



## Schmidt Parcel – District Infrastructure

FINAL DRAINAGE REPORT PCD File No. CDR2413

ALL TERRAIN ENGINEERING PROJECT NO: 24013

December 2024

**PREPARED FOR:** 

Turkey Canon Quarry Inc

Contact: James Morley

20 Boulder Crescent Street, Suite 200

Colorado Springs, CO 80903

**PREPARED BY:** 

ALL TERRAIN ENGINEERING LLC CONTACT: NICHOLAS Q. JOKERST NJOKERST@ALLTERRAINENG.COM (530) 391-7635

### **ENGINEER'S STATEMENT**

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by El Paso County for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors, or omissions on my part in preparing this report.

Ryan Burns, PE Date

State of Colorado No. 54412

For and on behalf of All Terrain Engineering LLC

### **DEVELOPER'S STATEMENT**

I, the developer, have read and will comply with all of the requirements specified in this drainage report and plan.

 Business Name:
 Turkey Canon Quarry, LLC

 By:
 James Morley

 Title:
 Manager

Address: 20 Boulder Crescent Street, Suite 200, Colorado Springs, CO 80903

### EL PASO COUNTY STATEMENT

El Paso County:	
Filed in accordance with the requirements of t Paso County Engineering Criteria Manual and	the Drainage Criteria Manual, Volumes 1 and 2, El d Land Development Code as amended.
Joshua Palmer, P.E. County Engineer / ECM Administrator	Date

Conditions:



## **Table of Contents**

١.	General Purpose, Location & Description	2
II.	Drainage Basins	3
III.	Drainage Design Criteria	6
IV.	Drainage Facility Design	7
V.	Summary	9
VI.	References	9

## **Appendices**

- A. Vicinity Map, FEMA Map, NRCS Soil Survey & NOAA Atlas 14
- B. Hydrologic Analysis
- C. Hydraulic Analysis
- D. Water Quality & Detention
- E. Reference Material
- F. Drainage Maps



## I. General Purpose, Location & Description

#### a. Purpose

The purpose of this Final Drainage Report (FDR) for Schmidt Parcel – District Infrastructure is to describe the site's onsite and offsite drainage patterns, existing and proposed storm infrastructure, and to safely route developed stormwater to adequate outfalls

#### b. Location

The Schmidt Parcel (hereby referred to as the "site") is an undeveloped parcel with a total area of approximately 37 acres. At this time, only district infrastructure will be installed to support future development of the site and adjacent parcels. And the proposed public roadway.

The site is in the south half of Section 32, Township 12 South, Range 65 West of the Sixth Principal Meridian in the County of El Paso, State of Colorado. The site is located to the west of the Vollmer Road and Marksheffel Road intersection. The site is bounded by Holiday Hills Filing No.1 to the north, by Vollmer Road to the east, by the Trails at Forest Meadows Filing No. 3 to the south, and by proposed Brush Top Road extension to the west. The parcel is planned to be platted after approval of the Preliminary Plan. A vicinity map is presented in Appendix A.

#### c. Description of Property

The site is approximately 37 acres of undeveloped land with existing vegetation consisting of native grasses. A drainage swale exists along the eastern and southern border of the site which intercepts runoff and carries it off-site to the west towards Cottonwood Creek. The site generally slopes from North to South at 2-4%.

The proposed improvements include overlot grading, construction of Marksheffel Road from Vollmer Road to the Brushtop Road corridor, extension of Brushtop Road from its current terminus to the Marksheffel Road corridor to the north, associated storm drainage improvements to support the road construction and future development of surrounding parcels. It is assumed that approximately 29 acres of the site will be developed as apartments in the future. The remainder of the site will be Public R.O.W. for Brushtop and Marksheffel Roads, and a tract for a detention and water quality pond. Water and Sanitary infrastructure will also be installed with this project to support future development.

Per a NRCS soil survey, the site is made up of Blakeland loamy sands, which are classified as a Type A soils. Group A soils have a high infiltration rate when thoroughly wet and have a high rate of water transmission. The NRCS soil survey is presented in Appendix A.

There are no known irrigation facilities located on the project site.



### d. Floodplain Statement

Based on the FEMA Firm Map Number 08041C0529G, revised December 7, 2018, the proposed site is located within Zone X. Zone X is defined as areas outside the Special Flood Hazard Area (SFHA) and higher than the elevation of the 0.2-percent-annual-chance (or 500-year) flood. A FEMA panel for the site is presented in Appendix A.

## II. Drainage Basins

### a. Major Basin Description

The site lies within the Sand Creek and Cottonwood Creek Drainage Basins. Approximately 5.5 acres along the site's eastern property line is within the Sand Creek Drainage Basin. The remainder of the site lies within the Cottonwood Creek Drainage Basin. All disturbance associated with the roadway and storm sewer improvements of this report fall within the Cottonwood Creek Drainage basin.

Cottonwood Creek is located to the west of the site and runs from north to south. The reach that runs to the west of the site was studied in the "Cottonwood Creek Drainage Basin Planning Study" (Cottonwood DBPS) completed by Matrix Design Group in July 2019. According to the Cottonwood Creek DBPS, reach RUC160 runs west of the site and has been identified as being in stable condition.

The Sand Creek Basin was studied in the "Sand Creek Drainage Basin Planning Study" (Sand DBPS) completed by Stantec in January 2021. The Sand Creek DBPS assumed the Schmidt Parcel property to have an "Open Space" use for the majority of the site, which is consistent with the proposed development at this time.

### b. Existing Subbasin Description

The existing condition describes the current state of the site after the early grading for the Schmidt Parcel. The existing condition consists of six on-site basins and one off-site basin. The existing sub-basin delineation is shown on the drainage map within Appendix D and is described as follows:

**Basin OSI4** is 27.16 acres of Silver Ponds Subdivision Filing 1. Values for this basin were taken from "Silver Ponds Subdivision Filing No.1 Final Drainage Report". Runoff from this basin ( $Q_5$ =19.0 cfs,  $Q_{100}$ =44.2 cfs) flows south and is intercepted by the existing swale/berm that directs runoff around the site. Flows are diverted to the west towards DPI4 and enter Cottonwood Creek.

**Basin EXA** is 0.25 acres of an existing berm with stabilized vegetation. Runoff from this basin ( $Q_5=0.0$  cfs,  $Q_{100}=0.3$  cfs) flows along the berm west and enters an existing swale at DP1. Flows in the existing swale combine with a portion of Basin OSI4 at DP14 ( $Q_5 = 19.0$  cfs,  $Q_{100} = 44.2$  cfs) and direct flows to the west towards Cottonwood Creek.

**Basin EXB** is 0.97 acres of an existing berm with stabilized vegetation. Runoff from this basin ( $Q_5$ =0.5 cfs,  $Q_{100}$ =1.7 cfs) flows east along the berm and enters existing dual 48" RCP culverts at DP2. Culvert flows are



directed south along Vollmer Road. There is no drainage infrastructure downstream, therefore; runoff that enters Vollmer Road right-of-way (R.O.W.) flows per existing drainage patterns southeast towards Sand Creek.

**Basin EXC** is 11.5 acres of native and stabilized vegetation. Runoff from this basin ( $Q_5$ =2.0 cfs,  $Q_{100}$ =13.1 cfs) flows overland southeast and enters an existing swale. The existing swale enters Basin EXD at DP3 and follows the drainage patterns of that Basin EXD.

**Basin EXD** is 21.8 acres of native and stabilized vegetation. Runoff from this basin ( $Q_5$ =3.7 cfs,  $Q_{100}$ =23.4 cfs) flows overland southwest and enters an existing swale at DP4. Flows from DP3 and DP4 combine at DP4.1 ( $Q_5$ =5.5 cfs,  $Q_{100}$ =35.6 cfs) and are conveyed via an existing swale to the existing off-site sediment basin. The sediment basin outfalls to Cottonwood Creek.

**Basin EXE** is 3.96 acres of undeveloped land with native vegetation. Runoff from this basin ( $Q_5=0.9$  cfs,  $Q_{100}=5.7$  cfs) flows overland southeast to DP5, where flow enters Vollmer Road R.O.W. There is no drainage infrastructure downstream, therefore; runoff that enters Vollmer Road R.O.W flows per existing drainage patterns southeast towards Sand Creek.

**Basin EXF** is 2.58 acres of native and stabilized vegetation. Runoff from this basin ( $Q_5=0.6$  cfs,  $Q_{100}=4.2$  cfs) flows overland south to DP6. Basin EXF overland flows south to Trails at Forest Meadows Filing No. 3. Basin EXF flow was accounted for in "Trails at Forest Meadows Filing No. 3 Final Drainage Report" (Trails No. 3 FDR) as Basins OS2 and OS3. Basin OS2 and OS3 total 1.56 acres and have a total flow of  $Q_5=1.0$  cfs and  $Q_{100}=3.6$  cfs.

#### c. Proposed Subbasin Description Proposed Sub-basin Drainage

For each sub-basin, notate which WQ PBMP each basin is tributary to and/or which WQ exclusion applies.

The proposed condition consists of 13 on-site basins and 1 off-site basin. The proposed sub-basin delineation is shown on the drainage map within Appendix D and is described as follows:

**Basin OSI4** is 27.16 acres of Silver Ponds Subdivision Filing 1. Values for this basin were taken from "Silver Ponds Subdivision Filing No.1 Final Drainage Report". Runoff from this basin ( $Q_5$ =19.0 cfs,  $Q_{100}$ =44.2 cfs) flows south and is intercepted by the existing swale/berm that directs runoff around the site. Flows are diverted to the west towards DP14 and enter Cottonwood Creek.

**Basin A** is 0.25 acres of an existing berm with stabilized vegetation. Runoff from this basin ( $Q_5$ =0.0 cfs,  $Q_{100}$ =0.3 cfs) flows along the berm west and enters an existing swale at DP1. Flows in the existing swale combine with a portion of Basin OSI4 at DP14 ( $Q_5$  = 19.0 cfs,  $Q_{100}$  = 44.2 cfs) and direct flows west to Cottonwood Creek. Check this basin. Does not

### match up with calculation tables

**Basin B** is 0.97 acres of an existing berm with stabilized vegetation. Runoff from this basin ( $Q_5$ =0.5 cfs,  $Q_{100}$ =1.7 cfs) flows along the berm east and enters an existing dual 48" RCP culvert at DP2. Flows in the existing culvert are directed to the south along Vollmer Road. There is no drainage infrastructure downstream, therefore; runoff that enters Vollmer Road R.O.W flows southeast towards Sand Creek.



**Basin C** is 1.12 acres of undeveloped land. For the purposes of storm sewer and pond sizing, Basin C has been analyzed as apartments. Runoff from this basin ( $Q_5$ =1.9 cfs,  $Q_{100}$ =4.1 cfs) flows overland to the south to DP3 and enters Basin D where flows combine at DP4, a proposed 5' Type R sump Inlet ( $Q_5$ =4.6 cfs,  $Q_{100}$ =9.2 cfs).

## how is this conveyed to the DP?

**Basin E** is 0.39 acres of future extension of Marksheffel Road. The western limits of Basin E are based upon an anticipated high point in the future extension of Marksheffel Road. Runoff from this basin ( $Q_5$ =1.3 cfs,  $Q_{100}$ =2.5 cfs) flows via curb and gutter to DP5 at Basin D. Basin flows are combined at DP4, a proposed 5' Type check that this is the correct DP; DP5 is south of the basin and flow would

**Basin D** is 0.73 acres of proposed Marksheffel Road and proposed to overtop the crown to reach it cfs,  $Q_{100}$ =3.5 cfs) flows via curb and gutter to DP4. Flows at DP4 are captured in a proposed 5' Type R sump inlet ( $Q_5$ =4.6 cfs,  $Q_{100}$ =9.2 cfs). This inlet was sized to capture all flow in the 5 and 100-year storm. In the event of inlet failure at DP4, the flow will overtop the roadway crown and flow south within proposed Brushtop Road. Captured flows at DP4 are piped to Pond A. Curb and gutter will not be built yet, how is this conveyed to the DP?

**Basin F** is 0.48 acres of future Marksheffel Road and future sidewalk. The western limits of Basin F are based upon an anticipated high point in the future extension of Marksheffel Road. Runoff from this basin ( $Q_5$ =1.3 cfs,  $Q_{100}$ =2.5 cfs) flows via curb and gutter to DP5 at Basin G. Basin flows are combined at DP6, a proposed 5' Type R sump inlet ( $Q_5$  = 3.3 cfs,  $Q_{100}$  = 6.2 cfs).

**Basin G** is 0.84 acres of proposed Marksheffel Road and Brushtop Road and associated sidewalk. Runoff from this basin ( $Q_5=2.1$  cfs,  $Q_{100}=4.0$  cfs) flows via curb and gutter to a 15' on-grade Type R inlet at DP6 ( $Q_5=3.3$  cfs,  $Q_{100}=6.2$  cfs). This inlet was sized to capture all flow in the 5 and 100-year storm. Captured flows at DP6 are piped to Pond A.

**Basin H** is 1.29 acres of the south half of Marksheffel Road, the east half of Brushtop Road and associated sidewalks. Runoff from this basin ( $Q_5$ =3.0 cfs,  $Q_{100}$ =5.8 cfs) flows via curb and gutter to an on-grade 15' Type R Inlet at DP7. This inlet was sized to capture all flow in the 5 and 100-year storm. All captured flow from DP7 is piped to DP7.1 ( $Q_5$ =10.4 cfs,  $Q_{100}$ =20.1 cfs) where it combines with flows from DP6.1. DP7.1 flows are piped to Pond A.

**Basin I** is 3.46 acres of undeveloped land. For the purposes of storm sewer and pond sizing, Basin I has been analyzed as apartments. This assumed land use is subject to change, but believed to be a conservative estimate of the potential future use in regards to runoff and impervious. Runoff from this basin ( $Q_5$ =5.8 cfs,  $Q_{100}$ =12.7cfs) overland flows south to DP8 ( $Q_5$ =5.8 cfs,  $Q_{100}$ =12.7cfs) where flows follow the drainage patterns described in Basin J below.

**Basin J** is 1.15 acres of the north half of proposed Marksheffel Road and associated sidewalk. Runoff from this basin ( $Q_5$ =2.8 cfs,  $Q_{100}$  = 5.3 cfs) flows via curb and gutter to a 10' Type R sump inlet at DP9 ( $Q_5$  = 7.8 cfs,  $Q_{100}$  = 22.6 cfs) and are piped to DP9.1 ( $Q_5$  = 7.8 cfs,  $Q_{100}$  = 22.6 cfs). This inlet was sized to capture all flows in the 5 and 100-yr design storms. In the event of inlet failure at DP9, flows will overtop to the east and enter

Please discuss discharge to the appropriate pond

Vollmer Road.



**Basin K** is 1.20 acres of the south half of proposed Marksheffel Road and associated sidewalk. Runoff from this basin ( $Q_5$ =2.9 cfs,  $Q_{100}$ =5.5 cfs) flows via curb and gutter to a proposed 5' Type R sump inlet at DP10. All flows in the 5 and 100-yr design storm events are captured and piped to DP10.1 ( $Q_5$  = 10.7 cfs and  $Q_{100}$  = 22.0 cfs) where they combine with piped flows from DP9.1. In the event of inlet failure at DP10, the flow will overtop to the east and enter Vollmer Road. Flows from DP10.1 are piped to Pond A.

**Basin M** is 23.9 acres of undeveloped land. For the purposes of storm sewer and pond sizing, Basin M is analyzed as a multi-family/apartment development within Lot 1. This site is being designed by others and will require a site specific FDR to confirm design assumptions of this report. The timing of the Lot 1 development is unknown and a site plan is not available at this time. It is anticipated future runoff ( $Q_5$ =32.5 cfs,  $Q_{100}$ =69.4 cfs) will flow within the development and be captured at DP13. DP13 flows are combined at the proposed manhole at DP13.1 ( $Q_5$ =41.7 cfs,  $Q_{100}$ =88.2 cfs) with upstream flows from DP10.1. All captured flow from DP13.1 are piped to Pond A. In the interim condition, the land within this basin will remain undeveloped and flow per existing drainage patterns to Pond A at DP14.

**Basin N** is 2.98 acres of Pond A within Tract C. Runoff from this basin ( $Q_5$ =1.2 cfs,  $Q_{100}$ = 5.0 cfs) flows overland to the concrete trickle channel at DP14 ( $Q_5$ =44.2 cfs,  $Q_{100}$ = 94.7 cfs) where they combine with piped flow from DP13.1. Pond A outlet structure discharges (Q5 = 1.0 cfs, Q100 = 16.6 cfs) into storm sewer under proposed Brushtop Road to the proposed outfall channel. The outfall channel discharges to Cottonwood Creek via an assumed existing outfall from the CDR-22-007 project.

**Basin O** is 0.22 acres of proposed Brushtop Road and its associated sidewalk. Basin O is located downstream of Pond A and will not be piped to Pond A. Runoff from this basin ( $Q_5$ =0.6 cfs,  $Q_{100}$ = 1.2 cfs) flows off-site to the south at DP15. DP15 follows historic drainage patterns towards the Trails at Forest Meadows Filing No. 3. Per the Trails No. 3 FDR, flows from the Schmidt parcel were accounted for in Basins OS2 and OS3. The basins total 1.56 acres and have a total flow of  $Q_5$ =1.0 cfs and  $Q_{100}$ =3.6 cfs. Therefore, the Basin O discharge is consistent with the Trails No. 3 FDR. There are no negative impacts anticipated for the adjacent property as a result of Basin O discharge.

## III. Drainage Design Criteria

### a. Development Criteria Reference

Storm drainage analysis and design criteria for this project were taken from the "City of Colorado Springs/El Paso County Drainage Criteria Manual" Volumes 1 and 2 (EPCDCM), dated October 12, 1994, the "Urban Storm Drainage Criteria Manual" Volumes 1 to 3 (USDCM) and Chapter 6 and Section 3.2.1 of Chapter 13 of the "Colorado Springs Drainage Criteria Manual" (CSDCM), dated May 2014, as adopted by El Paso County.

### b. Hydrologic Criteria

All hydrologic data was obtained from the "El Paso Drainage Criteria Manual" Volumes 1 and 2, and the "Urban Drainage and Flood Control District Urban Storm Drainage Criteria Manual" Volumes 1, 2, and 3. Onsite drainage improvements were designed based on the 5 year (minor) storm event and the 100-year (major) storm event. Runoff was calculated using the Rational Method, and rainfall intensities for the 5-year and the



100-year storm return frequencies were obtained from Table 6-2 of the CSDCM. One-hour point rainfall data for the storm events is identified in the chart below. Runoff coefficients were determined based on proposed land use and from data in Table 6-6 from the CSDCM. Time of concentrations were developed using equations from CSDCM. All runoff calculations and applicable charts and graphs are included in the Appendices.

Storm	Rainfall (in.)
5-year	1.50
100-year	2.52

	Table 1	- 1-hr	Point	Rainfall	Data
--	---------	--------	-------	----------	------

#### c. Hydraulic Criteria

The Rational Method and USDCM's SF-2 and SF-3 forms are used to determine the runoff from the minor and major storms. MHFD-Detention v4.06 spreadsheet is utilized for full-spectrum extended detention basin design. Hydraflow Express is used for hydraulic modeling of swale, spillway, and emergency overflow calculations. Proposed swales have been designed to meet El Paso County criteria for velocity, freeboard, and stability. Hydraflow Storm Sewers is used for storm sewer hydraulic analysis.

## IV. Drainage Facility Design

#### a. General Concept

Onsite stormwater will be conveyed via proposed curb and gutter to proposed Type R inlets. Captured storm water will be piped to Pond A; a full spectrum water quality and detention pond. Drainage infrastructure is sized to account for the assumed future condition of tributary areas. Pond A will discharge to Cottonwood Creek per historic drainage patterns.

#### b. Water Quality & Detention

Pond A provides full spectrum water quality and detention for Basins C-N. A total of 37.54 acres at 73% imperviousness are treated in Pond A. The WQCV and EURV are released in 40 and 72 hours, respectively. A concrete forebay is located at the two outfalls into the pond. A 6.0' concrete trickle channel conveys flow towards the full spectrum outlet structure. The outlet structure will release 100-year stormwater at less than historic rates to minimize adverse impacts to downstream stormwater facilities. For some minor storm events, the release rate is higher than the existing predevelopment flows. To release the 5-year storm in under 72 hours, the 5-50 year storms must release at rates greater than historic. The table below provides the volumes required for the proposed pond, along with the release rates for the 5-year and 100-year storm.

	Required Volume (ac-ft)		Provided Volume	WQCV (ac-ft)	EURV (ac-ft)	5-year Release	100-year Release	
			(ac-ft)			(cts)	(Cfs)	
Pond A		5.2	7.2	0.9	2.6	1.1	16.6	

Please make adjustments to the design to reduce the difference as much as possible. The difference in release rate is too much in the current design. Address how water quality requirements are met for the other basins.



A broad crested weir, lined with Type L buried soil riprap, is provided as an emergency spillway for Pond A. The emergency spillway conveys flow to a proposed emergency overflow structure (Type C sump inlet) between Pond A and Brushtop Road. The Type C sump inlet is designed to intercept 41.1 cfs of the peak 100-year flow, 96.7 cfs. The remaining 55.6 cfs will flow south in Brushtop Road towards Vanderwood Road. Vanderwood Road has a maximum capacity of 56 cfs and stormwater is captured or conveyed by the existing infrastructure within the Trails at Forest Meadows Filing No. 4.

The Pond A outfall channel (controlled release  $Q_5=1.1$  cfs,  $Q_{100}=16.6$  cfs), (emergency condition  $Q_{100}=41.1$  cfs) flows west to Cottonwood Creek. There are no expected impacts to water surface elevations in Cottonwood Creek from the development of this site. Pond A will be privately owned and maintained by Stonebridge Metropolitan District.

#### c. Major Drainageways

There are no major drainageways that traverse the site.

#### d. Operations & Maintenance

An Operations and Maintenance Manual has been submitted separately. The manual specifies maintenance intervals and required actions to maintain the function of the extended detention basin and appurtenances.

### e. Grading & Erosion Control Plan

Due to the project disturbance area, a separate Grading and Erosion Control plan is required. The Grading and Erosion Control Plan has been submitted in conjunction with this FDR.

#### f. Four Step Process

In accordance with the El Paso County Drainage Criteria Manual Volume 2, this site has implemented the four step process to minimize adverse impacts of urbanization. The four step process includes reducing runoff volumes, treating the water quality capture volume (WQCV), stabilizing drainage ways, and implementing long-term source controls.

Step 1 – Reducing Runoff Volumes: The proposed site development consists of multi-family homes with open spaces and lawn areas interspersed within the development that helps disconnect impervious areas and reduce runoff volumes.

Step 2 – Stabilize Drainageways: The majority of the site lies within the Cottonwood Creek Drainage Basin, while the eastern most portion on the property is within the Sand Creek Drainage Basin. Cottonwood Creek is located to the west of the site. Basin and bridge fees will be due at time of platting. There are no proposed improvements with the 100-year flood plain. According to the "Cottonwood Creek Drainage Basin Planning Study" (Cottonwood DBPS), the reach adjacent to the site is RUC160. This reach has been categorized as having no known or future expected erosion issues according to the Cottonwood DBPS Figure 4-7. Proposed outfalls will be analyzed in the final design stage for stability. Applicable excerpts from the Cottonwood DBPS are presented in Appendix D.



Step 3 – Treat the WQCV: Water quality treatment for this site is provided in a proposed full-spectrum EDB (Pond A). The runoff from this site will be captured by inlets and conveyed to Pond A via storm sewer. Upon entrance to the ponds, flows will be captured in concrete bottom forebays designed to promote settlement of suspended solids. A concrete trickle channel will help convey pond flows and minimize standing water. The outlet structure has been designed to detail the WQCV 40 hours and the EURV 72 hours. 100-year flows released from Pond A will be reduced to historic rates.

Step 4 – Consider Need for Industrial and Commercial BMPs: There are no commercial or industrial components to this development, therefore; no Industrial or Commercial BMPs are required. BMPs will be utilized to minimize off-site contaminants and to protect the downstream receiving waters. The site is not a high-risk site per Figure I-1 in ECM Appendix I. Site specific temporary source control BMPs that will be implemented include, but are not limited to, silt fencing placed around downstream areas of disturbance, construction vehicle tracking pads at the entrances, designated vehicle fueling areas, covered storage areas, and spill containment and control. The permanent erosion control BMPs include asphalt drives, storm inlets, storm sewer, Pond A, and permanent vegetation.

### g. Drainage Basin & Bridge Fees

Applicable drainage and bridge fees for the site will be paid at time of platting.

### V. Summary

Schmidt Parcel – District Infrastructure remains consistent with pre-development drainage conditions with the construction of the recommended drainage improvements. The proposed development will not adversely affect downstream stormwater infrastructure or surrounding developments. This report meets the latest El Paso County Drainage Criteria.

## VI. References

- 1. El Paso County Drainage Criteria Manual, Vol I & II, as amended.
- 2. El Paso County Engineering Criteria Manual, 2019.
- 3. Urban Storm Drainage Criteria Manual (Volumes 1, 2, and 3), Urban Drainage and Flood Control District, June 2001.
- 4. Final Drainage Report for Silver Ponds Subdivision Filing No. 1, M.V.E. Inc., February 2, 1995, Revised May 5, 1996.
- 5. Sand Creek Drainage Basin Planning Study, Stantec, January 2021.
- 6. Cottonwood Creek Drainage Basin Planning Study, Matrix Design Group, July 2019.
- 7. Trails at Forest Meadows Filing No. 3 Final Drainage Report, M&S Civil Consultants Inc., August 2015.
- 8. Trails at Forest Meadows Filing No. 4 Final Drainage Report, M&S Civil Consultants Inc., April 2016.

Include a cost estimate for each PBMP with line items for all components (ex: riprap, road base, forebay, trickle channel, outlet structure, outlet pipe, spillway, etc). Input the total value into the FAE form under "Permanent Pond/BMP (provide engineer's estimate)" in Section 1. The total should not include grading, which is a separate line item in Section 1: "Earthwork." The cost estimate should include labor costs (as a separate line item or added into the cost of each component).



## APPENDIX A – VICINITY MAP, FEMA MAP, NRCS WEB SOIL SURVEY & NOAA ATLAS 14





USDA Natural Resources Conservation Service



# Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
8	Blakeland loamy sand, 1 to 9 percent slopes	A	22.3	19.5%
19	Columbine gravelly sandy loam, 0 to 3 percent slopes	A	64.2	56.2%
71	Pring coarse sandy loam, 3 to 8 percent slopes	В	12.1	10.6%
85	Stapleton-Bernal sandy loams, 3 to 20 percent slopes	В	15.6	13.6%
Totals for Area of Intere	st		114.1	100.0%

## Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

## **Rating Options**

Aggregation Method: Dominant Condition Component Percent Cutoff: None Specified Tie-break Rule: Higher



NOTES TO USERS

NOTE: MAP AREA SHOWN ON THIS PANEL IS LOCATED WITHIN TOWNSHIP 12 SOUTH, RANGE 65 WEST, AND TOWNSHIP 13 SOUTH, RANGE 65 WEST.

	SPECIAL FLOOD INUNDATION BY The 1% annual chance flood (100) that has a 1% chance of being equi- Hazard Area is the area subject of Special Flood Hazard include Zones Elevation is the water-surface elevator ZONE A No Base Flood Elevator ZONE AE Base Flood Elevator ZONE AO Flood depths of 1 to depths determined determined. ZONE AR Special Flood Hazarn flood by a flood con mindicates that the for protection from the ZONE A99 Area to be protector protection system determined. ZONE V Coastal flood zone Elevations determined ZONE VE Coastal flood zone Elevations determined. ZONE X Areas of 0.2% annu average depths of square mile; and area COTHER AREAS ZONE X Areas determined to ZONE X Areas in which flood COASTAL BARRED	<ul> <li>DEGEEND</li> <li>D. HAZARD AREAS (SFHAS) SUBJECT TO (THE 1% ANNUAL CHANCE FLOOD)</li> <li>Agear flood), also known as the base flood, is the flood to flooding by the 1% annual chance flood. Areas of s A, AE, AH, AO, AR, A99, V, and VE. The Base Flood to flooding by the 1% annual chance flood. Areas of s A, AE, AH, AO, AR, A99, V, and VE. The Base Flood to flooding by the 1% annual chance flood. Areas of s A, AE, AH, AO, AR, A99, V, and VE. The Base Flood to flooding by the 1% annual chance flood.</li> <li>Attern Flood</li> <li>A feet (usually areas of ponding); Base Flood c.</li> <li>A feet (usually sheet flow on sloping terrain); average for areas of alluvial fan flooding, velocities also</li> <li>A frea Formerly protected from the 1% annual chance trol system that was subsequently decertified. Zone AR ormer flood control system is being restored to provide 1% annual chance or greater flood.</li> <li>A frea form 1% annual chance flood by a Federal flood under construction; no Base Flood Elevations</li> <li>with velocity hazard (wave action); no Base Flood ed.</li> <li>AS IN ZONE AE</li> <li>Bate chance flood; areas of 1% annual chance flood with less than 1 foot or with drainage areas less than 1 eas protected by levees from 1% annual chance flood</li> <li>A the usual flood is areas flood plain.</li> <li>A events de the 0.2% annual chance floodplain.</li> <li>A events de the 0.2% annual chance floodplain.</li> <li>A the areards are undetermined, but possible.</li> <li>A cursting area undetermined, but possible.</li> <li>A cursting area undetermined, but possible.</li> <li>A cursting area undetermined, but possible.</li> <li>A cursting areas are undetermined, but possible.</li> <li>A cursting areas are undetermined, but possible.</li> <li>A cursting area undetermined, but possible.</li> <li>A cursting area undetermined, but possible.</li> </ul>
		OTECTED AREAS (OPAs)
		lain boundary
	Floodw Zone D	vay boundary 9 Boundary
	CBRS a	and OPA boundary
TF	Bounda Flood E	ary dividing Special Flood Hazard Areas of different Base Elevations, flood depths or flood velocities.
		lood Elevation line and value; elevation in feet* lood Elevation value where uniform within zone;
	elevation** Referenced to the North American	on in feet* n Vertical Datum of 1988 (NAVD 88)
	A Cross s	section line
	(23)(23) Transe	ct line
	97° 07' 30.00" Geogra 32° 22' 30.00" Datum	aphic coordinates referenced to the North American of 1983 (NAD 83)
	<sup>42</sup> 75 <sup>000m</sup> N 1000-n zone 1.	neter Universal Transverse Mercator grid ticks, 3
	6000000 FT 5000-fe system	oot grid ticks: Colorado State Plane coordinate , central zone (FIPSZONE 0502),
	DX5510 Bench	rt Conformal Conic Projection mark (see explanation in Notes to Users section of
	X this FI	RM panel)
	• River M	
	Refer to	
	FLC	DOD INSURANCE RATE MAP MARCH 17, 1997
	EFFECTIVE DA DECEMBER 7, 2018 - to upda	ATE(S) OF REVISION(S) TO THIS PANEL ate corporate limits, to change Base Flood Elevations and
	Special Flood Hazard Areas, to incorporate pr	update map format, to add roads and road names, and to eviously issued Letters of Map Revision.
	For community map revision histor Map History Table located in the Flo	y prior to countywide mapping, refer to the Community ood Insurance Study report for this jurisdiction.
	To determine if flood insurance is agent or call the National Flood Ins	s available in this community, contact your insurance surance Program at 1-800-638-6620.
		MAP SCALE 1" = 500'
		150 300
		PANEL 0529G
		FIRM
		FLOOD INSURANCE RATE MAP
		FL PASO COUNTV
		COLORADO
		AND INCORPORATED AREAS
		PANEL 529 OF 1300
	TAT	(SEE MAP INDEX FOR FIRM PANEL LAYOUT)
	AAA	CONTAINS:           COMMUNITY         NUMBER         PANEL         SUFFIX
		COLORADO SPRINGS, CITY OF 080060 0529 G
		Notice to User: The <b>Map Number</b> shown below should be used when placing map orders: the <b>Community Number</b> shown above should be used on insurance applications for the subject
		08041C0529G
		DECEMBER 7, 2018
		Federal Emergency Management Agency
		The second



38° 56' 15.00"

RAINFALL DEPTHS

**UD-DETENTION** 

**USED FOR** 

Precipitation Frequency Data Server

NOAA Atlas 14, Volume 8, Version 2 Location name: Colorado Springs, Colorado, USA\* Latitude: 38.9556°, Longitude: -104.6899° Elevation: 7015 ft\*\* \* source: ESRI Maps \*\* source: USGS

#### POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Deborah Martin, Sandra Pavlovic, Ishani Roy, Michael St. Laurent, Carl Trypaluk, Dale Unruh, Michael Yekta, Geoffery Bonnin

NOAA, National Weather Service, Silver Spring, Maryland

PF\_tabular | PF\_graphical | Maps\_&\_aerials

### **PF** tabular

PC	<sup>2</sup> DS-based point precipitation frequency estimates with 90% confidence intervals (in inches) <sup>1</sup>											
Durat					Average	recurrence	interval (ye	ars)				
Durati	on	1	2	5	10	25	50	100	200	500	1000	
5-mi	n	<b>0.237</b> (0.195-0.291)	<b>0.290</b> (0.238-0.356)	<b>0.381</b> (0.311-0.469)	<b>0.461</b> (0.374-0.570)	<b>0.579</b> (0.456-0.748)	<b>0.675</b> (0.518-0.882)	<b>0.776</b> (0.574-1.04)	<b>0.884</b> (0.625-1.22)	<b>1.04</b> (0.702-1.46)	<b>1.16</b> (0.759-1.65)	
10-m	in	<b>0.348</b> (0.285-0.426)	<b>0.424</b> (0.348-0.521)	<b>0.557</b> (0.456-0.686)	<b>0.675</b> (0.548-0.835)	<b>0.847</b> (0.668-1.10)	<b>0.988</b> (0.758-1.29)	<b>1.14</b> (0.840-1.52)	<b>1.30</b> (0.915-1.78)	<b>1.52</b> (1.03-2.14)	<b>1.69</b> (1.11-2.42)	
15-m	in	<b>0.424</b> (0.348-0.520)	<b>0.517</b> (0.424-0.635)	<b>0.680</b> (0.556-0.837)	<b>0.823</b> (0.669-1.02)	<b>1.03</b> (0.814-1.34)	<b>1.20</b> (0.924-1.58)	<b>1.39</b> (1.02-1.86)	<b>1.58</b> (1.12-2.17)	<b>1.85</b> (1.25-2.61)	<b>2.06</b> (1.36-2.94)	
30-m	in	<b>0.613</b> (0.504-0.752)	<b>0.748</b> (0.613-0.918)	<b>0.981</b> (0.802-1.21)	<b>1.19</b> (0.964-1.47)	<b>1.49</b> (1.17-1.92)	<b>1.74</b> (1.33-2.27)	<b>2.00</b> (1.48-2.67)	<b>2.27</b> (1.61-3.13)	<b>2.66</b> (1.80-3.76)	<b>2.97</b> (1.95-4.24)	
60-m	in	<b>0.794</b> (0.652-0.974)	<b>0.948</b> (0.778-1.16)	<b>1.23</b> (1.00-1.51)	<b>1.48</b> (1.21-1.84)	<b>1.88</b> (1.49-2.44)	<b>2.21</b> (1.70-2.90)	<b>2.57</b> (1.90-3.46)	<b>2.96</b> (2.10-4.09)	<b>3.52</b> (2.39-4.99)	<b>3.97</b> (2.61-5.67)	
2-hr	•	<b>0.974</b> (0.806-1.19)	<b>1.15</b> (0.949-1.40)	<b>1.47</b> (1.21-1.80)	<b>1.78</b> (1.46-2.19)	<b>2.26</b> (1.82-2.94)	<b>2.68</b> (2.08-3.51)	<b>3.14</b> (2.35-4.21)	<b>3.64</b> (2.60-5.01)	<b>4.37</b> (3.00-6.17)	<b>4.97</b> (3.29-7.05)	
3-hr	•	<b>1.08</b> (0.893-1.30)	<b>1.25</b> (1.04-1.51)	<b>1.58</b> (1.31-1.93)	<b>1.92</b> (1.57-2.34)	<b>2.45</b> (1.98-3.19)	<b>2.92</b> (2.29-3.83)	<b>3.45</b> (2.60-4.62)	<b>4.03</b> (2.90-5.55)	<b>4.90</b> (3.38-6.90)	<b>5.61</b> (3.73-7.93)	
6-hr		<b>1.26 1.44</b> (1.05-1.51) (1.20-1.7		<b>1.81</b> (1.51-2.19)	<b>2.19</b> (1.81-2.65)	<b>2.81</b> (2.29-3.64)	<b>3.37</b> (2.66-4.39)	<b>4.00</b> (3.04-5.34)	<b>4.71</b> (3.42-6.45)	<b>5.76</b> (4.01-8.08)	<b>6.64</b> (4.45-9.32)	
12-h	r	<b>1.46</b> (1.23-1.74)	<b>1.68</b> (1.41-2.01)	<b>2.12</b> (1.78-2.54)	<b>2.56</b> (2.13-3.08)	<b>3.26</b> (2.68-4.19)	<b>3.89</b> (3.09-5.03)	<b>4.59</b> (3.51-6.08)	<b>5.38</b> (3.94-7.31)	<b>6.54</b> (4.58-9.11)	<b>7.50</b> (5.07-10.5)	
24-h	r	1.68         1.97         2.51           (1.43-1.99)         (1.67-2.34)         (2.12-2.99)		<b>2.51</b> (2.12-2.99)	<b>3.02</b> (2.54-3.61)	<b>3.81</b> (3.13-4.82)	<b>4.49</b> (3.58-5.73)	<b>5.23</b> (4.02-6.84)	<b>6.05</b> (4.45-8.13)	<b>7.23</b> (5.10-9.97)	<b>8.20</b> (5.59-11.4)	
2-da	у	<b>1.95</b> (1.67-2.30)	<b>2.32</b> (1.98-2.73)	<b>2.96</b> (2.52-3.50)	<b>3.54</b> (3.00-4.21)	<b>4.41</b> (3.63-5.50)	<b>5.14</b> (4.11-6.47)	<b>5.91</b> (4.56-7.63)	<b>6.74</b> (4.97-8.94)	<b>7.91</b> (5.60-10.8)	<b>8.85</b> (6.08-12.2)	
3-da	у	<b>2.15</b> (1.85-2.52)	<b>2.55</b> (2.18-2.99)	<b>3.24</b> (2.76-3.81)	<b>3.85</b> (3.27-4.55)	<b>4.77</b> (3.94-5.90)	<b>5.52</b> (4.44-6.92)	<b>6.33</b> (4.90-8.13)	<b>7.19</b> (5.33-9.50)	<b>8.40</b> (5.98-11.4)	<b>9.37</b> (6.46-12.9)	
4-da	у	<b>2.32</b> (2.00-2.72)	<b>2.73</b> (2.35-3.19)	<b>3.44</b> (2.95-4.03)	<b>4.08</b> (3.48-4.80)	<b>5.02</b> (4.16-6.20)	<b>5.81</b> (4.68-7.25)	<b>6.64</b> (5.16-8.50)	<b>7.53</b> (5.60-9.92)	<b>8.79</b> (6.27-11.9)	<b>9.80</b> (6.78-13.4)	
7-da	у	<b>2.75</b> (2.38-3.19)	<b>3.18</b> (2.75-3.70)	<b>3.94</b> (3.40-4.59)	<b>4.61</b> (3.96-5.40)	<b>5.62</b> (4.69-6.89)	<b>6.46</b> (5.24-8.01)	<b>7.35</b> (5.75-9.35)	<b>8.30</b> (6.21-10.9)	<b>9.64</b> (6.93-13.0)	<b>10.7</b> (7.47-14.6)	
10-da	ıy	<b>3.13</b> (2.72-3.61)	<b>3.59</b> (3.12-4.16)	<b>4.40</b> (3.81-5.11)	<b>5.13</b> (4.41-5.98)	<b>6.20</b> (5.18-7.55)	<b>7.08</b> (5.76-8.73)	<b>8.01</b> (6.29-10.1)	<b>9.01</b> (6.77-11.7)	<b>10.4</b> (7.50-13.9)	<b>11.5</b> (8.06-15.6)	
20-da	ıy	<b>4.20</b> (3.68-4.82)	<b>4.82</b> (4.22-5.53)	<b>5.86</b> (5.11-6.74)	<b>6.75</b> (5.85-7.81)	<b>8.03</b> (6.74-9.64)	<b>9.04</b> (7.40-11.0)	<b>10.1</b> (7.97-12.6)	<b>11.2</b> (8.46-14.4)	<b>12.7</b> (9.20-16.8)	<b>13.9</b> (9.77-18.7)	
30-da	ıy	<b>5.08</b> (4.47-5.80)	<b>5.83</b> (5.13-6.67)	<b>7.08</b> (6.20-8.11)	<b>8.12</b> (7.07-9.35)	<b>9.56</b> (8.03-11.4)	<b>10.7</b> (8.76-12.9)	<b>11.8</b> (9.35-14.7)	<b>13.0</b> (9.83-16.6)	<b>14.5</b> (10.6-19.1)	<b>15.7</b> (11.1-21.0)	
45-da	ıy	<b>6.17</b> (5.45-7.01)	<b>7.09</b> (6.26-8.07)	<b>8.58</b> (7.55-9.80)	<b>9.80</b> (8.57-11.2)	<b>11.4</b> (9.63-13.5)	<b>12.7</b> (10.4-15.2)	<b>13.9</b> (11.0-17.1)	<b>15.1</b> (11.5-19.2)	<b>16.7</b> (12.2-21.8)	<b>17.8</b> (12.7-23.8)	
60-da	ıy	<b>7.08</b> (6.28-8.03)	<b>8.15</b> (7.22-9.24)	<b>9.84</b> (8.68-11.2)	<b>11.2</b> (9.82-12.8)	<b>13.0</b> (10.9-15.2)	<b>14.3</b> (11.8-17.1)	<b>15.6</b> (12.4-19.1)	<b>16.8</b> (12.8-21.2)	<b>18.4</b> (13.4-23.9)	<b>19.5</b> (13.9-26.0)	

<sup>1</sup> Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values. Please refer to NOAA Atlas 14 document for more information.

Back to Top

**PF** graphical





Duration									
5-min	- 2-day								
- 10-min	— 3-day								
- 15-min	— 4-day								
— 30-min	- 7-day								
	— 10-day								
— 2-hr	— 20-day								
— 3-hr	— 30-day								
— 6-hr	— 45-day								
- 12-hr	— 60-day								
24-hr									

NOAA Atlas 14, Volume 8, Version 2

1

2

5

10

25

Average recurrence interval (years)

50

Created (GMT): Thu Aug 1 18:08:13 2024

500

1000

Back to Top

100

200

Maps & aerials

Small scale terrain



Large scale terrain





Large scale aerial



## **APPENDIX B – HYDROLOGIC CALCULATIONS**

## **COMPOSITE % IMPERVIOUS CALCULATIONS - EXISTING CONDITIONS**

Subdivision:

Location: El Paso County

Project Name: Schmidt Parcel-District Infrastructure

Project No.: 24013.00 Calculated By: REB

Checked By: NQJ

Date: 12/23/24

			Gravel Stree	et (80% Imp.	)		ed (2% Imp.	)	Basins Total		<b>Basins Total</b>	
Bacin ID	Total Area	C	C	Area (ac)	Weighted	Weighted		Area (ac)	Weighted	Weighted C		Weighted %
Basili ID	(ac)	C5	C <sub>100</sub>	Alea (ac)	% Imp.	<b>C</b> 5	C <sub>100</sub>	Alea (ac)	% Imp.	C₅	C <sub>100</sub>	Imp.
EXA	0.25	0.59	0.70	0.00	0.0%	0.09	0.36	0.25	2.0%	0.09	0.36	2.0%
EXB	0.97	0.59	0.70	0.27	22.3%	0.09	0.36	0.70	1.4%	0.23	0.45	23.7%
EXC	11.50	0.59	0.70	0.00	0.0%	0.09	0.36	11.50	2.0%	0.09	0.36	2.0%
EXD	21.80	0.59	0.70	0.27	1.0%	0.09	0.36	21.53	2.0%	0.10	0.36	3.0%
EXE	3.96	0.59	0.70	0.00	0.0%	0.09	0.36	3.96	2.0%	0.09	0.36	2.0%
EXF	2.58	0.59	0.70	0.00	0.0%	0.09	0.36	2.58	2.0%	0.09	0.36	2.0%
TOTAL	41.06											3.0%

### **STANDARD FORM SF-2 - EXISTING CONDITIONS** TIME OF CONCENTRATION

Subdivision:

Location: El Paso County

#### Project Name: Schmidt Parcel-District Infrastructure

Project No.: 24013.00

Calculated By: REB Checked By: NQJ

Date: 12/23/24

SUB-BASIN INITIAL/					AL/OVER	LAND	TRAVEL TIME					tc CHECK					
DATA			(T <sub>i</sub> )			(T <sub>t</sub> )				(URBANIZED BASINS)			FINAL				
BASIN	D.A.	Hydrologic	Impervious	C <sub>5</sub>	C <sub>100</sub>	L	<b>S</b> <sub>o</sub>	t,	L <sub>t</sub>	<b>S</b> <sub>t</sub>	К	VEL.	t <sub>t</sub>	COMP. t <sub>c</sub>	TOTAL	Urbanized $t_c$	t <sub>c</sub>
ID	(ac)	Soils Group	(%)			(ft)	(%)	(min)	(ft)	(%)		(ft/s)	(min)	(min)	LENGTH (ft)	(min)	(min)
EXA	0.25	A	2.0%	0.09	0.36	10.0	25.0%	2.0	1030	0.5%	7.0	0.5	34.7	36.7	1040.0	51.8	51.8
EXB	0.97	А	23.7%	0.23	0.45	10.0	25.0%	1.7	950	1.5%	15.0	1.8	8.6	10.3	960.0	32.5	32.5
EXC	11.50	А	2.0%	0.09	0.36	300.0	3.0%	22.0	1260	1.8%	7.0	0.9	22.5	44.5	1560.0	42.6	44.5
EXD	21.80	А	3.0%	0.10	0.36	300.0	2.3%	23.8	1400	1.8%	7.0	0.9	24.8	48.7	1700.0	44.0	48.7
EXE	3.96	А	2.0%	0.09	0.36	300.0	2.1%	24.8	425	2.1%	7.0	1.0	7.0	31.9	725.0	31.0	31.9
EXF	2.58	A	2.0%	0.09	0.36	235.0	2.6%	20.4	0	0.0%	7.0	0.0	0.0	20.4	235.0	25.7	25.7

#### NOTES:

NOTES:				Table 6-2. NRCS Convey	ance factors, K
$t_c = t_i + t_t$	Equation 6	$t_i = \frac{0.395(1.1 - C_5)\sqrt{L_i}}{c_1^{0.33}}$	Equation 6-3	Type of Land Surface	Conveyance
Where:		S <sub>o</sub>		Heavy meadow	2.
THREE.		Where:		Tillage/field	5
$t_c$ = computed time of concentration (minutes)		t = averland (initial) flam time (minutes)		Short pasture and lawns	7
$t_i$ = overland (initial) flow time (minutes)		$C_5 =$ runoff coefficient for 5-year frequency (from Table 6-4)		Nearly bare ground	10
		$L_i$ = length of overland flow (ft)		Grassed waterway	1:
$t_t = \text{channelized flow time (minutes)}.$		$S_0$ = average slope along the overland flow path (ff/ff).		Paved areas and shallow paved swales	20
$t_t = \frac{L_t}{60K\sqrt{S_o}} = \frac{L_t}{60V_t}$	Equation 6-4	$t_{r} = (26 - 17i) + \frac{L_{r}}{60(14i + 9)\sqrt{S_{r}}}$	Equation 6-5		
Where:		Where:			
$t_t$ = channelized flow time (travel time, min) $L_t$ = waterway length (ft) $S_0$ = waterway slope (ft)ft) $V_t$ = travel time velocity (ft/sec) = K $\lor$ S <sub>0</sub> K = NRCS conveyance factor (see Table 6-2).		$t_e = \minimum$ time of concentration for first design point when $L_t = \text{length of channelized flow path (ft)}$ T = imperviousness (expressed as a decimal) $S_t = \text{slope of the channelized flow path (ft) ft)}.$	less than te from Equation 6-	L)	

Use a minimum  $t_c$  value of 5 minutes for urbanized areas and a minimum  $t_c$  value of 10 minutes for areas that are not considered urban. Use minimum values even when calculations result in a lesser time of concentration.

Conveyance Factor, K 2.5 5 7 10 15

20

#### **STANDARD FORM SF-3 - EXISTING CONDITIONS**

#### STORM DRAINAGE SYSTEM DESIGN

(RATIONAL METHOD PROCEDURE)

Project Name: Schmidt Parcel-District Infrastructure

Subdivision: Location: El Paso County Design Storm: 5-Year

Project No.:	24013.00
Calculated By:	REB
Checked By:	NQJ

Date: 12/23/24

				DIF	RECT RU	NOFF			Т(	OTAL I	RUNO	FF		STREE	Г		PI	PE		TRA	/EL TII	ME	
STREET	Design Point	Basin ID	Area (Ac)	Runoff Coeff.	$t_c$ (min)	C*A (Ac)	/ (in/hr)	Q (cfs)	tc (min)	C*A (ac)	/ (in/hr)	Q (cfs)	Q <sub>street</sub> (cfs)	C*A (ac)	Slope (%)	Q <sub>pipe</sub> (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	$t_t$ (min)	REMARKS
	14	0614	27.40	0.00	20.2	0.45	2.22	10.0															Off-site Basin OSI4 Values from Sliver Pond FDR (Bains I4 &
	14	0514	27.16	0.30	29.2	8.15	2.33	19.0															DP21)
	1	EV A	0.25	0.00	F1 0	0.02	1.00	~ ~															Existing berm sends off-site flow from north to the west to
	1	EXA	0.25	0.09	51.8	0.02	1.66	0.0															the existing swale at DP1.
	2	EVD	0.07	0.22	22 5	0.22	2.20	0 5															Existing berm sends off-site flow from north to the east to
	2	EXB	0.97	0.23	32.5	0.22	2.30	0.5															the exisiting swale and cuivert at DP2.
	ч	FXC	11 50	0.09	44 5	1 04	1 89	2.0															Runon overland nows to existing swale and continues into
		LAC	11.50	0.05		1.04	1.05	2.0															Bunoff from Basin FXD, overland flows to existing swale at
	4	EXD	21.80	0.10	48.7	2.10	1.75	3.7															DP4.
																							Flows from DP3 and DP4 combine at DP2.1 and flows to the
	4.1								48.7	3.13	1.75	5.5											west to the existing sediment basin.
																							Runoff overland flows across exisitng field to DP5 where
	5	EXE	3.96	0.09	31.9	0.36	2.39	0.9															flow enters Vollmer Road R.O.W.
																							Runoff from Basin EXF overland flows south off-site and
( <b>I</b>	6	EXF	2.58	0.09	25.7	0.23	2.72	0.6															enters the adjacent property.

Values in BLUE indicate they are from the "Silver Ponds Subdivision Filing No. 1 Final Drainage Report", by M.V.E. Inc. revised May 5th, 1996.

#### **STANDARD FORM SF-3 - EXISTING CONDITIONS**

#### STORM DRAINAGE SYSTEM DESIGN

(RATIONAL METHOD PROCEDURE)

Subdivision: Location: El Paso County Design Storm: 100-Year

Project Name: S	chmidt Parcel	-District	Infrastructure
-----------------	---------------	-----------	----------------

Project No.: 24013.00

Calculated By: REB Checked By: NOJ

Date: 12/23/24

				DIRE	CT RU	NOFF			Т	OTAL F	RUNOF	F		STREE	Т		PI	PE		TRAV	EL TIN	ΛE	
STREET	Design Point	Basin ID	Area (ac)	Runoff Coeff.	$t_c$ (min)	C*A (ac)	/ (in/hr)	Q (cfs)	tc (min)	C*A (ac)	/ (in/hr)	Q (cfs)	Q <sub>street</sub> (cfs)	C*A (ac)	Slope (%)	Q <sub>pipe</sub> (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	$t_t$ (min)	REMARKS
	14	OSI4	27.16	0.40	29.2	10.86	4.07	44.2															Off-site Basin OSI4 Values from Sliver Pond FDR (Bains I4 & DP21)
	1	EXA	0.25	0.36	51.8	0.09	2.79	0.3															Existing berm sends off-site flow from north to the west to the existing swale at DP1.
	2	ЕХВ	0.97	0.45	32.5	0.44	3.97	1.7															Existing berm sends off-site flow from north to the east to the exisitng swale and culvert at DP2.
	3	EXC	11.50	0.36	44.5	4.14	3.17	13.1															Runoff overland flows to existing swale and continues into Basin EXD at DP3.
	4	EXD	21.80	0.36	48.7	7.94	2.94	23.4															Runoff from Basin EXD, overland flows to existing swale at DP4.
	4.1								48.7	12.08	2.94	35.6											Flows from DP3 and DP4 combine at DP2.1 and flows to the west to the existing sediment basin.
	5	EXE	3.96	0.36	31.9	1.43	4.01	5.7															Runoff overland flows across exisitng field to DP5 where flow enters Vollmer Road R.O.W.
	6	EXF	2.58	0.36	25.7	0.93	4.56	4.2															Runoff from Basin EXF overland flows south off-site and enters the adjacent property.
Notes: Street and Pipe C*	A value	es are d	etermir	ned by (	Ω∕i usin	ig the ca	atchme	nt's int	ensity	value.													

Values in BLUE indicate they are from the "Silver Ponds Subdivision Filing No. 1 Final Drainage Report", by IVI.V.E. Inc. revised May 5th, 1996.

#### **COMPOSITE % IMPERVIOUS CALCULATIONS - PROPOSED CONDITIONS**

Subdivision: Schmidt Parcel Location: El Paso County Project Name: Schmidt Parcel-District Infrastructure Project No.: 24013.00 Calculated By: NQJ Checked By: Date: 12/23/24

		Paved	Streets and	l Walks (100	% Imp.)		Apartment	ts (75% Imp.	)	Resid	ential-1	/8 Acre or	Less (65% Imp.)		Undevel	oped (2% Imp.)		Basin	s Total	Basins
Basin ID	Total Area	C₅	C <sub>100</sub>	Area (ac)	Weighted % Imp	C5	C <sub>100</sub>	Area (ac)	Weighted % Imp	C <sub>5</sub>	C <sub>100</sub>	Area (ac)	Weighted %	C <sub>5</sub>	C <sub>100</sub>	Area (ac)	Weighted % Imp	Weig C	hted C	Total Weighter
	(40)				70 mp.				70 mp.								70 mp.	C5	C <sub>100</sub>	weightet
Α	0.25	0.90	0.96	0.00	0.0%	0.45	0.59	0.00	0.0%	0.45	0.59	0.00	0.0%	0.09	0.36	0.25	2.0%	0.09	0.36	2.0%
В	0.09	0.90	0.96	0.00	0.0%	0.45	0.59	0.00	0.0%	0.45	0.59	0.00	0.0%	0.09	0.36	0.09	2.0%	0.09	0.36	2.0%
С	1.12	0.90	0.96	0.00	0.0%	0.45	0.59	1.12	75.0%	0.45	0.59	0.00	0.0%	0.09	0.36	0.00	0.0%	0.45	0.59	75.0%
D	0.73	0.90	0.96	0.58	80.0%	0.45	0.59	0.00	0.0%	0.45	0.59	0.00	0.0%	0.09	0.36	0.15	0.4%	0.74	0.84	80.4%
E	0.39	0.90	0.96	0.32	82.0%	0.45	0.59	0.00	0.0%	0.45	0.59	0.00	0.0%	0.09	0.36	0.07	0.4%	0.75	0.85	82.4%
F	0.48	0.90	0.96	0.40	84.0%	0.45	0.59	0.00	0.0%	0.45	0.59	0.00	0.0%	0.09	0.36	0.08	0.3%	0.77	0.86	84.3%
G	0.84	0.90	0.96	0.69	82.0%	0.45	0.59	0.00	0.0%	0.45	0.59	0.00	0.0%	0.09	0.36	0.15	0.4%	0.75	0.85	82.4%
н	1.29	0.90	0.96	1.06	82.0%	0.45	0.59	0.00	0.0%	0.45	0.59	0.00	0.0%	0.09	0.36	0.23	0.4%	0.75	0.85	82.4%
I	3.46	0.90	0.96	0.00	0.0%	0.45	0.59	3.46	75.0%	0.45	0.59	0.00	0.0%	0.09	0.36	0.00	0.0%	0.45	0.59	75.0%
J	1.15	0.90	0.96	0.92	80.0%	0.45	0.59	0.00	0.0%	0.45	0.59	0.00	0.0%	0.09	0.36	0.23	0.4%	0.74	0.84	80.4%
К	1.20	0.90	0.96	0.96	80.0%	0.45	0.59	0.00	0.0%	0.45	0.59	0.00	0.0%	0.09	0.36	0.24	0.4%	0.74	0.84	80.4%
М	23.90	0.90	0.96	2.00	8.4%	0.45	0.59	21.90	68.7%	0.45	0.59	0.00	0.0%	0.09	0.36	0.00	0.0%	0.49	0.62	77.1%
N	2.98	0.90	0.96	0.30	10.1%	0.45	0.59	0.00	0.0%	0.45	0.59	0.00	0.0%	0.09	0.36	2.68	1.8%	0.17	0.42	11.9%
0	0.22	0.90	0.96	0.18	82.0%	0.45	0.59	0.00	0.0%	0.45	0.59	0.00	0.0%	0.09	0.36	0.04	0.4%	0.75	0.85	82.4%
TOTAL POND (C-N)	37.54																			72.4%
TOTAL (ON-SITE)	38.10																			71.8%

### STANDARD FORM SF-2 - PROPOSED CONDITIONS TIME OF CONCENTRATION

Subdivision: Schmidt Parcel

Location: El Paso County

Project Name: Schmidt Parcel-District Infrastructure

Project No.: 24013.00

Calculated By: NQJ Checked By:

Date: 12/23/24

		SUB-I	BASIN			INITI	AL/OVER	RLAND		Т	RAVEL TIN	IE			tc CHECK		
		DA	<b>ATA</b>				(T <sub>i</sub> )				(T <sub>t</sub> )			(L	JRBANIZED BA	SINS)	FINAL
BASIN	D.A.	Hydrologic	Impervious	C₅	C <sub>100</sub>	L S <sub>o</sub> t <sub>i</sub>			L <sub>t</sub>	<b>S</b> <sub>t</sub>	К	VEL.	t <sub>t</sub>	COMP. t c	TOTAL	Urbanized t <sub>c</sub>	t <sub>c</sub>
ID	(ac)	Soils Group	(%)			(ft)	(%)	(min)	(ft)	(%)		(ft/s)	(min)	(min)	LENGTH (ft)	(min)	(min)
А	0.25	А	2.0%	0.09	0.36	10.0	25.0%	2.0	1030	0.5%	15.0	1.1	16.2	18.2	1040.0	51.8	51.8
В	0.09	А	2.0%	0.09	0.36	10.0	25.0%	2.0	385	0.5%	15.0	1.1	6.0	8.0	395.0	35.4	35.4
С	1.12	А	75.0%	0.45	0.59	85.0	3.0%	7.5	0	0.0%	20.0	0.1	0.0	7.5	85.0	13.3	13.3
D	0.73	А	80.4%	0.74	0.84	36.0	2.0%	3.1	480	1.2%	20.0	2.2	3.7	6.8	516.0	15.9	15.9
E	0.39	А	82.4%	0.75	0.85	36.0	2.0%	3.0	300	1.0%	20.0	2.0	2.5	5.5	336.0	14.4	14.4
F	0.48	А	84.3%	0.77	0.86	36.0	2.0%	2.8	300	1.0%	20.0	2.0	2.5	5.3	336.0	14.1	14.1
G	0.84	А	82.4%	0.75	0.85	42.0	2.0%	3.2	1065	2.5%	20.0	3.2	5.6	8.8	1107.0	17.5	17.5
н	1.29	А	82.4%	0.75	0.85	36.0	2.0%	3.0	1465	2.5%	20.0	3.2	7.7	10.7	1501.0	19.5	19.5
I	3.46	А	75.0%	0.45	0.59	170.0	5.0%	9.0	0	0.0%	20.0	0.1	0.0	9.0	170.0	13.3	13.3
J	1.15	А	80.4%	0.74	0.84	36.0	2.0%	3.1	880	1.7%	20.0	2.6	5.6	8.7	916.0	17.9	17.9
к	1.20	А	80.4%	0.74	0.84	36.0	2.0%	3.1	845	1.7%	20.0	2.6	5.4	8.5	881.0	17.7	17.7
М	23.90	А	77.1%	0.49	0.62	125	6.0%	6.8	1565	1.3%	20.0	2.3	11.4	18.3	1690.0	24.5	24.5
N	2.98	A	11.9%	0.17	0.42	30	25.0%	3.2	390	0.5%	15.0	1.1	6.1	9.3	420.0	32.6	32.6
0	0.22	A	82.4%	0.75	0.85	24	2.0%	2.4	160	2.5%	20.0	3.2	0.8	3.3	184.0	12.8	12.8

#### NOTES:

$t = t \perp t$		$0.395(1.1-C_{c})\sqrt{L_{i}}$		Table 6-2. NRCS Convey	ance factors, K
$i_c = i_i + i_j$	Equation of	$t_i = \frac{1}{S_o^{0.33}}$	Equation 6-3	Type of Land Surface	Conveyance Factor, K
Where:				Heavy meadow	2.5
$t_c = \text{computed time of concentration (minutes)}$		Where:		Tillage/field	5
		t <sub>i</sub> = overland (initial) flow time (minutes)		Short pasture and lawns	7
$t_i$ = overland (initial) flow time (minutes)		$C_5$ = runoff coefficient for 5-year frequency (from Table 6-4)		Nearly bare ground	10
$t_t$ = channelized flow time (minutes).		$S_0$ = average slope along the overland flow path (ft/ft).		Grassed waterway	15
L, L.		L.		Paved areas and shallow paved swales	20
$t_t = \frac{1}{60K\sqrt{S_o}} = \frac{1}{60V_t}$	Equation 6-4	$t_{c} = (26 - 1/i) + \frac{1}{60(14i + 9)\sqrt{S_{t}}}$	Equation 6-5	5	
Where:		Where:			
$t_i$ = channelized flow time (travel time, min) $L_i$ = waterway length (ft) $S_o$ = waterway slope (ft/ft) $V_i$ = travel time velocity (ft/scc) = K $\sqrt{S_o}$ K = NRCS conveysnce factor (see Table 6-2).		$t_c = \min$ mum time of concentration for first design point when les $L_i = \text{length of channelized flow path (ft)}$ $t = \min$ erviousness (expressed as a decimal) $S_i = \text{slope of the channelized flow path (ft/ft)}.$	s than t <sub>c</sub> from Equation 6-1.		

Use a minimum  $t_c$  value of 5 minutes for urbanized areas and a minimum  $t_c$  value of 10 minutes for areas that are not considered urban. Use minimum values even when calculations result in a lesser time of concentration.

#### STANDARD FORM SF-3 - PROPOSED CONDITIONS

STORM DRAINAGE SYSTEM DESIGN

(RATIONAL METHOD PROCEDURE)

Subdivision: Location: Design Storm:	Schmi El Pas	idt Pari o Cour ear	cel hty													Pro I Cale C	ject Na Project culate hecke	ame: t No.: d By: d By: Date:	Schm 2401 NQJ 12/2	nidt Pa 3.00 3/24	arcel-D	istric	t Infrastructure
	1			DIRE	CT RU	NOFF			Т	OTAL	RUNO	FF		STREE	г		PI	PE		TRA	VEL TIP	ИE	
STREET	Design Point	Basin ID	Area (ac)	Runoff Coeff.	t <sub>c</sub> (min)	C*A (ac)	/ (in/hr)	Q (cfs)	tc (min)	C*A (ac)	/ (in/hr)	Q (cfs)	Q <sub>street</sub> (cfs)	C*A (ac)	Slope (%)	Q <sub>pipe</sub> (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	t <sub>t</sub> (min)	REMARKS
	14	OSI4	27.16	0.40	29.2	10.86	4.07	44.2															
	1	A	0.25	0.36	51.8	0.09	2.79	0.3															
	2	в	0.09	0.36	35.4	0.03	3.74	0.12															Existing berm sends off-site flow from north to the east to the exisitng swale and culvert at DP2.
	3	с	1.12	0.59	13.3	0.66	6.22	4.1															BASIN C FLOW @ DP3, C&G FLOW TO DP4
		D	0.73	0.84	15.9	0.61	5.76	3.5															BASIN D FLOW @ DP4
		E	0.39	0.85	14.4	0.33	6.01	2.0															BASIN E FLOW @ DP4
	4								15.9	1.61	5.76	9.2				9.2	1.61	2.0	18	1100	8.8	2.1	COMBINED DP3, BASIN D & BASIN E FLOW @ DP4, CAPTURED IN 5' TYPE R (SUMP), PIPE TO 6.1
	5	F	0.48	0.86	14.1	0.41	6.07	2.5					2.5	0.41	2.5					1100			BASIN 5 FLOW @ DP5, C&G FLOW TO DP6
		G	0.84	0.85	17.5	0.72	5.53	4.0															BASIN G FLOW @ DP6
	6								17.5	1.13	5.53	6.2				6.2	1.13	2.0	18	16	8.0	0.0	COMBINED DP5 & BASIN G FLOW @ DP6, CAPTURED IN 15' TYPE R (ON GRADE PIPE TO DP6.1
	6.1								18.0	2.74	5.45	14.9				14.9	2.74	2.0	18	16	9.6	0.0	COMBINED DP4 & DP6 @ DP6.1, PIPE TO DP7.1
	7	н	1.29	0.85	19.5	1.10	5.25	5.8								5.8	1.10	2.0	18	0	7.9	0.0	BASIN H FLOW @ DP7, CAPTURED IN 15' TYPE R (ON GRADE), PIPE TO DP7.1
	7.1								19.5	3.84	5.25	20.1				20.1	3.84	2.0	24	63	10.8	0.1	COMBINED DP6.1 & DP7 FLOW @ DP7.1, PIPE TO DP14 (POND)
	8	1	3.46	0.59	13.3	2.04	6.22	12.7								12.7	2.04	2.0	18	26	9.4	0.0	BASIN I FLOW CAPTURED @ DP8, PIPE TO DP9.1
	9	L	1.15	0.84	17.9	0.97	5.47	5.3															BASIN J CAPTURED @ DP9 IN 5' TYPE R (SUMP), PIPE TO DP9.1
	9.1								17.9	3.01	5.47	16.4				16.4	3.01	2.0	24	84	10.2	0.1	COMBINED DP8 & DP9 @ DP9.1, PIPE TO DP10.1
	10	к	1.20	0.84	17.7	1.01	5.50	5.5															BASIN K CAPTURED @ DP10 IN 5' TYPE R (SUMP), PIPE TO DP10.1
	10.1								17.9	4.02	5.47	22.0				22.0	4.02	2.0	24	1272	10.9	1.9	COMBINED DP9.1 & DP10 @ DP10.1, PIPE TO DP13.1
	13	м	23.90	0.62	24.5	14.84	4.68	69.4															BASIN 13 FLOWS CAPTURED @ DP13, PIPE TO DP13.1
	13.1								24.5	18.86	4.68	88.2				88.2	18.86	2.0	36	34	15.2	0.0	COMBINED DP10.1 & DP13 FLOW @ DP13.1, PIPE TO DP14
	14	N	2.98	0.42	32.6	1.25	3.95	5.0	32.6	23.94	3.95	94.7											COMBINED DP7.1, DP13.1 & BASIN N COMBINED @ DP14
	15	0	0.22	0.85	12.8	0.19	6.31	1.2															BASIN O FLOW @ DP15, C&G FLOW OFFSITE IN BRUSH TOP ROAD

Notes: Street and Pipe C\*A values are determined by Q/i using the catchment's intensity value.

#### STANDARD FORM SF-3 - PROPOSED CONDITIONS

STORM DRAINAGE SYSTEM DESIGN

(RATIONAL METHOD PROCEDURE)

Subdivision: Location: Design Storm:	Schmi El Pas 5-Yea	dt Par o Cour r	cel hty													Pro I Cal C	ject Na Project culate hecke	ame: t No.: d By: d By:	Schm 2401 NQJ	idt Par 3.00	rcel-Di	strict	Infrastructure
																		Jate:	12/2	5/24			
				DIR	ECTRU	NOFF				OTAL	RUNO	-+		STREE			PI	PE	()	TRAV	EL TIN	IE	
STREET	Design Point	Basin ID	Area (Ac)	Runoff Coeff.	t <sub>c</sub> (min)	C*A (Ac)	/ (in/hr)	Q (cfs)	tc (min)	C*A (ac)	/ (in/hr)	Q (cfs)	Q <sub>street</sub> (cfs)	C*A (ac)	Slope (%)	Q <sub>pipe</sub> (cfs)	C*A (ac)	Slope (%)	Pipe Size (inche	Length (ft)	Velocity (fps)	$t_t$ (min)	REMARKS
	14	OSI4	27.16	0.30	29.2	8.15	2.33	19.0															Off-site Basin OSI4 Values from Sliver Pond FDR (Bains I4 & DP21)
	1	А	0.25	0.09	51.8	0.02	1.66	0.04															Existing berm sends off-site flow from north to the west to the existing swale at DP1.
	2	в	0.09	0.09	35.4	0.01	2.23	0.02															Existing berm sends off-site flow from north to the east to the exisitng swale and culvert at DP2.
	3	с	1.12	0.45	13.3	0.50	3.71	1.9															BASIN C FLOW @ DP3, C&G FLOW TO DP4
		D	0.73	0.74	15.9	0.54	3.43	1.8															BASIN D FLOW @ DP4
		Е	0.39	0.75	14.4	0.29	3.58	1.1															BASIN E FLOW @ DP4
	4								15.9	1.34	3.43	4.6				4.6	1.34	2.0	18	1100	7.3	2.5	COMBINED DP3, BASIN D & BASIN E FLOW @ DP4, CAPTURED IN 5' TYPE R (SUMP), PIPE TO 6.1
	5	F	0.48	0.77	14.1	0.37	3.62	1.3					1.3	0.37	2.5					1100			BASIN 5 FLOW @ DP5, C&G FLOW TO DP6
		6	0.84	0.75	17.5	0.63	3 29	2.1															BASIN G FLOW @ DP6
	6	0	0.04	0.75	17.5	0.05	5.25		17.5	1.00	3.29	3.3				3.3	1.00	2.0	18	16	6.6	0.0	COMBINED DP5 & BASIN G FLOW @ DP6, CAPTURED IN 15' TYPE R (ON GRADE), PIPE TO DP6.1
	6.1								18.5	2.34	3.21	7.5				7.5	2.34	2.0	18	16	8.4	0.0	COMBINED DP4 & DP6 @ DP6.1, PIPE TO DP7.1
	7	н	1.29	0.75	19.5	0.97	3.13	3.0								3.0	0.97	2.0	18	0	6.6	0.0	BASIN H FLOW @ DP7, CAPTURED IN 15' TYPE R (ON GRADE), PIPE TO DP7.1
	7.1								19.5	3.31	3.13	10.4				10.4	3.31	2.0	24	63	9.0	0.1	COMBINED DP6.1 & DP7 FLOW @ DP7.1, PIPE TO DP14 (POND)
	8	-	3.46	0.45	13.3	1.56	3.71	5.8								5.8	1.56	2.0	18	26	7.9	0.1	BASIN I FLOW CAPTURED @ DP8, PIPE TO DP9.1
	9	J	1.15	0.74	17.9	0.85	3.26	2.8															BASIN J CAPTURED @ DP9 IN 5' TYPE R (SUMP), PIPE TO DP9.1
	9.1								17.9	2.41	3.26	7.8				7.8	2.41	2.0	24	84	8.3	0.2	COMBINED DP8 & DP9 @ DP9.1, PIPE TO DP10.1
	10	к	1.20	0.74	17.7	0.89	3.28	2.9															BASIN K CAPTURED @ DP10 IN 5' TYPE R (SUMP), PIPE TO DP10.1
	10.1								17.9	3.29	3.26	10.7				10.7	3.29	2.0	24	1272	9.1	2.3	COMBINED DP9.1 & DP10 @ DP10.1, PIPE TO DP13.1
	13	м	23.90	0.49	24.5	11.66	2.79	32.5															BASIN 13 FLOWS CAPTURED @ DP13, PIPE TO DP13.1
	13.1								24.5	14.95	2.79	41.7				41.7	14.95	2.0	36	34	12.9	0.0	COMBINED DP10.1 & DP13 FLOW @ DP13.1, PIPE TO DP14
	14	N	2.98	0.17	32.6	0.51	2.36	1.2	32.6	18.77	2.36	44.2											COMBINED DP7.1, DP13.1 & BASIN N COMBINED @ DP14
	15	о	0.22	0.75	12.8	0.17	3.76	0.6															BASIN O FLOW @ DP15, C&G FLOW OFFSITE IN BRUSH TOP ROAD

Notes: Street and Pipe C\*A values are determined by Q/i using the catchment's intensity value.



## **APPENDIX C – HYDRAULIC CALCULATIONS**

#### MHFD-Inlet, Version 5.03 (August 2023)

### INLET MANAGEMENT

Worksheet Protected

INLET NAME	DP4	<u>DP6</u>	<u>DP7</u>
Site Type (Urban or Rural)	URBAN	URBAN	URBAN
Inlet Application (Street or Area)	STREET	STREET	STREET
Hydraulic Condition	In Sump	On Grade	On Grade
Inlet Type	CDOT Type R Curb Opening	CDOT Type R Curb Opening	CDOT Type R Curb Opening

#### **USER-DEFINED INPUT**

User-Defined Design Flows			
Minor Q <sub>Known</sub> (cfs)	4.6	3.3	3.0
Major Q <sub>Known</sub> (cfs)	9.2	6.2	5.8

#### Bypass (Carry-Over) Flow from Upstream Inlets must be organized from upstream (left) to downstream (right) in order for bypass flows to be linked.

Receive Bypass Flow from:	No Bypass Flow Received	No Bypass Flow Received	No Bypass Flow Received
Minor Bypass Flow Received, Q <sub>b</sub> (cfs)	0.0	0.0	0.0
Major Bypass Flow Received, Q <sub>b</sub> (cfs)	0.0	0.0	0.0

#### Watershed Characteristics

Subcatchment Area (acres)		
Percent Impervious		
NRCS Soil Type		

#### **Watershed Profile**

Overland Slope (ft/ft)		
Overland Length (ft)		
Channel Slope (ft/ft)		
Channel Length (ft)		

#### Minor Storm Rainfall Input

Design Storm Return Period, T <sub>r</sub> (years)		
One-Hour Precipitation, P <sub>1</sub> (inches)		

#### **Major Storm Rainfall Input**

Design Storm Return Period, T <sub>r</sub> (years)		
One-Hour Precipitation, P <sub>1</sub> (inches)		

#### CALCULATED OUTPUT

Minor Total Design Peak Flow, Q (cfs)	4.6	3.3	3.0
Major Total Design Peak Flow, Q (cfs)	9.2	6.2	5.8
Minor Flow Bypassed Downstream, Q <sub>b</sub> (cfs)	N/A	0.0	0.0
Major Flow Bypassed Downstream, Qb (cfs)	N/A	0.0	0.0

### MHFD-Inlet, Version 5.03 (August 2023)

## INLET MANAGEMENT

Worksheet Protected

INLET NAME	DP9	<u>DP10</u>
Site Type (Urban or Rural)	URBAN	URBAN
Inlet Application (Street or Area)	STREET	STREET
Hydraulic Condition	In Sump	In Sump
Inlet Type	CDOT Type R Curb Opening	CDOT Type R Curb Opening

#### USER-DEFINED INPUT

User-Defined Design Flows					
Minor Q <sub>Known</sub> (cfs)	7.8	2.9			
Major Q <sub>Known</sub> (cfs)	16.4	5.5			
Bypass (Carry-Over) Flow from Upstream					
Receive Bypass Flow from:	No Bypass Flow Received	No Bypass Flow Received			
Minor Bypass Flow Received, Q <sub>b</sub> (cfs)	0.0	0.0			
Major Bypass Flow Received, Q <sub>b</sub> (cfs)	0.0	0.0			
Watershed Characteristics					
Subcatchment Area (acres)					
Percent Impervious					
NRCS Soil Type					
Watershed Profile					
Overland Slope (ft/ft)					
Overland Length (ft)					
Channel Slope (ft/ft)					
Channel Length (ft)					
	-				
Minor Storm Rainfall Input					
Design Storm Return Period, T <sub>r</sub> (years)					
One-Hour Precipitation, P <sub>1</sub> (inches)					
·	~·				
Major Storm Rainfall Input					

Major Storm Kannan Input	
Design Storm Return Period, T <sub>r</sub> (years)	
One-Hour Precipitation, $P_1$ (inches)	

#### CALCULATED OUTPUT

Minor Total Design Peak Flow, Q (cfs)	7.8	2.9
Major Total Design Peak Flow, Q (cfs)	16.4	5.5
Minor Flow Bypassed Downstream, Q <sub>b</sub> (cfs)	N/A	N/A
Major Flow Bypassed Downstream, Q <sub>b</sub> (cfs)	N/A	N/A



# INLET IN A SUMP OR SAG LOCATION MHFD-Inlet, Version 5.03 (August 2023)





Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	]
Local Depression (additional to continuous gutter depression 'a' from above)	a <sub>local</sub> =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	6.0	9.7	inches
Grate Information		MINOR	MAJOR	Override Depths
Length of a Unit Grate	$L_{o}(G) =$	N/A	N/A	feet
Width of a Unit Grate	W <sub>o</sub> =	N/A	N/A	feet
Open Area Ratio for a Grate (typical values 0.15-0.90)	A <sub>ratio</sub> =	N/A	N/A	1
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_{f}(G) =$	N/A	N/A	1
Grate Weir Coefficient (typical value 2.15 - 3.60)	C <sub>w</sub> (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	$C_{o}(G) =$	N/A	N/A	1
Curb Opening Information	-	MINOR	MAJOR	-
Length of a Unit Curb Opening	$L_0(C) = $	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H <sub>vert</sub> =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H <sub>throat</sub> =	6.00	6.00	inches
Angle of Throat	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W <sub>p</sub> =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_{f}(C) =$	0.10	0.10	1
Curb Opening Weir Coefficient (typical value 2.3-3.7)	C <sub>w</sub> (C) =	3.60	3.60	1
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	ι <sub>ο</sub> (ι.) =	0.67	0.67	
Low Hood Performance Peduction (Calculated)		MINOD	MAIOD	
Double for Crote Midwidth	L او	MINUR	MAJOR	ام
Depth for Grate Midwidth	u <sub>Grate</sub> =	N/A	N/A	π A
Depth for Curb Opening Weir Equation	a <sub>Curb</sub> =	0.38	0.68	π
Grated Iniet Performance Reduction Factor for Long Iniets	RF <sub>Grate</sub> =	N/A	N/A	-
Curb Opening Performance Reduction Factor for Long Inlets	RF <sub>Curb</sub> =	1.00	1.00	-
Combination Inlet Performance Reduction Factor for Long Inlets	$RF_{Combination} = $	N/A	N/A	
		MINOR	MAIOR	
Total Inlet Interception Capacity (assumes clogged condition)	<b>Q</b> <sub>a</sub> = [	6.4	11.0	cfs
Inlet Capacity IS GOOD for Minor and Major Storms (>Q Peak)	Q PEAK REQUIRED =	4.6	9.2	cfs




Design Information (Input)		MINOR	MAJOR	_
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a <sub>LOCAL</sub> =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	3	3	
Length of a Single Unit Inlet (Grate or Curb Opening)	L <sub>o</sub> =	5.00	5.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	$W_o =$	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	$C_f(G) =$	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	$C_{f}(C) =$	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity		MINOR	MAJOR	_
Total Inlet Interception Capacity	Q =	3.3	6.2	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	$Q_b =$	0.0	0.0	cfs
Capture Percentage = $Q_a/Q_o$	C% =	100	100	%





Design Information (Input)		MINOR	MAJOR	_
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a <sub>LOCAL</sub> =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	3	3	
Length of a Single Unit Inlet (Grate or Curb Opening)	L <sub>o</sub> =	5.00	5.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	$W_o =$	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	$C_f(G) =$	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	$C_{f}(C) =$	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity		MINOR	MAJOR	_
Total Inlet Interception Capacity	Q =	3.0	5.8	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	$Q_b =$	0.0	0.0	cfs
Capture Percentage = $Q_a/Q_o$	C% =	100	100	%



## INLET IN A SUMP OR SAG LOCATION MHFD-Inlet, Version 5.03 (August 2023)





Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a <sub>local</sub> =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	2	2	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	6.0	9.7	inches
Grate Information		MINOR	MAJOR	Override Depths
Length of a Unit Grate	$L_{0}(G) =$	N/A	N/A	feet
Width of a Unit Grate	W <sub>o</sub> =	N/A	N/A	feet
Open Area Ratio for a Grate (typical values 0.15-0.90)	A <sub>ratio</sub> =	N/A	N/A	1
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_{f}(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C <sub>w</sub> (G) =	N/A	N/A	1
Grate Orifice Coefficient (typical value 0.60 - 0.80)	$C_{0}(G) =$	N/A	N/A	1
Curb Opening Information	-	MINOR	MAJOR	-
Length of a Unit Curb Opening	$L_{o}(C) = $	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H <sub>vert</sub> =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H <sub>throat</sub> =	6.00	6.00	inches
Angle of Throat	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W <sub>p</sub> =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_{f}(C) =$	0.10	0.10	1
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_{w}(C) =$	3.60	3.60	1
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_0(C) =$	0.67	0.67	
	-			-
Low Head Performance Reduction (Calculated)	-	MINOR	MAJOR	-
Depth for Grate Midwidth	d <sub>Grate</sub> =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d <sub>Curb</sub> =	0.38	0.68	ft
Grated Inlet Performance Reduction Factor for Long Inlets	RF <sub>Grate</sub> =	N/A	N/A	
Curb Opening Performance Reduction Factor for Long Inlets	RF <sub>Curb</sub> =	0.93	1.00	
Combination Inlet Performance Reduction Factor for Long Inlets	RF <sub>Combination</sub> =	N/A	N/A	
	0 -1	MINOR	MAJOR	ofe
Total Inlet Interception Capacity (assumes clogged condition)		7.9	16.4	LIS ofc
Inlet Capacity IS GOOD for Minor and Major Storms (>Q Peak)	✓ PEAK REQUIRED =	7.0	10.4	lus



## INLET IN A SUMP OR SAG LOCATION MHFD-Inlet, Version 5.03 (August 2023)





Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	]
Local Depression (additional to continuous gutter depression 'a' from above)	a <sub>local</sub> =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	6.0	9.7	inches
Grate Information		MINOR	MAJOR	Override Depths
Length of a Unit Grate	$L_{0}(G) =$	N/A	N/A	feet
Width of a Unit Grate	W <sub>o</sub> =	N/A	N/A	feet
Open Area Ratio for a Grate (typical values 0.15-0.90)	A <sub>ratio</sub> =	N/A	N/A	1
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_{f}(G) =$	N/A	N/A	1
Grate Weir Coefficient (typical value 2.15 - 3.60)	C <sub>w</sub> (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	$C_{0}(G) =$	N/A	N/A	1
Curb Opening Information	-	MINOR	MAJOR	-
Length of a Unit Curb Opening	L <sub>0</sub> (C) =	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H <sub>vert</sub> =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H <sub>throat</sub> =	6.00	6.00	inches
Angle of Throat	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W <sub>p</sub> =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_{f}(C) =$	0.10	0.10	1
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_{w}(C) =$	3.60	3.60	1
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_{0}(C) =$	0.67	0.67	
	-			-
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	-
Depth for Grate Midwidth	d <sub>Grate</sub> =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d <sub>Curb</sub> =	0.38	0.68	ft
Grated Inlet Performance Reduction Factor for Long Inlets	RF <sub>Grate</sub> =	N/A	N/A	
Curb Opening Performance Reduction Factor for Long Inlets	RF <sub>Curb</sub> =	1.00	1.00	
Combination Inlet Performance Reduction Factor for Long Inlets	RF <sub>Combination</sub> =	N/A	N/A	
	0 -	MINOR	MAJOR	] <b>. f</b> a
Total Inlet Interception Capacity (assumes clogged condition)		0.4	11.0	cis
Inlet Capacity IS GOOD for Minor and Major Storms (>Q Peak)	✓ PEAK REQUIRED -	2.9	5.5	us

Please put pond component hydraulic analyses in the next appendix with the rest of the pond calcs. Typical comment.

Pond A Spillway Inlet (Single Type C Grate)						
	Orifice Flow Calculation					
Q = C*A* s	quare root	(2gH)				
C = 0.6		A = 8.53 so	q ft	g = 32.2		
Head (ft)	CA	(2GH)	Sqrt (2GH)	Capacity		
1	5.118	64.40	8.025	41.1		
2	5.118	128.80	11.349	58.1		
3	5.118	193.20	13.900	71.1		
4	5.118	257.60	16.050	82.1		
5	5.118	322.00	17.944	91.8		
6	5.118	386.40	19.657	100.6		

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

### Pond A - Emergency Overflow Pipe (Q100 = 41.1 cfs)

Circular		Highlighted	
Diameter (ft)	= 3.00	Depth (ft) =	2.22
		Q (cfs) =	41.10
		Area (sqft) =	5.62
Invert Elev (ft)	= 1.00	Velocity (ft/s) =	7.31
Slope (%)	= 0.47	Wetted Perim (ft) =	6.23
N-Value	= 0.013	Crit Depth, Yc (ft) =	2.09
		Top Width (ft) =	2.63
Calculations		EGL (ft) =	3.05
Compute by:	Known Q		
Known Q (cfs)	= 41.10		





Project: Schmidt Phase 1 - District Infrastructure Project No: 24013 12/24/2024

Forebay #1 Sizing					
(Per USDCM Volume 3, Table 4-12)					
WQCV	WOCV	Forebay	Forebay	Forebay	
(ac-ft)	/ft <sup>3</sup> )	Area (ft <sup>2</sup> )	Depth (ft)	Volume (ft <sup>3</sup> )	
0.085	37.16	137.5	1.5	206.25	

Forebay Notch Sizing				
(Per USDCM Volume 3 Equation 4-1)				
w=9.23( $A_{FB}$ /t)(1/sqrt( $h_{max}$ ))				
$A_{FB}$ (ft <sup>2</sup> )	t (s)	h <sub>max</sub> (ft)	w (in)	
137.5	240	1.5	4.32	

Forebay #2 Sizing					
(Per USDCM Volume 3, Table 4-12)					
	44(14)001(43)	Forebay Area	Forebay Depth	Forebay	
WQCV (ac-it)	1% WQCV (π.)	(ft <sup>2</sup> )	(ft)	Volume (ft <sup>3</sup> )	
0.768	334.41	269.5	1.5	404.25	

Forebay Notch Sizing			
(Per USDCM Volume 3 Equation 4-1)			
w=9.23( $A_{FB}/t$ )(1/sqrt( $h_{max}$ ))			
$A_{FB}$ (ft <sup>2</sup> )	t (s)	h <sub>max</sub> (ft)	w (in)
269.5	240	1.5	8.46

Riprap Sizing - Pond A Spillway					
q (cfs/ft)	S (ft/ft)	C <sub>f</sub>	п	D <sub>50</sub> min. (in)	
2.981	0.20	2	0	8.42	

Type L Riprap (D<sub>50</sub> = 9") will be utilized for spillway protection

 $D_{50} = 5.23 \ S^{0.43} \ (1.35 \, C_{\rm f} \, q)^{0.56}$ 

Where:

 $D_{5\theta}$ median rock size (in) =

S= longitudinal slope (ft/ft)  $C_f$ 

= concentration factor (1.0 to 3.0)

unit discharge (cfs/ft) q=

When:

 $\eta$  (porosity) = 0.0 (i.e., for buried soil riprap)

### **Channel Report**

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Thursday, Aug 1 2024

### Trickle Channel (Q = 1% of 100-Year Peak Inflow = 9.24 cfs)

CDs detail this as 6'		
bottom width. Please	Highlighted	
= 5.67 <sup>2</sup> adjust to match	Depth (ft)	= 0.41
= 0.50	Q (cfs)	= 9.240
	Area (sqft)	= 2.32
= 7000.00	Velocity (ft/s)	= 3.97
= 0.50	Wetted Perim (ft)	= 6.49
= 0.013	Crit Depth, Yc (ft)	= 0.44
	Top Width (ft)	= 5.67
	EGL (ft)	= 0.66
Known Q		
= 9.24		
	<pre>CDs detail this as 6' bottom width. Please adjust to match = 0.50 = 7000.00 = 0.50 = 0.013 Known Q = 9.24</pre>	CDs detail this as 6' bottom width. Please adjust to matchHighlighted Depth (ft) Q (cfs) Area (sqft)= 7000.00Velocity (ft/s)= 0.50Wetted Perim (ft) Crit Depth, Yc (ft) Top Width (ft) EGL (ft)Known Q = 9.249.24



Reach (ft)

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

### FOREBAY #1 NOTCH: Q = 2% OF 100-YEAR PEAK FLOW (DP7.1) = 0.388 cfs

Rectangular Weir		Highlighted	
Crest	= Sharp	Depth (ft)	= 0.60
Bottom Length (ft)	= 0.25	Q (cfs)	= 0.390
Total Depth (ft)	= 1.50	Area (sqft)	= 0.15
		Velocity (ft/s)	= 2.59
Calculations		Top Width (ft)	= 0.25
Weir Coeff. Cw	= 3.33		
Compute by:	Known Q		
Known Q (cfs)	= 0.39		



Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

### FOREBAY #2 NOTCH: Q = 2% OF 100-YEAR PEAK FLOW (DP13.1) = 1.676 cfs

Rectangular Weir		Highlighted	
Crest	= Sharp	Depth (ft)	= 1.33
Bottom Length (ft)	= 0.33	Q (cfs)	= 1.676
Total Depth (ft)	= 1.50	Area (sqft)	= 0.44
		Velocity (ft/s)	= 3.83
Calculations		Top Width (ft)	= 0.33
Weir Coeff. Cw	= 3.33		
Compute by:	Known Q		
Known Q (cfs)	= 1.68		



### **Channel Report**

Include ready over a logification.	
Include Toadway classification	Tuesday, Aug 00 2000
Hydranow Express Extension for Autodeskee for added clarity	Tuesday, Aug 22 2023

### Brushtop Road-Emergency Overflow

User-defined		Highlighted	
Invert Elev (ft)	= 6998.49	Depth (ft)	= 0.60
Slope (%)	= 3.00	Q (cfs)	= 55.00
N-Value	= 0.019	Area (sqft)	= 11.04
		Velocity (ft/s)	= 4.98
Calculations		Wetted Perim (ft)	= 45.86
Compute by:	Known Q	Crit Depth, Yc (ft)	= 0.65
Known Q (cfs)	= 55.00	Top Width (ft)	= 45.02
		EGL (ft)	= 0.99

(Sta, El, n)-(Sta, El, n)... (0.00, 6999.14) -(7.50, 6998.99, 0.030) -(8.00, 6998.99, 0.013) -(8.10, 6998.49, 0.013) -(10.00, 6998.66, 0.016) -(25.00, 6998.96, 0.016) -(40.00, 6998.66, 0.016) -(41.90, 6998.49, 0.013) -(42.00, 6998.99, 0.013) -(42.50, 6998.99, 0.013) -(50.00, 6999.14, 0.030)

. . . . . .



### **Channel Report**

#### Hydraflow Express Extension for Autodesk® Cin Include roadway classification for added clarity

Wednesday, Aug 16 2023

### Vanderwood Road-Emergency Overflow

User-defined		Highlighted	
Invert Elev (ft)	= 6994.52	Depth (ft)	= 0.64
Slope (%)	= 1.10	Q (cfs)	= 55.00
N-Value	= 0.020	Area (sqft)	= 15.46
		Velocity (ft/s)	= 3.56
Calculations		Wetted Perim (ft)	= 49.21
Compute by:	Known Q	Crit Depth, Yc (ft)	= 0.65
Known Q (cfs)	= 55.00	Top Width (ft)	= 49.02
		EGL (ft)	= 0.84

(Sta, El, n)-(Sta, El, n)... (0.00, 6995.17) -(7.50, 6995.02, 0.030) -(7.75, 6995.02, 0.013) -(9.17, 6994.52, 0.013) -(10.00, 6994.60, 0.016) -(25.00, 6994.90, 0.016) -(40.00, 6994.60, 0.016) -(40.83, 6994.52, 0.013) -(42.25, 6995.02, 0.013) -(42.50, 6995.02, 0.013) -(50.00, 6995.17, 0.030)



Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

### Pond A Outfall Channel (Q100 = 41.1 cfs)

#### Trapezoidal

Bottom Width (ft) Side Slopes (z:1) Total Depth (ft) Invert Elev (ft) Slope (%) N-Value

#### = 15.00 = 4.00, 4.00= 2.25 = 1.00 = 0.59= 0.030

#### Calculations

Compute by: Known Q (cfs) Known Q = 41.10

How was the flow calculated? There appears to be additional flow tributary to the proposed channel that may not be accounted for (there is no watershed area delineated)

#### Highlighted

Depth (ft)	=	0.79
Q (cfs)	=	41.10
Area (sqft)	=	14.35
Velocity (ft/s)	=	2.86
Wetted Perim (ft)	=	21.51
Crit Depth, Yc (ft)	=	0.59
Top Width (ft)	=	21.32
EGL (ft)	=	0.92

FROUDE # = (2.86 FT/S) / SQRT(32.2 FT/S^2 x 0.59 FT) = 0.66

FLOW IS NON-EROSIVE, CHANNEL WILL BE UNLINED.



Tuesday, Dec 24 2024





Line No.	Vel Ave	Flow Rate	Line Size	Line Length	Invert Up	Invert Dn	Line Slope	Чр Цр	HGL	n-val Pipe	J-Loss Coeff		
	(ft/s)	(cfs)	(ii)	(tt)	(tt)	(II)	(%)	(ft)	(ft)				
-	6.14	41.70	42	33.720	6999.89	6999.21	2.02	7001.90 j	7002.06	0.013	1.00 z		
Ν	5.32	10.70	30	216.086	7001.97	7000.89	0.50	7003.06	7001.94	0.013	0.37 z		
ო	5.44	10.70	24	140.702	7003.17	7002.47	0.50	7004.37	7003.67	0.013	0.15		
4	5.46	10.70	24	207.911	7004.31	7003.27	0.50	7005.51	7004.47	0.013	0.84		
ъ	5.87	10.70	24	600.000	7013.80	7004.81	1.50	7014.97	7005.90	0.013	0.15 z		
9	5.82	10.70	24	128.870	7014.74	7013.90	0.65	7015.91	7015.00	0.013	0.50 z		
7	4.78	7.80	24	88.356	7015.48	7014.84	0.72	7016.47 j	7015.91	0.013	1.50 z		
Ø	4.62	5.80	24	90.467	7016.23	7015.78	0.50	7017.08	7016.61	0.013	0.79 z		
თ	5.26	5.80	24	25.656	7016.78	7016.53	0.97	7017.63	7017.23	0.013	1.00 z		
10	5.05	10.40	24	68.100	6998.49	6997.71	1.15	6999.65 j	6999.07	0.013	0.50 z		
1	4.71	7.50	24	11.910	6998.71	6998.59	1.01	( 89.6669	6999.65	0.013	1.00 z		
12	4.60	3.30	18	32.420	6999.50	6999.21	0.89	7000.19	6999.81	0.013	1.00 z		
13	6.27	4.60	18	289.870	7006.16	6999.21	2.40	7006.98	6999.76	0.013	0.29 z		
14	5.63	4.60	18	209.750	7011.39	7006.36	2.40	7012.21	7006.98	0.013	0.48 z		
15	5.63	4.60	18	293.990	7018.65	7011.59	2.40	7019.47	7012.21	0.013	0.31 z		
16	5.63	4.60	18	208.120	7023.35	7018.85	2.16	7024.17	7019.47	0.013	0.75 z		
17	4.90	4.60	18	121.930	7024.57	7023.65	0.75	7025.39	7024.40	0.013	1.00 z		
18	0.16	1.10	36	115.236	6994.31	6993.74	0.49	7019.84	7019.84	0.013	0.50		
19	0.62	1.10	18	44.289	6996.03	6995.81	0.50	7019.85	7019.84	0.013	1.00		
Schmi	dt - Dist	trict									_	Number of lines: 19	Date: 12/24/2024
NOTE	5: ** Cri	tical dept	th									_	

Page 1





Proj. file: Storm\_5.stm



Proj. file: Storm\_5.stm

	•												
Line No.	Vel Ave	Flow Rate	Line Size	Line Length	Invert Up	Invert Dn	Line Slope	ЧGL Ир	HGL	n-val Pipe	J-Loss Coeff		
	(ft/s)	(cfs)	(ii)	( <b>t</b> t)	(#)	(tt)	(%)	(tt)	(ft)				
-	10.41	88.20	42	33.720	6999.89	6999.21	2.02	7002.81	7002.06	0.013	1.00 z		
N	6.06	22.00	30	216.086	7001.97	7000.89	0.50	7003.56	7002.81	0.013	0.37 z		
ო	7.00	22.00	24	140.702	7003.17	7002.47	0.50	7005.80	7004.47	0.013	0.15		
4	7.00	22.00	24	207.911	7004.31	7003.27	0.50	7007.89	7005.92	0.013	0.84		
5ı	7.42	22.00	24	600.000	7013.80	7004.81	1.50	7015.47 j	7008.53	0.013	0.15 z		
Q	7.00	22.00	24	128.870	7014.74	7013.90	0.65	7017.12	7015.90	0.013	0.50		
7	5.22	16.40	24	88.356	7015.48	7014.84	0.72	7017.97	7017.50	0.013	1.50		
ω	4.04	12.70	24	90.467	7016.23	7015.78	0.50	7018.89	7018.60	0.013	0.79		
თ	4.04	12.70	24	25.656	7016.78	7016.53	0.97	7019.17	7019.09	0.013	1.00		
10	8.02	20.10	24	68.100	6998.49	6997.71	1.15	7000.10	6999.10	0.013	0.50 z		
11	5.87	14.00	24	11.910	6998.71	6998.59	1.01	7000.06 j	7000.10	0.013	1.00 z		
12	5.56	6.20	18	32.420	6999.50	6999.21	0.89	7000.46	7000.07	0.013	1.00 z		
13	7.58	9.20	18	289.870	7006.16	6999.21	2.40	7007.33	7000.06	0.013	0.29 z		
14	6.90	9.20	18	209.750	7011.39	7006.36	2.40	7012.56	7007.33	0.013	0.48 z		
15	6.90	9.20	18	293.990	7018.65	7011.59	2.40	7019.82	7012.56	0.013	0.31 z		
16	6.90	9.20	18	208.120	7023.35	7018.85	2.16	7024.52	7019.82	0.013	0.75 z		
17	5.88	9.20	18	121.930	7024.57	7023.65	0.75	7025.81	7024.89	0.013	1.00		
18	6.37	45.00	36	115.236	6994.31	6993.74	0.49	7020.37	7019.84	0.013	0.50		
19	9.39	16.60	18	44.289	6996.03	6995.81	0.50	7021.79	7020.68	0.013	1.00		
Schmi	dt - Dist	rict							-		_	Number of lines: 19	Date: 12/24/2024
NOTE	5: ** Cri	ical dept											

Page 1

100-yr





Proj. file: Storm\_100.stm

![](_page_58_Figure_1.jpeg)

![](_page_58_Figure_2.jpeg)

Proj. file: Storm\_100.stm

![](_page_59_Picture_0.jpeg)

### **APPENDIX D – WATER QUALITY & DETENTION**

#### DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.06 (July 2022)

#### Project: Schmidt Phase 1 - District Infrastructure Basin ID: Pond A ZONE 3 ZONE 2 ZONE 1 100-YEAR

		<u>B</u>					1							
ZONE	1 AND 2	ORIFICE	1		Depth Increment =		ft							
PERMANENT ORIFIC	ES		- Berrell				Optional			4.000	Optional		Valuma	
Example Zone G	configuratio	n (Retentio	n Pona)		Stage - Storage	Stage (#)	Override Stogo (#)	Length	Width (A)	(# <sup>2</sup> )	Aron (ft <sup>2</sup> )	Area (acro)	(0 3)	Volume
Watershed Information					Top of Micropool	(11)		(11)	(it)	(11)	Area (IL)	(acre)	(11)	(dC-IL)
watersneu information		1		6996.53	тор от місторооі		0.00				10	0.000		
Selected BMP Type =	EDB				6997		0.47				110	0.003	28	0.001
Watershed Area =	37.54	acres			6998		1.47				6,291	0.144	3,229	0.074
Watershed Length =	2,710	ft			6999		2.47				24,681	0.567	18,714	0.430
Watershed Length to Centroid -	1 260	e la			7000		3.47				42.835	0.083	52 472	1 205
Watershed Clans -	1,200	A/A			7000		4.47				F1 000	1 101	00.026	2 202
watersned slope =	0.025				7001		4.4/				51,092	1.191	99,030	2.292
Watershed Imperviousness =	/3.00%	percent			7002		5.4/				58,705	1.348	155,134	3.561
Percentage Hydrologic Soil Group A =	100.0%	percent			7003		6.47				62,845	1.443	215,909	4.957
Percentage Hydrologic Soil Group B =	0.0%	percent			7004		7.47				67,648	1.553	281,156	6.454
Percentage Hydrologic Soil Groups C/D =	0.0%	percent			7004.5		7.97				69,716	1.600	315,497	7.243
Target WOCV Drain Time =	40.0	hours			7005		8.47				72,420	1.663	351.031	8.059
Location for 1-br Rainfall Donths -	Licor Input	]			7006-Top		0.47				77 107	1 772	425 920	0.776
	osci input				7000-100		5.47				77,157	1.772	123,035	5.770
After providing required inputs above inc	luding 1-hour	rainfall											<u> </u>	
depths, click 'Run CUHP' to generate run the embedded Celevade Listen Hude	off hydrograph	s using											L	
the embedded Colorado Urban Hydro	graph Procedu	ire.	Optional Use	r Overrides										
Water Quality Capture Volume (WQCV) =	0.905	acre-feet		acre-feet										
Excess Urban Runoff Volume (EURV) =	3.513	acre-feet		acre-feet										
2-vr Pupoff Volume (P1 = 0.95 in ) =	1 992	acre-feet	0.95	inches										
2 yr Rafol Volume (P1 = 0.55 m.) =	2.001	dere leet	0.55	linenes									<b>├</b> ─────┘	
5-yi Kunon volume (P1 = 1.23 IR.) =	2.001	acresieer	1.25										<b>├</b> ────'	
10-yr Runoff Volume (P1 = 1.48 in.) =	3.287	acre-feet	1.48	inches									<b>└───</b> '	
25-yr Runoff Volume (P1 = 1.88 in.) =	4.380	acre-feet	1.88	inches										
50-yr Runoff Volume (P1 = 2.24 in.) =	5.457	acre-feet	2.24	inches										
100-yr Runoff Volume (P1 = 2.57 in.) =	6.531	acre-feet	2.57	inches										
500-vr Runoff Volume (P1 = 3.14 in ) =	8,333	acre-feet		inches										
Approximate 2-vr Detention Volume =	1 920	acro foot		Inches										
Approximate 2-yr Detention Volume =	1.050												'	
Approximate 5-yr Detention Volume =	2.455	acre-feet											L	
Approximate 10-yr Detention Volume =	3.036	acre-feet												
Approximate 25-yr Detention Volume =	4.030	acre-feet												
Approximate 50-yr Detention Volume =	4.680	acre-feet												
Approximate 100-vr Detention Volume =	5.205	acre-feet												
·····														
Define Zenes and Pasis Commeters													'	
Derine Zones and Basin Geometry		1											'	
Zone 1 Volume (WQCV) =	0.905	acre-feet											ļ'	
Zone 2 Volume (EURV - Zone 1) =	2.608	acre-feet												
Zone 3 Volume (100-year - Zones 1 & 2) =	1.692	acre-feet											'	
Total Detention Basin Volume =	5.205	acre-feet												
Initial Surcharge Volume (ISV) =	user	ft 3												
Initial Surcharge Dopth (ISD) =	user	A .												
initial Suichaige Deput (15D) =	usei												'	
Total Available Detention Depth (H <sub>total</sub> ) =	user	π											'	
Depth of Trickle Channel (H <sub>TC</sub> ) =	user	ft												
Slope of Trickle Channel (S <sub>TC</sub> ) =	user	ft/ft											'	
Slopes of Main Basin Sides (Smain) =	user	H:V												
Basin Length-to-Width Ratio (Ri Av) =	user	1												
5		1												
Initial Curchange Area (A ) -		]a2											<sup> </sup>	
Initial Suichaige Area (A <sub>ISV</sub> ) =	usei												<u> </u>	
Surcharge Volume Length (L <sub>ISV</sub> ) =	user	1											<b>└───</b> ′	
Surcharge Volume Width $(W_{ISV}) =$	user	ft											L	
Depth of Basin Floor $(H_{FLOOR}) =$	user	ft												
Length of Basin Floor $(L_{FLOOR}) =$	user	ft												
Width of Basin Floor (W <sub>FLOOP</sub> ) =	user	ft												
Area of Basin Floor (Arean) =	user	ft 2												
Volume of Basin Floor (V) =	licor	ф.3												
Death of Main Pools (VFLOOR) =	450												'	
Depth of Main Basin $(H_{MAIN}) =$	user	π											L	
Length of Main Basin $(L_{MAIN}) =$	user	ft												
Width of Main Basin (W <sub>MAIN</sub> ) =	user	ft												
Area of Main Basin (A <sub>MAIN</sub> ) =	user	ft 2											'	
Volume of Main Basin (V <sub>MAIN</sub> ) =	user	ft 3												
Calculated Total Basin Volume (V	user	acre-feet												
		1												
													<b>├───</b> │	
													<u> </u>	
													L	
													<u> </u>	
													<sup> </sup>	
												-		
													<b>└──</b> ─	
													'	

#### DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.06 (July 2022)

![](_page_61_Figure_2.jpeg)

	DE	TENTION	BASIN OUT	LET STRU	CTURE DES	SIGN			
Project	Schmidt Phase 1 -	M	1HFD-Detention, V	ersion 4.06 (July J	2022)				
Basin ID:	Pond A	District Initiasti de	luie						
ZONE 3				Estimated	Estimated				
		~		Stage (ft)	Volume (ac-ft)	Outlet Type			
VOLUME EURV WOCV	┫		Zone 1 (WOCV)	3 15	0.905	Orifice Plate	1		
± ± +			Zone 1 (WQEV)	5.15 E 44	2.505	Portongular Orifica			
ZONE 1 AND 2	ORIFICE		Zone Z (EURV)	5.44	2.608	Rectangular Onlice	-		
PERMANENT ORIFICES POOL Example Zone C	Configuration (Rete	ention Pond)	Zone 3 (100-year)	6.65	1.692	Weir&Pipe (Restrict)			
				Total (all zones)	5.205				
User Input: Orifice at Underdrain Outlet (typicall	y used to drain WQ	CV in a Filtration BN	<u>MP)</u>	<i>c</i>			Calculated Parame	eters for Underdrain	<u>1</u>
Underdrain Orifice Invert Depth =	N/A	ft (distance below	the filtration media	surface)	Underd	Irain Orifice Area =	N/A	ft <sup>e</sup>	
	N/A	Inches			Underdrait		N/A	leet	
User Input: Orifice Plate with one or more orific	es or Elliptical Slot '	Weir (typically user	to drain WOCV and	1/or FLIRV in a sedi	mentation BMP)		Calculated Parame	ters for Plate	
Centroid of Lowest Orifice =		ft (relative to basir	n bottom at Stage =	: 0 ft)	WO Orifi	ce Area per Row =	N/A	ft <sup>2</sup>	
Depth at top of Zone using Orifice Plate =	3.09	ft (relative to basir	n bottom at Stage =	= 0 ft)	Elli	iptical Half-Width =	N/A	feet	
Orifice Plate: Orifice Vertical Spacing =	N/A	inches		,	Ellipt	ical Slot Centroid =	N/A	feet	
Orifice Plate: Orifice Area per Row =	N/A	sq. inches	2.72		E	Elliptical Slot Area =	N/A	ft <sup>2</sup>	
								-	
User Input: Stage and Total Area of Each Orific	e Row (numbered f	rom lowest to high	<u>est)</u>						-
	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)	
Stage of Orifice Centroid (ft)	0.00	1/0	2,10						_
Orifice Area (sq. inches)	2.81	2.82	2.82						
			<b>D</b> 414 1	D 404			D 454 - 1	D (51)	1
	Row 9 (optional)	коw 10 (optional)	Row 11 (optional)	Kow 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)	-
Stage of Orlfice Centroid (ft)			-		-				_
Office Area (sq. inches)		u							
User Input: Vertical Orifice (Circular or Rectand	ular)	-					Calculated Parame	ters for Vertical Or	ifice
See The Content of the Content of the Content of the Content	Zone 2 Rectangular	Not Selected	]				Zone 2 Rectangula	Not Selected	1
Invert of Vertical Orifice =	3.09	N/A	ft (relative to basir	bottom at Stage =	= 0 ft) Ver	tical Orifice Area =	0.09	N/A	ft <sup>2</sup>
Depth at top of Zone using Vertical Orifice =	5.28	N/A	ft (relative to basir	bottom at Stage =	= 0 ft) Vertica	I Orifice Centroid =	0.08	N/A	feet
Vertical Orifice Height =	2.00	N/A	inches					•	-
Vertical Orifice Width =	6.50	E	inches						
User Input: Overflow Weir (Dropbox with Flat o	r Sloped Grate and	Outlet Pipe OR Rec	ctangular/Trapezoid	al Weir and No Out	let Pipe)		Calculated Parame	ters for Overflow V	Veir
User Input: Overflow Weir (Dropbox with Flat o	r Sloped Grate and Zone 3 Weir	Outlet Pipe OR Rec	ctangular/Trapezoid	al Weir and No Out	let Pipe)		Calculated Parame Zone 3 Weir	ters for Overflow V Not Selected	<u>Veir</u>
User Input: Overflow Weir (Dropbox with Flat or Overflow Weir Front Edge Height, Ho =	Zone 3 Weir 5.58	Outlet Pipe OR Rec Not Selected N/A	ctangular/Trapezoid	al Weir and No Out	let Pipe)_ ft) Height of Grate	e Upper Edge, H <sub>t</sub> =	Calculated Parame Zone 3 Weir 5.58	Not Selected	<u>Veir</u> feet
User Input: Overflow Weir (Dropbox with Flat or Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length =	r Sloped Grate and Zone 3 Weir 5.58 4.00	Outlet Pipe OR Rec Not Selected N/A N/A	ctangular/Trapezoid ft (relative to basin l feet	al Weir and No Out	let Pipe)	e Upper Edge, H <sub>t</sub> = /eir Slope Length =	Calculated Parame Zone 3 Weir 5.58 4.00	Not Selected N/A N/A	<u>Veir</u> feet feet
User Input: Overflow Weir (Dropbox with Flat or Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope =	r Sloped Grate and Zone 3 Weir 5.58 4.00 0.00	Outlet Pipe OR Rec Not Selected N/A N/A N/A	ctanqular/Trapezoid ft (relative to basin l feet H:V	al Weir and No Out pottom at Stage = 0 f Gra	let Pipe) (t) Height of Grate Overflow W ate Open Area / 10	e Upper Edge, H <sub>t</sub> = /eir Slope Length = 10-yr Orifice Area =	Calculated Parame Zone 3 Weir 5.58 4.00 8.43	Not Selected N/A N/A N/A N/A	Veir feet feet
User Input: Overflow Weir (Dropbox with Flat or Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides =	r Sloped Grate and Zope 3 Weir 5.58 4.00 0.00 4.00	Outlet Pipe OR Ren Not Selected N/A N/A N/A N/A	ctanqular/Trapezoid ft (relative to basin l feet H:V feet	al Weir and No Out pottom at Stage = 0 f Gra Ov	let Pipe) ft) Height of Grate Overflow W ate Open Area / 10 erflow Grate Open worflow Crate Open	e Upper Edge, H <sub>t</sub> = /eir Slope Length = 10-yr Orifice Area = Area w/o Debris = 0 Area w/ Debris =	Calculated Parame Zone 3 Weir 5.58 4.00 8.43 11.14	Not Selected N/A N/A N/A N/A N/A N/A	Veir feet feet ft <sup>2</sup>
User Input: Overflow Weir (Dropbox with Flat or Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogonian %	r Sloped Grate and Zope 3 Weir 5.58 4.00 0.00 4.00 77pe C Grate 50%	Outlet Pipe OR Rer Not Selected N/A N/A N/A N/A N/A N/A	ctangular/Trapezoid ft (relative to basin l feet H:V feet	al Weir and No Out pottom at Stage = 0 I Gr: Ov C	let Pipe) ft) Height of Gratu Overflow W ate Open Area / 10 verflow Grate Open verflow Grate Open	e Upper Edge, H <sub>t</sub> = /eir Slope Length = 10-yr Orifice Area = Area w/o Debris = n Area w/ Debris =	Calculated Parame           Zone 3 Weir           5.58           4.00           8.43           11.14           5.57	tters for Overflow V Not Selected N/A N/A N/A N/A N/A	<u>Veir</u> feet feet ft <sup>2</sup> ft <sup>2</sup>
User Input: Overflow Weir (Dropbox with Flat or Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % =	Zone 3 Weir 5.58 4.00 0.00 4.00 V/pe C Grate 50%	Outlet Pipe OR Red Not Selected N/A N/A N/A N/A N/A N/A	ctangular/Trapezoid ft (relative to basin l feet H:V feet %	al Weir and No Out pottom at Stage = 0 i Gra Ov C	let Pipe) t) Height of Gratu Overflow W ate Open Area / 10 erflow Grate Open verflow Grate Open	e Upper Edge, H <sub>t</sub> = /eir Slope Length = 10-yr Orifice Area = Area w/o Debris = n Area w/ Debris =	Calculated Parame           Zone 3 Weir           5.58           4.00           8.43           11.14           5.57	ters for Overflow V Not Selected N/A N/A N/A N/A N/A	<u>Veir</u> feet feet ft <sup>2</sup> ft <sup>2</sup>
User Input: Overflow Weir (Dropbox with Flat or Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate	Zone 3 Weir 5.58 4.00 0.00 4.00 70% 50% (Circular Orifice, R	Outlet Pipe OR Re Not Selected N/A N/A N/A N/A N/A N/A Strictor Plate, or R	ctangular/Trapezoid ft (relative to basin l feet H:V feet % Rectangular Orifice)	al Weir and No Out pottom at Stage = 0 i Gra Ov C	let Pipe) t) Height of Gratu Overflow W ate Open Area / 10 erflow Grate Open verflow Grate Open verflow Grate Open Ca	e Upper Edge, H <sub>t</sub> = /eir Slope Length = 10-yr Orifice Area = Area w/o Debris = n Area w/ Debris = Iculated Parameter:	Calculated Parame           Zone 3 Weir           5.58           4.00           8.43           11.14           5.57	ters for Overflow V Not Selected N/A N/A N/A N/A N/A Flow Restriction P	Veir feet feet ft <sup>2</sup> ft <sup>2</sup>
User Input: Overflow Weir (Dropbox with Flat of Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % =	r Sloped Grate and Zone 3 Weir 5.58 4.00 0.00 4.00 70% Fe C Grate 50% (Circular Orifice. R Zone 3 Restrictor	Outlet Pipe OR Re Not Selected N/A N/A N/A N/A N/A N/A estrictor Plate, or R Not Selected	ctangular/Trapezoid ft (relative to basin l feet H:V feet % <u>Rectangular Orifice)</u>	al Weir and No Out pottom at Stage = 0 I Gra Ov C	let Pipe) t) Height of Gratu Overflow W ate Open Area / 10 erflow Grate Open verflow Grate Open verflow Grate Open <u>Ca</u>	e Upper Edge, H <sub>t</sub> = /eir Slope Length = 10-yr Orifice Area = Area w/o Debris = n Area w/ Debris = Iculated Parameter	Calculated Parame           Zone 3 Weir           5.58           4.00           8.43           11.14           5.57           s for Outlet Pipe w,           Zone 3 Restrictor	ters for Overflow V Not Selected N/A N/A N/A N/A N/A V/A V/A N/A N/A	Veir feet feet ft <sup>2</sup> ft <sup>2</sup>
User Input: Overflow Weir (Dropbox with Flat of Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe =	A Sloped Grate and Zone 3 Weir 5.58 4.00 0.00 4.00 50% Corcular Orifice. R Zone 3 Restrictor 0.83	Outlet Pipe OR Rev Not Selected N/A N/A N/A N/A N/A N/A estrictor Plate, or R Not Selected N/A	ctangular/Trapezoid ft (relative to basin l feet H:V feet % <u>Rectangular Orifice)</u> ft (distance below b	al Weir and No Out pottom at Stage = 0 I Gra Ov C asin bottom at Stage	tet Pipe) t) Height of Gratu Overflow W ate Open Area / 10 erflow Grate Open verflow Grate Open <u>Ca</u> = 0 ft) O	e Upper Edge, H <sub>t</sub> = /eir Slope Length = 10-yr Orifice Area = Area w/o Debris = n Area w/ Debris = Iculated Parameter: utlet Orifice Area =	Calculated Parame           Zone 3 Weir           5.58           4.00           8.43           11.14           5.57           s for Outlet Pipe w,           Zone 3 Restrictor           1.32	ters for Overflow V Not Selected N/A N/A N/A N/A N/A Y Flow Restriction Pl Not Selected N/A	<u>Veir</u> feet feet ft <sup>2</sup> ft <sup>2</sup> ft <sup>2</sup>
User Input: Overflow Weir (Dropbox with Flat of Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter =	r Sloped Grate and Zone 3 Weir 5.58 4.00 0.00 4.00 700 C Grate 50% C(Circular Orifice. R Zone 3 Restrictor 0.83 18.00	Outlet Pipe OR Ref Not Selected N/A N/A N/A N/A N/A estrictor Plate, or R Not Selected N/A N/A	ctangular/Trapezoid ft (relative to basin l feet H:V feet % Rectangular Orifice) ft (distance below b inches	al Weir and No Out pottom at Stage = 0 I Gra Ov C asin bottom at Stage	tet Pipe) t) Height of Gratu Overflow W ate Open Area / 10 reflow Grate Open verflow Grate Open <u>Ca</u> = 0 ft) Or Outle	e Upper Edge, H <sub>t</sub> = /eir Slope Length = 10-yr Orifice Area = Area w/o Debris = n Area w/ Debris = <u>Iculated Parameter</u> : utlet Orifice Area = t Orifice Centroid =	Calculated Parame           Zone 3 Weir           5.58           4.00           8.43           11.14           5.57           s for Outlet Pipe w,           Zone 3 Restrictor           1.32           0.59	ters for Overflow V Not Selected N/A N/A N/A N/A V/A Flow Restriction Pl Not Selected N/A N/A	<u>Veir</u> feet feet ft <sup>2</sup> ft <sup>2</sup> ft <sup>2</sup> ft <sup>2</sup> fteet
User Input: Overflow Weir (Dropbox with Flat of Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert =	x Sloped Grate and Zone 3 Weir 5.58 4.00 0.00 4.00 50% Corcular Orifice, R Zone 3 Restrictor 0.83 18.00 12.60	Outlet Pipe OR Ref Not Selected N/A N/A N/A N/A N/A N/A estrictor Plate, or R Not Selected N/A N/A	ctangular/Trapezoid ft (relative to basin l feet H:V feet % <u>Rectangular Orifice)</u> ft (distance below be inches inches	al Weir and No Out pottom at Stage = 0 I Gra Ov C asin bottom at Stage Half-Cent	tet Pipe) t) Height of Gratu Overflow W ate Open Area / 10 rerflow Grate Open verflow Grate Open verflow Grate Open <u>Ca</u> = 0 ft) Or Outlef ral Angle of Restrict	e Upper Edge, H <sub>t</sub> = /eir Slope Length = 0-yr Orifice Area = Area w/o Debris = n Area w/ Debris = lculated Parameter: utlet Orifice Area = t Orifice Centroid = tor Plate on Pipe =	Calculated Parame           Zone 3 Weir           5.58           4.00           8.43           11.14           5.57           s for Outlet Pipe w,           Zone 3 Restrictor           1.32           0.59           1.98	ters for Overflow V Not Selected N/A N/A N/A N/A CFlow Restriction Pl Not Selected N/A N/A	<u>Veir</u> feet feet ft <sup>2</sup> ft <sup>2</sup> ft <sup>2</sup> ft <sup>2</sup> fteet radians
User Input: Overflow Weir (Dropbox with Flat of Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert =	Sloped Grate and           Zone 3 Weir           5.58           4.00           0.00           4.00           0.00           4.00           0.00           4.00           0.00           4.00           0.00           4.00           0.00           4.00           0.00           2.00           3 Restrictor           0.83           18.00           12.60	Outlet Pipe OR Ref Not Selected N/A N/A N/A N/A N/A estrictor Plate, or R N/A N/A N/A N/A	ctangular/Trapezoid ft (relative to basin l feet H:V feet % <u>Rectangular Orifice)</u> ft (distance below b inches inches	al Weir and No Out pottom at Stage = 0 I Gri Ov C asin bottom at Stage Half-Cent	tet Pipe) t) Height of Gratu Overflow W ate Open Area / 10 rerflow Grate Open verflow Grate Open <u>Ca</u> = 0 ft) Or Outlef ral Angle of Restric	e Upper Edge, H <sub>t</sub> = /eir Slope Length = 0-yr Orifice Area = Area w/o Debris = n Area w/ Debris = <u>lculated Parameter</u> : utlet Orifice Area = t Orifice Centroid = tor Plate on Pipe =	Calculated Parame           Zone 3 Weir           5.58           4.00           8.43           11.14           5.57           s for Outlet Pipe w,           Zone 3 Restrictor           1.32           0.59           1.98	ters for Overflow V Not Selected N/A N/A N/A N/A V Flow Restriction Pl Not Selected N/A N/A N/A	<u>Veir</u> feet feet ft <sup>2</sup> ft <sup>2</sup> ft <sup>2</sup> ft <sup>2</sup> fteet radians
User Input: Overflow Weir (Dropbox with Flat of Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or	Circular Orifice. R           Cone 3 Weir           5.58           4.00           0.00           4.00           0.00           4.00           0.00           4.00           0.00           4.00           0.00           4.00           0.00           4.00           0.00           4.00           0.00           0.00           0.00           0.83           18.00           12.60           Trapezoidal)	Outlet Pipe OR Ref Not Selected N/A N/A N/A N/A N/A N/A estrictor Plate, or R Not Selected N/A N/A	ctangular/Trapezoid ft (relative to basin l feet H:V feet % <u>Rectangular Orifice)</u> ft (distance below b inches inches	al Weir and No Out pottom at Stage = 0 I Gri Ov C asin bottom at Stage Half-Cent	tet Pipe) t) Height of Gratu Overflow W ate Open Area / 10 rerflow Grate Open verflow Grate Open verflow Grate Open <u>Ca</u> = 0 ft) O Outlef ral Angle of Restric	e Upper Edge, H <sub>t</sub> = /eir Slope Length = 10-yr Orifice Area = Area w/o Debris = n Area w/ Debris = lculated Parameter: utlet Orifice Area = t Orifice Centroid = tor Plate on Pipe =	Calculated Parame           Zone 3 Weir           5.58           4.00           8.43           11.14           5.57           s for Outlet Pipe w,           Zone 3 Restrictor           1.32           0.59           1.98           Calculated Parame	ters for Overflow V Not Selected N/A N/A N/A N/A N/A / Flow Restriction P Not Selected N/A N/A N/A	Veir feet feet ft <sup>2</sup> ft <sup>2</sup> ft <sup>2</sup> ft <sup>2</sup> fteet radians
User Input: Overflow Weir (Dropbox with Flat of Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage=	r Sloped Grate and Zone 3 Weir 5.58 4.00 0.00 4.00 Vpe C Grate 50% (Circular Orifice, R Zone 3 Restrictor 0.83 18.00 12.60 Trapezoidal) 7.00	Outlet Pipe OR Ref Not Selected N/A N/A N/A N/A N/A N/A estrictor Plate, or R Not Selected N/A N/A estrictor Plate, or selected N/A	tangular/Trapezoid ft (relative to basin l feet H:V feet 9% Rectangular Orifice) ft (distance below be inches inches	al Weir and No Out pottom at Stage = 0 I Gr Ov C asin bottom at Stage Half-Cent = 0 ft)	tet Pipe) t) Height of Gratı Overflow W ate Open Area / 10 rerflow Grate Open verflow Grate Open verflow Grate Open <u>Ca</u> = 0 ft) O Outled ral Angle of Restric Spillway D	e Upper Edge, H <sub>t</sub> = /eir Slope Length = 10-yr Orifice Area = Area w/o Debris = n Area w/ Debris = lculated Parameter: utlet Orifice Area = t Orifice Centroid = tor Plate on Pipe =	Calculated Parame           Zone 3 Weir           5.58           4.00           8.43           11.14           5.57           s for Outlet Pipe w,           Zone 3 Restrictor           1.32           0.59           1.98           Calculated Parame           0.93	ters for Overflow V Not Selected N/A N/A N/A N/A N/A / Flow Restriction P N/A N/A N/A N/A N/A N/A eters for Spillway feet	Veir feet feet ft <sup>2</sup> ft <sup>2</sup> ft <sup>2</sup> ftet radians
User Input: Overflow Weir (Dropbox with Flat of Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length =	r Sloped Grate and Zone 3 Weir 5.58 4.00 0.00 4.00 Vype C Grate 50% (Circular Orifice, R Zone 3 Restrictor 0.83 18.00 12.60 Trapezoidal) 7.00 31.00	Outlet Pipe OR Ref Not Selected N/A N/A N/A N/A N/A N/A estrictor Plate, or R Not Selected N/A N/A ft (relative to basin feet 30'	tangular/Trapezoid ft (relative to basin l feet H:V feet % Rectangular Orifice) ft (distance below be inches inches	al Weir and No Out pottom at Stage = 0 I Gr Ov C asin bottom at Stage Half-Cent = 0 ft)	tet Pipe) t) Height of Grati Overflow W ate Open Area / 10 rerflow Grate Open verflow Grate Open verflow Grate Open <u>Ca</u> = 0 ft) O Outlei ral Angle of Restric Spillway D Stage at T	e Upper Edge, H <sub>t</sub> = /eir Slope Length = 10-yr Orifice Area = Area w/o Debris = n Area w/ Debris = lculated Parameter: utlet Orifice Area = t Orifice Centroid = tor Plate on Pipe = pesign Flow Depth= Top of Freeboard =	Calculated Parame           Zone 3 Weir           5.58           4.00           8.43           11.14           5.57           s for Outlet Pipe w,           Zone 3 Restrictor           1.32           0.59           1.98           Calculated Parame           0.93           8.93	ters for Overflow V Not Selected N/A N/A N/A N/A N/A / Flow Restriction Pl Not Selected N/A N/A N/A N/A eters for Spillway feet feet	<u>Veir</u> feet feet ft <sup>2</sup> ft <sup>2</sup> ft <sup>2</sup> ft <sup>2</sup> feet radians
User Input: Overflow Weir (Dropbox with Flat of Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage = Spillway Crest Length = Spillway End Slopes =	r Sloped Grate and Zone 3 Weir 5.58 4.00 0.00 4.00 50% Circular Orifice, R. Zone 3 Restrictor 0.83 18.00 12.60 Trapezoidal) 7.00 31.00 4.00	Outlet Pipe OR Ref Not Selected N/A N/A N/A N/A N/A N/A N/A estrictor Plate, or R Not Selected N/A N/A if (relative to basin feet 30' H:V	tangular/Trapezoid ft (relative to basin l feet H:V feet % Rectangular Orifice) ft (distance below be inches inches n bottom at Stage =	al Weir and No Out pottom at Stage = 0 I Gr Ov C asin bottom at Stage Half-Cent : 0 ft)	tet Pipe) t) Height of Gratu Overflow W ate Open Area / 10 reflow Grate Open verflow Grate Open verflow Grate Open Ca = 0 ft) Or Outlet ral Angle of Restrict Spillway D Stage at T Basin Area at T	e Upper Edge, H <sub>t</sub> = /eir Slope Length = 0-yr Orifice Area = Area w/o Debris = n Area w/ Debris = lculated Parameter: utlet Orifice Area = t Orifice Centroid = tor Plate on Pipe = vesign Flow Depth= Fop of Freeboard =	Calculated Parame           Zone 3 Weir           5.58           4.00           8.43           11.14           5.57           s for Outlet Pipe w.           Zone 3 Restrictor           1.32           0.59           1.98           Calculated Parame           0.93           8.93           1.71	ters for Overflow V Not Selected N/A N/A N/A N/A N/A V Flow Restriction Pl Not Selected N/A N/A N/A N/A ters for Spillway feet feet acres	<u>Veir</u> feet feet ft <sup>2</sup> ft <sup>2</sup> ft <sup>2</sup> ft <sup>2</sup> feet radians
User Input: Overflow Weir (Dropbox with Flat of Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface =	r Sloped Grate and Zone 3 Weir 5.58 4.00 0.00 4.00 50% Circular Orifice, R Zone 3 Restrictor 0.83 18.00 12.60 Trapezoidal) 7.00 4.00 4.00	Outlet Pipe OR Ref Not Selected N/A N/A N/A N/A N/A N/A N/A estrictor Plate, or R Not Selected N/A N/A ft (relative to basin feet 30' H:V	tangular/Trapezoid ft (relative to basin l feet H:V feet 9% Rectangular Orifice) ft (distance below be inches inches	al Weir and No Out pottom at Stage = 0 I Gr Ov C asin bottom at Stage Half-Cent : 0 ft)	tet Pipe) t) Height of Grati Overflow W ate Open Area / 10 rerflow Grate Open verflow Grate Open verflow Grate Open Ca Ca Ca Ca Ca Ca Spillway D Stage at T Basin Area at T Basin Volume at T	e Upper Edge, H <sub>t</sub> = /eir Slope Length = 10-yr Orifice Area = Area w/o Debris = n Area w/ Debris = lculated Parameter: utlet Orifice Area = t Orifice Centroid = tor Plate on Pipe = rop of Freeboard = rop of Freeboard = rop of Freeboard =	Calculated Parame           Zone 3 Weir           5.58           4.00           8.43           11.14           5.57           s for Outlet Pipe w,           Zone 3 Restrictor           1.32           0.59           1.98           Calculated Parame           0.93           8.93           1.71           8.83	ters for Overflow V Not Selected N/A N/A N/A N/A N/A V Flow Restriction P Not Selected N/A N/A N/A N/A ters for Spillway feet feet acres acre-ft	<u>Veir</u> feet feet ft <sup>2</sup> ft <sup>2</sup> ft <sup>2</sup> ft <sup>2</sup> feet radians
User Input: Overflow Weir (Dropbox with Flat of Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface =	r Sloped Grate and Zone 3 Weir 5.58 4.00 0.00 4.00 700 50% C Grate 50% 2 (Circular Orifice, R Zone 3 Restrictor 0.83 18.00 12.60 Trapezoidal) 7.00 4.00 1.00	Outlet Pipe OR Red Not Selected N/A N/A N/A N/A N/A estrictor Plate, or R Not Selected N/A N/A estrictor Plate, or selected N/A N/A t (relative to basin feet 30' H:V feet	tangular/Trapezoid ft (relative to basin l feet H:V feet % Rectangular Orifice) ft (distance below be inches inches	al Weir and No Out pottom at Stage = 0 I Gr Ov C asin bottom at Stage Half-Cent : 0 ft)	tet Pipe) t) Height of Gratu Overflow W ate Open Area / 10 reflow Grate Open verflow Grate Open verflow Grate Open Ca Ca Ca Ca Ca Ca Ca Ca Ca Ca	e Upper Edge, H <sub>t</sub> = /eir Slope Length = 0-yr Orifice Area = Area w/o Debris = n Area w/ Debris = lculated Parameter: utlet Orifice Area = t Orifice Centroid = tor Plate on Pipe = vesign Flow Depth= Fop of Freeboard = Fop of Freeboard = Fop of Freeboard =	Calculated Parame           Zone 3 Weir           5.58           4.00           8.43           11.14           5.57           s for Outlet Pipe w.           Zone 3 Restrictor           1.32           0.59           1.98           Calculated Parame           0.93           8.93           1.71           8.83	ters for Overflow V Not Selected N/A N/A N/A N/A N/A V Flow Restriction Pl Not Selected N/A N/A N/A N/A N/A ters for Spillway feet feet acres acre-ft	<u>Veir</u> feet feet ft <sup>2</sup> ft <sup>2</sup> ft <sup>2</sup> feet radians
User Input: Overflow Weir (Dropbox with Flat of Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Routed Hydrograph Results	Circular Orifice, R           2000         4.00           4.00         4.00           4.00         50%           2000         7.00           2000         12.60           Trapezoidal)         7.00           4.00         1.00	Outlet Pipe OR Ref Not Selected N/A N/A N/A N/A N/A N/A estrictor Plate, or R Not Selected N/A N/A ft (relative to basin feet 30' H:V feet	tangular/Trapezoid ft (relative to basin l feet H:V feet 9% Rectangular Orifice) ft (distance below be inches inches n bottom at Stage =	al Weir and No Out pottom at Stage = 0 I Gra Ov C asin bottom at Stage Half-Cent = 0 ft) I runoff volumes by	tet Pipe) t) Height of Gratu Overflow W ate Open Area / 10 rerflow Grate Open verflow Grate Open verflow Grate Open Ca = 0 ft) On Outlet ral Angle of Restrict Spillway D Stage at T Basin Area at T Basin Volume at T Centering new value	e Upper Edge, H <sub>t</sub> = /eir Slope Length = /0-yr Orifice Area = Area w/o Debris = n Area w/ Debris = ilculated Parameter: utlet Orifice Area = t Orifice Centroid = to rifice Centroid = tor Plate on Pipe = /op of Freeboard = /op of Freeboard = /op of Freeboard = /op of Freeboard =	Calculated Parame           Zone 3 Weir           5.58           4.00           8.43           11.14           5.57           s for Outlet Pipe w.           Zone 3 Restrictor           1.32           0.59           1.98           Calculated Parame           0.93           8.93           1.71           8.83	ters for Overflow V Not Selected N/A N/A N/A N/A N/A V Flow Restriction Pl Not Selected N/A N/A N/A N/A N/A ters for Spillway feet feet acres acre-ft	Veir feet feet ft <sup>2</sup> ft <sup>2</sup> ft <sup>2</sup> fteet radians
User Input: Overflow Weir (Dropbox with Flat of Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Routed Hydrograph Results Design Storm Return Period =	r Sloped Grate and Zone 3 Weir 5.58 4.00 0.00 4.00 70 C Grate 50% 2006 3 Restrictor 0.83 18.00 12.60 7.00 31.00 4.00 1.00 7.00 7.00 7.00 7.00 7.00 7.00 7	Outlet Pipe OR Ref Not Selected N/A N/A N/A N/A N/A N/A N/A estrictor Plate, or R Not Selected N/A N/A ft (relative to basin feet 30' H:V feet	tangular/Trapezoid ft (relative to basin l feet H:V feet % Rectangular Orifice) ft (distance below be inches inches n bottom at Stage =	al Weir and No Out pottom at Stage = 0 i Gra Ov C asin bottom at Stage Half-Cent = 0 ft) <u>6 runoff volumes by</u> 5 Year	let Pipe) it) Height of Gratu Overflow V ate Open Area / 10 erflow Grate Open iverflow Grate Open iverflow Grate Open <u>Ca</u> = 0 ft) Or Outlet ral Angle of Restrict Spillway D Stage at T Basin Area at T Basin Volume at T i entering new valu 10 Year	e Upper Edge, H <sub>t</sub> = /eir Slope Length = /0-yr Orifice Area = Area w/o Debris = n Area w/ Debris = ilculated Parameter: utlet Orifice Area = t Orifice Centroid = t Orifice Centroid = tor Plate on Pipe = Pesign Flow Depth= Fop of Freeboard = Fop of Freeboard =	Calculated Parame           Zone 3 Weir           5.58           4.00           8.43           11.14           5.57           s for Outlet Pipe w           Zone 3 Restrictor           1.32           0.59           1.98           Calculated Parame           0.93           8.93           1.71           8.83           drographs table (CC           50 Year	ters for Overflow V Not Selected N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A	Veir feet feet ft <sup>2</sup> ft <sup>2</sup> ft <sup>2</sup> ft <sup>2</sup> feet radians
User Input: Overflow Weir (Dropbox with Flat of Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = One-Hour Rainfall Depth (in) = Of IHP Runoff Volume (acred)	r Sloped Grate and Zone 3 Weir 5.58 4.00 0.00 4.00 700 C Grate 50% 2006 3 Restrictor 0.83 18.00 12.60 7.00 31.00 4.00 1.00 7.00 7.00 7.00 7.00 7.00 7.00 7	Outlet Pipe OR Ref Not Selected N/A N/A N/A N/A N/A N/A N/A estrictor Plate, or R Not Selected N/A N/A ft (relative to basin feet 30' H:V feet	tangular/Trapezoid ft (relative to basin l feet H:V feet % Rectangular Orifice) ft (distance below be inches inches n bottom at Stage = HP hydrographs and 2 Year 0.95	al Weir and No Out pottom at Stage = 0 i Gra Ov C asin bottom at Stage Half-Cent = 0 ft) <u>6 Year</u> 1.23 2.661	let Pipe) it) Height of Gratu Overflow V ate Open Area / 10 erflow Grate Open iverflow Grate Open iverflow Grate Open <u>Ca</u> = 0 ft) Or Outlet ral Angle of Restrict Spillway D Stage at T Basin Area at T Basin Volume at T i entering new valu 10 Year 1.48 3.287	e Upper Edge, H <sub>t</sub> = /eir Slope Length = /o-yr Orifice Area = Area w/o Debris = n Area w/ Debris = ikulated Parameter: utlet Orifice Area = t Orifice Centroid = t Orifice Centroid = tor Plate on Pipe = Pesign Flow Depth= Fop of Freeboard = Fop of Freeboard = 1.88 4.380	Calculated Parame           Zone 3 Weir           5.58           4.00           8.43           11.14           5.57           s for Outlet Pipe w           Zone 3 Restrictor           1.32           0.59           1.98           Calculated Parame           0.93           8.93           1.71           8.83           drographs table (CC           50 Year           2.24           5.457	ters for Overflow V Not Selected N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A	Veir feet feet ft <sup>2</sup> ft <sup>2</sup> ft <sup>2</sup> ft <sup>2</sup> feet radians
User Input: Overflow Weir (Dropbox with Flat of Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Reuted Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) =	r Sloped Grate and Zone 3 Weir 5.58 4.00 0.00 4.00 7/pe C Grate 50% 20ne 3 Restrictor 0.83 18.00 12.60 7.00 31.00 4.00 1.00 7 <i>he user can overr</i> WQCV N/A 0.905 N/A	Outlet Pipe OR Ref Not Selected N/A N/A N/A N/A N/A N/A N/A estrictor Plate, or R Not Selected N/A N/A ft (relative to basin feet 30' H:V feet <i>ide the default CUI</i> EURV N/A 3.513 N/A	tangular/Trapezoid ft (relative to basin l feet H:V feet % & ectangular Orifice) ft (distance below be inches inches n bottom at Stage = HP hydrographs and 2 Year 0.95 1.992	al Weir and No Out pottom at Stage = 0 i Gra Ov C asin bottom at Stage Half-Cent = 0 ft) <u>1 runoff volumes by</u> <u>5 Year</u> 1.23 2.661 2.661	let Pipe) it) Height of Gratu Overflow V ate Open Area / 10 erflow Grate Open verflow Grate Open verflow Grate Open (24) (24	e Upper Edge, H <sub>t</sub> = /eir Slope Length = 10-yr Orifice Area = Area w/o Debris = n Area w/ Debris = Iculated Parameter: utlet Orifice Area = t Orifice Centroid = tor Plate on Pipe = lesign Flow Depth= Top of Freeboard = Top of Freeboard = Top of Freeboard = Cop of Freeboard = 1.88 4.380 4.380	Calculated Parame           Zone 3 Weir           5.58           4.00           8.43           11.14           5.57           s for Outlet Pipe w           Zone 3 Restrictor           1.32           0.59           1.98           Calculated Parame           0.93           8.93           1.71           8.83           drographs table (Colorgraphs	ters for Overflow V Not Selected N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A	Veir           feet           feet           ft²           ft²           ft²           ft²           feet           radians
User Input: Overflow Weir (Dropbox with Flat of Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Reuted Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = CUHP Predevelopment Peak Q (cfs) =	r Sloped Grate and Zone 3 Weir 5.58 4.00 0.00 4.00 7/pe C Grate 50% 2006 3 Restrictor 0.83 18.00 12.60 7.00 4.00 12.60 7.00 4.00 1.00 7.00 7.00 7.00 7.00 7.00 7.00 7	Outlet Pipe OR Ref Not Selected N/A N/A N/A N/A N/A N/A N/A N/A estrictor Plate, or R Not Selected N/A N/A ft (relative to basin feet 30' H:V feet <i>ide the default CUI</i> EURV N/A 3.513 N/A N/A	tangular/Trapezoid ft (relative to basin l feet H:V feet % Rectangular Orifice) ft (distance below b inches inches n bottom at Stage = HP hydrographs and 2 Year 0.95 1.992 0.0	al Weir and No Out cottom at Stage = 0 i Gra Ov C asin bottom at Stage Half-Cent i <i>runoff volumes by</i> 5 Year 1.23 2.661 2.661 0.2	let Pipe) t) Height of Gratu Overflow V ate Open Area / 10 erflow Grate Open verflow Grate Open verflow Grate Open (24)	e Upper Edge, H <sub>t</sub> = /eir Slope Length = 10-yr Orifice Area = Area w/o Debris = n Area w/ Debris = n Area w/ Debris = luculated Parameter: utlet Orifice Area = t Orifice Centroid = tor Plate on Pipe = tor Plate on Pipe = log of Freeboard = Top of Freeboard = Top of Freeboard = Top of Freeboard = Top of Freeboard = 1.88 4.380 4.380 2.7	Calculated Parame           Zone 3 Weir           5.58           4.00           8.43           11.14           5.57           s for Outlet Pipe w.           Zone 3 Restrictor           1.32           0.59           1.98           Calculated Parame           0.93           8.93           1.71           8.83           chographs table (CC           50 Year           2.24           5.457           10.1	ters for Overflow V Not Selected N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A	Veir           feet           feet           ft²           ft²           ft²           ft²           feet           ate           ft²           feet           same           feet           ft²           feet           same           ft²           feet           radians           4/?).           500 Year           3.14           8.333           31.2
User Input: Overflow Weir (Dropbox with Flat of Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Reuted Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = CUHP Predevelopment Peak Q (cfs) = OPTIONAL Override Predevelopment Peak Q (cfs) = OPTIONAL Override Predevelopment Peak Q (cfs) =	r Sloped Grate and Zone 3 Weir 5.58 4.00 0.00 4.00 7/pe C Grate 50% 2 (Circular Orifice, R Zone 3 Restrictor 0.83 18.00 12.60 7.00 4.00 1.00 7.00 4.00 1.00 7.00 7.00 7.00 7.00 7.00 7.00 7	Outlet Pipe OR Ref Not Selected N/A N/A N/A N/A N/A N/A N/A estrictor Plate, or R Not Selected N/A N/A ft (relative to basin feet 30' H:V feet <i>ide the default CUI</i> EURV N/A 3.513 N/A N/A N/A N/A	tangular/Trapezoid ft (relative to basin l feet H:V feet % Rectangular Orifice) ft (distance below b inches inches n bottom at Stage = HP hydrographs and 2 Year 0.95 1.992 0.0	al Weir and No Out cottom at Stage = 0 i Gri Ov C asin bottom at Stage Half-Cent i <i>runoff volumes by</i> 5 Year 1.23 2.661 0.2 0.01	let Pipe) t) Height of Gratu Overflow V ate Open Area / 10 erflow Grate Open verflow Grate Open verflow Grate Open (2 2 = 0 ft) O Outled ral Angle of Restrice Spillway D Stage at T Basin Area at T Basin Area at T Basin Volume at T (2 10 Year 1.48 3.287 0.4 0 01	e Upper Edge, H <sub>t</sub> = /eir Slope Length = 10-yr Orifice Area = Area w/o Debris = n Area w/ Debris = n Area w/ Debris = luculated Parameter: utlet Orifice Area = t Orifice Centroid = tor Plate on Pipe = tor Plate on Pipe = Pop of Freeboard = Top of Freeboard = 1.88 4.380 4.380 2.7 0.07	Calculated Parame           Zone 3 Weir           5.58           4.00           8.43           11.14           5.57           s for Outlet Pipe w,           Zone 3 Restrictor           1.32           0.59           1.98           Calculated Parame           0.93           8.93           1.71           8.83           Orographs table (Colorgraphs table (Colorgraphs table)           50 Year           2.24           5.457           10.1	ters for Overflow V Not Selected N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A	Veir           feet           feet           ft²           ft²           ft²           ft²           feet           ft²           ft²           ft²           feet           ft²           feet           ft²           feet           adians           3.14           8.333           31.2           0.82
User Input: Overflow Weir (Dropbox with Flat of Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length = Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Reuted Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = CUHP Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, q (cfs/acre) = Predevelopment Unit Peak Flow, q (cfs/acre) = Peak Inflow V (cfs) =	r Sloped Grate and Zone 3 Weir 5.58 4.00 0.00 4.00 7/pe C Grate 50% Circular Orifice, R Zone 3 Restrictor 0.83 18.00 12.60 Trapezoidal) 7.00 31.00 4.00 1.00 7.00 1.00 7.00 1.00 7.00 1.00 7.00 1.00 7.00 1.00 7.00 1.00 7.00 1.00 7.00 7	Outlet Pipe OR Ref Not Selected N/A N/A N/A N/A N/A N/A N/A estrictor Plate, or R Not Selected N/A N/A ft (relative to basin feet 30' H:V feet <i>ide the default CU/</i> Feet <i>ide the default CU/</i> N/A N/A N/A N/A N/A N/A	tangular/Trapezoid ft (relative to basin l feet H:V feet % Rectangular Orifice) ft (distance below be inches inches h bottom at Stage = HP hydrographs and 2 Year 0.95 1.992 0.0 0.00 28.0	al Weir and No Out pottom at Stage = 0 1 Gri Ov C asin bottom at Stage Half-Cent + 0 ft) 5 Year 1.23 2.661 2.661 0.2 	let Pipe) t) Height of Gratu Overflow W ate Open Area / 10 erflow Grate Open verflow Grate Open verflow Grate Open (Ca Ca = 0 ft) O Outled ral Angle of Restrice Spillway D Stage at T Basin Area at T Centering new value 10 Year 1.48 3.287 3.287 0.4 	e Upper Edge, H <sub>t</sub> = /eir Slope Length = 10-yr Orifice Area = Area w/o Debris = n Area w/ Debris = n Area w/ Debris = ilculated Parameter: utlet Orifice Area = t Orifice Centroid = tor Plate on Pipe = besign Flow Depth= Fop of Freeboard = Fop of Freeboard = Fop of Freeboard = Fop of Freeboard = 1.88 4.380 4.380 2.7 0.07 63.2	Calculated Parame           Zone 3 Weir           5.58           4.00           8.43           11.14           5.57           s for Outlet Pipe w,           Zone 3 Restrictor           1.32           0.59           1.98           Calculated Parame           0.93           8.93           1.71           8.83           drographs table (CC           50 Year           2.24           5.457           10.1           0.27           80.3	ters for Overflow V Not Selected N/A N/A N/A N/A N/A N/A N/A N/A N/A ters for Spillway feet feet acres acre-ft 100 Year 2.57 6.531 6.531 18.2 0.49 97.6	Veir           feet           feet           ft²           ft²           ft²           ft²           feet           ate           ft²           feet           same           feet           feet           feet           same           feet           radians           3.14           8.333           3.1.2           0.83           124.8
User Input: Overflow Weir (Dropbox with Flat of Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length = Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Reuted Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = OPTIONAL Override Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, q (cfs) area Peak Inflow Q (cfs) = Peak Unflow Q (cfs) =	r Sloped Grate and Zone 3 Weir 5.58 4.00 0.00 4.00 700 50% CGrate 50% CGrate 50% CGrate 50% Cone 3 Restrictor 0.83 18.00 12.60 Trapezoidal) 7.00 31.00 4.00 1.00 7.00 7.00 7.00 7.00 7.00 7.00 7	Outlet Pipe OR Ref Not Selected N/A N/A N/A N/A N/A N/A N/A N/A ft (relative to basir feet A N/A N/A N/A ft (relative to basir feet A N/A N/A N/A N/A N/A N/A N/A N/A N/A N	tangular/Trapezoid ft (relative to basin l feet H:V feet % Rectangular Orifice) ft (distance below be inches inches n bottom at Stage = HP hydrographs and 2 Year 0.95 1.992 1.992 1.992 0.0 0.0 0.0 0.9	al Weir and No Out cottom at Stage = 0 1 Gri Ov C asin bottom at Stage Half-Cent Half-Cent 1.23 2.661 2.661 2.661 0.2 1.1	tet Pipe) t) Height of Gratu Overflow W ate Open Area / 10 erflow Grate Open verflow Grate Open verflow Grate Open (2) (2) (2) (2) (2) (2) (2) (2)	e Upper Edge, H <sub>t</sub> = /eir Slope Length = /0-yr Orifice Area = Area w/o Debris = n Area w/ Debris = n Area w/ Debris = ////////////////////////////////////	Calculated Parame           Zone 3 Weir           5.58           4.00           8.43           11.14           5.57           s for Outlet Pipe w,           Zone 3 Restrictor           1.32           0.59           1.98           Calculated Parame           0.93           8.93           1.71           8.83           drographs table (CC           50 Year           2.24           5.457           10.1           0.27           80.3           12.2	ters for Overflow V Not Selected N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A	Veir           feet           feet           ft²           ft²           ft²           ft²           feet           ft²           feet           state           ft²           feet           feet           state           feet           radians           3.14           8.333           3.12           0.83           124.8           32.0
User Input: Overflow Weir (Dropbox with Flat of Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length = Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Reuted Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = OPTIONAL Override Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, q (cfs) = Peak Outflow to Predevelopment Q = Ratio Peak Outflow to Predevelopment Q =	r Sloped Grate and Zone 3 Weir 5.58 4.00 0.00 4.00 700 700 700 7.00 7.00 7.	Outlet Pipe OR Ref Not Selected N/A N/A N/A N/A N/A N/A N/A N/A estrictor Plate, or R Not Selected N/A N/A N/A ft (relative to basir feet 30' H:V feet EURV N/A 3.513 N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A	tangular/Trapezoid ft (relative to basin l feet H:V feet % Rectangular Orifice) ft (distance below be inches inches n bottom at Stage = <i>HP hydrographs and</i> 2 Year 0.95 1.992 1.992 1.992 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	al Weir and No Out pottom at Stage = 0 1 Gri Ov C asin bottom at Stage Half-Cent = 0 ft) = 1 runoff volumes by 5 Year 1.23 2.661 2.661 0.2 0.01 36.7 1.1 5.1 1.1 5.1 0 ft	tet Pipe) t) Height of Gratu Overflow W ate Open Area / 10 erflow Grate Open verflow Grate Open verflow Grate Open (enterilow Grate Open Stage at T Basin Area at T Basin Area at T Basin Volume at T (entering new valut) 10 Year 1.48 3.287 3.287 0.4 0.01 44.8 1.2 3.2 0.2 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7	e Upper Edge, H <sub>t</sub> = /eir Slope Length = /o-yr Orifice Area = Area w/o Debris = n Area w/ Debris = n Area w/ Debris = // Debri	Calculated Parame           Zone 3 Weir           5.58           4.00           8.43           11.14           5.57           s for Outlet Pipe w,           Zone 3 Restrictor           1.32           0.59           1.98           Calculated Parame           0.93           8.93           1.71           8.83           drographs table (CC           50 Year           2.24           5.457           10.1           0.27           80.3           12.2           1.2	ters for Overflow V Not Selected N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A	Veir           feet           feet           ft²           ft²           ft²           ft²           ft²           ft²           feet           ate           ft²           feet           ft²           feet           radians           31.4           8.333           8.333           8.333           1.24.8           32.0           1.0
User Input: Overflow Weir (Dropbox with Flat of Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length = Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Neter August Andrea Start (in) = CUHP Runoff Volume (acre-ft) = CUHP Runoff Volume (acre-ft) = CUHP Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Row, q (cfs) = Peak Inflow q (cfs) = Peak Outflow Q (cfs) = Ratio Peak Outflow to Predevelopment Q = Structure Controlling Flow = Max Velorix throunk Grate 1 (frec) = Max Velorix throunk Grate 1 (frec) =	r Sloped Grate and Zone 3 Weir 5.58 4.00 0.00 4.00 700 50% C Grate 50% C Grate 0.83 18.00 12.60 Trapezoidal) 7.00 4.00 1.00 C Grate 0.83 18.00 12.60 Trapezoidal) 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.0	Outlet Pipe OR Ref Not Selected N/A N/A N/A N/A N/A N/A N/A N/A estrictor Plate, or R Not Selected N/A N/A N/A ft (relative to basin feet 30' H:V feet <i>30'</i> H:V feet <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>100</i> <i>1</i>	tangular/Trapezoid ft (relative to basin l feet H:V feet % <u>Rectangular Orifice</u> ) ft (distance below be inches inches n bottom at Stage = <i>HP hydrographs and</i> 2 Year 0.95 1.992 1.992 1.992 0.0 0.0 0.0 0.0 0.0 0.9 N/A Vertical Orifice 1 N/A	al Weir and No Out pottom at Stage = 0 1 Gri Ov C asin bottom at Stage Half-Cent = 0 ft) 1 runoff volumes by 5 Year 1.23 2.661 2.661 2.661 0.2 0.1 36.7 1.1 5.1 yertical Orifice 1 N/A	tet Pipe) t) Height of Gratu Overflow W ate Open Area / 10 reflow Grate Open verflow Grate Open verflow Grate Open verflow Grate Open (ate open (	e Upper Edge, H <sub>t</sub> = /eir Slope Length = /0-yr Orifice Area = Area w/o Debris = n Area w/ Debris = n Area w/ Debris = ////////////////////////////////////	Calculated Parame           Zone 3 Weir           5.58           4.00           8.43           11.14           5.57           s for Outlet Pipe w,           Zone 3 Restrictor           1.32           0.59           1.98           Calculated Parame           0.93           8.93           1.71           8.83           drographs table (CC           50 Year           2.24           5.457           10.1           0.27           80.3           12.2           1.2           1.2           1.2           1.2           1.2           1.2	ters for Overflow V Not Selected N/A N/A N/A N/A N/A N/A V Flow Restriction Pl Not Selected N/A N/A N/A N/A N/A ters for Spillway feet feet feet acres acre-ft Dumns W through / 100 Year 2.57 6.531 6.531 18.2 - 0.49 97.6 16.6 0.9 Outlet Plate 1 14	Veir           feet           feet           ft²           ft²           ft²           ft²           feet           ft²           feet           radians           3.14           8.333           8.333           8.333           1.24.8           32.0           1.0           Spillway           1.4
User Input: Overflow Weir (Dropbox with Flat of Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Front Edge Length = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length = Spillway Crest Length = Spillway Crest Length = Spillway Crest Length = Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = CUHP Runoff Volume (acre) = Predevelopment Peak Q (cfs) = Predevelopment Peak Q (cfs) = Peak Inflow Q (cfs) = Ratio Peak Outflow to Predevelopment Q = Structure Controlling Flow = Max Velocity through Grate 1 (fps) = Max Velocity through Grate 1 (fps) =	Sloped Grate and           Zone 3 Weir           5.58           4.00           0.00           4.00           50%           50%           Circular Orifice, R           Cone 3 Restrictor           0.83           18.00           12.60           Trapezoidal)           7.00           31.00           4.00           1.00           7.00           31.00           4.00           1.00           7.00           31.00           4.00           1.00           7.00           31.00           4.00           1.00           7.00           31.00           4.00           1.00           7.00           31.00           4.00           1.00           7.00           31.00           4.00           0.905           N/A           N/A           N/A           N/A           N/A           N/A      N/A	Outlet Pipe OR Ref Not Selected N/A N/A N/A N/A N/A N/A N/A N/A estrictor Plate, or R Not Selected N/A N/A N/A ft (relative to basin feet 30' H:V feet CURV N/A 3.513 N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A	tangular/Trapezoid ft (relative to basin l feet H:V feet % Rectangular Orifice) ft (distance below be inches inches n bottom at Stage = HP hydrographs and 2 Year 0.95 1.992 1.992 1.992 1.992 0.0 0.0 0.9 N/A Vertical Orifice 1 N/A	al Weir and No Out pottom at Stage = 0 I Gri Ov C asin bottom at Stage Half-Cent = 0 ft) = 0 ft) = 1.23 = 2.661 = 2.661 = 0.2 = 0.01 = 0.01 = 0.2 = 0.11 = 5.1 Vertical Orifice 1 N/A N/A	tet Pipe) t) Height of Gratu Overflow W ate Open Area / 10 reflow Grate Open verflow Grate Open verflow Grate Open verflow Grate Open (ate open (	e Upper Edge, H <sub>t</sub> = /eir Slope Length = 10-yr Orifice Area = Area w/o Debris = n Area w/ Debris = n Area w/ Debris = lculated Parameter: utlet Orifice Area = t Orifice Centroid = tor Plate on Pipe = tor Plate on Pipe = Design Flow Depth= Top of Freeboard = Fop of Freeboard = Fop of Freeboard = Fop of Freeboard = 1.88 4.380 4.380 4.380 4.380 4.380 4.380 4.380 4.32 0.07 6.3.2 4.3 1.6 Overflow Weir 1 0.3 N/A	Calculated Parame           Zone 3 Weir           5.58           4.00           8.43           11.14           5.57           S for Outlet Pipe W,           Zone 3 Restrictor           1.32           0.59           1.98           Calculated Parame           0.93           8.93           1.71           8.83           drographs table (CC           5.457           5.457           10.1           0.27           80.3           12.2           1.2           Veriflow Weir 1           1.0           N/A	ters for Overflow V Not Selected N/A N/A N/A N/A N/A N/A N/A V Flow Restriction Pl Not Selected N/A N/A N/A ters for Spillway feet feet acres acre-ft Dumns W through / 100 Year 2.57 6.531 6.531 18.2 0.49 97.6 16.6 0.9 Outlet Plate 1 1.4 N/A	Veir           feet           feet           ft²           ft²           ft²           feet           ate           ft²           feet           radians           3.14           8.333           8.333           1.24.8           32.0           1.0           Spillway           1.4           N/A
User Input: Overflow Weir (Dropbox with Flat of Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length = Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = CUHP Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Riow, q (cfs/acre) = Peak Inflow Q (cfs) = Ratio Peak Outflow to Predevelopment Q = Structure Controlling Flow = Max Velocity through Grate 1 (fps) = Max Velocity through Grate 1 (fps) = Time to Drain 97% of Inflow Volume (hours) =	Sloped Grate and           Zope 3 Weir           5.58           4.00           0.00           4.00           50%           50%           Circular Orifice, R           Cone 3 Restrictor           0.83           18.00           12.60           Trapezoidal)           7.00           31.00           4.00           1.00           7.00           31.00           4.00           1.00           7.00           31.00           4.00           1.00           7.00           31.00           4.00           1.00           7.00           31.00           4.00           1.00           7.00           31.00           4.00           1.00           7.00           9.05           N/A           N/A           N/A           N/A           N/A           N/A           N/A           N/A           N/	Outlet Pipe OR Ref Not Selected N/A N/A N/A N/A N/A N/A N/A estrictor Plate, or R Not Selected N/A N/A N/A t (relative to basir feet 30' H:V feet CURV EURV N/A 3.513 N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A	tangular/Trapezoid ft (relative to basin I feet H:V feet (distance below be inches inches h bottom at Stage = HP hydrographs and 2 Year 0.95 1.992 1.992 1.992 0.00 28.0 0.9 N/A Vertical Orifice 1 N/A Vertical Orifice 1 N/A S4	al Weir and No Out pottom at Stage = 0 1 Gri Ov C asin bottom at Stage Half-Cent = 0 ft)	tet Pipe) t) Height of Gratu Overflow W ate Open Area / 10 rerflow Grate Open verflow Grate Open verflow Grate Open verflow Grate Open (2) = 0 ft) O Outlel ral Angle of Restrice Spillway D Stage at T Basin Area at T Basin Volume at T Basin Volume at T Basin Volume at T (entering new value) 10 Year 1.48 3.287 0.4 0.01 44.8 1.2 3.2 Vertical Orifice 1 N/A N/A 66	e Upper Edge, H <sub>t</sub> = /eir Slope Length = 10-yr Orifice Area = Area w/o Debris = n Area w/ Debris = iculated Parameter: utlet Orifice Area = t Orifice Centroid = tor Plate on Pipe = tor Plate on Pipe = Pesign Flow Depth= Top of Freeboard = Fop of Freeboard = Fop of Freeboard = Fop of Freeboard = 1.88 4.380 4.380 4.380 4.380 4.380 4.380 4.3 0.07 6.3.2 4.3 1.6 Overflow Weir 1 0.3 N/A 72 2.7	Calculated Parame           Zone 3 Weir           5.58           4.00           8.43           11.14           5.57           S for Outlet Pipe w,           Zone 3 Restrictor           1.32           0.59           1.98           Calculated Parame           0.93           8.93           1.71           8.83           drographs table (CC           5.457           5.457           10.1           0.27           80.3           12.2           1.2           0.27           80.3           12.2           1.2           N/A           70	ters for Overflow V Not Selected N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A	Veir           feet           feet           ft²           ft²           ft²           feet           radians           3.14           8.333           3.1.2           0.83           1.24.8           32.0           1.0           Spillway           1.4           N/A           66
User Input: Overflow Weir (Dropbox with Flat of Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage = Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = Inflow Hydrograph Nesults OPTIONAL Override Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, q (cfs/acre) = Peak Inflow Q (cfs) = Peak Inflow Q (cfs) = Max Velocity through Grate 1 (fps) = Max Velocity through Grate 1 (fps) = Time to Drain 97% of Inflow Volume (hours) =	r Sloped Grate and Zone 3 Weir 5.58 4.00 0.00 4.00 50% Circular Orifice, R Cone 3 Restrictor 0.83 18.00 12.60 Trapezoidal) 7.00 4.00 1.00 7.00 4.00 1.00 7.00 7.00 7.00 4.00 1.00 7.00 7.00 7.00 4.00 1.00 7.00 7.00 7.00 7.00 7.00 7.00 7	Outlet Pipe OR Ree Not Selected N/A N/A N/A N/A N/A N/A N/A estrictor Plate, or R Not Selected N/A N/A N/A t (relative to basir feet 30' H:V feet CURV Reet N/A S.513 N/A N/A N/A N/A N/A N/A N/A S.513 N/A N/A N/A N/A N/A S.513 N/A N/A S.513 N/A N/A S.513 N/A N/A S.513 N/A N/A S.513 N/A N/A S.513 N/A N/A S.513 N/A N/A S.513 N/A N/A S.513 N/A N/A S.513 N/A N/A S.513 N/A N/A S.513 N/A N/A S.513 N/A N/A S.513 N/A N/A S.513 N/A N/A S.513 N/A N/A N/A S.513 N/A N/A S.513 N/A N/A S.513 N/A N/A S.513 N/A N/A N/A S.513 N/A N/A N/A N/A N/A S.513 N/A N/A N/A S.513 N/A N/A N/A S.513 N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A	tangular/Trapezoid ft (relative to basin I feet H:V feet % Rectangular Orifice) ft (distance below be inches inches inches n bottom at Stage = <i>HP hydrographs and</i> 2 Year 0.95 1.992 1.992 0.0 0.00 28.0 0.9 N/A Vertical Orifice 1 N/A VA 54 58 000	al Weir and No Out pottom at Stage = 0 1 Gri Ov C asin bottom at Stage Half-Cent = 0 ft)	tet Pipe) t) Height of Gratu Overflow W ate Open Area / 10 rerflow Grate Open verflow Grate Open verflow Grate Open verflow Grate Open (22) = 0 ft) O Outlel ral Angle of Restrice Spillway D Stage at T Basin Area at T Basin Volume at T Basin Volume at T (entering new value) 10 Year 1.48 3.287 3.287 0.4 0.01 44.8 1.2 3.2 Vertical Orifice 1 N/A 66 71 5 11	e Upper Edge, H <sub>t</sub> = /eir Slope Length = /o-yr Orifice Area = Area w/o Debris = n Area w/ Debris = iculated Parameter: ////////////////////////////////////	Calculated Parame           Zone 3 Weir           5.58           4.00           8.43           11.14           5.57           s for Outlet Pipe w,           Zone 3 Restrictor           1.32           0.59           1.98           Calculated Parame           0.93           8.93           1.71           8.83           drographs table (CC           50 Year           2.24           5.457           5.457           10.1           0.27           80.3           12.2           1.2           0.27           80.3           12.2           1.2           0.77           1.0           N/A           70           6.14	ters for Overflow V Not Selected N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A	Veir           feet           feet           ft²           ft²           ft²           ft²           ft²           ft²           feet           radians           31.4           8.333           31.2           0.83           1.0           Spillway           1.4           N/A           66           7.6
User Input: Overflow Weir (Dropbox with Flat of Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Front Edge Length = Overflow Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage = Spillway Crest Length = Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = Predevelopment Deak Q (cfs) = Predevelopment Peak Q (cfs) = Predevelopment Peak Q (cfs) = Ratio Peak Outflow to Predevelopment Q = Structure Controlling Flow = Max Velocity through Grate 1 (fps) = Max Velocity through Grate 1 (fps) = Time to Drain 99% of Inflow Volume (hours) = Time to Drain 99% of Inflow Volume (hours) = Maximum Ponding Depth (ftr) =	r Sloped Grate and Zone 3 Weir 5.58 4.00 0.00 4.00 50% 2 (Circular Orifice, R 2 Table 2 Cone 3 Restrictor 0.83 18.00 12.60 7.00 7.00 4.00 1.00 7.00 7.00 7.00 7.00 7.00 7.00 7	Outlet Pipe OR Ref Not Selected N/A N/A N/A N/A N/A N/A N/A estrictor Plate, or R Not Selected N/A N/A N/A ft (relative to basir feet 30' H:V feet ride the default CU/ feet ride the default CU/ EURV N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A	tangular/Trapezoid ft (relative to basin I feet H:V feet % Rectangular Orifice) ft (distance below be inches inches n bottom at Stage = <i>IHP hydrographs and</i> 2 Year 0.95 1.992 1.992 1.992 0.0 0.00 28.0 0.9 N/A Vertical Orifice 1 N/A VA 58 4.09 1.11	al Weir and No Out pottom at Stage = 0 i Gra Ov C asin bottom at Stage Half-Cent = 0 ft)	tet Pipe) t) Height of Gratu Overflow W ate Open Area / 10 rerflow Grate Open verflow Grate Open verflow Grate Open verflow Grate Open (Ca Ca = 0 ft) O Outle ral Angle of Restrict Spillway D Stage at T Basin Area at T Basin Volume at T Basin Volume at T Centering new Value 10 Year 1.48 3.287 0.4 0.01 44.8 1.2 3.2 Vertical Orifice 1 N/A 66 71 5.11 1.29	e Upper Edge, H <sub>t</sub> = /eir Slope Length = 10-yr Orifice Area = Area w/o Debris = n Area w/ Debris = n Area w/ Debris = lculated Parameter: utlet Orifice Area = t Orifice Centroid = tor Plate on Pipe = tor Plate on Pipe = Pesign Flow Depth= Top of Freeboard = Fop of Freeboard = Fop of Freeboard = Fop of Freeboard = 1.88 4.380 4.380 2.7 0.07 63.2 4.3 1.6 Overflow Weir 1 0.3 N/A 72 78 5.81 1.38	Calculated Parame           Zone 3 Weir           5.58           4.00           8.43           11.14           5.57           S for Outlet Pipe w,           Zone 3 Restrictor           1.32           0.59           1.98           Calculated Parame           0.93           8.93           1.71           8.83           drographs table (CC           5.457           5.457           10.1           0.27           80.3           12.2           0.27           80.3           12.2           0.27           80.3           12.2           0.77           6.14           1.41	ters for Overflow V Not Selected N/A N/A N/A N/A N/A N/A N/A V Flow Restriction P Not Selected N/A N/A N/A N/A N/A N/A N/A N/A	Veir           feet           feet           ft²           ft²           ft²           ft²           feet           faile           ft²           feet           faile           feet           feet           faile           feet           saile           faile           feet           saile           feet           saile           saile           feet           saile           saile           feet           saile           saile           feet           saile           feet           saile           feet           saile           feet           saile           saile           feet           saile           feet           feet           saile           feet           feet           saile           feet           saile           feet <t< td=""></t<>
User Input: Overflow Weir (Dropbox with Flat c Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage = Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = CUHP Runoff Volume (acre-ft) = Inflow Hydrograph Nesults Override Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, q (cfs/acre) = Predevelopment Unit Peak Flow, q (cfs/acre) = Predevelopment Unit Peak Rlow, q (cfs/acre) = Ratio Peak Outflow to Predevelopment Q = Structure Controlling Flow = Max Velocity through Grate 1 (fps) = Max Velocity through Grate 1 (fps) = Maximum Ponding Depth (fit) = Time to Drain 97% of Inflow Volume (hours) = Time to Drain 97% of Inflow Volume (hours) = Maximum Ponding Depth (fit) = Area at Maximum Ponding Depth (fit) = Maximum Nolume Stored (acre-ft) = Maximum Volume Stored (acre-ft) =	r Sloped Grate and Zone 3 Weir 5.58 4.00 0.00 4.00 50% 2 (Circular Orifice, R 2 one 3 Restrictor 0.83 18.00 12.60 7.00 4.00 1.00 7.00 4.00 1.00 7.00 7.00 7.00 7.00 7.00 7.00 7	Outlet Pipe OR Ref Not Selected N/A N/A N/A N/A N/A N/A N/A N/A N/A estrictor Plate, or R Not Selected N/A N/A N/A ft (relative to basir feet 30' H:V feet CURV N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A	tangular/Trapezoid ft (relative to basin I feet H:V feet % Rectangular Orifice) ft (distance below be inches inches n bottom at Stage = (HP hydrographs and 2 Year 0.95 1.992 1.992 1.992 0.00 28.0 0.9 0.00 28.0 0.9 0.9 1.992 1.11 1.11 1.843	al Weir and No Out pottom at Stage = 0 1 Gra Ov C asin bottom at Stage Half-Cent = 0 ft)	let Pipe) it) Height of Gratu Overflow W ate Open Area / 10 erflow Grate Open iverflow Grate Open iverflow Grate Open iverflow Grate Open (and the o	e Upper Edge, H <sub>t</sub> = /eir Slope Length = 10-yr Orifice Area = Area w/o Debris = n Area w/ Debris = n Area w/ Debris = lculated Parameter: utlet Orifice Area = t Orifice Centroid = tor Plate on Pipe = lesign Flow Depth= Top of Freeboard = Top of Freeboard = Top of Freeboard = Fop of Freeboard = 1.88 4.380 2.7 0.07 63.2 4.3 1.6 Overflow Weir 1 0.3 N/A 72 78 5.81 1.38 4.025	Calculated Parame           Zone 3 Weir           5.58           4.00           8.43           11.14           5.57           s for Outlet Pipe w.           Zone 3 Restrictor           1.32           0.59           1.98           Calculated Parame           0.93           8.93           1.71           8.83           Corgraphs table (CC           50 Year           2.24           5.457           10.1           0.27           80.3           12.2           0.27           80.3           12.2           1.41           1.0           N/A           70           777           6.14           1.41	ters for Overflow V Not Selected N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A	Veir           feet           feet           ft²           ft²           ft²           ft²           feet           radians

please make adjustments to the design to reduce the peak outflow

24013\_MHFD-Detention\_v4-06.xlsm, Outlet Structure

![](_page_63_Figure_0.jpeg)

#### DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename:

	Inflow Hydrog	raphs								
	The user can o	verride the calcu	ulated inflow hyd	drographs from	this workbook v	vith inflow hydro	graphs develop	ed in a separate	program.	
	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.41	0.15	1.39
	0:15:00	0.00	0.00	1.96	4.13	5.67	4.54	6.47	6.55	9.28
	0:20:00	0.00	0.00	10.17	14.41	17.82	12.83	16.29	17.90	22.85
	0:25:00	0.00	0.00	22.73	30.27	37.75	27.19	33.38	36.88	47.13
	0:30:00	0.00	0.00	27.98	36.69	44.83	53.49	68.05	/8.35	100.82
	0:40:00	0.00	0.00	24.02	30.64	36.92	61.10	77.42	94.72	120.98
	0:45:00	0.00	0.00	21.02	27.15	32.85	54.83	69.22	86.46	110.57
	0:50:00	0.00	0.00	18.32	24.16	28.92	49.33	62.03	77.42	99.29
	0:55:00	0.00	0.00	16.01	21.20	25.46	43.07	53.91	68.17	87.37
	1:00:00	0.00	0.00	14.26	18.82	22.81	37.28	46.41	60.01	76.85
	1:05:00	0.00	0.00	13.13	17.28	21.14	32.83	40.67	53.68	68.84
	1:10:00	0.00	0.00	10.36	16.08	19.81	28.99	35.78	46.27	59.18
	1:20:00	0.00	0.00	9.12	12.88	16.19	22.05	27.13	32.81	41.62
	1:25:00	0.00	0.00	7.94	11.28	14.22	18.89	23.00	26.69	33.73
	1:30:00	0.00	0.00	6.96	9.97	12.19	15.65	18.95	21.43	26.95
	1:35:00	0.00	0.00	6.31	9.11	10.82	12.87	15.47	17.03	21.29
	1:40:00	0.00	0.00	5.98	8.20	10.03	11.00	13.15	14.05	17.50
	1:45:00	0.00	0.00	5.82	7.45	9.51	9.88	11.79	12.31	15.27
	1:50:00	0.00	0.00	5./1	6.92	9.13	9.15	10.91	10.29	13.79
	2:00:00	0.00	0.00	4.54	6.07	8.02	8.31	9.90	9.82	12.04
	2:05:00	0.00	0.00	3.59	4.83	6.37	6.66	7.93	7.74	9.47
	2:10:00	0.00	0.00	2.72	3.65	4.81	5.00	5.95	5.74	7.00
	2:15:00	0.00	0.00	2.07	2.76	3.63	3.77	4.48	4.31	5.25
	2:20:00	0.00	0.00	1.55	2.07	2.71	2.83	3.36	3.24	3.95
	2:25:00	0.00	0.00	1.16	1.53	2.01	2.10	2.49	2.42	2.95
	2:30:00	0.00	0.00	0.85	0.79	1.4/	1.53	1.82	1.78	2.16
	2:40:00	0.00	0.00	0.01	0.56	0.77	0.82	0.97	0.95	1.15
	2:45:00	0.00	0.00	0.28	0.38	0.52	0.56	0.67	0.65	0.79
	2:50:00	0.00	0.00	0.16	0.24	0.32	0.36	0.42	0.41	0.50
	2:55:00	0.00	0.00	0.08	0.13	0.17	0.20	0.23	0.23	0.27
	3:00:00	0.00	0.00	0.03	0.06	0.07	0.09	0.10	0.10	0.11
	3:05:00	0.00	0.00	0.01	0.01	0.02	0.02	0.02	0.02	0.02
	3:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:40:00 5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0.00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

#### DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.06 (July 2022)

Summary Stage-Area-Volume-Discharge Relationships The user can create a summary S-A-V-D by entering the desired stage increments and the remainder of the table will populate automatically. The user should graphically compare the summary S-A-V-D table to the full S-A-V-D table in the chart to confirm it captures all key transition points.

Stage - Storage	Stage	Area	Area	Volume	Volume	Total Outflow	
Description	[ft]	[ft <sup>2</sup> ]	[acres]	[ft <sup>3</sup> ]	[ac-ft]	[cfs]	
							For best results, include the
							stages of all grade slope
							changes (e.g. ISV and Floor)
							from the S-A-V table on
							Sheet Dash.
							Also include the inverts of all
							outlets (e.g. vertical orifice,
							overflow grate, and spillway, where applicable).
							1
							1
							1

![](_page_66_Picture_0.jpeg)

Schmidt Parcel – District Infrastructure Final Drainage Report Project No: 24013

#### **APPENDIX E – REFERENCE MATERIAL**

RECEIVED

MAY 10 1996

Planning Dapla

#### **SILVER PONDS SUBDIVISION FILING NO. 1**

#### FINAL DRAINAGE REPORT

February 2, 1995 Revised May 5, 1996 Project No. 60572

#### **PREPARED FOR:**

The Campbell Corporation 4975 Austin Bluffs Parkway Colorado Springs, CO 80918

#### **PREPARED BY:**

M.V.E., Inc. 1911 Lelaray St. Colorado Springs, CO 80909

60572fdr.wp6-d49

Design	Included Basins	Cumulative	5-yr	100-yr
Point		Drainage Area	Discharge	Discharge
		(Ac)	(cfs)	(cfs)
1	OSA1	18.14	13.1	30.4
2	OSA2	8.72	7.0	16.3
3	OSA1 thru A3	29.05	20.5	47.7
4	OSA1 thru A4	31.04	24.3	53.6
5	OSB1	39.26	29.8	69.3
6	OSB1 thru B2	44.66	25.9	60.3
7	OSB1 thru B3	50.03	35.7	83.1
8	OSB1 thru B4	52.02	39.2	89.8
9	OSD1	8.26	7.9	18.4
10	OSD1 thru D2	19.95	24.1	52.9
11	D3	3.41	4.5	9.9
12	E1	4.24	5.5	12.1
13	F1	4.26	6.6	14.4
14	OSG1	6.66	7.0	16.4
15	OSG1 thru G2	9.22	10.5	24.0
16	OSH1	17.22	17.5	38.4
17	OSH1 thru H2	28.28	27.9	61.3
18	OSI1	3.67	3.3	7.8
19	OSI1 thru I2	11.05	7.9	18.4
20	I3	8.01	6.3	14.6
21	OSI1 thru I4	27.16	19.0	44.2
22	J1	4.19	3.0	6.9

0

-

-

2

### Table 3.1 - Developed Condition Hydrologic Data

5-year and 100-Year

10

#### M.V.E., Inc. Colorado Springs, Colorado

Proj. No.: 60572 Project: SILVER PONDS

DEVELOPED DISCHARGES RAINFALL/RUNOFF ANALYSIS - RATIONAL METHOD i100 Q100 Design Area CS C100 Tc i5 05 Point (Ac) (min) (in/hr) (in/hr)(cfs) (cfs) \_\_\_\_\_\_ \_\_\_\_\_ 30.4 1 18.14 0.30 0.40 27.7 2.40 4.20 13.1 16.3 2 8.72 0.30 0.40 22.9 2.68 4.68 7.0 25.4 4.41 29.8 69.3 5 39.26 0.30 0.40 2.53 0.40 3.19 5.57 7.9 18.4 9 8.26 0.30 16.5 0.40 3.52 6.15 7.0 16.4 14 6.66 0.30 13.5 38.4 17.22 0.39 0.49 24.1 2.60 4.55 17.5 16 7.8 18 3.67 0.30 0.40 18.2 3.03 5.30 3.3 47.7 0.30 0.40 28.7 2.35 4.11 20.5 3 29.05 0.34 0.43 29.8 2.30 4.02 24.3 53.6 4 31.04 60.3 3.38 25.9 0.30 0.40 39.5 1.93 6 44.66 4.29 4.0 9.2 33 5.37 0.30 0.40 26.7 2.45 7 50.03 0.30 0.40 28.2 2.38 4.15 35.7 83.1 4.11 39.2 89.8 0.42 28.7 2.35 52.02 0.32 8 0.39 0.49 17.6 3.09 5.39 14.1 30.9 D2 11.69 52.9 24.1 10 19.95 0.39 0.49 17.5 3.10 5.41 0.39 11 3.41 0.49 14.5 3.40 5.94 4.5 9.9 5.85 0.49 15.0 3.35 5.5 12.1 12 4.24 0.39 3.94 6.89 6.6 14.4 13 4.26 0.39 0.49 10.5 7.8 6.24 3.6 G2 2.56 0.39 0.49 13.1 3.57 24.0 0.43 14.0 3.46 6.04. 10.5 15 9.22 0.33 H2 11.06 0.39 0.49 17.5 3.10 5.41 13.4 29.3 0.39 0.49 25.3 2.53 4.42 27.9 61.3 28.28 17 18.4 11.05 0.30 0.40 28.0 2.39 4.17 7.9 19 6.3 14.6 0.40 23.9 4.57 20 8.01 0.30 2.62 0.40 23.1 2.67 4.66 6.5 15.1 14 8.10 0.30 44.2 0.30 0.40 29.2 2.33 4.07 19.0 21 27.16 22 4.19 0.30 0.40 28.8 2.35 4.10 3.0 6.9

Date: 1-31-96

![](_page_70_Figure_0.jpeg)

![](_page_71_Picture_0.jpeg)

City of Colorado Springs 30 S. Nevada Ave Colorado Springs, CO 80903

# COTTONWOOD CREEK DRAINAGE BASIN PLANNING STUDY FINAL REPORT JULY 2019

C. TOR

Department of Public Works Water Resources Engineering

10 104 102.2

Prepared by:

![](_page_71_Picture_5.jpeg)










	0.12 mi <sup>2</sup>	
UC050 0.27 mi <sup>2</sup>		4 The
	UC100	
	0.34 mi <sup>2</sup>	
UC060	0.24 mi <sup>2</sup>	A Line
0.23 mi <sup>2</sup>		
70		15 128 143
mi <sup>2</sup>		
UC080 0.18 mi <sup>2</sup>		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
-		
WR120		M. N.
0.05 mi <sup>2</sup>	4 ~	
	0.10 mi <sup>2</sup>	AL A
		and the second s
		1
		7 5 10 13 13
		1
BRIARGATE PKWY		A Company
		10 States
0.19 mi <sup>2</sup>		1
0.23 mi <sup>2</sup>	Future Land Use - Cottonwood	Creek
	Land Use	% of Basin Area
	0-1.99 du/ac	5.3%
UC165	12.0-24.99 du/ac	1.7%
		0.3%
	2.5 AGRE RURAL RESIDENTIAL	7.0%
UC150 0.09 mi <sup>2</sup>	3 5-7 99 du/ac	21.4%
	35 ACRE TRACT	1.4%
	5 ACRE RURAL RESIDENTIAL	8.7%
	8.0-11.99 du/ac	2.8%
	CIVIC	4.7%
UC160	COMMERCIAL	8.7%
		1.3%
	INDUSTRIAL	1.8%
	NATURAL OPEN SPACE (PAIR CONDITION)	0.0%
	PARK/OPEN SPACE (FAIR CONDITION)	1.6%
A LEE LE PARTIE LE PARTIE	PARK/OPEN SPACE (GOOD CONDITION)	0.9%
and a start of the	ROW	13.5%
ure Development	WOODS (FAIR CONDITION)	2.9%
Planned		
The second se	Future Land Use - South Pine	Creek
	and liep	% of Basin Aroa
		0.7%
A set / A Barriston and another	12.0-24.99 du/ac	1.9%
And	2.0-3.49 du/ac	4.2%
	25+ du/ac	0.0%
	3.5-7.99 du/ac	29.4%
ALL DATE OF A STRAT	8.0-11.99 du/ac	2.3%
		6.2%
		18.1%
		4.2%
100 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		1.6%
	PARK/OPEN SPACE (FAIR CONDITION)	5.4%
	PARK/OPEN SPACE (GOOD CONDITION)	1.1%
	ROW	20.8%
CONTRACTOR OF A		

#### FIGURE 3-6 FUTURE CITY & COUNTY LAND USE COTTONWOOD CREEK & SOUTH PINE CREEK DBPS COLORADO SPRINGS, CO



1,000 2,000 3,000









# **SAND CREEK DRAINAGE BASIN PLANNING STUDY FINAL REPORT JANUARY 2021**

### Prepared for:





## Prepared by:

**Stantec** 



#### SAND CREEK - SAND CREEK DRAINAGE BASIN PLANNING STUDY

Basin Characteristics and Environmental Resources



Disclaiment his document has appended based on into matching powled by others as cles in the Notes section. General werked the accuracy analytic completeness of this information and chall not be responsible for any ensuing an other sections, which may as meaperated herein as a result. Barted assumes no response if the supplied in electronic formal, and the required accepts to i responsibility for vertiging the accuracy and completeness of the data.

Figure 2-7: NWI Wetlands Located in Sand Creek Drainage Basin (Page 4)

Dame & of a

#### SAND CREEK - SAND CREEK DRAINAGE BASIN PLANNING STUDY

Hydrology



Figure 3-15. Future Land Use MapFuture Condition Model Results





epared from the best data available at the time of plotting and is for internal use only. El Paso Colorado, makes no claim as to the completeness or accuracy of the data contained hereon. **GENERAL NOTES** 

- 1. ALL MATERIALS AND INSTALLATION PROCEDURES SHALL BE IN COMPLIANCE WITH THE CITY OF COLORADO SPRINGS, DEPARTMENT OF PUBLIC WORKS, SUBDIVISION POLICY MANUAL AND DIVISION "RULES FOR THE INSTALLATION OF SEWER MAINS AND SERVICES".
- 2. IT SHALL BE THE RESPONSIBILITY OF THE CONTRACTOR TO VERIFY THE EXISTENCE AND LOCATION OF ALL UNDERGROUND UTILITIES ALONG THE ROUTE OF THE WORK. THE OMISSION FROM OR THE INCLUSION OF UTILITY LOCATIONS ON THE PLANS IS NOT TO BE CONSIDERED AS THE NONEXISTENCE OF OR A DEFINITE LOCATION OF EXISTING UNDERGROUND UTILITIES.
- 3. THE CONTRACTOR WILL TAKE THE NECESSARY PRECAUTIONS TO PROTECT EXISTING UTILITIES FROM DAMAGE DUE TO THIS OPERATION. ANY DAMAGE TO THE UTILITIES WILL BE REPAIRED AT THE CONTRACTOR'S EXPENSE, AND ANY SERVICE DISRUPTION WILL BE SETTLED BY THE CONTRACTOR.
- 4. CONCRETE USED IN CURB AND GUTTER, SIDEWALK, AND CROSSPAN CONSTRUCTION WILL HAVE A MINIMUM COMPRESSIVE STRENGTH OF 4,000 PSI AT 28 DAYS.
- 5. ALL BACKFILL, SUB-BASE, AND/OR BASE COURSE (CLASS 6) MATERIAL SHALL BE COMPACTED PER THE SOILS ENGINEER'S RECOMMENDATIONS.
- 6. ALL STATIONING IS CENTERLINE OF IMPROVEMENTS UNLESS OTHERWISE INDICATED. ALL ELEVATIONS ARE FLOW LINE UNLESS OTHERWISE INDICATED AS TOP BACK OF CURB (TBC), ASPHALT (ASP), OR TOP OF INLET OR BOX (TOB).
- 7. ALL CURB RETURNS AND 10' EITHER SIDE OF CURB RETURNS SHALL BE 8" VERTICAL CURB, CITY OF COLORADO SPRINGS TYPE 1 CURB WITH AND ADDITIONAL 10' OF TRANSITION TO 6" RAMP CURB. CITY OF COLORADO SPRINGS MODIFIED TYPE 5 CURB, UNLESS OTHERWISE INDICATED.
- 8. PEDESTRIAN RAMPS SHALL BE INSTALLED AT INTERSECTIONS AS SHOWN AND CONFORM TO THE CITY OF COLORADO SPRINGS, DEPARTMENT OF PUBLIC WORKS STANDARDS AND SPECIFICATIONS. NOTE: WDTH OF PEDESTRIAN RAMPS MUST MATCH WDTH OF SIDEWALK.
- 9. IF A DISCREPANCY OCCURS BETWEEN THE CONSTRUCTION DOCUMENTS AND THE CITY OF COLORADO SPRINGS STANDARD SPECIFICATIONS, THE ENGINEER WILL BE NOTIFIED IMMEDIATELY FOR RESOLUTION.
- 10. THE CONTRACTOR SHALL SECURE ALL APPLICABLE LICENSES AND PERMITS TO COMPLETE THE CONSTRUCTION IN COMPLIANCE WITH ALL LOCAL, STATE. AND FEDERAL REGULATIONS.
- 11. CONTRACTOR TO OBTAIN COPIES OF THE SOILS REPORT FROM THE GEOTECHNICAL ENGINEER AND TO BE KEPT ON-SITE DURING ALL EARTHWORK OPERATIONS.

#### CONCRETE: CONCRETE REINFORCEMENT:

- 1. ALL CAST IN PLACE CONCRETE SHALL HAVE A MINIMUM COMPRESSIVE YIELD STRENGTH OF 4,000 PSI UNLESS OTHERWISE NOTED. HIGHER COMPRESSIVE STRENGTH CONCRETE IS ACCEPTABLE TO ACHIEVE EARLY CONCRETE STRENGTH THAT MAY BE DEEMED NECESSARY TO MEET CONSTRUCTION SCHEDULING PRIORITIES.
- 2. ALL CAST IN PLACE CONCRETE REINFORCEMENT SHALL HAVE A MINIMUM TENSILE YIELD STRENGTH OF 6,000 PSI UNLESS OTHERWISE NOTED, AND CONFORMANCE WITH CITY OF COLORADO SPRINGS SPECIFICATIONS, SECTION 603.
- 3. CONCRETE TESTING SHALL BE IN CONFORMANCE WITH CITY OF COLORADO SPRINGS SPECIFICATIONS. SECTION 506.

#### STORM SEWER NOTES:

- 1. CONSTRUCT AND INSTALL D-10-R INLETS PER CITY OF COLORADO SPRINGS SHEET D-10-R 1, 2, AND 3.
- 2. CONSTRUCT AND INSTALL TYPE I MANHOLES PER CITY OF COLORADO SPRINGS SHEETS D-20A (1) AND D-20D (4).
- 3. THE MINIMUM CLASS OF REINFORCED CONCRETE PIPE SHALL BE CLASS III.
- TRAFFIC ENGINEERING GENERAL NOTES:
- 1. CALL BEFORE EXCAVATING, CONTRACTOR SHALL VERIFY LOCATION OF UNDERGROUND UTILITIES.
- 2. CONTRACTOR SHALL BE RESPONSIBLE FOR ANY MONUMENTATION AND/OR BENCHMARKS WHICH WILL BE DISTURBED OR DESTROYED BY CONSTRUCTION. SUCH POINTS SHALL BE REFERENCED AND REPLACED WITH APPROPRIATE MONUMENTATION BY A REGISTERED CIVIL ENGINEER AUTHORIZED TO PRACTICE LAND SURVEYING.
- 3. APPROVAL OF THESE PLANS BY THE CITY ENGINEER DOES NOT AUTHORIZE ANY WORK TO BE PERFORMED UNTIL A PERMIT HAS BEEN ISSUED.
- 4. THE APPROVAL OF THESE PLANS OR ISSUANCE OF A PERMIT BY THE CITY OF COLORADO SPRINGS DOES NOT AUTHORIZE THE SUBDIVIDER AND OWNER TO VIOLATE ANY FEDERAL, STATE, OR CITY LAWS, ORDINANCES, REGULATIONS, OR POLICIES.
- 5. THE CONTRACTOR SHALL BE RESPONSIBLE FOR ALL NEW, TEMPORARY AND EXISTING TRAFFIC SIGNS FROM THE START OF THE CONSTRUCTION PROJECT UNTIL ACCEPTANCE BY CITY TRAFFIC ENGINEERING.
- 6. ALL TRAFFIC SIGNS, PAVEMENT MARKINGS, AND TRAFFIC SIGNALS SHALL MEET OR EXCEED M.T.U.C.D. STANDARDS.
- 7. THE CONTRACTOR SHALL NOT REMOVE ANY EXISTING SIGNS, PAVEMENT MARKINGS OR TRAFFIC SIGNALS DURING THE PROJECT WITHOUT SIGNED AUTHORIZATION OF THE CITY TRAFFIC ENGINEERING INSPECTOR ASSIGNED TO THE PROJECT.
- 8. CONTRACTOR SHALL PREPARE A DETAILED TRAFFIC CONTROL PLAN, SUBMIT TO CITY TRAFFIC ENGINEERING FOR APPROVAL, AND OBTAIN APPROPRIATE PERMITS IN ACCORDANCE WITH THE "TRAFFIC CONTROLS FOR STREET CONSTRUCTION, UTILITY WORK AND MAINTENANCE OPERATIONS", M.U.T.C.D. SUPPLEMENT FOR THE CITY OF COLORADO SPRINGS. AUGUST 1992.
- 9. THE CONTRACTOR SHALL BE RESPONSIBLE FOR ALL WORK ZONE TRAFFIC CONTROL. CONTRACTOR SHALL BE RESPONSIBLE FOR FURNISHING. INSTALLING AND MAINTAINING THE TEMPORARY TRAFFIC CONTROL DEVICES THROUGHOUT THE DURATION OF THE PROJECT.
- 10. THE CONTRACTOR SHALL BE RESPONSIBLE FOR ALL NEW, TEMPORARY, AND EXISTING TRAFFIC SIGNAL MODIFICATIONS.



THE CITY OF COLORADO SPRINGS RECOGNIZES THE DESIGN ENGINEER AS HAVING RESPONSIBILITY FOR THE DESIGN; THE CITY HAS LIMITED ITS SCOPE OF REVIEW ACCORDINGLY. RESUBMITTAL REQUIRED IF CONSTRUCTION HAS NOT COMMENCED WITHIN 180 DAYS AFTER REVIEW DATE.





# TRAILS AT FOREST MEADOWS FILING NO. 3 CITY OF COLORADO SPRINGS, EL PASO COUNTY, STATE OF COLORADO STREET IMPROVEMENT PLANS (INCLUDING STORM SEWER)



### **AGENCIES** OWNER:

**CIVIL ENGINEER:** 

**ENGINEERING DIVISION:** 

TRAFFIC ENGINEERING:

**DEVELOPMENT SERVICES:** 

GAS DEPARTMENT:

**ELECTRIC DEPARTMENT:** 

**COMMUNICATIONS:** 

CHALLENGER HOMES, INC. 13570 NORTHGATE ESTATES DRIVE COLORADO SPRINGS, CO 80921 ROGER MILLER (719) 598-5192 ROGEROMYCHALLENGERHOMES.COM M

NO. 3 SHEET

FILING COVER

MEADOWS NT PLANS

Ś

FORE

AT

F

IMPROVEMEN

L\_

ليبا

N

S

SPRIN 555.54

20 BOULDER COLORADO PHONE: 719,5

ND ON NVIL

S101

8

Б

N/A N/A

AS AS

9

M & S CIVIL CONSULTANTS, INC. 20 BOULDER CRESCENT, SUITE 110 COLORADO SPRINGS, CO 80903 VIRGIL A. SANCHEZ P.E. (719) 955-5485

CITY OF COLORADO SPRINGS 30 S. NEVADA AVE., SUITE 401 COLORADO SPRINGS, CO 80903 ELIZABETH NIJKAMP, P.E. (719) 385-5410

CITY OF COLORADO SPRINGS 30 S. NEVADA AVE., SUITE 401 COLORADO SPRINGS, CO 80903 KATHLEEN KRAGER (719) 385-7628

COLORADO SPRINGS UTILITIES 1521 HANCOCK EXPRESSWAY COLORADO SPRINGS, CO 80903

AL JUVERA (719) 668-8769

COLORADO SPRINGS UTILITIES 7710 DURANT DR. COLORADO SPRINGS, CO 80920 TIM WENDT (719) 668-3556

COLORADO SPRINGS UTILITIES 7710 DURANT DR. COLORADO SPRINGS, CO 80920 SARAH LABARRE (719) 668-4933

**OWEST COMMUNICATIONS** (U.N.C.C. LOCATORS) (800) 922-1987 AT&T (LOCATORS) (719) 635-3674

### DETAILED DRAINAGE CONSTRUCTION PLANS AND SPECIFICATIONS ENGINEER'S STATEMENT:

THESE DETAILED PLANS AND SPECIFICATIONS WERE PREPARED UNDER MY DIRECTION AND SUPERVISION. SAID DETAILED PLANS AND SPECIFICATIONS HAVE BEEN PREPARED ACCORDING TO THE ESTABLISHED CRITERIA FOR DETAILED DRAINAGE PLANS AND SPECIFICATIONS, AND SAID DETAILED PLANS AND SPECIFICATIONS ARE IN CONFORMITY WITH THE MASTER PLAN OF THE DRAINAGE BASIN. SAID DETAILED DRAINAGE PLANS AND SPECIFICATIONS MEET THE PURPOSES FOR WHICH THE PARTICULAR DRAINAGE FACILITY(S) IS DESIGNED. I ACCEPT RESPONSIBILITY FOR ANY LIABILITY CAUSED BY ANY NEGLIGENT ACTS, ERRORS OR OMISSIONS ON MY PART IN PREPARATION OF THE DETAILED DRAINAGE PLANS AND SPECIFICATIONS."

VIRGIL A. SANCHEZ, COLORADO P.E. NO. 37160 FOR AND ON BEHALF OF M&S CIVIL CONSULTANTS, INC.

PLAN REVIEW BY CITY OF COLORADO SPRINGS IS PROVIDED ONLY FOR GENERAL CONFORMANCE WITH DESIGN CRITERIA. THE CITY OF COLORADO SPRINGS IS NOT RESPONSIBLE FOR THE ACCURACY AND ADEQUACY OF THE DESIGN, DIMENSIONS, AND/OR ELEVATIONS WHICH SHALL BE CONFIRMED AT THE JOB SITE. THE CITY OF COLORADO SPRINGS, THROUGH THE APPROVAL OF THIS DOCUMENT, ASSUMES NO RESPONSIBILITY FOR COMPLETENESS AND/OR ACCURACY OF THIS DOCUMENT.

### SHEET INDEX

SHEET	1	TITLE SHEET
SHEET	2	PLAN & PROFILE - VANDERWOOD ROAD
SHEET	3	PLAN & PROFILE - VANDERWOOD ROAD
SHEET	4	PLAN & PROFILE - CEDAR BRUSH COURT
SHEET	5	PLAN & PROFILE - CREEK BRUSH DRIVE & BRUSH TOP ROAD
SHEET	6	PLAN & PROFILE - VOLLMER ROAD
SHEET	7	VANDERWOOD ROAD STORM DRAIN AND INLETS
SHEET	8	SIGNAGE AND STRIPING PLAN

PROJECT DATUM VERTICAL - NATIONAL GEODETIC VERTICAL DATUM 1929 (NGVD29) HORIZONTAL - NORTH AMERICAN DATUM 1983 (NAD83) CONTROL - COLORADO STATE PLANE CENTRAL ZONE

FINAL REVIEW:

DRAINAGE REVIEW:\_

2001. AS AMENDED

DRAINAGE DESIGN:

DESIGN DATA: \* FULL DEPTH ASPHALT SIDEWALKS: WIDTH ASPHALT THICKNESS: LOCATION: Attached D AC Surface -----Detached CENTERED IN 5' EASEMENT AC Base <del>XQQX</del> CURB TYPE AGG. BASE THICKNESS: 1 🔯 CURB TYPE 5 0 Class 6 H S P DATE: \_\_\_\_ EOP-EOP \_\_ ROW WIDTH Class 5 FILED IN ACCORDANCE WITH SECTION 7-7-906 OF COLORADO SPRINGS CODE RES\_\_\_\_HVEEM STREET TYPE Class 2 CAUTION





GRADING AND EROSION CONTROL NOTES:

- ANY LAND DISTURBANCE BY ANY OWNER, DEVELOPER, BUILDER, CONTRACTOR, OR OTHER PERSON SHALL COMPLY WITH THE BASIC GRADING, EROSION AND STORMWATER QUALITY CONTROL REQUIREMENTS AND GENERAL PROHIBITIONS NOTED IN THE DRAINAGE CRITERIA MANUAL VOLUME 2.
- 2. NO CLEARING, GRADING, EXCAVATION, FILLING OR OTHER LAND DISTURBING ACTIVITIES SHALL BE PERMITTED UNTIL SIGNOFF AND ACCEPTANCE OF THE GRADING PLAN AND EROSION AND STORMWATER QUALITY CONTROL PLAN IS RECEIVED FROM CITY ENGINEERING.
- 3. THE INSTALLATION OF THE FIRST LEVEL OF TEMPORARY EROSION CONTROL FACILITIES AND BMP'S SHALL BE INSTALLED AND INSPECTED PRIOR TO ANY EARTH DISTURBANCE OPERATIONS TAKING PLACE. CALL CITY STORMWATER INSPECTIONS, 385-5980, 48 HOURS PRIOR TO CONSTRUCTION.
- 4. SEDIMENT (MUD AND DIRT) TRANSPORTED ONTO A PUBLIC ROAD, REGARDLESS OF THE SIZE OF THE SITE, SHALL BE CLEANED IMMEDIATELY.
- 5. CONCRETE WASH WATER SHALL NOT BE DISCHARGED TO OR ALLOWED TO RUNOFF TO STATE WATERS, INCLUDING ANY SURFACE OR SUBSURFACE STORM DRAINAGE SYSTEM OR FACILITIES.
- 6. SOIL EROSION CONTROL MEASURES FOR ALL SLOPES, CHANNELS, DITCHES, OR ANY DISTURBED LAND AREA SHALL BE COMPLETED WITHIN TWENTY-ONE (21) CALENDAR DAYS AFTER FINAL GRADING OR FINAL EARTH DISTURBANCE HAS BEEN COMPLETED. DISTURBED AREAS AND STOCKPILES WHICH ARE NOT AT FINAL GRADE BUT WILL REMAIN DORMANT FOR LONGER THAN 30 DAYS SHALL ALSO BE MULCHED WITHIN 2 DAYS AFTER INTERIM GRADING. AN AREA THAT IS GOING TO REMAIN IN AN INTERIM STATE FOR MORE THAN 60 DAYS SHALL ALSO BE SEEDED ALL TEMPORARY SOIL EROSION CONTROL MEASURES AND BMP'S SHALL BE MAINTAINED UNTIL PERMANENT SOIL EROSION CONTROL MEASURES ARE IMPLEMENTED.
- 7. THE GRADING AND EROSION CONTROL PLAN WILL BE SUBJECT TO RE-REVIEW AND RE-ACCEPTANCE BY EDRD SHOULD ANY OF THE FOLLOWING OCCUR: GRADING DOES NOT COMMENCE WITHIN 12 MONTHS OF THE CITY ENGINEER'S ACCEPTANCE OF THE PLAN, A CHANGE IN PROPERTY OWNERSHIP, PROPOSED DEVELOPMENT CHANGES, OR PROPOSED GRADING REVISIONS.
- 8. THE PLAN SHALL NOT SUBSTANTIALLY CHANGE THE DEPTH OF COVER, OR ACCESS TO UTILITY LINES. ACCEPTANCE OF THIS PLAN DOES NOT CONSTITUTE APPROVAL TO GRADE IN ANY UTILITY EASEMENT OR RIGHT-OF-WAY. APPROVALS TO GRADE WITHIN UTILITY EASEMENTS MUST B OBTAINED FROM THE APPROPRIATE UTILITY COMPANY. IT IS NOT PERMISSIBLE FOR ANY PERSON TO MODIFY THE GRADE OF THE EARTH ON ANY COLORADO SPRINGS UTILITIES EASEMENT OR UTILITY RIGHT-OF-WAY WITHOUT THEIR WRITTEN APPROVAL. THE PLAN SHALL NOT INCREASE OF DIVERT WATER TOWARDS UTILITY FACILITIES. ANY CHANGES TO EXISTING UTILITY FACILITIES TO ACCOMODATE THE PLAN MUST BE APPROVED BY THE AFFECTED UTILITY OWNER PRIOR TO IMPLEMENTING THE PLAN. THE COST TO RELOCATE OR PROTECT EXISTING UTILITIES OR TO PROVIDE INTERIM ACCESS IS THE APPLICANT'S EXPENSE.

ANTICIPATED STARTING AND COMPLETION TIME PERIOD OF SITE GRADING:

JUNE 2014

EXPECTED DATE ON WHICH THE FINAL STABILIZATION WILL BE COMPLETED: DECEMBER 2014

AREAS

TOTAL AREA OF THE SITE TO BE CLEARED, EXCAVATED OR GRADED:

24.42 ACRES

RECEIVING WATERS NAME OF RECEIVING WATERS:

SAND CREEK

#### EROSION AND STORMWATER QUALITY CONTROL NOTES:

STORM WATER DISCHARGES FROM CONSTRUCTION SITES SHALL NOT CAUSE OR THREATEN TO CAUSE POLLUTION, CONTAMINATION OR DEGRADATION OF STATE WATERS.

CONCRETE WASH WATER SHALL NOT BE DISCHARGED TO OR ALLOWED TO RUNOFF TO STATE WATERS, INCLUDING ANY SURFACE OR SUBSURFACE STORM DRAINAGE SYSTEM OR FACILITIES.

BUILDING. CONSTRUCTION, EXCAVATION OR OTHER WASTE SHALL NOT BE TEMPORARILY PLACED OR STORED IN THE STREET, ALLEY, OR OTHER PUBLIC WAY, UNLESS IN ACCORDANCE WITH AN APPROVED TRAFFIC CONTROL PLAN. BMPS MAY BE REQUIRED BY CITY ENGINEERING IF DEEMED NECESSARY, BASED ON SPECIFIC CONDITIONS AND CIRCUMSTANCES (E.G., ESTIMATED TIME OF EXPOSURE, SEASON OF THE YEAR, ETC.).

VEHICLE TRACKING OF SOILS OFF-SITE SHALL BE MINIMIZED.

ALL WASTES COMPOSED OF BUILDING MATERIALS MUST BE REMOVED FROM THE CONSTRUCTION SITE FOR DISPOSAL IN ACCORDANCE WITH LOCAL AND STATE REGULATORY REQUIREMENTS. NO BUILDING MATERIAL WASTES OR UNUSED BUILDING MATERIALS SHALL BE BURIED, DUMPED OR DISCHARGED AT THE SITE.

NO CHEMICALS ARE TO BE USED BY THE CONTRACTOR. WHICH HAVE THE POTENTIAL TO BE RELEASED IN STORMWATER UNLESS PERMISSION FOR THE USE OF A SPECIFIC CHEMICAL IS GRANTED IN WRITING BY THE CITY ENGINEER. IN GRANTING THE USE OF SUCH CHEMICALS. SPECIAL CONDITIONS AND MONITORING MAY BE REQUIRED.

BULK STORAGE CONTAINERS FOR PETROLEUM PRODUCTS AND OTHER CHEMICALS SHALL HAVE ADEQUATE PROTECTION SO AS TO CONTAIN ALL SPILLS AND PREVENT ANY SPILLED MATERIAL FROM ENTERING STATE WATERS. INCLUDING ANY SURFACE OR SUBSURFACE STORM DRAINAGE SYSTEMS OR FACILITIES.

ALL PERSONS ENGAGED IN EARTH DISTURBANCE SHALL IMPLEMENT AND MAINTAIN ACCEPTABLE SOIL EROSION AND SEDIMENT CONTROL MEASURES INCLUDING BMPS IN CONFORMANCE WITH THE EROSION CONTROL TECHNICAL STANDARDS OF THE MANUAL AND IN ACCORDANCE WITH THE EROSION AND STORM WATER QUALITY CONTROL PLAN APPROVED BY THE CITY OF COLORADO SPRINGS, IF REQUIRED.

ALL TEMPORARY EROSION CONTROL FACILITIES INCLUDING BMPS AND ALL PERMANENT FACILITIES INTENDED TO CONTROL EROSION OF ANY EARTH DISTURBANCE OPERATIONS. SHALL BE INSTALLED AS DEFINED IN THE APPROVED PLANS AND THE MANUAL AND MAINTAINED THROUGHOUT THE DURATION OF THE EARTH DISTURBANCE OPERATION. THE INSTALLATION OF THE FIRST LEVEL OF TEMPORARY EROSION CONTROL FACILITIES AND BMPS SHALL BE INSTALLED AND INSPECTED PRIOR TO ANY EARTH DISTURBANCE OPERATIONS TAKING PLACE.

ANY EARTH DISTURBANCE SHALL BE CONDUCTED IN SUCH A MANOR SO AS TO EFFECTIVELY REDUCE ACCELERATED SOIL EROSION AND RESULTING SEDIMENTATION.

ALL EARTH DISTURBANCES SHALL BE DESIGNED, CONSTRUCTED AND COMPLETED IN SUCH A MANOR SO THAT THE EXPOSED AREA OF ANY DISTURBED LAND SHALL BE LIMITED TO THE SHORTEST PRACTICAL PERIOD OF TIME.

ALL WORK AND EARTH DISTURBANCES SHALL BE DONE IN A MANOR THAT MINIMIZES POLLUTION OF ANY ON-SITE OR OFF-SITE WATERS, INCLUDING WETLANDS.

SUSPENDED SEDIMENT CAUSED BY ACCELERATED SOIL EROSION SHALL BE MINIMIZED IN RUNOFF WATER BEFORE IT LEAVES THE SITE OF THE EARTH DISTURBANCE.

ANY TEMPORARY OR PERMANENT FACILITY DESIGNED AND CONSTRUCTED FOR THE CONVEYANCE OF STORMWATER AROUND, THROUGH OR FROM THE EARTH DISTURBANCE AREA SHALL BE DESIGNED TO LIMIT THE DISCHARGE TO A NON-EROSIVE VELOCITY.

TEMPORARY SOIL EROSION CONTROL FACILITIES SHALL BE REMOVED AND EARTH DISTURBANCE AREAS GRADED AND STABILIZED WITH PERMANENT SOIL EROSION CONTROL MEASURES PURSUANT TO THE STANDARDS AND SPECIFICATIONS PRESCRIBED IN THE MANUAL, AND IN ACCORDANCE WITH THE PERMANENT EROSION CONTROL FEATURES SHOWN ON THE EROSION AND STORM WATER QUALITY CONTROL PLANS APPROVED BY THE CITY OF COLORADO SPRINGS, IF REQUIRED.

SOIL EROSION CONTROL MEASURES FOR ALL SLOPES, CHANNELS, DITCHES OR ANY DISTURBED LAND AREA SHALL BE COMPLETED WITHIN TWENTY-ONE (21) CALENDAR DAYS AFTER FINAL GRADING, OR FINAL EARTH DISTURBANCE HAS BEEN COMPLETED. DISTURBED AREAS AND STOCK PILES WHICH ARE NOT AT FINAL GRADE BUT WILL REMAIN DORMANT FOR LONGER THAN 30 DAYS SHALL ALSO BE MULCHED WITHIN 21 AFTER INTERIM GRADING. AN AREA THAT IS GOING TO REMAIN IN AN INTERIM STATE FOR MORE THAN 60 DAYS SHALL ALSO BE SEEDED. ALL TEMPORARY SOIL EROSION CONTROL MEASURES AND BMPS SHALL BE MAINTAINED UNTIL PERMANENT SOIL EROSION CONTROL MEASURES ARE IMPLEMENTED.

NO PERSON SHALL CAUSE, PERMIT OR CONTRIBUTE TO THE DISCHARGE INTO THE MUNICIPAL SEPARATE STORM SEWER POLLUTANTS THAT COULD CAUSE THE CITY OF COLORADO SPRINGS TO BE IN VIOLATION OF ITS COLORADO DISCHARGE PERMIT SYSTEM MUNICIPAL STORMWATER DISCHARGE PERMIT.

## TRAILS AT FOREST MEADOWS FILING NO. 2 CITY OF COLORADO SPRINGS, EL PASO COUNTY, STATE OF COLORADO **GRADING & EROSION CONTROL PLAN APRIL 2014**



VICINITY MAP N.T.S.

#### EROSION AND STORMWATER QUALITY CONTROL NOTES (CONTINUED):

THE OWNER, SITE DEVELOPER, CONTRACTOR AND/OR THEIR AUTHORIZED AGENTS SHALL BE RESPONSIBLE FOR THE REMOVAL OF ALL CONSTRUCTION DEBRIS, DIRT, TRASH, ROCK, SEDIMENT AND SAND THAT MAY ACCUMULATE IN THE STORM SEWER OR OTHER DRAINAGE CONVEYANCE SYSTEM AND STORMWATER APPURTENANCES AS A RESULT OF SITE DEVELOPMENT.

NO PERSON SHALL CAUSE THE IMPEDIMENT OF STORMWATER FLOW IN THE FLOW LINE OF THE CURB AND GUTTER, INCLUDING THE TEMPORARY OR PERMANENT RAMPING WITH MATERIALS FOR VEHICLE ACCESS.

INDIVIDUALS SHALL COMPLY WITH THE "COLORADO WATER QUALITY CONTROL ACT" (TITLE 25, ARTICLE 8, CRS), AND THE "CLEAN WATER ACT" (33 USC 1344), REGULATIONS PROMULGATED, CERTIFICATIONS OR PERMITS ISSUED, IN ADDITION TO THE REQUIREMENTS INCLUDED IN THE MANUAL. IN THE EVENT OF CONFLICTS BETWEEN THESE REQUIREMENTS AND WATER QUALITY CONTROL LAWS, RULES OR REGULATIONS OF OTHER FEDERAL OR STATE AGENCIES, THE MORE RESTRICTIVE LAWS, RULES OR REGULATIONS SHALL APPLY.

THE QUANTITY OF MATERIALS STORED ON THE PROJECT SITE SHALL BE LIMITED, AS MUCH AS PRACTICAL, TO THAT QUANTITY REQUIRED TO PERFORM THE WORK IN AN ORDERLY SEQUENCE. ALL MATERIALS STORED ON-SITE SHALL BE STORED IN A NEAT ORDERLY MANOR, IN THERE ORIGINAL CONTAINERS, WITH THE ORIGINAL MANUFACTURE'S LABELS. MATERIALS SHALL NOT BE STORED IN A LOCATION WHERE THEY MAY BE CARRIED BY STORMWATER RUNOFF INTO A STATE WATER AT ANY TIME.

SPILL PREVENTION AND CONTAINMENT MEASURES SHALL BE USED AT STORAGE AND EQUIPMENT FUELING AND SERVICING AREAS TO PREVENT THE POLLUTION OF ANY STATE WATERS, INCLUDING WETLANDS. ALL SPILLS SHALL BE CLEANED UP IMMEDIATELY AFTER DISCOVERY OR CONTAINED UNTIL APPROPRIATE CLEAN UP METHODS CAN BE EMPLOYED. MANUFACTURE'S RECOMMENDED METHODS FOR SPILL CLEAN UP SHALL BE FOLLOWED. ALONG WITH PROPER DISPOSAL METHODS.

CITY OF COLORADO SPRINGS GRADING AND EROSION CONTROL REVIEW: THIS GRADING PLAN IS FILED IN ACCORDANCE WITH SECTION 7.7.1503 (ENACTED AS ORD. 82-56) OF THE CODE OF THE CITY OF COLORADO SPRINGS, 2001, AS AMENDED. EROSION CONTROL IS REVIEWED IN ACCORDANCE WITH THE DRAINAGE CRITERIA MANUAL VOLUME 1 (OCTOBER 1994) & VOLUME 2 (AUGUST 2002); LATEST REVISIONS.

FOR THE CITY ENGINEER

8/6/14

**BENCHMARKS:** 

1. THE TOP OF A YELLOW PLASTIC SURVEYORS CAP STAMPED "28890" APPROXIMATELY 56.8' EAST OF THE EAST EDGE OF ASPHALT ON BLACK FOREST ROAD, AND 94.0' NORTH FROM THE NORTH EDGE OF ASPHALT ON WOODMEN ROAD, AND 1.0' NORTH FROM FENCE POST. ELEVATION = 6919.80'

2. THE TOP OF A YELLOW PLASTIC SURVEYORS CAP STAMPED "35585" APPROXIMATELY 104.0' NORTH OF THE NORTH EDGE OF ASPHALT IN WOODMEN ROAD, AND 45.0' SOUTHWEST OF POWER POLE, AND 5.0' EAST OF FENCE POST ELEVATION = 6901.96'

SHEET INDEX 1. TITLE SHEET GRADING & EC PLAN 3. DETAIL SHEET

)	AGENCIES owner: civil engineer:	RIVERS DEVELOPMENT, LLC 13530 NORTHGATE ESTATES DRIVE, SUITE 200 COLORADO SPRINGS, CO 80921 JONATHAN MOORE M & S CIVIL CONSULTANTS, INC. 102 E. PIKES PEAK AVE., Ste 306 COLORADO SPRINGS, CO 80903 VIRGIL A. SANCHEZ P.E. (719) 955–5485 CITY OF COLORADO SPRINGS 30 S. NEVADA AVE., SUITE 401 COLORADO SPRINGS, CO 80903	TRAILS AT FOREST MEADOWS FILING NO. 2	GRADING AND EROSION CONTROL PLAN	ROJECT NO. 08-025 FILE: \DWG\CONST DWG\GRAD. & EROSION CONTROL\GRO1.DWG	ESIGNED BY: VAS SCALE UNIE: +/ 1+/ 2014 RAWN BY: VAS HORIZ: N/A SHEFT 1 OF 3 CD01
	TRAFFIC ENGINEERING:	ELIZABETH NIJKAMP, P.E. (719) 385–5410 CITY OF COLORADO SPRINGS 30 S. NEVADA AVE., SUITE 401 COLORADO SPRINGS, CO 80903 KATHLEEN KRAGER (719) 385–7628		CS, CO		
	DEVELOPMENT SERVICES:	COLORADO SPRINGS UTILITIES 1521 HANCOCK EXPRESSWAY COLORADO SPRINGS, CO 80903 AL JUVERA (719) 668-8769		COLORADO SPRIN 80901-1360		v 719.955.5485 f 719.444.8427
	GAS DEPARTMENT:	COLORADO SPRINGS UTILITIES 7710 DURANT DR. COLORADO SPRINGS, CO 80947 TIM WENDT(719) 668-4962		Æ	Ø	TS INC
	ELECTRIC DEPARTMENT:	COLORADO SPRINGS UTILITIES 7710 DURANT DR. COLORADO SPRINGS, CO 80920 TIM BENEDICT (719) 668-4933				
	COMMUNICATIONS:	QWEST COMMUNICATIONS (U.N.C.C. LOCATORS) (800) 922–1987 AT&T (LOCATORS) (719) 635–3674				
	*EROSION CONTROL AND	STORMWATER QUALITY COST ESTIMATE:				
	1132 LF SILT FENCE <b>©</b> \$1.50/LF= 2~BALE STRAW BARRIERS <b>©</b> \$12.00/ 4~INLET PROTECTION DEVICES <b>©</b> \$50 1 EA VTC'S <b>©</b> \$1500/EA= 4.32 ACRES RESEEDING <b>©</b> \$500.00/A	\$ 1,698.00 EA= \$ 24.00 /EA= \$ 200.00 \$ 1,500.00 AC= \$ 2160.00	NO. 37160	FOR AND ON BEHALF OF	M&S CIVIL CONSULTANTS, INC	
	SUBTOTAL: MAINTENANCE 40% TOTAL:	\$ 5,582.00 \$ 2,232.00* \$ <u>7.814.80</u>	DLORADO P.E.	SALABORANSEE		Ni ORINALLAS
	· SEE IRAILS AT FUREST MEADUWS F	ILING NU. I FUR DALANCE FINANCIAL ASSURANCES PUSIEU.		' 6 N	-» <b>V</b> <sup>e</sup> ~ ~	°. Bu Fr

GRADING PLAN / EROSION CONTROL STATEMENTS:

ENGINEER'S STATEMENT:

THIS EROSION AND STORMWATER QUALITY CONTROL/GRADING PLAN WAS PREPARED UNDER MY DIRECTION AND SUPERVISION AND IS CORRECT TO THE BEST OF MY KNOWLEDGE AND BELIEF. IF SUCH WORK IS PERFORMED IN ACCORDANCE WITH THE GRADING AND EROSION CONTROL PLAN, THE WORK WILL NOT BECOME A HAZARD TO LIFE AND LIMB, ENDANGERING PROPERTY, OR ADVERSELY AFFECT THE SAFETY, USE, OR STABILITY OF A PUBLIC WAY, DRAINAGE CHANNEL, OR OTHER PROPERTY.

8-5-14

VIRGIL A. SANCHEZ, COLORADO P.E. NO. 37160 ON BEHALF OF; M&S CIVIL CONSULTANTS, INC. 102 E. PIKES PEAK AVE., STE 306 COLORADO SPRINGS, CO 80903 719.955.5485 OFFICE 719.444.8427 FAX

#### **DEVELOPER'S STATEMENT:**

THE OWNER WILL COMPLY WITH THE REQUIREMENTS OF THE EROSION AND STORMWATER QUALITY CONTROL PLAN INCLUDING TEMPORARY BMP INSPECTION REQUIREMENTS AND FINAL STABILIZATION REQUIREMENTS. I ACKNOWLEDGE THE RESPONSIBILITY TO DETERMINE WHETHER THE CONSTRUCTION ACTIVITIES ON THESE PLANS REQUIRE COLORADO DISCHARGE PERMIT SYSTEM (CDPS) PERMITTING FOR STORMWATER DISCHARGES ASSOCIATED WITH CONSTRUCTION ACTIVITY.

BY: STATEMENT: THE CITY OF COLORADO SPRINGS RECOGNIZES THE DESIGN

ENGINEER AS HAVING

OF REVIEW ACCORDINGLY.

RESUBMITTAL REQUIRED IF

CONSTRUCTION HAS NOT

AFTER REVIEW DATE.

COMMENCED WITHIN 180 DAYS

**RESPONSIBILITY FOR THE DESIGN:** 

THE CITY HAS LIMITED ITS SCOPE

**TELEPHONE** LINES FOR BURIED UTILITY INFORMATION 48 HRS BEFORE YOU DIG CALL 1-800-922-1987

FOR LOCATING

& MARKING

GAS, ELECTRIC,

WATER &

Ω 王 ビ 王

₩ S S S S

μÎΖ

CAUTION





We need to know how much of the proposed area of disturbance (not just the impervious surfaces) is treated vs untreated and if there are any exclusions that apply to the untreated areas. So please create a basic overview map (or modify an existing drainage map) with color shading/hatching that shows areas tributary to each PBMP (pond, runoff reduction, etc.) and those disturbed areas that are not treated by a PBMP, with the applicable exclusion labeled (ex: 20% up to 1ac of development can be excluded per ECM App I.7.1.C.1 (only if using the WQCV Design Base Standard) and exclusions listed in ECM App I.7.1.B.#). An accompanying summary table on this map would also be very helpful (example provided):

#### **APPENDIX F – DRAINAGE MAPS**

	Water Quality Treatment Summary Table								
Basin ID	Total Area (ac)	Total Proposed Disturbed Area (ac)	Disturbed AreaDisturbed AreaDisturbed AArea Trib toTreated viaExcluded fromExcluded fromPond ARunoffWQ per ECMWQ per ECG(ac)ReductionApp I.7.1.C.1App I.7.1.E(ac)(ac)(ac)(ac)		Disturbed Area Excluded from WQ per ECM App I.7.1.B.# (ac)	Applicable WQ Exclusions (App I.7.1.B.#)			
А	4.50	4.50	4.50						
B	1.25	1.25		1.25					
С	6.00	4.00				4.00	ECM App I.7.1.B.5		
D	2.50	2.50	1.00		0.50	1.00	ECM App I.7.1.B.7		
E	3.00		3.00						
F	8.25								
Total	25.50	12.25	8.50	1.25	0.50	5.00			
Comments		[For each row, the sum of the values in Columns 4-7 must be greater than or equal to the value in Column 3 above.]	[Values in this column can be more than Column 3 if over- treating non- disturbed areas of the same land- use.]	[See RR calc spreadsheet.]	[Total must be <20% of site and <1ac.]				
		Total Proposed Disturbed Area (ac)	Total Propose (	ed Treated Area ac)	Total Proposed Disturbed Area Excluded from WQ (ac)		Minimum Area to be Treated (ac)		
		12.25	9	.75	5.	50	6.75		



	BASIN SUMMARY TABLE							
Tributary	Area	Percent			t <sub>c</sub>	Q₅	<b>Q</b> <sub>100</sub>	
Sub-basin	(acres)	Impervious	<b>C</b> <sub>5</sub>	<b>C</b> <sub>100</sub>	(min)	(cfs)	(cfs)	
EXA	0.25	2%	0.09	0.36	<mark>51.8</mark>	0.0	0.3	
EXB	0.97	24%	0.23	0.45	32.5	0.5	1.7	
EXC	11.50	2%	0.09	0.36	44.5	2.0	13.1	
EXD	21.80	3%	0.10	0.36	48.7	3.7	23.4	
EXE	3.96	2%	0.09	0.36	31.9	0.9	5.7	
EXF	2.58	2%	0.09	0.36	25.7	0.6	4.2	
OSI4	27.16	-	0.30	0.40	29.2	19.0	44.2	
Values	in BLUE inc Final Dra	dicate they ar ainage Repor	e from the t", by M.V.	"Silver Po E. Inc. revi	nds Subdiv sed May 5t	rision Filing h, 1996.	No. 1	

DESIGN PO	N
DP#	
1	
2	
3	
4	
4.1	
5	
6	
14	
Values in B	LU
from the "Sil	V

# SCHMIDT PARCEL **EXISTING CONDITIONS DRAINAGE MAP**



UE indicate they are ver Ponds Subdivisior Filing No. 1 Final Drainage Report" by M.V.E. Inc. revised May 5th, 1996.

#### LEGEND EXISTING PROPOSED SECTION LINE \_ \_ \_ \_ BOUNDARY LINE PROPERTY LINE EASEMENT LINE RIGHT OF WAY CENTERLINE STORM SEWER SWALE/WATERWAY FLOWLINE INDEX CONTOUR 6100 INTERMEDIATE CONTOUR FLOW DIRECTION DESIGN POINT DESIGNATION BASIN ID $\sum 1$ SUB-BASIN DRAINAGE AREA



ORIGINAL SCALE: 1" = 150'

PCD FILE NO: XXX-XX-XXX

SCH	GN	ЛD	)T	P	٩F	RCI	EL	-		





BASIN SUMMARY TABLE							
Tributary	Area	Percent			t <sub>c</sub>	Q <sub>5</sub>	Q <sub>100</sub>
Sub-basin	(acres)	Impervious	C <sub>5</sub>	C <sub>100</sub>	(min)	(cfs)	(cfs)
А	0.25	2%	0.09	0.36	51.8	0.0	0.3
В	0.09	2%	0.09	0.36	35.4	0.0	0.1
С	1.12	75%	0.45	0.59	13.3	1.9	4.1
D	0.73	80%	0.74	0.84	15.9	1.8	3.5
E	0.39	82%	0.75	0.85	14.4	1.1	2.0
F	0.48	84%	0.77	0.86	14.1	1.3	2.5
G	0.84	82%	0.75	0.85	17.5	2.1	4.0
Н	1.29	82%	0.75	0.85	19.5	3.0	5.8
I	3.46	75%	0.45	0.59	13.3	5.8	12.7
J	1.15	80%	0.74	0.84	17.9	2.8	5.3
К	1.20	80%	0.74	0.84	17.7	2.9	5.5
М	23.90	77%	0.49	0.62	24.5	32.5	69.4
N	2.98	12%	0.17	0.42	32.6	1.2	5.0
0	0.22	82%	0.75	0.85	12.8	0.6	1.2
OSI4	27.16	Ξ.	0.30	0.40	29.2	19.0	44.2
Value	es in RUUF i	ndicate they a	re from the	"Silver Por	nds Subdivis	ion Filing N	n 1

Final Drainage Report", by M.V.E. Inc. revised May 5th, 1996.

DESIGN POINT SOIV					
DP#	Q <sub>5-YR</sub>				
1	0.0				
2	0.0				
3	1.9				
4	4.6				
5	1.3				
6	3.3				
6.1	7.5				
7	3.0				
7.1	10.4				
8	5.8				
9	2.8				
9.1	7.8				
10	2.9				
10.1	10.7				
13	32.5				
13.1	41.7				
14	44.2				
15	0.6				
14	19.0				
Values in BLU	E indicate				
the "Silver P	Onds Sub				
NU. I FIIIdi	Diamage				

# SCHMIDT PARCEL **PROPOSED CONDITIONS DRAINAGE MAP**

	EXISTING	PROPOSED
SECTION LINE		
BOUNDARY LINE		
PROPERTY LINE		
EASEMENT LINE		
RIGHT OF WAY		
CENTERLINE		
STORM SEWER		
SWALE/WATERWAY FLOWLINE	/ ×_/ *	
INDEX CONTOUR	6100	6100
INTERMEDIATE CONTOUR		
FLOW DIRECTION	-	
BASIN ID	AC Q5 Q100 DESIGN POINT DESIGNATION	

ENGINEERING

ORIGINAL SCALE: 1" = 150'

e Report", by M.V.E. Inc. revised May 5th, 1996.