Final Drainage Report

Renehan Subdivision 5740 Burgess Road, Colorado Springs, CO 80908

Prepared for (Owner):

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Prepared by:

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Project #: 196624000 PCD File No. MS238

Prepared: January 5, 2024





CERTIFICATION

Conditions:

ENGINEERS STATEMENT

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the County for drainage reports and said report is in conformity with the applicable master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors, or omissions on my part in preparing this report.

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| | The Market | | |
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| (| Kevin Kofford, Colorado P.E | . No. 57234 | Date |
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| drainage report and plan | ave read and will comply with | all of the requirer | nents specified in this |
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| Name of Developer | | | |
| Jeff Renehan | Digitally signed by Jeff Renehan Date: 2024.06.11 15:08:46 -06'00' | | |
| Authorized Signature | Date | | |
| Jeffrey N. Renehan | | | |
| Printed Name | | | |
| | | | |
| Title | | | |
| 9548 Stoneglen Dr, Colo | Springs 80920 | | |
| Address: | | | |
| EL PASO COUNTY | | | |
| Filed in accordance with | the requirements of the Drain | aga Critaria Man | ual Valumaa 1 and 2 FL |
| | the requirements of the Drain g Criteria Manual and Land D | | |
| , , | - | 9/11/2024 | |
| Joshua Palmer, P.E. | | Date | |
| County Engineer / ECM | Administrator | | |



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INTRODUCTION

PURPOSE AND SCOPE OF STUDY

The purpose of this Final Drainage Report (FDR) is to provide the hydrologic and hydraulic calculations and to document and finalize the drainage design methodology in support of the proposed Renehan Minor Subdivision ("the Project") located at 5740 Burgess Road ("the Property"). The Project is located within the jurisdictional limits of El Paso County ("the County"). Thus, the guidelines for the hydrologic and hydraulic design components were based on the criteria for El Paso County, described below.

GENERAL PROJECT DESCRIPTION

The Site is located at 5740 Burgess Road and is bounded Burgess Road to the south and privately owned residential properties in each direction. The existing property is vacant.

The Property is to be platted as three individual lots. Lot 1 (southern region of the property) being 8.62 acres, Lot 2 (central/northeast region of the property) being 17.06 acres, and Lot 3 (northwestern region of the property) being 8.69 acres. A proposed wildlife protection zone is located at the Northwestern corner of the property (Proposed Lot 3). A shared private driveway is anticipated. Stormwater will ultimately outfall to Kettle Creek.

The confluence point for Kettle Creek and tributary Burgess Creek exists just to the north of the site

The property is currently owned by Bradley, Sandra, Jeffrey, Julie Renehan. The Survey for the Renehan Subdivision was completed on 01/04/2023 by Land Development Consultants, Inc. This is the basis for design for the drainage map and report.

SITE CHARACTERISTICS

The Project Site is approximately 34.37 acres in size. The Project involves the division of property into three single family lots ranging in size: 8.62 acres, 17.06 acres, and 8.69 acres, respectively. The existing site is vacant and undeveloped land, with an unmaintained driveway/trail providing access from Burgess Road. The Site is heavily wooded with pine trees covering about 80% of the Site.

The existing Project Site generally slopes from east to west & south to north, towards Kettle Creek, which meanders just north of the property. Slopes vary from 2% - 25% in grade, forming numerous on-site and off-site drainage basins facilitating flows towards Kettle Creek. There are no irrigation facilities located within the Site.

DRAINAGE BASIN PLANNING STUDY INFRASTRUCTURE AND ANALYSIS

The Property is located in the Kettle Creek drainage basin and is tributary to Black Squirrel Creek. The Drainage Basin Planning Study for the Kettle Creek drainage basin was prepared May 5th, 2015 by JR Engineering LLC. See Drainage Basin Planning Study in Appendix B



SOILS CONDITIONS

NRCS soil data is available for this Site and it has been noted that onsite soils are USCS Type B. The NRSC Soils map has been provided in Appendix C.

DRAINAGE DESIGN CRITERIA

DEVELOPMENT DESIGN CRITERIA REFERENCE AND CONSTRAINTS

The report is to be in compliance with the El Paso County "Drainage Criteria Manual (DCM)" dated October 2018 ("the MANUAL"), El Paso County "Engineering Criteria Manual" ("the Engineering Manual"), Chapter 6 and Section 3.2.1 of Chapter 13 of the City of Colorado Springs Drainage Criteria Manual dated May 2014 ("the Colorado Springs MANUAL").

HYDROLOGIC CRITERIA

The 5-year and 100-year design storm events were used in determining rainfall and runoff for the proposed drainage scenario per Volume 1 Update-Chapter 6 of the MANUAL. Table 6-2 of the MANUAL is the source for rainfall data for the 5-year and 100-year design storm events. Design runoff was calculated using the Rational Method for developed conditions as established in the MANUAL. Runoff coefficients for the proposed development were determined using Table 6-6 of the MANUAL by calculating weighted impervious values for each specific site sub-basin. A "forest" surface characteristic was used for this project, given the entirety of the Site is within a densely wooded forest.

HYDRAULIC CRITERIA

Applicable design methods were utilized to determine the culvert and drainage channels sizes which includes the use of the rational calculation's spreadsheet and FlowMaster, V8i software.

Existing drainage features on-site have been analyzed for the following design storm events:

Minor Storm: 5-year Storm EventMajor Storm: 100-year Storm Event

VARIANCES FROM CRITERIA

There are no proposed variances from the El Paso County Criteria for the Project.

EXISTING DRAINAGE CONDITIONS

EXISTING DRAINAGE CONDITIONS

The existing drainage conditions for the site consists of numerous basins ranging in size from 0.59 acres to 8.56 acres, with slopes varying from 2% - 25%. Flow is accepted to the site form adjacent residential lots to the east. Runoff associated with the site flows from south to north and east to west, towards Kettle Creek. Runoff from the area south of Burgess Road is collected in existing roadside ditches along the south side of Burgess and does not flow across the roadway into the Site.



Existing Basin E-A

Drainage Basin E-A is 3.65 acres with a weighted imperviousness of 0.0%. The basin encompasses the southernmost region of the property and is bounded by basin E-B to the north and OE-A to the east. Drainage Basin E-A will also accept flows from off-site basin OE-A. The Direct Runoff values for the 5-year and 100-year storm events are 1.03 and 7.59 cubic feet per second (cfs), respectively. All runoff conveyed within the basin's existing conditions will approximately flow to design point E1 and into the adjacent property at 5650 Burgess Road.

Existing Basin E-B

Drainage Basin E-B is 6.08 acres with a weighted imperviousness of 0.0%. The basin encompasses the south-central region of the property and is bounded by the property line to the east & west and basins E-C & E-A to the north and south. Drainage Basin E-B will also accept flows from off-site basin OE-B. The Direct Runoff values for the 5-year and 100-year storm events are 1.66 and 12.08 cfs, respectively. All runoff conveyed within the basin's existing conditions will approximately flow to design point E2 and into the adjacent properties at 5650 and 5680 Burgess Road.

Existing Basin E-C

Drainage Basin E-C is 8.56 acres with a weighted imperviousness of 0.0%. The basin encompasses the central region of the property and is bound by the property line to the East & West and basins E-D & E-B to the north and south. Drainage Basin E-C will also accept flows from off-site basin OE-C and partially from OE-D. The Direct Runoff values for the 5-year and 100-year storm events are 1.92 and 14.13 cfs, respectively. All runoff conveyed within the basin's existing conditions will approximately flow to design point E3 and into the adjacent property 5680 Burgess Road.

Existing Basin E-D

Drainage Basin E-D is 7.50 acres with a weighted imperviousness of 0.0%. The basin encompasses the northeastern region of the property and is bounded by the property lines to the north and east, basin E-G to the west, and E-C to the south. Drainage Basin E-D will also accept flows from off-site basin OE-D and OE-E. The Direct Runoff values for the 5-year and 100-year storm events are 1.80 and 13.19 cfs, respectively. All runoff conveyed within the basin's existing conditions will approximately flow to design point E4. From design point E-4, channelized flows continue north towards Kettle Creek.

Existing Basin E-E

Drainage Basin E-E is 0.83 acres with a weighted imperviousness of 0.0%. The basin encompasses the northern region of the property, bounded by basin E-G and the northern property line. The Direct Runoff values for the 5-year and 100-year storm events are 0.25 and 1.87 cfs, respectively. All runoff conveyed within the basin's existing conditions will approximately flow northwest to design point E5. From design point E-5, channelized flows continue north towards Kettle Creek.



Existing Basin E-F

Drainage Basin E-F is 0.59 acres with a weighted imperviousness of 0.0%. The basin encompasses a small portion of the northern region of the property, bounded by basin E-G to the north/west and the site's property line to the south. The Direct Runoff values for the 5-year and 100-year storm events are 0.19 and 1.39 cfs, respectively. All runoff conveyed within the basin's existing conditions will approximately flow northwest to design point E6. From design point E-6, channelized flows continue northwest towards Kettle Creek.

Existing Basin E-G

Drainage Basin E-G is 7.15 acres with a weighted imperviousness of 0.0%. The basin encompasses most of the northwestern region of the property, and accepts flows from offsite basin OE-H. E-G is bounded by property lines to the north, west, and south, and basins E-E, E-F, E-C, and E-D. E-G. The Direct Runoff values for the 5-year and 100-year storm events are 2.01 and 14.80 cfs, respectively. All runoff conveyed within the basin's existing conditions will approximately flow northwest to design point E7. From design point E-7, channelized flows continue northwest towards Kettle Creek.

Existing Basin OE-A

Drainage Basin OE-A is 0.10 acres with a weighted imperviousness of 0.0%. The basin encompasses a small off-site area bounded by the site's property line to the west and basin OE-B to the north and east. The Direct Runoff values for the 5-year and 100-year storm events are 0.04 and 0.27 cfs, respectively. All runoff conveyed within the basin's existing conditions will approximately flow to design point E8 and into basin E-A.

Existing Basin OE-B

Drainage Basin OE-B is 0.86 acres with a weighted imperviousness of 0.0%. The basin encompasses a small off-site area bounded by the site's property line to the west, basin OE-C to the north, basin OE-D to the east, and basin OE-A to the south. The Direct Runoff values for the 5-year and 100-year storm events are 0.27 and 1.96 cfs, respectively. All runoff conveyed within the basin's existing conditions will approximately flow to design point E9 and into basin E-B.

Existing Basin OE-C

Drainage Basin OE-C is 2.19 acres with a weighted imperviousness of 0.0%. The basin encompasses an off-site area bounded by the site's property line to the west, basin OE-D to the north and east, and basin OE-B to the south. The Direct Runoff values for the 5-year and 100-year storm events are 0.66 and 4.86 cfs, respectively. All runoff conveyed within the basin's existing conditions will approximately flow to design point E10 and into basin E-C.

Existing Basin OE-D

Drainage Basin OE-D is 20.33 acres with a weighted imperviousness of 0.0%. The basin encompasses an off-site area bounded by the site's property line to the west, basin OE-E to the north and east, and basin OE-C to the south. The Direct Runoff values for the 5-year and 100-year storm events are 5.63 and 41.36 cfs, respectively. All runoff conveyed within the basin's existing conditions will approximately flow to design point E11 and into basin E-D.



Existing Basin OE-E

Drainage Basin OE-E is 10.52 acres with a weighted imperviousness of 0.0%. The basin encompasses an off-site area bounded by the site's property line to the west and adjacent residential property to the north and east. Kettle Creek runs westward, directly north of this basin. The Direct Runoff values for the 5-year and 100-year storm events are 2.70 and 19.82 cfs, respectively. All runoff conveyed within the basin's existing conditions will approximately flow to design point E12 and into basin E-D towards design point E4 and eventually northwards towards Kettle Creek.

Existing Basin OE-H

Drainage Basin OE-H is 5.36 acres with a weighted imperviousness of 0.0%. The basin encompasses an off-site area bounded by the site's property line to the north and east and adjacent residential property to the south and west. The Direct Runoff values for the 5-year and 100-year storm events are 1.52 and 11.16 cfs, respectively. All runoff conveyed within the basin's existing conditions will approximately flow to design point E13 and into basin E-G through an existing natural channel towards design point E7 and continue north towards Kettle Creek.

PROPOSED DRAINAGE CONDITIONS

Drainage conditions for the proposed site are similar to that of the existing site, with improvements that prevent flows generated on-site from flowing into the adjacent properties to the west: 5650 and 5680 Burgess Road. These improvements are associated with the potential proposed shared driveway access for the three residential lots included in the plat. Along the eastern edge of the future driveway is a proposed ditch, conveying runoff northwards. Within the northern vicinity of proposed basin P-A is where a proposed culvert is identified to facilitate flow from the swale, beneath the potential future driveway, and northwest towards Kettle Creek. For this crossing a 36-inch CMP culvert will have the capacity for the 100-year storm or an 18-inch CMP for the 5-year storm with larger storm events topping the driveway. A concrete lowering with riprap placed both upstream and downstream of the lowering would also be acceptable. These improvements will be completed by home builder of Lot 3. Reference Appendix E for capacity calculations. The location and placement of the culvert will be determined with the driveway design but should be placed north of the existing property to corner to allow flows to remain on the Site without accumulated runoff entering the adjacent properties to the west.

There is natural drainage swale that conveys existing flows in existing conditions and the culvert accommodates the proposed flows. A 30-foot drainage easement is proposed along this drainage swale. The natural channel conveys these flows to a heavily vegetated forest and stable outfall. In existing conditions, no further alteration to the topography would be necessary.

Given the numerous unknowns regarding future development of the site, a generous assumption/estimate for weighted imperviousness was made regarding the quantity of proposed houses, and overall size of building footprints and driveways. The proposed conditions assume four total houses each with separate paved (future material unknown) driveways. Additionally, each building footprint is 10,000 SF, which is an extremely large size for this project (assuming a large house footprint and accessory structure). Even with utilizing these conservative parameters for imperviousness, the total weighted imperviousness for the site was calculated at approximately 3.3%. For a typical 5-acre lot, a 7% imperviousness has been widely accepted. The average lot size for these three lots is over 11 acres in size. In taking a general trend of



imperviousness vs. lot size, a 3.5% to 4% imperviousness is in line with an over 11-acre size. The provided 3.3% imperviousness matches these empirical assumptions.

PROPOSED DRAINAGE BASINS

Proposed Basin P-A

Drainage Basin P-A is 18.28 acres with a weighted imperviousness of 10.0%. The basin encompasses the southern and central regions of the property and is bounded by site property line to the south and west, basin OP-A to the east, and basin P-B to the north. Drainage Basin P-A will also accept flows from off-site basin OP-A and part of OP-B. The Direct Runoff values for the 5-year and 100-year storm events are 7.60 and 36.26 cfs, respectively. All runoff conveyed within the basin's proposed conditions will approximately flow to design point P1 into a proposed 18 inch CMP culvert (5 Year) 36 inch CMP culvert (100 YR) or concrete lowering to be design with the driveway of the home, and westwards to Kettle Creek.

Proposed Basin P-B

Drainage Basin P-B is 7.50 acres with a weighted imperviousness of 1.8%. The basin encompasses the northeastern region of the property and is bounded by site property line to the north, P-C to the west, OP-B & OP-C to the east, and basin P-A to the south. Basin P-B will also accept flows from off-site basin OP-B and part of OP-C. The Direct Runoff values for the 5-year and 100-year storm events are 2.06 and 15.16 cfs, respectively. All runoff conveyed within the basin's proposed conditions will approximately flow to design point P2, then northwards towards Kettle Creek.

Proposed Basin P-C

Drainage Basin P-C is 7.17 acres with a weighted imperviousness of 6.3%. The basin encompasses most of the northwestern region of the property and accepts flows from Drainage Basin P-A. P-C is bounded by the site property line to the north, west, and south, and basins P-A and P-B to the east and south. The Direct Runoff values for the 5-year and 100-year storm events are 2.57 and 15.01 cfs, respectively. All runoff conveyed within the basin's proposed conditions will approximately flow to design point P3, then north/west towards Kettle Creek.

Proposed Basin P-D

Drainage Basin P-D is 0.83 acres with a weighted imperviousness of 0.0%. The basin encompasses a small area within the northwestern region of the property. P-D is bounded by the site property line to the north and P-C to the west, east, and south. The Direct Runoff values for the 5-year and 100-year storm events are 0.25 and 1.87 cfs, respectively. All runoff conveyed within the basin's proposed conditions will approximately flow to design point P4, then north/west towards Kettle Creek.

Proposed Basin P-E

Drainage Basin P-E is 0.59 acres with a weighted imperviousness of 0.0%. The basin encompasses a small area within the northwestern region of the property. P-E is bounded by the site property line to the west & south and basin P-C to the north and east. The Direct Runoff



values for the 5-year and 100-year storm events are 0.19 and 1.39 cfs, respectively. All runoff conveyed within the basin's proposed conditions will approximately flow to design point P5, then north/west towards Kettle Creek.

Proposed Basin OP-A

Drainage Basin OP-A is 3.15 acres with a weighted imperviousness of 0.0%. The basin encompasses a small area within the northwestern region of the property. OP-A is bounded by the site property line to the west, Burgess Road to the south, and basin OP-B to the north and east. The Direct Runoff values for the 5-year and 100-year storm events are 0.95 and 6.98 cfs, respectively. All runoff conveyed within the basin's proposed conditions will approximately flow to design point P6, then north/west into basin P-A.

Proposed Basin OP-B

Drainage Basin OP-B is 20.33 acres with a weighted imperviousness of 0.0%. The basin encompasses a small area within the northwestern region of the property. OP-B is bounded by the site property line to the west, Burgess Road to the south, and basin OP-C to the north and east. The Direct Runoff values for the 5-year and 100-year storm events are 5.51 and 40.46 cfs, respectively. All runoff conveyed within the basin's proposed conditions will approximately flow to design point P7, then north/west into basin P-B.

Proposed Basin OP-C

Drainage Basin OP-C is 10.52 acres with a weighted imperviousness of 0.0%. The basin encompasses a small area within the northwestern region of the property. OP-C is bounded by the site property line to the west and OP-B to the south. The Direct Runoff values for the 5-year and 100-year storm events are 2.66 and 19.57 cfs, respectively. All runoff conveyed within the basin's proposed conditions will approximately flow to design point P8, then north/west into basin P-B.

Proposed Basin OP-H

Drainage Basin OP-H is 5.36 acres with a weighted imperviousness of 0.0%. The basin encompasses an off-site area bounded by the site's property line to the north and east and adjacent residential property to the south and west. The Direct Runoff values for the 5-year and 100-year storm events are 1.52 and 11.16 cfs, respectively. All runoff conveyed within the basin's existing conditions will approximately flow to design point P13 and into basin P-C through an existing natural channel towards design point P3 and continue north towards Kettle Creek.

EMERGENCY OVERFLOW ROUTING

All overflow routing will be directed to the Kettle Creek drainageway north of the site. This flow path is consistent with the historical stormwater runoff path.

HYDRAULIC ANALYSIS METHODOLOGY

The proposed drainage facilities were designed in accordance with the CRITERIA and MANUAL. Floodplain identification was determined using a custom FIRMette map by FEMA and information provided in the CRITERIA. Culvert capacity calculations were computed using Flow master.

There is no stormwater infrastructure proposed with the replat.



Guidance for future improvements is as follows: If platted lots are built out as single-family residential homes, a 18 inch CMP culvert (5 Year) or 36 CMP culvert (100 YR) would be an adequate solution to facilitate flow beneath the potential location for a driveway in Proposed Lot 2. FlowMaster modeling was used to size the potential proposed driveway culvert. See Appendix E for FlowMaster Calculations.

Four-Step Process

The Site was designed in accordance with the four-step process to minimize adverse impacts of urbanization, as outlined in Section I.7.2 BMP Selection of the MANUAL. The four-step process per the MANUAL provides guidance and requirements for the selection of siting of structural Best Management Practices (BMPs) for new development and significant redevelopment.

Step 1: Employ Runoff Reduction Practices

The purpose of this project is to replat the existing property, into three separate single-family lots. No infrastructure improvements are included with the replat. Per Section I.7.1B of Appendix I of the ECM, the single-family residences fall under the large lot exemption as the total impervious area is less than 10% of the area. A BESQCP permit will be required by the County to prevent erosion and mitigate any runoff due to those activities.

Step 2: Stabilize Drainageways

The Kettle Creek Drainageway flows just north of the Site. During a Site visit, it was found that the area (basins) tributary to the drainageway is currently well-stabilized and well-vegetated. As the drainageway is currently stable the existing drainageway can be left as-is in its stable condition. As noted in Chapter 1, Section 1.4 of the MANUAL, "Natural channel systems, primarily the designated Major Drainageways and Primary outfalls, serve to store flood waters, enhance water quality, provide for ground water recharge and preserve riparian corridors. The use of historical channels to convey storm water runoff from developed and developing areas is acceptable. However, if historical storm water flows are increased, or if historical channels are unstable in their natural conditions, these channels must be adequately stabilized to prevent excessive erosion." Additionally, Chapter 2, Section 2.2 of the MANUAL states, "A stable natural channel reaches 'equilibrium' over many years. Therefore, channel modifications should be minimal." Because the existing drainageway is properly stabilized, it is felt that attempts to change the natural channel may lead to destabilization of the drainageway and therefore, no changes to the drainageway, with the exception of stabilization at the location of the proposed ditches, or future accesses are driveways are recommended.

Step 3: Provide Water Quality Capture Volume (WQCV)

Per Section I.7.1B of Appendix I of the ECM, detention and water-quality facilities are not required for the Project. The purpose of this project is to replat the existing property into three separate single-family lots. No infrastructure improvements are included with the replat.

Full Exclusions per I.7.1.B.5

Large Lot Single Family Sites

A single-family residential lot, or agricultural zoned lands, greater than or equal to 2.5 acres in size per dwelling and having a total lot impervious area of less than 10 percent. A total lot imperviousness greater than 10 percent is allowed when a study specific to the watershed and/or MS4 shows that expected soil and vegetation conditions are suitable for infiltration/filtration of the WQCV for a typical site, and the permittee accepts such study as applicable within its MS4 boundaries. The maximum total lot impervious covered under this exclusion shall be 20 percent.



The 10% imperviousness includes the proposed shared private driveway within the calculations for the total impervious area for the lot. The builder will be forced to comply with the criteria to ensure the final impervious area is less than 10%.

Step 4: Consider Need for Industrial and Commercial BMPs

The proposed Project consists of a single-family subdivision. No industrial and commercial uses or developments are anticipated as part of the proposed development.

DETENTION AND WATER QUALITY REQUIREMENTS

As discussed in Section I.7.1B of Appendix I of the ECM, detention and water-quality facilities are not required for the Project as no improvements are to be made in association with the platting process. Therefore, there is also no addition of impervious area with the project.

Overall, the existing flows are approximately 25.57 CFS and 144.57 CFS for the 5-year and 100-year respectively. The proposed flows are approximately 23.33 CFS and 147.88 CFS for the 5-year and 100-year respectively.

There are two locations where the site outfalls in route to Kettle Creek. The first outfall is in the northwest corner of the site at design point E7 (existing) and P3 (proposed). Flows that are conveyed to this design point will travel via existing stabilized natural channels through forest and wooded vegetation (reference existing site photos). Total flows entering this area in existing conditions (sub-basins E-G, OE-H, E-C, OE-C, E-F, E-E, E-A, OE-A, E-B, OE-B) are approximately 9.56 CFS in the 5-year and 70.21 CFS in 100-year. In proposed conditions, the flows entering the area (sub-basins P-A, OP-A, OE-H, P-D, P-C, P-E) are approximately 13.09 CFS in the 5-year and 72.68 CFS in the 100-year. Refer to *Appendix G*, photos 1-6 for design point E7 (existing) P3 (proposed).

The second outfall is on the north end of the property of the site at design point E4 (existing) and P2 (proposed). Flows that are conveyed to this design point will travel via existing wooded vegetation. Total flows entering this area in existing conditions (sub-basins E-D, OE-E, OE-D) are approximately 10.12 CFS in the 5-year and 75.37 CFS in the 100-year. In proposed conditions, the flows entering the area (sub-basins P-B, OP-B, OP-C) are approximately 10.24 CFS in the 5-year and 75.20 CFS in the 100-year. Refer to **Appendix G**, photos 11-14 for design point E4 (existing) P2 (proposed).

Overall, the flows increase slightly from 144.57 CFS to 147.88 CFS in the 100-year event, a 3.31 CFS increase. Additionally, the proposed shared driveway is under 1-acre and less than 10% of total imperviousness for the entire proposed development. Additionally, the runoff generated from the proposed basins will sheet flow over densely wooded and naturally vegetated areas prior to entering Kettle Creek. These overland flow areas are extremely stable and the minimal increase in overall flow in the 100-year event will have a negligible impact. Subsequently, the proposed project would not pose any risk to existing downstream waterways or infrastructure.

Kettle Creek is a stable, healthy, and heavily vegetated existing waterway that has capacity and capability to accommodate the existing and proposed runoff. Additionally, flows conveyed to the design points travel approximately 700 ft before reaching Kettle Creek. Therefore, runoff flows have a major opportunity to infiltrate into the existing Type B soils.

The proposed project is adjacent to two existing properties on the west side of the site. The project proposes a shared driveway and a drainage ditch on the east side of the driveway to convey



runoff to the existing design point. Additionally, this drainage ditch will protect neighboring properties to the west by capturing any runoff that was conveyed in that direction pre-development and the new post-development flows. No proposed additional flows will negatively impact the adjacent properties.

EROSION CONTROL PLAN

Erosion Control Plans with the Minor Subdivision are not required. A BESQCP permit will be required by the County to prevent erosion and mitigate any runoff due to those activities.

FLOODPLAIN STATEMENT

The area within the site exists outside of any special flood hazard areas and are completely outside the 0.2% annual chance floodplain. This is represented on FEMA Maps 08041C0315G and 08041C0526 (Appendix D), revised on December 7, 2018; also, FEMA Firmette Map exported on December 1, 2021. The El Paso County Requirements specify that the Base Flood Elevation be shown on the Final Plat per section RBC313.18.5, as necessary.

FEES DEVELOPMENT

APPLICABLE FEES

The project is within the Kettle Creek Drainage Basin and per El Paso County Drainage Basin Fees for Kettle Creek the fee per acre of impervious area is \$12,463.00. The calculated weighted imperviousness for the site is 3.3% based on an assumed pavement and roof area. This may differ from actual areas at time of construction. The maximum allowable areas are provided on the proposed drainage map. Additional fees may be assessed should these areas increase at the time of building permit. A 25% reduction was applied to reduce imperviousness to 2.5%, per section 3.10.2a, Appendix L, of the El Paso County Engineering Criteria Manual. This is multiplied by the total site area and then multiplied by the fee per acre of impervious area. The total fee would be \$10,601.74 (see below). There are no bridge fees for Kettle Creek Drainage Basin.

| Receiving Waters Di | rainage Basin | Fee per Impervious Acre | Total Acres | Imperviousness | Imperviousness with 25% Reduction | Total Acres * I | Total Fee |
|---------------------|---------------|-------------------------|-------------|----------------|-----------------------------------|-----------------|-------------|
| Monument Creek Ke | ettle Creek | \$ 12,463.00 | 34.37 | 3.3% | 2.5% | 0.8506575 | \$10,601.74 |

CONSTRUCTION COST OPINION

There are no public drainage ponds or permanent control measures proposed as part of the Project.

MAINTENANCE AND OPERATIONS

There are no public drainage ponds or permanent control measures proposed as part of the Project.

SUMMARY

COMPLIANCE WITH STANDARDS

The drainage design presented within this report conforms to the El Paso County Storm Drainage Criteria and the Mile High Flood Control District Manual. Additionally, the minor subdivision plat will not adversely affect the downstream and surrounding developments or waterways.



REFERENCES

- 1. The City of Colorado Springs Drainage Criteria Manual, May 2014
- 2. El Paso County Drainage Criteria Manual, Vol. 1 and 2, October 1994
- 3. Urban Drainage and Flood Control District Drainage Criteria Manual (UDFCDCM), Vol. 1, prepared by Wright-McLaughlin Engineers, June 2001, with latest revisions.
- 4. Flood Insurance Rate Map, El Paso County, Colorado and Incorporated Areas, Map Number 08041C03040G, Effective Date December 7, 2018, prepared by the Federal Emergency Management Agency (FEMA).

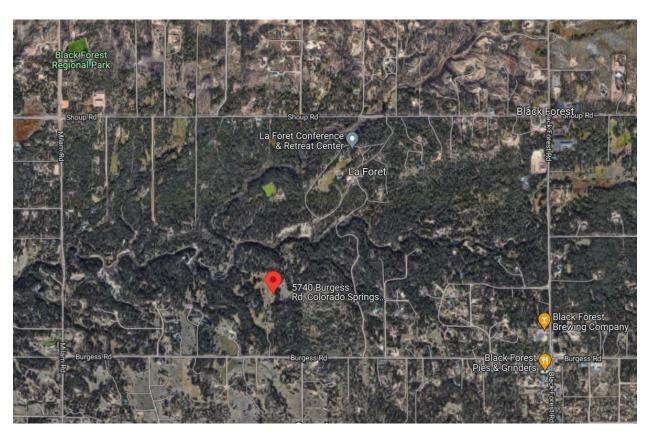


APPENDIX



APPENDIX A - VICINITY MAP





Appendix A

APPENDIX B - NRCS SOIL SURVEY

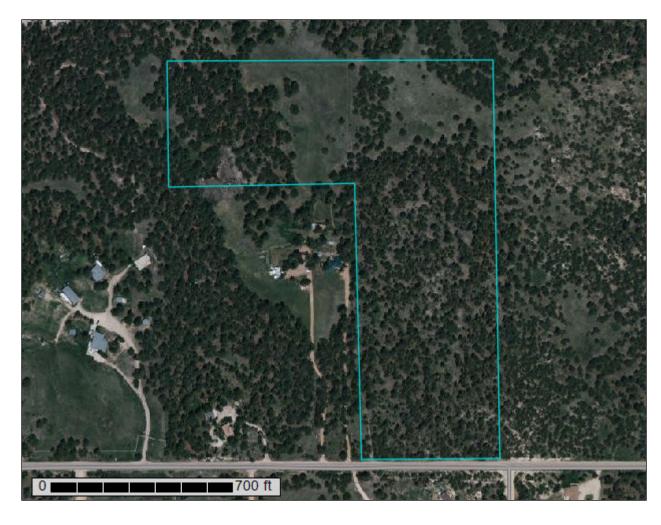




Natural Resources Conservation Service A product of the National Cooperative Soil Survey, a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local participants

Custom Soil Resource Report for El Paso County Area, Colorado

Renehan Subdivision



Preface

Soil surveys contain information that affects land use planning in survey areas. They highlight soil limitations that affect various land uses and provide information about the properties of the soils in the survey areas. Soil surveys are designed for many different users, including farmers, ranchers, foresters, agronomists, urban planners, community officials, engineers, developers, builders, and home buyers. Also, conservationists, teachers, students, and specialists in recreation, waste disposal, and pollution control can use the surveys to help them understand, protect, or enhance the environment.

Various land use regulations of Federal, State, and local governments may impose special restrictions on land use or land treatment. Soil surveys identify soil properties that are used in making various land use or land treatment decisions. The information is intended to help the land users identify and reduce the effects of soil limitations on various land uses. The landowner or user is responsible for identifying and complying with existing laws and regulations.

Although soil survey information can be used for general farm, local, and wider area planning, onsite investigation is needed to supplement this information in some cases. Examples include soil quality assessments (http://www.nrcs.usda.gov/wps/portal/nrcs/main/soils/health/) and certain conservation and engineering applications. For more detailed information, contact your local USDA Service Center (https://offices.sc.egov.usda.gov/locator/app?agency=nrcs) or your NRCS State Soil Scientist (http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/contactus/?cid=nrcs142p2 053951).

Great differences in soil properties can occur within short distances. Some soils are seasonally wet or subject to flooding. Some are too unstable to be used as a foundation for buildings or roads. Clayey or wet soils are poorly suited to use as septic tank absorption fields. A high water table makes a soil poorly suited to basements or underground installations.

The National Cooperative Soil Survey is a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local agencies. The Natural Resources Conservation Service (NRCS) has leadership for the Federal part of the National Cooperative Soil Survey.

Information about soils is updated periodically. Updated information is available through the NRCS Web Soil Survey, the site for official soil survey information.

The U.S. Department of Agriculture (USDA) prohibits discrimination in all its programs and activities on the basis of race, color, national origin, age, disability, and where applicable, sex, marital status, familial status, parental status, religion, sexual orientation, genetic information, political beliefs, reprisal, or because all or a part of an individual's income is derived from any public assistance program. (Not all prohibited bases apply to all programs.) Persons with disabilities who require

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How Soil Surveys Are Made

Soil surveys are made to provide information about the soils and miscellaneous areas in a specific area. They include a description of the soils and miscellaneous areas and their location on the landscape and tables that show soil properties and limitations affecting various uses. Soil scientists observed the steepness, length, and shape of the slopes; the general pattern of drainage; the kinds of crops and native plants; and the kinds of bedrock. They observed and described many soil profiles. A soil profile is the sequence of natural layers, or horizons, in a soil. The profile extends from the surface down into the unconsolidated material in which the soil formed or from the surface down to bedrock. The unconsolidated material is devoid of roots and other living organisms and has not been changed by other biological activity.

Currently, soils are mapped according to the boundaries of major land resource areas (MLRAs). MLRAs are geographically associated land resource units that share common characteristics related to physiography, geology, climate, water resources, soils, biological resources, and land uses (USDA, 2006). Soil survey areas typically consist of parts of one or more MLRA.

The soils and miscellaneous areas in a survey area occur in an orderly pattern that is related to the geology, landforms, relief, climate, and natural vegetation of the area. Each kind of soil and miscellaneous area is associated with a particular kind of landform or with a segment of the landform. By observing the soils and miscellaneous areas in the survey area and relating their position to specific segments of the landform, a soil scientist develops a concept, or model, of how they were formed. Thus, during mapping, this model enables the soil scientist to predict with a considerable degree of accuracy the kind of soil or miscellaneous area at a specific location on the landscape.

Commonly, individual soils on the landscape merge into one another as their characteristics gradually change. To construct an accurate soil map, however, soil scientists must determine the boundaries between the soils. They can observe only a limited number of soil profiles. Nevertheless, these observations, supplemented by an understanding of the soil-vegetation-landscape relationship, are sufficient to verify predictions of the kinds of soil in an area and to determine the boundaries.

Soil scientists recorded the characteristics of the soil profiles that they studied. They noted soil color, texture, size and shape of soil aggregates, kind and amount of rock fragments, distribution of plant roots, reaction, and other features that enable them to identify soils. After describing the soils in the survey area and determining their properties, the soil scientists assigned the soils to taxonomic classes (units). Taxonomic classes are concepts. Each taxonomic class has a set of soil characteristics with precisely defined limits. The classes are used as a basis for comparison to classify soils systematically. Soil taxonomy, the system of taxonomic classification used in the United States, is based mainly on the kind and character of soil properties and the arrangement of horizons within the profile. After the soil

Custom Soil Resource Report

scientists classified and named the soils in the survey area, they compared the individual soils with similar soils in the same taxonomic class in other areas so that they could confirm data and assemble additional data based on experience and research.

The objective of soil mapping is not to delineate pure map unit components; the objective is to separate the landscape into landforms or landform segments that have similar use and management requirements. Each map unit is defined by a unique combination of soil components and/or miscellaneous areas in predictable proportions. Some components may be highly contrasting to the other components of the map unit. The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The delineation of such landforms and landform segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, onsite investigation is needed to define and locate the soils and miscellaneous areas.

Soil scientists make many field observations in the process of producing a soil map. The frequency of observation is dependent upon several factors, including scale of mapping, intensity of mapping, design of map units, complexity of the landscape, and experience of the soil scientist. Observations are made to test and refine the soil-landscape model and predictions and to verify the classification of the soils at specific locations. Once the soil-landscape model is refined, a significantly smaller number of measurements of individual soil properties are made and recorded. These measurements may include field measurements, such as those for color, depth to bedrock, and texture, and laboratory measurements, such as those for content of sand, silt, clay, salt, and other components. Properties of each soil typically vary from one point to another across the landscape.

Observations for map unit components are aggregated to develop ranges of characteristics for the components. The aggregated values are presented. Direct measurements do not exist for every property presented for every map unit component. Values for some properties are estimated from combinations of other properties.

While a soil survey is in progress, samples of some of the soils in the area generally are collected for laboratory analyses and for engineering tests. Soil scientists interpret the data from these analyses and tests as well as the field-observed characteristics and the soil properties to determine the expected behavior of the soils under different uses. Interpretations for all of the soils are field tested through observation of the soils in different uses and under different levels of management. Some interpretations are modified to fit local conditions, and some new interpretations are developed to meet local needs. Data are assembled from other sources, such as research information, production records, and field experience of specialists. For example, data on crop yields under defined levels of management are assembled from farm records and from field or plot experiments on the same kinds of soil.

Predictions about soil behavior are based not only on soil properties but also on such variables as climate and biological activity. Soil conditions are predictable over long periods of time, but they are not predictable from year to year. For example, soil scientists can predict with a fairly high degree of accuracy that a given soil will have a high water table within certain depths in most years, but they cannot predict that a high water table will always be at a specific level in the soil on a specific date.

After soil scientists located and identified the significant natural bodies of soil in the survey area, they drew the boundaries of these bodies on aerial photographs and

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identified each as a specific map unit. Aerial photographs show trees, buildings, fields, roads, and rivers, all of which help in locating boundaries accurately.

Soil Map

The soil map section includes the soil map for the defined area of interest, a list of soil map units on the map and extent of each map unit, and cartographic symbols displayed on the map. Also presented are various metadata about data used to produce the map, and a description of each soil map unit.



MAP LEGEND

Area of Interest (AOI)

Area of Interest (AOI)

Soils

Soil Map Unit Polygons

-

Soil Map Unit Lines

Soil Map Unit Points

Special Point Features

(0)

Blowout

 \boxtimes

Borrow Pit

Ж

Clay Spot

364

Closed Depression

~

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Gravelly Spot

0

Landfill

٨.

Lava Flow

_

Marsh or swamp

Mine or Quarry

仌

Miscellaneous Water

0

Perennial Water

O

Rock Outcrop

+

Saline Spot

0.0

Sandy Spot

-

Severely Eroded Spot

Sinkhole

8

Slide or Slip

Ø

Sodic Spot

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Spoil Area Stony Spot

Ø

Very Stony Spot

8

Wet Spot Other

Δ

Special Line Features

Water Features

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Streams and Canals

Transportation

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Rails

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Interstate Highways

US Routes

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Major Roads

~

Local Roads

Background

Marie Contract

Aerial Photography

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24.000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service Web Soil Survey URL:

Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: El Paso County Area, Colorado Survey Area Data: Version 20, Sep 2, 2022

Soil map units are labeled (as space allows) for map scales 1:50.000 or larger.

Date(s) aerial images were photographed: Jun 9, 2021—Jun 12, 2021

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Map Unit Legend

| Map Unit Symbol | Map Unit Name | Acres in AOI | Percent of AOI | | | |
|-----------------------------|--|--------------|----------------|--|--|--|
| 40 | Kettle gravelly loamy sand, 3 to 8 percent slopes | 26.6 | 98.6% | | | |
| 41 | Kettle gravelly loamy sand, 8 to 40 percent slopes | 0.4 | 1.4% | | | |
| Totals for Area of Interest | | 27.0 | 100.0% | | | |

Map Unit Descriptions

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however,

Custom Soil Resource Report

onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An association is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

El Paso County Area, Colorado

40—Kettle gravelly loamy sand, 3 to 8 percent slopes

Map Unit Setting

National map unit symbol: 368g Elevation: 7,000 to 7,700 feet

Farmland classification: Not prime farmland

Map Unit Composition

Kettle and similar soils: 85 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Kettle

Setting

Landform: Hills

Landform position (three-dimensional): Side slope

Down-slope shape: Linear Across-slope shape: Linear

Parent material: Sandy alluvium derived from arkose

Typical profile

E - 0 to 16 inches: gravelly loamy sand *Bt - 16 to 40 inches:* gravelly sandy loam

C - 40 to 60 inches: extremely gravelly loamy sand

Properties and qualities

Slope: 3 to 8 percent

Depth to restrictive feature: More than 80 inches Drainage class: Somewhat excessively drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): High (2.00 to 6.00

in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water supply, 0 to 60 inches: Low (about 3.4 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 4e

Hydrologic Soil Group: B

Ecological site: F048AY908CO - Mixed Conifer

Hydric soil rating: No

Minor Components

Other soils

Percent of map unit: Hydric soil rating: No

Pleasant

Percent of map unit: Landform: Depressions Hydric soil rating: Yes

41—Kettle gravelly loamy sand, 8 to 40 percent slopes

Map Unit Setting

National map unit symbol: 368h Elevation: 7,000 to 7,700 feet

Farmland classification: Not prime farmland

Map Unit Composition

Kettle and similar soils: 85 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Kettle

Setting

Landform: Hills

Landform position (three-dimensional): Side slope

Down-slope shape: Linear Across-slope shape: Linear

Parent material: Sandy alluvium derived from arkose

Typical profile

E - 0 to 16 inches: gravelly loamy sand Bt - 16 to 40 inches: gravelly sandy loam

C - 40 to 60 inches: extremely gravelly loamy sand

Properties and qualities

Slope: 8 to 40 percent

Depth to restrictive feature: More than 80 inches Drainage class: Somewhat excessively drained

Runoff class: Medium

Capacity of the most limiting layer to transmit water (Ksat): High (2.00 to 6.00

in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water supply, 0 to 60 inches: Low (about 3.4 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 7e

Hydrologic Soil Group: B

Ecological site: F048AY908CO - Mixed Conifer

Hydric soil rating: No

Minor Components

Other soils

Percent of map unit: Hydric soil rating: No

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Pleasant

Percent of map unit: Landform: Depressions Hydric soil rating: Yes

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APPENDIX C – FEMA FIRM MAP



NOTES TO USERS

This map is for use in administering the National Flood Insurance Program. It does not necessarily identify all areas subject to flooding, particularly from local drainage sources of small size. The community map repository should be consulted for possible updated or additional flood hazard information.

To obtain more detailed information in areas where Base Flood Elevations (BFEs) and/or floodways have been determined, users are encouraged to consult the Flood Profiles and Floodway Data and/or Summary of Stillwater Elevations tables contained within the Flood Insurance Study (FIS) report that accompanies this FIRM. Users should be aware that BFEs shown on the FIRM represent rounded whole-foot elevations. These BFEs are intended for flood insurance rating purposes only and should not be used as the sole source of flood elevation information. Accordingly, flood elevation data presented in the FIS report should be utilized in conjunction with the FIRM for purposes of construction and/or floodplain management.

Coastal Base Flood Elevations shown on this map apply only landward of 0.0' North American Vertical Datum of 1988 (NAVD88). Users of this FIRM should be aware that coastal flood elevations are also provided in the Summary of Stillwater Elevations table in the Flood Insurance Study report for this jurisdiction. Elevations shown in the Summary of Stillwater Elevations table should be used for construction and/or floodplain management purposes when they are higher than the elevations shown on this FIRM.

Boundaries of the floodways were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations with regard to requirements of the National Flood Insurance Program. Floodway widths and other pertinent floodway data are provided in the Flood Insurance Study report for this jurisdiction.

Certain areas not in Special Flood Hazard Areas may be protected by flood control structures. Refer to section 2.4 "Flood Protection Measures" of the Flood Insurance Study report for information on flood control structures for this jurisdiction.

The projection used in the preparation of this map was Universal Transverse Mercator (UTM) zone 13. The horizontal datum was NAD83, GRS80 spheroid. Differences in datum, spheroid, projection or UTM zones zones used in the production of FIRMs for adjacent jurisdictions may result in slight positional differences in map features across jurisdiction boundaries. These differences do not affect the accuracy of this FIRM.

Flood elevations on this map are referenced to the North American Vertical Datum of 1988 (NAVD88). These flood elevations must be compared to structure and ground elevations referenced to the same vertical datum. For information regarding conversion between the National Geodetic Vertical Datum of 1929 and the North American Vertical Datum of 1988, visit the National Geodetic Survey website a http://www.ngs.noaa.gov/ or contact the National Geodetic Survey at the following

NGS Information Services NOAA, N/NGS12 National Geodetic Survey SSMC-3, #9202 1315 East-West Highway Silver Spring, MD 20910-3282

To obtain current elevation, description, and/or location information for bench marks shown on this map, please contact the Information Services Branch of the National Geodetic Survey at (301) 713-3242 or visit its website at http://www.ngs.noaa.gov/.

Base Map information shown on this FIRM was provided in digital format by El Paso County, Colorado Springs Utilities, City of Fountain, Bureau of Land Management, National Oceanic and Atmospheric Administration, United States Geological Survey, and Anderson Consulting Engineers, Inc. These data are current as of 2006.

This map reflects more detailed and up-to-date stream channel configurations and floodplain delineations than those shown on the previous FIRM for this jurisdiction. The floodplains and floodways that were transferred from the previous FIRM may have been adjusted to conform to these new stream channel configurations. As a result, the Flood Profiles and Floodway Data tables in the Flood Insurance Study Report (which contains authoritative hydraulic data) may reflect stream channe distances that differ from what is shown on this map. The profile baselines depicted on this map represent the hydraulic modeling baselines that match the flood profiles and Floodway Data Tables if applicable, in the FIS report. As a result, the profile paselines may deviate significantly from the new base map channel representation and may appear outside of the floodplain.

Corporate limits shown on this map are based on the best data available at the time of publication. Because changes due to annexations or de-annexations may have occurred after this map was published, map users should contact appropriate community officials to verify current corporate limit locations.

Please refer to the separately printed Map Index for an overview map of the county showing the layout of map panels; community map repository addresses; and a Listing of Communities table containing National Flood Insurance Program dates for each community as well as a listing of the panels on which each community is

Contact FEMA Map Service Center (MSC) via the FEMA Map Information eXchange (FMIX) 1-877-336-2627 for information on available products associated with this FIRM. Available products may include previously issued Letters of Map Change, a Flood Insurance Study Report, and/or digital versions of this map. The MSC may also be reached by Fax at 1-800-358-9620 and its website a http://www.msc.fema.gov/.

If you have questions about this map or questions concerning the National Flood Insurance Program in general, please call 1-877-FEMA MAP (1-877-336-2627) or visit the FEMA website at http://www.fema.gov/business/nfip.

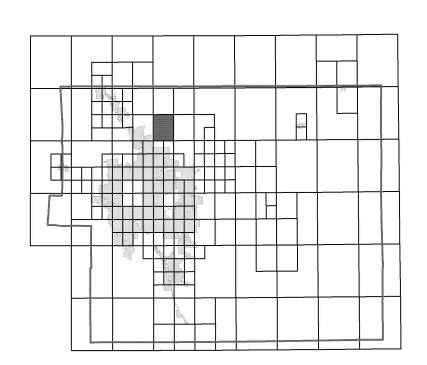
El Paso County Vertical Datum Offset Table

REFER TO SECTION 3.3 OF THE EL PASO COUNTY FLOOD INSURANCE STUDY

FOR STREAM BY STREAM VERTICAL DATUM CONVERSION INFORMATION

Flooding Source

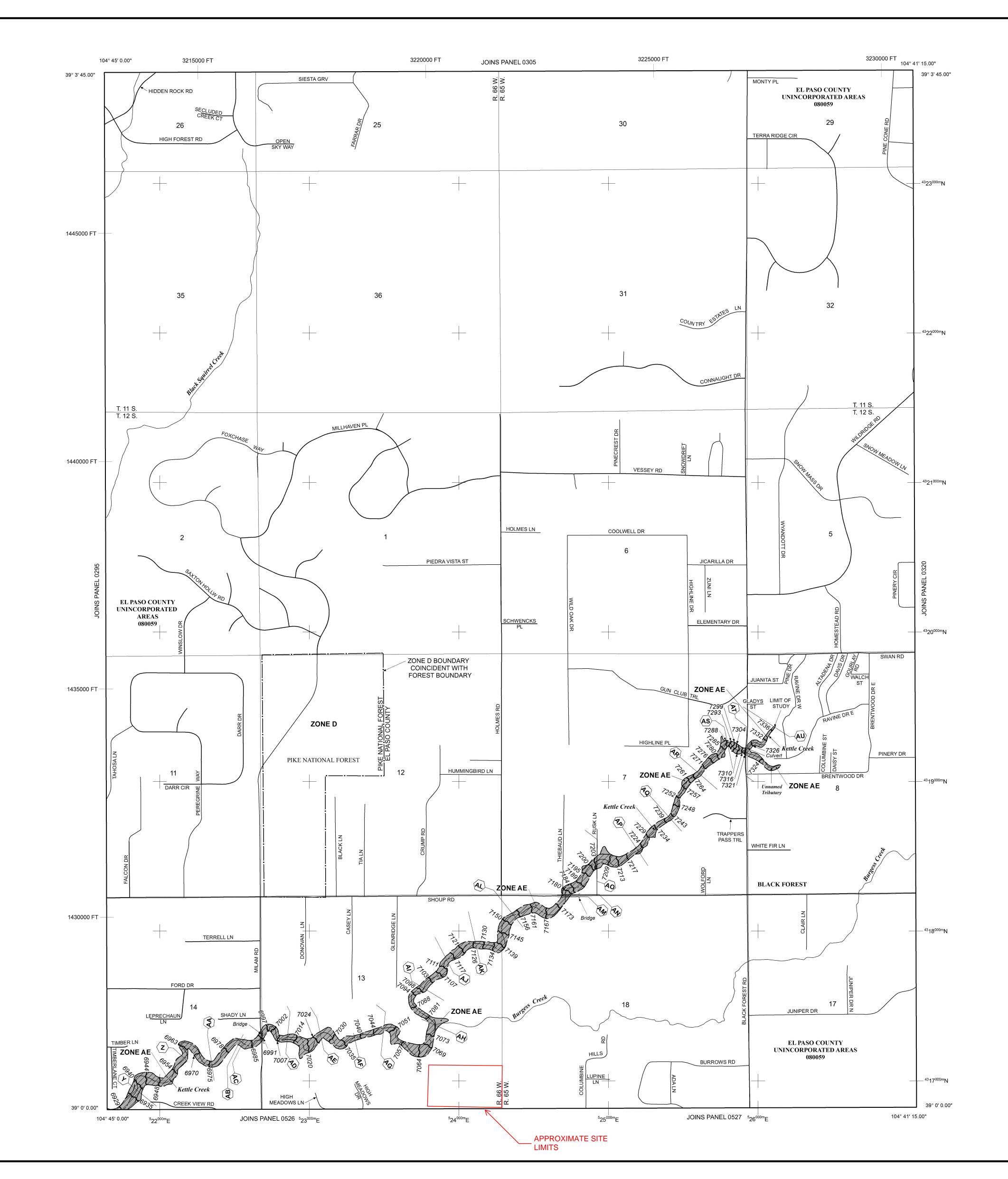
Panel Location Map



This Digital Flood Insurance Rate Map (DFIRM) was produced through a Cooperating Technical Partner (CTP) agreement between the State of Colorado Water Conservation Board (CWCB) and the Federal Emergency Management Agency (FEMA).



Additional Flood Hazard information and resources are available from local communities and the Colorado Water Conservation Board.



LEGEND

SPECIAL FLOOD HAZARD AREAS (SFHAS) SUBJECT TO INUNDATION BY THE 1% ANNUAL CHANCE FLOOD

The 1% annual chance flood (100-year flood), also known as the base flood, is the flood that has a 1% chance of being equaled or exceeded in any given year. The Special Flood Hazard Area is the area subject to flooding by the 1% annual chance flood. Areas of Special Flood Hazard include Zones A, AE, AH, AO, AR, A99, V, and VE. The Base Flood Elevation is the water-surface elevation of the 1% annual chance flood.

ZONE A No Base Flood Elevations determined. **ZONE AE** Base Flood Elevations determined.

Flood depths of 1 to 3 feet (usually areas of ponding); Base Flood Elevations determined

ZONE AO Flood depths of 1 to 3 feet (usually sheet flow on sloping terrain); average depths determined. For areas of alluvial fan flooding, velocities also

ZONE AR Special Flood Hazard Area Formerly protected from the 1% annual chance flood by a flood control system that was subsequently decertified. Zone AR indicates that the former flood control system is being restored to provide protection from the 1% annual chance or greater flood.

ZONE A99 Area to be protected from 1% annual chance flood by a Federal flood protection system under construction; no Base Flood Elevations

Coastal flood zone with velocity hazard (wave action); no Base Flood Elevations determined.

ZONE VE Coastal flood zone with velocity hazard (wave action); Base Flood

Elevations determined. FLOODWAY AREAS IN ZONE AE

The floodway is the channel of a stream plus any adjacent floodplain areas that must be kept free of encroachment so that the 1% annual chance flood can be carried without substantial increases in flood heights.

OTHER FLOOD AREAS

Areas of 0.2% annual chance flood; areas of 1% annual chance flood with average depths of less than 1 foot or with drainage areas less than 1 square mile; and areas protected by levees from 1% annual chance flood.

OTHER AREAS

Areas determined to be outside the 0.2% annual chance floodplain. Areas in which flood hazards are undetermined, but possible.

COASTAL BARRIER RESOURCES SYSTEM (CBRS) AREAS

OTHERWISE PROTECTED AREAS (OPAs)

CBRS areas and OPAs are normally located within or adjacent to Special Flood Hazard Areas.

Floodplain boundary Floodway boundary Zone D Boundary

••••••• CBRS and OPA boundary Boundary dividing Special Flood Hazard Areas of different Base

Flood Elevations, flood depths or flood velocities. *∼* 513 *∼* − Base Flood Elevation line and value; elevation in feet* (EL 987) Base Flood Elevation value where uniform within zone;

elevation in feet* * Referenced to the North American Vertical Datum of 1988 (NAVD 88)

Cross section line

97° 07' 30 00"

Geographic coordinates referenced to the North American 32° 22' 30.00" Datum of 1983 (NAD 83) 1000-meter Universal Transverse Mercator grid ticks,

5000-foot grid ticks: Colorado State Plane coordinate 6000000 FT system, central zone (FIPSZONE 0502),

Bench mark (see explanation in Notes to Users section of this FIRM panel)

MAP REPOSITORIES Refer to Map Repositories list on Map Index EFFECTIVE DATE OF COUNTYWIDE FLOOD INSURANCE RATE MAP

EFFECTIVE DATE(S) OF REVISION(S) TO THIS PANEL DECEMBER 7, 2018 - to update corporate limits, to change Base Flood Elevations and Special Flood Hazard Areas, to update map format, to add roads and road names, and to incorporate previously issued Letters of Map Revision.

MARCH 17, 1997

For community map revision history prior to countywide mapping, refer to the Community

Map History Table located in the Flood Insurance Study report for this jurisdiction.

To determine if flood insurance is available in this community, contact your insurance agent or call the National Flood Insurance Program at 1-800-638-6620.

PANEL 0315G

FIRM FLOOD INSURANCE RATE MAP

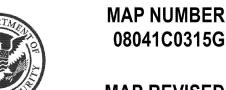
EL PASO COUNTY, **COLORADO** AND INCORPORATED AREAS

PANEL 315 OF 1300 (SEE MAP INDEX FOR FIRM PANEL LAYOUT)

CONTAINS:

NUMBER <u>PANEL</u> 080059 EL PASO COUNTY

Notice to User: The Map Number shown below should be used when placing map orders: the Community Number shown above should be used on insurance applications for the



08041C0315G **MAP REVISED**

DECEMBER 7, 2018

| | Federal Emergency Management Agency

NOTES TO USERS

This map is for use in administering the National Flood Insurance Program. It does not necessarily identify all areas subject to flooding, particularly from local drainage sources of small size. The community map repository should be consulted for possible updated or additional flood hazard information.

To obtain more detailed information in areas where Base Flood Elevations (BFEs) and/or floodways have been determined, users are encouraged to consult the Flood Profiles and Floodway Data and/or Summary of Stillwater Elevations tables contained within the Flood Insurance Study (FIS) report that accompanies this FIRM. Users should be aware that BFEs shown on the FIRM represent rounded whole-foot elevations. These BFEs are intended for flood insurance rating purposes only and should not be used as the sole source of flood elevation information. Accordingly, flood elevation data presented in the FIS report should be utilized in conjunction with the FIRM for purposes of construction and/or floodplain management.

Coastal Base Flood Elevations shown on this map apply only landward of 0.0' North American Vertical Datum of 1988 (NAVD88). Users of this FIRM should be aware that coastal flood elevations are also provided in the Summary of Stillwater Elevations table in the Flood Insurance Study report for this jurisdiction. Elevations shown in the Summary of Stillwater Elevations table should be used for construction and/or loodplain management purposes when they are higher than the elevations shown on

Boundaries of the floodways were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations with regard to requirements of the National Flood Insurance Program. Floodway widths and other pertinent floodway data are provided in the Flood Insurance Study report for this jurisdiction.

Certain areas not in Special Flood Hazard Areas may be protected by flood control **structures**. Refer to section 2.4 "Flood Protection Measures" of the Flood Insurance Study report for information on flood control structures for this jurisdiction.

The projection used in the preparation of this map was Universal Transverse Mercator (UTM) zone 13. The horizontal datum was NAD83, GRS80 spheroid. Differences in datum, spheroid, projection or UTM zones zones used in the production of FIRMs for adjacent jurisdictions may result in slight positional differences in map features across jurisdiction boundaries. These differences do not affect the accuracy of this FIRM.

Flood elevations on this map are referenced to the North American Vertical Datum of 1988 (NAVD88). These flood elevations must be compared to structure and ground elevations referenced to the same vertical datum. For information regarding conversion between the National Geodetic Vertical Datum of 1929 and the North American Vertical Datum of 1988, visit the National Geodetic Survey website at http://www.ngs.noaa.gov/ or contact the National Geodetic Survey at the following

NGS Information Services NOAA, N/NGS12 National Geodetic Survey SSMC-3, #9202 1315 East-West Highway Silver Spring, MD 20910-3282

To obtain current elevation, description, and/or location information for bench marks shown on this map, please contact the Information Services Branch of the National Geodetic Survey at (301) 713-3242 or visit its website at http://www.ngs.noaa.gov/.

Base Map information shown on this FIRM was provided in digital format by El Paso County, Colorado Springs Utilities, and Anderson Consulting Engineers, Inc. These data are current as of 2008.

This map reflects more detailed and up-to-date stream channel configurations and floodplain delineations than those shown on the previous FIRM for this jurisdiction. The floodplains and floodways that were transferred from the previous FIRM may have been adjusted to conform to these new stream channel configurations. As a result, the Flood Profiles and Floodway Data tables in the Flood Insurance Study Report (which contains authoritative hydraulic data) may reflect stream channel distances that differ from what is shown on this map. The profile baselines depicted on this map represent the hydraulic modeling baselines that match the flood profiles and Floodway Data Tables if applicable, in the FIS report. As a result, the profile baselines may deviate significantly from the new base map channel representation

Corporate limits shown on this map are based on the best data available at the time of publication. Because changes due to annexations or de-annexations may have occurred after this map was published, map users should contact appropriate community officials to verify current corporate limit locations.

Please refer to the separately printed Map Index for an overview map of the county showing the layout of map panels; community map repository addresses; and a Listing of Communities table containing National Flood Insurance Program dates for each community as well as a listing of the panels on which each community is

Contact FEMA Map Service Center (MSC) via the FEMA Map Information eXchange (FMIX) 1-877-336-2627 for information on available products associated with this FIRM. Available products may include previously issued Letters of Map Change, a Flood Insurance Study Report, and/or digital versions of this map. The MSC may also be reached by Fax at 1-800-358-9620 and its website at http://www.msc.fema.gov/.

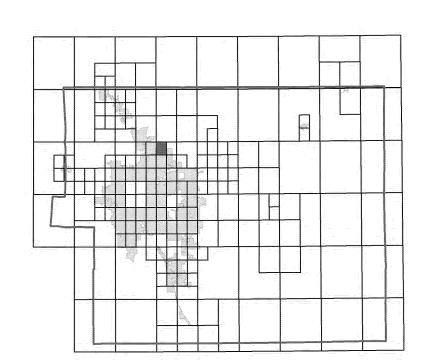
f you have questions about this map or questions concerning the National Flood nsurance Program in general, please call 1-877-FEMA MAP (1-877-336-2627) or visit the FEMA website at http://www.fema.gov/business/nfip.

El Paso County Vertical Datum Offset Table

Flooding Source

REFER TO SECTION 3.3 OF THE EL PASO COUNTY FLOOD INSURANCE STUDY FOR STREAM BY STREAM VERTICAL DATUM CONVERSION INFORMATION

Panel Location Map



This Digital Flood Insurance Rate Map (DFIRM) was produced through a Cooperating Technical Partner (CTP) agreement between the State of Colorado Water Conservation Board (CWCB) and the Federal Emergency Management Agency (FEMA).



Additional Flood Hazard information and resources are available from local communities and the Colorado Water Conservation Board.



LEGEND

SPECIAL FLOOD HAZARD AREAS (SFHAS) SUBJECT TO INUNDATION BY THE 1% ANNUAL CHANCE FLOOD

The 1% annual chance flood (100-year flood), also known as the base flood, is the flood that has a 1% chance of being equaled or exceeded in any given year. The Special Flood Hazard Area is the area subject to flooding by the 1% annual chance flood. Areas of Special Flood Hazard include Zones A, AE, AH, AO, AR, A99, V, and VE. The Base Flood Elevation is the water-surface elevation of the 1% annual chance flood.

ZONE A No Base Flood Elevations determined.

ZONE AE Base Flood Elevations determined. Flood depths of 1 to 3 feet (usually areas of ponding); Base Flood Elevations determined

ZONE AO Flood depths of 1 to 3 feet (usually sheet flow on sloping terrain); average depths determined. For areas of alluvial fan flooding, velocities also

ZONE AR Special Flood Hazard Area Formerly protected from the 1% annual chance flood by a flood control system that was subsequently decertified. Zone AR indicates that the former flood control system is being restored to provide

ZONE A99 Area to be protected from 1% annual chance flood by a Federal flood protection system under construction; no Base Flood Elevations

ZONE V Coastal flood zone with velocity hazard (wave action); no Base Flood

protection from the 1% annual chance or greater flood.

Elevations determined. **ZONE VE** Coastal flood zone with velocity hazard (wave action); Base Flood Elevations determined.

FLOODWAY AREAS IN ZONE AE

The floodway is the channel of a stream plus any adjacent floodplain areas that must be kept free of encroachment so that the 1% annual chance flood can be carried without substantial increases in flood heights.

OTHER FLOOD AREAS

Areas of 0.2% annual chance flood; areas of 1% annual chance flood with average depths of less than 1 foot or with drainage areas less than 1 square mile; and areas protected by levees from 1% annual chance flood.

OTHER AREAS

ZONE X Areas determined to be outside the 0.2% annual chance floodplain. Areas in which flood hazards are undetermined, but possible.

COASTAL BARRIER RESOURCES SYSTEM (CBRS) AREAS

OTHERWISE PROTECTED AREAS (OPAs)

CBRS areas and OPAs are normally located within or adjacent to Special Flood Hazard Areas. Floodplain boundary

Floodway boundary Zone D Boundary CBRS and OPA boundary

.......... Boundary dividing Special Flood Hazard Areas of different Base

Flood Elevations, flood depths or flood velocities. ~~ 513 ~~ Base Flood Elevation line and value; elevation in feet* Base Flood Elevation value where uniform within zone; (EL 987) elevation in feet*

* Referenced to the North American Vertical Datum of 1988 (NAVD 88)

Cross section line

6000000 FT

97° 07' 30.00" Geographic coordinates referenced to the North American 32° 22' 30.00" Datum of 1983 (NAD 83)

1000-meter Universal Transverse Mercator grid ticks, 4275000mN

system, central zone (FIPSZONE 0502), Bench mark (see explanation in Notes to Users section of

5000-foot grid ticks: Colorado State Plane coordinate

this FIRM panel)

MAP REPOSITORIES Refer to Map Repositories list on Map Index EFFECTIVE DATE OF COUNTYWIDE

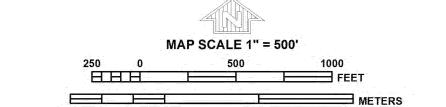
EFFECTIVE DATE(S) OF REVISION(S) TO THIS PANEL DECEMBER 7, 2018 - to update corporate limits, to change Base Flood Elevations and Special Flood Hazard Areas, to update map format, to add roads and road names, and to

FLOOD INSURANCE RATE MAP MARCH 17, 1997

incorporate previously issued Letters of Map Revision. For community map revision history prior to countywide mapping, refer to the Community

Map History Table located in the Flood Insurance Study report for this jurisdiction.

To determine if flood insurance is available in this community, contact your insurance agent or call the National Flood Insurance Program at 1-800-638-6620.



PANEL 0526G

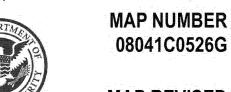
FIRM FLOOD INSURANCE RATE MAP **EL PASO COUNTY,** COLORADO AND INCORPORATED AREAS

PANEL 526 OF 1300

(SEE MAP INDEX FOR FIRM PANEL LAYOUT) **CONTAINS:**

EL PASO COUNTY

Notice to User: The Map Number shown below should be used when placing map orders: the Community Number shown above should be used on insurance applications for the subject



MAP REVISED **DECEMBER 7, 2018** Federal Emergency Management Agency

APPENDIX D - HYDROLOGIC CALCULATIONS



Weighted Imperviousness Existing Calculations: Existing

| | AREA | AREA | GRAVEL ROAD | GRAVEL ROAD | | GRAVE | L ROAD | | LANDSCAPE | LANDSCAPE | | LAND | SCAPE | | ROOF | ROOF | | RC | OF | | WEIGHTED | WEI | IGHTED C | COEFFICIE | ENTS |
|-----------|-----------|---------|-------------|-----------------------|-------|-------|--------|------|-----------|----------------|------|------|-------|------|------|-----------------------|------|------|-----|------|----------------|------|----------|-----------|------|
| SUB-BASIN | (SF) | (Acres) | AREA | IMPERVIOUSNESS | C2 | C5 | C10 | C100 | AREA | IMPERVIOUSNESS | C2 | C5 | C10 | C100 | AREA | IMPERVIOUSNESS | C2 | C5 | C10 | C100 | IMPERVIOUSNESS | C2 | C5 | C10 | C100 |
| Α | 158,991 | 3.65 | 0 | 80% | 0.00 | 0 | 0 | 0 | 158,991 | 0% | 0.02 | 0.08 | 0.15 | 0.35 | 0 | 90% | 0.00 | 0.00 | 0 | 0 | 0.0% | 0.02 | 0.08 | 0.15 | 0.35 |
| В | 265,057 | 6.08 | 0 | 80% | 0.00 | 0 | 0 | 0 | 265,057 | 0% | 0.02 | 0.08 | 0.15 | 0.35 | 0 | 90% | 0.00 | 0.00 | 0 | 0 | 0.0% | 0.02 | 0.08 | 0.15 | 0.35 |
| С | 373,006 | 8.56 | 0 | 80% | 0.00 | 0 | 0 | 0 | 373,006 | 0% | 0.02 | 0.08 | 0.15 | 0.35 | 0 | 90% | 0.00 | 0.00 | 0 | 0 | 0.0% | 0.02 | 0.08 | 0.15 | 0.35 |
| D | 326,517 | 7.50 | 0 | 80% | 0.00 | 0 | 0 | 0 | 326,517 | 0% | 0.02 | 0.08 | 0.15 | 0.35 | 0 | 90% | 0.00 | 0.00 | 0 | 0 | 0.0% | 0.02 | 0.08 | 0.15 | 0.35 |
| E | 36,355 | 0.83 | 0 | 80% | 0.00 | 0 | 0 | 0 | 36,355 | 0% | 0.02 | 0.08 | 0.15 | 0.35 | 0 | 90% | 0.00 | 0.00 | 0 | 0 | 0.0% | 0.02 | 0.08 | 0.15 | 0.35 |
| F | 25,618 | 0.59 | 0 | 80% | 0.00 | 0 | 0 | 0 | 25,618 | 0% | 0.02 | 0.08 | 0.15 | 0.35 | 0 | 90% | 0.00 | 0.00 | 0 | 0 | 0.0% | 0.02 | 0.08 | 0.15 | 0.35 |
| G | 311,534 | 7.15 | 0 | 80% | 0.00 | 0 | 0 | 0 | 311,534 | 0% | 0.02 | 0.08 | 0.15 | 0.35 | 0 | 90% | 0.00 | 0.00 | 0 | 0 | 0.0% | 0.02 | 0.08 | 0.15 | 0.35 |
| OE-A | 4,445 | 0.10 | 0 | 80% | 0.00 | 0 | 0 | 0 | 4,445 | 0% | 0.02 | 0.08 | 0.15 | 0.35 | 0 | 90% | 0.00 | 0.00 | 0 | 0 | 0.0% | 0.02 | 0.08 | 0.15 | 0.35 |
| OE-B | 37,383 | 0.86 | 0 | 80% | 0.00 | 0 | 0 | 0 | 37,383 | 0% | 0.02 | 0.08 | 0.15 | 0.35 | 0 | 90% | 0.00 | 0.00 | 0 | 0 | 0.0% | 0.02 | 0.08 | 0.15 | 0.35 |
| OE-C | 95,469 | 2.19 | 0 | 80% | 0.00 | 0 | 0 | 0 | 95,469 | 0% | 0.02 | 0.08 | 0.15 | 0.35 | 0 | 90% | 0.00 | 0.00 | 0 | 0 | 0.0% | 0.02 | 0.08 | 0.15 | 0.35 |
| OE-D | 885,654 | 20.33 | 0 | 80% | 0.00 | 0 | 0 | 0 | 885,654 | 0% | 0.02 | 0.08 | 0.15 | 0.35 | 0 | 90% | 0.00 | 0.00 | 0 | 0 | 0.0% | 0.02 | 0.08 | 0.15 | 0.35 |
| OE-E | 458,281 | 10.52 | 0 | 80% | 0.00 | 0 | 0 | 0 | 458,281 | 0% | 0.02 | 0.08 | 0.15 | 0.35 | 0 | 90% | 0.00 | 0.00 | 0 | 0 | 0.0% | 0.02 | 0.08 | 0.15 | 0.35 |
| OE-H | 233,578 | 5.36 | 0 | 80% | 0.00 | 0 | 0 | 0 | 233,578 | 0% | 0.02 | 0.08 | 0.15 | 0.35 | 0 | 90% | 0.00 | 0.00 | 0 | 0 | 0.0% | 0.02 | 0.08 | 0.15 | 0.35 |
| TOTAL | 3,211,887 | 73.73 | 0 | 80% | 10.00 | 0 | 0 | 0 | 2,520,028 | 0% | 0.02 | 0.08 | 0.15 | 0.35 | 0 | 90% | 0.00 | 0.00 | 0 | 0 | 0.0% | 0.02 | 0.06 | 0.12 | 0.27 |

| Renehan St | ubdivision | | | | | | | | | Watercours | se Coeffic | ent | | | | |
|-----------------|----------------|--------------|-------------|------|------------|-------------|-------------|---------------|------------|-------------|--------------|--------------|---------------|-----------------|----------|-------|
| Time of Cor | ncentration | Existing C | Calculatio | ons | Forest | & Meadow | 2.50 | Short Gr | ass Pastu | ire & Lawns | 7.00 | | | Grassed | Waterway | 15.0 |
| | | | | I | Fallow or | Cultivation | 5.00 | | Nearly B | are Ground | 10.00 | | Paved A | Area & Sha | | |
| | | SUB-BASIN | | | INITIA | AL / OVERL | AND* | TF | RAVEL TIN | ME | | | | T(c) CHEC | CK | FINAL |
| | | DATA | | | | TIME | | | T(t) | | | | | ANIZED BA | | T©* |
| DESIGN POINT | DRAIN BASIN | AREA sq. ft. | AREA ac. | C(5) | Length ft. | Slope % | T(i) min | Length ft. | Slope % | Coeff. | Velocity fps | T(t) min. | COMP. T(c) | TOTAL LENGTH | L/180+10 | min. |
| E1 | А | 158,991 | 3.65 | 0.08 | 118 | 14.0% | 8.4 | 742 | 13.0% | 2.50 | 0.9 | 13.7 | 22.1 | 859.889 | 14.8 | 14.8 |
| E2 | В | 265,057 | 6.08 | 0.08 | 119 | 6.0% | 11.2 | 991 | 14.0% | 2.50 | 0.9 | 17.7 | 28.9 | 1109.89 | 16.2 | 16.2 |
| E3 | С | 373,006 | 8.56 | 0.08 | 300 | 13.0% | 13.8 | 2237 | 20.0% | 2.50 | 1.1 | 33.3 | 47.1 | 2537 | 24.1 | 24.1 |
| E4 | D | 326,517 | 7.50 | 0.08 | 206 | 17.0% | 10.4 | 1832 | 19.0% | 2.50 | 1.1 | 28.0 | 38.5 | 2038 | 21.3 | 21.3 |
| E5 | E | 36,355 | 0.83 | 0.08 | 287 | 13.0% | 13.5 | 133 | 25.0% | 2.50 | 1.3 | 1.8 | 15.2 | 420 | 12.3 | 12.3 |
| E6 | F | 25,618 | 0.59 | 0.08 | 157 | 13.0% | 10.0 | 46 | 20.0% | 2.50 | 1.1 | 0.7 | 10.7 | 203 | 11.1 | 10.7 |
| E7 | G | 311,534 | 7.15 | 0.08 | 194 | 8.0% | 13.0 | 708 | 12.0% | 2.50 | 0.9 | 13.6 | 26.6 | 902 | 15.0 | 15.0 |
| E8 | OE-A | 4,445 | 0.10 | 0.08 | 38 | 5.0% | 6.7 | 31 | 5.0% | 2.50 | 0.6 | 0.9 | 7.7 | 69 | 10.4 | 7.7 |
| E9 | OE-B | 37,383 | 0.86 | 0.08 | 111 | 7.0% | 10.3 | 208 | 7.0% | 2.50 | 0.7 | 5.2 | 15.5 | 319 | 11.8 | 11.8 |
| E10 | OE-C | 95,469 | 2.19 | 0.08 | 69 | 5.0% | 9.1 | 412 | 12.0% | 2.50 | 0.9 | 7.9 | 17.0 | 481 | 12.7 | 12.7 |
| E11 | OE-D | 885,654 | 20.33 | 0.08 | 107 | 5.0% | 11.3 | 895 | 14.0% | 2.50 | 0.9 | 15.9 | 27.3 | 1002 | 15.6 | 15.6 |
| E12 | OE-E | 458,281 | 10.52 | 0.08 | 169 | 18.0% | 9.3 | 1366 | 13.0% | 2.50 | 0.9 | 25.3 | 34.5 | 1535 | 18.5 | 18.5 |
| E13 | OE-H | 233,578 | 5.36 | 0.08 | 105 | 9.0% | 9.2 | 753 | 7.0% | 2.50 | 0.7 | 19.0 | 28.2 | 858 | 14.8 | 14.8 |
| TOTAL | TOTAL | 3,211,887 | 73.73 | | | | | | | | | | | | | |

^{*}Note: El Paso County Drainage Manual Chapter 6 indicates that the maximum overland flow length is 100ft for urbanized areas and 300ft for rural areas. The minimum time of concentration is 5 min for developed conditions, 10 min for undeveloped conditions.

| | enehan Subdivision ime of Concentration Existing Calculations Design Storm 100 Year Storm Event | | | | | | | | | | | |
|-----------------|---|-------------|-----------------|-------------|--------|---------------|----------|-------------|------|------------|----------|-------|
| - | thod Procedure) | g | | | 2 00. | 9 2.00 | | | | • | | |
| B | ASIN INFORMATIO | N | | | DIRECT | RUNOFF | | CUN | ИMUL | ATIVE R | UNOFF | |
| DESIGN POINT | DRAIN BASIN | AREA ac. | RUNOFF COEFF | T(c) min | CxA | l in/hr | Q cfs | T(c) min | CxA | l in/hr | Q cfs | NOTES |
| E1 | А | 3.65 | 0.35 | 14.8 | 1.28 | 5.94 | 7.59 | | | | | |
| E2 | В | 6.08 | 0.35 | 16.2 | 2.13 | 5.72 | 12.18 | | | | | |
| E3 | С | 8.56 | 0.35 | 24.1 | 3.00 | 4.72 | 14.13 | | | | | |
| E4 | D | 7.50 | 0.35 | 21.3 | 2.62 | 5.03 | 13.19 | | | | | |
| E5 | E | 0.83 | 0.35 | 12.3 | 0.29 | 6.41 | 1.87 | | | | | |
| E6 | F | 0.59 | 0.35 | 10.7 | 0.21 | 6.77 | 1.39 | | | | | |
| E7 | G | 7.15 | 0.35 | 15.0 | 2.50 | 5.91 | 14.80 | | | | | |
| E8 | OE-A | 0.10 | 0.35 | 7.7 | 0.04 | 7.60 | 0.27 | | | | | |
| E9 | OE-B | 0.86 | 0.35 | 11.8 | 0.30 | 6.52 | 1.96 | | | | | |
| E10 | OE-C | 2.19 | 0.35 | 12.7 | 0.77 | 6.33 | 4.86 | | | | | |
| E11 | OE-D | 20.33 | 0.35 | 15.6 | 7.12 | 5.81 | 41.36 | | | | | |
| E12 | OE-E | 10.52 | 0.35 | 18.5 | 3.68 | 5.38 | 19.82 | | | | | |
| E13 | OE-H | 5.36 | 0.35 | 14.8 | 1.88 | 5.94 | 11.16 | | | | | |
| TOTAL | TOTAL | 73.73 | 0.35 | | | | 19.77 | | | | | |

Renehan Subdivision

Time of Concentration Existing Calculations Design Storm 5 Year Strom Event

(Rational Method Procedure)

| BASIN | INFORM | ATION | | DIR | ECT RUN | OFF | | | CUMMULAT | IVE RUNOFF | | |
|-----------------|----------------|-------------|-----------------|-------------|---------|------------|----------|-------------|----------|------------|----------|-------|
| DESIGN POINT | DRAIN BASIN | AREA ac. | RUNOFF COEFF | T(c) min | CxA | l in/hr | Q cfs | T(c) min | CxA | l in/hr | Q cfs | NOTES |
| E1 | Α | 3.65 | 0.08 | 14.8 | 0.29 | 3.54 | 1.03 | | | | | 0.00 |
| E2 | В | 6.08 | 0.08 | 16.2 | 0.49 | 3.41 | 1.66 | | | | | 0.00 |
| E3 | С | 8.56 | 0.08 | 24.1 | 0.69 | 2.81 | 1.92 | | | | | |
| E4 | D | 7.50 | 0.08 | 21.3 | 0.60 | 2.99 | 1.80 | | | | | |
| E5 | E | 0.83 | 0.08 | 12.3 | 0.07 | 3.82 | 0.25 | | | | | |
| E6 | F | 0.59 | 0.08 | 10.7 | 0.05 | 4.03 | 0.19 | | | | | |
| E7 | G | 7.15 | 0.08 | 15.0 | 0.57 | 3.52 | 2.01 | | | | | |
| E8 | OE-A | 0.10 | 0.08 | 7.7 | 0.01 | 4.53 | 0.04 | | | | | |
| E9 | OE-B | 0.86 | 0.08 | 11.8 | 0.07 | 3.88 | 0.27 | | | | | |
| E10 | OE-C | 2.19 | 0.08 | 12.7 | 0.18 | 3.77 | 0.66 | | | | | |
| E11 | OE-D | 20.33 | 0.08 | 15.6 | 1.63 | 3.46 | 5.63 | | | | | |
| E12 | OE-E | 10.52 | 0.08 | 18.5 | 0.84 | 3.21 | 2.70 | | | | | |
| E13 | OE-H | 5.36 | 0.08 | 14.8 | 0.43 | 3.54 | 1.52 | | | | | |
| TOTAL | TOTAL | 73.73 | 0.08 | | | | 2.69 | | | | | |

Weighted Imperviousness Calculations: Proposed

| | AREA | AREA | PAVEMENT | PAVEMENT | | PAVE | MENT | · | LANDSCAPE | LANDSCAPE | | LAND | SCAPE | | ROOF | ROOF | • | RC | OF | | WEIGHTED | WEI | IGHTED C | OEFFICI' | ENTS |
|-----------|-----------|---------|----------|----------------|------|------|------|------|-----------|----------------|------|------|-------|------|--------|----------------|------|------|-----|------|----------------|------|----------|----------|------|
| SUB-BASIN | (SF) | (Acres) | AREA | IMPERVIOUSNESS | C2 | C5 | C10 | C100 | AREA | IMPERVIOUSNESS | C2 | C5 | C10 | C100 | AREA | IMPERVIOUSNESS | C2 | C5 | C10 | C100 | IMPERVIOUSNESS | C2 | C5 | C10 | C100 |
| P-A | 796,440 | 18.28 | 56,872 | 100% | 0.89 | 0.9 | 0.92 | 0.96 | 739,568 | 0% | 0.02 | 0.08 | 0.15 | 0.35 | 25,166 | 90% | 0.00 | 0.00 | 0 | 0 | 10.0% | 0.08 | 0.14 | 0.20 | 0.39 |
| P-B | 326,515 | 7.50 | 0 | 100% | 0.89 | 0.9 | 0.92 | 0.96 | 326,515 | 0% | 0.02 | 0.08 | 0.15 | 0.35 | 6,676 | 90% | 0.00 | 0.00 | 0 | 0 | 1.8% | 0.02 | 0.08 | 0.15 | 0.35 |
| P-C | 312,137 | 7.17 | 9,973 | 100% | 0.89 | 0.9 | 0.92 | 0.96 | 302,164 | 0% | 0.02 | 0.08 | 0.15 | 0.35 | 10,614 | 90% | 0.00 | 0.00 | 0 | 0 | 6.3% | 0.05 | 0.11 | 0.17 | 0.37 |
| P-D | 36,355 | 0.83 | 0 | 100% | 0.89 | 0.9 | 0.92 | 0.96 | 36,355 | 0% | 0.02 | 0.08 | 0.15 | 0.35 | 0 | 90% | 0.00 | 0.00 | 0 | 0 | 0.0% | 0.02 | 0.08 | 0.15 | 0.35 |
| P-E | 25,618 | 0.59 | 0 | 100% | 0.89 | 0.9 | 0.92 | 0.96 | 25,618 | 0% | 0.02 | 0.08 | 0.15 | 0.35 | 0 | 90% | 0.00 | 0.00 | 0 | 0 | 0.0% | 0.02 | 0.08 | 0.15 | 0.35 |
| OP-A | 137,304 | 3.15 | 0 | 100% | 0.89 | 0.9 | 0.92 | 0.96 | 137,304 | 0% | 0.02 | 0.08 | 0.15 | 0.35 | 0 | 90% | 0.00 | 0.00 | 0 | 0 | 0.0% | 0.02 | 0.08 | 0.15 | 0.35 |
| OP-B | 885,656 | 20.33 | 0 | 100% | 0.89 | 0.9 | 0.92 | 0.96 | 885,656 | 0% | 0.02 | 0.08 | 0.15 | 0.35 | 0 | 90% | 0.00 | 0.00 | 0 | 0 | 0.0% | 0.02 | 0.08 | 0.15 | 0.35 |
| OP-C | 458,281 | 10.52 | 0 | 100% | 0.89 | 0.9 | 0.92 | 0.96 | 458,281 | 0% | 0.02 | 0.08 | 0.15 | 0.35 | 0 | 90% | 0.00 | 0.00 | 0 | 0 | 0.0% | 0.02 | 0.08 | 0.15 | 0.35 |
| OP-H | 233,578 | 5.36 | 0 | 100% | 0.89 | 0.9 | 0.92 | 0.96 | 233,578 | 0% | 0.02 | 0.08 | 0.15 | 0.35 | 0 | 90% | 0.00 | 0.00 | 0 | 0 | 0.0% | 0.02 | 0.08 | 0.15 | 0.35 |
| TOTAL | 3,211,884 | 73.73 | 66,845 | 100% | 0.89 | 0.9 | 0.92 | 0.96 | 2,911,461 | 0% | 0.02 | 0.08 | 0.15 | 0.35 | 42,456 | 90% | 0.00 | 0.00 | 0 | 0 | 3.3% | 0.04 | 0.09 | 0.16 | 0.34 |

1/30/2023 Calculated by: RES Checked by: KRK

| Renehan Su | ıbdivision | | | | | | | | | Watercours | e Coeffici | ent | | | | |
|-------------|-------------|-----------------|----------|-------|--------|-------------|-------|---------|------------|-------------|------------|------|---------|------------|----------|-------|
| Time of Cor | ncentration | Proposed | Calculat | tions | Forest | & Meadow | 2.50 | Short G | rass Pastu | ıre & Lawns | 7.00 | | | Grassed | Waterway | 15.00 |
| | | | | | | Cultivation | 5.00 | | | are Ground | 10.00 | | Paved A | Area & Sha | | |
| | | SUB-BASIN | | | INITIA | AL / OVERL | .AND* | TI | RAVEL TIM | ME | | | | T(c) CHEC | | FINAL |
| | | DATA | | | | TIME | | | T(t) | | | | | ANIZED BA | | T©* |
| DESIGN | DRAIN | AREA | AREA | C(5) | Length | Slope | T(i) | Length | Slope | Coeff. | Velocity | T(t) | COMP. | | L/180+10 | |
| POINT | BASIN | sq. ft. | ac. | | ft. | % | min | ft. | % | | fps | min. | T(c) | LENGTH | | min. |
| P1 | P-A | 796,440 | 18.28 | 0.14 | 298 | 7.0% | 15.9 | 1712 | 25.0% | 2.50 | 1.3 | 22.8 | 38.7 | 2010 | 21.2 | 21.2 |
| P2 | P-B | 326,515 | 7.50 | 0.08 | 300 | 18.0% | 12.4 | 738 | 20.0% | 2.50 | 1.1 | 11.0 | 23.4 | 1038 | 15.8 | 15.8 |
| P3 | P-C | 312,137 | 7.17 | 0.11 | 106 | 7.0% | 9.8 | 1068 | 12.0% | 2.50 | 0.9 | 20.6 | 30.4 | 1174.4 | 16.5 | 16.5 |
| P4 | P-D | 36,355 | 0.83 | 0.08 | 287 | 13.0% | 13.5 | 133 | 25.0% | 2.50 | 1.3 | 1.8 | 15.2 | 420 | 12.3 | 12.3 |
| P5 | P-E | 25,618 | 0.59 | 0.08 | 157 | 13.0% | 10.0 | 46 | 20.0% | 2.50 | 1.1 | 0.7 | 10.7 | 203 | 11.1 | 10.7 |
| P6 | OP-A | 137,304 | 3.15 | 0.08 | 93 | 5.0% | 10.5 | 393 | 11.0% | 2.50 | 0.8 | 7.9 | 18.4 | 486 | 12.7 | 12.7 |
| P7 | OP-B | 885,656 | 20.33 | 0.08 | 230 | 7.0% | 14.8 | 919 | 15.0% | 2.50 | 1.0 | 15.8 | 30.6 | 1149 | 16.4 | 16.4 |
| P8 | OP-C | 458,281 | 10.52 | 0.08 | 143 | 19.0% | 8.4 | 1468 | 14.0% | 2.50 | 0.9 | 26.2 | 34.5 | 1611 | 19.0 | 19.0 |
| P9 | OP-H | 233,578 | 5.36 | 0.08 | 105 | 9.0% | 9.2 | 753 | 7.0% | 2.50 | 0.7 | 19.0 | 28.2 | 858 | 14.8 | 14.8 |
| ТОТ | ΓAL | 3,211,884 | 73.73 | | | | | | | | | | | | | |

Renehan Subdivision

Time of Concentration Proposed Calculations

Design Storm 100 Year Storm Event

(Rational Method Procedure)

| В | ASIN INFORMATIO | ON | | | DIRECT | RUNOFF | | CUN | ИMUL | ATIVE R | UNOFF | |
|-----------------|-----------------|-------------|-----------------|-------------|--------|------------|----------|-------------|------|------------|----------|-------|
| DESIGN POINT | DRAIN BASIN | AREA ac. | RUNOFF COEFF | T(c) min | СхА | l in/hr | Q cfs | T(c) min | CxA | l in/hr | Q cfs | NOTES |
| P1 | P-A | 18.28 | 0.39 | 21.2 | 7.20 | 5.04 | 36.26 | | | , | | |
| P2 | P-B | 7.50 | 0.35 | 15.8 | 2.62 | 5.78 | 15.16 | | | | | |
| P3 | P-C | 7.17 | 0.37 | 16.5 | 2.65 | 5.67 | 15.01 | | | | | |
| P4 | P-D | 0.83 | 0.35 | 12.3 | 0.29 | 6.41 | 1.87 | | | | | |
| P5 | P-E | 0.59 | 0.35 | 10.7 | 0.21 | 6.77 | 1.39 | | | | | |
| P6 | OP-A | 3.15 | 0.35 | 12.7 | 1.10 | 6.33 | 6.98 | | | | | |
| P7 | OP-B | 20.33 | 0.35 | 16.4 | 7.12 | 5.69 | 40.46 | | | | | |
| P8 | OP-C | 10.52 | 0.35 | 19.0 | 3.68 | 5.32 | 19.57 | | | | | |
| P9 | OP-H | 5.36 | 0.35 | 14.8 | 1.88 | 5.94 | 11.16 | | | | | |
| Т | TOTAL 73.73 | | | | | 147.88 | | | | | | |

Renehan Subdivision

Time of Concentration Proposed Calculations Design Storm 5 Year Strom Event

(Rational Method Procedure)

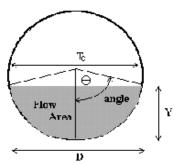
| BASIN | INFORM | ATION | | DIR | ECT RUN | OFF | | | CUMMULAT | IVE RUNOFF | | |
|-----------------|----------------|-------------|-----------------|-------------|---------|------------|----------|-------------|----------|------------|----------|-------|
| DESIGN POINT | DRAIN BASIN | AREA ac. | RUNOFF COEFF | T(c) min | CxA | l in/hr | Q cfs | T(c) min | CxA | l in/hr | Q cfs | NOTES |
| P1 | P-A | 18.28 | 0.14 | 21.2 | 2.53 | 3.00 | 7.60 | | | | | |
| P2 | P-B | 7.50 | 0.08 | 15.8 | 0.60 | 3.44 | 2.06 | | | | | |
| Р3 | P-C | 7.17 | 0.11 | 16.5 | 0.76 | 3.38 | 2.57 | | | | | |
| P4 | P-D | 0.83 | 0.08 | 12.3 | 0.07 | 3.82 | 0.25 | | | | | |
| P5 | P-E | 0.59 | 0.08 | 10.7 | 0.05 | 4.03 | 0.19 | | | | | |
| P6 | OP-A | 3.15 | 0.08 | 12.7 | 0.25 | 3.77 | 0.95 | | | | | |
| P7 | OP-B | 20.33 | 0.08 | 16.4 | 1.63 | 3.39 | 5.51 | | | | | |
| P8 | OP-C | 10.52 | 0.08 | 19.0 | 0.84 | 3.17 | 2.66 | | | | | |
| P9 | OP-H | 5.36 | 0.08 | 14.8 | 0.43 | 3.54 | 1.52 | | | | | |
| TO | TAL | 73.73 | | | | | 23.33 | | | | | |

APPENDIX E – HYDRAULIC CALCULATIONS



CIRCULAR CONDUIT FLOW (Normal & Critical Depth Computation) MHFD-Culvert, Version 4.00 (May 2020)

Project: Renehan Subdivision
Pipe ID: C-01



| <u>Design Information (Input)</u> | | | |
|--|-------------------|--------|--------------|
| Pipe Invert Slope | So = | 0.0200 | ft/ft |
| Pipe Manning's n-value | n = | 0.0230 | * |
| Pipe Diameter | D = | 18.00 | inches |
| Design discharge | Q = | 7.60 | cfs |
| | | | |
| Full-Flow Capacity (Calculated) | | | |
| Full-flow area | Af = | 1.77 | sq ft |
| Full-flow wetted perimeter | Pf = | 4.71 | ft |
| Half Central Angle | Theta = | 3.14 | radians |
| Full-flow capacity | Qf = | 8.42 | cfs |
| | | | |
| Calculation of Normal Flow Condition | | | |
| Half Central Angle (0 <theta<3.14)< td=""><td>Theta =</td><td>2.08</td><td>radians</td></theta<3.14)<> | Theta = | 2.08 | radians |
| Flow area | An = | 1.41 | sq ft |
| Top width | Tn = | 1.31 | ft |
| Wetted perimeter | Pn = | 3.12 | ft |
| Flow depth | Yn = | 1.12 | ft |
| Flow velocity | Vn = | 5.39 | fps |
| Discharge | Qn = | 7.60 | cfs |
| Percent of Full Flow | Flow = | 90.3% | of full flow |
| Normal Depth Froude Number | Fr _n = | 0.92 | subcritical |
| | | | |
| Calculation of Critical Flow Condition | | | |
| Half Central Angle (0 <theta-c<3.14)< td=""><td>Theta-c =</td><td>2.01</td><td>radians</td></theta-c<3.14)<> | Theta-c = | 2.01 | radians |
| Critical flow area | Ac = | 1.35 | sq ft |
| Critical top width | Tc = | 1.36 | ft |
| Critical flow depth | Yc = | 1.07 | ft |
| Critical flow velocity | Vc = | 5.65 | fps |
| Critical Depth Froude Number | Fr _c = | 1.00 | |
| | | | |

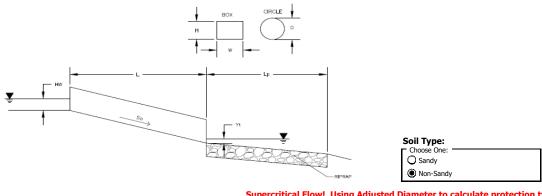
^{*} Unexpected value for Manning's n

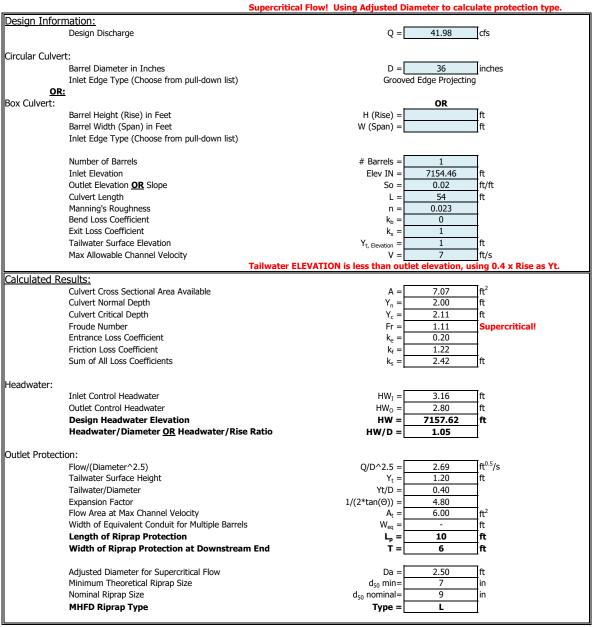
DETERMINATION OF CULVERT HEADWATER AND OUTLET PROTECTION

MHFD-Culvert, Version 4.00 (May 2020)

Project: Renehan Subdivision

ID: R-01



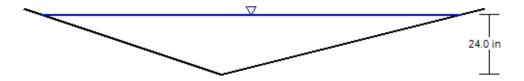


Driveway/Roadside Ditch Capacity Calculation

| Project Description | | |
|-----------------------|----------------------|--|
| | Manaira | |
| Friction Method | Manning Formula | |
| Solve For | Discharge | |
| | | |
| Input Data | | |
| Roughness Coefficient | 0.035 | |
| Channel Slope | 0.050 ft/ft | |
| Normal Depth | 24.0 in | |
| Left Side Slope | 3.000 H:V | |
| Right Side Slope | 4.000 H:V | |
| Results | | |
| Discharge | 129.41 cfs | |
| Flow Area | 14.0 ft ² | |
| Wetted Perimeter | 14.6 ft | |
| Hydraulic Radius | 11.5 in | |
| Top Width | 14.00 ft | |
| Critical Depth | 29.2 in | |
| Critical Slope | 0.018 ft/ft | |
| Velocity | 9.24 ft/s | |
| Velocity Head | 1.33 ft | |
| Specific Energy | 3.33 ft | |
| Froude Number | 1.630 | |
| Flow Type | Supercritical | |
| GVF Input Data | | |
| Downstream Depth | 0.0 in | |
| Length | 0.0 ft | |
| Number Of Steps | 0 | |
| GVF Output Data | | |
| Upstream Depth | 0.0 in | |
| Profile Description | N/A | |
| Profile Headloss | 0.00 ft | |
| Downstream Velocity | Infinity ft/s | |
| Upstream Velocity | Infinity ft/s | |
| Normal Depth | 24.0 in | |
| Critical Depth | 29.2 in | |
| Channel Slope | 0.050 ft/ft | |
| Critical Slope | 0.018 ft/ft | |

Driveway/Roadside Ditch Capacity Calculation

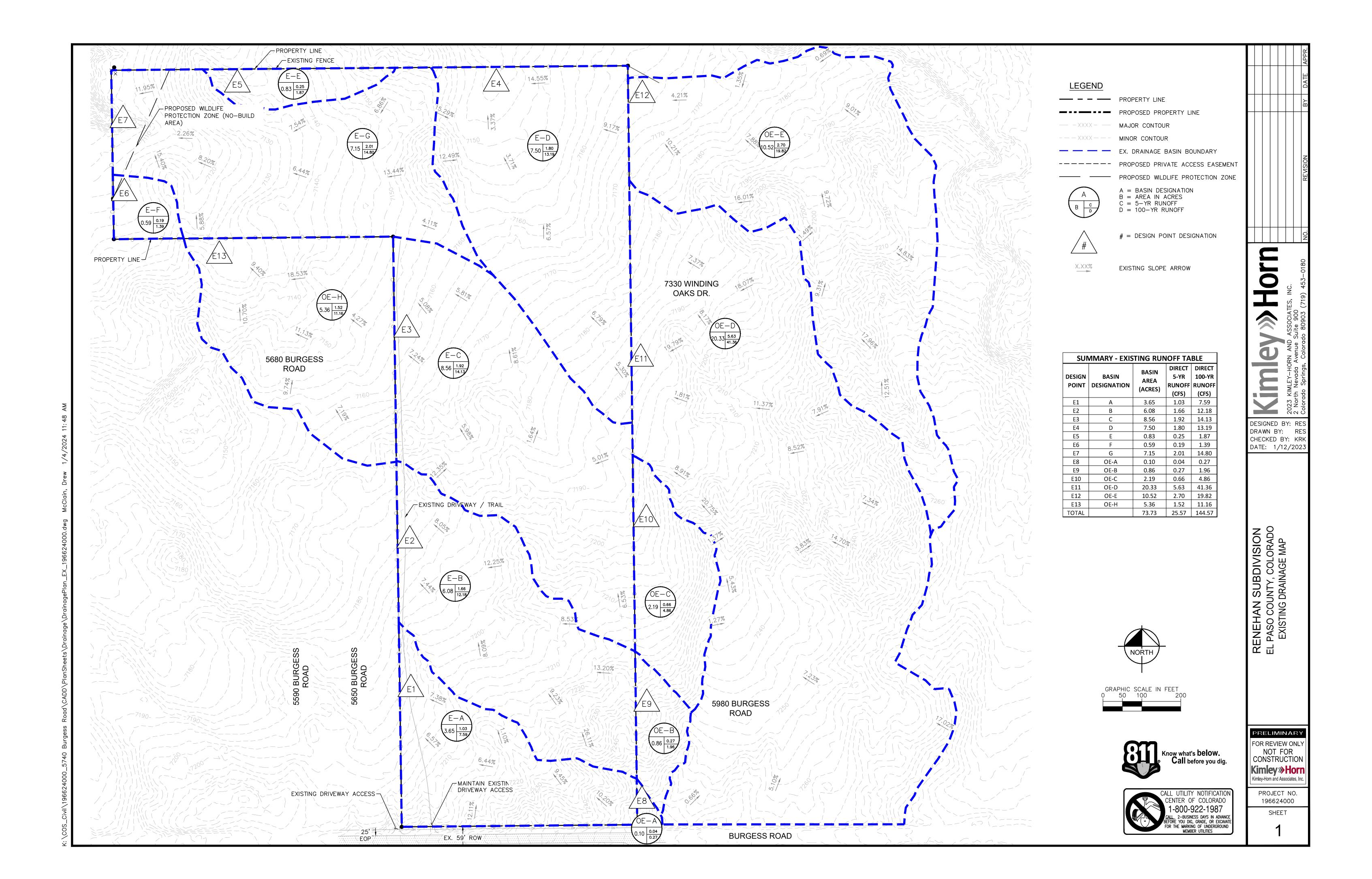
| Project Description | | |
|-----------------------|--------------------|--|
| Friction Method | Manning Formula | |
| Solve For | Discharge | |
| Input Data | | |
| Roughness Coefficient | 0.035 | |
| Channel Slope | 0.050 ft/ft | |
| Normal Depth | 24.0 in | |
| Left Side Slope | 3.000 H:V | |
| Right Side Slope | 4.000 H:V | |
| Discharge | 129.41 cfs | |

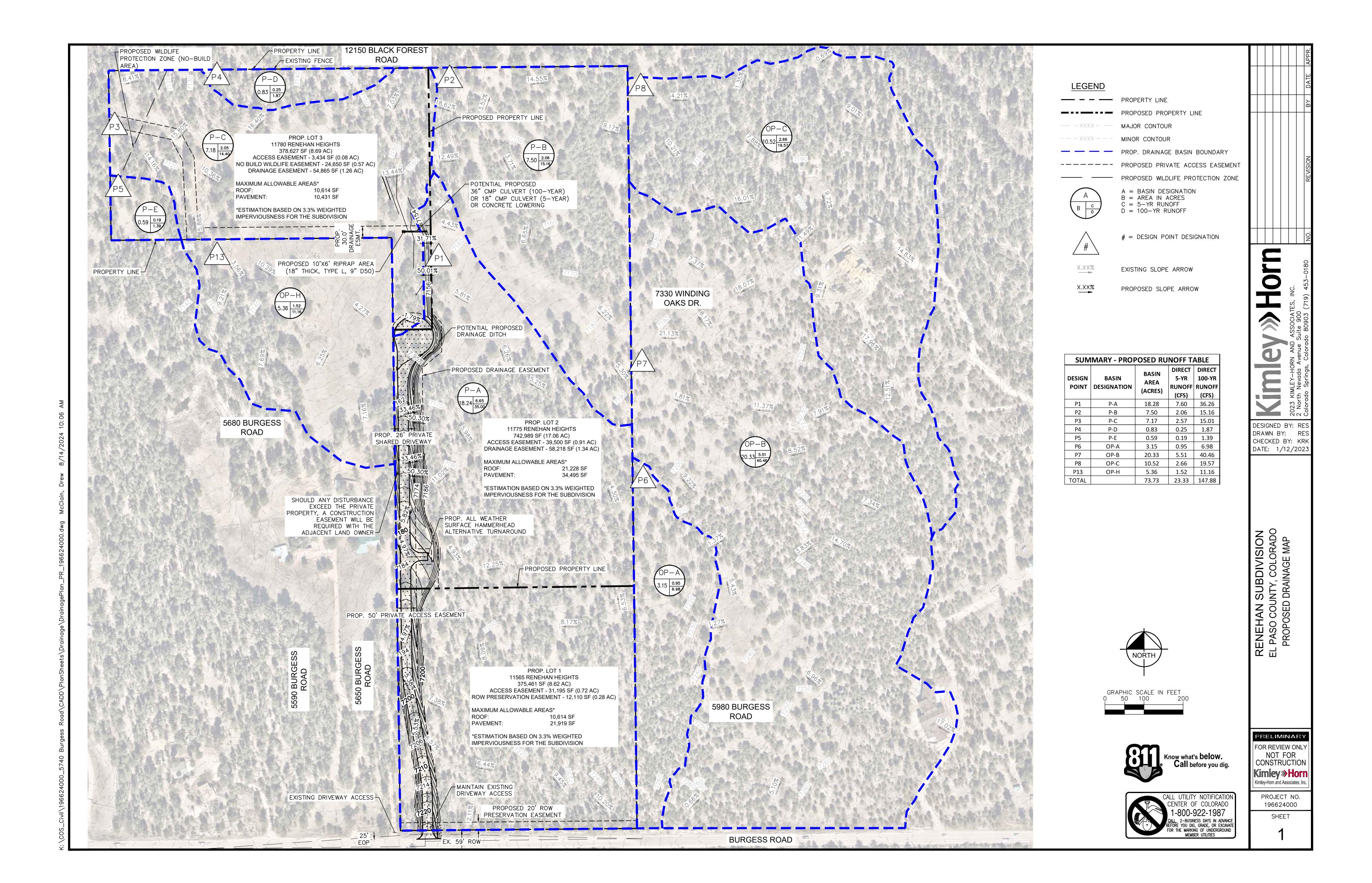


V: 1 \(\sum_{H: 1} \)

APPENDIX F - DRAINAGE EXHIBITS







APPENDIX G - SITE PHOTOS





Standing within the vicinity of design point P1, looking northwest towards design points P5 and P3.



Standing within the vicinity of proposed culvert, looking west along the proposed drainage easement adjacent to the southern property line (of the northwest area of the site) towards design points P5.



Moving west from the proposed culvert, walking through the proposed drainage easement towards the western property line.



Standing in the center of the northwest area of the site, looking northwest towards design point P3 along proposed drainage easement.



Standing in the center of the northwest area of the site, looking north towards northern property line and design point P4.



Standing in the center of the northwest area of the site, looking northwest towards western property line and design point P3 along the existing natural channel.



Standing at the central northern area of the site within proposed basin P-D, looking south.



Standing at the central northern area of the site within proposed basin P-D, looking east.



Standing at the central northern area of the site within proposed basin P-D, looking west.



Moving east from proposed basin P-D along the northern property line, looking west.



Moving east from proposed basin P-D and looking northeast, approaching design point P2.



Standing at same position from photo 11, looking southeast to show existing natural channel leading up to design point P2.



Standing at design point P2 along northern property boundary looking northeast.



Moving east from design point P2 standing at northern property boundary looking west towards design point P2.



Moving east from design point P2, standing at northern property line, looking east towards northeast corner of site.



Standing at the northeast corner of the property, looking west along northern property line towards design point P2.

























































































APPENDIX H - KETTLE CREEK DBPS



Drainage Basin Planning Study For Kettle Creek Basin

Prepared for:

High Valley Land Company, Inc. 1755 Telestar Drive, Suite 211 Colorado Springs, CO 80920 Contact: Tom Taylor

Prepared by:

JR Engineering LLC 3730 Sinton Road, Suite Colorado Springs, CO 80903 (719) 593-2593 Contact: Steve Rossoll

JR Project Number: 25100.00 May 5, 2015

Drainage Basin Planning Study For Kettle Creek

ENGINEER'S STATEMENT:

The attached Drainage Basin Planning Study was prepared under my direction and supervision and is correct to the best of my knowledge and belief. Said Drainage Basin Planning Study has been prepared according to the criteria established by the City for Drainage Basin Planning Studies and said report is in conformity with the master plan of the drainage basin area. I accept responsibility for any liability caused by any negligent acts, errors, or omissions on my part in preparing this report.

Steve Rossoll, Colorado P.E. # 34655 For and On Behalf of JR Engineering, LLC

DEVELOPER'S STATEMENT:

I, the developer, have read and will comply with all of the requirements specified in this Drainage Basin Planning Study.

34655

Business Name:

High Valley Land Company, Inc.

By:

Title:

Address:

Vice President
1755 Telestar Drive, Suite 211

Colorado Springs, CO 80920

Phone Number:

(719) 260-7477

CITY OF COLORADO SPRINGS ONLY:

Filed in accordance with Section 7.7.906 of the Code of the City of Colorado Springs, 2001, as amended.

For the City Engineer

Conditions:

DISCLAIMER:

This report has been prepared based on certain key assumptions made by JR Engineering, which substantially affect the conclusions and recommendations of this report. These assumptions, although thought to be reasonable and appropriate, may not prove true in the future. The conclusions and recommendations made by JR Engineering are conditioned upon these assumptions.

Background information, design bases, and other data have been furnished to JR Engineering by third parties, which JR Engineering has used in preparing this report. JR Engineering has relied on this information as furnished, and is not responsible for and has not confirmed the accuracy of this information. Information that became available after data procurement was complete was not incorporated.

THIS REPORT IS A PLANNING DOCUMENT AND IS NOT TO BE USED AS THE BASIS FOR FINAL DESIGN, CONSTRUCTION OR REMEDIAL ACTION, NOR AS A BASIS FOR MAJOR CAPITAL DECISIONS.

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1 INTRODUCTION

1.1 Contract Authorization

This Drainage Basin Planning Study was authorized under the terms of an agreement between the City of Colorado Springs Engineering Development Review and Stormwater Departments and High Valley Land Company, Inc. and paid for with private funds. This study covers drainage development only within the Kettle Creek Drainage Basin.

1.2 Purpose and Scope

The purpose of the drainage basin planning study is to give an initial comprehensive study of the entire Kettle Creek Basin. This Study shall show the conduits, channels, natural drainage courses, detention reservoirs, easements, culverts and all other hydraulic facilities required to control surface water from the 100-year event within the Kettle Creek Basin and to carry such waters to points of insignificant impact and to develop a plan to address future stormwater and infrastructure needs within the Kettle Creek Watershed. The process used to develop a DBPS provides opportunity for interested parties to offer input on drainage issues, needs, and facilities within the watershed. The DBPS is intended to provide an inventory of required drainage facilities and determine a drainage fee per developed acre.

1.3 Past Studies

A complete Drainage Basin Planning Study (DBPS) has not been performed for the entire Kettle Creek Watershed. However, Master Development Drainage Plans (MDDP) and Final Drainage Reports (FDR) have been prepared for areas within the study area that have been developed in the last 13 years. A number of previous studies and reports were reviewed during the preparation of the current study. The most relevant studies are listed below along with a brief synopsis of the relevance of the current study. Additional reports that were reviewed are noted in the reference section of this study.

Fountain Creek Watershed Study, January 2009, U.S. Army Corps of Engineers.

The Fountain Creek Watershed Study ties together four separate studies, a hydrology report, a hydraulics report, and environmental conditions report, and a geomorphology report, into a watershed study establishing the objectives for reduced flood risk, erosion, and sedimentation in the Fountain Creek Basin. The Watershed Study presents percent change data for existing versus future peak discharges and volumes in Monument Creek and adjacent tributaries, although no Kettle Creek flow data is presented in the Watershed Study. The hydrologic study and hydraulic study were not available from the City of Colorado Springs or from the U.S. Army Corps of Engineers to compare hydrology for common basins at the time of the preparation of this DBPS.

Master Development Drainage Plan For North Fork at Briargate, May, 2014, by JR Engineering.

A proposed mixed use development comprised of a single family residential, multifamily, an elementary school, and park site. The Site covers 267 acres located north-east of Powers Boulevard and Old Ranch Road.

Kettle Creek Drainage Basin Old Ranch Road Tributary Drainage Basin Planning Study and Master Development Drainage Plan, April 2001, by JR Engineering. (Kettle Creek MDDP/DBPS)

This MDDP/DBPS covers the portion of the Kettle Creek Basin along old Ranch Road. This study provides hydrologic data for the existing and future development along Old Ranch Road, Creekside Estates, and drainage facilities at Pine Creek High School.

U.S. Air Force Academy Kettle Creek Watershed Hydrology Study Findings and Recommendations Report, March 2002, by URS Group, Inc. (AFA Study)

This report was prepared for the U.S. Air Force Academy to study the hydrologic, hydraulic, and sediment transport for the entire Kettle Creek basin. The report recommends alternatives to reduce sediment accumulation, evaluate Preble's meadow jumping mouse habitat, and enhance existing wetlands on Academy property.

Flood Insurance Study for El Paso County and Incorporated Areas

FEMA performed a Flood Insurance Study (FIS) in 1999 with detailed analysis and base flood elevations from State Highway 83 to Templeton Gap Road at the headwaters of Kettle Creek in the Black Forest. The FEMA FIRM maps and FIS data are included in **Appendix B**.

1.4 Stakeholder Process

Stakeholders who may be affected by this study results must be identified and included in numerous public meetings and presentations to committees, council and commissions. This DBPS is prepared for the High Valley Land Company, Inc. and is the only stakeholder that is affected in the Kettle Creek Basin study. Thus there are no stakeholder meetings and presentations required.

1.5 Agency Jurisdictions

Future development in the Kettle Creek basin will predominately be located within the City of Colorado Springs city limits. Improvements outside the city limits will be located and governed by El Paso County.

1.6 General Basin Description

The Kettle Creek watershed is located in the north central portion of El Paso County, Colorado. Kettle Creek and its tributaries originate on the southern slope of the Black Forest and flow in a southwesterly direction towards the City of Colorado Springs. The Kettle Creek watershed has a contributing area of approximately 16.41 square miles at its junction with Interstate Highway 25 (I-25).

The headwaters of Kettle Creek are located in the Black Forest, an area dominated by ponderosa pine forest and grassland on undeveloped large acreage tracts and 2- to 5-acre rural residential lots. In the vicinity of Powers Boulevard, the watershed changes to predominately undeveloped grassland. Downstream of Powers Boulevard, the watershed is dominated by residential development consisting of single-family homes, commercial centers, and vacant land. A vicinity map is provided in **Figure 1-1**.

1.7 Data Sources

Data used to complete the analysis for this DBPS, includes digital topography, aerial photography, soils classification, land use, existing stormwater infrastructure, rainfall data, U.S. Geological Survey (USGS) gage data, and pertinent information from previously completed studies. Topography covering the entire Kettle Creek watershed was obtained from USGS quadrangle maps (Black Forest, Falcon NW, Monument, Pikeview). Topographic data was imported using NAD83 (Colorado State Planes, Central Zone, US Foot) in accordance with the notes on the USGS quad maps. Aerial imagery was orthorectified using approximate methods of analysis. This USGS topographic data was only used for the hydrologic analysis. City of Colorado Springs FIMS topographic data was obtained for the reach of Kettle Creek studied in the hydraulic analysis.

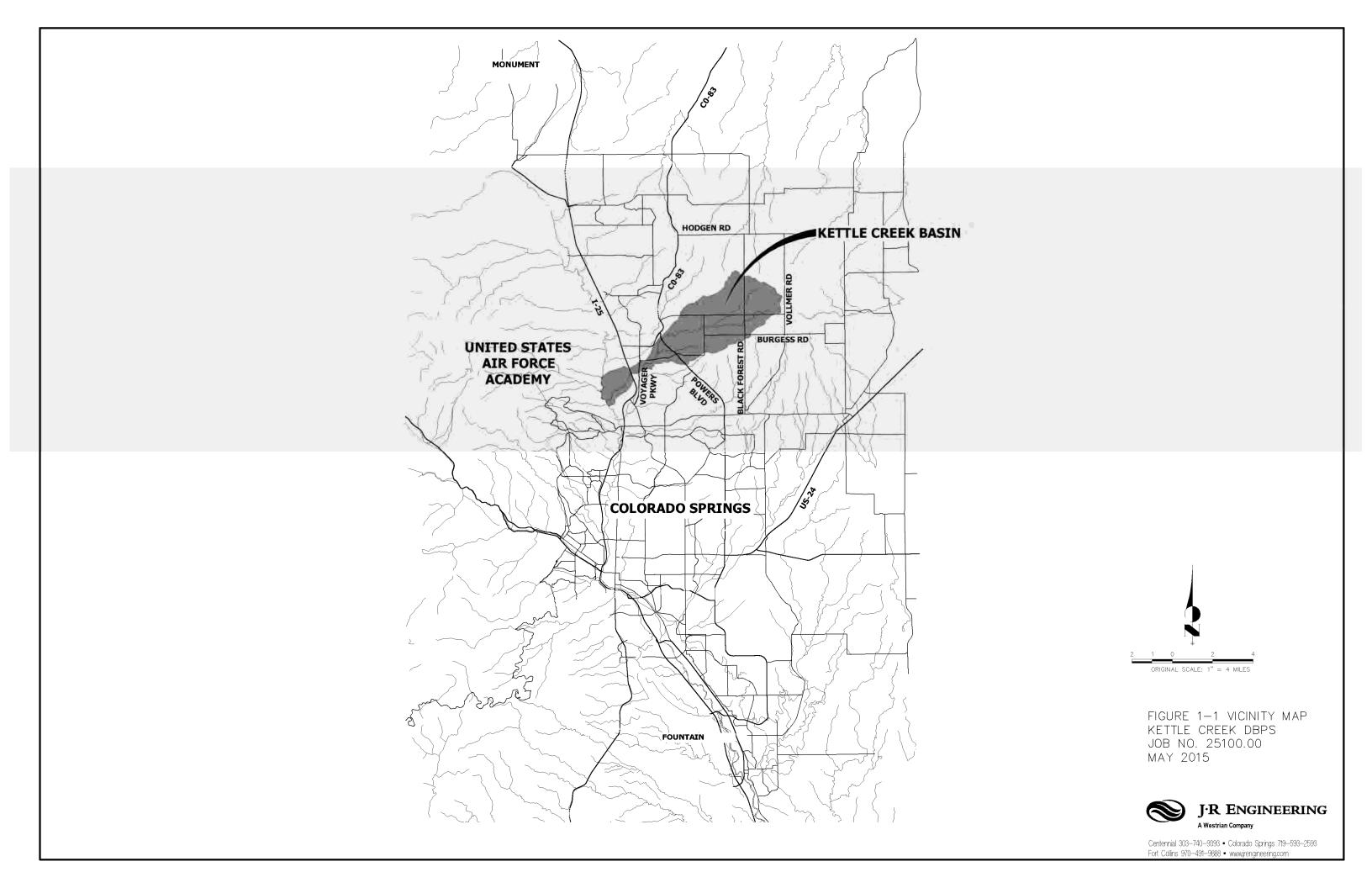
Rainfall data was obtained from the City of Colorado Springs Drainage Criteria Manual (DCM), Volume 1, dated May 2014. One-hour depths were obtained from the DCM and adjusted for elevation using the NOAA procedure. Soils data were obtained from the Natural Resources Conservation Service Web Soil Survey for El Paso County.

A hydrologic model for the Kettle Creek watershed was developed using the US Army Corps of Engineers (USACE) Hydrologic Engineering Center – Hydrologic Modeling System Version 4.0 (HEC-HMS) to simulate the rainfall-runoff process and generate flood hydrographs for select storm events.

A hydraulic model for the Kettle Creek channel was developed using the US Army Corps of Engineers (USACE) Hydrologic Engineering Center – River Analysis System Version 4.1.0 (HEC-RAS) to perform steady-state river hydraulics calculations with bridge analysis and stable channel analysis. City of Colorado Springs FIMS topographic data was used for the hydraulic analysis.

1.8 Applicable Criteria and Standards

The criteria and standards set forth in the City of Colorado Springs Drainage Criteria Manual (DCM), Volume 1 were applied to the entirety of the Kettle Creek DBPS for consistency, although much of the basin lies within unincorporated El Paso County. The Kettle Creek DBPS was prepared in accordance with the policies and procedures established in the DCM.



2 BASIN CHARACTERISTICS

2.1 Location in Watershed, Offsite Flows, Size

The Kettle Creek watershed is located in the north central portion of El Paso County and flows southwesterly from the southern slope of the Black Forest towards the U.S. Air Force Academy. The Kettle Creek watershed contains perennial streams and has a contributing drainage area of approximately 16.41 square miles at its junction with Interstate Highway 25 (I-25). The entire Kettle Creek basin upstream of the U.S. Air Force Academy was studied for this DBPS, from the Kettle Creek headwaters in the Black Forest to I-25. Accordingly, no offsite flows are accounted for in this study.

The headwaters of Kettle Creek are located in the Black Forest, an area dominated by ponderosa pine forest and grassland on undeveloped large acreage tracts and 2- to 5-acre rural residential lots. In the vicinity of Powers Boulevard, the watershed changes to predominately undeveloped grassland. Downstream of Powers Boulevard, the watershed is dominated by residential development consisting of single-family homes, commercial centers, and vacant land.

2.2 Climate, Geology, and Environmental

2.2.1 Climate

The Kettle Creek watershed is located northeast of the City of Colorado Springs. The watershed ranges in elevation from approximately 6,410 feet at I-25 to approximately 7,600 feet at the north end of the basin in the Black Forest. Kettle Creek is tributary to Monument Creek and the confluence with Monument Creek is located near I-25 and Academy Boulevard. Kettle Creek is located at the north end of the Fountain Creek basin, which is tributary to the Arkansas River.

The climate of the region is classified as a mid-latitude steppe, with total annual precipitation averaging 16.2 inches annually. Eighty percent of the region's precipitation comes in the growing season from March to October. Monsoon moisture in the form of thunderstorms in July and August contributes the most. Winter is the driest season of the year. The mean annual snowfall in the region is 84 inches with the peak amount in March.

2.2.2 Geology and Vegetation

The soils in the upper reaches of the Kettle Creek watershed, east of Power Boulevard, are predominately Kettle gravelly-loamy sand and Peyton-Pring complex. Smaller areas of Elbeth sandy loam and Tomah-Crowfoot sandy loam exist at higher elevations in the watershed. The dominant landform in this region is defined as hills, and the parent material is defined as arkosic alluvium derived from sedimentary rock and/or arkosic residuum weathered from sedimentary rock. The ecological site is specified as Sandy Divide. The soils in this region are all classified as Hydrologic Soils Group B. Group B soils are soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission. Surface runoff is slow, creating a low-to-moderate hazard of erosion.

Native vegetation of the Kettle soil is predominately woodland ponderosa pine with a rooting depth of 60 inches.

West of Powers Boulevard, the soils composition changes. In the vicinity of Kettle Creek the soils composition remains similar with Kettle gravelly-loamy sand and Peyton-Pring complex, however away from the creek the dominant soils types are Blakeland loamy sand and Columbine gravelly sand, both of which belong to Hydrologic Soils Group A. Group A soils are soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission. This region is located in a transition zone between forest, shrubland, and prairie. Much of the lower elevations are covered in Gambel oak and prairie grasses. The dominant landform in this region is defined as fans, fan terraces, floodplains, and swales, and the parent material is defined as alluvium derived from sedimentary rock and/or eolian deposits derived from sedimentary rock. The ecological site is specified as Gravelly Foothill.

2.2.3 Groundwater

Planning studies in adjacent basins (Falcon DBPS, prepared by Matrix Design Group, 2013) mapped the depth to groundwater in the Black Forest area and show that the water table is generally greater than 20 feet and more commonly greater than 100 feet below ground surface. It is assumed that these characteristics are typical throughout the upper reaches of the Black Forest area watersheds. The Falcon study speculated that the Black Forest is an infiltration area that recharges the Dawson aquifer because of the course-textured soils that dominate the forest. As groundwater from the Dawson aquifer flows south and southeasterly, it perches on the lower units of the formation (claystone and siltstone) and is 10 to 20 feet below the surface in some places. As elevation decreases in a southeasterly direction, the groundwater surfaces as low discharge springs or seeps. The hydraulic connection between the unconsolidated alluvial deposits in the unnamed tributaries and the Dawson aquifer is greatest where stream valleys have been eroded into the Dawson formation.

2.2.4 Development

Residential and commercial construction throughout the past 13 years has resulted in changes to the drainage pattern throughout the Kettle Creek watershed, particularly downstream of the Black Forest. These changes can either increase or decrease flows to various parts of the watershed. In multiple places, roadside ditches, culverts, and detention ponds have been constructed to manipulate historic flow patterns. These alterations can impact the drainage in two ways. First, the loss of hydrology from reducing flows to particular reaches will result in a change in vegetative structure. These areas have likely lost both wetland function and biodiversity. Second, diverted water may overload reaches that have not adapted to historic high flows. This condition usually results in bank erosion along the channel.

2.3 Major Drainageways and Structures

The major drainageway for the basin is Kettle Creek. Upstream of Powers Boulevard, storm runoff is captured in natural channels and conveyed to Kettle Creek predominately according to historic patterns. Kettle Creek has incised deep channels into the bedrock for much of its length.

Road crossings exist on Black Forest Road, Shoup Road, Milam Road, Powers Boulevard, Old Ranch Road, Voyager Parkway, and I-25. Many small culverts exist for Kettle Creek's smaller tributaries within the Black Forest, but were not considered in this analysis. These crossings were assumed to be adequate because minimal future development in the Black Forest area is expected to occur.

The existing bridges over Kettle Creek at Powers Boulevard, Old Ranch Road, and Voyager Parkway, as well as the regional detention facility at I-25, are assumed to be adequate for the current level of development and will remain for the future condition with no proposed modifications. Future development will be required to detain on-site to preserve the existing conditions discharges in Kettle Creek.

There are no known irrigation facilities in the Kettle Creek watershed.

2.3.1 Voyager Parkway/State Highway 83

It should be noted that later discussions refer to the Voyager Parkway crossing as "State Highway 83". Where the road is now owned by the City it is known as Voyager Parkway. Where the road remains CDOT controlled it is referred to as State Highway 83. Previous drainage studies use the old terminology and the designation State Highway 83 is kept herein to avoid confusion.

2.4 Existing and Proposed Land Uses

The Kettle Creek watershed reflects a variety of existing land uses including rural residential (5 acres, 2.5 acres, 0.5 acres), residential suburban (5000, 6000, 20000, some vacant), agricultural, planned unit development, commercial, and rights-of-way. Due to urban growth, land use is expected to change in the future condition with significant residential development planned in the lower-middle portion of the watershed. It is anticipated that the land uses in the Black Forest area will remain unchanged in the future condition.

3 HYDROLOGIC ANALYSIS

3.1 Major Basins and Sub-basins

3.1.1 Major Basin

The major basin was defined as the entire Kettle Creek watershed from its headwaters in the Black Forest to the I-25 crossing, approximately 16.41 square miles (10,506 acres). The I-25 crossing was determined to represent an adequate termination for the DBPS due to the proximity to the US Air Force Academy grounds (no basin development expected to occur) and the crossing is sufficiently downstream of future development within the Kettle Creek basin.

3.1.2 Sub-basins

The Kettle Creek watershed was divided into 32 sub-basins ranging from 0.12 square miles (79 acres) up to 1.33 square miles (853 acres). Slopes for areas of concentrated flow in the Kettle Creek watershed range from 0.69 percent to 9.64 percent, with shallower and steeper slopes located in the overland flow areas. Sub-basins were delineated at tributaries, major road crossings, changes in slope, changes in land use, and major drainage features. A routing schematic is provided in **Figure 3-1**. A drainage basin map is included as **Figure 3-2**.

3.1.2.1 Sub-basin Delineation

Topographic data for the hydrologic analysis of the entire watershed was obtained from USGS quadrangle maps (Black Forest, Falcon NW, Monument, Pikeview) and approximately traced into AutoCAD Civil 3D at 5-foot intervals.

The Kettle Creek watershed was divided into 3 major reaches: West Tributary, South Tributary, and East Tributary as shown on the basin map, **Figure 3-2**. The West Tributary consists of 19 sub-basins and 5 minor tributaries along the entire length of the watershed from the headwaters in the Black Forest to the crossing at I-25. These sub-basins primarily encompass rural land with pockets of residential development along the main stem of Kettle Creek. The East Tributary consists of 4 sub-basins and 1 minor tributary and encompasses rural residential land in the Black Forest. The Black Forest drains to The South Tributary. The South Tributary consists of 9 sub-basins and 2 minor tributaries. The area consists primarily of suburban residential located within the City of Colorado Springs city limits. This reach is where future development is expected to occur.

3.2 Methodology

3.2.1 Computer Models

A hydrology model for the Kettle Creek watershed was developed using the US Army Corps of Engineers (USACE) Hydrologic Engineering Center – Hydrologic Modeling System Version 4.0 (HEC-HMS) to simulate the rainfall-runoff process and generate flood hydrographs for select storm events. Each component of the model is described in detail following this section.

Sub-basin and stream reach physical characteristics including area, longest hydraulic flow path, reach length, slope, and topological connectivity were extracted for calculation of hydrologic parameters. Hydrologic parameters were calculated as outlined below and populated to the basin and meteorological components of the HEC-HMS model. A summary of selected methodologies for each HEC-HMS model component is provided in Table 3-1.

3.2.1.1 Rainfall Characteristics

The Specified Hyetograph method was chosen to model the hypothetical storm events as outlined in the City of Colorado Springs Drainage Criteria Manual (DCM), Volume 1, dated May 2014. Both the thunderstorm-type 2-Hour Design Storm Distribution (DCM Table 6-3) and the frontal-type NRCS 24-Hour Type II Design Storm Distribution (DCM Table 6-4) were applied to the point precipitation in order to generate the runoff hydrographs. Rainfall depths were obtained from Table 6-2 of the DCM and were verified for the higher elevations in the Kettle Creek watershed using the Urban Drainage and Flood Control District's UD-Rain Version 1.01 spreadsheet. At an average watershed elevation of 7120 feet, the 1-hour storm depth is 2.50 inches and the 24-hour storm depth is 4.60 inches. Point precipitation is shown in **Table 3-1**, below. Design storm input is included in **Appendix B**.

Rainfall Depth in Inches at Time Duration Return Period 15-min 30-min 1-hr 24-hr 5-min 10-min 2-hr 3-hr 6-hr 0.34 0.54 0.68 0.78 1.19 1.37 1.50 1.70 2-yr 2.10 1.00 1.52 1.72 5-yr 0.43 0.68 0.86 1.87 2.10 2.70 0.98 1.73 2.13 3.20 0.49 0.78 1.14 1.96 2.40 10-yr 0.57 0.90 1.14 1.31 2.00 2.31 2.54 2.90 3.60 25-yr 2.26 2.82 4.20 50-yr 0.64 1.02 1.28 1.48 2.58 3.20 100-yr 0.71 1.13 1.42 1.64 2.50 2.84 3.10 3.50 4.60

Table 3-1

Depth Area Reduction Factors (DARFs) are used to adjust point rainfall depths to average depths as the size of drainage basins increase. The largest sub-basin analyzed was slightly larger than one square mile in area, therefore, all sub-basins received the same design storm distribution and no DARFs were applied. Although design storms for a 24-hour NRCS Type II distribution are integrated into the HEC-HMS software program and the program will create a DARF-adjusted design storm, the program's storm distribution was bypassed and the Specified Hyetograph method was selected. This results in a slightly conservative analysis for both storm distributions for the sub-basins above one square mile in area, which are all located in the upper segments of the Kettle Creek watershed.

The rainfall hyetographs were imported into the HEC-HMS precipitation gage manager and applied to each sub-basin within the Kettle Creek watershed. The Colorado Springs frontal-type NRCS 24-Hour Type II Design Storm Distribution yielded higher discharges and this storm was selected as the basis for analysis in the Kettle Creek DBPS.

3.2.1.2 Model Parameters

Infiltration and runoff volumes were modeled using the NRCS Runoff Curve Number (CN) Loss Method. The composite runoff CN was calculated for each sub-basin using the NRCS Curve Numbers for Frontal Storms & Thunderstorms for Developed Conditions (ARCII) (Table 6-10) from the DCM and the composite CNs were imported into HEC-HMS. For modeling purposes, initial infiltration loss rates were automatically calculated as functions of composite runoff CNs by HEC-HMS.

Peak flow rate and hydrographs for this study were computed using the SCS design storm method, which utilizes rainfall together with each sub-basin's physical characteristics to determine rainfall runoff for each sub-basin. Sub-basin lag times were calculated from the time of concentration as computed using the method outlined in the Colorado Springs Drainage Criteria Manual, Section 3. The process is described in more detail in the sections below.

a) Hydrologic Soil Groups

Soils are classified into hydrologic soil groups (HSG) by the NRCS for hydrologic modeling. The HSG is a parameter assigned to each soil series by the NRCS to reflect the relative rate of infiltration of water into the soil profile and is ranked according to infiltration potential from soils of high infiltration (HSG A) to soils of low infiltration (HSG D).

The HSG was determined for each of the soil mapping units from the NRCS Soil Survey data for the El Paso County. Of the four hydrologic soil groups, only A and B soils are found within the Kettle Creek watershed. Group B soils, with moderate infiltration rates, dominate the Kettle Creek watershed at 97.3% coverage. A hydrologic soil group map is provided in **Figure 3-3** that shows the distribution and coverage of each group within the Kettle Creek watershed.

Table 3-2 Soil Coverage by Hydrologic Soil Group

| | , , , , , , , , , , , , , , , , , , , | |
|----------|---|----------|
| Land Use | Acreage | Coverage |
| HSG A | 307 | 2.9% |
| HSG B | 10,194 | 97.1% |

b) Land Use

Historical land use conditions were assigned based on the land use categories defined in the DCM that are consistent with the native land uses within the watershed. Historical land use conditions represent an undeveloped watershed condition and were used as the underlying land use for runoff CN development as described below. Undeveloped land use conditions were classified under the appropriate category of "Other Agricultural Lands" in Table 6-9 of the DCM for NRCS Curve Numbers for Pre-Development Thunderstorms Conditions (ARC I). The land uses are classified as being in good, fair, or poor condition. Woods (Good Condition) is the dominant underlying land use in upper portion of the Kettle Creek watershed while

Rangeland (Good Condition) is the dominant underlying land use throughout the remainder of the watershed. Each of these land uses categories were assigned a good condition based on field observation of ground cover.

Existing and future land use information for the Kettle Creek watershed was obtained from aerial imagery and El Paso County zoning information. Existing land uses were estimated form the aerial imagery (2011 and 2013). It was assumed that the land zoning can be used as a good indicator of fully developed conditions. The future land use data represents the current prediction of a full build-out scenario, sometime after 2030.

The Kettle Creek watershed reflects a variety of existing land uses including rural residential (5 acres, 2.5 acres, 0.5 acres), residential suburban (5000, 6000, 20000, some vacant), agricultural, planned unit development, commercial, and rights-of-way. Due to urban growth, land use is expected to change in the future condition with significant residential development planned in the lower middle portion of the watershed. It is anticipated that the land uses in the Black Forest area will remain unchanged in the future condition. Land use maps are shown in **Figure 3-4**, **Figure 3-5**, and **Figure 3-6** for historic, existing, and future conditions respectively. Summaries of land uses are shown in **Table 3-3**, **Table 3-4**, and **Table 3-5**, below.

Table 3-3 Historic Land Use Classes

| Land Use | Coverage |
|-----------------------------------|----------|
| Meadows, Good Condition, HSG A | 2.3% |
| Herbaceous, Good Condition, HSG B | 32.1% |
| Woods, Good Condition, HSG B | 65.6% |

Table 3-4
Existing Land Use Classes

| Land Use | Coverage |
|---|----------|
| Asphalt, HSG A | 0.1% |
| Asphalt, HSG B | 2.8% |
| Commercial Office, HSG A | 0.3% |
| Commercial Retail, HSG B | 0.4% |
| School, HSG B | 0.6% |
| Meadows, Good Condition, HSG A | 1.6% |
| Open Space Herbaceous, Good Condition, HSG B | 14.3% |
| Residential (5 ac lots) and Herbaceous, HSG B | 13.2% |
| Residential (5 ac lots) and Wooded, HSG B | 55.7% |
| Residential (2.5 ac lots) and Wooded, HSG B | 1.2% |
| Residential (2 lots per ac) and Wooded, HSG B | 2.6% |
| Residential 1/4 ac lots, HSG A | 0.8% |
| Residential 1/4 ac lots, HSG B | 2.3% |
| Special Uses | 4.2% |

Table 3-5
Future Land Use Classes

| Land Use | Coverage |
|--|----------|
| Asphalt, HSG A | 0.1% |
| Asphalt, HSG B | 2.8% |
| Commercial Office, HSG A | 1.0% |
| Commercial Retail, HSG B | 0.6% |
| School, HSG B | 0.7% |
| Meadows, Good Condition, HSG A | 0.5% |
| Open Space Herbaceous, Good Condition, HSG B | 4.3% |
| Residential (5 ac lots) and Herbaceous, HSG B | 14.9% |
| Residential (5 ac lots) and Wooded, HSG B | 55.6% |
| Residential (2.5 ac lots) and Wooded, HSG B | 3.1% |
| Residential (2 lots per ac) and Wooded, HSG B | 2.6% |
| Residential 1/4 ac lots, HSG A | 0.8% |
| Residential 1/4 ac lots, HSG B | 8.9% |
| Special Uses | 4.2% |

c) Runoff Curve Number Development

The Natural Resources Conservation Service (NRCS), U.S. Department of Agriculture, has instituted a soil classification system that relates the drainage characteristics of soil groups to a curve number, CN (SCS, 1972 and 1975). The NRCS provides information on relating soil group type to the curve number as a function of soil cover, antecedent moisture condition, and land use type. Curve number values were determined for each sub-basin. For the Kettle Creek basin, the predominant hydrologic soil group is B with an antecedent moisture condition of ARCII. The CN values differ between the existing and future conditions primarily to reflect the changes in the land use. Based on existing land use, zoning and known development plans, the basin is expected to generally change in places from an undeveloped pasture/woodland to low density residential. This is reflected by a 7% increase in the average basin CN from existing to future conditions. Tables illustrating the determination of the CN values are presented in **Appendix B**. Curve Number maps are shown in **Figure 3-7**, **Figure 3-8**, and **Figure 3-9** for historic, existing, and future conditions respectively. Curve number values for the respective land uses are shown in **Table 3-6**, below.

Kettle Creek DBPS Hydrologic Analysis 3-3

Table 3-6
Representative CN Values and Impervious Percentage by Land Use

| Land Use | CN | Percent |
|--|-----|------------|
| Land Use | CIV | Impervious |
| Meadows, Good Condition, HSG A (Existing) | 15 | 2 |
| Herbaceous, Good Condition, HSG B (Existing) | 41 | 2 |
| Woods, Good Condition, HSG B (Existing) | 34 | 2 |
| Asphalt, HSG A | 83 | 100 |
| Asphalt, HSG B | 89 | 100 |
| Commercial Office, HSG A | 89 | 95 |
| Commercial Retail, HSG B | 92 | 85 |
| School, HSG B | 72 | 40 |
| Meadows, Good Condition, HSG A | 39 | 2 |
| Open Space Herbaceous, Good Condition, HSG B | 62 | 2 |
| Residential (5 ac lots) and Herbaceous, HSG B | 65 | 15 |
| Residential (5 ac lots) and Wooded, HSG B | 65 | 15 |
| Residential (2.5 ac lots) and Wooded, HSG B | 65 | 20 |
| Residential (2 lots per ac) and Wooded, HSG B | 70 | 35 |
| Residential 1/4 ac lots, HSG A | 61 | 60 |
| Residential 1/4 ac lots, HSG B | 75 | 60 |
| Special Uses | 74 | 10 |

Average weighted curve numbers for the whole Kettle Creek basin are shown in Table 3-7, below.

Table 3-7
Average Weighted Runoff Curve Numbers

| Condition | Curve Number |
|-----------------------|--------------|
| Historic ¹ | 36 |
| Historic ² | 57 |
| Existing | 66 |
| Future | 69 |

¹Uses Pre-Development curve numbers (ARC-I) for 2-Hour Storm

² Uses Post-Development curve numbers (ARC-II) for 24-Hour Storm

d) Initial Abstraction

The initial abstraction (I_a) represents a volume of rainfall that must fall to satisfy losses in a drainage basin before runoff begins. Per the DCM chapter 6, the default value for I_a is 0.10 times the potential maximum retention (S). To apply this adjustment when using HEC-HMS it is necessary to provide the initial abstraction as a depth in inches. The initial abstraction in inches is calculated according to the equation:

 $I_a = 0.1 [(1000/CN) - 10].$

e) Time of Concentration

The times of concentration for the sub-basins were calculated according to the procedures outlined in the DCM, Chapter 6. The time of concentration is calculated following the guidance provided in TR-55 (NRCS 2005) by dividing the flow path into multiple segments. These segments can generally be categorized as overland flow, shallow concentrated flow and concentrated or channelized flow. For each of the flow segments, the estimated 2-year flow or the "low flow" should be used to calculate velocity. The time of concentration for the sub-basin is taken as the sum of the three flow regimes from the headwaters of the sub-basin to its discharge point.

f) Channel Routing

The Lag method was used for channel routing with lag times applied on an individual basis for each river reach. Lag times were calculated in accordance with Chapter 6 of the City DCM using Manning's equation to define average flow velocity. Approximate hydraulic characteristics for concentrated flow were used, taken from the UDFCD DCM Runoff chapter (Table RO-2). Reach delineations were performed for existing conditions and are unlikely to change significantly through later stages of development, as Kettle Creek and its tributaries are typically defined by deep earth channels with large areas of exposed bedrock.

3.2.1.3 Model Flow Diagram and Design Points

Design points were taken at every sub-basin junction where flow routing affected peak flows. In the model, reaches were used to connect junctions and provide routing of the concentrated flows at the specified length, slope, and roughness. A routing schematic is provided in **Figure 3-1**.

3.3 Basin Hydrology

The HEC-HMS model for the Kettle Creek watershed was run to simulate the rainfall-runoff process and generate flood hydrographs for historic, existing, and future land use conditions by applying a 2-hour and a 24- hour storm event with 2-, 5- 10-, 25- 50-, and 100-year recurrence intervals. As expected, future peak flows increased over existing conditions in conjunction with planned development. When compared to the 2-hour event, the 24-hour event has overall higher peak flows for the Kettle Creek basin and is therefore used for peak flow rates in the Kettle Creek DBPS hydraulic analysis and for floodplain delineation.

The results of the Kettle Creek Drainage Basin Old Ranch Road Tributary DBPS/MDDP by JR Engineering (2001) were used to represent the developed conditions discharge into Kettle Creek for existing and future

development in the DBPS/MDDP study. The hydrographs for the detained releases into Kettle Creek replace the undetained sub-basin discharges in the HEC-HMS model.

The existing and future conditions hydrologic model results reported herein do not reflect any other existing, proposed, or conceptual future detention, channel improvements, or other alternatives described in later sections of this report. The intent of this DBPS is to provide a baseline for future development in the Kettle Creek Basin. Historic, existing, and future results are illustrated in **Figure 3-12**, **Figure 3-13**, and **Figure 3-14**, respectively.

3.3.1 Historic Flows

The Kettle Creek DBPS presented herein assumed an undeveloped condition throughout the entire basin for historic conditions. Historic land uses consisted of woods and semi-arid Herbaceous rangeland (See **Figure 3-4**). Using the aforementioned methods of analysis, the historic conditions analysis determined a peak historic flow of 705 cfs (5-year) and 2,381 cfs (100-year) at State Highway 83. Historic conditions flow data is presented in **Figure 3-10** and **Figure 3-11**.

3.3.2 Existing Flows

The existing conditions analysis used 2013 land uses as shown in **Figure 3-5** to determine curve numbers and percent impervious for the Kettle Creek Basin. The existing conditions analysis yielded flows of 1,766 cfs (5-year) and 4,114 cfs (100-year) at State Highway 83. To incorporate the existing regional detention ponds, Sub-basins 24 through 27 have been replaced by outflow hydrographs gathered from the Kettle Creek Drainage Basin Old Ranch Tributary MDDP/DBPS. Existing conditions flow data is presented in **Figure 3-10** and **Figure 3-11**.

3.3.3 Future Flows

The future conditions analysis made use of available City of Colorado Springs and El Paso County zoning information to determine the land uses at full basin build-out. Future land uses are shown in **Figure 3-6**. The future conditions analysis yielded flows of 1,796 cfs (5-year) and 4,152 cfs (100-year) at State Highway 83. To incorporate the existing regional detention ponds, Sub-basins 24 through 27 have been replaced by outflow hydrographs gathered from the Kettle Creek Drainage Basin Old Ranch Tributary MDDP/DBPS. Future conditions flow data is presented in **Figure 3-10** and **Figure 3-11**.

3.3.4 Flows Comparison

The results of this hydrologic analysis were compared with previous reports. In this DBPS, 5-year and 100-year peak inflows to the Kettle Creek detention facility at I-25 of 1,845 cfs and 4,250 cfs, respectively, were generated under existing watershed conditions. This study employed SCS methodologies along with NRCS-based soils and land use data specific to the Kettle Creek watershed. Composite CNs were calculated using NRCS attributes. The location of Kettle Creek at State Highway 83 (now Voyager Parkway) was used as a basis of comparison because it is presented in Volume I of the FIS. Detailed hydrologic results are presented in **Appendix B**. Flow results at State Highway 83 are shown in **Table 3-8** below:

Table 3-8
Flow Comparison at State Highway 83

| Storm Recurrence Interval | Historic Flows (cfs) | | Existing Flows (cfs) | | Future Flows (cfs) | | |
|------------------------------|-------------------------|-----------------|-------------------------|-------|-----------------------|-------|-----------------|
| | | Kettle Creek | FIS | AFA | Kettle Creek | AFA | Kettle Creek |
| 24 Hr Duration | AFA Study | DBPS | Study | Study | DBPS | Study | DBPS |
| 2 | 115 | 354 | | 271 | 1,174 | 285 | 1,199 |
| 5 | 334 | 705 | | 743 | 1,766 | 783 | 1,796 |
| 10 | 686 | 1,073 | 2,600 | 1,308 | 2,332 | 1,372 | 2,364 |
| 25 | 1,328 | 1,410 | | 2,246 | 2,814 | 2,355 | 2,849 |
| 50 | 2,142 | 1,972 | | 3,327 | 3,580 | 3,486 | 3,617 |
| 100 | 2,912 | 2,381 | 9,300 | 4,287 | 4,114 | 4,475 | 4,152 |

There are no previous DBPS studies for the entire Kettle Creek basin. An existing study available for flows comparison is the FEMA FIS for El Paso County and Incorporated Areas, dated August 23, 1999. The FIS used a joint Colorado Water Conservation Board (CWCB), a USACE study conducted on Monument and Fountain creeks with the USGS hydrologic report, Manual for Estimating Flood Characteristics of Natural-Flow Streams in Colorado (1976), and rainfall data from the Flood Hazard Analyses, Portions of Jimmy Camp Creek and Tributaries (October 1975) report, combined with the SCS Soil Survey for El Paso County (July 1981) to determine peak flow rates, using the empirical USGS regression equations for the southwestern United States. The FIS presents Kettle Creek as having a drainage area of 16.3 square miles, with peak discharges of 2,600 cfs (10-year) and 9,300 cfs (100-year) at State Highway 83 (now known as Voyager Parkway). No other hydrologic data is presented in the FIS. The discrepancies between the FIS, the AFA Study, and this DBPS are potentially due to the differing USGS and SCS methodologies.

The AFA Study reported 2-, 5-, 10-, 25-, 50-, and 100-year peak inflows as shown in **Table 3-8**. The study also employed SCS methodologies along with GIS-based soils and land use data specific to the Kettle Creek watershed. The discrepancies in peak flows between the Air Force Academy (AFA) and this study were due to minor differences in composite CNs, sub basin delineation and lag time calculations. The AFA also used a Kinematic Wave method for Channel Routing instead of the Lag Method used herein. Two sub-regional ponds in Sub-basins 24-27 were also modeled herein, whereas the ponds did not exist during the time of the

Kettle Creek DBPS Hydrologic Analysis 3-5

AFA Study. The absence of these ponds would result in higher peak flows. The greater discrepancies in discharges with the smaller storm recurrence intervals are due to the Initial Abstraction values determined from the CNs. This DBPS uses an Initial Abstraction value of 0.1 times the potential maximum retention (S) in accordance with current City criteria, while the AFA study uses an Initial Abstraction value of 0.2 times S. Thus, the amount of water lost to infiltration during minor storm events is much greater in the AFA study.

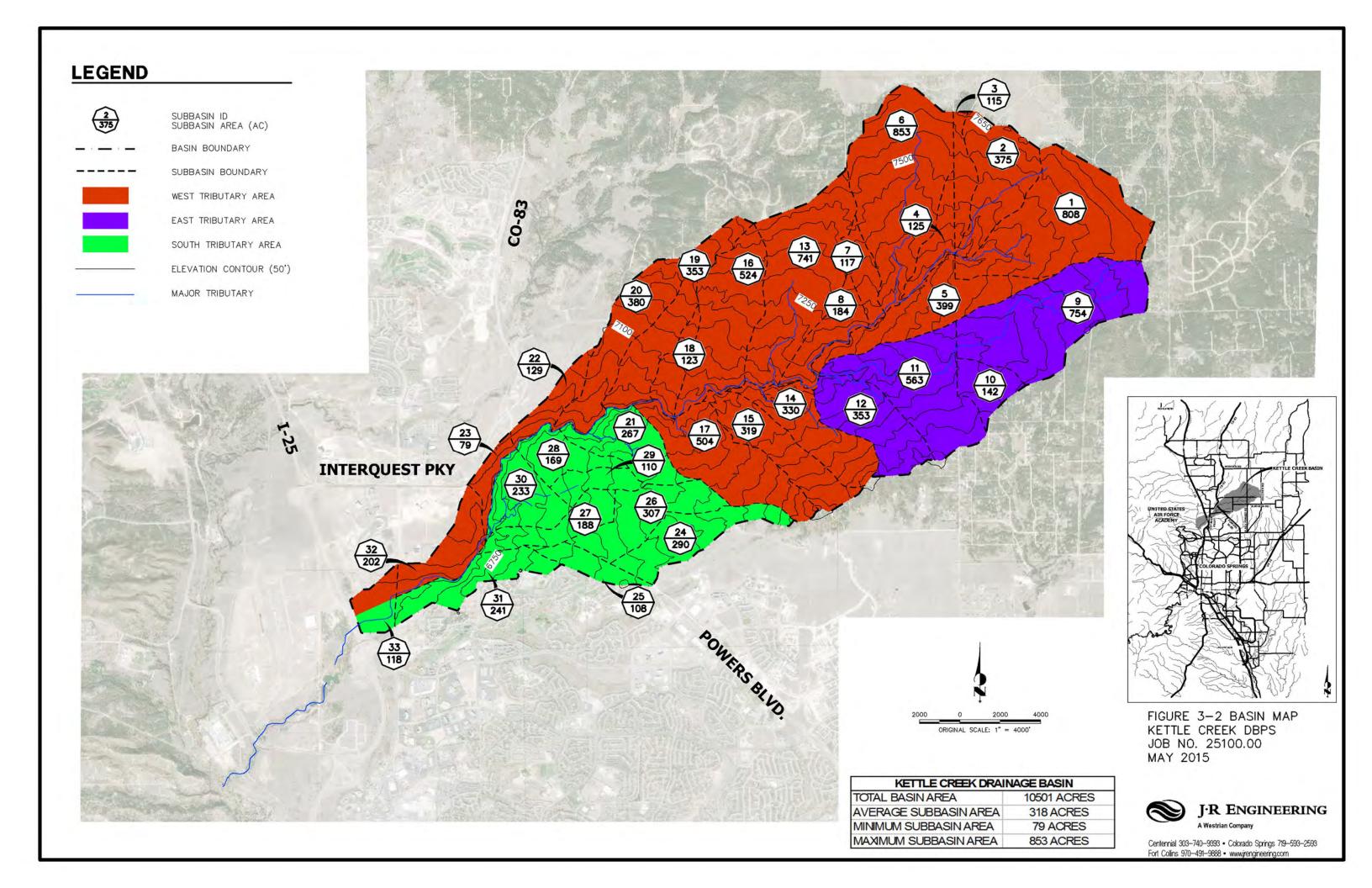
Topography covering the entire Kettle Creek watershed was obtained from USGS quadrangle maps (Black Forest, Falcon NW, Monument, Pikeview) and was used for the hydrologic analysis of the basin only, and current electronic contours were obtained from the City for the hydraulic analysis. Hydrologic modeling inputs were obtained from this topographic data as well as following the SCS methodologies stated in the City of Colorado Springs Drainage Criteria Manual (May 2014). Version 4.0 of the HEC-HMS modeling software was employed. With a percent error of only five percent, the resulting 100-year peak flows form this model was comparable with results found from the AFA Study.

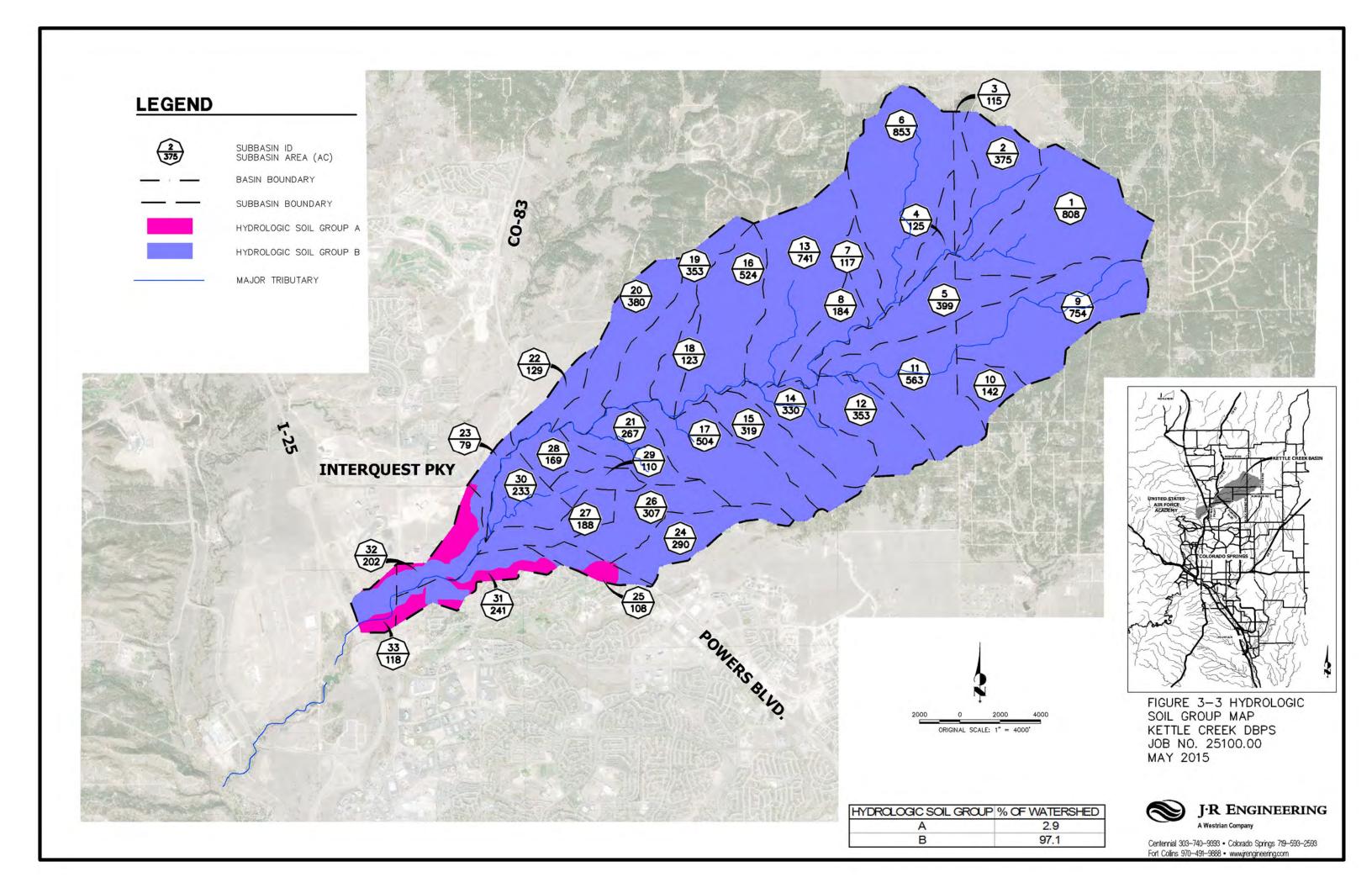
LEGEND SUBBASIN IDENTIFIER TRIBUTARY JUNCTION IDENTIFIER STREAM REACH IDENTIFIER SOUTH EAST TRIBUTARY B24 POWERS BLVD B1 (B28) (B15) (B17) (B14) (B2 (B3) (B7) (BB) (B16) (B18) (B19) (B20) (B22) (B30 (B23) (B32 WEST TRIBUTARY

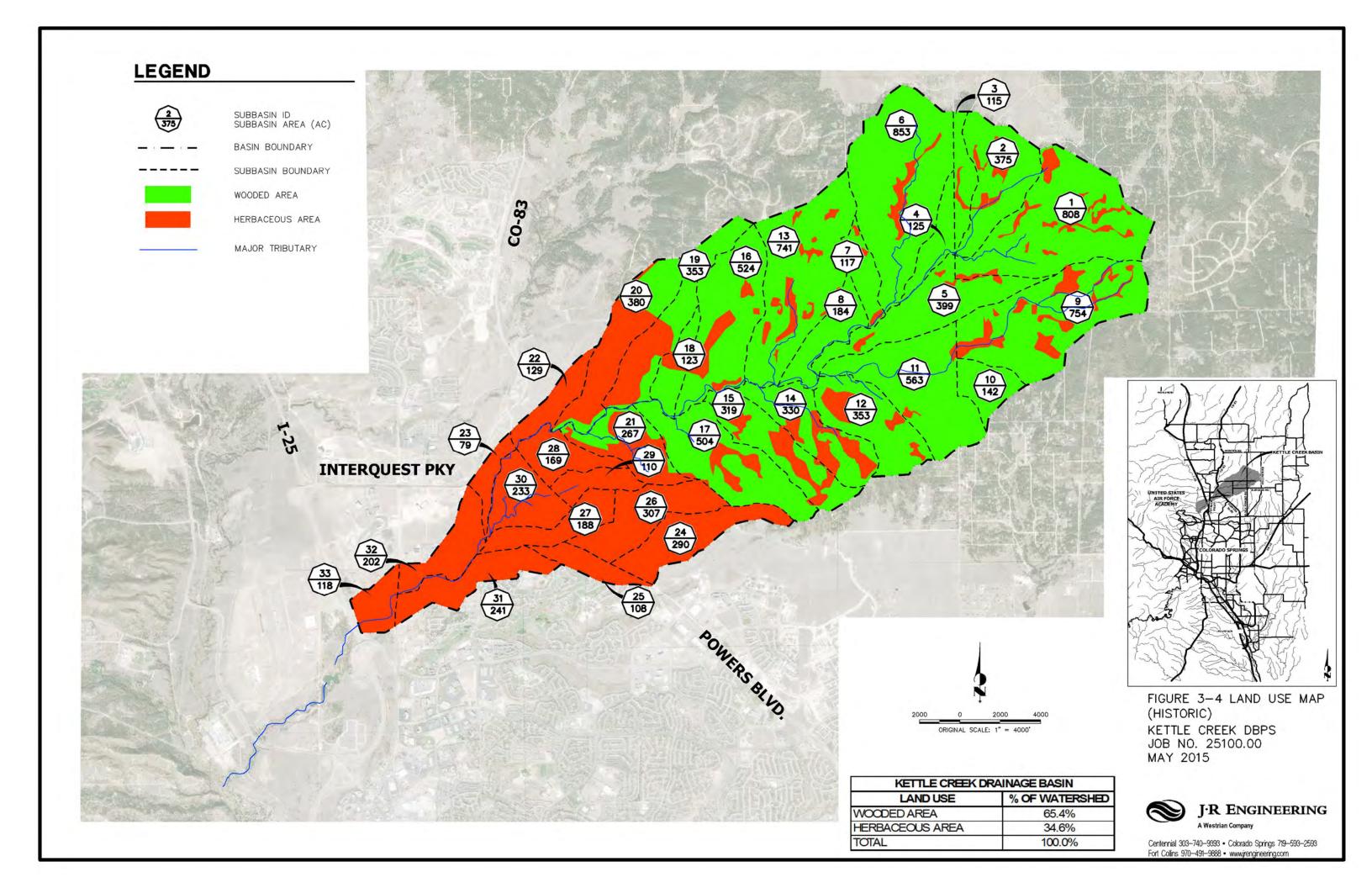
FIGURE 3-1
ROUTING SCHEMATIC
KETTLE CREEK DBPS
JOB NO. 25100.00
MAY 2015



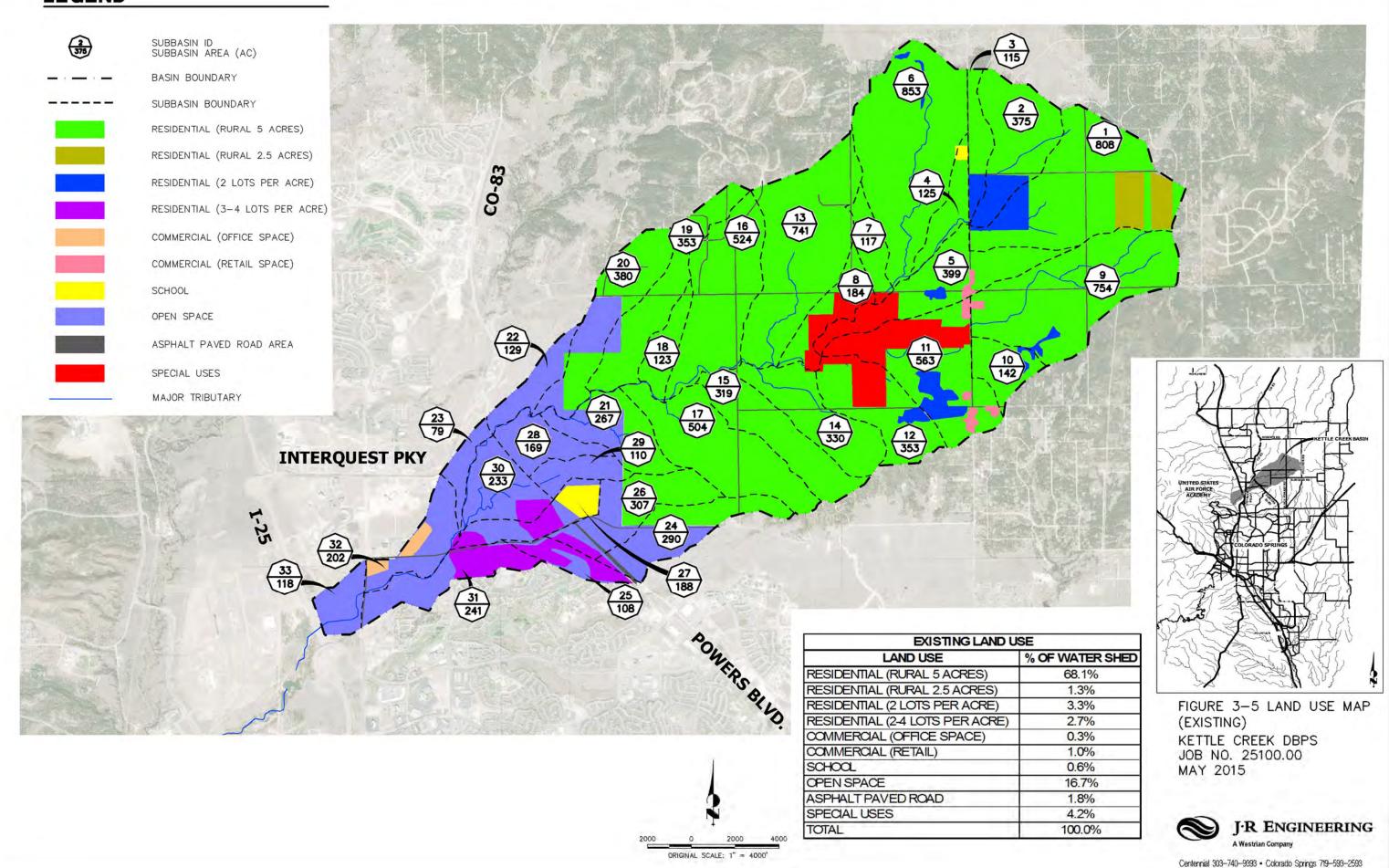
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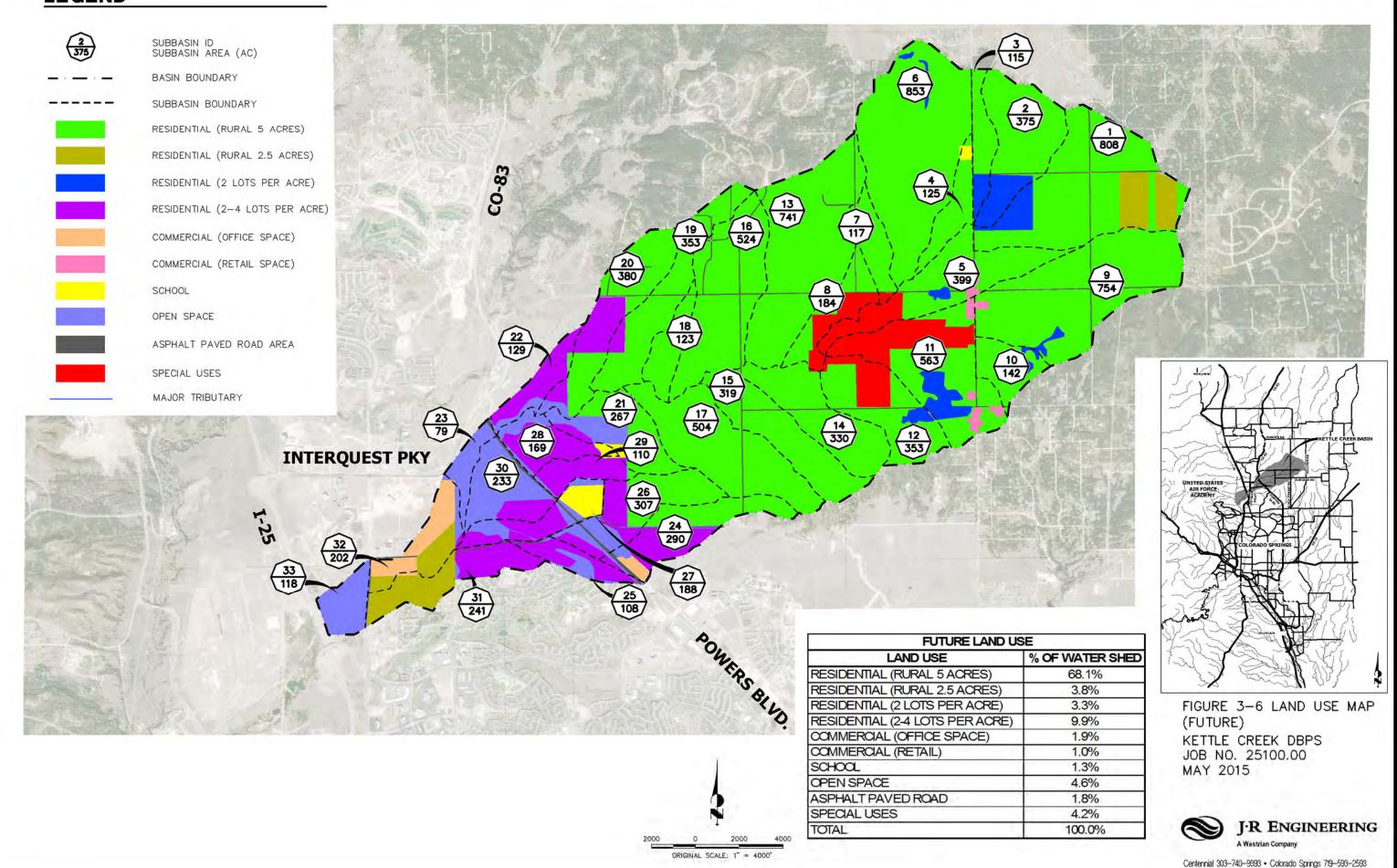


LEGEND

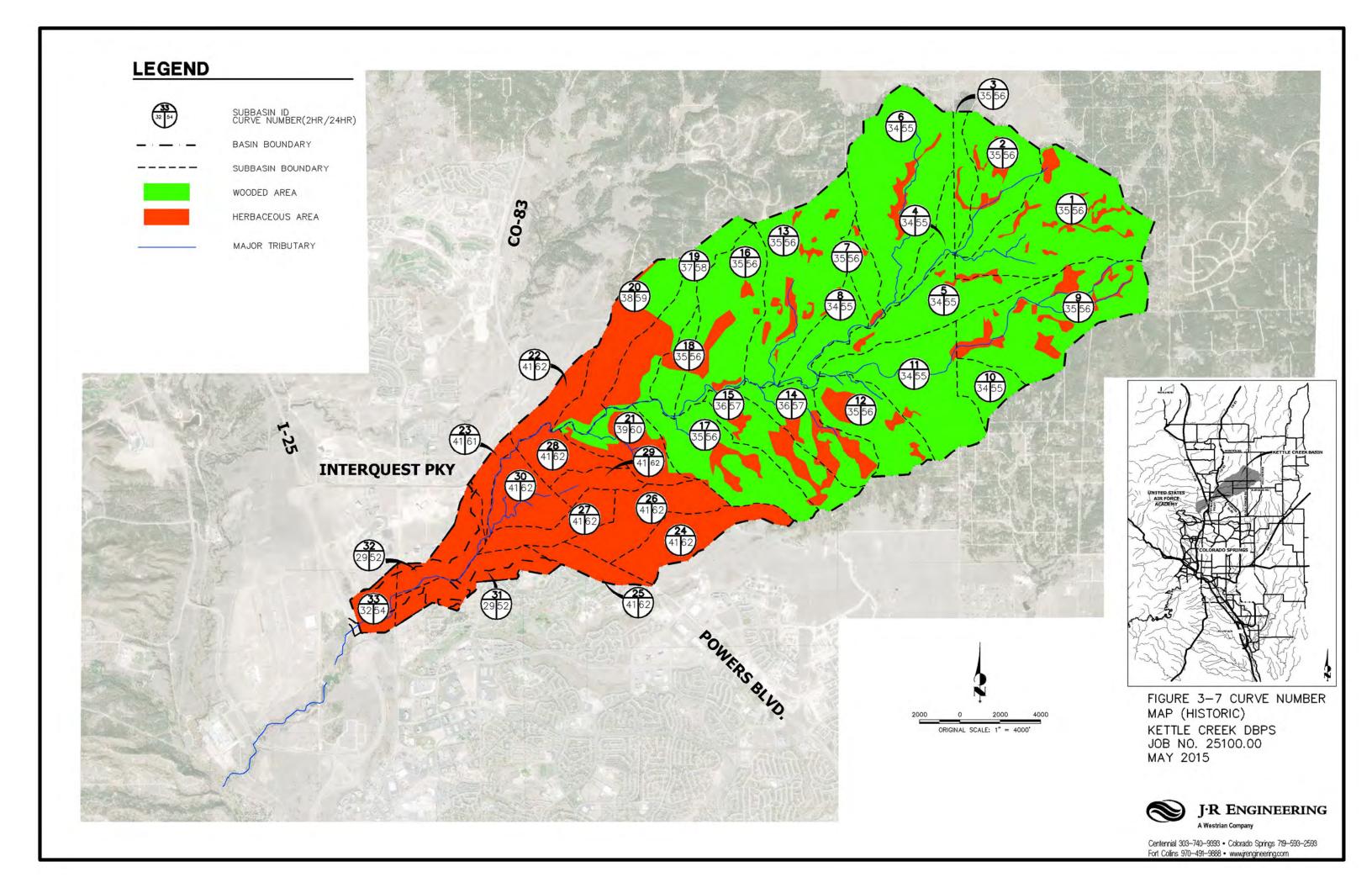


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LEGEND (2) (57) SUBBASIN ID CURVE NUMBER BASIN BOUNDARY 65 SUBBASIN BOUNDARY (2) (66) RESIDENTIAL (RURAL 5 ACRES) 66 RESIDENTIAL (RURAL 2.5 ACRES) CO-83 65 RESIDENTIAL (2 LOTS PER ACRE) RESIDENTIAL (3-4 LOTS PER ACRE) 66 16 66 19 65 COMMERCIAL (OFFICE SPACE) 5 69 COMMERCIAL (RETAIL SPACE) 70 66 SCHOOL OPEN SPACE 22 62 ASPHALT PAVED ROAD AREA SPECIAL USES 15 66 MAJOR TRIBUTARY 21 64 17 65 (23 62 14 65 28 62 29 63 **INTERQUEST PKY** 30 66 26 66 27 70 FIGURE 3-8 CURVE NUMBER MAP (EXISTING) KETTLE CREEK DBPS JOB NO. 25100.00 ORIGINAL SCALE: 1" = 4000' MAY 2015 J·R ENGINEERING A Westrian Company Centennial 303-740-9393 • Colorado Springs 719-593-2593 Fort Collins 970-491-9888 • www.jrengineering.com

LEGEND $\binom{2}{57}$ SUBBASIN ID CURVE NUMBER 65 BASIN BOUNDARY SUBBASIN BOUNDARY (2) (66) RESIDENTIAL (RURAL 5 ACRES) 66 RESIDENTIAL (RURAL 2.5 ACRES) CO-83 65 RESIDENTIAL (2 LOTS PER ACRE) 13 66 RESIDENTIAL (2-4 LOTS PER ACRE) 16 66 19 66 COMMERCIAL (OFFICE SPACE) COMMERCIAL (RETAIL SPACE) (5) (69) 9 66 70 SCHOOL OPEN SPACE 18 65 72 ASPHALT PAVED ROAD AREA SPECIAL USES 15 66 MAJOR TRIBUTARY 65 17 65 14 65 29 76 INTERQUEST PKY 26 68 FIGURE 3-9 CURVE NUMBER MAP (FUTURE) KETTLE CREEK DBPS JOB NO. 25100.00 ORIGINAL SCALE: 1" = 4000' MAY 2015



HISTORIC CONDITIONS MODEL RESULTS (5-YEAR)

| 5-Year, 24-Hour Storm | | | |
|-----------------------|-------------------------|-----------|--------|
| | | Peak | |
| Hydrologic | Drainage | Discharge | Volume |
| Element | Area (mi ²) | (CFS) | (in) |
| Subbasin-1 | 1.263 | 111 | 0.42 |
| Subbasin-2 | 0.586 | 59 | 0.42 |
| Subbasin-3 | 0.18 | 17 | 0.42 |
| Junction-1 | 2.029 | 185 | 0.42 |
| Reach-1 | 2.029 | 184 | 0.42 |
| Subbasin-4 | 0.195 | 20 | 0.4 |
| Junction-2 | 2.224 | 202 | 0.42 |
| Reach-2 | 2.224 | 195 | 0.42 |
| Subbasin-5 | 0.625 | 42 | 0.4 |
| Junction-3 | 2.849 | 235 | 0.41 |
| Reach-3 | 2.849 | 235 | 0.41 |
| Subbasin-6 | 1.333 | 93 | 0.4 |
| Junction-4 | 4.182 | 328 | 0.41 |
| Reach-4 | 4.182 | 323 | 0.41 |
| Subbasin-7 | 0.183 | 20 | 0.42 |
| Junction-5 | 4.365 | 333 | 0.41 |
| Reach-5 | 4.365 | 324 | 0.41 |
| Subbasin-8 | 0.288 | 35 | 0.4 |
| Junction-6 | 4.653 | 337 | 0.41 |
| Reach-6 | 4.653 | 336 | 0.41 |
| Subbasin-9 | 1.177 | 81 | 0.42 |
| Subbasin-10 | 0.222 | 24 | 0.4 |
| Junction-7 | 1.399 | 93 | 0.42 |
| Reach-7 | 1.399 | 92 | 0.42 |
| Subbasin-11 | 0.88 | 89 | 0.4 |
| Junction-8 | 2.279 | 152 | 0.41 |
| Reach-8 | 2.279 | 150 | 0.41 |
| Subbasin-12 | 0.552 | 52 | 0.43 |
| Junction-9 | 2.831 | 193 | 0.41 |
| Reach-9 | 2.831 | 191 | 0.41 |
| Junction-10 | 7.484 | 508 | 0.41 |
| Reach-10 | 7.484 | 500 | 0.41 |
| Subbasin-13 | 1.156 | 80 | 0.42 |
| Subbasin-14 | 0.516 | 59 | 0.45 |
| Junction-11 | 9.156 | 578 | 0.41 |
| Reach-11 | 9.156 | 576 | 0.41 |
| Subbasin-15 | 0.498 | 57 | 0.44 |
| Junction-12 | 9.654 | 590 | 0.42 |
| Reach-12 | 9.654 | 589 | 0.42 |
| Subbasin-16 | 0.819 | 68 | 0.42 |
| Subbasin-17 | 0.788 | 74 | 0.42 |
| Junction-13 | 11.261 | 631 | 0.42 |

| 5-Year, 24-Hour Storm | | | |
|-----------------------|------------|-----------|--------|
| | | Peak | |
| Hydrologic | Drainage | Discharge | Volume |
| Element | Area (mi²) | (CFS) | (in) |
| Reach-13 | 11.261 | 627 | 0.42 |
| Subbasin-18 | 0.192 | 23 | 0.42 |
| Junction-14 | 11.453 | 631 | 0.42 |
| Reach-14 | 11.453 | 624 | 0.42 |
| Subbasin-19 | 0.552 | 46 | 0.47 |
| Junction-15 | 12.005 | 641 | 0.42 |
| Reach-15 | 12.005 | 640 | 0.42 |
| Subbasin-20 | 0.594 | 73 | 0.5 |
| Junction-16 | 12.599 | 654 | 0.42 |
| Reach-16 | 12.599 | 653 | 0.42 |
| Subbasin-21 | 0.417 | 65 | 0.52 |
| Junction-17 | 13.016 | 661 | 0.43 |
| Reach-17 | 13.016 | 658 | 0.43 |
| Subbasin-22 | 0.2 | 35 | 0.57 |
| Junction-18 | 13.216 | 662 | 0.43 |
| Reach-18 | 13.216 | 660 | 0.43 |
| Subbasin-23 | 0.123 | 35 | 0.55 |
| Junction-19 | 13.339 | 662 | 0.43 |
| Reach-19 | 13.339 | 660 | 0.43 |
| Subbasin-24 | 0.453 | 54 | 0.57 |
| Subbasin-25 | 0.169 | 51 | 0.57 |
| Subbasin-26 | 0.48 | 64 | 0.57 |
| Junction-21 | 1.102 | 128 | 0.57 |
| Reach-21 | 1.102 | 125 | 0.57 |
| Subbasin-27 | 0.294 | 52 | 0.57 |
| Junction-22 | 1.396 | 164 | 0.57 |
| Reach-22 | 1.396 | 161 | 0.57 |
| Subbasin-28 | 0.264 | 38 | 0.57 |
| Subbasin-29 | 0.172 | 30 | 0.57 |
| Junction-20 | 0.436 | 68 | 0.57 |
| Reach-20 | 0.436 | 64 | 0.57 |
| Subbasin-30 | 0.364 | 65 | 0.57 |
| Junction-23 | 15.535 | 702 | 0.45 |
| Reach-23 | 15.535 | 697 | 0.45 |
| Subbasin-31 | 0.377 | 58 | 0.33 |
| Subbasin-32 | 0.316 | 37 | 0.33 |
| Junction-24 | 16.228 | 705 | 0.44 |
| Reach-24 | 16.228 | 702 | 0.44 |
| Subbasin-33 | 0.184 | 24 | 0.37 |
| Junction-25 | 16.412 | 704 | 0.44 |
| Reach-25 | 16.412 | 698 | 0.44 |
| Junction-26 | 16.412 | 698 | 0.44 |

EXISTING CONDITIONS MODEL RESULTS (5-YEAR)

| 5-Year, 24-Hour Storm | | | |
|-----------------------|-------------------------|-----------|--------|
| | | Peak | |
| Hydrologic | Drainage | Discharge | Volume |
| Element | Area (mi ²) | (CFS) | (in) |
| Subbasin-1 | 1.263 | 315 | 1.06 |
| Subbasin-2 | 0.586 | 173 | 1.06 |
| Subbasin-3 | 0.180 | 56 | 1.27 |
| Junction-1 | 2.029 | 527 | 1.08 |
| Reach-1 | 2.029 | 526 | 1.08 |
| Subbasin-4 | 0.195 | 56 | 0.97 |
| Junction-2 | 2.224 | 572 | 1.07 |
| Reach-2 | 2.224 | 568 | 1.07 |
| Subbasin-5 | 0.625 | 134 | 1.14 |
| Junction-3 | 2.849 | 689 | 1.08 |
| Reach-3 | 2.849 | 689 | 1.08 |
| Subbasin-6 | 1.333 | 240 | 0.94 |
| Junction-4 | 4.182 | 928 | 1.04 |
| Reach-4 | 4.182 | 917 | 1.04 |
| Subbasin-7 | 0.183 | 51 | 0.97 |
| Junction-5 | 4.365 | 940 | 1.03 |
| Reach-5 | 4.365 | 929 | 1.03 |
| Subbasin-8 | 0.288 | 117 | 1.1 |
| Junction-6 | 4.653 | 959 | 1.04 |
| Reach-6 | 4.653 | 944 | 1.04 |
| Subbasin-9 | 1.177 | 223 | 1.05 |
| Subbasin-10 | 0.222 | 62 | 0.93 |
| Junction-7 | 1.399 | 252 | 1.03 |
| Reach-7 | 1.399 | 250 | 1.03 |
| Subbasin-11 | 0.880 | 322 | 1.23 |
| Junction-8 | 2.279 | 484 | 1.11 |
| Reach-8 | 2.279 | 484 | 1.11 |
| Subbasin-12 | 0.552 | 144 | 1.06 |
| Junction-9 | 2.831 | 609 | 1.1 |
| Reach-9 | 2.831 | 594 | 1.1 |
| Junction-10 | 7.484 | 1,444 | 1.06 |
| Reach-10 | 7.484 | 1,428 | 1.06 |
| Subbasin-13 | 1.156 | 212 | 1 |
| Subbasin-14 | 0.516 | 138 | 0.95 |
| Junction-11 | 9.156 | 1,605 | 1.05 |
| Reach-11 | 9.156 | 1,604 | 1.05 |
| Subbasin-15 | 0.498 | 143 | 1 |
| Junction-12 | 9.654 | 1,636 | 1.05 |
| Reach-12 | 9.654 | 1,634 | 1.05 |

| 5-Year, 24-Hour Storm | | | |
|-----------------------|------------|-----------|--------|
| | | Peak | |
| Hydrologic | Drainage | Discharge | Volume |
| Element | Area (mi²) | (CFS) | (in) |
| Subbasin-16 | 0.819 | 193 | 1.06 |
| Subbasin-17 | 0.788 | 184 | 0.95 |
| Junction-13 | 11.261 | 1,730 | 1.04 |
| Reach-13 | 11.261 | 1,705 | 1.04 |
| Subbasin-18 | 0.192 | 55 | 0.95 |
| Junction-14 | 11.453 | 1,711 | 1.04 |
| Reach-14 | 11.453 | 1,710 | 1.04 |
| Subbasin-19 | 0.552 | 101 | 0.95 |
| Junction-15 | 12.005 | 1,745 | 1.03 |
| Reach-15 | 12.005 | 1,741 | 1.03 |
| Subbasin-20 | 0,594 | 134 | 0.86 |
| Junction-16 | 12.599 | 1,760 | 1.03 |
| Reach-16 | 12.599 | 1,741 | 1.03 |
| Subbasin-21 | 0.417 | 100 | 0.79 |
| Junction-17 | 13.016 | 1,752 | 1.02 |
| Reach-17 | 13.016 | 1,752 | 1.02 |
| Subbasin-22 | 0.200 | 36 | 0.59 |
| Junction-18 | 13.216 | 1,756 | 1.01 |
| Reach-18 | 13.216 | 1,746 | 1.01 |
| Subbasin-23 | 0.123 | 42 | 0.66 |
| Junction-19 | 13.339 | 1,748 | 1.01 |
| Reach-19 | 13.339 | 1,747 | 1.01 |
| Source-1 | 1.396 | 109 | 0.58 |
| Subbasin-28 | 0.264 | 38 | 0.57 |
| Subbasin-29 | 0.172 | 37 | 0.7 |
| Junction-20 | 0.436 | 75 | 0.62 |
| Reach-20 | 0.436 | 70 | 0.62 |
| Subbasin-30 | 0.364 | 116 | 1 |
| Junction-23 | 15.535 | 1,764 | 0.96 |
| Reach-23 | 15.535 | 1,751 | 0.96 |
| Subbasin-31 | 0.377 | 217 | 1.05 |
| Subbasin-32 | 0.316 | 124 | 1.01 |
| Junction-24 | 16.228 | 1,766 | 0.96 |
| Reach-24 | 16.228 | 1,754 | 0.96 |
| Subbasin-33 | 0.184 | 24 | 0.37 |
| Junction-25 | 16.412 | 1,756 | 0.96 |
| Reach-25 | 16.412 | 1,750 | 0.96 |
| Junction-26 | 16.412 | 1,750 | 0.96 |

FUTURE CONDITIONS MODEL RESULTS (5-YEAR)

| | -Year, 24-Ho | ur Storm | 1 |
|-------------|--------------|-----------|--------|
| | | Peak | |
| Hydrologic | Drainage | Discharge | Volume |
| Element | Area (mi²) | (CFS) | (in) |
| Subbasin-1 | 1.263 | 315 | 1.06 |
| Subbasin-2 | 0.586 | 173 | 1.06 |
| Subbasin-3 | 0.180 | 56 | 1.27 |
| Junction-1 | 2.029 | 527 | 1.08 |
| Reach-1 | 2.029 | 526 | 1.08 |
| Subbasin-4 | 0.195 | 56 | 0.97 |
| Junction-2 | 2.224 | 572 | 1.07 |
| Reach-2 | 2.224 | 568 | 1.07 |
| Subbasin-5 | 0.625 | 134 | 1.14 |
| Junction-3 | 2.849 | 689 | 1.08 |
| Reach-3 | 2.849 | 689 | 1.08 |
| Subbasin-6 | 1.333 | 240 | 0.94 |
| Junction-4 | 4.182 | 928 | 1.04 |
| Reach-4 | 4.182 | 917 | 1.04 |
| Subbasin-7 | 0.183 | 51 | 0.97 |
| Junction-5 | 4.365 | 940 | 1.03 |
| Reach-5 | 4.365 | 929 | 1.03 |
| Subbasin-8 | 0.288 | 117 | 1.1 |
| Junction-6 | 4.653 | 959 | 1.04 |
| Reach-6 | 4.653 | 944 | 1.04 |
| Subbasin-9 | 1.177 | 223 | 1.05 |
| Subbasin-10 | 0.222 | 62 | 0.93 |
| Junction-7 | 1.399 | 252 | 1.03 |
| Reach-7 | 1.399 | 250 | 1.03 |
| Subbasin-11 | 0.880 | 322 | 1.23 |
| Junction-8 | 2.279 | 484 | 1.11 |
| Reach-8 | 2.279 | 484 | 1.11 |
| Subbasin-12 | 0.552 | 144 | 1.06 |
| Junction-9 | 2.831 | 609 | 1.1 |
| Reach-9 | 2.831 | 594 | 1.1 |
| Junction-10 | 7.484 | 1,444 | 1.06 |
| Reach-10 | 7.484 | 1,428 | 1.06 |
| Subbasin-13 | 1.156 | 212 | 1 |
| Subbasin-14 | 0.516 | 138 | 0.95 |
| Junction-11 | 9.156 | 1,605 | 1.05 |
| Reach-11 | 9.156 | 1,604 | 1.05 |
| Subbasin-15 | 0.498 | 143 | 1 |
| Junction-12 | 9.654 | 1,636 | 1.05 |
| Reach-12 | 9.654 | 1,634 | 1.05 |

| 5-Year, 24-Hour Storm | | | |
|-----------------------|-------------------------|-----------|--------|
| | | Peak | |
| Hydrologic | Drainage | Discharge | Volume |
| Element | Area (mi ²) | (CFS) | (in) |
| Subbasin-16 | 0.819 | 193 | 1.06 |
| Subbasin-17 | 0.788 | 184 | 0.95 |
| Junction-13 | 11.261 | 1,730 | 1.04 |
| Reach-13 | 11.261 | 1,705 | 1.04 |
| Subbasin-18 | 0.192 | 55 | 0.95 |
| Junction-14 | 11.453 | 1,711 | 1.04 |
| Reach-14 | 11.453 | 1,710 | 1.04 |
| Subbasin-19 | 0.552 | 111 | 1.03 |
| Junction-15 | 12.005 | 1,747 | 1.04 |
| Reach-15 | 12.005 | 1,743 | 1.04 |
| Subbasin-20 | 0.594 | 206 | 1.29 |
| Junction-16 | 12.599 | 1,769 | 1.05 |
| Reach-16 | 12.599 | 1,750 | 1.05 |
| Subbasin-21 | 0.417 | 114 | 0.9 |
| Junction-17 | 13.016 | 1,761 | 1.04 |
| Reach-17 | 13.016 | 1,761 | 1.04 |
| Subbasin-22 | 0.200 | 112 | 1.76 |
| Junction-18 | 13.216 | 1,769 | 1.06 |
| Reach-18 | 13.216 | 1,760 | 1.06 |
| Subbasin-23 | 0.123 | 44 | 0.68 |
| Junction-19 | 13.339 | 1,763 | 1.05 |
| Reach-19 | 13.339 | 1,761 | 1.05 |
| Source-1 | 1.396 | 109 | 0.58 |
| Subbasin-28 | 0.264 | 123 | 1.74 |
| Subbasin-29 | 0.172 | 111 | 2.06 |
| Junction-20 | 0.436 | 230 | 1.86 |
| Reach-20 | 0.436 | 220 | 1.86 |
| Subbasin-30 | 0.364 | 158 | 1.34 |
| Junction-23 | 15.535 | 1,788 | 1.04 |
| Reach-23 | 15.535 | 1,774 | 1.04 |
| Subbasin-31 | 0.377 | 290 | 1.38 |
| Subbasin-32 | 0.316 | 274 | 2.2 |
| Junction-24 | 16,228 | 1,796 | 1.07 |
| Reach-24 | 16.228 | 1,785 | 1.07 |
| Subbasin-33 | 0.184 | 24 | 0.37 |
| Junction-25 | 16.412 | 1,787 | 1.06 |
| Reach-25 | 16.412 | 1,781 | 1.06 |
| Junction-26 | 16.412 | 1,781 | 1.06 |

FIGURE 3-10 HYDROLOGY MINOR STORM RESULTS KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015

NOTE

1. FUTURE AND EXISTING SUBBASIN 24-27 DATA IS REPLACED WITH DATA FROM THE KETTLE CREEK DRAINAGE BASIN OLD RANCH ROAD TRIBUTARY MASTER DEVELOPMENT DRAINAGE PLAN AND LABELED AS SOURCE-1 (S1).



HISTORIC CONDITIONS MODEL RESULTS (100-YEAR)

| 100-Year, 24-Hour Storm | | | |
|-------------------------|------------|-----------|--------|
| | | Peak | |
| Hydrologic | Drainage | Discharge | Volume |
| Element | Area (mi²) | (CFS) | (in) |
| Subbasin-1 | 1.263 | 402 | 1.31 |
| Subbasin-2 | 0.586 | 217 | 1.31 |
| Subbasin-3 | 0.180 | 60 | 1.31 |
| Junction-1 | 2.029 | 663 | 1.31 |
| Reach-1 | 2.029 | 661 | 1.31 |
| Subbasin-4 | 0.195 | 75 | 1.26 |
| Junction-2 | 2.224 | 724 | 1.31 |
| Reach-2 | 2.224 | 703 | 1.31 |
| Subbasin-5 | 0.625 | 150 | 1.27 |
| Junction-3 | 2.849 | 840 | 1.30 |
| Reach-3 | 2.849 | 840 | 1.30 |
| Subbasin-6 | 1.333 | 332 | 1.27 |
| Junction-4 | 4.182 | 1,168 | 1.29 |
| Reach-4 | 4.182 | 1,167 | 1.29 |
| Subbasin-7 | 0.183 | 71 | 1.31 |
| Junction-5 | 4.365 | 1,201 | 1.29 |
| Reach-5 | 4.365 | 1,179 | 1.29 |
| Subbasin-8 | 0.288 | 133.1 | 1.26 |
| Junction-6 | 4.653 | 1218.6 | 1.29 |
| Reach-6 | 4.653 | 1,205 | 1.29 |
| Subbasin-9 | 1.177 | 287 | 1.32 |
| Subbasin-10 | 0.222 | 87 | 1.26 |
| Junction-7 | 1.399 | 325 | 1.31 |
| Reach-7 | 1.399 | 325 | 1.31 |
| Subbasin-11 | 0.880 | 332 | 1.26 |
| Junction-8 | 2.279 | 556 | 1.29 |
| Reach-8 | 2.279 | 540 | 1.29 |
| Subbasin-12 | 0.552 | 184 | 1.32 |
| Junction-9 | 2.831 | 704 | 1.30 |
| Reach-9 | 2.831 | 694 | 1.30 |
| Junction-10 | 7.484 | 1,793 | 1.29 |
| Reach-10 | 7.484 | 1,788 | 1.29 |
| Subbasin-13 | 1.156 | 285 | 1.31 |
| Subbasin-14 | 0.516 | 207 | 1.37 |
| Junction-11 | 9.156 | 2,036 | 1.30 |
| Reach-11 | 9.156 | 2,022 | 1.30 |
| Subbasin-15 | 0.498 | 201 | 1.36 |
| Junction-12 | 9.654 | 2,064 | 1.30 |
| Reach-12 | 9.654 | 2,055 | 1.30 |
| Subbasin-16 | 0.819 | 241 | 1.31 |
| Subbasin-17 | 0.788 | 264 | 1.31 |
| Junction-13 | 11.261 | 2,194 | 1.30 |
| Junearon 13 | 11.201 | 2,157 | 1.50 |

| 100-Year, 24-Hour Storm | | | |
|-------------------------|------------|-----------|--------|
| | | Peak | |
| Hydrologic | Drainage | Discharge | Volume |
| Element | Area (mi²) | (CFS) | (in) |
| Reach-13 | 11.261 | 2,185 | 1.30 |
| Subbasin-18 | 0.192 | 80 | 1.32 |
| Junction-14 | 11.453 | 2,196 | 1.30 |
| Reach-14 | 11.453 | 2,176 | 1.30 |
| Subbasin-19 | 0.552 | 157 | 1.41 |
| Junction-15 | 12.005 | 2,234 | 1.31 |
| Reach-15 | 12.005 | 2,232 | 1.31 |
| Subbasin-20 | 0.594 | 244 | 1.48 |
| Junction-16 | 12.599 | 2,269 | 1.32 |
| Reach-16 | 12.599 | 2,255 | 1.32 |
| Subbasin-21 | 0.417 | 207 | 1.53 |
| Junction-17 | 13.016 | 2,276 | 1.32 |
| Reach-17 | 13.016 | 2,271 | 1.32 |
| Subbasin-22 | 0.200 | 107 | 1.63 |
| Junction-18 | 13.216 | 2,281 | 1.33 |
| Reach-18 | 13.216 | 2,254 | 1.33 |
| Subbasin-23 | 0.123 | 109 | 1.58 |
| Junction-19 | 13.339 | 2,259 | 1.33 |
| Reach-19 | 13.339 | 2,253 | 1.33 |
| Subbasin-24 | 0.453 | 166 | 1.63 |
| Subbasin-25 | 0.169 | 159 | 1.63 |
| Subbasin-26 | 0.480 | 199 | 1.63 |
| Junction-21 | 1.102 | 395 | 1.63 |
| Reach-21 | 1.102 | 387 | 1.63 |
| Subbasin-27 | 0.294 | 157 | 1.63 |
| Junction-22 | 1.396 | 505 | 1.63 |
| Reach-22 | 1.396 | 505 | 1.63 |
| Subbasin-28 | 0.264 | 120 | 1.63 |
| Subbasin-29 | 0.172 | 92 | 1.63 |
| Junction-20 | 0.436 | 212 | 1.63 |
| Reach-20 | 0.436 | 197 | 1.63 |
| Subbasin-30 | 0.364 | 200 | 1.63 |
| Junction-23 | 15.535 | 2,362 | 1.37 |
| Reach-23 | 15.535 | 2,358 | 1.37 |
| Subbasin-31 | 0.377 | 241 | 1.12 |
| Subbasin-32 | 0.316 | 147 | 1.12 |
| Junction-24 | 16.228 | 2,381 | 1.36 |
| Reach-24 | 16.228 | 2,357 | 1.36 |
| Subbasin-33 | 0.184 | 93 | 1.21 |
| Junction-25 | 16.412 | 2,362 | 1.36 |
| Reach-25 | 16.412 | 2,357 | 1.36 |
| Junction-26 | 16.412 | 2,357 | 1.36 |

EXISTING CONDITIONS MODEL RESULTS (100-YEAR)

| 100-Year, 24-Hour Storm | | | |
|-------------------------|-------------------------|-----------|--------------------|
| | 1011,2411 | Peak | Ι |
| Hydrologic | Drainage | Discharge | Volume |
| Element | Area (mi ²) | (CFS) | (in) |
| Subbasin-1 | | | - ' ' - |
| | 1.263 | 735 | 2.36 |
| Subbasin-2 | 0.586 | 403 | 2.37 |
| Subbasin-3 | 0.180 | 122 | 2.67 |
| Junction-1 | 2.029 | 1,217 | 2.39 |
| Reach-1 | 2.029 | 1,216 | 2.39 |
| Subbasin-4 | 0.195 | 135 | 2.22 |
| Junction-2 | 2.224 | 1,325 | 2.38 |
| Reach-2 | 2.224 | 1,322 | 2.38 |
| Subbasin-5 | 0.625 | 308 | 2.52 |
| Junction-3 | 2.849 | 1,602 | 2.41 |
| Reach-3 | 2.849 | 1,602 | 2.41 |
| Subbasin-6 | 1.333 | 588 | 2.18 |
| Junction-4 | 4.182 | 2,190 | 2.34 |
| Reach-4 | 4.182 | 2,153 | 2.34 |
| Subbasin-7 | 0.183 | 125 | 2.24 |
| Junction-5 | 4.365 | 2,208 | 2.33 |
| Reach-5 | 4.365 | 2,186 | 2.33 |
| Subbasin-8 | 0.288 | 273.3 | 2.48 |
| Junction-6 | 4.653 | 2253.3 | 2.34 |
| Reach-6 | 4.653 | 2,213 | 2.34 |
| Subbasin-9 | 1.177 | 520 | 2.35 |
| Subbasin-10 | 0.222 | 152 | 2.17 |
| Junction-7 | 1.399 | 593 | 2.32 |
| Reach-7 | 1.399 | 588 | 2.32 |
| Subbasin-11 | 0.880 | 720 | 2.66 |
| Junction-8 | 2.279 | 1,114 | 2.45 |
| Reach-8 | 2.279 | 1,112 | 2.45 |
| Subbasin-12 | 0.552 | 338 | 2.39 |
| Junction-9 | 2.831 | 1,403 | 2.44 |
| Reach-9 | 2.831 | 1,368 | 2.44 |
| Junction-10 | 7.484 | 3,375 | 2.38 |
| Reach-10 | 7.484 | 3,329 | 2.38 |
| Subbasin-13 | 1.156 | 505 | 2.28 |
| Subbasin-14 | 0.516 | 337 | 2.20 |
| Junction-11 | 9.156 | 3,761 | 2.36 |
| Reach-11 | 9.156 | 3,756 | 2.36 |
| Subbasin-15 | 0.498 | 342 | 2.28 |
| Junction-12 | 9.654 | 3,828 | 2.35 |
| Reach-12 | 9.654 | 3,823 | 2.35 |

| 100-Year, 24-Hour Storm | | | |
|-------------------------|------------|-----------|--------|
| | | Peak | |
| Hydrologic | Drainage | Discharge | Volume |
| Élement | Area (mi²) | (CFS) | (in) |
| Subbasin-16 | 0.819 | 449 | 2.37 |
| Subbasin-17 | 0.788 | 447 | 2.20 |
| Junction-13 | 11.261 | 4,038 | 2.34 |
| Reach-13 | 11.261 | 3,975 | 2.34 |
| Subbasin-18 | 0.192 | 134.1 | 2.2 |
| Junction-14 | 11.453 | 3,992 | 2.34 |
| Reach-14 | 11.453 | 3,987 | 2.34 |
| Subbasin-19 | 0.552 | 248 | 2.19 |
| Junction-15 | 12.005 | 4,069 | 2.33 |
| Reach-15 | 12.005 | 4,058 | 2.33 |
| Subbasin-20 | 0.594 | 343 | 2.06 |
| Junction-16 | 12.599 | 4,103 | 2.32 |
| Reach-16 | 12.599 | 4,064 | 2.32 |
| Subbasin-21 | 0.417 | 264 | 1.96 |
| Junction-17 | 13.016 | 4,091 | 2.31 |
| Reach-17 | 13.016 | 4,081 | 2.31 |
| Subbasin-22 | 0.200 | 109 | 1.66 |
| Junction-18 | 13.216 | 4,091 | 2.30 |
| Reach-18 | 13.216 | 4,080 | 2.30 |
| Subbasin-23 | 0.123 | 121 | 1.75 |
| Junction-19 | 13.339 | 4,086 | 2.29 |
| Reach-19 | 13.339 | 4,081 | 2.29 |
| Source-1 | 1.396 | 576 | 1.58 |
| Subbasin-28 | 0.264 | 120 | 1.63 |
| Subbasin-29 | 0.172 | 102 | 1.83 |
| Junction-20 | 0.436 | 222 | 1.71 |
| Reach-20 | 0.436 | 207 | 1.71 |
| Subbasin-30 | 0.364 | 279 | 2.28 |
| Junction-23 | 15.535 | 4,121 | 2.21 |
| Reach-23 | 15.535 | 4,081 | 2.21 |
| Subbasin-31 | 0.377 | 490 | 2.26 |
| Subbasin-32 | 0.316 | 289 | 2.22 |
| Junction-24 | 16.228 | 4,114 | 2.22 |
| Reach-24 | 16.228 | 4,096 | 2.22 |
| Subbasin-33 | 0.184 | 93 | 1.21 |
| Junction-25 | 16.412 | 4,102 | 2.20 |
| Reach-25 | 16.412 | 4,084 | 2.20 |
| | | | |

FUTURE CONDITIONS MODEL RESULTS (100-YEAR)

| 100-Year, 24-Hour Storm | | | |
|-------------------------|------------|-----------|-------|
| | | Peak | |
| Hydrologic | Drainage | Discharge | Volum |
| Element | Area (mi²) | (CFS) | (in) |
| Subbasin-1 | 1.263 | 735 | 2.36 |
| Subbasin-2 | 0.586 | 403 | 2.37 |
| Subbasin-3 | 0.180 | 122 | 2.67 |
| Junction-1 | 2.029 | 1,217 | 2.39 |
| Reach-1 | 2.029 | 1,216 | 2.39 |
| Subbasin-4 | 0.195 | 135 | 2.22 |
| Junction-2 | 2.224 | 1,325 | 2.38 |
| Reach-2 | 2.224 | 1,322 | 2.38 |
| Subbasin-5 | 0.625 | 308 | 2.52 |
| Junction-3 | 2.849 | 1,602 | 2.41 |
| Reach-3 | 2.849 | 1,602 | 2.41 |
| Subbasin-6 | 1.333 | 588 | 2.18 |
| Junction-4 | 4.182 | 2,190 | 2.34 |
| Reach-4 | 4.182 | 2,153 | 2.34 |
| Subbasin-7 | 0.183 | 125 | 2.24 |
| Junction-5 | 4.365 | 2,208 | 2.33 |
| Reach-5 | 4.365 | 2,186 | 2.33 |
| Subbasin-8 | 0.288 | 273.3 | 2.48 |
| Junction-6 | 4.653 | 2253.3 | 2.34 |
| Reach-6 | 4.653 | 2,213 | 2.34 |
| Subbasin-9 | 1.177 | 520 | 2.35 |
| Subbasin-10 | 0.222 | 152 | 2.17 |
| Junction-7 | 1.399 | 593 | 2.32 |
| Reach-7 | 1.399 | 588 | 2.32 |
| Subbasin-11 | 0.880 | 720 | 2.66 |
| Junction-8 | 2.279 | 1,114 | 2.45 |
| Reach-8 | 2.279 | 1,112 | 2.45 |
| Subbasin-12 | 0.552 | 338 | 2.39 |
| Junction-9 | 2.831 | 1,403 | 2.44 |
| Reach-9 | 2.831 | 1,368 | 2.44 |
| Junction-10 | 7.484 | 3,375 | 2.38 |
| Reach-10 | 7.484 | 3,329 | 2.38 |
| Subbasin-13 | 1.156 | 505 | 2.28 |
| Subbasin-14 | 0.516 | 337 | 2.20 |
| Junction-11 | 9.156 | 3,761 | 2.36 |
| Reach-11 | 9.156 | 3,756 | 2.36 |
| Subbasin-15 | 0.498 | 342 | 2.28 |
| Junction-12 | 9.654 | 3,828 | 2.35 |
| Reach-12 | 9.654 | 3.823 | 2.35 |

| 100-Year, 24-Hour Storm | | | |
|-------------------------|------------|-----------|--------|
| | | Peak | |
| Hydrologic | Drainage | Discharge | Volume |
| Element | Area (mi²) | (CFS) | (in) |
| Subbasin-16 | 0.819 | 449 | 2.37 |
| Subbasin-17 | 0.788 | 447 | 2.20 |
| Junction-13 | 11.261 | 4,038 | 2.34 |
| Reach-13 | 11.261 | 3,975 | 2.34 |
| Subbasin-18 | 0.192 | 134.1 | 2.2 |
| Junction-14 | 11.453 | 3,992 | 2.34 |
| Reach-14 | 11.453 | 3,987 | 2.34 |
| Subbasin-19 | 0.552 | 262 | 2.32 |
| Junction-15 | 12.005 | 4,072 | 2.34 |
| Reach-15 | 12.005 | 4,061 | 2.34 |
| Subbasin-20 | 0.594 | 448 | 2.70 |
| Junction-16 | 12.599 | 4,115 | 2.36 |
| Reach-16 | 12.599 | 4,077 | 2.36 |
| Subbasin-21 | 0.417 | 284 | 2.12 |
| Junction-17 | 13.016 | 4,105 | 2.35 |
| Reach-17 | 13.016 | 4,093 | 2.35 |
| Subbasin-22 | 0.200 | 219 | 3.37 |
| Junction-18 | 13.216 | 4,108 | 2.37 |
| Reach-18 | 13.216 | 4,099 | 2.37 |
| Subbasin-23 | 0.123 | 124 | 1.80 |
| Junction-19 | 13.339 | 4,104 | 2.36 |
| Reach-19 | 13.339 | 4,099 | 2.36 |
| Source-1 | 1.396 | 576 | 1.58 |
| Subbasin-28 | 0.264 | 241 | 3.34 |
| Subbasin-29 | 0.172 | 207 | 3.78 |
| Junction-20 | 0.436 | 439 | 3.51 |
| Reach-20 | 0.436 | 421 | 3.51 |
| Subbasin-30 | 0.364 | 340 | 2.78 |
| Junction-23 | 15.535 | 4,152 | 2.33 |
| Reach-23 | 15.535 | 4,110 | 2.33 |
| Subbasin-31 | 0.377 | 606 | 2.79 |
| Subbasin-32 | 0.316 | 500 | 3.98 |
| Junction-24 | 16.228 | 4,152 | 2.38 |
| Reach-24 | 16.228 | 4,137 | 2.38 |
| Subbasin-33 | 0.184 | 93 | 1.21 |
| Junction-25 | 16.412 | 4,142 | 2.36 |
| Reach-25 | 16.412 | 4,123 | 2.36 |
| Junction-26 | 16.412 | 4,123 | 2.36 |

FIGURE 3-11 HYDROLOGY MAJOR STORM RESULTS KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015

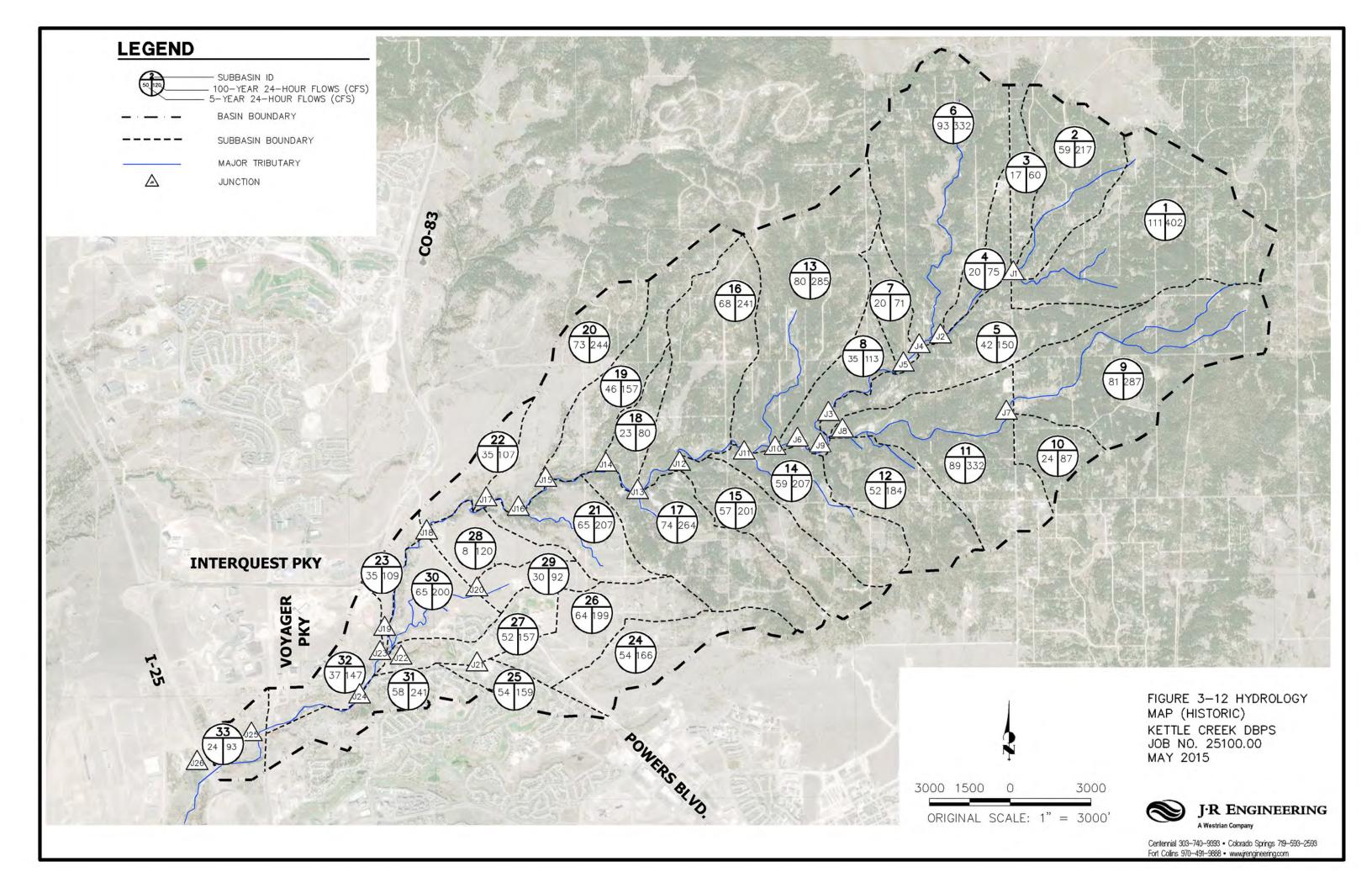
NOTE

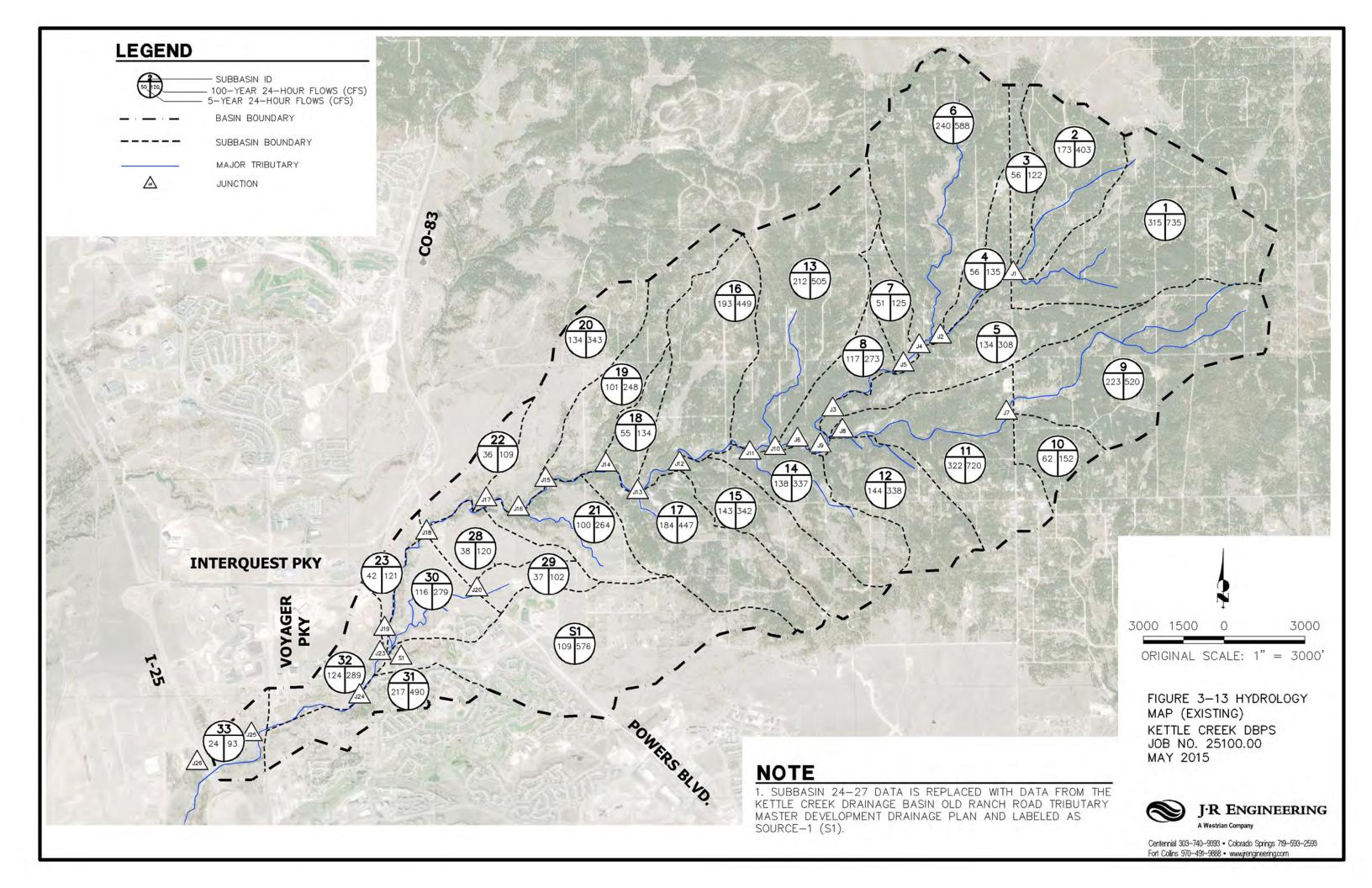
4,084 2.20

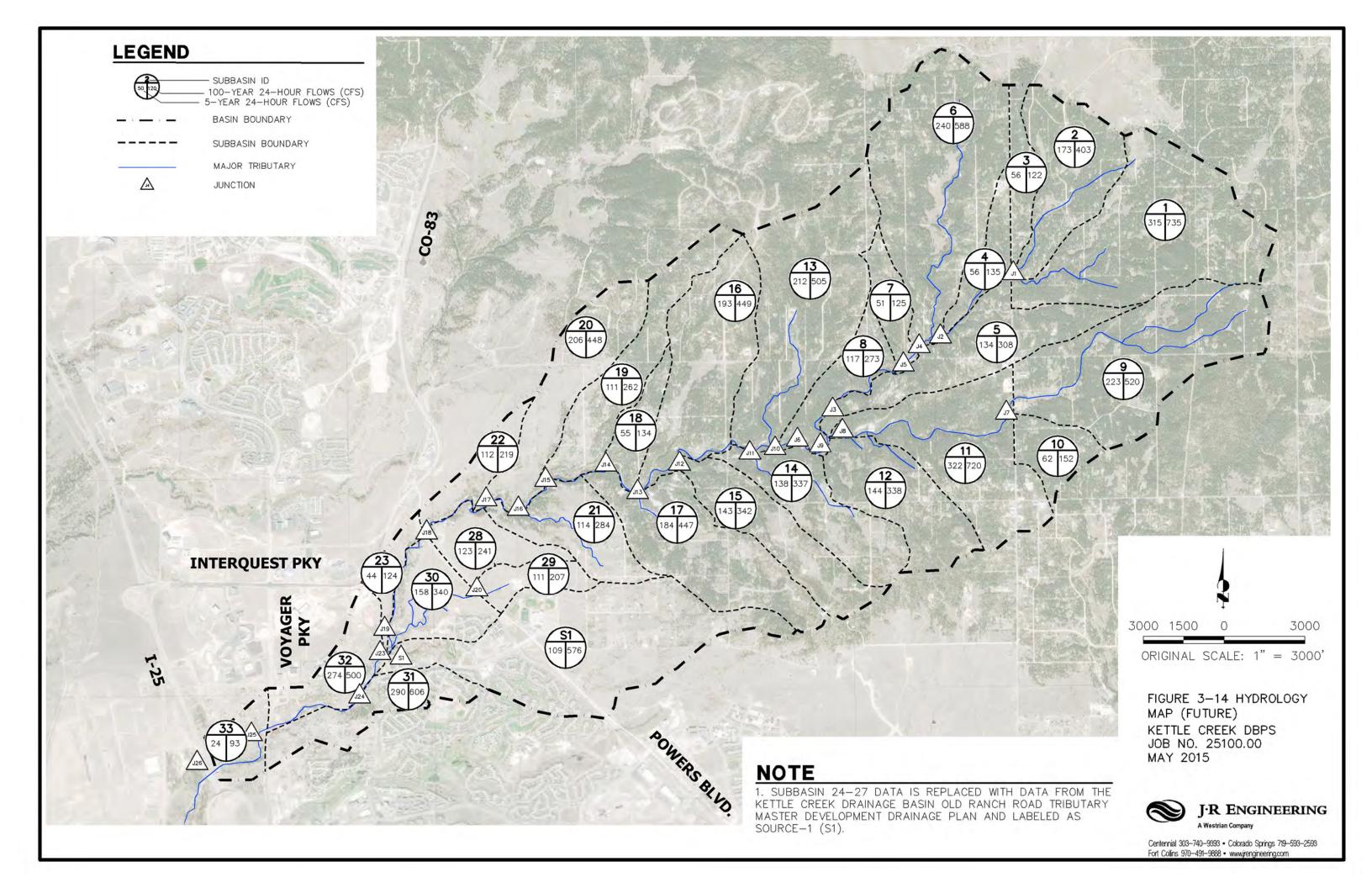
Junction-26 16.412

1. FUTURE AND EXISTING SUBBASIN 24-27 DATA IS REPLACED WITH DATA FROM THE KETTLE CREEK DRAINAGE BASIN OLD RANCH ROAD TRIBUTARY MASTER DEVELOPMENT DRAINAGE PLAN AND LABELED AS SOURCE-1 (S1).









4 HYDRAULIC ANALYSIS

4.1 Major Drainageways

A hydraulic analysis was undertaken to evaluate the distribution of flow, determine areas covered by water during flooding events, and related characteristics of the water flow in the channel and overbank areas along Kettle Creek. While the hydrologic computations define the rate of flow for floods of selected frequencies at various points within the drainage basin, the hydraulic computations reflect dynamic conditions of the water flowing downstream as affected by the channel size, subsurface roughness, structures along the channel, channel vegetation, and similar physical characteristics. The physical characteristics of Kettle Creek and its tributaries in combination with the peak flood discharge rates described in Section 3 of this report provide the primary input characteristics to the hydraulic analysis, and the basis for evaluating the hydraulic adequacy of the outfall system.

Kettle Creek and its tributaries in the Black Forest area are defined in many places by deep channels with steep side slopes. A field investigation was conducted throughout the lower portion of the drainage basin, which will be the segment primarily affected by future development. It is understood that little future development is expected to occur in the Black Forest.

A field investigation was conducted from Powers Boulevard to I-25 in August 2014. The site investigation established a basis to define any areas in need of improvements, and determine the adequacy of the assumed channel characteristics and existing structures in this area. The visit also identified some areas where stream bank and bed erosion exists in the lower portion of the basin, and where other physical problems have resulted due to the stream hydraulics. Some of these areas are presented in **Appendix D** with photos taken in August 2014.

4.2 Methodology

Hydraulic calculations were performed on Kettle Creek to determine the existing and future floodplain limits. This was accomplished by utilizing the U.S. Army Corps of Engineer's HEC-RAS River Analysis System program (version 4.1.0, January 2010). For this study, Kettle Creek was divided into separate reaches corresponding to the designations as shown on **Figure 3-2**, and described in Section 3 of this report. The delineated historic, existing and future floodplain boundaries can be seen on the work maps, **Figures 4-1** and **4-2**, and the depths are depicted on the profile sheets included as **Figure 4-3** through **Figure 4-7**.

4.2.1 Parameters

Hydraulic analyses for existing and future hydrologic conditions were completed for the main stem of Kettle Creek from Howells Road to I-25. These analyses were completed to represent peak flows for the flood events with 2-, 5-, 10-, 25-, 50- and 100-year recurrence intervals. Cross-section topography data was obtained from a triangulated irregular network (TIN) in AutoCAD that was created from the contour information obtained from City of Colorado Springs FIMS topographic data.

4.2.2 Structures

Bridges and ineffective flow areas were added to the HEC-RAS model. Physical parameters for measured structures were incorporated into the hydraulic model using HEC-RAS bridge and cross-section data editors. All of the drainageway crossings from Powers Boulevard to I-25 were modeled to represent existing conditions which consist of bridges over Kettle Creek. These crossings are located at Powers Boulevard (bridge), Old Ranch Road (bridge), Otero Avenue (bridge), and Voyager Parkway (State Highway 83) (bridge).

4.2.3 Reaches

The reach analyzed consists of the Kettle Creek main stem from Howells Road (approximate, Howells Road does not cross Kettle Creek) to the Kettle Creek Detention Facility just east of I-25, approximately 24,850 linear feet or 4.7 miles of channel. This downstream limit extends 3,000 feet past the FIS and FEMA FIRM maps. The upstream limit of model was taken to be the approximate limit of significant planned future development at the east city limits. Upstream of Howells Road is the Black Forest (El Paso County jurisdiction), where land use is expected to remain unchanged in the future. The downstream limit was taken to be the embankment of the regional detention pond at I-25. Information from the U.S. Air Force Academy Kettle Creek Watershed Hydrology Study (April 2002) was used to determine the water surface elevations of the Kettle Creek detention facility for each respective storm recurrence interval.

The main stem of Kettle Creek in the subject reach is defined by a deeply incised main channel with heavy brush and wetland-type vegetation. Above the banks of the main channel, overbanks exist within the Kettle Creek drainageway with steep side slopes and natural grasses and sparse scrub vegetation.

4.2.4 Manning's *n* Values

The Manning's n values were applied across the channel cross-section to reflect changes in vegetative cover between the main channel and overbank areas. Manning's n values were obtained from the Major Drainage chapter of the UDFCD Drainage Criteria Manual. The Manning's n values for the channels and floodplains are summarized in Table 4-1.

Table 4-1 Manning's *n* Values

| • | | | | | | |
|-----------------------|------------|------------|------------|--|--|--|
| | Historic | Existing | Future | | | |
| Parameter | Conditions | Conditions | Conditions | | | |
| Main Channel <i>n</i> | 0.100 | 0.100 | 0.100 | | | |
| Overbank n | 0.030 | 0.030 | 0.030 | | | |

The Manning's n for the main channel was selected for "very weedy reaches, deep pools, or floodways with heavy stand of timber and underbrush". Manning's n values for the overbank areas reflect conditions of

"clean, straight, full stage, no rifts or deep pools". The channel characteristics are assumed to remain consistent through all stages of development.

4.2.5 Cross-Sections

A total of 44 cross-sections were modeled along the reach, with cross-sections located at geometry changes and downstream of all crossings. Channel cross-section locations were manually selected to represent confluences, changes in channel geometry and slope. Each cross-section was adjusted to extend across the estimated floodplain and was placed perpendicular to the anticipated direction of flow in both the main channel and left/right floodplains. The cross-sections were bent in some locations to accomplish the requirement to lie perpendicular to the flow path as described in Chapter 3 of HEC-RAS Hydraulic Reference Manual.

There are existing bridges over Kettle Creek located at Powers Boulevard, Old Ranch Road, Otero Avenue, and Voyager Parkway (State Highway 83). At each of these locations, four cross-sections were added to the HEC-RAS model that included an upstream cross-section prior to flow contraction, a cross-section at the upstream face of the structure, a cross-section at the downstream face of the structure, and a downstream cross-section where flow is fully expanded. Pier location and dimensions and deck elevations were roughly measured in the field. Photos are included in **Appendix D**.

The cross sections generated from the surface TIN in AutoCAD Civil 3D may potentially represent the top of the vegetated surface and not necessarily the true channel invert. In locations where vegetation is sparse, and not deep, the channel invert is assumed to be accurately represented. In locations of dense and deep vegetative cover, the channel invert may not be accurately represented and could be shallower that what actually exists. This condition may result in cross sections with less flood capacity than actually exists and leads to a conservative estimation of floodplain widths.

Several non-critical model warnings were generated during model runs. To address model warnings by either defining numerous additional cross sections or by interpolating cross sections between every defined cross section would be necessary. Neither of these solutions was determined to be necessary given the level of detail required for this study and as such were not completed.

Expansion and contraction coefficients in the cross-sections were estimated based on the ratio of expansion and contraction of the effective flow area in the floodplain occurring at cross-sections and at major drainageway crossings. For subcritical flow conditions where the change in the stream cross-section is gradual, a contraction coefficient of 0.1 and expansion coefficient of 0.3 are typically used for hydraulic modeling. The channel characteristics for the study reach justified the use of these typical values. An contraction coefficient of 0.3 and an expansion coefficient of 0.5 were used at the two upstream sections and immediate downstream section at each bridge crossing in accordance with standard practice, which reflects the energy loss resulting from increased flow contraction approaching the bridge, and increased flow expansion when leaving the bridge.

4.2.6 Ineffective Flow Areas

Ineffective flow areas are used to describe portions of a cross section in which water does not actively flow. Ineffective flow is typically used at the upstream and downstream bounding cross sections of a drainageway crossing and for a side channel with stagnant storage. All ineffective flow is considered permanent and will not become effective flow until the barrier is overtopped. Ineffective flow areas were used at major drainageway crossings only and it was assumed that channel invert irregularities are all contributing flow areas for the purposes of this study.

4.2.7 Bridges

The surface TIN was used to develop the bounding cross sections upstream and downstream of each major drainageway crossing, in addition to the approximate roadway characteristics at each crossing. The required inputs for bridge modeling include data for the deck/roadway, pier, and sloping abutments. This data was obtained from the surface topography and approximate measurements taken during the site inspection.

4.2.8 Detention Ponds

No existing detention ponds lie along the study reach except for the regional detention facility located on the upstream side of I-25. Information from the U.S. Air Force Academy Kettle Creek Watershed Hydrology Study (AFA Study) was used to determine the storage and water surface elevations of the Kettle Creek detention facility.

4.2.9 Steady Flow and Boundary Conditions

Steady flow data were entered for the study reach based on the results of the hydrologic modeling in Section 3. Steady flow data corresponding to the peak flow for flood events with recurrence intervals of 2-, 5-, 10-, 25-, 50- and 100-years for historic, existing, and future hydrologic conditions was entered for each reach at points of significant hydrologic change as determined in the hydrologic model. A summary of hydrologic flows for each tributary at different points is provided in tabular form in **Appendix B**.

The upstream boundary condition for the reach was based on the estimated normal depth of Kettle Creek based on invert slope. The downstream boundary conditions were based on water surface elevations in the I-25 regional detention pond obtained from the AFA Study. A mix of supercritical and subcritical flow conditions was evaluated. The mixed flow regime was selected to provide conservative water surface elevations while reflecting maximum velocities, in order to present the results most consistent with actual flood conditions in the channel.

4.3 Approximate Floodplains

After the HEC-RAS model analysis was complete, the 100-year water surface elevations were exported back to AutoCAD Civil 3D. Approximate floodplains for the existing and future 100-year floods were delineated for Kettle Creek and are shown in **Figures 4-1** and **4-2**. Due to negligible differences in the water surface profiles at the scale shown, the existing and future flow results are shown as one water surface profile. The FEMA floodplains for the Kettle Creek watershed are overlaid in the plan for comparison to the results of this analysis. Flood profiles for the existing and future 100-year floods are shown in **Figure 4-3** through **Figure**

4-7. The approximate floodplains and profiles were used to assess where potential drainageway crossing deficiencies exist along the major drainageways and identify areas of potential flooding.

The approximate floodplain information shown on the figures above is intended primarily for the identification of flood prone areas along the main stem of Kettle Creek and to aid in the evaluation of potential future alternatives. The approximate floodplain data contained herein is not intended to replace the information presented in the City of Colorado Springs and El Paso County Flood Insurance studies (FEMA 1999) but should be used as a planning tool for potential future drainageway development projects. The FEMA floodplain remains as the regulatory floodplain.

4.4 Drainageway Crossing Deficiencies

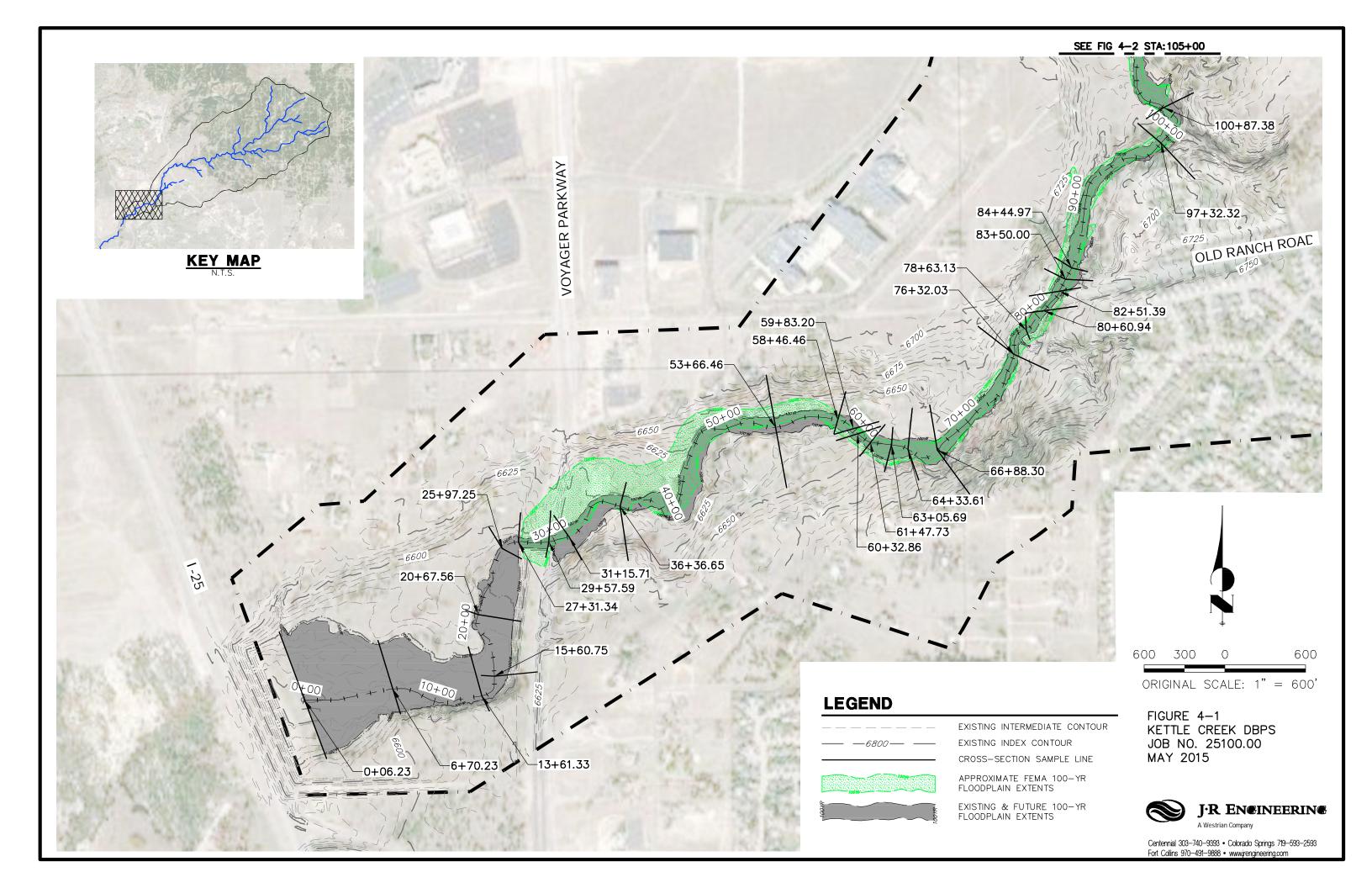
The four bridges over Kettle Creek in the hydraulic study area are sufficient based on approximate measurements of the structures during the site visit and estimates from aerial topography when compared to the calculated water surface elevation.

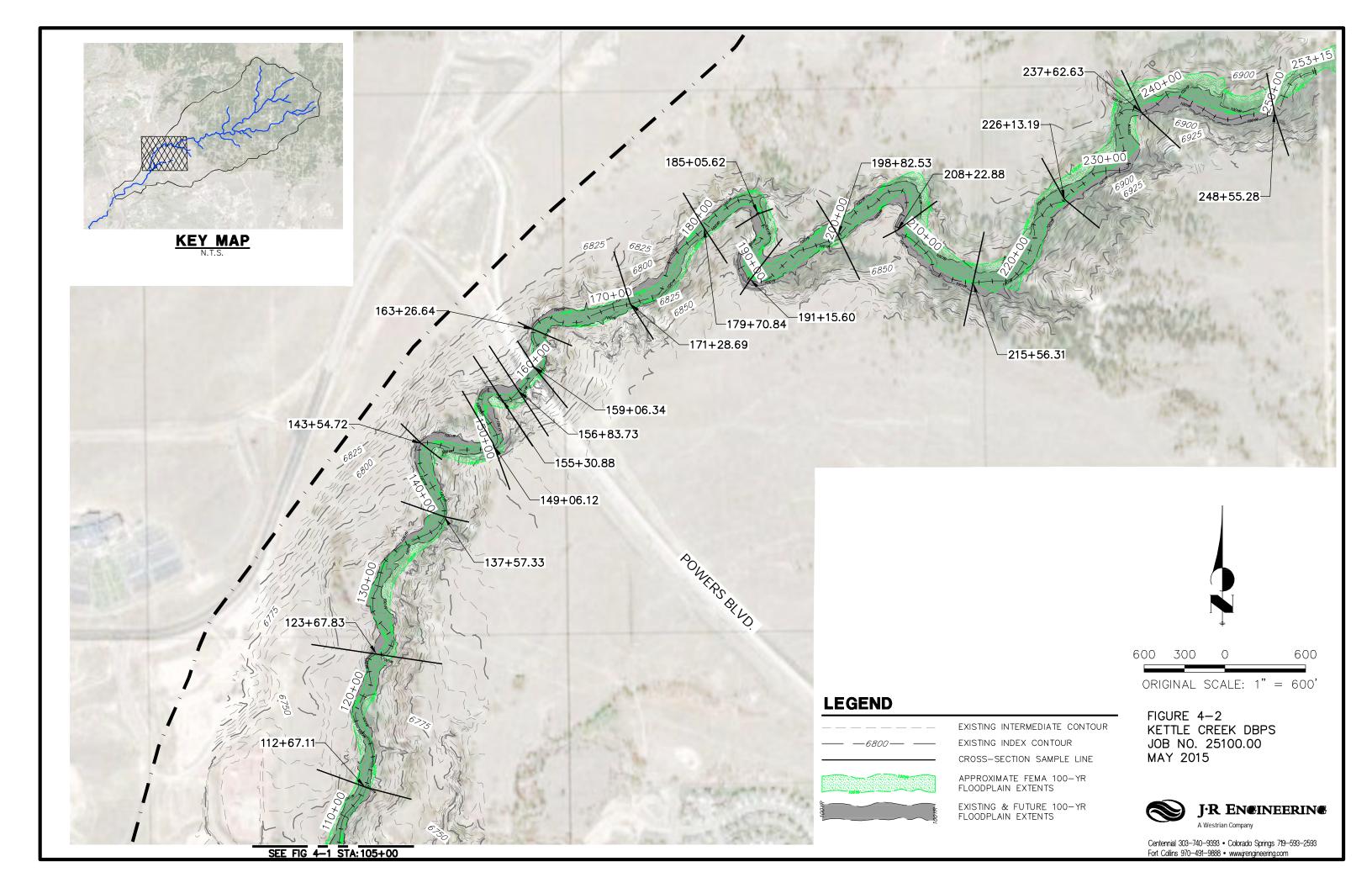
4.5 Areas of Geomorphic Instability

Several areas of erosion were located during the site visit and are noted in Appendix D. Due to the length of the reach and the heavy vegetation in the study reach, not all areas of instability may have been located.

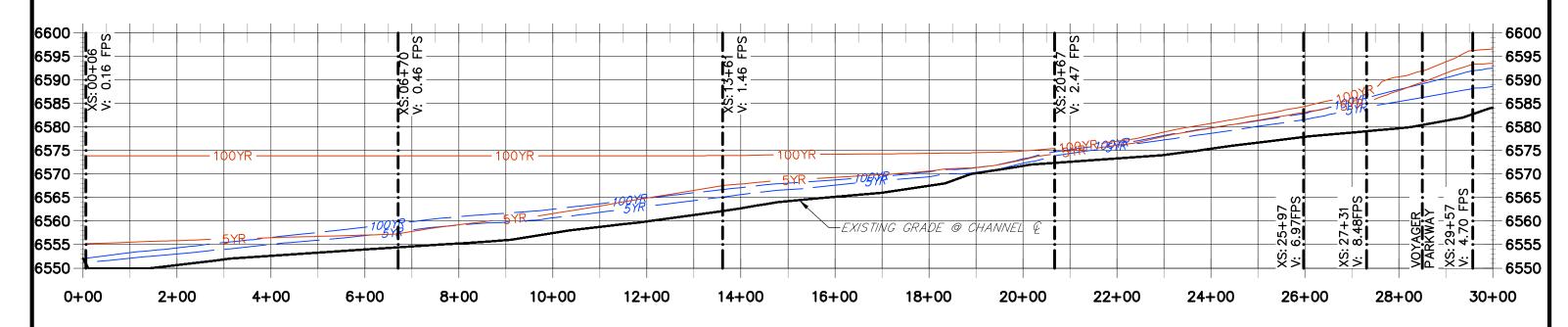
The results of the hydraulic analysis show areas where flows approach or exceed critical depth, and the fluctuation of flows between subcritical and supercritical is a known cause of channel instability. Additionally, due to the Kettle gravelly loamy sand soil type, channel velocities in these areas that exceed five feet per second may be erosive. **Figures 4-8** to **4-12** shows areas that check structures could be implemented to accomplish a stabilized channel. These structures were placed in areas where the calculated cross section velocities of future flows were greater than five feet per second. Conceptual stable channel calculations are provided in **Figure 4-12**. Due to permitting requirements and the Preble's meadow jumping mouse critical habitat along Kettle Creek, the conceptual future improvements shown herein may not be feasible in some or all areas.

Future development in the lower Kettle Creek basin should address stabilization of the main channel in further detail. It will be the responsibility of each developer to perform a geotechnical analysis and detailed hydraulic study on the channel to determine the appropriate setbacks from the channel. Environmental considerations including Preble's meadow jumping mouse critical habitat will also dictate limits of development adjacent to Kettle Creek.

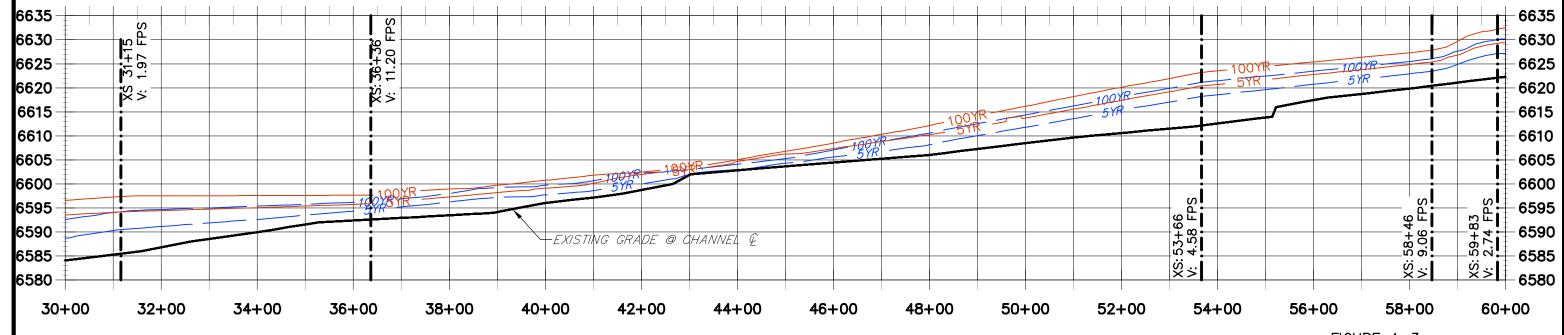








KETTLE CREEK CL ALIGNMENT (2) STA 30+00.00 TO 60+00.00

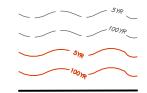


LEGNED

NOTE

1. VELOCITY SHOWN ON PROFILES ARE FUTURE FLOWS

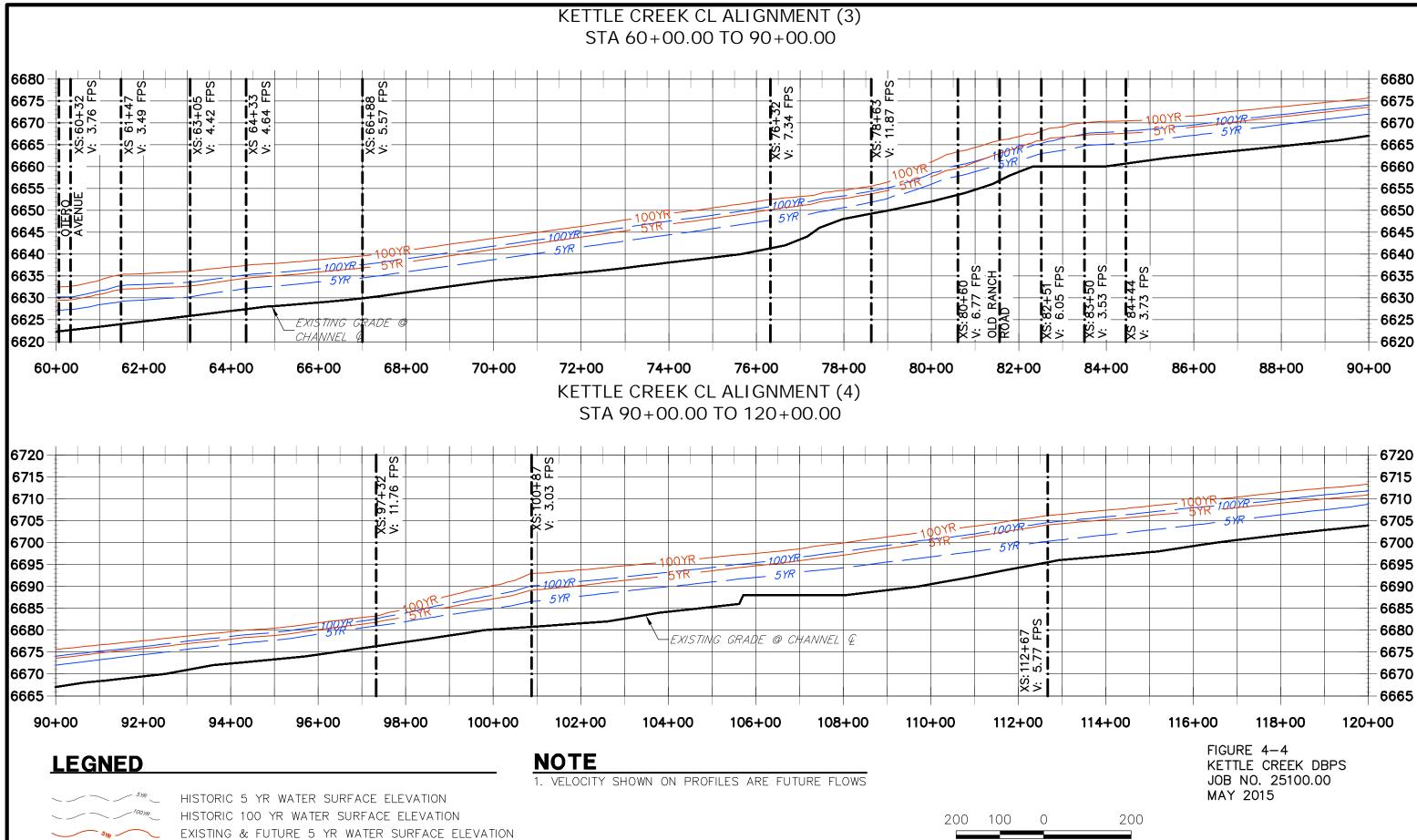
FIGURE 4-3 KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015



HISTORIC 5 YR WATER SURFACE ELEVATION
HISTORIC 100 YR WATER SURFACE ELEVATION
EXISTING & FUTURE 5 YR WATER SURFACE ELEVATION
EXISTING & FUTURE 100 YR WATER SURFACE ELEVATION
APPROXIMATE GRADE @ KETTLE CREEK \$\Phi\$







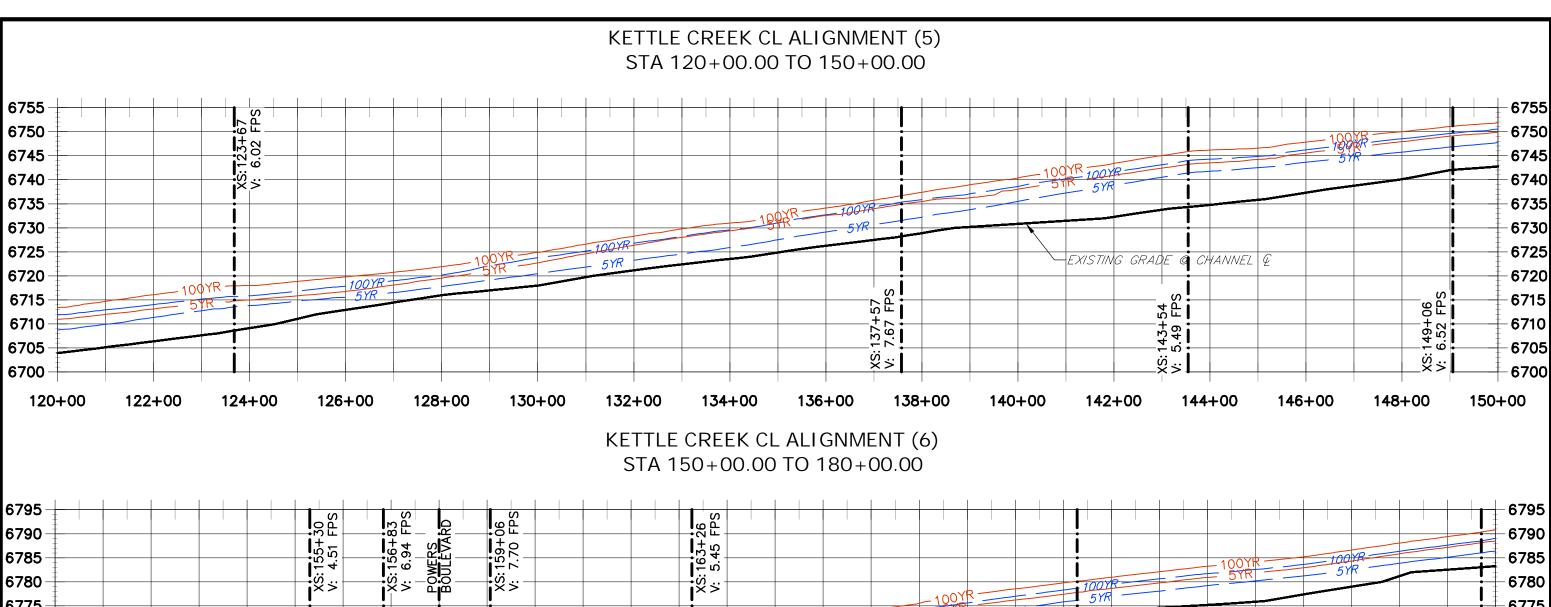
EXISTING & FUTURE 100 YR WATER SURFACE ELEVATION

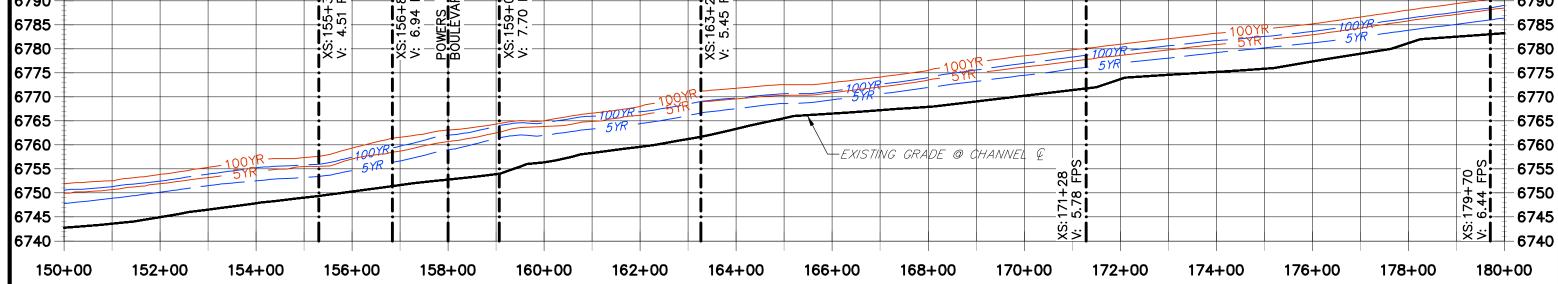
APPROXIMATE GRADE @ KETTLE CREEK &

J'R ENGINEERING

A Westrian Company

ORIGINAL SCALE: 1" = 200





LEGNED

NOTE

1. VELOCITY SHOWN ON PROFILES ARE FUTURE FLOWS

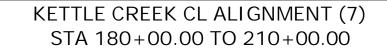
5/R 100/R

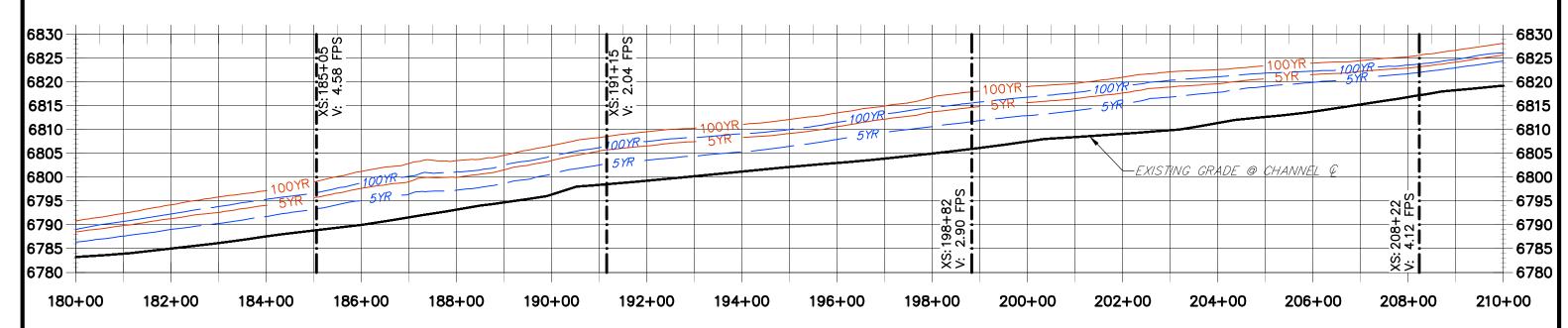
HISTORIC 5 YR WATER SURFACE ELEVATION
HISTORIC 100 YR WATER SURFACE ELEVATION
EXISTING & FUTURE 5 YR WATER SURFACE ELEVATION
EXISTING & FUTURE 100 YR WATER SURFACE ELEVATION
APPROXIMATE GRADE @ KETTLE CREEK &



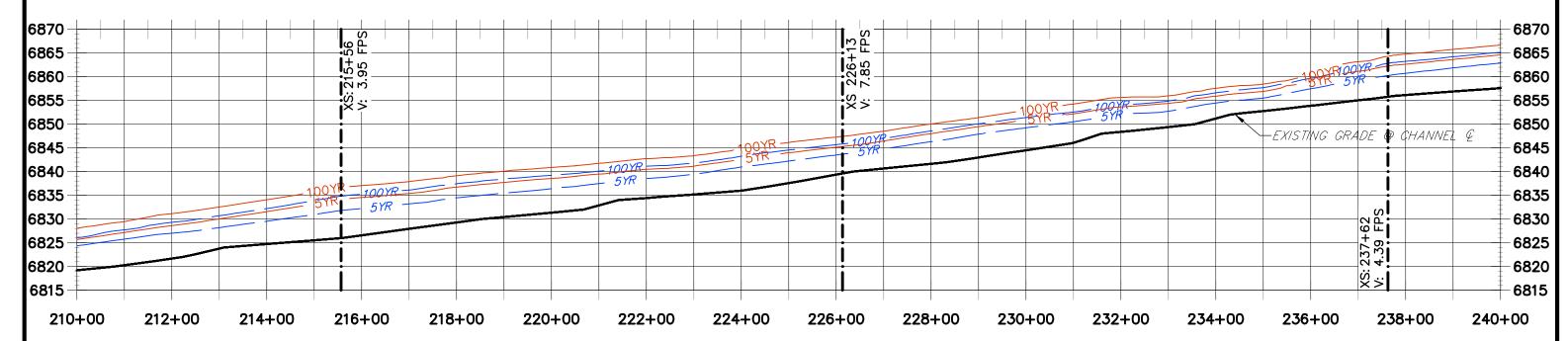
FIGURE 4-5 KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015







KETTLE CREEK CL ALIGNMENT (8) STA 210+00.00 TO 240+00.00

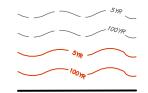


LEGNED

NOTE

1. VELOCITY SHOWN ON PROFILES ARE FUTURE FLOWS

FIGURE 4-6 KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015

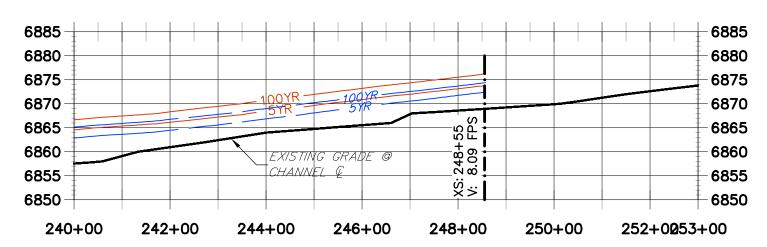


HISTORIC 5 YR WATER SURFACE ELEVATION
HISTORIC 100 YR WATER SURFACE ELEVATION
EXISTING & FUTURE 5 YR WATER SURFACE ELEVATION
EXISTING & FUTURE 100 YR WATER SURFACE ELEVATION
APPROXIMATE GRADE @ KETTLE CREEK \$\Phi\$





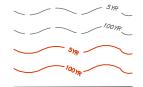
KETTLE CREEK CL ALIGNMENT (9) STA 240+00.00 TO 253+00.00



LEGNED

NOTE

1. VELOCITY SHOWN ON PROFILES ARE FUTURE FLOWS



HISTORIC 5 YR WATER SURFACE ELEVATION

HISTORIC 100 YR WATER SURFACE ELEVATION

EXISTING & FUTURE 5 YR WATER SURFACE ELEVATION

EXISTING & FUTURE 100 YR WATER SURFACE ELEVATION

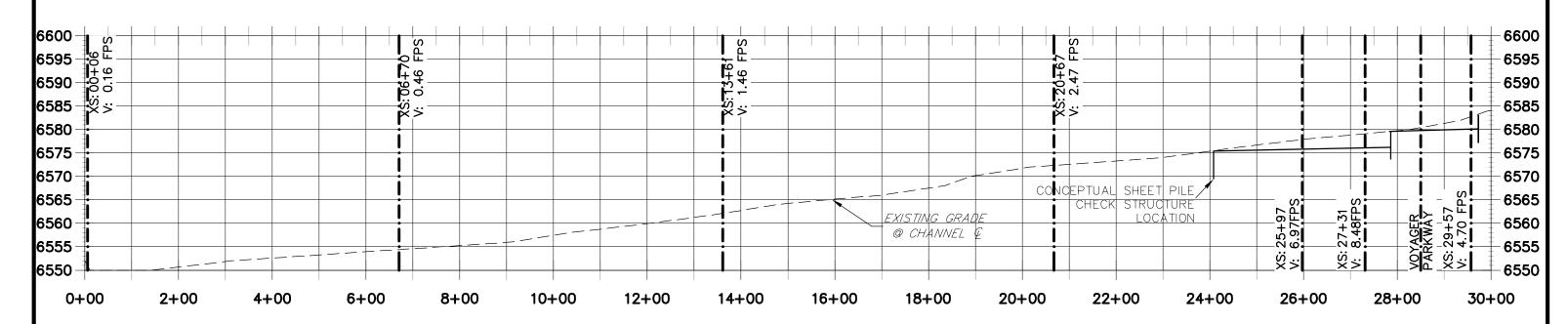
APPROXIMATE GRADE @ KETTLE CREEK &



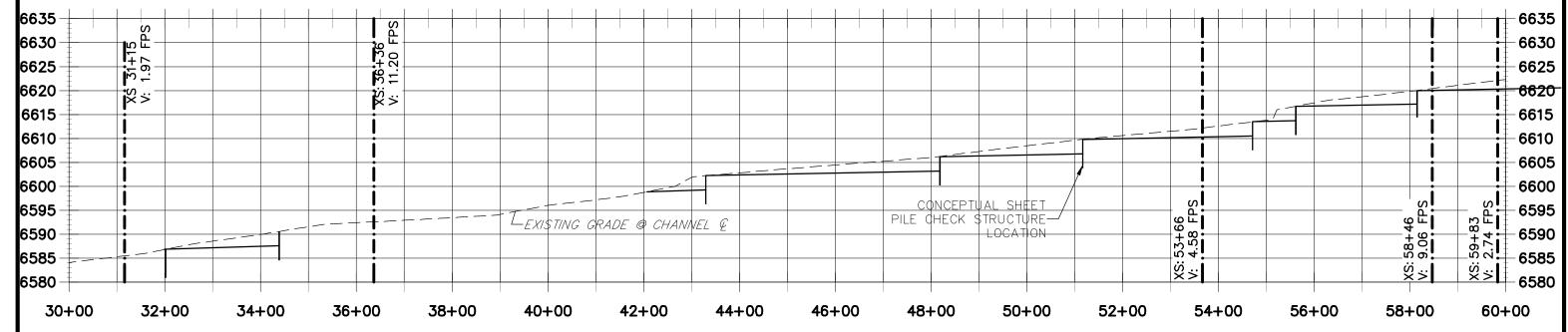
FIGURE 4-7 KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015



KETTLE CREEK CL ALIGNMENT (1) STA 0+00.00 TO 30+00.00



KETTLE CREEK CL ALIGNMENT (2) STA 30+00.00 TO 60+00.00



CONCEPTUAL CHECK STRUCTURE

EXISTING GRADE

FUTURE STABILIZED GRADE (0.20% GRADE)

<u>NOTE</u>

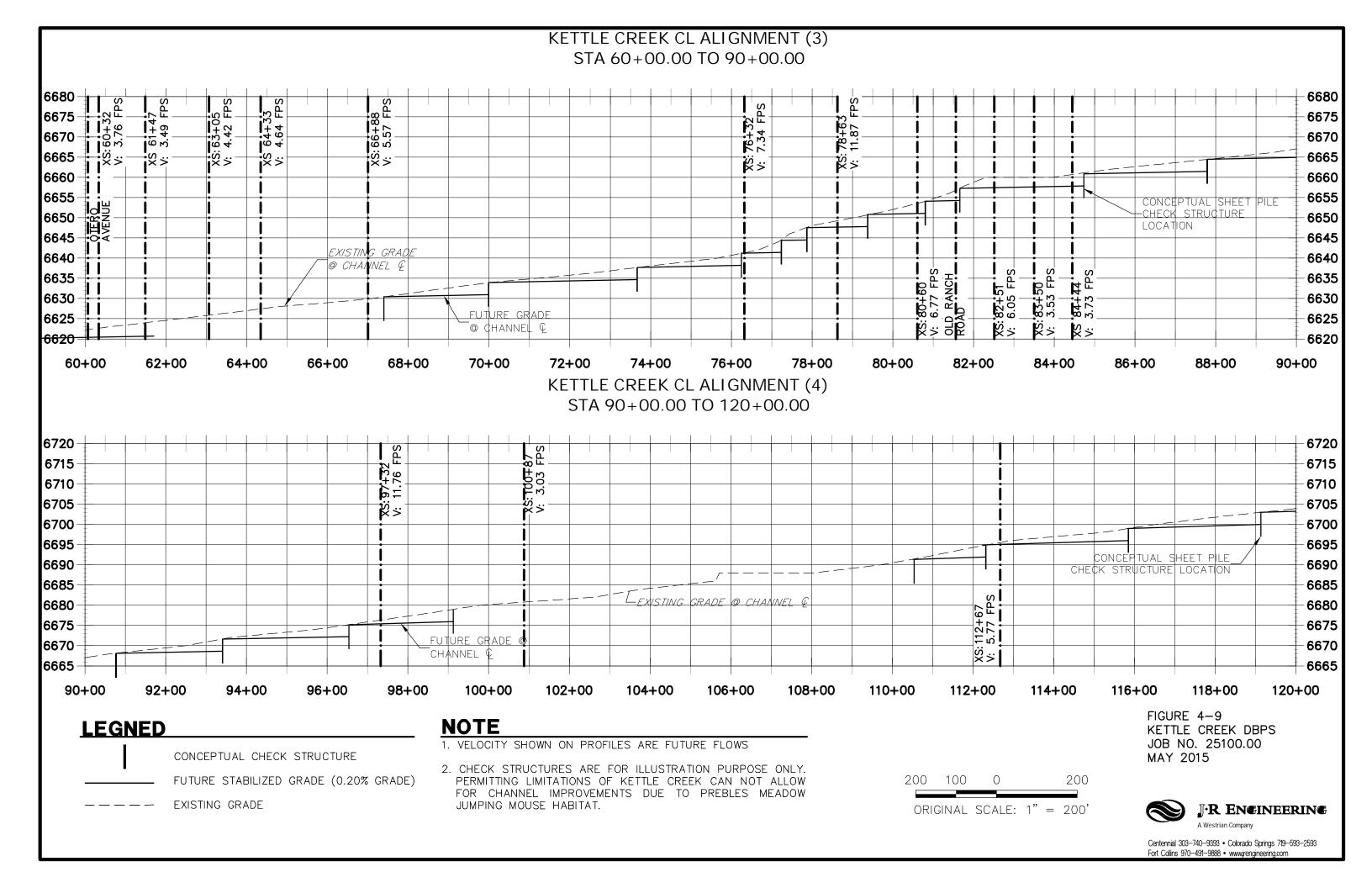
- 1. VELOCITY SHOWN ON PROFILES ARE FUTURE FLOWS
- 2. CHECK STRUCTURES ARE FOR ILLUSTRATION PURPOSE ONLY. PERMITTING LIMITATIONS OF KETTLE CREEK CAN NOT ALLOW FOR CHANNEL IMPROVEMENTS DUE TO PREBLES MEADOW JUMPING MOUSE HABITAT.

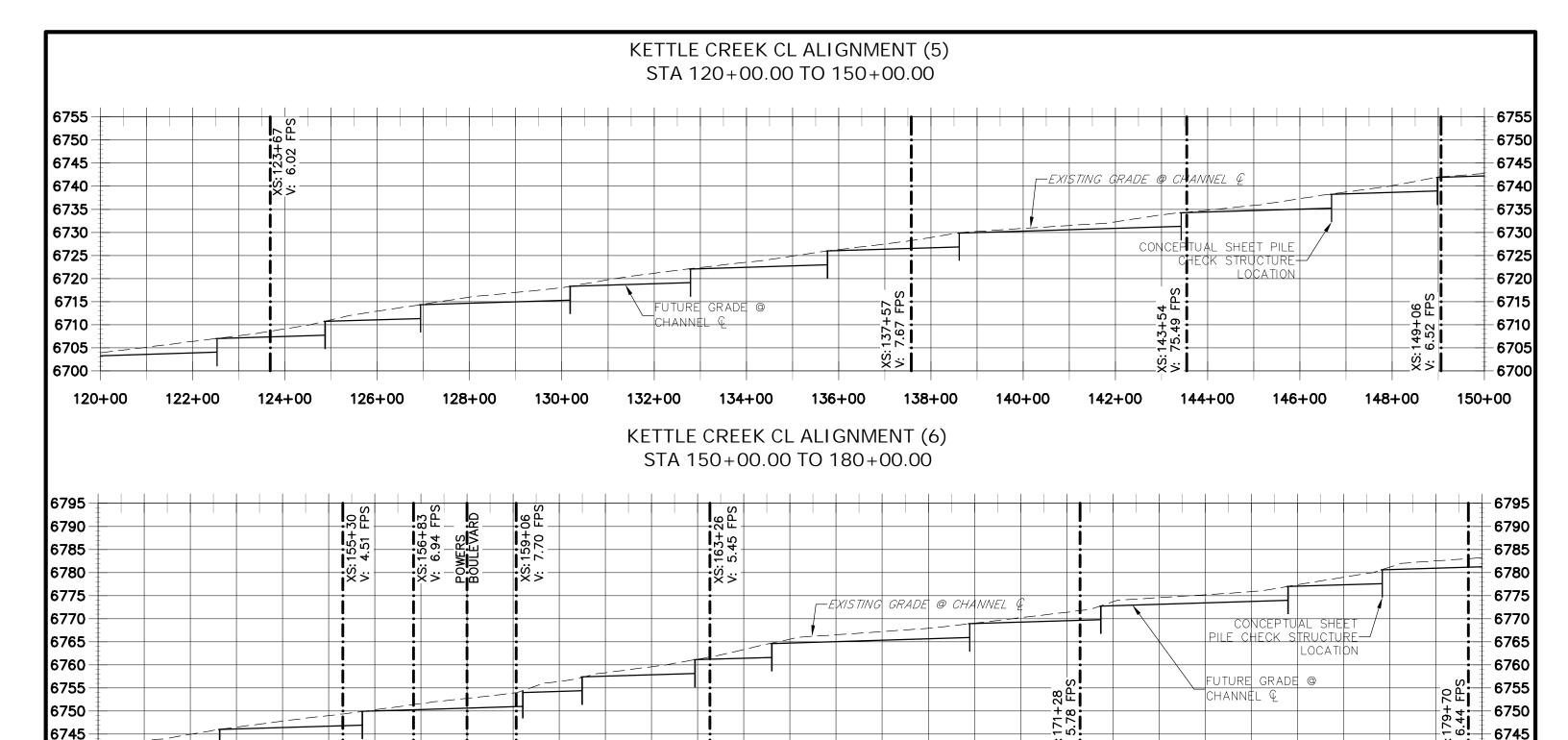
200 100 0 200

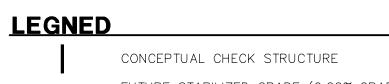
ORIGINAL SCALE: 1" = 200'

FIGURE 4-8
KETTLE CREEK DBPS
JOB NO. 25100.00
MAY 2015









154+00

FUTURE STABILIZED GRADE (0.20% GRADE)

156+00

---- Existing grade

152+00

6740

150+00

NOTE

160 + 00

158+00

1. VELOCITY SHOWN ON PROFILES ARE FUTURE FLOWS

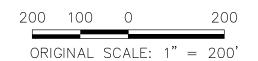
162+00

2. CHECK STRUCTURES ARE FOR ILLUSTRATION PURPOSE ONLY. PERMITTING LIMITATIONS OF KETTLE CREEK CAN NOT ALLOW FOR CHANNEL IMPROVEMENTS DUE TO PREBLES MEADOW JUMPING MOUSE HABITAT.

164+00

166+00

168+00



174+00

176+00

172+00

× × ×

170+00

FIGURE 4-10 KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015

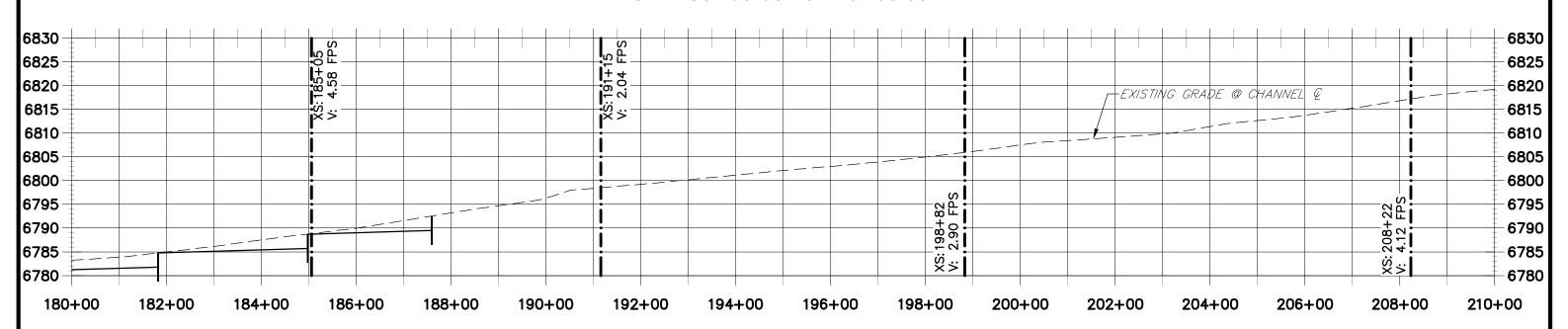
178+00



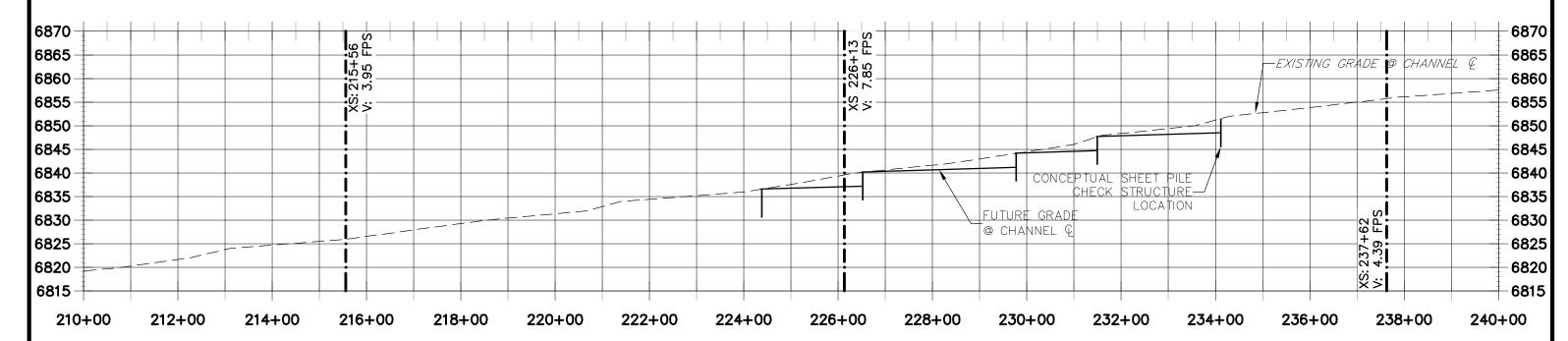
6740

180+00

KETTLE CREEK CL ALIGNMENT (7) STA 180+00.00 TO 210+00.00



KETTLE CREEK CL ALIGNMENT (8) STA 210+00.00 TO 240+00.00



LEGNED

NOTE

- 1. VELOCITY SHOWN ON PROFILES ARE FUTURE FLOWS
- 2. CHECK STRUCTURES ARE FOR ILLUSTRATION PURPOSE ONLY. PERMITTING LIMITATIONS OF KETTLE CREEK CAN NOT ALLOW FOR CHANNEL IMPROVEMENTS DUE TO PREBLES MEADOW JUMPING MOUSE HABITAT.

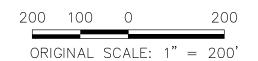


FIGURE 4-11 KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015

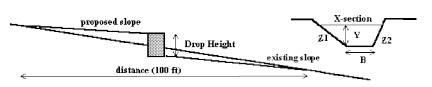


CONCEPTUAL STABLE CHANNEL TYPICAL SECTION CALCULATIONS

Design of Trapezoidal Grass-Lined Channel

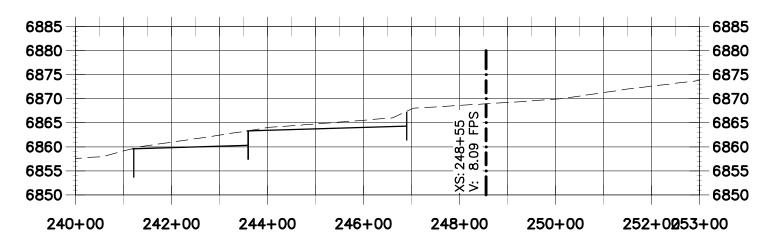
Project: Kettle Creek Drainage Basin Planning Study

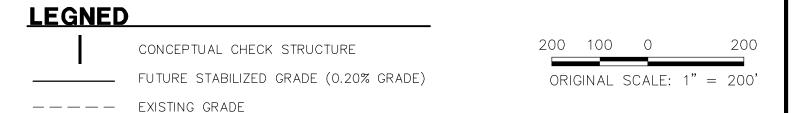
Channel ID:



| Existing Channel Condition (Input) | | | |
|--|-----------------------|----------------|----------------|
| Design Discharge | $Q_D =$ | 1199.00 cfs | |
| Design Discharge Return Period | Year _D = | 5 years | |
| Existing Ground Slope Along Channel Centerline | So = | 0.0136 ft/ft | |
| 100-Year Discharge | Q ₁₀₀ = | 4152.00 cfs | |
| Left Side Slope | Z1 = | 4.00 ft/ft | |
| Right Side Slope | Z2 = | 4.00 ft/ft | |
| Channel Manning's N (New Condition .030 typ.) | n _{new} = | 0.035 | |
| Channel Manning's N (Mature Condition .040 typ.) | n _{mature} = | 0.035 | |
| Check one of the following soil types | | | |
| | Sandy Soil | X check, Ol | R |
| N | on-Sandy Soil | check | |
| | | | |
| Proposed Channel Condition (Calculated) | | New Channel | Mature Channel |
| Bottom Width | B= | 146.08 ft | 146.08 ft |
| 100-Year Flow Depth (5' maximum) | Y ₁₀₀ = | 5,00 ft | 5.00 ft |
| 100-Year Flow Velocity | V ₁₀₀ = | 5.00 fps | 5.00 fps |
| 100-Year Top Width | T= | 186.08 ft | 186.08 ft |
| 100-Year Flow Area | A= | 830.40 sq ft | 830.40 sq ft |
| 100-Year Froude Number | Fr= | 0.42 | 0.42 |
| 100-Year Wetted Perimeter | P= | 187.31 ft | 187.31 ft |
| 100-Year Hydarulic Radius | R= | 4.43 ft | 4.43 ft |
| Design Discharge Flow Depth | Y _D = | 2.41 ft | 2.41 ft |
| Design Discharge Flow Velocity | V _D = | 3.19 fps | 3.19 fps |
| Design Discharge Top Width | T= | 165.38 ft | 165.38 ft |
| Design Discharge Flow Area | A= | 375.62 sq ft | 375.62 sq ft |
| Design Discharge Froude Number | Fr= | 0.37 | 0.37 |
| Design Discharge Wetted Perimeter | P= | 165.97 ft | 165.97 ft |
| Design Discharge Hydarulic Radius | R= | 2.26 ft | 2.26 ft |
| Drop Height | | | |
| Proposed New Channel Slope | Sd= | 0.0019 ft/ft | 0.0019 ft/ft |
| Drop Height per 100 ft | D = | 1.17 ft/100 ft | 1.17 ft/100 ft |

KETTLE CREEK CL ALIGNMENT (9) STA 240+00.00 TO 253+00.00





NOTE

- 1. VELOCITY SHOWN ON PROFILES ARE FUTURE FLOWS
- 2. CHECK STRUCTURES ARE FOR ILLUSTRATION PURPOSE ONLY. PERMITTING LIMITATIONS OF KETTLE CREEK CAN NOT ALLOW FOR CHANNEL IMPROVEMENTS DUE TO PREBLES MEADOW JUMPING MOUSE HABITAT.

FIGURE 4-12 KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015



5 ENVIRONMENTAL EVALUATIONS

5.1 Significant Existing or Potential Wetland and Riparian Areas Impact

The EPA and US Army Corps of Engineers (Corps) defines wetlands as "those areas that are inundated or saturated by surface or ground water at a frequency and duration sufficient to support, and that under normal circumstances do support, a prevalence of vegetation typically adapted for life in saturated soil conditions. Wetlands generally include swamps, marshes, bogs, and similar areas". Wetlands are areas that are covered by water or have waterlogged soils for long periods during the growing season.

Per the Colorado Division of Wildlife Wetlands Mapping Inventory, Kettle Creek from just upstream of Old Ranch Road to its confluence with Monument Creek is located in a designated Colorado Natural Heritage Program Wetland Conservation Area.

At the time of development planning in the Kettle Creek basin, a Corps Jurisdictional Determination (JD) will need to be requested by the developer to determine if jurisdictional waters of the United States or navigable waters of the United States, or both, are either present or absent on a particular site.

5.1.1 Riparian Areas

Monument Creek and several tributaries, including Kettle Creek, are reported in the <u>Survey of Critical Wetlands and Riparian Areas in El Paso and Pueblo Counties, Colorado</u>, prepared by the Colorado Natural Heritage Program of Colorado State University for the Colorado Department of Natural Resources, dated June 27, 2001. Per the report, the Monument Creek systems has a biodiversity rank of B2 (very high biodiversity significance).

Downstream of the Black Forest, the riparian vegetation is dominated by coyote willow (*Salix exigua*), peachleaf willow (*Salix amygdaloides*), and crack willow (*Salix fragilis*) with scattered stands of narrowleaf cottonwood (*Populus angustifolia*). Also found in these mesic habitats are snowberry (*Symphoricarpos occidentalis*), wild plum (*Prunus americana*), and Russian olive (*Elaeagnus angustifolia*). Stream banks retain native graminoid vegetation in the form of sedges (*Carex* spp.) and rushes (*Juncus* spp.).

Surrounding uplands are generally midgrass prairie that is composed of smooth brome (*Bromopsis inermis*), cheatgrass (*Bromus tectorum*), big bluestem (*Andropogon gerardii*), needle-and-thread (*Stipa comata*), and little blue stem (*Schizachyrium scoparium*). Ponderosa pine (*Pinus ponderosa*) and Gambel's oak (*Quercus gambelii*) occur in patches on either side of Kettle Creek and its tributaries and increase in density at higher elevations in the watershed.

5.1.2 Wildlife

Several hundred birds, mammals, reptiles and amphibians inhabit the Kettle Creek watershed either as yearround residents or seasonally; all of which contribute to the functioning ecosystem as a whole. However, some species are of greater state and federal concern and are therefore either protected or managed for conservation and sustainability. For the purpose of the environmental evaluation, wildlife species described herein were selected based on regulatory priority.

5.1.2.1 Migratory Birds

The Migratory Bird Treaty Act (MBTA) of 1918, as amended protects the majority of birds in the United States with few exceptions (invasive birds). All active wild bird nests and bird eggs are federally protected under the MBTA. It is also illegal to wound or kill any bird protected by the MBTA except for those managed under regulated hunting seasons. Migratory birds within the Kettle Creek watershed can be found nesting in wetland and riparian areas, grassland/rangelands, forests, and within urban habitats. Migratory birds include perching birds (sparrows, warblers etc.), water fowl, game birds, and raptors (birds of prey).

5.1.2.2 State and Federal Threatened and Endangered Species

The U.S. Fish and Wildlife Service lists ten species as Threatened, Endangered, or Candidate under the Endangered Species Act in El Paso County. The State of Colorado also lists several dozen species as either State Endangered, State Threatened, or State Special Concern. While not federally protected, species of State Special Concern have a higher management priority by the Colorado Division of Wildlife.

The ten species listed under the Endangered Species Act in El Paso County include the Preble's meadow jumping mouse, whooping crane, Mexican spotted owl, piping plover, least tern, greenback cutthroat trout, Pallid sturgeon, Arkansas darter, Western Prairie Fringed Orchid, and Ute-ladies' tresses orchid. Of those species, the Preble's meadow jumping mouse, Mexican spotted owl, and greenback cutthroat trout are the more likely to be encountered. The remaining species may either be found as occasional migrants or are listed for the County based on historical records.

5.1.2.3 Big Game

Big Game distribution within the Kettle Creek drainage basin includes the American black bear (*Ursus americanus*), pronghorn (*Antilocapra americana*), mule deer (*Odocoileus hemionus*), white-tailed deer (*Odocoileus virginianus*), and mountain lion (*puma concolor*). Both the mountain lion and black bear are known to occur in El Paso County and the ponderosa pine forest, riparian corridors, and forested wetlands within the Kettle Creek watershed provide suitable habitat. While it is possible for both species to follow drainages and forested areas from the mountains to the Kettle Creek watershed in search of food, their occurrence in the drainage area is likely uncommon. The drainage area has suitable habitat for elk, but their occurrence is also uncommon in the area. White-tailed deer, mule deer, and pronghorn are common both in El Paso County and within the Kettle Creek area. The construction of roads, water diversion structures, above-ground power lines, residential communities, and commercial sites impacts wildlife by fragmenting their habitat. Fragmentation can prevent animal movement or change movement patterns.

5.1.2.4 Other Significant Wildlife

The Bald and Golden Eagle Protection Act of 1940 provides further protections for eagles. While both Bald and Golden eagles are uncommon to rare in El Paso County, potentially suitable habitat does exist in the Kettle Creek watershed.

5.1.3 Preble's Meadow Jumping Mouse

The Monument Creek site supports an excellent (A-ranked) and a fair (C-ranked) occurrence of the globally and state imperiled Preble's meadow jumping mouse (*Zapus hudsonius preblei*), a species designated as sensitive, as federally threatened, and as a species of special concern. It is estimated that stresses may reduce the viability of the Preble's meadow jumping mice in the potential conservation area if protection action is not taken. Jumping mice have been documented in Kettle Creek outside of the U.S. Air Force Academy boundaries. This potential conservation area is of high significance because it is one of the best-known occurrences of Preble's meadow jumping mice in the Arkansas River drainage. The biggest threat to this conservation area is the encroachment of urban impacts.

The boundaries of the conservation area as presented in the Colorado Natural Heritage Program study were defined based on the presence of Preble's meadow jumping mice throughout the system. The boundary includes 300 meters on either side of the creek. This is designed to include the riparian vegetation and associated upland grass communities that have been documented as part of Preble's meadow jumping mouse habitat. The distance of 300 meters was intended to be conservative, likely including a greater amount of upland habitat than most mice will utilize, but sufficient to entirely cover the jumping mice habitat.

The City's Critical Habitat for the Preble's Meadow Jumping Mouse exhibit (see Appendix B) utilizes the stream width plus 120 meters (394 feet) on each side of the creek for the lower portion of Kettle Creek and tributaries, and the stream width plus 100 meters (361 feet) on each side of the creek for the middle portion of Kettle Creek (from approximately Old Ranch Road into unincorporated El Paso County). This Preble's meadow jumping mouse critical habitat width will dictate limits of development adjacent to Kettle Creek, in conjunction with the findings of geotechnical analyses and detailed hydraulic studies to be provided by each developer.

5.2 Stormwater Quality Considerations

The Colorado Department of Public Health and Environment (CDPHE) Water Quality Division has assembled a list of impaired waters in Colorado that have Total Maximum Daily Load (TMDL) restrictions for certain pollutants as required by Section 303d of the Clean Water Act. Kettle Creek is tributary to Monument Creek, which is tributary to Fountain Creek. Fountain Creek is tributary to the Arkansas River. The Arkansas River has 303d list TMDL restrictions to the state border, and Fountain Creek and Monument Creek are subject to E. coli monitoring and evaluation (CDPHE, 2012). The selenium water quality standard for Fountain Creek has a temporary modification for uncertainty. Kettle Creek and the unnamed tributaries in the Kettle Creek Watershed are not listed and, therefore, are not subject to Section 303d TMDL restrictions.

5.2.1 Hazardous Materials

A search of EPA Superfund sites and National Priorities List sites yielded no sites in the Kettle Creek watershed or in the vicinity of the watershed. Multiple facilities were listed on the EPA Facility Index System/Facility Registry System (FINDS) database in the Kettle Creek watershed, reflecting facilities which are regulated by the EPA but not necessarily in violation.

5.2.2 Water Quality

Water quality treatment shall be required for all stormwater detention basins within the City of Colorado Springs. The City will hold all development tributary to Kettle Creek to USAFA release standards.

5.3 Permitting Requirements

The portions of the Kettle Creek watershed to be developed must comply with all applicable El Paso County, and where applicable, City of Colorado Springs requirements for planning and zoning. A Permit from the Corps will be required to discharge fill or dredged material into jurisdictional waters. Additionally, due to the presence of the Preble's meadow jumping mouse, appropriate permits from the U.S. Fish and Wildlife Service may be required. Ongoing coordination with the U.S. Fish and Wildlife Service will be required to identify outfall points and limits of disturbance. Maintenance of the natural drainageways and features while providing stability for the Kettle Creek channel will be required. City and County review and approval will be necessary at all stages.

6 ALTERNATIVES EVALUATION

6.1 Evaluation Criteria

The purpose of an alternatives analysis for a DBPS is to synthesize the study results and to evaluate detention and reach improvement options. The outcome of detention alternatives and reach alternatives is typically presented at public meetings for shareholder and public discussion. The outcome of this section is a recommended detention alternative and prioritization to be carried forward to the plan development design phase for further analysis.

The full spectrum detention approach, as defined in Chapter 13 of the City Drainage Criteria Manual, shall be implemented as the standard detention approach. A result of full spectrum detention is that discharges from storms smaller than approximately the 2-year event will be reduced to very low flows near or below the sediment carrying threshold value for downstream drainageways. Full spectrum detention provides better control of the full range of runoff rates that pass through detention facilities than the conventional multi-stage concept. This concept also provides some mitigation of increased runoff volumes by releasing a portion of the increased runoff volume at a low rate over an extended period of time (up to 72 hours). The full spectrum detention approach is necessary for development in the Kettle Creek watershed because it reduces the flooding and stream degradation impacts associated with urban development by controlling peak flows in the stream for a wider range of events than traditional multi-stage detention outlet concepts.

6.2 Regional Detention Alternatives

The channel and structure capacities were determined to be sufficient for the historic, existing, and future conditions 100-year flood event, as presented in Section 4. However, it was determined that the existing and future levels of development in the Kettle Creek basin have an appreciable impact on the flow rates compared to historic rates, with potentially adverse impacts of erosion and deposition resulting from the higher flows.

As shown in the hydrologic results, the post-development hydrographs for Kettle Creek leaving the Black Forest reflect significant increases in flow rates. The objective of regional detention at this location is to mitigate impacts to the downstream channel caused by development in the Black Forest. To adjust the Kettle Creek flow rates to historic levels, two regional detention alternatives are viable along with a do-nothing alternative as it relates to regional detention:

- Regional detention upstream of Powers Boulevard within City open space,
- Regional detention upstream of Old Ranch Road within City open space, and
- No new regional detention facilities.

While it has been shown that multiple ponds placed in a parallel configuration (located on tributaries to major drainageways and serving relatively small drainage areas, as opposed to being placed on the major drainageways themselves) provide a better opportunity to accomplish stormwater management goals and results in lower overall system costs, development has taken place in the Black Forest over the last few

decades without stormwater detention considerations and existing land use and ownership makes sub-regional detention in the Black Forest impractical. Therefore, the regional detention alternatives proposed herein are by necessity located downstream of the Black Forest.

Per the City DCM, a regional detention facility should not serve a contributing area larger than 640 acres (one square mile). The design assumptions used to size the facilities, including uniform rainfall and undeveloped allowable release rates become less reliable with larger basins. Larger basins are also increase long term sediment loads and maintenance requirements. Limiting the contributing area to 640 acres also reduces the likelihood of the structure being regulated by the State Engineer's Office as a jurisdictional dam. The conceptual alternatives proposed herein would serve a contributing area larger than 640 acres, but the limitations in location for new regional detention facilities in the Black Forest preclude adherence to City and County criteria for the subject regional detention facility alternatives.

The regional detention option upstream of Powers Boulevard would be located within City open space (City of Colorado Springs 2020 Land Use map) and would detain flows from the Black Forest area just inside City limits. This would protect the Kettle Creek drainageway from Powers Boulevard to I-25 by discharging at historic rates.

Regional detention upstream of Old Ranch Road would accomplish the same objective but would make use of more available land (as determined from the City of Colorado Springs 2020 Land Use map). The larger tributary area would result in an overall increase in the storage requirements of the pond.

For both aforementioned regional detention options, off-line storage via a diversion of a portion of the Kettle Creek flows would allow for more usable open space with an attractive, multipurpose facility that is readily maintainable and safe for the public, under both dry and wet conditions. A facility that is located in-line with the drainageway and captures and routes the entire flood hydrograph is feasible, but is less advantageous because an in-line facility must be large enough to handle the total flood volume of the entire tributary catchment.

The do-nothing approach as it relates to regional detention would allow developed conditions discharges from the upper portion of the basin to continue to impact the stability of the channel in the lower reach of Kettle Creek. This alternative would make use of the existing regional detention at I-25 but would not provide any additional flood flow attenuation for managing channel-forming flows or flood flows higher in the watershed. This option may put Kettle Creek at risk for continued erosion, deposition, and flooding. However, the mandatory sub-regional detention approach as described in the following sections would limit discharges from new development to historic rates. Without regional detention higher in the reach, however, the Kettle Creek channel within City of Colorado Springs limits would still be subject to periodic flooding above historic rates caused by development higher in the basin.

The regional detention alternatives presented herein only are considered for the purposes of attenuating developed flow rates. Consideration of regional detention alternatives will have significant environmental impacts as discussed in Section 5. Sub-regional detention alone will not reduce flow rates in Kettle Creek to historic levels, as past development in the upper portion of the basin is a contributing factor to the increased flows under existing conditions. Regional detention must be owned and maintained by a public entity, with ownership and maintenance responsibilities clearly defined to ensure the proper function of the facility in perpetuity.

6.3 Sub-Regional Detention

The anticipated approach is sub-regional detention with full spectrum detention and water quality treatment. Any future development in the Kettle Creek basin within the City of Colorado Springs shall have sub-regional detention for each development/phase. Detention facilities serving drainage basins between 20 and 130 acres are considered "sub-regional detention". Sub-regional detention may be constructed by a public entity such as a municipality or special district to serve several landowners in the upstream watershed or by a single landowner. It may be possible for a single landowner to construct sub-regional detention if the upper part of the watershed is owned by others and if the necessary conditions are achieved. Sub-regional detention should be addressed in subsequent Master Development Drainage Plans (MDDP) for individual development projects. The ownership and maintenance of these ponds are anticipated to be public or quasi-public. In order to be considered for public maintenance the contributory area shall be in the range of 70-120 acres. A conceptual map illustrating the locations of required sub-regional detention facilities is shown in **Figure 6-1**.

6.3.1 Full Spectrum Detention

The full spectrum detention approach, as defined in Chapter 13 of the DCM, shall be implemented as the standard detention approach. Impervious surfaces associated with development increase peak flows, frequency of runoff and total volume of stormwater surface runoff when compared to pre-development conditions. This increase is most pronounced for the smaller, more frequent storms and can result in stream degradation and water quality impacts as well as flooding during large storm events.

In addition to detaining developed conditions stormwater discharge for flood control and for water quality considerations, it is also important to expand the focus to the range of flows responsible for transporting the most bedload in the receiving stream. This range depends on reach specific characteristics but is between the annual event and the 5-year event. Runoff events in this range can produce geomorphic changes in local receiving streams resulting in severe erosion, loss of riparian habitat, and water quality degradation.

Outflow hydrographs from traditional flood-control detention facilities tend to maintain flows near the maximum release rates for relatively long periods of time. This allows hydrographs released from multiple independent ponds to overlap and add to each other to generate flows exceeding pre-development conditions. Traditional flood-control detention concepts can result in an increase in total watershed discharges even if individual detention facilities each control peak discharges to pre-developed conditions. Full spectrum detention modeling reduces urban runoff peaks to levels similar to pre-development conditions for a wide range of storms over an entire watershed, even with multiple independent detention facilities. A result of full

spectrum detention is that discharges from storms smaller than approximately the 2-year event will be reduced to very low flows near or below the sediment carrying threshold value for downstream drainageways.

6.3.2 Water Quality

Each sub-regional detention pond shall detain flows not only for flood control, but also for water quality. The Water Quality Capture Volume (WQCV) is intended to capture most runoff events and reduce their pollutant load prior to discharging into drainageways. The size of this storage element depends primarily on the amount of tributary impervious area and can be reduced by implementing development practices that reduce the effective imperviousness, discussed in more detail below.

Future development in the basin shall consider other land planning and engineering design approaches to manage stormwater runoff and water quality. Low Impact Development (LID) is a comprehensive approach with the goal of mimicking the pre-development hydrologic regime. LID emphasizes conservation of natural features and use of engineered, on-site, small-scale hydrologic controls that infiltrate, filter, store, evaporate, and detain runoff close to its source. Portions of the site that aid in reducing the developed conditions discharge should be preserved, which may include mature trees, stream corridors, wetlands, and NRCS Type A/B soils with higher infiltration rates.

Minimizing Directly Connected Impervious Area (MDCIA) includes a variety of runoff reduction strategies based on reducing impervious areas and routing runoff from impervious surfaces over grassy areas to slow runoff and promote infiltration. MDCIA is a technique for reducing runoff peaks and volumes following urbanization. Paved areas can be reduced in extent to the minimum amount practical, and implement methods to route runoff over grassed areas rather than directly into storm sewer. When soils vary over the site, concentrate new impervious areas over NRCS Type C and D soils, while preserving NRCS Type A and B soils for landscape areas and other permeable surfaces. Increasing the number and lengths of flow paths will all reduce the impact of the development.

Volume reduction is a key hydrologic objective, as opposed to peak flow reduction being the only objective. Volume reduction is emphasized not only to reduce pollutant loading and peak flows, but also to move toward hydrologic regimes with flow durations and frequencies closer to the natural hydrologic regime.

6.4 Limited Channel Stabilization Alternative

Channel improvements may be necessary in the main study reach of Kettle Creek to limit erosion and deposition resulting from high velocities as determined in Section 4. However, grading and grade control structures may not be feasible in Kettle Creek due to the disturbance they would cause with the presence of the Preble's meadow jumping mouse. Conceptual check structure placement is provided for reference, should grade control structures become an option in the future.

The locations of these conceptual check structures were determined by areas where mean channel velocities exceeded 5 feet per second for the 100-year event. Future grade between check structures was estimated to stabilize at approximately 0.20 percent. Check structure placement was shown to lower velocities above 5

feet per second and to stabilize the channel. Channel improvements may be determined to be necessary in locations where public or private facilities would be in danger if the creek migrates.

LEGEND

JOVENCHI-I LLC

260 EB LLC

HIGH VALLEY LAND COMPANY INC

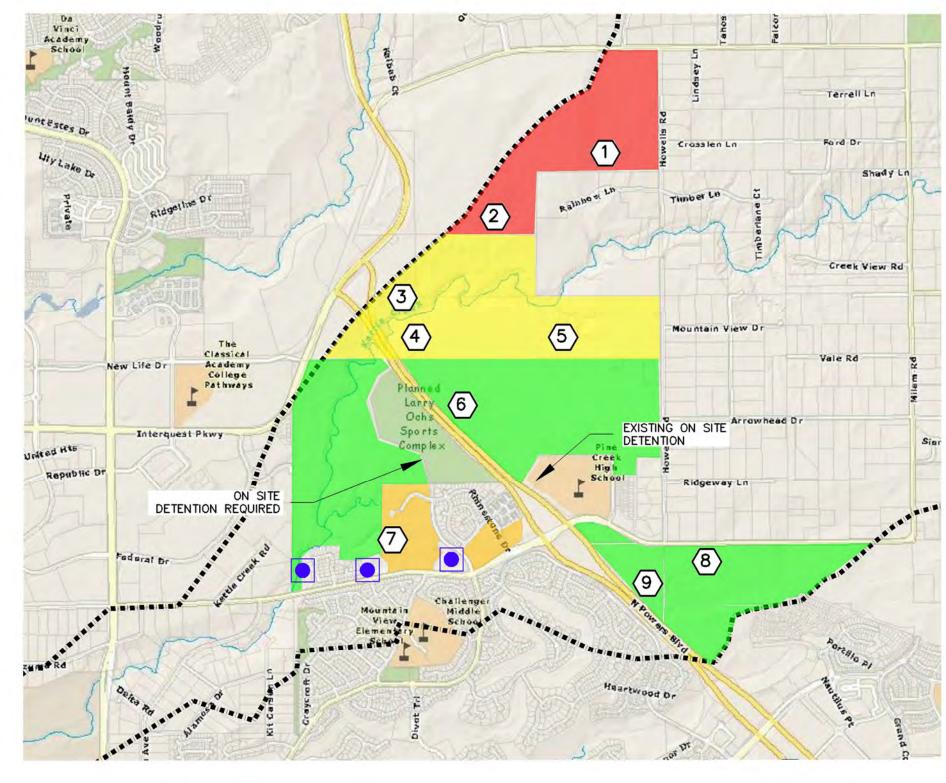
KETTLE CREEK LLC & VENEZIA JOHN FAMILY TRUST

1

ESTIMATED LOCATION OF PROPOSED SUBREGIONAL PONDS

EXISTING LOCATION OF SUBREGIONAL PONDS

KETTLE CREEK BASIN BOUNDARY



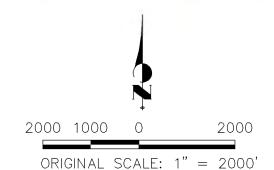


FIGURE 6-1 SUBREGIONAL POND LOCATIONS KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015



7 SELECTED PLAN

The anticipated approach is sub-regional detention with water quality treatment. Any future development in the Kettle Creek basin within the City of Colorado Springs shall have sub-regional detention for each development/phase. No regional detention is considered at this time.

Water quality treatment shall be required for all stormwater detention basins within the City of Colorado Springs. The City will hold all development tributary to Kettle Creek to USAFA release standards.

8 FEE DEVELOPMENT

8.1 General

The objective of the fee development exercise is to determine the equitable share of drainage improvement costs that a developer is responsible for paying to the City of Colorado Springs if they wish to plat a property. The end product of this section is typically a unit fee (cost/acre) that is a one-time charge to the developer for their portion of the reimbursable infrastructure. In the case of Kettle Creek it is expected that no drainage fees will be required and will be considered a closed basin

The City of Colorado Springs map "City of Colorado Springs Fee Basins" shows Kettle Creek as "misc. – unstudied". There has been a master development drainage report completed on a portion of Kettle Creek, which is currently a closed subbasin with no City drainage, bridge, or detention/land fees and no reimbursement for constructed improvements. El Paso County assesses an \$8,100 drainage basin fee for development in the Kettle Creek basin.

8.2 Developable Land

The Kettle Creek watershed has a total area of 10,506 acres. The majority of the watershed is within El Paso County 8,500 acres, with only approximately 1,253 acres of City land unplatted, according to calculations taken from the County Assessor's site. This land calculation also includes unplatted areas that cannot be developed because of specific land use designations. A complete summary of unplatted area land use is provided in **Appendix E**.

| Table 8-1 Land Classification | | | | | | |
|-------------------------------|-----------|--|--|--|--|--|
| Classification | Area (ac) | | | | | |
| Unplatted | 1,253 | | | | | |

8.3 Fee Calculation

The Kettle Creek Drainage Basin Old Ranch Road Tributary Drainage Basin Planning Study and Master Development Drainage Plan, prepared by JR Engineering April 2001 (Kettle Creek MDDP/DBPS), states that the MDDP/DBPS study area is a closed basin. Developers of the properties within the MDDP/DBPS subbasin study are responsible for construction of the drainage improvements. This existing closed basin area can be seen in **Appendix F**.

For all other undeveloped land, shown in **Appendix E**, developers will have direct access to Kettle Creek, and do not have upstream neighboring properties that will require additional infrastructure with the exception of parcel owned by 260 EB, LLC. All undeveloped property within the Kettle Creek basin will not be required to pay drainage fees and will not be reimbursed for any drainage infrastructure required for development.

Kettle Creek DBPS Fee Development 8-1

After analyzing the parcel of land owned by 260 EB LLC, it is found that a subbasin boundary runs through the middle of the property. Because of this, approximately 47 acres of the 180 total acres will flow onto the Jovenchi-I LLC property to the south. The 260 EB, LLC property will be required to detain their developed flows to historic levels in conformance with drainage criteria. Jovenchi-I LLC will have to accommodate the undeveloped (historic) flows from 260 EB, LLC (see Appendix F). The 260 EB, LLC developed flows will be detained in the proposed Pond 2. If necessary, the owners of 260 EB, LLC and Jovenchi-I, LLC will need to work cooperatively to determine an outfall point for the proposed Pond 2. Furthermore, they may opt to work together to combine Pond 2 and Pond 3 by allowing developed flows to pass through the downstream property and locating the combined pond at the site of Pond 3.

With the anticipated approach of having sub-regional detention for any future development in the Kettle Creek basin within the City of Colorado Springs, it is anticipated that the developed runoff from 260 EB, LLC will not generate enough stormwater runoff to necessitate the Jovenchi-I LLC development to construct reimbursable infrastructure. The remaining 133 acres from the 260 EB, LLC property will be required to detain to historic rates prior to the release onto platted county property.

It is proposed that the study area be considered a closed drainage basin. As a closed basin, development would not be required to pay drainage fees. The landowners/developers will not be reimbursed for the construction of these facilities and thus the financial implications to the City are negligible.

9 REFERENCES

Amendment No. 2 To Pine Creek Drainage Basin Planning Study And Master Development Drainage Plan For Pine Creek Subdivision (Portion Contributing to Pine Creek), JR Engineering, October 1998.

Black Forest Quadrangle, Colorado-El Paso Co.; U.S. Department of the Interior U.S. Geological Survey, 2013.

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Briargate Master Plan; DHM Design, June 18, 2007.

City of Colorado SpringsFee Basins; Colorado Springs Public Works - City Engineering, 2001.

City of Colorado Springs 2020 Land Use; City of Colorado Springs, January 2014.

<u>Colorado's Section 303(d) List of Impaired Waters</u>; Colorado Department of Public Health and Environment Water Quality Control Commission 5 CCR 1002-93 Regulation #93, March 2012.

Drainage Criteria Manual, Volume 1; City of Colorado Springs, March 2013.

Envirofacts Search Results Envirofacts; US EPA.

<u>Final Drainage Report for "Briargate Crossing East Filing No. 2" – Pine Creek Drainage Basin, Matrix Design Group, Inc., Revised October 2006.</u>

<u>Final Drainage Report for "Cordera Filing No. 3A" & Master Development Drainage Plan – Cordera Filing No. 3 – Pine Creek & Kettle Creek Drainage Basins;</u> Matrix Design Group, Inc., October 2007.

Flood Insurance Study: El Paso County Colorado and Incorporated Areas, Volumes 1-4, Rev. ed. GPO Publications No. 1999-454-605/00106). Federal Emergency Management Agency, 1999.

<u>Flood Insurance Rate Map Number 08041C0315 F (Panels 295, 315) El Paso County and Incorporated Areas;</u> Federal Emergency Management Agency, March 17, 1997.

Flood Insurance Rate Map Number 08041C0506 F (Panels 506, 507) El Paso County and Incorporated Areas; Federal Emergency Management Agency, March 17, 1997.

Fountain Creek Watershed Study; U.S. Army Corps of Engineers January 2009.

<u>HEC-RAS River Analysis System Hydraulic Reference Manual Version 4.1</u>; US Army Corps of Engineers. January 2010.

<u>Hydrologic Modeling System HEC-HMS User's Manual Version 4.0</u>; US Army Corps of Engineers, December 2013

Kettle Creek Watershed Hydrology Study; Air Force Civil Engineer Center, April 2002

Kettle Creek Drainage Basin Old Ranch Road Tributary Drainage Basin Planning Study and Master Development Drainage Plan; April 2001, JR Engineering.

<u>Land Use Compatibility Analysis and Watershed Growth Analysis Study</u>; Pikes Peak Area Council of Governments, 2004.

<u>Low Effect Habitat Conservation Plan for Preble's Meadow Jumping Mouse on the Kettle Creek Ranch, El Paso County, Colorado</u>; SWCA Environmental Consultants, August 2012.

Master Development Drainage Plan For North Fork at Briargate; May, 2014, JR Engineering.

<u>Permanent Stormwater Quality Report, I-25 North Design Build, El Paso County, Colorado;</u> RESPEC Engineering, August 2012.

Pikeview Quadrangle, Colorado-El Paso Co.; U.S. Department of the Interior U.S. Geological Survey, 2013.

<u>Soil Report for El Paso County, Colorado</u>; United States Department of Agriculture, Natural Resources Conservation Service, December 2013.

<u>Survey of Critical Wetlands and Riparian Areas in El Paso and Pueblo Counties</u>; Colorado; Colorado Natural Heritage Program, June 2001.

<u>Urban Storm Drainage Criteria Manual</u>; Urban Drainage and Flood Control District, June 2001, revised April 2008.

U.S. Air Force Academy Kettle Creek Watershed Hydrology Study Findings and Recommendations Report; URS Group, Inc., March 2002.

Zone Map (Map Numbers 522, 613, 621, 623, 624); El Paso County Development Services Department, March 2012.

Kettle Creek DBPS References 9-1

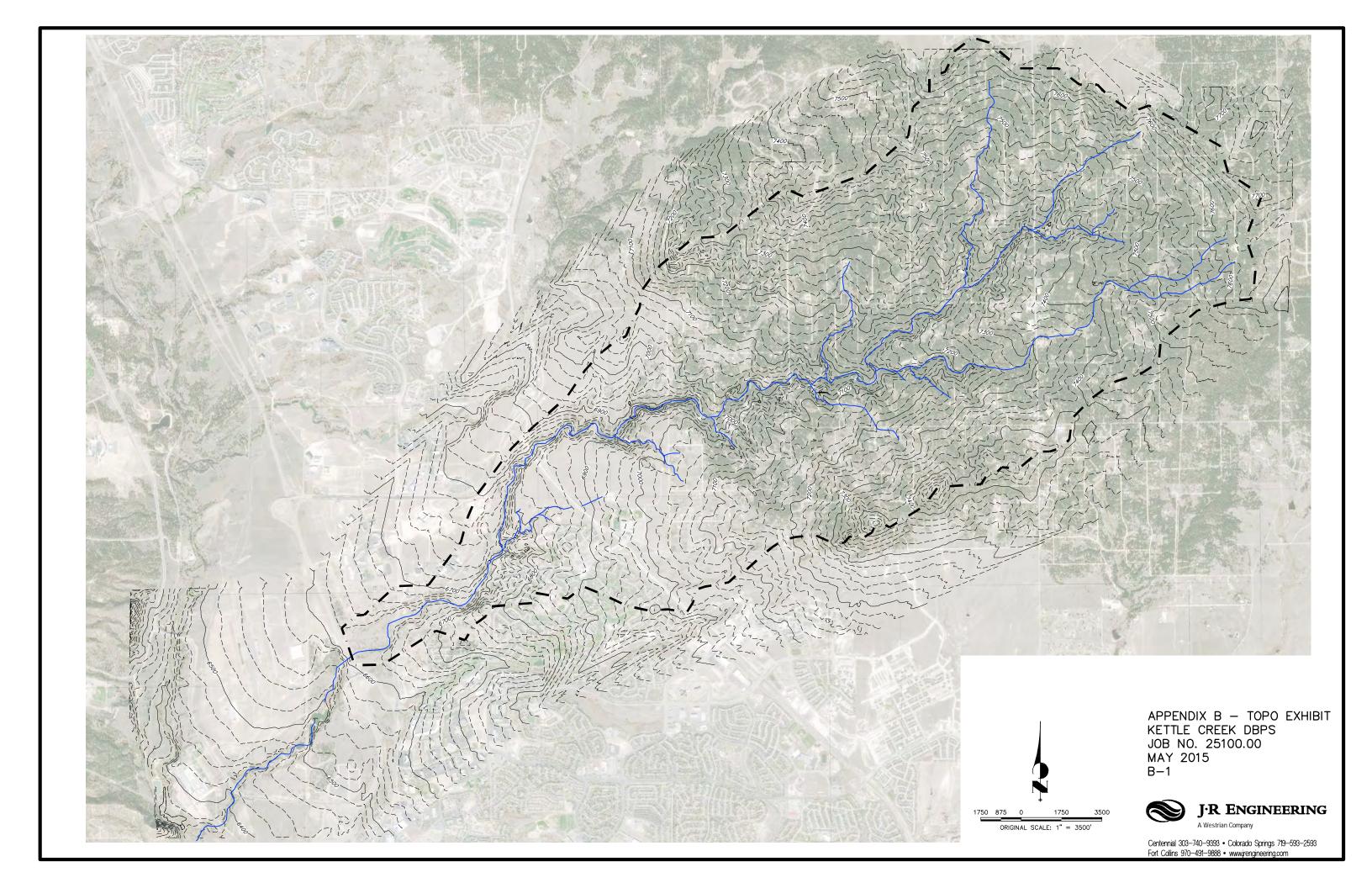
Appendix A – Stakeholder Meeting Summaries

-No Stakeholder Meetings Required

Kettle Creek DBPS Appendix

Appendix B – Hydrologic Calculations and Data

Kettle Creek DBPS Appendix



Depth-Duration-Frequency and Intensity-Duration-Frequency Tables for Colorado Hydrologic Zones 1 through 4

Depth-Duration-Frequency and Intensity-Duration-Frequency
Tables for Colorado Hydrologic Zones 1 through 4

Blue cells are inputs.

Project: Kettle Creek DBPS - Lower Sub-Basins



(Optional) Select a location within the UDFCD boundary:

1. Rainfall Depth-Duration-Frequency Table

If within the UDFCD Boundary, Enter the 1-hour and 6-hour rainfall depths from the USDCM Volume 1.

Otherwise, Enter the 6-hour and 24-hour rainfall depths from the NOAA Atlas 2 Volume III.

Return

Rainfall Depth in Inches at Time Duration

| Return | Rainfall Depth in Inches at Time Duration | | | | | | | | |
|--------|---|--------|--------|--------|------|------|------|------|-------|
| Period | 5-min | 10-min | 15-min | 30-min | 1-hr | 2-hr | 3-hr | 6-hr | 24-hr |
| 2-yr | 0.34 | 0.54 | 0.68 | 0.78 | 1.19 | 1.37 | 1.50 | 1.70 | 2.10 |
| 5-yr | 0.43 | 0.68 | 0.86 | 1.00 | 1.52 | 1.72 | 1.87 | 2.10 | 2.70 |
| 10-yr | 0.49 | 0.78 | 0.98 | 1.14 | 1.73 | 1.96 | 2.13 | 2.40 | 3.20 |
| 25-yr | 0.57 | 0.90 | 1.14 | 1.31 | 2.00 | 2.31 | 2.54 | 2.90 | 3.60 |
| 50-yr | 0.64 | 1.02 | 1.28 | 1.48 | 2.26 | 2.58 | 2.82 | 3.20 | 4.20 |
| 100-yr | 0.71 | 1.13 | 1.42 | 1.64 | 2.50 | 2.84 | 3.10 | 3.50 | 4.60 |
| 500-yr | 0.85 | 1.36 | 1.71 | 1.98 | 3.01 | 3.44 | 3.76 | 4.27 | 5.61 |

Note: Refer to Figures 4-1 through 4-12 of USDCM Volume 1 for 1-hr and 6-hr rainfall depths.

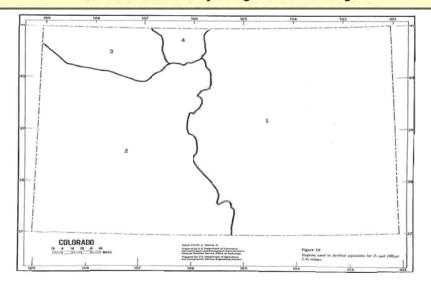
Refer to NOAA Atlas 2 Volume III isopluvial maps for 6-hr and 24-hr rainfall depths.

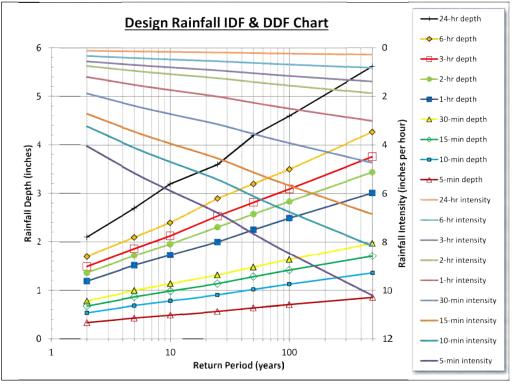
Rainfall depths for durations less than 1-hr are calculated using Equation 4-4 in USDCM Volume 1.

2. Rainfall Intensity-Duration-Frequency Table

| Return | Rainfall Intensity in Inches Per Hour at Time Duration | | | | | | | | |
|--------|--|--------|--------|--------|------|------|------|------|-------|
| Period | 5-min | 10-min | 15-min | 30-min | 1-hr | 2-hr | 3-hr | 6-hr | 24-hr |
| 2-yr | 4.05 | 3.23 | 2.71 | 1.87 | 1.19 | 0.74 | 0.55 | 0.33 | 0.11 |
| 5-yr | 5.15 | 4.11 | 3.45 | 2.38 | 1.52 | 0.94 | 0.70 | 0.41 | 0.14 |
| 10-yr | 5.88 | 4.69 | 3.93 | 2.72 | 1.73 | 1.08 | 0.80 | 0.47 | 0.16 |
| 25-yr | 6.79 | 5.42 | 4.55 | 3.14 | 2.00 | 1.24 | 0.92 | 0.55 | 0.19 |
| 50-yr | 7.66 | 6.11 | 5.12 | 3.54 | 2.26 | 1.40 | 1.04 | 0.62 | 0.21 |
| 100-yr | 8.47 | 6.75 | 5.67 | 3.92 | 2.50 | 1.55 | 1.15 | 0.68 | 0.23 |
| 500-yr | 10.22 | 8.15 | 6.84 | 4.73 | 3.01 | 1.87 | 1.39 | 0.82 | 0.28 |

Note: Intensity approximated using 1-hr rainfall depths and Equation 4-3 in USDCM Volume 1.





2510000 UD-Rain_v1.01.xlsm, DDF & IDF Tables 8/6/2014, 1:53 PM

APPENDIX B — RAINFALL DATA KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B-2



2-Hour Design Storm Distribution

| Rainfall Depth* 0:00 | | n Storm Distribution |
|--|------|----------------------|
| 0:00 0.000 0:05 0.014 0:10 0.046 0:15 0.079 0:20 0.120 0:25 0.179 0:30 0.258 0:35 0.421 0:40 0.712 0:45 0.824 0:50 0.892 0:55 0.935 1:00 0.972 1:05 1.004 1:10 1.018 1:20 1.041 1:25 1.052 1:30 1.063 1:35 1.072 1:40 1.082 1:45 1.091 1:50 1.100 1:55 1.109 | Time | Fraction of 1-Hour |
| 0:05 0.014 0:10 0.046 0:15 0.079 0:20 0.120 0:25 0.179 0:30 0.258 0:35 0.421 0:40 0.712 0:45 0.824 0:50 0.892 0:55 0.935 1:00 0.972 1:05 1.004 1:10 1.018 1:20 1.041 1:25 1.052 1:30 1.063 1:35 1.072 1:40 1.082 1:45 1.091 1:50 1.100 1:55 1.109 | | Rainfall Depth* |
| 0:10 0.046 0:15 0.079 0:20 0.120 0:25 0.179 0:30 0.258 0:35 0.421 0:40 0.712 0:45 0.824 0:50 0.892 0:55 0.935 1:00 0.972 1:05 1.004 1:10 1.018 1:20 1.041 1:25 1.052 1:30 1.063 1:35 1.072 1:40 1.082 1:45 1.091 1:50 1.100 1:55 1.109 | 0:00 | 0.000 |
| 0:15 0.079 0:20 0.120 0:25 0.179 0:30 0.258 0:35 0.421 0:40 0.712 0:45 0.824 0:50 0.892 0:55 0.935 1:00 0.972 1:05 1.004 1:10 1.018 1:20 1.041 1:25 1.052 1:30 1.063 1:35 1.072 1:40 1.082 1:45 1.091 1:50 1.100 1:55 1.109 | 0:05 | 0.014 |
| 0:20 0.120 0:25 0.179 0:30 0.258 0:35 0.421 0:40 0.712 0:45 0.824 0:50 0.892 0:55 0.935 1:00 0.972 1:05 1.004 1:10 1.018 1:15 1.030 1:20 1.041 1:25 1.052 1:30 1.063 1:35 1.072 1:40 1.082 1:45 1.091 1:50 1.100 1:55 1.109 | 0:10 | 0.046 |
| 0:25 0.179 0:30 0.258 0:35 0.421 0:40 0.712 0:45 0.824 0:50 0.892 0:55 0.935 1:00 0.972 1:05 1.004 1:15 1.030 1:20 1.041 1:25 1.052 1:30 1.063 1:35 1.072 1:40 1.082 1:45 1.091 1:50 1.100 1:55 1.109 | 0:15 | 0.079 |
| 0:30 0.258 0:35 0.421 0:40 0.712 0:45 0.824 0:50 0.892 0:55 0.935 1:00 0.972 1:05 1.004 1:10 1.018 1:15 1.030 1:20 1.041 1:25 1.052 1:30 1.063 1:35 1.072 1:40 1.082 1:45 1.091 1:50 1.100 1:55 1.109 | 0:20 | 0.120 |
| 0:35 0.421 0:40 0.712 0:45 0.824 0:50 0.892 0:55 0.935 1:00 0.972 1:05 1.004 1:10 1.018 1:15 1.030 1:20 1.041 1:25 1.052 1:30 1.063 1:35 1.072 1:40 1.082 1:45 1.091 1:50 1.100 1:55 1.109 | 0:25 | 0.179 |
| 0:40 0.712 0:45 0.824 0:50 0.892 0:55 0.935 1:00 0.972 1:05 1.004 1:10 1.018 1:15 1.030 1:20 1.041 1:25 1.052 1:30 1.063 1:35 1.072 1:40 1.082 1:45 1.091 1:50 1.100 1:55 1.109 | 0:30 | 0.258 |
| 0:45 0.824 0:50 0.892 0:55 0.935 1:00 0.972 1:05 1.004 1:10 1.018 1:15 1.030 1:20 1.041 1:25 1.052 1:30 1.063 1:35 1.072 1:40 1.082 1:45 1.091 1:50 1.100 1:55 1.109 | 0:35 | 0.421 |
| 0:50 0.892 0:55 0.935 1:00 0.972 1:05 1.004 1:10 1.018 1:15 1.030 1:20 1.041 1:25 1.052 1:30 1.063 1:35 1.072 1:40 1.082 1:45 1.091 1:50 1.100 1:55 1.109 | 0:40 | 0.712 |
| 0:55 0.935 1:00 0.972 1:05 1.004 1:10 1.018 1:15 1.030 1:20 1.041 1:25 1.052 1:30 1.063 1:35 1.072 1:40 1.082 1:45 1.091 1:50 1.100 1:55 1.109 | 0:45 | 0.824 |
| 1:00 0.972 1:05 1.004 1:10 1.018 1:15 1.030 1:20 1.041 1:25 1.052 1:30 1.063 1:35 1.072 1:40 1.082 1:45 1.091 1:50 1.100 1:55 1.109 | 0:50 | 0.892 |
| 1:05 1.004 1:10 1.018 1:15 1.030 1:20 1.041 1:25 1.052 1:30 1.063 1:35 1.072 1:40 1.082 1:45 1.091 1:50 1.100 1:55 1.109 | 0:55 | 0.935 |
| 1:10 1.018 1:15 1.030 1:20 1.041 1:25 1.052 1:30 1.063 1:35 1.072 1:40 1.082 1:45 1.091 1:50 1.100 1:55 1.109 | 1:00 | 0.972 |
| 1:15 1.030 1:20 1.041 1:25 1.052 1:30 1.063 1:35 1.072 1:40 1.082 1:45 1.091 1:50 1.100 1:55 1.109 | 1:05 | 1.004 |
| 1:20 1.041 1:25 1.052 1:30 1.063 1:35 1.072 1:40 1.082 1:45 1.091 1:50 1.100 1:55 1.109 | 1:10 | 1.018 |
| 1:25 1.052 1:30 1.063 1:35 1.072 1:40 1.082 1:45 1.091 1:50 1.100 1:55 1.109 | 1:15 | 1.030 |
| 1:30 1.063 1:35 1.072 1:40 1.082 1:45 1.091 1:50 1.100 1:55 1.109 | 1:20 | 1.041 |
| 1:35 1.072 1:40 1.082 1:45 1.091 1:50 1.100 1:55 1.109 | 1:25 | 1.052 |
| 1:40 1.082 1:45 1.091 1:50 1.100 1:55 1.109 | 1:30 | 1.063 |
| 1:45 1.091 1:50 1.100 1:55 1.109 | 1:35 | 1.072 |
| 1:50 1.100 1:55 1.109 | 1:40 | 1.082 |
| 1:55 1.109 | 1:45 | 1.091 |
| | 1:50 | 1.100 |
| 2:00 1.119 | 1:55 | 1.109 |
| | 2:00 | 1.119 |

NRCS 24-Hour Design Storm Distribution, <10mi²

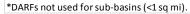
| NRCS 24-Hour Design Storm Distribution, <10mi | | | | | | | |
|---|---------------------|-------|---------------------|-------|---------------------|-------|---------------------|
| Time | Fraction of 24-Hour | Time | Fraction of 24-Hour | Time | Fraction of 24-Hour | Time | Fraction of 24-Hour |
| | Rainfall Depth* | | Rainfall Depth* | | Rainfall Depth* | | Rainfall Depth* |
| 0:00 | 0.0000 | 6:15 | 0.0850 | 12:30 | 0.7350 | 18:45 | 0.9340 |
| 0:15 | 0.0020 | 6:30 | 0.0900 | 12:45 | 0.7580 | 19:00 | 0.9380 |
| 0:30 | 0.0050 | 6:45 | 0.0950 | 13:00 | 0.7760 | 19:15 | 0.9420 |
| 0:45 | 0.0080 | 7:00 | 0.1000 | 13:15 | 0.7910 | 19:30 | 0.9460 |
| 1:00 | 0.0110 | 7:15 | 0.1050 | 13:30 | 0.8040 | 19:45 | 0.9500 |
| 1:15 | 0.0140 | 7:30 | 0.1100 | 13:45 | 0.8150 | 20:00 | 0.9530 |
| 1:30 | 0.0170 | 7:45 | 0.1150 | 14:00 | 0.8250 | 20:15 | 0.9560 |
| 1:45 | 0.0200 | 8:00 | 0.1200 | 14:15 | 0.8340 | 20:30 | 0.9590 |
| 2:00 | 0.0230 | 8:15 | 0.1260 | 14:30 | 0.8420 | 20:45 | 0.9620 |
| 2:15 | 0.0260 | 8:30 | 0.1330 | 14:45 | 0.8490 | 21:00 | 0.9650 |
| 2:30 | 0.0290 | 8:45 | 0.1400 | 15:00 | 0.8560 | 21:15 | 0.9680 |
| 2:45 | 0.0320 | 9:00 | 0.1470 | 15:15 | 0.8630 | 21:30 | 0.9710 |
| 3:00 | 0.0350 | 9:15 | 0.1550 | 15:30 | 0.8690 | 21:45 | 0.9740 |
| 3:15 | 0.0380 | 9:30 | 0.1630 | 15:45 | 0.8750 | 22:00 | 0.9770 |
| 3:30 | 0.0410 | 9:45 | 0.1720 | 16:00 | 0.8810 | 22:15 | 0.9800 |
| 3:45 | 0.0440 | 10:00 | 0.1810 | 16:15 | 0.8870 | 22:30 | 0.9830 |
| 4:00 | 0.0480 | 10:15 | 0.1910 | 16:30 | 0.8930 | 22:45 | 0.9860 |
| 4:15 | 0.0520 | 10:30 | 0.2030 | 16:45 | 0.8980 | 23:00 | 0.9890 |
| 4:30 | 0.0560 | 10:45 | 0.2180 | 17:00 | 0.9030 | 23:15 | 0.9920 |
| 4:45 | 0.0600 | 11:00 | 0.2360 | 17:15 | 0.9080 | 23:30 | 0.9950 |
| 5:00 | 0.0604 | 11:15 | 0.2570 | 17:30 | 0.9130 | 23:45 | 0.9980 |
| 5:15 | 0.0680 | 11:30 | 0.2830 | 17:45 | 0.9180 | 24:00 | 1.0000 |
| 5:30 | 0.0720 | 11:45 | 0.3870 | 18:00 | 0.9220 | | |
| 5:45 | 0.0760 | 12:00 | 0.6630 | 18:15 | 0.9260 | | |
| 6:00 | 0.0800 | 12:15 | 0.7070 | 18:30 | 0.9300 | | |

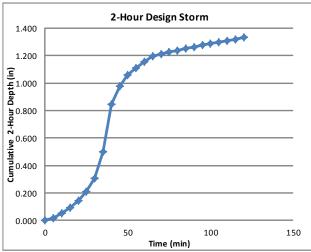
APPENDIX B — DESIGN STORM DISTRIBUTION DATA KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B-3

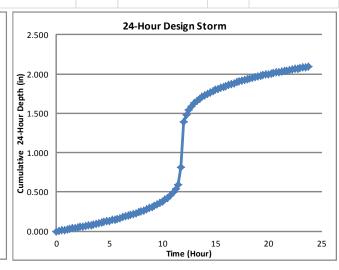


| | Thunderstrom | Frontal | | |
|---------------|--------------|---------------|--|--|
| | Analysis | Analysis | | |
| | z=7120' | z=7415' | | |
| Return Period | 1-Hour Depth | 24-Hour Depth | | |
| (Year) | (Inches) | (Inches) | | |
| 2 | 1.19 | 2.10 | | |

| | Cumulative Rainfall Depth | | | | | | | | | |
|---------|---------------------------|----------|----------------------|----------|--------------------|----------|--------------------|----------|--------------------|--|
| 2-Ho | ur Design Storm | | 24-Hour Design Storm | | | | | | | |
| Time | Cumulative | Time | Cumulative | Time | Cumulative | Time | Cumulative | Time | Cumulative | |
| (5 min) | 2-Hour Depth (in) | (15 min) | 24-Hour Depth (in) | (15 min) | 24-Hour Depth (in) | (15 min) | 24-Hour Depth (in) | (15 min) | 24-Hour Depth (in) | |
| 0:00 | 0.000 | 0:00 | 0.000 | 6:00 | 0.168 | 12:00 | 1.392 | 18:00 | 1.936 | |
| 0:05 | 0.017 | 0:15 | 0.004 | 6:15 | 0.179 | 12:15 | 1.485 | 18:15 | 1.945 | |
| 0:10 | 0.055 | 0:30 | 0.011 | 6:30 | 0.189 | 12:30 | 1.544 | 18:30 | 1.953 | |
| 0:15 | 0.094 | 0:45 | 0.017 | 6:45 | 0.200 | 12:45 | 1.592 | 18:45 | 1.961 | |
| 0:20 | 0.143 | 1:00 | 0.023 | 7:00 | 0.210 | 13:00 | 1.630 | 19:00 | 1.970 | |
| 0:25 | 0.213 | 1:15 | 0.029 | 7:15 | 0.221 | 13:15 | 1.661 | 19:15 | 1.978 | |
| 0:30 | 0.307 | 1:30 | 0.036 | 7:30 | 0.231 | 13:30 | 1.688 | 19:30 | 1.987 | |
| 0:35 | 0.501 | 1:45 | 0.042 | 7:45 | 0.242 | 13:45 | 1.712 | 19:45 | 1.995 | |
| 0:40 | 0.847 | 2:00 | 0.048 | 8:00 | 0.252 | 14:00 | 1.733 | 20:00 | 2.001 | |
| 0:45 | 0.981 | 2:15 | 0.055 | 8:15 | 0.265 | 14:15 | 1.751 | 20:15 | 2.008 | |
| 0:50 | 1.061 | 2:30 | 0.061 | 8:30 | 0.279 | 14:30 | 1.768 | 20:30 | 2.014 | |
| 0:55 | 1.113 | 2:45 | 0.067 | 8:45 | 0.294 | 14:45 | 1.783 | 20:45 | 2.020 | |
| 1:00 | 1.157 | 3:00 | 0.074 | 9:00 | 0.309 | 15:00 | 1.798 | 21:00 | 2.027 | |
| 1:05 | 1.195 | 3:15 | 0.080 | 9:15 | 0.326 | 15:15 | 1.812 | 21:15 | 2.033 | |
| 1:10 | 1.211 | 3:30 | 0.086 | 9:30 | 0.342 | 15:30 | 1.825 | 21:30 | 2.039 | |
| 1:15 | 1.226 | 3:45 | 0.092 | 9:45 | 0.361 | 15:45 | 1.838 | 21:45 | 2.045 | |
| 1:20 | 1.239 | 4:00 | 0.101 | 10:00 | 0.380 | 16:00 | 1.850 | 22:00 | 2.052 | |
| 1:25 | 1.252 | 4:15 | 0.109 | 10:15 | 0.401 | 16:15 | 1.863 | 22:15 | 2.058 | |
| 1:30 | 1.265 | 4:30 | 0.118 | 10:30 | 0.426 | 16:30 | 1.875 | 22:30 | 2.064 | |
| 1:35 | 1.276 | 4:45 | 0.126 | 10:45 | 0.458 | 16:45 | 1.886 | 22:45 | 2.071 | |
| 1:40 | 1.288 | 5:00 | 0.127 | 11:00 | 0.496 | 17:00 | 1.896 | 23:00 | 2.077 | |
| 1:45 | 1.298 | 5:15 | 0.143 | 11:15 | 0.540 | 17:15 | 1.907 | 23:15 | 2.083 | |
| 1:50 | 1.309 | 5:30 | 0.151 | 11:30 | 0.594 | 17:30 | 1.917 | 23:30 | 2.090 | |
| 1:55 | 1.320 | 5:45 | 0.160 | 11:45 | 0.813 | 17:45 | 1.928 | 23:45 | 2.096 | |
| 2:00 | 1.332 | | | | | | | | | |



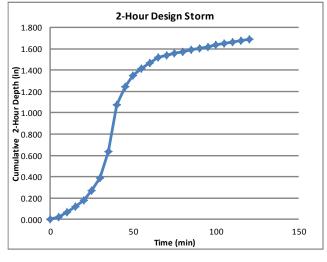


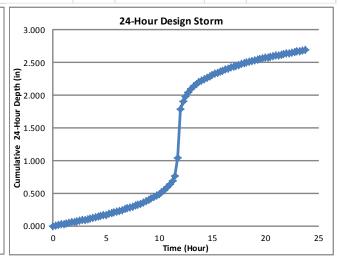


| | Thunderstrom | Frontal | | |
|---------------|--------------|---------------|--|--|
| | Analysis | Analysis | | |
| | z=7120' | z=7415' | | |
| Return Period | 1-Hour Depth | 24-Hour Depth | | |
| (Year) | (Inches) | (Inches) | | |
| 5 | 1.51 | 2.70 | | |

| | Cumulative Rainfall Depth | | | | | | | | |
|---------|---------------------------|----------|----------------------|----------|--------------------|----------|--------------------|----------|--------------------|
| 2-Ho | ur Design Storm | | 24-Hour Design Storm | | | | | | |
| Time | Cumulative | Time | Cumulative | Time | Cumulative | Time | Cumulative | Time | Cumulative |
| (5 min) | 2-Hour Depth (in) | (15 min) | 24-Hour Depth (in) | (15 min) | 24-Hour Depth (in) | (15 min) | 24-Hour Depth (in) | (15 min) | 24-Hour Depth (in) |
| 0:00 | 0.000 | 0:00 | 0.000 | 6:00 | 0.216 | 12:00 | 1.790 | 18:00 | 2.489 |
| 0:05 | 0.021 | 0:15 | 0.005 | 6:15 | 0.230 | 12:15 | 1.909 | 18:15 | 2.500 |
| 0:10 | 0.069 | 0:30 | 0.014 | 6:30 | 0.243 | 12:30 | 1.985 | 18:30 | 2.511 |
| 0:15 | 0.119 | 0:45 | 0.022 | 6:45 | 0.257 | 12:45 | 2.047 | 18:45 | 2.522 |
| 0:20 | 0.181 | 1:00 | 0.030 | 7:00 | 0.270 | 13:00 | 2.095 | 19:00 | 2.533 |
| 0:25 | 0.270 | 1:15 | 0.038 | 7:15 | 0.284 | 13:15 | 2.136 | 19:15 | 2.543 |
| 0:30 | 0.390 | 1:30 | 0.046 | 7:30 | 0.297 | 13:30 | 2.171 | 19:30 | 2.554 |
| 0:35 | 0.636 | 1:45 | 0.054 | 7:45 | 0.311 | 13:45 | 2.201 | 19:45 | 2.565 |
| 0:40 | 1.075 | 2:00 | 0.062 | 8:00 | 0.324 | 14:00 | 2.228 | 20:00 | 2.573 |
| 0:45 | 1.244 | 2:15 | 0.070 | 8:15 | 0.340 | 14:15 | 2.252 | 20:15 | 2.581 |
| 0:50 | 1.347 | 2:30 | 0.078 | 8:30 | 0.359 | 14:30 | 2.273 | 20:30 | 2.589 |
| 0:55 | 1.412 | 2:45 | 0.086 | 8:45 | 0.378 | 14:45 | 2.292 | 20:45 | 2.597 |
| 1:00 | 1.468 | 3:00 | 0.095 | 9:00 | 0.397 | 15:00 | 2.311 | 21:00 | 2.606 |
| 1:05 | 1.516 | 3:15 | 0.103 | 9:15 | 0.419 | 15:15 | 2.330 | 21:15 | 2.614 |
| 1:10 | 1.537 | 3:30 | 0.111 | 9:30 | 0.440 | 15:30 | 2.346 | 21:30 | 2.622 |
| 1:15 | 1.555 | 3:45 | 0.119 | 9:45 | 0.464 | 15:45 | 2.363 | 21:45 | 2.630 |
| 1:20 | 1.572 | 4:00 | 0.130 | 10:00 | 0.489 | 16:00 | 2.379 | 22:00 | 2.638 |
| 1:25 | 1.589 | 4:15 | 0.140 | 10:15 | 0.516 | 16:15 | 2.395 | 22:15 | 2.646 |
| 1:30 | 1.605 | 4:30 | 0.151 | 10:30 | 0.548 | 16:30 | 2.411 | 22:30 | 2.654 |
| 1:35 | 1.619 | 4:45 | 0.162 | 10:45 | 0.589 | 16:45 | 2.425 | 22:45 | 2.662 |
| 1:40 | 1.634 | 5:00 | 0.163 | 11:00 | 0.637 | 17:00 | 2.438 | 23:00 | 2.670 |
| 1:45 | 1.647 | 5:15 | 0.184 | 11:15 | 0.694 | 17:15 | 2.452 | 23:15 | 2.678 |
| 1:50 | 1.661 | 5:30 | 0.194 | 11:30 | 0.764 | 17:30 | 2.465 | 23:30 | 2.687 |
| 1:55 | 1.675 | 5:45 | 0.205 | 11:45 | 1.045 | 17:45 | 2.479 | 23:45 | 2.695 |
| 2:00 | 1.690 | | | | | | | | |

*DARFs not used for sub-basins (<1 sq mi).





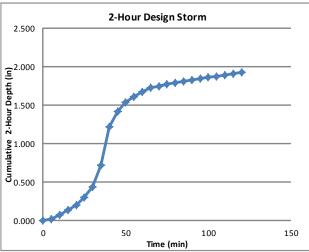
HYDROLOGIC DATA — DESIGN STORM 2 & 5 YR KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B-4

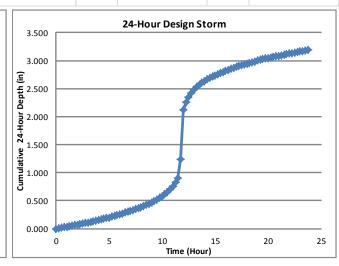


| | Thunderstrom | Frontal | | |
|---------------|--------------|---------------|--|--|
| | Analysis | Analysis | | |
| | z=7120' | z=7415' | | |
| Return Period | 1-Hour Depth | 24-Hour Depth | | |
| (Year) | (Inches) | (Inches) | | |
| 10 | 1.72 | 3.20 | | |

| | Cumulative Rainfall Depth | | | | | | | | | |
|---------|---------------------------|----------|----------------------|----------|--------------------|----------|--------------------|----------|--------------------|--|
| 2-Ho | ur Design Storm | | 24-Hour Design Storm | | | | | | | |
| Time | Cumulative | Time | Cumulative | Time | Cumulative | Time | Cumulative | Time | Cumulative | |
| (5 min) | 2-Hour Depth (in) | (15 min) | 24-Hour Depth (in) | (15 min) | 24-Hour Depth (in) | (15 min) | 24-Hour Depth (in) | (15 min) | 24-Hour Depth (in) | |
| 0:00 | 0.000 | 0:00 | 0.000 | 6:00 | 0.256 | 12:00 | 2.122 | 18:00 | 2.950 | |
| 0:05 | 0.024 | 0:15 | 0.006 | 6:15 | 0.272 | 12:15 | 2.262 | 18:15 | 2.963 | |
| 0:10 | 0.079 | 0:30 | 0.016 | 6:30 | 0.288 | 12:30 | 2.352 | 18:30 | 2.976 | |
| 0:15 | 0.136 | 0:45 | 0.026 | 6:45 | 0.304 | 12:45 | 2.426 | 18:45 | 2.989 | |
| 0:20 | 0.206 | 1:00 | 0.035 | 7:00 | 0.320 | 13:00 | 2.483 | 19:00 | 3.002 | |
| 0:25 | 0.308 | 1:15 | 0.045 | 7:15 | 0.336 | 13:15 | 2.531 | 19:15 | 3.014 | |
| 0:30 | 0.444 | 1:30 | 0.054 | 7:30 | 0.352 | 13:30 | 2.573 | 19:30 | 3.027 | |
| 0:35 | 0.724 | 1:45 | 0.064 | 7:45 | 0.368 | 13:45 | 2.608 | 19:45 | 3.040 | |
| 0:40 | 1.225 | 2:00 | 0.074 | 8:00 | 0.384 | 14:00 | 2.640 | 20:00 | 3.050 | |
| 0:45 | 1.417 | 2:15 | 0.083 | 8:15 | 0.403 | 14:15 | 2.669 | 20:15 | 3.059 | |
| 0:50 | 1.534 | 2:30 | 0.093 | 8:30 | 0.426 | 14:30 | 2.694 | 20:30 | 3.069 | |
| 0:55 | 1.608 | 2:45 | 0.102 | 8:45 | 0.448 | 14:45 | 2.717 | 20:45 | 3.078 | |
| 1:00 | 1.672 | 3:00 | 0.112 | 9:00 | 0.470 | 15:00 | 2.739 | 21:00 | 3.088 | |
| 1:05 | 1.727 | 3:15 | 0.122 | 9:15 | 0.496 | 15:15 | 2.762 | 21:15 | 3.098 | |
| 1:10 | 1.751 | 3:30 | 0.131 | 9:30 | 0.522 | 15:30 | 2.781 | 21:30 | 3.107 | |
| 1:15 | 1.772 | 3:45 | 0.141 | 9:45 | 0.550 | 15:45 | 2.800 | 21:45 | 3.117 | |
| 1:20 | 1.791 | 4:00 | 0.154 | 10:00 | 0.579 | 16:00 | 2.819 | 22:00 | 3.126 | |
| 1:25 | 1.809 | 4:15 | 0.166 | 10:15 | 0.611 | 16:15 | 2.838 | 22:15 | 3.136 | |
| 1:30 | 1.828 | 4:30 | 0.179 | 10:30 | 0.650 | 16:30 | 2.858 | 22:30 | 3.146 | |
| 1:35 | 1.844 | 4:45 | 0.192 | 10:45 | 0.698 | 16:45 | 2.874 | 22:45 | 3.155 | |
| 1:40 | 1.861 | 5:00 | 0.193 | 11:00 | 0.755 | 17:00 | 2.890 | 23:00 | 3.165 | |
| 1:45 | 1.877 | 5:15 | 0.218 | 11:15 | 0.822 | 17:15 | 2.906 | 23:15 | 3.174 | |
| 1:50 | 1.892 | 5:30 | 0.230 | 11:30 | 0.906 | 17:30 | 2.922 | 23:30 | 3.184 | |
| 1:55 | 1.907 | 5:45 | 0.243 | 11:45 | 1.238 | 17:45 | 2.938 | 23:45 | 3.194 | |
| 2:00 | 1.925 | | | | | | | | | |

*DARFs not used for sub-basins (<1 sq mi).

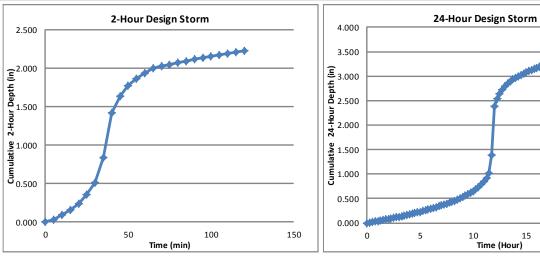




| | Thunderstrom | Frontal | | |
|---------------|--------------|---------------|--|--|
| | Analysis | Analysis | | |
| | z=7120' | z=7415' | | |
| Return Period | 1-Hour Depth | 24-Hour Depth | | |
| (Year) | (Inches) | (Inches) | | |
| 25 | 1.99 | 3.60 | | |

| | Cumulative Rainfall Depth | | | | | | | | | |
|---------|---------------------------|----------|--------------------|----------|--------------------|------------|--------------------|----------|--------------------|--|
| 2-Ho | ur Design Storm | | | | 24-Hour De | sign Storn | n | | | |
| Time | Cumulative | Time | Cumulative | Time | Cumulative | Time | Cumulative | Time | Cumulative | |
| (5 min) | 2-Hour Depth (in) | (15 min) | 24-Hour Depth (in) | (15 min) | 24-Hour Depth (in) | (15 min) | 24-Hour Depth (in) | (15 min) | 24-Hour Depth (in) | |
| 0:00 | 0.000 | 0:00 | 0.000 | 6:00 | 0.288 | 12:00 | 2.387 | 18:00 | 3.319 | |
| 0:05 | 0.028 | 0:15 | 0.007 | 6:15 | 0.306 | 12:15 | 2.545 | 18:15 | 3.334 | |
| 0:10 | 0.092 | 0:30 | 0.018 | 6:30 | 0.324 | 12:30 | 2.646 | 18:30 | 3.348 | |
| 0:15 | 0.157 | 0:45 | 0.029 | 6:45 | 0.342 | 12:45 | 2.729 | 18:45 | 3.362 | |
| 0:20 | 0.239 | 1:00 | 0.040 | 7:00 | 0.360 | 13:00 | 2.794 | 19:00 | 3.377 | |
| 0:25 | 0.356 | 1:15 | 0.050 | 7:15 | 0.378 | 13:15 | 2.848 | 19:15 | 3.391 | |
| 0:30 | 0.513 | 1:30 | 0.061 | 7:30 | 0.396 | 13:30 | 2.894 | 19:30 | 3.406 | |
| 0:35 | 0.838 | 1:45 | 0.072 | 7:45 | 0.414 | 13:45 | 2.934 | 19:45 | 3.420 | |
| 0:40 | 1.417 | 2:00 | 0.083 | 8:00 | 0.432 | 14:00 | 2.970 | 20:00 | 3.431 | |
| 0:45 | 1.640 | 2:15 | 0.094 | 8:15 | 0.454 | 14:15 | 3.002 | 20:15 | 3.442 | |
| 0:50 | 1.775 | 2:30 | 0.104 | 8:30 | 0.479 | 14:30 | 3.031 | 20:30 | 3.452 | |
| 0:55 | 1.861 | 2:45 | 0.115 | 8:45 | 0.504 | 14:45 | 3.056 | 20:45 | 3.463 | |
| 1:00 | 1.934 | 3:00 | 0.126 | 9:00 | 0.529 | 15:00 | 3.082 | 21:00 | 3.474 | |
| 1:05 | 1.998 | 3:15 | 0.137 | 9:15 | 0.558 | 15:15 | 3.107 | 21:15 | 3.485 | |
| 1:10 | 2.026 | 3:30 | 0.148 | 9:30 | 0.587 | 15:30 | 3.128 | 21:30 | 3.496 | |
| 1:15 | 2.050 | 3:45 | 0.158 | 9:45 | 0.619 | 15:45 | 3.150 | 21:45 | 3.506 | |
| 1:20 | 2.072 | 4:00 | 0.173 | 10:00 | 0.652 | 16:00 | 3.172 | 22:00 | 3.517 | |
| 1:25 | 2.093 | 4:15 | 0.187 | 10:15 | 0.688 | 16:15 | 3.193 | 22:15 | 3.528 | |
| 1:30 | 2.115 | 4:30 | 0.202 | 10:30 | 0.731 | 16:30 | 3.215 | 22:30 | 3.539 | |
| 1:35 | 2.133 | 4:45 | 0.216 | 10:45 | 0.785 | 16:45 | 3.233 | 22:45 | 3.550 | |
| 1:40 | 2.153 | 5:00 | 0.217 | 11:00 | 0.850 | 17:00 | 3.251 | 23:00 | 3.560 | |
| 1:45 | 2.171 | 5:15 | 0.245 | 11:15 | 0.925 | 17:15 | 3.269 | 23:15 | 3.571 | |
| 1:50 | 2.189 | 5:30 | 0.259 | 11:30 | 1.019 | 17:30 | 3.287 | 23:30 | 3.582 | |
| 1:55 | 2.207 | 5:45 | 0.274 | 11:45 | 1.393 | 17:45 | 3.305 | 23:45 | 3.593 | |
| 2:00 | 2.227 | | | | | | | | | |

*DARFs not used for sub-basins (<1 sq mi).



HYDROLOGIC DATA - DESIGN STORM 10 & 25 YR KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B-5

20

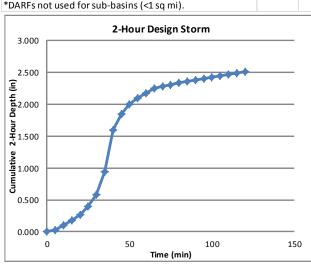
25

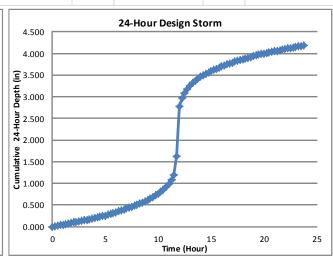
10 15 Time (Hour)



| | Thunderstrom | Frontal | | | |
|---------------|--------------|---------------|--|--|--|
| | Analysis | Analysis | | | |
| | z=7120' | z=7415' | | | |
| Return Period | 1-Hour Depth | 24-Hour Depth | | | |
| (Year) | (Inches) | (Inches) | | | |
| 50 | 2.24 | 4.20 | | | |

| | Cumulative Rainfall Depth | | | | | | | | | |
|---------|--|------------|--------------------|----------|--------------------|----------|--------------------|----------|--------------------|--|
| 2-Ho | 2-Hour Design Storm 24-Hour Design Storm | | | | | | | | | |
| Time | Cumulative | Time | Cumulative | Time | Cumulative | Time | Cumulative | Time | Cumulative | |
| (5 min) | 2-Hour Depth (in) | (15 min) | 24-Hour Depth (in) | (15 min) | 24-Hour Depth (in) | (15 min) | 24-Hour Depth (in) | (15 min) | 24-Hour Depth (in) | |
| 0:00 | 0.000 | 0:00 | 0.000 | 6:00 | 0.336 | 12:00 | 2.785 | 18:00 | 3.872 | |
| 0:05 | 0.031 | 0:15 | 0.008 | 6:15 | 0.357 | 12:15 | 2.969 | 18:15 | 3.889 | |
| 0:10 | 0.103 | 0:30 | 0.021 | 6:30 | 0.378 | 12:30 | 3.087 | 18:30 | 3.906 | |
| 0:15 | 0.177 | 0:45 | 0.034 | 6:45 | 0.399 | 12:45 | 3.184 | 18:45 | 3.923 | |
| 0:20 | 0.269 | 1:00 | 0.046 | 7:00 | 0.420 | 13:00 | 3.259 | 19:00 | 3.940 | |
| 0:25 | 0.401 | 1:15 | 0.059 | 7:15 | 0.441 | 13:15 | 3.322 | 19:15 | 3.956 | |
| 0:30 | 0.578 | 1:30 | 0.071 | 7:30 | 0.462 | 13:30 | 3.377 | 19:30 | 3.973 | |
| 0:35 | 0.943 | 1:45 | 0.084 | 7:45 | 0.483 | 13:45 | 3.423 | 19:45 | 3.990 | |
| 0:40 | 1.595 | 2:00 | 0.097 | 8:00 | 0.504 | 14:00 | 3.465 | 20:00 | 4.003 | |
| 0:45 | 1.846 | 2:15 | 0.109 | 8:15 | 0.529 | 14:15 | 3.503 | 20:15 | 4.015 | |
| 0:50 | 1.998 | 2:30 | 0.122 | 8:30 | 0.559 | 14:30 | 3.536 | 20:30 | 4.028 | |
| 0:55 | 2.094 | 2:45 | 0.134 | 8:45 | 0.588 | 14:45 | 3.566 | 20:45 | 4.040 | |
| 1:00 | 2.177 | 3:00 | 0.147 | 9:00 | 0.617 | 15:00 | 3.595 | 21:00 | 4.053 | |
| 1:05 | 2.249 | 3:15 | 0.160 | 9:15 | 0.651 | 15:15 | 3.625 | 21:15 | 4.066 | |
| 1:10 | 2.280 | 3:30 | 0.172 | 9:30 | 0.685 | 15:30 | 3.650 | 21:30 | 4.078 | |
| 1:15 | 2.307 | 3:45 | 0.185 | 9:45 | 0.722 | 15:45 | 3.675 | 21:45 | 4.091 | |
| 1:20 | 2.332 | 4:00 | 0.202 | 10:00 | 0.760 | 16:00 | 3.700 | 22:00 | 4.103 | |
| 1:25 | 2.356 | 4:15 | 0.218 | 10:15 | 0.802 | 16:15 | 3.725 | 22:15 | 4.116 | |
| 1:30 | 2.381 | 4:30 | 0.235 | 10:30 | 0.853 | 16:30 | 3.751 | 22:30 | 4.129 | |
| 1:35 | 2.401 | 4:45 | 0.252 | 10:45 | 0.916 | 16:45 | 3.772 | 22:45 | 4.141 | |
| 1:40 | 2.424 | 5:00 | 0.254 | 11:00 | 0.991 | 17:00 | 3.793 | 23:00 | 4.154 | |
| 1:45 | 2.444 | 5:15 | 0.286 | 11:15 | 1.079 | 17:15 | 3.814 | 23:15 | 4.166 | |
| 1:50 | 2.464 | 5:30 | 0.302 | 11:30 | 1.189 | 17:30 | 3.835 | 23:30 | 4.179 | |
| 1:55 | 2.484 | 5:45 | 0.319 | 11:45 | 1.625 | 17:45 | 3.856 | 23:45 | 4.192 | |
| 2:00 | 2.507 | | | | | | | | | |
| *DARFs | not used for sub-bas | ins (<1 sq | mi). | | | | | | | |

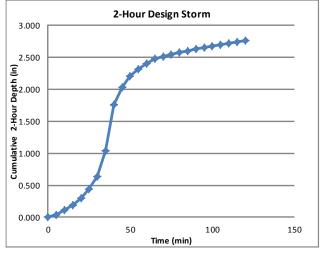


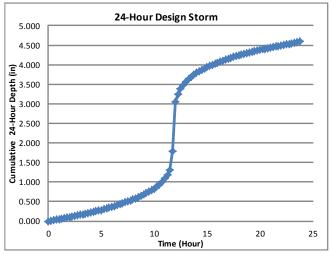


| | Thunderstrom | Frontal |
|---------------|--------------|---------------|
| | Analysis | Analysis |
| | z=7120' | z=7415' |
| Return Period | 1-Hour Depth | 24-Hour Depth |
| (Year) | (Inches) | (Inches) |
| 100 | 2.47 | 4.60 |

| | ur Design Storm | | | | | | | | |
|---------|-------------------|----------|--------------------|----------|--------------------|------------|--------------------|----------|--------------------|
| T T | | | | | 24-Hour De | sign Storn | n | | |
| Time | Cumulative | Time | Cumulative | Time | Cumulative | Time | Cumulative | Time | Cumulative |
| (5 min) | 2-Hour Depth (in) | (15 min) | 24-Hour Depth (in) | (15 min) | 24-Hour Depth (in) | (15 min) | 24-Hour Depth (in) | (15 min) | 24-Hour Depth (in) |
| 0:00 | 0.000 | 0:00 | 0.000 | 6:00 | 0.368 | 12:00 | 3.050 | 18:00 | 4.241 |
| 0:05 | 0.035 | 0:15 | 0.009 | 6:15 | 0.391 | 12:15 | 3.252 | 18:15 | 4.260 |
| 0:10 | 0.114 | 0:30 | 0.023 | 6:30 | 0.414 | 12:30 | 3.381 | 18:30 | 4.278 |
| 0:15 | 0.195 | 0:45 | 0.037 | 6:45 | 0.437 | 12:45 | 3.487 | 18:45 | 4.296 |
| 0:20 | 0.296 | 1:00 | 0.051 | 7:00 | 0.460 | 13:00 | 3.570 | 19:00 | 4.315 |
| 0:25 | 0.442 | 1:15 | 0.064 | 7:15 | 0.483 | 13:15 | 3.639 | 19:15 | 4.333 |
| 0:30 | 0.637 | 1:30 | 0.078 | 7:30 | 0.506 | 13:30 | 3.698 | 19:30 | 4.352 |
| 0:35 | 1.040 | 1:45 | 0.092 | 7:45 | 0.529 | 13:45 | 3.749 | 19:45 | 4.370 |
| 0:40 | 1.759 | 2:00 | 0.106 | 8:00 | 0.552 | 14:00 | 3.795 | 20:00 | 4.384 |
| 0:45 | 2.035 | 2:15 | 0.120 | 8:15 | 0.580 | 14:15 | 3.836 | 20:15 | 4.398 |
| 0:50 | 2.203 | 2:30 | 0.133 | 8:30 | 0.612 | 14:30 | 3.873 | 20:30 | 4.411 |
| 0:55 | 2.309 | 2:45 | 0.147 | 8:45 | 0.644 | 14:45 | 3.905 | 20:45 | 4.425 |
| 1:00 | 2.401 | 3:00 | 0.161 | 9:00 | 0.676 | 15:00 | 3.938 | 21:00 | 4.439 |
| 1:05 | 2.480 | 3:15 | 0.175 | 9:15 | 0.713 | 15:15 | 3.970 | 21:15 | 4.453 |
| 1:10 | 2.514 | 3:30 | 0.189 | 9:30 | 0.750 | 15:30 | 3.997 | 21:30 | 4.467 |
| 1:15 | 2.544 | 3:45 | 0.202 | 9:45 | 0.791 | 15:45 | 4.025 | 21:45 | 4.480 |
| 1:20 | 2.571 | 4:00 | 0.221 | 10:00 | 0.833 | 16:00 | 4.053 | 22:00 | 4.494 |
| 1:25 | 2.598 | 4:15 | 0.239 | 10:15 | 0.879 | 16:15 | 4.080 | 22:15 | 4.508 |
| 1:30 | 2.626 | 4:30 | 0.258 | 10:30 | 0.934 | 16:30 | 4.108 | 22:30 | 4.522 |
| 1:35 | 2.648 | 4:45 | 0.276 | 10:45 | 1.003 | 16:45 | 4.131 | 22:45 | 4.536 |
| 1:40 | 2.673 | 5:00 | 0.278 | 11:00 | 1.086 | 17:00 | 4.154 | 23:00 | 4.549 |
| 1:45 | 2.695 | 5:15 | 0.313 | 11:15 | 1.182 | 17:15 | 4.177 | 23:15 | 4.563 |
| 1:50 | 2.717 | 5:30 | 0.331 | 11:30 | 1.302 | 17:30 | 4.200 | 23:30 | 4.577 |
| 1:55 | 2.739 | 5:45 | 0.350 | 11:45 | 1.780 | 17:45 | 4.223 | 23:45 | 4.591 |
| 2:00 | 2.764 | | | | | | | | |

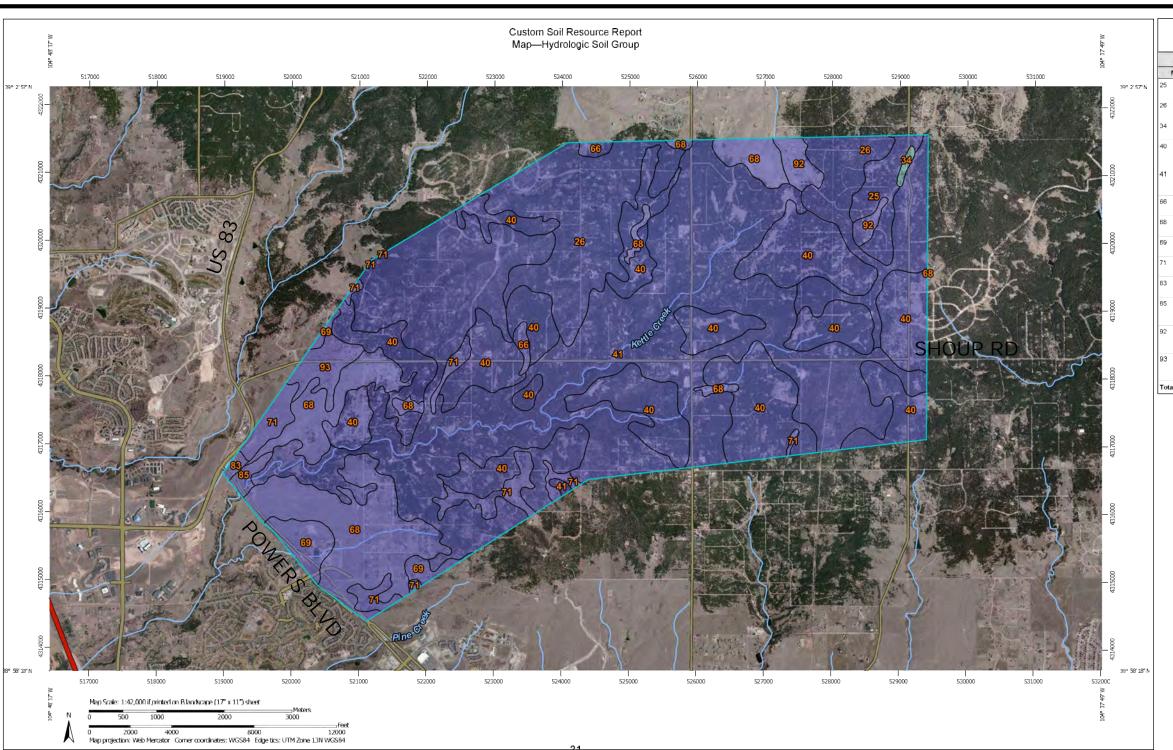
*DARFs not used for sub-basins (<1 sq mi).



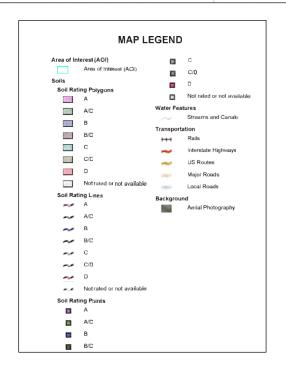


HYDROLOGIC DATA — DESIGN STORM 50 & 100 YR KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B-6



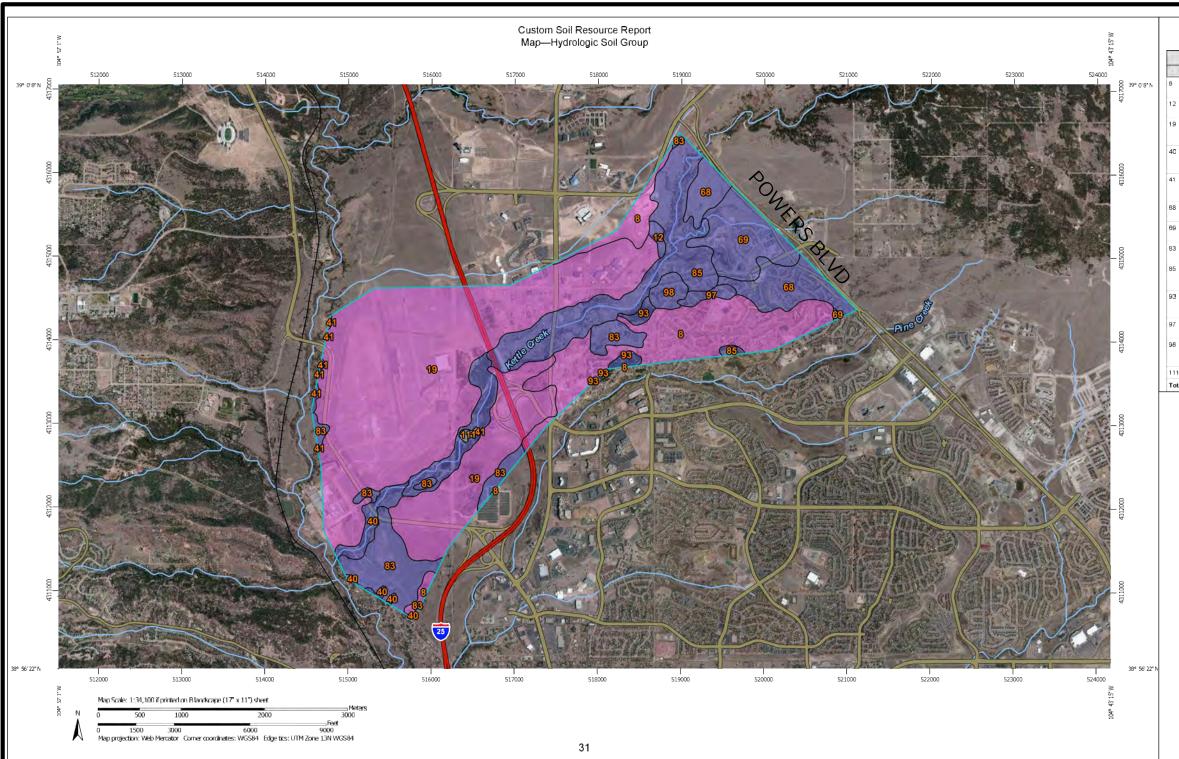


| Hydr | ologic Soil Group— Summi | ary by Map Unit — El Pa | so County Area, Colorado (C | 0625) |
|--------------------------|--|-------------------------|-----------------------------|----------------|
| Map unit symbol | Map unit name | Rating | Acres in AOI | Percent of AOI |
| 25 | Elbeth sandy loam, 3 to 8 percent slopes | В | 198.1 | 1.79 |
| 26 | Elbeth sandy loam, 8 to 15 percent slopes | В | 1,562.3 | 13.5 |
| 34 | Holderness loam, 1 to 5 percent slopes | С | 15.5 | 0.19 |
| 40 | Kettle gravelly loamy sand, 3 to 8 percent slopes | В | 3,089.3 | 26.79 |
| 41 | Kettle gravelly loarny sand, 8 to 40 percent slopes | В | 4,596.5 | 39.8 |
| 66 | Peyton sandy loam, 1 to 5 percent slopes | В | 51.1 | 0.49 |
| 68 | Peyton-Pring complex, 3 to 8 percent slopes | В | 1,205.5 | 10.4 |
| 69 | Peyton-Pring complex, 8 to 15 percent slopes | В | 186.8 | 1.69 |
| 71 | Pring coarse sandy loam, 3 to 8 percent slopes | В | 340.9 | 2.99 |
| B3 | Stapleton sandy loam, 3 to 8 percent slopes | В | 17.8 | 0.2 |
| 85 | Stapleton-Bernal sandy loams, 3 to 20 percent slopes | В | 38.9 | 0.39 |
| 92 | Tomah-Crowfoot loamy sands, 3 to 8 percent slopes | В | 120.7 | 1.04 |
| 93 | Tomah-Crowfoot complex, 8 to 15 percent slopes | В | 134.2 | 1.29 |
| Totals for Area of Inter | est | | 11,557.7 | 100.09 |



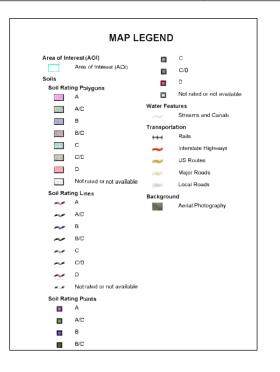
APPENDIX B — HYDROLOGIC SOIL GROUP MAP KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B-7





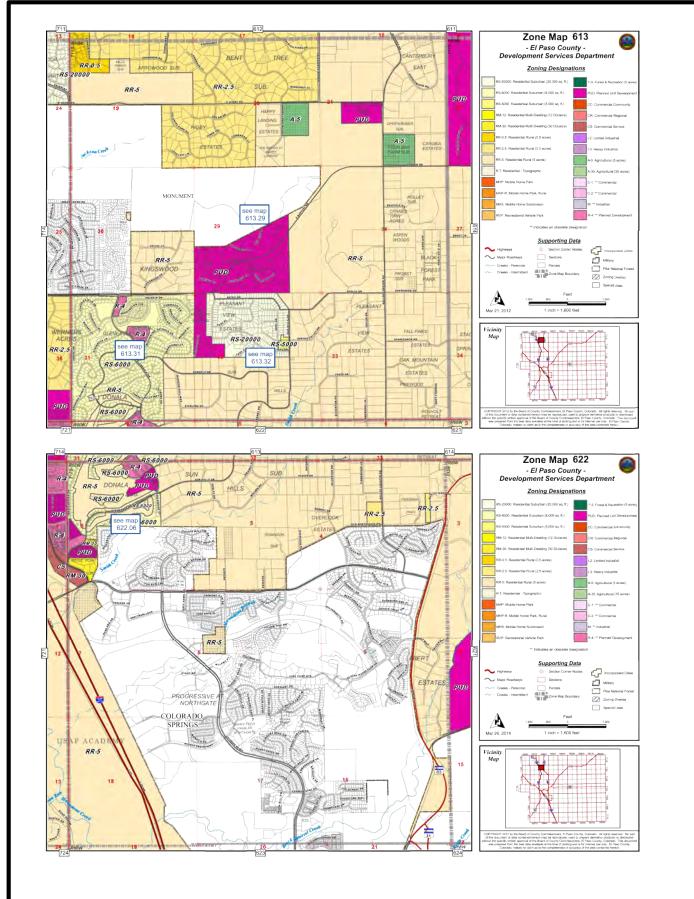
Table—Hydrologic Soil Group

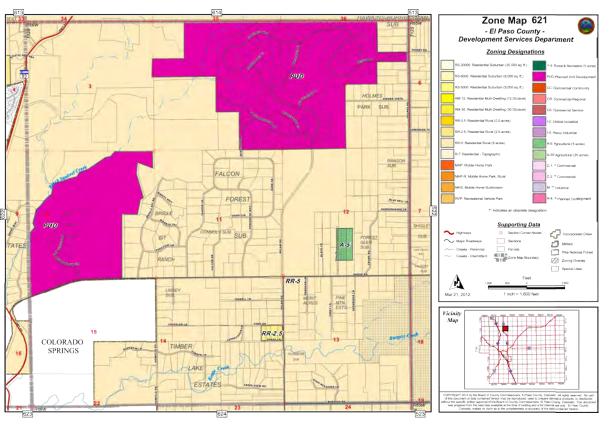
| Map unit symbol | Map unit name | Rating | Acres in AOI | Percent of AOI |
|--------------------------|--|---------|--|------------------|
| | 2014 20 10012 1001 | 174-75 | The second secon | 1,7417-9070-2356 |
| В | Blakeland loarny sand, 1 to 9 percent slopes | A | 523.1 | 14.6% |
| 12 | Bresser sandy loam, 3 to 5 percent slopes | В | 12.6 | 0.4% |
| 19 | Columbine gravelly sandy loam, 0 to 3 percent slopes | A | 1,762.3 | 49.1% |
| 40 | Kettle gravelly loarny sand, 3 to 8 percent slopes | В | 59.3 | 1.7% |
| 41 | Kettle gravelly loamy sand, 8 to 40 percent slopes | В | 103.8 | 2.9% |
| 68 | Peyton-Pring complex, 3 to 8 percent slopes | В | 199.8 | 5.6% |
| 69 | Peyton-Pring complex, 8 to 15 percent slopes | В | 191.2 | 5.3% |
| 83 | Stapleton sandy loam, 3 to 8 percent slopes | В | 250.4 | 7.0% |
| 85 | Stapleton-Bernal sandy loams, 3 to 20 percent slopes | В | 391.5 | 10.9% |
| 93 | Tomah-Crowfoot complex, 8 to 15 percent stopes | В | 28.1 | 0.8% |
| 97 | Truckton sandy loam, 3 to 9 percent slopes | В | 22.5 | 0.6% |
| 98 | Truckton-Blakeland complex, 9 to 20 percent slopes | В | 36.8 | 1.0% |
| 111 | Water | | 5.6 | 0.2% |
| Totals for Area of Inter | net | 3,587.0 | 100.0% | |



APPENDIX B — HYDROLOGIC SOIL GROUP MAP KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B-8

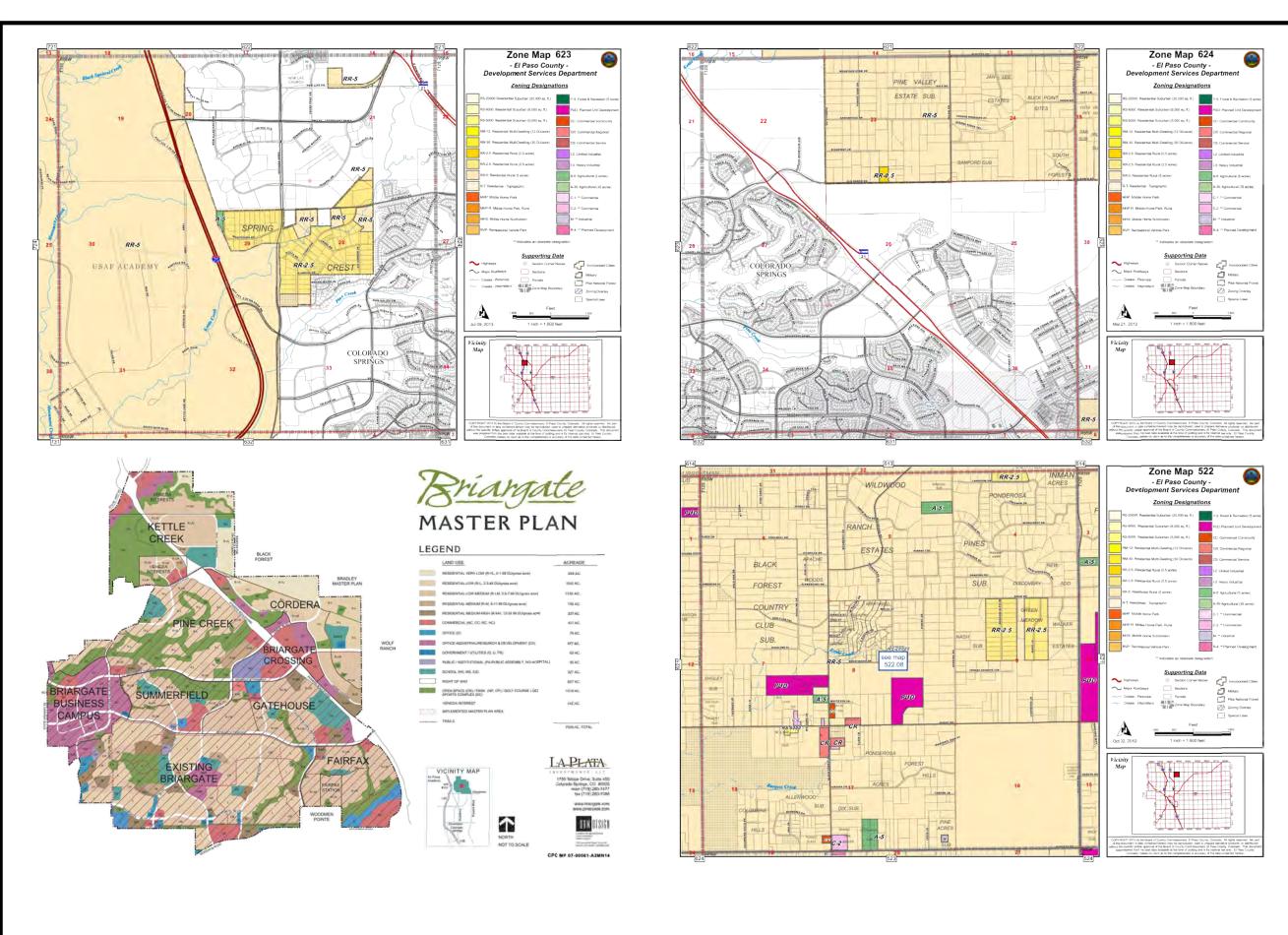






APPENDIX B — ZONING MAPS KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B-9

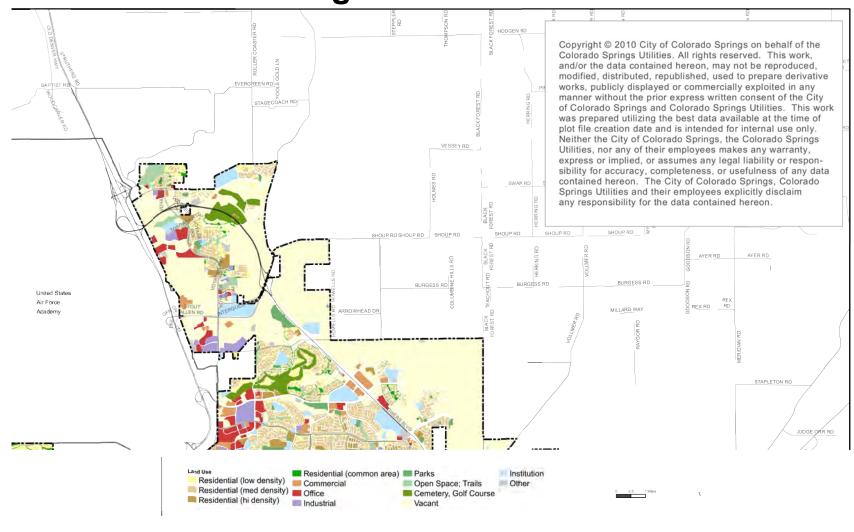


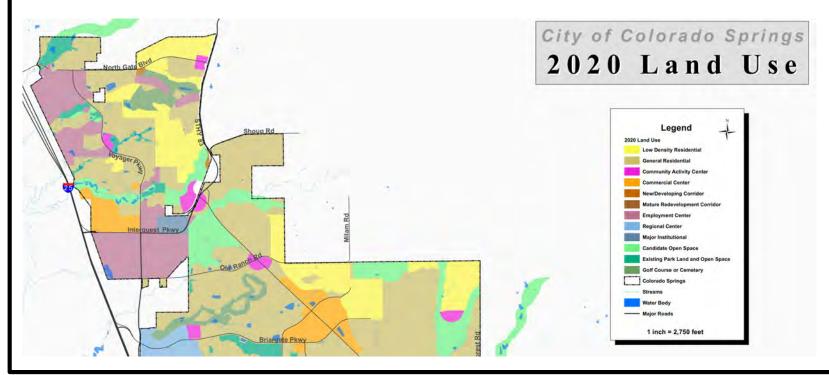


APPENDIX B - ZONING MAPS KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B-10



Existing Land Use





APPENDIX B - ZONING MAPS KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B-11



| 1 2 3 4 5 5 | nrea (mi) 1.263 0.586 0.180 0.195 0.623 1.333 0.183 | Area (ac) 808 375 115 125 399 853 | Soil Type A Area (ac) 0 0 0 0 | Soil Type A Area (%) 0.0% 0.0% 0.0% | Soil Type B Area (ac) 808 375 | Area (%) 100.0% | (ac) | 2 41 Herbaceous, Good Condition, HSG B (ac) | 2 34 Woods, Good Condition, HSG B (ac) | Composite CN Value | Initial Abstraction | Percent |
|--------------------------------|--|---|-------------------------------|---|--|--|---|---|--|-----------------------|---------------------|------------|
| 1 2 3 4 5 | 1.263 0.586 0.180 0.195 0.623 1.333 0.183 | Area (ac) 808 375 115 125 399 | Area (ac) 0 0 0 0 0 | Area (%) 0.0% 0.0% 0.0% | Soil Type B Area (ac) 808 375 | CN Values ¹ Soil Type B Area (%) 100.0% | Meadows, Good Condition, HSG A (ac) | Herbaceous, Good Condition, HSG B | Woods, Good Condition, HSG B | • | | Percent |
| 1 2 3 4 5 | 1.263 0.586 0.180 0.195 0.623 1.333 0.183 | Area (ac) 808 375 115 125 399 | Area (ac) 0 0 0 0 0 | Area (%) 0.0% 0.0% 0.0% | Soil Type B Area (ac) 808 375 | Soil Type B Area (%) 100.0% | Meadows, Good Condition, HSG A (ac) | Herbaceous, Good Condition, HSG B | Woods, Good Condition, HSG B | • | | Percent |
| 1 2 3 4 5 | 1.263 0.586 0.180 0.195 0.623 1.333 0.183 | Area (ac) 808 375 115 125 399 | Area (ac) 0 0 0 0 0 | Area (%) 0.0% 0.0% 0.0% | Area (ac) 808 375 | Area (%) 100.0% | Condition, HSG A (ac) | Condition, HSG B | Condition, HSG B | • | | Percent |
| 1 2 3 4 5 | 1.263 0.586 0.180 0.195 0.623 1.333 0.183 | Area (ac) 808 375 115 125 399 | Area (ac) 0 0 0 0 0 | Area (%) 0.0% 0.0% 0.0% | Area (ac) 808 375 | Area (%) 100.0% | (ac) | · | | • | | Percent |
| 1 2 3 4 5 | 1.263 0.586 0.180 0.195 0.623 1.333 0.183 | 808 375 115 125 399 | 0 0 0 0 | 0.0% 0.0% 0.0% | 808 375 | 100.0% | | (ac) | (ac) | CN Value | l (in) | |
| 2 3 4 5 | 0.586 0.180 0.195 0.623 1.333 0.183 | 375 115 125 399 | 0 0 0 | 0.0% 0.0% | 375 | | | | , , | | (in) | Impervious |
| 3 4 5 | 0.180 0.195 0.623 1.333 0.183 | 115 125 399 | 0 | 0.0% | | | 0 | 92 | 716 | 35 | 1.87 | 2.0 |
| 4 5 | 0.195 0.623 1.333 0.183 | 125 399 | 0 | | | 100.0% | 0 | 35 | 340 | 35 | 1.89 | 2.0 |
| 5 | 0.623 1.333 0.183 | 399 | | 0.0% | 115 | 100.0% | 0 | 9 | 106 | 35 | 1.89 | 2.0 |
| | 1.333 0.183 | | 0 | | 125 | 100.0% | 0 | 0 | 125 | 34 | 1.94 | 2.0 |
| 6 | 0.183 | 853 | | 0.0% | 399 | 100.0% | 0 | 19 | 380 | 34 | 1.91 | 2.0 |
| | | | 0 | 0.0% | 853 | 100.0% | 0 | 51 | 802 | 34 | 1.91 | 2.0 |
| | | 117 | 0 | 0.0% | 117 | 100.0% | 0 | 11 | 106 | 35 | 1.89 | 2.0 |
| | 0.288 | 184 | 0 | 0.0% | 184 | 100.0% | 0 | 0 | 184 | 34 | 1.94 | 2.0 |
| | 1.177 | 753 | 0 | 0.0% | 753 | 100.0% | 0 | 139 | 614 | 35 | 1.83 | 2.0 |
| | 0.222 | 142 | 0 | 0.0% | 142 | 100.0% | 0 | 0 | 142 | 34 | 1.94 | 2.0 |
| | 0.880 | 563 | 0 | 0.0% | 563 | 100.0% | 0 | 6 | 557 | 34 | 1.93 | 2.0 |
| | 0.552 | 353 | 0 | 0.0% | 353 | 100.0% | 0 | 70 | 283 | 35 | 1.83 | 2.0 |
| | 1.156 | 740 | 0 | 0.0% | 740 | 100.0% | 0 | 70 | 670 | 35 | 1.88 | 2.0 |
| | 0.516 | 330 | 0 | 0.0% | 330 | 100.0% | 0 | 115 | 215 | 36 | 1.74 | 2.0 |
| | 0.498 | 319 | 0 | 0.0% | 319 | 100.0% | 0 | 90 | 229 | 36 | 1.78 | 2.0 |
| | 0.819 | 524 | 0 | 0.0% | 524 | 100.0% | 0 | 67 | 457 | 35 | 1.87 | 2.0 |
| | 0.788 | 504 | 0 | 0.0% | 504 | 100.0% | 0 | 58 | 446 | 35 | 1.87 | 2.0 |
| | 0.192 | 123 | 0 | 0.0% | 123 | 100.0% | 0 | 23 | 100 | 35 | 1.83 | 2.0 |
| | 0.552 | 353 | 0 | 0.0% | 353 | 100.0% | 0 | 148 | 205 | 37 | 1.71 | 2.0 |
| | 0.594 | 380 | 0 | 0.0% | 380 | 100.0% | 0 | 238 | 142 | 38 | 1.61 | 2.0 |
| | 0.417 | 267 | 0 | 0.0% | 267 | 100.0% | 0 | 197 | 70 | 39 | 1.55 | 2.0 |
| | 0.200 | 128 | 0 | 0.0% | 128 | 100.0% | 0 | 128 | 0 | 41 | 1.44 | 2.0 |
| | 0.123 | 79 | 0 | 0.0% | 79 | 100.0% | 0 | 79 | 0 | 41 | 1.44 | 2.0 |
| | 0.453 | 290 | 0 | 0.0% | 290 | 100.0% | 0 | 290 | 0 | 41 | 1.44 | 2.0 |
| 25 | 0.169 | 108 | 0 | 0.0% | 108 | 100.0% | 0 | 108 | 0 | 41 | 1.44 | 2.0 |
| 26 | 0.480 | 307 | 0 | 0.0% | 307 | 100.0% | 0 | 307 | 0 | 41 | 1.44 | 2.0 |
| | 0.294 | 188 | 0 | 0.0% | 188 | 100.0% | 0 | 188 | 0 | 41 | 1.44 | 2.0 |
| | 0.264 | 169 | 0 | 0.0% | 169 | 100.0% | 0 | 169 | 0 | 41 | 1.44 | 2.0 |
| | 0.172 | 110 | 0 | 0.0% | 110 | 100.0% | 0 | 110 | 0 | 41 | 1.44 | 2.0 |
| | 0.364 | 233 | 0 | 0.0% | 233 | 100.0% | 0 | 233 | 0 | 41 | 1.44 | 2.0 |
| | 0.377 | 241 | 144 | 59.8% | 97 | 40.2% | 107 | 134 | 0 | 29 | 2.39 | 2.0 |
| | 0.316 | 202 | 121 | 59.9% | 81 | 40.1% | 90 | 112 | 0 | 29 | 2.40 | 2.0 |
| | 0.184 | 118 | 42 | 35.6% | 76 | 64.4% | 43 | 75 | 0 | 32 | 2.17 | 2.0 |
| Total/Avg. | 16.406 | 10,500 | 307 | 2.9% | 10,193 | 97.1% | 240 | 3,371 | 6,889 | 35.8 | 1.81 | 2.0 |
| ¹ Uses Pre-Developm | nent curve nu | umbers (ARC | C-I) | | | | | | | | | |

APPENDIX B — HYDROLOGIC DATA — HISTORIC KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B-12



| | | | | Historic I | and Use | and Curve | Number Data (| 24-Hour Duration S | torms) ² | | | |
|-----------------------------|----------------|-------------|-----------|-------------|-----------|------------------------|---------------|--------------------|---------------------|-----------|---------------------|------------|
| | | | | | | % Imperv. | 2 | 2 | 2 | | | |
| | | | | | | _ | 2 | 2 | | | | |
| | | | | | | CN Values ² | 39 | 62 | 55 | | | |
| | | | | | | | Meadows, Good | Herbaceous, Good | Woods, Good | | | |
| | | | | Soil Type A | | | | Condition, HSG B | Condition, HSG B | Composite | Initial Abstraction | Percent |
| Basin number | Area (mi) | Area (ac) | Area (ac) | Area (%) | Area (ac) | Area (%) | (ac) | (ac) | (ac) | CN Value | (in) | Impervious |
| 1 | 1.263 | 808 | 0 | 0.0% | 808 | 100.0% | 0 | 92 | 716 | 56 | 0.79 | 2.0 |
| 2 | 0.586 | 375 | 0 | 0.0% | 375 | 100.0% | 0 | 35 | 340 | 56 | 0.80 | 2.0 |
| 3 | 0.180 | 115 | 0 | 0.0% | 115 | 100.0% | 0 | 9 | 106 | 56 | 0.80 | 2.0 |
| 4 | 0.195 | 125 | 0 | 0.0% | 125 | 100.0% | 0 | 0 | 125 | 55 | 0.82 | 2.0 |
| 5 | 0.625 | 400 | 0 | 0.0% | 400 | 100.0% | 0 | 20 | 380 | 55 | 0.81 | 2.0 |
| 6 | 1.333 | 853 | 0 | 0.0% | 853 | 100.0% | 0 | 51 | 802 | 55 | 0.80 | 2.0 |
| 7 | 0.183 | 117 | 0 | 0.0% | 117 | 100.0% | 0 | 11 | 106 | 56 | 0.80 | 2.0 |
| 8 | 0.288 | 184 | 0 | 0.0% | 184 | 100.0% | 0 | 0 | 184 | 55 | 0.82 | 2.0 |
| 9 | 1.177 | 753 | 0 | 0.0% | 753 | 100.0% | 0 | 139 | 614 | 56 | 0.78 | 2.0 |
| 10 | 0.222 | 142 | 0 | 0.0% | 142 | 100.0% | 0 | 0 | 142 | 55 | 0.82 | 2.0 |
| 11 | 0.880 | 563 | 0 | 0.0% | 563 | 100.0% | 0 | 6 | 557 | 55 | 0.82 | 2.0 |
| 12 | 0.552 | 353 | 0 | 0.0% | 353 | 100.0% | 0 | 70 | 283 | 56 | 0.77 | 2.0 |
| 13 | 1.156 | 740 | 0 | 0.0% | 740 | 100.0% | 0 | 70 | 670 | 56 | 0.80 | 2.0 |
| 14 | 0.516 | 330 | 0 | 0.0% | 330 | 100.0% | 0 | 115 | 215 | 57 | 0.74 | 2.0 |
| 15 | 0.498 | 319 | 0 | 0.0% | 319 | 100.0% | 0 | 90 | 229 | 57 | 0.76 | 2.0 |
| 16 | 0.819 | 524 | 0 | 0.0% | 524 | 100.0% | 0 | 67 | 457 | 56 | 0.79 | 2.0 |
| 17 | 0.788 | 504 | 0 | 0.0% | 504 | 100.0% | 0 | 58 | 446 | 56 | 0.79 | 2.0 |
| 18 | 0.192 | 123 | 0 | 0.0% | 123 | 100.0% | 0 | 23 | 100 | 56 | 0.78 | 2.0 |
| 19 | 0.552 | 353 | 0 | 0.0% | 353 | 100.0% | 0 | 148 | 205 | 58 | 0.73 | 2.0 |
| 20 | 0.594 | 380 | 0 | 0.0% | 380 | 100.0% | 0 | 238 | 142 | 59 | 0.68 | 2.0 |
| 21 | 0.417 | 267 | 0 | 0.0% | 267 | 100.0% | 0 | 197 | 70 | 60 | 0.66 | 2.0 |
| 22 | 0.200 | 128 | 0 | 0.0% | 128 | 100.0% | 0 | 128 | 0 | 62 | 0.61 | 2.0 |
| 23 | 0.123 | 79 | 0 | 0.0% | 79 | 100.0% | 2 | 77 | 0 | 61 | 0.63 | 2.0 |
| 24 | 0.453 | 290 | 0 | 0.0% | 290 | 100.0% | 0 | 290 | 00 | 62 | 0.61 | 2.0 |
| 25 | 0.169 | 108 | 0 | 0.0% | 108 | 100.0% | 0 | 108 | 0 | 62 | 0.61 | 2.0 |
| 26 | 0.480 | 307 | 0 | 0.0% | 307 | 100.0% | 0 | 307 | 0 | 62 | 0.61 | 2.0 |
| 27 | 0.294 | 188 | 0 | 0.0% | 188 | 100.0% | 0 | 188 | 0 | 62 | 0.61 | 2.0 |
| 28 | 0.264 | 169 | 0 | 0.0% | 169 | 100.0% | 0 | 169 | 00 | 62 | 0.61 | 2.0 |
| 29 | 0.172 | 110 | 0 | 0.0% | 110 | 100.0% | 0 | 110 | 0 | 62 | 0.61 | 2.0 |
| 30 | 0.364 | 233 | 0 | 0.0% | 233 | 100.0% | 0 | 233 | 0 | 62 | 0.61 | 2.0 |
| 31 | 0.377 | 241 | 144 | 59.8% | 97 | 40.2% | 107 | 134 | 0 | 52 | 0.93 | 2.0 |
| 32 | 0.316 | 202 | 121 | 59.9% | 81 | 40.1% | 90 | 112 | 0 | 52 | 0.93 | 2.0 |
| 33 | 0.184 | 118 | 42 | 35.6% | 76 | 64.4% | 43 | 75 | 0 | 54 | 0.87 | 2.0 |
| Total/Avg. | 16.408 | 10,501 | 307 | 2.9% | 10,194 | 97.1% | 242 | 3,370 | 6,889 | 56.9 | 0.76 | 2.0 |
| ² Uses Post-Deve | elopment curve | numbers (AF | RC-II) | | | | | | | | | |

APPENDIX B — HYDROLOGIC DATA — HISTORIC KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B-13



| | | | | | | | | Ex | isting Land | d Use and C | urve N | umber Da | ata (2-Hour & | 24-Hour Du | ration Sto | rms) ¹ | | | | | | | |
|----------------------|-----------|------------|--------------|-------------|-----------|-------------|----------|----------|-------------|-------------|---------|----------|-----------------|----------------|-------------|-------------------|---------------|----------------|----------------|---------|-----------|-------------|------------|
| | | | | | | % Imperv. | 100 | 100 | 95 | 85 | 40 | 2 | 2 | 15 | 15 | 20 | 35 | 5 60 |) 60 | 10 |) | | |
| | | | | | | C values | 83 | | 89 | | 72 | 39 | 62 | | | 65 | | | | | | | |
| | | | | | | C values | 0.5 | 0.5 | - 03 | 32 | 72 | 33 | _ | Residential (5 | Residential | | | 01 | . 73 | / /- | | | |
| | | | | | | | | | Commercial | Commercial | | | Herbaceous, | aclots) | (5 ac lots) | (2.5 ac lots) | (0.5 ac lots) | Residential | Residential | | | | |
| | | | | | Soil Type | | Asphalt, | Asphalt, | Office, | Retail, | School, | Meadows, | Good Condition, | Herbaceous, | Wooded, | Wooded, | Wooded, | (0.25 ac lots) | (0.25 ac lots) | Special | | Initial | ' |
| Basin | | | Soil Type A | Soil Type A | | Soil Type B | - | HSG B | HSG A | HSG B | HSG B | HSG A | HSG B | HSG B | HSG B | HSG B | HSG B | HSG A | HSG B | Uses | Composite | Abstraction | Percent |
| number | Area (mi) | Area (ac) | | Area (%) | (ac) | Area (%) | (ac) | (ac) | (ac) | (ac) | (ac) | (ac) | (ac) | (ac) | (ac) | (ac) | (ac) | (ac) | (ac) | (ac) | CN Value | (in) | Impervious |
| 1 | 1.263 | 808 | 0 | 0.0% | 808 | 100.0% | | 24 | | | | | | 72 | 525 | 130 | 57 | | | | 66 | 0.51 | 19.7 |
| 2 | 0.586 | 375 | 0 | 0.0% | 375 | 100.0% | | 5 | | | | | | 36 | 260 | | 74 | | | | 66 | 0.51 | 20.1 |
| 3 | 0.180 | 115 | 0 | 0.0% | 115 | 100.0% | | 11 | | | | | | 9 | 70 | | 25 | | | | 68 | 0.46 | 27.5 |
| 4 | 0.195 | 125 | 0 | 0.0% | 125 | 100.0% | | | | | 8 | | | 4 | 113 | | | | | | 65 | 0.53 | 16.6 |
| 5 | 0.625 | 400 | 0 | 0.0% | 400 | 100.0% | | 19 | | 10 | | | | 20 | 255 | | 10 | | | 86 | 69 | 0.45 | 20.2 |
| 6 | 1.333 | 853 | 0 | 0.0% | 853 | 100.0% | | | | | 1 | | | 52 | 789 | | 11 | | | | 65 | 0.54 | 15.3 |
| 7 | 0.183 | 117 | 0 | 0.0% | 117 | 100.0% | | 1 | | | | | | 12 | 98 | | | | | 6 | 66 | 0.52 | 15.5 |
| 8 | 0.288 | 184 | 0 | 0.0% | 184 | 100.0% | | 8 | | | | | | | 96 | | | | | 80 | 70 | 0.43 | 16.5 |
| 9 | 1.177 | 753 | 0 | 0.0% | 753 | 100.0% | | 32 | | 5 | | | | 140 | 564 | | 12 | | | | 66 | 0.51 | 19.4 |
| 10 | 0.222 | 142 | 0 | 0.0% | 142 | 100.0% | | | | | | | | | 142 | | | | | | 65 | 0.54 | 15.0 |
| 11 | 0.880 | 563 | 0 | 0.0% | 563 | 100.0% | | 24 | | 22 | | | | 10 | 259 | | 66 | | | 182 | 71 | 0.42 | 22.1 |
| 12 | 0.552 | 353 | 0 | 0.0% | 353 | 100.0% | | 10 | | | | | | 70 | 171 | | 17 | | | 85 | 68 | 0.47 | 17.2 |
| 13 | 1.156 | 740 | 0 | 0.0% | 740 | 100.0% | | 19 | | | | | | 90 | 631 | | | | | | 66 | 0.52 | 17.2 |
| 14 | 0.516 | 330 | 0 | 0.0% | 330 | 100.0% | | 3 | | | | | | 115 | 212 | | | | | | 65 | 0.53 | 15.8 |
| 15 | 0.498 | 319 | 0 | 0.0% | 319 | 100.0% | | 8 | | | | | | 90 | 221 | | | | | | 66 | 0.52 | 17.1 |
| 16 | 0.819 | 524 | 0 | 0.0% | 524 | 100.0% | | 31 | | | | | | 65 | 428 | | | | | | 66 | 0.51 | 20.0 |
| 17 | 0.788 | 504 | 0 | 0.0% | 504 | 100.0% | | 5 | | | | | | 58 | 441 | | | | | | 65 | 0.53 | 15.8 |
| 18 | 0.192 | 123 | 0 | 0.0% | 123 | 100.0% | | 1 | | | | | | 23 | 99 | | | | | | 65 | 0.53 | 15.7 |
| 19 | 0.552 | 353 | 0 | 0.0% | 353 | 100.0% | | 5 | | | | | 19 | 131 | 198 | | | | | | 65 | 0.53 | 15.5 |
| 20 | 0.594 | 380 | 0 | 0.0% | 380 | 100.0% | | 7 | | | | | 123 | 120 | 130 | | | | | | 64 | 0.55 | 12.4 |
| 21 | 0.417 | 267 | 0 | 0.0% | 267 | 100.0% | | | | | | | 111 | 69 | 87 | | | | | | 64 | 0.57 | 9.6 |
| 22 | 0.200 | 128 | 0 | 0.0% | 128 | 100.0% | | | | | | | 119 | 6 | 3 | | | | | | 62 | 0.61 | 2.9 |
| 23 | 0.123 | 79 | 0 | 0.0% | 79 | 100.0% | | 3 | | | | 2 | 74 | | | | | | | | 62 | 0.60 | 5.7 |
| 24 | 0.453 | 290 | 0 | 0.0% | 290 | 100.0% | | 20 | | | | | 145 | 84 | 31 | | | | 10 | | 66 | 0.53 | 15.9 |
| 25 | 0.169 | 108 | 35 | 32.4% | 73 | 67.6% | | 7 | | | | | 7 | | | | | 32 | 62 | | 71 | 0.41 | 58.8 |
| 26 | 0.480 | 307 | 0 | 0.0% | 307 | 100.0% | | 16 | | | | | 123 | 108 | 21 | | | | 39 | | 66 | 0.51 | 19.9 |
| 27 | 0.294 | 188 | 0 | 0.0% | 188 | 100.0% | | 8 | | | 50 | | 75 | | | | | | 55 | | 70 | 0.44 | 33.2 |
| 28 | 0.264 | 169 | 0 | 0.0% | 169 | 100.0% | | | | | | | 169 | | | | | | | | 62 | 0.61 | 2.0 |
| 29 | 0.172 | 110 | 0 | 0.0% | 110 | 100.0% | | 5 | | | | | 105 | | | | | | | | 63 | 0.58 | 6.5 |
| 30 | 0.364 | 233 | 0 | 0.0% | 233 | 100.0% | | 18 | | | | | 185 | | | | | | 30 | | 66 | 0.52 | 17.0 |
| 31 | 0.377 | 241 | 144 | 59.8% | 97 | 40.2% | 2 | 1 | | | | 59 | 81 | | | | | 48 | 50 | | 59 | 0.69 | 26.8 |
| 32 | 0.316 | 202 | 121 | 59.9% | 81 | 40.1% | 5 | 5 | 29 | 7 | | 65 | 91 | | | | | | | | 61 | 0.65 | 23.1 |
| 33 | 0.184 | 118 | 42 | 35.6% | 76 | 64.4% | | | | | | 43 | 75 | | | | | | | | 54 | 0.87 | 2.0 |
| Total | 16.408 | 10,501 | 342 | 3.3% | 10,159 | 96.7% | 7 | 296 | 29 | 44 | 59 | 169 | 1502 | 1,384 | 5,844 | 130 | 272 | 80 | 246 | 439 | 66 | 0.52 | 17.8 |
| Percent | | | | | | | 0.07% | 2.82% | 0.28% | 0.42% | 0.56% | 1.61% | 14.30% | 13.18% | 55.65% | 1.24% | 2.59% | 0.76% | 2.34% | 4.18% | | | |
| ¹ Uses Po | st-Develo | pment curv | ve numbers (| ARC-II) | | | | | | | | | | | | | | | | | | | |

NOTE

1. SUBBASINS 24-27 DATA HAS BEEN REPLACED WITH KETTLE CREEK DRAINAGE BASIN OLD RANCH ROAD TRIBUTARY MASTER DEVELOPMENT PLAN FLOW DATA (JR ENG. 2001)

APPENDIX B — HYDROLOGIC DATA — EXISTING KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B-14



| | | | | | | | | Fu | uture Land | Use and Cu | ırve Nı | ımber Dat | ta (2-Hour & 2 | 24-Hour Dur | ation Stor | ms) ¹ | | | | | | | |
|----------|----------------|--------------|--------------------|---------------|------------|-----------------|----------|---------------|-----------------------|-----------------------|---------|-----------|--|---|---------------------------------------|---|---|-------|-------------------------------|---------|-----------|--------------|--------------|
| | | | | | | % Imperv. | 100 | 100 | 95 | 85 | 40 | 2 | 2 | 15 | 15 | 20 | 35 | 60 | 60 | 10 | | | |
| | | | | | | CN values | 83 | 89 | 89 | | 72 | 39 | 62 | 65 | 65 | 65 | 70 | | 75 | 74 | | | |
| | | | | | Soil Type | | Asphalt, | Asphalt, | Commercial Office, | Commercial Retail, | School, | Meadows, | Open Space Herbaceous, Good Condition, | Residential (5 ac lots) Herbaceous, | Residential (5 ac lots) Wooded, | Residential (2.5 ac lots) Wooded, | Residential (0.5 ac lots) Wooded, | | Residential (0.25 ac lots) | Special | | Initial | |
| Basin | | | Soil Type A | Soil Type A | B Area | Soil Type B | HSG A | HSG B | HSG A | HSG B | HSG B | HSG A | HSG B | HSG B | HSG B | HSG B | HSG B | HSG A | HSG B | Uses | Composite | Abstraction | |
| number | Area (mi) | ` ′ | Area (ac) | Area (%) | (ac) | Area (%) | (ac) | (ac) | (ac) | (ac) | (ac) | (ac) | (ac) | (ac) | (ac) | (ac) | (ac) | (ac) | (ac) | (ac) | CN Value | (in) | Impervious |
| 2 | 1.263 0.586 | 808 375 | 0 | 0.0% | 808 375 | 100.0% | | 24 5 | | | | | | 72 36 | 525 260 | 130 | 57 74 | | | | 66 66 | 0.51 0.51 | 19.7 |
| 3 | 0.380 | 115 | 0 | 0.0% | 115 | 100.0% | | 11 | | | | | | 9 | 70 | | 25 | | | | 68 | 0.46 | 27.5 |
| 4 | 0.195 | 125 | 0 | 0.0% | 125 | 100.0% | | 11 | | | 8 | | | 4 | 113 | | 23 | | | | 65 | 0.53 | 16.6 |
| 5 | 0.625 | 400 | 0 | 0.0% | 400 | 100.0% | | 19 | | 10 | | | | 20 | 255 | | 10 | | | 86 | 69 | 0.45 | 20.2 |
| 6 | 1.333 | 853 | 0 | 0.0% | 853 | 100.0% | | | | | 1 | | | 52 | 789 | | 11 | | | | 65 | 0.54 | 15.3 |
| 7 | 0.183 | 117 | 0 | 0.0% | 117 | 100.0% | | 1 | | | | | | 12 | 98 | | | | | 6 | 66 | 0.52 | 15.5 |
| 8 | 0.288 | 184 | 0 | 0.0% | 184 | 100.0% | | 8 | | | | | | | 96 | | | | | 80 | 70 | 0.43 | 16.5 |
| 9 | 1.177 | 753 | 0 | 0.0% | 753 | 100.0% | | 32 | | 5 | | | | 140 | 564 | | 12 | | | | 66 | 0.51 | 19.4 |
| 10 | 0.222 | 142 | 0 | 0.0% | 142 | 100.0% | | | | | | | | | 142 | | | | | | 65 | 0.54 | 15.0 |
| 11 | 0.880 | 563 | 0 | 0.0% | 563 | 100.0% | | 24 | | 22 | | | | 10 | 259 | | 66 | | | 182 | 71 | 0.42 | 22.1 |
| 12 | 0.552 1.156 | 353 740 | 0 | 0.0% | 353 740 | 100.0% | | 10 19 | | | | | | 70 90 | 171 631 | | 17 | | | 85 | 68 66 | 0.47 0.52 | 17.2 17.2 |
| 14 | 0.516 | 330 | 0 | 0.0% | 330 | 100.0% | | 3 | | | | | | 115 | 212 | | | | | | 65 | 0.52 | 15.8 |
| 15 | 0.498 | 319 | 0 | 0.0% | 319 | 100.0% | | 8 | | | | | | 90 | 221 | | | | | | 66 | 0.52 | 17.1 |
| 16 | 0.819 | 524 | 0 | 0.0% | 524 | 100.0% | | 31 | | | | | | 65 | 428 | | | | | | 66 | 0.51 | 20.0 |
| 17 | 0.788 | 504 | 0 | 0.0% | 504 | 100.0% | | 5 | | | | | | 58 | 441 | | | | | | 65 | 0.53 | 15.8 |
| 18 | 0.192 | 123 | 0 | 0.0% | 123 | 100.0% | | 1 | | | | | | 23 | 99 | | | | | | 65 | 0.53 | 15.7 |
| 19 | 0.552 | 353 | 0 | 0.0% | 353 | 100.0% | | 5 | | | | | | 131 | 198 | | | | 19 | | 66 | 0.52 | 18.6 |
| 20 | 0.594 | 380 | 0 | 0.0% | 380 | 100.0% | | 7 | | | | | 15 | 120 | 130 | | | | 108 | | 68 | 0.47 | 28.8 |
| 21 | 0.417 | 267 | 0 | 0.0% | 267 | 100.0% | | | | | 6 | | 91 | 69 | 87 | | | | 14 | | 65 | 0.55 | 13.5 |
| 22 | 0.200 | 128 | 0 | 0.0% | 128 | 100.0% | | _ | | | | | 18 | 6 | 3 | | | | 101 | | 72 | 0.38 | 48.7 |
| 23 | 0.123 | 79 | 0 | 0.0% | 79 | 100.0% | | 3 | | 16 | | | 76 | 94 | 20 | | | | 124 | | 63 | 0.59 | 5.7 |
| 24 25 | 0.453 0.169 | 290 108 | 35 | 0.0% 32.4% | 290 73 | 100.0% 67.6% | | 20 | | 16 | | | 16 7 | 84 | 30 | | | 32 | 124 62 | | 72 71 | 0.38 0.41 | 43.2 58.8 |
| 26 | 0.480 | 307 | 0 | 0.0% | 307 | 100.0% | | 16 | | | | | 72 | 108 | 21 | | | - 32 | 90 | | 68 | 0.41 | 29.6 |
| 27 | 0.400 | 188 | 0 | 0.0% | 188 | 100.0% | | 8 | | | -50 | | 50 | 100 | | | | | 80 | | 71 | 0.40 | 41.0 |
| 28 | 0.264 | 169 | 0 | 0.0% | 169 | 100.0% | | | | | 8 | | 34 | | | | | | 127 | | 72 | 0.38 | 47.4 |
| 29 | 0.172 | 110 | 0 | 0.0% | 110 | 100.0% | | 5 | | | | | | | | | | | 105 | | 76 | 0.32 | 61.8 |
| 30 | 0.364 | 233 | 0 | 0.0% | 233 | 100.0% | | 18 | | | | | | 170 | | | | | 45 | | 69 | 0.45 | 30.3 |
| 31 | 0.377 | 241 | 144 | 59.8% | 97 | 40.2% | 2 | 1 | | | | 10 | | | | 130 | | 48 | 50 | | 65 | 0.53 | 36.5 |
| 32 | 0.316 | 202 | 121 | 59.9% | 81 | 40.1% | 5 | 5 | 102 | 12 | | | | 10 | | 63 | | | 5 | | 80 | 0.25 | 66.4 |
| 33 | 0.184 | 118 | 42 | 35.6% | 76 | 64.4% | | | | | | 43 | 75 | | | | | | | | 54 | 0.87 | 2.0 |
| Total | 16.408 | 10,501 | 342 | 3.3% | 10,159 | 96.7% | 7 | 296 | 102 | 65 | 73 | 53 | 454 | 1,564 | 5,843 | 323 | 272 | 80 | 930 | 439 | 67 | 0.49 | 23.0 |
| Percent | | ana Frei-Air | | | | | 0.07% | 2.82% | 0.97% | 0.62% | 0.70% | 0.50% | 4.32% | 14.89% | 55.64% | 3.08% | 2.59% | 0.76% | 8.86% | 4.18% | | | |
| | | om Existing | g re numbers (/ | | | | 0.00% | 0.00% | 0.70% | 0.20% | 0.13% | -1.10% | -9.98% | 1.71% | -0.01% | 1.84% | 0.00% | 0.00% | 6.51% | 0.00% | | | |

NOTE

1. SUBBASINS 24-27 DATA HAS BEEN REPLACED WITH KETTLE CREEK DRAINAGE BASIN OLD RANCH ROAD TRIBUTARY MASTER DEVELOPMENT PLAN FLOW DATA (JR ENG. 2001)

APPENDIX B — HYDROLOGIC DATA — FUTURE KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B-15



| | | | | | | | | | Tin | ne of Co | ncentrat | ion and Lag | Time Data | | | | | | | | | |
|----------------|-------------|--------|-------------|---------|-----------|-------------|---|-----------|--------------|----------|----------|--------------|-------------|----------------|--------------|---------------|----------------|--------------|--------------|---------------|-----------------|----------------|
| | | Ov | erland Flov | N | | | | Shallow | Concentrated | Flow | | | | | Con | centrated Flo |)W | | | | | |
| | | Flow | 2yr, 24hr | | Overland | | | Тор | Bottom | | | Concentrated | | | Тор | Bottom | | | Concentrated | Time of | Total Time of | 1 |
| | | Length | rainfall | | Flow time | Conveyance | | Elevation | Elevation | | Velocity | Flow time | Conveyance | Length | Elevation | Elevation | | Velocity | Flow time | concentration | Concentration | Lag time |
| Basin | Manning's n | (ft) | (in) | Slope | (hr) | Coefficient | Length | (ft) | (ft) | Slope | (ft/s) | (hr) | Coefficient | (ft) | (ft) | (ft) | Slope | (ft/s) | (hr) | (hr) | (min) | (min) |
| 1 | 0.20 | 300 | 2.1 | 65.10% | 0.15 | 9 | 2,726 | 7660 | 7410 | 9.17% | 2.73 | 0.28 | 17 | 6,820 | 7410 | 7310 | 1.47% | 2.06 | 0.92 | 1.35 | 80.99 | 48.59 |
| 2 | 0.20 | 300 | 2.1 | 9.25% | 0.33 | 9 | 2,175 | 7625 | 7500 | 5.75% | 2.16 | 0.28 | 16 | 4,907 | 7500 | 7310 | 3.87% | 3.15 | 0.43 | 1.04 | 62.65 | 37.59 |
| 3 | 0.20 | 200 | 2.1 | 4.27% | 0.33 | 10 | 6,373 | 7650 | 7370 | 4.39% | 2.10 | 0.84 | 20 | 1,131 | 7370 | 7310 | 5.31% | 4.61 | 0.07 | 1.24 | 74.34 | 44.60 |
| Reach 1 | | | | | | | | | | | | | 20 | 465 | 7310 | 7285 | 5.38% | 4.64 | 0.03 | 0.03 | 1.67 | 1.67 |
| 4 | 0.20 | 300 | 2.1 | 5.22% | 0.42 | 9 | 3,142 | 7505 | 7350 | 4.93% | 2.00 | 0.44 | 16 | 944 | 7350 | 7290 | 6.36% | 4.03 | 0.07 | 0.92 | 55.08 | 33.05 |
| Reach 2 | | | | | | | | | | | | | 20 | 1,790 | 7285 | 7250 | 1.96% | 2.80 | 0.18 | 0.18 | | 10.67 |
| 5 | 0.20 | 300 | 2.1 | 3.92% | 0.47 | 9 | 6,683 | 7517 | 7354 | 2.44% | 1.41 | 1.32 | 15 | 1,787 | 7354 | 7250 | 5.82% | 3.62 | 0.14 | 1.92 | 115.49 | |
| Reach 3 | | | | | | | | | | | | | 20 | 2,460 | 7250 | 7205 | 1.83% | 2.71 | 0.25 | 0.25 | 15.16 | 15.16 |
| 6 | 0.15 | 300 | 2.1 | 4.35% | 0.36 | 10 | 6,911 | 7650 | 7380 | 3.91% | 1.98 | 0.97 | 17 | 5,490 | 7380 | 7205 | 3.19% | 3.04 | 0.50 | 1.83 | | 65.86 |
| Reach 4 | | | | | | | | | | | | | 20 | 1,230 | 7205 | 7174 | 2.52% | 3.18 | 0.11 | 0.11 | 6.46 | 6.46 |
| 7 | 0.15 | 300 | 2.1 | 5.02% | 0.34 | 9 | 3,600 | 7455 | 7270 | 5.14% | 2.04 | 0.49 | 16 | 1,850 | 7270 | 7174 | 5.19% | 3.64 | 0.14 | 0.97 | | 34.82 |
| Reach 5 | | | | | | | | | | | | | 20 | 700 | 7174 | 7160 | 2.00% | 2.83 | 0.07 | 0.07 | 4.12 | 4.12 |
| 8 | 0.20 | 300 | 2.1 | 6.32% | 0.39 | 9 | 1,970 | 7340 | 7213 | 6.45% | 2.29 | 0.24 | 14 | 605 | 7213 | 7160 | 8.76% | 4.14 | 0.04 | 0.67 | | 23.97 |
| Reach 6 | | | | | | | | | | | | | 20 | 4,123 | 7160 | 7090 | 1.70% | 2.61 | 0.44 | 0.44 | 26.37 | 26.37 |
| 9 | 0.18 | 300 | 2.1 | 3.99% | 0.43 | 9 | 5,070 | 7668 | 7460 | 4.10% | 1.82 | 0.77 | 14 | 6,816 | 7460 | 7280 | 2.64% | 2.28 | 0.83 | 2.03 | | 73.11 |
| 10 | 0.20 | 300 | 2.1 | 3.88% | 0.47 | 9 | 2,271 | 7430 | 7320 | 4.84% | 1.98 | 0.32 | 12 | 838 | 7320 | 7280 | 4.77% | 2.62 | 0.09 | 0.88 | | 31.54 |
| Reach 7 | 2.12 | 222 | | 4 000/ | 2.22 | 2 | | | | 4.050/ | 4.00 | 0.70 | 18 | 1,470 | 7280 | 7255 | 1.70% | 2.35 | 0.17 | 0.17 | | 10.44 |
| 11 | 0.18 | 300 | 2.1 | 4.83% | 0.39 | 9 | 4,020 | 7455 | 7260 | 4.85% | 1.98 | 0.56 | 10 | 4.450 | 72.50 | 7400 | 2.450/ | 2.40 | 0.20 | 0.96 | | 34.49 |
| Reach 8 | 0.45 | 200 | 2.1 | F 000/ | 0.24 | 0 | 4.000 | 7450 | 7200 | F 440/ | 2.02 | 0.67 | 18 | 4,450 | 7260 | 7120 | 3.15% | 3.19 | 0.39 | 0.39 | | 23.23 |
| 12 | 0.15 | 200 | 2.1 | 5.06% | 0.24 | 9 | 4,890 | 7450 | 7200 | 5.11% | 2.03 | 0.67 | 17 | 3,402 | 7200 | 7120 | 2.35% | 2.61 | 0.36 | 1.27 | | 45.80 |
| Reach 9 | | | | | | | | | | | | | 18 20 | 1,670 | 7120 7090 | 7090 | 1.80% | 2.41 2.76 | 0.19 0.37 | 0.19 | | 11.54 22.15 |
| Reach 10 13 | 0.20 | 300 | 2.1 | 7.81% | 0.35 | 9 | 8,650 | 7545 | 7163 | 4.42% | 1.89 | 1.27 | 17 | 3,671 3,900 | 7163 | 7020 | 1.91% 3.67% | 3.26 | 0.37 | 0.37 1.96 | | 70.47 |
| 14 | 0.20 | 300 | 2.1 | 20.37% | 0.33 | 9 | 5,047 | 7424 | 7130 | 5.83% | 2.17 | 0.65 | 18 | 2,428 | 7130 | 7020 7020 | 4.53% | 3.83 | 0.33 | 1.96 | 117.45 60.80 | 36.48 |
| Reach 11 | 0.13 | 300 | 2.1 | 20.57/0 | 0.19 | 9 | 3,047 | 7424 | 7130 | 3.63/6 | 2.1/ | 0.03 | 20 | 2,428 | 7020 | 6990 | 1.48% | 2.43 | 0.18 | 0.23 | 13.88 | 13.88 |
| 15 | 0.20 | 300 | 2.1 | 17.32% | 0.26 | 11 | 5,510 | 7405 | 7090 | 5.72% | 2.63 | 0.58 | 17 | 2,020 | 7090 | 6990 | 4.95% | 3.78 | 0.25 | 0.23 | | 35.57 |
| Reach 12 | 0.20 | 300 | 2.1 | 17.52/0 | 0.20 | | 3,310 | 7403 | 7030 | 3.72/0 | 2.03 | 0.38 | 20 | 3,658 | 6990 | 6950 | 1.09% | 2.09 | 0.13 | 0.33 | | 29.15 |
| 16 | 0.20 | 300 | 2.1 | 12.32% | 0.19 | 9 | 7,271 | 7440 | 7070 | 5.09% | 2.03 | 0.99 | 18 | 3,520 | 7070 | 6950 | 3.41% | 3.32 | 0.49 | 1.48 | | 53.31 |
| 17 | 0.20 | 300 | 2.1 | 8.01% | 0.35 | 10 | 6,365 | 7440 | 7040 | 6.28% | 2.51 | 0.71 | 18 | 2,160 | 7040 | 6950 | 4.17% | 3.67 | 0.16 | 1.48 | | 43.90 |
| Reach 13 | | 330 | | 5.0170 | 0.55 | - 10 | 0,303 | , 1-10 | 75-10 | 0.20/0 | 2.31 | 5.71 | 20 | 1,624 | 6950 | 6900 | 3.08% | 3.51 | 0.13 | 0.13 | | |
| 18 | 0.20 | 300 | 2.1 | 4.58% | 0.30 | 10 | 3,532 | 7185 | 7010 | 4.95% | 2.23 | 0.44 | 15 | 1,623 | 7010 | 6900 | 6.78% | 3.91 | 0.13 | 0.85 | | |
| Reach 14 | 5.25 | - 555 | | .13070 | 0.50 | | - 0,55 <u>L</u> | 7 100 | ,310 | | | 5. , , | 20 | 1,000 | 6900 | 6885 | 1.50% | 2.45 | 0.11 | 0.11 | | |
| 19 | 0.20 | 300 | 2.1 | 2.85% | 0.53 | 9 | 6,563 | 7475 | 7130 | 5.26% | 2.06 | 0.88 | 15 | 4,741 | 7130 | 6885 | 5.17% | 3.41 | 0.39 | 1.80 | | |
| Reach 15 | | | | | 2.55 | | -,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,, | .,,,, | | 2.2075 | | | 20 | 1,450 | 6885 | 6875 | 0.69% | 1.66 | 0.24 | 0.24 | | |
| 20 | 0.15 | 300 | 2.1 | 14.35% | 0.22 | 11 | 5,234 | 7260 | 7010 | 4.78% | 2.40 | 0.60 | 18 | 3,413 | 7010 | 6880 | 3.81% | 3.51 | 0.27 | 1.10 | | |
| Reach 16 | | | | | | | | | | | | | 20 | 1,660 | 6875 | 6850 | 1.51% | 2.45 | 0.19 | 0.19 | | 11.27 |
| 21 | 0.15 | 300 | 2.1 | 6.38% | 0.31 | 12 | 3,500 | 7110 | 6975 | 3.86% | 2.36 | 0.41 | 19 | 1,873 | 6975 | 6850 | 6.67% | 4.91 | 0.11 | 0.82 | | |
| Reach 17 | | | | | | | | | | | | | 20 | 2,382 | 6850 | 6820 | 1.26% | 2.24 | 0.29 | 0.29 | | 17.69 |
| 22 | 0.15 | 300 | 2.1 | 3.15% | 0.40 | 11 | 1,954 | 7060 | 6950 | 5.63% | 2.61 | 0.21 | 18 | 2,680 | 6950 | 6820 | 4.85% | 3.96 | 0.19 | 0.80 | | |
| Reach 18 | | | | | | | | | | | | | 20 | 5,850 | 6820 | 6730 | 1.54% | 2.48 | 0.66 | 0.66 | | |
| | | | | | | _ | | - | - | | | | | | | - | | • | | - | • | |

APPENDIX B — HYDROLOGIC DATA — TC KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B-16



| | | | | | | | | | Tin | ne of Co | ncentra | ion and Lag | Time Data | | | | | | | | | |
|----------|-------------|--------|-------------|--------|-----------|-------------|--------|-----------|--------------|----------|----------|--------------|-------------|--------|-----------|---------------|-------|----------|--------------|---------------|---------------|----------|
| | | Ov | erland Flov | v | | | | Shallow | Concentrated | Flow | | | | | Con | centrated Flo | ow | | | | | |
| | | Flow | 2yr, 24hr | | Overland | | | Тор | Bottom | | | Concentrated | | | Тор | Bottom | | | Concentrated | Time of | Total Time of | |
| | | Length | rainfall | | Flow time | Conveyance | | Elevation | Elevation | | Velocity | Flow time | Conveyance | Length | Elevation | Elevation | | Velocity | Flow time | concentration | Concentration | Lag time |
| Basin | Manning's n | (ft) | (in) | Slope | (hr) | Coefficient | Length | (ft) | (ft) | Slope | (ft/s) | (hr) | Coefficient | (ft) | (ft) | (ft) | Slope | (ft/s) | (hr) | (hr) | (min) | (min) |
| 23 | 0.15 | 150 | 2.1 | 4.41% | 0.20 | 15 | 750 | 6800 | 6760 | 5.33% | 3.46 | 0.06 | 20 | 401 | 6760 | 6730 | 7.48% | 5.47 | 0.02 | 0.28 | 17.02 | 10.21 |
| Reach 19 | | | | | | | | | | | | | 20 | 2,067 | 6730 | 6700 | 1.45% | 2.41 | 0.24 | 0.24 | 14.30 | 14.30 |
| 24 | 0.20 | 300 | 2.1 | 16.14% | 0.27 | 13 | 8,554 | 7323 | 6990 | 3.89% | 2.56 | 0.93 | 16 | 3,600 | 6990 | 6888 | 2.83% | 2.69 | 0.37 | 1.56 | 93.76 | 56.26 |
| 25 | 0.01 | 100 | 2.1 | 6.60% | 0.01 | 20 | 3,404 | 7000 | 6888 | 3.29% | 3.63 | 0.26 | | | | | | | | 0.27 | 16.50 | |
| 26 | 0.15 | 300 | 2.1 | 2.60% | 0.44 | 15 | 6,084 | 7185 | 6990 | 3.21% | 2.69 | 0.63 | 19 | 3,180 | 6990 | 6885 | 3.30% | 3.45 | 0.26 | 1.32 | 79.34 | 47.60 |
| Reach 21 | | | | | | | | | | | | | 20 | 1,175 | 6888 | 6840 | 4.09% | 4.04 | 0.08 | 0.08 | 4.84 | 4.84 |
| Reach 22 | | | | | | | | | | | | | 20 | 2,934 | 6840 | 6700 | 4.77% | 4.37 | 0.19 | 0.19 | 11.19 | |
| 27 | 0.18 | 300 | 2.1 | 3.10% | 0.47 | 18 | 2,126 | 7000 | 6910 | 4.23% | 3.70 | 0.16 | 20 | 2,345 | 6910 | 6840 | 2.99% | 3.46 | 0.19 | 0.82 | 49.16 | |
| 28 | 0.15 | 300 | 2.1 | 2.80% | 0.42 | 13 | 3,410 | 7015 | 6885 | 3.81% | 2.54 | 0.37 | 15 | 1,939 | 6885 | 6860 | 1.29% | 1.70 | 0.32 | 1.11 | | |
| 29 | 0.15 | 300 | 2.1 | 3.10% | 0.41 | 14 | 3,075 | 7045 | 6935 | 3.58% | 2.65 | 0.32 | 16 | 1,166 | 6935 | 6870 | 5.57% | 3.78 | 0.09 | 0.82 | | |
| Reach 20 | | | | | | | | | | | | | 17 | 4,516 | 6870 | 6700 | 3.76% | 3.30 | 0.38 | 0.38 | | |
| 30 | 0.15 | 300 | 2.1 | 5.62% | 0.32 | 12 | 1,693 | 6893 | 6835 | 3.43% | 2.22 | 0.21 | 19 | 3,350 | 6835 | 6700 | 4.03% | 3.81 | 0.24 | 0.78 | | |
| Reach 23 | | | | | | | | | | | | | 20 | 1,528 | 6700 | 6668 | 2.09% | 2.89 | 0.15 | 0.15 | | |
| 31 | 0.01 | 100 | 2.1 | 3.08% | 0.02 | 18 | 1,396 | 6890 | 6850 | 2.87% | 3.05 | 0.13 | 20 | 1,890 | 6850 | 6730 | 6.35% | 5.04 | 0.10 | 0.25 | | |
| 32 | 0.15 | 100 | 2.1 | 2.84% | 0.18 | 15 | 2,355 | 6775 | 6700 | 3.18% | 2.68 | 0.24 | 20 | 332 | 6700 | 6668 | 9.64% | 6.21 | 0.01 | 0.43 | | |
| Reach 24 | | | | | | | | | | | | | 20 | 5,047 | 6668 | 6610 | 1.15% | 2.14 | 0.65 | 0.65 | | |
| 33 | 0.15 | 300 | 2.1 | 3.00% | 0.41 | 15 | 563 | 6680 | 6658 | 3.91% | 2.97 | 0.05 | 20 | 691 | 6658 | 6612 | 6.66% | 5.16 | 0.04 | 0.50 | | |
| Reach 25 | | | | | | | | | | | | | 20 | 3,106 | 6612 | 6580 | 1.03% | 2.03 | 0.43 | 0.43 | 25.50 | 25.50 |

APPENDIX B — HYDROLOGIC DATA — TC KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B—17



HISTORIC CONDITIONS MODEL RESULTS (2-YEAR)

| 2 | -Year, 2-Hou | ır Storm | |
|-------------|--------------|-----------|--------|
| | | Peak | |
| Hydrologic | Drainage | Discharge | Volume |
| Element | Area (mi²) | (CFS) | (in) |
| Subbasin-1 | 1.263 | 11 | 0.03 |
| Subbasin-2 | 0.586 | 6 | 0.03 |
| Subbasin-3 | 0.180 | 2 | 0.03 |
| Junction-1 | 2.029 | 19 | 0.03 |
| Reach-1 | 2.029 | 19 | 0.03 |
| Subbasin-4 | 0.195 | 2 | 0.03 |
| Junction-2 | 2.224 | 21 | 0.03 |
| Reach-2 | 2.224 | 21 | 0.03 |
| Subbasin-5 | 0.625 | 4 | 0.03 |
| Junction-3 | 2.849 | 25 | 0.03 |
| Reach-3 | 2.849 | 25 | 0.03 |
| Subbasin-6 | 1.333 | 9 | 0.03 |
| Junction-4 | 4.182 | 34 | 0.03 |
| Reach-4 | 4.182 | 34 | 0.03 |
| Subbasin-7 | 0.183 | 2 | 0.03 |
| Junction-5 | 4.365 | 35 | 0.03 |
| Reach-5 | 4.365 | 35 | 0.03 |
| Subbasin-8 | 0.288 | 4 | 0.03 |
| Junction-6 | 4.653 | 35 | 0.03 |
| Reach-6 | 4.653 | 35 | 0.03 |
| Subbasin-9 | 1.177 | 8 | 0.03 |
| Subbasin-10 | 0.222 | 3 | 0.03 |
| Junction-7 | 1.399 | 9 | 0.03 |
| Reach-7 | 1.399 | 9 | 0.03 |
| Subbasin-11 | 0.880 | 10 | 0.03 |
| Junction-8 | 2.279 | 16 | 0.03 |
| Reach-8 | 2.279 | 16 | 0.03 |
| Subbasin-12 | 0.552 | 5 | 0.03 |
| Junction-9 | 2.831 | 20 | 0.03 |
| Reach-9 | 2.831 | 20 | 0.03 |
| Junction-10 | 7.484 | 51 | 0.03 |
| Reach-10 | 7.484 | 51 | 0.03 |
| Subbasin-13 | 1.156 | 8 | 0.03 |
| Subbasin-14 | 0.516 | 6 | 0.03 |
| Junction-11 | 9.156 | 56 | 0.03 |
| Reach-11 | 9.156 | 56 | 0.03 |
| Subbasin-15 | 0.498 | 6 | 0.03 |
| Junction-12 | 9.654 | 57 | 0.03 |
| Reach-12 | 9.654 | 57 | 0.03 |
| Subbasin-16 | 0.819 | 7 | 0.03 |
| Subbasin-17 | 0.788 | 8 | 0.03 |
| Junction-13 | 11.261 | 59 | 0.03 |

| 2 | -Year, 2-Hoι | ır Storm | |
|-------------|--------------|-----------|--------|
| | | Peak | |
| Hydrologic | Drainage | Discharge | Volume |
| Element | Area (mi²) | (CFS) | (in) |
| Reach-13 | 11.261 | 59 | 0.03 |
| Subbasin-18 | 0.192 | 2 | 0.03 |
| Junction-14 | 11.453 | 59 | 0.03 |
| Reach-14 | 11.453 | 59 | 0.03 |
| Subbasin-19 | 0.552 | 4 | 0.03 |
| Junction-15 | 12.005 | 60 | 0.03 |
| Reach-15 | 12.005 | 60 | 0.03 |
| Subbasin-20 | 0.594 | 6 | 0.03 |
| Junction-16 | 12.599 | 61 | 0.03 |
| Reach-16 | 12.599 | 61 | 0.03 |
| Subbasin-21 | 0.417 | 5 | 0.03 |
| Junction-17 | 13.016 | 61 | 0.03 |
| Reach-17 | 13.016 | 61 | 0.03 |
| Subbasin-22 | 0.200 | 3 | 0.03 |
| Junction-18 | 13.216 | 61 | 0.03 |
| Reach-18 | 13.216 | 61 | 0.03 |
| Subbasin-23 | 0.123 | 3 | 0.03 |
| Junction-19 | 13.339 | 61 | 0.03 |
| Reach-19 | 13.339 | 61 | 0.03 |
| Subbasin-24 | 0.453 | 4 | 0.03 |
| Subbasin-25 | 0.169 | 4 | 0.03 |
| Subbasin-26 | 0.480 | 4 | 0.03 |
| Junction-21 | 1.102 | 8 | 0.03 |
| Reach-21 | 1.102 | 8 | 0.03 |
| Subbasin-27 | 0.294 | 4 | 0.03 |
| Junction-22 | 1.396 | 11 | 0.03 |
| Reach-22 | 1.396 | 11 | 0.03 |
| Subbasin-28 | 0.264 | 3 | 0.03 |
| Subbasin-29 | 0.172 | 2 | 0.03 |
| Junction-20 | 0.436 | 5 | 0.03 |
| Reach-20 | 0.436 | 5 | 0.03 |
| Subbasin-30 | 0.364 | 5 | 0.03 |
| Junction-23 | 15.535 | 62 | 0.03 |
| Reach-23 | 15.535 | 62 | 0.03 |
| Subbasin-31 | 0.377 | 10 | 0.03 |
| Subbasin-32 | 0.316 | 6 | 0.03 |
| Junction-24 | 16.228 | 62 | 0.03 |
| Reach-24 | 16.228 | 62 | 0.03 |
| Subbasin-33 | 0.184 | 3 | 0.03 |
| Junction-25 | 16.412 | 62 | 0.03 |
| Reach-25 | 16.412 | 62 | 0.03 |
| Junction-26 | 16.412 | 62 | 0.03 |

| 2-Year, 24-Hour Storm | | | |
|-----------------------|------------|-----------|--------|
| | Duniumana | Peak | |
| Hydrologic | Drainage | Discharge | Volume |
| Element | Area (mi²) | (CFS) | (in) |
| Subbasin-1 | 1.263 | 52 | 0.23 |
| Subbasin-2 | 0.586 | 27 | 0.22 |
| Subbasin-3 | 0.180 | 8 | 0.22 |
| Junction-1 | 2.029 | 87 | 0.22 |
| Reach-1 | 2.029 | 86 | 0.22 |
| Subbasin-4 | 0.195 | 9 | 0.21 |
| Junction-2 | 2.224 | 95 | 0.22 |
| Reach-2 | 2.224 | 93 | 0.22 |
| Subbasin-5 | 0.625 | 20 | 0.21 |
| Junction-3 | 2.849 | 111 | 0.22 |
| Reach-3 | 2.849 | 111 | 0.22 |
| Subbasin-6 | 1.333 | 44 | 0.22 |
| Junction-4 | 4.182 | 156 | 0.22 |
| Reach-4 | 4.182 | 152 | 0.22 |
| Subbasin-7 | 0.183 | 9 | 0.22 |
| Junction-5 | 4.365 | 158 | 0.22 |
| Reach-5 | 4.365 | 155 | 0.22 |
| Subbasin-8 | 0.288 | 16 | 0.21 |
| Junction-6 | 4.653 | 161 | 0.22 |
| Reach-6 | 4.653 | 160 | 0.22 |
| Subbasin-9 | 1.177 | 39 | 0.23 |
| Subbasin-10 | 0.222 | 11 | 0.21 |
| Junction-7 | 1.399 | 45 | 0.23 |
| Reach-7 | 1.399 | 45 | 0.23 |
| Subbasin-11 | 0.880 | 41 | 0.21 |
| Junction-8 | 2.279 | 71 | 0.22 |
| Reach-8 | 2.279 | 71 | 0.22 |
| Subbasin-12 | 0.552 | 25 | 0.23 |
| Junction-9 | 2.831 | 91 | 0.22 |
| Reach-9 | 2.831 | 91 | 0.22 |
| Junction-10 | 7.484 | 244 | 0.22 |
| Reach-10 | 7.484 | 240 | 0.22 |
| Subbasin-13 | 1.156 | 38 | 0.22 |
| Subbasin-14 | 0.516 | 28 | 0.25 |
| Junction-11 | 9.156 | 279 | 0.22 |
| Reach-11 | 9.156 | 279 | 0.22 |
| Subbasin-15 | 0.498 | 27 | 0.24 |
| Junction-12 | 9.654 | 287 | 0.22 |
| Reach-12 | 9.654 | 286 | 0.22 |
| Subbasin-16 | 0.819 | 32 | 0.23 |
| Subbasin-17 | 0.788 | 35 | 0.23 |
| Junction-13 | 11.261 | 309 | 0.22 |

| 2-Year, 24-Hour Storm | | | |
|-----------------------|------------|-----------|--------|
| | | Peak | |
| Hydrologic | Drainage | Discharge | Volume |
| Element | Area (mi²) | (CFS) | (in) |
| Reach-13 | 11.261 | 306 | 0.22 |
| Subbasin-18 | 0.192 | 11 | 0.23 |
| Junction-14 | 11.453 | 308 | 0.22 |
| Reach-14 | 11.453 | 307 | 0.22 |
| Subbasin-19 | 0.552 | 23 | 0.26 |
| Junction-15 | 12.005 | 317 | 0.23 |
| Reach-15 | 12.005 | 316 | 0.23 |
| Subbasin-20 | 0.594 | 37 | 0.28 |
| Junction-16 | 12.599 | 323 | 0.23 |
| Reach-16 | 12.599 | 322 | 0.23 |
| Subbasin-21 | 0.417 | 33 | 0.29 |
| Junction-17 | 13.016 | 327 | 0.23 |
| Reach-17 | 13.016 | 325 | 0.23 |
| Subbasin-22 | 0.200 | 19 | 0.33 |
| Junction-18 | 13.216 | 328 | 0.23 |
| Reach-18 | 13.216 | 327 | 0.23 |
| Subbasin-23 | 0.123 | 18 | 0.31 |
| Junction-19 | 13.339 | 329 | 0.23 |
| Reach-19 | 13.339 | 328 | 0.23 |
| Subbasin-24 | 0.453 | 29 | 0.33 |
| Subbasin-25 | 0.169 | 27 | 0.33 |
| Subbasin-26 | 0.480 | 34 | 0.33 |
| Junction-21 | 1.102 | 67 | 0.33 |
| Reach-21 | 1.102 | 66 | 0.33 |
| Subbasin-27 | 0.294 | 27 | 0.33 |
| Junction-22 | 1.396 | 87 | 0.33 |
| Reach-22 | 1.396 | 85 | 0.33 |
| Subbasin-28 | 0.264 | 20 | 0.33 |
| Subbasin-29 | 0.172 | 16 | 0.33 |
| Junction-20 | 0.436 | 36 | 0.33 |
| Reach-20 | 0.436 | 34 | 0.33 |
| Subbasin-30 | 0.364 | 34 | 0.33 |
| Junction-23 | 15.535 | 353 | 0.25 |
| Reach-23 | 15.535 | 350 | 0.25 |
| Subbasin-31 | 0.377 | 23 | 0.17 |
| Subbasin-32 | 0.316 | 15 | 0.17 |
| Junction-24 | 16.228 | 354 | 0.24 |
| Reach-24 | 16.228 | 354 | 0.24 |
| Subbasin-33 | 0.184 | 10 | 0.19 |
| Junction-25 | 16.412 | 354.9 | 0.24 |
| Reach-25 | 16.412 | 352.9 | 0.24 |
| Junction-26 | 16.412 | 352.9 | 0.24 |

APPENDIX B — HYDROLOGIC RESULTS — HISTORIC 2—YR KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B—18



HISTORIC CONDITIONS MODEL RESULTS (5-YEAR)

| 5-Year, 2-Hour Storm | | | |
|----------------------|------------|-----------|--------|
| | | Peak | |
| Hydrologic | Drainage | Discharge | Volume |
| Element | Area (mi²) | (CFS) | (in) |
| Subbasin-1 | 1.263 | 20 | 0.03 |
| Subbasin-2 | 0.586 | 11 | 0.03 |
| Subbasin-3 | 0.18 | 3 | 0.03 |
| Junction-1 | 2.029 | 33 | 0.03 |
| Reach-1 | 2.029 | 33 | 0.03 |
| Subbasin-4 | 0.195 | 4 | 0.03 |
| Junction-2 | 2.224 | 37 | 0.03 |
| Reach-2 | 2.224 | 37 | 0.03 |
| Subbasin-5 | 0.625 | 8 | 0.03 |
| Junction-3 | 2.849 | 43 | 0.03 |
| Reach-3 | 2.849 | 43 | 0.03 |
| Subbasin-6 | 1.333 | 17 | 0.03 |
| Junction-4 | 4.182 | 60 | 0.03 |
| Reach-4 | 4.182 | 60 | 0.03 |
| Subbasin-7 | 0.183 | 4 | 0.03 |
| Junction-5 | 4.365 | 61 | 0.03 |
| Reach-5 | 4.365 | 61 | 0.03 |
| Subbasin-8 | 0.288 | 7 | 0.03 |
| Junction-6 | 4.653 | 62 | 0.03 |
| Reach-6 | 4.653 | 62 | 0.03 |
| Subbasin-9 | 1.177 | 14 | 0.03 |
| Subbasin-10 | 0.222 | 5 | 0.03 |
| Junction-7 | 1.399 | 15 | 0.03 |
| Reach-7 | 1.399 | 15 | 0.03 |
| Subbasin-11 | 0.88 | 17 | 0.03 |
| Junction-8 | 2.279 | 28 | 0.03 |
| Reach-8 | 2.279 | 28 | 0.03 |
| Subbasin-12 | 0.552 | 9 | 0.03 |
| Junction-9 | 2.831 | 35 | 0.03 |
| Reach-9 | 2.831 | 35 | 0.03 |
| Junction-10 | 7.484 | 89 | 0.03 |
| Reach-10 | 7.484 | 89 | 0.03 |
| Subbasin-13 | 1.156 | 14 | 0.03 |
| Subbasin-14 | 0.516 | 10 | 0.03 |
| Junction-11 | 9.156 | 98 | 0.03 |
| Reach-11 | 9.156 | 98 | 0.03 |
| Subbasin-15 | 0.498 | 10 | 0.03 |
| Junction-12 | 9.654 | 99 | 0.03 |
| Reach-12 | 9.654 | 99 | 0.03 |
| Subbasin-16 | 0.819 | 12 | 0.03 |
| Subbasin-17 | 0.788 | 13 | 0.03 |
| Junction-13 | 11.261 | 101 | 0.03 |

| 5-Year, 2-Hour Storm | | | |
|----------------------|------------|-----------|--------|
| | | Peak | |
| Hydrologic | Drainage | Discharge | Volume |
| Element | Area (mi²) | (CFS) | (in) |
| Reach-13 | 11.261 | 101 | 0.03 |
| Subbasin-18 | 0.192 | 4 | 0.03 |
| Junction-14 | 11.453 | 101 | 0.03 |
| Reach-14 | 11.453 | 101 | 0.03 |
| Subbasin-19 | 0.552 | 7 | 0.03 |
| Junction-15 | 12.005 | 102 | 0.03 |
| Reach-15 | 12.005 | 102 | 0.03 |
| Subbasin-20 | 0.594 | 11 | 0.03 |
| Junction-16 | 12.599 | 102 | 0.03 |
| Reach-16 | 12.599 | 102 | 0.03 |
| Subbasin-21 | 0.417 | 9 | 0.04 |
| Junction-17 | 13.016 | 102 | 0.03 |
| Reach-17 | 13.016 | 102 | 0.03 |
| Subbasin-22 | 0.2 | 5 | 0.04 |
| Junction-18 | 13.216 | 102 | 0.03 |
| Reach-18 | 13.216 | 102 | 0.03 |
| Subbasin-23 | 0.123 | 5 | 0.04 |
| Junction-19 | 13.339 | 102 | 0.03 |
| Reach-19 | 13.339 | 101 | 0.03 |
| Subbasin-24 | 0.453 | 7 | 0.04 |
| Subbasin-25 | 0.169 | 6 | 0.04 |
| Subbasin-26 | 0.48 | 8 | 0.04 |
| Junction-21 | 1.102 | 15 | 0.04 |
| Reach-21 | 1.102 | 15 | 0.04 |
| Subbasin-27 | 0.294 | 7 | 0.04 |
| Junction-22 | 1.396 | 20 | 0.04 |
| Reach-22 | 1.396 | 20 | 0.04 |
| Subbasin-28 | 0.264 | 5 | 0.04 |
| Subbasin-29 | 0.172 | 4 | 0.04 |
| Junction-20 | 0.436 | 8 | 0.04 |
| Reach-20 | 0.436 | 8 | 0.04 |
| Subbasin-30 | 0.364 | 8 | 0.04 |
| Junction-23 | 15.535 | 102 | 0.03 |
| Reach-23 | 15.535 | 101 | 0.03 |
| Subbasin-31 | 0.377 | 15 | 0.03 |
| Subbasin-32 | 0.316 | 10 | 0.03 |
| Junction-24 | 16.228 | 101 | 0.03 |
| Reach-24 | 16.228 | 101 | 0.03 |
| Subbasin-33 | 0.184 | 5 | 0.03 |
| Junction-25 | 16.412 | 101 | 0.03 |
| Reach-25 | 16.412 | 101 | 0.03 |
| Junction-26 | 16.412 | 101 | 0.03 |

| 5-Year, 24-Hour Storm | | | |
|-----------------------|------------|-----------|--------|
| | | Peak | |
| Hydrologic | Drainage | Discharge | Volume |
| Element | Area (mi²) | (CFS) | (in) |
| Subbasin-1 | 1.263 | 111 | 0.42 |
| Subbasin-2 | 0.586 | 59 | 0.42 |
| Subbasin-3 | 0.18 | 17 | 0.42 |
| Junction-1 | 2.029 | 185 | 0.42 |
| Reach-1 | 2.029 | 184 | 0.42 |
| Subbasin-4 | 0.195 | 20 | 0.4 |
| Junction-2 | 2.224 | 202 | 0.42 |
| Reach-2 | 2.224 | 195 | 0.42 |
| Subbasin-5 | 0.625 | 42 | 0.4 |
| Junction-3 | 2.849 | 235 | 0.41 |
| Reach-3 | 2.849 | 235 | 0.41 |
| Subbasin-6 | 1.333 | 93 | 0.4 |
| Junction-4 | 4.182 | 328 | 0.41 |
| Reach-4 | 4.182 | 323 | 0.41 |
| Subbasin-7 | 0.183 | 20 | 0.42 |
| Junction-5 | 4.365 | 333 | 0.41 |
| Reach-5 | 4.365 | 324 | 0.41 |
| Subbasin-8 | 0.288 | 35 | 0.4 |
| Junction-6 | 4.653 | 337 | 0.41 |
| Reach-6 | 4.653 | 336 | 0.41 |
| Subbasin-9 | 1.177 | 81 | 0.42 |
| Subbasin-10 | 0.222 | 24 | 0.4 |
| Junction-7 | 1.399 | 93 | 0.42 |
| Reach-7 | 1.399 | 92 | 0.42 |
| Subbasin-11 | 0.88 | 89 | 0.4 |
| Junction-8 | 2.279 | 152 | 0.41 |
| Reach-8 | 2.279 | 150 | 0.41 |
| Subbasin-12 | 0.552 | 52 | 0.43 |
| Junction-9 | 2.831 | 193 | 0.41 |
| Reach-9 | 2.831 | 191 | 0.41 |
| Junction-10 | 7.484 | 508 | 0.41 |
| Reach-10 | 7.484 | 500 | 0.41 |
| Subbasin-13 | 1.156 | 80 | 0.42 |
| Subbasin-14 | 0.516 | 59 | 0.45 |
| Junction-11 | 9.156 | 578 | 0.41 |
| Reach-11 | 9.156 | 576 | 0.41 |
| Subbasin-15 | 0.498 | 57 | 0.44 |
| Junction-12 | 9.654 | 590 | 0.42 |
| Reach-12 | 9.654 | 589 | 0.42 |
| Subbasin-16 | 0.819 | 68 | 0.42 |
| Subbasin-17 | 0.788 | 74 | 0.42 |
| Junction-13 | 11.261 | 631 | 0.42 |

| 5-Year, 24-Hour Storm | | | |
|-----------------------|------------|-----------|--------|
| | | Peak | |
| Hydrologic | Drainage | Discharge | Volume |
| Element | Area (mi²) | (CFS) | (in) |
| Reach-13 | 11.261 | 627 | 0.42 |
| Subbasin-18 | 0.192 | 23 | 0.42 |
| Junction-14 | 11.453 | 631 | 0.42 |
| Reach-14 | 11.453 | 624 | 0.42 |
| Subbasin-19 | 0.552 | 46 | 0.47 |
| Junction-15 | 12.005 | 641 | 0.42 |
| Reach-15 | 12.005 | 640 | 0.42 |
| Subbasin-20 | 0.594 | 73 | 0.5 |
| Junction-16 | 12.599 | 654 | 0.42 |
| Reach-16 | 12.599 | 653 | 0.42 |
| Subbasin-21 | 0.417 | 65 | 0.52 |
| Junction-17 | 13.016 | 661 | 0.43 |
| Reach-17 | 13.016 | 658 | 0.43 |
| Subbasin-22 | 0.2 | 35 | 0.57 |
| Junction-18 | 13.216 | 662 | 0.43 |
| Reach-18 | 13.216 | 660 | 0.43 |
| Subbasin-23 | 0.123 | 35 | 0.43 |
| Junction-19 | 13.339 | 662 | 0.33 |
| Reach-19 | 13.339 | 660 | 0.43 |
| | | | |
| Subbasin-24 | 0.453 | 54 | 0.57 |
| Subbasin-25 | 0.169 | 51 | 0.57 |
| Subbasin-26 | 0.48 | 64 | 0.57 |
| Junction-21 | 1.102 | 128 | 0.57 |
| Reach-21 | 1.102 | 125 | 0.57 |
| Subbasin-27 | 0.294 | 52 | 0.57 |
| Junction-22 | 1.396 | 164 | 0.57 |
| Reach-22 | 1.396 | 161 | 0.57 |
| Subbasin-28 | 0.264 | 38 | 0.57 |
| Subbasin-29 | 0.172 | 30 | 0.57 |
| Junction-20 | 0.436 | 68 | 0.57 |
| Reach-20 | 0.436 | 64 | 0.57 |
| Subbasin-30 | 0.364 | 65 | 0.57 |
| Junction-23 | 15.535 | 702 | 0.45 |
| Reach-23 | 15.535 | 697 | 0.45 |
| Subbasin-31 | 0.377 | 58 | 0.33 |
| Subbasin-32 | 0.316 | 37 | 0.33 |
| Junction-24 | 16.228 | 705 | 0.44 |
| Reach-24 | 16.228 | 702 | 0.44 |
| Subbasin-33 | 0.184 | 24 | 0.37 |
| Junction-25 | 16.412 | 704 | 0.44 |
| Reach-25 | 16.412 | 698 | 0.44 |
| Junction-26 | 16.412 | 698 | 0.44 |

APPENDIX B — HYDROLOGIC RESULTS — HISTORIC 5—YR KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B—19



HISTORIC CONDITIONS MODEL RESULTS (10-YEAR)

| 10-Year, 2-Hour Storm | | | |
|-----------------------|------------|-----------|--------|
| | | Peak | |
| Hydrologic | Drainage | Discharge | Volume |
| Element | Area (mi²) | (CFS) | (in) |
| Subbasin-1 | 1.263 | 23 | 0.04 |
| Subbasin-2 | 0.586 | 13 | 0.04 |
| Subbasin-3 | 0.180 | 3 | 0.04 |
| Junction-1 | 2.029 | 38 | 0.04 |
| Reach-1 | 2.029 | 38 | 0.04 |
| Subbasin-4 | 0.195 | 5 | 0.04 |
| Junction-2 | 2.224 | 42 | 0.04 |
| Reach-2 | 2.224 | 42 | 0.04 |
| Subbasin-5 | 0.625 | 9 | 0.04 |
| Junction-3 | 2.849 | 50 | 0.04 |
| Reach-3 | 2.849 | 50 | 0.04 |
| Subbasin-6 | 1.333 | 19 | 0.04 |
| Junction-4 | 4.182 | 69 | 0.04 |
| Reach-4 | 4.182 | 69 | 0.04 |
| Subbasin-7 | 0.183 | 4 | 0.04 |
| Junction-5 | 4.365 | 70 | 0.04 |
| Reach-5 | 4.365 | 70 | 0.04 |
| Subbasin-8 | 0.288 | 8 | 0.04 |
| Junction-6 | 4.653 | 71 | 0.04 |
| Reach-6 | 4.653 | 71 | 0.04 |
| Subbasin-9 | 1.177 | 15 | 0.04 |
| Subbasin-10 | 0.222 | 5 | 0.04 |
| Junction-7 | 1.399 | 17 | 0.04 |
| Reach-7 | 1.399 | 17 | 0.04 |
| Subbasin-11 | 0.880 | 20 | 0.04 |
| Junction-8 | 2.279 | 32 | 0.04 |
| Reach-8 | 2.279 | 32 | 0.04 |
| Subbasin-12 | 0.552 | 10 | 0.04 |
| Junction-9 | 2.831 | 41 | 0.04 |
| Reach-9 | 2.831 | 40 | 0.04 |
| Junction-10 | 7.484 | 102 | 0.04 |
| Reach-10 | 7.484 | 102 | 0.04 |
| Subbasin-13 | 1.156 | 16 | 0.04 |
| Subbasin-14 | 0.516 | 11 | 0.04 |
| Junction-11 | 9.156 | 113 | 0.04 |
| Reach-11 | 9.156 | 113 | 0.04 |
| Subbasin-15 | 0.498 | 11 | 0.04 |
| Junction-12 | 9.654 | 114 | 0.04 |
| Reach-12 | 9.654 | 114 | 0.04 |
| Subbasin-16 | 0.819 | 14 | 0.04 |
| Subbasin-17 | 0.788 | 15 | 0.04 |
| Junction-13 | 11.261 | 117 | 0.04 |

| 10-Year, 2-Hour Storm | | | |
|-----------------------|-------------------------|-----------|--------|
| | | Peak | |
| Hydrologic | Drainage | Discharge | Volume |
| Element | Area (mi ²) | (CFS) | (in) |
| Reach-13 | 11.261 | 117 | 0.04 |
| Subbasin-18 | 0.192 | 5 | 0.04 |
| Junction-14 | 11.453 | 117 | 0.04 |
| Reach-14 | 11.453 | 116 | 0.04 |
| Subbasin-19 | 0.552 | 8 | 0.04 |
| Junction-15 | 12.005 | 118 | 0.04 |
| Reach-15 | 12.005 | 118 | 0.04 |
| Subbasin-20 | 0.594 | 13 | 0.05 |
| Junction-16 | 12.599 | 118 | 0.04 |
| Reach-16 | 12.599 | 118 | 0.04 |
| Subbasin-21 | 0.417 | 11 | 0.05 |
| Junction-17 | 13.016 | 118 | 0.04 |
| Reach-17 | 13.016 | 118 | 0.04 |
| Subbasin-22 | 0.200 | 6 | 0.06 |
| Junction-18 | 13.216 | 118 | 0.04 |
| Reach-18 | 13.216 | 118 | 0.04 |
| Subbasin-23 | 0.123 | 5 | 0.06 |
| Junction-19 | 13.339 | 118 | 0.04 |
| Reach-19 | 13.339 | 118 | 0.04 |
| Subbasin-24 | 0.453 | 9 | 0.04 |
| Subbasin-25 | 0.453 | 7 | 0.06 |
| Subbasin-25 | 0.480 | 10 | 0.06 |
| | 1.102 | 21 | 0.06 |
| Junction-21 | | | |
| Reach-21 | 1.102 | 21 | 0.06 |
| Subbasin-27 | 0.294 | 8 | 0.06 |
| Junction-22 | 1.396 | 27 | 0.06 |
| Reach-22 | 1.396 | 27 | 0.06 |
| Subbasin-28 | 0.264 | 6 | 0.06 |
| Subbasin-29 | 0.172 | 5 | 0.06 |
| Junction-20 | 0.436 | 11 | 0.06 |
| Reach-20 | 0.436 | 11 | 0.06 |
| Subbasin-30 | 0.364 | 10 | 0.06 |
| Junction-23 | 15.535 | 118 | 0.04 |
| Reach-23 | 15.535 | 118 | 0.04 |
| Subbasin-31 | 0.377 | 17 | 0.04 |
| Subbasin-32 | 0.316 | 11 | 0.04 |
| Junction-24 | 16.228 | 118 | 0.04 |
| Reach-24 | 16.228 | 118 | 0.04 |
| Subbasin-33 | 0.184 | 6 | 0.04 |
| Junction-25 | 16.412 | 117.8 | 0.04 |
| Reach-25 | 16.412 | 117.8 | 0.04 |
| Junction-26 | 16.412 | 117.8 | 0.04 |

| 10-Year, 24-Hour Storm | | | |
|------------------------|------------|-----------|--------|
| Undrologio | Drainage | Peak | Volume |
| Hydrologic | _ | Discharge | |
| Element | Area (mi²) | (CFS) | (in) |
| Subbasin-1 | 1.263 | 174 | 0.62 |
| Subbasin-2 | 0.586 | 93 | 0.61 |
| Subbasin-3 | 0.180 | 26 | 0.61 |
| Junction-1 | 2.029 | 290 | 0.62 |
| Reach-1 | 2.029 | 288 | 0.62 |
| Subbasin-4 | 0.195 | 32 | 0.59 |
| Junction-2 | 2.224 | 316 | 0.61 |
| Reach-2 | 2.224 | 304 | 0.61 |
| Subbasin-5 | 0.625 | 65 | 0.59 |
| Junction-3 | 2.849 | 367 | 0.61 |
| Reach-3 | 2.849 | 367 | 0.61 |
| Subbasin-6 | 1.333 | 144 | 0.60 |
| Junction-4 | 4.182 | 511 | 0.61 |
| Reach-4 | 4.182 | 506 | 0.61 |
| Subbasin-7 | 0.183 | 31 | 0.61 |
| Junction-5 | 4.365 | 522 | 0.61 |
| Reach-5 | 4.365 | 509 | 0.61 |
| Subbasin-8 | 0.288 | 56.3 | 0.59 |
| Junction-6 | 4.653 | 528 | 0.61 |
| Reach-6 | 4.653 | 525 | 0.61 |
| Subbasin-9 | 1.177 | 126 | 0.62 |
| Subbasin-10 | 0.222 | 38 | 0.59 |
| Junction-7 | 1.399 | 144 | 0.62 |
| Reach-7 | 1.399 | 142 | 0.62 |
| Subbasin-11 | 0.880 | 142 | 0.59 |
| Junction-8 | 2.279 | 239 | 0.61 |
| Reach-8 | 2.279 | 234 | 0.61 |
| Subbasin-12 | 0.552 | 81 | 0.63 |
| Junction-9 | 2.831 | 303 | 0.61 |
| Reach-9 | 2.831 | 300 | 0.61 |
| Junction-10 | 7.484 | 789 | 0.61 |
| Reach-10 | 7.484 | 779 | 0.61 |
| Subbasin-13 | 1.156 | 124 | 0.61 |
| Subbasin-14 | 0.516 | 92 | 0.66 |
| Junction-11 | 9.156 | 896 | 0.61 |
| Reach-11 | 9.156 | 891 | 0.61 |
| Subbasin-15 | 0.498 | 88 | 0.65 |
| Junction-12 | 9.654 | 912 | 0.61 |
| Reach-12 | 9.654 | 910 | 0.61 |
| Subbasin-16 | 0.819 | 105 | 0.62 |
| Subbasin-17 | 0.788 | 116 | 0.62 |
| Junction-13 | 11.261 | 970 | 0.61 |

| 10-Year, 24-Hour Storm | | | |
|------------------------|------------------------|----------------------------|----------------|
| Hydrologic Element | Drainage Area (mi²) | Peak Discharge (CFS) | Volume (in) |
| Reach-13 | 11.261 | 967 | 0.61 |
| Subbasin-18 | 0.192 | 35.2 | 0.62 |
| Junction-14 | 11.453 | 973 | 0.61 |
| Reach-14 | 11.453 | 959 | 0.61 |
| Subbasin-19 | 0.552 | 70 | 0.68 |
| Junction-15 | 12.005 | 987 | 0.62 |
| Reach-15 | 12.005 | 987 | 0.62 |
| Subbasin-20 | 0.594 | 111 | 0.72 |
| Junction-16 | 12.599 | 1,007 | 0.62 |
| Reach-16 | 12.599 | 1,004 | 0.62 |
| Subbasin-21 | 0.417 | 97 | 0.75 |
| Junction-17 | 13.016 | 1,015 | 0.63 |
| Reach-17 | 13.016 | 1,011 | 0.63 |
| Subbasin-22 | 0.200 | 52 | 0.82 |
| Junction-18 | 13.216 | 1,017 | 0.63 |
| Reach-18 | 13.216 | 1,010 | 0.63 |
| Subbasin-23 | 0.123 | 52 | 0.79 |
| Junction-19 | 13.339 | 1,012 | 0.63 |
| Reach-19 | 13.339 | 1,010 | 0.63 |
| Subbasin-24 | 0.453 | 80 | 0.82 |
| Subbasin-25 | 0.169 | 76 | 0.82 |
| Subbasin-26 | 0.480 | 95 | 0.82 |
| Junction-21 | 1.102 | 189 | 0.82 |
| Reach-21 | 1.102 | 184 | 0.82 |
| Subbasin-27 | 0.294 | 76 | 0.82 |
| Junction-22 | 1.396 | 241 | 0.82 |
| Reach-22 | 1.396 | 239 | 0.82 |
| Subbasin-28 | 0.264 | 57 | 0.82 |
| Subbasin-29 | 0.172 | 44 | 0.82 |
| Junction-20 | 0.436 | 101 | 0.82 |
| Reach-20 | 0.436 | 95 | 0.82 |
| Subbasin-30 | 0.364 | 95 | 0.82 |
| Junction-23 | 15.535 | 1,066 | 0.66 |
| Reach-23 | 15.535 | 1,062 | 0.66 |
| Subbasin-31 | 0.377 | 97 | 0.50 |
| Subbasin-32 | 0.316 | 60 | 0.50 |
| Junction-24 | 16.228 | 1,073 | 0.65 |
| Reach-24 | 16.228 | 1,067 | 0.65 |
| Subbasin-33 | 0.184 | 39 | 0.55 |
| Junction-25 | 16.412 | 1,070 | 0.65 |
| Reach-25 | 16.412 | 1,060 | 0.65 |
| Junction-26 | 16.412 | 1,060 | 0.65 |

APPENDIX B — HYDROLOGIC RESULTS — HISTORIC 10—YR KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B-20



HISTORIC CONDITIONS MODEL RESULTS (25-YEAR)

| 25-Year, 2-Hour Storm | | | |
|-----------------------|------------|-----------|--------|
| | | Peak | |
| Hydrologic | Drainage | Discharge | Volume |
| Element | Area (mi²) | (CFS) | (in) |
| Subbasin-1 | 1.263 | 27 | 0.05 |
| Subbasin-2 | 0.586 | 15 | 0.05 |
| Subbasin-3 | 0.180 | 4 | 0.05 |
| Junction-1 | 2.029 | 45 | 0.05 |
| Reach-1 | 2.029 | 44 | 0.05 |
| Subbasin-4 | 0.195 | 5 | 0.05 |
| Junction-2 | 2.224 | 49 | 0.05 |
| Reach-2 | 2.224 | 49 | 0.05 |
| Subbasin-5 | 0.625 | 10 | 0.05 |
| Junction-3 | 2.849 | 58 | 0.05 |
| Reach-3 | 2.849 | 58 | 0.05 |
| Subbasin-6 | 1.333 | 23 | 0.05 |
| Junction-4 | 4.182 | 81 | 0.05 |
| Reach-4 | 4.182 | 81 | 0.05 |
| Subbasin-7 | 0.183 | 5 | 0.05 |
| Junction-5 | 4.365 | 83 | 0.05 |
| Reach-5 | 4.365 | 83 | 0.05 |
| Subbasin-8 | 0.288 | 9 | 0.05 |
| Junction-6 | 4.653 | 85 | 0.05 |
| Reach-6 | 4.653 | 85 | 0.05 |
| Subbasin-9 | 1.177 | 19 | 0.05 |
| Subbasin-10 | 0.222 | 6 | 0.05 |
| Junction-7 | 1.399 | 21 | 0.05 |
| Reach-7 | 1.399 | 21 | 0.05 |
| Subbasin-11 | 0.880 | 23 | 0.05 |
| Junction-8 | 2.279 | 37 | 0.05 |
| Reach-8 | 2.279 | 37 | 0.05 |
| Subbasin-12 | 0.552 | 12 | 0.05 |
| Junction-9 | 2.831 | 48 | 0.05 |
| Reach-9 | 2.831 | 48 | 0.05 |
| Junction-10 | 7.484 | 124 | 0.05 |
| Reach-10 | 7.484 | 123 | 0.05 |
| Subbasin-13 | 1.156 | 19 | 0.05 |
| Subbasin-14 | 0.516 | 14 | 0.06 |
| Junction-11 | 9.156 | 139 | 0.05 |
| Reach-11 | 9.156 | 139 | 0.05 |
| Subbasin-15 | 0.498 | 13 | 0.06 |
| Junction-12 | 9.654 | 141 | 0.05 |
| Reach-12 | 9.654 | 141 | 0.05 |
| Subbasin-16 | 0.819 | 16 | 0.05 |
| Subbasin-17 | 0.788 | 18 | 0.05 |
| Junction-13 | 11.261 | 145 | 0.05 |

| 25-Year, 2-Hour Storm | | | |
|-----------------------|------------|-----------|--------|
| | | Peak | |
| Hydrologic | Drainage | Discharge | Volume |
| Element | Area (mi²) | (CFS) | (in) |
| Reach-13 | 11.261 | 145 | 0.05 |
| Subbasin-18 | 0.192 | 6 | 0.05 |
| Junction-14 | 11.453 | 145 | 0.05 |
| Reach-14 | 11.453 | 145 | 0.05 |
| Subbasin-19 | 0.552 | 11 | 0.06 |
| Junction-15 | 12.005 | 147 | 0.05 |
| Reach-15 | 12.005 | 147 | 0.05 |
| Subbasin-20 | 0.594 | 17 | 0.07 |
| Junction-16 | 12.599 | 148 | 0.05 |
| Reach-16 | 12.599 | 148 | 0.05 |
| Subbasin-21 | 0.417 | 15 | 0.07 |
| Junction-17 | 13.016 | 148 | 0.05 |
| Reach-17 | 13.016 | 148 | 0.05 |
| Subbasin-22 | 0.200 | 9 | 0.08 |
| Junction-18 | 13.216 | 148 | 0.05 |
| Reach-18 | 13.216 | 147 | 0.05 |
| Subbasin-23 | 0.123 | 7 | 0.08 |
| Junction-19 | 13.339 | 147 | 0.05 |
| Reach-19 | 13.339 | 147 | 0.05 |
| Subbasin-24 | 0.453 | 14 | 0.08 |
| Subbasin-25 | 0.169 | 10 | 0.08 |
| Subbasin-26 | 0.480 | 16 | 0.08 |
| Junction-21 | 1.102 | 32 | 0.08 |
| Reach-21 | 1.102 | 32 | 0.08 |
| Subbasin-27 | 0.294 | 13 | 0.08 |
| Junction-22 | 1.396 | 41 | 0.08 |
| Reach-22 | 1.396 | 41 | 0.08 |
| Subbasin-28 | 0.264 | 10 | 0.08 |
| Subbasin-29 | 0.172 | 7 | 0.08 |
| Junction-20 | 0.436 | 17 | 0.08 |
| Reach-20 | 0.436 | 17 | 0.08 |
| Subbasin-30 | 0.364 | 16 | 0.08 |
| Junction-23 | 15.535 | 148 | 0.06 |
| Reach-23 | 15.535 | 147 | 0.06 |
| Subbasin-31 | 0.377 | 20 | 0.04 |
| Subbasin-32 | 0.316 | 13 | 0.04 |
| Junction-24 | 16.228 | 147 | 0.04 |
| Reach-24 | 16.228 | 147 | 0.06 |
| Subbasin-33 | 0.184 | 7 | 0.04 |
| Junction-25 | 16.412 | 147.4 | 0.04 |
| Reach-25 | 16.412 | 147.4 | 0.06 |
| Junction-26 | 16.412 | 147.4 | 0.06 |
| Julicul011-20 | 10.412 | 14/.4 | 0.00 |

| 25-Year, 24-Hour Storm | | | |
|------------------------|------------|-----------|--------|
| | | Peak | |
| Hydrologic | Drainage | Discharge | Volume |
| Element | Area (mi²) | (CFS) | (in) |
| Subbasin-1 | 1.263 | 233 | 0.80 |
| Subbasin-2 | 0.586 | 125 | 0.79 |
| Subbasin-3 | 0.180 | 35 | 0.79 |
| Junction-1 | 2.029 | 385 | 0.80 |
| Reach-1 | 2.029 | 384 | 0.80 |
| Subbasin-4 | 0.195 | 43 | 0.76 |
| Junction-2 | 2.224 | 421 | 0.79 |
| Reach-2 | 2.224 | 404 | 0.79 |
| Subbasin-5 | 0.625 | 87 | 0.77 |
| Junction-3 | 2.849 | 489 | 0.79 |
| Reach-3 | 2.849 | 489 | 0.79 |
| Subbasin-6 | 1.333 | 191 | 0.77 |
| Junction-4 | 4.182 | 680 | 0.78 |
| Reach-4 | 4.182 | 675 | 0.78 |
| Subbasin-7 | 0.183 | 41 | 0.79 |
| Junction-5 | 4.365 | 696 | 0.78 |
| Reach-5 | 4.365 | 681 | 0.78 |
| Subbasin-8 | 0.288 | 76 | 0.76 |
| Junction-6 | 4.653 | 705 | 0.78 |
| Reach-6 | 4.653 | 699 | 0.78 |
| Subbasin-9 | 1.177 | 168 | 0.80 |
| Subbasin-10 | 0.222 | 50 | 0.76 |
| Junction-7 | 1.399 | 190 | 0.80 |
| Reach-7 | 1.399 | 189 | 0.80 |
| Subbasin-11 | 0.880 | 190 | 0.76 |
| Junction-8 | 2.279 | 320 | 0.78 |
| Reach-8 | 2.279 | 312 | 0.78 |
| Subbasin-12 | 0.552 | 107 | 0.81 |
| Junction-9 | 2.831 | 405 | 0.79 |
| Reach-9 | 2.831 | 401 | 0.79 |
| Junction-10 | 7.484 | 1,046 | 0.78 |
| Reach-10 | 7.484 | 1,037 | 0.78 |
| Subbasin-13 | 1.156 | 166 | 0.79 |
| Subbasin-14 | 0.516 | 122 | 0.84 |
| Junction-11 | 9.156 | 1,188 | 0.79 |
| Reach-11 | 9.156 | 1,181 | 0.79 |
| Subbasin-15 | 0.498 | 117 | 0.83 |
| Junction-12 | 9.654 | 1,208 | 0.79 |
| Reach-12 | 9.654 | 1,204 | 0.79 |
| Subbasin-16 | 0.819 | 140 | 0.80 |
| Subbasin-17 | 0.788 | 154 | 0.80 |
| Junction-13 | 11.261 | 1,281 | 0.79 |

| 25-Year, 24-Hour Storm | | | |
|------------------------|------------|-----------|--------------|
| | | Peak | |
| Hydrologic | Drainage | Discharge | Volume |
| Element | Area (mi²) | (CFS) | (in) |
| Reach-13 | 11.261 | 1,280 | 0.79 |
| Subbasin-18 | 0.192 | 47 | 0.80 |
| Junction-14 | 11.453 | 1,287 | 0.79 |
| Reach-14 | 11.453 | 1,270 | 0.79 |
| Subbasin-19 | 0.552 | 93 | 0.87 |
| Junction-15 | 12.005 | 1,307 | 0.80 |
| Reach-15 | 12.005 | 1,306 | 0.80 |
| Subbasin-20 | 0.594 | 146 | 0.92 |
| Junction-16 | 12.599 | 1,330 | 0.80 |
| Reach-16 | 12.599 | 1,325 | 0.80 |
| Subbasin-21 | 0.417 | 126 | 0.95 |
| Junction-17 | 13.016 | 1,339 | 0.81 |
| Reach-17 | 13.016 | 1,335 | 0.81 |
| Subbasin-22 | 0.200 | 66 | 1.03 |
| Junction-18 | 13.216 | 1,341 | 0.81 |
| Reach-18 | 13.216 | 1,341 | 0.81 |
| Subbasin-23 | 0.123 | 67 | 1.00 |
| Junction-19 | | | |
| | 13.339 | 1,333 | 0.81 0.81 |
| Reach-19 | 13.339 | 1,329 | |
| Subbasin-24 | 0.453 | 102 | 1.03 |
| Subbasin-25 | 0.169 | 98 | 1.03 |
| Subbasin-26 | 0.480 | 122 | 1.03 |
| Junction-21 | 1.102 | 243 | 1.03 |
| Reach-21 | 1.102 | 237 | 1.03 |
| Subbasin-27 | 0.294 | 97 | 1.03 |
| Junction-22 | 1.396 | 310 | 1.03 |
| Reach-22 | 1.396 | 309 | 1.03 |
| Subbasin-28 | 0.264 | 73 | 1.03 |
| Subbasin-29 | 0.172 | 57 | 1.03 |
| Junction-20 | 0.436 | 130 | 1.03 |
| Reach-20 | 0.436 | 121 | 1.03 |
| Subbasin-30 | 0.364 | 122 | 1.03 |
| Junction-23 | 15.535 | 1,399 | 0.84 |
| Reach-23 | 15.535 | 1,395 | 0.84 |
| Subbasin-31 | 0.377 | 133 | 0.66 |
| Subbasin-32 | 0.316 | 82 | 0.66 |
| Junction-24 | 16.228 | 1,410 | 0.83 |
| Reach-24 | 16.228 | 1,399 | 0.83 |
| Subbasin-33 | 0.184 | 53 | 0.72 |
| Junction-25 | 16.412 | 1402.8 | 0.83 |
| Reach-25 | 16.412 | 1393.8 | 0.83 |
| Junction-26 | 16.412 | 1393.8 | 0.83 |

APPENDIX B — HYDROLOGIC RESULTS — HISTORIC 25—YR KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B-21



HISTORIC CONDITIONS MODEL RESULTS (50-YEAR)

| 50-Year, 2-Hour Storm | | | |
|-----------------------|------------|-----------|--------|
| | | Peak | |
| Hydrologic | Drainage | Discharge | Volume |
| Element | Area (mi²) | (CFS) | (in) |
| Subbasin-1 | 1.263 | 35 | 0.07 |
| Subbasin-2 | 0.586 | 18 | 0.07 |
| Subbasin-3 | 0.180 | 5 | 0.07 |
| Junction-1 | 2.029 | 57 | 0.07 |
| Reach-1 | 2.029 | 57 | 0.07 |
| Subbasin-4 | 0.195 | 6 | 0.07 |
| Junction-2 | 2.224 | 62 | 0.07 |
| Reach-2 | 2.224 | 62 | 0.07 |
| Subbasin-5 | 0.625 | 13 | 0.07 |
| Junction-3 | 2.849 | 75 | 0.07 |
| Reach-3 | 2.849 | 75 | 0.07 |
| Subbasin-6 | 1.333 | 29 | 0.07 |
| Junction-4 | 4.182 | 104 | 0.07 |
| Reach-4 | 4.182 | 103 | 0.07 |
| Subbasin-7 | 0.183 | 6 | 0.07 |
| Junction-5 | 4.365 | 107 | 0.07 |
| Reach-5 | 4.365 | 107 | 0.07 |
| Subbasin-8 | 0.288 | 11 | 0.07 |
| Junction-6 | 4.653 | 110 | 0.07 |
| Reach-6 | 4.653 | 110 | 0.07 |
| Subbasin-9 | 1.177 | 26 | 0.07 |
| Subbasin-10 | 0.222 | 7 | 0.07 |
| Junction-7 | 1.399 | 29 | 0.07 |
| Reach-7 | 1.399 | 29 | 0.07 |
| Subbasin-11 | 0.880 | 28 | 0.07 |
| Junction-8 | 2.279 | 47 | 0.07 |
| Reach-8 | 2.279 | 46 | 0.07 |
| Subbasin-12 | 0.552 | 16 | 0.07 |
| Junction-9 | 2.831 | 61 | 0.07 |
| Reach-9 | 2.831 | 61 | 0.07 |
| Junction-10 | 7.484 | 164 | 0.07 |
| Reach-10 | 7.484 | 164 | 0.07 |
| Subbasin-13 | 1.156 | 25 | 0.07 |
| Subbasin-14 | 0.516 | 19 | 0.08 |
| Junction-11 | 9.156 | 186 | 0.07 |
| Reach-11 | 9.156 | 185 | 0.07 |
| Subbasin-15 | 0.498 | 18 | 0.08 |
| Junction-12 | 9.654 | 188 | 0.07 |
| Reach-12 | 9.654 | 188 | 0.07 |
| Subbasin-16 | 0.819 | 21 | 0.07 |
| Subbasin-17 | 0.788 | 23 | 0.07 |
| Junction-13 | 11.261 | 193 | 0.07 |

| 50-Year, 2-Hour Storm | | | |
|-----------------------|-------------------------|-----------|--------|
| Peak | | | |
| Hydrologic | Drainage | Discharge | Volume |
| Element | Area (mi ²) | (CFS) | (in) |
| Reach-13 | 11.261 | 193 | 0.07 |
| Subbasin-18 | 0.192 | 7 | 0.07 |
| Junction-14 | 11.453 | 193 | 0.07 |
| Reach-14 | 11.453 | 193 | 0.07 |
| Subbasin-19 | 0.552 | 15 | 0.09 |
| Junction-15 | 12.005 | 197 | 0.07 |
| Reach-15 | 12.005 | 197 | 0.07 |
| Subbasin-20 | 0.594 | 25 | 0.10 |
| Junction-16 | 12.599 | 197 | 0.07 |
| Reach-16 | 12.599 | 197 | 0.07 |
| Subbasin-21 | 0.417 | 22 | 0.10 |
| Junction-17 | 13.016 | 197 | 0.07 |
| Reach-17 | 13.016 | 197 | 0.07 |
| Subbasin-22 | 0.200 | 13 | 0.12 |
| Junction-18 | 13.216 | 197 | 0.07 |
| Reach-18 | 13.216 | 197 | 0.07 |
| Subbasin-23 | 0.123 | 11 | 0.12 |
| Junction-19 | 13.339 | 197 | 0.07 |
| Reach-19 | 13.339 | 197 | 0.07 |
| Subbasin-24 | 0.453 | 20 | 0.12 |
| Subbasin-25 | 0.169 | 15 | 0.12 |
| Subbasin-26 | 0.480 | 24 | 0.12 |
| Junction-21 | 1.102 | 47 | 0.12 |
| Reach-21 | 1.102 | 47 | 0.12 |
| Subbasin-27 | 0.294 | 19 | 0.12 |
| Junction-22 | 1.396 | 61 | 0.12 |
| Reach-22 | 1.396 | 61 | 0.12 |
| Subbasin-28 | 0.264 | 14 | 0.12 |
| Subbasin-29 | 0.172 | 11 | 0.12 |
| Junction-20 | 0.436 | 25 | 0.12 |
| Reach-20 | 0.436 | 25 | 0.12 |
| Subbasin-30 | 0.364 | 24 | 0.12 |
| Junction-23 | 15.535 | 197 | 0.08 |
| Reach-23 | 15.535 | 197 | 0.08 |
| Subbasin-31 | 0.377 | 22 | 0.05 |
| Subbasin-32 | 0.316 | 15 | 0.05 |
| Junction-24 | 16.228 | 197 | 0.08 |
| Reach-24 | 16.228 | 197 | 0.08 |
| Subbasin-33 | 0.184 | 8 | 0.06 |
| Junction-25 | 16.412 | 196.9 | 0.08 |
| Reach-25 | 16.412 | 196.9 | 0.08 |
| Junction-26 | 16.412 | 196.9 | 0.08 |

| 50-Year, 24-Hour Storm | | | |
|------------------------|-------------------------|-----------|--------|
| | D | Peak | |
| Hydrologic | Drainage | Discharge | Volume |
| Element | Area (mi ²) | (CFS) | (in) |
| Subbasin-1 | 1.263 | 330 | 1.10 |
| Subbasin-2 | 0.586 | 178 | 1.09 |
| Subbasin-3 | 0.180 | 49 | 1.09 |
| Junction-1 | 2.029 | 546 | 1.09 |
| Reach-1 | 2.029 | 544 | 1.09 |
| Subbasin-4 | 0.195 | 62 | 1.05 |
| Junction-2 | 2.224 | 596 | 1.09 |
| Reach-2 | 2.224 | 577 | 1.09 |
| Subbasin-5 | 0.625 | 124 | 1.06 |
| Junction-3 | 2.849 | 692 | 1.08 |
| Reach-3 | 2.849 | 692 | 1.08 |
| Subbasin-6 | 1.333 | 273 | 1.06 |
| Junction-4 | 4.182 | 962 | 1.08 |
| Reach-4 | 4.182 | 959 | 1.08 |
| Subbasin-7 | 0.183 | 59 | 1.09 |
| Junction-5 | 4.365 | 988 | 1.08 |
| Reach-5 | 4.365 | 969 | 1.08 |
| Subbasin-8 | 0.288 | 109 | 1.05 |
| Junction-6 | 4.653 | 1,002 | 1.08 |
| Reach-6 | 4.653 | 992 | 1.08 |
| Subbasin-9 | 1.177 | 237 | 1.10 |
| Subbasin-10 | 0.222 | 72 | 1.05 |
| Junction-7 | 1.399 | 268 | 1.09 |
| Reach-7 | 1.399 | 267 | 1.09 |
| Subbasin-11 | 0.880 | 272 | 1.05 |
| Junction-8 | 2.279 | 456 | 1.08 |
| Reach-8 | 2.279 | 443 | 1.08 |
| Subbasin-12 | 0.552 | 152 | 1.11 |
| Junction-9 | 2.831 | 578 | 1.08 |
| Reach-9 | 2.831 | 570 | 1.08 |
| Junction-10 | 7.484 | 1,478 | 1.08 |
| Reach-10 | 7.484 | 1,471 | 1.08 |
| Subbasin-13 | 1.156 | 234 | 1.09 |
| Subbasin-14 | 0.516 | 171 | 1.15 |
| Junction-11 | 9.156 | 1,678 | 1.08 |
| Reach-11 | 9.156 | 1,668 | 1.08 |
| Subbasin-15 | 0.498 | 166 | 1.14 |
| Junction-12 | 9.654 | 1,703 | 1.09 |
| Reach-12 | 9.654 | 1,696 | 1.09 |
| Subbasin-16 | 0.819 | 198 | 1.10 |
| Subbasin-17 | 0.788 | 218 | 1.10 |
| Junction-13 | 11.261 | 1,808 | 1.09 |
| | | =, | |

| 50-Year, 24-Hour Storm | | | |
|-------------------------|------------|-------------|--------------|
| Peak | | | |
| Hydrologic | Drainage | Discharge | Volume |
| Element | Area (mi²) | (CFS) | (in) |
| Reach-13 | 11.261 | 1,804 | 1.09 |
| Subbasin-18 | 0.192 | 66 | 1.10 |
| Junction-14 | 11.453 | 1,813 | 1.09 |
| Reach-14 | 11.453 | 1,794 | 1.09 |
| Subbasin-19 | 0.552 | 130 | 1.19 |
| Junction-15 | 12.005 | 1,844 | 1.09 |
| Reach-15 | 12.005 | 1,842 | 1.09 |
| Subbasin-20 | 0.594 | 203 | 1.24 |
| Junction-16 | 12.599 | 1,874 | 1.10 |
| Reach-16 | 12.599 | 1,863 | 1.10 |
| Subbasin-21 | 0.417 | 173 | 1.29 |
| Junction-17 | 13.016 | 1,882 | 1.11 |
| Reach-17 | 13.016 | 1,877 | 1.11 |
| Subbasin-22 | 0.200 | 90 | 1.38 |
| Junction-18 | 13.216 | 1,885 | 1.11 |
| Reach-18 | 13.216 | 1,865 | 1.11 |
| Subbasin-23 | 0.123 | 92 | 1.34 |
| Junction-19 | 13.339 | 1,869 | 1.11 |
| Reach-19 | 13.339 | 1,864 | 1.11 |
| Subbasin-24 | 0.453 | 139 | 1.38 |
| Subbasin-25 | 0.169 | 133 | 1.38 |
| Subbasin-26 | 0.480 | 167 | 1.38 |
| Junction-21 | 1.102 | 331 | 1.38 |
| Reach-21 | 1.102 | 324 | 1.38 |
| Subbasin-27 | 0.294 | 132 | 1.38 |
| Junction-22 | 1.396 | 423 | 1.38 |
| Reach-22 | 1.396 | 423 | 1.38 |
| Subbasin-28 | 0.264 | 100 | 1.38 |
| Subbasin-29 | 0.172 | 77 | 1.38 |
| Junction-20 | 0.436 | 178 | 1.38 |
| Reach-20 | 0.436 | 165 | 1.38 |
| Subbasin-30 | 0.364 | 167 | 1.38 |
| Junction-23 | 15.535 | 1,953 | 1.15 |
| Reach-23 | 15.535 | 1,953 | 1.15 |
| Subbasin-31 | 0.377 | 1,955 | 0.92 |
| | 0.377 | | |
| Subbasin-32 | | 120 | 0.92 1.14 |
| Junction-24 | 16.228 | 1,972 | |
| Reach-24 Subbasin-33 | 16.228 | 1,954 76 | 1.14 1.00 |
| | 0.184 | | |
| Junction-25 | 16.412 | 1958.8 | 1.14 |
| Reach-25 | 16.412 | 1951.7 | 1.14 |
| Junction-26 | 16.412 | 1951.7 | 1.14 |

APPENDIX B — HYDROLOGIC RESULTS — HISTORIC 50—YR KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B-22



HISTORIC CONDITIONS MODEL RESULTS (100-YEAR)

| 100-Year, 2-Hour Storm | | | |
|------------------------|------------|-----------|--------|
| | | Peak | |
| Hydrologic | Drainage | Discharge | Volume |
| Element | Area (mi²) | (CFS) | (in) |
| Subbasin-1 | 1.263 | 49 | 0.10 |
| Subbasin-2 | 0.586 | 25 | 0.10 |
| Subbasin-3 | 0.180 | 7 | 0.10 |
| Junction-1 | 2.029 | 80 | 0.10 |
| Reach-1 | 2.029 | 80 | 0.10 |
| Subbasin-4 | 0.195 | 8 | 0.09 |
| Junction-2 | 2.224 | 87 | 0.10 |
| Reach-2 | 2.224 | 87 | 0.10 |
| Subbasin-5 | 0.625 | 18 | 0.09 |
| Junction-3 | 2.849 | 104 | 0.10 |
| Reach-3 | 2.849 | 104 | 0.10 |
| Subbasin-6 | 1.333 | 41 | 0.09 |
| Junction-4 | 4.182 | 144 | 0.10 |
| Reach-4 | 4.182 | 144 | 0.10 |
| Subbasin-7 | 0.183 | 8 | 0.10 |
| Junction-5 | 4.365 | 149 | 0.10 |
| Reach-5 | 4.365 | 149 | 0.10 |
| Subbasin-8 | 0.288 | 14 | 0.09 |
| Junction-6 | 4.653 | 154 | 0.10 |
| Reach-6 | 4.653 | 154 | 0.10 |
| Subbasin-9 | 1.177 | 37 | 0.10 |
| Subbasin-10 | 0.222 | 10 | 0.09 |
| Junction-7 | 1.399 | 42 | 0.10 |
| Reach-7 | 1.399 | 42 | 0.10 |
| Subbasin-11 | 0.880 | 38 | 0.09 |
| Junction-8 | 2.279 | 65 | 0.10 |
| Reach-8 | 2.279 | 65 | 0.10 |
| Subbasin-12 | 0.552 | 23 | 0.10 |
| Junction-9 | 2.831 | 85 | 0.10 |
| Reach-9 | 2.831 | 84 | 0.10 |
| Junction-10 | 7.484 | 230 | 0.10 |
| Reach-10 | 7.484 | 230 | 0.10 |
| Subbasin-13 | 1.156 | 35 | 0.10 |
| Subbasin-14 | 0.516 | 27 | 0.11 |
| Junction-11 | 9.156 | 260 | 0.10 |
| Reach-11 | 9.156 | 259 | 0.10 |
| Subbasin-15 | 0.498 | 25 | 0.11 |
| Junction-12 | 9.654 | 262 | 0.10 |
| Reach-12 | 9.654 | 262 | 0.10 |
| Subbasin-16 | 0.819 | 30 | 0.10 |
| Subbasin-17 | 0.788 | 32 | 0.10 |
| Junction-13 | 11.261 | 269 | 0.10 |

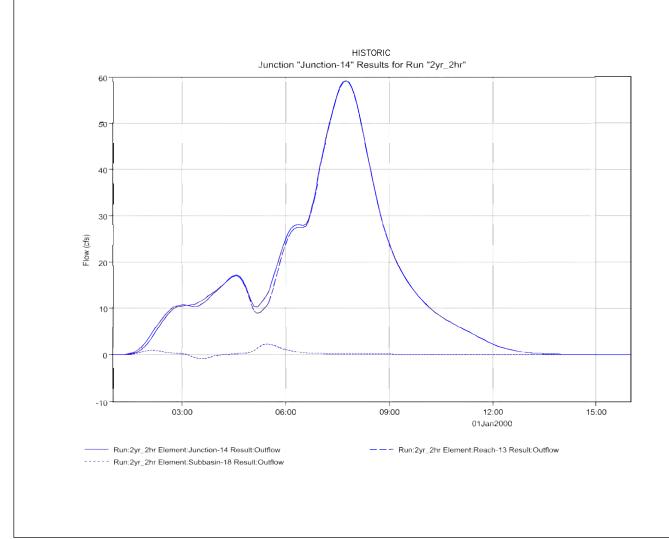
| 100-Year, 2-Hour Storm | | | | |
|------------------------|-------------------------|-----------|--------|--|
| Peak | | | | |
| Hydrologic | Drainage | Discharge | Volume | |
| Element | Area (mi ²) | (CFS) | (in) | |
| Reach-13 | 11.261 | 269 | 0.10 | |
| Subbasin-18 | 0.192 | 10 | 0.10 | |
| Junction-14 | 11.453 | 269 | 0.10 | |
| Reach-14 | 11.453 | 269 | 0.10 | |
| Subbasin-19 | 0.552 | 22 | 0.12 | |
| Junction-15 | 12.005 | 274 | 0.10 | |
| Reach-15 | 12.005 | 274 | 0.10 | |
| Subbasin-20 | 0.594 | 36 | 0.14 | |
| Junction-16 | 12.599 | 274 | 0.10 | |
| Reach-16 | 12.599 | 274 | 0.10 | |
| Subbasin-21 | 0.417 | 32 | 0.15 | |
| Junction-17 | 13.016 | 274 | 0.10 | |
| Reach-17 | 13.016 | 274 | 0.10 | |
| Subbasin-22 | 0.200 | 19 | 0.17 | |
| Junction-18 | 13.216 | 274 | 0.10 | |
| Reach-18 | 13.216 | 274 | 0.10 | |
| Subbasin-23 | 0.123 | 17 | 0.17 | |
| Junction-19 | 13.339 | 274 | 0.10 | |
| Reach-19 | 13.339 | 274 | 0.10 | |
| Subbasin-24 | 0.453 | 29 | 0.17 | |
| Subbasin-25 | 0.169 | 23 | 0.17 | |
| Subbasin-26 | 0.480 | 34 | 0.17 | |
| Junction-21 | 1.102 | 68 | 0.17 | |
| Reach-21 | 1.102 | 67 | 0.17 | |
| Subbasin-27 | 0.294 | 27 | 0.17 | |
| Junction-22 | 1.396 | 86 | 0.17 | |
| Reach-22 | 1.396 | 86 | 0.17 | |
| Subbasin-28 | 0.264 | 21 | 0.17 | |
| Subbasin-29 | 0.172 | 16 | 0.17 | |
| Junction-20 | 0.436 | 35 | 0.17 | |
| Reach-20 | 0.436 | 35 | 0.17 | |
| Subbasin-30 | 0.364 | 34 | 0.17 | |
| Junction-23 | 15.535 | 274 | 0.17 | |
| Reach-23 | 15.535 | 274 | 0.11 | |
| Subbasin-31 | 0.377 | 25 | 0.06 | |
| Subbasin-32 | 0.377 | 16 | 0.06 | |
| Junction-24 | 16.228 | 274 | 0.00 | |
| Reach-24 | 16.228 | 274 | 0.11 | |
| Subbasin-33 | 0.184 | 9 | 0.11 | |
| Junction-25 | 16.412 | 274 | 0.07 | |
| Reach-25 | 16.412 | 274 | 0.11 | |
| Junction-26 | 16.412 | 274 | 0.11 | |
| วนที่เดียด์ที่-26 | 10.412 | 2/4 | 0.11 | |

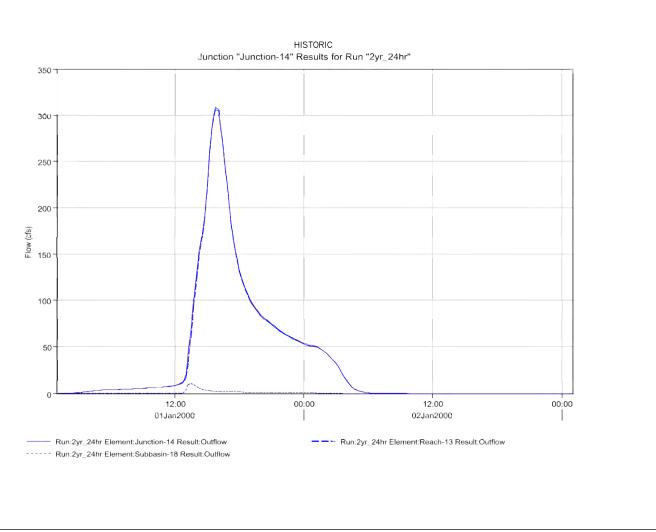
| 100-Year, 24-Hour Storm | | | |
|-------------------------|-------------------------|-----------|--------|
| | Drainago | Peak | |
| Hydrologic | Drainage | Discharge | Volume |
| Element | Area (mi ²) | (CFS) | (in) |
| Subbasin-1 | 1.263 | 402 | 1.31 |
| Subbasin-2 | 0.586 | 217 | 1.31 |
| Subbasin-3 | 0.180 | 60 | 1.31 |
| Junction-1 | 2.029 | 663 | 1.31 |
| Reach-1 | 2.029 | 661 | 1.31 |
| Subbasin-4 | 0.195 | 75 | 1.26 |
| Junction-2 | 2.224 | 724 | 1.31 |
| Reach-2 | 2.224 | 703 | 1.31 |
| Subbasin-5 | 0.625 | 150 | 1.27 |
| Junction-3 | 2.849 | 840 | 1.30 |
| Reach-3 | 2.849 | 840 | 1.30 |
| Subbasin-6 | 1.333 | 332 | 1.27 |
| Junction-4 | 4.182 | 1,168 | 1.29 |
| Reach-4 | 4.182 | 1,167 | 1.29 |
| Subbasin-7 | 0.183 | 71 | 1.31 |
| Junction-5 | 4.365 | 1,201 | 1.29 |
| Reach-5 | 4.365 | 1,179 | 1.29 |
| Subbasin-8 | 0.288 | 133.1 | 1.26 |
| Junction-6 | 4.653 | 1218.6 | 1.29 |
| Reach-6 | 4.653 | 1,205 | 1.29 |
| Subbasin-9 | 1.177 | 287 | 1.32 |
| Subbasin-10 | 0.222 | 87 | 1.26 |
| Junction-7 | 1.399 | 325 | 1.31 |
| Reach-7 | 1.399 | 325 | 1.31 |
| Subbasin-11 | 0.880 | 332 | 1.26 |
| Junction-8 | 2.279 | 556 | 1.29 |
| Reach-8 | 2.279 | 540 | 1.29 |
| Subbasin-12 | 0.552 | 184 | 1.32 |
| Junction-9 | 2.831 | 704 | 1.30 |
| Reach-9 | 2.831 | 694 | 1.30 |
| Junction-10 | 7.484 | 1,793 | 1.29 |
| Reach-10 | 7.484 | 1,788 | 1.29 |
| Subbasin-13 | 1.156 | 285 | 1.31 |
| Subbasin-14 | 0.516 | 207 | 1.37 |
| Junction-11 | 9.156 | 2,036 | 1.30 |
| Reach-11 | 9.156 | 2,022 | 1.30 |
| Subbasin-15 | 0.498 | 201 | 1.36 |
| Junction-12 | 9.654 | 2,064 | 1.30 |
| Reach-12 | 9.654 | 2,055 | 1.30 |
| Subbasin-16 | 0.819 | 241 | 1.31 |
| Subbasin-17 | 0.788 | 264 | 1.31 |
| Junction-13 | 11.261 | 2,194 | 1.30 |

| 100-Year, 24-Hour Storm | | | |
|-------------------------|------------|-----------|--------|
| Peak | | | |
| Hydrologic | Drainage | Discharge | Volume |
| Element | Area (mi²) | (CFS) | (in) |
| Reach-13 | 11.261 | 2,185 | 1.30 |
| Subbasin-18 | 0.192 | 80 | 1.32 |
| Junction-14 | 11.453 | 2,196 | 1.30 |
| Reach-14 | 11.453 | 2,176 | 1.30 |
| Subbasin-19 | 0.552 | 157 | 1.41 |
| Junction-15 | 12.005 | 2,234 | 1.31 |
| Reach-15 | 12.005 | 2,232 | 1.31 |
| Subbasin-20 | 0.594 | 244 | 1.48 |
| Junction-16 | 12.599 | 2,269 | 1.32 |
| Reach-16 | 12.599 | 2,255 | 1.32 |
| Subbasin-21 | 0.417 | 207 | 1.53 |
| Junction-17 | 13.016 | 2,276 | 1.32 |
| Reach-17 | 13.016 | 2,271 | 1.32 |
| Subbasin-22 | 0.200 | 107 | 1.63 |
| Junction-18 | 13.216 | 2,281 | 1.33 |
| Reach-18 | 13.216 | 2,254 | 1.33 |
| Subbasin-23 | 0.123 | 109 | 1.58 |
| Junction-19 | 13.339 | 2,259 | 1.33 |
| Reach-19 | 13.339 | 2,253 | 1.33 |
| Subbasin-24 | 0.453 | 166 | 1.63 |
| Subbasin-25 | 0.169 | 159 | 1.63 |
| Subbasin-26 | 0.480 | 199 | 1.63 |
| Junction-21 | 1.102 | 395 | 1.63 |
| Reach-21 | 1.102 | 387 | 1.63 |
| Subbasin-27 | 0.294 | 157 | 1.63 |
| Junction-22 | 1.396 | 505 | 1.63 |
| Reach-22 | 1.396 | 505 | 1.63 |
| Subbasin-28 | 0.264 | 120 | 1.63 |
| Subbasin-29 | 0.172 | 92 | 1.63 |
| Junction-20 | 0.436 | 212 | 1.63 |
| Reach-20 | 0.436 | 197 | 1.63 |
| Subbasin-30 | 0.364 | 200 | 1.63 |
| Junction-23 | 15.535 | 2,362 | 1.37 |
| Reach-23 | 15.535 | 2,358 | 1.37 |
| Subbasin-31 | 0.377 | 241 | 1.12 |
| Subbasin-32 | 0.316 | 147 | 1.12 |
| Junction-24 | 16.228 | 2,381 | 1.36 |
| Reach-24 | 16.228 | 2,357 | 1.36 |
| Subbasin-33 | 0.184 | 93 | 1.21 |
| Junction-25 | 16.412 | 2,362 | 1.36 |
| Reach-25 | 16.412 | 2,357 | 1.36 |
| Junction-26 | 16.412 | 2,357 | 1.36 |

APPENDIX B — HYDROLOGIC RESULTS — HISTORIC 100—YR KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B-23





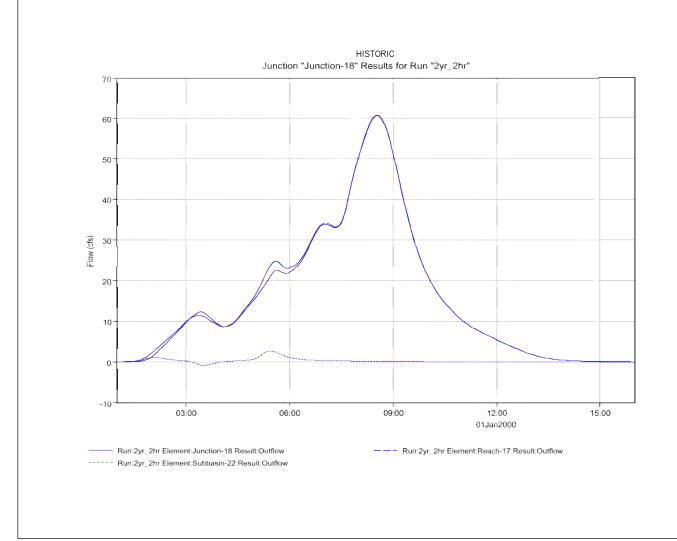


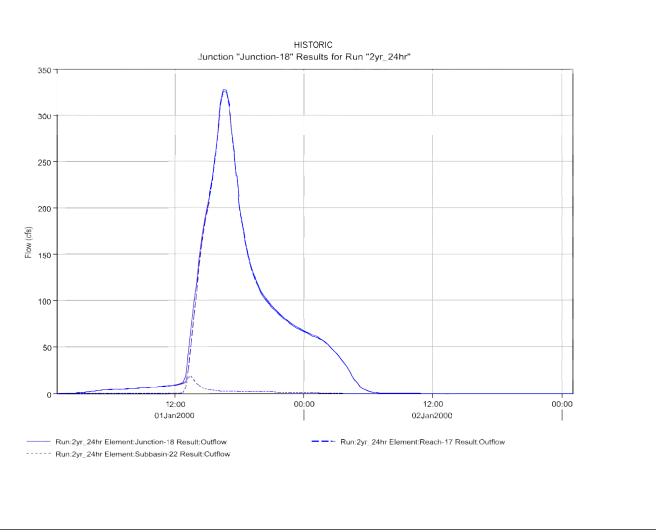
2-YR 2-HR 24-HR

> JUNCTION 14 HOWELLS ROAD (APPROXIMATE)

HISTORIC CONDITIONS HYDROGRAPHS AT SELECT LOCATIONS 2-YEAR APPENDIX B — HYDROLOGIC RESULTS — HISTORIC HYDROGRAPHS 2—YR J—14 KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B—24







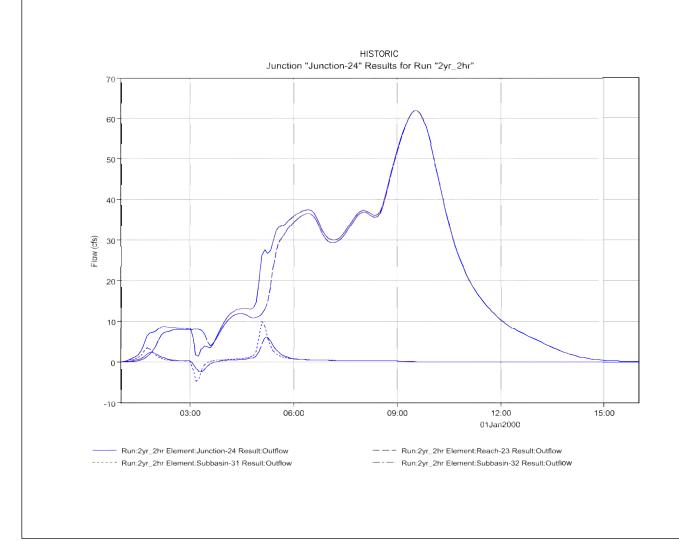
2-YR 2-HR 24-HR

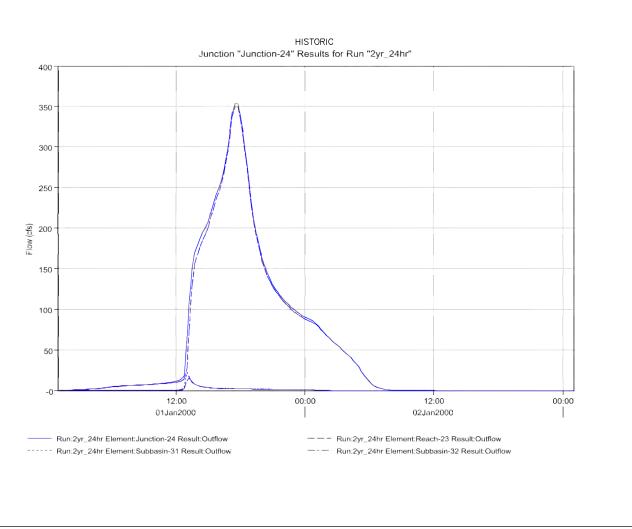
> JUNCTION 18 POWERS BLVD BRIDGE

HISTORIC CONDITIONS HYDROGRAPHS
AT SELECT LOCATIONS
2-YEAR

APPENDIX B — HYDROLOGIC RESULTS — HISTORIC HYDROGRAPHS 2—YR J—18 KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B—25







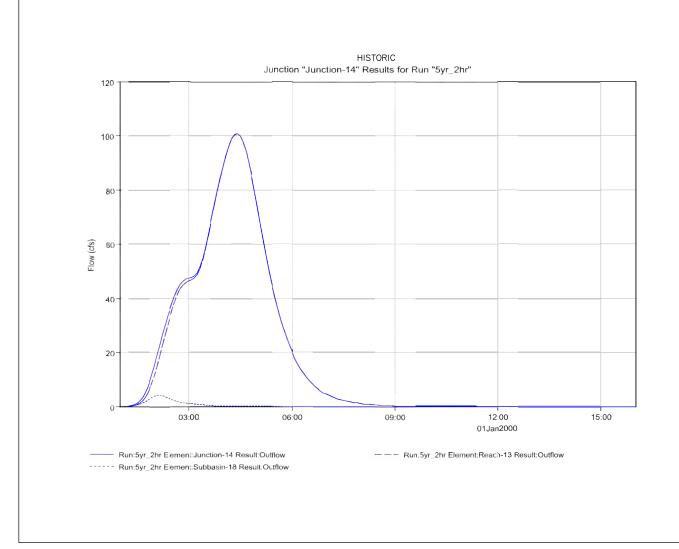
2-YR 2-HR 24-HR

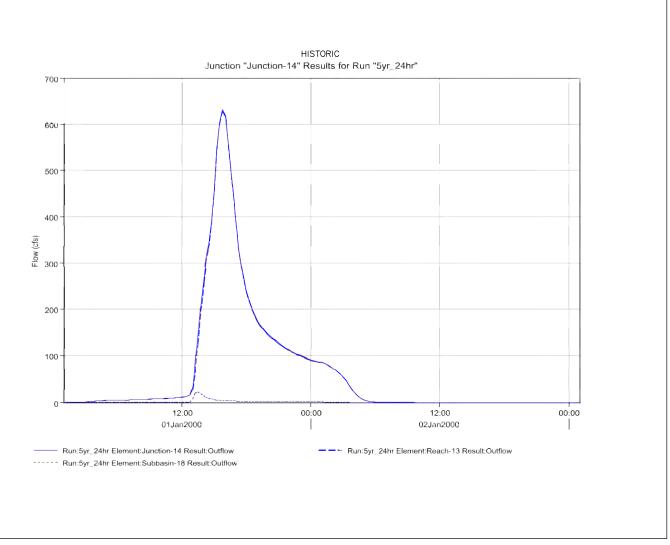
> JUNCTION 24 HWY 83 BRIDGE

HISTORIC CONDITIONS HYDROGRAPHS
AT SELECT LOCATIONS
2-YEAR

APPENDIX B — HYDROLOGIC RESULTS — HISTORIC HYDROGRAPHS 2—YR J—24 KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B—26





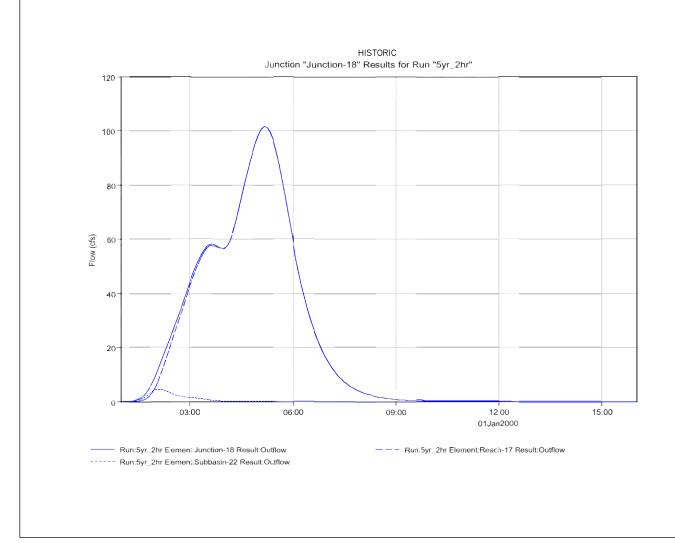


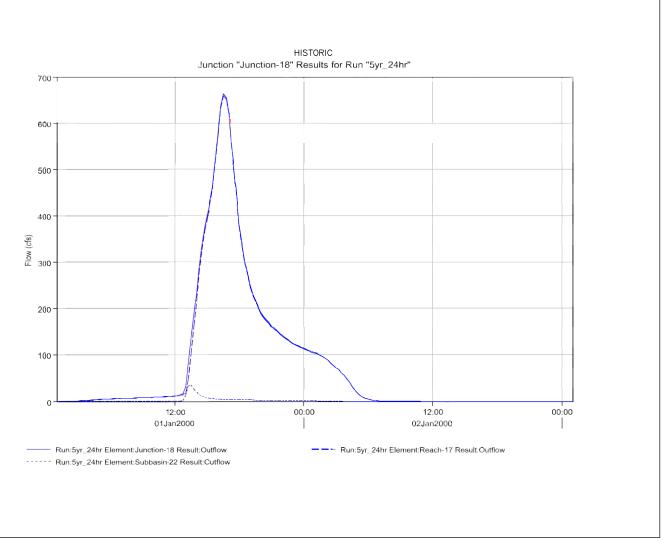
5-YR 2-HR 5-YR 24-HR

JUNCTION 14
HOWELLS ROAD (APPROXIMATE)
HISTORIC CONDITIONS HYDROGRAPHS
AT SELECT LOCATIONS
5-YEAR

APPENDIX B — HYDROLOGIC RESULTS — HISTORIC HYDROGRAPHS 5—YR J—14 KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B—27





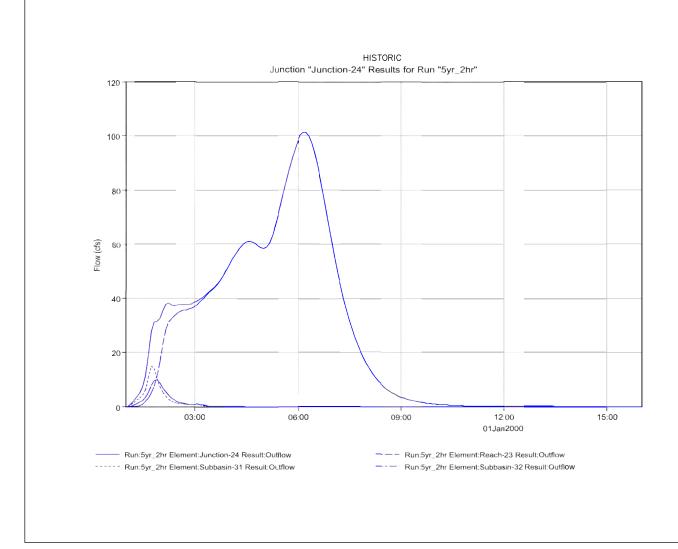


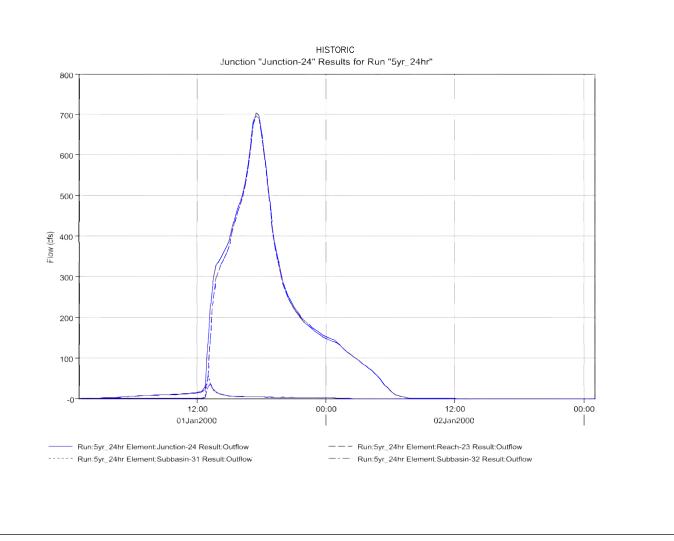
5-YR 2-HR 5-YR 24-HR

> JUNCTION 18 POWERS BLVD BRIDGE

HISTORIC CONDITIONS HYDROGRAPHS AT SELECT LOCATIONS 5-YEAR APPENDIX B — HYDROLOGIC RESULTS — HISTORIC HYDROGRAPHS 5—YR J—18 KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B—28





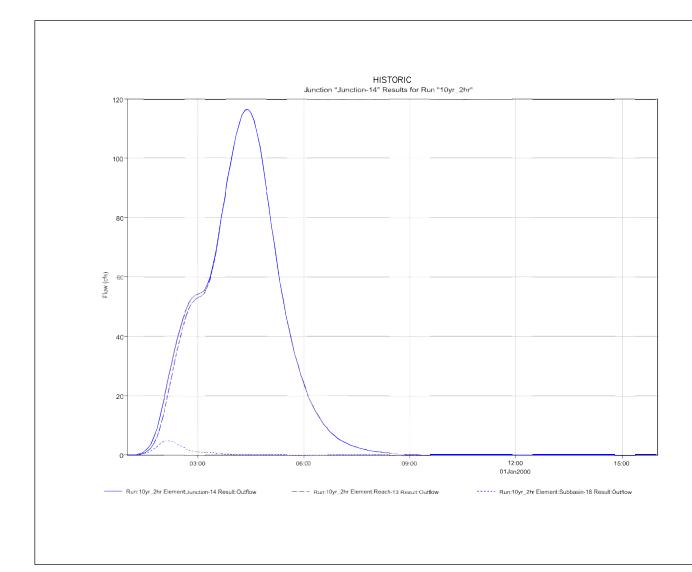


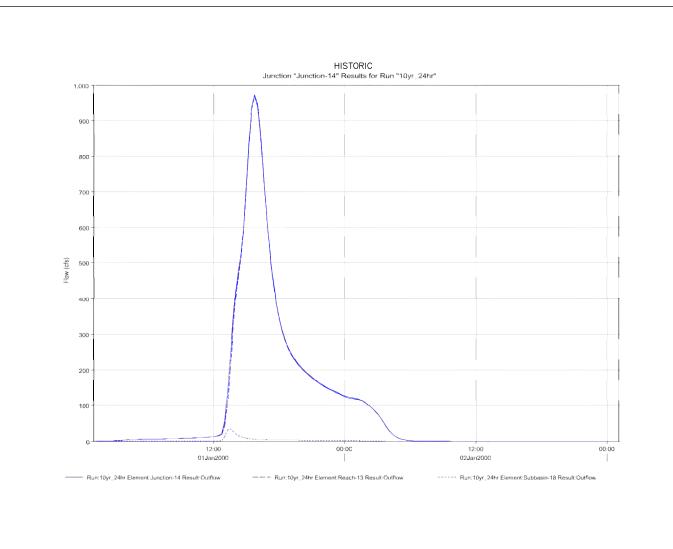
5-YR 2-HR 5-YR 24-HR

JUNCTION 24
HWY 83 BRIDGE
HISTORIC CONDITIONS HYDROGRAPHS
AT SELECT LOCATIONS
5-YEAR

APPENDIX B — HYDROLOGIC RESULTS — HISTORIC HYDROGRAPHS 5—YR J—24 KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B—29





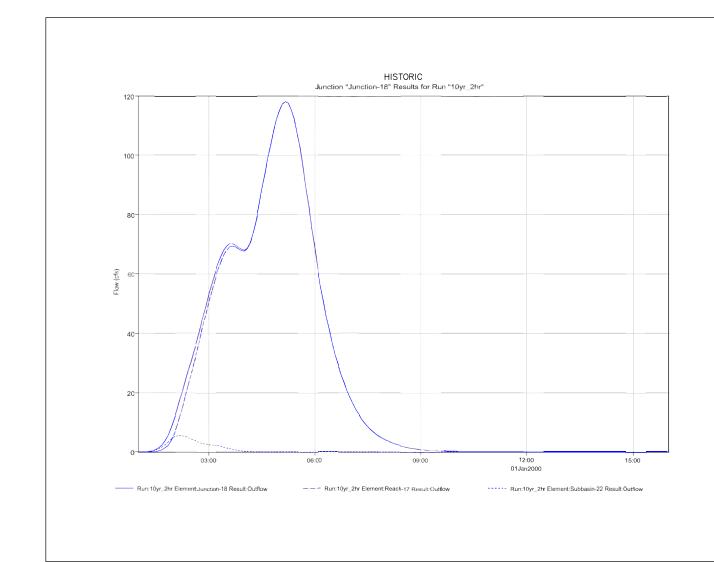


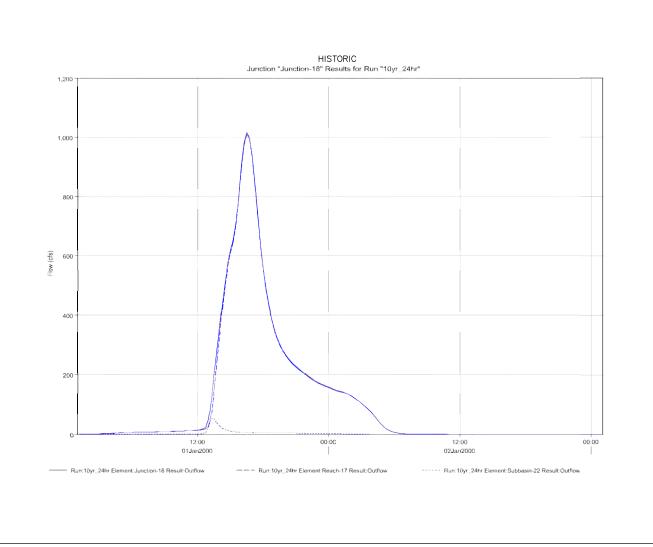
10-YR 24-HR 10-YR 2-HR

> JUNCTION 14 HOWELLS ROAD (APPROXIMATE)

HISTORIC CONDITIONS HYDROGRAPHS AT SELECT LOCATIONS 10-YEAR APPENDIX B — HYDROLOGIC RESULTS — HISTORIC HYDROGRAPHS 10—YRJ—14 KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B—30





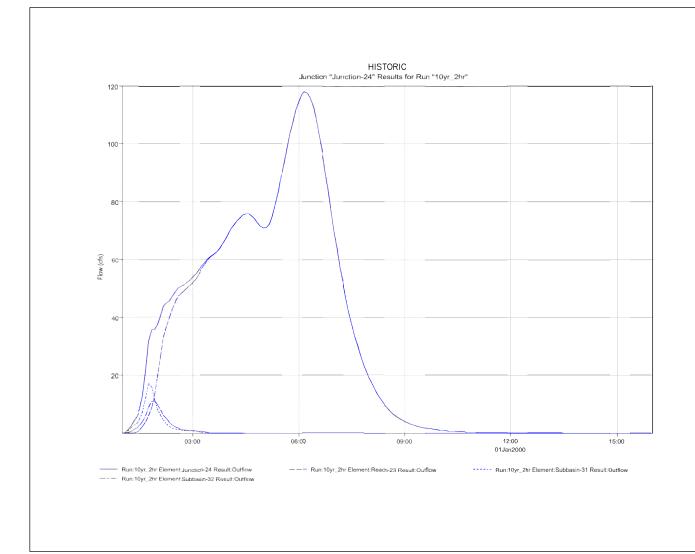


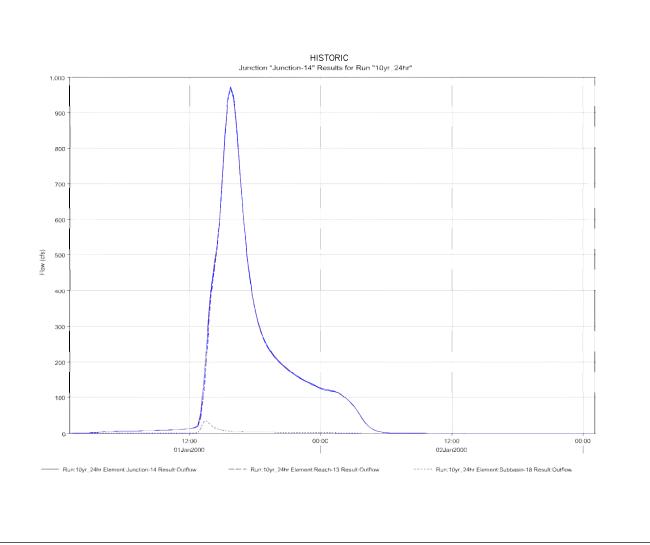
10-YR 24-HR 10-YR 2-HR

> JUNCTION 18 POWERS BLVD BRIDGE

HISTORIC CONDITIONS HYDROGRAPHS AT SELECT LOCATIONS 10-YEAR APPENDIX B — HYDROLOGIC RESULTS — HISTORIC HYDROGRAPHS 10—YRJ—18 KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B—31





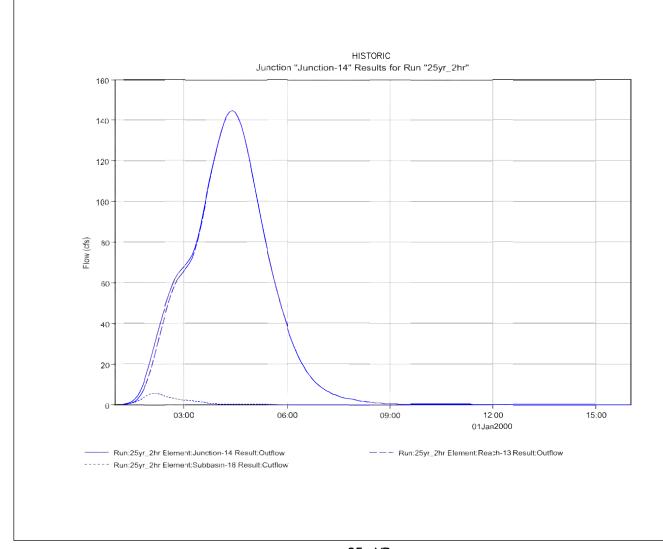


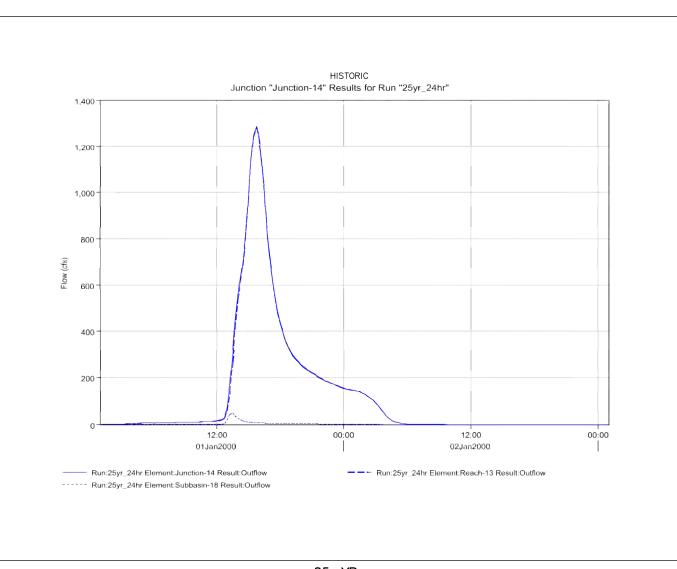
10-YR 24-HR 10-YR 2-HR

> JUNCTION 24 HWY 83 BRIDGE

HISTORIC CONDITIONS HYDROGRAPHS AT SELECT LOCATIONS 10-YEAR APPENDIX B — HYDROLOGIC RESULTS — HISTORIC HYDROGRAPHS 10—YRJ—24 KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B—32







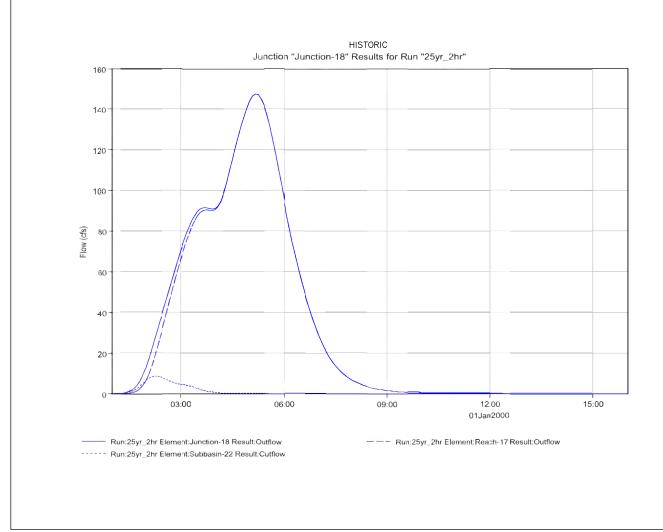
25-YR 2-HR 25-YR 24-HR

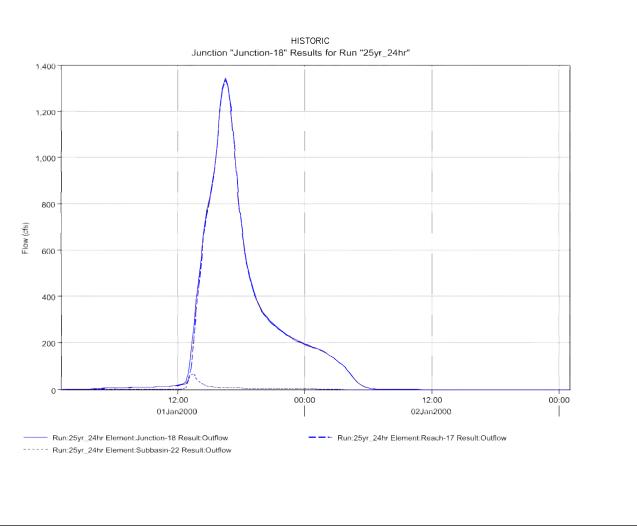
JUNCTION 14 HOWELLS ROAD (APPROXIMATE)

HISTORIC CONDITIONS HYDROGRAPHS
AT SELECT LOCATIONS
25-YEAR

APPENDIX B — HYDROLOGIC RESULTS — HISTORIC HYDROGRAPHS 25—YRJ—14 KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B—33







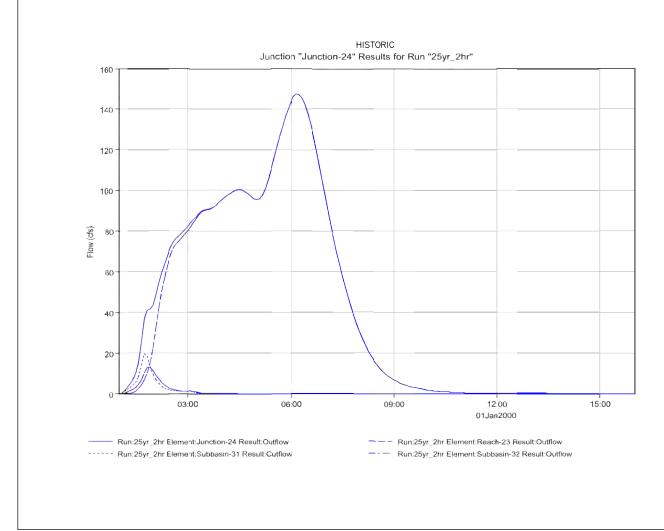
25-YR 2-HR 25-YR 24-HR

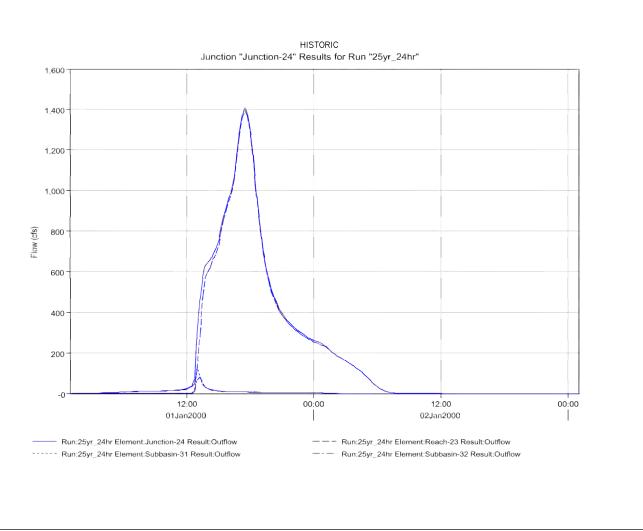
JUNCTION 18
POWERS BLVD BRIDGE

HISTORIC CONDITIONS HYDROGRAPHS
AT SELECT LOCATIONS
25-YEAR

APPENDIX B — HYDROLOGIC RESULTS — HISTORIC HYDROGRAPHS 25—YRJ—18 KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B—34





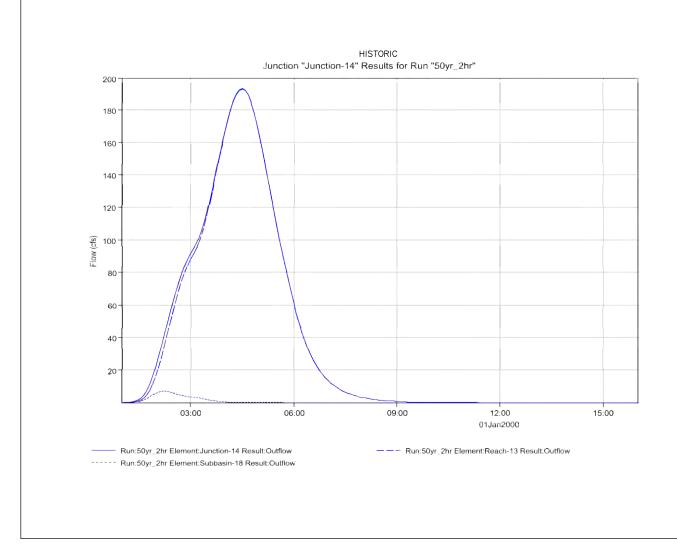


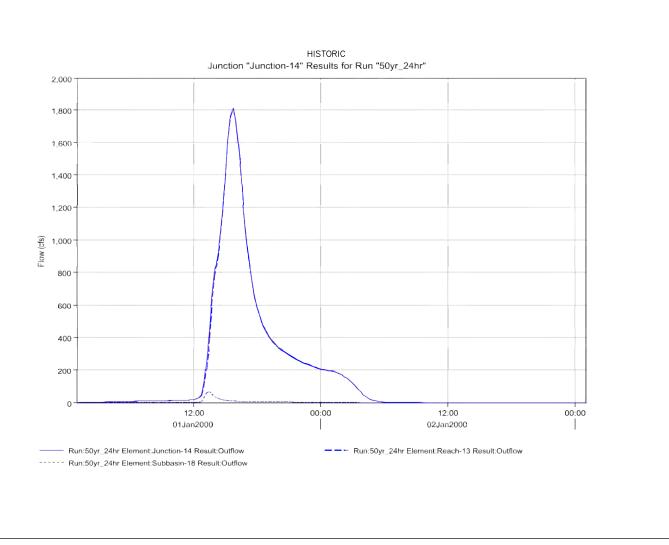
25-YR 2-HR 25-YR 24-HR

JUNCTION 24
HWY 83 BRIDGE
HISTORIC CONDITIONS HYDROGRAPHS
AT SELECT LOCATIONS
25-YEAR

APPENDIX B — HYDROLOGIC RESULTS — HISTORIC HYDROGRAPHS 25—YRJ—24 KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B—35





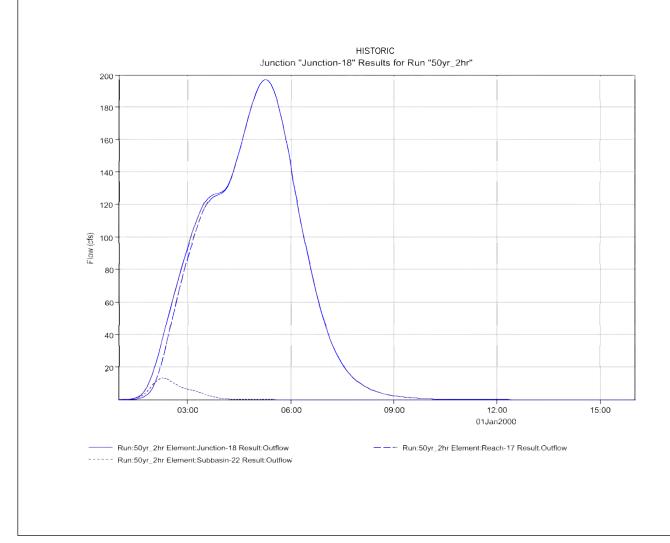


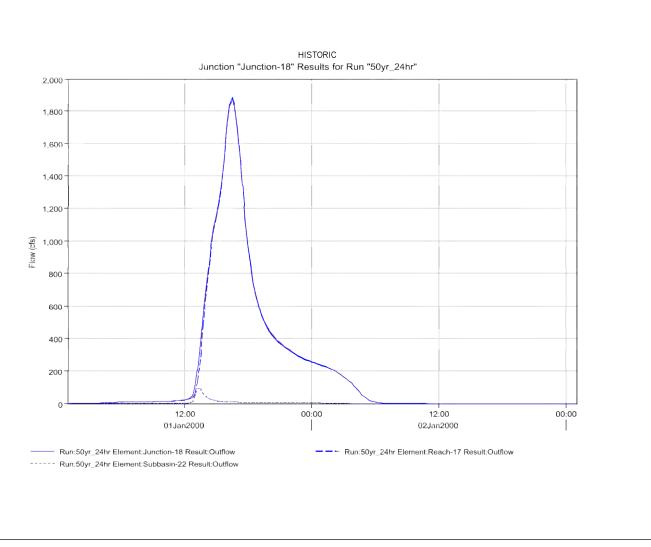
50-YR 2-HR 50-YR 24-HR

> JUNCTION 14 HOWELLS ROAD (APPROXIMATE)

HISTORIC CONDITIONS HYDROGRAPHS AT SELECT LOCATIONS 50-YEAR APPENDIX B — HYDROLOGIC RESULTS — HISTORIC HYDROGRAPHS 50—YRJ—14 KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B—36





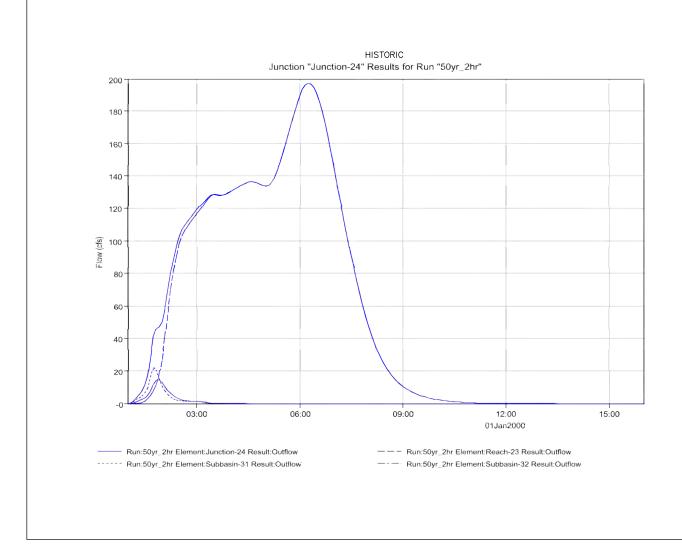


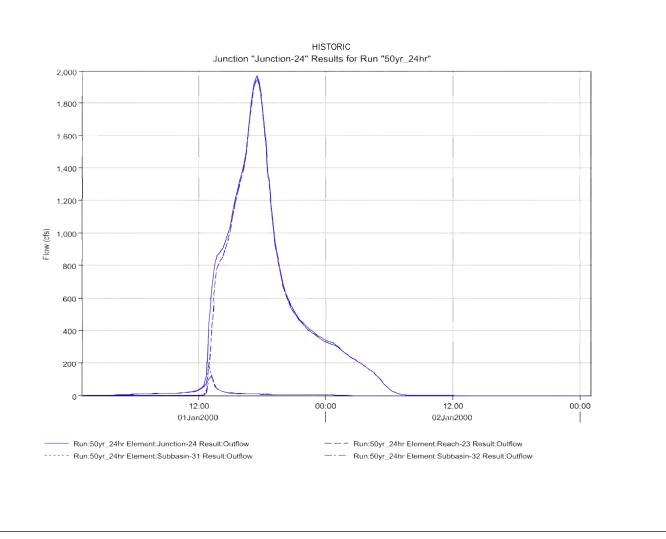
50-YR 2-HR 50-YR 24-HR

> JUNCTION 18 POWERS BLVD BRIDGE

HISTORIC CONDITIONS HYDROGRAPHS AT SELECT LOCATIONS 50-YEAR APPENDIX B — HYDROLOGIC RESULTS — HISTORIC HYDROGRAPHS 50—YRJ—18 KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B—37







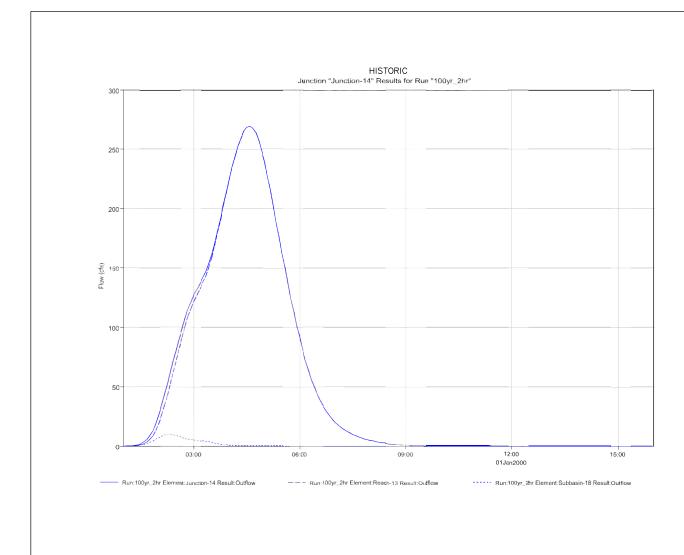
50-YR 2-HR 50-YR 24-HR

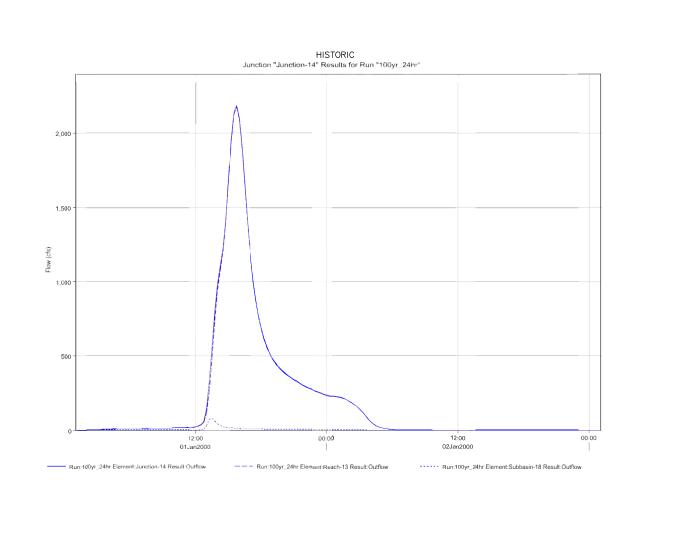
JUNCTION 24
HWY 83 BRIDGE

HISTORIC CONDITIONS HYDROGRAPHS
AT SELECT LOCATIONS
50-YEAR

APPENDIX B — HYDROLOGIC RESULTS — HISTORIC HYDROGRAPHS 50—YRJ—24 KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B—38



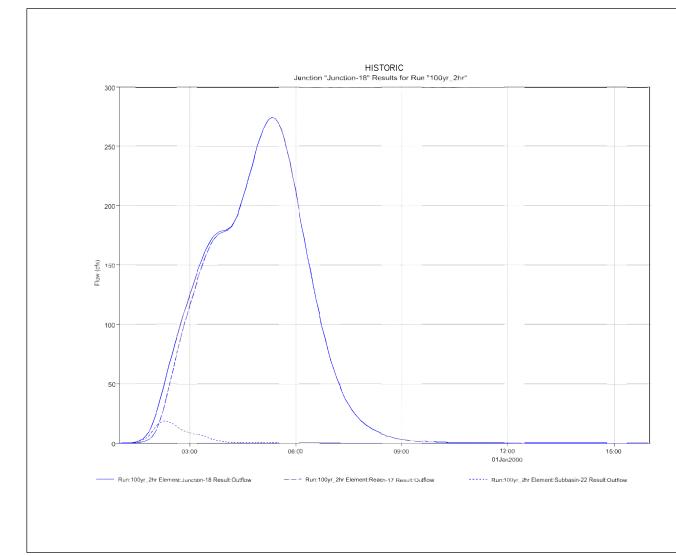


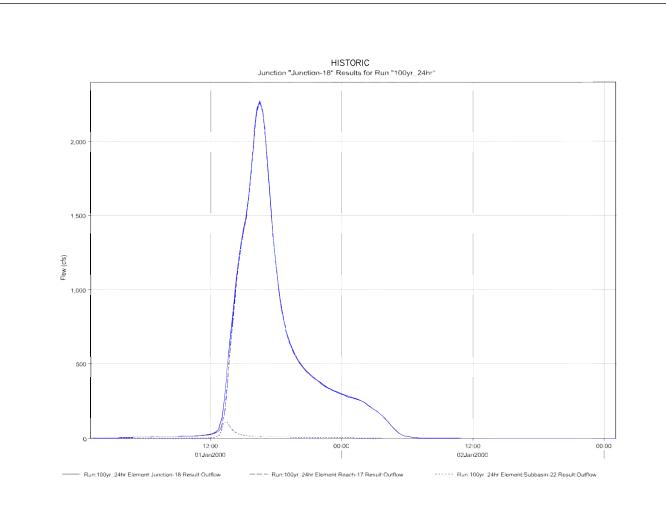


JUNCTION 14
HOWELLS ROAD (APPROXIMATE)
HISTORIC CONDITIONS HYDROGRAPHS
AT SELECT LOCATIONS
100-YEAR

APPENDIX B — HYDROLOGIC RESULTS HISTORIC HYDROGRAPHS 100—YRJ—14 KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B—39



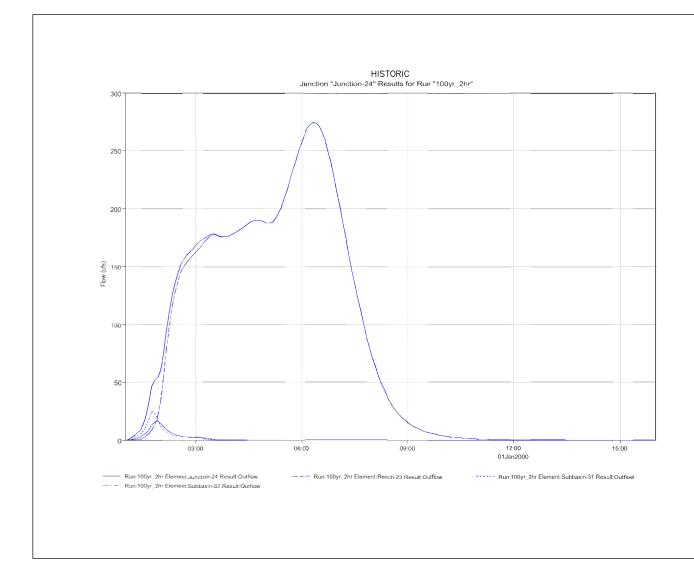


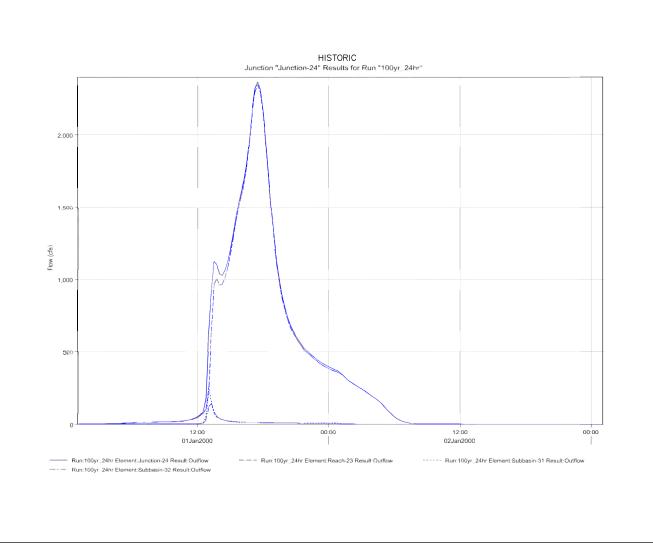


JUNCTION 18
POWERS BLVD BRIDGE
HISTORIC CONDITIONS HYDROGRAPHS
AT SELECT LOCATIONS
100-YEAR

APPENDIX B — HYDROLOGIC RESULTS HISTORIC HYDROGRAPHS 100—YRJ—18 KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B-40







> JUNCTION 24 HWY 83 BRIDGE

HISTORIC CONDITIONS HYDROGRAPHS AT SELECT LOCATIONS 100-YEAR APPENDIX B — HYDROLOGIC RESULTS HISTORIC HYDROGRAPHS 100—YRJ—24 KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B-41



EXISTING CONDITIONS MODEL RESULTS (2-YEAR)

| 2-Year, 2-Hour Storm | | | |
|----------------------|------------|-----------|--------|
| | | Peak | |
| Hydrologic | Drainage | Discharge | Volume |
| Element | Area (mi²) | (CFS) | (in) |
| Subbasin-1 | 1.263 | 140 | 0.35 |
| Subbasin-2 | 0.586 | 79 | 0.36 |
| Subbasin-3 | 0.180 | 29 | 0.47 |
| Junction-1 | 2.029 | 242 | 0.36 |
| Reach-1 | 2.029 | 242 | 0.39 |
| Subbasin-4 | 0.195 | 24 | 0.31 |
| Junction-2 | 2.224 | 263 | 0.38 |
| Reach-2 | 2.224 | 263 | 0.38 |
| Subbasin-5 | 0.625 | 59 | 0.38 |
| Junction-3 | 2.849 | 316 | 0.38 |
| Reach-3 | 2.849 | 316 | 0.39 |
| Subbasin-6 | 1.333 | 96 | 0.29 |
| Junction-4 | 4.182 | 412 | 0.36 |
| Reach-4 | 4.182 | 410 | 0.36 |
| Subbasin-7 | 0.183 | 21 | 0.3 |
| Junction-5 | 4.365 | 420 | 0.36 |
| Reach-5 | 4.365 | 420 | 0.36 |
| Subbasin-8 | 0.288 | 51 | 0.35 |
| Junction-6 | 4.653 | 431 | 0.36 |
| Reach-6 | 4.653 | 430 | 0.36 |
| Subbasin-9 | 1.177 | 95 | 0.35 |
| Subbasin-10 | 0.222 | 26 | 0.29 |
| Junction-7 | 1.399 | 106 | 0.34 |
| Reach-7 | 1.399 | 106 | 0.35 |
| Subbasin-11 | 0.880 | 152 | 0.42 |
| Junction-8 | 2.279 | 215 | 0.38 |
| Reach-8 | 2.279 | 215 | 0.39 |
| Subbasin-12 | 0.552 | 61 | 0.34 |
| Junction-9 | 2.831 | 268 | 0.38 |
| Reach-9 | 2.831 | 268 | 0.38 |
| Junction-10 | 7.484 | 639 | 0.37 |
| Reach-10 | 7.484 | 638 | 0.37 |
| Subbasin-13 | 1.156 | 88 | 0.32 |
| Subbasin-14 | 0.516 | 58 | 0.3 |
| Junction-11 | 9.156 | 709 | 0.36 |
| Reach-11 | 9.156 | 708 | 0.36 |
| Subbasin-15 | 0.498 | 61 | 0.32 |
| Junction-12 | 9.654 | 719 | 0.35 |
| Reach-12 | 9.654 | 718 | 0.35 |
| Subbasin-16 | 0.819 | 86 | 0.36 |
| Subbasin-17 | 0.788 | 78 | 0.3 |
| Junction-13 | 11.261 | 754 | 0.35 |

| 2-Year, 2-Hour Storm | | | |
|----------------------|-------------------------|-----------|--------|
| | | Peak | |
| Hydrologic | Drainage | Discharge | Volume |
| Element | Area (mi ²) | (CFS) | (in) |
| Reach-13 | 11.261 | 754 | 0.35 |
| Subbasin-18 | 0.192 | 24 | 0.3 |
| Junction-14 | 11.453 | 756 | 0.35 |
| Reach-14 | 11.453 | 756 | 0.35 |
| Subbasin-19 | 0.552 | 41 | 0.29 |
| Junction-15 | 12.005 | 769 | 0.35 |
| Reach-15 | 12.005 | 768 | 0.35 |
| Subbasin-20 | 0.594 | 52 | 0.25 |
| Junction-16 | 12.599 | 776 | 0.34 |
| Reach-16 | 12.599 | 776 | 0.34 |
| Subbasin-21 | 0.417 | 36 | 0.21 |
| Junction-17 | 13.016 | 780 | 0.34 |
| Reach-17 | 13.016 | 779 | 0.34 |
| Subbasin-22 | 0.200 | 8 | 0.11 |
| Junction-18 | 13.216 | 780 | 0.33 |
| Reach-18 | 13.216 | 779 | 0.33 |
| Subbasin-23 | 0.123 | 13 | 0.15 |
| Junction-19 | 13.339 | 780 | 0.33 |
| Reach-19 | 13.339 | 779 | 0.33 |
| Subbasin-24 | 0.453 | 38 | 0.3 |
| Subbasin-25 | 0.169 | 131 | 0.85 |
| Subbasin-26 | 0.480 | 54 | 0.36 |
| Junction-21 | 1.102 | 151 | 0.41 |
| Reach-21 | 1.102 | 149 | 0.43 |
| Subbasin-27 | 0.294 | 73 | 0.54 |
| Junction-22 | 1.396 | 200 | 0.46 |
| Reach-22 | 1.396 | 198 | 0.47 |
| Subbasin-28 | 0.264 | 8 | 0.1 |
| Subbasin-29 | 0.172 | 11 | 0.17 |
| Junction-20 | 0.436 | 18 | 0.13 |
| Reach-20 | 0.436 | 18 | 0.13 |
| Subbasin-30 | 0.364 | 52 | 0.32 |
| Junction-23 | 15.535 | 800 | 0.34 |
| Reach-23 | 15.535 | 800 | 0.34 |
| Subbasin-31 | 0.377 | 139 | 0.4 |
| Subbasin-32 | 0.316 | 75 | 0.36 |
| Junction-24 | 16.228 | 800 | 0.34 |
| Reach-24 | 16.228 | 799 | 0.34 |
| Subbasin-33 | 0.184 | 4 | 0.05 |
| Junction-25 | 16.412 | 1841.3 | 0.6 |
| Reach-25 | 16.412 | 1841.3 | 0.6 |
| Junction-26 | 16.412 | 1841.3 | 0.6 |

| 2-Year, 24-Hour Storm | | | |
|-----------------------|------------|-----------|--------|
| | | Peak | |
| Hydrologic | Drainage | Discharge | Volume |
| Element | Area (mi²) | (CFS) | (in) |
| Subbasin-1 | 1.263 | 207 | 0.71 |
| Subbasin-2 | 0.586 | 114 | 0.72 |
| Subbasin-3 | 0.180 | 38 | 0.88 |
| Junction-1 | 2.029 | 348 | 0.73 |
| Reach-1 | 2.029 | 348 | 0.73 |
| Subbasin-4 | 0.195 | 36 | 0.64 |
| Junction-2 | 2.224 | 377 | 0.72 |
| Reach-2 | 2.224 | 373 | 0.72 |
| Subbasin-5 | 0.625 | 89 | 0.78 |
| Junction-3 | 2.849 | 453 | 0.74 |
| Reach-3 | 2.849 | 453 | 0.74 |
| Subbasin-6 | 1.333 | 152 | 0.62 |
| Junction-4 | 4.182 | 606 | 0.70 |
| Reach-4 | 4.182 | 600 | 0.70 |
| Subbasin-7 | 0.183 | 33 | 0.64 |
| Junction-5 | 4.365 | 615 | 0.70 |
| Reach-5 | 4.365 | 607 | 0.70 |
| Subbasin-8 | 0.288 | 75.7 | 0.74 |
| Junction-6 | 4.653 | 626.9 | 0.7 |
| Reach-6 | 4.653 | 617 | 0.70 |
| Subbasin-9 | 1.177 | 146 | 0.71 |
| Subbasin-10 | 0.222 | 39 | 0.61 |
| Junction-7 | 1.399 | 165 | 0.69 |
| Reach-7 | 1.399 | 164 | 0.69 |
| Subbasin-11 | 0.880 | 216 | 0.85 |
| Junction-8 | 2.279 | 321 | 0.75 |
| Reach-8 | 2.279 | 321 | 0.75 |
| Subbasin-12 | 0.552 | 93 | 0.71 |
| Junction-9 | 2.831 | 402 | 0.74 |
| Reach-9 | 2.831 | 393 | 0.74 |
| Junction-10 | 7.484 | 946 | 0.72 |
| Reach-10 | 7.484 | 937 | 0.72 |
| Subbasin-13 | 1.156 | 137 | 0.67 |
| Subbasin-14 | 0.516 | 88 | 0.63 |
| Junction-11 | 9.156 | 1,051 | 0.70 |
| Reach-11 | 9.156 | 1,051 | 0.70 |
| Subbasin-15 | 0.498 | 92 | 0.67 |
| Junction-12 | 9.654 | 1,072 | 0.70 |
| Reach-12 | 9.654 | 1,071 | 0.70 |

| 2-Year, 24-Hour Storm | | | |
|-----------------------|------------|-----------|--------|
| | | Peak | |
| Hydrologic | Drainage | Discharge | Volume |
| Element | Area (mi²) | (CFS) | (in) |
| Subbasin-16 | 0.819 | 127 | 0.72 |
| Subbasin-17 | 0.788 | 118 | 0.63 |
| Junction-13 | 11.261 | 1,134 | 0.70 |
| Reach-13 | 11.261 | 1,119 | 0.70 |
| Subbasin-18 | 0.192 | 35.3 | 0.63 |
| Junction-14 | 11.453 | 1,123 | 0.70 |
| Reach-14 | 11.453 | 1,121 | 0.70 |
| Subbasin-19 | 0.552 | 65 | 0.62 |
| Junction-15 | 12.005 | 1,144 | 0.69 |
| Reach-15 | 12.005 | 1,141 | 0.69 |
| Subbasin-20 | 0.594 | 83 | 0.55 |
| Junction-16 | 12.599 | 1,154 | 0.69 |
| Reach-16 | 12.599 | 1,142 | 0.69 |
| Subbasin-21 | 0.417 | 60 | 0.50 |
| Junction-17 | 13.016 | 1,149 | 0.68 |
| Reach-17 | 13.016 | 1,149 | 0.68 |
| Subbasin-22 | 0.200 | 20 | 0.34 |
| Junction-18 | 13.216 | 1,151 | 0.68 |
| Reach-18 | 13.216 | 1,144 | 0.68 |
| Subbasin-23 | 0.123 | 24 | 0.40 |
| Junction-19 | 13.339 | 1,145 | 0.67 |
| Reach-19 | 13.339 | 1,145 | 0.67 |
| Subbasin-28 | 0.264 | 20 | 0.33 |
| Subbasin-29 | 0.172 | 21 | 0.43 |
| Junction-20 | 0.436 | 41 | 0.37 |
| Reach-20 | 0.436 | 38 | 0.37 |
| Subbasin-30 | 0.364 | 74 | 0.66 |
| Source-1 | 1.396 | 87 | 0.33 |
| Junction-23 | 15.535 | 1,172 | 0.63 |
| Reach-23 | 15.535 | 1,164 | 0.63 |
| Subbasin-31 | 0.377 | 147 | 0.74 |
| Subbasin-32 | 0.316 | 83 | 0.69 |
| Junction-24 | 16.228 | 1,174 | 0.64 |
| Reach-24 | 16.228 | 1,166 | 0.64 |
| Subbasin-33 | 0.184 | 10 | 0.19 |
| Junction-25 | 16.412 | 1,167 | 0.63 |
| Reach-25 | 16.412 | 1,164 | 0.63 |
| Junction-26 | 16.412 | 1,164 | 0.63 |

NOTE:

1. SOURCE-1 IS THE 24 HOUR FLOW DATA FOR SUBBASINS 24-27, JUNCTION 22, AND REACHES 21-22. SUBBASINS 24-27 DATA HAS BEEN REPLACED WITH KETTLE CREEK DRAINAGE BASIN OLD RANCH ROAD TRIBUTARY MASTER DEVELOPMENT PLAN FLOW DATA (JR ENG. 2001).

APPENDIX B — HYDROLOGIC RESULTS — EXISTING 2—YR KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B-42



EXISTING CONDITIONS MODEL RESULTS (5-YEAR)

| 5-Year, 2-Hour Storm | | | |
|----------------------|------------|-----------|--------|
| | | Peak | |
| Hydrologic | Drainage | Discharge | Volume |
| Element | Area (mi²) | (CFS) | (in) |
| Subbasin-1 | 1.263 | 286 | 0.51 |
| Subbasin-2 | 0.586 | 160 | 0.52 |
| Subbasin-3 | 0.180 | 56 | 0.65 |
| Junction-1 | 2.029 | 492 | 0.52 |
| Reach-1 | 2.029 | 490 | 0.52 |
| Subbasin-4 | 0.195 | 50 | 0.45 |
| Junction-2 | 2.224 | 536 | 0.52 |
| Reach-2 | 2.224 | 536 | 0.52 |
| Subbasin-5 | 0.625 | 119 | 0.56 |
| Junction-3 | 2.849 | 644 | 0.53 |
| Reach-3 | 2.849 | 644 | 0.53 |
| Subbasin-6 | 1.333 | 203 | 0.43 |
| Junction-4 | 4.182 | 846 | 0.5 |
| Reach-4 | 4.182 | 846 | 0.5 |
| Subbasin-7 | 0.183 | 45 | 0.44 |
| Junction-5 | 4.365 | 865 | 0.49 |
| Reach-5 | 4.365 | 862 | 0.49 |
| Subbasin-8 | 0.288 | 104 | 0.52 |
| Junction-6 | 4.653 | 885 | 0.49 |
| Reach-6 | 4.653 | 883 | 0.49 |
| Subbasin-9 | 1.177 | 195 | 0.51 |
| Subbasin-10 | 0.222 | 55 | 0.43 |
| Junction-7 | 1.399 | 217 | 0.49 |
| Reach-7 | 1.399 | 217 | 0.49 |
| Subbasin-11 | 0.880 | 302 | 0.61 |
| Junction-8 | 2.279 | 437 | 0.54 |
| Reach-8 | 2.279 | 434 | 0.54 |
| Subbasin-12 | 0.552 | 127 | 0.5 |
| Junction-9 | 2.831 | 546 | 0.53 |
| Reach-9 | 2.831 | 545 | 0.53 |
| Junction-10 | 7.484 | 1,305 | 0.51 |
| Reach-10 | 7.484 | 1,305 | 0.51 |
| Subbasin-13 | 1.156 | 183 | 0.47 |
| Subbasin-14 | 0.516 | 122 | 0.44 |
| Junction-11 | 9.156 | 1,437 | 0.5 |
| Reach-11 | 9.156 | 1,435 | 0.5 |
| Subbasin-15 | 0.498 | 127 | 0.47 |
| Junction-12 | 9.654 | 1,445 | 0.5 |
| Reach-12 | 9.654 | 1,442 | 0.5 |
| Subbasin-16 | 0.819 | 175 | 0.51 |
| Subbasin-17 | 0.788 | 164 | 0.44 |
| Junction-13 | 11.261 | 1,475 | 0.49 |

| 5-Year, 2-Hour Storm | | | |
|----------------------|------------|-----------|--------|
| | | Peak | |
| Hydrologic | Drainage | Discharge | Volume |
| Element | Area (mi²) | (CFS) | (in) |
| Reach-13 | 11.261 | 1,473 | 0.49 |
| Subbasin-18 | 0.192 | 50 | 0.44 |
| Junction-14 | 11.453 | 1,473 | 0.49 |
| Reach-14 | 11.453 | 1,473 | 0.49 |
| Subbasin-19 | 0.552 | 86 | 0.44 |
| Junction-15 | 12.005 | 1,488 | 0.49 |
| Reach-15 | 12.005 | 1,485 | 0.49 |
| Subbasin-20 | 0.594 | 113 | 0.38 |
| Junction-16 | 12.599 | 1,487 | 0.49 |
| Reach-16 | 12.599 | 1,487 | 0.49 |
| Subbasin-21 | 0.417 | 82 | 0.43 |
| Junction-17 | 13.016 | 1,487 | 0.33 |
| Reach-17 | 13.016 | 1,487 | 0.48 |
| | | , | |
| Subbasin-22 | 0.200 | 24 | 0.21 |
| Junction-18 | 13.216 | 1,486 | 0.48 |
| Reach-18 | 13.216 | 1,484 | 0.48 |
| Subbasin-23 | 0.123 | 30 | 0.25 |
| Junction-19 | 13.339 | 1,484 | 0.47 |
| Reach-19 | 13.339 | 1,482 | 0.47 |
| Subbasin-24 | 0.453 | 81 | 0.45 |
| Subbasin-25 | 0.169 | 206 | 1.12 |
| Subbasin-26 | 0.480 | 111 | 0.51 |
| Junction-21 | 1.102 | 250 | 0.58 |
| Reach-21 | 1.102 | 245 | 0.58 |
| Subbasin-27 | 0.294 | 139 | 0.75 |
| Junction-22 | 1.396 | 346 | 0.61 |
| Reach-22 | 1.396 | 344 | 0.61 |
| Subbasin-28 | 0.264 | 25 | 0.19 |
| Subbasin-29 | 0.172 | 28 | 0.27 |
| Junction-20 | 0.436 | 50 | 0.22 |
| Reach-20 | 0.436 | 50 | 0.22 |
| Subbasin-30 | 0.364 | 107 | 0.47 |
| Junction-23 | 15.535 | 1,484 | 0.48 |
| Reach-23 | 15.535 | 1,482 | 0.48 |
| Subbasin-31 | 0.377 | 219 | 0.55 |
| Subbasin-32 | 0.316 | 137 | 0.5 |
| Junction-24 | 16.228 | 1,482 | 0.48 |
| Reach-24 | 16.228 | 1,481 | 0.48 |
| Subbasin-33 | 0.184 | 13 | 0.1 |
| Junction-25 | 16.412 | 1481.1 | 0.48 |
| Reach-25 | 16.412 | 1481.1 | 0.48 |
| Junction-26 | 16.412 | 1481.1 | 0.48 |

| 5-Year, 24-Hour Storm | | | |
|-----------------------|------------|-----------|--------|
| | | Peak | |
| Hydrologic | Drainage | Discharge | Volume |
| Element | Area (mi²) | (CFS) | (in) |
| Subbasin-1 | 1.263 | 315 | 1.06 |
| Subbasin-2 | 0.586 | 173 | 1.06 |
| Subbasin-3 | 0.180 | 56 | 1.27 |
| Junction-1 | 2.029 | 527 | 1.08 |
| Reach-1 | 2.029 | 526 | 1.08 |
| Subbasin-4 | 0.195 | 56 | 0.97 |
| Junction-2 | 2.224 | 572 | 1.07 |
| Reach-2 | 2.224 | 568 | 1.07 |
| Subbasin-5 | 0.625 | 134 | 1.14 |
| Junction-3 | 2.849 | 689 | 1.08 |
| Reach-3 | 2.849 | 689 | 1.08 |
| Subbasin-6 | 1.333 | 240 | 0.94 |
| Junction-4 | 4.182 | 928 | 1.04 |
| Reach-4 | 4.182 | 917 | 1.04 |
| Subbasin-7 | 0.183 | 51 | 0.97 |
| Junction-5 | 4.365 | 940 | 1.03 |
| Reach-5 | 4.365 | 929 | 1.03 |
| Subbasin-8 | 0.288 | 117 | 1.1 |
| Junction-6 | 4.653 | 959 | 1.04 |
| Reach-6 | 4.653 | 944 | 1.04 |
| Subbasin-9 | 1.177 | 223 | 1.05 |
| Subbasin-10 | 0.222 | 62 | 0.93 |
| Junction-7 | 1.399 | 252 | 1.03 |
| Reach-7 | 1.399 | 250 | 1.03 |
| Subbasin-11 | 0.880 | 322 | 1.23 |
| Junction-8 | 2.279 | 484 | 1.11 |
| Reach-8 | 2.279 | 484 | 1.11 |
| Subbasin-12 | 0.552 | 144 | 1.06 |
| Junction-9 | 2.831 | 609 | 1.1 |
| Reach-9 | 2.831 | 594 | 1.1 |
| Junction-10 | 7.484 | 1,444 | 1.06 |
| Reach-10 | 7.484 | 1,428 | 1.06 |
| Subbasin-13 | 1.156 | 212 | 1 |
| Subbasin-14 | 0.516 | 138 | 0.95 |
| Junction-11 | 9.156 | 1,605 | 1.05 |
| Reach-11 | 9.156 | 1,604 | 1.05 |
| Subbasin-15 | 0.498 | 143 | 1 |
| Junction-12 | 9.654 | 1,636 | 1.05 |
| Reach-12 | 9.654 | 1,634 | 1.05 |

| 5-Year, 24-Hour Storm | | | |
|-----------------------|------------|-----------|--------|
| | | Peak | |
| Hydrologic | Drainage | Discharge | Volume |
| Element | Area (mi²) | (CFS) | (in) |
| Subbasin-16 | 0.819 | 193 | 1.06 |
| Subbasin-17 | 0.788 | 184 | 0.95 |
| Junction-13 | 11.261 | 1,730 | 1.04 |
| Reach-13 | 11.261 | 1,705 | 1.04 |
| Subbasin-18 | 0.192 | 55 | 0.95 |
| Junction-14 | 11.453 | 1,711 | 1.04 |
| Reach-14 | 11.453 | 1,710 | 1.04 |
| Subbasin-19 | 0.552 | 101 | 0.95 |
| Junction-15 | 12.005 | 1,745 | 1.03 |
| Reach-15 | 12.005 | 1,741 | 1.03 |
| Subbasin-20 | 0.594 | 134 | 0.86 |
| Junction-16 | 12.599 | 1,760 | 1.03 |
| Reach-16 | 12.599 | 1,741 | 1.03 |
| Subbasin-21 | 0.417 | 100 | 0.79 |
| Junction-17 | 13.016 | 1,752 | 1.02 |
| Reach-17 | 13.016 | 1,752 | 1.02 |
| Subbasin-22 | 0.200 | 36 | 0.59 |
| Junction-18 | 13.216 | 1,756 | 1.01 |
| Reach-18 | 13.216 | 1,746 | 1.01 |
| Subbasin-23 | 0.123 | 42 | 0.66 |
| Junction-19 | 13.339 | 1,748 | 1.01 |
| Reach-19 | 13.339 | 1,747 | 1.01 |
| Source-1 | 1.396 | 109 | 0.58 |
| Subbasin-28 | 0.264 | 38 | 0.57 |
| Subbasin-29 | 0.172 | 37 | 0.7 |
| Junction-20 | 0.436 | 75 | 0.62 |
| Reach-20 | 0.436 | 70 | 0.62 |
| Subbasin-30 | 0.364 | 116 | 1 |
| Junction-23 | 15.535 | 1,764 | 0.96 |
| Reach-23 | 15.535 | 1,751 | 0.96 |
| Subbasin-31 | 0.377 | 217 | 1.05 |
| Subbasin-32 | 0.316 | 124 | 1.01 |
| Junction-24 | 16.228 | 1,766 | 0.96 |
| Reach-24 | 16.228 | 1,754 | 0.96 |
| Subbasin-33 | 0.184 | 24 | 0.37 |
| Junction-25 | 16.412 | 1,756 | 0.96 |
| Reach-25 | 16.412 | 1,750 | 0.96 |
| Junction-26 | 16.412 | 1,750 | 0.96 |

NOTE:

1. SOURCE-1 IS THE 24 HOUR FLOW DATA FOR SUBBASINS 24-27, JUNCTION 22, AND REACHES 21-22. SUBBASINS 24-27 DATA HAS BEEN REPLACED WITH KETTLE CREEK DRAINAGE BASIN OLD RANCH ROAD TRIBUTARY MASTER DEVELOPMENT PLAN FLOW DATA (JR ENG. 2001).

APPENDIX B — HYDROLOGIC RESULTS — EXISTING 5—YR KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B-43



EXISTING CONDITIONS MODEL RESULTS (10-YEAR)

| 10-Year, 2-Hour Storm | | | |
|-----------------------|------------|-----------|--------|
| | | Peak | |
| Hydrologic | Drainage | Discharge | Volume |
| Element | Area (mi²) | (CFS) | (in) |
| Subbasin-1 | 1.263 | 354 | 0.63 |
| Subbasin-2 | 0.586 | 198 | 0.64 |
| Subbasin-3 | 0.180 | 68 | 0.79 |
| Junction-1 | 2.029 | 608 | 0.65 |
| Reach-1 | 2.029 | 606 | 0.65 |
| Subbasin-4 | 0.195 | 63 | 0.57 |
| Junction-2 | 2.224 | 663 | 0.64 |
| Reach-2 | 2.224 | 663 | 0.64 |
| Subbasin-5 | 0.625 | 147 | 0.69 |
| Junction-3 | 2.849 | 797 | 0.65 |
| Reach-3 | 2.849 | 797 | 0.65 |
| Subbasin-6 | 1.333 | 255 | 0.54 |
| Junction-4 | 4.182 | 1,051 | 0.62 |
| Reach-4 | 4.182 | 1,051 | 0.62 |
| Subbasin-7 | 0.183 | 56 | 0.56 |
| Junction-5 | 4.365 | 1,074 | 0.61 |
| Reach-5 | 4.365 | 1,071 | 0.61 |
| Subbasin-8 | 0.288 | 131 | 0.65 |
| Junction-6 | 4.653 | 1,099 | 0.62 |
| Reach-6 | 4.653 | 1,097 | 0.62 |
| Subbasin-9 | 1.177 | 242 | 0.63 |
| Subbasin-10 | 0.222 | 70 | 0.54 |
| Junction-7 | 1.399 | 269 | 0.61 |
| Reach-7 | 1.399 | 269 | 0.61 |
| Subbasin-11 | 0.880 | 373 | 0.75 |
| Junction-8 | 2.279 | 540 | 0.67 |
| Reach-8 | 2.279 | 537 | 0.67 |
| Subbasin-12 | 0.552 | 159 | 0.62 |
| Junction-9 | 2.831 | 677 | 0.66 |
| Reach-9 | 2.831 | 675 | 0.66 |
| Junction-10 | 7.484 | 1,619 | 0.63 |
| Reach-10 | 7.484 | 1,619 | 0.63 |
| Subbasin-13 | 1.156 | 229 | 0.59 |
| Subbasin-14 | 0.516 | 153 | 0.55 |
| Junction-11 | 9.156 | 1,784 | 0.62 |
| Reach-11 | 9.156 | 1,782 | 0.62 |
| Subbasin-15 | 0.498 | 159 | 0.59 |
| Junction-12 | 9.654 | 1,795 | 0.62 |
| Reach-12 | 9.654 | 1,792 | 0.62 |
| Subbasin-16 | 0.819 | 217 | 0.64 |
| Subbasin-17 | 0.788 | 206 | 0.55 |
| Junction-13 | 11.261 | 1,833 | 0.62 |
| J G 110 C1 O11 13 | 11.201 | 1,000 | 0.02 |

| 10-Year, 2-Hour Storm | | | |
|-----------------------|------------|-----------|--------|
| | | Peak | |
| Hydrologic | Drainage | Discharge | Volume |
| Element | Area (mi²) | (CFS) | (in) |
| Reach-13 | 11.261 | 1,830 | 0.62 |
| Subbasin-18 | 0.192 | 63 | 0.55 |
| Junction-14 | 11.453 | 1,831 | 0.62 |
| Reach-14 | 11.453 | 1,830 | 0.62 |
| Subbasin-19 | 0.552 | 108 | 0.55 |
| Junction-15 | 12.005 | 1,850 | 0.61 |
| Reach-15 | 12.005 | 1,847 | 0.61 |
| Subbasin-20 | 0.594 | 145 | 0.48 |
| Junction-16 | 12.599 | 1,849 | 0.61 |
| Reach-16 | 12.599 | 1,849 | 0.61 |
| Subbasin-21 | 0.417 | 107 | 0.43 |
| Junction-17 | 13.016 | 1,849 | 0.43 |
| Reach-17 | 13.016 | 1,847 | 0.6 |
| Subbasin-22 | 0.200 | 35 | 0.29 |
| Junction-18 | 13.216 | 1,847 | 0.6 |
| Reach-18 | 13.216 | 1,845 | 0.6 |
| Subbasin-23 | 0.123 | 41 | 0.34 |
| | 13.339 | 1,845 | 0.59 |
| Junction-19 | | , | |
| Reach-19 | 13.339 | 1,843 | 0.59 |
| Subbasin-24 | 0.453 | 102 | 0.56 |
| Subbasin-25 | 0.169 | 242 | 1.31 |
| Subbasin-26 | 0.480 | 138 | 0.63 |
| Junction-21 | 1.102 | 295 | 0.71 |
| Reach-21 | 1.102 | 289 | 0.71 |
| Subbasin-27 | 0.294 | 167 | 0.9 |
| Junction-22 | 1.396 | 410 | 0.75 |
| Reach-22 | 1.396 | 409 | 0.75 |
| Subbasin-28 | 0.264 | 35 | 0.27 |
| Subbasin-29 | 0.172 | 38 | 0.37 |
| Junction-20 | 0.436 | 70 | 0.31 |
| Reach-20 | 0.436 | 69 | 0.31 |
| Subbasin-30 | 0.364 | 135 | 0.58 |
| Junction-23 | 15.535 | 1,845 | 0.6 |
| Reach-23 | 15.535 | 1,842 | 0.6 |
| Subbasin-31 | 0.377 | 264 | 0.66 |
| Subbasin-32 | 0.316 | 168 | 0.61 |
| Junction-24 | 16.228 | 1,842 | 0.6 |
| Reach-24 | 16.228 | 1,841 | 0.6 |
| Subbasin-33 | 0.184 | 20 | 0.16 |
| Junction-25 | 16.412 | 1841.3 | 0.6 |
| Reach-25 | 16.412 | 1841.3 | 0.6 |
| Junction-26 | 16.412 | 1841.3 | 0.6 |

| 10-Year, 24-Hour Storm | | | |
|------------------------|------------|-----------|--------|
| | | Peak | |
| Hydrologic | Drainage | Discharge | Volume |
| Element | Area (mi²) | (CFS) | (in) |
| Subbasin-1 | 1.263 | 416 | 1.37 |
| Subbasin-2 | 0.586 | 228 | 1.38 |
| Subbasin-3 | 0.180 | 72 | 1.61 |
| Junction-1 | 2.029 | 693 | 1.40 |
| Reach-1 | 2.029 | 692 | 1.40 |
| Subbasin-4 | 0.195 | 75 | 1.27 |
| Junction-2 | 2.224 | 753 | 1.38 |
| Reach-2 | 2.224 | 748 | 1.38 |
| Subbasin-5 | 0.625 | 176 | 1.48 |
| Junction-3 | 2.849 | 908 | 1.41 |
| Reach-3 | 2.849 | 908 | 1.41 |
| Subbasin-6 | 1.333 | 322 | 1.23 |
| Junction-4 | 4.182 | 1,230 | 1.35 |
| Reach-4 | 4.182 | 1,213 | 1.35 |
| Subbasin-7 | 0.183 | 69 | 1.27 |
| Junction-5 | 4.365 | 1,244 | 1.35 |
| Reach-5 | 4.365 | 1,230 | 1.35 |
| Subbasin-8 | 0.288 | 154.4 | 1.44 |
| Junction-6 | 4.653 | 1269 | 1.35 |
| Reach-6 | 4.653 | 1,248 | 1.35 |
| Subbasin-9 | 1.177 | 294 | 1.36 |
| Subbasin-10 | 0.222 | 84 | 1.23 |
| Junction-7 | 1.399 | 333 | 1.34 |
| Reach-7 | 1.399 | 331 | 1.34 |
| Subbasin-11 | 0.880 | 419 | 1.58 |
| Junction-8 | 2.279 | 636 | 1.44 |
| Reach-8 | 2.279 | 635 | 1.44 |
| Subbasin-12 | 0.552 | 190 | 1.38 |
| Junction-9 | 2.831 | 800 | 1.43 |
| Reach-9 | 2.831 | 781 | 1.43 |
| Junction-10 | 7.484 | 1,907 | 1.38 |
| Reach-10 | 7.484 | 1,885 | 1.38 |
| Subbasin-13 | 1.156 | 282 | 1.31 |
| Subbasin-14 | 0.516 | 185 | 1.25 |
| Junction-11 | 9.156 | 2,122 | 1.36 |
| Reach-11 | 9.156 | 2,120 | 1.36 |
| Subbasin-15 | 0.498 | 190 | 1.31 |
| Junction-12 | 9.654 | 2,162 | 1.36 |
| Reach-12 | 9.654 | 2,160 | 1.36 |

| 10-Year, 24-Hour Storm | | | |
|------------------------|-------------------------|-----------|--------|
| | | Peak | |
| Hydrologic | Drainage | Discharge | Volume |
| Element | Area (mi ²) | (CFS) | (in) |
| Subbasin-16 | 0.819 | 254 | 1.38 |
| Subbasin-17 | 0.788 | 247 | 1.25 |
| Junction-13 | 11.261 | 2,284 | 1.35 |
| Reach-13 | 11.261 | 2,250 | 1.35 |
| Subbasin-18 | 0.192 | 74 | 1.25 |
| Junction-14 | 11.453 | 2,258 | 1.35 |
| Reach-14 | 11.453 | 2,257 | 1.35 |
| Subbasin-19 | 0.552 | 136 | 1.24 |
| Junction-15 | 12.005 | 2,304 | 1.35 |
| Reach-15 | 12.005 | 2,298 | 1.35 |
| Subbasin-20 | 0.594 | 183 | 1.14 |
| Junction-16 | 12.599 | 2,324 | 1.34 |
| Reach-16 | 12.599 | 2,298 | 1.34 |
| Subbasin-21 | 0.417 | 139 | 1.06 |
| Junction-17 | 13.016 | 2,312 | 1.33 |
| Reach-17 | 13.016 | 2,312 | 1.33 |
| Subbasin-22 | 0.200 | 53 | 0.84 |
| Junction-18 | 13.216 | 2,318 | 1.32 |
| Reach-18 | 13.216 | 2,307 | 1.32 |
| Subbasin-23 | 0.123 | 60 | 0.91 |
| Junction-19 | 13.339 | 2,310 | 1.32 |
| Reach-19 | 13.339 | 2,308 | 1.32 |
| Source-1 | 1.396 | 188 | 0.77 |
| Subbasin-28 | 0.264 | 57 | 0.82 |
| Subbasin-29 | 0.172 | 52 | 0.96 |
| Junction-20 | 0.436 | 109 | 0.88 |
| Reach-20 | 0.436 | 101 | 0.88 |
| Subbasin-30 | 0.364 | 155 | 1.31 |
| Junction-23 | 15.535 | 2,331 | 1.26 |
| Reach-23 | 15.535 | 2,311 | 1.26 |
| Subbasin-31 | 0.377 | 282 | 1.35 |
| Subbasin-32 | 0.316 | 164 | 1.30 |
| Junction-24 | 16.228 | 2,332 | 1.26 |
| Reach-24 | 16.228 | 2,317 | 1.26 |
| Subbasin-33 | 0.184 | 39 | 0.55 |
| Junction-25 | 16.412 | 2,320 | 1.25 |
| Reach-25 | 16.412 | 2,312 | 1.25 |
| Junction-26 | 16.412 | 2,312 | 1.25 |

NOTE:

1. SOURCE-1 IS THE 24 HOUR FLOW DATA FOR SUBBASINS 24-27, JUNCTION 22, AND REACHES 21-22. SUBBASINS 24-27 DATA HAS BEEN REPLACED WITH KETTLE CREEK DRAINAGE BASIN OLD RANCH ROAD TRIBUTARY MASTER DEVELOPMENT PLAN FLOW DATA (JR ENG. 2001).

APPENDIX B — HYDROLOGIC RESULTS — EXISTING 10—YR KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B-44



EXISTING CONDITIONS MODEL RESULTS (25-YEAR)

| 25-Year, 2-Hour Storm | | | |
|-----------------------|------------|-----------|--------|
| | | Peak | |
| Hydrologic | Drainage | Discharge | Volume |
| Element | Area (mi²) | (CFS) | (in) |
| Subbasin-1 | 1.263 | 442 | 0.78 |
| Subbasin-2 | 0.586 | 248 | 0.79 |
| Subbasin-3 | 0.180 | 83 | 0.96 |
| Junction-1 | 2.029 | 757 | 0.80 |
| Reach-1 | 2.029 | 755 | 0.80 |
| Subbasin-4 | 0.195 | 80 | 0.71 |
| Junction-2 | 2.224 | 827 | 0.79 |
| Reach-2 | 2.224 | 827 | 0.79 |
| Subbasin-5 | 0.625 | 184 | 0.85 |
| Junction-3 | 2.849 | 994 | 0.81 |
| Reach-3 | 2.849 | 994 | 0.81 |
| Subbasin-6 | 1.333 | 324 | 0.68 |
| Junction-4 | 4.182 | 1,316 | 0.77 |
| Reach-4 | 4.182 | 1,316 | 0.77 |
| Subbasin-7 | 0.183 | 72 | 0.70 |
| Junction-5 | 4.365 | 1,346 | 0.76 |
| Reach-5 | 4.365 | 1,341 | 0.76 |
| Subbasin-8 | 0.288 | 166 | 0.81 |
| Junction-6 | 4.653 | 1,376 | 0.77 |
| Reach-6 | 4.653 | 1,374 | 0.77 |
| Subbasin-9 | 1.177 | 302 | 0.78 |
| Subbasin-10 | 0.222 | 89 | 0.68 |
| Junction-7 | 1.399 | 337 | 0.76 |
| Reach-7 | 1.399 | 337 | 0.76 |
| Subbasin-11 | 0.880 | 463 | 0.92 |
| Junction-8 | 2.279 | 672 | 0.82 |
| Reach-8 | 2.279 | 669 | 0.82 |
| Subbasin-12 | 0.552 | 201 | 0.78 |
| Junction-9 | 2.831 | 844 | 0.82 |
| Reach-9 | 2.831 | 843 | 0.82 |
| Junction-10 | 7.484 | 2,025 | 0.79 |
| Reach-10 | 7.484 | 2,023 | 0.79 |
| Subbasin-13 | 1.156 | 288 | 0.73 |
| Subbasin-14 | 0.516 | 194 | 0.69 |
| Junction-11 | 9.156 | 2,228 | 0.77 |
| Reach-11 | 9.156 | 2,226 | 0.77 |
| Subbasin-15 | 0.498 | 201 | 0.73 |
| Junction-12 | 9.654 | 2,242 | 0.77 |
| Reach-12 | 9.654 | 2,238 | 0.77 |
| Subbasin-16 | 0.819 | 270 | 0.79 |
| Subbasin-17 | 0.788 | 261 | 0.69 |
| Junction-13 | 11.261 | 2,288 | 0.77 |

| 25-Year, 2-Hour Storm | | | |
|-----------------------|------------|-----------|--------|
| | | Peak | |
| Hydrologic | Drainage | Discharge | Volume |
| Element | Area (mi²) | (CFS) | (in) |
| Reach-13 | 11.261 | 2,285 | 0.77 |
| Subbasin-18 | 0.192 | 80 | 0.69 |
| Junction-14 | 11.453 | 2,286 | 0.77 |
| Reach-14 | 11.453 | 2,284 | 0.77 |
| Subbasin-19 | 0.552 | 137 | 0.69 |
| Junction-15 | 12.005 | 2,309 | 0.76 |
| Reach-15 | 12.005 | 2,305 | 0.76 |
| Subbasin-20 | 0.594 | 186 | 0.70 |
| Junction-16 | | | |
| | 12.599 | 2,308 | 0.76 |
| Reach-16 | 12.599 | 2,307 | 0.76 |
| Subbasin-21 | 0.417 | 141 | 0.55 |
| Junction-17 | 13.016 | 2,307 | 0.75 |
| Reach-17 | 13.016 | 2,305 | 0.75 |
| Subbasin-22 | 0.200 | 48 | 0.39 |
| Junction-18 | 13.216 | 2,305 | 0.74 |
| Reach-18 | 13.216 | 2,303 | 0.74 |
| Subbasin-23 | 0.123 | 57 | 0.45 |
| Junction-19 | 13.339 | 2,303 | 0.74 |
| Reach-19 | 13.339 | 2,300 | 0.74 |
| Subbasin-24 | 0.453 | 129 | 0.71 |
| Subbasin-25 | 0.169 | 285 | 1.54 |
| Subbasin-26 | 0.480 | 172 | 0.79 |
| Junction-21 | 1.102 | 349 | 0.87 |
| Reach-21 | 1.102 | 343 | 0.87 |
| Subbasin-27 | 0.294 | 203 | 1.09 |
| Junction-22 | 1.396 | 496 | 0.92 |
| Reach-22 | 1.396 | 495 | 0.92 |
| Subbasin-28 | 0.264 | 49 | 0.38 |
| Subbasin-29 | 0.172 | 51 | 0.48 |
| Junction-20 | 0.436 | 96 | 0.42 |
| Reach-20 | 0.436 | 95 | 0.42 |
| Subbasin-30 | 0.364 | 171 | 0.73 |
| Junction-23 | 15.535 | 2,302 | 0.75 |
| Reach-23 | 15.535 | 2,298 | 0.75 |
| Subbasin-31 | 0.377 | 325 | 0.80 |
| Subbasin-32 | 0.316 | 209 | 0.75 |
| Junction-24 | 16.228 | 2,298 | 0.75 |
| Reach-24 | 16.228 | 2,298 | 0.75 |
| Subbasin-33 | 0.184 | 31 | 0.23 |
| Junction-25 | 16.412 | 2297.5 | 0.74 |
| Reach-25 | 16.412 | 2297.5 | 0.74 |
| Junction-26 | 16.412 | 2297.5 | 0.74 |

| 25-Year, 24-Hour Storm | | | | | |
|------------------------|------------|-----------|--------|--|--|
| | Peak | | | | |
| Hydrologic | Drainage | Discharge | Volume | | |
| Element | Area (mi²) | (CFS) | (in) | | |
| Subbasin-1 | 1.263 | 502 | 1.64 | | |
| Subbasin-2 | 0.586 | 276 | 1.65 | | |
| Subbasin-3 | 0.180 | 86 | 1.90 | | |
| Junction-1 | 2.029 | 835 | 1.67 | | |
| Reach-1 | 2.029 | 834 | 1.67 | | |
| Subbasin-4 | 0.195 | 91 | 1.53 | | |
| Junction-2 | 2.224 | 907 | 1.65 | | |
| Reach-2 | 2.224 | 903 | 1.65 | | |
| Subbasin-5 | 0.625 | 212 | 1.76 | | |
| Junction-3 | 2.849 | 1,095 | 1.68 | | |
| Reach-3 | 2.849 | 1,095 | 1.68 | | |
| Subbasin-6 | 1.333 | 393 | 1.49 | | |
| Junction-4 | 4.182 | 1,488 | 1.62 | | |
| Reach-4 | 4.182 | 1,467 | 1.62 | | |
| Subbasin-7 | 0.183 | 84 | 1.53 | | |
| Junction-5 | 4.365 | 1,504 | 1.61 | | |
| Reach-5 | 4.365 | 1,488 | 1.61 | | |
| Subbasin-8 | 0.288 | 187 | 1.72 | | |
| Junction-6 | 4.653 | 1,535 | 1.62 | | |
| Reach-6 | 4.653 | 1,509 | 1.62 | | |
| Subbasin-9 | 1.177 | 355 | 1.63 | | |
| Subbasin-10 | 0.222 | 102 | 1.48 | | |
| Junction-7 | 1.399 | 403 | 1.61 | | |
| Reach-7 | 1.399 | 401 | 1.61 | | |
| Subbasin-11 | 0.880 | 501 | 1.88 | | |
| Junction-8 | 2.279 | 766 | 1.71 | | |
| Reach-8 | 2.279 | 764 | 1.71 | | |
| Subbasin-12 | 0.552 | 230 | 1.65 | | |
| Junction-9 | 2.831 | 964 | 1.70 | | |
| Reach-9 | 2.831 | 941 | 1.70 | | |
| Junction-10 | 7.484 | 2,304 | 1.65 | | |
| Reach-10 | 7.484 | 2,276 | 1.65 | | |
| Subbasin-13 | 1.156 | 342 | 1.57 | | |
| Subbasin-14 | 0.516 | 226 | 1.51 | | |
| Junction-11 | 9.156 | 2,565 | 1.63 | | |
| Reach-11 | 9.156 | 2,563 | 1.63 | | |
| Subbasin-15 | 0.498 | 231 | 1.57 | | |
| Junction-12 | 9.654 | 2,613 | 1.63 | | |
| Reach-12 | 9.654 | 2,609 | 1.63 | | |

| 25-Year, 24-Hour Storm | | | |
|------------------------|-------------------------|-----------|--------|
| | | Peak | |
| Hydrologic | Drainage | Discharge | Volume |
| Element | Area (mi ²) | (CFS) | (in) |
| Subbasin-16 | 0.819 | 307 | 1.65 |
| Subbasin-17 | 0.788 | 301 | 1.51 |
| Junction-13 | 11.261 | 2,759 | 1.62 |
| Reach-13 | 11.261 | 2,715 | 1.62 |
| Subbasin-18 | 0.192 | 90 | 1.50 |
| Junction-14 | 11.453 | 2,726 | 1.62 |
| Reach-14 | 11.453 | 2,725 | 1.62 |
| Subbasin-19 | 0.552 | 166 | 1.50 |
| Junction-15 | 12.005 | 2,781 | 1.62 |
| Reach-15 | 12.005 | 2,774 | 1.62 |
| Subbasin-20 | 0.594 | 226 | 1.39 |
| Junction-16 | 12.599 | 2,806 | 1.60 |
| Reach-16 | 12.599 | 2,774 | 1.60 |
| Subbasin-21 | 0.417 | 172 | 1.30 |
| Junction-17 | 13.016 | 2,793 | 1.59 |
| Reach-17 | 13.016 | 2,791 | 1.59 |
| Subbasin-22 | 0.200 | 68 | 1.06 |
| Junction-18 | 13.216 | 2,798 | 1.59 |
| Reach-18 | 13.216 | 2,787 | 1.59 |
| Subbasin-23 | 0.123 | 76 | 1.13 |
| Junction-19 | 13.339 | 2,791 | 1.58 |
| Reach-19 | 13.339 | 2,788 | 1.58 |
| Source-1 | 1.396 | 333 | 1.11 |
| Subbasin-28 | 0.264 | 73 | 1.03 |
| Subbasin-29 | 0.172 | 65 | 1.19 |
| Junction-20 | 0.436 | 138 | 1.10 |
| Reach-20 | 0.436 | 129 | 1.10 |
| Subbasin-30 | 0.364 | 188 | 1.57 |
| Junction-23 | 15.535 | 2,816 | 1.53 |
| Reach-23 | 15.535 | 2,791 | 1.53 |
| Subbasin-31 | 0.377 | 338 | 1.59 |
| Subbasin-32 | 0.316 | 197 | 1.55 |
| Junction-24 | 16.228 | 2,814 | 1.53 |
| Reach-24 | 16.228 | 2,798 | 1.53 |
| Subbasin-33 | 0.184 | 53 | 0.72 |
| Junction-25 | 16.412 | 2,802 | 1.52 |
| Reach-25 | 16.412 | 2,791 | 1.52 |
| Junction-26 | 16.412 | 2,791 | 1.52 |

NOTE:

1. SOURCE-1 IS THE 24 HOUR FLOW DATA FOR SUBBASINS 24-27, JUNCTION 22, AND REACHES 21-22. SUBBASINS 24-27 DATA HAS BEEN REPLACED WITH KETTLE CREEK DRAINAGE BASIN OLD RANCH ROAD TRIBUTARY MASTER DEVELOPMENT PLAN FLOW DATA (JR ENG. 2001).

APPENDIX B — HYDROLOGIC RESULTS — EXISTING 25—YR KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B-45



EXISTING CONDITIONS MODEL RESULTS (50-YEAR)

| 50-Year, 2-Hour Storm | | | |
|-----------------------|------------|-----------|--------|
| | | Peak | |
| Hydrologic | Drainage | Discharge | Volume |
| Element | Area (mi²) | (CFS) | (in) |
| Subbasin-1 | 1.263 | 533 | 0.94 |
| Subbasin-2 | 0.586 | 299 | 0.95 |
| Subbasin-3 | 0.180 | 98 | 1.14 |
| Junction-1 | 2.029 | 911 | 0.96 |
| Reach-1 | 2.029 | 909 | 0.96 |
| Subbasin-4 | 0.195 | 97 | 0.86 |
| Junction-2 | 2.224 | 996 | 0.95 |
| Reach-2 | 2.224 | 996 | 0.95 |
| Subbasin-5 | 0.625 | 221 | 1.02 |
| Junction-3 | 2.849 | 1,197 | 0.97 |
| Reach-3 | 2.849 | 1,197 | 0.97 |
| Subbasin-6 | 1.333 | 395 | 0.83 |
| Junction-4 | 4.182 | 1,590 | 0.92 |
| Reach-4 | 4.182 | 1,589 | 0.92 |
| Subbasin-7 | 0.183 | 88 | 0.86 |
| Junction-5 | 4.365 | 1,626 | 0.92 |
| Reach-5 | 4.365 | 1,620 | 0.92 |
| Subbasin-8 | 0.288 | 202 | 0.98 |
| Junction-6 | 4.653 | 1,662 | 0.92 |
| Reach-6 | 4.653 | 1,659 | 0.92 |
| Subbasin-9 | 1.177 | 364 | 0.94 |
| Subbasin-10 | 0.222 | 109 | 0.82 |
| Junction-7 | 1.399 | 406 | 0.92 |
| Reach-7 | 1.399 | 406 | 0.92 |
| Subbasin-11 | 0.880 | 555 | 1.10 |
| Junction-8 | 2.279 | 808 | 0.99 |
| Reach-8 | 2.279 | 804 | 0.99 |
| Subbasin-12 | 0.552 | 243 | 0.94 |
| Junction-9 | 2.831 | 1,017 | 0.98 |
| Reach-9 | 2.831 | 1,015 | 0.98 |
| Junction-10 | 7.484 | 2,442 | 0.95 |
| Reach-10 | 7.484 | 2,440 | 0.95 |
| Subbasin-13 | 1.156 | 349 | 0.89 |
| Subbasin-14 | 0.516 | 237 | 0.84 |
| Junction-11 | 9.156 | 2,688 | 0.93 |
| Reach-11 | 9.156 | 2,686 | 0.93 |
| Subbasin-15 | 0.498 | 245 | 0.89 |
| Junction-12 | 9.654 | 2,705 | 0.93 |
| Reach-12 | 9.654 | 2,700 | 0.93 |
| Subbasin-16 | 0.819 | 325 | 0.95 |
| Subbasin-17 | 0.788 | 318 | 0.84 |
| Junction-13 | 11.261 | 2,759 | 0.93 |

| 50-Year, 2-Hour Storm | | | |
|-----------------------|------------|-----------|--------|
| | | Peak | |
| Hydrologic | Drainage | Discharge | Volume |
| Element | Area (mi²) | (CFS) | (in) |
| Reach-13 | 11.261 | 2,757 | 0.93 |
| Subbasin-18 | 0.192 | 98 | 0.84 |
| Junction-14 | 11.453 | 2,757 | 0.92 |
| Reach-14 | 11.453 | 2,756 | 0.92 |
| Subbasin-19 | 0.552 | 167 | 0.84 |
| Junction-15 | 12.005 | 2,786 | 0.92 |
| Reach-15 | 12.005 | 2,781 | 0.92 |
| Subbasin-20 | 0.594 | 230 | 0.75 |
| Junction-16 | 12.599 | 2,784 | 0.91 |
| Reach-16 | 12.599 | 2,784 | 0.91 |
| Subbasin-21 | 0.417 | 177 | 0.69 |
| Junction-17 | 13.016 | 2,784 | 0.91 |
| Reach-17 | 13.016 | 2,780 | 0.91 |
| Subbasin-22 | 0.200 | 63 | 0.51 |
| Junction-18 | 13.216 | 2,780 | 0.90 |
| Reach-18 | 13.216 | 2,778 | 0.90 |
| Subbasin-23 | 0.123 | 74 | 0.57 |
| Junction-19 | 13.339 | 2,778 | 0.90 |
| Reach-19 | 13.339 | 2,775 | 0.90 |
| Subbasin-24 | 0.453 | 157 | 0.86 |
| Subbasin-25 | 0.169 | 329 | 1.77 |
| Subbasin-26 | 0.480 | 207 | 0.95 |
| Junction-21 | 1.102 | 404 | 1.04 |
| Reach-21 | 1.102 | 397 | 1.04 |
| Subbasin-27 | 0.294 | 240 | 1.28 |
| Junction-22 | 1.396 | 587 | 1.09 |
| Reach-22 | 1.396 | 586 | 1.09 |
| Subbasin-28 | 0.264 | 65 | 0.49 |
| Subbasin-29 | 0.172 | 65 | 0.61 |
| Junction-20 | 0.436 | 124 | 0.54 |
| Reach-20 | 0.436 | 123 | 0.54 |
| Subbasin-30 | 0.364 | 208 | 0.89 |
| Junction-23 | 15.535 | 2,777 | 0.90 |
| Reach-23 | 15.535 | 2,772 | 0.90 |
| Subbasin-31 | 0.377 | 388 | 0.95 |
| Subbasin-32 | 0.316 | 251 | 0.90 |
| Junction-24 | 16.228 | 2,772 | 0.90 |
| Reach-24 | 16.228 | 2,772 | 0.90 |
| Subbasin-33 | 0.184 | 43 | 0.31 |
| Junction-25 | 16.412 | 2771.5 | 0.9 |
| Reach-25 | 16.412 | 2771.5 | 0.9 |
| Junction-26 | 16.412 | 2771.5 | 0.9 |

| 50-Year, 24-Hour Storm | | | | |
|------------------------|-------------------------|-------------------|--------|--|
| | | | | |
| Hudrologic | Drainage | Peak Discharge | Volume | |
| Hydrologic Element | Area (mi ²) | | | |
| | ì | (CFS) | (in) | |
| Subbasin-1 | 1.263 | 639 | 2.06 | |
| Subbasin-2 | 0.586 | 351 | 2.07 | |
| Subbasin-3 | 0.180 | 107 | 2.36 | |
| Junction-1 | 2.029 | 1,060 | 2.09 | |
| Reach-1 | 2.029 | 1,059 | 2.09 | |
| Subbasin-4 | 0.195 | 117 | 1.94 | |
| Junction-2 | 2.224 | 1,153 | 2.08 | |
| Reach-2 | 2.224 | 1,150 | 2.08 | |
| Subbasin-5 | 0.625 | 268 | 2.21 | |
| Junction-3 | 2.849 | 1,393 | 2.11 | |
| Reach-3 | 2.849 | 1,393 | 2.11 | |
| Subbasin-6 | 1.333 | 508 | 1.90 | |
| Junction-4 | 4.182 | 1,901 | 2.04 | |
| Reach-4 | 4.182 | 1,871 | 2.04 | |
| Subbasin-7 | 0.183 | 108 | 1.95 | |
| Junction-5 | 4.365 | 1,918 | 2.04 | |
| Reach-5 | 4.365 | 1,899 | 2.04 | |
| Subbasin-8 | 0.288 | 238 | 2.17 | |
| Junction-6 | 4.653 | 1,958 | 2.04 | |
| Reach-6 | 4.653 | 1,923 | 2.04 | |
| Subbasin-9 | 1.177 | 452 | 2.06 | |
| Subbasin-10 | 0.222 | 132 | 1.89 | |
| Junction-7 | 1.399 | 515 | 2.03 | |
| Reach-7 | 1.399 | 511 | 2.03 | |
| Subbasin-11 | 0.880 | 631 | 2.34 | |
| Junction-8 | 2.279 | 971 | 2.15 | |
| Reach-8 | 2.279 | 969 | 2.15 | |
| Subbasin-12 | 0.552 | 294 | 2.09 | |
| Junction-9 | 2.831 | 1,223 | 2.14 | |
| Reach-9 | 2.831 | 1,193 | 2.14 | |
| Junction-10 | 7.484 | 2,934 | 2.08 | |
| Reach-10 | 7.484 | 2,896 | 2.08 | |
| Subbasin-13 | 1.156 | 438 | 1.99 | |
| Subbasin-14 | 0.516 | 291 | 1.92 | |
| Junction-11 | 9.156 | 3,269 | 2.06 | |
| Reach-11 | 9.156 | 3,265 | 2.06 | |
| Subbasin-15 | 0.498 | 296 | 1.99 | |
| Junction-12 | 9.654 | 3,328 | 2.06 | |
| Reach-12 | 9.654 | 3,324 | 2.06 | |

| 50-Year, 24-Hour Storm | | | |
|------------------------|-------------------------|-----------|--------|
| | | Peak | |
| Hydrologic | Drainage | Discharge | Volume |
| Element | Area (mi ²) | (CFS) | (in) |
| Subbasin-16 | 0.819 | 391 | 2.07 |
| Subbasin-17 | 0.788 | 387 | 1.92 |
| Junction-13 | 11.261 | 3,512 | 2.05 |
| Reach-13 | 11.261 | 3,456 | 2.05 |
| Subbasin-18 | 0.192 | 116 | 1.91 |
| Junction-14 | 11.453 | 3,471 | 2.05 |
| Reach-14 | 11.453 | 3,469 | 2.05 |
| Subbasin-19 | 0.552 | 214 | 1.91 |
| Junction-15 | 12.005 | 3,540 | 2.04 |
| Reach-15 | 12.005 | 3,530 | 2.04 |
| Subbasin-20 | 0.594 | 294 | 1.78 |
| Junction-16 | 12.599 | 3,570 | 2.03 |
| Reach-16 | 12.599 | 3,534 | 2.03 |
| Subbasin-21 | 0.417 | 226 | 1.69 |
| Junction-17 | 13.016 | 3,557 | 2.02 |
| Reach-17 | 13.016 | 3,551 | 2.02 |
| Subbasin-22 | 0.200 | 92 | 1.41 |
| Junction-18 | 13.216 | 3,560 | 2.01 |
| Reach-18 | 13.216 | 3,549 | 2.01 |
| Subbasin-23 | 0.123 | 102 | 1.50 |
| Junction-19 | 13.339 | 3,553 | 2.00 |
| Reach-19 | 13.339 | 3,549 | 2.00 |
| Source-1 | 1.396 | 459 | 1.34 |
| Subbasin-28 | 0.264 | 100 | 1.38 |
| Subbasin-29 | 0.172 | 87 | 1.56 |
| Junction-20 | 0.436 | 187 | 1.45 |
| Reach-20 | 0.436 | 174 | 1.45 |
| Subbasin-30 | 0.364 | 242 | 1.99 |
| Junction-23 | 15.535 | 3,584 | 1.93 |
| Reach-23 | 15.535 | 3,551 | 1.93 |
| Subbasin-31 | 0.377 | 427 | 1.99 |
| Subbasin-32 | 0.316 | 251 | 1.94 |
| Junction-24 | 16.228 | 3,580 | 1.93 |
| Reach-24 | 16.228 | 3,563 | 1.93 |
| Subbasin-33 | 0.184 | 76 | 1.00 |
| Junction-25 | 16.412 | 3,568 | 1.92 |
| Reach-25 | 16.412 | 3,553 | 1.92 |
| Junction-26 | 16.412 | 3,553 | 1.92 |

NOTE:

1. SOURCE-1 IS THE 24 HOUR FLOW DATA FOR SUBBASINS 24-27, JUNCTION 22, AND REACHES 21-22. SUBBASINS 24-27 DATA HAS BEEN REPLACED WITH KETTLE CREEK DRAINAGE BASIN OLD RANCH ROAD TRIBUTARY MASTER DEVELOPMENT PLAN FLOW DATA (JR ENG. 2001).

APPENDIX B — HYDROLOGIC RESULTS — EXISTING 50—YR KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B-46



EXISTING CONDITIONS MODEL RESULTS (100-YEAR)

| 100-Year, 2-Hour Storm | | | |
|------------------------|------------|-----------|--------|
| | | Peak | |
| Hydrologic | Drainage | Discharge | Volume |
| Element | Area (mi²) | (CFS) | (in) |
| Subbasin-1 | 1.263 | 634 | 1.12 |
| Subbasin-2 | 0.586 | 355 | 1.13 |
| Subbasin-3 | 0.180 | 115 | 1.33 |
| Junction-1 | 2.029 | 1,082 | 1.14 |
| Reach-1 | 2.029 | 1,080 | 1.14 |
| Subbasin-4 | 0.195 | 117 | 1.03 |
| Junction-2 | 2.224 | 1,184 | 1.13 |
| Reach-2 | 2.224 | 1,184 | 1.13 |
| Subbasin-5 | 0.625 | 262 | 1.21 |
| Junction-3 | 2.849 | 1,423 | 1.15 |
| Reach-3 | 2.849 | 1,423 | 1.15 |
| Subbasin-6 | 1.333 | 474 | 0.99 |
| Junction-4 | 4.182 | 1,895 | 1.10 |
| Reach-4 | 4.182 | 1,894 | 1.10 |
| Subbasin-7 | 0.183 | 106 | 1.03 |
| Junction-5 | 4.365 | 1,938 | 1.10 |
| Reach-5 | 4.365 | 1,931 | 1.10 |
| Subbasin-8 | 0.288 | 242 | 1.17 |
| Junction-6 | 4.653 | 1,980 | 1.10 |
| Reach-6 | 4.653 | 1,977 | 1.10 |
| Subbasin-9 | 1.177 | 433 | 1.11 |
| Subbasin-10 | 0.222 | 132 | 0.99 |
| Junction-7 | 1.399 | 483 | 1.09 |
| Reach-7 | 1.399 | 483 | 1.09 |
| Subbasin-11 | 0.880 | 657 | 1.30 |
| Junction-8 | 2.279 | 959 | 1.17 |
| Reach-8 | 2.279 | 953 | 1.17 |
| Subbasin-12 | 0.552 | 291 | 1.12 |
| Junction-9 | 2.831 | 1,208 | 1.16 |
| Reach-9 | 2.831 | 1,205 | 1.16 |
| Junction-10 | 7.484 | 2,905 | 1.12 |
| Reach-10 | 7.484 | 2,903 | 1.12 |
| Subbasin-13 | 1.156 | 418 | 1.06 |
| Subbasin-14 | 0.516 | 285 | 1.01 |
| Junction-11 | 9.156 | 3,198 | 1.11 |
| Reach-11 | 9.156 | 3,195 | 1.11 |
| Subbasin-15 | 0.498 | 293 | 1.06 |
| Junction-12 | 9.654 | 3,218 | 1.11 |
| Reach-12 | 9.654 | 3,213 | 1.11 |
| Subbasin-16 | 0.819 | 387 | 1.12 |
| Subbasin-17 | 0.788 | 382 | 1.01 |
| Junction-13 | 11.261 | 3,283 | 1.10 |

| 100-Year, 2-Hour Storm | | | |
|------------------------|-------------------------|-----------|--------|
| | | Peak | |
| Hydrologic | Drainage | Discharge | Volume |
| Element | Area (mi ²) | (CFS) | (in) |
| Reach-13 | 11.261 | 3,280 | 1.10 |
| Subbasin-18 | 0.192 | 118 | 1.01 |
| Junction-14 | 11.453 | 3,281 | 1.10 |
| Reach-14 | 11.453 | 3,279 | 1.10 |
| Subbasin-19 | 0.552 | 201 | 1.00 |
| Junction-15 | 12.005 | 3,314 | 1.09 |
| Reach-15 | 12.005 | 3,309 | 1.09 |
| Subbasin-20 | 0.594 | 279 | 0.91 |
| Junction-16 | 12.599 | 3,313 | 1.09 |
| Reach-16 | 12.599 | 3,312 | 1.09 |
| Subbasin-21 | 0.417 | 217 | 0.84 |
| Junction-17 | 13.016 | 3,312 | 1.08 |
| Reach-17 | 13.016 | 3,308 | 1.08 |
| Subbasin-22 | 0.200 | 81 | 0.64 |
| Junction-18 | 13.216 | 3,308 | 1.07 |
| Reach-18 | 13.216 | 3,305 | 1.07 |
| Subbasin-23 | 0.123 | 93 | 0.71 |
| Junction-19 | 13.339 | 3,305 | 1.07 |
| Reach-19 | 13.339 | 3,302 | 1.07 |
| Subbasin-24 | 0.453 | 188 | 1.03 |
| Subbasin-25 | 0.169 | 374 | 2.01 |
| Subbasin-26 | 0.480 | 247 | 1.12 |
| Junction-21 | 1.102 | 463 | 1.22 |
| Reach-21 | 1.102 | 463 | 1.22 |
| Subbasin-27 | 0.294 | 279 | 1.49 |
| Junction-22 | 1.396 | 689 | 1.28 |
| Reach-22 | 1.396 | 687 | 1.28 |
| Subbasin-28 | 0.264 | 83 | 0.62 |
| Subbasin-29 | 0.172 | 80 | 0.75 |
| Junction-20 | 0.436 | 157 | 0.67 |
| Reach-20 | 0.436 | 156 | 0.67 |
| Subbasin-30 | 0.364 | 250 | 1.06 |
| Junction-23 | 15.535 | 3,305 | 1.08 |
| Reach-23 | 15.535 | 3,298 | 1.08 |
| Subbasin-31 | 0.377 | 458 | 1.11 |
| Subbasin-32 | 0.316 | 298 | 1.06 |
| Junction-24 | 16.228 | 3,298 | 1.08 |
| Reach-24 | 16.228 | 3,297 | 1.08 |
| Subbasin-33 | 0.184 | 57 | 0.41 |
| Junction-25 | 16.412 | 3297.4 | 1.07 |
| Reach-25 | 16.412 | 3297.4 | 1.07 |
| Junction-26 | 16.412 | 3297.4 | 1.07 |

| 100-Year, 24-Hour Storm | | | | | |
|-------------------------|------------|-----------|--------|--|--|
| | Peak | | | | |
| Hydrologic | Drainage | Discharge | Volume | | |
| Element | Area (mi²) | (CFS) | (in) | | |
| Subbasin-1 | 1.263 | 735 | 2.36 | | |
| Subbasin-2 | 0.586 | 403 | 2.37 | | |
| Subbasin-3 | 0.180 | 122 | 2.67 | | |
| Junction-1 | 2.029 | 1,217 | 2.39 | | |
| Reach-1 | 2.029 | 1,216 | 2.39 | | |
| Subbasin-4 | 0.195 | 135 | 2.22 | | |
| Junction-2 | 2.224 | 1,325 | 2.38 | | |
| Reach-2 | 2.224 | 1,322 | 2.38 | | |
| Subbasin-5 | 0.625 | 308 | 2.52 | | |
| Junction-3 | 2.849 | 1,602 | 2.41 | | |
| Reach-3 | 2.849 | 1,602 | 2.41 | | |
| Subbasin-6 | 1.333 | 588 | 2.18 | | |
| Junction-4 | 4.182 | 2,190 | 2.34 | | |
| Reach-4 | 4.182 | 2,153 | 2.34 | | |
| Subbasin-7 | 0.183 | 125 | 2.24 | | |
| Junction-5 | 4.365 | 2,208 | 2.33 | | |
| Reach-5 | 4.365 | 2,186 | 2.33 | | |
| Subbasin-8 | 0.288 | 273.3 | 2.48 | | |
| Junction-6 | 4.653 | 2253.3 | 2.34 | | |
| Reach-6 | 4.653 | 2,213 | 2.34 | | |
| Subbasin-9 | 1.177 | 520 | 2.35 | | |
| Subbasin-10 | 0.222 | 152 | 2.17 | | |
| Junction-7 | 1.399 | 593 | 2.32 | | |
| Reach-7 | 1.399 | 588 | 2.32 | | |
| Subbasin-11 | 0.880 | 720 | 2.66 | | |
| Junction-8 | 2.279 | 1,114 | 2.45 | | |
| Reach-8 | 2.279 | 1,112 | 2.45 | | |
| Subbasin-12 | 0.552 | 338 | 2.39 | | |
| Junction-9 | 2.831 | 1,403 | 2.44 | | |
| Reach-9 | 2.831 | 1,368 | 2.44 | | |
| Junction-10 | 7.484 | 3,375 | 2.38 | | |
| Reach-10 | 7.484 | 3,329 | 2.38 | | |
| Subbasin-13 | 1.156 | 505 | 2.28 | | |
| Subbasin-14 | 0.516 | 337 | 2.20 | | |
| Junction-11 | 9.156 | 3,761 | 2.36 | | |
| Reach-11 | 9.156 | 3,756 | 2.36 | | |
| Subbasin-15 | 0.498 | 342 | 2.28 | | |
| Junction-12 | 9.654 | 3,828 | 2.35 | | |
| Reach-12 | 9.654 | 3,823 | 2.35 | | |

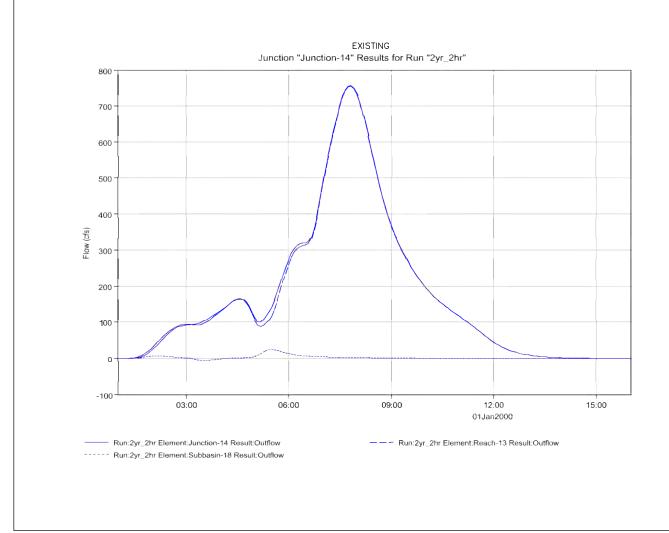
| 100-Year, 24-Hour Storm | | | |
|-------------------------|------------|-----------|--------|
| | | Peak | |
| Hydrologic | Drainage | Discharge | Volume |
| Element | Area (mi²) | (CFS) | (in) |
| Subbasin-16 | 0.819 | 449 | 2.37 |
| Subbasin-17 | 0.788 | 447 | 2.20 |
| Junction-13 | 11.261 | 4,038 | 2.34 |
| Reach-13 | 11.261 | 3,975 | 2.34 |
| Subbasin-18 | 0.192 | 134.1 | 2.2 |
| Junction-14 | 11.453 | 3,992 | 2.34 |
| Reach-14 | 11.453 | 3,987 | 2.34 |
| Subbasin-19 | 0.552 | 248 | 2.19 |
| Junction-15 | 12.005 | 4,069 | 2.33 |
| Reach-15 | 12.005 | 4,058 | 2.33 |
| Subbasin-20 | 0.594 | 343 | 2.06 |
| Junction-16 | 12.599 | 4,103 | 2.32 |
| Reach-16 | 12.599 | 4,064 | 2.32 |
| Subbasin-21 | 0.417 | 264 | 1.96 |
| Junction-17 | 13.016 | 4,091 | 2.31 |
| Reach-17 | 13.016 | 4,081 | 2.31 |
| Subbasin-22 | 0.200 | 109 | 1.66 |
| Junction-18 | 13.216 | 4,091 | 2.30 |
| Reach-18 | 13.216 | 4,080 | 2.30 |
| Subbasin-23 | 0.123 | 121 | 1.75 |
| Junction-19 | 13.339 | 4,086 | 2.29 |
| Reach-19 | 13.339 | 4,081 | 2.29 |
| Source-1 | 1.396 | 576 | 1.58 |
| Subbasin-28 | 0.264 | 120 | 1.63 |
| Subbasin-29 | 0.172 | 102 | 1.83 |
| Junction-20 | 0.436 | 222 | 1.71 |
| Reach-20 | 0.436 | 207 | 1.71 |
| Subbasin-30 | 0.364 | 279 | 2.28 |
| Junction-23 | 15.535 | 4,121 | 2.21 |
| Reach-23 | 15.535 | 4,081 | 2.21 |
| Subbasin-31 | 0.377 | 490 | 2.26 |
| Subbasin-32 | 0.316 | 289 | 2.22 |
| Junction-24 | 16.228 | 4,114 | 2.22 |
| Reach-24 | 16.228 | 4,096 | 2.22 |
| Subbasin-33 | 0.184 | 93 | 1.21 |
| Junction-25 | 16.412 | 4,102 | 2.20 |
| Reach-25 | 16.412 | 4,084 | 2.20 |
| Junction-26 | 16.412 | 4,084 | 2.20 |

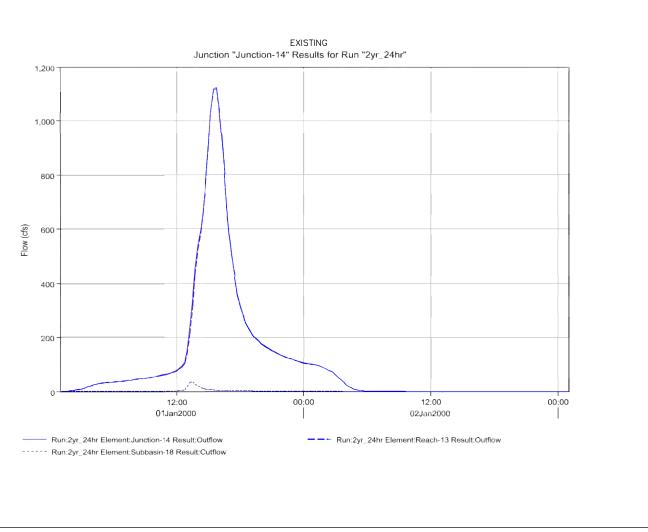
NOTE:

1. SOURCE-1 IS THE 24 HOUR FLOW DATA FOR SUBBASINS 24-27, JUNCTION 22, AND REACHES 21-22. SUBBASINS 24-27 DATA HAS BEEN REPLACED WITH KETTLE CREEK DRAINAGE BASIN OLD RANCH ROAD TRIBUTARY MASTER DEVELOPMENT PLAN FLOW DATA (JR ENG. 2001).

APPENDIX B — HYDROLOGIC RESULTS — EXISTING 100—YR KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B-47





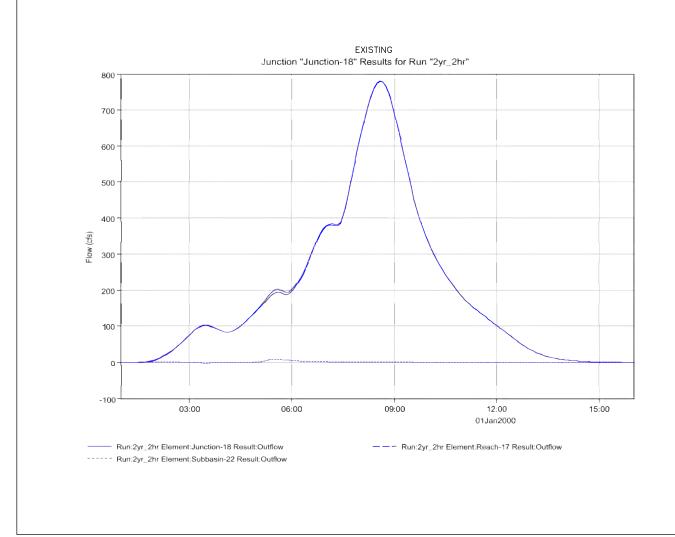


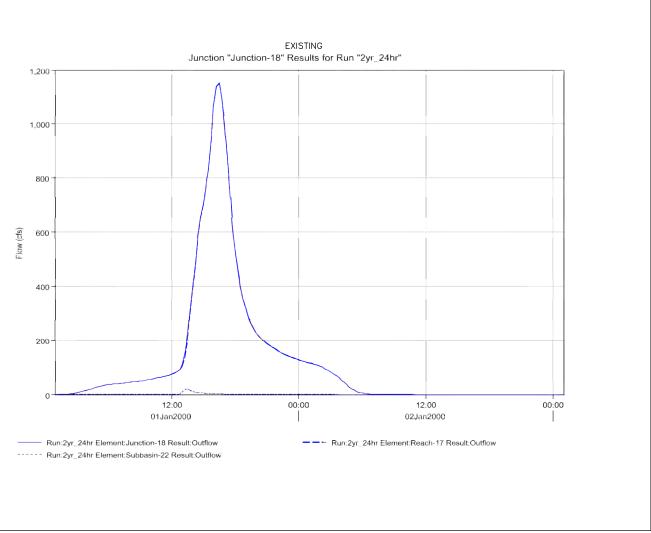
> JUNCTION 14 HOWELLS ROAD (APPROXIMATE)

EXISTING CONDITIONS HYDROGRAPHS
AT SELECT LOCATIONS
2-YEAR

APPENDIX B — HYDROLOGIC RESULTS — EXISTING HYDROGRAPHS 2—YR J—14 KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B—48





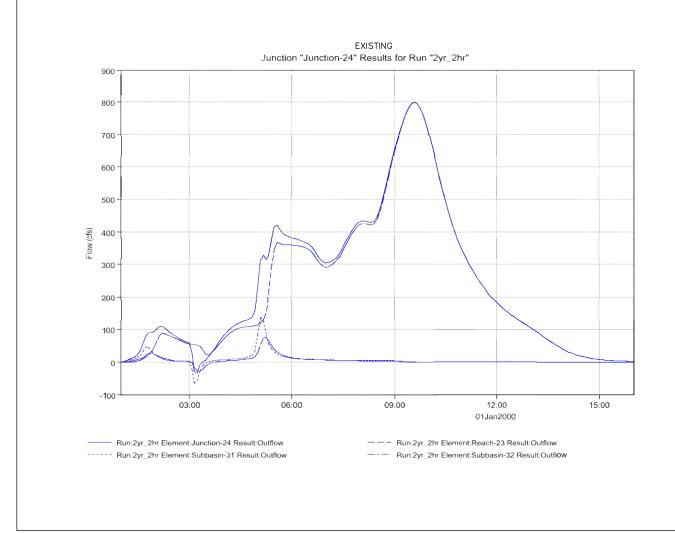


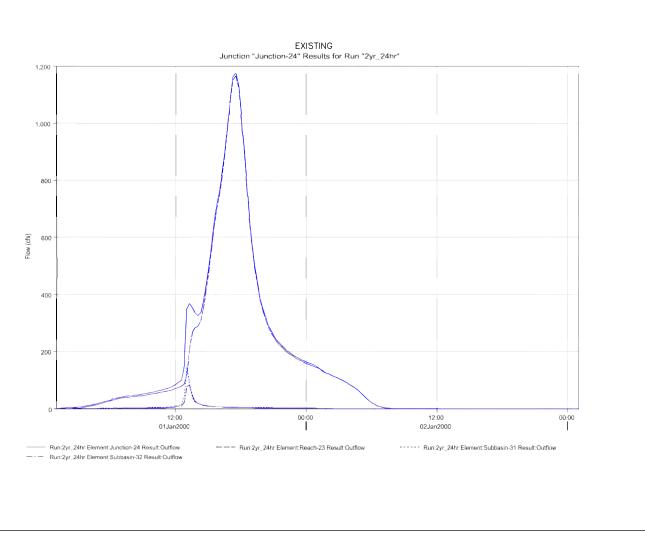
> JUNCTION 18 POWERS BLVD BRIDGE

EXISTING CONDITIONS HYDROGRAPHS
AT SELECT LOCATIONS
2-YEAR

APPENDIX B — HYDROLOGIC RESULTS — EXISTING HYDROGRAPHS 2—YR J—18 KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B—49





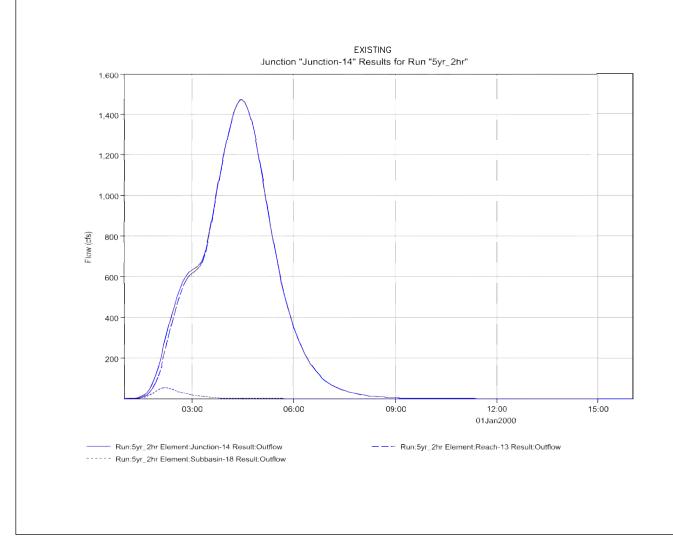


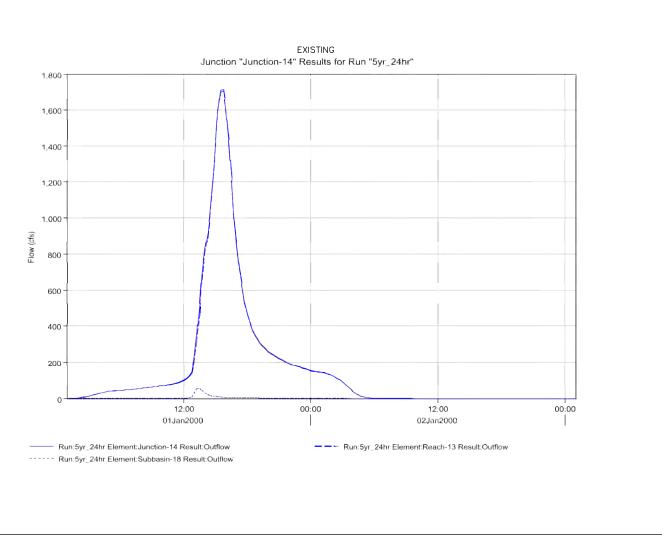
JUNCTION 24
HWY 83 BRIDGE

EXISTING CONDITIONS HYDROGRAPHS
AT SELECT LOCATIONS
2-YEAR

APPENDIX B — HYDROLOGIC RESULTS — EXISTING HYDROGRAPHS 2—YR J—24 KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B—50







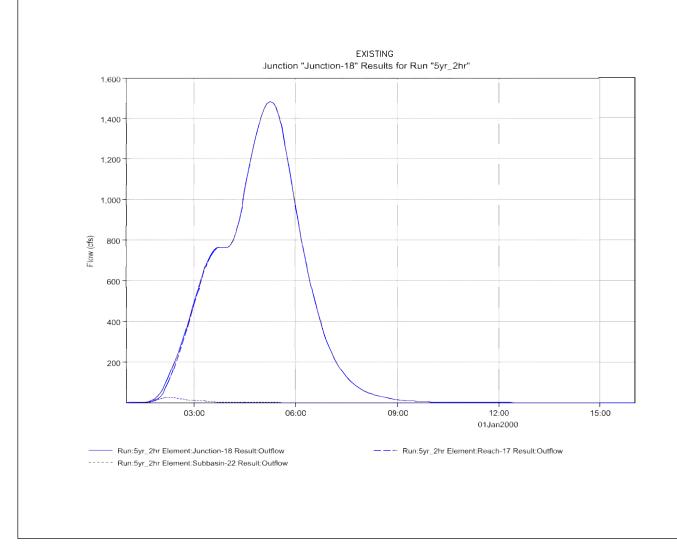
5–YR 2–HR 5–YR 24–HR

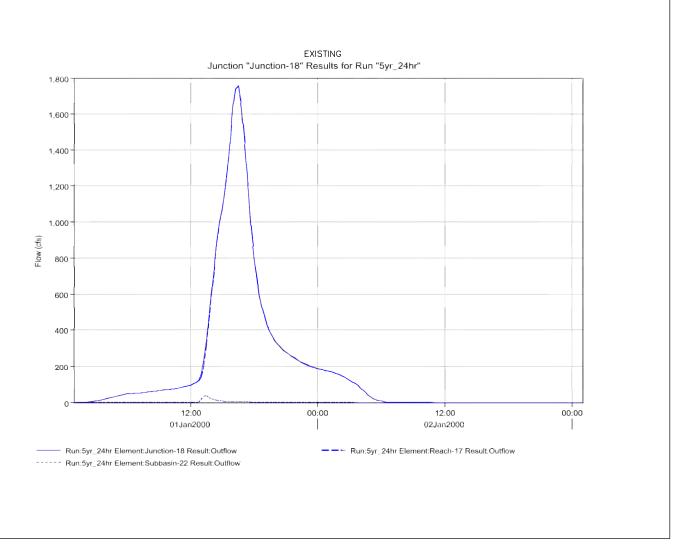
> JUNCTION 14 HOWELLS ROAD (APPROXIMATE)

EXISTING CONDITIONS HYDROGRAPHS
AT SELECT LOCATIONS
5-YEAR

APPENDIX B — HYDROLOGIC RESULTS — EXISTING HYDROGRAPHS 5—YR J—14 KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B—51







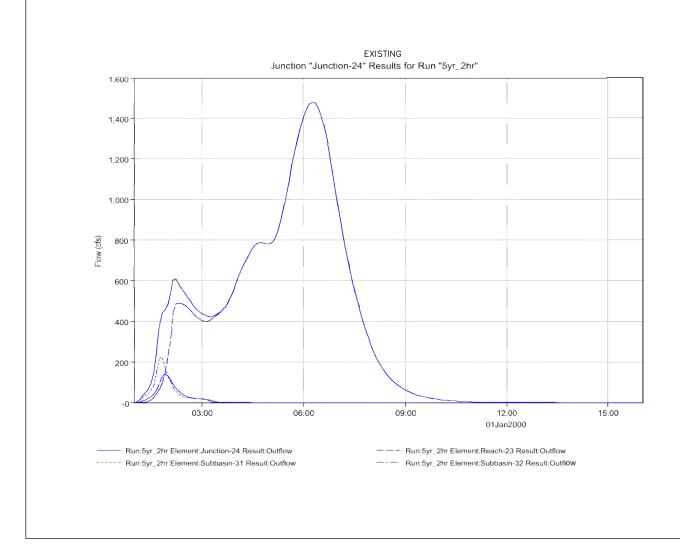
5–YR 2–HR 5–YR 24–HR

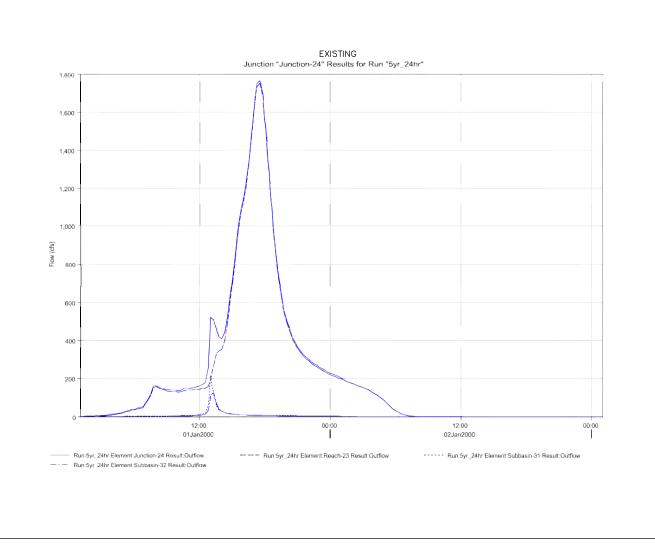
> JUNCTION 18 POWERS BLVD BRIDGE

EXISTING CONDITIONS HYDROGRAPHS
AT SELECT LOCATIONS
5-YEAR

APPENDIX B — HYDROLOGIC RESULTS — EXISTING HYDROGRAPHS 5—YR J—18 KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B—52







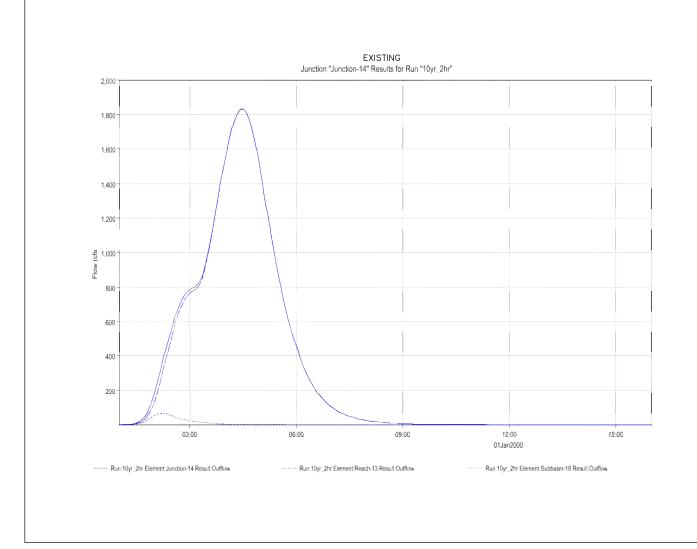
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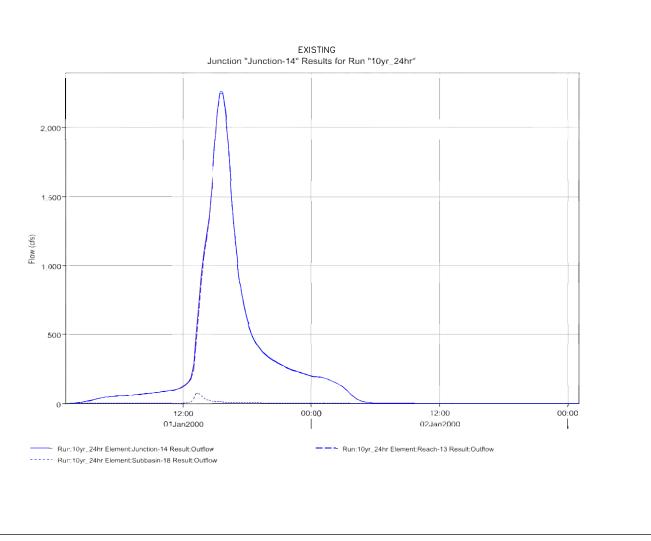
> JUNCTION 24 HWY 83 BRIDGE

EXISTING CONDITIONS HYDROGRAPHS
AT SELECT LOCATIONS
5-YEAR

APPENDIX B — HYDROLOGIC RESULTS — EXISTING HYDROGRAPHS 5—YR J—24 KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B—53





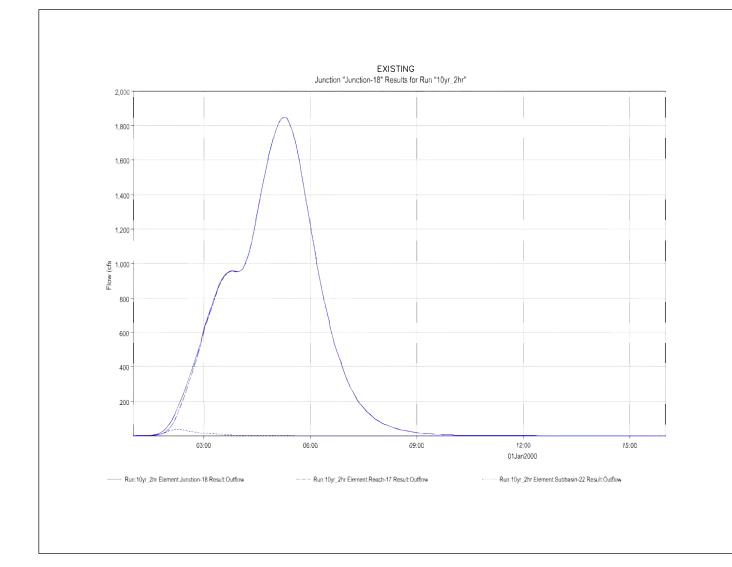


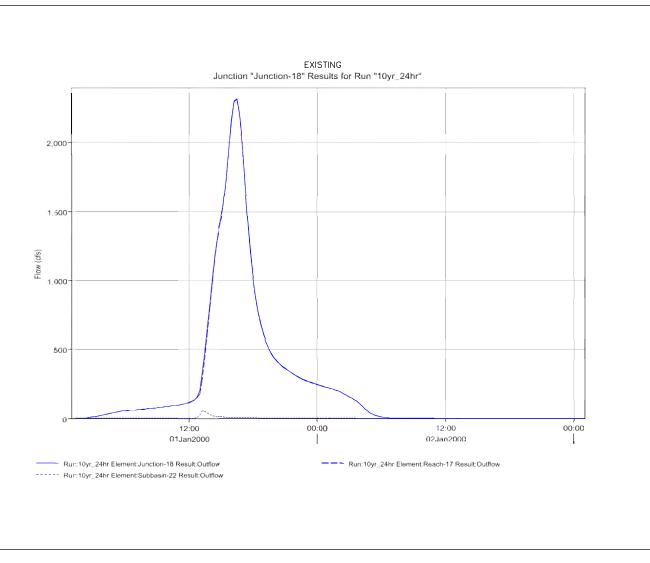
> JUNCTION 14 HOWELLS ROAD (APPROXIMATE)

EXISTING CONDITIONS HYDROGRAPHS
AT SELECT LOCATIONS
10-YEAR

APPENDIX B — HYDROLOGIC RESULTS— EXISTING HYDROGRAPHS 10—YR J—14 KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B—54





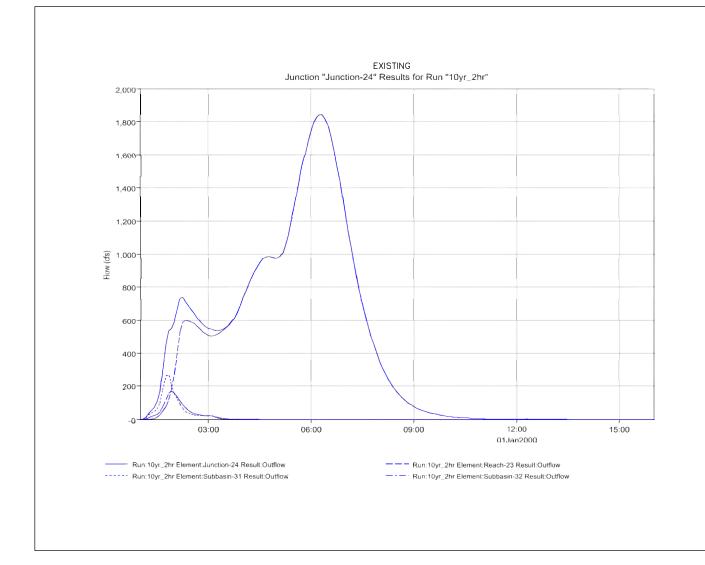


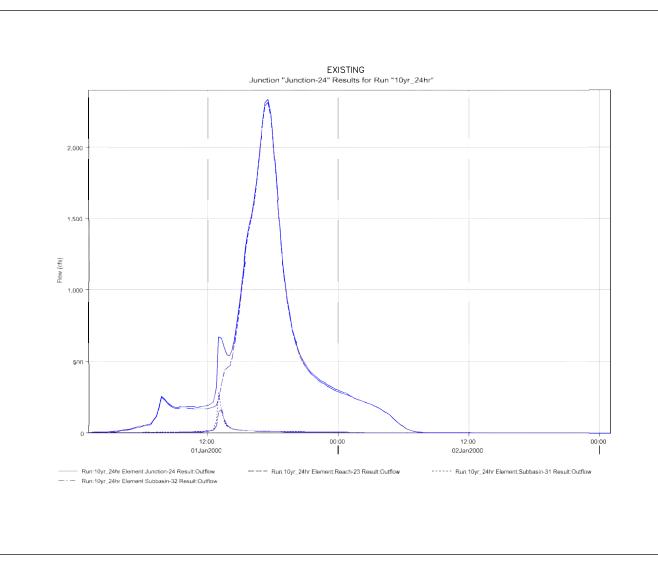
> JUNCTION 18 POWERS BLVD BRIDGE

EXISTING CONDITIONS HYDROGRAPHS
AT SELECT LOCATIONS
10-YEAR

APPENDIX B — HYDROLOGIC RESULTS— EXISTING HYDROGRAPHS 10—YR J—18 KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B—55





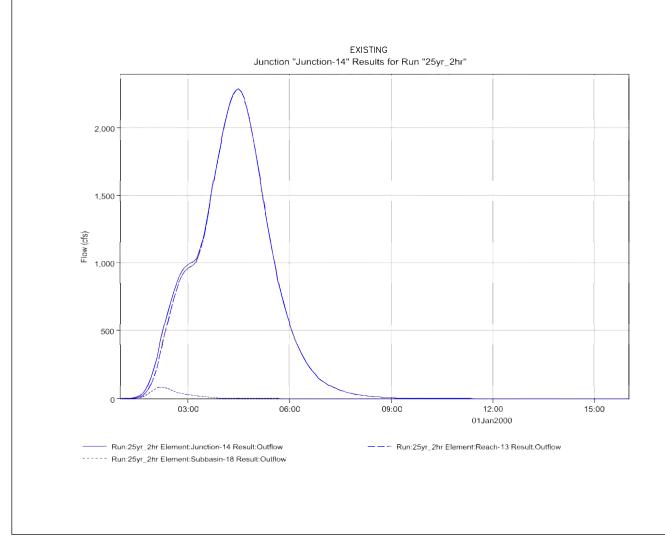


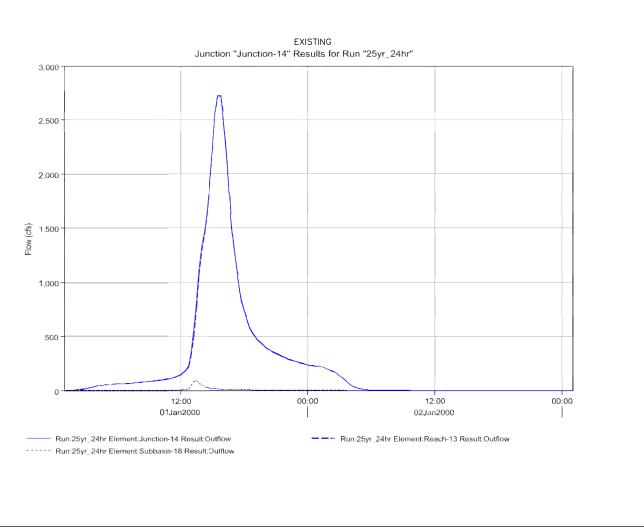
JUNCTION 24
HWY 83 BRIDGE

EXISTING CONDITIONS HYDROGRAPHS
AT SELECT LOCATIONS
10-YEAR

APPENDIX B — HYDROLOGIC RESULTS— EXISTING HYDROGRAPHS 10—YR J—24 KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B—56







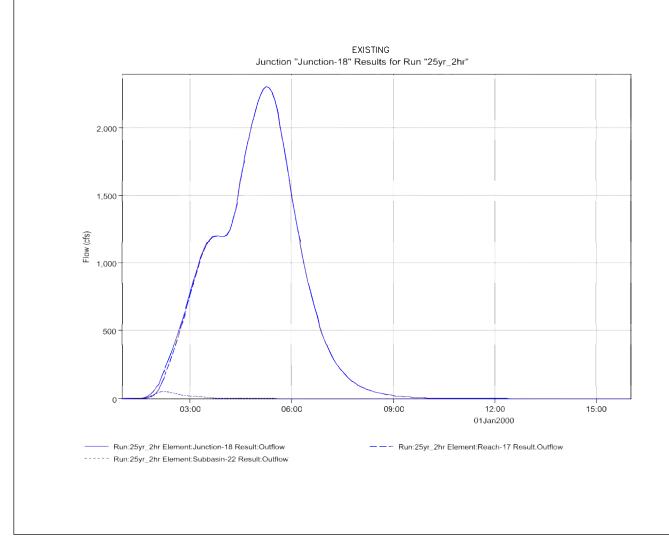
25-YR 2-HR 25-YR 24-HR

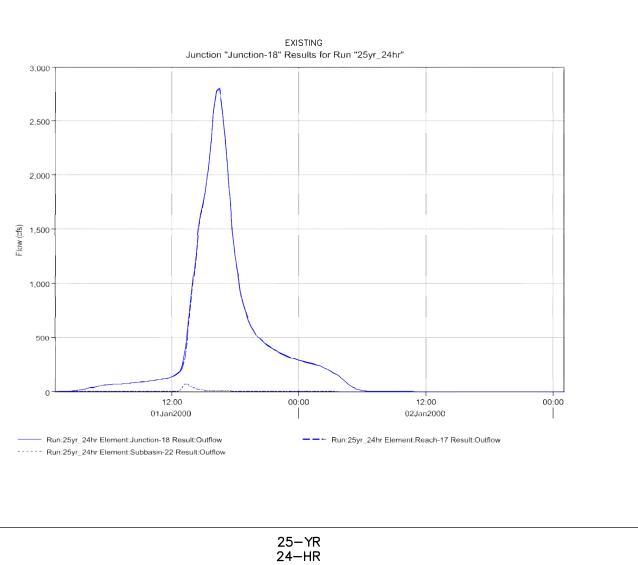
JUNCTION 14
HOWELLS ROAD (APPROXIMATE)

EXISTING CONDITIONS HYDROGRAPHS
AT SELECT LOCATIONS
25-YEAR

APPENDIX B — HYDROLOGIC RESULTS— EXISTING HYDROGRAPHS 25—YR J—14 KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B—57







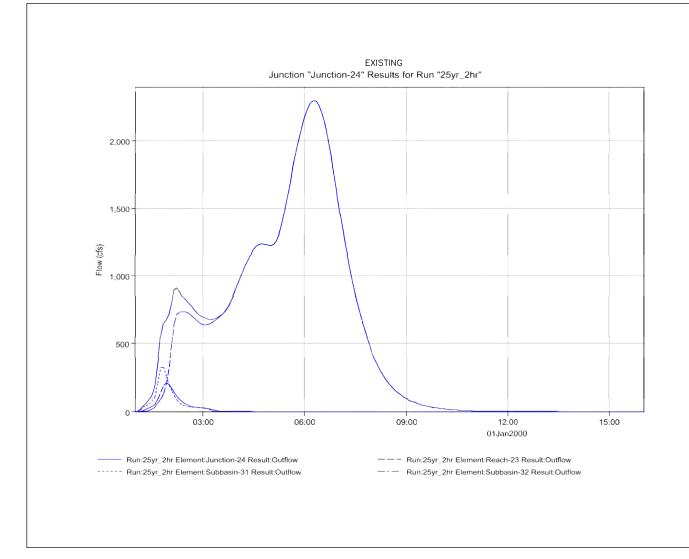
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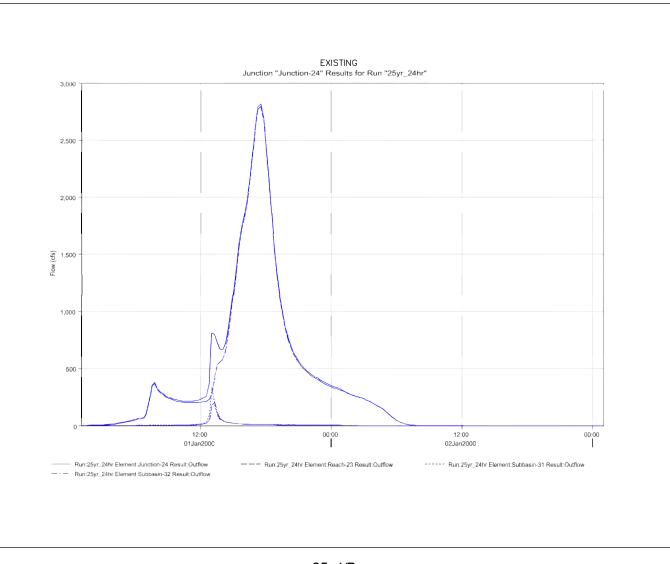
> JUNCTION 18 POWERS BLVD BRIDGE

EXISTING CONDITIONS HYDROGRAPHS
AT SELECT LOCATIONS
25-YEAR

APPENDIX B — HYDROLOGIC RESULTS— EXISTING HYDROGRAPHS 25—YR J—18 KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B—58







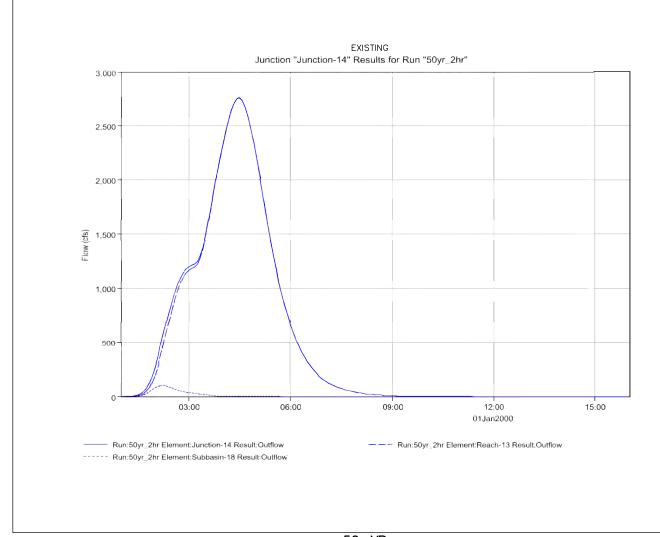
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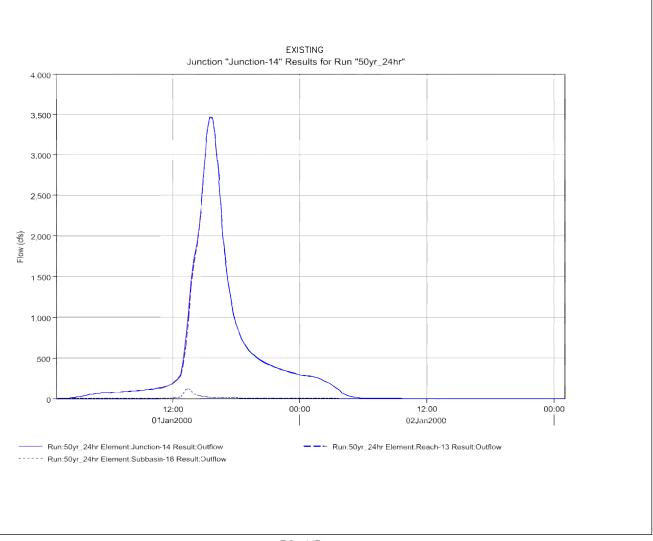
JUNCTION 24
HWY 83 BRIDGE

EXISTING CONDITIONS HYDROGRAPHS
AT SELECT LOCATIONS
25-YEAR

APPENDIX B — HYDROLOGIC RESULTS— EXISTING HYDROGRAPHS 25—YR J—24 KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B—59





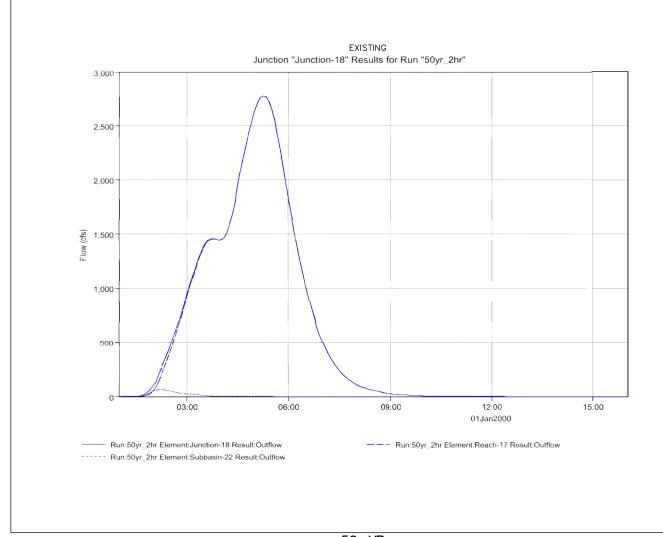


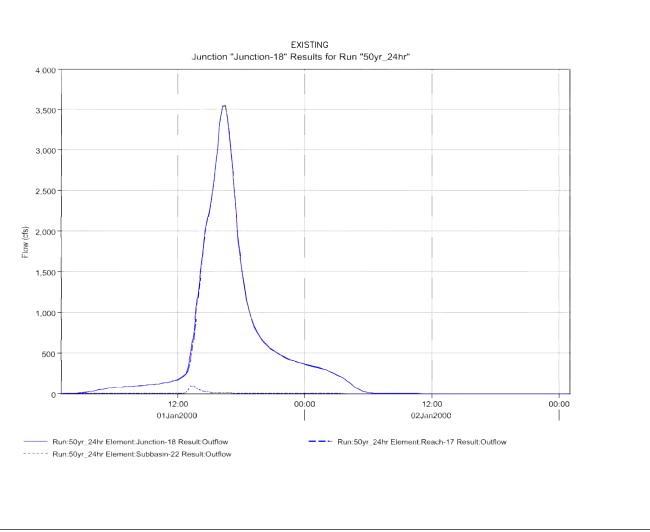
> JUNCTION 14 HOWELLS ROAD (APPROXIMATE)

EXISTING CONDITIONS HYDROGRAPHS
AT SELECT LOCATIONS
50-YEAR

APPENDIX B — HYDROLOGIC RESULTS— EXISTING HYDROGRAPHS 50—YR J—14 KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B—60





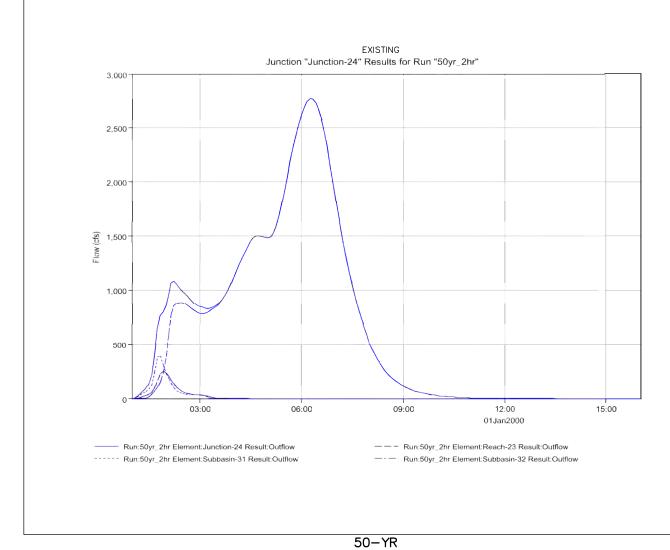


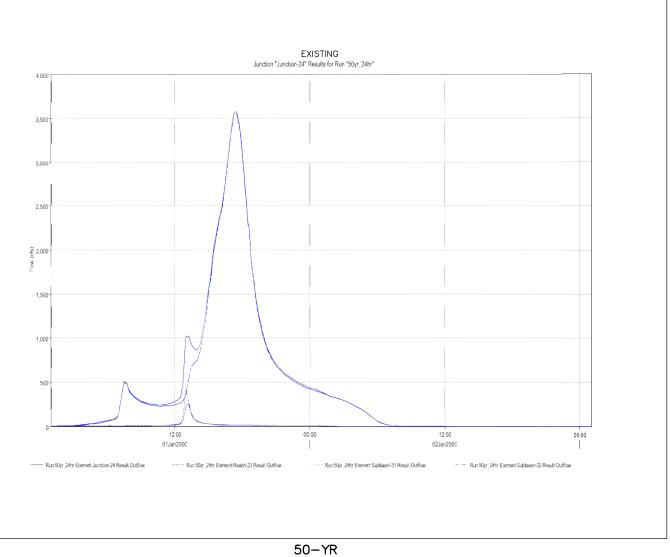
JUNCTION 18
POWERS BLVD BRIDGE

EXISTING CONDITIONS HYDROGRAPHS
AT SELECT LOCATIONS
50-YEAR

APPENDIX B — HYDROLOGIC RESULTS— EXISTING HYDROGRAPHS 50—YR J—18 KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B—61







24-HR

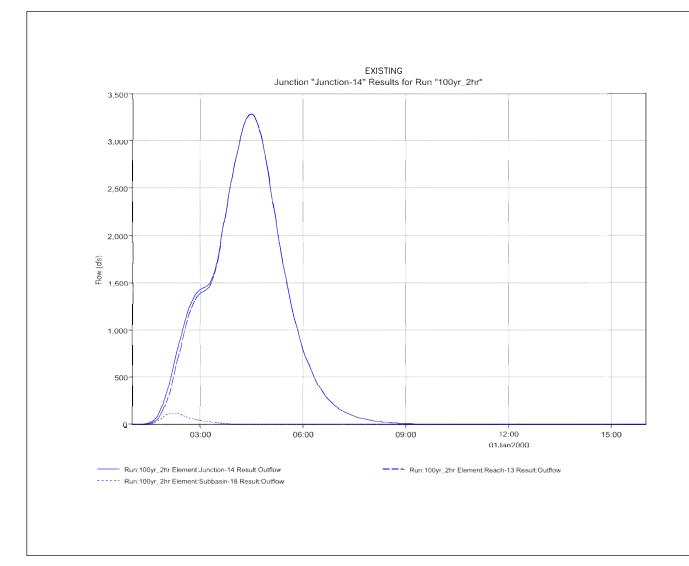
50—YR 2—HR

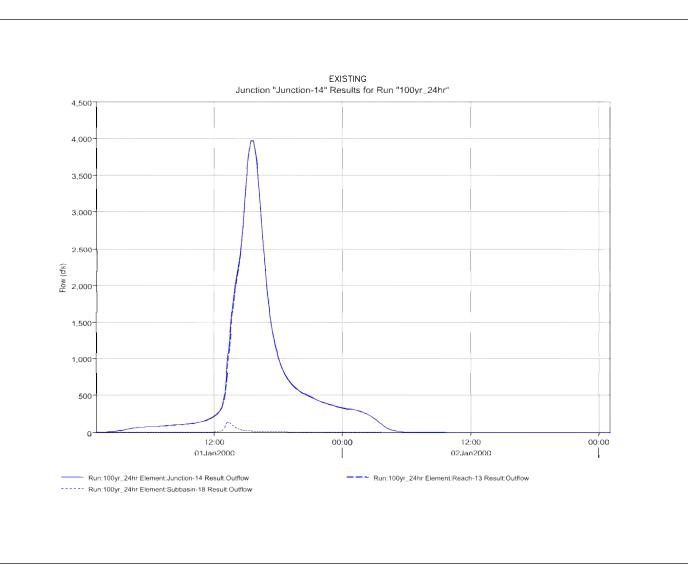
JUNCTION 24
HWY 83 BRIDGE

EXISTING CONDITIONS HYDROGRAPHS
AT SELECT LOCATIONS
50-YEAR

APPENDIX B — HYDROLOGIC RESULTS— EXISTING HYDROGRAPHS 50—YR J—28 KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B—62



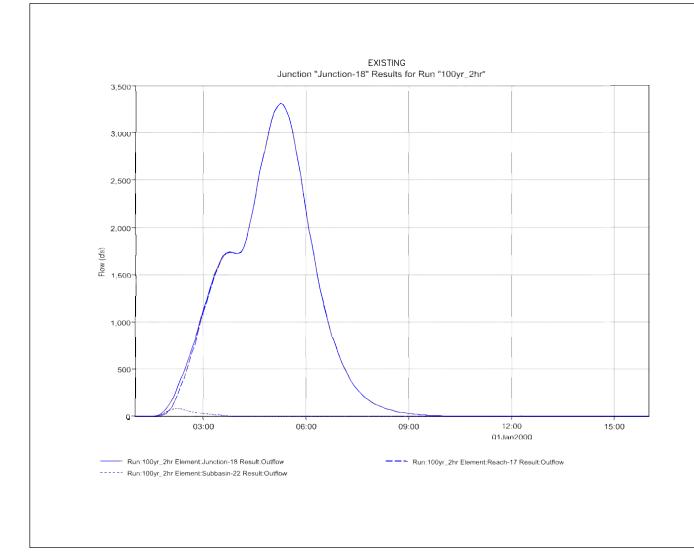


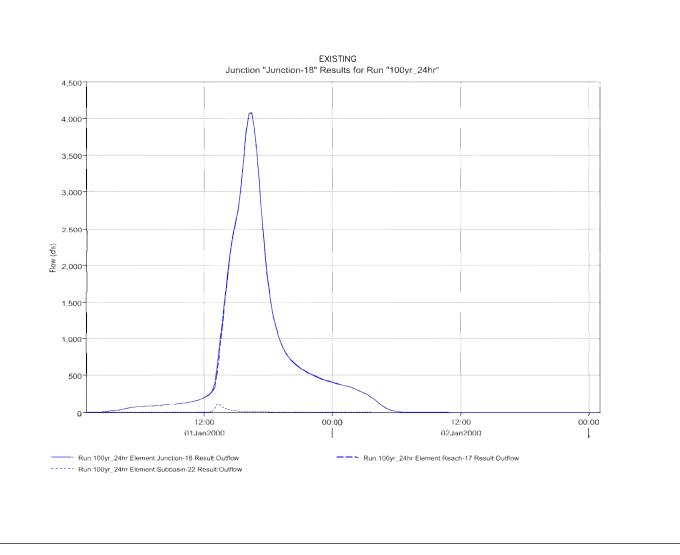


> JUNCTION 14 HOWELLS ROAD (APPROXIMATE)

EXISTING CONDITIONS HYDROGRAPHS AT SELECT LOCATIONS 100-YEAR APPENDIX B— HYDROLOGIC RESULTS— EXISTING HYDROGRAPHS 100—YR J—14 KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B—63



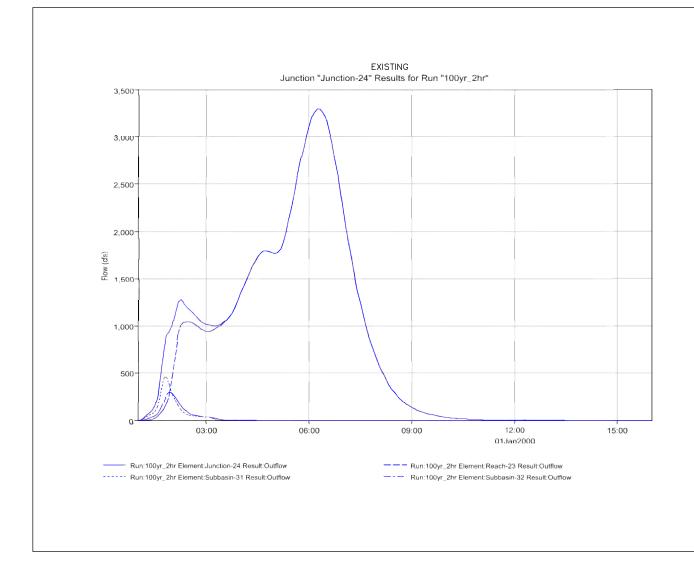


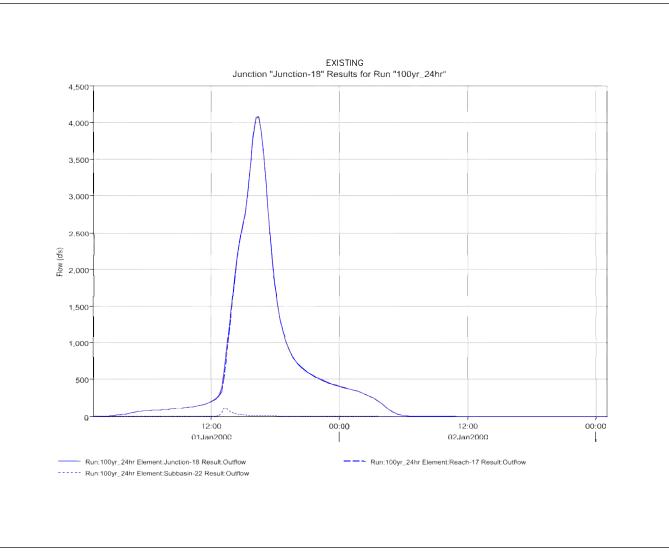


> JUNCTION 18 POWERS BLVD BRIDGE

EXISTING CONDITIONS HYDROGRAPHS AT SELECT LOCATIONS 100-YEAR APPENDIX B— HYDROLOGIC RESULTS— EXISTING HYDROGRAPHS 100—YR J—18 KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B—64







> JUNCTION 24 HWY 83 BRIDGE

EXISTING CONDITIONS HYDROGRAPHS AT SELECT LOCATIONS 100-YEAR APPENDIX B- HYDROLOGIC RESULTS- EXISTING HYDROGRAPHS 100-YR J-24 KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B-65



FUTURE CONDITIONS MODEL RESULTS (2-YEAR)

| 2-Year, 2-Hour Storm | | | |
|----------------------|------------|-----------|--------|
| | | Peak | |
| Hydrologic | Drainage | Discharge | Volume |
| Element | Area (mi²) | (CFS) | (in) |
| Subbasin-1 | 1.263 | 140 | 0.35 |
| Subbasin-2 | 0.586 | 79 | 0.36 |
| Subbasin-3 | 0.180 | 29 | 0.47 |
| Junction-1 | 2.029 | 242 | 0.36 |
| Reach-1 | 2.029 | 242 | 0.39 |
| Subbasin-4 | 0.195 | 24 | 0.31 |
| Junction-2 | 2.224 | 263 | 0.38 |
| Reach-2 | 2.224 | 263 | 0.38 |
| Subbasin-5 | 0.625 | 59 | 0.38 |
| Junction-3 | 2.849 | 316 | 0.38 |
| Reach-3 | 2.849 | 316 | 0.39 |
| Subbasin-6 | 1.333 | 96 | 0.29 |
| Junction-4 | 4.182 | 412 | 0.36 |
| Reach-4 | 4.182 | 410 | 0.36 |
| Subbasin-7 | 0.183 | 21 | 0.3 |
| Junction-5 | 4.365 | 420 | 0.36 |
| Reach-5 | 4.365 | 420 | 0.36 |
| Subbasin-8 | 0.288 | 51 | 0.35 |
| Junction-6 | 4.653 | 431 | 0.36 |
| Reach-6 | 4.653 | 430 | 0.36 |
| Subbasin-9 | 1.177 | 95 | 0.35 |
| Subbasin-10 | 0.222 | 26 | 0.29 |
| Junction-7 | 1.399 | 106 | 0.34 |
| Reach-7 | 1.399 | 106 | 0.35 |
| Subbasin-11 | 0.880 | 152 | 0.42 |
| Junction-8 | 2.279 | 215 | 0.38 |
| Reach-8 | 2.279 | 215 | 0.39 |
| Subbasin-12 | 0.552 | 61 | 0.34 |
| Junction-9 | 2.831 | 268 | 0.38 |
| Reach-9 | 2.831 | 268 | 0.38 |
| Junction-10 | 7.484 | 639 | 0.37 |
| Reach-10 | 7.484 | 638 | 0.37 |
| Subbasin-13 | 1.156 | 88 | 0.32 |
| Subbasin-14 | 0.516 | 58 | 0.3 |
| Junction-11 | 9.156 | 709 | 0.36 |
| Reach-11 | 9.156 | 708 | 0.36 |
| Subbasin-15 | 0.498 | 61 | 0.32 |
| Junction-12 | 9.654 | 719 | 0.35 |
| Reach-12 | 9.654 | 718 | 0.35 |
| Subbasin-16 | 0.819 | 86 | 0.36 |
| Subbasin-17 | 0.788 | 78 | 0.3 |
| Junction-13 | 11.261 | 754 | 0.35 |

| 2-Year, 2-Hour Storm | | | |
|-------------------------|------------|------------|--------|
| | | Peak | |
| Hydrologic | Drainage | Discharge | Volume |
| Element | Area (mi²) | (CFS) | (in) |
| Reach-13 | 11.261 | 754 | 0.35 |
| Subbasin-18 | 0.192 | 24 | 0.3 |
| Junction-14 | 11.453 | 756 | 0.35 |
| Reach-14 | 11.453 | 756 | 0.35 |
| Subbasin-19 | 0.552 | 47 | 0.34 |
| Junction-15 | 12.005 | 771 | 0.35 |
| Reach-15 | 12.005 | 770 | 0.35 |
| Subbasin-20 | 0.594 | 106 | 0.48 |
| Junction-16 | 12.599 | 782 | 0.35 |
| Reach-16 | 12.599 | 781 | 0.35 |
| Subbasin-21 | 0.417 | 47 | 0.27 |
| Junction-17 | 13.016 | 786 | 0.35 |
| Reach-17 | 13.016 | 785 | 0.35 |
| Subbasin-22 | 0.200 | 70 | 0.74 |
| Junction-18 | 13.216 | 790 | 0.36 |
| Reach-18 | 13.216 | 789 | 0.36 |
| Subbasin-23 | 0.123 | 14 | 0.15 |
| Junction-19 | 13.339 | 789 | 0.36 |
| Reach-19 | 13.339 | 788 | 0.36 |
| Subbasin-24 | 0.453 | 90 | 0.68 |
| Subbasin-25 | 0.169 | 131 | 0.85 |
| Subbasin-26 | 0.480 | 77 | 0.49 |
| Junction-21 | 1.102 | 179 | 0.62 |
| Reach-21 | 1.102 | 179 | 0.66 |
| Subbasin-27 | 0.294 | 88 | 0.65 |
| Junction-22 | 1.396 | 242 | 0.66 |
| Reach-22 | 1.396 | 242 | 0.67 |
| Subbasin-28 | 0.264 | 73 | 0.73 |
| Subbasin-29 | 0.172 | 74 | 0.73 |
| Junction-20 | 0.436 | 142 | 0.32 |
| Reach-20 | 0.436 | 142 | 0.89 |
| Subbasin-30 | 0.364 | 86 | 0.89 |
| Junction-23 | 15.535 | 823 | 0.3 |
| Reach-23 | 15.535 | | 0.4 |
| Subbasin-31 | 0.377 | 823 197 | 0.4 |
| Subbasin-32 | 0.377 | 225 | 0.99 |
| Junction-24 | 16.228 | 824 | 0.99 |
| | 16.228 | 823 | 0.42 |
| Reach-24 Subbasin-33 | 0.184 | 4 | 0.42 |
| | | | |
| Junction-25 | 16.412 | 822.7 | 0.41 |
| Reach-25 | 16.412 | 822.7 | 0.41 |
| Junction-26 | 16.412 | 822.7 | 0.41 |

| 2-Year, 24-Hour Storm | | | |
|-----------------------|------------|-----------|--------|
| | | Peak | |
| Hydrologic | Drainage | Discharge | Volume |
| Element | Area (mi²) | (CFS) | (in) |
| Subbasin-1 | 1.263 | 207 | 0.71 |
| Subbasin-2 | 0.586 | 114 | 0.72 |
| Subbasin-3 | 0.180 | 38 | 0.88 |
| Junction-1 | 2.029 | 348 | 0.73 |
| Reach-1 | 2.029 | 348 | 0.73 |
| Subbasin-4 | 0.195 | 36 | 0.64 |
| Junction-2 | 2.224 | 377 | 0.72 |
| Reach-2 | 2.224 | 373 | 0.72 |
| Subbasin-5 | 0.625 | 89 | 0.78 |
| Junction-3 | 2.849 | 453 | 0.74 |
| Reach-3 | 2.849 | 453 | 0.74 |
| Subbasin-6 | 1.333 | 152 | 0.62 |
| Junction-4 | 4.182 | 606 | 0.7 |
| Reach-4 | 4.182 | 600 | 0.7 |
| Subbasin-7 | 0.183 | 33 | 0.64 |
| Junction-5 | 4.365 | 615 | 0.7 |
| Reach-5 | 4.365 | 607 | 0.7 |
| Subbasin-8 | 0.288 | 76 | 0.74 |
| Junction-6 | 4.653 | 627 | 0.7 |
| Reach-6 | 4.653 | 617 | 0.7 |
| Subbasin-9 | 1.177 | 146 | 0.71 |
| Subbasin-10 | 0.222 | 39 | 0.61 |
| Junction-7 | 1.399 | 165 | 0.69 |
| Reach-7 | 1.399 | 164 | 0.69 |
| Subbasin-11 | 0.880 | 216 | 0.85 |
| Junction-8 | 2.279 | 321 | 0.75 |
| Reach-8 | 2.279 | 321 | 0.75 |
| Subbasin-12 | 0.552 | 93 | 0.71 |
| Junction-9 | 2.831 | 402 | 0.74 |
| Reach-9 | 2.831 | 393 | 0.74 |
| Junction-10 | 7.484 | 946 | 0.72 |
| Reach-10 | 7.484 | 937 | 0.72 |
| Subbasin-13 | 1.156 | 137 | 0.67 |
| Subbasin-14 | 0.516 | 88 | 0.63 |
| Junction-11 | 9.156 | 1,051 | 0.7 |
| Reach-11 | 9.156 | 1,051 | 0.7 |
| Subbasin-15 | 0.498 | 92 | 0.67 |
| Junction-12 | 9.654 | 1,072 | 0.7 |
| Reach-12 | 9.654 | 1,071 | 0.7 |

| 2-Year, 24-Hour Storm | | | |
|-----------------------|-------------------------|-----------|--------|
| | | Peak | |
| Hydrologic | Drainage | Discharge | Volume |
| Element | Area (mi ²) | (CFS) | (in) |
| Subbasin-16 | 0.819 | 127 | 0.72 |
| Subbasin-17 | 0.788 | 118 | 0.63 |
| Junction-13 | 11.261 | 1,134 | 0.7 |
| Reach-13 | 11.261 | 1,119 | 0.7 |
| Subbasin-18 | 0.192 | 35 | 0.63 |
| Junction-14 | 11.453 | 1,123 | 0.7 |
| Reach-14 | 11.453 | 1,121 | 0.7 |
| Subbasin-19 | 0.552 | 72 | 0.69 |
| Junction-15 | 12.005 | 1,146 | 0.7 |
| Reach-15 | 12.005 | 1,143 | 0.7 |
| Subbasin-20 | 0.594 | 142 | 0.9 |
| Junction-16 | 12.599 | 1,161 | 0.71 |
| Reach-16 | 12.599 | 1,149 | 0.71 |
| Subbasin-21 | 0.417 | 71 | 0.58 |
| Junction-17 | 13.016 | 1,157 | 0.7 |
| Reach-17 | 13.016 | 1,156 | 0.7 |
| Subbasin-22 | 0.200 | 81 | 1.29 |
| Junction-18 | 13.216 | 1,162 | 0.71 |
| Reach-18 | 13.216 | 1,156 | 0.71 |
| Subbasin-23 | 0.123 | 24 | 0.41 |
| Junction-19 | 13.339 | 1,157 | 0.71 |
| Reach-19 | 13.339 | 1,156 | 0.71 |
| Subbasin-28 | 0.264 | 89 | 1.27 |
| Subbasin-29 | 0.172 | 83 | 1.54 |
| Junction-20 | 0.436 | 169 | 1.38 |
| Reach-20 | 0.436 | 162 | 1.38 |
| Subbasin-30 | 0.364 | 109 | 0.95 |
| Source-1 | 1.396 | 87 | 0.33 |
| Junction-23 | 15.535 | 1,192 | 0.7 |
| Reach-23 | 15.535 | 1,183 | 0.7 |
| Subbasin-31 | 0.377 | 205 | 0.99 |
| Subbasin-32 | 0.316 | 205 | 1.66 |
| Junction-24 | 16.228 | 1,199 | 0.72 |
| Reach-24 | 16.228 | 1,192 | 0.72 |
| Subbasin-33 | 0.184 | 10 | 0.19 |
| Junction-25 | 16.412 | 1,193 | 0.72 |
| Reach-25 | 16.412 | 1,189 | 0.72 |
| Junction-26 | 16.412 | 1,189 | 0.72 |

NOTE:

1. SOURCE-1 IS THE 24 HOUR FLOW DATA FOR SUBBASINS 24-27, JUNCTION 22, AND REACHES 21-22. SUBBASINS 24-27 DATA HAS BEEN REPLACED WITH KETTLE CREEK DRAINAGE BASIN OLD RANCH ROAD TRIBUTARY MASTER DEVELOPMENT PLAN FLOW DATA (JR ENG. 2001).

APPENDIX B — HYDROLOGIC RESULTS — FUTURE 2—YR KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B-66



FUTURE CONDITIONS MODEL RESULTS (5-YEAR)

| 5-Year, 2-Hour Storm | | | |
|----------------------|-------------------------|-----------|--------|
| | | Peak | |
| Hydrologic | Drainage | Discharge | Volume |
| Element | Area (mi ²) | (CFS) | (in) |
| Subbasin-1 | 1.263 | 286 | 0.51 |
| Subbasin-2 | 0.586 | 160 | 0.52 |
| Subbasin-3 | 0.180 | 56 | 0.65 |
| Junction-1 | 2.029 | 492 | 0.52 |
| Reach-1 | 2.029 | 490 | 0.52 |
| Subbasin-4 | 0.195 | 50 | 0.45 |
| Junction-2 | 2.224 | 536 | 0.52 |
| Reach-2 | 2.224 | 536 | 0.52 |
| Subbasin-5 | 0.625 | 119 | 0.56 |
| Junction-3 | 2.849 | 644 | 0.53 |
| Reach-3 | 2.849 | 644 | 0.53 |
| Subbasin-6 | 1.333 | 203 | 0.43 |
| Junction-4 | 4.182 | 846 | 0.5 |
| Reach-4 | 4.182 | 846 | 0.5 |
| Subbasin-7 | 0.183 | 45 | 0.44 |
| Junction-5 | 4.365 | 865 | 0.49 |
| Reach-5 | 4.365 | 862 | 0.49 |
| Subbasin-8 | 0.288 | 104 | 0.52 |
| Junction-6 | 4.653 | 885 | 0.49 |
| Reach-6 | 4.653 | 883 | 0.49 |
| Subbasin-9 | 1.177 | 195 | 0.51 |
| Subbasin-10 | 0.222 | 55 | 0.43 |
| Junction-7 | 1.399 | 217 | 0.49 |
| Reach-7 | 1.399 | 217 | 0.49 |
| Subbasin-11 | 0.880 | 302 | 0.61 |
| Junction-8 | 2.279 | 437 | 0.54 |
| Reach-8 | 2.279 | 434 | 0.54 |
| Subbasin-12 | 0.552 | 127 | 0.5 |
| Junction-9 | 2.831 | 546 | 0.53 |
| Reach-9 | 2.831 | 545 | 0.53 |
| Junction-10 | 7.484 | 1,305 | 0.51 |
| Reach-10 | 7.484 | 1,305 | 0.51 |
| Subbasin-13 | 1.156 | 183 | 0.47 |
| Subbasin-14 | 0.516 | 122 | 0.44 |
| Junction-11 | 9.156 | 1,437 | 0.5 |
| Reach-11 | 9.156 | 1,435 | 0.5 |
| Subbasin-15 | 0.498 | 127 | 0.47 |
| Junction-12 | 9.654 | 1,445 | 0.5 |
| Reach-12 | 9.654 | 1,442 | 0.5 |
| Subbasin-16 | 0.819 | 175 | 0.51 |
| Subbasin-17 | 0.788 | 164 | 0.44 |
| Junction-13 | 11.261 | 1,475 | 0.49 |

| Hydrologic Element Drainage Area (mi²) (CFS) (in) Volume (in) Reach-13 11.261 1,473 0.49 Subbasin-18 0.192 50 0.44 Junction-14 11.453 1,473 0.49 Reach-14 11.453 1,473 0.49 Subbasin-19 0.552 98 0.49 Junction-15 12.005 1,490 0.49 Reach-15 12.005 1,487 0.49 Subbasin-20 0.594 205 0.67 Junction-16 12.599 1,489 0.5 Reach-16 12.599 1,489 0.5 Subbasin-21 0.417 100 0.4 Junction-17 13.016 1,488 0.5 Subbasin-22 0.200 128 0.99 Junction-18 13.216 1,488 0.51 Reach-18 13.216 1,487 0.5 Subbasin-23 0.123 31 0.26 Junction-19 13.339 1,487 </th <th colspan="4">5-Year, 2-Hour Storm</th> | 5-Year, 2-Hour Storm | | | |
|--|----------------------|------------|-----------|----------|
| Element Area (mi²) (CFS) (in) Reach-13 11.261 1,473 0.49 Subbasin-18 0.192 50 0.44 Junction-14 11.453 1,473 0.49 Reach-14 11.453 1,473 0.49 Subbasin-19 0.552 98 0.49 Junction-15 12.005 1,490 0.49 Reach-15 12.005 1,487 0.49 Subbasin-20 0.594 205 0.67 Junction-16 12.599 1,490 0.5 Reach-16 12.599 1,489 0.5 Subbasin-21 0.417 100 0.4 Junction-17 13.016 1,488 0.5 Subbasin-22 0.200 128 0.99 Junction-18 13.216 1,488 0.51 Reach-18 13.216 1,487 0.51 Subbasin-23 0.123 31 0.26 Junction-19 13.339 1,487 <t< td=""><td></td><td></td><td>Peak</td><td></td></t<> | | | Peak | |
| Element Area (mi²) (CFS) (in) Reach-13 11.261 1,473 0.49 Subbasin-18 0.192 50 0.44 Junction-14 11.453 1,473 0.49 Reach-14 11.453 1,473 0.49 Subbasin-19 0.552 98 0.49 Junction-15 12.005 1,490 0.49 Reach-15 12.005 1,487 0.49 Subbasin-20 0.594 205 0.67 Junction-16 12.599 1,489 0.5 Subbasin-21 0.417 100 0.4 Junction-17 13.016 1,488 0.5 Subbasin-22 0.200 128 0.99 Junction-18 13.216 1,487 0.51 Subbasin-23 0.123 31 0.26 Junction-19 13.339 1,487 0.5 Reach-19 13.339 1,485 0.5 Subbasin-24 0.453 170 <td< td=""><td>Hydrologic</td><td>Drainage</td><td>Discharge</td><td>Volume</td></td<> | Hydrologic | Drainage | Discharge | Volume |
| Reach-13 11.261 1,473 0.49 Subbasin-18 0.192 50 0.44 Junction-14 11.453 1,473 0.49 Reach-14 11.453 1,473 0.49 Subbasin-19 0.552 98 0.49 Junction-15 12.005 1,480 0.49 Reach-15 12.005 1,487 0.49 Subbasin-20 0.594 205 0.67 Junction-16 12.599 1,490 0.5 Reach-16 12.599 1,489 0.5 Subbasin-21 0.417 100 0.4 Junction-17 13.016 1,489 0.5 Subbasin-22 0.200 128 0.99 Junction-18 13.216 1,488 0.51 Reach-18 13.216 1,487 0.51 Subbasin-23 0.123 31 0.26 Junction-19 13.339 1,487 0.5 Subbasin-24 0.453 170 0. | , , | Area (mi²) | _ | (in) |
| Subbasin-18 0.192 50 0.44 Junction-14 11.453 1,473 0.49 Reach-14 11.453 1,473 0.49 Subbasin-19 0.552 98 0.49 Junction-15 12.005 1,490 0.49 Reach-15 12.005 1,487 0.49 Subbasin-20 0.594 205 0.67 Junction-16 12.599 1,490 0.5 Reach-16 12.599 1,489 0.5 Subbasin-21 0.417 100 0.4 Junction-17 13.016 1,489 0.5 Subbasin-22 0.200 128 0.99 Junction-18 13.216 1,488 0.51 Reach-18 13.216 1,487 0.51 Subbasin-23 0.123 31 0.26 Junction-19 13.339 1,487 0.5 Reach-19 13.339 1,485 0.5 Subbasin-24 0.453 170 0.9 | | | | <u> </u> |
| Junction-14 11.453 1,473 0.49 Reach-14 11.453 1,473 0.49 Subbasin-19 0.552 98 0.49 Junction-15 12.005 1,490 0.49 Reach-15 12.005 1,487 0.49 Subbasin-20 0.594 205 0.67 Junction-16 12.599 1,490 0.5 Reach-16 12.599 1,489 0.5 Subbasin-21 0.417 100 0.4 Junction-17 13.016 1,489 0.5 Reach-17 13.016 1,488 0.5 Subbasin-22 0.200 128 0.99 Junction-18 13.216 1,488 0.51 Reach-18 13.216 1,487 0.51 Subbasin-23 0.123 31 0.26 Junction-19 13.339 1,487 0.5 Subbasin-24 0.453 170 0.92 Subbasin-25 0.169 206 1. | | | , | |
| Reach-14 11.453 1,473 0.49 Subbasin-19 0.552 98 0.49 Junction-15 12.005 1,490 0.49 Reach-15 12.005 1,487 0.49 Subbasin-20 0.594 205 0.67 Junction-16 12.599 1,490 0.5 Reach-16 12.599 1,489 0.5 Subbasin-21 0.417 100 0.4 Junction-17 13.016 1,489 0.5 Reach-17 13.016 1,488 0.5 Subbasin-22 0.200 128 0.99 Junction-18 13.216 1,488 0.51 Reach-18 13.216 1,488 0.51 Subbasin-23 0.123 31 0.26 Junction-19 13.339 1,487 0.5 Subbasin-24 0.453 170 0.92 Subbasin-25 0.169 206 1.12 Subbasin-26 0.480 149 0.68< | | | | |
| Subbasin-19 0.552 98 0.49 Junction-15 12.005 1,490 0.49 Reach-15 12.005 1,487 0.49 Subbasin-20 0.594 205 0.67 Junction-16 12.599 1,490 0.5 Reach-16 12.599 1,489 0.5 Subbasin-21 0.417 100 0.4 Junction-17 13.016 1,489 0.5 Reach-17 13.016 1,488 0.5 Subbasin-22 0.200 128 0.99 Junction-18 13.216 1,488 0.51 Reach-18 13.216 1,487 0.51 Subbasin-23 0.123 31 0.26 Junction-19 13.339 1,487 0.5 Reach-19 13.339 1,487 0.5 Subbasin-24 0.453 170 0.92 Subbasin-25 0.169 206 1.12 Subbasin-26 0.480 149 0.68 </td <td></td> <td></td> <td></td> <td></td> | | | | |
| Junction-15 12.005 1,490 0.49 Reach-15 12.005 1,487 0.49 Subbasin-20 0.594 205 0.67 Junction-16 12.599 1,490 0.5 Reach-16 12.599 1,489 0.5 Subbasin-21 0.417 100 0.4 Junction-17 13.016 1,489 0.5 Reach-17 13.016 1,488 0.5 Subbasin-22 0.200 128 0.99 Junction-18 13.216 1,488 0.51 Reach-18 13.216 1,487 0.51 Subbasin-23 0.123 31 0.26 Junction-19 13.339 1,487 0.5 Subbasin-24 0.453 170 0.92 Subbasin-25 0.169 206 1.12 Subbasin-26 0.480 149 0.68 Junction-21 1.102 337 0.84 Subbasin-27 0.294 163 0.88 | | | , | |
| Reach-15 12.005 1,487 0.49 Subbasin-20 0.594 205 0.67 Junction-16 12.599 1,490 0.5 Reach-16 12.599 1,489 0.5 Subbasin-21 0.417 100 0.4 Junction-17 13.016 1,489 0.5 Reach-17 13.016 1,488 0.5 Subbasin-22 0.200 128 0.99 Junction-18 13.216 1,488 0.51 Reach-18 13.216 1,487 0.51 Subbasin-23 0.123 31 0.26 Junction-19 13.339 1,487 0.5 Reach-19 13.339 1,485 0.5 Subbasin-24 0.453 170 0.92 Subbasin-25 0.169 206 1.12 Subbasin-26 0.480 149 0.68 Junction-21 1.102 337 0.84 Reach-21 1.102 336 0.84 | | | | |
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| Reach-16 12.599 1,489 0.5 Subbasin-21 0.417 100 0.4 Junction-17 13.016 1,489 0.5 Reach-17 13.016 1,488 0.5 Subbasin-22 0.200 128 0.99 Junction-18 13.216 1,488 0.51 Reach-18 13.216 1,487 0.51 Subbasin-23 0.123 31 0.26 Junction-19 13.339 1,487 0.5 Reach-19 13.339 1,485 0.5 Subbasin-24 0.453 170 0.92 Subbasin-25 0.169 206 1.12 Subbasin-26 0.480 149 0.68 Junction-21 1.102 337 0.84 Reach-21 1.102 336 0.84 Subbasin-27 0.294 163 0.88 Junction-22 1.396 458 0.85 Subbasin-28 0.264 134 0.97 | | | | |
| Subbasin-21 0.417 100 0.4 Junction-17 13.016 1,489 0.5 Reach-17 13.016 1,488 0.5 Subbasin-22 0.200 128 0.99 Junction-18 13.216 1,488 0.51 Reach-18 13.216 1,487 0.51 Subbasin-23 0.123 31 0.26 Junction-19 13.339 1,487 0.5 Reach-19 13.339 1,485 0.5 Subbasin-24 0.453 170 0.92 Subbasin-25 0.169 206 1.12 Subbasin-26 0.480 149 0.68 Junction-21 1.102 337 0.84 Reach-21 1.102 336 0.84 Subbasin-27 0.294 163 0.88 Junction-22 1.396 458 0.85 Reach-22 1.396 458 0.85 Subbasin-28 0.264 134 0.97 < | | | | |
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| Reach-17 13.016 1,488 0.5 Subbasin-22 0.200 128 0.99 Junction-18 13.216 1,488 0.51 Reach-18 13.216 1,487 0.51 Subbasin-23 0.123 31 0.26 Junction-19 13.339 1,487 0.5 Reach-19 13.339 1,485 0.5 Subbasin-24 0.453 170 0.92 Subbasin-25 0.169 206 1.12 Subbasin-26 0.480 149 0.68 Junction-21 1.102 337 0.84 Reach-21 1.102 336 0.84 Subbasin-27 0.294 163 0.88 Junction-22 1.396 458 0.85 Subbasin-28 0.264 134 0.97 Subbasin-29 0.172 133 1.2 Junction-20 0.436 258 1.06 Reach-20 0.436 258 1.06 <td></td> <td></td> <td></td> <td></td> | | | | |
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| Junction-18 13.216 1,488 0.51 Reach-18 13.216 1,487 0.51 Subbasin-23 0.123 31 0.26 Junction-19 13.339 1,487 0.5 Reach-19 13.339 1,485 0.5 Subbasin-24 0.453 170 0.92 Subbasin-25 0.169 206 1.12 Subbasin-26 0.480 149 0.68 Junction-21 1.102 337 0.84 Reach-21 1.102 336 0.84 Subbasin-27 0.294 163 0.88 Junction-22 1.396 458 0.85 Reach-22 1.396 458 0.85 Subbasin-28 0.264 134 0.97 Subbasin-29 0.172 133 1.2 Junction-20 0.436 258 1.06 Reach-20 0.436 258 1.06 Subbasin-30 0.364 164 0.7 | | | , | |
| Reach-18 13.216 1,487 0.51 Subbasin-23 0.123 31 0.26 Junction-19 13.339 1,487 0.5 Reach-19 13.339 1,485 0.5 Subbasin-24 0.453 170 0.92 Subbasin-25 0.169 206 1.12 Subbasin-26 0.480 149 0.68 Junction-21 1.102 337 0.84 Reach-21 1.102 336 0.84 Subbasin-27 0.294 163 0.88 Junction-22 1.396 458 0.85 Reach-22 1.396 458 0.85 Subbasin-28 0.264 134 0.97 Subbasin-29 0.172 133 1.2 Junction-20 0.436 258 1.06 Reach-20 0.436 258 1.06 Subbasin-30 0.364 164 0.7 Junction-23 15.535 1,486 0.56 | | | | |
| Subbasin-23 0.123 31 0.26 Junction-19 13.339 1,487 0.5 Reach-19 13.339 1,485 0.5 Subbasin-24 0.453 170 0.92 Subbasin-25 0.169 206 1.12 Subbasin-26 0.480 149 0.68 Junction-21 1.102 337 0.84 Reach-21 1.102 336 0.84 Subbasin-27 0.294 163 0.88 Junction-22 1.396 458 0.85 Reach-22 1.396 458 0.85 Subbasin-28 0.264 134 0.97 Subbasin-29 0.172 133 1.2 Junction-20 0.436 258 1.06 Reach-20 0.436 258 1.06 Subbasin-30 0.364 164 0.7 Junction-23 15.535 1,487 0.56 Subbasin-31 0.377 309 0.75 | | | | |
| Junction-19 13.339 1,487 0.5 Reach-19 13.339 1,485 0.5 Subbasin-24 0.453 170 0.92 Subbasin-25 0.169 206 1.12 Subbasin-26 0.480 149 0.68 Junction-21 1.102 337 0.84 Reach-21 1.102 336 0.84 Subbasin-27 0.294 163 0.88 Junction-22 1.396 458 0.85 Reach-21 1.396 458 0.85 Reach-22 1.396 458 0.85 Subbasin-28 0.264 134 0.97 Subbasin-29 0.172 133 1.2 Junction-20 0.436 258 1.06 Reach-20 0.436 258 1.06 Subbasin-30 0.364 164 0.7 Junction-23 15.535 1,487 0.56 Subbasin-31 0.377 309 0.75 | | | , | |
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| Subbasin-25 0.169 206 1.12 Subbasin-26 0.480 149 0.68 Junction-21 1.102 337 0.84 Reach-21 1.102 336 0.84 Subbasin-27 0.294 163 0.88 Junction-22 1.396 458 0.85 Reach-22 1.396 458 0.85 Subbasin-28 0.264 134 0.97 Subbasin-29 0.172 133 1.2 Junction-20 0.436 258 1.06 Reach-20 0.436 258 1.06 Subbasin-30 0.364 164 0.7 Junction-23 15.535 1,487 0.56 Subbasin-31 0.377 309 0.75 Subbasin-32 0.316 377 1.3 Junction-24 16.228 1,486 0.57 Reach-24 16.228 1,485 0.57 Subbasin-33 0.184 13 0.1 | | | , | |
| Subbasin-26 0.480 149 0.68 Junction-21 1.102 337 0.84 Reach-21 1.102 336 0.84 Subbasin-27 0.294 163 0.88 Junction-22 1.396 458 0.85 Reach-22 1.396 458 0.85 Subbasin-28 0.264 134 0.97 Subbasin-29 0.172 133 1.2 Junction-20 0.436 258 1.06 Reach-20 0.436 258 1.06 Subbasin-30 0.364 164 0.7 Junction-23 15.535 1,487 0.56 Subbasin-31 0.377 309 0.75 Subbasin-32 0.316 377 1.3 Junction-24 16.228 1,486 0.57 Reach-24 16.228 1,485 0.57 Subbasin-33 0.184 13 0.1 Junction-25 16.412 1484.7 0.57 </td <td></td> <td></td> <td></td> <td></td> | | | | |
| Junction-21 1.102 337 0.84 Reach-21 1.102 336 0.84 Subbasin-27 0.294 163 0.88 Junction-22 1.396 458 0.85 Reach-22 1.396 458 0.85 Subbasin-28 0.264 134 0.97 Subbasin-29 0.172 133 1.2 Junction-20 0.436 258 1.06 Reach-20 0.436 258 1.06 Subbasin-30 0.364 164 0.7 Junction-23 15.535 1,487 0.56 Subbasin-31 0.377 309 0.75 Subbasin-32 0.316 377 1.3 Junction-24 16.228 1,486 0.57 Reach-24 16.228 1,485 0.57 Subbasin-33 0.184 13 0.1 Junction-25 16.412 1484.7 0.57 Reach-25 16.412 1484.7 0.57 < | | | | |
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| Subbasin-27 0.294 163 0.88 Junction-22 1.396 458 0.85 Reach-22 1.396 458 0.85 Subbasin-28 0.264 134 0.97 Subbasin-29 0.172 133 1.2 Junction-20 0.436 258 1.06 Reach-20 0.436 258 1.06 Subbasin-30 0.364 164 0.7 Junction-23 15.535 1,487 0.56 Reach-23 15.535 1,486 0.56 Subbasin-31 0.377 309 0.75 Subbasin-32 0.316 377 1.3 Junction-24 16.228 1,486 0.57 Reach-24 16.228 1,485 0.57 Subbasin-33 0.184 13 0.1 Junction-25 16.412 1484.7 0.57 Reach-25 16.412 1484.7 0.57 | Junction-21 | | 337 | 0.84 |
| Junction-22 1.396 458 0.85 Reach-22 1.396 458 0.85 Subbasin-28 0.264 134 0.97 Subbasin-29 0.172 133 1.2 Junction-20 0.436 258 1.06 Reach-20 0.436 258 1.06 Subbasin-30 0.364 164 0.7 Junction-23 15.535 1,487 0.56 Reach-23 15.535 1,486 0.56 Subbasin-31 0.377 309 0.75 Subbasin-32 0.316 377 1.3 Junction-24 16.228 1,486 0.57 Reach-24 16.228 1,485 0.57 Subbasin-33 0.184 13 0.1 Junction-25 16.412 1484.7 0.57 Reach-25 16.412 1484.7 0.57 | | | 336 | 0.84 |
| Reach-22 1.396 458 0.85 Subbasin-28 0.264 134 0.97 Subbasin-29 0.172 133 1.2 Junction-20 0.436 258 1.06 Reach-20 0.436 258 1.06 Subbasin-30 0.364 164 0.7 Junction-23 15.535 1,487 0.56 Reach-23 15.535 1,486 0.56 Subbasin-31 0.377 309 0.75 Subbasin-32 0.316 377 1.3 Junction-24 16.228 1,486 0.57 Reach-24 16.228 1,485 0.57 Subbasin-33 0.184 13 0.1 Junction-25 16.412 1484.7 0.57 Reach-25 16.412 1484.7 0.57 | Subbasin-27 | 0.294 | 163 | 0.88 |
| Subbasin-28 0.264 134 0.97 Subbasin-29 0.172 133 1.2 Junction-20 0.436 258 1.06 Reach-20 0.436 258 1.06 Subbasin-30 0.364 164 0.7 Junction-23 15.535 1,487 0.56 Reach-23 15.535 1,486 0.56 Subbasin-31 0.377 309 0.75 Subbasin-32 0.316 377 1.3 Junction-24 16.228 1,486 0.57 Reach-24 16.228 1,485 0.57 Subbasin-33 0.184 13 0.1 Junction-25 16.412 1484.7 0.57 Reach-25 16.412 1484.7 0.57 | Junction-22 | 1.396 | 458 | 0.85 |
| Subbasin-29 0.172 133 1.2 Junction-20 0.436 258 1.06 Reach-20 0.436 258 1.06 Subbasin-30 0.364 164 0.7 Junction-23 15.535 1,487 0.56 Reach-23 15.535 1,486 0.56 Subbasin-31 0.377 309 0.75 Subbasin-32 0.316 377 1.3 Junction-24 16.228 1,486 0.57 Reach-24 16.228 1,485 0.57 Subbasin-33 0.184 13 0.1 Junction-25 16.412 1484.7 0.57 Reach-25 16.412 1484.7 0.57 | Reach-22 | 1.396 | 458 | 0.85 |
| Junction-20 0.436 258 1.06 Reach-20 0.436 258 1.06 Subbasin-30 0.364 164 0.7 Junction-23 15.535 1,487 0.56 Reach-23 15.535 1,486 0.56 Subbasin-31 0.377 309 0.75 Subbasin-32 0.316 377 1.3 Junction-24 16.228 1,486 0.57 Reach-24 16.228 1,485 0.57 Subbasin-33 0.184 13 0.1 Junction-25 16.412 1484.7 0.57 Reach-25 16.412 1484.7 0.57 | Subbasin-28 | 0.264 | 134 | 0.97 |
| Reach-20 0.436 258 1.06 Subbasin-30 0.364 164 0.7 Junction-23 15.535 1,487 0.56 Reach-23 15.535 1,486 0.56 Subbasin-31 0.377 309 0.75 Subbasin-32 0.316 377 1.3 Junction-24 16.228 1,486 0.57 Reach-24 16.228 1,485 0.57 Subbasin-33 0.184 13 0.1 Junction-25 16.412 1484.7 0.57 Reach-25 16.412 1484.7 0.57 | Subbasin-29 | 0.172 | 133 | 1.2 |
| Subbasin-30 0.364 164 0.7 Junction-23 15.535 1,487 0.56 Reach-23 15.535 1,486 0.56 Subbasin-31 0.377 309 0.75 Subbasin-32 0.316 377 1.3 Junction-24 16.228 1,486 0.57 Reach-24 16.228 1,485 0.57 Subbasin-33 0.184 13 0.1 Junction-25 16.412 1484.7 0.57 Reach-25 16.412 1484.7 0.57 | Junction-20 | 0.436 | 258 | 1.06 |
| Junction-23 15.535 1,487 0.56 Reach-23 15.535 1,486 0.56 Subbasin-31 0.377 309 0.75 Subbasin-32 0.316 377 1.3 Junction-24 16.228 1,486 0.57 Reach-24 16.228 1,485 0.57 Subbasin-33 0.184 13 0.1 Junction-25 16.412 1484.7 0.57 Reach-25 16.412 1484.7 0.57 | Reach-20 | 0.436 | 258 | 1.06 |
| Reach-23 15.535 1,486 0.56 Subbasin-31 0.377 309 0.75 Subbasin-32 0.316 377 1.3 Junction-24 16.228 1,486 0.57 Reach-24 16.228 1,485 0.57 Subbasin-33 0.184 13 0.1 Junction-25 16.412 1484.7 0.57 Reach-25 16.412 1484.7 0.57 | Subbasin-30 | 0.364 | 164 | 0.7 |
| Subbasin-31 0.377 309 0.75 Subbasin-32 0.316 377 1.3 Junction-24 16.228 1,486 0.57 Reach-24 16.228 1,485 0.57 Subbasin-33 0.184 13 0.1 Junction-25 16.412 1484.7 0.57 Reach-25 16.412 1484.7 0.57 | Junction-23 | 15.535 | 1,487 | 0.56 |
| Subbasin-31 0.377 309 0.75 Subbasin-32 0.316 377 1.3 Junction-24 16.228 1,486 0.57 Reach-24 16.228 1,485 0.57 Subbasin-33 0.184 13 0.1 Junction-25 16.412 1484.7 0.57 Reach-25 16.412 1484.7 0.57 | Reach-23 | 15.535 | 1,486 | 0.56 |
| Junction-24 16.228 1,486 0.57 Reach-24 16.228 1,485 0.57 Subbasin-33 0.184 13 0.1 Junction-25 16.412 1484.7 0.57 Reach-25 16.412 1484.7 0.57 | Subbasin-31 | 0.377 | 309 | |
| Junction-24 16.228 1,486 0.57 Reach-24 16.228 1,485 0.57 Subbasin-33 0.184 13 0.1 Junction-25 16.412 1484.7 0.57 Reach-25 16.412 1484.7 0.57 | Subbasin-32 | 0.316 | 377 | 1.3 |
| Reach-24 16.228 1,485 0.57 Subbasin-33 0.184 13 0.1 Junction-25 16.412 1484.7 0.57 Reach-25 16.412 1484.7 0.57 | Junction-24 | | 1,486 | 0.57 |
| Subbasin-33 0.184 13 0.1 Junction-25 16.412 1484.7 0.57 Reach-25 16.412 1484.7 0.57 | Reach-24 | 16.228 | 1,485 | |
| Junction-25 16.412 1484.7 0.57 Reach-25 16.412 1484.7 0.57 | | | , | |
| Reach-25 16.412 1484.7 0.57 | Junction-25 | 16.412 | 1484.7 | 0.57 |
| | Reach-25 | 16.412 | | |
| Junction-26 16.412 1484.7 0.57 | | | | |

| 5 | -Year, 24-Ho | ur Storm | |
|-------------|--------------|-----------|--------|
| | | Peak | |
| Hydrologic | Drainage | Discharge | Volume |
| Element | Area (mi²) | (CFS) | (in) |
| Subbasin-1 | 1.263 | 315 | 1.06 |
| Subbasin-2 | 0.586 | 173 | 1.06 |
| Subbasin-3 | 0.180 | 56 | 1.27 |
| Junction-1 | 2.029 | 527 | 1.08 |
| Reach-1 | 2.029 | 526 | 1.08 |
| Subbasin-4 | 0.195 | 56 | 0.97 |
| Junction-2 | 2.224 | 572 | 1.07 |
| Reach-2 | 2.224 | 568 | 1.07 |
| Subbasin-5 | 0.625 | 134 | 1.14 |
| Junction-3 | 2.849 | 689 | 1.08 |
| Reach-3 | 2.849 | 689 | 1.08 |
| Subbasin-6 | 1.333 | 240 | 0.94 |
| Junction-4 | 4.182 | 928 | 1.04 |
| Reach-4 | 4.182 | 917 | 1.04 |
| Subbasin-7 | 0.183 | 51 | 0.97 |
| Junction-5 | 4.365 | 940 | 1.03 |
| Reach-5 | 4.365 | 929 | 1.03 |
| Subbasin-8 | 0.288 | 117 | 1.1 |
| Junction-6 | 4.653 | 959 | 1.04 |
| Reach-6 | 4.653 | 944 | 1.04 |
| Subbasin-9 | 1.177 | 223 | 1.05 |
| Subbasin-10 | 0.222 | 62 | 0.93 |
| Junction-7 | 1.399 | 252 | 1.03 |
| Reach-7 | 1.399 | 250 | 1.03 |
| Subbasin-11 | 0.880 | 322 | 1.23 |
| Junction-8 | 2.279 | 484 | 1.11 |
| Reach-8 | 2.279 | 484 | 1.11 |
| Subbasin-12 | 0.552 | 144 | 1.06 |
| Junction-9 | 2.831 | 609 | 1.1 |
| Reach-9 | 2.831 | 594 | 1.1 |
| Junction-10 | 7.484 | 1,444 | 1.06 |
| Reach-10 | 7.484 | 1,428 | 1.06 |
| Subbasin-13 | 1.156 | 212 | 1 |
| Subbasin-14 | 0.516 | 138 | 0.95 |
| Junction-11 | 9.156 | 1,605 | 1.05 |
| Reach-11 | 9.156 | 1,604 | 1.05 |
| Subbasin-15 | 0.498 | 143 | 1 |
| Junction-12 | 9.654 | 1,636 | 1.05 |
| Reach-12 | 9.654 | 1,634 | 1.05 |

| 5-Year, 24-Hour Storm | | | |
|-----------------------|-------------------------|-----------|--------|
| | | Peak | |
| Hydrologic | Drainage | Discharge | Volume |
| Element | Area (mi ²) | (CFS) | (in) |
| Subbasin-16 | 0.819 | 193 | 1.06 |
| Subbasin-17 | 0.788 | 184 | 0.95 |
| Junction-13 | 11.261 | 1,730 | 1.04 |
| Reach-13 | 11.261 | 1,705 | 1.04 |
| Subbasin-18 | 0.192 | 55 | 0.95 |
| Junction-14 | 11.453 | 1,711 | 1.04 |
| Reach-14 | 11.453 | 1,710 | 1.04 |
| Subbasin-19 | 0.552 | 111 | 1.03 |
| Junction-15 | 12.005 | 1,747 | 1.04 |
| Reach-15 | 12.005 | 1,743 | 1.04 |
| Subbasin-20 | 0.594 | 206 | 1.29 |
| Junction-16 | 12.599 | 1,769 | 1.05 |
| Reach-16 | 12.599 | 1,750 | 1.05 |
| Subbasin-21 | 0.417 | 114 | 0.9 |
| Junction-17 | 13.016 | 1,761 | 1.04 |
| Reach-17 | 13.016 | 1,761 | 1.04 |
| Subbasin-22 | 0.200 | 112 | 1.76 |
| Junction-18 | 13.216 | 1,769 | 1.06 |
| Reach-18 | 13.216 | 1,760 | 1.06 |
| Subbasin-23 | 0.123 | 44 | 0.68 |
| Junction-19 | 13.339 | 1,763 | 1.05 |
| Reach-19 | 13.339 | 1,761 | 1.05 |
| Source-1 | 1.396 | 109 | 0.58 |
| Subbasin-28 | 0.264 | 123 | 1.74 |
| Subbasin-29 | 0.172 | 111 | 2.06 |
| Junction-20 | 0.436 | 230 | 1.86 |
| Reach-20 | 0.436 | 220 | 1.86 |
| Subbasin-30 | 0.364 | 158 | 1.34 |
| Junction-23 | 15.535 | 1,788 | 1.04 |
| Reach-23 | 15.535 | 1,774 | 1.04 |
| Subbasin-31 | 0.377 | 290 | 1.38 |
| Subbasin-32 | 0.316 | 274 | 2.2 |
| Junction-24 | 16.228 | 1,796 | 1.07 |
| Reach-24 | 16.228 | 1,785 | 1.07 |
| Subbasin-33 | 0.184 | 24 | 0.37 |
| Junction-25 | 16.412 | 1,787 | 1.06 |
| Reach-25 | 16.412 | 1,781 | 1.06 |
| Junction-26 | 16.412 | 1,781 | 1.06 |

NOTE:

1. SOURCE-1 IS THE 24 HOUR FLOW DATA FOR SUBBASINS 24-27, JUNCTION 22, AND REACHES 21-22. SUBBASINS 24-27 DATA HAS BEEN REPLACED WITH KETTLE CREEK DRAINAGE BASIN OLD RANCH ROAD TRIBUTARY MASTER DEVELOPMENT PLAN FLOW DATA (JR ENG. 2001).

APPENDIX B — HYDROLOGIC RESULTS — FUTURE 5—YR KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B-67



FUTURE CONDITIONS MODEL RESULTS (10-YEAR)

| 10-Year, 2-Hour Storm | | | |
|-----------------------|-------------------------|-----------|--------|
| | | Peak | |
| Hydrologic | Drainage | Discharge | Volume |
| Element | Area (mi ²) | (CFS) | (in) |
| Subbasin-1 | 1.263 | 354 | 0.63 |
| Subbasin-2 | 0.586 | 198 | 0.64 |
| Subbasin-3 | 0.180 | 68 | 0.79 |
| Junction-1 | 2.029 | 608 | 0.65 |
| Reach-1 | 2.029 | 606 | 0.65 |
| Subbasin-4 | 0.195 | 63 | 0.57 |
| Junction-2 | 2.224 | 663 | 0.64 |
| Reach-2 | 2.224 | 663 | 0.64 |
| Subbasin-5 | 0.625 | 147 | 0.69 |
| Junction-3 | 2.849 | 797 | 0.65 |
| Reach-3 | 2.849 | 797 | 0.65 |
| Subbasin-6 | 1.333 | 255 | 0.54 |
| Junction-4 | 4.182 | 1,051 | 0.62 |
| Reach-4 | 4.182 | 1,051 | 0.62 |
| Subbasin-7 | 0.183 | 56 | 0.56 |
| Junction-5 | 4.365 | 1,074 | 0.61 |
| Reach-5 | 4.365 | 1,071 | 0.61 |
| Subbasin-8 | 0.288 | 131 | 0.65 |
| Junction-6 | 4.653 | 1,099 | 0.62 |
| Reach-6 | 4.653 | 1,097 | 0.62 |
| Subbasin-9 | 1.177 | 242 | 0.63 |
| Subbasin-10 | 0.222 | 70 | 0.54 |
| Junction-7 | 1.399 | 269 | 0.61 |
| Reach-7 | 1.399 | 269 | 0.61 |
| Subbasin-11 | 0.880 | 373 | 0.75 |
| Junction-8 | 2.279 | 540 | 0.67 |
| Reach-8 | 2.279 | 537 | 0.67 |
| Subbasin-12 | 0.552 | 159 | 0.62 |
| Junction-9 | 2.831 | 677 | 0.66 |
| Reach-9 | 2.831 | 675 | 0.66 |
| Junction-10 | 7.484 | 1,619 | 0.63 |
| Reach-10 | 7.484 | 1,619 | 0.63 |
| Subbasin-13 | 1.156 | 229 | 0.59 |
| Subbasin-14 | 0.516 | 153 | 0.55 |
| Junction-11 | 9.156 | 1,784 | 0.62 |
| Reach-11 | 9.156 | 1,782 | 0.62 |
| Subbasin-15 | 0.498 | 159 | 0.59 |
| Junction-12 | 9.654 | 1,795 | 0.62 |
| Reach-12 | 9.654 | 1,792 | 0.62 |
| Subbasin-16 | 0.819 | 217 | 0.64 |
| Subbasin-17 | 0.788 | 206 | 0.55 |
| Junction-13 | 11.261 | 1,833 | 0.62 |

| 10-Year, 2-Hour Storm | | | |
|-----------------------|------------------|-----------|--------|
| | | Peak | |
| Hydrologic | Drainage | Discharge | Volume |
| Element | Area (mi²) | (CFS) | (in) |
| Reach-13 | 11.261 | 1,830 | 0.62 |
| Subbasin-18 | 0.192 | 63 | 0.55 |
| Junction-14 | 11.453 | 1,831 | 0.62 |
| Reach-14 | 11.453 | 1,830 | 0.62 |
| Subbasin-19 | 0.552 | 121 | 0.61 |
| Junction-15 | 12.005 | 1,852 | 0.61 |
| Reach-15 | 12.005 | 1,849 | 0.61 |
| Subbasin-20 | 0.594 | 249 | 0.81 |
| Junction-16 | 12.599 | 1,851 | 0.62 |
| Reach-16 | 12.599 | 1,851 | 0.62 |
| Subbasin-21 | 0.417 | 128 | 0.51 |
| Junction-17 | 13.016 | 1,852 | 0.62 |
| Reach-17 | 13.016 | 1,850 | 0.62 |
| Subbasin-22 | 0.200 | 151 | 1.17 |
| Junction-18 | | 1,850 | |
| Reach-18 | 13.216 13.216 | , | 0.63 |
| | | 1,848 | 0.63 |
| Subbasin-23 | 0.123 | 43 | 0.35 |
| Junction-19 | 13.339 | 1,848 | 0.63 |
| Reach-19 | 13.339 | 1,846 | 0.63 |
| Subbasin-24 | 0.453 | 201 | 1.09 |
| Subbasin-25 | 0.169 | 242 | 1.31 |
| Subbasin-26 | 0.480 | 181 | 0.82 |
| Junction-21 | 1.102 | 403 | 1.01 |
| Reach-21 | 1.102 | 402 | 1.01 |
| Subbasin-27 | 0.294 | 195 | 1.04 |
| Junction-22 | 1.396 | 546 | 1.02 |
| Reach-22 | 1.396 | 545 | 1.02 |
| Subbasin-28 | 0.264 | 159 | 1.15 |
| Subbasin-29 | 0.172 | 156 | 1.41 |
| Junction-20 | 0.436 | 304 | 1.25 |
| Reach-20 | 0.436 | 303 | 1.25 |
| Subbasin-30 | 0.364 | 199 | 0.85 |
| Junction-23 | 15.535 | 1,848 | 0.68 |
| Reach-23 | 15.535 | 1,846 | 0.68 |
| Subbasin-31 | 0.377 | 369 | 0.89 |
| Subbasin-32 | 0.316 | 440 | 1.52 |
| Junction-24 | 16.228 | 1,846 | 0.71 |
| Reach-24 | 16.228 | 1,845 | 0.71 |
| Subbasin-33 | 0.184 | 20 | 0.16 |
| Junction-25 | 16.412 | 1845.4 | 0.7 |
| Reach-25 | 16.412 | 1845.4 | 0.7 |
| Junction-26 | 16.412 | 1845.4 | 0.7 |

| 10-Year, 24-Hour Storm | | | |
|------------------------|------------|-----------|--------|
| | | Peak | |
| Hydrologic | Drainage | Discharge | Volume |
| Element | Area (mi²) | (CFS) | (in) |
| Subbasin-1 | 1.263 | 416 | 1.37 |
| Subbasin-2 | 0.586 | 228 | 1.38 |
| Subbasin-3 | 0.180 | 72 | 1.61 |
| Junction-1 | 2.029 | 693 | 1.40 |
| Reach-1 | 2.029 | 692 | 1.40 |
| Subbasin-4 | 0.195 | 75 | 1.27 |
| Junction-2 | 2.224 | 753 | 1.38 |
| Reach-2 | 2.224 | 748 | 1.38 |
| Subbasin-5 | 0.625 | 176 | 1.48 |
| Junction-3 | 2.849 | 908 | 1.41 |
| Reach-3 | 2.849 | 908 | 1.41 |
| Subbasin-6 | 1.333 | 322 | 1.23 |
| Junction-4 | 4.182 | 1,230 | 1.35 |
| Reach-4 | 4.182 | 1,213 | 1.35 |
| Subbasin-7 | 0.183 | 69 | 1.27 |
| Junction-5 | 4.365 | 1,244 | 1.35 |
| Reach-5 | 4.365 | 1,230 | 1.35 |
| Subbasin-8 | 0.288 | 154.4 | 1.44 |
| Junction-6 | 4.653 | 1269 | 1.35 |
| Reach-6 | 4.653 | 1,248 | 1.35 |
| Subbasin-9 | 1.177 | 294 | 1.36 |
| Subbasin-10 | 0.222 | 84 | 1.23 |
| Junction-7 | 1.399 | 333 | 1.34 |
| Reach-7 | 1.399 | 331 | 1.34 |
| Subbasin-11 | 0.880 | 419 | 1.58 |
| Junction-8 | 2.279 | 636 | 1.44 |
| Reach-8 | 2.279 | 635 | 1.44 |
| Subbasin-12 | 0.552 | 190 | 1.38 |
| Junction-9 | 2.831 | 800 | 1.43 |
| Reach-9 | 2.831 | 781 | 1.43 |
| Junction-10 | 7.484 | 1,907 | 1.38 |
| Reach-10 | 7.484 | 1,885 | 1.38 |
| Subbasin-13 | 1.156 | 282 | 1.31 |
| Subbasin-14 | 0.516 | 185 | 1.25 |
| Junction-11 | 9.156 | 2,122 | 1.36 |
| Reach-11 | 9.156 | 2,120 | 1.36 |
| Subbasin-15 | 0.498 | 190 | 1.31 |
| Junction-12 | 9.654 | 2,162 | 1.36 |
| Reach-12 | 9.654 | 2,160 | 1.36 |

| 10-Year, 24-Hour Storm | | | |
|------------------------|-------------------------|-----------|--------|
| | | Peak | |
| Hydrologic | Drainage | Discharge | Volume |
| Element | Area (mi ²) | (CFS) | (in) |
| Subbasin-16 | 0.819 | 254 | 1.38 |
| Subbasin-17 | 0.788 | 247 | 1.25 |
| Junction-13 | 11.261 | 2,284 | 1.35 |
| Reach-13 | 11.261 | 2,250 | 1.35 |
| Subbasin-18 | 0.192 | 74 | 1.25 |
| Junction-14 | 11.453 | 2,258 | 1.35 |
| Reach-14 | 11.453 | 2,257 | 1.35 |
| Subbasin-19 | 0.552 | 147 | 1.34 |
| Junction-15 | 12.005 | 2,306 | 1.35 |
| Reach-15 | 12.005 | 2,301 | 1.35 |
| Subbasin-20 | 0.594 | 265 | 1.64 |
| Junction-16 | 12.599 | 2,333 | 1.37 |
| Reach-16 | 12.599 | 2,307 | 1.37 |
| Subbasin-21 | 0.417 | 154 | 1.19 |
| Junction-17 | 13.016 | 2,323 | 1.36 |
| Reach-17 | 13.016 | 2,322 | 1.36 |
| Subbasin-22 | 0.200 | 139 | 2.17 |
| Junction-18 | 13.216 | 2,332 | 1.37 |
| Reach-18 | 13.216 | 2,323 | 1.37 |
| Subbasin-23 | 0.123 | 62 | 0.94 |
| Junction-19 | 13.339 | 2,326 | 1.37 |
| Reach-19 | 13.339 | 2,323 | 1.37 |
| Source-1 | 1.396 | 188 | 0.77 |
| Subbasin-28 | 0.264 | 153 | 2.14 |
| Subbasin-29 | 0.172 | 136 | 2.50 |
| Junction-20 | 0.436 | 283 | 2.28 |
| Reach-20 | 0.436 | 271 | 2.28 |
| Subbasin-30 | 0.364 | 203 | 1.70 |
| Junction-23 | 15.535 | 2,357 | 1.35 |
| Reach-23 | 15.535 | 2,337 | 1.35 |
| Subbasin-31 | 0.377 | 368 | 1.73 |
| Subbasin-32 | 0.316 | 332 | 2.66 |
| Junction-24 | 16.228 | 2,364 | 1.38 |
| Reach-24 | 16.228 | 2,351 | 1.38 |
| Subbasin-33 | 0.184 | 39 | 0.55 |
| Junction-25 | 16.412 | 2,354 | 1.37 |
| Reach-25 | 16.412 | 2,345 | 1.37 |
| Junction-26 | 16.412 | 2,345 | 1.37 |

NOTE:

1. SOURCE-1 IS THE 24 HOUR FLOW DATA FOR SUBBASINS 24-27, JUNCTION 22, AND REACHES 21-22. SUBBASINS 24-27 DATA HAS BEEN REPLACED WITH KETTLE CREEK DRAINAGE BASIN OLD RANCH ROAD TRIBUTARY MASTER DEVELOPMENT PLAN FLOW DATA (JR ENG. 2001).

APPENDIX B — HYDROLOGIC RESULTS — FUTURE 10—YR KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B-68



FUTURE CONDITIONS MODEL RESULTS (25-YEAR)

| 25-Year, 2-Hour Storm | | | |
|-----------------------|------------|-----------|--------|
| | | Peak | |
| Hydrologic | Drainage | Discharge | Volume |
| Element | Area (mi²) | (CFS) | (in) |
| Subbasin-1 | 1.263 | 442 | 0.78 |
| Subbasin-2 | 0.586 | 248 | 0.79 |
| Subbasin-3 | 0.180 | 83 | 0.96 |
| Junction-1 | 2.029 | 757 | 0.80 |
| Reach-1 | 2.029 | 755 | 0.80 |
| Subbasin-4 | 0.195 | 80 | 0.71 |
| Junction-2 | 2.224 | 827 | 0.79 |
| Reach-2 | 2.224 | 827 | 0.79 |
| Subbasin-5 | 0.625 | 184 | 0.85 |
| Junction-3 | 2.849 | 994 | 0.81 |
| Reach-3 | 2.849 | 994 | 0.81 |
| Subbasin-6 | 1.333 | 324 | 0.68 |
| Junction-4 | 4.182 | 1,316 | 0.77 |
| Reach-4 | 4.182 | 1,316 | 0.77 |
| Subbasin-7 | 0.183 | 72 | 0.70 |
| Junction-5 | 4.365 | 1,346 | 0.76 |
| Reach-5 | 4.365 | 1,341 | 0.76 |
| Subbasin-8 | 0.288 | 166 | 0.81 |
| Junction-6 | 4.653 | 1,376 | 0.77 |
| Reach-6 | 4.653 | 1,374 | 0.77 |
| Subbasin-9 | 1.177 | 302 | 0.78 |
| Subbasin-10 | 0.222 | 89 | 0.68 |
| Junction-7 | 1.399 | 337 | 0.76 |
| Reach-7 | 1.399 | 337 | 0.76 |
| Subbasin-11 | 0.880 | 463 | 0.92 |
| Junction-8 | 2.279 | 672 | 0.82 |
| Reach-8 | 2.279 | 669 | 0.82 |
| Subbasin-12 | 0.552 | 201 | 0.78 |
| Junction-9 | 2.831 | 844 | 0.82 |
| Reach-9 | 2.831 | 843 | 0.82 |
| Junction-10 | 7.484 | 2,025 | 0.79 |
| Reach-10 | 7.484 | 2,023 | 0.79 |
| Subbasin-13 | 1.156 | 288 | 0.73 |
| Subbasin-14 | 0.516 | 194 | 0.69 |
| Junction-11 | 9.156 | 2,228 | 0.77 |
| Reach-11 | 9.156 | 2,226 | 0.77 |
| Subbasin-15 | 0.498 | 201 | 0.73 |
| Junction-12 | 9.654 | 2,242 | 0.77 |
| Reach-12 | 9.654 | 2,238 | 0.77 |
| Subbasin-16 | 0.819 | 270 | 0.79 |
| Subbasin-17 | 0.788 | 261 | 0.69 |
| Junction-13 | 11.261 | 2,288 | 0.77 |

| 25-Year, 2-Hour Storm | | | |
|-----------------------|-------------------------|-----------|--------|
| | | Peak | |
| Hydrologic | Drainage | Discharge | Volume |
| Element | Area (mi ²) | (CFS) | (in) |
| Reach-13 | 11.261 | 2,285 | 0.77 |
| Subbasin-18 | 0.192 | 80 | 0.69 |
| Junction-14 | 11.453 | 2,286 | 0.77 |
| Reach-14 | 11.453 | 2,284 | 0.77 |
| Subbasin-19 | 0.552 | 152 | 0.76 |
| Junction-15 | 12.005 | 2,311 | 0.77 |
| Reach-15 | 12.005 | 2,307 | 0.77 |
| Subbasin-20 | 0.594 | 304 | 0.98 |
| Junction-16 | 12.599 | 2,311 | 0.78 |
| Reach-16 | 12.599 | 2,310 | 0.78 |
| Subbasin-21 | 0.417 | 164 | 0.65 |
| Junction-17 | 13.016 | 2,311 | 0.77 |
| Reach-17 | 13.016 | 2,308 | 0.77 |
| Subbasin-22 | 0.200 | 180 | 1.39 |
| Junction-18 | 13.216 | 2,308 | 0.78 |
| Reach-18 | 13.216 | 2,306 | 0.78 |
| Subbasin-23 | 0.123 | 59 | 0.76 |
| Junction-19 | 13.339 | 2,306 | 0.40 |
| Reach-19 | 13.339 | , | 0.78 |
| Subbasin-24 | | 2,303 | 1.30 |
| | 0.453 | 241 | |
| Subbasin-25 | 0.169 | 285 | 1.54 |
| Subbasin-26 | 0.480 | 220 | 1.00 |
| Junction-21 | 1.102 | 485 | 1.21 |
| Reach-21 | 1.102 | 484 | 1.21 |
| Subbasin-27 | 0.294 | 234 | 1.25 |
| Junction-22 | 1.396 | 656 | 1.21 |
| Reach-22 | 1.396 | 655 | 1.21 |
| Subbasin-28 | 0.264 | 189 | 1.37 |
| Subbasin-29 | 0.172 | 183 | 1.65 |
| Junction-20 | 0.436 | 360 | 1.48 |
| Reach-20 | 0.436 | 358 | 1.48 |
| Subbasin-30 | 0.364 | 243 | 1.03 |
| Junction-23 | 15.535 | 2,306 | 0.84 |
| Reach-23 | 15.535 | 2,303 | 0.84 |
| Subbasin-31 | 0.377 | 446 | 1.07 |
| Subbasin-32 | 0.316 | 516 | 1.77 |
| Junction-24 | 16.228 | 2,303 | 0.87 |
| Reach-24 | 16.228 | 2,302 | 0.87 |
| Subbasin-33 | 0.184 | 31 | 0.23 |
| Junction-25 | 16.412 | 2302 | 0.86 |
| Reach-25 | 16.412 | 2302 | 0.86 |
| Junction-26 | 16.412 | 2302 | 0.86 |

| 25-Year, 24-Hour Storm | | | |
|------------------------|-------------------------|-----------|--------|
| | | Peak | |
| Hydrologic | Drainage | Discharge | Volume |
| Element | Area (mi ²) | (CFS) | (in) |
| Subbasin-1 | 1.263 | 502 | 1.64 |
| Subbasin-2 | 0.586 | 276 | 1.65 |
| Subbasin-3 | 0.180 | 86 | 1.90 |
| Junction-1 | 2.029 | 835 | 1.67 |
| Reach-1 | 2.029 | 834 | 1.67 |
| Subbasin-4 | 0.195 | 91 | 1.53 |
| Junction-2 | 2.224 | 907 | 1.65 |
| Reach-2 | 2.224 | 903 | 1.65 |
| Subbasin-5 | 0.625 | 212 | 1.76 |
| Junction-3 | 2.849 | 1,095 | 1.68 |
| Reach-3 | 2.849 | 1,095 | 1.68 |
| Subbasin-6 | 1.333 | 393 | 1.49 |
| Junction-4 | 4.182 | 1,488 | 1.62 |
| Reach-4 | 4.182 | 1,467 | 1.62 |
| Subbasin-7 | 0.183 | 84 | 1.53 |
| Junction-5 | 4.365 | 1,504 | 1.61 |
| Reach-5 | 4.365 | 1,488 | 1.61 |
| Subbasin-8 | 0.288 | 187 | 1.72 |
| Junction-6 | 4.653 | 1,535 | 1.62 |
| Reach-6 | 4.653 | 1,509 | 1.62 |
| Subbasin-9 | 1.177 | 355 | 1.63 |
| Subbasin-10 | 0.222 | 102 | 1.48 |
| Junction-7 | 1.399 | 403 | 1.61 |
| Reach-7 | 1.399 | 401 | 1.61 |
| Subbasin-11 | 0.880 | 501 | 1.88 |
| Junction-8 | 2.279 | 766 | 1.71 |
| Reach-8 | 2.279 | 764 | 1.71 |
| Subbasin-12 | 0.552 | 230 | 1.65 |
| Junction-9 | 2.831 | 964 | 1.70 |
| Reach-9 | 2.831 | 941 | 1.70 |
| Junction-10 | 7.484 | 2,304 | 1.65 |
| Reach-10 | 7.484 | 2,276 | 1.65 |
| Subbasin-13 | 1.156 | 342 | 1.57 |
| Subbasin-14 | 0.516 | 226 | 1.51 |
| Junction-11 | 9.156 | 2,565 | 1.63 |
| Reach-11 | 9.156 | 2,563 | 1.63 |
| Subbasin-15 | 0.498 | 231 | 1.57 |
| Junction-12 | 9.654 | 2,613 | 1.63 |
| Reach-12 | 9.654 | 2,609 | 1.63 |

| 25-Year, 24-Hour Storm | | | |
|------------------------|-------------------------|-----------|--------|
| | | Peak | |
| Hydrologic | Drainage | Discharge | Volume |
| Element | Area (mi ²) | (CFS) | (in) |
| Subbasin-16 | 0.819 | 307 | 1.65 |
| Subbasin-17 | 0.788 | 301 | 1.51 |
| Junction-13 | 11.261 | 2,759 | 1.62 |
| Reach-13 | 11.261 | 2,715 | 1.62 |
| Subbasin-18 | 0.192 | 90 | 1.50 |
| Junction-14 | 11.453 | 2,726 | 1.62 |
| Reach-14 | 11.453 | 2,725 | 1.62 |
| Subbasin-19 | 0.552 | 178 | 1.61 |
| Junction-15 | 12.005 | 2,784 | 1.62 |
| Reach-15 | 12.005 | 2,777 | 1.62 |
| Subbasin-20 | 0.594 | 315 | 1.93 |
| Junction-16 | 12.599 | 2,816 | 1.63 |
| Reach-16 | 12.599 | 2,786 | 1.63 |
| Subbasin-21 | 0.417 | 189 | 1.44 |
| Junction-17 | 13.016 | 2,805 | 1.63 |
| Reach-17 | 13.016 | 2,802 | 1.63 |
| Subbasin-22 | 0.200 | 161 | 2.50 |
| Junction-18 | 13.216 | 2,813 | 1.64 |
| Reach-18 | 13.216 | 2,804 | 1.64 |
| Subbasin-23 | 0.123 | 79 | 1.17 |
| Junction-19 | 13.339 | 2,807 | 1.64 |
| Reach-19 | 13.339 | 2,804 | 1.64 |
| Source-1 | 1.396 | 333 | 1.11 |
| Subbasin-28 | 0.264 | 177 | 2.47 |
| Subbasin-29 | 0.172 | 156 | 2.86 |
| Junction-20 | 0.436 | 327 | 2.63 |
| Reach-20 | 0.436 | 313 | 2.63 |
| Subbasin-30 | 0.364 | 241 | 2.00 |
| Junction-23 | 15.535 | 2,843 | 1.63 |
| Reach-23 | 15.535 | 2,817 | 1.63 |
| Subbasin-31 | 0.377 | 433 | 2.02 |
| Subbasin-32 | 0.316 | 380 | 3.03 |
| Junction-24 | 16.228 | 2,849 | 1.66 |
| Reach-24 | 16.228 | 2,835 | 1.66 |
| Subbasin-33 | 0.184 | 53 | 0.72 |
| Junction-25 | 16.412 | 2,838 | 1.65 |
| Reach-25 | 16.412 | 2,827 | 1.65 |
| Junction-26 | 16.412 | 2,827 | 1.65 |

NOTE:

1. SOURCE-1 IS THE 24 HOUR FLOW DATA FOR SUBBASINS 24-27, JUNCTION 22, AND REACHES 21-22. SUBBASINS 24-27 DATA HAS BEEN REPLACED WITH KETTLE CREEK DRAINAGE BASIN OLD RANCH ROAD TRIBUTARY MASTER DEVELOPMENT PLAN FLOW DATA (JR ENG. 2001).

APPENDIX B — HYDROLOGIC RESULTS — FUTURE 25—YR KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B-69



FUTURE CONDITIONS MODEL RESULTS (50-YEAR)

| 50-Year, 2-Hour Storm | | | |
|-----------------------|------------|-----------|--------|
| | | Peak | |
| Hydrologic | Drainage | Discharge | Volume |
| Element | Area (mi²) | (CFS) | (in) |
| Subbasin-1 | 1.263 | 533 | 0.94 |
| Subbasin-2 | 0.586 | 299 | 0.95 |
| Subbasin-3 | 0.180 | 98 | 1.14 |
| Junction-1 | 2.029 | 911 | 0.96 |
| Reach-1 | 2.029 | 909 | 0.96 |
| Subbasin-4 | 0.195 | 97 | 0.86 |
| Junction-2 | 2.224 | 996 | 0.95 |
| Reach-2 | 2.224 | 996 | 0.95 |
| Subbasin-5 | 0.625 | 221 | 1.02 |
| Junction-3 | 2.849 | 1,197 | 0.97 |
| Reach-3 | 2.849 | 1,197 | 0.97 |
| Subbasin-6 | 1.333 | 395 | 0.83 |
| Junction-4 | 4.182 | 1,590 | 0.92 |
| Reach-4 | 4.182 | 1,589 | 0.92 |
| Subbasin-7 | 0.183 | 88 | 0.86 |
| Junction-5 | 4.365 | 1,626 | 0.92 |
| Reach-5 | 4.365 | 1,620 | 0.92 |
| Subbasin-8 | 0.288 | 202 | 0.98 |
| Junction-6 | 4.653 | 1,662 | 0.92 |
| Reach-6 | 4.653 | 1,659 | 0.92 |
| Subbasin-9 | 1.177 | 364 | 0.94 |
| Subbasin-10 | 0.222 | 109 | 0.82 |
| Junction-7 | 1.399 | 406 | 0.92 |
| Reach-7 | 1.399 | 406 | 0.92 |
| Subbasin-11 | 0.880 | 555 | 1.10 |
| Junction-8 | 2.279 | 808 | 0.99 |
| Reach-8 | 2.279 | 804 | 0.99 |
| Subbasin-12 | 0.552 | 243 | 0.94 |
| Junction-9 | 2.831 | 1,017 | 0.98 |
| Reach-9 | 2.831 | 1,015 | 0.98 |
| Junction-10 | 7.484 | 2,442 | 0.95 |
| Reach-10 | 7.484 | 2,440 | 0.95 |
| Subbasin-13 | 1.156 | 349 | 0.89 |
| Subbasin-14 | 0.516 | 237 | 0.84 |
| Junction-11 | 9.156 | 2,688 | 0.93 |
| Reach-11 | 9.156 | 2,686 | 0.93 |
| Subbasin-15 | 0.498 | 245 | 0.89 |
| Junction-12 | 9.654 | 2,705 | 0.93 |
| Reach-12 | 9.654 | 2,700 | 0.93 |
| Subbasin-16 | 0.819 | 325 | 0.95 |
| Subbasin-17 | 0.788 | 318 | 0.84 |
| Junction-13 | 11.261 | 2,759 | 0.93 |

| 50-Year, 2-Hour Storm | | | |
|-----------------------|------------|-----------|--------|
| | | Peak | |
| Hydrologic | Drainage | Discharge | Volume |
| Element | Area (mi²) | (CFS) | (in) |
| Reach-13 | 11.261 | 2,757 | 0.93 |
| Subbasin-18 | 0.192 | 98 | 0.84 |
| Junction-14 | 11.453 | 2,757 | 0.92 |
| Reach-14 | 11.453 | 2,756 | 0.92 |
| Subbasin-19 | 0.552 | 183 | 0.92 |
| Junction-15 | 12.005 | 2,788 | 0.92 |
| Reach-15 | 12.005 | 2,783 | 0.92 |
| Subbasin-20 | 0.594 | 361 | 1.16 |
| Junction-16 | 12.599 | 2,788 | 0.93 |
| Reach-16 | 12.599 | 2,787 | 0.93 |
| Subbasin-21 | 0.417 | 203 | 0.79 |
| Junction-17 | 13.016 | 2,787 | 0.93 |
| Reach-17 | 13.016 | 2,784 | 0.93 |
| Subbasin-22 | 0.200 | 208 | 1.61 |
| Junction-18 | 13.216 | 2,784 | 0.94 |
| Reach-18 | 13.216 | 2,782 | 0.94 |
| Subbasin-23 | 0.123 | 76 | 0.59 |
| Junction-19 | 13.339 | 2,782 | 0.94 |
| Reach-19 | 13.339 | 2,778 | 0.94 |
| Subbasin-24 | 0.453 | 280 | 1.51 |
| Subbasin-25 | 0.169 | 329 | 1.77 |
| Subbasin-26 | 0.480 | 261 | 1.18 |
| Junction-21 | 1.102 | 568 | 1.41 |
| Reach-21 | 1.102 | 567 | 1.41 |
| Subbasin-27 | 0.294 | 273 | 1.45 |
| Junction-22 | 1.396 | 766 | 1.41 |
| Reach-22 | 1.396 | 764 | 1.41 |
| Subbasin-28 | 0.264 | 219 | 1.58 |
| Subbasin-29 | 0.172 | 210 | 1.89 |
| Junction-20 | 0.436 | 415 | 1.71 |
| Reach-20 | 0.436 | 413 | 1.71 |
| Subbasin-30 | 0.364 | 287 | 1.21 |
| Junction-23 | 15.535 | 2,782 | 1.01 |
| Reach-23 | 15.535 | 2,777 | 1.01 |
| Subbasin-31 | 0.377 | 524 | 1.25 |
| Subbasin-32 | 0.316 | 591 | 2.02 |
| Junction-24 | 16.228 | 2,777 | 1.03 |
| Reach-24 | 16.228 | 2,776 | 1.03 |
| Subbasin-33 | 0.184 | 43 | 0.31 |
| Junction-25 | 16.412 | 2776.4 | 1.03 |
| Reach-25 | 16.412 | 2776.4 | 1.03 |
| Junction-26 | 16.412 | 2776.4 | 1.03 |

| 50-Year, 24-Hour Storm | | | |
|------------------------|-------------------------|-----------|--------|
| | | Peak | |
| Hydrologic | Drainage | Discharge | Volume |
| Element | Area (mi ²) | (CFS) | (in) |
| Subbasin-1 | 1.26 | 533.20 | 0.94 |
| Subbasin-2 | 0.59 | 298.70 | 0.95 |
| Subbasin-3 | 0.18 | 98.40 | 1.14 |
| Junction-1 | 2.03 | 910.80 | 0.96 |
| Reach-1 | 2.03 | 909.20 | 0.96 |
| Subbasin-4 | 0.20 | 97.30 | 0.86 |
| Junction-2 | 2.22 | 995.80 | 0.95 |
| Reach-2 | 2.22 | 995.80 | 0.95 |
| Subbasin-5 | 0.63 | 220.70 | 1.02 |
| Junction-3 | 2.85 | 1197.40 | 0.97 |
| Reach-3 | 2.85 | 1197.40 | 0.97 |
| Subbasin-6 | 1.33 | 394.70 | 0.83 |
| Junction-4 | 4.18 | 1590.30 | 0.92 |
| Reach-4 | 4.18 | 1589.40 | 0.92 |
| Subbasin-7 | 0.18 | 87.60 | 0.86 |
| Junction-5 | 4.37 | 1625.90 | 0.92 |
| Reach-5 | 4.37 | 1620.10 | 0.92 |
| Subbasin-8 | 0.29 | 201.70 | 0.98 |
| Junction-6 | 4.65 | 1661.80 | 0.92 |
| Reach-6 | 4.65 | 1659.30 | 0.92 |
| Subbasin-9 | 1.18 | 364.20 | 0.94 |
| Subbasin-10 | 0.22 | 109.00 | 0.82 |
| Junction-7 | 1.40 | 406.10 | 0.92 |
| Reach-7 | 1.40 | 406.10 | 0.92 |
| Subbasin-11 | 0.88 | 555.40 | 1.10 |
| Junction-8 | 2.28 | 808.10 | 0.99 |
| Reach-8 | 2.28 | 803.50 | 0.99 |
| Subbasin-12 | 0.55 | 243.30 | 0.94 |
| Junction-9 | 2.83 | 1016.70 | 0.98 |
| Reach-9 | 2.83 | 1014.60 | 0.98 |
| Junction-10 | 7.48 | 2442.20 | 0.95 |
| Reach-10 | 7.48 | 2440.30 | 0.95 |
| Subbasin-13 | 1.16 | 349.30 | 0.89 |
| Subbasin-14 | 0.52 | 236.80 | 0.84 |
| Junction-11 | 9.16 | 2687.70 | 0.93 |
| Reach-11 | 9.16 | 2685.80 | 0.93 |
| Subbasin-15 | 0.50 | 244.50 | 0.89 |
| Junction-12 | 9.65 | 2704.90 | 0.93 |
| Reach-12 | 9.65 | 2700.30 | 0.93 |

| 50-Year, 24-Hour Storm | | | |
|------------------------|-------------------------|-----------|--------|
| | | Peak | |
| Hydrologic | Drainage | Discharge | Volume |
| Element | Area (mi ²) | (CFS) | (in) |
| Subbasin-16 | 0.82 | 325.40 | 0.95 |
| Subbasin-17 | 0.79 | 317.90 | 0.84 |
| Junction-13 | 11.26 | 2759.40 | 0.93 |
| Reach-13 | 11.26 | 2756.60 | 0.93 |
| Subbasin-18 | 0.19 | 97.90 | 0.84 |
| Junction-14 | 11.45 | 2757.30 | 0.92 |
| Reach-14 | 11.45 | 2755.70 | 0.92 |
| Subbasin-19 | 0.55 | 183.40 | 0.92 |
| Junction-15 | 12.01 | 2787.70 | 0.92 |
| Reach-15 | 12.01 | 2783.40 | 0.92 |
| Subbasin-20 | 0.59 | 360.50 | 1.16 |
| Junction-16 | 12.60 | 2787.50 | 0.93 |
| Reach-16 | 12.60 | 2787.00 | 0.93 |
| Subbasin-21 | 0.42 | 202.80 | 0.79 |
| Junction-17 | 13.02 | 2787.20 | 0.93 |
| Reach-17 | 13.02 | 2783.60 | 0.93 |
| Subbasin-22 | 0.20 | 208.40 | 1.61 |
| Junction-18 | 13.22 | 2783.70 | 0.94 |
| Reach-18 | 13.22 | 2781.60 | 0.94 |
| Subbasin-23 | 0.12 | 76.20 | 0.59 |
| Junction-19 | 13.34 | 2781.60 | 0.94 |
| Reach-19 | 13.34 | 2778.30 | 0.94 |
| Source-1 | 1.40 | 485.70 | 1.33 |
| Subbasin-28 | 0.26 | 218.90 | 1.58 |
| Subbasin-29 | 0.17 | 210.10 | 1.89 |
| Junction-20 | 0.44 | 414.50 | 1.71 |
| Reach-20 | 0.44 | 412.90 | 1.71 |
| Subbasin-30 | 0.36 | 287.40 | 1.21 |
| Junction-23 | 15.54 | 2779.50 | 1.00 |
| Reach-23 | 15.54 | 2774.50 | 1.00 |
| Subbasin-31 | 0.38 | 524.10 | 1.25 |
| Subbasin-32 | 0.32 | 590.70 | 2.02 |
| Junction-24 | 16.23 | 2774.50 | 1.03 |
| Reach-24 | 16.23 | 2773.70 | 1.02 |
| Subbasin-33 | 0.18 | 42.80 | 0.31 |
| Junction-25 | 16.41 | 2773.70 | 1.01 |
| Reach-25 | 16.41 | 2773.70 | 1.01 |
| Junction-26 | 16.41 | 2773.70 | 1.01 |

NOTE:

1. SOURCE-1 IS THE 24 HOUR FLOW DATA FOR SUBBASINS 24-27, JUNCTION 22, AND REACHES 21-22. SUBBASINS 24-27 DATA HAS BEEN REPLACED WITH KETTLE CREEK DRAINAGE BASIN OLD RANCH ROAD TRIBUTARY MASTER DEVELOPMENT PLAN FLOW DATA (JR ENG. 2001).

APPENDIX B — HYDROLOGIC RESULTS — FUTURE 50—YR KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B-70



FUTURE CONDITIONS MODEL RESULTS (100-YEAR)

| 100-Year, 2-Hour Storm | | | |
|------------------------|------------|-----------|--------|
| | | Peak | |
| Hydrologic | Drainage | Discharge | Volume |
| Element | Area (mi²) | (CFS) | (in) |
| Subbasin-1 | 1.263 | 634 | 1.12 |
| Subbasin-2 | 0.586 | 355 | 1.13 |
| Subbasin-3 | 0.180 | 115 | 1.33 |
| Junction-1 | 2.029 | 1,082 | 1.14 |
| Reach-1 | 2.029 | 1,080 | 1.14 |
| Subbasin-4 | 0.195 | 117 | 1.03 |
| Junction-2 | 2.224 | 1,184 | 1.13 |
| Reach-2 | 2.224 | 1,184 | 1.13 |
| Subbasin-5 | 0.625 | 262 | 1.21 |
| Junction-3 | 2.849 | 1,423 | 1.15 |
| Reach-3 | 2.849 | 1,423 | 1.15 |
| Subbasin-6 | 1.333 | 474 | 0.99 |
| Junction-4 | 4.182 | 1,895 | 1.10 |
| Reach-4 | 4.182 | 1,894 | 1.10 |
| Subbasin-7 | 0.183 | 106 | 1.03 |
| Junction-5 | 4.365 | 1,938 | 1.10 |
| Reach-5 | 4.365 | 1,931 | 1.10 |
| Subbasin-8 | 0.288 | 242 | 1.17 |
| Junction-6 | 4.653 | 1,980 | 1.10 |
| Reach-6 | 4.653 | 1,977 | 1.10 |
| Subbasin-9 | 1.177 | 433 | 1.11 |
| Subbasin-10 | 0.222 | 132 | 0.99 |
| Junction-7 | 1.399 | 483 | 1.09 |
| Reach-7 | 1.399 | 483 | 1.09 |
| Subbasin-11 | 0.880 | 657 | 1.30 |
| Junction-8 | 2.279 | 959 | 1.17 |
| Reach-8 | 2.279 | 953 | 1.17 |
| Subbasin-12 | 0.552 | 291 | 1.12 |
| Junction-9 | 2.831 | 1,208 | 1.16 |
| Reach-9 | 2.831 | 1,205 | 1.16 |
| Junction-10 | 7.484 | 2,905 | 1.12 |
| Reach-10 | 7.484 | 2,903 | 1.12 |
| Subbasin-13 | 1.156 | 418 | 1.06 |
| Subbasin-14 | 0.516 | 285 | 1.01 |
| Junction-11 | 9.156 | 3,198 | 1.11 |
| Reach-11 | 9.156 | 3,195 | 1.11 |
| Subbasin-15 | 0.498 | 293 | 1.06 |
| Junction-12 | 9.654 | 3,218 | 1.11 |
| Reach-12 | 9.654 | 3,213 | 1.11 |
| Subbasin-16 | 0.819 | 387 | 1.12 |
| Subbasin-17 | 0.788 | 382 | 1.01 |
| Junction-13 | 11.261 | 3,283 | 1.10 |

| 100-Year, 2-Hour Storm | | | |
|------------------------|------------|-----------|--------|
| | | Peak | |
| Hydrologic | Drainage | Discharge | Volume |
| Element | Area (mi²) | (CFS) | (in) |
| Reach-13 | 11.261 | 3,280 | 1.10 |
| Subbasin-18 | 0.192 | 118 | 1.01 |
| Junction-14 | 11.453 | 3,281 | 1.10 |
| Reach-14 | 11.453 | 3,279 | 1.10 |
| Subbasin-19 | 0.552 | 219 | 1.09 |
| Junction-15 | 12.005 | 3,317 | 1.10 |
| Reach-15 | 12.005 | 3,312 | 1.10 |
| Subbasin-20 | 0.594 | 422 | 1.36 |
| Junction-16 | 12.599 | 3,316 | 1.11 |
| Reach-16 | 12.599 | 3,316 | 1.11 |
| Subbasin-21 | 0.417 | 246 | 0.95 |
| Junction-17 | 13.016 | 3,316 | 1.11 |
| Reach-17 | 13.016 | 3,312 | 1.11 |
| Subbasin-22 | 0.200 | 239 | 1.84 |
| Junction-18 | 13.216 | 3,312 | 1.12 |
| Reach-18 | 13.216 | 3,309 | 1.12 |
| Subbasin-23 | 0.123 | 96 | 0.73 |
| Junction-19 | 13.339 | 3,309 | 1.11 |
| Reach-19 | 13.339 | 3,305 | 1.11 |
| Subbasin-24 | 0.453 | 322 | 1.74 |
| Subbasin-25 | 0.169 | 374 | 2.01 |
| Subbasin-26 | 0.480 | 305 | 1.38 |
| Junction-21 | 1.102 | 657 | 1.62 |
| Reach-21 | 1.102 | 656 | 1.62 |
| Subbasin-27 | 0.294 | 315 | 1.67 |
| Junction-22 | 1.396 | 886 | 1.63 |
| Reach-22 | 1.396 | 884 | 1.63 |
| Subbasin-28 | 0.264 | 251 | 1.82 |
| Subbasin-29 | 0.172 | 239 | 2.15 |
| Junction-20 | 0.436 | 473 | 1.95 |
| Reach-20 | 0.436 | 471 | 1.95 |
| Subbasin-30 | 0.364 | 336 | 1.41 |
| Junction-23 | 15.535 | 3,310 | 1.19 |
| Reach-23 | 15.535 | 3,304 | 1.19 |
| Subbasin-31 | 0.377 | 608 | 1.45 |
| Subbasin-32 | 0.316 | 669 | 2.29 |
| Junction-24 | 16.228 | 3,304 | 1.22 |
| Reach-24 | 16.228 | 3,303 | 1.22 |
| Subbasin-33 | 0.184 | 57 | 0.41 |
| Junction-25 | 16.412 | 3302.7 | 1.21 |
| Reach-25 | 16.412 | 3302.7 | 1.21 |
| Junction-26 | 16.412 | 3302.7 | 1.21 |

| 100-Year, 24-Hour Storm | | | | | |
|-------------------------|----------------|-----------|--------|--|--|
| | Peak | | | | |
| Hydrologic | Drainage | Discharge | Volume | | |
| Element | Area (mi²) | (CFS) | (in) | | |
| Subbasin-1 | 1.263 | 735 | 2.36 | | |
| Subbasin-2 | 0.586 | 403 | 2.37 | | |
| Subbasin-3 | 0.180 | 122 | 2.67 | | |
| Junction-1 | 2.029 | 1,217 | 2.39 | | |
| Reach-1 | 2.029 | 1,216 | 2.39 | | |
| Subbasin-4 | 0.195 | 135 | 2.22 | | |
| Junction-2 | 2.224 | 1,325 | 2.38 | | |
| Reach-2 | 2.224 | 1,323 | 2.38 | | |
| Subbasin-5 | 0.625 | 308 | 2.52 | | |
| Junction-3 | 2.849 | 1,602 | 2.41 | | |
| Reach-3 | 2.849 | 1,602 | 2.41 | | |
| Subbasin-6 | | 588 | 2.41 | | |
| Junction-4 | 1.333 4.182 | | 2.34 | | |
| | | 2,190 | | | |
| Reach-4 | 4.182 | 2,153 | 2.34 | | |
| Subbasin-7 | 0.183 | 125 | 2.24 | | |
| Junction-5 | 4.365 | 2,208 | 2.33 | | |
| Reach-5 | 4.365 | 2,186 | 2.33 | | |
| Subbasin-8 | 0.288 | 273.3 | 2.48 | | |
| Junction-6 | 4.653 | 2253.3 | 2.34 | | |
| Reach-6 | 4.653 | 2,213 | 2.34 | | |
| Subbasin-9 | 1.177 | 520 | 2.35 | | |
| Subbasin-10 | 0.222 | 152 | 2.17 | | |
| Junction-7 | 1.399 | 593 | 2.32 | | |
| Reach-7 | 1.399 | 588 | 2.32 | | |
| Subbasin-11 | 0.880 | 720 | 2.66 | | |
| Junction-8 | 2.279 | 1,114 | 2.45 | | |
| Reach-8 | 2.279 | 1,112 | 2.45 | | |
| Subbasin-12 | 0.552 | 338 | 2.39 | | |
| Junction-9 | 2.831 | 1,403 | 2.44 | | |
| Reach-9 | 2.831 | 1,368 | 2.44 | | |
| Junction-10 | 7.484 | 3,375 | 2.38 | | |
| Reach-10 | 7.484 | 3,329 | 2.38 | | |
| Subbasin-13 | 1.156 | 505 | 2.28 | | |
| Subbasin-14 | 0.516 | 337 | 2.20 | | |
| Junction-11 | 9.156 | 3,761 | 2.36 | | |
| Reach-11 | 9.156 | 3,756 | 2.36 | | |
| Subbasin-15 | 0.498 | 342 | 2.28 | | |
| Junction-12 | 9.654 | 3,828 | 2.35 | | |
| Reach-12 | 9.654 | 3,823 | 2.35 | | |

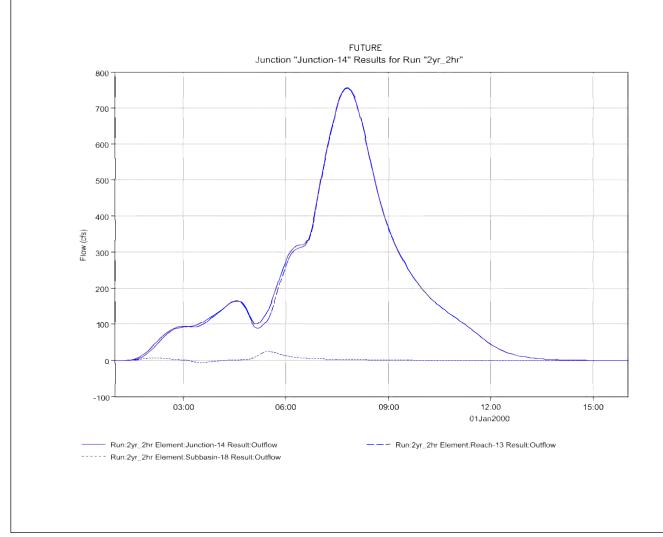
| 100-Year, 24-Hour Storm | | | |
|-------------------------|-------------------------|-----------|--------|
| | | Peak | |
| Hydrologic | Drainage | Discharge | Volume |
| Element | Area (mi ²) | (CFS) | (in) |
| Subbasin-16 | 0.819 | 449 | 2.37 |
| Subbasin-17 | 0.788 | 447 | 2.20 |
| Junction-13 | 11.261 | 4,038 | 2.34 |
| Reach-13 | 11.261 | 3,975 | 2.34 |
| Subbasin-18 | 0.192 | 134.1 | 2.2 |
| Junction-14 | 11.453 | 3,992 | 2.34 |
| Reach-14 | 11.453 | 3,987 | 2.34 |
| Subbasin-19 | 0.552 | 262 | 2.32 |
| Junction-15 | 12.005 | 4,072 | 2.34 |
| Reach-15 | 12.005 | 4,061 | 2.34 |
| Subbasin-20 | 0.594 | 448 | 2.70 |
| Junction-16 | 12.599 | 4,115 | 2.36 |
| Reach-16 | 12.599 | 4,077 | 2.36 |
| Subbasin-21 | 0.417 | 284 | 2.12 |
| Junction-17 | 13.016 | 4,105 | 2.35 |
| Reach-17 | 13.016 | 4,093 | 2.35 |
| Subbasin-22 | 0.200 | 219 | 3.37 |
| Junction-18 | 13.216 | 4,108 | 2.37 |
| Reach-18 | 13.216 | 4,099 | 2.37 |
| Subbasin-23 | 0.123 | 124 | 1.80 |
| Junction-19 | 13.339 | 4,104 | 2.36 |
| Reach-19 | 13.339 | 4,099 | 2.36 |
| Source-1 | 1.396 | 576 | 1.58 |
| Subbasin-28 | 0.264 | 241 | 3.34 |
| Subbasin-29 | 0.172 | 207 | 3.78 |
| Junction-20 | 0.436 | 439 | 3.51 |
| Reach-20 | 0.436 | 421 | 3.51 |
| Subbasin-30 | 0.364 | 340 | 2.78 |
| Junction-23 | 15.535 | 4,152 | 2.33 |
| Reach-23 | 15.535 | 4,110 | 2.33 |
| Subbasin-31 | 0.377 | 606 | 2.79 |
| Subbasin-32 | 0.316 | 500 | 3.98 |
| Junction-24 | 16.228 | 4,152 | 2.38 |
| Reach-24 | 16.228 | 4,137 | 2.38 |
| Subbasin-33 | 0.184 | 93 | 1.21 |
| Junction-25 | 16.412 | 4,142 | 2.36 |
| Reach-25 | 16.412 | 4,123 | 2.36 |
| Junction-26 | 16.412 | 4,123 | 2.36 |

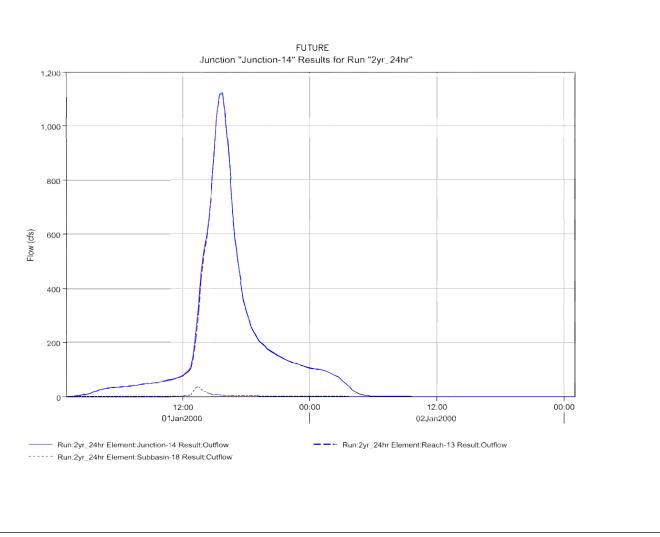
NOTE:

1. SOURCE-1 IS THE 24 HOUR FLOW DATA FOR SUBBASINS 24-27, JUNCTION 22, AND REACHES 21-22. SUBBASINS 24-27 DATA HAS BEEN REPLACED WITH KETTLE CREEK DRAINAGE BASIN OLD RANCH ROAD TRIBUTARY MASTER DEVELOPMENT PLAN FLOW DATA (JR ENG. 2001).

APPENDIX B — HYDROLOGIC RESULTS — FUTURE 100—YR KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B—71





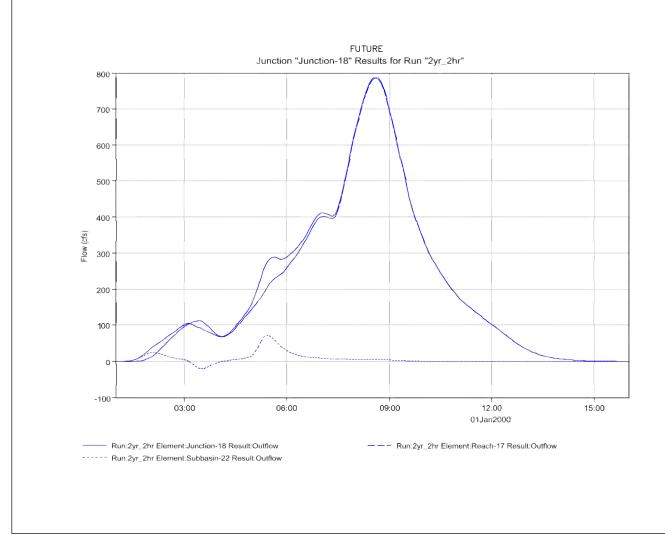


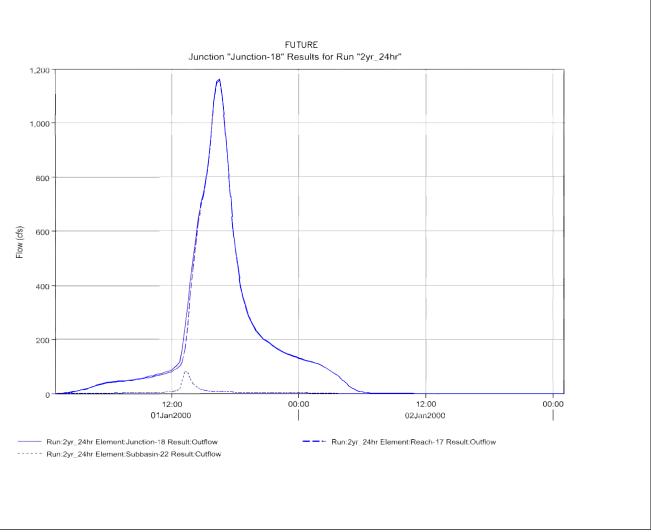
> JUNCTION 14 HOWELLS ROAD (APPROXIMATE)

FUTURE CONDITIONS HYDROGRAPHS
AT SELECT LOCATIONS
2-YEAR

APPENDIX B — HYDROLOGIC RESULTS— FUTURE HYDROGRAPHS 2—YR J—14 KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B—72





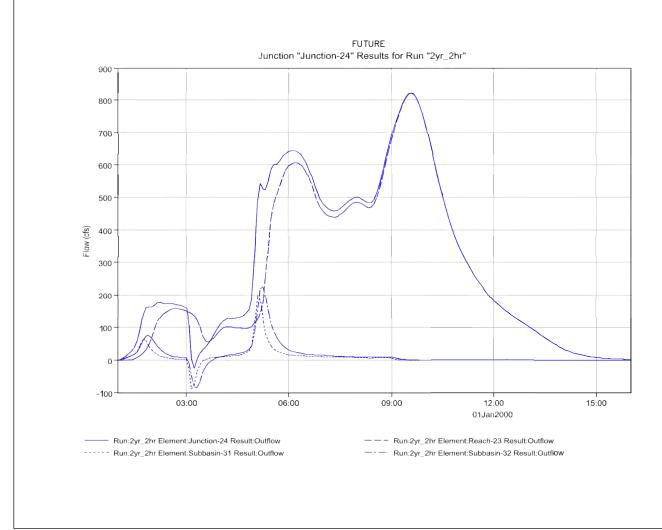


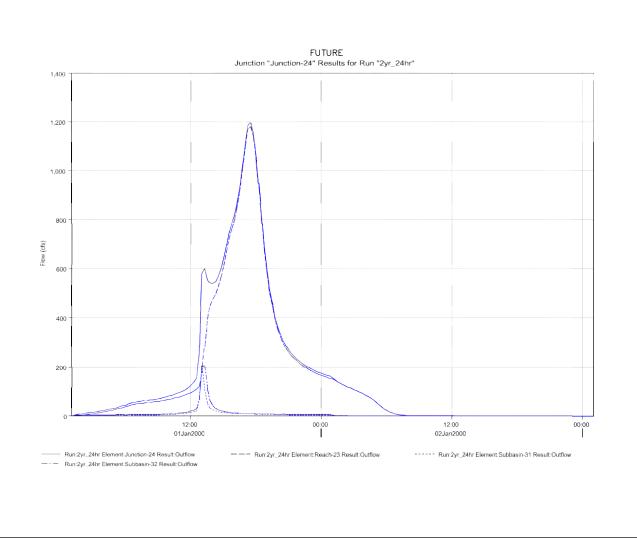
> JUNCTION 18 POWERS BLVD BRIDGE

FUTURE CONDITIONS HYDROGRAPHS
AT SELECT LOCATIONS
2-YEAR

APPENDIX B — HYDROLOGIC RESULTS— FUTURE HYDROGRAPHS 2—YR J—18 KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B—73





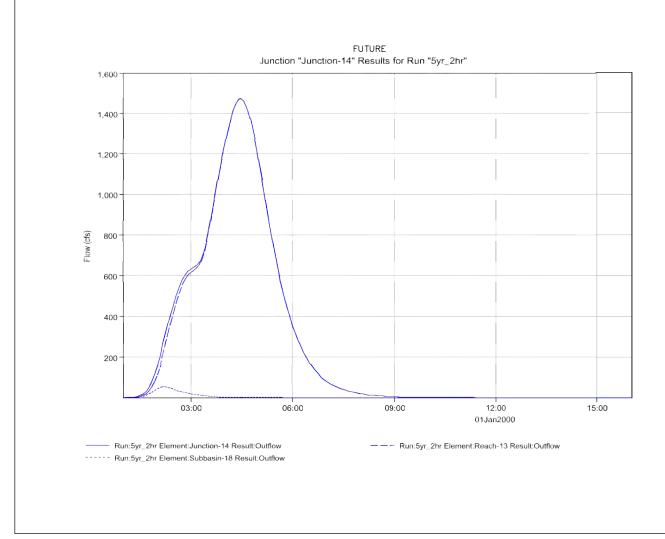


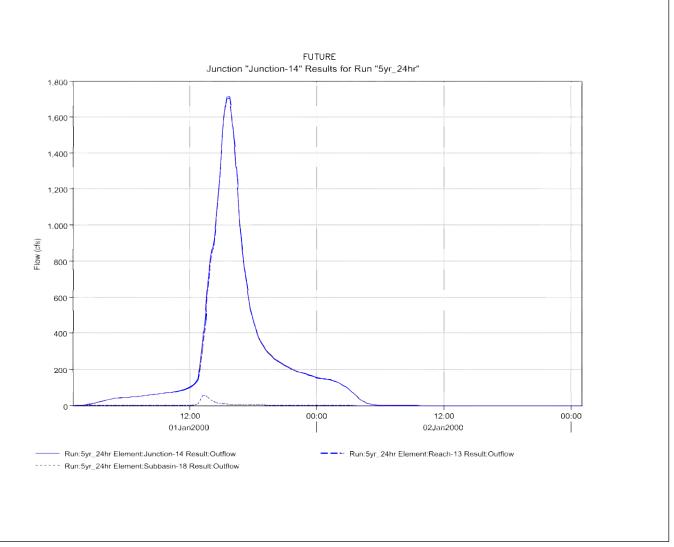
> JUNCTION 18 POWERS BLVD BRIDGE

FUTURE CONDITIONS HYDROGRAPHS
AT SELECT LOCATIONS
2-YEAR

APPENDIX B — HYDROLOGIC RESULTS— FUTURE HYDROGRAPHS 2—YR J—24 KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B—74







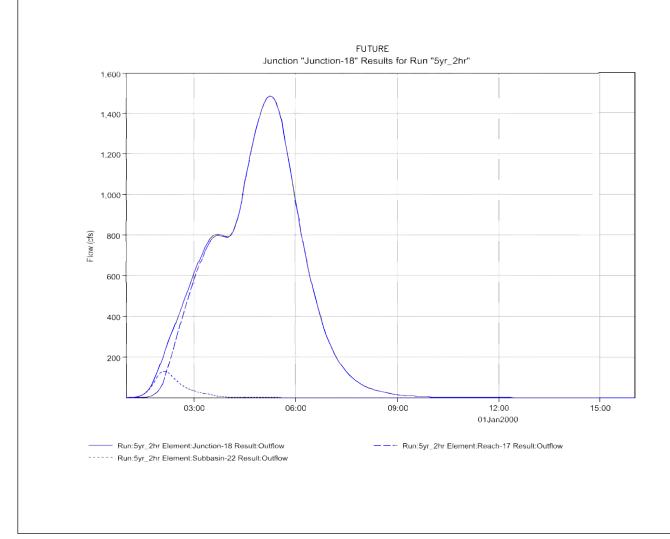
5-YR 2-HR 5-YR 24-HR

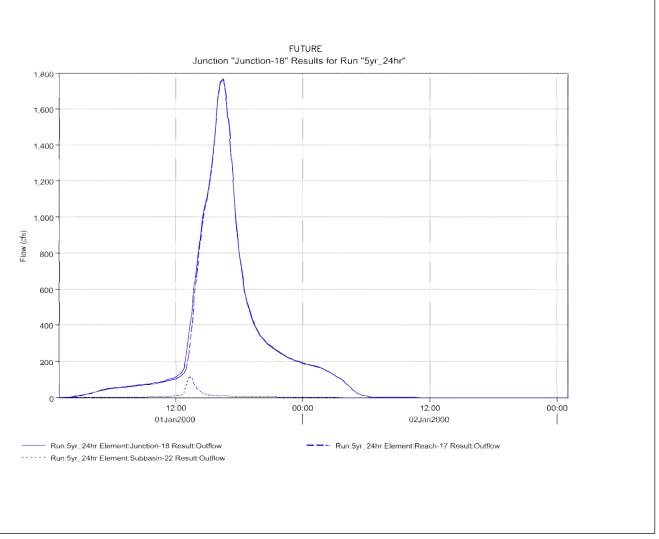
> JUNCTION 14 HOWELLS ROAD (APPROXIMATE)

FUTURE CONDITIONS HYDROGRAPHS
AT SELECT LOCATIONS
5-YEAR

APPENDIX B — HYDROLOGIC RESULTS— FUTURE HYDROGRAPHS 5—YR J—14 KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B—75





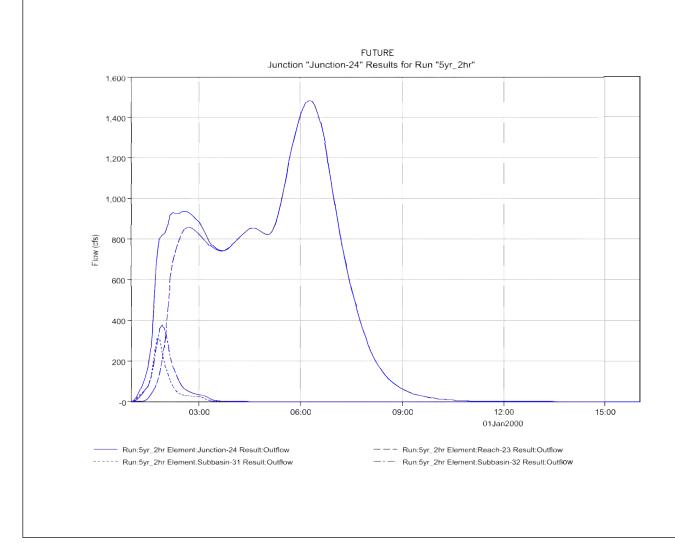


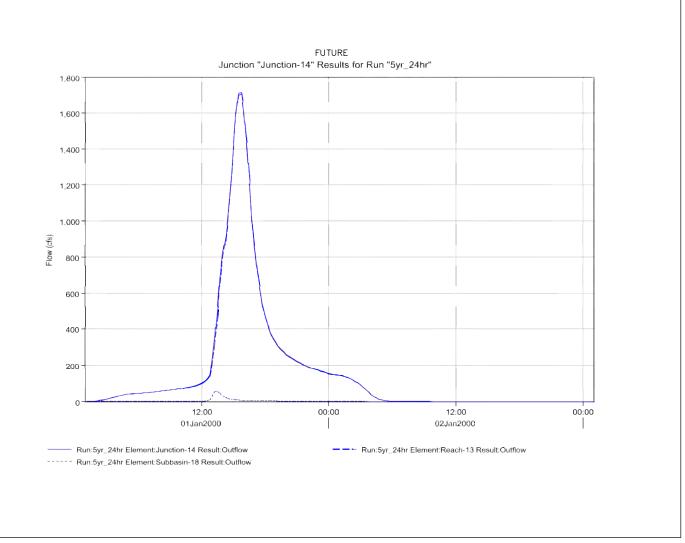
5-YR 2-HR 5-YR 24-HR

> JUNCTION 18 POWERS BLVD BRIDGE

FUTURE CONDITIONS HYDROGRAPHS AT SELECT LOCATIONS 5-YEAR APPENDIX B — HYDROLOGIC RESULTS— FUTURE HYDROGRAPHS 5—YR J—18 KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B—76





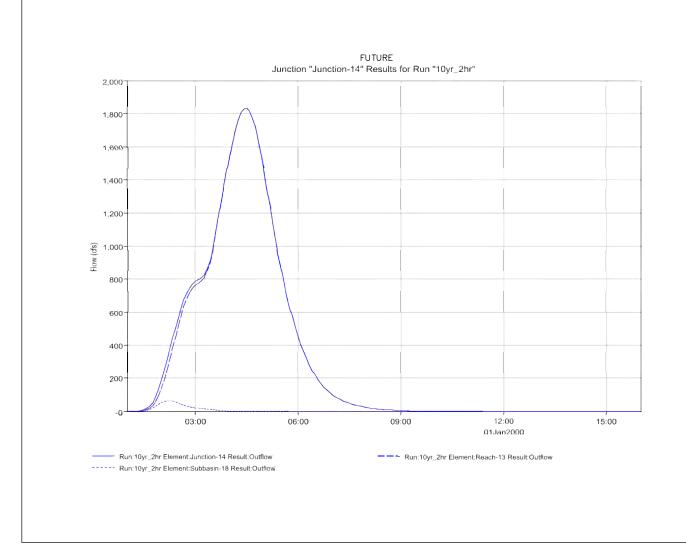


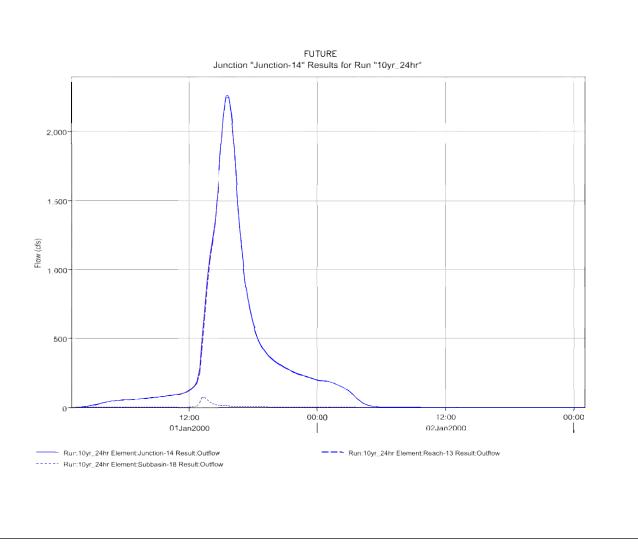
5-YR 2-HR 5-YR 24-HR

> JUNCTION 24 HWY 83 BRIDGE

FUTURE CONDITIONS HYDROGRAPHS AT SELECT LOCATIONS 5-YEAR APPENDIX B — HYDROLOGIC RESULTS— FUTURE HYDROGRAPHS 5—YR J—24 KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B—77





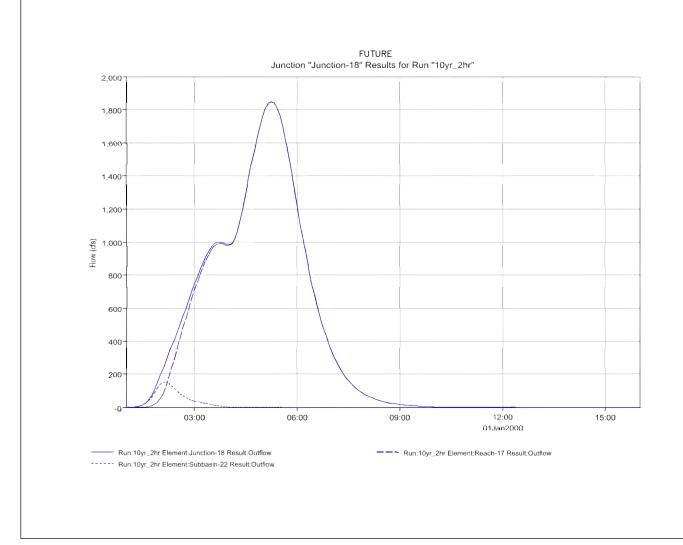


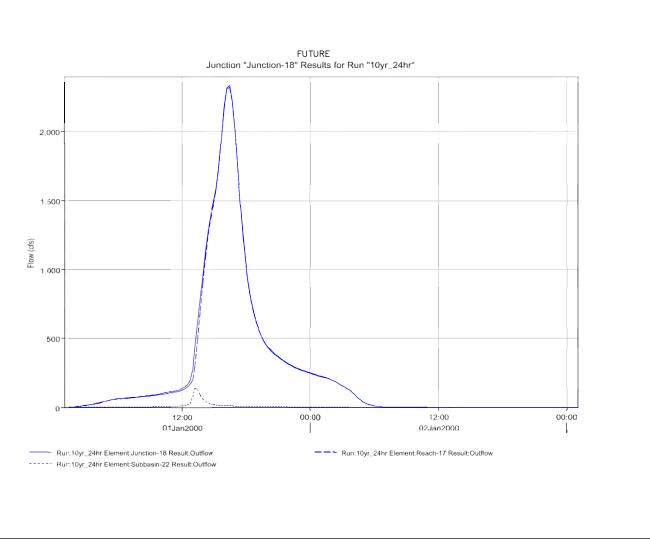
10-YR 2-HR 10-YR 24-HR

> JUNCTION 14 HOWELLS ROAD (APPROXIMATE)

FUTURE CONDITIONS HYDROGRAPHS AT SELECT LOCATIONS 10-YEAR APPENDIX B — HYDROLOGIC RESULTS— FUTURE HYDROGRAPHS 10—YR J—14 KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B—78







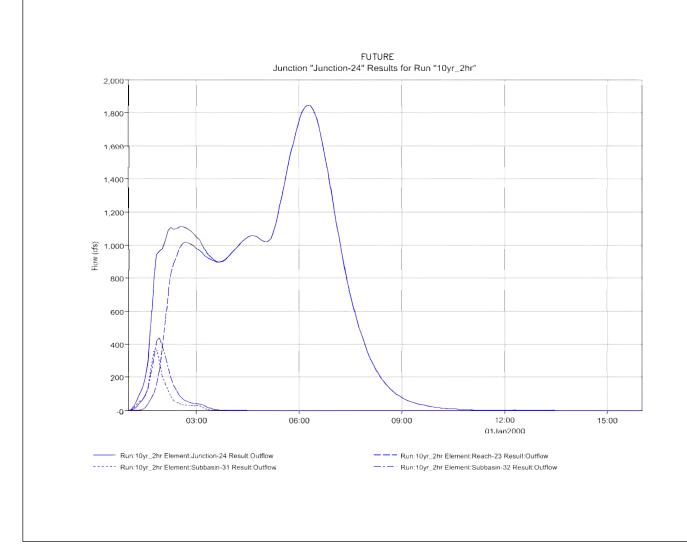
10-YR 2-HR 10-YR 24-HR

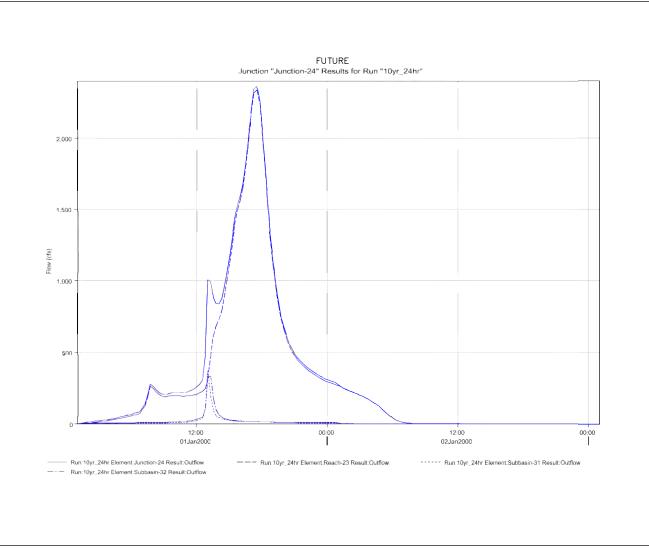
JUNCTION 18
POWERS BLVD BRIDGE

FUTURE CONDITIONS HYDROGRAPHS
AT SELECT LOCATIONS
10-YEAR

APPENDIX B — HYDROLOGIC RESULTS— FUTURE HYDROGRAPHS 10—YR J—18 KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B—79





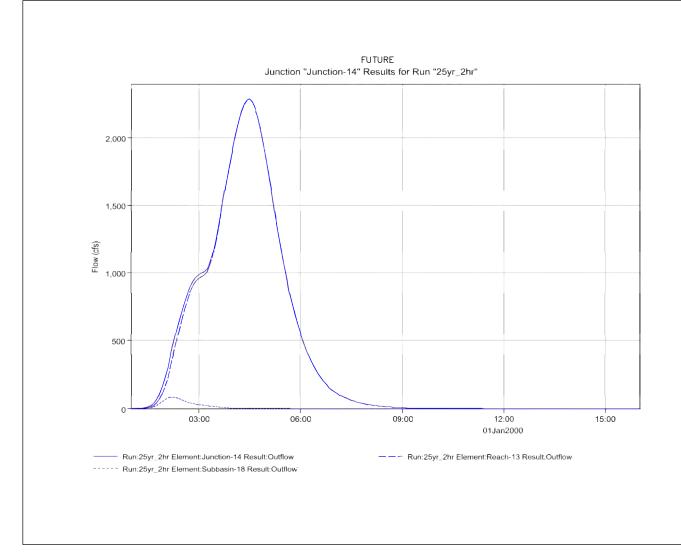


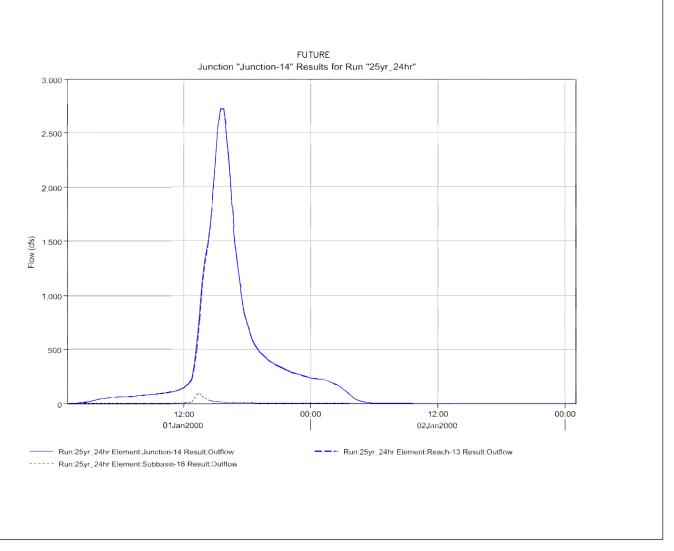
10-YR 2-HR 10-YR 24-HR

> JUNCTION 24 HWY 83 BRIDGE

FUTURE CONDITIONS HYDROGRAPHS AT SELECT LOCATIONS 10-YEAR APPENDIX B — HYDROLOGIC RESULTS— FUTURE HYDROGRAPHS 10—YR J—24 KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B—80





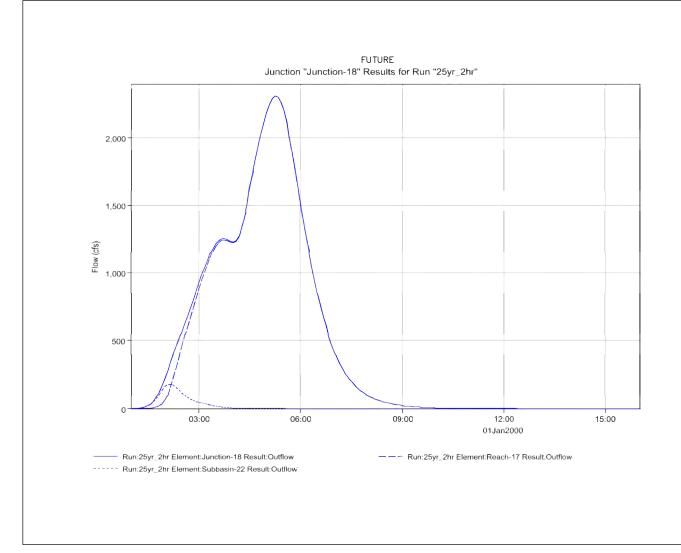


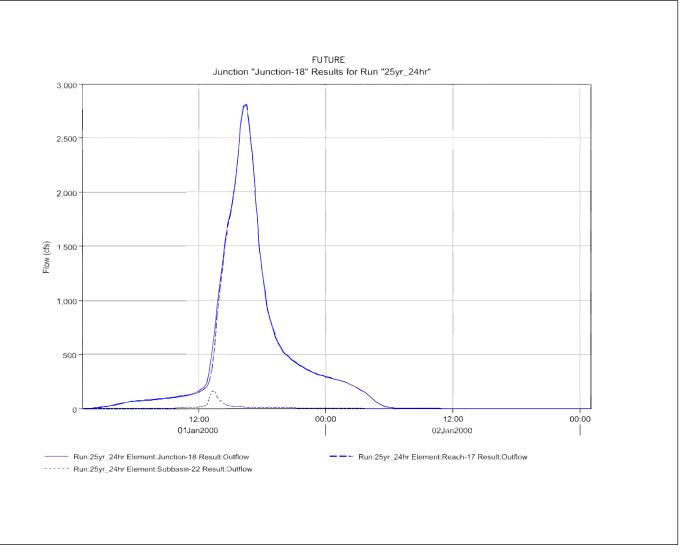
25-YR 2-HR 25-YR 24-HR

JUNCTION 14 HOWELLS ROAD (APPROXIMATE)

FUTURE CONDITIONS HYDROGRAPHS AT SELECT LOCATIONS 25-YEAR APPENDIX B — HYDROLOGIC RESULTS— FUTURE HYDROGRAPHS 25—YR J—14 KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B—81





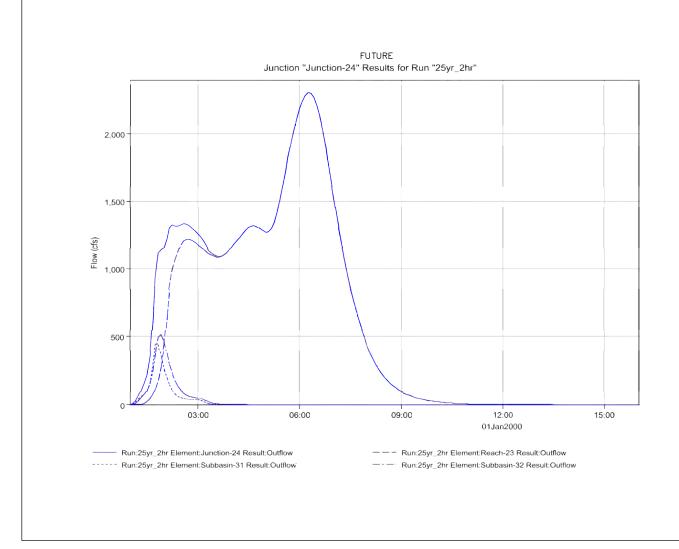


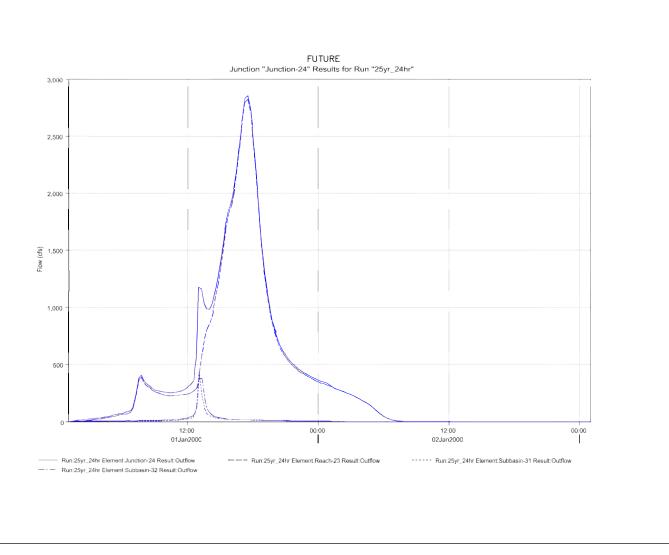
25-YR 2-HR 25-YR 24-HR

JUNCTION 18 POWERS BLVD BRIDGE

FUTURE CONDITIONS HYDROGRAPHS AT SELECT LOCATIONS 25-YEAR APPENDIX B — HYDROLOGIC RESULTS— FUTURE HYDROGRAPHS 25—YR J—18 KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B—82





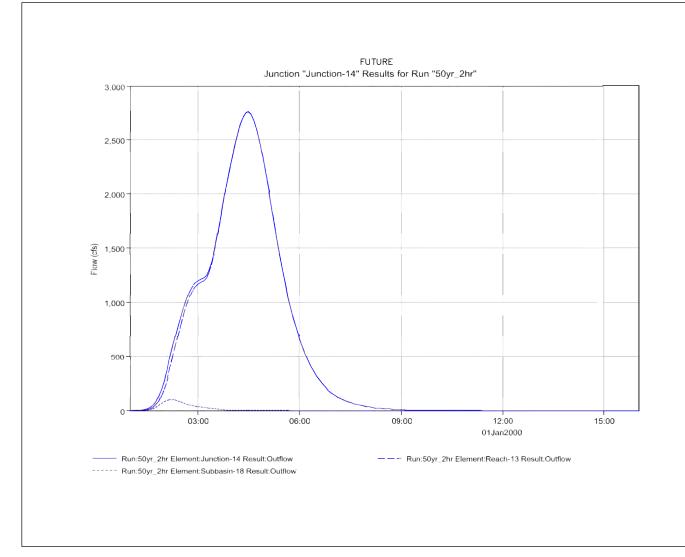


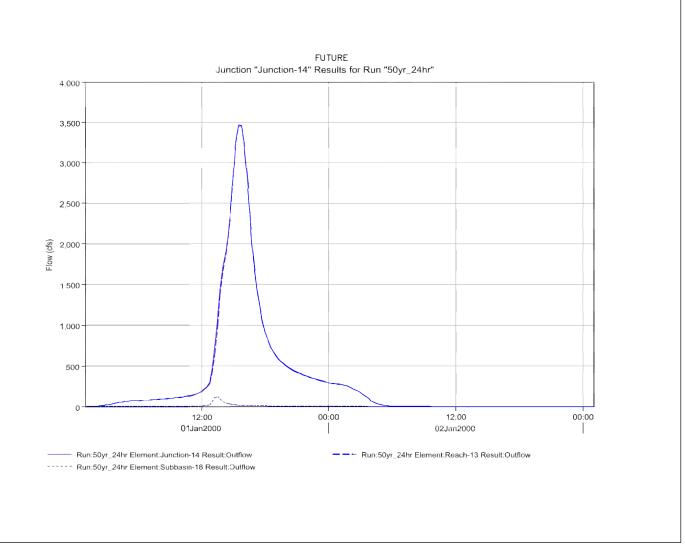
25-YR 2-HR 25-YR 24-HR

JUNCTION 24 HWY 83 BRIDGE

FUTURE CONDITIONS HYDROGRAPHS AT SELECT LOCATIONS 25-YEAR APPENDIX B — HYDROLOGIC RESULTS— FUTURE HYDROGRAPHS 25—YR J—24 KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B—83







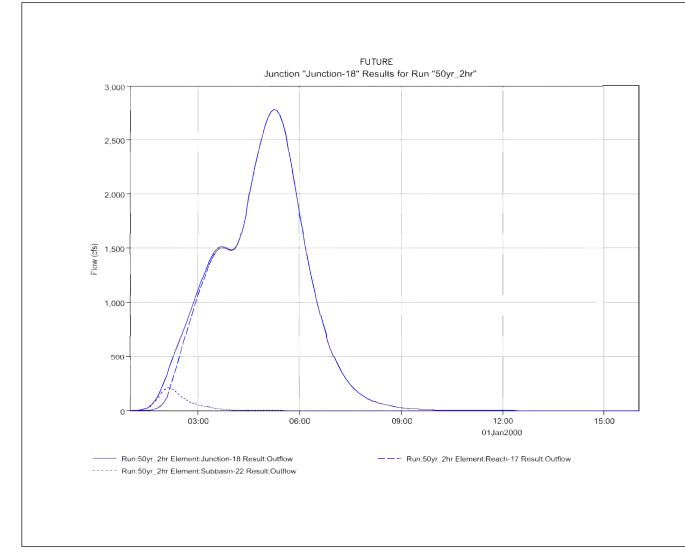
50-YR 2-HR 50-YR 24-HR

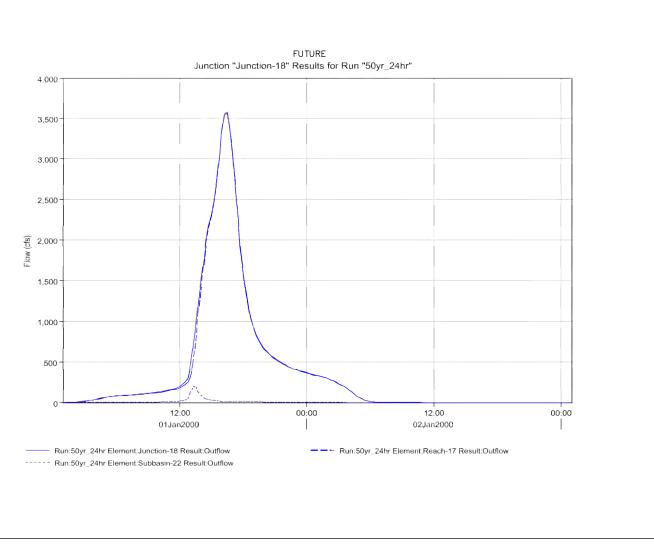
> JUNCTION 14 HOWELLS ROAD (APPROXIMATE)

FUTURE CONDITIONS HYDROGRAPHS
AT SELECT LOCATIONS
50-YEAR

APPENDIX B — HYDROLOGIC RESULTS— FUTURE HYDROGRAPHS 50—YR J—14 KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B—84







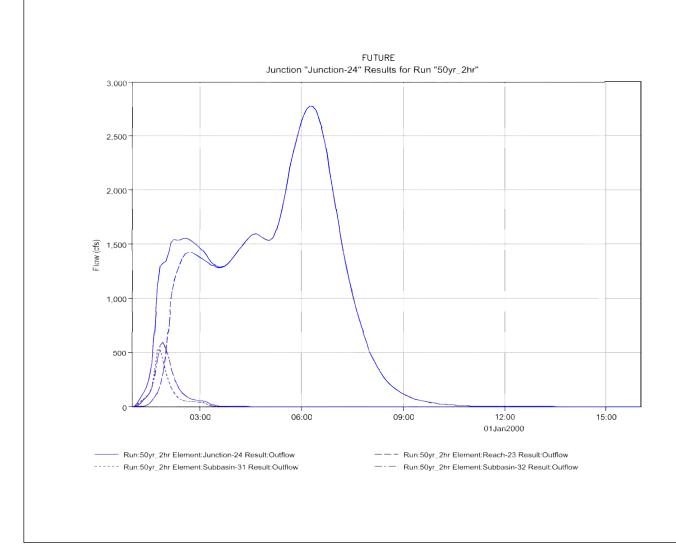
50-YR 2-HR 50-YR 24-HR

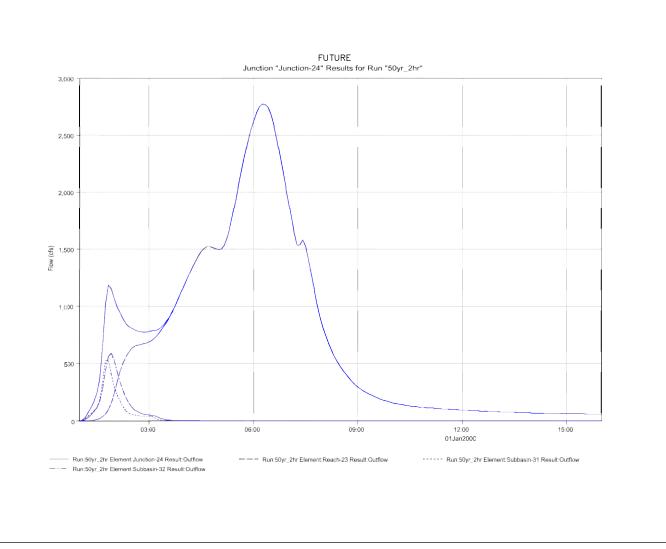
> JUNCTION 18 POWERS BLVD BRIDGE

FUTURE CONDITIONS HYDROGRAPHS
AT SELECT LOCATIONS
50-YEAR

APPENDIX B — HYDROLOGIC RESULTS— FUTURE HYDROGRAPHS 50—YR J—18 KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B—85







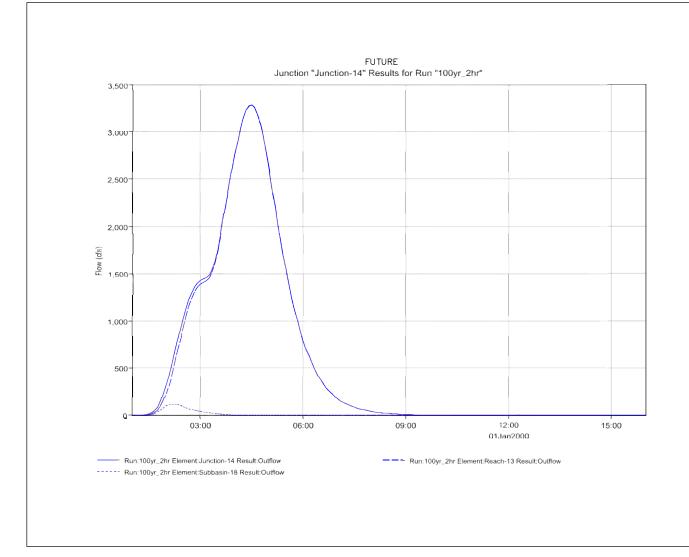
50-YR 2-HR 50-YR 24-HR

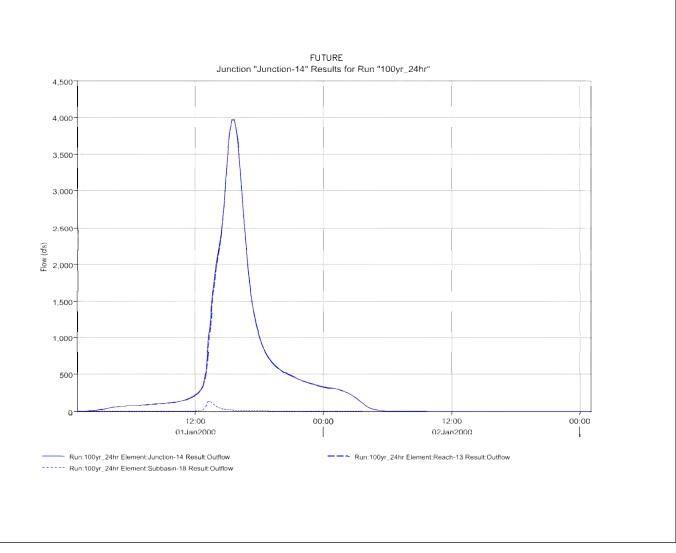
> JUNCTION 24 HWY 83 BRIDGE

FUTURE CONDITIONS HYDROGRAPHS
AT SELECT LOCATIONS
50-YEAR

APPENDIX B — HYDROLOGIC RESULTS— FUTURE HYDROGRAPHS 50—YR J—24 KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B—86





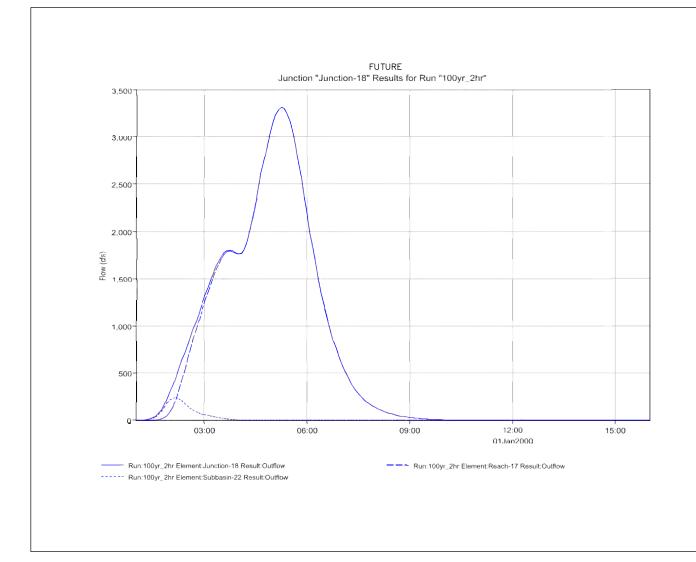


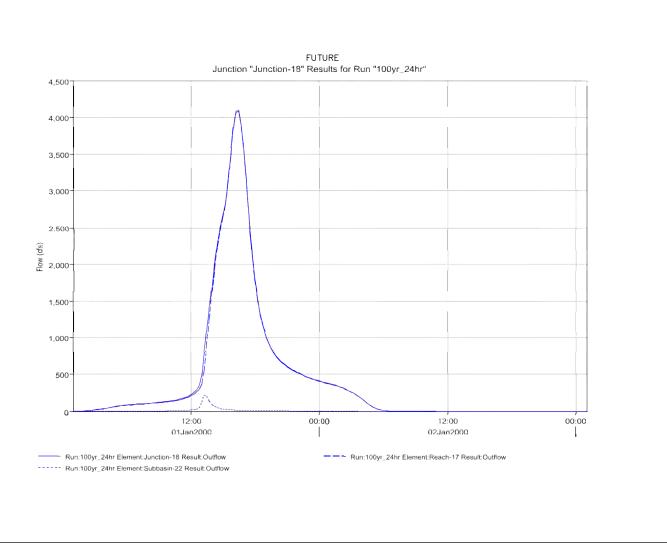
100-YR 2-HR 100-YR 24-HR

> JUNCTION 14 HOWELLS ROAD (APPROXIMATE)

FUTURE CONDITIONS HYDROGRAPHS AT SELECT LOCATIONS 100-YEAR APPENDIX B— HYDROLOGIC RESULTS— FUTURE HYDROGRAPHS 100—YR J—14 KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B—87







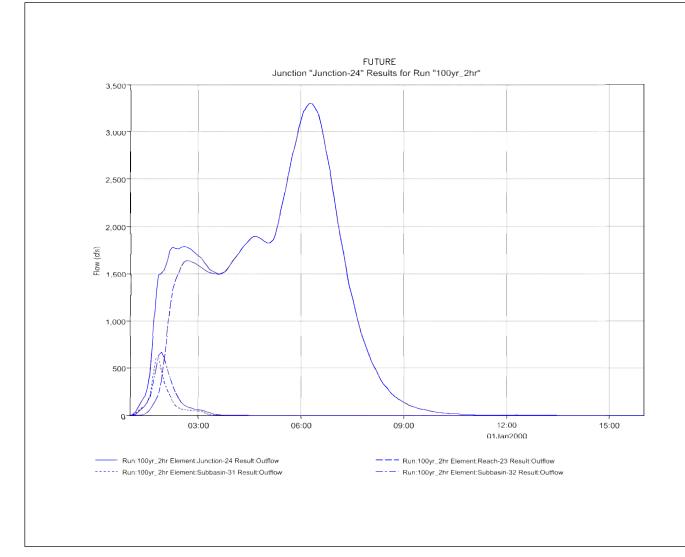
100-YR 2-HR 100-YR 24-HR

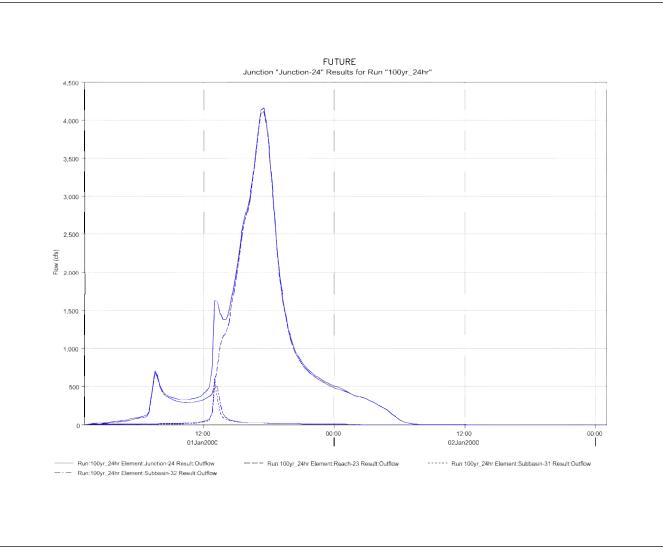
JUNCTION 18
POWERS BLVD BRIDGE

FUTURE CONDITIONS HYDROGRAPHS
AT SELECT LOCATIONS
100-YEAR

APPENDIX B— HYDROLOGIC RESULTS— FUTURE HYDROGRAPHS 100—YR J—18 KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B—88







100-YR 2-HR 100-YR 24-HR

> JUNCTION 24 HWY 83 BRIDGE

FUTURE CONDITIONS HYDROGRAPHS
AT SELECT LOCATIONS
100-YEAR

APPENDIX B— HYDROLOGIC RESULTS— FUTURE HYDROGRAPHS 100—YR J—24 KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B—89



FLOWS COMPARISON FOR 2 HOUR STORM EVENT BY RIVER STATION

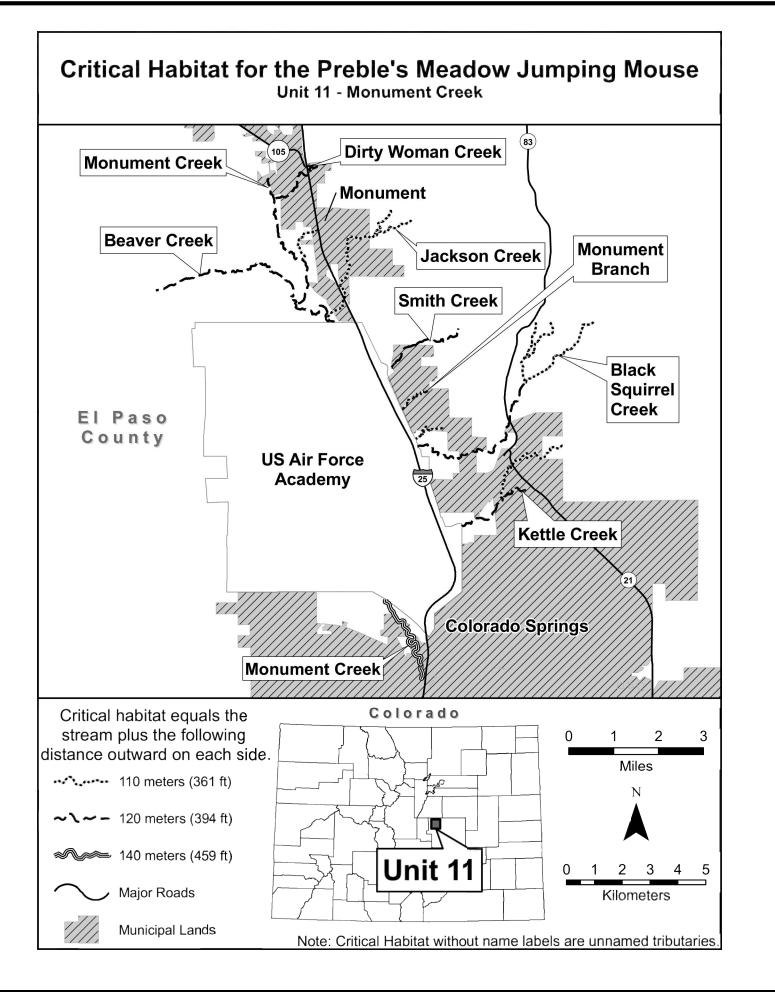
| HEC-HIVIS | HEC-RAS | | | Historic F | lows (cfs) | | | | | Existing F | lows (cfs) | | | | | Future F | lows (cfs) | | |
|-------------|----------------------|--------|--------|------------|------------|---------|----------|--------|--------|------------|------------|---------|----------|--------|--------|----------|------------|---------|----------|
| | | 2 Year | 5 Year | 10 Year | 25 Year | 50 Year | 100 Year | 2 Year | 5 Year | 10 Year | 25 Year | 50 Year | 100 Year | 2 Year | 5 Year | 10 Year | 25 Year | 50 Year | 100 Year |
| Junction | Cross Section | Event | Event | Event | Event | Event | Event | Event | Event | Event | Event | Event | Event | Event | Event | Event | Event | Event | Event |
| Junction-14 | 253+00 | 59 | 101 | 117 | 145 | 193 | 269 | 756 | 1,473 | 1,831 | 2,286 | 2,757 | 3,281 | 756 | 1,473 | 1,831 | 2,286 | 2,757 | 3,281 |
| Junction-15 | 237+50 | 60 | 102 | 118 | 147 | 197 | 274 | 769 | 1,488 | 1,850 | 2,309 | 2,786 | 3,314 | 771 | 1,490 | 1,852 | 2,311 | 2,788 | 3,317 |
| Junction-16 | 217+50 | 61 | 102 | 118 | 148 | 197 | 274 | 776 | 1,487 | 1,849 | 2,308 | 2,784 | 3,313 | 782 | 1,490 | 1,851 | 2,311 | 2,788 | 3,316 |
| Junction-17 | 203+00 | 61 | 102 | 118 | 148 | 197 | 274 | 780 | 1,487 | 1,849 | 2,307 | 2,784 | 3,312 | 786 | 1,489 | 1,852 | 2,311 | 2,787 | 3,316 |
| Junction-18 | 169+00 | 61 | 102 | 118 | 148 | 197 | 274 | 780 | 1,486 | 1,847 | 2,305 | 2,780 | 3,308 | 790 | 1,488 | 1,850 | 2,308 | 2,784 | 3,312 |
| Junction-19 | 120+75 | 61 | 102 | 118 | 147 | 197 | 274 | 780 | 1,484 | 1,845 | 2,303 | 2,778 | 3,305 | 789 | 1,487 | 1,848 | 2,306 | 2,782 | 3,309 |
| Junction-23 | 106+50 | 62 | 102 | 118 | 148 | 197 | 274 | 800 | 1,484 | 1,845 | 2,302 | 2,777 | 3,305 | 823 | 1,487 | 1,848 | 2,306 | 2,782 | 3,310 |
| Junction-24 | 87+50 | 62 | 101 | 118 | 147 | 197 | 274 | 800 | 1,482 | 1,842 | 2,298 | 2,772 | 3,298 | 824 | 1,486 | 1,846 | 2,303 | 2,777 | 3,304 |

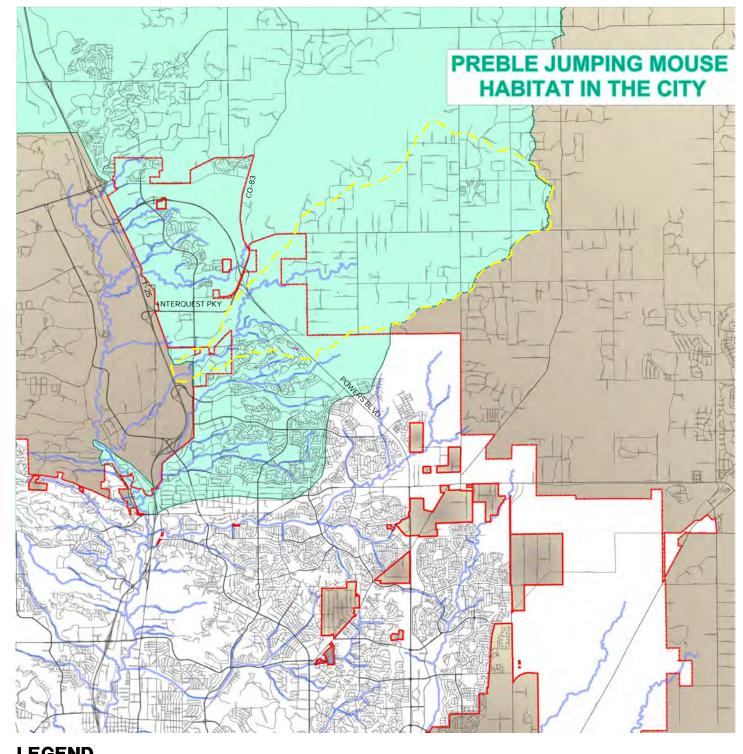
FLOWS COMPARISON FOR 24 HOUR STORM EVENT BY RIVER STATION

| HEC-HIMS | HEC-RAS | | | Historic F | lows (cfs) | | | | | Existing F | lows (cfs) | | | | | Future Fl | ows (cfs) | | |
|-------------|----------------------|--------|--------|------------|------------|---------|----------|--------|--------|------------|------------|---------|----------|--------|--------|-----------|-----------|---------|----------|
| | | 2 Year | 5 Year | 10 Year | 25 Year | 50 Year | 100 Year | 2 Year | 5 Year | 10 Year | 25 Year | 50 Year | 100 Year | 2 Year | 5 Year | 10 Year | 25 Year | 50 Year | 100 Year |
| Junction | Cross Section | Event | Event | Event | Event | Event | Event | Event | Event | Event | Event | Event | Event | Event | Event | Event | Event | Event | Event |
| Junction-14 | 253+00 | 308 | 631 | 973 | 1,287 | 1,813 | 2,196 | 1,123 | 1,711 | 2,258 | 2,726 | 3,471 | 3,992 | 1,123 | 1,711 | 2,258 | 2,726 | 3,471 | 3,992 |
| Junction-15 | 237+50 | 317 | 641 | 987 | 1,307 | 1,844 | 2,234 | 1,144 | 1,745 | 2,304 | 2,781 | 3,540 | 4,069 | 1,146 | 1,747 | 2,306 | 2,784 | 3,543 | 4,072 |
| Junction-16 | 217+50 | 323 | 654 | 1,007 | 1,330 | 1,874 | 2,269 | 1,154 | 1,760 | 2,324 | 2,806 | 3,570 | 4,103 | 1,161 | 1,769 | 2,333 | 2,816 | 3,581 | 4,115 |
| Junction-17 | 203+00 | 327 | 661 | 1,015 | 1,339 | 1,882 | 2,276 | 1,149 | 1,752 | 2,312 | 2,793 | 3,557 | 4,091 | 1,157 | 1,761 | 2,323 | 2,805 | 3,571 | 4,105 |
| Junction-18 | 169+00 | 328 | 662 | 1,017 | 1,341 | 1,885 | 2,281 | 1,151 | 1,756 | 2,318 | 2,798 | 3,560 | 4,091 | 1,162 | 1,769 | 2,332 | 2,813 | 3,576 | 4,108 |
| Junction-19 | 120+75 | 329 | 662 | 1,012 | 1,333 | 1,869 | 2,259 | 1,145 | 1,748 | 2,310 | 2,791 | 3,553 | 4,086 | 1,157 | 1,763 | 2,326 | 2,807 | 3,571 | 4,104 |
| Junction-23 | 106+50 | 353 | 702 | 1,066 | 1,399 | 1,953 | 2,362 | 1,185 | 1,807 | 2,385 | 2,880 | 3,664 | 4,211 | 1,213 | 1,839 | 2,421 | 2,917 | 3,704 | 4,252 |
| Junction-24 | 87+50 | 354 | 705 | 1,073 | 1,410 | 1,972 | 2,381 | 1,186 | 1,808 | 2,385 | 2,877 | 3,658 | 4,202 | 1,219 | 1,845 | 2,426 | 2,921 | 3,705 | 4,250 |

APPENDIX B— HYDROLOGIC RESULTS COMPARISON KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B-90







LEGEND

CITY LIMITS KETTLE CREEK BASIN MOUSE HABITAT

EL PASO COUNTY

APPENDIX B- PREBLE JUMPING MOUSE HABITAT IN THE CITY KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B-91



J·R ENGINEERING

Centennial 303-740-9393 • Colorado Springs 719-593-2593

| Kettl | e Cree | k Drainag | | | | d Tributa | γ |
|----------|--------|-----------|-------|-----------|-------|-----------|-------|
| | | | | lopment I | Plan | | |
| | | | | orm data | | | |
| Time | Flow | Time | Flow | Time | Flow | Time | Flow |
| (hr min) | (CFS) | (hr min) | (CFS) | (hr min) | (CFS) | (hr min) | (CFS) |
| 0 | 0 | 915 | 1 | 1830 | 0 | 2730 | 11.9 |
| 15 | 0 | 930 | 1 | 1845 | 0 | 2745 | 11.4 |
| 30 | 0.1 | 945 | 1.1 | 1900 | 0 | 2800 | 11.1 |
| 45 | 0.2 | 1000 | 1.2 | 1915 | 0 | 2815 | 10.8 |
| 100 | 0.2 | 1015 | 1.2 | 1930 | 0 | 2830 | 10.7 |
| 115 | 0.3 | 1030 | 1.3 | 1945 | 0 | 2845 | 10.6 |
| 130 | 0.4 | 1045 | 1.5 | 2000 | 0 | 2900 | 10.3 |
| 145 | 0.4 | 1100 | 1.7 | 2015 | 0 | 2915 | 9.9 |
| 200 | 0.4 | 1115 | 2 | 2030 | 0 | 2930 | 9.5 |
| 215 | 0.4 | 1130 | 2.3 | 2045 | 0 | 2945 | 9 |
| 230 | 0.4 | 1145 | 5.9 | 2100 | 0 | 3000 | 8.8 |
| 245 | 0.4 | 1200 | 38.1 | 2115 | 0 | 3015 | 8.5 |
| 300 | 0.4 | 1215 | 68 | 2130 | 0 | 3030 | 8.3 |
| 315 | 0.5 | 1230 | 83.2 | 2145 | 0 | 3045 | 8.2 |
| 330 | 0.5 | 1245 | 86.5 | 2200 | 0 | 3100 | 8.2 |
| 345 | 0.4 | 1300 | 82 | 2215 | 0 | 3115 | 8.2 |
| 400 | 0.5 | 1315 | 72 | 2230 | 0 | 3130 | 8.1 |
| 415 | 0.5 | 1330 | 60.2 | 2245 | 0 | 3145 | 8.2 |
| 430 | 0.5 | 1345 | 50.2 | 2300 | 0 | 3200 | 8.2 |
| 445 | 0.5 | 1400 | 42.5 | 2315 | 1 | 3215 | 8.2 |
| 500 | 0.5 | 1415 | 36.3 | 2330 | 1 | 3230 | 8.3 |
| 515 | 0.5 | 1430 | 31.4 | 2345 | 1 | 3245 | 8.3 |
| 530 | 0.6 | 1445 | 27.4 | 2400 | 1 | 3300 | 7.5 |
| 545 | 0.6 | 1500 | 24.3 | 2415 | 1 | 3315 | 6.2 |
| 600 | 0.6 | 1515 | 21.9 | 2430 | 1 | 3330 | 4.8 |
| 615 | 0.6 | 1530 | 20 | 2445 | 1 | 3345 | 3.5 |
| 630 | 0.7 | 1545 | 18.5 | 2500 | 1 | 3400 | 2.4 |
| 645 | 0.7 | 1600 | 17.3 | 2515 | 1 | 3415 | 1.5 |
| 700 | 0.7 | 1615 | 16.5 | 2530 | 1 | 3430 | 1 |
| 715 | 0.7 | 1630 | 15.8 | 2545 | 1 | 3445 | 0.7 |
| 730 | 0.7 | 1645 | 15.2 | 2600 | 1 | 3500 | 0.4 |
| 745 | 0.7 | 1700 | 14.6 | 2615 | 1 | 3515 | 0.3 |
| 800 | 0.7 | 1715 | 14.1 | 2630 | 1 | 3530 | 0.2 |
| 815 | 0.8 | 1730 | 13.6 | 2645 | 1 | 3545 | 0.1 |
| 830 | 0.8 | 1745 | 13.3 | 2700 | 1 | 3600 | 0.1 |
| 845 | 0.9 | 1800 | 12.8 | 2715 | 1 | 3615 | 0.1 |
| 900 | 0.9 | 1815 | 12.4 | | | | |

APPENDIX B- MDDP 2-YR FLOW DATA KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B-92



| | | | | Kettl | e Cree | | | n Old Ran | | d Tributa | ry | | | | |
|------------------|------|-------------------|------|------------|--------|------------|-----------------|------------------|----------|--------------|------------|--------------|----------|------------------|----------|
| | | | | | | | | lopment | Plan | | | | | | |
| Timo | Flow | Timo | Flow | Time | Flow | 5 Y | /ear St Flow | orm data | Flow | Time | Flow | Time | Flow | Time | Flow |
| Time (hr min) | | Time (hr min) | | (hr min) | | (hr min) | (CFS) | Time (hr min) | | (hr min) | | (hr min) | | Time (hr min) | (CFS) |
| 0 | 0 | 154 | 0 | 345 | 0 | 539 | 1 | 730 | 83 | 924 | 65 | 1115 | 52 | 1306 | 43 |
| 3 | 0 | 157 | 0 | 348 | 0 | 542 | 2 | 733 | 81 | 927 | 65 | 1113 | 51 | 1309 | 43 |
| 6 | 0 | 200 | 0 | 351 | 0 | 545 | 4 | 736 | 80 | 930 | 65 | 1121 | 51 | 1312 | 42 |
| 9 | 0 | 203 | 0 | 354 | 0 | 548 | 8 | 739 | 79 | 933 | 65 | 1124 | 50 | 1315 | 42 |
| 12 | 0 | 206 | 0 | 357 | 0 | 551 | 13 | 742 | 77 | 936 | 65 | 1127 | 50 | 1318 | 42 |
| 15 | 0 | 209 | 0 | 400 | 0 | 554 | 21 | 745 | 76 | 939 | 65 | 1130 | 50 | 1321 | 42 |
| 18 | 0 | 212 | 0 | 403 | 0 | 557 | 29 | 748 | 75 | 942 | 64 | 1133 | 49 | 1324 | 42 |
| 21 | 0 | 215 | 0 | 406 | 0 | 600 | 38 | 751 | 74 | 945 | 64 | 1136 | 49 | 1327 | 42 |
| 24 | 0 | 218 | 0 | 409 | 0 | 603 | 46 | 754 | 74 | 948 | 63 | 1139 | 48 | 1330 | 42 |
| 27 | 0 | 221 | 0 | 412 | 0 | 606 | 48 | 757 | 73 | 951 | 63 | 1142 | 48 | 1333 | 42 |
| 30 | 0 | 224 | 0 | 415 | 0 | 609 | 46 | 800 | 73 | 954 | 62 | 1145 | 48 | 1336 | 41 |
| 33 | 0 | 227 | 0 | 418 | 0 | 612 | 43 | 803 | 72 | 957 | 62 | 1148 | 47 | 1339 | 41 |
| 36 | 0 | 230 | 0 | 421 | 0 | 615 | 41 | 806 | 72 | 1000 | 61 | 1151 | 47 | 1342 | 41 |
| 39 | 0 | 233 | 0 | 424 | 0 | 618 | 40 | 809 | 71 | 1003 | 61 | 1154 | 47 | 1345 | 41 |
| 42 | 0 | 236 | 0 | 427 | 0 | 621 | 40 | 812 | 71 | 1006 | 60 | 1157 | 46 | 1348 | 41 |
| 45 | 0 | 239 | 0 | 430 | 0 | 624 | 60 | 815 | 70 | 1009 | 60 | 1200 | 46 | 1351 | 41 |
| 48 | 0 | 242 | 0 | 433 | 0 | 627 | 91 | 818 | 69 | 1012 | 60 | 1203 | 46 | 1354 | 41 |
| 51 | 0 | 245 | 0 | 436 | 0 | 630 | 98 | 821 | 69 | 1015 | 59 | 1206 | 45 | 1357 | 40 |
| 54 | 0 | 248 | 0 | 439 | 0 | 633 | 104 | 824 | 68 | 1018 | 59 | 1209 | 45 | 1400 | 40 |
| 57 | 0 | 251 | 0 | 442 | 0 | 636 | 110 | 827 | 67 | 1021 | 59 | 1212 | 44 | 1403 | 40 |
| 100 | 0 | 254 | 0 | 445 | 0 | 639 | 108 | 830 | 67 | 1024 | 58 | 1215 | 44 | 1406 | 40 |
| 103 | 0 | 257 | 0 | 448 | 0 | 642 | 111 | 833 | 66 | 1027 | 58 | 1218 | 44 | 1409 | 40 |
| 106 | 0 | 300 | 0 | 451 | 0 | 645 | 109 | 836 | 65 | 1030 | 58 | 1221 | 44 | 1412 | 40 |
| 109 | 0 | 303 | 0 | 454 | 0 | 648 | 108 | 839 | 64 | 1033 | 57 | 1224 | 44 | 1415 | 39 |
| 112 | 0 | 306 | 0 | 457 | 0 | 651 | 107 | 842 | 63 | 1036 | 57 | 1227 | 44 | 1418 | 39 |
| 115 | 0 | 309 | 0 | 500 | 0 | 654 | 105 | 845 | 62 | 1039 | 56 | 1230 | 44 | 1421 | 39 |
| 118 | 0 | 312 | 0 | 503 | 0 | 657 | 104 | 848 | 61 | 1042 | 56 | 1233 | 44 | 1424 | 39 |
| 121 | 0 | 315 | 0 | 506 | 0 | 700 | 101 | 851 | 61 | 1045 | 56 | 1236 | 43 | 1427 | 39 |
| 124 | 0 | 318 | 0 | 509 | 0 | 703 | 99 | 854 | 60 | 1048 | 55 | 1239 | 43 | 1430 | 38 |
| 127 | 0 | 321 | 0 | 512 | 0 | 706 | 97 | 857 | 59 | 1051 | 55 | 1242 | 43 | 1433 | 38 |
| 130 | 0 | 324 | 0 | 515 | 0 | 709 | 95 | 900 | 58 | 1054 | 54 | 1245 | 43 | 1436 | 38 |
| 133 136 | 0 | 327 330 | 0 | 518 521 | 1 | 712 715 | 92 91 | 903 906 | 59 60 | 1057 1100 | 54 54 | 1248 1251 | 43 43 | 1439 1442 | 38 38 |
| 139 | 0 | 333 | 0 | 521 | 1 | 718 | 89 | 909 | 62 | 1100 | 53 | 1251 | 43 | 1442 | 38 |
| 142 | 0 | 336 | 0 | 527 | 1 | 721 | 87 | 909 | 63 | 1103 | 53 | 1254 | 43 | 1445 | 37 |
| 145 | 0 | 339 | 0 | 530 | 1 | 721 | 86 | 915 | 64 | 1100 | 52 | 1300 | 43 | 1451 | 37 |
| 143 | 0 | 342 | 0 | 533 | 1 | 727 | 84 | 918 | 64 | 1112 | 52 | 1303 | 43 | 1451 | 37 |
| 151 | 0 | J -1 2 | - | 536 | 1 | , 21 | 04 | 921 | 65 | 1112 | J <u>Z</u> | 1303 | 73 | 1457 | 37 |

5 YR EXISTING AND FUTURE FLOW DATA FOR JUNCTION 22 (MPPD JUNCTION 24)

APPENDIX B- MDDP 5-YR FLOW DATA KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B-93



| | | | | Kettl | e Cree | k Drainag | e Basii | n Old Ran | ch Roa | d Tributa | ry | | | | |
|----------|-------|----------|-------|----------|--------|-----------|---------|-----------|--------|-----------|-------|----------|-------|----------|-------|
| | | | | | | Maste | r Deve | lopment | Plan | | | | | | |
| | | | | | | | | orm data | | | | | | | |
| Time | Flow | Time | Flow | Time | Flow | Time | Flow | Time | Flow | Time | Flow | Time | Flow | Time | Flow |
| (hr min) | (CFS) | (hr min) | (CFS) | (hr min) | (CFS) | (hr min) | (CFS) | (hr min) | (CFS) | (hr min) | (CFS) | (hr min) | (CFS) | (hr min) | (CFS) |
| 0 | 0 | 154 | 0 | 345 | 0 | 539 | 1 | 730 | 113 | 924 | 84 | 1115 | 59 | 1306 | 47 |
| 3 | 0 | 157 | 0 | 348 | 0 | 542 | 3 | 733 | 111 | 927 | 83 | 1118 | 59 | 1309 | 46 |
| 6 | 0 | 200 | 0 | 351 | 0 | 545 | 7 | 736 | 109 | 930 | 82 | 1121 | 59 | 1312 | 46 |
| 9 | 0 | 203 | 0 | 354 | 0 | 548 | 13 | 739 | 107 | 933 | 81 | 1124 | 58 | 1315 | 46 |
| 12 | 0 | 206 | 0 | 357 | 0 | 551 | 21 | 742 | 105 | 936 | 80 | 1127 | 58 | 1318 | 45 |
| 15 | 0 | 209 | 0 | 400 | 0 | 554 | 32 | 745 | 103 | 939 | 79 | 1130 | 58 | 1321 | 45 |
| 18 | 0 | 212 | 0 | 403 | 0 | 557 | 42 | 748 | 102 | 942 | 78 | 1133 | 57 | 1324 | 45 |
| 21 | 0 | 215 | 0 | 406 | 0 | 600 | 53 | 751 | 100 | 945 | 77 | 1136 | 57 | 1327 | 44 |
| 24 | 0 | 218 | 0 | 409 | 0 | 603 | 58 | 754 | 99 | 948 | 77 | 1139 | 56 | 1330 | 44 |
| 27 | 0 | 221 | 0 | 412 | 0 | 606 | 58 | 757 | 97 | 951 | 76 | 1142 | 56 | 1333 | 44 |
| 30 | 0 | 224 | 0 | 415 | 0 | 609 | 55 | 800 | 96 | 954 | 76 | 1145 | 56 | 1336 | 44 |
| 33 | 0 | 227 | 0 | 418 | 0 | 612 | 50 | 803 | 95 | 957 | 75 | 1148 | 55 | 1339 | 44 |
| 36 | 0 | 230 | 0 | 421 | 0 | 615 | 48 | 806 | 97 | 1000 | 75 | 1151 | 55 | 1342 | 44 |
| 39 | 0 | 233 | 0 | 424 | 0 | 618 | 86 | 809 | 99 | 1003 | 74 | 1154 | 55 | 1345 | 44 |
| 42 | 0 | 236 | 0 | 427 | 0 | 621 | 161 | 812 | 100 | 1006 | 74 | 1157 | 54 | 1348 | 44 |
| 45 | 0 | 239 | 0 | 430 | 0 | 624 | 177 | 815 | 101 | 1009 | 73 | 1200 | 54 | 1351 | 44 |
| 48 | 0 | 242 | 0 | 433 | 0 | 627 | 184 | 818 | 101 | 1012 | 72 | 1203 | 53 | 1354 | 43 |
| 51 | 0 | 245 | 0 | 436 | 0 | 630 | 188 | 821 | 101 | 1015 | 72 | 1206 | 53 | 1357 | 43 |
| 54 | 0 | 248 | 0 | 439 | 0 | 633 | 186 | 824 | 101 | 1018 | 71 | 1209 | 53 | 1400 | 43 |
| 57 | 0 | 251 | 0 | 442 | 0 | 636 | 187 | 827 | 101 | 1021 | 70 | 1212 | 52 | 1403 | 43 |
| 100 | 0 | 254 | 0 | 445 | 0 | 639 | 184 | 830 | 100 | 1024 | 70 | 1215 | 52 | 1406 | 43 |
| 103 | 0 | 257 | 0 | 448 | 0 | 642 | 182 | 833 | 99 | 1027 | 69 | 1218 | 52 | 1409 | 43 |
| 106 | 0 | 300 | 0 | 451 | 0 | 645 | 179 | 836 | 99 | 1030 | 68 | 1221 | 51 | 1412 | 43 |
| 109 | 0 | 303 | 0 | 454 | 0 | 648 | 175 | 839 | 98 | 1033 | 67 | 1224 | 51 | 1415 | 43 |
| 112 | 0 | 306 | 0 | 457 | 0 | 651 | 171 | 842 | 98 | 1036 | 67 | 1227 | 51 | 1418 | 43 |
| 115 | 0 | 309 | 0 | 500 | 1 | 654 | 164 | 845 | 97 | 1039 | 66 | 1230 | 50 | 1421 | 43 |
| 118 | 0 | 312 | 0 | 503 | 1 | 657 | 158 | 848 | 96 | 1042 | 65 | 1233 | 50 | 1424 | 43 |
| 121 | 0 | 315 | 0 | 506 | 1 | 700 | 152 | 851 | 95 | 1045 | 64 | 1236 | 50 | 1427 | 43 |
| 124 | 0 | 318 | 0 | 509 | 1 | 703 | 147 | 854 | 94 | 1048 | 64 | 1239 | 49 | 1430 | 42 |
| 127 | 0 | 321 | 0 | 512 | 1 | 706 | 141 | 857 | 93 | 1051 | 63 | 1242 | 49 | 1433 | 42 |
| 130 | 0 | 324 | 0 | 515 | 1 | 709 | 137 | 900 | 92 | 1054 | 62 | 1245 | 49 | 1436 | 42 |
| 133 | 0 | 327 | 0 | 518 | 1 | 712 | 133 | 903 | 91 | 1057 | 61 | 1248 | 48 | 1439 | 42 |
| 136 | 0 | 330 | 0 | 521 | 1 | 715 | 128 | 906 | 90 | 1100 | 61 | 1251 | 48 | 1442 | 42 |
| 139 | 0 | 333 | 0 | 524 | 1 | 718 | 125 | 909 | 89 | 1103 | 61 | 1254 | 48 | 1445 | 42 |
| 142 | 0 | 336 | 0 | 527 | 1 | 721 | 121 | 912 | 88 | 1106 | 60 | 1257 | 48 | 1448 | 42 |
| 145 | 0 | 339 | 0 | 530 | 1 | 724 | 118 | 915 | 87 | 1109 | 60 | 1300 | 47 | 1451 | 42 |
| 148 | 0 | 342 | 0 | 533 | 1 | 727 | 115 | 918 | 86 | 1112 | 60 | 1303 | 47 | 1454 | 41 |
| 151 | 0 | | | 536 | 1 | | | 921 | 85 | | | | | 1457 | 41 |

APPENDIX B- MDDP 10-YR FLOW DATA KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B-94



| | | | | Kettl | e Cree | k Drainag | e Basiı | n Old Ran | ch Roa | d Tributa | ry | | | | |
|----------|-------|----------|-------|----------|--------|-----------|---------|-----------|--------|-----------|-------|----------|-------|----------|-------|
| | | | | | | Maste | r Deve | lopment l | Plan | | | | | | |
| | | | | | | | _ | orm data | | | | | | | |
| Time | Flow | Time | Flow | Time | Flow | Time | Flow | Time | Flow | Time | Flow | Time | Flow | Time | Flow |
| (hr min) | (CFS) | (hr min) | (CFS) | (hr min) | (CFS) | • | · / | (hr min) | ` ' | (hr min) | (CFS) | (hr min) | (CFS) | (hr min) | (CFS) |
| 0 | 0 | 154 | 0 | 345 | 0 | 539 | 2 | 730 | 187 | 924 | 104 | 1115 | 75 | 1306 | 58 |
| 3 | 0 | 157 | 0 | 348 | 0 | 542 | 7 | 733 | 182 | 927 | 103 | 1118 | 75 | 1309 | 58 |
| 6 | 0 | 200 | 0 | 351 | 0 | 545 | 13 | 736 | 177 | 930 | 102 | 1121 | 74 | 1312 | 58 |
| 9 | 0 | 203 | 0 | 354 | 0 | 548 | 23 | 739 | 173 | 933 | 102 | 1124 | 74 | 1315 | 57 |
| 12 | 0 | 206 | 0 | 357 | 0 | 551 | 36 | 742 | 169 | 936 | 101 | 1127 | 73 | 1318 | 57 |
| 15 | 0 | 209 | 0 | 400 | 0 | 554 | 50 | 745 | 165 | 939 | 100 | 1130 | 73 | 1321 | 57 |
| 18 | 0 | 212 | 0 | 403 | 0 | 557 | 61 | 748 | 162 | 942 | 100 | 1133 | 72 | 1324 | 56 |
| 21 | 0 | 215 | 0 | 406 | 0 | 600 | 70 | 751 | 159 | 945 | 99 | 1136 | 72 | 1327 | 56 |
| 24 | 0 | 218 | 0 | 409 | 0 | 603 | 75 | 754 | 156 | 948 | 98 | 1139 | 71 | 1330 | 55 |
| 27 | 0 | 221 | 0 | 412 | 0 | 606 | 74 | 757 | 154 | 951 | 98 | 1142 | 70 | 1333 | 55 |
| 30 | 0 | 224 | 0 | 415 | 0 | 609 | 68 | 800 | 152 | 954 | 97 | 1145 | 70 | 1336 | 55 |
| 33 | 0 | 227 | 0 | 418 | 0 | 612 | 105 | 803 | 151 | 957 | 96 | 1148 | 69 | 1339 | 54 |
| 36 | 0 | 230 | 0 | 421 | 0 | 615 | 234 | 806 | 149 | 1000 | 95 | 1151 | 69 | 1342 | 54 |
| 39 | 0 | 233 | 0 | 424 | 0 | 618 | 275 | 809 | 147 | 1003 | 95 | 1154 | 68 | 1345 | 54 |
| 42 | 0 | 236 | 0 | 427 | 0 | 621 | 308 | 812 | 145 | 1006 | 94 | 1157 | 68 | 1348 | 53 |
| 45 | 0 | 239 | 0 | 430 | 0 | 624 | 348 | 815 | 143 | 1009 | 93 | 1200 | 67 | 1351 | 53 |
| 48 | 0 | 242 | 0 | 433 | 0 | 627 | 345 | 818 | 141 | 1012 | 92 | 1203 | 66 | 1354 | 53 |
| 51 | 0 | 245 | 0 | 436 | 0 | 630 | 333 | 821 | 139 | 1015 | 92 | 1206 | 66 | 1357 | 52 |
| 54 | 0 | 248 | 0 | 439 | 0 | 633 | 324 | 824 | 137 | 1018 | 91 | 1209 | 65 | 1400 | 52 |
| 57 | 0 | 251 | 0 | 442 | 1 | 636 | 303 | 827 | 135 | 1021 | 90 | 1212 | 64 | 1403 | 52 |
| 100 | 0 | 254 | 0 | 445 | 1 | 639 | 289 | 830 | 132 | 1024 | 89 | 1215 | 64 | 1406 | 52 |
| 103 | 0 | 257 | 0 | 448 | 1 | 642 | 273 | 833 | 130 | 1027 | 88 | 1218 | 63 | 1409 | 51 |
| 106 | 0 | 300 | 0 | 451 | 1 | 645 | 264 | 836 | 128 | 1030 | 87 | 1221 | 63 | 1412 | 51 |
| 109 | 0 | 303 | 0 | 454 | 1 | 648 | 254 | 839 | 126 | 1033 | 86 | 1224 | 62 | 1415 | 51 |
| 112 | 0 | 306 | 0 | 457 | 1 | 651 | 242 | 842 | 123 | 1036 | 85 | 1227 | 62 | 1418 | 50 |
| 115 | 0 | 309 | 0 | 500 | 1 | 654 | 233 | 845 | 121 | 1039 | 85 | 1230 | 62 | 1421 | 50 |
| 118 | 0 | 312 | 0 | 503 | 1 | 657 | 227 | 848 | 119 | 1042 | 84 | 1233 | 61 | 1424 | 50 |
| 121 | 0 | 315 | 0 | 506 | 1 | 700 | 221 | 851 | 118 | 1045 | 83 | 1236 | 61 | 1427 | 49 |
| 124 | 0 | 318 | 0 | 509 | 1 | 703 | 219 | 854 | 116 | 1048 | 82 | 1239 | 61 | 1430 | 49 |
| 127 | 0 | 321 | 0 | 512 | 1 | 706 | 217 | 857 | 114 | 1051 | 81 | 1242 | 61 | 1433 | 49 |
| 130 | 0 | 324 | 0 | 515 | 1 | 709 | 215 | 900 | 113 | 1054 | 80 | 1245 | 60 | 1436 | 49 |
| 133 | 0 | 327 | 0 | 518 | 1 | 712 | 212 | 903 | 111 | 1057 | 79 | 1248 | 60 | 1439 | 48 |
| 136 | 0 | 330 | 0 | 521 | 1 | 715 | 210 | 906 | 110 | 1100 | 78 | 1251 | 60 | 1442 | 48 |
| 139 | 0 | 333 | 0 | 524 | 1 | 718 | 207 | 909 | 109 | 1103 | 77 | 1254 | 60 | 1445 | 48 |
| 142 | 0 | 336 | 0 | 527 | 1 | 721 | 204 | 912 | 107 | 1106 | 77 | 1257 | 59 | 1448 | 47 |
| 145 | 0 | 339 | 0 | 530 | 1 | 724 | 199 | 915 | 106 | 1109 | 76 | 1300 | 59 | 1451 | 47 |
| 148 | 0 | 342 | 0 | 533 | 1 | 727 | 192 | 918 | 106 | 1112 | 76 | 1303 | 59 | 1454 | 47 |
| 151 | 0 | | | 536 | 1 | | | 921 | 105 | | | | | 1457 | 47 |

APPENDIX B- MDDP 25-YR FLOW DATA KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B-95



25 YR EXISTING AND FUTURE FLOW DATA FOR JUNCTION 22 (MPPD JUNCTION 24)

| | | | | Kettl | e Cree | k Drainag | e Basi | n Old Ran | ch Roa | d Tributa | ry | | | | |
|----------|-------|----------|-------|----------|--------|-----------|--------|-----------|--------|-----------|-------|----------|-------|----------|-------|
| | | | | | | Maste | r Deve | lopment I | Plan | | | | | | |
| | | | | | | 50 | year S | orm data | | | | | | | |
| Time | Flow | Time | Flow | Time | Flow | Time | Flow | Time | Flow | Time | Flow | Time | Flow | Time | Flow |
| (hr min) | (CFS) | (hr min) | (CFS) | (hr min) | (CFS) | (hr min) | (CFS) | (hr min) | (CFS) | (hr min) | (CFS) | (hr min) | (CFS) | (hr min) | (CFS) |
| 0 | 0 | 154 | 0 | 345 | 0 | 539 | 4 | 730 | 222 | 924 | 116 | 1115 | 89 | 1306 | 67 |
| 3 | 0 | 157 | 0 | 348 | 0 | 542 | 9 | 733 | 217 | 927 | 115 | 1118 | 88 | 1309 | 67 |
| 6 | 0 | 200 | 0 | 351 | 0 | 545 | 18 | 736 | 211 | 930 | 114 | 1121 | 87 | 1312 | 66 |
| 9 | 0 | 203 | 0 | 354 | 0 | 548 | 32 | 739 | 204 | 933 | 113 | 1124 | 86 | 1315 | 66 |
| 12 | 0 | 206 | 0 | 357 | 0 | 551 | 47 | 742 | 198 | 936 | 112 | 1127 | 86 | 1318 | 65 |
| 15 | 0 | 209 | 0 | 400 | 0 | 554 | 61 | 745 | 194 | 939 | 111 | 1130 | 85 | 1321 | 64 |
| 18 | 0 | 212 | 0 | 403 | 0 | 557 | 72 | 748 | 188 | 942 | 110 | 1133 | 84 | 1324 | 63 |
| 21 | 0 | 215 | 0 | 406 | 0 | 600 | 81 | 751 | 185 | 945 | 110 | 1136 | 83 | 1327 | 63 |
| 24 | 0 | 218 | 0 | 409 | 0 | 603 | 87 | 754 | 180 | 948 | 109 | 1139 | 83 | 1330 | 63 |
| 27 | 0 | 221 | 0 | 412 | 0 | 606 | 85 | 757 | 177 | 951 | 108 | 1142 | 82 | 1333 | 62 |
| 30 | 0 | 224 | 0 | 415 | 0 | 609 | 113 | 800 | 174 | 954 | 107 | 1145 | 81 | 1336 | 62 |
| 33 | 0 | 227 | 0 | 418 | 0 | 612 | 276 | 803 | 171 | 957 | 107 | 1148 | 81 | 1339 | 62 |
| 36 | 0 | 230 | 0 | 421 | 0 | 615 | 384 | 806 | 168 | 1000 | 106 | 1151 | 80 | 1342 | 62 |
| 39 | 0 | 233 | 0 | 424 | 0 | 618 | 455 | 809 | 165 | 1003 | 106 | 1154 | 79 | 1345 | 61 |
| 42 | 0 | 236 | 0 | 427 | 0 | 621 | 501 | 812 | 163 | 1006 | 105 | 1157 | 78 | 1348 | 61 |
| 45 | 0 | 239 | 0 | 430 | 0 | 624 | 476 | 815 | 160 | 1009 | 105 | 1200 | 78 | 1351 | 61 |
| 48 | 0 | 242 | 0 | 433 | 0 | 627 | 476 | 818 | 157 | 1012 | 104 | 1203 | 77 | 1354 | 60 |
| 51 | 0 | 245 | 0 | 436 | 1 | 630 | 459 | 821 | 155 | 1015 | 103 | 1206 | 77 | 1357 | 60 |
| 54 | 0 | 248 | 0 | 439 | 1 | 633 | 431 | 824 | 153 | 1018 | 103 | 1209 | 77 | 1400 | 60 |
| 57 | 0 | 251 | 0 | 442 | 1 | 636 | 414 | 827 | 150 | 1021 | 102 | 1212 | 76 | 1403 | 59 |
| 100 | 0 | 254 | 0 | 445 | 1 | 639 | 380 | 830 | 147 | 1024 | 101 | 1215 | 76 | 1406 | 59 |
| 103 | 0 | 257 | 0 | 448 | 1 | 642 | 359 | 833 | 145 | 1027 | 101 | 1218 | 75 | 1409 | 59 |
| 106 | 0 | 300 | 0 | 451 | 1 | 645 | 334 | 836 | 142 | 1030 | 100 | 1221 | 75 | 1412 | 58 |
| 109 | 0 | 303 | 0 | 454 | 1 | 648 | 317 | 839 | 140 | 1033 | 99 | 1224 | 74 | 1415 | 58 |
| 112 | 0 | 306 | 0 | 457 | 1 | 651 | 300 | 842 | 138 | 1036 | 98 | 1227 | 74 | 1418 | 58 |
| 115 | 0 | 309 | 0 | 500 | 1 | 654 | 291 | 845 | 136 | 1039 | 98 | 1230 | 73 | 1421 | 57 |
| 118 | 0 | 312 | 0 | 503 | 1 | 657 | 282 | 848 | 134 | 1042 | 97 | 1233 | 73 | 1424 | 57 |
| 121 | 0 | 315 | 0 | 506 | 1 | 700 | 272 | 851 | 132 | 1045 | 96 | 1236 | 72 | 1427 | 57 |
| 124 | 0 | 318 | 0 | 509 | 1 | 703 | 263 | 854 | 130 | 1048 | 95 | 1239 | 72 | 1430 | 56 |
| 127 | 0 | 321 | 0 | 512 | 1 | 706 | 256 | 857 | 128 | 1051 | 95 | 1242 | 72 | 1433 | 56 |
| 130 | 0 | 324 | 0 | 515 | 1 | 709 | 248 | 900 | 126 | 1054 | 94 | 1245 | 71 | 1436 | 56 |
| 133 | 0 | 327 | 0 | 518 | 1 | 712 | 244 | 903 | 125 | 1057 | 93 | 1248 | 71 | 1439 | 55 |
| 136 | 0 | 330 | 0 | 521 | 1 | 715 | 241 | 906 | 123 | 1100 | 92 | 1251 | 70 | 1442 | 55 |
| 139 | 0 | 333 | 0 | 524 | 1 | 718 | 238 | 909 | 122 | 1103 | 92 | 1254 | 70 | 1445 | 55 |
| 142 | 0 | 336 | 0 | 527 | 1 | 721 | 233 | 912 | 121 | 1106 | 91 | 1257 | 69 | 1448 | 55 |
| 145 | 0 | 339 | 0 | 530 | 1 | 724 | 230 | 915 | 119 | 1109 | 90 | 1300 | 69 | 1451 | 54 |
| 148 | 0 | 342 | 0 | 533 | 1 | 727 | 226 | 918 | 118 | 1112 | 89 | 1303 | 68 | 1454 | 54 |
| 151 | 0 | | | 536 | 1 | | | 921 | 117 | | | | | 1457 | 54 |

APPENDIX B- MDDP 50-YR FLOW DATA KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B-96



50 YR EXISTING AND FUTURE FLOW DATA FOR JUNCTION 22 (MPPD JUNCTION 24)

| | | | | Kettl | e Cree | k Drainag | e Basi | n Old Ran | ch Roa | d Tributa | ry | | | | |
|----------|-------|------|-------|-------|--------|-----------|--------|-----------|--------|-----------|------|----------|------|----------|-------|
| | | | | | | | | lopment l | | | | | | | |
| | | | | | | | | torm data | | | | | | | |
| Time | Flow | Time | Flow | Time | Flow | Time | Flow | Time | Flow | Time | Flow | Time | Flow | Time | Flow |
| (hr min) | (CFS) | • | (CFS) | · | , , | | · · | (hr min) | (CFS) | ` ' | | (hr min) | ` , | (hr min) | (CFS) |
| 0 | 0 | 154 | 0 | 345 | 0 | 539 | 6 | 730 | 243 | 924 | 128 | 1115 | 100 | 1306 | 67 |
| 3 | 0 | 157 | 0 | 348 | 0 | 542 | 13 | 733 | 239 | 927 | 127 | 1118 | 99 | 1309 | 78 |
| 6 | 0 | 200 | 0 | 351 | 0 | 545 | 25 | 736 | 234 | 930 | 126 | 1121 | 99 | 1312 | 77 |
| 9 | 0 | 203 | 0 | 354 | 0 | 548 | 41 | 739 | 230 | 933 | 125 | 1124 | 98 | 1315 | 77 |
| 12 | 0 | 206 | 0 | 357 | 0 | 551 | 59 | 742 | 226 | 936 | 124 | 1127 | 98 | 1318 | 77 |
| 15 | 0 | 209 | 0 | 400 | 0 | 554 | 71 | 745 | 222 | 939 | 124 | 1130 | 97 | 1321 | 76 |
| 18 | 0 | 212 | 0 | 403 | 0 | 557 | 83 | 748 | 216 | 942 | 123 | 1133 | 97 | 1324 | 76 |
| 21 | 0 | 215 | 0 | 406 | 0 | 600 | 94 | 751 | 210 | 945 | 122 | 1136 | 96 | 1327 | 75 |
| 24 | 0 | 218 | 0 | 409 | 0 | 603 | 100 | 754 | 205 | 948 | 121 | 1139 | 96 | 1330 | 75 |
| 27 | 0 | 221 | 0 | 412 | 0 | 606 | 114 | 757 | 201 | 951 | 120 | 1142 | 95 | 1333 | 74 |
| 30 | 0 | 224 | 0 | 415 | 0 | 609 | 297 | 800 | 197 | 954 | 120 | 1145 | 94 | 1336 | 73 |
| 33 | 0 | 227 | 0 | 418 | 0 | 612 | 453 | 803 | 193 | 957 | 119 | 1148 | 94 | 1339 | 73 |
| 36 | 0 | 230 | 0 | 421 | 0 | 615 | 571 | 806 | 189 | 1000 | 118 | 1151 | 93 | 1342 | 72 |
| 39 | 0 | 233 | 0 | 424 | 0 | 618 | 626 | 809 | 186 | 1003 | 118 | 1154 | 93 | 1345 | 72 |
| 42 | 0 | 236 | 0 | 427 | 1 | 621 | 612 | 812 | 182 | 1006 | 117 | 1157 | 92 | 1348 | 71 |
| 45 | 0 | 239 | 0 | 430 | 1 | 624 | 630 | 815 | 179 | 1009 | 116 | 1200 | 92 | 1351 | 71 |
| 48 | 0 | 242 | 0 | 433 | 1 | 627 | 589 | 818 | 175 | 1012 | 115 | 1203 | 91 | 1354 | 70 |
| 51 | 0 | 245 | 0 | 436 | 1 | 630 | 576 | 821 | 172 | 1015 | 115 | 1206 | 90 | 1357 | 70 |
| 54 | 0 | 248 | 0 | 439 | 1 | 633 | 539 | 824 | 168 | 1018 | 114 | 1209 | 90 | 1400 | 69 |
| 57 | 0 | 251 | 0 | 442 | 1 | 636 | 515 | 827 | 165 | 1021 | 113 | 1212 | 89 | 1403 | 69 |
| 100 | 0 | 254 | 0 | 445 | 1 | 639 | 485 | 830 | 161 | 1024 | 112 | 1215 | 89 | 1406 | 68 |
| 103 | 0 | 257 | 0 | 448 | 1 | 642 | 458 | 833 | 158 | 1027 | 111 | 1218 | 88 | 1409 | 67 |
| 106 | 0 | 300 | 0 | 451 | 1 | 645 | 427 | 836 | 155 | 1030 | 110 | 1221 | 87 | 1412 | 67 |
| 109 | 0 | 303 | 0 | 454 | 1 | 648 | 395 | 839 | 153 | 1033 | 109 | 1224 | 87 | 1415 | 66 |
| 112 | 0 | 306 | 0 | 457 | 1 | 651 | 367 | 842 | 151 | 1036 | 108 | 1227 | 86 | 1418 | 65 |
| 115 | 0 | 309 | 0 | 500 | 1 | 654 | 346 | 845 | 148 | 1039 | 107 | 1230 | 85 | 1421 | 65 |
| 118 | 0 | 312 | 0 | 503 | 1 | 657 | 327 | 848 | 146 | 1042 | 107 | 1233 | 85 | 1424 | 64 |
| 121 | 0 | 315 | 0 | 506 | 1 | 700 | 316 | 851 | 144 | 1045 | 106 | 1236 | 84 | 1427 | 63 |
| 124 | 0 | 318 | 0 | 509 | 1 | 703 | 306 | 854 | 142 | 1048 | 105 | 1239 | 84 | 1430 | 63 |
| 127 | 0 | 321 | 0 | 512 | 1 | 706 | 295 | 857 | 141 | 1051 | 105 | 1242 | 83 | 1433 | 63 |
| 130 | 0 | 324 | 0 | 515 | 1 | 709 | 285 | 900 | 139 | 1054 | 104 | 1245 | 82 | 1436 | 63 |
| 133 | 0 | 327 | 0 | 518 | 1 | 712 | 276 | 903 | 137 | 1057 | 103 | 1248 | 82 | 1439 | 62 |
| 136 | 0 | 330 | 0 | 521 | 1 | 715 | 268 | 906 | 136 | 1100 | 103 | 1251 | 81 | 1442 | 62 |
| 139 | 0 | 333 | 0 | 524 | 1 | 718 | 261 | 909 | 134 | 1103 | 102 | 1254 | 81 | 1445 | 62 |
| 142 | 0 | 336 | 0 | 527 | 1 | 721 | 256 | 912 | 133 | 1106 | 102 | 1257 | 80 | 1448 | 61 |
| 145 | 0 | 339 | 0 | 530 | 1 | 724 | 252 | 915 | 132 | 1109 | 101 | 1300 | 79 | 1451 | 61 |
| 148 | 0 | 342 | 0 | 533 | 1 | 727 | 247 | 918 | 131 | 1112 | 101 | 1303 | 79 | 1454 | 61 |
| 151 | 0 | | | 536 | 2 | | | 921 | 129 | | | | 78 | 1457 | 61 |

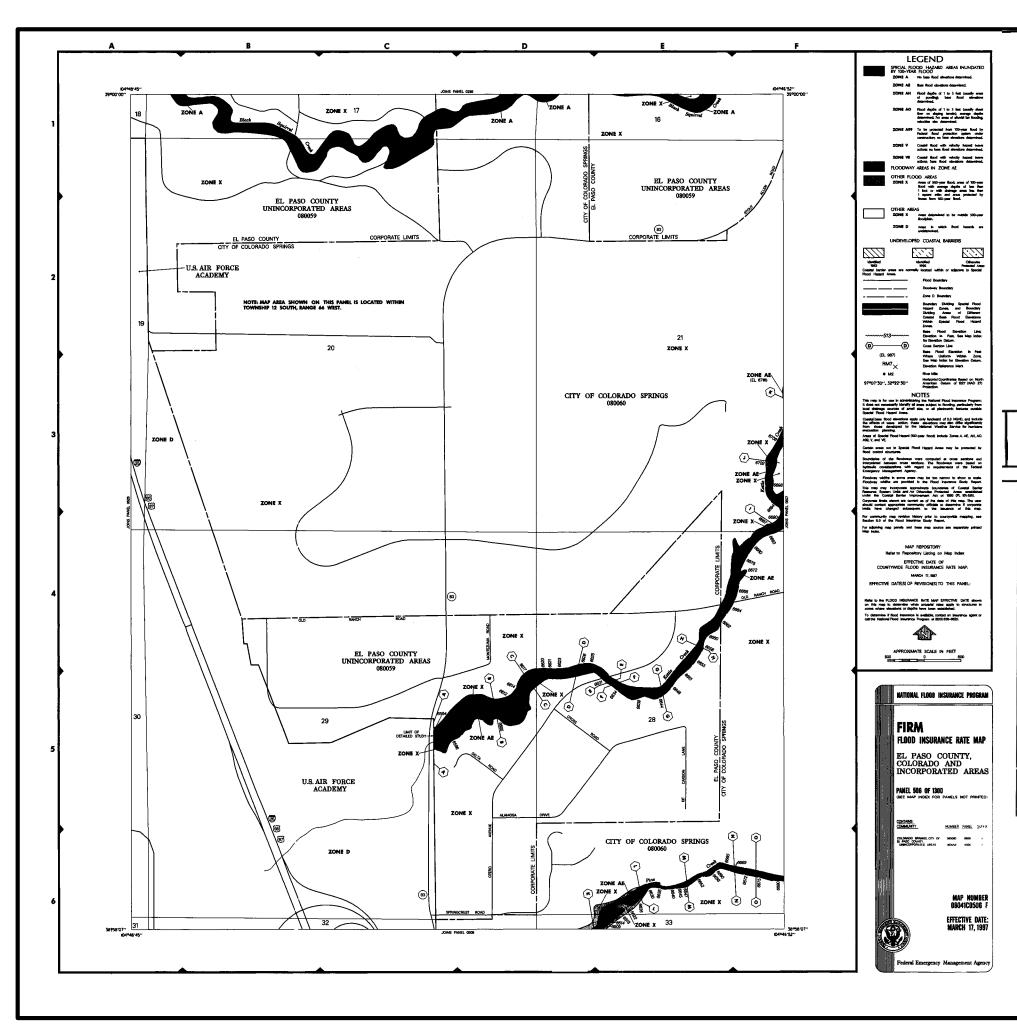
100 YR EXISTING AND FUTURE FLOW DATA FOR JUNCTION 22 (MPPD JUNCTION 24)

APPENDIX B- MDDP 100-YR FLOW DATA KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 B-97



Appendix C – Hydraulic Calculations and Data

Kettle Creek DBPS Appendix



| FLOODING SC | OURCE | | FLOODWAY | , | | BASE F WATER SURFA | LOOD CE ELEVATION | |
|---------------|-----------------------|-----------------|-------------------------------------|--|------------|------------------------------|---------------------------|----------|
| CROSS SECTION | DISTANCE ¹ | WIDTH (FEET) | SECTION AREA (SQUARE FEET) | MEAN VELOCITY (FEET PER SECOND) | REGULATORY | WITHOUT FLOODWAY (FEET | WITH FLOODWAY NGVD) | INCREASE |
| Kettle Creek | | | | | | | | |
| A | 0 | 95 | 825 | 11.3 | 6.593.6 | 6.593.6 | 6,593.6 | 0.0 |
| В | 1,120 | 130 | 706 | 13.2 | 6,604.4 | 6,604.4 | 6,604.4 | 0.0 |
| C | 2,000 | 95 | 685 | 13.6 | 6,616.7 | 6,616.7 | 6,616.7 | 0.0 |
| D | 2,720 | 130 | 838 | 11.1 | 6,625.9 | 6,625.9 | 6,626.8 | 0.9 |
| E | 3,120 | 100 | 643 | 14.5 | 6,631.4 | 6,631.4 | 6,631.4 | 0.0 |
| F | 3,150 | 100 | 829 | 11.2 | 6,633.3 | 6,633.3 | 6,633.3 | 0.0 |
| G | 3,930 | 120 | 896 | 10.4 | 6,644.5 | 6,644.5 | 6,644.9 | 0.4 |
| H | 4,780 | 90 | 738 | 12.6 | 6,657.8 | 6,657.8 | 6,657.8 | 0.0 |
| I | 6,740 | 120 | 792 | 9.4 | 6,687.1 | 6,687.1 | 6,687.3 | 0.2 |
| j | 7,860 | 100 | 653 | 11.4 | 6,702.4 | 6,702.4 | 6,702.4 | 0.0 |
| K | 8,790 | 110 | 539 | 12.4 | 6,712.1 | 6,712.1 | 6,712.1 | 0.0 |
| L | 9,490 | 90 | 581 | 11.4 | 6,723.5 | 6,723.5 | 6,724.0 | 0.5 |
| M | 10,460 | 130 | 683 | 9.7 | 6,735.8 | 6,735.8 | 6,735.8 | 0.0 |
| N | 11,290 | 131 | 654 | 10.1 | 6,747.2 | 6,747.2 | 6,747.2 | 0.0 |
| 0 | 12,440 | 110 | 654 | 10.1 | 6,764.4 | 6,764.4 | 6,764.5 | 0.1 |
| P | 13,590 | 110 | 645 | 10.2 | 6,780.0 | 6,780.0 | 6,780.0 | 0.0 |
| Q | 14,590 | 100 | 563 | 11.7 | 6,792.8 | 6,792.8 | 6,792.9 | 0.1 |
| R | 16,650 | 140 | 590 | 10.1 | 6,817.5 | 6,817.5 | 6,817.6 | 0.1 |
| S | 18,000 | 140 | 614 | 9.7 | 6,836.1 | 6,836.1 | 6,836.1 | 0.0 |
| T | 18,940 | 142 | 620 | 9.6 | 6,849.4 | 6,849.4 | 6,849.4 | 0.0 |
| U | 20,320 | 136 | 613 | 9.7 | 6,868.5 | 6,868.5 | 6,868.5 | 0.0 |
| V | 21,090 | 80 | 472 | 12.6 | 6,880.8 | 6,880.8 | 6,880.8 | 0.0 |
| W | 22,530 | 99 | 514 | 11.6 | 6,896.7 | 6,896.7 | 6,896.8 | 0.1 |
| X | 23,380 | 160 | 624 | 8.7 | 6,906.5 | 6,906.5 | 6,906.5 | 0.0 |
| Y | 25,180 | 130 | 586 | 9.2 | 6,933.5 | 6,933.5 | 6,933.7 | 0.2 |
| Z | 26,880 | 138 | 667 | 8.1 | 6,954.7 | 6,954.7 | 6,954.8 | 0.1 |

¹Feet Above State Highway 83

FEDERAL EMERGENCY MANAGEMENT AGENCY

EL PASO COUNTY, CO
AND INCORPORATED AREAS

FLOODWAY DATA

KETTLE CREEK

| FLOODING SC | OURCE | | FLOODWAY | r | | | FLOOD CE ELEVATION | |
|---------------|-----------------------|-----------------|----------------------------|--|------------|---------------------|-----------------------|----------|
| CROSS SECTION | DISTANCE ¹ | WIDTH (FEET) | SECTION AREA (SQUARE | MEAN VELOCITY (FEET PER SECOND) | REGULATORY | WITHOUT FLOODWAY | WITH FLOODWAY | INCREASE |
| | | | PEET) | SECOND) | | (FEET | NGVD) | |
| Kettle Creek | | | i | ĺ | | l | | |
| (Cont'd) | } | l | ı | ı | | l | 1 | |
| AA | 28,200 | 136 | 648 | 8.3 | 6.971.8 | 6,971.8 | 6.971.9 | 0.1 |
| AB | 29,110 | 88 | 503 | 9.2 | 6,976.1 | 6,976.1 | 6,976.1 | 0.0 |
| AC | 29,140 | 88 | 526 | 8.8 | 6,976.4 | 6,976.4 | 6,976.4 | 0.0 |
| AD | 30,630 | 96 | 478 | 9.7 | 7,007.6 | 7,007.6 | 7,007.6 | 0.0 |
| AE | 31,720 | 78 | 472 | 9.9 | 7,022.1 | 7,022.1 | 7,022.6 | 0.5 |
| AF | 32,650 | 80 | 428 | 10.9 | 7,034.3 | 7,034.3 | 7,034.6 | 0.3 |
| AG | 33,350 | 218 | 452 | 9.1 | 7,043.3 | 7,043.3 | 7,043.3 | 0.0 |
| AH | 35,350 | 131 | 491 | 8.3 | 7,072.8 | 7,072.8 | 7,072.8 | 0.0 |
| IA | 36,610 | 126 | 440 | 6.5 | 7,095.5 | 7,095.5 | 7,095.5 | 0.0 |
| LA. | 37,350 | 120 | 367 | 7.9 | 7,110.1 | 7,110.1 | 7,110.1 | 0.0 |
| AK | 38,290 | 111 | 310 | 9.3 | 7,123.0 | 7,123.0 | 7,123.0 | 0.0 |
| AL | 39,930 | 114 | 322 | 8.9 | 7,150.1 | 7,150.1 | 7,150.1 | 0.0 |
| AM | 41,440 | 96 | 395 | 5.4 | 7,173.5 | 7,173.5 | 7,173.5 | 0.0 |
| AN | 41,470 | 96 | 400 | 5.4 | 7,173.6 | 7,173.6 | 7,173.6 | 0.0 |
| AO | 42,490 | 193 | 321 | 6.7 | 7,200.5 | 7,200.5 | 7,200.5 | 0.0 |
| AP | 43,530 | 101 | 354 | 6.0 | 7,217.6 | 7,217.6 | 7,217.6 | 0.0 |
| AQ | 44,580 | 74 | 163 | 8.6 | 7,237.4 | 7,237.4 | 7,237.4 | 0.0 |
| AR | 45,740 | 53 | 169 | 8.3 | 7,262.8 | 7,262.8 | 7,262.8 | 0.0 |
| AS | 46,770 | 37 | 137 | 10.2 | 7,284.7 | 7,284.7 | 7,284.7 | 0.0 |
| AT | 47,240 | 89 | 30 | 3.4 | 7,319.5 | 7,319.5 | 7,319.5 | 0.0 |
| UA | 48,120 | 41 | 123 | 7.6 | 7.333.4 | 7,333.4 | 7,333.4 | 0.0 |
| | | | 1 1 | | | | | |
| | | | | | | | | |
| | | | | | | | 1 | |
| | | | | | 1 | | ! ! | |

¹Feet Above State Highway 83

APPENDIX C — FIRM MAPS KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 C-1



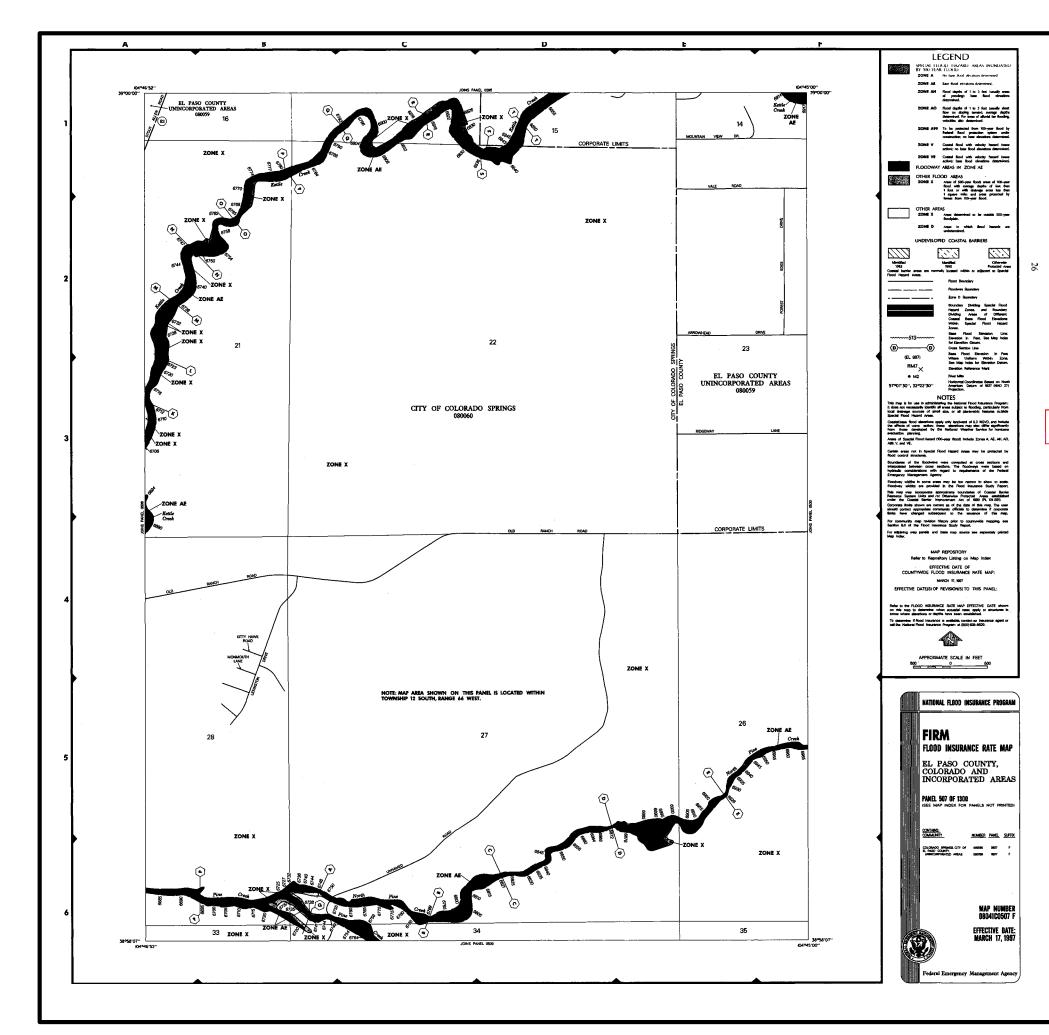


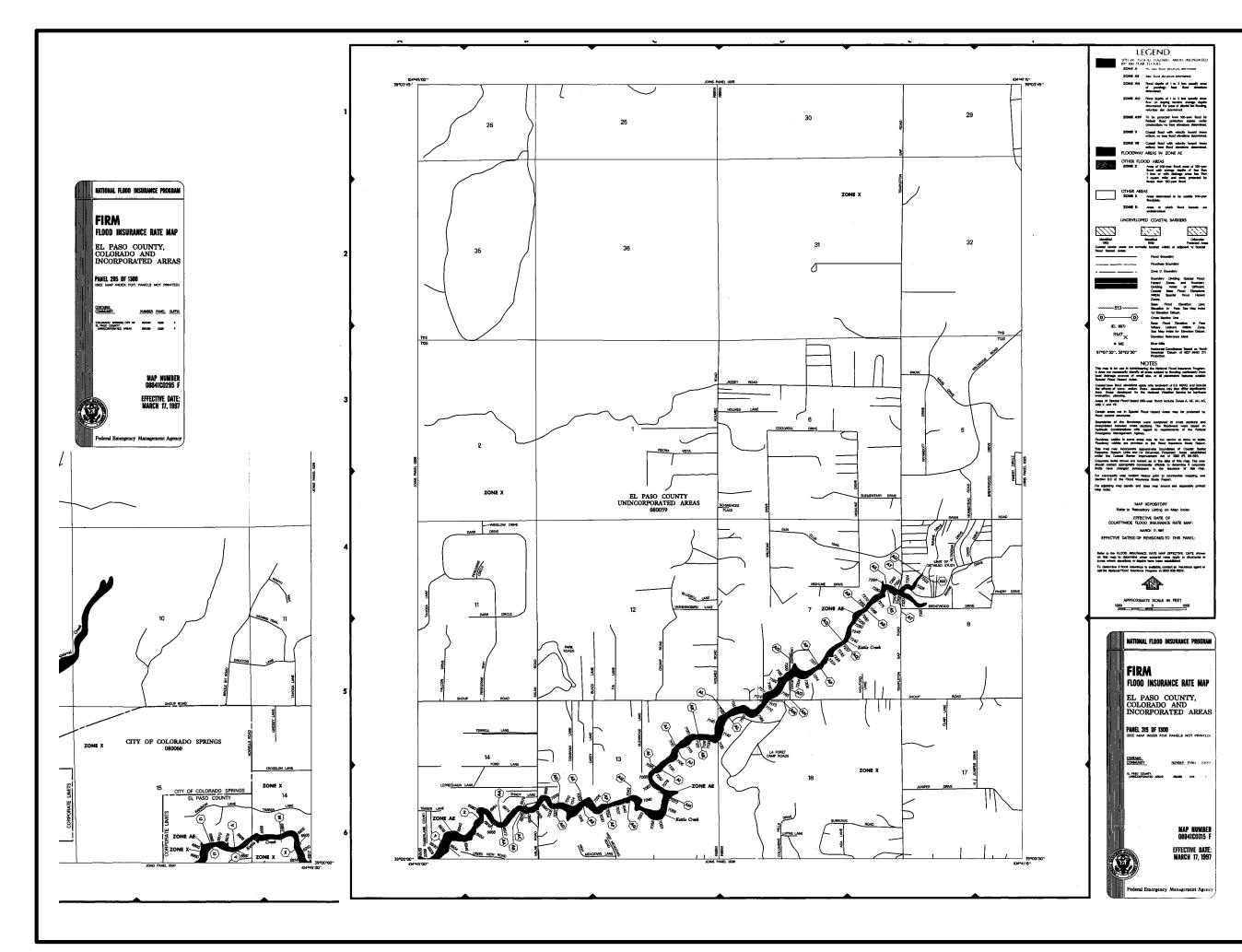
Table 3. Summary of Discharges (Cont'd)

| | Drainage Area | Pea | k Discharges (0 | Cubic Feet Per Se | cond) |
|--|----------------|---------|-----------------|-------------------|----------|
| Flooding Source and Location | (Square Miles) | 10-Усат | 50-Year | 100-Year | 500-Year |
| Fisher's Canyon-Above Loomis Avenue | | | | | |
| At West Meadows Drive | 3.59 | 1 | 1 | 1,640 | |
| Upstream of Fisher's Canyon-South Branch | 2.36 | 1 | ' | 440 | 1 |
| Fisher's Canyon-South Branch | | | | | |
| At confluence with Fisher's Canyon | 1.23 | 1 | 1 | 1,290 | 1 |
| Fountain Creek | | | | | |
| At El Paso-Pueblo County Line | 772 0 | 21,300 | 64,000 | 93,000 | 215,000 |
| Downstream of confluence with Sand Creek | 456.0 | 12,700 | 38,000 | 57,000 | 132,000 |
| Downstream of confluence with Monument | | | | | |
| Creek | 358.0 | 9,200 | 28,500 | 42,200 | 98,000 |
| Upstream of confluence with Monument Creek | 120.0 | 4,400 | 14,000 | 20,500 | 47,000 |
| Upstream of City of Colorado Springs | | | | | |
| corporate limits | 71.0 | 3,750 | 11,800 | 17,100 | 40,000 |
| At El Paso-Teller County Line | 7.8 | 2,200 | 5,800 | 7,500 | 14,000 |
| Franceville Tributary to Jimmy Camp Creek | | | | | |
| At confluence with Jimmy Camp Creek | 4.1 | 1,700 | 2,800 | 3,500 | 4,300 |
| Jimmy Camp Creek | | | | | |
| At confluence with Fountain Creek | 66.4 | 8,500 | 12,400 | 16,000 | 20,500 |
| Jimmy Camp East Tributary | | | | | |
| At confluence with Jimmy Camp Creek | 9.2 | 2,800 | 4,600 | 5,500 | 6,900 |
| Jimmy Camp West Tributary | | | | | |
| At confluence with Jimmy Camp Creek | 3.93 | 1,160 | 2,280 | 2,780 | 4,500 |
| Kettle Creek | | | | | |
| At State Highway 83 | 16.3 | 2,600 | 6,600 | 9,300 | 19,300 |
| | | | | | |

Data not available

APPENDIX C - FIRM MAPS KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 C-2





APPENDIX C — FIRM MAPS KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 C-3



HEC-RAS Plan: Historic River: Kettle Creek Reach: Kettle Creek

| Reach | River Sta | Profile | Q Total | Min Ch El | W.S. Elev | Crit W.S. | E.G. Elev | E.G. Slope | Vel Chnl | Flow Area | Top Width | Froude # Chl |
|--------------|-----------|---------|---------|-----------|-----------|-----------|-----------|------------|----------|-----------|-----------|--------------|
| | | | (cfs) | (ft) | (ft) | (ft) | (ft) | (ft/ft) | (ft/s) | (sq ft) | (ft) | |
| Kettle Creek | 24855.28 | 2-YR | 308.10 | 6868.95 | 6871.74 | 6871.00 | 6871.91 | 0.018830 | 3.23 | 95.51 | 66.48 | 0.47 |
| Kettle Creek | 24855.28 | 5-YR | 630.50 | 6868.95 | 6872.45 | | 6872.74 | 0.022547 | 4.30 | 146.66 | 76.39 | 0.55 |
| Kettle Creek | 24855.28 | 10-YR | 972.50 | 6868.95 | 6872.86 | | 6873.32 | 0.029283 | 5.44 | 178.91 | 80.16 | 0.64 |
| Kettle Creek | 24855.28 | 25-YR | 1286.50 | 6868.95 | 6873.25 | | 6873.83 | 0.031105 | 6.10 | 211.14 | 83.81 | 0.67 |
| Kettle Creek | 24855.28 | 50-YR | 1812.80 | 6868.95 | 6873.91 | 6873.15 | 6874.62 | 0.029451 | 6.75 | 268.50 | 89.98 | 0.67 |
| Kettle Creek | 24855.28 | 100-YR | 2195.90 | 6868.95 | 6874.38 | 6873.52 | 6875.15 | 0.026780 | 7.06 | 310.82 | 91.90 | 0.66 |
| Kettle Creek | 23762.63 | 2-YR | 316.60 | 6855.75 | 6859.47 | | 6859.53 | 0.007615 | 1.78 | 174.54 | 112.91 | 0.25 |
| Kettle Creek | 23762.63 | 5-YR | 641.00 | 6855.75 | 6860.34 | | 6860.44 | 0.006747 | 2.23 | 275.20 | 118.68 | 0.25 |
| Kettle Creek | 23762.63 | 10-YR | 987.40 | 6855.75 | 6861.15 | | 6861.28 | 0.005721 | 2.48 | 372.90 | 122.80 | 0.24 |
| Kettle Creek | 23762.63 | 25-YR | 1307.00 | 6855.75 | 6861.74 | | 6861.90 | 0.005489 | 2.70 | 445.83 | 125.94 | 0.24 |
| Kettle Creek | 23762.63 | 50-YR | 1843.70 | 6855.75 | 6862.50 | | 6862.73 | 0.005582 | 3.07 | 542.70 | 129.04 | 0.25 |
| Kettle Creek | 23762.63 | 100-YR | 2234.40 | 6855.75 | 6862.93 | | 6863.22 | 0.005861 | 3.34 | 598.52 | 130.50 | 0.26 |
| Kettle Creek | 22613.19 | 2-YR | 316.60 | 6839.60 | 6842.62 | | 6842.94 | 0.036979 | 4.56 | 69.43 | 33.27 | 0.56 |
| Kettle Creek | 22613.19 | 5-YR | 641.00 | 6839.60 | 6843.72 | | 6844.22 | 0.045594 | 5.66 | 113.27 | 46.17 | 0.64 |
| Kettle Creek | 22613.19 | 10-YR | 987.40 | 6839.60 | 6844.19 | | 6845.00 | 0.076972 | 7.23 | 136.63 | 57.42 | 0.83 |
| Kettle Creek | 22613.19 | 25-YR | 1307.00 | 6839.60 | 6844.75 | 6844.44 | 6845.62 | 0.090424 | 7.47 | 174.92 | 79.40 | 0.89 |
| Kettle Creek | 22613.19 | 50-YR | 1843.70 | 6839.60 | 6845.52 | 6845.22 | 6846.38 | 0.086852 | 7.43 | 248.18 | 110.76 | 0.87 |
| Kettle Creek | 22613.19 | 100-YR | 2234.40 | 6839.60 | 6845.96 | 6845.63 | 6846.82 | 0.073922 | 7.42 | 301.50 | 125.28 | 0.82 |
| Kettle Creek | 21556.31 | 2-YR | 323.20 | 6825.98 | 6830.25 | | 6830.32 | 0.005854 | 2.00 | 161.92 | 68.65 | 0.23 |
| Kettle Creek | 21556.31 | 5-YR | 653.80 | 6825.98 | 6831.84 | | 6831.91 | 0.005205 | 2.14 | 306.09 | 115.04 | 0.22 |
| Kettle Creek | 21556.31 | 10-YR | 1006.50 | 6825.98 | 6832.80 | | 6832.89 | 0.004345 | 2.37 | 421.46 | 123.04 | 0.21 |
| Kettle Creek | 21556.31 | 25-YR | 1330.30 | 6825.98 | 6833.46 | | 6833.58 | 0.004141 | 2.57 | 504.71 | 126.94 | 0.21 |
| Kettle Creek | 21556.31 | 50-YR | 1873.60 | 6825.98 | 6834.36 | | 6834.51 | 0.004095 | 2.89 | 620.24 | 132.37 | 0.22 |
| Kettle Creek | 21556.31 | 100-YR | 2268.90 | 6825.98 | 6834.88 | | 6835.06 | 0.004191 | 3.11 | 689.96 | 135.75 | 0.23 |
| Kettle Creek | 20822.88 | 2-YR | 323.20 | 6817.21 | 6821.39 | | 6821.51 | 0.013524 | 2.15 | 141.19 | 100.61 | 0.32 |
| Kettle Creek | 20822.88 | 5-YR | 653.80 | 6817.21 | 6822.06 | | 6822.27 | 0.020785 | 2.67 | 228.99 | 162.15 | 0.40 |
| Kettle Creek | 20822.88 | 10-YR | 1006.50 | 6817.21 | 6822.35 | | 6822.66 | 0.028506 | 3.44 | 275.92 | 169.82 | 0.48 |
| Kettle Creek | 20822.88 | 25-YR | 1330.30 | 6817.21 | 6822.65 | | 6823.01 | 0.028958 | 3.85 | 328.12 | 172.87 | 0.49 |
| Kettle Creek | 20822.88 | 50-YR | 1873.60 | 6817.21 | 6823.23 | | 6823.62 | 0.024962 | 4.17 | 430.48 | 180.68 | 0.48 |
| Kettle Creek | 20822.88 | 100-YR | 2268.90 | 6817.21 | 6823.70 | | 6824.08 | 0.021155 | 4.22 | 516.23 | 187.76 | 0.45 |
| Kettle Creek | 19882.53 | 2-YR | 326.80 | 6805.92 | 6810.22 | 6808.86 | 6810.28 | 0.006672 | 1.91 | 170.74 | 94.30 | 0.24 |
| Kettle Creek | 19882.53 | 5-YR | 661.30 | 6805.92 | 6811.63 | | 6811.71 | 0.003565 | 1.99 | 312.29 | 106.08 | 0.19 |
| Kettle Creek | 19882.53 | 10-YR | 1015.10 | 6805.92 | 6812.86 | | 6812.96 | 0.002426 | 2.02 | 447.91 | 114.13 | 0.16 |
| Kettle Creek | 19882.53 | 25-YR | 1339.20 | 6805.92 | 6813.73 | | 6813.86 | 0.002090 | 2.10 | 549.17 | 119.01 | 0.16 |



HEC-RAS Plan: Historic River: Kettle Creek Reach: Kettle Creek (Continued)

| Reach | River Sta | Profile | Q Total | Min Ch El | W.S. Elev | Crit W.S. | E.G. Elev | E.G. Slope | Vel Chnl | Flow Area | Top Width | Froude # Chl |
|--------------|-----------|---------|---------|-----------|-----------|-----------|-----------|------------|----------|-----------|-----------|--------------|
| | | | (cfs) | (ft) | (ft) | (ft) | (ft) | (ft/ft) | (ft/s) | (sq ft) | (ft) | |
| Kettle Creek | 19882.53 | 50-YR | 1881.70 | 6805.92 | 6814.91 | | 6815.07 | 0.001856 | 2.25 | 693.29 | 125.40 | 0.15 |
| Kettle Creek | 19882.53 | 100-YR | 2276.20 | 6805.92 | 6815.60 | | 6815.79 | 0.001812 | 2.37 | 780.84 | 129.10 | 0.15 |
| Kettle Creek | 19115.6 | 2-YR | 327.50 | 6798.52 | 6801.07 | | 6801.15 | 0.010962 | 2.28 | 142.68 | 82.89 | 0.30 |
| Kettle Creek | 19115.6 | 5-YR | 662.30 | 6798.52 | 6802.72 | | 6802.80 | 0.004157 | 2.18 | 295.69 | 108.10 | 0.21 |
| Kettle Creek | 19115.6 | 10-YR | 1016.60 | 6798.52 | 6804.03 | | 6804.12 | 0.002468 | 2.08 | 449.54 | 127.91 | 0.17 |
| Kettle Creek | 19115.6 | 25-YR | 1341.40 | 6798.52 | 6804.95 | | 6805.04 | 0.001976 | 2.10 | 580.41 | 157.85 | 0.16 |
| Kettle Creek | 19115.6 | 50-YR | 1885.30 | 6798.52 | 6806.14 | | 6806.24 | 0.001528 | 2.09 | 791.49 | 204.19 | 0.14 |
| Kettle Creek | 19115.6 | 100-YR | 2280.90 | 6798.52 | 6806.79 | | 6806.90 | 0.001302 | 2.05 | 927.93 | 215.92 | 0.13 |
| Kettle Creek | 18505.62 | 2-YR | 327.50 | 6788.84 | 6792.13 | | 6792.21 | 0.006034 | 2.17 | 146.94 | 66.15 | 0.24 |
| Kettle Creek | 18505.62 | 5-YR | 662.30 | 6788.84 | 6793.40 | | 6793.56 | 0.004932 | 2.56 | 233.77 | 70.63 | 0.23 |
| Kettle Creek | 18505.62 | 10-YR | 1016.60 | 6788.84 | 6794.36 | | 6794.60 | 0.004729 | 2.91 | 303.57 | 73.86 | 0.23 |
| Kettle Creek | 18505.62 | 25-YR | 1341.40 | 6788.84 | 6795.11 | | 6795.41 | 0.004615 | 3.16 | 359.30 | 76.07 | 0.24 |
| Kettle Creek | 18505.62 | 50-YR | 1885.30 | 6788.84 | 6796.15 | | 6796.56 | 0.004586 | 3.53 | 439.84 | 79.30 | 0.24 |
| Kettle Creek | 18505.62 | 100-YR | 2280.90 | 6788.84 | 6796.81 | | 6797.30 | 0.004554 | 3.75 | 493.69 | 81.56 | 0.25 |
| Kettle Creek | 17970.84 | 2-YR | 327.50 | 6783.01 | 6785.29 | | 6785.48 | 0.027013 | 3.53 | 92.49 | 58.28 | 0.47 |
| Kettle Creek | 17970.84 | 5-YR | 662.30 | 6783.01 | 6786.00 | | 6786.38 | 0.030500 | 4.71 | 136.64 | 65.58 | 0.53 |
| Kettle Creek | 17970.84 | 10-YR | 1016.60 | 6783.01 | 6786.74 | | 6787.25 | 0.024786 | 5.06 | 187.12 | 71.25 | 0.50 |
| Kettle Creek | 17970.84 | 25-YR | 1341.40 | 6783.01 | 6787.27 | | 6787.92 | 0.022675 | 5.37 | 226.19 | 75.30 | 0.49 |
| Kettle Creek | 17970.84 | 50-YR | 1885.30 | 6783.01 | 6788.05 | | 6788.84 | 0.020495 | 5.79 | 287.83 | 84.29 | 0.48 |
| Kettle Creek | 17970.84 | 100-YR | 2280.90 | 6783.01 | 6788.51 | | 6789.46 | 0.019150 | 5.97 | 327.30 | 86.95 | 0.47 |
| Kettle Creek | 17128.69 | 2-YR | 327.50 | 6771.75 | 6775.02 | | 6775.09 | 0.007009 | 2.06 | 158.76 | 73.23 | 0.25 |
| Kettle Creek | 17128.69 | 5-YR | 662.30 | 6771.75 | 6776.21 | | 6776.31 | 0.006281 | 2.55 | 257.23 | 87.22 | 0.25 |
| Kettle Creek | 17128.69 | 10-YR | 1016.60 | 6771.75 | 6776.94 | | 6777.11 | 0.007047 | 3.05 | 322.05 | 90.46 | 0.27 |
| Kettle Creek | 17128.69 | 25-YR | 1341.40 | 6771.75 | 6777.50 | | 6777.72 | 0.007452 | 3.42 | 373.01 | 93.15 | 0.29 |
| Kettle Creek | 17128.69 | 50-YR | 1885.30 | 6771.75 | 6778.28 | | 6778.60 | 0.007971 | 3.94 | 447.05 | 96.47 | 0.30 |
| Kettle Creek | 17128.69 | 100-YR | 2280.90 | 6771.75 | 6778.74 | | 6779.15 | 0.008423 | 4.29 | 492.37 | 98.53 | 0.32 |
| Kettle Creek | 16326.64 | 2-YR | 327.50 | 6761.71 | 6765.20 | | 6765.47 | 0.024916 | 4.16 | 78.87 | 33.57 | 0.47 |
| Kettle Creek | 16326.64 | 5-YR | 662.30 | 6761.71 | 6766.67 | | 6766.93 | 0.028840 | 3.99 | 163.80 | 85.29 | 0.50 |
| Kettle Creek | 16326.64 | 10-YR | 1016.60 | 6761.71 | 6767.39 | | 6767.71 | 0.023135 | 4.39 | 227.16 | 89.81 | 0.47 |
| Kettle Creek | 16326.64 | 25-YR | 1341.40 | 6761.71 | 6767.92 | | 6768.31 | 0.021173 | 4.73 | 275.72 | 92.98 | 0.46 |
| Kettle Creek | 16326.64 | 50-YR | 1885.30 | 6761.71 | 6768.63 | | 6769.09 | 0.019608 | 5.18 | 350.55 | 109.34 | 0.46 |
| Kettle Creek | 16326.64 | 100-YR | 2280.90 | 6761.71 | 6769.07 | | 6769.63 | 0.018115 | 5.35 | 399.77 | 110.77 | 0.45 |
| Kettle Creek | 15906.34 | 2-YR | 327.50 | 6753.98 | 6760.15 | | 6760.24 | 0.007350 | 2.47 | 132.91 | 51.15 | 0.26 |



HEC-RAS Plan: Historic River: Kettle Creek Reach: Kettle Creek (Continued)

| Reach | River Sta | Profile | Q Total | Min Ch El | W.S. Elev | Crit W.S. | E.G. Elev | E.G. Slope | Vel Chnl | Flow Area | Top Width | Froude # Chl |
|--------------|-----------|---------|---------|-----------|-----------|-----------|-----------|------------|----------|-----------|-----------|--------------|
| | | | (cfs) | (ft) | (ft) | (ft) | (ft) | (ft/ft) | (ft/s) | (sq ft) | (ft) | |
| Kettle Creek | 19882.53 | 50-YR | 1881.70 | 6805.92 | 6814.91 | | 6815.07 | 0.001856 | 2.25 | 693.29 | 125.40 | 0.15 |
| Kettle Creek | 19882.53 | 100-YR | 2276.20 | 6805.92 | 6815.60 | | 6815.79 | 0.001812 | 2.37 | 780.84 | 129.10 | 0.15 |
| Kettle Creek | 19115.6 | 2-YR | 327.50 | 6798.52 | 6801.07 | | 6801.15 | 0.010962 | 2.28 | 142.68 | 82.89 | 0.30 |
| Kettle Creek | 19115.6 | 5-YR | 662.30 | 6798.52 | 6802.72 | | 6802.80 | 0.004157 | 2.18 | 295.69 | 108.10 | 0.21 |
| Kettle Creek | 19115.6 | 10-YR | 1016.60 | 6798.52 | 6804.03 | | 6804.12 | 0.002468 | 2.08 | 449.54 | 127.91 | 0.17 |
| Kettle Creek | 19115.6 | 25-YR | 1341.40 | 6798.52 | 6804.95 | | 6805.04 | 0.001976 | 2.10 | 580.41 | 157.85 | 0.16 |
| Kettle Creek | 19115.6 | 50-YR | 1885.30 | 6798.52 | 6806.14 | | 6806.24 | 0.001528 | 2.09 | 791.49 | 204.19 | 0.14 |
| Kettle Creek | 19115.6 | 100-YR | 2280.90 | 6798.52 | 6806.79 | | 6806.90 | 0.001302 | 2.05 | 927.93 | 215.92 | 0.13 |
| Kettle Creek | 18505.62 | 2-YR | 327.50 | 6788.84 | 6792.13 | | 6792.21 | 0.006034 | 2.17 | 146.94 | 66.15 | 0.24 |
| Kettle Creek | 18505.62 | 5-YR | 662.30 | 6788.84 | 6793.40 | | 6793.56 | 0.004932 | 2.56 | 233.77 | 70.63 | 0.23 |
| Kettle Creek | 18505.62 | 10-YR | 1016.60 | 6788.84 | 6794.36 | | 6794.60 | 0.004729 | 2.91 | 303.57 | 73.86 | 0.23 |
| Kettle Creek | 18505.62 | 25-YR | 1341.40 | 6788.84 | 6795.11 | | 6795.41 | 0.004615 | 3.16 | 359.30 | 76.07 | 0.24 |
| Kettle Creek | 18505.62 | 50-YR | 1885.30 | 6788.84 | 6796.15 | | 6796.56 | 0.004586 | 3.53 | 439.84 | 79.30 | 0.24 |
| Kettle Creek | 18505.62 | 100-YR | 2280.90 | 6788.84 | 6796.81 | | 6797.30 | 0.004554 | 3.75 | 493.69 | 81.56 | 0.25 |
| Kettle Creek | 17970.84 | 2-YR | 327.50 | 6783.01 | 6785.29 | | 6785.48 | 0.027013 | 3.53 | 92.49 | 58.28 | 0.47 |
| Kettle Creek | 17970.84 | 5-YR | 662.30 | 6783.01 | 6786.00 | | 6786.38 | 0.030500 | 4.71 | 136.64 | 65.58 | 0.53 |
| Kettle Creek | 17970.84 | 10-YR | 1016.60 | 6783.01 | 6786.74 | | 6787.25 | 0.024786 | 5.06 | 187.12 | 71.25 | 0.50 |
| Kettle Creek | 17970.84 | 25-YR | 1341.40 | 6783.01 | 6787.27 | | 6787.92 | 0.022675 | 5.37 | 226.19 | 75.30 | 0.49 |
| Kettle Creek | 17970.84 | 50-YR | 1885.30 | 6783.01 | 6788.05 | | 6788.84 | 0.020495 | 5.79 | 287.83 | 84.29 | 0.48 |
| Kettle Creek | 17970.84 | 100-YR | 2280.90 | 6783.01 | 6788.51 | | 6789.46 | 0.019150 | 5.97 | 327.30 | 86.95 | 0.47 |
| Kettle Creek | 17128.69 | 2-YR | 327.50 | 6771.75 | 6775.02 | | 6775.09 | 0.007009 | 2.06 | 158.76 | 73.23 | 0.25 |
| Kettle Creek | 17128.69 | 5-YR | 662.30 | 6771.75 | 6776.21 | | 6776.31 | 0.006281 | 2.55 | 257.23 | 87.22 | 0.25 |
| Kettle Creek | 17128.69 | 10-YR | 1016.60 | 6771.75 | 6776.94 | | 6777.11 | 0.007047 | 3.05 | 322.05 | 90.46 | 0.27 |
| Kettle Creek | 17128.69 | 25-YR | 1341.40 | 6771.75 | 6777.50 | | 6777.72 | 0.007452 | 3.42 | 373.01 | 93.15 | 0.29 |
| Kettle Creek | 17128.69 | 50-YR | 1885.30 | 6771.75 | 6778.28 | | 6778.60 | 0.007971 | 3.94 | 447.05 | 96.47 | 0.30 |
| Kettle Creek | 17128.69 | 100-YR | 2280.90 | 6771.75 | 6778.74 | | 6779.15 | 0.008423 | 4.29 | 492.37 | 98.53 | 0.32 |
| Kettle Creek | 16326.64 | 2-YR | 327.50 | 6761.71 | 6765.20 | | 6765.47 | 0.024916 | 4.16 | 78.87 | 33.57 | 0.47 |
| Kettle Creek | 16326.64 | 5-YR | 662.30 | 6761.71 | 6766.67 | | 6766.93 | 0.028840 | 3.99 | 163.80 | 85.29 | 0.50 |
| Kettle Creek | 16326.64 | 10-YR | 1016.60 | 6761.71 | 6767.39 | | 6767.71 | 0.023135 | 4.39 | 227.16 | 89.81 | 0.47 |
| Kettle Creek | 16326.64 | 25-YR | 1341.40 | 6761.71 | 6767.92 | | 6768.31 | 0.021173 | 4.73 | 275.72 | 92.98 | 0.46 |
| Kettle Creek | 16326.64 | 50-YR | 1885.30 | 6761.71 | 6768.63 | | 6769.09 | 0.019608 | 5.18 | 350.55 | 109.34 | 0.46 |
| Kettle Creek | 16326.64 | 100-YR | 2280.90 | 6761.71 | 6769.07 | | 6769.63 | 0.018115 | 5.35 | 399.77 | 110.77 | 0.45 |
| Kettle Creek | 15906.34 | 2-YR | 327.50 | 6753.98 | 6760.15 | | 6760.24 | 0.007350 | 2.47 | 132.91 | 51.15 | 0.26 |



HEC-RAS Plan: Historic River: Kettle Creek Reach: Kettle Creek (Continued)

| Reach | River Sta | Profile | Q Total | Min Ch El | W.S. Elev | Crit W.S. | E.G. Elev | E.G. Slope | Vel Chnl | Flow Area | Top Width | Froude # Chl |
|--------------|-----------|---------|---------|-----------|-----------|-----------|-----------|------------|----------|-----------|-----------|--------------|
| | | | (cfs) | (ft) | (ft) | (ft) | (ft) | (ft/ft) | (ft/s) | (sq ft) | (ft) | |
| Kettle Creek | 13757.33 | 100-YR | 2280.90 | 6727.92 | 6735.34 | | 6736.57 | 0.022250 | 6.72 | 282.31 | 80.42 | 0.49 |
| Kettle Creek | 12367.83 | 2-YR | 327.50 | 6708.58 | 6712.16 | | 6712.21 | 0.003857 | 1.80 | 181.55 | 66.19 | 0.19 |
| Kettle Creek | 12367.83 | 5-YR | 662.30 | 6708.58 | 6713.60 | | 6713.69 | 0.003939 | 2.36 | 278.69 | 69.28 | 0.20 |
| Kettle Creek | 12367.83 | 10-YR | 1016.60 | 6708.58 | 6713.70 | | 6713.90 | 0.008571 | 3.54 | 285.63 | 69.49 | 0.30 |
| Kettle Creek | 12367.83 | 25-YR | 1341.40 | 6708.58 | 6714.28 | | 6714.54 | 0.009806 | 4.05 | 328.88 | 77.18 | 0.33 |
| Kettle Creek | 12367.83 | 50-YR | 1885.30 | 6708.58 | 6715.19 | | 6715.54 | 0.010156 | 4.63 | 399.98 | 79.51 | 0.34 |
| Kettle Creek | 12367.83 | 100-YR | 2280.90 | 6708.58 | 6715.78 | | 6716.20 | 0.010202 | 4.96 | 448.09 | 81.66 | 0.35 |
| Kettle Creek | 11267.11 | 2-YR | 327.50 | 6695.53 | 6699.06 | 6698.91 | 6699.98 | 0.116324 | 7.71 | 42.49 | 20.98 | 0.95 |
| Kettle Creek | 11267.11 | 5-YR | 662.30 | 6695.53 | 6700.34 | 6700.34 | 6701.44 | 0.104178 | 8.44 | 78.83 | 36.34 | 0.94 |
| Kettle Creek | 11267.11 | 10-YR | 1016.60 | 6695.53 | 6702.66 | | 6703.12 | 0.011298 | 4.32 | 203.90 | 66.60 | 0.35 |
| Kettle Creek | 11267.11 | 25-YR | 1341.40 | 6695.53 | 6703.34 | | 6703.92 | 0.009487 | 4.32 | 250.74 | 71.28 | 0.33 |
| Kettle Creek | 11267.11 | 50-YR | 1885.30 | 6695.53 | 6704.12 | | 6704.93 | 0.009151 | 4.64 | 308.54 | 77.03 | 0.33 |
| Kettle Creek | 11267.11 | 100-YR | 2280.90 | 6695.53 | 6704.59 | | 6705.55 | 0.009161 | 4.87 | 345.61 | 81.11 | 0.33 |
| Kettle Creek | 10087.38 | 2-YR | 328.50 | 6680.77 | 6684.95 | | 6685.04 | 0.002512 | 1.70 | 159.07 | 56.13 | 0.16 |
| Kettle Creek | 10087.38 | 5-YR | 661.50 | 6680.77 | 6686.52 | | 6686.66 | 0.002290 | 2.09 | 254.86 | 69.77 | 0.16 |
| Kettle Creek | 10087.38 | 10-YR | 1012.30 | 6680.77 | 6687.64 | | 6687.82 | 0.002195 | 2.34 | 343.59 | 87.25 | 0.17 |
| Kettle Creek | 10087.38 | 25-YR | 1333.10 | 6680.77 | 6688.36 | | 6688.58 | 0.002116 | 2.47 | 406.94 | 90.09 | 0.17 |
| Kettle Creek | 10087.38 | 50-YR | 1869.30 | 6680.77 | 6689.42 | | 6689.71 | 0.001962 | 2.61 | 503.92 | 92.80 | 0.16 |
| Kettle Creek | 10087.38 | 100-YR | 2258.80 | 6680.77 | 6690.11 | | 6690.45 | 0.001878 | 2.70 | 569.13 | 94.66 | 0.16 |
| Kettle Creek | 9732.32 | 2-YR | 328.50 | 6676.00 | 6679.62 | | 6679.78 | 0.014215 | 3.12 | 105.41 | 44.21 | 0.36 |
| Kettle Creek | 9732.32 | 5-YR | 661.50 | 6676.00 | 6680.96 | | 6681.19 | 0.015232 | 3.83 | 172.63 | 57.27 | 0.38 |
| Kettle Creek | 9732.32 | 10-YR | 1012.30 | 6676.00 | 6681.55 | | 6681.92 | 0.019446 | 4.86 | 209.28 | 67.14 | 0.45 |
| Kettle Creek | 9732.32 | 25-YR | 1333.10 | 6676.00 | 6681.82 | | 6682.35 | 0.025998 | 5.89 | 227.43 | 70.49 | 0.52 |
| Kettle Creek | 9732.32 | 50-YR | 1869.30 | 6676.00 | 6682.28 | | 6683.07 | 0.032827 | 7.13 | 261.08 | 74.66 | 0.60 |
| Kettle Creek | 9732.32 | 100-YR | 2258.80 | 6676.00 | 6682.51 | | 6683.54 | 0.038535 | 7.99 | 278.90 | 76.19 | 0.65 |
| Kettle Creek | 8444.97 | 2-YR | 353.10 | 6660.69 | 6664.35 | | 6664.48 | 0.010189 | 2.87 | 123.62 | 53.24 | 0.31 |
| Kettle Creek | 8444.97 | 5-YR | 701.50 | 6660.69 | 6665.42 | | 6665.62 | 0.009957 | 3.54 | 195.76 | 81.59 | 0.32 |
| Kettle Creek | 8444.97 | 10-YR | 1066.00 | 6660.69 | 6666.22 | | 6666.47 | 0.008287 | 3.67 | 269.36 | 100.58 | 0.30 |
| Kettle Creek | 8444.97 | 25-YR | 1398.50 | 6660.69 | 6666.81 | | 6667.14 | 0.006870 | 3.63 | 330.40 | 104.18 | 0.28 |
| Kettle Creek | 8444.97 | 50-YR | 1953.40 | 6660.69 | 6667.60 | | 6668.03 | 0.006059 | 3.74 | 414.16 | 110.69 | 0.27 |
| Kettle Creek | 8444.97 | 100-YR | 2361.60 | 6660.69 | 6668.12 | | 6668.62 | 0.005609 | 3.81 | 473.94 | 116.54 | 0.26 |
| Kettle Creek | 8350 | 2-YR | 353.10 | 6660.00 | 6663.84 | | 6663.91 | 0.003711 | 2.04 | 164.36 | 65.11 | 0.19 |
| Kettle Creek | 8350 | 5-YR | 701.50 | 6660.00 | 6664.85 | | 6665.02 | 0.004274 | 2.60 | 235.14 | 74.09 | 0.22 |



HEC-RAS Plan: Historic River: Kettle Creek Reach: Kettle Creek (Continued)

| Reach | River Sta | Profile | Q Total | Min Ch El | W.S. Elev | Crit W.S. | E.G. Elev | E.G. Slope | Vel Chnl | Flow Area | Top Width | Froude # Chl |
|--------------|-----------|---------|---------|-----------|-----------|-----------|-----------|------------|----------|-----------|-----------|--------------|
| | | | (cfs) | (ft) | (ft) | (ft) | (ft) | (ft/ft) | (ft/s) | (sq ft) | (ft) | |
| Kettle Creek | 8350 | 10-YR | 1066.00 | 6660.00 | 6665.64 | | 6665.91 | 0.004490 | 2.97 | 296.61 | 82.32 | 0.23 |
| Kettle Creek | 8350 | 25-YR | 1398.50 | 6660.00 | 6666.27 | | 6666.61 | 0.004560 | 3.23 | 352.35 | 97.72 | 0.23 |
| Kettle Creek | 8350 | 50-YR | 1953.40 | 6660.00 | 6667.12 | | 6667.55 | 0.004276 | 3.42 | 438.67 | 104.63 | 0.23 |
| Kettle Creek | 8350 | 100-YR | 2361.60 | 6660.00 | 6667.68 | | 6668.17 | 0.004090 | 3.53 | 498.53 | 109.43 | 0.23 |
| Kettle Creek | 8251.39 | 2-YR | 353.10 | 6660.00 | 6662.16 | 6662.16 | 6662.77 | 0.139520 | 6.25 | 56.55 | 47.96 | 1.00 |
| Kettle Creek | 8251.39 | 5-YR | 701.50 | 6660.00 | 6662.98 | 6662.86 | 6663.78 | 0.089996 | 7.10 | 98.01 | 52.88 | 0.88 |
| Kettle Creek | 8251.39 | 10-YR | 1066.00 | 6660.00 | 6663.70 | 6663.45 | 6664.67 | 0.067145 | 7.51 | 137.80 | 57.70 | 0.80 |
| Kettle Creek | 8251.39 | 25-YR | 1398.50 | 6660.00 | 6664.26 | | 6665.38 | 0.056623 | 7.80 | 170.79 | 61.78 | 0.76 |
| Kettle Creek | 8251.39 | 50-YR | 1953.40 | 6660.00 | 6665.01 | 6664.69 | 6666.39 | 0.047749 | 8.22 | 219.99 | 68.22 | 0.72 |
| Kettle Creek | 8251.39 | 100-YR | 2361.60 | 6660.00 | 6665.49 | 6665.17 | 6667.04 | 0.043694 | 8.47 | 253.41 | 72.46 | 0.70 |
| Kettle Creek | 8060.94 | 2-YR | 353.10 | 6653.57 | 6656.87 | 6655.93 | 6657.22 | 0.011326 | 3.29 | 86.15 | 37.48 | 0.33 |
| Kettle Creek | 8060.94 | 5-YR | 701.50 | 6653.57 | 6657.83 | 6657.05 | 6658.50 | 0.013120 | 4.27 | 125.51 | 43.90 | 0.38 |
| Kettle Creek | 8060.94 | 10-YR | 1066.00 | 6653.57 | 6658.53 | 6657.93 | 6659.49 | 0.014608 | 5.01 | 157.55 | 48.51 | 0.41 |
| Kettle Creek | 8060.94 | 25-YR | 1398.50 | 6653.57 | 6659.04 | 6658.62 | 6660.25 | 0.015630 | 5.56 | 183.29 | 52.29 | 0.43 |
| Kettle Creek | 8060.94 | 50-YR | 1953.40 | 6653.57 | 6659.74 | 6659.55 | 6661.33 | 0.016802 | 6.28 | 222.21 | 57.94 | 0.46 |
| Kettle Creek | 8060.94 | 100-YR | 2361.60 | 6653.57 | 6660.17 | 6660.10 | 6662.02 | 0.017487 | 6.71 | 247.86 | 61.29 | 0.47 |
| Kettle Creek | 7863.13 | 2-YR | 353.10 | 6649.24 | 6651.10 | 6651.10 | 6651.77 | 0.128027 | 6.54 | 54.02 | 41.06 | 0.98 |
| Kettle Creek | 7863.13 | 5-YR | 701.50 | 6649.24 | 6651.94 | 6651.87 | 6652.90 | 0.092227 | 7.62 | 90.48 | 46.02 | 0.90 |
| Kettle Creek | 7863.13 | 10-YR | 1066.00 | 6649.24 | 6652.67 | 6652.53 | 6653.87 | 0.071768 | 8.12 | 125.51 | 50.74 | 0.84 |
| Kettle Creek | 7863.13 | 25-YR | 1398.50 | 6649.24 | 6653.22 | 6653.07 | 6654.65 | 0.061406 | 8.43 | 154.57 | 54.11 | 0.80 |
| Kettle Creek | 7863.13 | 50-YR | 1953.40 | 6649.24 | 6653.99 | 6653.91 | 6655.79 | 0.051887 | 8.85 | 198.10 | 58.45 | 0.76 |
| Kettle Creek | 7863.13 | 100-YR | 2361.60 | 6649.24 | 6654.49 | 6654.49 | 6656.52 | 0.047530 | 9.12 | 227.90 | 61.60 | 0.74 |
| Kettle Creek | 7632.03 | 2-YR | 353.10 | 6641.32 | 6646.20 | | 6646.31 | 0.008952 | 2.75 | 128.33 | 45.40 | 0.29 |
| Kettle Creek | 7632.03 | 5-YR | 701.50 | 6641.32 | 6647.79 | | 6647.96 | 0.008705 | 3.36 | 208.44 | 55.76 | 0.30 |
| Kettle Creek | 7632.03 | 10-YR | 1066.00 | 6641.32 | 6648.80 | | 6649.04 | 0.009046 | 3.96 | 267.75 | 61.25 | 0.32 |
| Kettle Creek | 7632.03 | 25-YR | 1398.50 | 6641.32 | 6649.49 | | 6649.80 | 0.009543 | 4.45 | 311.28 | 64.84 | 0.33 |
| Kettle Creek | 7632.03 | 50-YR | 1953.40 | 6641.32 | 6650.38 | | 6650.82 | 0.010474 | 5.15 | 371.58 | 70.06 | 0.36 |
| Kettle Creek | 7632.03 | 100-YR | 2361.60 | 6641.32 | 6650.94 | | 6651.46 | 0.011028 | 5.59 | 411.37 | 74.09 | 0.37 |
| Kettle Creek | 6688.3 | 2-YR | 354.00 | 6629.79 | 6633.04 | | 6633.28 | 0.023936 | 3.87 | 91.51 | 40.83 | 0.46 |
| Kettle Creek | 6688.3 | 5-YR | 704.60 | 6629.79 | 6634.52 | | 6634.80 | 0.025676 | 4.25 | 165.73 | 68.02 | 0.48 |
| Kettle Creek | 6688.3 | 10-YR | 1073.00 | 6629.79 | 6635.47 | | 6635.78 | 0.024632 | 4.45 | 240.95 | 89.79 | 0.48 |
| Kettle Creek | 6688.3 | 25-YR | 1409.70 | 6629.79 | 6636.14 | | 6636.47 | 0.022839 | 4.60 | 306.37 | 103.14 | 0.47 |
| Kettle Creek | 6688.3 | 50-YR | 1972.40 | 6629.79 | 6637.06 | | 6637.42 | 0.020117 | 4.85 | 406.97 | 116.81 | 0.45 |
| Kettle Creek | 6688.3 | 100-YR | 2381.00 | 6629.79 | 6637.64 | | 6638.02 | 0.018858 | 4.99 | 476.81 | 125.69 | 0.45 |



HEC-RAS Plan: Historic River: Kettle Creek Reach: Kettle Creek (Continued)

| Reach | River Sta | Profile | Q Total | Min Ch El | W.S. Elev | Crit W.S. | E.G. Elev | E.G. Slope | Vel Chnl | Flow Area | Top Width | Froude # Chl |
|--------------|-----------|---------|---------|-----------|-----------|-----------|-----------|------------|----------|-----------|-----------|--------------|
| | | | (cfs) | (ft) | (ft) | (ft) | (ft) | (tt/ft) | (ft/s) | (sq ft) | (ft) | |
| Kettle Creek | 6433.61 | 2-YR | 354.00 | 6627.42 | 6631.00 | | 6631.05 | 0.004341 | 1.81 | 195.85 | 77.32 | 0.20 |
| Kettle Creek | 6433.61 | 5-YR | 704.60 | 6627.42 | 6632.27 | | 6632.35 | 0.004804 | 2.33 | 302.53 | 89.52 | 0.22 |
| Kettle Creek | 6433.61 | 10-YR | 1073.00 | 6627.42 | 6633.19 | | 6633.31 | 0.004951 | 2.77 | 387.95 | 96.32 | 0.23 |
| Kettle Creek | 6433.61 | 25-YR | 1409.70 | 6627.42 | 6633.86 | | 6634.01 | 0.005135 | 3.10 | 453.58 | 100.30 | 0.24 |
| Kettle Creek | 6433.61 | 50-YR | 1972.40 | 6627.42 | 6634.80 | | 6635.00 | 0.005312 | 3.54 | 550.18 | 104.92 | 0.26 |
| Kettle Creek | 6433.61 | 100-YR | 2381.00 | 6627.42 | 6635.39 | | 6635.63 | 0.005402 | 3.80 | 613.39 | 108.34 | 0.26 |
| Kettle Creek | 6305.69 | 2-YR | 354.00 | 6625.87 | 6629.15 | | 6629.24 | 0.010035 | 2.37 | 149.39 | 73.11 | 0.29 |
| Kettle Creek | 6305.69 | 5-YR | 704.60 | 6625.87 | 6630.20 | | 6630.34 | 0.011142 | 3.02 | 233.62 | 86.14 | 0.32 |
| Kettle Creek | 6305.69 | 10-YR | 1073.00 | 6625.87 | 6631.14 | | 6631.32 | 0.010466 | 3.37 | 318.99 | 95.90 | 0.32 |
| Kettle Creek | 6305.69 | 25-YR | 1409.70 | 6625.87 | 6631.86 | | 6632.06 | 0.009444 | 3.62 | 390.35 | 103.34 | 0.32 |
| Kettle Creek | 6305.69 | 50-YR | 1972.40 | 6625.87 | 6632.89 | | 6633.13 | 0.008184 | 3.92 | 502.50 | 113.70 | 0.31 |
| Kettle Creek | 6305.69 | 100-YR | 2381.00 | 6625.87 | 6633.55 | | 6633.81 | 0.007508 | 4.07 | 579.41 | 120.17 | 0.30 |
| Kettle Creek | 6147.73 | 2-YR | 354.00 | 6623.99 | 6627.84 | | 6627.91 | 0.007051 | 2.06 | 171.58 | 90.53 | 0.25 |
| Kettle Creek | 6147.73 | 5-YR | 704.60 | 6623.99 | 6629.27 | | 6629.37 | 0.003841 | 2.14 | 306.59 | 96.98 | 0.20 |
| Kettle Creek | 6147.73 | 10-YR | 1073.00 | 6623.99 | 6630.32 | | 6630.45 | 0.003280 | 2.35 | 410.64 | 101.90 | 0.19 |
| Kettle Creek | 6147.73 | 25-YR | 1409.70 | 6623.99 | 6631.09 | | 6631.26 | 0.003087 | 2.53 | 490.56 | 105.29 | 0.19 |
| Kettle Creek | 6147.73 | 50-YR | 1972.40 | 6623.99 | 6632.18 | | 6632.40 | 0.002932 | 2.78 | 607.89 | 110.61 | 0.19 |
| Kettle Creek | 6147.73 | 100-YR | 2381.00 | 6623.99 | 6632.86 | | 6633.12 | 0.002864 | 2.94 | 684.30 | 113.74 | 0.19 |
| Kettle Creek | 6032.86 | 2-YR | 354.00 | 6622.67 | 6626.21 | | 6626.27 | 0.004310 | 1.86 | 182.42 | 83.84 | 0.20 |
| Kettle Creek | 6032.86 | 5-YR | 704.60 | 6622.67 | 6627.31 | | 6627.44 | 0.003932 | 2.24 | 278.07 | 90.33 | 0.20 |
| Kettle Creek | 6032.86 | 10-YR | 1073.00 | 6622.67 | 6628.14 | | 6628.33 | 0.003912 | 2.56 | 355.44 | 95.50 | 0.21 |
| Kettle Creek | 6032.86 | 25-YR | 1409.70 | 6622.67 | 6628.74 | | 6628.99 | 0.004031 | 2.82 | 413.10 | 98.91 | 0.22 |
| Kettle Creek | 6032.86 | 50-YR | 1972.40 | 6622.67 | 6629.62 | | 6629.96 | 0.004050 | 3.13 | 502.76 | 103.97 | 0.22 |
| Kettle Creek | 6032.86 | 100-YR | 2381.00 | 6622.67 | 6630.21 | | 6630.61 | 0.003981 | 3.31 | 564.66 | 107.03 | 0.23 |
| Kettle Creek | 5983.2 | 2-YR | 354.00 | 6622.04 | 6626.06 | | 6626.11 | 0.002492 | 1.59 | 198.91 | 90.80 | 0.16 |
| Kettle Creek | 5983.2 | 5-YR | 704.60 | 6622.04 | 6627.19 | | 6627.29 | 0.002153 | 1.81 | 310.58 | 106.47 | 0.15 |
| Kettle Creek | 5983.2 | 10-YR | 1073.00 | 6622.04 | 6628.04 | | 6628.18 | 0.002031 | 1.99 | 406.65 | 118.33 | 0.15 |
| Kettle Creek | 5983.2 | 25-YR | 1409.70 | 6622.04 | 6628.65 | | 6628.84 | 0.001923 | 2.08 | 479.06 | 119.70 | 0.15 |
| Kettle Creek | 5983.2 | 50-YR | 1972.40 | 6622.04 | 6629.56 | | 6629.81 | 0.001829 | 2.24 | 590.12 | 124.90 | 0.15 |
| Kettle Creek | 5983.2 | 100-YR | 2381.00 | 6622.04 | 6630.16 | | 6630.44 | 0.001795 | 2.35 | 667.83 | 130.97 | 0.15 |
| Kettle Creek | 5846.46 | 2-YR | 354.00 | 6620.39 | 6622.52 | | 6622.96 | 0.085660 | 5.32 | 66.56 | 48.91 | 0.80 |
| Kettle Creek | 5846.46 | 5-YR | 704.60 | 6620.39 | 6623.45 | | 6624.03 | 0.066162 | 6.07 | 116.12 | 57.50 | 0.75 |
| Kettle Creek | 5846.46 | 10-YR | 1073.00 | 6620.39 | 6624.20 | | 6624.89 | 0.057157 | 6.65 | 161.47 | 63.80 | 0.73 |



HEC-RAS Plan: Historic River: Kettle Creek Reach: Kettle Creek (Continued)

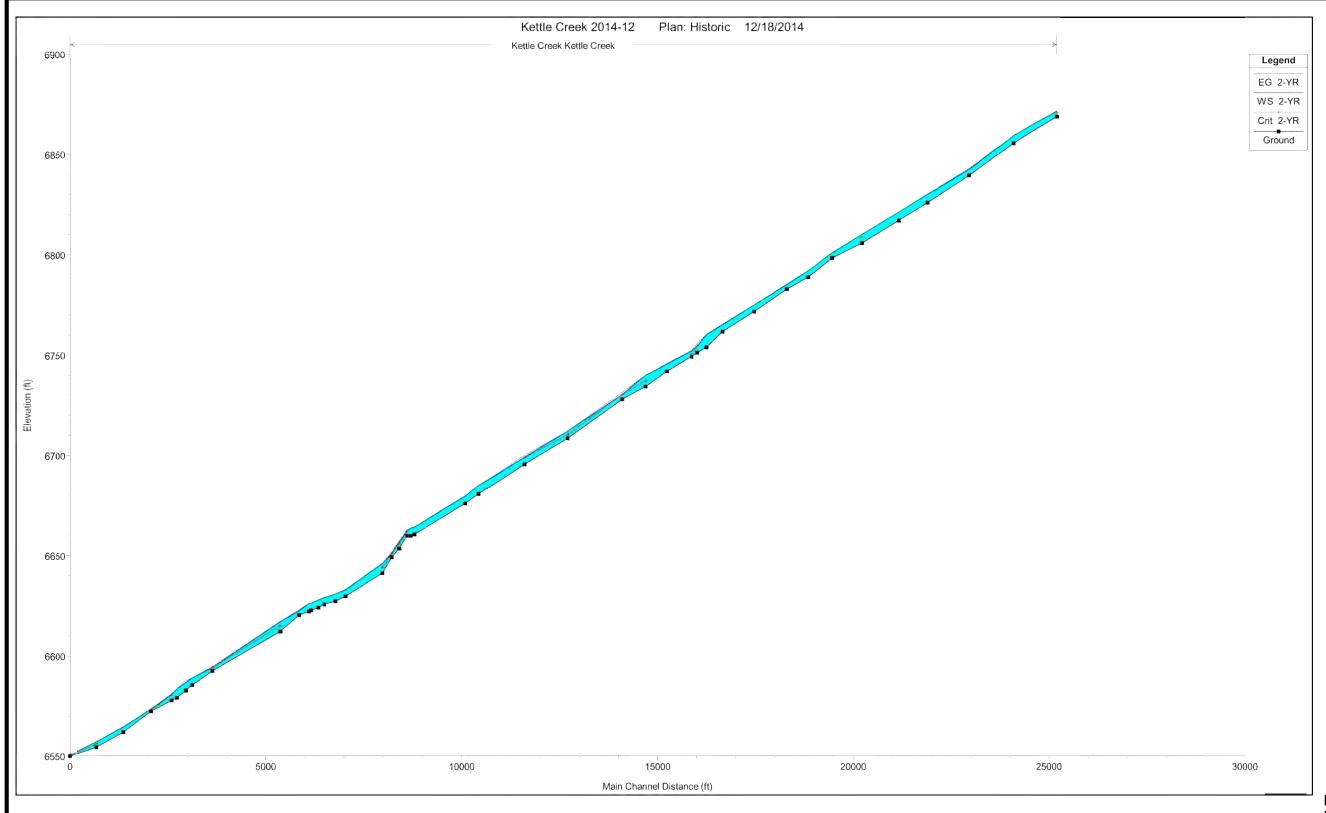
| Reach | River Sta | Profile | Q Total | Min Ch El | W.S. Elev | Crit W.S. | E.G. Elev | E.G. Slope | Vel Chnl | Flow Area | Top Width | Froude # Chl |
|--------------|-----------|---------|---------|-----------|-----------|-----------|-----------|------------|----------|-----------|-----------|--------------|
| | | | (cfs) | (ft) | (ft) | (ft) | (ft) | (ft/ft) | (ft/s) | (sq ft) | (ft) | |
| Kettle Creek | 5846.46 | 25-YR | 1409.70 | 6620.39 | 6624.75 | | 6625.54 | 0.051331 | 7.16 | 197.40 | 67.93 | 0.71 |
| Kettle Creek | 5846.46 | 50-YR | 1972.40 | 6620.39 | 6625.53 | | 6626.48 | 0.044721 | 7.76 | 253.12 | 73.24 | 0.69 |
| Kettle Creek | 5846.46 | 100-YR | 2381.00 | 6620.39 | 6626.03 | | 6627.09 | 0.041561 | 8.10 | 290.28 | 76.50 | 0.68 |
| Kettle Creek | 5366.46 | 2-YR | 354.00 | 6612.16 | 6617.10 | 6614.99 | 6617.15 | 0.004483 | 1.82 | 194.57 | 81.26 | 0.20 |
| Kettle Creek | 5366.46 | 5-YR | 704.60 | 6612.16 | 6618.22 | 6615.79 | 6618.31 | 0.004637 | 2.37 | 293.22 | 92.61 | 0.22 |
| Kettle Creek | 5366.46 | 10-YR | 1073.00 | 6612.16 | 6619.06 | 6616.34 | 6619.20 | 0.004783 | 2.77 | 372.23 | 95.87 | 0.23 |
| Kettle Creek | 5366.46 | 25-YR | 1409.70 | 6612.16 | 6619.70 | 6616.75 | 6619.88 | 0.004881 | 3.06 | 433.84 | 98.08 | 0.24 |
| Kettle Creek | 5366.46 | 50-YR | 1972.40 | 6612.16 | 6620.60 | 6617.35 | 6620.86 | 0.005031 | 3.46 | 523.66 | 101.72 | 0.25 |
| Kettle Creek | 5366.46 | 100-YR | 2381.00 | 6612.16 | 6621.16 | 6617.73 | 6621.48 | 0.005117 | 3.70 | 581.99 | 103.99 | 0.25 |
| Kettle Creek | 3636.65 | 2-YR | 354.00 | 6592.57 | 6594.21 | 6594.19 | 6594.63 | 0.146748 | 5.20 | 68.07 | 77.77 | 0.98 |
| Kettle Creek | 3636.65 | 5-YR | 704.60 | 6592.57 | 6594.70 | 6594.70 | 6595.37 | 0.137839 | 6.57 | 107.32 | 82.35 | 1.01 |
| Kettle Creek | 3636.65 | 10-YR | 1073.00 | 6592.57 | 6595.15 | 6595.15 | 6596.00 | 0.125751 | 7.41 | 144.88 | 86.50 | 1.01 |
| Kettle Creek | 3636.65 | 25-YR | 1409.70 | 6592.57 | 6595.50 | 6595.50 | 6596.50 | 0.118884 | 8.04 | 175.35 | 88.66 | 1.01 |
| Kettle Creek | 3636.65 | 50-YR | 1972.40 | 6592.57 | 6596.01 | 6596.01 | 6597.24 | 0.109233 | 8.91 | 221.60 | 91.56 | 1.00 |
| Kettle Creek | 3636.65 | 100-YR | 2381.00 | 6592.57 | 6596.34 | 6596.34 | 6597.73 | 0.104607 | 9.44 | 252.22 | 92.88 | 1.00 |
| Kettle Creek | 3115.71 | 2-YR | 354.00 | 6585.47 | 6589.02 | | 6589.06 | 0.003484 | 1.47 | 235.63 | 121.59 | 0.18 |
| Kettle Creek | 3115.71 | 5-YR | 704.60 | 6585.47 | 6590.45 | | 6590.50 | 0.001932 | 1.53 | 420.88 | 137.69 | 0.14 |
| Kettle Creek | 3115.71 | 10-YR | 1073.00 | 6585.47 | 6591.69 | | 6591.76 | 0.001332 | 1.55 | 599.41 | 149.24 | 0.12 |
| Kettle Creek | 3115.71 | 25-YR | 1409.70 | 6585.47 | 6592.65 | | 6592.73 | 0.001084 | 1.58 | 747.56 | 158.05 | 0.12 |
| Kettle Creek | 3115.71 | 50-YR | 1972.40 | 6585.47 | 6593.70 | | 6593.80 | 0.001058 | 1.74 | 917.40 | 167.04 | 0.12 |
| Kettle Creek | 3115.71 | 100-YR | 2381.00 | 6585.47 | 6594.34 | | 6594.45 | 0.001069 | 1.86 | 1025.77 | 174.09 | 0.12 |
| Kettle Creek | 2957.59 | 2-YR | 354.00 | 6582.74 | 6586.82 | | 6587.60 | 0.045479 | 6.79 | 50.68 | 18.96 | 0.66 |
| Kettle Creek | 2957.59 | 5-YR | 704.60 | 6582.74 | 6588.24 | 6587.73 | 6589.50 | 0.039862 | 8.08 | 80.96 | 24.34 | 0.66 |
| Kettle Creek | 2957.59 | 10-YR | 1073.00 | 6582.74 | 6589.22 | 6589.00 | 6590.93 | 0.037660 | 8.91 | 107.60 | 29.74 | 0.66 |
| Kettle Creek | 2957.59 | 25-YR | 1409.70 | 6582.74 | 6590.16 | 6590.16 | 6592.00 | 0.029911 | 8.79 | 137.55 | 34.66 | 0.60 |
| Kettle Creek | 2957.59 | 50-YR | 1972.40 | 6582.74 | 6591.52 | 6591.52 | 6593.13 | 0.022892 | 8.71 | 201.24 | 61.95 | 0.54 |
| Kettle Creek | 2957.59 | 100-YR | 2381.00 | 6582.74 | 6591.99 | 6591.99 | 6593.75 | 0.021745 | 8.82 | 232.06 | 67.51 | 0.53 |
| Kettle Creek | 2731.34 | 2-YR | 354.00 | 6579.12 | 6583.41 | | 6583.59 | 0.008741 | 3.21 | 105.13 | 39.32 | 0.30 |
| Kettle Creek | 2731.34 | 5-YR | 704.60 | 6579.12 | 6584.34 | | 6584.73 | 0.011926 | 4.37 | 146.35 | 48.54 | 0.36 |
| Kettle Creek | 2731.34 | 10-YR | 1073.00 | 6579.12 | 6584.94 | | 6585.61 | 0.014531 | 5.24 | 176.94 | 52.41 | 0.41 |
| Kettle Creek | 2731.34 | 25-YR | 1409.70 | 6579.12 | 6585.39 | 6584.16 | 6586.31 | 0.016387 | 5.88 | 200.86 | 55.38 | 0.44 |
| Kettle Creek | 2731.34 | 50-YR | 1972.40 | 6579.12 | 6585.99 | 6585.20 | 6587.32 | 0.019024 | 6.79 | 235.85 | 60.21 | 0.48 |
| Kettle Creek | 2731.34 | 100-YR | 2381.00 | 6579.12 | 6586.35 | 6585.86 | 6587.99 | 0.020698 | 7.35 | 257.97 | 63.06 | 0.5 |



HEC-RAS Plan: Historic River: Kettle Creek Reach: Kettle Creek (Continued)

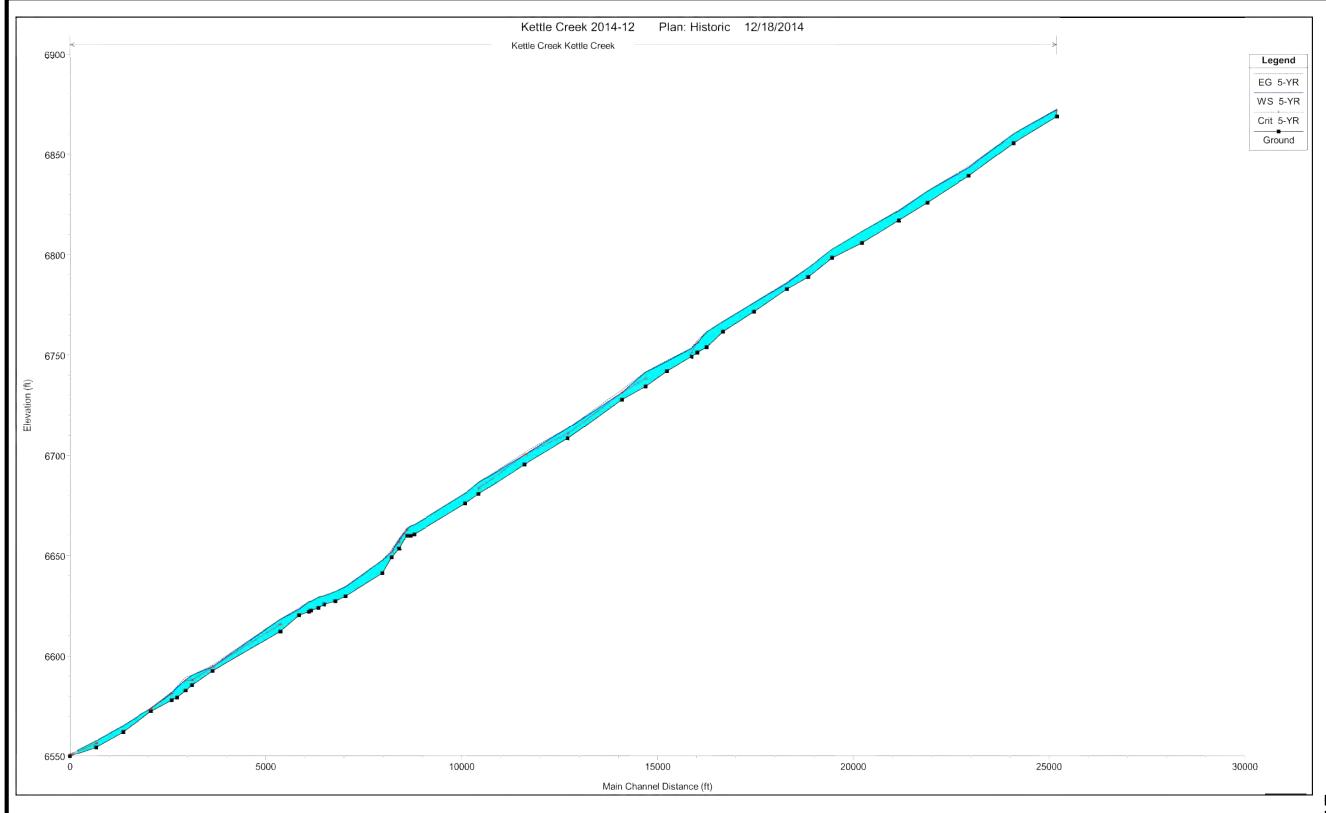
| Reach | River Sta | Profile | Q Total | Min Ch El | W.S. Elev | Crit W.S. | E.G. Elev | E.G. Slope | Vel Chnl | Flow Area | Top Width | Froude # Chl |
|--------------|-----------|---------|---------|-----------|-----------|-----------|-----------|------------|----------|-----------|-----------|--------------|
| | | | (cfs) | (ft) | (ft) | (ft) | (ft) | (ft/ft) | (ft/s) | (sq ft) | (ft) | |
| Kettle Creek | 2597.25 | 2-YR | 354.00 | 6577.88 | 6581.02 | 6580.64 | 6581.20 | 0.055461 | 3.39 | 104.29 | 107.64 | 0.61 |
| Kettle Creek | 2597.25 | 5-YR | 704.60 | 6577.88 | 6581.62 | 6581.18 | 6581.86 | 0.048160 | 3.95 | 178.52 | 134.67 | 0.60 |
| Kettle Creek | 2597.25 | 10-YR | 1073.00 | 6577.88 | 6582.01 | 6581.53 | 6582.35 | 0.046669 | 4.61 | 232.45 | 139.01 | 0.62 |
| Kettle Creek | 2597.25 | 25-YR | 1409.70 | 6577.88 | 6582.29 | 6581.80 | 6582.71 | 0.047913 | 5.16 | 271.74 | 140.88 | 0.64 |
| Kettle Creek | 2597.25 | 50-YR | 1972.40 | 6577.88 | 6582.69 | 6582.18 | 6583.26 | 0.050104 | 5.94 | 327.77 | 143.50 | 0.67 |
| Kettle Creek | 2597.25 | 100-YR | 2381.00 | 6577.88 | 6582.93 | 6582.42 | 6583.62 | 0.052246 | 6.46 | 362.15 | 145.09 | 0.70 |
| Kettle Creek | 2067.56 | 2-YR | 354.00 | 6572.37 | 6573.48 | 6573.27 | 6573.67 | 0.006821 | 0.80 | 110.53 | 146.69 | 0.19 |
| Kettle Creek | 2067.56 | 5-YR | 704.60 | 6572.37 | 6573.95 | 6573.70 | 6574.19 | 0.007371 | 0.98 | 196.15 | 224.10 | 0.21 |
| Kettle Creek | 2067.56 | 10-YR | 1073.00 | 6572.37 | 6574.26 | 6574.09 | 6574.53 | 0.007628 | 1.27 | 279.70 | 286.19 | 0.23 |
| Kettle Creek | 2067.56 | 25-YR | 1409.70 | 6572.37 | 6574.43 | 6574.23 | 6574.77 | 0.007727 | 1.42 | 328.69 | 287.15 | 0.23 |
| Kettle Creek | 2067.56 | 50-YR | 1972.40 | 6572.37 | 6574.68 | 6574.47 | 6575.13 | 0.007828 | 1.63 | 401.36 | 288.57 | 0.24 |
| Kettle Creek | 2067.56 | 100-YR | 2381.00 | 6572.37 | 6574.85 | 6574.65 | 6575.37 | 0.007839 | 1.76 | 449.76 | 289.51 | 0.25 |
| Kettle Creek | 1361.33 | 2-YR | 354.00 | 6562.11 | 6564.71 | | 6564.79 | 0.032083 | 2.28 | 155.56 | 196.41 | 0.45 |
| Kettle Creek | 1361.33 | 5-YR | 704.60 | 6562.11 | 6565.18 | | 6565.30 | 0.027398 | 2.82 | 250.24 | 203.79 | 0.45 |
| Kettle Creek | 1361.33 | 10-YR | 1073.00 | 6562.11 | 6565.60 | | 6565.76 | 0.024637 | 3.19 | 336.78 | 210.32 | 0.44 |
| Kettle Creek | 1361.33 | 25-YR | 1409.70 | 6562.11 | 6565.93 | | 6566.12 | 0.023139 | 3.45 | 408.20 | 215.39 | 0.44 |
| Kettle Creek | 1361.33 | 50-YR | 1972.40 | 6562.11 | 6566.44 | | 6566.66 | 0.021278 | 3.80 | 518.80 | 222.31 | 0.44 |
| Kettle Creek | 1361.33 | 100-YR | 2381.00 | 6562.11 | 6566.76 | | 6567.01 | 0.020307 | 4.03 | 591.30 | 224.27 | 0.44 |
| Kettle Creek | 670.23 | 2-YR | 354.00 | 6554.40 | 6557.16 | 6556.20 | 6557.20 | 0.005494 | 1.44 | 239.86 | 174.10 | 0.21 |
| Kettle Creek | 670.23 | 5-YR | 704.60 | 6554.40 | 6557.81 | | 6557.88 | 0.005714 | 1.87 | 355.41 | 183.27 | 0.22 |
| Kettle Creek | 670.23 | 10-YR | 1073.00 | 6554.40 | 6558.32 | | 6558.43 | 0.005904 | 2.19 | 450.43 | 190.11 | 0.24 |
| Kettle Creek | 670.23 | 25-YR | 1409.70 | 6554.40 | 6558.70 | | 6558.85 | 0.006032 | 2.42 | 524.49 | 194.28 | 0.24 |
| Kettle Creek | 670.23 | 50-YR | 1972.40 | 6554.40 | 6559.25 | | 6559.45 | 0.006240 | 2.74 | 631.42 | 199.94 | 0.26 |
| Kettle Creek | 670.23 | 100-YR | 2381.00 | 6554.40 | 6559.59 | | 6559.84 | 0.006379 | 2.95 | 700.27 | 203.50 | 0.26 |
| Kettle Creek | 6.23 | 2-YR | 354.00 | 6550.00 | 6550.73 | 6550.40 | 6550.79 | 0.018792 | 1.63 | 206.21 | 297.05 | 0.34 |
| Kettle Creek | 6,23 | 5-YR | 704.60 | 6550.00 | 6551.08 | 6550.63 | 6551.18 | 0.018806 | 2.11 | 312.90 | 311.00 | 0.36 |
| Kettle Creek | 6.23 | 10-YR | 1073.00 | 6550.00 | 6551.37 | 6550.83 | 6551.52 | 0.018814 | 2.44 | 405.23 | 325.03 | 0.38 |
| Kettle Creek | 6.23 | 25-YR | 1409.70 | 6550.00 | 6551.60 | 6550.99 | 6551.78 | 0.018835 | 2.68 | 480.15 | 337.18 | 0.38 |
| Kettle Creek | 6.23 | 50-YR | 1972.40 | 6550.00 | 6551.91 | 6551.23 | 6552.15 | 0.018811 | 3.04 | 587.01 | 345.75 | 0.40 |
| Kettle Creek | 6,23 | 100-YR | 2381.00 | 6550.00 | 6552.11 | 6551.40 | 6552.39 | 0.018804 | 3.26 | 655.86 | 349.99 | 0.40 |







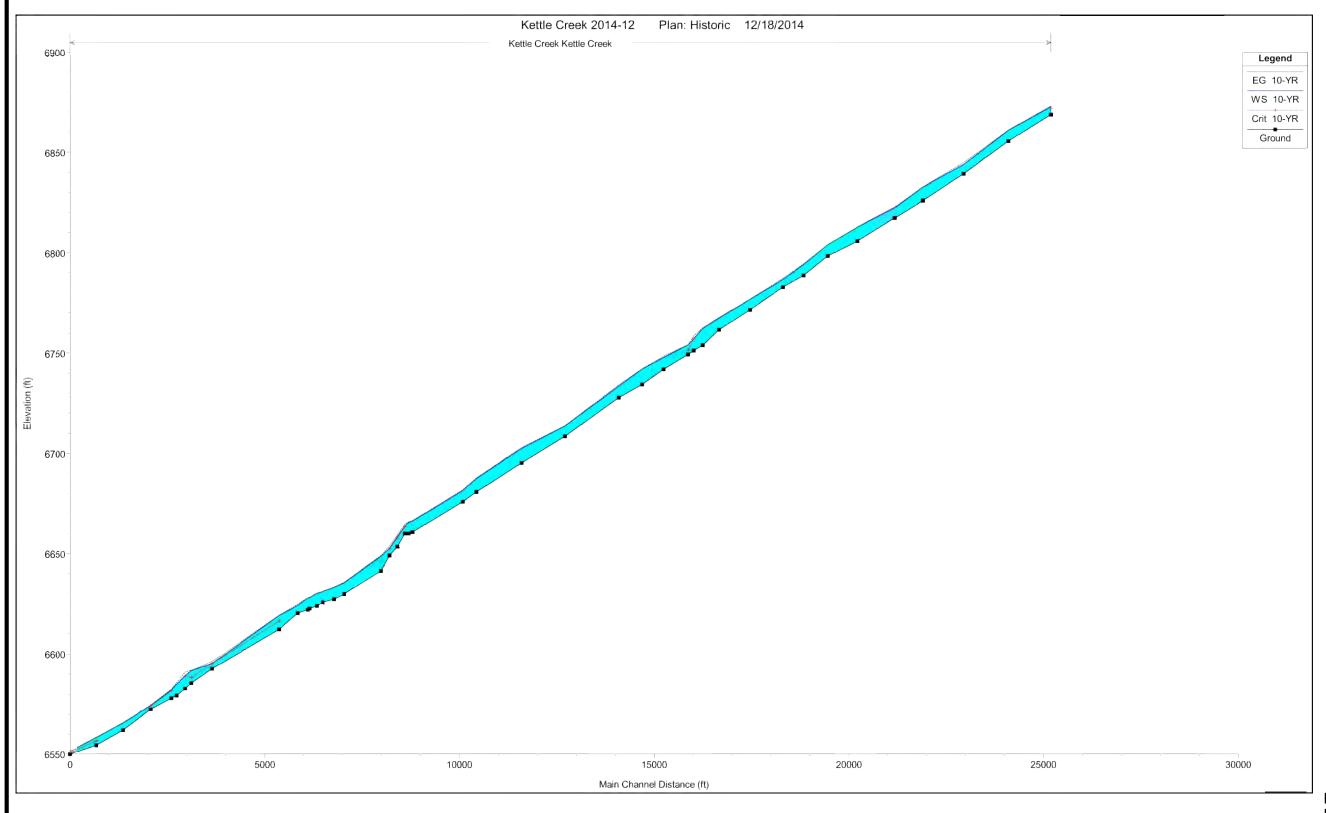


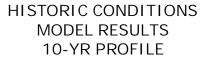




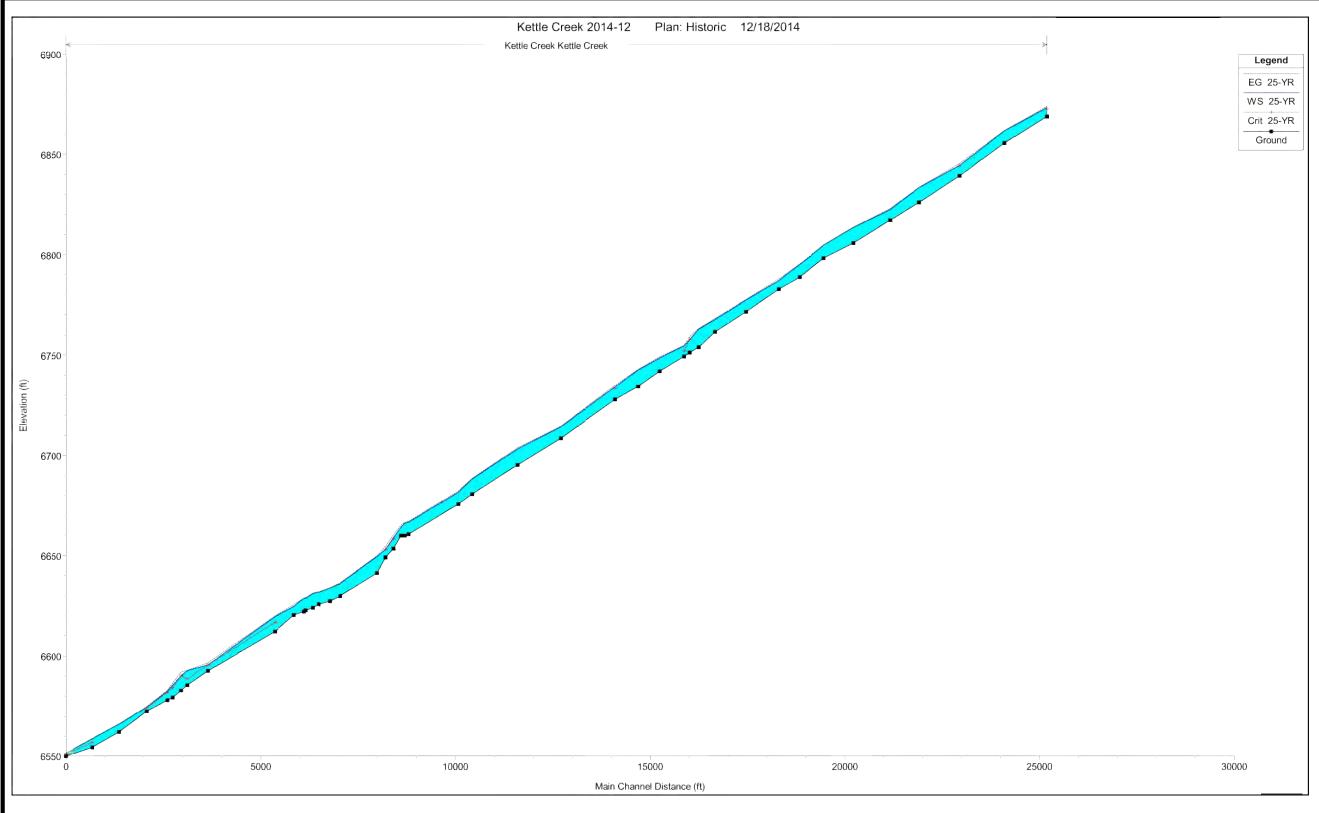


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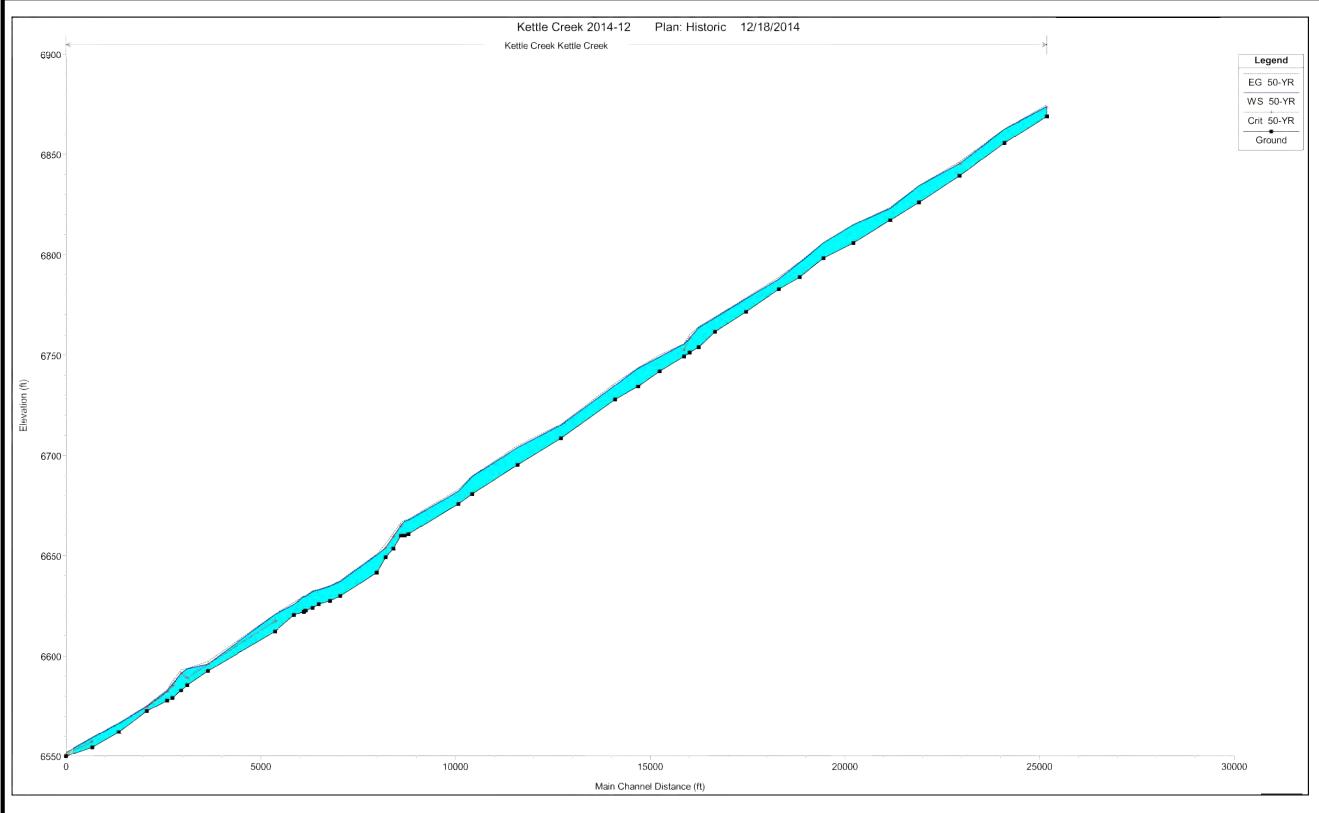


HISTORIC CONDITIONS

HYDRAULIC RESULTS -HISTORIC KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 C-15



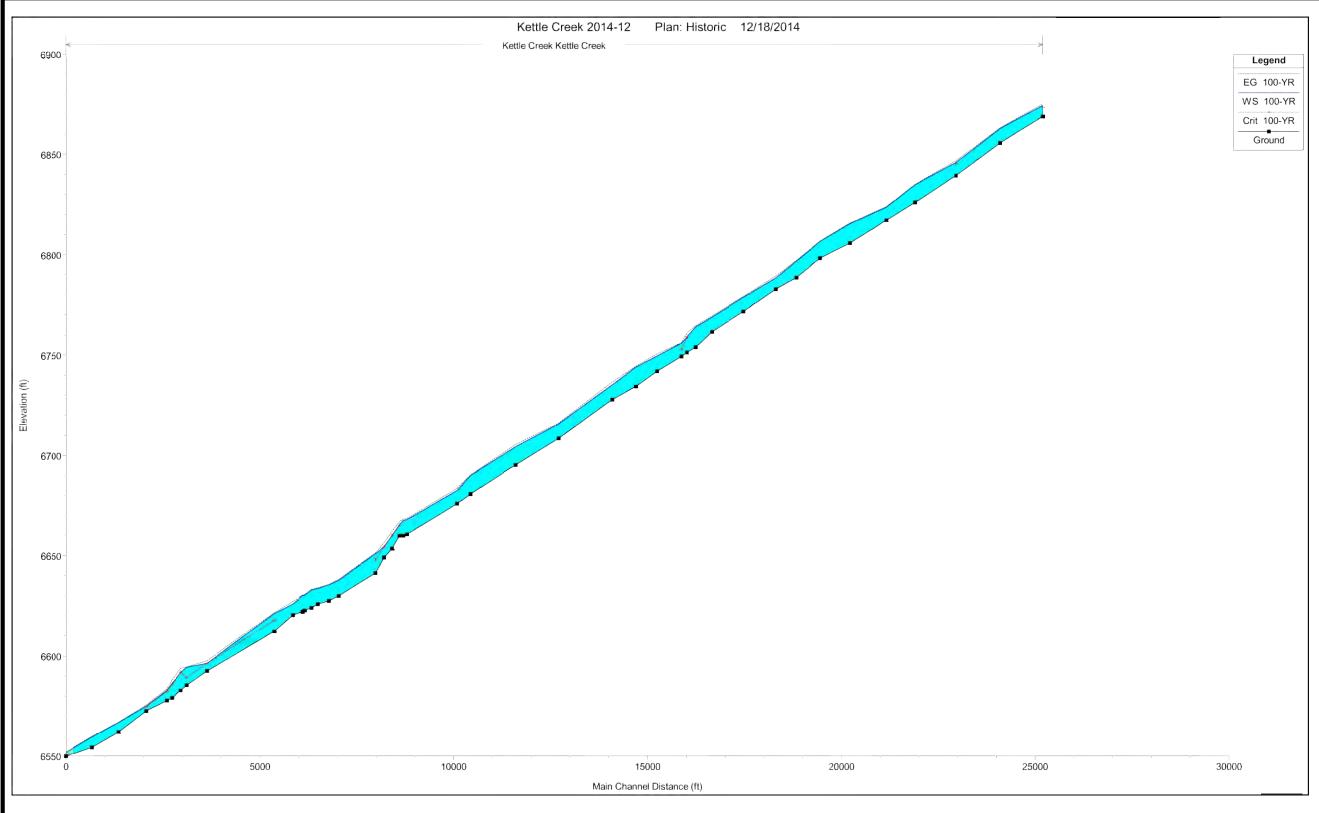
MODEL RESULTS 25-YR PROFILE Centennial 303-740-9393 • Colorado Springs 719-593-2593 Fort Collins 970-491-9888 • www.jrengineering.com

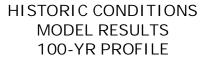




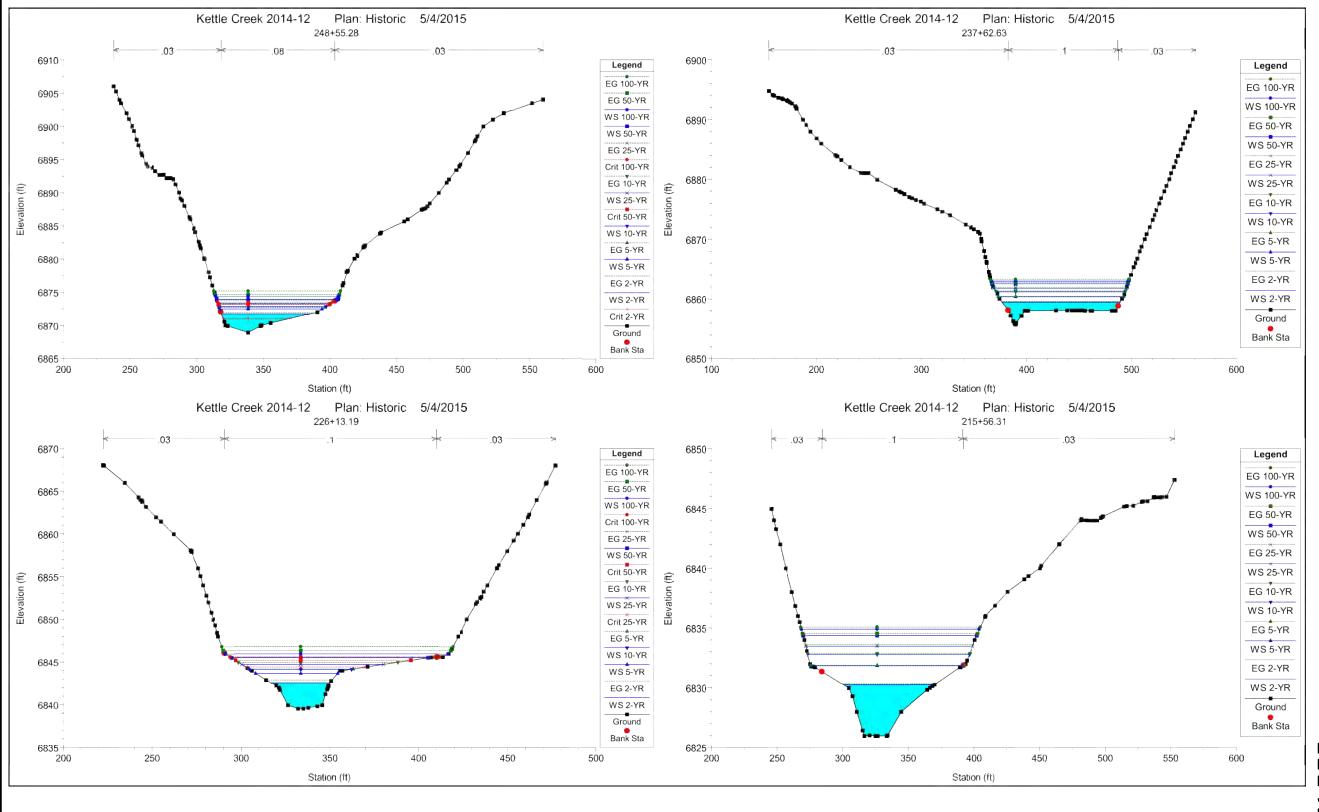


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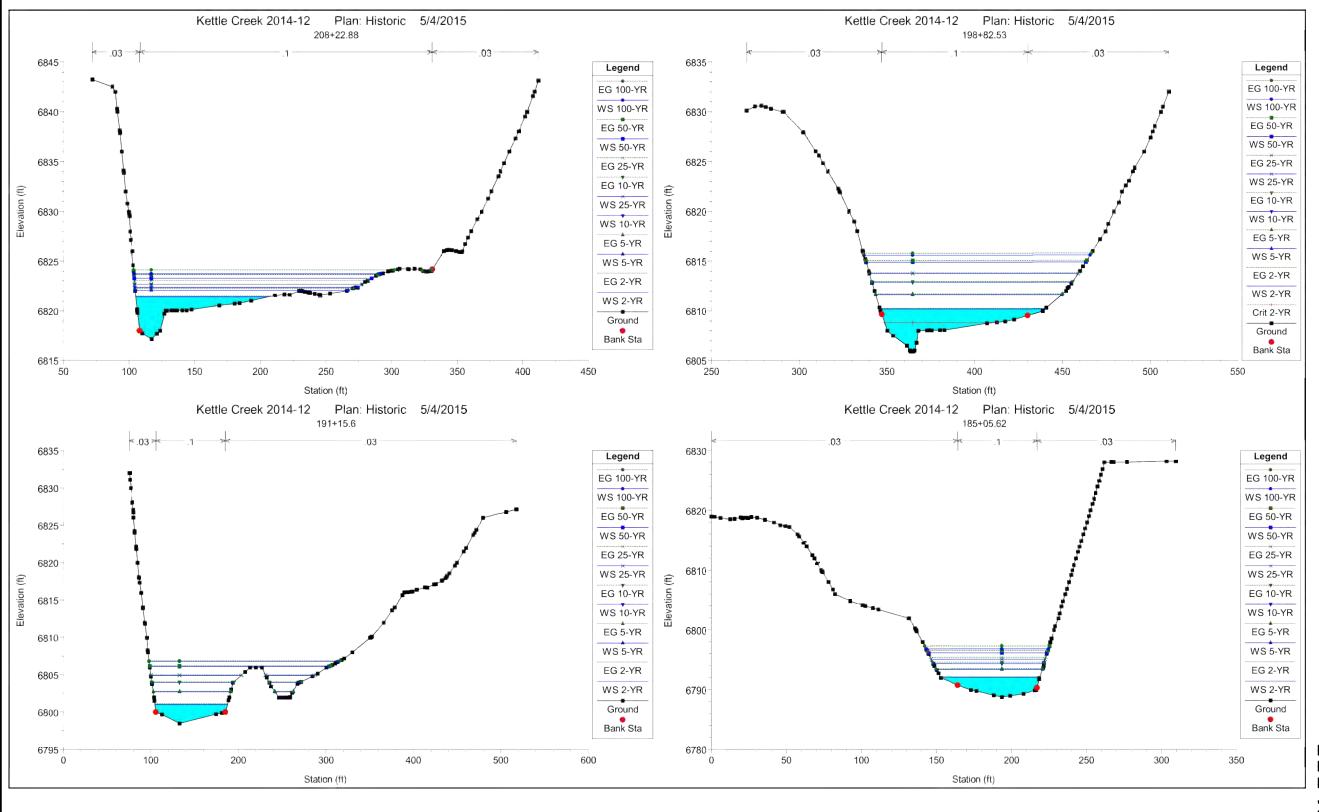


HISTORIC CONDITIONS MODEL RESULTS

HYDRAULIC RESULTS — HISTORIC KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 C-18

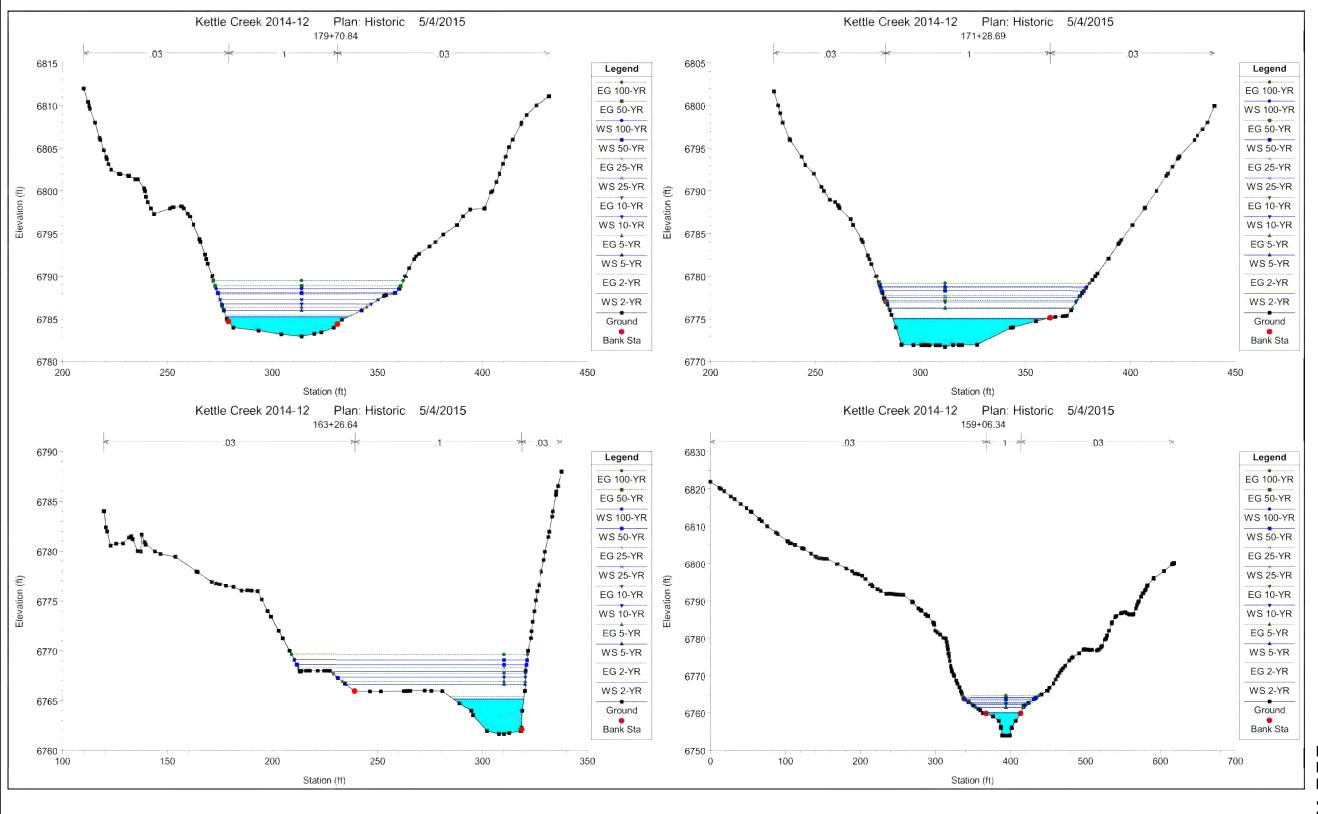


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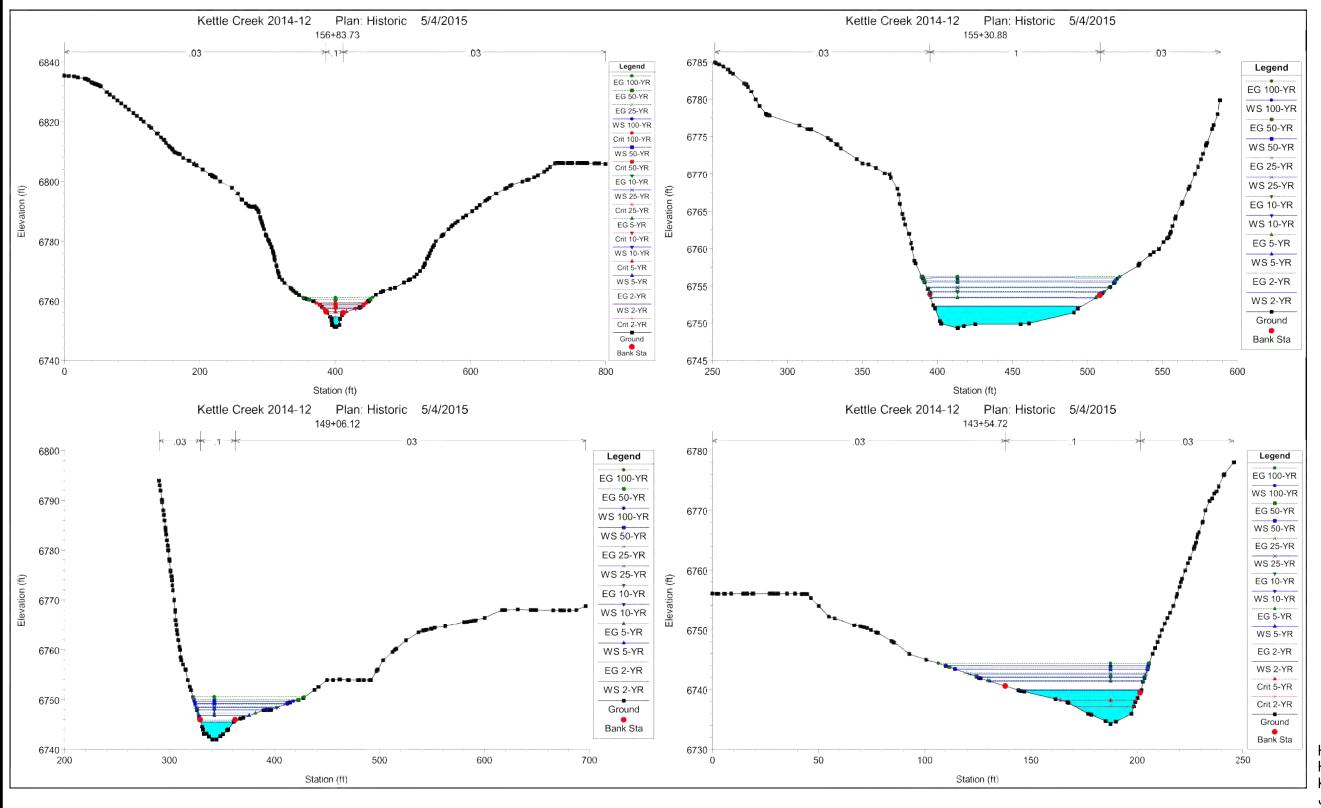






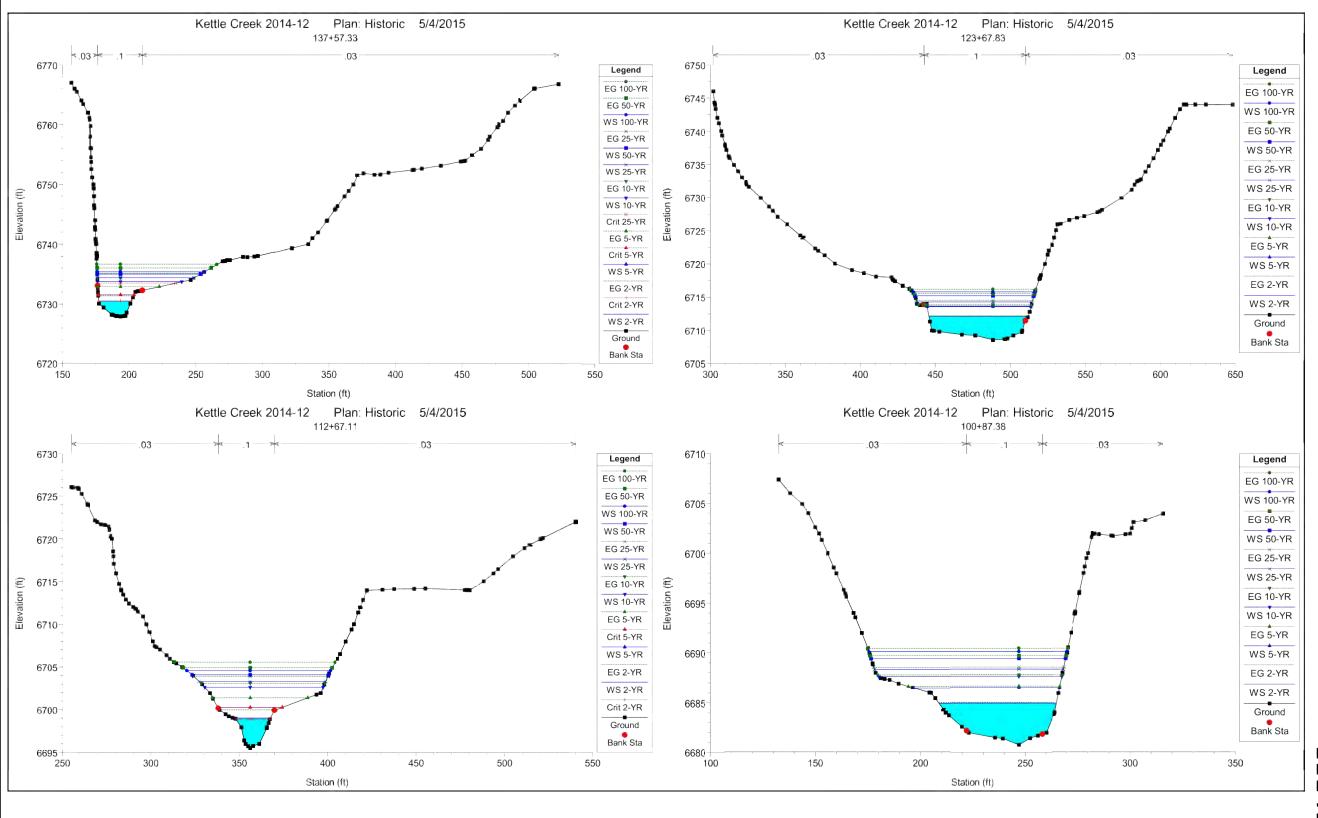






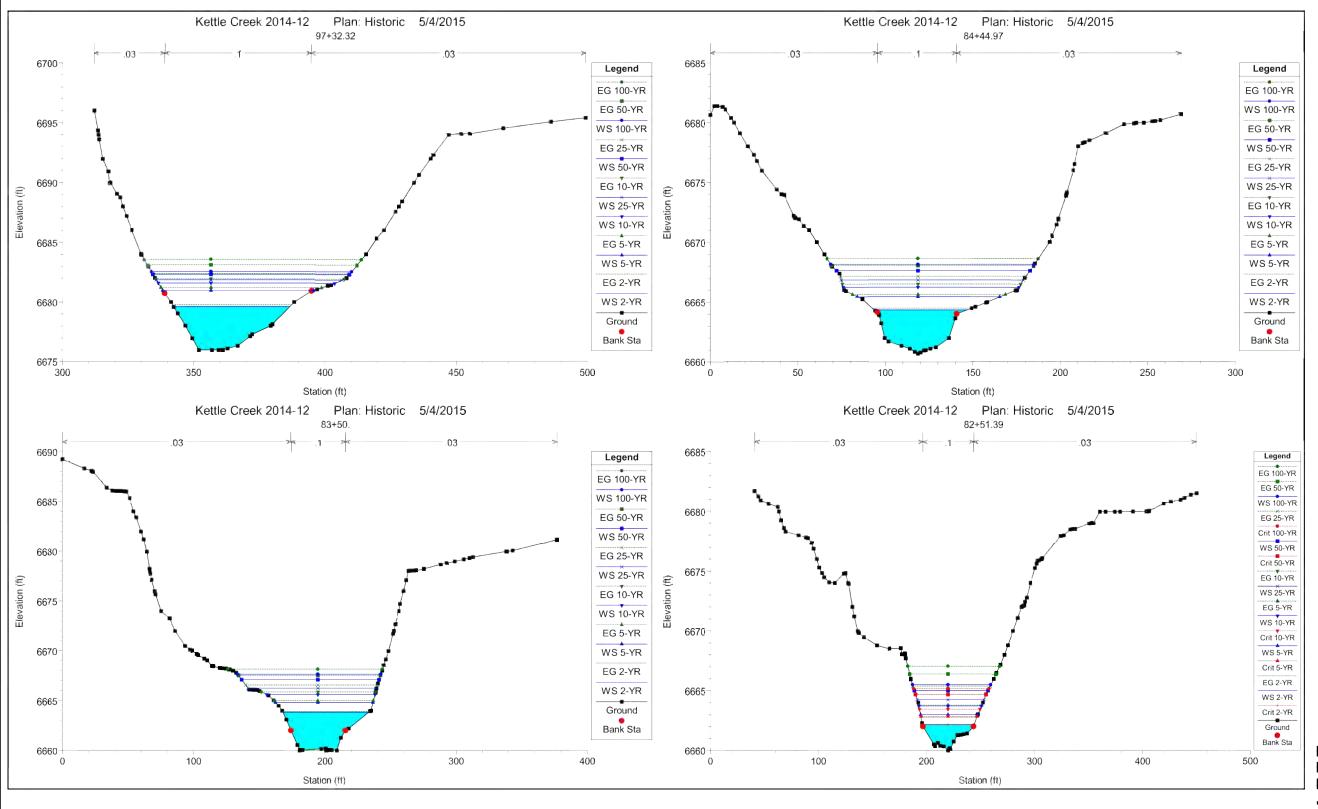






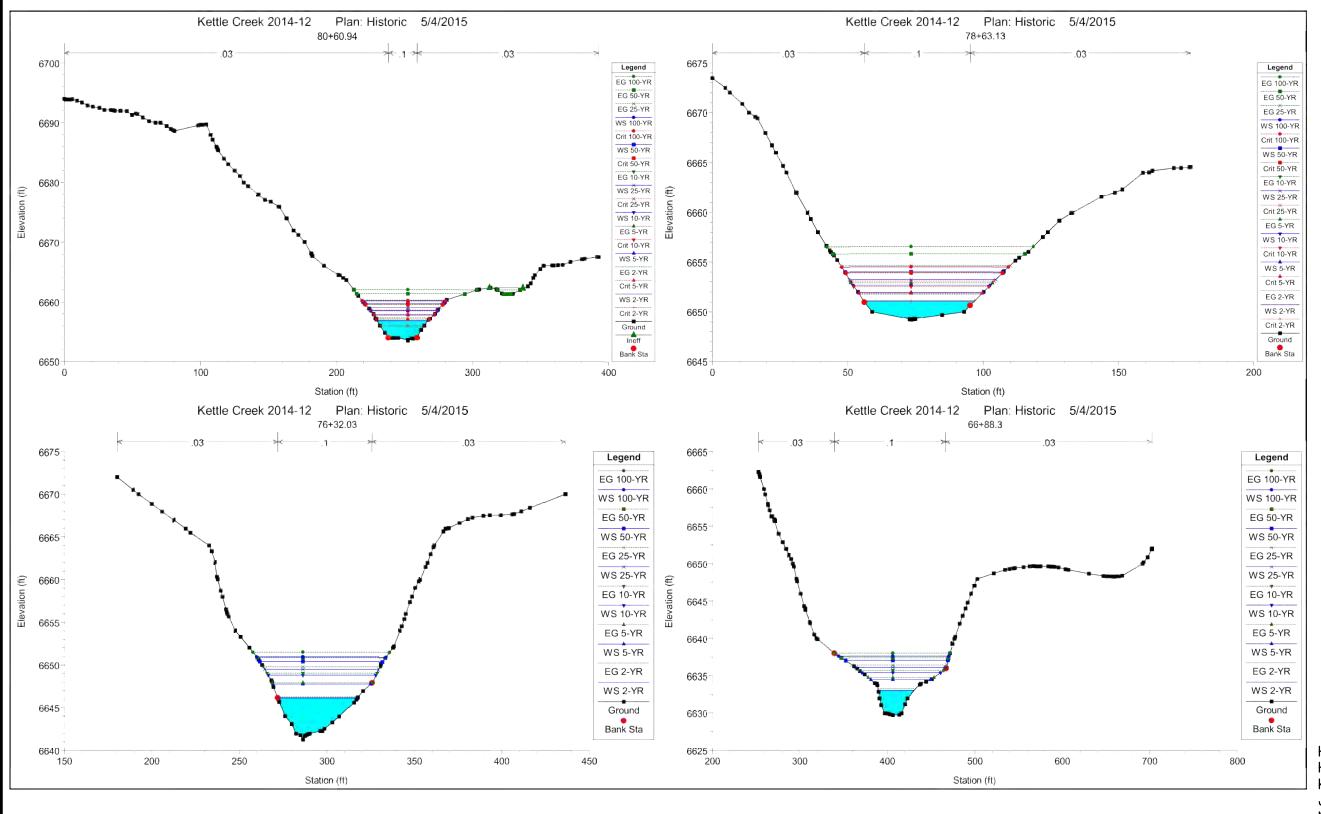






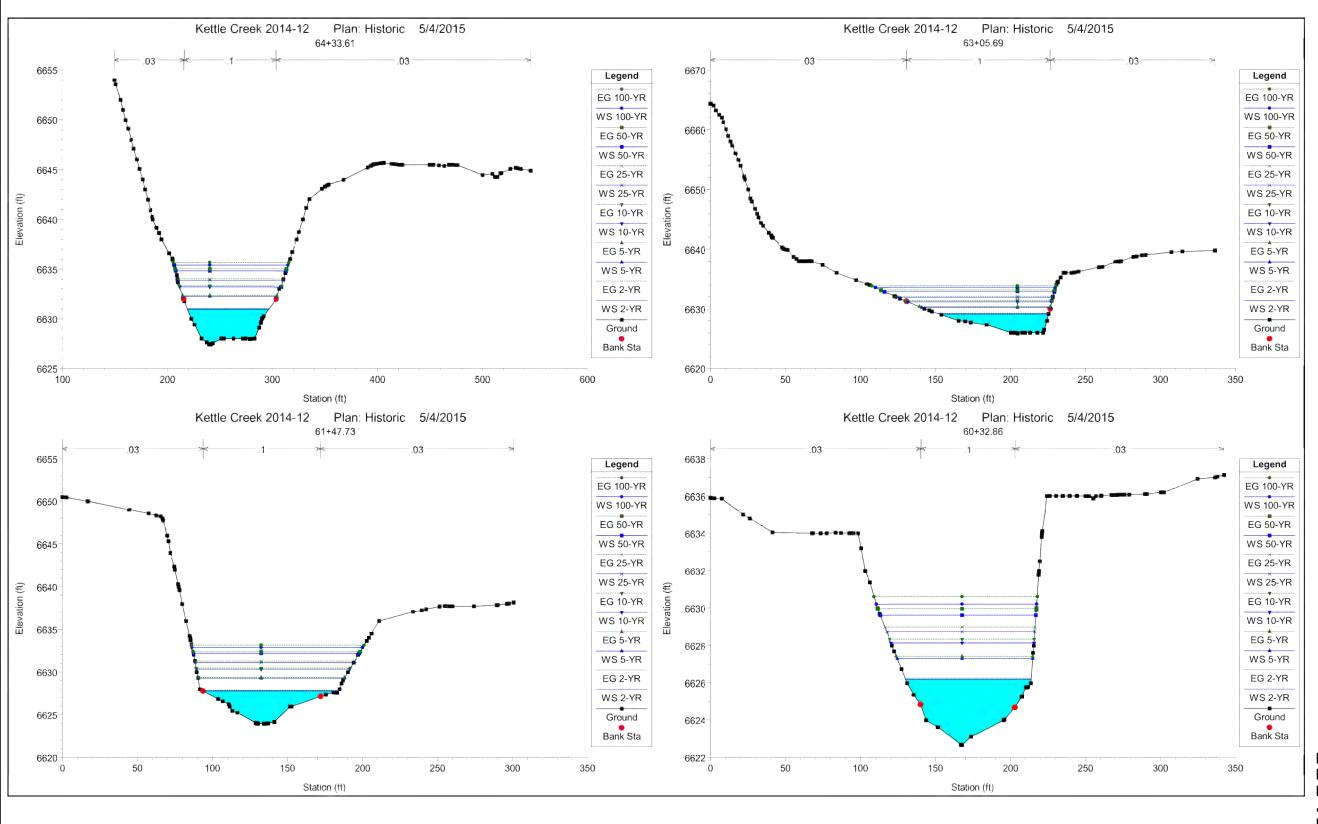






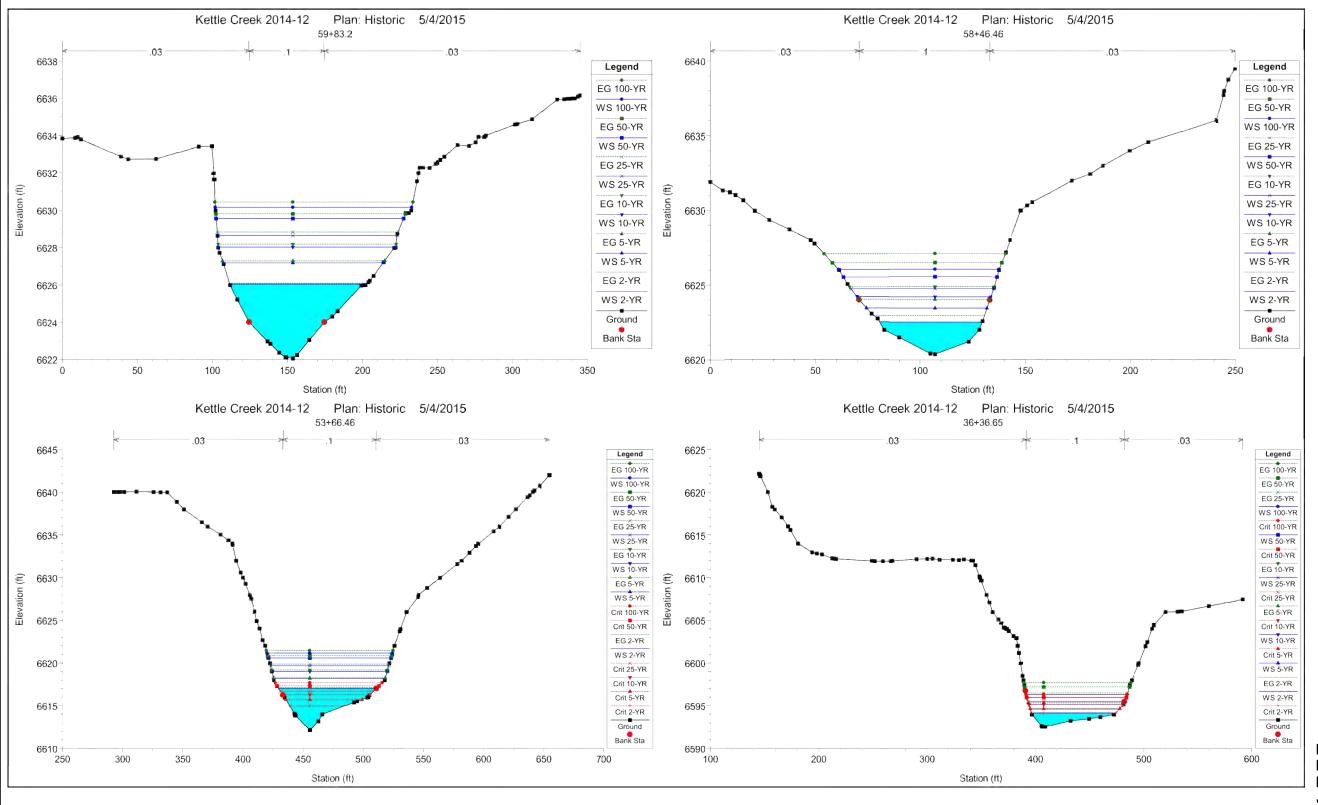






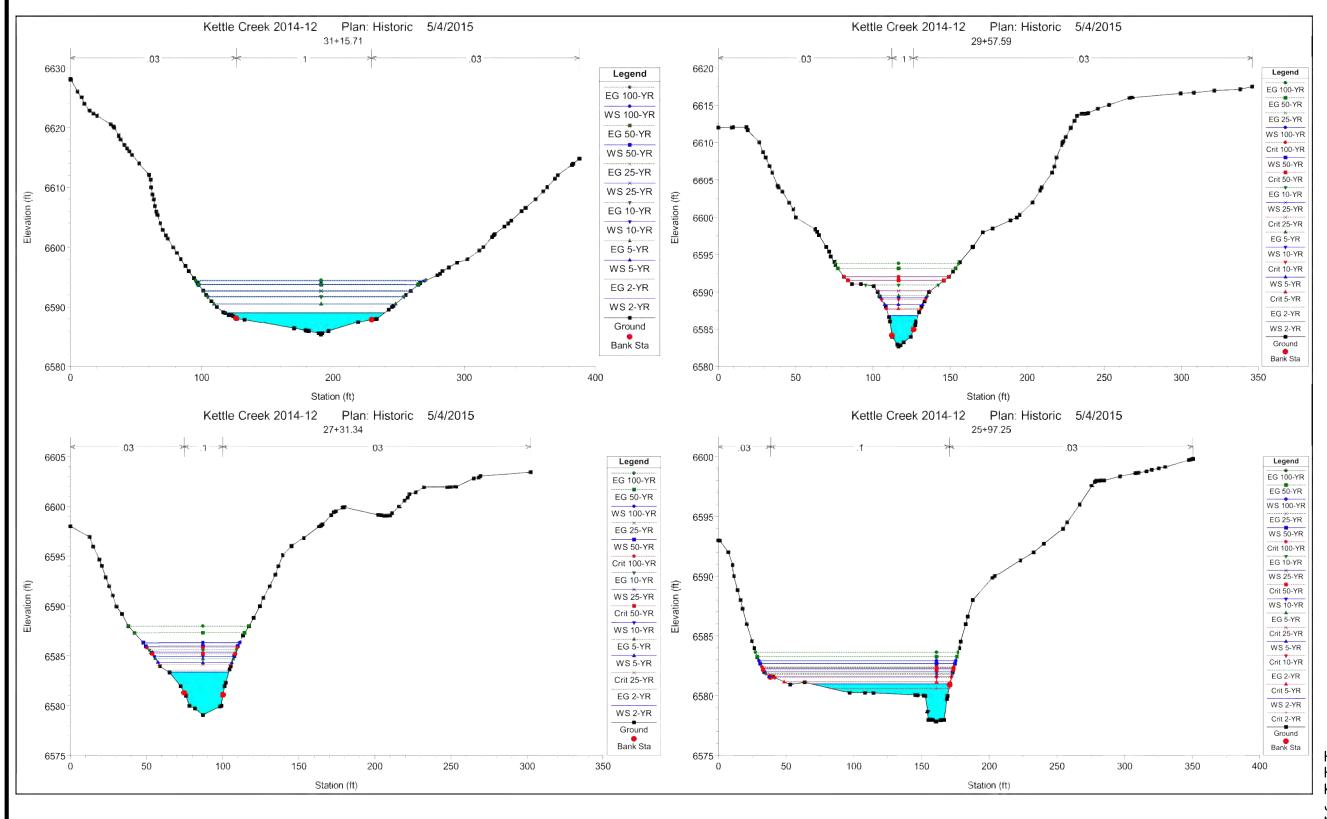






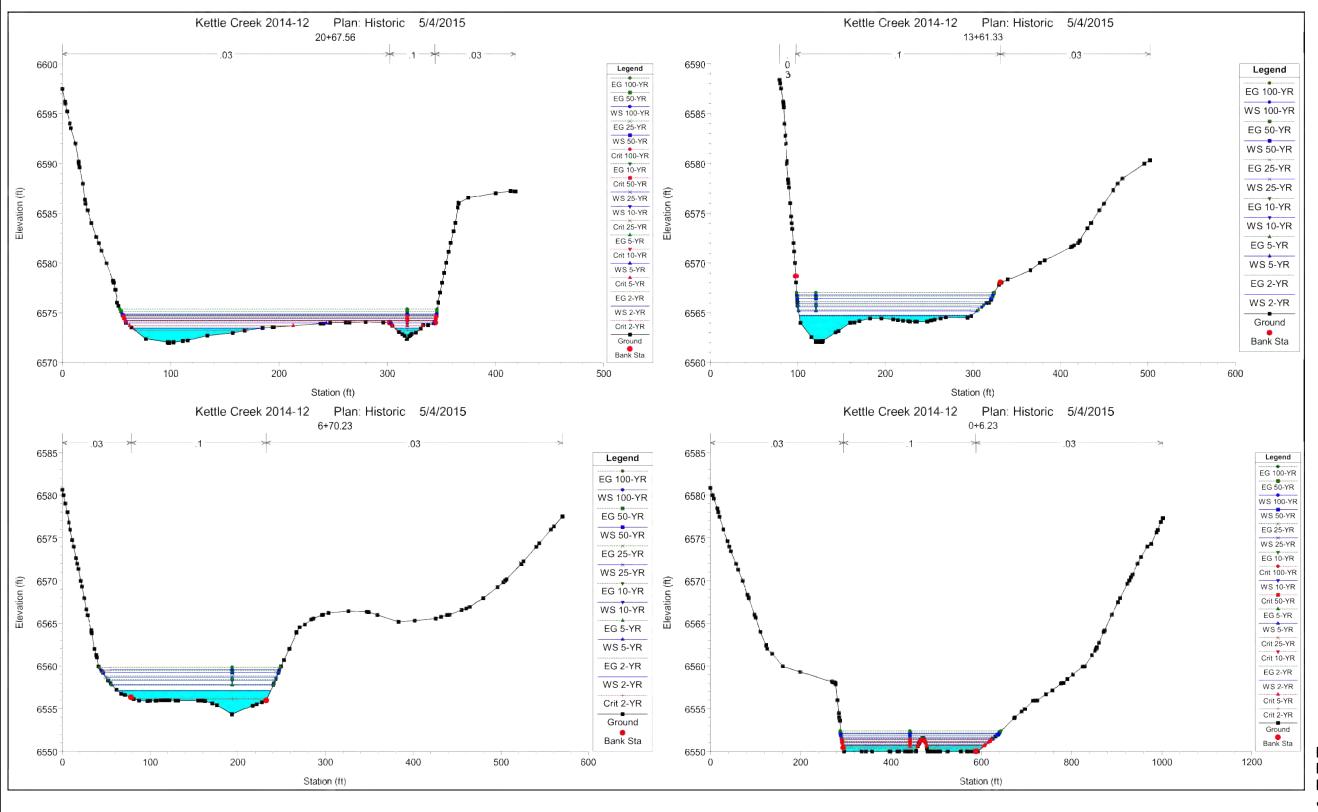
















HEC-RAS Plan: Existing River: Kettle Creek Reach: Kettle Creek

| Reach | River Sta | Profile | Q Total | Min Ch El | W.S. Elev | Crit W.S. | E.G. Elev | E.G. Slope | Vel Chnl | Flow Area | Top Width | Froude # Chl |
|--------------|-----------|---------|---------|-----------|-----------|-----------|-----------|------------|----------|-----------|-----------|--------------|
| | | | (cfs) | (ft) | (ft) | (ft) | (ft) | (ft/ft) | (ft/s) | (sq ft) | (ft) | |
| Kettle Creek | 24855.28 | 2-YR | 1122.90 | 6868.95 | 6873.07 | | 6873.58 | 0.029829 | 5.75 | 195.59 | 82.07 | 0.65 |
| Kettle Creek | 24855.28 | 5-YR | 1711.40 | 6868.95 | 6873.81 | 6873.05 | 6874.49 | 0.029547 | 6.61 | 258.97 | 88.97 | 0.67 |
| Kettle Creek | 24855.28 | 10-YR | 2258.20 | 6868.95 | 6874.46 | 6873.58 | 6875.24 | 0.026301 | 7.10 | 317.92 | 92.16 | 0.65 |
| Kettle Creek | 24855,28 | 25-YR | 2725.50 | 6868.95 | 6874.94 | 6873.98 | 6875.82 | 0.024792 | 7.49 | 363.05 | 93.79 | 0.65 |
| Kettle Creek | 24855.28 | 50-YR | 3471.20 | 6868.95 | 6875.75 | 6874.52 | 6876.72 | 0.021327 | 7.83 | 440.48 | 96.58 | 0.62 |
| Kettle Creek | 24855.28 | 100-YR | 3992.10 | 6868.95 | 6876.25 | | 6877.29 | 0.020026 | 8.09 | 488.91 | 98.22 | 0.61 |
| Kettle Creek | 23762.63 | 2-YR | 1144.00 | 6855.75 | 6861.44 | | 6861.59 | 0.005648 | 2.60 | 408.50 | 124.34 | 0.24 |
| Kettle Creek | 23762.63 | 5-YR | 1744.80 | 6855.75 | 6862.36 | | 6862.58 | 0.005592 | 3.01 | 525.28 | 128.58 | 0.25 |
| Kettle Creek | 23762.63 | 10-YR | 2303.50 | 6855.75 | 6863.00 | | 6863.30 | 0.005915 | 3.39 | 607.64 | 130.74 | 0.26 |
| Kettle Creek | 23762.63 | 25-YR | 2781.20 | 6855.75 | 6863.49 | | 6863.86 | 0.006096 | 3.66 | 672.98 | 132.72 | 0.27 |
| Kettle Creek | 23762.63 | 50-YR | 3539.60 | 6855.75 | 6864.09 | | 6864.57 | 0.006744 | 4.11 | 752.85 | 134.98 | 0.29 |
| Kettle Creek | 23762.63 | 100-YR | 4068.60 | 6855.75 | 6864.48 | | 6865.04 | 0.007090 | 4.39 | 805.18 | 136.32 | 0.30 |
| Kettle Creek | 22613.19 | 2-YR | 1144.00 | 6839.60 | 6844.57 | | 6845.35 | 0.079777 | 7.08 | 161.52 | 72.20 | 0.83 |
| Kettle Creek | 22613.19 | 5-YR | 1744.80 | 6839.60 | 6845.42 | 6845.12 | 6846.26 | 0.085640 | 7.34 | 237.71 | 106.85 | 0.87 |
| Kettle Creek | 22613.19 | 10-YR | 2303.50 | 6839.60 | 6846.03 | 6845.68 | 6846.89 | 0.071601 | 7.43 | 310.59 | 126.15 | 0.81 |
| Kettle Creek | 22613.19 | 25-YR | 2781.20 | 6839.60 | 6846.39 | 6846.05 | 6847.34 | 0.066647 | 7.80 | 355.83 | 127.99 | 0.80 |
| Kettle Creek | 22613.19 | 50-YR | 3539.60 | 6839.60 | 6847.11 | | 6848.10 | 0.049388 | 7.78 | 449.53 | 131.24 | 0.72 |
| Kettle Creek | 22613.19 | 100-YR | 4068.60 | 6839.60 | 6847.55 | | 6848.59 | 0.043285 | 7.85 | 507.89 | 133.17 | 0.68 |
| Kettle Creek | 21556.31 | 2-YR | 1154.20 | 6825.98 | 6833.10 | | 6833.20 | 0.004293 | 2.47 | 458.98 | 124.83 | 0.22 |
| Kettle Creek | 21556.31 | 5-YR | 1760.20 | 6825.98 | 6834.18 | | 6834.32 | 0.004117 | 2.83 | 596.76 | 131.21 | 0.22 |
| Kettle Creek | 21556.31 | 10-YP | 2323.80 | 6825.98 | 6834.94 | | 6835.14 | 0.004206 | 3.14 | 699.05 | 136.19 | 0.23 |
| Kettle Creek | 21556.31 | 25-YR | 2805.50 | 6825.98 | 6835.55 | | 6835.79 | 0.004171 | 3.34 | 783.46 | 140.16 | 0.23 |
| Kettle Creek | 21556.31 | 50-YR | 3570.00 | 6825.98 | 6836.25 | | 6836.56 | 0.004526 | 3.72 | 883.27 | 145.82 | 0.24 |
| Kettle Creek | 21556.31 | 100-YR | 4103.10 | 6825.98 | 6836.70 | | 6837.05 | 0.004715 | 3.95 | 949.48 | 150.55 | 0.25 |
| Kettle Creek | 20822.88 | 2-YR | 1154.20 | 6817.21 | 6822.51 | 6822.10 | 6822.84 | 0.028017 | 3.61 | 302.83 | 171.40 | 0.48 |
| Kettle Creek | 20822.88 | 5-YR | 1760.20 | 6817.21 | 6823.12 | | 6823.50 | 0.025462 | 4.10 | 410.71 | 179.31 | 0.48 |
| Kettle Creek | 20822.88 | 10-YR | 2323.80 | 6817.21 | 6823.77 | | 6824.15 | 0.020618 | 4.21 | 530.55 | 190.21 | 0.44 |
| Kettle Creek | 20822.88 | 25-YR | 2805.50 | 6817.21 | 6824.43 | | 6824.78 | 0.017689 | 4.03 | 668.52 | 229.08 | 0.42 |
| Kettle Creek | 20822.88 | 50-YR | 3570.00 | 6817.21 | 6825.19 | | 6825.52 | 0.013398 | 4.09 | 843.52 | 233.36 | 0.38 |
| Kettle Creek | 20822.88 | 100-YR | 4103.10 | 6817.21 | 6825.70 | | 6826.03 | 0.011418 | 4.12 | 964.25 | 236.25 | 0.35 |
| Kettle Creek | 19882.53 | 2-YR | 1149.20 | 6805.92 | 6813.22 | | 6813.34 | 0.002287 | 2.06 | 489.51 | 116.16 | 0.16 |
| Kettle Creek | 19882.53 | 5-YR | 1751.90 | 6805.92 | 6814.64 | | 6814.79 | 0.001910 | 2.22 | 659.32 | 123.94 | 0.15 |
| Kettle Creek | 19882.53 | 10-YR | 2312.20 | 6805.92 | 6815.65 | | 6815.84 | 0.001818 | 2.39 | 787.27 | 129.36 | 0.15 |
| Kettle Creek | 19882.53 | 25-YR | 2792.50 | 6805.92 | 6816.36 | | 6816.59 | 0.001811 | 2.53 | 881.04 | 133.12 | 0.16 |



HEC-RAS Plan: Existing River: Kettle Creek Reach: Kettle Creek (Continued)

| Reach | River Sta | Profile | Q Total | Min Ch El | W.S. Elev | Crit W.S. | E.G. Elev | E.G. Slope | Vel Chnl | Flow Area | Top Width | Froude # Chl |
|--------------|-----------|---------|---------|-----------|-----------|-----------|-----------|------------|----------|-----------|-----------|--------------|
| | | | (cfs) | (ft) | (ft) | (ft) | (ft) | (ft/ft) | (ft/s) | (sq ft) | (ft) | |
| Kettle Creek | 19882.53 | 50-YR | 3557.00 | 6805.92 | 6817.33 | | 6817.62 | 0.001841 | 2.75 | 1012.11 | 138.06 | 0.16 |
| Kettle Creek | 19882.53 | 100-YR | 4090.50 | 6805.92 | 6817.92 | | 6818.24 | 0.001878 | 2.90 | 1094.16 | 141.30 | 0.16 |
| Kettle Creek | 19115.6 | 2-YR | 1151.10 | 6798.52 | 6804.47 | | 6804.55 | 0.002197 | 2.08 | 507.88 | 142.27 | 0.16 |
| Kettle Creek | 19115.6 | 5-YR | 1755.60 | 6798.52 | 6805.89 | | 6805.99 | 0.001549 | 2.06 | 741.52 | 184.54 | 0.14 |
| Kettle Creek | 19115.6 | 10-YR | 2317.70 | 6798.52 | 6806.86 | | 6806.97 | 0.001273 | 2.04 | 942.95 | 217.14 | 0.13 |
| Kettle Creek | 19115.6 | 25-YR | 2797.90 | 6798.52 | 6807.53 | | 6807.65 | 0.001121 | 2.03 | 1091.17 | 226.86 | 0.12 |
| Kettle Creek | 19115.6 | 50-YR | 3559.70 | 6798.52 | 6808.46 | | 6808.60 | 0.000971 | 2.03 | 1307.16 | 238.12 | 0.12 |
| Kettle Creek | 19115.6 | 100-YR | 4090.90 | 6798.52 | 6809.04 | | 6809.20 | 0.000903 | 2.04 | 1448.23 | 245.02 | 0.11 |
| Kettle Creek | 18505.62 | 2-YR | 1151.10 | 6788.84 | 6794.60 | | 6794.88 | 0.004990 | 3.09 | 321.21 | 74.52 | 0.24 |
| Kettle Creek | 18505.62 | 5-YR | 1755.60 | 6788.84 | 6795.81 | | 6796.22 | 0.004891 | 3.53 | 413.73 | 78.24 | 0.25 |
| Kettle Creek | 18505.62 | 10-YR | 2317.70 | 6788.84 | 6796.78 | | 6797.29 | 0.004790 | 3.84 | 490.94 | 81.45 | 0.25 |
| Kettle Creek | 18505.62 | 25-YR | 2797.90 | 6788.84 | 6797.51 | | 6798.11 | 0.004736 | 4.07 | 551.53 | 83.95 | 0.25 |
| Kettle Creek | 18505.62 | 50-YR | 3559.70 | 6788.84 | 6798.55 | | 6799.27 | 0.004665 | 4.38 | 640.51 | 87.27 | 0.26 |
| Kettle Creek | 18505.62 | 100-YR | 4090.90 | 6788.84 | 6799.21 | | 6800.00 | 0.004631 | 4.58 | 698.51 | 89.51 | 0.26 |
| Kettle Creek | 17970.84 | 2-YR | 1151.10 | 6783.01 | 6787.19 | | 6787.69 | 0.018181 | 4.74 | 220.59 | 74.74 | 0.44 |
| Kettle Creek | 17970.84 | 5-YR | 1755.60 | 6783.01 | 6788.14 | | 6788.80 | 0.016176 | 5.21 | 295.68 | 84.82 | 0.43 |
| Kettle Creek | 17970.84 | 10-YR | 2317.70 | 6783.01 | 6788.78 | | 6789.66 | 0.015429 | 5.55 | 350.89 | 88.00 | 0.43 |
| Kettle Creek | 17970.84 | 25-YR | 2797.90 | 6783.01 | 6789.25 | | 6790.32 | 0.015047 | 5.81 | 392.75 | 89.67 | 0.43 |
| Kettle Creek | 17970.84 | 50-YR | 3559.70 | 6783.01 | 6789.91 | | 6791.28 | 0.014776 | 6.19 | 452.33 | 91.88 | 0.43 |
| Kettle Creek | 17970.84 | 100-YR | 4090.90 | 6783.01 | 6790.32 | | 6791.89 | 0.014671 | 6.43 | 490.72 | 93.30 | 0.44 |
| Kettle Creek | 17128.69 | 2-YR | 1151.10 | 6771.75 | 6776.93 | | 6777.14 | 0.009134 | 3.47 | 320.99 | 90.41 | 0.31 |
| Kettle Creek | 17128.69 | 5-YR | 1755.60 | 6771.75 | 6777.76 | | 6778.11 | 0.010244 | 4.17 | 397.94 | 94.22 | 0.34 |
| Kettle Creek | 17128.69 | 10-YR | 2317.70 | 6771.75 | 6778.44 | | 6778.90 | 0.010715 | 4.67 | 462.84 | 97.19 | 0.35 |
| Kettle Creek | 17128.69 | 25-YR | 2797.90 | 6771.75 | 6778.95 | | 6779.52 | 0.011024 | 5.03 | 513.16 | 99.45 | 0.36 |
| Kettle Creek | 17128.69 | 50-YR | 3559.70 | 6771.75 | 6779.70 | | 6780.41 | 0.011262 | 5.50 | 588.34 | 102.98 | 0.38 |
| Kettle Creek | 17128.69 | 100-YR | 4090.90 | 6771.75 | 6780.16 | | 6780.98 | 0.011382 | 5.79 | 637.10 | 105.28 | 0.38 |
| Kettle Creek | 16326.64 | 2-YR | 1151.10 | 6761.71 | 6768.09 | | 6768.34 | 0.013475 | 3.90 | 292.71 | 107.82 | 0.37 |
| Kettle Creek | 16326.64 | 5-YR | 1755.60 | 6761.71 | 6768.97 | | 6769.31 | 0.011888 | 4.27 | 388.32 | 110.45 | 0.36 |
| Kettle Creek | 16326.64 | 10-YR | 2317.70 | 6761.71 | 6769.60 | | 6770.07 | 0.011460 | 4.59 | 459.11 | 112.42 | 0.36 |
| Kettle Creek | 16326.64 | 25-YR | 2797.90 | 6761.71 | 6770.09 | | 6770.66 | 0.011213 | 4.83 | 513.71 | 113.96 | 0.37 |
| Kettle Creek | 16326.64 | 50-YR | 3559.70 | 6761.71 | 6770.75 | | 6771.50 | 0.011130 | 5.20 | 590.02 | 116.38 | 0.37 |
| Kettle Creek | 16326.64 | 100-YR | 4090.90 | 6761.71 | 6771.17 | | 6772.05 | 0.011084 | 5.43 | 639.38 | 117.92 | 0.37 |
| Kettle Creek | 15906.34 | 2-YR | 1151.10 | 6753.98 | 6761.79 | 6759.97 | 6762.19 | 0.016162 | 4.94 | 227.34 | 65.49 | 0.41 |



HEC-RAS Plan: Existing River: Kettle Creek Reach: Kettle Creek (Continued)

| Reach | River Sta | Profile | Q Total | Min Ch El | W.S. Elev | Crit W.S. | E.G. Elev | E.G. Slope | Vel Chnl | Flow Area | Top Width | Froude # Chl |
|--------------|-----------|---------|---------|-----------|-----------|-----------|-----------|------------|----------|-----------|-----------|--------------|
| | | | (cfs) | (ft) | (ft) | (ft) | (ft) | (ft/ft) | (ft/s) | (sq ft) | (ft) | |
| Kettle Creek | 15906.34 | 5-YR | 1755.60 | 6753.98 | 6762.57 | 6760.94 | 6763.21 | 0.018572 | 5.89 | 282.60 | 75.97 | 0.45 |
| Kettle Creek | 15906.34 | 10-YR | 2317.70 | 6753.98 | 6763.18 | 6761.61 | 6764.02 | 0.019313 | 6.46 | 331.24 | 84.52 | 0.47 |
| Kettle Creek | 15906.34 | 25-YR | 2797.90 | 6753.98 | 6763.60 | 6762.11 | 6764.62 | 0.020024 | 6.88 | 368.19 | 90.84 | 0.48 |
| Kettle Creek | 15906.34 | 50-YR | 3559.70 | 6753.98 | 6764.20 | 6762.95 | 6765.48 | 0.020166 | 7.34 | 425.15 | 98.79 | 0.49 |
| Kettle Creek | 15906.34 | 100-YR | 4090.90 | 6753.98 | 6764.56 | 6763.56 | 6766.05 | 0.020099 | 7.57 | 461.34 | 102.32 | 0.49 |
| Kettle Creek | 15906 | | Bridge | | | | | | | | | |
| Kettle Creek | 15683.73 | 2-YR | 1151.10 | 6751.41 | 6757.63 | 6757.63 | 6758.94 | 0.062898 | 8.85 | 126.25 | 51.62 | 0.77 |
| Kettle Creek | 15683.73 | 5-YR | 1755.60 | 6751.41 | 6758.45 | 6758.45 | 6760.22 | 0.051347 | 9.02 | 173.56 | 62.60 | 0.71 |
| Kettle Creek | 15683.73 | 10-YR | 2317.70 | 6751.41 | 6759.40 | 6759.40 | 6761.21 | 0.030985 | 7.88 | 238.24 | 74.47 | 0.57 |
| Kettle Creek | 15683.73 | 25-YR | 2797.90 | 6751.41 | 6759.98 | 6759.98 | 6761.90 | 0.025350 | 7.59 | 284.17 | 82.33 | 0.52 |
| Kettle Creek | 15683.73 | 50-YR | 3559.70 | 6751.41 | 6760.93 | 6760.93 | 6762.82 | 0.018071 | 7.01 | 370.27 | 100.69 | 0.45 |
| Kettle Creek | 15683.73 | 100-YR | 4090.90 | 6751.41 | 6761.38 | 6761.38 | 6763.35 | 0.016362 | 6.94 | 416.57 | 106.10 | 0.44 |
| Kettle Creek | 15530.88 | 2-YR | 1151.10 | 6749.40 | 6754.39 | | 6754.50 | 0.005703 | 2.69 | 428.06 | 118.46 | 0.24 |
| Kettle Creek | 15530.88 | 5-YR | 1755.60 | 6749.40 | 6755.32 | | 6755.48 | 0.006156 | 3.24 | 541.58 | 125.69 | 0.26 |
| Kettle Creek | 15530.88 | 10-YR | 2317.70 | 6749.40 | 6756.05 | | 6756.26 | 0.006360 | 3.63 | 634.79 | 130.29 | 0.27 |
| Kettle Creek | 15530.88 | 25-YR | 2797.90 | 6749.40 | 6756.60 | | 6756.84 | 0.006511 | 3.91 | 707.83 | 136.27 | 0.28 |
| Kettle Creek | 15530.88 | 50-YR | 3559.70 | 6749.40 | 6757.36 | | 6757.66 | 0.006648 | 4.29 | 815.03 | 144.12 | 0.29 |
| Kettle Creek | 15530.88 | 100-YR | 4090.90 | 6749.40 | 6757.84 | | 6758.18 | 0.006684 | 4.50 | 885.30 | 148.71 | 0.30 |
| Kettle Creek | 14906.12 | 2-YR | 1151.10 | 6742.04 | 6748.24 | | 6748.76 | 0.017659 | 5.45 | 201.85 | 73.53 | 0.44 |
| Kettle Creek | 14906.12 | 5-YR | 1755.60 | 6742.04 | 6749.14 | | 6749.85 | 0.015094 | 5.64 | 273.31 | 85.81 | 0.42 |
| Kettle Creek | 14906.12 | 10-YR | 2317.70 | 6742.04 | 6749.77 | | 6750.64 | 0.014292 | 5.89 | 330.11 | 95.71 | 0.41 |
| Kettle Creek | 14906.12 | 25-YR | 2797.90 | 6742.04 | 6750.20 | | 6751.22 | 0.013939 | 6.08 | 373.64 | 102.33 | 0.41 |
| Kettle Creek | 14906.12 | 50-YR | 3559.70 | 6742.04 | 6750.77 | | 6752.04 | 0.013641 | 6.35 | 433.20 | 107.89 | 0.41 |
| Kettle Creek | 14906.12 | 100-YR | 4090.90 | 6742.04 | 6751.12 | | 6752.56 | 0.013505 | 6.51 | 471.08 | 110.65 | 0.41 |
| Kettle Creek | 14354.72 | 2-YR | 1151.10 | 6734.36 | 6742.29 | | 6742.49 | 0.007728 | 3.62 | 316.88 | 80.15 | 0.29 |
| Kettle Creek | 14354.72 | 5-YR | 1755.60 | 6734.36 | 6743.23 | | 6743.54 | 0.008686 | 4.33 | 396.21 | 88.58 | 0.32 |
| Kettle Creek | 14354.72 | 10-YR | 2317.70 | 6734.36 | 6743.99 | | 6744.39 | 0.008879 | 4.76 | 465.89 | 95.25 | 0.33 |
| Kettle Creek | 14354.72 | 25-YR | 2797.90 | 6734.36 | 6744.58 | | 6745.05 | 0.008790 | 5.02 | 524.07 | 100.95 | 0.33 |
| Kettle Creek | 14354.72 | 50-YR | 3559.70 | 6734.36 | 6745.42 | | 6746.00 | 0.008500 | 5.32 | 612.65 | 109.18 | 0.33 |
| Kettle Creek | 14354.72 | 100-YR | 4090.90 | 6734.36 | 6745.95 | | 6746.60 | 0.008290 | 5.49 | 671.39 | 114.20 | 0.33 |
| Kettle Creek | 13757.33 | 2-YR | 1151.10 | 6727.92 | 6733.99 | 6733.14 | 6734.63 | 0.026816 | 6.18 | 180.61 | 69.56 | 0.51 |
| Kettle Creek | 13757.33 | 5-YR | 1755.60 | 6727.92 | 6734.90 | 6734.00 | 6735.79 | 0.020945 | 6.18 | 247.35 | 76.93 | 0.47 |
| Kettle Creek | 13757.33 | 10-YR | 2317.70 | 6727.92 | 6735.48 | 6734.50 | 6736.67 | 0.020074 | 6.48 | 293.46 | 81.51 | 0.47 |



HEC-RAS Plan: Existing River: Kettle Creek Reach: Kettle Creek (Continued)

| Reach | River Sta | Profile | Q Total | Min Ch El | W.S. Elev | Crit W.S. | E.G. Elev | E.G. Slope | Vel Chnl | Flow Area | Top Width | Froude # Chl |
|--------------|-----------|---------|---------|-----------|-----------|-----------|-----------|------------|----------|-----------|-----------|--------------|
| | | | (cfs) | (ft) | (ft) | (ft) | (ft) | (ft/ft) | (ft/s) | (sq ft) | (ft) | |
| Kettle Creek | 13757,33 | 25-YR | 2797.90 | 6727.92 | 6735.87 | 6735.05 | 6737.32 | 0.020353 | 6.81 | 325.83 | 84.60 | 0.48 |
| Kettle Creek | 13757.33 | 50-YR | 3559.70 | 6727.92 | 6736.38 | 6735.96 | 6738.25 | 0.021302 | 7.33 | 369.80 | 88.59 | 0.49 |
| Kettle Creek | 13757.33 | 100-YR | 4090.90 | 6727.92 | 6736.69 | 6736.50 | 6738.86 | 0.021950 | 7.66 | 397.69 | 91.02 | 0.50 |
| Kettle Creek | 12367.83 | 2-YR | 1151.10 | 6708.58 | 6713.95 | | 6714.17 | 0.009200 | 3.76 | 303.64 | 75.16 | 0.3 |
| Kettle Creek | 12367.83 | 5-YR | 1755.60 | 6708.58 | 6714.87 | | 6715.22 | 0.010880 | 4.61 | 375.26 | 78.52 | 0.35 |
| Kettle Creek | 12367.83 | 10-YR | 2317.70 | 6708.58 | 6715.69 | | 6716.14 | 0.011150 | 5.14 | 440.38 | 81.16 | 0.37 |
| Kettle Creek | 12367.83 | 25-YR | 2797.90 | 6708.58 | 6716.39 | | 6716.90 | 0.010864 | 5.45 | 498.90 | 86.32 | 0.37 |
| Kettle Creek | 12367.83 | 50-YR | 3559.70 | 6708.58 | 6717.38 | | 6717.98 | 0.010320 | 5.81 | 589.65 | 96.16 | 0.37 |
| Kettle Creek | 12367.83 | 100-YR | 4090.90 | 6708.58 | 6717.97 | | 6718.64 | 0.010019 | 6.01 | 646.95 | 99.38 | 0.37 |
| Kettle Creek | 11267.11 | 2-YR | 1151.10 | 6695.53 | 6702.97 | | 6703.48 | 0.010294 | 4.30 | 224.49 | 68.56 | 0.33 |
| Kettle Creek | 11267.11 | 5-YR | 1755.60 | 6695.53 | 6704.07 | | 6704.78 | 0.008346 | 4.40 | 304.04 | 76.56 | 0.3 |
| Kettle Creek | 11267.11 | 10-YR | 2317.70 | 6695.53 | 6704.79 | | 6705.69 | 0.008144 | 4.68 | 361.71 | 82.91 | 0.3 |
| Kettle Creek | 11267.11 | 25-YR | 2797.90 | 6695.53 | 6705.25 | | 6706.33 | 0.008516 | 5.00 | 400.68 | 87.41 | 0.32 |
| Kettle Creek | 11267.11 | 50-YR | 3559.70 | 6695.53 | 6705.84 | | 6707.21 | 0.009202 | 5.47 | 454.58 | 93.36 | 0.34 |
| Kettle Creek | 11267.11 | 100-YR | 4090.90 | 6695.53 | 6706.21 | | 6707.76 | 0.009606 | 5.76 | 488.97 | 96.31 | 0.35 |
| Kettle Creek | 10087.38 | 2-YR | 1145.30 | 6680.77 | 6687.96 | | 6688.15 | 0.002153 | 2.39 | 371.42 | 88.96 | 0.17 |
| Kettle Creek | 10087.38 | 5-YR | 1748.30 | 6680.77 | 6689.11 | | 6689.39 | 0.002103 | 2.64 | 475.54 | 92.02 | 0.17 |
| Kettle Creek | 10087:38 | 10-YR | 2310.00 | 6680.77 | 6690.07 | 6686.59 | 6690.43 | 0.002011 | 2.79 | 565.25 | 94.54 | 0.17 |
| Kettle Creek | 10087.38 | 25-YR | 2790.50 | 6680.77 | 6690.89 | 6687.11 | 6691.29 | 0.001887 | 2.87 | 643.04 | 96.84 | 0.16 |
| Kettle Creek | 10087.38 | 50-YR | 3553.20 | 6680.77 | 6692.10 | 6687.72 | 6692.58 | 0.001717 | 2.97 | 763.04 | 100.32 | 0.16 |
| Kettle Creek | 10087.38 | 100-YR | 4085.50 | 6680.77 | 6692.90 | 6688.11 | 6693.41 | 0.001624 | 3.03 | 843.83 | 102.58 | 0.16 |
| Kettle Creek | 9732.32 | 2-YR | 1145.30 | 6676.00 | 6681.22 | | 6681.80 | 0.034847 | 6.11 | 187.86 | 61.63 | 0.59 |
| Kettle Creek | 9732.32 | 5-YR | 1748.30 | 6676.00 | 6681.56 | | 6682.64 | 0.057775 | 8.39 | 209.55 | 67.19 | 0.77 |
| Kettle Creek | 9732.32 | 10-YR | 2310.00 | 6676.00 | 6681.83 | 6681.83 | 6683.42 | 0.077142 | 10.17 | 228.29 | 70.65 | 0.90 |
| Kettle Creek | 9732.32 | 25-YR | 2790.50 | 6676.00 | 6682.24 | 6682.24 | 6684.05 | 0.075615 | 10.76 | 258.46 | 74.43 | 0.9 |
| Kettle Creek | 9732.32 | 50-YR | 3553.20 | 6676.00 | 6682.82 | 6682.82 | 6685.01 | 0.072800 | 11.46 | 302.38 | 78.16 | 0.9 |
| Kettle Creek | 9732.32 | 100-YR | 4085.50 | 6676.00 | 6683.21 | 6683.21 | 6685.65 | 0.068956 | 11.75 | 333.84 | 80.71 | 0.90 |
| Kettle Creek | 8444.97 | 2-YR | 1184.90 | 6660.69 | 6666.67 | | 6666.92 | 0.005788 | 3.27 | 316.02 | 103.35 | 0.26 |
| Kettle Creek | 8444.97 | 5-YR | 1807.00 | 6660.69 | 6667.70 | | 6668.05 | 0.004719 | 3.34 | 425.90 | 111.97 | 0.24 |
| Kettle Creek | 8444.97 | 10-YR | 2385.10 | 6660.69 | 6668.53 | | 6668.96 | 0.004086 | 3.39 | 522.84 | 120.22 | 0.23 |
| Kettle Creek | 8444.97 | 25-YR | 2879.90 | 6660.69 | 6669.18 | | 6669.65 | 0.003697 | 3.42 | 601.93 | 125.95 | 0.22 |
| Kettle Creek | 8444.97 | 50-YR | 3663.90 | 6660.69 | 6670.08 | | 6670.63 | 0.003291 | 3.48 | 719.93 | 133.88 | 0.21 |
| Kettle Creek | 8444.97 | 100-YR | 4211.20 | 6660.69 | 6670.61 | | 6671.21 | 0.003155 | 3.55 | 791.43 | 137.54 | 0.2 |



HEC-RAS Plan: Existing River: Kettle Creek Reach: Kettle Creek (Continued)

| Reach | River Sta | Profile | Q Total | Min Ch El | W.S. Elev | Crit W.S. | E.G. Elev | E.G. Slope | Vel Chnl | Flow Area | Top Width | Froude # Chl |
|--------------|-----------|---------|---------|-----------|-----------|-----------|-----------|------------|----------|-----------|-----------|--------------|
| | | | (cfs) | (ft) | (ft) | (ft) | (ft) | (ft/ft) | (ft/s) | (sq ft) | (ft) | |
| Kettle Creek | 8350 | 2-YR | 1184.90 | 6660.00 | 6666.27 | | 6666.52 | 0.003254 | 2.73 | 352.97 | 97.77 | 0.20 |
| Kettle Creek | 8350 | 5-YR | 1807.00 | 6660.00 | 6667.37 | | 6667.69 | 0.003021 | 2.94 | 464.67 | 106.68 | 0.20 |
| Kettle Creek | 8350 | 10-YR | 2385.10 | 6660.00 | 6668.23 | | 6668.62 | 0.002958 | 3.15 | 561.08 | 121.35 | 0.20 |
| Kettle Creek | 8350 | 25-YR | 2879.90 | 6660.00 | 6668.91 | | 6669.34 | 0.002773 | 3.22 | 650.27 | 134.75 | 0.19 |
| Kettle Creek | 8350 | 50-YR | 3663.90 | 6660.00 | 6669.88 | | 6670.34 | 0.002477 | 3.27 | 786.50 | 148.07 | 0.19 |
| Kettle Creek | 8350 | 100-YR | 4211.20 | 6660.00 | 6670.43 | | 6670.92 | 0.002373 | 3.33 | 870.55 | 154.76 | 0.18 |
| Kettle Creek | 8251.39 | 2-YR | 1184.90 | 6660.00 | 6665.53 | 6663.62 | 6665.91 | 0.010606 | 4.20 | 256.21 | 72.80 | 0.35 |
| Kettle Creek | 8251.39 | 5-YR | 1807.00 | 6660.00 | 6666.53 | 6664.46 | 6667.09 | 0.010200 | 4.70 | 333.81 | 81.18 | 0.35 |
| Kettle Creek | 8251.39 | 10-YR | 2385.10 | 6660.00 | 6667.31 | 6665.20 | 6668.00 | 0.009802 | 5.02 | 399.11 | 87.50 | 0.35 |
| Kettle Creek | 8251.39 | 25-YR | 2879.90 | 6660.00 | 6667.92 | 6665.75 | 6668.72 | 0.009244 | 5.19 | 454.36 | 91.94 | 0.35 |
| Kettle Creek | 8251.39 | 50-YR | 3663.90 | 6660.00 | 6668.88 | 6666.52 | 6669.75 | 0.008948 | 5.56 | 552.96 | 122.98 | 0.35 |
| Kettle Creek | 8251.39 | 100-YR | 4211.20 | 6660.00 | 6669.48 | 6667.05 | 6670.37 | 0.007895 | 5.49 | 631.26 | 135.89 | 0.33 |
| Kettle Creek | 8251 | | Bridge | | | | | | | | | |
| Kettle Creek | 8060.94 | 2-YR | 1184.90 | 6653.57 | 6658.73 | 6658.23 | 6659.78 | 0.014856 | 5.20 | 167.44 | 49.84 | 0.42 |
| Kettle Creek | 8060.94 | 5-YR | 1807.00 | 6653.57 | 6659.58 | 6659.31 | 6661.06 | 0.016409 | 6.09 | 212.92 | 56.64 | 0.45 |
| Kettle Creek | 8060.94 | 10-YR | 2385.10 | 6653.57 | 6660.21 | 6660.13 | 6662.06 | 0.017418 | 6.72 | 249.75 | 61.52 | 0.47 |
| Kettle Creek | 8060.94 | 25-YR | 2879.90 | 6653.57 | 6660.84 | 6660.84 | 6662.75 | 0.016851 | 7.04 | 291.70 | 71.31 | 0.47 |
| Kettle Creek | 8060.94 | 50-YR | 3663.90 | 6653.57 | 6661.63 | 6661.63 | 6663.71 | 0.016094 | 7.39 | 353.30 | 95.52 | 0.47 |
| Kettle Creek | 8060.94 | 100-YR | 4211.20 | 6653.57 | 6662.63 | 6662.63 | 6664.20 | 0.011363 | 6.73 | 469.57 | 130.09 | 0.40 |
| Kettle Creek | 7863.13 | 2-YR | 1184.90 | 6649.24 | 6652.87 | 6652.74 | 6654.16 | 0.067479 | 8.24 | 136.20 | 52.11 | 0.82 |
| Kettle Creek | 7863.13 | 5-YR | 1807.00 | 6649.24 | 6653.81 | 6653.69 | 6655.51 | 0.053491 | 8.73 | 187.44 | 57.41 | 0.76 |
| Kettle Creek | 7863.13 | 10-YR | 2385.10 | 6649.24 | 6654.53 | 6654.53 | 6656.56 | 0.046955 | 9.11 | 230.10 | 61.83 | 0.73 |
| Kettle Creek | 7863.13 | 25-YR | 2879.90 | 6649.24 | 6655.17 | 6655.17 | 6657.35 | 0.039738 | 9.11 | 271.03 | 65.97 | 0.69 |
| Kettle Creek | 7863.13 | 50-YR | 3663.90 | 6649.24 | 6656.00 | 6656.00 | 6658.41 | 0.034690 | 9.36 | 328.42 | 72.80 | 0.66 |
| Kettle Creek | 7863.13 | 100-YR | 4211.20 | 6649.24 | 6656.51 | 6656.51 | 6659.11 | 0.031746 | 9.44 | 366.77 | 76.23 | 0.64 |
| Kettle Creek | 7632.03 | 2-YR | 1184.90 | 6641.32 | 6649.06 | | 6649.33 | 0.009212 | 4.15 | 284.17 | 62.63 | 0.32 |
| Kettle Creek | 7632.03 | 5-YR | 1807.00 | 6641.32 | 6650.16 | | 6650.57 | 0.010273 | 4.99 | 356.19 | 68.49 | 0.35 |
| Kettle Creek | 7632.03 | 10-YR | 2385.10 | 6641.32 | 6650.96 | | 6651.49 | 0.011087 | 5.61 | 413.22 | 74.28 | 0.37 |
| Kettle Creek | 7632.03 | 25-YR | 2879.90 | 6641.32 | 6651.51 | | 6652.16 | 0.011854 | 6.10 | 454.84 | 78.34 | 0.39 |
| Kettle Creek | 7632.03 | 50-YR | 3663.90 | 6641.32 | 6652.18 | | 6653.03 | 0.013282 | 6.84 | 509.30 | 83.26 | 0.42 |
| Kettle Creek | 7632.03 | 100-YR | 4211.20 | 6641.32 | 6652.57 | | 6653.57 | 0.014255 | 7.31 | 542.28 | 85.57 | 0.44 |
| Kettle Creek | 6688.3 | 2-YR | 1186.40 | 6629.79 | 6635.71 | | 6636.03 | 0.024177 | 4.50 | 263.62 | 95.43 | 0.48 |
| Kettle Creek | 6688.3 | 5-YR | 1807.50 | 6629.79 | 6636.81 | | 6637.16 | 0.020802 | 4.79 | 377.74 | 112.95 | 0.46 |



HEC-RAS Plan: Existing River: Kettle Creek Reach: Kettle Creek (Continued)

| Reach | River Sta | Profile | Q Total | Min Ch El | W.S. Elev | Crit W.S. | E.G. Elev | E.G. Slope | Vel Chnl | Flow Area | Top Width | Froude # Chl |
|--------------|-----------|---------|---------|-----------|-----------|-----------|-----------|------------|----------|-----------|-----------|--------------|
| | | | (cfs) | (ft) | (ft) | (ft) | (ft) | (ft/ft) | (ft/s) | (sq ft) | (ft) | |
| Kettle Creek | 6688.3 | 10-YR | 2384.50 | 6629.79 | 6637.64 | | 6638.03 | 0.018846 | 4.99 | 477.42 | 125.76 | 0.45 |
| Kettle Creek | 6688.3 | 25-YR | 2877.00 | 6629.79 | 6638.25 | | 6638.67 | 0.017332 | 5.16 | 556.82 | 134.66 | 0.44 |
| Kettle Creek | 6688.3 | 50-YR | 3657.80 | 6629.79 | 6639.08 | | 6639.54 | 0.015097 | 5.41 | 673.77 | 145.63 | 0.42 |
| Kettle Creek | 6688.3 | 100-YR | 4201.90 | 6629.79 | 6639.61 | | 6640.10 | 0.013940 | 5.55 | 752.55 | 152.65 | 0.4 |
| Kettle Creek | 6433.61 | 2-YR | 1186.40 | 6627.42 | 6633.43 | | 6633.56 | 0.005007 | 2.89 | 411.33 | 98.04 | 0.24 |
| Kettle Creek | 6433.61 | 5-YR | 1807.50 | 6627.42 | 6634.55 | | 6634.73 | 0.005253 | 3.42 | 523.63 | 103.48 | 0.25 |
| Kettle Creek | 6433.61 | 10-YR | 2384.50 | 6627.42 | 6635.41 | | 6635.64 | 0.005379 | 3.80 | 614.71 | 108.41 | 0.26 |
| Kettle Creek | 6433.61 | 25-YR | 2877.00 | 6627.42 | 6636.06 | | 6636.34 | 0.005440 | 4.07 | 686.47 | 112.67 | 0.27 |
| Kettle Creek | 6433.61 | 50-YR | 3657.80 | 6627.42 | 6636.98 | | 6637.32 | 0.005471 | 4.42 | 793.53 | 120.10 | 0.27 |
| Kettle Creek | 6433.61 | 100-YR | 4201.90 | 6627.42 | 6637.56 | | 6637.95 | 0.005431 | 4.61 | 865.62 | 125.16 | 0.27 |
| Kettle Creek | 6305.69 | 2-YR | 1186.40 | 6625.87 | 6631.40 | | 6631.59 | 0.010044 | 3.45 | 344.45 | 98.60 | 0.32 |
| Kettle Creek | 6305.69 | 5-YR | 1807.50 | 6625.87 | 6632.63 | | 6632.85 | 0.008366 | 3.83 | 472.87 | 111.08 | 0.3 |
| Kettle Creek | 6305.69 | 10-YR | 2384.50 | 6625.87 | 6633.59 | | 6633.85 | 0.007334 | 4.05 | 584.12 | 120.56 | 0.30 |
| Kettle Creek | 6305.69 | 25-YR | 2877.00 | 6625.87 | 6634.32 | | 6634.61 | 0.006664 | 4.18 | 675.13 | 128.74 | 0.29 |
| Kettle Creek | 6305.69 | 50-YR | 3657.80 | 6625.87 | 6635.36 | | 6635.68 | 0.005820 | 4.31 | 816.51 | 143.12 | 0.28 |
| Kettle Creek | 6305.69 | 100-YR | 4201.90 | 6625.87 | 6636.03 | | 6636.38 | 0.005340 | 4.37 | 916.05 | 158.12 | 0.27 |
| Kettle Creek | 6147.73 | 2-YR | 1186.40 | 6623.99 | 6630.61 | | 6630.76 | 0.003154 | 2.40 | 440.53 | 103.18 | 0.19 |
| Kettle Creek | 6147.73 | 5-YR | 1807.50 | 6623.99 | 6631.92 | | 6632.12 | 0.002898 | 2.69 | 579.21 | 109.37 | 0.19 |
| Kettle Creek | 6147.73 | 10-YR | 2384.50 | 6623.99 | 6632.92 | | 6633.17 | 0.002781 | 2.91 | 690.92 | 114.01 | 0.19 |
| Kettle Creek | 6147.73 | 25-YR | 2877.00 | 6623.99 | 6633.66 | | 6633.96 | 0.002724 | 3.08 | 777.40 | 117.54 | 0.19 |
| Kettle Creek | 6147.73 | 50-YR | 3657.80 | 6623.99 | 6634.71 | | 6635.08 | 0.002662 | 3.31 | 903.75 | 122.52 | 0.19 |
| Kettle Creek | 6147.73 | 100-YR | 4201.90 | 6623.99 | 6635.40 | | 6635.80 | 0.002609 | 3.44 | 988.82 | 126.00 | 0.19 |
| Kettle Creek | 6032.86 | 2-YR | 1186.40 | 6622.67 | 6628.47 | 6625.82 | 6628.68 | 0.003558 | 2.55 | 387.37 | 97.40 | 0.20 |
| Kettle Creek | 6032.86 | 5-YR | 1807.50 | 6622.67 | 6629.56 | 6626.35 | 6629.86 | 0.003538 | 2.91 | 496.93 | 103.65 | 0.2 |
| Kettle Creek | 6032.86 | 10-YR | 2384.50 | 6622.67 | 6630.46 | 6626.93 | 6630.83 | 0.003399 | 3.13 | 591.99 | 108.18 | 0.2 |
| Kettle Creek | 6032.86 | 25-YR | 2877.00 | 6622.67 | 6631.12 | 6627.46 | 6631.55 | 0.003352 | 3.30 | 664.12 | 111.18 | 0.2 |
| Kettle Creek | 6032.86 | 50-YR | 3657.80 | 6622.67 | 6632.08 | 6628.20 | 6632.60 | 0.003269 | 3.54 | 774.02 | 116.50 | 0.2 |
| Kettle Creek | 6032.86 | 100-YR | 4201.90 | 6622.67 | 6632.78 | 6628.68 | 6633.34 | 0.003056 | 3.60 | 855.85 | 118.67 | 0.2 |
| Kettle Creek | 6000 | | Bridge | | | | | | | | | |
| W-W- O | roon o | o vin | 4400.40 | 0000.04 | 2222 22 | | 0000 44 | 0.004000 | 4.00 | 420.07 | 440.00 | 0.44 |
| Kettle Creek | 5983.2 | 2-YR | 1186.40 | 6622.04 | 6628.29 | | 6628.44 | 0.001920 | 1.99 | 436.07 | 118.89 | 0.15 |
| Kettle Creek | 5983.2 | 5-YR | 1807.50 | 6622.04 | 6629.35 | | 6629.58 | 0.001787 | 2.17 | 564.57 | 123.65 | 0.15 |
| Kettle Creek | 5983.2 | 10-YR | 2384.50 | 6622.04 | 6630.23 | | 6630.51 | 0.001717 | 2.32 | 676.91 | 131.18 | 0.15 |
| Kettle Creek | 5983.2 | 25-YR | 2877.00 | 6622.04 | 6630.87 | | 6631.19 | 0.001655 | 2.40 | 761.38 | 133.12 | 0.15 |



HEC-RAS Plan: Existing River: Kettle Creek Reach: Kettle Creek (Continued)

| Reach | River Sta | Profile | Q Total | Min Ch El | W.S. Elev | Crit W.S. | E.G. Elev | E.G. Slope | Vel Chnl | Flow Area | Top Width | Froude # Chl |
|--------------|-----------|---------|---------|-----------|-----------|-----------|-----------|------------|----------|-----------|-----------|--------------|
| | | | (cfs) | (ft) | (ft) | (ft) | (ft) | (ft/ft) | (ft/s) | (sq ft) | (ft) | |
| Kettle Creek | 5983.2 | 50-YR | 3657.80 | 6622.04 | 6631.80 | | 6632.19 | 0.001583 | 2.53 | 886.53 | 136.02 | 0.15 |
| Kettle Creek | 5983.2 | 100-YR | 4201.90 | 6622.04 | 6632.51 | | 6632.90 | 0.001608 | 2.68 | 985.42 | 149.06 | 0.15 |
| Kettle Creek | 5846.46 | 2-YR | 1186.40 | 6620.39 | 6624.39 | | 6625.12 | 0.054764 | 6.83 | 173.98 | 65.27 | 0.72 |
| Kettle Creek | 5846.46 | 5-YR | 1807.50 | 6620.39 | 6625.32 | | 6626.22 | 0.046349 | 7.60 | 237.36 | 71.85 | 0.70 |
| Kettle Creek | 5846.46 | 10-YR | 2384.50 | 6620.39 | 6626.04 | | 6627.09 | 0.041528 | 8.10 | 290.62 | 76.54 | 0.68 |
| Kettle Creek | 5846.46 | 25-YR | 2877.00 | 6620.39 | 6626.58 | | 6627.76 | 0.038478 | 8.43 | 334.06 | 81.76 | 0.67 |
| Kettle Creek | 5846.46 | 50-YR | 3657.80 | 6620.39 | 6627.34 | | 6628.70 | 0.034949 | 8.83 | 398.47 | 88.84 | 0.65 |
| Kettle Creek | 5846.46 | 100-YR | 4201.90 | 6620.39 | 6627.83 | | 6629.31 | 0.032396 | 8.98 | 443.61 | 93.39 | 0.63 |
| Kettle Creek | 5366.46 | 2-YR | 1186.40 | 6612.16 | 6619.29 | 6616.48 | 6619.44 | 0.004810 | 2.87 | 394.04 | 96.66 | 0.23 |
| Kettle Creek | 5366.46 | 5-YR | 1807.50 | 6612.16 | 6620.35 | 6617.19 | 6620.59 | 0.004990 | 3.35 | 498.61 | 100.65 | 0.25 |
| Kettle Creek | 5366.46 | 10-YR | 2384.50 | 6612.16 | 6621.17 | 6617.73 | 6621.49 | 0.005120 | 3.71 | 582.39 | 104.00 | 0.25 |
| Kettle Creek | 5366.46 | 25-YR | 2877.00 | 6612.16 | 6621.78 | 6618.08 | 6622.16 | 0.005223 | 3.97 | 646.28 | 106.18 | 0.26 |
| Kettle Creek | 5366.46 | 50-YR | 3657.80 | 6612.16 | 6622.66 | 6618.62 | 6623.14 | 0.005334 | 4.34 | 742.28 | 110.85 | 0.27 |
| Kettle Creek | 5366.46 | 100-YR | 4201.90 | 6612.16 | 6623.15 | 6618.94 | 6623.70 | 0.005553 | 4.60 | 796.65 | 113.16 | 0.28 |
| Kettle Creek | 3636.65 | 2-YR | 1186.40 | 6592.57 | 6595.26 | 6595.26 | 6596.17 | 0.124453 | 7.65 | 154.98 | 87.35 | 1.01 |
| Kettle Creek | 3636.65 | 5-YR | 1807.50 | 6592.57 | 6595.87 | 6595.87 | 6597.03 | 0.111612 | 8.67 | 208.51 | 90.76 | 1.00 |
| Kettle Creek | 3636.65 | 10-YR | 2384.50 | 6592.57 | 6596.35 | 6596.35 | 6597.73 | 0.104123 | 9.43 | 252.81 | 92.90 | 1.00 |
| Kettle Creek | 3636.65 | 25-YR | 2877.00 | 6592.57 | 6596.73 | 6596.73 | 6598.27 | 0.098322 | 9.95 | 288.94 | 94.43 | 0.99 |
| Kettle Creek | 3636.65 | 50-YR | 3657.80 | 6592.57 | 6597.26 | 6597.26 | 6599.07 | 0.093574 | 10.75 | 339.14 | 96.49 | 0.99 |
| Kettle Creek | 3636.65 | 100-YR | 4201.90 | 6592.57 | 6597.74 | 6597.64 | 6599.59 | 0.080575 | 10.82 | 385.88 | 98.53 | 0.94 |
| Kettle Creek | 3115.71 | 2-YR | 1186.40 | 6585.47 | 6593.04 | | 6593.08 | 0.000587 | 1.21 | 808.77 | 161.34 | 0.09 |
| Kettle Creek | 3115.71 | 5-YR | 1807.50 | 6585.47 | 6594.35 | | 6594.42 | 0.000611 | 1.41 | 1028.49 | 174.30 | 0.09 |
| Kettle Creek | 3115.71 | 10-YR | 2384.50 | 6585.47 | 6595.36 | | 6595.45 | 0.000628 | 1.55 | 1211.38 | 187.67 | 0.09 |
| Kettle Creek | 3115.71 | 25-YR | 2877.00 | 6585.47 | 6596.11 | | 6596.21 | 0.000627 | 1.64 | 1354.39 | 194.33 | 0.09 |
| Kettle Creek | 3115.71 | 50-YR | 3657.80 | 6585.47 | 6597.16 | | 6597.28 | 0.000633 | 1.77 | 1564.67 | 206.13 | 0.10 |
| Kettle Creek | 3115.71 | 100-YR | 4201.90 | 6585.47 | 6597.82 | | 6597.95 | 0.000641 | 1.86 | 1702.59 | 215.55 | 0.10 |
| Kettle Creek | 2957.59 | 2-YR | 1186.40 | 6582.74 | 6592.42 | 6589.30 | 6592.77 | 0.003681 | 3.75 | 261.47 | 70.77 | 0.22 |
| Kettle Creek | 2957.59 | 5-YR | 1807.50 | 6582.74 | 6593.61 | 6591.30 | 6594.07 | 0.003327 | 3.88 | 350.43 | 79.16 | 0.22 |
| Kettle Creek | 2957.59 | 10-YR | 2384.50 | 6582.74 | 6594.51 | 6591.98 | 6595.07 | 0.003129 | 3.98 | 424.77 | 85.02 | 0.21 |
| Kettle Creek | 2957.59 | 25-YR | 2877.00 | 6582.74 | 6595.19 | 6592.47 | 6595.82 | 0.003019 | 4.07 | 483.72 | 89.32 | 0.21 |
| Kettle Creek | 2957.59 | 50-YR | 3657.80 | 6582.74 | 6596.13 | 6593.21 | 6596.86 | 0.002920 | 4.22 | 570.82 | 95.69 | 0.21 |
| Kettle Creek | 2957.59 | 100-YR | 4201.90 | 6582.74 | 6596.71 | 6593.71 | 6597.51 | 0.002871 | 4.31 | 627.68 | 99.37 | 0.21 |
| Kettle Creek | 2850 | | Bridge | | | | | | | | | |



HEC-RAS Plan: Existing River: Kettle Creek Reach: Kettle Creek (Continued)

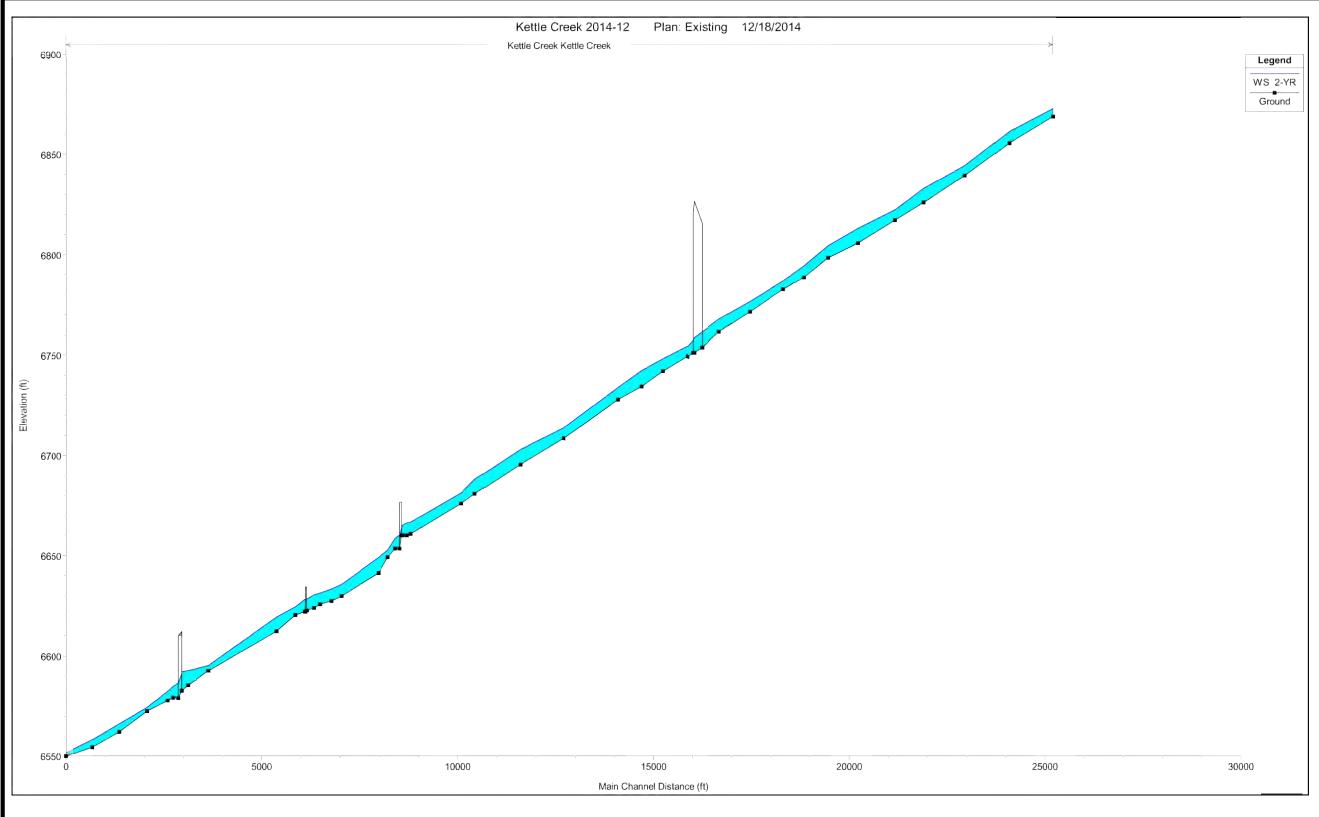
| Reach | River Sta | Profile | Q Total | Min Ch El | W.S. Elev | Crit W.S. | E.G. Elev | E.G. Slope | Vel Chni | Flow Area | Top Width | Froude # Chl |
|--------------|-----------|---------|---------|-----------|-----------|-----------|-----------|------------|----------|-----------|-----------|--------------|
| | | | (cfs) | (ft) | (ft) | (ft) | (ft) | (ft/ft) | (ft/s) | (sq ft) | (ft) | |
| Kettle Creek | 2731.34 | 2-YR | 1186.40 | 6579.12 | 6584.99 | | 6585.78 | 0.017018 | 5.70 | 179.20 | 52.69 | 0.44 |
| Kettle Creek | 2731.34 | 5-YR | 1807.50 | 6579.12 | 6585.58 | 6584.88 | 6586.95 | 0.022663 | 7.08 | 211.80 | 56.94 | 0.52 |
| Kettle Creek | 2731.34 | 10-YR | 2384.50 | 6579.12 | 6586.13 | 6585.86 | 6587.95 | 0.024786 | 7.86 | 244.31 | 61.32 | 0.55 |
| Kettle Creek | 2731.34 | 25-YR | 2877.00 | 6579.12 | 6587.10 | 6586.59 | 6588.79 | 0.017325 | 7.22 | 307.81 | 70.05 | 0.47 |
| Kettle Creek | 2731.34 | 50-YR | 3657.80 | 6579.12 | 6587.51 | 6587.51 | 6589.79 | 0.021067 | 8.26 | 337.30 | 74.11 | 0.52 |
| Kettle Creek | 2731.34 | 100-YR | 4201.90 | 6579.12 | 6588.00 | 6588.00 | 6590.44 | 0.019970 | 8.38 | 375.21 | 79.01 | 0.52 |
| Kettle Creek | 2597.25 | 2-YR | 1186.40 | 6577.88 | 6582.41 | 6581.63 | 6582.67 | 0.028079 | 4.09 | 287.60 | 141.63 | 0.49 |
| Kettle Creek | 2597.25 | 5-YR | 1807.50 | 6577.88 | 6583.18 | 6582.07 | 6583.51 | 0.021716 | 4.42 | 399.13 | 146.77 | 0.46 |
| Kettle Creek | 2597.25 | 10-YR | 2384.50 | 6577.88 | 6583.52 | 6582.42 | 6583.99 | 0.025342 | 5.14 | 449.29 | 148.75 | 0.50 |
| Kettle Creek | 2597.25 | 25-YR | 2877.00 | 6577.88 | 6582.67 | 6582.67 | 6583.91 | 0.109793 | 8.74 | 324.90 | 143.37 | 1.00 |
| Kettle Creek | 2597.25 | 50-YR | 3657.80 | 6577.88 | 6583.74 | 6583.10 | 6584.71 | 0.047100 | 7.32 | 481.74 | 149.99 | 0.69 |
| Kettle Creek | 2597.25 | 100-YR | 4201.90 | 6577.88 | 6584.34 | 6583.36 | 6585.29 | 0.034433 | 6.97 | 573.33 | 153.16 | 0.61 |
| Kettle Creek | 2067.56 | 2-YR | 1186.40 | 6572.37 | 6574.23 | 6574.15 | 6574.58 | 0.010365 | 1.44 | 270.89 | 286.02 | 0.26 |
| Kettle Creek | 2067.56 | 5-YR | 1807.50 | 6572.37 | 6574.41 | 6574.41 | 6574.99 | 0.013484 | 1.85 | 322.80 | 287.04 | 0.31 |
| Kettle Creek | 2067.56 | 10-YR | 2384.50 | 6572.37 | 6574.65 | 6574.65 | 6575.33 | 0.012373 | 2.02 | 391.92 | 288.39 | 0.31 |
| Kettle Creek | 2067.56 | 25-YR | 2877.00 | 6572.37 | 6575.34 | | 6575.77 | 0.004658 | 1.63 | 591.22 | 292.23 | 0.20 |
| Kettle Creek | 2067.56 | 50-YR | 3657.80 | 6572.37 | 6575.24 | 6575.10 | 6576.02 | 0.008805 | 2.17 | 563.71 | 291.70 | 0.27 |
| Kettle Creek | 2067.56 | 100-YR | 4201.90 | 6572.37 | 6575.28 | 6575.28 | 6576.26 | 0.010960 | 2.45 | 573.82 | 291.89 | 0.31 |
| Kettle Creek | 1361.33 | 2-YR | 1186.40 | 6562.11 | 6566.03 | | 6566.15 | 0.014241 | 2.77 | 428.75 | 219.14 | 0.35 |
| Kettle Creek | 1361.33 | 5-YR | 1807.50 | 6562.11 | 6567.55 | 6565.28 | 6567.64 | 0.005012 | 2.34 | 771.03 | 230.13 | 0.23 |
| Kettle Creek | 1361.33 | 10-YR | 2384.50 | 6562.11 | 6567.84 | | 6567.97 | 0.006692 | 2.84 | 838.33 | 232.38 | 0.26 |
| Kettle Creek | 1361.33 | 25-YR | 2877.00 | 6562.11 | 6565.80 | 6565.80 | 6566.69 | 0.122082 | 7.60 | 378.78 | 213.39 | 1.00 |
| Kettle Creek | 1361.33 | 50-YR | 3657.80 | 6562.11 | 6567.96 | | 6568.24 | 0.014175 | 4.22 | 866.64 | 233.29 | 0.39 |
| Kettle Creek | 1361.33 | 100-YR | 4201.90 | 6562.11 | 6572.62 | | 6572.68 | 0.000877 | 1.80 | 2204.36 | 330.56 | 0.11 |
| Kettle Creek | 670.23 | 2-YR | 1186.40 | 6554.40 | 6558.15 | 6556.90 | 6558.30 | 0.009335 | 2.63 | 417.76 | 187.86 | 0.29 |
| Kettle Creek | 670.23 | 5-YR | 1807.50 | 6554.40 | 6557.25 | 6557.25 | 6558.08 | 0.116483 | 6.88 | 254.96 | 175.42 | 0.96 |
| Kettle Creek | 670.23 | 10-YR | 2384.50 | 6554.40 | 6558.13 | | 6558.75 | 0.038510 | 5.32 | 415.19 | 187.68 | 0.60 |
| Kettle Creek | 670.23 | 25-YR | 2877.00 | 6554.40 | 6562.37 | | 6562.49 | 0.001111 | 1.76 | 1295.19 | 223.69 | 0.12 |
| Kettle Creek | 670.23 | 50-YR | 3657.80 | 6554.40 | 6567.79 | | 6567.83 | 0.000154 | 0.97 | 2958.07 | 451.29 | 0.05 |
| Kettle Creek | 670.23 | 100-YR | 4201.90 | 6554.40 | 6572.60 | | 6572.61 | 0.000030 | 0.53 | 5287.89 | 512.72 | 0.02 |
| Kettle Creek | 6.23 | 2-YR | 1186.40 | 6550.00 | 6551.80 | 6550.89 | 6551.90 | 0.008487 | 1.96 | 549.53 | 342.68 | 0.26 |
| Kettle Creek | 6,23 | 5-YR | 1807.50 | 6550.00 | 6554.80 | 6551.15 | 6554.83 | 0.000460 | 0.90 | 1674.92 | 408.50 | 0.07 |
| Kettle Creek | 6.23 | 10-YR | 2384.50 | 6550.00 | 6558.30 | 6551.40 | 6558.31 | 0.000091 | 0.58 | 3281.63 | 527.79 | 0.04 |



HEC-RAS Plan: Existing River: Kettle Creek Reach: Kettle Creek (Continued)

| Reach | River Sta | Profile | Q Total | Min Ch El | W.S. Elev | Crit W.S. | E.G. Elev (ft) | E.G. Slope (ft/ft) | Vel Chnl | Flow Area | Top Width | Froude # Chl |
|--------------|-----------|---------|---------|-----------|-----------|-----------|-------------------|-----------------------|----------|-----------|-----------|--------------|
| | | | (cfs) | (ft) | (ft) | (ft) | | | (ft/s) | (sq ft) | (ft) | |
| Kettle Creek | 6.23 | 25-YR | 2877.00 | 6550.00 | 6562.40 | 6551.61 | 6562.41 | 0.000019 | 0.34 | 5987.04 | 736.04 | 0.02 |
| Kettle Creek | 6.23 | 50-YR | 3657.80 | 6550.00 | 6567.80 | 6551.91 | 6567.80 | 0.000005 | 0.23 | 10188.80 | 820.31 | 0.01 |
| Kettle Creek | 6.23 | 100-YR | 4201.90 | 6550.00 | 6572.60 | 6551.98 | 6572.60 | 0.000002 | 0.17 | 14318.65 | 901.20 | 0.01 |

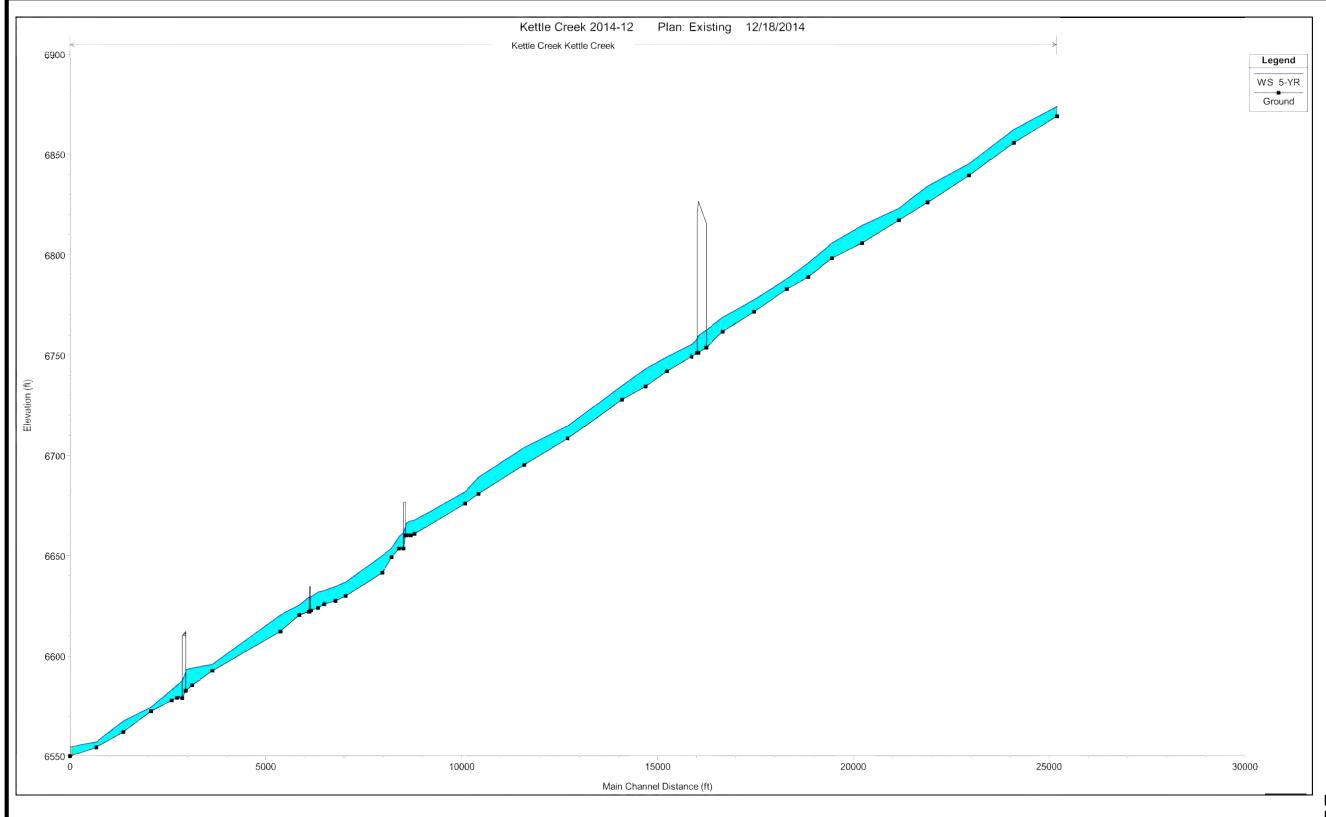


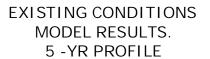






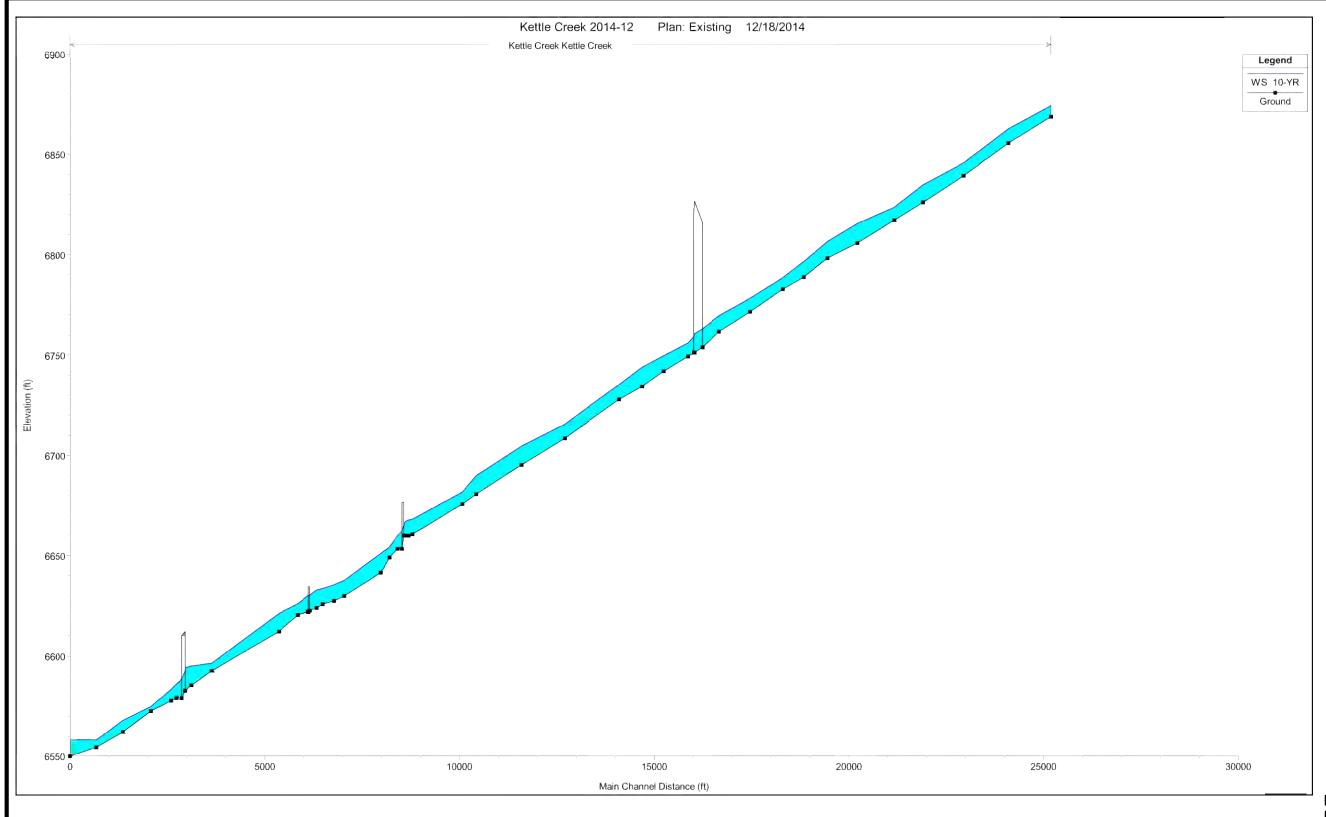
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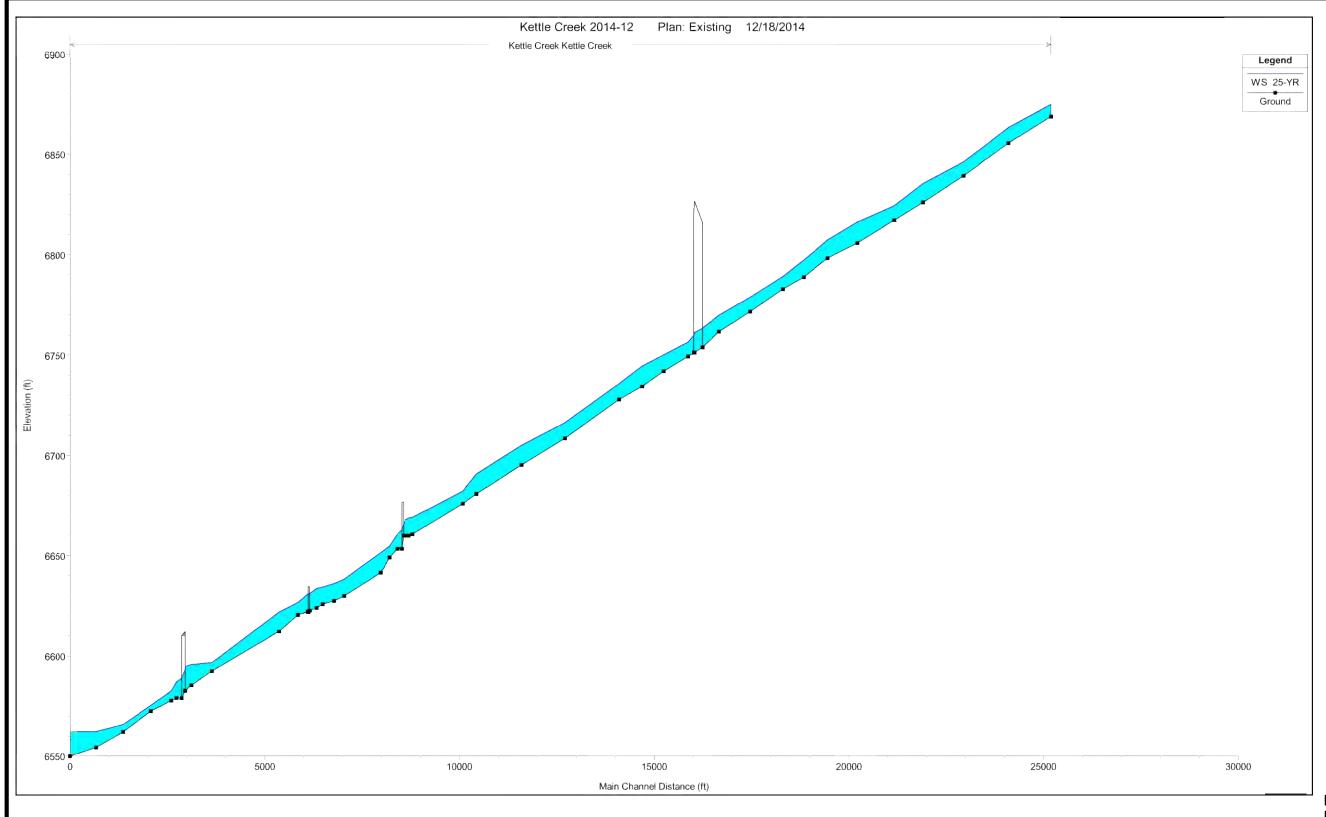
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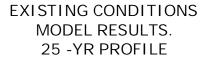






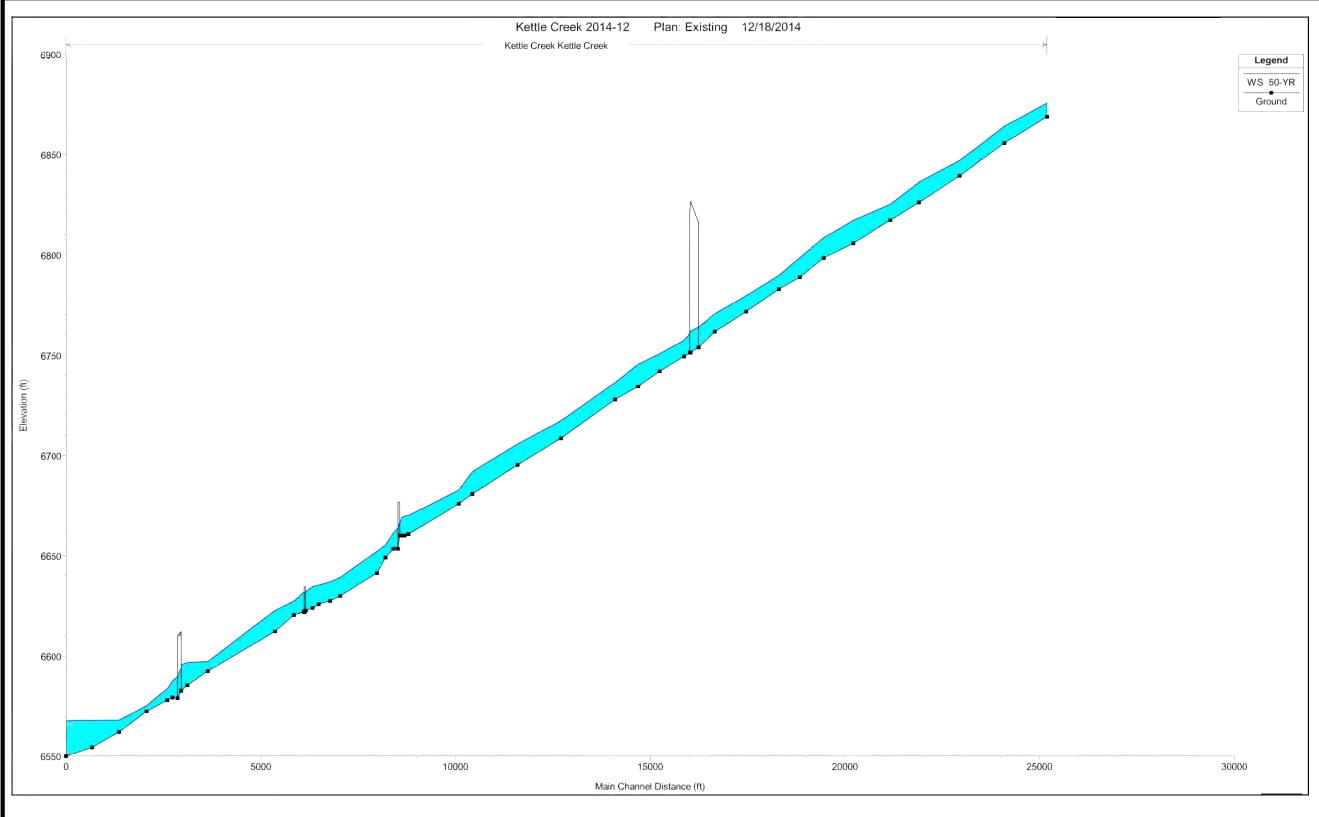
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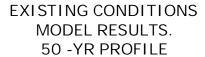






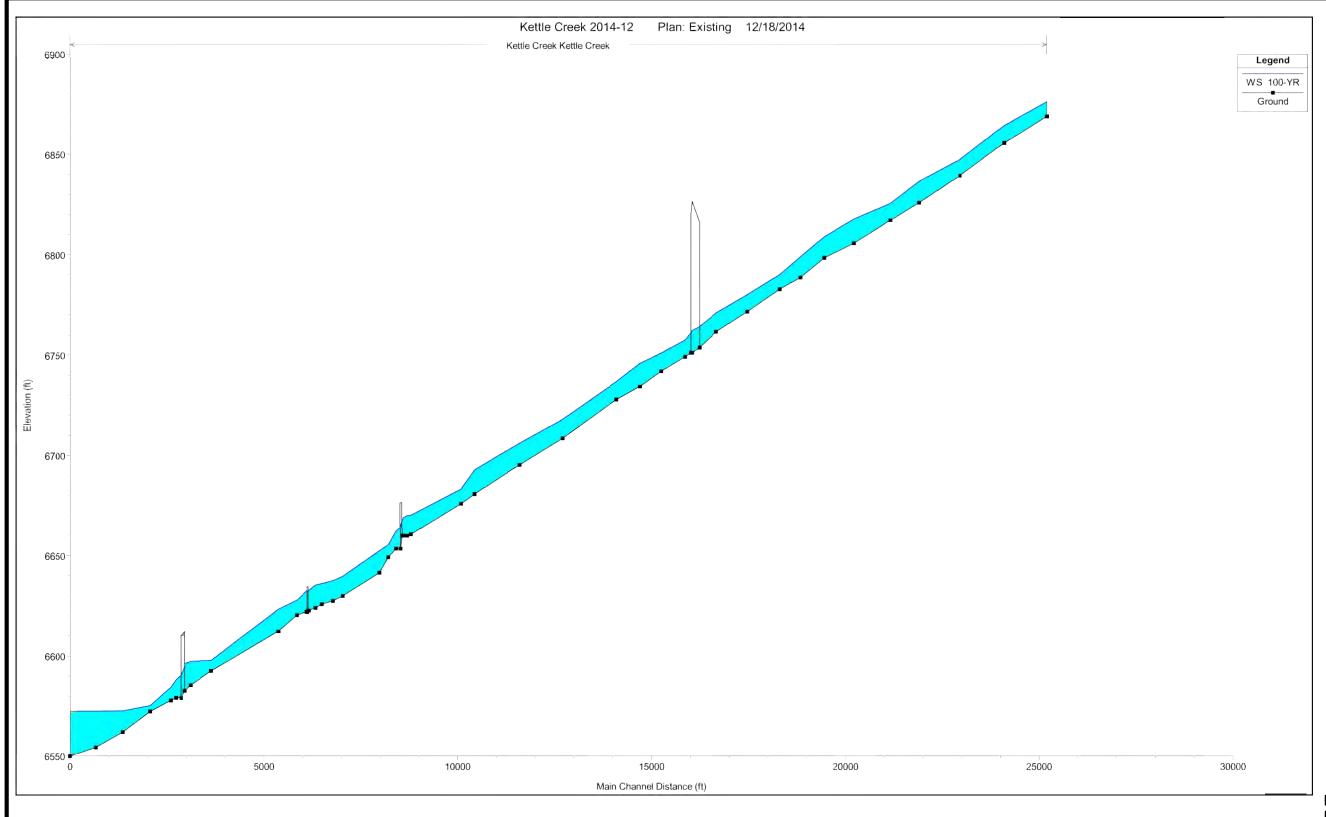
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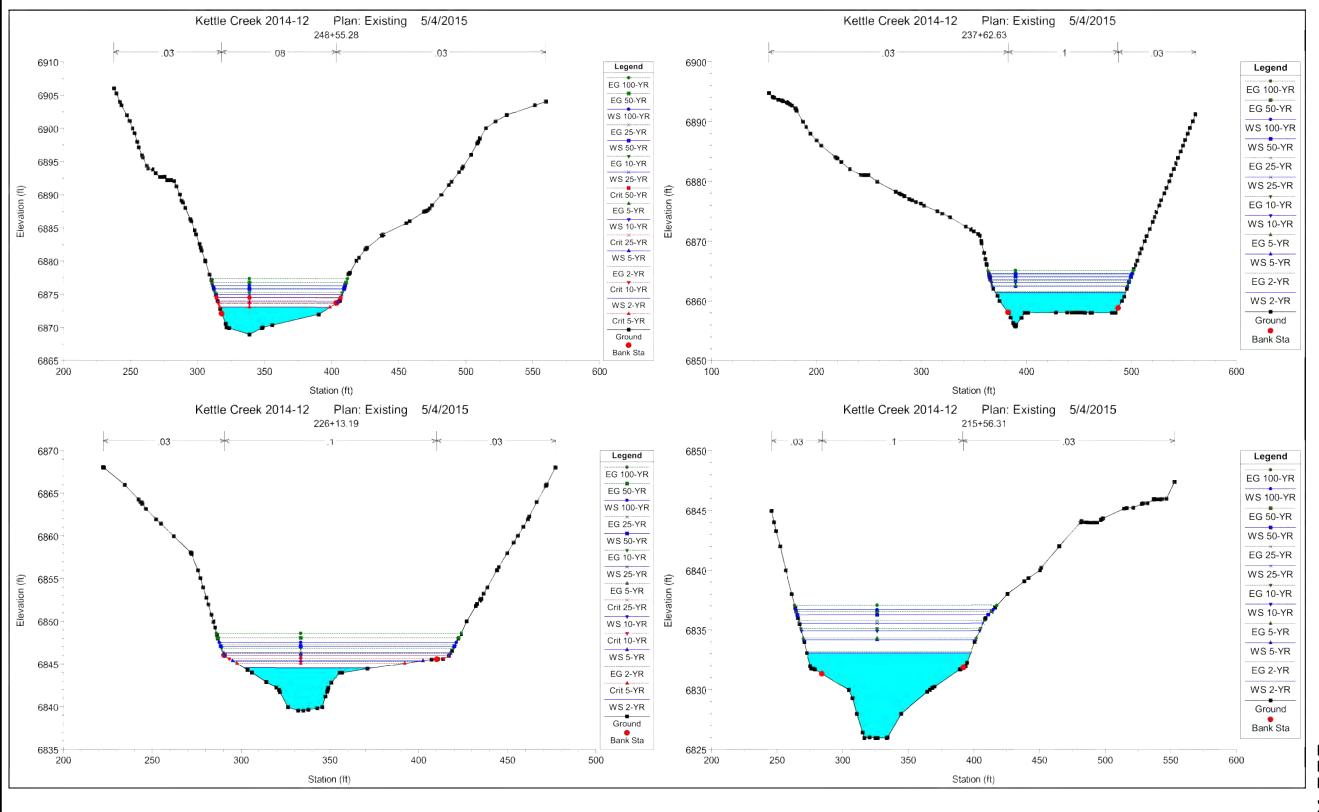
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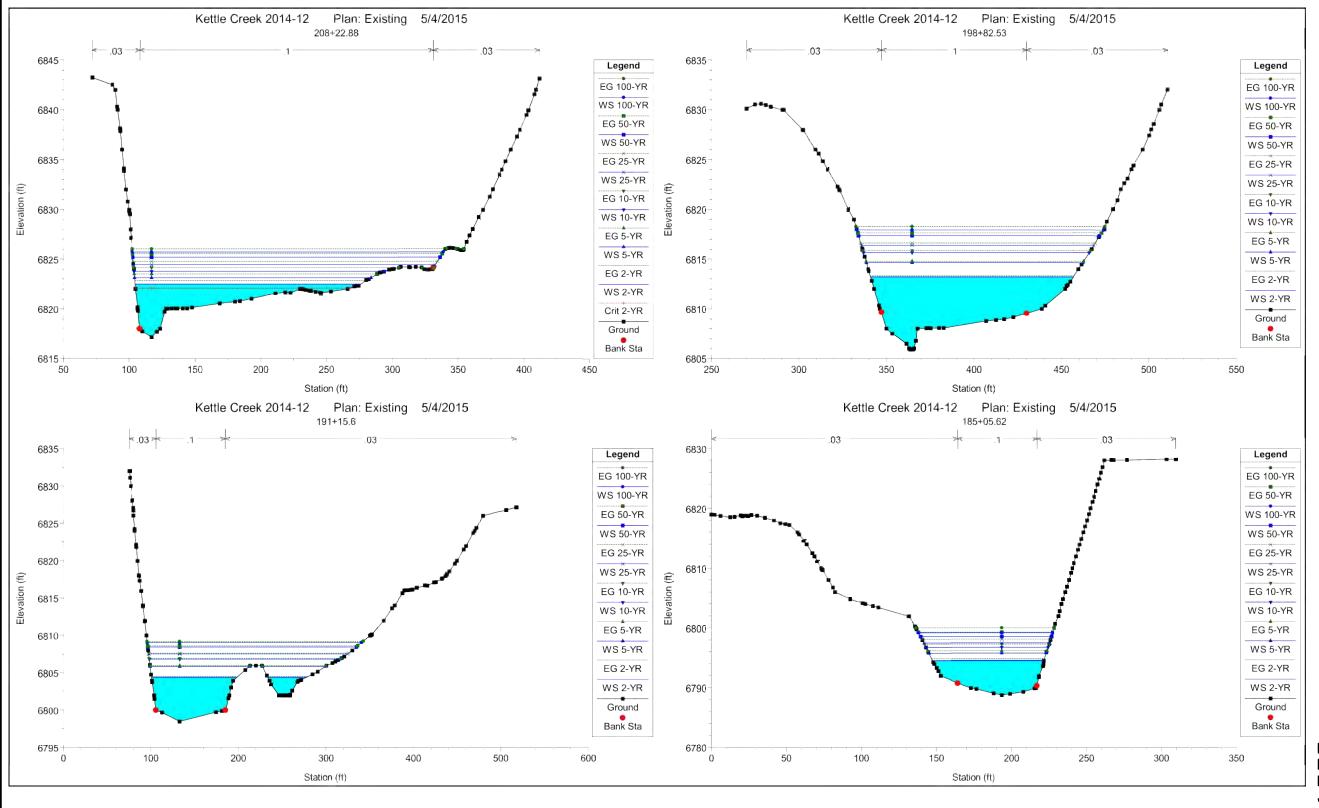


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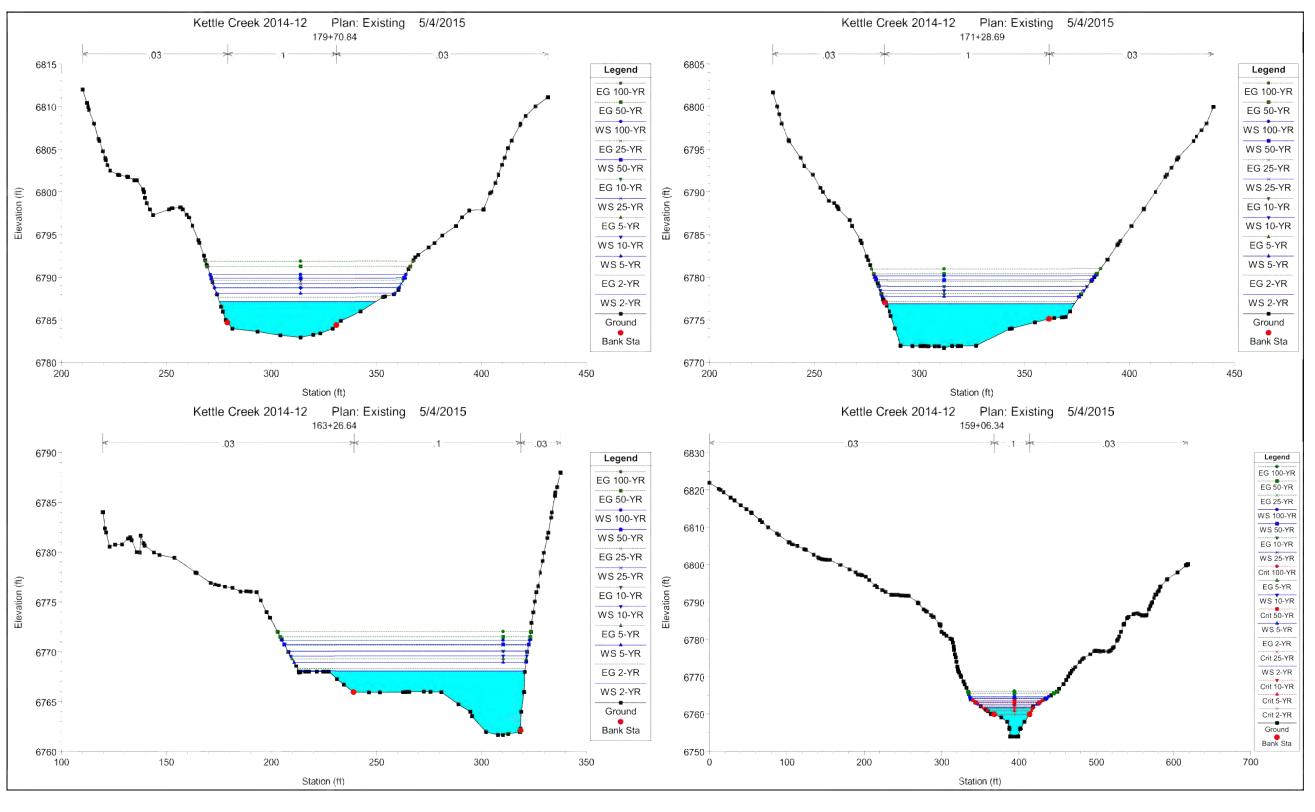






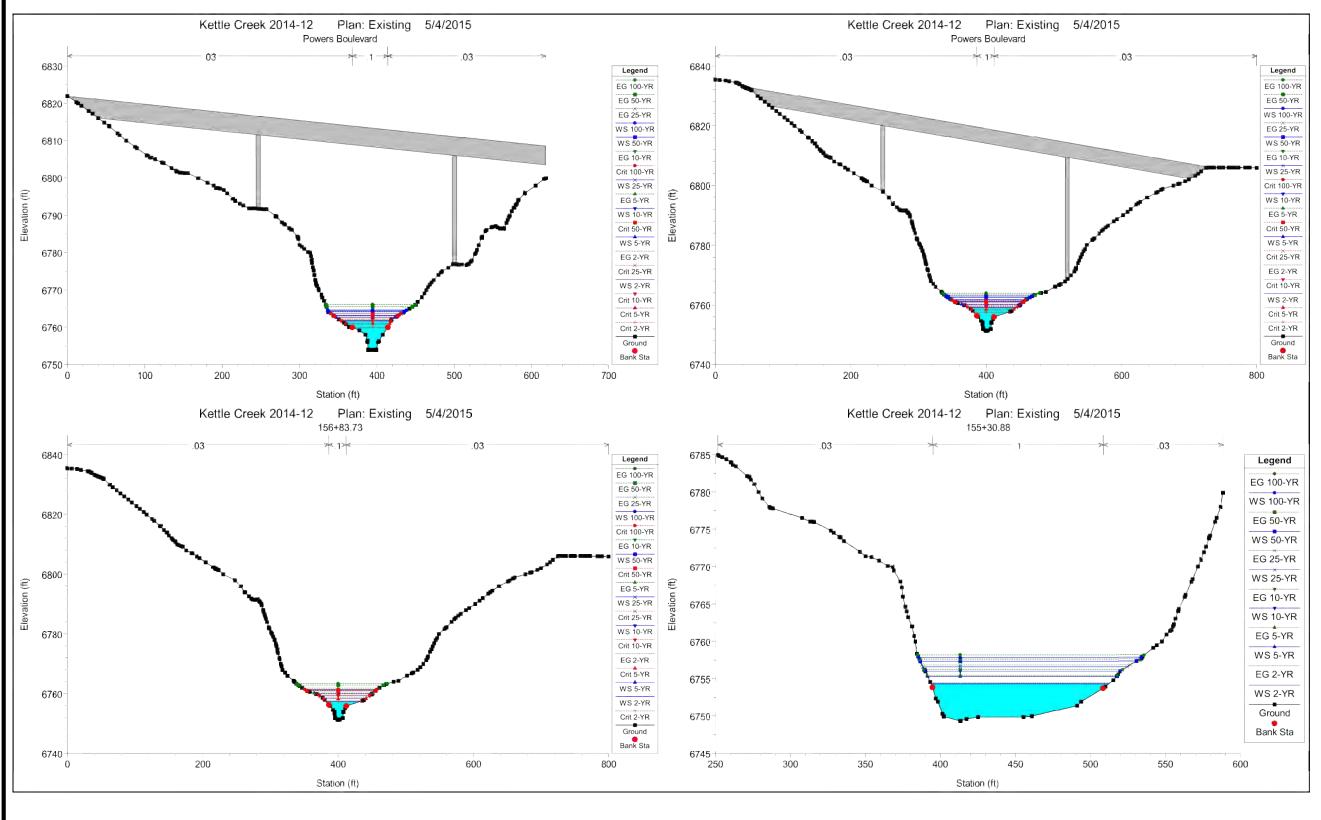






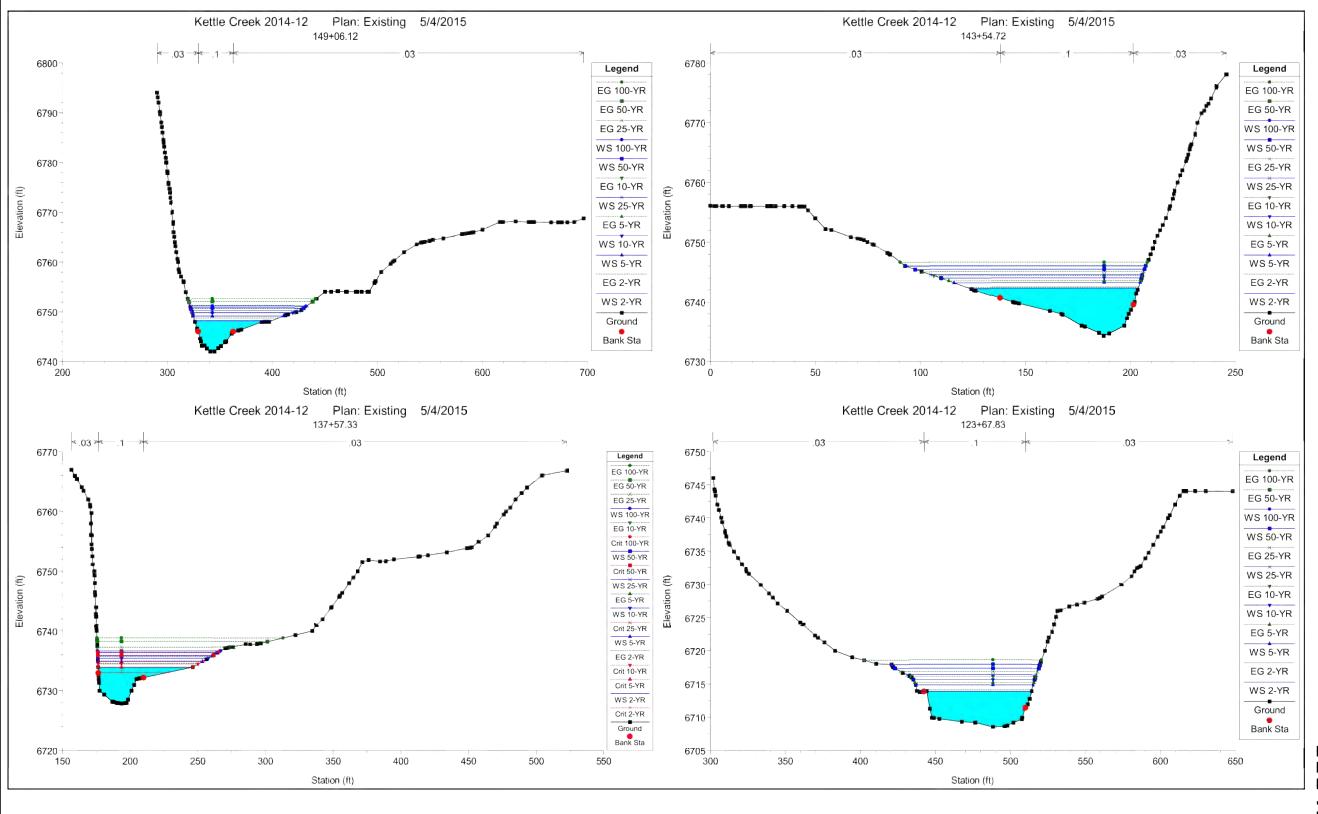






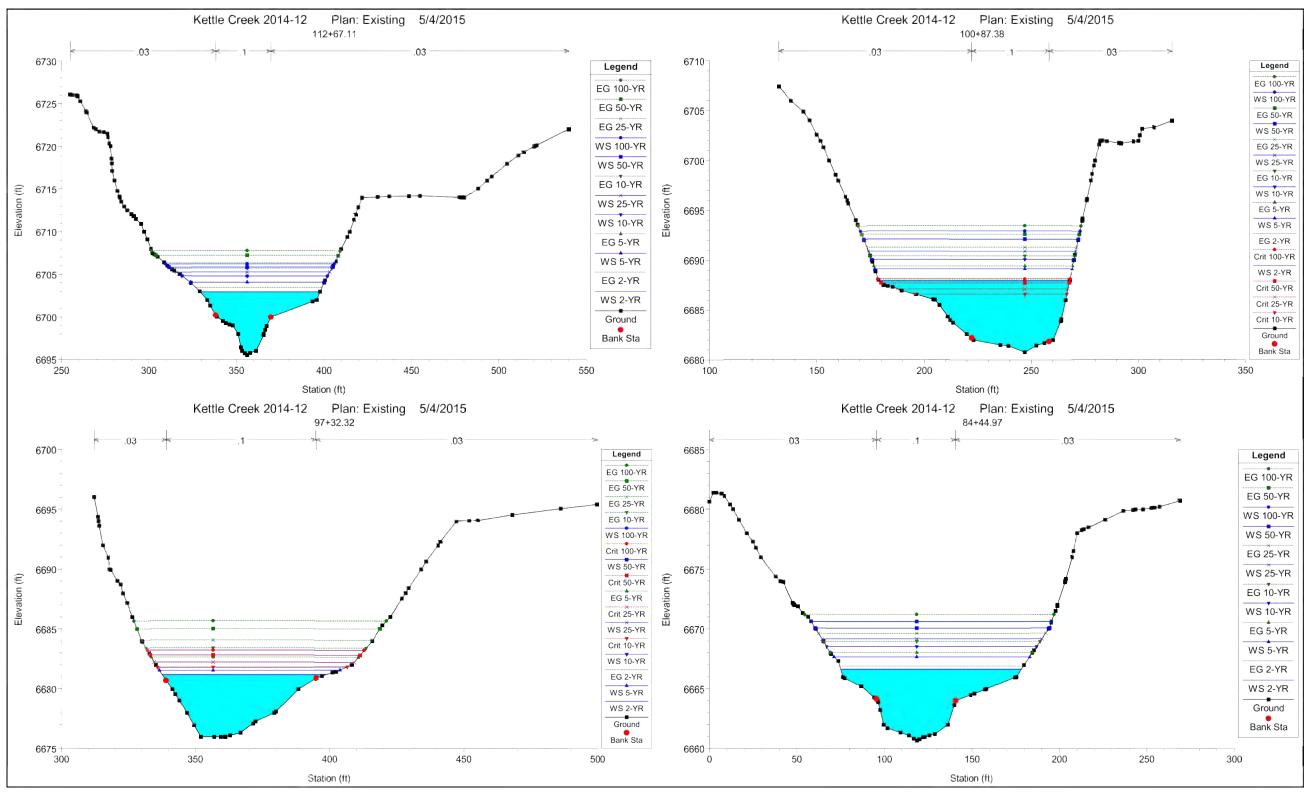






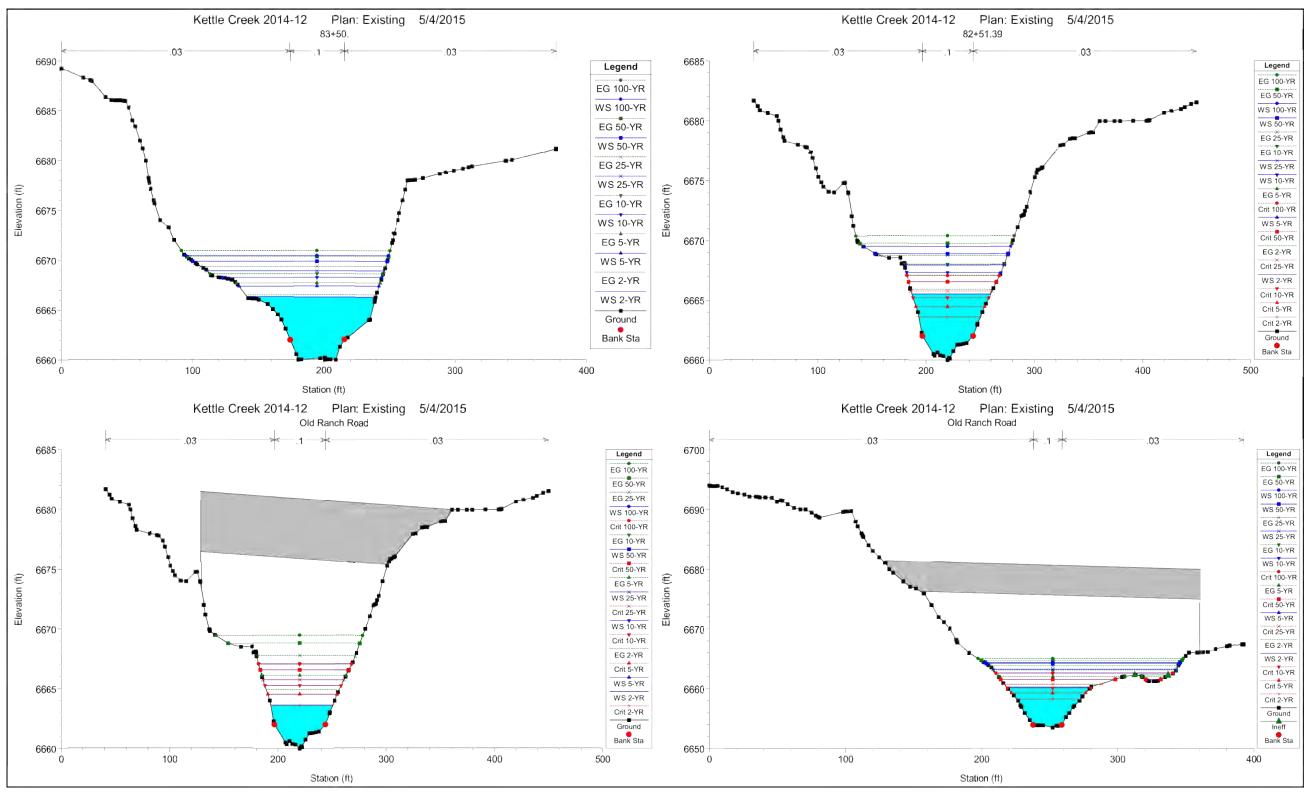








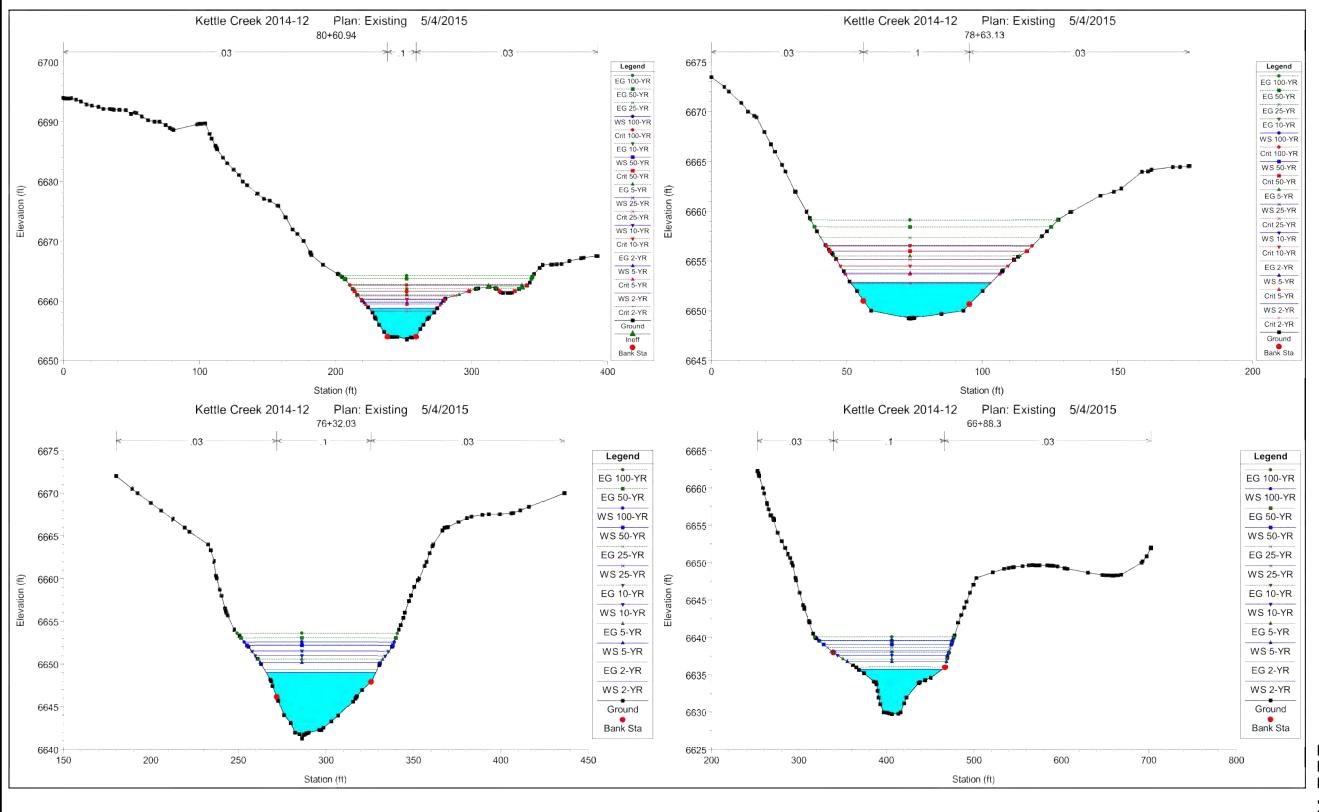






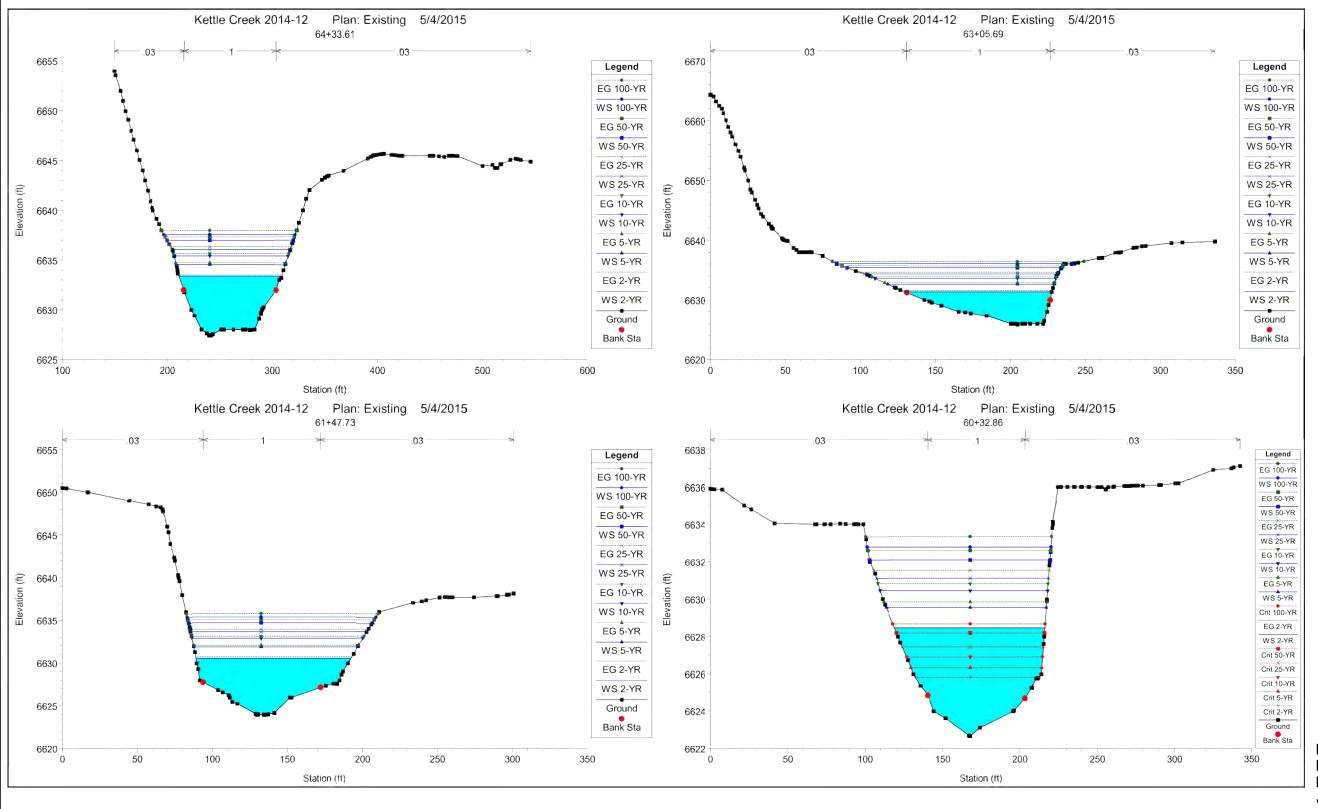


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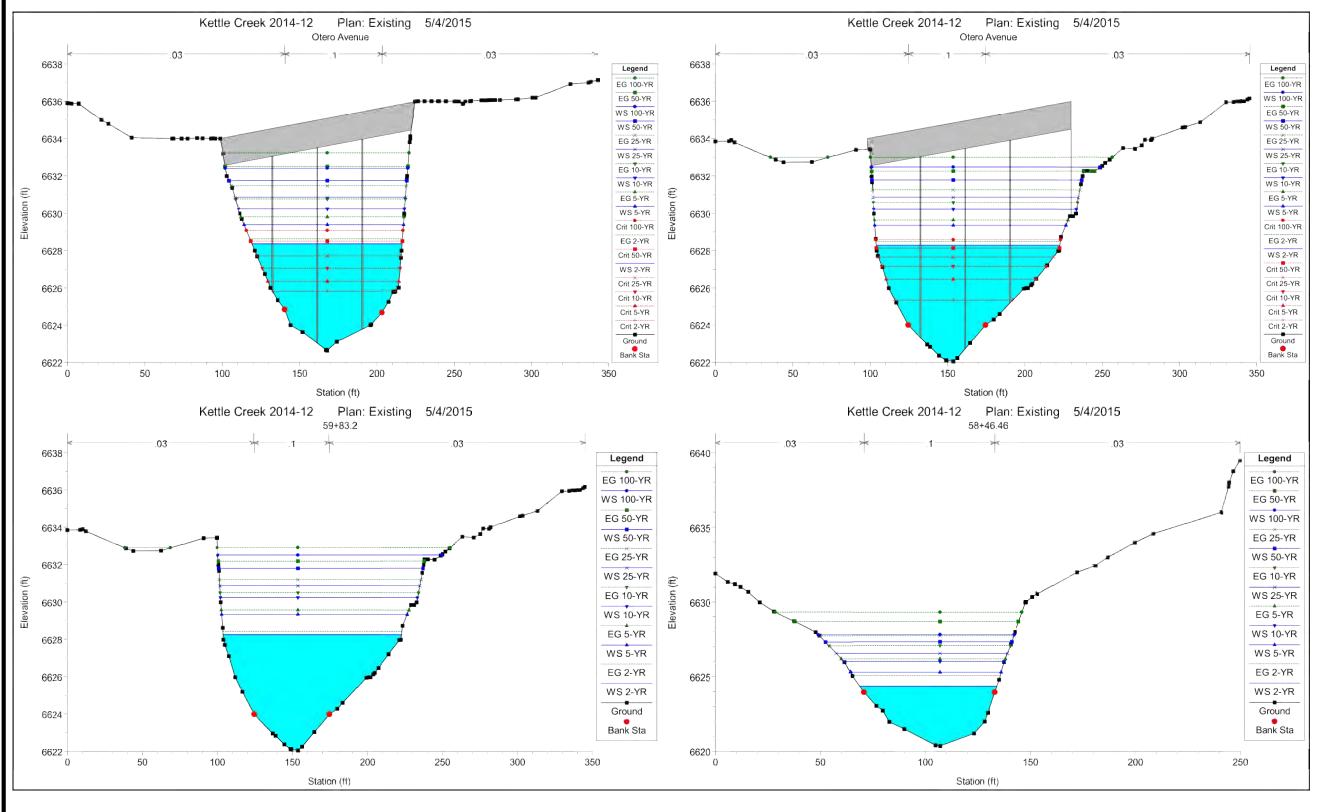






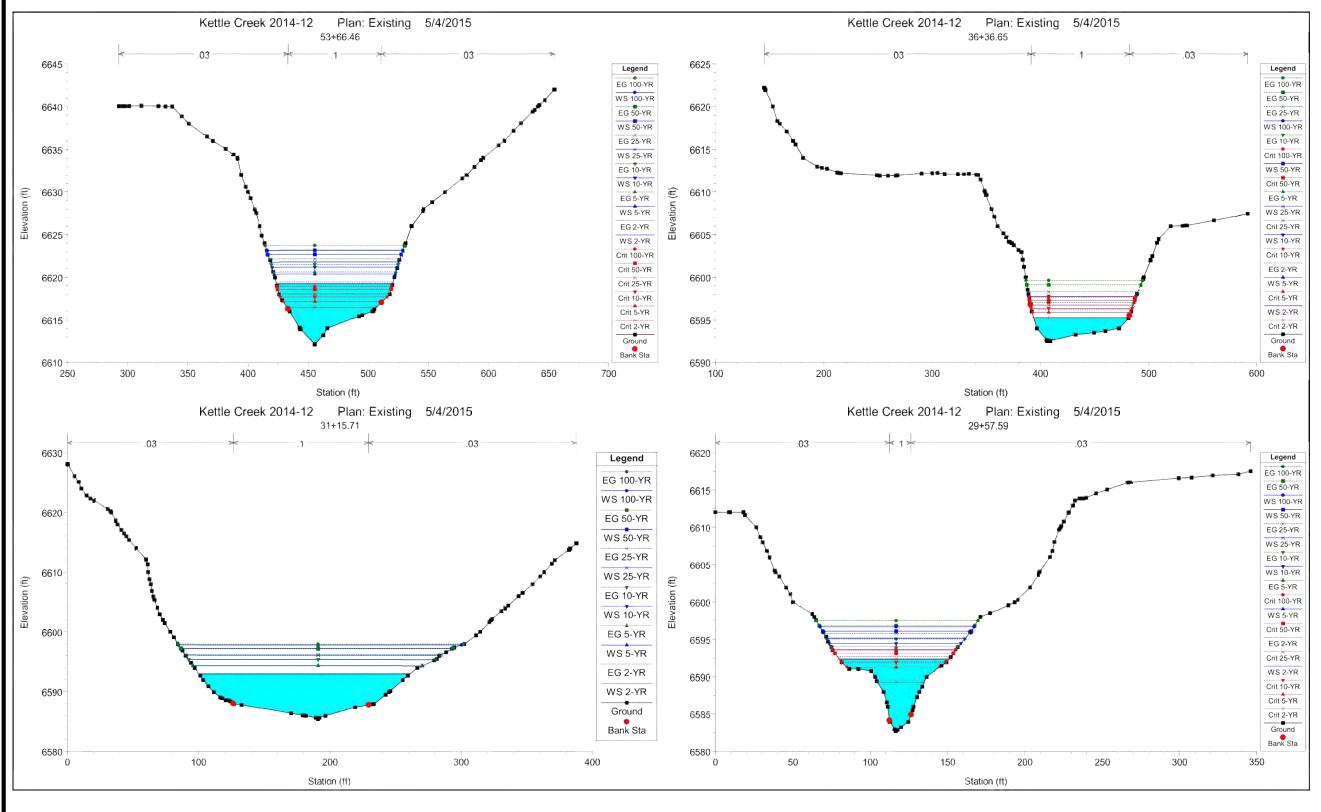






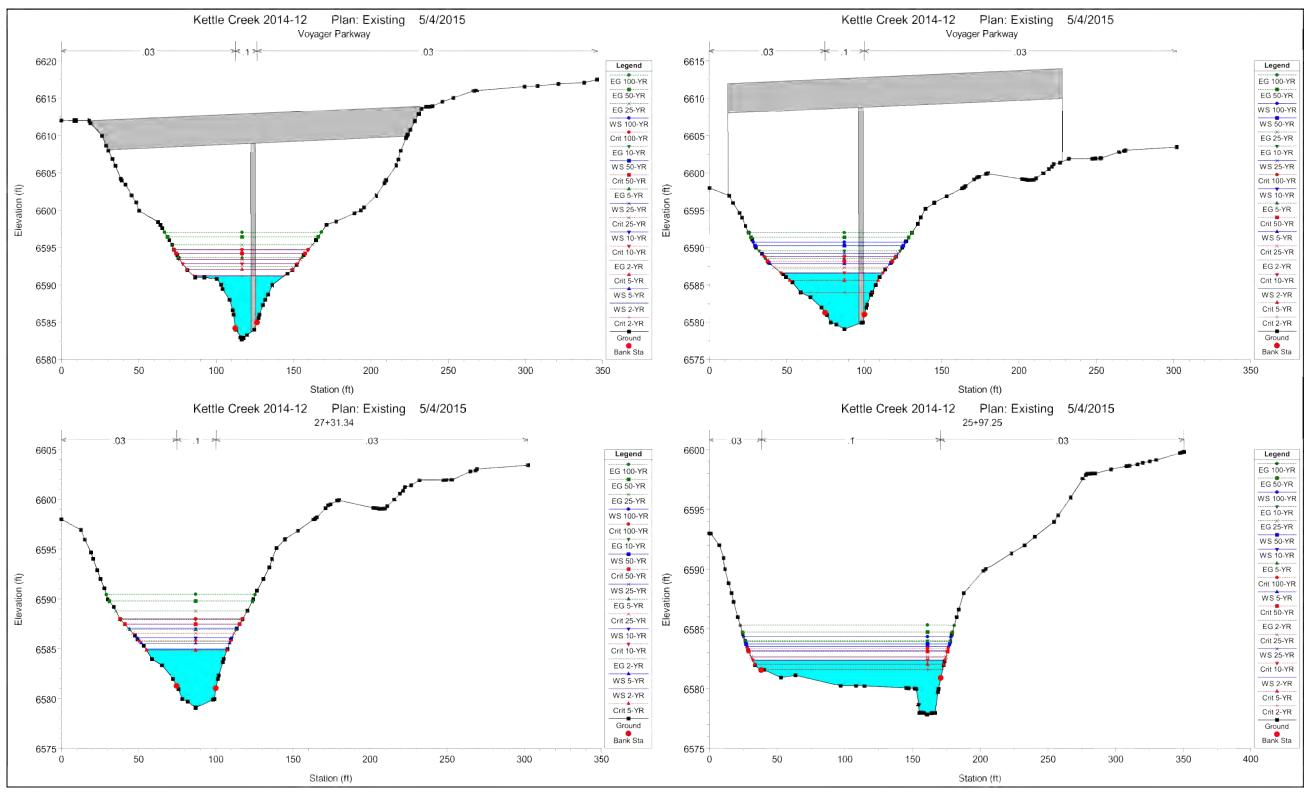






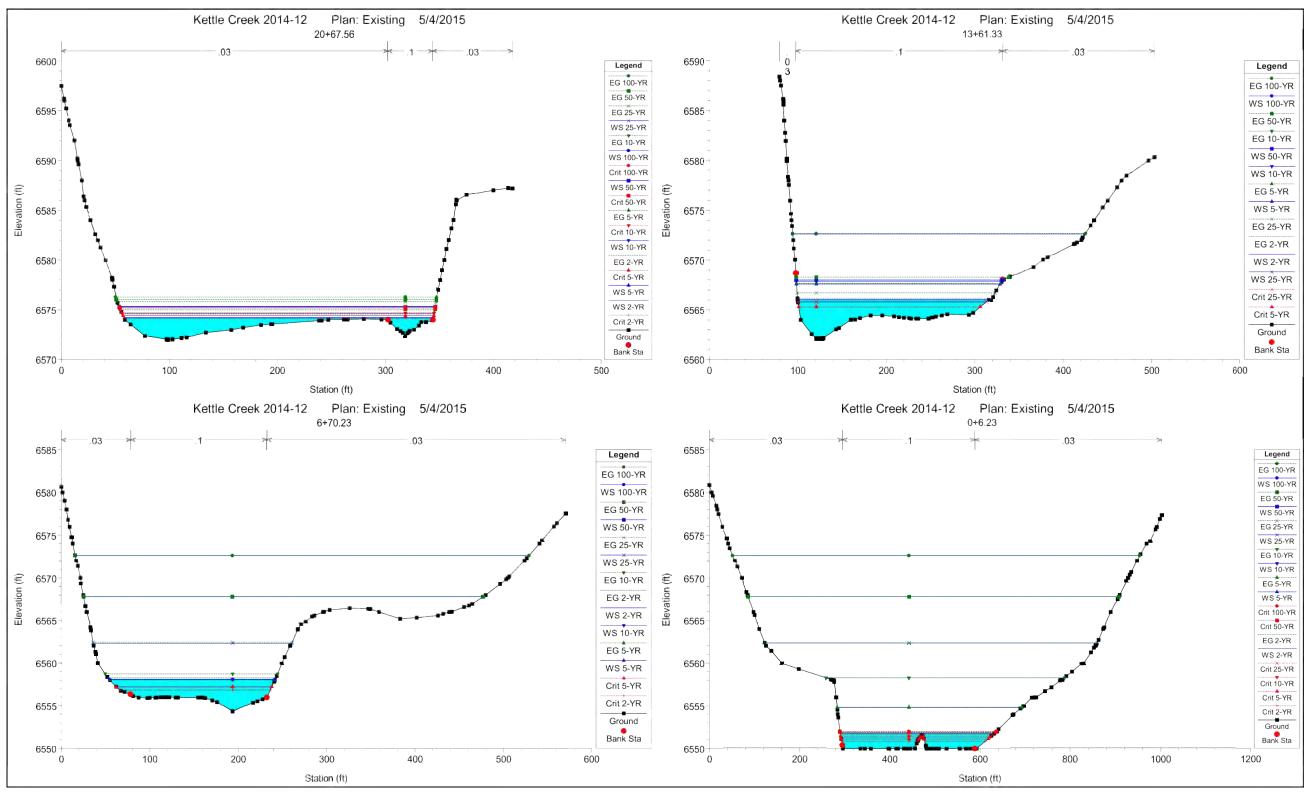
















HEC-RAS Plan: Future River: Kettle Creek Reach: Kettle Creek

| Reach | River Sta | Profile | Q Total | Min Ch El | W.S. Elev | Crit W.S. | E.G. Elev | E.G. Slope | Vel Chni | Flow Area | Top Width | Froude # Chl |
|--------------|-----------|---------|---------|-----------|-----------|-----------|-----------|------------|----------|-----------|-----------|--------------|
| | | | (cfs) | (ft) | (ft) | (ft) | (ft) | (ft/ft) | (ft/s) | (sq ft) | (ft) | |
| Kettle Creek | 24855.28 | 2-YR | 1122.90 | 6868.95 | 6873.06 | | 6873.58 | 0.030051 | 5.76 | 195.11 | 82.02 | 0.65 |
| Kettle Creek | 24855.28 | 5-YR | 1711.40 | 6868.95 | 6873.81 | 6873.05 | 6874.48 | 0.029613 | 6.61 | 258.80 | 88.95 | 0.67 |
| Kettle Creek | 24855.28 | 10-YR | 2258.20 | 6868.95 | 6874.45 | 6873.58 | 6875.24 | 0.026325 | 7.10 | 317.83 | 92.16 | 0.66 |
| Kettle Creek | 24855,28 | 25-YR | 2725.50 | 6868.95 | 6874.94 | 6873.98 | 6875.82 | 0.024772 | 7.49 | 363.14 | 93.79 | 0.65 |
| Kettle Creek | 24855.28 | 50-YR | 3471.20 | 6868.95 | 6875.75 | 6874.52 | 6876.72 | 0.021342 | 7.83 | 440.39 | 96.58 | 0.62 |
| Kettle Creek | 24855.28 | 100-YR | 3992.10 | 6868.95 | 6876.25 | | 6877.29 | 0.020000 | 8.09 | 489.10 | 98.23 | 0.61 |
| Kettle Creek | 23762.63 | 2-YR | 1146.00 | 6855.75 | 6861.45 | | 6861.60 | 0.005625 | 2.60 | 409.41 | 124.38 | 0.24 |
| Kettle Creek | 23762.63 | 5-YR | 1747.20 | 6855.75 | 6862.37 | | 6862.59 | 0.005586 | 3.02 | 525.84 | 128.59 | 0.25 |
| Kettle Creek | 23762.63 | 10-YR | 2306.30 | 6855.75 | 6863.00 | | 6863.30 | 0.005915 | 3.39 | 608.09 | 130.75 | 0.26 |
| Kettle Creek | 23762.63 | 25-YR | 2784.30 | 6855.75 | 6863.49 | | 6863.86 | 0.006102 | 3.66 | 673.23 | 132.72 | 0.27 |
| Kettle Creek | 23762.63 | 50-YR | 3543.00 | 6855.75 | 6864.09 | | 6864.57 | 0.006741 | 4.11 | 753.38 | 134.99 | 0.29 |
| Kettle Creek | 23762.63 | 100-YR | 4072.10 | 6855.75 | 6864.48 | | 6865.04 | 0.007096 | 4.39 | 805.38 | 136.33 | 0.30 |
| Kettle Creek | 22613.19 | 2-YR | 1146.00 | 6839.60 | 6844.55 | | 6845.35 | 0.081202 | 7.16 | 160.15 | 71.42 | 0.84 |
| Kettle Creek | 22613.19 | 5-YR | 1747.20 | 6839.60 | 6845.42 | 6845.11 | 6846.26 | 0.086001 | 7.35 | 237.56 | 106.79 | 0.87 |
| Kettle Creek | 22613.19 | 10-YR | 2306.30 | 6839.60 | 6846.03 | 6845.68 | 6846.89 | 0.071821 | 7.44 | 310.53 | 126.15 | 0.81 |
| Kettle Creek | 22613.19 | 25-YR | 2784.30 | 6839.60 | 6846.39 | 6846.04 | 6847.34 | 0.066562 | 7.80 | 356.21 | 128.00 | 0.80 |
| Kettle Creek | 22613.19 | 50-YR | 3543.00 | 6839.60 | 6847.12 | | 6848.10 | 0.049389 | 7.78 | 449.79 | 131.25 | 0.72 |
| Kettle Creek | 22613.19 | 100-YR | 4072.10 | 6839.60 | 6847.56 | | 6848.60 | 0.043173 | 7.85 | 508.54 | 133.19 | 0.68 |
| Kettle Creek | 21556,31 | 2-YR | 1161.30 | 6825.98 | 6833.12 | | 6833.22 | 0.004278 | 2.48 | 461.11 | 124.93 | 0.22 |
| Kettle Creek | 21556.31 | 5-YR | 1768.70 | 6825.98 | 6834.19 | | 6834.34 | 0.004118 | 2.84 | 598.42 | 131.29 | 0.22 |
| Kettle Creek | 21556.31 | 10-YR | 2333.30 | 6825.98 | 6834.96 | | 6835.15 | 0.004204 | 3.14 | 700.85 | 136.27 | 0.23 |
| Kettle Creek | 21556.31 | 25-YR | 2815.70 | 6825.98 | 6835.56 | | 6835.80 | 0.004177 | 3.34 | 784.83 | 140.22 | 0.23 |
| Kettle Creek | 21556.31 | 50-YR | 3581.10 | 6825.98 | 6836.26 | | 6836.57 | 0.004527 | 3.72 | 884.84 | 145.93 | 0.24 |
| Kettle Creek | 21556.31 | 100-YR | 4114.60 | 6825.98 | 6836.71 | | 6837.06 | 0.004721 | 3.96 | 950.73 | 150.63 | 0.25 |
| Kettle Creek | 20822.88 | 2-YR | 1161.30 | 6817.21 | 6822.51 | 6822.11 | 6822.84 | 0.028241 | 3.63 | 303.24 | 171.42 | 0.48 |
| Kettle Creek | 20822.88 | 5-YR | 1768.70 | 6817.21 | 6823.13 | | 6823.51 | 0.025390 | 4.10 | 412.37 | 179.43 | 0.48 |
| Kettle Creek | 20822.88 | 10-YR | 2333.30 | 6817.21 | 6823.79 | | 6824.16 | 0.020564 | 4.21 | 532.50 | 190.41 | 0.44 |
| Kettle Creek | 20822.88 | 25-YR | 2815.70 | 6817.21 | 6824.44 | | 6824.79 | 0.017615 | 4.03 | 670.86 | 229.14 | 0.41 |
| Kettle Creek | 20822.88 | 50-YR | 3581.10 | 6817.21 | 6825.20 | | 6825.53 | 0.013351 | 4.09 | 846.03 | 233.42 | 0.38 |
| Kettle Creek | 20822.88 | 100-YR | 4114.60 | 6817.21 | 6825.72 | | 6826.04 | 0.011361 | 4.12 | 967.36 | 236.32 | 0.35 |
| Kettle Creek | 19882.53 | 2-YR | 1156.70 | 6805.92 | 6813.25 | | 6813.36 | 0.002271 | 2.06 | 492.35 | 116.30 | 0.16 |
| Kettle Creek | 19882.53 | 5-YR | 1760.90 | 6805.92 | 6814.66 | | 6814.81 | 0.001906 | 2.22 | 661.74 | 124.04 | 0.15 |
| Kettle Creek | 19882.53 | 10-YR | 2323.10 | 6805.92 | 6815.67 | | 6815.86 | 0.001816 | 2.39 | 789.74 | 129.46 | 0.15 |
| Kettle Creek | 19882.53 | 25-YR | 2805.10 | 6805.92 | 6816.38 | | 6816.61 | 0.001811 | 2.54 | 883.45 | 133.21 | 0.16 |



HEC-RAS Plan: Future River: Kettle Creek Reach: Kettle Creek (Continued)

| Reach | River Sta | Profile | Q Total | Min Ch El | W.S. Elev | Crit W.S. | E.G. Elev | E.G. Slope | Vel Chnl | Flow Area | Top Width | Froude # Chl |
|--------------|-----------|---------|---------|-----------|-----------|-----------|-----------|------------|----------|-----------|-----------|--------------|
| | | | (cfs) | (ft) | (ft) | (ft) | (ft) | (ft/ft) | (ft/s) | (sq ft) | (ft) | |
| Kettle Creek | 19882.53 | 50-YR | 3570.80 | 6805.92 | 6817.34 | | 6817.63 | 0.001841 | 2.75 | 1014.40 | 138.15 | 0.16 |
| Kettle Creek | 19882.53 | 100-YR | 4104.90 | 6805.92 | 6817.93 | | 6818.26 | 0.001879 | 2.90 | 1096.30 | 141.38 | 0.16 |
| Kettle Creek | 19115.6 | 2-YR | 1162.10 | 6798.52 | 6804.50 | | 6804.58 | 0.002183 | 2.08 | 512.13 | 143.23 | 0.16 |
| Kettle Creek | 19115.6 | 5-YR | 1768.50 | 6798.52 | 6805.91 | | 6806.01 | 0.001539 | 2.05 | 746.39 | 185.26 | 0.14 |
| Kettle Creek | 19115.6 | 10-YR | 2332.00 | 6798.52 | 6806.88 | | 6806.99 | 0.001267 | 2.04 | 947.51 | 217.51 | 0.13 |
| Kettle Creek | 19115.6 | 25-YR | 2813.20 | 6798.52 | 6807.55 | | 6807.67 | 0.001117 | 2.03 | 1095.71 | 227.11 | 0.12 |
| Kettle Creek | 19115.6 | 50-YR | 3576.10 | 6798.52 | 6808.47 | | 6808.62 | 0.000969 | 2.03 | 1311.58 | 238.34 | 0.12 |
| Kettle Creek | 19115.6 | 100-YR | 4108.00 | 6798.52 | 6809.06 | | 6809.22 | 0.000901 | 2.04 | 1452.78 | 245.24 | 0.11 |
| Kettle Creek | 18505.62 | 2-YR | 1162.10 | 6788.84 | 6794.63 | | 6794.90 | 0.004982 | 3.09 | 323.14 | 74.60 | 0.24 |
| Kettle Creek | 18505.62 | 5-YR | 1768.50 | 6788.84 | 6795.84 | | 6796.24 | 0.004888 | 3.53 | 415.61 | 78.31 | 0.25 |
| Kettle Creek | 18505.62 | 10-YR | 2332.00 | 6788.84 | 6796.80 | | 6797.32 | 0.004790 | 3.85 | 492.77 | 81.52 | 0.25 |
| Kettle Creek | 18505.62 | 25-YR | 2813.20 | 6788.84 | 6797.54 | | 6798.13 | 0.004733 | 4.08 | 553.41 | 84.02 | 0.25 |
| Kettle Creek | 18505.62 | 50-YR | 3576.10 | 6788.84 | 6798.57 | | 6799.29 | 0.004665 | 4.39 | 642.26 | 87.33 | 0.26 |
| Kettle Creek | 18505.62 | 100-YR | 4108.00 | 6788.84 | 6799.23 | | 6800.02 | 0.004631 | 4.58 | 700.30 | 89.57 | 0.26 |
| Kettle Creek | 17970.84 | 2-YR | 1162.10 | 6783.01 | 6787.21 | | 6787.71 | 0.018099 | 4.75 | 222.12 | 74.89 | 0.44 |
| Kettle Creek | 17970.84 | 5-YR | 1768.50 | 6783.01 | 6788.16 | | 6788.82 | 0.016152 | 5.22 | 297.05 | 84.92 | 0.43 |
| Kettle Creek | 17970.84 | 10-YR | 2332.00 | 6783.01 | 6788.79 | | 6789.68 | 0.015410 | 5.56 | 352.22 | 88.06 | 0.43 |
| Kettle Creek | 17970.84 | 25-YR | 2813.20 | 6783.01 | 6789.26 | | 6790.34 | 0.015057 | 5.82 | 393.89 | 89.72 | 0.43 |
| Kettle Creek | 17970.84 | 50-YR | 3576.10 | 6783.01 | 6789.92 | | 6791.30 | 0.014768 | 6.19 | 453.59 | 91.93 | 0.43 |
| Kettle Creek | 17970.84 | 100-YR | 4108.00 | 6783.01 | 6790.34 | | 6791.91 | 0.014651 | 6.44 | 492.08 | 93.36 | 0.44 |
| Kettle Creek | 17128.69 | 2-YR | 1162.10 | 6771.75 | 6776.95 | | 6777.16 | 0.009159 | 3.48 | 322.58 | 90.49 | 0.31 |
| Kettle Creek | 17128.69 | 5-YR | 1768.50 | 6771.75 | 6777.78 | | 6778.13 | 0.010250 | 4.18 | 399.60 | 94.30 | 0.34 |
| Kettle Creek | 17128.69 | 10-YR | 2332.00 | 6771.75 | 6778.45 | | 6778.92 | 0.010739 | 4.68 | 464.22 | 97.26 | 0.35 |
| Kettle Creek | 17128.69 | 25-YR | 2813.20 | 6771.75 | 6778.97 | | 6779.53 | 0.011028 | 5.04 | 514.76 | 99.52 | 0.36 |
| Kettle Creek | 17128.69 | 50-YR | 3576.10 | 6771.75 | 6779.71 | | 6780.43 | 0.011275 | 5.51 | 589.75 | 103.05 | 0.38 |
| Kettle Creek | 17128.69 | 100-YR | 4108.00 | 6771.75 | 6780.17 | | 6781.00 | 0.011409 | 5.80 | 638.23 | 105.33 | 0.38 |
| Kettle Creek | 16326.64 | 2-YR | 1162.10 | 6761.71 | 6768.11 | | 6768.35 | 0.013462 | 3.91 | 294.50 | 107.87 | 0.37 |
| Kettle Creek | 16326.64 | 5-YR | 1768.50 | 6761.71 | 6768.98 | | 6769.33 | 0.011883 | 4.28 | 389.99 | 110.49 | 0.36 |
| Kettle Creek | 16326.64 | 10-YR | 2332.00 | 6761.71 | 6769.62 | | 6770.09 | 0.011431 | 4.60 | 461.03 | 112.47 | 0.36 |
| Kettle Creek | 16326.64 | 25-YR | 2813.20 | 6761.71 | 6770.10 | | 6770.68 | 0.011211 | 4.84 | 515.32 | 114.01 | 0.37 |
| Kettle Creek | 16326.64 | 50-YR | 3576.10 | 6761.71 | 6770.76 | | 6771.52 | 0.011127 | 5.21 | 591.61 | 116.43 | 0.37 |
| Kettle Creek | 16326.64 | 100-YR | 4108.00 | 6761.71 | 6771.18 | | 6772.06 | 0.011089 | 5.43 | 640.82 | 117.96 | 0.38 |
| Kettle Creek | 15906.34 | 2-YR | 1162.10 | 6753.98 | 6761.81 | 6760.00 | 6762.22 | 0.016165 | 4.96 | 228.66 | 65.69 | 0.41 |



HEC-RAS Plan: Future River: Kettle Creek Reach: Kettle Creek (Continued)

| Reach | River Sta | Profile | Q Total | Min Ch El | W.S. Elev | Crit W.S. | E.G. Elev | E.G. Slope | Vel Chnl | Flow Area | Top Width | Froude # Chl |
|--------------|-----------|---------|---------|-----------|-----------|-----------|-----------|------------|----------|-----------|-----------|--------------|
| | | | (cfs) | (ft) | (ft) | (ft) | (ft) | (ft/ft) | (ft/s) | (sq ft) | (ft) | |
| Kettle Creek | 15906.34 | 5-YR | 1768.50 | 6753.98 | 6762.59 | 6760.95 | 6763.23 | 0.018583 | 5.91 | 283.83 | 76.21 | 0.45 |
| Kettle Creek | 15906.34 | 10-YR | 2332.00 | 6753.98 | 6763.19 | 6761.62 | 6764.04 | 0.019388 | 6.48 | 332.11 | 84.68 | 0.47 |
| Kettle Creek | 15906.34 | 25-YR | 2813.20 | 6753.98 | 6763.61 | 6762.13 | 6764.63 | 0.020032 | 6.89 | 369.39 | 91.04 | 0.48 |
| Kettle Creek | 15906.34 | 50-YR | 3576.10 | 6753.98 | 6764.21 | 6762.98 | 6765.50 | 0.020185 | 7.35 | 426.16 | 98.89 | 0.49 |
| Kettle Creek | 15906.34 | 100-YR | 4108.00 | 6753.98 | 6764.57 | 6763.57 | 6766.07 | 0.020080 | 7.58 | 462.59 | 102.44 | 0.49 |
| Kettle Creek | 15906 | | Bridge | | | | | | | | | |
| Kettle Creek | 15683.73 | 2-YR | 1162.10 | 6751.41 | 6757.65 | 6757.65 | 6758.97 | 0.062284 | 8.84 | 127.42 | 52.00 | 0.76 |
| Kettle Creek | 15683.73 | 5-YR | 1768.50 | 6751.41 | 6758.47 | 6758.47 | 6760.24 | 0.051052 | 9.02 | 174.61 | 62.77 | 0.71 |
| Kettle Creek | 15683.73 | 10-YR | 2332.00 | 6751.41 | 6759.40 | 6759.40 | 6761.23 | 0.031305 | 7.92 | 238.38 | 74.49 | 0.57 |
| Kettle Creek | 15683.73 | 25-YR | 2813.20 | 6751.41 | 6760.00 | 6760.00 | 6761.92 | 0.025215 | 7.58 | 285.62 | 82.60 | 0.52 |
| Kettle Creek | 15683.73 | 50-YR | 3576.10 | 6751.41 | 6760.95 | 6760.95 | 6762.84 | 0.017924 | 7.00 | 372.29 | 100.95 | 0.45 |
| Kettle Creek | 15683.73 | 100-YR | 4108.00 | 6751.41 | 6761.39 | 6761.39 | 6763.36 | 0.016342 | 6.94 | 417.81 | 106.24 | 0.44 |
| Kettle Creek | 15530.88 | 2-YR | 1162.10 | 6749.40 | 6754.41 | | 6754.52 | 0.005714 | 2.70 | 430.31 | 118.62 | 0.25 |
| Kettle Creek | 15530.88 | 5-YR | 1768.50 | 6749.40 | 6755.34 | | 6755.50 | 0.006164 | 3.25 | 543.79 | 125.81 | 0.26 |
| Kettle Creek | 15530.88 | 10-YR | 2332.00 | 6749.40 | 6756.06 | | 6756.27 | 0.006382 | 3.64 | 636.51 | 130.42 | 0.28 |
| Kettle Creek | 15530.88 | 25-YR | 2813.20 | 6749.40 | 6756.61 | | 6756.86 | 0.006514 | 3.92 | 710.09 | 136.44 | 0.28 |
| Kettle Creek | 15530.88 | 50-YR | 3576.10 | 6749.40 | 6757.38 | | 6757.68 | 0.006649 | 4.29 | 817.28 | 144.28 | 0.29 |
| Kettle Creek | 15530.88 | 100-YR | 4108.00 | 6749.40 | 6757.85 | | 6758.20 | 0.006684 | 4.51 | 887.48 | 148.78 | 0.30 |
| Kettle Creek | 14906.12 | 2-YR | 1162.10 | 6742.04 | 6748.26 | | 6748.78 | 0.017584 | 5.45 | 203.29 | 73.80 | 0.44 |
| Kettle Creek | 14906.12 | 5-YR | 1768.50 | 6742.04 | 6749.15 | | 6749.87 | 0.015056 | 5.65 | 274.74 | 86.04 | 0.42 |
| Kettle Creek | 14906.12 | 10-YR | 2332.00 | 6742.04 | 6749.78 | | 6750.66 | 0.014256 | 5.89 | 331.66 | 95.99 | 0.41 |
| Kettle Creek | 14906.12 | 25-YR | 2813.20 | 6742.04 | 6750.22 | | 6751.24 | 0.013937 | 6.09 | 374.89 | 102.48 | 0.41 |
| Kettle Creek | 14906.12 | 50-YR | 3576.10 | 6742.04 | 6750.78 | | 6752.06 | 0.013629 | 6.35 | 434.46 | 107.98 | 0.41 |
| Kettle Creek | 14906.12 | 100-YR | 4108.00 | 6742.04 | 6751.13 | | 6752.58 | 0.013506 | 6.52 | 472.21 | 110.73 | 0.41 |
| Kettle Creek | 14354.72 | 2-YR | 1162.10 | 6734.36 | 6742.31 | | 6742.51 | 0.007755 | 3.64 | 318.40 | 80.32 | 0.29 |
| Kettle Creek | 14354.72 | 5-YR | 1768.50 | 6734.36 | 6743.25 | | 6743.56 | 0.008711 | 4.34 | 397.64 | 88.72 | 0.32 |
| Kettle Creek | 14354.72 | 10-YR | 2332.00 | 6734.36 | 6744.00 | | 6744.41 | 0.008891 | 4.77 | 467.43 | 95.39 | 0.33 |
| Kettle Creek | 14354.72 | 25-YR | 2813.20 | 6734.36 | 6744.60 | | 6745.08 | 0.008780 | 5.02 | 525.99 | 101.14 | 0.33 |
| Kettle Creek | 14354.72 | 50-YR | 3576.10 | 6734.36 | 6745.44 | | 6746.02 | 0.008495 | 5.33 | 614.46 | 109.34 | 0.33 |
| Kettle Creek | 14354.72 | 100-YR | 4108.00 | 6734.36 | 6745.96 | | 6746.62 | 0.008289 | 5.49 | 673.11 | 114.34 | 0.33 |
| Kettle Creek | 13757,33 | 2-YR | 1162.10 | 6727.92 | 6734.01 | 6733.16 | 6734.65 | 0.026612 | 6.18 | 182.11 | 69.92 | 0.51 |
| Kettle Creek | 13757.33 | 5-YR | 1768.50 | 6727.92 | 6734.91 | 6734.01 | 6735.82 | 0.020840 | 6.18 | 248.74 | 77.07 | 0.47 |
| Kettle Creek | 13757.33 | 10-YR | 2332.00 | 6727.92 | 6735.49 | 6734.51 | 6736.69 | 0.020009 | 6.48 | 294.78 | 81.64 | 0.47 |



HEC-RAS Plan: Future River: Kettle Creek Reach: Kettle Creek (Continued)

| Reach | River Sta | Profile | Q Total | Min Ch El | W.S. Elev | Crit W.S. | E.G. Elev | E.G. Slope | Vel Chnl | Flow Area | Top Width | Froude # Chl |
|--------------|-----------|---------|---------|-----------|-----------|-----------|-----------|------------|----------|-----------|-----------|--------------|
| | | | (cfs) | (ft) | (ft) | (ft) | (ft) | (ft/ft) | (ft/s) | (sq ft) | (ft) | |
| Kettle Creek | 13757,33 | 25-YR | 2813.20 | 6727.92 | 6735.88 | 6735.07 | 6737.34 | 0.020406 | 6.82 | 326.61 | 84.68 | 0.48 |
| Kettle Creek | 13757.33 | 50-YR | 3576.10 | 6727.92 | 6736.39 | 6735.98 | 6738.27 | 0.021336 | 7.34 | 370.62 | 88.66 | 0.49 |
| Kettle Creek | 13757.33 | 100-YR | 4108.00 | 6727.92 | 6736.70 | 6736.51 | 6738.88 | 0.021941 | 7.67 | 398.71 | 91.11 | 0.50 |
| Kettle Creek | 12367.83 | 2-YR | 1162.10 | 6708.58 | 6713.98 | | 6714.21 | 0.009228 | 3.77 | 306.07 | 76.03 | 0.3 |
| Kettle Creek | 12367.83 | 5-YR | 1768.50 | 6708.58 | 6714.89 | | 6715.24 | 0.010921 | 4.63 | 376.48 | 78.55 | 0.35 |
| Kettle Creek | 12367.83 | 10-YR | 2332.00 | 6708.58 | 6715.71 | | 6716.16 | 0.011163 | 5.15 | 441.88 | 81.26 | 0.37 |
| Kettle Creek | 12367.83 | 25-YR | 2813.20 | 6708.58 | 6716.42 | | 6716.93 | 0.010844 | 5.46 | 500.93 | 86.58 | 0.37 |
| Kettle Creek | 12367.83 | 50-YR | 3576.10 | 6708.58 | 6717.40 | | 6718.01 | 0.010303 | 5.82 | 591.62 | 96.32 | 0.37 |
| Kettle Creek | 12367.83 | 100-YR | 4108.00 | 6708.58 | 6717.99 | | 6718.66 | 0.010011 | 6.02 | 648.70 | 99.45 | 0.36 |
| Kettle Creek | 11267.11 | 2-YR | 1162.10 | 6695.53 | 6702.99 | | 6703.50 | 0.010289 | 4.31 | 225.73 | 68.68 | 0.34 |
| Kettle Creek | 11267.11 | 5-YR | 1768.50 | 6695.53 | 6704.09 | | 6704.80 | 0.008310 | 4.41 | 305.72 | 76.74 | 0.3 |
| Kettle Creek | 11267.11 | 10-YR | 2332.00 | 6695.53 | 6704.81 | | 6705.72 | 0.008140 | 4.69 | 363.12 | 83.07 | 0.3 |
| Kettle Creek | 11267.11 | 25-YR | 2813.20 | 6695.53 | 6705.26 | | 6706.35 | 0.008537 | 5.01 | 401.75 | 87.53 | 0.32 |
| Kettle Creek | 11267.11 | 50-YR | 3576.10 | 6695.53 | 6705.85 | | 6707.23 | 0.009219 | 5.48 | 455.63 | 93.46 | 0.34 |
| Kettle Creek | 11267.11 | 100-YR | 4108.00 | 6695.53 | 6706.22 | | 6707.78 | 0.009624 | 5.77 | 489.95 | 96.39 | 0.35 |
| Kettle Creek | 10087.38 | 2-YR | 1157.20 | 6680.77 | 6687.99 | | 6688.18 | 0.002147 | 2.40 | 373.99 | 89.12 | 0.17 |
| Kettle Creek | 10087.38 | 5-YR | 1762.50 | 6680.77 | 6689.13 | | 6689.42 | 0.002103 | 2.64 | 477.70 | 92.08 | 0.17 |
| Kettle Creek | 10087.38 | 10-YR | 2325.70 | 6680.77 | 6690.10 | 6686.62 | 6690.46 | 0.002009 | 2.79 | 567.65 | 94.62 | 0.17 |
| Kettle Creek | 10087.38 | 25-YR | 2807.30 | 6680.77 | 6690.91 | 6687.15 | 6691.32 | 0.001883 | 2.87 | 645.74 | 96.92 | 0.16 |
| Kettle Creek | 10087.38 | 50-YR | 3571.30 | 6680.77 | 6692.13 | 6687.76 | 6692.60 | 0.001714 | 2.97 | 765.78 | 100.40 | 0.16 |
| Kettle Creek | 10087.38 | 100-YR | 4104.30 | 6680.77 | 6692.93 | 6688.12 | 6693.44 | 0.001621 | 3.03 | 846.59 | 102.65 | 0.16 |
| Kettle Creek | 9732.32 | 2-YR | 1157.20 | 6676.00 | 6681.18 | | 6681.79 | 0.036988 | 6.25 | 185.55 | 61.02 | 0.6 |
| Kettle Creek | 9732.32 | 5-YR | 1762.50 | 6676.00 | 6681.53 | | 6682.65 | 0.060140 | 8.52 | 207.94 | 66.89 | 0.79 |
| Kettle Creek | 9732.32 | 10-YR | 2325.70 | 6676.00 | 6681.84 | 6681.84 | 6683.44 | 0.077089 | 10.19 | 229.33 | 70.83 | 0.90 |
| Kettle Creek | 9732.32 | 25-YR | 2807.30 | 6676.00 | 6682.26 | 6682.26 | 6684.08 | 0.075478 | 10.77 | 259.55 | 74.53 | 0.9 |
| Kettle Creek | 9732.32 | 50-YR | 3571.30 | 6676.00 | 6682.83 | 6682.83 | 6685.03 | 0.072678 | 11.48 | 303.45 | 78.25 | 0.9 |
| Kettle Creek | 9732.32 | 100-YR | 4104.30 | 6676.00 | 6683.23 | 6683.23 | 6685.67 | 0.068874 | 11.76 | 334.86 | 80.79 | 0.90 |
| Kettle Creek | 8444.97 | 2-YR | 1212.60 | 6660.69 | 6666.73 | | 6666.99 | 0.005652 | 3.26 | 322.23 | 103.71 | 0.25 |
| Kettle Creek | 8444.97 | 5-YR | 1839.30 | 6660.69 | 6667.75 | | 6668.11 | 0.004677 | 3.34 | 431.54 | 112.58 | 0.24 |
| Kettle Creek | 8444.97 | 10-YR | 2420.50 | 6660.69 | 6668.59 | | 6669.02 | 0.004022 | 3.38 | 529.84 | 120.74 | 0.23 |
| Kettle Creek | 8444.97 | 25-YR | 2917.30 | 6660.69 | 6669.21 | | 6669.69 | 0.003708 | 3.43 | 606.06 | 126.24 | 0.22 |
| Kettle Creek | 8444.97 | 50-YR | 3703.70 | 6660.69 | 6670.13 | | 6670.67 | 0.003271 | 3.48 | 725.82 | 134.19 | 0.21 |
| Kettle Creek | 8444.97 | 100-YR | 4252.40 | 6660.69 | 6670.65 | | 6671.25 | 0.003153 | 3.55 | 796.20 | 137.79 | 0.2 |



HEC-RAS Plan: Future River: Kettle Creek Reach: Kettle Creek (Continued)

| Reach | River Sta | Profile | Q Total | Min Ch El | W.S. Elev | Crit W.S. | E.G. Elev | E.G. Slope | Vel Chnl | Flow Area | Top Width | Froude # Chl |
|--------------|-----------|---------|---------|-----------|-----------|-----------|-----------|------------|----------|-----------|-----------|--------------|
| | | | (cfs) | (ft) | (ft) | (ft) | (ft) | (ft/ft) | (ft/s) | (sq ft) | (ft) | |
| Kettle Creek | 8350 | 2-YR | 1212.60 | 6660.00 | 6666.34 | | 6666.59 | 0.003197 | 2.72 | 359.77 | 98.32 | 0.20 |
| Kettle Creek | 8350 | 5-YR | 1839.30 | 6660.00 | 6667.42 | | 6667.75 | 0.003009 | 2.95 | 470.25 | 107.11 | 0.20 |
| Kettle Creek | 8350 | 10-YR | 2420.50 | 6660.00 | 6668.29 | | 6668.69 | 0.002973 | 3.17 | 568.40 | 125.14 | 0.20 |
| Kettle Creek | 8350 | 25-YR | 2917.30 | 6660.00 | 6668.95 | | 6669.37 | 0.002784 | 3.24 | 654.62 | 135.05 | 0.20 |
| Kettle Creek | 8350 | 50-YR | 3703.70 | 6660.00 | 6669.92 | | 6670.38 | 0.002461 | 3.27 | 793.46 | 148.64 | 0.19 |
| Kettle Creek | 8350 | 100-YR | 4252.40 | 6660.00 | 6670.47 | | 6670.96 | 0.002371 | 3.33 | 876.15 | 155.16 | 0.19 |
| Kettle Creek | 8251.39 | 2-YR | 1212.60 | 6660.00 | 6665.61 | 6663.66 | 6665.99 | 0.010287 | 4.18 | 262.21 | 73.53 | 0.34 |
| Kettle Creek | 8251.39 | 5-YR | 1839.30 | 6660.00 | 6666.58 | 6664.52 | 6667.14 | 0.010163 | 4.72 | 337.74 | 81.58 | 0.35 |
| Kettle Creek | 8251.39 | 10-YR | 2420.50 | 6660.00 | 6667.37 | 6665.25 | 6668.06 | 0.009665 | 5.02 | 404.33 | 87.96 | 0.35 |
| Kettle Creek | 8251.39 | 25-YR | 2917.30 | 6660.00 | 6667.93 | 6665.79 | 6668.75 | 0.009410 | 5.24 | 455.44 | 92.02 | 0.35 |
| Kettle Creek | 8251.39 | 50-YR | 3703.70 | 6660.00 | 6668.93 | 6666.56 | 6669.80 | 0.008802 | 5.54 | 559.90 | 124.18 | 0.35 |
| Kettle Creek | 8251.39 | 100-YR | 4252.40 | 6660.00 | 6669.52 | 6667.09 | 6670.41 | 0.007862 | 5.49 | 636.19 | 136.64 | 0.33 |
| Kettle Creek | 8251 | | Bridge | | | | | | | | | |
| Kettle Creek | 8060.94 | 2-YR | 1212.60 | 6653.57 | 6658.77 | 6658.25 | 6659.84 | 0.014912 | 5.24 | 169.73 | 50.19 | 0.42 |
| Kettle Creek | 8060.94 | 5-YR | 1839.30 | 6653.57 | 6659.62 | 6659.37 | 6661.12 | 0.016483 | 6.13 | 215.06 | 56.94 | 0.45 |
| Kettle Creek | 8060.94 | 10-YR | 2420.50 | 6653.57 | 6660.24 | 6660.11 | 6662.11 | 0.017474 | 6.75 | 251.86 | 61.77 | 0.47 |
| Kettle Creek | 8060.94 | 25-YR | 2917.30 | 6653.57 | 6660.89 | 6660.89 | 6662.80 | 0.016738 | 7.05 | 295.27 | 72.14 | 0.47 |
| Kettle Creek | 8060.94 | 50-YR | 3703.70 | 6653.57 | 6661.73 | 6661.73 | 6663.75 | 0.015425 | 7.30 | 361.45 | 98.48 | 0.46 |
| Kettle Creek | 8060.94 | 100-YR | 4252.40 | 6653.57 | 6662.64 | 6662.64 | 6664.23 | 0.011479 | 6.77 | 470.96 | 130.17 | 0.40 |
| Kettle Creek | 7863.13 | 2-YR | 1212.60 | 6649.24 | 6652.92 | 6652.79 | 6654.22 | 0.066748 | 8.28 | 138.55 | 52.40 | 0.82 |
| Kettle Creek | 7863.13 | 5-YR | 1839.30 | 6649.24 | 6653.85 | 6653.74 | 6655.57 | 0.053024 | 8.75 | 189.91 | 57.65 | 0.76 |
| Kettle Creek | 7863.13 | 10-YR | 2420.50 | 6649.24 | 6654.56 | 6654.56 | 6656.62 | 0.046704 | 9.14 | 232.52 | 62.08 | 0.73 |
| Kettle Creek | 7863.13 | 25-YR | 2917.30 | 6649.24 | 6655.23 | 6655.23 | 6657.41 | 0.038665 | 9.06 | 275.46 | 66.44 | 0.68 |
| Kettle Creek | 7863.13 | 50-YR | 3703.70 | 6649.24 | 6656.02 | 6656.02 | 6658.46 | 0.034771 | 9.40 | 330.34 | 72.99 | 0.66 |
| Kettle Creek | 7863.13 | 100-YR | 4252.40 | 6649.24 | 6656.55 | 6656.55 | 6659.16 | 0.031597 | 9.45 | 369.45 | 76.47 | 0.64 |
| Kettle Creek | 7632.03 | 2-YR | 1212.60 | 6641.32 | 6649.12 | | 6649.40 | 0.009234 | 4.18 | 288.04 | 62.95 | 0.32 |
| Kettle Creek | 7632.03 | 5-YR | 1839.30 | 6641.32 | 6650.21 | | 6650.63 | 0.010320 | 5.02 | 359.61 | 68.84 | 0.35 |
| Kettle Creek | 7632.03 | 10-YR | 2420.50 | 6641.32 | 6651.01 | | 6651.55 | 0.011123 | 5.65 | 416.60 | 74.61 | 0.37 |
| Kettle Creek | 7632.03 | 25-YR | 2917.30 | 6641.32 | 6651.54 | | 6652.20 | 0.011931 | 6.14 | 457.56 | 78.59 | 0.39 |
| Kettle Creek | 7632.03 | 50-YR | 3703.70 | 6641.32 | 6652.21 | | 6653.07 | 0.013350 | 6.87 | 511.87 | 83.46 | 0.42 |
| Kettle Creek | 7632.03 | 100-YR | 4252.40 | 6641.32 | 6652.60 | | 6653.61 | 0.014318 | 7.34 | 544.75 | 85.73 | 0.44 |
| Kettle Creek | 6688.3 | 2-YR | 1218.70 | 6629.79 | 6635.78 | | 6636.10 | 0.024002 | 4.51 | 269.96 | 96.75 | 0.48 |
| Kettle Creek | 6688.3 | 5-YR | 1845.30 | 6629.79 | 6636.87 | | 6637.22 | 0.020600 | 4.80 | 384.72 | 113.89 | 0.46 |



HEC-RAS Plan: Future River: Kettle Creek Reach: Kettle Creek (Continued)

| Reach | River Sta | Profile | Q Total | Min Ch El | W.S. Elev | Crit W.S. | E.G. Elev | E.G. Slope | Vel Chnl | Flow Area | Top Width | Froude # Chl |
|---|-----------|---------|---------|-----------|-----------|-----------|-----------|------------|----------|-----------|-----------|--------------|
| | | | (cfs) | (ft) | (ft) | (ft) | (ft) | (ft/ft) | (ft/s) | (sq ft) | (ft) | |
| Kettle Creek | 6688.3 | 10-YR | 2426.00 | 6629.79 | 6637.70 | | 6638.09 | 0.018731 | 5.00 | 484.45 | 126.63 | 0.45 |
| Kettle Creek | 6688.3 | 25-YR | 2920.90 | 6629.79 | 6638.30 | | 6638.72 | 0.017171 | 5.17 | 563.61 | 135.32 | 0.44 |
| Kettle Creek | 6688.3 | 50-YR | 3704.50 | 6629.79 | 6639.13 | | 6639.59 | 0.014998 | 5.43 | 680.47 | 146.23 | 0.42 |
| Kettle Creek | 6688.3 | 100-YR | 4250.10 | 6629.79 | 6639.66 | | 6640.15 | 0.013840 | 5.56 | 759.57 | 153.27 | 0.41 |
| Kettle Creek | 6433.61 | 2-YR | 1218.70 | 6627.42 | 6633.50 | | 6633.63 | 0.005028 | 2.92 | 417.66 | 98.42 | 0.24 |
| Kettle Creek | 6433.61 | 5-YR | 1845.30 | 6627.42 | 6634.61 | | 6634.80 | 0.005265 | 3.45 | 529.85 | 103.80 | 0.25 |
| Kettle Creek | 6433.61 | 10-YR | 2426.00 | 6627.42 | 6635.46 | | 6635.71 | 0.005386 | 3.82 | 620.92 | 108.75 | 0.26 |
| Kettle Creek | 6433.61 | 25-YR | 2920.90 | 6627.42 | 6636.11 | | 6636.40 | 0.005444 | 4.09 | 692.70 | 113.10 | 0.27 |
| Kettle Creek | 6433.61 | 50-YR | 3704.50 | 6627.42 | 6637.03 | | 6637.38 | 0.005470 | 4.44 | 799.75 | 120.54 | 0.27 |
| Kettle Creek | 6433.61 | 100-YR | 4250.10 | 6627.42 | 6637.61 | | 6638.01 | 0.005426 | 4.63 | 871.92 | 125.59 | 0.28 |
| Kettle Creek | 6305.69 | 2-YR | 1218.70 | 6625.87 | 6631.47 | | 6631.66 | 0.009936 | 3.47 | 351.31 | 99.32 | 0.32 |
| Kettle Creek | 6305.69 | 5-YR | 1845.30 | 6625.87 | 6632.70 | | 6632.92 | 0.008284 | 3.84 | 480.43 | 111.76 | 0.31 |
| Kettle Creek | 6305.69 | 10-YR | 2426.00 | 6625.87 | 6633.65 | | 6633.91 | 0.007272 | 4.06 | 591.85 | 121.19 | 0.30 |
| Kettle Creek | 6305.69 | 25-YR | 2920.90 | 6625.87 | 6634.38 | | 6634.67 | 0.006612 | 4.19 | 683.20 | 129.62 | 0.29 |
| Kettle Creek | 6305.69 | 50-YR | 3704.50 | 6625.87 | 6635.42 | | 6635.74 | 0.005771 | 4.31 | 824.99 | 143.90 | 0.28 |
| Kettle Creek | 6305.69 | 100-YR | 4250.10 | 6625.87 | 6636.09 | | 6636.44 | 0.005302 | 4.37 | 925.02 | 160.54 | 0.27 |
| Kettle Creek | 6147.73 | 2-YR | 1218.70 | 6623.99 | 6630.68 | | 6630.84 | 0.003134 | 2.42 | 448.35 | 103.51 | 0.19 |
| Kettle Creek | 6147.73 | 5-YR | 1845.30 | 6623.99 | 6631.99 | | 6632.20 | 0.002890 | 2.71 | 586.91 | 109.72 | 0.19 |
| Kettle Creek | 6147.73 | 10-YR | 2426.00 | 6623.99 | 6632.98 | | 6633.24 | 0.002775 | 2.93 | 698.44 | 114.31 | 0.19 |
| Kettle Creek | 6147.73 | 25-YR | 2920.90 | 6623.99 | 6633.73 | | 6634.03 | 0.002720 | 3.09 | 784.87 | 117.87 | 0.19 |
| Kettle Creek | 6147.73 | 50-YR | 3704.50 | 6623.99 | 6634.77 | | 6635.14 | 0.002658 | 3.32 | 911.12 | 122.83 | 0.19 |
| Kettle Creek | 6147.73 | 100-YR | 4250.10 | 6623.99 | 6635.46 | | 6635.86 | 0.002605 | 3.45 | 996.03 | 126.29 | 0.19 |
| Kettle Creek | 6032.86 | 2-YR | 1218.70 | 6622.67 | 6628.53 | 6625.86 | 6628.74 | 0.003565 | 2.58 | 393.28 | 97.75 | 0.20 |
| Kettle Creek | 6032.86 | 5-YR | 1845.30 | 6622.67 | 6629.63 | 6626.38 | 6629.93 | 0.003531 | 2.93 | 503.31 | 104.00 | 0.21 |
| Kettle Creek | 6032.86 | 10-YR | 2426.00 | 6622.67 | 6630.52 | 6626.97 | 6630.89 | 0.003392 | 3.15 | 598.39 | 108.45 | 0.21 |
| Kettle Creek | 6032.86 | 25-YR | 2920.90 | 6622.67 | 6631.18 | 6627.51 | 6631.61 | 0.003345 | 3.32 | 670.54 | 111.44 | 0.21 |
| Kettle Creek | 6032.86 | 50-YR | 3704.50 | 6622.67 | 6632.14 | 6628.24 | 6632.65 | 0.003261 | 3.55 | 780.34 | 116.68 | 0.21 |
| Kettle Creek | 6032.86 | 100-YR | 4250.10 | 6622.67 | 6632.83 | 6628.74 | 6633.40 | 0.003047 | 3.61 | 862.28 | 118.83 | 0.21 |
| Kettle Creek | 6000 | | Bridge | | | | | | | | | |
| Kettle Creek | 5983.2 | 2-YR | 1218.70 | 6622.04 | 6628.35 | | 6628.51 | 0.001911 | 2.00 | 443.10 | 119.02 | 0.15 |
| Kettle Creek | 5983.2 | 5-YR | 1845.30 | 6622.04 | 6629.41 | | 6629.64 | 0.001911 | 2.18 | 572.01 | 124.02 | 0.15 |
| Kettle Creek | 5983.2 | 10-YR | 2426.00 | 6622.04 | 6630.29 | | 6630.57 | 0.001781 | 2.10 | 684.48 | 131.35 | 0.15 |
| CONTRACTOR OF THE PARTY OF THE | 5983.2 | 25-YR | | | | | | | 2.32 | | | |
| Kettle Creek | 0900.2 | 20-1 PC | 2920.90 | 6622.04 | 6630.93 | | 6631.25 | 0.001650 | 2.41 | 768.79 | 133.29 | 0.15 |



HEC-RAS Plan: Future River: Kettle Creek Reach: Kettle Creek (Continued)

| Reach | River Sta | Profile | Q Total | Min Ch El | W.S. Elev | Crit W.S. | E.G. Elev | E.G. Slope | Vel Chni | Flow Area | Top Width | Froude # Chl |
|--------------|-----------|---------|---------|-----------|-----------|-----------|-----------|------------|----------|-----------|-----------|--------------|
| | | | (cfs) | (ft) | (ft) | (ft) | (ft) | (ft/ft) | (ft/s) | (sq ft) | (ft) | |
| Kettle Creek | 5983.2 | 50-YR | 3704.50 | 6622.04 | 6631.86 | | 6632.24 | 0.001580 | 2.54 | 893.71 | 136.21 | 0.15 |
| Kettle Creek | 5983.2 | 100-YR | 4250.10 | 6622.04 | 6632.56 | | 6632.96 | 0.001608 | 2.69 | 993.52 | 149.95 | 0.15 |
| Kettle Creek | 5846.46 | 2-YR | 1218.70 | 6620.39 | 6624.45 | | 6625.18 | 0.053734 | 6.86 | 177.92 | 65.73 | 0.72 |
| Kettle Creek | 5846.46 | 5-YR | 1845.30 | 6620.39 | 6625.37 | | 6626.28 | 0.045954 | 7.64 | 241.02 | 72.17 | 0.69 |
| Kettle Creek | 5846.46 | 10-YR | 2426.00 | 6620.39 | 6626.08 | | 6627.15 | 0.041223 | 8.13 | 294.40 | 77.01 | 0.68 |
| Kettle Creek | 5846.46 | 25-YR | 2920.90 | 6620.39 | 6626.63 | | 6627.81 | 0.038242 | 8.45 | 337.82 | 82.20 | 0.67 |
| Kettle Creek | 5846.46 | 50-YR | 3704.50 | 6620.39 | 6627.38 | | 6628.76 | 0.034749 | 8.84 | 402.26 | 89.22 | 0.65 |
| Kettle Creek | 5846.46 | 100-YR | 4250.10 | 6620.39 | 6627.88 | | 6629.37 | 0.032056 | 8.98 | 448.18 | 93.90 | 0.63 |
| Kettle Creek | 5366.46 | 2-YR | 1218.70 | 6612.16 | 6619.34 | 6616.52 | 6619.50 | 0.004844 | 2.90 | 399.43 | 96.85 | 0.23 |
| Kettle Creek | 5366.46 | 5-YR | 1845.30 | 6612.16 | 6620.41 | 6617.23 | 6620.65 | 0.004999 | 3.37 | 504.47 | 100.90 | 0.25 |
| Kettle Creek | 5366.46 | 10-YR | 2426.00 | 6612.16 | 6621.22 | 6617.77 | 6621.54 | 0.005132 | 3.73 | 587.88 | 104.19 | 0.26 |
| Kettle Creek | 5366.46 | 25-YR | 2920.90 | 6612.16 | 6621.83 | 6618.11 | 6622.22 | 0.005231 | 3.99 | 651.73 | 106.37 | 0.26 |
| Kettle Creek | 5366.46 | 50-YR | 3704.50 | 6612.16 | 6622.71 | 6618.64 | 6623.19 | 0.005346 | 4.36 | 747.43 | 111.08 | 0.27 |
| Kettle Creek | 5366.46 | 100-YR | 4250.10 | 6612.16 | 6623.18 | 6618.97 | 6623.74 | 0.005604 | 4.63 | 799.91 | 113.30 | 0.28 |
| Kettle Creek | 3636.65 | 2-YR | 1218.70 | 6592.57 | 6595.31 | 6595.31 | 6596.22 | 0.120579 | 7.65 | 159.21 | 87.62 | 1.00 |
| Kettle Creek | 3636.65 | 5-YR | 1845.30 | 6592.57 | 6595.90 | 6595.90 | 6597.08 | 0.111442 | 8.74 | 211.31 | 90.94 | 1.00 |
| Kettle Creek | 3636.65 | 10-YR | 2426.00 | 6592.57 | 6596.38 | 6596.38 | 6597.78 | 0.103264 | 9.47 | 256.17 | 93.04 | 0.99 |
| Kettle Creek | 3636.65 | 25-YR | 2920.90 | 6592.57 | 6596.76 | 6596.76 | 6598.32 | 0.098063 | 9.99 | 291.89 | 94.55 | 0.99 |
| Kettle Creek | 3636.65 | 50-YR | 3704.50 | 6592.57 | 6597.29 | 6597.29 | 6599.12 | 0.092906 | 10.78 | 342.49 | 96.63 | 0.99 |
| Kettle Creek | 3636.65 | 100-YR | 4250.10 | 6592.57 | 6597.81 | 6597.65 | 6599.64 | 0.077689 | 10.75 | 392.87 | 98.85 | 0.92 |
| Kettle Creek | 3115.71 | 2-YR | 1218.70 | 6585.47 | 6593.11 | | 6593.16 | 0.000588 | 1.22 | 821.09 | 161.99 | 0.09 |
| Kettle Creek | 3115.71 | 5-YR | 1845.30 | 6585.47 | 6594.42 | | 6594.49 | 0.000612 | 1.42 | 1041.29 | 175.28 | 0.09 |
| Kettle Creek | 3115.71 | 10-YR | 2426.00 | 6585.47 | 6595.43 | | 6595.51 | 0.000629 | 1.56 | 1223.68 | 188.39 | 0.09 |
| Kettle Creek | 3115.71 | 25-YR | 2920.90 | 6585.47 | 6596.17 | | 6596.27 | 0.000629 | 1.65 | 1366.27 | 195.03 | 0.10 |
| Kettle Creek | 3115.71 | 50-YR | 3704.50 | 6585.47 | 6597.23 | | 6597.35 | 0.000631 | 1.78 | 1578.29 | 206.86 | 0.10 |
| Kettle Creek | 3115.71 | 100-YR | 4250.10 | 6585.47 | 6597.87 | | 6598.01 | 0.000642 | 1.86 | 1715.04 | 216.47 | 0.10 |
| Kettle Creek | 2957.59 | 2-YR | 1218.70 | 6582.74 | 6592.49 | 6589.37 | 6592.84 | 0.003655 | 3.76 | 266.46 | 71.30 | 0.22 |
| Kettle Creek | 2957.59 | 5-YR | 1845.30 | 6582.74 | 6593.67 | 6591.33 | 6594.14 | 0.003299 | 3.88 | 355.77 | 79.52 | 0.21 |
| Kettle Creek | 2957.59 | 10-YR | 2426.00 | 6582.74 | 6594.57 | 6591.98 | 6595.13 | 0.003125 | 3.99 | 429.68 | 85.44 | 0.21 |
| Kettle Creek | 2957.59 | 25-YR | 2920.90 | 6582.74 | 6595.24 | 6592.53 | 6595.88 | 0.003016 | 4.08 | 488.52 | 89.64 | 0.21 |
| Kettle Creek | 2957.59 | 50-YR | 3704.50 | 6582.74 | 6596.20 | 6593.26 | 6596.93 | 0.002895 | 4.21 | 577.09 | 96.10 | 0.21 |
| Kettle Creek | 2957.59 | 100-YR | 4250.10 | 6582.74 | 6596.77 | 6593.76 | 6597.57 | 0.002863 | 4.31 | 632.88 | 99.70 | 0.21 |
| Kettle Creek | 2850 | | Bridge | | | | | | | | | |



HEC-RAS Plan: Future River: Kettle Creek Reach: Kettle Creek (Continued)

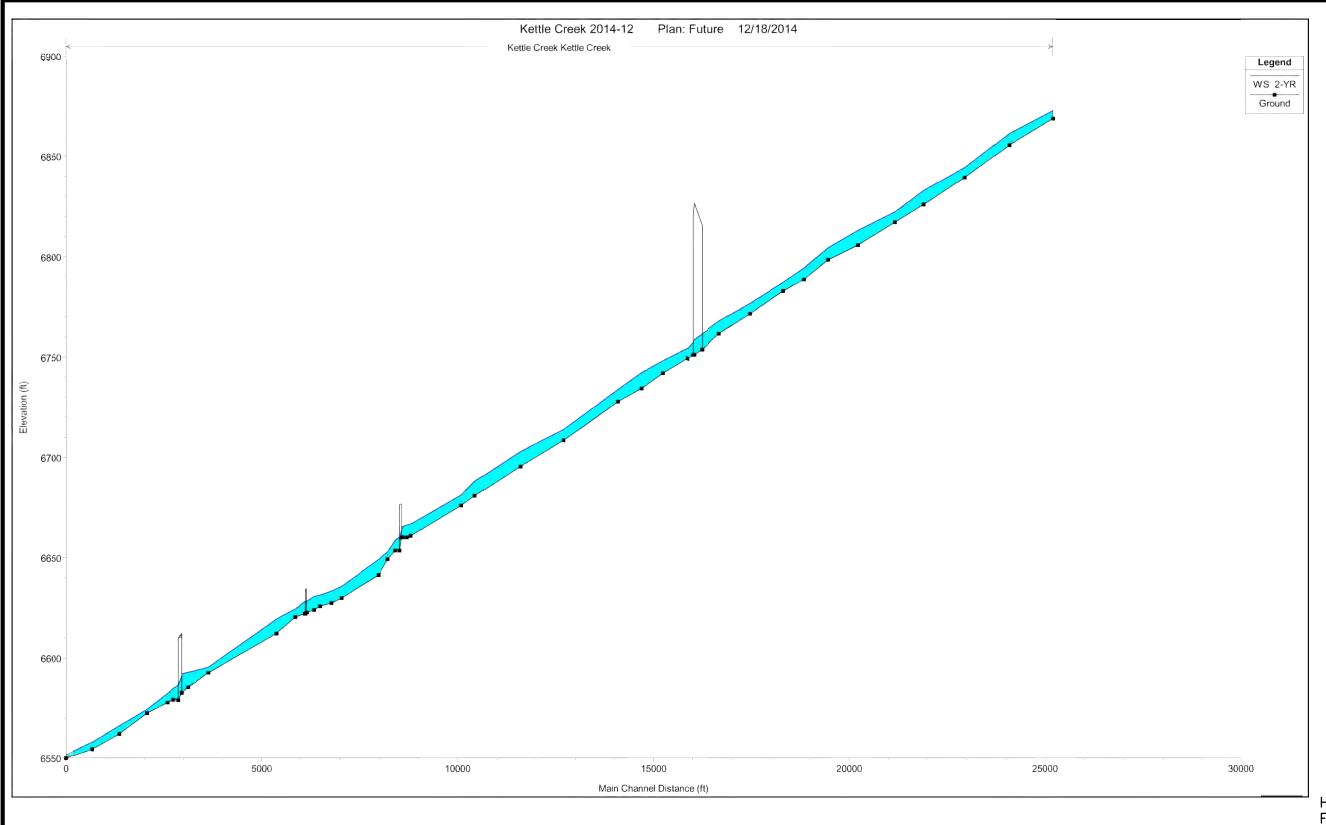
| Reach | River Sta | Profile | Q Total | Min Ch El | W.S. Elev | Crit W.S. | E.G. Elev | E.G. Slope | Vel Chnl | Flow Area | Top Width | Froude # Chl |
|--------------|-----------|---------|---------|-----------|-----------|-----------|-----------|------------|----------|-----------|-----------|--------------|
| | | | (cfs) | (ft) | (ft) | (ft) | (ft) | (ft/ft) | (ft/s) | (sq ft) | (ft) | |
| Kettle Creek | 2731.34 | 2-YR | 1218.70 | 6579.12 | 6585.00 | | 6585.83 | 0.017732 | 5.83 | 179.87 | 52.77 | 0.45 |
| Kettle Creek | 2731.34 | 5-YR | 1845.30 | 6579.12 | 6585.63 | 6584.91 | 6587.02 | 0.022646 | 7.11 | 214.56 | 57.32 | 0.52 |
| Kettle Creek | 2731.34 | 10-YR | 2426.00 | 6579.12 | 6586.17 | 6585.92 | 6588.02 | 0.024762 | 7.89 | 246.98 | 61.66 | 0.55 |
| Kettle Creek | 2731.34 | 25-YR | 2920.90 | 6579.12 | 6587.13 | 6586.63 | 6588.85 | 0.017437 | 7.27 | 310.17 | 70.38 | 0.47 |
| Kettle Creek | 2731.34 | 50-YR | 3704.50 | 6579.12 | 6587.57 | 6587.57 | 6589.85 | 0.020784 | 8.24 | 341.55 | 74.67 | 0.52 |
| Kettle Creek | 2731.34 | 100-YR | 4250.10 | 6579.12 | 6588.00 | 6588.00 | 6590.49 | 0.020451 | 8.48 | 375.09 | 79.00 | 0.52 |
| Kettle Creek | 2597.25 | 2-YR | 1218.70 | 6577.88 | 6582.50 | 6581.65 | 6582.76 | 0.025529 | 4.01 | 300.70 | 142.24 | 0.47 |
| Kettle Creek | 2597.25 | 5-YR | 1845.30 | 6577.88 | 6583.19 | 6582.10 | 6583.53 | 0.022457 | 4.51 | 400.07 | 146.81 | 0.47 |
| Kettle Creek | 2597.25 | 10-YR | 2426.00 | 6577.88 | 6583.52 | 6582.44 | 6584.01 | 0.026103 | 5.22 | 449.94 | 148.78 | 0.51 |
| Kettle Creek | 2597.25 | 25-YR | 2920.90 | 6577.88 | 6582.70 | 6582.70 | 6583.95 | 0.108552 | 8.76 | 328.96 | 143.56 | 0.99 |
| Kettle Creek | 2597.25 | 50-YR | 3704.50 | 6577.88 | 6584.15 | 6583.13 | 6584.95 | 0.031990 | 6.50 | 544.03 | 152.22 | 0.58 |
| Kettle Creek | 2597.25 | 100-YR | 4250.10 | 6577.88 | 6584.38 | 6583.38 | 6585.33 | 0.034034 | 6.97 | 579.17 | 153.35 | 0.61 |
| Kettle Creek | 2067.56 | 2-YR | 1218.70 | 6572.37 | 6574.22 | 6574.16 | 6574.60 | 0.011145 | 1.49 | 269.36 | 285.99 | 0.27 |
| Kettle Creek | 2067.56 | 5-YR | 1845.30 | 6572.37 | 6574.43 | 6574.43 | 6575.01 | 0.013128 | 1.85 | 329.53 | 287.17 | 0.31 |
| Kettle Creek | 2067.56 | 10-YR | 2426.00 | 6572.37 | 6574.67 | 6574.65 | 6575.35 | 0.012134 | 2.02 | 398.40 | 288.51 | 0.30 |
| Kettle Creek | 2067.56 | 25-YR | 2920.90 | 6572.37 | 6575.36 | | 6575.80 | 0.004652 | 1.64 | 596.93 | 292.33 | 0.20 |
| Kettle Creek | 2067.56 | 50-YR | 3704.50 | 6572.37 | 6575.12 | 6575.12 | 6576.02 | 0.011227 | 2.35 | 527.57 | 291.01 | 0.31 |
| Kettle Creek | 2067.56 | 100-YR | 4250.10 | 6572.37 | 6575.28 | 6575.28 | 6576.29 | 0.011068 | 2.47 | 576.10 | 291.94 | 0.31 |
| Kettle Creek | 1361.33 | 2-YR | 1218.70 | 6562.11 | 6566.13 | | 6566.24 | 0.012843 | 2.71 | 450.19 | 220.02 | 0.33 |
| Kettle Creek | 1361.33 | 5-YR | 1845.30 | 6562.11 | 6567.60 | 6565.30 | 6567.68 | 0.005008 | 2.36 | 781.38 | 230.48 | 0.23 |
| Kettle Creek | 1361.33 | 10-YR | 2426.00 | 6562.11 | 6567.46 | | 6567.62 | 0.009879 | 3.24 | 749.49 | 229.39 | 0.32 |
| Kettle Creek | 1361.33 | 25-YR | 2920.90 | 6562.11 | 6565.81 | 6565.81 | 6566.72 | 0.121868 | 7.63 | 382.64 | 213.66 | 1.01 |
| Kettle Creek | 1361.33 | 50-YR | 3704.50 | 6562.11 | 6569.09 | | 6569.25 | 0.005902 | 3.24 | 1146.70 | 263.74 | 0.26 |
| Kettle Creek | 1361.33 | 100-YR | 4250.10 | 6562.11 | 6573.91 | | 6573.96 | 0.000478 | 1.46 | 2637.29 | 341.57 | 0.08 |
| Kettle Creek | 670.23 | 2-YR | 1218.70 | 6554.40 | 6558.10 | 6556.91 | 6558.27 | 0.010512 | 2.76 | 409.88 | 187.31 | 0.31 |
| Kettle Creek | 670.23 | 5-YR | 1845.30 | 6554.40 | 6557.26 | 6557.26 | 6558.11 | 0.117338 | 6.95 | 257.53 | 175.63 | 0.97 |
| Kettle Creek | 670.23 | 10-YR | 2426.00 | 6554.40 | 6558.82 | | 6559.22 | 0.015452 | 3.97 | 547.04 | 195.49 | 0.39 |
| Kettle Creek | 670.23 | 25-YR | 2920.90 | 6554.40 | 6563.07 | | 6563.17 | 0.000769 | 1.56 | 1453.84 | 227.88 | 0.10 |
| Kettle Creek | 670.23 | 50-YR | 3704.50 | 6554.40 | 6568.99 | | 6569.02 | 0.000090 | 0.79 | 3513.16 | 469.76 | 0.04 |
| Kettle Creek | 670.23 | 100-YR | 4250.10 | 6554.40 | 6573.90 | | 6573.91 | 0.000020 | 0.46 | 5963.43 | 526.34 | 0.02 |
| Kettle Creek | 6.23 | 2-YR | 1218.70 | 6550.00 | 6551.90 | 6550.90 | 6551.99 | 0.007307 | 1.89 | 583.97 | 345.51 | 0.25 |
| Kettle Creek | 6,23 | 5-YR | 1845.30 | 6550.00 | 6555.20 | 6551.18 | 6555.22 | 0.000350 | 0.83 | 1840.45 | 417.90 | 0.06 |
| Kettle Creek | 6.23 | 10-YR | 2426.00 | 6550.00 | 6558.90 | 6551.43 | 6558.91 | 0.000070 | 0.53 | 3612.81 | 576.66 | 0.03 |

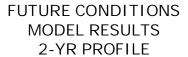


HEC-RAS Plan: Future River: Kettle Creek Reach: Kettle Creek (Continued)

| Reach | River Sta | Profile | Q Total | Min Ch El | W.S. Elev | Crit W.S. | E.G. Elev | E.G. Slope | Vel Chnl | Flow Area | Top Width | Froude # Chl |
|--------------|-----------|---------|---------|-----------|-----------|-----------|-----------|------------|----------|-----------|-----------|--------------|
| | | | (cfs) | (ft) | (ft) | (ft) | (ft) | (ft/ft) | (ft/s) | (sq ft) | (ft) | |
| Kettle Creek | 6.23 | 25-YR | 2920.90 | 6550.00 | 6563.10 | 6551.63 | 6563.10 | 0.000015 | 0.31 | 6506.39 | 747.30 | 0.02 |
| Kettle Creek | 6,23 | 50-YR | 3704.50 | 6550.00 | 6569.00 | 6551.92 | 6569.00 | 0.000004 | 0.20 | 11184.88 | 840.06 | 0.01 |
| Kettle Creek | 6.23 | 100-YR | 4250.10 | 6550.00 | 6573.90 | 6552.00 | 6573.90 | 0.000002 | 0.16 | 15505.39 | 924.54 | 0.01 |

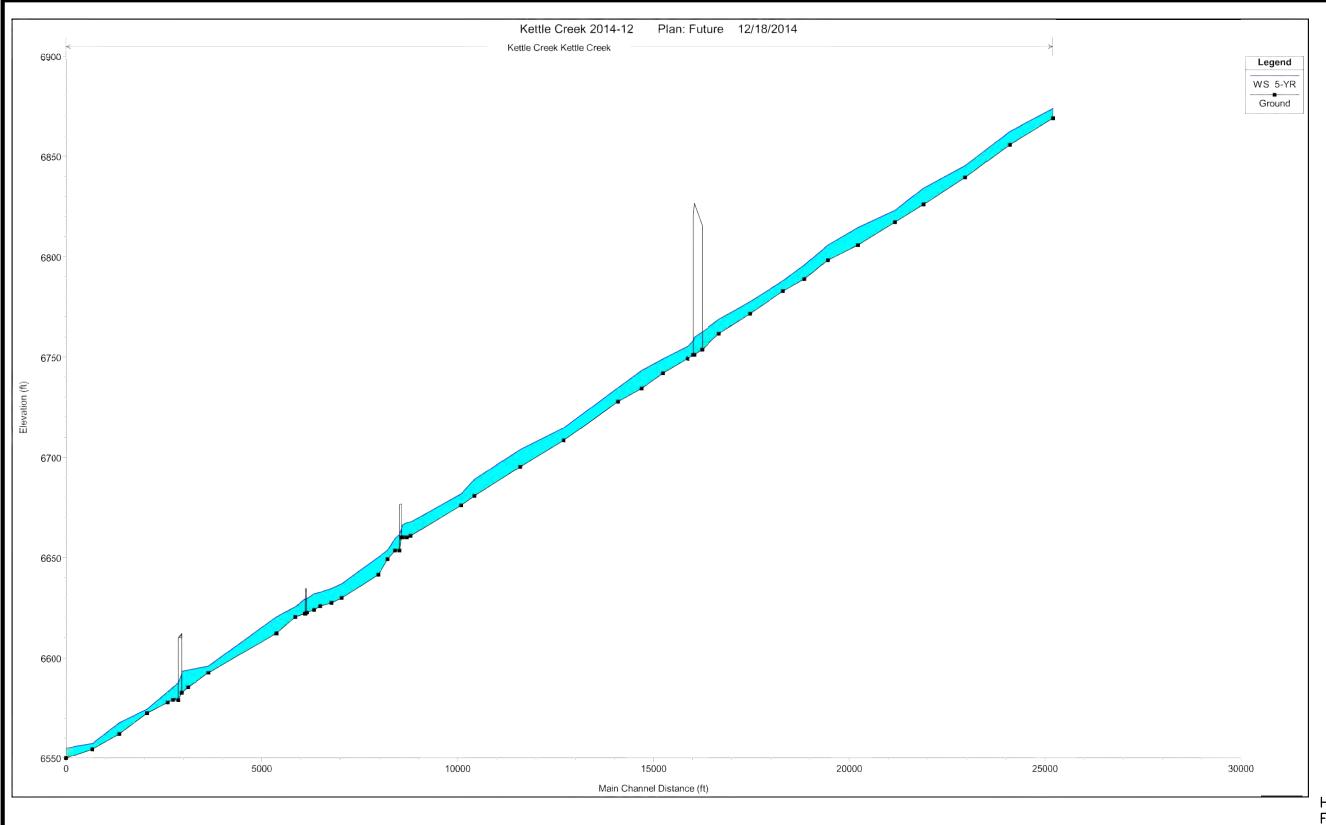








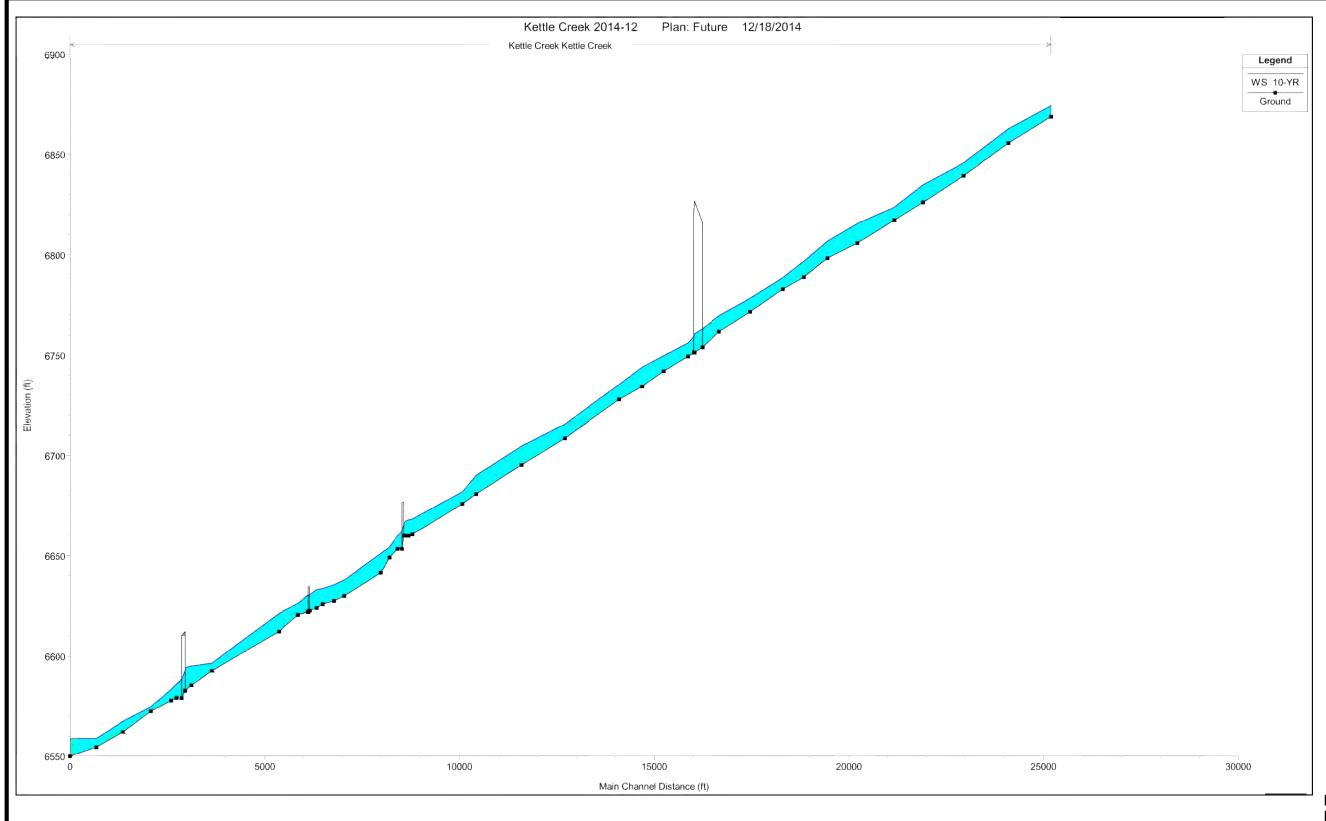
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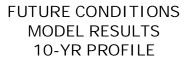




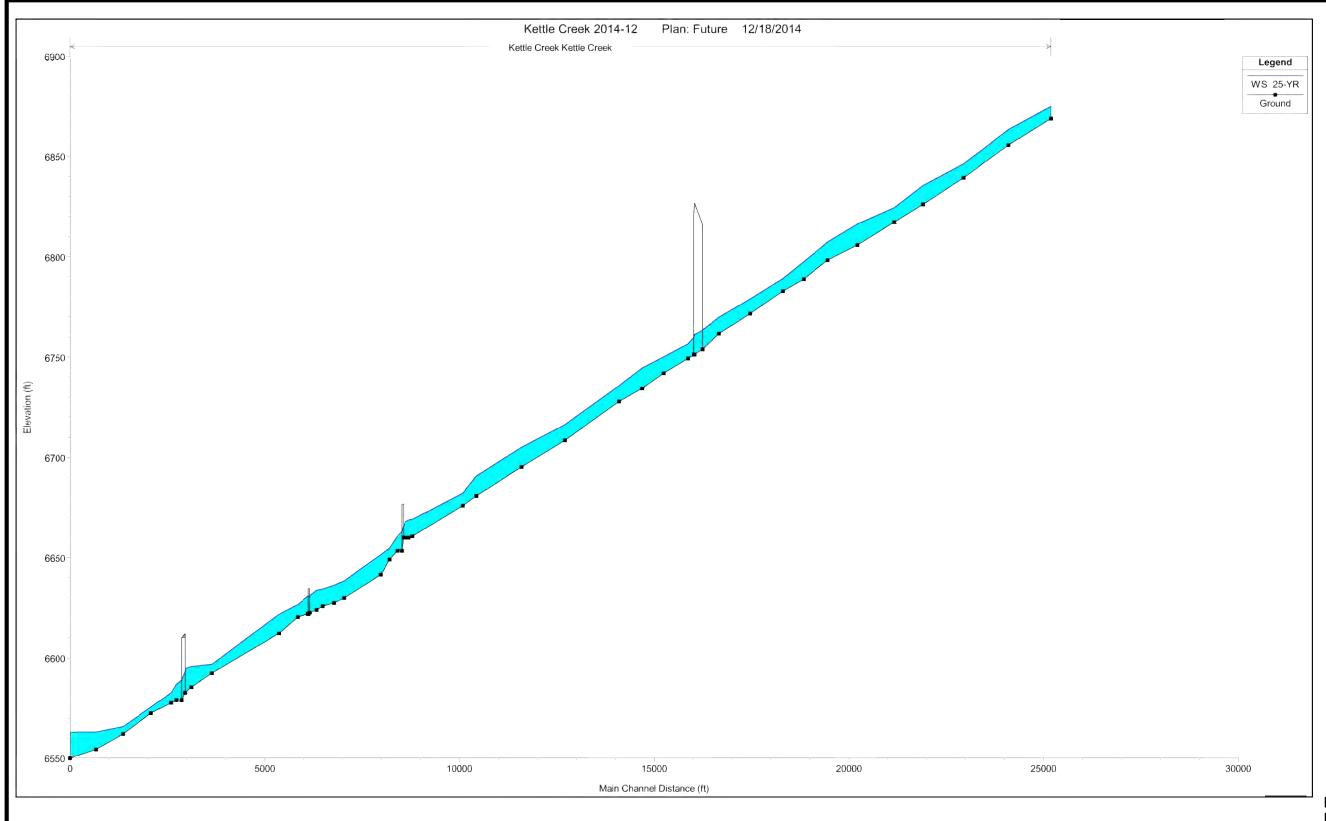


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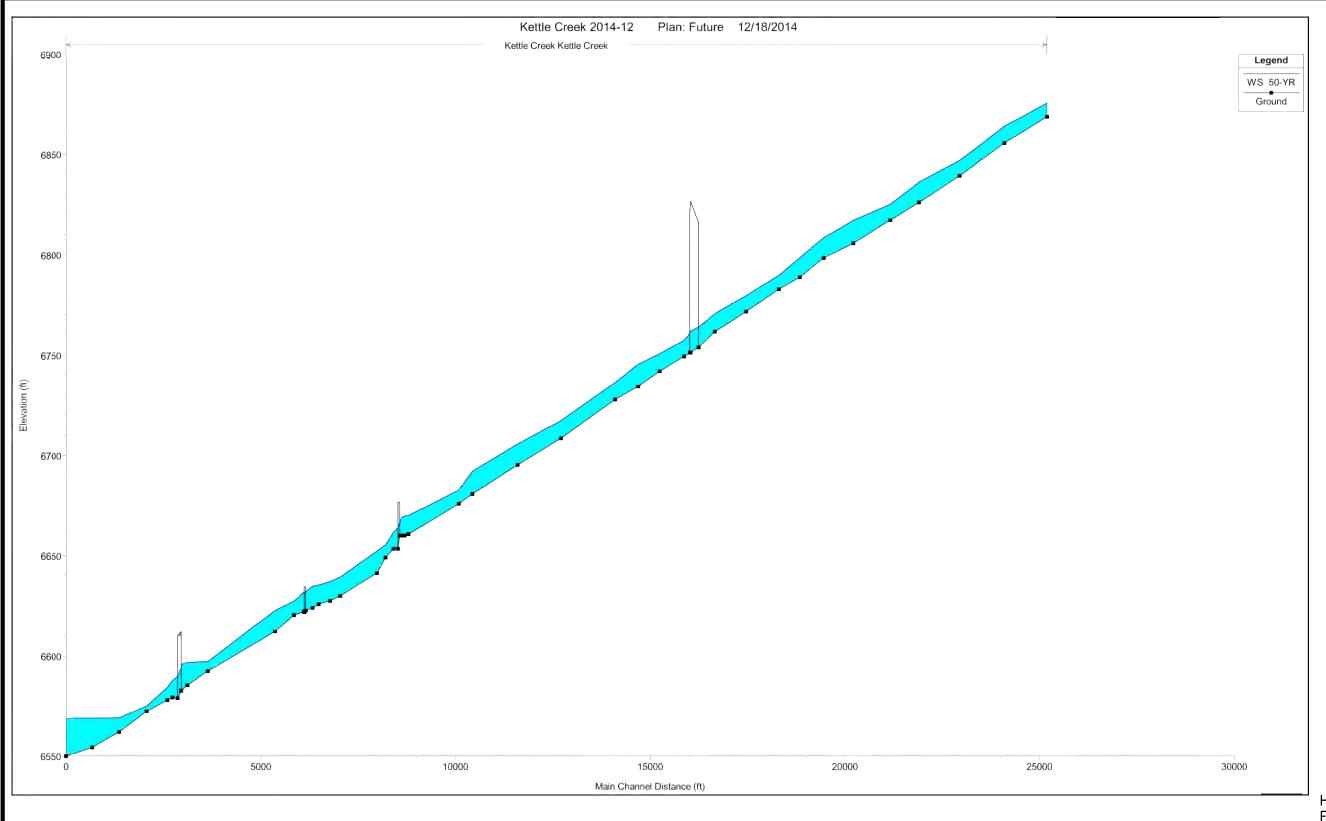








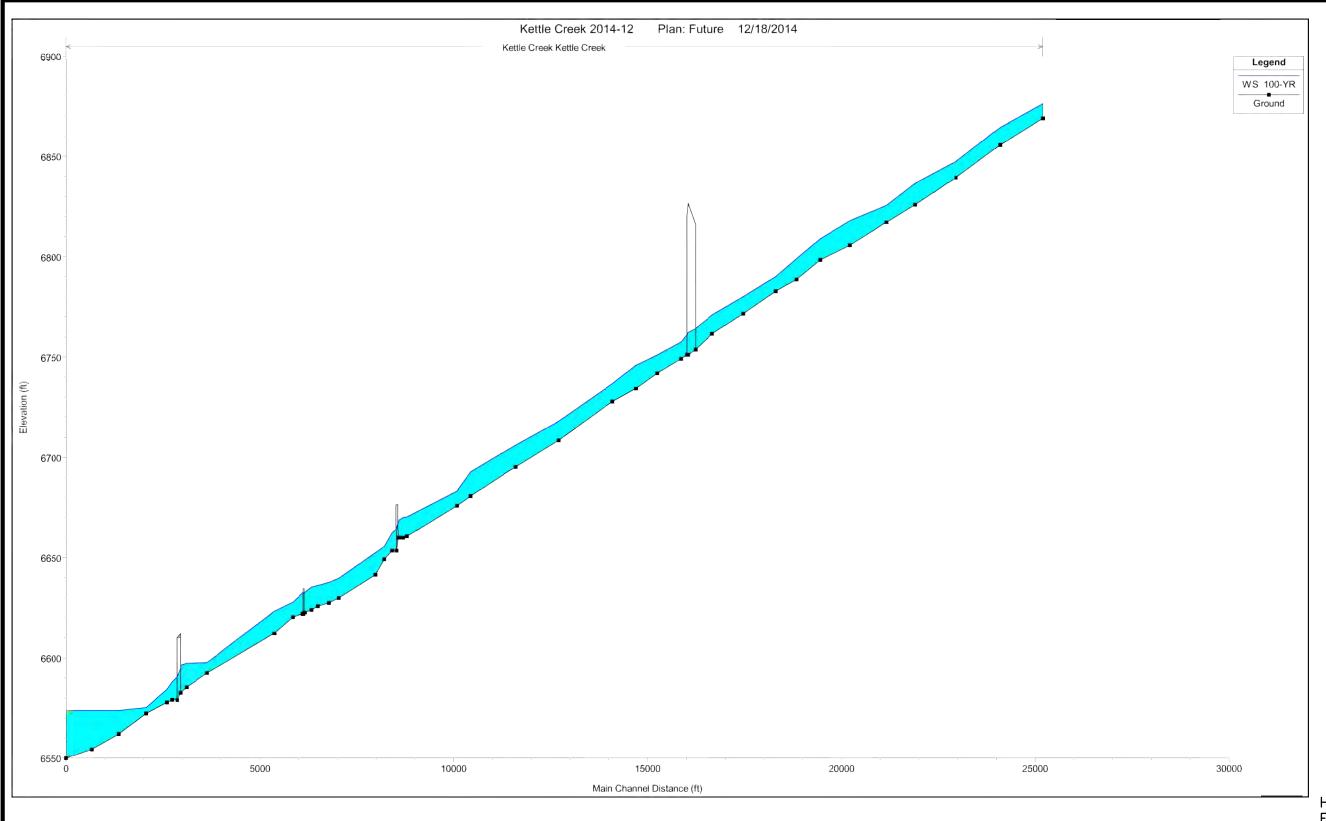








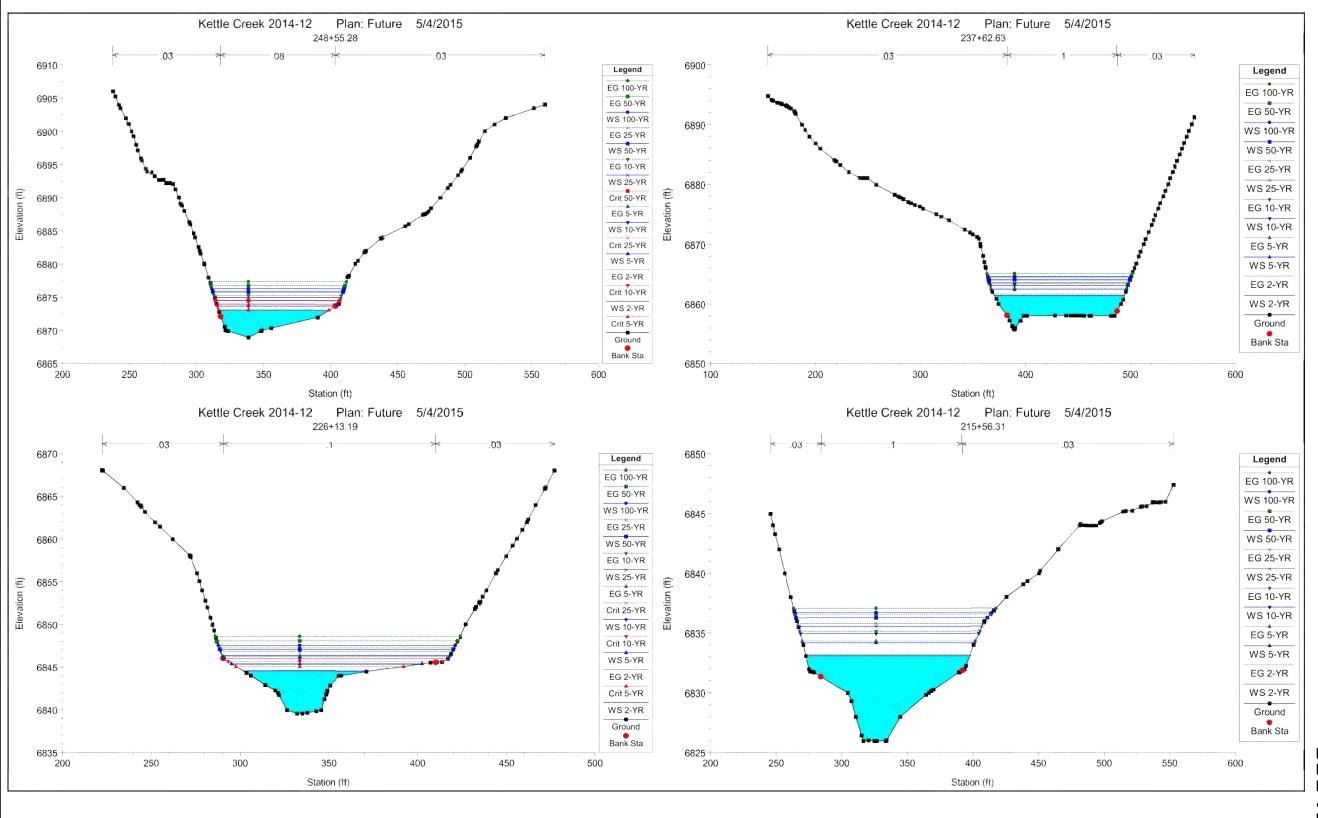
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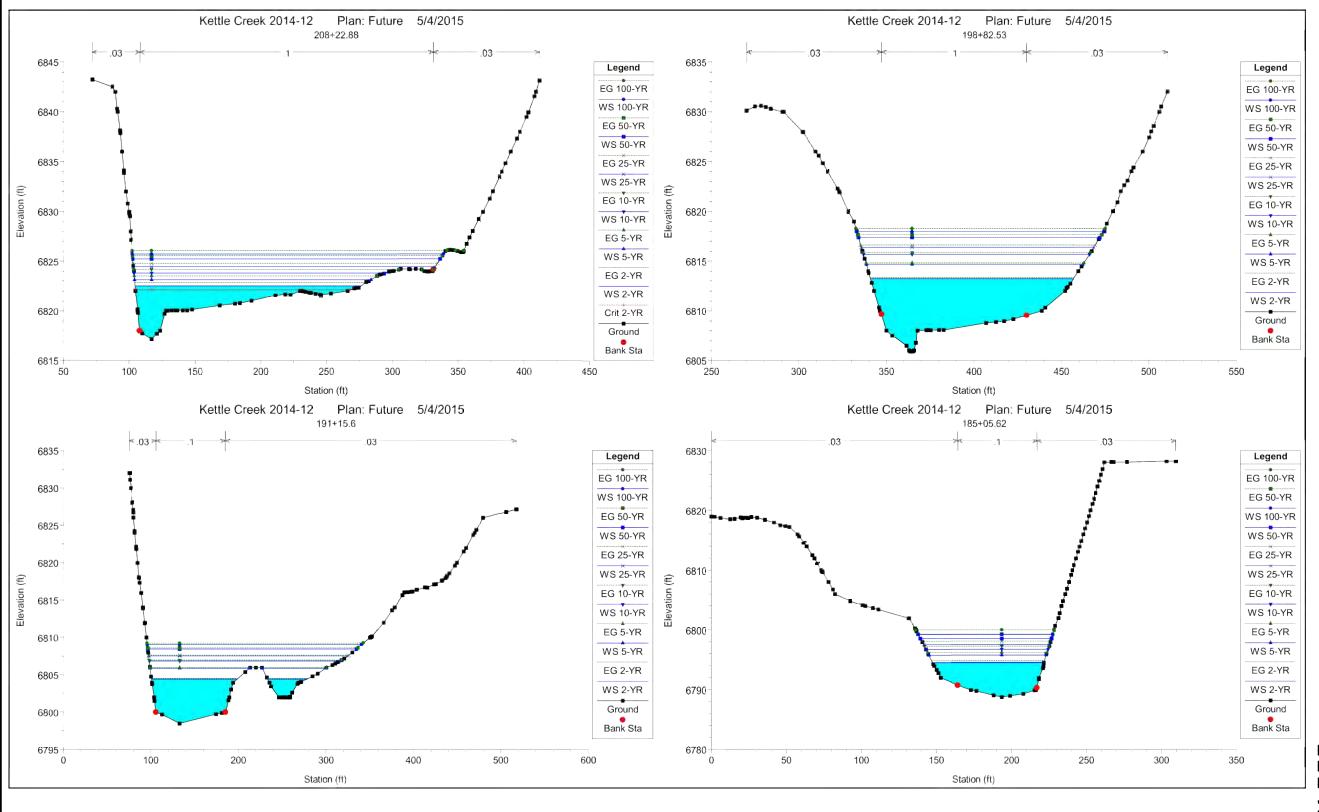


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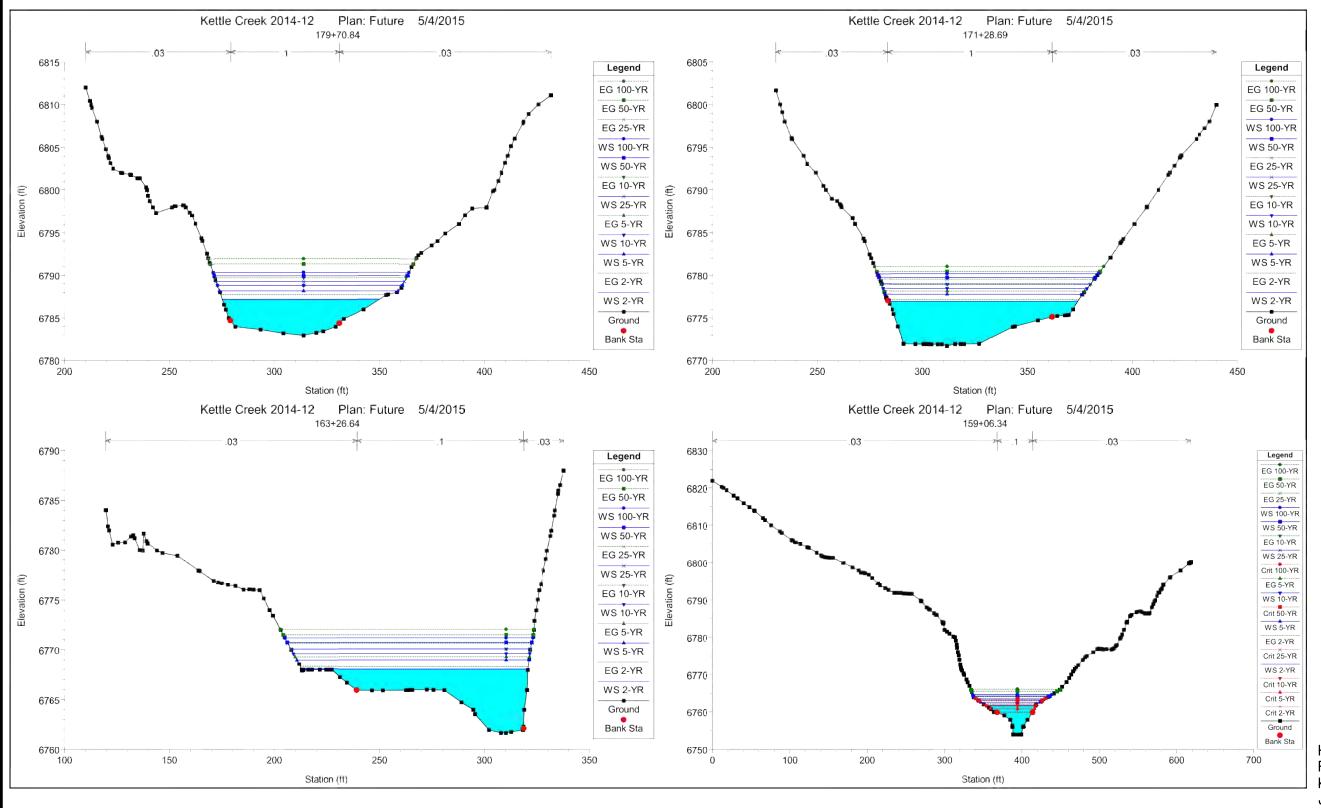






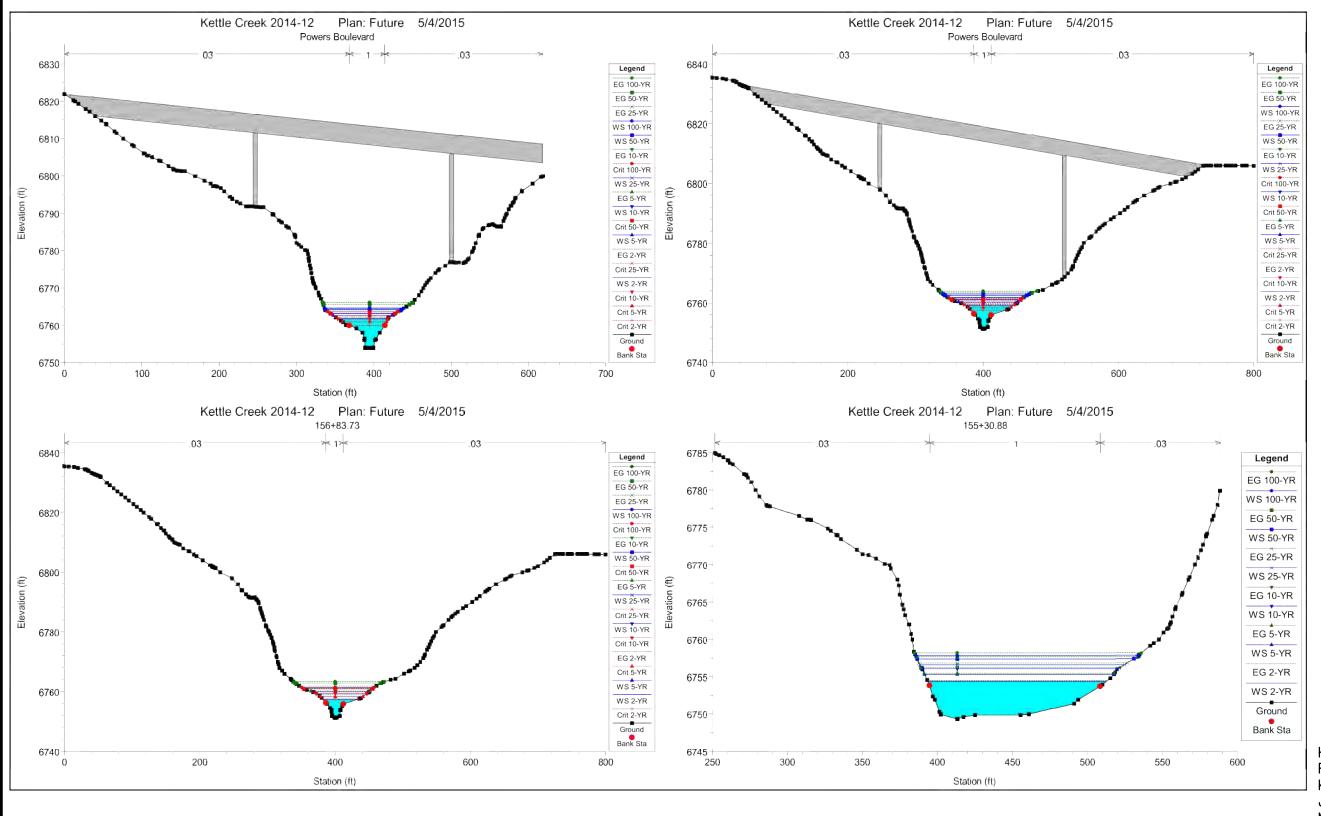








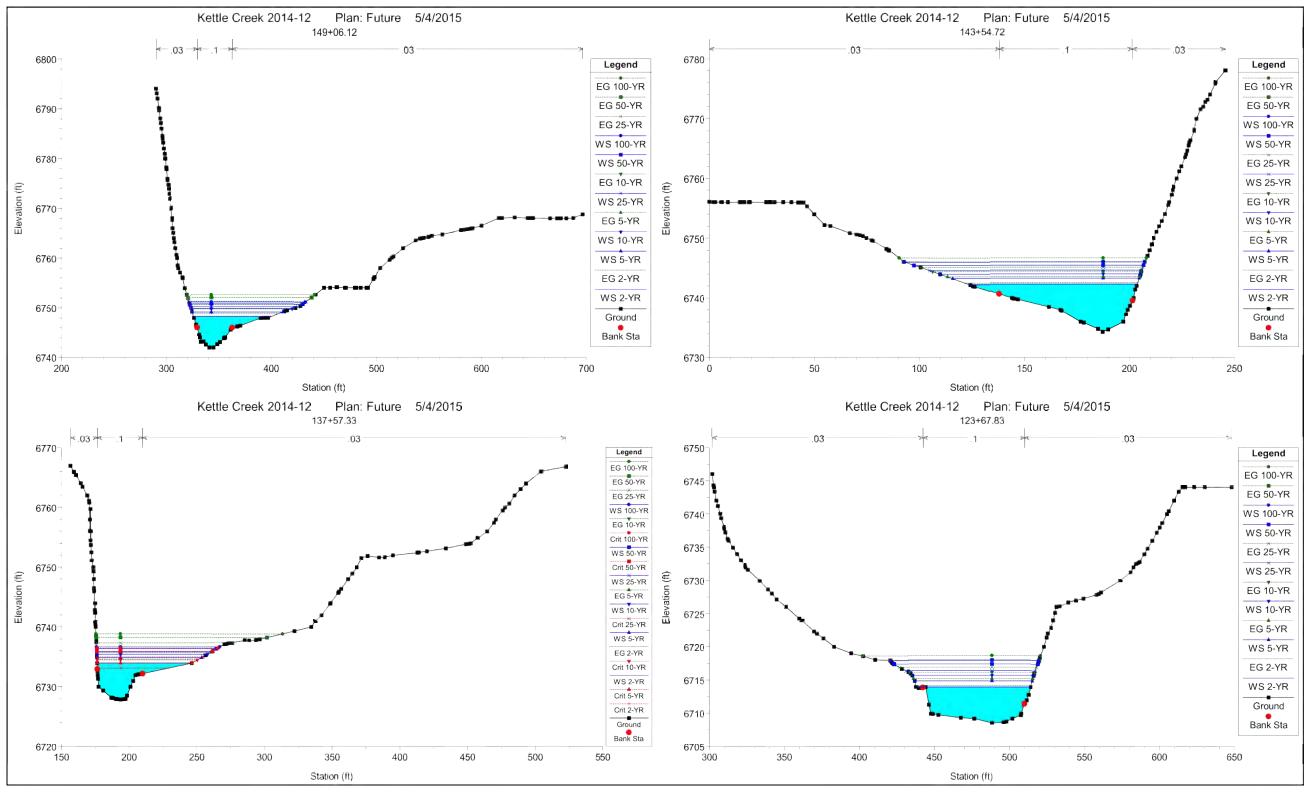




FUTURE CONDITIONS MODEL RESULTS

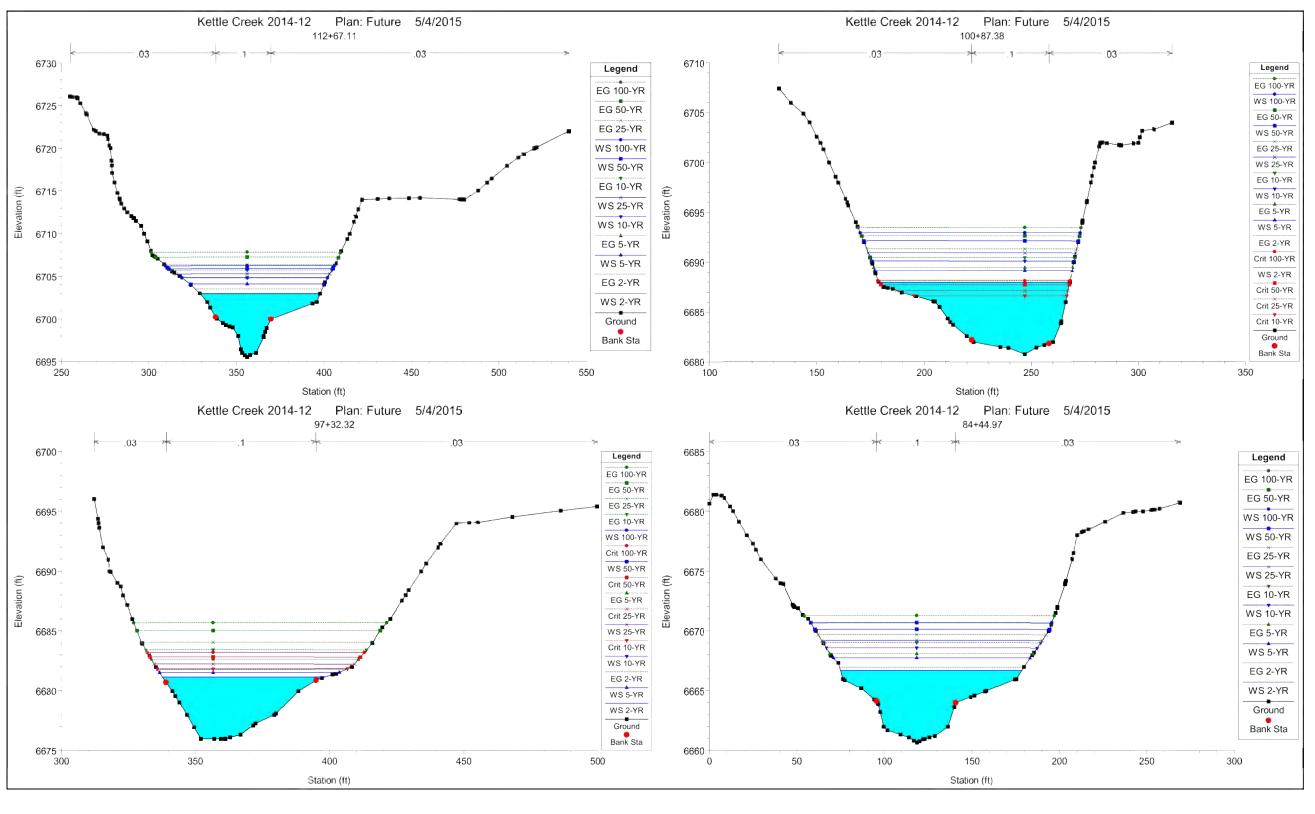


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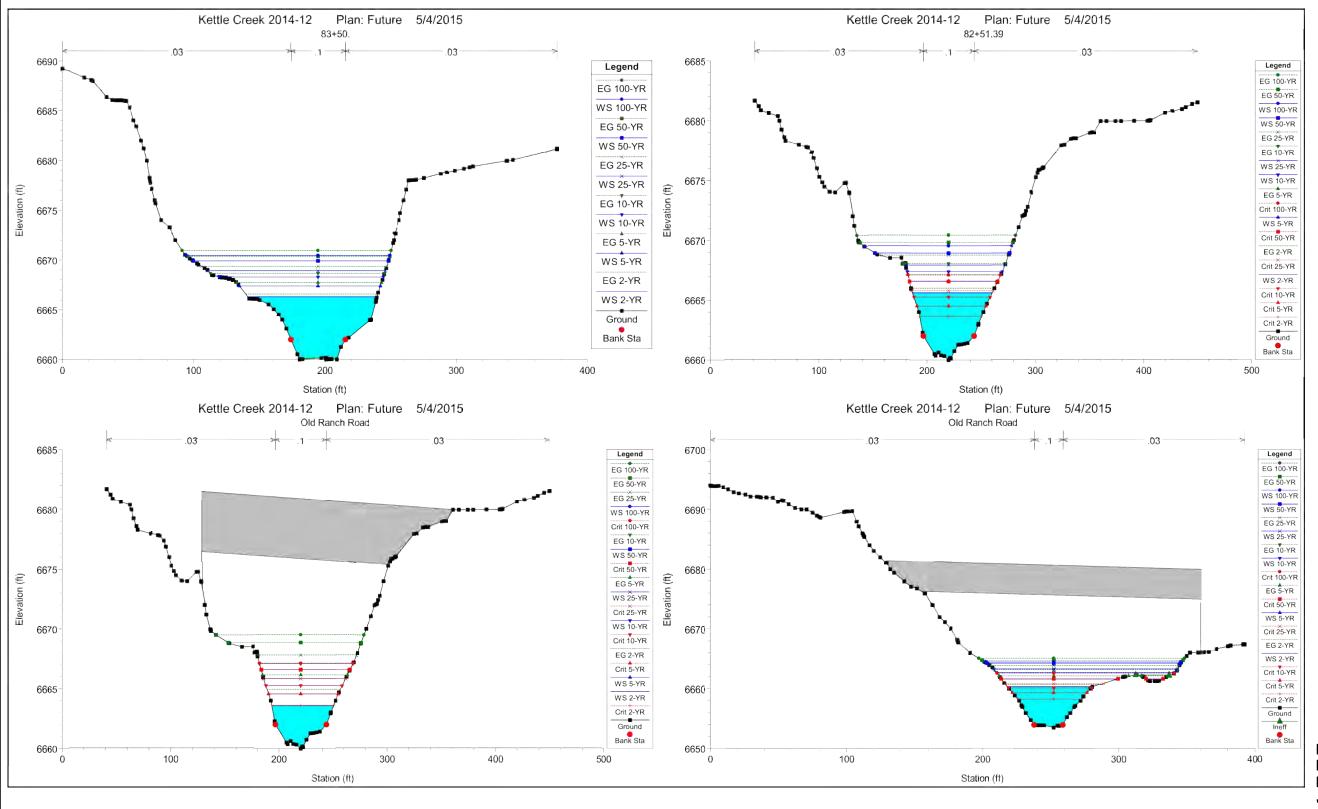
FUTURE CONDITIONS MODEL RESULTS







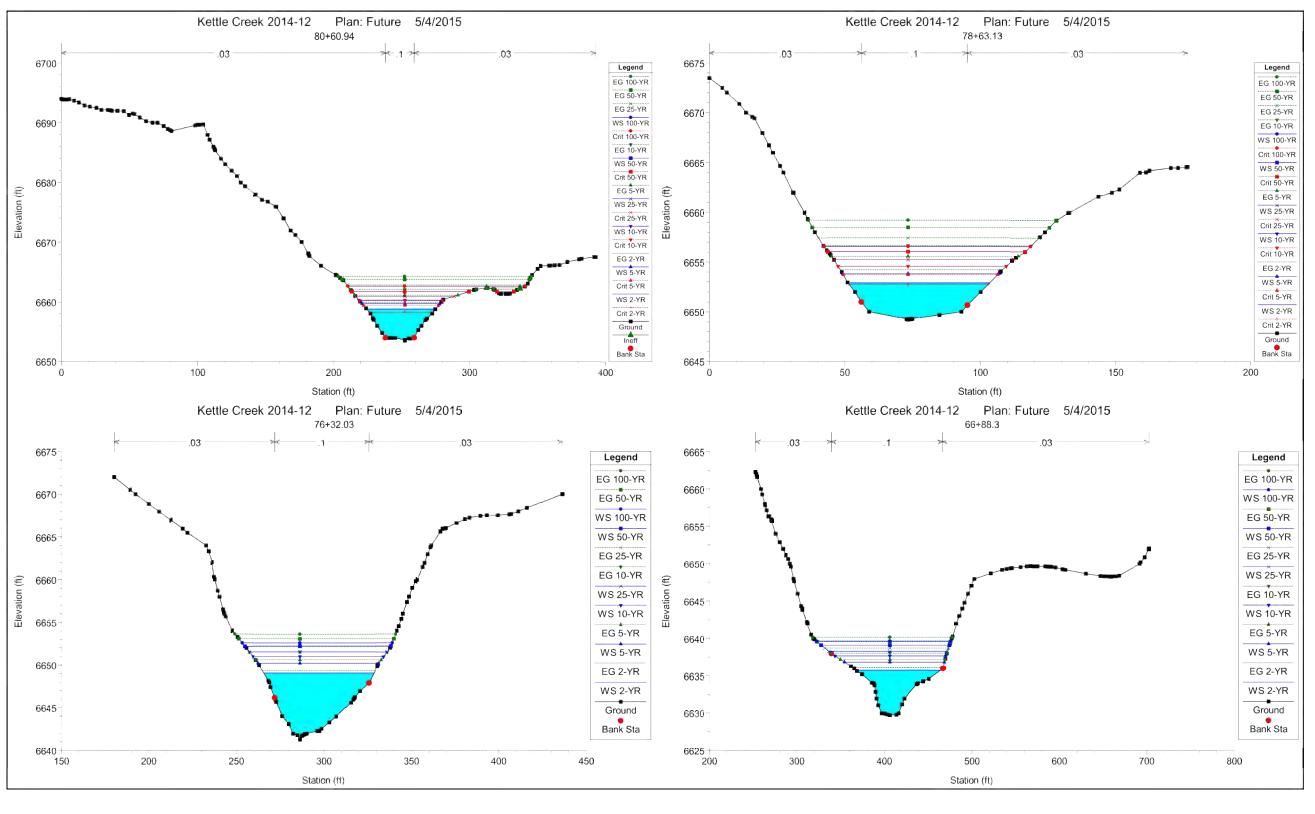






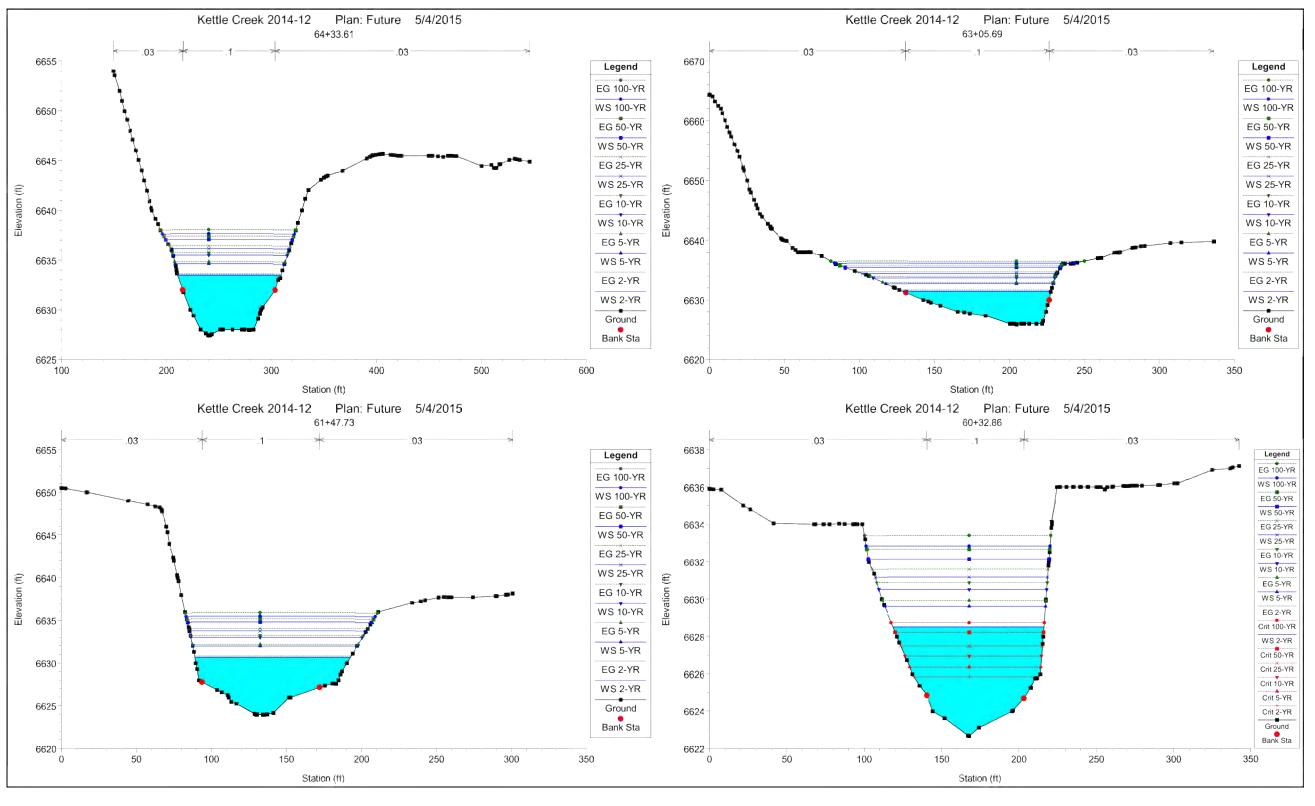


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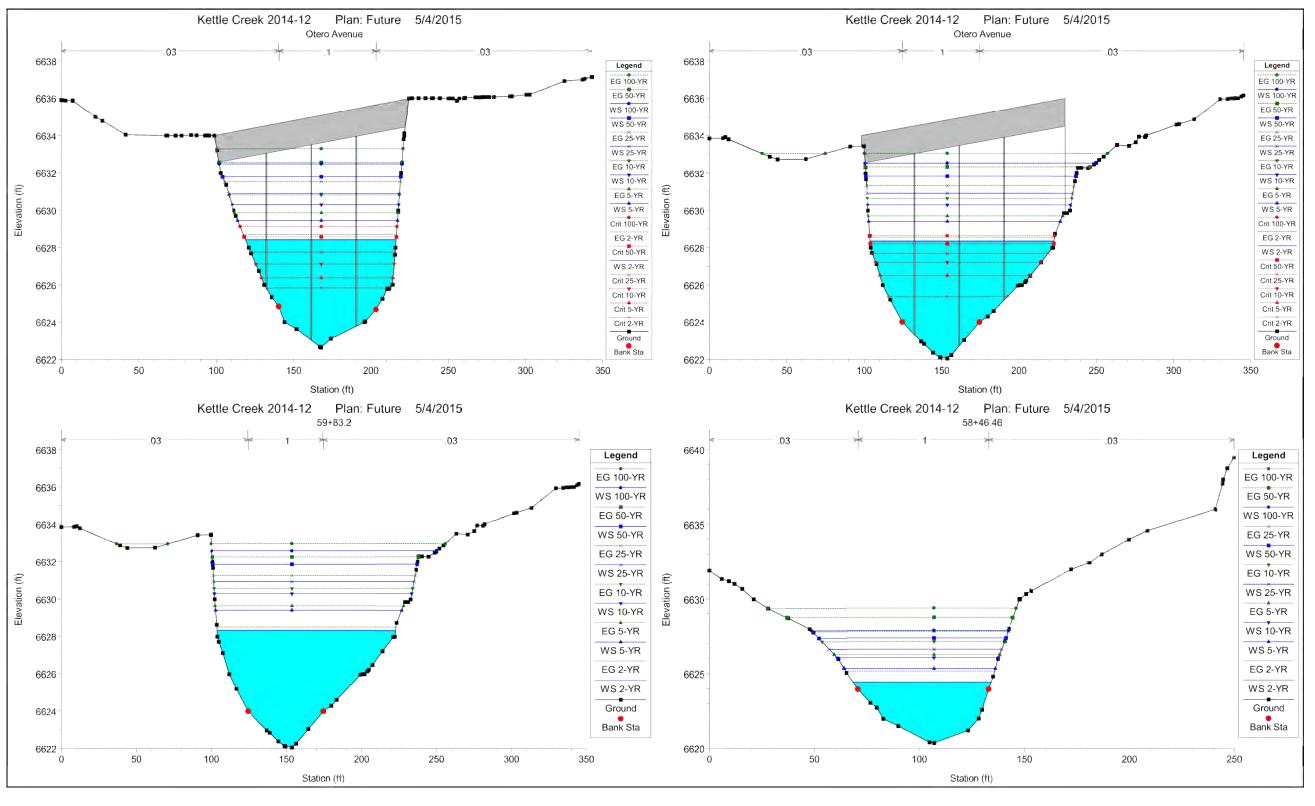






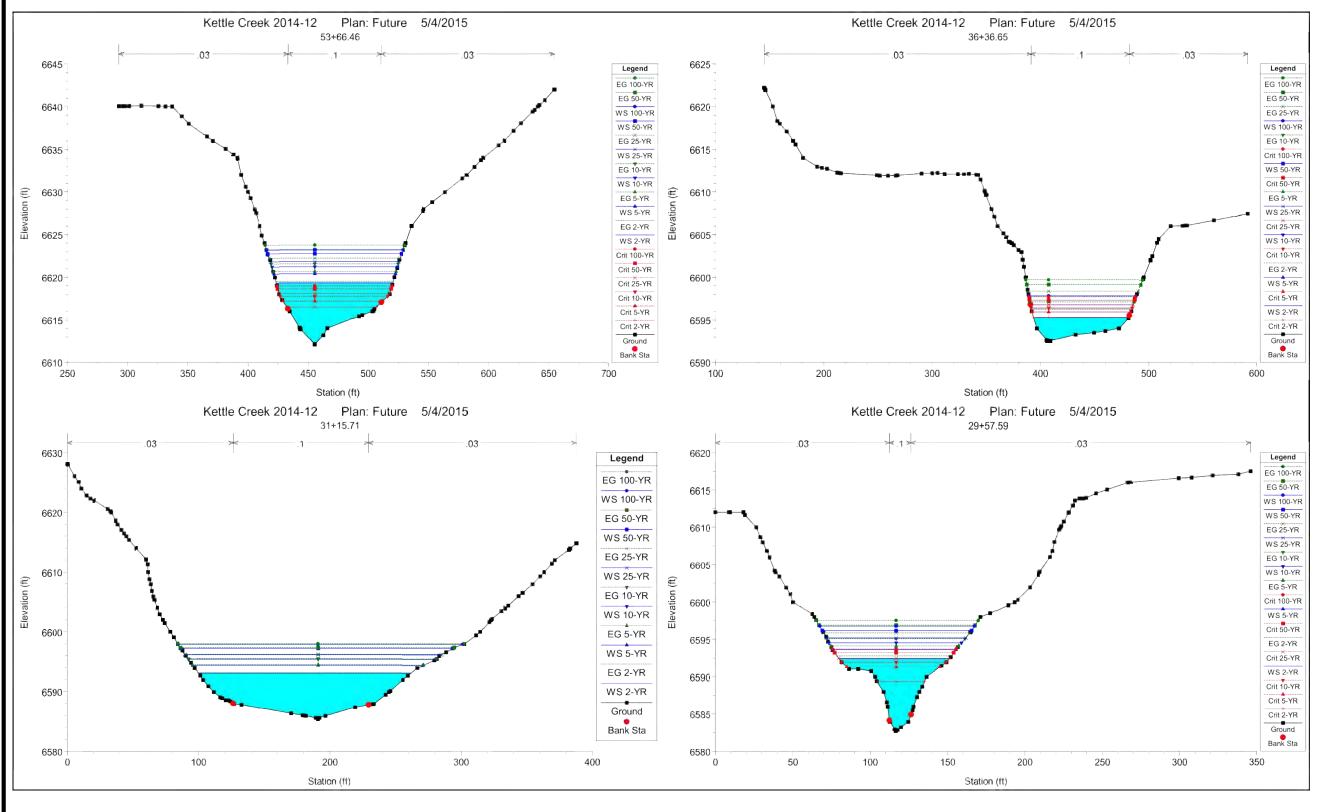






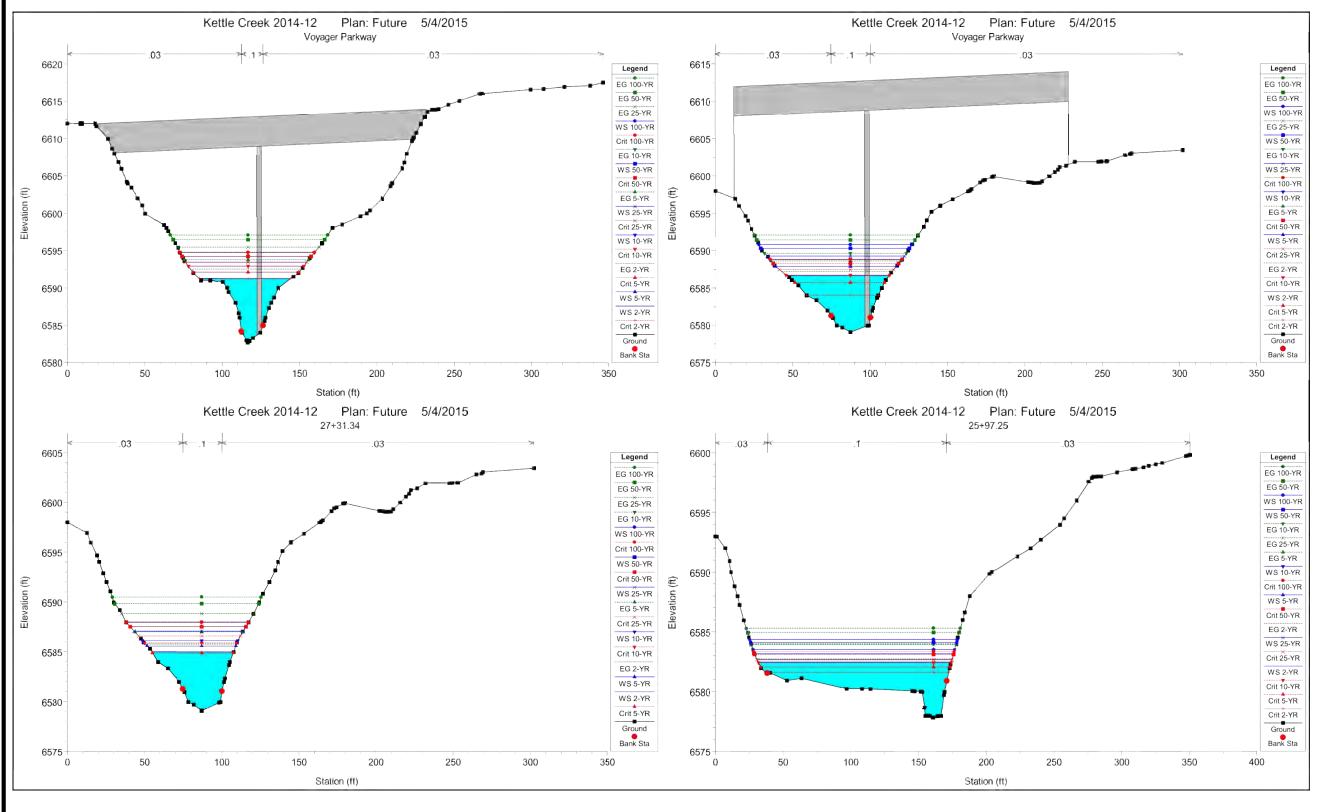






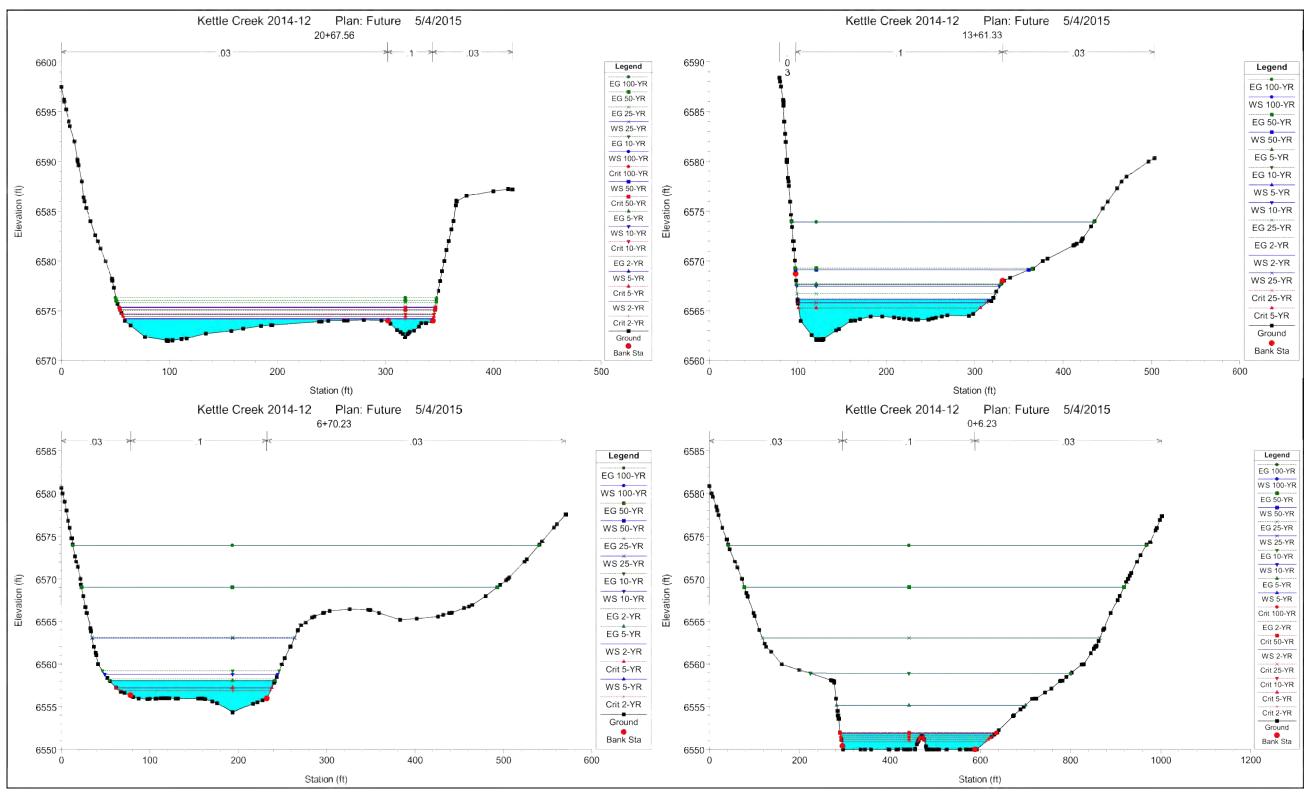
















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Kettle Creek DBPS Appendix



POWERS BLVD BRIDGE LOOKING NORTH



OLD RANCH ROAD BRIDGE DOWNSTREAM



POWERS BLVD BRIDGE LOOKING UPSTREAM



OLD RANCH ROAD BRIDGE LOOKING NORTH



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OLD RANCH ROAD BRIDGE LOOKING UPSTREAM



OTERO AVE BRIDGE LOOKING UPSTREAM



OLD RANCH ROAD BRIDGE LOOKING UPSTREAM



OTERO AVE BRIDGE LOOKING UPSTREAM



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HWY 83 BRIDGE LOOKING NORTH



HWY 83 BRIDGE LOOKING UPSTREAM





CHANNEL CONDITIONS APPROX. STA 80+00



CHANNEL CONDITIONS APPROX. STA 165+00



CHANNEL CONDITIONS APPROX. STA 160+00



CHANNEL CONDITIONS APPROX. STA 175+00



CHANNEL CONDITIONS APPROX. STA 169+00



CHANNEL CONDITIONS APPROX. STA 104+00

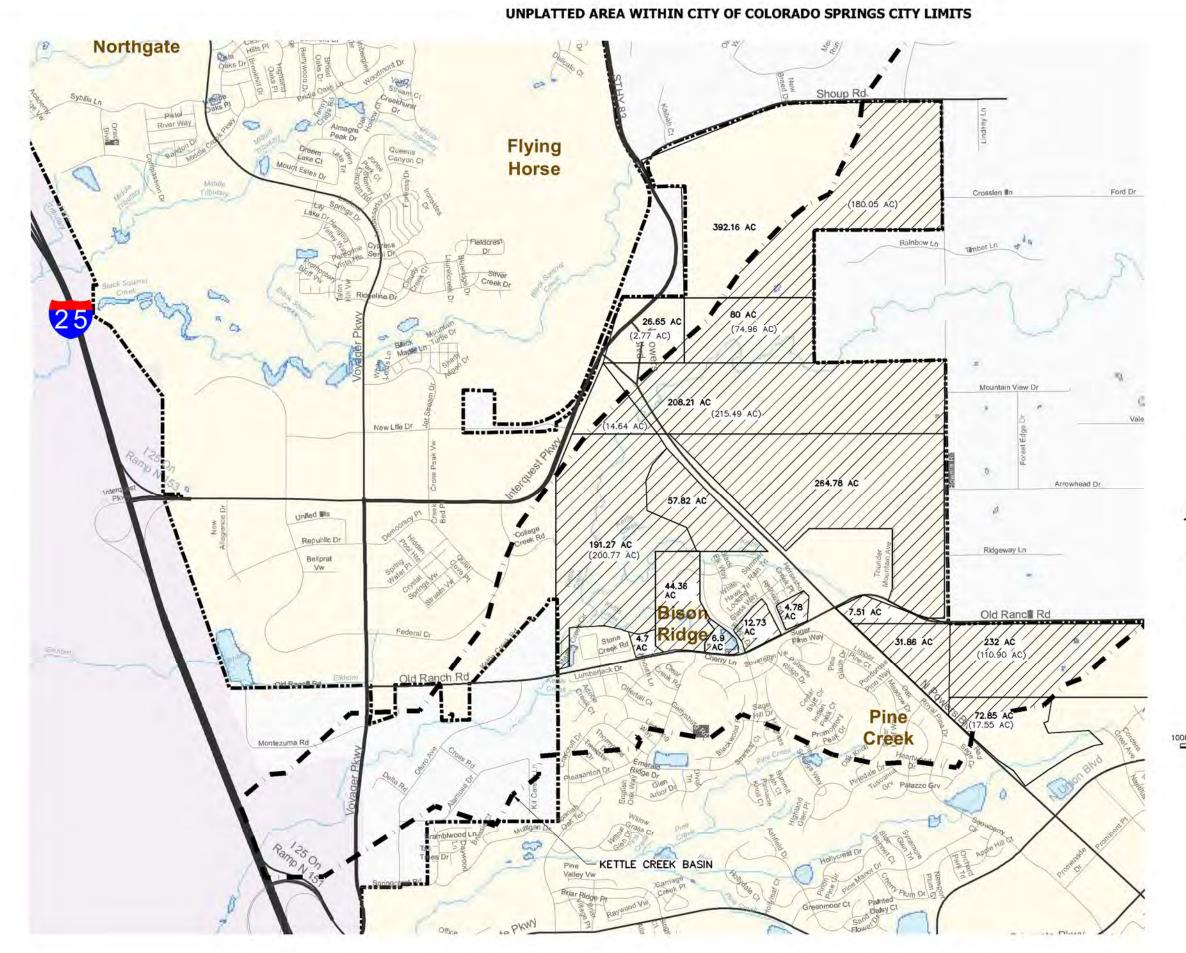


CHANNEL CONDITIONS APPROX. STA 58+00



Centennial 303-740-9393 • Colorado Springs 719-593-2593 Fort Collins 970-491-9888 • www.jrengineering.com **Appendix E – Unplatted Area Calculations**

Kettle Creek DBPS Appendix

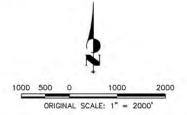


| Unplatted Area in t | the Kettle Creek Basin |
|---------------------|------------------------|
| Acreage | |
| | 180.05 |
| | 74.96 |
| | 2.77 |
| | 215.49 |
| | 14.64 |
| | 200.77 |
| | 57.82 |
| | 264.78 |
| | 44.36 |
| | 4.70 |
| | 6.90 |
| | 12.73 |
| | 4.78 |
| | 7.51 |
| | 31.86 |
| | 110.90 |
| | 17.55 |
| | 1252.57 |

LEGEND







APPENDIX E — UNPLATTED AREA CALCULATIONS KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 E-1



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LEGEND

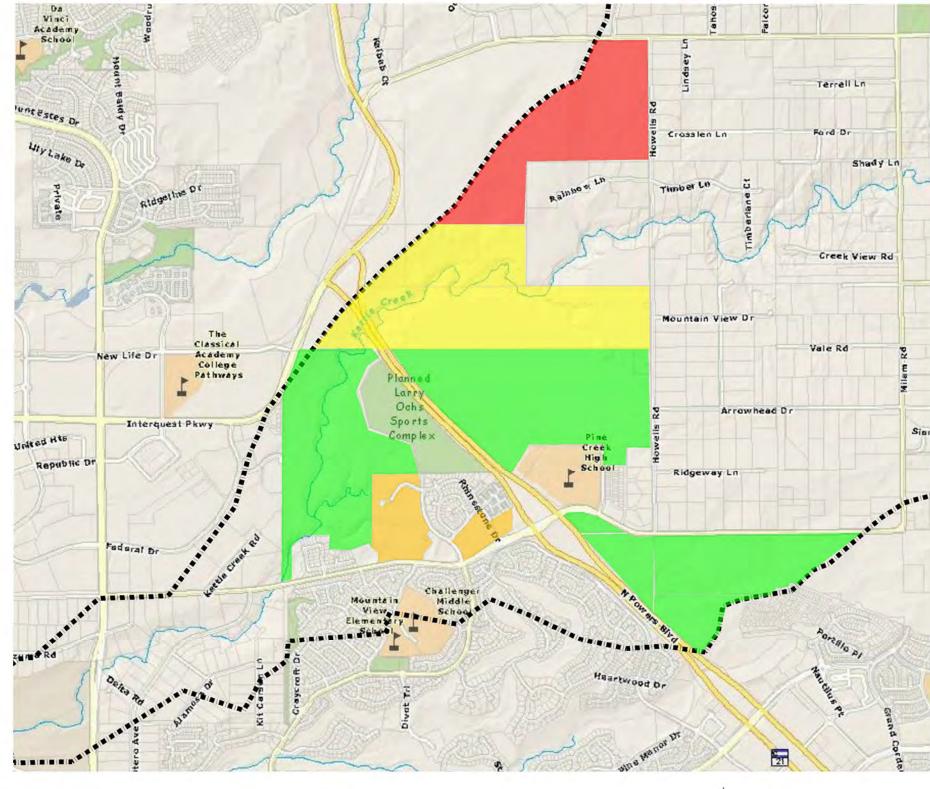
JOVENCHI-I LLC

260 EB LLC

HIGH VALLEY LAND COMPANY INC

KETTLE CREEK LLC & VENEZIA JOHN FAMILY TRUST

KETTLE CREEK BASIN BOUNDARY



| KETTLE CREEK UNDEVELOPED LAND OWNERS | | | | | | | | | |
|--------------------------------------|-----------|------------|--|--|--|--|--|--|--|
| PROPERTY OWNER | AREA (AC) | PERCENTAGE | | | | | | | |
| JOENCHII LLC | 307 | 27.2% | | | | | | | |
| 260 EB LLC | 180 | 15.9% | | | | | | | |
| HIGH VALLEY LAND COMAPANY | 580 | 51.4% | | | | | | | |
| KETTLE CREEK LLC & | | | | | | | | | |
| VENEZIA JOHN FAMILY TRUST | 62 | 5.5% | | | | | | | |
| Total | 1129 | 100.0% | | | | | | | |

2000 1000 0 2000 ORIGINAL SCALE: 1" = 2000' APPENDIX E —
UNDEVELOPED LAND
OWNERS
KETTLE CREEK DBPS
JOB NO. 25100.00
MAY 2015
E-2



J·R ENGINEERING

A Westrian Company

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Kettle Creek DBPS Appendix

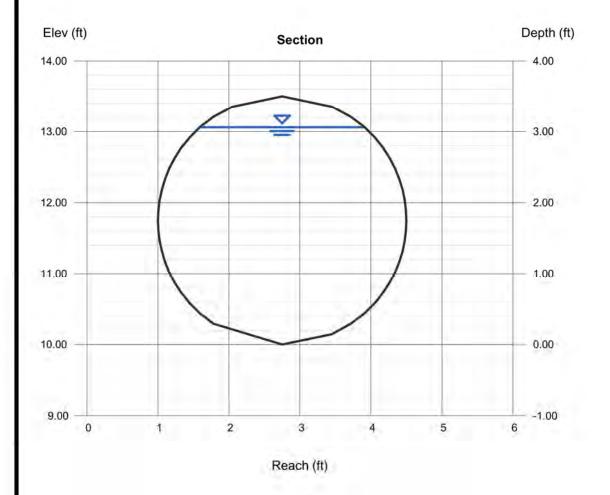
Channel Report

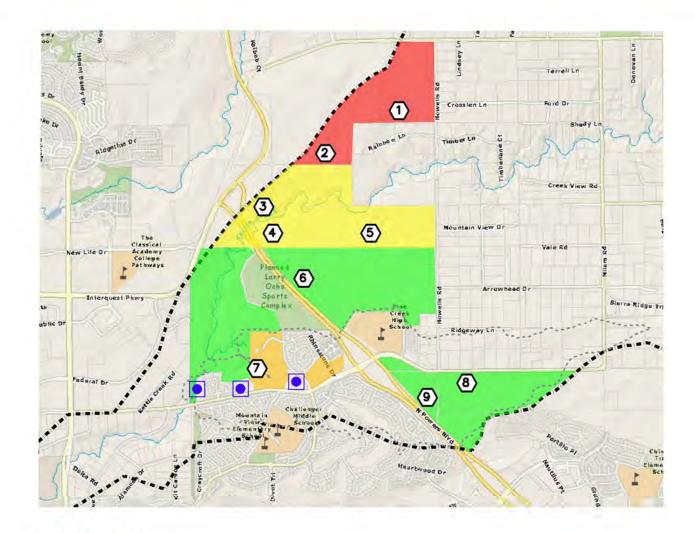
Hydraflow Express Extension for AutoCAD® Civil 3D® 2012 by Autodesk, Inc.

Wednesday, Jan 21 2015

Conceptual Outfall From 260 EB LLC

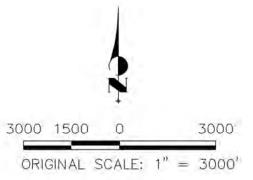
| Circular | | Highlighted | |
|------------------|---------|---------------------|---------|
| Diameter (ft) | = 3.50 | Depth (ft) | = 3.06 |
| | | Q (cfs) | = 94.50 |
| | | Area (sqft) | = 8.93 |
| Invert Elev (ft) | = 10.00 | Velocity (ft/s) | = 10.58 |
| Slope (%) | = 0.80 | Wetted Perim (ft) | = 8.47 |
| N-Value | = 0.013 | Crit Depth, Yc (ft) | = 3.00 |
| | | Top Width (ft) | = 2.31 |
| Calculations | | EGL (ft) | = 4.80 |
| Compute by: | Known Q | | |
| Known Q (cfs) | = 94.50 | | |





LEGEND





APPENDIX F — BASIN FEE EXHIBIT KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015



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DRAINAGE CALCULATIONS FOR FEE DETERMINATION*

FOR 260 EB LLC to Jovenchi-I LLC Property

| Subdivision: 260 EB LLC | Project Name: Kettle Creek DBPS |
|-------------------------|---------------------------------|
| Location: Kettle Creek | Project No.: 25100.00 |
| | Calculated By: Mark Fischer |
| | Checked By: |
| | Date: 1/13/15 |

| SUB-BASIN DATA | | | | | | | AL/OVE | RLAND | | | FLOWS | | | | | |
|-------------------|--------------|---------------------------|------|------------------|----------------|--------|----------|-------------------------|-----------|-------|-------|---------------|-------------------------|-------------------------------|------------------|------------|
| | | | | | | | (T_i) | | | | v - 1 | | | | | |
| BASIN ID | D.A. (AC) | Hydrologic Soils Group | | C ₁₀₀ | C ₅ | L (FT) | S (%) | T _i (MIN) | L (FT) | S (%) | Cv | VEL. (FPS) | T _i (MIN) | COMP. T _c (MIN) | 1 100 (IN/HR) | Q (CFS) |
| 260 EB | 47.00 | В | 2.00 | 0,36 | 0.08 | 200 | 3.0 | 18.3 | 3113 | 4.0 | 7.0 | 1.4 | 37.1 | 55.4 | 2,6 | 44.0 |
| JOVENCHI | 54.00 | В | 2.00 | 0.36 | 80,0 | 100 | 3.0 | 13.0 | 1038 | 7.0 | 5.0 | 1,3 | 13.1 | 26.0 | 4.5 | 87.5 |
| | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | |
| | - | | | | | | | | | | | | | | | |

NOTES:

$$\begin{split} T_i &= (0.395*(1.1 - C_5)*(L)^0.5)/((S)^0.33), \ S \ in \ fl/ft \\ T_i &= L/60V \ (Velocity \ From \ Fig. 501) \\ Velocity \ V &= C_V *S^0.5, \ S \ in \ fl/ft \\ \Gamma_c \ Check &= 10 + L/180 \\ I_{100} &= (-2.52*ln(T_c)) + 12.735 \\ Q &= C_{100}*(D.A.)*I_{100} \end{split}$$

STANDARD FORM SF-3 STORM DRAINAGE SYSTEM DESIGN (RATIONAL METHOD PROCEDURE)

| Location: Arapahoe County | Project Name: Kettle Creek DBPS |
|---------------------------|---------------------------------|
| Subdivision: | Project No.: 25100:00 |
| Location: Arapahoe County | Calculated By: Mark Fischer |
| Design Storm: 100-Year | Checked By: Tristan Bonser |
| | Date: 1/13/15 |

| | =150 | DIRECT RUNOFF | | | | | | | | TOTAL RUNOFF | | | | | PIPE | | | TRA | VEL. | TIME | |
|----------------|--------------|---------------|-----------|---------------|---------|-----------|-----------|---------|---------|--------------|------------|---------|-----------|-------------------|-------------------|-----------|--------------------|-------------|----------------|----------|---------|
| STREET | Design Point | Basin ID | Area (Ac) | Runoff Coeff. | Tc (mm) | Ç. A (Ac) | l (in/br) | Q (cfs) | Te (mm) | C*A (Ac) | I (iiv/hr) | Q (cfs) | Slope (%) | Street Flow (cfs) | Design Flow (efs) | Slope (%) | Pipe Size (inches) | Length (ft) | Velocity (fps) | Tr (min) | REMARKS |
| 260 EB LLC | | 260 | 47.00 | 0.36 | 55.4 | 16.92 | 2.60 | 44.0 | - | | | | | | | | | | | | |
| Jovenshi-I LLC | | T. | 54.00 | 0.36 | 26.0 | 19,44 | 4.50 | 87.5 | 55,4 | 36,36 | 2.60 | 94.5 | T | | | | | - | | | |

*NOTE: NO DRAINAGE FEES IN THE KETTLE CREEK BASIN. CALCULATIONS FOR REFERENCE ONLY.

APPENDIX F — BASIN FEE FLOW DATA KETTLE CREEK DBPS JOB NO. 25100.00 MAY 2015 F-2

