

FINAL DRAINAGE REPORT

FOR

MAYBERRY, COLORADO SPRINGS - FILING NO. 3

PREPARED FOR:

COLORADO SPRINGS MAYBERRY, LLC 3296 DEVINE HEIGHTS #208 COLORADO SPRINGS, CO 80922

PREPARED BY:

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> R&R JOB #MC22110 EPC PROJECT NO. SF2219

ORIGINAL SUBMITTAL: MAY 2022 2ND SUBMITTAL: SEPTEMBER 2022

ENGINEER'S STATEMENT:

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the County for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for liability caused by negligent acts, errors or omissions on my part in preparing this report.

SIGNATURE: _	
	Clif Dayton, P.E.
	Registered Professional Engineer
	State of Colorado No. 51674

DEVELOPER'S STATEMENT:

I, the developer, have read and will comply with all of the requirements specified in this drainage report and plan.

SIGNATURE:	
	John Mick
	Colorado Springs Mayberry, LLC
	3296 Devine Heights #208
	Colorado Springs, CO 80922

EL PASO COUNTY'S STATEMENT:

Filed in accordance with the requirements of the El Paso County Land Development Code, Drainage Criteria Manual, Volumes 1 and 2, and Engineering Criteria Manual as amended.

SIGNATURE:		
	Joshua Palmer, P.E.	
	County Engineer/ECM	Administrator

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I. GENERAL LOCATION AND DESCRIPTION

A. Background

Mayberry, Colorado Springs (formerly known as "Ellicott Town Center") is a proposed subdivision located west of Ellicott, Colorado in El Paso County. The development is located on the south side of State Highway 94, approximately 1-1/2 miles west of Ellicott Highway, as shown in Figure A1 (Appendix F). The approved Ellicott Town Center Sketch Plan and Overall PUD includes a total of 1,048 single-family dwelling units and 32 acres of commercial space. The Amended Mayberry, Colorado Springs Phase 1 PUD was approved by BOCC in April, 2022, which maintained the originally approved 240 Phase 1 lots, but revised various street and lot configurations based on current market conditions. Filing No. 3 comprises the easterly 142 residential lots within the Amended Phase 1 PUD.

B. Scope

This report has been prepared in support of the Final Plat application for Mayberry, Colorado Springs Filing No. 3. The report is intended to fulfill the El Paso County requirements for a Final Drainage Report (FDR).

The report will provide a summary of site drainage issues impacting the proposed development, including analysis of impacts from upstream drainage patterns, site-specific developed drainage patterns, and impacts on downstream facilities. This drainage report was prepared based on the guidelines and criteria presented in the El Paso County Drainage Criteria Manual, providing preliminary design of required drainage facilities for this phase of the project.

C. Site Location and Description

The Mayberry, Colorado Springs (Ellicott Town Center) parcel comprises the west half of Section 14 along with the contiguous east quarter of Section 15, as well the west half of the northeast quarter of Section 14, Township 14 South, Range 63 West of the 6th Principal Meridian. The site is located at an elevation of approximately 6,060 feet above mean sea level. Filing No. 3 comprises 105.8-acres in the northeast area of the Mayberry development.

State Highway 94 borders Filing 3 to the north along with Filing 2, and unplatted agricultural properties (zoned A35) border Filing 3 on the east and south sides. Unplatted property zoned PUD and Filing 1 border Filing 3 to the west.

The primary access to Filing 3 will be provided by construction of Springs Road, which will run through the site from north to south as a minor collector roadway (65' right-

of-way). Additionally, Filing 3 will be accessed by New Log Road via Village Main Street (60' right-of-way). Both roads intersect SH94 to the north.

The intermittent streams throughout this area drain into the Black Squirrel Creek Basin which ultimately outfalls into the Arkansas River. Filing 3 is located within the Ellicott Consolidated Drainage Basin (CHBS1200). This basin conveys surface drainage to the West Fork of Black Squirrel Creek, which is located east of this parcel between the site and Ellicott Highway.

The terrain is generally flat with gentle northwest to southeast slopes ranging from one to two percent. Historic drainage patterns from the site are conveyed overland to the south and east boundaries of the site. The entire site is covered with native grasses.

D. General Soil Conditions

According to the Soil Survey of El Paso County prepared by the Soil Conservation Service, on-site soils are comprised primarily of "Blakeland series (type 8)" soils (see Figure A2). The Blakeland soils are characterized as well-drained loamy sand with rapid permeability, slow surface runoff rates, and moderate hazard of erosion. These soils are classified as hydrologic soils group "A" for drainage analysis purposes.

E. References

City of Colorado Springs & El Paso County "Drainage Criteria Manual," revised October 12, 1994.

City of Colorado Springs "Drainage Criteria Manual, Volumes 1 and 2," revised May, 2014.

CDOT, "CDOT Drainage Design Manual," 2004.

David R. Sellon & Associates Inc., "Antelope Park Ranchettes Interior Drainage Plan," March, 1972.

El Paso County Planning Department, "Ellicott Valley Comprehensive Plan," March, 1989.

El Paso County "Engineering Criteria Manual," January 9, 2006.

El Paso County Resolution No. 15-042 (El Paso County adoption of "Chapter 6: Hydrology" and "Chapter 13, Section 3.2.1: Full Spectrum Detention" of the City of Colorado Springs Drainage Criteria Manual dated May 2014).

JPS Engineering, "Master Development Drainage Plan for Ellicott Town Center," November 22, 2005 (approved by El Paso County 12/02/05).

JPS Engineering, "Master Development Drainage Plan and Preliminary Drainage Report for Springs East Village," March 21, 2002 (approved by El Paso County 10/23/02).

JPS Engineering, "Master Development Drainage Plan and Preliminary Drainage Report for Viewpoint Village," January 28, 2002 (approved by El Paso County 9/11/02).

JPS Engineering, "Preliminary Drainage Report for Ellicott Town Center - Phase 1," January 15, 2007.

JPS Engineering, "Preliminary & Final Drainage Report for Mayberry, Colorado Springs - Filing No. 1," revised October 27, 2020 (approved by El Paso County November 5, 2020).

JPS Engineering, "Preliminary Drainage Report Amendment for Mayberry, Colorado Springs – Phase 1 PUD," revised February 2022

Leigh Whitehead & Associates, Inc., "Master Development Drainage Plan for Sunset Village," May, 2000 (approved by El Paso County 8/31/00).

Pacific Summits Engineering, "Final Drainage Report for Viewpoint Estates," January 6, 1998 (approved by El Paso County 10/6/99).

United Planning and Engineering, "Preliminary Drainage Plan & Report for Springs East," November 19, 1999.

United Planning and Engineering, "Drainage Plan & Report for Viewpoint Subdivision," May, 2000.

USDA/NRCS, "Soil Survey of El Paso County Area, Colorado," June, 1981.

II. DRAINAGE BASINS AND SUB-BASINS

A. Major Drainage Basins

The proposed development lies primarily within the Ellicott Consolidated Drainage Basin (CHBS1200) as classified by El Paso County. This basin is comprised of the area tributary to the West Fork of Black Squirrel Creek, with the majority of the basin bounded by SH94 to the north and Ellicott Highway to the east. No drainage planning study has been completed for the Ellicott Consolidated Drainage Basin or any adjacent drainage basins.

The major drainage basins lying in and around the proposed development are depicted in Figure EX1 and is sourced from the Phase 1 PUD Amended Drainage Report. Mayberry, Colorado Springs is located primarily within the Ellicott Consolidated Drainage Basin, which comprises a tributary area of about 13 square miles, or 8,320 acres. The proposed subdivision represents a total of 551 acres of development, or 7 percent of the total basin area. An "on-site" drainage planning approach has been proposed based on the relatively small developed area in comparison to the remaining undeveloped basin area, which is primarily agricultural land.

The existing site topography has one off-site drainage basin (EC-10) that enters the northeast corner of Filing 3. Triple 30-inch CMP culverts cross SH94 at this location combines with on-site flows, following existing grass-lined swales southeasterly through the site. Filing 3 historically consists of one major basin conveying flows towards the south and eastern boundaries of the site, as shown in Figure EX2. Flows from Filing 3 combine with the tributary areas from Filing 1 and surrounding offsite areas downstream of the site, flowing southeasterly to an existing natural channel towards Black Squirrel Creek.

B. Floodplain Impacts

Mayberry – Filing 3, Colorado Springs is located approximately one mile southwest of the 100-year floodplain limits for the West Fork of Black Squirrel Creek, as delineated by the Federal Emergency Management Agency (FEMA). The floodplain limits in the vicinity of the site are shown in Flood Insurance Rate Map (FIRM) Number 08041C0810G, dated December 7, 2018 (see Figure A3).

C. Sub-Basin Description

The developed drainage basins lying within Filing 3 are depicted in Figure D1. The interior site layout has been delineated into several drainage basins (C-E) based on the proposed interior road layout and grading scheme. The natural drainage patterns will be impacted through development by site grading and concentration of runoff in subdivision street gutters, storm drains, and channels. Most sub-basins drain to the southeast, collecting in the interior roads and drainage channels. On-site flows will be diverted to a proposed extended detention basin (EDB) located at the southeast boundary of the site, and detained runoff flows will discharge to the east, following historic drainage paths.

III. DRAINAGE DESIGN CRITERIA

A. Development Criteria Reference

The Ellicott Consolidated Drainage Basin has not had a Drainage Basin Planning Study performed for the basin. Most areas within the basin are comprised of agricultural lands and rural residential uses.

A "Master Development Drainage Plan (MDDP) for Ellicott Town Center" was approved concurrent with the original Overall PUD, and a Preliminary Drainage Report for Ellicott Town Center Phase One was approved with the original Phase One PUD and Preliminary Plan.

JPS Engineering prepared the "Preliminary & Final Drainage Report for Mayberry, Colorado Springs - Filing No. 1," revised October 27, 2020 (approved by El Paso County November 5, 2020) in support of the final approval and recording of Filing No. 1.

This "Final Drainage Report for Mayberry, Colorado Springs – Filing No. 3" fully conforms to the previously approved MDDP and Preliminary/Final Drainage Reports, along with the "Preliminary Drainage Report Amendment for Mayberry, Colorado Springs Phase 1 PUD" dated February, 2022 prepared in support of the Phase 1 PUD Amendment.

B. Hydrologic Criteria

SCS procedures were utilized for analysis of major basin flows impacting the site. In accordance with El Paso County drainage criteria, SCS hydrologic calculations were based on the following assumptions:

Design storm (minor)
 Design storm (major)
 Storm distribution
 100-year
 SCS Type IIA (eastern Colorado)
 100-year, 24-hour rainfall
 5-year, 24-hour rainfall
 Hydrologic soil type
 5-year
 5-year
 Hydrologic soil type

• SCS curve number - undeveloped conditions

61 (pasture / range)

- SCS curve number developed conditions 80 (1/8-1/4 acre lots)
- SCS curve number developed conditions 92 (commercial areas)

Hydraflow Hydrographs was utilized for the modeling of these storms.

Rational method procedures were utilized for calculation of peak flows within the on-site drainage basins. Rational method hydrologic calculations were based on the following assumptions:

Shouldn't this be A as

indicated in page 2 and the sheet below? Please revise as necessary

•	Design storm (minor)	5-year	
•	Design storm (major)	100-year	
•	Rainfall Intensities	El Paso Coun	ty I-D-F Curve
•	Hydrologic soil type	Α	
		C5	C100
•	Runoff Coefficients - undeveloped:		
	Existing pasture/range areas	0.25	0.35
•	Runoff Coefficients - developed:		
	Proposed Residential (1/8-1/4 acre lots)	0.375	0.545
	Proposed Neighborhood Commercial	0.49	0.62

Composite runoff coefficients for the developed residential areas have been calculated based on average lot sizes between 1/8-acre and 1/4-acre. A rational method spreadsheet was utilized for modeling these flows.

C. Hydraulic Criteria

Street and inlet capacities were calculated using the UD_Inlet utilizing the street geometries at each inlet. The criteria used for street and inlet capacities was that for the 5 year storm, flow depths would not exceed 6 inches or overtop the street crown while for the 100 year storm, the depth of water at the flow line would not exceed 12 inches.

Three pipe systems are proposed as part of the Filing 3 development. Pipes are sized so that the 100 year HGLs are a minimum of 1 foot below finished grades. HGLs are derived using Bentley StormCAD software. Velocities in pipes do not exceed 18 fps as stated in the EPC DCM. All peak flows for pipes were derived via the Rational Method.

Four grass lined channels are proposed as part of the Filing 3 development: C2, D, E, and F. Channels are sized so that there is a minimum of 1 foot of freeboard between the 100 year water surface elevation and the top of channels. Channel linings are chosen based on the calculated velocities/slopes and conform to Table 10-4 of the EPC DCM. Channel E utilized the SCS method to determine the peak flow from the upstream offsite basin. Peak flows for Channels C2 and D were derived via the Rational Method while peak flows for Channel F were obtained from the release rates from upstream extended detention basin D combined with offsite flows routed by Channel E.

Rip-Rap was sized for the 100 year storm per UDFCD Section 3.2.1. Rip-rap is placed where all pipes discharge into channels across the site.

Two temporary culverts are proposed beneath temporary cul-de-sacs east of the proposed development. The culverts are designed so that during the 100 year storm event, water levels do not exceed 12 inches above finished grade when overtopping the roadway above.

D. Detention and Water Quality Criteria

Detention volumes and required release rates will be calculated using the UD_Detention Spreadsheet from UDFCD. An extended detention basin will be utilized to provide water quality and detention for Filing 3. The facility is designed to pass and release the water quality captured volume (WQCV), excess urban runoff volume (EURV), and 100 year storm to meet all local and state regulations by means of a multi-stage outlet structure.

The WQCV will be routed through an orifice plate installed within the outlet structure and sized to have a 40 hour draw down time. The orifice plate will also drain 97% the EURV within 72 hours. Finally, a restrictor plate and weir combination will pass the 100 year flow at 90% of the pre-developed rate.

Per El Paso County Engineering Criteria Manual Section 1.7.1.C.1, up to one acre of development may be exempt from stormwater treatment. Due to the requirement that temporary cul-de-sacs be provided for fire department access to Union Pacific and El Reno Way, these developed areas are unable to drain to the proposed detention pond. These areas will drain to Channel E and flow offsite undetained. These cul-de-sac areas total to 0.3 acres, so well below the 1 acre requirement.

IV. DRAINAGE PLANNING FOUR STEP PROCESS

El Paso County Drainage Criteria require drainage planning to include a Four Step Process for receiving water protection that focuses on reducing runoff volumes, treating the water quality capture volume (WQCV), stabilizing drainageways, and implementing long-term source controls.

As stated in DCM Volume 2, the Four Step Process is applicable to all new and redevelopment projects with construction activities that disturb 1 acre or greater or that disturb less than 1 acre but are part of a larger common plan of development. The Four Step Process has been implemented as follows in the planning of this project:

Step 1: Employ Runoff Reduction Practices

- Minimize Impacts: The approved Planned Unit Development includes significant open space, play areas, and parks, resulting in a moderate level of impervious site development.
- Minimize Directly Connected Impervious Areas (MDCIA): The proposed development will include landscaped areas adjoining the proposed building and parking lots, providing for impervious areas to drain across pervious areas where feasible.
- Grass Swales: The proposed drainage plan incorporates grass-lined swales in

selected locations to encourage stormwater infiltration while providing positive drainage through the site.

Step 2: Stabilize Drainageways

• Proper erosion control measures will be implemented along the grass-lined drainage channels to provide stabilized drainageways within the site.

Step 3: Provide Water Quality Capture Volume (WQCV)

- EDB: The developed areas of the site will drain through proposed Full-Spectrum Extended Detention Basins (EDB) southeast of the developed areas. Site drainage will be routed through the extended detention basins, which will capture and slowly release the WQCV over an extended release period.
- Stormwater detention and WQCV for Filing as well as future Filings 2 and 4 will be provided by EDB-D.

Step 4: Consider Need for Industrial and Commercial BMPs

 No industrial or commercial land uses are proposed as part of the Filing No. 3 residential development.

V. GENERAL DRAINAGE RECOMMENDATIONS

The developed drainage plan for the site is to provide and maintain positive drainage away from structures and conform to the established drainage patterns for the overall site. Positive drainage shall be established and maintained away from all structures within the site in conformance with applicable building codes and geotechnical engineering recommendations.

Site grading and drainage improvements performed as a part of subdivision infrastructure development includes overlot grading and subdivision drainage improvements depicted on the subdivision construction drawings. Individual lot grading is the sole responsibility of the individual builders and property owners. Final grading of each home site should establish proper protective slopes and positive drainage in accordance with HUD guidelines and building codes. In general, main floor elevations for each home should be established approximately 2 feet above the top of curb of the adjoining street.

In general, we recommend a minimum of 6 inches clearance from the top of concrete foundation walls to adjacent finished site grades. Positive drainage slopes should be maintained away from all structures, with a minimum recommended slope of 5 percent for the first 10 feet away from buildings in landscaped areas, a minimum recommended slope of 2 percent for the first 10 feet away from buildings in paved areas, and a minimum slope of 1 percent for paved areas beyond buildings.

VI. DRAINAGE FACILITY DESIGN

A. General Concept

Consistent with generally accepted practices in eastern El Paso County, the general concept for management of stormwater from development of Mayberry – Filing 3 will be to construct an extended detention basin along the southeast boundary of the site to mitigate the impacts of developed runoff flows from the site.

Development of the Mayberry – Filing 3 project will require site grading and paving, resulting in additional impervious areas across the site. The general drainage pattern will consist of grading away from home sites to drainage swales and gutters along the internal roads within the subdivision, conveying runoff flows through the site. The Amended PUD includes 4-foot minimum side-lot drainage easements, and the proposed easements are adequate for the required side-lot drainage swales to accommodate proper grading of the individual home sites.

Runoff from the site will flow by street gutters to curb inlets at low points and road intersections, thence by storm drains and drainage channels to the proposed detention ponds. The storm inlets and storm sewer system within the development will be designed as the "minor" drainage system, sized for 5-year developed peak flows. The internal road system, drainage channels, and detention ponds will be designed as the "major" drainage system, sized for 100-year peak flows. Street flows within subdivision streets will be maintained below allowable levels in accordance with El Paso County drainage criteria.

Due to an offsite basin north of SH94 flowing onto the subject property, the site has been designed to convey this flow through the site via a series of temporary swales and culverts. The offsite flow will be routed around the proposed development and will combine with the pond discharge via a swale that conveys flow east of the site.

B. Specific Details

Existing Basins

Historic drainage conditions for Filing 3 are depicted in Figure EX2. The site has been divided into one major basin (EX-D). The undeveloped site currently has no drainage facilities within the area. The existing off-site drainage basins north of Filing 3 generally combine with on-site basins as shown on Figure EX2, flowing southeasterly through the site within existing grass-lined drainage swales and channels.

Off-site flows from Basin EC10 north of this property cross State Highway 94 in

? what are the other previously the report may: REPORT the Old Log Road Ditch i.e. a have discussed culverts for

Please identify in the narrative how culverts. I believe FILING 3 the flow is conveyed from DPEX5 to swale/channel at the south property another triple basin FC111 Revise rossing near the northeast corner of this street

These flows drain through an existing grass-lined swale across the east side of Basin EX-D to Design Point #EX-5, with historic peak flows of $Q_5 = 15.25$ cfs and $Q_{100} = 110.9$ cfs (SCS Method). As shown on Sheet EX2, two existing driveway culverts on the south side of SH94 convey flows from the roadside ditch on the south side of SH94 easterly to converge with the existing swale on the downstream side of the triple 30-inch CMP culverts, combining with Basin EC10.

The downstream drainage continues southeast to a more defined natural channel, forming the West Tributary to the Middle Fork of Black, Squirrel Creek. Historic drainage from Basin EX-D flows southeast to the westerly ditch along "Old" Log Road, then turns east and follows the southerly ditch of Handle Road to its confluence with the main channel of the Middle Fork of Black Squirrel Creek.

Developed Drainage Basins

The developed drainage basins and projected flows are shown in Figures D1, D1.1-D1.5. The developed Filing 3 site has been divided into three major basins (C2-E) and one major design point (DP25), as shown on the enclosed Drainage Plan. Hydrologic flow schematics and calculations are enclosed in Appendix B.

Major Basin C2 (Sub-basins C2.1-C2.4, C3.0) will be routed to the extended detention basin via Channel C2 where it will combine with major basin D (Sub-basins D1.1-D1.11, C2.0-D2.1). Channels C2 and D are also sized to convey future flows from the area south of Filing 3 which is currently undeveloped. Offsite basin EC-10 will combine with onsite major Basin E (Sub-basin E1.0) reviseddevelop at Channel E. Basin EC-10 will be routed around Filing 3 and will combine with Pond D's discharge downstream of the pond at Channel F. FYI: it is shown as E1 on the drainage map

All onsite basin peak flows were derived via the Rational Method while the offsite basin EC-10 was analyzed by the SCS Method due to the tributary area. Detailed breakdowns of each sub-basin are listed below:

Sub-basin C2.1 is a 0.77 acre onsite area that is collected by a curb inlet. This basin consists of single family lots and a portion of Solaire Loop. Runoff from this basin drains to the street curb and gutter and enters the public storm sewer system. The 5 year and 100 year developed peak flows are 1.1 and 2.7 cfs respectively

Sub-basin C2.2 is a 0.33 acre onsite area that is collected by a curb inlet. This basin consists of single family lots and a portion of Solaire Loop. Runoff from this basin drains to the street curb and gutter and enters the public storm sewer system. The 5 year and 100 year developed peak flows are 0.6 and 1.4 cfs respectively

Sub-basin C2.3 is a 11.41 acre onsite area that is collected by a curb inlet in Mayberry Drive. This basin consists of single family lots and a portions of Solaire Loop, Galveston

please make clear that the developed flows entering this basin will be conveyed to the Pond.

commercial development.

Terrace, Cattlemen Run, Achison Way, and Village Main Street. Runoff from this basin is routed via curb/gutter and crosspans, enters a Type R curb inlet, and is discharged into the piped storm sewer system. The 5 year and 100 year developed peak flows are 13.2 and 32.2 cfs respectively.

Sub-basin C2.4 is a 1.16 acre onsite area that is collected by a curb inlet on the south side of Mayberry Drive. This basin consists of south section of the Mayberry Drive ROW. Runoff from this basin is routed via curb/gutter, enters a double Type R curb inlet, and is discharged into the piped storm sewer system. The 5 year and 100 year developed peak flows are 4.1 and 7.8 cfs respectively.

Sub-basin C3.0 is a 35.40 acre basin south of the Filing 3 development. The basin was analyzed for future development and assumed to comprise both single family lots and park area. The basin will ultimately drain to Pond D via future storm sewer improvements. During the interim condition the basin will be undeveloped with part of the basin bypassing Pond D. The 5 year and 100 year developed peak flows are 22 and 72.7 cfs respectively.

Sub-basin D1.1 is a 10.45 acre basin comprising single family lots and portions of Cattlemen Run, Solaire Loop, Besseyi Way and Filing 2. The basin was analyzed for future development of Filing 2 and comprised totally of single family lots. The basin drain via curb and gutter to a Type R inlet on the north side of Besseyi Way. The 5 year and 100 year developed peak flows are 11.6 and 28.4 cfs respectively.

Sub-basin D1.2 is a 2.57 acre basin comprising single family lots and portions of Solaire Loop and Besseyi Way. Runoff from this basin is routed via curb/gutter and crosspans, enters a Type R curb inlet on the south side of Besseyi Way, and is discharged into the piped storm sewer system. The 5 year and 100 year developed peak flows are 3.4 and 8.3 cfs respectively.

Sub-basin D1.3 is a 2.02 acre basin comprising single family lots and portions of Union Pacific Way and El Reno Way. Runoff from this basin is routed via curb/gutter and crosspans, enters a Type R curb inlet on the north side of El Reno Way, and is discharged into the piped storm sewer system. The 5 year and 100 year developed peak flows are 3.1 and 7.5 cfs respectively.

Sub-basin D1.4 is a 3.55 acre basin comprising single family lots and portions of Besseyi Way, Union Pacific Way, Springs Road and El Reno Way. Runoff from this basin is routed via curb/gutter and crosspans, enters a Type R curb inlet on the south side of El Reno Way, and is discharged into the piped storm sewer system. The 5 year and 100 year developed peak flows are 4.7 and 11.5 cfs respectively.

Sub-basin D1.5 is a 9.37 acre basin comprising the future Filing 4 area and is assumed to be Commercial/Industrial in nature. Runoff from this basin will be routed via

Please identify that your are discussing a future condition and that this inlet would not be installed at this stage (or will it?).

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curb/gutter and crosspans and enter inlets within the future development. The inlets will be piped to the east to the proposed piping that will convey Basin EC-10's offsite flow through the development. The 5 year and \100 year developed peak flows are 19.8 and 39.4 cfs respectively.

The offsite flow from EC-10 will

appears to state that it will be

combined with EC-10 flow that will

developed. Is the flow conveyed to

as stub as being capped. please

Sub-basin D1.6 is a 1.94 acre basin comprising single family not be treated but the future Pacific Way. Runoff from this basin is routed via cultb/gutter developed flow from basin D1.5 Type R curb inlet on the north side of Union Pacific Way, and must be treated. Please clarify piped storm sewer system to the east. The 5 year and 100 yexput intent for this future flow as it are 2.6 and 6.3 cfs respectively.

not be treated. Please also **Sub-basin D1.7** is a 1.56 acre basin comprising single family discuss this flow in terms of the Pacific Way. Runoff from this basin is routed via curb/gutter filing 3 stage when it is not on the south side of Union Pacific Way, and is discharged in system to the east. The 5 year and 100 year developed peak Channel E at this stage or the respectively. DP12 stub? The CD's identify this

Sub-basin D1.8 is a 1.30 acre basin comprising single family letarity portions of El Reno Way. Runoff from this basin is routed via curb/gutter, enters a Type R curb inlet on the north side of El Reno Way, and is discharged into the piped storm sewer system to the east. The 5 year and 100 year developed peak flows are 1.8 and 4.4 cfs respectively.

Sub-basin D1.9 is a 0.54 acre basin comprising single family lots and portions of El Reno Way. Runoff from this basin is routed via curb/gutter, enters a Type R curb inlet on the south side of El Reno Way, and is discharged into the piped storm sewer system to the east. The 5 year and 100 year developed peak flows are 0.9 and 2.1 cfs respectively.

Sub-basin D1.10 is a 2.12 acre basin comprisiple also clarify whether the inlet at DP17 Mayberry Drive. Runoff-from this basin is routhat collects this basins flow will be installed at inlet on the north side of Mayberry Drive, anthis stage as it appears that this section of sewer system. The 5 year and 100 year deve Mayberry Drive will not be constructed. If not, then please identify how the developed flow will respectively. be conveyed to Pond D in the interim condition.

Sub-basin D1.11 is a 1.23 acre basin comprising a portion of Mayberry Drive. Runoff from this basin is routed via curb/gutter, enters a Type R curb inlet on the south side of Mayberry Drive, and is discharged into the piped storm sewer system. The 5 year and 100 year developed peak flows are 4 and 7.7 cfs respectively.

Sub-basin D2.0 is a 11.90 acre basin sputh of the Filing 3 development. The basin was analyzed for future development and assumed to comprise both single family lots and park area. The basin will ultimately drain to Pond D via future storm sewer improvements. The 5 year and 100 year developed peak flows are 10.3 and 27.7 cfs

> Similar to the comment above on basin D1.10, please also discuss how the flow will be conveyed to the south in the interim condition.

Mayberry - Filing 3

FINAL DRAINAGE REPOPTEASE label basin EC10 on the proposed conditions drainage plans.

Currently it is only shown on the historic conditions plan

respectively.

Sub-basin D2.1 is a 3.15 acre basin south of the Filing 3 development. The basin comprises the area around Detention Pond D. The basin will ultimately surface flow. The 5 year and 100 year developed peak flows are 0.9 and 6.6 cfs respectively.

Sub-basin E1.0 is a 4.63 acre basin east/northeast of the Filing 3 development. The basin comprises Channel E south of SH94 and bypasses the site to the east, ultimately discharging into Channel F to the east of Pond D. The basin also comprises the temporary cul-de-sacs required at the ends of El Reno Way and Union Pacific Drive. The 5 year and 100 year developed peak flows are 0.4 and 3.3 cfs respectively.

Sub-basin EC-10 is a 317 acre agricultural basin north of SH94 and drains into Channel E via culverts beneath SH94. The basin combines with flows generated by Basin E1.0 and bypasses the site to the east, ultimately discharging into Channel F to the east of Pond D. Due to the size of the basin, the generated peak flows were derived via the SCS Method. The 5 year and 100 year peak flows are 15.3 and 110.9 cfs respectively.

C. Emergency Conditions Analysis

In the event of clogging, the storm inlets within the Filing 3 development area will overflow to the adjoining public streets, which all generally flow southeasterly. Emergency overflows would sheet flow southeasterly along the public streets, flowing into Channels C2, D, and Detention Pond D.

Pond D also has measures in place to mitigate an emergency condition. A buried riprap emergency spillway will route emergency flows over the embankment and into a swale that will carry flows east of the site.

D. Comparison of Developed to Historic Discharges

Based on the hydrologic calculations in the Appendix, the total developed flows from the site will exceed historic flows from the parcel. Due to the increased impervious areas in the developed site, the total undetained flow from the site would be significantly higher than the historic flow. The increase in developed flows will be mitigated by an on-site

extended detention basin. <

E. Detention Design

comparing the historic flows to the developed flows after detention.

The total developed storm runoff downstream of the Filing No. 3 development along with the future developments of Filings 2, 2A, 4, and the area south of Filing 3 area will be maintained at historic levels by routing flows through the proposed Detention Pond D located at the southeast corner of the subdivision. The proposed detention facility has It appears that Pond D is designed for the total build-out

It appears that Pond D is designed for the total build-out (filings 1 -4 and basins C3.0, D2.0) and is shown to meet the required drain times. As filing 4 and basins C3.0 & D2.0 have yet to be submitted please also run a scenario with these areas as undeveloped to show that Pond D will still meet the required drain times.

Please provide the runoff values

been sized to attenuate onsite peak flows through the pond, mitigating developed drainage impacts.

The total volume requiring storage is equivalent to the 100 Year + ½ WQCV produced by the onsite developed area. The calculated volume to be stored is 8.3 ac-ft and was calculated by means of the UD_Detention spreadsheet. The detention volume will be routed through the extended detention basin by means of a modified CDOT Type C structure. The WQCV and EURV will be controlled by a multi-stage orifice plate within the Type C structure. The 100-year volume will be routed through a 36" pipe with restrictor plate within the Type C structure.

The proposed detention pond will be privately owned and maintained by the Metropolitan District, under the terms of a "Private Detention Basin Maintenance Agreement" recorded during final platting. Gravel maintenance access roads will be provided around the perimeter of the detention ponds to facilitate maintenance access.

The pond outlet structures have been designed to release historic flows southeast of the site towards the existing natural swales downstream. Based on the proposed approach of reducing developed flows to historic levels at the site boundaries, no significant downstream drainage impacts are anticipated, and no downstream drainage improvements are proposed.

F. Onsite Drainage Facility Design

Storm Sewer System Layout

Generally, streets are designed with cross slopes of 2%, pushing water from the centerlines to curb and gutter systems. The systems convey flows to low points at various points around the site where Type R curb inlets are proposed to convey street flows to an underground storm sewer system. The storm sewer system contains reinforced concrete pipes (RCP) with minimum sizes of 18 inches and minimum slopes of 0.5%.

Basins C2.1-C2.4 drains to a dedicated storm sewer system that discharged to channel C2. Basins D1.1-D1.4 and D1.10-D1.11 drain to another dedicated storm sewer system that discharges into Channel D at DP19. Basins D1.5-D1.9 drain into a third dedicated storm sewer system on the eastern edge of the Filing 3 boundary. This system also discharges into Channel D at DP19. Both channels ultimately drain to Detention Pond D.

Open Channel System Layout

Four open channels are proposed as part of this development: C2, D, E, and F. These channels will generally be designed as stable grass-lined channels with subcritical flow regimes. Drainage channels will be designed to convey 100-year flows, with trapezoidal cross-sections, side slopes of 4:1, and minimum freeboard of 1-foot.

Mayberry – Filing 3 FINAL DRAINAGE REPORT

It appears that the undeveloped flows from basin D1.5 will enter Channel E. Please be sure that Channel E accounts for these flows in this interim condition.

Channel C2 conveys flows from DP4 along with flows from future basin C3.0. The channel is trapezoidal with a bottom width of 8 feet and a depth of 3 feet. The channel will be lined with a grass-legume mixture.

Channel D conveys flows from DP19 along with flows from future basin D2.0. The channel is trapezoidal with a bottom width of 8 feet and a depth of 4 feet. The channel will be seeded with Kentucky bluegrass, tall fescue, or reed canarygrass.

Channel E conveys flows from offsite basin EC-10 along with flows from onsite basin E1.0. The channel is trapezoidal with a bottom width of 8 feet and a depth of 3 feet. The channel will be seeded with sodded grass.

Channel F conveys flows from the outfalls of Detention Pond D and combines with Channel E downstream of the pond. The channel will convey flows to the eastern ditch adjacent to Log Road. The channel is trapezoidal with a bottom width of 8 feet and a depth of 4 feet. The channel will be seeded with Kentucky bluegrass, tall fescue, or reed canarygrass.

G. Analysis of Existing and Proposed Downstream Facilities

Provide calculations where Channel F meets the existing roadside ditch. Provide existing and proposed flows and capacities for the roadside ditch.

The general concept of the proposed drainage plan is to attenuate peak flows from the for the 90 degree bend developed site by routing flows through the proposed on-site detention ponds. Combined flows from the Mayberry site flow southeasterly towards the existing Middle Fork of Black Squirrel Creek. The existing channels downstream of the site consist of broad grass-lined swales with no signs of active erosion. As previously discussed, there is an existing drainage crossing of Ellicott Highway approximately 2-1/2 miles downstream of this site where a future culvert should be installed. Recognizing that this historically deficient crossing is miles downstream of the site, no cost contribution to this off-site drainage improvement was requested during previous approval of the Ellicott Town Center MDDP, and no contribution is proposed at this time. An on-site stormwater detention pond will be provided to mitigate developed drainage impacts, so no off-site or downstream drainage improvements are proposed.

H. Anticipated Drainage Problems and Solutions

The proposed stormwater detention pond is designed to mitigate the impacts of developed drainage from this project. The overall drainage plan for the subdivision includes a system of improved public streets with curb and gutter, storm inlets, and storm sewers conveying developed flows to improved drainage channels running through the site. The primary drainage problems anticipated within this development will consist of maintenance of these storm sewer systems, culverts, drainage channels, and detention pond facilities. Care will need to be taken to implement proper erosion control measures in the proposed channels and swales, which will be designed to meet

allowable velocity criteria.

A trail system will be constructed along the major drainage channels to provide maintenance access to the drainage facilities throughout the development. Proper construction and maintenance of the proposed detention facilities will minimize downstream drainage impacts. The proposed public streets will be owned and maintained by El Paso County. The proposed detention ponds and channels running through open space tracts and storm drains through private alleys will be privately owned and maintained by the homeowners association or metropolitan district.

VII. EROSION CONTROL

The Contractor will be required to implement best management practices (BMP's) for erosion control during construction. The proposed erosion control plan is included in the Grading & Erosion Control (GEC) Plans submitted with the subdivision construction drawings. Erosion control measures will include installation of silt fence at the toe of disturbed slopes and hay bales protecting drainage ditches. Cut and fill slopes will be stabilized during excavation if necessary and vegetation will be established for stabilization of the disturbed areas. All ditches have been designed to meet El Paso County criteria for slope and velocity. Additionally, gravel vehicle tracking pads will be installed at construction access points and inlet protection will be provided to minimize conveyance of sediment into storm inlets.

VIII. COST ESTIMATE AND DRAINAGE FEES

The developer will pay all capital costs for roadway and drainage improvements. As detailed in Appendix C, the engineer's estimate for Filing 3 drainage improvements is approximately \$1,088,557.80. Filing 3 is located entirely within the Ellicott Consolidated Drainage Basin, which currently does not have a drainage or bridge fee requirement. As such, no drainage basin fees are applicable.

IX. MAINTENANCE

All proposed road and drainage construction within the Mayberry – Filing 3, Colorado Springs project will be performed to El Paso County Standards. Interior roads will be dedicated as public right-of-way. Roads and drainage facilities within the public right-of-way will be maintained by El Paso County upon final acceptance of these facilities after the warranty period. The Metropolitan District will maintain drainage channels and stormwater detention pond within the proposed open space areas.

X. SUMMARY

The Mayberry – Filing 3, Colorado Springs consists of 142 residential lots in the

northeast part of the master development, with access connections to State Highway 94 at Springs Road. The residential lots are platted within Filing 3. The development will generate an increase in developed runoff from the site, which will be mitigated through on-site stormwater detention and water quality facility.

The proposed drainage patterns will remain consistent with historic conditions, and new drainage facilities constructed to El Paso County standards will safely convey runoff to adequate outfalls. Construction of the proposed Detention Pond D southeast of the development areas will ensure that developed flows remain below historic levels. Construction and proper maintenance of the proposed drainage and erosion control facilities will ensure that this subdivision has no significant adverse drainage impacts on downstream or surrounding areas.

XI. APPENDICES

Appendix A - Hydrologic Computations

- 1. Hydrologic References
- 2. Pre Developed Flow Rates
- 3. Post Developed Flow Rates

Appendix B – Hydraulic Computations

- 1. Detention and Water Quality Facility Design
- 2. Storm Sewer Capacity
- 3. Inlet and Street Capacity
- 4. Rip Rap Calculations
- 5. Channel Design

Appendix C – Reference Information

- 1. Cost Estimate
- 2. NRCS Soils Report
- 3. FEMA Flood Insurance Maps
- 4. Drainage Maps



Land Use or	Land Use or Percent Surface Impervious		Runoff Coefficients										
Characteristics	impervious	2-year	•	5-year		10-yea	ar	25-yea	ar	50-yea	nr	100-ує	ear
		HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D
Business													
Commercial Areas	95	0.79	0.80	0.81	0.82	0.83	0.84	0.85	0.87	0.87	0.88	0.88	0.89
Neighborhood Areas	70	0.45	0.49	0.49	0.53	0.53	0.57	0.58	0.62	0.60	0.65	0.62	0.68
Residential	Lots are 1/6 acre, used	_						I I	ots are 1				
% Acre or less	<mark>65</mark>	0.41	0.45	<mark>0.4</mark> 5	0.49	0.49	0.54	0.54	0.59	0.57	0.62	<mark>0.59</mark>	0.65
(1/4 Acre)	40	0.23	0.28	0.30	0.35	0.36	0.42	0.42	0.50	0.46	0.54	0.50	0.58
⅓ Acre	30	0.18	0.22	0.25	0.30	0.32	0.38	0.39	0.47	0.43	0.52	0.47	0.57
½ Acre	25	0.15	0.20	0.22	0.28	0.30	0.36	0.37	0.46	0.41	0.51	0.46	0.56
1 Acre	20	0.12	0.17	0.20	0.26	0.27	0.34	0.35	0.44	0.40	0.50	0.44	0.55

(Industrial)													
(Light Areas)	80	0.57	0.60	0.59	0.63	0.63	0.66	0.66	0.70	0.68	0.72	0.70	0.74
Heavy Areas	90	0.71	0.73	0.73	0.75	0.75	0.77	0.78	0.80	0.80	0.82	0.81	0.83
Parks and Cemeteries	7	0.05	0.09	0.12	0.19	0.20	0.29	0.30	0.40	0.34	0.46	0.39	0.52
Playgrounds	13	0.07	0.13	0.16	0.23	0.24	0.31	0.32	0.42	0.37	0.48	0.41	0.54
Railroad Yard Areas	40	0.23	0.28	0.30	0.35	0.36	0.42	0.42	0.50	0.46	0.54	0.50	0.58
Undeveloped Areas													
Historic Flow Analysis— Greenbelts, Agriculture	2	0.03	0.05	0.09	0.16	0.17	0.26	0.26	0.38	0.31	0.45	0.36	0.51
Pasture/Meadow	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50
Forest	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50

Exposed Rock	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Offsite Flow Analysis (when landuse is undefined)	45	0.26	0.31	0.32	0.37	0.38	0.44	0.44	0.51	0.48	0.55	0.51	0.59
Streets													
(<mark>Paved</mark>)	(100)	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Gravel	80	0.57	0.60	0.59	0.63	0.63	0.66	0.66	0.70	0.68	0.72	0.70	0.74
Drive and Walks	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Roofs	90	0.71	0.73	0.73	0.75	0.75	0.77	0.78	0.80	0.80	0.82	0.81	0.83
(Lawns)	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50

I know we've talked about a possible deviation to expand the footprint of the driveway at some homes. Has this additional area been added to the percent imperviousness for the individual lots?

- 1/6 AC -USE 80

EYPAND

Fully Developed Urban	Treatment	Hydrologic	% I	Pre-D	Pre-Development CN					
Areas (vegetation established) ¹		Condition		HSG A	HSG B	HSG C	HSG D			
Open space (lawns, parks, golf courses, cemeteries, etc.):										
Poor condition (grass cover < 50%)		_	-	68	79	86	89			
Fair condition (grass cover 50% to 75%)	_	_	_	49	69	79	84			
Good condition (grass cover > 75%)	_		-	39	61	74	80			
Impervious areas:										
Paved parking lots, roofs, driveways, etc. (excluding right-of-way			_	98	98	98	98			
Streets and roads:										
Paved; curbs and storm sewers (excluding right-of-way)				98	98	98	98			
Paved; open ditches (including right-of-way)		_	-	83	89	92	93			
Gravel (including right- of-way)		_	-	76	85	89	91			
Dirt (including right-of- way)		_	-	72	82	87	89			
Western desert urban areas:										
Natural desert landscaping (pervious areas only)			_	63	77	85	88			
Artificial desert landscaping (impervious weed barrier, desert shrub with 1- to 2-inch sand or gravel mulch and basin borders)			_	96	96	96	96			
Urban districts:										

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4.0. - NRCS CURVE NUMBER LOSS AND DIMENSIONLESS UNIT HYDROGRAPH METHOD | Drainage Criteria Manual | El P...

22/22, 12:26 PM	4.0 NRCS	CURVE NU	MBER I	LOSS A	ND DIN	MENSIO	NLESS
Small grain	SR	Poor	_	65	76	84	88
		Good	-	63	75	83	87
	SR + CR	Poor	_	64	75	83	86
		Good	_	60	72	80	84
	С	Poor	_	63	74	82	85
		Good	_	61	73	81	84
	C + CR	Poor	_	62	73	81	84
	Poor	Good	_	60	72	80	83
	C&T	Poor	_	61	72	79	82
		Good	-	59	70	78	81
	C&T+ CR	Poor	-	60	71	78	81
		Good	-	58	69	77	80
Pasture, grassland, or	_	Poor	_	68	79	86	89
range—continuous forage for grazing ⁴	-	Fair	-	49	69	79	84
	-	Good	-	39	61	74	80
Meadow-continuous	_	_	-	30	58	71	78
grass, protected from grazing and generally							
mowed for hay							
Brush-brush-weed-grass mixture with brush the		Poor	-	48	67	77	83
major element 5	-	Fair	-	35	56	70	77
	-	Good	-	30	48	65	73
Woods-grass		Poor	-	57	73	82	86
combination (orchard or tree farm) ⁶	-	Fair	_	43	65	76	82
	-	Good	_	32	58	72	79
Woods 7	_	Poor	_	45	66	77	83
		Fair	_	36	60	73	79
	-	Good	_	30	55	70	77
Farmsteads-buildings, lanes, driveways, and surrounding lots				59	74	82	86
Arid and Semi-arid Rangelands ¹	Treatment	Hydrologic Condition ⁸	% I	HSG A	HSG B	HSG C	HSG D
Herbaceous-mixture of	_	Poor	_	_	80	87	93
grass, weeds, and low-							

22/22, 12:26 PM	4.0 NRCS	CURVE NUM	NREK I	LUSS A	ND DIN	IENSIO	NLESS
Commercial and business			85	89	92	94	95
Industrial			72	81	88	91	93
Residential districts by average lot size:							
% acre or less (town houses)			65	77	85	90	92
1/4 acre			38	61	75	83	87
1/4 acre			30	57	72	81	86
1/2 acre			25	54	70	80	85
1 acre			20	51	68	79	84
2 acres		-	12	46	65	77	82
Developing Urban Areas ¹	Treatment ²	Hydrologic Condition ³	% I	HSG A	HSG B	HSG C	HSG D
Newly graded areas (pervious areas only, no vegetation)	_		_	77	86	91	94
Cultivated Agricultural Lands ¹	Treatment	Hydrologic Condition	% I	HSG A	HSG B	HSG C	HSG D
Fallow	Bare soil		_	77	86	91	94
	Crop	Poor	-	76	85	90	93
	residue cover (CR)	Good	_	74	83	88	90
Row crops	Straight	Poor	_	72	81	88	91
	row (SR)	Good	_	67	78	85	89
	SR + CR	Poor	_	71	80	87	90
	SR + CR	Poor	_	71	80 75	87	90
	Contoured		_ _ _				-
		Good	 	64	75	82	85
	Contoured	Good	- - - -	64	75	82	85
	Contoured (C)	Good Poor Good		64 70 65	75 79 75	82 84 82	85 88 86
	Contoured (C) C+CR Contoured	Good Poor Good Poor		64 70 65 69	75 79 75 78	82 84 82 83	85 88 86 87
	Contoured (C)	Good Poor Good Poor Good	 	64 70 65 69	75 79 75 78 74	82 84 82 83 81	85 88 86 87 85
	Contoured (C) C + CR Contoured & terraced	Good Poor Good Poor Good Poor	 	64 70 65 69 64 66	75 79 75 78 74	82 84 82 83 81	85 88 86 87 85

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growing brush, with brush the minor element	_	Fair	_	_	71	81	89
brush the minor element	_	Good	_	_	62	74	85
Oak-aspen-mountain		Poor	_	_	66	74	79
brush mixture of oak brush, aspen, mountain	_	Fair	_		48	57	63
mahogany, bitter brush, maple, and other brush	_	Good	_	_	30	41	48
Pinyon-juniper-pinyon,		Poor	_	_	75	85	89
juniper, or both; grass understory	_	Fair	_	_	58	73	80
	_	Good	_	_	41	61	71
Sagebrush with grass		Poor	-	_	67	80	85
understory	_	Fair	_	_	51	63	70
	_	Good	-		35	47	55
Desert shrub—major plants include saltbush,		Poor	_	63	77	85	88
greasewood, creosotebush, blackbrush, bursage,	_	Fair	-	55	72	81	86
palo verde, mesquite, and cactus	-	Good	_	49	68	79	84
¹ Ia = 0.1 S							
Crop residue cover applie year.	es only if resid	ue is on at lea	st 5% of	the surf	ace thro	ughout th	ne
3 Hydraulic condition is bar (a) density and canopy of v grass or close-seeded legu and (e) degree of surface i runoff. Good: Factors enco decrease runoff.	regetative area umes, (d) perce oughness. Po	as, (b) amount ent of residue or: Factors imp	of year- cover or pair infilt	round or the lan ration ar	over, (c) d surface nd tend to	amount of good a concrease	of : 20%), se
4 Poor: <50%) ground cow not heavily grazed. Good:					-	ound co	ver and
5 Poor: <50% ground cove	r. Fair: 50 to 7	5% ground cov	ver. God	d: >75%	ground	cover.	
6. CN's shown were computed combinations of conditions				-	s (pastur	e) cover	. Other
7- Poor: Forest litter, small t							
Fair: Woods are grazed bu protected from grazing, an					e soil. G	ood: Wo	ods are

Table 6-9. NRCS Curve Numbers for Pre-Development Thunderstorms Conditions (ARC I)

Fully Developed Urban	Treatment	Hydrologic	% I	Pre-De	evelopm	ent CN	
Areas (vegetation established) ¹		Condition		HSG A	HSG B	HSG C	HSG D
Open space (lawns, parks, golf courses,							
cemeteries, etc.):							
Poor condition (grass cover < 50%)	-	-	-	47	61	72	77
Fair condition (grass cover 50% to 75%)	-	-	-	29	48	61	69
Good condition (grass cover > 75%)	-	-	-	21	40	54	63
Impervious areas:							
Paved parking lots, roofs, driveways, etc. (excluding right-of-way)	_	-	_	95	95	95	95
Streets and roads:							
Paved; curbs and storm sewers (excluding right-of-way)	_	-	_	95	95	95	95
Paved; open ditches (including right-of-way)	-	_	_	67	77	83	85
Gravel (including right- of-way)	-	_	_	57	70	77	81
Dirt (including right-of- way)	_	-	_	52	66	74	77
Western desert urban areas:							
Natural desert landscaping (pervious areas only)	_	-	_	42	58	70	75
Artificial desert landscaping (impervious weed barrier, desert shrub with 1- to 2-inch sand or gravel mulch and basin borders)	-	-	-	91	91	91	91
Developing Urban Areas ¹	Treatment ²	Hydrologic Condition ³	% I	HSG A	HSG B	HSG C	HSG D

 $https://library.municode.com/co/el_paso_county/codes/drainage_criteria_manual?nodeld=VO1UP_CH6HY_4.0NRCUNULODIUNHYME$

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Close-seeded or	SR	Poor	_	45	58	70	77
broadcast legumes or rotation meadow		Good	-	37	52	64	70
	С	Poor	_	43	56	67	70
		Good	_	34	48	60	67
	C&T	Poor	_	42	53	63	67
		Good	_	30	46	57	63
Pasture, grassland, or	_	Poor	_	47	61	72	77
range-continuous forage for grazing ⁴	_	Fair	_	29	48	61	69
ior grazing ·		Good	_	21	40	54	63
							-
Meadow-continuous grass, protected from grazing and generally mowed for hay	_	_	_	15	37	51	60
Brush-brush-weed-grass	_	Poor	_	28	46	58	67
mixture with brush the major element ⁵	_	Fair	_	18	35	49	58
	_	Good	_	15	28	44	53
Woods-grass	_	Poor	_	36	53	66	72
combination (orchard or tree farm) ⁶	_	Fair	_	24	44	57	66
	_	Good	_	17	37	52	61
Woods 7	_	Poor	-	26	45	58	67
	_	Fair	_	19	39	53	61
	_	Good	_	15	34	49	58
Farmsteads-buildings, lanes, driveways, and surrounding lots	_	_	_	38	54	66	72
Arid and Semi-arid Rangelands ¹	Treatment	Hydrologic Condition ⁸	% I	HSG A	HSG B	HSG C	HSG D
Herbaceous-mixture of		Poor	_	_	63	74	85
grass, weeds, and low- growing brush, with brush	_	Poor	_	_	63 51	74 64	85 77
grass, weeds, and low-	_ 		_ _ _	- -			
grass, weeds, and low- growing brush, with brush the minor element Oak-aspen-mountain	_ _ _	Fair	- - - -		51	64	77
grass, weeds, and low- growing brush, with brush the minor element Oak-aspen-mountain brush mixture of oak brush, aspen, mountain		Fair Good	- - -	_ _ _ _	51	64	77
grass, weeds, and low- growing brush, with brush the minor element Oak-aspen-mountain brush mixture of oak		Fair Good Poor	_ _ _ _ _		51 41 45	64 54 54	77 70 61

Newly graded areas (pervious areas only, no vegetation)	-	-	-	58	72	81	87
Cultivated Agricultural Lands ¹	Treatment	Hydrologic Condition	% I	HSG A	HSG B	HSG C	HSG D
Fallow	Bare soil	-	-	58	72	81	87
	Crop residue	Poor	-	57	70	79	85
	cover (CR)	Good	-	54	67	75	79
Row crops	Straight row (SR)	Poor	-	52	64	75	81
	TOW (SR)	Good	-	46	60	70	77
	SR + CR	Poor	-	51	63	74	79
		Good	-	43	56	66	70
	Contoured (C)	Poor	-	49	61	69	75
		Good	-	44	56	66	72
	C + CR	Poor	-	48	60	67	74
		Good	-	43	54	64	70
	Contoured & terraced	Poor	-	45	54	63	66
	(C&T)	Good	_	41	51	60	64
	C&T+ CR	Poor	-	44	53	61	64
		Good	-	40	49	58	63
Small grain	SR	Poor	-	44	57	69	75
		Good	-	42	56	67	74
	SR + CR	Poor	_	43	56	67	72
		Good	-	39	52	63	69
	С	Poor	_	42	54	66	70
		Good	_	40	53	64	69
	C + CR Poor	Poor	_	41	53	64	69
		Good	_	39	52	63	67
	C&T	Poor	-	40	52	61	66
		Good	-	38	49	60	64
	C&T+ CR	Poor	_	39	51	60	64
		Good	_	37	48	58	63

 $https://library.municode.com/co/el_paso_county/codes/drainage_criteria_manual?nodeld=VO1UP_CH6HY_4.0NRCUNULODIUNHYME$

7/22/22, 12:26 PM 4.0. - NRCS CURVE NUMBER LOSS AND DIMENSIONLESS UNIT HYDROGRAPH METHOD | Drainage Criteria Manual | El P...

juniper, or both; grass understory	-	Fair	-	-	37	53	63
	-	Good	_	-	23	40	51
Sagebrush with grass	-	Poor	-	-	46	63	70
understory	-	Fair	-	-	30	42	49
	-	Good	_	-	18	27	34
Desert shrub—major plants include saltbush,	_	Poor	-	42	58	70	75
greasewood, creosotebush, blackbrush, bursage,	_	Fair	-	34	52	64	72
palo verde, mesquite, and cactus	_	Good	-	29	47	61	69

2. Crop residue cover applies only if residue is on at least 5% of the surface throughout the year.

3. Hydraulic condition is based on combination factors that affect infiltration and runoff, including (a) density and canopy of vegetative areas, (b) amount of year-round cover, (c) amount of grass or close-seeded legumes, (d) percent of residue cover on the land surface (good ≥ 20%), and (e) degree of surface roughness. Poor: Factors impair infiltration and tend to increase runoff. Good: Factors encourage average and better than average infiltration and tend to decrease runoff.

⁴ Poor: <50%) ground cover or heavily grazed with no mulch. Fair: 50 to 75% ground cover and not heavily grazed. Good: > 75% ground cover and lightly or only occasionally grazed.

⁵ Poor: <50% ground cover. Fair: 50 to 75% ground cover. Good: >75% ground cover.

6. CN's shown were computed for areas with 50% woods and 50% grass (pasture) cover. Other combinations of conditions may be computed from the CN's for woods and pasture.

⁷ Poor: Forest litter, small trees, and brush are destroyed by heavy grazing or regular burning. Fair: Woods are grazed but not burned, and some forest litter covers the soil. Good: Woods are protected from grazing, and litter and brush adequately cover the soil.

8. Poor: <30% ground cover (litter, grass, and brush overstory). Fair: 30 to 70% ground cover.</p> Good: > 70% ground cover

Chapter 6 Hydrology

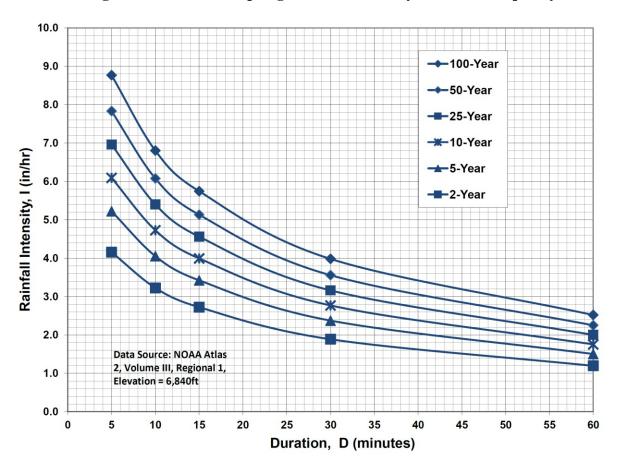


Figure 6-5. Colorado Springs Rainfall Intensity Duration Frequency

IDF Equations

 $I_{100} = -2.52 \ln(D) + 12.735$

 $I_{50} = -2.25 \ln(D) + 11.375$

 $I_{25} = -2.00 \ln(D) + 10.111$

 $I_{10} = -1.75 \ln(D) + 8.847$

 $I_5 = -1.50 \ln(D) + 7.583$

 $I_2 = -1.19 \ln(D) + 6.035$

Note: Values calculated by equations may not precisely duplicate values read from figure.

EXISTING C VALUES

Designer: ESJ

Company: R&R Engineers-Surveyors

Date: 8/5/2022

Project: Mayberry Filing 3

Location: El Paso County



Globa	al Parameters ¹		
Land Use	% Imp.	C ₅	C ₁₀₀
Agriculture	2	0.09	0.36
Hardscape	100	0.9	0.96
Commercial/Industrial	80	0.59	0.7
Landscape/Park	2	0.08	0.35

Summ	nary
Total Area (ac)	102.00
Composite Impervious	2.0%
Cells of this color are fo	r required user-input
Cells of this color are fo	r optional user-input

¹ From Table 6-6 in El Paso County DCM

² From Table 6-6 in El Paso County DCM

Basin Name	Area	NRCS Hydrologic Soil Group	Agric	culture	н	ardscape	Commercial/	Industrial	Landsca	pe/Park	% Check	% Check Percent Imperviousness		Runoff Coefficient, C ²			t, C²	
	(ac)	, , ,	Area (ac)	%	Area (ac)	%	Area (ac)	%	Area (ac)	%		•	2-yr	5-yr	10-yr	25-yr	100-yr	
EX-D1	90.50	А	90.50	100.0%	0.00	0.0%	0.00	0.0%	0.00	0.0%	100.00%	2.0%		0.09			0.36	
EX-D2	11.50	А	11.50	100.0%	0.00	0.0%	0.00	0.0%	0.00	0.0%	100.00%	2.0%		0.09			0.36	

a single basin is shown on the drainage plan. Please revise so that they are consistent with each other.

EX DEVELOPMENT CN VALUES

Designer: ESJ

Company: R&R Engineers-Surveyors

Date: 8/5/2022

Project: Mayberry Filing 3

Location: El Paso County



Global Parameters ¹	
Land Use	CN
PASTURE - GOOD	61

Basin Name	Area	NRCS Hydrologic Soil Group	PASTUI	RE - GOOD	% Check	SCS CN
	(ac)		Area (ac)	%		CN
EC10	317.30	А	317.30	100.0%		61.00
EX-D1	93.50	А	93.50	100.0%		61.00
EX-D2	11.50	А	11.50	100.0%		61.00

TIME OF CONCENTRATION

Designer: ESJ

Company: R&R Engineers-Surveyors

Date: 8/5/2022

Project: Aspen Distillers

Location: El Paso County

 $t_i = \frac{0.395(1.1 - C_5)\sqrt{L_i}}{S_i^{0.33}}$

 $Computed \, t_c = t_i + t_t$

t_{minimum}= 5 (urban) t_{minimum}= 10 (non-urban) Non Urban Li max = 300' Urban Li Max = 100'



 $=\frac{L_t}{60V}$

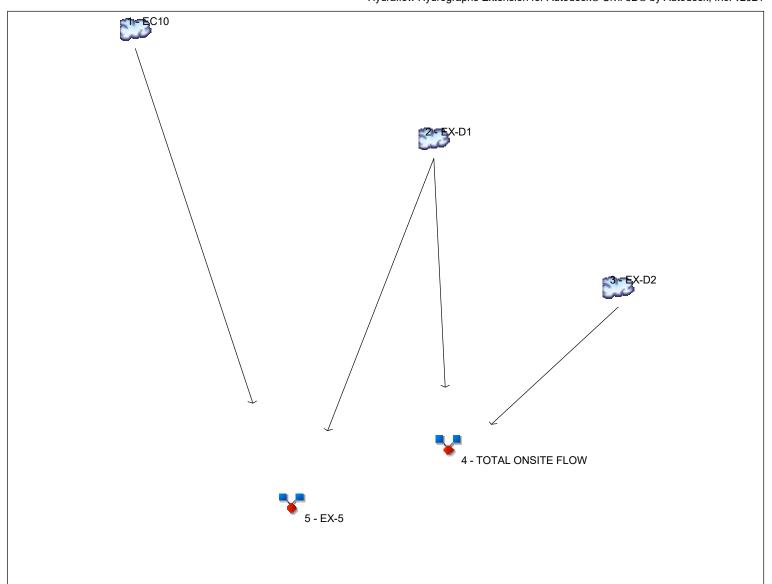
 $Selected \ t_c = max\{t_{minimum} \ \text{, } min(Computed \ t_c \ \text{, } Regional \ t_c)\}$

Regional $t_c = (26 - 17i) + \frac{L_t}{60(14i + 9)\sqrt{S_t}}$

Cells of this color are for required user-input

	Subbasin Data O						w Time	Channelized (Travel) Flow Time					Time of Concentration			
Bas	sin	Area	% Impervious	C 5	Overland Flow Length L _i (ft)	Overland Flow Slope S _i (ft/ft)	Overland Flow Time t _i (min)		Channelized Flow Slope S _t (ft/ft)	NRCS Conveyance Factor K	Channelized Flow Velocity V _t (ft/sec)	Channelized Flow Time t _t (min)	Computed t _c (min)	Regional t _c (min)	Selected t _c (min)	Remarks
EX-	-D1	90.50	2.0%	0.09	300.00	0.020	25.13	2845.00	0.020	10	1.41	33.53	58.66	61.79	58.66	
EX-	-D2	11.50	2.0%	0.09	300.00	0.020	25.13	1395.00	0.020	10	1.41	16.44	41.57	43.38	41.57	

Watershed Model Schematic



Legend

<u>Hyd.</u>	<u>Origin</u>	<u>Description</u>
1	SCS Runoff	EC10
2	SCS Runoff	EX-D1
3	SCS Runoff	EX-D2
4	Combine	TOTAL ONSITE FLOW
5	Combine	EX-5

Project: SCS ROUTING - EX.gpw

Friday, 08 / 5 / 2022

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Friday, 08 / 5 / 2022

Watershed Model Schematic	1
Hydrograph Return Period Recap	2
5 - Year Summary Report	3
Hydrograph Reports	4
Hydrograph No. 1, SCS Runoff, EC10	
Hydrograph No. 2, SCS Runoff, EX-D1	
Hydrograph No. 3, SCS Runoff, EX-D2	6
Hydrograph No. 4, Combine, TOTAL ONSITE FLOW	7
Hydrograph No. 5, Combine, EX-5	8
100 - Year	
Summary Report	9
Hydrograph Reports	
Hydrograph No. 1, SCS Runoff, EC10	10
Hydrograph No. 2, SCS Runoff, EX-D1	11
Hydrograph No. 3, SCS Runoff, EX-D2	
Hydrograph No. 4, Combine, TOTAL ONSITE FLOW	
Hydrograph No. 5, Combine, EX-5	14
IDF Report	15

Hydrograph Return Period Recap

Hyd. Hydrograph No. type (origin)	Inflow				Peak Out	tflow (cfs)				Hydrograph	
		hyd(s)	1-yr	2-yr	3-yr	5-yr	10-yr	25-yr	50-yr	100-yr	Description
1	SCS Runoff					15.25				110.89	EC10
2	SCS Runoff					5.630				44.96	EX-D1
3	SCS Runoff					0.834				7.112	EX-D2
4	Combine	2, 3				6.383				51.31	TOTAL ONSITE FLOW
5	Combine	1, 2,				20.08				149.38	EX-5

Proj. file: SCS ROUTING - EX.gpw

Friday, 08 / 5 / 2022

Hydrograph Report

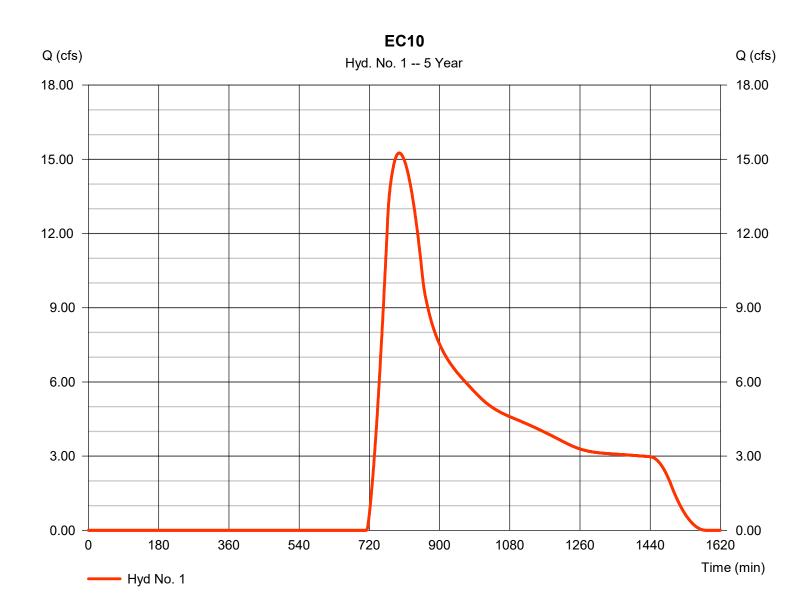
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Friday, 08 / 5 / 2022

Hyd. No. 1

EC₁₀

= 15.25 cfsHydrograph type = SCS Runoff Peak discharge Storm frequency = 5 yrsTime to peak = 797 min Time interval = 1 min Hyd. volume = 262,872 cuft Drainage area Curve number = 320.000 ac = 61 = 0 ftBasin Slope = 0.0 %Hydraulic length Tc method Time of conc. (Tc) = 90.00 min = User Total precip. = 2.60 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



Hydrograph Report

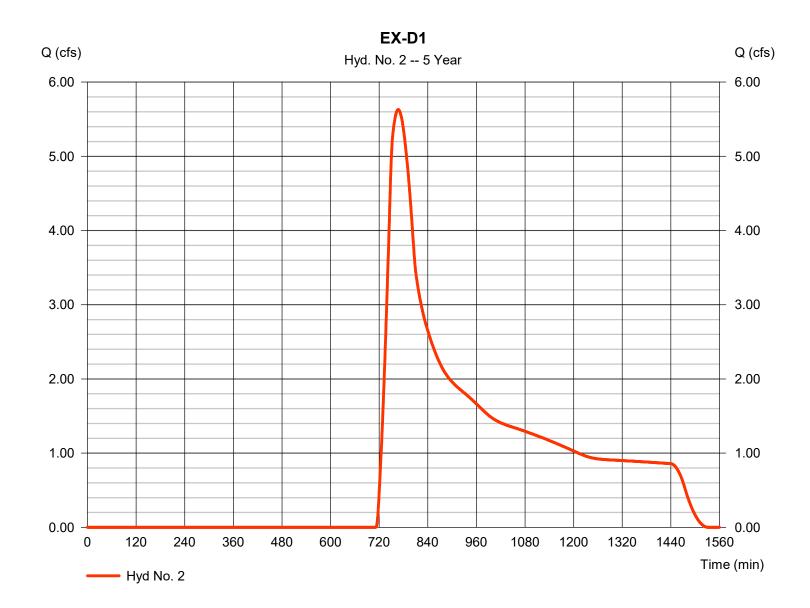
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Friday, 08 / 5 / 2022

Hyd. No. 2

EX-D1

Hydrograph type = SCS Runoff Peak discharge = 5.630 cfsStorm frequency = 5 yrsTime to peak = 767 min Time interval = 1 min Hyd. volume = 76,534 cuft Drainage area Curve number = 93.500 ac= 61 = 0 ftBasin Slope = 0.0 %Hydraulic length Tc method Time of conc. (Tc) = 58.00 min = User Total precip. = 2.60 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



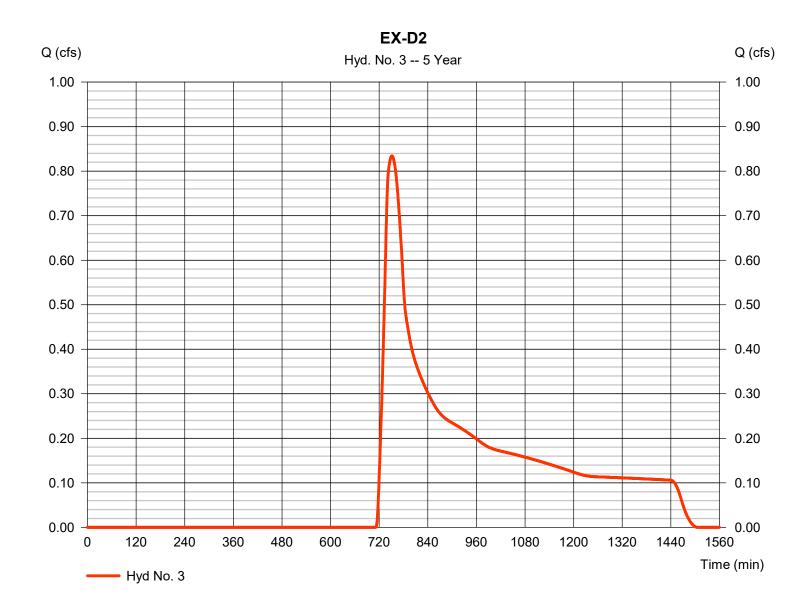
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Friday, 08 / 5 / 2022

Hyd. No. 3

EX-D2

Hydrograph type = SCS Runoff Peak discharge = 0.834 cfsStorm frequency = 5 yrsTime to peak = 751 min Time interval = 1 min Hyd. volume = 9.494 cuft Drainage area = 11.500 ac Curve number = 61 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc) = 41.00 min = User Total precip. = 2.60 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



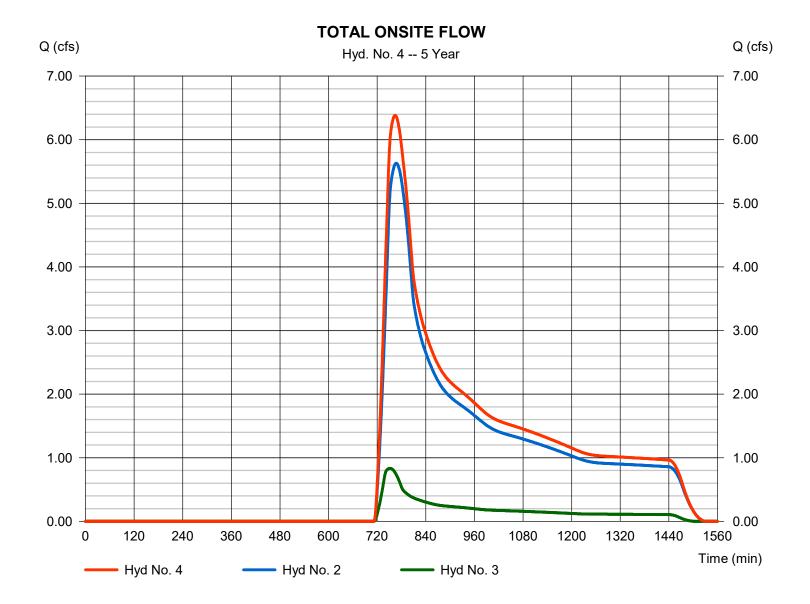
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Friday, 08 / 5 / 2022

Hyd. No. 4

TOTAL ONSITE FLOW

Hydrograph type = Combine Peak discharge = 6.383 cfsStorm frequency Time to peak = 5 yrs= 764 min Time interval = 1 min Hyd. volume = 86,028 cuft Inflow hyds. = 2, 3 Contrib. drain. area = 105.000 ac



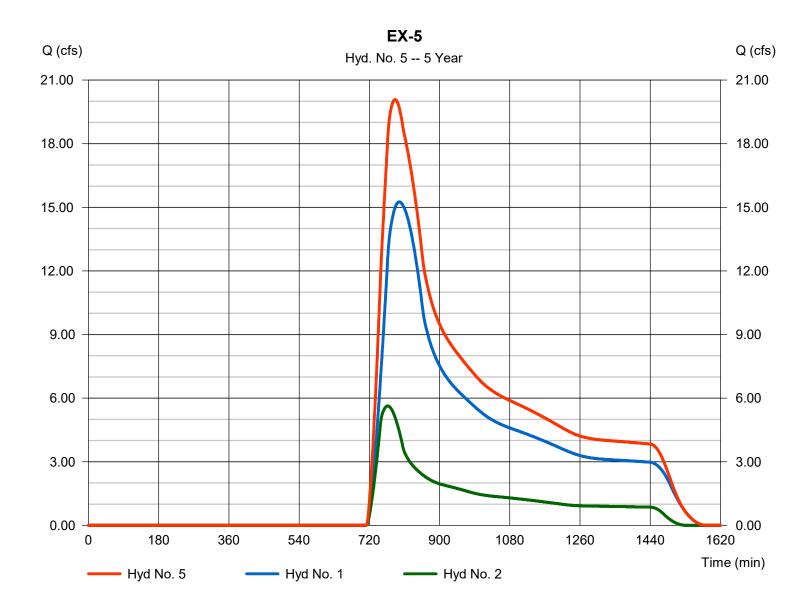
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Friday, 08 / 5 / 2022

Hyd. No. 5

EX-5

Hydrograph type = Combine Peak discharge = 20.08 cfsStorm frequency Time to peak = 5 yrs= 786 min Time interval = 1 min Hyd. volume = 339,405 cuft Inflow hyds. = 1, 2 Contrib. drain. area = 413.500 ac



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

= 24 hrs

Friday, 08 / 5 / 2022

= 484

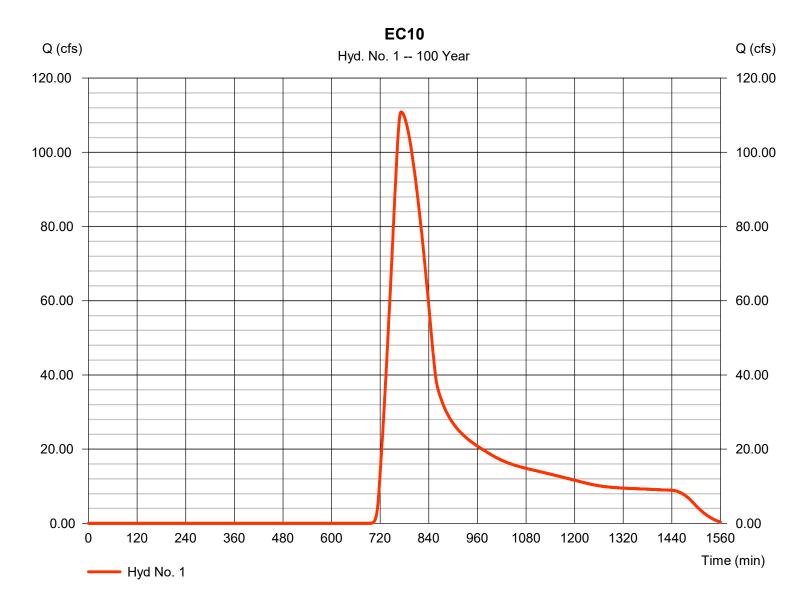
Hyd. No. 1

Storm duration

EC₁₀

Hydrograph type = SCS Runoff Peak discharge = 110.89 cfsStorm frequency = 100 yrsTime to peak = 772 min Time interval = 1 min Hyd. volume = 1,189,408 cuft Drainage area Curve number = 320.000 ac= 61 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 90.00 min = User Total precip. = 4.40 inDistribution = Type II

Shape factor



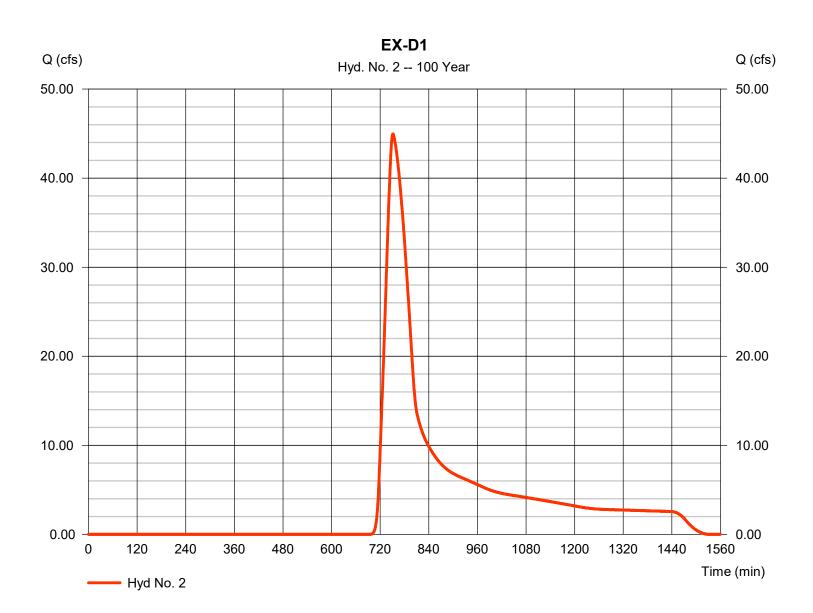
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

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Hyd. No. 2

EX-D1

Hydrograph type = SCS Runoff Peak discharge = 44.96 cfsStorm frequency = 100 yrsTime to peak = 752 min Time interval = 1 min Hyd. volume = 346,289 cuft Drainage area Curve number = 93.500 ac= 61 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 58.00 min = User Total precip. = 4.40 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



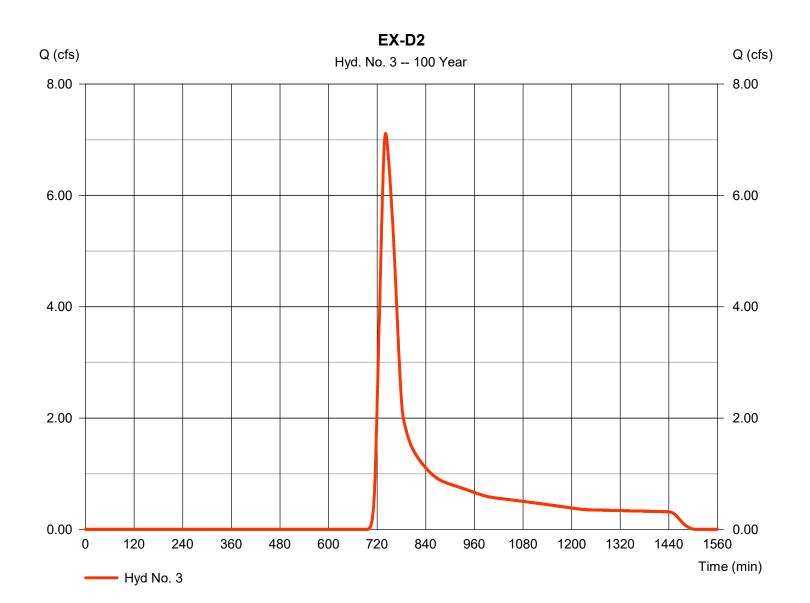
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Friday, 08 / 5 / 2022

Hyd. No. 3

EX-D2

= 7.112 cfsHydrograph type = SCS Runoff Peak discharge Storm frequency = 100 yrsTime to peak = 741 min Time interval = 1 min Hyd. volume = 42,958 cuft Drainage area = 11.500 ac Curve number = 61 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 41.00 min = User Total precip. = 4.40 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



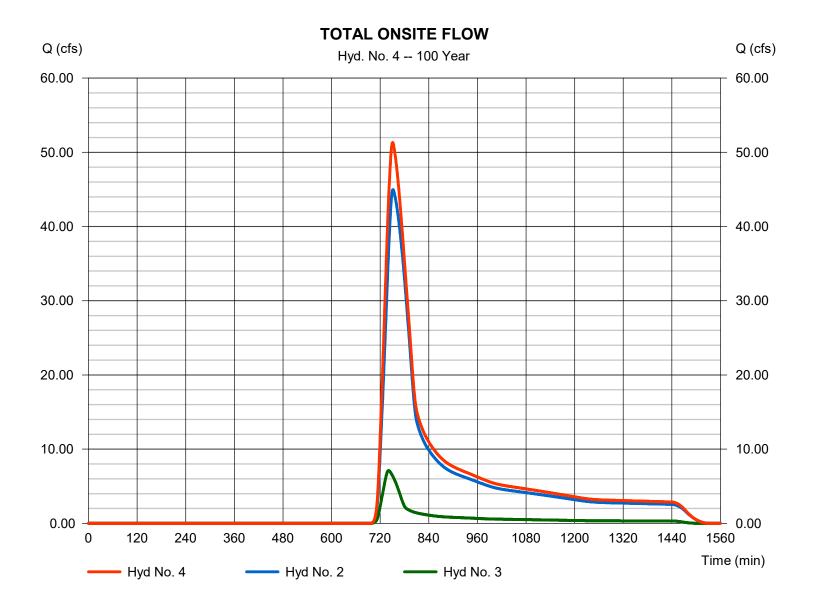
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Friday, 08 / 5 / 2022

Hyd. No. 4

TOTAL ONSITE FLOW

Hydrograph type = Combine Peak discharge = 51.31 cfsStorm frequency Time to peak = 100 yrs= 751 min Time interval = 1 min Hyd. volume = 389,247 cuft Inflow hyds. = 2, 3 Contrib. drain. area = 105.000 ac

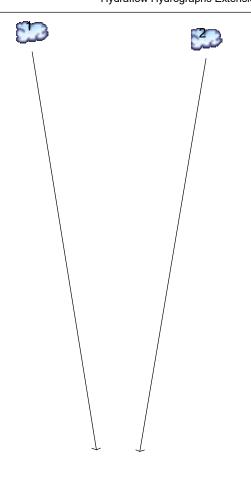


Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Friday, 08 / 26 / 2022

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Hydrograph No. 3, Combine, DP24	6
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Hydrograph No. 1, SCS Runoff, EC10 - PRESENT	. 8
Hydrograph No. 2, SCS Runoff, E1	. 9
Hydrograph No. 3, Combine, DP24	10

Watershed Model Schematic





Legend

 Hyd.
 Origin
 Description

 1
 SCS Runoff
 EC10 - PRESENT

 2
 SCS Runoff
 E1

2 SCS Runoff E1 3 Combine DP24

Project: SCS ROUTING.gpw

Friday, 08 / 26 / 2022

Hydrograph Return Period Recap

lyd.	Hydrograph	Inflow				Peak Ou	tflow (cfs)			Hydrograph
lo.	type (origin)	hyd(s)	1-yr	2-yr	3-yr	5-yr	10-yr	25-yr	50-yr	100-yr	Description
1	SCS Runoff					15.25				110.89	EC10 - PRESENT
2	SCS Runoff					0.369				3.248	E1
3	Combine	1, 2				15.41				111.80	DP24

Proj. file: SCS ROUTING.gpw

Friday, 08 / 26 / 2022

Hydrograph Summary Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	15.25	1	797	262,872				EC10 - PRESENT
2	SCS Runoff	0.369	1	745	3,803				E1
						1, 2			

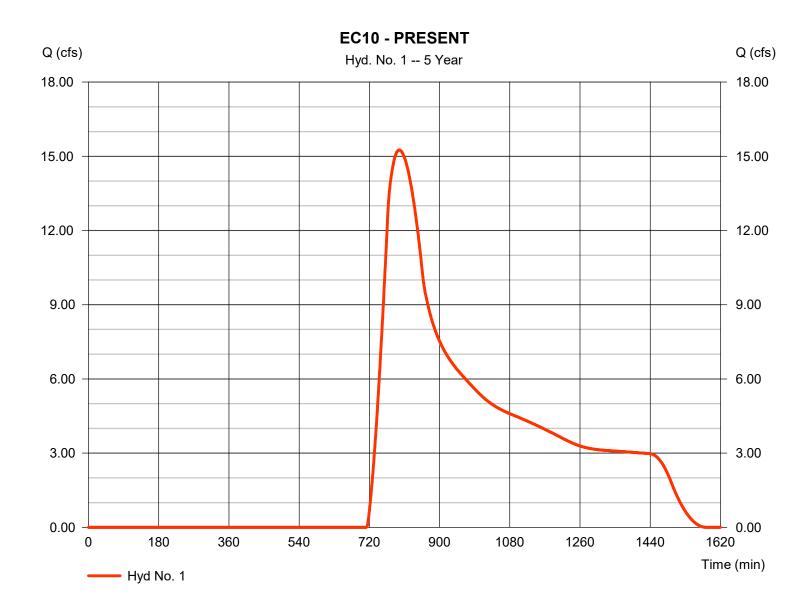
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Friday, 08 / 26 / 2022

Hyd. No. 1

EC10 - PRESENT

= 15.25 cfsHydrograph type = SCS Runoff Peak discharge Storm frequency = 5 yrsTime to peak = 797 min Time interval = 1 min Hyd. volume = 262,872 cuft Drainage area Curve number = 320.000 ac = 61 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc) = 90.00 min = User Total precip. = 2.60 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



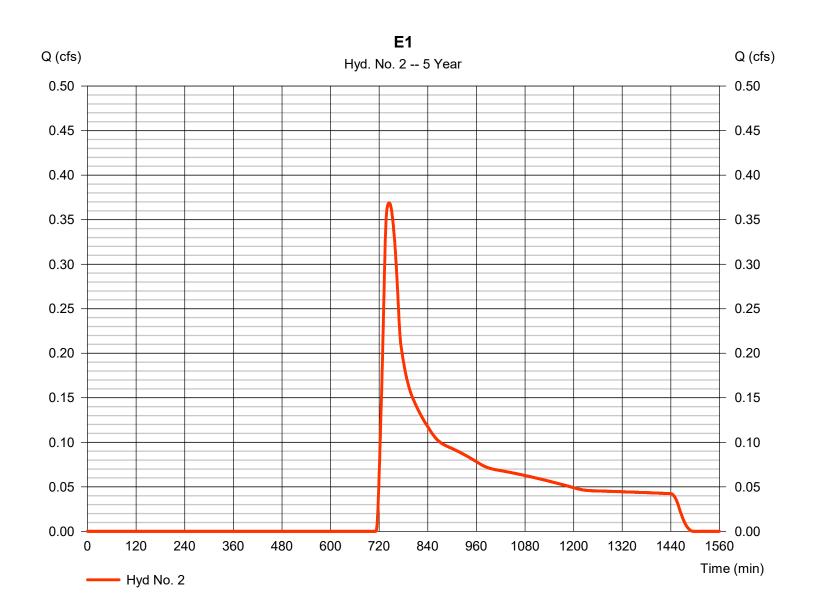
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Friday, 08 / 26 / 2022

Hyd. No. 2

E1

Hydrograph type = SCS Runoff Peak discharge = 0.369 cfsStorm frequency = 5 yrsTime to peak = 745 min Time interval = 1 min Hyd. volume = 3,803 cuftDrainage area = 4.630 acCurve number = 61 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc) = 34.00 min = User Total precip. = 2.60 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



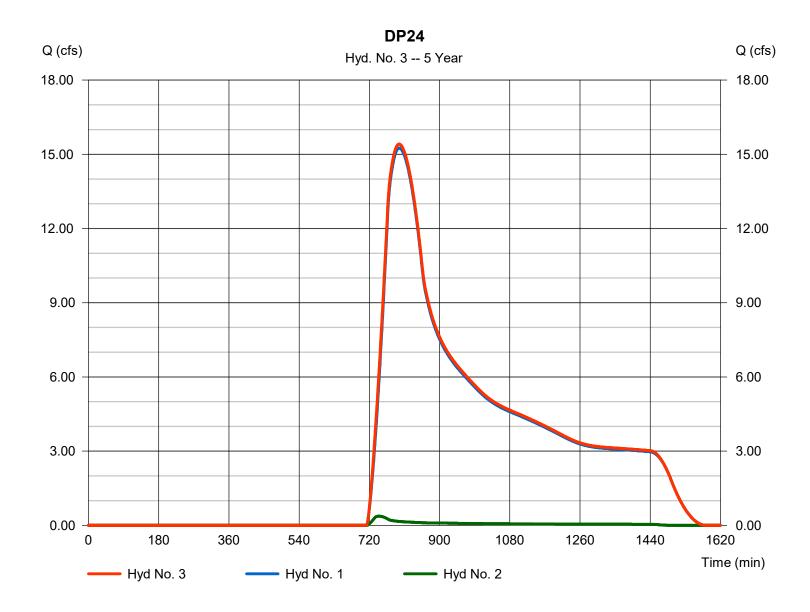
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Friday, 08 / 26 / 2022

Hyd. No. 3

DP24

Hydrograph type = Combine Peak discharge = 15.41 cfsStorm frequency Time to peak = 5 yrs= 796 min Time interval = 1 min Hyd. volume = 266,675 cuft Inflow hyds. = 1, 2 Contrib. drain. area = 324.630 ac



Hydrograph Summary Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	110.89	1	772	1,189,408				EC10 - PRESENT
2	SCS Runoff	3.248	1	736	17,209				E1
3	Combine	111.80	1	772	1,206,616	1, 2			DP24
sc	S ROUTING.	gpw			Return P	eriod: 100	Year	Friday, 08 /	26 / 2022

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

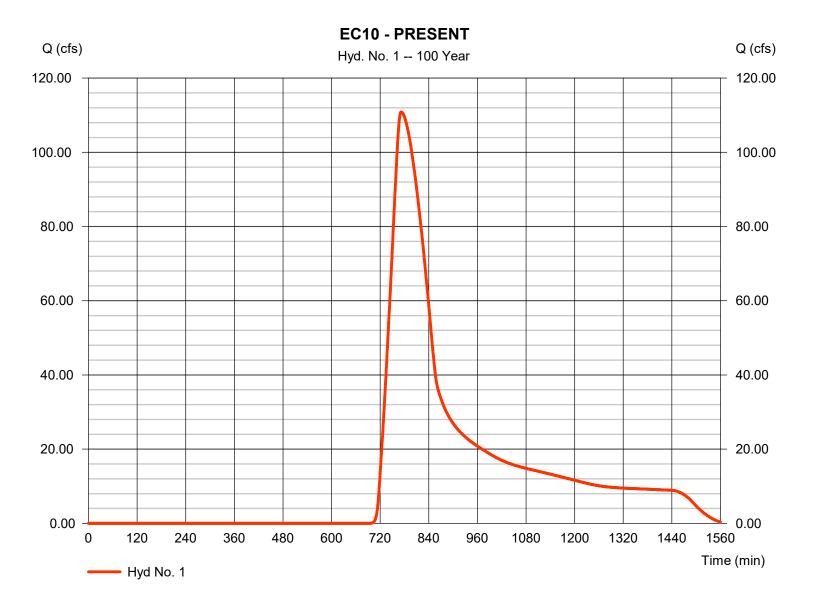
Friday, 08 / 26 / 2022

Hyd. No. 1

EC10 - PRESENT

Hydrograph type = SCS Runoff Peak discharge = 110.89 cfsStorm frequency = 100 yrsTime to peak = 772 min Time interval = 1 min Hyd. volume = 1,189,408 cuft Drainage area Curve number = 320.000 ac= 61 Basin Slope = 0.0 %Hydraulic length = 0 ft

Tc method = User Time of conc. (Tc) = 90.00 min
Total precip. = 4.40 in Distribution = Type II
Storm duration = 24 hrs Shape factor = 484



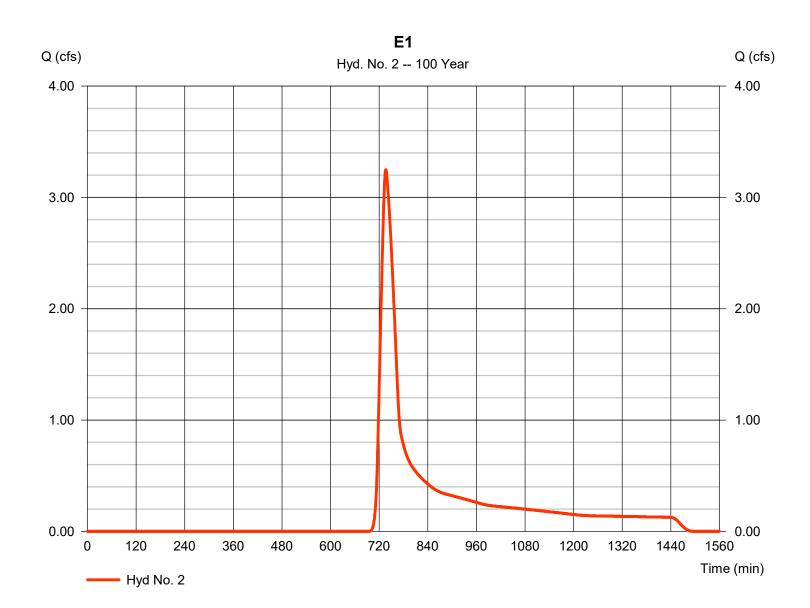
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Friday, 08 / 26 / 2022

Hyd. No. 2

E1

Hydrograph type = SCS Runoff Peak discharge = 3.248 cfsStorm frequency = 100 yrsTime to peak = 736 min Time interval = 1 min Hyd. volume = 17,209 cuft Drainage area = 4.630 acCurve number = 61 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 34.00 min = User Total precip. = 4.40 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

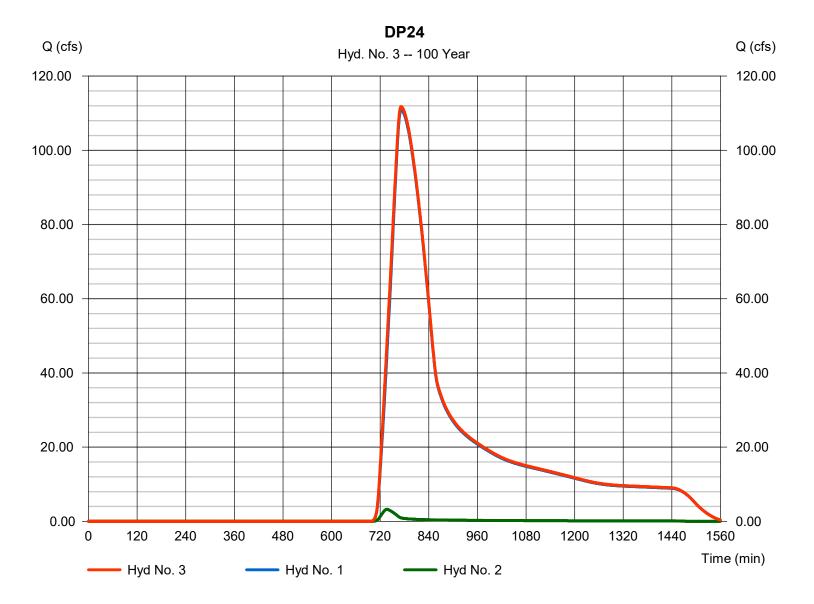
Friday, 08 / 26 / 2022

Hyd. No. 3

DP24

Hydrograph type = Combine Peak discharge = 111.80 cfs
Storm frequency = 100 yrs Time to peak = 772 min

Time interval = 1 min Hyd. volume = 1,206,616 cuft Contrib. drain. area = 324.630 ac



POST-DEVELOPMENT C VALUES

Designer: ESJ

Company: R&R Engineers-Surveyors

Date: 8/29/2022

Project: Mayberry Filing 3

Location: El Paso County



Glob	al Parameters ¹		
Land Use	% Imp.	C ₅	C ₁₀₀
SF LOTS (1/6 AC)	47.5	0.375	0.545
Hardscape	100	0.9	0.96
Commercial/Industrial	80	0.59	0.7
Landscape/Park	2	0.08	0.35

Sumn	nary									
Total Area (ac)	198.39									
Composite Impervious	41.5%									
Cells of this color are for required user-input										
Cells of this color are for optional user-input										

¹ From Table 6-6 in El Paso County DCM

² From Table 6-6 in El Paso County DCM

Basin Name	Area	NRCS Hydrologic Soil Group	SF LOT	S (1/6 AC)	н	ardscape	Commercial,	/Industrial	Landsca	pe/Park	% Check	Percent Imperviousness		Runo	off Coefficien	t, C²	
	(ac)	,	Area (ac)	%	Area (ac)	%	Area (ac)	%	Area (ac)	%	,		2-yr	5-yr	10-yr	25-yr	100-yr
C2.1	0.77	А	0.77	100.0%	0.00	0.0%	0.00	0.0%	0.00	0.0%	100.00%	47.5%		0.38			0.55
C2.2	0.33	А	0.33	100.0%	0.00	0.0%	0.00	0.0%	0.00	0.0%	100.00%	47.5%		0.38			0.55
C2.3	11.41	Α	11.41	100.0%	0.00	0.0%	0.00	0.0%	0.00	0.0%	100.00%	47.5%		0.38			0.55
C2.4	1.16	А	0.00	0.0%	0.93	80.0%	0.00	0.0%	0.23	20.0%	100.00%	80.4%		0.74			0.84
C3.0	35.40	А	17.70	50.0%	0.00	0.0%	0.00	0.0%	17.70	50.0%	100.00%	24.8%		0.23			0.45
D1.1	10.45	А	10.45	100.0%	0.00	0.0%	0.00	0.0%	0.00	0.0%	100.00%	47.5%		0.38			0.55
D1.2	2.57	А	2.57	100.0%	0.00	0.0%	0.00	0.0%	0.00	0.0%	100.00%	47.5%		0.38			0.55
D1.3	2.02	А	2.02	100,0%	0.00	0.0%	0.00	0.0%	0.00	0.0%	100.00%	47.5%		0.38			0.55
D1.4	3.55	А	3.55	100.0%	0.00	0.0%	0.00	0.0%	0.00	0.0%	100.00%	47.5%		0.38			0.55
D1.5	9.37	Α	0.00	0.0%	0.00	0.0%	9.37	100.0%	0.00	0.0%	100.00%	80.0%		0.59			0.70
D1.6	1.94	Α	1.94	100.0%	0.00	0.0%	0.00	0.0%	0.00	0.0%	100.00%	47.5%		0.38			0.55
D1.7	1.56	A	1.56	100.0%	0.00	0.0%	0.00	0.0%	0.00	0.0%	100.00%	4 7.5%		0.38			0.55
D1.8	1.30	A	1.30	100.0%	0.00	0.0%	0.00	0.0%	0.00	0.0%	100.00%	47.5%		0.38			0.55
D1.9	0.54	A	0.54	100.0%	0.00	0.0%	0.00	0.0%	0.00	0.0%	100.00%	47.5%		0.38			0.55
D1.10	2.12	A	2.12	100.0%	0.00	0.0%	0.00	0.0%	0.00	0.0%	100.00%	47.5%		0.38			0.55
D1.11	1.23	A	0.00	0.0%	0.98	80.0%	0.00	0.0%	0.25	20.0%	100.00%	80.4%		0.74			0.84
D2.0	11.90	A	9.50	79.8%	0.00	0.0%	0.00	0.0%	2.40	20.2%	100.00%	38.3%		0.32			0.51
E1	4.63	A	0.00	0.0%	0.00	0.0%	0.00	0.0%	4.63	100.0%	100.00%	2.0%		0.08			0.35
D2.1	3.15	А	0.00	0.0%	0.00	0.0%	0.00	0.0%	3.15	100.0%	100.00%	2.0%		0.08			0.35

Basin D1.1 does not account for the commercial development of filing 2. Please revise accordingly.

80% impervious appears low for a property zoned commercial. This basin encompasses Future filing 4 which is zoned CS (commercial service). A 90-95% impervious value is more in line with the current zoning of the property and would allow more flexibility when developing this filing. Please update.

POST-DEVELOPMENT CN VALUES

Designer: ESJ

Company: R&R Engineers-Surveyors

Date: 8/29/2022

Project: Mayberry Filing 3

Location: El Paso County



Global Parameters ¹	
Land Use	CN
SF LOTS (1/6 AC)	80
PASTURE - GOOD	61
COMMERCIAL	92
OPEN SPACE - GOOD	61
PAVED STREETS	98

Basin Name	Area	NRCS Hydrologic Soil Group	SF LOT	S (1/6 AC)	PASTU	JRE - GOOD	СОММЕ	RCIAL	OPEN SPA	CE - GOOD	PAVED S	STREETS	% Check	SCS CN
	(ac)		Area (ac)	%	Area (ac)	%	Area (ac)	%	Area (ac)	%	Area (ac)	%		CN
E1	4.63	А	0.00	0.0%	0.00	0.0%	0.00	0.0%	4.63	100.0%	0.00	0.0%	100.00%	61.00
EC10	317.30		0.00		317.30		0.00		0.00		0.00			61.00

TIME OF CONCENTRATION

Designer: ESJ

Company: R&R Engineers-Surveyors

Date: 8/29/2022

Project: Aspen Distillers

Location: El Paso County

 $t_i = \frac{0.395(1.1 - C_5)\sqrt{L_i}}{S_i^{0.33}}$

 $Computed \, t_c = t_i + t_t$

t_{minimum}= 5 (urban) t_{minimum}= 10 (non-urban) Non Urban Li max = 300' Urban Li Max = 100'

 $Selected \ t_c = \max\{t_{minimum} \text{ , } min(Computed \ t_c \text{ , } Regional \ t_c)\}$

Regional $t_c = (26 - 17i) + \frac{L_t}{60(14i + 9)\sqrt{S_t}}$

Cells of this color are for required user-input



								»/γ»t							
	Subbasir	n Data		Overlan	nd (Initial) Flo	w Time		Channe	lized (Travel) F	low Time			Time of C	Concentration	
Basin	Area	% Impervious	C 5	Overland Flow Length L _i (ft)	Overland Flow Slope S _i (ft/ft)		Channelized Flow Length L _t (ft)	Channelized Flow Slope S _t (ft/ft)	NRCS Conveyance Factor K	Channelized Flow Velocity V _t (ft/sec)	Channelized Flow Time t_t (min)	Computed t _c (min)	Regional t _c (min)	Selected t _c (min)	Remarks
C2.1	0.77	47.5%	0.38	100.00	0.020	10.41	242.00	0.020	20	2.83	1.43	11.84	19.75	11.84	
C2.2	0.33	47.5%	0.38	36.00	0.020	6.25	152.00	0.020	20	2.83	0.90	7.14	19.07	7.14	
C2.3	11.41	47.5%	0.38	100.00	0.020	10.41	1165.00	0.010	20	2.00	9.71	20.12	30.33	20.12	
C2.4	1.16	80.4%	0.74	12.00	0.020	1.81	534.00	0.009	20	1.90	4.69	6.50	16.96	6.50	
C3.0	35.40	24.8%	0.23	100.00	0.020	12.53	1536.00	0.010	20	2.00	12.80	25.33	42.33	25.33	
D1.1	10.45	47.5%	0.38	100.00	0.020	10.41	1356.00	0.010	20	2.00	11.30	21.71	32.37	21.71	
D1.2	2.57	47.5%	0.38	100.00	0.020	10.41	533.00	0.010	20	2.00	4.44	14.86	23.60	14.86	
D1.3	2.02	47.5%	0.38	36.00	0.020	6.25	495.00	0.010	20	2.00	4.13	10.37	23.20	10.37	
D1.4	3.55	47.5%	0.38	100.00	0.020	10.41	634.00	0.014	20	2.37	4.47	14.88	23.63	14.88	
D1.5	9.37	80.0%	0.59	100.00	0.020	7.33	856.00	0.010	20	2.00	7.13	14.46	19.46	14.46	
D1.6	1.94	47.5%	0.38	100.00	0.020	10.41	534.00	0.010	20	2.00	4.45	14.86	23.61	14.86	
D1.7	1.56	47.5%	0.38	100.00	0.020	10.41	530.00	0.010	20	2.00	4.42	14.83	23.57	14.83	
D1.8	1.30	47.5%	0.38	100.00	0.020	10.41	325.00	0.010	20	2.00	2.71	13.12	21.39	13.12	
D1.9	0.54	47.5%	0.38	36.00	0.020	6.25	389.00	0.010	20	2.00	3.24	9.49	22.07	9.49	
D1.10	2.12	47.5%	0.38	36.00	0.020	6.25	465.00	0.010	20	2.00	3.88	10.12	22.88	10.12	
D1.11	1.23	80.4%	0.74	12.00	0.020	1.81	962.00	0.017	20	2.61	6.15	7.96	18.40	7.96	
D2.0	11.90	38.3%	0.32	100.00	0.020	11.27	1750.00	0.011	20	2.10	13.90	25.17	38.84	25.17	
D2.1	3.15	2.0%	0.08	100.00	0.021	14.42						14.42		14.42	
E1	4.63	2.0%	0.08				2811.00	0.008	15	1.37	34.28		81.07	34.28	
EC10	317.30		0.08	1000.00	0.010	58.24	8100.00	0.045	20	4.24	31.82	90.06	96.71	90.06	

max 300 ft for non-urban land uses (DCMV1 CH6 section 3.2). Please revise

PROPOSED STORM DRAINAGE SYSTEM DESIGN - 5-YEAR DESIGN STORM

Designer: ESJ

Company: R&R Engineers-Surveyors

Date: 8/29/2022

Project: Mayberry Filing 3

Location: El Paso County

Cells of this color are for required user-input

Cells of this color are for optional user-input $I_5 = -1.50 \ln(D) + 7.583$



														ī		I							SURVEYORS (5
DECCIN	STREET/	B		DII	RECT RUNC	OFF	1			T	OTAL RUNG	OFF		STREET	BYPASS		PIPE	I		TRAVE	L TIME	ı	
DESGIN POINT	CONTRIBUTING BASINS	Basin Name	Area	Coeff	Тс	C*A	I	Q	Tc	Sum Area	Sum C*A	I	Q	Slope	Street Q	Design Q	Slope	PIPE	L	VEL	Tt	Q add'l	Remarks
			(ac)	С	(min)	(ac)		(cfs)	(min)	(ac)	(ac)	in/hr	cfs	%	cfs	cfs	%	SIZE	ft	ft/sec	min		
		C2.1	0.77	0.38	11.8	0.29	3.88	1.12															
1	C2.1								11.8	0.77	0.29	3.88	1.12						33	5	0.10		
		C2.2	0.33	0.38	7.1	0.12	4.63	0.57												_			
2	DP1, C2.2			0.20		4.20	2.00	42.40	11.9	1.10	0.41	3.86	1.59						450	5	1.50		
2		C2.3	11.41	0.38	20.1	4.28	3.08	13.18				2.00	44.45						10	5	0.00		
3	C2.3, DP2	62.4	1.15	0.74	6.5	0.05	4 77	4.00	20.1	12.51	4.69	3.08	14.45						64	5	0.20		
4	C2 2 DD2	C2.4	1.16	0.74	6.5	0.85	4.77	4.08	20.2	42.67		2.07	17.00						1500	5	5.30		
4	C2.3, DP3	D1 1	10.45	0.20	24.7	3.92	2.07	11.62	20.3	13.67	5.55	3.07	17.00						1590	5	5.30		
5	D1.1	D1.1	10.45	0.38	21.7	3.92	2.97	11.02	21.7	10.45	3.92	2.97	11.62						28	5	0.10		
3	D1.1	D1.2	2.57	0.38	14.9	0.96	3.54	3.41	21.7	10.45	5.92	2.97	11.02						20	3	0.10		
6	D1.2	D1.2	2.37	0.38	14.5	0.90	3.34	3.41	14.9	2.57	0.96	3.54	3.41						10	5	0.00		
0	D1.2								14.9	2.57	0.90	3.54	3.41						10		0.00		
7	DP5, DP6								21.8	13.02	4.88	2.96	14.45						512	5	1.70		
,	013,010	D1.3	2.02	0.38	10.4	0.76	4.07	3.09	21.0	13.02	4.00	2.30	14.43						312		1.70		
8	D1.3	51.5	2.02	0.50	10.1	0.70	1.07	3.03	10.4	2.02	0.76	4.07	3.09						27	5	0.10		
	220																				0.110		
9	DP7, DP8								23.51	15.04	5.64	2.85	16.06						10	5	0.00		
	,	D1.4	3.55	0.38	14.9	1.33	3.53	4.70															
10	DP9, D1.4								23.51	18.6	7.0	2.85	19.84						827	5	2.80		
		EC10	317.30		90.1		0.83																
11	FC10												15.25						2011.6	_	0.40		Offsite flow, Input from Hydraflow
11	EC10												15.25						2811.6	5	9.40		Hydrographs, Calculated via SCS Method
		D1.5	9.37	0.59	14.5	5.53	3.58	19.8															
12	D1.5								14.5	9.37	5.53	3.58	19.77						135	5	0.50		
		D1.6	1.94	0.38	14.9	0.73	3.53	2.6															
13	DP12, D1.6								14.96	11.3	6.3	3.53	22.05						35	5	0.10		
		D1.7	1.56	0.38	14.8	0.59	3.54	2.1					0										
14	DP13, D1.7			0.00		0.10	2.72	4.0	15.06	12.9	6.8	3.52	24.05						232	5	0.80		
15	DD44 D4 0	D1.8	1.3	0.38	13.1	0.49	3.72	1.8	45.00	440	7.0	2.44	25.40						25	_	0.10		
15	DP14, D1.8	D1 0	0.54	0.20	0.5	0.20	4.24	0.0	15.86	14.2	7.3	3.44	25.19						35	5	0.10		
16	DD1E D1 0	D1.9	0.54	0.38	9.5	0.20	4.21	0.9	15.00	117	7.5	2.42	25.03						137	Г	0.50		
16	DP15, D1.9	D1.10	2.12	0.38	10.1	0.80	4.11	3.3	15.96	14.7	7.5	3.43	25.82						137	5	0.50		
17	D1.10	D1.10	2.12	0.36	10.1	0.80	4.11	3.3	10.12	2.1	0.8	4.11	3.27						20	5	0.10		
1/	D1.10	D1.11	1.23	0.74	8.0	0.91	4.47	4.0	10.12	2.1	0.8	4.11	3.27						10	5	0.10		
18	D1.11, DP17, DP10	D1.11	1.23	0.74	0.0	0.91	7.47	4.0	26.3	21.9	8.7	2.68	23.22						63	5	0.20		
10	D1.11, D1 17, D1 10								20.5	21.9	0.7	2.00	23.22						03		0.20		
																							Total into upper Channel D, Input from
19	DP16, DP18								26.5	36.7	16.2	2.67	43.20						1024	5	3.40		Hydraflow Hydrographs
		D2.0	11.9	0.32	25.2	3.75	2.74	10.3]											

																	 	_	_	
20	DP19, D2.0								29.91	48.6	20.0	2.49	49.60							
		C3.0	35.4	0.23	25.3	8.05	2.73	22.0												
21	DP4, C3.0								25.6	49.1	13.6	2.72	36.96							To channel C2
		D2.1	3.15	0.08	14.4	0.25	3.58	0.9												
22	D2.1, DP20, DP21								26.5	100.8	33.8	2.67	90.15		90.1					
23	POND D OUTFLOW												1.20							100 YEAR RELEASE RATE FOR POND D
																				T 1
		E1	4.63	0.08	34.3	0.37		0.4					0.40							nput from Hydraflow Hydrographs,
		LI	4.03	0.08	54.5	0.37		0.4					0.40							Calculated via SCS Method
24	E1, DP11									321.9			15.40							
25	DP23, DP24												16.60							
																				/
																			1	
																			/	
																			/	
																			/	

5 yr release rate?

PROPOSED STORM DRAINAGE SYSTEM DESIGN - 100-YEAR DESIGN STORM

Designer: ESJ

Company: R&R Engineers-Surveyors
Date: 8/29/2022 Project: Mayberry Filing 3 Location: El Paso County

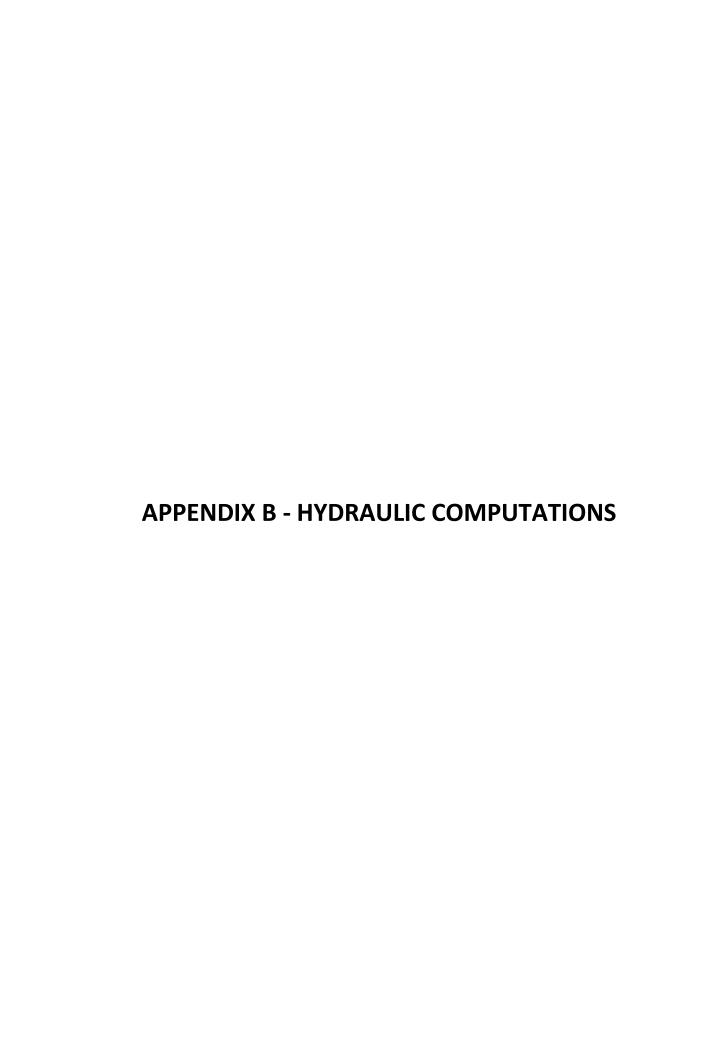
Cells of this color are for required user-input Cells of this color are for optional user-input

 $I_{100} = -2.52 \ln(D) + 12.735$



				DIRE	CT RUNOFF	•					OTAL RUNG)FF		CTREET	BYPASS	<u> </u>	PIPE		Γ	TDAV	LTIME		SURVEYORS
DESGIN POINT	STREET/ CONTRIBUTING	Basin Name	Area	Coeff	Tc	C*A	ı	Q	Тс	Sum Area	Sum C*A		Q		Street Q	Design Q		PIPE	L	VEL	Tt	Q add'l	Remarks
10	BASINS		(ac)	С	(min)	(ac)		(cfs)	(min)	(ac)	(ac)	in/hr	cfs	%	cfs	cfs	%	SIZE	ft	ft/sec	min		
		C2.1	0.77	0.55	11.8	0.42	6.51	2.73	, ,	, ,	, ,												
1	C2.1								11.8	0.77	0.42	6.51	2.73						33	5	0.10		
		C2.2	0.33	0.55	7.1	0.18	7.78	1.40															
2	DP1, C2.2								11.9	1.10	0.60	6.49	3.89						450	5	1.50		
		C2.3	11.41	0.55	20.1	6.22	5.17	32.15											10	5	0.00		
3	C2.3, DP2								20.1	12.51	6.82	5.17	35.25						64	5	0.20		
		C2.4	1.16	0.84	6.5	0.97	8.02	7.79				- 45	40.00						4500		5.00		
4	C2.3, DP3	D4.4	10.15	0.55	24.7	F 70	4.00	20.25	20.3	13.67	7.79	5.15	40.08						1590	5	5.30		
Г	D1 1	D1.1	10.45	0.55	21.7	5.70	4.98	28.35	24.7	10.45	F 70	4.98	28.35						20	5	0.10		
5	D1.1	D1.2	2.57	0.55	14.9	1.40	5.94	8.31	21.7	10.45	5.70	4.98	28.35						28	5	0.10		
6	D1.2	D1.2	2.37	0.55	14.5	1.40	3.34	6.31	14.9	2.57	1.40	5.94	8.31						10	5	0.00		
0	D1.2								14.5	2.57	1.40	3.54	0.51						10		0.00		
7	DP5, DP6								21.8	13.02	7.10	4.97	35.25						512	5	1.70		
	-, -	D1.3	2.02	0.55	10.4	1.10	6.84	7.53			-												
8	D1.3								10.4	2.02	1.10	6.84	7.53						27	5	0.10		
9	DP7, DP8								23.51	15.04	8.20	4.78	39.16						10	5	0.00		
		D1.4	3.55	0.55	14.9	1.93	5.93	11.48															
10	DP9, D1.4								23.51	18.6	10.1	4.78	48.41						827	5	2.80		
		EC10	317.30		90.1																		
11	EC10												110.89						2811.6	5	9.40		Offsite flow, Input from Hydraflow Hydrographs, Calculated via SCS Method
		D1.5	9.37	0.70	14.5	6.56	6.00	39.4															
12	D1.5								14.5	9.37	6.56	6.00	39.38						135	5	0.50		
		D1.6	1.94	0.55	14.9	1.06	5.93	6.3												_	0.10		
13	DP12, D1.6	D4 7	4.56	0.55	440	0.05	F 04	F 0	14.96	11.3	7.6	5.92	45.07						35	5	0.10		
14	DP13, D1.7	D1.7	1.56	0.55	14.8	0.85	5.94	5.0	15.06	12.9	8.5	5.90	49.96						232	5	0.80		
	DI 13, D1.7	D1.8	1.3	0.55	13.1	0.71	6.25	4.4	13.00	12.5	0.5	3.30	43.30						232		0.00		
15	DP14, D1.8	21.0	2.0	0.00	20.2	0.7.2	0.20		15.86	14.2	9.2	5.77	52.94						35	5	0.10		
		D1.9	0.54	0.55	9.5	0.29	7.06	2.1															
16	DP15, D1.9								15.96	14.7	9.5	5.75	54.49						137	5	0.50		
		D1.10	2.12	0.55	10.1	1.16	6.90	8.0															
17	D1.10								10.12	2.1	1.2	6.90	7.97						20	5	0.10		
		D1.11	1.23	0.84	8.0	1.03	7.51	7.7			15.	4 10							10	5	0.00		
18	D1.11, DP17, DP10								26.3	21.9	12.3	4.49	55.36						63	5	0.20		
																							Total into upper Channel D, Input from
19	DP16, DP18								26.5	36.7	21.8	4.48	97.50						1024	5	3.40		Hydraflow Hydrographs
		D2.0	11.9	0.51	25.2	6.02	4.61	27.7															
20	DP19, D2.0								29.91	48.6	27.8	4.17	115.98										

		C3.0	35.4	0.45	25.3	15.84	4.59	72.7				1							
21	DP4, C3.0								25.6	49.1	23.6	4.56	107.80						To channel C2
		D2.1	3.15	0.35	14.4	1.10	6.01	6.6											
22	D2.1, DP20, DP21								26.5	100.8	52.5	4.48	235.13		235.1				
23	POND D OUTFLOW												39.60						100 YEAR RELEASE RATE FOR POND D
		Г1	4.63	0.35	34.3	1.62		3.3					3.25						Input from Hydraflow Hydrographs,
		E1	4.03	0.55	34.3	1.02		3.3					3.25						Calculated via SCS Method
24	E1, DP11									321.9			111.80						
25	DP23, DP24												151.40						

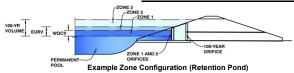


DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.06 (July 2022)

Project: MAYBERRY FILING 3

Basin ID: DETENTION POND D



Watershed Information

Selected BMP Type =	EDB	
Watershed Area =	101.00	acres
Watershed Length =	2,867	ft
Watershed Length to Centroid =	1,433	ft
Watershed Slope =	0.010	ft/ft
Watershed Imperviousness =	41.00%	percent
Percentage Hydrologic Soil Group A =	100.0%	percent
Percentage Hydrologic Soil Group B =	0.0%	percent
Percentage Hydrologic Soil Groups C/D =	0.0%	percent
Target WQCV Drain Time =	40.0	hours
Location for 1-hr Rainfall Depths =	User Input	•

After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

the embedded colorado orban nydro	grapii riocedu	ie.
Water Quality Capture Volume (WQCV) =	1.536	acre-feet
Excess Urban Runoff Volume (EURV) =	4.517	acre-feet
2-yr Runoff Volume (P1 = 1.19 in.) =	3.434	acre-feet
5-yr Runoff Volume (P1 = 1.5 in.) =	4.616	acre-feet
10-yr Runoff Volume (P1 = 1.75 in.) =	5.562	acre-feet
25-yr Runoff Volume (P1 = 2 in.) =	7.292	acre-feet
50-yr Runoff Volume (P1 = 2.25 in.) =	8.982	acre-feet
100-yr Runoff Volume (P1 = 2.52 in.) =	11.188	acre-feet
500-yr Runoff Volume (P1 = 3.14 in.) =	15.946	acre-feet
Approximate 2-yr Detention Volume =	2.879	acre-feet
Approximate 5-yr Detention Volume =	3.810	acre-feet
Approximate 10-yr Detention Volume =	4.693	acre-feet
Approximate 25-yr Detention Volume =	5.813	acre-feet
Approximate 50-yr Detention Volume =	6.565	acre-feet
Approximate 100-yr Detention Volume =	7.595	acre-feet

Optional User Overrides

	acre-feet
	acre-feet
1.19	inches
1.50	inches
1.75	inches
2.00	inches
2.25	inches
2.52	inches
3.14	inches

Define Zones and Basin Geometry

Zone 1 Volume (WQCV) =	1.536	acre-feet
Zone 2 Volume (EURV - Zone 1) =	2.981	acre-feet
Zone 3 (100yr + 1 / 2 WQCV - Zones 1 & 2) =	3.846	acre-feet
Total Detention Basin Volume =	8.363	acre-feet
Initial Surcharge Volume (ISV) =	user	ft ³
Initial Surcharge Depth (ISD) =	user	ft
Total Available Detention Depth $(H_{total}) =$	user	ft
Depth of Trickle Channel (H_{TC}) =	user	ft
Slope of Trickle Channel (S_{TC}) =	user	ft/ft
Slopes of Main Basin Sides $(S_{main}) =$	user	H:V
Basin Length-to-Width Ratio ($R_{L/W}$) =	user	
		='
Initial Surcharge Area $(A_{ISV}) =$	user	ft²
Surcharge Volume Length $(L_{ISV}) =$	user	ft
Surcharge Volume Width $(W_{ISV}) =$	user	ft
Depth of Basin Floor $(H_{FLOOR}) =$	user	ft
Length of Basin Floor $(L_{FLOOR}) =$	user	ft
Width of Basin Floor $(W_{FLOOR}) =$	user	ft
Area of Basin Floor $(A_{FLOOR}) =$	user	ft²
Volume of Basin Floor $(V_{FLOOR}) =$	user	ft ³
Depth of Main Basin (H_{MAIN}) =	user	ft

Length of Main Basin (L_{MAIN}) =

Width of Main Basin (W_{MAIN}) =

 $\label{eq:Volume of Main Basin (V_MAIN) = Calculated Total Basin Volume (V_{total}) = Calculated Total Basin Volume (V_{total}) = Calculated Total Basin Volume (V_{total}) = Calculated Total Basin (V_MAIN) =$

Area of Main Basin (A_{MAIN}) =

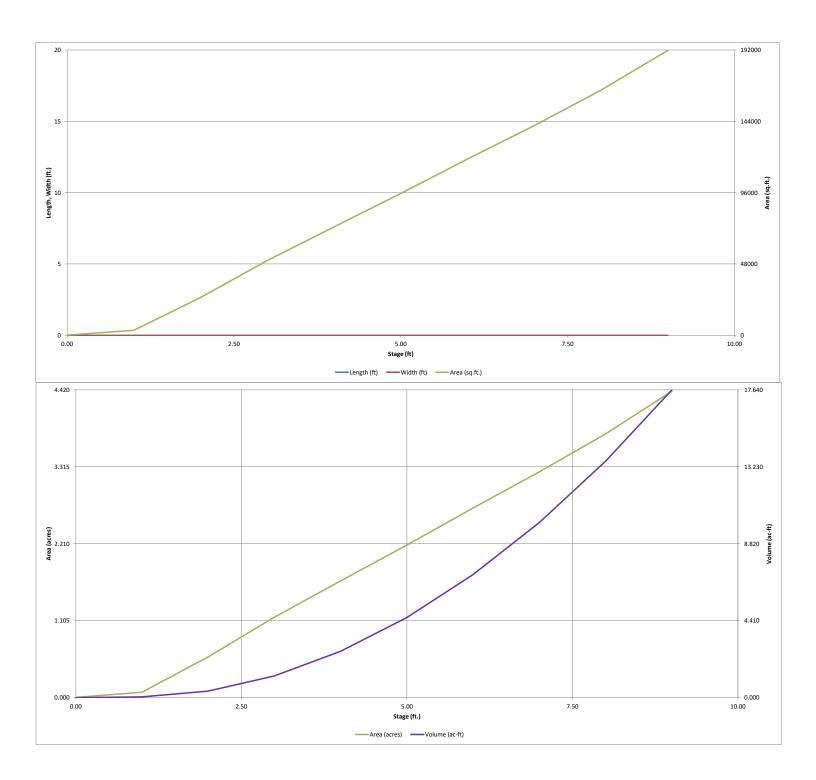
user

user

user

user

Double In constant]_							
Depth Increment =		ft Optional				Optional			
Stage - Storage Description	Stage (ft)	Override Stage (ft)	Length (ft)	Width (ft)	Area (ft 2)	Override Area (ft ²)	Area (acre)	Volume (ft 3)	Volume (ac-ft)
Top of Micropool		0.00				170	0.004	(16.)	(uc-it)
6027		1.00				3,344	0.077	1,757	0.040
6028		2.00				25,396	0.583	16,127	0.370
6029		3.00				50,286	1.154	53,968	1.239
6030		4.00				72,956	1.675	115,589	2.654
6031		5.00				95,393	2.190	199,763	4.586
6032		6.00				118,525	2.721	306,722	7.041
6033		7.00				141,085	3.239	436,527	10.021
6034 6035		8.00 9.00				164,866 191,669	3.785 4.400	589,503 767,770	13.533 17.626
0033		9.00				191,009	1.100	707,770	17.020
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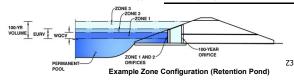


POND D - MHFD-Detention .xlsm, Basin 8/29/2022, 8:11 AM

DETENTION BASIN OUTLET STRUCTURE DESIGN

Estimated

Project: MAYBERRY FILING 3 Basin ID: DETENTION POND D



	Locimatea	Lournacca	
	Stage (ft)	Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	3.25	1.536	Orifice Plate
Zone 2 (EURV)	4.97	2.981	Orifice Plate
(100+1/2WQCV)	6.47	3.846	Weir&Pipe (Restrict)
	Total (all zones)	8.363	

Estimated

<u>User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)</u>

Underdrain Orifice Invert Depth = ft (distance below the filtration media surface) N/A Underdrain Orifice Diameter = N/A inches

	Calculated Parameters for Underd					
Underdrain Orifice Area =	N/A	ft ²				
Underdrain Orifice Centroid =	N/A	feet				

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP) ft (relative to basin bottom at Stage = 0 ft) Centroid of Lowest Orifice = 0.00 ft (relative to basin bottom at Stage = 0 ft)

Depth at top of Zone using Orifice Plate = 4.97 Orifice Plate: Orifice Vertical Spacing = N/A inches Orifice Plate: Orifice Area per Row = N/A sq. inches

BMP)	Calculated Paramet	ters for Plate
WQ Orifice Area per Row =	N/A	ft ²
Elliptical Half-Width =	N/A	feet
Elliptical Slot Centroid =	N/A	feet
Elliptical Slot Area =	N/A	ft ²
·		

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

Row 1 (required) Row 2 (optional) Row 3 (optional) Row 4 (optional) Row 5 (optional) Row 6 (optional) Row 7 (optional) Stage of Orifice Centroid (ft) 0.00 1.66 3.32 Orifice Area (sq. inches) 6.00 7.00 9.00

Row 9 (optional) Row 10 (optional) Row 11 (optional) Row 12 (optional) Row 13 (optional) Row 14 (optional) Row 15 (optional) Row 16 (optional) Stage of Orifice Centroid (ft) Orifice Area (sq. inches)

User Input: Vertical Orifice (Circular or Rectangular)

ser Input: Vertical Orifice (Circular or Rectangu	ılar)				Calculated Paramet	ters for Vertical Orif	fice
	Not Selected	Not Selected			Not Selected	Not Selected	
Invert of Vertical Orifice =	N/A	N/A	ft (relative to basin bottom at Stage = 0 ft)	Vertical Orifice Area =	N/A	N/A	ft ²
Depth at top of Zone using Vertical Orifice =	N/A	N/A	ft (relative to basin bottom at Stage = 0 ft)	Vertical Orifice Centroid =	N/A	N/A	feet
Vertical Orifice Diameter =	N/A	N/A	inches	-			

User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir and No Outlet Pipe)

	Zone 3 Weir	Not Selected		
Overflow Weir Front Edge Height, Ho =	5.50	N/A	ft (relative to basin bottom at Stage = 0 ft)	Height of Grate Upper E
Overflow Weir Front Edge Length =	7.00	N/A	feet	Overflow Weir Slope
Overflow Weir Grate Slope =	0.00	N/A	H:V Grate	e Open Area / 100-yr Orific
Horiz. Length of Weir Sides =	6.00	N/A	feet Over	flow Grate Open Area w/o
Overflow Grate Type =	Type C Grate	N/A	Ove	erflow Grate Open Area w/
Debris Clogging % =	50%	N/A	%	

Calculated Parameters for Overflow Weir					
	Zone 3 Weir	Not Selected			
Grate Upper Edge, H_t =	5.50	N/A	feet		
w Weir Slope Length =	6.00	N/A	feet		
/ 100-yr Orifice Area =	6.46	N/A			
pen Area w/o Debris =	29.23	N/A	ft ²		
Open Area w/ Debris =	14.62	N/A	ft ²		
•			-		

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

	Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	0.00	N/A	ft (distance below basin bottom at Stage = 0 ft)
Outlet Pipe Diameter =	36.00	N/A	inches
Restrictor Plate Height Above Pipe Invert =	22.00		inches Half-Central Angle

	Calculated Parameters	for Outlet Pipe w/	Flow Restriction P	late
		Zone 3 Restrictor	Not Selected	
m at Stage = 0 ft)	Outlet Orifice Area =	4.53	N/A	ft ²
	Outlet Orifice Centroid =	1.04	N/A	feet
Half-Central Angle	of Restrictor Plate on Pipe =	1.79	N/A	radia

User Input: Emergency Spillway (Rectangular or Trapezoidal)

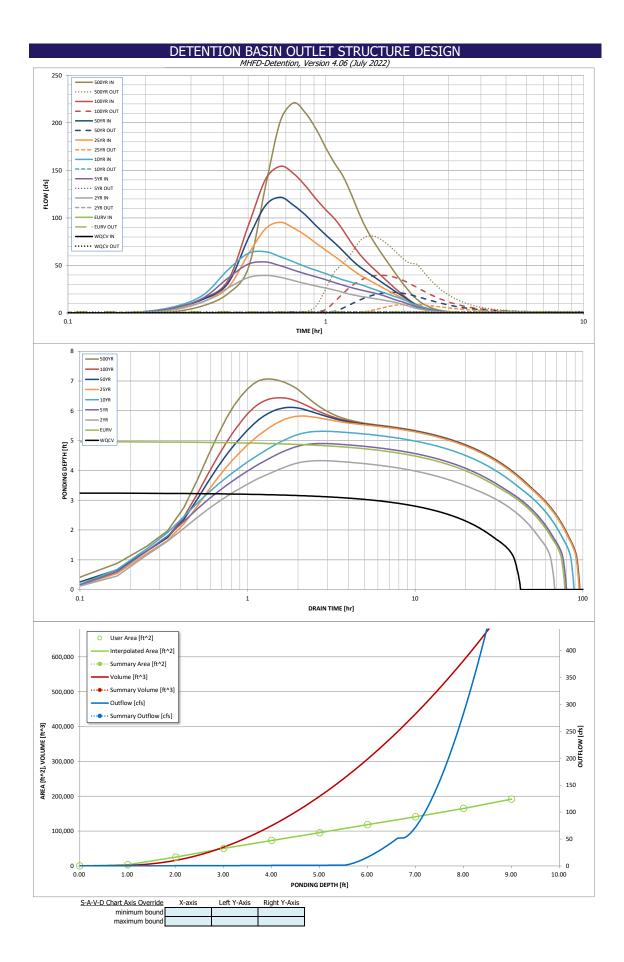
Spillway Invert Stage=	6.75	ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length =	50.00	feet
Spillway End Slopes =	4.00	H:V
Freeboard above Max Water Surface =	1.00	feet

	Calculated Parameters for Spillwa				
Spillway Design Flow Depth=	0.97	feet			
Stage at Top of Freeboard =		feet			
Basin Area at Top of Freeboard =	4.22	acres			
Basin Volume at Top of Freeboard =	16.38	acre-ft			

Routed Hydrograph Results Design Storm Return Per One-Hour Rainfall Depth CUHP Runoff Volume (acre Inflow Hydrograph Volume (acre CUHP Predevelopment Peak O (OPTIONAL Override Predevelopment Peak Q (o Predevelopment Unit Peak Flow, q (cfs/ac Peak Inflow Q (cfs/ac Peak Outflow Q (d Ratio Peak Outflow to Predevelopmer Structure Controlling F Max Velocity through Grate 1 (f Max Velocity through Grate 2 (f Time to Drain 97% of Inflow Volume (hou Time to Drain 99% of Inflow Volume (hou

a nyarograph kesuits	The user can over	ride the default CUF	IP hydrographs and	runoff volumes by	entering new value	es in the Inflow Hydi	rographs table (Coll	umns W through Af	<i>).</i>
Design Storm Return Period =	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
One-Hour Rainfall Depth (in) =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52	3.14
CUHP Runoff Volume (acre-ft) =	1.536	4.517	3.434	4.616	5.562	7.292	8.982	11.188	15.946
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	3.434	4.616	5.562	7.292	8.982	11.188	15.946
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A	0.6	1.2	1.7	15.8	31.6	52.4	95.2
DNAL Override Predevelopment Peak Q (cfs) =	N/A	N/A							
redevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.01	0.01	0.02	0.16	0.31	0.52	0.94
Peak Inflow Q (cfs) =	N/A	N/A	39.6	53.6	64.5	95.4	121.6	154.4	221.0
Peak Outflow Q (cfs) =	0.7	1.3	1.1	1.2	1.3	9.2	21.6	39.6	81.1
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	1.0	0.8	0.6	0.7	0.8	0.9
Structure Controlling Flow =	Plate	Plate	Plate	Plate	Plate	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Spillway
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	N/A	N/A	0.3	0.7	1.3	1.8
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
ime to Drain 97% of Inflow Volume (hours) =	39	70	61	71	79	83	81	80	76
ime to Drain 99% of Inflow Volume (hours) =	41	75	65	76	84	90	89	89	86
Maximum Ponding Depth (ft) =	3.25	4.97	4.33	4.90	5.31	5.83	6.11	6.44	7.07
Area at Maximum Ponding Depth (acres) =	1.28	2.17	1.84	2.14	2.35	2.63	2.78	2.94	3.27
Maximum Volume Stored (acre-ft) =	1.544	4.520	3.216	4.370	5.290	6.560	7.344	8.259	10.217

POND D - MHFD-Detention .xlsm, Outlet Structure 8/29/2022, 8:11 AM



POND D - MHFD-Detention .xlsm, Outlet Structure 8/29/2022, 8:11 AM

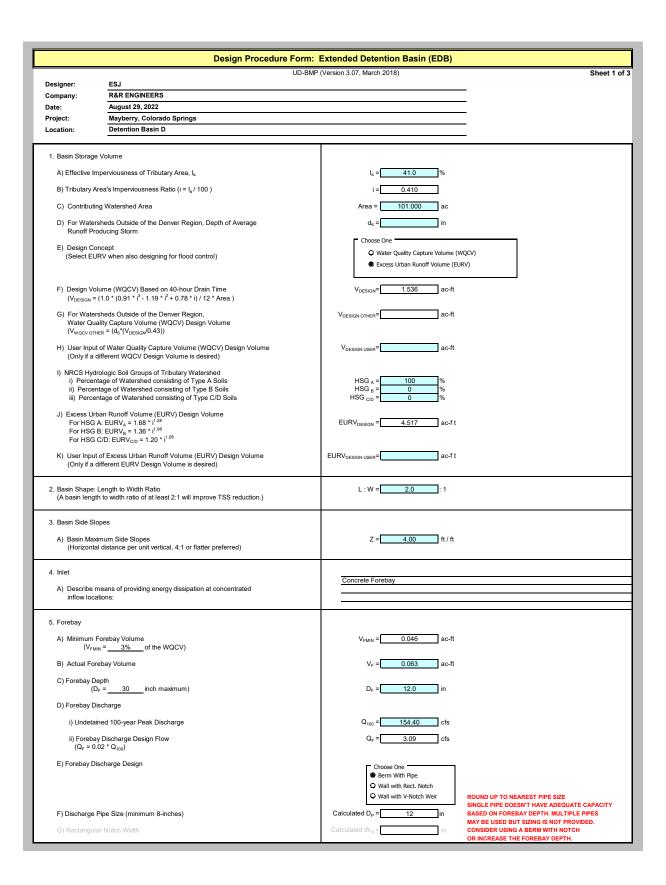
DETENTION BASIN OUTLET STRUCTURE DESIGN Outflow Hydrograph Workbook Filename:

Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

				I I I I I I I I I I I I I I I I I I I				ed in a separate p	Jiograffi.	
	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
3.00 111111	0:05:00									
		0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.33	0.03	1.06
	0:15:00	0.00	0.00	2.83	4.61	5.75	3.89	5.06	4.81	7.48
	0:20:00	0.00	0.00	11.58	15.65	18.69	12.00	14.26	15.04	20.21
	0:25:00	0.00	0.00	26.23	36.54	45.11	26.36	31.00	33.85	46.70
	0:30:00	0.00	0.00	37.24	51.33	62.55	61.58	78.11	91.35	132.74
	0:35:00	0.00	0.00	39.59	53.59	64.46	88.46	112.86	140.38	202.05
	0:40:00	0.00	0.00	37.47	49.62	59.12	95.38	121.60	154.38	220.99
	0:45:00	0.00	0.00	34.08	45.13	53.77	89.26	113.22	146.64	210.50
	0:50:00	0.00	0.00	30.91	41.27	48.81	81.79	103.12	133.85	193.65
	0:55:00	0.00	0.00	28.35	37.99	44.88	73.39	91.80	119.99	173.89
	1:00:00	0.00	0.00	26.20	34.94	41.34	66.03	82.14	108.52	157.39
	1:05:00	0.00	0.00	24.10	31.93	37.92	59.47	73.62	98.94	143.85
	1:10:00	0.00	0.00	21.73	29.24	34.82	52.95	65.16	87.17	126.32
	1:15:00	0.00	0.00	19.59	26.85	32.54	46.64	56.91	74.81	107.56
	1:20:00	0.00	0.00	18.01	24.92	30.63	41.23	50.04	64.10	91.81
	1:25:00	0.00	0.00	16.79	23.25	28.36	37.06	44.78	55.85	79.59
	1:30:00	0.00	0.00	15.69	21.71	25.98	33.28	40.04	49.01	69.33
	1:35:00	0.00	0.00	14.67	20.26	23.76	29.76	35.62	43.07	60.44
	1:40:00	0.00	0.00	13.64	18.43	21.67	26.45	31.47	37.54	52.20
	1:45:00	0.00	0.00	12.61	16.44	19.66	23.35	27.56	32.29	44.39
	1:50:00	0.00	0.00	11.59	14.50	17.74	20.38	23.81	27.31	37.05
	1:55:00					15.91				30.35
		0.00	0.00	10.19	12.81		17.64	20.36	22.76	
	2:00:00	0.00	0.00	8.82	11.35	14.18	15.20	17.29	18.70	24.42
	2:05:00	0.00	0.00	7.36	9.64	12.06	12.29	13.88	14.65	19.08
	2:10:00	0.00	0.00	6.03	7.92	9.91	9.71	10.94	11.33	14.69
	2:15:00	0.00	0.00	4.89	6.41	8.05	7.69	8.63	8.78	11.27
	2:20:00	0.00	0.00	3.99	5.21	6.56	6.16	6.89	6.86	8.71
	2:25:00	0.00	0.00	3.23	4.22	5.31	4.91	5.49	5.35	6.72
	2:30:00	0.00	0.00	2.60	3.42	4.27	3.93	4.38	4.16	5.16
	2:35:00	0.00	0.00	2.08	2.73	3.39	3.10	3.45	3.20	3.92
	2:40:00	0.00	0.00	1.65	2.15	2.65	2.42	2.68	2.48	3.03
	2:45:00	0.00	0.00	1.32	1.67	2.07	1.88	2.09	1.93	2.36
	2:50:00	0.00	0.00	1.04	1.31	1.62	1.48	1.64	1.53	1.87
	2:55:00	0.00	0.00	0.81	1.02	1.27	1.16	1.28	1.21	1.47
	3:00:00	0.00	0.00	0.61	0.76	0.97	0.88	0.97	0.92	1.11
	3:05:00	0.00	0.00	0.44	0.55	0.71	0.65	0.71	0.67	0.80
	3:10:00	0.00	0.00	0.30	0.38	0.49	0.45	0.49	0.46	0.55
	3:15:00	0.00	0.00	0.18	0.25	0.31	0.29	0.32	0.29	0.34
	3:20:00	0.00	0.00	0.10	0.15	0.17	0.17	0.18	0.16	0.18
	3:25:00	0.00	0.00	0.04	0.07	0.08	0.08	0.08	0.07	0.07
	3:30:00	0.00	0.00	0.01	0.02	0.02	0.02	0.02	0.01	0.01
	3:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:35:00 4:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:10:00 5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:50:00 5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0.00.00	0.00	0.00	0.00	0.00	0.00	0.00	3.00	0.00	3.00

POND D - MHFD-Detention .xlsm, Outlet Structure 8/29/2022, 8:11 AM



	Design Procedure Form:	Extended Detention Basin (EDB)
Dooignos	ESJ	Sheet 2 of 3
Designer: Company:	R&R ENGINEERS	
Date:	August 29, 2022	
Project:	Mayberry, Colorado Springs	
Location:	Detention Basin D	
6. Trickle Channe	al Control of the Con	Choose One
A) Type of Tric	okla Channal	● Concrete
A) Type of The	ine Chainei	○ Soft Bottom
F) Slope of Trie	ckle Channel	S = 0.0050 ft / ft
7. Micropool and 0	Outlet Structure	
A) Depth of Mic	cropool (2.5-feet minimum)	D _M = 2.5 ft
B) Surface Are	ea of Micropool (10 ft² minimum)	A _M = 170 sq ft
C) Outlet Type		
-, - ,		Choose One Orifice Plate
		O Other (Describe):
		Garage (Security)
	mension of Orifice Opening Based on Hydrograph Routing	
(Use UD-Deten	ition)	D _{orffce} = 6.00 inches
E) Total Outlet	Area	A _{ot} = 22.00 square inches
Initial Surcharge	e Volume	
A) D4b61-4	tial Surcharge Volume	D _{IS} = 4 in
	ecommended depth is 4 inches)	D _{IS} = 4 in
R) Minimum Init	tial Surcharge Volume	V _{IS} = 201 cu ft
	lume of 0.3% of the WQCV)	V _{IS} 201
C) Initial Surcha	arge Provided Above Micropool	V _s = 56.7 cu ft
,		·
9. Trash Rack		
A) Water Quali	ity Screen Open Area: A _t = A _{ot} * 38.5*(e ^{-0.095D})	A _t = 479 square inches
	een (If specifying an alternative to the materials recommended	Aluminum Amico-Klemp SR Series with Cross Rods 4" O.C.
	indicate "other" and enter the ratio of the total open are to the e for the material specified.)	
	Other (Y/N): N	
C) Ratio of Tota	al Open Area to Total Area (only for type 'Other')	User Ratio =
D) Total Water	Quality Screen Area (based on screen type)	A _{total} = 622 sq. in.
	sign Volume (EURV or WQCV) design concept chosen under 1E)	H=feet
F) Height of Wa	ater Quality Screen (H _{TR})	H _{TR} = 87.64 inches
	ater Quality Screen Opening (W _{opening})	W _{opening} = 12.0 inches VALUE LESS THAN RECOMMENDED MIN. WIDTH.
(Minimum of 12	2 inches is recommended)	WIDTH HAS BEEN SET TO 12 INCHES.

	Design Procedure Form	: Extended Detention Basin (EDB)
Designer: Company: Date: Project: Location:	ESJ R&R ENGINEERS August 29, 2022 Mayberry, Colorado Springs Detention Basin D	Sheet 3 of 3
B) Slope of	nbankment e embankment protection for 100-year and greater overtopping: Overflow Embankment tlal distance per unit vertical, 4:1 or flatter preferred)	Buried Riprap Spillway Ze = 4.00 ft / ft Choose One O Irrigated Not Irrigated
12. Access A) Describe Notes:	e Sediment Removal Procedures	Periodic inspection and sediment removal as required; Access ramp provided to pond bottom
Notes:		

R&R Engineers-Surveyors Mayberry Filing 3 MC22110

MC22110 8/22/2022

Extended Detention Basin - Forebay 1 Sizing Calculations

SEDIMENT FOREBAY S	SIZING		
Contributing Tributary Area	48.60	AC	
Imperviousness	52.0%		
Contributing Area WQCV	0.212	watershed ir	nches
Required WQCV	0.858 37,361	AC-ft ft ³	
Contributing Impervious Acres	> 20	Acres	
Req. % of WQCV	3%		
Minimum Forebay Volume Maximum Forebay Depth	1,121 2.5	ft ³ ft	
Provided Forebay Depth	1.00	ft	
Provided Forebay Volume	1,360	ft ³	
FOREBAY RELEASE RATE CA	CULATION	ıc	
Pipe Diameter (feet)	0.83	ft	
Undetained 100-Year Peak Flow	116.0	cfs	
Required Outlet Flow (q)	2.3	cfs	
Provided Max Outlet Flow	1.3		From Hydraflow xpress

R&R Engineers-Surveyors Mayberry Filing 3 MC22110

MC22110 8/22/2022

Extended Detention Basin - Forebay 2 Sizing Calculations

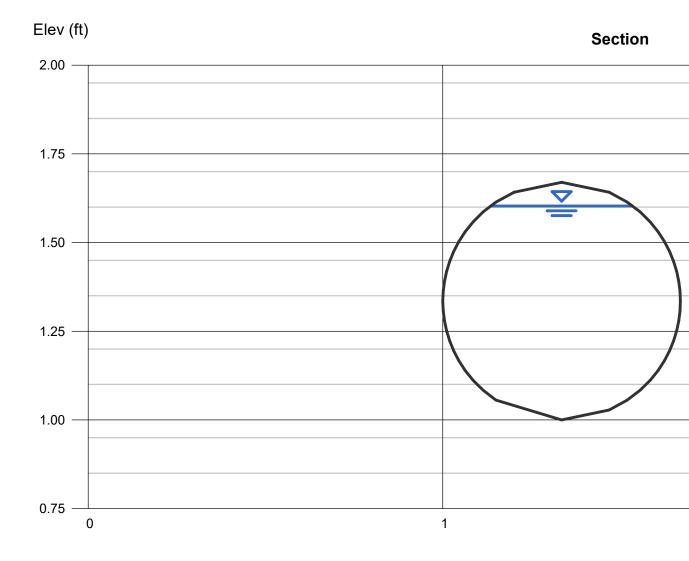
SEDIMENT FOREBAY S		
Contributing Tributary Area	49.10	AC
Imperviousness	32.0%	
Contributing Area WQCV	0.158	watershed inches
Required WQCV	0.645 28,083	AC-ft ft ³
Contributing Impervious Acres	5-20	Acres
Req. % of WQCV	3%	
Minimum Forebay Volume	842	ft ³
Maximum Forebay Depth	2.5	ft
Provided Forebay Depth	1.00	ft
Provided Forebay Volume	1,370	ft ³
FOREBAY RELEASE RATE CA	LCULATION	NS
Pipe Diameter (feet)	0.67	ft
Undetained 100-Year Peak Flow	107.8	cfs
Required Outlet Flow (q)	2.2	cfs
Provided Max Outlet Flow	1.3	cfs * From Hydraflo Express

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Friday, Aug 26 2022

Forebay 1 and 2 - Outlet Pipe

Circular		Highlighted	
Diameter (ft)	= 0.67	Depth (ft)	= 0.60
		Q (cfs)	= 1.333
		Area (sqft)	= 0.33
Invert Elev (ft)	= 1.00	Velocity (ft/s)	= 3.99
Slope (%)	= 0.50	Wetted Perim (ft)	= 1.68
N-Value	= 0.009	Crit Depth, Yc (ft)	= 0.55
		Top Width (ft)	= 0.40
Calculations		EGL (ft)	= 0.85
Compute by:	Q vs Depth		
No. Increments	= 10		



Scenario: 5 year Current Time Step: 0.000 h FlexTable: Conduit Table

Start Node	Stop Node	Invert (Start) (ft)	Section Type	Span	(ft)	Rise (ft)	Invert (Stop) (ft)	Length (User Defined) (ft)	Slope (Calculated) (ft/ft)	Diameter (in)	Manning's n	Flow (cfs)	Velocity (ft/s)	Hydraulic Grade Line (In) (ft)	Hydraulic Grade Line (Out) (ft)	Energy Grade Line (In) (ft)	Energy Grade Line (Out) (ft)
C2.4C	C2.5B	6,047.92	Circle	-		-	6,046.35	313.6	0.005	24.0	0.013	1.59	3.25	6,048.36	6,047.93	6,048.51	6,047.93
C2.4A	C2.4B	6,049.40	Circle	-		-	6,049.21	37.3	0.005	18.0	0.013	1.12	3.05	6,049.80	6,049.60	6,049.94	6,049.75
C2.4B	C2.4C	6,048.71	Circle	-		-	6,048.02	138.3	0.005	24.0	0.013	1.59	3.25	6,049.15	6,048.45	6,049.30	6,048.61
C2.5B	C2.5C	6,046.25	Circle	-		-	6,045.91	68.6	0.005	36.0	0.013	14.45	5.85	6,047.46	6,047.36	6,047.92	6,047.64
C2.5A	C2.5B	6,046.42	Circle	-		-	6,046.36	5.4	0.010	30.0	0.013	13.18	7.44	6,047.64	6,047.47	6,048.11	6,048.08
C2.5C	0-4	6,045.81	Circle	-		-	6,045.48	65.9	0.005	36.0	0.013	17.00	6.13	6,047.13	6,046.72	6,047.63	6,047.31
2.8C	C2.8D	6,042.53	Circle	-		-	6,041.27	234.4	0.005	36.0	0.013	14.10	5.98	6,043.73	6,042.49	6,044.17	6,042.91
C2.8C	2.8C	6,042.85	Circle	-		-	6,042.82	5.5	0.005	18.0	0.013	3.00	3.98	6,044.16	6,044.15	6,044.21	6,044.21
C2.8A	2.8C	6,043.21	Circle	-		-	6,043.03	27.5	0.007	30.0	0.013	11.62	6.16	6,044.35	6,044.07	6,044.79	6,044.63
C2.9C	D1.5D	6,037.56	Circle	-		-	6,034.76	559.5	0.005	36.0	0.013	19.51	6.36	6,038.98	6,036.56	6,039.52	6,036.86
C2.8D	C2.8E	6,041.07	Circle	-		-	6,039.92	144.0	0.008	36.0	0.013	14.10	6.90	6,042.27	6,041.41	6,042.71	6,041.66
C2.8E	C2.9A	6,039.82	Circle	-		-	6,038.89	133.6	0.007	36.0	0.013	14.10	6.57	6,041.02	6,040.58	6,041.46	6,040.77
C2.9A	C2.9B	6,038.79	Circle	-		-	6,038.76	5.7	0.005	36.0	0.013	15.72	6.13	6,040.39	6,040.39	6,040.65	6,040.64
C2.9B	C2.9C	6,038.66	Circle	-		-	6,037.66	199.3	0.005	36.0	0.013	19.51	6.36	6,040.08	6,039.50	6,040.63	6,039.79
2.9A	C2.9A	6,039.55	Circle	-		-	6,039.39	32.5	0.005	30.0	0.013	3.09	3.83	6,040.65	6,040.65	6,040.68	6,040.67
D1.3B	D1.4A	6,038.48	Ellipse		3.8	2.4	6,036.82	237.7	0.007	-	0.013	24.05	7.39	6,039.81	6,037.93	6,040.35	6,038.78
D1.3A	D1.3B	6,039.00	Ellipse		3.8	2.4	6,038.78	32.3	0.007	-	0.013	22.05	7.13	6,040.27	6,039.89	6,040.78	6,040.61
D1.4B	D4	6,036.42	Ellipse		3.8	2.4	6,034.71	199.4	0.009	-	0.013	25.82	8.11	6,037.80	6,035.81	6,038.37	6,036.83
D1.4A	D1.4B	6,036.72	Ellipse		3.8	2.4	6,036.52	32.3	0.006	-	0.013	25.19	7.19	6,038.08	6,037.73	6,038.64	6,038.48
D4	O-6	6,034.18	Ellipse		3.8	2.4	6,033.86	45.4	0.007		0.013	25.82	7.58	6,035.56	6,035.05	6,036.13	6,035.88
D1.5D	MH-3	6,034.66	Circle	-		-	6,034.48	34.5	0.005	36.0	0.013	22.91	6.73	6,036.20	6,035.94	6,036.81	6,036.64
D1.6	D1.5D	6,035.01	Circle	-		-	6,034.86	7.5	0.020	18.0	0.013	4.00	2.26	6,036.78	6,036.77	6,036.86	6,036.85
D1.5A	D1.5D	6,035.53	Circle	-		-	6,034.86	66.5	0.010	18.0	0.013	3.30	5.27	6,036.85	6,036.79	6,036.91	6,036.84
H-1	D1.3A	6,039.79	Ellipse		3.8	2.4	6,039.11	136.0	0.005	-	0.013	19.77	6.21	6,041.00	6,040.22	6,041.48	6,040.82
MH-3	0-7	6,034.38	Ellipse		3.8	2.4	6,033.86	58.1	0.009	-	0.013	22.91	7.93	6,035.68	6,034.91	6,036.20	6,035.81

Please provide a schematic of the storm pipes. As the storm pipes/inlets are not labeled on the drainage plan it is difficult to discern where each of the storm pipes occur. Scenario: 100 Year

Current Time Step: 0.000 h FlexTable: Conduit Table

Start Node	Stop Node	Invert (Start) (ft)	Section Type	Span (ft)	Rise (ft)	Invert (Stop) (ft)	Length (User Defined) (ft)	Slope (Calculated) (ft/ft)	Diameter (in)	Manning's n	Flow (cfs)	Velocity (ft/s)	Hydraulic Grade Line (In) (ft)	Hydraulic Grade Line (Out) (ft)	Energy Grade Line (In) (ft)	Energy Grade Line (Out) (ft)
C2.4C	C2.5B	6,047.92	Circle	-	-	6,046.35	313.6	0.005	24.0	0.013	3.89	4.20	6,049.14	6,049.07	6,049.20	6,049.09
C2.4A	C2.4B	6,049.40	Circle	-	-	6,049.21	37.3	0.005	18.0	0.013	2.73	3.91	6,050.03	6,049.84	6,050.26	6,050.07
C2.4B	C2.4C	6,048.71	Circle	-	l -	6,048.02	138.3	0.005	24.0	0.013	3.89	4.20	6,049.40	6,049.17	6,049.65	6,049.23
C2.5B	C2.5C	6,046.25	Circle	-	-	6,045.91	68.6	0.005	36.0	0.013	35.25	7.29	6,048.41	6,048.31	6,049.06	6,048.84
C2.5A	C2.5B	6,046.42	Circle	-	-	6,046.36	5.4	0.010	30.0	0.013	32.15	9.25	6,048.35	6,048.19	6,049.32	6,049.28
C2.5C	0-4	6,045.81	Circle	-	l -	6,045.48	65.9	0.005	36.0	0.013	40.08	7.49	6,047.93	6,047.54	6,048.81	6,048.47
2.8C	C2.8D	6,042.53	Circle	-	-	6,041.27	234.4	0.005	36.0	0.013	34.41	7.49	6,044.54	6,044.24	6,045.27	6,044.61
C2.8C	2.8C	6,042.85	Circle	-	-	6,042.82	5.5	0.005	18.0	0.013	7.31	4.14	6,045.10	6,045.07	6,045.36	6,045.34
C2.8A	2.8C	6,043.21	Circle	-	-	6,043.03	27.5	0.007	30.0	0.013	28.35	7.59	6,045.03	6,044.81	6,045.88	6,045.70
C2.9C	D1.5D	6,037.56	Circle	-	-	6,034.76	559.5	0.005	36.0	0.013	47.60	6.73	6,040.63	6,037.78	6,041.34	6,038.49
C2.8D	C2.8E	6,041.07	Circle	-	-	6,039.92	144.0	0.008	36.0	0.013	34.41	8.73	6,043.94	6,043.57	6,044.32	6,043.94
C2.8E	C2.9A	6,039.82	Circle	-	-	6,038.89	133.6	0.007	36.0	0.013	34.41	4.87	6,043.26	6,042.90	6,043.63	6,043.27
C2.9A	C2.9B	6,038.79	Circle	-	-	6,038.76	5.7	0.005	36.0	0.013	38.36	5.43	6,042.48	6,042.47	6,042.94	6,042.92
C2.9B	C2.9C	6,038.66	Circle	-	-	6,037.66	199.3	0.005	36.0	0.013	47.60	6.73	6,042.19	6,041.17	6,042.89	6,041.87
2.9A	C2.9A	6,039.55	Circle	-	-	6,039.39	32.5	0.005	30.0	0.013	7.53	1.53	6,042.97	6,042.96	6,043.01	6,043.00
D1.3B	D1.4A	6,038.48	Ellipse	3.8	2.4	6,036.82	237.7	0.007	-	0.013	49.96	9.02	6,040.41	6,039.01	6,041.43	6,039.83
D1.3A	D1.3B	6,039.00	Ellipse	3.8		6,038.78	32.3	0.007	-	0.013	45.07	8.75	6,040.84	6,040.46	6,041.75	6,041.56
D1.4B	D4	6,036.42	Ellipse	3.8		6,034.71	199.4	0.009	-	0.013	54.49	9.97	6,038.42	6,036.42	6,039.55	6,037.97
D1.4A	D1.4B	6,036.72	Ellipse	3.8		6,036.52	32.3	0.006	-	0.013	52.94	8.55	6,038.70	6,038.61	6,039.79	6,039.60
D4	O-6	6,034.18	Ellipse	3.8	2.4	6,033.86	45.4	0.007	-	0.013	54.49	9.13	6,036.18	6,035.75	6,037.31	6,037.01
D1.5D	MH-3	6,034.66	Circle	-	-	6,034.48	34.5	0.005	36.0	0.013	54.60	7.72	6,037.28	6,036.88	6,038.36	6,038.14
D1.6	D1.5D	6,035.01	Circle	-	-	6,034.86	7.5	0.020	18.0	0.013	7.70	4.36	6,038.19	6,038.15	6,038.48	6,038.44
D1.5A	D1.5D	6,035.53	Circle	-	-	6,034.86	66.5	0.010	18.0	0.013	8.00	4.53	6,038.51	6,038.13	6,038.83	6,038.45
H-1	D1.3A	6,039.79	Ellipse	3.8		6,039.11	136.0	0.005	-	0.013	39.38	7.54	6,041.52	6,041.24	6,042.33	6,041.78
MH-3	0-7	6,034.38	Ellipse	3.8	2.4	6,033.86	58.1	0.009	-	0.013	54.60	10.15	6,036.38	6,035.62	6,037.52	6,037.09

 $\verb|\label{loss} $$ \label{loss} $$ \label{los$

Culvert Report

Please label these on the Drainage Plan

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Wednesday, Aug 24 2022

Culverts E1 and E2

Invert Elev Dn (ft)	= 6038.35
Pipe Length (ft)	= 115.00
Slope (%)	= 0.70
Invert Elev Up (ft)	= 6039.16
Rise (in)	= 38.0
Shape	= Elliptical
Span (in)	= 60.0
No. Barrels	= 1
n-Value	= 0.013

Culvert Type = Horizontal Ellipse Concrete
Culvert Entrance = Square edge w/headwall (H)
Coeff. K,M,c,Y,k = 0.01, 2, 0.0398, 0.67, 0.5

Embankment

Top Elevation (ft) = 6044.25Top Width (ft) = 64.00Crest Width (ft) = 60.80

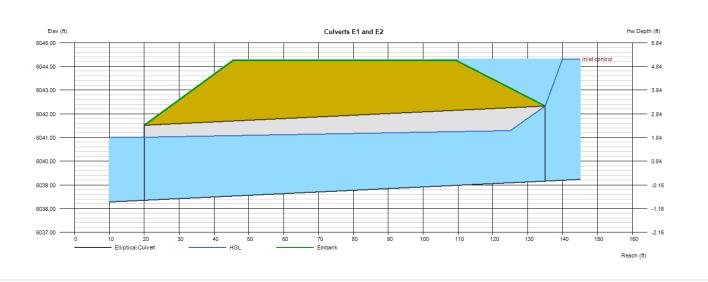
Calculations

 $\begin{array}{lll} \text{Qmin (cfs)} & = 15.00 \\ \text{Qmax (cfs)} & = 115.00 \\ \text{Tailwater Elev (ft)} & = (dc+D)/2 \end{array}$

Highlighted

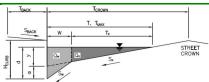
Qtotal (cfs) = 111.00Qpipe (cfs) = 108.71Qovertop (cfs) = 2.29Veloc Dn (ft/s) = 9.35Veloc Up (ft/s) = 11.66 HGL Dn (ft) = 6041.01 HGL Up (ft) = 6041.31Hw Elev (ft) = 6044.31Hw/D (ft) = 1.63

Flow Regime = Inlet Control

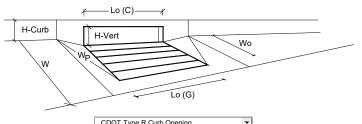


(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: MAYBERRY FILING 3
Inlet ID: C2.3 - DP3



laximum Allowable Width for Spread Behind Curb Side Slope Behind Curb (leave blank for no conveyance credit behind curb) S_{BACK} 0.020 ft/ft Manning's Roughness Behind Curb (typically between 0.012 and 0.020) n_{BACK} = 0.013 Height of Curb at Gutter Flow Line H_{CURB} : 6.00 nches Distance from Curb Face to Street Crown T_{CROWN} 28.0 Gutter Width W = 2.00 Street Transverse Slope ft/ft 0.020 Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) ft/ft 0.083 Street Longitudinal Slope - Enter 0 for sump condition S_0 ft/ft 0.000 Manning's Roughness for Street Section (typically between 0.012 and 0.020) n_{STREET} = 0.013 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm 28.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm inches 6.0 12.0 Check boxes are not applicable in SUMP conditions Maximum Capacity for 1/2 Street based On Allowable Spread Minor Storm Major Storm Water Depth without Gutter Depression (Eq. ST-2) Vertical Depth between Gutter Lip and Gutter Flowline (usually 2") y = d_C = 6.72 inches 6.72 inches 2.0 Gutter Depression (d_C - (W * S_x * 12)) a = inches 1.51 1.51 Water Depth at Gutter Flowline inches d = 8.23 8.23 Allowable Spread for Discharge outside the Gutter Section W (T - W) 26.0 26.0 Gutter Flow to Design Flow Ratio by FHWA HEC-22 method (Eq. ST-7) E_O = 0.209 0.209 Discharge outside the Gutter Section W, carried in Section T_X $\,Q_X\,$ cfs 0.0 0.0 Discharge within the Gutter Section W $(Q_T - Q_X)$ $Q_W =$ cfs 0.0 0.0 Discharge Behind the Curb (e.g., sidewalk, driveways, & lawns) Q_{BACK} cfs 0.0 0.0 Q_T = Maximum Flow Based On Allowable Spread cfs SUMP SUMP Flow Velocity within the Gutter Section V = 0.0 fps 0.0 V*d Product: Flow Velocity times Gutter Flowline Depth V*d = Maximum Capacity for 1/2 Street based on Allowable Depth Minor Storm Major Storm T_{TH} = Theoretical Water Spread 18.7 43.7 Theoretical Spread for Discharge outside the Gutter Section W (T - W) T_{X TH} = 16.7 41 7 Gutter Flow to Design Flow Ratio by FHWA HEC-22 method (Eq. ST-7) Eo = 0.318 0.130 Theoretical Discharge outside the Gutter Section W, carried in Section $T_{X\,TH}$ Q_{X TH} = 0.0 0.0 Actual Discharge outside the Gutter Section W, (limited by distance T_{CROWN}) Q_X = 0.0 0.0 Discharge within the Gutter Section W (Q_d - Q_X) Q_{W} cfs 0.0 0.0 Discharge Behind the Curb (e.g., sidewalk, driveways, & lawns) Q_{BACK} 0.0 cfs 0.0 Total Discharge for Major & Minor Storm (Pre-Safety Factor) cfs Q = 0.0 0.0 Average Flow Velocity Within the Gutter Section 0.0 0.0 fps V*d Product: Flow Velocity Times Gutter Flowline Depth V*d = 0.0 0.0 Slope-Based Depth Safety Reduction Factor for Major & Minor (d \geq 6") Storm SUMF SUMP Max Flow Based on Allowable Depth (Safety Factor Applied) $Q_d =$ SUMP cfs SUMP Resultant Flow Depth at Gutter Flowline (Safety Factor Applied) inches Resultant Flow Depth at Street Crown (Safety Factor Applied) d_{CROWN} = inches MINOR STORM Allowable Capacity is based on Depth Criterion MAJOR STORM Allowable Capacity is based on Depth Criterion Minor Storm SUMP $Q_{allow} =$



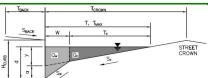
The County is not inclined to allow such a large inlet. Per the flow at this location it appears that a smaller inlet would work. INLET IN A SUMP OR SAG LOCATION Please reduce as much as possible.

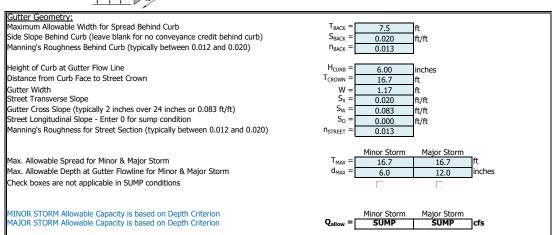
> I ran the calculation using an older MHFD version and the latest 5.02 and it appears that a 15' inlet may work. Please verify/revise the calc.

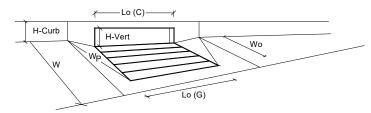
CDOT Type R Curb Opening _ accordingly. Design Information (Input) MINOR CDOT Type R Curb Opening inches Local Depression (additional to continuous gutter depression 'a' from above) 3.00 Number of Unit Inlets (Grate or Curb Opening) ✓ Override De No Ponding Depth = Water Depth at Flowline (outside of local depression) 6.0 12.0 linches Grate Information MINOR MAJOR Length of a Unit Grate L_o (G) = N/A Width of a Unit Grate N/A Area Opening Ratio for a Grate (typical values 0.15-0.90) N/A Clogging Factor for a Single Grate (typical value 0.50 - 0.70) $C_f(G) =$ N/A C_w (G) = C_o (G) = Grate Weir Coefficient (typical value 2.15 - 3.60) N/A Grate Orifice Coefficient (typical value 0.60 - 0.80) N/A Curb Opening Information MINO MAJOR L_o (C) = Length of a Unit Curb Opening 30.00 Height of Vertical Curb Opening in Inches H_{vert} 6.00 inches Height of Curb Orifice Throat in Inches H_{throat} 6.00 inches Angle of Throat (see USDCM Figure ST-5) Side Width for Depression Pan (typically the gutter width of 2 feet) Theta = 63.40 2.00 degrees feet Clogging Factor for a Single Curb Opening (typical value 0.10) C_f (C) = 0.10 0.10 Curb Opening Weir Coefficient (typical value 2.3-3.7) $C_w(C) =$ Curb Opening Orifice Coefficient (typical value 0.60 - 0.70) (L) = 0.67 Resultant Street Conditions MAJOR MINOR 30.00 30.00 feet Total Inlet Length Resultant Street Flow Spread (based on street geometry from above) ft.>T-Crown 18.7 0.0 Τ: 43.7 Resultant Flow Depth at Street Crown MINOR 18.0 MAJOR **78.9** Q. = Total Inlet Interception Capacity (assumes clogged condition) cfs Q PEAK REQUIRED

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: MAYBERRY FILING 3
Inlet ID: C2.1 - DP1



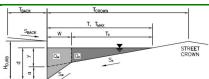


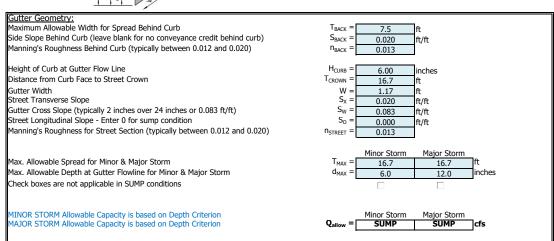


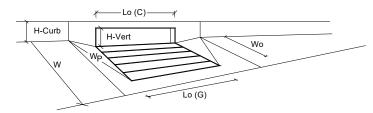
CDOT Type R Curb Opening				
Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	7
Water Depth at Flowline (outside of local depression)	Ponding Depth =	4.9	4.9	Override Depths
Grate Information	_	MINOR	MAJOR	 '
Length of a Unit Grate	$L_o(G) =$	N/A	N/A	feet
Width of a Unit Grate	W _o =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_f(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	$C_w(G) =$	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	$C_o(G) =$	N/A	N/A	
Curb Opening Information	_	MINOR	MAJOR	_
Length of a Unit Curb Opening	$L_o(C) =$	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	$H_{throat} =$	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	$W_p =$	1.17	1.17	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	C₀ (C) =	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	T _{ft}
Depth for Curb Opening Weir Equation	d _{Curb} =	0.31	0.31	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	0.63	0.63	
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	1.00	1.00	1
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A	
				
	0 -	MINOR	MAJOR	٦,
Total Inlet Interception Capacity (assumes clogged condition)	Q _a =	4.0	4.0	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	1.1	2.7	cfs

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: MAYBERRY FILING 3
Inlet ID: C2.2



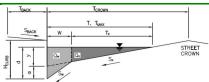




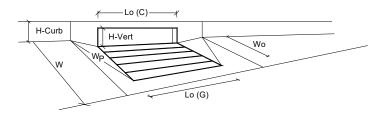
CDOT Type R Curb Opening				
Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	7_
Water Depth at Flowline (outside of local depression)	Ponding Depth =	4.9	4.9	Override Depths
Grate Information		MINOR	MAJOR	_
Length of a Unit Grate	$L_o(G) =$	N/A	N/A	feet
Width of a Unit Grate	W _o =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_f(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C_w (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	$C_o(G) =$	N/A	N/A	
Curb Opening Information	-	MINOR	MAJOR	_
Length of a Unit Curb Opening	$L_o(C) =$	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	$H_{throat} =$	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	$W_p =$	1.17	1.17	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	C₀ (C) =	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	$d_{Grate} =$	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d _{Curb} =	0.31	0.31	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	0.63	0.63	†
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	1.00	1.00	
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A	
	Glate	,	, ,,,,	
	<u>-</u>	MINOR	MAJOR	
Total Inlet Interception Capacity (assumes clogged condition)	$Q_a = $	4.0	4.0	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	0.6	1.4	cfs

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: MAYBERRY FILING 3
Inlet ID: D1.1 - DP5



Maximum Allowable Width for Spread Behind Curb
Side Slope Behind Curb (leave blank for no conveyance credit behind curb)
Manning's Roughness Behind Curb (typically between 0.012 and 0.020) T_{BACK} : S_{BACK} = 0.020 ft/ft n_{BACK} = 0.013 Height of Curb at Gutter Flow Line H_{CURB} = 6.00 nches Distance from Curb Face to Street Crown T_{CROWN} 17.0 W = S_X = Gutter Width 2.00 0.020 Street Transverse Slope ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) ft/ft 0.083 Street Longitudinal Slope - Enter 0 for sump condition S_0 ft/ft 0.000 Manning's Roughness for Street Section (typically between 0.012 and 0.020) n_{STREET} : 0.013 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm Max. Allowable Depth at Gutter Flowline for Minor & Major Storm 17.0 inches 6.0 12.0 Check boxes are not applicable in SUMP conditions MINOR STORM Allowable Capacity is based on Depth Criterion MAJOR STORM Allowable Capacity is based on Depth Criterion Minor Storm SUMP Major Storm SUMP

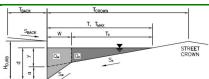


Design Information (Input)			MINOR	MAJOR	
Type of Inlet	CDOT Type R Curb Opening	Type =	CDOT Type R	Curb Opening	
	ntinuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Co	urb Opening)	No =	1	1	
Water Depth at Flowline (outside	of local depression)	Ponding Depth =	5.6	12.0	inches
Grate Information			MINOR	MAJOR	Override Depths
Length of a Unit Grate		$L_o(G) =$	N/A	N/A	reet
Width of a Unit Grate		$W_o =$	N/A	N/A	feet
Area Opening Ratio for a Grate (ty	pical values 0.15-0.90)	A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grate	(typical value 0.50 - 0.70)	$C_f(G) =$	N/A	N/A	
Grate Weir Coefficient (typical val		C_w (G) =	N/A	N/A	
Grate Orifice Coefficient (typical va	alue 0.60 - 0.80)	$C_o(G) =$	N/A	N/A	
Curb Opening Information		-	MINOR	MAJOR	<u></u>
Length of a Unit Curb Opening		$L_o(C) =$	15.00	15.00	feet
Height of Vertical Curb Opening in	Inches	$H_{vert} =$	6.00	6.00	inches
Height of Curb Orifice Throat in Ir	nches	$H_{throat} =$	6.00	6.00	inches
Angle of Throat (see USDCM Figur	re ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (ty	pically the gutter width of 2 feet)	$W_p =$	2.00	2.00	feet
Clogging Factor for a Single Curb	Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (ty	pical value 2.3-3.7)	$C_w(C) =$	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	C₀ (C) =	0.67	0.67	
Low Head Performance Reduct	cion (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth		d _{Grate} =	N/A	N/A	Tft.
Depth for Curb Opening Weir Equ	ation	d _{Curb} =	0.30	0.83	ft
Combination Inlet Performance Re		RF _{Combination} =	0.53	1.00	
Curb Opening Performance Reduc	5	RF _{Curb} =	0.76	1.00	1
Grated Inlet Performance Reduction	5	RF _{Grate} =	N/A	N/A	

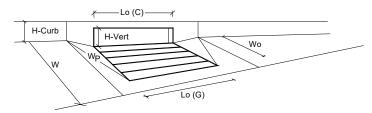
L	1 199	O _a = [MINOR 8.0	MAJOR 39.1	ີcfs
Total Inlet Interception Capacity (Q PEAK REQUIRED =	11.6	28.4	cfs
WARNING: Inlet Capacity less	than Q Peak for Minor Storm	✓ PEAK REQUIRED —	11.0	20.4	us

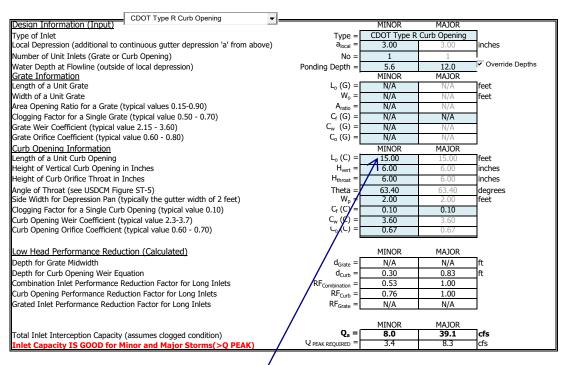
(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: MAYBERRY FILING 3
Inlet ID: D1.2 - DP6



Maximum Allowable Width for Spread Behind Curb
Side Slope Behind Curb (leave blank for no conveyance credit behind curb)
Manning's Roughness Behind Curb (typically between 0.012 and 0.020) T_{BACK} S_{BACK} = 0.020 ft/ft n_{BACK} = 0.013 Height of Curb at Gutter Flow Line H_{CURB} = 6.00 nches Distance from Curb Face to Street Crown T_{CROWN} 17.0 W = S_X = Gutter Width 2.00 0.020 Street Transverse Slope ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) ft/ft 0.083 Street Longitudinal Slope - Enter 0 for sump condition S_0 ft/ft 0.000 Manning's Roughness for Street Section (typically between 0.012 and 0.020) n_{STREET} : 0.013 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm Max. Allowable Depth at Gutter Flowline for Minor & Major Storm 17.0 inches 6.0 12.0 Check boxes are not applicable in SUMP conditions MINOR STORM Allowable Capacity is based on Depth Criterion MAJOR STORM Allowable Capacity is based on Depth Criterion Minor Storm SUMP Major Storm SUMP

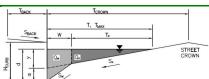




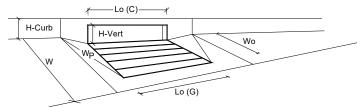
a 5' inlet is shown on the CD's and is drawn on the drainage plan. Revise.

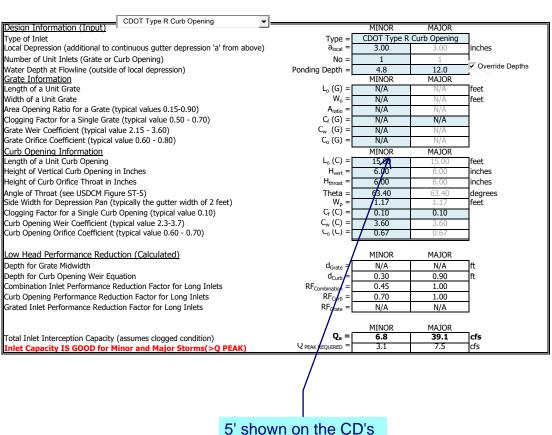
(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: MAYBERRY FILING 3
Inlet ID: D1.3 - DP8



Maximum Allowable Width for Spread Behind Curb
Side Slope Behind Curb (leave blank for no conveyance credit behind curb)
Manning's Roughness Behind Curb (typically between 0.012 and 0.020) T_{BACK} S_{BACK} = 0.020 ft/ft n_{BACK} = 0.013 Height of Curb at Gutter Flow Line H_{CURB} : 6.00 nches Distance from Curb Face to Street Crown T_{CROWN} 16.2 W = S_X = Gutter Width 1.17 Street Transverse Slope ft/ft 0.020 Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) ft/ft 0.083 Street Longitudinal Slope - Enter 0 for sump condition S_0 ft/ft 0.000 Manning's Roughness for Street Section (typically between 0.012 and 0.020) n_{STREET} : 0.013 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm Max. Allowable Depth at Gutter Flowline for Minor & Major Storm 16.2 inches 6.0 12.0 Check boxes are not applicable in SUMP conditions MINOR STORM Allowable Capacity is based on Depth Criterion MAJOR STORM Allowable Capacity is based on Depth Criterion Minor Storm SUMP Major Storm SUMP

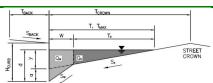


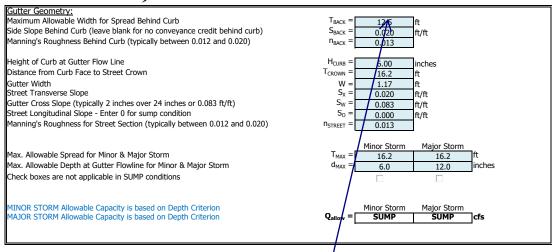


and drainage plan. Revise

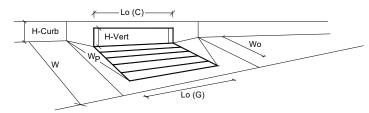
(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

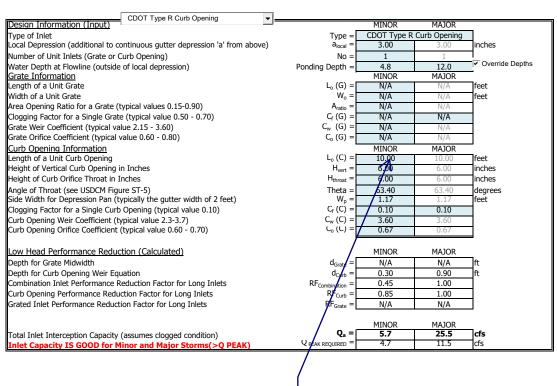
Project: MAYBERRY FILING 3
Inlet ID: D1.4





There is only approx. 7.5 ft. to the ROW. revise



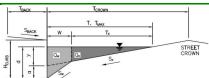


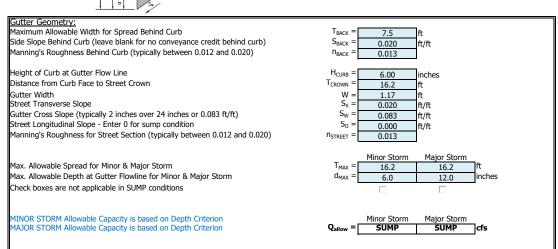
a 5' inlet is shown on the CD's. Revise the CD's accordingly so that they are consistent.

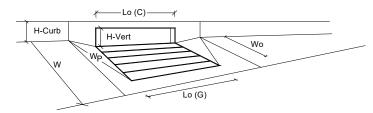
Verify that all storm inlets provided on the CD's match with the design calculations.

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: MAYBERRY FILING 3
Inlet ID: D1.6



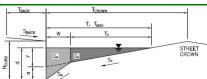


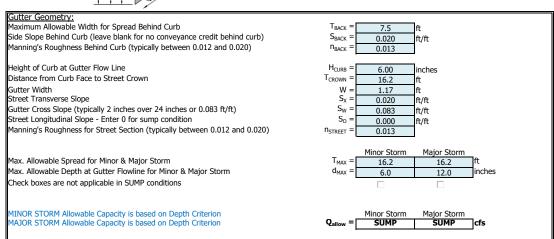


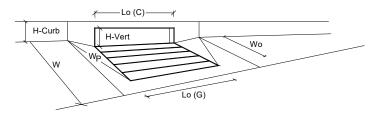
Design Information (Input)		MINOR	MAJOR	
Type of Inlet CDOT Type R Curb Opening	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	4.8	12.0	inches
Grate Information	_	MINOR	MAJOR	✓ Override Depths
Length of a Unit Grate	L ₀ (G) =	N/A	N/A	reet
Width of a Unit Grate	W _o =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_f(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C_w (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	$C_o(G) =$	N/A	N/A	
Curb Opening Information	=	MINOR	MAJOR	<u></u>
Length of a Unit Curb Opening	$L_o(C) =$	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	$H_{throat} =$	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	$W_p =$	1.17	1.17	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	C ₀ (C) =	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d _{Curb} =	0.30	0.90	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	0.61	1.00	1
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	1.00	1.00	1
Grated Inlet Performance Reduction Factor for Long Inlets	$RF_{Grate} =$	N/A	N/A	
		MINOR	MAJOR	
Total Inlet Interception Capacity (assumes cloqged condition)	Q _a =	3.8	12.3	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	2.6	6.3	cfs

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: MAYBERRY FILING 3
Inlet ID: D1.7



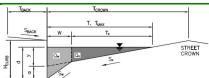




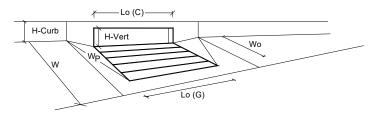
CDOT Type R Curb Opening				
Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	7
Water Depth at Flowline (outside of local depression)	Ponding Depth =	4.8	12.0	Override Depths
Grate Information	_	MINOR	MAJOR	_
Length of a Unit Grate	$L_o(G) =$	N/A	N/A	feet
Width of a Unit Grate	W _o =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_f(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	$C_w(G) =$	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	$C_o(G) =$	N/A	N/A	
Curb Opening Information	_	MINOR	MAJOR	_
Length of a Unit Curb Opening	$L_o(C) =$	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	$H_{throat} =$	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	$W_p =$	1.17	1.17	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	C₀ (C) =	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d _{Curb} =	0.30	0.90	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	0.61	1.00	†
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	1.00	1.00	
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A	
	Gate _	,		_
		MINOR	MAJOR	
Total Inlet Interception Capacity (assumes clogged condition)	Q _a =	3.8	12.3	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	2.1	5.0	cfs

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: MAYBERRY FILING 3
Inlet ID: D1.8



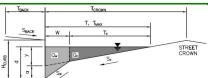
Gutter Geometry:
Maximum Allowable Width for Spread Behind Curb
Side Slope Behind Curb (leave blank for no conveyance credit behind curb)
Manning's Roughness Behind Curb (typically between 0.012 and 0.020) T_{BACK} S_{BACK} = 0.020 ft/ft n_{BACK} = 0.013 Height of Curb at Gutter Flow Line H_{CURB} : 6.00 nches Distance from Curb Face to Street Crown T_{CROWN} 16.2 W = S_X = Gutter Width 1.17 Street Transverse Slope ft/ft 0.020 Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) ft/ft 0.083 Street Longitudinal Slope - Enter 0 for sump condition S_0 ft/ft 0.000 Manning's Roughness for Street Section (typically between 0.012 and 0.020) n_{STREET} : 0.013 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm Max. Allowable Depth at Gutter Flowline for Minor & Major Storm 16.2 inches 6.0 12.0 Check boxes are not applicable in SUMP conditions MINOR STORM Allowable Capacity is based on Depth Criterion MAJOR STORM Allowable Capacity is based on Depth Criterion Minor Storm SUMP Major Storm SUMP



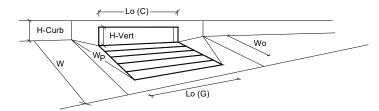
Design Information (Input)			MINOR	MAJOR	
Type of Inlet CDOT Type	R Curb Opening	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gut	ter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)		No =	1	1	
Water Depth at Flowline (outside of local depre	ession)	Ponding Depth =	4.8	12.0	inches
Grate Information			MINOR	MAJOR	✓ Override Depths
Length of a Unit Grate		$L_o(G) =$	N/A	N/A	reet
Width of a Unit Grate		$W_o =$	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values	•	A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grate (typical value	e 0.50 - 0.70)	$C_f(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60		C_w (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.	80)	$C_o(G) =$	N/A	N/A	
Curb Opening Information		-	MINOR	MAJOR	<u></u>
Length of a Unit Curb Opening		$L_o(C) =$	5.00	5.00	feet
Height of Vertical Curb Opening in Inches		$H_{vert} =$	6.00	6.00	inches
Height of Curb Orifice Throat in Inches		$H_{throat} =$	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)		Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gu	•	$W_p =$	1.17	1.17	feet
Clogging Factor for a Single Curb Opening (typ	ical value 0.10)	$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.		$C_w(C) =$	3.60	3.60	
Curb Opening Orifice Coefficient (typical value	0.60 - 0.70)	C ₀ (C) =	0.67	0.67	
Low Head Performance Reduction (Calcula	ted)		MINOR	MAJOR	
Depth for Grate Midwidth		d _{Grate} =	N/A	N/A	ft
Depth for Curb Opening Weir Equation		d _{Curb} =	0.30	0.90	ft
Combination Inlet Performance Reduction Fact	or for Long Inlets	RF _{Combination} =	0.61	1.00	T
Curb Opening Performance Reduction Factor fo	5	RF _{Curb} =	1.00	1.00	
Grated Inlet Performance Reduction Factor for	5	RF _{Grate} =	N/A	N/A	1
		_			
		0 -0	MINOR	MAJOR	٦.
Total Inlet Interception Capacity (assumes clos		Q _a =	3.8	12.3	cfs
Inlet Capacity IS GOOD for Minor and Ma	jor Storms(>Q PEAK)	Q PEAK REQUIRED =	1.8	4.4	cfs

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: MAYBERRY FILING 3
Inlet ID: D1.9



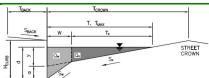
Maximum Allowable Width for Spread Behind Curb
Side Slope Behind Curb (leave blank for no conveyance credit behind curb)
Manning's Roughness Behind Curb (typically between 0.012 and 0.020) T_{BACK} S_{BACK} = 0.020 ft/ft n_{BACK} = 0.013 Height of Curb at Gutter Flow Line H_{CURB} : 6.00 nches Distance from Curb Face to Street Crown T_{CROWN} 16.2 W = S_X = Gutter Width 1.17 Street Transverse Slope ft/ft 0.020 Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) ft/ft 0.083 Street Longitudinal Slope - Enter 0 for sump condition S_0 ft/ft 0.000 Manning's Roughness for Street Section (typically between 0.012 and 0.020) n_{STREET} : 0.013 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm Max. Allowable Depth at Gutter Flowline for Minor & Major Storm 16.2 inches 6.0 12.0 Check boxes are not applicable in SUMP conditions MINOR STORM Allowable Capacity is based on Depth Criterion MAJOR STORM Allowable Capacity is based on Depth Criterion Minor Storm SUMP Major Storm SUMP



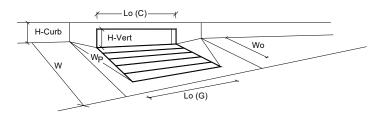
Design Information (Input)		MINOR	MAJOR	
Type of Inlet CDOT Type R Curb Opening	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	4.8	12.0	inches
Grate Information	_	MINOR	MAJOR	Override Depths
Length of a Unit Grate	$L_o(G) =$	N/A	N/A	feet
Width of a Unit Grate	W _o =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_f(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	$C_w(G) =$	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	$C_o(G) =$	N/A	N/A	
Curb Opening Information	-	MINOR	MAJOR	_
Length of a Unit Curb Opening	$L_o(C) =$	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	$H_{throat} =$	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	$W_p =$	1.17	1.17	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	C ₀ (C) =	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d _{Curb} =	0.30	0.90	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	0.61	1.00	
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	1.00	1.00	1
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A]
		MINOR	MAJOR	
Total Inlet Interception Capacity (assumes clogged condition)	Q _a = [3.8	12.3	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	0.9	2.1	cfs

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: MAYBERRY FILING 3
Inlet ID: D1.10



Maximum Allowable Width for Spread Behind Curb
Side Slope Behind Curb (leave blank for no conveyance credit behind curb)
Manning's Roughness Behind Curb (typically between 0.012 and 0.020) T_{BACK} S_{BACK} = 0.020 ft/ft n_{BACK} = 0.013 Height of Curb at Gutter Flow Line H_{CURB} : 6.00 nches Distance from Curb Face to Street Crown T_{CROWN} 28.0 W = S_X = Gutter Width 2.00 0.020 Street Transverse Slope ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) ft/ft 0.083 Street Longitudinal Slope - Enter 0 for sump condition S_0 ft/ft 0.000 Manning's Roughness for Street Section (typically between 0.012 and 0.020) n_{STREET} : 0.013 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm Max. Allowable Depth at Gutter Flowline for Minor & Major Storm 28.0 inches 6.0 12.0 Check boxes are not applicable in SUMP conditions MINOR STORM Allowable Capacity is based on Depth Criterion MAJOR STORM Allowable Capacity is based on Depth Criterion Minor Storm SUMP Major Storm SUMP



Design Information (Input)		MINOR	MAJOR	
Type of Inlet CDOT Type R Curb Opening	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	6.0	8.2	inches
Grate Information	·-	MINOR	MAJOR	Override Depths
Length of a Unit Grate	L ₀ (G) =	N/A	N/A	reet
Width of a Unit Grate	W _o =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_f(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C_w (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	$C_o(G) =$	N/A	N/A	
Curb Opening Information	=	MINOR	MAJOR	_
Length of a Unit Curb Opening	$L_o(C) =$	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H _{throat} =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	$W_p =$	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	C ₀ (C) =	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	T _{ft}
Depth for Curb Opening Weir Equation	d _{Curb} =	0.33	0.52	T _{ft}
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	0.77	1.00	
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	1.00	1.00	1
Grated Inlet Performance Reduction Factor for Long Inlets	$RF_{Grate} =$	N/A	N/A]
		MINOR	MAJOR	
Total Inlet Interception Capacity (assumes cloqged condition)	Q _a =	5.4	9.6	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	3.3	8.0	cfs

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: MAYBERRY FILING 3
Inlet ID: Mayberry Drive

TRACK
TCROWN

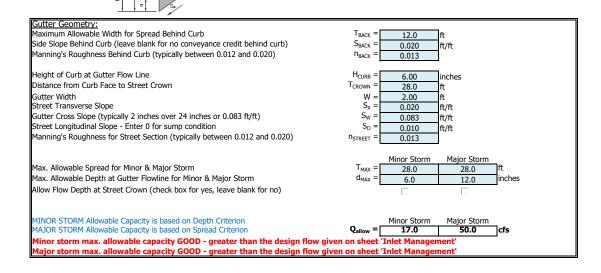
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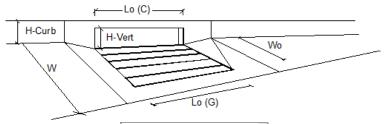
SPACE

SPACE

TO STREET
CROWN



INLET ON A CONTINUOUS GRADE MHFD-Inlet, Version 5.01 (April 2021)



	<u> </u>			
Design Information (Input)		MINOR	MAJOR	_
Type of Inlet	Type =			
Local Depression (additional to continuous gutter depression 'a')	$a_{LOCAL} =$			inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =			
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =			ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =			ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C_f - $G =$			
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C_f - $C =$			
		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =			cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	$Q_b =$			cfs
Capture Percentage = Q_a/Q_o =	C% =			%

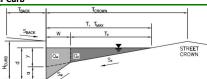
LOWEST LONGITUDINAL SLOPE OF THIS ROADWAY SECTION

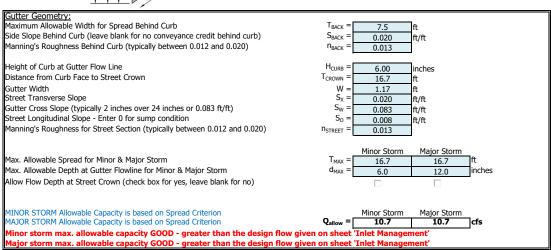
MHFD-Inlet, Version 5.01 (April 2021)

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: MAYBERRY FILING 3
Inlet ID: 50' ROW - 6" Rollover Curb





Please provide a capacity calculation for the roadway Galveston Terrace (60' ROW). This roadway is conveying the majority of the runoff from basin C2.3 to DP3 in Mayberry drive. Staff has concerns as to whether it has the capacity to convey these flows.

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Friday, Aug 26 2022

Channel C2 - 5 Year (DP21)

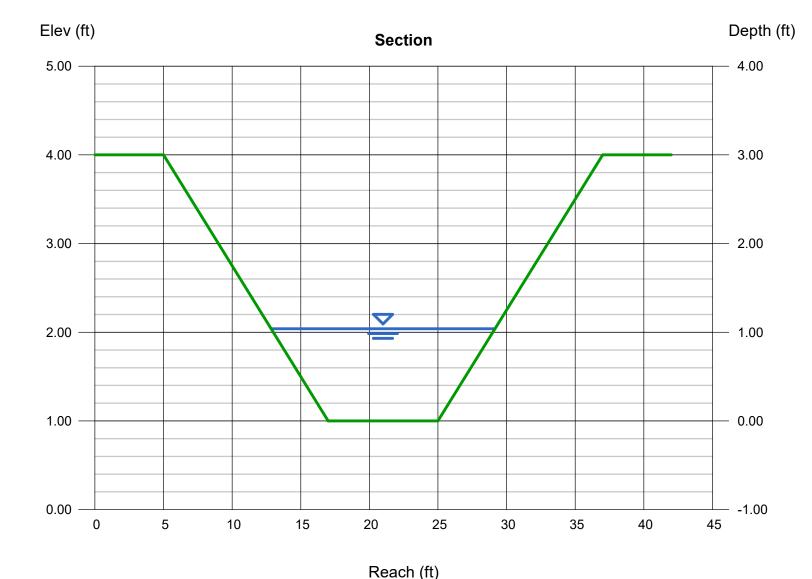
Trapezoidal

Bottom Width (ft) = 8.00 Side Slopes (z:1) = 4.00, 4.00 Total Depth (ft) = 3.00 Invert Elev (ft) = 1.00 Slope (%) = 0.50 N-Value = 0.030

Calculations

Compute by: Known Q Known Q (cfs) = 36.96 Highlighted

= 1.04 Depth (ft) Q (cfs) = 36.96Area (sqft) = 12.65Velocity (ft/s) = 2.92 Wetted Perim (ft) = 16.58 Crit Depth, Yc (ft) = 0.77Top Width (ft) = 16.32EGL (ft) = 1.17



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Friday, Aug 26 2022

Channel C2 - 100 Year (DP21)

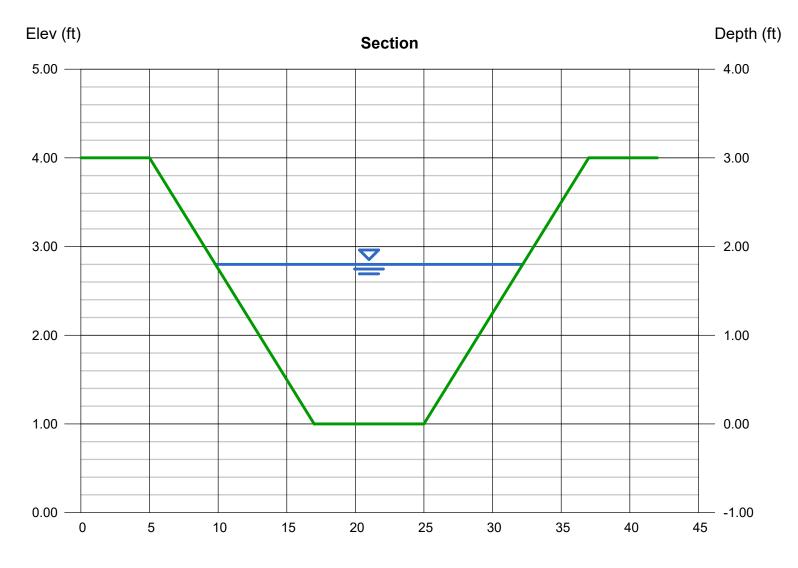
Trapezoidal

Bottom Width (ft) = 8.00 Side Slopes (z:1) = 4.00, 4.00 Total Depth (ft) = 3.00 Invert Elev (ft) = 1.00 Slope (%) = 0.50 N-Value = 0.030

Calculations

Compute by: Known Q Known Q (cfs) = 107.80 Highlighted

Depth (ft) = 1.80Q (cfs) = 107.80Area (sqft) = 27.36Velocity (ft/s) = 3.94Wetted Perim (ft) = 22.84Crit Depth, Yc (ft) = 1.41 Top Width (ft) = 22.40EGL (ft) = 2.04



Reach (ft)

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Friday, Aug 26 2022

Channel D - DP20 5 YEAR FLOW

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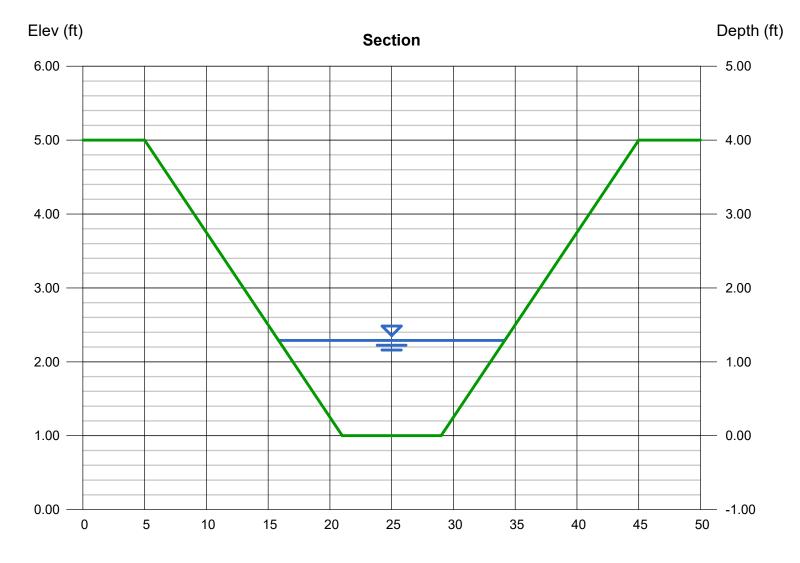
Bottom Width (ft) = 8.00
Side Slopes (z:1) = 4.00, 4.00
Total Depth (ft) = 4.00
Invert Elev (ft) = 1.00
Slope (%) = 0.40
N-Value = 0.030

Calculations

Compute by: Known Q Known Q (cfs) = 49.60

Highlighted

= 1.29Depth (ft) Q (cfs) = 49.60Area (sqft) = 16.98Velocity (ft/s) = 2.92Wetted Perim (ft) = 18.64 Crit Depth, Yc (ft) = 0.91Top Width (ft) = 18.32EGL (ft) = 1.42



Reach (ft)

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Friday, Aug 26 2022

Channel D - DP20 100 YEAR

Trapezoi	dal
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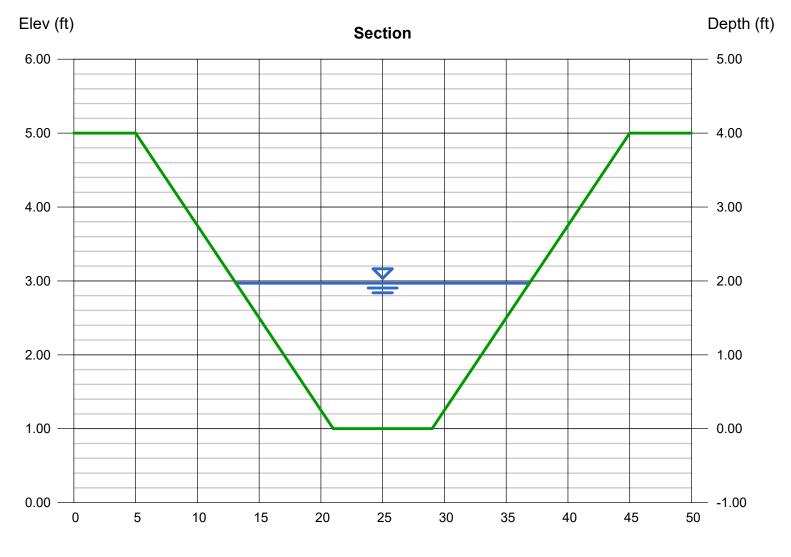
Bottom Width (ft) = 8.00
Side Slopes (z:1) = 4.00, 4.00
Total Depth (ft) = 4.00
Invert Elev (ft) = 1.00
Slope (%) = 0.40
N-Value = 0.030

Calculations

Compute by: Known Q Known Q (cfs) = 115.98

Highlighted

= 1.97Depth (ft) Q (cfs) = 115.98Area (sqft) = 31.28Velocity (ft/s) = 3.71Wetted Perim (ft) = 24.25Crit Depth, Yc (ft) = 1.46Top Width (ft) = 23.76EGL (ft) = 2.18



Reach (ft)

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Friday, Aug 26 2022

Channel E - DP24 100 Year

Trapezoida

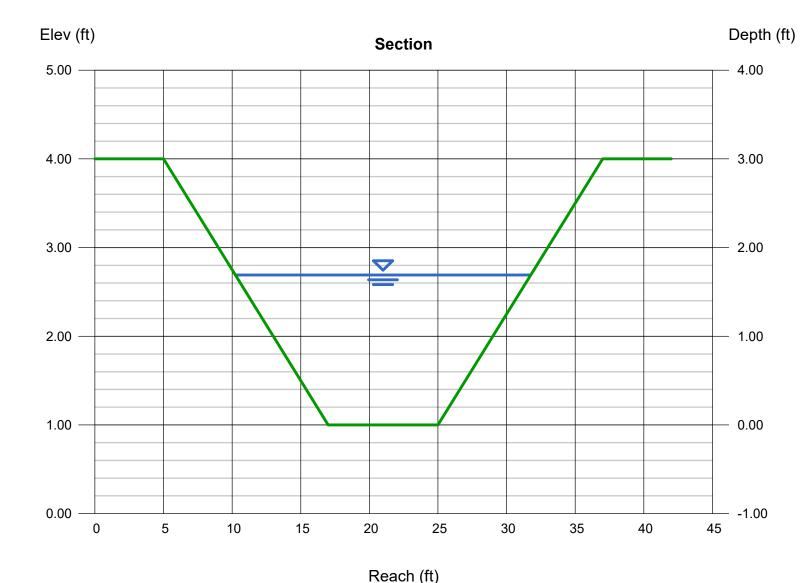
Bottom Width (ft) = 8.00 Side Slopes (z:1) = 4.00, 4.00 Total Depth (ft) = 3.00 Invert Elev (ft) = 1.00 Slope (%) = 0.70 N-Value = 0.030

Calculations

Compute by: Known Q Known Q (cfs) = 111.80

Highlighted

Depth (ft) = 1.69Q (cfs) = 111.80Area (sqft) = 24.94Velocity (ft/s) = 4.48 Wetted Perim (ft) = 21.94Crit Depth, Yc (ft) = 1.44 Top Width (ft) = 21.52 EGL (ft) = 2.00



Channel E - Superelevation Calculation						
С	0.5					
Velocity (V - fps)	4.5	*From Hydraflow Express				
Channel Width (W - ft)	21.5	*From Hydraflow Express				
g - constant (ft/sec^2)	32.2					
Channel /Bend Radius (ft)	50					
H - additional freeboard - (ft)	0.14					
Depth at 100 Year Flow (ft)	1.70	*From Hydraflow Express				
Channel Depth Provided (ft)	3					
Total Freeboard Provided (ft)	1.30	*min 1.14 feet required				

$$H = C \frac{v^2 W}{qR}$$
 (10-4)

where:

C = coefficient;

= 0.5, subcritical flow, simple curve

= 1.0, supercritical flow, simple curve

v = average velocity of flow in channel, in fps;

W = channel width at level water surface

g = acceleration of gravity constant, 32.2 ft/sec 2 ;

R = channel centerline radius of curvature, in ft; and

H = additional height of freeboard on outside edge of channel, in ft.

Channel Report

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Friday, Aug 26 2022

CHANNEL F - 100 YEAR FLOW

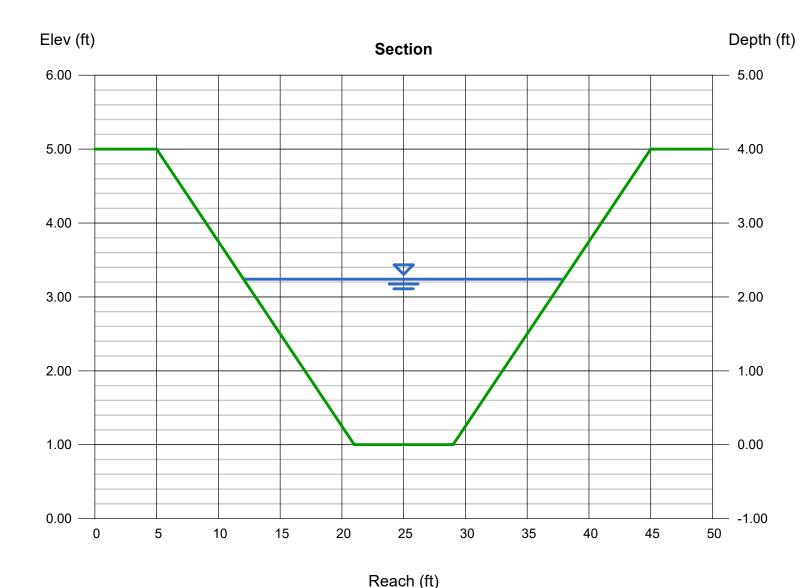
Trapezoidal

Bottom Width (ft) = 8.00 Side Slopes (z:1) = 4.00, 4.00 Total Depth (ft) = 4.00 Invert Elev (ft) = 1.00 Slope (%) = 0.40 N-Value = 0.030

Calculations

Compute by: Known Q Known Q (cfs) = 151.40 Highlighted

= 2.24Depth (ft) Q (cfs) = 151.40Area (sqft) = 37.99Velocity (ft/s) = 3.99Wetted Perim (ft) = 26.47Crit Depth, Yc (ft) = 1.69Top Width (ft) = 25.92EGL (ft) = 2.49



Per UDFCD Section 3.2.1 - Riprap Apron

Parameter	Unit	Value
Diameter of Conduit	ft	3
Design Discharge	ft ³ /s	40.1
Tailwater Depth	ft	1.7
Allowable Velocity	ft/s	5
Required Area of Flow	ft ²	8.02
Froude Parameter		2.57
Tailwater Depth/Conduit Diameter		0.57
Expansion Factor		6.6
Length of Protection	ft	12
Length of Protection *Length will extend until tie out to extends.		12
•		12 4.332314
*Length will extend until tie out to e	xisting grade	
*Length will extend until tie out to ex Expansion Angle	xisting grade degrees	4.332314
*Length will extend until tie out to e Expansion Angle Width of Protection	xisting grade degrees	4.332314
*Length will extend until tie out to e Expansion Angle Width of Protection RipRap Size (Figure 9-38)	xisting grade degrees	4.332314 5

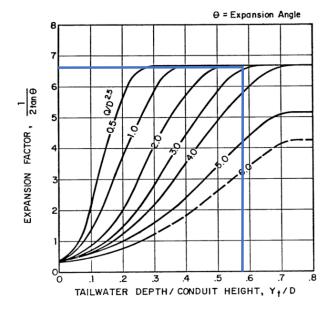
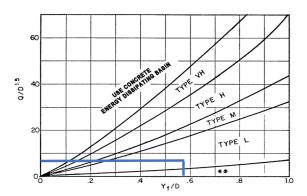


Figure 9-35. Expansion factor for circular conduits



Use $\,D_{d}$ instead of D whenever flow is supercritical in the barrel. **Use Type L for a distance of 3D downstream $\,.\,$

Figure 9-38. Riprap erosion protection at circular conduit outlet (valid for Q/D2.5 \leq 6.0)

Per UDFCD Section 3.2.1 - Riprap Apron

Parameter	Unit	Value
Diameter of Conduit	ft	3.75
Design Discharge	ft ³ /s	97.5
Tailwater Depth	ft	1.97
Allowable Velocity	ft/s	5
Required Area of Flow	ft ²	19.5
Froude Parameter		3.58
Tailwater Depth/Conduit Diameter		0.53
Expansion Factor		5.5
Longth of Protection	4	24
Length of Protection	ft	34
*Length will extend until tie out to e	xisting grade	
<u> </u>	• •	34 5.194429
*Length will extend until tie out to e	xisting grade	
*Length will extend until tie out to e Expansion Angle	xisting grade degrees	5.194429
*Length will extend until tie out to e Expansion Angle Width of Protection	xisting grade degrees	5.194429
*Length will extend until tie out to e Expansion Angle Width of Protection RipRap Size (Figure 9-38)	xisting grade degrees	5.194429 10

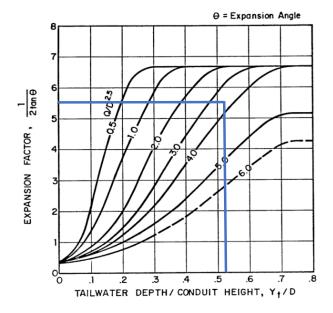
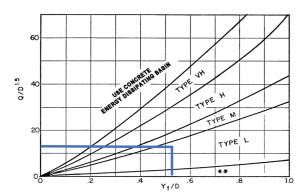


Figure 9-35. Expansion factor for circular conduits



Use D $_{\rm d}$ instead of D whenever flow is supercritical in the barrel. **Use Type L for a distance of 3D downstream .

Figure 9-38. Riprap erosion protection at circular conduit outlet (valid for Q/D2.5 \leq 6.0)

Per UDFCD Section 3.2.1 - Riprap Apron

Parameter	Unit	Value
Diameter of Conduit	ft	3
Design Discharge	ft ³ /s	39.6
Tailwater Depth	ft	2.24
Allowable Velocity	ft/s	5
Required Area of Flow	ft ²	7.92
Froude Parameter		2.54
Tailwater Depth/Conduit Diameter		0.75
Expansion Factor		6.8
Length of Protection	ft	4
Length of Protection	ft	4
*Length will extend until tie out to e	xisting grade	•
<u> </u>	• •	4 4.205357
*Length will extend until tie out to e	xisting grade	•
*Length will extend until tie out to e Expansion Angle	xisting grade degrees	4.205357
*Length will extend until tie out to e Expansion Angle Width of Protection	xisting grade degrees	4.205357 4 7.62
*Length will extend until tie out to e Expansion Angle Width of Protection RipRap Size (Figure 9-38)	xisting grade degrees	4.205357 4

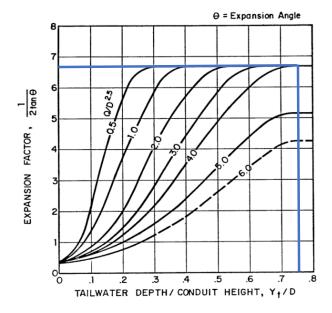
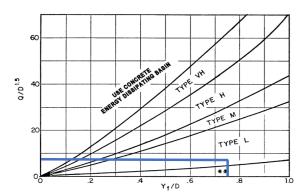
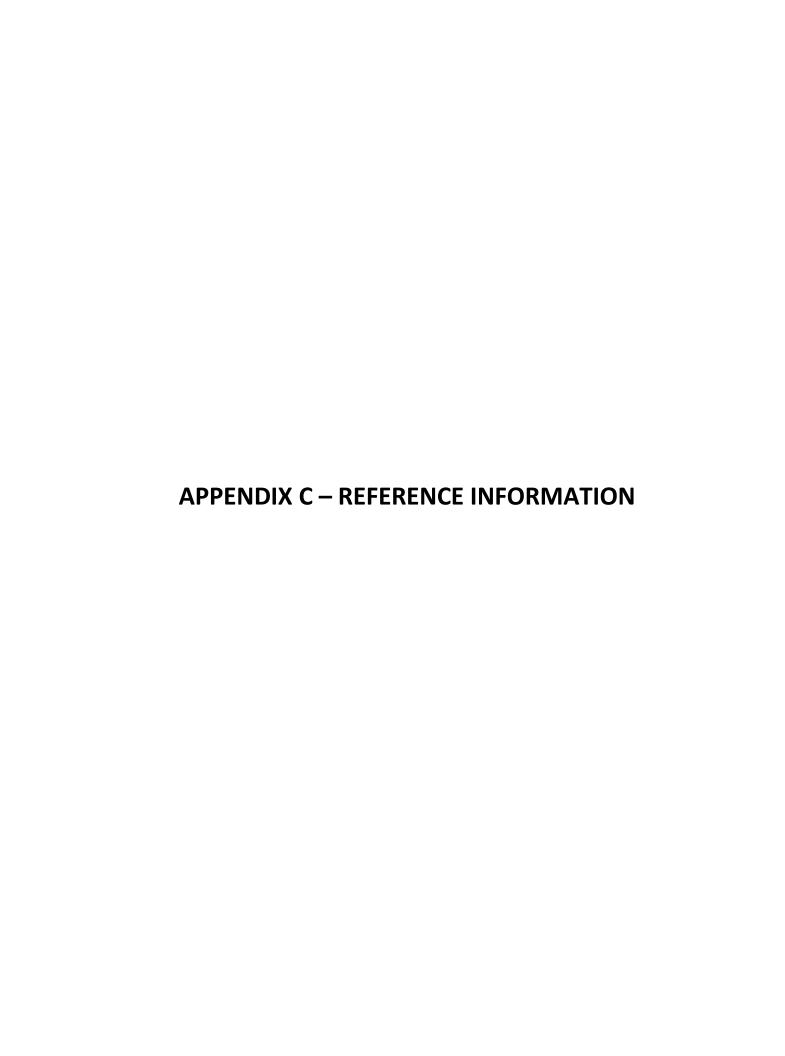


Figure 9-35. Expansion factor for circular conduits



Use $\,D_{d}$ instead of D whenever flow is supercritical in the barrel. **Use Type L for a distance of 3D downstream $\,.\,$

Figure 9-38. Riprap erosion protection at circular conduit outlet (valid for Q/D2.5 \leq 6.0)

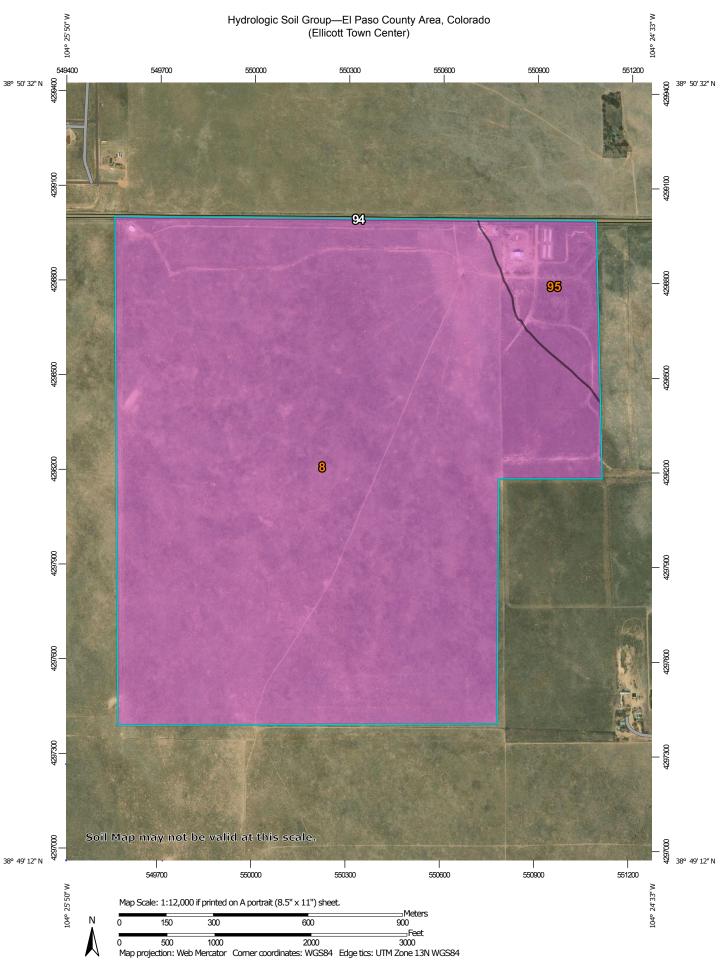




ENGINEER'S OPINION OF PROBABLE COSTS FOR

Mayberry Filing 3 - Drainage Improvements

Item	Description	Total Work Units	Unit Price	Total Cost
Riprap		10 CY	125.00 CY	1,250.00
18" RCP			\$	\$ 6,968.00
24" RCP		907 LF	\$ 81.00 LF	\$ 73,467.00
30" RCP		989 LF	\$ 100.00 LF	\$ 98,900.00
36" RCP		2,712 LF	\$ 124.00 LF	\$ 336,288.00
29"x45" RCP		927 LF	\$ 202.00 LF	\$ 187,254.00
5' Type R		6 EA	\$ 5,736.00 EA	\$ 34,416.00
10' Type R		6 EA	\$ 7,894.00 EA	\$ 47,364.00
15' Type R		4 EA	\$ 10,265.00 EA	\$ 41,060.00
Storm Manhole		15 EA	\$ 6,619.00 EA	\$ 99,285.00
36" FES		1 EA	\$ 744.00 EA	\$ 744.00
60" FES		2 EA	\$ 1,788.00 EA	\$ 3,576.00
Pond Forebay		2 EA	\$ 4,000.00 EA	\$ 8,000.00
Pond Outlet Structure		1 EA	\$ 8,000.00 EA	\$ 8,000.00
Grass Channels		3 AC	\$ 1,520.00 EA	\$ 4,560.00
SUBTOTAL		•		\$ 946,572.00
Contingency (15%)				\$ 141,985.80
TOTAL				\$ 1,088,557.80



is severely eroded and blowouts have developed, the new

Windbreaks and environmental plantings are generally suited to this soil. Soil blowing is the main limitation for the establishment of trees and shrubs. This limitation can be overcome by cultivating only in the tree rows and leaving a strip of vegetation between the rows. Supplemental irrigation may be necessary when planting and during dry periods. Trees that are best suited and have good survival are Rocky Mountain juniper eastern redcedar, bonderosa pine, Siberian elm, Russian-olive, and hackberry. Shrubs that are best suited are skunkbush sumac, lilac, and Siberian peashrub.

This soil is suited to wildlife habitat. It is best suited to habitat for openland and rangeland wildlife. In cropland areas, habitat favorable for ring-necked pheasant, mourning dove, and many nongame species can be developed by establishing areas for nesting and escape cover. For pheasant, the provision of undisturbed nesting cover is vital and should be included in plans for habitat development. Rangeland wildlife, such as pronghorn antelope, can be encouraged by developing livestock watering facilities, properly managing livestock grazing, and reseeding range where needed.

This soil has good potential for use as homesites. Shallow excavation is severely limited because cut banks cave in. This sandy soil requires special management practices to reduce water erosion and soil blowing. Capability subclasses IIIe, irrigated, and IVe, nonirrigated.

7—Bijou sandy loam, 3 to 8 percent slopes. This deep, well drained soil is on flood plains, terraces, and uplands. It formed in sandy alluvium and eolian material derived from arkose deposits. Elevation ranges from 5,400 to 6,200 feet. The average annual precipitation is about 13 inches, the average annual air temperature is about 49 degrees F, and the average frost-free period is about 145 days.

Typically, the surface layer is brown sandy loam about 4 inches thick. The subsoil is brown or grayish brown sandy loam about 24 inches thick. The substratum is pale brown loamy coarse sand.

Included with this soil in mapping are small areas of Olney sandy loam, 3 to 5 percent slopes; Walent sand, 1 to 9 percent slopes; Vona sandy loam, 3 to 9 percent slopes; and Wigton loamy sand, 1 to 8 percent slopes.

Permeability of this Bijou soil is rapid. Effective rooting depth is 60 inches or more. Available water capacity is moderate. Organic matter content of the surface layer is low. Surface runoff is slow, and the hazards of erosion and soil/blowing are moderate.

Almost all areas of this soil are used for range.

This soil is suited to the production of native vegetation suitable for grazing. Because of the hazards of water erosion and soil blowing, the soil is not suited to nonirrigated crops.

Native vegetation is dominantly blue grama, sand dropseed, needleandthread, side-oats grama, and buckwheat. Seeding is a suitable practice if the range has deteriorated. Seeding the native grasses is a good practice. If the tange is severely eroded and blowouts have developed, the new seeding should be fertilized Brush control and grazing management may be needed to improve the depleted range. Grazing should be managed so that enough forage is left standing to protect the soil from blowing, to increase infiltration of water, and to catch and hold snow.

Windbreaks and environmental plantings are generally suited to this soil. Soil blowing is the main limitation for the establishment of trees and shrubs. This limitation can be overcome by cultivating only in the tree rows and leaving a strip of vegetation between the rows. Supplemental irrigation may be needed when planting and during dry periods. Trees that are best suited and have good survival are Rocky Mountain Juniper, eastern redcedar, ponderosa pine, Siberian elm, Russian-olive, and hackberry. Shrubs that are best suited are skunkbush sumac, lilac, and Siberian peashrub.

This soil is suited to wildlife habitat. It is best suited to habitat for openland and rangeland wildlife. Rangeland wildlife, such as pronghorn antelope, can be encouraged by developing livestock watering facilities, by properly managing livestock grazing, and by reseeding range where needed.

This soil has good potential for use as homesites Shallow excavation is severely limited because cut banks cave in. This soil requires special management practices to reduce water erosion and soil blowing. Capability subclass VIe.

8—Blakeland loamy sand, 1 to 9 percent slopes. This deep, somewhat excessively drained soil formed in alluvial and eolian material derived from arkosic sedimentary rock on uplands. The average annual precipitation is about 15 inches, the average annual air temperature is about 47 degrees F, and the average frost-free period is about 135 days.

Typically, the surface layer is dark grayish brown loamy sand about 11 inches thick. The substratum, to a depth of 27 inches, is brown loamy sand; it grades to pale brown sand that extends to a depth of 60 inches.

Included with this soil in mapping are small areas of Bresser sandy loam, 0 to 3 percent slopes; Bresser sandy loam, 3 to 5 percent slopes; Truckton sandy loam, 0 to 3 percent slopes; Truckton sandy loam, 3 to 9 percent slopes; and Stapleton sandy loam, 3 to 8 percent slopes. In some areas, mainly north of Colorado Springs in the Cottonwood Creek area, arkosic beds of sandstone and shale are at a depth of 0 to 40 inches.

Permeability of this Blakeland soil is rapid. Effective rooting depth is 60 inches or more. Available water capacity is low to moderate. Organic matter content of the surface layer is medium. Surface runoff is slow, the hazard of erosion is moderate, and the hazard of soil blowing is severe.

Most areas of this soil are used for range, homesites, and wildlife habitat.

SOIL SURVEY

Native vegetation is dominantly western wheatgrass, side-oats grama, and needleandthread. This soil is best suited to deep-rooted grasses.

Proper range management is necessary to prevent excessive removal of plant cover from the soil. Interseeding improves the existing vegetation. Deferment of grazing in spring increases plant vigor and soil stability. Proper location of livestock watering facilities helps to control graz-

Windbreaks and environmental plantings are fairly well suited to this soil. Blowing sand and low available water capacity are the main limitations for the establishment of trees and shrubs. The soil is so loose that trees need to be planted in shallow furrows and plant cover needs to be maintained between the rows. Supplemental irrigation may be needed to insure survival. Trees that are best suited and have good survival are Rocky Mountain juniper, eastern redcedar, ponderosa pine, and Siberian elm. Shrubs that are best suited are skunkbush sumac, lilac, and Siberian peashrub.

This soil is suited to wildlife habitat. It is best suited to habitat for openland and rangeland wildlife. Rangeland wildlife, such as pronghorn antelope, can be encouraged by developing livestock watering facilities, properly managing livestock grazing, and reseeding range where

This soil has good potential for urban development. Soil blowing is a hazard if protective vegetation is removed. Special erosion control practices must be provided to

minimize soil losses. Capability subclass VIe.

9-Blakeland complex, 1 to 9 percent slopes. This complex is on uplands, mostly in the Falcon area, The average annual precipitation is about 15 inches, the average annual air temperature is about 47 degrees F, and the frost-free period is about 135 days.

This complex is about 60 percent Blakeland loamy sand, about 30 percent Fluvaquentic Haplaquolls, and 10 per-

cent other soils.

Included with these soils in mapping are areas of Columbine gravelly sandy loam, 0 to 3 percent slopes, Ellicott loamy coarse sand, 0 to 5 percent slopes, and Ustic Torrifluvents, loamy.

The Blakeland soil is in the more sloping areas. It is deep and somewhat excessively drained. It formed in sandy alluvium and eolian material derived from arkosic sedimentary rock. Typically, the surface layer is dark grayish brown loamy sand about 11 inches thick. The substratum, to a depth of 27 inches, is brown loamy sand; it grades to pale brown sand that extends to a depth of 60 inches or more.

Permeability of the Blakeland soil is rapid. The effective rooting depth is more than 60 inches. The available water capacity is moderate to low. Surface runoff is slow,

and the hazard of erosion is moderate.

The Flyvaquentic Haplaquolls are in swale areas. They are deep, poorly drained soils. They formed in alluvium derived from arkosic sedimentary rock. Typically, the surface layer is brown. The texture is variable throughout. The water table is at a depth of 0 to 3 feet.

The Blakeland soil is well suited to deep-rooted grasses. Native vegetation is dominantly western wheatgrass, side-oats grama, and needleandthread. Rangeland vegetation on the Fluvaquentic Haplaquolls is dominantly tall grasses, including sand bluestem, switchgrass, grairie corderass, little bluestem, and sand reedgrass. Cattails and bulrushes are common in the swampy areas.

Proper range management is needed to prevent excess removal of plant cover from these soils. It is also needed to maintain the productive grasses. Interseeding improves the existing vegetation. Deferment of grazing during the growing season increases plant vigor and soil stability, and it helps to maintain and improve range condition. Proper location of livestock watering facilities helps to

control grazing of animals.

Windbreaks and environmental plantings are fairly well suited to these soils. Blowing sand and low available water capacity are the main limitations to the establishment of trees and shrubs. The soils are so loose that trees need to be planted in shallow furrows and plant cover needs to be maintained between the rows. Supplemental irrigation may be needed to insure survival. Trees that are best suited and have good survival are Rocky Mountain juniper, eastern kedcedar, ponderosa pine, and Siberian elm. Shrubs that are best suited are skunkbush sumac, lilac, and Siberian peashrub.

The Blakeland soil is well suited to wildlife habitat. It is best suited to habitat for penland and rangeland wildlife. Rangeland wildlife, such as pronghorn antelope, can be encouraged by developing livestock watering facilities, properly managing livestock grazing, and reseeding range where needed. Wetland wildlife can be attracted to the Fluvaquentic Haplaquolls and the wetland habitat can be enhanced by several means. Shallow water developments can be created by digging or by blasting potholes to create open-water areas. Fencing to control livestock grazing is beneficial/and it allows wetland plants such as cattails, reed canarygrass, and rushes to grow. Control of unplanned burning and prevention of drainage that would remove water from the wetlands\are good practices. Openland wildlife use the vegetation on these soils for nesting and escape cover. These shallow marsh areas are especially important for winter cover if natural vegetation is allowed to grow.

The Blake and soil has good potential for homesites. roads, and streets. It needs to be protected from erosion when vegetation has been removed from building sites. The Fluvaquentic Haplaquolls have poor potential for homesites. Their main limitations for this use are the high water table and the hazard of flooding. Capability sub-

class VIe.

10-Blendon sandy loam, 0 to 3 percent slopes. This deep,/well drained soil formed in sandy arkosic alluvium on alluvial fans and terraces. The average \annua prefipitation is about 15 inches, the mean annual aly temperature is about 47 degrees F, and the average frostfree period is about 135 days.

Permeability of the Crowfoot soil is moderate. Effective rooting depth is 60 inches or more. Available water capacity is moderate. Surface runoff is medium, and the hazard of erosion is moderate. Some gullies are present in some drainageways and along stock trails.

The soils in this complex are used as rangeland, for

recreation and wildlife habitat, and as homesites.

Native vegetation is mainly mountain muhly, bluestem, mountain brome, needleandthread, and blue grama. These soils are subject to invasion by Kentucky bluegrass and Gambel oak. Noticeable forbs are hairy goldenrod, geranium, milkvetch, low larkspur, fringed sage, and buckwheat.

Proper location of livestock watering facilities helps to control grazing. Timely deferment of grazing is needed to

protect the plant cover.

Windbreaks and environmental plantings are fairly well suited to these soils. Blowing sand and moderate available water capacity are the main limitations for the establishment of trees and shrubs. The soils are so loose that trees need to be planted in shallow furrows and plant cover needs to be maintained between the rows. Supplemental irrigation may be needed to insure survival. Trees that are best suited and have good survival are Rocky Mountain juniper, eastern redcedar, ponderosa pine, and Siberian elm. Shrubs that are best suited are skunkbush sumac, lilac, and Siberian peashrub.

These soils are best suited to habitat for openland wildlife species, such as pronghorn antelope and sharp-tailed grouse. Although sharp-tailed grouse are not plentiful, they could be encouraged on these soils, especially where brush species are interspersed with grasses and forbs. If these soils are used as rangeland, wildlife production can be increased by managing livestock grazing to preclude overuse of the more desirable grass species and depletion

of the various brush species.

The main limitations for urban uses are frost-action potential and slope on the Crowfoot soil and slope on the Tomah soil. Buildings and roads must be designed to overcome these limitations. Access roads must have adequate cut-slope grade and be provided with drains to control surface runoff. Maintaining the existing vegetation on building sites during construction helps to control erosion. Capability subclass VIe.

94—Travessilla-Rock outcrop complex, 8 to 90 percent slopes. This moderately sloping to extremely steep complex is mostly on rocky uplands (fig. 5). Elevation ranges from 6,200 to 6,700 feet. The average annual precipitation is about 15 inches, the average annual air temperature is about 47 degrees F, and the average frost-

free period is about 140 days.

The Travessilla soil makes up about 45 percent of the complex Rock outcrop about 30 percent, and included

areas about 25 percent.

Included with this complex in mapping are areas of Bresser sandy loam, 5 to 9 percent slopes, Elbeth sandy loam, 8 to 15 percent slopes, Kettle gravelly loamy sand, 8 to 40 percent slopes, and Louviers silty clay loam, 3 to 18 percent slopes. The Elbeth and Kettle soils commonly are of the north-facing slopes.

The Travessilla soil is shallow and well drained. It formed in residuum derived from sandstone. Typically, the surface layer is light brownish gray sandy loam about 3 inches thick. The underlying material is pale brown sandy loam about 8 inches thick. Hard arkosic sandstone that has some fractures is at a depth of about 11 inches.

Permeability of the Travessilla soil is moderately rapid. Effective rooting depth is 6 to 20 inches. Available water capacity is low. Surface runoff is medium to rapid, and the hazard of erosion is high. Gullies are common along

drainageways and trails.

Rock outcrop occurs mostly as ledges on cliffs.

This complex is used for urban development, as

homesites, and for recreation and wildlife habitat.

This complex is suited to the production of ponderosa pine. The main limitations are the presence of stones and rock outcrop on the surface and a high hazard of erosion. Stones on the surface can hinder felling, yarding, and other operations involving the use of equipment. Practices must be used to minimize soil erosion when harvesting timber. The low available water capacity can influence seedling survival.

Wildlife on these soils is limited mostly to small animals such as cottontail, squirrel, and birds because of the extent of urban development. Ponderosa pine, mountainmahogany, Gambel oak, and various grasses provide food,

cover, and nesting areas.

This complex is extensively used for urban development and as homesites (fig. 6). The main limitations for these uses are depth to bedrock, rock outcrop, and steep slopes. Septic tank absorption fields do not function properly because of the depth to bedrock. Special designs for buildings and roads and streets are needed to overcome the limitations. Plans for homesite development should provide for the preservation of as many trees as possible because of their esthetic value. Capability subclass VIIe.

95—Truckton loamy sand, 1 to 9 percent slopes. This deep, well drained soil formed in alluvium and residuum derived from arkosic sedimentary rock on uplands. Elevation ranges from 6,000 to 7,000 feet. The average annual precipitation is about 15 inches, the average annual air temperature is about 47 degrees F, and the average frost-free period is about 135 days.

Typically, the surface layer is grayish brown loamy sand about 8 inches thick. The subsoil is brown sandy loam about 18 inches thick. The substratum is light yellowish brown coarse sandy loam to a depth of 60 inches or more.

Included with this soil in mapping are small areas of Blakeland loamy sand, 1 to 9 percent slopes; Bresser sandy loam, 3 to 5 percent slopes; Bresser sandy loam, 5 to 9 percent slopes; Truckton sandy loam, 0 to 3 percent slopes; and Truckton sandy loam, 3 to 9 percent slopes.

Permeability of this Truckton soil is moderately rapid. Effective rooting depth is 60 inches or more. Available water capacity is moderate. Surface runoff is slow, and the hazard of erosion is moderate to high.

SOIL SURVEY

Almost all areas of this soil are used as rangeland. A few areas of crops such as alfalfa and corn are grown

under sprinkler irrigation.

This soil is well suited to the production of native vegetation suitable for grazing. It is best suited to deeprooted grasses. The native vegetation is mainly cool- and warm-season grasses such as western wheatgrass, sideoats grama, and needleandthread.

Proper range management is needed to prevent excessive removal of the plant cover. Interseeding is used to improve the existing vegetation. Deferment of grazing in spring increases plant vigor and soil stability. Properly locating livestock watering facilities helps to control graz-

ing.

Windbreaks and environmental plantings are fairly well suited to this soil. Blowing sand is the main limitation for the establishment of trees and shrubs. The soil is so loose that trees need to be planted in shallow furrows and plant cover needs to be maintained between the rows. Supplemental irrigation may be needed to insure survival. Trees that are best suited and have good survival are Rocky Mountain juniper, eastern redcedar, ponderosa pine, and Siberian elm. Shrubs that are best suited are skunkbush sumac, lilac, and Siberian peashrub.

This soil is suited to wildlife habitat. It is best suited to openland and rangeland wildlife habitat. Rangeland wildlife, such as pronghorn antelope, can be encouraged by developing livestock watering facilities, properly managing livestock grazing, and reseeding range where needed. This soil has good potential for use as homesites. The main limitation of this soil for roads and streets is frost action potential. Special designs for roads are needed to minimize this limitation. Practices are needed to control soil blowing and water erosion on construction sites where the plant cover has been removed. Capability sub-

class VIe, nonirrigated.

96—Truckton sandy loam, 0 to 3 percent slopes. This deep, well drained soil formed in alluvium and residuum derived from arkosic sedimentary rock on uplands. Elevation ranges from 6,000 to 7,000 feet. The average annual precipitation is about 15 inches, the average annual air temperatue is about 47 degrees F, and the average frost-free period is about 135 days.

Typically, the surface layer is grayish brown sandy loam about 5 inches thick. The next layer is dark grayish brown sandy loam about 3 inches thick. The subsoil is brown sandy loam about 16 inches thick. The substratum is light yellowish brown coarse sandy loam to a depth of

60 inches or more.

Included with this soil in mapping are small areas of Blakeland loamy sand, 1 to 9 percent slopes; Bresser sandy loam, 0 to 8 percent slopes; Ellicott loamy coarse sand, 0 to 5 percent slopes; and Ustic Torrifluvents, loamy.

Permeability of this Truckton soil is moderately rapid. Effective rooting depth is 60 inches or more. Available water capacity is moderate. Surface runoff is slow, and the lazards of erosion and soil blowing are moderate.

This soil is used mainly for cultivated crops. It is also used for livestock grazing, for wildlife habitat, and as homesites.

crops are commonly grown in combination with summer fallow because moisture is insufficient for annual cropping. Alfalfa can also be grown on this soil. When this soil is used as cropland, crop residue management and minimum tillage are necessary conservation practices.

This soil is well suited to the production of native vegetation suitable for grazing (fig. 7). It favors deeprooted grasses. The native vegetation is mainly cool- and warm-season grasses such as western wheatgrass, side-

oats grama and needleandthread.

Proper range management is needed to prevent excessive removal of the plant cover. Interseeding is used to improve the existing vegetation. Deferment of grazing in spring increases plant vigor and soil stability. Properly locating livestock watering facilities helps to control grazing.

Windbreaks and environmental plantings generally are suited to this soil. Soil blowing is the main limitation to the establishment of trees and shrubs. This limitation can be overcome by cultivating only in the tree rows and leaving a strip of vegetation between the rows. Supplemental irrigation may be needed when planting and during dry periods. Trees that are best suited and have good survival are Rocky Mountain juniper, eastern redcedar, ponderosa pine, Siberian elm, Russian-olive, and hackberry. Shrubs that are best suited are skunkbush sumac, lilac, and Siberian peashrub.

This soil is suited to wildlife habitat. It is best suited to habitat for openland and rangeland wildlife. In cropland areas, habitat favorable for ring-necked pheasant, mourning dove, and many nongame species can be developed by establishing areas for nesting and escape cover. For pheasant, undisturbed resting cover is vital and should be provided in plans for habitat development. This is especially true in areas of intensive farming. Rangeland wildlife, such as pronghorn antelope, can be encouraged by developing livestock watering facilities, properly managing livestock grazing, and reseeding range where needed.

This soil has good potential for use as homesites. The main limitation of this soil for roads and streets is frost-action potential. Special designs for roads are needed to overcome this limitation. Capability subclasses IIIe, nonir-

rigated, and I/e, irrigated.

97—Truckton sandy loam, 3 to 9 percent slopes. This deep, well drained soil formed in alluvium and residuum derived from arkosic sedimentary rock on uplands. Elevation ranges from 6,000 to 7,000 feet. The average annual precipitation is about 15 inches, the average annual air temperature is about 47 degrees F, and the average frost-free period is about 135 days.

Typically, the surface layer is grayish brown sandy loam about 5 inches thick. The next layer is dark grayish brown sandy loam about 3 inches thick. The subsoil is brown sandy loam about 16 inches thick. The substratum is light yellowish brown coarse sandy loam to a depth of

60 inches or more.

EL PASO COUNTY AREA, COLORADO

TABLE 16. -- SOIL AND WATER FEATURES

[Absence of an entry indicates the feature is not a concern. See "flooding" in Glossary for definition of terms as "rare," "brief," and "very brief." The symbol > means greater than]

	l III.	Flooding			j Be	- Potentici	
Soil name and map symbol	Hydro- logic group	Frequency	Duration	Months	Depth	Hardness	Potential frost action
lamosa:	С	Frequent	Brief	May-Jun	<u>In</u> >60		High.
scalon: 2, 3	В	None			>60		 Moderate:
Badland: 4	D						
Bijou: 5, 6, 7	В	None			>60		Low.
Blakeland: 8	A	None			>60		Low.
19: Blakeland part-	Α	None			>60		Low.
Fluvaquentic Haplaquolls part	D	Common	Very brief	Mar-Aug	>60		High.
lendon: 10	В	None	·		>60		Moderate.
resser: 11, 12, 13	В	None			>60		Low.
russett: 14, 15	В	None			>60		Moderate.
haseville: 16, 17	A	None			>60		Low.
118: Chaseville part	A	None			>60		Low.
Midway part	D	None			10-20	Rippable	Moderate.
olumbine:	A	None to rare			>60		Low.
onnerton: 120: Connerton part-	В	 None			>60		High.
Rock outerop	D						
ruckton:	В	None			>60		Moderate.
ushman: 22, 23	С	None			20-40	Rippable	Moderate.
124: Cushman part	С	None			20-40	Rippable	Moderate.
Kutch part	С	None			20-40	Rippable	Moderate.
lbeth: 25, 26	В	None			>60		 Moderate.
127: Elbeth part	В	 None			>60		 Moderate.

See footnote at end of table.

EL PASO COUNTY AREA, COLORADO

TABLE 16. -- SOIL AND WATER FEATURES -- Continued

		1	Flooding	i Bed	1		
Soil name and map symbol	Hydro- logic group	Frequency	Duration	Months	 Depth 	Hardness	Potential frost action
		i			<u>In</u>		
Tomah: 192, 193: Tomah part	В	None			>60		 Moderate.
Crowfoot part	В	None			>60		Moderate.
Travessilla:					1		
Travessilla part	D	 None			6-20	Hard	Low.
Rock outerop part	D						
Truckton: 95, 96, 97-	B	None			>60		Moderate.
198: Truckton part	В	None			>60		Moderate.
Blakeland part-	A	None			>60		Low.
199, 1100: Truckton part	В	None			>60		Moderate.
Bresser part	В	None		na n ere zelo	>60		Low.
Ustic Torrifluvents: 101	В	Occasional	Very brief	Mar-Aug	>60		Moderate.
Valent: 102, 103	A	None			>60		Low.
Vona: 104, 105	В	None		I	>60		Moderate.
Wigton: 106	A	None			>60		Low.
Wiley: 107, 108	В	None		1	>60		Low.
Yoder: 109, 110	В	None			>60		Low.

 $1_{
m This}$ map unit is made up of two or more dominant kinds of soil. See map unit description for the composition and behavior characteristics of the map unit.

NOTES TO USERS

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Boundaries of the **floodways** were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations with regard to requirements of the National Flood Insurance Program. Floodway widths and other pertinent floodway data are provided in the Flood Insurance Study report for this jurisdiction.

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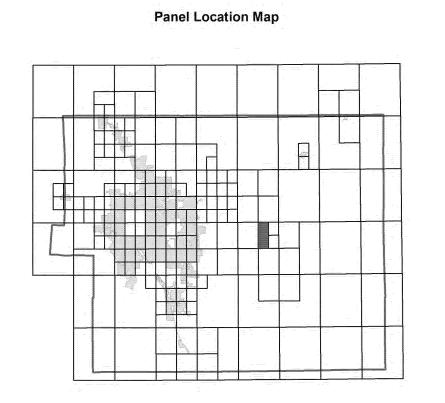
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El Paso County Vertical Datum Offset Table

Vertical Datum

Flooding Source Vertical Datur
Offset (f

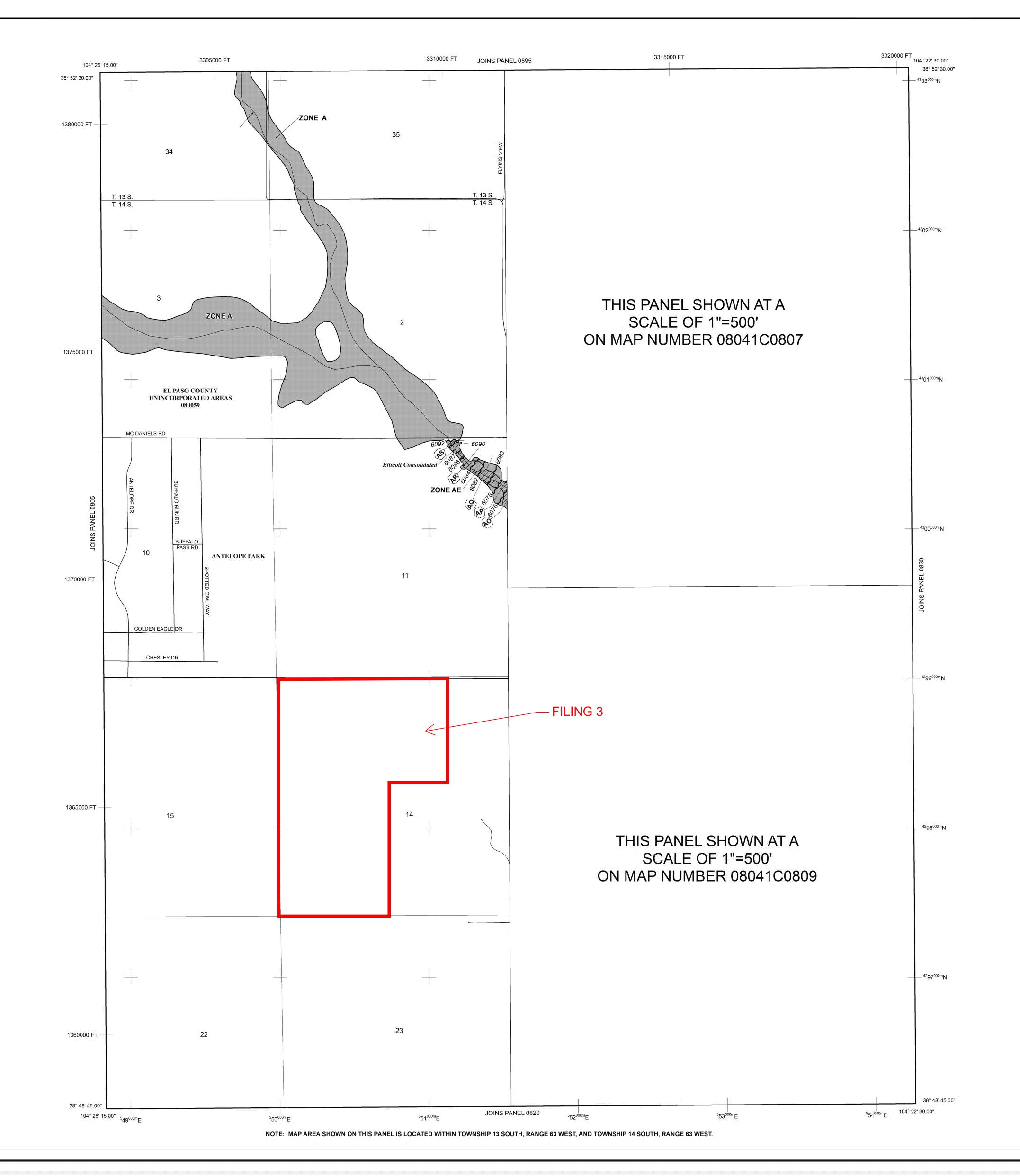
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LEGEND

SPECIAL FLOOD HAZARD AREAS (SFHAS) SUBJECT TO INUNDATION BY THE 1% ANNUAL CHANCE FLOOD

The 1% annual chance flood (100-year flood), also known as the base flood, is the flood that has a 1% chance of being equaled or exceeded in any given year. The Special Flood Hazard Area is the area subject to flooding by the 1% annual chance flood. Areas of Special Flood Hazard include Zones A, AE, AH, AO, AR, A99, V, and VE. The Base Flood Elevation is the water-surface elevation of the 1% annual chance flood.

ZONE A No Base Flood Elevations determined.

ZONE AE
Base Flood Elevations determined.

Flood depths of 1 to 3 feet (usually areas of ponding); Base Flood Elevations determined.

ZONE AO

Flood depths of 1 to 3 feet (usually sheet flow on sloping terrain); average depths determined. For areas of alluvial fan flooding, velocities also determined.

protection from the 1% annual chance or greater flood.

ZONE AR Special Flood Hazard Area Formerly protected from the 1% annual chance flood by a flood control system that was subsequently decertified. Zone AR indicates that the former flood control system is being restored to provide

Area to be protected from 1% annual chance flood by a Federal flood protection system under construction; no Base Flood Elevations determined.

ZONE V Coastal flood zone with velocity hazard (wave action); no Base Flood Elevations determined.

ZONE VE Coastal flood zone with velocity hazard (wave action); Base Flood Elevations determined.

FLOODWAY AREAS IN ZONE AE

The floodway is the channel of a stream plus any adjacent floodplain areas that must be kept free of encroachment so that the 1% annual chance flood can be carried without substantial increases in flood heights.

OTHER FLOOD AREAS

Areas of 0.2% annual chance flood; areas of 1% annual chance flood with average depths of less than 1 foot or with drainage areas less than 1 square mile; and areas protected by levees from 1% annual chance flood.

OTHER AREAS

Areas determined to be outside the 0.2% annual chance floodplain.

D Areas in which flood hazards are undetermined, but possible.

COASTAL BARRIER RESOURCES SYSTEM (CBRS) AREAS

OTHERWISE PROTECTED AREAS (OPAs)

CBRS areas and OPAs are normally located within or adjacent to Special Flood Hazard Areas.

Floodplain boundary

Floodway boundary

Zone D Boundary

CBRS and OPA boundary

Boundary dividing Special Flood Hazard Areas of different Base

Flood Elevations, flood depths or flood velocities.

513 Sase Flood Elevation line and value; elevation in feet*

(EL 987) Base Flood Elevation value where uniform within zone; elevation in feet*

* Referenced to the North American Vertical Datum of 1988 (NAVD 88)

A Cross section line

-----Transect line

97° 07' 30.00" Geographic coordinates referenced to the North American Datum of 1983 (NAD 83)

4275^{000m}N 1000-meter Universal Transverse Mercator grid ticks, zone 13
6000000 FT 5000-foot grid ticks: Colorado State Plane coordinate

DX5510 Bench mark (see explanation in Notes to Users section of this FIRM panel)

system, central zone (FIPSZONE 0502),

River Mile

MAP REPOSITORIES
Refer to Map Repositories list on Map Index
EFFECTIVE DATE OF COUNTYWIDE

FLOOD INSURANCE RATE MAP

EFFECTIVE DATE(S) OF REVISION(S) TO THIS PANEL

DECEMBER 7, 2018 - to update corporate limits, to change Base Flood Elevations and

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MAP SCALE 1" = 1000'

500 0 1000 2000

HHH FEET

PANEL 0810G

FIRM

FLOOD INSURANCE RATE MAP
EL PASO COUNTY,
COLORADO

AND INCORPORATED AREAS

NEL 040 0E 400

PANEL 810 OF 1300
(SEE MAP INDEX FOR FIRM PANEL LAYOUT)

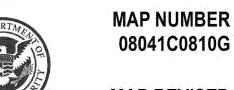
CONTAINS:

NINS:

UNITY NUMBER PANEL SUFFIX

COUNTY 080059 0810 G

Notice to User: The **Map Number** shown below should be used when placing map orders: the **Community Number** shown above should be used on insurance applications for the subject



MAP REVISED DECEMBER 7, 2018

DECEMBER 7, 2018
Federal Emergency Management Agency

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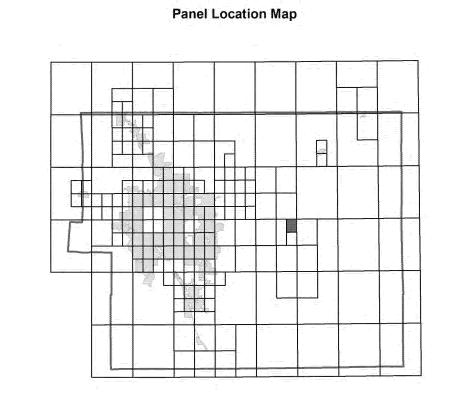
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El Paso County Vertical Datum Offset Table

Vertical Datum

Flooding Source Vertical Date
Offset

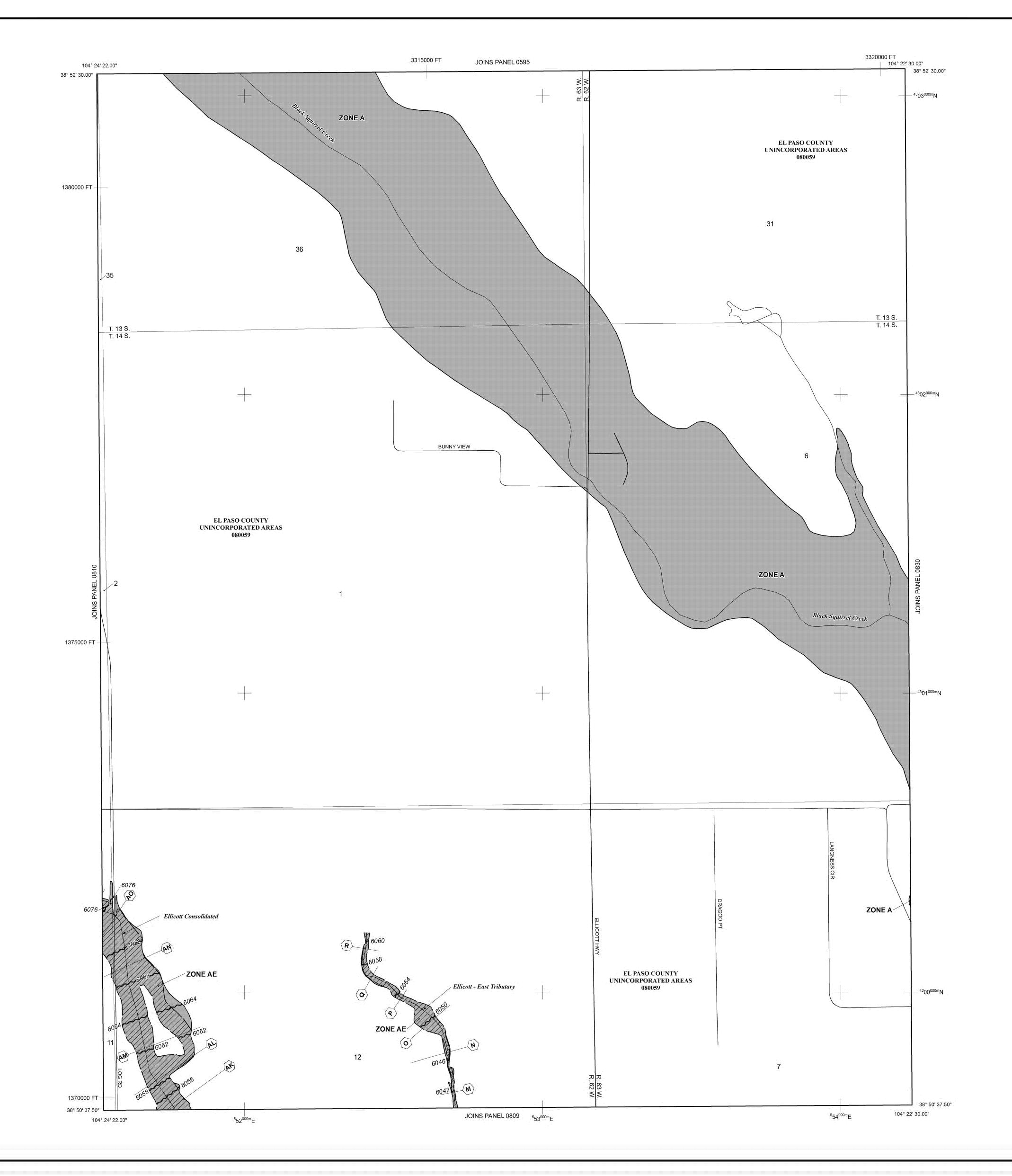
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ZONE AH Flood depths of 1 to 3 feet (usually areas of ponding); Base Flood Elevations determined.

protection from the 1% annual chance or greater flood.

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system, central zone (FIPSZONE 0502),
Lambert Conformal Conic Projection

X5510

Bench mark (see explanation in Notes to Users section of this FIRM panel)

River Mile

MAP REPOSITORIES Refer to Map Repositories list on Map Index

EFFECTIVE DATE OF COUNTYWIDE

FLOOD INSURANCE RATE MAP

MARCH 17, 1997

EFFECTIVE DATE(S) OF REVISION(S) TO THIS PANEL

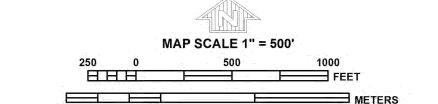
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PANEL 0807G

FIRM
FLOOD INSURANCE RATE MAP

EL PASO COUNTY, COLORADO AND INCORPORATED AREAS

PANEL 807 OF 1300

(SEE MAP INDEX FOR FIRM PANEL LAYOUT)

<u>CONTAINS:</u>

CONTAINS:

COMMUNITY

EL BASO COUNTY

 IITY
 NUMBER
 PANEL
 SUFFIX

 JNTY
 080059
 0807
 G

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MAP REVISED

MAP NUMBER 08041C0807G

DECEMBER 7, 2018
Federal Emergency Management Agency

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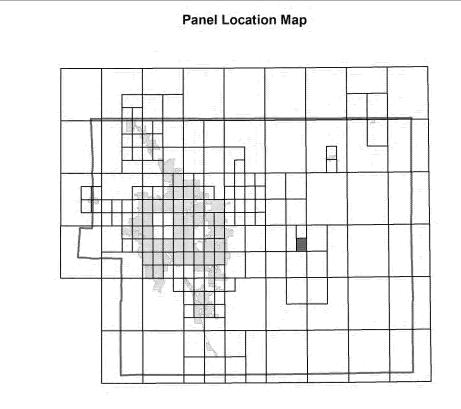
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> El Paso County Vertical Datum Offset Table Vertical Datum Flooding Source

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ZONE V Coastal flood zone with velocity hazard (wave action); no Base Flood Elevations determined. **ZONE VE** Coastal flood zone with velocity hazard (wave action); Base Flood

Elevations determined. FLOODWAY AREAS IN ZONE AE

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..........

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Flood Elevations, flood depths or flood velocities. ~~ 513 ~~ Base Flood Elevation line and value; elevation in feet* Base Flood Elevation value where uniform within zone;

elevation in feet* * Referenced to the North American Vertical Datum of 1988 (NAVD 88)

Cross section line

97° 07' 30 00" Geographic coordinates referenced to the North American 32° 22' 30.00" Datum of 1983 (NAD 83)

1000-meter Universal Transverse Mercator grid ticks,

5000-foot grid ticks: Colorado State Plane coordinate 6000000 FT system, central zone (FIPSZONE 0502),

Bench mark (see explanation in Notes to Users section of this FIRM panel)

MAP REPOSITORIES Refer to Map Repositories list on Map Index EFFECTIVE DATE OF COUNTYWIDE

EFFECTIVE DATE(S) OF REVISION(S) TO THIS PANEL DECEMBER 7, 2018 - to update corporate limits, to change Base Flood Elevations and Special Flood Hazard Areas, to update map format, to add roads and road names, and to incorporate previously issued Letters of Map Revision.

FLOOD INSURANCE RATE MAP

For community map revision history prior to countywide mapping, refer to the Community

Map History Table located in the Flood Insurance Study report for this jurisdiction. To determine if flood insurance is available in this community, contact your insurance

agent or call the National Flood Insurance Program at 1-800-638-6620.

PANEL 0809G

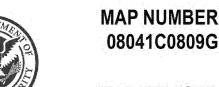
FIRM FLOOD INSURANCE RATE MAP EL PASO COUNTY, COLORADO AND INCORPORATED AREAS

PANEL 809 OF 1300

(SEE MAP INDEX FOR FIRM PANEL LAYOUT) CONTAINS: NUMBER PANEL SUFFIX

080059

Notice to User. The Map Number shown below should be used when placing map orders: the Community Number shown above should be used on insurance applications for the subject



MAP REVISED **DECEMBER 7, 2018**

Federal Emergency Management Agency

