appendix.

There are no existing major drainageways such as formal channels or water ways. There are existing natural tertiary swales and channels throughout the parcels that convey stormwater and are addressed in this PDR for the developed conditions. There are no existing stormwater facilities within the proposed PUD parcels. Adjacent filings that are developed such as the golf course, Filing No. 1, and the concurrent review of Filing No. 3 have public and private storm infrastructure such as storm sewer main, inlets, and detention basins. There are no existing irrigation facilities within the PUD parcels. There are existing irrigation facilities within the adjacent existing golf course property. Existing minor drainage channels within the site are planned to be maintained to the maximum extent possible as a part of parkways and greenways with the development. These will continue to be used for conveyance of storm drainage flows.

The Franktown Parker Dam (080130) is located near the northwest corner of site. The dam is designated as a jurisdictional dam and has a low hazard class. It is located along East Cherry Creek. See Appendix A for characteristics and location of dam.

Drainageways of note including grass-lined swales and emergency overflow Tracts are described within this report with preliminary parameters to demonstrate compliance with swale design criteria and capacities.

The soils that existing within the PUD boundaries include the following:

- Brussett loam hydrologic soils group B.
- Elbeth sandy loam hydrologic soils group B.
- Kettle gravelly loamy sand hydrologic soils group B.
- Peyton sandy loam hydrologic soils group B.
- Peyton-Pring complex hydrologic soils group B.
- Pring coarse sandy loam hydrologic soils group B.

Per the NRCS web soil survey, the site is made up entirely of Type B soils. The ridge line between the Arkansas River and South Platte River Basins creates different soil environments for each. The portion of site that is within the Black Squirrel Drainage Basin, which includes Flying Horse Norse Filing No. 2 and No. 3, are predominately Elbeth sandy loam. The remaining filings are within the East Cherry Creek Basin which consists of Peyton sandy loam and Peyton-Pring complex. See Appendix A for the NRCS soil map.

The property for the PUD Parcels 1-6 do not consist of any existing utilities such as potable water main, wastewater main, natural gas facilities, or electric facilities. There are no encumbrances by utilities including platted easements that contain facilities for removal or relocation. Platted easements and other legal items are shown on the PUD Preliminary Plan set drawings.



II. Drainage Basins and Sub-Basins

Drainage Basin Information

Flying Horse North is located within both the Black Squirrel Drainage Basin and East Cherry Creek Basin. Predominantly, the existing Filing No.1 and part of the proposed Filing No.2 is located within the Black Squirrel Drainage Basin. This drainage basin encompasses 10.9 square miles of mostly forested area and generally slopes from east to west and outfalls into Monument Creek. Black Squirrel is a sub-basin of the Arkansas River. The remaining filings and part of Filing No. 2 is located within the East Cherry Creek Basin. There is not a current planning study of the drainage basin, but generally it slopes from southwest to northeast. The basin eventually flows into the South Platte River.

As the site generally lies at the top of each of the respective basins, minimal offsite flows are conveyed onto the site. The Black Squirrel Creek Drainage basin has no offsite flow come onto the site sans those flows generated as part of Filing 1 of F.H.N.. The development which is within the Black Squirrel Creek Drainage Basin is unchanged from the FDR shown in Filing 1.

DBPS Investigations

Flying Horse North is split by the Arkansas River Basin and South Platte Basin. Within each of those river basins, the site stretches across the Black Squirrel Basin and East Cherry Creek Drainage Basins.

The Black Squirrel Drainage Basin Planning Study (DBPS) Preliminary Design Report prepared by URS Corporation was reviewed to determine existing plans and constraints that would influence the design of the F.H.N. Development. The proposed plans for F.H.N. are in general conformance with the DBPS.

Flying Horse North Parcels 1-6 is located within a major portion of the East Cherry Creek Drainage Basin to the east of the larger F.H.N. subdivision and the west portion of the site is within the Black Squirrel Creek Drainage Basin. A MDDP developed by HR Green Development, LLC. that includes the proposed Parcels 1-6 area was approved by the County in September of 2022 and it is the intent of this PDR to follow the general drainage approach for this area where densities for the development will remain similar to the report.

For the portion of F.H.N. which lies within the East Cherry Creek Drainage Basin, a DBPS does not currently exist and the MDDP will comply with standard El Paso County regulations regarding drainage within this corridor.

Compliance with DBPS

This PDR is in general conformance with the guidelines outlined in the Black Squirrel DBPS and current drainage flows of the East Cherry Creek Basin. Flying Horse North will construct multiple full spectrum detention facilities to limit the effects of development and mimic natural flow patterns.

Existing downstream infrastructure is currently limited to the historic drainage channels and minimal downstream improvements exist. As such, the site follows the DBPS and restricts offsite flow rates to not exceed historic flow rates. The site's ultimate outfalls will generally be along the same historic tributaries. Although outfall rates will be at or below historic, the cumulative volume of runoff will increase and therefore downstream facilities may see an increase in the duration of flows. This may provide a net benefit to the downstream facilities by providing more water to assist with the sustenance of vegetation. However, it should be noted that increased volume may expedite potential erosion or channel movement.



III. Hydrologic Analysis

Existing Major Basin Descriptions

Design Point 1 (Q₅**=4.3 CFS, Q**₁₀₀**=24.9 CFS)** represents flows from existing sub basin EX1. This basin is located within parcel 1 and is part of the East Cherry Creek Basin. Run-off from this sub-basin consists mostly of sheet flows that collect within a roadside ditch section on the west side of Allen Ranch Road. The swale flows from south to north to the round-about that intersects Allen Ranch Road and Old Stagecoach Road. From there the flows continue east within a roadside ditch section on the south side of Old Stagecoach Road where a 36" RCP culvert diverts flow north to detention pond 12 that has been developed as part of F.H.N. Filing No. 1.

Design Point 2 (Q₅**=0.3 CFS, Q**₁₀₀**=2.2 CFS)** represents flows from existing sub basin EX2. This basin is located within parcel 1 and is part of the Black Squirrel Creek Basin. Run-off from this sub-basin consists mostly of sheet flows that flow directly offsite into a tract within the F.H.N. Golf Course.

Design Point 3 (Q₅**=0.6 CFS, Q**₁₀₀**=4.3 CFS)** represents flows from existing sub basin EX3. This basin is located within parcel 1 and is part of the Black Squirrel Creek Basin. Run-off from this sub-basin consists mostly of sheet flows that drain directly west offsite into a tract within the F.H.N. Golf Course.

Design Point 4 (Q₅=4.3 CFS, Q₁₀₀=31.4 CFS) represents flows from existing sub basin EX4. This basin is located within parcel 2 and is part of the Black Squirrel Creek Basin. Run-off from this sub-basin consists mostly of sheet flows that collect within an existing tertiary drainage swale. The swale flows east to west to the associated design point where the run-off drains directly off-site into tract K of the F.H.N. Golf Course.

Design Point 5 (Q $_5$ **=2.0 CFS, Q** $_{100}$ **=14.6 CFS)** represents flows from existing sub basin EX5. This basin is located within parcel 2 and is part of the Black Squirrel Creek Basin. Run-off from this sub-basin consist of sheet flows that drain west directly off-site into tract K of F.H.N. Golf Course.

Design Point 5.1 (Q_5 =**1.8 CFS**, Q_{100} =**13.0 CFS**) represents flows from existing sub basin EX5.1. This basin is located within parcel 2 and is part of the East Cherry Creek Basin. Run-off from this sub-basin consists of sheet flows that drain east. Under the current conditions as of the date of this report, stormwater from this basin continues to drain east into the undeveloped portion of land that is a part of F.H.N. Filing No. 3 and eventually is captured within the irrigation pond located within tract L of the adjacent golf course. Under future conditions, once F.H.N. filing no. 3 has been constructed, flows from this basin will be collected within the EPC type A curb and gutter along Allen Ranch Road within F.H.N. Filing No. 3, of which is concurrently being reviewed. Flows collected within the existing curb and gutter are collected within 2 CDOT type R ongrade inlets sized 15' and 10'. Runoff not collected within the on-grade inlets are captured within a 15' Type R sump inlet. The captured flows are then directed to F.H.N. Filing 3 pond A to be detained and released at historic rates into an existing tertiary drainage swale located within tract L of the Flying Horse Golf Course.

Design Point 6 (Q $_5$ **=3.9 CFS, Q** $_{100}$ **=28.8 CFS)** represents flows from existing sub basin EX6. This basin is located within parcel 3 and is part of the East Cherry Creek Basin. Run-off from this sub-basin consists mostly of sheet flows that drain south off-site into Edmonds Subdivision.



Design Point 7 (Q_5 =22.7 **CFS**, Q_{100} =150.9 **CFS**) represents flows from existing sub basin EX7 and off-site basin OS1. Basin OS1 flows into EX7 from the east at design point 26. This basin is located within parcel 3 and is part of the East Cherry Creek Basin. Run-off from this sub-basin consists mostly of sheet flows that collect within an existing tertiary drainage swale. The swale flows from east to west to the associated design point. This design point continues into off-site basin OS6, tract L of the Flying Horse Golf Course.

Design Point 8 (Q₅**=23.2 CFS, Q**₁₀₀**=144.5 CFS)** represents flows from existing sub basin EX8 and off-site basin OS2. Basin OS2 flows into EX8 from the east at design point 27. This basin is located within parcel 3 and is part of the East Cherry Creek Basin. Run-off from this sub-basin consists mostly of sheet flows that collect within an existing tertiary drainage swale. The swale flows from south-east to north-west, into off-site basin OS6, which represents tract L of the F.H.N. Golf Course.

Design Point 9 (Q_5 =6.0 CFS, Q_{100} =44.2 CFS) represents flows from existing sub basin EX9. This basin is located within parcel 3 and is part of the East Cherry Creek Basin. Run-off from this sub-basin consists of sheet flows that drain north-west into off-site basin OS7 which represents tract M of the F.H.N. Golf Course.

Design Point 10 (Q_5 =**10.5 CFS**, Q_{100} =**70.3 CFS**) represents flows from existing sub basin EX10 and off-site basin OS3. Basin OS3 flows into EX10 from the south at design point 28. This basin is located within parcel 3 and is part of the East Cherry Creek Basin. Run-off from this sub-basin consists mostly of sheet flows that collect within an existing tertiary drainage swale. The swale flows from south-east to north-west, into off-site basin OS7, which represents tract M of the F.H.N. Golf Course.

Design Point 11 (Q_5 =42.5 **CFS**, Q_{100} =235.3 **CFS**) represents flows from existing sub basin EX11 and offsite basin OS4. Basin OS4 flows into EX11 from the south at design point 29. This basin is located within parcel 3 and is part of the East Cherry Creek Basin. Run-off from this sub-basin consists mostly of sheet flows that collect within an existing tertiary drainage swale. The swale flows from south to north-east to the associated design point.

Design Point 12 (Q_5 =6.8 CFS, Q_{100} =49.6 CFS) represents flows from existing sub basin EX12. This basin is located within parcel 3 and is part of the East Cherry Creek Basin. Run-off from this sub-basin consists of sheet flows that drains east directly off site to the associated design point.

Design Point 13 (Q_5 =5.4 **CFS**, Q_{100} =39.8 **CFS**) represents flows from existing sub basin EX13. This basin is located within a portion of parcel 3 and parcel 4 and is part of the East Cherry Creek Basin. Run-off from this sub-basin consists mostly of sheet flows that collect at an existing public storm culvert that runs from south to north through Old Stagecoach Road. Flows continue north into basin EX23.

Design Point 14 (Q_5 =12.4 CFS, Q_{100} =41.0 CFS) represents flows from existing sub basin EX14 and a third of the runoff from basin OS9. This basin is located within a portion of parcel 3 and parcel 5 and is part of the East Cherry Creek Basin. Run-off from sub-basin EX14 consists of sheet flows that collect at an existing public storm culvert that runs from south to north through Old Stagecoach Road. Run-off from OS9 is led to the DP via roadside swales on Old Stagecoach Road. Flows continue north into basin EX21.

Design Point 15 (Q_5 =30.7 CFS, Q_{100} =175.3 CFS) represents flows from existing sub basin EX15. This basin is located within parcel 3 and is part of the East Cherry Creek Basin. Run-off from sub-basin EX15 consists mostly of sheet flows that collect within an existing tertiary drainage swale. The swale flows from south to north to the associated design point where an existing public storm culvert that runs from south to



north through Old Stagecoach Road carries flows to basin EX20. Run-off from basin OS9 is led to the DP via roadside swales on Old Stagecoach Road.

Design Point 16 (Q_5 =2.3 CFS, Q_{100} =16.6 CFS) represents flows from existing sub basin EX16. This basin is located within parcel 3 and is part of the East Cherry Creek Basin. Run-off from this sub-basin consists of sheet flows that drain directly west into off-site basin OS7 which represents tract M of the F.H.N. Golf Course where an existing tertiary swale conveys flows north-west.

Design Point 17 (Q_5 =**4.4 CFS**, Q_{100} =**32.3 CFS**) represents flows from existing sub basin EX17. This basin is located within parcel 3 and is part of the East Cherry Creek Basin. Run-off from this sub-basin consists of sheet flows that drain west directly into off-site basin OS6. Drainage from basin EX17 making its way into OS6 goes directly into the existing retention pond/water feature within off-site basin OS6.

Design Point 18 (Q_5 =23.5 CFS, Q_{100} =165.9 CFS) represents run-off from off-site sub-basin OS7 in addition to run-off entering basin OS7 at design points 9, 10, and 16. This basin is located within parcel 3 and is part of the East Cherry Creek Basin. The associated sub-basin, OS7, is representative of tract M within the F.H.N. Golf Course and is actively in use. Within the tract there are several golf course features including fairways, greens, golf cart paths, a cart bridge over an existing natural drainage swale, and a retention pond. The retention pond has been designed with an overflow spillway at the west side of the pond/tract that releases water into the larger golf course water feature/retention pond that is in off-site sub-basin OS6 (tract L of F.H.N. Golf course). All drainage entering the tract will make its way down to the existing golf course retention pond via the existing tertiary drainage swale and will be released once the water surface elevation reaches a height that allows spillage to occur into the downstream pond in basin OS6.

Design Point 19 (Q_5 =**7.0 CFS**, Q_{100} =**203.7 CFS**) represents flows from existing sub basins EX18 & EX19 as well as the release flow from the jurisdictional irrigation reservoir at design point 31. These basins are located within parcel 5 and are a part of the East Cherry Creek Basin. Run-off from this sub-basin consists mostly of sheet flows that are directed south-north and collect within an existing tertiary drainage swale. The minor (Q5=4.0 cfs) and major (182.0 cfs) flows that are released from the upstream irrigation reservoir are done so via a set of twin concrete box culverts (4'x10') that spill out into a 20' wide rock chute that leads down to a 2' deep plunge pool. Released flows are then directed into the existing natural drainage swale that flows off-site to the north.

Design Point 20 (Q₅**=34.9 CFS, Q**₁₀₀**=205.9 CFS)** represents flows from existing sub basin EX20 and design point 15. Design point 15 enters basin EX20 from the culvert outlet on the north side of Old Stagecoach Road. This basin is located within parcel 5 and is part of the East Cherry Creek Basin. Run-off from this sub-basin consists mostly of sheet flows that collect within an existing tertiary drainage swale. The swale flows from south to north to the associated design point which continues north off-site.

Design Point 21 (Q₅**=26.6 CFS, Q**₁₀₀**=144.9 CFS)** represents flows from existing sub basin EX21 and design point 14. Design point 14 enters basin EX21 from the culvert outlet on the north side of Old Stagecoach Road. This basin is located within parcel 5 and is part of the East Cherry Creek Basin. Run-off from this sub-basin consists mostly of sheet flows that collect within an existing tertiary drainage swale. The swale flows from south to north to the associated design point where the flows will continue north off-site.



Design Point 22 (Q_5 =6.7 CFS, Q_{100} =49.3 CFS) represents flows from existing sub basin EX22. This basin is located within parcel 4 and is part of the East Cherry Creek Basin. Run-off from this sub-basin consists of sheet flows that drain north-west directly off-site.

Design Point 23 (Q₅**=65.9 CFS, Q**₁₀₀**=443.4 CFS)** represents flows from existing sub basin EX23 and design points 13 and 32. Design point 13 represents flows from basin EX13 and makes its way into basin EX23 via a culvert that runs under the eastern most round-about on Old Stagecoach Road. Design point 32 represent basin OS5 which enters the basin EX23 via a natural drainage swale from the south of basin EX23. Basin EX23 is located within parcel 4, contains the entirety of parcel 6, and is part of the East Cherry Creek Basin. Run-off from this sub-basin consists mostly of sheet flows that collect within multiple existing tertiary drainage swales. The swales flow from south to north to the associated design point and continue off-site.

Design Point 24 (Q_5 =3.3 CFS, Q_{100} =24.0 CFS) represents flows from existing sub basin EX24. This basin is located within parcel 4 and is part of the East Cherry Creek Basin. Run-off from this sub-basin consists mostly of sheet flows that collect within an existing tertiary drainage swale. The swale flows from south to north to the associated design point where the flows exit the site.

Design Point 25 (Q₅=11.2 CFS, Q_{100} =82.1 CFS) represents flows from existing sub basin EX25. This basin is located within parcel 4 and is part of the East Cherry Creek Basin. Run-off from this sub-basin consists mostly of sheet flows that drain north-west directly off-site towards Hodgen Road. The swale flows from south to north to the associated design point.

Design Point 26 (Q_5 =7.9 CFS, Q_{100} =42.7 CFS) represents flows from existing sub basin OS1. This basin is located just east of basin EX7 and is part of the East Cherry Creek Basin. Run-off from this sub-basin consists mostly of sheet flows that drain west towards the associated design point and enter the site via basin EX7. Flows that enter the site are then naturally collected within an existing tertiary drainage swale and continue to flow west.

Design Point 27 (Q_5 =13.5 CFS, Q_{100} =73.4 CFS) represents flows from existing sub basin OS2. This basin is located just east of existing sub-basins EX7 and EX8 and is part of the East Cherry Creek Basin. This off-site basin contains a part of the Palmer Divide subdivision which is a cul-de-sac containing 5 acre lots. Run-off from this sub-basin consists mostly of sheet flows that flow west and collect within an existing tertiary drainage swale that begins at the associated design point. The flows continue west, combining with run-off from basin EX8.

Design Point 28 (Q_5 =8.2 **CFS**, Q_{100} =53.9 **CFS**) represents flows from existing sub basin OS3. This basin is located east of basin EX9 and south of EX10 and is part of the East Cherry Creek Basin. Part of this basin lies within the Country View Estates subdivisions which consists of 5 acre lots. Run-off from this subbasin consists of sheet flows that collect within an existing tertiary drainage swale. The swale flows from south to north to the associated design point where it then enters the proposed site.

Design Point 29 (Q_5 =28.8 CFS, Q_{100} =134.6 CFS) represents flows from existing sub basin OS4. This basin is located directly south of basin EX11 and is part of the East Cherry Creek Basin. The off-site basin is comprised entirely of the Country View Estates Subdivision which contains 5 acre lots. Run-off from this sub-basin consists mostly of sheet flows that collect within an existing tertiary drainage swale. The swale flows from south to north to the associated design point where is enters the site through basin EX11.



Design Point 30 (Q_5 =3.8 **CFS**, Q_{100} =4.4 **CFS**) represents flows from existing off-site sub-basin OS8. This basin is located directly east of basin EX5.1 and is part of the East Cherry Creek Basin. This basin contains existing storm infrastructure that had been constructed during the F.H.N. Filing 3 development. Infrastructure includes 2 on-grade storm inlets, 2 sump inlets, and a full spectrum detention pond. The detention pond releases flows at historic rates which are reflected in the design points flow rates. Detained stormwater is released from the pond into the existing tertiary drainage swale located in off-site basin OS7.

Design Point 31 (Q_5 =102.7 CFS, Q_{100} =624.8 CFS) represents flows from existing sub basin OS6 as well as run-off from design points 7, 8, 17, 18, and 30. Basin OS6 is representative of a majority of tract L within F.H.N. Golf Course and is part of the East Cherry Creek Basin. This tract contains several golf course features as well as the irrigation reservoir. Flows entering this reservoir are retained and released at historic rates as shown with the flows associated with this design point. Stormwater exiting the reservoir does so through a small jurisdictional dam where twin concrete box culverts sized 4' x 10' allow water to pass under the roadway (Old Stagecoach Road) and into a 20' wide rock chute. The rock chute then releases water into an existing natural drainage swale that continues north, off-site. Calculated flows for this design point have been overridden by design flows from Classic Consulting's approved JD design report to provide a more accurate depiction of existing flows exiting the reservoir.

Design Point 32 (Q_5 =16.2 CFS, Q_{100} =78.3 CFS) represents flows from existing off-site sub-basin OS5. This basin is located directly east of basin EX13 and is part of the East Cherry Creek Basin. This basin contains a portion of F.H.N. Filing 1 development which includes several lots and a culvert that allows flows to pass underneath Old Stagecoach Road. Flows exiting the subbasin do so at the northern end of the subbasin which enter an existing natural drainage swale and flow into basin EX23.

There are offsite drainage basins that are conveyed onto or through the site on the southwestern portion. There are also offsite basins shown that are central to the greater PUD that represent the existing F.H.N. Golf Course areas. These basins are generally conveyed through the development via natural drainage ways or overland sheet flow. The proposed PUD is to either continue conveyance of these offsite basins or capture and convey them for onsite detention prior to release to downstream areas. The specific basins are described below in detail for comparison to developed conditions in a later section.

- Basin OS1 is approximately 19.0 acres and is located offsite to the south of parcel no. 3, adjacent and upstream to Basin EX7. The offsite basin was analyzed in the MDDP as Basin A and categorized as all open space with native weeds/grasses. In this report, basin OS1 has been analyzed as majority existing 5-acre residential lots with a portion of the basin remaining as open space. Existing developments within this basin are from the Edmonds Subdivision and Palmer Divide subdivision. Both subdivisions consist largely of 5 acre lots that did not require detention at their time of approval. Flows entering the proposed site are routed via overland sheet flow and eventually collect within existing drainage swales located on-site. The basin has a composite imperviousness of 5.2% and the 5-year minor storm event and the 100-year major storm event are 7.7 cfs and 40.8 cfs, respectively.
- Basin OS2 is approximately 36.4 acres and is located offsite to the southeast of parcel no. 3, adjacent and upstream to Basin EX8. The offsite basin was analyzed in the MDDP as Basin C and categorized as all open space with native weeds/grasses. In this report, basin OS2 has been analyzed as majority existing 5 acre residential with a portion of the basin remaining as open space. Existing developments within this basin are a part of the adjacent Palmer Divide subdivision. Run-



off coming from the mentioned subdivision did not require any detention at the time of approval. This off-site stormwater makes it way on-site via overland sheet flow that collects within an existing drainage swale, beginning at the property line. The basin has a composite imperviousness of 5.1% and the runoff rates for the 5-year minor storm event and the 100-year major storm event are 13.1 cfs and 69.9 cfs, respectively.

- Basin OS3 is approximately 25.25 acres and is located offsite to the southeast of parcel no. 3, adjacent and upstream to Basin EX10. The offsite basin was analyzed in the MDDP as Basin F and categorized as all open space with native weeds/grasses. In this report, basin OS3 has been analyzed as majority existing open space with native weeds/grasses and a portion of the basin now categorized as existing 5 acre residential. Existing developments within this basin are a part of the adjacent Country View Estates subdivision. Run-off entering the proposed site from the mentioned subdivision did not require any detention at the time of approval. This off-site stormwater makes it way on-site via overland sheet flow that collects within an existing drainage swale, beginning at the property line. The basin has a composite imperviousness of 3.0% and the runoff rates for the 5-year minor storm event and the 100-year major storm event are 8.2 cfs and 53.9 cfs, respectively.
- Basin OS4 is approximately 72.3 acres and is located offsite to the southeast of parcel no. 3, adjacent and upstream to Basin EX11. The offsite basin was analyzed in the MDDP as Basin Q and categorized as all open space with native weeds/grasses. In this report, basin OS4 has been analyzed as entirely existing 5 acre residential. Existing developments within this basin are a part of the adjacent Country View Estates subdivision. Run-off entering the proposed site from the mentioned subdivision did not require any detention at the time of approval. This off-site stormwater makes it way on-site via overland sheet flow that collects within an existing 18" HDPE culvert to cross under a gravel driveway that borders the north side of Country View Estates. The flows exit the culvert and enter an existing natural drainage swale that travels into parcel no. 3 of the proposed site. The basin has a composite imperviousness of 7.0% and the runoff rates for the 5-year minor storm event and the 100-year major storm event are 28.8 cfs and 134.6 cfs, respectively.
- Basin OS5 is approximately 41.2 acres and is located offsite to the east of parcel no. 3 and south of parcel no. 4, adjacent and upstream to basin EX23. The offsite basin was analyzed in the MDDP as Basin V and categorized as mostly 5-acre residential with the rest of the area as open space, and this categorization remains in this report. Existing developments within this basin are 5-acre residential that have been developed as a part of F.H.N. Filing No. 1. Flows from the south of this subbasin are sheet flows that pass through a culvert that runs underneath Old Stagecoach Road and continue north into an existing drainage swale. This swale continues north and enters parcel no. 4, basin EX23, from the southern edge. The basin has a composite imperviousness of 6.5% and the runoff rates for the 5-year minor storm event and the 100-year major storm event are 16.2 cfs and 78.3 cfs, respectively.
- Basin OS6 is approximately 83.6 acres and is located west of parcel no. 3. The offsite basin was analyzed in the MDDP as part of Basin E and categorized as all open space which remains as the categorization within this report. Existing developments within this basin are a part of the adjacent F.H.N. North Golf Course and consist of golf course infrastructure/features. Run-off coming from and making its way into the golf course tract collect within the existing irrigation reservoir. Water released from the reservoir is done so through the small jurisdiction dam via twin 4'x10' concrete box culverts that allows the released waters to pass underneath Old Stagecoach Road, into a rock



chute, and finally into an existing natural drainage swale that flows north off-site. The basin has a composite imperviousness of 2.0% and the discharge rates, from the reservoir, for the 5-year minor storm event and the 100-year major storm event are 12.0 cfs and 124.0 cfs, respectively.

- Basin OS7 is approximately 20.1 acres and is located within the western half of parcel no. 3, adjacent and downstream to Basins EX9, EX10, and EX16. The offsite basin was analyzed in the MDDP as Basin G and categorized as all open space with native weeds/grasses and remains as this categorization within this report. Existing developments within this basin are a part of the adjacent F.H.N. Golf Course and consist of golf course infrastructure/features. Run-off coming from and making its way into the golf course tract collect within a retention pond/water feature. Water released from the pond is directed into the downstream irrigation reservoir. The basin has a composite imperviousness of 2.0% and the runoff rates for the 5-year minor storm event and the 100-year major storm event are 4.7 cfs and 34.9 cfs, respectively.
- Basin OS8 is approximately 8.0 acres and is located east of parcel no. 2, adjacent and downstream to Basin EX5.1. The offsite basin was analyzed in the MDDP as a part of Basin E and categorized as all open space with native weeds/grasses. This basin is a part of F.H.N. Filing No. 3 and contains a part of Allen Ranch Road as well as an existing full spectrum detention pond. Run-off coming from and making its way into this basin, from basin EX5.1, is collected with the 4 type-R inlets along Allen Ranch Road that direct the stormwater into the detention pond which is then released at historic rates into the existing adjacent F.H.N. Golf Course tract. The basin has a composite imperviousness of 58.1% and the runoff rates for the 5-year minor storm event and the 100-year major storm event are 3.8 cfs and 4.4 cfs, respectively.
- Basin OS9 is approximately 9.4 acres and is located in between parcels 3 and 4. The offsite basin was analyzed in the MDDP as a part of several basins, but now represents the area of Old Stagecoach Road that splits F.H.N. parcels 3 and 4. Because of this, this basin is categorized as mostly paved surface. This was developed as a part of F.H.N. Filing No. 1 and several pieces of stormwater infrastructure, all of which are culverts, allow flow from the south to cross underneath the road and continue north. Runoff from Old Stagecoach Road is captured in roadside swales and discharged into the culverts at design points 14 and 15, with the remaining flows discharging into

the irrigation reservoir in offsite basin OS6. The basin has a c and the runoff rates for the 5-year minor storm event and the 1 cfs and 50.6 cfs, respectively.

There are no exemptions for detention in the criteria. Please revise the statement and see comments on the drainage plan.

Proposed Major Basin Descriptions

This PDR discusses the hydrology of the larger basins that representing the water quality and full spectrum detention ponds for the developed and disturbed basin areas. Any basin areas that drain directly offsite will consist of grass buffers that provide 100 perce runoff reduction and/or are exempt from detention requirements. An exhibit showing what are throughout all parcels of the development that will be exempt from detention requirements will be shown in appendix F. All basins that are stated to have 100% run-off reduction from water quality are support with UDBMP spreadsheet calculations that can be found in appendix D. These calculations represe "worst case scenarios" for percent imperviousness of 2.5 acres lots and larger and ensure that the large lots still receive runoff reduction. The major basins yield overall minor and major storm ever runoff rates calculated by the Rational Method that are to be captured in the public roadways with public storm sewer inlets and routed to their respective detention facility via public and private storm pipes. A





combination of inlet sump locations, on-grade inlets, and grass lined swales are to be utilized for capture and conveyance. Design details such as specified inlet types and sizes, pipe sizing and hydraulic grade line analysis, and roadway capacities are to be presented in a future FDR in which sub-basins are delineated and additional design points where runoff is captured within major basins are presented. The PDR delineates the major basin throughout the development and provides preliminary sizing for proposed permanent control measures only.

Below are the major basins within the PUD Preliminary Plan Parcels 1-6 and their description including tributary area size, location, land use makeup, downstream design point and permanent control measure, as well as minor and major storm runoff totals. Basin descriptions are used as a PUD and PDR level of design is more clearly explained by describing land uses within a basin. Design Points are mentioned for each basin. Emergency overflow pathways are described for each detention pond in a further section of the report.

- Basin A is approximately 74.1 acres located to the south of the PUD within Parcel No. 3 and is east of the existing F.H.N. Golf Course. The basin consists of ½-acre sized single-family residential lots with a network of paved roadways within the 60' local urban rights-of-way. The basin contains a large area of open space tract including Detention Pond A, Design Point 3. The basin has a composite imperviousness of 15.0% and the runoff rates for the 5-year minor storm event and the 100-year major storm event are 38.9 cfs and 161.6 cfs, respectively.
- Basin A1 is approximately 12.6 acres located to the south of the PUD within Parcel No. 3 and the east onsite area downstream of offsite basin OS1. The basin consists of 5.0-acre estate single-family residential lots that include mostly pervious lawn area, and the basin includes an existing tertiary channel that is intended to be undisturbed and flow through the PUD via a public culvert pipe crossing at Design Point 4. This design point will also convey the upstream Basin OS2, and ultimately drain to the existing Golf Course Irrigation Pond, Design Point 6, where the basin will receive detention. Refer to table 4 in section 6.d of this report for supporting calculations that prove that the irrigation pond will not receive more major stormwater flow than historical conditions. The basin has a composite imperviousness of 7.0% and the runoff rates for the 5-year minor storm event and the 100-year major storm event are 6.0 cfs and 29.0 cfs, respectively.
- Basin A2 is approximately 6.5 acres located to the south of the PUD within Parcel No. 3 and is east of the existing Flying Horse North Golf Course. The basin consists of the rear of ½-acre sized single-family residential lots that include mostly pervious lawn area and the majority of the basin includes an existing tertiary channel that is intended to be undisturbed and flow through the PUD via a public culvert pipe crossing at **Design Point 5** conveying the upstream Basin OS2, ultimately to the existing F.H.N. Golf Course Irrigation Pond, **Design Point 6**, where basin A2 will receive storage detention. Refer to table 4 in section 6.d of this report for supporting calculations that prove that the irrigation pond will not receive more major stormwater flow than historical conditions. The basin has a composite imperviousness of 13.1% and the runoff rates for the 5-year minor storm event and the 100-year major storm event are 3.4 cfs and 15.3 cfs, respectively.
- Basin B is approximately 32.7 acres and is located north of Basin A, within the south half of the PUD in Parcel No. 3 and is east of the existing golf course. The basin consists of 1/2-acre and 1/3-acre sized single-family residential lots with a network of paved roadways within the 60' local urban rights-of-way. The basin contains an area of open space tract to its south and tract area to the north for Detention Pond B, Design Point 7. The basin has a composite imperviousness of 24.1% and

tl





the runoff rates for the 5-year minor storm event and the 100-year major storm event are 24.6 cfs and 86.1 cfs, respectively.

- Basin C is approximately 121.0 acres and is located northeast of Basin OS7 and west of Basin D, within the south half and central areas of the PUD in Parcel No. 3. The basin consists of a mix of land uses consisting of ½-acre and ¼-acre sized single-family residential lots with paved roadways within the 60' local urban rights-of-way and the extension of Old Stagecoach Road. The basin contains a large area of open space tract central to the basin including designated Park Space. This open space area consists of existing tertiary swales to remain undisturbed. These swales convey stormwater runoff to an existing public 48" RCP culvert pipe (Design Point 10) that crosses Old Stagecoach Road that will now outfall to Detention Pond C, Design Point 11. Proposed flows leading to the existing RCP culvert will be analyzed further in the FDR. The basin has a composite imperviousness of 31.6% and the runoff rates for the 5-year minor storm event and the 100-year major storm event are 81.4 cfs and 251.4 cfs, respectively.
- **Basin D** is approximately 86.2 acres and is located east of Basin C within the southeast of the PUD in Parcel No. 3. The basin consists of ¼ -acre, 1/8-acre (0.2-acres), and 5-acre estate single-family residential lots with paved roadways within the 60' local urban rights-of-way. The basin contains open space at the filing boundary to the east which includes Detention Pond D, **Design Point 13**. The basin has a composite imperviousness of 26.8% and the runoff rates for the 5-year minor storm event and the 100-year major storm event are 54.8 cfs and 177.1 cfs, respectively.
- Basin E is approximately 52.4 acres and is located northeast of Basin C and north of Basin D and is within the central north half of the PUD and is a part of Parcel No. 3 and No. 5 which is the dedicated future amenities and recreation/gym facility parcel. The basin consists of ¼ -acre single-family residential lots with paved roadways within the 60' local urban rights-of-way and the extension of Old Stagecoach Road. Parcel No. 5 is assumed at 75% future commercial land use area. The basin drains due northwest and is tributary to Detention Pond E, Design Point 15. Within the basin is a culvert pipe that is to cross Old Stagecoach Road, Design Point 14. Sub-basins within Basin E are to be delineated in a future FDR to size the culvert pipe crossing. The future commercial amenities center area within Parcel No. 5 is assumed to drain directly to the public storm system that outfalls to Detention Pond E. The basin has a composite imperviousness of 43.7% and the runoff rates for the 5-year minor storm event and the 100-year major storm event are 67.7 cfs and 171.0 cfs, respectively.
- Basin F is a large area of the northern portion of the PUD totaling approximately 197.5 acres and is located northeast of Basin E and east of Basin G and extends to the north and northeast filing boundary within Parcel No. 4 and Parcel No. 6 which is the commercial lot at the northeast of the PUD. The basin consists of a mix of 1/8-acre, 1/4 -acre and 2.5-acre single-family residential lots with paved roadways within the 60' local urban rights-of-way and a short extension of Old Stagecoach Road to a roundabout connection to the local and collector roadways. The basin contains a large area of open space tract area to the east of the filing as a buffer from surrounding subdivision. This tract consists of existing natural tertiary channels and swales that drain due north. Portions of these tertiary swales will be re-graded to ensure proper bury depth of public sanitary sewer crossings from the Parcel's south residential blocks to the north area. There are interior tract areas of open space and a designated Park Area to the north central portion of the basin. The very northeast corner of the basin and filing contains a future commercial development parcel of

Review C1: Please address whether the development has or will obtain the necessary downstream easements to accept the developed flows of this basin as the development of these lots will increase historic flows and they are not being mitigated as required. Analysis of the downstream will be required with the FDR.

rth Phase 2 Parcels 1-6 minary Drainage Report Project No.: 211030

Review C2: Unresolved. It appears that section 6.c does not include information about the effect on downstream from storm water release points at basin H. Additionally, Appendix D shows that 100% of the WQCV is captured but does not address detention of flows from this area. Please identify how the increase in flows from these basins will be mitigated.

ention Pond F, off rates for the and 366.3 cfs,

g, west of Basin re single-family

residential lots with paved roadways within the 60' local urban rights-of-way and the connection to Hodgen Road. The basin contains a large area of open space tract at the north boundary of the site which contains Detention Pond G, **Design Point 18**. Additionally, the tract provides an emergency spillway overland path to the pond. The basin drains due north and northwest to the proposed pond. The basin has a composite imperviousness of 16.4% and the runoff rates for the 5-year minor storm event and the 100-year major storm event are 16.4 cfs and 68.4 cfs, respectively.

- Basin H is approximately 74.0 acres and is located onsite at the east filing boundary on the north half of the filing, adjacent to Basins C, E, F and G within Parcel No. 4. The basin consists of 5-acre rural single-family residential estate lots to act as buffers to the urban areas of the development. The developed areas within this basin are large estate lots that have sufficient undeveloped open space downstream for grass buffers that provide 100 percent runoff reduction and therefore do not have to be captured and detained onsite, as per the PBMP applicability item part II.E, which classifies lots greater than 2.5 acres with less than 10% imperviousness. Additionally, run-off reduction supporting calculations can be found in appendix D and an exhibit can be found in appendix F showing areas that do not require detention. The basin has a composite imperviousness of 7.0% and the runoff rates for the 5-year minor storm event and the 100-year major storm event are 37.6 cfs and 180.4 cfs, respectively. Design Point 19 represents the respective downstream outfall areas at the filing border with offsite adjacent properties for the rural lots that drain directly offsite. See section 6.c of this report for more information about the effect on downstream properties from stormwater release points.
- Basin I is approximately 7.1 acres and is in the northwest portion of Par No. 1, west of Basin C and north of Basin OS7. The basin consist residential lots and a Tract at the northern cul-de-sac. The basin drain Point 20) at the northern cul-de-sac which is to outfall to the exist Pond/Reservoir (Design Point 6) matching the historical drainage patt flows from this basin are lower than the proposed flows to the irrigation part flowrates leading to the irrigation pond are to be reduced in proposed conflows leading the existing irrigation pond will be lower for the proposed historical values, the flows exiting basin I can be discharged into the exit to section 6.d of this report for supporting calculations. The basin has a of 26.4% and the runoff rates for the 5-year minor storm event and the 1 are 6.1 cfs and 20.7 cfs, respectively.

Language added to this paragraph to explain mitigation is accomplished with on-site overdetention so that the overall outflow from the development is equal to or less than existing conditions.

Basin J is approximately 15.8 acres and is in the west area of the PUD in Parcel No. 1, adjacent to F.H.N. Filing No. 1. The basin consists of the proposed permanent golf course clubhouse development with parking lot. The basin drains due north toward Old Stagecoach Road and west into Pond J, Design Point 21. The basin has a composite imperviousness of 86.1% which



conservatively includes an assumed 95% imperviousness for most of the developed commercial parcel and 1.5 acre of pond open space. The runoff rates for the 5-year minor storm event and the 100-year major storm event are 59.8 cfs and 112.4 cfs, respectively.

Basin K is approximately 18.0 acres and is in the west commercial and flats area of Parcel No. 2, adjacent to Filing Nos. 1 and 3. The basin consists of the hotel and resort parking areas and various amenities buildings in addition to the main hote building as well as a casitas residential development with paved access roadwa due west to proposed Detention Pond K, Design Point 22 which outfalls du existing golf course and F.H.N. Filing No. 1. The basin has a composite imper SEE THE EXISTING which conservatively includes an assumed 95% imperviousness for mos commercial and residential parcel and 1.75 acre of pond open space area. The 5-year minor storm event and the 100-year major storm event are 64.4 respectively.

POND 8 CANNOT BE SEEN ON THE PROPOSED DRAINAGE MAP. DRAINAGE CONDITIONS MAP FROM THE MDDP IN THE REFERENCED **MATERIAL** APPENDIX.

- **Basin L** is approximately 7.1 acres and is in the west commercial and flats a adjacent to Filing Nos. 1 and 3. The basin consists of the Flats which includes the puncings, queess drives, and landscaping that are conceptual at this point. Assumed imperviousness for this basin is 40% open space landscaped area and 60% roof and pavement. The basin drains due west through the existing F.H.N. Golf Course and is tributary to existing Pond 8 in Filing No. 1. In the final design of this basin, it will be demonstrated that Pond 8 has sufficient capacity for the contributing flow and that the pond will continue to function as intended and without maintenance deficiencies. This tributary basin was discussed in the 2018 Classic Consulting PDR/FDR and the 2023 F.H.N. Filing No. 3 FDR by HR Green Development, LLC. The basin has a composite imperviousness of 57.8% and the runoff rates for the 5-year minor storm event and the 100-year major storm event are 19.0 cfs and 41.1 cfs, respectively. Design Point 23 represents the basin's west outfall location at the golf course from the flats area. The adjacent development to the east is a part of Filing No. 3 and is described in the Filing No. 3 FDR to be detained in Pond A of Filing No. 3 located adjacent to the golf course.
- Basin M is approximately 5.0 acres and is in the west commercial and flats area in Parcel No. 2, adjacent to Filing Nos. 1 and 3. The basin consists of the Flats which includes the buildings, access drives, and landscaping that are conceptual at this point. Assumed imperviousness for this basin is 40% open space landscaped area and 60% roof and pavement. The basin has a composite imperviousness of 57.8% and the runoff rates for the 5-year minor storm event and the 100-year major storm event are 9.9 cfs and 21.3 cfs, respectively. The basin drains due east to F.H.N. Filing No. 3, which is being reviewed concurrently, into a section of Allen Ranch Road that contains several pieces of drainage infrastructure including 4 CDOT Type-R inlets. Stormwater that exits the basin is captured within those inlets and then piped down to full spectrum detention pond A, a part of F.H.N. Filing No. 3, which will release flows at historic rates. Flows released from the pond eventually end up in the irrigation reservoir that has been developed as part of F.H.N. Filing No. 1. This portion of Allen Ranch Road and the detention pond have been assessed for fully developed conditions of the Flats area as part of the F.H.N. Filing No. 3 FDR.

The following are the Offsite Basins that the upstream tributary areas that drain to and through the proposed PUD that will require collection and conveyance to downstream permanent control measures or routing around or through the development. The offsite basins are described as undeveloped open space Revie plan

Revie Unre label propo map.



consisting of their native grasses and weeds with sparse areas of barren pervious soils per the NRCS Soils Maps included in the Appendix. Any future development of these upstream adjacent properties are to require onsite water quality and detention and any stormwater release to and through the Flying Horse North subdivision will be restricted to be at or less than historical rates and via overland sheet flow. There are also offsite basins that represent the existing F.H.N. Golf Course areas, as relevant to this PUD.

- Basin OS1 is approximately 19.0 acres and is located offsite to the southeast of the filing, adjacent and upstream to Basin A. The offsite basin was analyzed in the MDDP as Basin A and remains as its existing undeveloped open space with native grasses and weeds. There are no developments within this major offsite basin and any future development of the area will require onsite water quality and detention. The offsite basin is tributary to onsite Detention Pond A / Design Point 3. Detention Pond A outfalls to the existing golf course at or below historical stormwater runoff rates and drains to the existing Golf Course Irrigation Pond (Design Point 6). The offsite basin is routed via overland sheet flow to the roadway in the PUD and is to cross and outfall into undisturbed open space in Basin A via public culvert pipes sited at Design Points 1 and 2. The basin is to be split into two sub-basins to assess each culvert pipe design in a future FDR. The basin has a composite imperviousness of 2.0% and the runoff rates for the 5-year minor storm event and the 100-year major storm event are 5.6 cfs and 41.3 cfs, respectively.
- Basin OS2 is approximately 36.4 acres and is adjacent and upstream of Basin A1. The offsite basin was analyzed in the MDDP as Basin B and remains as its existing undeveloped open space with native grasses and weeds. There are no developments within this major offsite portion of the basin and there is a small area of 5-acre development within the Site where the existing tertiary channel crossing through the development. Any future development of the off-site area will require onsite water quality and detention to release at historical rates as it passes through the F.H.N. PUD. The offsite basin is tributary to the existing Irrigation Pond (Design Point 6) that was built as a part of the F.H.N. Golf Course development. The offsite basin is routed via overland sheet flow and is conveyed through the PUD via public culvert pipes (Design Point 4) through the PUD roadways and through the existing tertiary channel in Basin A2. The basin has a composite imperviousness of 2.0% and the runoff rates for the 5-year minor storm event and the 100-year major storm event are 9.2 cfs and 67.9 cfs, respectively.
- Basin OS3 is approximately 25.3 acres and is located offsite to the southeast of the filing, adjacent and upstream to Basin BB. The offsite basin was analyzed in the MDDP as Basin C and remains as its existing undeveloped open space with native grasses and weeds. There are no developments within this major offsite basin and any future development of the area will require onsite water quality and detention. The offsite basin overland sheet flows to the roadway at the south portion of Basin BB and C and is conveyed directly to the open space existing F.H.N. Golf Course area in Basin BB via a public culvert pipe (Design Point 8) and is directed offsite, ultimately to the existing Irrigation Pond at the Golf Course (Design Point 6). The basin has a composite imperviousness of 2.0% and the runoff rates for the 5-year minor storm event and the 100-year major storm event are 6.8 cfs and 49.9 cfs, respectively.
- Basin OS4 is approximately 72.3 acres and is located offsite to the southeast of the filing, adjacent
 and upstream to Basin D. The offsite basin was analyzed in the MDDP as Basin D and remains as
 its existing undeveloped open space with native grasses and weeds. There are no developments
 within this major offsite basin and any future development of the area will require onsite water



quality and detention. The basin drains onto the PUD site via overland flow until it is channelized in a tertiary swale at **Design Point** 12. The offsite basin is tributary to onsite Detention Pond D / **Design Point** 13. The offsite basin is routed via overland sheet flow and is channelized through onsite Basin F via existing natural channels. The basin has a composite imperviousness of 2.0% and the runoff rates for the 5-year minor storm event and the 100-year major storm event are 18.3 cfs and 134.5 cfs, respectively.

- Basin OS5 is approximately 41.2 acres and is located offsite central east boundary of the filing, adjacent to Basin E and upstream to Basin F. The offsite basin was analyzed in the MDDP as Basins V2, U, W, and X3 and remains as existing 2.5 acre lots and partion open space with native weeds and grasses. The existing developments within this site will receive detention as a part of the development of parcel no. 4 of this PUD. The offsite basin is tributary to onsite Detention Pond F / Design Point 17. The offsite basin is routed via overland sheet flow and is channelized through onsite Basin F via existing natural channels on the east side of parcel no. 4, entering the Site at Design Point 16 where proposed estate lots are sited. It is expected that driveway culvert pipes for these estate lots will be required to convey the upstream off-site stormwater runoff. The basin has a composite imperviousness of 2.0% and the runoff rates for the 5-year minor storm event and the 100-year major storm event are 15.9 cfs and 78.8 cfs, respectively.
- Basin OS6 is approximately 95.0 acres and represents the existing F.H.N. Golf Course area between the west Parcels 1 and 2, Filing No. 1, and Filing No. 3 and the east PUD residential areas for Parcels 3-6. The existing golf course area includes areas of pervious grassed surfaces for the golf course, and rear of residential lots of various lot sizes that drain through the course. This basin includes the existing Irrigation Pond/Reservoir, **Design Point 6** that is the ultimate drainage control measure for many basins and pond outfalls within the PUD. The offsite basin was analyzed in the MDDP as Basin E and most of the basin remains as the existing golf course development with the addition of some rear of developed PUD lots adjacent to Basins A, B, I, and Filing No. 1 and 3 estate lots. The basin has been reduced in size from the MDDP as the PUD development of Basins A. B. and I will capture stormwater runoff where historic conditions have areas within these basins that flow directly to the Irrigation Reservoir. In cases where the back half of a proposed lot will be directed to flow into basin OS6, the lot will be provided detention via the irrigation pond within basin OS6. The offsite basin is routed via overland sheet flow and is channelized through grass-lined swales along its east edge adjacent to Basins A and B. The basin has a composite imperviousness of 4.6% and the runoff rates for the 5-year minor storm event and the 100-year major storm event are 23.0 cfs and 143.5 cfs, respectively.
- Basin OS7 is approximately 28.2 acres and is located north of Basin B and southwest of Basin C, within the south half of the PUD in Parcel No. 3 and is comprised of existing golf course area that is not to be disturbed. The basin includes some onsite area (7.6 ac.) of developed single-family residential lots which are the rear half of the lots backing up to the existing golf course. The basin flows directly offsite at Design Point 9 and has 100 percent runoff reduction via the grass buffer in the existing Golf Course and ultimately drains to the existing Irrigation Pond/Reservoir (Design Point 6). The basin has a composite imperviousness of 8.2% and the runoff rates for the 5-year minor storm event and the 100-year major storm event are 10.6 cfs and 57.7 cfs, respectively. The basin is all open space and has 100 percent water quality runoff reduction via a grass buffer and is directed offsite.



• Basin OS8 is approximately 8.0 acres and is located east of parcel no. 2, adjacent and downstream to Basin M. The offsite basin was analyzed in the MDDP as a part of Basin E and categorized as all open space with native weeds/grasses. This basin is a part of F.H.N. Filing No. 3 and contains a part of Allen Ranch Road as well as an existing full spectrum detention pond. Run-off coming from and making its way into this basin, from basin M, is collected with the 4 type-R inlets along Allen Ranch Road that direct the stormwater into the detention pond which is then released at historic rates into the existing adjacent F.H.N. Golf Course tract. The basin has a composite imperviousness of 58.1% and the runoff rates for the 5-year minor storm event and the 100-year major storm event are 3.8 cfs and 4.4 cfs, respectively.

The above-mentioned basins are large planning area basins and as the Final Drainage Report is developed for the filing, additional analysis and calculations will be required to assess proposed storm sewer conveyance, roadway and inlet capacities, capacities and routing of natural and proposed channels and swales, and detention pond infrastructure.

IV. Drainage Design Criteria

a. Development Criteria Reference

The following criteria manuals and reports were used as reference material for the preparation of and its hydrologic and hydraulic design parameters.

- NOAA Atlas 14
- NRCS Soil Survey for El Paso County Area, Colorado
- El Paso County Assessor Property Records
- El Paso County Drainage Criteria Manual, 2014
- City of Colorado Springs Drainage Criteria Manual, May 2014
- Urban Storm Drainage Criteria Manual, Urban Drainage Flood Control District, Januar

The following reports were used as reference documents for surrounding developments and the n drainage basin that the proposed PUD lies within.

- Preliminary Drainage Report for Flying Horse North Preliminary Plan and Final Draina for Flying Horse North Filing No. 1, Classic Consulting Engineers and Surveyors, Nov
- Flying Horse North Filing No. 3 Final Drainage Report prepared by HR Green Develop

 latest revision August 2023
- Flying Horse North Master Development Drainage Plan, HR Green Development, LLC September 2022
- Flying Horse North Irrigation Reservoir Embankment Design Report, Classic Consulti Engineers and Surveyors, August 2018
- Black Squirrel Drainage Basin Planning Study (DBPS), URS Consultants, January 1989

b. Hydrologic Criteria

Design rainfall was determined utilizing Table 6-2 from the City of Colorado Springs Drainage Criteria Manual to determine the 5-year and 100-year rainfall values for the 1-hour events. The 1-hour rainfall depths are 1.5 and 2.52 in/hr respectively. The Rational Method is used for stormwater runoff calculations.

Composite percent impervious calculations were completed for each subbasin based on the density of lots and can be found in Appendix B. The El Paso County Drainage Criteria Manual Table 5-1 was used for

A paragraph has been added to thi section and the summary about he future FDR's tha finalize ponds are include over-detention to mitigate downstrea flow increases a basins that drair directly offsite. A summary table o existing outflow versus develope outflow cannot b provided at the PL

stage as there are

finalized outlet

structure

calculations at the

stage for each por



reference when correlating land use to percent impervious values and located in Appendix F. Impervious values for 5-Acre Rural Lots, 2.5-Acre Rural Lots, 1/2-acre, 1/3-acre, 1/4-acre, 1/8-acre single family residential lots and Commercial Lots have impervious values of 7%, 11%, 25%, 30%, 40%, 65%, 95%, respectively. Open space, lawn, and golf course areas have 2% impervious values. Rainfall intensity and peak runoff calculations are provided in Appendix B.

Basins are routed to their respective design points and detention ponds as shown on the Hydrology Maps in Appendix F. Calculations performed in the Mile High Flood District BMP and Detention spreadsheets are used to determine pond storage sizing and detention discharge release rates at the preliminary design level.

c. Applicable Criteria and Standards

Per the DBPS and El Paso County Criteria Manual, flows from the proposed site will be limited to historic flows to maintain the stability of the existing channels within the drainage basins. The master plan follows the Drainage Criteria Manual for El Paso County which refers to the City of Colorado Springs Drainage Criteria Manuals as amended. Criteria within the County and City manuals refer to the Mile High Flood District manuals, particularly for extended detention basin design and runoff reduction calculations which are utilized in this report.

V. Hydraulic Analysis

Major Drainageways

There are no major drainage ways that exist within the PUD development; however, natural tertiary tributaries are within the site currently and function to convey flows to unnamed tributaries of the East Cherry Creek and Black Squirrel Creek. Open spaces including tracts and park areas have natural drainageways that will remain undisturbed and are assessed within this report for capacity and stabilization. This PDR does not include hydraulic analysis for the storm systems to be designed as a part a future FDR, however, there are preliminary design points with storm pipes such as culvert crossings, tract drainageways, and other conveyances that are included in the hydraulic analysis of this PDR.

Hydraulic analysis is provided in this PDR for the following:

- Locations where upstream off-site basins will cross roadways in the development and culverts are sited
- Natural channels both onsite and offsite that will either be undisturbed or graded into an engineered channel.
- Locations where existing culvert storm infrastructure will be used to convey newly proposed flows underneath Old Stagecoach Road.

VI. Drainage Facility Design

a. General Concept

For the PUD Preliminary Plan to be in compliance with off-site runoff requirements, the developed conditions require conveyance of upstream off-site areas through or around the developed areas. The off-site tributary basins are to be captured and conveyed within the major basins of the developed PUD parcels and routed to downstream design points that are full spectrum detention basins. This PDR includes preliminary hydraulic design for the conveyance of off-site stormwater runoff but does not include detailed



analysis of proposed storm systems within the major basins. It is anticipated that developed rights-of-way will include public stormwater infrastructure including inlets that will capture stormwater runoff and convey the runoff downstream via storm main to their respective detention basins. Off-site areas that drain directly onto the developed areas are to be captured either by culvert pipes or drainage swales and conveyed to storm sewer systems that ultimately outfall to detention basins.

The content included in this PDR to demonstrate drainage facility design at the preliminary level include hydrology design calculations including the Rational Method tabulations for determining major basin composite coefficients, imperviousness, time of concentration, rainfall intensity, and peak runoff rates for minor and major storm events; MHFD Detention and BMP tabulations for basin stage-storage and detention discharge rates; tables and figures from the El Paso County Drainage Criteria Manual for Land Use Coefficients and Percent Imperviousness; tables and figures from the City of Colorado Springs Drainage Criteria Manuals Volumes 1 and 2 for roadway stormwater capacity; and hydrology maps for the predevelopment and developed conditions of the PUD to show major basin delineations, acreage of tributary areas, and design point routing.

b. Specific Details

This PDR includes Appendix F hydrology/drainage maps showing the major basin tributary areas associated with the PUD development for both the pre-developed and developed conditions. The appendix calculations and drainage maps include tables summarizing the stormwater peak runoff rates fo the minor (5-year) and major (100-year) events. The maps and calculations include off-site tributary areas entering the PUD parcels and the outfall locations for pond outlet pipes and any basins with direct runoff exiting the PUD parcels to off-site downstream locations.

The approach to accommodate drainage impacts on existing or proposed improvements includes the delineation of major basins at the PDR level to determine the required location and sizing of full spectrum detention basins to provide water quality and detention and release stormwater downstream at or below historical rates. The general concept for future delineated sub-basins and a storm system design to be presented in a future FDR includes public and private storm inlets and pipes that will collect and convey off-site and on-site stormwater runoff within roadways that ultimately outfall to detention ponds. A future FDR will include storm system design based on roadway capacity, inlet capacity, and hydraulic grade lines. The PDR summarizes the major basin areas and provides preliminary calculations for each major basin and their downstream control measures.

The proposed water quality and full spectrum detention basins are preliminarily sized in this PDR for the purpose of siting, and the outlet structures and orifice plate design are to be designed for release rates at or below historical rates in a future FDR. Pond designs are also preliminarily shown on the developed conditions drainage map including the required stormwater infrastructure for extended detention basins including concrete forebays, concrete trickle channels, concrete micropools and outlet structures with orifice plates and/or outlet pipe restrictor plates, emergency spillways with weirs, maintenance pathways, outlet pipes.

The drainage impact of site constraints such as streets, utilities, existing and proposed structures are mitigated by following typical sections for right-of-way improvements per the County Engineering Criteria Manual. The majority of the PUD parcels include urban local and urban collector roadways with standard alignments for storm sewer, water main, and sanitary sewer. A future FDR is to include sited storm sewer



alignments and inlet locations with consideration for vertical clearances of utility crossings. There are no existing structures or utilities currently in conflict with the preliminary storm design.

There are no known environmental features or issues applicable to the drainage facility design of the PUD.

Maintenance access is required by the County for the perpetual access and maintenance of stormwater facilities. The PDR level of design presented in this report and its maps shows that each detention facility will require a standard maintenance pathway from the public rights-of-way to access all pond infrastructure including forebays and outlet structures. Access to drainage facilities are to include a pathway from the public rights-of-way or a pathway within an access easement.

c. Detention Pond Preliminary Design Summary

The following table summarizes the full spectrum detention ponds sited for the PUD Preliminary Plan. The ponds are designed for WQCV, EURV, and 100-year storage volumes. Preliminary design has been done for the outlet structures to release at or below historical rates.

Pond Name	Preliminary Bottom Elev. (ft)	Preliminary Top of Pond Elev. (ft)	WQCV (ac-ft)	EURV (ac-ft)	100-Year (ac-ft)	Total Required Volume (ac-ft)	Total Preliminary Design Volume * (ac-ft)
Pond A	7562.00	7572.00	0.618	0.476	2.699	3.793	10.504
Pond B	7552.00	7558.00	0.359	0.436	1.110	1.904	2.780
Pond C	7526.00	7534.00	1.577	2.364	4.361	8.302	12.062
Pond D	7530.00	7538.00	1.264	1.127	4.863	7.254	9.082
Pond E	7550.00	7557.00	0.828	1.594	2.032	4.454	6.316
Pond F	7438.00	7446.00	1.768	1.484	7.158	10.409	15.680
Pond G	7442.00	7447.00	0.227	0.210	0.849	1.287	3.045
Pond J	7583.00	7591.00	0.487	1.031	0.751	2.270	2.985
Pond K	7501.00	7511.00	0.554	1.174	0.856	2.584	3.436

Table 3: Preliminary Pond Design Information

The following descriptions of each detention pond are provided to describe outfall locations, emergency spillway routing, and ultimate outfall locations downstream. All pond embankments have been designed to be no greater than 10 feet in height, therefore there are no proposed jurisdictional dams.

Pond outlet locations have been strategically selected and designed to reduce the impact on downstream properties/conditions. Additionally, pond outfalls will have rip-rap to provide energy dissipation which will be analyzed in the future FDR. In the subsequent pond de This should be OS8 locations will be described and This should be DP3 is will be explained.

Pond A (Design Point 1) provides water quality and full-spectrum detention for tributary basins A and OS1. This extended detention basin outfalls due west into Basin OS6, the existing F.H.N. Golf Course, under the adjacent western roadway. The golf course has an existing grass-lined swale that drains due north to its existing Irrigation Pond/Reservoir that was designed and constructed as a part of Filing No. 1. Analysis of this existing pond is included in this report to demonstrate compliance for upstream stormwater detention and ponds in-series. The emergency spillway of this pond is to consist of a rip-rap weir designed for the peak inflow to the pond and is to be directed west toward the Tract located across the street so that emergency stormwater overflow is ultimately directed toward the golf course. Detained stormwater is released in Tract E which then allows flows to enter into an existing swale located in tract L of the Flying

^{*} Total basin volumes include the required 1' of freeboard to top of pond.





Horse Golf Course. Flows travel to the existing irrigation pond and ultimately travel north to be captured in a roadside swale along Hodgen Road.

Pond B (Design Point 7) provides water quality and full-spectrum detention for tributary basin B. This extended detention basin outfalls due north into Basin OS6, the existing F.H.N. Golf Course, under the existing maintenance and golf car path to its north. The golf course has an existing grass-lined swale that drains due north to its existing Irrigation Pond/Reservoir that was designed and constructed as a part of Filing No. 1. Analysis of this existing pond is included in this report to demonstrate compliance for upstream stormwater detention and ponds in-series. The emergency spillway of this pond is to consist of a rip-rap weir designed for the peak inflow to the pond and is to be directed northwest toward the existing golf course swale. Detained stormwater is released in Tract M of the Flying Horse Golf Course and enters an existing swale which travels to Tract L of the golf course. Flows travel to the existing irrigation pond and ultimately travel north to be captured in a roadside swale along Hodgen Road.

Pond C (Design Point 11) provides water quality and full-spectrum detention for tributary basin C. This extended detention basin outfalls due north directly offsite. The emergency spillway of this pond is to consist of a rip-rap weir designed for the peak inflow to the pond and is to be directed northwest, directly offsite. Detained stormwater is released into the headwaters of an existing swale directly north-west of the pond. Flows travel north, off-site, and ultimately are captured in a roadside swale along Hodgen Road.

Pond D (Design Point 13) provides water quality and full-spectrum detention for tributary basin D. This extended detention basin outfalls due north directly offsite. The emergency spillway of this pond consists of a rip-rap weir designed for the peak inflow to the pond and is to be directed northwest, directly offsite. Detained stormwater is released east into a roadside swale along Black Forest Road. Flows ultimately travel north to an unnamed tributary.

Pond E (Design Point 15) provides water quality and full-spectrum detention for tributary basin E which includes the future amenities center with gym/recreation building(s) that has assumed imperviousness described in the proposed basins section. This extended detention basin outfalls due northwest directly offsite into an existing swale that travels north and ultimately is collected in a roadside swale along Hodgen Road. The emergency spillway of this pond is to consist of a rip-rap weir designed for the peak inflow to the pond and is to be directed northwest, directly offsite.

Pond F (Design Point 17) provides water quality and full-spectrum detention for tributary basin F and OS5. This extended detention basin outfalls due north toward Hodgens Road where an existing culvert pipe crosses to the north side of the roadway and is directed offsite. The emergency spillway of this pond is to consist of a rip-rap weir designed for the peak inflow to the pond and is to be directed north, following the same drainage pattern as the outlet pipe.

Pond G (Design Point 15) provides water quality and full-spectrum detention for tributary basin G. This extended detention basin outfalls due north toward Hodgens Road where an existing culvert pipe crosses to the north side of the roadway and is directed offsite. The emergency spillway of this pond is to consist of a rip-rap weir designed for the peak inflow to the pond and is to be directed north, following the same drainage pattern as the outlet pipe.



Pond J (Design Point 18) provides water quality and full-spectrum detention for tributary basin J which is Parcel No. 1, the future commercial golf course club house with parking. Assumed imperviousness and land uses for the parcel are described in the proposed basins section. This extended detention basin outfalls due north to the roadside swale of Old Stagecoach Road which drains due west to an existing culvert pipe crosses to the north side of the roadway and is directed to an existing detention pond that was constructed as a part of Filing No. 1. This pond was designed to detain the runoff from this Parcel as 2.5 acre lots. On-site detention of the commercial development will reduce the runoff from this area to historic rates. The emergency spillway of this pond is to consist of a rip-rap weir designed for the peak inflow to the pond and is to be directed northwest, following the same drainage pattern as the outlet pipe.

Pond K (Design Point 19) provides water quality and full-spectrum detention for tributary basin K which is part of Parcel No. 2 area that is for the future commercial hotel and resort with parking and residential casitas development. Assumed imperviousness and land uses for the parcel are described in the proposed basins section. This extended detention basin outfalls due west directly to Filing No. 1. The downstream existing Pond 8, which was constructed as a part of Filing No. 1, accounted for runoff from this basin as existing undeveloped area. In the final design of this pond, it will be demonstrated that Pond 8 has sufficient capacity for the contributing flow being released from this pond, and that Pond 8 will continue to function as intended and without maintenance deficiencies. On-site detention of the commercial development will reduce the runoff from this area to historic rates, matching that of the assumed runoff rates for Filing No. 1. The emergency spillway of this pond is to consist of a rip-rap weir designed for the peak inflow to the pond and is to be directed west, following the same drainage pattern as the outlet pipe.

d. Existing Tract L Irrigation Pond & Reservoir, Filing No. 1



Per the Flying Horse North Irrigation Reservoir Embankment Design Report, the Existing Tract L Irrigation Pond and Reservoir acts as an irrigation reservoir and detention pond for the golf course and surrounding tributary area as seen in Figure 2.



Figure 2: Existing Tract L Irrigation Pond and Reservoir

The full proposed drainage map is provided in Appendix F. The Flying Horse North Irrigation Design Report can be found in Appendix E.

The development of Parcels 1-6 results in an increase in land density from 2 acre lots to $\frac{1}{2}$ acre residential lots upstream of the irrigation pond. To reduce runoff to historic rates, detention ponds will be added upstream of the reservoir. The table below shows the existing and proposed runoff rates of each basin tributary to the irrigation pond through Tract L.

Table 4: Preliminary Existing and Proposed Runoff Rates

Existing Conditions			Proposed Conditions ¹			
Design Point	Contributing Basins	100 Year Runoff Rate (cfs)	Design Point	Contributing Basins	100 Year Runoff Rate (cfs)	
17	EX17	32.3	25 ¹	OS8	10.5	
18	OS5, DP9, 16, 10	165.9	3 ²	A, OS1	43.1	
8	EX8 & DP27	144.5	5	A2, A1, OS2	117.4	
7	EX7 & DP26	150.9	7 ³	В	22.8	
30	OS8	4.4	9	OS7, OS3	124.7	
	OS6	110.0	20		15.7	
	036			OS6	161.12	
Total 608		Total ⁴		459.3		



1. All proposed runoff rates are from the CUHP model 2. DP 25 100-year runoff rate is FHN Filing No. 3 Pond A's peak discharge rate 2. DP3 100-year runoff rate is proposed Pond A's peak discharge rate 3. DP7 100-year runoff rate is proposed Pond B's discharge rate

4. Value derived from total inflow into irrigation pond per SWMM and accounts for timing of peak runoff rates from basins.

The proposed conditions were modeled in EPA SWMM to ensure the ponds in series meet compliance with Senate Bill 15-212 for drain times and evaluate the storage capacity and outlet structure of the existing irrigation pond. Per the Flying Horse North Irrigation Reservoir Embankment Report, the existing irrigation pond was designed to hold an inflow runoff rate of 609 cfs. The peak has been reduced to 460 cfs. The table below shows the existing and proposed parameters of the irrigation pond.

	North Irrigation Reservoir Design Report Design Values	Proposed Irrigation Pond Design Values
Total Design Inflows (cfs)	609	460
100-Year WSE (ft)	7534.23	7534.98
Peak Discharge (ft)	182	206

Table 5: Irrigation Pond Design Value Comparison

Please note that different hydrologic and hydraulic methods were used when modeling the pond. The FHN Irrigation Reservoir Embankment Design Report uses the SCS Curve Number Method and Pond Pack to design the pond. This differs from the CUHP/ EPA SWMM Modeling approach and will result in different values. CUHP utilizes 1-hr rainfall depths whereas Pond Pack uses 24-hr rainfall depths.

Per discussions with El Paso County, EPA SWMM is an acceptable method to model the poli*Reworded to be mo* peak but higher volume of runoff is a result of the use of the different rainfall depths and met Furthermore, the County has agreed that retrofits will not be required.

appropriate.

Per the model, all pond drain times do not exceed 120 hours and are within compliance for events greater than the 5-year storms outlined in Senate Bill 15-212.

All SWMM results and supporting information is located in Appendix C.

VII. 4-Step Process

In accordance with the Engineering Criteria Manual I.7.2.A and DCM V2, this site has implemented the four-step process to minimize adverse impacts of urbanization. The four-step process includes reducing runoff volumes, stabilizing drainageways, treating the water quality capture volume, and considering the need for Industrial Commercial BMPs. The PDR stage of design for the 4-step process is conceptual in nature and is to be more specifically described within a future FDR when storm system routing at the subbasin level is available.

Step 1 - Reducing Runoff Volumes: The development of the project site includes a variety of land uses including open and vegetated areas interspersed to help disconnect imperious areas and reduce runoff volumes. Single-family residential lots are standardized to include side yard swales that roof runoff drain to via downspouts. Runoff reduction is provided within side yard swales for each lot.



Step 2 – Stabilize Drainageways: Altered drainage ways will be designed in a manner that provides water quality benefits through infiltration and the removal of pollutants via phytoremediation. Vegetation will also be selected to stabilize the drainage ways by reducing the velocity of flows and decreasing any scour. Should the final drainage ways require, grade control structures may be implemented to further reduce flow velocities and protect against erosion. These improvements will help stabilize drainageways.

Step 3 – Provide WQCV: Runoff from this development is treated through capture and slow release of the WQCV via detention ponds that are designed per current El Paso County DCM V2.

Step 4 – Consider the need for Industrial and Commercial BMP's: A site specific storm water quality and erosion control plan and narrative will be prepared with subsequent land use approvals prepared in conjunction with the report prior to any construction. Site specific temporary source control BMPs as well as permanent BMPs are detailed in this plan and narrative. Guidelines detailed in the EI Paso DCM V2 4.2 pertaining to the covering and storage handline and spill containment and control shall be followed as necessary.

VIII. Drawings

Please refer to the appendices for vicinity maps and drainage basin maps.

The drainage maps identify drainage flows entering and leaving the development and general drainage patterns. The maps identify any major construction such as existing and proposed detention facilities, culverts, and preliminarily sited storm sewer infrastructure. The Drainage plans delineate all subbasins and proposed initial and major facilities as well as a provide a summary of all initial and major flow rates at design points. All floodplains effecting the site are shown.

IX. Summary

Flying Horse North is a large master planned community consisting of various densities of dwelling units to include single family homes, multifamily homes, parks, institutional sites, and commercial areas. Due to development, increased runoff will occur. To mitigate downstream impacts, full spectrum detention facilities will be built to reduce the runoff rate to be at or below historic levels. These detention facilities will provide water quality enhancements to account for the increased urbanization of the upstream catchment areas. The ponds are preliminarily sized to ensure that the 5-year and 100-year release rates are equal to or less than the historic rates.

Additional analysis will be required and completed to review the hydraulics of the proposed major drainage channels and sub-basins to be included in a future submittal of an FDR. The proposed design, as described in this report, is not anticipated to cause any adverse impact to downstream properties. Implementation of the four-step process above and any additional measures that are within reason to disconnect impervious areas and increase infiltration should be pursued within a future FDR.

This PDR includes major basin analysis and provides descriptions and calculations for best management practices for stormwater collection and conveyance at the preliminary design stage.

Review C1: Please address the floodplain at the Northwest corner of the site and the requirement to demonstrate baseflood elevations(CLOMR/LOMR) with the final plat application.

Review C2: Unresolved. Please address the above comment. Verify with FEMA as the section within the development may be Zone AE.

Floodpla addresso lift stat was mo outside



X. References

Mile High Flood District Urban Drainage Criteria Manuals, Volumes 1-3

NOAA Atlas 14

NRCS Soil Survey for El Paso County Area, Colorado

FEMA FIRM 08041C0305G and FIRM 08041C0315G (eff. 12/7/2018)

El Paso County Assessor Property Records

El Paso County – Drainage Criteria Manual, 2014

City of Colorado Springs - Drainage Criteria Manual, May 2014

Urban Storm Drainage Criteria Manual, Urban Drainage Flood Control District, January 2018

Preliminary Drainage Report for Flying Horse North Preliminary Plan and Final Drainage Report for Flying Horse North Filing No. 1, Classic Consulting Engineers and Surveyors, November 2017

Flying Horse North Filing No. 3 Final Drainage Report prepared by HR Green Development, LLC. – latest revision August 2023

Flying Horse North Master Development Drainage Plan, HR Green Development, LLC., September 2022

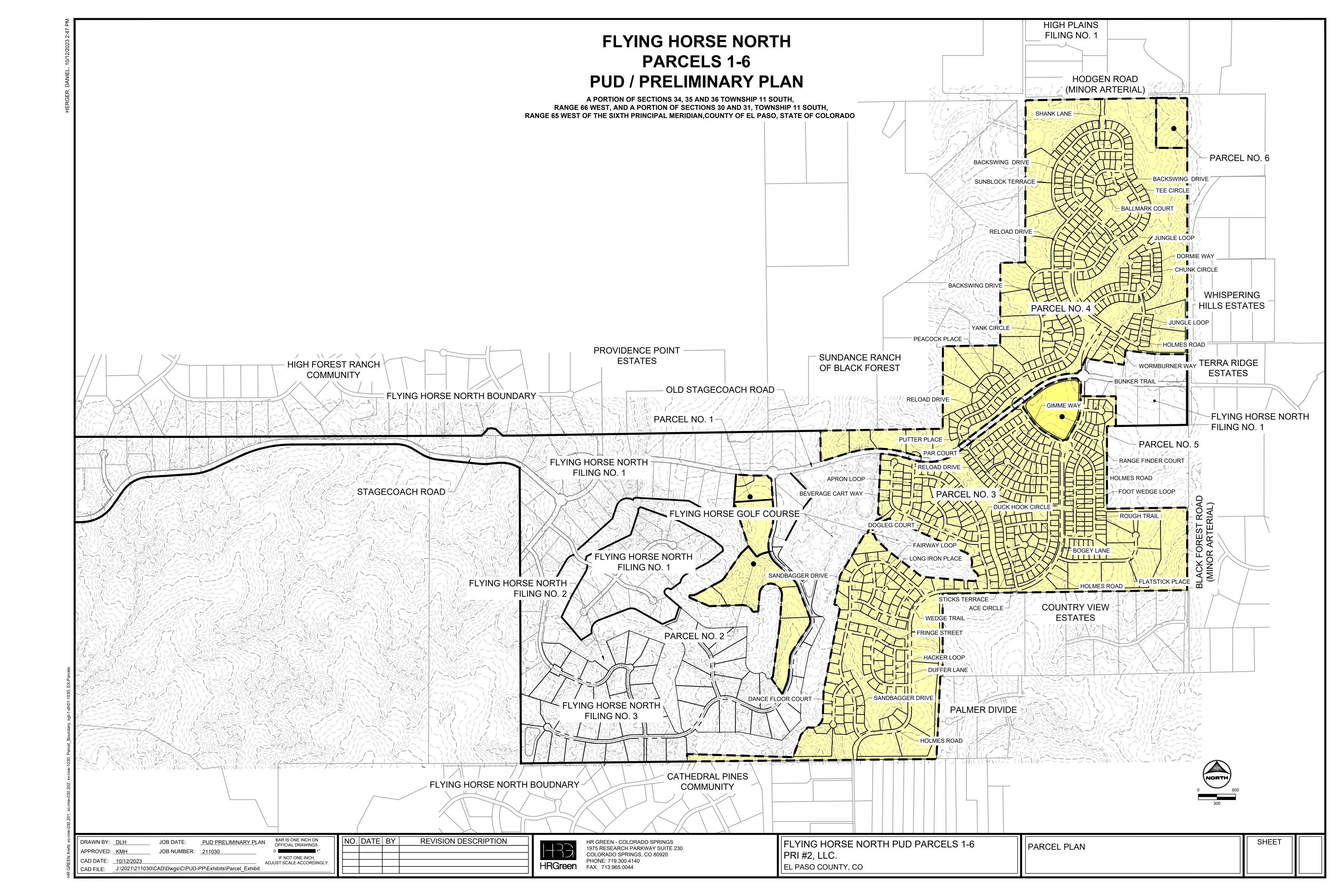
Flying Horse North Irrigation Reservoir Embankment Design Report, Classic Consulting Engineers and Surveyors, August 2018

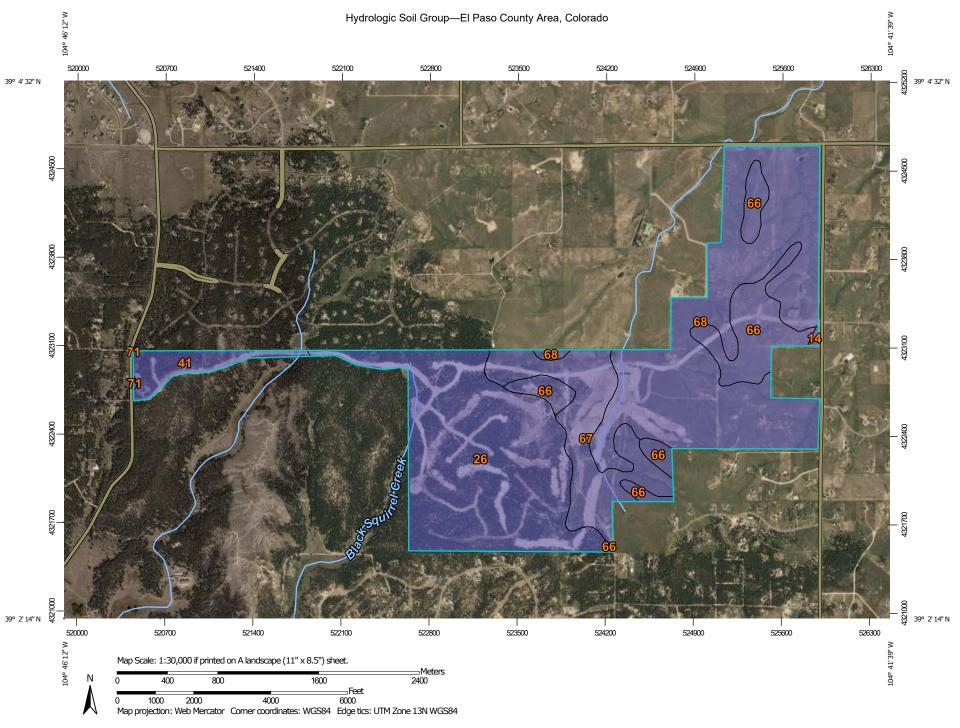
Black Squirrel Drainage Basin Planning Study (DBPS), URS Consultants, January 1989



Appendix A:

Vicinity Map, NRCS Soils Map, and FEMA Floodplain Map





MAP LEGEND MAP INFORMATION The soil surveys that comprise your AOI were mapped at Area of Interest (AOI) С 1:24.000. Area of Interest (AOI) C/D Please rely on the bar scale on each map sheet for map Soils D measurements. Soil Rating Polygons Not rated or not available Α Source of Map: Natural Resources Conservation Service Web Soil Survey URL: **Water Features** A/D Coordinate System: Web Mercator (EPSG:3857) Streams and Canals В Maps from the Web Soil Survey are based on the Web Mercator Transportation projection, which preserves direction and shape but distorts B/D Rails distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more Interstate Highways accurate calculations of distance or area are required. C/D **US Routes** This product is generated from the USDA-NRCS certified data as D Major Roads of the version date(s) listed below. Not rated or not available -Local Roads Soil Survey Area: El Paso County Area, Colorado Soil Rating Lines Survey Area Data: Version 19, Aug 31, 2021 Background Aerial Photography Soil map units are labeled (as space allows) for map scales 1:50.000 or larger. Date(s) aerial images were photographed: Aug 19, 2018—May 26, 2019 B/D The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor C/D shifting of map unit boundaries may be evident. D Not rated or not available **Soil Rating Points** A/D B/D

Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
14	Brussett loam, 1 to 3 percent slopes	В	1.9	0.1%
26	Elbeth sandy loam, 8 to 15 percent slopes	В	474.2	33.7%
41	Kettle gravelly loamy sand, 8 to 40 percent slopes	В	53.4	3.8%
66	Peyton sandy loam, 1 to 5 percent slopes	В	160.9	11.4%
67	Peyton sandy loam, 5 to 9 percent slopes	В	182.8	13.0%
68	Peyton-Pring complex, 3 to 8 percent slopes	В	533.4	37.9%
71	Pring coarse sandy loam, 3 to 8 percent slopes	В	0.6	0.0%
Totals for Area of Inter	rest		1,407.3	100.0%

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

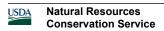
If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

Rating Options

Aggregation Method: Dominant Condition

Component Percent Cutoff: None Specified

Tie-break Rule: Higher



NOTES TO USERS

This map is for use in administering IN Adlonal Flood Insurance Program. It does not necessarily identify all areas subject to flooding, particularly from local drainage sources of small size. The community map repository should be consulted for possible updated or additional flood hazard information.

o obtain more detailed information in greas where Base Flood Flevations (REF To obtain more detailed information in areas where Base Flood Elevations (REEs) and/or floodways have been determined, users are encouraged to consult the Flood and/or floodways have been determined, users are encouraged to consult the Flood insurance. Suby (FIS) report that encompanies this FIRM. Users should be aware that BFEs shown in the FIRM represent rounded whether obtained be waren that BFEs shown in the FIRM represent rounded whether obtained be waren that BFEs shown in the FIRM representation. Accordingly, food elevation, state and the FIRM representation. Accordingly, food elevation data presented in the FIRM representation, and the FIRM or proposed or construction and/or flood/glin management.

Coastal Base Flood Elevations shown on this map apply only landward of 0.0" North American Vertical Datum of 1980 (VAVDSB). Users of this FIRM invoid be aware table in the Flood Invariance Study report for the jurisdiction. Elevations shown in the Summary of Sillivater Elevations table should be used for construction and/or bookland management purposes when they are higher than the elevations shown on

Boundaries of the **floodways** were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations with regard to requirements of the National Flood Insurance Program. In Goodway widths and other pertinent floodway data are provided in the Flood Insurance Study report for this invisrience.

Certain areas not in Special Flood Hazard Areas may be protected by **flood contro** structures. Refer to section 2.4 "Flood Protection Measures" of the Flood Insuranci Study report for information on flood control structures for this jurisdiction.

The projection used in the preparation of this map was Universal Transverse Mercatic (UTM) zone 13. The horizontal datum was MADS, GR-650 opherod. GR-650 opherod. The production of Filter for adjust in significant production of Filter for adjusted instructions may result in sight positional differences in map features across jurisdiction boundaries. These differences do not affect the accuracy of this FIRM.

Flood elevations on this map are referenced to the North American Vertical Datus of 1988 (NAVD8). These flood elevations must be compared to structure as ground elevations referenced to the same vertical datum. For information regarding conversion between the National Geodetic Vertical Datum of 1929 and the Nort American Vertical Datum of 1939, with the National Geodetic Survey website http://www.ngs.nosa.govi or contact the National Geodetic Survey with the Solitowin addresse:

NGS Information Services NOAA, N/NGS12 NOAA, N/NGS12 National Geodetic Survey SSMC-3, #9202 1315 East-West Highway Silver Spring, MD 20910-3282

o obtain current elevation, description, and/or location information for bench man hown on this map, please contact the Information Services Branch of the Natio Seodetic Survey at (301) 713-3242 or visit its website at http://www.ngs.noaa.gov/.

Base Map information shown on this FIRM was provided in digital format by EI Paso County, Colorado Springs Utilities, City of Fountain, Bureau of Land Management, National Coeanic and Armospheric Administration, United States Geological Survey, and Anderson Consulting Engineers, Inc. These data are current as of 2006.

This map reflects not be detailed and up-to-date stream channel configurations and floodplain delineations than those shown on the previous FIRM for this princidion. The floodplains and floodplain delineations than floos shown on the previous FIRM for this princidion. The floodplains and floodplain floodpla

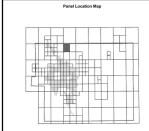
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Please refer to the separately printed Map Index for an overview map of the county showing the layout of map panels, community map repository addresses; and a Listing of Communities take containing National Flood Insurance Program dates for each community as well as a listing of the panels on which each community is located.

Contact FEMA Map Service Center (MSC) via the FEMA Map Information eXchange (FMX), 1-87-338-2627 for information on available products associated with this Post of the Contact of Contac

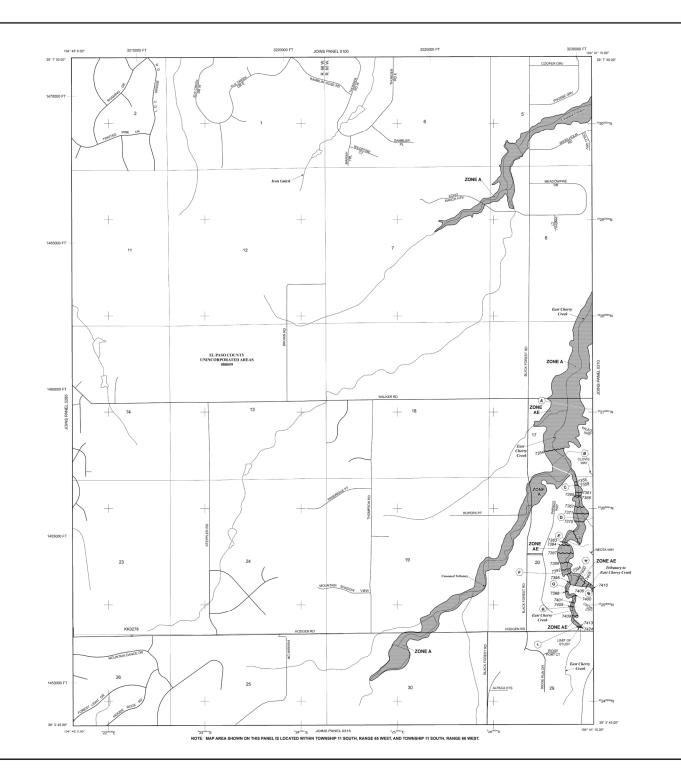
If you have questions about this map or questions concerning the National Floor insurance Program in general, please call 1-877-FEMA MAP (1-877-336-2627) or wist the FEMA website at http://www.fema.gov/businessynfip.

Flooding Source REFER TO SECTION 3.3 OF THE EL PASO COUNTY FLOOD INSURANCE STUDY FOR STREAM BY STREAM VERTICAL DATUM CONVERSION INFORMATION



This Digital Flood Insurance Rate Map (DFIRM) was produced through a Cooperating Technical Partner (CTP) agreement between the State of Colorado Water Conservation Board (CWCB) and the Federal Emergency Management Agency (FEMA).





LEGEND

The 1% annual chance flood (1,00-year flood), also known as the base flood, is the flood that has a 1% chance of being equated or exceeded in any given year. The Special Flood hazard Area is the area subject to flooding by the 1% annual chance flood. Areas of Special Flood Hazard include zones A, AE, AH, AD, AR, A99, V, and VE. The Base Flood Benedion is the water-surface elevation of the 1% annual chance flood.

ZONE AE ZONE AH

No Base Flood Elevations determined.
Base Flood Elevations determined.
Flood depths of 1 to 3 feet (usually areas of ponding); Base Flood Elevations determined.

Flood depths of 1 to 3 feet (usually sheet flow on sloping terrain); average depths determined. For areas of alluvial fan flooding, velocities also determined.

Special Road Hazard Area Formerly protected from the 1% annual chance flood by a flood control system that was subsequently decertified. Zone AP indicates that the former flood control system is being restored to provide protection from the 1% annual chance or greater flood. Area to be protected from 1% annual chance flood by a Federal flood protection system under construction; no Base Flood Elevations determined.

ZONE V Coastal flood zone with velocity hazard (wave action); no Base Flood Bevations determined.

ZONE VE Coastal flood zone with velocity hazard (wave action); Base Flood Elevations determined.

FLOODWAY AREAS IN ZONE AE

OTHER FLOOD AREAS

Areas of 0.2% annual chance flood; areas of 1% annual chance flood with average depths of less than 1 foot or with drainage areas less than 1 square mile; and areas protected by levees from 1% annual chance flood. ZONE X

OTHER AREAS

Areas determined to be outside the 0.2% annual chance floodplai Areas in which flood hazards are undetermined, but possible.

COASTAL BARRIER RESOURCES SYSTEM (CBRS) AREAS

OTHERWISE PROTECTED AREAS (OPAs)

Floodolain boundary

Zone D Boundary

..... CRPS and ORA boundar Boundary dividing Special Flood Hazard Areas of differ Flood Elevations, flood depths or flood velocities.

~~ 512 ~~ Base Flood Elevation line and value: elevation in feet* Base Flood Elevation value where uniform within zone; elevation in feet*

(A)—(A)

23-----23

Geographic coordinates referenced to the North American Datum of 1983 (NAD 83) 97° 07' 30.00" 32° 22' 30.00"

DX5510_

M1.5

NEATION PALIFICO OD HINSULA VANCETPAKO

MAP REPOSITORIES Refer to Map Repositories list on Map Index

For community map revision history prior to countywide mapping, refer to the Common Map History Table located in the Flood Insurance Study report for this jurisdiction. To determine if flood insurance is available in this community, contact your insurance agent or call the National Flood Insurance Program at 1-800-638-6620.

MAP SCALE 1" = 1000" 500 0 1000 HHH H

PANEL 0305G

COLORADO

FIRM FLOOD INSURANCE RATE MAP EL PASO COUNTY,

AND INCORPORATED AREAS

PANEL 305 OF 1300

(SEE MAP INDEX FOR FIRM PANEL LAYOUT)

NUMBER PANEL SUFFIX COMMUNITY

MAP NUMBER



DECEMBER 7, 2018

Federal Emergency Management Agency

NOTES TO USERS

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Costal Base Flood Elevations shown on this map apply only landward of 0.0' North American Vertical Datum of 1988 (NAVD88). Users of this FIRM should be ware that costal flood elevations are also provided in the Summary of Sillivate Elevations table in the Flood Insurance Study report for this jurisdiction. Elevations shown in the Summary of Sillivate Elevations table should be used for construction and/or floodplain management purposes when they are higher than the elevations shown on this FIRM.

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Flood elevations on this map are referenced to the North American Vertical Datu of 1988 (RAVD88). These food elevations must be compared to structure an gound elevations referenced to this same vertical datum. For information regardin American Vertical Datum. 1989, with the National Geodetic Survey website. 18tb://www.nps.ncas.govi or contact the National Geodetic Survey website.

NGS Information Services NOAA, N/NGS12 NOAA, N/NGS12 National Geodetic Survey SSMC-3, #9202 1315 East-West Highway Silver Spring, MD 20910-3282

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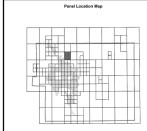
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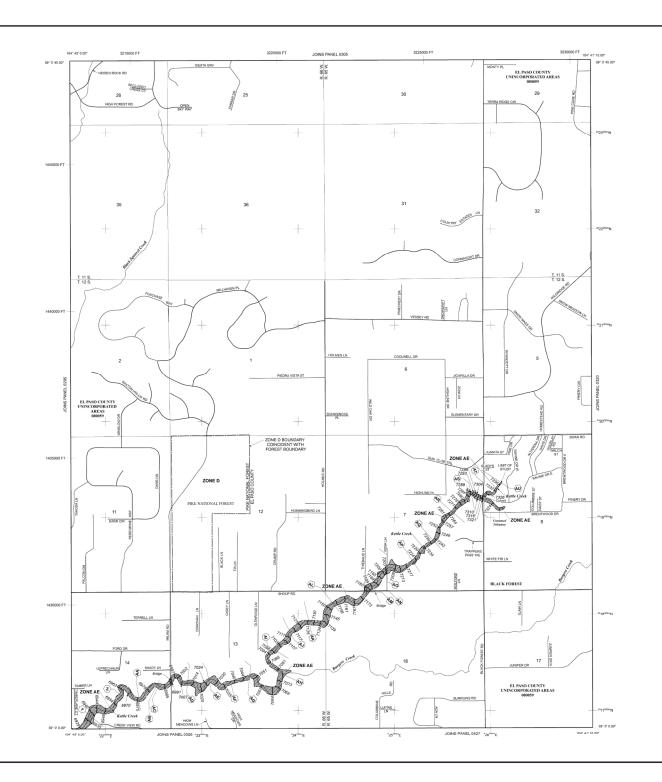
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LEGEND

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ZONE AE ZONE AH

No Base Rood Elevations determined.
Base Rood Elevations determined.
Rood elevations determined.
Rood elevations determined.
Rood elevation determined.

Flood depths of 1 to 3 feet (usually sheet flow on sloping terrain); average depths determined. For areas of alluvial fan flooding, velocities also determined.

Area to be protected from 1% annual chance flood by a Federal flood protection system under construction; no Base Flood Elevations determined.

ZONE V Coastal flood zone with velocity hazard (wave action); no Base Flood Elevations determined. ZONE VE Coastal flood zone with velocity hazard (wave action); Base Flood Flevetions determined.

FLOODWAY AREAS IN ZONE AE

Areas of 0.2% annual chance flood; areas of 1% annual chance flood with average depths of less than 1 foot or with drainage areas less than 1 square mile; and areas protected by levees from 1% annual chance flood. ZONE X

OTHER AREAS

Areas determined to be outside the 0.2% annual chance floodpla

Areas in which flood hazards are undetermined, but possible COASTAL BARRIER RESOURCES SYSTEM (CBRS) AREAS

OTHERWISE PROTECTED AREAS (OPAs)

Floodolain boundary Zone D Boundary

..... CRPS and ORA houndary

~~ 512 ~~ Data Flood Elevation line and value: elevation in fact?

 $\langle A \rangle \longrightarrow \langle A \rangle$

23----23

Geographic coordinates referenced to the North American Datum of 1983 (NAD 83) 97" 07" 30.00" 32" 22" 30.00"

M1.5

<u> APAHANINAH THOODHINANINAHAN AN</u>

To determine if flood insurance is available in this community, contact your insurance agent or call the National Flood Insurance Program at 1-800-638-6620.

MAP SCALE 1" = 1000" 500 0 1000 HHH H

PANEL 0315G

FIRM

FLOOD INSURANCE RATE MAP EL PASO COUNTY, COLORADO AND INCORPORATED AREAS

PANEL 315 OF 1300

(SEE MAP INDEX FOR FIRM PANEL LAYOUT)

CONTAINS: NUMBER PANEL SUFFIX

COMMUNITY



MAP NUMBER 08041C0315G

DECEMBER 7, 2018 Federal Emergency Management Agency





Appendix B:

Hydrologic Calculations



Calc'd by:

Checked by:

Date:

RDL 1/8/2024

DLH

SUMMARY RUNOFF TABLE										
BASIN	AREA (ac)	% IMP.	C ₅	C ₁₀₀	Q ₅ (cfs)	Q ₁₀₀ (cfs)				
EX1	12.4	4.2	0.11	0.37	4.3	24.9				
EX2	0.8	2.0	0.08	0.35	0.3	2.2				
EX3	1.5	2.0	0.08	0.35	0.6	4.3				
EX4	16.5	2.0	0.08	0.35	4.3	31.4				
EX5	6.4	2.0	0.08	0.35	2.0	14.6				
EX5.1	7.4	2.0	0.08	0.35	1.8	13.0				
EX6	13.7	2.0	0.08	0.35	3.9	28.8				
EX7	64.7	2.0	0.08	0.35	14.7	108.1				
EX8	41.6	2.0	0.08	0.35	9.7	71.1				
EX9	21.7	2.0	0.08	0.35	6.0	44.2				
EX10	7.6	2.0	0.08	0.35	2.2	16.4				
EX11	55.3	2.0	0.08	0.35	13.7	100.7				
EX12	27.5	2.0	0.08	0.35	6.8	49.6				
EX13	20.0	2.0	0.08	0.35	5.4	39.8				
EX14	12.2	2.0	0.08	0.35	3.3	24.2				
EX15	90.1	2.0	0.08	0.35	21.6	158.5				
EX16	8.0	2.0	0.08	0.35	2.3	16.6				
EX17	15.6	2.0	0.08	0.35	4.4	32.3				
EX18	5.4	2.0	0.08	0.35	1.4	10.4				
EX19	5.4	2.0	0.08	0.35	1.5	11.3				
EX20	14.9	2.0	0.08	0.35	4.2	30.5				
EX21	48.4	2.0	0.08	0.35	14.1	103.8				
EX22	24.6	2.0	0.08	0.35	6.7	49.3				
EX23	164.4	2.0	0.08	0.35	44.3	325.4				
EX24	17.3	2.0	0.08	0.35	3.3	24.0				
EX25	42.7	2.0	0.08	0.35	11.2	82.1				
OS1	19.0	5.1	0.12	0.37	7.9	42.7				
OS2	36.4	5.0	0.12	0.37	13.5	73.4				
OS3	25.3	3.0	0.09	0.36	8.2	53.9				
OS4	72.3	7.0	0.14	0.39	28.8	134.6				
OS5	41.2	6.5	0.13	0.39	16.2	78.3				
OS6	83.6	2.5	0.09	0.35	16.0	110.0				
OS7	20.1	2.0	0.08	0.35	4.7	34.9				
OS8	8.0	58.1	0.55	0.70	3.8	4.4				
OS9	9.4	90.2	0.82	0.90	27.4	50.6				
TOTAL ONSITE	746.0	2.04%	0.08	0.35	193.9	1417.2				
TOTAL OFFSITE	315.2	8.54%	0.14	0.40	126.6	582.8				
TOTAL	1061.2	3.97%	0.10	0.36	320.5	2000.0				

	DESIGN	POINT	SUMMAR	RY TABLE	
DESIGN POINT	CONTRIBUTING BASINS	ΣQ ₅ (cfs)	ΣQ ₁₀₀ (cfs)	Tributary Area (ac.)	Weighted % Impervious
1	EX1	4.3	24.9	12.4	4.23
2	EX2	0.3	2.2	0.8	2.00
3	EX3	0.6	4.3	1.5	2.00
4	EX4	4.3	31.4	16.5	2.00
5	EX5	2.0	14.6	6.4	2.00
5.1	EX5.1	1.8	13.0	7.4	2.00
6	EX6	3.9	28.8	13.7	2.00
7	EX7 & DP26	22.7	150.9	83.6	2.70
8	EX8 & DP27	23.2	144.5	78.0	3.39
9	EX9	6.0	44.2	21.7	2.00
10	EX10 & DP28	10.5	70.3	32.9	2.76
11	EX11 & DP29	42.5	235.3	127.6	4.83
12	EX12	6.8	49.6	27.5	2.00
13	EX13	5.4	39.8	20.0	2.00
14	EX14 & 1/3RD OS9	12.4	41.0	15.3	20.02
15	EX15 & 1/3RD OS9	30.7	175.3	93.3	4.96
16	EX16	2.3	16.6	8.0	2.00
17	EX17	4.4	32.3	15.6	2.00
18	OS5, DP9, 16, 10	23.5	165.9	82.6	1.39
19	EX18, EX19, DP31	7.0	203.7	374.2	3.57
20	EX20 & DP15	34.9	205.9	108.2	1.94
21	EX21 & DP14	26.6	144.9	63.8	1.90
22	EX22	6.7	49.3	24.6	2.00
23	EX23, DP13 &32	65.9	443.4	184.4	2.00
24	EX24	3.3	24.0	17.3	2.00
25	EX25	11.2	82.1	42.7	2.00
26	OS1	7.9	42.7	19.0	5.06
27	OS2	13.5	73.4	36.4	4.99
28	OS3	8.2	53.9	25.3	2.99
29	OS4	28.8	134.6	72.3	7.00
30	OS8	3.8	4.4	20.1	2.00
31	OS6, DP7, 8, 17, 18, 30	102.7	624.8	363.5	3.61
32	OS5	16.2	78.3	41.2	6.47
	TOTAL	320.5	2000.0	1061.2	3.97%



FLYING HORSE NORTH - PARCELS 1-6	Calc'd by:	DLH
EXISTING CONDITIONS	Checked bv:	RDL
EL PASO COUNTY, COLORADO	Date	1/8/2024

1/8/2024 COMPOSITE 'C' FACTORS OPEN SPACE / RESIDENTIAL (5 COMPOSITE ROADWAY / OPEN SPACE / **RESIDENTIAL (5** ROADWAY / TOTAL **IMPERVIOUSNESS & C BASIN LAWN** AC LOT) **PAVEMENT** SOIL TYPE **LAWN** AC LOT) **PAVEMENT** C₁₀₀ C₅ **ACRES %**I C₅ % **%**I C₁₀₀ C₁₀₀ C₅ C₁₀₀ 6.84 5.52 0.00 12.36 В 2 0.08 0.35 0.14 0.39 100 0.90 0.96 4.2 0.11 0.37 EX1 EX2 0.80 0.00 0.00 0.80 В 2 0.08 0.35 0.14 0.39 100 0.90 0.96 2.0 0.08 0.35 2 FX3 1 48 0.00 0.00 1 48 В 0.08 0.35 7 0.14 0.39 100 0.90 0.96 2.0 0.08 0.35 16.53 0.00 0.00 16.53 2 100 0.08 EX4 В 80.0 0.35 7 0.14 0.39 0.90 0.96 2.0 0.35 7 EX5 6.36 0.00 0.00 6.36 В 2 80.0 0.35 0.14 0.39 100 0.90 0.96 2.0 0.08 0.35 EX5.1 7.37 0.00 0.00 7.37 В 2 0.08 0.35 0.39 100 0.90 0.96 0.08 0.35 7 0.14 2.0 EX6 13.74 0.00 0.00 13.74 В 2 0.08 0.35 0.14 0.39 100 0.90 0.96 2.0 0.08 0.35 EX7 64.65 0.00 0.00 64.65 В 2 0.08 0.35 0.14 0.39 100 0.90 0.96 2.0 0.08 0.35 EX8 41.56 0.00 0.00 41.56 В 2 0.08 0.35 0.14 0.39 100 0.90 0.96 2.0 0.08 0.35 21.68 21.68 EX9 0.00 0.00 В 2 0.35 7 0.14 0.39 0.90 0.96 2.0 0.08 0.35 0.08 100 **EX10** 7.62 0.00 0.00 7.62 В 2 0.08 0.35 0.14 0.39 100 0.90 0.96 2.0 0.08 0.35 EX11 55.34 0.00 0.00 55.34 В 2 0.08 0.35 0.14 0.39 100 0.90 0.96 2.0 0.08 0.35 EX12 27.47 0.00 0.00 27.47 В 2 0.08 0.35 0.14 0.39 100 0.90 0.96 0.08 2.0 0.35 **EX13** 19.98 0.00 0.00 19.98 2 7 0.14 100 0.90 В 0.08 0.35 0.39 0.96 2.0 0.08 0.35 2 EX14 12.20 0.00 0.00 12.20 В 80.0 0.35 7 0.14 0.39 100 0.90 0.96 2.0 0.08 0.35 EX15 90.14 0.00 0.00 90.14 В 2 80.0 0.35 7 0.14 0.39 100 0.90 0.96 2.0 0.08 0.35 0.00 **EX16** 8.02 0.00 8.02 В 2 0.08 0.35 0.14 0.39 100 0.90 0.96 2.0 0.08 0.35 **EX17** 15.59 0.00 0.00 15.59 В 2 0.08 0.35 0.14 0.39 100 0.90 0.96 2.0 0.08 0.35 0.00 **EX18** 5.35 0.00 5.35 В 2 0.08 0.35 0.14 0.39 100 0.90 0.96 2.0 0.08 0.35 5 35 2 FX19 5.35 0.00 0.00 В 0.08 0.35 7 0.14 0.39 100 0.90 0.96 2.0 0.08 0.35 **EX20** 0.00 0.00 14.89 2 100 0.08 14.89 В 0.08 0.35 7 0.14 0.39 0.90 0.96 2.0 0.35 FX21 48 43 0.00 0.00 48 43 В 2 0.08 0.35 7 0.14 0.39 100 0.90 0.96 20 0.08 0.35 EX22 0.00 24.63 0.00 24.63 В 2 0.08 0.35 7 0.14 0.39 100 0.90 0.96 2.0 0.08 0.35 164.44 0.00 0.00 164.44 0.96 2.0 0.35 EX23 В 2 80.0 0.35 7 0.14 0.39 100 0.90 0.08 EX24 17.27 0.00 0.00 17.27 В 2 0.08 0.35 0.14 0.39 100 0.90 0.96 2.0 0.08 0.35 EX25 42.71 0.00 0.00 42.71 В 2 0.08 0.35 0.14 0.39 100 0.90 0.96 2.0 0.08 0.35 7.36 11.63 0.00 18.99 2 0.14 0.39 100 0.90 OS1 В 0.08 0.35 0.96 5.1 0.12 0.37 OS₂ 14.65 21.74 0.00 36.39 В 2 0.08 0.35 0.14 0.39 100 0.90 0.96 5.0 0.12 0.37 OS₃ 20.25 5.00 0.00 25.25 В 2 0.08 0.35 7 0.14 0.39 100 0.90 0.96 3.0 0.09 0.36 72.29 OS4 0.00 0.00 72.29 В 2 0.08 0.35 0.14 0.39 100 0.90 0.96 7.0 0.14 0.39 OS₅ 4.37 36.87 0.00 41.24 В 2 0.08 0.35 0.14 0.39 100 0.90 0.96 6.5 0.13 0.39 OS7 20.07 0.00 0.00 20.07 В 2 0.08 0.35 0.14 0.39 100 0.90 0.96 2.0 0.08 0.35 OS8 3.42 0.00 4.58 В 2 7 0.14 0.39 100 0.90 0.96 0.55 8.00 0.08 0.35 58.1 0.70 OS₆ 74.56 9.00 0.00 83.56 В 2 80.0 0.35 7 0.14 0.39 100 0.90 0.96 2.5 0.09 0.35 OS9 0.94 0.00 8.46 9.40 В 2 0.08 0.35 0.14 0.39 100 0.90 0.96 90.2 0.82 0.90 740.44 5.52 **TOTAL ONSITE** 0.00 745.96 0.08 0.35 0.14 0.39 100 0.90 0.96 2.04 0.08 0.35 **TOTAL OFFSITE** 145.62 156.53 13.04 315.19 2 0.08 0.35 0.14 0.39 100 0.90 0.96 8.54 0.40 0.14 **GRAND TOTAL** 886.06 162.05 13.04 1061.15 0.08 0.35 0.14 0.39 100 0.90 0.96 3.97 0.10 0.36



FLYING HORSE NORTH - PARCELS 1-6 EXISTING CONDITIONS

EL PASO COUNTY, COLORADO

Calc'd by:	DLH
Checked by:	RDL
Date:	1/8/2024

					TIME	OF CON	CENTRAT	ION					
BAS	IN DATA		OVERI	LAND TIM	E (T _i)		TRAV	EL TIME (T_t)		TOTAL	tc=(L/180)+10	Design to
DESIGNATION	C ₅	AREA (ac)	LENGTH (ft)	SLOPE %	t _i (min)	C _V	LENGTH (ft)	SLOPE %	V (ft/s)	t _t (min)	t _c (min)	tc max	tc design (min)
EX1	0.11	12.36	300	2.2	24.3	7	1100	2.3	1.1	17.3	41.5	17.8	17.8
EX2	0.08	0.80	100	21.0	6.8	7	100	20.0	3.1	0.5	7.3	11.1	7.3
EX3	0.08	1.48	25	5.0	5.5	7	25	5.0	1.6	0.3	5.7	10.3	5.7
EX4	0.08	16.53	300	10.3	14.9	7	1180	5.9	1.7	11.6	26.5	18.2	18.2
EX5	0.08	6.36	200	16.0	10.5	7	200	16.0	2.8	1.2	11.7	12.2	11.7
EX5.1	0.08	7.37	270	6.7	16.3	7	1770	2.0	1.0	29.8	46.1	21.3	21.3
EX6	0.08	13.74	300	13.8	13.5	7	510	7.8	2.0	4.3	17.9	14.5	14.5
EX7	0.08	64.65	300	5.0	18.9	7	2130	2.0	1.0	35.9	54.8	23.5	23.5
EX8	0.08	41.56	300	8.0	16.2	7	1950	2.5	1.1	29.4	45.6	22.5	22.5
EX9	0.08	21.68	300	3.0	22.5	7	700	4.0	1.4	8.3	30.8	15.6	15.6
EX10	0.08	7.62	300	6.4	17.4	7	370	3.6	1.3	4.6	22.1	13.7	13.7
EX11	0.08	55.34	300	6.6	17.3	7	1480	2.2	1.0	23.8	41.0	19.9	19.9
EX12	0.08	27.47	300	7.1	16.9	7	1540	4.9	1.5	16.6	33.4	20.2	20.2
EX13	0.08	19.98	300	3.4	21.5	7	850	3.3	1.3	11.1	32.7	16.4	16.4
EX14	0.08	12.20	300	5.1	18.8	7	880	4.9	1.5	9.5	28.3	16.6	16.6
EX15	0.08	90.14	300	11.1	14.5	7	1740	5.5	1.6	17.7	32.2	21.3	21.3
EX16	0.08	8.02	300	5.7	18.1	7	600	5.3	1.6 6.2		24.3	15.0	15.0
EX17	0.08	15.59	300	6.9	17.0	7	980	5.7 1.6		6.2	23.2	15.0	15.0
EX18	0.08	5.35	300	7.0	16.9	7	480	4.7	1.7	9.8	26.7	17.1	17.1
EX19	0.08	5.35	300	5.0	18.9	7	660	5.3	1.5	5.3	24.2	14.3	14.3
EX20	0.08	14.89	300	6.1	17.7	7	380	3.9	1.6	6.8	24.6	15.3	15.3
EX21	0.08	48.43	300	7.0	16.9	7	820	4.6	1.4	4.6	21.5	13.8	13.8
EX22	0.08	24.63	300	8.3	16.0	7	890	4.0	1.5	9.1	25.1	16.2	16.2
EX23	0.08	164.44	300	4.5	19.6	7	3730	3.0	1.4	10.6	30.2	16.6	16.6
EX24	0.08	17.27	300	9.2	15.5	7	1090	3.8	1.2	51.3	66.7	32.4	32.4
EX25	0.08	42.71	300	9.2	15.5	7	1200	3.9	1.4	13.3	28.8	17.7	17.7
OS1	0.12	18.99	300	5.5	17.7	7	500	6.6	1.8	4.6	22.3	14.4	14.4
OS2	0.12	36.39	300	5.8	17.4	7	1213	4.9	1.5	13.0	30.4	18.4	18.4
OS3	0.09	25.25	300	5.7	17.9	7	540	7.3	1.9	4.8	22.7	14.7	14.7
OS4	0.14	72.29	300	6.1	16.7	7	2140	4.0	1.4	25.5	42.2	23.6	23.6
OS5	0.13	41.24	300	5.0	17.9	7	1900	5.0	1.6	20.2	38.2	22.2	22.2
OS7	0.08	20.07	280	9.0	15.0	15	1850	2.8	2.5	12.3	27.3	21.8	21.8
OS8	0.55	8.00	OVERR	IDDEN		20	OVERR	IDDEN	0.0				
OS6	0.09	83.56	300	7.0	16.8	15	4350	3.0	2.6	27.9	44.7	35.8	35.8
OS9	0.82	9.40	15	2	1.6	15	1650	2	2.1	13.0	14.6	19.3	14.6

FORMULAS:

$$t_i = \frac{0.395(1.1 - C_5)\sqrt{L}}{S^{0.33}}$$
 $V = C_{\nu}S_{\nu}^{0.5}$

Table 6-7. Conveyance Coefficient, C_{ν}

Type of Land Surface	C_{ν}
Heavy meadow	2.5
Tillage/field	5
Riprap (not buried)*	6.5
Short pasture and lawns	7
Nearly bare ground	10
Grassed waterway	15
Paved areas and shallow paved swales	20

^{*}For buried riprap, select C_v value based on type of vegetative cover.



FLYING HORSE NORTH - PARCELS 1-6	Calc'd by:	DLH
EXISTING CONDITIONS	Checked by	:RDL
DESIGN STORM: 5-YEAR	Date:	1/8/2024

3.266076143

			3.266076143																				
			DIRECT RUNOFF TOTAL RUNOFF							OVERLAND PIPE TF							TR	AVEL .	ГІМЕ	REMARKS			
STREET	DESIGN POINT	BASIN ID	AREA (ac)	Ce	t _c (min)	C ₅ *A (ac)	/ (in./ hr.)	Q (cfs)	t _c (min)	C ₅ *A (ac)	/ (in./ hr.)	Q (cfs)	Q _{street} (cfs)	C₅*A (ac)	% adons	Q _{PIPE} (cfs)	C ₅ *A (ac)	SLOPE %	PIPE SIZE (FT)	LENGTH (FT)	VEL. (FPS)	TRAVEL TIME (min	
	1	EX1	12.36	0.11	17.8	1.32	3.27	4.3															DRAINS EAST INTO ALLEN RANCH ROAD
	2	EX2	0.80	0.08	7.3	0.06	4.60	0.3															DRAINS WEST OFF INTO GOLF COURSE TRACT
	3	EX3	1.48	0.08	5.7	0.12	4.96	0.6															DRAINS SOUTH WEST INTO EX4
	4	EX4	16.53	0.08	18.2	1.32	3.23	4.3													1	1	DRAINS SOUTH WEST INTO FLYING HORSE GOLF COURSE TRACT
	_	EV.E	0.00	0.00	44.7	0.54	0.00	0.0															
-	5	EX5	6.36	0.08	11.7	0.51	3.90	2.0													1	1	DRAINS WEST INTO FLYING HORSE GOLF COURSE
	5.1	EX5.1	7.37	0.08	21.3	0.59	2.99	1.8															BASIN DRAINS EAST INTO ALLEN RANCH ROAD
-	3.1	EAG.1	1.31	0.06	21.3	0.59	2.99	1.0													+	+	BASIN DIVAINS EAST INTO ALLEIN MINCH NOAD
	6	EX6	13.74	0.08	14.5	1.10	3.57	3.9															DRAINS SOUTH WEST OFFSITE INTO EDMONDS SUBDIVISION
		LAU	13.74	0.00	14.5	1.10	0.01	5.5													1	1	BIGAING GOOTH WEST OFF SITE INTO EDMONDO GODDIVIDON
	7	EX7	64.65	0.08	23.5	5.17	2.85	14.7		7.39		22.7											BASIN & OS1 COLLECT INTO EX. TERTIARY DRAINAGE SWALE, FLOWS TO NORTHWEST TO DP7
		L/(I	04.00	0.00	20.0	0.17	2.00	14.7		7.00		22.1									1	1	Brown & Got Cotted in the Data Text and Data
	8	EX8	41.56	0.08	22.5	3.32	2.91	9.7		7.54		23.2											BASIN & OS2 COLLECT INTO EX. TERTIARY DRAINAGE SWALE, FLOWS TO NORTHWEST TO DP8
	Ť			0.00		0.02	2.01	0.7		7.01		20.2											
	9	EX9	21.68	0.08	15.6	1.73	3.47	6.0															DRAINS NORTH WEST INTO OS7
	10	EX10	7.62	0.08	13.7	0.61	3.65	2.2		2.93		10.5											EX10 & OS3 COLLECT INTO EX NATURAL DRAINAGE SWALE AND INTO OS7
	11	EX11	55.34	0.08	19.9	4.43	3.10	13.7		14.55		42.5											SHEET FLOWS EAST INTO BLACK FOREST ROAD
	12	EX12	27.47	0.08	20.2	2.20	3.07	6.8															SHEET FLOWS EAST OFFSITE
	13	EX13	19.98	0.08	16.4	1.60	3.39	5.4															SHEET FLOWS NORTH-EAST INTO CULVERT AT DP13
																		l			1	1	
	14	EX14	12.20	0.08	16.6	0.98	3.37	3.3		3.54		12.4									1	1	SHEET FLOWS NORTH INTO CULVERT AT DP14 + ONE THIRD OF FLOWS FROM OS9
	!																	l			1	1	SHEET FLOWS AND COLLECTS INTO NATURAL DRAINAGE SWALE, FLOWS NORTH TO CULVERT @ DP15
	15	EX15	90.14	0.08	21.3	7.21	2.99	21.6		9.77		30.7						<u> </u>			<u> </u>	<u> </u>	+ ONE THRID OF FLOWS FROM OS9



FLYING HORSE NORTH - PARCELS 1-6	Calc'd by:	DLH
EXISTING CONDITIONS	Checked by	:RDL
DESIGN STORM: 5-YEAR	Date:	1/8/2024

3.266076143

			<u></u>	3.266076143																			
					DIRECT	RUN	OFF		Т	OTAL F	RUNOF	F	OVERLAND PIPE TRAVE								AVEL '	TIME	REMARKS
STREET	DESIGN POINT	BASIN ID	AREA (ac)	້	t _c (min)	C ₅ *A (ac)	/ (in./ hr.)	Q (cfs)	t _c (min)	C ₅ *A (ac)	/ (in./ hr.)	Q (cfs)	Q _{street} (cfs)	C ₅ *A (ac)	SLOPE %	Q _{PIPE} (cfs)	C ₅ *A (ac)	SLOPE %	PIPE SIZE (FT)	LENGTH (FT)	VEL. (FPS)	TRAVEL TIME (min	
	16	EX16	8.02	0.08	15.0	0.64	3.52	2 2.3															SHEET FLOWS SOUTH-WEST INTO OS7
	10	LXIO	0.02	0.00	13.0	0.04	3.32	2.5															GILETTEONS GOTTI-WEST INTO GOT
	17	EX17	15.59	0.08	15.0	1.25	3.52	4.4															SHEET FLOWS WEST INTO OS6
	40		ļ							0.04		00.5											DD IO OLIMILI ATRIE OF DDO 40 40 AND 007
-	18		1					1		6.91		23.5									1	1	DP IS CUMULATIVE OF DP9, 16, 10 AND OS7
		EX18	5.35	0.08	17.1	0.43	3.32	1.4															SHEET FLOWS EAST INTO EX NATURAL DRAINAGE SWALE THAT FLOWS NORTH OFF-SITE
		EX19	5.35	0.08	14.3	0.43	3.59	1.5															SHEET FLOWS WEST INTO EX NATURAL DRAINAGE SWALE THAT FLOWS NORTH OFF-SITE
	19							1		35.56		7.0											DP19 HAS BEEN OVERRIDDEN TO SHOW RELEASE FLOWS FROM THE JD DESIGN + EX18 AND EX19
	13									33.30		7.0											BI 13 TIAG BEEN OVERVIBBEN TO GLOW NEEDAGE LEGWOT NOW THE 8B BEGION - EXTO AND EXTO
	20	EX20	14.89	0.08	15.3	1.19	3.49	4.2		10.97		34.9											SHEEET FLOWS COLLECT INTO NATURAL DRAINAGE SWALE AT DP20
		E1/0/	10.10		40.0																		
-	21	EX21	48.43	0.08	13.8	3.87	3.65	14.1		7.41		26.6						-	-			1	SHEET FLOWS COLLECT INTO NATURAL DRAINAGE SWALE , FLOWS NORTH OFF-SITE
	22	EX22	24.63	0.08	16.2	1.97	3.40	6.7															SHEET FLOWS NORTH WEST OFF-SITE
	23	EX23	164.44	0.08	16.6	13.16	3.37	44.3		20.27		65.9											SHEET FLOWS COLLECT INTO MULTIPLE NATURAL SWALES THAT FLOW NORTH TO HODGEN ROAD
	24	EX24	17.27	0.08	32.4	1.38	2.37	3.3															FLOWS NORTH TO HODGEN ROAD
-	24	LAZ4	17.27	0.00	32.4	1.50	2.31	3.3											1		+	1	TEOWO NONTH TO HOBBELT TOAD
	25	EX25	42.71	0.08	17.7	3.42	3.27	11.2															FLOWS NORTH-WEST OFF-SITE TO HODGEN ROAD
-	26	OS1	18.99	0.12	14.4	2.22	3.58	7.9											-				FLOWS NORTH-WEST INTO SITE AT DP26 INTO EX7
	27	OS2	36.39	0.12	18.4	4.22	3.21	13.5															FLOWS NORTH-WEST INTO SITE AT DP27 INTO EX8
		002	00.00	0.12	10.1		0.2	10.0															
	28	OS3	25.25	0.09	14.7	2.32	3.55	8.2															FLOWS NORTH INTO SITE AT DP28 INTO EX10
	29	OS4	72.29	0.14	23.6	10.12	2.04	28.8															FLOWS NORTH-EAST TO DP29 AND INTO EX11
	29	034	12.29	0.14	23.0	10.12	2.04	20.0											-				FLOWS NORTH-EAST TO DE29 AND INTO EXTT
	32	OS5	41.24	0.13	22.2	5.51	2.93	16.2															FLOWS NORTH, THROUGH EX CULVERT UNDER O.S.R. INTO EX23
	<u> </u>	OS7	20.07	0.08	21.8	1.61	2.96	4.7													1	1	SHEET FLOWS INTO EX SWALE THROUGH GOLF COURSE. COMBINED FLOWS IN DP18
	30	OS8	8.00	0.55		4.40		1				3.8									1		OS6 IS ENTIRELY CAPTURED WITHIN AN EXISTING POND IN FHN FILING 3 RELEASED AT HISTORIC RATES AS CALCULATED IN F.H.N. FILING 3
	30	000	0.00	0.55		7.70						5.0							-		 		SHEET FLOWS INTO MULTIPLE EX SWALES IN GOLF COURSE, LEADS DOWN TO
		OS6	83.56	0.09	35.8	7.22	2.21	16.0		9.79		25.1											IRRIGATION RESERVOIR
	_																						DP31 REPRESENTS RELEASE FROM IRRIGATIONAL RESERVIOR (OVERRIDDEN BY DESIGN RELEASE)
	31	<u> </u>	 					1		34.71		102.7									1	1	CUMULATIVE OF BASIN OS6, OS9, AND DP7, 8, 17, 18, 30 RUNOFF FROM OLD STAGECOACH ROAD HAS BEEN SPLIT INTO THIRDS FOR SIMPLICITY
		OS9	9.40	0.82	14.6	7.69	3 57	27.4													1		ENTERING DP14, DP15, AND OS6
		000	∂.+0	0.02	17.0	1.09	5.51	21.4											1				ENTERMOOD 14, DI 10, AND 000



FLYING HORSE NORTH - PARCELS 1-6	Calc'd by: DLH
EXISTING CONDITIONS	Checked by: RDL
DESIGN STORM: 100-YEAR	Date: 1/8/2024

HR	Gre	en																					
				D	IRECT	RUNC	FF		Т	OTAL F	RUNOF	F	ov	ERLA	ND		PI	PE		TR	AVEL		REMARKS
STREET	DESIGN PONT	BASIN ID	AREA (ac)	C ₁₀₀	<i>t_c (</i> min)	C ₁₀₀ *A (ac)	/ (in./ hr.)	Q (cfs)	t _c (min)	C ₁₀₀ *A (ac)	/ (in./ hr.)	Q (cfs)	Q _{street} (cfs)	C ₁₀₀ *A (ac)	SLOPE %	Q _{PIPE} (cfs)	C ₁₀₀ *A (ac)	SLOPE %	PIPE SIZE (ft)	LENGTH (ft)	VEL. (ft/s)	TRAVEL TIME (min)	
	1	EX1	12.36	0.37	17.8	4.55	5.48	24.9															DRAINS EAST INTO ALLEN RANCH ROAD
		E)/0	0.00	0.05		0.00																	PRINCE WEST SET INTO COLE COLUMN TO LOT
	2	EX2	0.80	0.35	7.3	0.28	7.72	2.2															DRAINS WEST OFF INTO GOLF COURSE TRACT
	3	EX3	1.48	0.35	5.7	0.52	8.33	4.3															DRAINS SOUTH WEST INTO EX4
	4	EX4	10.50	0.25	40.0	F 70	F 40	24.4	-														DDAING COUTHWEST INTO FLYING HODGE COLE COUDSE TRACT
	4	EX4	16.53	0.35	18.2	5.79	5.42	31.4															DRAINS SOUTH WEST INTO FLYING HORSE GOLF COURSE TRACT
	5	EX5	6.36	0.35	11.7	2.23	6.54	14.6															DRAINS WEST INTO FLYING HORSE GOLF COURSE
	5.1	EX5.1	7.37	0.35	21.3	2.58	5.02	13.0															BASIN DRAINS EAST INTO ALLEN RANCH ROAD
	5.1	L/(0.1	7.57	0.55	21.0	2.50	3.02	10.0															STORES OF THE STREET OF THE ST
	6	EX6	13.74	0.35	14.5	4.81	6.00	28.8															DRAINS SOUTH WEST OFFSITE INTO EDMONDS SUBDIVISION
	7	EX7	64.65	0.35	23.5	22.63	4.78	108.1	-	29.74		150.9											BASIN & OS1 COLLECT INTO EX. TERTIARY DRAINAGE SWALE, FLOWS TO NORTHWEST TO DP7
	8	EX8	41.56	0.35	22.5	14.55	4.89	71.1		28.15		144.5											BASIN & OS2 COLLECT INTO EX. TERTIARY DRAINAGE SWALE, FLOWS TO NORTHWEST TO DP8
	9	EX9	21.68	0.35	15.6	7.59	5.82	44.2															DRAINS NORTH WEST INTO OS7
		E)///0	7.00	0.05	40.7	0.07	0.14	10.1		44.70		70.0											EVAN A COS COLLECTIVITO EVANTURAL ROLLINGE RIVALE AND INTO COL
	10	EX10	7.62	0.35	13.7	2.67	6.14	16.4		11.70		70.3											EX10 & OS3 COLLECT INTO EX NATURAL DRAINAGE SWALE AND INTO OS7
	11	EX11	55.34	0.35	19.9	19.37	5.20	100.7		47.56		235.3											SHEET FLOWS EAST INTO BLACK FOREST ROAD
	12	EX12	27.47	0.35	20.2	9.61	5.16	49.6															SHEET FLOWS EAST OFFSITE
	12	LXIZ	21.41	0.33	20.2	9.01	5.10	43.0															GILETT EONG EAGT OF GILE
	13	EX13	19.98	0.35	16.4	6.99	5.69	39.8															SHEET FLOWS NORTH-EAST INTO CULVERT AT DP13
	14	EX14	12.20	0.35	16.6	4.27	5.66	24.2	-	7.09		41.0											SHEET FLOWS NORTH INTO CULVERT AT DP14 + ONE THIRD OF FLOWS FROM OS9
							5.00			7.50		0											SHEET FLOWS AND COLLECTS INTO NATURAL DRAINAGE SWALE, FLOWS NORTH TO CULVERT @ DP15
-	15	EX15	90.14	0.35	21.3	31.55	5.02	158.5		34.37		175.3							ļ				+ ONE THRID OF FLOWS FROM OS9
	16	EX16	8.02	0.35	15.0	2.81	5.91	16.6															SHEET FLOWS SOUTH-WEST INTO OS7



FLYING HORSE NORTH - PARCELS 1-6	Calc'd by:	DLH
EXISTING CONDITIONS	Checked by	RDL
DESIGN STORM: 100-YEAR	Date:	1/8/2024

יחח	ai e	CII																					
				0	DIRECT	T RUN	OFF		Т	OTAL I	RUNOF	F	0\	/ERLA	ND		PI	PE		TR	AVEL 1	ГІМЕ	REMARKS
STREET	DESIGN PONT	BASIN ID	AREA (ac)	C ₁₀₀	t _c (min)	C ₁₀₀ *A (ac)	/ (in./ hr.)	Q (cfs)	t _c (min)	C ₁₀₀ *A (ac)	/ (in./ hr.)	Q (cfs)	Q _{street} (cfs)	C ₁₀₀ *A (ac)	% 3401 S	Q _{PIPE} (cfs)	C ₁₀₀ *A (ac)	% 3401S	PIPE SIZE (ft)	LENGTH (ft)	VEL. (ft/s)	TRAVEL TIME (min)	
	17	EX17	15.59	0.35	15.0	5.46	5.91	32.3	2														SHEET FLOWS WEST INTO OS6
	- 17	LXII	13.39	0.55	13.0	3.40	3.9	32.0	,														SHEET FEOWS WEST INTO 030
	18									29.12		165.9											DP IS CUMULATIVE OF DP9, 16, 10 AND OS7
		EV40	5.05	0.05	47.4	4.07		10.4															CUEFT FLOWO FACT INTO EVALUATIONAL PRAINAGE OWALF THAT FLOWS MODILLOFF OUT
		EX18	5.35	0.35	17.1	1.87	5.58	10.4								1					1		SHEET FLOWS EAST INTO EX NATURAL DRAINAGE SWALE THAT FLOWS NORTH OFF-SITE
		EX19	5.35	0.35	14.3	1.87	6.03	3 11.3	3														SHEET FLOWS WEST INTO EX NATURAL DRAINAGE SWALE THAT FLOWS NORTH OFF-SITE
	19							-		131.42		203.7											DP19 HAS BEEN OVERRIDDEN TO SHOW RELEASE FLOWS FROM THE JD DESIGN + EX18 AND EX19
	20	EX20	14.89	0.35	15.3	5.21	5.86	30.5	5	39.58		205.9											SHEEET FLOWS COLLECT INTO NATURAL DRAINAGE SWALE AT DP20
	21	EX21	48.43	0.35	13.8	16.95	6.12	103.8	3	24.04		144.9											SHEET FLOWS COLLECT INTO NATURAL DRAINAGE SWALE , FLOWS NORTH OFF-SITE
	22	EX22	24.63	0.35	16.2	8.62	5.71	49.3	3														SHEET FLOWS NORTH WEST OFF-SITE
		LAZZ	24.00	0.00	10.2	0.02	0.7	70.0													1		
	23	EX23	164.44	0.35	16.6	57.55	5.65	325.4	Į.	80.46		443.4											SHEET FLOWS COLLECT INTO MULTIPLE NATURAL SWALES THAT FLOW NORTH TO HODGEN ROAD
	24	EX24	17.27	0.35	32.4	6.04	3.97	7 24.0	,														FLOWS NORTH TO HODGEN ROAD
	24	EA24	11.21	0.33	32.4	0.04	3.91	24.0	1														PLOWS NORTH TO HODGEN ROAD
	25	EX25	42.71	0.35	17.7	14.95	5.49	82.1	Ī														FLOWS NORTH-WEST OFF-SITE TO HODGEN ROAD
-	26	OS1	18.99	0.37	14.4	7.11	6.01	42.7													 		FLOWS NORTH-WEST INTO SITE AT DP26 INTO EX7
	27	OS2	36.39	0.37	18.4	13.61	5.40	73.4	ı														FLOWS NORTH-WEST INTO SITE AT DP27 INTO EX8
-	28	OS3	25.25	0.36	14.7	9.04	5.97	53.9	9												1		FLOWS NORTH INTO SITE AT DP28 INTO EX10
	29	OS4	72.29	0.39	23.6	28.19	4.77	134.6	5														FLOWS NORTH-EAST TO DP29 AND INTO EX11
	32	OS5	41.24	0.39	22.2	15.91	4.92	78.3	3														FLOWS NORTH, THROUGH EX CULVERT UNDER O.S.R. INTO EX23
		OS7	20.07	0.35	21.8	7.02	4.96	34.9	1														SHEET FLOWS INTO EX SWALE THROUGH GOLF COURSE. COMBINED FLOWS IN DP18
		007	20.01	0.00	21.0	1.02	7.50	, 54.5															OS6 IS ENTIRELY CAPTURED WITHIN AN EXISTING POND IN FHN FILING 3
	30	OS8	8.00	0.70		5.59						4.4											RELEASED AT HISTORIC RATES AS CALCULATED IN F.H.N. FILING 3
		000	00.50	0.25	25.0	20.64	0.70	140.0	-	20.40		100.0											SHEET FLOWS INTO MULTIPLE EX SWALES IN GOLF COURSE, LEADS DOWN TO IRRIGATION RESERVOIR
1		OS6	83.56	0.35	35.8	29.61	3.72	110.0	J	32.42		126.9				1							IRRIGATION RESERVOIR DP31 REPRESENTS RELEASE FROM IRRIGATIONAL RESERVIOR (OVERRIDDEN BY DESIGN RELEASE)
	31									127.67		624.8											CUMULATIVE OF BASIN OS6, OS9, AND DP7, 8, 17, 18, 30
																							RUNOFF FROM OLD STAGECOACH ROAD HAS BEEN SPLIT INTO THIRDS FOR SIMPLICITY
		OS9	9.40	0.90	14.6	8.45	5.99	50.6	6														ENTERING DP14, DP15, AND OS6



FLYING HORSE NORTH PARCELS 1-6 PROPOSED CONDITIONS HRGreen EL PASO COUNTY, COLORADO

Calc'd by:	DLH
Checked by:	RDL
Date:	10/30/2023

A 74.1 15.0 0.17 0.42 38.9 1 A1 12.6 7.0 0.14 0.39 6.0 2 A2 6.5 13.1 0.15 0.40 3.4 B 32.7 24.1 0.22 0.45 24.6 8 C 121.0 31.6 0.26 0.47 81.4 2 D 86.2 26.8 0.23 0.45 54.8 1 E 52.4 43.7 0.37 0.55 67.7 1 F 197.5 15.7 0.19 0.43 95.9 3 G 27.3 16.4 0.16 0.41 16.4 6 H 74.0 7.0 0.14 0.39 37.6 1 I 7.1 26.4 0.23 0.46 6.1 2 J 15.8 86.1 0.74 0.83 59.8 1 K 18.0 86.0 0.74 0.83 64.4 1 L 7.1 57.8	
A1 12.6 7.0 0.14 0.39 6.0 2 A2 6.5 13.1 0.15 0.40 3.4 7 B 32.7 24.1 0.22 0.45 24.6 8 C 121.0 31.6 0.26 0.47 81.4 2 D 86.2 26.8 0.23 0.45 54.8 1 E 52.4 43.7 0.37 0.55 67.7 1 F 197.5 15.7 0.19 0.43 95.9 3 G 27.3 16.4 0.16 0.41 16.4 6 H 74.0 7.0 0.14 0.39 37.6 1 I 7.1 26.4 0.23 0.46 6.1 2 J 15.8 86.1 0.74 0.83 59.8 1 K 18.0 86.0 0.74 0.83 64.4 1 L 7.1 57.8 0.52 0.67 19.0 2 OS1 19.0	₀ (cfs)
A2 6.5 13.1 0.15 0.40 3.4 6.5 B 32.7 24.1 0.22 0.45 24.6 8 C 121.0 31.6 0.26 0.47 81.4 2 D 86.2 26.8 0.23 0.45 54.8 1 E 52.4 43.7 0.37 0.55 67.7 1 F 197.5 15.7 0.19 0.43 95.9 3 G 27.3 16.4 0.16 0.41 16.4 6 H 74.0 7.0 0.14 0.39 37.6 1 I 7.1 26.4 0.23 0.46 6.1 2 J 15.8 86.1 0.74 0.83 59.8 1 K 18.0 86.0 0.74 0.83 64.4 1 L 7.1 57.8 0.52 0.67 19.0 4 M 5.0 57.8 0.52 0.67 19.0 4 OS1 19.0	61.6
B 32.7 24.1 0.22 0.45 24.6 8 C 121.0 31.6 0.26 0.47 81.4 2 D 86.2 26.8 0.23 0.45 54.8 1 E 52.4 43.7 0.37 0.55 67.7 1 F 197.5 15.7 0.19 0.43 95.9 3 G 27.3 16.4 0.16 0.41 16.4 6 H 74.0 7.0 0.14 0.39 37.6 1 I 7.1 26.4 0.23 0.46 6.1 2 J 15.8 86.1 0.74 0.83 59.8 1 K 18.0 86.0 0.74 0.83 64.4 1 L 7.1 57.8 0.52 0.67 19.0 2 M 5.0 57.8 0.52 0.67 9.9 2 OS1 19	29.0
C 121.0 31.6 0.26 0.47 81.4 2 D 86.2 26.8 0.23 0.45 54.8 1 E 52.4 43.7 0.37 0.55 67.7 1 F 197.5 15.7 0.19 0.43 95.9 3 G 27.3 16.4 0.16 0.41 16.4 6 H 74.0 7.0 0.14 0.39 37.6 1 I 7.1 26.4 0.23 0.46 6.1 2 J 15.8 86.1 0.74 0.83 59.8 1 K 18.0 86.0 0.74 0.83 64.4 1 L 7.1 57.8 0.52 0.67 19.0 2 M 5.0 57.8 0.52 0.67 9.9 2 OS1 19.0 2.0 0.08 0.35 5.6 2 OS2 36	5.3
D 86.2 26.8 0.23 0.45 54.8 1 E 52.4 43.7 0.37 0.55 67.7 1 F 197.5 15.7 0.19 0.43 95.9 3 G 27.3 16.4 0.16 0.41 16.4 6 H 74.0 7.0 0.14 0.39 37.6 1 I 7.1 26.4 0.23 0.46 6.1 2 J 15.8 86.1 0.74 0.83 59.8 1 K 18.0 86.0 0.74 0.83 64.4 1 L 7.1 57.8 0.52 0.67 19.0 2 M 5.0 57.8 0.52 0.67 9.9 2 OS1 19.0 2.0 0.08 0.35 5.6 2 OS2 36.4 2.0 0.08 0.35 6.8 2 OS4 72.3 2.0 0.08 0.35 18.3 1	86.1
E 52.4 43.7 0.37 0.55 67.7 1 F 197.5 15.7 0.19 0.43 95.9 3 G 27.3 16.4 0.16 0.41 16.4 6 H 74.0 7.0 0.14 0.39 37.6 1 I 7.1 26.4 0.23 0.46 6.1 2 J 15.8 86.1 0.74 0.83 59.8 1 K 18.0 86.0 0.74 0.83 64.4 1 L 7.1 57.8 0.52 0.67 19.0 4 M 5.0 57.8 0.52 0.67 9.9 2 OS1 19.0 2.0 0.08 0.35 5.6 4 OS2 36.4 2.0 0.08 0.35 9.2 6 OS3 25.3 2.0 0.08 0.35 6.8 4 OS4 72.3 2.0 0.08 0.35 18.3 1	51.4
F 197.5 15.7 0.19 0.43 95.9 3 G 27.3 16.4 0.16 0.41 16.4 6 H 74.0 7.0 0.14 0.39 37.6 1 I 7.1 26.4 0.23 0.46 6.1 2 J 15.8 86.1 0.74 0.83 59.8 1 K 18.0 86.0 0.74 0.83 64.4 1 L 7.1 57.8 0.52 0.67 19.0 2 M 5.0 57.8 0.52 0.67 9.9 2 OS1 19.0 2.0 0.08 0.35 5.6 2 OS2 36.4 2.0 0.08 0.35 9.2 6 OS3 25.3 2.0 0.08 0.35 6.8 2 OS4 72.3 2.0 0.08 0.35 18.3 1	77.1
G 27.3 16.4 0.16 0.41 16.4 6 H 74.0 7.0 0.14 0.39 37.6 1 I 7.1 26.4 0.23 0.46 6.1 2 J 15.8 86.1 0.74 0.83 59.8 1 K 18.0 86.0 0.74 0.83 64.4 1 L 7.1 57.8 0.52 0.67 19.0 2 M 5.0 57.8 0.52 0.67 9.9 2 OS1 19.0 2.0 0.08 0.35 5.6 2 OS2 36.4 2.0 0.08 0.35 9.2 6 OS3 25.3 2.0 0.08 0.35 6.8 2 OS4 72.3 2.0 0.08 0.35 18.3 1	71.0
H 74.0 7.0 0.14 0.39 37.6 1 I 7.1 26.4 0.23 0.46 6.1 2 J 15.8 86.1 0.74 0.83 59.8 1 K 18.0 86.0 0.74 0.83 64.4 1 L 7.1 57.8 0.52 0.67 19.0 4 M 5.0 57.8 0.52 0.67 9.9 2 OS1 19.0 2.0 0.08 0.35 5.6 4 OS2 36.4 2.0 0.08 0.35 9.2 6 OS3 25.3 2.0 0.08 0.35 18.3 1 OS4 72.3 2.0 0.08 0.35 18.3 1	66.3
I 7.1 26.4 0.23 0.46 6.1 2 J 15.8 86.1 0.74 0.83 59.8 1 K 18.0 86.0 0.74 0.83 64.4 1 L 7.1 57.8 0.52 0.67 19.0 4 M 5.0 57.8 0.52 0.67 9.9 2 OS1 19.0 2.0 0.08 0.35 5.6 4 OS2 36.4 2.0 0.08 0.35 9.2 6 OS3 25.3 2.0 0.08 0.35 6.8 4 OS4 72.3 2.0 0.08 0.35 18.3 1	8.4
J 15.8 86.1 0.74 0.83 59.8 1 K 18.0 86.0 0.74 0.83 64.4 1 L 7.1 57.8 0.52 0.67 19.0 2 M 5.0 57.8 0.52 0.67 9.9 2 OS1 19.0 2.0 0.08 0.35 5.6 2 OS2 36.4 2.0 0.08 0.35 9.2 6 OS3 25.3 2.0 0.08 0.35 6.8 2 OS4 72.3 2.0 0.08 0.35 18.3 1	80.4
K 18.0 86.0 0.74 0.83 64.4 1 L 7.1 57.8 0.52 0.67 19.0 2 M 5.0 57.8 0.52 0.67 9.9 2 OS1 19.0 2.0 0.08 0.35 5.6 2 OS2 36.4 2.0 0.08 0.35 9.2 6 OS3 25.3 2.0 0.08 0.35 6.8 2 OS4 72.3 2.0 0.08 0.35 18.3 1	20.7
L 7.1 57.8 0.52 0.67 19.0 4 M 5.0 57.8 0.52 0.67 9.9 2 OS1 19.0 2.0 0.08 0.35 5.6 4 OS2 36.4 2.0 0.08 0.35 9.2 6 OS3 25.3 2.0 0.08 0.35 6.8 4 OS4 72.3 2.0 0.08 0.35 18.3 1	12.4
M 5.0 57.8 0.52 0.67 9.9 2 OS1 19.0 2.0 0.08 0.35 5.6 4 OS2 36.4 2.0 0.08 0.35 9.2 6 OS3 25.3 2.0 0.08 0.35 6.8 4 OS4 72.3 2.0 0.08 0.35 18.3 1	21.2
OS1 19.0 2.0 0.08 0.35 5.6 4 OS2 36.4 2.0 0.08 0.35 9.2 6 OS3 25.3 2.0 0.08 0.35 6.8 4 OS4 72.3 2.0 0.08 0.35 18.3 1	1.1
OS2 36.4 2.0 0.08 0.35 9.2 6 OS3 25.3 2.0 0.08 0.35 6.8 2 OS4 72.3 2.0 0.08 0.35 18.3 1	21.3
OS3 25.3 2.0 0.08 0.35 6.8 4 OS4 72.3 2.0 0.08 0.35 18.3 1	1.3
OS4 72.3 2.0 0.08 0.35 18.3 1	67.9
	9.9
OS5 412 65 013 039 159 7	34.5
555 F1.2 5.0 5.10 5.00 10.0	'8.8
	43.5
	57.7
	4.4
TOTAL ONSITE 747.3 24.6% 0.24 0.46 585.8 18	323.4
TOTAL OFFSITE 313.9 5.4% 0.11 0.38 93.3 5	77.8
TOTAL 1061.2 18.9% 0.20 0.44 679.1 24	01.2

	CUMULATIVE DESIG	N POIN	T SUMMA	ARY TABLE	Ē
DESIGN POINT	CONTRIBUTING BASINS	ΣQ_5 (cfs)	ΣQ ₁₀₀ (cfs)	Tributary Area (ac.)	Weighted % Impervious
1	A, OS1 (portions)	14.5	69.1	31.7	11.1%
2	A, OS1 (portions)	14.5	69.1	31.7	11.1%
3	A, OS1	44.5	202.8	93.1	12.3%
4	A1, OS2	15.3	96.9	49.0	3.3%
5	A1, A2, OS2	18.7	112.2	55.5	4.4%
6	A1, A2, I, OS2, OS3, OS6, OS7 + Outlet Q's of A, B, Pond A (Fil. 3)	72.1	459.3	217.7	5.4%
7	В	24.6	86.1	32.7	24.1%
8	OS3	6.8	49.9	25.3	2.0%
9	OS3, OS7	17.4	107.6	53.5	4.7%
10	С	81.4	251.4	121.0	31.6%
11	С	81.4	251.4	121.0	31.6%
12	OS4	18.3	134.5	72.3	2.0%
13	D, OS4	73.1	311.6	158.5	15.5%
14	E (portion)	33.8	85.5	26.2	43.7%
15	E	67.7	171.0	52.4	43.7%
16	OS5	15.9	78.8	41.2	6.5%
17	F, OS5	111.8	445.1	238.7	14.1%
18	G	16.4	68.4	27.3	16.4%
19	Н	37.6	180.4	74.0	7.0%
20	I	6.1	20.7	7.1	26.4%
21	J	59.8	112.4	15.8	86.1%
22	K	64.4	121.2	18.0	86.0%
23	L	19.0	41.1	7.1	57.8%
24	M	9.9	21.3	5.0	57.8%
25	OS8	3.8	4.4	8.0	58.1%
	*FINAL Q5 AND 100 OF DESIGN POINT 6 WILL REG	QUIRE DETERMIN	ATION OF OUTLET P	EAK FLOWS AS DESIGNI	ED IN FUTURE FDR

*PRELIMINARY OUTLET STRUCTURE CALCS AND RELEASE RATES ARE INCLUDED IN THIS REPORT, SEE POND A AND POND B CALCS



FLYING HORSE NORTH PARCELS 1-6 PROPOSED CONDITIONS

Calc'd by: DLH

Checked by: RDL

EL PASO COUNTY, COLORADO

Date: 10/19/2023

									CO	MPOSI	TE 'C' FAC	CTORS	;																				
	OPEN SPACE /		ROADWAY /	RESIDENTIAL			RESIDENTIAL					OPEN	SPAC	E /	MAREDO		ROAD	WAY /	RES	IDENTI.	AL RE	SIDENTIA	AL RESI	DENTIA	RESIDE	NTIAL	RESIDE	NTIAL	RESIDE	NTIAL	CC	OMPOSITE	
BASIN	LAWN	COMMERCIAL	PAVEMENT	(5 AC LOT)	(2.5 AC LOT)	(1/2-AC LOT)	(1/3-AC LOT)	(1/4-AC LOT)	(1/8-AC LOT)	TOTAL	SOIL TYPE	L	.AWN	CO	MMERC	IAL	PAVE	MENT	(5	AC LOT) (2.	5 AC LOT	r) L (*	1/2-AC	(1/3-AC	S LOT)	(1/4-AC	LOT)	(1/8-AC	LOT)	IMPERV	/IOUSNES	S & C
					ACRES							% I	C ₅	C ₁₀₀ %I	C ₅ C	100	%I (C ₅ C ₁₀									%I C ₅				%I	C ₅	C ₁₀₀
A	12.50			27.35		27.15	7.11			74.11	В	2	0.08	0.35 95	0.81 0	0.88		.90 0.9	96 7	0.14 0.	39 11	0.17 0.4	12 25 0	.22 0.46	30 0.2	5 0.47	40 0.30	0.50	65 0.45	5 0.59	15.0		0.42
A1				12.58						12.58	В	2	0.08	0.35 95	0.81 0	0.88	100 0.	.90 0.9	96 7	0.14 0.	39 11	0.17 0.4	12 25 0	.22 0.46	30 0.2	5 0.47	40 0.30	0.50 f	65 0.45	5 0.59	7.0		0.39
A2	3.95						2.58			6.53	В	2	0.08	0.35 95	0.81 0	0.88	100 0.	.90 0.9	96 7	0.14 0.	39 11	0.17 0.4	12 25 0	.22 0.46	30 0.2'	5 0.47	40 0.30	0.50 F	65 0.45	5 0.59	13.1	0.15	0.40
В	1.70			3.25		14.20	13.54			32.69	В	2	0.08	0.35 95	0.81 0	0.88	100 0.	.81 0.8	38 7	0.14 0.	39 11	0.17 0.4	12 25 0	.22 0.46	30 0.2	5 0.47	40 0.30	0.50 f	65 0.45	5 0.59	24.1		0.45
С	29.76		3.56			6.47		81.24		121.03	В	2	0.08	0.35 95	0.81 0	0.88	100 0.	.81 0.8	88 7	0.14 0.	39 11	0.17 0.4	12 25 0	.22 0.46	30 0.2	5 0.47	40 0.30	0.50 f	65 0.45	5 0.59	31.6		0.47
D	24.04			29.10				3.58	29.44	86.16	В	2	0.08	0.35 95	0.81 0	0.88	100 0.	.81 0.8	88 7	0.14 0.	39 11	0.17 0.4	12 25 0	.22 0.46	30 0.2	5 0.47	40 0.30	0.50 f	65 0.45	5 0.59	26.8		0.45
E	14.30	11.04	2.15					24.87		52.36	В	2	0.08	0.35 95	0.81 0	0.88	100 0.	.81 0.8	88 7	0.14 0.	39 11	0.17 0.4	12 25 0	.22 0.46	30 0.25	5 0.47	40 0.30	0.50 f	65 0.45	5 0.59	43.7		0.55
F	76.45	9.18			96.02				15.80	197.45	В	2	0.08	0.35 95	0.81 0	0.88	100 0.	.81 0.8	88 7	0.14 0.	39 11	0.17 0.4	12 25 0	.22 0.46	30 0.2	5 0.47	40 0.30	0.50 f	65 0.45	0.59 ز	15.7		0.43
G	16.98							10.32		27.30	В	2	0.08	0.35 95	0.81 0	1.88	100 0.	.81 0.8	38 7	0.14 0.	39 11	0.17 0.4	12 25 0	.22 0.46	30 0.25	5 0.47	40 0.30	0.50 F	65 0.45	ا 0.59 اذ	16.4		0.41
Н				74.02						74.02	В	2	0.08	0.35 95	0.81 0	1.88	100 0.	.81 0.8	88 7	0.14 0.	39 11	0.17 0.4	12 25 0	.22 0.46	30 0.25	5 0.47	40 0.30	0.50 F	65 0.45	0.59 ز	7.0		0.39
	0.56					2.06	4.51			7.13	В	2	0.08	0.35 95	0.81 0	1.88	100 0.	.81 0.8	88 7	0.14 0.	39 11	0.17 0.4	12 25 0	.22 0.46	30 0.25	5 0.47	40 0.30	0.50 F	65 0.45	0.59 ز	26.4	0.23	0.46
J	1.50	14.26								15.76	В	2	0.08	0.35 95	0.81 0	1.88	100 0.	.81 0.8	88 7	0.14 0.	39 11	0.17 0.4	12 25 0	.22 0.46	30 0.25	5 0.47	40 0.30	0.50 F	65 0.45	0.59 ز	86.1		0.83
K	1.75	16.25								18.00	В	2	0.08	0.35 95		1.88	100 0.	.81 0.8	88 7	0.14 0.	39 11	0.17 0.4	12 25 0	.22 0.46	30 0.25	5 0.47	40 0.30	0.50 F	65 0.45	0.59 ز	86.0		0.83
L	2.84	4.25								7.09	В	2	0.08	0.35 95	0.81 0	1.88	100 0.	.81 0.8	88 7	0.14 0.	39 12	0.17 0.4	12 25 0	.22 0.46	30 0.25	5 0.47	40 0.30	0.50 F	65 0.45	0.59 ز	57.8	0.52	0.67
M	1.99	2.98								4.97	В	2	0.08	0.35 95	0.81 0	1.88	100 0.	.81 0.8	88 7	0.14 0.	39 13	0.17 0.4	12 25 0	.22 0.46	30 0.25	5 0.47	40 0.30	0.50	∂5 0.45	ا 0.59	57.8	0.52	0.67
OS1	18.99									18.99	В	2	0.08	0.35 95	0.81 0	1.88	100 0.	.81 0.8	38 7	0.14 0.	39 11	0.17 0.4	12 25 0	.22 0.46	30 0.25	5 0.47	40 0.30	0.50 6	∂5 0.45	0.59 ز	2.0		0.35
OS2	36.39									36.39	В	2	0.08	0.35 95	0.81 0	1.88	100 0.	.81 0.8	38 7	0.14 0.	39 11	0.17 0.4	12 25 0	.22 0.46	30 0.25	5 0.47	40 0.30	0.50 6	∂5 0.45	0.59 ز	2.0	0.08	0.35
OS3	25.25									25.25	В	2	0.08	0.35 95	0.81 0	1.88	100 0.	.81 0.8	38 7	0.14 0.	39 11	0.17 0.4	12 25 0	.22 0.46	30 0.25	5 0.47	40 0.30	0.50	∂5 0.45	0.59 ز	2.0		0.35
OS4	72.29									72.29	В	2	0.08	0.35 95	0.81 0	0.88 1	100 0.	.81 0.8	88 7	0.14 0.	39 11	0.17 0.4	12 25 0	.22 0.46	30 0.25	5 0.47	40 0.30	0.50 6	<u>85</u> 0.45	0.59 ز	2.0		0.35
OS5	4.37			36.87						41.24	В	2	0.08	0.35 95	0.81 0	0.88 1	100 0.	.81 0.8	88 7	0.14 0.	39 11	0.17 0.4	12 25 0	.22 0.46	30 0.25	5 0.47	40 0.30	0.50 6	<u>85</u> 0.45	0.59 ز	6.5	0.13	0.39
OS6	79.28				6.59	7.76				93.63	В	2	0.08	0.35 95	0.81 0	0.88 1	100 0.	.81 0.8	88 7	0.14 0.	39 11	0.17 0.4	12 25 0	.22 0.46	30 0.25	5 0.47	40 0.30	0.50 6	<u>85</u> 0.45	0.59 ز	4.5	0.10	0.36
OS7	20.65					7.57				28.22	В	2	0.08	0.35 95	0.81 0).88 1	100 0.	.81 0.8	38 7	0.14 0.	39 11	0.17 0.4	12 25 0	.22 0.46	30 0.25	5 0.47	40 0.30	0.50 6	65 0.45	5 0.59	8.2		0.38
OS8	3.42		4.58							8.00	В	2	0.08	0.35 95	0.81 0).88 1	100 0.	.81 0.8	38 7	0.14 0.	39 12	0.17 0.4	12 25 0	.22 0.46	30 0.25	5 0.47	40 0.30	0.50 6	35 0.45	0.59 ز	58.1		0.65
TOTAL ONSITE	195.88	57.97	5.71	146.30	96.02	57.45	27.74	120.01	45.24	744.75		2	0.08	0.35 95	0.81 0.	.88 1	100 0.	81 0.8	8 7	0.14 0.3	39 11	0.17 0.4	2 25 0.	.22 0.46	30 0.25	0.47	40 0.30	0.50 6	55 0.45	0.59	24.9	0.24	0.47
TOTAL OFFSITE	253.07	0.00	4.58	36.87	6.59	7.76	0.00	0.00	0.00	316.44		2	0.08	0.35 95	0.81 0.	.88 1	100 0.	81 0.8	8 7	0.14	39 11	0.17 0.4	25 0.	.22 0.46	30 0.25	0.47	40 0.30	0.50 6	55 0.45	0.59	4.7	0.10	0.36
GRAND TOTAL	448.95	57.97	10.29	183.17	102.61	65.21	27.74	120.01	45.24	1061.19		2	0.08	0.35 95	0.81 0.	.88 1	100 0.	81 0.8	8 7	0.14 0.3	39 11	0.17 0.4	25 0	.22 0.46	30 0.25	0.47	40 0.30	0.50 6	55 0.45	0.59	18.9	0.20	0.44

NOTES:
* The areas highlighted in OS6 & OS7 is on-site tributary area. These figures are included in the on-site area total and excluded from the offsite area total.



FLYING HORSE NORTH PARCELS 1-6 PROPOSED CONDITIONS

HRGreen EL PASO COUNTY, COLORADO

Calc'd by: DLH

Checked by: RDL

Date: 10/19/2023

					TIME (OF CON	CENTRAT	ION					
BAS	IN DATA		OVERI	LAND TIM	E (T _i)		TRAV	EL TIME (T _t)		TOTAL	tc=(L/180)+10	Design tc
DESIGNATION	C ₅	AREA (ac)	LENGTH (ft)	SLOPE %	t _i (min)	C_{V}	LENGTH (ft)	SLOPE %	V (ft/s)	t _t (min)	t_c (min)	tc max	tc design (min)
Α	0.17	74.11	100	4.0	10.8	20	1650	2.0	2.8	9.7	20.5	19.7	19.7
A1	0.14	12.58	100	3.0	12.2	7	850	3.0	1.2	11.7	23.9	15.3	15.3
A2	0.15	6.53	100	3.0	12.1	7	800	3.0	1.2	11.0	23.1	15.0	15.0
В	0.22	32.69	100	4.0	10.2	20	1265	4.0	4.0	5.3	15.5	17.6	15.5
С	0.26	121.03	100	1.0	15.5	20	3020	1.0	2.0	25.2	40.6	27.3	27.3
D	0.23	86.16	100	2.0	12.6	20	2750	2.5	3.2	14.5	27.1	25.8	25.8
Е	0.37	52.36	100	5.0	7.8	20	1750	4.0	4.0	7.3	15.1	20.3	15.1
F	0.19	197.45	100	4.0	10.5	20	3600	3.0	3.5	17.3	27.9	30.6	27.9
G	0.16	27.30	100	25.0	5.9	20	1600	3.0	3.5	7.7	13.6	19.4	13.6
Н	0.14	74.02	100	5.0	10.3	7	500	5.0	1.6	5.3	15.6	13.3	13.3
	0.23	7.13	100	5.0	9.3	20	900	5.0	4.5	3.4	12.7	15.6	12.7
J	0.74	15.76	100	5.0	3.9	20	350	5.0	4.5	1.3	5.2	12.5	5.2
K	0.74	18.00	100	10.0	3.1	20	1000	7.0	5.3	3.1	6.2	16.1	6.2
L	0.52	7.09	100	25.0	3.6	20	250	12.0	6.9	0.6	5.0	11.9	5.0
M	0.52	4.97	100	5.5	6.0	20	1050	2.0	2.8	6.2	12.2	16.4	12.2
OS1	0.08	18.99	300	7.0	16.9	10	300	7.0	2.6	1.9	18.8	13.3	13.3
OS2	0.08	36.39	300	4.0	20.4	10	1300	4.0	2.0	10.8	31.2	18.9	18.9
OS3	0.08	25.25	300	6.0	17.8	10	900	6.0	2.4	6.1	23.9	16.7	16.7
OS4	0.08	72.29	300	7.0	16.9	10	1320	6.0	2.4	9.0	25.9	19.0	19.0
OS5	0.13	41.24	300	5.0	18.0	10	1900	5.0	2.2	14.2	32.2	22.2	22.2
OS6	0.10	93.63	100	2.5	13.5	15	3400	2.5	2.4	23.9	37.4	29.4	29.4
OS7	0.12	28.22	100	5.0	10.5	15	1600	5.0	3.4	8.0	18.5	19.4	18.5
OS8	0.50	8.00	OVERF	RIDEN	#VALUE!	20	OVERF	RIDEN	0.0	######	#VALUE!	#VALUE!	#VALUE!

FORMULAS:

$$V = C_{\nu} S_{w}^{0.5}$$

$$V = C_{\nu} S_{w}^{0.5}$$

$$V = C_{\nu} S_{w}^{0.5}$$

Table 6-7. Conveyance Coefficient, C_{ν}

Type of Land Surface	C_{ν}
Heavy meadow	2.5
Tillage/field	5
Riprap (not buried)*	6.5
Short pasture and lawns	7
Nearly bare ground	10
Grassed waterway	15
Paved areas and shallow paved swales	20

For buried riprap, select C_v value based on type of vegetative cover.



FLYING HORSE NORTH PARCELS 1-6 PROPOSED CONDITIONS DESIGN STORM: 5-YEAR

Calc'd by: DLH

Checked by: RDL

Date: 10/19/2023

				D	DIRECT	r RUNO)FF		ТО	TAL R	UNO	FF	OV	ERLAN	ND		PII	PE		TI	RAVEL	TIME	REMARKS
DESIGN POINT(S)	ULTIMATEDESIGN	BASIN ID	AREA (ac)	C ₅	t_c (min)	C ₅ *A (ac)	/ (in./ hr.)	Q (cfs)	t _c (min)	C ₅ *A (ac)	/ (in./ hr.)	Q (cfs)	Q _{street} (cfs)	C ₅ *A (ac)	SLOPE %	Q _{PIPE} (cfs)	C ₅ *A (ac)	SLOPE %	PIPE SIZE (FT)	LENGTH (FT)	VEL. (FPS)	TRAVEL TIME (min)	
1, 2, 3	3	Α	74.11	0.17	19.7	12.51	3.11	38.9															DETENTION IN POND A, OUTLETS TO EX. FIL. NO. 1 POND 13
4	6	A1	12.58				3.49																DIRECTLY DRAINS OFFSITE, CONVEYS OFFSITE FLOW THROUGH THE DEVELOPMENT. ULTIMATELY OUTFALLS TO EX. FIL. NO. 1 POND 13.
5, 6	6	A2	6.53	0.15	15.0	0.96	3.52	3.4															DIRECTLY DRAINS OFFSITE, CONVEYS OFFSITE FLOW THROUGH THE DEVELOPMENT. ULTIMATELY OUTFALLS TO EX. FIL. NO. 1 POND 13.
7	7	В	32.69	0.22	15.5	7.09	3.47	24.6															DETENTION IN POND B, OUTLETS TO EX. FIL. NO. 1 POND 13
10, 11	11	С	121.03	0.26	27.3	31.06	2.62	81.4															DETENTION IN POND C. OUTLETS OFFSITE DUE NORTH.
13	13	D	86.16	0.23	25.8	20.24	2.71	54.8															DETENTION IN POND D. OUTLETS OFFSITE DUE NORTHWEST.
14, 15	15	Е	52.36	0.37	15.1	19.29	3.51	67.7															DETENTION IN POND E. OUTLETS OFFSITE DUE NORTH.
17	17	F	197.45	0.19	27.9	37.00	2.59	95.9															DETENTION IN POND F. OUTLETS ONSITE DUE NORTH.
18	18	G	27.30	0.16	13.6	4.45	3.67	16.4															DETENTION IN POND G. OUTLETS ONSITE DUE NORTH.
19	19	Н	74.02			10.17		37.6															DIRECTLY DRAINS OFFSITE. RUNOFF REDUCTION VIA GRASS BUFFERS.
6, 20	6	I	7.13	0.23	12.7	1.63	3.77	6.1															DIRECTLY DRAINS OFFSITE TO EX. FIL. NO. 1 POND 13



FLYING HORSE NORTH PARCELS 1-6 PROPOSED CONDITIONS DESIGN STORM: 5-YEAR

Calc'd by: DLH

Checked by: RDL

Date: 10/19/2023

				D	IRECT	RUNC	OFF		ТО	TAL R	UNOFF	0	VERLA	ND		PI	PE		T	RAVEL	TIME	REMARKS
DESIGN POINT(S)	ULTIMATEDESIGN PONT	BASIN ID	AREA (ac)	c _s	t _c (min)	С ₅ *А (ас)	/ (in./ hr.)	Q (cfs)	t _c (min)	C ₅ *A (ac)	/ (in./ hr.) Q (cfs)	Q _{street} (cfs)	C ₅ *A (ac)	SLOPE %	Q _{PIPE} (cfs)	C ₅ *A (ac)	SLOPE %	PIPE SIZE (FT)	LENGTH (FT)	VEL. (FPS)	TRAVEL TIME (min)	
21	21	J	15.76	0.74	5.2	11.67	5.12	59.8														DETENTION IN POND J. OUTLETS OFFSITE DUE WEST.
22, Pond 8 (Fil. 1)	22	К	18.00			13.30		64.4														DETENTION IN POND K. OUTLETS OFFSITE DUE WEST. ULTIMATELY DRAINS TO EX. FIL. NO. 1 POND 8.
23, Pond 8 (Fil. 1)	23	L	7.09																			DRAINS OFFSITE TO GOLF COURSE AND ULTIMATLEY TO EX. FIL. NO. 1 POND 8.
24	6	M	4.97																			DRAINS INTO ADJACENT ALLEN RANCH ROAD AND INTO F.H.N. FILING NO. 3 POND
1, 2, 3	3	OS1	18.99																			DRAINS THROUGH TO BASIN A. TWO CULVERT PIPE LOCATIONS TO CROSS ROADWAYS.
4, 5, 6	6	OS2	36.39																			DRAINS THROUGH TO BASINS A1 AND A2. ULTIMATELY OUTFALLS TO EX. FIL. NO. 1 POND 13.
6, 8, 9	6	OS3	25.25																			DRAINS THROUGH TO BASIN OS7. ULTIMATELY OUTFALLS TO EX. FIL. NO. 1 POND 13.
12, 13	13	OS4	72.29																			DRAINS THROUGH TO BASIN D. DETENTION IN POND D.
16, 17	17	OS5	41.24																			DRAINS THROUGH TO BASIN F. DETENTION IN POND F.
6	6		93.63				2.93															DIRECTLY DRAINS TO EX. FIL. NO. 1 POND 13
-	6	OS6																				
6, 9	Ů	OS7	28.22		18.5		3.21	10.6														DIRECTLY DRAINS TO EX. FIL. NO. 1 POND 13
25	6	OS8	8.00	0.50		3.98						3.8										F.H.N. FILING NO. 3 POND DRAINS DIRECTLY DRAINS TO EX. FIL. NO. 1 POND 13



FLYING HORSE NORTH PARCELS 1-6

PROPOSED CONDITIONS

Calc'd by: DLH

Checked by: RDL DESIGN STORM: 100-YEAR **Date:** 10/19/2023

		_			DIRECT	RUNC	OFF			TOTAL R	UNOFF		0\	/ERLAI	ND		PI	PE		TI	RAVEL	TIME	REMARKS
DESIGN POINT(S)	ULTIMATEDESIGN PONT	BASIN ID	AREA (ac)	C ₁₀₀	t _c (min)	C ₁₀₀ *A (ac)	/ (in./ hr.)	Q (cfs)	t _o (min)	C ₁₀₀ *A (ac)	/ (in./ hr.)	Q (cfs)	Q _{street} (cfs)	C ₁₀₀ *A (ac)	SLOPE %	Q _{PIPE} (cfs)	C ₁₀₀ *A (ac)	SLOPE %	PIPE SIZE (ft)	LENGTH (ft)	VEL. (ft/s)	TRAVEL TIME (min)	
1, 2, 3	3	Α	74.11	0.42	10.7	30.95	5.22	161.6															DETENTION IN POND A, OUTLETS TO EX. FIL. NO. 1 POND 13
1, 2, 3	3		7-7.11	0.42	13.7	30.33	0.22	101.0															BETERTION IN LOND A, GOTEETO TO EX. TE. NO. 11 OND 10
4	6	A1	12.58	0.39	15.3	4.94	5.86	29.0															DIRECTLY DRAINS OFFSITE, CONVEYS OFFSITE FLOW THROUGH THE DEVELOPMENT. ULTIMATEL OUTFALLS TO EX. FIL. NO. 1 POND 13.
5, 6	6	A2	6.53	0.40	15.0	2.60	5.91	15.3															DIRECTLY DRAINS OFFSITE, CONVEYS OFFSITE FLOW THROUGH THE DEVELOPMENT. ULTIMATEL OUTFALLS TO EX. FIL. NO. 1 POND 13.
7	7	В	32.69	0.45	15.5	14.77	5.83	86.1															DETENTION IN POND B, OUTLETS TO EX. FIL. NO. 1 POND 13
10, 11	11	С	121.03	0.47	27.3	57.15	4.40	251.4															DETENTION IN POND C. OUTLETS OFFSITE DUE NORTH.
13	13	D	86.16	0.45	25.8	39.00	4.54	177.1															DETENTION IN POND D. OUTLETS OFFSITE DUE NORTHWEST.
14, 15	15	E	52.36	0.55	15.1	29.05	5.89	171.0															DETENTION IN POND E. OUTLETS OFFSITE DUE NORTH.
17	17	F	197.45	0.43	27.9	84.21	4.35	366.3															DETENTION IN POND F. OUTLETS ONSITE DUE NORTH.
18	18	G	27.30	0.41	13.6	11.10	6.16	68.4					_										DETENTION IN POND G. OUTLETS ONSITE DUE NORTH.
19	19	Н	74.02	0.39	13.3	29.07	6.21	180.4					_										DIRECTLY DRAINS OFFSITE. RUNOFF REDUCTION VIA GRASS BUFFERS.
6, 20	6	I	7.13				6.33	20.7															DIRECTLY DRAINS OFFSITE TO EX. FIL. NO. 1 POND 13



FLYING HORSE NORTH PARCELS 1-6 PROPOSED CONDITIONS

DESIGN STORM: 100-YEAR

Calc'd by: DLH
Checked by: RDL
Date: 10/19/2023

			DIRECT RUNOFF					TOTAL RUNOFF OVERLAND			PIPE TRAVEL		TIME	REMARKS									
						1.0140				I JIAL K				LIXEA				- 	1	- "	TOTAL E		REWARKS
DESIGN POINT(S)	ULTIMATEDESIGN PONT	BASIN ID	AREA (ac)	C ₁₀₀	<i>t_c (</i> min)	C ₁₀₀ *A (ac)	/ (in./ hr.)	Q (cfs)	t _c (min)	C ₁₀₀ *A (ac)	/ (in./ hr.)	Q (cfs)	Q _{street} (cfs)	C ₁₀₀ *A (ac)	SLOPE %	Q _{PIPE} (cfs)	C ₁₀₀ *A (ac)	SLOPE %	PIPE SIZE (ft)	LENGTH (ft)	VEL. (ft/s)	TRAVEL TIME (min)	
21	21		15.76	0.83	5.2	13.07	8.60	112.4															DETENTION IN POND J. OUTLETS OFFSITE DUE WEST.
21	21	-	10.70	0.00	0.2	10.07	0.00	112.7															BETENTION IN TONE U. COTEETO OTTOTE DOE WEST.
22, Pond 8 (Fil. 1)	22	К	18.00	0.83	6.2	14.91	8.13	121.2															DETENTION IN POND K. OUTLETS OFFSITE DUE WEST. ULTIMATELY DRAINS TO EX. FIL. NO. 1 POND 8.
23, Pond 8 (Fil. 1)	23	L	7.09	0.67	5.0	4.74	8.68	41.1															DRAINS OFFSITE TO GOLF COURSE AND ULTIMATLEY TO EX. FIL. NO. 1 POND 8.
24	6	М	4.97	0.67	12.2	3.32	6.42	21.3															DRAINS INTO ADJACENT ALLEN RANCH ROAD AND INTO F.H.N. FILING NO. 3 POND
1, 2, 3	3	OS1	18.99	0.35	13.3	6.65	6.21	41.3															DRAINS THROUGH TO BASIN A. TWO CULVERT PIPE LOCATIONS TO CROSS ROADWAYS.
4, 5, 6	6	OS2	36.39	0.35	18.9	12.74	5.33	67.9															DRAINS THROUGH TO BASINS A1 AND A2. ULTIMATELY OUTFALLS TO EX. FIL. NO. 1 POND 13.
1, 0, 0	Ŭ	002	00.00	0.00	10.0	12.7	0.00	07.0															
6, 8, 9	6	OS3	25.25	0.35	16.7	8.84	5.65	49.9															DRAINS THROUGH TO BASIN OS7. ULTIMATELY OUTFALLS TO EX. FIL. NO. 1 POND 13.
12, 13	13	OS4	72.29	0.35	19.0	25.30	5.32	134.5															DRAINS THROUGH TO BASIN D. DETENTION IN POND D.
16, 17	17	OS5	41.24	0.39	22.2	16.01	4.92	78.8															DRAINS THROUGH TO BASIN F. DETENTION IN POND F.
6	6	OS6	93.63	0.36	29.4	34.07	4.21	143.5															DIRECTLY DRAINS TO EX. FIL. NO. 1 POND 13
6, 9	6	OS7	28.22	0.38	18.5	10.71	5.38	57.7															DIRECTLY DRAINS TO EX. FIL. NO. 1 POND 13
25	6	OS8	8.00	0.65		5.23						4.4											F.H.N. FILING NO. 3 POND DRAINS DIRECTLY DRAINS TO EX. FIL. NO. 1 POND 13





Appendix C:

Hydraulic Calculations

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Tuesday, Oct 10 2023

Section A-A OFF-SITE CHANNEL: 5-YR

Trapezoidal

Bottom Width (ft) = 50.00 Side Slopes (z:1) = 89.00, 8.00 Total Depth (ft) = 2.00 Invert Elev (ft) = 1.00 Slope (%) = 2.70 N-Value = 0.035

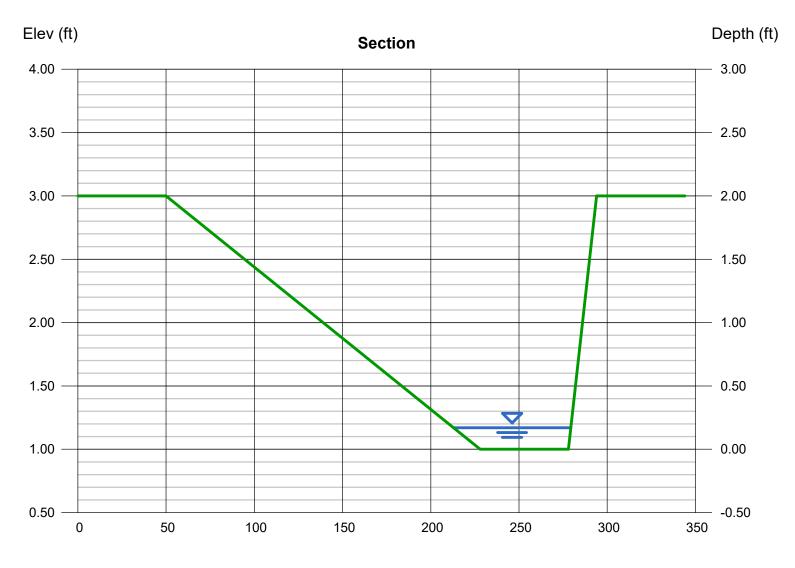
Calculations

Compute by: Known Q Known Q (cfs) = 18.30

CHANNEL LOCATION: WITHIN BASIN OS4

Highlighted

Depth (ft) = 0.17Q (cfs) = 18.30 Area (sqft) = 9.90Velocity (ft/s) = 1.85Wetted Perim (ft) = 66.50Crit Depth, Yc (ft) = 0.16Top Width (ft) = 66.49EGL (ft) = 0.22



Reach (ft)

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Tuesday, Oct 10 2023

Section A-A OFF-SITE CHANNEL: 100-YR

Trapezoidal

Bottom Width (ft) = 50.00 Side Slopes (z:1) = 89.00, 8.00

Total Depth (ft) = 2.00 Invert Elev (ft) = 1.00 Slope (%) = 2.70 N-Value = 0.035

Calculations

Compute by: Known Q Known Q (cfs) = 134.50

CHANNEL LOCATION: WITHIN BASIN OS4

Highlighted

Depth (ft) = 0.50Q (cfs) = 134.50Area (sqft) = 37.12Velocity (ft/s) = 3.62Wetted Perim (ft) = 98.53Crit Depth, Yc (ft) = 0.52Top Width (ft) = 98.50EGL (ft) = 0.70

Recommended BMP:

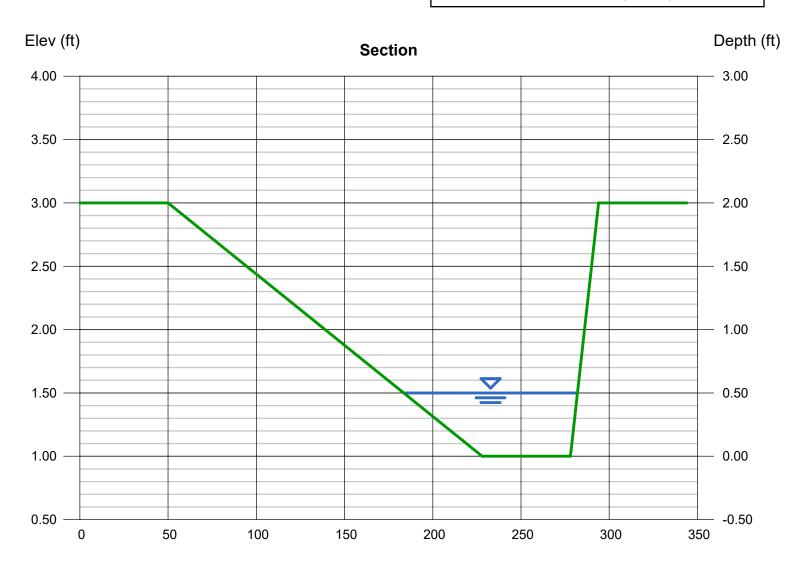
North American Green

Rollmax Permanent Turf Reinforcement Mat

P300 (or equiv.)

Permissible Velocity (ft/s) = 9.0

Permissible Shear Stress (lb/ft^2) = 3.0



Reach (ft)

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Monday, Oct 9 2023

Section B-B OFF-SITE CHANNEL: 5-YR

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Side Slopes (z:1) = 6.00, 10.00= 5.00

Total Depth (ft)

Invert Elev (ft) = 1.00 Slope (%) = 5.70N-Value = 0.035

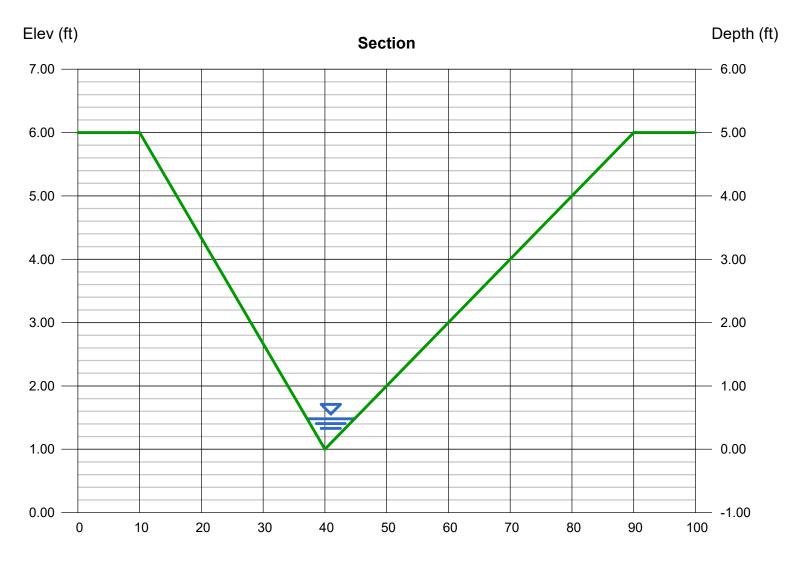
Calculations

Compute by: Known Q Known Q (cfs) = 6.80

CHANNEL LOCATION: WITHIN BASIN OS3

Highlighted

= 0.48Depth (ft) Q (cfs) = 6.800Area (sqft) = 1.84Velocity (ft/s) = 3.69Wetted Perim (ft) = 7.74Crit Depth, Yc (ft) = 0.54Top Width (ft) = 7.68EGL (ft) = 0.69



Reach (ft)

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Monday, Oct 9 2023

Section B-B OFF-SITE CHANNEL: 100-YR

Triangular

Side Slopes (z:1) = 6.00, 10.00

Total Depth (ft) = 5.00

Invert Elev (ft) = 1.00 Slope (%) = 5.70 N-Value = 0.035

Calculations

Compute by: Known Q Known Q (cfs) = 49.90

CHANNEL LOCATION: WITHIN BASIN OS3

Highlighted

Depth (ft) = 1.00Q (cfs) = 49.90Area (sqft) = 8.00Velocity (ft/s) = 6.24 Wetted Perim (ft) = 16.13Crit Depth, Yc (ft) = 1.20Top Width (ft) = 16.00EGL (ft) = 1.60

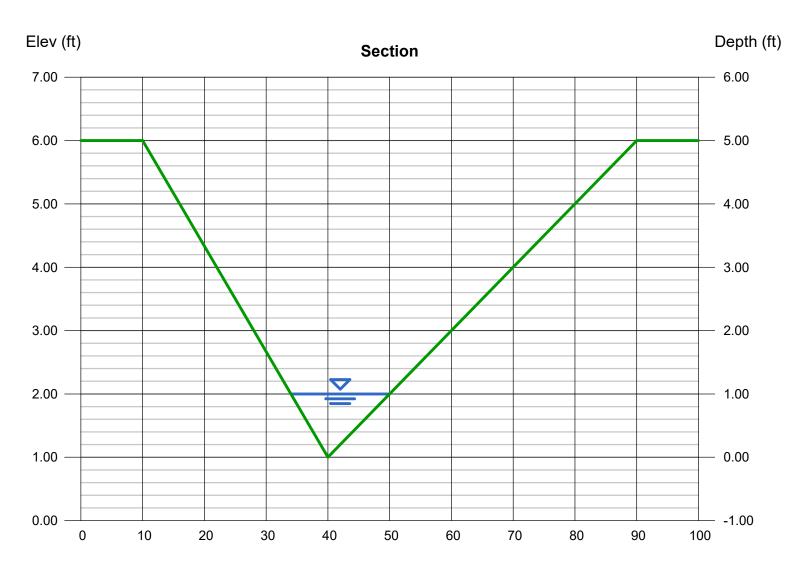
Recommended BMP:

Rollmax Permanent Turf Reinforcement Mat

TMAX (or equiv.)

Permissible Velocity (ft/s) = 25.0

Permissible Shear Stress (lb/ft^2) = 15.0



Reach (ft)

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Tuesday, Oct 10 2023

Section C-C OFF-SITE CHANNEL: 5-YR

Trapezoidal

Bottom Width (ft) = 23.00 Side Slopes (z:1) = 39.00, 10.00 Total Depth (ft) = 1.20 Invert Elev (ft) = 1.00 Slope (%) = 6.60

N-Value = 0.035

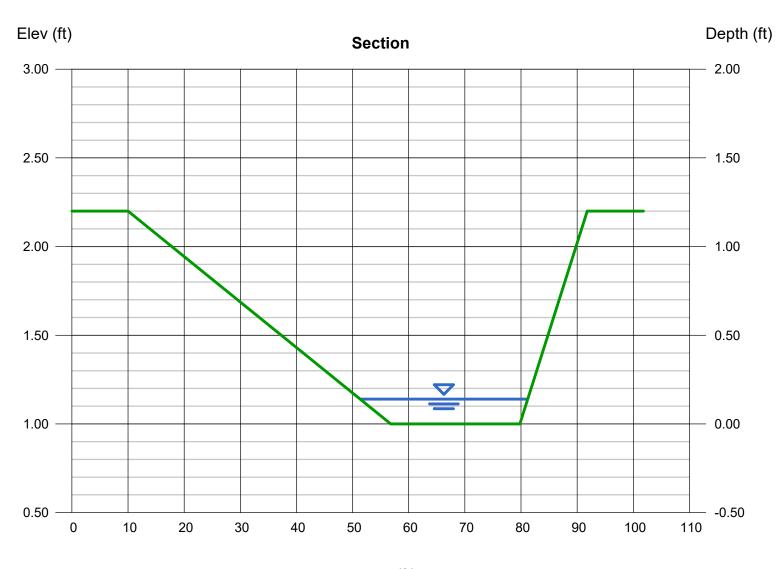
Calculations

Compute by: Known Q Known Q (cfs) = 9.20

CHANNEL LOCATION: WITHIN BASIN OS2

Highlighted

= 0.14Depth (ft) Q (cfs) = 9.200Area (sqft) = 3.70Velocity (ft/s) = 2.49Wetted Perim (ft) = 29.87Crit Depth, Yc (ft) = 0.17Top Width (ft) = 29.86EGL (ft) = 0.24



Reach (ft)

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Tuesday, Oct 10 2023

Section C-C OFF-SITE CHANNEL: 100-YR

Trapezoidal

Bottom Width (ft) = 23.00

Side Slopes (z:1) = 39.00, 10.00

Total Depth (ft) = 1.20 Invert Elev (ft) = 1.00 Slope (%) = 6.60 N-Value = 0.035

Calculations

Compute by: Known Q Known Q (cfs) = 67.90

CHANNEL LOCATION: WITHIN BASIN OS2

Highlighted

Depth (ft) = 0.41Q (cfs) = 67.90Area (sqft) = 13.55Velocity (ft/s) = 5.01 Wetted Perim (ft) = 43.12Crit Depth, Yc (ft) = 0.54Top Width (ft) = 43.09EGL (ft) = 0.80

Recommended BMP:

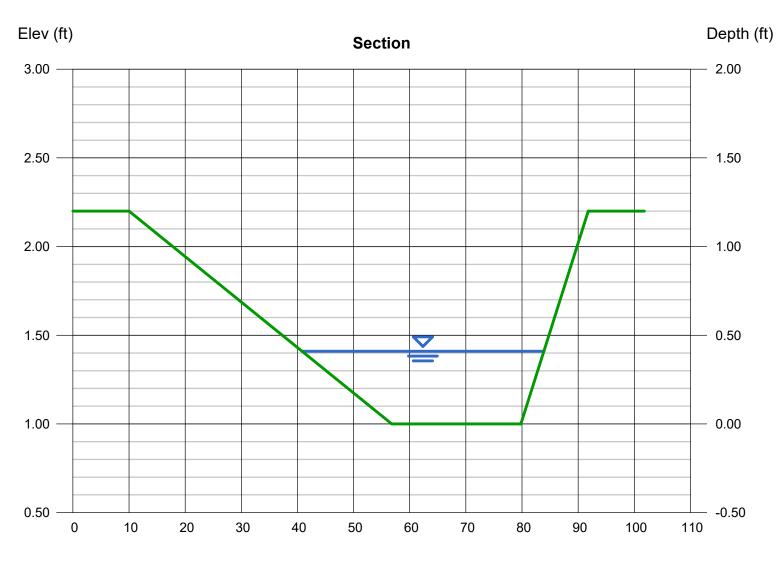
North American Green

Rollmax Permanent Turf Reinforcement Mat

P300 (or equiv.)

Permissible Velocity (ft/s) = 9.0

Permissible Shear Stress (lb/ft^2) = 3.0



Reach (ft)

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Tuesday, Oct 10 2023

Section D-D ON-SITE CHANNEL: 5-YR

Trapezoidal

Bottom Width (ft) = 40.00 Side Slopes (z:1) = 44.00, 14.00 Total Depth (ft) = 1.00 Invert Elev (ft) = 1.00

Invert Elev (ft) = 1.00 Slope (%) = 2.50 N-Value = 0.035

Calculations

Compute by: Known Q Known Q (cfs) = 81.40

CHANNEL LOCATION: WITHIN BASIN C

Highlighted

= 0.46Depth (ft) Q (cfs) = 81.40Area (sqft) = 24.54Velocity (ft/s) = 3.32Wetted Perim (ft) = 66.70Crit Depth, Yc (ft) = 0.46Top Width (ft) = 66.68EGL (ft) = 0.63

Elev (ft) Depth (ft) Section 2.00 3.00 -2.50 -- 1.50 2.00 -- 1.00 1.50 -- 0.50 1.00 -0.00 0.50 -0.50 0 10 20 30 40 50 60 70 80 90 100 110 120

Reach (ft)

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Tuesday, Oct 10 2023

Section D-D ON-SITE CHANNEL: 100-YR

Trapezoidal

Bottom Width (ft) = 40.00

Side Slopes (z:1) = 44.00, 14.00

Total Depth (ft) = 1.00 Invert Elev (ft) = 1.00 Slope (%) = 2.50 N-Value = 0.035

Calculations

Compute by: Known Q Known Q (cfs) = 251.40

CHANNEL LOCATION:

WITHIN BASIN C

Highlighted

Depth (ft) = 0.83Q (cfs) = 251.40Area (sqft) = 53.18 Velocity (ft/s) = 4.73Wetted Perim (ft) = 88.18Crit Depth, Yc (ft) = 0.87Top Width (ft) = 88.14 EGL (ft) = 1.18

Recommended BMP:

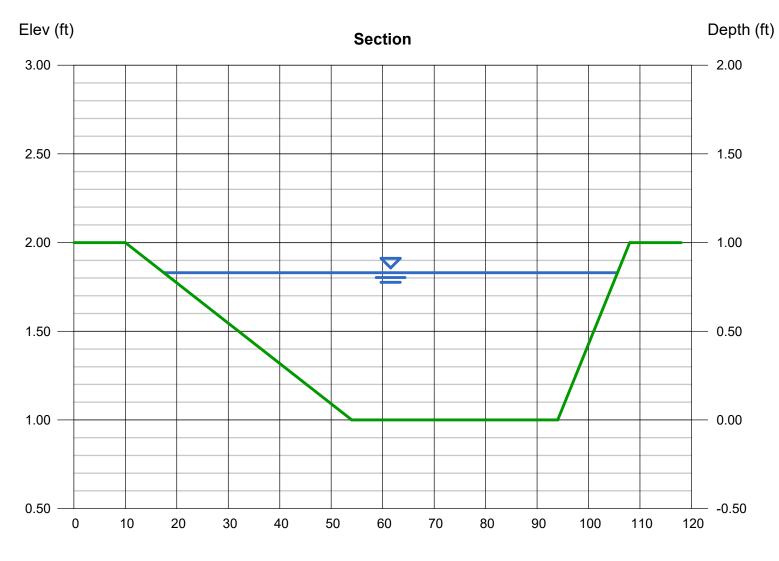
North American Green

Rollmax Permanent Turf Reinforcement Mat

P300 (or equiv.)

Permissible Velocity (ft/s) = 9.0

Permissible Shear Stress (lb/ft^2) = 3.0



Reach (ft)

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Tuesday, Oct 10 2023

Section E-E ON-SITE CHANNEL: 5-YR

Trapezoidal

Bottom Width (ft) = 22.50 Side Slopes (z:1) = 7.00, 8.00 Total Depth (ft) = 3.90 Invert Elev (ft) = 1.00 Slope (%) = 2.10 N-Value = 0.035

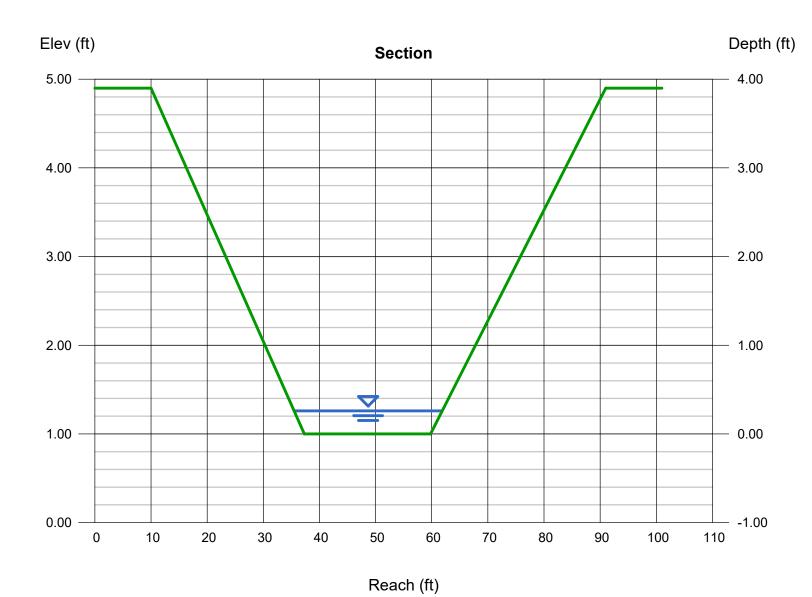
Calculations

Compute by: Known Q Known Q (cfs) = 14.50

CHANNEL LOCATION: WITHIN BASIN A

Highlighted

Depth (ft) = 0.26Q (cfs) = 14.50Area (sqft) = 6.36Velocity (ft/s) = 2.28 Wetted Perim (ft) = 26.43Crit Depth, Yc (ft) = 0.23Top Width (ft) = 26.40EGL (ft) = 0.34



Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Tuesday, Oct 10 2023

Section E-E ON-SITE CHANNEL: 100-YR

Trapezoidal

Bottom Width (ft) = 22.50 Side Slopes (z:1) = 7.00, 8.00 Total Depth (ft) = 3.90 Invert Elev (ft) = 1.00 Slope (%) = 2.10 N-Value = 0.035

Calculations

Compute by: Known Q Known Q (cfs) = 69.10

CHANNEL LOCATION: WITHIN BASIN A

Highlighted

Depth (ft) = 0.63Q (cfs) = 69.10Area (sqft) = 17.15Velocity (ft/s) = 4.03Wetted Perim (ft) = 32.03Crit Depth, Yc (ft) = 0.62Top Width (ft) = 31.95EGL (ft) = 0.88

Recommended BMP:

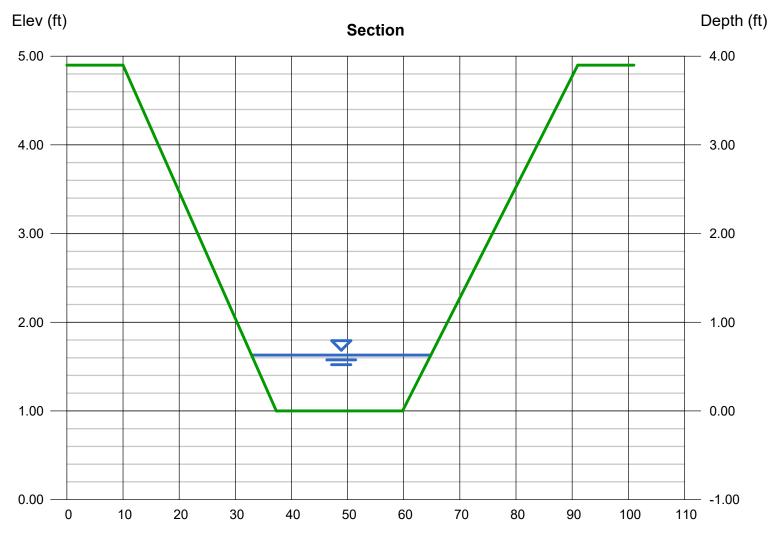
North American Green

Rollmax Permanent Turf Reinforcement Mat

P300 (or equiv.)

Permissible Velocity (ft/s) = 9.0

Permissible Shear Stress (lb/ft^2) = 3.0



Reach (ft)

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Tuesday, Oct 10 2023

= 0.89

Section F-F ON-SITE CHANNEL: 5-YR

Triangular

Side Slopes (z:1) = 8.00, 14.00

Total Depth (ft) = 4.00

Invert Elev (ft) = 1.00Slope (%) = 2.10

N-Value = 0.035

Calculations

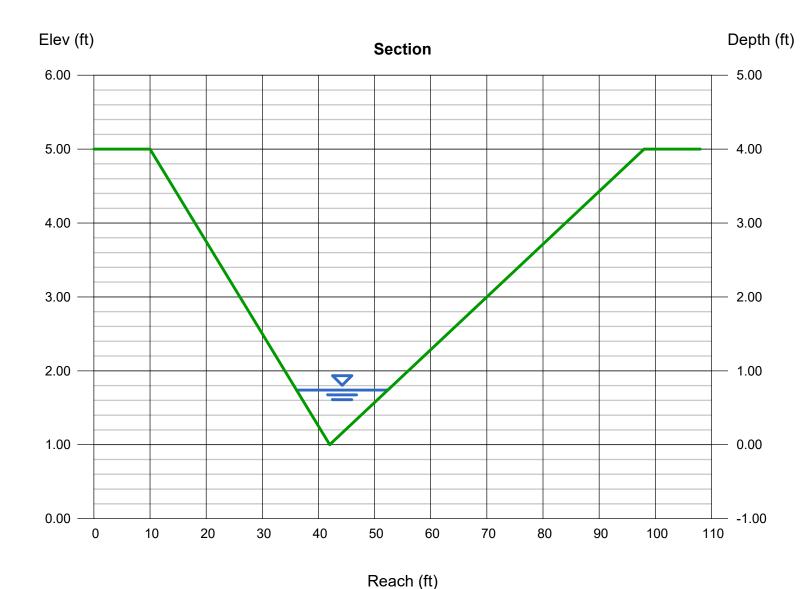
Compute by: Known Q Known Q (cfs) = 18.70

CHANNEL LOCATION: WITHIN BASIN A2

Highlighted

EGL (ft)

Depth (ft) = 0.74 Q (cfs) = 18.70 Area (sqft) = 6.02 Velocity (ft/s) = 3.10 Wetted Perim (ft) = 16.35 Crit Depth, Yc (ft) = 0.71 Top Width (ft) = 16.28



Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Tuesday, Oct 10 2023

Section F-F ON-SITE CHANNEL: 100-YR

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Side Slopes (z:1) = 8.00, 14.00Total Depth (ft) = 4.00

Invert Elev (ft) = 1.00 Slope (%) = 2.10 N-Value = 0.035

Calculations

Compute by: Known Q Known Q (cfs) = 112.20

CHANNEL LOCATION: WITHIN BASIN A2

Highlighted

Depth (ft) = 1.44Q (cfs) = 112.20Area (sqft) = 22.81Velocity (ft/s) = 4.92Wetted Perim (ft) = 31.82Crit Depth, Yc (ft) = 1.46Top Width (ft) = 31.68EGL (ft) = 1.82

Recommended BMP:

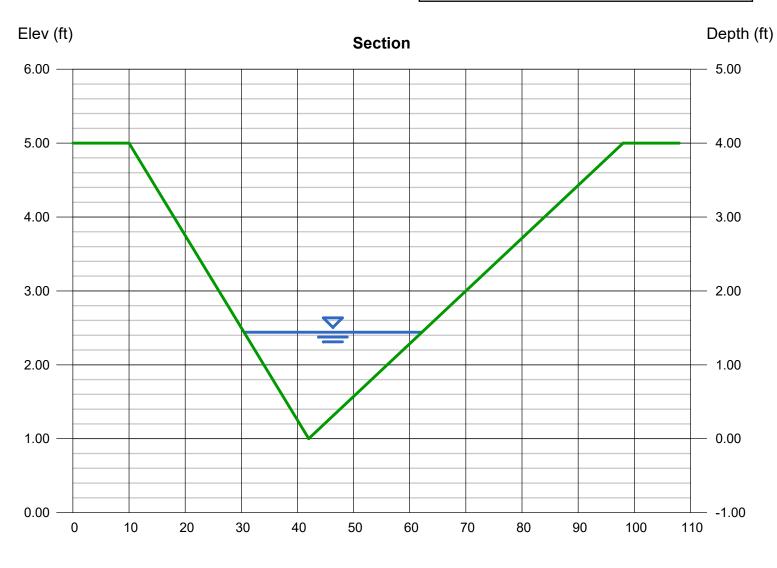
North American Green

Rollmax Permanent Turf Reinforcement Mat

P300 (or equiv.)

Permissible Velocity (ft/s) = 9.0

Permissible Shear Stress (lb/ft^2) = 3.0



Reach (ft)

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Tuesday, Oct 10 2023

Section G-G ON-SITE CHANNEL: 5-YR

Trapezoidal

Bottom Width (ft) = 22.50 Side Slopes (z:1) = 6.00, 21.00 Total Depth (ft) = 4.00 Invert Elev (ft) = 1.00 Slope (%) = 5.30 N-Value = 0.035

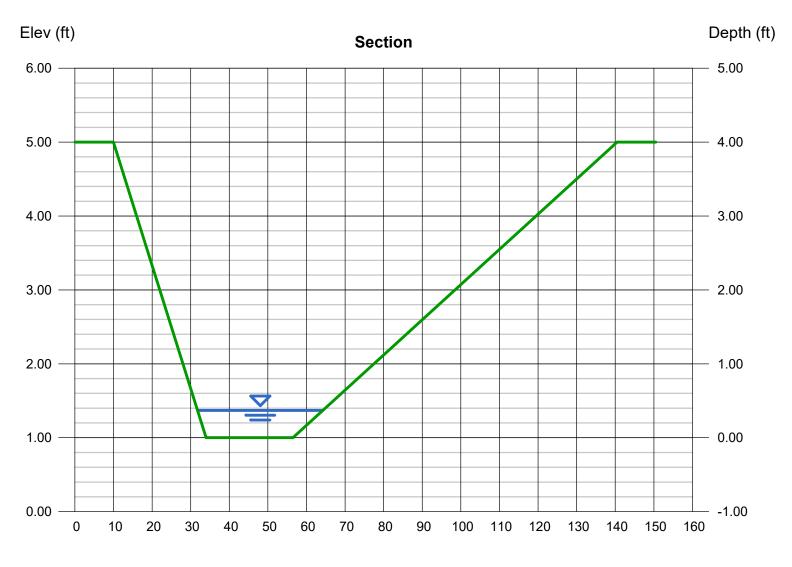
Calculations

Compute by: Known Q Known Q (cfs) = 44.30

CHANNEL LOCATION: WITHIN BASIN F

Highlighted

Depth (ft) = 0.37Q (cfs) = 44.30Area (sqft) = 10.17Velocity (ft/s) = 4.35Wetted Perim (ft) = 32.53Crit Depth, Yc (ft) = 0.45Top Width (ft) = 32.49EGL (ft) = 0.66



Reach (ft)

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Tuesday, Oct 10 2023

Section G-G ON-SITE CHANNEL: 100-YR

Trapezoidal

Bottom Width (ft) = 22.50 Side Slopes (z:1) = 6.00, 21.00 Total Depth (ft) = 4.00

Invert Elev (ft) = 1.00 Slope (%) = 5.30 N-Value = 0.035

Calculations

Compute by: Known Q Known Q (cfs) = 325.40

CHANNEL LOCATION: WITHIN BASIN F

Highlighted

Depth (ft) = 1.08Q (cfs) = 325.40Area (sqft) = 40.05Velocity (ft/s) = 8.13Wetted Perim (ft) = 51.78Crit Depth, Yc (ft) = 1.41 Top Width (ft) = 51.66EGL (ft) = 2.11

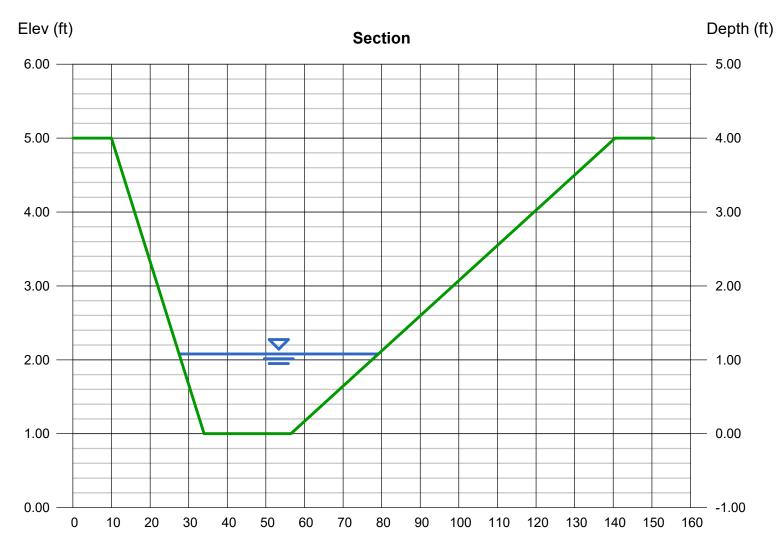
Recommended BMP:

Rollmax Permanent Turf Reinforcement Mat

TMAX (or equiv.)

Permissible Velocity (ft/s) = 25.0

Permissible Shear Stress (lb/ft^2) = 15.0



Reach (ft)

FRO	UDE NUMBI	ER CALCULATIONS	CALCULATED BY:	DLH	DATE:	10/10/2023			
PF	ROJECT: 211	.030 Parcels 1-6	CHECKED BY:	RL					
		Froude Nur	nber Calculations: 100-YR						
		Gravitational		X-Sectional					
Section	Velocity	Constant	Hydraulic depth	Area	top Width	Froude #			
-	ft/s	ft/s^2	ft	ft^2	ft	N/A			
A-A	3.62	32.17	0.38	37.12	98.50	1.04			
В-В	6.24	32.17	0.50	8.00	16.00	1.56			
C-C	5.01	32.17	0.31	13.55	43.09	1.58			
D-D	4.73	32.17	0.60	53.18	88.14	1.07			
E-E	4.03	32.17	0.54	17.15	31.95	0.97			
F-F	4.92	32.17	0.72	22.81	31.68	1.02			
G-G	8.13	32.17	0.78	40.05	51.66	1.63			

Shear Stress Calculations: 100-YR									
Section	Unit Weight of	Depth of	Clana	Shear					
Section	Water	flow	Slope	Stress					
-	lb/ft^3	ft	ft/ft	lb/ft^2					
A-A	62.43	0.50	0.03	0.84					
В-В	62.43	1.00	0.057	3.56					
C-C	62.43	0.41	0.066	1.69					
D-D	62.43	1.00	0.025	1.56					
E-E	62.43	0.63	0.021	0.83					
F-F	62.43	1.44	0.021	1.89					
G-G	62.43	1.08	0.053	3.57					

Channel Lining Determination									
С	alculated Valu	es	P300 Max						
Section	Shear Stress	Velocity	Shear Stress	Velocity	Lining Required				
A-A	0.84	3.62	3	9	P300				
B-B	3.56	6.24	3	9	TMAX				
C-C	1.69	5.01	3	9	P300				
D-D	1.56	4.73	3	9	P300				
E-E	0.83	4.03	3	9	P300				
F-F	1.89	4.92	3	9	P300				
G-G	3.57	8.13	3	9	TMAX				

Culvert Report

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Monday, Oct 9 2023

CULVERT-01

Invert Elev Dn (ft) = 7581.40 Pipe Length (ft) = 272.80Slope (%) = 3.92Invert Elev Up (ft) = 7592.09Rise (in) = 48.0= Circular Shape Span (in) = 48.0= 1 No. Barrels n-Value = 0.012

Culvert Type = Circular Concrete

Culvert Entrance = Square edge w/headwall (C) Coeff. K,M,c,Y,k = 0.0098, 2, 0.0398, 0.67, 0.5

Embankment

Top Elevation (ft) = 7609.50 Top Width (ft) = 124.00 Crest Width (ft) = 100.00

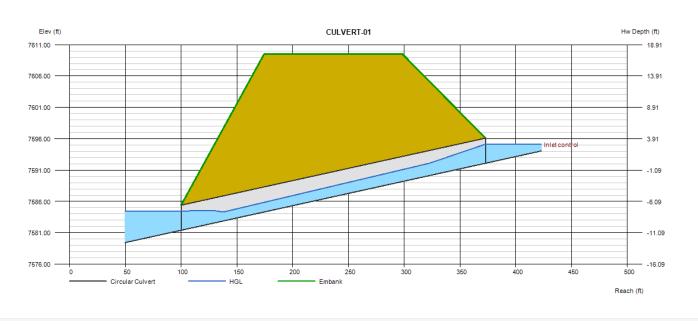
CULVERT LOCATION: PARCEL 3, BASIN B, CROSSING HOLMES ROAD, DESIGN POINT 8 **Calculations**

Qmin (cfs) = 6.80 Qmax (cfs) = 49.90 Tailwater Elev (ft) = (dc+D)/2

Highlighted

Qtotal (cfs) = 49.80Qpipe (cfs) = 49.80Qovertop (cfs) = 0.00Veloc Dn (ft/s) = 4.83Veloc Up (ft/s) = 7.38HGL Dn (ft) = 7584.46 HGL Up (ft) = 7594.21Hw Elev (ft) = 7595.13Hw/D (ft) = 0.76

Flow Regime = Inlet Control



Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Thursday, Oct 19 2023

Culvert-02

Invert Elev Dn (ft) = 7582.02 Pipe Length (ft) = 188.00Slope (%) = 2.12Invert Elev Up (ft) = 7586.01Rise (in) = 42.0= Circular Shape Span (in) = 42.0= 1 No. Barrels n-Value = 0.012

Culvert Type = Circular Concrete

Culvert Entrance = Square edge w/headwall (C) Coeff. K,M,c,Y,k = 0.0098, 2, 0.0398, 0.67, 0.5

Embankment

Top Elevation (ft) = 7609.50Top Width (ft) = 55.00Crest Width (ft) = 100.00

CULVERT LOCATION: PARCEL 3,

BASIN A1-A2, CROSSING

HOLMES ROAD, DESIGN POINT 4

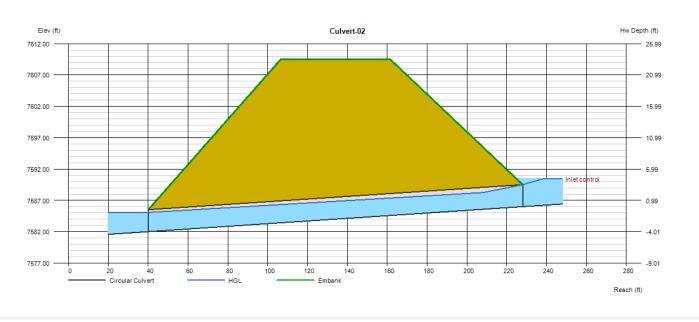
Calculations

Qmin (cfs) = 10.00 Qmax (cfs) = 70.00 Tailwater Elev (ft) = (dc+D)/2

Highlighted

Qtotal (cfs) = 70.00Qpipe (cfs) = 70.00Qovertop (cfs) = 0.00Veloc Dn (ft/s) = 7.85Veloc Up (ft/s) = 9.06HGL Dn (ft) = 7585.08HGL Up (ft) = 7588.63 Hw Elev (ft) = 7590.42Hw/D (ft) = 1.26

Flow Regime = Inlet Control



Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Monday, Oct 9 2023

CULVERT-03

Invert Elev Dn (ft) = 7601.62 Pipe Length (ft) = 167.11Slope (%) = 2.94Invert Elev Up (ft) = 7606.53Rise (in) = 48.0Shape = Circular Span (in) = 48.0= 1 No. Barrels n-Value = 0.012

Culvert Type = Circular Concrete

Culvert Entrance = Square edge w/headwall (C) Coeff. K,M,c,Y,k = 0.0098, 2, 0.0398, 0.67, 0.5

Embankment

Top Elevation (ft) = 7620.26Top Width (ft) = 60.00Crest Width (ft) = 100.00

CULVERT LOCATION: PARCEL 3, BASIN A, CROSSING HOLMES

ROAD, DESIGN POINT 2

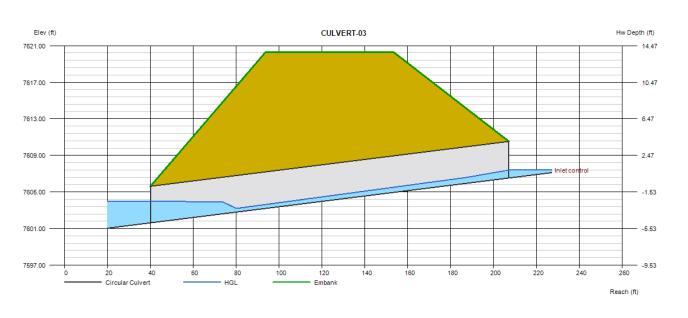
Calculations

Qmin (cfs) = 5.60 Qmax (cfs) = 41.30 Tailwater Elev (ft) = (dc+D)/2

Highlighted

Qtotal (cfs) = 5.60Qpipe (cfs) = 5.60Qovertop (cfs) = 0.00Veloc Dn (ft/s) = 0.73Veloc Up (ft/s) = 3.92HGL Dn (ft) = 7603.96HGL Up (ft) = 7607.21Hw Elev (ft) = 7607.40Hw/D (ft) = 0.22

Flow Regime = Inlet Control



Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Tuesday, Oct 10 2023

CULVERT-04

Invert Elev Dn (ft) = 7596.23 Pipe Length (ft) = 183.00Slope (%) = 2.82Invert Elev Up (ft) = 7601.39Rise (in) = 36.0= Circular Shape Span (in) = 36.0= 1 No. Barrels n-Value = 0.012

Culvert Type = Circular Concrete

Culvert Entrance = Square edge w/headwall (C) Coeff. K,M,c,Y,k = 0.0098, 2, 0.0398, 0.67, 0.5

Embankment

Top Elevation (ft) = 7619.36 Top Width (ft) = 60.00 Crest Width (ft) = 50.00

CULVERT LOCATION: PARCEL 3, BASIN A, CROSSING HOLMES

ROAD, DESIGN POINT 1

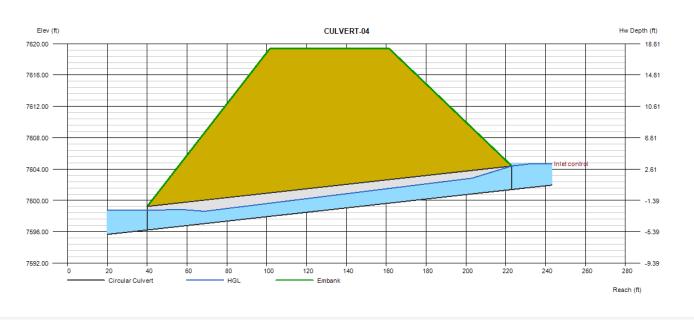
Calculations

Qmin (cfs) = 5.60 Qmax (cfs) = 41.30 Tailwater Elev (ft) = (dc+D)/2

Highlighted

Qtotal (cfs) = 40.60Qpipe (cfs) = 40.60Qovertop (cfs) = 0.00Veloc Dn (ft/s) = 6.37Veloc Up (ft/s) = 7.79HGL Dn (ft) = 7598.77HGL Up (ft) = 7603.46Hw Elev (ft) = 7604.69Hw/D (ft) = 1.10

Flow Regime = Inlet Control



Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Tuesday, Oct 10 2023

EX-CULVERT-01

Invert Elev Dn (ft) = 7532.00Pipe Length (ft) = 89.39Slope (%) = 3.36Invert Elev Up (ft) = 7535.00Rise (in) = 48.0= Circular Shape Span (in) = 48.0= 1 No. Barrels n-Value = 0.012

Culvert Type = Circular Concrete

Culvert Entrance = Square edge w/headwall (C) = 0.0098, 2, 0.0398, 0.67, 0.5Coeff. K,M,c,Y,k

Embankment

Top Elevation (ft) = 7543.82 Top Width (ft) = 50.00Crest Width (ft) = 50.00

CULVERT LOCATION: PARCEL 3-4, BASIN C, CROSSING OLD STAGECOACH ROAD, DESIGN

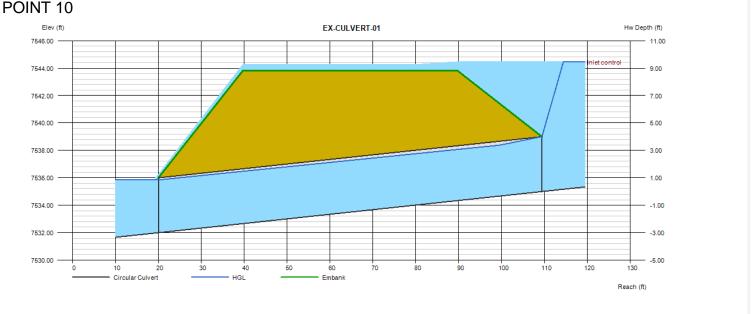
Calculations

Qmin (cfs) = 81.40Qmax (cfs) = 251.40Tailwater Elev (ft) = (dc+D)/2

Highlighted

Qtotal (cfs) = 241.40Qpipe (cfs) = 164.69Qovertop (cfs) = 76.71Veloc Dn (ft/s) = 13.27Veloc Up (ft/s) = 13.58HGL Dn (ft) = 7535.85 HGL Up (ft) = 7538.70Hw Elev (ft) = 7544.45Hw/D (ft) = 2.36

Flow Regime = Inlet Control



FLOW TO DP10 OVERTOPS OLD STAGECOACH ROAD UNDER SINGLE PIPE ANALYSIS, FUTURE FDR TO DELINEATE SUBBASINS AND REDUCE FLOW TO EXISTING **CULVERT PIPE**

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Tuesday, Oct 10 2023

EX-CULVERT-02

Invert Elev Dn (ft) = 7565.03Pipe Length (ft) = 70.34Slope (%) = 4.54Invert Elev Up (ft) = 7568.22Rise (in) = 30.0= Circular Shape Span (in) = 30.0No. Barrels = 1 n-Value = 0.012

Culvert Type = Circular Concrete

Culvert Entrance = Square edge w/headwall (C) Coeff. K,M,c,Y,k = 0.0098, 2, 0.0398, 0.67, 0.5

Embankment

Top Elevation (ft) = 7572.92Top Width (ft) = 50.00Crest Width (ft) = 50.00

CULVERT LOCATION: PARCEL 5-4,

BASIN E, CROSSING OLD STAGECOACH ROAD, DESIGN

POINT 14

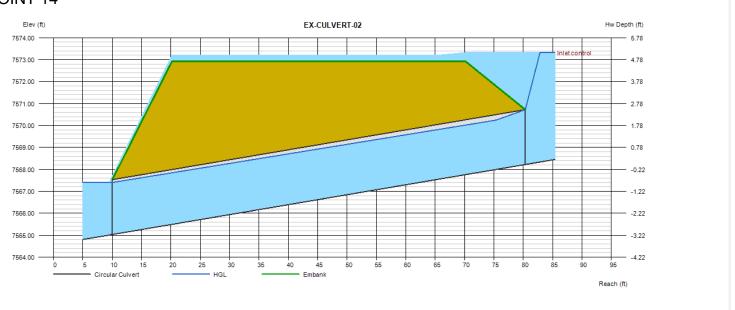
Calculations

Qmin (cfs) = 33.80 Qmax (cfs) = 85.50 Tailwater Elev (ft) = (dc+D)/2

Highlighted

Qtotal (cfs) = 83.80Qpipe (cfs) = 45.88Qovertop (cfs) = 37.92Veloc Dn (ft/s) = 9.54Veloc Up (ft/s) = 9.90HGL Dn (ft) = 7567.40HGL Up (ft) = 7570.46Hw Elev (ft) = 7573.32Hw/D (ft) = 2.04

Flow Regime = Inlet Control



FLOW TO DP14 OVERTOPS OLD STAGECOACH ROAD UNDER SINGLE PIPE ANALYSIS, FUTURE FDR TO DELINEATE SUBBASINS AND REDUCE FLOW TO EXISTING CULVERT PIPE

SWMM Model Schematic



NOTE: The summary statistics displayed in this report are based on results found at every computational time step, not just on results from each reporting time step.

Analysis Options ********

Flow Units CFS

Process Models:

Rainfall/Runoff NO
RDII NO
Snowmelt NO
Groundwater NO
Flow Routing YES
Ponding Allowed NO
Water Quality NO

Flow Routing Method KINWAVE

Starting Date 01/01/2005 00:00:00 Ending Date 01/04/2005 00:00:00

Antecedent Dry Days 0.0
Report Time Step 00:05:00
Routing Time Step 30.00 sec

********	Volume	Volume
Flow Routing Continuity	acre-feet	10^6 gal

Dry Weather Inflow	0.000	0.000
Wet Weather Inflow	0.000	0.000
Groundwater Inflow	0.000	0.000
RDII Inflow	0.000	0.000
External Inflow	63.827	20.799
External Outflow	63.465	20.681
Flooding Loss	0.000	0.000
Evaporation Loss	0.000	0.000
Exfiltration Loss	0.000	0.000
Initial Stored Volume	0.000	0.000
Final Stored Volume	0.368	0.120
Continuity Error (%)	-0.009	

Highest Flow Instability Indexes

Link 601 (1)

Routing Time Step Summary ************

Minimum Time Step : 30.00 sec
Average Time Step : 30.00 sec
Maximum Time Step : 30.00 sec
Percent in Steady State : 0.00
Average Iterations per Step : 1.00
Percent Not Converging : 0.00

STORAGE

STORAGE

Average Maximum Maximum Time of Max Reported Depth Depth HGL Occurrence Max Depth Node Type Feet Feet Feet days hr:min Feet 0.62 0S2 JUNCTION 0.01 7643.62 00:40 0.62 0S3 JUNCTION 0.02 0.68 7650.68 00:40 0.68 Α1 JUNCTION 0.01 0.61 7613.61 00:48 0.61 Α2 JUNCTION 0.04 1.32 7571.32 00:48 1.32 0S7 JUNCTION 0.02 0.68 7555.68 00:41 0.68 0.00 7558.00 Ι JUNCTION 0.00 00:00 0.00 056 0.04 1.32 00:49 JUNCTION 7553.32 1.32 0.00 01 OUTFALL 0.00 7511.00 00:00 0.00 IRR POND 0.44 3.98 7534.98 02:04 3.98 **STORAGE** 0 DP25 STORAGE 3.26 8.18 7567.18 0 01:27 8.18

8.70

5.18

7571.70

7557.18

01:30

01:24

8.70

5.18

DP3

DP7

Maximum Maximum Lateral
Total Flow
Lateral Total Time of Max Inflow
Inflow Balance
Inflow Inflow Occurrence Volume

3.00

0.14

Volume Node gal	Error Percent	Туре	CFS	CFS	days	hr:min	10^6 gal	10^6
052		JUNCTION	82.92	82.92	0	00:40	2.5	
2.5	0.000							
0S3		JUNCTION	65.20	65.20	0	00:40	1.73	
1.73	-0.000							
A1	0.000	JUNCTION	27.93	108.39	0	00:47	0.863	
3.38 A2	0.000	JUNCTION	9.10	117.37	0	00:48	0.45	
3.83	0.000	JUNCTION	9.10	11/.5/	Ø	00.40	0.45	
0S7	0.000	JUNCTION	59.52	124.65	0	00:41	1.94	
3.67	0.000				_			
I		JUNCTION	15.72	15.72	0	00:40	0.488	
0.488	0.000							
0S6		JUNCTION	161.12	313.79	0	00:56	6.45	
15.1	0.000	OUTEALL	0.00	206 27	•	02.04	•	
01 20.7	0.000	OUTFALL	0.00	206.37	0	02:04	0	
IRR_F		STORAGE	0.00	459.33	0	00:52	0	
20.7	0.060	STORAGE	0.00	- 32.33	Ū	00.52	· ·	
DP25		STORAGE	63.88	63.88	0	00:35	1.18	
1.18	0.068							
DP3		STORAGE	187.41	187.41	0	00:40	3.75	
3.75	0.052							
DP7	0.005	STORAGE	64.85	64.85	0	00:40	1.44	
1.44	0.006							

No nodes were flooded.

of Max Maximum	Average	Avg	Evap Exfil	Maximum	Max	Time
OT TIEX TIEXTIIIIII	Volume	Pcnt	Pcnt Pcnt	Volume	Pcnt	
Occurrence Outflow						

Storag hr:min	e Unit CFS	1000 ft3	Full	Loss	Loss	1000 ft3	Full	days
IRR_PO	ND	144.161	2	0	0	1374.169	21	0
02:03	206.37							
DP25		23.148	12	0	0	130.463	69	0
01:27	10.46							
DP3		59.026	13	0	0	359.899	79	0
01:29	43.10							
DP7		2.228	1	0	0	97.286	37	0
01:23	22.75	2.220	-	Ū	Ū	27.200	3,	Ŭ

Outfall Node	Flow Freq Pcnt	Avg Flow CFS	Max Flow CFS	Total Volume 10^6 gal
01	99.72	10.70	206.37	20.679
System	99.72	10.70	206.37	20.679

Link	Type	Maximum Flow CFS	0ccı	of Max urrence hr:min	Maximum Veloc ft/sec	Max/ Full Flow	Max/ Full Depth
400	CONDUIT	81.34	0	00:48	3.52	0.26	0.51
200	CONDUIT	65.16	0	00:41	20.26	0.00	0.14
401	CONDUIT	108.37	0	00:48	6.88	0.15	0.38
104	DUMMY	15.72	0	00:40			
402	CONDUIT	117.32	0	00:49	6.10	0.05	0.33
201	DUMMY	124.65	0	00:41			
602	DUMMY	313.79	0	00:56			
IRR_OUTLET	DUMMY	206.37	0	02:04			
601	DUMMY	10.46	0	01:27			
301	DUMMY	22.75	0	01:24			
502	DUMMY	43.10	0	01:30			

No conduits were surcharged.

Analysis begun on: Wed Oct 18 09:07:08 2023 Analysis ended on: Wed Oct 18 09:07:08 2023

Total elapsed time: < 1 sec

Summary of Unit Hydrograph Parameters Used By Program and Calculated Results (Version 2.0.1)

		Unit Hydrograph Parameters and Results									Precip.		Storm H	ydrograph	
Catchment Name/ID	СТ	Ср	W50 (min.)	W50 Before Peak	W75 (min.)	W75 Before Peak	Time to Peak (min.)	Peak (cfs)	Volume (c.f)	Excess (inches)	Excess (c.f.)	Time to Peak (min.)	Peak Flow (cfs)	Total Volume (c.f.)	Runoff per Unit Area (cfs/acre)
OS3	0.156	0.109	22.8	3.40	11.8	2.40	5.7	52	91,839	2.54	233,060	40.0	65	230,694	2.58
OS7	0.133	0.099	31.1	3.87	16.2	2.73	6.4	42	102,366	2.55	260,801	40.0	60	259,724	2.11
OS6	0.146	0.185	43.4	7.65	22.6	5.41	12.8	101	339,768	2.54	863,660	50.0	161	862,778	1.72
A1	0.137	0.071	28.8	3.07	15.0	2.17	5.1	21	45,738	2.55	116,439	40.0	28	115,392	2.22
A2	0.121	0.048	56.2	3.56	29.2	2.52	5.9	5	23,595	2.56	60,301	50.0	9	60,162	1.40
	0.103	0.050	28.9	2.60	15.0	1.84	4.3	12	25,773	2.58	66,421	40.0	16	65,254	2.21
OS2	0.156	0.128	28.1	4.26	14.6	3.01	7.1	61	132,132	2.54	335,312	40.0	83	334,189	2.28

Summary of CUHP Input Parameters (Version 2.0.1)

								Depression	n Storage	Storage Horton's Infiltration Parameters DCIA Level and Fractions				ctions		
Catchment Name/ID	SWMM Node/ID	Raingage Name/ID	Area (sq.mi.)	Dist. to Centroid (miles)	Length (miles)	Slope (ft./ft.)	Percent Imperv.	Pervious (inches)	Imperv. (inches)	Initial Rate (in./hr.)	Final Rate (in.hr.)	Decay Coeff. (1/sec.)	DCIA Level	Dir. Con'ct Imperv. Fraction	Receiv. Perv. Fraction	Percent Eff. Imperv.
OS3	OS3	100-YR	0.040	0.114	0.227	0.060	2.0	0.35	0.08	4.50	0.00	0.6000	0.00	0.04	0.02	2.00
OS7	OS7	100-YR	0.044	0.161	0.322	0.050	8.2	0.35	0.08	4.50	0.00	0.6000	0.00	0.16	0.08	8.20
OS6	OS6	100-YR	0.146	0.331	0.663	0.025	4.6	0.35	0.08	4.50	0.00	0.6000	0.00	0.09	0.05	4.60
A1	A1	100-YR	0.020	0.080	0.180	0.025	7.0	0.35	0.08	4.50	0.00	0.6000	0.00	0.14	0.07	7.00
A2	A2	100-YR	0.010	0.142	0.259	0.030	13.1	0.35	0.08	4.50	0.00	0.6000	0.00	0.26	0.11	13.10
I	I	100-YR	0.011	0.095	0.189	0.050	26.4	0.35	0.08	4.50	0.00	0.6000	0.00	0.53	0.16	26.40
OS2	OS2	100-YR	0.057	0.152	0.303	0.040	2.0	0.35	0.08	4.50	0.00	0.6000	0.00	0.04	0.02	2.00

Printouts for Storm Hydrographs

flow in cfs

The last color The		flow in cfs			•	•	•	,
5 0.00 0.	me in minutes	S3	25	98	1	2		S2
10							_	
15	-							
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105 15.80 24.02 90.14 10.26 6.26 5.74 29.45 110 13.58 22.24 83.47 9.37 5.98 5.25 26.76 115 12.08 20.56 78.19 8.54 5.70 4.77 24.20 120 11.15 18.97 74.07 7.74 5.42 4.32 21.78 125 8.95 16.28 69.09 6.35 4.99 3.55 17.83 130 6.98 13.55 63.09 5.03 4.56 2.81 14.02 135 5.44 10.96 57.15 3.93 4.17 2.20 11.02 140 4.21 8.68 51.50 3.14 3.84 1.75 8.81 145 3.26 6.83 46.26 2.52 3.55 1.41 7.04 150 2.51 5.47 41.53 2.02 3.30 1.13 5.63 155 1.93 4.42	95	21.41	28.11	105.10	12.22		6.85	35.41
110 13.58 22.24 83.47 9.37 5.98 5.25 26.76 115 12.08 20.56 78.19 8.54 5.70 4.77 24.20 120 11.15 18.97 74.07 7.74 5.42 4.32 21.78 125 8.95 16.28 69.09 6.35 4.99 3.55 17.83 130 6.98 13.55 63.09 5.03 4.56 2.81 14.02 135 5.44 10.96 57.15 3.93 4.17 2.20 11.02 140 4.21 8.68 51.50 3.14 3.84 1.75 8.81 145 3.26 6.83 46.26 2.52 3.55 1.41 7.04 150 2.51 5.47 41.53 2.02 3.30 1.13 5.63 155 1.93 4.42 37.07 1.61 3.07 0.90 4.47 160 1.48 3.54	100	18.51	25.95	97.48	11.19	6.54	6.27	32.30
115 12.08 20.56 78.19 8.54 5.70 4.77 24.20 120 11.15 18.97 74.07 7.74 5.42 4.32 21.78 125 8.95 16.28 69.09 6.35 4.99 3.55 17.83 130 6.98 13.55 63.09 5.03 4.56 2.81 14.02 135 5.44 10.96 57.15 3.93 4.17 2.20 11.02 140 4.21 8.68 51.50 3.14 3.84 1.75 8.81 145 3.26 6.83 46.26 2.52 3.55 1.41 7.04 150 2.51 5.47 41.53 2.02 3.30 1.13 5.63 155 1.93 4.42 37.07 1.61 3.07 0.90 4.47 160 1.48 3.54 32.83 1.27 2.85 0.71 3.51 165 1.16 2.83	105	15.80	24.02	90.14	10.26	6.26	5.74	29.45
120 11.15 18.97 74.07 7.74 5.42 4.32 21.78 125 8.95 16.28 69.09 6.35 4.99 3.55 17.83 130 6.98 13.55 63.09 5.03 4.56 2.81 14.02 135 5.44 10.96 57.15 3.93 4.17 2.20 11.02 140 4.21 8.68 51.50 3.14 3.84 1.75 8.81 145 3.26 6.83 46.26 2.52 3.55 1.41 7.04 150 2.51 5.47 41.53 2.02 3.30 1.13 5.63 155 1.93 4.42 37.07 1.61 3.07 0.90 4.47 160 1.48 3.54 32.83 1.27 2.85 0.71 3.51 165 1.16 2.83 28.78 1.00 2.65 0.56 2.74 170 0.88 2.24 <td< td=""><td>110</td><td>13.58</td><td>22.24</td><td>83.47</td><td>9.37</td><td>5.98</td><td>5.25</td><td>26.76</td></td<>	110	13.58	22.24	83.47	9.37	5.98	5.25	26.76
125 8.95 16.28 69.09 6.35 4.99 3.55 17.83 130 6.98 13.55 63.09 5.03 4.56 2.81 14.02 135 5.44 10.96 57.15 3.93 4.17 2.20 11.02 140 4.21 8.68 51.50 3.14 3.84 1.75 8.81 145 3.26 6.83 46.26 2.52 3.55 1.41 7.04 150 2.51 5.47 41.53 2.02 3.30 1.13 5.63 155 1.93 4.42 37.07 1.61 3.07 0.90 4.47 160 1.48 3.54 32.83 1.27 2.85 0.71 3.51 165 1.16 2.83 28.78 1.00 2.65 0.56 2.74 170 0.88 2.24 24.87 0.79 2.46 0.44 2.17 175 0.64 1.78 21	115	12.08	20.56	78.19	8.54	5.70	4.77	24.20
130 6.98 13.55 63.09 5.03 4.56 2.81 14.02 135 5.44 10.96 57.15 3.93 4.17 2.20 11.02 140 4.21 8.68 51.50 3.14 3.84 1.75 8.81 145 3.26 6.83 46.26 2.52 3.55 1.41 7.04 150 2.51 5.47 41.53 2.02 3.30 1.13 5.63 155 1.93 4.42 37.07 1.61 3.07 0.90 4.47 160 1.48 3.54 32.83 1.27 2.85 0.71 3.51 165 1.16 2.83 28.78 1.00 2.65 0.56 2.74 170 0.88 2.24 24.87 0.79 2.46 0.44 2.17 175 0.64 1.78 21.04 0.64 2.28 0.36 1.75 180 0.43 1.43 17.3	120	11.15	18.97	74.07	7.74	5.42	4.32	21.78
135 5.44 10.96 57.15 3.93 4.17 2.20 11.02 140 4.21 8.68 51.50 3.14 3.84 1.75 8.81 145 3.26 6.83 46.26 2.52 3.55 1.41 7.04 150 2.51 5.47 41.53 2.02 3.30 1.13 5.63 155 1.93 4.42 37.07 1.61 3.07 0.90 4.47 160 1.48 3.54 32.83 1.27 2.85 0.71 3.51 165 1.16 2.83 28.78 1.00 2.65 0.56 2.74 170 0.88 2.24 24.87 0.79 2.46 0.44 2.17 175 0.64 1.78 21.04 0.64 2.28 0.36 1.75 180 0.43 1.43 17.30 0.51 2.11 0.29 1.40 185 0.27 1.17 13.75<	125	8.95	16.28	69.09	6.35	4.99	3.55	17.83
140 4.21 8.68 51.50 3.14 3.84 1.75 8.81 145 3.26 6.83 46.26 2.52 3.55 1.41 7.04 150 2.51 5.47 41.53 2.02 3.30 1.13 5.63 155 1.93 4.42 37.07 1.61 3.07 0.90 4.47 160 1.48 3.54 32.83 1.27 2.85 0.71 3.51 165 1.16 2.83 28.78 1.00 2.65 0.56 2.74 170 0.88 2.24 24.87 0.79 2.46 0.44 2.17 175 0.64 1.78 21.04 0.64 2.28 0.36 1.75 180 0.43 1.43 17.30 0.51 2.11 0.29 1.40 185 0.27 1.17 13.75 0.41 1.95 0.23 1.10 190 0.15 0.94 10.79 <td>130</td> <td>6.98</td> <td>13.55</td> <td>63.09</td> <td>5.03</td> <td>4.56</td> <td>2.81</td> <td>14.02</td>	130	6.98	13.55	63.09	5.03	4.56	2.81	14.02
145 3.26 6.83 46.26 2.52 3.55 1.41 7.04 150 2.51 5.47 41.53 2.02 3.30 1.13 5.63 155 1.93 4.42 37.07 1.61 3.07 0.90 4.47 160 1.48 3.54 32.83 1.27 2.85 0.71 3.51 165 1.16 2.83 28.78 1.00 2.65 0.56 2.74 170 0.88 2.24 24.87 0.79 2.46 0.44 2.17 175 0.64 1.78 21.04 0.64 2.28 0.36 1.75 180 0.43 1.43 17.30 0.51 2.11 0.29 1.40 185 0.27 1.17 13.75 0.41 1.95 0.23 1.10 190 0.15 0.94 10.79 0.32 1.79 0.18 0.84 195 0.06 0.75 8.68 <td>135</td> <td>5.44</td> <td>10.96</td> <td></td> <td>3.93</td> <td>4.17</td> <td>2.20</td> <td>11.02</td>	135	5.44	10.96		3.93	4.17	2.20	11.02
150 2.51 5.47 41.53 2.02 3.30 1.13 5.63 155 1.93 4.42 37.07 1.61 3.07 0.90 4.47 160 1.48 3.54 32.83 1.27 2.85 0.71 3.51 165 1.16 2.83 28.78 1.00 2.65 0.56 2.74 170 0.88 2.24 24.87 0.79 2.46 0.44 2.17 175 0.64 1.78 21.04 0.64 2.28 0.36 1.75 180 0.43 1.43 17.30 0.51 2.11 0.29 1.40 185 0.27 1.17 13.75 0.41 1.95 0.23 1.10 190 0.15 0.94 10.79 0.32 1.79 0.18 0.84 195 0.06 0.75 8.68 0.24 1.64 0.13 0.61 200 0.01 0.57 7.09	140	4.21	8.68		3.14	3.84	1.75	8.81
155 1.93 4.42 37.07 1.61 3.07 0.90 4.47 160 1.48 3.54 32.83 1.27 2.85 0.71 3.51 165 1.16 2.83 28.78 1.00 2.65 0.56 2.74 170 0.88 2.24 24.87 0.79 2.46 0.44 2.17 175 0.64 1.78 21.04 0.64 2.28 0.36 1.75 180 0.43 1.43 17.30 0.51 2.11 0.29 1.40 185 0.27 1.17 13.75 0.41 1.95 0.23 1.10 190 0.15 0.94 10.79 0.32 1.79 0.18 0.84 195 0.06 0.75 8.68 0.24 1.64 0.13 0.61 200 0.01 0.57 7.09 0.17 1.48 0.10 0.42 205 0.00 0.32 4.81		3.26	6.83	46.26	2.52	3.55	1.41	7.04
160 1.48 3.54 32.83 1.27 2.85 0.71 3.51 165 1.16 2.83 28.78 1.00 2.65 0.56 2.74 170 0.88 2.24 24.87 0.79 2.46 0.44 2.17 175 0.64 1.78 21.04 0.64 2.28 0.36 1.75 180 0.43 1.43 17.30 0.51 2.11 0.29 1.40 185 0.27 1.17 13.75 0.41 1.95 0.23 1.10 190 0.15 0.94 10.79 0.32 1.79 0.18 0.84 195 0.06 0.75 8.68 0.24 1.64 0.13 0.61 200 0.01 0.57 7.09 0.17 1.48 0.10 0.42 205 0.00 0.42 5.83 0.11 1.33 0.06 0.26 210 0.00 0.30 4.81	150		5.47	41.53	2.02	3.30	1.13	5.63
165 1.16 2.83 28.78 1.00 2.65 0.56 2.74 170 0.88 2.24 24.87 0.79 2.46 0.44 2.17 175 0.64 1.78 21.04 0.64 2.28 0.36 1.75 180 0.43 1.43 17.30 0.51 2.11 0.29 1.40 185 0.27 1.17 13.75 0.41 1.95 0.23 1.10 190 0.15 0.94 10.79 0.32 1.79 0.18 0.84 195 0.06 0.75 8.68 0.24 1.64 0.13 0.61 200 0.01 0.57 7.09 0.17 1.48 0.10 0.42 205 0.00 0.42 5.83 0.11 1.33 0.06 0.26 210 0.00 0.30 4.81 0.07 1.19 0.04 0.14 215 0.00 0.11 3.22	155	1.93	4.42	37.07	1.61	3.07	0.90	4.47
170 0.88 2.24 24.87 0.79 2.46 0.44 2.17 175 0.64 1.78 21.04 0.64 2.28 0.36 1.75 180 0.43 1.43 17.30 0.51 2.11 0.29 1.40 185 0.27 1.17 13.75 0.41 1.95 0.23 1.10 190 0.15 0.94 10.79 0.32 1.79 0.18 0.84 195 0.06 0.75 8.68 0.24 1.64 0.13 0.61 200 0.01 0.57 7.09 0.17 1.48 0.10 0.42 205 0.00 0.42 5.83 0.11 1.33 0.06 0.26 210 0.00 0.30 4.81 0.07 1.19 0.04 0.14 215 0.00 0.19 3.95 0.03 1.04 0.02 0.06 220 0.00 0.11 3.22								
175 0.64 1.78 21.04 0.64 2.28 0.36 1.75 180 0.43 1.43 17.30 0.51 2.11 0.29 1.40 185 0.27 1.17 13.75 0.41 1.95 0.23 1.10 190 0.15 0.94 10.79 0.32 1.79 0.18 0.84 195 0.06 0.75 8.68 0.24 1.64 0.13 0.61 200 0.01 0.57 7.09 0.17 1.48 0.10 0.42 205 0.00 0.42 5.83 0.11 1.33 0.06 0.26 210 0.00 0.30 4.81 0.07 1.19 0.04 0.14 215 0.00 0.19 3.95 0.03 1.04 0.02 0.06 220 0.00 0.11 3.22 0.01 0.90 0.01 0.01 225 0.00 0.05 2.61	165	1.16	2.83	28.78	1.00	2.65	0.56	2.74
180 0.43 1.43 17.30 0.51 2.11 0.29 1.40 185 0.27 1.17 13.75 0.41 1.95 0.23 1.10 190 0.15 0.94 10.79 0.32 1.79 0.18 0.84 195 0.06 0.75 8.68 0.24 1.64 0.13 0.61 200 0.01 0.57 7.09 0.17 1.48 0.10 0.42 205 0.00 0.42 5.83 0.11 1.33 0.06 0.26 210 0.00 0.30 4.81 0.07 1.19 0.04 0.14 215 0.00 0.19 3.95 0.03 1.04 0.02 0.06 220 0.00 0.11 3.22 0.01 0.90 0.01 0.01 225 0.00 0.05 2.61 0.00 0.63 0.00 0.00 230 0.00 0.01 2.14	170	0.88	2.24	24.87	0.79	2.46	0.44	2.17
185 0.27 1.17 13.75 0.41 1.95 0.23 1.10 190 0.15 0.94 10.79 0.32 1.79 0.18 0.84 195 0.06 0.75 8.68 0.24 1.64 0.13 0.61 200 0.01 0.57 7.09 0.17 1.48 0.10 0.42 205 0.00 0.42 5.83 0.11 1.33 0.06 0.26 210 0.00 0.30 4.81 0.07 1.19 0.04 0.14 215 0.00 0.19 3.95 0.03 1.04 0.02 0.06 220 0.00 0.11 3.22 0.01 0.90 0.01 0.01 225 0.00 0.05 2.61 0.00 0.76 0.00 0.00 230 0.00 0.01 2.14 0.00 0.63 0.00 0.00 235 0.00 0.00 1.73	175	0.64	1.78	21.04	0.64	2.28	0.36	1.75
190 0.15 0.94 10.79 0.32 1.79 0.18 0.84 195 0.06 0.75 8.68 0.24 1.64 0.13 0.61 200 0.01 0.57 7.09 0.17 1.48 0.10 0.42 205 0.00 0.42 5.83 0.11 1.33 0.06 0.26 210 0.00 0.30 4.81 0.07 1.19 0.04 0.14 215 0.00 0.19 3.95 0.03 1.04 0.02 0.06 220 0.00 0.11 3.22 0.01 0.90 0.01 0.01 225 0.00 0.05 2.61 0.00 0.76 0.00 0.00 230 0.00 0.01 2.14 0.00 0.63 0.00 0.00 235 0.00 0.00 1.73 0.00 0.51 0.00 0.00	180	0.43	1.43	17.30	0.51	2.11	0.29	1.40
195 0.06 0.75 8.68 0.24 1.64 0.13 0.61 200 0.01 0.57 7.09 0.17 1.48 0.10 0.42 205 0.00 0.42 5.83 0.11 1.33 0.06 0.26 210 0.00 0.30 4.81 0.07 1.19 0.04 0.14 215 0.00 0.19 3.95 0.03 1.04 0.02 0.06 220 0.00 0.11 3.22 0.01 0.90 0.01 0.01 225 0.00 0.05 2.61 0.00 0.76 0.00 0.00 230 0.00 0.01 2.14 0.00 0.63 0.00 0.00 235 0.00 0.00 1.73 0.00 0.51 0.00 0.00	185	0.27	1.17	13.75	0.41	1.95	0.23	1.10
200 0.01 0.57 7.09 0.17 1.48 0.10 0.42 205 0.00 0.42 5.83 0.11 1.33 0.06 0.26 210 0.00 0.30 4.81 0.07 1.19 0.04 0.14 215 0.00 0.19 3.95 0.03 1.04 0.02 0.06 220 0.00 0.11 3.22 0.01 0.90 0.01 0.01 225 0.00 0.05 2.61 0.00 0.76 0.00 0.00 230 0.00 0.01 2.14 0.00 0.63 0.00 0.00 235 0.00 0.00 1.73 0.00 0.51 0.00 0.00	190	0.15	0.94	10.79	0.32	1.79	0.18	0.84
205 0.00 0.42 5.83 0.11 1.33 0.06 0.26 210 0.00 0.30 4.81 0.07 1.19 0.04 0.14 215 0.00 0.19 3.95 0.03 1.04 0.02 0.06 220 0.00 0.11 3.22 0.01 0.90 0.01 0.01 225 0.00 0.05 2.61 0.00 0.76 0.00 0.00 230 0.00 0.01 2.14 0.00 0.63 0.00 0.00 235 0.00 0.00 1.73 0.00 0.51 0.00 0.00	195	0.06	0.75	8.68	0.24	1.64	0.13	0.61
210 0.00 0.30 4.81 0.07 1.19 0.04 0.14 215 0.00 0.19 3.95 0.03 1.04 0.02 0.06 220 0.00 0.11 3.22 0.01 0.90 0.01 0.01 225 0.00 0.05 2.61 0.00 0.76 0.00 0.00 230 0.00 0.01 2.14 0.00 0.63 0.00 0.00 235 0.00 0.00 1.73 0.00 0.51 0.00 0.00	200	0.01	0.57	7.09	0.17	1.48	0.10	0.42
215 0.00 0.19 3.95 0.03 1.04 0.02 0.06 220 0.00 0.11 3.22 0.01 0.90 0.01 0.01 225 0.00 0.05 2.61 0.00 0.76 0.00 0.00 230 0.00 0.01 2.14 0.00 0.63 0.00 0.00 235 0.00 0.00 1.73 0.00 0.51 0.00 0.00	205	0.00	0.42	5.83	0.11	1.33	0.06	0.26
220 0.00 0.11 3.22 0.01 0.90 0.01 0.01 225 0.00 0.05 2.61 0.00 0.76 0.00 0.00 230 0.00 0.01 2.14 0.00 0.63 0.00 0.00 235 0.00 0.00 1.73 0.00 0.51 0.00 0.00	210	0.00	0.30	4.81	0.07	1.19	0.04	0.14
225 0.00 0.05 2.61 0.00 0.76 0.00 0.00 230 0.00 0.01 2.14 0.00 0.63 0.00 0.00 235 0.00 0.00 1.73 0.00 0.51 0.00 0.00	215	0.00	0.19	3.95	0.03	1.04	0.02	0.06
230 0.00 0.01 2.14 0.00 0.63 0.00 0.00 235 0.00 0.00 1.73 0.00 0.51 0.00 0.00	220	0.00	0.11	3.22	0.01	0.90	0.01	0.01
235 0.00 0.00 1.73 0.00 0.51 0.00 0.00	225	0.00	0.05	2.61	0.00	0.76	0.00	0.00
	230	0.00	0.01	2.14	0.00	0.63	0.00	0.00
240 0.00 0.00 1.38 0.00 0.40 0.00 0.00	235	0.00	0.00	1.73	0.00	0.51	0.00	0.00
	240	0.00	0.00	1.38	0.00	0.40	0.00	0.00

245	0.00	0.00	1.07	0.00	0.33	0.00	0.00
250	0.00	0.00	0.80	0.00	0.27	0.00	0.00
255	0.00	0.00	0.57	0.00	0.23	0.00	0.00
260	0.00	0.00	0.37	0.00	0.19	0.00	0.00
265	0.00	0.00	0.22	0.00	0.15	0.00	0.00
270	0.00	0.00	0.11	0.00	0.12	0.00	0.00
275	0.00	0.00	0.03	0.00	0.10	0.00	0.00
280	0.00	0.00	0.00	0.00	0.08	0.00	0.00
285	0.00	0.00	0.00	0.00	0.07	0.00	0.00
290	0.00	0.00	0.00	0.00	0.05	0.00	0.00
295	0.00	0.00	0.00	0.00	0.04	0.00	0.00
300	0.00	0.00	0.00	0.00	0.03	0.00	0.00
305	0.00	0.00	0.00	0.00	0.02	0.00	0.00
310	0.00	0.00	0.00	0.00	0.01	0.00	0.00
315	0.00	0.00	0.00	0.00	0.01	0.00	0.00
320	0.00	0.00	0.00	0.00	0.00	0.00	0.00
325	0.00	0.00	0.00	0.00	0.00	0.00	0.00
330	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Printouts for Unit Hydrographs

flow in cfs

	flow in cfs	1	1	1			1
time in minutes	623	250	950	A1	A2		052
5	51.09	39.50	49.24	20.51	5.23	11.52	53.35
10	49.36	41.72	94.61	19.77	5.39	10.99	59.82
15	39.36	38.17	100.74	17.46	5.26	9.64	53.72
20	32.65	31.77	96.65	14.56	5.04	8.10	43.95
25	26.09	27.93	88.26	12.57	4.73	7.00	37.74
30	22.25	24.08	75.74	10.59	4.32	5.90	31.53
35	18.43	20.65	68.93	9.28	3.94	5.19	27.43
40	14.60	18.38	62.12	8.10	3.68	4.53	23.81
45	10.78	16.12	55.31	6.92	3.42	3.87	20.19
50	9.26	13.86	49.38	5.75	3.16	3.22	16.58
55	7.99	11.59	45.46	4.57	2.90	2.56	12.96
60	6.72	9.33	41.53	3.87	2.67	2.17	11.22
65	5.44	8.02	37.60	3.47	2.51	1.95	10.01
70	4.17	7.26	33.67	3.08	2.35	1.74	8.80
75	2.89	6.51	29.75	2.69	2.19	1.52	7.60
80	1.62	5.75	25.82	2.30	2.04	1.30	6.39
85	0.34	5.00	21.89	1.90	1.88	1.08	5.18
90	0.00	4.25	19.48	1.51	1.72	0.86	3.98
95		3.49	18.17	1.12	1.56	0.64	2.77
100		2.74	16.86	0.73	1.41	0.42	1.57
105		1.98	15.55	0.33	1.25	0.20	0.36
110		1.23	14.24	0.00	1.09	0.00	0.00
115		0.47	12.93		1.03		
120		0.00	11.62		0.98		
125			10.31		0.93		
130			9.00		0.88		
135			7.70		0.82		
140			6.39		0.77		
145			5.08		0.72		
150			3.77		0.67		
155			2.46		0.61		
160			1.15		0.56		
165			0.00		0.51		
170					0.46		
175					0.41		
180					0.35		
185					0.30		
190					0.25		
195					0.20		
200					0.14		
205					0.09		
210					0.04		
215					0.00		





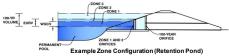
Appendix D:

Water Quality & Detention Basin Calculations

MHFD-Detention, Version 4.06 (July 2022)

Project: FLYING HORSE NORTH PUD PRELIMINARY PLAN





Watershed Information

ersilea mitorinadori		
Selected BMP Type =	EDB	
Watershed Area =	93.10	acres
Watershed Length =	2,250	ft
Watershed Length to Centroid =	800	ft
Watershed Slope =	0.040	ft/ft
Watershed Imperviousness =	12.30%	percent
Percentage Hydrologic Soil Group A =	0.0%	percent
Percentage Hydrologic Soil Group B =	100.0%	percent
Percentage Hydrologic Soil Groups C/D =	0.0%	percent
Target WQCV Drain Time =	40.0	hours
Location for 1-hr Rainfall Depths =	User Input	

After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using

the embedded Colorado Urban Hydro	graph Procedu	re.
Water Quality Capture Volume (WQCV) =	0.618	acre-feet
Excess Urban Runoff Volume (EURV) =	1.094	acre-feet
2-yr Runoff Volume (P1 = 1.19 in.) =	1.411	acre-feet
5-yr Runoff Volume (P1 = 1.5 in.) =	2.948	acre-feet
10-yr Runoff Volume (P1 = 1.75 in.) =	4.463	acre-feet
25-yr Runoff Volume (P1 = 2 in.) =	7.102	acre-feet
50-yr Runoff Volume (P1 = 2.25 in.) =	8.925	acre-feet
100-yr Runoff Volume (P1 = 2.52 in.) =	11.525	acre-feet
500-yr Runoff Volume (P1 = 3.14 in.) =	16.296	acre-feet
Approximate 2-yr Detention Volume =	0.714	acre-feet
Approximate 5-yr Detention Volume =	1.100	acre-feet
Approximate 10-yr Detention Volume =	2.097	acre-feet
Approximate 25-yr Detention Volume =	2.828	acre-feet
Approximate 50-yr Detention Volume =	2.973	acre-feet
Approximate 100-yr Detention Volume =	3.793	acre-feet

Define Zones and Basin Geometry

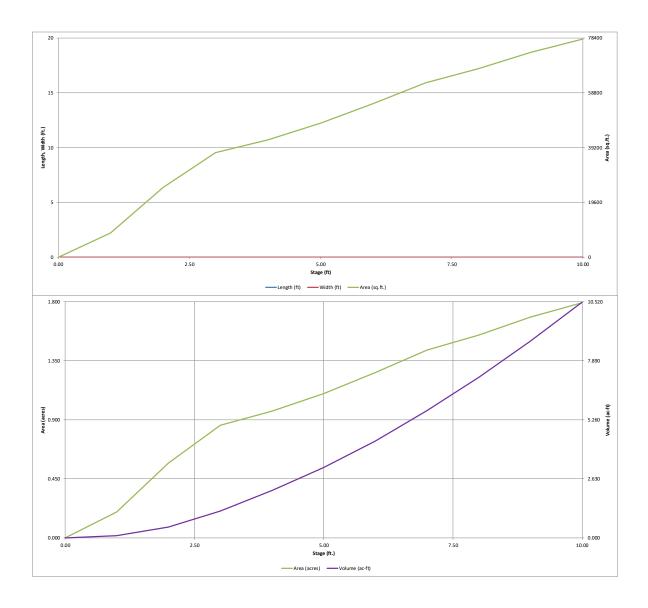
Define Zones and Basin Geometry		
Zone 1 Volume (WQCV) =	0.618	acre-
Zone 2 Volume (EURV - Zone 1) =	0.476	acre-
Zone 3 Volume (100-year - Zones 1 & 2) =	2.699	acre-
Total Detention Basin Volume =	3.793	acre-
Initial Surcharge Volume (ISV) =	user	ft ³
Initial Surcharge Depth (ISD) =	user	ft
Total Available Detention Depth (H _{total}) =	user	ft
Depth of Trickle Channel (H _{TC}) =	user	ft
Slope of Trickle Channel $(S_{TC}) =$	user	ft/ft
Slopes of Main Basin Sides (Smain) =	user	H:V
Basin Length-to-Width Ratio (R _{L/W}) =	user	

Initial Surcharge Area $(A_{ISV}) =$	user	ft²
Surcharge Volume Length (L_{ISV}) =	user	ft
Surcharge Volume Width $(W_{ISV}) =$	user	ft
Depth of Basin Floor $(H_{FLOOR}) =$	user	ft
Length of Basin Floor (L_{FLOOR}) =	user	ft
Width of Basin Floor $(W_{FLOOR}) =$	user	ft
Area of Basin Floor $(A_{FLOOR}) =$	user	ft 2
Volume of Basin Floor (V _{FLOOR}) =	user	ft ³
Depth of Main Basin (H _{MAIN}) =	user	ft
Length of Main Basin (LMAIN) =	user	ft
Width of Main Basin (W _{MAIN}) =	user	ft
Area of Main Basin $(A_{MAIN}) =$	user	ft 2
Volume of Main Basin (V_{MAIN}) =	user	ft ³
Calculated Total Basin Volume (Vtotal) =	user	acre-fe

Depth Increment =		fl
Stage - Storage	Stage	

on Pond)		Stage - Storage Description	Stage (ft)	Optional Override Stage (ft)	Length (ft)	Width (ft)	Area (ft²)	Optional Override Area (ft ²)	Area (acre)	Volume (ft ³)	Volume (ac-ft)
	7562	Top of Micropool		0.00	-		-	0	0.000		
				1.00 2.00			-	8,622 24,877	0.198 0.571	4,311 21,060	0.099
				3.00	_	-	-	37,363	0.858	52,180	1.198
				4.00	-		-	42,000	0.964	91,862	2.109
				5.00	-		-	47,874	1.099	136,799	3.140
				6.00 7.00			-	54,892 62,293	1.260	188,182 246,774	4.320 5.665
				8.00	-		-	67,350	1.546	311,596	7.153
				9.00	-		-	73,250	1.682	381,896	8.767
		TOP: 7572		10.00	-		-	78,100	1.793	457,571	10.504
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Optional Use	acre-feet				-		-				
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1.50	inches inches				-	-	-				
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Pond A_PUD-10-19-23.xlsm, Basin 10/19/2023, 9:34 AM



Pond A_PUD-10-19-23.xkm, Basin 10/19/2023, 9:34 AM

DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.06 (July 2022)
Project: FLYING HORSE NORTH PUD PRELIMINARY PLAN

Basin ID: BASINS: A, OS1; DESIGN POINT 3

Example Zone Configuration (Retention Pond)

	Estimated	Estimated	
_	Stage (ft)	Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	2.23	0.618	Orifice Plate
Zone 2 (EURV)	2.88	0.476	Orifice Plate
Zone 3 (100-year)	5.58	2.699	Weir&Pipe (Restrict)
-	Total (all zones)	3.793	

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

N/A ft (distance below the filtration media surface) Underdrain Orifice Invert Depth = Underdrain Orifice Diameter = N/A inches

Calculated Parameters for Underdrain Underdrain Orifice Area ft² N/A Underdrain Orifice Centroid = feet N/A

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Centroid of Lowest Orifice = 0.00 ft (relative to basin bottom at Stage = 0 ft) Depth at top of Zone using Orifice Plate : 3.00 ft (relative to basin bottom at Stage = 0 ft) Orifice Plate: Orifice Vertical Spacing N/A inches Orifice Plate: Orifice Area per Row = 4.00 sq. inches (use rectangular openings)

Calculated Parameters for Plate WQ Orifice Area per Row 2.778E-02 ft² Elliptical Half-Width N/A feet Elliptical Slot Centroid N/A feet ft² Elliptical Slot Area = N/A

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	1.50	2.50					
Orifice Area (sq. inches)	4.00	4.00	4.00					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

	Not Selected	Not Selected		
Invert of Vertical Orifice =	N/A	N/A	ft (relative to basin bottom at Stage = 0 ft)	Vertical Orifice Area =
Depth at top of Zone using Vertical Orifice =	N/A	N/A	ft (relative to basin bottom at Stage = 0 ft)	Vertical Orifice Centroid =
Vertical Orifice Diameter =	N/A	N/A	inches	·

Calculated Parameters for Vertical Orif Not Selected Not Selected N/A N/A N/A N/A

nput: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir and No Outlet Pipe) Calculated Parameters for Overflow W								
	Zone 3 Weir	Not Selected		Zone 3 Weir	Not Selected			
Overflow Weir Front Edge Height, Ho =	4.00	N/A	ft (relative to basin bottom at Stage = 0 ft) $\frac{1}{2}$ Height of Grate Upper Edge, $\frac{1}{2}$	6.00	N/A			
Overflow Weir Front Edge Length =	6.00	N/A	feet Overflow Weir Slope Length =	6.32	N/A			
Overflow Weir Grate Slope =	3.00	N/A	H:V Grate Open Area / 100-yr Orifice Area =	8.45	N/A			
Horiz. Length of Weir Sides =	6.00	N/A	feet Overflow Grate Open Area w/o Debris =	26.41	N/A			
Overflow Grate Type =	Type C Grate	N/A	Overflow Grate Open Area w/ Debris =	13.21	N/A			
Debris Clogging % =	50%	N/A	%					

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

er Input: Outlet Pipe w/ Flow Restriction Plate	(Circular Orifice, Re	estrictor Plate, or R	ectangular Orifice)	Calculated Parameters	Calculated Parameters for Outlet Pipe w/ Flow Res		
	Zone 3 Restrictor	Not Selected			Zone 3 Restrictor	Not Selected	1
Depth to Invert of Outlet Pipe =	0.50	N/A	ft (distance below basin bottom at Stage = 0 ft)	Outlet Orifice Area =	3.13	N/A	1
Outlet Pipe Diameter =	24.00	N/A	inches	Outlet Orifice Centroid =	1.00	N/A	1
Restrictor Plate Height Above Pipe Invert =	23.50		inches Half-Central And	gle of Restrictor Plate on Pipe =	2.85	N/A	1

<u>User Input: Emergency Spillway (Rectangular or Trapezoidal)</u>

ut: Emergency Spiliway (Rectangular or	<u>rrapezoidar)</u>	
Spillway Invert Stage=	9.00	ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length =	50.00	feet
Spillway End Slopes =	4.00	H:V
Freeboard above Max Water Surface =	1.00	feet
•		='

Calculated Parameters for Spillway

Spillway Design Flow Depth=	1.10	feet
Stage at Top of Freeboard =	11.10	feet
Basin Area at Top of Freeboard =	1.79	acres
Basin Volume at Top of Freeboard =	10.50	acre-ft

Routed Hydrograph Results Design Storm Return Perio One-Hour Rainfall Depth (in Inflow CUHP

OPTIONAL Override

CUHP Runoff Volume (acre-ft) =
Inflow Hydrograph Volume (acre-ft) =
CUHP Predevelopment Peak Q (cfs) =
TIONAL Override Predevelopment Peak Q (cfs) =
Predevelopment Unit Peak Flow, q (cfs/acre) =
Peak Inflow Q (cfs) =
Peak Outflow Q (cfs) =
Ratio Peak Outflow to Predevelopment Q =
Structure Controlling Flow =
Max Velocity through Grate 1 (fps) =
Max Velocity through Grate 2 (fps) =
Time to Drain 97% of Inflow Volume (hours) =
Time to Drain 99% of Inflow Volume (hours) =
Maximum Ponding Depth (ft) =

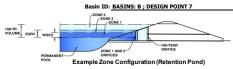
Area at Maximum Ponding Depth (acres

ograph Results	The user can overt	ride the default CUF	IP hydrographs and	runoff volumes by	entering new value	es in the Inflow Hyd	rographs table (Col	umns W through Ai
Design Storm Return Period =	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year
One-Hour Rainfall Depth (in) =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52
CUHP Runoff Volume (acre-ft) =	0.618	1.094	1.411	2.948	4.463	7.102	8.925	11.525
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	1.411	2.948	4.463	7.102	8.925	11.525
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A	15.8	43.9	65.0	113.0	141.5	177.4
verride Predevelopment Peak Q (cfs) =	N/A	N/A						
lopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.17	0.47	0.70	1.21	1.52	1.91
Peak Inflow Q (cfs) =	N/A	N/A	27.2	55.4	76.6	123.4	151.6	187.4
Peak Outflow Q (cfs) =	0.3	0.5	0.5	2.5	9.9	28.3	39.7	43.1
Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	0.1	0.2	0.3	0.3	0.2
Structure Controlling Flow =	Plate	Plate	Plate	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Outlet Plate 1	Outlet Plate 1
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	0.1	0.3	1.0	1.5	1.6
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Drain 97% of Inflow Volume (hours) =	38	51	58	76	74	69	65	62
Drain 99% of Inflow Volume (hours) =	40	54	62	82	83	81	80	78
Maximum Ponding Depth (ft) =	2.23	2.88	3.16	4.62	5.54	6.78	7.46	8.69
at Maximum Ponding Depth (acres) =		0.82	0.87	1.05	1.19	1.39	1.48	1.64
Maximum Volume Stored (acre-ft) =	0.622	1.097	1.336	2.733	3.757	5.355	6.335	8.252

Pond A PUD-10-19-23.xlsm, Outlet Structure 10/19/2023, 3:20 PM

MHFD-Detention, Version 4.06 (July 2022)

Project: FLYING HORSE NORTH PUD PRELIMINARY PLAN



Watershed Information

ersned information		
Selected BMP Type =	EDB	
Watershed Area =	32.69	acres
Watershed Length =	1,500	ft
Watershed Length to Centroid =	650	ft
Watershed Slope =	0.040	ft/ft
Watershed Imperviousness =	24.10%	percent
Percentage Hydrologic Soil Group A =	0.0%	percent
Percentage Hydrologic Soil Group B =	100.0%	percent
Percentage Hydrologic Soil Groups C/D =	0.0%	percent
Target WQCV Drain Time =	40.0	hours
Location for 1-br Rainfall Denths =	User Input	

After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using

the embedded Colorado Urban Hydrograph Procedure.							
Water Quality Capture Volume (WQCV) =	0.359	acre-feet					
Excess Urban Runoff Volume (EURV) =	0.794	acre-feet					
2-yr Runoff Volume (P1 = 1.19 in.) =	0.830	acre-feet					
5-yr Runoff Volume (P1 = 1.5 in.) =	1.433	acre-feet					
10-yr Runoff Volume (P1 = 1.75 in.) =	1.999	acre-feet					
25-yr Runoff Volume (P1 = 2 in.) =	2.889	acre-feet					
50-yr Runoff Volume (P1 = 2.25 in.) =	3.542	acre-feet					
100-yr Runoff Volume (P1 = 2.52 in.) =	4.433	acre-feet					
500-yr Runoff Volume (P1 = 3.14 in.) =	6.124	acre-feet					
Approximate 2-yr Detention Volume =	0.556	acre-feet					
Approximate 5-yr Detention Volume =	0.810	acre-feet					
Approximate 10-yr Detention Volume =	1.244	acre-feet					
Approximate 25-yr Detention Volume =	1.493	acre-feet					
Approximate 50-yr Detention Volume =	1.576	acre-feet					
Approximate 100-yr Detention Volume =	1.904	acre-feet					

r Overrides
acre-feet
acre-feet
inches

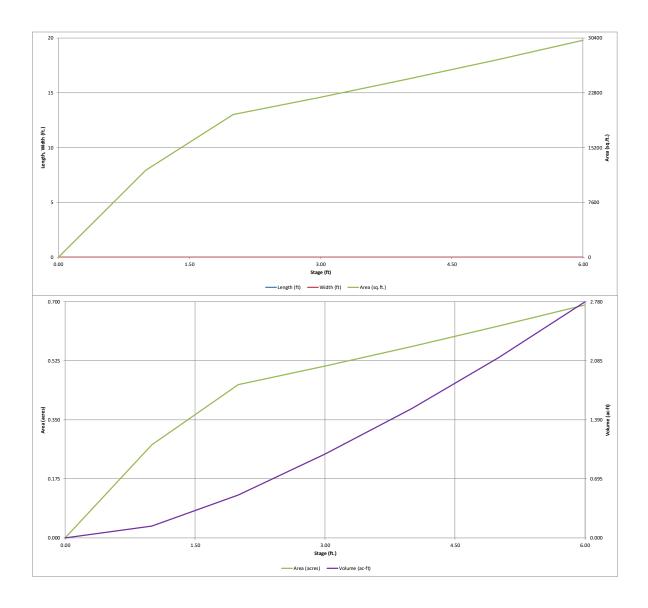
Define Zones and Basin Geometry

		Define Zones and Dasin Geomedy
acre-fe	0.359	Zone 1 Volume (WQCV) =
acre-fe	0.436	Zone 2 Volume (EURV - Zone 1) =
acre-fe	1.110	Zone 3 Volume (100-year - Zones 1 & 2) =
acre-fe	1.904	Total Detention Basin Volume =
ft ³	user	Initial Surcharge Volume (ISV) =
ft	user	Initial Surcharge Depth (ISD) =
ft	user	Total Available Detention Depth (H _{total}) =
ft	user	Depth of Trickle Channel (H_{TC}) =
ft/ft	user	Slope of Trickle Channel $(S_{TC}) =$
H:V	user	Slopes of Main Basin Sides (Smain) =
	user	Basin Length-to-Width Ratio (R _{L/W}) =

Initial Surcharge Area $(A_{ISV}) =$	user	ft ²
Surcharge Volume Length $(L_{ISV}) =$	user	ft
Surcharge Volume Width $(W_{ISV}) =$	user	ft
Depth of Basin Floor $(H_{FLOOR}) =$	user	ft
Length of Basin Floor (L_{FLOOR}) =	user	ft
Width of Basin Floor $(W_{FLOOR}) =$	user	ft
Area of Basin Floor $(A_{FLOOR}) =$		ft²
Volume of Basin Floor $(V_{FLOOR}) =$	user	ft ³
Depth of Main Basin $(H_{MAIN}) =$	user	ft
Length of Main Basin $(L_{MAIN}) =$	user	ft
Width of Main Basin $(W_{MAIN}) =$	user	ft
Area of Main Basin $(A_{MAIN}) =$		ft²
Volume of Main Basin $(V_{MAIN}) =$	user	ft ³
Calculated Total Basin Volume (V_{total}) =	user	acre-feet

_	ı		1							
	Depth Increment =		ft Optional				Optional			I
	Stage - Storage	Stage	Override	Length	Width	Area	Override	Area	Volume	Volume
7552	Description Top of Micropool	(ft) 	Stage (ft) 0.00	(ft) 	(ft) 	(ft²)	Area (ft 2)	(acre) 0.000	(ft ³)	(ac-ft)
/552			1.00	_		-	12,035	0.276	6,017	0.138
			2.00	-		_	19,768	0.454	21,919	0.503
			3.00	-		-	22,182	0.509	42,894	0.985
		-	4.00	-	-	-	24,710	0.567	66,340	1.523
			5.00	-	-	-	27,347	0.628	92,368	2.120
	TOP:7558		6.00	-		-	30,105	0.691	121,094	2.780
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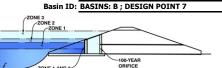
Pond B_PUD, Basin 9/28/2023, 12:39 PM



Pond B_PUD, Basin 9/28/2023, 12:39 PM

DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.06 (July 2022)
Project: FLYING HORSE NORTH PUD PRELIMINARY PLAN



Example Zone Configuration (Retention Pond)

	Estimated	Estimated	
_	Stage (ft)	Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	1.66	0.359	Orifice Plate
Zone 2 (EURV)	2.62	0.436	Orifice Plate
one 3 (100-year)	4.65	1.110	Weir&Pipe (Restrict)
·	Total (all zones)	1.904	

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth = N/A ft (distance below the filtration media surface) Underdrain Orifice Diameter = inches N/A

Calculated Parameters for Underdrain Underdrain Orifice Area N/A Underdrain Orifice Centroid = feet N/A

Calculated Parameters for Plate

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Centroid of Lowest Orifice = 0.00 ft (relative to basin bottom at Stage = 0 ft) Depth at top of Zone using Orifice Plate : 3.50 ft (relative to basin bottom at Stage = 0 ft) Orifice Plate: Orifice Vertical Spacing N/A inches Orifice Plate: Orifice Area per Row = N/A sq. inches

WQ Orifice Area per Row N/A ft² Elliptical Half-Width N/A feet Elliptical Slot Centroid N/A feet ft² Elliptical Slot Area = N/A

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	1.50	2.50					
Orifice Area (sq. inches)	3.25	3.25	6.00					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (ontional)	Row 13 (ontional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)		rton 10 (optional)	rion 11 (optional)	rion 12 (optional)	rtorr 15 (optional)	rion 11 (optional)	rion 15 (optional)	rion 10 (optional)
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

	Not Selected	Not Selected	
Invert of Vertical Orifice =	N/A	N/A	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Vertical Orifice =	N/A	N/A	ft (relative to basin bottom at Stage = 0 ft)
Vertical Orifice Diameter =	N/A	N/A	inches

Calculated Parameters for Vertical Orif Not Selected Not Selected Vertical Orifice Area N/A N/A Vertical Orifice Centroid = N/A N/A

Calculated Parameters for Overflow We

lot Selected N/A N/A N/A N/A N/A

User Input:	Overflow Weir	(Dropbox with Fl	at or Slop	ed Grate an	d Outlet Pipe	e OR Recta	angular/Tr	rapezoidal Weir	r and No Outlet Pi	ipe)
			7,	no 2 Mair	Not So	locted				

	Zone 3 Weir	Not Selected		Zone 3 Weir	No
Overflow Weir Front Edge Height, Ho =	4.00	N/A	ft (relative to basin bottom at Stage = 0 ft) Height of Grate Upper Edge, H_t =	4.00	
Overflow Weir Front Edge Length =	6.00	N/A	feet Overflow Weir Slope Length =	6.00	
Overflow Weir Grate Slope =	0.00	N/A	H:V Grate Open Area / 100-yr Orifice Area =	9.91	
Horiz. Length of Weir Sides =	6.00	N/A	feet Overflow Grate Open Area w/o Debris =	25.06	
Overflow Grate Type =	Type C Grate	N/A	Overflow Grate Open Area w/ Debris =	12.53	
Debris Clogging % =	50%	N/A	%		

er Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Re			ectangular Orifice)	Calculated Parameters	Calculated Parameters for Outlet Pipe w/ Flow Restrict		
	Zone 3 Restrictor	Not Selected			Zone 3 Restrictor	Not Selected	ı
Depth to Invert of Outlet Pipe =	0.50	N/A	ft (distance below basin bottom at Stage	= 0 ft) Outlet Orifice Area =	2.53	N/A	ı
Outlet Pipe Diameter =	24.00	N/A	inches	Outlet Orifice Centroid =	0.83	N/A	ı
Restrictor Plate Height Above Pipe Invert =	18.00		inches Half-Cen	tral Angle of Restrictor Plate on Pipe =	2.09	N/A	ı

The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through A

User Input: Emergency Spillway (Rectangular or Trapezoidal)

but. Emergency Spiliway (Rectangular or	TTUPCZOIGGI)	
Spillway Invert Stage=	6.00	ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length =	50.00	feet
Spillway End Slopes =	4.00	H:V
Freeboard above Max Water Surface =	1.00	feet

Calculated Parameters for Spillway

Spillway Design Flow Depth=	0.55	feet
Stage at Top of Freeboard =	7.55	feet
Basin Area at Top of Freeboard =	0.69	acres
Basin Volume at Top of Freeboard =	2.78	acre-ft

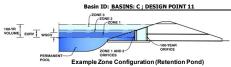
Routed Hydrograph Results

Design Storm Return Period =	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year
One-Hour Rainfall Depth (in) =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52
CUHP Runoff Volume (acre-ft) =		0.794	0.830	1.433	1.999	2.889	3.542	4.433
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	0.830	1.433	1.999	2.889	3.542	4.433
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A	4.8	13.2	19.8	34.8	43.6	54.6
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A						
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.15	0.41	0.61	1.06	1.33	1.67
Peak Inflow Q (cfs) =	N/A	N/A	12.9	22.3	29.8	44.1	53.3	64.8
Peak Outflow Q (cfs) =	0.2	0.4	0.3	0.6	5.6	19.2	25.9	27.9
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	0.0	0.3	0.6	0.6	0.5
Structure Controlling Flow =	Plate	Plate	Plate	Plate	Overflow Weir 1	Overflow Weir 1	Outlet Plate 1	Outlet Plate 1
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	N/A	0.2	0.7	1.0	1.1
Max Velocity through Grate 2 (fps) =		N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	38	57	59	70	72	69	66	63
Time to Drain 99% of Inflow Volume (hours) =	40	60	62	75	78	77	76	74
Maximum Ponding Depth (ft) =	1.66	2.62	2.59	3.68	4.25	4.61	4.85	5.57
Area at Maximum Ponding Depth (acres) =		0.49	0.49	0.55	0.58	0.60	0.62	0.66
Maximum Volume Stored (acre-ft) =	0.359	0.795	0.776	1.344	1.667	1.880	2.027	2.489

Pond B_PUD.xlsm, Outlet Structure 10/19/2023, 3:16 PM

MHFD-Detention, Version 4.06 (July 2022)

Project: FLYING HORSE NORTH PUD PRELIMINARY PLAN



Watershed Information

Selected BMP Type =	EDB				
Watershed Area =	121.00	acres			
Watershed Length =	2,500	ft			
Watershed Length to Centroid =	1,250	ft			
Watershed Slope =	0.010	ft/ft			
Watershed Imperviousness =	31.60%	percent			
Percentage Hydrologic Soil Group A =	0.0%	percent			
Percentage Hydrologic Soil Group B =	100.0%	percent			
Percentage Hydrologic Soil Groups C/D =	0.0%	percent			
Target WQCV Drain Time =	40.0	hours			
Location for 1-hr Rainfall Depths = User Input					

After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Liban Hydrograph Procedure

the embedded Colorado Urban Hydrograph Procedure.					
Water Quality Capture Volume (WQCV) =	1.577	acre-feet			
Excess Urban Runoff Volume (EURV) =	3.940	acre-feet			
2-yr Runoff Volume (P1 = 1.19 in.) =	3.965	acre-feet			
5-yr Runoff Volume (P1 = 1.5 in.) =	6.340	acre-feet			
10-yr Runoff Volume (P1 = 1.75 in.) =	8.517	acre-feet			
25-yr Runoff Volume (P1 = 2 in.) =	11.776	acre-feet			
50-yr Runoff Volume (P1 = 2.25 in.) =	14.262	acre-feet			
100-yr Runoff Volume (P1 = 2.52 in.) =	17.560	acre-feet			
500-yr Runoff Volume (P1 = 3.14 in.) =	23.960	acre-feet			
Approximate 2-yr Detention Volume =	2.834	acre-feet			
Approximate 5-yr Detention Volume =	4.038	acre-feet			
Approximate 10-yr Detention Volume =	5.823	acre-feet			
Approximate 25-yr Detention Volume =	6.705	acre-feet			
Approximate 50-yr Detention Volume =	7.060	acre-feet			
Approximate 100-yr Detention Volume =	8.302	acre-feet			
		=			

Optional User Overrides				
	acre-feet			
	acre-feet			
1.19	inches			
1.50	inches			
1.75	inches			
2.00	inches			
2.25	inches			
2.52	inches			
	inches			

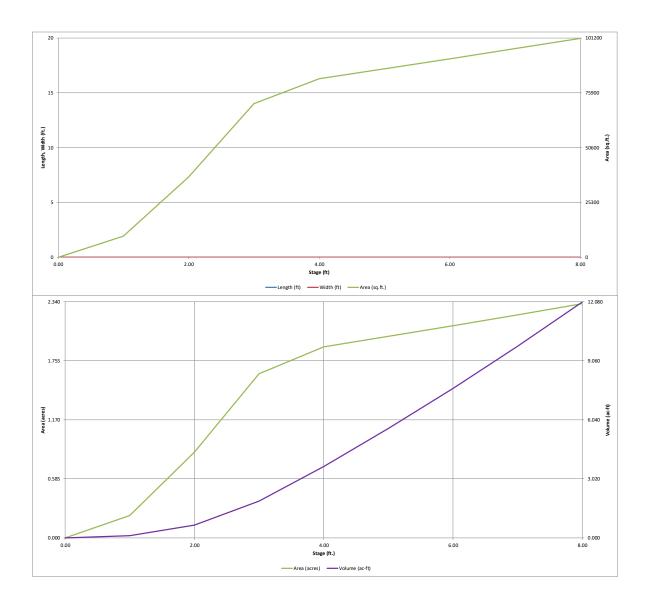
Define Zones and Basin Geometry

Define Zones and Basin Geometry		
Zone 1 Volume (WQCV) =	1.577	acre-feet
Zone 2 Volume (EURV - Zone 1) =	2.364	acre-feet
Zone 3 Volume (100-year - Zones 1 & 2) =	4.361	acre-feet
Total Detention Basin Volume =	8.302	acre-feet
Initial Surcharge Volume (ISV) =	user	ft ³
Initial Surcharge Depth (ISD) =	user	ft
Total Available Detention Depth (H _{total}) =	user	ft
Depth of Trickle Channel (H _{TC}) =	user	ft
Slope of Trickle Channel (S_{TC}) =	user	ft/ft
Slopes of Main Basin Sides (Smain) =	user	H:V
Basin Length-to-Width Ratio (R _{L/W}) =	user	

Initial Surcharge Area $(A_{ISV}) =$	user	ft ²
Surcharge Volume Length $(L_{ISV}) =$	user	ft
Surcharge Volume Width $(W_{ISV}) =$	user	ft
Depth of Basin Floor $(H_{FLOOR}) =$	user	ft
Length of Basin Floor (L_{FLOOR}) =	user	ft
Width of Basin Floor $(W_{FLOOR}) =$	user	ft
Area of Basin Floor $(A_{FLOOR}) =$	user	ft²
Volume of Basin Floor (V _{FLOOR}) =	user	ft ³
Depth of Main Basin $(H_{MAIN}) =$	user	ft
Length of Main Basin $(L_{MAIN}) =$	user	ft
Width of Main Basin $(W_{MAIN}) =$	user	ft
Area of Main Basin $(A_{MAIN}) =$	user	ft ²
Volume of Main Basin $(V_{MAIN}) =$	user	ft ³
Calculated Total Basin Volume (V_{total}) =	user	acre-fee

	1		اـ							
	Depth Increment =		ft Optional				Optional			
	Stage - Storage Description	Stage (ft)	Override Stage (ft)	Length (ft)	Width (ft)	Area (ft²)	Override Area (ft ²)	Area (acre)	Volume (ft 3)	Volume (ac-ft)
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		-	1.00	-	-	-	9,667	0.222	4,833	0.111
			2.00				37,002	0.849	28,168	0.647
			3.00	-		-	70,876	1.627	82,106	1.885
	7531		4.00 5.00	-		-	82,455 86,963	1.893 1.996	158,772 243,481	3.645 5.590
	7531		6.00	_		-	91,578	2.102	332,751	7.639
			7.00	-			96,300	2.211	426,690	9.795
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Pond C_PUD, Basin 9/28/2023, 12:41 PM

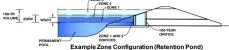


Pond C_PUD, Basin 9/28/2023, 12:41 PM

MHFD-Detention, Version 4.06 (July 2022)

Project: FLYING HORSE NORTH PUD PRELIMINARY PLAN





Watershed Information

tershed Information		
Selected BMP Type =	EDB	
Watershed Area =	158.50	acres
Watershed Length =	2,250	ft
Watershed Length to Centroid =	1,100	ft
Watershed Slope =	0.025	ft/ft
Watershed Imperviousness =	15.50%	percent
Percentage Hydrologic Soil Group A =	0.0%	percent
Percentage Hydrologic Soil Group B =	100.0%	percent
Percentage Hydrologic Soil Groups C/D =	0.0%	percent
Target WQCV Drain Time =	40.0	hours
Location for 1-hr Rainfall Depths =	User Input	

After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using

the embedded Colorado Urban Hydrograph Procedure.					
Water Quality Capture Volume (WQCV) =	1.264	acre-feet			
Excess Urban Runoff Volume (EURV) =	2.391	acre-feet			
2-yr Runoff Volume (P1 = 1.19 in.) =	2.840	acre-feet			
5-yr Runoff Volume (P1 = 1.5 in.) =	5.559	acre-feet			
10-yr Runoff Volume (P1 = 1.75 in.) =	8.198	acre-feet			
25-yr Runoff Volume (P1 = 2 in.) =	12.663	acre-feet			
50-yr Runoff Volume (P1 = 2.25 in.) =	15.793	acre-feet			
100-yr Runoff Volume (P1 = 2.52 in.) =	20.207	acre-feet			
500-yr Runoff Volume (P1 = 3.14 in.) =	28.375	acre-feet			
Approximate 2-yr Detention Volume =	1.597	acre-feet			
Approximate 5-yr Detention Volume =	2.416	acre-feet			
Approximate 10-yr Detention Volume =	4.232	acre-feet			
Approximate 25-yr Detention Volume =	5.479	acre-feet			
Approximate 50-yr Detention Volume =	5.780	acre-feet			
Approximate 100-yr Detention Volume =	7.254	acre-feet			

Define Zones and Basin Geometry

Define Zones and Basin Geometry		
Zone 1 Volume (WQCV) =	1.264	acre-feet
Zone 2 Volume (EURV - Zone 1) =	1.127	acre-feet
Zone 3 Volume (100-year - Zones 1 & 2) =	4.863	acre-feet
Total Detention Basin Volume =	7.254	acre-feet
Initial Surcharge Volume (ISV) =	user	ft ³
Initial Surcharge Depth (ISD) =	user	ft
Total Available Detention Depth (H _{total}) =	user	ft
Depth of Trickle Channel (H _{TC}) =	user	ft
Slope of Trickle Channel (S_{TC}) =	user	ft/ft
Slopes of Main Basin Sides (Smain) =	user	H:V
Basin Length-to-Width Ratio (R _{L/W}) =	user	

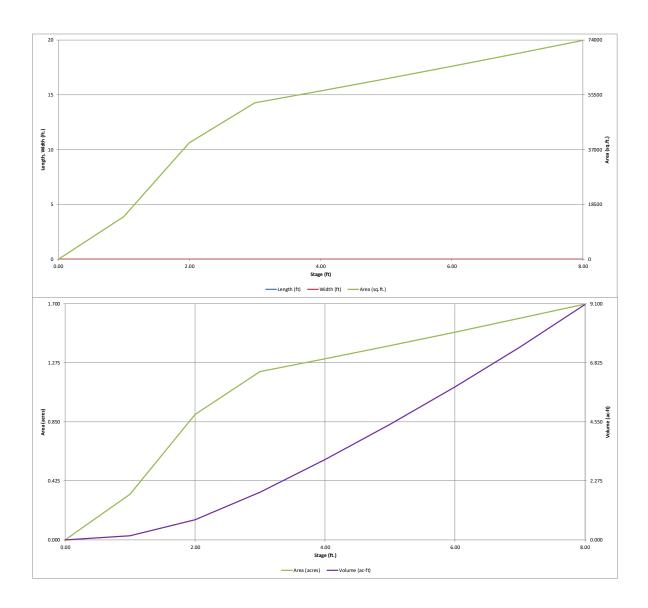
Initial Surcharge Area $(A_{ISV}) =$	user	ft ²
Surcharge Volume Length $(L_{ISV}) =$	user	ft
Surcharge Volume Width $(W_{ISV}) =$	user	ft
Depth of Basin Floor $(H_{FLOOR}) =$	user	ft
Length of Basin Floor (L_{FLOOR}) =	user	ft
Width of Basin Floor $(W_{FLOOR}) =$	user	ft
Area of Basin Floor $(A_{FLOOR}) =$	user	ft²
Volume of Basin Floor $(V_{FLOOR}) =$	user	ft ³
Depth of Main Basin $(H_{MAIN}) =$	user	ft
Length of Main Basin $(L_{MAIN}) =$	user	ft
Width of Main Basin (W_{MAIN}) =	user	ft
Area of Main Basin $(A_{MAIN}) =$	user	ft²
Volume of Main Basin $(V_{MAIN}) =$	user	ft ³
Calculated Total Basin Volume (V_{total}) =	user	acre-feet

Not	e: L	/ w	Ratio	< 1
L / 1	W R	atio	= 0.7	3

1.19 inches 1.50 inches 1.75 inches 2.00 inches 2.25 inches 2.52 inches inches

7530 Top of Micropool 0.00 0 0.000 W Ratio < 1 1.00 14,296 0.328 7,147 0.164		Depth Increment = Stage - Storage Description	Stage (ft)	ft Optional Override Stage (ft)	Length (ft)	Width (ft)	Area (ft²)	Optional Override Area (ft ²)	Area (acre)	Volume (ft ³)	Volume (ac-ft)
*** Natio 4*** 1 100	7530										
1	W Ratio < 1		1	1.00	-		-	14,296	0.328	7,147	0.164
1	o = 0.73		1	2.00	-		-	39,265	0.901	33,928	0.779
				3.00				52,784	1.212	79,952	1.835
1.0 5.00 1.0			-	4.00	-		-	56,790	1.304	134,739	3.093
1007538			-	5.00	-		-	60,908	1.398	193,588	4.444
TOP7398			ł	6.00	-	-	-	65,138	1.495	256,611	5.891
			1	7.00	-	-	-	69,479	1.595	323,920	7.436
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Pond D_PUD, Basin 9/28/2023, 1:16 PM



Pond D_PUD, Basin 9/28/2023, 1:16 PM

MHFD-Detention, Version 4.06 (July 2022)

Project: FLYING HORSE NORTH PUD PRELIMINARY PLAN



Watershed Information

CI SIICG IIII GIIII GUOII		
Selected BMP Type =	EDB	
Watershed Area =	52.40	acres
Watershed Length =	1,700	ft
Watershed Length to Centroid =	650	ft
Watershed Slope =	0.050	ft/ft
Watershed Imperviousness =	43.70%	percent
Percentage Hydrologic Soil Group A =	0.0%	percent
Percentage Hydrologic Soil Group B =	100.0%	percent
Percentage Hydrologic Soil Groups C/D =	0.0%	percent
Target WQCV Drain Time =	40.0	hours
Location for 1-br Rainfall Denths =	User Innut	

After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using

the embedded Colorado Urban Hydrograph Procedure.					
Water Quality Capture Volume (WQCV) =	0.828	acre-feet			
Excess Urban Runoff Volume (EURV) =	2.422	acre-feet			
2-yr Runoff Volume (P1 = 1.19 in.) =	2.287	acre-feet			
5-yr Runoff Volume (P1 = 1.5 in.) =	3.360	acre-feet			
10-yr Runoff Volume (P1 = 1.75 in.) =	4.316	acre-feet			
25-yr Runoff Volume (P1 = 2 in.) =	5.656	acre-feet			
50-yr Runoff Volume (P1 = 2.25 in.) =	6.714	acre-feet			
100-yr Runoff Volume (P1 = 2.52 in.) =	8.081	acre-feet			
500-yr Runoff Volume (P1 = 3.14 in.) =	10.820	acre-feet			
Approximate 2-yr Detention Volume =	1.802	acre-feet			
Approximate 5-yr Detention Volume =	2.498	acre-feet			
Approximate 10-yr Detention Volume =	3.384	acre-feet			
Approximate 25-yr Detention Volume =	3.748	acre-feet			
Approximate 50-yr Detention Volume =	3.928	acre-feet			
Approximate 100-yr Detention Volume =	4.454	acre-feet			

Optional User Overrides				
	acre-feet			
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1.19	inches			
1.50	inches			
1.75	inches			
2.00	inches			
2.25	inches			
2.52	inches			
	inches			

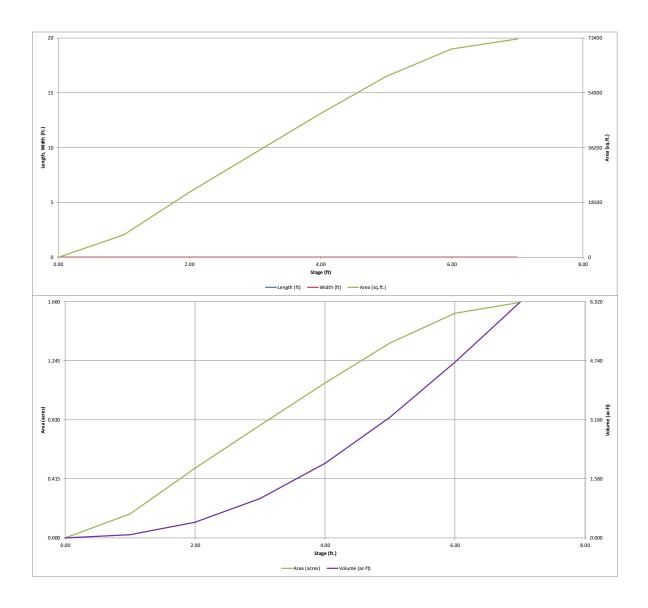
Define Zones and Basin Geometry

Define Zones and Basin Geometry		
Zone 1 Volume (WQCV) =	0.828	acre-feet
Zone 2 Volume (EURV - Zone 1) =	1.594	acre-feet
Zone 3 Volume (100-year - Zones 1 & 2) =	2.032	acre-feet
Total Detention Basin Volume =	4.454	acre-feet
Initial Surcharge Volume (ISV) =	user	ft ³
Initial Surcharge Depth (ISD) =	user	ft
Total Available Detention Depth (H _{total}) =	user	ft
Depth of Trickle Channel (H _{TC}) =	user	ft
Slope of Trickle Channel $(S_{TC}) =$	user	ft/ft
Slopes of Main Basin Sides (Smain) =	user	H:V
Basin Length-to-Width Ratio ($R_{L/W}$) =	user	

Initial Surcharge Area $(A_{ISV}) =$	user	ft ²
Surcharge Volume Length $(L_{ISV}) =$	user	ft
Surcharge Volume Width $(W_{ISV}) =$	user	ft
Depth of Basin Floor $(H_{FLOOR}) =$	user	ft
Length of Basin Floor (L_{FLOOR}) =	user	ft
Width of Basin Floor $(W_{FLOOR}) =$		ft
Area of Basin Floor $(A_{FLOOR}) =$		ft²
Volume of Basin Floor $(V_{FLOOR}) =$	user	ft ³
Depth of Main Basin (H _{MAIN}) =	user	ft
Length of Main Basin $(L_{MAIN}) =$	user	ft
Width of Main Basin $(W_{MAIN}) =$	user	ft
Area of Main Basin $(A_{MAIN}) =$	user	ft ²
Volume of Main Basin (V _{MAIN}) =	user	ft 3
Calculated Total Basin Volume (V_{total}) =	user	acre-feet

	Depth Increment = Stage - Storage Description	Stage (ft)	ft Optional Override Stage (ft)	Length (ft)	Width (ft)	Area (ft²)	Optional Override Area (ft ²)	Area (acre)	Volume (ft ³)	Volume (ac-ft)
7550	Top of Micropool		0.00	-		-	0	0.000		
			1.00			-	7,378	0.169	3,689	0.085
			2.00	-		-	21,376	0.491	18,066	0.415
			3.00	-	1	1	34,450	0.791	45,979	1.056
			4.00	-	-	1	47,390	1.088	86,899	1.995
			5.00	-		-	59,670	1.370	140,429	3.224
			6.00	-		-	68,780	1.579	204,654	4.698
	TOP:7557		7.00			-	72,120	1.656	275,104	6.316
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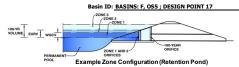
Pond E_PUD, Basin 9/28/2023, 1:22 PM



Pond E_PUD, Basin 9/28/2023, 1:22 PM

MHFD-Detention, Version 4.06 (July 2022)

Project: FLYING HORSE NORTH PUD PRELIMINARY PLAN



Watershed Information

croned information					
Selected BMP Type =	EDB				
Watershed Area =	238.70	acres			
Watershed Length =	5,000	ft			
Watershed Length to Centroid =	1,200	ft			
Watershed Slope =	0.040	ft/ft			
Watershed Imperviousness =	14.10%	percent			
Percentage Hydrologic Soil Group A =	0.0%	percent			
Percentage Hydrologic Soil Group B =	100.0%	percent			
Percentage Hydrologic Soil Groups C/D =	0.0%	percent			
Target WQCV Drain Time =	40.0	hours			
Location for 1-br Rainfall Denths = User Input					

After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using

the embedded Colorado Urban Hydrograph Procedure.						
Water Quality Capture Volume (WQCV) =	1.768	acre-feet				
Excess Urban Runoff Volume (EURV) =	3.252	acre-feet				
2-yr Runoff Volume (P1 = 1.19 in.) =	4.000	acre-feet				
5-yr Runoff Volume (P1 = 1.5 in.) =	8.042	acre-feet				
10-yr Runoff Volume (P1 = 1.75 in.) =	11.991	acre-feet				
25-yr Runoff Volume (P1 = 2 in.) =	18.755	acre-feet				
50-yr Runoff Volume (P1 = 2.25 in.) =	23.467	acre-feet				
100-yr Runoff Volume (P1 = 2.52 in.) =	30.144	acre-feet				
500-yr Runoff Volume (P1 = 3.14 in.) =	42.456	acre-feet				
Approximate 2-yr Detention Volume =	2.151	acre-feet				
Approximate 5-yr Detention Volume =	3.279	acre-feet				
Approximate 10-yr Detention Volume =	5.936	acre-feet				
Approximate 25-yr Detention Volume =	7.816	acre-feet				
Approximate 50-yr Detention Volume =	8.236	acre-feet				
Approximate 100-yr Detention Volume =	10.409	acre-feet				

Define Zones and Basin Geometry

Define Zones and Basin Geometry		
Zone 1 Volume (WQCV) =	1.768	acre-feet
Zone 2 Volume (EURV - Zone 1) =	1.484	acre-feet
Zone 3 Volume (100-year - Zones 1 & 2) =	7.158	acre-feet
Total Detention Basin Volume =	10.409	acre-feet
Initial Surcharge Volume (ISV) =	user	ft ³
Initial Surcharge Depth (ISD) =	user	ft
Total Available Detention Depth (H _{total}) =	user	ft
Depth of Trickle Channel (H _{TC}) =	user	ft
Slope of Trickle Channel $(S_{TC}) =$	user	ft/ft
Slopes of Main Basin Sides (Smain) =	user	H:V
Basin Length-to-Width Ratio (R _{L/W}) =	user	

Initial Surcharge Area $(A_{ISV}) =$	user	ft ²
Surcharge Volume Length $(L_{ISV}) =$	user	ft
Surcharge Volume Width $(W_{ISV}) =$	user	ft
Depth of Basin Floor (H_{FLOOR}) =	user	ft
Length of Basin Floor (L_{FLOOR}) =	user	ft
Width of Basin Floor $(W_{FLOOR}) =$	user	ft
Area of Basin Floor $(A_{FLOOR}) =$	user	ft ²
Volume of Basin Floor (V _{FLOOR}) =	user	ft ³
Depth of Main Basin $(H_{MAIN}) =$	user	ft
Length of Main Basin $(L_{MAIN}) =$	user	ft
Width of Main Basin (W _{MAIN}) =	user	ft
Area of Main Basin $(A_{MAIN}) =$	user	ft ²
Volume of Main Basin (V_{MAIN}) =	user	ft ³
Calculated Total Basin Volume (V_{total}) =	user	acre-fee

	Depth Increment =		ft					
	Stage - Storage Description	Stage (ft)	Optional Override Stage (ft)	Length (ft)	Width (ft)	Area (ft²)	Optional Override Area (ft ²)	Area (acre)
7438	Top of Micropool	-	0.00	-		-	0	0.000
		-	1.00	-		-	13,590	0.312
			2.00	-		-	46,610	1.070
			3.00	-		-	78,060	1.792
		1	4.00	-		1	104,890	2.408
	7443	1	5.00	-		1	116,640	2.678
		-	6.00	-		1	123,550	2.836
			7.00	-		-	130,667	3.000
	7446		8.00	-		-	138,017	3.168
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Volume (ft ³)

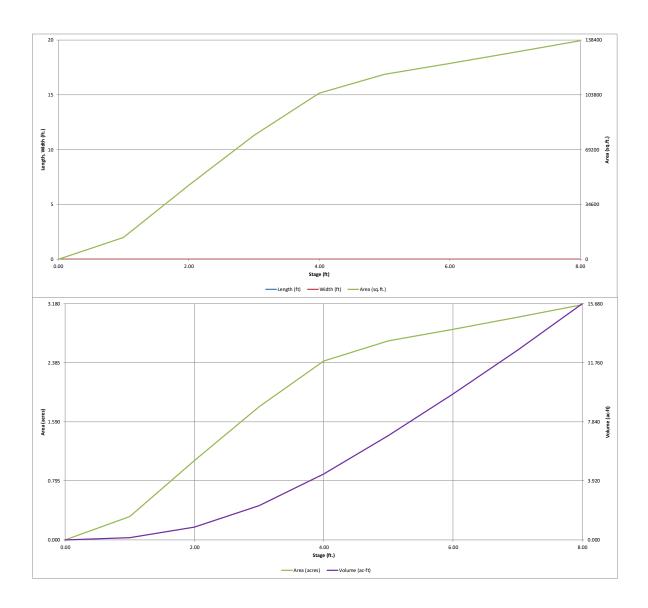
6,795 0.156 36,894

Volume (ac-ft)

0.847

			-	2.00	-		-	46,610	1.0/0	36,894	0.847
			1	3.00	-		-	78,060	1.792	99,229	2.278
				4.00	-		-	104,890	2.408	190,704	4.378
		7443	-	5.00	-		-	116,640	2.678	301,469	6.921
				6.00	-		-	123,550	2.836	421,564	9.678
				7.00	-		-	130,667	3.000	548,673	12.596
		7446	_	8.00	_		_	138,017	3.168	683,015	15.680
		7440	-	0.00	_		_	130,017	3.100	003,013	13.000
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Optional User	r Overrides				-		-				
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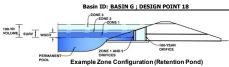
Pond F_PUD, Basin 9/28/2023, 1:23 PM



Pond F_PUD, Basin 9/28/2023, 1:23 PM

MHFD-Detention, Version 4.06 (July 2022)

Project: FLYING HORSE NORTH PUD PRELIMINARY PLAN



Watershed Information

Selected BMP Type =	EDB				
Watershed Area =	27.30	acres			
Watershed Length =	1,650	ft			
Watershed Length to Centroid =	800	ft			
Watershed Slope =	0.030	ft/ft			
Watershed Imperviousness =	16.40%	percent			
Percentage Hydrologic Soil Group A =	0.0%	percent			
Percentage Hydrologic Soil Group B =	100.0%	percent			
Percentage Hydrologic Soil Groups C/D =	0.0%	percent			
Target WQCV Drain Time =	40.0	hours			
Location for 1-hr Rainfall Depths = User Input					

After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure

the embedded Colorado Urban Hydrograph Procedure.						
Water Quality Capture Volume (WQCV) =	0.227	acre-feet				
Excess Urban Runoff Volume (EURV) =	0.438	acre-feet				
2-yr Runoff Volume (P1 = 1.19 in.) =	0.511	acre-feet				
5-yr Runoff Volume (P1 = 1.5 in.) =	0.984	acre-feet				
10-yr Runoff Volume (P1 = 1.75 in.) =	1.441	acre-feet				
25-yr Runoff Volume (P1 = 2 in.) =	2.209	acre-feet				
50-yr Runoff Volume (P1 = 2.25 in.) =	2.749	acre-feet				
100-yr Runoff Volume (P1 = 2.52 in.) =	3.509	acre-feet				
500-yr Runoff Volume (P1 = 3.14 in.) =	4.918	acre-feet				
Approximate 2-yr Detention Volume =	0.294	acre-feet				
Approximate 5-yr Detention Volume =	0.443	acre-feet				
Approximate 10-yr Detention Volume =	0.761	acre-feet				
Approximate 25-yr Detention Volume =	0.976	acre-feet				
Approximate 50-yr Detention Volume =	1.030	acre-feet				
Approximate 100-yr Detention Volume =	1.287	acre-feet				
		-				

Optional User Overrides				
	acre-feet			
	acre-feet			
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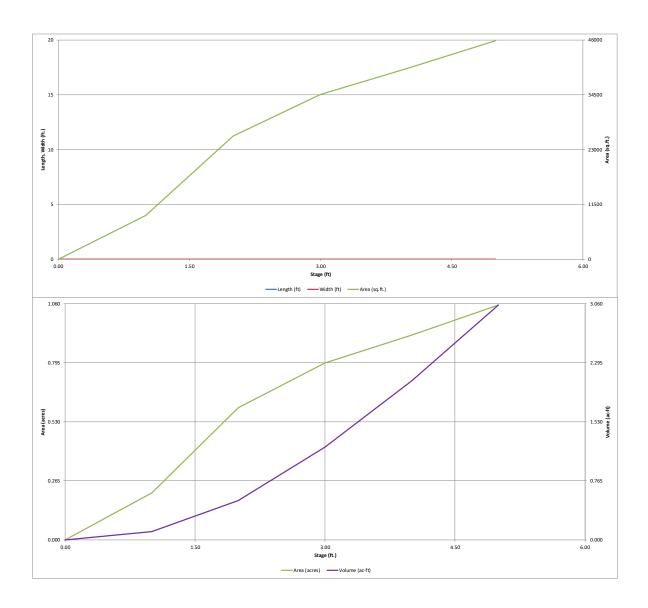
Define Zones and Basin Geometry

Define Zones and Basin Geometry		
Zone 1 Volume (WQCV) =	0.227	acre-feet
Zone 2 Volume (EURV - Zone 1) =	0.210	acre-feet
Zone 3 Volume (100-year - Zones 1 & 2) =	0.849	acre-feet
Total Detention Basin Volume =	1.287	acre-feet
Initial Surcharge Volume (ISV) =	user	ft ³
Initial Surcharge Depth (ISD) =	user	ft
Total Available Detention Depth (H _{total}) =	user	ft
Depth of Trickle Channel (H _{TC}) =	user	ft
Slope of Trickle Channel (S_{TC}) =	user	ft/ft
Slopes of Main Basin Sides (Smain) =	user	H:V
Basin Length-to-Width Ratio (R _{L/W}) =	user	

Initial Surcharge Area $(A_{ISV}) =$	user	ft ²
Surcharge Volume Length $(L_{ISV}) =$	user	ft
Surcharge Volume Width $(W_{ISV}) =$	user	ft
Depth of Basin Floor $(H_{FLOOR}) =$	user	ft
Length of Basin Floor (L_{FLOOR}) =	user	ft
Width of Basin Floor $(W_{FLOOR}) =$	user	ft
Area of Basin Floor $(A_{FLOOR}) =$	user	ft²
Volume of Basin Floor (V _{FLOOR}) =	user	ft ³
Depth of Main Basin $(H_{MAIN}) =$	user	ft
Length of Main Basin $(L_{MAIN}) =$	user	ft
Width of Main Basin $(W_{MAIN}) =$	user	ft
Area of Main Basin $(A_{MAIN}) =$	user	ft ²
Volume of Main Basin $(V_{MAIN}) =$	user	ft ³
Calculated Total Basin Volume (V_{total}) =	user	acre-fee

			1							
	Depth Increment =		ft Optional		I	I	Optional			
	Stage - Storage	Stage (ft)	Override	Length	Width	Area	Override	Area (acre)	Volume	Volume (ac-ft)
442	Description Top of Micropool	(π)	Stage (ft) 0.00	(ft) 	(ft) 	(ft²) 	Area (ft ²)	0.000	(ft ³)	(ac-π)
772			1.00	-		-	9,180	0.211	4,590	0.105
			2.00	-		-	25,856	0.594	22,108	0.508
			3.00	-		-	34,590	0.794	52,331	1.201
			4.00	-		-	40,046	0.919	89,649	2.058
	TOP:7447		5.00	-		-	45,920	1.054	132,632	3.045
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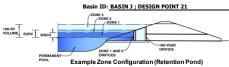
Pond G_PUD, Basin 9/28/2023, 1:24 PM



Pond G_PUD, Basin 9/28/2023, 1:24 PM

MHFD-Detention, Version 4.06 (July 2022)

Project: FLYING HORSE NORTH PUD PRELIMINARY PLAN



Watershed Information

Selected BMP Type =	EDB	
Watershed Area =	15.80	acres
Watershed Length =	1,150	ft
Watershed Length to Centroid =	350	ft
Watershed Slope =	0.040	ft/ft
Watershed Imperviousness =	86.10%	percent
Percentage Hydrologic Soil Group A =	0.0%	percent
Percentage Hydrologic Soil Group B =	100.0%	percent
Percentage Hydrologic Soil Groups C/D =	0.0%	percent
Target WQCV Drain Time =	40.0	hours
Location for 1-hr Rainfall Depths =	User Input	

After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Liban Hydrograph Procedure

the embedded Colorado Urban Hydrograph Procedure.					
Water Quality Capture Volume (WQCV) =	0.487	acre-feet			
Excess Urban Runoff Volume (EURV) =	1.519	acre-feet			
2-yr Runoff Volume (P1 = 1.19 in.) =	1.272	acre-feet			
5-yr Runoff Volume (P1 = 1.5 in.) =	1.665	acre-feet			
10-yr Runoff Volume (P1 = 1.75 in.) =	1.988	acre-feet			
25-yr Runoff Volume (P1 = 2 in.) =	2.332	acre-feet			
50-yr Runoff Volume (P1 = 2.25 in.) =	2.662	acre-feet			
100-yr Runoff Volume (P1 = 2.52 in.) =	3.031	acre-feet			
500-yr Runoff Volume (P1 = 3.14 in.) =	3.854	acre-feet			
Approximate 2-yr Detention Volume =	1.213	acre-feet			
Approximate 5-yr Detention Volume =	1.588	acre-feet			
Approximate 10-yr Detention Volume =	1.955	acre-feet			
Approximate 25-yr Detention Volume =	2.094	acre-feet			
Approximate 50-yr Detention Volume =	2.174	acre-feet			
Approximate 100-yr Detention Volume =	2.270	acre-feet			

Optional User Overrides						
		acre-feet				
		acre-feet				
	1.19	inches				
	1.50	inches				
	1.75	inches				
	2.00	inches				
	2.25	inches				
	2.52	inches				
		inches				

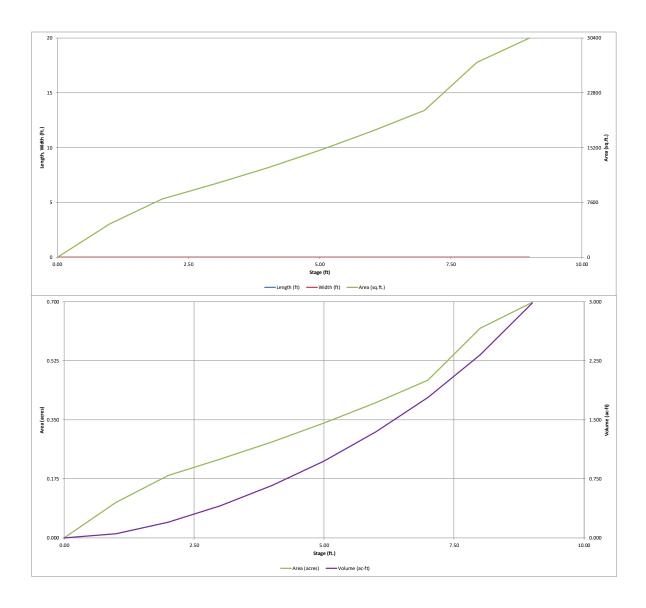
Define Zones and Basin Geometry

0.487	acre-feet
1.031	acre-feet
0.751	acre-feet
2.270	acre-feet
user	ft ³
user	ft
user	ft
user	ft
user	ft/ft
user	H:V
user	
	1.031 0.751 2.270 user user user user user

Initial Surcharge Area $(A_{ISV}) =$	user	ft²
Surcharge Volume Length $(L_{ISV}) =$	user	ft
Surcharge Volume Width $(W_{ISV}) =$	user	ft
Depth of Basin Floor $(H_{FLOOR}) =$	user	ft
Length of Basin Floor (L_{FLOOR}) =	user	ft
Width of Basin Floor $(W_{FLOOR}) =$	user	ft
Area of Basin Floor $(A_{FLOOR}) =$	user	ft ²
Volume of Basin Floor (V _{FLOOR}) =	user	ft ³
Depth of Main Basin (H _{MAIN}) =	user	ft
Length of Main Basin $(L_{MAIN}) =$	user	ft
Width of Main Basin $(W_{MAIN}) =$	user	ft
Area of Main Basin $(A_{MAIN}) =$		ft ²
Volume of Main Basin $(V_{MAIN}) =$	user	ft ³
Calculated Total Basin Volume (V_{total}) =	user	acre-fee

Depth Increment =		ft Optional				Optional			
Stage - Storage	Stage	Override	Length	Width	Area	Override Area (ft ²)	Area	Volume (ft 3)	Volume (ac-ft)
Description Top of Micropool	(ft) 	Stage (ft) 0.00	(ft) 	(ft) 	(ft²)	0	(acre) 0.000	(IL*)	(dC-IL)
83 100 01 1 11 11 10 10 10 11		1.00	_		_	4,576	0.105	2,288	0.053
		2.00	_			8,060	0.185	8,606	0.198
	-	3.00	_	-	-	10,142	0.233	17,707	0.406
	-	4.00	-	-	-	12,370	0.284	28,963	0.665
		5.00	-		-	14,814	0.340	42,555	0.977
		6.00	-		-	17,475	0.401	58,699	1.348
	-	7.00	-		-	20,351	0.467	77,612	1.782
		8.00	-	-	-	27,036	0.621	101,306	2.326
TOP:7592		9.00	-			30,400	0.698	130,024	2.985
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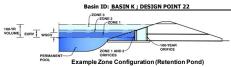
Pond J_PUD, Basin 9/28/2023, 1:25 PM



Pond J_PUD, Basin 9/28/2023, 1:25 PM

MHFD-Detention, Version 4.06 (July 2022)

Project: FLYING HORSE NORTH PUD PRELIMINARY PLAN



Watershed Information

Selected BMP Type =	EDB	
Watershed Area =	18.00	acres
Watershed Length =	1,400	ft
Watershed Length to Centroid =	500	ft
Watershed Slope =	0.060	ft/ft
Watershed Imperviousness =	86.00%	percent
Percentage Hydrologic Soil Group A =	0.0%	percent
Percentage Hydrologic Soil Group B =	100.0%	percent
Percentage Hydrologic Soil Groups C/D =	0.0%	percent
Target WQCV Drain Time =	40.0	hours
Location for 1-hr Rainfall Depths =	User Input	

After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Liban Hydrograph Procedure

the embedded Colorado Urban Hydrograph Procedure.					
Water Quality Capture Volume (WQCV) =	0.554	acre-feet			
Excess Urban Runoff Volume (EURV) =	1.728	acre-feet			
2-yr Runoff Volume (P1 = 1.19 in.) =	1.470	acre-feet			
5-yr Runoff Volume (P1 = 1.5 in.) =	1.925	acre-feet			
10-yr Runoff Volume (P1 = 1.75 in.) =	2.299	acre-feet			
25-yr Runoff Volume (P1 = 2 in.) =	2.697	acre-feet			
50-yr Runoff Volume (P1 = 2.25 in.) =	3.079	acre-feet			
100-yr Runoff Volume (P1 = 2.52 in.) =	3.507	acre-feet			
500-yr Runoff Volume (P1 = 3.14 in.) =	4.460	acre-feet			
Approximate 2-yr Detention Volume =	1.380	acre-feet			
Approximate 5-yr Detention Volume =	1.807	acre-feet			
Approximate 10-yr Detention Volume =	2.225	acre-feet			
Approximate 25-yr Detention Volume =	2.383	acre-feet			
Approximate 50-yr Detention Volume =	2.474	acre-feet			
Approximate 100-yr Detention Volume =	2.584	acre-feet			

Optional User Overrides						
		acre-feet				
		acre-feet				
	1.19	inches				
	1.50	inches				
	1.75	inches				
	2.00	inches				
	2.25	inches				
	2.52	inches				
		inches				

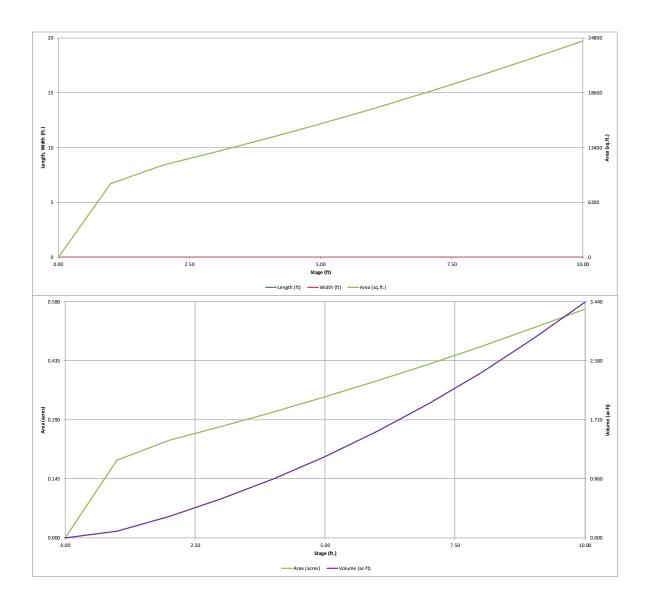
Define Zones and Basin Geometry

Define Zones and Basin Geometry		
Zone 1 Volume (WQCV) =	0.554	acre-feet
Zone 2 Volume (EURV - Zone 1) =	1.174	acre-feet
Zone 3 Volume (100-year - Zones 1 & 2) =	0.856	acre-feet
Total Detention Basin Volume =	2.584	acre-feet
Initial Surcharge Volume (ISV) =	user	ft ³
Initial Surcharge Depth (ISD) =	user	ft
Total Available Detention Depth (H _{total}) =	user	ft
Depth of Trickle Channel (H_{TC}) =	user	ft
Slope of Trickle Channel $(S_{TC}) =$	user	ft/ft
Slopes of Main Basin Sides (Smain) =	user	H:V
Basin Length-to-Width Ratio (R _{L/W}) =	user	

Initial Surcharge Area $(A_{ISV}) =$	user	ft ²
Surcharge Volume Length $(L_{ISV}) =$	user	ft
Surcharge Volume Width $(W_{ISV}) =$	user	ft
Depth of Basin Floor $(H_{FLOOR}) =$	user	ft
Length of Basin Floor (L_{FLOOR}) =	user	ft
Width of Basin Floor $(W_{FLOOR}) =$		ft
Area of Basin Floor $(A_{FLOOR}) =$		ft²
Volume of Basin Floor $(V_{FLOOR}) =$	user	ft ³
Depth of Main Basin (H _{MAIN}) =	user	ft
Length of Main Basin $(L_{MAIN}) =$	user	ft
Width of Main Basin $(W_{MAIN}) =$	user	ft
Area of Main Basin (A _{MAIN}) =	user	ft ²
Volume of Main Basin (V _{MAIN}) =	user	ft 3
Calculated Total Basin Volume (V_{total}) =	user	acre-feet

	Depth Increment =		ft Optional				Optional			
	Stage - Storage Description	Stage (ft)	Override Stage (ft)	Length (ft)	Width (ft)	Area (ft²)	Override Area (ft ²)	Area (acre)	Volume (ft 3)	Volume (ac-ft)
7501	Top of Micropool		0.00	-		-	0	0.000		
			1.00	-		-	8,296	0.190	4,148	0.095
		-	2.00	-		-	10,427	0.239	13,509	0.310
			3.00 4.00	-		-	11,897 13,449	0.273	24,671 37,344	0.566 0.857
			5.00	-		_	15,082	0.346	51,610	1.185
			6.00				16,797	0.386	67,549	1.551
			7.00	-	-	-	18,594	0.427	85,245	1.957
		-	8.00	-		-	20,473	0.470	104,778	2.405
	TOP:7511		9.00 10.00	-		-	22,433 24,475	0.515 0.562	126,231 149,685	2.898 3.436
	10P:/511		10.00	-		-	24,475	0.502	149,000	3.430
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Pond K_PUD, Basin 9/28/2023, 1:26 PM



Pond K_PUD, Basin 9/28/2023, 1:26 PM

			Desig	gn Procedu	ıre Form: I	Runoff Red	luction					
				UD-BMP (Ve	ersion 3.07, Ma	rch 2018)						Sheet 1 of 1
Designer:	DLH										_	
Company:	HR GREEN										_	
Date:											_	
Project:	FLYING HOR	SE NORTH PU)								_	
Location:											-	
SITE INFORMATION (Us	er Input in Bl	ue Cells)										
	WQCV F	Rainfall Depth	0.60	inches								
Depth of Average Ru	unoff Producin	ig Storm, d ₆ =	0.43	inches (for V	/atersheds O	utside of the D	Denver Region	n, Figure 3-1 i	n USDCM Vo	l. 3)		
Area Tuna	LIIA-DDA											
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Runoff (in)	0.00											
Runoff (ft ³)	0											
Runoff Reduction (ft ³)	1667											
CALCIII ATED WOCV P	EQUITE											
1 .												
WQCV Reduction (%)	100%											
Untreated WQCV (ft ³)	0											
CALCUL ATER REGION I	DOINT DECU	I TO (:41- 41	D	Desire Dei	(ID)				
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Designer DLH Company HG SEEN January 15, 2024 Project January 15, 2024 January 16, 2025 January 16, 2025												
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		results from	all columns	_								
	<u> </u>			NC	TE: THE	PRESE	ENTED L	JDBMP (CALCUL	ATIONS	SHOW	N HERE
				RF	PRESE	NT THE	WORST	CASE S	CENAR	IO RUN	OFF	
												RES.
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		•						(LA, A I	OTAL VV	QOV KL	.500110	

Large lot (2.5 acres & greater) SFD are excluded from water quality per exclusion I.7.2XXXX. This exclusion does not include detention requirements. Please identify how increase in flows from the developed areas will be mitigated if not being conveyed to a full spectrum detention ponds

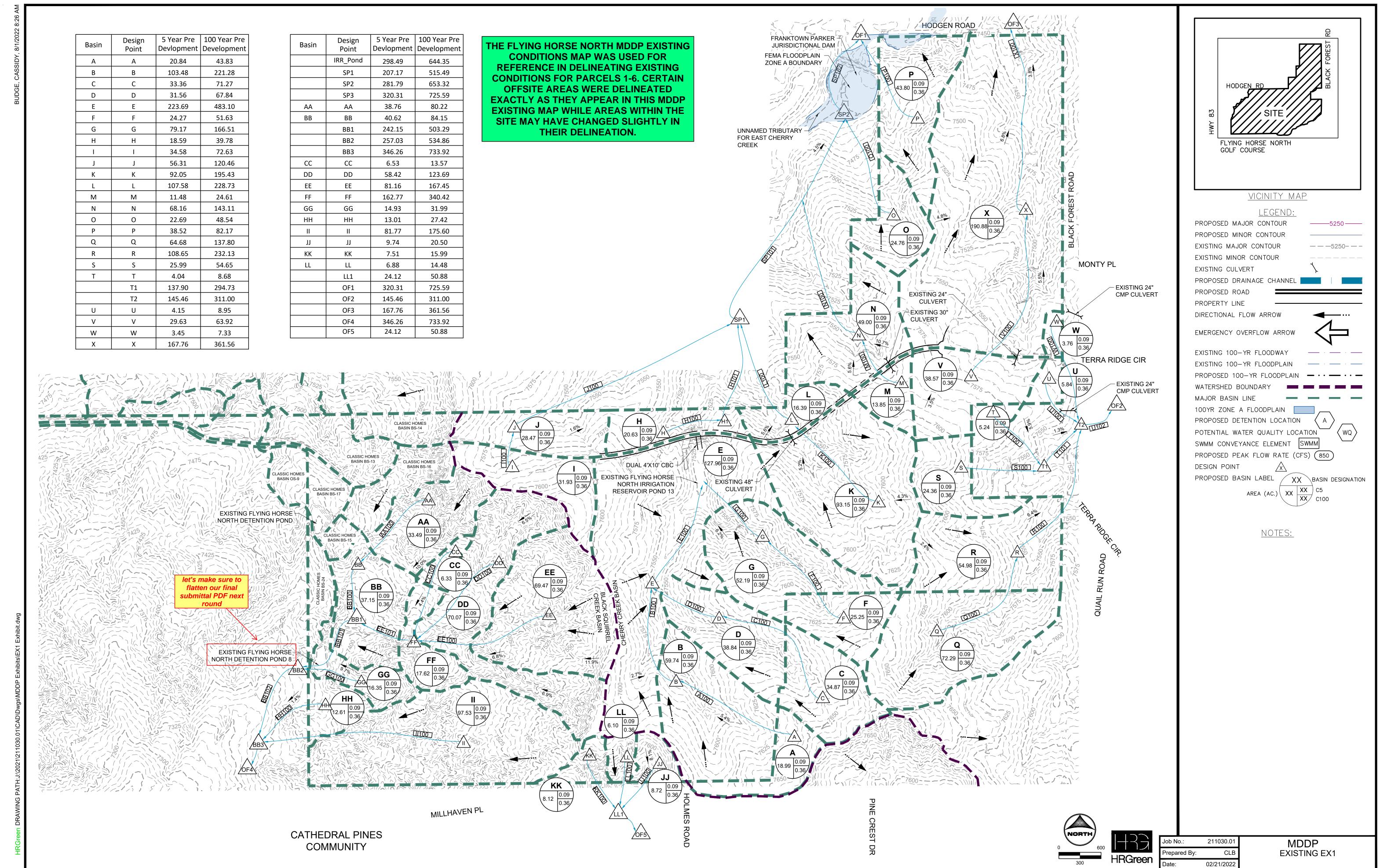
let's get some clarity on this - are they a part of the exclusion if they are assumed at 11% impervious?





Appendix E:

Reference Report Excerpts and Materials





INNOVATIVE DESIGN. CLASSIC RESULTS.

FLYING HORSE NORTH

IRRIGATION RESERVOIR EMBANKMENT

DESIGN REPORT

DAMID: 080459 Construction File No.: C-2085

AUGUST 2018

THIS REPORT WAS **USED FOR REFERENCE** IN THE SWMM **CALCULATIONS AS WELL AS THE CALLOUT OF EXISTING INFRASTRUCTURE IN** THE EX AND PR DRAINAGE MAPS. THE **FOLLOWING PAGES** THAT ARE APART OF THIS DESIGN REPORT WILL HAVE OUTLINES AND HIGHLIGHTED **TEXT THAT WERE** SPECIFICALLY USED **DURING THE** PREPERATION OF THIS PDR.

Prepared for:
PRI #2 LLC
6385 CORPORATE DRIVE SUITE 200
COLORADO SPRINGS CO 80919
(719) 592-9333

Prepared by:
CLASSIC CONSULTING ENGINEERS &
SURVEYORS

619 N. CASCADE AVE SUITE 200 COLORADO SPRINGS CO 80903 (719) 785-0790

> Job no. 1096.11 PCD File No. SF-18-001



*7513.0

*7514.0

*7515.0

7516.0

7517.0

7518.0

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31.88

36.40

41.16

51.42

56.89

62.61

68.57

74.77

87.91

94.89

102.22

109.90

118.00

126.57

3.05

3.26

3.48

4.16

4.40

4.64

4.88

5.36

5.59

5.84

6.08

6.33

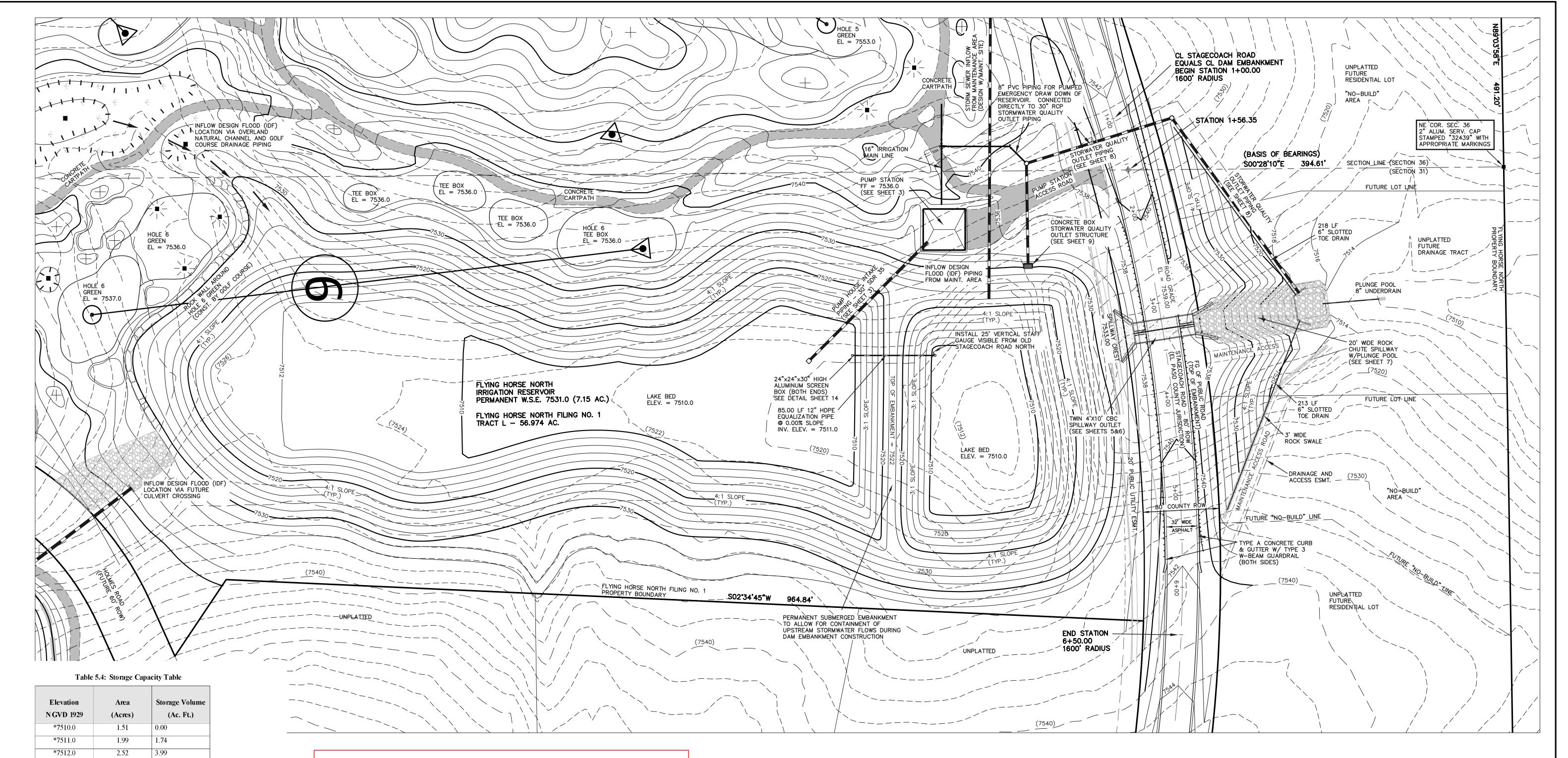
6.57

6.81

7.15

8.37

*Indicates dead storage below pumping ability



T. I. F. F. D	Carlana Table
Table 5.5: Reservoir D	ischarge Labie

	1 abic 3.3. R	servon Discharge Table	•
	Discharge (cfs)	Discharge (cfs)	Discharge (cfs)
Elevation	(SWQ Outlet Box)	(Twin CBC Spillway)	(Total)
7531.0	0.0	0.0	0.0
7532.0	13.89	0.0	13.89
7533.0	27.77	0.0	27.77
7534.0	51.31	49.05	100.36
7535.0	69.52	138.56	208.08
7536.0	74.61	254.72	329.33
D . II	ICT		

PRESERVE ANY AND ALL UNDERGROUND UTILITIES.

Permanent WSE = 7531.0

Top of SWQ Outlet box = 7533.0

Spillway elevation = 7533.0

NOTES:

1. TOPOGRAPHIC BASE MAPPING PRODUCED FROM AERIAL PHOTOGRAPHY PROVIDED BY NORTH AMERICAN MAPPING IN 2009. HORIZONTAL CONTROL IS BASED ON LOCAL CALIBRATION TIED TO SECTION CORNER AND VERTICAL CONTROL IS BASED ON NGVD 1929 DATUM.

2. PERMANENT WSE = 7531.0

3. RESERVOIR LINER INSTALLED UP TO ELEVATION 7534.0

STAFF GAUGE DETAILS:

- 1. 12"X25'X1/2" PVC
- 2. LASER CUT ACRYLIC NUMBERS AND HATCH MARKS LIQUID WELDED TO PVC ON 1 FT. INCREMENTS
- 3. MOUNTED ON ALUMINUM FRAME WITH CROSS BRACKETS ANCHORED INTO SLOPE
- 4. BASE FASTENED TO 12" PIPE
- 5. ELEVATION DISPLAY RANGE: 7512-7535

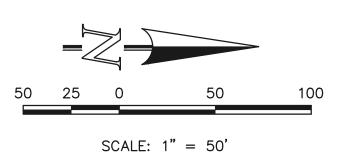


FIGURE 1.3

STATE ENGINEER'S CONSTRUCTION FILE NUMBER: C-2085

48 HOURS BEFORE YOU DIG, CALL UTILITY LOCATORS	NO.	REVISION	DATE
811	1	REVISED PER STATE COMMENTS	5-14-18
UTILITY NOTIFICATION CENTER OF COLORADO	2	REVISED PER COUNTY COMMENTS	7-31-18
IT'S THE LAW			
THE LOCATIONS OF EXISTING UNDERGROUND UTILITIES ARE SHOWN IN AN APPROXIMATE WAY ONLY. THE CONTRACTOR			
SHALL DETERMINE THE EXACT LOCATION OF ALL EXISTING UTILITIES BEFORE COMMENCING WORK. THE CONTRACTOR SHALL			
BE FULLY RESPONSIBLE FOR ANY AND ALL DAMAGES WHICH			
MIGHT BE CAUSED BY HIS FAILURE TO EXACTLY LOCATE AND			

REVIEW: PREPARED UNDER MY DIRECT SUPERVISION FOR AND ON BEHALF OF 7-31-18 CLASSIC CONSULTING ENGINEERS AND SURVEYORS, LLC

MARC A. WHORTON, COLORADO P.E. #37155

CONSULTING **ENGINEERS & SURVEYORS** 619 N. Cascade Avenue, Suite 200 Colorado Springs, Colorado 80903

FLYING HORSE NORTH IRRIGATION RESERVOIR EMBANKMENT SITE LAYOUT WITH GRADING

DAM ID - 080459 DESIGNED BY | MAW | SCALE DATE 1-4-18 MAW | (H) 1"= 50' | SHEET 4 OF 14 DRAWN BY (V) 1"= N/A JOB NO. CHECKED BY

SECTION 4: RESERVOIR AND DAM

4.1 DESIGN CRITERIA

The proposed dam for the Flying Horse North Irrigation Reservoir was designed in accordance with Rule 5 of the State of Colorado Rules and Regulations for Dam Safety and Dam Construction, dated January 2007.

4.2 RESERVOIR

This watershed will contain development of a private golf course (currently under construction) including an outdoor golf maintenance facility, along with 2.5 ac. rural residential lot development accessed by rural County paved roadways. As such, the irrigation reservoir will also be designed with a separate stormwater detention and SWQ component per El Paso County criteria. This separate structure will be in the form of a concrete outlet box with an orifice plate and 30" RCP outlet allowing the release of the smaller storm events to meet the standards as specified per this criteria and the County's MS4 permit with the State. This SWQ release through the 30" RCP will be constructed outside of the reservoir embankment. The specific location of this reservoir is within a portion of Section 36, township 11 south, range 66 west of the sixth principal meridian, and a portion of Section 31 township 11 south, range 65 west of the sixth principal meridian, El Paso County Colorado. (See Figure 1.3)

The reservoir has a surface area at its permanent WSE (Elev. 7531.0) of 7.0 acres with a storage volume of 94.9 acre feet. The maximum depth at this elevation is 21 feet with the lake bed at 7510. The reservoir will have a liner constructed of a flexible membrane. This liner will be laid up to a maximum elevation of 7534. The reservoir is supplied by water from a well located on the Clubhouse site within the development approximately 1/4 mile west of the reservoir. The level in the reservoir is controlled by the two outlet structures. The Detention/SWQ structure will facilitate the State required 72 hr. drain time for the smaller stormwater events and help maintain the permanent water level while the twin box culvert spillway will allow for the County required 100 yr. detention release of the major stormwater events. The total storage capacity table is found in Section 5, Table 5.4.

4.3 DAM EMBANKMENT

The dam embankment for this reservoir will be constructed within the County owned and maintained Old Stagecoach Road (80' ROW - Collector). The subdivision Improvement Agreement (SIA) as required by El



Paso County for this subdivision, will be recorded along with the Final Plat and specify ownership and maintenance responsibilities related to the embankment and associated drainage structures. The crest of the embankment, which will be the finished grade of asphalt for the roadway is at elevation 7539.0 at the lowest point. The regulatory height from the twin box culvert emergency spillway invert to the native channel grade equals 23.0°. The length of the embankment measured from the toe of slopes on each side is approximately 450°. Both the upstream and downstream slopes of the embankment will be constructed at no greater than a 4:1 slope. The roadway will have a typical 2% crown with an asphalt width of 32.0° with El Paso County Type A concrete curb and gutter on both sides and then 6:1 maximum to edge of ROW with a County required clear zone of 14.0°. The twin box culvert emergency spillway structure is outside this clear zone. El Paso County will also require CDOT Type 3 W-Beam guardrail along both sides of the embankment. The embankment itself will be constructed of local material found on-site and tested by the Geotech. According to the State of Colorado Rules and Regulations for Dam Safety and Dam Construction, Rule 4.2.5.4, this facility is considered a "Small Jurisdictional Dam" given the jurisdictional height greater than 20 feet but less than 50 feet and a capacity greater than 100 acre-feet.

4.4 SPILLWAY AND OUTLET WORKS

This facility will be designed with two separate outlet structures. One will facilitate the State/County required detention/SWQ component of the facility while the other will allow for the 100 yr. stormwater event and emergency flow situations. A low level outlet will be built into the pump station design allowing for an emergency drawdown of the reservoir to be with connection to the SWQ outlet piping.

Detention / SWQ Outlet

Per the County's MS4 permit with the State, this development is required to provide detention and stormwater quality within this reservoir facility. The design for this is being handled by a separate concrete outlet box constructed outside the formal dam embankment. This structure is a 4'x8' concrete box with a steel flow control plate and protective well screen located on the front. The control plate is designed with three rectangular holes to facilitate the State required drain times. The first hole is located at elevation 7531.0 with the top of box at elevation 7533.0. The top of box will be constructed with a grate to allow flows to enter the box as well. A 30" RCP outlet pipe will allow for the release of all the flows entering the box structure. The design of this structure meets all State and County requirements for both EURV and



WQCV. The 30" RCP outlet piping will be routed around the dam embankment and into the rock chute and plunge pool at the base of the emergency spillway.

Spillway Outlet

Given that the embankment for this reservoir will be a County roadway, the conventional emergency spillway channel design at the crest of the embankment was not appropriate. But rather a concrete box culvert spillway design under the roadway to allow for both the major stormwater events and emergency release has been employed. Twin 4'x10' concrete box culverts (CBC) will facilitate the required releases. The crest of the spillway will be constructed at elevation 7533.0 where the release will then travel under the roadway and into a 20' wide rock chute. The rock chute will have a 4:1 slope with 3:1 side slopes and a total drop of 18.0' into a 2.0' deep plunge pool. The following roughness coefficients were used: CBCs 0.013 and Rock Chute 0.035. The rip-rap thickness will be 56" with a gradation specified by the Geotech. (See Design Plans) The spillway CBCs and Rock Chute have been designed to accommodate both the 100 yr. release of 182 cfs with a headwater depth ratio (Hw/D) of 0.54 and the total basin inflow of 609 cfs with a (Hw/D) of 1.31. This design is within the maximum County criteria of (Hw/D) of 1.40. The freeboard design is as follows: 100 Yr. = 4.39' and 500 Yr. = 3.03'. The velocity at inlet of chute = 15.6 fps and velocity at outlet of chute = 6.99 fps, both at normal depth. 1.76' of Freeboard is included in chute design.

Low Level Outlet

This reservoir will not be designed with a formal low level outlet given the nature of the facility and the ability for the pump station to facilitate the draining of the reservoir for embankment inspection or emergency purposes. Thus, directly off of the 16" irrigation main just outside the pump station, a 16"x8" tee with gate valves and a 8" drain line will be installed to allow for the pumped release and draining of the reservoir. This 8" drain line will then connect directly to the 30" RCP storm system via a Type II concrete storm manhole constructed as a part of the release of the Detention/SWQ component as required by El Paso County. This 30" storm system then daylights into the base of the rock chute and plunge pool on the backside of the embankment. The 8" drain line @ 110 psi is expected to release 800-1200 GPM. However, using the maximum pump station capacity of 2,250 GPM while opening system drain valves and irrigation heads, the drain time is as follows: As mentioned earlier, the pumps will allow for release down to an elevation of 7515.67. Based on the permanent WSE of 7531, this equates to a total of approximately 26 million gallons (MG) to be drained. The total drain time is estimated at approximately 8 days.



Hazard Classification" as described in section 5.6 of this report the Inflow Design Flood Requirements (IDF) as found in Rule 5.9.1, Table 5.1 utilize the (NOAA 14 – 24 Hr. duration) 100 Yr. storm event. The UD-Detention v3.07 spreadsheet (Per Urban Drainage Vol. 3) will also be utilized in the final design of the Detention and SWQ aspects of this facility. This spreadsheet uses 1 Hr. precipitation depths. See Table 5.1 for precipitation depth comparison. Please note that the higher precipitation amounts have been used for each return period.

Table 5.1: Precipitation Depth Comparison

Return Period	1-Hr. Depth (City/County)	1-Hr. Depth (NOAA 14)	24-Hr. Depth (City/County)	24-Hr. Depth (NOAA 14)
2	1.19	0.92	2.10	1.93
5	1.50	1.20	2.70	2.44
50	2.25	2.15	4.20	4.33
100	2.52	2.49	4.60	5.04

5.2 WATER RIGHTS

Based on the water decree filed October 6, 2017 (See Appendix), PRI #2, LLC has the water rights to pump and store in the on-site Flying Horse North reservoir. PRI #2, LLC has a lease from the State Land Board for the following water rights: 515 AF in the Dawson, 577 AF in the Denver, 239 AF in the Arapahoe and 182 AF in the Laramie Fox Hills. The Arapahoe and Laramie Fox Hills are both deemed non-tributary reservoirs. The Flying Horse North Golf Course will take an average of 200 AF per year from their Arapahoe well that will be pumped into the reservoir. Evaporative loss is not an issue when pumping from a non-tributary source. Upon termination of the State Land Board Lease in 2048, all water rights revert automatically back to PRI #2, LLC who will own them in perpetuity.



5.3 WATERSHED CHARACTERISTICS

The watershed of the irrigation reservoir includes a total area of 366.8 acres within the East Cherry Creek drainage basin and just north of the Palmer Divide. A portion of this area is outside the Flying Horse North development as shown in basins OS-12, OS-13 and OS-14. These basins are both currently undeveloped and developed as County zoned RR-5 (5 ac. rural residential). All the on-site basins are zoned PUD for either 2.5 ac. rural residential or golf course/open space. (See Tables 5.2 and 5.3 for sub-basin CN values and associated Tc times) Nearly the entire watershed is outside of the black forest tree line and mainly consists of prairie grasses with grades ranging from 2%-20% with three major natural ravines that drain in a northwesterly direction directly towards the planned irrigation reservoir. The golf course layout aides in the natural conveyance of the majority of the stormwater flows to the reservoir. The storage capacity table for the reservoir is listed in Table 5.4.

	ALL	LAND ASSUN	MED 2 ACRE RES	IDENTIAL LOTS	S OR	
GOOD	CONDITION OP	EN SPACE (L	AWNS, PARKS (OLF COURSE	S, CEMETARIES	ETC.)
	Cn '	VALUES	- DEVELOP	ED COND	ITIONS	
BASIN	BASIN	GOLF (COURSE (B)	2 AC. RES	SIDENTIAL (B)	COMPOSI
(label)	AREA			1 1		C _N
,	(Ac)	CN	AREA	CN	AREA	
	,		(Ac.)		(Ac.)	
CC-1	22.3	61	0.0	65	22.3	65.0
CC-2	36.4	61	0.0	65	36.4	65.0
CC-3	51.9	61	19.1	65	32.8	63.5
CC-4A	108.2	61	63.2	65	45.0	62.7
CC-4B	17.0	61	5.5	65	11.5	63.7
OS-12	67.7	61	0.0	65	67.7	65.0
OS-13	36.9	61	0.0	65	36.9	65.0
OS-14	26.4	61	0.0	65	26.4	65.0



Table 5.3: Sub-basin Time of Concentration

			TIME	OF CONC	ENTRATIO	ON DEVE	LOPED			
	COMPOSITE		OVERLAND		STREET / C	CHANNEL FL	OW(DCM Vo	l. 1 Fig. 6-25)	Tc	Tc
BASIN	Cn	Length	Height	Tc	Length	Slope	Velocity	Tc	TOTAL	LAG (0.6tc)
		(ft)	(ft)	(hr)	(ft)	(%)	(fps)	(hr)	(hr)	(hr)
CC-1	65.0	300	10	0.40	900	2.0%	1.8	0.14	0.53	0.32
CC-2	65.0	300	10	0.40	1700	2.0%	1.8	0.26	0.66	0.39
CC-3	63.5	300	14	0.35	900	2.5%	2.4	0.10	0.45	0.27
CC-4A	62.7	300	14	0.35	2900	2.0%	2.1	0.38	0.73	0.44
CC-4B	63.7	300	12	0.37	900	3.0%	2.5	0.10	0.47	0.28
OS-12	65.0	300	14	0.35	1500	3.0%	2.5	0.17	0.51	0.31
OS-13	65.0	300	16	0.33	900	3.0%	2.5	0.10	0.43	0.26
OS-14	65.0	300	14	0.35	600	3.5%	2.7	0.06	0.41	0.24

Table 5.4: Storage Capacity Table

Elevation NGVD 1929	Area (Acres)	Storage Volume (Ac. Ft.)
*7510.0	1.51	0.00
*7511.0	1.99	1.74
*7512.0	2.52	3.99
*7513.0	2.85	6.68
*7514.0	3.05	9.63
*7515.0	3.26	12.78
7516.0	3.48	16.15
7517.0	3.70	19.74
7518.0	3.93	23.56
7519.0	4.16	27.60
7520.0	4.40	31.88
7521.0	4.64	36.40
7522.0	4.88	41.16



7523.0	5.14	46.17
7524.0	5.36	51.42
7525.0	5.59	56.89
7526.0	5.84	62.61
7527.0	6.08	68.57
7528.0	6.33	74.77
7529.0	6.57	81.22
7530.0	6.81	87.91
7531.0	7.15	94.89
7532.0	7.52	102.22
7533.0	7.83	109.90
7534.0	8.37	118.00
7535.0	8.77	126.57
7536.0	9.17	135.53

^{*}Indicates dead storage below pumping ability

5.4 HYDROLOGIC MODEL

The PondPack model produced peak discharges for the 2-yr, 5-yr, 50-yr and 100-yr storm events assuming a permanent pool elevation of 7531.0. Reference Appendix B for specific hydrologic model results. Table 5.5 below shows the results of these storm events upon the irrigation reservoir.

Table 5.5: Inflow Design Flood (IDF) Summary Table

			Total
Storm Event	Peak Inflow	Max. WSE	Discharge
	(cfs)	(ft.)	(cfs)
2-yr (City/County)	48	7531.40	6
5-yr (City/County)	119	7531.87	12
50-yr (NOAA 14)	431	7533.58	64
100-yr (NOAA 14)	609	7534.23	124



5.5 HYDRAULIC MODEL

Both the SWQ Outlet and the CBC Spillway were modeled using both PondPack (24-hr. precipitation) and the Urban Drainage UD Detention Spreadsheet (1-hr precipitation) as required by County design criteria. Table 5.6 below shows the results of the PondPack model. Reference Appendix B for the UD Detention – Retention Pond Spreadsheet results. As this facility is required to meet both detention and SWQ criteria, the following is applicable to these design components:

Required WQCV = 1.36 ac-ft. Provided WQCV = 15.01 ac-ft. Required EURV = 2.83 ac-ft. Provided EURV = 15.01 ac-ft. Required 100-yr. = 12.42 ac-ft. Provided 100-yr = 27.35 ac-ft.

Table 5.6: Reservoir Discharge Table

	Discharge (cfs)	Discharge (cfs)	Discharge (cfs)
Elevation	(SWQ Outlet Box)	(Twin CBC Spillway)	(Total)
7531.0	0.0	0.0	0.0
7532.0	13.89	0.0	13.89
7533.0	27.77	0.0	27.77
7534.0	51.31	49.05	100.36
7535.0	69.52	138.56	208.08
7536.0	74.61	254.72	329.33

Permanent WSE = 7531.0

Top of SWQ Outlet box = 7533.0

Spillway elevation = 7533.0

The twin 4'x10' CBC Spillway design has the following results:

100-yr storm release = 182 cfs Hw/D = 0.54

Emergency release – Max. basin IDF = 609 cfs Hw/D = 1.31

County Criteria (max.) Hw/D = 1.40



DETENTION BASIN STAGE-STORAGE TABLE BUILDER

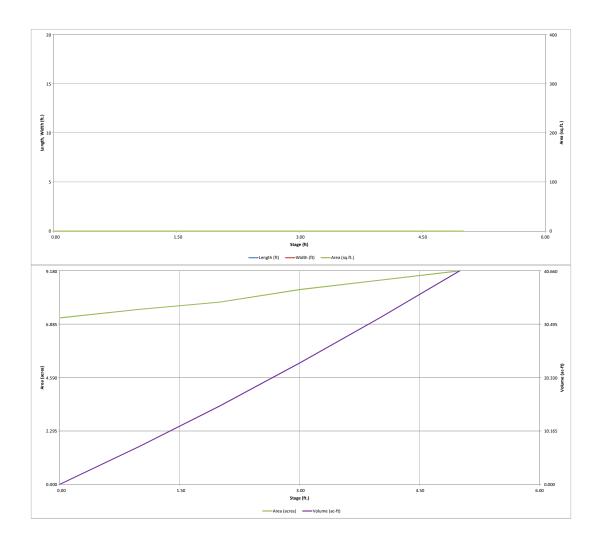
UD-Detention, Version 3.07 (February 2017)

Project: Flying Hors	e North	UD-L	Detention, Version 3	3.07 (Febru	ary 2017)							
Basin ID: Golf Cours		eservoir (Pond - 13)										
ZONE 2 ZONE 1												
STATE CAMP T WOODY	L											
	100-19	40			1							
PERMANENT DIRECTS	DANK	4	Depth Increment =	0.5	ft Optional				Optional			
Example Zone Configurat	ion (Retenti	on Pond)	Stage - Storage	Stage	Override Stone (ft)	Length	Width	Area (ft^2)	Override Area (ft^2)	Area (acre)	Volume (ft^3)	Volume
Required Volume Calculation			Description Permanent Pool	(ft) 	0.00	(ft) 	(ft) 	(ft°2)	311,545	(acre) 7.152	(II:3)	(ac-ft)
Selected BMP Type = RP			7532	_	1.00	-	-	_	327,571	7.520	316,283	7.261
Watershed Area = 366.80	acres		7533	-	2.00	-	-	-	341,084	7.830	650,475	14.933
Watershed Length = 5,175	ft		7534	-	3.00	-	-	-	364,597	8.370	1,006,726	23.111
Watershed Slope = 0.015	ft/ft		7535	-	4.00	-	-	-	382,021	8.770	1,380,035	31.681
Watershed Imperviousness = 8.30%	percent		7536	-	5.00	-	-		399,445	9.170	1,770,768	40.651
Percentage Hydrologic Soil Group A = 0.0%	percent			-								
Percentage Hydrologic Soil Group B = 100.0%	percent			-		-		-				
Percentage Hydrologic Soil Groups C/D = 0.0%	percent					-	-	-				
Desired WQCV Drain Time = 12.0 Location for 1-hr Rainfall Depths = User Input	hours			-			-	-				
Water Quality Capture Volume (WQCV) = 1.395	acre-feet	Optional User Override						-				
Excess Urban Runoff Volume (EURV) = 2.819	acre-feet	1-hr Precipitation		-			-	-				
2-yr Runoff Volume (P1 = 1.19 in.) = 1.903	acre-feet	1.19 inches		-				-				
5-yr Runoff Volume (P1 = 1.5 in.) = 3.006	acre-feet	1.50 inches		-		-	-	-				
10-yr Runoff Volume (P1 = 1.75 in.) = 7.525	acre-feet	1.75 inches		-				-				
25-yr Runoff Volume (P1 = 2 in.) = 21.442	acre-feet	2.00 inches		-				-				
50-yr Runoff Volume (P1 = 2.25 in.) = 30.109	acre-feet	2.25 inches										
100-yr Runoff Volume (P1 = 2.52 in.) = 41.427	acre-feet	2.52 inches		-			-	-			-	\vdash
500-yr Runoff Volume (P1 = 3.39 in.) = 68.375 Approximate 2-yr Detention Volume = 1.765	acre-feet acre-feet	3.39 inches		-			-	-			-	
Approximate 2-yr Detention Volume = 1.765 Approximate 5-yr Detention Volume = 2.813	acre-feet			-			-	-				
Approximate 3-yr Detention Volume = 2.313 Approximate 10-yr Detention Volume = 6.361	acre-feet			-			-	-				
Approximate 25-yr Detention Volume = 9.142	acre-feet			-				-				
Approximate 50-yr Detention Volume = 9.507	acre-feet			-				-				
Approximate 100-yr Detention Volume = 12.417	acre-feet			-				-				
				-		-	-				_	
Stage-Storage Calculation	_			-		-	-	-				
Zone 1 Volume (WQCV) = 1.395 Zone 2 Volume (EURV - Zone 1) = 1.424	acre-feet			-		-	-	-				
Zone 2 Volume (EURV - Zone 1) = 1.424 Zone 3 Volume (100-year - Zones 1 & 2) = 9.598	acre-feet			-		-	-	-				
Total Detention Basin Volume = 12.417	acre-feet acre-feet			_		_	_	-				
Initial Surcharge Volume (ISV) = N/A	ft^3			-		-	-	-				
Initial Surcharge Depth (ISD) = N/A	ft			-		-	-	-				
Total Available Detention Depth (H _{total}) = user	ft			-		-	-	-				
Depth of Trickle Channel (H _{TC}) = N/A	ft					-	-	-				
Slope of Trickle Channel (S _{TC}) = N/A	ft/ft			-		-	-	-				
Slopes of Main Basin Sides (S _{main}) = user Basin Length-to-Width Ratio (R _{I/W}) = user	H:V			-		-	-	-				
Basin Length-to-Width Ratio (R _{L/W}) = user				-		-	-	-				
Initial Surcharge Area (A _{SV}) = user	ft^2			-		-	-	-				
Surcharge Volume Length (L _{ISV}) = user	ft			-		-	-	-				
Surcharge Volume Width (W _{ISV}) = user	ft			-		-	-	-				
Depth of Basin Floor (H _{FLOOR}) = user	ft			-		-	-					
Length of Basin Floor (L _{ROOR}) = user Width of Basin Floor (W _{ROOR}) = user	ft			-		-	-	-				
Width of Basin Floor (W _{FLOOR}) = user Area of Basin Floor (A _{FLOOR}) = user	- ft						-					
Volume of Basin Floor (V _{FLOOR}) = user	ft^2 ft^3			-		-	-	-				
Depth of Main Basin (H _{MAIN}) = user	ft.			-		-	-	-				
Length of Main Basin (L _{MAIN}) = user	ft					-	-	-				
Width of Main Basin (W _{MAIN}) = user	ft					-	-					
Area of Main Basin (A _{MAIN}) = user	ft^2			-		-	-	-				
Volume of Main Basin (V _{MAIN}) = user Calculated Total Basin Volume (V _{total}) = user	ft^3			-		-	-	-				
Calculated Lotal Dasin Volume (V _{total}) = user	acre-feet			<u> </u>			-	-				
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UD-Detention_v3.07 JD POND rev.xtem, Basin 8202018, 9:00 AM

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

UD-Detention, Version 3.07 (February 2017)

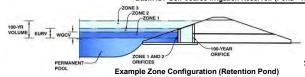


UD-Detention_v3.07 JD POND rev.xtem, Basin 8202018, 9:00 AM

UD-Detention, Version 3.07 (February 2017)

Project: Flying Horse North

Basin ID: Golf Course Irrigation Reservoir (Pond - 13)



	Stage (ft)	Zone Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	0.20	1.395	Orifice Plate
Zone 2 (EURV)	0.40	1.424	Orifice Plate
one 3 (100-year)	1.67	9.598	Weir&Pipe (Restrict)
		12.417	Total

Ve

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth = N/A ft (distance below the filtration media surface)
Underdrain Orifice Diameter = N/A inches

Calculate	ed Parameters for Un	derdrain
Underdrain Orifice Area =	N/A	ft ²
Underdrain Orifice Centroid =	N/A	feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice =	0.00	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Orifice Plate =	2.00	ft (relative to basin bottom at Stage = 0 ft)
Orifice Plate: Orifice Vertical Spacing =	8.00	inches
Orifice Plate: Orifice Area per Row =	195.00	sq. inches (use rectangular openings)

Calcu	lated Parameters for	Plate
VQ Orifice Area per Row =	1.354E+00	ft ²
Elliptical Half-Width =		feet
Elliptical Slot Centroid =	N/A	feet
Elliptical Slot Area =		ft ²

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

ila Total Alca of Lacil Office	itow (nambered noi	ii lowest to inglicat						
	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	0.70	1.40					
Orifice Area (sq. inches)	195.00	195.00	195.00					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

	Not Selected	Not Selected				
Invert of Vertical Orifice =	N/A	N/A	ft (relative to basin bottom at Stage = 0 ft)			
Depth at top of Zone using Vertical Orifice =	N/A	N/A	ft (relative to basin bottom at Stage = 0 ft)			
Vertical Orifice Diameter =	N/A	N/A	inches			

Calculated Parameters for Vertical Orifice				
	Not Selected	Not Selected]	
Vertical Orifice Area =	N/A	N/A	ft ²	
ertical Orifice Centroid =	N/A	N/A	feet	

User Input: Overflow Weir (Dropbox) and Grate (Flat or Sloped)

	Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	2.00	N/A	ft (relative to basin bottom at Stage = 0 ft)
Overflow Weir Front Edge Length =	8.00	N/A	feet
Overflow Weir Slope =	4.00	N/A	H:V (enter zero for flat grate)
Horiz. Length of Weir Sides =	4.00	N/A	feet
Overflow Grate Open Area % =	75%	N/A	%, grate open area/total area
Debris Clogging % =	50%	N/A	%

Calculated Parameters for Overflow Weir			
	Zone 3 Weir	Not Selected	
Height of Grate Upper Edge, H_t =	3.00	N/A	feet
Over Flow Weir Slope Length =	4.12	N/A	feet
Grate Open Area / 100-yr Orifice Area =	5.04	N/A	should be >
Overflow Grate Open Area w/o Debris =	24.74	N/A	ft ²
Overflow Grate Open Area w/ Debris =	12.37	N/A	ft ²
		•	-

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

		,	
	Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	4.00	N/A	ft (distance below basin bottom at Stage = 0 ft)
Outlet Pipe Diameter =	30.00	N/A	inches
Restrictor Plate Height Above Pipe Invert =	30.00		inches Half-Cent

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate

Zone 3 Restrictor Not Selected

Que = 0 ft) Outlet Orifice Area = 4.91 N/A ft²

Outlet Orifice Centroid = 1.25 N/A feet

Half-Central Angle of Restrictor Plate on Pipe = 3.14 N/A radians

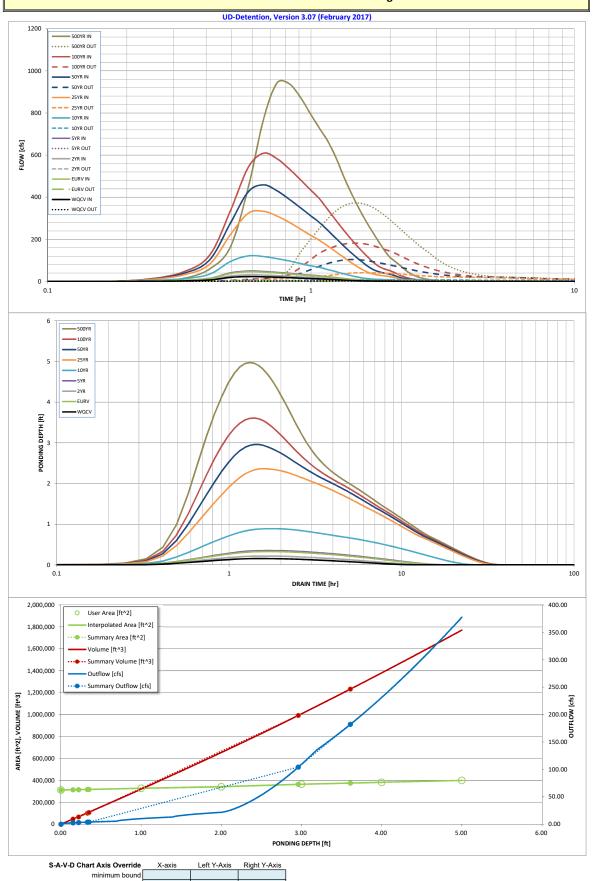
User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage=	2.00	ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length =	20.00	feet
Spillway End Slopes =	0.00	H:V
Freeboard above Max Water Surface =	1.00	feet

Calcula	ted Parameters for S	pillway
Spillway Design Flow Depth=	4.13	feet
Stage at Top of Freeboard =	7.13	feet
Basin Area at Top of Freeboard =	9.17	acres

Routed Hydrograph Results

,,									
Design Storm Return Period =	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
One-Hour Rainfall Depth (in) =	0.53	1.07	1.19	1.50	1.75	2.00	2.25	2.52	3.39
Calculated Runoff Volume (acre-ft) =	1.395	2.819	1.903	3.006	7.525	21.442	30.109	41.427	68.375
OPTIONAL Override Runoff Volume (acre-ft) =									
Inflow Hydrograph Volume (acre-ft) =	1.395	2.819	1.902	3.006	7.522	21.445	30.113	41.428	68.385
Predevelopment Unit Peak Flow, q (cfs/acre) =	0.00	0.00	0.01	0.02	0.20	0.67	0.93	1.25	2.00
Predevelopment Peak Q (cfs) =	0.0	0.0	4.5	7.8	75.1	247.4	342.3	460.1	734.0
Peak Inflow Q (cfs) =	23.2	46.4	31.5	49.5	121.4	333.1	458.5	608.8	941.9
Peak Outflow Q (cfs) =	2.6	3.7	3.0	3.9	9.0	41.5	103.9	182.0	373.2
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	0.5	0.1	0.2	0.3	0.4	0.5
Structure Controlling Flow =	Plate	Plate	Plate	Plate	Plate	Spillway	Spillway	Spillway	Spillway
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	N/A	N/A	0.1	0.7	1.1	1.0
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	11	15	12	15	22	27	27	25	23
Time to Drain 99% of Inflow Volume (hours) =	12	16	14	16	24	31	31	30	29
Maximum Ponding Depth (ft) =	0.15	0.33	0.22	0.35	0.89	2.36	2.96	3.61	4.97
Area at Maximum Ponding Depth (acres) =	7.21	7.27	7.23	7.28	7.48	8.02	8.34	8.61	9.16
Maximum Volume Stored (acre-ft) =	1.077	2.308	1.510	2.453	6.436	17.865	22.693	28.205	40.376
ц									



maximum bound

Outflow Hydrograph Workbook Filename:

Storm Inflow Hydrographs

UD-Detention, Version 3.07 (February 2017)

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

1								ed in a separate		
	SOURCE	WORKBOOK	WORKBOOK	WORKBOOK	WORKBOOK	WORKBOOK	WORKBOOK	WORKBOOK	WORKBOOK	WORKBOOK
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
4.95 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:04:57	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Hydrograph	0:09:54	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Constant	0:14:51	1.01	1.97	1.36	2.10	4.69	9.77	11.39	12.89	15.10
1.010	0:19:48	2.74	5.42	3.70	5.77	13.49	31.71	39.07	46.76	59.45
	0:24:45	7.04	13.91	9.51	14.80	34.64	82.12	102.73	124.75	164.90
	0:29:42	19.32	38.17	26.10	40.61	94.81	223.20	277.98	336.63	444.01
	0:34:39	23.19	46.42	31.50	49.46	121.39	323.47	425.12	541.27	768.07
	0:39:36 0:44:33	22.19	44.52	30.16	47.44	118.28	333.14	458.54	608.77	941.94
	0:49:30	20.20 18.10	40.51 36.44	27.45 24.64	43.17 38.84	108.29 97.66	310.79 281.42	431.04 390.98	582.87 535.69	939.56 878.35
	0:54:27	15.70	31.77	21.42	33.89	85.81	250.82	352.31	485.61	800.60
	0:59:24	13.65	27.68	18.60	29.53	75.09	221.36	315.01	438.24	731.15
	1:04:21	12.38	25.04	16.87	26.71	67.46	196.13	281.72	395.12	668.65
	1:09:18	10.29	20.92	14.06	22.33	56.98	169.57	244.05	343.20	594.66
	1:14:15	8.46	17.30	11.59	18.47	47.35	142.96	207.70	294.13	509.61
	1:19:12	6.60	13.63	9.08	14.56	37.87	117.65	173.58	249.28	435.39
	1:24:09	4.99	10.46	6.92	11.19	29.48	94.26	142.59	208.99	372.25
	1:29:06	3.64	7.75	5.08	8.30	22.24	74.08	115.60	173.54	316.50
	1:34:03	2.78	5.85	3.86	6.26	16.51	56.37	91.58	142.20	268.83
	1:39:00	2.28	4.73	3.14	5.06	13.16	42.77	70.68	113.81	225.24
	1:43:57	1.92	3.99	2.65	4.26	11.04	34.92	55.08	89.03	185.28
	1:48:54	1.68	3.48	2.32	3.72	9.57	29.75	45.79	70.94	149.07
	1:53:51 1:58:48	1.51	3.12	2.08	3.33	8.53	26.20	39.69	59.85	118.87
	2:03:45	1.39	2.86	1.91	3.05	7.79 5.92	23.63 18.97	35.39	52.61 43.64	99.74 83.33
	2:08:42	0.75	2.12 1.54	1.41	2.26 1.64	4.27	13.83	28.99 21.64	33.32	65.70
	2:13:39	0.75	1.13	0.76	1.21	3.17	10.12	15.73	24.54	49.44
	2:18:36	0.41	0.84	0.56	0.90	2.35	7.55	11.63	18.13	37.08
	2:23:33	0.29	0.61	0.41	0.66	1.73	5.63	8.83	13.58	27.60
	2:28:30	0.21	0.44	0.29	0.47	1.25	4.16	6.61	10.30	20.70
	2:33:27	0.15	0.32	0.21	0.34	0.91	3.03	4.92	7.75	15.78
	2:38:24	0.10	0.22	0.14	0.24	0.64	2.25	3.67	5.84	11.98
	2:43:21	0.06	0.14	0.09	0.15	0.42	1.58	2.71	4.47	9.20
	2:48:18	0.03	0.08	0.05	0.08	0.25	1.03	1.90	3.30	7.18
	2:53:15	0.01	0.03	0.02	0.04	0.12	0.60	1.23	2.30	5.41
	2:58:12	0.00	0.01	0.00	0.01	0.04	0.28	0.71	1.49	3.89
	3:03:09	0.00	0.00	0.00	0.00	0.00	0.08	0.33	0.85	2.62
	3:08:06	0.00	0.00	0.00	0.00	0.00	0.00	0.09	0.39	1.60
	3:13:03 3:18:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.11	0.83
	3:22:57	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.30
	3:27:54	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:32:51	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:37:48	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:42:45	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:47:42	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:52:39	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:57:36	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:02:33	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:07:30	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:12:27 4:17:24	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:17:24	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:27:18	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:32:15	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:37:12	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:42:09 4:47:06	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:47:06	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:57:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:01:57	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:06:54	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:11:51 5:16:48	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:16:48	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:26:42	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:31:39	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:36:36	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:41:33	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:46:30	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:51:27 5:56:24	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5.50.24	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

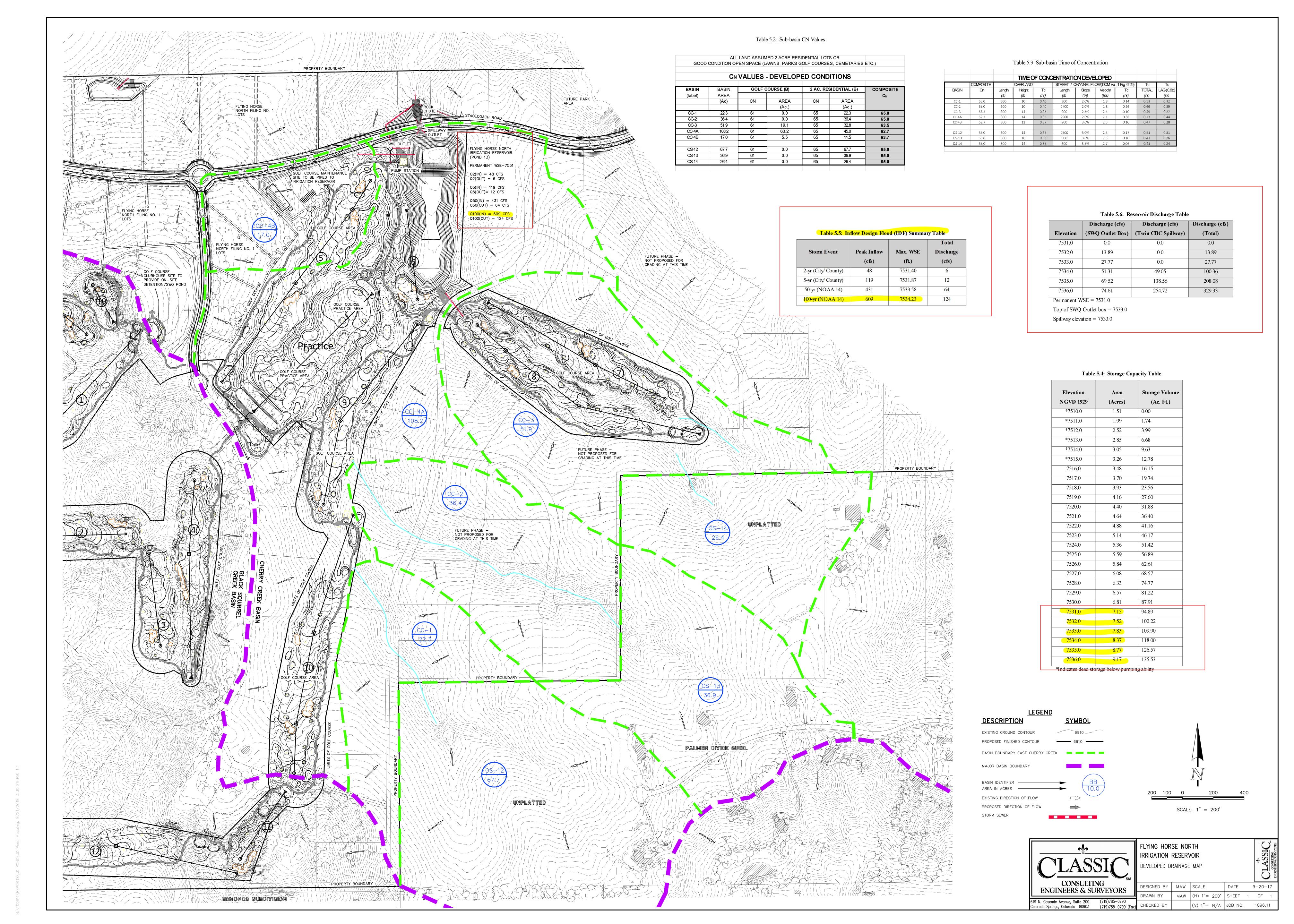
UD-Detention, Version 3.07 (February 2017)

Summary Stage-Area-Volume-Discharge Relationships

The user can create a summary S-A-V-D by entering the desired stage increments and the remainder of the table will populate automatically.

The user should graphically compare the summary S-A-V-D table to the full S-A-V-D table in the chart to confirm it captures all key transition points.

	Stage	Area	Area	Volume	Volume	Total] '
Stage - Storage Description						Outflow	
·	[ft]	[ft^2]	[acres]	[ft^3]	[ac-ft]	[cfs]	
PERMANENT WSE	0.00	311,545	7.152	0	0.000	0.00	For best results, include the
WQCV	0.15	313,949	7.207	46,912	1.077	2.53	stages of all grade slope
2 YR. WSE	0.22	314,910	7.229	65,778	1.510	2.99	changes (e.g. ISV and Floor) from the S-A-V table on
EURV	0.33	316,673	7.270	100,515	2.308	3.69	Sheet 'Basin'.
5 YR. WSE	0.35	316,994	7.277	106,852	2.453	3.80	
50 YR. WSE	2.96	363,656	8.348	992,161	22.777	104.11	Also include the inverts of all
100 YR. WSE	3.61	375,226	8.614	1,232,372	28.291	182.18	outlets (e.g. vertical orifice,
							overflow grate, and spillway,
							where applicable).
							1
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						-	1
						1	†
]
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						-	1
						1	-
		l	l	l	l	1	J







Flying Horse North Filing No. 3 Final Drainage Report

July 27, 2023

Prepared For:

Mr. Drew Balsick

Vice President / Project Manager

Flying Horse Development, LLC 2138 Flying Horse Club Drive

Colorado Springs, CO 80921

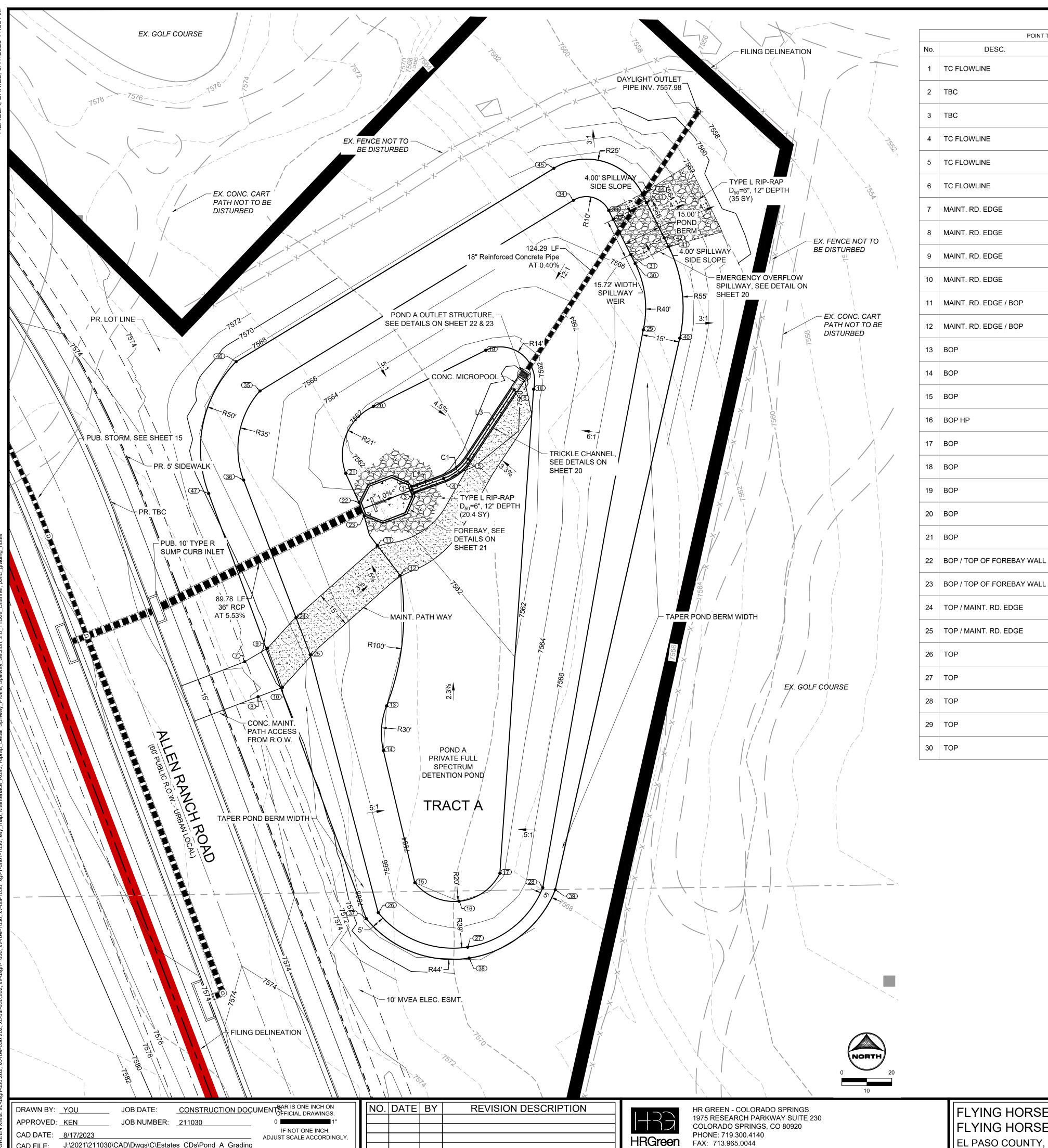
(719) 785-3237

Prepared By:

HR Green Development, LLC
Contact: Richie Lyon, PE
Richie.Lyon@hrgreen.com
719-318-0871

PCD File No. SF-XXXX

THE FLYING HORSE **FILING NO. 3 FDR CONTAINS A SECTION** OF ALLEN RANCH ROAD **AS WELL AS A DETENTION POND THAT** ARE TO BE USED IN THE **CAPTURE AND DETENTION OF BASINS EX5.1 AND M, EXISTING** AND PROPOSED, **LOCATED WITHIN** PARCEL NO. 2 OF THIS PDR. THE FDR HAS **INCLUDED THESE BASINS INTO THE DESIGN OF ITS** PROPOSED STORM INFRASTRUCTURE.



CAD FILE: J:\2021\211030\CAD\Dwgs\C\Estates_CDs\Pond_A_Grading

	POINT T	ARI F			PC
No.	DESC.	NORTHING & EASTING	ELEV	No.	DESC.
1	TC FLOWLINE	N: 444526.79 E: 222290.46	7559.59	31	SPILLWAY WEIR INV.
2	ТВС	N: 444528.27 E: 222290.12	7560.17	32	SPILLWAY WEIR INV.
3	TBC	N: 444525.45 E: 222291.16	7560.17	33	TOP
4	TC FLOWLINE	N: 444531.40 E: 222303.06	7559.46	34	TOP
5	TC FLOWLINE	N: 444539.14 E: 222312.88	7559.33	35	TOP
6	TC FLOWLINE	N: 444566.88 E: 222331.26	7559.00	36	ТОР
7	MAINT. RD. EDGE	N: 444457.98 E: 222223.41	7570.90	37	ТОР
8	MAINT. RD. EDGE	N: 444443.96 E: 222228.75	7571.06	38	ТОР
9	MAINT. RD. EDGE	N: 444463.39 E: 222232.50	7569.66	39	ТОР
10	MAINT. RD. EDGE	N: 444447.66 E: 222238.48	7569.82	40	TOP
11	MAINT. RD. EDGE / BOP	N: 444504.59 E: 222276.51	7564.00	41	ТОР
12	MAINT. RD. EDGE / BOP	N: 444492.60 E: 222285.61	7564.00	42	SPILLWAY WEIR INV.
13	ВОР	N: 444440.25 E: 222280.19	7564.00	43	SPILLWAY WEIR INV.
14	ВОР	N: 444422.39 E: 222278.94	7564.00	44	ТОР
15	ВОР	N: 444369.45 E: 222291.52	7564.00	45	ТОР
16	BOP HP	N: 444362.04 E: 222309.25	7564.00	46	ТОР
17	ВОР	N: 444373.24 E: 222325.60	7563.62	47	ТОР
18	ВОР	N: 444567.11 E: 222339.11	7561.50		
19	ВОР	N: 444582.71 E: 222319.90	7561.50		
20	ВОР	N: 444560.21 E: 222274.90	7561.63		
21	ВОР	N: 444533.46 E: 222263.80	7562.25		
22	BOP / TOP OF FOREBAY WALL	N: 444521.77 E: 222269.18	7565.33		
1		1			

N: 444516.38

E: 222271.24

N: 444475.69

E: 222243.95

N: 444460.75

E: 222249.64

N: 444357.48

E: 222276.86

N: 444343.67

E: 222312.66

N: 444367.45

E: 222342.78

N: 444590.85

E: 222383.01

N: 444617.49

E: 222379.77

7565.33

7567.50

7567.50

7567.50

7567.50

THIS HSEET HAS BEEN UPDATED TO REFLECT THE CHANGES MADE IN

FILING 3

19 20	1 2 3 ARTZ OREEK ORIVE 29 28 21 22 ALLEN RANCH 7 16 15	27 25 23 24 ROAD	35 7 35 30 30 30 30 30 30 30 30 30 30	39 40 41 42 49	FLYING HORSE NORTH GOLF COURSE
			Line Table		
	Line #	Length	Direction	Centerline/Flowline	
	L1	13.42	N 69°56'16" E	Centerline	
	L3	33.28	N 33°31'34" E	Centerline	

Line Table						
Line #	Length	Direction	Centerline/Flowline			
L1	13.42	N 69°56'16" E	Centerline			
L3	33.28	N 33°31'34" E	Centerline			

Curve Table								
Curve #	Length	Radius	Delta	Centerline/Flowline				
C1	12.71	20.00	36°24'43"	Flowline				
	· ·	<u> </u>		·				

POND GRADING NOTES:

POINT TABLE

NORTHING & EASTING | ELEV

7566.50

7566.50

7567.50

7567.50

7567.50

7567.50

7567.50

7567.82

7567.50

7567.50

7567.50

7566.50

7566.50

7567.50

7567.50

7569.66

N: 444621.06

E: 222377.98

N: 444635.13

E: 222370.96

N: 444638.71

E: 222369.17

N: 444642.78

E: 222355.03

N: 444566.42

E: 222229.50

N: 444530.71

E: 222222.96

N: 444355.04

E: 222272.11

N: 444339.28

E: 222313.25

N: 444366.66

E: 222347.77

N: 444587.56

E: 222397.64

N: 444624.19

E: 222393.19

N: 444627.76

E: 222391.40

N: 444641.83

E: 222384.38

N: 444645.41

E: 222382.59

N: 444655.60 E: 222347.23

N: 444578.17

E: 222219.95

N: 444525.36

E: 222208.95

- 1. TWO SIGNS OF MINIMUM 3 SQ. FT. AREA, SHALL BE INSTALLED AROUND THE POND PERIMETER. THE SIGNS WILL BE CONSTRUCTED OF A DURABLE MATERIAL SUCH AS METAL OR PLASTIC AND HAVE RED LETTERING ON A WHITE BACKGROUND STATING, "WARNING- THIS AREA IS A STORMWATER FACILITY AND IS SUBJECT TO PERIODIC FLOODING.
- 2. SEE LANDSCAPE PLAN FOR RE-SEEDING AREAS ASSOCIATED WITH PERMANENT CONTROL MEASURE IMPROVEMENTS.
- 3. SEE GRADING & EROSION CONTROL PLANS FOR ANY EXISTING VEGETATION IN THE AREA. CLEARING AND GRUBBING WILL OCCUR PRIOR TO POND
- CONSTRUCTION AND THEREFORE, NO EXISTING VEGETATION WILL BE PRESENT. 4. ALL RIPRAP MUST BE INSTALLED PER DETAIL ON NEXT PAGE.

ABBREVIATIONS:

B.O.P ~ BOTTOM OF POND T.O.P. ~ TOP OF POND T.C. ~TRICKLE CHANNEL T.B.C~ TOP BACK OF CURB C.L.~ CENTERLINE E.O.G~ EDGE OF GRADING S.W ~ SPILLWAY

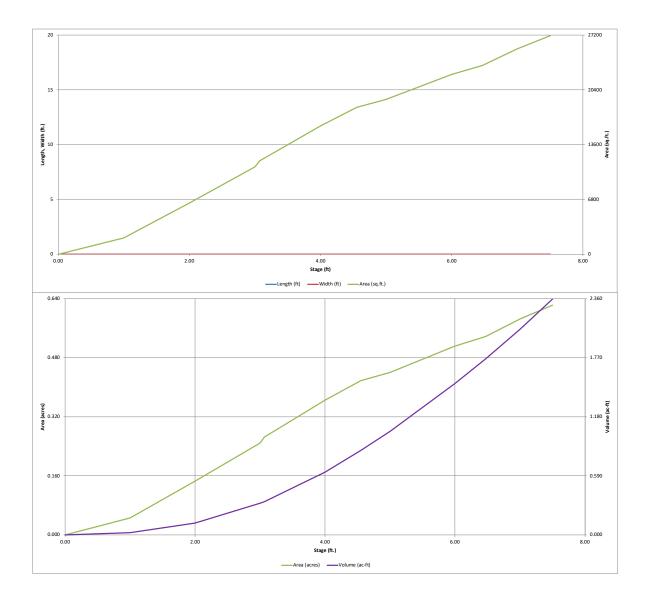
FLYING HORSE NORTH FILING 3 FLYING HORSE NORTH, LLC EL PASO COUNTY, CO

DRAINAGE DETAILS POND A GRADING PLAN

SHEET PND

THESE DETENTION BASIN STAGE-STORAGE TABLE E MHFD-Detention, Version 4.06 (July 2022) **CALCULATIONS** Project: FLYING HORSE NORTH FILING NO. 3 **HAVE BEEN** Basin ID: DESIGN POINT 2 (FLATS/CONDO AREA) UPDATED FOR THE 100-YR VOLUME EURV WQCV **CHANGES THAT** Depth Increment Stage - Storage Length **TOOK PLACE IN** Example Zone Configuration (Retention Pond) cription (ft) tage (ft) (ft) Watershed Information Top of Micropool 0.00 FILING 3 Selected BMP Type = EDB 7560 1.00 0.023 Watershed Area = 25.30 7561 2.00 6.349 0.146 5.165 0.119 Watershed Length = 1,800 7562 3.00 10,825 0.249 13,752 0.316 Watershed Length to Centroid = WQCV: 7562.07 Watershed Slope = 0.050 n/n 7563 4.00 15.899 0.365 27,304 0.627 Watershed Imperviousness = 32.24% EURV: 7563.55 percent 4.55 18,200 0.418 36,682 0.842 Percentage Hydrologic Soil Group A = 5.00 19,188 45,093 1.035 Percentage Hydrologic Soil Group B = 100.0% ercent 7565 6.00 22,288 0.512 65.830 1.511 Percentage Hydrologic Soil Groups C/D = 0.0% 100-YR: 7565.47 6.47 0.537 76,566 1.758 23,400 Target WQCV Drain Time = 40.0 2.055 CREST: 7566.5 Location for 1-hr Rainfall Depths = User Input 7.50 27,130 0.623 102,684 2.357 After providing required inputs above including 1-hour rainfall pths, click 'Run CUHP' to generate runoff hydrogra the embedded Colorado Urban Hydrograph Proce Water Quality Capture Volume (WQCV) = 0.334 Excess Urban Runoff Volume (EURV) = 0.842 acre-feet cre-feet 2-yr Runoff Volume (P1 = 1.19 in.) = 1.19 0.828 acre-feet inches 5-yr Runoff Volume (P1 = 1.5 in.) = 10-yr Runoff Volume (P1 = 1.75 in.) = 1.762 acre-feet 1.75 inches 25-yr Runoff Volume (P1 = 2 in.) = acre-feet 2.426 2.00 50-yr Runoff Volume (P1 = 2.25 in.) = inches 100-yr Runoff Volume (P1 = 2.52 in.) = 3.607 acre-feet 2.52 inches 500-yr Runoff Volume (P1 = 3.14 in.) = 4.918 Approximate 2-yr Detention Volume = Approximate 5-yr Detention Volume = 0.607 acre-feet 0.863 acre-feet Approximate 10-yr Detention Volume Approximate 25-yr Detention Volume = 1.423 acre-feet Approximate 50-yr Detention Volume = acre-feet Approximate 100-yr Detention Volume = 1.758 Define Zones and Basin Geometry Zone 1 Volume (WQCV) = 0.334 Zone 2 Volume (EURV - Zone 1) = 0.508 acre-feet Zone 3 Volume (100-year - Zones 1 & 2) = 0.916 Total Detention Basin Volume : 1.758 Initial Surcharge Volume (ISV) = user Initial Surcharge Depth (ISD) = Total Available Detention Depth (Htotal) = Depth of Trickle Channel (H_{TC}) = user Slope of Trickle Channel (S_{TC}) = user Slopes of Main Basin Sides (Smain) = H:V Basin Length-to-Width Ratio (R_{I/W}) = Initial Surcharge Area (A_{ISV}) = Surcharge Volume Length (L_{ISV}) = Surcharge Volume Width $(W_{ISV}) =$ Depth of Basin Floor (HFLOOR) = Length of Basin Floor (L_{FLOOR}) = Width of Basin Floor (W_{FLOOR}) = Area of Basin Floor (A_{FLOOR}) = user Volume of Basin Floor (V_{FLOOR}) = Depth of Main Basin (H_{MAIN}) = Length of Main Basin (L_{MAIN}) = Width of Main Basin (W_{MAIN}) = Area of Main Basin (A_{MAIN}) = user Volume of Main Basin (V_{MAIN}) = user Calculated Total Basin Volume (V_{total}) =

Pond A_DP2_Flats, Basin 8/2/2023, 10:30 AM

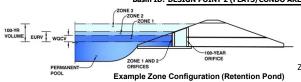


Pond A_DP2_Flats, Basin 8/2/2023, 10:30 AM

DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.06 (July 2022)

Project: FLYING HORSE NORTH FILING NO. 3 Basin ID: DESIGN POINT 2 (FLATS/CONDO AREA)



	Estimated	Estimated	
	Stage (ft)	Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	3.08	0.334	Orifice Plate
Zone 2 (EURV)	4.55	0.508	Orifice Plate
one 3 (100-year)	6.48	0.916	Weir&Pipe (Restrict)
•	Total (all zones)	1.758	

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth = N/A ft (distance below the filtration media surface)
Underdrain Orifice Diameter = N/A inches

	Calculated Parameters for Underdrai					
Underdrain Orifice Area =	N/A	ft ²				
Underdrain Orifice Centroid =	N/A	feet				

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Centroid of Lowest Orifice = 0.00 ft (relative to basin bottom at Stage = 0 ft)

Depth at top of Zone using Orifice Plate = 4.00 ft (relative to basin bottom at Stage = 0 ft)

Orifice Plate: Orifice Vertical Spacing = N/A inches

Orifice Plate: Orifice Area per Row = 2.00 sq. inches (diameter = 1-9/16 inches)

<u>te</u>

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	2.55						
Orifice Area (sq. inches)	2.00	2.00						

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

	Not Selected	Not Selected	
Invert of Vertical Orifice =	N/A	N/A	ft (rela
Depth at top of Zone using Vertical Orifice =	N/A	N/A	ft (rela
Vertical Orifice Diameter =	N/A	N/A	inches

ft (relative to basin bottom at Stage = 0 ft)
ft (relative to basin bottom at Stage = 0 ft)

	Calculated Parame	ters for Vertical Or	ifice
	Not Selected	Not Selected	
Vertical Orifice Area =	N/A	N/A	ft ²
ertical Orifice Centroid =	N/A	N/A	feet

User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir and No Outlet Pipe)

	Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	4.50	N/A	ft (relative to basin bottom at Stage =
Overflow Weir Front Edge Length =	3.00	N/A	feet
Overflow Weir Grate Slope =	0.00	N/A	H:V
Horiz. Length of Weir Sides =	2.50	N/A	feet
Overflow Grate Type =	Type C Grate	N/A	
Debris Clogging % =	50%	N/A	%
`			-

No Outlet Pipe)	Calculated Parameters for Overflow Weir				
	Zone 3 Weir	Not Selected			
$e = 0$ ft) Height of Grate Upper Edge, $H_t =$	4.50	N/A	feet		
Overflow Weir Slope Length =	2.50	N/A	feet		
Grate Open Area / 100-yr Orifice Area =	15.11	N/A			
Overflow Grate Open Area w/o Debris =	5.22	N/A	ft ²		
Overflow Grate Open Area w/ Debris =	2.61	N/A	ft ²		
			_		

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

c (Circular Orifice, i	Councid Flate, or	rectarig
Zone 3 Restrictor	Not Selected	
0.50	N/A	ft (dista
18.00	N/A	inches
4.50		inches
	Zone 3 Restrictor 0.50 18.00	0.50 N/A 18.00 N/A

ft (distance below basin bottom at Stage = 0 ft)
inches
Ou
inches
Half-Central Angle of Res

В

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate							
	Zone 3 Restrictor	Not Selected					
Outlet Orifice Area =	0.35	N/A	ft ²				
utlet Orifice Centroid =	0.22	N/A	feet				
strictor Plate on Pipe =	1.05	N/A	radians				

User Input: Emergency Spillway (Rectangular or Trapezoidal)

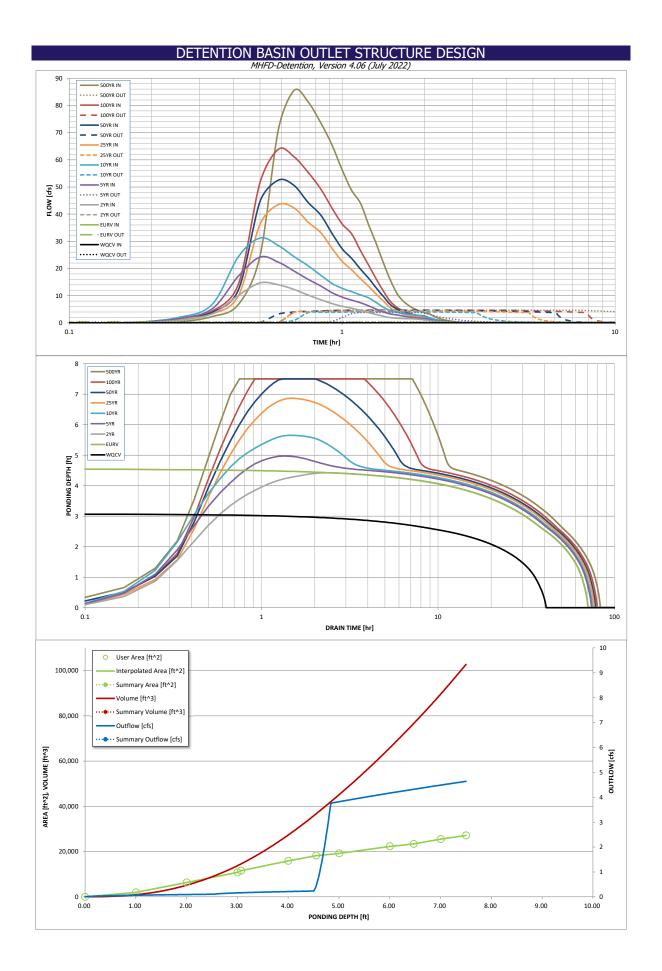
Spillway Invert Stage=	8.00	ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length =	23.72	feet
Spillway End Slopes =	4.00	H:V
Freeboard above Max Water Surface =	1.00	feet

Calculated Parameters for Spillway

Spillway Design Flow Depth=		feet
Stage at Top of Freeboard =		feet
Basin Area at Top of Freeboard =	0.62	acres
Basin Volume at Top of Freeboard =	2.36	acre-ft
		•

Routed Hydrograph Results 7	The user can ove	erride the default CUF	HP hydrographs ar	nd runoff volumes b	y entering new vall	ues in the Inflow Hy	vdrographs table (C	Columns W through	h AF).
Design Storm Return Period =	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
One-Hour Rainfall Depth (in) =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52	3.14
CUHP Runoff Volume (acre-ft) =	0.334	0.842	0.828	1.315	1.762	2.426	2.934	3.607	4.918
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	0.828	1.315	1.762	2.426	2.934	3.607	4.918
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A	4.0	10.9	16.1	28.3	35.4	44.3	61.5
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A							
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.16	0.43	0.64	1.12	1.40	1.75	2.43
Peak Inflow Q (cfs) =	N/A	N/A	14.7	24.2	31.2	43.5	52.5	63.9	85.5
Peak Outflow Q (cfs) =	0.2	0.4	0.2	3.8	4.1	4.4	4.6	4.6	4.6
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	0.4	0.3	0.2	0.1	0.1	0.1
Structure Controlling Flow =	Plate	Overflow Weir 1	Plate	Outlet Plate 1	Outlet Plate 1	Outlet Plate 1	N/A	N/A	N/A
Max Velocity through Grate 1 (fps) =	N/A	0.04	N/A	0.7	0.7	0.8	0.8	0.8	0.8
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	38	65	65	66	65	63	63	62	60
Time to Drain 99% of Inflow Volume (hours) =	40	68	68	70	71	71	71	72	73
Maximum Ponding Depth (ft) =	3.08	4.55	4.42	4.97	5.65	6.86	7.50	7.50	7.50
Area at Maximum Ponding Depth (acres) =	0.27	0.42	0.41	0.44	0.49	0.57	0.62	0.62	0.62
Maximum Volume Stored (acre-ft) =	0.336	0.842	0.789	1.018	1.332	1.974	2.357	2.357	2.357

Pond A_DP2_Flats, Outlet Structure 8/2/2023, 10:30 AM



Pond A_DP2_Flats, Outlet Structure 8/2/2023, 10:30 AM

DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename:

Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]		10 Year [cfs]			100 Year [cfs]	
	0:00:00									
5.00 min	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:15:00	0.00	0.00	0.00	1.55	1.93	1.30	1.63	1.60	0.35 2.30
	0:20:00	0.00	0.00	3.31	5.09	6.71	3.28	3.83	4.27	6.78
	0:25:00	0.00	0.00	10.10	17.17	24.32	10.02	12.14	14.18	24.52
	0:30:00	0.00	0.00	14.72	24.19	31.21	36.23	44.60	51.55	71.06
	0:35:00	0.00	0.00	14.02	22.32	28.42	43.51	52.50	63.88	85.54
	0:40:00	0.00	0.00	12.28	19.07	24.39	42.25	50.54	61.11	81.34
	0:45:00	0.00	0.00	10.21	16.02	21.02	37.05	44.30	55.38	73.68
	0:50:00	0.00	0.00	8.54	13.61	17.56	33.24	39.74	49.35	65.56
	0:55:00	0.00	0.00	7.10	11.14	14.54	27.55	33.02	42.33	56.29
	1:00:00	0.00	0.00	6.09	9.46	12.70	22.63	27.28	36.39	48.75
	1:05:00 1:10:00	0.00	0.00	5.42 4.56	8.36 7.40	11.44 10.29	19.54 16.23	23.70 19.78	32.74 26.60	44.02 36.09
	1:15:00	0.00	0.00	3.78	6.26	9.17	13.39	16.39	21.23	29.15
	1:20:00	0.00	0.00	3.06	5.04	7.49	10.53	12.85	16.11	22.03
	1:25:00	0.00	0.00	2.43	3.98	5.69	8.02	9.72	11.67	15.91
	1:30:00	0.00	0.00	1.95	3.27	4.54	5.61	6.78	7.95	11.07
	1:35:00	0.00	0.00	1.69	2.93	3.89	4.16	5.11	5.78	8.20
	1:40:00	0.00	0.00	1.58	2.50	3.46	3.30	4.09	4.51	6.45
	1:45:00	0.00	0.00	1.52	2.18	3.15	2.76	3.43	3.62	5.22
	1:50:00	0.00	0.00	1.48	1.95	2.95	2.39	2.98	3.00	4.37
	1:55:00	0.00	0.00	1.29	1.77	2.70	2.16	2.70	2.58	3.77
	2:00:00	0.00	0.00	1.13	1.60	2.33	2.00	2.50	2.28	3.35
	2:05:00 2:10:00	0.00	0.00	0.86	1.20	1.74	1.48	1.85	1.64	2.41
	2:10:00	0.00	0.00	0.64	0.88	1.26	1.08	1.34	1.19	1.74
	2:20:00	0.00	0.00	0.48	0.65 0.47	0.90 0.65	0.78 0.57	0.97 0.70	0.87	1.26 0.93
	2:25:00	0.00	0.00	0.26	0.33	0.03	0.40	0.50	0.46	0.66
	2:30:00	0.00	0.00	0.18	0.23	0.33	0.29	0.35	0.32	0.47
	2:35:00	0.00	0.00	0.13	0.16	0.23	0.20	0.25	0.23	0.33
	2:40:00	0.00	0.00	0.08	0.10	0.15	0.14	0.17	0.15	0.22
	2:45:00	0.00	0.00	0.05	0.06	0.09	0.08	0.10	0.09	0.13
	2:50:00	0.00	0.00	0.02	0.03	0.04	0.04	0.05	0.05	0.06
	2:55:00	0.00	0.00	0.01	0.01	0.01	0.02	0.02	0.01	0.02
	3:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:10:00 3:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:00:00 4:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:25:00 4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:45:00 4:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:05:00 5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:30:00 5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:55:00 6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0.00.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

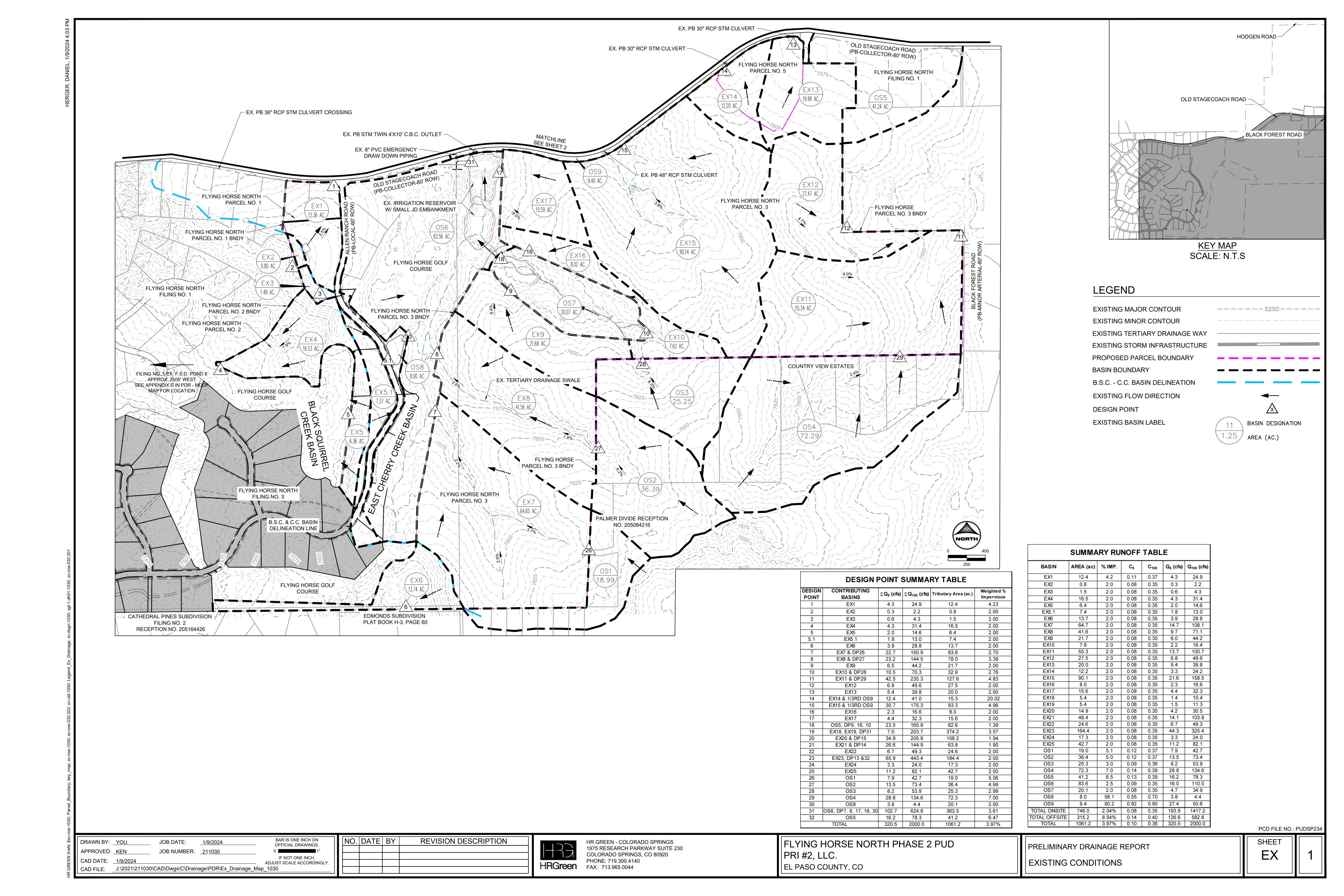
Pond A_DP2_Flats, Outlet Structure 8/2/2023, 10:30 AM

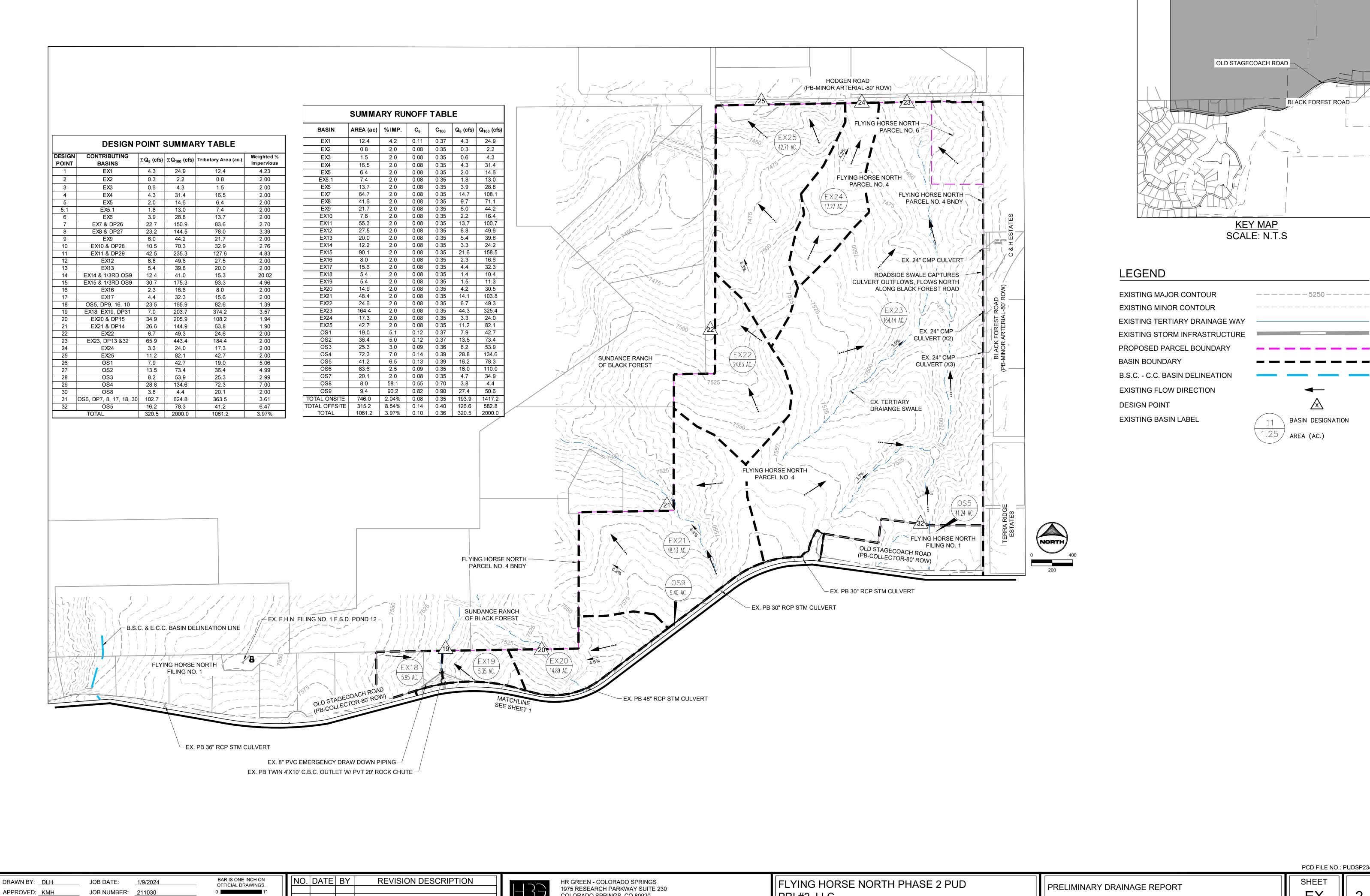




Appendix F:

Drainage Maps





COLORADO SPRINGS, CO 80920

PHONE: 719.300.4140

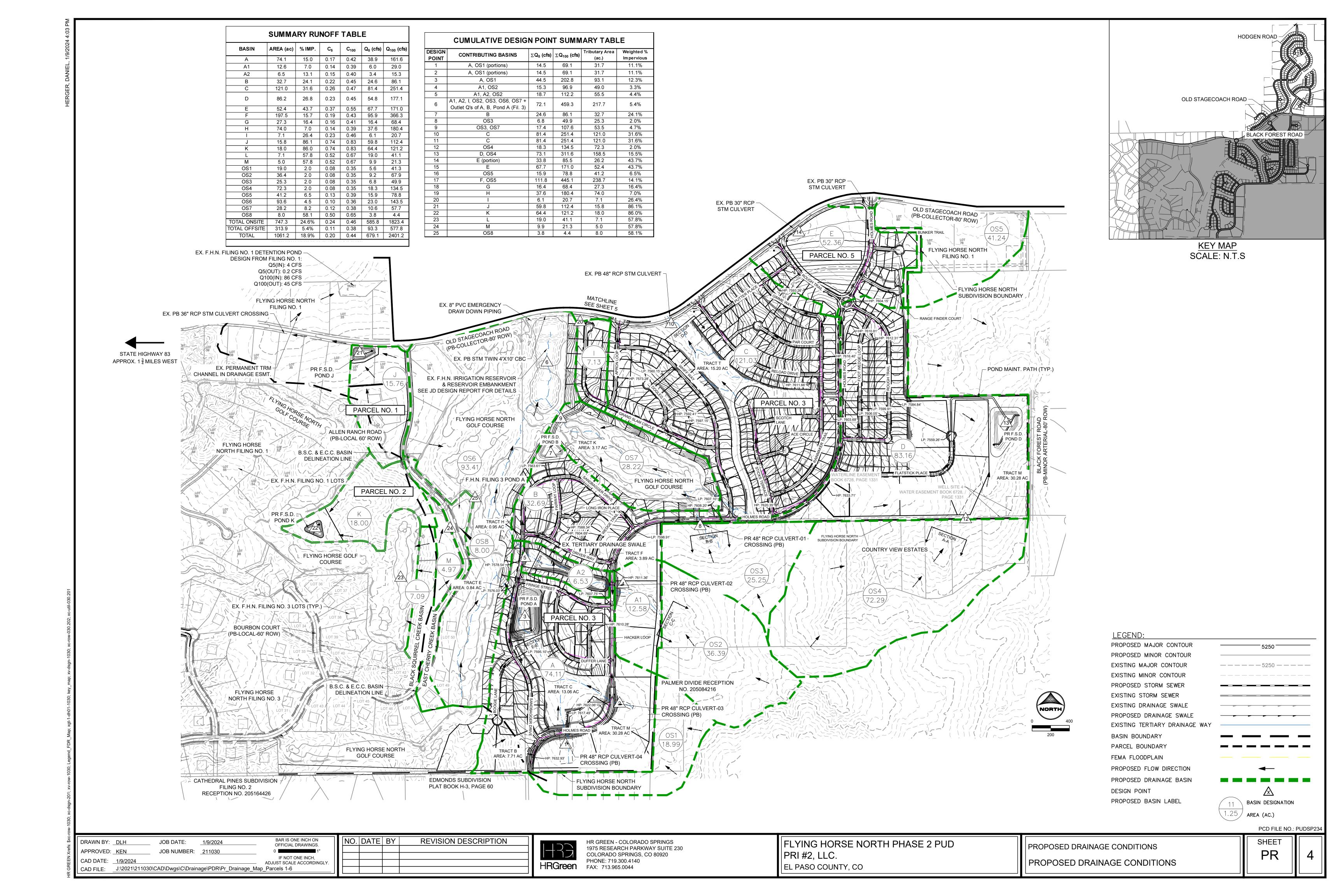
HRGreen FAX: 713.965.0044

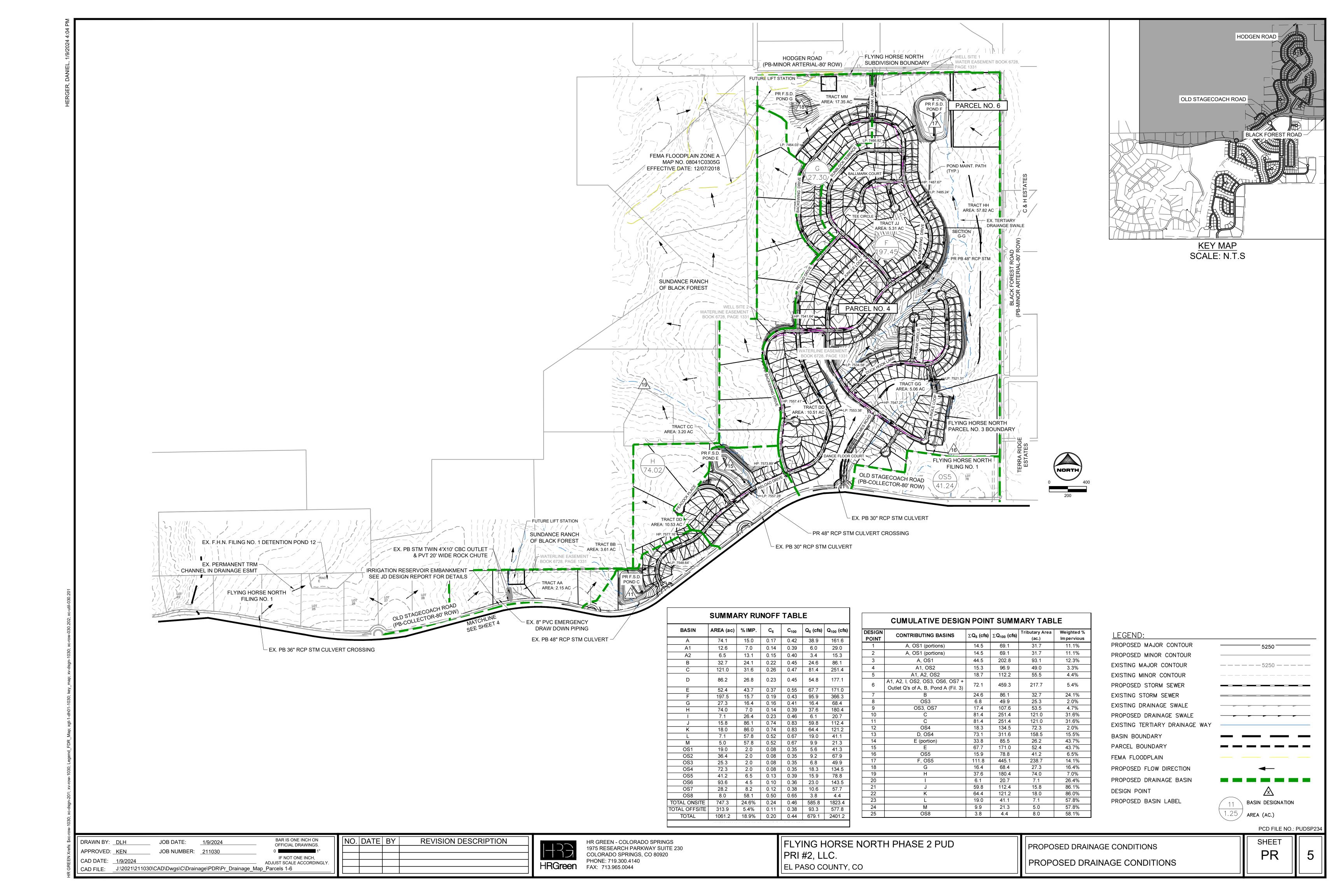
IF NOT ONE INCH, ADJUST SCALE ACCORDINGLY.

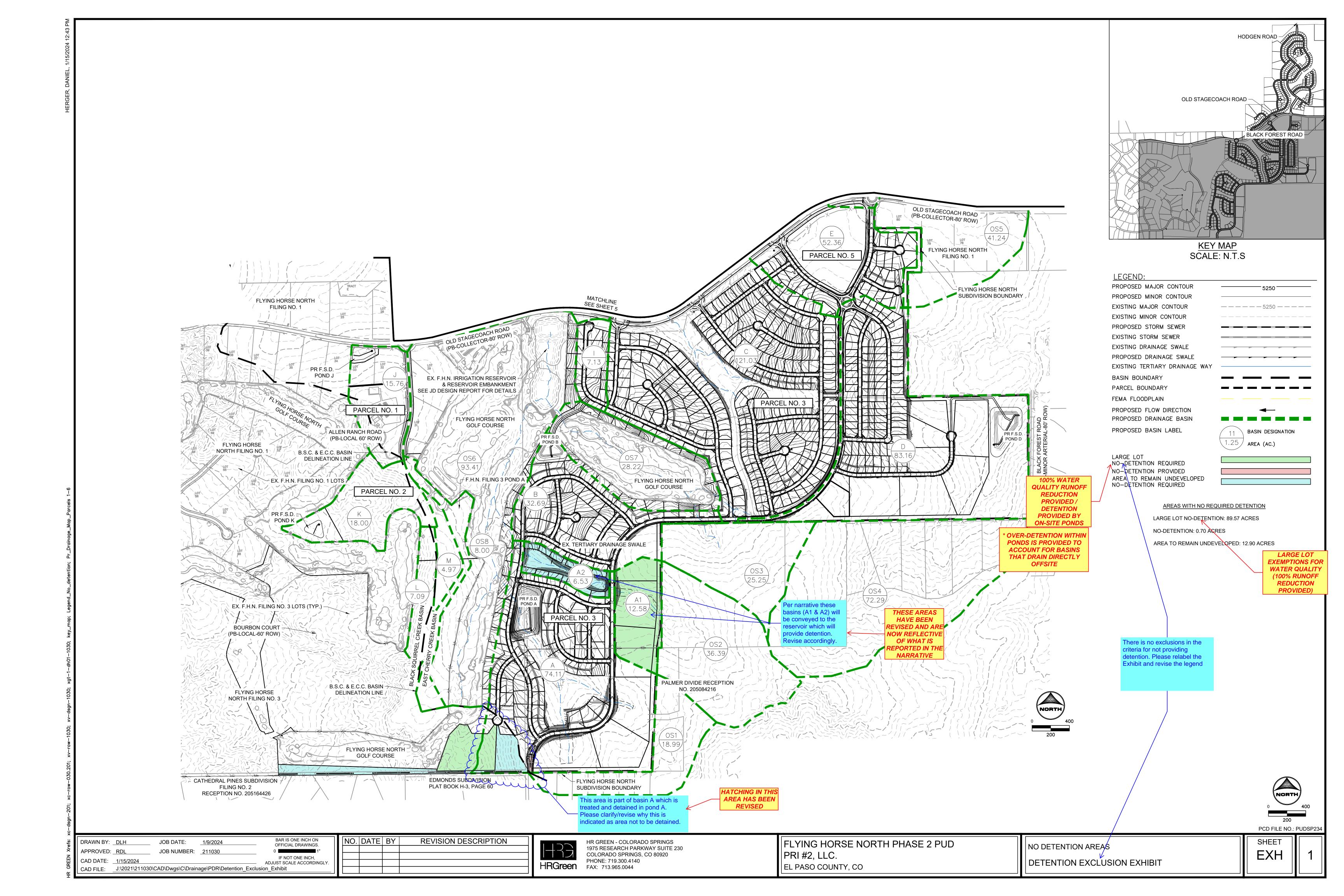
CAD DATE: <u>1/9/2024</u>

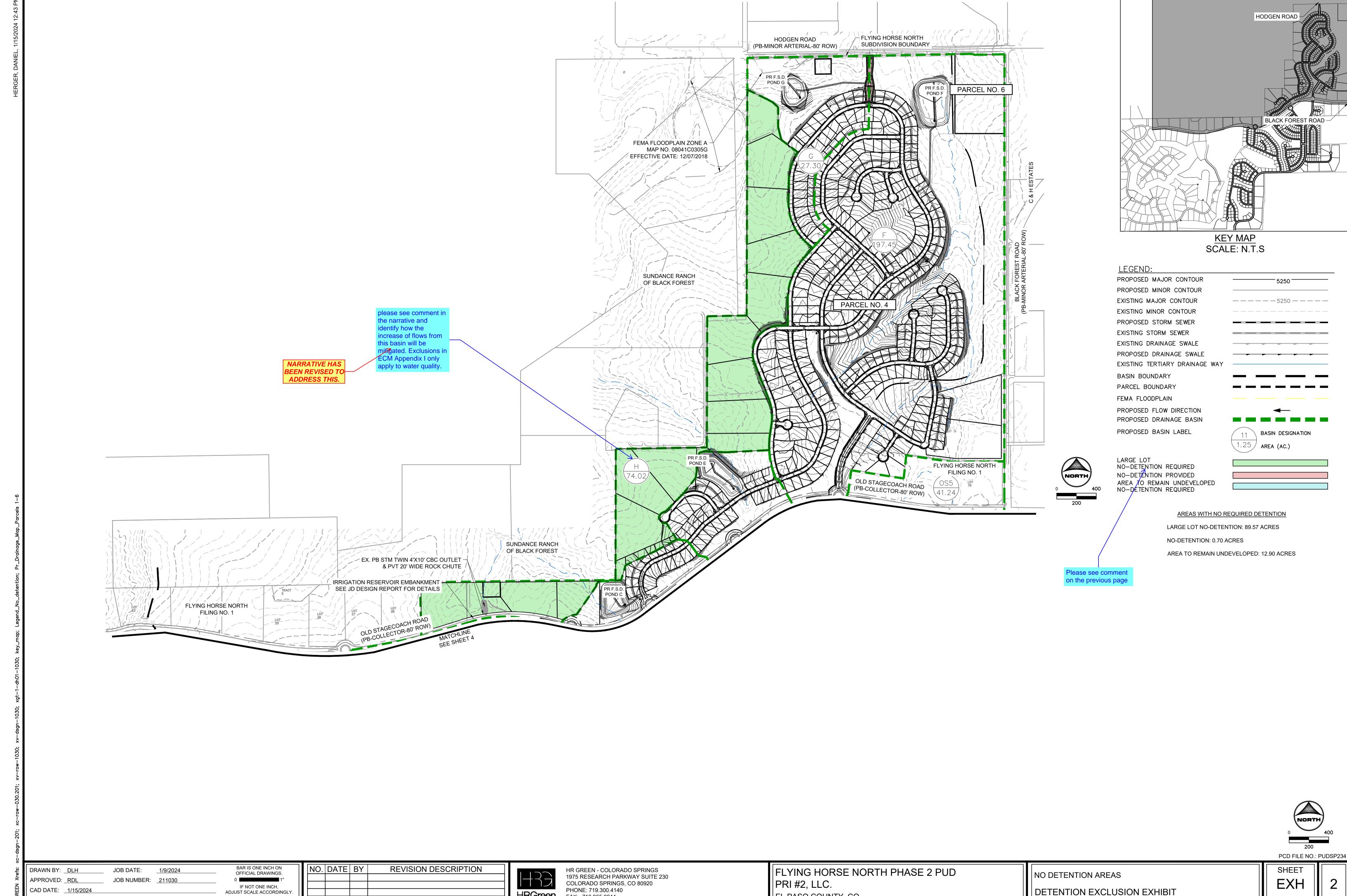
CAD FILE: J:\2021\211030\CAD\Dwgs\C\Drainage\PDR\Ex_Drainage_Map_1030

HODGEN ROAD









EL PASO COUNTY, CO

HRGreen PHONE: 719.300.414 FAX: 713.965.0044

CAD DATE: <u>1/15/2024</u>

CAD FILE: J:\2021\211030\CAD\Dwgs\C\Drainage\PDR\Detention_Exclusion_Exhibit

DETENTION EXCLUSION EXHIBIT

EXH