



Marksheffel Road – Segment M3 CDRs

Final Drainage Report

PCD File No: CDR2413

All Terrain Engineering Project No: 24013

April 2026

PREPARED FOR:

Turkey Canon Quarry Inc

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PREPARED BY:

All Terrain Engineering LLC

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ENGINEER'S STATEMENT

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by El Paso County for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors, or omissions on my part in preparing this report.

Ryan Burns, PE

Date

State of Colorado No. 54412

For and on behalf of All Terrain Engineering LLC

DEVELOPER'S STATEMENT

I, the developer, have read and will comply with all of the requirements specified in this drainage report and plan.

Business Name: Turkey Canon Quarry Inc

By: James Morley

Title: Manager

Address: 20 Boulder Crescent Street, Suite 200, Colorado Springs, CO 80903

EL PASO COUNTY STATEMENT

Filed in accordance with the requirements of the EL Paso County Drainage Criteria Manual, Volumes 1 and 2, El Paso County Engineering Criteria Manual and Land Development Code, as amended.

Joshua J. Palmer, P.E.

Date

County Engineer/ECM Administrator

Conditions:



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I. General Purpose, Location & Description

a. Purpose

The purpose of this Final Drainage Report (FDR) for Marksheffel Road – Segment M3 CDRs is to describe the site’s onsite and offsite drainage patterns, existing and proposed storm infrastructure, and to safely route developed stormwater to adequate outfalls. This report also supports the construction of future public roadways, Marksheffel & Brushtop Roads, associated utilities and stormwater infrastructure to support future development. No development is proposed with this report, except for the infrastructure described above.

b. Location

The Schmidt Parcel (hereby referred to as the “site”) is a collection of undeveloped parcels with a total area of approximately 98 acres, consisting of (4) Parcels per the EPC Assessor, including parcel # 5200000577, owned by Turkey Canon Quarry Inc., parcel #'s 5200000575 & 5200000576, owned by SRW Residential Partners LP LTD., and parcel # 5200000570 owned by Steve Martin.

The site is in the south half of Section 32, Township 12 South, Range 65 West of the Sixth Principal Meridian in the County of El Paso, State of Colorado. The site is located to the west of Vollmer Road and Marksheffel Road intersection. The site is bound by Holiday Hills Filing No.1 to the north, by Vollmer Road to the east, by the Trails at Forest Meadows Filing No. 3 & 4 to the south, and by Black Forest Road, Cottonwood Creek, and Parcel # 520000056 (8585 Black Forest Road to the west. The parcel is planned to be platted after approval of the “Schmidt PUD Preliminary Plan. A vicinity map is presented in Appendix A.

c. Description of Property

The site is approximately 98 acres of undeveloped land with existing vegetation consisting of native grasses. The total disturbance area associated with this FDR is 51.55 acres. A drainage swale exists along the eastern and southern border of the site which intercepts runoff and carries it off-site to the west towards Cottonwood Creek. An existing sediment basin installed with ECP project # CDR22-007 currently intercepts flows and releases them to Cottonwood Creek. The site generally slopes from North to South at 2-4%.

The proposed improvements include overlot grading, construction of Marksheffel Road from Vollmer Road to proposed Brushtop Road, an extension of Brushtop Road from its current terminus at the site’s southern border to proposed Marksheffel Road, and storm drainage improvements to support the road construction and future development of on-site parcels. Water and wastewater infrastructure will also be constructed with this project to support future development. It is assumed that approximately 29 acres of the site (parcels 5200000575 & 5200000576) will be developed as multi-family residential in the future. Areas west of Brushtop Road are also assumed to be developed into single family and single family attached residential in the future, and will be detailed in the forth-coming “Schmidt PUD Preliminary Plan”. The remainder of the site will be Public R.O.W. for Brushtop Road and Marksheffel Road, and a tract for a storm infrastructure and water quality pond (Pond A). Pond A, is sized to support the proposed construction within the CDR submittal this FDR supports, and considered a temporary condition until any of the vacant land develops. Any future development will require a site-specific FDR/drainage report, pond expansion, and additional storm/drainage infrastructure.

Per a NRCS soil survey, the site is made up of Blakeland loamy sands and Columbine gravelly sandy loam, which are classified as a Group A soils. Group A soils have a high infiltration rate when thoroughly wet and have a high rate of water transmission. The NRCS soil survey is presented in Appendix A.

There are no known irrigation facilities located on the project site.

d. Floodplain Statement

Based on the FEMA Firm Map Number 08041C0529G, revised December 7, 2018, the proposed site is located within Zone X. Zone X is defined as areas outside the Special Flood Hazard Area (SFHA) and higher than the elevation of the 0.2-percent-annual-chance (or 500-year) flood. A FEMA panel for the site is presented in Appendix A.

II. Drainage Basins

a. Major Basin Description

The site lies within the Sand Creek and Cottonwood Creek Drainage Basins. According to FEMA FIRM 08041C0529G a portion of site lies within the existing Zone AE 100-yr flood plain. It should also be noted that as part of the Colorado Spring Black Forest Road Widening Project, a LOMR application was submitted to FEMA under case # 23-08-0623X, but is currently under review.

Based upon the Sand Creek and Cottonwood Creek Drainage Basin Planning Studies, the site partially falls within each basin while most of the site was not included in either. The site was an active quarry in the past and a berm was constructed along the southern border, which intercepted the majority of overland flows, and directed them to Cottonwood Creek, or a low point roughly located where the existing sediment basin is located per # CDR22-007, which also discharges to Cottonwood Creek. Recent site visits have confirmed that the majority of the flows that did not infiltrate into the ground, were tributary to Cottonwood Creek and according to the Master Development Drainage Plan Update for Woodmen Heights Developed Drainage and the various Trails at Forest Meadows FDR's, this condition has been present since the early 2000's. For this reason, a drainage basin line is shown on the drainage maps, based upon current topography, for the split between Cottonwood Creek and Sand Creek drainage basins. It should also be noted, that per the "Trails at Forest Meadows Filing No. 3 & 4 Drainage Report, this berm was constructed to ensure flows did not negatively impact the residential homes to the South. It appears that there is no viable outfall to the south, as the bordering properties did not provide surface drainage paths, or the overflow path as identified in the "Master Development Drainage Plan Update for Woodmen Heights Developed Drainage" and the existing storm infrastructure cannot support the total flows generated from the project site.

Based upon the above, approximately 17 acres of the site is within the Sand Creek Drainage Basin. The remainder of the site lies within the Cottonwood Creek Drainage Basin. The proposed Cottonwood Creek-Sand Creek Drainage Basin line is presented on the drainage maps in Appendix F.

Cottonwood Creek is located to the west of the site and runs from north to south. The reach that runs to the west of the site was studied in the Colorado Springs, "Cottonwood Creek Drainage Basin Planning Study" (Cottonwood DBPS) completed by Matrix Design Group in July 2019. According to the Cottonwood Creek

DBPS, reach RUC160 runs west of the site and has been identified as being in stable condition. Cottonwood Creek was also studied in the June 1994, “Cottonwood Creek Drainage Basin Planning Study” by URS Consultants, and identified the on-site reach as the segment between Design Points 6 & 7. The study characterized the reach as a naturalized channel with ecological value including wetlands and riparian vegetation.

The channel will be analyzed for stability and required improvements with the forthcoming Schmidt PUD and Preliminary Plan and any required creek improvements will be identified with that project.

The Sand Creek Basin was studied many times over the years by various companies and in various reports. One of the most recent reports adopted by the County is the “Master Development Drainage Plan Amendment for Sterling Ranch” prepared by JR Engineering in March 2023. This report did not include the subject site in the Sand Creek Basin, and neither did the original 2018 “Sterling Ranch Master Development Drainage Plan” prepared by M&S in 2018. Although not adopted by the County, the site was partially included in the “Sand Creek Drainage Basin Planning Study” (Sand DBPS) completed by Stantec in January 2021, however it only showed approximately 17 acres of the eastern most portion of the site as tributary to Sand Creek. The Stantec Sand Creek DBPS assumed the Schmidt Parcel property to have an “Open Space” use which is consistent with the property at this time and the Basin line they showed, is generally consistent with the existing site topography.

b. Existing Subbasin Description

The existing condition describes the current state of the site after the early grading for the Schmidt Parcel. The existing condition consists of six on-site basins and one off-site basin. The existing sub-basin delineation is shown on the drainage map within Appendix F and is described as follows:

Basin OSI4 is 27.16 acres of Silver Ponds Subdivision Filing 1 & the existing Colorado Springs R.O.W. reserved for the future Marksheffel Road extension. Values for this basin were taken from “Silver Ponds Subdivision Filing No.1 Final Drainage Report”. Runoff from this basin ($Q_5=19.0$ cfs, $Q_{100}=44.2$ cfs) flows south and is intercepted by the existing swale/berm that directs runoff around the site. Flows are diverted to the west towards DPI4 and enter Cottonwood Creek.

Basin EXA is 0.25 acres of an existing berm with stabilized vegetation. Runoff from this basin ($Q_5=0.0$ cfs, $Q_{100}=0.3$ cfs) flows along the berm west and enters an existing swale at DP1 and flows offsite and into basin OSI4. Flows in the existing swale combine with a portion of Basin OSI4 at DP14 ($Q_5 = 19.0$ cfs, $Q_{100} = 44.2$ cfs) and direct flows to the west towards Cottonwood Creek.

Basin EXB is 1.51 acres of an existing berm with stabilized vegetation, and includes a portion of the “Tahiti Road” R.O.W. Although the R.O.W. exists, the road is shut down and no longer active and generally consists of only a dirt 2-track or varying width drive. Runoff from this basin ($Q_5=0.6$ cfs, $Q_{100}=2.4$ cfs) flows east along the berm and enters existing dual 48” RCP culverts at DP2. Culvert flows are directed south along Vollmer Road. There is no drainage infrastructure downstream, therefore; runoff that enters Vollmer Road right-of-way (R.O.W.) flows per existing drainage patterns southeast towards Sand Creek.

Basin EXC is 11.5 acres of native and stabilized vegetation except for a temporary vehicle tracking pad and access that was installed with the CDR22-007 project. Runoff from this basin ($Q_5=2.0$ cfs, $Q_{100}=13.2$ cfs) flows overland southeast and enters an existing swale also installed with the CDR22-007 project. The existing swale enters Basin EXD at DP3 and follows the drainage patterns of that Basin EXD.

Basin EXD is 21.8 acres of native and stabilized vegetation. Runoff from this basin ($Q_5=3.7$ cfs, $Q_{100}=23.3$ cfs) flows overland southwest and enters an existing swale at DP4. Flows from DP3 and DP4 combine at DP4.1 ($Q_5=5.5$ cfs, $Q_{100}=35.6$ cfs) and are conveyed via an existing swale through Basin EX-G and towards the existing Temporary Sediment Basin. The sediment basin outfalls to Cottonwood Creek at DP7.1. See Basin EXG description below.

Basin EXE is 3.96 acres of undeveloped land with native vegetation. Runoff from this basin ($Q_5=0.9$ cfs, $Q_{100}=5.7$ cfs) flows overland southeast to DP5, where flow enters Vollmer Road R.O.W. There is no drainage infrastructure downstream, therefore; runoff that enters Vollmer Road R.O.W flows per existing drainage patterns southeast towards Sand Creek.

Basin EXF is 2.58 acres of native and stabilized vegetation. Runoff from this basin ($Q_5=0.6$ cfs, $Q_{100}=4.1$ cfs) flows overland south to DP6. Basin EXF overland flows south to Trails at Forest Meadows Filing No. 3. Basin EXF flow was accounted for in “Trails at Forest Meadows Filing No. 3 Final Drainage Report” (Trails No. 3 FDR) as Basins OS2 and OS3. Basin OS2 and OS3 total 1.56 acres and have a total flow of $Q_5=1.0$ cfs and $Q_{100}=3.6$ cfs.

Basin EXG is 39.7 acres of native and stabilized vegetation, although, disturbance from the CDR22-007 project may be present at the time of writing this report. Runoff from this basin ($Q_5=4.9$ cfs, $Q_{100}=32.9$ cfs) flows overland southwest and enters an existing sediment basin installed with the CDR22-007 project, at DP7. Flows are then either released through the sediment basin outlet, to DP7.1 or over-top the spillway, and flow to DP7.1 ($Q_5 = 9.2$ cfs, $Q_{100} = 60.8$ cfs), where they combine with flows from DP4.1 and enter Cottonwood Creek and continue off-site. Total flow in Cottonwood Creek, including the site flows, is 854 CFS per the “Cottonwood Creek DBPS” by URS, dated 1994.

Historically, this basin flowed to a low point in roughly the same location as the existing sediment basin and flows either infiltrated or over-topped the low-point and entered Cottonwood Creek. The site was previously an active quarry, and therefore the drainage patterns were altered with mining activities over the years. Construction of the Trails at Forest Meadows development to the south stated that the construction company running the mine constructed a large berm to ensure flows did not enter the Trails Subdivision and instead were diverted west.

Basin EXI is 10.3 acres of native and stabilized vegetation, including wetland and riparian vegetation within the Cottonwood Creek Flood Plain. Runoff from this basin ($Q_5=2.4$ cfs, $Q_{100}=16.3$ cfs) flows overland south and towards Cottonwood Creek. Flows enter the Creek and combine with flows from upstream and DP7.1 flows and continue south off-site. Total flow in Cottonwood Creek, including the site flows, is 854 CFS per the “Cottonwood Creek DBPS” by URS, dated 1994.

Basin EXJ is 0.33 acres of native and stabilized vegetation and includes just a small sliver of land from the southern property line to the top of a small berm that keeps the majority of the site flows from entering the “Trails at Forest Meadows Filing No. 4 Subdivision. Runoff from this basin ($Q_5=0.1$ cfs, $Q_{100}=0.5$ cfs) flows overland south to DP10. Flows are distributed over the length of the basin, and are not concentrated. This area was analyzed as part of Trails at Forest Meadows Filing No. 4 drainage report and was delineated as basins OS4 and Basin OS2 which had a combined flow of $Q_5 = 1.0$ cfs & $Q_{100} = 4.7$ cfs.

c. Proposed Subbasin Description

Proposed Sub-basin Drainage

The proposed condition consists of 13 on-site basins and 1 off-site basin. The proposed sub-basin delineation is shown on the drainage map within Appendix F and is described as follows:

Basin OSI4 is 27.16 acres of Silver Ponds Subdivision Filing 1. Values for this basin were taken from “Silver Ponds Subdivision Filing No.1 Final Drainage Report”. Runoff from this basin ($Q_5=19.0$ cfs, $Q_{100}=44.2$ cfs) flows south and is intercepted by the existing swale/berm that directs runoff around the site. Flows are diverted to the west towards DP14 and enter Cottonwood Creek. Basin OSI4 will not be captured nor detained in Pond A. No exclusion is necessary for Basin OSI4 as it is an offsite, undisturbed basin shown for reference only.

Basin A is 0.25 acres of an existing berm with stabilized vegetation. Runoff from this basin ($Q_5=0.0$ cfs, $Q_{100}=0.2$ cfs) flows along the berm west and enters an existing swale at DP1 and enters an existing swale at DP1 and flows offsite and into basin OSI4. Flows in the existing swale combine with a portion of Basin OSI4 at DP14 ($Q_5 = 19.0$ cfs, $Q_{100} = 44.2$ cfs) and direct flows west to Cottonwood Creek. Basin A will not be captured or detained in Pond A. Water quality is not required for Basin A as it will remain in its existing condition and will not be disturbed.

Basin B is 0.09 acres of an existing berm with stabilized vegetation. Runoff from this basin ($Q_5=0.0$ cfs, $Q_{100}=0.1$ cfs) flows along the berm east and enters an existing pond adjacent to Vollmer Road. Basin B will follow historic drainage patterns. Water quality is not required for Basin B as it will remain in its existing condition and will not be disturbed.

Basin C is 1.12 acres of undeveloped land and a portion of the north side of Marksheffel Roadway. Runoff from this basin ($Q_5=1.6$ cfs, $Q_{100}=4.4$ cfs) flows overland to the south to the CS Type 1 C&G which transports flows west to a 5' Type R sump inlet (CS Type 2 Inlet) at DP3. All flows are captured by the inlet and are piped to DP4.1 where they combine with flows Captured at DP4. This inlet was sized to capture all flow in the 5 and 100-year storm and in the event of inlet failure at DP3, the flow will overtop the roadway crown and flow either to the inlet at DP4 or south in Brushtop Road curb and gutter. See Basin D description below. WQ and detention will be provided for this basin in Interim Pond A.

Basin D is 1.18 acres of proposed Marksheffel Road and proposed sidewalk. Runoff from this basin ($Q_5=1.8$ cfs, $Q_{100}=4.0$ cfs) flows toward the CS Type 1 C&G and are transported west to a 5' Type R sump inlet (CS Type 2 Inlet at DP4. All flows at DP4 are captured and piped to DP4.1($Q_5 = 3.2$ cfs, $Q_{100} = 7.9$ cfs), where they combine with DP3 flows. This inlet was sized to capture all flow in the 5 and 100-year storm. In the event of inlet failure at DP4, the flow will overtop the roadway crown and flow south in Brushtop Road curb and gutter.

Captured flows at DP4 are piped to proposed swale E1 which carries them to DP5. See basin E description below. Water quality and detention for Basin D is provided in Interim Pond A.

Basin E is 6.66 acres of undeveloped land and proposed swale E1. Runoff generated ($Q_5 = 1.2$ cfs & $Q_{100} = 8.5$ cfs) flows overland south and towards proposed swale E1. Flows enter the swale and are transported to design point 5 ($Q_5 = 3.9$ cfs, $Q_{100} = 15.1$ cfs) where they combine with Basin D flows. Swale E1 is sized to remain stable while carrying the 100-yr storm flows. with 1'+ of freeboard. Flows at DP5 are transported in the swale E1 to swale L1 at design point 5.1 ($Q_5 = 13.4$ cfs & $Q_{100} = 44.8$ cfs), where they combine in the swale with flows from design point 11.2 ($Q_5 = 10.4$ cfs & $Q_{100} = 44.3$ cfs). Swale L1 is sized to remain stable while conveying the 100-yr flows with 1'+ of freeboard. Flows at design point 5.1 continue west in swale L1 to design point 13.1, see Basin L description below. Water quality and detention for Basin E is provided in Interim Pond A.

Basin F is 2.56 acres of the east half of Brush Top Road and sidewalk and undeveloped open space. Runoff ($Q_5 = 1.5$ cfs & $Q_{100} = 5.4$ cfs) flows towards the EPC Type A curb and gutter and is transported south to a 15' CDOT type R on-grade inlet at design point 6. This inlet was sized to capture all flow in the 5 and 100-year storms. Captured flows are piped to DP7.1. See basin G description below. Water quality and detention for Basin E is provided in Interim Pond A.

Basin G is 0.78 acres of the west half of Brush Top Road and sidewalk. Runoff ($Q_5 = 2.0$ cfs & $Q_{100} = 3.8$ cfs) flows towards the EPC Type A curb and gutter and is transported south to a 15' CDOT type R on-grade inlet at design point 7. This inlet was sized to capture all flow in the 5 and 100-year storms. Captured flows are piped to DP7.1 ($Q_5 = 3.4$ cfs & $Q_{100} = 8.3$ cfs) where they combine in the pipe with flows from DP6. Flows at DP7.1 are piped to DP 11.2 ($Q_5 = 10.4$ cfs, $Q_{100} = 44.3$ cfs) where they combine with flows from DP11.1 and continue to DP5.1 in swale L1. See Basin K description below & Basin E description above. Water quality and detention for Basin E is provided in Interim Pond A.

Basin H is 3.59 acres of undeveloped land and open space consisting of stabilized and native vegetation. No disturbance is proposed in this basin with this project. Runoff ($Q_5 = 0.7$ cfs & $Q_{100} = 5.2$ cfs) sheet flows south and east towards the Marksheffel R.O.W. and basin I boundary. Flows enter Basin I and combine with Basin I flows at DP9 ($Q_5 = 2.9$ cfs, $Q_{100} = 9.3$ cfs). See basin I description below. Water quality and detention for Basin E is provided in Interim Pond A.

Although no development is proposed in this basin with this project, a 24" storm stub out is provided at the basins low-point and boundary with Basin I to support potential, future development. The stub will remain plugged with this project. A site specific drainage report will be required if this basin develops to confirm storm sizing and routing as well as water quality and detention requirements.

Basin I is 1.22 acres of a portion of the north side of Marksheffel Roadway. Runoff from this basin ($Q_5 = 2.9$ cfs, $Q_{100} = 5.6$ cfs) flows to the CS Type 1 C&G which transports flows southeast to a 10' Type R sump inlet (CS Type 2 Inlet) at DP9 ($Q_5 = 2.9$ cfs, $Q_{100} = 9.3$ cfs) where flows combine with Basin H flows. All flows are captured by the inlet and are piped to DP10.1 where they combine with flows Captured at DP10, see Basin J description below. This inlet was sized to capture all flow in the 5 and 100-year storm and in the event of inlet failure at DP9, the flow will overtop the roadway crown and flow either to the inlet at DP10 or into the Vollmer Road

R.O.W and to an existing CDOT 10' Type R sump inlet. Water quality and detention for Basin I is provided in Interim Pond A.

Basin J is 1.28 acres of a portion of the south half of proposed Marksheffel Road and associated sidewalk. Runoff from this basin ($Q_5=3.5$ cfs, $Q_{100} = 6.5$ cfs) flows to the CS Type 1 C&G which transports flows southeast to a 10' Type R sump inlet (CS Type 2 Inlet) at DP10 ($Q_5=3.5$ cfs, $Q_{100} = 6.5$ cfs). Captured flows are piped to DP10.1 ($Q_5 = 5.3$ & $Q_{100} = 13.9$ cfs) where they combine in the pipe with flows from DP9. Flows from DP10.1 continue in the pipes to DP11.1 ($Q_5 = 7.9$ cfs & $Q_{100} = 38.0$ cfs). The storm system is over-size to accommodate the potential for future developed flows. See Basin K description below. This inlet was sized to capture all flows in the 5 and 100-yr design storms. In the event of inlet failure at DP10, flows will overtop to the east and enter Vollmer Road. Water quality and detention for Basin J is provided in Interim Pond A.

Basin K is 24.33 acres of undeveloped land with native vegetation. Overlot grading is proposed for this basin at this time but it will remain undeveloped with this project, with exception of stormwater and utility infrastructure to support potential future development. Runoff ($Q_5 = 3.7$ cfs, $Q_{100} = 27.3$ cfs) sheet flows overland south and enters swale K1, which carries flows west to DP11 ($Q_5 = 3.7$ cfs, $Q_{100} = 27.3$ cfs). Swale K1 was sized to remain stable while conveying the 100-yr design storm flows with 1'+ of freeboard. A berm is proposed along the eastern site/basin boundary to ensure any nuisance flows are directed to proposed swale K1 and DP11. Flows at DP 11 will enter a 36" FES and are piped to DP11.1 ($Q_5 = 7.9$ cfs & $Q_{100} = 38.0$ cfs). Flows at DP11.1 continue to DP11.2 in the pipe where they combine with flows from 7.1. See Basin G description above. Water quality and detention for Basin K is provided in Interim Pond A.

Although no development is proposed in this basin with this project, a 36" storm stub out is provided at the lower limits of the basin along its eastern boundary to support potential, future development. The stub will remain plugged with this project. The storm system was up-sized to accommodate future developed flows and consists of a 42" RCP main trunk line. It is also anticipated that the existing 36" FES and associated 36" RCP will accept future developed flows. A site specific drainage report will be required if this basin develops to confirm storm sizing and routing as well as water quality and detention requirements.

Basin L is 36.07 acres of undeveloped open space. Runoff ($Q_5 = 4.6$ cfs & $Q_{100} = 34.1$ cfs) flows towards the proposed swale L1 at design point 13 ($Q_5 = 4.6$ & $Q_{100} = 34.1$). Flows enter Swale L1 and continue to design point 13.1 ($Q_5 = 16.3$ cfs, $Q_{100} = 82.8$ cfs) where they combine in the swale with flows from DP5.1. Swale L1 is sized to remain stable while carrying the 100-yr storm flows with 1'+ of freeboard. Flows at DP13.1 enter the proposed Interim Pond A and associated low-tailwater basin & forebay and combine with Basin M flows at DP14, see Basin description below. Water quality and detention for Basin L is provided in Interim Pond A.

Basin M is 4.86 acres of undeveloped open space and proposed Interim Pond A. Runoff ($Q_5 = 0.7$ cfs & $Q_{100} = 5.4$ cfs) sheet flows towards the proposed Interim Pond A and combines with DP13.1 flows in the pond a DP14 ($Q_5 = 17$ cfs, $Q_{100} = 87.4$ cfs). Water quality and detention for Basin M is provided in Interim Pond A.

Basin N is 0.34 acres of undeveloped land, with the exception of proposed storm sewer. Runoff ($Q_5 = 0.1$ cfs, $Q_{100} = 0.5$ cfs) sheet flows east, offsite towards Vollmer Road R.O.W. Flows are distributed along the length of the basin and are not concentrated. The basin is undeveloped land that will remain undeveloped and the proposed disturbance will not alter existing drainage patterns and therefore no water quality or detention is required.

Basin O is 0.56 acres of undeveloped land and a portion of the southern limits of the proposed Bursh Top Road extension. Basin O runoff ($Q_5 = 0.1$ cfs and $Q_{100} = .9$ cfs) overland flows south to Trails at Forest Meadows Filing No. 3 at DP16 (same flows). Basin O flow was accounted for in “Trails at Forest Meadows Filing No. 3 Final Drainage Report” (Trails No. 3 FDR) as Basins OS2 and OS3. Basin OS2 and OS3 total 1.56 acres and have a total flow of $Q_5=1.0$ cfs and $Q_{100}=3.6$ cfs and these flows are tributary to the “Sand Creek Detention Pond No. 6” which provide both detention and water quality per the “Trails at Forest Meadows Filing No. 3 Final Drainage Report” (Trails No. 3 FDR).

Basin P is 2.68 acres of undeveloped land that will remain undeveloped. Runoff ($Q_5 = 0.6$ cfs and $Q_{100} = 4.2$ cfs) sheets flows south and west per existing drainage patterns. The majority of this basin will remain undisturbed, except for a portion of the southern limits of this basin along the sites boundary with the “Trails at Forest Meadows Filing No. 4” development. The proposed disturbance is intended to restore the existing property line berm, to ensure no flows negatively impact the homes to the south. Please note, this grading will not changes existing drainage patterns, and flows will be distributed along the length of the basin and not concentrated and the basin will; remain undeveloped with this project,. And therefore, no water quality or detonation is required.

Basin Q 10.29 acres of undeveloped land and native and stabilized vegetation, including wetland and riparian vegetation within the Cottonwood Creek Flood Plain. Runoff from this basin ($Q_5=1.5$ cfs, $Q_{100}=10.8$ cfs) flows overland south and towards Cottonwood Creek. Flows enter the Creek and combine with flows from upstream and DP7.1 flows and continue south off-site. Total flow in Cottonwood Creek, including the site flows, is 854 CFS per the “Cottonwood Creek DBPS” by URS, dated 1994.

2.68 acres of undeveloped land that will remain undeveloped. Runoff ($Q_5 = 0.6$ cfs and $Q_{100} = 4.2$ cfs) sheets flows south and west per existing drainage patterns. The majority of this basin will remain undisturbed, except for a portion of the southern limits of this basin along the sites boundary with the “Trails at Forest Meadows Filing No. 4” development. The proposed disturbance is intended to restore the existing property line berm, to ensure no flows negatively impact the homes to the south. Please note, this grading will not changes existing drainage patterns, and flows will be distributed along the length of the basin and not concentrated and the basin will; remain undeveloped with this project,. And therefore, no water quality or detonation is required.

III. Drainage Design Criteria

a. Development Criteria Reference

Storm drainage analysis and design criteria for this project were taken from the “City of Colorado Springs/El Paso County Drainage Criteria Manual” Volumes 1 and 2 (EPCDCM), dated October 12, 1994, the “Urban Storm Drainage Criteria Manual” Volumes 1 to 3 (USDCM) and Chapter 6 and Section 3.2.1 of Chapter 13 of the “Colorado Springs Drainage Criteria Manual” (CSDCM), dated May 2014, as adopted by El Paso County.

b. Hydrologic Criteria

All hydrologic data was obtained from the “El Paso Drainage Criteria Manual” Volumes 1 and 2, and the “Urban Drainage and Flood Control District Urban Storm Drainage Criteria Manual” Volumes 1, 2, and 3. On-

site drainage improvements were designed based on the 5 year (minor) storm event and the 100-year (major) storm event. Runoff was calculated using the Rational Method, and rainfall intensities for the 5-year and the 100-year storm return frequencies were obtained from Table 6-2 of the CSDCM. One-hour point rainfall data for the storm events is identified in the chart below. Runoff coefficients were determined based on proposed land use and from data in Table 6-6 from the CSDCM. Time of concentrations were developed using equations from CSDCM. All runoff calculations and applicable charts and graphs are included in the Appendices.

Table 1 - 1-hr Point Rainfall Data

Storm	Rainfall (in.)
5-year	1.50
100-year	2.52

c. Hydraulic Criteria

The Rational Method and USDCM’s SF-2 and SF-3 forms are used to determine the runoff from the minor and major storms. MHFD-Detention v4.06 spreadsheet is utilized for full-spectrum extended detention basin design. Hydraflow Express is used for hydraulic modeling of swale, spillway, and emergency overflow calculations. Proposed swales have been designed to meet El Paso County criteria for velocity, freeboard, and stability. Hydraflow Storm Sewers is used for storm sewer hydraulic analysis.

IV. Drainage Facility Design

a. General Concept

Onsite stormwater will be conveyed via proposed curb and gutter to proposed Type R inlets. Captured storm water will be piped to Pond A, a full spectrum water quality and detention pond. Drainage infrastructure is sized to account for the assumed future condition of tributary areas. Pond A will discharge to Cottonwood Creek per historic drainage patterns.

b. Water Quality & Detention

Interim Pond A provides full spectrum water quality and detention for Basins C-M. It is the intent of the developer that this pond will be expanded and retrofitted in the future to accommodate developed flows from the entire area this drainage report encompasses. However, the nature and timing of the future development is in the works still, and therefore, the interim pond provides water quality and detention only for the construction proposed with this report and CDR submittal. Individual and site specific drainage reports will be required to support any future development and to address water quality and detention.

See Proposed subbasin descriptions for excluded basins (A, B, N, O, P, Q). A total of 84.37 acres at 5.5% imperviousness are treated in Interim Pond A. The WQCV and EURV are released in 40 and 42 hours, respectively. A concrete bottom forebay is located at the outfall into the pond. A 3.0’ riprap lined trickle channel conveys flow towards the full spectrum outlet structure. The outlet structure will release 100-year stormwater at less than historic rates to minimize adverse impacts to downstream stormwater facilities. For some minor storm events, the release rate is higher than the existing predevelopment flows. The table below

provides the volumes required for the proposed pond, along with the release rates for the 5-year and 100-year storm.

	Required Volume (ac-ft)	Provided Volume (ac-ft)	WQCV (ac-ft)	EURV (ac-ft)	5-year Release (cfs)	100-year Release (cfs)
Pond A	1.39	1.51	0.27	0.009	0.1	40.9

A broad crested weir, lined with Type L buried soil riprap, is provided as an emergency spillway for Pond A. The emergency spillway conveys flow (57.2 cfs) to Cottonwood Creek at the location of the existing sediment basin outfall.

The Pond A outfall pipe controlled release $Q_5=0.1$ cfs, $Q_{100}= 40.9$ cfs through a 30” RCP pipe releases flows west to Cottonwood Creek. There are no expected impacts to water surface elevations in Cottonwood Creek from the development of this site. Pond A will be privately owned and maintained by Stonebridge Metropolitan District #4.

c. Major Drainageways

The Cottonwood Creek major drainage basin and Creek traverses the western portions of the site. According to FEMA FIRM 08041C0529G a portion of site lies within the existing Zone AE 100-yr flood plain. It should also be noted that as part of the Colorado Spring Black Forest Road Widening Project, a LOMR application was submitted to FEMA under case # 23-08-0623X, but is currently under review.

d. Operations & Maintenance

An Operations and Maintenance Manual has been submitted separately. The manual specifies maintenance intervals and required actions to maintain the function of the extended detention basin and appurtenances.

e. Grading & Erosion Control Plan

Due to the project disturbance area, a separate Grading and Erosion Control plan is required. The Grading and Erosion Control Plan has been submitted in conjunction with this FDR.

f. Four Step Process

In accordance with the El Paso County Drainage Criteria Manual Volume 2, this site has implemented the four step process to minimize adverse impacts of urbanization. The four step process includes reducing runoff volumes, treating the water quality capture volume (WQCV), stabilizing drainage ways, and implementing long-term source controls.

Step 1 – Reducing Runoff Volumes: The proposed site development consists of multi-family homes with open spaces and lawn areas interspersed within the development that helps disconnect impervious areas and reduce runoff volumes.

Step 2 – Stabilize Drainageways: The majority of the site lies within the Cottonwood Creek Drainage Basin, while the eastern most portion on the property is within the Sand Creek Drainage Basin. Cottonwood Creek is located to the west of the site. Basin and bridge fees will be due at time of platting. There are no proposed improvements with the 100-year flood plain. According to the “Cottonwood Creek Drainage Basin Planning Study” by URS, 1994 (Cottonwood DBPS), the reach adjacent to the site is DP 6 -7, with design point 7 being the Black Forest Road crossing. The report identifies the reach as having an acceptable slope and velocity range for all alternatives. Proposed outfalls will be analyzed in the final design stage for stability. Applicable excerpts from the Cottonwood DBPS are presented in Appendix D.

Step 3 – Treat the WQCV: Water quality treatment for this site is provided in a proposed full-spectrum EDB (Interim Pond A). The runoff from this site will be captured by inlets and conveyed to Interim Pond A via storm sewer and open channel. Upon entrance to the ponds, flows will be captured in a concrete bottom forebay designed to promote settlement of suspended solids. A riprap lined trickle channel will help convey pond flows and minimize standing water. The outlet structure has been designed to detail the WQCV 40 hours and the EURV 42 hours. 100-year flows released from Pond A will be reduced to historic rates.

Step 4 – Consider Need for Industrial and Commercial BMPs: There are no commercial or industrial components to this development, therefore; no Industrial or Commercial BMPs are required. BMPs will be utilized to minimize off-site contaminants and to protect the downstream receiving waters. The site is not a high-risk site per Figure I-1 in ECM Appendix I. Site specific temporary source control BMPs that will be implemented include, but are not limited to, silt fencing placed around downstream areas of disturbance, construction vehicle tracking pads at the entrances, designated vehicle fueling areas, covered storage areas, and spill containment and control. The permanent erosion control BMPs include asphalt drives, storm inlets, storm sewer, Pond A, and permanent vegetation.

g. Drainage Basin & Bridge Fees

Applicable drainage and bridge fees for the site will be paid at time of platting.

V. Summary

Marksheffel Road – Segment M3 CDRs remains consistent with pre-development drainage conditions with the construction of the recommended drainage improvements. The proposed development will not adversely affect downstream stormwater infrastructure or surrounding developments. This report meets the latest El Paso County Drainage Criteria.

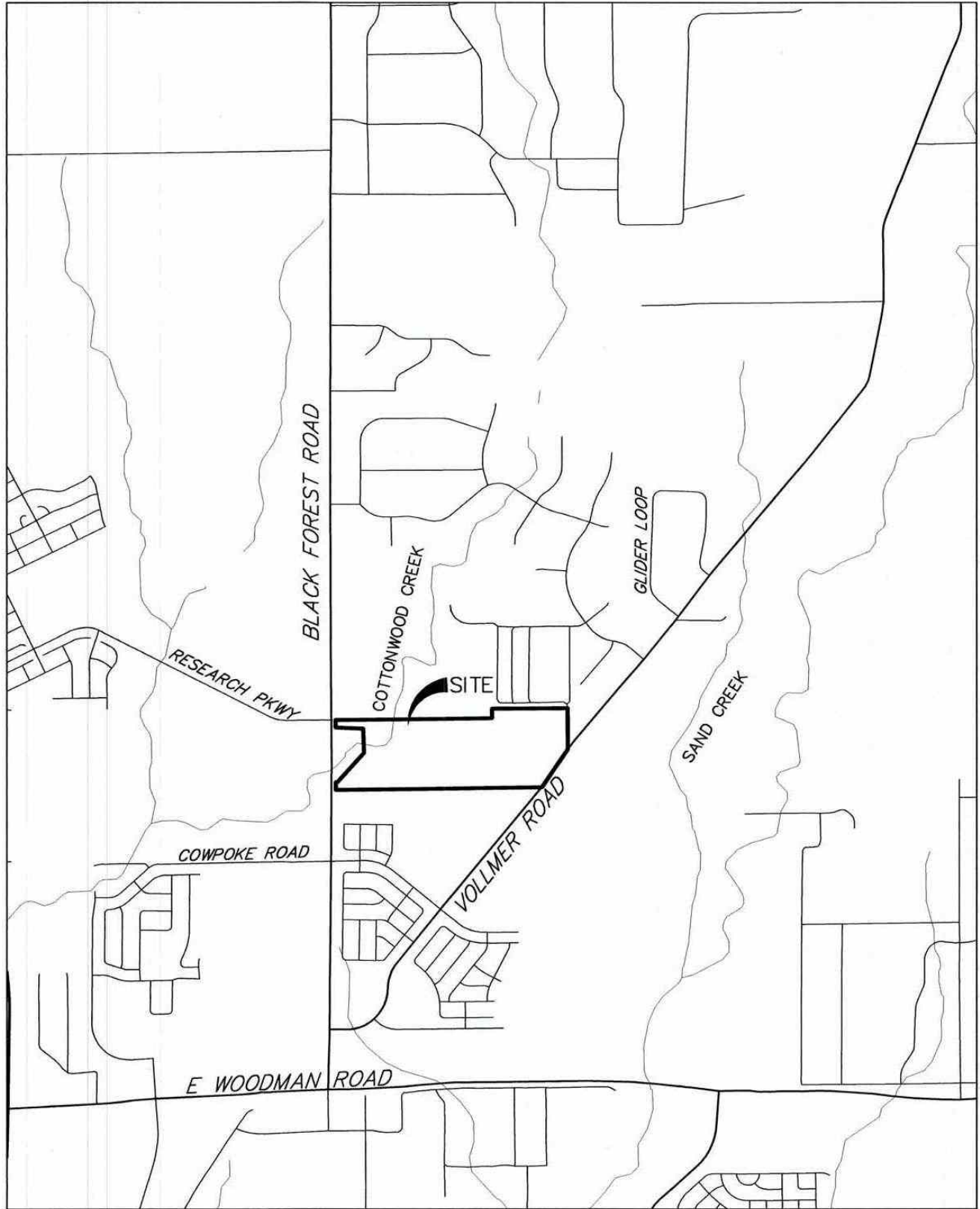
VI. References

1. El Paso County Drainage Criteria Manual, Vol I & II, as amended.
2. El Paso County Engineering Criteria Manual, 2019.
3. Urban Storm Drainage Criteria Manual (Volumes 1, 2, and 3), Urban Drainage and Flood Control District, June 2001.
4. Final Drainage Report for Silver Ponds Subdivision Filing No. 1, M.V.E. Inc., February 2, 1995, Revised May 5, 1996.



5. Sand Creek Drainage Basin Planning Study, Stantec, January 2021.
6. Cottonwood Creek Drainage Basin Planning Study, Matrix Design Group, July 2019.
7. Trails at Forest Meadows Filing No. 3 Final Drainage Report, M&S Civil Consultants Inc., August 2015.
8. Trails at Forest Meadows Filing No. 4 Final Drainage Report, M&S Civil Consultants Inc., April 2016.
9. “Cottonwood Creek Drainage Basin Planning Study” June 1994, by URS Consultants
10. LOMR associated w/ Black Forest Road Widening – Case # 23-08-0623X, FEMA
11. “Master Development Drainage Plan Amendment for Sterling Ranch” prepared by JR Engineering, March 2023

**APPENDIX A – VICINITY MAP, FEMA MAP, NRCS WEB SOIL SURVEY & NOAA
ATLAS 14**

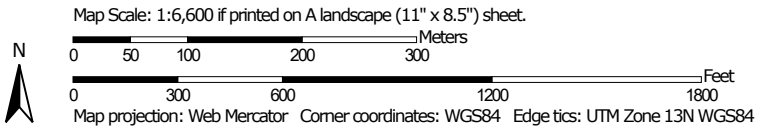
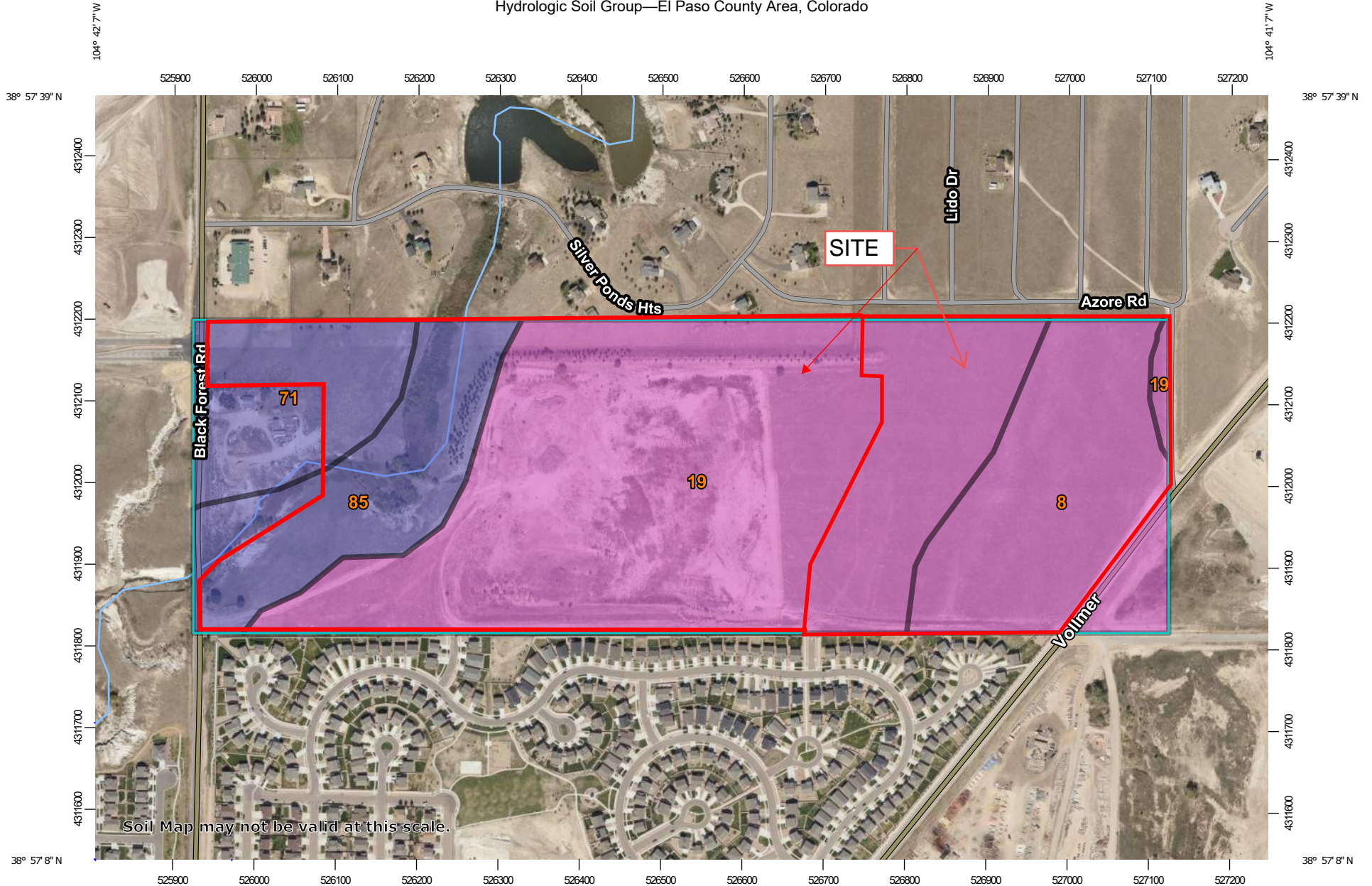


VICINITY MAP

































SCALE: 1"=2000'



Hydrologic Soil Group—El Paso County Area, Colorado



MAP LEGEND

- Area of Interest (AOI)**
 -  Area of Interest (AOI)
- Soils**
 - Soil Rating Polygons**
 -  A
 -  A/D
 -  B
 -  B/D
 -  C
 -  C/D
 -  D
 -  Not rated or not available
 - Soil Rating Lines**
 -  A
 -  A/D
 -  B
 -  B/D
 -  C
 -  C/D
 -  D
 -  Not rated or not available
 - Soil Rating Points**
 -  A
 -  A/D
 -  B
 -  B/D
- Water Features**
 -  Streams and Canals
- Transportation**
 -  Rails
 -  Interstate Highways
 -  US Routes
 -  Major Roads
 -  Local Roads
- Background**
 -  Aerial Photography
- Other**
 -  C
 -  C/D
 -  D
 -  Not rated or not available

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24,000.

Warning: Soil Map may not be valid at this scale.
 Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service
 Web Soil Survey URL:
 Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: El Paso County Area, Colorado
 Survey Area Data: Version 19, Aug 31, 2021

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Aug 19, 2018—Sep 23, 2018

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
8	Blakeland loamy sand, 1 to 9 percent slopes	A	22.3	19.5%
19	Columbine gravelly sandy loam, 0 to 3 percent slopes	A	64.2	56.2%
71	Pring coarse sandy loam, 3 to 8 percent slopes	B	12.1	10.6%
85	Stapleton-Bernal sandy loams, 3 to 20 percent slopes	B	15.6	13.6%
Totals for Area of Interest			114.1	100.0%

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

Rating Options

Aggregation Method: Dominant Condition

Component Percent Cutoff: None Specified

Tie-break Rule: Higher

NOTES TO USERS

This map is for use in administering the National Flood Insurance Program. It does not necessarily identify all areas subject to flooding, particularly from local drainage sources of small size. The community map repository should be consulted for possible updated or additional flood hazard information.

To obtain more detailed information in areas where **Base Flood Elevations (BFEs)** and/or **floodways** have been determined, users are encouraged to consult the Flood Profiles and Floodway Data and/or Summary of Stillwater Elevations tables contained within the Flood Insurance Study (FIS) report that accompanies this FIRM. Users should be aware that BFEs shown on the FIRM represent rounded whole-foot elevations. These BFEs are intended for flood insurance rating purposes only and should not be used as the sole source of flood elevation information. Accordingly, flood elevation data presented in the FIS report should be utilized in conjunction with the FIRM for purposes of construction and/or floodplain management.

Coastal Base Flood Elevations shown on this map apply only to landward of 0.0' North American Vertical Datum of 1988 (NAVD88). Users of this FIRM should be aware that coastal flood elevations are also provided in the Summary of Stillwater Elevations table in the Flood Insurance Study report for this jurisdiction. Elevations shown in the Summary of Stillwater Elevations table should be used for construction and/or floodplain management purposes when they are higher than the elevations shown on this FIRM.

Boundaries of the **floodways** were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations with regard to requirements of the National Flood Insurance Program. Floodway widths and other pertinent floodway data are provided in the Flood Insurance Study report for this jurisdiction.

Certain areas not in Special Flood Hazard Areas may be protected by **flood control structures**. Refer to section 2.4 "Flood Protection Measures" of the Flood Insurance Study report for information on flood control structures for this jurisdiction.

The **projection** used in the preparation of this map was Universal Transverse Mercator (UTM) zone 13. The **horizontal datum** was NAD83, GRS80 spheroid. Differences in datum, spheroid, projection or UTM zones used in the production of FIRMs for adjacent jurisdictions may result in slight positional differences in map features across jurisdiction boundaries. These differences do not affect the accuracy of this FIRM.

Flood elevations on this map are referenced to the **North American Vertical Datum of 1988 (NAVD88)**. These flood elevations must be compared to structure and ground elevations referenced to the same vertical datum. For information regarding conversion between the National Geodetic Vertical Datum of 1929 and the North American Vertical Datum of 1988, visit the National Geodetic Survey website at <http://www.ngs.noaa.gov/> or contact the National Geodetic Survey at the following address:

NGS Information Services
NOAA, NINGS12
National Geodetic Survey
SSMC-3, #9202
1315 East-West Highway
Silver Spring, MD 20910-3282

To obtain current elevation, description, and/or location information for **bench marks** shown on this map, please contact the Information Services Branch of the National Geodetic Survey at (301) 713-3242 or visit its website at <http://www.ngs.noaa.gov/>.

Base Map information shown on this FIRM was provided in digital format by El Paso County, Colorado Springs Utilities, and Anderson Consulting Engineers, Inc. These data are current as of 2008.

This map reflects more detailed and up-to-date stream channel configurations and floodplain delineations than those shown on the previous FIRM for this jurisdiction. The floodplains and floodways that were transferred from the previous FIRM may have been adjusted to conform to these new stream channel configurations. As a result, the Flood Profiles and Floodway Data tables in the Flood Insurance Study Report (which contains authoritative hydraulic data) may reflect stream channel distances that differ from what is shown on this map. The profile baselines depicted on this map represent the hydraulic modeling baselines that match the flood profiles and Floodway Data Tables if applicable, in the FIS report. As a result, the profile baselines may deviate significantly from the new base map channel representation and may appear outside of the floodplain.

Corporate limits shown on this map are based on the best data available at the time of publication. Because changes due to annexations or de-annexations may have occurred after this map was published, map users should contact appropriate community officials to verify current corporate limit locations.

Please refer to the separately printed **Map Index** for an overview map of the county showing the layout of map panels, community map repository addresses, and a Listing of Communities table containing National Flood Insurance Program dates for each community as well as a listing of the panels on which each community is located.

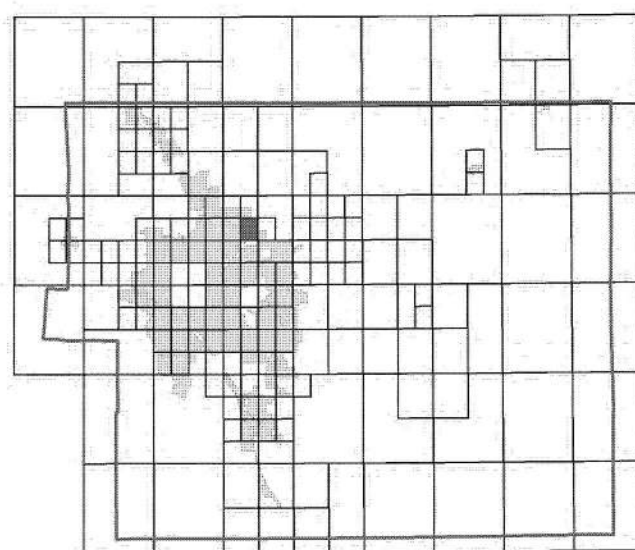
Contact **FEMA Map Service Center (MSC)** via the FEMA Map Information eXchange (FMIX) 1-877-336-2627 for information on available products associated with this FIRM. Available products may include previously issued Letters of Map Change, a Flood Insurance Study Report, and/or digital versions of this map. The MSC may also be reached by Fax at 1-800-358-9620 and its website at <http://www.msc.fema.gov/>.

If you have **questions about this map** or questions concerning the National Flood Insurance Program in general, please call 1-877-FEMA MAP (1-877-336-2627) or visit the FEMA website at <http://www.fema.gov/business/nfp>.

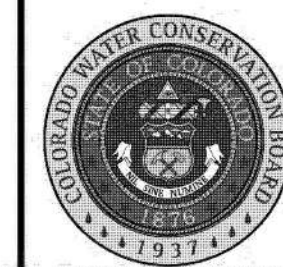
El Paso County Vertical Datum Offset Table

Flooding Source	Vertical Datum Offset (ft)
REFER TO SECTION 3.3 OF THE EL PASO COUNTY FLOOD INSURANCE STUDY FOR STREAM BY STREAM VERTICAL DATUM CONVERSION INFORMATION	

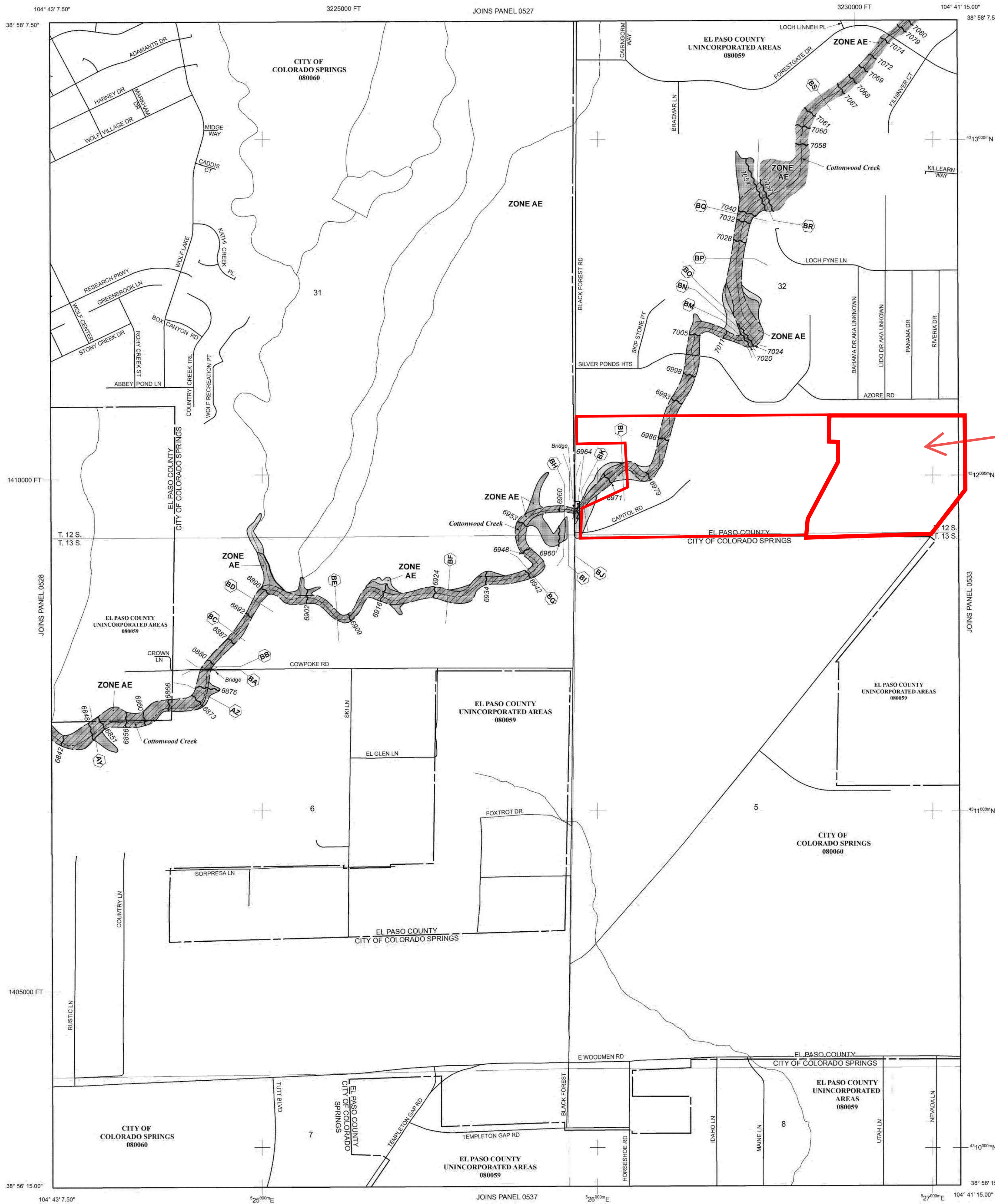
Panel Location Map



This Digital Flood Insurance Rate Map (DFIRM) was produced through a Cooperating Technical Partner (CTP) agreement between the State of Colorado Water Conservation Board (CWCB) and the Federal Emergency Management Agency (FEMA).



Additional Flood Hazard information and resources are available from local communities and the Colorado Water Conservation Board.



NOTE: MAP AREA SHOWN ON THIS PANEL IS LOCATED WITHIN TOWNSHIP 12 SOUTH, RANGE 65 WEST, AND TOWNSHIP 13 SOUTH, RANGE 65 WEST.

LEGEND

- SPECIAL FLOOD HAZARD AREAS (SFHAs) SUBJECT TO INUNDATION BY THE 1% ANNUAL CHANCE FLOOD
- The 1% annual chance flood (100-year flood), also known as the base flood, is the flood that has a 1% chance of being equaled or exceeded in any given year. The Special Flood Hazard Area is the area subject to flooding by the 1% annual chance flood. Areas of Special Flood Hazard include Zones A, AE, AH, AO, AR, A99, V, and VE. The Base Flood Elevation is the water-surface elevation of the 1% annual chance flood.
- ZONE A** No Base Flood Elevations determined.
- ZONE AE** Base Flood Elevations determined.
- ZONE AH** Flood depths of 1 to 3 feet (usually areas of ponding); Base Flood Elevations determined.
- ZONE AO** Flood depths of 1 to 3 feet (usually sheet flow on sloping terrain); average depths determined. For areas of alluvial fan flooding, velocities also determined.
- ZONE AR** Special Flood Hazard Area Formerly protected from the 1% annual chance flood by a flood control system that was subsequently derelictified. Zone AR indicates that the former flood control system is being restored to provide protection from the 1% annual chance or greater flood.
- ZONE A99** Area to be protected from 1% annual chance flood by a Federal flood protection system under construction; no Base Flood Elevations determined.
- ZONE V** Coastal flood zone with velocity hazard (wave action); no Base Flood Elevations determined.
- ZONE VE** Coastal flood zone with velocity hazard (wave action); Base Flood Elevations determined.
- FLOODWAY AREAS IN ZONE AE
- The floodway is the channel of a stream plus any adjacent floodplain areas that must be kept free of encroachment so that the 1% annual chance flood can be carried without substantial increases in flood heights.
- OTHER FLOOD AREAS
- ZONE X** Areas of 0.2% annual chance flood; areas of 1% annual chance flood with average depths of less than 1 foot or with drainage areas less than 1 square mile; and areas protected by levees from 1% annual chance flood.
- OTHER AREAS
- ZONE X** Areas determined to be outside the 0.2% annual chance floodplain.
- ZONE D** Areas in which flood hazards are undetermined, but possible.
- COASTAL BARRIER RESOURCES SYSTEM (CBRS) AREAS
- OTHERWISE PROTECTED AREAS (OPAs)
- CBRS areas and OPAs are normally located within or adjacent to Special Flood Hazard Areas.
- Floodplain boundary
- Floodway boundary
- Zone D boundary
- CBRS and OPA boundary
- Boundary dividing Special Flood Hazard Areas of different Base Flood Elevations, flood depths or flood velocities.
- Base Flood Elevation line and value; elevation in feet* (EL 987)
- Base Flood Elevation value where uniform within zone; elevation in feet
- * Referenced to the North American Vertical Datum of 1988 (NAVD 88)
- Cross section line
- Transect line
- Geographic coordinates referenced to the North American Datum of 1983 (NAD 83)
- 1000-meter Universal Transverse Mercator grid ticks, zone 13
- 5000-foot grid ticks: Colorado State Plane coordinate system, central zone (FIPSZONE 0502), Lambert Conformal Conic Projection
- Bench mark (see explanation in Notes to Users section of this FIRM panel)
- River Mile
- MAP REPOSITORIES
- Refer to Map Repositories list on Map Index
- EFFECTIVE DATE OF COUNTYWIDE FLOOD INSURANCE RATE MAP
MARCH 17, 1997
- EFFECTIVE DATE(S) OF REVISION(S) TO THIS PANEL
DECEMBER 7, 2018 - to update corporate limits, to change Base Flood Elevations and Special Flood Hazard Areas, to update map format, to add roads and road names, and to incorporate previously issued Letters of Map Revision.
- For community map revision history prior to countywide mapping, refer to the Community Map History Tables located in the Flood Insurance Study report for this jurisdiction.
- To determine if flood insurance is available in this community, contact your insurance agent or call the National Flood Insurance Program at 1-800-638-6620.

PANEL 0529G

FIRM
FLOOD INSURANCE RATE MAP
EL PASO COUNTY, COLORADO AND INCORPORATED AREAS

PANEL 529 OF 1300
(SEE MAP INDEX FOR FIRM PANEL LAYOUT)

CONTAINS:

COMMUNITY	NUMBER	PANEL	SUFFIX
COLORADO SPRINGS, CITY OF	08006	0529	G
EL PASO COUNTY	08029	0529	G

Notice to User: The Map Number shown below should be used when placing map orders. The Community Number shown above should be used on insurance applications for the subject community.

MAP NUMBER
08041C0529G

MAP REVISED
DECEMBER 7, 2018

Federal Emergency Management Agency



APPENDIX B – HYDROLOGIC CALCULATIONS

BASIN SUMMARY TABLE							
Tributary Sub-basin	Area (a.cres)	Percent Impervious	C_s	C_{100}	t_c (min)	Q_s (cfs)	Q_{100} (cfs)
EXA	0.25	2%	0.09	0.36	51.8	0.0	0.3
EXB	1.51	16%	0.18	0.42	34.8	0.6	2.4
EXC	11.55	2%	0.09	0.36	44.5	2.0	13.2
EXD	21.78	3%	0.10	0.36	48.7	3.7	23.3
EXE	3.96	2%	0.09	0.36	31.9	0.9	5.7
EXF	2.58	2%	0.09	0.36	27.1	0.6	4.1
EXG	39.67	2%	0.09	0.36	62.7	4.9	32.9
EXH	6.67	2%	0.09	0.36	26.6	1.6	10.7
EXI	10.29	2%	0.09	0.36	27.3	2.4	16.3
EXJ	0.33	2%	0.09	0.36	25.7	0.1	0.5
OSI4	27.16	-	0.30	0.40	29.2	19.0	44.2

Values in BLUE indicate they are from the "Silver Ponds Subdivision Filing No. 1 Final Drainage Report", by M.V.E. Inc. revised May 5th, 1996.

DESIGN POINT SUMMARY TABLE		
DP#	Q_{s-YR}	Q_{100-YR}
1	0.0	0.3
2	0.6	2.4
3	2.0	13.2
4	3.7	23.3
4.1	5.5	35.6
5	0.9	5.7
6	0.6	4.1
7	4.9	32.9
7.1	9.2	60.8
8	1.6	10.7
9	2.4	16.3
10	0.1	0.5
14	19.0	44.2

Values in BLUE indicate they are from the "Silver Ponds Subdivision Filing No. 1 Final Drainage Report", by M.V.E. Inc. revised May 5th, 1996.

COMPOSITE % IMPERVIOUS CALCULATIONS -EXISTING CONDITIONS

Subdivision: _____
 Location: El Paso County

Project Name: Schmidt Parcel-District Infrastructure
 Project No.: 24013.00
 Calculated By: REB
 Checked By: NQJ
 Date: 4/23/26

Basin ID	Total Area (ac)	Gravel Street (80% Imp.)				Undeveloped (2% Imp.)				Basins Total Weighted C		Basins Total Weighted % Imp.
		C ₅	C ₁₀₀	Area (ac)	Weighted % Imp.	C ₅	C ₁₀₀	Area (ac)	Weighted % Imp.	C ₅	C ₁₀₀	
										C ₅	C ₁₀₀	
EXA	0.25	0.59	0.70	0.00	0.0%	0.09	0.36	0.25	2.0%	0.09	0.36	2.0%
EXB	1.51	0.59	0.70	0.27	14.3%	0.09	0.36	1.24	1.6%	0.18	0.42	16.0%
EXC	11.55	0.59	0.70	0.00	0.0%	0.09	0.36	11.55	2.0%	0.09	0.36	2.0%
EXD	21.78	0.59	0.70	0.27	1.0%	0.09	0.36	21.51	2.0%	0.10	0.36	3.0%
EXE	3.96	0.59	0.70	0.00	0.0%	0.09	0.36	3.96	2.0%	0.09	0.36	2.0%
EXF	2.58	0.59	0.70	0.00	0.0%	0.09	0.36	2.58	2.0%	0.09	0.36	2.0%
EXG	39.67	0.59	0.70	0.00	0.0%	0.09	0.36	39.67	2.0%	0.09	0.36	2.0%
EXH	6.67	0.59	0.70	0.00	0.0%	0.09	0.36	6.67	2.0%	0.09	0.36	2.0%
EXI	10.29	0.59	0.70	0.00	0.0%	0.09	0.36	10.29	2.0%	0.09	0.36	2.0%
EXJ	0.33	0.59	0.70	0.00	0.0%	0.09	0.36	0.33	2.0%	0.09	0.36	2.0%
TOTAL	98.58											2.4%

STANDARD FORM SF-2 - EXISTING CONDITIONS TIME OF CONCENTRATION

Subdivision: _____
 Location: El Paso County

Project Name: Schmidt Parcel-District Infrastructure
 Project No.: 24013.00
 Calculated By: REB
 Checked By: NOJ
 Date: 4/27/26

SUB-BASIN DATA						INITIAL/OVERLAND (T _i)			TRAVEL TIME (T _t)					t _c CHECK (URBANIZED BASINS)			FINAL
BASIN ID	D.A. (ac)	Hydrologic Soils Group	Impervious (%)	C ₅	C ₁₀₀	L (ft)	S _o (%)	t _i (min)	L _t (ft)	S _t (%)	K	VEL. (ft/s)	t _t (min)	COMP. t _c (min)	TOTAL LENGTH (ft)	Urbanized t _c (min)	t _c (min)
EXA	0.25	A	2.0%	0.09	0.36	10.0	25.0%	2.0	1030	0.5%	7.0	0.5	34.7	36.7	1040.0	51.8	51.8
EXB	1.51	A	16.0%	0.18	0.42	10.0	25.0%	1.8	950	1.5%	15.0	1.8	8.6	10.4	960.0	34.8	34.8
EXC	11.55	A	2.0%	0.09	0.36	300.0	3.0%	22.0	1260	1.8%	7.0	0.9	22.5	44.5	1560.0	42.6	44.5
EXD	21.78	A	3.0%	0.10	0.36	300.0	2.3%	23.8	1400	1.8%	7.0	0.9	24.8	48.7	1700.0	44.0	48.7
EXE	3.96	A	2.0%	0.09	0.36	300.0	2.1%	24.8	425	2.1%	7.0	1.0	7.0	31.9	725.0	31.0	31.9
EXF	2.58	A	2.0%	0.09	0.36	200.0	2.6%	18.9	123	2.3%	7.0	1.1	1.9	20.8	323.0	27.1	27.1
EXG	39.67	A	2.0%	0.09	0.36	200.0	1.0%	25.8	2300	2.2%	7.0	1.0	36.9	62.7	2500.0	53.5	62.7
EXH	6.67	A	2.0%	0.09	0.36	180.0	2.6%	17.9	100	4.0%	7.0	1.4	1.2	19.1	280.0	26.6	26.6
EXI	10.29	A	2.0%	0.09	0.36	300.0	2.0%	25.1	261	8.0%	7.0	2.0	2.2	27.3	561.0	27.3	27.3
EXJ	0.33	A	2.0%	0.09	0.36	22.0	2.6%	6.3	0	0.0%	7.0	0.0	0.0	6.3	22.0	25.7	25.7

NOTES:

$$t_c = t_i + t_t$$

Where:

t_c = computed time of concentration (minutes)

t_i = overland (initial) flow time (minutes)

t_t = channelized flow time (minutes).

$$t_t = \frac{L_t}{60K\sqrt{S_o}} = \frac{L_t}{60V_t}$$

Where:

t_t = channelized flow time (travel time, min)
 L_t = waterway length (ft)
 S_o = waterway slope (ft/ft)
 V_t = travel time velocity (ft/sec) = K√S_o
 K = NRCS conveyance factor (see Table 6-2).

Equation 6-2
$$t_i = \frac{0.395(1.1 - C_5)\sqrt{L}}{S_o^{0.33}}$$

Where:

t_i = overland (initial) flow time (minutes)
 C₅ = runoff coefficient for 5-year frequency (from Table 6-4)
 L = length of overland flow (ft)
 S_o = average slope along the overland flow path (ft/ft).

Equation 6-4
$$t_t = (26 - 17i) + \frac{L_t}{60(14i + 9)\sqrt{S_t}}$$

Where:

t_t = minimum time of concentration for first design point when less than t_c from Equation 6-1.
 L_t = length of channelized flow path (ft)
 i = imperviousness (expressed as a decimal)
 S_t = slope of the channelized flow path (ft/ft).

Table 6-2. NRCS Conveyance factors, K

Type of Land Surface	Conveyance Factor, K
Heavy meadow	2.5
Tillage/field	5
Short pasture and lawns	7
Nearly bare ground	10
Grassed waterway	15
Paved areas and shallow paved swales	20

Equation 6-5

Use a minimum t_c value of 5 minutes for urbanized areas and a minimum t_c value of 10 minutes for areas that are not considered urban. Use minimum values even when calculations result in a lesser time of concentration.

STANDARD FORM SF-2 - EXISTING CONDITIONS TIME OF CONCENTRATION

Subdivision: _____
 Location: El Paso County

Project Name: Schmidt Parcel-District Infrastructure
 Project No.: 24013.00
 Calculated By: REB
 Checked By: NOJ
 Date: 4/27/26

SUB-BASIN DATA						INITIAL/OVERLAND (T _i)			TRAVEL TIME (T _t)					t _c CHECK (URBANIZED BASINS)			FINAL
BASIN ID	D.A. (ac)	Hydrologic Soils Group	Impervious (%)	C ₅	C ₁₀₀	L (ft)	S _o (%)	t _i (min)	L _t (ft)	S _t (%)	K	VEL. (ft/s)	t _t (min)	COMP. t _c (min)	TOTAL LENGTH (ft)	Urbanized t _c (min)	t _c (min)
EXA	0.25	A	2.0%	0.09	0.36	10.0	25.0%	2.0	1030	0.5%	7.0	0.5	34.7	36.7	1040.0	51.8	51.8
EXB	1.51	A	16.0%	0.18	0.42	10.0	25.0%	1.8	950	1.5%	15.0	1.8	8.6	10.4	960.0	34.8	34.8
EXC	11.55	A	2.0%	0.09	0.36	300.0	3.0%	22.0	1260	1.8%	7.0	0.9	22.5	44.5	1560.0	42.6	44.5
EXD	21.78	A	3.0%	0.10	0.36	300.0	2.3%	23.8	1400	1.8%	7.0	0.9	24.8	48.7	1700.0	44.0	48.7
EXE	3.96	A	2.0%	0.09	0.36	300.0	2.1%	24.8	425	2.1%	7.0	1.0	7.0	31.9	725.0	31.0	31.9
EXF	2.58	A	2.0%	0.09	0.36	200.0	2.6%	18.9	123	2.3%	7.0	1.1	1.9	20.8	323.0	27.1	27.1
EXG	39.67	A	2.0%	0.09	0.36	200.0	1.0%	25.8	2300	2.2%	7.0	1.0	36.9	62.7	2500.0	53.5	62.7
EXH	6.67	A	2.0%	0.09	0.36	180.0	2.6%	17.9	100	4.0%	7.0	1.4	1.2	19.1	280.0	26.6	26.6
EXI	10.29	A	2.0%	0.09	0.36	300.0	2.0%	25.1	261	8.0%	7.0	2.0	2.2	27.3	561.0	27.3	27.3
EXJ	0.33	A	2.0%	0.09	0.36	22.0	2.6%	6.3	0	0.0%	7.0	0.0	0.0	6.3	22.0	25.7	25.7

NOTES:

$$t_c = t_i + t_t$$

Where:

t_c = computed time of concentration (minutes)

t_i = overland (initial) flow time (minutes)

t_t = channelized flow time (minutes).

$$t_t = \frac{L_t}{60K\sqrt{S_t}} = \frac{L_t}{60V_t}$$

Where:

t_t = channelized flow time (travel time, min)
 L_t = waterway length (ft)
 S_t = waterway slope (ft/ft)
 V_t = travel time velocity (ft/sec) = K√S_t
 K = NRCS conveyance factor (see Table 6-2).

Equation 6-2
$$t_i = \frac{0.395(1.1 - C_5)\sqrt{L}}{S_o^{0.33}}$$

Where:

t_i = overland (initial) flow time (minutes)
 C₅ = runoff coefficient for 5-year frequency (from Table 6-4)
 L = length of overland flow (ft)
 S_o = average slope along the overland flow path (ft/ft).

Equation 6-4
$$t_t = (26 - 17i) + \frac{L_t}{60(14i + 9)\sqrt{S_t}}$$

Where:

t_t = minimum time of concentration for first design point when less than t_c from Equation 6-1.
 L_t = length of channelized flow path (ft)
 i = imperviousness (expressed as a decimal)
 S_t = slope of the channelized flow path (ft/ft).

Table 6-2. NRCS Conveyance factors, K

Type of Land Surface	Conveyance Factor, K
Heavy meadow	2.5
Tillage/field	5
Short pasture and lawns	7
Nearly bare ground	10
Grassed waterway	15
Paved areas and shallow paved swales	20

Equation 6-5

Use a minimum t_c value of 5 minutes for urbanized areas and a minimum t_c value of 10 minutes for areas that are not considered urban. Use minimum values even when calculations result in a lesser time of concentration.

STANDARD FORM SF-3 - EXISTING CONDITIONS
STORM DRAINAGE SYSTEM DESIGN
(RATIONAL METHOD PROCEDURE)

Subdivision: _____
Location: El Paso County _____
Design Storm: 5-Year _____

Project Name: Schmidt Parcel-District Infrastructure _____
Project No.: 24013.00 _____
Calculated By: REB _____
Checked By: NQJ _____
Date: 4/27/26 _____

STREET	Design Point	DIRECT RUNOFF							TOTAL RUNOFF				STREET			PIPE			TRAVEL TIME			REMARKS	
		Basin ID	Area (Ac)	Runoff Coeff.	t_c (min)	C*A (Ac)	I (in/hr)	Q (cfs)	t_c (min)	C*A (ac)	I (in/hr)	Q (cfs)	Q_{street} (cfs)	C*A (ac)	Slope (%)	Q_{pipe} (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)		t_t (min)
	14	OS14	27.16	0.30	29.2	8.15	2.33	19.0															Off-site Basin OS14 Values from Sliver Pond FDR (Bains I4 & DP21)
	1	EXA	0.25	0.09	51.8	0.02	1.66	0.0															Existing berm sends off-site flow from north to the west to the existing swale at DP1.
	2	EXB	1.51	0.18	34.8	0.27	2.26	0.6															Existing berm sends off-site flow from north to the east to the existing swale and culvert at DP2.
	3	EXC	11.55	0.09	44.5	1.04	1.89	2.0															Runoff overland flows to existing swale and continues into Basin EXD at DP3.
	4	EXD	21.78	0.10	48.7	2.10	1.75	3.7															Runoff from Basin EXD, overland flows to existing swale at DP4.
	4.1								48.7	3.13	1.75	5.5	48.7	27.75	1.2								Flows from DP3 and DP4 combine at DP4.1 and flows to the west to the existing TSB, continue to DP7.1
	5	EXE	3.96	0.09	31.9	0.36	2.39	0.9															Runoff overland flows across existing field to DPS where flow enters Vollmer Road R.O.W.
	6	EXF	2.58	0.09	27.1	0.23	2.63	0.6															Runoff from Basin EXF overland flows south off-site and enters the adjacent property.
	7	EXG	39.67	0.09	62.7	3.57	1.38	4.9															Runoff overland flows SW, enters ex TSB, continues to DP7.1
	7.1								62.7	6.71	1.38	9.2											Combined flow @ DP7.1 from Basin G and DP 4.1, enters Cottonwood Creek and flows off-site
	8	EXH	6.67	0.09	26.6	0.60	2.66	1.6															Runoff from Basin EXH overland flows west, off-site and enters Cottonwood Creek @ DP8
	9	EXI	10.29	0.09	27.3	0.93	2.62	2.4															Runoff from Basin EXI overland flows south and enters Cottonwood Creek & flow off-site.
	10	EXJ	0.33	0.09	25.7	0.03	2.72	0.1															Runoff from Basin EXJ overland flows south off-site and enters the adjacent property.

Notes:
Street and Pipe C*A values are determined by Q/i using the catchment's intensity value.
Values in BLUE indicate they are from the "Silver Ponds Subdivision Filing No. 1 Final Drainage Report", by M.V.E. Inc. revised May 5th, 1996.

IDF Equations

$I_{100} = -2.52 \ln(D) + 12.735$

$I_{50} = -2.25 \ln(D) + 11.375$

$I_{25} = -2.00 \ln(D) + 10.111$

$I_{10} = -1.75 \ln(D) + 8.847$

$I_5 = -1.50 \ln(D) + 7.583$

$I_1 = -1.19 \ln(D) + 6.035$

Note: Values calculated by equations may not precisely duplicate values read from figure.

STANDARD FORM SF-3 - EXISTING CONDITIONS
STORM DRAINAGE SYSTEM DESIGN
(RATIONAL METHOD PROCEDURE)

Subdivision: _____
Location: El Paso County _____
Design Storm: 100-Year _____

Project Name: Schmidt Parcel-District Infrastructure _____
Project No.: 24013.00 _____
Calculated By: REB _____
Checked By: NJQ _____
Date: 4/27/26 _____

STREET	Design Point	DIRECT RUNOFF							TOTAL RUNOFF				STREET			PIPE				TRAVEL TIME			REMARKS
		Basin ID	Area (ac)	Runoff Coeff.	t _c (min)	C*A (ac)	I (in/hr)	Q (cfs)	t _c (min)	C*A (ac)	I (in/hr)	Q (cfs)	Q _{street} (cfs)	C*A (ac)	Slope (%)	Q _{pipe} (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	t _r (min)	
	14	OSI4	27.16	0.40	29.2	10.86	4.07	44.2															Off-site Basin OSI4 Values from Sliver Pond FDR (Bains I4 & DP21)
	1	EXA	0.25	0.36	51.8	0.09	2.79	0.3															Existing berm sends off-site flow from north to the west to the existing swale at DP1.
	2	EXB	1.51	0.42	34.8	0.63	3.79	2.4															Existing berm sends off-site flow from north to the east to the existing swale and culvert at DP2.
	3	EXC	11.55	0.36	44.5	4.16	3.17	13.2															Runoff overland flows to existing swale and continues into Basin EXD at DP3.
	4	EXD	21.78	0.36	48.7	7.93	2.94	23.3															Runoff from Basin EXD, overland flows to existing swale at DP4.
	4.1								48.7	12.09	2.94	35.6	48.7	16.5	1.2					1231	1.6	12.5	Flows from DP3 and DP4 combine at DP2.1 and flows to the west to the existing sediment basin.
	5	EXE	3.96	0.36	31.9	1.42	4.01	5.7															Runoff overland flows across existing field to DP5 where flow enters Vollmer Road R.O.W.
	6	EXF	2.58	0.36	27.1	0.93	4.42	4.1															Runoff from Basin EXF overland flows south off-site and enters the adjacent property.
	7	EXG	39.67	0.36	62.7	14.28	2.31	32.9															Runoff overland flows SW, enters ex TSB, continues to DP7.1
	7.1								62.7	26.37	2.31	60.8											Combined flow @ DP7.1 from Basin G and DP 4.1, enters Cottonwood Creek and flows off-site
	8	EXH	6.67	0.36	26.6	2.40	4.47	10.7															Runoff from Basin EXH overland flows west, off-site and enters Cottonwood Creek @ DP8
	9	EXI	10.29	0.36	27.3	3.70	4.40	16.3															Runoff from Basin EXI overland flows south and enters Cottonwood Creek & flow off-site.
	10	EXJ	0.33	0.36	25.7	0.12	4.56	0.5															Runoff from Basin EXJ overland flows south off-site and enters the adjacent property.

Notes:
Street and Pipe C*A values are determined by Q/i using the catchment's intensity value.
Values in BLUE indicate they are from the "Silver Ponds Subdivision Filing No. 1 Final Drainage Report", by M.V.E. Inc. revised May 5th, 1996.

IDF Equations

$I_{100} = -2.52 \ln(D) + 12.735$
 $I_{50} = -2.25 \ln(D) + 11.375$
 $I_{25} = -2.00 \ln(D) + 10.111$
 $I_{10} = -1.75 \ln(D) + 8.847$
 $I_1 = -1.50 \ln(D) + 7.583$
 $I_2 = -1.19 \ln(D) + 6.035$

Note: Values calculated by equations may not precisely duplicate values read from figure.

BASIN SUMMARY TABLE							
Tributary Sub-basin	Area (acres)	Percent Impervious	C ₅	C ₁₀₀	t _c (min)	Q ₅ (cfs)	Q ₁₀₀ (cfs)
A	0.25	0%	0.08	0.35	53.0	0.0	0.2
B	0.09	0%	0.08	0.35	36.1	0.0	0.1
C	1.85	31%	0.34	0.54	26.9	1.6	4.4
D	1.18	54%	0.52	0.68	21.5	1.8	4.0
E	6.66	0%	0.08	0.35	36.8	1.2	8.5
F	2.56	25%	0.29	0.50	29.5	1.8	5.4
G	0.78	85%	0.78	0.87	16.9	2.0	3.8
H	3.59	0%	0.08	0.35	30.7	0.7	5.2
I	1.22	80%	0.73	0.84	17.5	2.9	5.6
J	1.28	87%	0.79	0.88	16.0	3.5	6.5
K	24.33	0%	0.08	0.35	43.9	3.7	27.3
L	36.07	0%	0.08	0.35	53.6	4.6	34.1
M	4.86	0%	0.08	0.35	44.3	0.7	5.4
N	0.34	0%	0.08	0.35	26.1	0.1	0.5
O	0.56	0%	0.08	0.35	26.7	0.1	0.9
P	2.68	0%	0.08	0.35	26.1	0.6	4.2
Q	10.29	0%	0.08	0.35	47.7	1.5	10.8
OSI4	27.16	-	0.30	0.40	29.2	19.0	44.2

Values in BLUE indicate they are from the "Silver Ponds Subdivision Filing No. 1 Final Drainage Report", by M.V.E. Inc. revised May 5th, 1996.

DESIGN POINT SUMMARY TABLE		
DP#	Q _{5-YR}	Q _{100-YR}
1	0.0	0.2
2	0.0	0.1
3	1.6	4.4
4	1.8	4.0
4.1	3.2	7.9
5	3.9	15.1
5.1	13.4	55.8
6	1.8	5.4
7	2.0	3.8
7.1	3.4	8.3
9	2.9	9.3
10	3.5	6.5
10.1	5.3	13.9
11	3.7	27.3
11.1	7.9	38.0
11.2	10.4	44.3
13	4.6	34.1
13.1	16.3	82.8
14	17.0	87.4
15	0.1	0.5
16	0.1	0.9
17	0.6	4.2
18	1.5	10.8
14	19.0	44.2

Values in BLUE indicate they are from the "Silver Ponds Subdivision Filing No. 1 Final Drainage Report", by M.V.E. Inc. revised May 5th, 1996.



COMPOSITE % IMPERVIOUS CALCULATIONS -PROPOSED CONDITIONS

Subdivision: Schmidt Parcel - District P1
Location: El Paso County

Project Name: Schmidt Parcel - INTERIM
Project No.: 24013.00
Calculated By: REB
Checked By:
Date: 4/29/26

Basin ID	Total Area (ac)	Paved Streets and Walks (100% Imp.)				Apartments/Mixed Use (75% Imp.)				FUTURE DEVELOPMENT (62.5%)				Lawns/Pasture (0% Imp.)				Basins Total Weighted C		Basins Total Weighted
		C ₅	C ₁₀₀	Area (ac)	Weighted % Imp.	C ₅	C ₁₀₀	Area (ac)	Weighted % Imp.	C ₅	C ₁₀₀	Area (ac)	Weighted % Imp.	C ₅	C ₁₀₀	Area (ac)	Weighted % Imp.	C ₅	C ₁₀₀	
A	0.25	0.90	0.96	0.00	0.0%	0.53	0.66	0.00	0.0%	0.45	0.59	0.00	0.0%	0.08	0.35	0.25	0.0%	0.08	0.35	0.0%
B	0.09	0.90	0.96	0.00	0.0%	0.53	0.66	0.00	0.0%	0.45	0.59	0.00	0.0%	0.08	0.35	0.09	0.0%	0.08	0.35	0.0%
C	1.85	0.90	0.96	0.58	31.2%	0.53	0.66	0.00	0.0%	0.45	0.59	0.00	0.0%	0.08	0.35	1.27	0.0%	0.34	0.54	31.2%
D	1.18	0.90	0.96	0.64	54.2%	0.53	0.66	0.00	0.0%	0.45	0.59	0.00	0.0%	0.08	0.35	0.54	0.0%	0.52	0.68	54.2%
E	6.66	0.90	0.96	0.00	0.0%	0.53	0.66	0.00	0.0%	0.45	0.59	0.00	0.0%	0.08	0.35	6.66	0.0%	0.08	0.35	0.0%
F	2.56	0.90	0.96	0.65	25.3%	0.53	0.66	0.00	0.0%	0.45	0.59	0.00	0.0%	0.08	0.35	1.91	0.0%	0.29	0.50	25.3%
G	0.78	0.90	0.96	0.67	85.1%	0.53	0.66	0.00	0.0%	0.45	0.59	0.00	0.0%	0.08	0.35	0.12	0.0%	0.78	0.87	85.1%
H	3.59	0.90	0.96	0.00	0.0%	0.53	0.66	0.00	0.0%	0.45	0.59	0.00	0.0%	0.08	0.35	3.59	0.0%	0.08	0.35	0.0%
I	1.22	0.90	0.96	0.97	79.6%	0.53	0.66	0.00	0.0%	0.45	0.59	0.00	0.0%	0.08	0.35	0.25	0.0%	0.73	0.84	79.6%
J	1.28	0.90	0.96	1.12	87.2%	0.53	0.66	0.00	0.0%	0.45	0.59	0.00	0.0%	0.08	0.35	0.16	0.0%	0.79	0.88	87.2%
K	24.33	0.90	0.96	0.00	0.0%	0.53	0.66	0.00	0.0%	0.45	0.59	0.00	0.0%	0.08	0.35	24.33	0.0%	0.08	0.35	0.0%
L	36.07	0.90	0.96	0.00	0.0%	0.53	0.66	0.00	0.0%	0.45	0.59	0.00	0.0%	0.08	0.35	36.07	0.0%	0.08	0.35	0.0%
M	4.86	0.90	0.96	0.00	0.0%	0.53	0.66	0.00	0.0%	0.45	0.59	0.00	0.0%	0.08	0.35	4.86	0.0%	0.08	0.35	0.0%
N	0.34	0.90	0.96	0.00	0.0%	0.53	0.66	0.00	0.0%	0.45	0.59	0.00	0.0%	0.08	0.35	0.34	0.0%	0.08	0.35	0.0%
O	0.56	0.90	0.96	0.00	0.0%	0.53	0.66	0.00	0.0%	0.45	0.59	0.00	0.0%	0.08	0.35	0.56	0.0%	0.08	0.35	0.0%
P	2.68	0.90	0.96	0.00	0.0%	0.53	0.66	0.00	0.0%	0.45	0.59	0.00	0.0%	0.08	0.35	2.68	0.0%	0.08	0.35	0.0%
Q	10.29	0.90	0.96	0.00	0.0%	0.53	0.66	0.00	0.0%	0.45	0.59	0.00	0.0%	0.08	0.35	10.29	0.0%	0.08	0.35	0.0%
TOTAL POND	84.37																			5.5%
TOTAL (ON-SITE)	98.58																			4.7%



STANDARD FORM SF-2 - PROPOSED CONDITIONS TIME OF CONCENTRATION

Subdivision: Schmidt Parcel - District P1
Location: El Paso County

Project Name: Schmidt Parcel - INTERIM
Project No.: 24013.00
Calculated By: REB
Checked By: _____
Date: 4/24/26

SUB-BASIN						INITIAL/OVERLAND			TRAVEL TIME					tc CHECK			FINAL
DATA						(T _i)			(T _t)					(URBANIZED BASINS)			
BASIN ID	D.A. (ac)	Hydrologic Soils Group	Impervious (%)	C _s	C ₁₀₀	L (ft)	S _o (%)	t _i (min)	L _t (ft)	S _t (%)	K	VEL. (ft/s)	t _t (min)	COMP. t _c (min)	TOTAL LENGTH (ft)	Urbanized t _c (min)	
A	0.25	A	0.0%	0.08	0.35	10.0	25.0%	2.0	1030	0.5%	15.0	1.1	16.2	18.2	1040.0	53.0	53.0
B	0.09	A	0.0%	0.08	0.35	10.0	25.0%	2.0	385	0.5%	15.0	1.1	6.0	8.1	395.0	36.1	36.1
C	1.85	A	31.2%	0.34	0.54	100.0	1.8%	11.4	525	1.1%	20.0	2.1	4.2	15.5	625.0	26.9	26.9
D	1.18	A	54.2%	0.52	0.68	85.0	2.0%	7.6	490	1.1%	20.0	2.1	3.9	11.5	575.0	21.5	21.5
E	6.66	A	0.0%	0.08	0.35	100.0	6.0%	10.2	900	2.4%	15.0	2.3	6.5	16.7	1000.0	36.8	36.8
F	2.56	A	25.3%	0.29	0.50	45.0	2.0%	7.8	1050	3.2%	20.0	3.6	4.9	12.7	1095.0	29.5	29.5
G	0.78	A	85.1%	0.78	0.87	50.0	2.0%	3.3	1050	2.4%	20.0	3.1	5.6	8.9	1100.0	16.9	16.9
H	3.59	A	0.0%	0.08	0.35	100.0	4.5%	11.2	435	3.0%	15.0	2.6	2.8	14.0	535.0	30.7	30.7
I	1.22	A	79.6%	0.73	0.84	85.0	2.0%	4.9	820	1.8%	20.0	2.7	5.1	10.0	905.0	17.5	17.5
J	1.28	A	87.2%	0.79	0.88	85.0	2.0%	4.0	820	1.8%	20.0	2.7	5.1	9.1	905.0	16.0	16.0
K	24.33	A	0.0%	0.08	0.35	100.0	2.9%	13.0	1530	2.5%	7.0	1.1	23.0	36.0	1630.0	43.9	43.9
L	36.07	A	0.0%	0.08	0.35	100.0	2.0%	14.7	2000	1.8%	7.0	0.9	35.5	50.1	2100.0	53.6	53.6
M	4.86	A	0.0%	0.08	0.35	100.0	2.0%	14.7	700	0.5%	15.0	1.1	11.0	25.7	800.0	44.3	44.3
N	0.34	A	0.0%	0.08	0.35	10	25.0%	2.0	5	2.0%	10.0	1.4	0.1	2.1	15.0	26.1	26.1
O	0.56	A	0.0%	0.08	0.35	25	2.0%	7.3	60	2.5%	10.0	1.6	0.6	8.0	85.0	26.7	26.7
P	2.68	A	0.0%	0.08	0.35	10	25.0%	2.0	5	0.5%	10.0	0.7	0.1	2.1	15.0	26.1	26.1
Q	10.29	A	0.0%	0.08	0.35	100	30.0%	6.0	1170	1.0%	10.0	1.0	19.5	25.5	1270.0	47.7	47.7

NOTES:

$$t_c = t_i + t_t$$

Where:

t_c = computed time of concentration (minutes)

t_i = overland (initial) flow time (minutes)

t_t = channelized flow time (minutes)

$$t_t = \frac{L_t}{60K\sqrt{S_o}} = \frac{L_t}{60V_t}$$

Where:

t_t = channelized flow time (travel time, min)

L_t = waterway length (ft)

S_o = waterway slope (ft/ft)

V_t = travel time velocity (ft/sec) = K√S_o

K = NRCS conveyance factor (see Table 6-2)

Equation 6-2

$$t_i = \frac{0.395(1.1 - C_i)\sqrt{L}}{S_o^{0.333}}$$

Where:

t_i = overland (initial) flow time (minutes)

C_s = runoff coefficient for 5-year frequency (from Table 6-4)

L_i = length of overland flow (ft)

S_o = average slope along the overland flow path (ft/ft)

Equation 6-4

$$t_t = (26 - 17i) + \frac{L_t}{60(14i + 9)\sqrt{S_o}}$$

Where:

t_t = minimum time of concentration for first design point when less than t_c from Equation 6-1.

L_t = length of channelized flow path (ft)

i = imperviousness (expressed as a decimal)

S_o = slope of the channelized flow path (ft/ft)

Equation 6-3

Equation 6-5

Table 6-2. NRCS Conveyance factors, K

Type of Land Surface	Conveyance Factor, K
Heavy meadow	2.5
Tillage/field	5
Short pasture and lawns	7
Nearly bare ground	10
Grassed waterway	15
Paved areas and shallow paved swales	20

Use a minimum t_c value of 5 minutes for urbanized areas and a minimum t_c value of 10 minutes for areas that are not considered urban. Use minimum values even when calculations result in a lesser time of concentration.

STANDARD FORM SF-3 - PROPOSED CONDITIONS
STORM DRAINAGE SYSTEM DESIGN
(RATIONAL METHOD PROCEDURE)

Subdivision: Schmidt Parcel - District P1
Location: El Paso County
Design Storm: 5-Year

Project Name: Schmidt Parcel - INTERIM
Project No.: 24013.00
Calculated By: REB
Checked By:
Date: 4/24/26

STREET	Design Point	DIRECT RUNOFF							TOTAL RUNOFF				STREET			PIPE			TRAVEL TIME		REMARKS		
		Basin ID	Area (Ac)	Runoff Coeff.	t_c (min)	C^*A (Ac)	I (in/hr)	Q (cfs)	t_c (min)	C^*A (ac)	I (in/hr)	Q (cfs)	Q_{street} (cfs)	C^*A (ac)	Slope (%)	Q_{pipe} (cfs)	C^*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)		Velocity (fps)	t_c (min)
	14	OS14	27.16	0.30	29.2	8.15	2.33	19.0															Off-site Basin OS14 Values from Sliver Pond FDR (Bains I4 & DP21)
	1	A	0.25	0.08	53.0	0.02	1.63	0.03															Existing berm sends off-site flow from north to the west to the existing swale at DP1.
	2	B	0.09	0.08	36.1	0.01	2.20	0.02															Existing berm sends off-site flow from north to the east to the existing swale and culvert at DP2.
	3	C	1.85	0.34	26.9	0.62	2.64	1.6							1.6	0.62	1.0	18	85	4.2	0.3		RUNOFF SHEET FLOWS TO C&G, CARRIED TO 5' TYPE R SUMP INLET @ DP3, CAPTURED FLOWS CONTINUE IN PIPE TO DP4.1
	3																						TOTAL FLOW @ DP3 [5' TYPE R SUMP INLET], CAPTURED FLOWS ARE PIPED TO DP4.1
	4	D	1.18	0.52	21.5	0.62	2.98	1.8															RUNOFF SHEET FLOWS TO C&G, CARRIED TO DP4 (5' TYPE R SUMP INLET), CAPTURED FLOWS PIPED TO DP4.1 WHERE THEY COMBINE WITH DP3 FLOWS
	4.1								27.3	1.24	2.62	3.2	3.2	1.24	2.8	3.2	1.24	2.0	24	1000	2.5	6.6	COMBINED FLOW IN PIPE FROM DP3 & 4, FLOWS DISCHARGE TO SWALE E1 AND ARE CARRIED TO DPS WHERE THEY COMBINE WITH BASIN E FLOWS
	5	E	6.66	0.08	36.8	0.53	2.18	1.2															RUNOFF SHEET FLOWS TOWARDS SWALE E1, FLOWS CONTINUE IN SWALE TO DPS, WHERE THEY COMBINE WITH FLOWS FROM DP4.1
	5								36.8	1.77	2.18	3.9											COMBINED FLOW IN SWALE E1 @ DPS, FLOWS CONTINUE TO DPS-1 IN SWALE L1
	6	F	2.56	0.29	29.5	0.74	2.51	1.8							1.8	0.74	1.0	18	40	4.4	0.2		RUNOFF SHEET FLOWS TO C&G, IS CARRIED TO 15' TYPE R ON-GRADE INLET @ DP 6, CAPTURED FLOWS ARE PIPED TO DP7.1
	7	G	0.78	0.78	16.9	0.61	3.34	2.0															RUNOFF SHEET FLOWS TO C&G, IS CARRIED TO 15' TYPE R ON-GRADE INLET @ DP 7, CAPTURED FLOWS ARE PIPED TO DP7.1
	7.1								29.6	1.35	2.50	3.4			3.4	1.35	1.0	24	45	5.1	0.1		COMBINED FLOW FROM DP6 & 7 IN 24" RCP, FLOWS ARE PIPED TO DP11.2
	9	H	3.59	0.08	30.7	0.29	2.45	0.7															BASIN H RUNOFF SHEET FLOWS TO C&G IN BASIN I, FLOWS CONTINUE TO DP9 (10' TYPE R SUMP) WHERE THEY COMBINE WITH BASIN I FLOWS
	9	I	1.22	0.73	17.5	0.89	3.29	2.9	30.7	1.18	2.45	2.9			2.9	1.18	1.0	24	90	4.8	0.3		BASIN I RUNOFF CARRIED BY C&G TO 10' TYPE R SUMP INLET @ DP9, WHERE FLOWS COMBINE WITH BASIN H FLOWS, CAPTURED FLOWS PIPED TO DP10.1
	10	J	1.28	0.79	16.0	1.02	3.43	3.5															BASIN J RUNOFF SHEET FLOWS TO C&G, IS CARRIED TO DP10 (5' TYPE R SUMP INLET), CAPTURED FLOWS ARE PIPED TO DP10.1
	10.1								31.0	2.19	2.43	5.3			5.3	2.19	1.0	36	1880	5.6	5.6		COMBINED FLOW IN PIPE @ DP10.1, FLOWS CONTINUE IN PIPE TO DP11.1
	11	K	24.33	0.08	43.9	1.95	1.91	3.7							3.7	1.95	2.3	36	136	6.6	0.3		RUNOFF SHEET FLOWS TOWARDS SWALE K1, FLOWS CONTINUE IN SWALE TO DP11. A TYPE C SUMP INLET/ CAPTURED FLOWS ARE PIPED TO DP11.1
	11.1								44.3	4.14	1.90	7.9			7.9	4.14	2.8	42	46	8.8	0.1		COMBINED FLOW IN PIPE @ DP 11.1 FROM DP11 RUNOFF & DP10.1 PIPED FLOW, FLOW CONTINUES IN 42" RCP TO DP11.2
	11.2								44.3	5.49	1.89	10.4	10.4	5.49	0.65								COMBINED FLOW IN PIPE @ DP 11.2, OUTFALLS TO SWALE L1, CONTINUE TO DPS.1, WHERE FLOWS COMBINE WITH DPS FLOWS IN SWALE L1
	5.1								46.0	7.26	1.84	13.4	13.4	7.26	1				1600	1.5	17.8		COMBINED FLOW IN SWALE L1 @ DP5.1, FLOWS CONTINUE IN SWALE TO DP13.1, WHERE THEY COMBINE WITH BASIN L RUNOFF
	13	L	36.07	0.08	53.6	2.89	1.61	4.6															RUNOFF FROM BASIN L, SHEET FLOWS TO SWALE @ DP13, FLOWS CONTINUE IN SWALE TO DP13.1 WHERE THEY COMBINE WITH DP5.1 FLOWS
	13.1								53.6	10.14	1.61	16.3											TOTAL FLOWS IN SWALE L1 @ DP13.1, FLOWS CONTINUE TO POND A @ DP14
	14	M	4.86	0.08	44.3	0.39	1.90	0.7	53.6	10.53	1.61	17.0											RUNOFF SHEET FLOWS INTO POND @ DP14 AND COMBINES WITH FLOWS FROM DP13.1
	15	N	0.34	0.08	26.1	0.03	2.69	0.1															RUNOFF SHEET FLOWS OFF-SITE @ DP 15
	16	O	0.56	0.08	26.7	0.04	2.66	0.1															RUNOFF SHEET FLOWS OFF-SITE @ DP 16
	17	P	2.68	0.08	26.1	0.21	2.69	0.6															RUNOFF SHEET FLOWS OFF-SITE @ DP 17
	18	Q	10.29	0.08	47.7	0.82	1.79	1.5															RUNOFF SHEET FLOWS OFF-SITE @ DP 18

Notes:
Street and Pipe C*A values are determined by Q/I using the catchment's intensity value.

IDF Equations
 $I_{30} = -2.52 \ln(D) + 12.735$
 $I_{60} = -2.25 \ln(D) + 11.375$
 $I_{90} = -2.00 \ln(D) + 10.111$
 $I_{120} = -1.75 \ln(D) + 8.847$
 $I_{180} = -1.50 \ln(D) + 7.583$
 $I_{240} = -1.19 \ln(D) + 6.325$
Note: Values estimated by equation may not precisely duplicate values read from figure.

STANDARD FORM SF-3 - PROPOSED CONDITIONS
STORM DRAINAGE SYSTEM DESIGN
 (RATIONAL METHOD PROCEDURE)

Subdivision: Schmidt Parcel - District P1
 Location: El Paso County
 Design Storm: 100-Year

Project Name: Schmidt Parcel - INTERIM
 Project No.: 24013.00
 Calculated By: REB
 Checked By:
 Date: 4/27/26

STREET	Design Point	DIRECT RUNOFF						TOTAL RUNOFF				STREET			PIPE			TRAVEL TIME			REMARKS					
		Basin ID	Area (ac)	Runoff Coeff.	t_c (min)	C*A (ac)	I (in/hr)	Q (cfs)	t_c (min)	C*A (ac)	I (in/hr)	Q (cfs)	Q_{street} (cfs)	C*A (ac)	Slope (%)	Q_{pipe} (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)		Velocity (fps)	t_t (min)			
	14	OS14	27.16	0.40	29.2	10.86	4.07	44.2															Existing berm sends off-site flow from north to the west to the existing swale at DP1.			
	1	A	0.25	0.35	53.0	0.09	2.73	0.2															Existing berm sends off-site flow from north to the east to the existing swale and culvert at DP2.			
	2	B	0.09	0.35	36.1	0.03	3.70	0.1															RUNOFF SHEET FLOWS TO C&G, CARRIED TO 5' TYPE R SUMP INLET @ DP3, CAPTURED FLOWS CONTINUE IN PIPE TO DP4.1			
	3	C	1.85	0.54	26.9	1.00	4.44	4.4							4.4	1.00	1.0	18	85	5.7	0.2		RUNOFF SHEET FLOWS TO C&G, CARRIED TO DP4 (5' TYPE R SUMP INLET). CAPTURED FLOWS PIPED TO DP4.1 WHERE THEY COMBINE WITH DP3 FLOWS			
	4	D	1.18	0.68	21.5	0.80	5.01	4.0															COMBINED FLOW IN PIPE FROM DP3 & 4, FLOWS DISCHARGE TO SWALE E1 AND ARE CARRIED TO DP5 WHERE THEY COMBINE WITH BASIN E FLOWS			
	4.1								27.2	1.80	4.41	7.9	7.9	1.8	2.8	7.9	1.80	2.0	24	1000	2.5	6.6	RUNOFF SHEET FLOWS TOWARDS SWALE E1, FLOWS CONTINUE IN SWALE TO DP5, WHERE THEY COMBINE WITH FLOWS FROM DP4.1			
	5	E	6.66	0.35	36.8	2.33	3.65	8.5															COMBINED FLOW IN SWALE E1 @ DP5, FLOWS CONTINUE TO DP5.1 IN SWALE L1			
	5								36.8	4.13	3.65	15.1														
	6	F	2.56	0.50	29.5	1.29	4.21	5.4								5.4	1.29	1.0	18	40	6.0	0.1	RUNOFF SHEET FLOWS TO C&G, IS CARRIED TO 15' TYPE R ON-GRADE INLET @ DP 6, CAPTURED FLOWS ARE PIPED TO DP7.1			
	7	G	0.78	0.87	16.9	0.68	5.60	3.8															RUNOFF SHEET FLOWS TO C&G, IS CARRIED TO 15' TYPE R ON-GRADE INLET @ DP 7, CAPTURED FLOWS ARE PIPED TO DP7.1			
	7.1								29.6	1.97	4.20	8.3											COMBINED FLOW FROM DP6 & 7 IN 24" RCP, FLOWS ARE PIPED TO DP11.2			
	9	H	3.59	0.35	30.7	1.26	4.11	5.2															BASIN H RUNOFF SHEET FLOWS TO C&G IN BASIN I, FLOWS CONTINUE TO DP9 (10' TYPE R SUMP) WHERE THEY COMBINE WITH BASIN I FLOWS			
	9	I	1.22	0.84	17.5	1.02	5.52	5.6	30.7	2.27	4.11	9.3				9.3	2.27	1.0	24	90	6.8	0.2	BASIN I RUNOFF CARREID BY C&G TO 10' TYPE R SUMP INLET @ DP9, WHERE FLOWS COMBINE WITH BASIN H FLOWS, CAPTURED FLOWS PIPED TO DP10.1			
	10	J	1.28	0.88	16.0	1.13	5.75	6.5															BASIN J RUNOFF SHEET FLOWS TO C&G, IS CARRIED TO DP10 (5' TYPE R SUMP INLET), CAPTURED FLOWS ARE PIPED TO DP10.1			
	10.1								30.9	3.40	4.09	13.9				13.9	3.40	1.0	36	1880	7.5	4.2	COMBINED FLOW IN PIPE @ DP10.1, FLOWS CONTINUE IN PIPE TO DP11.1			
	11	K	24.33	0.35	43.9	8.52	3.20	27.3								27.3	8.52	2.3	36	136	12.1	0.2	RUNOFF SHEET FLOWS TOWARDS SWALE K1, FLOWS CONTINUE IN SWALE TO DP11, A TYPE C SUMP INLET/ CAPTURED FLOWS ARE PIPED TO DP11.1			
	11.1								44.1	11.92	3.19	38.0				38.0	11.92	2.8	42	46	14.2	0.1	COMBINED FLOW IN PIPE @ DP 11.1 FROM DP11 RUNOFF & DP10.1 PIPED FLOW, FLOW CONTINUES IN 42" RCP TO DP11.2			
	11.2								44.2	13.89	3.19	44.3	44.3	13.9	0.65								120	1.2	1.7	COMBINED FLOW IN PIPE @ DP 11.2, OUTFALLS TO SWALE L1, CONTINUE TO DP5.1, WHERE FLOWS COMBINE WITH DP5 FLOWS IN SWALE L1
	5.1								45.8	18.02	3.10	55.8	55.8	18	1								1600	1.5	17.8	COMBINED FLOW IN SWALE L1 @ DP5.1, FLOWS CONTINUE IN SWALE TO DP13.1, WHERE THEY COMBINE WITH BASIN L RUNOFF
	13	L	36.07	0.35	53.6	12.63	2.70	34.1																RUNOFF FROM BASIN L, SHEET FLOWS TO SWALE @ DP13, FLOWS CONTINUE IN SWALE TO DP13.1 WHERE THEY COMBINE WITH DP5.1 FLOWS		
	13.1								53.6	30.64	2.70	82.8												TOTAL FLOWS IN SWALE L1 @ DP13.1, FLOWS CONTINUE TO POND A @ DP14		
	14	M	4.86	0.35	44.3	1.70	3.18	5.4	53.6	32.34	2.70	87.4												RUNOFF SHEET FLOWS INTO POND @ DP14 AND COMBINES WITH FLOWS FROM DP13.1		
	15	N	0.34	0.35	26.1	0.12	4.52	0.5																RUNOFF SHEET FLOWS OFF-SITE @ DP 15		
	16	O	0.56	0.35	26.7	0.20	4.46	0.9																RUNOFF SHEET FLOWS OFF-SITE @ DP 16		
	17	P	2.68	0.35	26.1	0.94	4.51	4.2																RUNOFF SHEET FLOWS OFF-SITE @ DP 17		
	18	Q	10.29	0.35	47.7	3.60	3.00	10.8																RUNOFF SHEET FLOWS OFF-SITE @ DP 18		

Notes:
 Street and Pipe C*A values are determined by Q/I using the catchment's intensity value.

IDF Equations

$$I_{60} = -2.52 \ln(D) + 12.735$$

$$I_{30} = -2.25 \ln(D) + 11.375$$

$$I_{24} = -2.00 \ln(D) + 10.111$$

$$I_{18} = -1.75 \ln(D) + 8.847$$

$$I_9 = -1.50 \ln(D) + 7.583$$

$$I_3 = -1.19 \ln(D) + 6.035$$

Note: Values calculated by equations may not precisely duplicate values read from figure.



APPENDIX C – HYDRAULIC CALCULATIONS

INLET MANAGEMENT

Worksheet Protected

INLET NAME	DP4	DP6	DP7
Site Type (Urban or Rural)	URBAN	URBAN	URBAN
Inlet Application (Street or Area)	STREET	STREET	STREET
Hydraulic Condition	In Sump	On Grade	On Grade
Inlet Type	CDOT Type R Curb Opening	CDOT Type R Curb Opening	CDOT Type R Curb Opening

USER-DEFINED INPUT

User-Defined Design Flows

Minor Q_{Known} (cfs)	1.8	1.8	2.0
Major Q_{Known} (cfs)	4.0	5.4	3.8

Bypass (Carry-Over) Flow from Upstream Inlets must be organized from upstream (left) to downstream (right) in order for bypass flows to be linked.

Receive Bypass Flow from:	No Bypass Flow Received	No Bypass Flow Received	No Bypass Flow Received
Minor Bypass Flow Received, Q_b (cfs)	0.0	0.0	0.0
Major Bypass Flow Received, Q_b (cfs)	0.0	0.0	0.0

Watershed Characteristics

Subcatchment Area (acres)			
Percent Impervious			
NRCS Soil Type			

Watershed Profile

Overland Slope (ft/ft)			
Overland Length (ft)			
Channel Slope (ft/ft)			
Channel Length (ft)			

Minor Storm Rainfall Input

Design Storm Return Period, T_r (years)			
One-Hour Precipitation, P_1 (inches)			

Major Storm Rainfall Input

Design Storm Return Period, T_r (years)			
One-Hour Precipitation, P_1 (inches)			

CALCULATED OUTPUT

Minor Total Design Peak Flow, Q (cfs)	1.8	1.8	2.0
Major Total Design Peak Flow, Q (cfs)	4.0	5.4	3.8
Minor Flow Bypassed Downstream, Q_b (cfs)	N/A	0.0	0.0
Major Flow Bypassed Downstream, Q_b (cfs)	N/A	0.0	0.0

INLET MANAGEMENT

Worksheet Protected

INLET NAME	DP9	DP10	DP3
Site Type (Urban or Rural)	URBAN	URBAN	URBAN
Inlet Application (Street or Area)	STREET	STREET	STREET
Hydraulic Condition	In Sump	In Sump	In Sump
Inlet Type	CDOT Type R Curb Opening	CDOT Type R Curb Opening	CDOT Type R Curb Opening

USER-DEFINED INPUT

User-Defined Design Flows

Minor Q_{known} (cfs)	2.9	3.5	1.6
Major Q_{known} (cfs)	9.3	6.5	4.4

Bypass (Carry-Over) Flow from Upstream

Receive Bypass Flow from:	No Bypass Flow Received	No Bypass Flow Received	No Bypass Flow Received
Minor Bypass Flow Received, Q_b (cfs)	0.0	0.0	0.0
Major Bypass Flow Received, Q_b (cfs)	0.0	0.0	0.0

Watershed Characteristics

Subcatchment Area (acres)			
Percent Impervious			
NRCS Soil Type			

Watershed Profile

Overland Slope (ft/ft)			
Overland Length (ft)			
Channel Slope (ft/ft)			
Channel Length (ft)			

Minor Storm Rainfall Input

Design Storm Return Period, T_r (years)			
One-Hour Precipitation, P_1 (inches)			

Major Storm Rainfall Input

Design Storm Return Period, T_r (years)			
One-Hour Precipitation, P_1 (inches)			

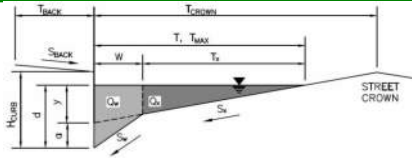
CALCULATED OUTPUT

Minor Total Design Peak Flow, Q (cfs)	2.9	3.5	1.6
Major Total Design Peak Flow, Q (cfs)	9.3	6.5	4.4
Minor Flow Bypassed Downstream, Q_b (cfs)	N/A	N/A	N/A
Major Flow Bypassed Downstream, Q_b (cfs)	N/A	N/A	N/A

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

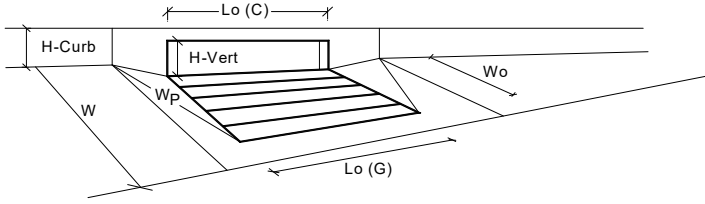
Project: Schmidt Parcel - District Infrastructure
Inlet ID: DP4



Gutter Geometry:						
Maximum Allowable Width for Spread Behind Curb	$T_{BACK} = 17.0$ ft					
Side Slope Behind Curb (leave blank for no conveyance credit behind curb)	$S_{BACK} = 0.020$ ft/ft					
Manning's Roughness Behind Curb (typically between 0.012 and 0.020)	$n_{BACK} = 0.020$					
Height of Curb at Gutter Flow Line	$H_{CURB} = 8.00$ inches					
Distance from Curb Face to Street Crown	$T_{CROWN} = 36.0$ ft					
Gutter Width	$W = 2.00$ ft					
Street Transverse Slope	$S_X = 0.020$ ft/ft					
Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)	$S_W = 0.083$ ft/ft					
Street Longitudinal Slope - Enter 0 for sump condition	$S_O = 0.000$ ft/ft					
Manning's Roughness for Street Section (typically between 0.012 and 0.020)	$n_{STREET} = 0.013$					
Max. Allowable Spread for Minor & Major Storm	<table border="1" style="display: inline-table; border-collapse: collapse;"> <tr> <td style="text-align: center;">Minor Storm</td> <td style="text-align: center;">Major Storm</td> <td rowspan="2" style="text-align: right; vertical-align: middle;">ft</td> </tr> <tr> <td style="text-align: center;">$T_{MAX} = 36.0$</td> <td style="text-align: center;">36.0</td> </tr> </table>	Minor Storm	Major Storm	ft	$T_{MAX} = 36.0$	36.0
Minor Storm	Major Storm	ft				
$T_{MAX} = 36.0$	36.0					
Max. Allowable Depth at Gutter Flowline for Minor & Major Storm	<table border="1" style="display: inline-table; border-collapse: collapse;"> <tr> <td style="text-align: center;">Minor Storm</td> <td style="text-align: center;">Major Storm</td> <td rowspan="2" style="text-align: right; vertical-align: middle;">inches</td> </tr> <tr> <td style="text-align: center;">$d_{MAX} = 8.0$</td> <td style="text-align: center;">8.0</td> </tr> </table>	Minor Storm	Major Storm	inches	$d_{MAX} = 8.0$	8.0
Minor Storm	Major Storm	inches				
$d_{MAX} = 8.0$	8.0					
Check boxes are not applicable in SUMP conditions	<input type="checkbox"/> <input type="checkbox"/>					
MINOR STORM Allowable Capacity is not applicable to Sump Condition						
MAJOR STORM Allowable Capacity is not applicable to Sump Condition						
	<table border="1" style="display: inline-table; border-collapse: collapse;"> <tr> <td style="text-align: center;">Minor Storm</td> <td style="text-align: center;">Major Storm</td> <td rowspan="2" style="text-align: right; vertical-align: middle;">cfs</td> </tr> <tr> <td style="text-align: center;">$Q_{allow} = \text{SUMP}$</td> <td style="text-align: center;">SUMP</td> </tr> </table>	Minor Storm	Major Storm	cfs	$Q_{allow} = \text{SUMP}$	SUMP
Minor Storm	Major Storm	cfs				
$Q_{allow} = \text{SUMP}$	SUMP					

INLET IN A SUMP OR SAG LOCATION

MHFD-Inlet, Version 5.03 (August 2023)

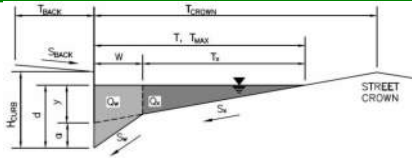


Design Information (Input)		<table border="1" style="margin-left: auto; margin-right: auto;"> <tr> <th style="width: 50%;">MINOR</th> <th style="width: 50%;">MAJOR</th> </tr> <tr> <td colspan="2" style="text-align: center;">CDOT Type R Curb Opening</td> </tr> <tr> <td>Type =</td> <td>CDOT Type R Curb Opening</td> </tr> <tr> <td>a_{local} =</td> <td>1.00</td> </tr> <tr> <td>No =</td> <td>1</td> </tr> <tr> <td>Ponding Depth =</td> <td>8.0</td> </tr> <tr> <td colspan="2" style="text-align: center;">Override Depths</td> </tr> <tr> <td>L_o (G) =</td> <td>N/A</td> </tr> <tr> <td>W_o =</td> <td>N/A</td> </tr> <tr> <td>A_{ratio} =</td> <td>N/A</td> </tr> <tr> <td>C_f (G) =</td> <td>N/A</td> </tr> <tr> <td>C_w (G) =</td> <td>N/A</td> </tr> <tr> <td>C_o (G) =</td> <td>N/A</td> </tr> <tr> <td colspan="2" style="text-align: center;">MINOR</td> </tr> <tr> <td>L_o (C) =</td> <td>5.00</td> </tr> <tr> <td>H_{vert} =</td> <td>6.00</td> </tr> <tr> <td>H_{throat} =</td> <td>6.00</td> </tr> <tr> <td>Theta =</td> <td>63.40</td> </tr> <tr> <td>W_p =</td> <td>2.00</td> </tr> <tr> <td>C_f (C) =</td> <td>0.10</td> </tr> <tr> <td>C_w (C) =</td> <td>3.60</td> </tr> <tr> <td>C_o (C) =</td> <td>0.67</td> </tr> <tr> <td colspan="2" style="text-align: center;">MAJOR</td> </tr> <tr> <td>L_o (C) =</td> <td>5.00</td> </tr> <tr> <td>H_{vert} =</td> <td>6.00</td> </tr> <tr> <td>H_{throat} =</td> <td>6.00</td> </tr> <tr> <td>Theta =</td> <td>63.40</td> </tr> <tr> <td>W_p =</td> <td>2.00</td> </tr> <tr> <td>C_f (C) =</td> <td>0.10</td> </tr> <tr> <td>C_w (C) =</td> <td>3.60</td> </tr> <tr> <td>C_o (C) =</td> <td>0.67</td> </tr> </table>		MINOR	MAJOR	CDOT Type R Curb Opening		Type =	CDOT Type R Curb Opening	a _{local} =	1.00	No =	1	Ponding Depth =	8.0	Override Depths		L _o (G) =	N/A	W _o =	N/A	A _{ratio} =	N/A	C _f (G) =	N/A	C _w (G) =	N/A	C _o (G) =	N/A	MINOR		L _o (C) =	5.00	H _{vert} =	6.00	H _{throat} =	6.00	Theta =	63.40	W _p =	2.00	C _f (C) =	0.10	C _w (C) =	3.60	C _o (C) =	0.67	MAJOR		L _o (C) =	5.00	H _{vert} =	6.00	H _{throat} =	6.00	Theta =	63.40	W _p =	2.00	C _f (C) =	0.10	C _w (C) =	3.60	C _o (C) =	0.67
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Type of Inlet	CDOT Type R Curb Opening																																																																
Local Depression (additional to continuous gutter depression 'a' from above)																																																																	
Number of Unit Inlets (Grate or Curb Opening)																																																																	
Water Depth at Flowline (outside of local depression)																																																																	
Grate Information																																																																	
Length of a Unit Grate																																																																	
Width of a Unit Grate																																																																	
Open Area Ratio for a Grate (typical values 0.15-0.90)																																																																	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)																																																																	
Grate Weir Coefficient (typical value 2.15 - 3.60)																																																																	
Grate Orifice Coefficient (typical value 0.60 - 0.80)																																																																	
Curb Opening Information																																																																	
Length of a Unit Curb Opening																																																																	
Height of Vertical Curb Opening in Inches																																																																	
Height of Curb Orifice Throat in Inches																																																																	
Angle of Throat																																																																	
Side Width for Depression Pan (typically the gutter width of 2 feet)																																																																	
Clogging Factor for a Single Curb Opening (typical value 0.10)																																																																	
Curb Opening Weir Coefficient (typical value 2.3-3.7)																																																																	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)																																																																	
Low Head Performance Reduction (Calculated)																																																																	
Depth for Grate Midwidth																																																																	
Depth for Curb Opening Weir Equation																																																																	
Grated Inlet Performance Reduction Factor for Long Inlets																																																																	
Curb Opening Performance Reduction Factor for Long Inlets																																																																	
Combination Inlet Performance Reduction Factor for Long Inlets																																																																	
Total Inlet Interception Capacity (assumes clogged condition)																																																																	
Inlet Capacity IS GOOD for Minor and Major Storms (>Q Peak)																																																																	
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ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

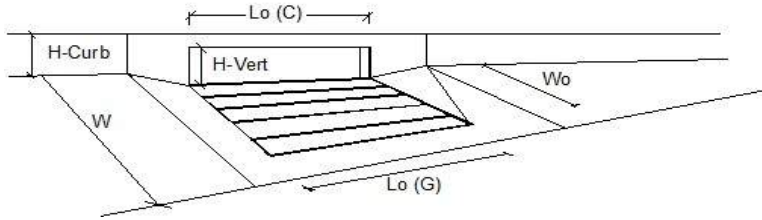
Project: Schmidt Parcel - District Infrastructure
Inlet ID: DP6



Gutter Geometry:						
Maximum Allowable Width for Spread Behind Curb	$T_{BACK} = 9.5$ ft					
Side Slope Behind Curb (leave blank for no conveyance credit behind curb)	$S_{BACK} = 0.020$ ft/ft					
Manning's Roughness Behind Curb (typically between 0.012 and 0.020)	$n_{BACK} = 0.020$					
Height of Curb at Gutter Flow Line	$H_{CURB} = 6.00$ inches					
Distance from Curb Face to Street Crown	$T_{CROWN} = 20.0$ ft					
Gutter Width	$W = 2.00$ ft					
Street Transverse Slope	$S_X = 0.020$ ft/ft					
Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)	$S_W = 0.063$ ft/ft					
Street Longitudinal Slope - Enter 0 for sump condition	$S_O = 0.024$ ft/ft					
Manning's Roughness for Street Section (typically between 0.012 and 0.020)	$n_{STREET} = 0.013$					
Max. Allowable Spread for Minor & Major Storm	<table border="1" style="display: inline-table; border-collapse: collapse;"> <tr> <td style="text-align: center;">Minor Storm</td> <td style="text-align: center;">Major Storm</td> <td rowspan="2" style="text-align: right; padding-left: 10px;">ft</td> </tr> <tr> <td style="text-align: center;">$T_{MAX} = 20.0$</td> <td style="text-align: center;">20.0</td> </tr> </table>	Minor Storm	Major Storm	ft	$T_{MAX} = 20.0$	20.0
Minor Storm	Major Storm	ft				
$T_{MAX} = 20.0$	20.0					
Max. Allowable Depth at Gutter Flowline for Minor & Major Storm	<table border="1" style="display: inline-table; border-collapse: collapse;"> <tr> <td style="text-align: center;">Minor Storm</td> <td style="text-align: center;">Major Storm</td> <td rowspan="2" style="text-align: right; padding-left: 10px;">inches</td> </tr> <tr> <td style="text-align: center;">$d_{MAX} = 6.0$</td> <td style="text-align: center;">8.3</td> </tr> </table>	Minor Storm	Major Storm	inches	$d_{MAX} = 6.0$	8.3
Minor Storm	Major Storm	inches				
$d_{MAX} = 6.0$	8.3					
Allow Flow Depth at Street Crown (check box for yes, leave blank for no)	<table border="1" style="display: inline-table; border-collapse: collapse;"> <tr> <td style="text-align: center;">Minor Storm</td> <td style="text-align: center;">Major Storm</td> </tr> <tr> <td style="text-align: center;"><input type="checkbox"/></td> <td style="text-align: center;"><input type="checkbox"/></td> </tr> </table>	Minor Storm	Major Storm	<input type="checkbox"/>	<input type="checkbox"/>	
Minor Storm	Major Storm					
<input type="checkbox"/>	<input type="checkbox"/>					
MINOR STORM Allowable Capacity is based on Depth Criterion						
MAJOR STORM Allowable Capacity is based on Spread Criterion						
Minor storm max. allowable capacity GOOD - greater than the design peak flow of 1.80 cfs on sheet 'Inlet Management'						
Major storm max. allowable capacity GOOD - greater than the design peak flow of 5.40 cfs on sheet 'Inlet Management'						
$Q_{allow} =$	<table border="1" style="display: inline-table; border-collapse: collapse;"> <tr> <td style="text-align: center;">Minor Storm</td> <td style="text-align: center;">Major Storm</td> <td rowspan="2" style="text-align: right; padding-left: 10px;">cfs</td> </tr> <tr> <td style="text-align: center;">29.7</td> <td style="text-align: center;">30.4</td> </tr> </table>	Minor Storm	Major Storm	cfs	29.7	30.4
Minor Storm	Major Storm	cfs				
29.7	30.4					

INLET ON A CONTINUOUS GRADE

MHFD-Inlet, Version 5.03 (August 2023)

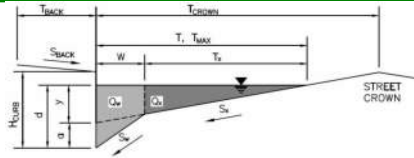


Design Information (Input)	MINOR	MAJOR	
Type of Inlet	CDOT Type R Curb Opening		
Local Depression (additional to continuous gutter depression 'a')	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	3	3	
Length of a Single Unit Inlet (Grate or Curb Opening)	5.00	5.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity			
Total Inlet Interception Capacity	Q = 1.8	Q = 5.4	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q_b = 0.0	Q_b = 0.0	cfs
Capture Percentage = Q _i /Q _s	C% = 100	C% = 100	%

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

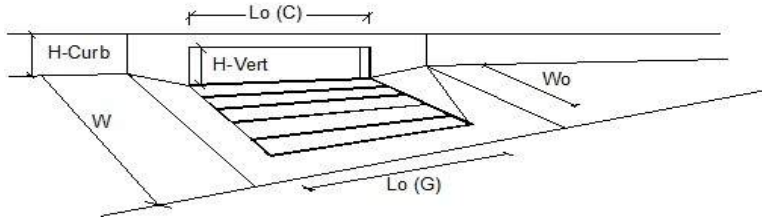
Project: Schmidt Parcel - District Infrastructure
Inlet ID: DP7



Gutter Geometry:					
Maximum Allowable Width for Spread Behind Curb	$T_{BACK} = 9.5$ ft				
Side Slope Behind Curb (leave blank for no conveyance credit behind curb)	$S_{BACK} = 0.020$ ft/ft				
Manning's Roughness Behind Curb (typically between 0.012 and 0.020)	$n_{BACK} = 0.020$				
Height of Curb at Gutter Flow Line	$H_{CURB} = 6.00$ inches				
Distance from Curb Face to Street Crown	$T_{CROWN} = 20.0$ ft				
Gutter Width	$W = 2.00$ ft				
Street Transverse Slope	$S_X = 0.020$ ft/ft				
Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)	$S_W = 0.063$ ft/ft				
Street Longitudinal Slope - Enter 0 for sump condition	$S_O = 0.024$ ft/ft				
Manning's Roughness for Street Section (typically between 0.012 and 0.020)	$n_{STREET} = 0.013$				
Max. Allowable Spread for Minor & Major Storm	<table border="1" style="display: inline-table; margin-right: 10px;"> <tr> <td>Minor Storm</td> <td>Major Storm</td> </tr> <tr> <td>20.0</td> <td>20.0</td> </tr> </table> ft	Minor Storm	Major Storm	20.0	20.0
Minor Storm	Major Storm				
20.0	20.0				
Max. Allowable Depth at Gutter Flowline for Minor & Major Storm	<table border="1" style="display: inline-table; margin-right: 10px;"> <tr> <td>Minor Storm</td> <td>Major Storm</td> </tr> <tr> <td>6.0</td> <td>8.3</td> </tr> </table> inches	Minor Storm	Major Storm	6.0	8.3
Minor Storm	Major Storm				
6.0	8.3				
Allow Flow Depth at Street Crown (check box for yes, leave blank for no)	<table border="1" style="display: inline-table; margin-right: 10px;"> <tr> <td><input type="checkbox"/></td> <td><input type="checkbox"/></td> </tr> </table>	<input type="checkbox"/>	<input type="checkbox"/>		
<input type="checkbox"/>	<input type="checkbox"/>				
MINOR STORM Allowable Capacity is based on Depth Criterion					
MAJOR STORM Allowable Capacity is based on Spread Criterion					
Minor storm max. allowable capacity GOOD - greater than the design peak flow of 2.00 cfs on sheet 'Inlet Management'					
Major storm max. allowable capacity GOOD - greater than the design peak flow of 3.80 cfs on sheet 'Inlet Management'					
$Q_{allow} =$	<table border="1" style="display: inline-table;"> <tr> <td>Minor Storm</td> <td>Major Storm</td> </tr> <tr> <td>29.7</td> <td>30.4</td> </tr> </table> cfs	Minor Storm	Major Storm	29.7	30.4
Minor Storm	Major Storm				
29.7	30.4				

INLET ON A CONTINUOUS GRADE

MHFD-Inlet, Version 5.03 (August 2023)

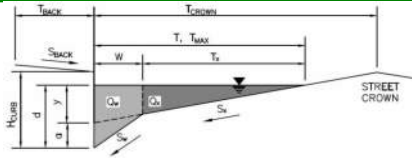


Design Information (Input)	MINOR	MAJOR	
Type of Inlet	CDOT Type R Curb Opening		
Local Depression (additional to continuous gutter depression 'a')	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	3	3	
Length of a Single Unit Inlet (Grate or Curb Opening)	5.00	5.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity			
Total Inlet Interception Capacity	Q = 2.0	3.8	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q_b = 0.0	0.0	cfs
Capture Percentage = Q _i /Q _s	C% = 100	100	%

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

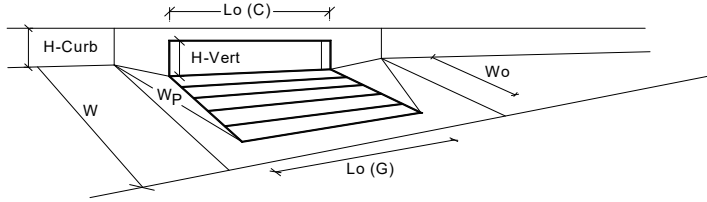
Project: Schmidt Parcel - District Infrastructure
Inlet ID: DP9



Gutter Geometry:										
Maximum Allowable Width for Spread Behind Curb	$T_{BACK} = 17.0$ ft									
Side Slope Behind Curb (leave blank for no conveyance credit behind curb)	$S_{BACK} = 0.020$ ft/ft									
Manning's Roughness Behind Curb (typically between 0.012 and 0.020)	$n_{BACK} = 0.012$									
Height of Curb at Gutter Flow Line	$H_{CURB} = 8.00$ inches									
Distance from Curb Face to Street Crown	$T_{CROWN} = 36.0$ ft									
Gutter Width	$W = 2.00$ ft									
Street Transverse Slope	$S_X = 0.020$ ft/ft									
Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)	$S_W = 0.063$ ft/ft									
Street Longitudinal Slope - Enter 0 for sump condition	$S_O = 0.000$ ft/ft									
Manning's Roughness for Street Section (typically between 0.012 and 0.020)	$n_{STREET} = 0.013$									
Max. Allowable Spread for Minor & Major Storm	<table style="width: 100%; border: none;"> <tr> <td style="text-align: center;">Minor Storm</td> <td style="text-align: center;">Major Storm</td> <td></td> </tr> <tr> <td style="text-align: center;">$T_{MAX} = 36.0$</td> <td style="text-align: center;">36.0</td> <td style="text-align: right;">ft</td> </tr> </table>	Minor Storm	Major Storm		$T_{MAX} = 36.0$	36.0	ft			
Minor Storm	Major Storm									
$T_{MAX} = 36.0$	36.0	ft								
Max. Allowable Depth at Gutter Flowline for Minor & Major Storm	<table style="width: 100%; border: none;"> <tr> <td style="text-align: center;">Minor Storm</td> <td style="text-align: center;">Major Storm</td> <td></td> </tr> <tr> <td style="text-align: center;">$d_{MAX} = 6.0$</td> <td style="text-align: center;">10.1</td> <td style="text-align: right;">inches</td> </tr> <tr> <td style="text-align: center;"><input type="checkbox"/></td> <td style="text-align: center;"><input type="checkbox"/></td> <td></td> </tr> </table>	Minor Storm	Major Storm		$d_{MAX} = 6.0$	10.1	inches	<input type="checkbox"/>	<input type="checkbox"/>	
Minor Storm	Major Storm									
$d_{MAX} = 6.0$	10.1	inches								
<input type="checkbox"/>	<input type="checkbox"/>									
Check boxes are not applicable in SUMP conditions										
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INLET IN A SUMP OR SAG LOCATION

MHFD-Inlet, Version 5.03 (August 2023)

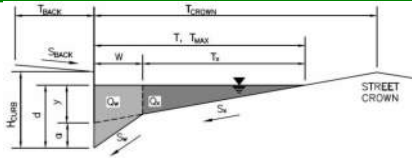


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ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

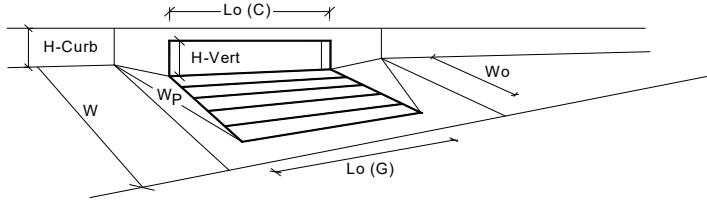
Project: Schmidt Parcel - District Infrastructure
Inlet ID: DP10



Gutter Geometry:										
Maximum Allowable Width for Spread Behind Curb	$T_{BACK} = 17.0$ ft									
Side Slope Behind Curb (leave blank for no conveyance credit behind curb)	$S_{BACK} = 0.020$ ft/ft									
Manning's Roughness Behind Curb (typically between 0.012 and 0.020)	$n_{BACK} = 0.020$									
Height of Curb at Gutter Flow Line	$H_{CURB} = 8.00$ inches									
Distance from Curb Face to Street Crown	$T_{CROWN} = 36.0$ ft									
Gutter Width	$W = 2.00$ ft									
Street Transverse Slope	$S_X = 0.020$ ft/ft									
Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)	$S_W = 0.063$ ft/ft									
Street Longitudinal Slope - Enter 0 for sump condition	$S_0 = 0.000$ ft/ft									
Manning's Roughness for Street Section (typically between 0.012 and 0.020)	$n_{STREET} = 0.013$									
Max. Allowable Spread for Minor & Major Storm	<table style="width: 100%; border: none;"> <tr> <td style="text-align: center;">Minor Storm</td> <td style="text-align: center;">Major Storm</td> <td style="border: none;"></td> </tr> <tr> <td style="border: 1px solid black; text-align: center;">36.0</td> <td style="border: 1px solid black; text-align: center;">36.0</td> <td style="border: none;">ft</td> </tr> </table>	Minor Storm	Major Storm		36.0	36.0	ft			
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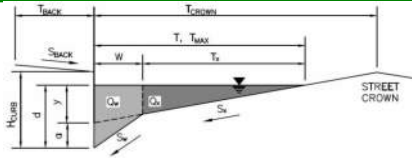


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Grate Weir Coefficient (typical value 2.15 - 3.60)	N/A	N/A																																																																																																																									
Grate Orifice Coefficient (typical value 0.60 - 0.80)	N/A	N/A																																																																																																																									
Curb Opening Information																																																																																																																											
Length of a Unit Curb Opening	5.00	5.00	feet																																																																																																																								
Height of Vertical Curb Opening in Inches	6.00	6.00	inches																																																																																																																								
Height of Curb Orifice Throat in Inches	6.00	6.00	inches																																																																																																																								
Angle of Throat	63.40	63.40	degrees																																																																																																																								
Side Width for Depression Pan (typically the gutter width of 2 feet)	2.00	2.00	feet																																																																																																																								
Clogging Factor for a Single Curb Opening (typical value 0.10)	0.10	0.10																																																																																																																									
Curb Opening Weir Coefficient (typical value 2.3-3.7)	3.60	3.60																																																																																																																									
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	0.67	0.67																																																																																																																									
Low Head Performance Reduction (Calculated)																																																																																																																											
Depth for Grate Midwidth	N/A	N/A	ft																																																																																																																								
Depth for Curb Opening Weir Equation	0.38	0.68	ft																																																																																																																								
Grated Inlet Performance Reduction Factor for Long Inlets	N/A	N/A																																																																																																																									
Curb Opening Performance Reduction Factor for Long Inlets	1.00	1.00																																																																																																																									
Combination Inlet Performance Reduction Factor for Long Inlets	N/A	N/A																																																																																																																									
Total Inlet Interception Capacity (assumes clogged condition)																																																																																																																											
Inlet Capacity IS GOOD for Minor and Major Storms (>Q Peak)	6.3	9.9	cfs																																																																																																																								
Q _{PEAK REQUIRED}	3.5	6.5	cfs																																																																																																																								

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

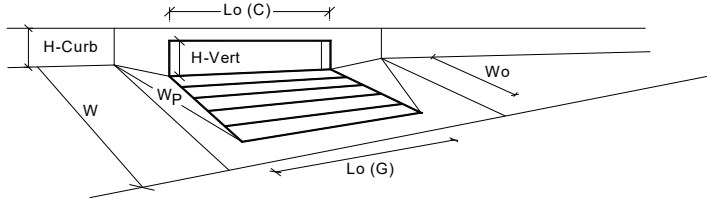
Project: Schmidt Parcel - District Infrastructure
Inlet ID: DP3



Gutter Geometry:						
Maximum Allowable Width for Spread Behind Curb	$T_{BACK} = 17.0$ ft					
Side Slope Behind Curb (leave blank for no conveyance credit behind curb)	$S_{BACK} = 0.020$ ft/ft					
Manning's Roughness Behind Curb (typically between 0.012 and 0.020)	$n_{BACK} = 0.020$					
Height of Curb at Gutter Flow Line	$H_{CURB} = 8.00$ inches					
Distance from Curb Face to Street Crown	$T_{CROWN} = 36.0$ ft					
Gutter Width	$W = 2.00$ ft					
Street Transverse Slope	$S_X = 0.020$ ft/ft					
Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)	$S_W = 0.083$ ft/ft					
Street Longitudinal Slope - Enter 0 for sump condition	$S_O = 0.000$ ft/ft					
Manning's Roughness for Street Section (typically between 0.012 and 0.020)	$n_{STREET} = 0.013$					
Max. Allowable Spread for Minor & Major Storm	<table border="1" style="display: inline-table; border-collapse: collapse;"> <tr> <td style="text-align: center;">Minor Storm</td> <td style="text-align: center;">Major Storm</td> <td rowspan="2" style="text-align: right;">ft</td> </tr> <tr> <td style="text-align: center;">$T_{MAX} = 36.0$</td> <td style="text-align: center;">36.0</td> </tr> </table>	Minor Storm	Major Storm	ft	$T_{MAX} = 36.0$	36.0
Minor Storm	Major Storm	ft				
$T_{MAX} = 36.0$	36.0					
Max. Allowable Depth at Gutter Flowline for Minor & Major Storm	<table border="1" style="display: inline-table; border-collapse: collapse;"> <tr> <td style="text-align: center;">Minor Storm</td> <td style="text-align: center;">Major Storm</td> <td rowspan="2" style="text-align: right;">inches</td> </tr> <tr> <td style="text-align: center;">$d_{MAX} = 8.0$</td> <td style="text-align: center;">8.0</td> </tr> </table>	Minor Storm	Major Storm	inches	$d_{MAX} = 8.0$	8.0
Minor Storm	Major Storm	inches				
$d_{MAX} = 8.0$	8.0					
Check boxes are not applicable in SUMP conditions	<input type="checkbox"/> <input type="checkbox"/>					
MINOR STORM Allowable Capacity is not applicable to Sump Condition						
MAJOR STORM Allowable Capacity is not applicable to Sump Condition						
	<table border="1" style="display: inline-table; border-collapse: collapse;"> <tr> <td style="text-align: center;">Minor Storm</td> <td style="text-align: center;">Major Storm</td> <td rowspan="2" style="text-align: right;">cfs</td> </tr> <tr> <td style="text-align: center;">$Q_{allow} = \text{SUMP}$</td> <td style="text-align: center;">SUMP</td> </tr> </table>	Minor Storm	Major Storm	cfs	$Q_{allow} = \text{SUMP}$	SUMP
Minor Storm	Major Storm	cfs				
$Q_{allow} = \text{SUMP}$	SUMP					

INLET IN A SUMP OR SAG LOCATION

MHFD-Inlet, Version 5.03 (August 2023)



Design Information (Input)		<table border="1" style="margin-left: auto; margin-right: auto;"> <tr> <th style="width: 50%;">MINOR</th> <th style="width: 50%;">MAJOR</th> </tr> <tr> <td colspan="2" style="text-align: center;">CDOT Type R Curb Opening</td> </tr> <tr> <td>Type =</td> <td>CDOT Type R Curb Opening</td> </tr> <tr> <td>a_{local} =</td> <td>1.00</td> </tr> <tr> <td>No =</td> <td>1</td> </tr> <tr> <td>Ponding Depth =</td> <td>8.0</td> </tr> <tr> <td colspan="2" style="text-align: center;">Override Depths</td> </tr> <tr> <td>L_o (G) =</td> <td>N/A</td> </tr> <tr> <td>W_o =</td> <td>N/A</td> </tr> <tr> <td>A_{ratio} =</td> <td>N/A</td> </tr> <tr> <td>C_f (G) =</td> <td>N/A</td> </tr> <tr> <td>C_w (G) =</td> <td>N/A</td> </tr> <tr> <td>C_o (G) =</td> <td>N/A</td> </tr> <tr> <td colspan="2" style="text-align: center;">MINOR</td> </tr> <tr> <td>L_o (C) =</td> <td>5.00</td> </tr> <tr> <td>H_{vert} =</td> <td>6.00</td> </tr> <tr> <td>H_{throat} =</td> <td>6.00</td> </tr> <tr> <td>Theta =</td> <td>63.40</td> </tr> <tr> <td>W_p =</td> <td>2.00</td> </tr> <tr> <td>C_f (C) =</td> <td>0.10</td> </tr> <tr> <td>C_w (C) =</td> <td>3.60</td> </tr> <tr> <td>C_o (C) =</td> <td>0.67</td> </tr> <tr> <td colspan="2" style="text-align: center;">MAJOR</td> </tr> <tr> <td>L_o (C) =</td> <td>5.00</td> </tr> <tr> <td>H_{vert} =</td> <td>6.00</td> </tr> <tr> <td>H_{throat} =</td> <td>6.00</td> </tr> <tr> <td>Theta =</td> <td>63.40</td> </tr> <tr> <td>W_p =</td> <td>2.00</td> </tr> <tr> <td>C_f (C) =</td> <td>0.10</td> </tr> <tr> <td>C_w (C) =</td> <td>3.60</td> </tr> <tr> <td>C_o (C) =</td> <td>0.67</td> </tr> </table>		MINOR	MAJOR	CDOT Type R Curb Opening		Type =	CDOT Type R Curb Opening	a _{local} =	1.00	No =	1	Ponding Depth =	8.0	Override Depths		L _o (G) =	N/A	W _o =	N/A	A _{ratio} =	N/A	C _f (G) =	N/A	C _w (G) =	N/A	C _o (G) =	N/A	MINOR		L _o (C) =	5.00	H _{vert} =	6.00	H _{throat} =	6.00	Theta =	63.40	W _p =	2.00	C _f (C) =	0.10	C _w (C) =	3.60	C _o (C) =	0.67	MAJOR		L _o (C) =	5.00	H _{vert} =	6.00	H _{throat} =	6.00	Theta =	63.40	W _p =	2.00	C _f (C) =	0.10	C _w (C) =	3.60	C _o (C) =	0.67
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Type of Inlet	CDOT Type R Curb Opening																																																																
Local Depression (additional to continuous gutter depression 'a' from above)																																																																	
Number of Unit Inlets (Grate or Curb Opening)																																																																	
Water Depth at Flowline (outside of local depression)																																																																	
Grate Information																																																																	
Length of a Unit Grate																																																																	
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Line No.	DnStm Ln No	Flow Rate (cfs)	Capac Full (cfs)	n-val Pipe	Invert Dn (ft)	Invert Up (ft)	Vel Ave (ft/s)	HGL Dn (ft)	HGL Up (ft)	EGL Dn (ft)	EGL Up (ft)	Line Size (in)	Line Length (ft)
1	Outfall	3.20	26.25	0.013	7021.44	7021.78	3.84	7022.06	7022.40	7022.29	7022.634296875	24	25.225
2	1	3.20	22.64	0.013	7022.08	7022.80	4.45	7022.59	7023.42	7022.82	7023.65431640625	24	71.848
3	2	1.60	9.59	0.013	7023.30	7024.01	3.67	7023.72	7024.48	7023.89	7024.654375	18	85.167
4	Outfall	10.40	100.34	0.013	6993.46	6993.92	4.73	6994.44	6994.90 j	6994.79	6995.2455078125	42	46.243
5	4	7.90	82.03	0.013	6994.02	6994.33	4.30	6994.90	6995.18 j	6995.20	6995.4767578125	42	46.639
6	5	5.30	82.01	0.013	6994.63	6995.46	4.37	6995.23	6996.15	6995.48	6996.390390625	42	124.922
7	6	5.30	82.23	0.013	6995.76	6998.19	4.38	6996.36	6998.88	6996.60	6999.12037109375	42	363.779
8	7	5.30	82.15	0.013	6998.29	7001.35	4.37	6998.89	7002.04	6999.14	7002.28052734375	42	459.002
9	8	5.30	81.94	0.013	7001.65	7002.50	4.37	7002.25	7003.19	7002.50	7003.4304296875	42	128.163
10	9	5.30	66.92	0.013	7003.00	7004.89	4.85	7003.57	7005.61	7003.83	7005.87083984375	36	187.764
11	10	5.30	29.90	0.012	7005.89	7013.28	5.80	7006.46	7014.09	7006.77	7014.40130859375	24	496.348
12	11	5.30	19.70	0.012	7013.58	7014.40	4.87	7014.29	7015.21	7014.59	7015.52142578125	24	126.786
13	12	3.40	19.69	0.012	7014.70	7015.29	4.29	7015.26	7015.93	7015.50	7016.17408203125	24	91.347
14	4	3.40	22.71	0.013	6995.42	6995.88	4.54	6995.94	6996.52	6996.18	6996.76392578125	24	45.605
15	14	1.80	10.46	0.013	6996.38	6996.79	3.94	6996.80	6997.29	6996.99	6997.47443359375	18	41.333
16	5	3.70	131.65	0.012	6994.83	6998.15	5.91	6995.18	6998.75	6995.39	6998.95951171875	36	100.000
17	Outfall	0.10	43.18	0.013	6968.40	6970.40	1.50	6968.50	6970.50	6968.53	6970.53146484375	30	180.403

Project File: DVDP_P1_interim.stm

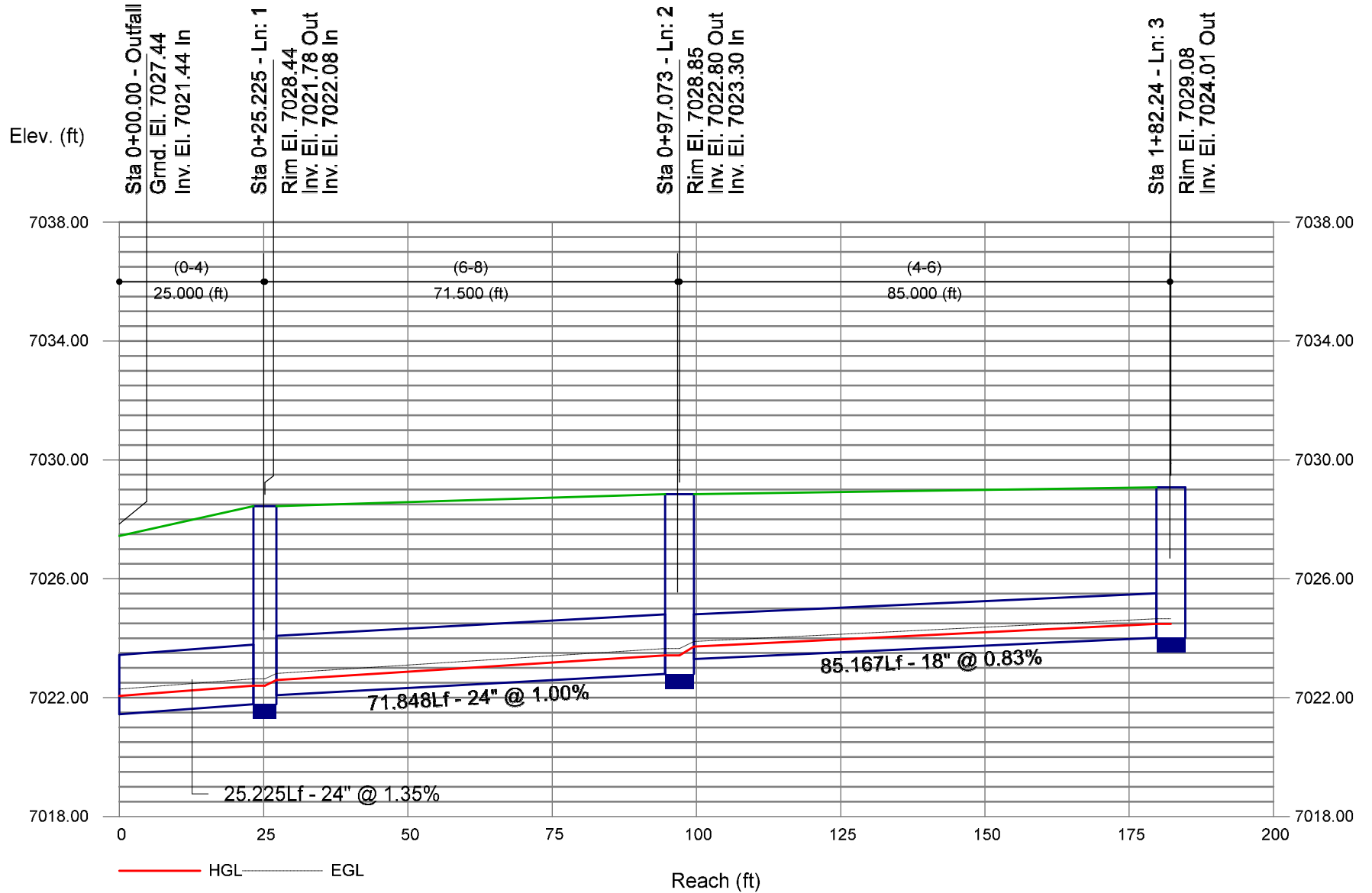
Number of lines: 17

Date: 4/29/2026

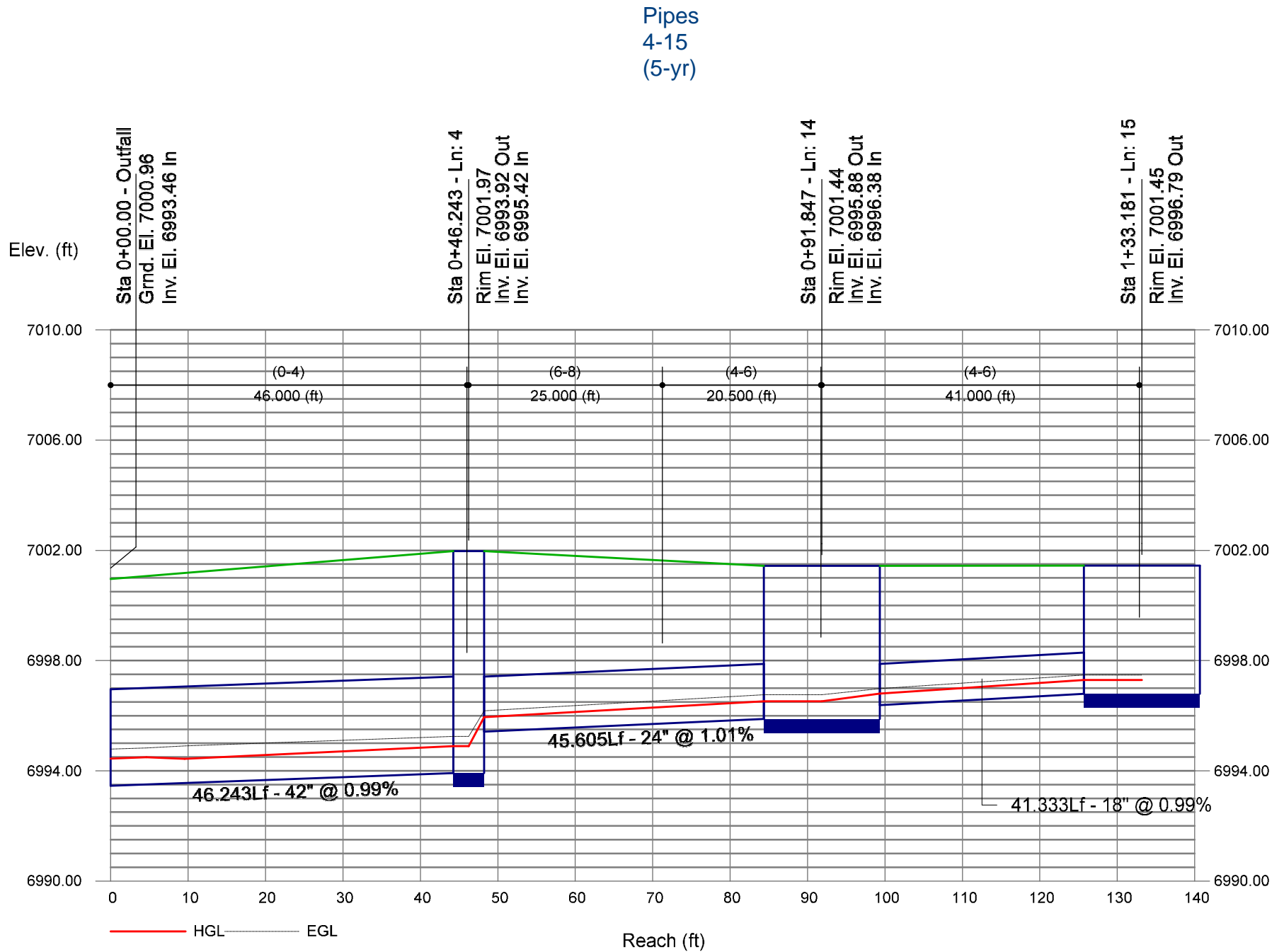
NOTES: ** Critical depth

Storm Sewer Profile

Pipes 1-3
(5-yr)

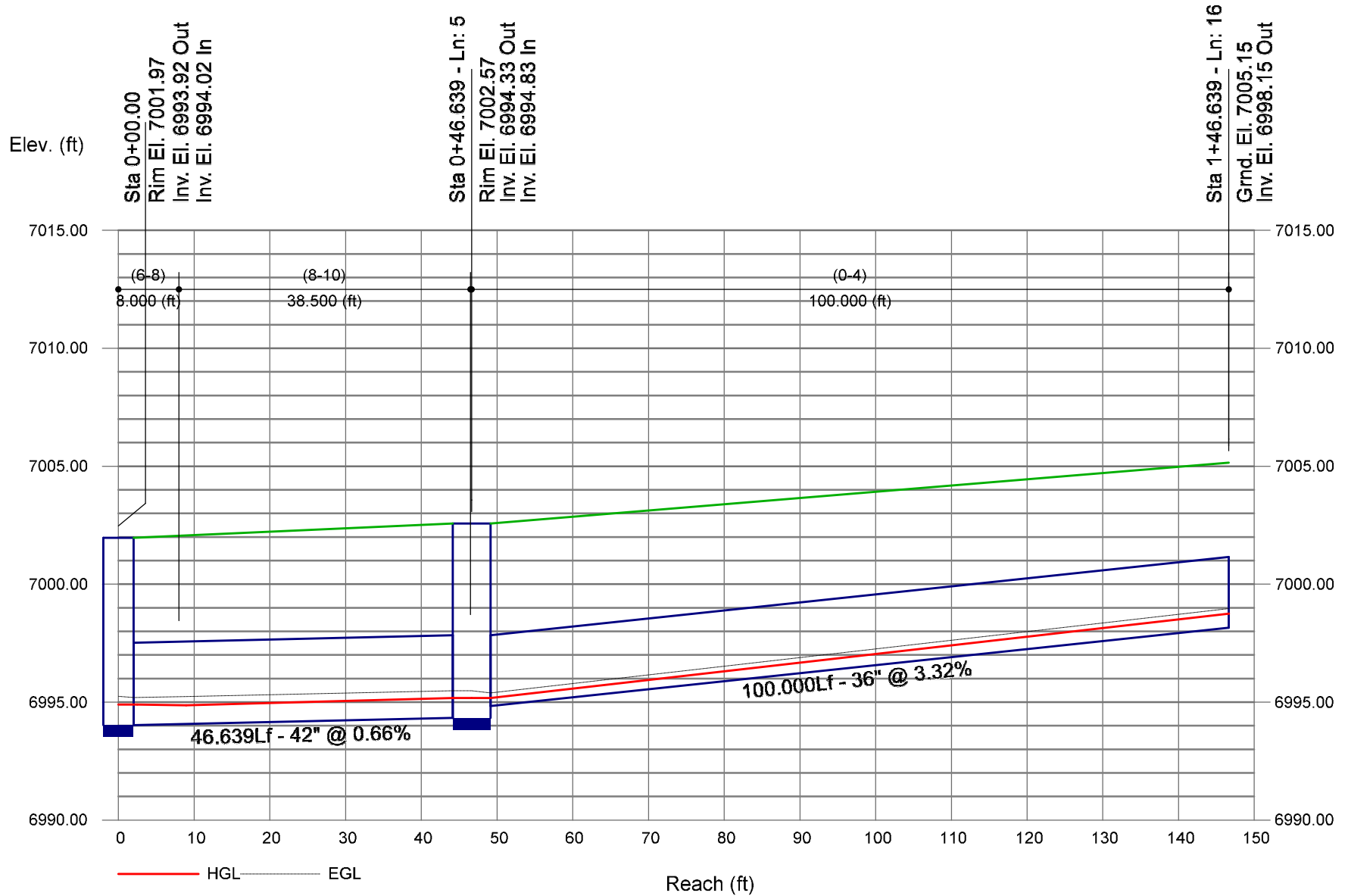


Storm Sewer Profile

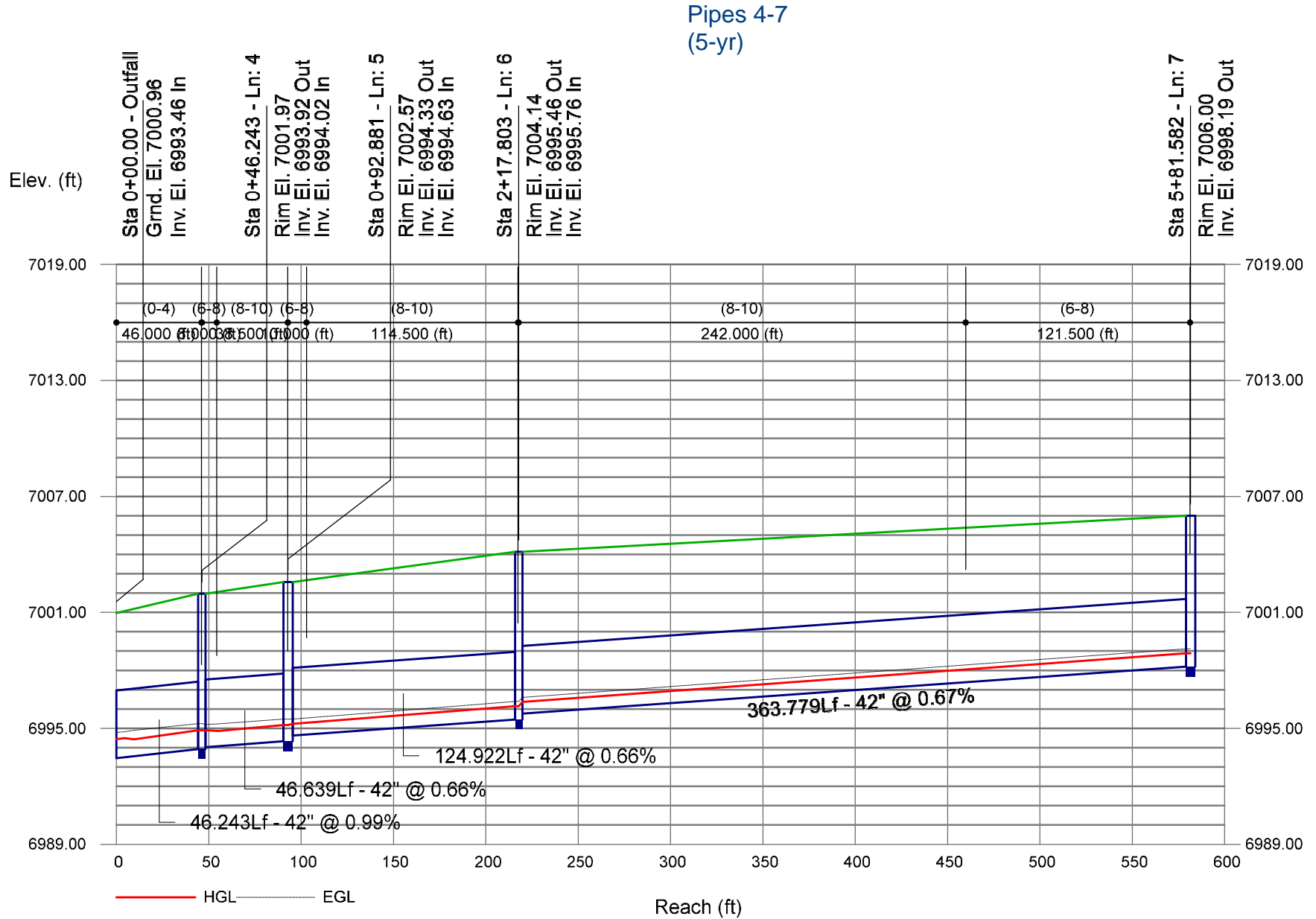


Storm Sewer Profile

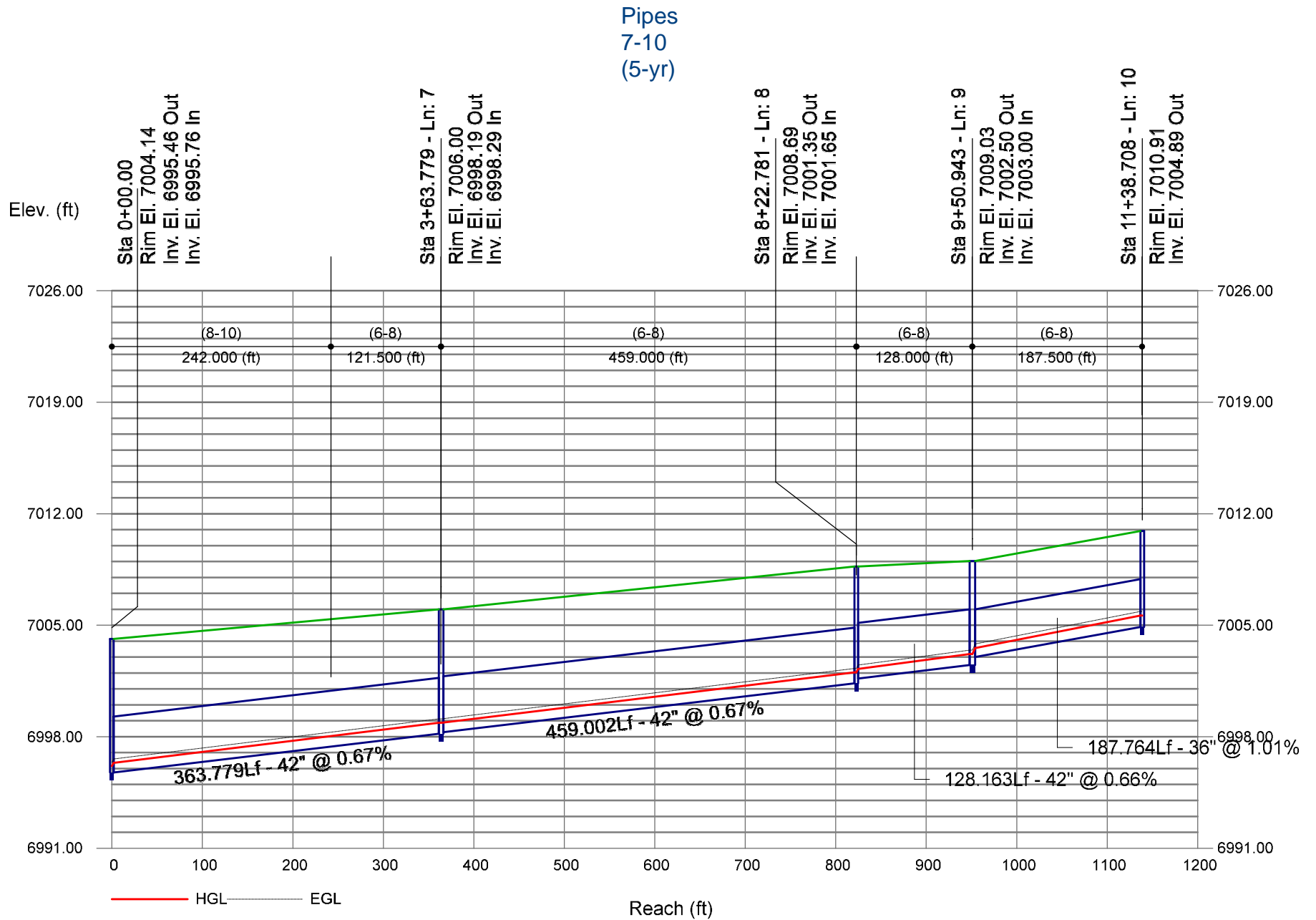
Pipes
5-16
(5-yr)



Storm Sewer Profile

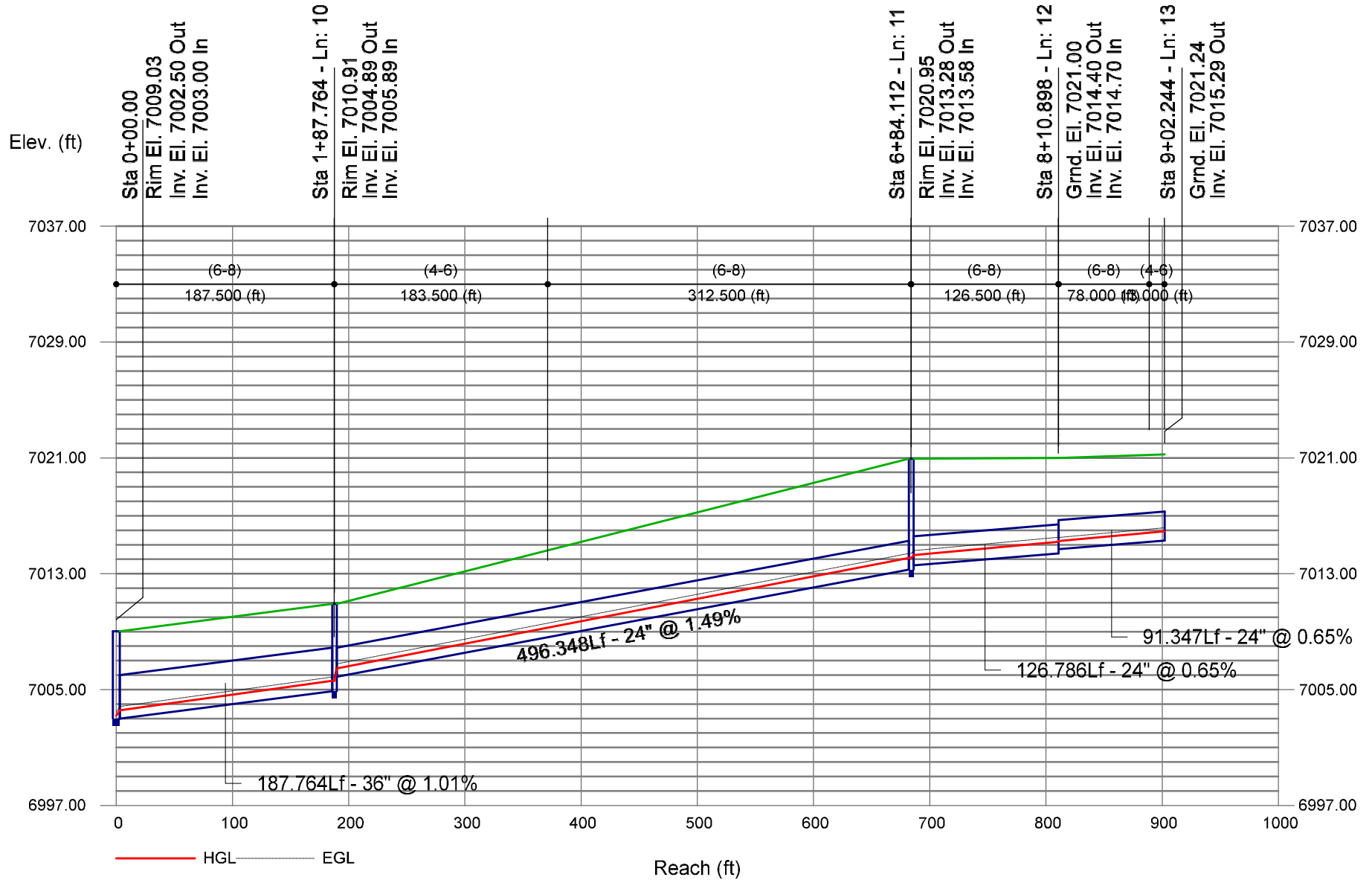


Storm Sewer Profile



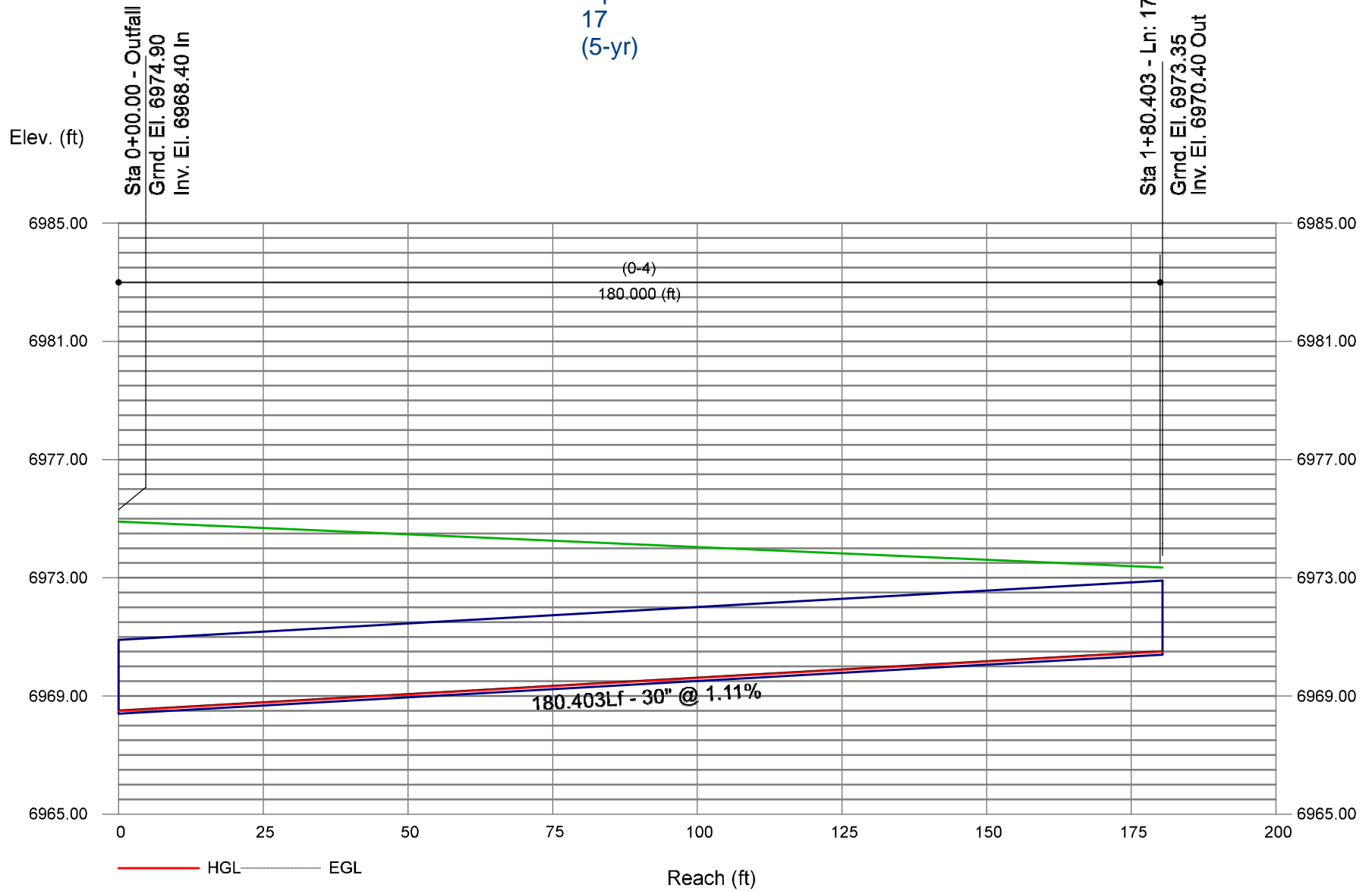
Storm Sewer Profile

Pipes
10-13
(5-yr)



Storm Sewer Profile

Pipes
17
(5-yr)



Line No.	DnStm Ln No	Flow Rate (cfs)	Capac Full (cfs)	n-val Pipe	Invert Dn (ft)	Invert Up (ft)	Vel Ave (ft/s)	HGL Dn (ft)	HGL Up (ft)	EGL Dn (ft)	EGL Up (ft)	Line Size (in)	Line Length (ft)
1	Outfall	7.90	26.25	0.013	7021.44	7021.78	4.08	7022.94	7022.78	7023.33	7023.16880859375	24	25.225
2	1	7.90	22.64	0.013	7022.08	7022.80	5.80	7022.90	7023.80	7023.29	7024.188828125	24	71.848
3	2	4.40	9.59	0.013	7023.30	7024.01	4.93	7024.01	7024.81	7024.34	7025.13396484375	18	85.167
4	Outfall	44.30	100.34	0.013	6993.46	6993.92	6.43	6996.25	6995.99	6997.12	6996.8631640625	42	46.243
5	4	38.00	82.03	0.013	6994.02	6994.33	6.93	6995.99	6996.24 j	6996.77	6997.01365234375	42	46.639
6	5	13.90	82.01	0.013	6994.63	6995.46	4.18	6996.24	6996.59 j	6996.66	6997.0027734375	42	124.922
7	6	13.90	82.23	0.013	6995.76	6998.19	5.76	6996.73	6999.32	6997.15	6999.73275390625	42	363.779
8	7	13.90	82.15	0.013	6998.29	7001.35	5.51	6999.32	7002.48	6999.74	7002.89291015625	42	459.002
9	8	13.90	81.94	0.013	7001.65	7002.50	5.75	7002.63	7003.63	7003.04	7004.0428125	42	128.163
10	9	13.90	66.92	0.013	7003.00	7004.89	6.40	7003.93	7006.08	7004.37	7006.516171875	36	187.764
11	10	13.90	29.90	0.012	7005.89	7013.28	7.77	7006.85	7014.62	7007.45	7015.22158203125	24	496.348
12	11	13.90	19.70	0.012	7013.58	7014.40	6.50	7014.82	7015.74	7015.42	7016.34169921875	24	126.786
13	12	5.20	19.69	0.012	7014.70	7015.29	3.77	7015.74	7016.09 j	7016.04	7016.39375	24	91.347
14	5	27.30	131.65	0.012	6994.83	6998.15	7.50	6996.24	6999.84	6996.94	7000.52740234375	36	100.000
15	Outfall	8.30	22.71	0.013	6995.42	6995.88	4.19	6996.93	6996.91 j	6997.34	6997.31576171875	24	45.605
16	15	5.40	10.46	0.013	6996.38	6996.79	5.44	6997.14	6997.69	6997.52	6998.0645703125	18	41.333
17	Outfall	46.40	43.18	0.013	6968.40	6970.40	9.83	6970.65	6972.75	6972.20	6974.21146484375	30	180.403

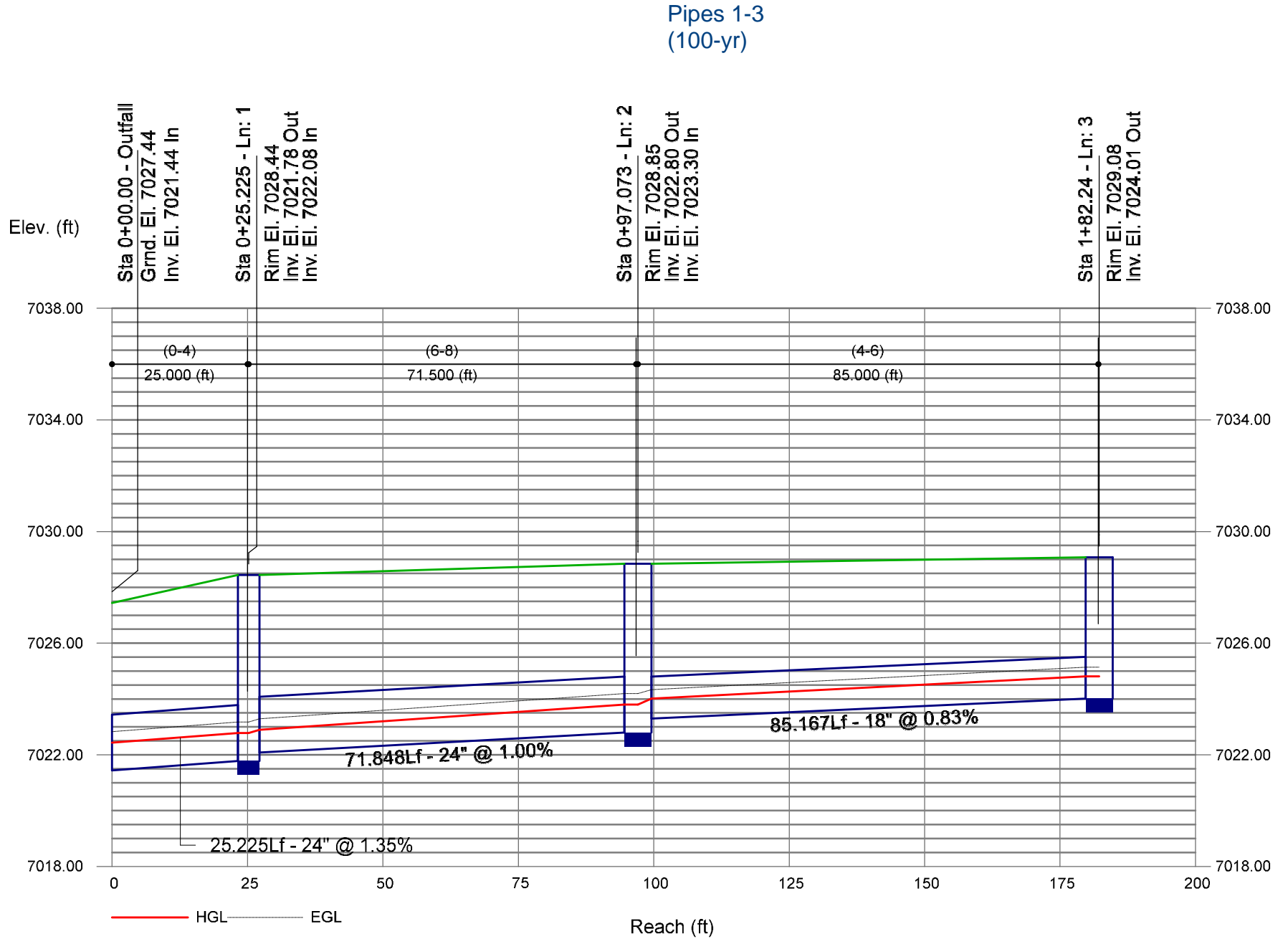
Project File: DVDP_P1_interim_100ur.stm

Number of lines: 17

Date: 4/29/2026

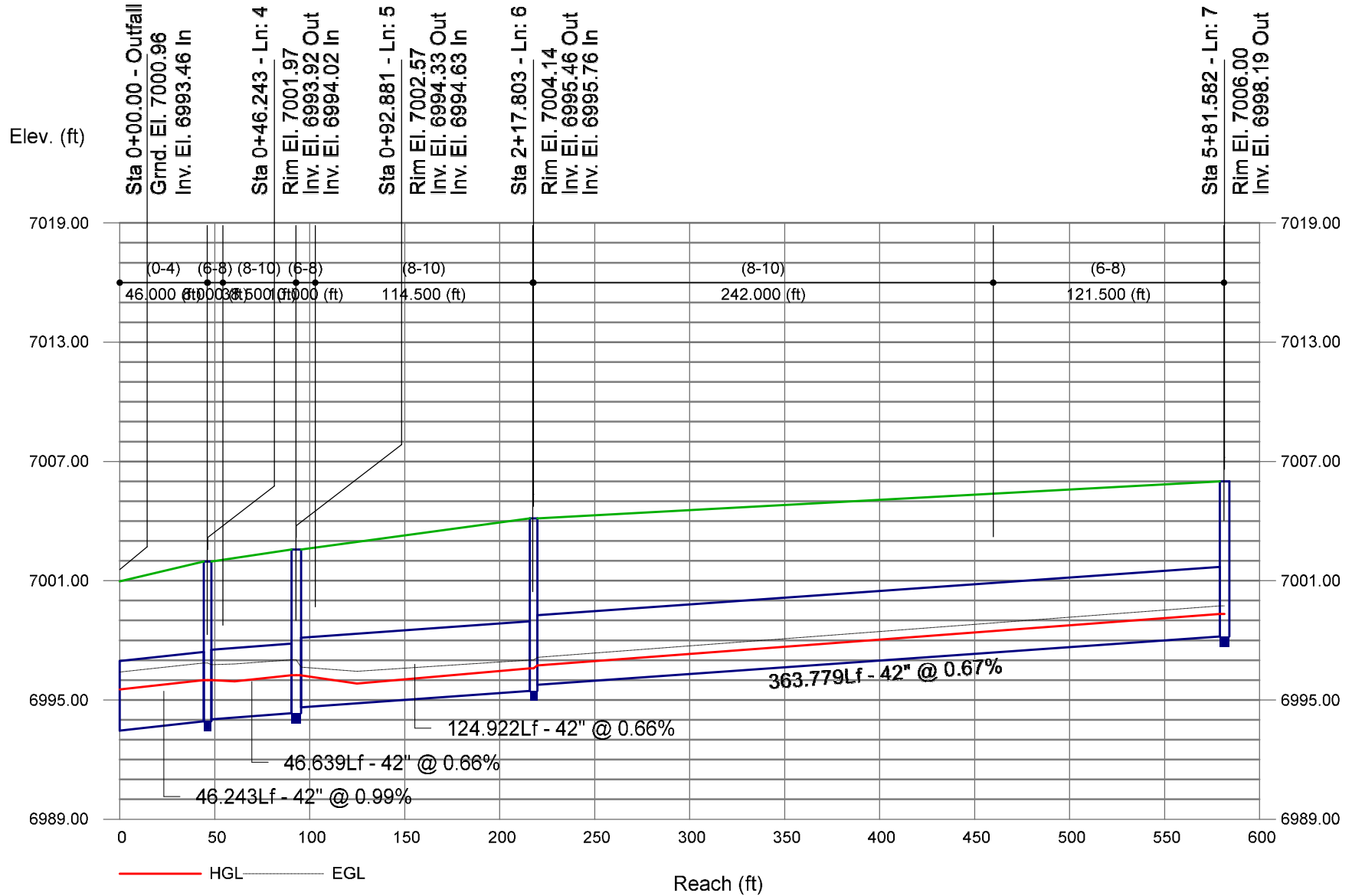
NOTES: ** Critical depth

Storm Sewer Profile

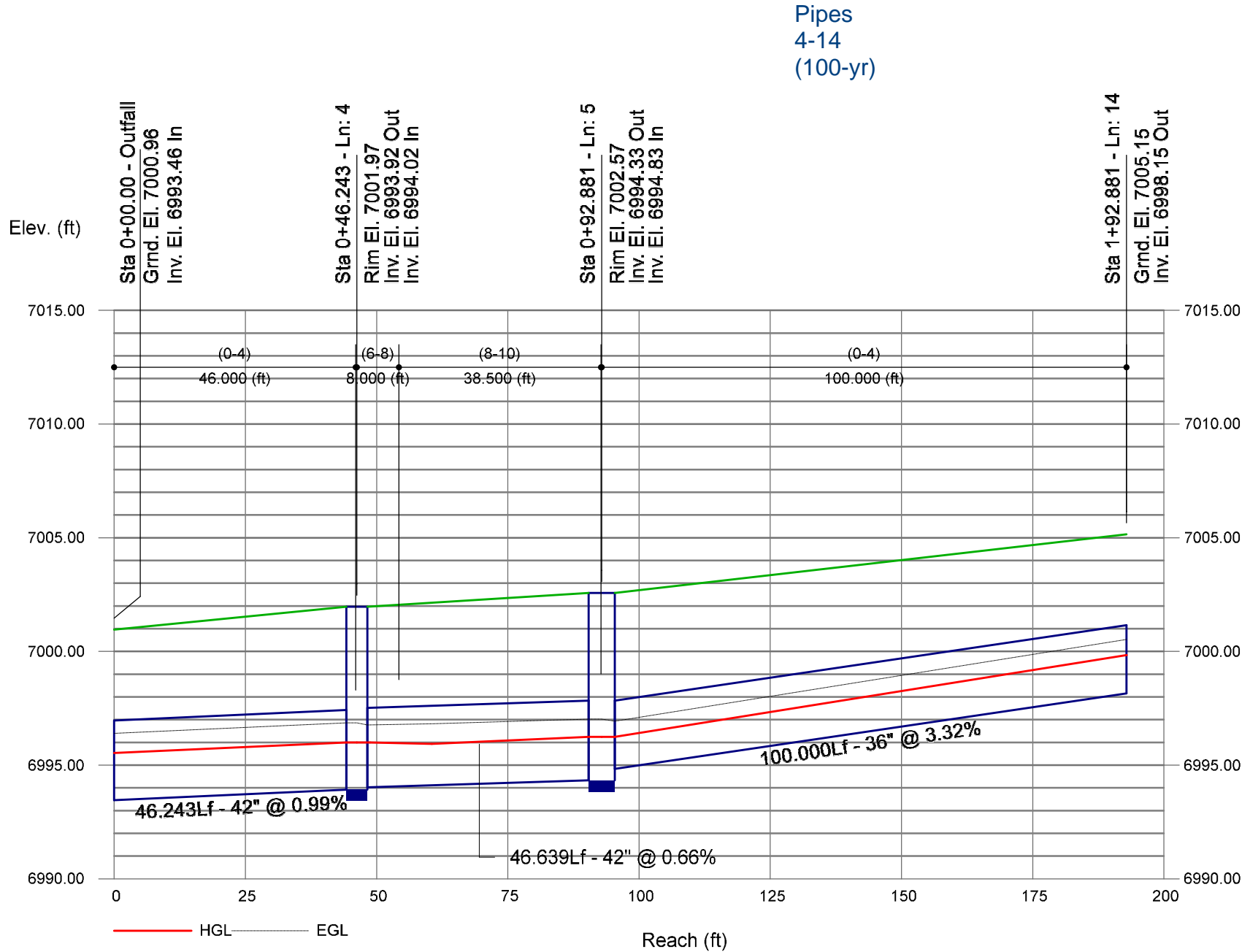


Storm Sewer Profile

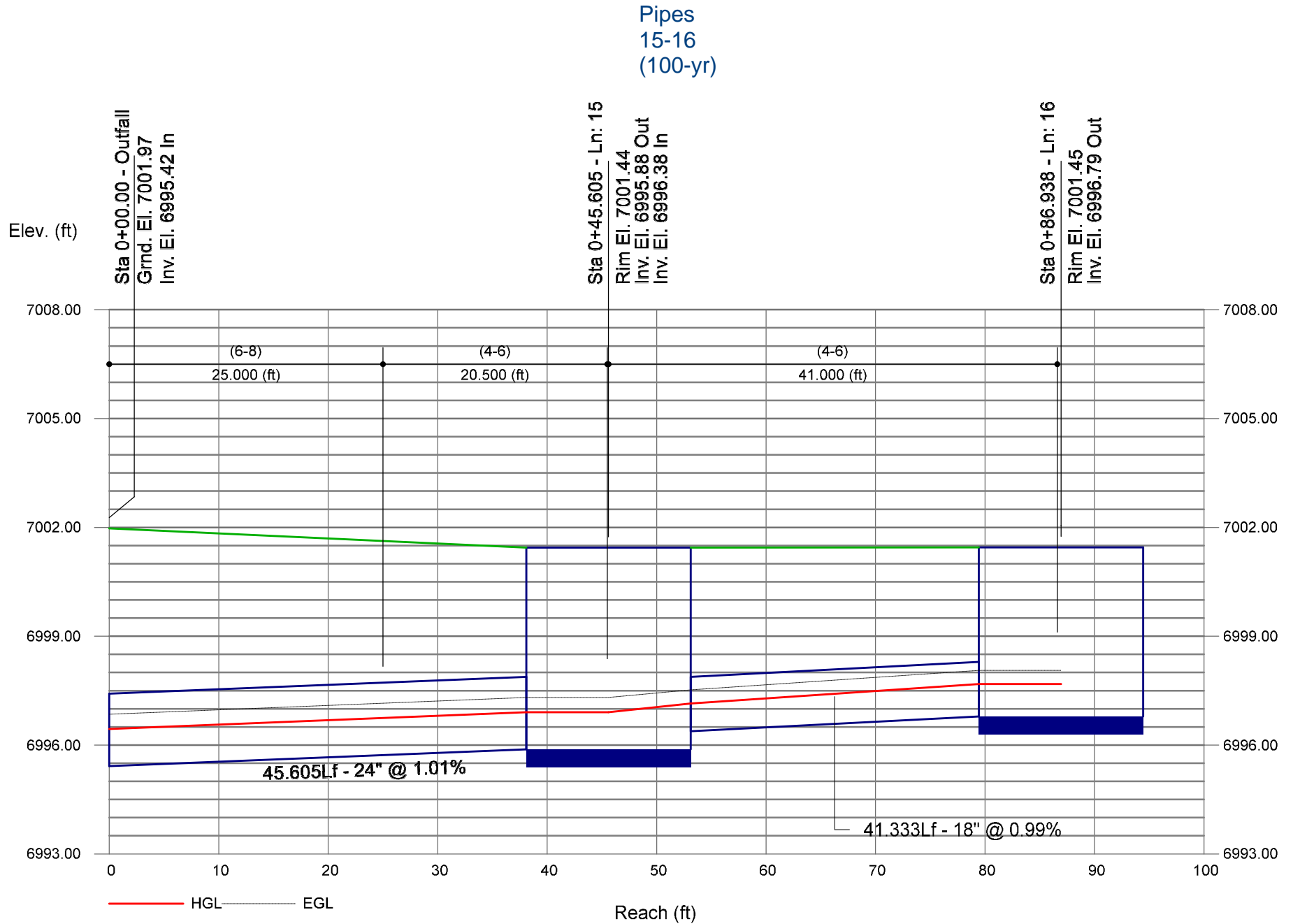
Pipes 4-7
(100-yr)



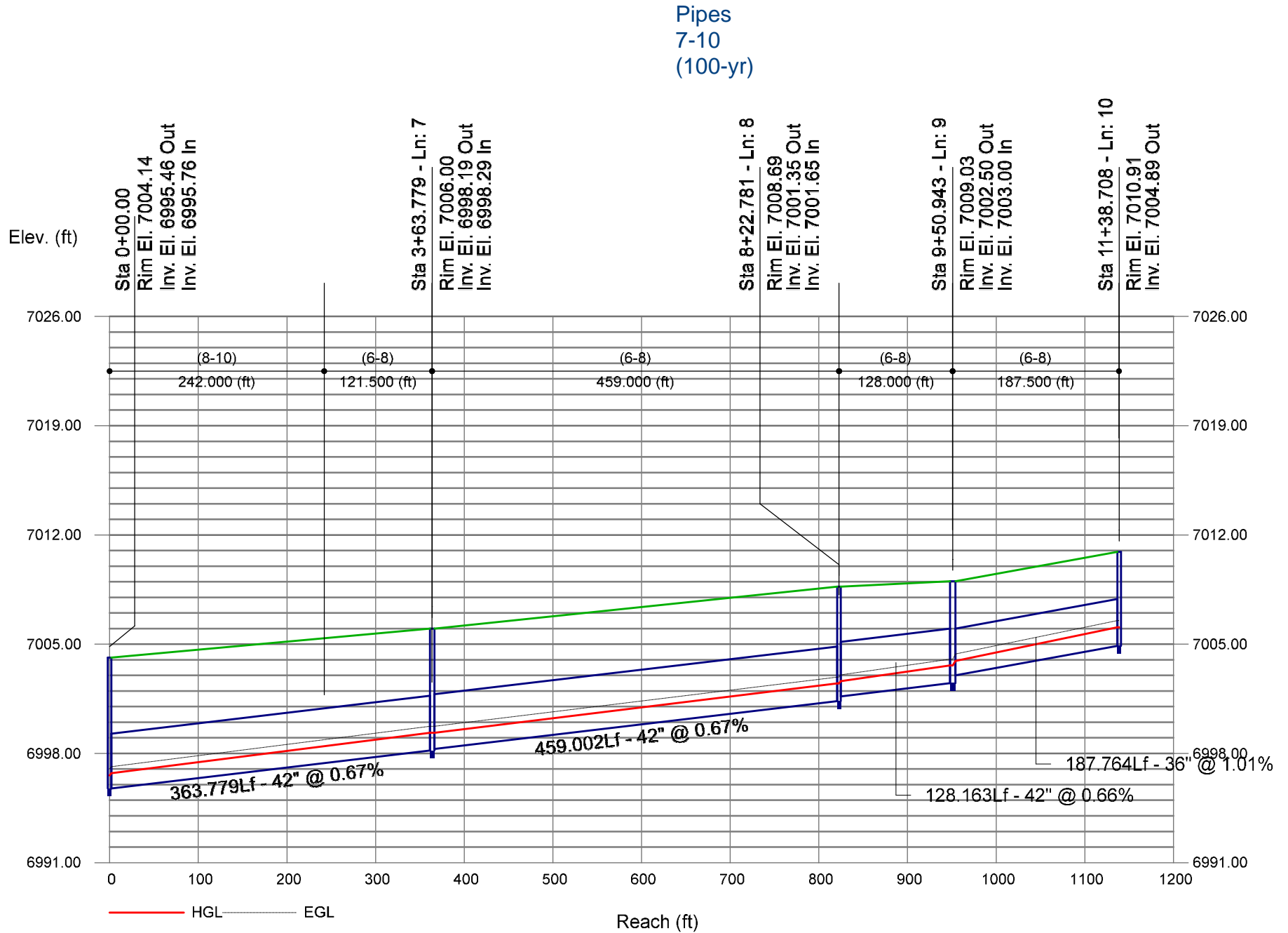
Storm Sewer Profile



Storm Sewer Profile

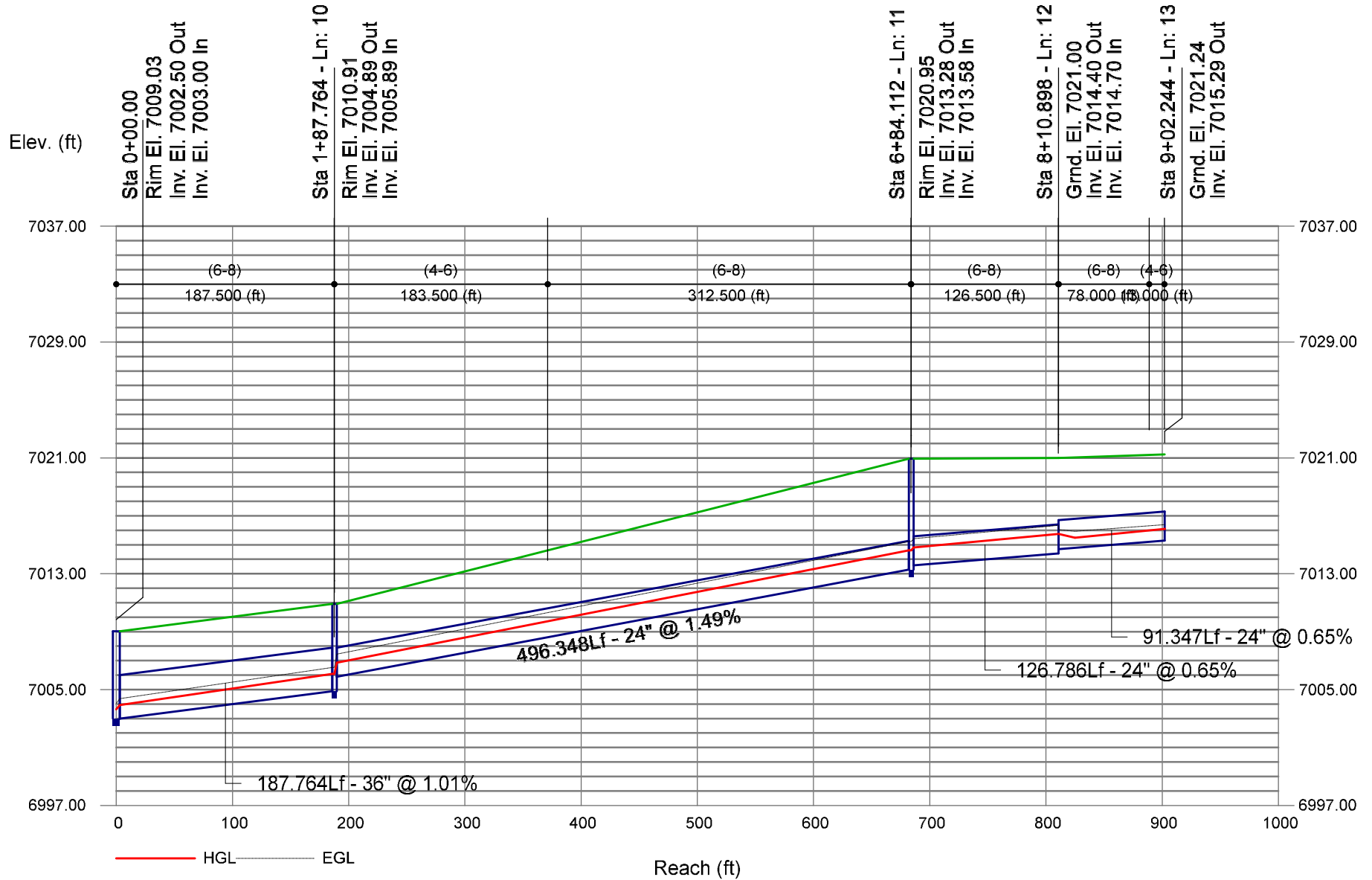


Storm Sewer Profile

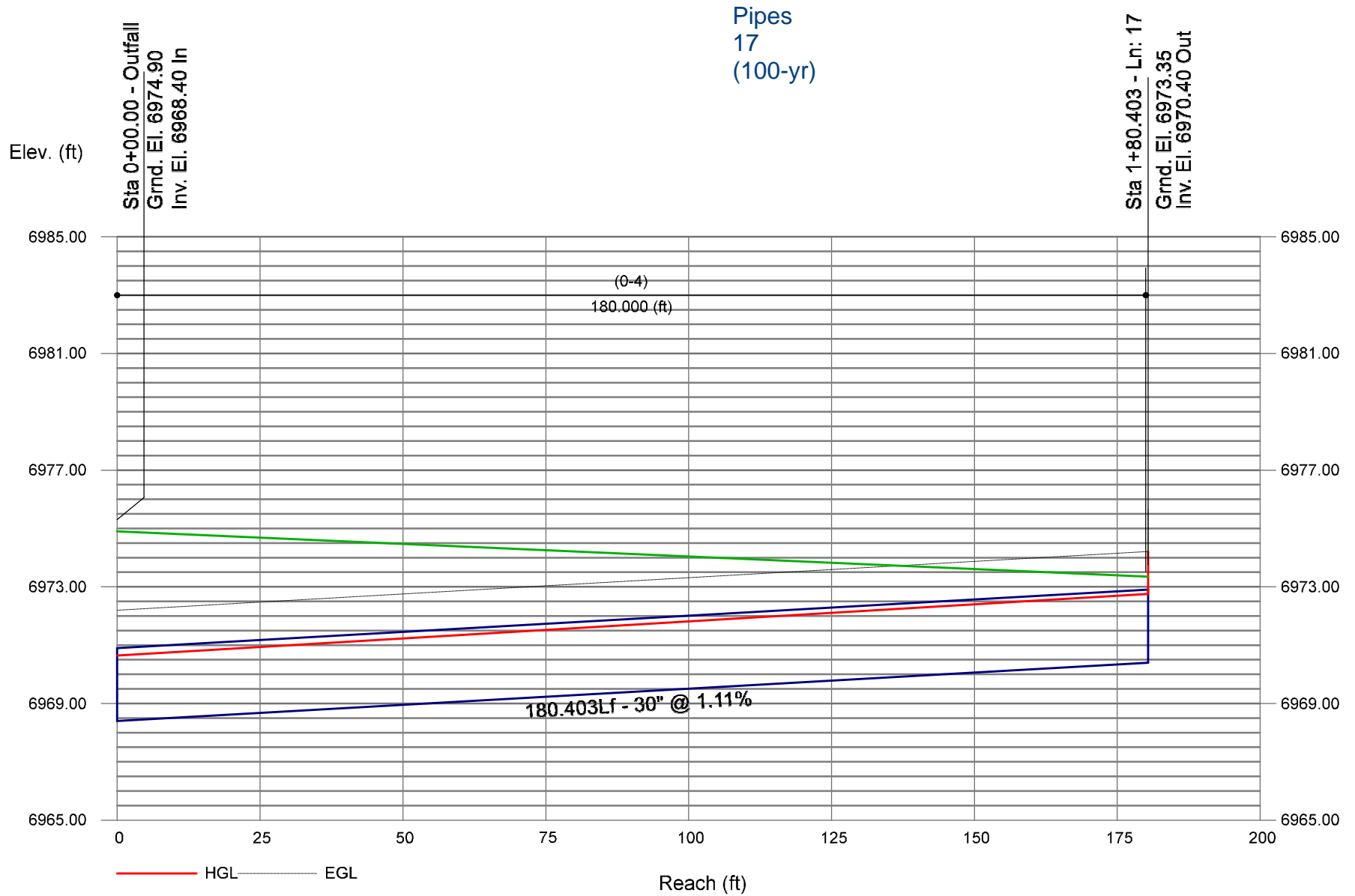


Storm Sewer Profile

Pipes
10-13
(100-yr)



Storm Sewer Profile





PIPE OUTFALL RIPRAP SIZING CALCULATIONS

Subdivision: Schmidt Parcel - District P1
 Location: El Paso County

Project Name: Schmidt Parcel - INTERIM
 Project No.: 24013.00
 Calculated By: REB
 Checked By: _____
 Date: 4/27/26

	STORM DRAIN SYSTEM			Notes
	DESIGN POINT 4.1	DESIGN POINT 11.2	DESIGN POINT 14.1	
Q ₁₀₀ (cfs):	7.9	44.3	46.4	
Conduit	Pipe	Pipe	Pipe	
D _c , Pipe Diameter (in):	24	42	30	
W, Box Width (ft):	N/A			
H, Box Height (ft):	N/A			
Y _t , Tailwater Depth (ft):	0.80	1.00	1.00	If unknown, use Y _t /D _c (or H)=0.4
Y _t /D _c or Y _t /H	0.40	0.29	0.40	
Q/D ^{2.5} or Q/(WH ^{3/2})	1.40	1.93	4.70	
Supercritical?	No	No	No	
Y _n , Normal Depth (ft) [Supercritical]:				
D _a , H _a (in) [Supercritical]:	N/A	N/A	N/A	D _a =(D _c +Y _n)/2
Riprap d ₅₀ (in) [Supercritical]:	N/A	N/A	N/A	
Riprap d ₅₀ (in) [Subcritical]:	2.33	8.40	9.73	
Required Riprap Size:	L	L	M	Fig. 9-38 or Fig. 9-36
d₅₀ (in):	9	9	12	
Expansion Factor, 1/(2 tan θ):	6.50	4.00	2.50	Read from Fig. 9-35 or 9-36
θ:	0.08	0.12	0.20	
Erosive Soils?	No	No		
Area of Flow, A _t (ft ²):	1.13	6.33	6.63	A _t =Q/V
Length of Protection, L _p (ft):	-3.8	11.3	10.3	L=(1/(2 tan θ))(A _t /Y _t - D)
Min Length (ft)	6.0	10.5	7.5	Min L=3D or 3H
Max Length (ft)	20.0	35.0	25.0	Max L=10D or 10H
Min Bottom Width, T (ft):	1.4	6.3	6.6	T=2*(L _p *tanθ)+W
Design Length (ft)	6.0	12.0	11.0	
Design Width (ft)	1.4	6.3	6.6	
Riprap Depth (in)	18	18	24	Depth=2(d ₅₀)
Type II Bedding Depth (in)*	6	6	6	*Not used if Soil Riprap
Cutoff Wall	No	No	No	
Cutoff Wall Depth (ft)				Depth of Riprap and Base
Cutoff Wall Width (ft)				

Note: No Type II Base to be used if Soil Riprap is specified within the plans
 * For use when the flow in the culvert is supercritical (and less than full).

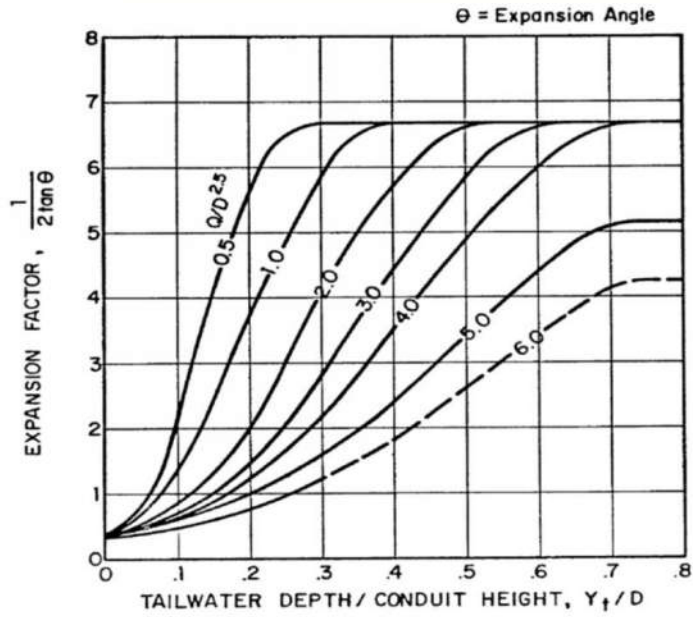


Figure 9-35. Expansion factor for circular conduits

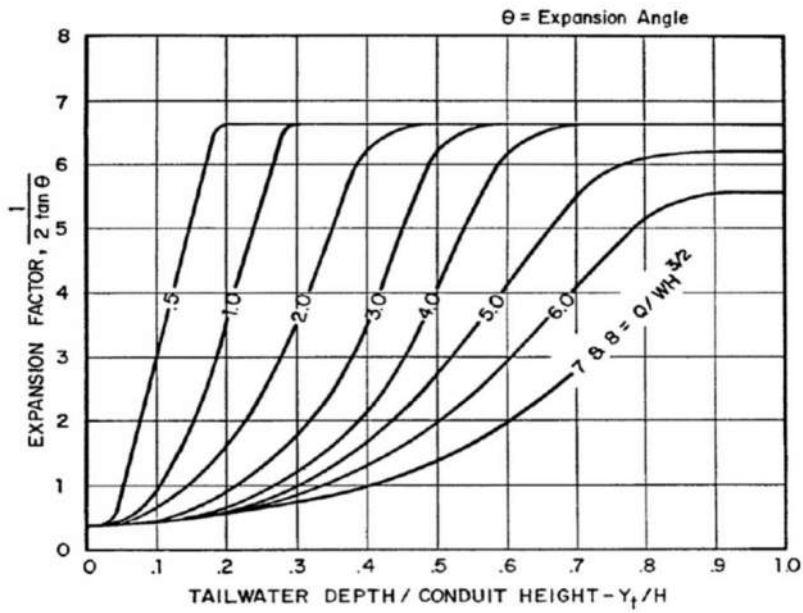


Figure 9-36. Expansion factor for rectangular conduits



Subdivision: ANTLER RANGE F1
Location: El Paso County
Project Name: ANTLER RANGE F1
Project Number: 24013
Calculated By: NQJ
Checked By: REB
Date: 4/13/2026

Proposed Conditions - Drainageway/Swale Summary Table						
Channel Section	Section Slope, ft/ft	100-year Depth, ft	100-year Velocity, ft/s	100-year Hydraulic Radius, ft	Froude, 100-yr	Shear Stress, 100-yr
E1	0.0456	0.8	4.72	0.39	0.93	1.1
K1	0.0110	1.42	1.42	0.69	0.21	0.5
L1	0.0172	0.95	0.95	0.78	0.17	0.8

Channel Report

SWALE E1 - DP5 Q100 (MAX SLOPE)

Triangular

Side Slopes (z:1) = 5.00, 5.00

Total Depth (ft) = 2.00

Invert Elev (ft) = 1.00

Slope (%) = 4.56

N-Value = 0.035

Calculations

Compute by: Known Q

Known Q (cfs) = 15.10

Highlighted

Depth (ft) = 0.80

Q (cfs) = 15.10

Area (sqft) = 3.20

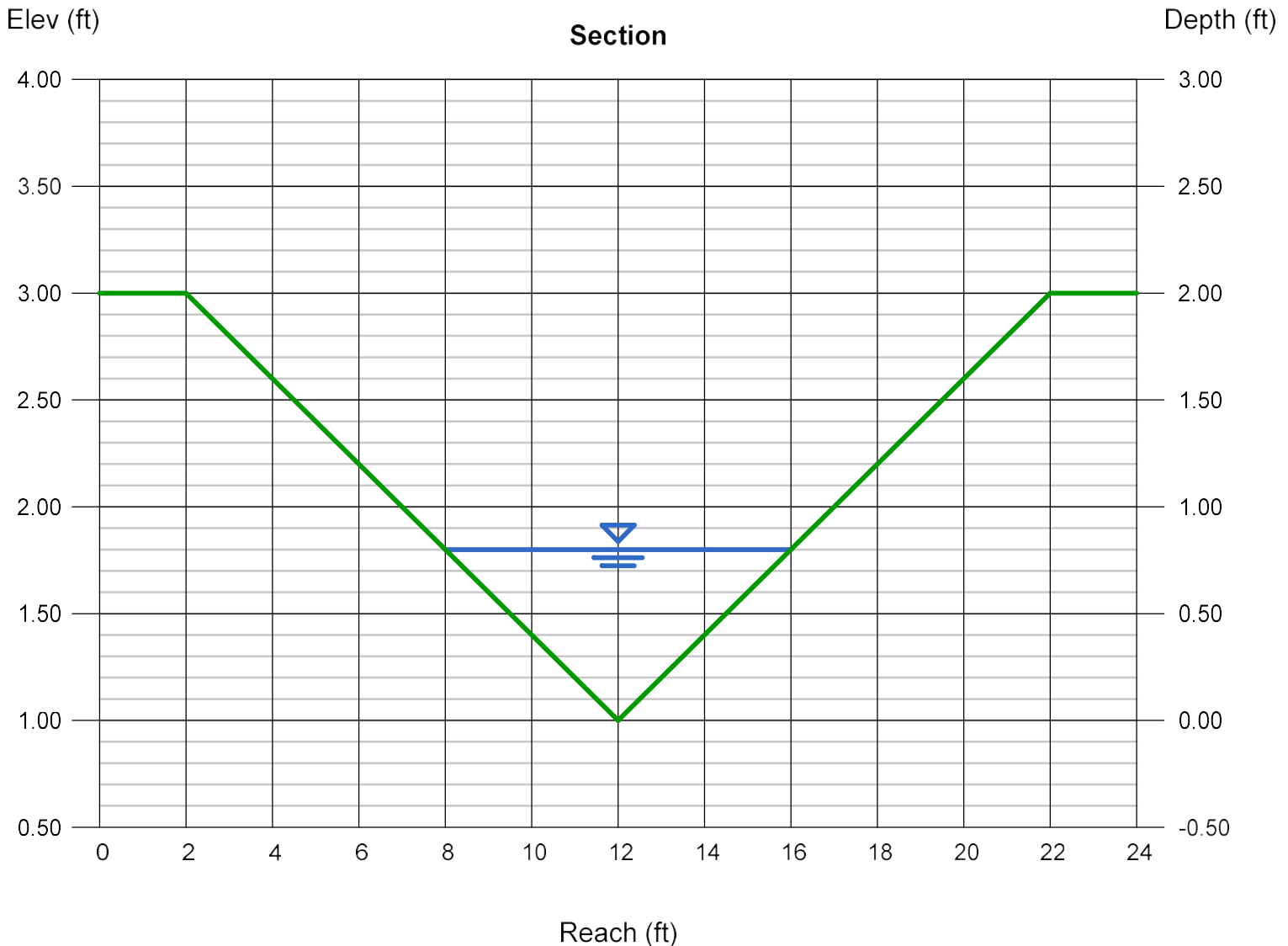
Velocity (ft/s) = 4.72

Wetted Perim (ft) = 8.16

Crit Depth, Yc (ft) = 0.90

Top Width (ft) = 8.00

EGL (ft) = 1.15



Channel Report

SWALE K1 - DP11 Q100

Triangular

Side Slopes (z:1) = 4.00, 4.00

Total Depth (ft) = 2.50

Invert Elev (ft) = 1.00

Slope (%) = 1.10

N-Value = 0.035

Calculations

Compute by: Known Q

Known Q (cfs) = 28.00

Highlighted

Depth (ft) = 1.42

Q (cfs) = 28.00

Area (sqft) = 8.07

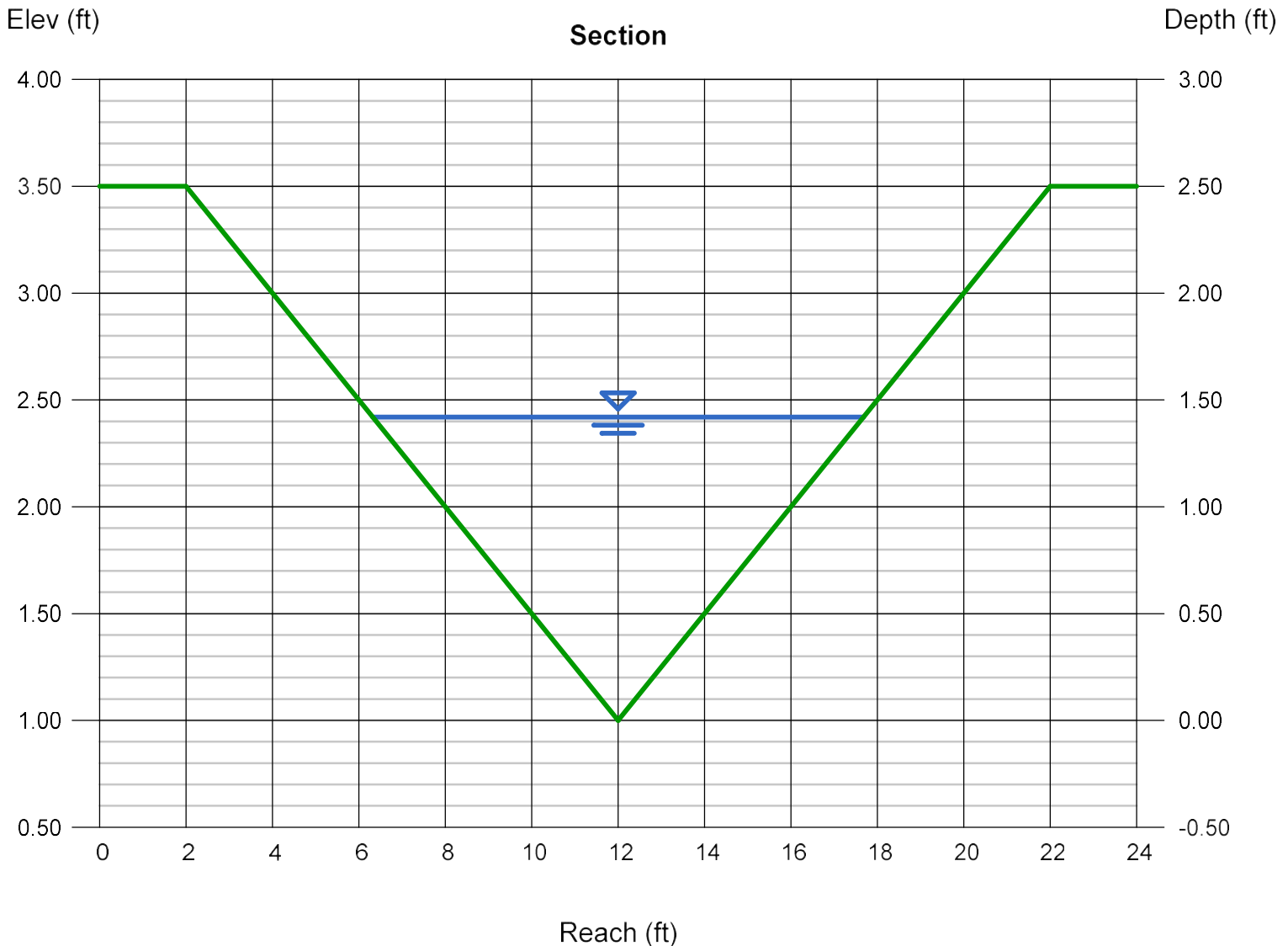
Velocity (ft/s) = 3.47

Wetted Perim (ft) = 11.71

Crit Depth, Yc (ft) = 1.25

Top Width (ft) = 11.36

EGL (ft) = 1.61



Channel Report

SWALE L1 - DP5.1 Q100 (CAPACITY)

Trapezoidal

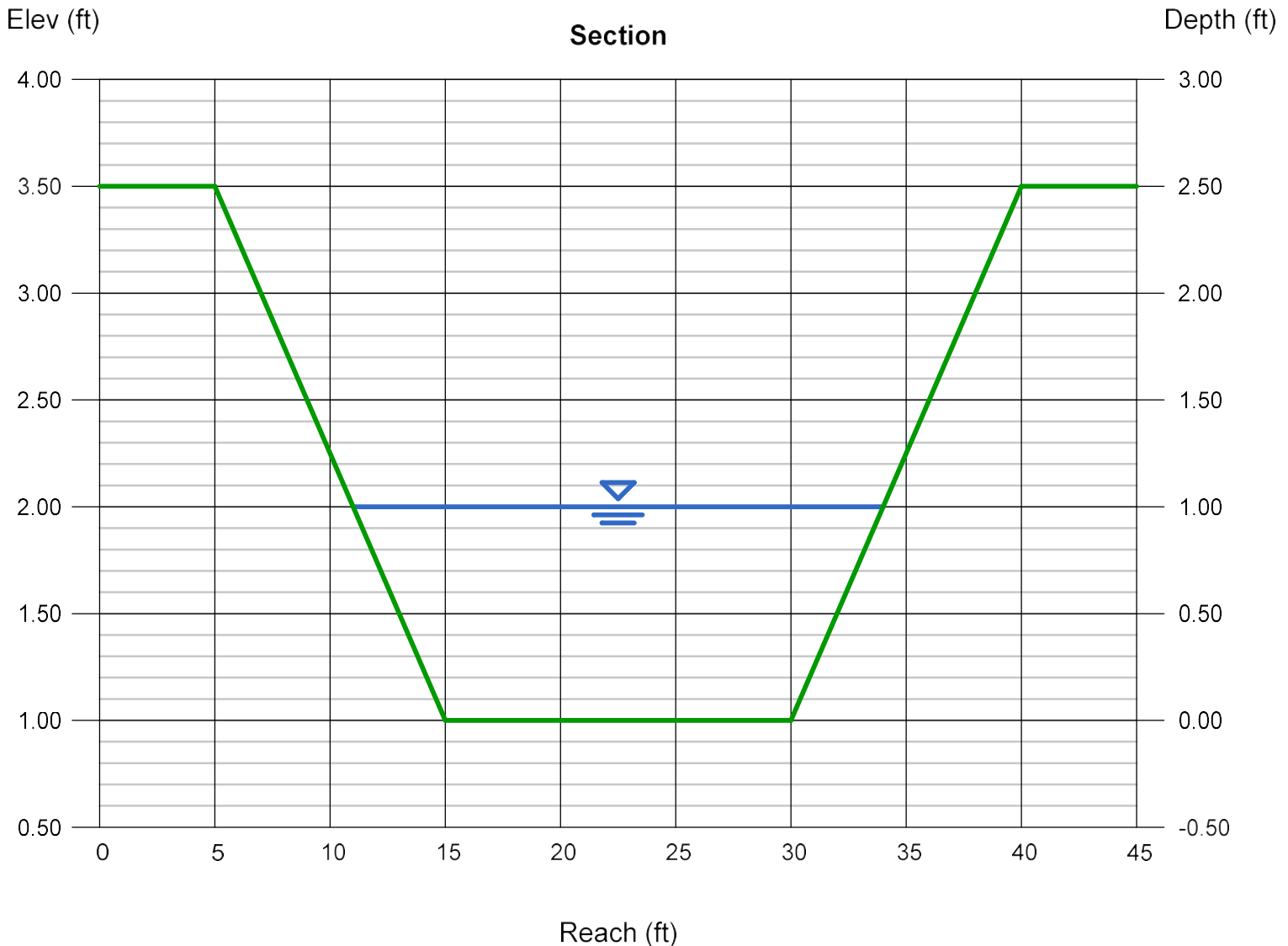
Bottom Width (ft)	= 15.00
Side Slopes (z:1)	= 4.00, 4.00
Total Depth (ft)	= 2.50
Invert Elev (ft)	= 1.00
Slope (%)	= 0.64
N-Value	= 0.035

Highlighted

Depth (ft)	= 1.00
Q (cfs)	= 56.00
Area (sqft)	= 19.00
Velocity (ft/s)	= 2.95
Wetted Perim (ft)	= 23.25
Crit Depth, Yc (ft)	= 0.71
Top Width (ft)	= 23.00
EGL (ft)	= 1.14

Calculations

Compute by:	Known Q
Known Q (cfs)	= 56.00



Channel Report

SWALE L1 - DP13.1 Q100 (MAX SLOPE)

Trapezoidal

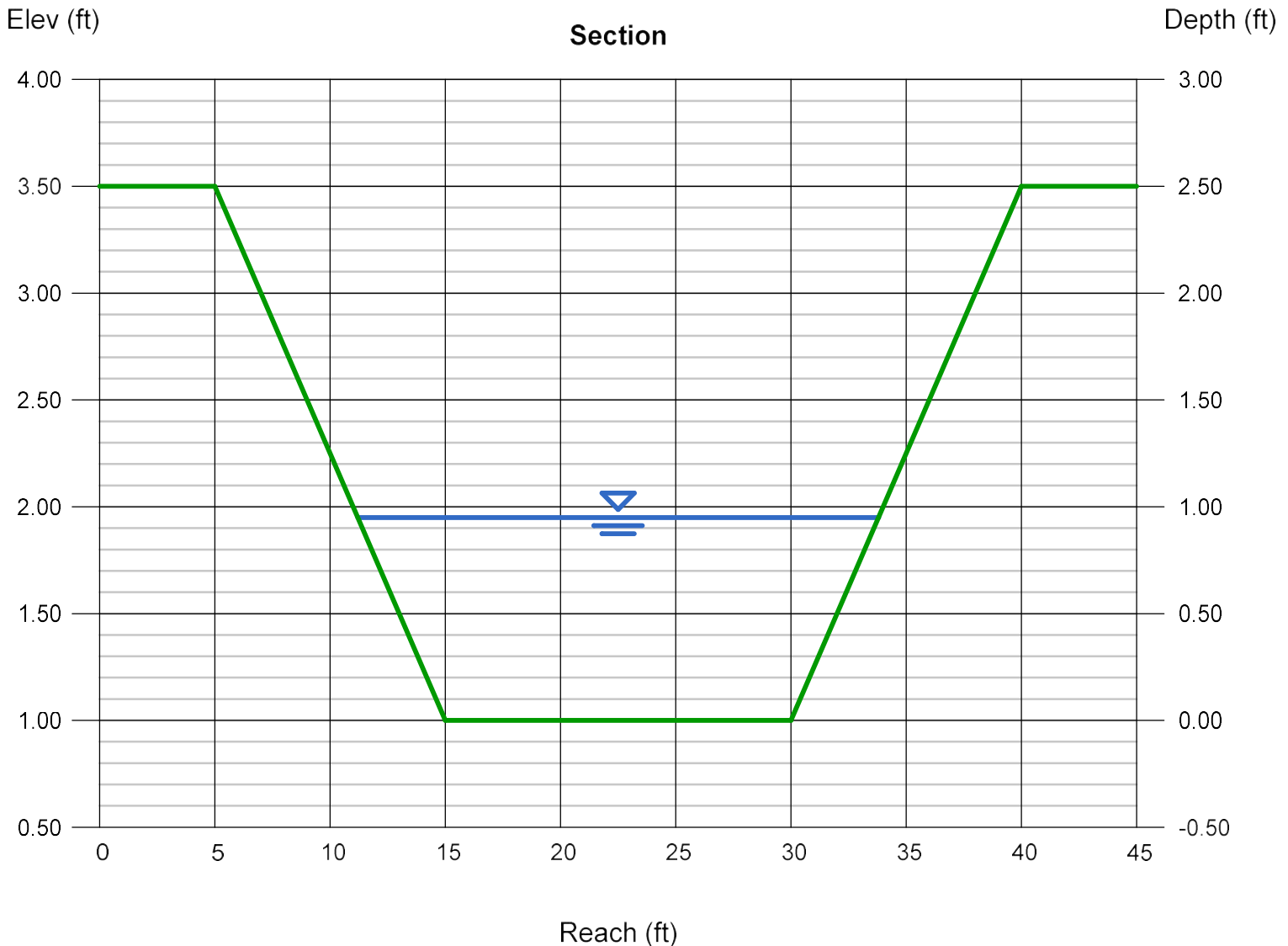
Bottom Width (ft)	= 15.00
Side Slopes (z:1)	= 4.00, 4.00
Total Depth (ft)	= 2.50
Invert Elev (ft)	= 1.00
Slope (%)	= 1.72
N-Value	= 0.035

Highlighted

Depth (ft)	= 0.95
Q (cfs)	= 83.00
Area (sqft)	= 17.86
Velocity (ft/s)	= 4.65
Wetted Perim (ft)	= 22.83
Crit Depth, Yc (ft)	= 0.91
Top Width (ft)	= 22.60
EGL (ft)	= 1.29

Calculations

Compute by:	Known Q
Known Q (cfs)	= 83.00



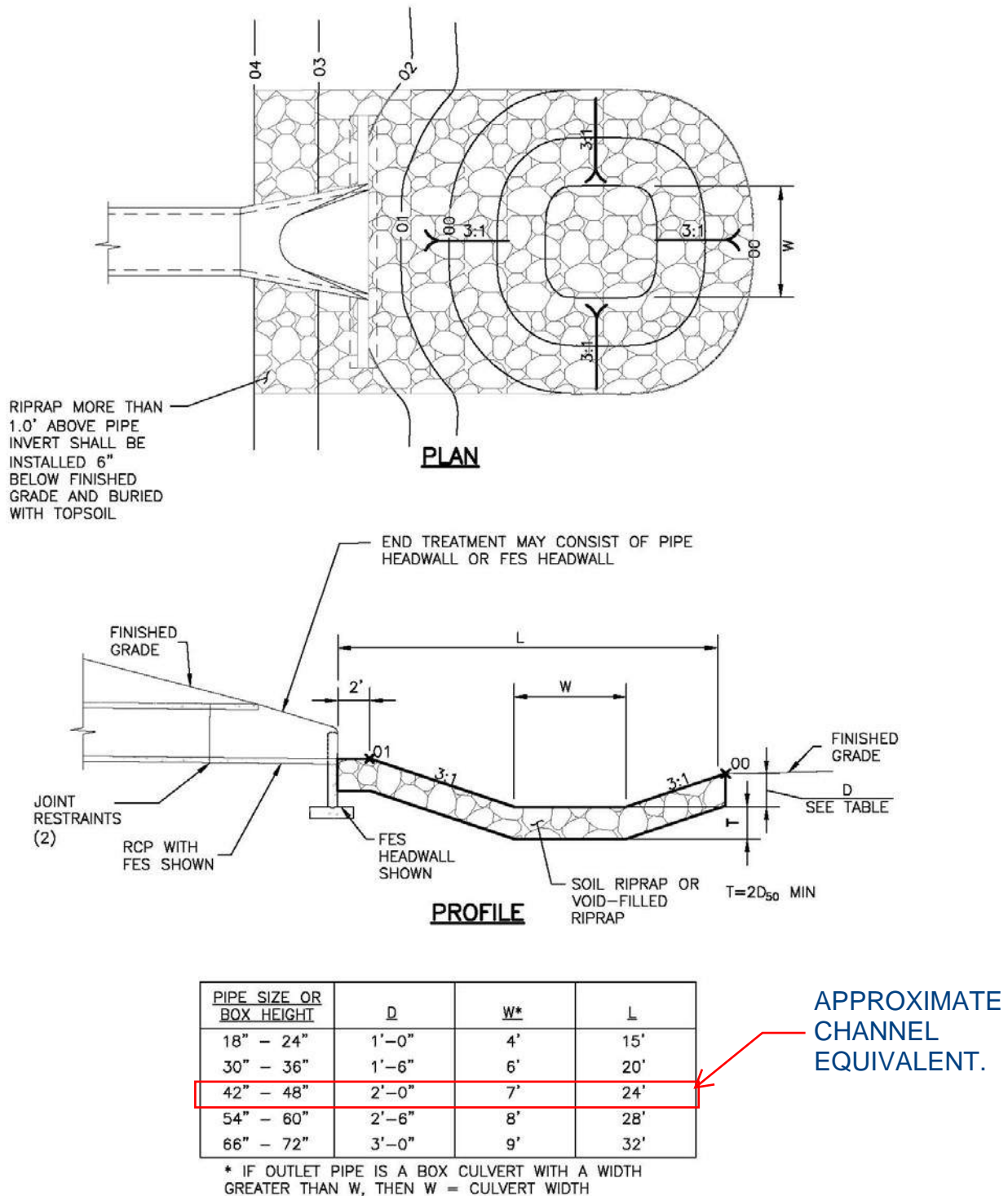


Figure 9-37. Low tailwater riprap basin

Q (DP13.1) = 83 CFS Figure 9-39 is valid for $Q/WH^{1.5}$ of 8.0 or less.
 W = 15
 H = 2
 $Q/WH^{1.5} = 1.95 = <8$ (VALID)

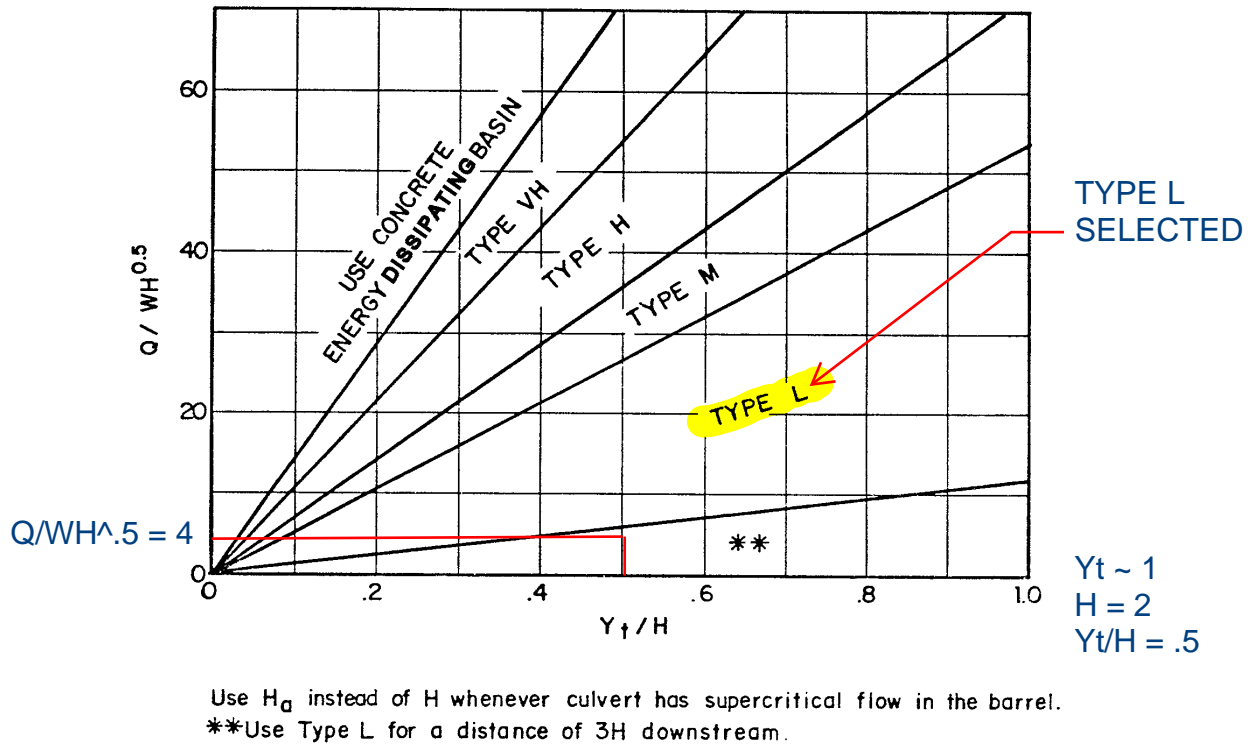


Figure 9-39. Riprap erosion protection at rectangular conduit outlet (valid for $Q/WH^{1.5} \leq 8.0$)

3.2.4 Outfalls and Rundowns

A grouted boulder outfall or “rundown” dissipates energy and provides erosion control protection. Grouted boulder outfalls are most commonly used in large rivers like the South Platte. Figure 9-40 provides a plan view and cross section for a standard grouted boulder rundown. See the grouted boulder drop profiles (A1, A2, and A3) in Figure 9-12 for site specific profile options, (i.e., depressed or free-draining basin for use with a stable downstream channel or with no basin for use in channels subject to degradation). Figure 9-41 provides a plan view of the same structure for use when the structure is in-line with the channel. Evaluate the following when designing a grouted boulder outfall or rundown:

- Minimize disturbance to channel bank
- Determine water surface elevation in receiving channel for base flow and design storm(s)
- Determine flow rate, velocity, depth, etc. of flow exiting the outfall pipe for the design storm(s)
- Evaluate permitting procedures and requirements for construction adjacent to large river system.



APPENDIX D – WATER QUALITY & DETENTION

$$w = 9.23 (A_{FB} / t) (1 / \sqrt{h_{max}})$$

Equation 4-1

Where:

w = width of the rectangular vertical notch (inches)

A_{FB} = surface area of the forebay (square feet)

t = emptying time of the brim-full forebay (seconds)

h_{max} = maximum depth of the forebay (feet)

TABLE 4-12. FOREBAY SIZING CRITERIA

FOREBAY SIZING CRITERIA	WATERSHED IMPERVIOUS AREA (IA)				
	IA UP TO 2 ACRES	IA 2 UP TO 5 ACRES	IA 5 UP TO 10 ACRES	IA 10 UP TO 20 ACRES	IA GREATER THAN 20 ACRES
Forebay Release Rate and Configuration	Concrete sediment pad with dense grasses surrounding,	Size to drain in 4 to 5 minutes using Equation 4-1			
Minimum Forebay Volume ¹	concrete pad with slotted metal edge, or similar design				
Forebay Depth ¹		12 to 15 inches	15 to 18 inches	18 to 24 inches	24 to 30 inches

¹ Appropriate volume and depth should consider maintenance and access needs. The values provided are approximate and provide a starting point for design.

IA = 5.5% * 84.37 acres = 4.64 IA's
 Design Depth = 15" - 18"

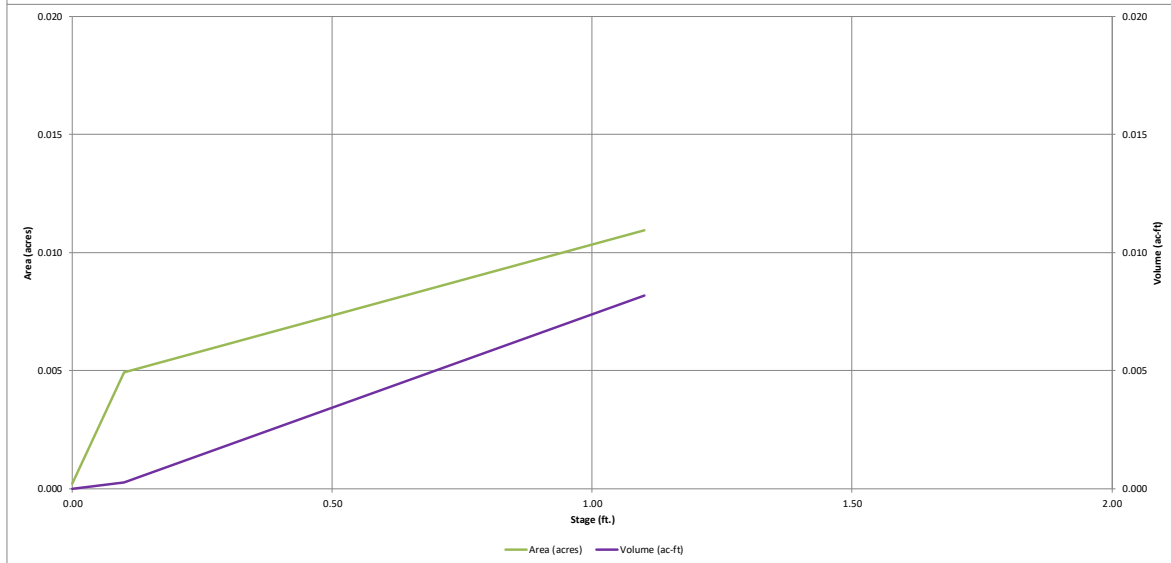
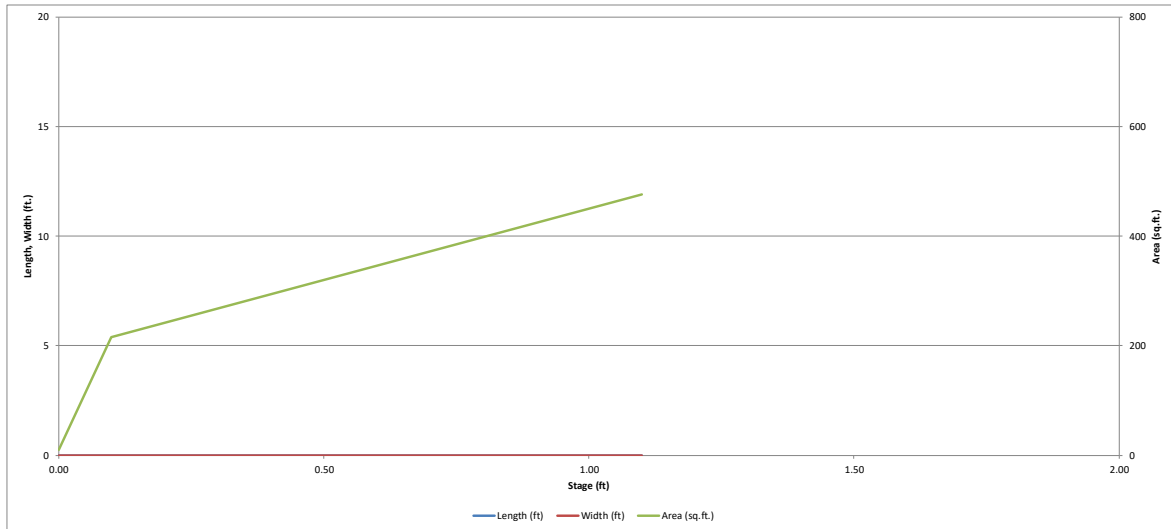
Minimum Volume = 1% of WQCV = 1% * 0.277 ac-ft * 43,560 = 120 CF MIN.

Provided Volume ~ 357 CF (see MHFD Volume Calc)

Design utilizes (1) 8" culvert pipes (see culvert calc on next page)
 flow rate @ design full = 3 CFS
 Drain Time = 347 CF / 1.4CFS = 248 seconds or 4.13 minutes

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.07 (June 2025)



Culvert Report

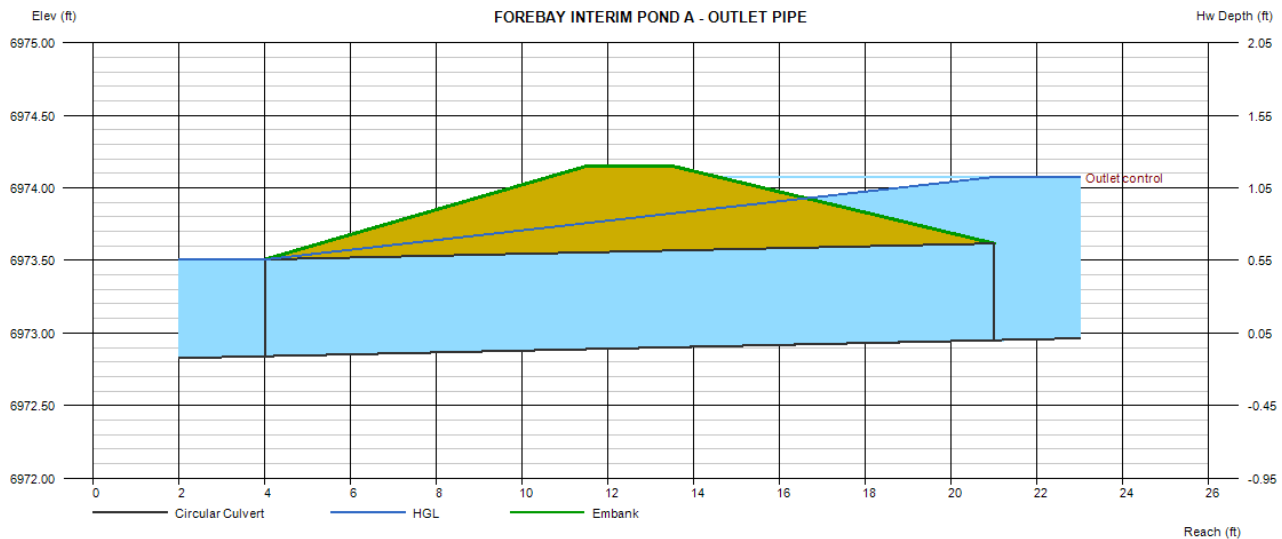
FOREBAY INTERIM POND A - OUTLET PIPE

Invert Elev Dn (ft)	= 6972.84
Pipe Length (ft)	= 17.00
Slope (%)	= 0.649126851931214
Invert Elev Up (ft)	= 6972.95
Rise (in)	= 8.0
Shape	= Circular
Span (in)	= 8.0
No. Barrels	= 1
n-Value	= 0.012
Culvert Type	= Circular Culvert
Culvert Entrance	= Smooth tapered inlet throat
Coeff. K,M,c,Y,k	= 0.534, 0.555, 0.0196, 0.9, 0.2

Embankment	
Top Elevation (ft)	= 6974.15
Top Width (ft)	= 2.00
Crest Width (ft)	= 45.00

Calculations	
Qmin (cfs)	= 1.40
Qmax (cfs)	= 1.40
Tailwater Elev (ft)	= Crown

Highlighted	
Qtotal (cfs)	= 1.40
Qpipe (cfs)	= 1.40
Qovertop (cfs)	= 0.00
Veloc Dn (ft/s)	= 4.01
Veloc Up (ft/s)	= 4.01
HGL Dn (ft)	= 6973.51
HGL Up (ft)	= 6974.08
Hw Elev (ft)	= 6974.08
Hw/D (ft)	= 1.69
Flow Regime	= Outlet Control



Channel Report

TRICKLE CHANNEL CAPACITY (2X FOREBAY RELEASE)

Triangular

Side Slopes (z:1) = 2.00, 2.00

Total Depth (ft) = 1.00

Invert Elev (ft) = 1.00

Slope (%) = 0.50

N-Value = 0.030

Calculations

Compute by: Known Q

Known Q (cfs) = 2.80

Highlighted

Depth (ft) = 0.87

Q (cfs) = 2.800

Area (sqft) = 1.51

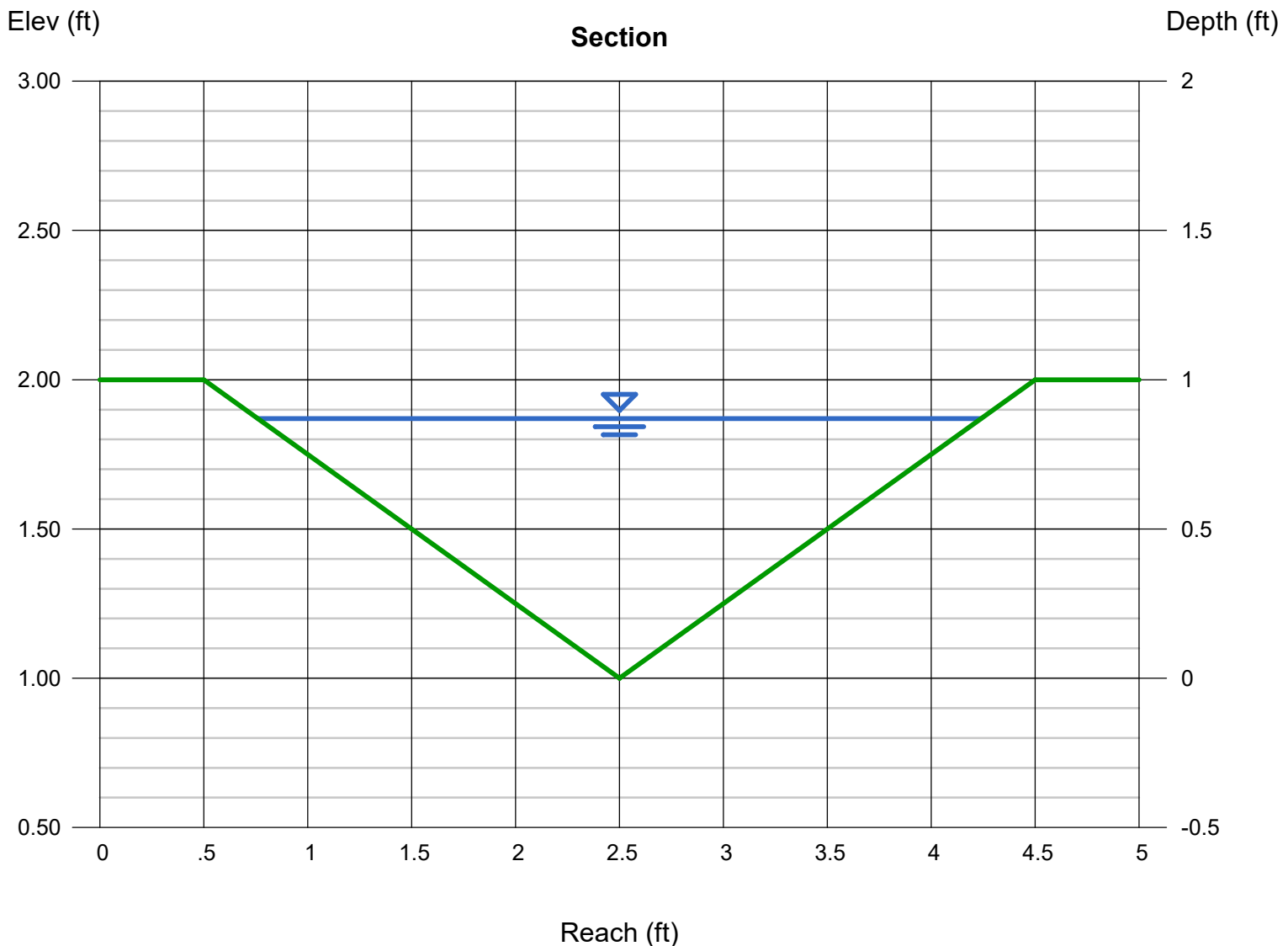
Velocity (ft/s) = 1.85

Wetted Perim (ft) = 3.89

Crit Depth, Yc (ft) = 0.66

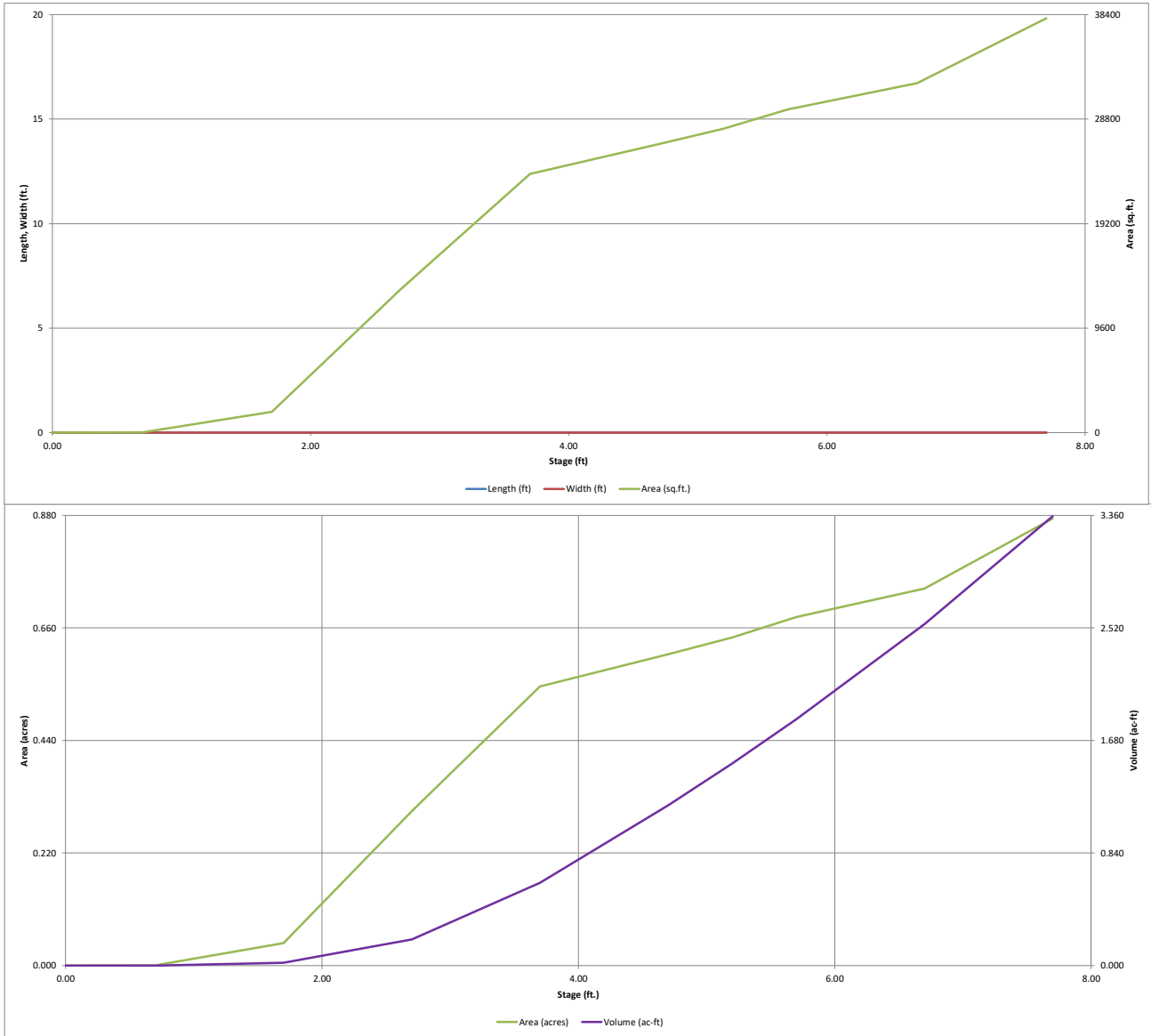
Top Width (ft) = 3.48

EGL (ft) = 0.92



DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-*Detention*, Version 4.06 (July 2022)

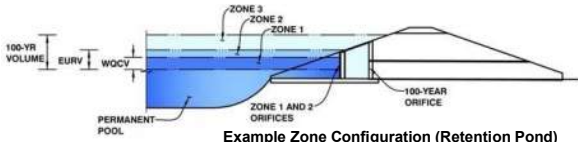


DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.06 (July 2022)

Project: Schmidt Phase 1 - District Infrastructure

Basin ID: Pond A - Interim



Example Zone Configuration (Retention Pond)

	Estimated Stage (ft)	Estimated Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	2.94	0.273	Orifice Plate
Zone 2 (EURV)	2.96	0.009	Orifice Plate
Zone 3 (100-year)	5.02	1.109	Weir&Pipe (Restrict)
Total (all zones)		1.391	

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth = ft (distance below the filtration media surface)
 Underdrain Orifice Diameter = inches

Calculated Parameters for Underdrain

Underdrain Orifice Area = ft²
 Underdrain Orifice Centroid = feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Centroid of Lowest Orifice = 0.00 ft (relative to basin bottom at Stage = 0 ft)
 Depth at top of Zone using Orifice Plate = 2.86 ft (relative to basin bottom at Stage = 0 ft)
 Orifice Plate: Orifice Vertical Spacing = N/A inches
 Orifice Plate: Orifice Area per Row = N/A sq. inches

Calculated Parameters for Plate

WQ Orifice Area per Row = N/A ft²
 Elliptical Half-Width = N/A feet
 Elliptical Slot Centroid = N/A feet
 Elliptical Slot Area = N/A ft²

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	1.00	2.30					
Orifice Area (sq. inches)	0.79	0.79	0.99					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

	Not Selected	Not Selected	
Invert of Vertical Orifice =	<input type="text"/>	<input type="text"/>	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Vertical Orifice =	<input type="text"/>	<input type="text"/>	ft (relative to basin bottom at Stage = 0 ft)
Vertical Orifice Diameter =	<input type="text"/>	<input type="text"/>	inches

Calculated Parameters for Vertical Orifice

	Not Selected	Not Selected	
Vertical Orifice Area =	<input type="text"/>	<input type="text"/>	ft ²
Vertical Orifice Centroid =	<input type="text"/>	<input type="text"/>	feet

User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir and No Outlet Pipe)

	Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	3.00	N/A	ft (relative to basin bottom at Stage = 0 ft)
Overflow Weir Front Edge Length =	3.76	N/A	feet
Overflow Weir Grate Slope =	0.00	N/A	H:V
Horiz. Length of Weir Sides =	3.76	N/A	feet
Overflow Grate Type =	Close Mesh Grate	N/A	
Debris Clogging % =	50%	N/A	%

Calculated Parameters for Overflow Weir

	Zone 3 Weir	Not Selected	
Height of Grate Upper Edge, H ₁ =	3.00	N/A	feet
Overflow Weir Slope Length =	3.76	N/A	feet
Grate Open Area / 100-yr Orifice Area =	2.28	N/A	
Overflow Grate Open Area w/o Debris =	11.18	N/A	ft ²
Overflow Grate Open Area w/ Debris =	5.59	N/A	ft ²

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

	Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	0.90	N/A	ft (distance below basin bottom at Stage = 0 ft)
Outlet Pipe Diameter =	30.00	N/A	inches
Restrictor Plate Height Above Pipe Invert =	30.00		inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate

	Zone 3 Restrictor	Not Selected	
Outlet Orifice Area =	4.91	N/A	ft ²
Outlet Orifice Centroid =	1.25	N/A	feet
Half-Central Angle of Restrictor Plate on Pipe =	3.14	N/A	radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage = 5.10 ft (relative to basin bottom at Stage = 0 ft)
 Spillway Crest Length = 16.00 feet
 Spillway End Slopes = 4.00 H:V
 Freeboard above Max Water Surface = 1.00 feet

Calculated Parameters for Spillway

Spillway Design Flow Depth = 0.99 feet
 Stage at Top of Freeboard = 7.09 feet
 Basin Area at Top of Freeboard = 0.79 acres
 Basin Volume at Top of Freeboard = 2.85 acre-ft

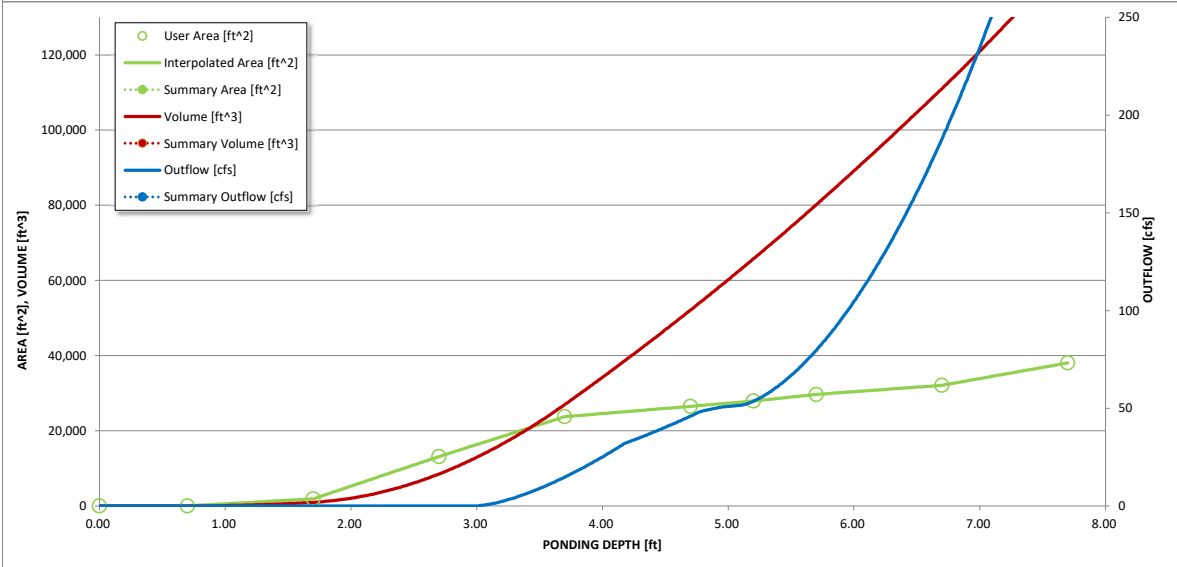
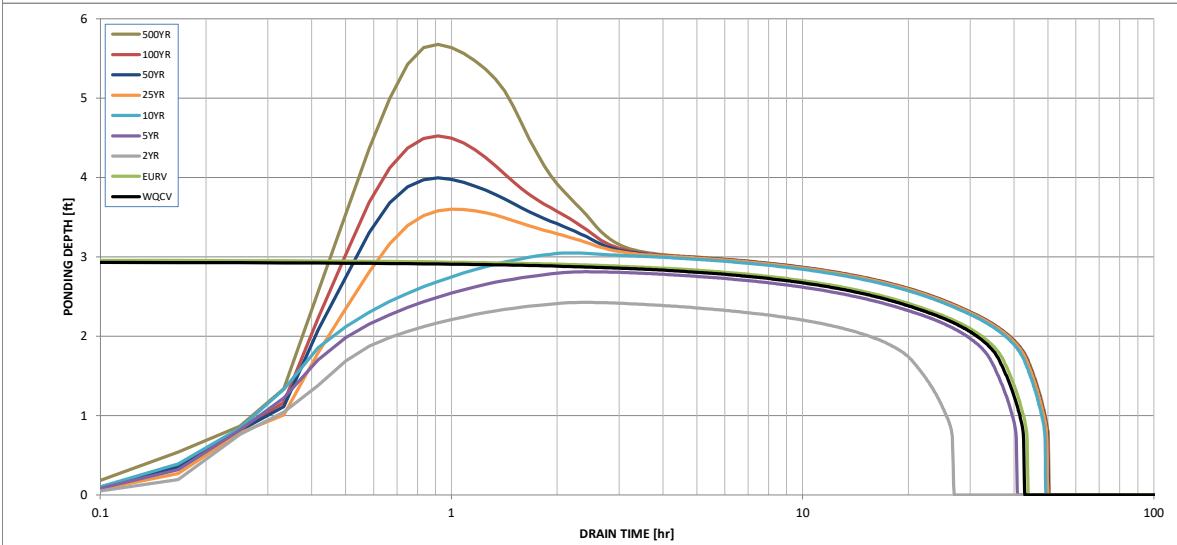
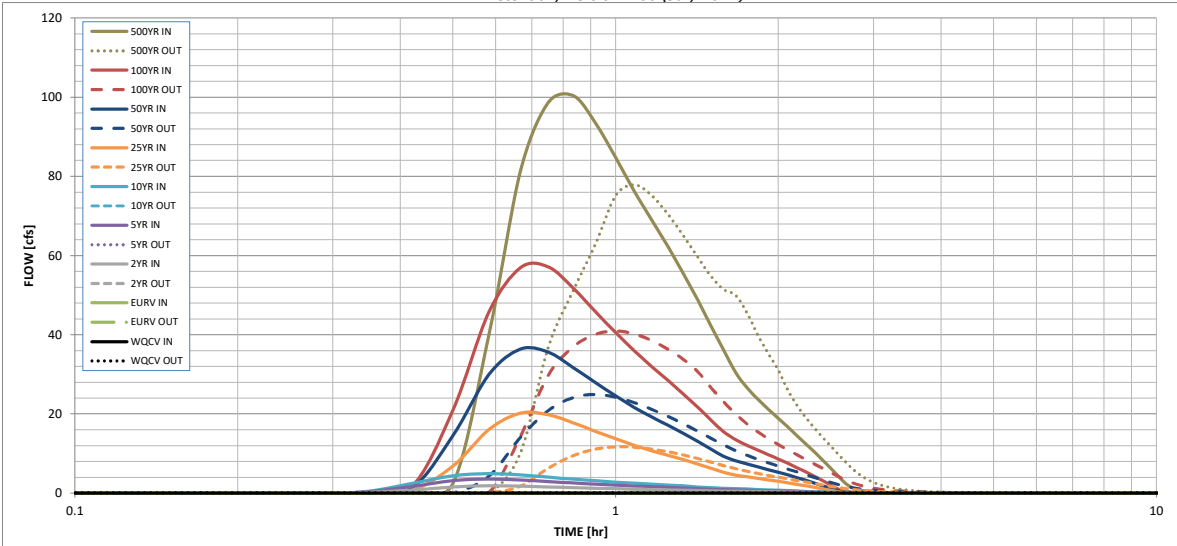
Routed Hydrograph Results

The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).

	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =									
One-Hour Rainfall Depth (in) =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52	3.14
CUHP Runoff Volume (acre-ft) =	0.273	0.282	0.137	0.250	0.346	1.378	2.483	4.017	7.513
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	0.137	0.250	0.346	1.378	2.483	4.017	7.513
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A	0.7	1.3	1.8	16.2	32.2	53.0	96.2
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A							
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.01	0.02	0.02	0.19	0.38	0.63	1.14
Peak Inflow Q (cfs) =	N/A	N/A	1.9	3.6	4.9	20.2	36.4	57.2	100.5
Peak Outflow Q (cfs) =	0.1	0.1	0.1	0.1	0.4	11.7	24.9	40.9	77.9
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	0.1	0.2	0.7	0.8	0.8	0.8
Structure Controlling Flow =	Plate	Plate	Plate	Plate	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Spillway
Max Velocity through Gate 1 (fps) =	N/A	N/A	N/A	N/A	0.0	1.0	2.2	3.6	4.9
Max Velocity through Gate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	40	41	25	38	46	40	34	26	13
Time to Drain 99% of Inflow Volume (hours) =	42	42	26	40	48	45	43	40	34
Maximum Ponding Depth (ft) =	2.94	2.96	2.43	2.81	3.05	3.60	3.99	4.52	5.67
Area at Maximum Ponding Depth (acres) =	0.36	0.37	0.23	0.33	0.38	0.52	0.56	0.60	0.68
Maximum Volume Stored (acre-ft) =	0.275	0.282	0.121	0.230	0.312	0.561	0.780	1.088	1.819

DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.06 (July 2022)



S-A-V-D Chart Axis Override	X-axis	Left Y-Axis	Right Y-Axis
minimum bound			
maximum bound			

DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename: _____

Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

Time Interval	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.01
	0:15:00	0.00	0.00	0.03	0.05	0.06	0.04	0.05	0.05	0.07
	0:20:00	0.00	0.00	0.12	0.16	0.20	0.13	0.15	0.16	0.21
	0:25:00	0.00	0.00	0.71	1.60	2.34	0.52	0.97	1.25	2.32
	0:30:00	0.00	0.00	1.56	3.16	4.42	6.80	14.48	20.85	40.05
	0:35:00	0.00	0.00	1.87	3.56	4.91	16.09	29.97	45.75	81.21
	0:40:00	0.00	0.00	1.78	3.33	4.60	20.22	36.42	56.91	98.58
	0:45:00	0.00	0.00	1.59	2.92	4.01	19.79	35.64	57.18	100.45
	0:50:00	0.00	0.00	1.40	2.57	3.54	17.81	31.77	51.87	93.63
	0:55:00	0.00	0.00	1.25	2.28	3.13	15.63	27.99	45.87	84.77
	1:00:00	0.00	0.00	1.11	2.02	2.76	13.76	24.58	40.59	76.14
	1:05:00	0.00	0.00	1.01	1.82	2.49	12.09	21.63	35.90	68.97
	1:10:00	0.00	0.00	0.92	1.65	2.26	10.71	19.22	31.97	62.26
	1:15:00	0.00	0.00	0.82	1.48	2.06	9.57	17.13	28.44	55.51
	1:20:00	0.00	0.00	0.73	1.30	1.84	8.46	15.12	25.06	48.87
	1:25:00	0.00	0.00	0.64	1.13	1.59	7.36	13.12	21.76	42.40
	1:30:00	0.00	0.00	0.56	0.97	1.35	6.28	11.14	18.52	36.20
	1:35:00	0.00	0.00	0.50	0.87	1.22	5.27	9.33	15.52	30.50
	1:40:00	0.00	0.00	0.47	0.81	1.12	4.57	8.15	13.48	26.61
	1:45:00	0.00	0.00	0.44	0.74	1.03	4.13	7.33	12.08	23.71
	1:50:00	0.00	0.00	0.40	0.68	0.94	3.74	6.62	10.87	21.18
	1:55:00	0.00	0.00	0.37	0.61	0.85	3.36	5.94	9.73	18.87
	2:00:00	0.00	0.00	0.33	0.54	0.75	2.99	5.26	8.62	16.67
	2:05:00	0.00	0.00	0.29	0.47	0.65	2.61	4.58	7.51	14.50
	2:10:00	0.00	0.00	0.24	0.39	0.54	2.23	3.90	6.41	12.40
	2:15:00	0.00	0.00	0.20	0.32	0.43	1.85	3.22	5.32	10.36
	2:20:00	0.00	0.00	0.15	0.24	0.33	1.47	2.54	4.23	8.33
	2:25:00	0.00	0.00	0.11	0.17	0.23	1.09	1.87	3.15	6.31
	2:30:00	0.00	0.00	0.08	0.10	0.14	0.72	1.20	2.07	4.30
	2:35:00	0.00	0.00	0.05	0.07	0.09	0.36	0.56	1.02	2.33
	2:40:00	0.00	0.00	0.04	0.06	0.08	0.15	0.23	0.44	1.28
	2:45:00	0.00	0.00	0.04	0.05	0.06	0.09	0.12	0.23	0.77
	2:50:00	0.00	0.00	0.03	0.04	0.05	0.06	0.08	0.13	0.47
	2:55:00	0.00	0.00	0.02	0.03	0.04	0.04	0.06	0.09	0.29
	3:00:00	0.00	0.00	0.02	0.03	0.04	0.03	0.04	0.06	0.18
	3:05:00	0.00	0.00	0.02	0.02	0.03	0.03	0.03	0.04	0.09
	3:10:00	0.00	0.00	0.01	0.02	0.02	0.02	0.02	0.02	0.03
	3:15:00	0.00	0.00	0.01	0.01	0.02	0.02	0.02	0.02	0.02
	3:20:00	0.00	0.00	0.01	0.01	0.01	0.01	0.01	0.01	0.01
	3:25:00	0.00	0.00	0.01	0.01	0.01	0.01	0.01	0.01	0.01
	3:30:00	0.00	0.00	0.01	0.01	0.01	0.01	0.01	0.01	0.01
	3:35:00	0.00	0.00	0.00	0.00	0.01	0.01	0.01	0.01	0.01
	3:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.01	0.00	0.01
	3:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
4:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
4:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
4:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
4:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
4:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
4:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
4:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
4:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
4:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
5:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
5:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	



APPENDIX E – REFERENCE MATERIAL

RECEIVED

MAY 10 1996

Planning Dept.

SILVER PONDS SUBDIVISION FILING NO. 1

FINAL DRAINAGE REPORT

**February 2, 1995
Revised May 5, 1996
Project No. 60572**

PREPARED FOR:

**The Campbell Corporation
4975 Austin Bluffs Parkway
Colorado Springs, CO 80918**

PREPARED BY:

**M.V.E., Inc.
1911 Lelaray St.
Colorado Springs, CO 80909**

Table 3.1 - Developed Condition Hydrologic Data
5-year and 100-Year

Design Point	Included Basins	Cumulative Drainage Area (Ac)	5-yr Discharge (cfs)	100-yr Discharge (cfs)
1	OSA1	18.14	13.1	30.4
2	OSA2	8.72	7.0	16.3
3	OSA1 thru A3	29.05	20.5	47.7
4	OSA1 thru A4	31.04	24.3	53.6
5	OSB1	39.26	29.8	69.3
6	OSB1 thru B2	44.66	25.9	60.3
7	OSB1 thru B3	50.03	35.7	83.1
8	OSB1 thru B4	52.02	39.2	89.8
9	OSD1	8.26	7.9	18.4
10	OSD1 thru D2	19.95	24.1	52.9
11	D3	3.41	4.5	9.9
12	E1	4.24	5.5	12.1
13	F1	4.26	6.6	14.4
14	OSG1	6.66	7.0	16.4
15	OSG1 thru G2	9.22	10.5	24.0
16	OSH1	17.22	17.5	38.4
17	OSH1 thru H2	28.28	27.9	61.3
18	OSI1	3.67	3.3	7.8
19	OSI1 thru I2	11.05	7.9	18.4
20	I3	8.01	6.3	14.6
21	OSI1 thru I4	27.16	19.0	44.2
22	J1	4.19	3.0	6.9

DEVELOPED DISCHARGES
 RAINFALL/RUNOFF ANALYSIS - RATIONAL METHOD

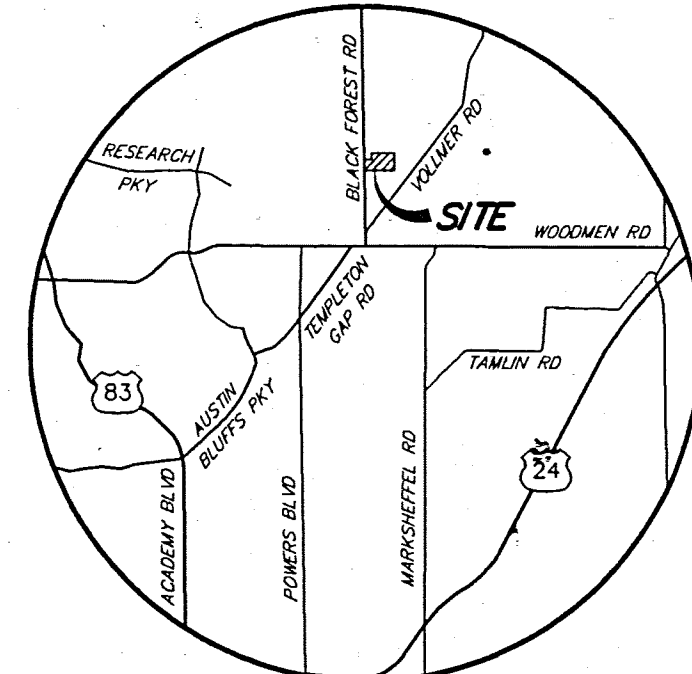
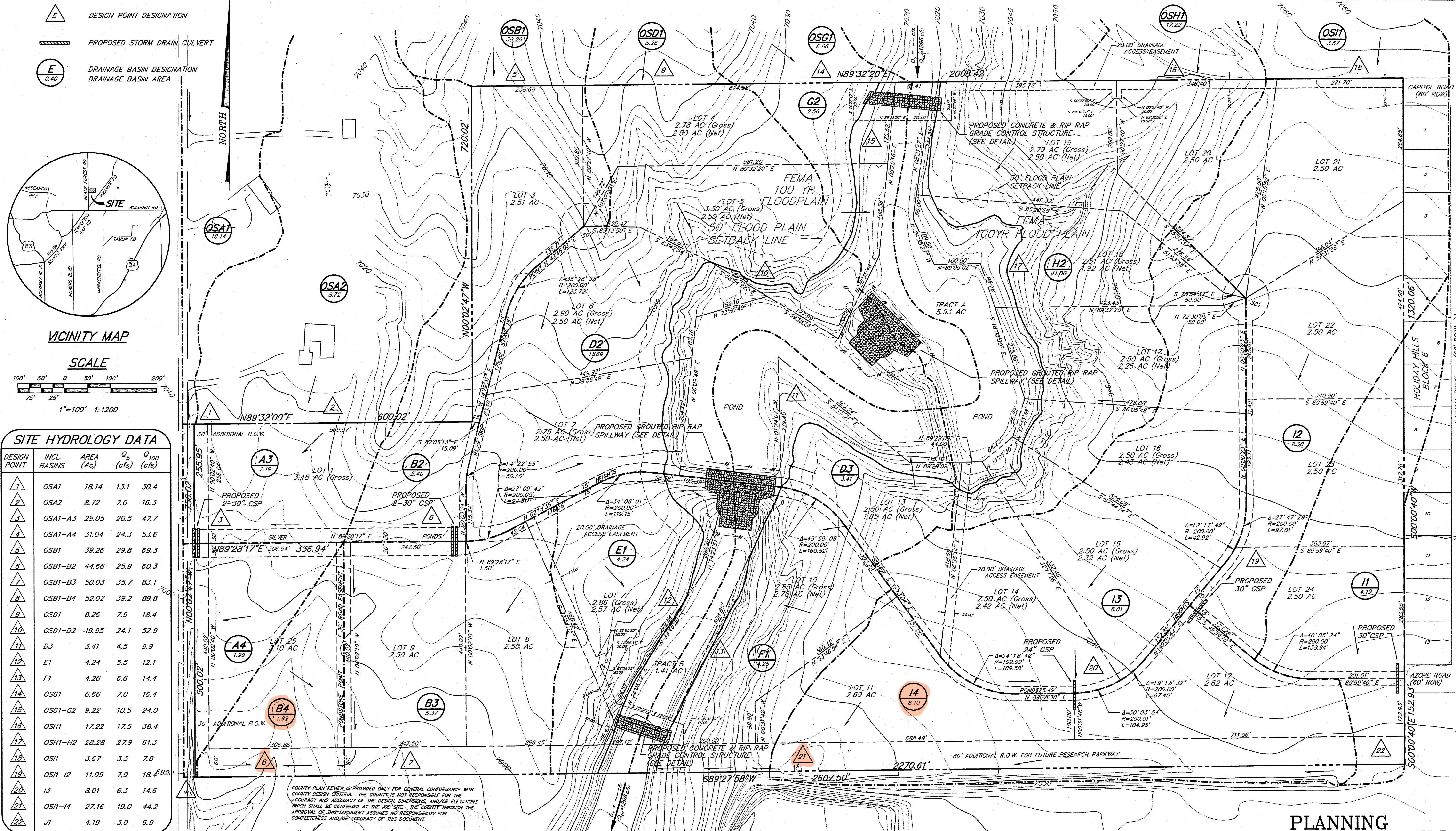
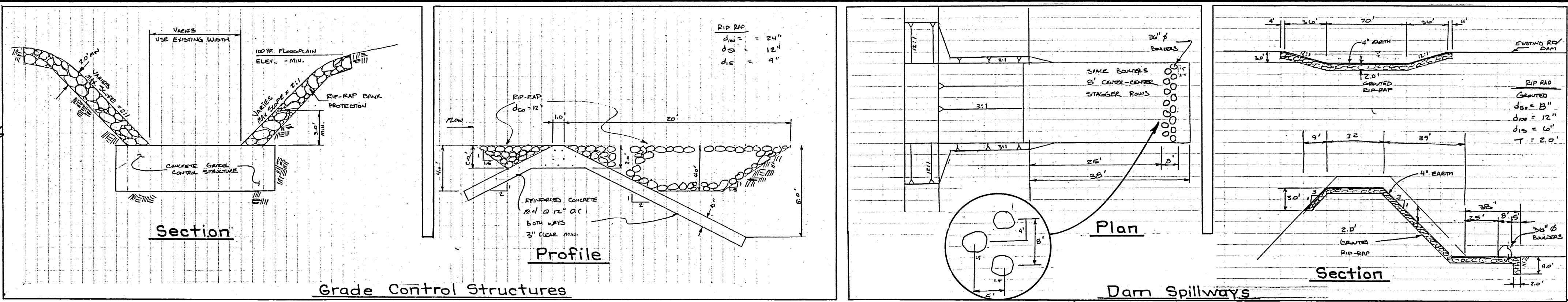
Design Point	Area (Ac)	C5	C100	Tc (min)	i5 (in/hr)	i100 (in/hr)	Q5 (cfs)	Q100 (cfs)
1	18.14	0.30	0.40	27.7	2.40	4.20	13.1	30.4
2	8.72	0.30	0.40	22.9	2.68	4.68	7.0	16.3
5	39.26	0.30	0.40	25.4	2.53	4.41	29.8	69.3
9	8.26	0.30	0.40	16.5	3.19	5.57	7.9	18.4
14	6.66	0.30	0.40	13.5	3.52	6.15	7.0	16.4
16	17.22	0.39	0.49	24.1	2.60	4.55	17.5	38.4
18	3.67	0.30	0.40	18.2	3.03	5.30	3.3	7.8
3	29.05	0.30	0.40	28.7	2.35	4.11	20.5	47.7
4	31.04	0.34	0.43	29.8	2.30	4.02	24.3	53.6
6	44.66	0.30	0.40	39.5	1.93	3.38	25.9	60.3
B3	5.37	0.30	0.40	26.7	2.45	4.29	4.0	9.2
7	50.03	0.30	0.40	28.2	2.38	4.15	35.7	83.1
8	52.02	0.32	0.42	28.7	2.35	4.11	39.2	89.8
D2	11.69	0.39	0.49	17.6	3.09	5.39	14.1	30.9
10	19.95	0.39	0.49	17.5	3.10	5.41	24.1	52.9
11	3.41	0.39	0.49	14.5	3.40	5.94	4.5	9.9
12	4.24	0.39	0.49	15.0	3.35	5.85	5.5	12.1
13	4.26	0.39	0.49	10.5	3.94	6.89	6.6	14.4
G2	2.56	0.39	0.49	13.1	3.57	6.24	3.6	7.8
15	9.22	0.33	0.43	14.0	3.46	6.04	10.5	24.0
H2	11.06	0.39	0.49	17.5	3.10	5.41	13.4	29.3
17	28.28	0.39	0.49	25.3	2.53	4.42	27.9	61.3
19	11.05	0.30	0.40	28.0	2.39	4.17	7.9	18.4
20	8.01	0.30	0.40	23.9	2.62	4.57	6.3	14.6
I4	8.10	0.30	0.40	23.1	2.67	4.66	6.5	15.1
21	27.16	0.30	0.40	29.2	2.33	4.07	19.0	44.2
22	4.19	0.30	0.40	28.8	2.35	4.10	3.0	6.9

LEGEND

- EXISTING INDEX CONTOUR
- EXISTING INTERMEDIATE CONTOUR
- DRAINAGE BASIN BOUNDARY LINE
- SUBDIVISION BOUNDARY LINE
- SILT FENCE
- DRAINAGE DIRECTION ARROW
- DESIGN POINT DESIGNATION
- PROPOSED STORM DRAIN CULVERT
- DRAINAGE BASIN DESIGNATION
- DRAINAGE BASIN AREA

THESE DETAILED PLANS AND SPECIFICATIONS WERE PREPARED UNDER MY DIRECTION AND SUPERVISION. SAID DETAILED PLANS AND SPECIFICATIONS HAVE BEEN PREPARED ACCORDING TO THE CRITERIA ESTABLISHED BY THE COUNTY FOR DETAILED PLANS AND SPECIFICATIONS, AND SAID DETAILED PLANS AND SPECIFICATIONS ARE IN CONFORMITY WITH THE MASTER PLAN OF THE DRAINAGE BASIN. SAID DETAILED DRAINAGE PLANS AND SPECIFICATIONS MEET THE PURPOSES FOR WHICH THE PARTICULAR DRAINAGE FACILITY IS DESIGNED. I ACCEPT RESPONSIBILITY FOR ANY LIABILITY CAUSED BY ANY NEGLIGENCE, ACTS, OMISSIONS OR ERRORS ON MY PART IN PREPARATION OF THE DETAILED DRAINAGE PLANS AND SPECIFICATIONS.

REGISTERED PROFESSIONAL ENGINEER
 CHARLES C. WALKER, P.E.
 LICENSE NO. 13348
 STATE OF COLORADO
 DATE: 5/9/96



SITE HYDROLOGY DATA

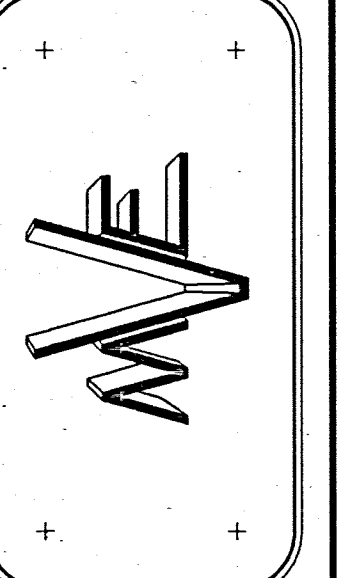
DESIGN POINT	INCL. BASINS	AREA (Ac)	Q ₅ (cfs)	Q ₁₀₀ (cfs)
1	OSA1	18.14	1.31	30.4
2	OSA2	8.72	7.0	16.3
3	OSA1-A3	29.05	20.5	47.7
4	OSA1-A4	31.04	24.3	53.6
5	OSB1	39.26	29.8	69.3
6	OSB1-B2	44.66	25.9	60.3
7	OSB1-B3	50.03	35.7	83.1
8	OSB1-B4	52.02	39.2	89.8
9	OSD1	8.26	7.9	18.4
10	OSD1-D2	19.95	24.1	52.9
11	D3	3.41	4.5	9.9
12	E1	4.24	5.5	12.1
13	F1	4.26	6.6	14.4
14	OSG1	6.66	7.0	16.4
15	OSG1-G2	9.22	10.5	24.0
16	OSH1	17.22	17.5	38.4
17	OSH1-H2	28.28	27.9	61.3
18	OSI1	3.67	3.3	7.8
19	OSI1-I2	11.05	7.9	18.4
20	I3	8.01	6.3	14.6
21	OSI1-I4	27.16	19.0	44.2
22	J1	4.19	3.0	6.9

COUNTY PLAN REVIEW IS PROVIDED ONLY FOR GENERAL CONFORMANCE WITH COUNTY DESIGN CRITERIA. THE COUNTY IS NOT RESPONSIBLE FOR THE ACCURACY AND ADEQUACY OF THE DESIGN, DIMENSIONS AND/OR ELEVATIONS WHICH SHALL BE CONFIRMED AT THE JOB SITE. THE COUNTY THROUGH THE APPROVAL OF THIS DOCUMENT ASSUMES NO RESPONSIBILITY FOR COMPLETENESS AND/OR ACCURACY OF THIS DOCUMENT.

Charles C. Walker, P.E. 5/9/96
 MURRAY D. STEWART, JR., P.E.
 COUNTY ENGINEER

NOTE: SEE OFFSITE DRAINAGE BASIN MAP FOR OFFSITE BASINS (OS...)

PROJECT: SILVER PONDS SUBDIVISION FILING NO. 1
 TITLE: DRAINAGE IMPROVEMENT DETAILS



MONUMENT VALLEY ENGINEERS INC.
 ENGINEERS • SURVEYORS
 1911 LELARAY STREET
 COLORADO SPRINGS, COLORADO 80909
 PHONE (719) 635-5736

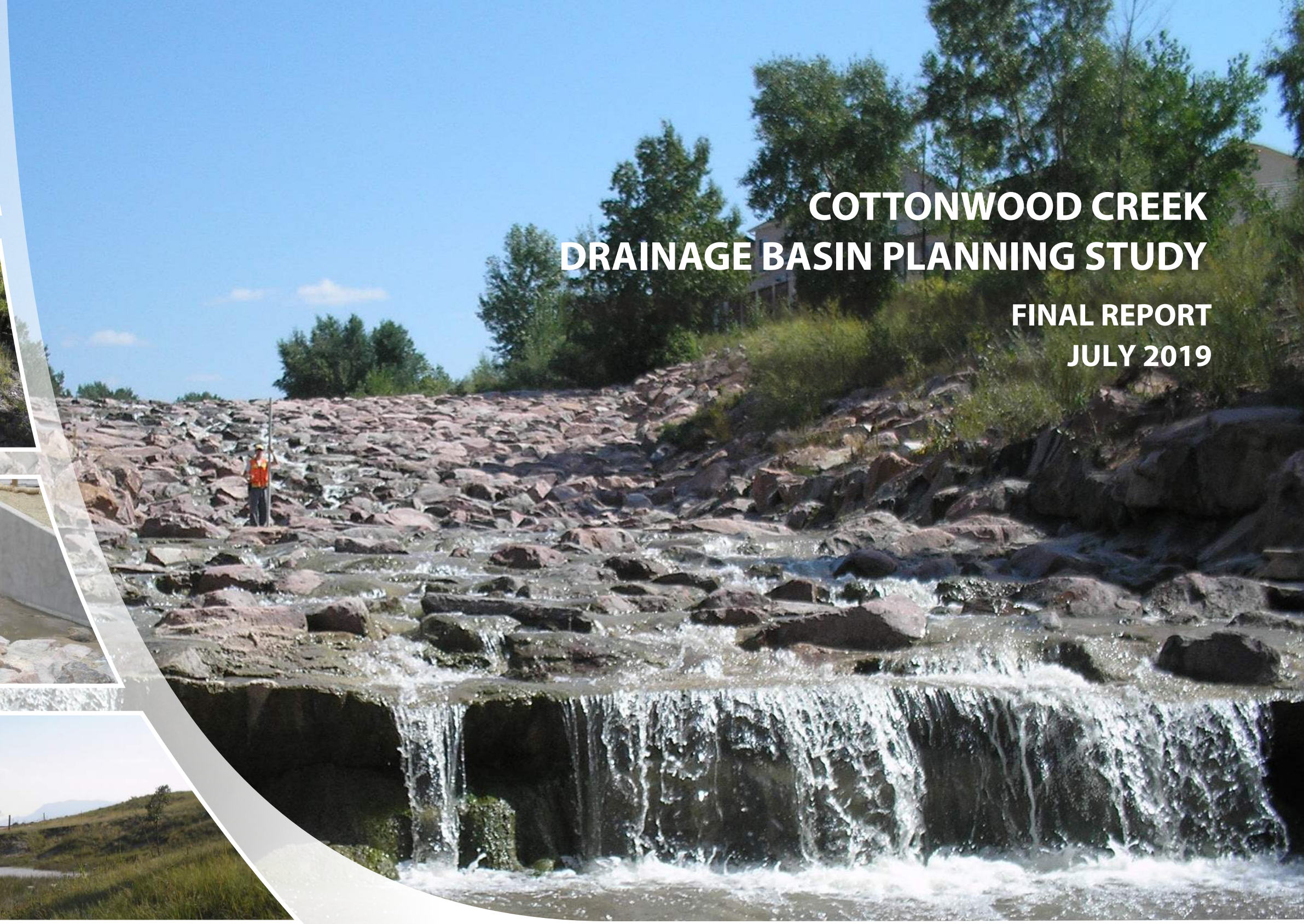
PROJ. NO. 60572
 DRAWN: DRG
 ENGINEER: DRG
 CHECKED: DRG
 SCALE: 1" = 100'
 DATE: 3/18/96
 REVISIONS: ITEM
 NO. DATE: 1 5/17/96 ADD
 COMMENTS: SILT FENCE
 & DETAIL

SHEET
 1 OF 1
 DRAWING NO.
60572008
 DISK NO. 1516

PLANNING
 KEVIN J. WALKER & ASSOCIATES
 105 EAST WENARD AVE., SUITE 800 COLORADO SPRINGS, CO 80903 (719) 473-8343

COTTONWOOD CREEK DRAINAGE BASIN PLANNING STUDY

FINAL REPORT
JULY 2019



Prepared for:

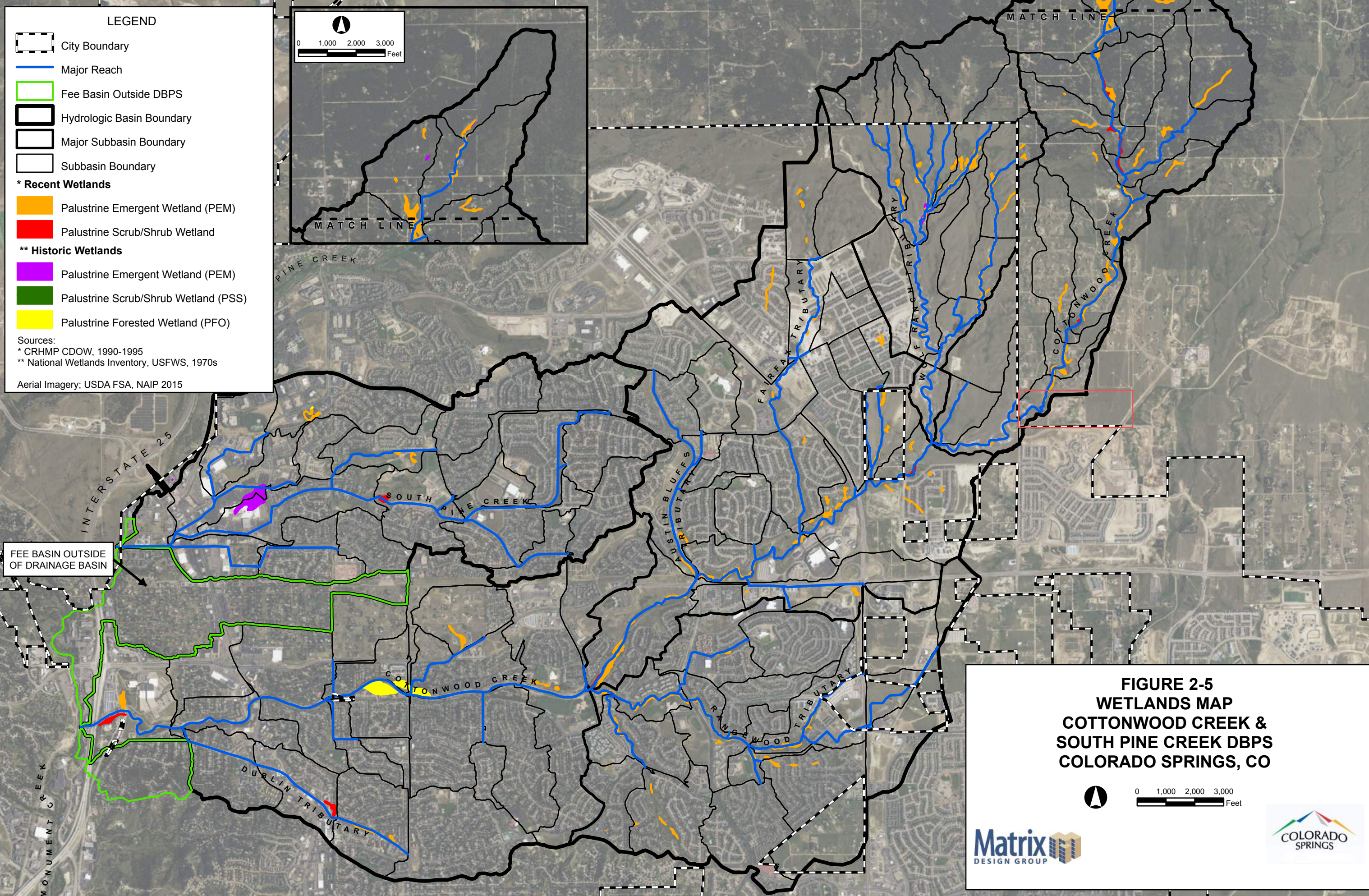


Department of Public Works
Water Resources Engineering

City of Colorado Springs
30 S. Nevada Ave
Colorado Springs, CO 80903

Prepared by:

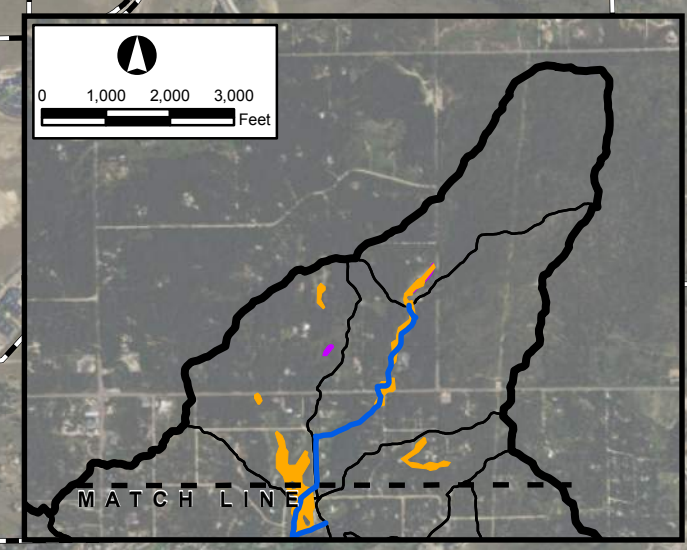




LEGEND

- City Boundary
- Major Reach
- Fee Basin Outside DBPS
- Hydrologic Basin Boundary
- Major Subbasin Boundary
- Subbasin Boundary
- * Recent Wetlands**
 - Palustrine Emergent Wetland (PEM)
 - Palustrine Scrub/Shrub Wetland
- ** Historic Wetlands**
 - Palustrine Emergent Wetland (PEM)
 - Palustrine Scrub/Shrub Wetland (PSS)
 - Palustrine Forested Wetland (PFO)

Sources:
 * CRHMP CDOW, 1990-1995
 ** National Wetlands Inventory, USFWS, 1970s
 Aerial Imagery; USDA FSA, NAIP 2015



FEE BASIN OUTSIDE OF DRAINAGE BASIN

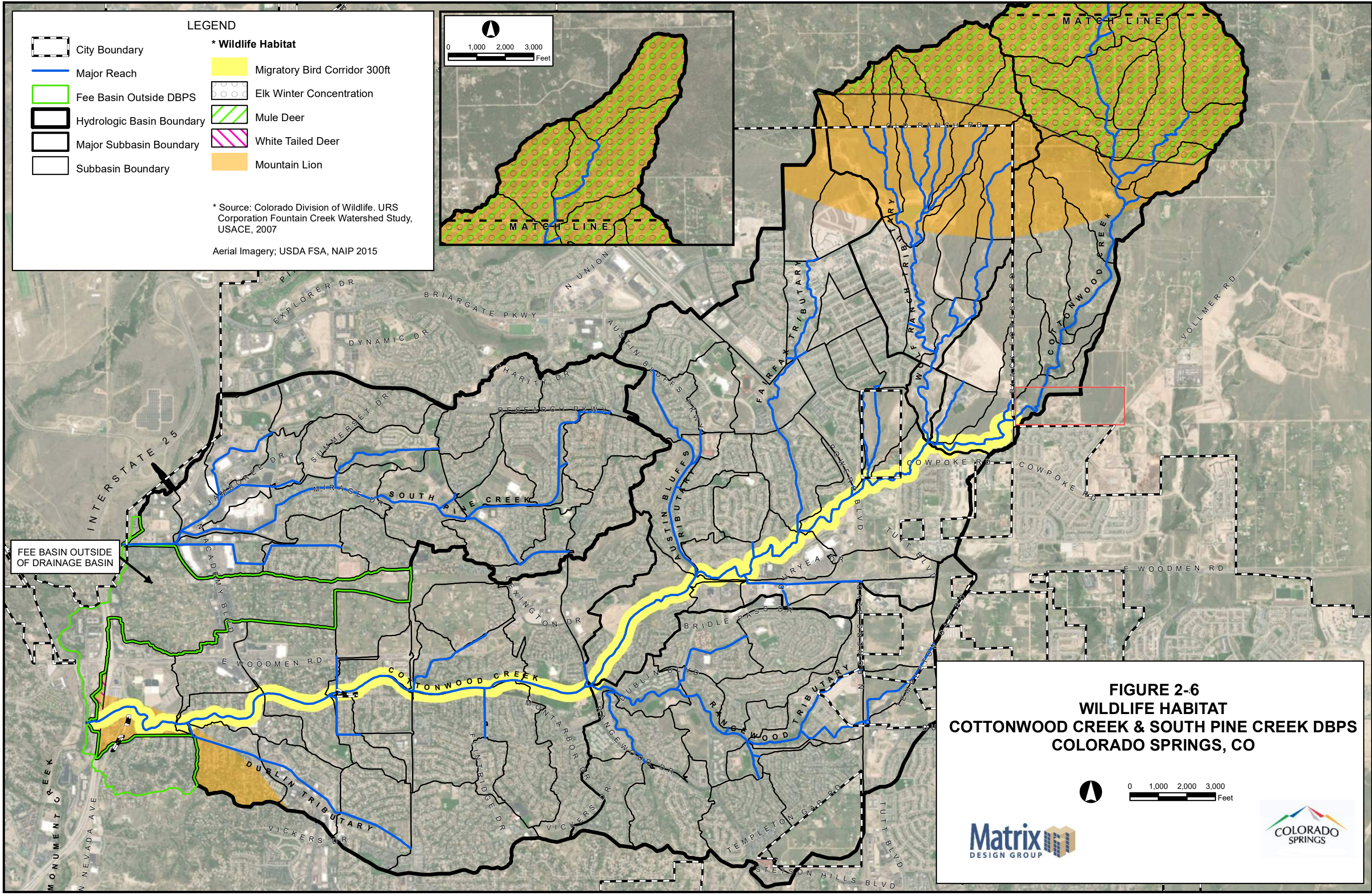
**FIGURE 2-5
 WETLANDS MAP
 COTTONWOOD CREEK &
 SOUTH PINE CREEK DBPS
 COLORADO SPRINGS, CO**

0 1,000 2,000 3,000 Feet

Matrix
 DESIGN GROUP

COLORADO SPRINGS

FILE: G:\projects\Cottonwood_Creek_DBPS_2017\updates\DBPS_Report\Figure_2_4_CottonwoodCreek_Wetlands_20171221.mxd, 12/21/2017, jrf_cmts

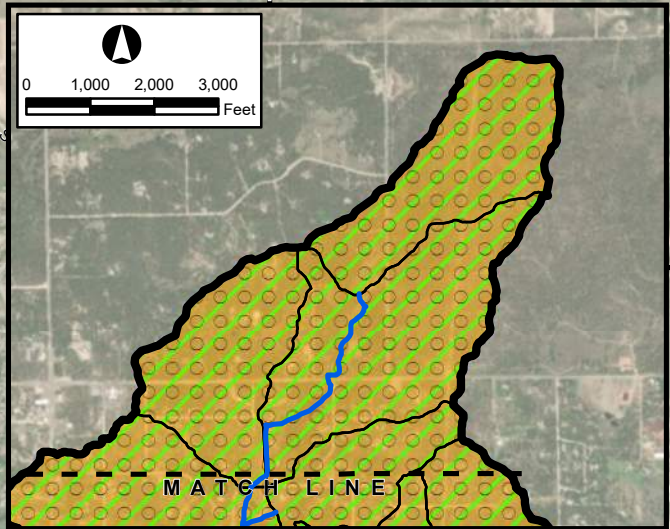


LEGEND

- City Boundary
- Major Reach
- Fee Basin Outside DBPS
- Hydrologic Basin Boundary
- Major Subbasin Boundary
- Subbasin Boundary
- * Wildlife Habitat
 - Migratory Bird Corridor 300ft
 - Elk Winter Concentration
 - Mule Deer
 - White Tailed Deer
 - Mountain Lion

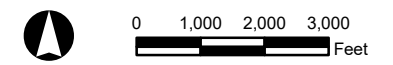
* Source: Colorado Division of Wildlife. URS Corporation Fountain Creek Watershed Study, USACE, 2007

Aerial Imagery; USDA FSA, NAIP 2015

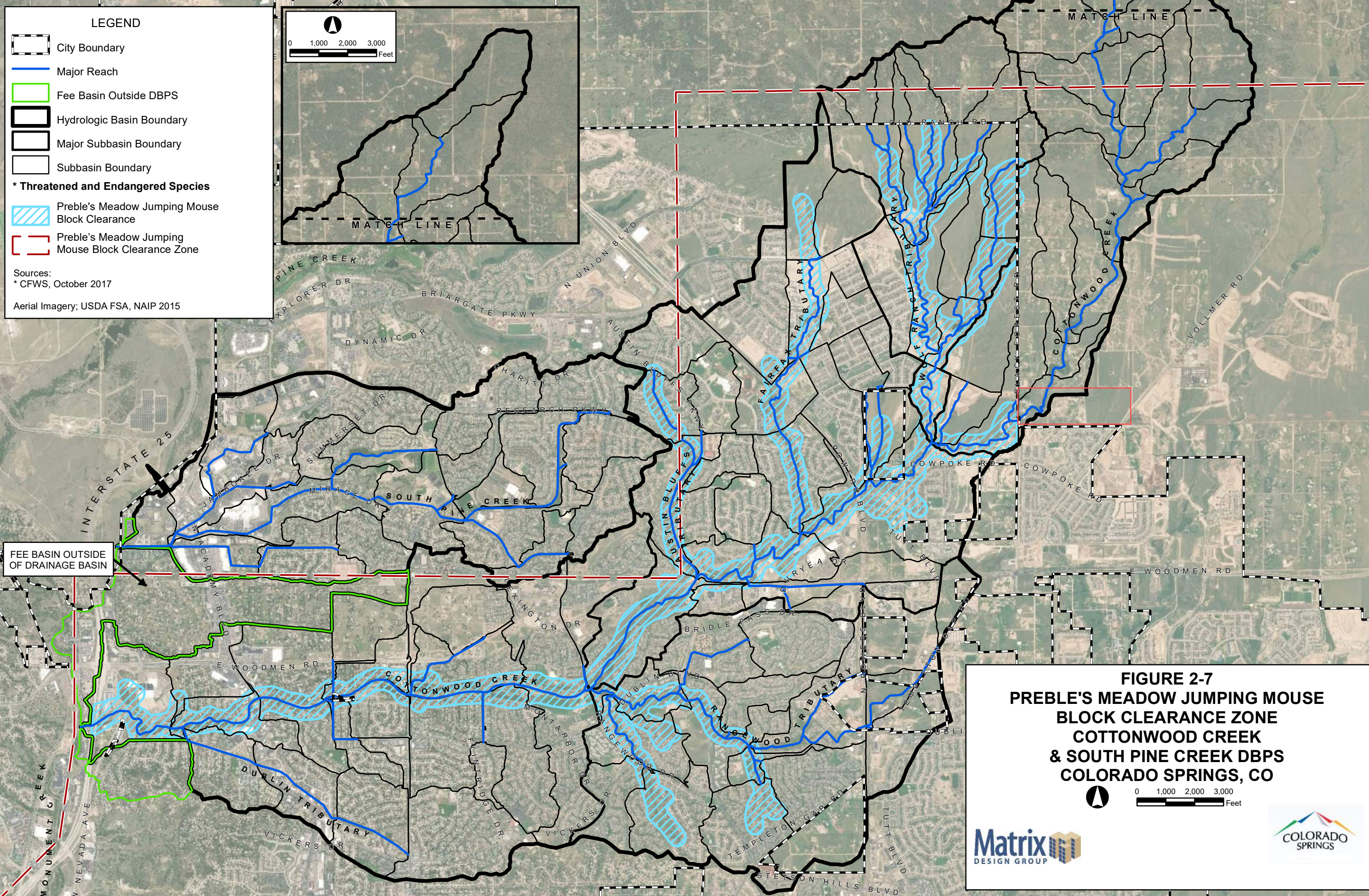


FEE BASIN OUTSIDE OF DRAINAGE BASIN

**FIGURE 2-6
WILDLIFE HABITAT
COTTONWOOD CREEK & SOUTH PINE CREEK DBPS
COLORADO SPRINGS, CO**



FILE: G:\p\proj\cottonwood_creek_dbps_2017\updates\DBPS_Report\Figure_2_6_CottonwoodCreek_Wildlife_and_Mig_Corridors_2019_07_01_DAP.mxd, 7/12/2019, Drew_Philips



LEGEND

- City Boundary
- Major Reach
- Fee Basin Outside DBPS
- Hydrologic Basin Boundary
- Major Subbasin Boundary
- Subbasin Boundary

*** Threatened and Endangered Species**

- Preble's Meadow Jumping Mouse Block Clearance
- Preble's Meadow Jumping Mouse Block Clearance Zone

Sources:
 * CFWS, October 2017
 Aerial Imagery; USDA FSA, NAIP 2015

FEE BASIN OUTSIDE OF DRAINAGE BASIN

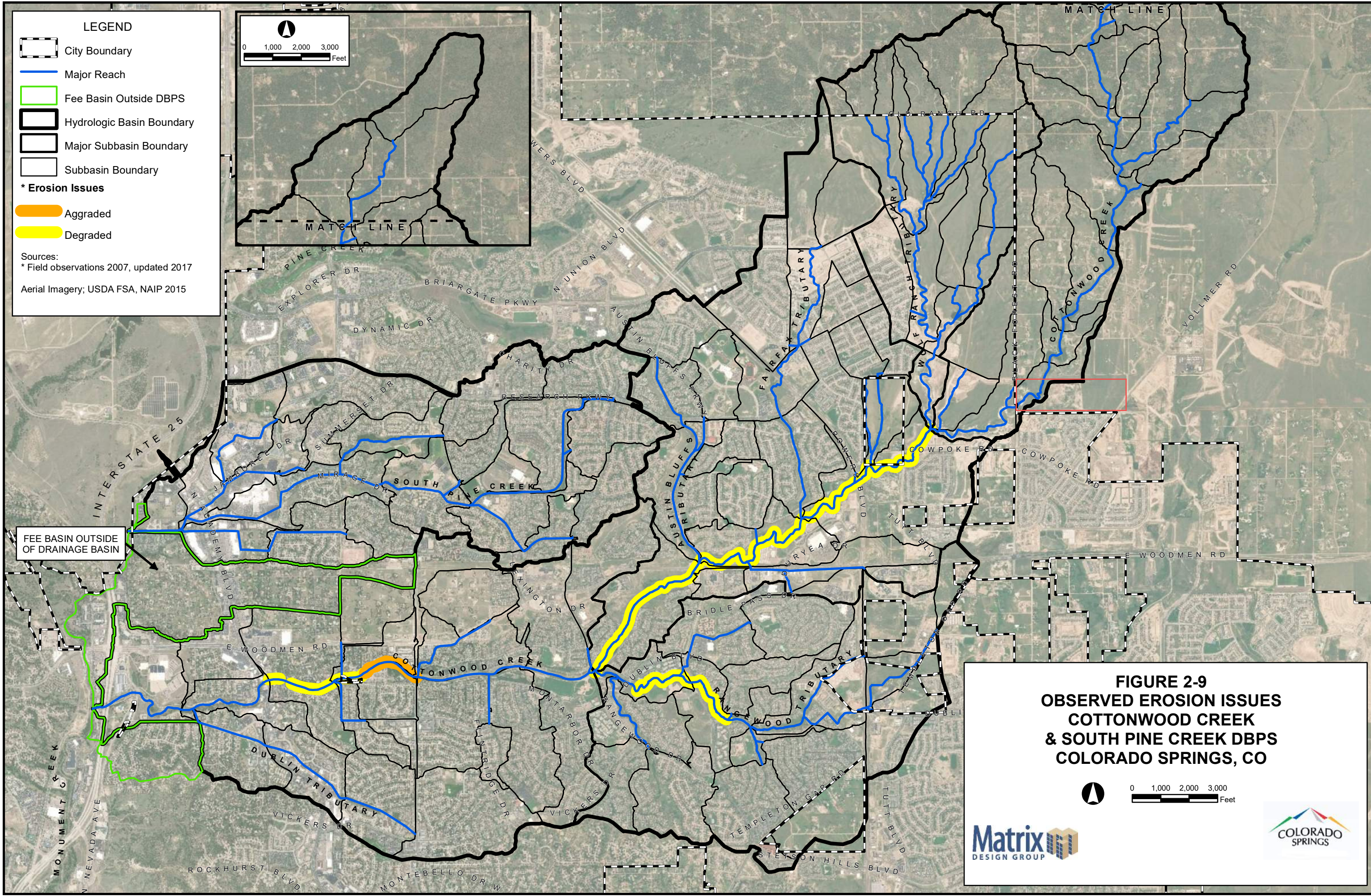
FIGURE 2-7
PREBLE'S MEADOW JUMPING MOUSE
BLOCK CLEARANCE ZONE
COTTONWOOD CREEK
& SOUTH PINE CREEK DBPS
COLORADO SPRINGS, CO

0 1,000 2,000 3,000 Feet

Matrix
 DESIGN GROUP

COLORADO
 SPRINGS

FILE: G:\p\p\projects\Cottonwood_Creek_DBPS_2017\ac\slaps\DBPS_Report\Fig_2_4_CottonwoodCreek_TE_Species_20171221.mxd, 5/30/2018, Drew_Phillips



LEGEND

- City Boundary
- Major Reach
- Fee Basin Outside DBPS
- Hydrologic Basin Boundary
- Major Subbasin Boundary
- Subbasin Boundary
- * Erosion Issues**
- Aggraded
- Degraded

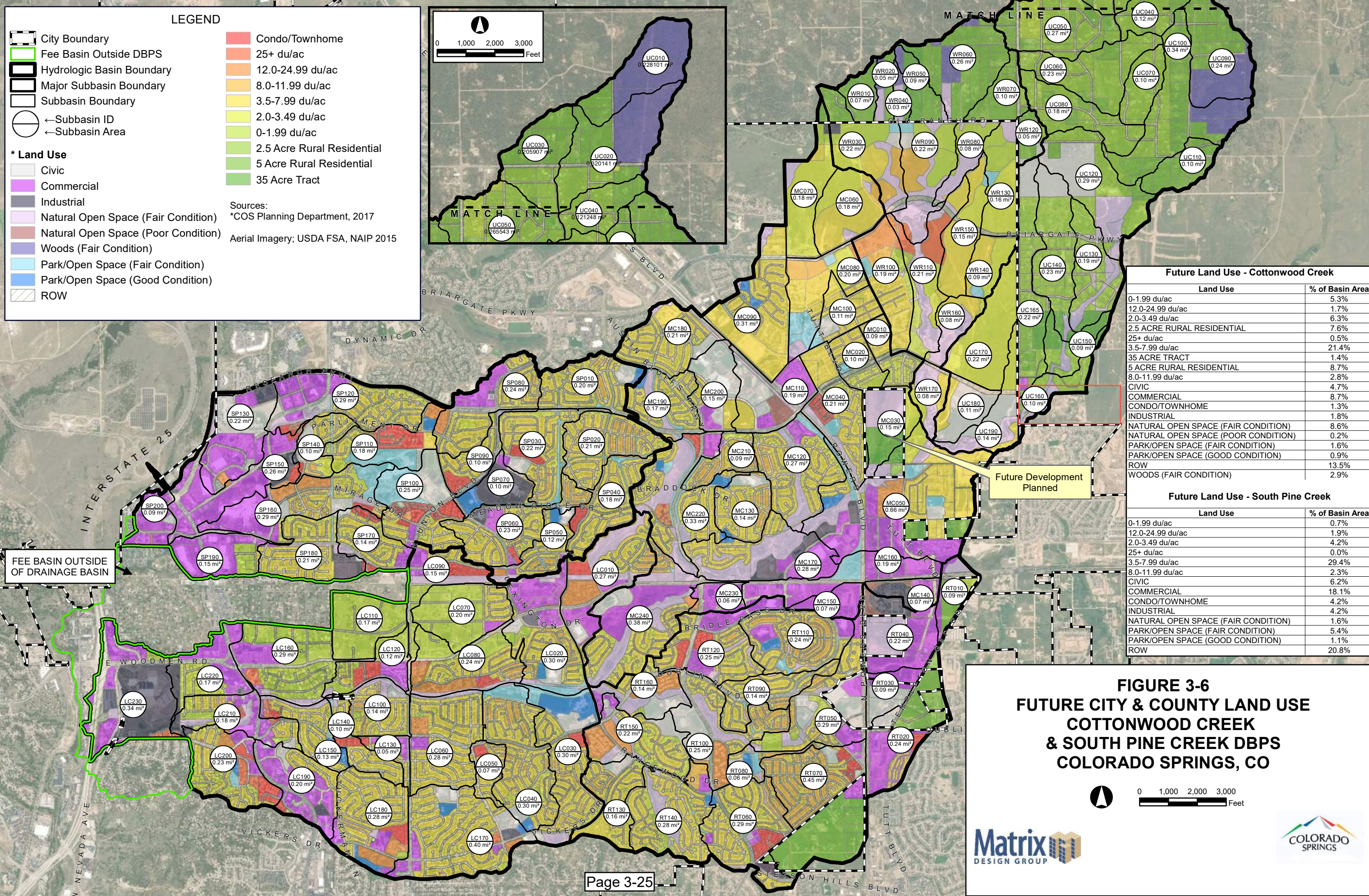
Sources:
 * Field observations 2007, updated 2017
 Aerial Imagery; USDA FSA, NAIP 2015

FEE BASIN OUTSIDE OF DRAINAGE BASIN

**FIGURE 2-9
 OBSERVED EROSION ISSUES
 COTTONWOOD CREEK
 & SOUTH PINE CREEK DBPS
 COLORADO SPRINGS, CO**

Matrix
 DESIGN GROUP

FILE: G:\p\proj\cottonwood_creek_dbps_2017\cottonwood_dbps_report\fig_2_9_cottonwood_creek_erosion_issues_20190530.mxd, 5/30/2019, Drew Phillips



LEGEND

- City Boundary
- Fee Basin Outside DBPS
- Hydrologic Basin Boundary
- Major Subbasin Boundary
- Subbasin Boundary
- ← Subbasin ID
- ← Subbasin Area

*** Land Use**

- Civic
- Commercial
- Industrial
- Natural Open Space (Fair Condition)
- Natural Open Space (Poor Condition)
- Woods (Fair Condition)
- Park/Open Space (Fair Condition)
- Park/Open Space (Good Condition)
- ROW

Land Use Density

- Condo/Townhome
- 25+ du/ac
- 12.0-24.99 du/ac
- 8.0-11.99 du/ac
- 3.5-7.99 du/ac
- 2.0-3.49 du/ac
- 0-1.99 du/ac
- 2.5 Acre Rural Residential
- 5 Acre Rural Residential
- 35 Acre Tract

Sources:
 *COS Planning Department, 2017
 Aerial Imagery; USDA FSA, NAIP 2015

Future Land Use - Cottonwood Creek

Land Use	% of Basin Area
0-1.99 du/ac	5.3%
12.0-24.99 du/ac	1.7%
2.0-3.49 du/ac	6.3%
2.5 ACRE RURAL RESIDENTIAL	7.6%
25+ du/ac	0.5%
3.5-7.99 du/ac	21.4%
35 ACRE TRACT	1.4%
5 ACRE RURAL RESIDENTIAL	8.7%
8.0-11.99 du/ac	2.8%
CIVIC	4.7%
COMMERCIAL	8.7%
CONDO/TOWNHOME	1.3%
INDUSTRIAL	1.8%
NATURAL OPEN SPACE (FAIR CONDITION)	8.6%
NATURAL OPEN SPACE (POOR CONDITION)	0.2%
PARK/OPEN SPACE (FAIR CONDITION)	1.6%
PARK/OPEN SPACE (GOOD CONDITION)	0.9%
ROW	13.5%
WOODS (FAIR CONDITION)	2.9%

Future Land Use - South Pine Creek

Land Use	% of Basin Area
0-1.99 du/ac	0.7%
12.0-24.99 du/ac	1.9%
2.0-3.49 du/ac	4.2%
25+ du/ac	0.0%
3.5-7.99 du/ac	29.4%
8.0-11.99 du/ac	2.3%
CIVIC	6.2%
COMMERCIAL	18.1%
CONDO/TOWNHOME	4.2%
INDUSTRIAL	4.2%
NATURAL OPEN SPACE (FAIR CONDITION)	1.6%
PARK/OPEN SPACE (FAIR CONDITION)	5.4%
PARK/OPEN SPACE (GOOD CONDITION)	1.1%
ROW	20.8%

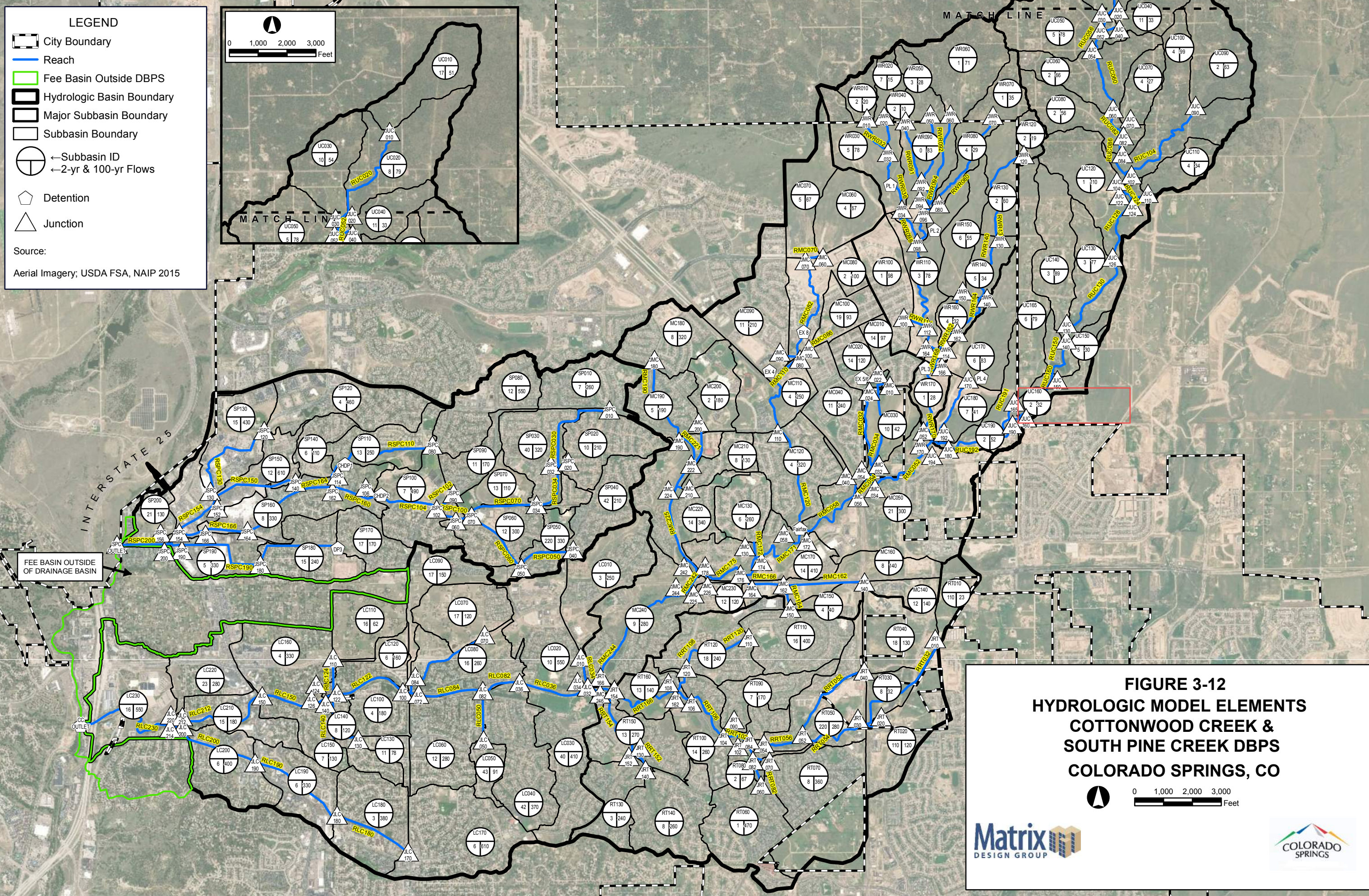
FIGURE 3-6
FUTURE CITY & COUNTY LAND USE
COTTONWOOD CREEK
& SOUTH PINE CREEK DBPS
COLORADO SPRINGS, CO

0 1,000 2,000 3,000 Feet

Matrix
DESIGN GROUP

COLORADO SPRINGS

FILE: G:\gis_projects\Cottonwood_Creek_DBPs_2017\active\MapDBPs_Report\Figure_3_6_CottonwoodCreek_Land_Use_Future_20190530.mxd, 5/30/2019, Drew_Phillips



LEGEND

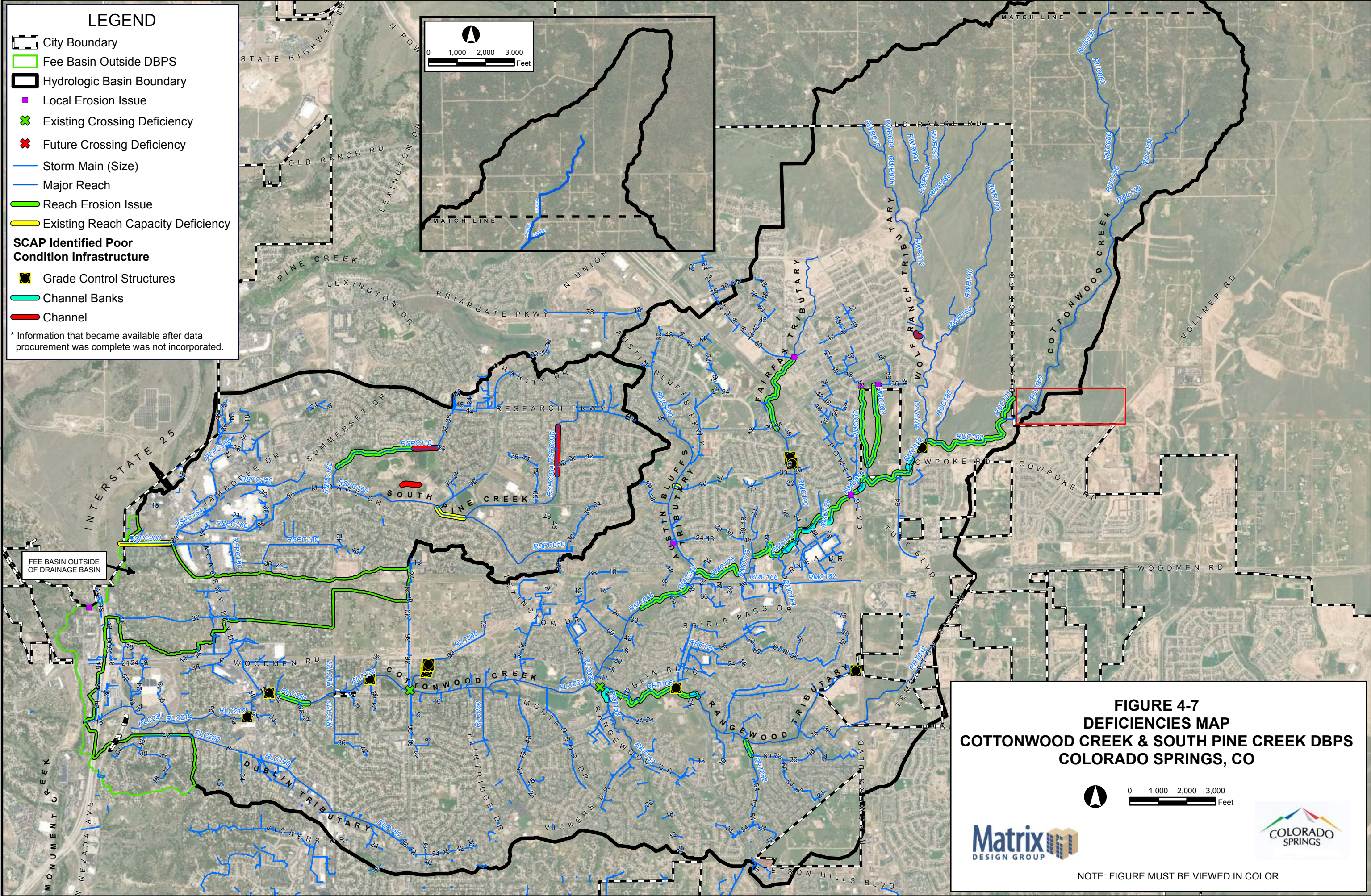
- City Boundary
- Reach
- Fee Basin Outside DBPS
- Hydrologic Basin Boundary
- Major Subbasin Boundary
- Subbasin Boundary
- ← Subbasin ID
- ← 2-yr & 100-yr Flows
- Detention
- Junction

Source:
Aerial Imagery; USDA FSA, NAIP 2015

FIGURE 3-12
HYDROLOGIC MODEL ELEMENTS
COTTONWOOD CREEK &
SOUTH PINE CREEK DBPs
COLORADO SPRINGS, CO

0 1,000 2,000 3,000 Feet

FILE: G:\projects\Cottonwood_Creek_DBPs_2017\active\maps\DBPs_Report\Figure_3_12_CottonwoodCreek_Hydrology_Existing_20180226.mxd, 6/29/2018, jmf_sonts



LEGEND

- City Boundary
- Fee Basin Outside DBPS
- Hydrologic Basin Boundary
- Local Erosion Issue
- Existing Crossing Deficiency
- Future Crossing Deficiency
- Storm Main (Size)
- Major Reach
- Reach Erosion Issue
- Existing Reach Capacity Deficiency

SCAP Identified Poor Condition Infrastructure

- Grade Control Structures
- Channel Banks
- Channel

* Information that became available after data procurement was complete was not incorporated.

FIGURE 4-7 DEFICIENCIES MAP COTTONWOOD CREEK & SOUTH PINE CREEK DBPS COLORADO SPRINGS, CO

Matrix
DESIGN GROUP

COLORADO SPRINGS

NOTE: FIGURE MUST BE VIEWED IN COLOR

FILE G:\gis_projects\Cottonwood_Creek_DBPS_2017\active\map\DBPS_Report\Figure_4-7_CottonwoodCreek_Deficiencies.mxd, 4/11/2019, jpf, docx



SAND CREEK DRAINAGE BASIN PLANNING STUDY FINAL REPORT JANUARY 2021

Prepared for:

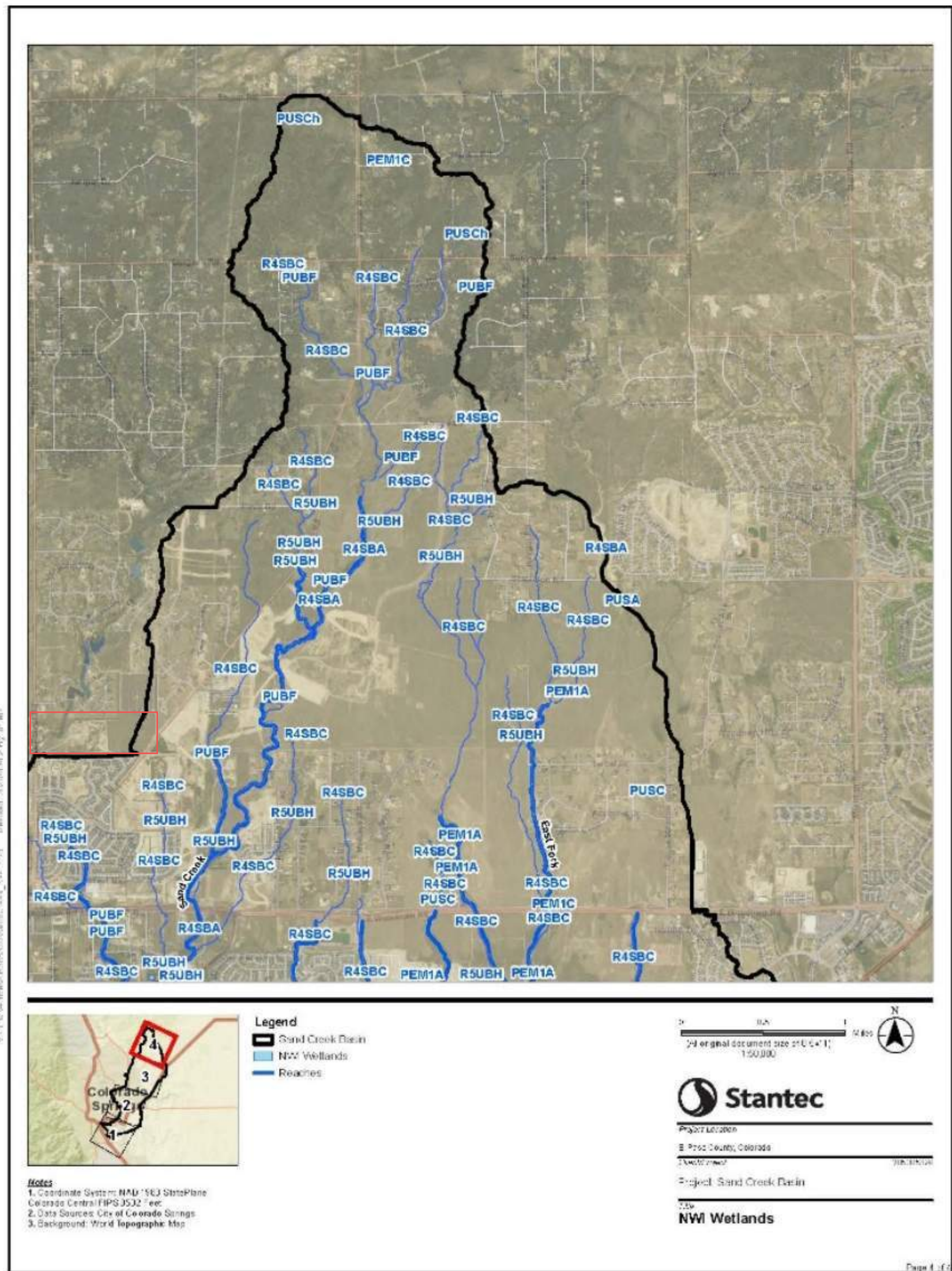


Prepared by:



SAND CREEK – SAND CREEK DRAINAGE BASIN PLANNING STUDY

Basin Characteristics and Environmental Resources



Disclaimer: This document has been prepared based on information provided by others as cited in the Notes section. Stantec has not verified the accuracy and/or completeness of this information and shall not be responsible for any errors or omissions which may be incorporated herein as a result. Stantec assumes no responsibility for data supplied in electronic format, and the recipient accepts full responsibility for verifying the accuracy and completeness of the data.

Figure 2-7: NWI Wetlands Located in Sand Creek Drainage Basin (Page 4)

Hydrology

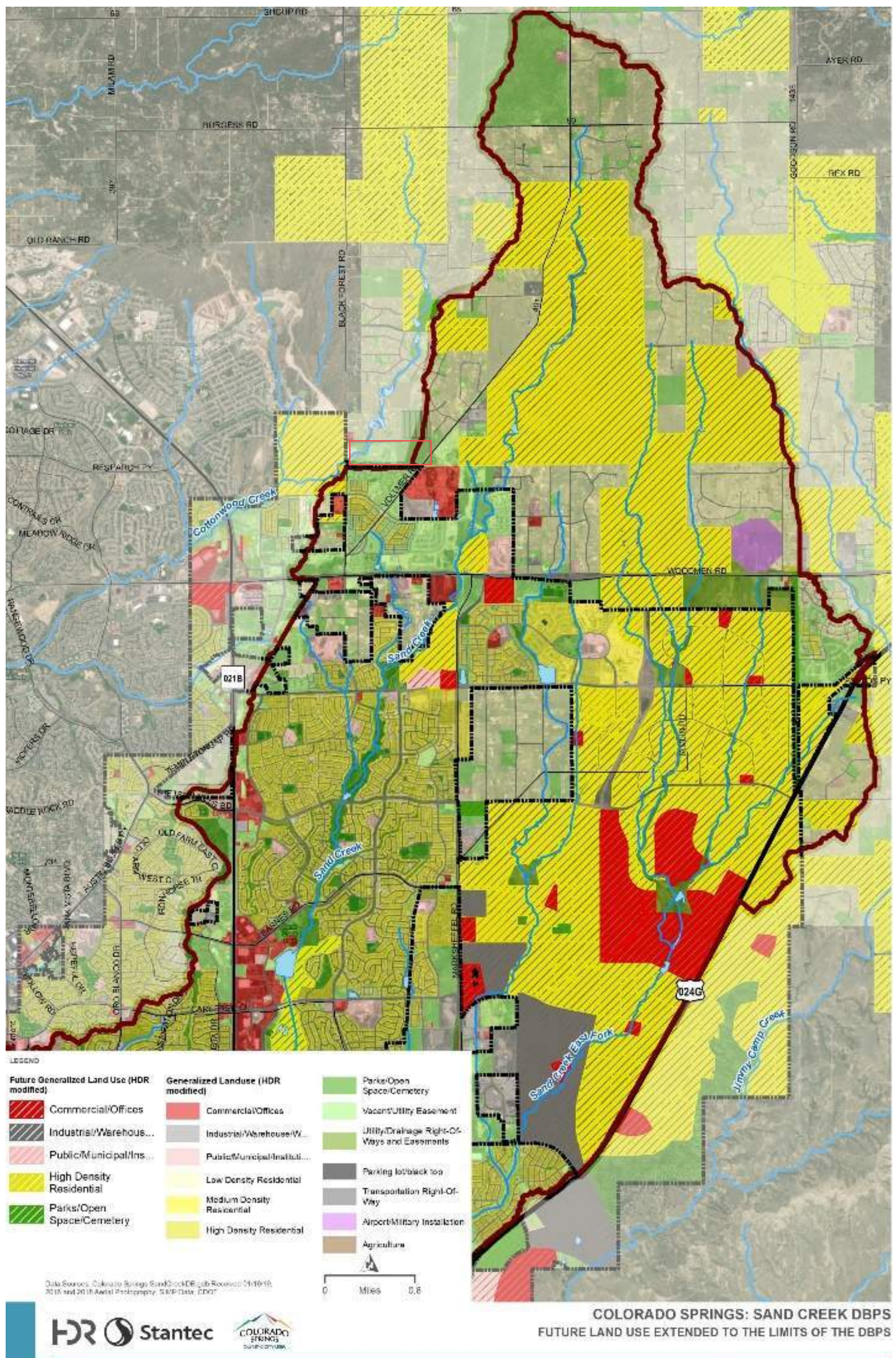
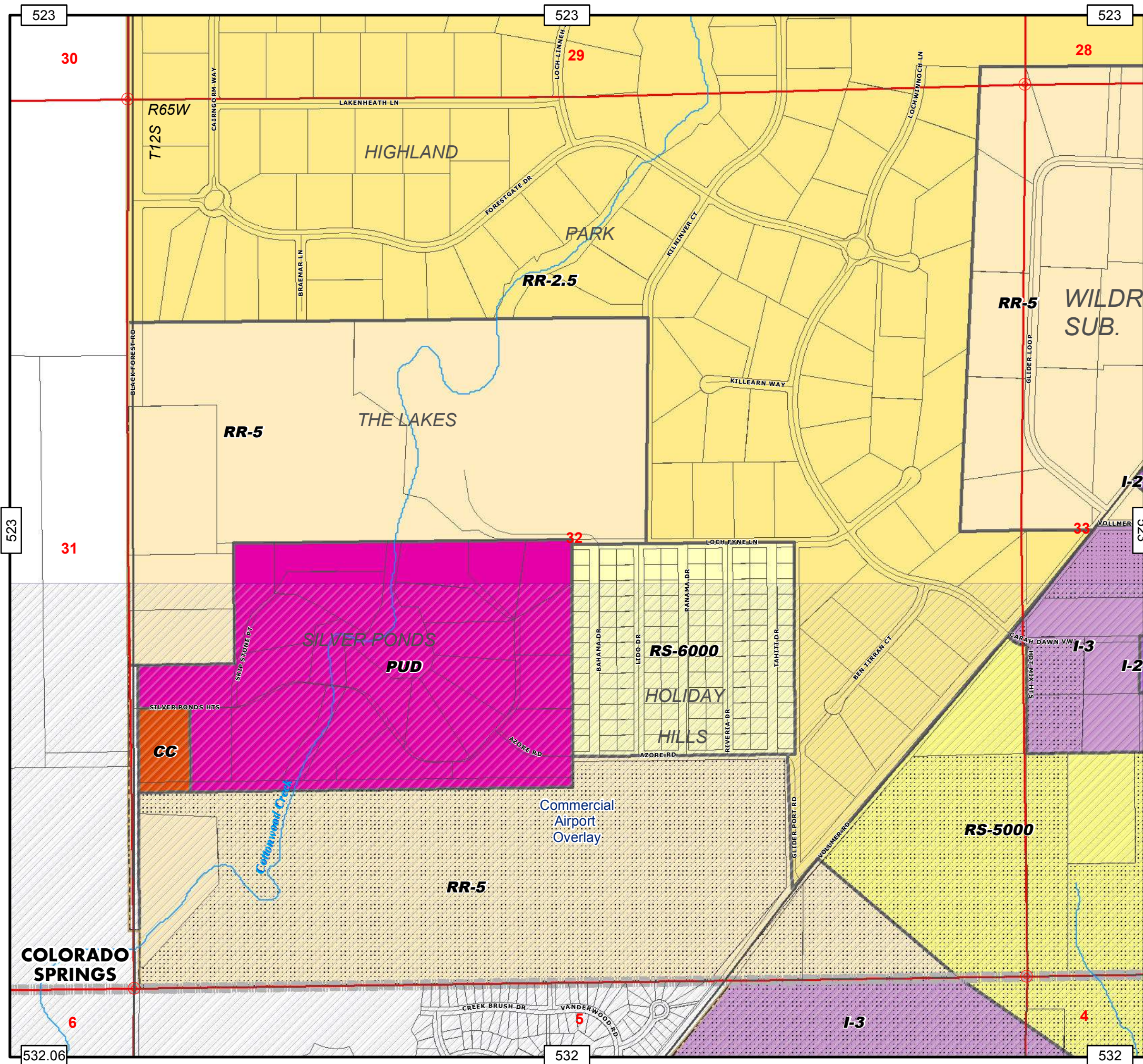


Figure 3-15. Future Land Use Map Future Condition Model Results



Zone Map 523.32

- El Paso County -
Development Services Department

Zoning Designations

	RS-20000: Residential Suburban (20,000 sq. ft.)		F-5: Forest & Recreation (5 acres)
	RS-6000: Residential Suburban (6,000 sq. ft.)		PUD: Planned Unit Development
	RS-5000: Residential Suburban (5,000 sq. ft.)		CC: Commercial Community
	RM-12: Residential Multi-Dwelling (12 DU/acre)		CR: Commercial Regional
	RM-30: Residential Multi-Dwelling (30 DU/acre)		CS: Commercial Service
	RR-0.5: Residential Rural (0.5 acres)		I-2: Limited Industrial
	RR-2.5: Residential Rural (2.5 acres)		I-3: Heavy Industrial
	RR-5: Residential Rural (5 acres)		A-5: Agricultural (5 acres)
	R-T: Residential - Topographic		A-35: Agricultural (35 acres)
	MHP: Mobile Home Park		C-1: ** Commercial
	MHP-R: Mobile Home Park, Rural		C-2: ** Commercial
	MHS: Mobile Home Subdivision		M: ** Industrial
	RVP: Recreational Vehicle Park		R-4: ** Planned Development

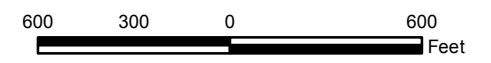
** Indicates an obsolete designation

Supporting Data

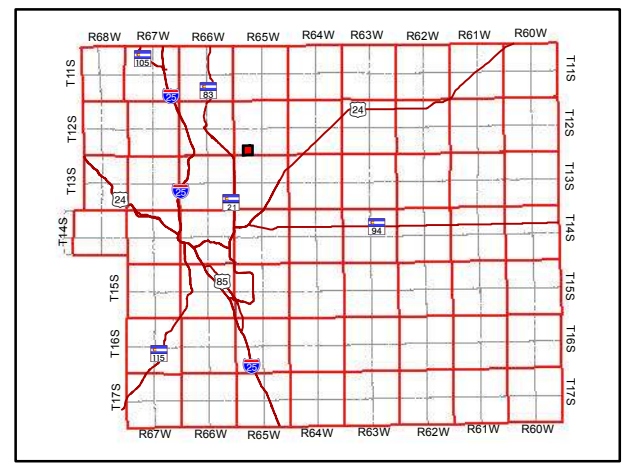
	Highways		Sections		Incorporated Cities
	Major Roadways		Parcels		Zone Map Boundary
	Creeks - Perennial		Military		Zoning Overlay
	Creeks - Intermittent		Pike National Forest		Special Uses
	Section Corner Nodes				



May 25, 2016



Vicinity Map



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TRAILS AT FOREST MEADOWS FILING NO. 3 FINAL DRAINAGE REPORT

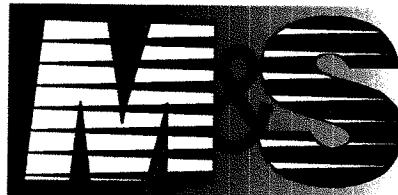
**AMENDMENT TO:
MASTER DEVELOPMENT DRAINAGE PLAN UPDATE FOR WOODMEN HEIGHTS
AND FINAL DRAINAGE REPORT FOR FOREST MEADOWS FILING NO.1 AND NO.4**

August 2015

Prepared for:

Rivers Development, Inc.
13530 Northgate Estates Drive, Suite 200
Colorado Springs, CO 80921

Prepared by:



CIVIL CONSULTANTS, INC.
20 Boulder Crescent, Suite 110
Colorado Springs, CO 80903
(719) 955-5485

Project #08-029

OFFICE COPY

ranges from 12 to 14 inches per year, with the majority of this moisture occurring in the spring and summer in the form of rainfall. Thunderstorms are common during the summer months.

FLOODPLAIN STATEMENT

According to the Federal Emergency Management Agency (FEMA) Flood Insurance Rate Map (FIRM) Panel No. 08041C0529, effective date March 17, 1997, no portion of the site lies within a designated floodplain.

DRAINAGE CRITERIA

The drainage analysis has been prepared in accordance with the current City of Colorado Springs/E Paso County Drainage Criteria Manual. Calculations were performed to determine runoff quantities during the 5-year and 100-year frequency storms for developed conditions using the Rational Method as required for basins having areas less than 100 acres.

EXISTING DRAINAGE CONDITIONS

The overall site consists of 18.172 acres and is currently undeveloped, with the initial grading project proposed to disturb 18.172 acres for Filing No. 3 residential subdivision. Filing No.3 proposes 87 single family residential lots. The number of lots to be platted in the future filings to the west is unknown at this time. All of the streets, curb, gutter, sidewalk and utilities for the development of Vanderwood Road, Cedar Brush Court, Brush Top Road, and Creek Brush Drive, will be constructed in Filing No. 3 Vanderwood Road will be extended in the future filings of Trails at Forest Meadows.

As shown by the historic drainage map for "Trails at Forest Meadows Filing 2", included in the appendix, offsite historic flows, tributary to Vollmer (EX1 ~ Q5=66 cfs and Q100=300.7 cfs, EX2 ~ Q5=23 cfs and Q100=106 cfs, and EX3 ~ Q5=1.8 cfs and Q100=8.0 cfs, see Historic drainage map DP-1), have been estimated to reach proposed Vollmer Road infrastructure at the Dry Needle Place/Vollmer Road intersection and northerly boundary of Filing No. 2. It has been determined that due to limited roadside capacity along the West side of Vollmer Roadway much of this historic runoff may cross Vollmer prior to reaching DP3 (see proposed Drainage Conditions for addition discussion). No new developed flow will be introduced onto Vollmer Road, north of the intersection. Any new developed flows, south of the intersection, will be intercepted by 2-20' D-10-R inlets within the proposed Vollmer Road Section. It should be noted that upon the construction of the Sterling Ranch subdivision a large percentage of the historic flows, once reaching the subject site (north and west of Vollmer Road/ future Marksheffel Road) will be collected and conveyed in a proposed 54" RCP to Sand Creek.

Per review of the existing topographic drainage patterns, the off-site historic flows, north of the property (OS1, see Historic drainage map DP-1), are conveyed west by an existing berm and swale to an existing gravel borrow pit, as evident by the eroded embankment at the southeast corner of the gravel borrow pit and evaluation of grade during onsite visits. Per the "Master Development Drainage Plan for Woodmen Heights Master Plan" prepared by Classic Consulting Engineers and Surveyors, dated June 2004, it was inferred that the entire watershed (historic flows of Q5=65 cfs and Q100=162 cfs) would be transported to the future detention facility through our site. This report was amended by the "Master Development Drainage Plan, Update for Woodmen Heights and Final Drainage Report for Forest Meadows Filing No.1 and No. 4" (MDDP) by Engineering and Surveying, Inc., dated February 2006, in which it states that 50% of the flow from OS1 (Q5=34 cfs, Q100=84 cfs) will be collected by a proposed concrete pipe and will be conveyed through and combined with the flows of Trails at Forest Meadows Filings to Sand Creek Regional Detention Facility No. 6. Per historic drainage patterns and per the "Preliminary/Final Drainage Report for Highland Park Filing No.2", prepared by Law and Mariotti Consultants, dated June 2002, the remainder of the flows will be transported via road side swale on the west side of Vollmer Road to the proposed drainage infrastructure in Vollmer Road. Any increase in flows due to future development of

Basin OS1 will require the construction of a proposed detention facility, as per the Sand Creek DBPS. Historic flows (EX4-Q5=5.1 cfs and Q100=22.9 cfs, see Historic drainage map DP-1) south of OS1, sheet flow to an existing abandoned road swale and outlet to a roadside swale on Black Forest Road. There are road side swales on either side of the abandoned road. Since topographic drainage patterns have been altered since the approval of the MDDP, existing historic flows have been diverted to the gravel borrow pit, Vollmer Road and Black Forest Road.

The site is tributary to Sand Creek Detention Basin No. 6. The stormwater infrastructure downstream of the subject site has already been constructed to the aforementioned detention pond. Specifically, flows initially intercepted at Design Point E3 are conveyed within the Vollmer Road Storm Sewer System which parallels the west side of Vollmer prior to out-falling (at the East Side of Vollmer Road) into a partially riprap lined channel. The existing channel, which parallels both the southwest and western edge of Forest Meadows Filing No. 1, directs runoff under Forest Meadows Avenue and into the existing Sand Creek Detention Pond No. 6. A rip rap plunge pool and energy dissipater aid to slow the incoming flows while the receiving facility provides both WQCV and detention for this development.

The site was originally studied in the "Sand Creek Drainage Basin Planning Study Preliminary Design Report" (DBPS) prepared by Kiowa Engineering. This study was then updated in the "Sand Creek Drainage Basin Planning Study Preliminary Design Report Technical Addendum" by Kiowa, revised October 1995.

It should be noted that the subject site was most currently studied in the "Master Development Drainage Plan Update for Woodmen Heights and Final Drainage Report for Forest Meadows Filing No. 1 and No. 4, where the proposed land use had been revised to single-family residential development from previously planned commercial usage.

PROPOSED DRAINAGE CONDITIONS

The following is a description of the onsite basins, offsite bypass flows and the overall proposed drainage characteristics for the development of Trails at Forest Meadows Filing No.3. The following Design Points and Basins were determined using the Rational Method since each individual basin is less than 100 acres and the combined acreage at any Design Point is also less than 100 acres. This method offers a more conservative approach to calculating swale cross sections and storm drain. The proposed drainage design for this subdivision is typical for single family residential, consisting of; homes, landscaping, rear and side lot drainage swales, curb & gutter, streets, curb inlets, and pipes to convey developed flows downstream. Rear and side lot swales will be constructed to get developed flows to street curb and gutter.

Filing No.2 - Basins F2-F, F2-I and F2-J are located to the south of the subject site, in the central and east portions of the Filing 2 site. The flows from these basins were previously analyzed as part of "The Trails at Forest Meadows Filing No. 2 Preliminary/Final Drainage Report" (FDR2). Runoff produced within Basins F2-F, F2-I and F2-J flow to existing inlets in the Trails at Forest Meadows Filing No. 2 subdivision and have been accounted for.

Basin K is located in the northerly portion of the site and contains 0.92 acres of portions of single family residential lots and streets. Basin K has proposed design flows of 1.8 cfs for the minor storm event (5-Year) and 3.9 cfs for the major storm event (100-Year). Runoff from Basin K will flow, overland via side lot swales, to the curb and gutter of existing streets within Basin F2-F (Filing No. 2) to Design Point 1 (6.1 cfs/12.8 cfs), an existing 12' D-10-R inlet in a sump condition. See FDR2 Basin F for pipe conveyance information and over flow conditions. Pipe 2 and 3 have been sized to accept these developed flows and do not exceed the pipe design flows in FDR2.

Basin L is located in the northerly portion of the site and contains 0.55 acres of rear yards of single family residential lots. Basin L has proposed design flows of 1.2 cfs for the minor storm event (5-Year) and 2.5 cfs for the major storm event (100-Year). Runoff from Basin L will flow, overland, to lots and tracts within Basin F2-J (Filing No. 2) and be conveyed, via side lot swales, to the curb and gutter of the adjacent streets to Design Point 5 (4.9 cfs/7.4 cfs). Runoff will be intercepted at DP-5 via an existing at-grade 12' D-10-R inlet. See FDR2 Basin J for pipe conveyance information and over flow conditions. Pipes 5, 7, 8, 9 and 11- have been sized to accept these developed flows and do not exceed the pipe design flows determined within the FDR for Filing 2.

Basin M is located in the northeast portion of the site and contains 2.62 acres of single family residential lots, landscaping, and an asphalt roadway. Basin M has proposed design flows of 5.4 cfs for the minor storm event (5-Year) and 11.3 cfs for the major storm event (100-Year). Runoff from Basin M will flow, via side lot swales, to the curb and gutter and will be conveyed south to Design Point 10, a 10' D-10-R inlet in an at-grade condition. The inlet at Design Point 10 has been sized to accept flows from Basin M in the developed condition. Collected flows from Design Point 10 will be conveyed in an 18" RCP (Pipe 20) to Design Point II, a 12' D-10-R at-grade inlet.

Basin M-1 is located in the northeast portion of the site and contains 0.65 acres of single family residential lots and asphalt roadway. Basin M-1 has proposed design flows of 1.3 cfs for the minor storm event (5-Year) and 2.7 cfs for the major storm event (100-Year). Basin M-1 was part of a Basin Min FDR2 and is identified only to account for design flows to Design Point 6, an existing 8' D-10-R inlet in a sump condition. See FDR2 Basin M for pipe conveyance information and over flow conditions. Pipes 8, 9 and 11 have been sized to accept these developed flows and do not exceed the pipe design flows in FDR2.

Basin O is located in the northeast portion of the site and contains 0.70 acres of rear yards of single family residential lots and Tract G. Basin O has proposed design flows of 1.6 cfs for the minor storm event (5-Year) and 3.3 cfs for the major storm event (100-Year). The runoff from Basin O will flow overland thru Tract G via the side lot swales, to the curb and gutter of Aspen Brush Court, w/o crossing any lots within Filing 2. Runoff collected by the roadway continues southerly (down-gradient) to Design Point 5, an existing 12' D-10-R inlet in an at-grade condition. See FDR2 Basin J for pipe conveyance information and over flow conditions. Pipe 5, 7, 8, 9 and 11 have been sized to accept these developed flows and do not exceed the pipe design flows in FDR2.

Basin P is located in the northerly portion of the site and contains 2.14 acres of single family residential lots, landscaping, and an asphalt roadway. Basin P has proposed design flows of 4.2 cfs for the minor storm event (5-Year) and 8.8 cfs for the major storm event (100-Year). Runoff from Basin P will flow, via side lot swales, to the curb and gutter and then westward to Design Point 9 (accumulated flows 10.2 cfs-5 year, 22.4 cfs-100 year). A temporary riprap pad will be constructed at the end of the proposed roadway to dissipate energy and prevent local scour. The existing diversion swale established with FDR2 (which previously directed runoff reaching this location to the south) will be abandoned by the construction of a new swale which will be to redirect runoff westward to the existing 48" RCP (Pipe 14). It should be noted that the majority of the existing swale along the western boundary of Filing No.2 remain in place to protect existing lots and serve as a secondary level of protection should the swale leading to pipe 14 fail. Pipes 14 and 3 have been sized to accept the contributing developed flows and do not exceed the pipe design flows in FDR2.

Basin Q is located in the northerly portion of the site and contains 3.66 acres of single family residential lots, landscaping, and proposed roadways. Basin Q has proposed design flows of 6.1 cfs for the minor storm event (5-Year) and 12.8 cfs for the major storm event (100-Year). Runoff from Basin Q will flow, via side lot swales, to the curb and gutter to Design Point 9 (accumulated flows 10.2 cfs-5 year, 22.4 cfs-100 year), before continuing within the aforementioned swale to Pipe 14. A temporary sediment basin is recommended to be constructed upstream of Pipe 14, to aid in deterring sediment transport, while riprap protection will be placed immediately adjacent to the pipe entrance to protect the transition slope to the mouth of the pipe. A perimeter berm will be constructed (within a permanent drainage easement) along the north of the filing within Basin Q to ensure that on site property owners are protected from offsite flows (OS1) should lack of maintenance or

removal of the existing offsite berm occur. The combination of the existing grade north of the proposed berm and the berm itself aids to direct any potential runoff to the west. A proposed 3' wide sidewalk chase will be constructed to convey the minor runoff from Basin OS-3 and east third of Basin OS-2 into Brush Top Road. Limited flow from the north is anticipated reach Brush Top, with future development as a high point will be planned to be placed near the north boundary line.

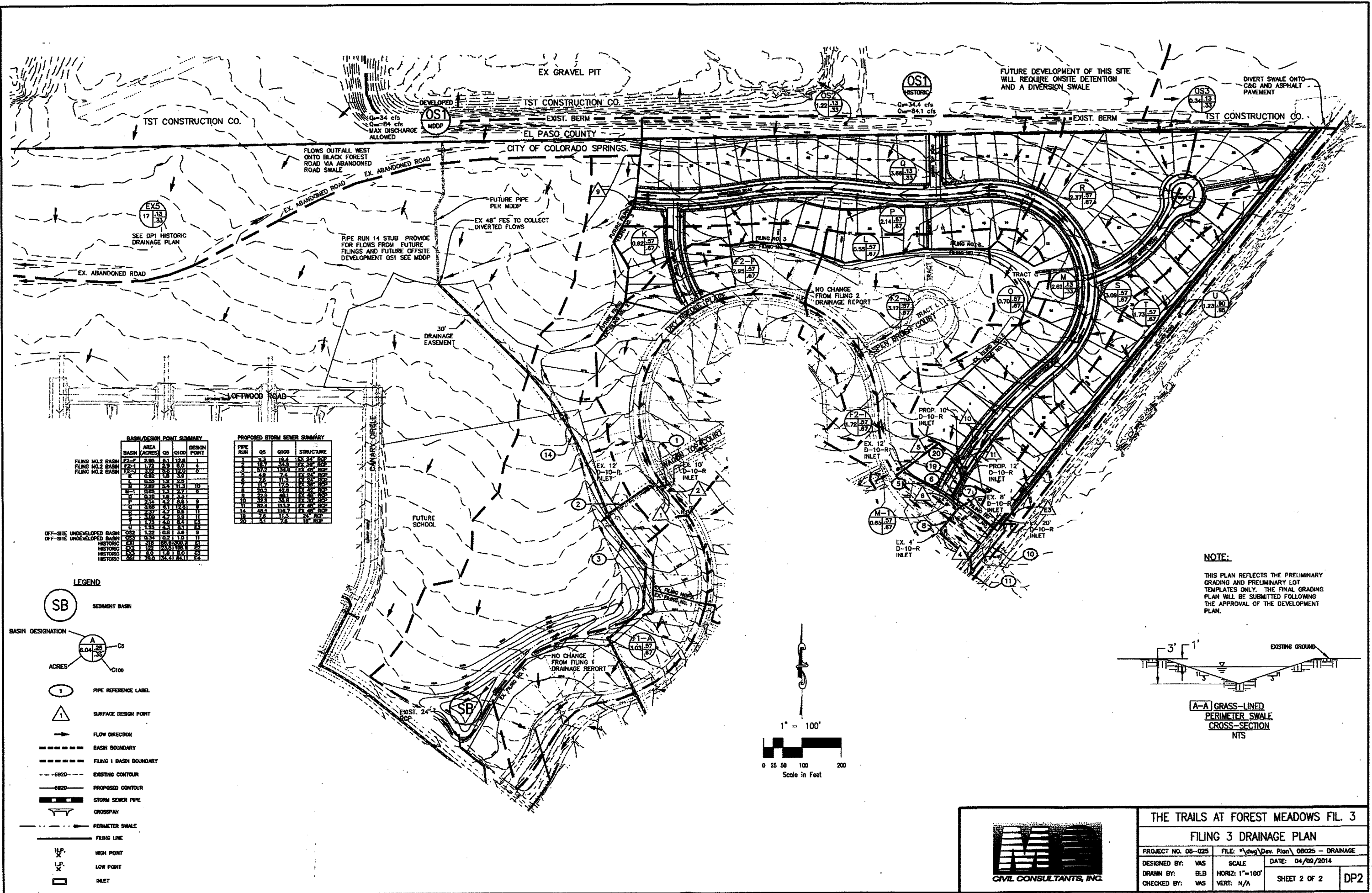
It should be noted that the contours on the provided drainage map illustrate the potential for a low point or break in the existing offsite berm immediately to the north of Brush Top Road which would allow for flows from Basin OS-1 to reach Basin OS-2. M&S Civil Consultants traveled to the sight and evaluated the onsite conditions at this location and determined that the existing contours shown on the provided map are not entirely representative of the current conditions. M&S Civil further ascertained the existing swale/berm at this location maintains a positive grade to the west and is somewhere between 1.7 to 2.0 feet tall which should provide adequate temporary capacity to redirect the offsite flows to the west.

Refer to the existing condition section of this report, the "Master Development Drainage Plan, Update for Woodmen Heights and Final Drainage Report for Forest Meadows Filing No.1 and No. 4", and Preliminary/Final Drainage Report for Highland Park Filing No.2" for additional information regarding offsite development in this area.

Basin R is located in the northerly portion of the site and contains 2.37 acres of single family residential lots, landscaping, and an asphalt roadway. Basin R has proposed design flows of 4.7 cfs for the minor storm event (5-Year) and 9.9 cfs for the major storm event (100-Year). Runoff from Basin R will flow, via side lot swales, to the curb and gutter to Design Point 11, a 12' D-10-R inlet in an at-grade condition. The inlet at Design Point 11 has been sized to accept flows from Basin R, S and OS3 in the developed condition. Collected flows from Design Point 11 will be conveyed in a 24" RCP (pipe 19) to pipe 6, an existing 24" RCP stub. Pipe 6, 7, 8, 9 and 11 have been sized to accept these developed flows and do not exceed the pipe design flows in FDR2. A perimeter berm will be constructed (within a permanent drainage easement) along the north of the filing within Basin R to ensure that on site property owners are protected from offsite flows (OS1) should lack of maintenance or removal of the existing offsite berm occur. The combination of the existing grade north of the proposed berm and the berm itself aids in directing any potential runoff to west.

Basin S is located in the easterly portion of the site and contains 3.09 acres of single family residential lots, landscaping, and an asphalt roadway. Basin S has proposed design flows of 4.7 cfs for the minor storm event (5-Year) and 9.9 cfs for the major storm event (100-Year). Runoff from Basins will flow, via side lot swales, to the curb and gutter to Design Point 11, a 12' D-10-R inlet in an at-grade condition. The inlet at Design Point 11 has been sized to accept flows from Basin R, S and OS3 in the developed condition. Collected flows from Design Point 11 will be conveyed in a 24" RCP (pipe 19) to pipe 6, an existing 24" RCP stub. Pipe 6, 7, 8, 9 and 11 have been sized to accept these developed flows and do not exceed the pipe design flows in FDR2. A perimeter berm will be constructed (within a permanent drainage easement) along the north and northeast edges of the proposed filing within Basin S to ensure that on site property owners are protected from offsite flows (OS3). The existing offsite berm located on the adjacent property to the currently aids in directing flows around the majority of the northeast edge of the filing, but terminates prior to eastern boundary line and cannot be relied on in perpetuity for flood control. Flows reaching the onsite berm will be directed to a pair of proposed 4' sidewalk chases which will aid to discharge runoff to the curb and gutter of Vollmer Road.

Basin T is located in the easterly portion of the site and contains 1.73 acres of rear yards of single family residential lots. Basin T has proposed design flows of 4.0 cfs for the minor storm event (5-Year) and 8.4 cfs for the major storm event (100-Year). Runoff from Basin T will flow, via side lot swales, to the curb and gutter in Vollmer Road to Design Point E3, an existing 12' D-10-R inlet, in an at-grade condition. The inlet at Design Point E3 has been sized to accept flows from Basin T, U and historic flows EX1 and EX2. Collected flows from Design Point E3 will be conveyed in an existing 30" RCP (pipe 10) to pipe 11, an existing 48" RCP. Combined flows in 9, 10 and 11 have been sized to accept these developed flows and do not exceed the pipe design flows in FDR2.



BASIN/DESIGN POINT SUMMARY

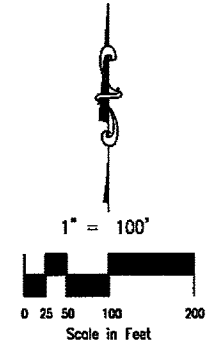
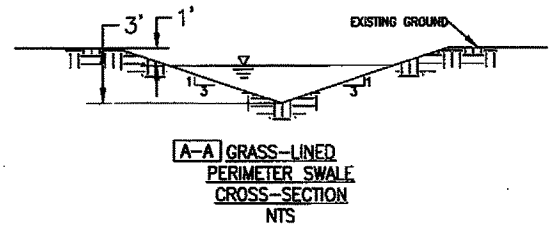
FLING NO./DESIGN POINT	AREA (ACRES)	QS	Q100	DESIGN POINT
FLING NO. 2 BASIN	2.85	8.1	12.8	1
FLING NO. 2 BASIN	1.72	2.9	8.0	2
FLING NO. 2 BASIN	1.12	1.9	5.0	3
FLING NO. 2 BASIN	0.92	1.4	4.0	4
FLING NO. 2 BASIN	0.88	1.3	3.9	5
FLING NO. 2 BASIN	0.85	1.2	3.7	6
FLING NO. 2 BASIN	0.82	1.1	3.5	7
FLING NO. 2 BASIN	0.79	1.0	3.3	8
FLING NO. 2 BASIN	0.76	0.9	3.1	9
FLING NO. 2 BASIN	0.73	0.8	2.9	10
FLING NO. 2 BASIN	0.70	0.7	2.7	11
FLING NO. 2 BASIN	0.67	0.6	2.5	12
FLING NO. 2 BASIN	0.64	0.5	2.3	13
FLING NO. 2 BASIN	0.61	0.4	2.1	14
FLING NO. 2 BASIN	0.58	0.3	1.9	15
FLING NO. 2 BASIN	0.55	0.2	1.7	16
FLING NO. 2 BASIN	0.52	0.1	1.5	17
FLING NO. 2 BASIN	0.49	0.0	1.3	18
FLING NO. 2 BASIN	0.46	0.0	1.1	19
FLING NO. 2 BASIN	0.43	0.0	0.9	20
FLING NO. 2 BASIN	0.40	0.0	0.7	21
FLING NO. 2 BASIN	0.37	0.0	0.5	22
FLING NO. 2 BASIN	0.34	0.0	0.3	23
FLING NO. 2 BASIN	0.31	0.0	0.1	24

PROPOSED STORM SEWER SUMMARY

PIPE RUN	QS	Q100	STRUCTURE
1	0.3	0.8	EX 20" RCP
2	1.9	5.5	EX 24" RCP
3	1.9	5.5	EX 24" RCP
4	1.9	5.5	EX 24" RCP
5	1.9	5.5	EX 24" RCP
6	1.9	5.5	EX 24" RCP
7	1.9	5.5	EX 24" RCP
8	1.9	5.5	EX 24" RCP
9	1.9	5.5	EX 24" RCP
10	1.9	5.5	EX 24" RCP
11	1.9	5.5	EX 24" RCP
12	1.9	5.5	EX 24" RCP
13	1.9	5.5	EX 24" RCP
14	1.9	5.5	EX 24" RCP
15	1.9	5.5	EX 24" RCP
16	1.9	5.5	EX 24" RCP
17	1.9	5.5	EX 24" RCP
18	1.9	5.5	EX 24" RCP
19	1.9	5.5	EX 24" RCP
20	1.9	5.5	EX 24" RCP

- LEGEND**
- SEDIMENT BASIN
 - BASIN DESIGNATION**
 - A C100
 - A C5
 - ACRES
 - PIPE REFERENCE LABEL
 - SURFACE DESIGN POINT
 - FLOW DIRECTION
 - BASIN BOUNDARY
 - FLING 1 BASIN BOUNDARY
 - EXISTING CONTOUR
 - PROPOSED CONTOUR
 - STORM SEWER PIPE
 - CROSSSPAN
 - PERIMETER SWALE
 - FLING LINE
 - HIGH POINT
 - LOW POINT
 - INLET

NOTE:
 THIS PLAN REFLECTS THE PRELIMINARY GRADING AND PRELIMINARY LOT TEMPLATES ONLY. THE FINAL GRADING PLAN WILL BE SUBMITTED FOLLOWING THE APPROVAL OF THE DEVELOPMENT PLAN.

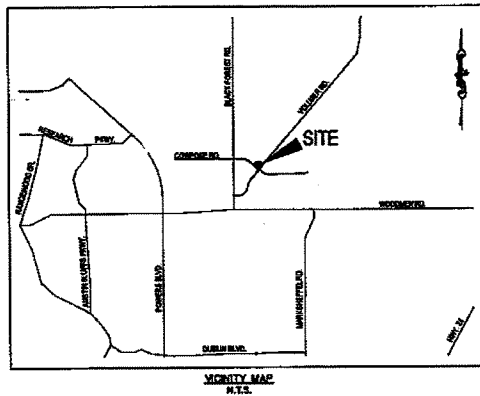


CIVIL CONSULTANTS, INC.

THE TRAILS AT FOREST MEADOWS FIL. 3

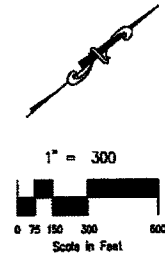
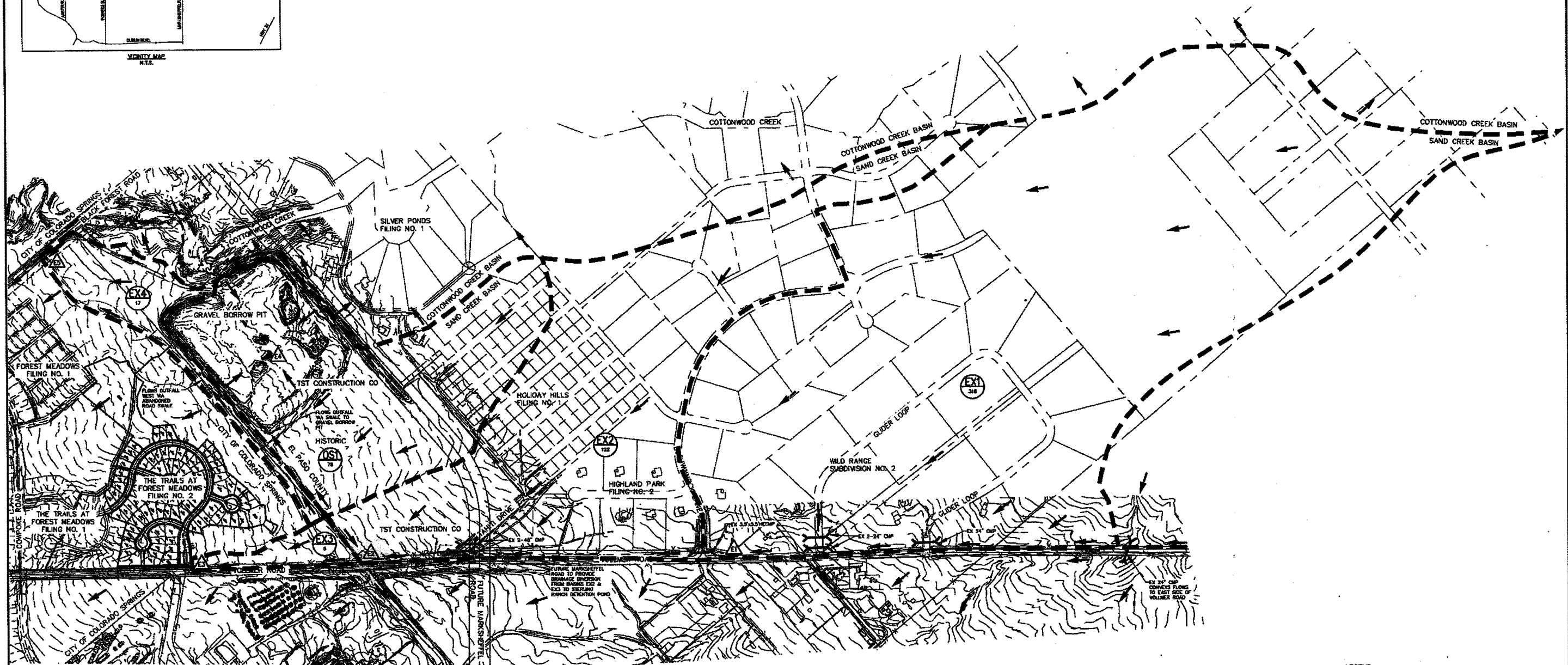
FILING 3 DRAINAGE PLAN

PROJECT NO. 08-025		FILE: "dwg\Dev. Plan\ 08025 - DRAINAGE"	
DESIGNED BY: VAS	SCALE: DATE: 04/09/2014		
DRAWN BY: BLB	HORIZ: 1"=100'		
CHECKED BY: VAS	VERT: N/A	SHEET 2 OF 2	DP2



HISTORIC BASIN SUMMARY			
BASIN	AREA (Acres)	Q _a (cfs)	Q ₁₀₀ (cfs)
EX1	318	66.6	300.7
EX2	122	23.5	108.1
EX3	6	1.8	8.0
OS1	78	34.4	84.1
EX5	17	5.1	22.9

HISTORIC SURFACE ROUTING SUMMARY			
DESIGN POINT	DESIGN BASIN	Q _a (cfs)	Q ₁₀₀ (cfs)
E1	EX1	66.6	300.7
E2	EX2 & DP E1	84.7	382.6
E3	EX3 & DP E2	85.8	387.8
E4	OS1	34.4	84.1
E5	EX4	5.1	22.9



LEGEND

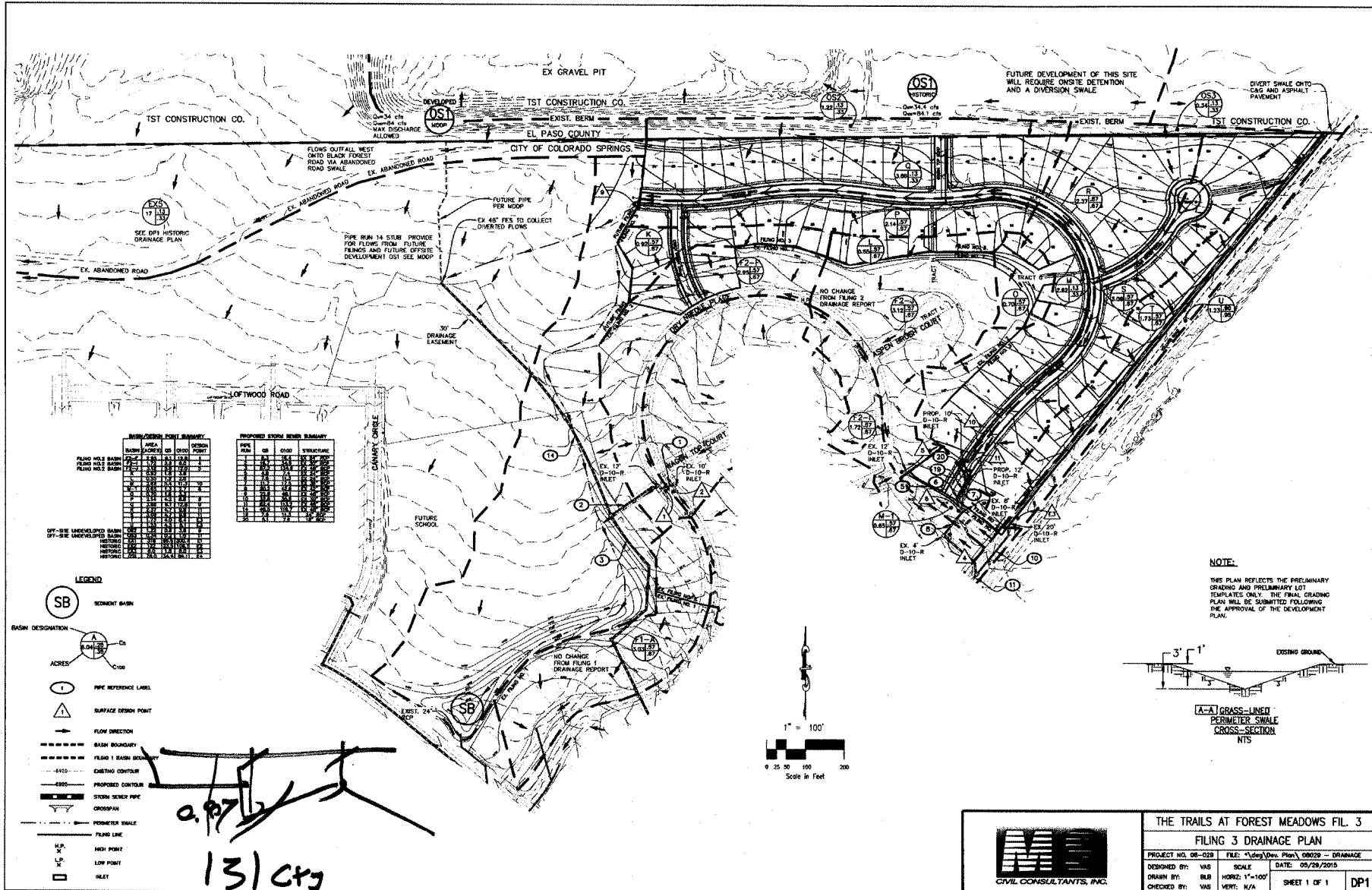
- EX1 23.2
EXISTING WATER BASIN ACREAGE
- △
EXISTING FLOW RELEASE POINT
- FLOW DIRECTION
- - -
BASIN BOUNDARY
- 100
EXISTING CONTOUR
- CULVERT PIPE

CIVIL CONSULTANTS, INC.
E. PINE PEAK AVE., STE 306
COLORADO SPRINGS, CO 80901
(719) 235-5248, FAX (719) 444-8427

THE TRAILS AT FOREST MEADOWS FIL. NO. 2
HISTORIC - DRAINAGE MAP

PROJECT NO. 08-025	FILE: *LongView Plan/08-025-HISTORIC
DESIGNED BY: ET	SCALE: DATE: 05/01/14
DRAWN BY: ET	HORIZ: 1"=300'
CHECKED BY:	VERT: N/A

SHEET 1 OF 2 DP1



EXISTING POINT ELEVATIONS

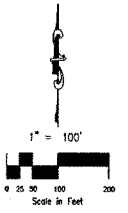
AREA	POINT	ELEVATION
1	1	5113.1
1	2	5113.1
1	3	5113.1
1	4	5113.1
1	5	5113.1
1	6	5113.1
1	7	5113.1
1	8	5113.1
1	9	5113.1
1	10	5113.1
1	11	5113.1
1	12	5113.1
1	13	5113.1
1	14	5113.1
1	15	5113.1
1	16	5113.1
1	17	5113.1
1	18	5113.1
1	19	5113.1
1	20	5113.1
1	21	5113.1
1	22	5113.1
1	23	5113.1
1	24	5113.1
1	25	5113.1
1	26	5113.1
1	27	5113.1
1	28	5113.1
1	29	5113.1
1	30	5113.1
1	31	5113.1
1	32	5113.1
1	33	5113.1
1	34	5113.1
1	35	5113.1
1	36	5113.1
1	37	5113.1
1	38	5113.1
1	39	5113.1
1	40	5113.1
1	41	5113.1
1	42	5113.1
1	43	5113.1
1	44	5113.1
1	45	5113.1
1	46	5113.1
1	47	5113.1
1	48	5113.1
1	49	5113.1
1	50	5113.1
1	51	5113.1
1	52	5113.1
1	53	5113.1
1	54	5113.1
1	55	5113.1
1	56	5113.1
1	57	5113.1
1	58	5113.1
1	59	5113.1
1	60	5113.1
1	61	5113.1
1	62	5113.1
1	63	5113.1
1	64	5113.1
1	65	5113.1
1	66	5113.1
1	67	5113.1
1	68	5113.1
1	69	5113.1
1	70	5113.1
1	71	5113.1
1	72	5113.1
1	73	5113.1
1	74	5113.1
1	75	5113.1
1	76	5113.1
1	77	5113.1
1	78	5113.1
1	79	5113.1
1	80	5113.1
1	81	5113.1
1	82	5113.1
1	83	5113.1
1	84	5113.1
1	85	5113.1
1	86	5113.1
1	87	5113.1
1	88	5113.1
1	89	5113.1
1	90	5113.1
1	91	5113.1
1	92	5113.1
1	93	5113.1
1	94	5113.1
1	95	5113.1
1	96	5113.1
1	97	5113.1
1	98	5113.1
1	99	5113.1
1	100	5113.1

PROPOSED STORM SEWER SUMMARY

LINE	SIZE	DEPTH	STRUCTURE
1	12"	10'-R	INLET
2	12"	10'-R	INLET
3	12"	10'-R	INLET
4	12"	10'-R	INLET
5	12"	10'-R	INLET
6	12"	10'-R	INLET
7	12"	10'-R	INLET
8	12"	10'-R	INLET
9	12"	10'-R	INLET
10	12"	10'-R	INLET
11	12"	10'-R	INLET
12	12"	10'-R	INLET
13	12"	10'-R	INLET
14	12"	10'-R	INLET
15	12"	10'-R	INLET
16	12"	10'-R	INLET
17	12"	10'-R	INLET
18	12"	10'-R	INLET
19	12"	10'-R	INLET
20	12"	10'-R	INLET
21	12"	10'-R	INLET
22	12"	10'-R	INLET
23	12"	10'-R	INLET
24	12"	10'-R	INLET
25	12"	10'-R	INLET
26	12"	10'-R	INLET
27	12"	10'-R	INLET
28	12"	10'-R	INLET
29	12"	10'-R	INLET
30	12"	10'-R	INLET
31	12"	10'-R	INLET
32	12"	10'-R	INLET
33	12"	10'-R	INLET
34	12"	10'-R	INLET
35	12"	10'-R	INLET
36	12"	10'-R	INLET
37	12"	10'-R	INLET
38	12"	10'-R	INLET
39	12"	10'-R	INLET
40	12"	10'-R	INLET
41	12"	10'-R	INLET
42	12"	10'-R	INLET
43	12"	10'-R	INLET
44	12"	10'-R	INLET
45	12"	10'-R	INLET
46	12"	10'-R	INLET
47	12"	10'-R	INLET
48	12"	10'-R	INLET
49	12"	10'-R	INLET
50	12"	10'-R	INLET
51	12"	10'-R	INLET
52	12"	10'-R	INLET
53	12"	10'-R	INLET
54	12"	10'-R	INLET
55	12"	10'-R	INLET
56	12"	10'-R	INLET
57	12"	10'-R	INLET
58	12"	10'-R	INLET
59	12"	10'-R	INLET
60	12"	10'-R	INLET
61	12"	10'-R	INLET
62	12"	10'-R	INLET
63	12"	10'-R	INLET
64	12"	10'-R	INLET
65	12"	10'-R	INLET
66	12"	10'-R	INLET
67	12"	10'-R	INLET
68	12"	10'-R	INLET
69	12"	10'-R	INLET
70	12"	10'-R	INLET
71	12"	10'-R	INLET
72	12"	10'-R	INLET
73	12"	10'-R	INLET
74	12"	10'-R	INLET
75	12"	10'-R	INLET
76	12"	10'-R	INLET
77	12"	10'-R	INLET
78	12"	10'-R	INLET
79	12"	10'-R	INLET
80	12"	10'-R	INLET
81	12"	10'-R	INLET
82	12"	10'-R	INLET
83	12"	10'-R	INLET
84	12"	10'-R	INLET
85	12"	10'-R	INLET
86	12"	10'-R	INLET
87	12"	10'-R	INLET
88	12"	10'-R	INLET
89	12"	10'-R	INLET
90	12"	10'-R	INLET
91	12"	10'-R	INLET
92	12"	10'-R	INLET
93	12"	10'-R	INLET
94	12"	10'-R	INLET
95	12"	10'-R	INLET
96	12"	10'-R	INLET
97	12"	10'-R	INLET
98	12"	10'-R	INLET
99	12"	10'-R	INLET
100	12"	10'-R	INLET

- LEGEND**
- SB SEDIMENT BASIN
 - BASIN DESIGNATION: 1-10, 11-20, 21-30, 31-40, 41-50, 51-60, 61-70, 71-80, 81-90, 91-100
 - ACRES: 0.04, 0.05, 0.06, 0.07, 0.08, 0.09, 0.10
 - PIPE REFERENCE LABEL: 1, 2, 3, 4, 5, 6, 7, 8, 9, 10, 11, 12, 13, 14, 15, 16, 17, 18, 19, 20, 21, 22, 23, 24, 25, 26, 27, 28, 29, 30, 31, 32, 33, 34, 35, 36, 37, 38, 39, 40, 41, 42, 43, 44, 45, 46, 47, 48, 49, 50, 51, 52, 53, 54, 55, 56, 57, 58, 59, 60, 61, 62, 63, 64, 65, 66, 67, 68, 69, 70, 71, 72, 73, 74, 75, 76, 77, 78, 79, 80, 81, 82, 83, 84, 85, 86, 87, 88, 89, 90, 91, 92, 93, 94, 95, 96, 97, 98, 99, 100
 - SURFACE DESIGN POINT: 1, 2, 3, 4, 5, 6, 7, 8, 9, 10, 11, 12, 13, 14, 15, 16, 17, 18, 19, 20, 21, 22, 23, 24, 25, 26, 27, 28, 29, 30, 31, 32, 33, 34, 35, 36, 37, 38, 39, 40, 41, 42, 43, 44, 45, 46, 47, 48, 49, 50, 51, 52, 53, 54, 55, 56, 57, 58, 59, 60, 61, 62, 63, 64, 65, 66, 67, 68, 69, 70, 71, 72, 73, 74, 75, 76, 77, 78, 79, 80, 81, 82, 83, 84, 85, 86, 87, 88, 89, 90, 91, 92, 93, 94, 95, 96, 97, 98, 99, 100
 - FLOW DIRECTION: arrow
 - BASIN BOUNDARY: dashed line
 - FLAG 1 BASIN BOWL: dashed line
 - EXISTING CONTOUR: solid line
 - PROPOSED CONTOUR: dashed line
 - STORM SEWER PIPE: thick solid line
 - CROSSSPAN: triangle
 - PERIMETER SWALE: dashed line
 - FINISH LINE: thin solid line
 - HP HIGH POINT
 - LP LOW POINT
 - INLET: rectangle

Handwritten signature and notes:
 a. 0.07
 131 cty



NOTE:
 THIS PLAN REFLECTS THE PRELIMINARY GRADING AND PRELIMINARY LOT TEMPLATES ONLY. THE FINAL GRADING PLAN WILL BE SUBMITTED FOLLOWING THE APPROVAL OF THE DEVELOPMENT PLAN.

A-A] GRASS-LINED PERIMETER SWALE CROSS-SECTION NTS

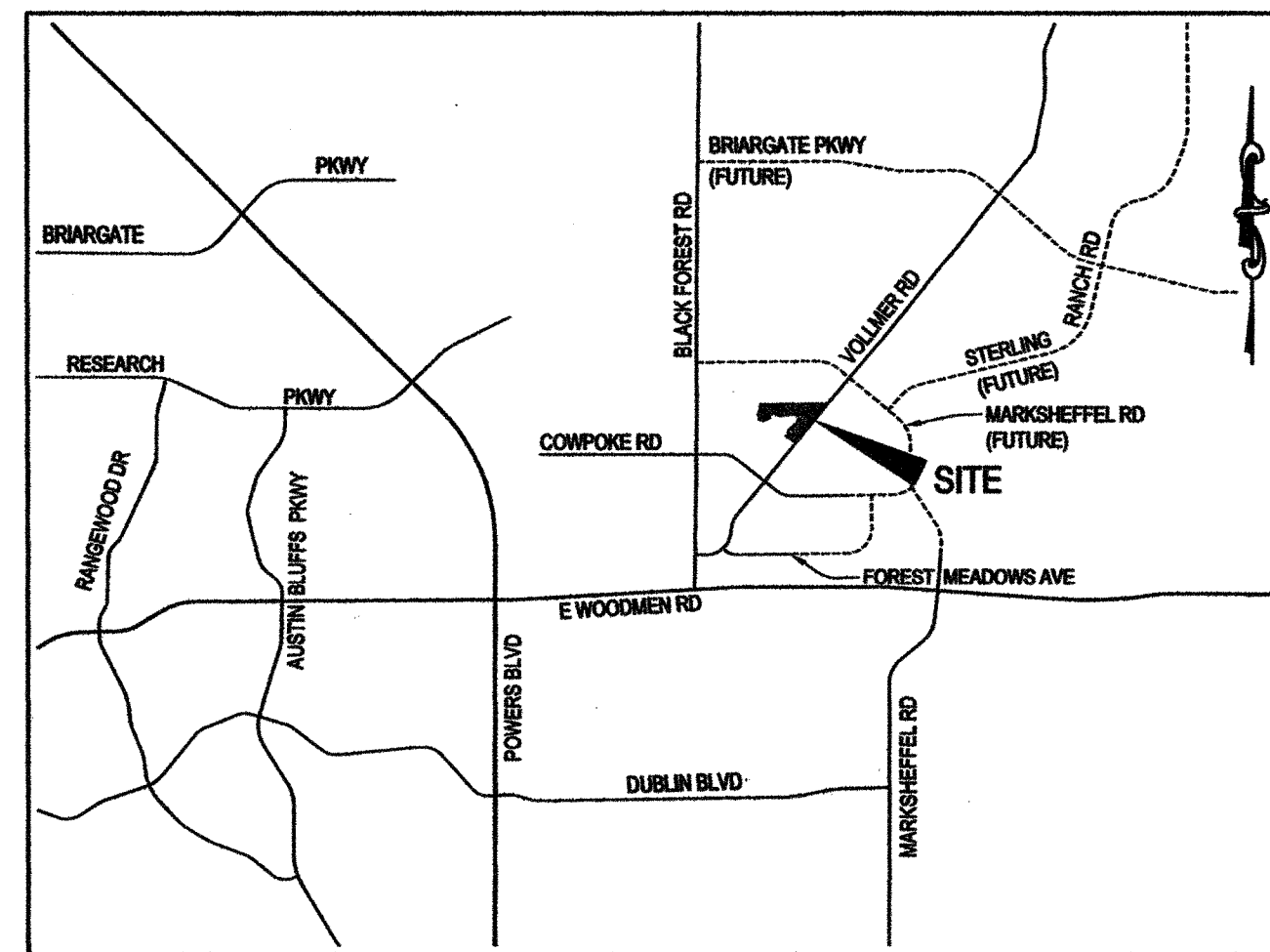
	THE TRAILS AT FOREST MEADOWS FIL. 3			
	FILING 3 DRAINAGE PLAN			
	PROJECT NO. 08-028	FILE: \\civ\proj\Plan\08028 - DRAINAGE		
	DESIGNED BY: VAS	SCALE:	DATE: 05/29/2010	
	DRAWN BY: BLB	HORIZ: 1"=100'	VERT: N/A	SHEET 1 OF 1 DP1

TRAILS AT FOREST MEADOWS FILING NO. 3

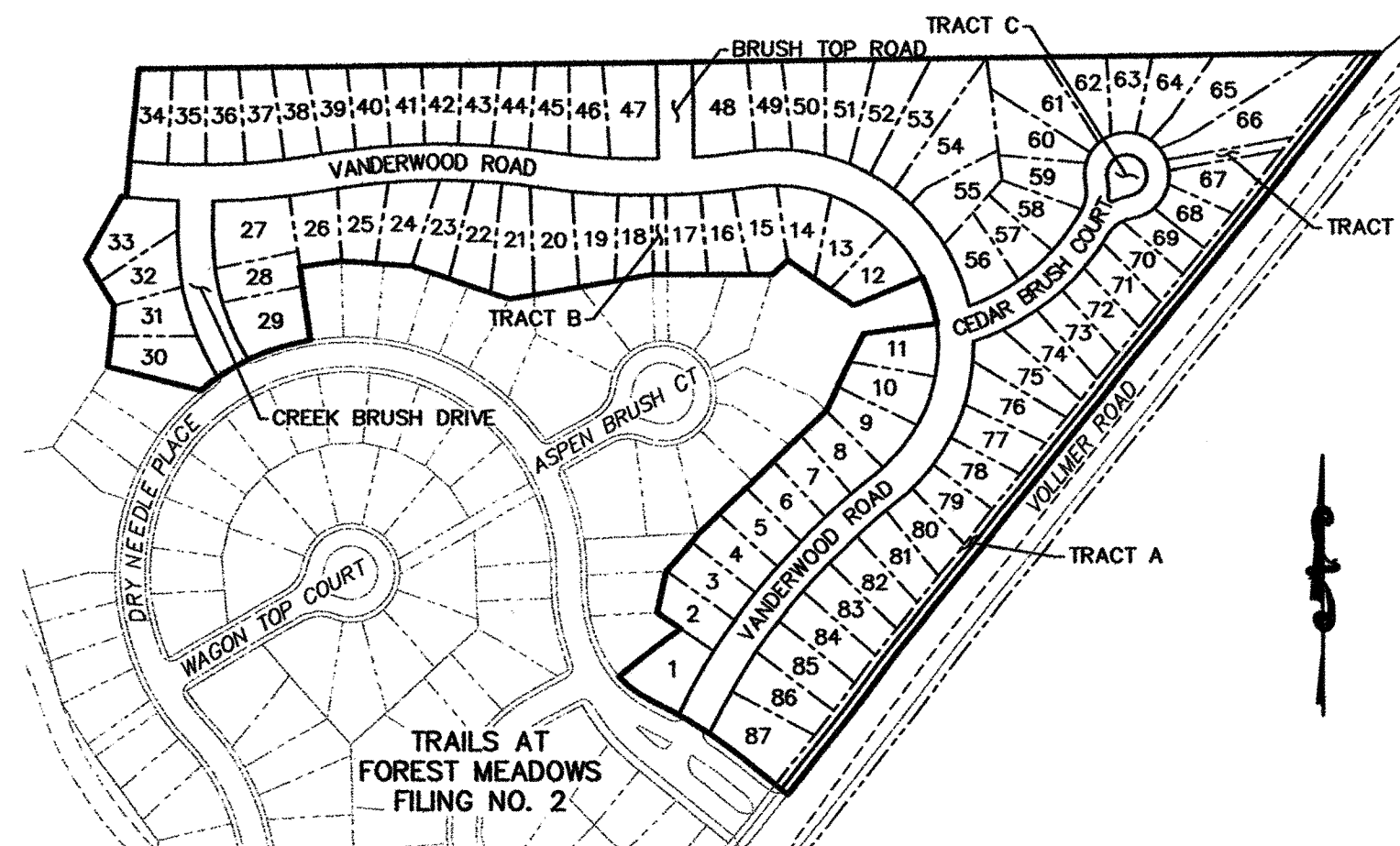
CITY OF COLORADO SPRINGS, EL PASO COUNTY, STATE OF COLORADO

STREET IMPROVEMENT PLANS (INCLUDING STORM SEWER)

AUGUST 2015



VICINITY MAP
N.T.S.



KEY MAP
N.T.S.

GENERAL NOTES

- ALL MATERIALS AND INSTALLATION PROCEDURES SHALL BE IN COMPLIANCE WITH THE CITY OF COLORADO SPRINGS, DEPARTMENT OF PUBLIC WORKS, SUBDIVISION POLICY MANUAL AND DIVISION "RULES FOR THE INSTALLATION OF SEWER MAINS AND SERVICES".
- IT SHALL BE THE RESPONSIBILITY OF THE CONTRACTOR TO VERIFY THE EXISTENCE AND LOCATION OF ALL UNDERGROUND UTILITIES ALONG THE ROUTE OF THE WORK. THE OMISSION FROM OR THE INCLUSION OF UTILITY LOCATIONS ON THE PLANS IS NOT TO BE CONSIDERED AS THE NONEXISTENCE OF OR A DEFINITE LOCATION OF EXISTING UNDERGROUND UTILITIES.
- THE CONTRACTOR WILL TAKE THE NECESSARY PRECAUTIONS TO PROTECT EXISTING UTILITIES FROM DAMAGE DUE TO THIS OPERATION. ANY DAMAGE TO THE UTILITIES WILL BE REPAIRED AT THE CONTRACTOR'S EXPENSE, AND ANY SERVICE DISRUPTION WILL BE SETTLED BY THE CONTRACTOR.
- CONCRETE USED IN CURB AND GUTTER, SIDEWALK, AND CROSSSPAN CONSTRUCTION WILL HAVE A MINIMUM COMPRESSIVE STRENGTH OF 4,000 PSI AT 28 DAYS.
- ALL BACKFILL, SUB-BASE, AND/OR BASE COURSE (CLASS 6) MATERIAL SHALL BE COMPACTED PER THE SOILS ENGINEER'S RECOMMENDATIONS.
- ALL STATIONING IS CENTERLINE OF IMPROVEMENTS UNLESS OTHERWISE INDICATED. ALL ELEVATIONS ARE FLOW LINE UNLESS OTHERWISE INDICATED AS TOP BACK OF CURB (TBC), ASPHALT (ASP), OR TOP OF INLET OR BOX (TOB).
- ALL CURB RETURNS AND 10' EITHER SIDE OF CURB RETURNS SHALL BE 8" VERTICAL CURB, CITY OF COLORADO SPRINGS TYPE 1 CURB WITH AN ADDITIONAL 10' OF TRANSITION TO 6" RAMP CURB. CITY OF COLORADO SPRINGS MODIFIED TYPE 5 CURB, UNLESS OTHERWISE INDICATED.
- PEDESTRIAN RAMPS SHALL BE INSTALLED AT INTERSECTIONS AS SHOWN AND CONFORM TO THE CITY OF COLORADO SPRINGS, DEPARTMENT OF PUBLIC WORKS STANDARDS AND SPECIFICATIONS.
NOTE: WIDTH OF PEDESTRIAN RAMPS MUST MATCH WIDTH OF SIDEWALK.
- IF A DISCREPANCY OCCURS BETWEEN THE CONSTRUCTION DOCUMENTS AND THE CITY OF COLORADO SPRINGS STANDARD SPECIFICATIONS, THE ENGINEER WILL BE NOTIFIED IMMEDIATELY FOR RESOLUTION.
- THE CONTRACTOR SHALL SECURE ALL APPLICABLE LICENSES AND PERMITS TO COMPLETE THE CONSTRUCTION IN COMPLIANCE WITH ALL LOCAL, STATE, AND FEDERAL REGULATIONS.
- CONTRACTOR TO OBTAIN COPIES OF THE SOILS REPORT FROM THE GEOTECHNICAL ENGINEER AND TO BE KEPT ON-SITE DURING ALL EARTHWORK OPERATIONS.

CONCRETE: CONCRETE REINFORCEMENT:

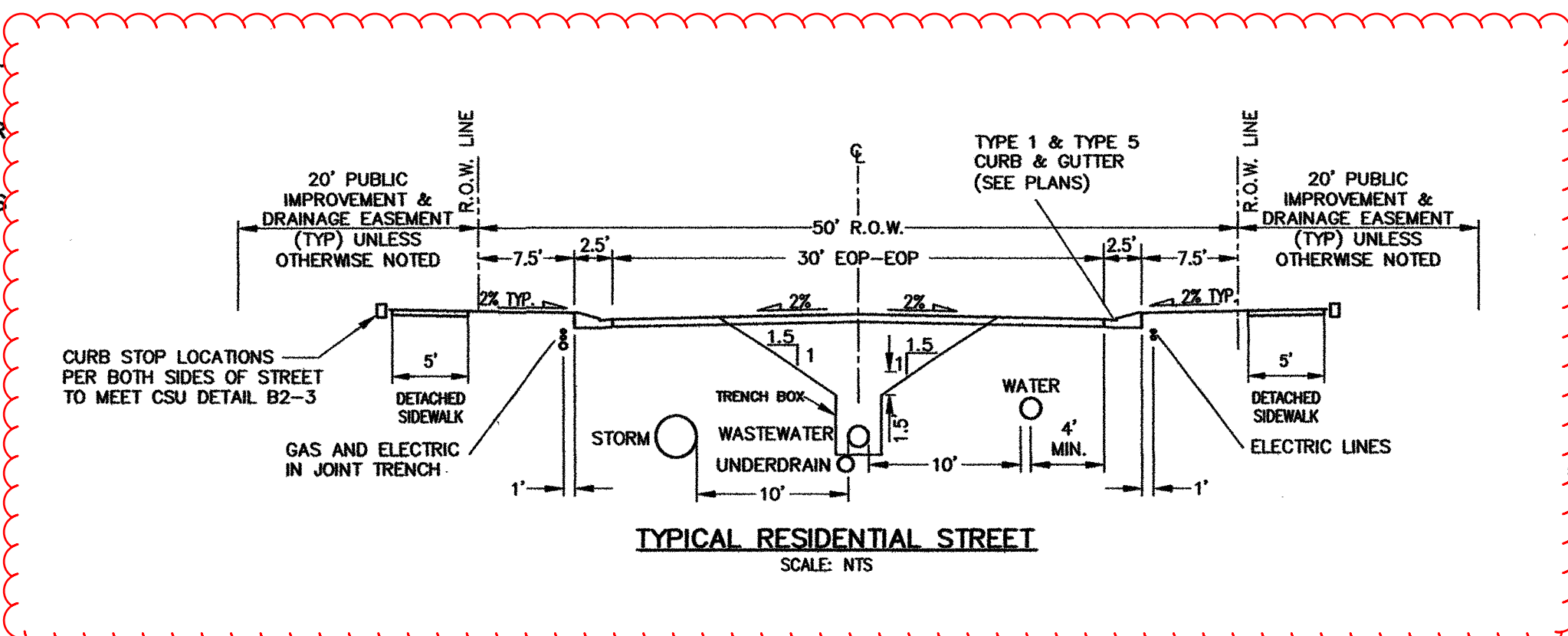
- ALL CAST IN PLACE CONCRETE SHALL HAVE A MINIMUM COMPRESSIVE YIELD STRENGTH OF 4,000 PSI UNLESS OTHERWISE NOTED. HIGHER COMPRESSIVE STRENGTH CONCRETE IS ACCEPTABLE TO ACHIEVE EARLY CONCRETE STRENGTH THAT MAY BE DEEMED NECESSARY TO MEET CONSTRUCTION SCHEDULING PRIORITIES.
- ALL CAST IN PLACE CONCRETE REINFORCEMENT SHALL HAVE A MINIMUM TENSILE YIELD STRENGTH OF 60,000 PSI UNLESS OTHERWISE NOTED, AND CONFORMANCE WITH CITY OF COLORADO SPRINGS SPECIFICATIONS, SECTION 603.
- CONCRETE TESTING SHALL BE IN CONFORMANCE WITH CITY OF COLORADO SPRINGS SPECIFICATIONS, SECTION 506.

STORM SEWER NOTES:

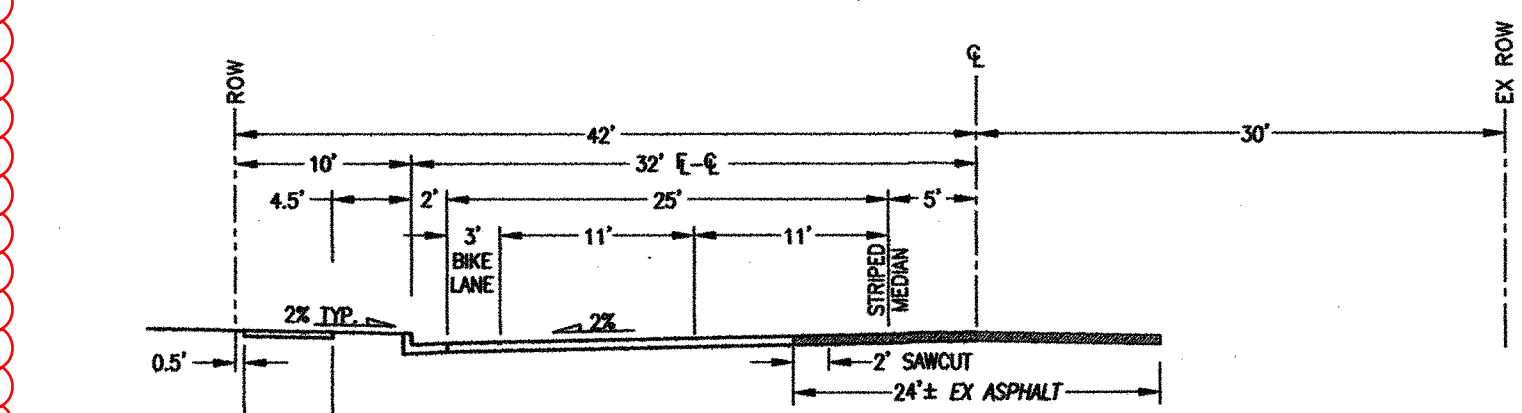
- CONSTRUCT AND INSTALL D-10-R INLETS PER CITY OF COLORADO SPRINGS SHEET D-10-R 1, 2, AND 3.
- CONSTRUCT AND INSTALL TYPE I MANHOLES PER CITY OF COLORADO SPRINGS SHEETS D-20A (1) AND D-20D (4).
- THE MINIMUM CLASS OF REINFORCED CONCRETE PIPE SHALL BE CLASS III.

TRAFFIC ENGINEERING GENERAL NOTES:

- CALL BEFORE EXCAVATING, CONTRACTOR SHALL VERIFY LOCATION OF UNDERGROUND UTILITIES.
- CONTRACTOR SHALL BE RESPONSIBLE FOR ANY MONUMENTATION AND/OR BENCHMARKS WHICH WILL BE DISTURBED OR DESTROYED BY CONSTRUCTION. SUCH POINTS SHALL BE REFERENCED AND REPLACED WITH APPROPRIATE MONUMENTATION BY A REGISTERED CIVIL ENGINEER AUTHORIZED TO PRACTICE LAND SURVEYING.
- APPROVAL OF THESE PLANS BY THE CITY ENGINEER DOES NOT AUTHORIZE ANY WORK TO BE PERFORMED UNTIL A PERMIT HAS BEEN ISSUED.
- THE APPROVAL OF THESE PLANS OR ISSUANCE OF A PERMIT BY THE CITY OF COLORADO SPRINGS DOES NOT AUTHORIZE THE SUBDIVIDER AND OWNER TO VIOLATE ANY FEDERAL, STATE, OR CITY LAWS, ORDINANCES, REGULATIONS, OR POLICIES.
- THE CONTRACTOR SHALL BE RESPONSIBLE FOR ALL NEW, TEMPORARY AND EXISTING TRAFFIC SIGNS FROM THE START OF THE CONSTRUCTION PROJECT UNTIL ACCEPTANCE BY CITY TRAFFIC ENGINEERING.
- ALL TRAFFIC SIGNS, PAVEMENT MARKINGS, AND TRAFFIC SIGNALS SHALL MEET OR EXCEED M.T.U.C.D. STANDARDS.
- THE CONTRACTOR SHALL NOT REMOVE ANY EXISTING SIGNS, PAVEMENT MARKINGS OR TRAFFIC SIGNALS DURING THE PROJECT WITHOUT SIGNED AUTHORIZATION OF THE CITY TRAFFIC ENGINEERING INSPECTOR ASSIGNED TO THE PROJECT.
- CONTRACTOR SHALL PREPARE A DETAILED TRAFFIC CONTROL PLAN, SUBMIT TO CITY TRAFFIC ENGINEERING FOR APPROVAL, AND OBTAIN APPROPRIATE PERMITS IN ACCORDANCE WITH THE "TRAFFIC CONTROLS FOR STREET CONSTRUCTION, UTILITY WORK AND MAINTENANCE OPERATIONS", M.U.T.C.D. SUPPLEMENT FOR THE CITY OF COLORADO SPRINGS. AUGUST 1992.
- THE CONTRACTOR SHALL BE RESPONSIBLE FOR ALL WORK ZONE TRAFFIC CONTROL. CONTRACTOR SHALL BE RESPONSIBLE FOR FURNISHING, INSTALLING AND MAINTAINING THE TEMPORARY TRAFFIC CONTROL DEVICES THROUGHOUT THE DURATION OF THE PROJECT.
- THE CONTRACTOR SHALL BE RESPONSIBLE FOR ALL NEW, TEMPORARY, AND EXISTING TRAFFIC SIGNAL MODIFICATIONS.



TYPICAL RESIDENTIAL STREET
SCALE: N.T.S.



TYPICAL MINOR ARTERIAL
STREET/UTILITY SECTION (VOLLMER ROAD)
SCALE: N.T.S.

PROJECT DATUM
VERTICAL - NATIONAL GEODETIC VERTICAL DATUM 1929 (NGVD29)
HORIZONTAL - NORTH AMERICAN DATUM 1983 (NAD83)
CONTROL - COLORADO STATE PLANE CENTRAL ZONE

AGENCIES

OWNER: CHALLENGER HOMES, INC.
13570 NORTHGATE ESTATES DRIVE
COLORADO SPRINGS, CO 80921
ROGER MILLER (719) 588-5192
ROGER@CHALLENGERHOMES.COM

CIVIL ENGINEER: M & S CIVIL CONSULTANTS, INC.
20 BOULDER CRESCENT, SUITE 110
COLORADO SPRINGS, CO 80903
VIRGIL A. SANCHEZ P.E. (719) 955-5485

ENGINEERING DIVISION: CITY OF COLORADO SPRINGS
30 S. NEVADA AVE., SUITE 401
COLORADO SPRINGS, CO 80903
ELIZABETH NIJKAMP, P.E. (719) 385-5410

TRAFFIC ENGINEERING: CITY OF COLORADO SPRINGS
30 S. NEVADA AVE., SUITE 401
COLORADO SPRINGS, CO 80903
KATHLEEN KRAGER (719) 385-7628

DEVELOPMENT SERVICES: COLORADO SPRINGS UTILITIES
1521 HANCOCK EXPRESSWAY
COLORADO SPRINGS, CO 80903
AL JUVERA (719) 688-8769

GAS DEPARTMENT: COLORADO SPRINGS UTILITIES
7710 DURANT DR.
COLORADO SPRINGS, CO 80920
TIM WENDT (719) 688-3556

ELECTRIC DEPARTMENT: COLORADO SPRINGS UTILITIES
7710 DURANT DR.
COLORADO SPRINGS, CO 80920
SARAH LABARRE (719) 688-4933

COMMUNICATIONS: QWEST COMMUNICATIONS
(U.N.C.C. LOCATORS) (800) 922-1987
AT&T (LOCATORS) (719) 635-3674

DETAILED DRAINAGE CONSTRUCTION PLANS AND SPECIFICATIONS ENGINEER'S STATEMENT:

THESE DETAILED PLANS AND SPECIFICATIONS WERE PREPARED UNDER MY DIRECTION AND SUPERVISION. SAID DETAILED PLANS AND SPECIFICATIONS HAVE BEEN PREPARED ACCORDING TO THE ESTABLISHED CRITERIA FOR DETAILED DRAINAGE PLANS AND SPECIFICATIONS, AND SAID DETAILED PLANS AND SPECIFICATIONS ARE IN CONFORMITY WITH THE MASTER PLAN OF THE DRAINAGE BASIN. SAID DETAILED DRAINAGE PLANS AND SPECIFICATIONS MEET THE PURPOSES FOR WHICH THE PARTICULAR DRAINAGE FACILITY(S) IS DESIGNED. I ACCEPT RESPONSIBILITY FOR ANY LIABILITY CAUSED BY ANY NEGLIGENT ACTS, ERRORS OR OMISSIONS ON MY PART IN PREPARATION OF THE DETAILED DRAINAGE PLANS AND SPECIFICATIONS.

Virgil A. Sanchez
VIRGIL A. SANCHEZ, COLORADO P.E. NO. 37160
FOR AND ON BEHALF OF M&S CIVIL CONSULTANTS, INC. DATE: 9/16/15

PLAN REVIEW BY CITY OF COLORADO SPRINGS IS PROVIDED ONLY FOR GENERAL CONFORMANCE WITH DESIGN CRITERIA. THE CITY OF COLORADO SPRINGS IS NOT RESPONSIBLE FOR THE ACCURACY AND ADEQUACY OF THE DESIGN, DIMENSIONS, AND/OR ELEVATIONS WHICH SHALL BE CONFIRMED AT THE JOB SITE. THE CITY OF COLORADO SPRINGS, THROUGH THE APPROVAL OF THIS DOCUMENT, ASSUMES NO RESPONSIBILITY FOR COMPLETENESS AND/OR ACCURACY OF THIS DOCUMENT.

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SHEET 5	PLAN & PROFILE - CREEK BRUSH DRIVE & BRUSH TOP ROAD
SHEET 6	PLAN & PROFILE - VOLLMER ROAD
SHEET 7	VANDERWOOD ROAD STORM DRAIN AND INLETS
SHEET 8	SIGNAGE AND STRIPING PLAN

STATEMENT:
THE CITY OF COLORADO SPRINGS RECOGNIZES THE DESIGN ENGINEER AS HAVING RESPONSIBILITY FOR THE DESIGN. THE CITY HAS LIMITED ITS SCOPE OF REVIEW ACCORDINGLY. RESIDENTIAL REQUIRED IF CONSTRUCTION HAS NOT COMMENCED WITHIN 180 DAYS AFTER REVIEW DATE.

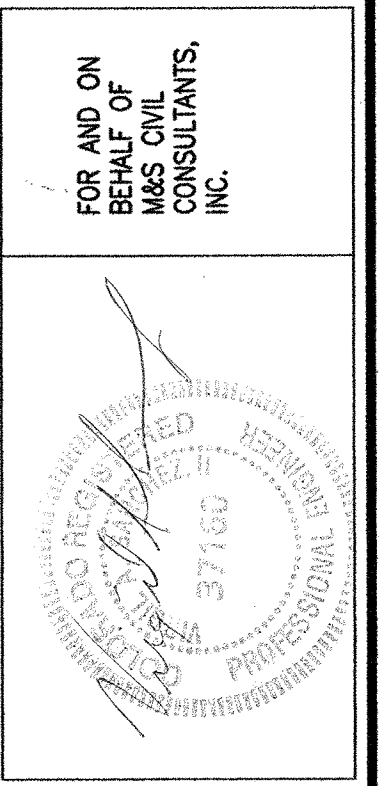
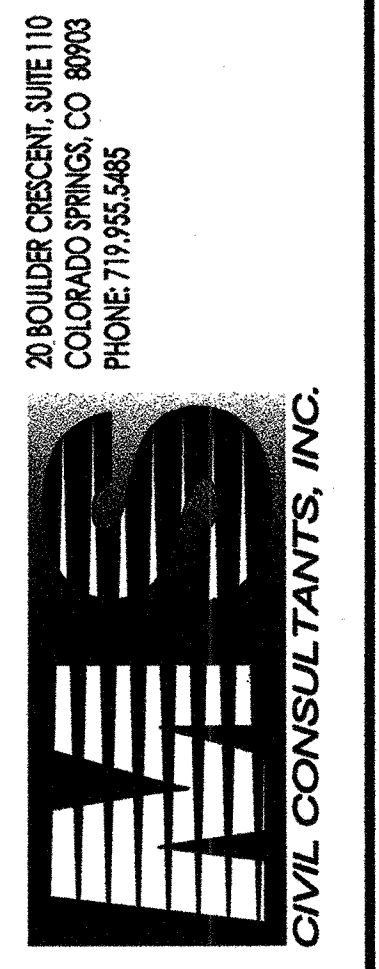


STREET DESIGN:
REVIEW:
TRAFFIC ENGINEERING: DATE: 9/18/15
CURB & GUTTER: DATE: 9/18/15
FINAL REVIEW: *See indiv. sheets* DATE:
DRAINAGE DESIGN:
DRAINAGE REVIEW: DATE:
FILED IN ACCORDANCE WITH SECTION 7-7-906 OF COLORADO SPRINGS CODE 2001, AS AMENDED.

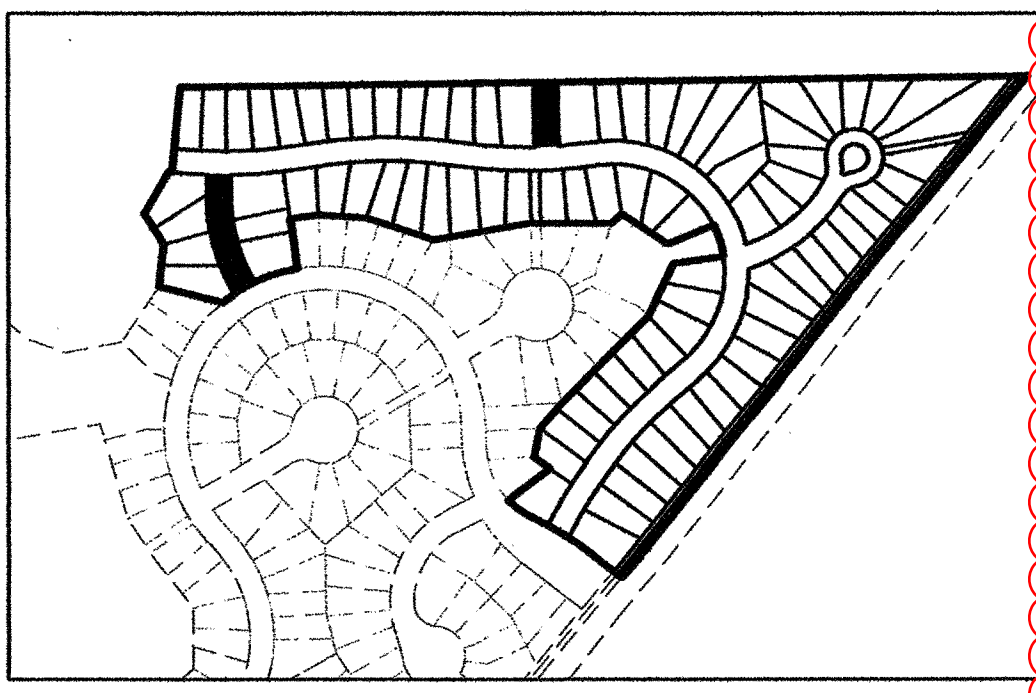
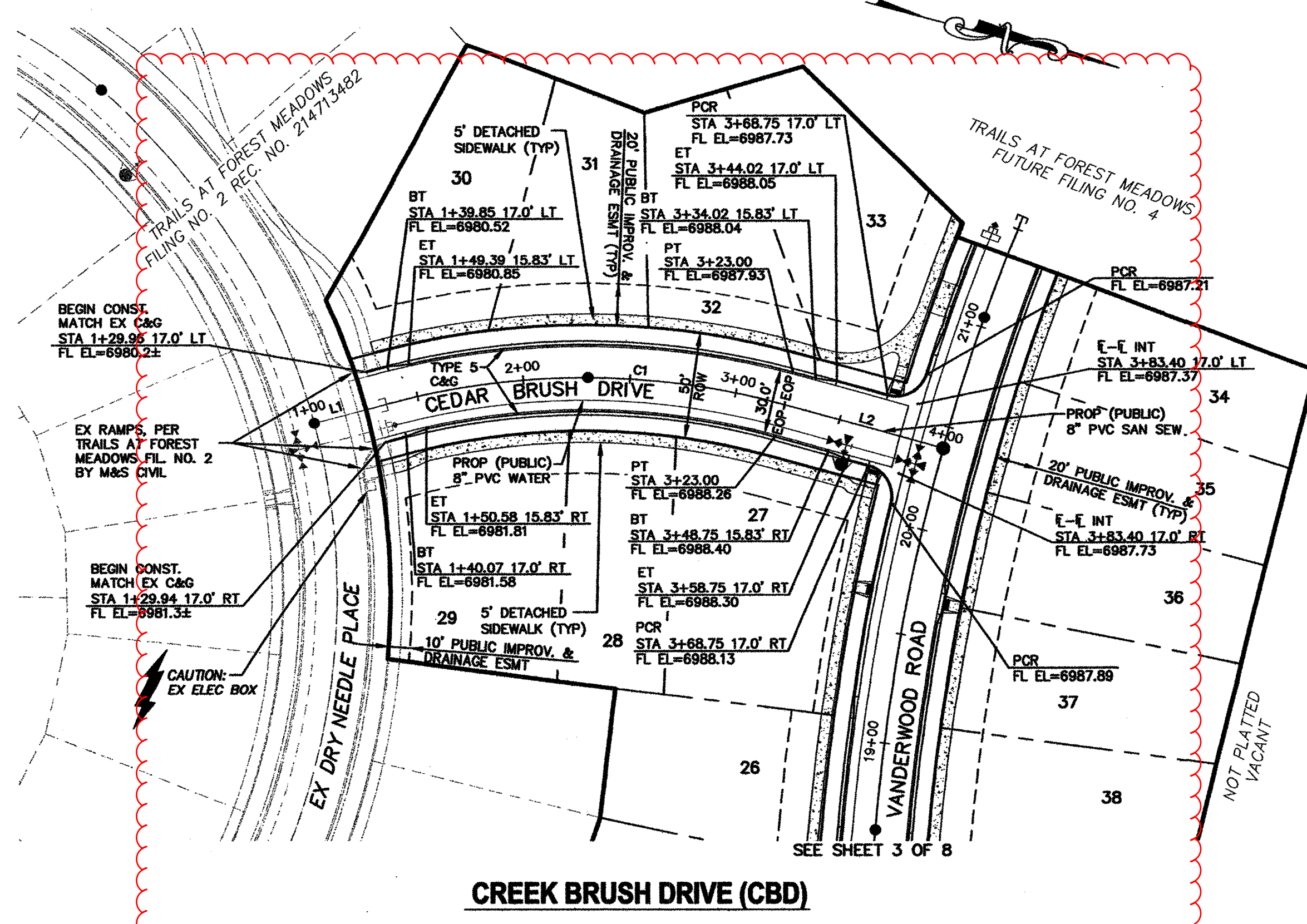
DESIGN DATA:
SIDEWALKS: WIDTH 5' FULL DEPTH ASPHALT
LOCATION: Attached AC Surface
DRAINAGE: DETACHED OR CENTERED IN 5' EASEMENT
CURB TYPE: 1 1/2" Class 6
CURB TYPE: 5 1/2" Class 5
ROW WIDTH: 50' EOP-EOP 30'
STREET TYPE: RES HVEEM Class 2

NO.	DATE	BY	DESCRIPTION

TRAILS AT FOREST MEADOWS FILING NO. 3
STREET IMPROVEMENT PLANS COVER SHEET
PROJECT NO. 08-029 FILE: Virg Cons - Draw - Street Improv... (S01).dwg
DESIGNED BY: GW SCALE: N/A
DRAWN BY: BB HORIZ: N/A
CHECKED BY: VAS VERT: N/A
SHEET 1 OF 8
S101

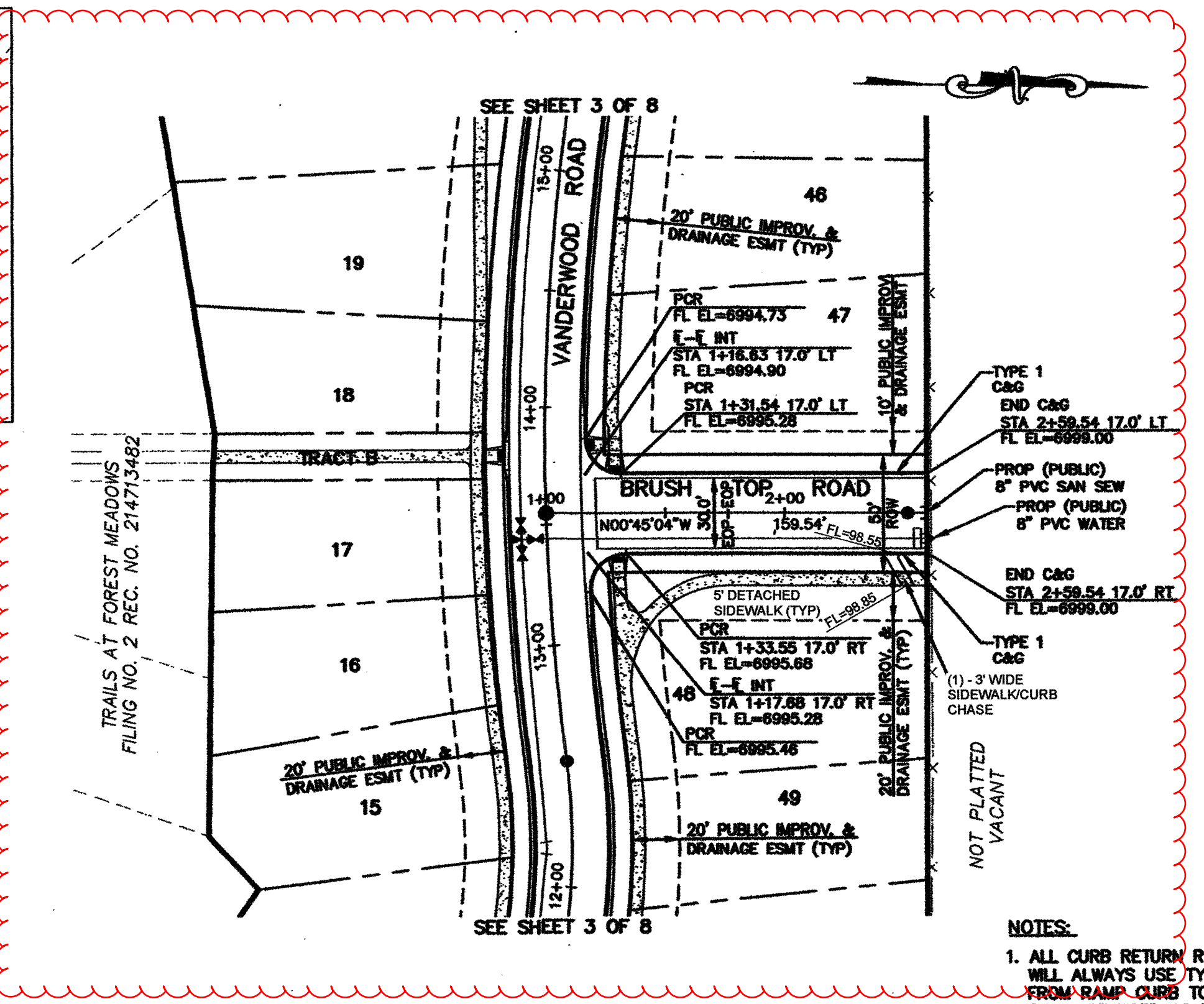
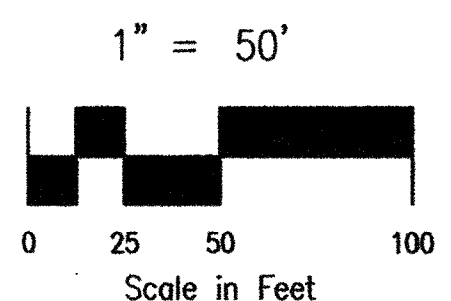


THE ENGINEER PREPARING THESE PLANS WILL NOT BE RESPONSIBLE FOR UNAUTHORIZED CHANGES TO OR ERRORS IN THESE PLANS. ALL CHANGES TO THE PLANS MUST BE IN WRITING AND MUST BE APPROVED BY THE PREPARER OF THESE PLANS.
CAUTION



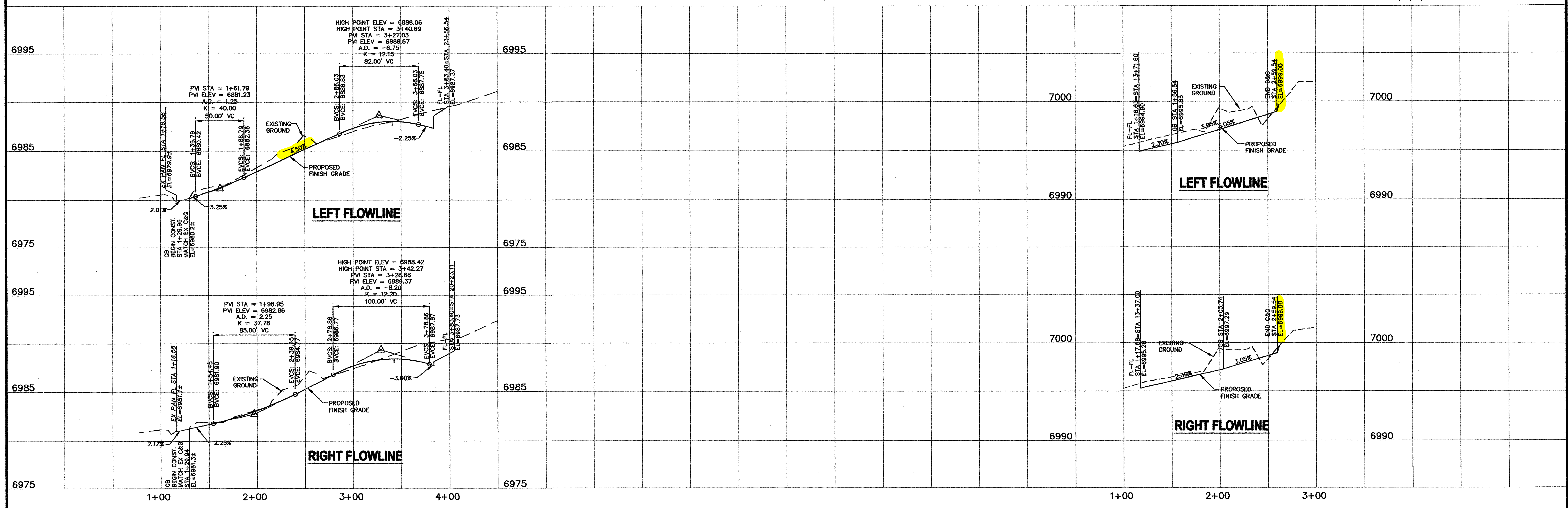
LINE TABLE		
LINE	LENGTH	BEARING
L1	37.44'	N29°53'25"W
L2	77.26'	N00°29'11"E

CURVE TABLE			
CURVE	DELTA	RADIUS	LENGTH
C1	30°22'36"	350.00'	185.56'



- STREET ABBREVIATIONS**
- VR VANDERWOOD ROAD
 - VR-2 VOLLMER ROAD
 - CBC CEDAR BRUSH COURT
 - BTR BRUSH TOP ROAD
 - CBD CREEK BRUSH DRIVE
 - DNP DRY NEEDLE PLACE

- NOTES:**
- ALL CURB RETURN RADIUS SHALL BE 15.00'. CURB RETURNS WILL ALWAYS USE TYPE 1 VERTICAL CURB. WHEN TRANSITIONING FROM RAMP CURB TO VERTICAL CURB A 20 FOOT TRANSITION SHALL BE USED AS FOLLOWS: BEGINNING AT THE P.T.C.R., TEN FEET OF VERTICAL CURB AND 10 FEET OF TRANSITION SECTION.
 - ALL SIDEWALKS SHALL BE 5' WIDE AND DETACHED UNLESS OTHERWISE STATED.
 - ALL CROSS PANS SHALL BE CITY STANDARD D-7 (6" PAN) AS SHOWN.
 - ALL PED RAMP LOCATED AT INTERSECTIONS SHALL BE CITY STD D-8A AND ALL MID STREET PED RAMP SHALL BE CITY STD D-8D.
 - DRIVEWAYS FOR LOTS 1, 33, 75, & 87 SHALL BE PER CITY STANDARD D-16



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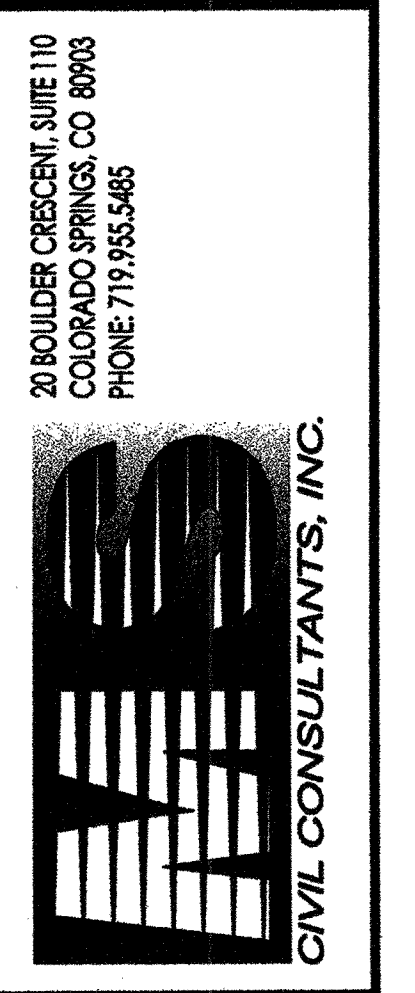


STREET DESIGN:
REVIEW: _____ DATE: _____
TRAFFIC ENGINEERING: _____ DATE: 9/18/15
CURB & GUTTER: _____ DATE: 10/21/15
FINAL REVIEW: _____ DATE: _____
DRAINAGE DESIGN: _____ DATE: _____
DRAINAGE REVIEW: _____ DATE: _____
FILED IN ACCORDANCE WITH SECTION 7-7-906 OF COLORADO SPRINGS CODE 2001, AS AMENDED.

DESIGN DATA:

SIDEWALKS: WIDTH 5' FULL DEPTH ASPHALT
 LOCATION: Attached AC Surface
 Detached CENTERED IN 5' EASEMENT AC Base
 CURB TYPE: 1 AGG. BASE THICKNESS: 4"
 CURB TYPE: 5 Class 6
 ROW WIDTH: 50' EOP-EOP: 30' Class 5
 STREET TYPE: RES HVEEM Class 2

TRAILS AT FOREST MEADOWS FILING NO. 3
STREET IMPROVEMENT ~ CREEK BRUSH CT/BRUSH TOP RD
PROJECT NO. 08-028 FILE: Vwg/Cons./Draw./Street Improv./S105.dwg
DESIGNED BY: GW SCALE: DATE: 8-05-15
DRAWN BY: BB HORIZ: 1"=50'
CHECKED BY: VAS VERT: 1"=5'



FOR AND ON BEHALF OF CIVIL CONSULTANTS, INC.
Virgil A. Sanchez, Colorado P.E. No. 37160

NO.	DATE	BY	DESCRIPTION

THE ENGINEER PREPARING THESE PLANS WILL NOT BE RESPONSIBLE, OR LIABLE FOR, UNAUTHORIZED CHANGES TO OR USES OF THESE PLANS. ALL CHANGES TO THE PLANS MUST BE IN WRITING AND MUST BE APPROVED BY THE PREPARER OF THESE PLANS.

CAUTION

TRAILS AT FOREST MEADOWS FILING NO. 4 FINAL DRAINAGE REPORT

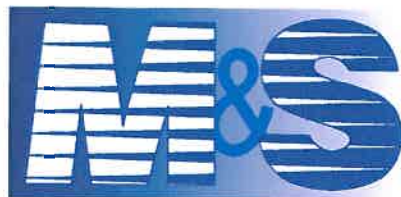
**AMENDMENT TO:
MASTER DEVELOPMENT DRAINAGE PLAN UPDATE FOR WOODMEN HEIGHTS
AND FINAL DRAINAGE REPORT FOR FOREST MEADOWS FILING NO.1AND NO.4**

April 2016

Prepared for:

Challenger Homes, Inc.
13530 Northgate Estates Drive, Suite 200
Colorado Springs, CO 80921
(719) 598-5192

Prepared by:



CIVIL CONSULTANTS, INC.
20 Boulder Crescent, Suite 110
Colorado Springs, CO 80903
(719) 955-5485

Project #08-032

ranges from 12 to 14 inches per year, with the majority of this moisture occurring in the spring and summer in the form of rainfall. Thunderstorms are common during the summer months.

FLOODPLAIN STATEMENT

According to the Federal Emergency Management Agency (FEMA) Flood Insurance Rate Map (FIRM) Panel No. 08041C0529, effective date March 17, 1997, no portion of the site lies within a designated floodplain.

DRAINAGE CRITERIA

The drainage analysis has been prepared in accordance with the current City of Colorado Springs/El Paso County Drainage Criteria Manual. Calculations were performed to determine runoff quantities during the 5-year and 100-year frequency storms for developed conditions using the Rational Method as required for basins having areas less than 100 acres.

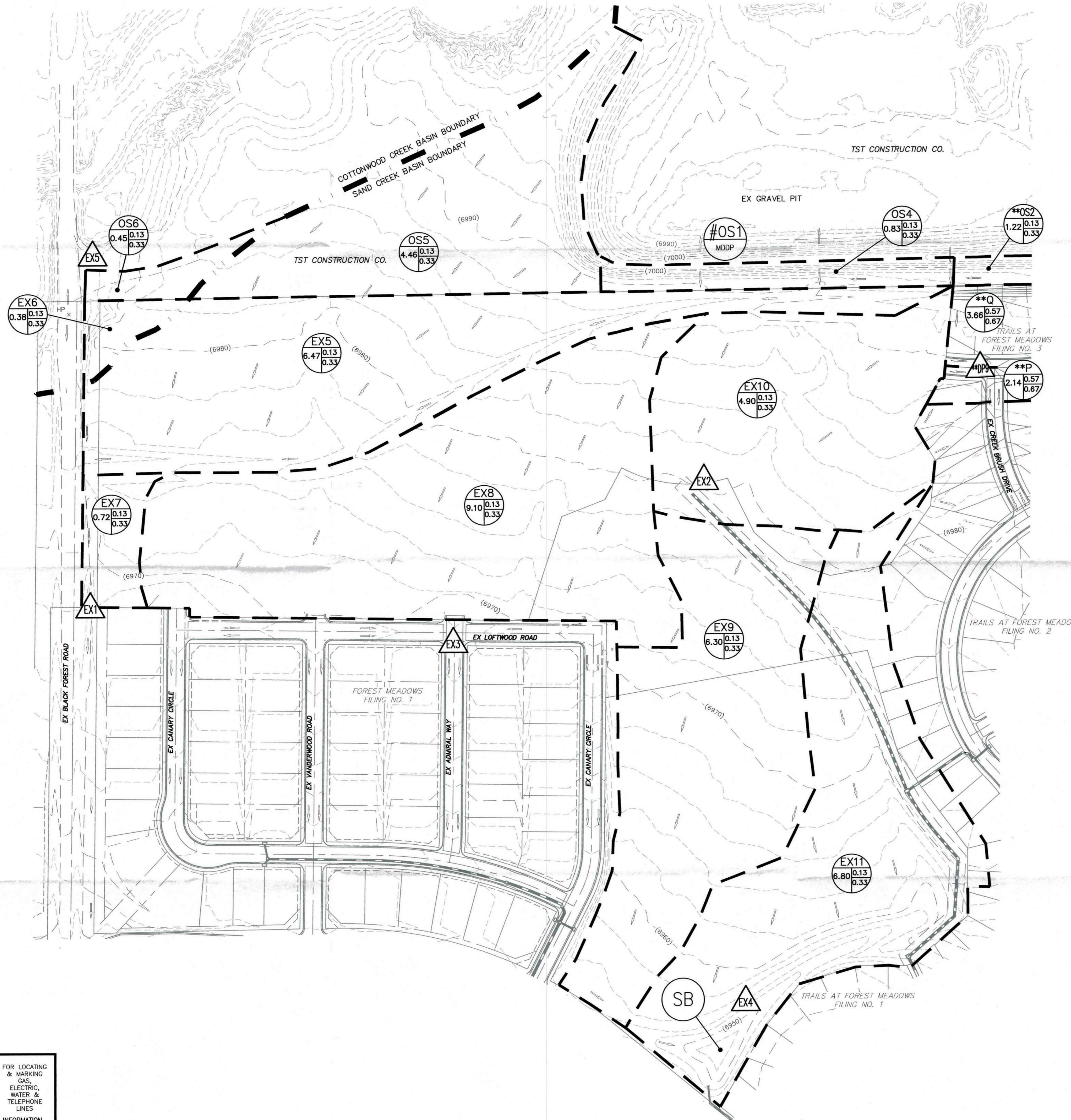
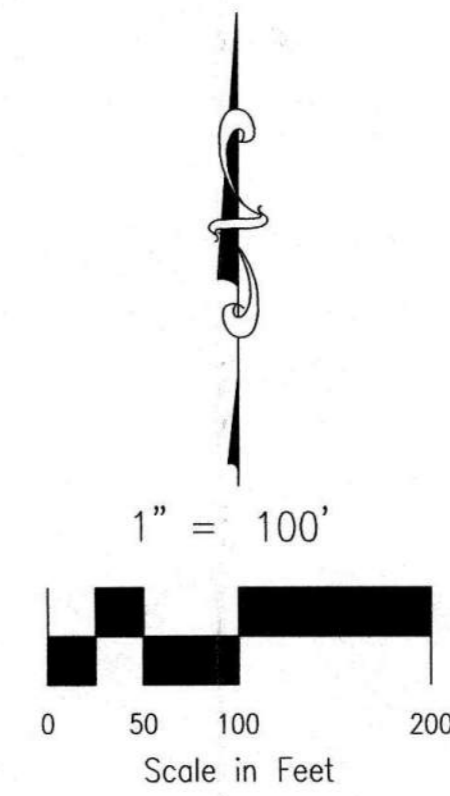
EXISTING DRAINAGE CONDITIONS

The overall site consists of 20.514 acres and is currently undeveloped, with the initial grading project proposed to disturb 20.514 acres for Filing No. 4 residential subdivision. Filing No.4 proposes 90 single family residential lots. All of the streets, curb, gutter, sidewalk and utilities for the development of Vanderwood Road, Oak Vine Court, Salt Brush Road, Leaf Wood Court and Admiral Way, will be constructed in Filing No. 4.

In order to compare past studies, a portion of the drainage basins within this study are denoted by asterisks. The drainage basins labels preceded (or followed) by an single hashtag (#) are referencing watersheds previously illustrated and/or described within the "Master Development Drainage Plan Update for Woodmen Heights and Final Drainage Report for Forest Meadows Filing No.1 & No.4" (MDDP), by Classic Consulting Engineers, & Surveyors, dated February 2006. Those drainage basins labels preceded (or followed) by two asterisks (**) are referencing watersheds previously illustrated and/or described within the "Trails at Forest Meadows Filing No. 3 Final Drainage Report"(TFM 3 FDR), by M&S Civil Consultants, Inc., dated September 2015.

Per review of the existing topographic drainage patterns, the off-site historic flows, north of the property (OS1), are conveyed west by an existing berm and swale to an existing gravel borrow pit, as evident by the eroded embankment at the southeast corner of the gravel borrow pit and evaluation of grade during onsite visits. Per the "Master Development Drainage Plan for Woodmen Heights Master Plan" prepared by Classic Consulting Engineers and Surveyors, dated June 2004, it was inferred that the entire watershed (historic flows of Q5=65 cfs and Q100=162 cfs) would be transported to the future detention facility through our site. This report was amended by the "Master Development Drainage Plan Update for Woodmen Heights and Final Drainage Report for Forest Meadows Filing No.1 and No. 4" (MDDP) by Engineering and Surveying, Inc., dated February 2006, in which it states that 50% of the flow from OS1 (Q5=34 cfs, Q100=84 cfs) will be collected by a proposed concrete pipe and will be conveyed through and combined with the flows of Trails at Forest Meadows Filings to Sand Creek Regional Detention Facility No. 6. Per historic drainage patterns and per the "Preliminary/Final Drainage Report for Highland Park Filing No.2", prepared by Law and Mariotti Consultants, dated June 2002, which is referenced in the MDDP, the remainder of the flows will be transported via road side swale on the west side of Vollmer Road to the proposed drainage infrastructure in Vollmer Road. The flows on Vollmer Road were addressed in the "Trails at Forest Meadows Filing No. 3 Final Drainage Report"(TFM 3 FDR). Any increase in flows due to future development of Basin OS1 will require the construction of a proposed detention facility, as per the Sand Creek DBPS.

In the interim, Historic flows **OS2-Q5=0.8 cfs and Q100=3.6 cfs, OS4-Q5=0.4 cfs and Q100=1.8 cfs, OS5-Q5=2.1 cfs and Q100=9.0 cfs, EX5- Q5=1.8 cfs and Q100=7.5 cfs, EX7- Q5=0.3 cfs and Q100=1.1 cfs, see



LEGEND

- SEDIMENT BASIN
- PIPE RUN REFERENCE LABEL
- SURFACE DESIGN POINT
- BASIN BOUNDARY
- EXISTING CONTOUR
- PROPOSED CONTOUR
- STORM SEWER PIPE
- CROSSSPAN
- INLET
- BASIN DESIGNATION
- EXISTING FLOW DIRECTION ARROW
- EMERGENCY OVERTFLOW DIRECTION
- FLOW DIRECTION
- FLARED END SECTION
- PERIMETER SWALE
- FILING LINE
- 11 LOT NUMBER
- 2.5% STREET GRADE W/DIRECTION
- H.P. X HIGH POINT
- L.P. X LOW POINT

BASIN SUMMARY			
BASIN	AREA (ACRES)	Q5	Q100
#OS1	78	34.4	84.1
**OS2	1.22	0.8	3.6
OS4	0.83	0.4	1.8
OS5	4.46	2.1	9.0
OS6	0.45	0.1	0.6
EX5	6.47	1.8	7.5
EX6	0.38	0.2	0.6
EX7	0.72	0.3	1.1
EX8	9.10	3.1	13.3
EX9	6.30	1.7	7.4
EX10	4.90	1.5	6.4
EX11	6.80	1.5	6.3
**P	2.14	4.2	8.8
**Q	3.66	6.1	12.8

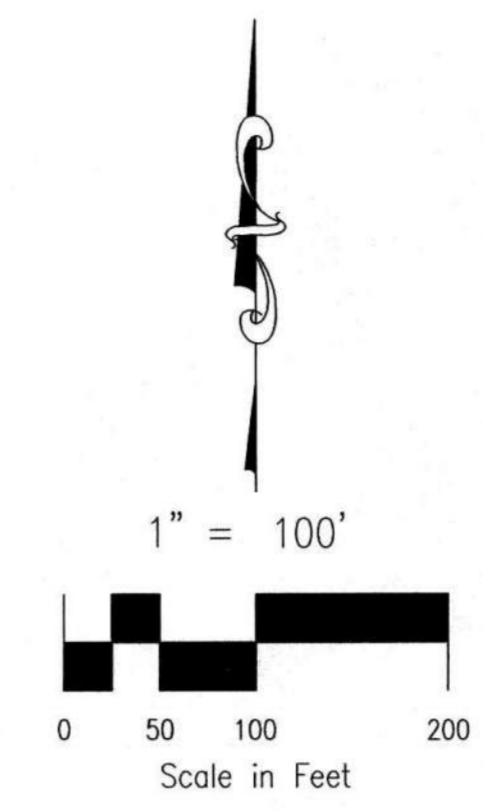
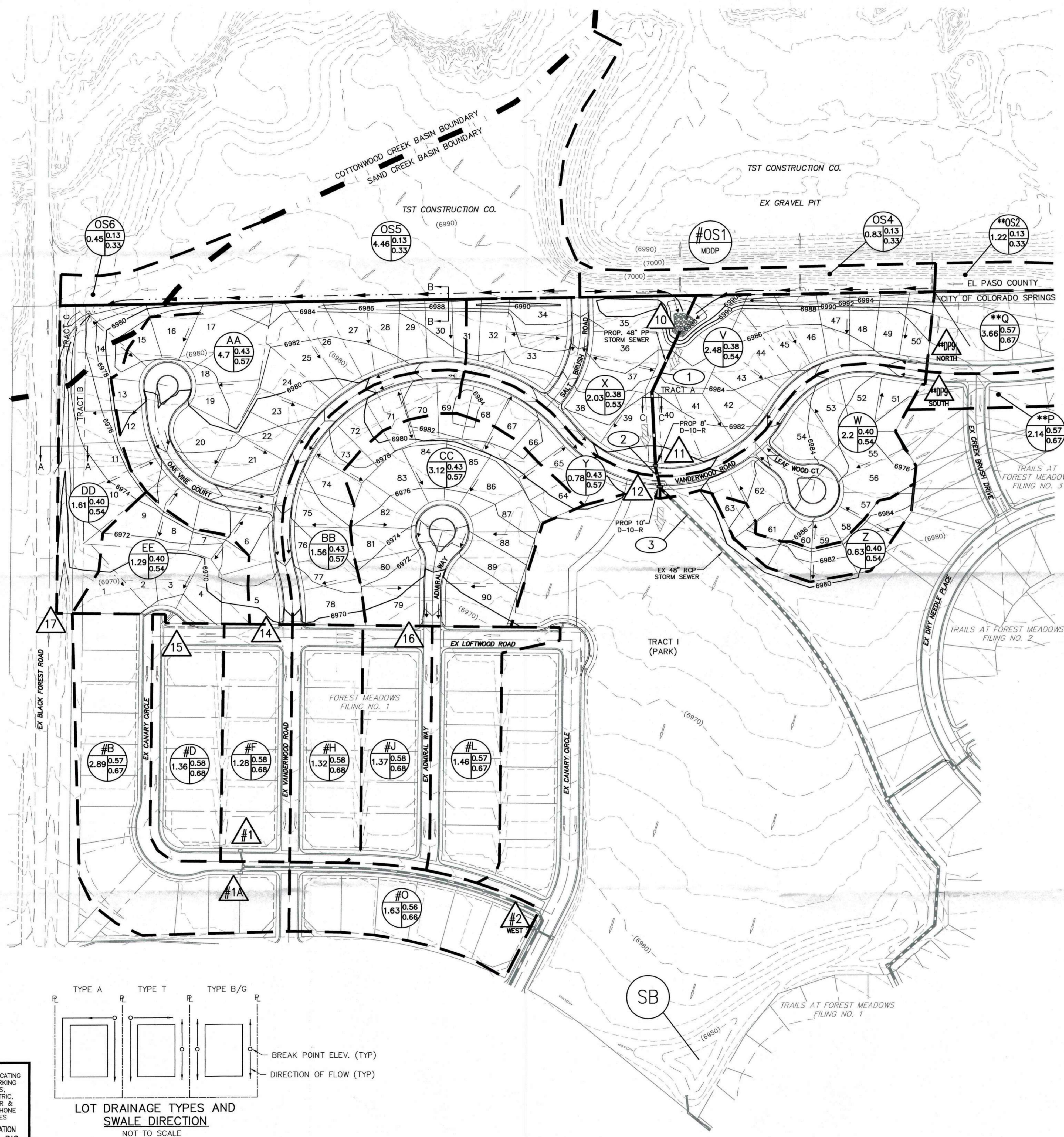
DESIGN POINT SUMMARY			
DESIGN POINT	Q5	Q100	BASIN
DP9	10.2	22.4	**DP90,DP9P
EX1	3.7	16.7	**OS2,OS4,OS5,EX5,EX7
EX2	11.5	28.5	**DP9,EX10
EX3	3.1	13.3	EX8
EX4	3.0	13.4	EX9,EX11
EX5	0.3	1.2	OS6,EX6

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FOR BURIED UTILITY INFORMATION 48 HRS BEFORE YOU DIG CALL 1-800-922-1987

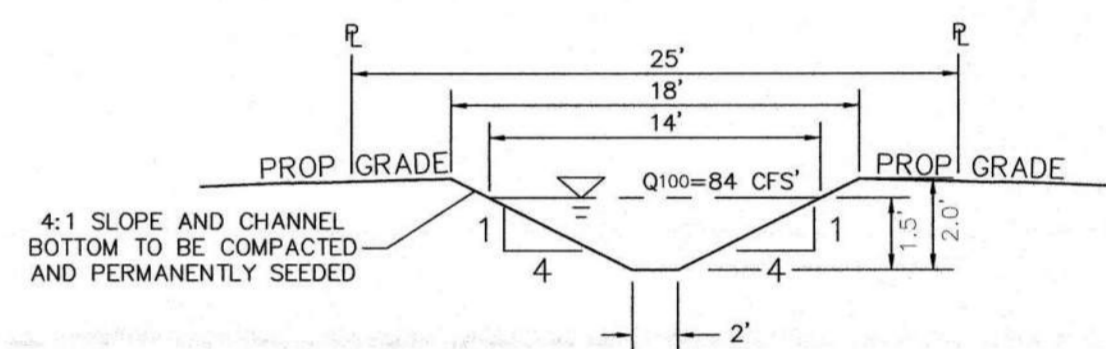
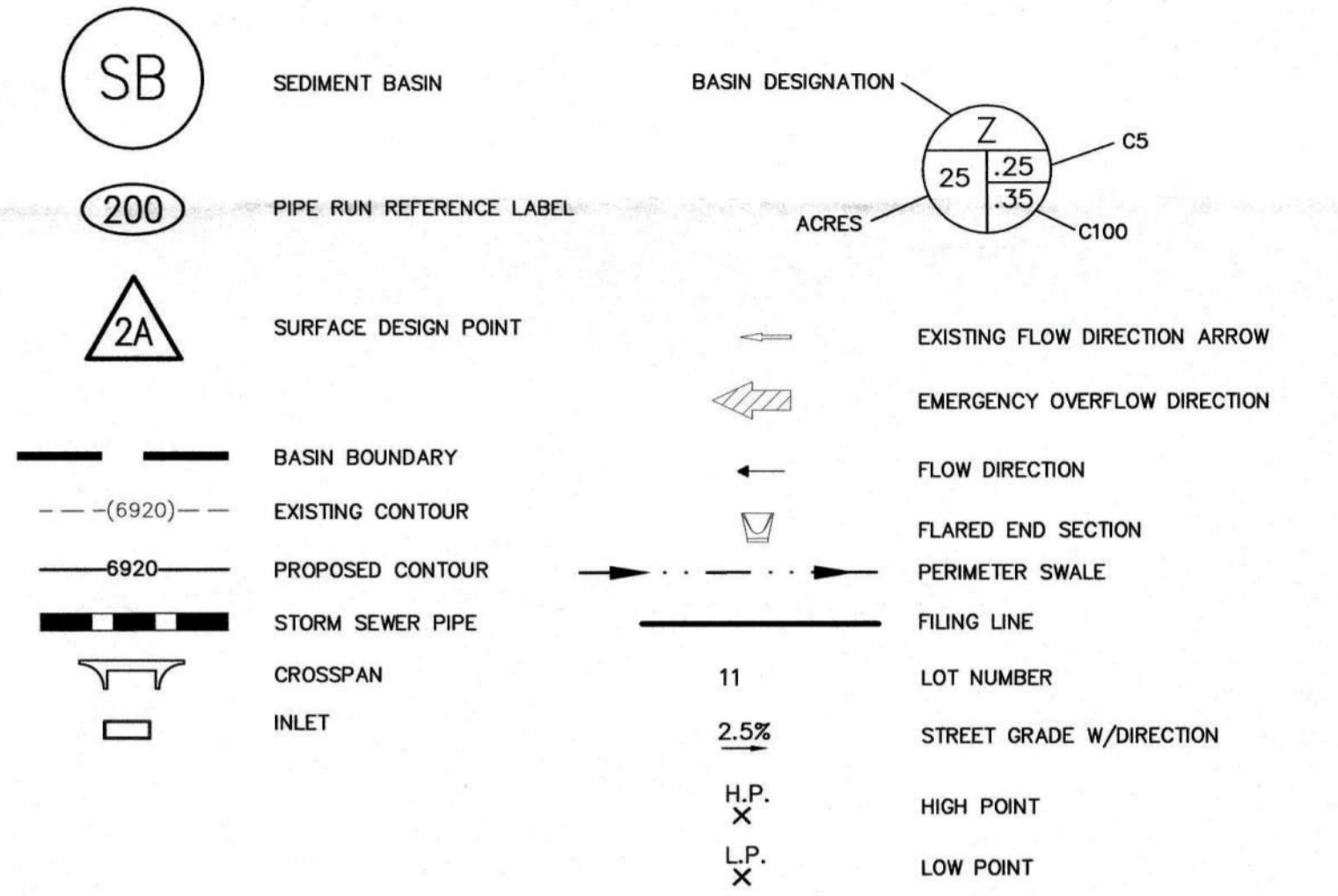
20 BOULDER CRESCENT, SUITE 110
COLORADO SPRINGS, CO 80903
PHONE: 719.955.5485

TRAILS AT FOREST MEADOWS FILING NO. 4
EXISTING DRAINAGE PLAN

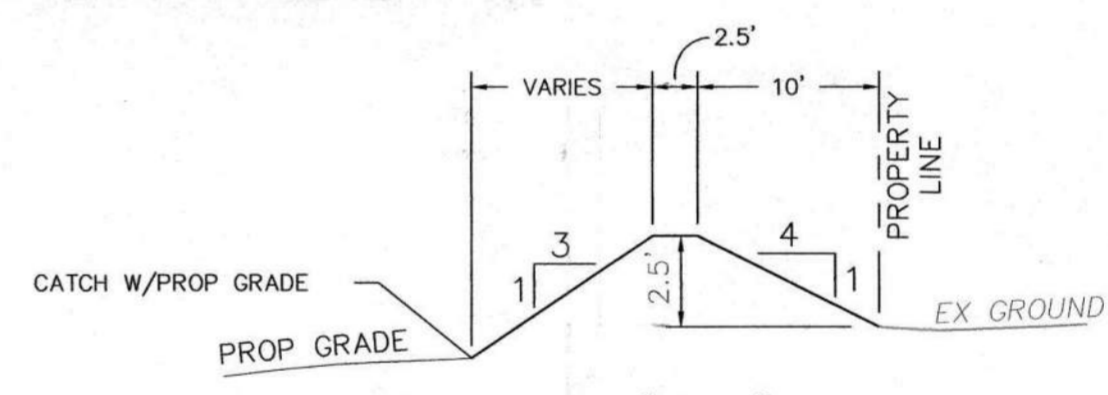
PROJECT NO. 08-032	FILE: \\dwg\Eng Exhibits\DP1.dwg	DATE: 3/28/16
DESIGNED BY: ET	SCALE: N/A	SHEET 1 OF 2
DRAWN BY: BB	HORIZ: 1"=100'	
CHECKED BY: ET	VERT: N/A	DP1



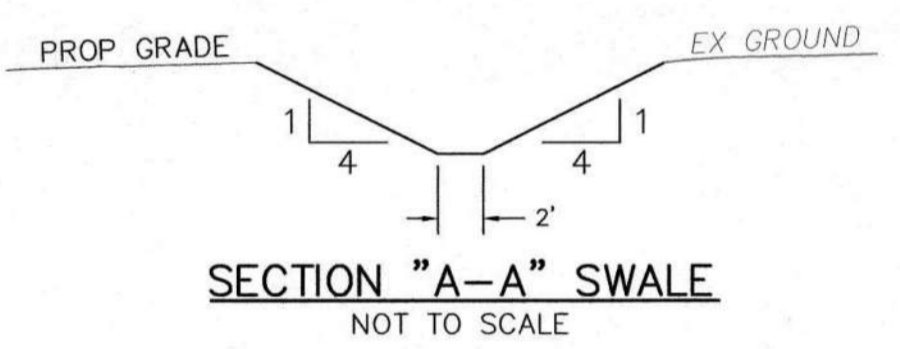
LEGEND



SECTION "C-C" OVERFLOW SWALE
NOT TO SCALE



SECTION "B-B" BERM
NOT TO SCALE

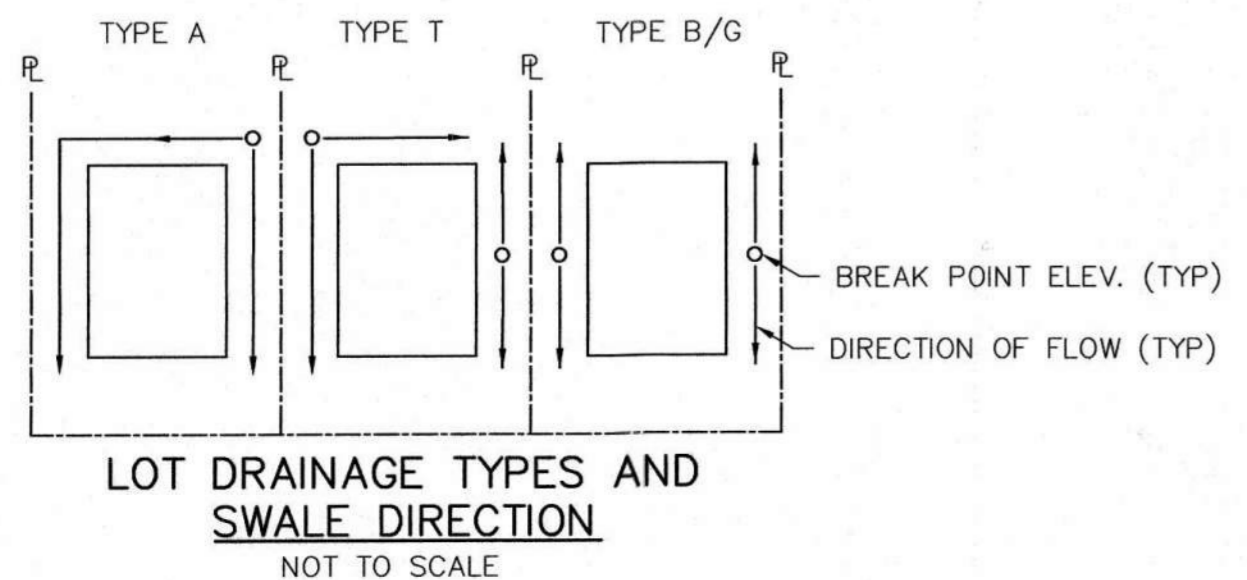


SECTION "A-A" SWALE
NOT TO SCALE

BASIN SUMMARY			
BASIN	AREA (ACRES)	Q5	Q100
V	2.48	3.2	7.6
W	2.20	3.1	7.1
X	2.03	2.7	6.4
Y	0.78	1.2	2.8
Z	0.63	1.2	2.7
AA	4.70	7.2	15.9
BB	1.56	2.4	5.3
CC	3.12	5.1	11.3
DD	1.61	2.6	5.8
EE	1.29	2.3	5.3
OS4	0.83	0.4	1.8
OS5	4.46	2.1	9.0
OS6	0.45	0.1	0.6
#OS1	78.0	34.4	84.1
**OS2	1.22	0.8	3.6
**P	2.14	4.2	8.8
**Q	3.66	6.1	12.8
#B	2.89	6.4	13.4
#D	1.36	3.3	7.0
#F	1.28	3.0	6.3
#H	1.32	3.1	6.5
#J	1.37	3.2	6.8
#L	1.46	3.4	7.0
#O	1.63	3.6	7.6

DESIGN POINT SUMMARY			
DESIGN POINT	Q5	Q100	BASIN
**DP9 NORTH	6.1	12.8	**DP9Q
**DP9 SOUTH	3.6	7.5	**DP9P
10	1.0	4.7	OS4,**OS2
11	11.0	25.2	**DP9Q,V,X
12	7.5	16.8	**DP9Q,W,Y
11-12	18.1	41.1	**DP9Q,**DP9P,V,X,W,Y
14	9.4	22.1	AA,BB
15	2.3	5.3	EE
#1 & #1A	22.9	50.7	AA,BB,EE,#B,#D,#F,#H
16	5.0	11.9	CC
#2 WEST	12.9	28.2	CC,#J,#L,#O
17	4.2	14.5	OS5,OS6,DD

STORM SEWER SUMMARY			
PIPE RUN	Q5	Q100	PIPE SIZE
1	34.4	84.1	48" PP
2	41.3	100.0	48" PP
3	45.8	110.0	EX 48" RCP



LOT DRAINAGE TYPES AND SWALE DIRECTION
NOT TO SCALE

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20 BOULDER CRESCENT, SUITE 110
COLORADO SPRINGS, CO 80903
PHONE: 719.955.5485

TRAILS AT FOREST MEADOWS FILING NO. 4

PROPOSED DRAINAGE PLAN

PROJECT NO. 08-032	FILE: \\dwg\Eng Exhibits\DP2.dwg	DATE: 3/28/16	SHEET 2 OF 2	DP2
DESIGNED BY: ET	SCALE: HORIZ: 1"=100'	VERT: N/A		
DRAWN BY: BB				
CHECKED BY: ET				

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**Cottonwood Creek
Drainage Basin Planning Study**

City of Colorado Springs and El Paso County

**APPENDIX B
SUPPORTING DOCUMENTATION**

JUNE 9, 1994

COTTONWOOD CREEK DBPS - TABLE 3
CHANNEL & CULVERT RECOMMENDATIONS

PAGE 81
09-Jun-94

REACH	HEC-1 FLOW w/det. (CFS)	CHANNEL OR CULVERT LENGTH (FT)	EXISTING IMPROVEMENT	RECOMMENDED IMPROVEMENT	TOTAL BOTTOM WIDTH (FT)	TOTAL DEPTH (FT)
21 TO DESIGN POINT 20	11,173	1,800	NATURAL	NATURAL EXCEPT PROVIDE BURIED RIPRAP & GRADE CONTROL AT I-25 BRIDGES ONLY (500' & 2 DROPS)	50	14.0
20 TO DESIGN POINT 19	11,112	2,400	NATURAL	NATURAL EXCEPT PROVIDE GABION WALLS & GRADE CONTROL AT BRIDGES (600') & PORTIONS OF SOUTH BANK (1,550')	40	15.0
19 TO DESIGN POINT 19.2	11,127	1,500	NATURAL	NATURAL EXCEPT PROVIDE GABION WALLS & GRADE CONTROL FOR PORTIONS OF SOUTH BANK (300') & NORTH BANK (500')	40	15.0
19.2 TO DESIGN POINT 19.1	11,127	700	NATURAL	NATURAL BOTTOM WITH BURIED RIPRAP BANKS & GRADE CONTROL (WITH 3 DROPS)	40	16.0
19.1 TO DESIGN POINT 18	11,127	1,200	P.LINED	NO IMPROVEMENT REQUIRED	80	12.0
18 TO DESIGN POINT 18.1	10,000	400	P.LINED	NO IMPROVEMENT REQUIRED	115	12.0
18.1 TO DESIGN POINT 17	10,000	2,000	NATURAL	NATURAL BOTTOM WITH BURIED RIPRAP BANKS & GRADE CONTROL (WITH 12 DROPS)	115	12.0
17 TO DESIGN POINT 17.2	9,837	1,000	P.LINED	NATURAL BOTTOM WITH BURIED RIPRAP BANKS & GRADE CONTROL (WITH 5 DROPS)	115	12.0
17.2 TO DESIGN POINT 17.1	9,837	1,100	P.LINED	NO IMPROVEMENT REQUIRED	115	9.0
17.1 TO DESIGN POINT 16	9,837	1,000	NATURAL	NATURAL BOTTOM WITH BURIED RIPRAP BANKS & GRADE CONTROL (WITH 2 DROPS)	100	11.0
16 TO DESIGN POINT 15	9,416	2,500	P.LINED	LOWER CHANNEL BOTTOM BY NATURAL EROSION WITH PHASED BURIED RIPRAP BANKS & GRADE CONTROL (WITH 2 DROPS)	150	8.0
15 TO DESIGN POINT 14	8,790	1,400	P.LINED	INCREASE DEPTH OF BURIED RIPRAP LINING ON NORTH SIDE & GRADE CONTROL (WITH 4 DROPS)	150	7.5
14 TO DESIGN POINT 14.1	8,598	1,300	P.LINED	NO IMPROVEMENT REQUIRED	200	8.0
14.1 TO DESIGN POINT 13	8,598	1,000	P.LINED	INCREASE DEPTH OF BURIED RIPRAP LINING ON NORTH SIDE	200	6.5
13 TO DESIGN POINT 13.2	4,702	2,000	P.LINED	REED BURIED RIPRAP LINING ON SOUTH SIDE & GRADE CONTROL (WITH 3 DROPS)	200	5.0
13.2 TO DESIGN POINT 13.1	4,702	1,100	P.LINED	REED BURIED RIPRAP LINING ON SOUTH SIDE & GRADE CONTROL (WITH 3 DROPS)	105	7.0
13.1 TO DESIGN POINT 12	4,702	2,300	NATURAL	NATURAL BOTTOM WITH BURIED RIPRAP BANKS & GRADE CONTROL (WITH 5 DROPS)	105	7.0
12 TO DESIGN POINT 11	4,026	5,500	NATURAL	NATURAL BOTTOM WITH BURIED RIPRAP BANKS & GRADE CONTROL (WITH 16 DROPS)	80	8.0
11 TO DESIGN POINT 10	3,008	1,100	NATURAL	NATURAL BOTTOM WITH BURIED RIPRAP BANKS & GRADE CONTROL (WITH 3 DROPS)	80	6.5
10 TO DESIGN POINT 9	2,531	1,800	NATURAL	NATURAL BOTTOM WITH BURIED RIPRAP BANKS & GRADE CONTROL (WITH 4 DROPS)	80	6.5
9 TO DESIGN POINT 8	2,332	3,000	NATURAL	NATURAL BOTTOM WITH GRASS/SHRUB BANKS & GRADE CONTROL (WITH 10 DROPS)	80	6.5
8 TO DESIGN POINT 7	1,715	3,500	NATURAL	NATURAL BOTTOM WITH GRASS/SHRUB BANKS & GRADE CONTROL (WITH 12 DROPS)	80	5.0
7 TO DESIGN POINT 6	854	3,500	NATURAL	NATURAL BOTTOM WITH GRASS/SHRUB BANKS & GRADE CONTROL (WITH 9 DROPS)	50	4.5
6 TO DESIGN POINT 5	673	7,000	NATURAL	NATURAL BOTTOM WITH GRASS/SHRUB BANKS & GRADE CONTROL (WITH 12 DROPS)	50	4.0
5 TO DESIGN POINT 4	870	3,000	VEG. LINING	GRADE CONTROL (7 DROPS)	50	4.0
4 TO DESIGN POINT 3	467	3,500	VEG. LINING	GRADE CONTROL (12 DROPS)	20	4.5
3 TO DESIGN POINT 2	335	3,500	VEG. LINING	GRADE CONTROL (11 DROPS)	20	4.0
2 TO DESIGN POINT 1	114	2,300	NATURAL	NATURAL BOTTOM WITH GRASS/SHRUB BANKS & GRADE CONTROL (WITH 5 DROPS)	20	3.0
T4B TO DESIGN POINT 19G	528	1,700	STORM/NAT.	STORM SEWER FROM EXISTING 48" CMP OUTLET DOWNSTREAM TO MAIN CHANNEL	72" RCP	N/A
19E TO DESIGN POINT 19F	1,560	2,400	CONCRETE	NO IMPROVEMENT REQUIRED	12	6.0
19D TO DESIGN POINT 19E	1,285	3,400	CONCRETE	NO IMPROVEMENT REQUIRED	13	6.0
19B TO DESIGN POINT 19C	810	2,800	CONCRETE	NO IMPROVEMENT REQUIRED	5	5.0
Q1 TO DESIGN POINT 19A	390	2,200	72" PIPE	PARALLEL PIPE (1,650')	36" RCP	N/A
T4A TO DESIGN POINT 18A	260	1,200	48" PIPE	NO IMPROVEMENT REQUIRED	N/A	N/A
17A TO DESIGN POINT 17	312	1,000	66" PIPE	NO IMPROVEMENT REQUIRED	N/A	N/A
T2 TO DESIGN POINT 17A	205	1,200	NATURAL	STORM SEWER	48" RCP	N/A
P2 TO DESIGN POINT 16C	368	2,300	48" PIPE	NO IMPROVEMENT REQUIRED	N/A	N/A
M4 TO DESIGN POINT 16B	492	2,400	P.LINED	NO IMPROVEMENT REQUIRED	N/A	N/A
M3 TO DESIGN POINT 16	291	1,400	36" PIPE	PARALLEL PIPE (1,250')	30" RCP	N/A
M1 TO DESIGN POINT 14C	513	3,000	48" PIPE	PARALLEL PIPE (2,000')	48" RCP	N/A
O1 TO DESIGN POINT 14B	426	3,700	48" PIPE	PARALLEL PIPE (2,600')	48" RCP	N/A
L1 TO DESIGN POINT 14A	371	1,700	42" PIPE	PARALLEL PIPE (1,700')	36"/42" RCP	N/A
J1 TO DESIGN POINT 13S	425	3,100	42" PIPE	PARALLEL PIPE	48" RCP	N/A
13Q TO DESIGN POINT 13R	1,058	750	NATURAL	NATURAL BOTTOM WITH GRASS/SHRUB BANKS & GRADE CONTROL (WITH 1 DROP)	75	4.0

COTTONWOOD CREEK DBPS - TABLE 4 BRIDGE RECOMMENDATIONS			
LOCATION	HEC-1 FLOW w/det. (CFS)	EXISTING IMPROVEMENT	PROPOSED IMPROVEMENT
CDOT BRIDGES			
I-25 (DP 21)	11,173	BRIDGE, T=137,B=113,D=18	REPL. BRIDGES (8 LANES), 2 @ 70' WIDE X 140' LONG
I-25 (DP 31)	5,613	BRIDGE, T=189,B=39,D=43	REPL. BRIDGES (8 LANES), 2 @ 70' WIDE X 190' LONG

CITY BRIDGES			
CORPORATE DRIVE (DP 21)	11,173	BRIDGE, T=123,B=61,D=15.8	NO IMPROVEMENT REQUIRED
VINCENT DRIVE (DP 20)	11,112	BRIDGE, T=209,B=53,D=33.5	REPL. BRIDGE (6 LANE ART.), 107' WIDE BY 210' LONG
CURRENT ACCESS RD (DP 20)	11,112	HORSESHOE - 2 @ 22' x 22'	NO IMPROVEMENT REQUIRED
ACADEMY BLVD (DP 18)	10,000	CBC - 5 @ 20' x 9'	NO IMPROVEMENT REQUIRED
UNION BLVD (DP 16)	9,416	CBC - 7 @ 12' x 6'	REPL. BRIDGE (6 LANE ART.), 107' WIDE BY 150' LONG
RANGEWOOD DRIVE (DP 13)	7,844	CM ARCH - 4 @ 25.5' x 13'	NO IMPROVEMENT REQUIRED
WOODMEN ROAD (DP 12)	4,026	BRIDGE - 118' x 22'	REPL. BRIDGE (8 LANE ART.), 143' WIDE BY 200' LONG
AUSTIN BLUFFS (DP 12)	4,026	N/A	REPL. BRIDGE (8 LANE ART.), 143' WIDE BY 200' LONG
POWERS BLVD (DP 9)	2,332	N/A	TRIPLE 10' X 9' CBC (360')
DUBLIN BLVD (DP 130)	2,414	CMP - 2 @ 132"	ADD PARALLEL 108" CMP
AUSTIN BLUFFS (DP 13J)	3,686	CMP - 2@120"	QUADRUPLE 12' X 9' CBC
RESEARCH PKWY (DP 8G)	1,632	N/A	TRIPLE 14' X 6' CBC
PINE CREEK RD (DP 31)	5,613	BRIDGE, T=185,B=45,D=41	NO IMPROVEMENT REQUIRED
OLD RAILROAD GRADE (DP 31)	5,613	HORSESHOE - 2 @ 25' x 21'	NO IMPROVEMENT REQUIRED
ACADEMY BLVD N (DP SUM13)	2,586	CBC - 10' x 6'	REPLACE WITH TRIPLE 12' X 9' CBC

COUNTY BRIDGES			
BLACK FOREST ROAD (DP 7)	854	BRIDGE, T=40,B=26,D=17	REPL. BRIDGE (5 LANE ART.), 70' WIDE BY 110' LONG

COTTONWOOD CREEK DBPS RESULTS OF BASIN INVENTORY

TABLE 8

REACH	EXISTING PROTECTION	AVAILABLE/ADDITIONAL CAPACITY	EROSION CONSIDERATIONS	WETLAND CONSIDERATIONS	WILDLIFE CONSIDERATIONS	COMPATIBILITY W/ UTILITIES	LAND USE COMPATIBILITY	LAND AVAILABILITY	MULTI-USE OPPORTUNITIES	CAPITAL COST PER ALTERNATIVE	MAINTENANCE CONSIDERATIONS PER ALTERNATIVE	SAFETY OR FLOOD PROTECTION CONSIDERATIONS	COMMENTS	CONCLUSIONS
DES. PT. 9 DES. PT. 10	NATURAL OR VEGETATED CHANNEL 80' W x 10' D, 2:1 SIDE-SLOPE	CAPACITY AVAILABLE FOR FULL FLOW THROUGH HYDROLOGY VELOCITY= 10 TO 20 FPS	MODERATELY ERODIBLE SOIL BOTTOM AND SIDE-SLOPES	MOST LIKELY JURISDICTIONAL WETLANDS ARE PRESENT	MOST LIKELY JURISDICTIONAL WILDLIFE CORRIDORS OR HABITAT ARE PRESENT	PROPOSED MAJOR UTILITY MAIN ON NORTH SIDE OF CHANNEL NEEDS TO BE CONSIDERED IN FINAL DESIGN AND ROW REQUIREMENTS	PAIRS OF OPEN SPACE LAND USES NEXT TO FACILITY	ADJACENT PROPERTY UNDEVELOPED NEXT TO FACILITY	PLANNED TRAIL CORRIDOR PLANNED LINEAR PARK PLANNED UTILITY CORRIDOR	FULL LINE = \$ 447,000 PARTIAL LINE = \$ 313,000 NATURAL = \$ 1,450,000	MAINTENANCE OF ALTERNATIVE A IS NOT PRACTICAL DUE TO HIGH VELOCITIES AND EROSION - OTHER ALTERNATIVES ARE ACCEPTABLE	HIGH VELOCITIES IMPROVED - PRACTICAL ALTERNATIVE MAY NOT BE PRACTICAL SLOPE RANGE IS ACCEPTABLE FOR ALL ALTERNATIVES 100% RAINFALL > 300 CFS		USE ALTERNATIVE B
DES. PT. 8 DES. PT. 9	NATURAL OR VEGETATED CHANNEL 80' W x 10' D, 2:1 SIDE-SLOPE	CAPACITY AVAILABLE FOR FULL FLOW THROUGH HYDROLOGY VELOCITY= 10 TO 20 FPS	MODERATELY ERODIBLE SOIL BOTTOM AND SIDE-SLOPES	LIKELY SOME JURISDICTIONAL WETLANDS ARE PRESENT DETAILED STUDY REQUIRED AT FINAL DESIGN TO DETERMINE EXTENT OF WETLANDS	MAY BE JURISDICTIONAL WILDLIFE CORRIDORS OR HABITAT PRESENT	PROPOSED MAJOR UTILITY MAIN ON NORTH SIDE OF CHANNEL NEEDS TO BE CONSIDERED IN FINAL DESIGN AND ROW REQUIREMENTS	PAIRS OF OPEN SPACE LAND USES NEXT TO FACILITY	ADJACENT PROPERTY UNDEVELOPED NEXT TO FACILITY	PLANNED TRAIL CORRIDOR PLANNED LINEAR PARK PLANNED UTILITY CORRIDOR	FULL LINE = \$ 774,000 PARTIAL LINE = \$ 628,000 NATURAL = \$ 1,840,000	MAINTENANCE OF ALTERNATIVE A IS NOT PRACTICAL DUE TO HIGH VELOCITIES AND EROSION - OTHER ALTERNATIVES ARE ACCEPTABLE	HIGH VELOCITIES IMPROVED - PRACTICAL ALTERNATIVE MAY NOT BE PRACTICAL SLOPE RANGE IS ACCEPTABLE FOR ALL ALTERNATIVES 100% RAINFALL > 300 CFS		USE ALTERNATIVE B
DES. PT. 7 DES. PT. 8	NATURAL OR VEGETATED CHANNEL 80' W x 10' D, 2:1 SIDE-SLOPE	CAPACITY AVAILABLE FOR FULL FLOW THROUGH HYDROLOGY VELOCITY= 10 TO 20 FPS	MODERATELY ERODIBLE BOTTOM SIDE-SLOPES MODERATE IN ROW	LIKELY SOME JURISDICTIONAL WETLANDS ARE PRESENT DETAILED STUDY REQUIRED AT FINAL DESIGN TO DETERMINE EXTENT OF WETLANDS	MAY BE JURISDICTIONAL WILDLIFE CORRIDORS OR HABITAT PRESENT	NO EXISTING OR PROPOSED MAJOR UTILITY MAINS ANTICIPATED	PAIRS OF OPEN SPACE LAND USES NEXT TO FACILITY	ADJACENT PROPERTY UNDEVELOPED NEXT TO FACILITY	PLANNED TRAIL CORRIDOR PLANNED LINEAR PARK	FULL LINE = \$ 742,000 PARTIAL LINE = \$ 505,000 NATURAL = \$ 898,000	SIMILAR MAINTENANCE CONSIDERATIONS FOR ALL THREE ALTERNATIVES	SLOPE RANGE IS ACCEPTABLE FOR ALL ALTERNATIVES VELOCITY RANGE IS ACCEPTABLE FOR ALL ALTERNATIVES 100% RAINFALL > 300 CFS		USE ALTERNATIVE B
DES. PT. 6 DES. PT. 7	NATURAL OR VEGETATED CHANNEL 80' W x 10' D, 2:1 SIDE-SLOPE	CAPACITY AVAILABLE FOR FULL FLOW THROUGH HYDROLOGY VELOCITY= 5 TO 10 FPS	MODERATELY ERODIBLE BOTTOM SIDE-SLOPES MODERATE IN ROW	MOST LIKELY JURISDICTIONAL WETLANDS ARE PRESENT DETAILED STUDY REQUIRED AT FINAL DESIGN STAGE	MOST LIKELY JURISDICTIONAL WILDLIFE CORRIDORS OR HABITAT ARE PRESENT	NO EXISTING OR PROPOSED MAJOR UTILITY MAINS ANTICIPATED	RESIDENTIAL LAND USES NEXT TO FACILITY	ADJACENT PROPERTY UNDEVELOPED NEXT TO FACILITY		FULL LINE = \$ 1,050,000 PARTIAL LINE = \$ 1,837,000 NATURAL = \$ 1,748,000	SIMILAR MAINTENANCE CONSIDERATIONS FOR ALL THREE ALTERNATIVES	SLOPE RANGE IS ACCEPTABLE FOR ALL ALTERNATIVES VELOCITY RANGE IS ACCEPTABLE FOR ALL ALTERNATIVES 100% RAINFALL > 300 CFS		USE ALTERNATIVE B
DES. PT. 5 DES. PT. 6	NATURAL OR VEGETATED CHANNEL 80' W x 10' D, 2:1 SIDE-SLOPE	CAPACITY AVAILABLE FOR FULL FLOW THROUGH HYDROLOGY VELOCITY= 5 TO 10 FPS	MODERATELY ERODIBLE BOTTOM SIDE-SLOPES MODERATE IN ROW	MOST LIKELY JURISDICTIONAL WETLANDS ARE PRESENT DETAILED STUDY REQUIRED AT FINAL DESIGN STAGE	MOST LIKELY JURISDICTIONAL WILDLIFE CORRIDORS OR HABITAT ARE PRESENT	NO EXISTING OR PROPOSED MAJOR UTILITY MAINS ANTICIPATED	RESIDENTIAL LAND USES NEXT TO FACILITY	ADJACENT PROPERTY UNDEVELOPED NEXT TO FACILITY		FULL LINE = \$ 1,148,000 PARTIAL LINE = \$ 940,000 NATURAL = \$ 1,706,000	SIMILAR MAINTENANCE CONSIDERATIONS FOR ALL THREE ALTERNATIVES	SLOPE RANGE IS ACCEPTABLE FOR ALL ALTERNATIVES VELOCITY RANGE IS ACCEPTABLE FOR ALL ALTERNATIVES 100% RAINFALL > 300 CFS	RURAL TYPE SETTING	USE ALTERNATIVE B USE ALTERNATIVE A
DES. PT. 4 DES. PT. 5	NATURAL OR VEGETATED CHANNEL 80' W x 10' D, 2:1 SIDE-SLOPE	CAPACITY AVAILABLE FOR FULL FLOW THROUGH HYDROLOGY VELOCITY= 5 TO 10 FPS	MODERATELY ERODIBLE SOIL BOTTOM AND SIDE-SLOPES	MOST LIKELY JURISDICTIONAL WETLANDS ARE PRESENT DETAILED STUDY REQUIRED AT FINAL DESIGN STAGE	MOST LIKELY JURISDICTIONAL WILDLIFE CORRIDORS OR HABITAT ARE PRESENT	NO EXISTING OR PROPOSED MAJOR UTILITY MAINS ANTICIPATED	RESIDENTIAL LAND USES NEXT TO FACILITY	ADJACENT PROPERTY UNDEVELOPED NEXT TO FACILITY		FULL LINE = \$ 347,000 PARTIAL LINE = \$ 464,000 NATURAL = \$ 797,000	SIMILAR MAINTENANCE CONSIDERATIONS FOR ALL THREE ALTERNATIVES	SLOPE RANGE IS ACCEPTABLE FOR ALL ALTERNATIVES VELOCITY RANGE IS ACCEPTABLE FOR ALL ALTERNATIVES 100% RAINFALL > 300 CFS	RURAL TYPE SETTING	USE ALTERNATIVE A
DES. PT. 3 DES. PT. 4	NATURAL OR VEGETATED CHANNEL 20' W x 4' D, 2:1 SIDE-SLOPE	CAPACITY AVAILABLE FOR FULL FLOW THROUGH HYDROLOGY VELOCITY= 5 TO 10 FPS	MODERATELY ERODIBLE SOIL BOTTOM AND SIDE-SLOPES	LIKELY SOME JURISDICTIONAL WETLANDS ARE PRESENT DETAILED STUDY REQUIRED AT FINAL DESIGN TO DETERMINE EXTENT OF WETLANDS	MAY BE JURISDICTIONAL WILDLIFE CORRIDORS OR HABITAT PRESENT	NO EXISTING OR PROPOSED MAJOR UTILITY MAINS ANTICIPATED	RESIDENTIAL LAND USES NEXT TO FACILITY	ADJACENT PROPERTY UNDEVELOPED NEXT TO FACILITY		FULL LINE = \$ 728,000 PARTIAL LINE = \$ 828,000 NATURAL = \$ 1,216,000	SIMILAR MAINTENANCE CONSIDERATIONS FOR ALL THREE ALTERNATIVES	100% RAINFALL 300 CFS - PRACTICAL ALTERNATIVES ARE STORM SEWER SYSTEMS OR ROADSIDE DITCHES	RURAL TYPE SETTING	USE ALTERNATIVE A
DES. PT. 2 DES. PT. 3	NATURAL OR VEGETATED CHANNEL 20' W x 4' D, 2:1 SIDE-SLOPE	CAPACITY AVAILABLE FOR FULL FLOW THROUGH HYDROLOGY VELOCITY= 5 TO 10 FPS	MODERATELY ERODIBLE SOIL BOTTOM AND SIDE-SLOPES	LIKELY SOME JURISDICTIONAL WETLANDS ARE PRESENT DETAILED STUDY REQUIRED AT FINAL DESIGN TO DETERMINE EXTENT OF WETLANDS	MAY BE JURISDICTIONAL WILDLIFE CORRIDORS OR HABITAT PRESENT	NO EXISTING OR PROPOSED MAJOR UTILITY MAINS ANTICIPATED	RESIDENTIAL LAND USES NEXT TO FACILITY	ADJACENT PROPERTY UNDEVELOPED NEXT TO FACILITY		FULL LINE = \$ 910,000 PARTIAL LINE = \$ 698,000 NATURAL = \$ 401,000	SIMILAR MAINTENANCE CONSIDERATIONS FOR ALL THREE ALTERNATIVES	100% RAINFALL 300 CFS - PRACTICAL ALTERNATIVES ARE STORM SEWER SYSTEMS OR ROADSIDE DITCHES	RURAL TYPE SETTING	USE ALTERNATIVE A
DES. PT. 1 DES. PT. 2	NATURAL OR VEGETATED CHANNEL 20' W x 4' D, 2:1 SIDE-SLOPE	CAPACITY AVAILABLE FOR FULL FLOW THROUGH HYDROLOGY VELOCITY= 5 TO 10 FPS	MODERATELY ERODIBLE SOIL BOTTOM AND SIDE-SLOPES	LIKELY SOME JURISDICTIONAL WETLANDS ARE PRESENT CONTACT WITH CORPS OF OUR REPRESENTATIVE MAY SUFFICE	MOST LIKELY NOT JURISDICTIONAL WILDLIFE CORRIDORS OR HABITAT PRESENT	NO EXISTING OR PROPOSED MAJOR UTILITY MAINS ANTICIPATED	RESIDENTIAL LAND USES NEXT TO FACILITY	ADJACENT PROPERTY UNDEVELOPED NEXT TO FACILITY		FULL LINE = \$ 190,000 PARTIAL LINE = \$ 242,000 NATURAL = \$ 296,000	SIMILAR MAINTENANCE CONSIDERATIONS FOR ALL THREE ALTERNATIVES	100% RAINFALL 300 CFS - PRACTICAL ALTERNATIVES ARE STORM SEWER SYSTEMS OR ROADSIDE DITCHES	RURAL TYPE SETTING	USE ALTERNATIVE A
DES. PT. 5A DES. PT. 5	NATURAL OR VEGETATED CHANNEL 20' W x 4' D, 2:1 SIDE-SLOPE	CAPACITY AVAILABLE FOR FULL FLOW THROUGH HYDROLOGY VELOCITY= 5 TO 10 FPS	MODERATELY ERODIBLE SOIL BOTTOM AND SIDE-SLOPES	MOST LIKELY JURISDICTIONAL WETLANDS ARE PRESENT DETAILED STUDY REQUIRED AT FINAL DESIGN STAGE	MOST LIKELY JURISDICTIONAL WILDLIFE CORRIDORS OR HABITAT ARE PRESENT	NO EXISTING OR PROPOSED MAJOR UTILITY MAINS ANTICIPATED	RESIDENTIAL LAND USES NEXT TO FACILITY	ADJACENT PROPERTY UNDEVELOPED NEXT TO FACILITY		FULL LINE = \$ 333,000 PARTIAL LINE = \$ 418,000 NATURAL = \$ 388,000	SIMILAR MAINTENANCE CONSIDERATIONS FOR ALL THREE ALTERNATIVES	100% RAINFALL 300 CFS - PRACTICAL ALTERNATIVES ARE STORM SEWER SYSTEMS OR ROADSIDE DITCHES	RURAL TYPE SETTING	USE ALTERNATIVE A
DES. PT. B2 DES. PT. 6A	NATURAL OR VEGETATED CHANNEL 20' W x 4' D, 2:1 SIDE-SLOPE	CAPACITY AVAILABLE FOR FULL FLOW THROUGH HYDROLOGY VELOCITY= 5 TO 10 FPS	MODERATELY ERODIBLE SOIL BOTTOM AND SIDE-SLOPES	LIKELY SOME JURISDICTIONAL WETLANDS ARE PRESENT DETAILED STUDY REQUIRED AT FINAL DESIGN STAGE	MAY BE JURISDICTIONAL WILDLIFE CORRIDORS OR HABITAT PRESENT	NO EXISTING OR PROPOSED MAJOR UTILITY MAINS ANTICIPATED	RESIDENTIAL LAND USES NEXT TO FACILITY	ADJACENT PROPERTY UNDEVELOPED NEXT TO FACILITY		FULL LINE = \$ 438,000 PARTIAL LINE = \$ 414,000 NATURAL = \$ 876,000	SIMILAR MAINTENANCE CONSIDERATIONS FOR ALL THREE ALTERNATIVES	100% RAINFALL 300 CFS - PRACTICAL ALTERNATIVES ARE STORM SEWER SYSTEMS OR ROADSIDE DITCHES		USE ALTERNATIVE B
DES. PT. C2 DES. PT. 6A	NATURAL OR VEGETATED CHANNEL 20' W x 4' D, 2:1 SIDE-SLOPE	CAPACITY AVAILABLE FOR FULL FLOW THROUGH HYDROLOGY VELOCITY= 5 TO 10 FPS	MODERATELY ERODIBLE SOIL BOTTOM AND SIDE-SLOPES	LIKELY SOME JURISDICTIONAL WETLANDS ARE PRESENT DETAILED STUDY REQUIRED AT FINAL DESIGN TO DETERMINE EXTENT OF WETLANDS	MAY BE JURISDICTIONAL WILDLIFE CORRIDORS OR HABITAT PRESENT	NO EXISTING OR PROPOSED MAJOR UTILITY MAINS ANTICIPATED	RESIDENTIAL LAND USES NEXT TO FACILITY	ADJACENT PROPERTY UNDEVELOPED NEXT TO FACILITY		FULL LINE = \$ 233,000 PARTIAL LINE = \$ 478,000 NATURAL = \$ 794,000	SIMILAR MAINTENANCE CONSIDERATIONS FOR ALL THREE ALTERNATIVES	100% RAINFALL 300 CFS - PRACTICAL ALTERNATIVES ARE STORM SEWER SYSTEMS OR ROADSIDE DITCHES		USE A COMBINATION OF STREETS/TORM SEWER OR STREETS/ROADSIDE DITCH
DES. PT. 6A DES. PT. 8B	NATURAL OR VEGETATED CHANNEL 40' W x 4' D, 2:1 SIDE-SLOPE	CAPACITY AVAILABLE FOR FULL FLOW THROUGH HYDROLOGY VELOCITY= 5 TO 10 FPS	MODERATELY ERODIBLE SOIL BOTTOM AND SIDE-SLOPES	LIKELY SOME JURISDICTIONAL WETLANDS ARE PRESENT DETAILED STUDY REQUIRED AT FINAL DESIGN TO DETERMINE EXTENT OF WETLANDS	MAY BE JURISDICTIONAL WILDLIFE CORRIDORS OR HABITAT PRESENT	NO EXISTING OR PROPOSED MAJOR UTILITY MAINS ANTICIPATED	PAIRS OF OPEN SPACE LAND USES NEXT TO FACILITY	ADJACENT PROPERTY UNDEVELOPED NEXT TO FACILITY	PLANNED OPEN SPACE	FULL LINE = \$ 817,000 PARTIAL LINE = \$ 809,000 NATURAL = \$ 1,250,000	SIMILAR MAINTENANCE CONSIDERATIONS FOR ALL THREE ALTERNATIVES	EXISTING SLOPES > 30% LESS THAN 30% IS ADAPT VELOCITY RANGE IS ACCEPTABLE FOR ALL ALTERNATIVES 100% RAINFALL > 300 CFS		USE ALTERNATIVE B
DES. PT. 8C DES. PT. 8D	NATURAL OR VEGETATED CHANNEL 40' W x 4' D, 2:1 SIDE-SLOPE	CAPACITY AVAILABLE FOR FULL FLOW THROUGH HYDROLOGY VELOCITY= 5 TO 10 FPS	MODERATELY ERODIBLE SOIL BOTTOM AND SIDE-SLOPES	LIKELY SOME JURISDICTIONAL WETLANDS ARE PRESENT DETAILED STUDY REQUIRED AT FINAL DESIGN TO DETERMINE EXTENT OF WETLANDS	MAY BE JURISDICTIONAL WILDLIFE CORRIDORS OR HABITAT PRESENT	NO EXISTING OR PROPOSED MAJOR UTILITY MAINS ANTICIPATED	RESIDENTIAL LAND USES NEXT TO FACILITY	ADJACENT PROPERTY UNDEVELOPED NEXT TO FACILITY		FULL LINE = \$ 816,000 PARTIAL LINE = \$ 778,000 NATURAL = \$ 1,184,000	SIMILAR MAINTENANCE CONSIDERATIONS FOR ALL THREE ALTERNATIVES	100% RAINFALL 300 CFS - PRACTICAL ALTERNATIVES ARE STORM SEWER SYSTEMS OR ROADSIDE DITCHES		USE A COMBINATION OF STREETS/TORM SEWER OR STREETS/ROADSIDE DITCH

NOTE: FINAL RECOMMENDATIONS ARE INCLUDED IN THE DBPS AND REFLECT REVISION CHANGES DUE TO COMMENTS AND/OR MORE DETAILED EVALUATION.

COTTONWOOD CREEK DBPS - TABLE 12
SUBBASIN TIME OF CONCENTRATION DATA
DATE 18-May-92

BASIN	"C"	OVERLAND			STREET			PIPE			CHANNEL			ADDED TIMES	USING OVERALL Tc		ACTUAL Tc PICKED	
		S(%)	L(FT)	t(MIN)	L(FT)	V(FPS)	t(MIN)	L(FT)	V(FPS)	t(MIN)	L(FT)	V(FPS)	t(MIN)	TOTAL T(MIN)	TOTAL L(MI)	TOTAL T(MIN)	USE T(MIN)	LAG (HR)
A1	0.25	5.0	750	25.0	600	3.0	3.3		7.0	0.0	3800	5.0	12.7	41.0	0.98	17.8	41.0	0.41
A2	0.25	5.0	500	22.0	600	3.0	3.3		7.0	0.0	3100	5.0	10.3	35.7	0.80	15.3	35.7	0.36
A3	0.25	5.0	500	22.0	600	3.0	3.3		7.0	0.0	3500	5.0	11.7	37.0	0.87	16.4	37.0	0.37
A4	0.25	8.0	500	18.0	600	3.0	3.3		7.0	0.0	3100	5.0	10.3	31.7	0.80	12.7	31.7	0.32
A5	0.25	6.0	500	20.0	600	3.0	3.3		7.0	0.0	3600	5.0	12.0	35.3	0.89	15.5	35.3	0.35
A6	0.25	7.0	500	19.0	600	3.0	3.3		7.0	0.0	3500	5.0	11.7	34.0	0.87	14.4	34.0	0.34
A7	0.25	5.0	500	22.0	600	3.0	3.3		7.0	0.0	3100	5.0	10.3	35.7	0.80	15.3	35.7	0.36
A8	0.25	4.0	500	24.0	600	3.0	3.3		7.0	0.0	3500	5.0	11.7	39.0	0.87	17.8	39.0	0.39
A9	0.25	7.0	500	19.0	600	3.0	3.3		7.0	0.0	3200	5.0	10.7	33.0	0.81	13.6	33.0	0.33
A10	0.25	6.0	500	20.0	600	3.0	3.3		7.0	0.0	4000	5.0	13.3	36.7	0.97	16.5	36.7	0.37
A11	0.25	8.0	500	18.0	600	3.0	3.3		7.0	0.0	2300	5.0	7.7	29.0	0.64	10.8	29.0	0.29
A12	0.25	8.0	500	18.0	600	3.0	3.3		7.0	0.0	2300	5.0	7.7	29.0	0.64	10.8	29.0	0.29
A13	0.25	4.0	500	24.0	600	3.0	3.3		7.0	0.0	2600	5.0	8.7	36.0	0.70	15.1	36.0	0.36
B1	0.25	8.0	500	18.0	600	3.0	3.3		7.0	0.0	2800	5.0	9.3	30.7	0.74	12.0	30.7	0.31
B2	0.25	8.0	500	18.0	600	3.0	3.3		7.0	0.0	2700	7.5	6.0	27.3	0.72	11.8	27.3	0.27
B3	0.25	5.0	300	16.0	600	3.0	3.3		7.0	0.0	2800	7.5	6.2	25.6	0.70	13.8	25.6	0.26
B4	0.25	5.0	300	16.0	600	3.0	3.3		7.0	0.0	5000	10.0	8.3	27.7	1.12	19.8	27.7	0.28
B5	0.90	5.0	100	10.0	600	3.0	3.3	750	7.0	1.8	2300	10.0	3.8	19.0	0.71	14.0	19.0	0.19
B6	0.55	4.0	100	10.0	600	3.0	3.3	1650	7.0	3.9	2000	10.0	3.3	20.6	0.82	17.1	20.6	0.21
B7	0.55	3.0	100	10.0	600	3.0	3.3	8550	7.0	20.4		10.0	0.0	33.7	1.75	34.1	34.1	0.34
B8	0.55	3.0	100	10.0	600	3.0	3.3	6000	7.0	14.3		10.0	0.0	27.6	1.27	26.6	27.6	0.28
B9	0.60	3.0	100	10.0	600	3.0	3.3	3000	7.0	7.1	7000	10.0	11.7	32.1	2.03	38.2	38.2	0.38
C1	0.25	7.0	500	19.0	600	3.0	3.3		7.0	0.0	3500	10.0	5.8	28.2	0.87	14.4	28.2	0.28
C2	0.25	7.0	500	19.0	600	3.0	3.3		7.0	0.0	2400	10.0	4.0	26.3	0.66	11.6	26.3	0.26
C3	0.25	7.0	500	19.0	600	3.0	3.3		7.0	0.0	4300	10.0	7.2	29.5	1.02	16.3	29.5	0.30
C4	0.25	7.0	500	19.0	600	3.0	3.3		7.0	0.0	5000	10.0	8.3	30.7	1.16	17.9	30.7	0.31
C5	0.25	4.0	500	24.0	600	3.0	3.3	6000	7.0	14.3	700	10.0	1.2	42.8	1.48	26.8	42.8	0.43
C6	0.50	3.0	100	10.0	600	3.0	3.3	3600	7.0	8.6	2000	10.0	3.3	25.2	1.19	25.4	25.4	0.25
C7	0.50	5.0	100	10.0	600	3.0	3.3	4500	7.0	10.7	3000	10.0	5.0	29.0	1.55	25.5	29.0	0.29

 COTTONWOOD CREEK DBPS - TABLE 13
 URS PROJECT NUMBER 49209
 SUMMARY OF ALTERNATIVE CONSTRAINTS

 AREA 5

COTTONWOOD CREEK MAIN CHANNEL
 BLACK FOREST ROAD TO EAST SIDE OF THE BASIN

 100-YEAR FLOW RANGES FROM LOW TO 1,500 CFS

 100-YEAR VELOCITY RANGES FROM 5 TO 8 FPS

 DESCRIPTION

The existing channel in this area transitions from the deeply incised channel characteristic of area 4 to numerous small tributaries in the Black Forest area. The channel varies in width from 20 to 80 feet. The capacity is available to handle the 100-year storm. This area predominantly has herbaceous wetlands where they are present with some shrub wetlands. The potential for wetlands is high with a significant amount of open water but it has been grazed and disturbed. The wildlife habitat has relatively high beta diversity along the channel but is not very significant away from the channel. The land uses planned for this area transition from urban residential densities by Black Forest Road to rural five acre lot densities in the Colorado Black Forest. The soils in this area include some sandstone and claystone outcrops with the majority being glacial deposits. The area in the forest will be difficult to maintain with heavy construction equipment since there is limited access available.

 ALTERNATIVE ADVANTAGES OF ALTERNATIVE

ALTERNATIVE A The right-of-way is available for this type of channel since the planned densities are low
 Limited permitting involved - only for bridges, grade control where needed, isolated bank protection and maintenance considerations
 Limited mitigation required only for any new bridges planned

ALTERNATIVE B Minimal right-of-way requirements beyond the existing channel width
 Use of drop structures could actually enhance the diversity of the wetland types and wildlife habitat
 Able to control erosion problems that are occurring
 May be able to improve aesthetics with this treatment

ALTERNATIVE C/D

This alternative was eliminated due the the difficulties with construction and mitigation

 RECOMMENDATIONS

For this area the recommended solution is a combination of alternatives A and B. Alternative B would be used mostly in the westerly portion of the basin in order to transition from the reach downstream and alternative A would be used for the remainder of the area.

 DISADVANTAGES OF ALTERNATIVE

Downcutting of the streambed and bank erosion may be a problem
 High maintenance costs may be involved due to the erodable nature of the soils and the access difficulties

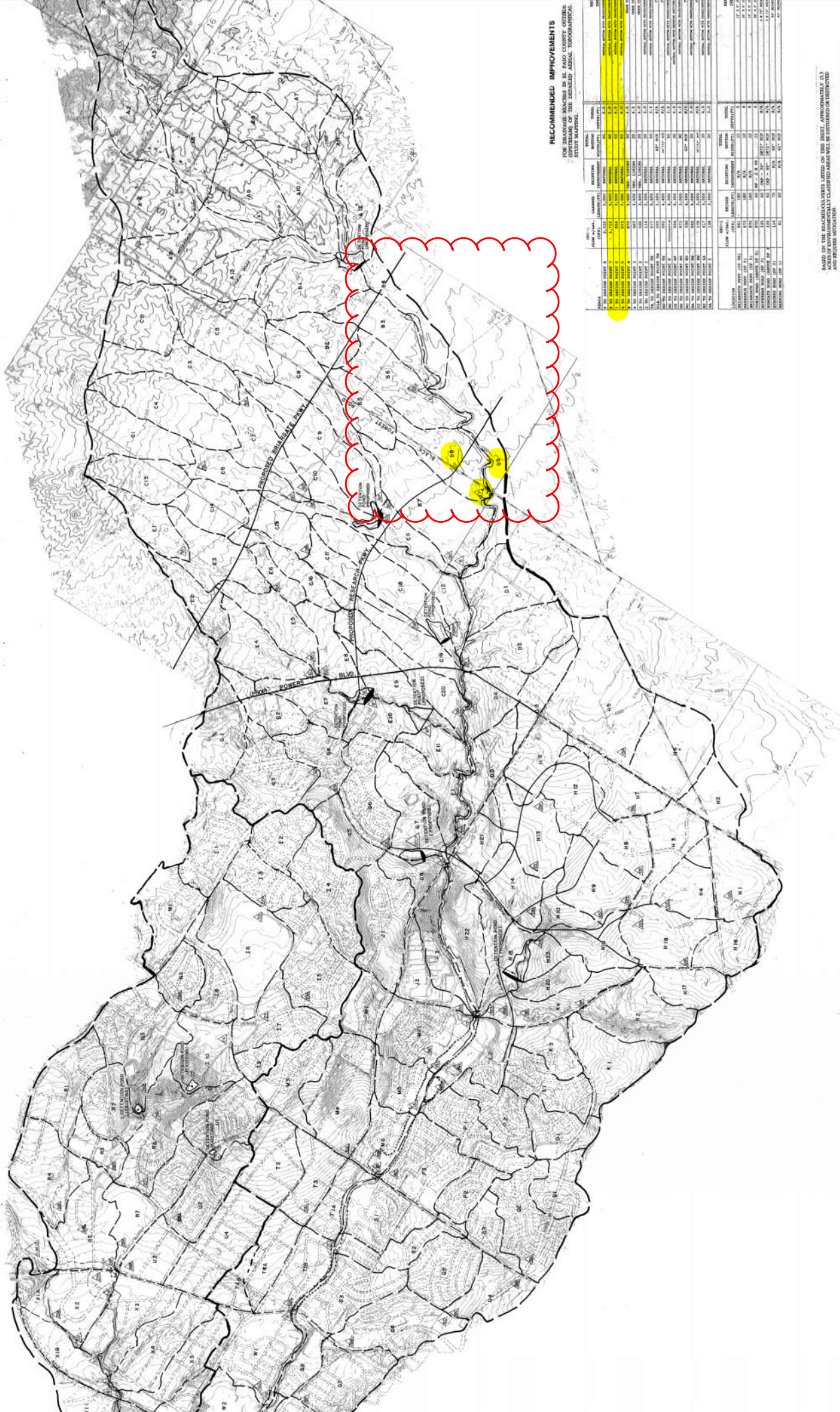
May require some removal and replacement of existing vegetation
 Some onsite mitigation may be required
 Some disturbance of wetlands will occur during construction
 May have some problems with actually constructing this type of facility in the forest area

COTTONWOOD CREEK DBPS - TABLE 16
RATIONAL METHOD - SUBBASIN HYDROLOGIC DATA - PLATTED AREAS
 DATE: 18-May-92

BASIN	HYDROLOGIC SOIL TYPE	AVERAGE LAND USE TYPE AND AREA IN ACRES										OVERALL VALUES		
		COMMER OR BUSIN	INDUST	PARKS	RESID 1/8 AC	RESID 1/6 AC	RESID 1/4 AC	RESID 1/3 AC	RESID 1/2 AC	RESID 1 AC	RESID 5 AC	SCHOOL /CHUR	AREA AC/SM	C
B6	B C D	0.0			0.0	0.0	9.9						9.9 0.015	0.58
B7	B C D				0.0 0.0	0.0 0.0	0.0 0.0			0.0	0.0	0.0	0.0 0.000	N/A
B8	B C D	0.0			0.0								0.0 0.000	N/A
B9	B C D				0.0	0.0	21.6						21.6 0.034	0.65
C1	B C D						0.0			38.1	0		38.1 0.060	0.40
C2	B C D									0.0	0.0		0.0 0.000	N/A
C3	B C D						0.0			0.0	2.0		2.0 0.003	0.20
C4	B C D						0.0			0.0	2.0		2.0 0.003	0.20
C5	B C D						0.0			0.0	37.2		37.2 0.058	0.20

RATIONAL METHOD - SUBBASIN HYDROLOGIC DATA - UNPLATTED AREAS
 DATE: 18-May-92

BASIN	HYDROLOGIC SOIL TYPE	PARKS	AVERAGE LAND USE TYPE AND AREA IN ACRES										OVERALL VALUES			
			COMMER OR BUSIN	INDUST	1/8 AC	1/6 AC	1/4 AC	1/3 AC	1/2 AC	1 AC	5 AC	SCHOOL /CHUR	AREA AC/SM	C		
B6	B C D		11.5	24.5	46.3	25.0									107.3 0.168	0.65
B7	B C D			13.5 5.6	104.3 28.6	21.6 3.7				6.4	6.4				190.1 0.297	0.63
B8	B C D		39.4		62.4										101.8 0.159	0.73
B9	B C D				64.8	21.6									86.4 0.135	0.71
C1	B C D					15.6				33.7	17.9				67.2 0.105	0.39
C2	B C D									12.1	86.2				98.3 0.154	0.22
C3	B C D					27.1				49.0	25.5				101.6 0.159	0.40
C4	B C D					53.2				68.8	13.2	5.9			141.1 0.220	0.46
C5	B C D					54.9				45.7	7.8				108.4 0.169	0.47



RECOMMENDED IMPROVEMENTS
 FOR DRAINAGE BRANCHES IN EL PASO COUNTY, OUTSIDE
 PERIPHERY OF THE METROPOLITAN AREA

BRANCH	NO. OF DESIGN POINTS	NO. OF DESIGN POINTS WITH IMPROVEMENTS	PERCENTAGE OF DESIGN POINTS WITH IMPROVEMENTS
BRANCH 1	1	1	100%
BRANCH 2	1	1	100%
BRANCH 3	1	1	100%
BRANCH 4	1	1	100%
BRANCH 5	1	1	100%
BRANCH 6	1	1	100%
BRANCH 7	1	1	100%
BRANCH 8	1	1	100%
BRANCH 9	1	1	100%
BRANCH 10	1	1	100%
BRANCH 11	1	1	100%
BRANCH 12	1	1	100%
BRANCH 13	1	1	100%
BRANCH 14	1	1	100%
BRANCH 15	1	1	100%
BRANCH 16	1	1	100%
BRANCH 17	1	1	100%
BRANCH 18	1	1	100%
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BRANCH 94	1	1	100%
BRANCH 95	1	1	100%
BRANCH 96	1	1	100%
BRANCH 97	1	1	100%
BRANCH 98	1	1	100%
BRANCH 99	1	1	100%
BRANCH 100	1	1	100%

NOTE: ALL THE DESIGN POINTS LISTED ON THIS SHEET, APPROXIMATELY 133
 POINTS OF ENVIRONMENTALLY CLASSIFIED AREAS WILL BE RESTORED OR IMPROVED
 AND REQUIRE MITIGATION.

NO.	NAME	ADDRESS	CITY	STATE	ZIP	PHONE	FAX	EMAIL
1	URS	10000	EL PASO	TX	79904	972-596-1000	972-596-1001	urs@urscorp.com
2	LANDMARK	10000	EL PASO	TX	79904	972-596-1000	972-596-1001	landmark@landmark.com

LEGEND:

- AI SUB-BASIN DESIGNATION
- △ DESIGN POINT
- MAJOR BASIN BOUNDARY
- SUB-BASIN BOUNDARY

MAPPING: LANDMARK MAPPING!

ENGINEER: URS CONSULTANTS
 MARKING TECHNOLOGY WORK
 COLORADO SPRINGS, CO. 80909
 (719)534-4000

PROJECT: COTTONWOOD CREEK
 OVERALL BASIN MAP
 SCALE: 1" = 1,000'

SHEET INDEX:

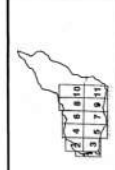


NOT TO SCALE. UNLESS OTHERWISE NOTED, ALL DIMENSIONS ARE AS SHOWN ON THIS PROFILE.

PROJECT:
 COTTONWOOD CREEK
 LAND USE PLAN
 SCALE 1" = 1000'

ENGINEER:
 URS
 CONSULTANTS
 LANDMARK TECHNOLOGY WORK
 CONSULTANTS
 10000 N. 100TH AVENUE, SUITE 200
 DENVER, CO 80231

MAPPING:
 LANDMARK
 MAPPING, INC.
 10000 N. 100TH AVENUE, SUITE 200
 DENVER, CO 80231



SHEET INDEX:

1	2	3	4	5	6	7	8	9	10	11
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LEGEND:

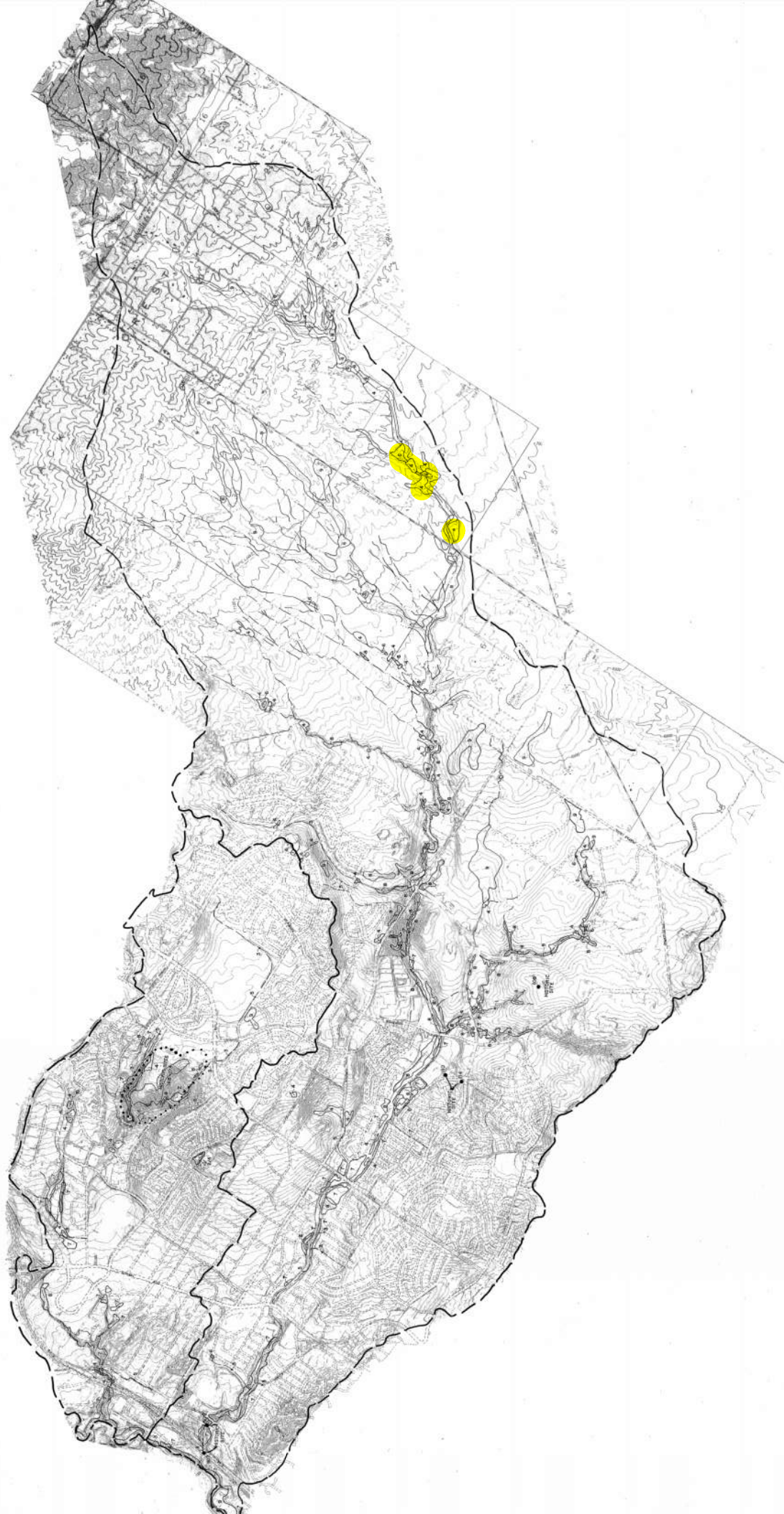
[Symbol]	SCHOOL & CHURCH
[Symbol]	PARK
[Symbol]	AIR FORCE ACADEMY
[Symbol]	PUBLIC OPEN SPACE

LEGEND:

[Symbol]	RESIDENTIAL - 1/8 AC
[Symbol]	RESIDENTIAL - 1/4 AC
[Symbol]	RESIDENTIAL - 1/3 AC
[Symbol]	RESIDENTIAL - 1/2 AC
[Symbol]	RESIDENTIAL - 1 AC
[Symbol]	RESIDENTIAL - 2 1/2 AC
[Symbol]	RESIDENTIAL - 5 AC
[Symbol]	OFFICE, COMMERCIAL
[Symbol]	INDUSTRIAL, GOVERNMENT

LEGEND:

[Symbol]	RESIDENTIAL - 1/8 AC
[Symbol]	RESIDENTIAL - 1/4 AC
[Symbol]	RESIDENTIAL - 1/3 AC
[Symbol]	RESIDENTIAL - 1/2 AC
[Symbol]	RESIDENTIAL - 1 AC
[Symbol]	RESIDENTIAL - 2 1/2 AC
[Symbol]	RESIDENTIAL - 5 AC
[Symbol]	OFFICE, COMMERCIAL
[Symbol]	INDUSTRIAL, GOVERNMENT



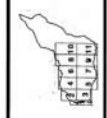
NOTE: UNUSUAL OBSTRUCTIONS AND FEATURES ARE ALSO SHOWN ON THIS FIGURE.

1000 0

PROJECT:
COTTONWOOD CREEK DRAINAGE BASIN PLANNING
ENVIRONMENTAL INVENTORY
SCALE: 1" = 1000'
CONTOUR INTERVAL = 2'
FIGURE 5 SHEET

ENGINEER:
URS
CONSULTANTS
3700 W. 100TH AVENUE, SUITE 200
DENVER, CO 80231
(303) 751-4000

MAPPING:
LANDMARK
MAPPING, INC.
1111 17TH AVENUE, SUITE 100
DENVER, CO 80202
(303) 733-1111



SHEET INDEX:

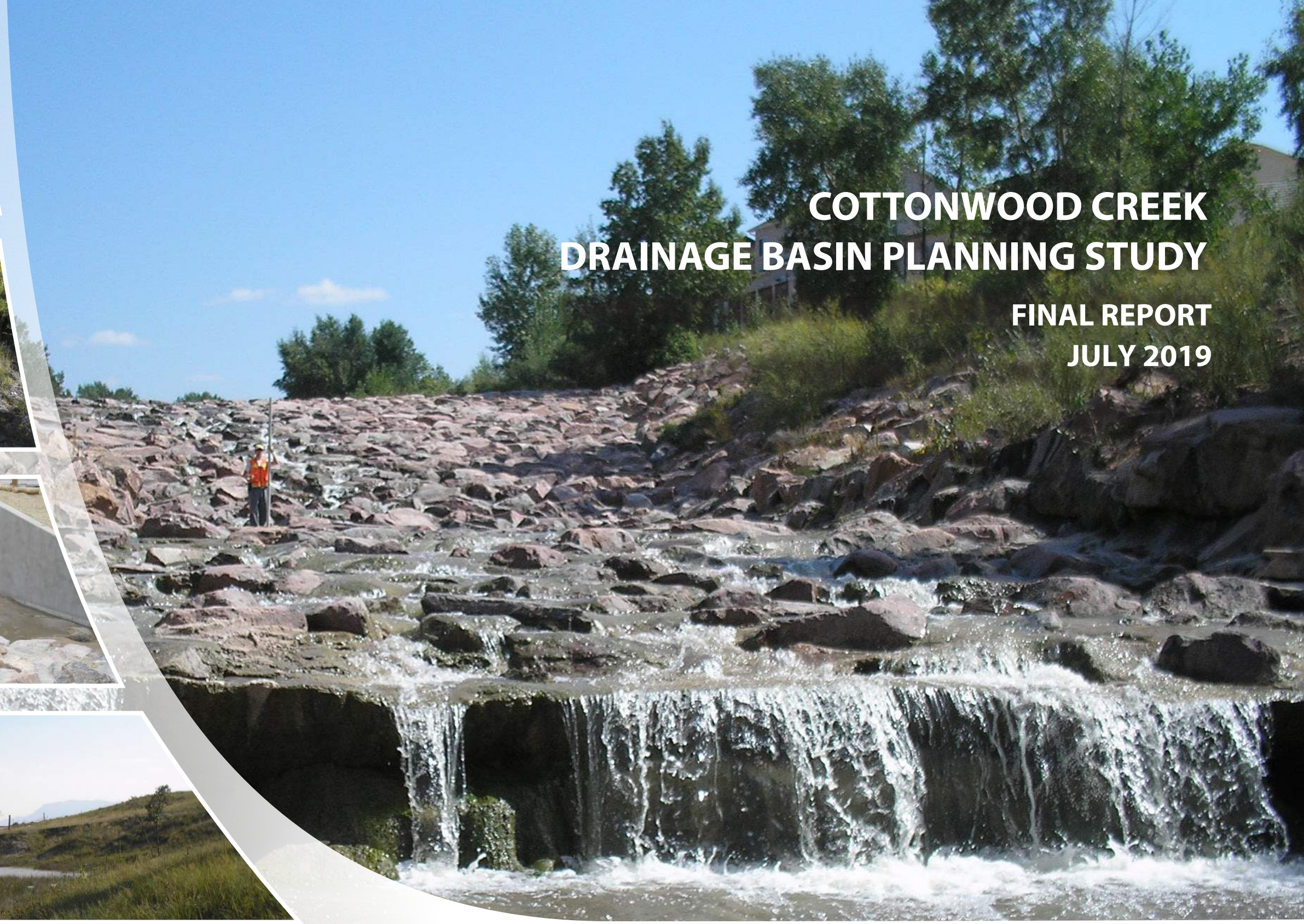
NOTE: DISTURBED AREAS THAT ARE NOT CONSIDERED HAVE BEEN INVESTIGATED BUT WERE NOT CONSIDERED IN THE INVENTORY. EXAMPLES OF THIS ARE: BURNED AREAS, AREAS WITH REMAINING STUMP PILES, AND AREAS WITH REMAINING STUMP PILES.

LEGEND:

- 1 AGRICULTURAL CHANNEL - drainage transecting pastures and fields
- 2 BACKWATER FLOODING - exposed steps or obstructions above obstructions
- 3 HORIZONTAL BARRIERS - mountains, ponds, and proposed passes along channels
- 4 OPEN WATERS - ponds, reservoirs, (includes flowing channels)
- 5 FLOOD PLAINS - areas of low elevation (5 ft. or less elevation)
- 6 SHEEP WATERS - areas of low elevation (5 ft. or less elevation)
- 7 WETLANDS - areas of low elevation (5 ft. or less elevation)
- 8 WETLANDS - areas of low elevation (5 ft. or less elevation)
- 9 WETLANDS - areas of low elevation (5 ft. or less elevation)

COTTONWOOD CREEK DRAINAGE BASIN PLANNING STUDY

FINAL REPORT
JULY 2019



Prepared for:

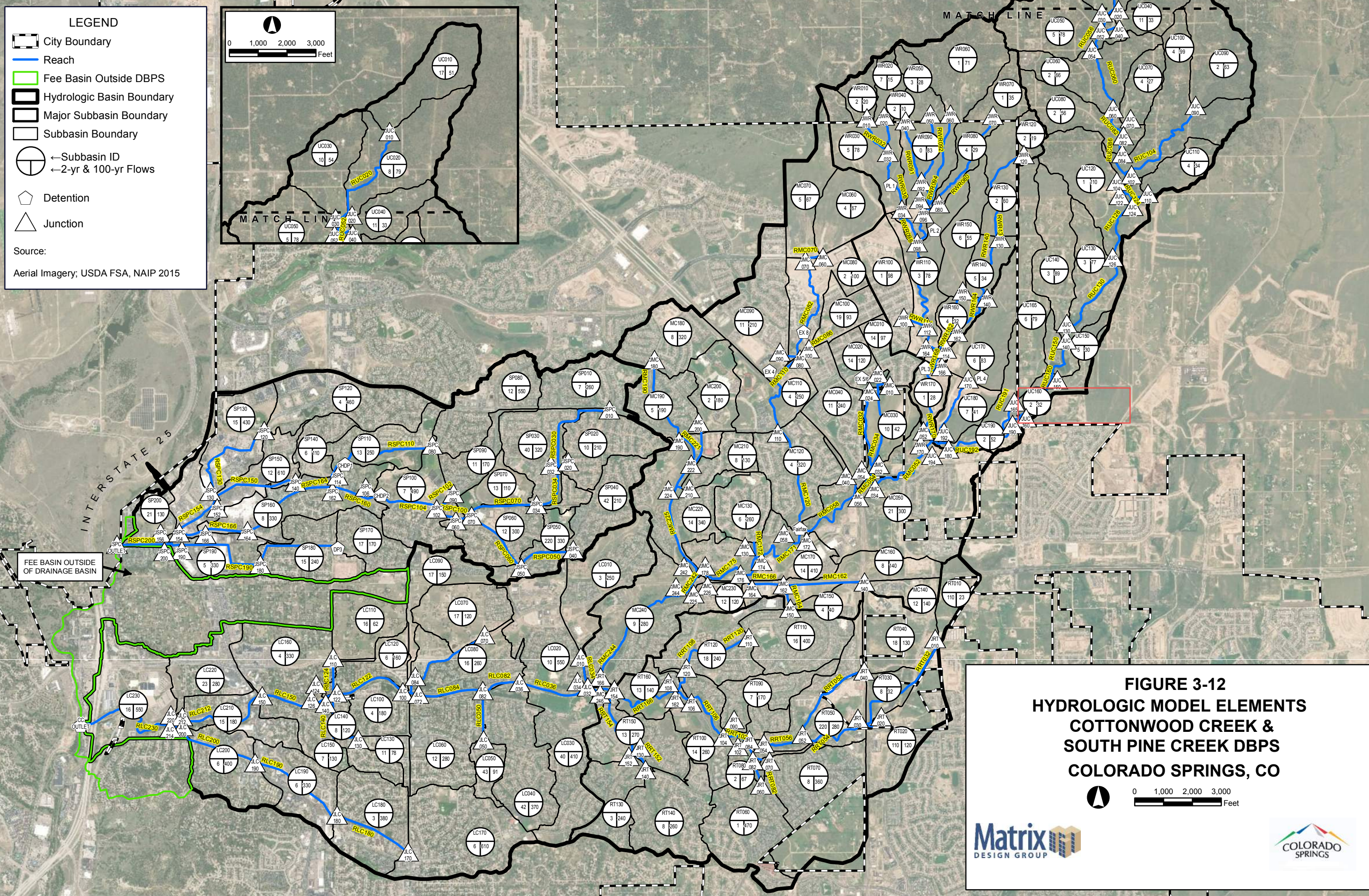


Department of Public Works
Water Resources Engineering

City of Colorado Springs
30 S. Nevada Ave
Colorado Springs, CO 80903

Prepared by:





LEGEND

- City Boundary
- Reach
- Fee Basin Outside DBPS
- Hydrologic Basin Boundary
- Major Subbasin Boundary
- Subbasin Boundary
- ← Subbasin ID
- ← 2-yr & 100-yr Flows
- Detention
- Junction

Source:
Aerial Imagery; USDA FSA, NAIP 2015

FIGURE 3-12
HYDROLOGIC MODEL ELEMENTS
COTTONWOOD CREEK &
SOUTH PINE CREEK DBPs
COLORADO SPRINGS, CO

0 1,000 2,000 3,000
 Feet

FILE: G:\projects\Cottonwood_Creek_DBPs_2017\active\maps\DBPs_Report\Figure_3_12_CottonwoodCreek_Hydrology_Existing_20180226.mxd, 6/29/2018, jmf_sonts



SAND CREEK DRAINAGE BASIN PLANNING STUDY FINAL REPORT JANUARY 2021

Prepared for:

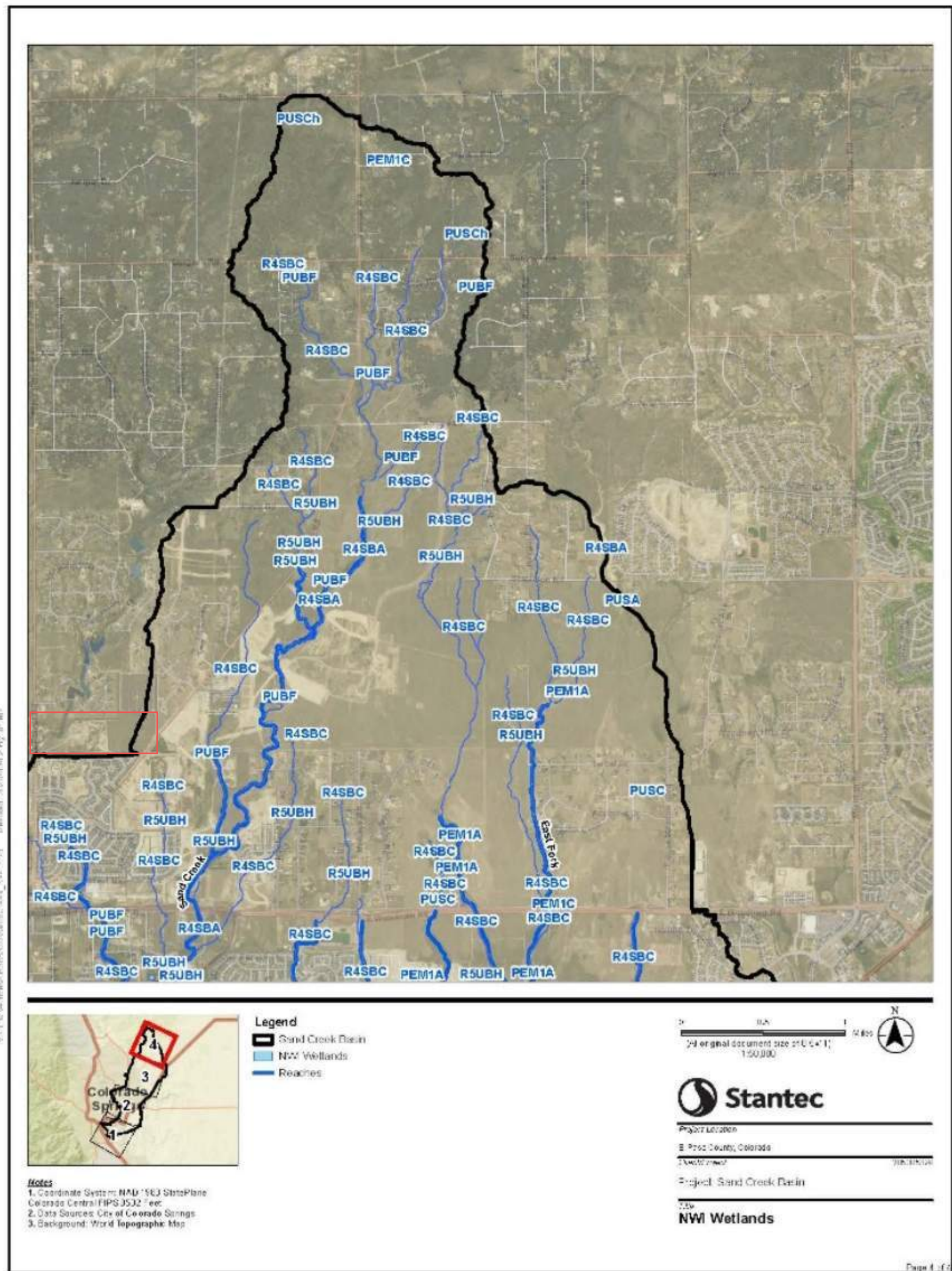


Prepared by:



SAND CREEK – SAND CREEK DRAINAGE BASIN PLANNING STUDY

Basin Characteristics and Environmental Resources



Disclaimer: This document has been prepared based on information provided by others as cited in the Notes section. Stantec has not verified the accuracy and/or completeness of this information and shall not be responsible for any errors or omissions which may be incorporated herein as a result. Stantec assumes no responsibility for data supplied in electronic format, and the recipient accepts full responsibility for verifying the accuracy and completeness of the data.

Figure 2-7: NWI Wetlands Located in Sand Creek Drainage Basin (Page 4)

**MASTER DEVELOPMENT DRAINAGE PLAN
AMENDMENT
FOR
STERLING RANCH**

**Prepared For:
SR Land, LLC
20 Boulder Crescent, 2nd Floor
Colorado Springs, CO 80903
(719) 491-3024**

**March 29th, 2023
Project No. 25188.04**

**Prepared By:
JR Engineering, LLC
5475 Tech Center Drive
Colorado Springs, CO 80919
(303)-267-6240
Contact: Mike Bramlett, PE**

PURPOSE

This document is an amendment to the approved Master Development Drainage Plan (MDDP) for Sterling Ranch. The purpose of this MDDP Amendment report is to:

1. Amend the approved MDDP to account for completed and planned on-site development within Sterling Ranch, including detention from completed filings.
2. Document all differences between the analysis and conclusions reached in the MDDP and this Amendment.
3. Provide analysis and conceptual design information for the on-line Detention Pond at Sterling Ranch Road (PNDW3).
4. This amendment is not intended to address drainage and bridge fees or credits for DBPS improvements. Subsequent submittals will address this.

GENERAL LOCATION AND DESCRIPTION

Location

Sterling Ranch, known as “the site” from herein, is a parcel of land located in Section 27, 28, 33 and 34, Township 12 South, and Section 4, Township 13 South, Range 65 West of the 6th Principal Meridian in El Paso County, Colorado. To the west the site is bound by Vollmer Road. To the north and east, the site is bounded by undeveloped land. To the south, the site is bound by the Pawnee Rancheros and Woodmen Heights developments. A vicinity map is presented in Appendix A.

Description of Property

Sterling Ranch is 1444 acres and is a Planned Unit Development to be built in multiple phases. The site is currently in various stages of development, with portions already in construction, with others unoccupied and undeveloped. The existing ground cover is sparse vegetation and open space, typical of a Colorado rolling range land condition. In general, the site slopes from north to south and the existing drainageways follow this topography.

Per a NRCS web soil survey of the area, the site is made up of Type A and B soils. Type A soils cover roughly 65% of the site while Type B soils cover the remaining 35% of the site. Group A soils have a high infiltration rate when thoroughly wet. Type B soils have a moderate infiltration when thoroughly wet. Type D soils have a very slow infiltration rate when thoroughly wet and have a high shrink-swell potential. A NRCS soil survey map has been presented in Appendix A.

Floodplain Statement

Based on the FEMA FIRM Map numbers 08041C0533G and 08041C0535G, dated December 7, 2018, the site lies within Zone AE and Zone X of the Sand Creek floodplain. Zone AE is defined as area subject to inundation by the 1-percent-annual-chance flood event. Zone X is defined as area outside the Special Flood Hazard Area (SFHA) and higher than the elevation of the 0.2-percent-annual-chance (or 500-year) flood. All proposed development within the site occurs in Zone X. The current FIRM Map has been presented in Appendix A.

DRAINAGE BASINS AND SUBBASINS

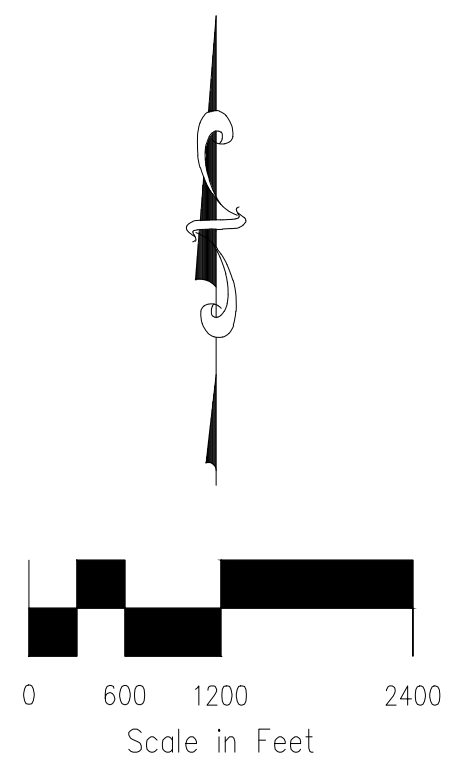
Major Basin Descriptions

The site lies within two major drainage basins: the Sand Creek Drainage Basin and the East Fork of Sand Creek Drainage Basin. Both Basins have been previously studied firstly in the 1996 Drainage Basin Planning Study (DBPS) and again in the 2018 Sterling Ranch MDDP by M&S, and finally in the 2021 DBPS by Stantec which has not been adopted by the El Paso County.

The Sand Creek Drainage Basin covers approximately 22 square miles and begins approximately five miles northeast of the Town of Falcon and travels approximately 15 miles to the southeast. The majority of the area within the basin is undeveloped and is characterized as rolling range land typically associated with Colorado's semi-arid climates. Anticipated land use for the basin includes residential, industrial, agricultural and commercial development. Residential developments will range from 0.125 – 5 acre lots with a mix of low, medium and high density developments.

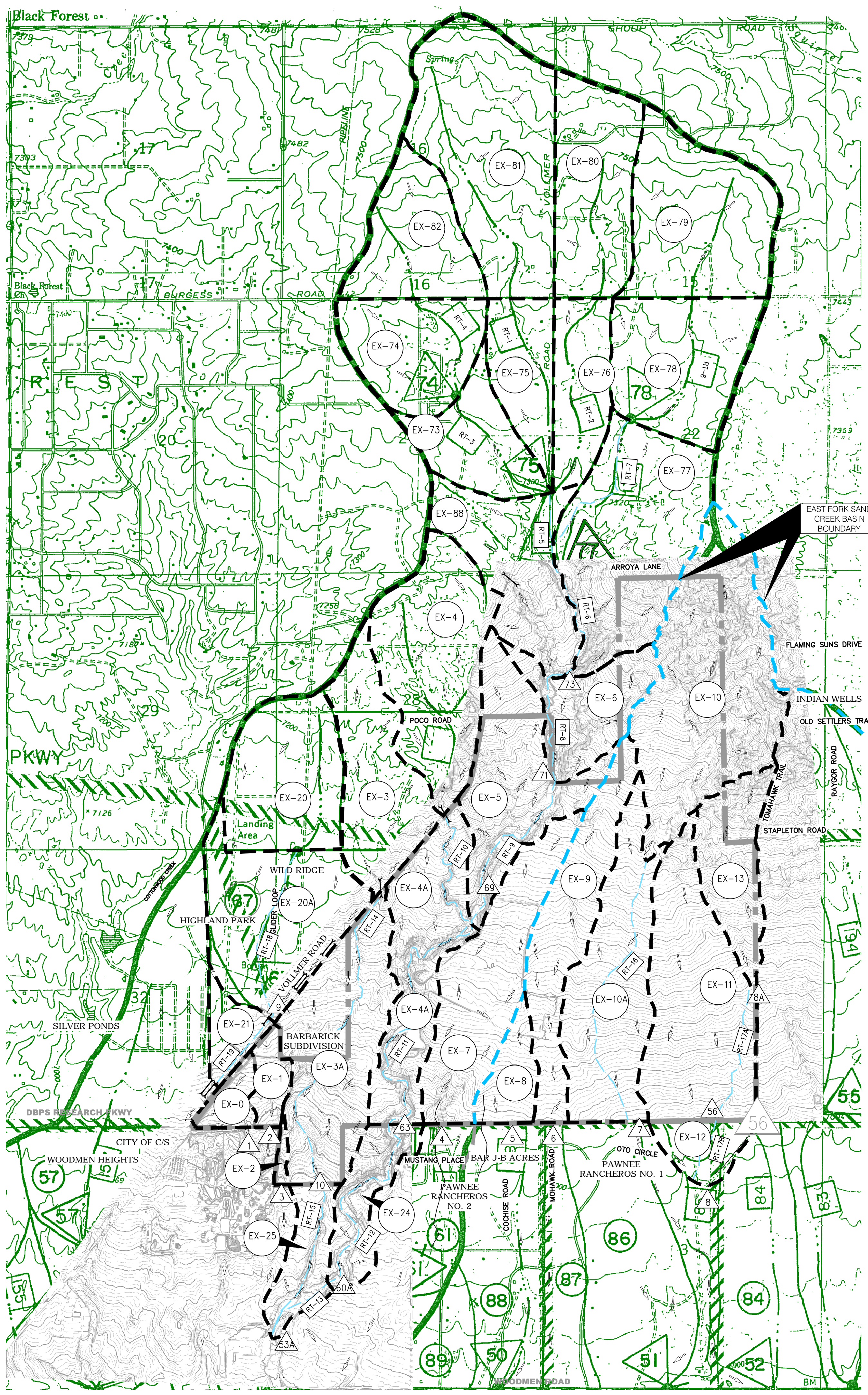
As part of its drainage research, JR Engineering reviewed the following drainage studies and reports:

- Sand Creek Drainage Basin Study prepared by Kiowa in 1996
- Upper Sand Creek Basin Drainage Study prepared by Wilson in 2011
- Sand Creek Drainage Basin Study prepared by Stantec in 2021
- Sterling Ranch Master Development Drainage Plan prepared by M&S in 2018
- Sterling Ranch Filing 1 Final Drainage report prepared by M&S in 2016
- Upper Sand Creek Basin Detention Evaluation Report by Wilson in 2009
- Branding Iron at Sterling Ranch Filing 1 Drainage Report prepared by M&S in 2018
- Branding Iron at Sterling Ranch Filing 2 Drainage Report prepared by M&S in 2020
- Sterling Ranch East Preliminary Drainage Report prepared by Classic Consultants in 2022



LEGEND

- BASIN ID - SC3-77
- DESIGN POINT - 87
- REACH IDENTIFIER - RT-17A
- BASIN BOUNDARY - - - - -
- EAST FORK SAND CREEK - - - - -
- BASIN BOUNDARY - - - - -
- FLOW DIRECTION - >>>



BASIN SUMMARY									
BASIN	CN	AREA (ACRES)	AREA (SQ MI)	Q ₂ (CFS)	Q ₅ (CFS)	Q ₁₀ (CFS)	Q ₂₅ (CFS)	Q ₅₀ (CFS)	Q ₁₀₀ (CFS)
EX-0	62	23.8	0.037	5.0	8.2	13.0	19.6	25.7	32.2
EX-1	62	25.7	0.040	4.8	7.9	12.4	18.7	24.5	30.9
EX-2	62	5.5	0.009	1.1	1.8	2.8	4.3	5.6	7.1
EX-3	62	136.8	0.214	22.0	36.4	57.6	86.9	114.0	143.1
EX-3A	61	188.1	0.294	28.3	47.4	75.7	115.1	152.2	192.6
EX-4	62	192.0	0.300	30.1	49.9	79.1	119.5	157.0	197.3
EX-4A	62	151.5	0.237	24.7	40.8	64.4	97.0	127.2	160.1
EX-5	62	153.9	0.240	24.2	40.0	63.4	95.9	125.9	158.2
EX-6	62	90.2	0.141	15.3	25.5	40.1	60.7	79.9	100.5
EX-7	56	165.0	0.258	11.6	21.5	37.5	60.9	83.1	107.4
EX-8	45	42.0	0.066	0.5	1.7	4.5	9.4	14.5	20.5
EX-9	54	131.9	0.206	12.2	23.9	43.1	70.9	97.0	125.2
EX-10	60	270.7	0.423	32.7	56.0	91.1	140.1	185.9	236.1
EX-10A	41	179.3	0.280	0.6	2.2	7.3	17.4	29.1	43.1
EX-11	43	209.3	0.327	18.0	29.8	47.7	73.4	98.3	126.1
EX-12	51	39.5	0.062	2.2	5.1	10.1	17.7	25.1	33.3
EX-13	55	89.3	0.139	7.7	15.2	27.1	44.2	60.5	78.4
EX-20	62	143.4	0.224	25.4	42.1	66.7	100.7	132.3	166.2
EX-20A	64	179.7	0.281	32.2	51.9	80.5	119.8	155.9	194.6
EX-21	65	33.3	0.052	8.6	13.5	20.7	30.5	39.4	49.0
EX-24	59	63.1	0.099	9.5	16.6	27.5	42.9	57.4	73.0
EX-25	43	54.4	0.085	0.3	1.5	4.8	10.7	17.2	25.1
EX-73	63	90.0	0.141	16.4	26.4	41.3	62.1	81.3	102.0
EX-74	63	119.7	0.187	22.3	36.5	57.3	85.9	112.3	140.7
EX-75	63	79.3	0.124	13.1	21.5	33.7	50.5	66.1	82.8
EX-76	63	86.4	0.135	14.2	23.1	36.4	54.6	71.4	89.6
EX-77	62	230.6	0.360	34.7	56.9	90.6	137.5	180.9	227.7
EX-78	63	155.6	0.243	28.1	45.3	70.6	106.2	139.1	174.5
EX-79	63	189.0	0.295	34.9	57.0	89.5	134.3	175.6	220.1
EX-80	63	147.7	0.231	27.3	44.3	69.6	104.5	136.8	171.4
EX-81	62	262.9	0.411	42.6	70.2	111.0	167.4	219.6	275.7
EX-82	62	117.8	0.184	20.0	33.2	52.8	80.0	105.1	132.3
EX-88	62	139.2	0.217	22.2	36.7	58.0	87.6	115.0	144.4

DESIGN POINT SUMMARY (PEAK FLOW)							
DESIGN POINT	AREA (SQ MI)	Q ₂ (CFS)	Q ₅ (CFS)	Q ₁₀ (CFS)	Q ₂₅ (CFS)	Q ₅₀ (CFS)	Q ₁₀₀ (CFS)
DP-74	0.371	39.3	65.3	104.8	158.9	209.1	262.8
DP-75	1.413	141.2	235.1	376.6	566.6	750.9	950.5
DP-78	0.538	59.7	98.4	154.0	232.6	306.2	385.3
DP-73	2.528	225.9	380.7	618.0	957.0	1260.4	1582.3
DP-71	2.669	229.3	388.9	629.7	978.8	1277.3	1637.9
DP-69	3.209	253.0	434.8	707.7	1100.0	1453.3	1870.4
DP-63	3.446	251.4	430.7	713.1	1113.2	1496.2	1911.5
DP-10	0.508	36.5	56.0	106.4	162.9	220.6	287.2
DP-9A	0.557	55.3	94.3	150.3	227.7	299.5	380.5
DP-9	0.505	52.8	88.8	142.1	214.2	281.0	351.4
DP-8A	0.139	7.7	15.2	27.1	44.2	60.5	78.4
DP-8	0.528	24.2	45.1	77.8	124.4	169.5	220.9
DP-7	0.703	32.4	57.1	97.3	156.1	213.8	277.9
DP-6	0.206	12.2	23.9	43.1	70.9	97.0	125.2
DP-5	0.066	0.5	1.7	4.5	9.4	14.5	20.5
DP-4	0.258	11.6	21.5	37.5	60.9	83.1	107.4
DP-3	0.009	1.1	1.8	2.8	4.3	5.6	7.1
DP-2	0.040	4.8	7.9	12.4	18.7	24.5	30.9
DP-1	0.037	5.0	8.2	13.0	19.6	25.7	32.2
DP-60A	3.545	247.7	430.2	707.1	1113.0	1496.6	1913.5
DP-56	0.466	23.2	42.5	71.9	115.6	157.4	202.9
DP-53A	4.138	262.1	454.0	763.2	1196.5	1609.8	2061.5

DESIGN POINT SUMMARY (VOLUME)							
DESIGN POINT	AREA (SQ MI)	V ₂ (AC-FT)	V ₅ (AC-FT)	V ₁₀ (AC-FT)	V ₂₅ (AC-FT)	V ₅₀ (AC-FT)	V ₁₀₀ (AC-FT)
DP-74	0.371	5.9	9.0	13.6	19.8	25.5	31.6
DP-75	1.413	22.7	34.5	51.7	75.4	97.1	120.5
DP-78	0.538	8.9	13.5	20.1	29.3	37.7	46.7
DP-73	2.528	40.4	61.5	92.1	134.3	173.1	214.9
DP-71	2.669	42.5	64.9	97.1	141.6	182.5	226.6
DP-69	3.209	50.7	77.4	116.1	169.4	216.6	271.4
DP-63	3.446	54.1	82.5	123.8	180.8	233.3	289.9
DP-10	0.508	7.6	11.7	17.6	25.8	33.4	41.6
DP-9A	0.557	9.3	14.1	21.1	30.7	39.4	48.8
DP-9	0.505	8.4	12.7	19.0	27.6	35.5	44.0
DP-8A	0.139	1.3	2.1	3.4	5.2	7.0	8.9
DP-8	0.528	4.4	7.0	11.1	16.8	22.3	28.4
DP-7	0.703	6.1	10.0	15.9	24.3	32.4	41.3
DP-6	0.206	2.4	4.0	6.3	9.6	12.7	16.0
DP-5	0.066	0.2	0.4	0.8	1.4	1.9	2.6
DP-4	0.258	2.6	4.2	6.7	10.2	13.5	17.2
DP-3	0.009	0.1	0.2	0.3	0.5	0.6	0.8
DP-2	0.040	0.6	0.9	1.4	2.1	2.7	3.4
DP-1	0.037	0.6	0.9	1.3	1.9	2.5	3.1
DP-60A	3.545	55.3	84.4	126.4	184.8	238.5	296.6
DP-56	0.466	4.0	6.3	9.9	14.9	19.8	25.1
DP-53A	4.138	63.0	96.4	144.7	211.8	273.9	340.9

EFCS DBPS DESIGN POINT SUMMARY (PEAK FLOW)			
DBPS DESIGN POINT	AREA (SQ MI)	Q ₂ (CFS)	Q ₁₀₀ (CFS)
DP-50	0.32	47.0	195.7
DP-51 (BASIN 86)	0.33	17.7	74.1
DP-52	1.67	80.5	456.5
DP-56	0.79	63.6	265.0

Values reported from SCDBPS
 (DP 50, 51, 52 Not analyzed as a part of this study)
 DBPS Reach 85(Basin#1)=Q10=28.8cfs Q100=115.2cfs

M&S CIVIL CONSULTANTS, INC.
 20 BOULDER CRESCENT, SUITE 110
 COLORADO SPRINGS, CO 80903
 PHONE: 719.955.5485

2018 STERLING RANCH MDDP EXISTING HYDROLOGIC CONDITIONS MAP

PROJECT NO. 09-002 FILE: \\dvg\Eng Exhibits\2018-MDDP-ExistCondWS\Map.dwg

DESIGNED BY: DLM SCALE: DATE: 08-22-18
 DRAWN BY: DLM HORIZ: NTS
 CHECKED BY: VAS VERT: NTS

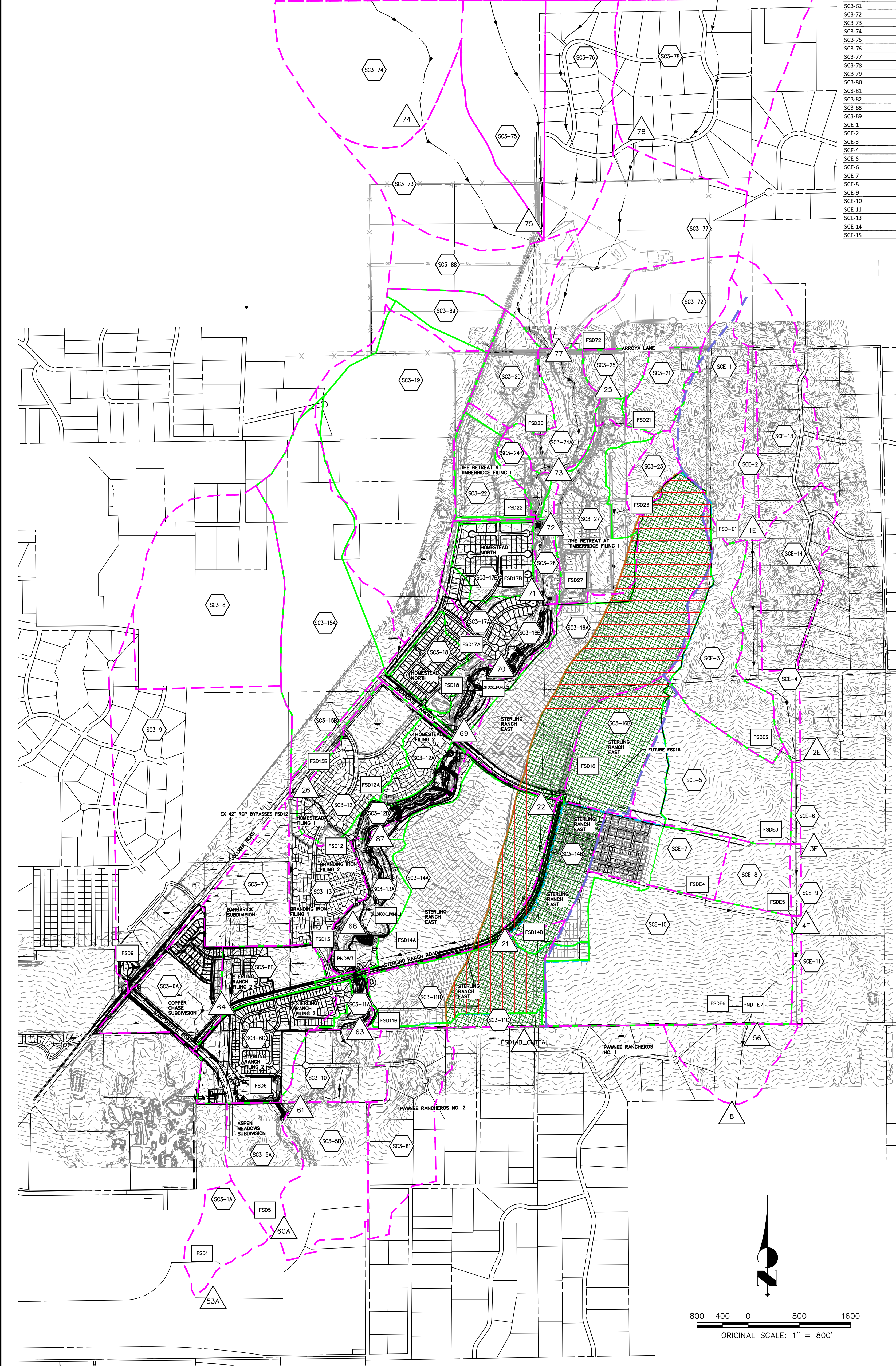
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File: C:\09002A\Sterling Ranch - District\Eng Exhibits\2018-MDDP-ExistCondWS\Map.dwg Plotstamp: 11/13/2018 1:52 PM

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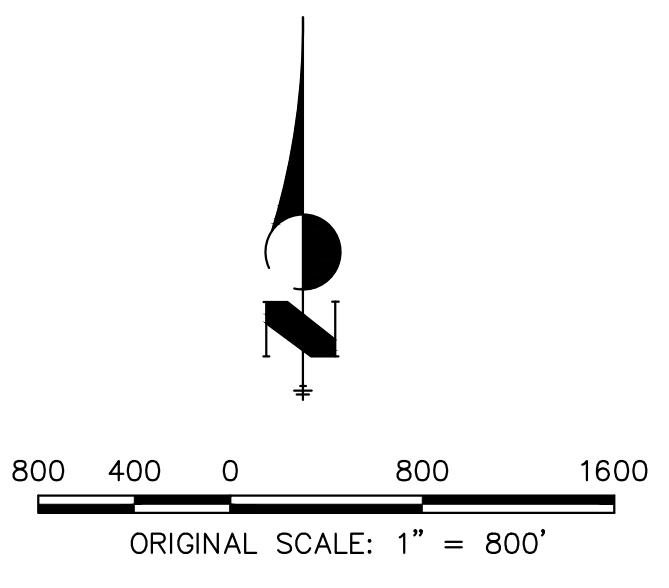
Proposed Conditions Design Point Summary						
Design Point	Q ₂ (cfs)	Q ₅ (cfs)	Q ₁₀ (cfs)	Q ₂₅ (cfs)	Q ₅₀ (cfs)	Q ₁₀₀ (cfs)
DP-74	33.68	94.55	145.74	187.2	251.03	293.76
DP-75	95.13	274.57	427.98	555.2	754.29	887.87
DP-77	144.08	426.57	672.84	877.81	1201.19	1423.89
DP-78	52.82	138.33	210.37	269.64	360.98	422.09
DP-73	147.28	442.59	703.56	919.81	1257.44	1497.12
DP-72	148.02	450.59	718.2	939.53	1285.42	1527.18
DP-71	149.28	472.6	771.35	1012.75	1386.32	1644.05
DP-70	149.57	477.23	780.47	1025.79	1405.32	1666.98
DP-69	146.52	512.38	847.55	1108.89	1497.55	1763.93
DP-87	143.88	533.15	890.76	1170.95	1589.82	1880.33
DP-68	126.27	579.69	994.15	1327.63	1837.13	2160.43
DP-64	89.76	133.15	167.21	194.25	233.42	259.48
DP-63	128.57	480.38	763.81	1005.42	1368.28	1585.19
DP-61	132.9	535.22	851.44	1123.05	1549.17	1859.67
DP-60A	135.75	544.14	863.88	1138.24	1569.79	1882.17
DP-53A	135.8	545.87	866.46	1141.24	1573.95	1887.54
DP-1E	12.41	29.33	43.32	54.71	72.19	83.84
DP-2E	24.93	56.12	81.89	103.16	135.52	157.2
DP-3E	26.73	59.28	86.63	109.01	143.9	176.03
DP-4E	28.34	61.94	91.01	114.79	152.57	184.7
DP-56	24.04	43.91	62.31	79.42	106.6	136.21
DP-8	26.31	47.57	67.39	84.03	107.24	137.04
DP-21	8.07	45.76	92.48	128.9	153.87	200.93
DP-22	8.07	45.78	92.52	128.94	153.88	191.38
DP-25	5.58	12.02	17.2	21.1	26.97	30.8
DP-26	13.62	38.67	59.76	76.94	102.99	120.45
EX STOCK POND 1	133.68	512.29	863.82	1143.6	1561.29	1848.83
EX STOCK POND 2	149.57	477.23	780.47	1025.79	1405.32	1666.98
FSD14B Outfall	2.57	20.53	44.05	64.95	98.12	116.66
PND-E7	31.92	68.33	100.59	126.9	176	222.77
PNDW3	126.27	579.69	994.15	1327.63	1837.12	2160.43

Proposed Conditions Basin Summary						
Basin	Q ₂ (cfs)	Q ₅ (cfs)	Q ₁₀ (cfs)	Q ₂₅ (cfs)	Q ₅₀ (cfs)	Q ₁₀₀ (cfs)
SC3-1A	15.4	32.05	44.63	54.22	68.02	77.21
SC3-5A	48.38	75.2	95.88	112.35	135.5	150.82
SC3-5B	60.26	97.13	126.36	149	181.48	203.13
SC3-6A	59.98	84.21	106.32	123.77	149.06	165.69
SC3-6B	30	47.16	60.52	70.92	85.96	95.97
SC3-6C	52.26	84.02	115.61	140.03	174.32	196.64
SC3-7	60.94	87.91	109.28	126.05	150.45	166.71
SC3-8	56.41	93.96	122.75	146.13	185.44	215.44
SC3-9	24.66	73.44	114.01	146.06	193.77	225.81
SC3-10	2.94	14.36	23.62	30.77	41.33	48.66
SC3-11A	1.99	5.36	8.05	10.06	13.08	15.09
SC3-11B	68	99.65	126.13	146.85	176.93	196.96
SC3-11C	1.37	5.83	9.3	11.93	15.66	18.16
SC3-12	47.61	71.53	91.34	106.54	129.44	144.67
SC3-12A	15.01	24.03	31.22	36.66	44.86	50.9
SC3-12B	2.17	6.35	9.82	12.6	16.83	19.66
SC3-13	56.24	80.96	100.72	115.86	138.53	153.6
SC3-13A	2.61	7.62	11.81	15.18	20.28	23.7
SC3-14A	110.65	160.22	203.13	237.5	287.18	320.18
SC3-14B	63.13	90	115.58	136.1	165.72	185.1
SC3-15A	13.21	38.41	59.28	76.32	102.43	119.86
SC3-15B	8.38	12.29	15.45	17.9	21.56	24
SC3-16	180.7	266.34	343.24	404.73	493.4	552.27
SC3-17A	25.63	39.59	50.91	59.5	72.46	81.07
SC3-17B	20.59	32.3	41.97	49.43	60.7	68.19
SC3-18	22.75	32.96	41.34	47.83	57.56	64.05
SC3-18B	1.53	4.45	6.89	8.86	11.91	13.95
SC3-19	28	78.96	120.84	154.22	205.45	239.67
SC3-20	9.29	21.02	30.73	38.5	50.17	57.99
SC3-21	9.77	20.68	29.45	36.03	45.92	52.53
SC3-22	7.15	16.35	24.05	30.08	39.14	45.22
SC3-23	10.92	22.1	31.23	38.2	48.72	55.73
SC3-24A	6.43	15.26	22.51	28.3	37.09	42.98
SC3-24B	1.96	4.78	7.12	8.98	11.76	13.62
SC3-25	5.58	12.02	17.2	21.1	26.97	30.9
SC3-26	1.66	4.37	6.61	8.4	11.13	12.95
SC3-27	14.49	27.87	39.1	48.09	61.8	70.95
SC3-61	5.61	22.4	36.4	47.4	63.67	74.61
SC3-72	9.55	23.84	35.61	44.98	59.19	68.7
SC3-73	12.16	33.03	50.14	63.89	84.94	99.04
SC3-74	22.51	53.27	79.1	99.77	131.03	151.94
SC3-75	11.12	26.37	38.98	49.21	64.91	75.41
SC3-76	10.85	27.09	40.54	51.45	68.18	79.38
SC3-77	8.93	27.11	42.16	54.46	73.59	86.36
SC3-78	32.29	77.46	114.83	144.42	189.21	219.17
SC3-79	32.26	82.54	123.52	156.01	205.95	239.34
SC3-80	22.36	57.34	86.09	109.14	144.5	168.15
SC3-81	26.67	81	125.85	162.22	218.65	256.32
SC3-82	17.01	50.83	79.48	102.02	136.18	158.98
SC3-88	6.28	18.99	29.44	37.84	50.8	59.46
SC3-89	2.86	8.64	13.39	17.14	22.87	26.69
SCE-1	9.82	21.3	30.85	38.58	50.51	58.52
SCE-2	1.42	3.35	4.95	6.27	8.3	9.66
SCE-3	8.5	16.95	25.2	31.78	41.56	48.16
SCE-4	4.18	7.52	10.35	12.67	16.29	18.71
SCE-5	71.79	99.51	125.72	146.92	177.89	198.17
SCE-6	0.18	0.55	1.03	1.42	2	2.39
SCE-7	33.06	46.14	56.71	64.87	77.06	85.19
SCE-8	47.1	61.37	73.41	82.94	97.16	106.61
SCE-9	0.22	0.68	1.27	1.75	2.46	2.94
SCE-10	106.33	165.76	230.7	283.77	358.46	407.13
SCE-11	0.77	2.52	4.75	6.5	8.93	10.51
SC3-13	10.9	25.85	38.21	48.24	63.64	73.94
SC3-14	8	19.04	28.21	35.59	46.77	54.26
SCE-15	13.6	27.2	38.53	47.35	60.67	69.54



- SCE-11 SWMM BASIN
- PND-E7 SWMM DETENTION POND
- 56 SWMM DESIGN POINT
- 2018 EAST FORK BASIN TRANSFER AREA
- 2022 EAST FORK BASIN TRANSFER AREA
- HISTORIC EAST FORK BASIN BOUNDARY
- 2018 MDDP PROPOSED EAST FORK BASIN BOUNDARY
- 2022 EAST FORK BASIN BOUNDARY
- 2018 MDDP DRAINAGE BASIN BOUNDARY
- 2022 MODIFIED DRAINAGE BASIN BOUNDARY

PROPOSED DRAINAGE MAP
 SAND CREEK MDDP AMENDMENT
 JOB NO. 25188.04
 01/17/23
 SHEET 1 OF 1

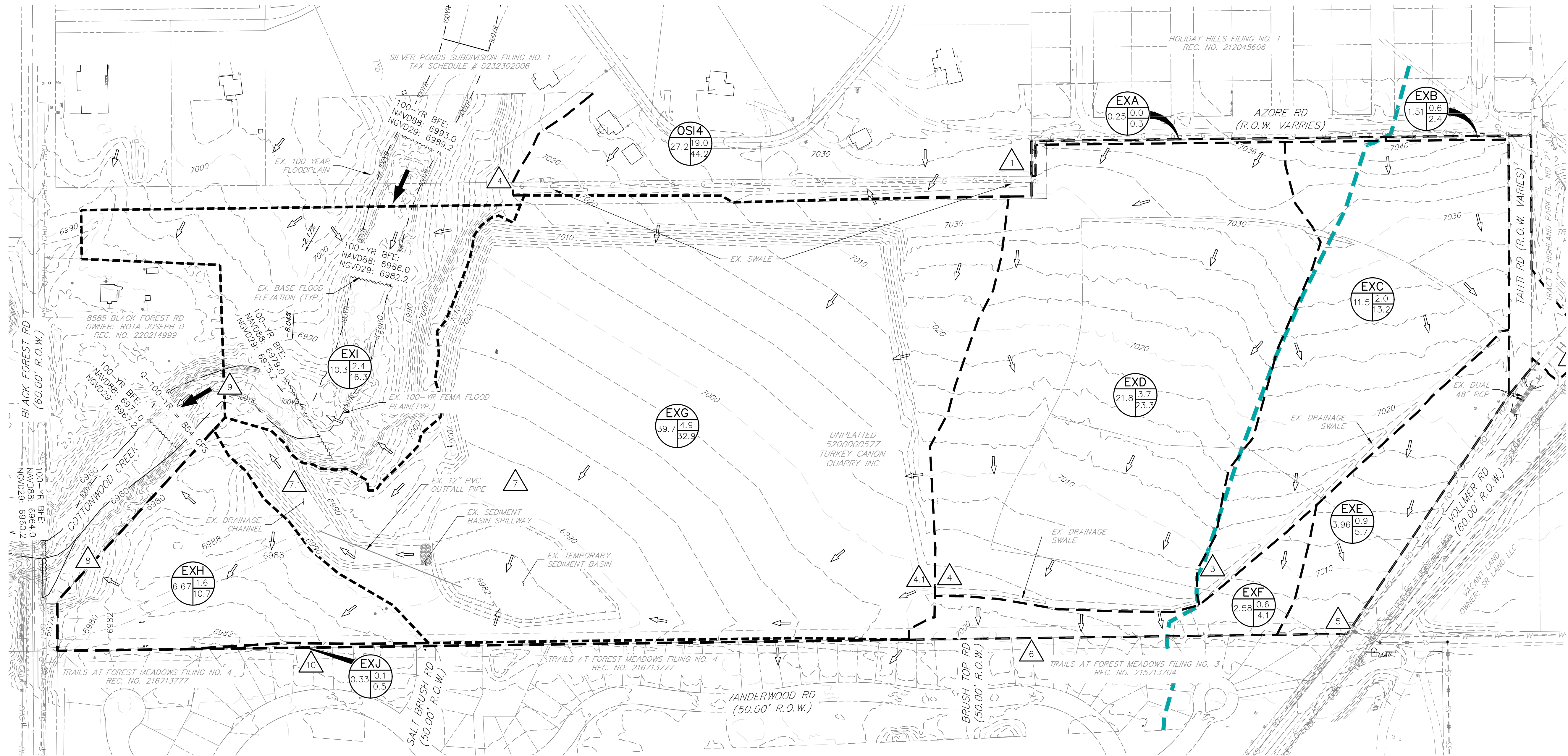




APPENDIX F – DRAINAGE MAPS

SCHMIDT PARCEL

EXISTING CONDITIONS DRAINAGE MAP



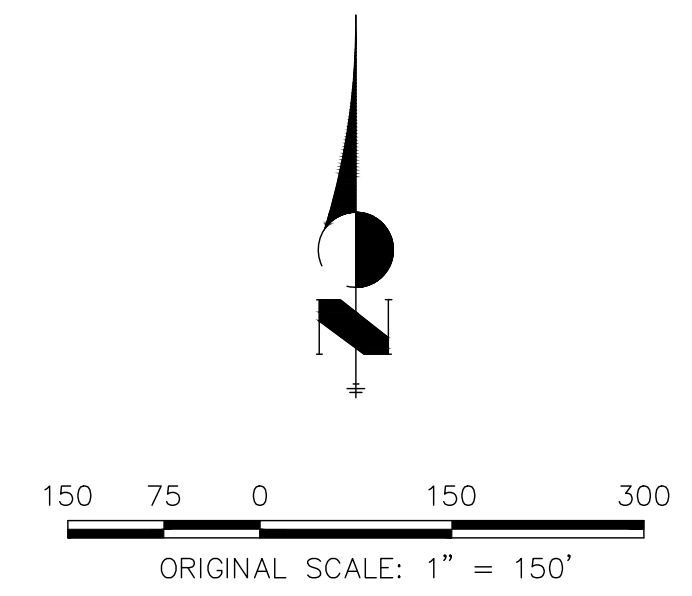
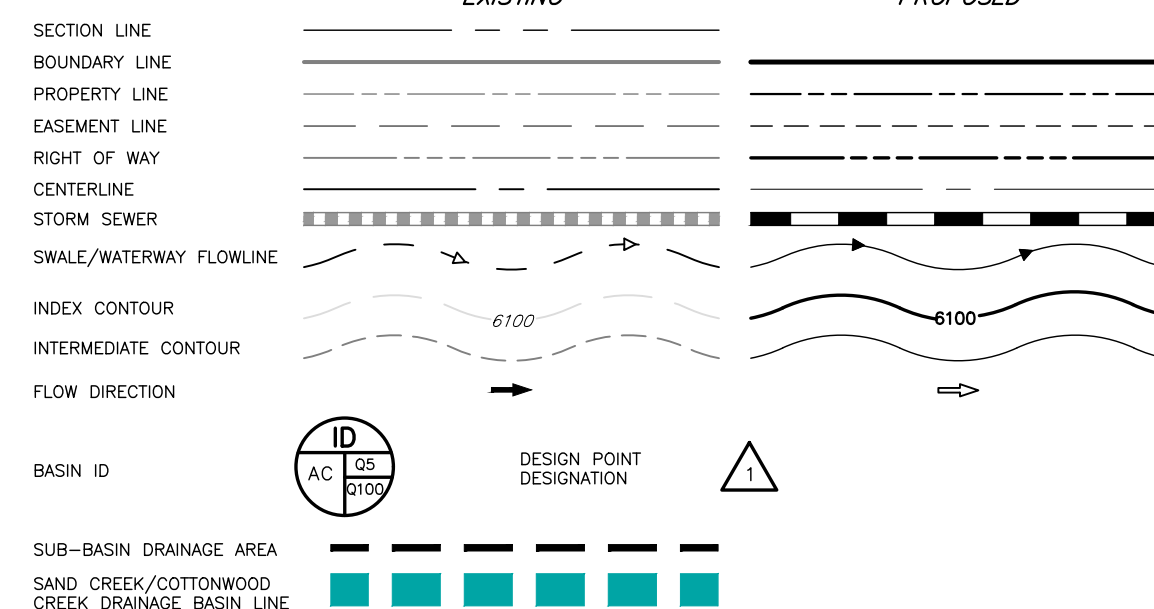
Tributary Sub-basin	Area (acres)	Percent Impervious	C _s	C ₁₀₀	t _c (min)	Q _s (cfs)	Q ₁₀₀ (cfs)
EXA	0.25	2%	0.09	0.36	51.8	0.0	0.3
EXB	1.51	16%	0.18	0.42	34.8	0.6	2.4
EXC	11.55	2%	0.09	0.36	44.5	2.0	13.2
EXD	21.78	3%	0.10	0.36	48.7	3.7	23.3
EXE	3.96	2%	0.09	0.36	31.9	0.9	5.7
EXF	2.58	2%	0.09	0.36	27.1	0.6	4.1
EXG	39.67	2%	0.09	0.36	62.7	4.9	32.9
EXH	6.67	2%	0.09	0.36	26.6	1.6	10.7
EXI	10.29	2%	0.09	0.36	27.3	2.4	16.3
EXJ	0.33	2%	0.09	0.36	25.7	0.1	0.5
OS14	27.16	-	0.30	0.40	29.2	19.0	44.2

Values in BLUE indicate they are from the "Silver Ponds Subdivision Filing No. 1 Final Drainage Report", by M.V.E. Inc. revised May 5th, 1996.

DP#	Q _s -YR	Q ₁₀₀ -YR
1	0.0	0.3
2	0.6	2.4
3	2.0	13.2
4	3.7	23.3
4.1	5.5	35.6
5	0.9	5.7
6	0.6	4.1
7	4.9	32.9
7.1	9.2	60.8
8	1.6	10.7
9	2.4	16.3
10	0.1	0.5
14	19.0	44.2

Values in BLUE indicate they are from the "Silver Ponds Subdivision Filing No. 1 Final Drainage Report", by M.V.E. Inc. revised May 5th, 1996.

LEGEND

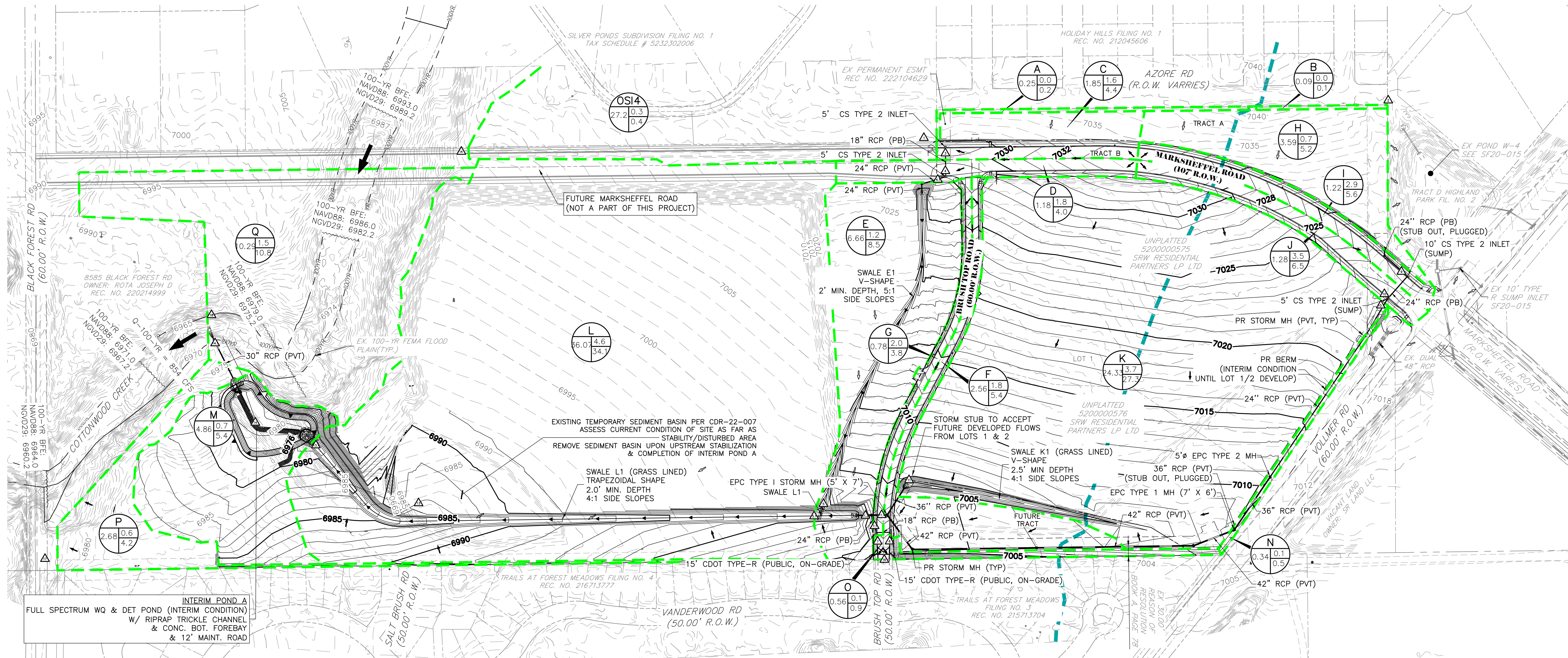


SCHMIDT PARCEL	
EXISTING CONDITIONS DRAINAGE MAP	
JOB NO. 24013	SHEET
LOCATION: EPC	1
2026-04-23	

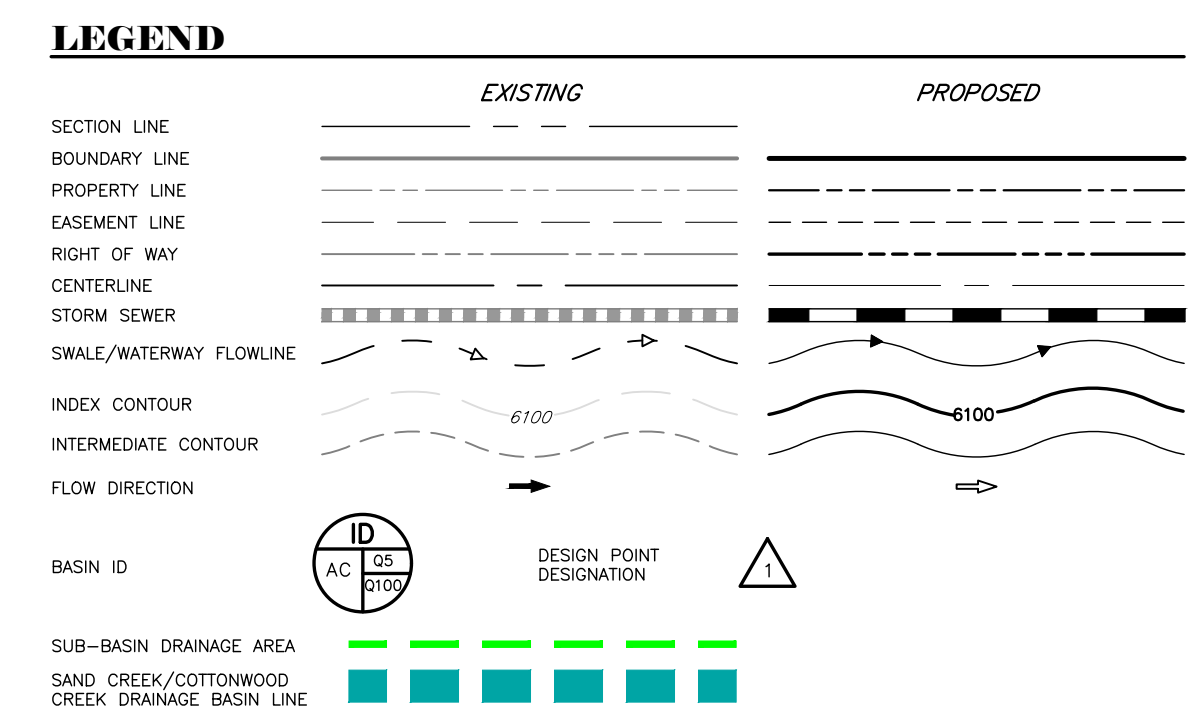


SCHMIDT PARCEL

PROPOSED CONDITIONS DRAINAGE MAP



INTERIM POND A
 FULL SPECTRUM WQ & DET POND (INTERIM CONDITION)
 W/ RIPRAP TRICKLE CHANNEL
 & CONC. BOT. FOREBAY
 & 12' MAINT. ROAD



BASIN SUMMARY TABLE

Tributary Sub-basin	Area (acres)	Percent Impervious	C _s	C ₁₀₀	t _c (min)	Q _s (cfs)	Q ₁₀₀ (cfs)
A	0.25	0%	0.08	0.35	53.0	0.0	0.2
B	0.09	0%	0.08	0.35	36.1	0.0	0.1
C	1.85	31%	0.34	0.54	26.9	1.6	4.4
D	1.18	54%	0.52	0.68	21.5	1.8	4.0
E	6.66	0%	0.08	0.35	36.8	1.2	8.5
F	2.56	25%	0.29	0.50	29.5	1.8	5.4
G	0.78	85%	0.78	0.87	16.9	2.0	3.8
H	3.59	0%	0.08	0.35	30.7	0.7	5.2
I	1.22	80%	0.73	0.84	17.5	2.9	5.6
J	1.28	87%	0.79	0.88	16.0	3.5	6.5
K	24.33	0%	0.08	0.35	43.9	3.7	27.3
L	36.07	0%	0.08	0.35	53.6	4.6	34.1
M	4.86	0%	0.08	0.35	44.3	0.7	5.4
N	0.34	0%	0.08	0.35	26.1	0.1	0.5
O	0.56	0%	0.08	0.35	26.7	0.1	0.9
P	2.68	0%	0.08	0.35	26.1	0.6	4.2
Q	10.29	0%	0.08	0.35	47.7	1.5	10.8
OS14	27.16	-	0.30	0.40	29.2	19.0	44.2

Values in BLUE indicate they are from the "Silver Ponds Subdivision Filing No. 1 Final Drainage Report", by M.V.E. Inc. revised May 5th, 1996.

DESIGN POINT SUMMARY TABLE

DPH	Q _s -yr	Q ₁₀₀ -yr
1	0.0	0.2
2	0.0	0.1
3	1.6	4.4
4	1.8	4.0
4.1	3.2	7.9
5	3.9	15.1
5.1	13.4	55.8
6	1.8	5.4
7	2.0	3.8
7.1	3.4	8.3
9	2.9	9.3
10	3.5	6.5
10.1	5.3	13.9
11	3.7	27.3
11.1	7.9	38.0
11.2	10.4	44.3
13	4.6	34.1
13.1	16.3	82.8
14	17.0	87.4
15	0.1	0.5
16	0.1	0.9
17	0.6	4.2
18	1.5	10.8
14	19.0	44.2

Values in BLUE indicate they are from the "Silver Ponds Subdivision Filing No. 1 Final Drainage Report", by M.V.E. Inc. revised May 5th, 1996.

150 75 0 150 300
 ORIGINAL SCALE: 1" = 150'

SCHMIDT PARCEL	
PROPOSED CONDITIONS DRAINAGE MAP	
JOB NO. 24013	SHEET
LOCATION: EPC	1
2026-04-23	

ALL TERRAIN
ENGINEERING