# PRELIMINARY DRAINAGE REPORT FOR <br> URBAN COLLECTION AT PALMER VILLAGE 

Prepared For:<br>MDC Holdings - Richmond American Homes<br>4350 South Monaco Street<br>Denver, CO 80237

720-977-3827

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Project No. 25149.01

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## ENGINEERS STATEMENT:

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by El Paso County for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors, or omissions on my part in preparing this report.


Glenn D. Ellis, Colorado P.E. 38861
For and On Behalf of JR Engineering, LLC


## DEVELOPER'S STATEMENT:

I, the developer, have read and will comply with all of the requirements specified in this drainage report and plan.

Business Name: $\quad$ MDC Holdings - Richmond American Homes

By:

Title:
Address:


VP of Land Acquisition \& Entitlements
4350 South Monaco Street
Denver, CO 80237

## El Pass County:

Filed in accordance with the requirements of the El Pass County Land Development Code, Drainage Criteria Manual, Volumes 1 and 2 and Engineering Criteria Manual, as amended.

[^0]Date

Conditions:

## JR Engineering

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## Purpose

This document is the Preliminary Drainage Report for Urban Collection at Palmer Village. The purpose of this report is to identify on-site and off-site drainage patterns, storm sewer, culvert and inlet locations, areas tributary to the site, and to safely route developed storm water to adequate outfall facilities.

## General Site Description

## General Location

Urban Collection at Palmer Village is a proposed development on six un-platted parcels with a total area of 23.1 acres. The site is located in the northeast quarter of Section 5, Township 14 South, Range 65 West of the Sixth Principal Meridian in the County of El Paso, State of Colorado. The site is located immediately south of Constitution Avenue on the west and east side of Hannah Ridge Drive, extending to the east to Marksheffel Road. The site is bounded by Constitution Avenue to the north, Marksheffel Road to the east, Jessica Heights Filing No. 1 to the south, and the Cherokee Park Townhomes to the west. The parcels are planned to be platted after approval of the Development Plan. Refer to the vicinity map in Appendix A.

## Description of Property

A 100-unit residential development is proposed on the four western parcels (totaling 10.83 acres) (hereby referred to as the "site") per the corresponding preliminary Development Plan this drainage report supports. Two parcels are on the east side of Hannah Ridge Drive, and two are on the west side. The two parcels along Constitution Avenue, east to Marksheffel Road will not be developed at this time. They are referenced in this report only in the context of being included in plat of the proposed development. Any development of these two parcels shall require separate drainage analysis and drainage reports. The existing western parcels are undeveloped other than a sanitary sewer easement that follows the eastern border of the two parcels on the east side of Hannah Ridge Drive. The proposed development site is comprised of variable sloping grasslands that generally slope east at approximately $3 \%$ on the east side of Hannah Ridge Drive. On the west side of Hannah Ridge Drive the land slopes at about $1 \%$ to the east, draining into the curb and gutter in Hannah Ridge Drive.

Soil characteristics are comprised of Blakeland loamy sand. NRCS rates this soil designation as Hydrologic Group A. Group A soils exhibit a high infiltration rate when thoroughly wet and consist chiefly of deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a high rate of water transmission. Refer to the soil survey mapping in Appendix A.

There are no major drainageways on the proposed development site, although a tributary to the East Fork Sand Creek is immediately to the east of the site, within the undeveloped tracts.

There are no known irrigation facilities located on the project site. A 12 " PVC sanitary sewer runs along the eastern side of the site within an easement.

## FLOODPLAIN STATEMENT

Based on the FEMA Firm Map Number 08041C0752G, revised December 7, 2018, the entire development is located within Zone X, or areas area outside the Special Flood Hazard Area (SFHA) and higher than the elevation of the 0.2 -percent-annual-chance (or 500 -year) flood. The FEMA map containing the site has been presented in Appendix A.

## Existing Drainage Conditions

## MAjor Basin Descriptions

The site lies within the Sand Creek Drainage Basin based on the "Sand Creek Drainage Basin Planning Study" completed by Kiowa Engineering Corporation in January 1993. The Sand Creek Drainage Basin covers approximately 54 square miles and is divided into five major sub-basins: Sand Creek Mainstem, East Fork Sand Creek, Central Tributary to East Fork, West Fork, and East Fork Subtributary. The site is within the East Fork Sand Creek sub-basin, as shown in Appendix E. The Sand Creek Basin discharges into Fountain Creek approximately 1.5 miles upstream of Academy Boulevard Bridge over Fountain Creek.

As development occurred within the basin, the site was analyzed with the "Jessica Heights Filing No. 1 Final Drainage Report" completed by M.V.E. Inc. in April 2005. The portion of the site west of Hannah Ridge Drive was identified as Basin C1 and the portion of the site east of Hannah Ridge Drive was identified as Basin A2. Basin C 1 contributes existing flows of $\mathrm{Q}_{5}=2.8 \mathrm{cfs}$ and $\mathrm{Q}_{100}=6.8$ cfs. Basin A2 contributes existing flows of $\mathrm{Q}_{5}=3.2 \mathrm{cfs}$ and $\mathrm{Q}_{100}=7.6 \mathrm{cfs}$. Runoff from both basins flows east. Basin C1 is captured in Hannah Ridge Drive curb and gutter and is conveyed to Constitution Avenue, while Basin A2 sheet flows off site to the adjacent parcel to the east.

Most recently, the site was analyzed within the "Hannah Ridge at Feathergrass Master Drainage Development Plan" completed by M.V.E. Inc in November 2007. The site was identified as Basin OSA14 with existing flows of $\mathrm{Q}_{5}=14$ and $\mathrm{Q}_{100}=27$ cfs flowing easterly to Tributary to Sand Creek East Fork Reach No. 6.

As previously stated, there are no known irrigation facilities within the site that would impact drainage. An existing 12 " PVC sanitary sewer runs along the eastern boundary of the site and is contained within a dedicated easement.

## Existing Sub-basin Drainage

The site is bisected by Hannah Ridge Drive, dividing the site into east and west parcels. The east side drains directly into a tributary to the East Fork Sand Creek (Tributary to Sand Creek - East Fork Reach No. 6). Runoff from the west site sheet flows across the site and is collected in Hannah Ridge Drive curb and gutter and is conveyed either north to Constitution Avenue or south to the Jessica Heights Subdivision. The west site is comprised of existing Basins EX3 and EX4. The east site is comprised of Basin EX6. Basins EX1 and EX2 are offsite basins that sheet flow onto Basins EX3 and EX4, respectively. Basin EX5 flows offsite to Constitution Avenue. The basins shown in the "Jessica Heights Filing No. 1 Final Drainage Report" created by M.V.E., Inc. in April, 2005 correspond to the existing basins in this report in the following manner: $\mathrm{OSA}=\mathrm{EX} 1, \mathrm{OSB}=\mathrm{EX} 2$, $\mathrm{C} 1=\mathrm{EX} 3$ and EX4, A4 = EX5, A2 = EX6.

Existing Basin EX1 is approximately 0.15 acres and is consistent with the Jessica Heights Filing No. 1 Final Drainage Report Basin OSA. Flow from this basin sheet flows onto the site to Basin EX3 at Design Point ( DP ) $1\left(\mathrm{Q}_{5}=0.04 \mathrm{cfs}, \mathrm{Q}_{100}=0.4 \mathrm{cfs}\right.$ ), eventually reaching DP 3 , a local depression.

Existing Basin EX2 is approximately 0.46 acres and is consistent with the Jessica Heights Filing No. 1 Final Drainage Report Basin OSB. Flow from this basin ( $\mathrm{Q}_{5}=0.2 \mathrm{cfs}, \mathrm{Q}_{1 \text { oo }}=1.2 \mathrm{cfs}$ ) sheet flows onto the site to Basin EX4 at DP2, eventually reaching Hannah Ridge Drive at DP4.

Existing Basin EX3 is approximately 4.27 acres and consists of prairie grasses. Flow from this basin $\left(\mathrm{Q}_{5}=1.2 \mathrm{cfs}, \mathrm{Q}_{1 \text { oo }}=9.0 \mathrm{cfs}\right)$ sheet flows to the local depression at DP3. According to the available contour data, once the local depression has filled, the overtopping flow travels to the northeast. The flow then is conveyed to the curb and gutter along the south side of Constitution Avenue, where it is conveyed to an inlet and discharges into a tributary to the East Fork Sand Creek.

Existing Basin EX4 is approximately 1.62 acres and consists of prairie grasses and a portion of Hannah Ridge Drive. Flow from this basin $\left(\mathrm{Q}_{5}=1.1 \mathrm{cfs}, \mathrm{Q}_{100}=4.0 \mathrm{cfs}\right)$ sheet flows to the curb and gutter in Hannah Ridge Drive at DP4. The flow then is conveyed south via the Jessica Heights Subdivision storm sewer system, eventually discharging into a tributary to the East Fork Sand Creek.

Existing Basin EX5 is approximately 0.37 acres and consists of a portion of Hannah Ridge Drive and prairie grasses. Flow from this basin $\left(\mathrm{Q}_{5}=1.4 \mathrm{cfs}, \mathrm{Q}_{1 \text { оо }}=2.7 \mathrm{cfs}\right)$ flows north along the Hannah Ridge Drive curb and gutter until it reaches the curb and gutter on the south side of Constitution Avenue at DP5. From there, the flow travels along the Constitution Avenue curb and gutter until reaching an inlet and discharges into a tributary to the East Fork Sand Creek.

Existing Basin EX6 is approximately 5.25 acres and consists of prairie grasses. Flow from this basin $\left(\mathrm{Q}_{5}=1.5 \mathrm{cfs}, \mathrm{Q}_{1 \text { oo }}=11.1 \mathrm{cfs}\right)$ sheet flows to the east and enters a tributary to the East Fork Sand Creek.

As stated previously, the undeveloped tracts east of the site have not been analyzed in their existing conditions as part of this report. Future development of these tracts will require a separate drainage report.

## Proposed Drainage Conditions

## Proposed Sub-basin Drainage

The proposed site was broken into two major basins: Basin A (west parcels) and Basin B (east parcels). The proposed basin (and sub-basin) delineation is shown on the drainage basin map and is described as follows;

Basin A1 consists of approximately 0.74 acres and includes walks, drives, roofs and landscape areas. Flow from this basin ( $\mathrm{Q}_{5}=2.0 \mathrm{cfs}$ and $\mathrm{Q}_{100}=4.2 \mathrm{cfs}$ ) will be collected and conveyed in a 3.0' concrete pan, that follows the centerline of Vanhoutte View, to DP1. At DP1, flow enters Type A curb and gutter and is conveyed to an on-grade Double Denver Type 16 Combination Inlet (Double Type 16) at DP3, where it combines with Basin A2 flow. Discussion of DP3 captured flow versus flow-by is presented in the Basin A2 description.

Basin A2 consists of approximately 0.17 acres and includes walks, drives, and landscape areas. Flow from this basin ( $\mathrm{Q}_{5}=0.5 \mathrm{cfs}$ and $\mathrm{Q}_{100}=1.0 \mathrm{cfs}$ ) will be collected and conveyed in Type A curb and gutter in Wayfaring Tree Heights to an on-grade Double Type 16 at DP3. Total flows at DP3 are $\mathrm{Q}_{5}=2.4 \mathrm{cfs}$ and $\mathrm{Q}_{100}=5.3 \mathrm{cfs}$. In the 5-year event, 1.9 cfs is captured, and 3.3 cfs is captured in the 100 -year event. DP3 flow-by of $\mathrm{Q}_{5}=0.5 \mathrm{cfs}$ and $\mathrm{Q}_{100}=2.0 \mathrm{cfs}$ continues in curb and gutter to DP5 where it combines with Basin A5 flow. DP3 captured flows are piped in 18" RCP to DP8.1 before discharging into Pond A at DP10.

Basin A3 consists of approximately 0.11 acres and includes walks, drives, and landscape areas. Flow from this basin ( $\mathrm{Q}_{5}=0.3 \mathrm{cfs}$ and $\mathrm{Q}_{100}=0.7 \mathrm{cfs}$ ) will be collected and conveyed in Type A curb and gutter in Wayfaring Tree Heights to an on-grade Double Type 16 at DP4, where it combines with Basin A4 flow. Total flows at DP4 are $\mathrm{Q}_{5}=2.4 \mathrm{cfs}$ and $\mathrm{Q}_{100}=5.8 \mathrm{cfs}$. In the 5-year event, 1.9 cfs is captured and 3.5 cfs is captured in the 100 -year event. DP4 flow-by of $\mathrm{Q}_{5}=0.5 \mathrm{cfs}$ and $\mathrm{Q}_{100}=2.3 \mathrm{cfs}$ continues in curb and gutter to DP6 where it combines with Basin A7 flow. DP4 captured flows are piped in 18 " RCP to DP4.1, where it combines with flow from DP3 and ultimately discharges into Pond A at DP10.

Basin A4 consists of approximately 0.72 acres and includes walks, drives, roofs and landscape areas. Flow from this basin ( $\mathrm{Q}_{5}=2.0 \mathrm{cfs}$ and $\mathrm{Q}_{100}=4.2 \mathrm{cfs}$ ) will be collected and conveyed in a 3.0' concrete pan that follows the centerline of Vanhoutte View, to DP2. At DP2, flow enters Type A curb and gutter and is conveyed to an on-grade Double Type 16 at DP4, where it combines with Basin A3 flow. Discussion of DP4 captured flow versus flow-by is presented in the Basin A3 description.

Basin A5 consists of approximately 0.77 acres and includes walks, drives, roofs and landscape areas. Flow from this basin $\left(\mathrm{Q}_{5}=1.7 \mathrm{cfs}\right.$ and $\left.\mathrm{Q}_{100}=3.8 \mathrm{cfs}\right)$ will be collected and conveyed in a 3.0 ' concrete pan that follows the centerline of Serviceberry Grove, to DP5. At DP5, flow enters Type A curb and gutter and combines with DP3 flow-by. The combined flow is conveyed to a sump Double Type 16 at DP8, where it combines with Basin A6 and DP7 flow. Discussion of DP8 captured flow is presented in the Basin A6 description.

Basin A6 consists of approximately 0.26 acres and includes walks, drives, and landscape areas. Flow from this basin ( $\mathrm{Q}_{5}=0.9 \mathrm{cfs}$ and $\mathrm{Q}_{100}=1.6 \mathrm{cfs}$ ) will be collected and conveyed in Type A curb and gutter in Wayfaring Tree Heights to a sump Double Type 16 at DP8. The total combined flow at DP8 from DP5, DP7 and Basin A6 is $\mathrm{Q}_{5}=4.1 \mathrm{cfs}$ and $\mathrm{Q}_{1 \text { 1oo }}=10.0 \mathrm{cfs}$. All flow at DP8 is captured and piped in a 30 " RCP to DP9.1, and discharges into Pond A at DP10. If the sump inlet at DP8 were to become clogged, overflows would spill over the crown to the Denver Triple Type 16 at DP9.

Basin A7 consists of approximately 0.54 acres and includes walks, drives, roofs and landscape areas. Flow from this basin ( $\mathrm{Q}_{5}=1.3 \mathrm{cfs}$ and $\mathrm{Q}_{100}=2.8 \mathrm{cfs}$ ) will be collected and conveyed in a 3.0' concrete pan that follows the centerline of Serviceberry Grove, to DP6. At DP6, flow enters Type A curb and gutter and combines with DP4 flow-by. The combined flow is conveyed to a sump Denver Triple Type 16 at DP9, where it combines with Basin A9 flow. Discussion of DP9 captured flow is presented in the Basin A9 description.

Basin A8 consists of approximately 0.70 acres and includes walks, drives, roofs and landscape areas. Flow from this basin $\left(\mathrm{Q}_{5}=1.4 \mathrm{cfs}\right.$ and $\left.\mathrm{Q}_{100}=3.2 \mathrm{cfs}\right)$ will be collected and conveyed in a 3.0 ' concrete pan that follows the centerline of Fountain Grass Grove, to DP7. At DP7, flow enters Type A curb and gutter and is conveyed to a sump Double Type 16 at DP8 where it combines with DP5 and Basin A6 flows. Discussion of DP8 captured flow is presented in the Basin A6 description.

Basin A9 consists of approximately 0.72 acres and includes walks, drives, roofs and landscape areas. Flow from this basin $\left(\mathrm{Q}_{5}=1.8 \mathrm{cfs}\right.$ and $\left.\mathrm{Q}_{1 \mathrm{oo}}=3.8 \mathrm{cfs}\right)$ will be collected and conveyed in Type A curb and gutter in Fountain Grass Grove to a sump Triple Type 16 at DP9. The total combined flow at DP9 from DP6 and Basin A9 is $\mathrm{Q}_{5}=3.3 \mathrm{cfs}$ and $\mathrm{Q}_{100}=8.4 \mathrm{cfs}$. All flow at DP9 is captured and piped in $30 "$ RCP to DP10. If the sump inlet at DP9 were to become clogged, overflows would overtop the curb and discharge directly into Pond A.

Basin A10 consists of approximately 0.46 acres of landscaped areas and contains Full Spectrum Water Quality and Detention Pond A. Flow from this basin ( $\mathrm{Q}_{5}=0.2 \mathrm{cfs}$ and $\mathrm{Q}_{100}=1.2 \mathrm{cfs}$ ) is captured in a grass-lined swale that discharges directly into Pond A where it combines with flow from Basins A1-A9. A detailed discussion of Full Spectrum Water Quality and Detention Pond A is presented in the Water Quality section later in this report.

Basin A11 consists of approximately 0.29 acres of landscaped area, emergency access, and sidewalk. Due to topographical constraints and the degree of development therein, Basin A11 ( $\mathrm{Q}_{5}=0.4 \mathrm{cfs}$ and $\mathrm{Q}_{100}=1.2 \mathrm{cfs}$ ) will discharge directly into Constitution Avenue curb and gutter.

Basin A12 consists of approximately 0.14 acres of landscaped area and sidewalk. Due to topographical constraints and the degree of development therein, Basin $\mathrm{A} 11\left(\mathrm{Q}_{5}=0.2\right.$ cfs and $\mathrm{Q}_{100}=0.6 \mathrm{cfs}$ ) flow will discharge directly into Constitution Avenue curb and gutter.

Basin B1 consists of approximately 0.65 acres and includes walks, drives, roofs and landscape areas. Flow from this basin ( $\mathrm{Q}_{5}=1.4 \mathrm{cfs}$ and $\mathrm{Q}_{100}=3.3 \mathrm{cfs}$ ) will be collected and conveyed in a 3.0' concrete pan that follows the centerline of Fountain Grass Grove, to DP15. At DP15, flow enters Type A curb and gutter and is conveyed to an on-grade Double Denver Type 16 Combination Inlet (Double Type 16) at DP17, where it combines with Basin B2 flow. Discussion of DP17 captured flow versus flowby is presented in the Basin B2 description.

Basin B2 consists of approximately 0.08 acres and includes walks and drives. Flow from this basin $\left(\mathrm{Q}_{5}=0.4 \mathrm{cfs}\right.$ and $\left.\mathrm{Q}_{100}=0.7 \mathrm{cfs}\right)$ will be collected and conveyed in Type A curb and gutter in Blue Avena View to an on-grade Double Type 16 at DP17. Total flows at DP17 from DP15 and Basin B2 are $\mathrm{Q}_{5}=1.7 \mathrm{cfs}$ and $\mathrm{Q}_{100}=3.8 \mathrm{cfs}$. In the 5-year event, 1.4 cfs is captured and 2.4 cfs is captured in the 100 -year event. DP17 flow-by of $\mathrm{Q}_{5}=0.3 \mathrm{cfs}$ and $\mathrm{Q}_{100}=1.4 \mathrm{cfs}$ continues in curb and gutter to DP19 where it combines with Basin B5 flow. DP17 captured flows are piped in 18" RCP to DP18.1, where it combines with flow from DP18, before discharging into Pond B at DP25.

Basin B3 consists of approximately 0.11 acres and includes walks, drives, and landscape areas. Flow from this basin $\left(\mathrm{Q}_{5}=0.5 \mathrm{cfs}\right.$ and $\left.\mathrm{Q}_{100}=0.9 \mathrm{cfs}\right)$ will be collected and conveyed in Type A curb and gutter in Blue Avena View to an on-grade Double Type 16 at DP18, where it combines with DP16 flow. Total flows at DP18 from DP16 and Basin B3 are $\mathrm{Q}_{5}=2.8 \mathrm{cfs}$ and $\mathrm{Q}_{100}=5.6 \mathrm{cfs}$. In the 5 -year event, 2.0 cfs is captured and 3.1 cfs is captured in the 100 -year event. DP18 flow-by of $\mathrm{Q}_{5}=0.8 \mathrm{cfs}$ and $\mathrm{Q}_{100}=2.5 \mathrm{cfs}$ continues in curb and gutter to DP20 where it combines with Basin B8 flow. DP18 captured flows are piped in 18 " RCP to DP18.1 before discharging into Pond B at DP25.

Basin B4 consists of approximately 0.88 acres and includes walks, drives, roofs and landscape areas. Flow from this basin $\left(\mathrm{Q}_{5}=2.5 \mathrm{cfs}\right.$ and $\left.\mathrm{Q}_{1 \mathrm{loo}}=5.1 \mathrm{cfs}\right)$ will be collected and conveyed in a 3.0' concrete pan that follows the centerline of Fountain Grass Grove, to DP16. At DP16, flow enters Type A curb and gutter and is conveyed to an on-grade Double Type 16 at DP18, where it combines with Basin B3 flow. Discussion of DP18 captured flow versus flow-by is presented in the Basin B3 description.

Basin B5 consists of approximately 0.60 acres and includes walks, drives, roofs and landscape areas. Flow from this basin $\left(\mathrm{Q}_{5}=1.4 \mathrm{cfs}\right.$ and $\left.\mathrm{Q}_{100}=3.1 \mathrm{cfs}\right)$ will be collected and conveyed in a 3.0 ' concrete pan that follows the centerline of Purple Fountain Point, to an on-grade Single Type 16 at DP19, where it combines with DP17 flow-by. Total flows at DP19 from Basin B5 and DP17 flow-by are
$\mathrm{Q}_{5}=1.7 \mathrm{cfs}$ and $\mathrm{Q}_{100}=4.6 \mathrm{cfs}$. In the 5-year event, 1.2 cfs is captured and 2.1 cfs is captured in the 100 -year event. DP19 flow-by of $\mathrm{Q}_{5}=0.5 \mathrm{cfs}$ and $\mathrm{Q}_{100}=2.5 \mathrm{cfs}$ continues in curb and gutter to DP24 where it combines with Basin B6 flow. DP19 captured flow is conveyed to DP19 and piped in 18" RCP to DP 24.1 before discharging into Pond B at DP25.

Basin B6 consists of approximately 0.08 acres and includes walks, drives and landscape areas. Flow from this basin $\left(\mathrm{Q}_{5}=0.3 \mathrm{cfs}\right.$ and $\left.\mathrm{Q}_{100}=0.6 \mathrm{cfs}\right)$ will be collected and conveyed in Type A curb and gutter in Blue Avena View to a sump Triple Type 16 at DP24. The total combined flow at DP24 from Basin B6 and DP19 flow-by is $\mathrm{Q}_{5}=0.8 \mathrm{cfs}$ and $\mathrm{Q}_{1 \mathrm{oo}}=3.0 \mathrm{cfs}$. All flow at DP24 is captured and piped in 30 " RCP to DP24.1 before discharging into Pond B at DP25. If the sump inlet at DP24 were to become clogged, flow would overtop the curb and discharge directly into Pond B.

Basin B7 consists of approximately 0.13 acres and includes walks, drives, and landscape areas. Flow from this basin $\left(\mathrm{Q}_{5}=0.5 \mathrm{cfs}\right.$ and $\left.\mathrm{Q}_{100}=1.0 \mathrm{cfs}\right)$ will be collected and conveyed in Type A curb and gutter in Blue Avena View to a sump Denver Double Type 16 at DP23. The total combined flow at DP23 from Basin B7, DP20, and DP21 flow-by is $\mathrm{Q}_{5}=3.3 \mathrm{cfs}$ and $\mathrm{Q}_{1 \mathrm{oo}}=8.3 \mathrm{cfs}$. All flow at DP23 is captured in the 5 -year event, however; in the 100 -year event 0.4 cfs is not captured and will overtop the street crown to the Triple Type 16 at DP24. Captured flows are piped to DP23.1 where it combines with flows from DP22.1 before discharging into Pond B at DP25.

Basin B8 consists of approximately 0.73 acres and includes walks, drives, roofs and landscape areas. Flow from this basin $\left(\mathrm{Q}_{5}=2.1 \mathrm{cfs}\right.$ and $\left.\mathrm{Q}_{100}=4.3 \mathrm{cfs}\right)$ will be collected and conveyed in a 3.0' concrete pan, that follows the centerline of Purple Fountain Point, to DP20. At DP20, flow enters Type A curb and gutter and combines with DP18 flow-by for a total flow of $\mathrm{Q}_{5}=2.6 \mathrm{cfs}$ and $\mathrm{Q}_{100}=6.4 \mathrm{cfs}$. The combined flow is conveyed to a sump Denver Double Type 16 at DP23, where it combines with Basin B7 and DP22 flow-by flow. Discussion of DP23 captured flow is presented in the Basin B7 description.

Basin B9 consists of approximately 0.54 acres and includes walks, drives, roofs and landscape areas. Flow from this basin $\left(\mathrm{Q}_{5}=1.5 \mathrm{cfs}\right.$ and $\left.\mathrm{Q}_{1 \mathrm{oo}}=3.1 \mathrm{cfs}\right)$ will be collected and conveyed in Type A curb and gutter in Foerster Grass View, to DP22. At DP22, flow is captured in a Denver Double Type 16 ( $\mathrm{Q}_{5}=1.4 \mathrm{cfs}$ and $\mathrm{Q}_{100}=2.3 \mathrm{cfs}$ ). DP21 flow-by $\left(\mathrm{Q}_{5}=0.1 \mathrm{cfs}\right.$ and $\mathrm{Q}_{1 \mathrm{oo}}=0.8 \mathrm{cfs}$ ) continues in Type A curb and gutter to DP23 where it combines with Basin B7 and DP20 flow. Discussion of DP23 captured flow is presented in the Basin B7 description.

Basin B10 consists of approximately 0.48 acres of landscaped areas and contains Full Spectrum Water Quality and Detention Pond B. Flow from this basin ( $\mathrm{Q}_{5}=0.2 \mathrm{cfs}$ and $\mathrm{Q}_{100}=1.5 \mathrm{cfs}$ ) sheet flows directly into Pond B where it combines with flow from Basins B1-B9 and B15. A detailed discussion of Full Spectrum Water Quality and Detention Pond B is presented in the Water Quality section later in this report.

Basin B11 consists of approximately 0.19 acres of landscaped areas and contains approximately 1,870 square feet of asphalt roadway. Flow from this basin $\left(\mathrm{Q}_{5}=0.5 \mathrm{cfs}\right.$ and $\left.\mathrm{Q}_{100}=1.2 \mathrm{cfs}\right)$ follows historic drainage patterns and sheet flows offsite, along the eastern site boundary, eventually flowing directly into the Tributary to Sand Creek - East Fork Reach No. 6.
Basin B12 consists of approximately 0.07 acres of landscaped areas and sidewalk. Due to topographical constraints and the degree of development therein, flow from this basin $\left(\mathrm{Q}_{5}=0.1 \mathrm{cfs}\right.$ and $\mathrm{Q}_{100}=0.3 \mathrm{cfs}$ ) will discharge directly into Constitution Avenue curb and gutter.

Basin B13 consists of approximately 0.23 acres of landscaped areas and sidewalk. Due to topographical constraints and the degree of development therein, flow from this basin $\left(\mathrm{Q}_{5}=0.3 \mathrm{cfs}\right.$ and $\mathrm{Q}_{100}=0.9 \mathrm{cfs}$ ) will discharge directly into Constitution Avenue curb and gutter.

Basin B14 consists of approximately 0.12 acres of landscaped areas and will remain undeveloped. Flow from this basin $\left(\mathrm{Q}_{5}=0.1 \mathrm{cfs}\right.$ and $\left.\mathrm{Q}_{100}=0.4 \mathrm{cfs}\right)$ follows historic drainage patterns and sheet flows easterly offsite to Tributary to Sand Creek - East Fork Reach No. 6.

Basin B15 consists of approximately 0.24 acres of landscaped areas and sidewalk. Flow from this basin ( $\mathrm{Q}_{5}=0.4 \mathrm{cfs}$ and $\mathrm{Q}_{100}=1.0 \mathrm{cfs}$ ) is conveyed in a grass-lined swale to a Type C Inlet at DP21. All Basin B15 flow is captured at DP21 and is piped in 18" RCP to DP22.1 ( $\mathrm{Q}_{5}=1.7$ cfs and $\mathrm{Q}_{100}=3.2$ cfs) where it combines with captured flows at DP22. Basin B15's ultimate outfall is Pond B at DP25.

Basin B16 consists of approximately 0.11 acres of landscaped areas and will remain undeveloped. Flow from this basin ( $\mathrm{Q}_{5}=0.1 \mathrm{cfs}$ and $\mathrm{Q}_{100}=0.4 \mathrm{cfs}$ ) is conveyed in a grass-lined swale onsite before discharging to the east. From here, the flow follows historic drainage patterns to the Tributary to Sand Creek - East Fork Reach No. 6.

## Drainage Design Criteria

## Development Criteria Reference

Storm drainage analysis and design criteria for this project were taken from the "City of Colorado Springs/El Paso County Drainage Criteria Manual" Volumes 1 and 2 (EPCDCM), dated October 12, 1994, the "Urban Storm Drainage Criteria Manual" Volumes 1 to 3 (USDCM) and Chapter 6 and Section 3.2.1 of Chapter 13 of the "Colorado Springs Drainage Criteria Manual" (CSDCM), dated May 2014, as adopted by El Paso County.

## Hydrologic Criteria

All hydrologic data was obtained from the "El Paso Drainage Criteria Manual" Volumes 1 and 2, and the "Urban Drainage and Flood Control District Urban Storm Drainage Criteria Manual" Volumes 1, 2, and 3. Onsite drainage improvements were designed based on the 5 year (minor) storm event and the 100 -year (major) storm event. Runoff was calculated using the Rational Method, and
rainfall intensities for the 5 -year and the 100-year storm return frequencies were obtained from Table 6-2 of the CSDCM. One hour point rainfall data for the storm events is identified in the chart below. Runoff coefficients were determined based on proposed land use and from data in Table 6-6 from the CSDCM. Time of concentrations were developed using equations from CSDCM. All runoff calculations and applicable charts and graphs are included in the Appendices.

Table 2-1-hr Point Rainfall Data

| Storm | Rainfall (in.) |
| :---: | :---: |
| 5-year | 1.50 |
| 100-year | 2.52 |

## Hydraulic Criteria

The Rational Method and USDCM's SF-2 and SF-3 forms were used to determine the runoff from the minor and major storms on the site, and the UDFCD UD-Detention v3.07 spreadsheet was utilized for evaluating proposed detention and water quality pond. Sump and on-grade inlets were sized using UDFCD UD-Inlet v2.07. Manning's equation was used to size the proposed pipes in this report and StormCAD will be used to model the proposed storm sewer system and to analyze the proposed HGL calculations for Construction Drawings.

## Drainage Facility Design

## Four Step Process to Minimize Adverse Impacts of Urbanization

In accordance with the El Paso County Drainage Criteria Manual Volume 2, this site has implemented the four step process to minimize adverse impacts of urbanization. The four step process includes reducing runoff volumes, treating the water quality capture volume (WQCV), stabilizing drainage ways, and implementing long-term source controls.

Step 1 - Reducing Runoff Volumes: The Urban Collection at Palmer Village development project consists of 50 duplex structures with open spaces and lawn areas interspersed within the development which helps disconnect impervious areas and reduce runoff volumes. Roof drains from the structures will discharge to lawn areas, where feasible, to allow for infiltration and runoff volume reduction.

Step 2 - Stabilize Drainageways: The site lies within the Sand Creek Drainage Basin. Basin and bridge fees will be paid at time of platting. These funds will be used on future projects within the basin to stabilize drainageways. The site does not discharge directly into the open drainageway of Sand Creek, therefore no downstream stabilization will be accomplished with this project.

Step 3 - Treat the WQCV: Water Quality treatment for this site is provided in two proposed full spectrum water quality detention ponds: Pond A and Pond B. The runoff from this site will be collected within inlets and conveyed to the proposed ponds via storm sewer. Upon entrance to the ponds, flows will be captured in a forebay designed to promote settlement of suspended solids. A
trickle channel is also incorporated into the ponds to minimize the amount of standing water. The outlet structure has been designed to detain the water quality capture volume (WQCV) for 40 hours, and the extended urban runoff volume (EURV) for 72 hours. All flows released from the ponds will be reduced to less than historic rates.

Step 4 - Consider Need for Industrial and Commercial BMPs: BMPs will be utilized to minimize off-site contaminants and to protect the downstream receiving waters. Site specific temporary source control BMPs that will be implemented include, but are not limited to, silt fencing placed around downstream areas of disturbance, construction vehicle tracking pads at the entrances, designated concrete truck washout basin, designated vehicle fueling areas, covered storage areas, spill containment and control, etc. The permanent erosion control BMPs include asphalt drives and parking, storm inlets and storm pipe, two full spectrum water quality and detention ponds, and permanent vegetation.

## Water Quality

The site is split by Hannah Ridge Drive, therefore; a full spectrum water quality and detention pond is provided on both sides. Basin A, located west of Hannah Ridge Drive, will discharge to Pond A, while the east side of Hannah Ridge Drive, Basin B, will discharge to Pond B. Both ponds have been designed per Section 13.3.2.1 of Resolution 15-042 of the El Paso County Drainage Criteria Manual.

Full Spectrum Water Quality and Detention Pond A is designed for a total contributing acreage of 5.80 acres at $48.4 \%$ impervious from Basins A1-A10. The total WQCV is 0.098 ac-ft, the excess urban runoff volume (EURV) is $0.223 \mathrm{ac}-\mathrm{ft}$, and the total required detention volume is $0.514 \mathrm{ac}-\mathrm{ft}$. The WQCV is released over 41 hours, the EURV is released over 72 hours, and the 100 -year volume is released over 86 hours. The 100-year discharge of 2.2 cfs is equal to $90 \%$ of predevelopment rates. A riprap spillway is provided that conveys the full undetained, peak 100-year flow of 25.3 cfs with a $1.0^{\prime}$ freeboard. The spillway has a crest length of $20^{\prime}$ and a total depth of $1.50^{\prime}$. Additionally, emergency overflow inlets are included below the emergency spillway to capture emergency flows. 12 " RCP connects overflow inlets to the next downstream manhole.

Pond A's outlet structure outfalls into an 18 " RCP, eventually upsizing to 24 " RCP , that flows along the site's southern property line before discharging into the existing double $10 \times 6$ ' RCBC located in the adjacent parcel, east of the eastern parcel. A drainage easement will be provided for both the onsite and offsite portions of this pond outfall. The ultimate discharge of the double $10^{\prime} \times 6$, RCBC is the "Tributary to Sand Creek - East Fork Reach No. 6". A drainage map including Pond A and its outfall has been presented in Appendix F. Due to the fact that there are no upstream regional detention facilities, an "emergency conditions" scenario was not analyzed for Pond A.

Pond B is designed for a total contributing acreage of 4.28 acres at $56.5 \%$ impervious from Basins B1-B10 \& B15. The total WQCV is $0.080 \mathrm{ac}-\mathrm{ft}$, the excess urban runoff volume (EURV) is $0.208 \mathrm{ac}-$ ft and the total required detention volume is $0.444 \mathrm{ac}-\mathrm{ft}$. The WQCV is released over 40 hours, the

EURV is released over 76 hours and the 100 -year volume is released over 95 hours. The 100 -year discharge of 1.7 cfs is equal to $90 \%$ of predevelopment rates. A riprap spillway is provided that conveys the full undetained, peak 100-year flow of 21.9 cfs with a $1.0^{\prime}$ freeboard. The spillway has a crest length of $20^{\prime}$ and a total depth of $1.50^{\prime}$. Additionally, emergency overflow inlets are included below the emergency spillway to capture emergency flows. 12 " RCP connects overflow inlets to the next downstream manhole.

The pond outfalls into an $18^{\prime \prime}$ RCP that flows easterly before discharging into the existing double $10^{\prime}$ x $6^{\prime}$ RCBC located in the adjacent parcel to the east. A drainage easement will be provided for both the onsite and offsite portions of this pond outfall. The ultimate discharge of the double 10 ' x $6^{\prime}$ RCBC is the" Tributary to Sand Creek - East Fork Reach No. 6". A drainage map including Pond B and it's outfall has been presented in Appendix F. Due to the fact that there are no upstream regional detention facilities, an "emergency conditions" scenario was not analyzed for Pond B.

## Erosion Control Plan

We respectfully request that the Erosion Control Plan and Cost Estimate be submitted in conjunction with the grading and erosion control plan and construction assurances posted prior to obtaining a grading permit. The PUDSP plan set includes a preliminary grading plan.

## Operation \& Maintenance

In order to ensure the function and effectiveness of the stormwater infrastructure, maintenance activities such as inspection, routine maintenance, restorative maintenance, rehabilitation and repair, are required. The property owner shall be responsible for the inspection, maintenance, rehabilitation and repair of stormwater and erosion control facilities located on the property unless another party accepts such responsibility in writing and responsibility is properly assigned through legal documentation. Access is provided from onsite facilities and easements for proposed infrastructure located offsite. We respectfully request that the Operation \& Maintenance Manual be submitted in conjunction with the construction documents, prior to obtaining a grading permit.

## Drainage and Bridge Fees

The site lies within the Sand Creek Drainage Basin. Anticipated drainage and bridge fees are presented below, based on Resolution No. 19-441, and will be paid at time of platting. Fees could change, and are dependent on the timing of the plat.

| 2020 DRAINAGE AND BRIDGE FEES - URBAN COLLECTION AT PALMER VILLAGE |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Impervious Acres | Drainage Fee <br> (Per Imp. Acre) | Bridge Fee <br> (Per Imp. Acre) | Urban Collection <br> at Palmer Village <br> Drainage Fee | Urban Collection at <br> Palmer Village <br> Bridge Fee |
| 5.67 | $\$ 19,698$ | $\$ 8,057$ | $\$ 111,688$ | $\$ 45,683$ |

## JR ENGINEERING

## Summary

The proposed Urban Collection at Palmer Village development drainage improvements, including storm sewer and two full spectrum water quality and detention ponds were designed to meet or exceed the El Paso County Drainage Criteria. The proposed development will not adversely affect the offsite drainageways or surrounding development. This report is in conformance and meets the latest El Paso County Storm Drainage Criteria requirements for this site.

## References

1. City of Colorado Springs Drainage Criteria Manual (Volumes I \& II), City of Colorado Springs, Colorado, Updated May, 2014.
2. Urban Storm Drainage Criteria Manual (Volumes 1, 2, and 3), Urban Drainage and Flood Control District, June 2001.
3. Sand Creek Drainage Basin Planning Study, prepared Kiowa Engineering Corporation, January, 1993.
4. Jessica Heights Filing No. 1 Final Drainage Report, prepared by M.V.E., Inc, April, 2005.
5. Hannah Ridge at Feathergrass Master Drainage Development Plan, prepared by M.V.E., Inc., November 15, 2007.

Appendix A
Vicinity Map, Soil Descriptions, FEMA Floodplain Map




## MAP LEGEND

| Area of Interest (AOI) | $\square$ | C |
| :---: | :---: | :---: |
| $\square$ Area of Interest (AOI) | $\square$ | C/D |
| Soils $\square$ |  |  |
| Soil Rating Polygons $\square$ |  |  |
| $\square \mathrm{A}$ | $\square$ | Not rated or not available |
| A/D | Water Fe | ures |
|  | $\sim$ | Streams and Canals |
| B |  |  |
|  | Transpo | tion |
| B/D | H+ | Rails |
| C | - | Interstate Highways |
| C/D | - | US Routes |
| D | $\approx$ | Major Roads |
| Not rated or not available | $\cdots$ | Local Roads |
| Soil Rating Lines | Backgro |  |
| $\cdots$ A |  | Aerial Photography |
| $\cdots$ A/D |  |  |
| $\cdots$ |  |  |
| $\cdots$ B/D |  |  |
| $\cdots \mathrm{C}$ |  |  |
| $\cdots \mathrm{C} / \mathrm{D}$ |  |  |
| $\cdots$ D |  |  |
| * Not rated or not available |  |  |
| Soil Rating Points |  |  |
| $\square \quad \mathrm{A}$ |  |  |
| $\square \quad \mathrm{A} / \mathrm{D}$ |  |  |
| $\square \quad \mathrm{B}$ |  |  |
| $\square \mathrm{B} / \mathrm{D}$ |  |  |

## MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24,000.

Warning: Soil Map may not be valid at this scale.
Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale

Please rely on the bar scale on each map sheet for map measurements

Source of Map: Natural Resources Conservation Service Web Soil Survey URL
Coordinate System: Web Mercator (EPSG:3857)
Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required
This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.
Soil Survey Area: El Paso County Area, Colorado
Survey Area Data: Version 17, Sep 13, 2019
Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Apr 15, 2011-Jun 17, 2014

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

## Hydrologic Soil Group

| Map unit symbol | Map unit name | Rating | Acres in AOI | Percent of AOI |
| :--- | :---: | :---: | ---: | ---: |
| 8 | Blakeland loamy sand, 1 <br> to 9 percent slopes | A | 11.3 | $100.0 \%$ |
| Totals for Area of Interest | $\mathbf{1 1 . 3}$ | $\mathbf{1 0 0 . 0 \%}$ |  |  |

## Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

## Rating Options

Aggregation Method: Dominant Condition
Component Percent Cutoff: None Specified

Tie-break Rule: Higher

# Appendix B Hydrologic Calculations 

## PALMER VILLAGE - EXISTING DRAINAGE SUM MARY

| EXISTING BASIN SUMM ARY TABLE |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Tributary <br> Sub-basin | Area <br> (acres) | Percent <br> Impervious | $\mathbf{c}_{\mathbf{5}}$ | $\mathbf{c}_{100}$ | $\mathbf{t}_{\mathbf{c}}$ <br> (min) | $\mathbf{Q}_{\mathbf{5}}$ <br> (cfs) | $\mathbf{Q}_{\mathbf{1 0 0}}$ <br> (cfs) |  |
|  |  |  |  |  |  |  |  |  |
| EX1 | 0.15 | $2 \%$ | 0.08 | 0.35 | 7.9 | 0.04 | 0.4 |  |
| EX2 | 0.46 | $2 \%$ | 0.08 | 0.35 | 8.1 | 0.2 | 1.2 |  |
| EX3 | 4.27 | $2 \%$ | 0.08 | 0.35 | 14.2 | 1.2 | 9.0 |  |
| EX4 | 1.62 | $19 \%$ | 0.22 | 0.45 | 17.9 | 1.1 | 4.0 |  |
| EX5 | 0.37 | $82 \%$ | 0.75 | 0.85 | 5.0 | 1.4 | 2.7 |  |
| EX6 | 5.25 | $2 \%$ | 0.08 | 0.35 | 14.4 | 1.5 | 11.1 |  |


| EXISTING DESIGN POINT <br> SUM M ARY TABLE |  |  |  |
| :---: | :---: | :---: | :---: |
| DP | $\mathbf{Q}_{\mathbf{5}}$ | $\mathbf{Q}_{\mathbf{1 0 0}}$ |  |
| 1 | 0.04 | 0.4 |  |
| 2 | 0.2 | 1.2 |  |
| 3 | 1.3 | 9.3 |  |
| 4 | 1.3 | 4.9 |  |
| 5 | 1.4 | 2.7 |  |
| 6 | 1.5 | 11.1 |  |

'o IMPERVIOUS \& COM POSITE RUNOFF COEFFICIENT C.

| Subdivision: | PALMER VILAGE | PALMER VIUAGE |
| :--- | :--- | :--- |
| Location: | Colorado Springs | $2000-5149.01$ |
|  |  | $\frac{\text { RPD }}{}$ |
|  |  | $\frac{\mathrm{NQ}}{1 / 30 / 20}$ |
|  |  |  |


| Basin ID | Total Area (ac) | PAVED STREETS |  |  | UNDEVELOPED MEADOW |  |  | Basins Total Weighted \% Imp. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | \% Imp. | Area <br> (ac) | Weighted \% Imp. | \% Imp. | Area <br> (ac) | Weighted \% Imp. |  |
| EX1 | 0.15 | 100\% | 0.00 | 0.0\% | 2\% | 0.15 | 2.0\% | 2.0\% |
| EX2 | 0.46 | 100\% | 0.00 | 0.0\% | 2\% | 0.46 | 2.0\% | 2.0\% |
| EX3 | 4.27 | 100\% | 0.00 | 0.0\% | 2\% | 4.27 | 2.0\% | 2.0\% |
| EX4 | 1.62 | 100\% | 0.27 | 17.0\% | 2\% | 1.35 | 1.7\% | 18.6\% |
| EX5 | 0.37 | 100\% | 0.30 | 81.8\% | 2\% | 0.07 | 0.4\% | 82.1\% |
| EX6 | 5.25 | 100\% | 0.00 | 0.0\% | 2\% | 5.25 | 2.0\% | 2.0\% |
| TOTAL | 12.12 |  |  |  |  |  |  | 6.7\% |

Table 6-6. Runoff Coefficients for Rational Method
(Source: UDFCD 2001)

| Land Use or Surface Characteristics | $\begin{array}{\|c\|} \hline \text { Percent } \\ \text { Impervious } \end{array}$ | Runoff Coefficients |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 2 -year |  | 5 -year |  | 10-year |  | 25 -year |  | 50-year |  | 100 -year |  |
|  |  | HSG A8B | HSGC8D | HSG ARB | HSGC8D | HSG ARB | HSGC8D | HSG ARB | H5GC8D | HSG ARB | H5G C8, | HSG ARB | HS6 C8D |
| Business |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Commercial Areas | 95 | 0.79 | 0.80 | 0.81 | 0.82 | 0.83 | 0.84 | 0.85 | 0.87 | 0.87 | 0.88 | 0.88 | 0.89 |
| Neighborhood Areas | 70 | 0.45 | 0.49 | 0.49 | 0.53 | 0.53 | 0.57 | 0.58 | 0.62 | 0.60 | 0.65 | 0.62 | 0.68 |
| Residential |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1/8Acre orless | 65 | 0.41 | 0.45 | 0.45 | 0.49 | 0.49 | 0.54 | 0.54 | 0.59 | 0.57 | 0.62 | 0.59 | 0.65 |
| 1/4Acre | 40 | 0.23 | 0.28 | 0.30 | 0.35 | 0.36 | 0.42 | 0.42 | 0.50 | 0.46 | 0.54 | 0.50 | 0.58 |
| 1/3Acre | 30 | 0.18 | 0.22 | 0.25 | 0.30 | 0.32 | 0.38 | 0.39 | 0.47 | 0.43 | 0.52 | 0.47 | 0.57 |
| 1/2Acre | 25 | 0.15 | 0.20 | 0.22 | 0.28 | 0.30 | 0.36 | 0.37 | 0.46 | 0.41 | 0.51 | 0.46 | 0.56 |
| 1 Acre | 20 | 0.12 | 0.17 | 0.20 | 0.26 | 0.27 | 0.34 | 0.35 | 0.44 | 0.40 | 0.50 | 0.44 | 0.55 |
| Industrial |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lightareas | 80 | 0.57 | 0.60 | 0.59 | 0.63 | 0.63 | 0.66 | 0.66 | 0.70 | 0.68 | 0.72 | 0.70 | 0.74 |
| Heavy Areas | 90 | 0.71 | 0.73 | 0.73 | 0.75 | 0.75 | 0.77 | 0.78 | 0.80 | 0.80 | 0.82 | 0.81 | 0.83 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Parks and Cemeteries | 7 | 0.05 | 0.09 | 0.12 | 0.19 | 0.20 | 0.29 | 0.30 | 0.40 | 0.34 | 0.46 | 0.39 | 0.52 |
| Playgrounds | 13 | 0.07 | 0.13 | 0.16 | 0.23 | 0.24 | 0.31 | 0.32 | 0.42 | 0.37 | 0.48 | 0.41 | 0.54 |
| Railroad Yard Areas | 40 | 0.23 | 0.28 | 0.30 | 0.35 | 0.36 | 0.42 | 0.42 | 0.50 | 0.46 | 0.54 | 0.50 | 0.58 |
| Undeveloped Areas |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Historic Flow Analysis-Greenbelts, Agriculture | 2 | 0.03 | 0.05 | 0.09 | 0.16 | 0.17 | 0.26 | 0.26 | 0.38 | 0.31 | 0.45 | 0.36 | 0.51 |
| Pasture/Meadow | 0 | 0.02 | 0.04 | 0.08 | 0.15 | 0.15 | 0.25 | 0.25 | 0.37 | 0.30 | 0.44 | 0.35 | 0.50 |
| Forest | 0 | 0.02 | 0.04 | 0.08 | 0.15 | 0.15 | 0.25 | 0.25 | 0.37 | 0.30 | 0.44 | 0.35 | 0.50 |
| Exposed Rock | 100 | 0.89 | 0.89 | 0.90 | 0.90 | 0.92 | 0.92 | 0.94 | 0.94 | 0.95 | 0.95 | 0.96 | 0.96 |
| Offsite Flow Analysis (when landuse is undefined) | 45 | 0.26 | 0.31 | 0.32 | 0.37 | 0.38 | 0.44 | 0.44 | 0.51 | 0.48 | 0.55 | 0.51 | 0.59 |
| Streets |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Paved | 100 | 0.89 | 0.89 | 0.90 | 0.90 | 0.92 | 0.92 | 0.94 | 0.94 | 0.95 | 0.95 | 0.96 | 0.96 |
| Gravel | 80 | 0.57 | 0.60 | 0.59 | 0.63 | 0.63 | 0.66 | 0.66 | 0.70 | 0.68 | 0.72 | 0.70 | 0.74 |
| Drive and Walks | 100 | 0.89 | 0.89 | 0.90 | 0.90 | 0.92 | 0.92 | 0.94 | 0.94 | 0.95 | 0.95 | 0.96 | 0.96 |
| Roofs | 90 | 0.71 | 0.73 | 0.73 | 0.75 | 0.75 | 0.77 | 0.78 | 0.80 | 0.80 | 0.82 | 0.81 | 0.83 |
| Lawns | 0 | 0.02 | 0.04 | 0.08 | 0.15 | 0.15 | 0.25 | 0.25 | 0.37 | 0.30 | 0.44 | 0.35 | 0.50 |

Subdivision: PALMER VIШAGE
Location: Colorado Springs

Project Name: PALMERVIШAGE
Project No.: 2000-5149.01
Calculated By: RPD
Checked By: NQ
Date: 1/30/20

| Basin ID | Total Area (ac) | Basins Total Weighted \% Imp. | Hydrologic Soil Group |  |  | Land Use |  | M inor Coefficients |  | Major Coefficients |  | Basins Total Weighted $\mathrm{C}_{5}$ | Basins Total Weighted $\mathrm{C}_{100}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Area A (ac) | Area B (ac) | Area C/D (ac) | Area Paved <br> Streets (ac) | Area <br> Undeveloped Meadow (ac) | $\mathrm{C}_{5, \mathrm{~A}, \mathrm{PaVED} \text { Streets }}$ | $\mathrm{C}_{5, \mathrm{~A}, \text { UNDEVELOPED MEADOW }}$ | $\mathrm{C}_{100, \mathrm{~A}, \mathrm{PAVED} \text { STREETS }}$ | $\mathrm{C}_{100, \mathrm{~A}, \text { UNDEVELOPED Meadow }}$ |  |  |
| EX1 | 0.15 | 2.0\% | 0.15 | 0.00 | 0.00 | 0.00 | 0.15 | 0.90 | 0.08 | 0.96 | 0.35 | 0.08 | 0.35 |
| EX2 | 0.46 | 2.0\% | 0.46 | 0.00 | 0.00 | 0.00 | 0.46 | 0.90 | 0.08 | 0.96 | 0.35 | 0.08 | 0.35 |
| EX3 | 4.27 | 2.0\% | 4.27 | 0.00 | 0.00 | 0.00 | 4.27 | 0.90 | 0.08 | 0.96 | 0.35 | 0.08 | 0.35 |
| EX4 | 1.62 | 18.6\% | 1.62 | 0.00 | 0.00 | 0.27 | 1.35 | 0.90 | 0.08 | 0.96 | 0.35 | 0.22 | 0.45 |
| EX5 | 0.37 | 82.1\% | 0.37 | 0.00 | 0.00 | 0.30 | 0.07 | 0.90 | 0.08 | 0.96 | 0.35 | 0.75 | 0.85 |
| EX6 | 5.25 | 2.0\% | 5.25 | 0.00 | 0.00 | 0.00 | 5.25 | 0.90 | 0.08 | 0.96 | 0.35 | 0.08 | 0.35 |
| TOTAL | 12.12 | 6.7\% | 12.12 | 0.00 | 0.00 | 5\% | 95\% | --- | --- | --- | --- | 0.12 | 0.38 |

Table 6-6. Runoff Coefficients for Rational Method
(Source: UDFCD 2001)


## STANDARD FORM SF-2 TIME OF CONCENTRATION

Subdivision: PALMERVIШAGE
Location: Colorado Springs

Project Name: PALMERVILAGE
Project No.: 2000-5149.01
Calculated By: RPD
Checked By: NQJ
Date: 1/30/20

| SUB-BASIN |  |  |  |  |  | INITIAL/ OVERLAND |  |  | TRAVELTIME |  |  |  |  | tc CHECK |  |  | FINAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| DATA |  |  |  |  |  | $\left(\mathrm{T}_{\mathrm{i}}\right.$ ) |  |  | $\left(\mathrm{T}_{\mathrm{t}}\right)$ |  |  |  |  | (URBANIZED BASINS) |  |  |  |
| $\begin{gathered} \hline \text { BASIN } \\ \hline \end{gathered}$ | D.A. <br> (ac) | Hydrologic <br> Soils Group | Impervious <br> (\%) | C5 | $\mathrm{C}_{100}$ | L <br> (ft) | So <br> (\%) | $\begin{gathered} \mathbf{t}_{\mathbf{i}} \\ (\mathrm{min}) \\ \hline \end{gathered}$ | $\begin{aligned} & \mathbf{L}_{\mathbf{t}} \\ & \text { (ft) } \end{aligned}$ | $\begin{aligned} & \hline \mathbf{S}_{\mathrm{t}} \\ & (\%) \\ & \hline \end{aligned}$ | K | VEL (ft/s) | $\begin{gathered} \mathbf{t}_{\mathbf{t}} \\ (\min ) \\ \hline \end{gathered}$ | COMP. $\mathrm{t}_{\mathrm{c}}$ <br> (min) | TOTAL LENGTH (ft) | Urbanized $\mathbf{t}_{\mathbf{c}}$ $(\min )$ | $\begin{gathered} \mathbf{t}_{\mathbf{c}} \\ (\min ) \\ \hline \end{gathered}$ |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| EX1 | 0.15 | A | 2\% | 0.08 | 0.35 | 50 | 5.0\% | 7.7 | 26 | 5.0\% | 10.0 | 2.2 | 0.2 | 7.9 | 76.0 | 25.9 | 7.9 |
| EX2 | 0.46 | A | 2\% | 0.08 | 0.35 | 50 | 5.0\% | 7.7 | 56 | 5.0\% | 10.0 | 2.2 | 0.4 | 8.1 | 106.0 | 26.1 | 8.1 |
| EX3 | 4.27 | A | 2\% | 0.08 | 0.35 | 50 | 7.8\% | 6.6 | 471 | 1.1\% | 10.0 | 1.0 | 7.6 | 14.2 | 521.0 | 33.9 | 14.2 |
| EX4 | 1.62 | A | 19\% | 0.22 | 0.45 | 50 | 7.8\% | 5.7 | 643 | 0.8\% | 10.0 | 0.9 | 12.2 | 17.9 | 693.0 | 33.3 | 17.9 |
| EX5 | 0.37 | A | 82\% | 0.75 | 0.85 | 0 | /A | N/A | 189 | 0.5\% | 20.0 | 1.4 | 2.3 | 2.3 | 189.0 | 14.3 | 5.0 |
| EX6 | 5.25 | A | 2\% | 0.08 | 0.35 | 50 | 3.0\% | 9.1 | 550 | 3.0\% | 10.0 | 1.7 | 5.3 | 14.4 | 600.0 | 31.4 | 14.4 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

NOTES:

```
tc}=\mp@subsup{t}{i}{}+\mp@subsup{t}{t}{
Where:
    &= computed time of concentration (minutes)
    ti= overland (initial) flow time (minutes)
    t}=\mathrm{ channelized flow time (minutes)
    t}=\frac{\mp@subsup{L}{t}{}}{60K\sqrt{}{\mp@subsup{S}{o}{\prime}}}=\frac{\mp@subsup{L}{t}{}}{60\mp@subsup{V}{t}{}
Where:
    tr
    L
    lol
    N
```

Use a minimum $t_{c}$ value of 5 minutes for urbanized areas and a minimum $t_{c}$ value of 10 minutes for areas
that are not considered urban. Use minimum values even when calculations result in a lesser time of
concentration.

## STANDARD FORM SF-3

 STORM DRAINAGE SYSTEM DESIGN| Subdivision: PALM ER VILLAGE Location: Colorado Springs Design Storm: 5 -Year |  |  |  |  |  |  |  |  |  |  |  |  | ```Project Name: PALMER VILLAGE Project No.: 2000-5149. Calculated By: RPD Checked By: NQ Date: \(1 / 30 / 20\)``` |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| STREET |  | DIRECT RUNOFF |  |  |  |  |  |  | TOTAL RUNOFF |  |  |  | OVERLAND |  |  | PIPE |  |  | TRAVELTIME |  |  |  | REM ARKS |
|  |  | $\begin{aligned} & 0 \\ & =\frac{1}{0} \\ & \underline{0} \\ & \hline \end{aligned}$ | $\begin{aligned} & \frac{8}{4} \\ & \frac{8}{4} \end{aligned}$ |  | $\overline{\underline{\xi}}$ | $\begin{aligned} & \frac{y}{4} \\ & \mathbb{t} \\ & \hline \end{aligned}$ |  | $\begin{aligned} & \frac{\pi}{\hat{Z}} \\ & \hline 0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { T. } \\ & \underset{y}{\xi} \end{aligned}$ |  | $\begin{aligned} & \stackrel{\Sigma}{E} \\ & \stackrel{E}{E} \end{aligned}$ | $\begin{gathered} \frac{\hat{x}}{0} \\ \underline{0} \\ \hline \end{gathered}$ |  | $\begin{aligned} & \text { Øon } \\ & \underset{t}{t} \\ & \hline \end{aligned}$ | $\begin{array}{r} \text { 巳 } \\ \stackrel{0}{0} \\ \stackrel{0}{0} \\ \hline \end{array}$ | $\begin{gathered} \hat{8} \\ \frac{8}{0} 0_{0}^{2} \\ \hline \end{gathered}$ | $$ | $\begin{array}{\|c} \stackrel{\circ}{0} \\ \stackrel{0}{0} \\ \stackrel{0}{0} \\ \hline \end{array}$ |  | $\begin{array}{\|l} \mathbb{E} \\ \text { E5 } \\ \text { EI } \\ \hline \end{array}$ | $\begin{aligned} & \frac{\pi}{2} \\ & \stackrel{y}{c} \\ & \frac{0}{6} \\ & \frac{0}{0} \\ & \hline \end{aligned}$ | $\underset{\mathrm{s}}{\underset{\mathrm{~s}}{\mathrm{~g}}}$ |  |
|  | 1 | EX1 | 0.15 | 0.08 | 7.9 | 0.01 | 4.49 | 0.04 |  |  |  |  | 0.04 | 0.01 | 1.90 |  |  |  |  | 468 | 1.4 | 5.7 | BASIN EX1 FLOW AT DP1, OVERLAND FLOW TO DP3 |
|  | 2 | EX2 | 0.46 | 0.08 | 8.1 | 0.04 | 4.45 | 0.2 |  |  |  |  | 0.2 | 0.04 | 1.61 |  |  |  |  | 626 | 1.3 | 8.2 | BASIN EX2 FLOW AT DP2, OVERLAND FLOW TO DP4 |
|  |  | EX3 | 4.27 | 0.08 | 14.2 | 0.34 | 3.60 | 1.2 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | BASIN EX3 FLOW AT DP3 (LOCAL DEPRESSION) |
|  | 3 |  |  |  |  |  |  |  | 14.2 | 0.35 | 3.60 | 1.3 |  |  |  |  |  |  |  |  |  |  | COM BINED DP1 AND EX3 FLOW AT DP3 (LOCAL DEPRESSION) |
|  |  | EX4 | 1.62 | 0.22 | 17.9 | 0.35 | 3.26 | 1.1 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | BASIN EX4 FLOW AT DP4, FLOWS SOUTH ALONG C\&G |
|  | 4 |  |  |  |  |  |  |  | 17.9 | 0.39 | 3.26 | 1.3 |  |  |  |  |  |  |  |  |  |  | COM BINED DP2 AND EX4 FLOW AT DP4 |
|  | 5 | EX5 | 0.37 | 0.75 | 5.0 | 0.28 | 5.17 | 1.4 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | BASIN EX5 FLOW AT DP5, FLOWS EAST ALONG C\&G |
|  | 6 | EX6 | 5.25 | 0.08 | 14.4 | 0.42 | 3.59 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | BASIN EX6 FLOW AT DP6 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
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| DFF Equatios |
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| $\mathrm{I}=1.20 \mathrm{mman}(\mathrm{d} \mathrm{D}+7.583$ |
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| Nat veneme |
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Notes:
Street and Pipe C*A values are determined by $\mathrm{Q} / \mathrm{i}$ using the catchment's intensity value.

STANDARD FORM SF-3

## STORM DRAINAGE SYSTEM DESIGN

(RATIONAL M ETHOD PROCEDURE)


Notes:
Street and Pipe $C * A$ values are determined by Q/i using the catchment's intensity value.

PALRMER VILAGE - PROPOSED DRAINAGE SUMMARY

| BASIN 'A' SUM M ARY TABLE |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Tributary | Area | Percent |  |  | $\mathbf{t}_{\mathbf{c}}$ | $\mathbf{Q}_{\mathbf{5}}$ | $\mathbf{Q}_{100}$ |  |
| Sub-basin | (acres) | Impervious | $\mathbf{C}_{\mathbf{5}}$ | $\mathbf{C}_{100}$ | (min) | (cfs) | (cfs) |  |
| EX1 | 0.15 | $0 \%$ | 0.08 | 0.35 | 7.9 | 0.04 | 0.4 |  |
| EX2 | 0.46 | $0 \%$ | 0.08 | 0.35 | 8.1 | 0.2 | 1.2 |  |
| A1 | 0.74 | $63 \%$ | 0.56 | 0.70 | 6.4 | 2.0 | 4.2 |  |
| A2 | 0.17 | $71 \%$ | 0.66 | 0.78 | 7.4 | 0.5 | 1.0 |  |
| A3 | 0.11 | $64 \%$ | 0.60 | 0.74 | 6.1 | 0.3 | 0.7 |  |
| A4 | 0.72 | $65 \%$ | 0.58 | 0.71 | 5.9 | 2.0 | 4.2 |  |
| A5 | 0.77 | $51 \%$ | 0.47 | 0.63 | 7.2 | 1.7 | 3.8 |  |
| A6 | 0.26 | $83 \%$ | 0.74 | 0.84 | 7.9 | 0.9 | 1.6 |  |
| A7 | 0.54 | $54 \%$ | 0.50 | 0.66 | 6.8 | 1.3 | 2.8 |  |
| A8 | 0.70 | $47 \%$ | 0.44 | 0.61 | 7.8 | 1.4 | 3.2 |  |
| A9 | 0.72 | $60 \%$ | 0.56 | 0.70 | 8.0 | 1.8 | 3.8 |  |
| A10 | 0.46 | $4 \%$ | 0.12 | 0.38 | 9.5 | 0.2 | 1.2 |  |
| A11 | 0.29 | $28 \%$ | 0.33 | 0.61 | 11.0 | 0.4 | 1.2 |  |
| A12 | 0.14 | $36 \%$ | 0.37 | 0.57 | 8.0 | 0.2 | 0.6 |  |


| DESIGN POINT SUMMARY |  |  |
| :---: | :---: | :---: |
| TABLE |  |  |$|$| Design <br> Point | $\mathbf{Q}_{\mathbf{5}}$ (cfs) | $\mathbf{Q}_{100}$ (cfs) |
| :---: | :---: | :---: |
| EX1 | 0.04 | $\mathbf{0 . 2}$ |
| EX2 | 0.2 | $\mathbf{0 . 7}$ |
| 1 | 1.9 | 4.3 |
| 2 | 2.0 | 5.0 |
| 3 | 2.4 | 5.3 |
| 4 | 2.4 | 5.8 |
| 4.1 | 3.8 | 6.7 |
| 5 | 2.1 | 5.6 |
| 6 | 1.7 | 4.9 |
| 7 | 1.4 | 3.3 |
| 8 | 4.1 | 10.0 |
| 8.1 | 7.7 | 16.3 |
| 9 | 3.3 | 8.4 |
| 9.1 | 10.8 | 24.1 |
| 10 | 11.0 | 25.3 |


| BASIN 'B' SUM M ARY TABLE |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Tributary | Area | Percent |  |  | $\mathbf{t}_{\mathbf{c}}$ | $\mathbf{Q}_{\mathbf{5}}$ | $\mathbf{Q}_{100}$ |  |  |
| Sub-basin | (acres) | Impervious | $\mathbf{C}_{5}$ | $\mathbf{C}_{100}$ | (min) | (cfs) | (cfs) |  |  |
| B1 | 0.65 | $51 \%$ | 0.47 | 0.63 | 6.5 | 1.4 | 3.3 |  |  |
| B2 | 0.08 | $100 \%$ | 0.90 | 0.96 | 5.0 | 0.4 | 0.7 |  |  |
| B3 | 0.11 | $91 \%$ | 0.83 | 0.90 | 5.0 | 0.5 | 0.9 |  |  |
| B4 | 0.88 | $66 \%$ | 0.59 | 0.72 | 6.7 | 2.5 | 5.1 |  |  |
| B5 | 0.60 | $53 \%$ | 0.49 | 0.64 | 6.2 | 1.4 | 3.1 |  |  |
| B6 | 0.08 | $88 \%$ | 0.80 | 0.88 | 5.0 | 0.3 | 0.6 |  |  |
| B7 | 0.13 | $85 \%$ | 0.77 | 0.87 | 5.0 | 0.5 | 1.0 |  |  |
| B8 | 0.73 | $65 \%$ | 0.58 | 0.71 | 5.7 | 2.1 | 4.3 |  |  |
| B9 | 0.54 | $64 \%$ | 0.58 | 0.71 | 6.5 | 1.5 | 3.1 |  |  |
| B10 | 0.48 | $2 \%$ | 0.10 | 0.36 | 5.7 | 0.2 | 1.5 |  |  |
| B11 | 0.19 | $58 \%$ | 0.55 | 0.70 | 5.0 | 0.5 | 1.2 |  |  |
| B12 | 0.07 | $29 \%$ | 0.31 | 0.52 | 5.1 | 0.1 | 0.3 |  |  |
| B13 | 0.23 | $30 \%$ | 0.33 | 0.54 | 7.5 | 0.3 | 0.9 |  |  |
| B14 | 0.12 | $0 \%$ | 0.08 | 0.35 | 5.0 | 0.1 | 0.4 |  |  |
| B15 | 0.24 | $25 \%$ | 0.29 | 0.50 | 5.0 | 0.4 | 1.0 |  |  |
| B16 | 0.11 | $9 \%$ | 0.15 | 0.41 | 5.0 | 0.1 | 0.4 |  |  |


| DESIGN POINT SUMM ARY <br> TABLE |  |  |
| :---: | :---: | :---: |
| Design <br> Point | $\mathbf{Q}_{5}$ (cfs) | $\mathbf{Q}_{100}$ (cfs) |
| 15 | 1.4 | 3.3 |
| 16 | 2.5 | 5.1 |
| 17 | 1.7 | 3.8 |
| 18 | 2.8 | 5.6 |
| 18.1 | 3.4 | 5.5 |
| 19 | 1.7 | 4.6 |
| 20 | 2.6 | 6.4 |
| 21 | 0.4 | 1.0 |
| 22 | 1.5 | 3.1 |
| 22.1 | 1.7 | 3.2 |
| 23 | 3.3 | 8.3 |
| 23.1 | 8.1 | 16.0 |
| 24 | 0.8 | 3.0 |
| 24.1 | 9.9 | 20.7 |
| 25 | 10.1 | 21.9 |

Subdivision: PALMER VLAGE
Location: Colorado Springs

Project Name: PALMER VILAGE
Project No.: 2514901
Calculated By: NQ
Checked By:
Date: $\overline{2 / 6 / 20}$

| Basin ID | Total Area (ac) | Drives/Walks |  |  | Roofs |  |  | Lawns |  |  | Basins Total Weighted \% Imp. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | \% Imp. | Area (ac) | Weighted \% <br> Imp. | \% Imp. | Area (ac) | Weighted \% Imp. | \% Imp. | Area (ac) | $\begin{gathered} \hline \text { Weighted \% } \\ \text { Imp. } \end{gathered}$ |  |
| EX1 | 0.15 | 100\% | 0.00 | 0.0\% | 90\% | 0.00 | 0.0\% | 0\% | 0.15 | 0.0\% | 0.0\% |
| EX2 | 0.46 | 100\% | 0.00 | 0.0\% | 90\% | 0.00 | 0.0\% | 0\% | 0.46 | 0.0\% | 0.0\% |
| A1 | 0.74 | 100\% | 0.19 | 25.7\% | 90\% | 0.31 | 37.7\% | 0\% | 0.24 | 0.0\% | 63.4\% |
| A2 | 0.17 | 100\% | 0.12 | 70.6\% | 90\% | 0.00 | 0.0\% | \%\% | 0.05 | 0.0\% | 70.6\% |
| A3 | 0.11 | 100\% | 0.07 | 63.6\% | 90\% | 0.00 | 0.0\% | 0\% | 0.04 | 0.0\% | 63.6\% |
| A4 | 0.72 | 100\% | 0.19 | 26.4\% | 90\% | 0.31 | 38.8\% | 0\% | 0.22 | 0.0\% | 65.1\% |
| A5 | 0.77 | 100\% | 0.16 | 20.8\% | 90\% | 0.26 | 30.4\% | 0\% | 0.35 | 0.0\% | 51.2\% |
| A6 | 0.26 | 100\% | 0.17 | 65.4\% | 90\% | 0.05 | 17.3\% | 0\% | 0.04 | 0.0\% | 82.7\% |
| A7 | 0.54 | 100\% | 0.15 | 27.8\% | 90\% | 0.16 | 26.7\% | 0\% | 0.23 | 0.0\% | 54.4\% |
| A8 | 0.70 | 100\% | 0.14 | 20.0\% | 90\% | 0.21 | 27.0\% | \%\% | 0.35 | 0.0\% | 47.0\% |
| A9 | 0.72 | 100\% | 0.34 | 47.2\% | 90\% | 0.10 | 12.5\% | 0\% | 0.28 | 0.0\% | 59.7\% |
| A10 | 0.46 | 100\% | 0.02 | 4.3\% | 90\% | 0.00 | 0.0\% | 0\% | 0.44 | 0.0\% | 4.3\% |
| All | 0.29 | 100\% | 0.08 | 27.6\% | 90\% | 0.00 | 0.0\% | 0\% | 0.29 | 0.0\% | 27.6\% |
| A12 | 0.14 | 100\% | 0.05 | 35.7\% | 90\% | 0.00 | 0.0\% | \%\% | 0.09 | 0.0\% | 35.7\% |
|  |  |  |  |  |  |  |  |  |  |  |  |
| B1 | 0.65 | 100\% | 0.14 | 21.5\% | 90\% | 0.21 | 29.1\% | 0\% | 0.30 | 0.0\% | 50.6\% |
| B2 | 0.08 | 100\% | 0.08 | 100.0\% | 90\% | 0.00 | 0.0\% | 0\% | 0.00 | 0.0\% | 100.0\% |
| B3 | 0.11 | 100\% | 0.10 | 90.9\% | 90\% | 0.00 | 0.0\% | 0\% | 0.01 | 0.0\% | 90.9\% |
| B4 | 0.88 | 100\% | 0.31 | 35.2\% | 90\% | 0.30 | 30.7\% | 0\% | 0.27 | 0.0\% | 65.9\% |
| B5 | 0.60 | 100\% | 0.13 | 21.7\% | 90\% | 0.21 | 31.5\% | 0\% | 0.26 | 0.0\% | 53.2\% |
| B6 | 0.08 | 100\% | 0.07 | 87.5\% | 90\% | 0.00 | 0.0\% | 0\% | 0.01 | 0.0\% | 87.5\% |
| B7 | 0.13 | 100\% | 0.11 | 84.6\% | 90\% | 0.00 | 0.0\% | \%\% | 0.02 | 0.0\% | 84.6\% |
| B8 | 0.73 | 100\% | 0.19 | 26.0\% | 90\% | 0.32 | 39.5\% | 0\% | 0.22 | 0.0\% | 65.5\% |
| B9 | 0.54 | 100\% | 0.20 | 37.0\% | 90\% | 0.16 | 26.7\% | 0\% | 0.18 | 0.0\% | 63.7\% |
| B10 | 0.48 | 100\% | 0.01 | 2.1\% | 90\% | 0.00 | 0.0\% | 0\% | 0.47 | 0.0\% | 2.1\% |
| B11 | 0.19 | 100\% | 0.11 | 57.9\% | 90\% | 0.00 | 0.0\% | 0\% | 0.08 | 0.0\% | 57.9\% |
| B12 | 0.07 | 100\% | 0.02 | 28.6\% | 90\% | 0.00 | 0.0\% | 0\% | 0.05 | 0.0\% | 28.6\% |
| B13 | 0.23 | 100\% | 0.07 | 30.4\% | 90\% | 0.00 | 0.0\% | 0\% | 0.16 | 0.0\% | 30.4\% |
| B14 | 0.12 | 100\% | 0.00 | 0.0\% | 90\% | 0.00 | 0.0\% | 0\% | 0.12 | 0.0\% | 0.0\% |
| B15 | 0.24 | 100\% | 0.06 | 25.0\% | 90\% | 0.00 | 0.0\% | 0\% | 0.18 | 0.0\% | 25.0\% |
| B16 | 0.11 | 100\% | 0.01 | 9.1\% | 90\% | 0.00 | 0.0\% | 0\% | 0.10 | 0.0\% | 9.1\% |
|  |  |  |  |  |  |  |  |  |  |  |  |
| SITE TOTAL | 11.47 |  |  |  |  |  |  |  |  | SITE | 49.1\% |
| WEST POND | 5.80 |  |  |  |  |  |  |  |  | WEST POND | 48.4\% |
| EAST POND | 4.28 |  |  |  |  |  |  |  |  | EAST POND | 56.5\% |

Subdivision: PALMERVILAGE Location: Colorado Springs

Project Name: PALMERVILAGE
Project No.: 2514901
Calculated By: NQ
Checked By:
Date:

| Basin ID | Total Area (ac) | Basins Total Weighted \% Imp. | Hydrologic Soil Group |  |  | Land Use |  |  | Minor Coefficients |  |  | Major Coefficients |  |  | Basins Total <br> Weighted $\mathrm{C}_{5}$ | Basins Total Weighted $\mathrm{C}_{100}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Area A (ac) | Area B (ac) | Area C/D (ac) | Area <br>  <br> Drives <br> (ac) | $\left\lvert\, \begin{gathered} \text { Area } \\ \text { Roofs (ac) } \end{gathered}\right.$ | Area Lawns (ac) | $\mathrm{C}_{5, \mathrm{~A}, \mathrm{WaLKS} \text { \& dives }}$ | $\mathrm{C}_{5, \text { ARoofs }}$ | $\mathrm{C}_{5, \mathrm{a}, \mathrm{awns}}$ | $\mathrm{C}_{100, \mathrm{~A}, \text { walus } \& \text { drives }}$ | $\mathrm{C}_{\text {100,A,ROoFs }}$ | $\mathrm{C}_{100, \mathrm{a}, \mathrm{awns}}$ |  |  |
| EX1 | 0.15 | 0\% | 0.15 | 0.00 | 0.00 | 0.00 | 0.00 | 0.15 | 0.90 | 0.73 | 0.08 | 0.96 | 0.81 | 0.35 | 0.08 | 0.35 |
| EX2 | 0.46 | 0\% | 0.46 | 0.00 | 0.00 | 0.00 | 0.00 | 0.46 | 0.90 | 0.73 | 0.08 | 0.96 | 0.81 | 0.35 | 0.08 | 0.35 |
| A1 | 0.74 | 63\% | 0.74 | 0.00 | 0.00 | 0.19 | 0.31 | 0.24 | 0.90 | 0.73 | 0.08 | 0.96 | 0.81 | 0.35 | 0.56 | 0.70 |
| A2 | 0.17 | 71\% | 0.17 | 0.00 | 0.00 | 0.12 | 0.00 | 0.05 | 0.90 | 0.73 | 0.08 | 0.96 | 0.81 | 0.35 | 0.66 | 0.78 |
| A3 | 0.11 | 64\% | 0.11 | 0.00 | 0.00 | 0.07 | 0.00 | 0.04 | 0.90 | 0.73 | 0.08 | 0.96 | 0.81 | 0.35 | 0.60 | 0.74 |
| A4 | 0.72 | 65\% | 0.72 | 0.00 | 0.00 | 0.19 | 0.31 | 0.22 | 0.90 | 0.73 | 0.08 | 0.96 | 0.81 | 0.35 | 0.58 | 0.71 |
| A5 | 0.77 | 51\% | 0.77 | 0.00 | 0.00 | 0.16 | 0.26 | 0.35 | 0.90 | 0.73 | 0.08 | 0.96 | 0.81 | 0.35 | 0.47 | 0.63 |
| A6 | 0.26 | 83\% | 0.26 | 0.00 | 0.00 | 0.17 | 0.05 | 0.04 | 0.90 | 0.73 | 0.08 | 0.96 | 0.81 | 0.35 | 0.74 | 0.84 |
| A7 | 0.54 | 54\% | 0.54 | 0.00 | 0.00 | 0.15 | 0.16 | 0.23 | 0.90 | 0.73 | 0.08 | 0.96 | 0.81 | 0.35 | 0.50 | 0.66 |
| A8 | 0.70 | 47\% | 0.70 | 0.00 | 0.00 | 0.14 | 0.21 | 0.35 | 0.90 | 0.73 | 0.08 | 0.96 | 0.81 | 0.35 | 0.44 | 0.61 |
| A9 | 0.72 | 60\% | 0.72 | 0.00 | 0.00 | 0.34 | 0.10 | 0.28 | 0.90 | 0.73 | 0.08 | 0.96 | 0.81 | 0.35 | 0.56 | 0.70 |
| A10 | 0.46 | 4\% | 0.46 | 0.00 | 0.00 | 0.02 | 0.00 | 0.44 | 0.90 | 0.73 | 0.08 | 0.96 | 0.81 | 0.35 | 0.12 | 0.38 |
| A11 | 0.29 | 28\% | 0.29 | 0.00 | 0.00 | 0.08 | 0.00 | 0.29 | 0.90 | 0.73 | 0.08 | 0.96 | 0.81 | 0.35 | 0.33 | 0.61 |
| A12 | 0.14 | 36\% | 0.14 | 0.00 | 0.00 | 0.05 | 0.00 | 0.09 | 0.90 | 0.73 | 0.08 | 0.96 | 0.81 | 0.35 | 0.37 | 0.57 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| B1 | 0.65 | 51\% | 0.65 | 0.00 | 0.00 | 0.14 | 0.21 | 0.30 | 0.90 | 0.73 | 0.08 | 0.96 | 0.81 | 0.35 | 0.47 | 0.63 |
| B2 | 0.08 | 100\% | 0.08 | 0.00 | 0.00 | 0.08 | 0.00 | 0.00 | 0.90 | 0.73 | 0.08 | 0.96 | 0.81 | 0.35 | 0.90 | 0.96 |
| B3 | 0.11 | 91\% | 0.11 | 0.00 | 0.00 | 0.10 | 0.00 | 0.01 | 0.90 | 0.73 | 0.08 | 0.96 | 0.81 | 0.35 | 0.83 | 0.90 |
| B4 | 0.88 | 66\% | 0.88 | 0.00 | 0.00 | 0.31 | 0.30 | 0.27 | 0.90 | 0.73 | 0.08 | 0.96 | 0.81 | 0.35 | 0.59 | 0.72 |
| B5 | 0.60 | 53\% | 0.60 | 0.00 | 0.00 | 0.13 | 0.21 | 0.26 | 0.90 | 0.73 | 0.08 | 0.96 | 0.81 | 0.35 | 0.49 | 0.64 |
| B6 | 0.08 | 88\% | 0.08 | 0.00 | 0.00 | 0.07 | 0.00 | 0.01 | 0.90 | 0.73 | 0.08 | 0.96 | 0.81 | 0.35 | 0.80 | 0.88 |
| B7 | 0.13 | 85\% | 0.13 | 0.00 | 0.00 | 0.11 | 0.00 | 0.02 | 0.90 | 0.73 | 0.08 | 0.96 | 0.81 | 0.35 | 0.77 | 0.87 |
| B8 | 0.73 | 65\% | 0.73 | 0.00 | 0.00 | 0.19 | 0.32 | 0.22 | 0.90 | 0.73 | 0.08 | 0.96 | 0.81 | 0.35 | 0.58 | 0.71 |
| B9 | 0.54 | 64\% | 0.54 | 0.00 | 0.00 | 0.20 | 0.16 | 0.18 | 0.90 | 0.73 | 0.08 | 0.96 | 0.81 | 0.35 | 0.58 | 0.71 |
| B10 | 0.48 | 2\% | 0.48 | 0.00 | 0.00 | 0.01 | 0.00 | 0.47 | 0.90 | 0.73 | 0.08 | 0.96 | 0.81 | 0.35 | 0.10 | 0.36 |
| B11 | 0.19 | 58\% | 0.19 | 0.00 | 0.00 | 0.11 | 0.00 | 0.08 | 0.90 | 0.73 | 0.08 | 0.96 | 0.81 | 0.35 | 0.55 | 0.70 |
| B12 | 0.07 | 29\% | 0.07 | 0.00 | 0.00 | 0.02 | 0.00 | 0.05 | 0.90 | 0.73 | 0.08 | 0.96 | 0.81 | 0.35 | 0.31 | 0.52 |
| B13 | 0.23 | 30\% | 0.23 | 0.00 | 0.00 | 0.07 | 0.00 | 0.16 | 0.90 | 0.73 | 0.08 | 0.96 | 0.81 | 0.35 | 0.33 | 0.54 |
| B14 | 0.12 | 0\% | 0.12 | 0.00 | 0.00 | 0.00 | 0.00 | 0.12 | 0.90 | 0.73 | 0.08 | 0.96 | 0.81 | 0.35 | 0.08 | 0.35 |
| B15 | 0.24 | 25\% | 0.24 | 0.00 | 0.00 | 0.06 | 0.00 | 0.18 | 0.90 | 0.73 | 0.08 | 0.96 | 0.81 | 0.35 | 0.29 | 0.50 |
| B16 | 0.11 | 9\% | 0.11 | 0.00 | 0.00 | 0.01 | 0.00 | 0.10 | 0.90 | 0.73 | 0.08 | 0.96 | 0.81 | 0.35 | 0.15 | 0.41 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| TOTAL | 11.47 | 49.1\% | 11.47 | 0.00 | 0.00 | 3.29 | 2.60 | 5.66 | $\cdots$ | $\cdots$ | $\cdots$ | --- | $\cdots$ | $\cdots$ | 0.46 | 0.63 |

## TIME OF CONCENTRATION

Subdivision: PALMERVIUAGE
Location: Colorado Springs

| SUB-BASIN |  |  |  |  |  | INITIALIUVERLAND |  |  | TRAVELTIME |  |  |  |  | tc CHECK |  |  | FINAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| DATA |  |  |  |  |  | $\left(\mathrm{T}_{\mathrm{i}}\right)$ |  |  | ( $\mathrm{T}_{\mathrm{t}}$ ) |  |  |  |  | (URBANIZED BASINS) |  |  |  |
| $\begin{gathered} \hline \text { BASIN } \\ \text { ID } \\ \hline \hline \end{gathered}$ | $\begin{aligned} & \text { D.A. } \\ & \text { (ac) } \\ & \hline \end{aligned}$ | Hydrologic Soils Group <br> Soils Group | $\begin{array}{\|c\|} \hline \begin{array}{c} \text { Impervious } \\ (\%) \end{array} \\ \hline \end{array}$ | $\mathrm{C}_{5}$ | $\mathrm{C}_{100}$ | $\begin{gathered} \hline \mathbf{L} \\ (\mathrm{ft}) \end{gathered}$ | $\begin{aligned} & \begin{array}{l} \mathbf{S o}_{\mathbf{o}} \\ (\%) \end{array} \\ & \hline \end{aligned}$ | $\begin{gathered} \mathbf{t}_{\mathbf{i}} \\ (\min ) \end{gathered}$ | $\begin{gathered} \mathbf{c}_{\mathbf{t}} \\ \text { (ft) } \end{gathered}$ | $\begin{gathered} \mathbf{S}_{\mathbf{t}} \\ (\%) \\ \hline \end{gathered}$ | K | $\begin{aligned} & \text { VEL } \\ & (\mathrm{ft} / \mathrm{s}) \end{aligned}$ | $\begin{gathered} \mathbf{t}_{\mathbf{t}} \\ (\mathrm{min}) \end{gathered}$ | $\begin{array}{\|c\|} \hline{ }^{\text {COMP. } \mathbf{t}_{\mathrm{c}}} \\ (\mathrm{~min}) \end{array}$ | $\begin{array}{\|c\|} \hline \text { TOTAL } \\ \text { LENGTH (ft) } \\ \hline \end{array}$ | $\begin{gathered} \text { Urbanized } \mathbf{t}_{\mathbf{c}} \\ (\text { min }) \end{gathered}$ | $\begin{gathered} \mathbf{t}_{\mathbf{c}} \\ (\min ) \\ \hline \hline \end{gathered}$ |
| EX1 | 0.15 | A | 0\% | 0.08 | 0.35 | 50 | 5.0\% | 7.7 | 26 | 5.0\% | 10.0 | 2.2 | 0.2 | 7.9 | 76.0 | 26.2 | 7.9 |
| EX2 | 0.46 | A | 0\% | 0.08 | 0.35 | 50 | 5.0\% | 7.7 | 56 | 5.0\% | 10.0 | 2.2 | 0.4 | 8.1 | 106.0 | 26.5 | 8.1 |
| A1 | 0.74 | A | 63\% | 0.56 | 0.70 | 87 | 5.0\% | 5.3 | 155 | 1.4\% | 20.0 | 2.4 | 1.1 | 6.4 | 242.0 | 16.4 | 6. |
| A2 | 0.17 | A | 71\% | 0.66 | 0.78 | 87 | 2.0\% | 5.9 | 180 | 1.0\% | 20.0 | 2.0 | 1.5 | 7.4 | 267.0 | 15.6 | 7. |
| A3 | 0.11 | A | 64\% | 0.60 | 0.74 | 87 | 6.0\% | 4.6 | 180 | 1.0\% | 20.0 | 2.0 | 1.5 | 6.1 | 267.0 | 16.9 | 6.1 |
| A4 | 0.72 | A | 65\% | 0.58 | 0.71 | 87 | 6.0\% | 4.9 | 150 | 1.6\% | 20.0 | 2.5 | 1.0 | 5.9 | 237.0 | 16.0 | 5.9 |
| A5 | 0.77 | A | 51\% | 0.47 | 0.63 | 87 | 5.0\% | 6.2 | 150 | 1.6\% | 20.0 | 2.5 | 1.0 | 7.2 | 237.0 | 18.5 | 7.2 |
| A6 | 0.26 | A | 83\% | 0.74 | 0.84 | 99 | 1.0\% | 6.4 | 178 | 1.0\% | 20.0 | 2.0 | 1.5 | 7.9 | 277.0 | 13.4 | 7.9 |
| A7 | 0.54 | A | 54\% | 0.50 | 0.66 | 87 | 5.5\% | 5.8 | 153 | 1.6\% | 20.0 | 2.5 | 1.0 | 6.8 | 240.0 | 18.0 | 6.8 |
| A8 | 0.70 | A | 47\% | 0.44 | 0.61 | 90 | 4.5\% | 6.9 | 115 | 1.1\% | 20.0 | 2.1 | 0.9 | 7.8 | 205.0 | 19.2 | 7.8 |
| A9 | 0.72 | A | 60\% | 0.56 | 0.70 | 87 | 3.0\% | 6.4 | 200 | 1.0\% | 20.0 | 2.0 | 1.7 | 8.0 | 287.0 | 17.8 | 8.0 |
| A10 | 0.46 | A | 4\% | 0.12 | 0.38 | 50 | 15.0\% | 5.1 | 325 | 0.7\% | 15.0 | 1.3 | 4.3 | 9.5 | 375.0 | 32.0 | 9.5 |
| All | 0.29 | A | 28\% | 0.33 | 0.61 | 90 | 2.0\% | 10.5 | 55 | 1.0\% | 20.0 | 2.0 | 0.5 | 11.0 | 145.0 | 22.0 | 11.0 |
| A12 | 0.14 | A | 36\% | 0.37 | 0.57 | 20 | 2.0\% | 4.7 | 280 | 0.5\% | 20.0 | 1.4 | 3.3 | 8.0 | 300.0 | 24.6 | 8.0 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| B1 | 0.65 | A | 51\% | 0.47 | 0.63 | 97 | 8.0\% | 5.7 | 105 | 1.0\% | 20.0 | 2.0 | 0.9 | 6.5 | 202.0 | 18.5 | 6.5 |
| B2 | 0.08 | A | 100\% | 0.90 | 0.96 | 12 | 2.0\% | 1.0 | 182 | 2.3\% | 20.0 | 3.1 | 1.0 | 2.0 | 194.0 | 9.9 | 5.0 |
| B3 | 0.11 | A | 91\% | 0.83 | 0.90 | 12 | 2.0\% | 1.4 | 190 | 2.3\% | 20.0 | 3.0 | 1.0 | 2.4 | 202.0 | 11.5 | 5.0 |
| B4 | 0.88 | A | 66\% | 0.59 | 0.72 | 120 | 6.0\% | 5.6 | 183 | 2.0\% | 20.0 | 2.8 | 1.1 | 6.7 | 303.0 | 16.0 | 6.7 |
| B5 | 0.60 | A | 53\% | 0.49 | 0.64 | 97 | 8.0\% | 5.5 | 103 | 1.6\% | 20.0 | 2.5 | 0.7 | 6.2 | 200.0 | 17.8 | 6.2 |
| B6 | 0.08 | A | 88\% | 0.80 | 0.88 | 12 | 2.0\% | 1.5 | 160 | 2.5\% | 20.0 | 3.2 | 0.8 | 2.3 | 172.0 | 11.9 | 5.0 |
| B7 | 0.13 | A | 85\% | 0.77 | 0.87 | 12 | 2.0\% | 1.6 | 170 | 2.5\% | 20.0 | 3.2 | 0.9 | 2.5 | 182.0 | 12.5 | 5.0 |
| B8 | 0.73 | A | 65\% | 0.58 | 0.71 | 97 | 9.0\% | 4.5 | 145 | 1.0\% | 20.0 | 2.0 | 1.2 | 5.7 | 242.0 | 16.2 | 5.7 |
| B9 | 0.54 | A | 64\% | 0.58 | 0.71 | 87 | 5.0\% | 5.2 | 155 | 1.0\% | 20.0 | 2.0 | 1.3 | 6.5 | 242.0 | 16.6 | 6.5 |
| B10 | 0.48 | A | 2\% | 0.10 | 0.36 | 15 | 2.0\% | 5.6 | 40 | 33.0\% | 15.0 | 8.6 | 0.1 | 5.7 | 55.0 | 25.8 | 5.7 |
| B11 | 0.19 | A | 58\% | 0.55 | 0.70 | 20 | 2.0\% | 3.5 | 20 | 2.0\% | 20.0 | 2.8 | 0.1 | 3.6 | 40.0 | 16.3 | 5.0 |
| B12 | 0.07 | A | 29\% | 0.31 | 0.52 | 20 | 2.0\% | 5.0 | 19 | 2.5\% | 20.0 | 3.2 | 0.1 | 5.1 | 39.0 | 21.3 | 5.1 |
| B13 | 0.23 | A | 30\% | 0.33 | 0.54 | 20 | 2.0\% | 4.9 | 450 | 2.2\% | 20.0 | 3.0 | 2.5 | 7.5 | 470.0 | 24.6 | 7.5 |
| B14 | 0.12 | A | 0\% | 0.08 | 0.35 | 20 | 25.0\% | 2.8 | 35 | 25.0\% | 15.0 | 7.5 | 0.1 | 2.9 | 55.0 | 26.1 | 5.0 |
| B15 | 0.24 | A | 25\% | 0.29 | 0.50 | 15 | 10.0\% | 2.7 | 365 | 3.0\% | 15.0 | 2.6 | 2.3 | 5.0 | 380.0 | 24.6 | 5.0 |
| B16 | 0.11 | A | 9\% | 0.15 | 0.41 | 15 | 10.0\% | 3.1 | 150 | 1.5\% | 15.0 | 1.9 | 1.3 | 4.4 | 165.0 | 26.4 | 5.0 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

Project Name: PALMER VLAGE
Project No.: 2514901
Checked B
Date: $\overline{2 / 6 / 2}$
TRAVELTIME

| RAVEL |
| :---: |
| $\mathrm{T}_{\mathrm{t}}$ |
| K |



|  |  | DIRECT RUNOFF |  |  |  |  |  | Total RUNOFF |  |  | STREET |  | PIPE |  |  | TRAVELTIME |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| STREET | $\begin{array}{\|r} \frac{匕 匕}{2} \\ \frac{2}{9} \\ \frac{6}{8} \\ \hline \end{array}$ |  | $\begin{array}{\|l} \frac{g}{8} \\ \frac{8}{4} \\ \hline \end{array}$ |  | $$ |  |  | $\begin{array}{r} \hat{e} \\ \underline{\xi} \\ \hline \\ \hline \end{array}$ | $\begin{array}{\|} \text { g} \\ \text { t } \\ \hline \end{array}$ | $\begin{array}{\|c\|c} \bar{E} \\ \hline \end{array}$ | $\begin{aligned} & \frac{\pi}{6} \\ & \frac{y}{b} \\ & 0 \end{aligned}$ |  |  | $\begin{array}{r} \text { 哥 } \\ \text { B } \\ \hline \end{array}$ |  |  | E | REM ARKS |
|  | 15 | B1 | 0.65 | 0.47 | 6.5 | 0.30 | 4.76 |  |  |  |  | 0.302 .33 |  |  |  |  |  | BASIN E1 Flow＠PP15，CQG FLOW TO DP17 |
|  | 17 | B2 | 0.08 | 0.90 | 5.0 |  | 5.170 .4 |  | ． 40.37 | 4.58 | 0.3 | $\begin{array}{lll}0.06 & 2.3\end{array}$ |  | 0.31 | $5.0 \quad 18$ |  | 0.4 0.1 | DP17 FLOW－BY，C\＆G FLOW TO DP19 <br> BASIN B2 AND DP15 FLOW＠DP17，CAPTURED IN DBL．DENVER TYPE 16 COM BO INLET，PPIE TO DP18． 1 |
|  |  | в3 | 0.11 |  | 5.0 |  | $\begin{array}{lll}5.17 & 0.5\end{array}$ |  |  |  |  |  |  |  |  |  |  | BASIN B3 FLOW＠DP18（ROUTED IN SF2） |
|  | 16 | B4 |  |  |  |  | 4.74 |  |  |  | 2.5 | $\begin{array}{llll}0.52 & 2.3\end{array}$ |  |  |  | $185 \quad 3.1$ | 1.0 | BASN B4 LLOW＠DP16，C8G FLOW TO DP18 |
|  |  |  |  |  |  |  |  |  |  |  | 0.8 | $0.17 \quad 2.3$ |  |  |  | 75.30 | 0.4 | DP18 FLOW－BY，CQG F Low To DP20 |
|  | 18 |  |  |  |  |  |  |  | ． 70.61 | $1.53 \quad 2.8$ |  |  |  | 0.44 | 2.018 | 55.7 | 0.0 | BASIN B3 \＆DP16 FLOW＠DP18，CAPTURED BY DBL DENVER TPPE 16 COMBO INLET，PPPE TO DP18． 1 |
|  | 18.1 |  |  |  |  |  |  |  | ． 70.75 | $\begin{array}{llll}4.52 & 3.4\end{array}$ |  |  |  | 0.75 | 2.018 | $160 \quad 6.7$ | 0.4 | DP17 \＆DP18 CAPTURED FLOW，PIPE FLOW TO DP22．1 |
|  | 19 | B5 | 0.60 | 0.49 | 6.2 | 0.29 | 4.85 |  | 6． 0.35 | $\begin{array}{llll}4.85 & 1.7\end{array}$ | 0.5 | $\begin{array}{lll}0.11 & 2.5\end{array}$ |  | 0.25 | $2.0 \quad 18$ | $\begin{aligned} & 103.2 \\ & 103 \\ & 10.0 \\ & 5.0 \end{aligned}$ | 0.5 0.3 | DP19 FLOW－BY．C\＆G FLOW TO DP23 <br> BASIN B5 \＆DP17 FLOW－BY＠DP19，CAPTURED IN SINGLE DENVER TYPE 16 COM BO INLET，PIPE TO DP23． 1 |
|  |  | B6 | 0.08 | 0.80 | 5.0 | 0.06 | $\begin{array}{llll}5.17 & 0.3\end{array}$ |  |  |  |  |  |  |  |  |  |  | BASIN B6 FLOW AT DP23（ROUTEDIN SF2） |
|  |  | B7 | 0.13 | 0.77 | 5.0 | 0.10 | $5.17 \quad 0.5$ |  |  |  |  |  |  |  |  |  |  | BASIN B7 Llow at dp22（ROUTEDIN SF2） |
|  | 20 | B8 | 0.73 | 0.58 | 5.7 | 0.42 | $4.97 \quad 2.1$ | ． 18.1 | 8.10 .59 | $4.45 \quad 2.6$ | 2.6 | $\begin{array}{lll}0.59 & 2.5\end{array}$ |  |  |  | $125 \quad 3.2$ | 0.7 | BASIN B8 \＆DP18 8 LLW－BY＠DP20，C\＆G FLOW TO DP22 |
|  | 21 | B15 | 0.24 | 0.29 | 5.0 | 0.07 | $\begin{array}{llll}5.17 & 0.4\end{array}$ |  |  |  |  |  |  | 0.07 | 1.018 | $145 \quad 2.6$ | 0.9 | BASIN B15 FLLW＠DP21，CAPTURED IN TYPE CIILET，PPPEDTO DP22．1 |
|  | 22 | B9 | 0.54 | 0.58 | 6.5 | 0.31 | $4.78 \quad 1.5$ |  |  |  |  | 0.02 |  | 0.29 | $2.0 \quad 18$ | $\begin{array}{ll} 65 & 2.0 \\ 45 & 5.1 \\ \hline \end{array}$ |  | DP22 FLOW－BY C\＆G FLOW TO DP23 <br> BASIN B9 FLOW CAPTURED BY DBL DENVER TYPE 16 COMBO INLET，PIPE TO DP22．1 |
|  | 22.1 |  |  |  |  |  |  |  | 6.60 .36 | 4.75 |  |  |  | 0.36 | 2.018 | $25 \quad 5.5$ | 0.1 | COM BINED DP21 \＆DP22 CAPTURED FLOW，PIPE TO DP23．1 |
|  | 23 |  |  |  |  |  |  |  | ． 00.71 | $\begin{array}{llll}4.66 & 3.3\end{array}$ |  |  |  | 0.71 | $5.0 \quad 18$ | $33 \quad 9.3$ | 0.1 | BASIN B7，DP20 FLOw－BY \＆DP22 FLOW－BY＠DP23，CAPTURED IN DBL Denver TYPE 16 COMBO ILLET，PPEETO DP23．1 |
|  | 23.1 |  |  |  |  |  |  |  | ${ }^{1} 1.818$ | $\begin{array}{llllll}4.45 & 8.1\end{array}$ |  |  |  | 1.82 | 3.024 | 339.7 | 0.1 | DP23 CAPTURED FLOW \＆DP22．11 LLOW，PIPE TO DP24．1 |
|  | 24 |  |  |  |  |  |  |  | 6．7 0.17 | 4.720 .8 |  |  |  | 0.17 | $5.0 \quad 24$ | 55.6 | 0.0 | BASIN B6 \＆DP19 FLOW－BY＠DP24，CAPTURED IN TRIPLE denver Tree 16 COM Bo inlet，Plpe To dP24．1 |
|  | 24.1 |  |  |  |  |  |  |  | 3.12 .23 |  |  |  | 9.9 | 2.23 | 5.030 | 5512.1 | 0.1 | COMBIIEED DP23．1\＆DP24 LLOW，PPIETO DP25 |
|  | 25 | 810 | 0.48 | 0.10 | 5.7 | 0.05 | 4.98 | ． 2.8 | 3．2 2.28 | 284.4210 .1 |  |  |  |  |  |  |  | DP24．1 AND BASIN B10 FLOW，TOTAL FLLW＠DP25（FSD WATER QUALITY POND） |
|  |  | B11 | 0.19 | 0.55 | 5.0 | 0.11 | $\begin{array}{llll}5.17 & 0.6\end{array}$ |  |  |  |  |  |  |  |  |  |  | BASIN B11 FLOW，FOLOW EX PATITRNS \＆FLOWS EAST OFF STE |
|  |  | B12 |  | 0.31 |  |  | $\begin{array}{ll}5.13 & 0.1\end{array}$ |  |  |  |  |  |  |  |  |  |  | BASIN B12 FLOW，Follow Ex Patterns \＆FLows north To Constitution avenue |
|  |  | B13 | 0.23 | 0.33 | 7.5 | 0.08 | 4.57 |  |  |  |  |  |  |  |  |  |  | BASIN B13 LLOW，FoLow Ex Patterns \＆flows north to constitution avenue |
|  |  | B14 | 0.12 | 0.08 | 5.0 | 0.01 | 5.170 .1 |  |  |  |  |  |  |  |  |  |  | BASIN B11 FLOW，FOLOW EXPATTERNS \＆FLOWS EAST OFF STE |
|  |  |  |  |  |  | 0.02 | $\begin{array}{lll}5.17 & 0.1\end{array}$ |  |  |  |  |  |  |  |  |  |  | BASIN B11 Llow，sWale convers flow Offsite East（fomows Hisoric patterns） |

Notes：
Street and Pipe C C＊A values are determined by $\mathrm{Q} / \mathrm{i}$ using the catchment＇s intensity value．

## STANDARD FORM SF－3

STORM DRAINAGE SYSTEM DESIGN
（atolat

## ：Palmervilage

Project Name：PALMER VILLAGE
joect Name：
Project No：：
2514901
251
Project No．：
Chectated By：
Che
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ced By：
Date：
$2 / 6 / 20$

|  |  | DIRECT RUNOFF |  |  |  |  |  |  | TOTAL RUNOFF |  |  |  | STREET |  |  | PIPE ${ }^{\text {a }}$ |  |  |  | TRAVELTIME |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TRE： |  |  | $\begin{aligned} & \dot{0} \\ & 8 \\ & 8 \\ & \hline \end{aligned}$ |  | $\underset{~ c}{\hat{\xi}}$ | $$ | $\stackrel{\substack{E}}{\stackrel{E}{s}}$ | $\begin{aligned} & \text { 會 } \\ & \hline \end{aligned}$ | $\begin{aligned} & \hat{y} \\ & \text { § } \\ & \hline \end{aligned}$ |  | $\begin{aligned} & \stackrel{E}{E} \\ & \underline{E} \end{aligned}$ | $\begin{gathered} \frac{\pi}{0} \\ 0 \\ \hline \end{gathered}$ |  | $$ |  | $\begin{array}{\|l\|} \frac{\tilde{x}}{8} \\ \frac{8}{2} \\ \hline 0 \end{array}$ |  | $\begin{aligned} & \text { £ } \\ & \vdots \\ & \stackrel{0}{\square} \\ & 0 \\ & \hline \end{aligned}$ |  |  | $\begin{aligned} & \widehat{0} \\ & 0 \\ & 0 \\ & 0 \\ & \frac{0}{y} \\ & \hline \end{aligned}$ | $$ | REM ARKS |
|  | Ex1 | Ex1 | 0.15 | 0.35 | 7.9 | 0.05 | 4.49 | 0.2 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | OFFSTEE BASIN EX1 FLOW＠DPEX1，FLOW INTO BASIN A1 |
|  | EX2 | EX2 | 0.46 | 0.35 | 8.1 | 0.16 | 4.45 | 0.7 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | BASIN EX2 FLOW＠DPEX2， |
|  | 1 | A1 | 0.74 | 0.70 |  | 0.52 | 8.06 | 4.2 |  | 90.57 | 77.54 | ． 4.3 | $3^{4.3}$ | 30.57 | 1.0 |  |  |  |  | 170 | 2.0 | 1.4 | BASIN A1\＆DPEX1 FLOW＠DP1，C\＆G FLOW TO DP3 |
|  |  | A2 | 0.17 | 0.78 | 7.4 | 0.13 | 7.69 | 1.0 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | BASIN A2 FLOW＠DP3（ROUTED IN SF2） |
|  |  | A3 | 0.11 | 0.74 | 6.1 | 0.08 | 8.16 | 0.7 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | BASIN A3 FLOW＠DP4（ROUTEDIN SF2） |
|  | 2 | A4 | 0.72 | 0.71 | 5.9 | 0.51 | 8.27 | 4.2 | 8.1 | 10.67 | 77.47 | 5.0 |  |  | 1.0 |  |  |  |  | 170 | 2.0 | 1.4 | BASIN A4 \＆DPEX2 FLOW＠DP2，C\＆G TO DP4 |
|  | 3 |  |  |  |  |  |  |  | 7.8 | 80.70 | 7 7.55 | 5.5 | ${ }^{2.0}$ | 0.26 |  | 3.3 |  | 2.0 |  | 60 5 | $\begin{aligned} & 2.0 \\ & 6.8 \end{aligned}$ | 0.0 | DP3 FLOW－BY，C\＆G FLOW TO DP5 DP1 \＆BASIN A2 FLOW CAPTURED IN DBL．DENVER TYPE 16 COM BO INLET，PIPE TO DP4． 1 |
|  | 4 |  |  |  |  |  |  |  |  | 30.75 | 7 7.72 | .75 | ${ }^{2.3}$ | 30.3 |  | 3.5 |  | 2.0 |  | 60 31 | 2.0 2.0 6.8 | ［ 0.5 | PP4 LLOW－BY，c¢G FLow To DP6 |
|  | 4.1 |  |  |  |  |  |  |  |  | 80.89 | 97.55 | 6．7 |  |  |  | 6.7 |  |  |  | 123 | 8.2 |  | COMBIIED DP3 \＆DP4 CAPTURED FLOW，PIPE FLOW TO DP8． 1 |
|  | 5 | A5 | 0.77 | 0.63 | 7.2 | 0.49 | 7.75 | 3.8 | 8.3 | 30.75 | 57.40 | 4， 5.6 | ${ }^{5.6}$ | 60.75 |  |  |  |  |  | 115 | 2.0 | 1.0 | BASIN A5 \＆DP3 FLOW－BY＠DP5，C\＆G FLOW TO DP8 |
|  |  | A6 | 0.26 | 0.84 | 7.9 | 0.22 | 7.52 | 1.7 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | BASIN A6 FLOW＠DP8（ROUTED IN SF2） |
|  | 6 | A7 | 0.54 | 0.66 | 6.8 |  | 7.91 |  | 7.8 | 80.65 | 57.56 | 64.9 | 4.9 | 90.65 |  |  |  |  |  | 130 | 2.0 | 1.1 | BASIN A7 FLOW \＆DP4 FLOW－BY＠DP6，C\＆G FLOW TO DP9 |
|  | 6 | A8 |  |  |  |  |  | 2.8 |  | 8 0.65 |  |  |  | 30.43 |  |  |  |  |  | 100 | 2.0 | 0.8 | BASIN A8 LLOW＠DP7，C\＆G FLOW TO DP8 |
|  | 8 |  |  |  |  |  |  |  |  | 31.40 | 7.12 | 120．0 |  |  |  | 10.0 |  | 2.0 | 30 | 5 | 8.7 | 0.0 | BASIN A6，DP5 \＆DP7 FLOW＠DP8，CAPTURED BY DBL Denver thpe 16 COM BO InLet，PIPE FLOW TO DP9． 1 |
|  | 8.1 |  |  |  |  |  |  |  |  | 32.29 | 97.12 | 16.3 |  |  |  | 16.3 |  | 2.0 | 30 | 55 | 2.0 | 0.5 | DP4．1 1 DP8 FLOW＠DP8．1，PPPE FLOW To DP9． 1 |
|  | 9 | A9 | 0.72 | 0.70 | 8.0 | 0.51 | 7.49 | 3.8 | 8.9 | 91.16 | 67.23 | 8.4 |  |  |  | 8.4 |  | 2.0 | 30 |  | 8.3 | 0.0 | DP6 \＆BASIN A9 FLOW＠DP9，CAPTURED BY TPL DENVER TYPE 16 COM BO InLET，PIPE FLOW TO DP9． 1 |
|  | 9.1 |  |  |  |  |  |  |  |  | 73.45 | 57.00 | 24.1 |  |  |  |  |  | 5.0 | 30 | 55 | 15.7 | 0.1 | DP8． 1 \＆DP9 FLOW＠DP9．1，PIPE FLOW TO DP10（WATER QUALTY POND） |
|  | 10 | A10 | 0.46 | 0.38 | 9.5 | 0.17 | 7.07 | 1.2 | 9.8 | 83.62 | 26.98 | 25.3 |  |  |  |  |  |  |  |  |  |  | BASIN A1－10 FLOW＠DP10，TOTAL FLOW Entering water quautr pond |
|  |  | Al1 | 0.29 | 0.61 | 11.0 | 0.18 | 6.70 | 1.2 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | BASIN A11 FLOW，FOLLOWS HISTORIC DRAINAGE PATTERNS TO CONSTITUTION AVENUE |
|  |  | A12 | 0.14 | 0.57 | 8.0 | 0.08 | 7.50 | 0.6 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | BASIN A12 FLOW，FOLLOWS HISTORIC DRAINAGE PATTERNS TO CONSTITUTION AVENUE |

## STANDARD FORM SF－3

STORM DRAINAGE SYSTEM DESIGN
Project Name：PALMER VILAGE
Project No：．：$\frac{\text { PALMER }}{2514901}$
Prect
Calculated By：
Checked By

## PALMERVLAGE

Checked By：
Date：
2／6／20

|  |  | DIRECT RUNOFF |  |  |  |  |  |  | TOTAL RUNOFF |  |  |  | STREET |  |  | PIPE |  |  |  | TRAVELTIME |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TREE | $\begin{array}{\|l} \hline \frac{匕 匕}{\circ} \\ \frac{⿺}{6} \\ \frac{6}{8} \\ \hline \end{array}$ | $\begin{aligned} & \frac{0}{c} \\ & \bar{y} \\ & \hline \end{aligned}$ | $\begin{aligned} & \dot{0} \\ & \text { 区 } \\ & \hline 8 \\ & \hline \end{aligned}$ |  | $\begin{gathered} \hat{\mathrm{c}} \\ \substack{\xi \\ \hline} \end{gathered}$ | $\begin{aligned} & \text { 弟 } \\ & \underline{t} \\ & \hline ⿰ ⿺ 乚 一 匕 \end{aligned}$ | E | $\begin{gathered} \frac{\pi}{0} \\ 0 \\ \hline \end{gathered}$ | $\begin{aligned} & \hat{\xi} \\ & \text { 会 } \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { 苞 } \\ & \text { I } \\ & \hline \end{aligned}$ | E | $\begin{aligned} & \stackrel{y}{\mathrm{y}} \\ & 0 \end{aligned}$ |  |  | $\begin{aligned} & \stackrel{\circ}{0} \\ & \frac{0}{0} \\ & \stackrel{0}{0} \end{aligned}$ | $\begin{array}{\|l\|} \hline \frac{\tilde{x}}{8} \\ \frac{8}{2} \\ \hline \end{array}$ | $$ | $\begin{aligned} & \text { む } \\ & \stackrel{0}{0} \\ & \text { ö } \\ & \hline \end{aligned}$ |  |  | $\begin{aligned} & \frac{8}{2} \\ & 0 \\ & \frac{8}{8} \\ & \hline \end{aligned}$ | $\begin{aligned} & \hat{\hat{\xi}} \\ & \underline{\xi} \\ & \hline \end{aligned}$ | REM ARKS |
|  | 15 | B1 | 0.65 | 0.63 | 6.5 | 0.41 | 8.00 | 3.3 |  |  |  |  |  |  | 2.3 |  |  |  |  | 160 | 3.1 | 0.9 | BASII B1 FLOW＠DP15，C\＆G FLOW TO DP17 |
|  |  |  |  |  |  |  |  |  |  |  |  |  | 1.4 | 0.18 | 2.3 |  |  |  |  | 70 | 3.1 | 0.4 | DP17 FLOW－BY，C\＆G FLow To DP19 |
|  | 17 | B2 | 0.08 | 0.96 | 5.0 | 0.08 | 8.68 | 0.7 | 7.4 | 0.49 | 7.68 | 3.8 |  |  |  | 2.4 | 0.31 | 5.0 | 18 | 33 | 8.3 | 0.1 | BASIN B2 AND DP15 FLOW＠DP17，CAPTURED IN DBLL DENVER TYPE 16 COM BO INLET，PIPE TO DP18．1 |
|  |  | B3 | 0.11 | 0.90 | 5.0 | 0.10 | 8.68 | 0.9 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | BASIN B3 FLOW＠DP18（ROUTEDIN SF2） |
|  | 16 | B4 | 0.88 | 0.72 |  | 0.64 | 7.96 | 5.1 |  |  |  |  |  | 0.64 | 2.3 |  |  |  |  | 185 | 3.1 | 1.0 | BASIN B4 FLOW＠DP16，C\＆G FLOW To DP18 |
|  |  |  |  |  |  |  |  |  |  |  |  |  | 2.5 | 0.33 | 2.3 |  |  |  |  | 75 | 3.0 | 0.4 | DP18 FLOW－BY，C\＆G FLOW TO DP20 |
|  | 18 |  |  |  |  |  |  |  | 7.7 | 0.74 | 7.60 | 5.6 |  |  |  | 3.1 | 0.41 | 2.0 | 18 | 5 | 6.6 | 0.0 | BASIN B3 \＆DP16 FLOW＠DP18，CAPTURED BY DBL DENVER TYPE 16 COM BO ILLET，PIPE TO DP18．1 |
|  | 18.1 |  |  |  |  |  |  |  | 7.7 | 0.72 | 7.60 | 5.5 |  |  |  | 5.5 | 0.72 | 2.0 | 18 | 160 | 7.8 | 0.3 | DP17 \＆DP18 CAPTURED FLOW，PPIPE FLOW TO DP22．1 |
|  |  |  |  |  |  |  |  |  |  |  |  |  | 2.5 | 0.31 | 2.5 |  |  |  |  | 103 | 3.2 | 0.5 | DP19 FLOW－BY，C\＆G FLOW TO DP23 |
|  | 19 | ${ }^{6} 5$ | 0.60 | 0.64 | 6.2 | 0.39 | 8.14 | 3.2 | 6.2 | 0.57 | 8.14 | 4.6 |  |  |  | 2.1 | 0.26 | 2.0 | 18 | 103 | 5.8 | 0.3 | BASIN B5 \＆DP17 FLOW－BY＠DP19，CAPTURED IN SINGLE DENVER TYPE 16 COM BO INLET，PPIE TO DP23．1 |
|  |  | B6 | 0.08 | 0.88 | 5.0 | 0.07 | 8.68 | 0.6 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | BASIN B6 FLOW AT DP23（ROUTED IN SF2） |
|  |  | B7 | 0.13 | 0.87 | 5.0 | 0.11 | 8.68 | 1.0 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | BASIN B7 FLOW AT DP22（ROUTEDIN SF2） |
|  | 20 | B8 | 0.73 | 0.71 | 5.7 | 0.52 | 8.35 | 4.3 | 8.1 | 0.85 | 7.47 | 6.4 | 6.4 | 0.85 | 2.5 |  |  |  |  | 125 | 3.2 | 0.7 | BASIN B8 \＆DP18 FLOW－BY＠DP20，C\＆G FLOW TO DP22 |
|  | 21 | B15 | 0.24 | 0.50 | 5.0 | 0.12 | 8.68 | 1.0 |  |  |  |  |  |  |  | 1.0 | 0.12 | 1.0 | 18 | 145 | 3.8 | 0.6 | BASIN B15 FLOW＠DP21．CAPTURED IN TYPECIILET．PIPED TO DP22．1 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  | 0.09 |  |  |  |  |  | ${ }_{6}^{65}$ | 2.0 | 0.5 | DP22 LLOW－BY，C\＆GG LLOW TO DP23 |
|  | 22 | B9 | 0.54 | 0.71 | 6.5 | 0.38 | 8.03 | 3.1 |  |  |  |  |  |  |  | 2.3 | 0.29 | 2.0 | 18 | 45 | 6.1 | 0.1 | BASIN B9 FLOW CAPTURED BY DBL DENVER TTPE 16 COM Bo INLET，PIPE TO DP22．1 |
|  | 22.1 |  |  |  |  |  |  |  | 6.6 | 0.41 | 7.98 | 3.2 |  |  |  | 3.2 | 0.41 | 2.0 | 18 | 25 | 6.7 | 0.1 | COM BINED DP21 \＆DP22 CAPTURED FLOW，PIPE TO DP23．1 |
|  | 23 |  |  |  |  |  |  |  | 7.0 | 1.06 | 7.82 | 8.3 |  | 0.05 |  | 7.9 | 1.01 | 5.0 | 18 | 33 | 12.0 | 0.0 | DP23 FLOW BY，OVERTOP CROWN TO DP24 <br> BASIN B7，DP20 FLOW－BY \＆DP22 FLOW－BY＠DP23，CAPTURED IN DBL DENVER TYPE 16 COM BO INLET，PIPETO DP23．1 |
|  | 23.1 |  |  |  |  |  |  |  |  | 2.14 | 7.49 | 16.0 |  |  |  | 16.0 | 2.14 | 3.0 | 24 | 33 | 11.8 | 0.0 | DP23 CAPTURED FLOW \＆DP22．1 FLOW，PPPE TO DP24．1 |
|  | 24 |  |  |  |  |  |  |  |  | 0.38 | 7.93 | 3.0 |  |  |  | 3.0 | 0.38 | 5.0 | 24 | 5 | 8.5 |  | BASIN B6 \＆DP19 FLOW－BY＠DP24，CAPTURED IN TRIPLE DENVER TYPE 16 COM BO INLET，PPPE TO DP24． 1 |
|  | 24.1 |  |  |  |  |  |  |  |  | 2.77 | 7.47 | 20.7 |  |  |  | 20.7 |  | 5.0 | 30 | 55 | 15.1 | 0.1 | COM BIIED DP23．1 \＆DP24 FLOW，PIPE TO DP25 |
|  | 25 | B10 | 0.48 | 0.36 | 5.7 | 0.17 | 8.37 | 1.4 | 8.1 | 2.94 | 7.45 | 21.9 |  |  |  |  |  |  |  |  |  |  | DP24．1 AND BASIN B10 FLOW，TOTAL FLOW＠DP25（FSD WATER QUALTY POND） |
|  |  | B11 | 0.19 | 0.70 | 5.0 | 0.13 | 8.68 | 1.1 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | BASIN B11 FLOW，FOLOW EXPATTERNS \＆FLOWS EAST OFF S STE |
|  |  | B12 | 0.07 | 0.52 | 5.1 | 0.04 | 8.61 | 0.3 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | BAIIN B12 FLOW，FOLOW EXPATTERNS \＆FLOWS NORTH TO CONSTITUTION AVENUE |
|  |  | B13 | 0.23 | 0.54 | 7.5 | 0.12 | 7.67 | 0.9 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | BAIIN B13 FLOW，FOLLOW EXPATTERNS \＆FLOWS NORTH TO CONSTTUTION AVENUE |
|  |  | B14 |  | 0.35 |  | 0.04 |  | 0.3 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | BASIN B11 FLOW，FOLOW EXPATTERNS \＆FLOWS EAST OFF S STE |
|  |  |  | 0.11 | 0.41 | 5.0 |  |  | 0.3 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | BASIN B11 FLOW，SWALE CONVEYS FLOW OfFSITE EAST（FOЩ－WWS HISTORIC PATTERNS） |

Street and Pipe $C^{*} A$ values are determined by $Q / i$ using the catchment＇s intensity value．

## Appendix C Hydraulic Calculations

## Alley Street Capacity - 1\% CL - Allowable Spread - Edge of Pavement

| User-defined |  |
| :--- | :--- |
| Invert Elev (ft) | $=0.36$ |
| Slope (\%) | $=1.00$ |
| N-Value | $=0.016$ |
| Calculations |  |
| Compute by: | Known Q |
| Known Q (cfs) | $=6.00$ |

(Sta, EI, n)-(Sta, EI, n)...
( $0.00,1.00)-(8.00,0.60,0.016)-(20.00,0.36,0.016)-(32.00,0.60,0.016)-(40.00,1.00,0.016)$


## Alley Street Capacity - 1.55\% CL - Allowable Spread - Edge of Pavement

| User-defined |  |
| :--- | :--- |
| Invert Elev (ft) | $=0.36$ |
| Slope (\%) | $=1.55$ |
| N-Value | $=0.016$ |
| Calculations |  |
| Compute by: | Known Q |
| Known Q (cfs) | $=8.00$ |

(Sta, EI, n)-(Sta, EI, n)...
( $0.00,1.00)-(8.00,0.60,0.016)-(20.00,0.36,0.016)-(32.00,0.60,0.016)-(40.00,1.00,0.016)$


\section*{| Version 4.05 Released March 2017 |
| :--- |
| INLET MANAGEMENT |}


| INLET NAME | DP3 | DP4 | STREET CAPACITY @ DP4 | DP8 | DP9 | DP24 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Site Type (Urban or Rural) | URBAN | URBAN | URBAN | URBAN | URBAN | URBAN |
| Inlet Application (Street or Area) | STREET | STREET | STREET | STREET | STREET | STREET |
| Hydraulic Condition | On Grade | On Grade | On Grade | In Sump | In Sump | In Sump |
| Inlet Type | Denver No. 16 Combination | Denver No. 16 Combination |  | Denver No. 16 Combination | Denver No. 16 Combination | Denver No. 16 Combination |



| Minor Total Design Peak Flow, Q (cts) | 2.4 | 2.4 | 2.4 | 4.1 | 3.3 | 0.8 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Major Total Design Peak Flow, Q (cfs) | 5.3 | 5.8 | 5.8 | 10.0 | 8.4 | 3.0 |
| Minor Flow Bypassed Downstream, $Q_{\text {b }}$ (cfs) | 0.5 | 0.5 |  | N/A | N/A | N/A |
| Major Flow Bypassed Downstream, $Q_{0}$ (ctis) | 2.0 | 2.3 |  | N/A | N/A | N/A |
| Minor Storm (Calculated) Analysis of Flow Time |  |  |  |  |  |  |
| C | N/A | N/A | N/A | N/A | N/A | N/A |
| $\mathrm{C}_{5}$ | N/A | N/A | N/A | N/A | N/A | N/A |
| Overland Flow Velocity, Vi | N/A | N/A | N/A | N/A | N/A | N/A |
| Channel Flow Velocity, Vt | N/A | N/A | N/A | N/A | N/A | N/A |
| Overland Flow Time, Ti | N/A | N/A | N/A | N/A | N/A | N/A |
| Channel Travel Time, Tt | N/A | N/A | N/A | N/A | N/A | N/A |
| Calculated Time of Concentration, $\mathrm{T}_{\text {c }}$ | N/A | N/A | N/A | N/A | N/A | N/A |
| Regional $\mathrm{T}_{\text {c }}$ | N/A | N/A | N/A | N/A | N/A | N/A |
| Recommended $\mathrm{T}_{\text {c }}$ | N/A | N/A | N/A | N/A | N/A | N/A |
| $\mathrm{T}_{\mathrm{c}}$ selected by User | N/A | N/A | N/A | N/A | N/A | N/A |
| Design Rainfall Intensity, 1 | N/A | N/A | N/A | N/A | N/A | N/A |
| Calculated Local Peak Flow, $Q_{P}$ | N/A | N/A | N/A | N/A | N/A | N/A |
| Maior Storm (Calculated) Analysis of Flow Time |  |  |  |  |  |  |
| C | N/A | N/A | N/A | N/A | N/A | N/A |
| $\mathrm{C}_{5}$ | N/A | N/A | N/A | N/A | N/A | N/A |
| Overland Flow Velocity, Vi | N/A | N/A | N/A | N/A | N/A | N/A |
| Channel Flow Velocity, Vt | N/A | N/A | N/A | N/A | N/A | N/A |
| Overland Flow Time, Ti | N/A | N/A | N/A | N/A | N/A | N/A |
| Channel Travel Time, Tt | N/A | N/A | N/A | N/A | N/A | N/A |
| Calculated Time of Concentration, $\mathrm{T}_{\mathrm{c}}$ | N/A | N/A | N/A | N/A | N/A | N/A |
| Regional $\mathrm{T}_{\text {c }}$ | N/A | N/A | N/A | N/A | N/A | N/A |
| Recommended $\mathrm{T}_{\mathrm{c}}$ | N/A | N/A | N/A | N/A | N/A | N/A |
| $\mathrm{T}_{\mathrm{c}}$ selected by User | N/A | N/A | N/A | N/A | N/A | N/A |
| Design Rainfall Intensity, , | N/A | N/A | N/A | N/A | N/A | N/A |
| Calculated Local Peak Flow, $Q_{p}$ | N/A | N/A | N/A | N/A | N/A | N/A |



## Version 4.05 Released March 2017

## ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor \& Major Storm)



| Gutter Geometry (Enter data in the blue cells) |  |  | $\mathrm{ft}_{\mathrm{ft}}^{\mathrm{ft} / \mathrm{ft}}$ |  |
| :---: | :---: | :---: | :---: | :---: |
| Maximum Allowable Width for Spread Behind Curb <br> Side Slope Behind Curb (leave blank for no conveyance credit behind curb) Manning's Roughness Behind Curb (typically between 0.012 and 0.020 ) | $\mathrm{T}_{\text {BACK }}=$ | 7.5 |  |  |
|  | $\mathrm{S}_{\text {BACK }}=$ | 0.020 |  |  |
|  | $\mathrm{n}_{\text {BACK }}=$ | 0.018 |  |  |
| Height of Curb at Gutter Flow Line <br> Distance from Curb Face to Street Crown <br> Gutter Width <br> Street Transverse Slope <br> Gutter Cross Slope (typically 2 inches over 24 inches or $0.083 \mathrm{ft} / \mathrm{ft}$ ) <br> Street Longitudinal Slope - Enter 0 for sump condition <br> Manning's Roughness for Street Section (typically between 0.012 and 0.020 ) | $\mathrm{H}_{\text {CURB }}=$ | 6.00 | inchesftft$\mathrm{ft} / \mathrm{ft}$$\mathrm{ft} / \mathrm{ft}$$\mathrm{ft} / \mathrm{ft}$$\quad$Major Storm |  |
|  | $\mathrm{T}_{\text {CROWN }}=$ | 21.0 |  |  |
|  | $\mathrm{W}=$ | 2.00 |  |  |
|  | $\mathrm{S}_{\mathrm{x}}=$ | 0.020 |  |  |
|  | $\mathrm{S}_{\mathrm{w}}=$ | 0.083 |  |  |
|  | $\mathrm{S}_{\mathrm{O}}=$ | 0.010 |  |  |
|  | $\mathrm{n}_{\text {STREET }}=$ | 0.014 |  |  |
| Manning's Roughness for Street Section (typically between 0.012 and 0.020 ) |  | Minor Storm |  | ft <br> inches |
| Max. Allowable Spread for Minor \& Major Storm | $\mathrm{T}_{\text {MAX }}=$ | 12.0 | 21.0 |  |
| Max. Allowable Depth at Gutter Flowline for Minor \& Major Storm | $\mathrm{d}_{\text {MAX }}=$ | 4.4 | 7.0 |  |
| Allow Flow Depth at Street Crown (leave blank for no) |  | Г | $\Gamma$ | check $=$ yes |
| MINOR STORM Allowable Capacity is based on Spread Criterion |  | Minor Storm | Major Storm |  |
| MAJOR STORM Allowable Capacity is based on Spread Criterion | $\mathbf{Q}_{\text {allow }}=$ | 5.4 | 21.1 | fs |
| Minor storm max. allowable capacity GOOD - greater than the design flo Major storm max. allowable capacity GOOD - greater than the design flo | Manageme <br> Manageme |  |  |  |

## INLET ON A CONTINUOUS GRADE



| Design Information (Input) |  | MINOR | MAJOR | inches |
| :---: | :---: | :---: | :---: | :---: |
| Lly ${ }^{\text {Type of Inlet }}$ Local Depression (additional to continuous gutter depression 'a') | Type $=$ | Denver No. 16 Combination |  |  |
|  | $\mathrm{a}_{\text {LOCAL }}=$ | 2.0 | 2.0 |  |
| Total Number of Units in the Inlet (Grate or Curb Opening) | No = | 2 | 2 |  |
| Length of a Single Unit Inlet (Grate or Curb Opening) | $\mathrm{L}_{0}=$ | 3.00 | 3.00 |  |
| Width of a Unit Grate (cannot be greater than W, Gutter Width) | $\mathrm{W}_{\mathrm{o}}$ = | 1.73 | 1.73 |  |
| Clogging Factor for a Single Unit Grate (typical min. value $=0.5$ ) | $\mathrm{C}_{\mathrm{f}}-\mathrm{G}=$ | 0.50 | 0.50 |  |
| Clogging Factor for a Single Unit Curb Opening (typical min. value =0.1) | $\mathrm{C}_{\text {f }}-\mathrm{C}=$ | 0.10 | 0.10 |  |
| Street Hydraulics: OK - Q < Allowable Street Capacity' |  | MINOR | MAJOR |  |
| Total Inlet Interception Capacity | Q = | 1.9 | 3.3 | cfs |
| Total Inlet Carry-Over Flow (flow bypassing inlet) | $\mathrm{Q}_{\mathrm{b}}=$ | 0.5 | 2.0 | cfs |
| Capture Percentage $=\mathbf{Q}_{\mathbf{a}} / \mathbf{Q}_{0}=$ | $\mathrm{C} \%=$ | 81 | 62 | \% |

Version 4.05 Released March 2017
ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor \& Major Storm)



## INLET ON A CONTINUOUS GRADE



| Design Information (Input) |  | MINOR | MAJOR | inches |
| :---: | :---: | :---: | :---: | :---: |
| \|ly ${ }^{\text {Type of Inlet }}$ Local Depression (additional to continuous gutter depression 'a') | Type $=$ | Denver No. 16 Combination |  |  |
|  | $\mathrm{a}_{\text {LOCAL }}=$ | 2.0 | 2.0 |  |
| Total Number of Units in the Inlet (Grate or Curb Opening) | No = | 2 | 2 |  |
| Length of a Single Unit Inlet (Grate or Curb Opening) | $\mathrm{L}_{0}=$ | 3.00 | 3.00 |  |
| Width of a Unit Grate (cannot be greater than W, Gutter Width) | $\mathrm{W}_{\mathrm{o}}$ = | 1.73 | 1.73 |  |
| Clogging Factor for a Single Unit Grate (typical min. value $=0.5$ ) | $\mathrm{C}_{\mathrm{f}}-\mathrm{G}=$ | 0.50 | 0.50 |  |
| Clogging Factor for a Single Unit Curb Opening (typical min. value $=0.1$ ) | $\mathrm{C}_{\text {f }}-\mathrm{C}=$ | 0.10 | 0.10 |  |
| Street Hydraulics: WARNING: Q > ALLOWABLE Q FOR MAJOR STORM |  | MINOR | MAJOR |  |
| Total Inlet Interception Capacity | Q = | 1.9 | 3.5 | cfs |
| Total Inlet Carry-Over Flow (flow bypassing inlet) | $\mathrm{Q}_{\mathrm{b}}=$ | 0.5 | 2.3 | cfs |
| Capture Percentage $=\mathbf{Q}_{\mathbf{a}} / \mathbf{Q}_{0}=$ | $\mathrm{C} \%=$ | 81 | 61 | \% |

## Version 4.05 Released March 2017

## ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor \& Major Storm)



Gutter Geometry (Enter data in the blue cells)
Maximum Allowable Width for Spread Behind Curb
Side Slope Behind Curb (leave blank for no conveyance credit behind curb)
Manning's Roughness Behind Curb (typically between 0.012 and 0.020 )
Height of Curb at Gutter Flow Line
Distance from Curb Face to Street Crown
Gutter Width
Street Transverse Slope
Gutter Cross Slope (typically 2 inches over 24 inches or $0.083 \mathrm{ft} / \mathrm{ft}$ )
Street Longitudinal Slope - Enter 0 for sump condition
Manning's Roughness for Street Section (typically between 0.012 and 0.020 )

Max. Allowable Spread for Minor \& Major Storm
Max. Allowable Depth at Gutter Flowline for Minor \& Major Storm
Check boxes are not applicable in SUMP conditions




MINOR STORM Allowable Capacity is based on Depth Criterion MAJOR STORM Allowable Capacity is based on Depth Criterion

## INLET IN A SUMP OR SAG LOCATION

Version 4.05 Released March 2017


| Design Information (Input) |  | MINOR | MAJOR |  |
| :---: | :---: | :---: | :---: | :---: |
| Type of Inlet \| Denver No. 16 Combinatio | Type $=$ | Denver N | nbination |  |
| Local Depression (additional to continuous gutter depression 'a' from above) | $\mathrm{a}_{\text {iocal }}=$ | 2.00 | 2.00 | inches |
| Number of Unit Inlets (Grate or Curb Opening) | No = | 2 | 2 |  |
| Water Depth at Flowline (outside of local depression) | Ponding Depth $=$ | 6.0 | 8.0 | inches |
| Grate Information |  | MINOR | MAJOR | Override Depths |
| Length of a Unit Grate | $\mathrm{L}_{0}(\mathrm{G})=$ | 3.00 | 3.00 | feet |
| Width of a Unit Grate | $\mathrm{W}_{0}=$ | 1.73 | 1.73 | feet |
| Area Opening Ratio for a Grate (typical values 0.15-0.90) | $\mathrm{A}_{\text {ratio }}=$ | 0.31 | 0.31 |  |
| Clogging Factor for a Single Grate (typical value 0.50-0.70) | $\mathrm{C}_{\mathrm{f}}(\mathrm{G})=$ | 0.50 | 0.50 |  |
| Grate Weir Coefficient (typical value 2.15-3.60) | $\mathrm{C}_{\mathrm{w}}(\mathrm{G})=$ | 3.60 | 3.60 |  |
| Grate Orifice Coefficient (typical value 0.60-0.80) | $\mathrm{C}_{0}(\mathrm{G})=$ | 0.60 | 0.60 |  |
| Curb Opening Information |  | MINOR | MAJOR |  |
| Length of a Unit Curb Opening | $\mathrm{L}_{0}(\mathrm{C})=$ | 3.00 | 3.00 | feet |
| Height of Vertical Curb Opening in Inches | $\mathrm{H}_{\text {vert }}=$ | 6.50 | 6.50 | inches |
| Height of Curb Orifice Throat in Inches | $\mathrm{H}_{\text {trroat }}=$ | 5.25 | 5.25 | inches |
| Angle of Throat (see USDCM Figure ST-5) | Theta $=$ | 0.00 | 0.00 | degrees |
| Side Width for Depression Pan (typically the gutter width of 2 feet) | $\mathrm{W}_{\mathrm{p}}=$ | 2.00 | 2.00 | feet |
| Clogging Factor for a Single Curb Opening (typical value 0.10) | $\mathrm{C}_{\text {f }}(\mathrm{C})=$ | 0.10 | 0.10 |  |
| Curb Opening Weir Coefficient (typical value 2.3-3.7) | $\mathrm{C}_{\mathrm{w}}(\mathrm{C})=$ | 3.70 | 3.70 |  |
| Curb Opening Orifice Coefficient (typical value 0.60-0.70) | $\mathrm{C}_{0}(\mathrm{C})=$ | 0.66 | 0.66 |  |
| Low Head Performance Reduction (Calculated) |  | MINOR | MAJOR |  |
| Depth for Grate Midwidth | $\mathrm{d}_{\text {Grate }}=$ | 0.523 | 0.689 | ft |
| Depth for Curb Opening Weir Equation | $\mathrm{d}_{\text {curb }}=$ | 0.33 | 0.50 | ft |
| Combination Inlet Performance Reduction Factor for Long Inlets | $\mathrm{RF}_{\text {combination }}=$ | 0.71 | 0.94 |  |
| Curb Opening Performance Reduction Factor for Long Inlets | $\mathrm{RF}_{\text {curb }}=$ | 1.00 | 1.00 |  |
| Grated Inlet Performance Reduction Factor for Long Inlets | $\mathrm{RF}_{\text {Grate }}=$ | 0.71 | 0.94 |  |
|  |  | MINOR | MAJOR |  |
| Total Inlet Interception Capacity (assumes clogged condition) | $\mathrm{Q}_{\mathrm{a}}=$ | 6.2 | 12.8 | cfs |
| Lnlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK) | $Q_{\text {Peak ReQuired }}=$ | 4.1 | 10.0 | cfs |

## Version 4.05 Released March 2017

## ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor \& Major Storm)



Gutter Geometry (Enter data in the blue cells)
Maximum Allowable Width for Spread Behind Curb
Side Slope Behind Curb (leave blank for no conveyance credit behind curb)
Manning's Roughness Behind Curb (typically between 0.012 and 0.020 )
Height of Curb at Gutter Flow Line
Distance from Curb Face to Street Crown
Gutter Width
Street Transverse Slope
Gutter Cross Slope (typically 2 inches over 24 inches or $0.083 \mathrm{ft} / \mathrm{ft}$ )
Street Longitudinal Slope - Enter 0 for sump condition
Manning's Roughness for Street Section (typically between 0.012 and 0.020 )

Max. Allowable Spread for Minor \& Major Storm
Max. Allowable Depth at Gutter Flowline for Minor \& Major Storm
Check boxes are not applicable in SUMP conditions


| $\mathrm{H}_{\text {CURB }}=$ | 6.00 |
| :---: | :---: |
| $\mathrm{T}_{\text {CROWN }}=$ | 21.0 |
| W = | 2.00 |
| $\mathrm{S}_{\mathrm{x}}=$ | 0.020 |
| $\mathrm{S}_{\mathrm{w}}=$ | 0.083 |
| $\mathrm{S}_{\mathrm{O}}=$ | 0.000 |
| $\mathrm{n}_{\text {STREET }}=$ | 0.014 |



MINOR STORM Allowable Capacity is based on Depth Criterion MAJOR STORM Allowable Capacity is based on Depth Criterion

## INLET IN A SUMP OR SAG LOCATION

Version 4.05 Released March 2017


| Design Information (Input) |  | MINOR | MAJOR |  |
| :---: | :---: | :---: | :---: | :---: |
| Type of Inlet \| Denver No. 16 Combinatio | Type $=$ | Denver N | mbination |  |
| Local Depression (additional to continuous gutter depression 'a' from above) | $\mathrm{a}_{\text {iocal }}=$ | 2.00 | 2.00 | inches |
| Number of Unit Inlets (Grate or Curb Opening) | No = | 3 | 3 |  |
| Water Depth at Flowline (outside of local depression) | Ponding Depth $=$ | 6.0 | 6.6 | inches |
| Grate Information |  | MINOR | MAJOR | Override Depths |
| Length of a Unit Grate | $\mathrm{L}_{0}(\mathrm{G})=$ | 3.00 | 3.00 | feet |
| Width of a Unit Grate | $\mathrm{W}_{0}=$ | 1.73 | 1.73 | feet |
| Area Opening Ratio for a Grate (typical values 0.15-0.90) | $\mathrm{A}_{\text {ratio }}=$ | 0.31 | 0.31 |  |
| Clogging Factor for a Single Grate (typical value 0.50-0.70) | $\mathrm{C}_{\mathrm{f}}(\mathrm{G})=$ | 0.50 | 0.50 |  |
| Grate Weir Coefficient (typical value 2.15-3.60) | $\mathrm{C}_{\mathrm{w}}(\mathrm{G})=$ | 3.60 | 3.60 |  |
| Grate Orifice Coefficient (typical value 0.60-0.80) | $\mathrm{C}_{0}(\mathrm{G})=$ | 0.60 | 0.60 |  |
| Curb Opening Information |  | MINOR | MAJOR |  |
| Length of a Unit Curb Opening | $\mathrm{L}_{0}(\mathrm{C})=$ | 3.00 | 3.00 | feet |
| Height of Vertical Curb Opening in Inches | $\mathrm{H}_{\text {vert }}=$ | 6.50 | 6.50 | inches |
| Height of Curb Orifice Throat in Inches | $\mathrm{H}_{\text {trroat }}=$ | 5.25 | 5.25 | inches |
| Angle of Throat (see USDCM Figure ST-5) | Theta $=$ | 0.00 | 0.00 | degrees |
| Side Width for Depression Pan (typically the gutter width of 2 feet) | $\mathrm{W}_{\mathrm{p}}=$ | 2.00 | 2.00 | feet |
| Clogging Factor for a Single Curb Opening (typical value 0.10) | $\mathrm{C}_{\text {f }}(\mathrm{C})=$ | 0.10 | 0.10 |  |
| Curb Opening Weir Coefficient (typical value 2.3-3.7) | $\mathrm{C}_{\mathrm{w}}(\mathrm{C})=$ | 3.70 | 3.70 |  |
| Curb Opening Orifice Coefficient (typical value 0.60-0.70) | $\mathrm{C}_{0}(\mathrm{C})=$ | 0.66 | 0.66 |  |
| Low Head Performance Reduction (Calculated) |  | MINOR | MAJOR |  |
| Depth for Grate Midwidth | $\mathrm{d}_{\text {Grate }}=$ | 0.523 | 0.569 | ft |
| Depth for Curb Opening Weir Equation | $\mathrm{d}_{\text {curb }}=$ | 0.33 | 0.38 | ft |
| Combination Inlet Performance Reduction Factor for Long Inlets | $\mathrm{RF}_{\text {combination }}=$ | 0.57 | 0.62 |  |
| Curb Opening Performance Reduction Factor for Long Inlets | $\mathrm{RF}_{\text {curb }}=$ | 0.97 | 1.00 |  |
| Grated Inlet Performance Reduction Factor for Long Inlets | $\mathrm{RF}_{\text {Grate }}=$ | 0.57 | 0.62 |  |
|  |  | MINOR | MAJOR |  |
| Total Inlet Interception Capacity (assumes clogged condition) | $\mathrm{Q}_{\mathrm{a}}=$ | 7.6 | 9.6 | cfs |
| Lnlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK) | $Q_{\text {Peak ReQuired }}=$ | 3.3 | 8.4 | cfs |

Version 4.05 Released March 2017
ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor \& Major Storm)



## INLET ON A CONTINUOUS GRADE



| Design Information (Input) |  | MINOR | MAJOR | inches |
| :---: | :---: | :---: | :---: | :---: |
| \|ly ${ }^{\text {Type of Inlet }}$ Local Depression (additional to continuous gutter depression 'a') | Type = | Denver No. 16 Combination |  |  |
|  | $\mathrm{a}_{\text {LOCAL }}=$ | 2.0 | 2.0 |  |
| Total Number of Units in the Inlet (Grate or Curb Opening) | No = | 2 | 2 |  |
| Length of a Single Unit Inlet (Grate or Curb Opening) | $\mathrm{L}_{0}=$ | 3.00 | 3.00 |  |
| Width of a Unit Grate (cannot be greater than W, Gutter Width) | $\mathrm{W}_{\mathrm{o}}$ = | 1.73 | 1.73 |  |
| Clogging Factor for a Single Unit Grate (typical min. value $=0.5$ ) | $\mathrm{C}_{\mathrm{f}}-\mathrm{G}=$ | 0.50 | 0.50 |  |
| Clogging Factor for a Single Unit Curb Opening (typical min. value =0.1) | $\mathrm{C}_{\text {f }}-\mathrm{C}=$ | 0.10 | 0.10 |  |
| Street Hydraulics: OK - Q < Allowable Street Capacity' |  | MINOR | MAJOR |  |
| Total Inlet Interception Capacity | Q = | 1.4 | 2.4 | cfs |
| Total Inlet Carry-Over Flow (flow bypassing inlet) | $\mathrm{Q}_{\mathrm{b}}=$ | 0.3 | 1.4 | cfs |
| Capture Percentage $=\mathbf{Q}_{\mathbf{a}} / \mathbf{Q}_{0}=$ | $\mathrm{C} \%=$ | 84 | 64 | \% |

Version 4.05 Released March 2017
ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor \& Major Storm)


| Gutter Geometry (Enter data in the blue cells) |  |  | $f_{\mathrm{ft}}$ |  |
| :---: | :---: | :---: | :---: | :---: |
| Maximum Allowable Width for Spread Behind Curb | $\mathrm{T}_{\mathrm{BACK}}=$ | 5.0 |  |  |
| Side Slope Behind Curb (leave blank for no conveyance credit behind curb) | $\mathrm{S}_{\text {BACK }}=$ | 0.020 |  |  |
| Manning's Roughness Behind Curb (typically between 0.012 and 0.020) | $\mathrm{n}_{\text {BACK }}=$ | 0.018 |  |  |
| Height of Curb at Gutter Flow Line | $\mathrm{H}_{\text {CURB }}=$ | 6.00 | inches |  |
| Distance from Curb Face to Street Crown | $\mathrm{T}_{\text {CROWN }}=$ | 21.0 | ft |  |
| Gutter Width | $\mathrm{W}=$ | 2.00 | ft |  |
| Street Transverse Slope | $\mathrm{S}_{\mathrm{x}}=$ | 0.020 | $\mathrm{ft} / \mathrm{ft}$ |  |
| Gutter Cross Slope (typically 2 inches over 24 inches or $0.083 \mathrm{ft} / \mathrm{ft}$ ) | $\mathrm{S}_{\mathrm{w}}=$ | 0.083 | $\mathrm{ft} / \mathrm{ft}$ |  |
| Street Longitudinal Slope - Enter 0 for sump condition | $\mathrm{S}_{\mathrm{O}}=$ | 0.023 | $\mathrm{ft} / \mathrm{ft}$ |  |
| Manning's Roughness for Street Section (typically between 0.012 and 0.020) | $\mathrm{n}_{\text {STREET }}=$ | 0.014 |  |  |
|  |  | Minor Storm | Major Storm |  |
| Max. Allowable Spread for Minor \& Major Storm | $\mathrm{T}_{\text {max }}=$ | 21.0 | 21.0 | ft |
| Max. Allowable Depth at Gutter Flowline for Minor \& Major Storm | $\mathrm{d}_{\text {max }}=$ | 6.0 | 8.0 | inches |
| Allow Flow Depth at Street Crown (leave blank for no) |  | Г | Г | check = yes |
| MINOR STORM Allowable Capacity is based on Depth Criterion |  | Minor Storm | Major Storm |  |
| MAJOR STORM Allowable Capacity is based on Spread Criterion | $Q_{\text {allow }}=$ | 22.0 | 32.1 | cfs |
| Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management' Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management' |  |  |  |  |

## INLET ON A CONTINUOUS GRADE



| Design Information (Input) $\quad$ Denver No. 16 Combination | $\text { Type }=$ | MINOR | MAJOR | inches |
| :---: | :---: | :---: | :---: | :---: |
| Type of Inlet ${ }_{\text {\| }}$ Denver No. 16 Co |  | Denver No. 16 Combination |  |  |
| Local Depression (additional to continuous gutter depression 'a') | $a_{\text {LOCAL }}=$ | 2.0 | 2.0 |  |
| Total Number of Units in the Inlet (Grate or Curb Opening) | No = | 2 | 2 |  |
| Length of a Single Unit Inlet (Grate or Curb Opening) | $\mathrm{L}_{0}=$ | 3.00 | 3.00 |  |
| Width of a Unit Grate (cannot be greater than W, Gutter Width) | $\mathrm{W}_{\mathrm{o}}=$ | 1.73 | 1.73 |  |
| Clogging Factor for a Single Unit Grate (typical min. value $=0.5$ ) | $\mathrm{C}_{\mathrm{f}}-\mathrm{G}=$ | 0.50 | 0.50 |  |
| Clogging Factor for a Single Unit Curb Opening (typical min. value $=0.1$ ) | $\mathrm{C}_{\mathrm{t}}-\mathrm{C}=$ | 0.10 | 0.10 |  |
| Street Hydraulics: OK - - Allowable Street Capacity' |  | MINOR | MAJOR |  |
| Total Inlet Interception Capacity | $Q=$ | 2.0 | 3.1 | cfs |
| Total Inlet Carry-Over Flow (flow bypassing inlet) | $\mathrm{Q}_{\mathrm{b}}=$ | 0.8 | 2.5 | cfs |
| Capture Percentage $=\mathrm{Q}_{\mathrm{a}} / \mathrm{Q}_{0}=$ | $\mathrm{C} \%=$ | 72 | 55 | \% |

Version 4.05 Released March 2017
ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor \& Major Storm)



## INLET ON A CONTINUOUS GRADE



| Design Information (Input) $\quad$ Denver No. 16 Combination | Type = | MINOR MAJOR |  | inches |
| :---: | :---: | :---: | :---: | :---: |
| Type of Inlet Denver No.16 Combination - |  | Denver | mbination |  |
| Local Depression (additional to continuous gutter depression 'a') | $\mathrm{a}_{\text {LOCAL }}=$ | 2.0 | 2.0 |  |
| Total Number of Units in the Inlet (Grate or Curb Opening) | No = | 1 | 1 |  |
| Length of a Single Unit Inlet (Grate or Curb Opening) | $\mathrm{L}_{0}=$ | 3.00 | 3.00 |  |
| Width of a Unit Grate (cannot be greater than W, Gutter Width) | $\mathrm{W}_{\mathrm{o}}=$ | 1.73 | 1.73 |  |
| Clogging Factor for a Single Unit Grate (typical min. value $=0.5$ ) | $\mathrm{C}_{\text {t }}-\mathrm{G}=$ | 0.50 | 0.50 |  |
| Clogging Factor for a Single Unit Curb Opening (typical min. value $=0.1$ ) | $\mathrm{C}_{\mathrm{f}}-\mathrm{C}=$ | 0.10 | 0.10 |  |
| Street Hydraulics: OK - Q < Allowable Street Capacity' |  | MINOR | MAJOR |  |
| Total Inlet Interception Capacity | Q = | 1.2 | 2.1 | cfs |
| Total Inlet Carry-Over Flow (flow bypassing inlet) | $\mathrm{Q}_{\mathrm{b}}=$ | 0.5 | 2.5 | cfs |
| Capture Percentage $=\mathrm{Q}_{\mathrm{a}} / \mathrm{Q}_{0}=$ | $\mathrm{C} \%=$ | 70 | 46 | \% |

## Version 4.05 Released March 2017

## AREA INLET IN A SWALE



Analysis of Trapezoidal Grass-Lined Channel Using SCS Method
NRCS Vegetal Retardance (A, B, C, D, or E)
Manning's $n$ (Leave cell D16 blank to manually enter an $n$ value)
Channel Invert Slope
Bottom Width
Left Side Slope
Right Side Slope

| Check one of the following soil types: |  |  |
| :---: | :---: | :---: |
| Soil Type: | Max. Velocity $\left(\mathrm{V}_{\text {max }}\right)$ | Max Froude No. ( $\mathrm{F}_{\text {max }}$ ) |
| Non-Cohesive | 5.0 fps | 0.60 |
| Cohesive | 7.0 fps | 0.80 |
| Paved | N/A | N/A |

Max. Allowable Top Width of Channel for Minor \& Major Storm
Max. Allowable Water Depth in Channel for Minor \& Major Storm
A, B, C, D or



Water Depth in Channel Based On Design Peak Flow
Design Peak Flow
Water Depth


Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'
Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

## Version 4.05 Released March 2017

## AREA INLET IN A SWALE



Version 4.05 Released March 2017
ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor \& Major Storm)


| Gutter Geometry (Enter data in the blue cells) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Maximum Allowable Width for Spread Behind Curb | $\mathrm{T}_{\mathrm{BACK}}=$ | 5.0 | $\left\lvert\, \begin{aligned} & \mathrm{ft} \\ & \mathrm{ft} / \mathrm{ft} \end{aligned}\right.$ |  |
| Side Slope Behind Curb (leave blank for no conveyance credit behind curb) | $\mathrm{S}_{\text {BACK }}=$ | 0.020 |  |  |
| Manning's Roughness Behind Curb (typically between 0.012 and 0.020) | $\mathrm{n}_{\text {BACK }}=$ | 0.018 |  |  |
| Height of Curb at Gutter Flow Line | $\mathrm{H}_{\text {CURB }}=$ | 6.00 | inches |  |
| Distance from Curb Face to Street Crown | $\mathrm{T}_{\text {CROWN }}=$ | 12.0 |  |  |
| Gutter Width | W = | 2.00 | ft |  |
| Street Transverse Slope | $\mathrm{S}_{\mathrm{x}}=$ | 0.020 | $\mathrm{ft} / \mathrm{ft}$ |  |
| Gutter Cross Slope (typically 2 inches over 24 inches or $0.083 \mathrm{ft} / \mathrm{ft}$ ) | $\mathrm{S}_{\mathrm{w}}=$ | 0.083 | $\mathrm{ft} / \mathrm{tt}$ |  |
| Street Longitudinal Slope - Enter 0 for sump condition | $\mathrm{S}_{\mathrm{O}}=$ | 0.010 | $\mathrm{ft} / \mathrm{tt}$ |  |
| Manning's Roughness for Street Section (typically between 0.012 and 0.020) | $\mathrm{n}_{\text {STREET }}=$ | 0.014 |  |  |
|  |  | Minor Storm | Major Storm | ft |
| Max. Allowable Spread for Minor \& Major Storm | $\mathrm{T}_{\text {MAX }}=$ | 12.0 | 12.0 |  |
| Max. Allowable Depth at Gutter Flowline for Minor \& Major Storm | $\mathrm{d}_{\text {max }}=$ | 6.0 | 6.0 | inches |
| Allow Flow Depth at Street Crown (leave blank for no) |  | Г | Г | check $=$ yes |
| MINOR STORM Allowable Capacity is based on Spread Criterion |  | Minor Storm | Major Storm |  |
| MAJOR STORM Allowable Capacity is based on Spread Criterion | $Q_{\text {allow }}=$ | 5.4 | 5.4 | fs |
| Minor storm max. allowable capacity GOOD - greater than the design flow Major storm max. allowable capacity GOOD - greater than the design flow | Manageme Manageme |  |  |  |

## INLET ON A CONTINUOUS GRADE



| Design Information (Input) $\quad$ Denver No. 16 Combination | $\text { Type }=$ | MINOR | MAJOR | inches |
| :---: | :---: | :---: | :---: | :---: |
| Type of Inlet ${ }_{\text {\| }}$ Denver No. 16 Co |  | Denver No. 16 Combination |  |  |
| Local Depression (additional to continuous gutter depression 'a') | $a_{\text {LOCAL }}=$ | 2.0 | 2.0 |  |
| Total Number of Units in the Inlet (Grate or Curb Opening) | No = | 2 | 2 |  |
| Length of a Single Unit Inlet (Grate or Curb Opening) | $\mathrm{L}_{0}=$ | 3.00 | 3.00 |  |
| Width of a Unit Grate (cannot be greater than W, Gutter Width) | $\mathrm{W}_{\mathrm{o}}=$ | 1.73 | 1.73 |  |
| Clogging Factor for a Single Unit Grate (typical min. value $=0.5$ ) | $\mathrm{C}_{\mathrm{f}}-\mathrm{G}=$ | 0.50 | 0.50 |  |
| Clogging Factor for a Single Unit Curb Opening (typical min. value $=0.1$ ) | $\mathrm{C}_{\mathrm{t}}-\mathrm{C}=$ | 0.10 | 0.10 |  |
| Street Hydraulics: OK - - Allowable Street Capacity' |  | MINOR | MAJOR |  |
| Total Inlet Interception Capacity | $Q=$ | 1.4 | 2.3 | cfs |
| Total Inlet Carry-Over Flow (flow bypassing inlet) | $\mathrm{Q}_{\mathrm{b}}=$ | 0.1 | 0.8 | cfs |
| Capture Percentage $=\mathrm{Q}_{\mathrm{a}} / \mathrm{Q}_{0}=$ | $\mathrm{C} \%=$ | 92 | 75 | \% |

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## ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor \& Major Storm)



Gutter Geometry (Enter data in the blue cells)
Maximum Allowable Width for Spread Behind Curb
Side Slope Behind Curb (leave blank for no conveyance credit behind curb)
Manning's Roughness Behind Curb (typically between 0.012 and 0.020 )
Height of Curb at Gutter Flow Line
Distance from Curb Face to Street Crown
Gutter Width
Street Transverse Slope
Gutter Cross Slope (typically 2 inches over 24 inches or $0.083 \mathrm{ft} / \mathrm{tt}$ )
Street Longitudinal Slope - Enter 0 for sump condition
Manning's Roughness for Street Section (typically between 0.012 and 0.020 )

Max. Allowable Spread for Minor \& Major Storm
Max. Allowable Depth at Gutter Flowline for Minor \& Major Storm
Check boxes are not applicable in SUMP conditions


| $\mathrm{H}_{\text {CURB }}=$ | 6.00 | inches |
| :---: | :---: | :---: |
| $\mathrm{T}_{\text {CROWN }}=$ | 21.0 | ft |
| W = | 2.00 | ft |
| $\mathrm{S}_{\mathrm{x}}=$ | 0.020 | $\mathrm{ft} / \mathrm{ft}$ |
| $\mathrm{S}_{\mathrm{w}}=$ | 0.083 | $\mathrm{ft} / \mathrm{ft}$ |
| $\mathrm{S}_{\mathrm{O}}=$ | 0.000 | $\mathrm{ft} / \mathrm{ft}$ |
| $\mathrm{n}_{\text {STREET }}=$ | 0.014 |  |



MINOR STORM Allowable Capacity is based on Depth Criterion MAJOR STORM Allowable Capacity is based on Depth Criterion

## INLET IN A SUMP OR SAG LOCATION

Version 4.05 Released March 2017


| Design Information (Input) |  | MINOR | MAJOR |  |
| :---: | :---: | :---: | :---: | :---: |
| Type of Inlet ${ }^{\text {a }}$ Denver No. 16 Combinatio | Type $=$ | Denver N | nbination |  |
| Local Depression (additional to continuous gutter depression 'a' from above) | $\mathrm{a}_{\text {iocal }}=$ | 2.00 | 2.00 | inches |
| Number of Unit Inlets (Grate or Curb Opening) | No = | 2 | 2 |  |
| Water Depth at Flowline (outside of local depression) | Ponding Depth $=$ | 6.0 | 6.6 | inches |
| Grate Information |  | MINOR | MAJOR | Override Depths |
| Length of a Unit Grate | $\mathrm{L}_{0}(\mathrm{G})=$ | 3.00 | 3.00 | feet |
| Width of a Unit Grate | $\mathrm{W}_{0}=$ | 1.73 | 1.73 | feet |
| Area Opening Ratio for a Grate (typical values 0.15-0.90) | $\mathrm{A}_{\text {ratio }}=$ | 0.31 | 0.31 |  |
| Clogging Factor for a Single Grate (typical value 0.50-0.70) | $\mathrm{C}_{\mathrm{f}}(\mathrm{G})=$ | 0.50 | 0.50 |  |
| Grate Weir Coefficient (typical value 2.15-3.60) | $\mathrm{C}_{\mathrm{w}}(\mathrm{G})=$ | 3.60 | 3.60 |  |
| Grate Orifice Coefficient (typical value 0.60-0.80) | $\mathrm{C}_{0}(\mathrm{G})=$ | 0.60 | 0.60 |  |
| Curb Opening Information |  | MINOR | MAJOR |  |
| Length of a Unit Curb Opening | $\mathrm{L}_{0}(\mathrm{C})=$ | 3.00 | 3.00 | feet |
| Height of Vertical Curb Opening in Inches | $\mathrm{H}_{\text {vert }}=$ | 6.50 | 6.50 | inches |
| Height of Curb Orifice Throat in Inches | $\mathrm{H}_{\text {trroat }}=$ | 5.25 | 5.25 | inches |
| Angle of Throat (see USDCM Figure ST-5) | Theta $=$ | 0.00 | 0.00 | degrees |
| Side Width for Depression Pan (typically the gutter width of 2 feet) | $\mathrm{W}_{\mathrm{p}}=$ | 2.00 | 2.00 | feet |
| Clogging Factor for a Single Curb Opening (typical value 0.10) | $\mathrm{C}_{\text {f }}(\mathrm{C})=$ | 0.10 | 0.10 |  |
| Curb Opening Weir Coefficient (typical value 2.3-3.7) | $\mathrm{C}_{\mathrm{w}}(\mathrm{C})=$ | 3.70 | 3.70 |  |
| Curb Opening Orifice Coefficient (typical value 0.60-0.70) | $\mathrm{C}_{0}(\mathrm{C})=$ | 0.66 | 0.66 |  |
| Low Head Performance Reduction (Calculated) |  | MINOR | MAJOR |  |
| Depth for Grate Midwidth | $\mathrm{d}_{\text {Grate }}=$ | 0.523 | 0.569 | ft |
| Depth for Curb Opening Weir Equation | $\mathrm{d}_{\text {curb }}=$ | 0.33 | 0.38 | ft |
| Combination Inlet Performance Reduction Factor for Long Inlets | $\mathrm{RF}_{\text {combination }}=$ | 0.71 | 0.77 |  |
| Curb Opening Performance Reduction Factor for Long Inlets | $\mathrm{RF}_{\text {curb }}=$ | 1.00 | 1.00 |  |
| Grated Inlet Performance Reduction Factor for Long Inlets | $\mathrm{RF}_{\text {Grate }}=$ | 0.71 | 0.77 |  |
|  |  | MINOR | MAJOR |  |
| Total Inlet Interception Capacity (assumes clogged condition) | $\mathrm{Q}_{\mathrm{a}}=$ | 6.2 | 7.9 | cfs |
| WARNING: Inlet Capacity less than Q Peak for Major Storm | $Q_{\text {Peak ReQuired }}=$ | 3.3 | 8.3 | cfs |

Version 4.05 Released March 2017

## ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor \& Major Storm)



Gutter Geometry (Enter data in the blue cells)
Maximum Allowable Width for Spread Behind Curb
Side Slope Behind Curb (leave blank for no conveyance credit behind curb)
Manning's Roughness Behind Curb (typically between 0.012 and 0.020 )
Height of Curb at Gutter Flow Line
Distance from Curb Face to Street Crown
Gutter Width
Street Transverse Slope
Gutter Cross Slope (typically 2 inches over 24 inches or $0.083 \mathrm{ft} / \mathrm{tt}$ )
Street Longitudinal Slope - Enter 0 for sump condition
Manning's Roughness for Street Section (typically between 0.012 and 0.020 )

Max. Allowable Spread for Minor \& Major Storm
Max. Allowable Depth at Gutter Flowline for Minor \& Major Storm
Check boxes are not applicable in SUMP conditions


| $\mathrm{H}_{\text {CURB }}=$ | 6.00 | inches |
| :---: | :---: | :---: |
| $\mathrm{T}_{\text {CROWN }}=$ | 12.0 | ft |
| W = | 2.00 | ft |
| $\mathrm{S}_{\mathrm{x}}=$ | 0.020 | $\mathrm{ft} / \mathrm{ft}$ |
| $\mathrm{S}_{\mathrm{w}}=$ | 0.083 | $\mathrm{ft} / \mathrm{ft}$ |
| $\mathrm{S}_{\mathrm{O}}=$ | 0.000 | $\mathrm{ft} / \mathrm{ft}$ |
| $\mathrm{n}_{\text {STREET }}=$ | 0.014 |  |



MINOR STORM Allowable Capacity is based on Depth Criterion MAJOR STORM Allowable Capacity is based on Depth Criterion

## INLET IN A SUMP OR SAG LOCATION

Version 4.05 Released March 2017


| Design Information (Input) |  | MINOR | MAJOR |  |
| :---: | :---: | :---: | :---: | :---: |
| Type of Inlet $\quad$ Denver No. 16 Combination | Type = | Denver N | mbination |  |
| Local Depression (additional to continuous gutter depression 'a' from above) | $\mathrm{a}_{\text {iocal }}=$ | 2.00 | 2.00 | inches |
| Number of Unit Inlets (Grate or Curb Opening) | No = | 3 | 3 |  |
| Water Depth at Flowline (outside of local depression) | Ponding Depth $=$ | 4.4 | 4.4 | inches |
| Grate Information |  | MINOR | MAJOR | Override Depths |
| Length of a Unit Grate | $\mathrm{L}_{0}(\mathrm{G})=$ | 3.00 | 3.00 | feet |
| Width of a Unit Grate | $\mathrm{W}_{0}=$ | 1.73 | 1.73 | feet |
| Area Opening Ratio for a Grate (typical values 0.15-0.90) | $\mathrm{A}_{\text {ratio }}=$ | 0.31 | 0.31 |  |
| Clogging Factor for a Single Grate (typical value 0.50-0.70) | $\mathrm{C}_{\mathrm{f}}(\mathrm{G})=$ | 0.50 | 0.50 |  |
| Grate Weir Coefficient (typical value 2.15-3.60) | $\mathrm{C}_{\mathrm{w}}(\mathrm{G})=$ | 3.60 | 3.60 |  |
| Grate Orifice Coefficient (typical value 0.60-0.80) | $\mathrm{C}_{0}(\mathrm{G})=$ | 0.60 | 0.60 |  |
| Curb Opening Information |  | MINOR | MAJOR |  |
| Length of a Unit Curb Opening | $\mathrm{L}_{0}(\mathrm{C})=$ | 3.00 | 3.00 | feet |
| Height of Vertical Curb Opening in Inches | $\mathrm{H}_{\text {vert }}=$ | 6.50 | 6.50 | inches |
| Height of Curb Orifice Throat in Inches | $\mathrm{H}_{\text {trroat }}=$ | 5.25 | 5.25 | inches |
| Angle of Throat (see USDCM Figure ST-5) | Theta $=$ | 0.00 | 0.00 | degrees |
| Side Width for Depression Pan (typically the gutter width of 2 feet) | $\mathrm{W}_{\mathrm{p}}=$ | 2.00 | 2.00 | feet |
| Clogging Factor for a Single Curb Opening (typical value 0.10) | $\mathrm{C}_{\text {f }}(\mathrm{C})=$ | 0.10 | 0.10 |  |
| Curb Opening Weir Coefficient (typical value 2.3-3.7) | $\mathrm{C}_{\mathrm{w}}(\mathrm{C})=$ | 3.70 | 3.70 |  |
| Curb Opening Orifice Coefficient (typical value 0.60-0.70) | $\mathrm{C}_{0}(\mathrm{C})=$ | 0.66 | 0.66 |  |
| Low Head Performance Reduction (Calculated) |  | MINOR | MAJOR |  |
| Depth for Grate Midwidth | $\mathrm{d}_{\text {Grate }}=$ | 0.389 | 0.389 | ft |
| Depth for Curb Opening Weir Equation | $\mathrm{d}_{\text {curb }}=$ | 0.20 | 0.20 | ft |
| Combination Inlet Performance Reduction Factor for Long Inlets | $\mathrm{RF}_{\text {combination }}=$ | 0.41 | 0.41 |  |
| Curb Opening Performance Reduction Factor for Long Inlets | $\mathrm{RF}_{\text {curb }}=$ | 0.86 | 0.86 |  |
| Grated Inlet Performance Reduction Factor for Long Inlets | $\mathrm{RF}_{\text {Grate }}=$ | 0.41 | 0.41 |  |
|  |  | MINOR | MAJOR |  |
| Total Inlet Interception Capacity (assumes clogged condition) | $\mathrm{Q}_{\mathrm{a}}=$ | 3.2 | 3.2 | cfs |
| Lnlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK) | $Q_{\text {Peak ReQuired }}=$ | 0.8 | 3.0 | cfs |

Nyloplast 3' x 3' Road \& Highway Inlet Capacity Chart


3130 Verona Avenue • Buford, GA 30518
(866) 888-8479 / (770) 932-2443 • Fax: (770) 932-2490 (C) Nyloplast Inlet Capacity Charts June 2012

## Weir Report

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

## Pond A Spillway (Q_100 = Peak Undetained Q_100 (SF3 Major) = 21.5 cfs

Trapezoidal Weir Crest
Bottom Length (ft)
Total Depth (ft)
Side Slope (z:1)

## Calculations

Weir Coeff. Cw
Compute by:
Known Q (cfs)
= Sharp
$=20.00$
$=1.50$
$=4.00$
$=3.10$
Known Q
$=21.50$

Highlighted
Depth (ft)
$=0.48$
Q (cfs)
Area (sqft)
Velocity (ft/s)
Top Width (ft)
$=21.50$
$=10.52$
$=2.04$
$=23.84$


## Weir Report

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

## Pond B Spillway (Q_100 = Peak Undetained Q_100 (SF3 Major) = 20.0 cfs

Trapezoidal Weir Crest
Bottom Length (ft)
Total Depth (ft)
Side Slope (z:1)
= Sharp
$=20.00$
$=1.50$
$=4.00$

## Calculations

Weir Coeff. Cw
Compute by:
Known Q (cfs)
$=3.10$
Known Q
$=20.00$

Highlighted
Depth (ft)
$=0.45$
Q (cfs)
Area (sqft)
Velocity (ft/s)
Top Width (ft)
$=20.00$
$=9.81$
$=2.04$
$=23.60$

Depth (ft) Pond B Spillway (Q_100 = Peak Undetained Q_100 (SF3 Major) = $\mathbf{2 0 . 0} \mathbf{c f s} \quad$ Depth (ft)


## Appendix D Water Quality \& Detention



DETENTION BASIN STAGE-STORAGE TABLE BUILDER
UD-Detention, Version 3.07 (February 2017)



| User Input: Vertical Orifice (Circular or Rectangular) |  |  | ft (relative to basin bottom at Stage $=0 \mathrm{ft}$ ) ft (relative to basin bottom at Stage $=0 \mathrm{ft}$ ) inches | Calculated Parameters for Vertical Orifice |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Not Selected | Not Selected |  | Vertical Orifice Area $=$ <br> Vertical Orifice Centroid = | Not Selected | Not Selected |
| Invert of Vertical Orifice $=$ | N/A | N/A |  |  | N/A | N/A |
| Depth at top of Zone using Vertical Orifice $=$ | N/A | N/A |  |  | N/A | N/A |
| Vertical Orifice Diameter = | N/A | N/A |  |  |  |  |


| User Input: Overflow Weir (Dropbox) and Grate (Flat or Sloped) |  |  | ft (relative to basin bottom at Stage $=0 \mathrm{ft}$ ) | Calculated Parameters for Overflow Weir |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Zone 3 Weir | Not Selected |  |  | Zone 3 Weir | Not Selected |
| Overflow Weir Front Edge Height, $\mathrm{Ho}=$ | 5.73 | N/A |  | Height of Grate Upper Edge, $\mathrm{H}_{\mathrm{t}}=$ | 5.73 | N/A |
| Overflow Weir Front Edge Length $=$ | 3.00 | N/A |  | Over Flow Weir Slope Length = | 3.00 | N/A |
| Overflow Weir Slope = | 0.00 | N/A | $\mathrm{H}: \mathrm{V}$ (enter zero for flat grate) | Grate Open Area / 100-yr Orifice Area $=$ | 34.18 | N/A |
| Horiz. Length of Weir Sides = | 3.00 | N/A | feet | Overflow Grate Open Area w/o Debris = | 6.30 | N/A |
| Overflow Grate Open Area \% = | 70\% | N/A | \%, grate open area/total area | Overflow Grate Open Area w/ Debris $=$ | 3.15 | N/A |
| Debris Clogging \% = | 50\% | N/A | \% |  |  |  |

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

|  | Zone 3 Restrictor | Not Selected | ft (distance below basin bottom at Stage $=0 \mathrm{ft}$ ) | Outlet Orifice Area $=$ | Zone 3 Restrictor | Not Selected | $\mathrm{ft}^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Depth to Invert of Outlet Pipe $=$ | 0.00 | N/A |  |  | 0.18 | N/A |  |
| Outlet Pipe Diameter $=$ | 18.00 | N/A | inches |  | 0.14 | N/A | feet |
| Restrictor Plate Height Above Pipe Invert = | 2.90 |  | inches Half-Centr | Restrictor Plate on Pipe = | 0.83 | N/A | radians |


| Spillway Invert Stage= | 7.22 | ft (relative to basin bottom at Stage $=0 \mathrm{ft}$ ) |
| :---: | :---: | :---: |
| Spillway Crest Length = | 20.00 | feet |
| Spillway End Slopes = | 4.00 | $\mathrm{H}: \mathrm{V}$ |
| Freeboard above M ax Water Surface $=$ | 1.00 | feet |


| Calculated Parameters for Spillway |  |
| ---: | :--- |
| Spillway Design Flow Depth | $=0.34$ |
| Stage at Top of Freeboard | feet |
|  | 8.56 |
| feet |  |




## Detention Basin Outlet Structure Design

Outflow Hydrograph Workbook Filename:
Storm Inflow Hydrographs UD-Detention, Version 3.07 (February 2017)
The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

|  | SOURCE | WORKBOOK | WORKBOOK | WORKBOOK | WORKBOOK | WORKBOOK | WORKBOOK | WORKBOOK | WORKBOOK | \#N/A |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Time Interval | TIME | WQCV [cfs] | EURV [cfs] | 2 Year [cfs] | 5 Year [cfs] | 10 Year [cfs] | 25 Year [cfs] | 50 Year [cfs] | 100 Year [cfs] | 500 Year [cfs] |
| 5.36 min | 0:00:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
|  | 0:05:22 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
| Hydrograph | 0:10:43 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
| Constant | 0:16:05 | 0.07 | 0.23 | 0.16 | 0.20 | 0.25 | 0.31 | 0.38 | 0.47 | \#N/A |
| 0.932 | 0:21:26 | 0.19 | 0.60 | 0.41 | 0.54 | 0.66 | 0.83 | 1.03 | 1.27 | \#N/A |
|  | 0:26:48 | 0.48 | 1.55 | 1.06 | 1.39 | 1.71 | 2.12 | 2.65 | 3.27 | \#N/A |
|  | 0:32:10 | 1.32 | 4.25 | 2.92 | 3.82 | 4.69 | 5.83 | 7.28 | 9.00 | \#N/A |
|  | 0:37:31 | 1.54 | 5.00 | 3.42 | 4.48 | 5.52 | 6.89 | 8.62 | 10.69 | \#N/A |
|  | 0:42:53 | 1.46 | 4.76 | 3.25 | 4.27 | 5.26 | 6.56 | 8.22 | 10.20 | \#N/A |
|  | 0:48:14 | 1.32 | 4.34 | 2.96 | 3.88 | 4.79 | 5.97 | 7.49 | 9.29 | \#N/A |
|  | 0:53:36 | 1.17 | 3.86 | 2.63 | 3.45 | 4.26 | 5.33 | 6.68 | 8.30 | \#N/A |
|  | 0:58:58 | 1.00 | 3.32 | 2.25 | 2.97 | 3.66 | 4.59 | 5.76 | 7.17 | \#N/A |
|  | 1:04:19 | 0.87 | 2.89 | 1.97 | 2.59 | 3.20 | 4.00 | 5.02 | 6.24 | \#N/A |
|  | 1:09:41 | 0.79 | 2.62 | 1.78 | 2.34 | 2.90 | 3.62 | 4.55 | 5.66 | \#N/A |
|  | 1:15:02 | 0.64 | 2.15 | 1.45 | 1.92 | 2.37 | 2.98 | 3.75 | 4.67 | \#N/A |
|  | 1:20:24 | 0.51 | 1.74 | 1.17 | 1.55 | 1.93 | 2.42 | 3.06 | 3.82 | \#N/A |
|  | 1:25:46 | 0.38 | 1.33 | 0.89 | 1.18 | 1.47 | 1.86 | 2.35 | 2.94 | \#N/A |
|  | 1:31:07 | 0.27 | 0.97 | 0.65 | 0.87 | 1.08 | 1.37 | 1.75 | 2.19 | \#N/A |
|  | 1:36:29 | 0.20 | 0.71 | 0.47 | 0.63 | 0.79 | 1.00 | 1.27 | 1.59 | \#N/A |
|  | 1:41:50 | 0.16 | 0.56 | 0.37 | 0.50 | 0.62 | 0.78 | 0.98 | 1.23 | \#N/A |
|  | 1:47:12 | 0.13 | 0.46 | 0.31 | 0.41 | 0.51 | 0.64 | 0.81 | 1.01 | \#N/A |
|  | 1:52:34 | 0.11 | 0.39 | 0.26 | 0.35 | 0.43 | 0.54 | 0.69 | 0.86 | \#N/A |
|  | 1:57:55 | 0.10 | 0.34 | 0.23 | 0.31 | 0.38 | 0.48 | 0.60 | 0.75 | \#N/A |
|  | 2:03:17 | 0.09 | 0.31 | 0.21 | 0.28 | 0.34 | 0.43 | 0.54 | 0.68 | \#N/A |
|  | 2:08:38 | 0.08 | 0.29 | 0.19 | 0.26 | 0.32 | 0.40 | 0.50 | 0.63 | \#N/A |
|  | 2:14:00 | 0.06 | 0.21 | 0.14 | 0.19 | 0.23 | 0.29 | 0.37 | 0.46 | \#N/A |
|  | 2:19:22 | 0.05 | 0.15 | 0.10 | 0.14 | 0.17 | 0.21 | 0.27 | 0.34 | \#N/A |
|  | 2:24:43 | 0.03 | 0.11 | 0.08 | 0.10 | 0.12 | 0.16 | 0.20 | 0.25 | \#N/A |
|  | 2:30:05 | 0.02 | 0.08 | 0.06 | 0.07 | 0.09 | 0.11 | 0.15 | 0.18 | \#N/A |
|  | 2:35:26 | 0.02 | 0.06 | 0.04 | 0.05 | 0.06 | 0.08 | 0.10 | 0.13 | \#N/A |
|  | 2:40:48 | 0.01 | 0.04 | 0.03 | 0.04 | 0.05 | 0.06 | 0.07 | 0.09 | \#N/A |
|  | 2:46:10 | 0.01 | 0.03 | 0.02 | 0.03 | 0.03 | 0.04 | 0.05 | 0.07 | \#N/A |
|  | 2:51:31 | 0.00 | 0.02 | 0.01 | 0.02 | 0.02 | 0.03 | 0.03 | 0.04 | \#N/A |
|  | 2:56:53 | 0.00 | 0.01 | 0.01 | 0.01 | 0.01 | 0.02 | 0.02 | 0.03 | \#N/A |
|  | 3:02:14 | 0.00 | 0.00 | 0.00 | 0.00 | 0.01 | 0.01 | 0.01 | 0.01 | \#N/A |
|  | 3:07:36 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
|  | 3:12:58 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
|  | 3:18:19 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
|  | 3:23:41 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
|  | 3:29:02 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
|  | 3:34:24 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
|  | 3:39:46 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
|  | 3:45:07 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
|  | 3:50:29 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
|  | 3:55:50 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
|  | 4:01:12 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
|  | 4:06:34 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
|  | 4:11:55 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
|  | 4:17:17 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
|  | 4:22:38 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
|  | 4:28:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
|  | 4:33:22 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
|  | 4:38:43 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
|  | 4:44:05 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
|  | 4:49:26 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
|  | 4:54:48 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
|  | 5:00:10 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
|  | 5:05:31 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
|  | 5:10:53 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
|  | 5:16:14 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
|  | 5:21:36 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
|  | 5:26:58 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
|  | 5:32:19 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
|  | 5:37:41 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
|  | 5:43:02 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
|  | 5:48:24 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
|  | 5:53:46 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
|  | 5:59:07 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
|  | 6:04:29 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
|  | 6:09:50 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
|  | 6:15:12 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
|  | 6:20:34 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
|  | 6:25:55 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |

## Detention Basin Outlet Structure Design

UD-Detention, Version 3.07 (February 2017)

## Summary Stage-Area-Volume-Discharge Relationships

The user can create a summary S-A-V-D by entering the desired stage increments and the remainder of the table will populate automatically.

| Stage - Storage Description | Stage <br> [ft] | Area [ft²] | Area <br> [acres] | Volume <br> [ft^3] | Volume [ac-ft] | $\begin{gathered} \text { Total } \\ \text { Outflow } \\ \text { [cfs] } \end{gathered}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0.00 | 0 | 0.000 | 0 | 0.000 | 0.00 | For best results, include the stages of all grade slope changes (e.g. ISV and Floor) from the S-A-V table on Sheet 'Basin'. <br> Also include the inverts of all outlets (e.g. vertical orifice, overflow grate, and spillway, where applicable). |
|  | 1.00 | 2,418 | 0.055 | 1,521 | 0.035 | 0.03 |  |
|  | 2.00 | 3,198 | 0.073 | 4,323 | 0.099 | 0.05 |  |
|  | 3.00 | 4,043 | 0.093 | 7,971 | 0.183 | 0.08 |  |
|  | 4.00 | 4,957 | 0.114 | 12,461 | 0.286 | 0.12 |  |
|  | 5.00 | 5,946 | 0.136 | 17,903 | 0.411 | 0.16 |  |
|  | 6.00 | 7,010 | 0.161 | 24,372 | 0.560 | 2.15 |  |
|  | 7.00 | 8,179 | 0.188 | 31,949 | 0.733 | 2.32 |  |
|  | 8.00 | 8,445 | 0.194 | 33,778 | 0.775 | 2.36 |  |
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DETENTION BASIN STAGE-STORAGE TABLE BUILDER
UD-Detention, Version 3.07 (February 2017)



| User Input: Vertical Orifice (Circular or Rectangular) |  |  | ft (relative to basin bottom at Stage $=0 \mathrm{ft}$ ) <br> ft (relative to basin bottom at Stage $=0 \mathrm{ft}$ ) | Calculated Parameters for Vertical Orifice |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Not Selected | Not Selected |  | Vertical Orifice Area $=$ <br> Vertical Orifice Centroid $=$ | Not Selected | Not Selected |
| Invert of Vertical Orifice $=$ | N/A | N/A |  |  | N/A | N/A |
| Depth at top of Zone using Vertical Orifice $=$ | N/A | N/A |  |  | N/A | N/A |



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| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | WQCV | EURV | 2 Year | 5 Year | 10 Year | 25 Year | 50 Year | 100 Year | 500 Year |
|  | 0.53 | 1.07 | 1.19 | 1.50 | 1.75 | 2.00 | 2.25 | 2.52 | 0.00 |
|  | 0.080 | 0.289 | 0.198 | 0.259 | 0.317 | 0.390 | 0.476 | 0.577 | 0.000 |
|  |  |  |  |  |  |  |  |  |  |
|  | 0.080 | 0.288 | 0.197 | 0.258 | 0.317 | 0.390 | 0.476 | 0.577 | \#N/A |
|  | 0.00 | 0.00 | 0.00 | 0.00 | 0.01 | 0.03 | 0.19 | 0.45 | 0.00 |
|  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.1 | 0.8 | 1.9 | 0.0 |
|  | 1.3 | 4.7 | 3.2 | 4.2 | 5.1 | 6.3 | 7.7 | 9.3 | \#N/A |
|  | 0.0 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 1.7 | \#N/A |
|  | N/A | N/A | N/A | 4.3 | 2.1 | 1.0 | 0.2 | 0.9 | \#N/A |
|  | Plate | Plate | Plate | Plate | Plate | Plate | Plate | Outlet Plate 1 | \#N/A |
|  | N/A | N/A | N/A | N/A | N/A | N/A | N/A | 0.1 | \#N/A |
|  | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | \#N/A |
|  | 38 | 71 | 61 | 68 | 74 | 80 | 87 | 87 | \#N/A |
|  | 40 | 76 | 64 | 72 | 79 | 86 | 94 | 95 | \#N/A |
|  | 0.94 | 2.05 | 1.59 | 1.90 | 2.19 | 2.53 | 2.92 | 3.10 | \#N/A |
|  | 0.16 | 0.20 | 0.18 | 0.19 | 0.20 | 0.21 | 0.22 | 0.23 | \#N/A |
|  | 0.073 | 0.273 | 0.186 | 0.244 | 0.301 | 0.372 | 0.455 | 0.496 | \#N/A |



## Detention Basin Outlet Structure Design

Outflow Hydrograph Workbook Filename:
Storm Inflow Hydrographs UD-Detention, Version 3.07 (February 2017)
The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

|  | SOURCE | WORKBOOK | WORKBOOK | WORKBOOK | WORKBOOK | WORKBOOK | WORKBOOK | WORKBOOK | WORKBOOK | \#N/A |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Time Interval | TIM E | WQCV [cfs] | EURV [cfs] | 2 Year [ffs] | 5 Year [cfs] | 10 Year [cfs] | 25 Year [cfs] | 50 Year [cfs] | 100 Year [cfs] | 500 Year [cfs] |
| 5.17 min | 0:00:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
|  | 0:05:10 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
| Hydrograph Constant | 0:10:20 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
|  | 0:15:31 | 0.06 | 0.21 | 0.15 | 0.19 | 0.23 | 0.28 | 0.34 | 0.41 | \#N/A |
| 0.968 | 0:20:41 | 0.16 | 0.56 | 0.39 | 0.51 | 0.62 | 0.76 | 0.92 | 1.11 | \#N/A |
|  | 0:25:51 | 0.41 | 1.45 | 1.00 | 1.30 | 1.59 | 1.94 | 2.36 | 2.85 | \#N/A |
|  | 0:31:01 | 1.14 | 3.98 | 2.74 | 3.57 | 4.36 | 5.34 | 6.49 | 7.83 | \#N/A |
|  | 0:36:11 | 1.32 | 4.67 | 3.21 | 4.19 | 5.13 | 6.30 | 7.67 | 9.28 | \#N/A |
|  | 0:41:22 | 1.25 | 4.45 | 3.05 | 3.99 | 4.89 | 6.01 | 7.32 | 8.85 | \#N/A |
|  | 0:46:32 | 1.13 | 4.05 | 2.78 | 3.63 | 4.45 | 5.47 | 6.66 | 8.05 | \#N/A |
|  | 0:51:42 | 1.00 | 3.60 | 2.46 | 3.23 | 3.96 | 4.87 | 5.94 | 7.19 | \#N/A |
|  | 0:56:52 | 0.85 | 3.09 | 2.11 | 2.77 | 3.40 | 4.19 | 5.12 | 6.20 | \#N/A |
|  | 1:02:02 | 0.75 | 2.70 | 1.84 | 2.42 | 2.97 | 3.66 | 4.46 | 5.41 | \#N/A |
|  | 1:07:13 | 0.67 | 2.44 | 1.67 | 2.19 | 2.69 | 3.31 | 4.04 | 4.90 | \#N/A |
|  | 1:12:23 | 0.54 | 2.00 | 1.36 | 1.79 | 2.20 | 2.72 | 3.32 | 4.04 | \#N/A |
|  | 1:17:33 | 0.43 | 1.62 | 1.10 | 1.45 | 1.79 | 2.21 | 2.71 | 3.29 | \#N/A |
|  | 1:22:43 | 0.32 | 1.23 | 0.83 | 1.10 | 1.36 | 1.69 | 2.08 | 2.53 | \#N/A |
|  | 1:27:53 | 0.23 | 0.90 | 0.60 | 0.80 | 1.00 | 1.25 | 1.54 | 1.88 | \#N/A |
|  | 1:33:04 | 0.17 | 0.66 | 0.44 | 0.59 | 0.73 | 0.91 | 1.12 | 1.36 | \#N/A |
|  | 1:38:14 | 0.14 | 0.52 | 0.35 | 0.46 | 0.57 | 0.71 | 0.87 | 1.06 | \#N/A |
|  | 1:43:24 | 0.11 | 0.43 | 0.29 | 0.38 | 0.47 | 0.58 | 0.71 | 0.87 | \#N/A |
|  | 1:48:34 | 0.10 | 0.36 | 0.24 | 0.32 | 0.40 | 0.49 | 0.61 | 0.74 | \#N/A |
|  | 1:53:44 | 0.08 | 0.32 | 0.22 | 0.28 | 0.35 | 0.44 | 0.53 | 0.65 | \#N/A |
|  | 1:58:55 | 0.08 | 0.29 | 0.19 | 0.26 | 0.32 | 0.39 | 0.48 | 0.59 | \#N/A |
|  | 2:04:05 | 0.07 | 0.27 | 0.18 | 0.24 | 0.29 | 0.36 | 0.44 | 0.54 | \#N/A |
|  | 2:09:15 | 0.05 | 0.20 | 0.13 | 0.17 | 0.22 | 0.27 | 0.33 | 0.40 | \#N/A |
|  | 2:14:25 | 0.04 | 0.14 | 0.10 | 0.13 | 0.16 | 0.20 | 0.24 | 0.29 | \#N/A |
|  | 2:19:35 | 0.03 | 0.10 | 0.07 | 0.09 | 0.12 | 0.14 | 0.18 | 0.21 | \#N/A |
|  | 2:24:46 | 0.02 | 0.08 | 0.05 | 0.07 | 0.08 | 0.10 | 0.13 | 0.16 | \#N/A |
|  | 2:29:56 | 0.01 | 0.05 | 0.04 | 0.05 | 0.06 | 0.07 | 0.09 | 0.11 | \#N/A |
|  | 2:35:06 | 0.01 | 0.04 | 0.03 | 0.03 | 0.04 | 0.05 | 0.06 | 0.08 | \#N/A |
|  | 2:40:16 | 0.01 | 0.03 | 0.02 | 0.02 | 0.03 | 0.04 | 0.05 | 0.06 | \#N/A |
|  | 2:45:26 | 0.00 | 0.02 | 0.01 | 0.02 | 0.02 | 0.02 | 0.03 | 0.04 | \#N/A |
|  | 2:50:37 | 0.00 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 0.02 | 0.02 | \#N/A |
|  | 2:55:47 | 0.00 | 0.00 | 0.00 | 0.00 | 0.01 | 0.01 | 0.01 | 0.01 | \#N/A |
|  | 3:00:57 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
|  | 3:06:07 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
|  | 3:11:17 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
|  | 3:16:28 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
|  | 3:21:38 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
|  | 3:26:48 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
|  | 3:31:58 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
|  | 3:37:08 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
|  | 3:42:19 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
|  | 3:47:29 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
|  | 3:52:39 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
|  | 3:57:49 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
|  | 4:02:59 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
|  | 4:08:10 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
|  | 4:13:20 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#V/A |
|  | 4:18:30 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
|  | 4:23:40 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
|  | 4:28:50 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
|  | 4:34:01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
|  | 4:39:11 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
|  | 4:44:21 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
|  | 4:49:31 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
|  | 4:54:41 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
|  | 4:59:52 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
|  | 5:05:02 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
|  | 5:10:12 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
|  | 5:15:22 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
|  | 5:20:32 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
|  | 5:25:43 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
|  | 5:30:53 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
|  | 5:36:03 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
|  | 5:41:13 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
|  | 5:46:23 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
|  | 5:51:34 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
|  | 5:56:44 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
|  | 6:01:54 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
|  | 6:07:04 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |
|  | 6:12:14 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | \#N/A |

## Detention Basin Outlet Structure Design

UD-Detention, Version 3.07 (February 2017)

## Summary Stage-Area-Volume-Discharge Relationships

The user can create a summary S-A-V-D by entering the desired stage increments and the remainder of the table will populate automatically.
The user should graphically compare the summary S-A-V-D table to the full S-A-V-D table in the chart to confirm it captures all key transition points.


# Appendix E <br> <br> Reference Material 

 <br> <br> Reference Material}

Resolution No. 18-470

| Basin <br> Number | Receiving <br> Waters | Year <br> Studied | Drainage Basin Name | 2019 Drainage Fee <br> (per Impervious Acre) | 2019 Bridge Fee <br> (per Imperviops Acre) |
| :---: | :---: | :---: | :---: | :---: | :---: |


| Drainage Basins with DBPS's: |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| CHMS0200 | Chico Creek | 2013 | Haegler Ranch | \$10,324 | \$1,524 |
| CHWS1200 | Chico Creek | 2001 | Bennell Ranch | \$11,558 | \$4,433 |
| CHWS 1400 | Chico Creek | 2013 | Falcon | \$29,622 | \$4,069 |
| FOFO2000 | Fountain Creek | 2001 | West Fork Jimmy Camp Creek | \$12,564 | \$3,717 |
| FOFO2600 | Fountain Creek | 1991* | Big Johnson / Crews Gulch | \$18,350 | \$2,370 |
| FOFO2800 | Fountain Creek | 1988* | Widefield | \$18,350 | \$0 |
| FOFO2900 | Fountain Creek | 1988* | Security | \$18,350 | \$0 |
| FOFO3000 | Fountain Creek | 1991* | Windmill Gulch | \$18,350 | \$275 |
| FOFO3100 / FOFO3200 | Fountain Creek | 1988* | Carson Street / Little Johnson | \$11,192 | \$0 |
| FOFO3400 | Fountain Creek | 1984* | Peterson Field | \$13,235 | \$1,004 |
| FOFO3600 | Fountain Creek | 1991* | Fisher's Canyon | \$18,350 | \$0 |
| FOFO4000 | Fountain Creek | 1996 | Sand Creek | \$18,940 | \$5,559 |
| FOFO4200 | Fountain Creek | 1977 | Spring Creek | \$9,517 | \$0 |
| FOFO4600 | Fountain Creek | 1984* | Soulhwest Area | \$18,350 | \$0 |
| FOFO4800 | Fountain Creek | 1991 | Bear Creek | \$18,350 | \$1,004 |
| FOFO5400 | Fountain Creek | 1977 | 21st Street | \$5,521 | \$0 |
| FOFO5600 | Fountain Creek | 1964 | 19th Street | \$3,611 | \$0 |
| FOFO5800 | Fountain Creek | 1964 | Camp Creek | \$2,033 | \$0 |
| FOMO0400 | Monument Creek | 1986" | Mesa | \$9,598 | \$0 |
| FOM01000 | Monument Creek | 1981 | Douglas Creek | \$11,540 | \$255 |
| FOM01200 | Monument Creek | 1977 | Templeton Gap | \$11,847 | \$275 |
| FOM01400 | Monument Creek | 1976 | Pope's Bluft | \$3,676 | \$627 |
| FOM01600 | Monument Creek | 1976 | South Rockrimmon | \$4,314 | \$0 |
| FOMO1800 | Monument Creek | 1973 | North Rockrimmon | \$5,521 | \$0 |
| FOMO2000 | Monument Creek | 1971 | Pulpit Rock | \$6,085 | \$0 |
| FOMO2200 | Monument Creek | 1994 | Cottonwood Creek / S. Pine | \$18,350 | \$1,004 |
| FOMO2400 | Monument Creek | 1966 | Dry Creek | \$14,486 | \$524 |
| FOMO3600 | Monument Creek | 1989* | Black Squirrel Creek | \$8,331 | \$524 |
| FOMO3700 | Monument Creek | 1987* | Middle Tributary | \$15,312 | \$0 |
| FOMO3800 | Monument Creek | 1987* | Monument Branch | \$18,350 | \$0 |
| FOMO4000 | Monument Creek | 1996 | Smith Creek | \$7,481 | \$1,004 |
| FOMO4200 | Monument Creek | 1989* | Black Forest | \$18,350 | \$500 |
| FOMO5200 | Monument Creek | 1993* | Dirty Wornan Creek | \$18,350 | \$1,004 |
| FOMO5300 | Fountain Creek | 1993* | Crystal Creek | \$18,350 | \$1,004 |
| Miscellaneous Drainage Basins: ${ }^{\text {a }}$ |  |  |  |  |  |
| CHBS 0800 | Chico Creek |  | Book Ranch | \$17,217 | \$2,492 |
| CHEC0400 | Chico Creek |  | Upper East Chico | \$9,380 | \$272 |
| CHWS0200 | Chico Creek |  | Telephane Exchange | \$10,306 | \$241 |
| CHWS0400 | Chico Creek |  | Livestock Company | \$16,976 | \$202 |
| CHWS0600 | Chico Creek |  | West Squirrel | \$8,849 | \$3,672 |
| CHWS0800 | Chico Creek |  | Solberg Ranch | \$18,350 | \$0 |
| FOFO1200 | Fountain Creek |  | Crooked Canyon | \$5,540 | \$0 |
| FOFO1400 | Fountain Creek |  | Calhan Reservoir | \$4,625 | \$270 |
| FOFO1600 | Fountain Creek |  | Sand Canyon | \$3,342 | \$0 |
| FOFO2000 | Fountain Creek |  | Jimmy Camp Creek ${ }^{\text {J }}$ | \$18,350 | \$858 |
| FOFO2200 | Fountain Creek |  | Fort Carson | \$14,486 | \$524 |
| FOFO2700 | Fountain Creek |  | West Little Johnson | \$1,209 | \$0 |
| FOFO3800 | Fountain Creek |  | Stratton | \$8,801 | \$394 |
| FOFO5000 | Fountain Creek |  | Midland | \$14,486 | \$524 |
| FOFO6000 | Fountain Creek |  | Palmer Trail | \$14,486 | \$524 |
| FOFO6800 | Fountain Creek |  | Black Canyon | \$14,486 | \$524 |
| FOMO4600 | Monument Creek |  | Beaver Creek | \$10,970 | \$0 |
| FОМО3000 | Monument Creek |  | Kettle Creek | \$9,909 | \$0 |
| FOMO3400 | Monument Creek |  | Elikhom | \$1,665 | \$0 |
| FOMO5000 | Monument Creek |  | Monument Rock | \$7,953 | \$0 |
| FOMO5400 | Monument Creek |  | Palmer Lake | \$12,717 | \$0 |
| FOMO5600 | Monument Creek |  | Raspberry Mountain | \$4,278 | \$0 |
| PLPL0200 | Monument Creek |  | Bald Mountain | \$9,116 | \$0 |
| Interim Drainage Basins: ? |  |  |  |  |  |
| FOFO1800 | Fountain Creek |  | Little Fountain Creek | \$2,346 | \$0 |
| FOMO4400 | Monument Creek |  | Jackson Creek | \$7,263 | \$0 |
| FOMO4800 | Monument Creek |  | Teachout Creek | \$5,044 | \$758 |

1. The miscellaneous drainage fee previous to September 1999 resolution was the average of all drainage fees for basins with Basin Planning Studies perform
2. Interim Drainage Fees are based upon draft Drainage Basin Planning Studies or the Drainage Basin Identification and Fee Estimation Report. (Best availabl
3. This is an interim fee and will be adjusted when a DBPS is completed. In addition to the Drainage Fee a surety in the amount of $\$ 7,285$ per impervious acre shi the DBPS results in a fee greater than the current fee. Fees paid in excess of the future revised fee will be reimbursed. See Resolution 06-326 (9/14/06) and Res

# SAND CREEK DRAINAGE BASIN PLANNING STUDY PRELIMINARY DESIGN REPORT 

CITY OF COLORADO SPRINGS, EL PASO COUNTY, COLORADO


## II. STUDY AREA DESCRIPTION

The Sand Creek drainage basin is a left-bank tributary to the Fountain Creek lying in the west-central portions of El Paso County. Sand Creek's drainage area at Fountain Creek is approximately 54 square miles of which approximately 18.8 square miles are inside the City of Colorado Springs corporate limits. The basin is divided into five major sub-basins, the Sand Creek mainstem, the East Fork Sand Creek, the Central Tributary to East Fork, the West Fork, and the East Fork Subtributary. Figure II-1 shows the location of the Sand Creek basin.

## Basin Description

The Sand Creek basin covers a total of 54 square miles in unincorporated El Paso County and Colorado Springs, Colorado. Of this total, approximately 28 square miles is encompassed by the Sand Creek basin, and 26 square miles for the East Fork Sand Creek basin. The basin trends in generally a south to southwesterly direction, entering the Fountain Creek approximately two miles upstream of the Academy Boulevard bridge over Fountain Creek. Two main tributaries drain the basin, those being the mainstem of Sand Creek and East Fork Sand Creek. Development presence in most evident along the mainstream. At this time, approximately 25 percent of the basin is developed. This alternative evaluation focuses upon the Sand Creek basin only.

The maximum basin elevation is approximately 7,620 feet above mean sea level, and falls to approximately 5,790 feet at the confluence with Fountain Creek. The headwaters of the basin originate in the conifer covered areas of The Black Forest. The middle eastern portions of the basin are typified by rolling range land with fair to good vegetative cover associated with semi-arid climates.

## Climate

This area of El Paso County can be described, in general as high plains, with total precipitation amounts typical of a semi-arid region. Winters are generally cold and dry. Precipitation ranges from 14 to 16 inches per year, with the majority of this precipitation occurring in spring and summer in the form of rainfall. Thunderstorms are common during the summer months, and are typified by quick-moving low pressure cells which draw moisture from the Gulf of Mexico into the region. Average temperatures range from about $30^{\circ} \mathrm{F}$ in the winter
to $75^{\circ}$ in the summer. The relative humidity ranges from about 25 percent in the summer to 45 percent in the winter.

## Soils and Geology

Soils within the Sand Creek basin vary between soil types A through D, as identified by the U. S. Department of Agriculture, Soil Conservation Service. The predominant soil groupings are in the Truckton and Bresser soil associations. The soils consist of deep, well drained soils that formed in alluvium and residium, derived from sedimentary rock. The soils have high to moderate infiltration rates, and are extremely susceptible to wind and water erosion where poor vegetation cover exists. In undeveloped areas, the predominance of Type A and B soils give this basin a lower runoff per unit area as compared to basins with soils dominated by Types C and D. Presented on Figure II-2 is the Hydrologic Soil distribution map for the Sand Creek basin.

## Property Ownership and Impervious Land Densities

Property ownership along the major drainageway within the Sand Creek basin vary from public to private. Along the developed reaches, drainage right-of-ways and greenbelts have been dedicated during the development of the adjacent residential and commercial land. Where development has not occurred, the drainageways remain under private ownership with no delineated drainage right-of-way or easements. There are several public parks which abut the mainstem of Sand Creek. Roadway and utility easements abutting or crossing the major drainageways occur most frequently in the developed portions of the basin.

Land use information for the existing and future conditions were reviewed as part of the planning effort. This information is used in the hydrologic analysis to predict runoff rates and volumes for the purposes of facility evaluation. The identification of land uses abutting the drainageways is also useful in the identification of feasible plans for stabilization and aesthetic treatment of the creek. Presented on Figure II-3 is the proposed land use map used in the evaluation of impervious land densities discussed in the hydrologic section of this report. Figure II-3 is not intended to reflect the future zoning or land use policies of the City or the County.

The land use information within the Banning-Lewis Ranch property was obtained from Aries Properties during the time the draft East Fork Sand Creek Drainage Basin Planning Study was being prepared. The land use information was again reviewed with the City of Colorado Springs Department of Planning and was found to be appropriate for use in the estimation of hydrology for the East Fork Basin. The location of future arterial streets and roadways within


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EPC DEVELOPMENT SEAVICES

# HANNAH RIDGE AT FEATHERGRASS MASTER DRAINAGE DEVELOPMENT PLAN 

November 15, 2007
Project No. 60754

## PREPARED FOR:

FEATHERGRASS INVESTMENTS, LLC<br>4715 North Chestnut Street<br>Colorado Springs, CO 80907 (719) 593-8367

Kenneth P. Driscoll, Manager

PREPARED BY:
M.V.E., Inc.

1903 Lelaray Street, Suite 200
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discharges of $Q_{5}=2 \mathrm{cfs}$ and $\mathrm{Q}_{100}=5 \mathrm{cfs}$. Basin OSA8, on the east side of Akers Drive, drains south onto the eastern section of the property with peak discharges of $Q_{5}=30 \mathrm{cfs}$ and $\mathrm{Q}_{100}=60 \mathrm{cfs}$. Flows from Basin OSA3 and a portion of Basin OSA8 enters Akers Drive. The existing Akers Drive and Akers drainage improvements were designed by M.V.E., Inc. and approved by El Paso County D.O.T. in September 2006. The system was designed to capture and convey developed flows in Akers Drive. One 10 ft Type R inlet and one 15 ft Type R inlet, connected by an 18" RCP are installed on the east side of Akers, just north of the Constitution intersection. A 10 ft Type R inlet is located on the west side of Akers. The flows collected by the inlets are discharged at the CBC opening, just to the west, with a $24^{\prime \prime}$ RCP. The inlets and connecting pipes are adequate to collect and route developed 100 year flows of 20.9 cfs to the creek. In the 100 -year event, bypass flows of 5.1 cfs reaches Constitution and travels west to the sump inlet at the CBC crossing. Off-site basins OSA11, OSA12, and OSA13 contain portions of Constitution Avenue. These basins drain to the existing double $12^{\prime} \times 6^{\prime} \mathrm{CBC}$ under Constitution Avenue. Runoff from Basin OSA 14 drains easterly onto the southern portion of the proposed project located on the south side of Constitution Avenue with flows of $Q_{5}=14 \mathrm{cfs}$ and $Q_{100}=27 \mathrm{cfs}$. Basin OSA14 is currently undeveloped commercial property, just north of the Jessica Heights Filing Nol. 1 residential subdivision. A storm drain pipe from Jessica Heights delivers an additional $\mathrm{Q}_{5}=9.8 \mathrm{cfs}$ and $\mathrm{Q}_{100}=18.5 \mathrm{cfs}$ to the Tributary 6 channel. These flow enter the property and then travel to the creek flowing to the south.

## IV. ON-SITE DRAINAGE BASINS

The existing site drains southerly and easterly from the old Rock Island Railroad that bounds the property on the north and west. Tributary 6 to the East Fork of Sand Creek runs north to south through the property to Constitution Avenue. Offsite storm discharges from the Tributary enter onsite Basin A4 at Design Point 1 (the existing 7'x7' CBC). The existing channel area from the railroad culvert to existing Electronic Drive will be maintained in nearly existing condition. Basin A4 will contain single family residential development with open space components and produce runoff quantities of $\mathrm{Q}_{5}=41 \mathrm{cfs}$ and $\mathrm{Q}_{100}=83 \mathrm{cfs}$. Flows from Basin A 4 , along with the Tributary flows will drain to Design Point 2 at proposed Under Saddle Street. A new CBC beneath the street will allow runoff into Basin A9, where flows will enter a park area by way of an improved channel from the DP 2 culvert. Basin A9 contains single family residential development and open space. Developed runoff discharges of $Q_{5}=51 \mathrm{cfs}$ and $\mathrm{Q}_{100}=109 \mathrm{cfs}$ are generated by the basin. A storm


# JESSICA HEIGHTS FILING NO. 1 FINAL DRAINAGE REPORT 

April 27, 2005
Project No. 60742

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roads will be paved county streets within 50 to 80 foot of right-of-ways. Curb \& gutter will be constructed on the streets and route storm water flows to storm water inlets. Grading operations will be done in order to improve drainage conditions and to direct runoff to a desired location. Overlot grading will be necessary for subdivision development.

The included Drainage Map - Developed Condition shows the proposed road scheme, lot layout, and developed drainage basins with basin designations. The basin sizes and estimated peak storm runoff flows are shown in the table below and on the included map.

| Table 3.1 - Developed Condition Hydrologic Data |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Design Point or Basin | Cumulative Drainage Area (Ac) | 5-yr <br> Discharge <br> (cfs) | $100-\mathrm{yr}$ <br> Discharge <br> (cfs) |
|  | OSA | 0.15 | 0.6 | 1.1 |
|  | OSB | 0.46 | 1.8 | 3.3 |
|  | OSC | 0.88 | 3.3 | 6.0 |
|  | A1 | 0.96 | 2.0 | 4.0 |
|  | A2 | 5.25 | 3.2 | 7.6 |
|  | A3 | 0.51 | 1.4 | 2.8 |
|  | A4 | O. 32 | 1.3 | 2.3 |
|  | B1 | 2.27 | 4.1 | 8.2 |
| DP 2 | B2 | 0.70 | 2.0 | 3.8 |
| DP 3a | B3a | 0.77 | 1.7 | 3.4 |
| DP 3b | B3b | 2.53 | 4.8 | 9.6 |
|  | B3c | 1.35 | 3.2 | 6.6 |
| DP3 | B3 $+3 \mathrm{~b}+3 \mathrm{c}$ | 4.65 | 8.4 | 16.9 |
|  | B4 | 0.51 | 1.4 | 2.7 |
|  | B5 | 1.06 | 2.5 | 5.0 |
| DP5 | B6 | 0.53 | 1.4 | 2.6 |
| DP6 | B8 | 1.98 | 3.9 | 7.8 |


| Table 3.1 - Developed Condition Hydrologic Data |  |  |  |
| :---: | ---: | ---: | ---: |
| Design Point or Basin | Cumulative <br> Drainage Area <br> (Ac) | 5-yr <br> Discharge <br> (cfs) | 100-yr <br> Discharge <br> (cfs) |
| DP7 | B9 | 1.29 | 3.3 |

The future lot owners in Jessica Heights Filing No. 1 will adhere to proper construction technics and erosion control. The recommendations within this report need to be followed by the new lot owners. We also recommend that the existing down gradient lot owners not construct their homes in existing drainage swales or flow paths.

The developed conditions will route storm water flows over the site in sheet flow and shallow concentrated flow, depending on the topography and the contributing flow areas. These flows will be routed to the streets. The five and one hundred year frequency storm water flows will be collected and routed to the offsite earthen channel.

The nature of this development dictates that some lots will contribute storm flows onto other lots. This cross-lot drainage cannot be avoided. It is the responsibility of the individual lot owners and the building contractors to locate new structures on each lot so that the structures do not interfere with the proposed drainage pathways. The individual lot owners and contractors should provide positive drainage away from all structures. Individual lot owners are also responsible for maintaining their properties in such a manner that does not allow soil movement from one lot to another.

### 3.2 Offsite

The offsite pipe flow will continue to drain easterly. The pipe will be extended easterly and shall, in addition to the offsite flow, carry the proposed pipe flows from Jessica Heights. The small strip of land adjacent to the west boundary of the site shall continue to drain onto the site as defined by Basin OSC to the north and Basin OSB to the south. Basin C1, which is not being developed at this time, will continue to drain to the east. A berm and swale will direct runoff to the northeast where the flow will enter Hannah Ridge Drive and flow north. When Basin C1 is developed, all flows will be collected and piped to the east. Basin A2 is also not to be developed at this time. Basin A2 will continue to drain to the east.

### 3.3 Onsite

Basin OSC overland storm water flows enter the subdivision along the western boundary of Basin B1 and travel easterly overland to Great Sky Road. These flows then travel southerly in the street section of said Great Sky Road to a 10' inlet at Design Point No.1. The inlet intercepts $\mathrm{Q}_{5}=$ $4.5 \mathrm{cfs} / \mathrm{Q}_{100}=6.5 \mathrm{cfs}$ of the calculated storm water runoff.

Basin B2 overland storm water flows enter Great Sky Road from the adjacent lots and travel southerly in the street section of said Great Sky Road to a 5' inlet at Design Point No. 2. The inlet intercepts $\mathrm{Q}_{5}=1.4 \mathrm{cfs} / \mathrm{Q}_{100}=1.9 \mathrm{cfs}$ of the calculated storm water runoff. This collected inlet runoff flows via a $15^{\prime \prime}$ reinforced concrete pipe (RC Pipe) to the $10^{\prime}$ inlet at Design Point No. 1. The combined collected flows of Design Point No's $1 \& 2$ then flow in a $24^{\prime \prime}$ RC Pipe which connects to a Type I Manhole along with the extended existing 42" corrugated metal pipe in Palmer Park Boulevard. A 42" RC Pipe continues east in Palmer Park Boulevard.

Basins B3a, B3b and B3c overland storm water flows enter Buffalo Plains Court, Majestic plains Court, and Talus Ridge Drive. These flows travel via street section easterly, westerly, and


## Appendix F

## Drainage Maps

## URBAN COLLECTION AT PALMER VILLAGE EXISTING DRAINAGE MAP



| ExISting basin summary table |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | ${ }_{\text {a }}^{\substack{\text { area } \\ \text { ares }}}$ | Percent | $\mathrm{c}_{5}$ | $\mathrm{c}_{10}$ | $\underbrace{\text { tin }}_{\text {(min) }}$ | $\begin{aligned} & a_{6} \\ & (\text { (fs) } \end{aligned}$ | $\underbrace{}_{\substack{\text { amo } \\ \text { (fs) }}}$ |
|  |  |  |  |  |  |  |  |
| ${ }_{\text {ex1 }}^{\text {ex }}$ | 0.15 0.46 | ${ }_{2 \%}^{2 \%}$ | 0.08 0.08 | 0.35 <br> 0.35 | ${ }_{81} 7$ | 0.04 | 0.4 12 |
| Ex | 4.27 | 2\% | 0.08 | 0.35 | 14.2 | 1.2 | 9.0 |
| Ex4 | 1.62 | ${ }^{19 \%}$ | 0.22 | 0.45 | 17.9 | 1 | 4.0 |
| S | ${ }^{0.37}$ | ${ }^{82 \%}$ | 0.75 | 0.85 | 50 | 1.4 | 27 |
| Ex6 | 5.25 | ${ }_{2 \%}^{2 \%}$ | ${ }_{0} 0.08$ | 0.35 | 144 | 15 | 11. |


| EXISTING DESIGN POIN |  |  |
| :---: | :---: | :---: |
| DP | ${ }^{\circ}$ | $\mathrm{a}_{100}$ |
| 1 | 0.04 | 0.4 |
| 2 | 0.2 | 12 |
| 3 | 13 |  |
| 4 | 13 | 4.9 |
|  | 14 |  |
| 6 | 15 |  |



EXISTING DRAINAGE MAP
URBAN COIECTON AT
URBAN COLLECTION AT PAMMER VILLAGE JoB NO. 25149.0
$01 / 30 / 2020$
SHETT 1051
©
J•R EnGINEERING




[^0]:    Jennifer Irvine, P.E.
    County Engineer/ ECM Administrator

