LOT 8 AKERS ACRES

EL PASO COUNTY, CO FINAL DRAINAGE REPORT

Submittal Date: Issued for Review July 27, 2018 Revision Date: December 10, 2018

OWNER/APPLICANT

ABC SUPPLY CO

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CONSULTANT

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> OWA Project No. 18022 PCD File No. PPR1848

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CERTIFICATIONS

Design Engineer's Statement:

The attached drainage plan and report were prepared correct to the best of my knowledge and belief. Sai according to the criteria established by the County from conformity with the applicable master plan of the drainability caused by any negligent acts, errors or omissions.	d drainage report has been prepared for drainage reports and said report is in rainage basin. I accept responsibility for any
Name	Date
Owner/Developer's Statement:	
I, the owner/developer have read and will comply w drainage report and plan.	vith all of the requirements specified in this
By	Date
Title	
Address	
El Paso County:	
Filed in accordance with the requirements of the Dr Paso County Engineering Criteria Manual and Land	
Name:	Date
Jennifer Irvine, P.E.	
County Engineer/ECM Administrator	
Conditions:	

Obering, Wurth & Associates Consulting Civil Engineers Professional Land Surveyors

1046 Elkton Drive ° Colorado Springs, Colorado ° 80907 ° Phone 719-531-6200 ° Fax 719-531-6266

Please update the FIRM # and date to the current December 2018 date, typical.

Drainage Report for Lot 8 Akers Acres

Project No. 18022

FLOODPLAIN STATEMENT

To the best of my knowledge and belief, Lot 8 Akers Acres is not located within a designated 100 year floodplain as shown on FIRM map number 08041CO756-F (effective date March 17, 1997). A copy of a portion of the FIRM map is included as an attachment to this report.

Roland G. Obering, P.E. & P.L.S Colorado 13226

Roland G. Obering, F.E. & F.E.S Colorado 13220

INTRODUCTION

This report is not based on any previous know drainage studies. The goal of the project is to add

an approximate 300' x 300' asphalt yard directly to the east of the existing building.

The purpose of the following Final Drainage Report (FDR) is to present drainage improvements

for Lot 8 Akers Acres. Final design and sizing of structures is presented in this document.

Drainage improvements will include conveyance by a gutter that bisects the proposed asphalt

into a proposed curb opening inlet, then outfalling into a full spectrum water quality pond on the

east. This report encompasses approximately 1.97 acres for the yard addition. The Lot 8 Akers

Acres FDR is limited to the hydrology and hydraulics as it is routed through the proposed yard.

Historically this runoff is routed to the Sand Creek East Fork Subtributary.

This report includes an analysis of the proposed storm system, including the gutter, an inlet and

storm pipe. Also, the design for the full spectrum detention pond is presented.

The area of study is bounded by Asphalt Recovery Specialists to the north, Akers Drive to the

west, vacant land and Constitution Avenue to the south and Marksheffel Road to the east.

GENERAL PROPERTY DESCRIPTION

The proposed Lot 8 Akers Acres is approximately 9.33 acres in total and is located within

Section 32, Township 13 South, Range 65 West of the 6th Principal Meridian.

The proposed site is zoned in the El Paso County as "M"-Industrial (obsolete).

The topography of the surrounding area is typical of a high desert, short prairie grass with slopes

generally at 1% to 3%. The area generally sheet flows to the east or south across the vacant site

to the edges of the site where the slopes become steeper. From there the runoff is directed into

roadway drainage systems along Marksheffel and Constitution. At its closest point, Sand Creek

East Fork Subtributary is approximately 700' from the site.

The Lot 8 Akers Acres is located in the Sand Creek Street Drainage Basin. This basin has been

studied.

The development area is located in El Paso County, Colorado along the west side of Marksheffel

Road, north of Constitution Avenue and east of Akers Drive. Specifically, the area of study is

bounded by Asphalt Recovery Specialists to the north, Akers Drive to the west, vacant land and

Constitution Avenue to the south and Marksheffel Road to the east.

The Flood Insurance Rate Map (FIRM No. 08041CO756-F (effective date March 17, 1997))

indicates that there is not a floodplain on the proposed site. The closest floodplain shown is

approximately 700' to the east of the site. This floodplain is designated as "Zone X", which

identifies the area as an area of a 500-year flood, area of 100-year flooding with an average depth

less than 1 foot or a drainage area less than 1 square mile, or an area protected by levees from a

100-year flood. FEMA does not require any modifications to the floodplain maps when

construction is located in this zone area.

Soil Conservation Service soil survey records indicate the project area is covered by soils

classified in the Blakeland loamy sand, 1 to 9 percent slopes and the Blendon sandy loam, 0 to 3

percent slopes series, which are categorized in the Hydrological Group A and B, respectively.

Please see the attached Soil Report for more information.

EXISTING DRAINAGE CHARACTERISTICS

The existing site is covered with grasses, dirt-graded areas, asphalt and buildings. The area on

which the proposed asphalt lot will sit is covered with dirt-graded areas and asphalt. Slopes in

this vicinity range from approximately 1% to 3% and generally falls from the north to the

southeast via sheet flow. The runoff continues to travel offsite toward Marksheffel Road and

Constitution Avenues, where it is intercepted each roadway's storm system.

Pre-development peak flows and volumes for the proposed pond are derived from the Urban

Drainage and Flood Control District's UD Detention version 3.07. The program requires the

input of watershed area, slope, length, imperviousness and percentage of each hydrologic soils

group. Output from the program includes peak existing flows for the WQV, EURV, 2YR, 5YR,

10YR, 25YR, 50YR, 100YR and 500YR storms. The pre-development runoff rates for the 5

and 100 year storms are 0.01 cfs and 1.08 cfs respectfully. This is summarized on the page

entitled "Detention Basin Outlet Design", at the bottom in the table entitled "Routed Hydrograph

Results."

PROPOSED DRAINAGE CHARACTERISTICS

For the developed condition, the site will include only the 1.97 acres of paved storage yard.

Runoff will be collected in a gutter system, to a curb opening inlets, through RCP pipes and

oufalling into a full spectrum detention pond east of the site.

See the attached sheet C2: "Grading and Drainage Plan" later in this report for more information

including sub-basin areas, storm drain layout, and proposed grading.

For the other hydrologic calculations including those for inlets, pipes and gutters, the Rational

Method is used, consistent with the El Paso County requirements. This results in the peak

discharge rates from the proposed yard into proposed structure A6 at Q5=9.2 cfs and Q100=16.6

cfs. For more information see the "Hydrologic Summary" in the Appendix.

For the proposed full spectrum detention pond, proposed peak discharge rates are calculated

from UD Detention version 3.04. The proposed runoff rates for the 5 and 100 year storms are 4.6

cfs and 7.9 cfs respectfully. This is summarized on the page entitled "Detention Basin Outlet

Design", at the bottom in the table entitled "Routed Hydrograph Results."

DETENTION

A full-spectrum pond will be constructed as part of the project to provide water quality (WQCV)

& EURV) and attenuate peak flows from the ultimate developed condition. The pond will

include the construction of an approximately 10' high embankment, a trickle channel, and

excavation to achieve the desired storage. The outlet structure will consist of a rectangular

concrete riser, with orifice plate and three round orifices, and overflow grate discharging into an

18" RCP. A 5' emergency spillway will be also formed into the embankment. The pond will

contain 0.38 ac-ft of detention volume for the 100-year storm.

It is noted that this pond will act as a temporary sediment basin during construction.

UD-Dentention v304 shows the 5 and 100 year storms through the proposed pond yields 0.1 cfs

and 0.8 cfs for the 5 and 100-year storms, respectively. See the attached UDFCD drainage

calculations for further detail. This is summarized on the page entitled "Detention Basin Outlet

Design", at the bottom in the table entitled "Routed Hydrograph Results."

Comparing the existing and proposed discharge rates indicates that proposed outflow from the

pond will be less than existing runoff values for all storms but the 5, 10 and 25 year events.

However, both the pre-development inflows and peak outflows are extremely low at 0.012 cfs,

0.027 and 0.059 respectively.

The pond will be privately owned and maintained by the property owner. Maintenance access

will be provided via a graded ramp to the bottom of the pond from the proposed asphalt storage

yard.

EROSION CONTROL

During construction, best management practices for erosion control will be employed based on

the El Paso County criteria and the erosion control plans.

The detention pond will be configured to act as a temporary sediment basin during construction.

Upon adequate site stabilization, the pond will be converted for use as a full spectrum detention

water quality pond.

Silt fencing and vehicle-tracking controls will be in place to minimize erosion from the site. Silt

fencing will be placed along the downsloping portions of the site. This will prevent suspended

sediment from leaving the site during construction. Silt fencing is to remain in place until

landscaping and vegetation is reestablished after completion of construction.

Best erosion control practices will be utilized as deemed necessary by the Contractor or Engineer

and are not limited to the measures described above.

DRAINAGE FEES

This property has already been platted and drainage fee obligations have previously been met.

The drainage fee has not been previously paid. Drainage fees are not due with this application because it is not a

final plat application. Please revise.

CONCLUSION

The proposed drainage design for the Lot 8 Akers Acres will be effective to convey and control storm runoff. With the detention provided, there should be no anticipated adverse effects to downstream properties. This final drainage report for the site is in accordance with Section 4.4 of the Drainage Criteria manual. The following pages include calculations and drainage maps in support of the design.

Section I.7.2 of the Engineering Criteria Manual discusses BMP selections. The selection of appropriate BMPs is based on the characteristics of the site and potential pollutants. The Four-Step Process provides a method of going through the selection process. The four step process states *All sites defined as "New Development and Significant Redevelopment" and all stormwater quality detention, as listed above in Section I.7.1.B shall address stormwater quality by providing the WQCV.* The new storage lot will be collected on the east side in a sag inlet and directed to the full spectrum extended detention basin (EDB). The EDB is mentioned in Step 3 of the selection process, which is to provide water quality capture volume (WQCV). See the details on the Grading and Erosion Control Plans for the EDB details.

Step 1 of the selection process is employ runoff reduction practices and "minimizing directly connected impervious areas" (MDCIA). The principal behind MDCIA is twofold -- to reduce impervious areas and to route runoff from impervious surfaces over grassy areas to slow down runoff and promote infiltration. The use of grass swales instead of storm sewers, like grass buffers, slows down runoff and promotes infiltration, also reducing effective imperviousness. It also may reduce the size and cost of downstream storm sewers and detention. The ABC site uses various landscape unpaved areas to do slow down runoff and promote infiltration.

Where are these landscaped features located on the site? Based on the GEC, it appears that the drainage area is entirely asphalt.

Step 2 of the four step selection process will stabilize drainage ways. Within drainage ways, natural and manmade, erosion can be a major source of sediment and associated constituents,

such as phosphorus. Natural drainage ways are often subject to bed and bank erosion when urbanizing areas increase the frequency, rate, and volume of runoff. Therefore, drainage ways are required to be stabilized. The outlet channel from the EDB will be stabilized with riprap and filter fabric. See the details on the Grading and Erosion Control Plans.

Step 4 of the four step selection process considers the need for industrial and commercial BMPs. If a new development or significant redevelopment activity is planned for an industrial or commercial site, the need for specialized BMPs must be considered. Two approaches are covering of storage/handling areas, and spill containment and control. Since this site will only store building materials such as siding, no spill containment measures are proposed.

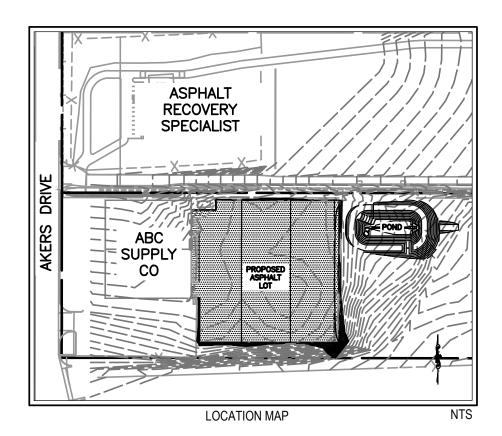
Is the outlet channel the only drainage way on the site? Identify if there are any other drainage ways on site. Based on the GEC it appears that there is a swale on the north site of the lot.

APPENDICES

VICINITY AND LOCATION MAPS



VICINITY MAP N



VICINITY AND LOCATION MAPS

RATIONAL METHOD CALCULATIONS

Hydrologic Summary

Lot 8 Akers Acres Proposed Conditions

Basin	Area	Тс	C5	C100	I5	I100	Q5	Q100
To Inlet A6	1.97	5.00	0.90	0.96	5.20	8.80	9.22	16.64
Total	0.00							



WEIGHTED RATIONAL COEFFICIENT Lot 8 Akers Acres Proposed Conditions 5 Year 100 Year Asphalt Lot Area (AC) CxA CxA Light Industrial 1.97 0.90 1.77 0.96 1.89 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 P-2 TOTALS 1.97 1.77 1.89 0.90 0.96 Cw TOTAL 1.97 NOTE: HYDROLOGIC SOIL TYPE A.

							Time of	Concentra	tion							
							Lot 8 Akers Ac	res Proposed C	onditions		<u> </u>					
																,
			OVERLA	ND FLOW							TRAVEL TIME					
DESIGN POINT	C5	D _{OVERLAND}	ELEV _{UPPER} OVERLAND PATH	ELEV LOWER OVERLAND PATH	S _{OVERLAND}	Ti _{overland}	$ m L_{TOTALFLOWPATH}$	L CHANNEL FLOW	ELEV _{UPPER} CHANNEL PATH	ELEV _{LOWER} CHANNEL PATH	Н	S0	Cv	V	Tt	TC
		FT	FT	FT	%	MIN	FT	FT	FT	FT	FT	%		FPS	MIN	MIN
To Inlet A3	0.90	289.00	6483.00	6480.13	1	1.35	290.00	1.00	6480.13	6480.00	0.13	13.00%	5.0	1.80	0.01	10.00



Hydrology Chapter 6

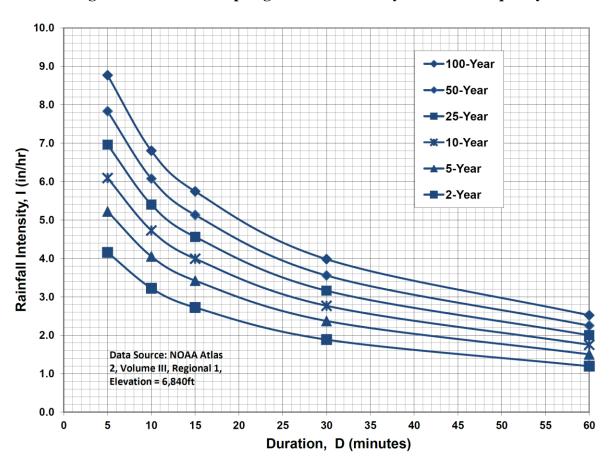


Figure 6-5. Colorado Springs Rainfall Intensity Duration Frequency

IDF Equations

$$I_{100} = -2.52 \ln(\text{*D}) + 12.735$$

$$I_{50} = -2.25 \ln(\text{*D}) + 11.375$$

$$I_{25} = -2.00 \ln(\text{xD}) + 10.111$$

$$I_{10} = -1.75 \ln(\text{xD}) + 8.847$$

$$I_5 = -1.50 \ln(\text{xD}) + 7.583$$

$$I_2 = -1.19 \ln(\text{xD}) + 6.035$$

Note: Values calculated by equations may not precisely duplicate values read from figure. Chapter 6 Hydrology

Table 6-6. Runoff Coefficients for Rational Method

(Source: UDFCD 2001)

Land Use or Surface	Percent						Runoff Co	efficients					
Characteristics	Impervious	2-у	ear	5-у	ear	10-	year	25-	/ear	50- ₁	/ear	100-	year
		HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D
Business													
Commercial Areas	95	0.79	0.80	0.81	0.82	0.83	0.84	0.85	0.87	0.87	0.88	0.88	0.89
Neighborhood Areas	70	0.45	0.49	0.49	0.53	0.53	0.57	0.58	0.62	0.60	0.65	0.62	0.68
Residential													
1/8 Acre or less	65	0.41	0.45	0.45	0.49	0.49	0.54	0.54	0.59	0.57	0.62	0.59	0.65
1/4 Acre	40	0.23	0.28	0.30	0.35	0.36	0.42	0.42	0.50	0.46	0.54	0.50	0.58
1/3 Acre	30	0.18	0.22	0.25	0.30	0.32	0.38	0.39	0.47	0.43	0.52	0.47	0.57
1/2 Acre	25	0.15	0.20	0.22	0.28	0.30	0.36	0.37	0.46	0.41	0.51	0.46	0.56
1 Acre	20	0.12	0.17	0.20	0.26	0.27	0.34	0.35	0.44	0.40	0.50	0.44	0.55
Industrial													
Light Areas	80	0.57	0.60	0.59	0.63	0.63	0.66	0.66	0.70	0.68	0.72	0.70	0.74
Heavy Areas	90	0.71	0.73	0.73	0.75	0.75	0.77	0.78	0.80	0.80	0.82	0.81	0.83
Parks and Cemeteries	7	0.05	0.09	0.12	0.19	0.20	0.29	0.30	0.40	0.34	0.46	0.39	0.52
Playgrounds	13	0.07	0.13	0.16	0.23	0.24	0.31	0.32	0.42	0.37	0.48	0.41	0.54
Railroad Yard Areas	40	0.23	0.28	0.30	0.35	0.36	0.42	0.42	0.50	0.46	0.54	0.50	0.58
Undeveloped Areas													
Historic Flow Analysis Greenbelts, Agriculture	2	0.03	0.05	0.09	0.16	0.17	0.26	0.26	0.38	0.31	0.45	0.36	0.51
Pasture/Meadow	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50
Forest	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50
Exposed Rock	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Offsite Flow Analysis (when landuse is undefined)	45	0.26	0.31	0.32	0.37	0.38	0.44	0.44	0.51	0.48	0.55	0.51	0.59
Streets													
Paved	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Gravel	80	0.57	0.60	0.59	0.63	0.63	0.66	0.66	0.70	0.68	0.72	0.70	0.74
Drive and Walks	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Roofs	90	0.71	0.73	0.73	0.75	0.75	0.77	0.78	0.80	0.80	0.82	0.81	0.83
Lawns	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50

3.2 Time of Concentration

One of the basic assumptions underlying the Rational Method is that runoff is a function of the average rainfall rate during the time required for water to flow from the hydraulically most remote part of the drainage area under consideration to the design point. However, in practice, the time of concentration can be an empirical value that results in reasonable and acceptable peak flow calculations.

For urban areas, the time of concentration (t_c) consists of an initial time or overland flow time (t_i) plus the travel time (t_t) in the storm sewer, paved gutter, roadside drainage ditch, or drainage channel. For non-urban areas, the time of concentration consists of an overland flow time (t_i) plus the time of travel in a concentrated form, such as a swale or drainageway. The travel portion (t_i) of the time of concentration can be estimated from the hydraulic properties of the storm sewer, gutter, swale, ditch, or drainageway. Initial time, on the other hand, will vary with surface slope, depression storage, surface cover, antecedent rainfall, and infiltration capacity of the soil, as well as distance of surface flow. The time of concentration is represented by Equation 6-7 for both urban and non-urban areas.

INLET & STORM DRAIN CALCULATIONS

Inlet Report Q5

Line No.	Inlet ID	Area	Inlet Time	Int.	Runoff Coeff.	Q = CIA	Q Carry- over	Q Captured	Q Bypassed	Junct Type	Curb Height	Curb Length	Grate Area	Grate Length	Grate Width	Gutter Slope	Gutter Width	Cross Slope, Sw	Cross Slope, Sx	Local Depr.	Inlet Depth	Inlet Spread	Gutter Depth	Gutter Spread	Bypass Line No.
		(ac)	(min)	(in/hr)	(C)	(cfs)	(cfs)	(cfs)	(cfs)		(in)	(ft)	(sqft)	(ft)	(ft)	(ft/ft)	(ft)	(ft/ft)	(ft/ft)	(in)	(ft)	(ft)	(ft)	(ft)	
1	A5	0.00	0.0	0.00	0.00	0.00				MH															
2	A6	2.07	5.0	5.19	0.90	9.67	0.00	9.67	0.00	Curb	6.0	10.00				Sag	2.00	0.080	0.010	1.0	0.54	31.72	0.46	31.72	Sag

Inlet Report Q100

Line No.	Inlet ID	Area	Inlet Time	Int.	Runoff Coeff.	Q = CIA	Q Carry- over	Q Captured	Q Bypassed	Junct Type	Curb Height	Curb Length	Grate Area	Grate Length	Grate Width	Gutter Slope	Gutter Width	Cross Slope, Sw	Cross Slope, Sx	Local Depr.	Inlet Depth	Inlet Spread	Gutter Depth	Gutter Spread	Bypass Line No.
		(ac)	(min)	(in/hr)	(C)	(cfs)	(cfs)	(cfs)	(cfs)		(in)	(ft)	(sqft)	(ft)	(ft)	(ft/ft)	(ft)	(ft/ft)	(ft/ft)	(in)	(ft)	(ft)	(ft)	(ft)	
1	A5	0.00	0.0	0.00	0.00	0.00				MH															
2	A6	2.07	5.0	9.00	0.90	16.76	0.00	16.76	0.00	Curb	6.0	10.00				Sag	2.00	0.080	0.010	1.0	0.74	43.62	0.66	43.62	Sag

Pipe Report Q5

Line	To Line	Line Length	Incr. Area	Total Area		Incr C x A	Total C x A	Inlet Time	Time Conc	Rnfal Int	Total Runoff	Adnl Flow	Total Flow	Capac Full	Veloc	Pipe Size	Pipe Slope	Inv Elev Dn	Inv Elev Up	HGL Dn	HGL Up	Grnd/Rim Dn	Grnd/Rim Up	Line ID
		(ft)	(ac)	(ac)	(C)			(min)	(min)	(in/hr)	(cfs)	(cfs)	(cfs)	(cfs)	(ft/s)	(in)	(%)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	
1	Outfall	68.00	0.00	2.07	0.00	0.00	1.86	0.0	5.1	5.2	9.64	0.00	9.64	24.43	6.32	18	5.41	6469.61	6473.29	6470.83	6474.49	6471.82	6475.09	P3
2	1	25.00	2.07	2.07	0.90	1.86	1.86	5.0	5.0	5.2	9.67	0.00	9.67	24.49	6.39	18	5.44	6473.29	6474.65	6474.49	6475.85	6475.09	6479.62	P5
-																								

Pipe Report Q100

Line	To Line	Line Length	Incr. Area	Total Area	Coeff.	Incr C x A	Total C x A		Time Conc		Total Runoff			Capac Full		3126		Inv Elev Dn	Inv Elev Up	HGL Dn	HGL Up	Dn	Grnd/Rim Up	Line ID
		Drag colu	mn to m	ove)	(C)			(min)	(min)	(in/hr)	(cfs)	(cfs)	(cfs)	(cfs)	(ft/s)	(in)	(%)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	
1		68.00		2.07	0.00	0.00	1.86	0.0	5.0	9.0	16.72	0.00	16.72	24.43	10.23	18	5.41	6469.61	6473.29	6470.83	6474.73	6471.82	6475.09	P3
2	1	25.00	2.07	2.07	0.90	1.86	1.86	5.0	5.0	9.0	16.76	0.00	16.76	24.49	9.63	18	5.44	6473.29	6474.65	6474.73	6476.09	6475.09	6479.62	P5

FULL SPECTRUM DETENTION CALCULATIONS

	Design Procedure Form:	Extended Detention Basin (EDB)
		P (Version 3.07, March 2018) Sheet 1 of 3
Designer:	CLD	
Company: Date:	OWA December 5, 2018	
Project:	Akers Acres Lot 8	
Location:	ABC Supply CO	
1. Basin Storage \	Volume	
A) Effective Imp	perviousness of Tributary Area, I _a	I _a = 100.0 %
B) Tributary Are	ea's Imperviousness Ratio (i = I _a / 100)	i = 1.000
C) Contributing	g Watershed Area	Area = 1.970 ac
	heds Outside of the Denver Region, Depth of Average ducing Storm	d ₆ = in
		Choose One —
E) Design Con (Select EUR	N when also designing for flood control)	O Water Quality Capture Volume (WQCV)
		Excess Urban Runoff Volume (EURV)
E) Docima Val	umo (MOCV) Pasad on 40 hour Pasis Time	V 0.002 20.4
	ıme (WQCV) Based on 40-hour Drain Time 1.0 * (0.91 * i³ - 1.19 * i² + 0.78 * i) / 12 * Area)	V _{DESIGN} = 0.082 ac-ft
G) For Waters	heds Outside of the Denver Region,	V _{DESIGN OTHER} = ac-ft
Water Qual	ity Capture Volume (WQCV) Design Volume	
	$_{\rm IR} = (d_6^*(V_{\rm DESIGN}/0.43))$	
	of Water Quality Capture Volume (WQCV) Design Volume fferent WQCV Design Volume is desired)	V _{DESIGN USER} = ac-ft
	ologic Soil Groups of Tributary Watershed age of Watershed consisting of Type A Soils	HSG _A = 100 %
	age of Watershed consisting of Type B Soils tage of Watershed consisting of Type C/D Soils	$HSG_B = 0$ $HSG_{CD} = 0$ %
		1100 CB -
	an Runoff Volume (EURV) Design Volume x: EURV _A = 1.68 * i ^{1.28}	EURV _{DESIGN} = 0.276 ac-f t
For HSG B	EEURV _B = 1.36 * i ^{1.08} E/D: EURV _{C/D} = 1.20 * i ^{1.08}	
	of Excess Urban Runoff Volume (EURV) Design Volume fferent EURV Design Volume is desired)	EURV _{DESIGN USER} = ac-f t
	ength to Width Ratio	L:W= 4.0 :1
(A basin length	to width ratio of at least 2:1 will improve TSS reduction.)	
Basin Side Slop	pes	
	num Side Slopes	Z = 3.00 ft / ft
,	distance per unit vertical, 4:1 or flatter preferred)	DIFFICULT TO MAINTAIN, INCREASE WHERE POSSIBLE
4. Inlet		Forebay
	eans of providing energy dissipation at concentrated	
inflow locati	ions:	
5. Forebay		
,	who Million	V
A) Minimum Fo (V _{FMIN}	orebay Volume =1%of the WQCV)	V _{FMIN} = 0.001 ac-ft
B) Actual Forel		V _F = 0.001 ac-ft
		·, 0.00.
C) Forebay Dep (D _F	pth = <u>12</u> inch maximum)	D _F = 6.0 in
D) Forebay Dis	· · · · · · · · · · · · · · · · · · ·	_
		0 - 46.60
	ed 100-year Peak Discharge	Q ₁₀₀ = 16.60 cfs
ii) Forebay (Q _F = 0.0	Discharge Design Flow 12 * Q ₁₀₀)	Q _F = 0.33 cfs
E) Forebay Dise	charge besign	Choose One O Berm With Pipe Flow too small for berm w/ pipe
		Wall with Rect. Notch
		O Wall with V-Notch Weir
F) Discharge Pi	ipe Size (minimum 8-inches)	Calculated D _P =
G) Rectangular		Calculated W _N = 4.6 in
O) Necialiyulal	ITOIGH TTIGHT	Galodiated VV

Akers UD-BMP_v3.07.xlsm, EDB 12/5/2018, 10:25 AM

	Design Procedure Form: I	Extended Detention Basin (EDB) Sheet 2 of 3
Designer: Company: Date: Project: Location:	CLD OWA December 5, 2018 Akers Acres Lot 8 ABC Supply CO	Sileet 2 01 3
Trickle Channel A) Type of Trick F) Slope of Trick	kle Channel	Choose One © Concrete O Soft Bottom S = 0.0100 ft / ft
	cropool (2.5-feet minimum) a of Micropool (10 ft ² minimum)	$D_{M} = 2.5$ $A_{M} = 16$ $Sq ft$ $Choose One$ $© Orifice Plate$ $Other (Describe):$
D) Smallest Dir (Use UD-Detent E) Total Outlet A	,	$D_{crifice} = $
(Minimum red B) Minimum Initi (Minimum vol	e Volume ial Surcharge Volume commended depth is 4 inches) ial Surcharge Volume lume of 0.3% of the WQCV) arge Provided Above Micropool	$D_{IS} = 4$ in $V_{IS} = 5.3$ cu ft
B) Type of Screin the USDCM, total screen are C) Ratio of Total D) Total Water (E) Depth of Des (Based on c	ty Screen Open Area: A ₁ = A ₁ * 38.5*(e ^{-0.095D}) ten (If specifying an alternative to the materials recommended indicate "other" and enter the ratio of the total open are to the for the material specified.) Other (Y/N): N If Open Area to Total Area (only for type 'Other') Quality Screen Area (based on screen type) sign Volume (EURV or WQCV) design concept chosen under 1E)	A _t = 103 square inches S.S. Well Screen with 60% Open Area User Ratio =
	ter Quality Screen Opening (W _{opening}) inches is recommended)	W _{opening} = 12.0 inches VALUE LESS THAN RECOMMENDED MIN. WIDTH. WIDTH HAS BEEN SET TO 12 INCHES.

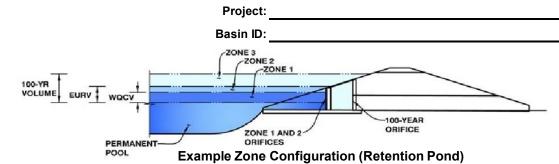
Akers UD-BMP_v3.07.xlsm, EDB 12/5/2018, 10:25 AM

	Design Procedure Form:	Extended Detention Basin (EDB)
Designer: Company: Date: Project: Location:	CLD OWA December 5, 2018 Akers Acres Lot 8 ABC Supply CO	Sheet 3 of 3
B) Slope of O	embankment protection for 100-year and greater overtopping: everflow Embankment Il distance per unit vertical, 4:1 or flatter preferred)	Emergency spillway has 6" compacted fill over 12" riprap TY VL over 12" granualr bedding TY 2 Ze = 4.00 ft / ft
11. Vegetation		Choose One ○ Irrigated ● Not Irrigated
12. Access A) Describe S	Sediment Removal Procedures	Access ramp provided in NW corner. Equiment access bottom of pond to clean sediment and debris
,		
Notes:		

Akers UD-BMP_v3.07.xlsm, EDB 12/5/2018, 10:25 AM

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

UD-Detention, Version 3.07 (February 2017)



Required Volume Calculation

• • • • • • • • • • • • • • • • • • • •		_
Selected BMP Type =	EDB	
Watershed Area =	1.97	acres
Watershed Length =	300	ft
Watershed Slope =	0.010	ft/ft
Watershed Imperviousness =	100.00%	percent
Percentage Hydrologic Soil Group A =	100.0%	percent
Percentage Hydrologic Soil Group B =	0.0%	percent
Percentage Hydrologic Soil Groups C/D =	0.0%	percent
Desired WQCV Drain Time =	40.0	hours
Location for 1-hr Rainfall Depths =	User Input	ī

Desired WQCV Drain Time =	40.0	hours
Location for 1-hr Rainfall Depths =	User Input	
Water Quality Capture Volume (WQCV) =	0.082	acre-feet
Excess Urban Runoff Volume (EURV) =	0.276	acre-feet
2-yr Runoff Volume (P1 = 1.19 in.) =	0.192	acre-feet
5-yr Runoff Volume (P1 = 1.5 in.) =	0.248	acre-feet
10-yr Runoff Volume (P1 = 1.75 in.) =	0.296	acre-feet
25-yr Runoff Volume (P1 = 2 in.) =	0.343	acre-feet
50-yr Runoff Volume (P1 = 2.25 in.) =	0.381	acre-feet
100-yr Runoff Volume (P1 = 2.52 in.) =	0.432	acre-feet
500-yr Runoff Volume (P1 = 3.29 in.) =	0.570	acre-feet
Approximate 2-yr Detention Volume =	0.183	acre-feet
Approximate 5-yr Detention Volume =	0.236	acre-feet
Approximate 10-yr Detention Volume =	0.279	acre-feet
Approximate 25-yr Detention Volume =	0.327	acre-feet
Approximate 50-yr Detention Volume =	0.355	acre-feet
Approximate 100-yr Detention Volume =	0.377	acre-feet

Optional User Override

1-hr Precipitation					
1.19	inches				
1.50	inches				
1.75	inches				
2.00	inches				
2.25	inches				
2.52	inches				
3.29	inches				
	="				

Stage-Storage Calculation

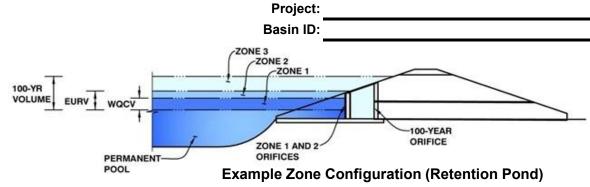
_		•
acre-feet	0.082	Zone 1 Volume (WQCV) =
acre-feet	0.194	Zone 2 Volume (EURV - Zone 1) =
acre-feet	0.101	Zone 3 Volume (100-year - Zones 1 & 2) =
acre-feet	0.377	Total Detention Basin Volume =
ft^3	11	Initial Surcharge Volume (ISV) =
ft	0.50	Initial Surcharge Depth (ISD) =
ft	6.00	Total Available Detention Depth (H_{total}) =
ft	0.50	Depth of Trickle Channel (H_{TC}) =
ft/ft	0.010	Slope of Trickle Channel (S_{TC}) =
H:V	3	Slopes of Main Basin Sides (S_{main}) =
	4	Basin Length-to-Width Ratio $(R_{L/W})$ =

Initial Surcharge Area (A _{ISV}) =	21	ft^2
Surcharge Volume Length (L_{ISV}) =	4.6	ft
Surcharge Volume Width (W_{ISV}) =	4.6	ft
Depth of Basin Floor (H_{FLOOR}) =	0.80	ft
Length of Basin Floor (L_{FLOOR}) =	87.5	ft
Width of Basin Floor (W_{FLOOR}) =	24.7	ft
Area of Basin Floor (A_{FLOOR}) =	2,165	ft^2
Volume of Basin Floor (V_{FLOOR}) =	644	ft^3
Depth of Main Basin (H_{MAIN}) =	4.20	ft
Length of Main Basin (L_{MAIN}) =	112.7	ft
Width of Main Basin (W_{MAIN}) =	49.9	ft
Area of Main Basin (A_{MAIN}) =	5,623	ft^2
Volume of Main Basin (V_{MAIN}) =	15,771	ft^3
Calculated Total Basin Volume (V _{total}) =	0.377	acre-feet

Stage - Storage Description Top of Micropool	Stage (ft) 0.00	Optional Override Stage (ft)	Length (ft) 4.6	Width (ft)	Area (ft^2) 21	Optional Override Area (ft^2)	Area (acre) 0.000	Volume (ft^3)	Volum (ac-ft)
ISV			4.6		21			44	0.000
15 V	0.50			4.6			0.000	11	0.000
	0.60		4.6	4.6	21		0.000	13	0.000
	0.70		4.6	4.6 4.6	21		0.000	15 17	0.000
	0.80		4.6	4.6	21		0.000	19	0.000
	1.00		4.6	4.6	21		0.000	21	0.000
	1.10		13.9	6.9	96		0.002	26	0.001
	1.20		24.2	9.4	227		0.002	42	0.001
	1.30		34.5	11.9	410		0.009	74	0.002
	1.40		44.8	14.4	644		0.015	126	0.003
	1.50		55.1	16.9	930		0.021	204	0.005
	1.60		65.4	19.4	1,268		0.029	314	0.007
	1.70		75.7	21.9	1,656		0.038	459	0.011
	1.80		86.0	24.4	2,097		0.048	647	0.015
Floor	1.80		87.0	24.6	2,144		0.049	668	0.015
	1.90		88.0	25.3	2,222		0.051	865	0.020
	2.00		88.6	25.9	2,291		0.053	1,091	0.025
	2.10		89.3	26.5	2,367		0.054	1,347	0.031
	2.20		89.9	27.1	2,437		0.056	1,587	0.036
	2.30		90.5	27.7	2,507		0.058	1,834	0.042
	2.40		91.1	28.3	2,578		0.059	2,088	0.048
	2.50		91.7	28.9	2,650		0.061	2,350	0.054
	2.60		92.3	29.5	2,723		0.063	2,618	0.060
	2.70		92.9	30.1	2,796		0.064	2,894	0.066
	2.80		93.5	30.7	2,871		0.066	3,178	0.073
	2.90		94.1	31.3	2,945		0.068	3,469	0.080
Zone 1 (WQCV)	2.94		94.3	31.6	2,976		0.068	3,587	0.082
,	3.00		94.7	31.9	3,021		0.069	3,767	0.086
	3.10		95.3	32.5	3,097		0.071	4,073	0.093
	3.20		95.9	33.1	3,174		0.073	4,386	0.101
	3.30		96.5	33.7	3,252		0.075	4,708	0.108
	3.40		97.1	34.3	3,331		0.076	5,037	0.116
	3.50		97.7	34.9	3,410		0.078	5,374	0.123
	3.60		98.3	35.5	3,490		0.080	5,719	0.131
	3.70		98.9	36.1	3,570		0.082	6,072	0.139
	3.80		99.5	36.7	3,652		0.084	6,433	0.148
	3.90		100.1	37.3	3,734		0.086	6,802	0.156
	4.00		100.7	37.9	3,817		0.088	7,180	0.165
	4.10		101.3	38.5	3,900		0.090	7,566	0.174
	4.20		101.9	39.1	3,984		0.091	7,960	0.183
	4.30		102.5	39.7	4,069		0.093	8,362	0.192
	4.40		103.1	40.3	4,155		0.095	8,774	0.201
	4.50		103.7	40.9	4,241		0.097	9,193	0.211
	4.60		104.3	41.5	4,328		0.099	9,622	0.221
	4.70		104.9	42.1	4,416		0.101	10,059	0.231
	4.80		105.5	42.7	4,505		0.103	10,505	0.241
	4.90		106.1	43.3	4,594		0.105	10,960	0.252
	5.00		106.7	43.9	4,684		0.108	11,424	0.262
	5.10		107.3	44.5	4,775		0.110	11,897	0.273
Zone 2 (EURV)	5.13		107.4	44.7	4,802		0.110	12,041	0.276
	5.20		107.9	45.1	4,866		0.112	12,379	0.284
	5.30		108.5	45.7	4,958		0.114	12,870	0.295
	5.40		109.1	46.3	5,051		0.116	13,371	0.307
	5.50 5.60		109.7 110.3	46.9 47.5	5,145 5,239		0.118 0.120	13,880 14,400	0.319
	5.70		110.9	48.1	5,334		0.122	14,928	0.343
	5.80 5.90		111.5 112.1	48.7 49.3	5,430 5,526		0.125 0.127	15,466 16,014	0.355
one 3 (100-year)	5.98		112.5	49.8	5,604		0.129	16,459	0.378
 -	6.00 6.10		112.7 113.3	49.9 50.5	5,623 5,721		0.129 0.131	16,572	0.380
	6.20		113.9	51.1	5,820		0.134	17,139 17,716	0.407
	6.30		114.5	51.7	5,919		0.136	18,303	0.420
	6.40 6.50		115.1 115.7	52.3 52.9	6,019 6,120		0.138 0.140	18,900 19,507	0.434 0.448
	6.60		116.3	53.5	6,222		0.143	20,124	0.462
	6.70 6.80		116.9 117.5	54.1 54.7	6,324 6,427		0.145 0.148	20,751 21,389	0.476
	6.90		118.1	55.3	6,530		0.150	22,036	0.506
	7.00 7.10		118.7 119.3	55.9 56.5	6,635 6,740		0.152 0.155	22,695 23,363	0.521 0.536
	7.20		119.9	57.1	6,846		0.157	24,043	0.552
	7.30		120.5	57.7	6,952		0.160	24,733	0.568
	7.40 7.50		121.1 121.7	58.3 58.9	7,060 7,168		0.162 0.165	25,433 26,145	0.584 0.600
	7.60		122.3	59.5	7,276		0.167	26,867	0.617
	7.70 7.80		122.9 123.5	60.1 60.7	7,386 7,496		0.170 0.172	27,600 28,344	0.634 0.651
-	7.90		124.1	61.3	7,607		0.175	29,099	0.668
	8.00 8.10		124.7 125.3	61.9 62.5	7,718 7,831		0.177 0.180	29,865 30,643	0.686 0.703
	8.20		125.9	62.5	7,944		0.180	31,431	0.722
	8.30		126.5	63.7	8,057		0.185	32,231	0.740
	8.40 8.50		127.1 127.7	64.3 64.9	8,172 8,287		0.188 0.190	33,043 33,866	0.759 0.777
	8.60		128.3	65.5	8,403		0.193	34,700	0.797
	8.70 8.80		128.9 129.5	66.1 66.7	8,520 8,637		0.196 0.198	35,546 36,404	0.816
	8.90		130.1	67.3	8,755		0.201	37,274	0.856
	9.00		130.7	67.9	8,874		0.204	38,155	0.876
	9.10 9.20		131.3 131.9	68.5 69.1	8,993 9,113		0.206 0.209	39,049 39,954	0.896
	9.30		132.5	69.7	9,234		0.212	40,871	0.938
	9.40 9.50		133.1 133.7	70.3 70.9	9,356 9,478		0.215 0.218	41,801	0.960
			133.7 134.3	70.9	9,478		0.218	42,743 43,697	0.981 1.003
	9.60		134.3	11.5	3,002		0.220	TO,001	1.000

Detention Basin Outlet Structure Design

UD-Detention, Version 3.07 (February 2017)



		Stage (ft)	Zone Volume (ac-ft)	Outlet Type
	Zone 1 (WQCV)	2.94	0.082	Orifice Plate
	Zone 2 (EURV)	5.13	0.194	Orifice Plate
ļ	one 3 (100-year)	5.98	0.101	Weir&Pipe (Rect.)
			0.377	Total

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

at order aram outlet (typically asea to aram tractor in a rint ation sim)							
Underdrain Orifice Invert Depth =	N/A	ft (distance below the filtration media surface)					
Underdrain Orifice Diameter =	N/A	inches					

Calculated Parameters for Underdrai			
Underdrain Orifice Area =	N/A	ft ²	
Underdrain Orifice Centroid =	N/A	feet	

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

		(1) 11 12 13 14 15 16 16 16 16 16 16 16
Invert of Lowest Orifice =	0.00	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Orifice Plate =	5.13	ft (relative to basin bottom at Stage = 0 ft)
Orifice Plate: Orifice Vertical Spacing =	N/A	inches
Orifice Plate: Orifice Area per Row =	N/A	inches

Calcu	lated Parameters for	Plate
WQ Orifice Area per Row =	N/A	ft ²
Elliptical Half-Width =	N/A	feet
Elliptical Slot Centroid =	N/A	feet
Elliptical Slot Area =	N/A	ft ²

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

ia rotal Alba of Each Office from Indinibuted from Indinibuted									
	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)	
Stage of Orifice Centroid (ft)	0.00	1.70	3.40	5.10					
Orifice Area (sq. inches)	0.37	0.35	1.65	1.00					
Diameter (in)	11/16	11/16	1 7/16	1 2/16					
	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)	
Stage of Orifice Centroid (ft)									

User Input: Vertical Orifice (Circular or Rectangular)

Orifice Area (sq. inches)

	Not Selected	Not Selected	
Invert of Vertical Orifice =	N/A	N/A	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Vertical Orifice =	N/A	N/A	ft (relative to basin bottom at Stage = 0 ft)
Vertical Orifice Diameter =	N/A	N/A	inches

Calculated Parameters for Vertical Orifice							
Not Selected Not Selected							
Vertical Orifice Area =	N/A	N/A	ft ²				
Vertical Orifice Centroid =	N/A	N/A	fee				

User Input: Overflow Weir (Dropbox) and Grate (Flat or Sloped)

	Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	5.80	N/A	ft (relative to basin bottom at Stage = 0 ft)
Overflow Weir Front Edge Length =	5.00	N/A	feet
Overflow Weir Slope =	0.00	N/A	H:V (enter zero for flat grate)
Horiz. Length of Weir Sides =	4.00	N/A	feet
Overflow Grate Open Area % =	50%	N/A	%, grate open area/total area
Debris Clogging % =	50%	N/A	%
•			-

Calculated Parameters for Overflow Weir						
	Zone 3 Weir	Not Selected				
Height of Grate Upper Edge, H_t =	5.80	N/A	feet			
Over Flow Weir Slope Length =	4.00	N/A	feet			
Grate Open Area / 100-yr Orifice Area =	154.84	N/A	should be <u>></u> 4			
Overflow Grate Open Area w/o Debris =	10.00	N/A	ft ²			
Overflow Grate Open Area w/ Debris =	5.00	N/A	ft ²			
•			_			

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

	Zone 3 Rectangular	Not Selected	
Depth to Invert of Outlet Pipe =	0.50	N/A	ft (distance below basin bottom at Stage = 0 ft)
Rectangular Orifice Width =	3.10	N/A	inches
Rectangular Orifice Height =	3.00		inches Half-Ce

	Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate								
		Zone 3 Rectangular	Not Selected]					
age = 0 ft)	Outlet Orifice Area =	0.06	N/A	ft ²					
	Outlet Orifice Centroid =	0.13	N/A	feet					
Half-Central Ang	le of Restrictor Plate on Pipe =	N/A	N/A	radians					

User Input: Emergency Spillway (Rectangular or Trapezoidal)

) · · · · · · /	_
Spillway Invert Stage=	6.30	ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length =	5.00	feet
Spillway End Slopes =	4.00	H:V
Freeboard above Max Water Surface =	1.00	feet

Calcula	ted Parameters	for Spillway
ou Donth-	0.55	foot

Spillway Design Flow Depth=	0.55	feet
Stage at Top of Freeboard =	7.85	feet
Basin Area at Top of Freeboard =	0.17	acres
· · · · · · · · · · · · · · · · · · ·		

Routed I	Hydrograph	Results

Kouted Hydrograph Results_									
Design Storm Return Period =	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
One-Hour Rainfall Depth (in) =	0.53	1.07	1.19	1.50	1.75	2.00	2.25	2.52	3.29
Calculated Runoff Volume (acre-ft) =	0.082	0.276	0.192	0.248	0.296	0.343	0.381	0.432	0.570
OPTIONAL Override Runoff Volume (acre-ft) =									
Inflow Hydrograph Volume (acre-ft) =	0.081	0.275	0.192	0.247	0.296	0.342	0.381	0.431	0.569
Predevelopment Unit Peak Flow, q (cfs/acre) =	-	-	0.001	0.006	0.014	0.030	0.227	0.547	1.282
Predevelopment Peak Q (cfs) =	0.000	0.000	0.001	0.012	0.027	0.059	0.447	1.078	2.525
Peak Inflow Q (cfs) =	1.5	5.1	3.6	4.6	5.5	6.3	7.0	7.9	10.4
Peak Outflow Q (cfs) =	0.0	0.1	0.1	0.1	0.1	0.2	0.3	0.8	2.7
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	9.5	4.9	2.6	0.6	0.7	1.1
Structure Controlling Flow =	Plate	Plate	Plate	Plate	Plate	Plate	Overflow Grate 1	Outlet Plate 1	Spillway
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	0.0	0.1	0.1
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	39	67	60	65	69	71	73	72	70
Time to Drain 99% of Inflow Volume (hours) =	40	72	63	69	73	77	79	79	78
Maximum Ponding Depth (ft) =	2.86	4.98	4.18	4.73	5.16	5.54	5.83	5.99	6.53
Area at Maximum Ponding Depth (acres) =	0.07	0.11	0.09	0.10	0.11	0.12	0.13	0.13	0.14
Maximum Volume Stored (acre-ft) =	0.076	0.260	0.180	0.233	0.280	0.323	0.358	0.378	0.452
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SOIL REPORT & MAP



NRCS

Natural Resources Conservation Service A product of the National Cooperative Soil Survey, a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local participants

Custom Soil Resource Report for El Paso County Area, Colorado



Preface

Soil surveys contain information that affects land use planning in survey areas. They highlight soil limitations that affect various land uses and provide information about the properties of the soils in the survey areas. Soil surveys are designed for many different users, including farmers, ranchers, foresters, agronomists, urban planners, community officials, engineers, developers, builders, and home buyers. Also, conservationists, teachers, students, and specialists in recreation, waste disposal, and pollution control can use the surveys to help them understand, protect, or enhance the environment.

Various land use regulations of Federal, State, and local governments may impose special restrictions on land use or land treatment. Soil surveys identify soil properties that are used in making various land use or land treatment decisions. The information is intended to help the land users identify and reduce the effects of soil limitations on various land uses. The landowner or user is responsible for identifying and complying with existing laws and regulations.

Although soil survey information can be used for general farm, local, and wider area planning, onsite investigation is needed to supplement this information in some cases. Examples include soil quality assessments (http://www.nrcs.usda.gov/wps/portal/nrcs/main/soils/health/) and certain conservation and engineering applications. For more detailed information, contact your local USDA Service Center (https://offices.sc.egov.usda.gov/locator/app?agency=nrcs) or your NRCS State Soil Scientist (http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/contactus/?cid=nrcs142p2 053951).

Great differences in soil properties can occur within short distances. Some soils are seasonally wet or subject to flooding. Some are too unstable to be used as a foundation for buildings or roads. Clayey or wet soils are poorly suited to use as septic tank absorption fields. A high water table makes a soil poorly suited to basements or underground installations.

The National Cooperative Soil Survey is a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local agencies. The Natural Resources Conservation Service (NRCS) has leadership for the Federal part of the National Cooperative Soil Survey.

Information about soils is updated periodically. Updated information is available through the NRCS Web Soil Survey, the site for official soil survey information.

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How Soil Surveys Are Made

Soil surveys are made to provide information about the soils and miscellaneous areas in a specific area. They include a description of the soils and miscellaneous areas and their location on the landscape and tables that show soil properties and limitations affecting various uses. Soil scientists observed the steepness, length, and shape of the slopes; the general pattern of drainage; the kinds of crops and native plants; and the kinds of bedrock. They observed and described many soil profiles. A soil profile is the sequence of natural layers, or horizons, in a soil. The profile extends from the surface down into the unconsolidated material in which the soil formed or from the surface down to bedrock. The unconsolidated material is devoid of roots and other living organisms and has not been changed by other biological activity.

Currently, soils are mapped according to the boundaries of major land resource areas (MLRAs). MLRAs are geographically associated land resource units that share common characteristics related to physiography, geology, climate, water resources, soils, biological resources, and land uses (USDA, 2006). Soil survey areas typically consist of parts of one or more MLRA.

The soils and miscellaneous areas in a survey area occur in an orderly pattern that is related to the geology, landforms, relief, climate, and natural vegetation of the area. Each kind of soil and miscellaneous area is associated with a particular kind of landform or with a segment of the landform. By observing the soils and miscellaneous areas in the survey area and relating their position to specific segments of the landform, a soil scientist develops a concept, or model, of how they were formed. Thus, during mapping, this model enables the soil scientist to predict with a considerable degree of accuracy the kind of soil or miscellaneous area at a specific location on the landscape.

Commonly, individual soils on the landscape merge into one another as their characteristics gradually change. To construct an accurate soil map, however, soil scientists must determine the boundaries between the soils. They can observe only a limited number of soil profiles. Nevertheless, these observations, supplemented by an understanding of the soil-vegetation-landscape relationship, are sufficient to verify predictions of the kinds of soil in an area and to determine the boundaries.

Soil scientists recorded the characteristics of the soil profiles that they studied. They noted soil color, texture, size and shape of soil aggregates, kind and amount of rock fragments, distribution of plant roots, reaction, and other features that enable them to identify soils. After describing the soils in the survey area and determining their properties, the soil scientists assigned the soils to taxonomic classes (units). Taxonomic classes are concepts. Each taxonomic class has a set of soil characteristics with precisely defined limits. The classes are used as a basis for comparison to classify soils systematically. Soil taxonomy, the system of taxonomic classification used in the United States, is based mainly on the kind and character of soil properties and the arrangement of horizons within the profile. After the soil

Custom Soil Resource Report

scientists classified and named the soils in the survey area, they compared the individual soils with similar soils in the same taxonomic class in other areas so that they could confirm data and assemble additional data based on experience and research.

The objective of soil mapping is not to delineate pure map unit components; the objective is to separate the landscape into landforms or landform segments that have similar use and management requirements. Each map unit is defined by a unique combination of soil components and/or miscellaneous areas in predictable proportions. Some components may be highly contrasting to the other components of the map unit. The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The delineation of such landforms and landform segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, onsite investigation is needed to define and locate the soils and miscellaneous areas.

Soil scientists make many field observations in the process of producing a soil map. The frequency of observation is dependent upon several factors, including scale of mapping, intensity of mapping, design of map units, complexity of the landscape, and experience of the soil scientist. Observations are made to test and refine the soil-landscape model and predictions and to verify the classification of the soils at specific locations. Once the soil-landscape model is refined, a significantly smaller number of measurements of individual soil properties are made and recorded. These measurements may include field measurements, such as those for color, depth to bedrock, and texture, and laboratory measurements, such as those for content of sand, silt, clay, salt, and other components. Properties of each soil typically vary from one point to another across the landscape.

Observations for map unit components are aggregated to develop ranges of characteristics for the components. The aggregated values are presented. Direct measurements do not exist for every property presented for every map unit component. Values for some properties are estimated from combinations of other properties.

While a soil survey is in progress, samples of some of the soils in the area generally are collected for laboratory analyses and for engineering tests. Soil scientists interpret the data from these analyses and tests as well as the field-observed characteristics and the soil properties to determine the expected behavior of the soils under different uses. Interpretations for all of the soils are field tested through observation of the soils in different uses and under different levels of management. Some interpretations are modified to fit local conditions, and some new interpretations are developed to meet local needs. Data are assembled from other sources, such as research information, production records, and field experience of specialists. For example, data on crop yields under defined levels of management are assembled from farm records and from field or plot experiments on the same kinds of soil.

Predictions about soil behavior are based not only on soil properties but also on such variables as climate and biological activity. Soil conditions are predictable over long periods of time, but they are not predictable from year to year. For example, soil scientists can predict with a fairly high degree of accuracy that a given soil will have a high water table within certain depths in most years, but they cannot predict that a high water table will always be at a specific level in the soil on a specific date.

After soil scientists located and identified the significant natural bodies of soil in the survey area, they drew the boundaries of these bodies on aerial photographs and

identified each as a specific map unit. Aerial photographs show trees, buildings, fields, roads, and rivers, all of which help in locating boundaries accurately.

Soil Map

The soil map section includes the soil map for the defined area of interest, a list of soil map units on the map and extent of each map unit, and cartographic symbols displayed on the map. Also presented are various metadata about data used to produce the map, and a description of each soil map unit.



MAP LEGEND

Area of Interest (AOI)

Area of Interest (AOI)

Soils

Soil Map Unit Polygons

Soil Map Unit Lines



Soil Map Unit Points

Special Point Features

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Blowout

Borrow Pit

Clay Spot

Closed Depression

Gravel Pit

Gravelly Spot

Landfill

Lava Flow Marsh or swamp

Mine or Quarry

Miscellaneous Water Perennial Water

Rock Outcrop

Saline Spot

Sandy Spot Severely Eroded Spot

Sinkhole

Slide or Slip

Sodic Spot

Spoil Area



Stony Spot

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Very Stony Spot

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Wet Spot Other

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Special Line Features

Water Features

Streams and Canals

Transportation

Rails

Interstate Highways

US Routes

Major Roads

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Local Roads

Background

Aerial Photography

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24.000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service Web Soil Survey URL:

Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: El Paso County Area, Colorado Survey Area Data: Version 15, Oct 10, 2017

Soil map units are labeled (as space allows) for map scales 1:50.000 or larger.

Date(s) aerial images were photographed: Jun 3, 2014—Jun 17, 2014

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
8	Blakeland loamy sand, 1 to 9 percent slopes	9.0	82.9%
10	Blendon sandy loam, 0 to 3 percent slopes	1.9	17.1%
Totals for Area of Interest		10.8	100.0%

Map Unit Descriptions

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however,

onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An association is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

El Paso County Area, Colorado

8—Blakeland loamy sand, 1 to 9 percent slopes

Map Unit Setting

National map unit symbol: 369v Elevation: 4,600 to 5,800 feet

Mean annual precipitation: 14 to 16 inches Mean annual air temperature: 46 to 48 degrees F

Frost-free period: 125 to 145 days

Farmland classification: Not prime farmland

Map Unit Composition

Blakeland and similar soils: 85 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Blakeland

Setting

Landform: Flats, hills

Landform position (three-dimensional): Side slope, talf

Down-slope shape: Linear Across-slope shape: Linear

Parent material: Alluvium derived from sedimentary rock and/or eolian deposits

derived from sedimentary rock

Typical profile

A - 0 to 11 inches: loamy sand AC - 11 to 27 inches: loamy sand

C - 27 to 60 inches: sand

Properties and qualities

Slope: 1 to 9 percent

Depth to restrictive feature: More than 80 inches Natural drainage class: Somewhat excessively drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): High to very high (5.95

to 19.98 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Calcium carbonate, maximum in profile: 5 percent Available water storage in profile: Low (about 4.5 inches)

Interpretive groups

Land capability classification (irrigated): 3e Land capability classification (nonirrigated): 6e

Hydrologic Soil Group: A

Ecological site: Sandy Foothill (R049BY210CO)

Hydric soil rating: No

Minor Components

Other soils

Percent of map unit: Hydric soil rating: No

Pleasant

Percent of map unit: Landform: Depressions Hydric soil rating: Yes

10—Blendon sandy loam, 0 to 3 percent slopes

Map Unit Setting

National map unit symbol: 3671 Elevation: 6,000 to 6,800 feet

Mean annual precipitation: 14 to 16 inches
Mean annual air temperature: 46 to 48 degrees F

Frost-free period: 125 to 145 days

Farmland classification: Not prime farmland

Map Unit Composition

Blendon and similar soils: 85 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Blendon

Setting

Landform: Alluvial fans, terraces Down-slope shape: Linear Across-slope shape: Linear

Parent material: Sandy alluvium derived from arkose

Typical profile

A - 0 to 10 inches: sandy loam
Bw - 10 to 36 inches: sandy loam
C - 36 to 60 inches: gravelly sandy loam

Properties and qualities

Slope: 0 to 3 percent

Depth to restrictive feature: More than 80 inches

Natural drainage class: Well drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to

high (0.60 to 2.00 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Calcium carbonate, maximum in profile: 2 percent

Available water storage in profile: Moderate (about 6.2 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 3e

Hydrologic Soil Group: B

Ecological site: Sandy Foothill (R049BY210CO)

Hydric soil rating: No

Minor Components

Other soils

Percent of map unit: Hydric soil rating: No

Pleasant

Percent of map unit: Landform: Depressions Hydric soil rating: Yes

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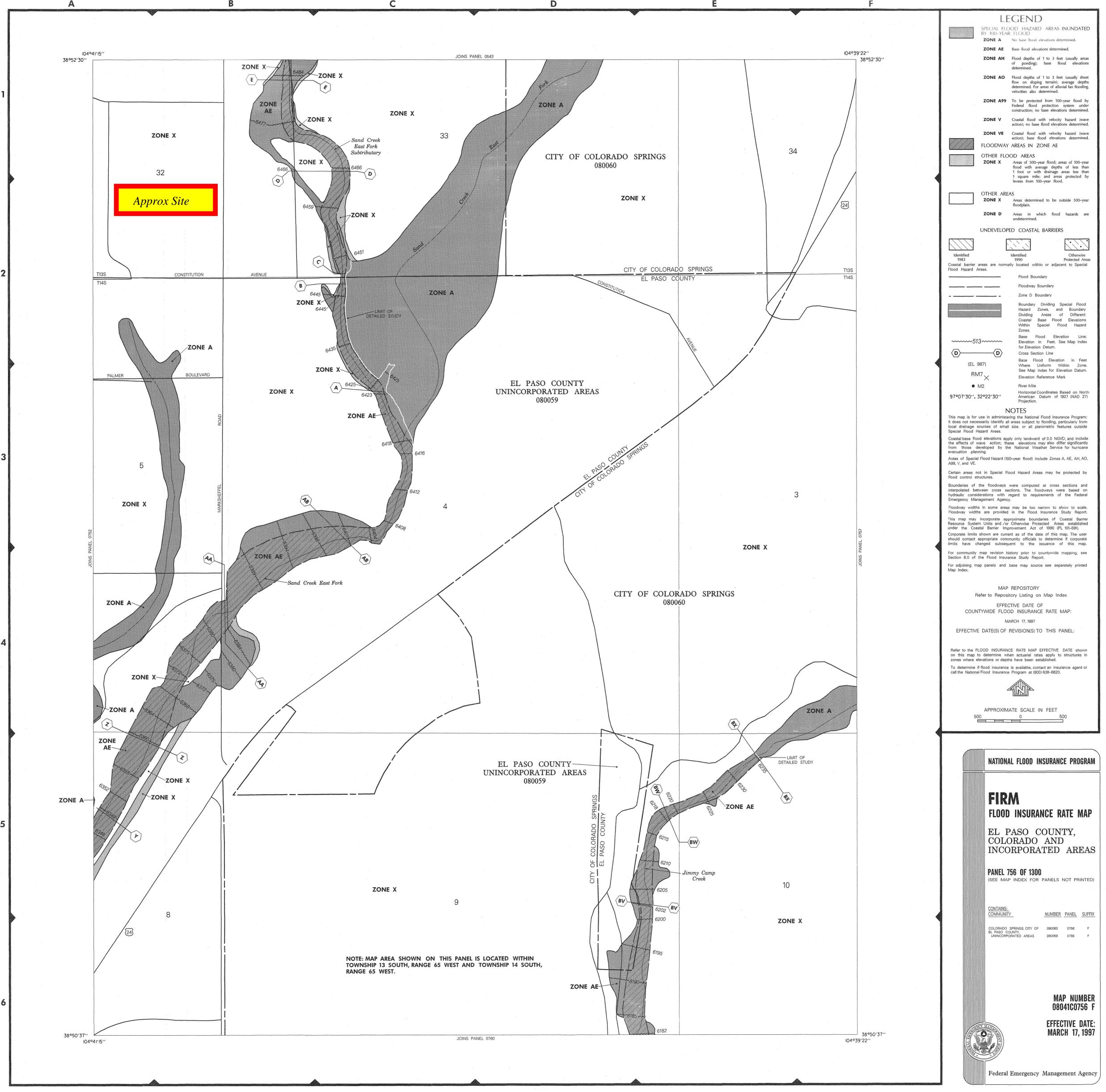
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FLOOD PLAIN MAP



DRAINAGE AND GRADING PLAN

