FINAL DRAINAGE REPORT: MARIAH TRAIL FILING NO. 1 MAJOR SUBDIVISION

A PORITION OF THE NORTHWEST QUARTER OF SECTION 17, TOWNSHIP 14 SOUTH, RANGE 66 WEST OF THE 6TH P.M. COUNTY OF EL PASO, STATE OF COLORADO

> LOTS 1-6 MARIAH TRAIL FILING NO. 1 EL PASO COUNTY, COLORADO

> > PREPARED FOR: MR. THOMAS KIRK, JR. 19205 MARIAH TRAIL COLORADO SPRINGS, CO EMAIL: PCD File No. SF-2315

LATEST REVISION DATE: August 4, 2023

PREPARED BY

CARLOS SERRANO, PE ENGINEERING LOCAL XPERTS



PROJECT NO. 100678

2320 W. COLORADO AVENUE, STE. 122 | COLORADO SPRINGS, CO 80904 | 719.308.9146

Engineer's Statement

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the city/county for drainage reports and said report is in conformity with the master of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.

SIGNATURE (Affix Seal): _

Carlos David Serrano, Colorado P.E. No.: 52048 For and on Behalf of Engineering Local Xperts Date

SEAL:

DEVELOPER'S STATEMENT

I, <u>Mr. Thomas Kirk, Jr.</u>, the developer, have read and will comply with all of the requirements specified in this drainage report and plan.

| Name of Developer | | |
|----------------------|------|--|
| Authorized Signature | Date | |
| | | |
| Printed Name | | |
| Title | | |
| Address | | |

EL PASO COUNTY STATEMENT:

Filed in accordance with the requirements of the Drainage Criteria Manual, Volumes 1 and 2, El Paso County Engineering Criteria Manual and Land Development Code as amended.

| Joshua Palmer, P.E. |
|-------------------------------------|
| County Engineer / ECM Administrator |
| Conditions: |

Date

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1) INTRODUCTION

The purpose of this report is to identify on-site and offsite drainage patterns, assess stormwater conditions per delineated project sub-basins, demonstrate adequate design standards for storm water conveyance and release into the existing storm water system (on-site or off-site), and provide a narrative for any other drainage considerations on the development. The purpose of the project is to subdivide an existing 35-acre RR-5 zoned parcel into six single-family residential lots as a Major Subdivision. A Drainage Letter is sufficient for the purposes of a final plat and "small subdivision" per County standards.

2) EXISTING CONDITIONS

LOCATION

The property of interest, henceforth referred to as the Site, addressed as 19205 Mariah Trail, is an unplatted 35-acre RR-5 zoned parcel within El Paso County with Schedule No. 5100000511. The Site within the northwest quarter of Section 7, Township 11 South, Range 65 West of the sixth P.M.. The Site is south of the County's 60-foot right-of-way of Mariah Trail, a rural local gravel roadway. The property is accessed via a private access drive within a 16-foot width common access easement (Reception No. 213070061). The adjacent properties or subdivisions are as follows:

North: El Creek Ranches Filing No. 1 (Lots 24-26)

East: 19275 Mariah Trail, Schedule No. 5100000512, Zoned RR-5, Unplatted 40.23 acre property

South: 18885 Brown Road, Schedule No. 5100000447, Zoned RR-5, Unplatted 61.55 acre property

West: Part of Section 12-11-66, Schedule No. 6100000224, Zoned RR-5, Unplatted 80 acre property

The Site is currently zoned RR-5 (Rural Residential), allowing 5-acre minimum lots with 25-foot front, rear, and side setbacks for principal structures, and a 200-foot minimum lot frontage width.

EXISTING SOILS

The soils indicative to the site are classified as Brussett loam and Peyton-Print complex by the USDA Soil Conservation Service and are listed as NRCS (National Resources Conservation Service) Hydrologic Soil Group B. A USDA Soil Map is provided in Appendix C.

EXISTING DRAINAGE CONDITIONS

The existing topography of the Site consists of slopes between 2.0 percent and 15 percent generally draining from the west to the east. There are several local topographic high points and

grasslined swales across the property. The natural landscape comes to a swale located on the eastern property boundary, central to the Site. The majority of the Site drains to this point where it continues to flow due east. The stormwater runoff to this area is via overland sheet flow and remains generally as sheet flow until the swale reduces in width downstream to channelized flow. The ultimate outfall location is East Cherry Creek approximately 1.5 miles east of the Site.

There are no major drainageways or existing facilities on the Site.

The Site lies within the East Cherry Creek Drainage Basin according to the El Paso County Drainage Basins map. There are no known non-stormwater discharges that contribute to the storm water systems on site and downstream, both private and public.

The project site does not lie within a designated floodplain according to information published in the Federal Emergency Management Agency Floodplain Map No. 08041C0305G, dated December 7, 2018. The FEMA FIRM panel is provided in Appendix B.

The existing percent imperviousness of the Site is less than 0.1% as evidence by aerial photography and site visits. The only non-vegetation land is a dirt path within a common access easement at the north of the Site. The existing vegetative cover of the Site is approximately 99.9% with sparse native grasses and weeds, also as evidence by aerial photography and site visits.

3) PROPOSED DEVELOPMENT

The proposed project scope is for a small subdivision for a total of six lots with a public 60' width right-of-way extension for the roadway of Mariah Trail. A Final Plat and Major Development Plan show Lots 1 through 6 with minimum areas of 5 acres to meet RR-5 rural residential zoning standards. A 32' width gravel surface roadway is proposed as an extension of Mariah Trail with a cul-de-sac at the termination point of the proposed right-of-way for an emergency vehicle turnaround. The typical section of the roadway follows County Standard Detail SD-2-10, a 32' width gravel section with a 4% crown with roadside swales of minimum 2' depth within the 60' right-of-way section and an additional 5' of public improvement easement on each side.

The small subdivision is to remain zoned as RR-5, allowing for single-family residences and accessory structures within the El Paso County zoning code's allowed land uses. Covenants for the Mariah Trail Filing No. 1 subdivision shall meet El Paso County land use and development standards at a minimum with the following minimum criteria per the County:

- Minimum 200' width lot frontage
- 25' front, side, and rear principal building setbacks
- 25% maximum coverage
- 7% Imperviousness (Table 3-1, Appendix L)

Proposed construction activity for the major subdivision is for the Mariah Trail right-of-way extension of the gravel roadway section and roadside ditch. Future developed lots are to connect to the gravel roadway with future driveways and 18" CMP culvert pipes within the roadside ditches. No driveway connections or culverts are proposed at this time.

The limits of disturbance and construction is to establish the roadway is approximately 5.0 acres or 11.4% of the total Site area. The interim developed condition is the initial roadway buildout of a gravel section with roadside ditches. Further interim conditions are to include driveways and culvert pipes from the roadway and lot development of single-family residences. The ultimate developed condition consists of a full build out of Lots 1 through 6 with single-family residences, driveways, hardscape, accessory structures, etc. to an assumed percent imperviousness of 7% per for the six lots per El Paso County criteria (Table 3-1, Appendix L). The total imperviousness of the Site is 8.82% for the ultimate developed condition which includes full development of all lots and the roadway.

This Drainage Letter demonstrates that Water Quality is met via the grass buffers of the large acre lots prior to exiting the Site within the concentrated swale area to the east. Runoff Reduction calculations are provided within the Appendix. While disturbance is over once acre for construction of the road, detention is not required for this rural major subdivision due to runoff reduction and infiltration within the site and a stabilized outfall exiting the site. There is no increase or decrease in flows on the site from existing to proposed. A natural drainage swale exists on the eastern boundary that conveys stormwater due east toward the East Cherry Creek. This natural swale is not a formal drainageway and is a part of the existing topography of the Site. Appendix calculations show a cross section of the existing swale with calculations for stormwater velocities during the major and minor storm events.

The construction timeline is anticipated to commence following the Subdivision Plat,

Entitlements, and Construction Drawings processes with the County anticipated to be August 2023. Construction of the roadway is anticipated to take two months with final stabilization occurring in November of 2023. Erosion and sediment control measures for the Site are to be established prior to any disturbance or construction activity as required by the County and per the GEC Plan Set and Stormwater Management Report.

a) **PROPOSED DRAINAGE CONDITIONS**

The final drainage pattern of the ultimate buildout of the small subdivision generally follows the existing conditions by sheet flowing west to east and flowing to the concentrated swale within the central east area of the Site. The difference between existing patterns and developed is that a gravel roadway will capture upstream (west) runoff in its swale and convey it to a culvert pipe at the low point of the roadway which will flow due east to a level spreader so that the stormwater will continue due east via overland sheet flow.

Unresolved from Submittal 1 - Discuss use of Exclusion in ECM App I.7.1.B.5. Note about that exclusion: Per direction from the State, subdivision developments that include impervious pavement roads do not qualify for Exclusion E (Large Lot Single-Family Site) on the PBMP form for soil disturbances associated with the construction of those roadway areas. Therefore, a permanent WQ facility should be designed to treat runoff from the impervious roadway area and the subsequent grading like roadside ditches (but only if the total area of soil disturbance is >1ac). A driveway that feeds and crosses multiple lots counts toward roadway impervious area. But individual driveways for individual lots counts towards the impervious area for the large single-family lot.

There is no expected increases in stormwater runoff due to impervious areas. Impervious areas are treated for water quality via grass buffers as is expected in rural settings with large areas of undeveloped land. The gravel roadway extension experiences 100% water quality runoff reduction via grass buffers as shown in the Appendix calculations (UD-BMP).

There are no stream crossings located within the construction site boundary. The lots are not within a streamside boundary and there are no preservation easements or existing no-build areas on or within the vicinity of construction/disturbance. There are no anticipated negative impacts to surrounding or downstream developments or infrastructure as a result of development of this small subdivision.

The downstream outfall location of the site is along the east property boundary where a natural grasslined swale is located per existing topography. The major storm event does not have excessive stormwater velocities that would scour the natural swale and therefore is deemed stabilized.

The proposed conditions narrative identify that there is an increase. Revise statement accordingly.

4) DRAINAGE BASINS AND SUB-BASINS

a) EXISTING MAJOR DRAINAGE BASIN AND SUB-BASINS

Basin E1 (1.85 ac. ; $Q_5 = 0.58$ cfs, $Q_{100} = 4.23$ cfs) is a sub-basin within the northwest corner of the Site that consists of undeveloped area with native grasses and open meadow/pasture. The drainage pattern of the sub-basin consist of overland sheet flow due northwest directed offsite to **Design Point 1**. There are no significant natural features or storm infrastructure that capture or convey the runoff and the stormwater continues due north offsite.

Basin E2 (28.42 ac. ; $Q_5 = 8.84$ cfs, $Q_{100} = 64.91$ cfs) is the sub-basin that consists of most of the undeveloped Site. The vast majority of the area consist of native grass and open meadow/pasture and the topography has natural grasslined swales that convey stormwater runoff due east toward the Site's outfall point at **Design Point 2**. There is existing fenceline and dirt trail within an existing access easement at the northeast area of the sub-basin. Most of the stormwater runoff is overland sheet flow and is concentrated within the existing natural grass swales that flow along the east property boundary. The outfall point at **Design Point 2** is not a formal channel or drainage way and continues due east until it ultimately outfalling at the East Cherry Creek.

Basin E3 (0.83 ac. ; $Q_5 = 0.26$ cfs, $Q_{100} = 1.90$ cfs) is a sub-basin within the southwest corner of the Site that consists of undeveloped area with native grasses and open meadow/pasture. The drainage pattern of the sub-basin consist of overland sheet flow due southeast directed offsite to **Design Point 3**. There are no significant natural features or storm infrastructure that capture or convey the runoff and the stormwater continues due southeast offsite toward East Cherry Creek.

- RPA/SPA limits must be shown on GEC Plans (not just FDR) so our SW inspectors and the QSM know that these areas are to remain pervious and vegetated. Our SW inspectors do not look at drainage reports.

Unresolved from Submittal 1-Additional Runoff Reduction notes/requirements:

⁻ The runoff reduction RPA is considered a WQ Facility and requires a signed Maintenance Agreement

⁻ All RPA/SPA areas will need to be within a no build/drainage easement (or tract) and discussed in the maintenance agreement and O&M manual. - For O&M Manual, see City's O&M for Grass Buffers / Grass Swales on their website:

https://coloradosprings.gov/stormwater-enterprise/page/operations-and-maintenance-permanent-bmps?mlid=6126

Provide a detail for the UIA:RPA interface that shows the recommended vertical drop of 4".

Basin E4 (3.90 ac. ; $Q_5 = 1.21 \text{ cfs}$, $Q_{100} = 8.91 \text{ cfs}$) is a sub-basin within the northeast corner of the Site that consists of undeveloped area with native grasses, open meadow/pasture, and a dirt pathway within an existing access easement. The drainage pattern of the sub-basin consist of overland sheet flow due northeast directed offsite to **Design Point 4**. There are no significant natural features or storm infrastructure that capture or convey the runoff and the stormwater continues due east offsite toward East Cherry Creek.

Basin OS1 (0.64 ac. ; $Q_5 = 0.20$ cfs, $Q_{100} = 1.46$ cfs) is a relatively small sub-basin located off-site adjacent to the west property boundary of the Site. The stormwater runoff from this sub-basin contributes to sub-basin E2 and Design Point 2. There is a high point west of the Site that flows in all directions and this sub-basins drainage pattern is directed west through the Site via overland sheet flow. The area consist of native grasses and open meadow/pasture. The offsite basin is split into these two off-site sub-basins to be consistent with the developed conditions hydrology map's design points.

Basin OS2 (0.29 ac. ; $Q_5 = 0.09$ cfs, $Q_{100} = 0.66$ cfs) is a relatively small sub-basin located off-site adjacent to the west property boundary of the Site. The stormwater runoff from this sub-basin contributes to sub-basin E2 and Design Point 2. There is a high point west of the Site that flows in all directions and this sub-basins drainage pattern is directed west through the Site via overland sheet flow. The area consist of native grasses and open meadow/pasture. The offsite basin is split into these two off-site sub-basins to be consistent with the developed conditions hydrology map's design points.

The total stormwater runoff for the existing conditions of the Site is 11.17 cfs for the minor (5year) storm event and 82.06 cfs for the major (100-year) storm event which includes offsite contributions.

The offsite stormwater runoff contribution to and through the Site is 0.29 cfs for the minor (5year) storm event and 2.12 cfs for the major (100-year) storm event.

The notable outfall point for the Site is **Design Point 2**, a grasslined swale that conveys stormwater runoff due east offsite toward East Cherry Creek. The existing conditions for the undeveloped Site contribute 9.13 cfs for the minor (5-year) storm event and 67.03 cfs for the major (100-year) storm event at this design point, including offsite contributions.

b) Developed Major Drainage Basin and Sub-basins

Basin D1 (1.85 ac. ; $Q_5 = 0.58$ cfs, $Q_{100} = 4.23$ cfs) is the sub-basin that corresponds to the Existing Conditions Hydrology Map's sub-basin E1. There are no changes to this sub-basin from existing undeveloped conditions because it is assumed that any Lot 1 development occurs within subbasin D2 to conservatively account for stormwater runoff to the developed roadway's ditch and culvert pipe. The sub-basin is within the northwest corner of the Site that consists of undeveloped area with native grasses and open meadow/pasture. The drainage pattern of the sub-basin consist of overland sheet flow due northwest directed offsite to **Design Point 1**. There are no significant natural features or storm infrastructure that capture or convey the runoff and the stormwater continues due north offsite.

Basin D2 (9.48 ac. ; $Q_5 = 5.65$ cfs, $Q_{100} = 24.83$ cfs) is a sub-basin on the west side of the developed gravel roadway, the extended Mariah Trail. The sub-basin consists of developed lots 1 and 2 with an assumed imperviousness of 7 percent. Undeveloped areas within the minimum 5-acre lots are assumed to remain meadow/pasture areas of native grasses. It also consists of the west side of the developed gravel roadway and it's roadside ditch that has a low point where a proposed 18" CMP culvert pipe is located to flow under the roadway from west to east, at Design Point 5. The concentrated stormwater runoff from the culvert pipe continues east to Design Point 2, the existing grasslined swale that conveys most of the Site's stormwater runoff due east toward East Cherry Creek.

Basin D3 (0.83 ac. ; $Q_5 = 0.26$ cfs, $Q_{100} = 1.90$ cfs) is a sub-basin that corresponds to the Existing Conditions Hydrology Map's sub-basin E3. There are no changes to this sub-basin from existing undeveloped conditions because it is assumed that any Lot 3 development occurs within subbasin E4. The sub-basin is located within the southwest corner of the Site that consists of undeveloped area with native grasses and open meadow/pasture. The drainage pattern of the sub-basin consist of overland sheet flow due southeast directed offsite to **Design Point 3**. There are no significant natural features or storm infrastructure that capture or convey the runoff and the stormwater continues due southeast offsite toward East Cherry Creek.

Basin D4 (18.02 ac. ; $Q_5 = 9.66$ cfs, $Q_{100} = 45.97$ cfs) is a sub-basin that encompasses the south and east areas of the Site with developed lots 3, 4, 5, and 6 with an assumed imperviousness of 7 percent. The sub-basin includes existing fenceline and some dirt trail within the existing access easement to the north of the Site. Undeveloped areas within the minimum 5-acre lots are assumed to remain meadow/pasture areas of native grasses. The sub-basin consists of overland sheet flow from the developed RR-5 lots toward existing natural topographic grasslined swales along the east property boundary that flow to **Design Point 2** which conveys stormwater runoff due east offsite toward East Cherry Creek.

Basin D5 (0.92 ac. ; $Q_5 = 1.13$ cfs, $Q_{100} = 3.07$ cfs) is a sub-basin that consists solely of the east side of the developed gravel roadway and roadside ditch. The sub-basin is delineated in order to model the capacity of the roadside ditch on the east side of the extended Mariah Trail roadway. The subbasin consists of overland sheet flow from the developed gravel roadway into its east ditch where it is concentrated to a low point near the proposed 18" CMP culvert pipe outlet point where the ditch outfalls along the lot line between lots 4 and 5. The stormwater runoff continues east to **Design Point 2** which conveys stormwater runoff due east offsite toward East Cherry Creek.

Basin D6 (3.90 ac. ; $Q_5 = 1.21$ cfs, $Q_{100} = 8.91$ cfs) is the sub-basin that corresponds to Existing Conditions Hydrology Map's sub-basin E4. There are no changes to this sub-basin from existing

undeveloped conditions because it is assumed that any Lot 6 development occurs within subbasin D4 to conservatively account for stormwater runoff toward **Design Point 2**. It is the subbasin within the northeast corner of the Site that consists of undeveloped area with native grasses, open meadow/pasture, and a dirt pathway within an existing access easement. The drainage pattern of the sub-basin consist of overland sheet flow due northeast directed offsite to **Design Point 4**. There are no significant natural features or storm infrastructure that capture or convey the runoff and the stormwater continues due east offsite toward East Cherry Creek.

Basin OS1 (0.64 ac. ; $Q_5 = 0.20$ cfs, $Q_{100} = 1.46$ cfs) is the sub-basin that corresponds to Existing Conditions Hydrology Map sub-basin OS1 and is unchanged from existing conditions. It is a relatively small sub-basin located off-site adjacent to the west property boundary of the Site. The stormwater runoff from this sub-basin contributes to sub-basin **D2** and **Design Point 5**. There is a high point west of the Site that flows in all directions and this sub-basins drainage pattern is directed west through the Site via overland sheet flow. The area consist of native grasses and open meadow/pasture.

Basin OS2 (0.29 ac. ; $Q_5 = 0.09$ cfs, $Q_{100} = 0.66$ cfs) is the sub-basin that corresponds to Existing Conditions Hydrology Map sub-basin OS1 and is unchanged from existing conditions. It is a relatively small sub-basin located off-site adjacent to the west property boundary of the Site. The stormwater runoff from this sub-basin contributes to sub-basin **D4** and **Design Point 2**. There is a high point west of the Site that flows in all directions and this sub-basins drainage pattern is directed west through the Site via overland sheet flow. The area consist of native grasses and open meadow/pasture.

The total stormwater runoff for the existing conditions of the Site is 18.77 cfs for the minor (5year) storm event and 91.03 cfs for the major (100-year) storm event which includes offsite contributions. This is an increase of 7.6 cfs for the minor storm event and 8.97 cfs for the major storm event compared to existing undeveloped conditions. This is considered a relatively major increase in stormwater runoff due to development for a 35 acre onsite area with 0.93 acre offsite

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area. How is this major increase of 7.6 cfs and 8.97 cfs addressed?
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The offsite stormwater runoff contribution to and through the Site remains 0.29 cfs for the minor (5-year) storm event and 2.12 cfs for the major (100-year) storm event.

The notable outfall point for the Site is **Design Point 2**, a grasslined swale that conveys stormwater runoff due east offsite toward East Cherry Creek. The developed conditions for the Site contribute 16.72 cfs for the minor (5-year) storm event and 76.00 cfs for the major (100year) storm event at this design point, including offsite contributions.

Another notable design point is **Design Point 5** which is the location of the proposed 18" CMP culvert pipe that conveys stormwater runoff from basins **D2 and OS1** east under the gravel roadway toward **Design Point 2**. The culvert pipe is to be sized for the major storm event which experiences 26.30 cfs. The emergency overflow condition of **Design Point 5** consists of pooling

The total site flows do increase.

within roadside ditch until overtopping the centerline of the roadway which is 2.64 feet above the culvert's inflow invert. There is no increase or decrease in flows from existing to proposed

conditions located on the site. Overtopping of the roadwa toward Design Point 2. The emergency overflow condition impacts to onsite development of the lots nor downstream The analysis indicates that

protection is required. EAM STORM INFRASTRUCTURE EVALUATION Please revise the narrative accordingly to reflect what is rainage reports on file with El Paso Co

Review 1 comment: See DCM 6-4 for overtopping requirements for rural roads. Update culvert analysis to include overtopping depth. Staff recommends HY-8 is used. Size culvert accordingly.

Review 2: Unresolved. Narrative indicates that the culvert is sized for the major storm. needed/proposed ins that account for this property as an offsite ba provide analysis of the culvert for the major conditions of the Site remaining within the typical residentic (100yr) storm. Please indicate in the text will be no negative impacts to surrounding and downstream whether or not the over topping criteria in DCMV1 CH6 is met. Additionally, provide assessment of the existing natural drainage way on the east report to demonstrate that the outfall of the major subdivanalysis of the protection required at the culvert outfall. outfall that does not require detention or structural of stormwater runoff or provide additional energy dissipation.

Review 1 comment: Per ECM 3.2.4 a suitable outfall is required for developed flows. Flows at this outfall increase by over 10% with development. Discuss in a narrative whether detention will be required based on the increase of the flows since the are not negligible at this moment. Provide an analysis of the outfall and determine whether any protection improvements are necessary.

Review 2: Unresolved. No additional discussion has been added to the narrative regarding how the increase of flows are mitigated. Please address the previous comment.

Step 1 – Reducing Runoff Volumes: Low impact development (LID) practices are utilized to reduce runoff at the source. In general, stormwater discharges are routed across pervious areas prior to capture in storm sewer. This practice promotes infiltration and reduces peak runoff rates. The Runoff Reduction Factor method was used and is presented in Appendix B.

Step 2 – Stabilize Drainageways: No onsite full-spectrum detention is proposed and therefore developers will employ runoff reduction measures to achieve water quality treatment.

Step 3 – Provide WQCV: Runoff from this development is treated through capture and slow release of the WQCV via detention ponds that are designed per current El Paso County DCM V2.

Step 4 – Consider the need for industrial and Commercial BMP's: No industrial or commercial uses are proposed within this development and therefore no source controls are proposed.

V. SUMMARY

The hydrology calculations presented in Appendix E and F quantify stormwater runoff and the existing and developed hydrology maps presented in Appendix G visually present stormwater runoff drainage patterns for the Site and offsite areas. The developed conditions show the Please revise report for consistency. Previous sections state there is no increase in runoff or there is a minor increase.

Additionally, page 7 indicates that there is a

major increased vided lots and the hydrology calculations and map quantify the developed roadway and each lot's runoff contribution to their respective design points. There is no alteration to the general drainage pattern of the Site and the proposed construction to the Site yields a minor increase to the total stormwater runoff from the onsite 35 acres and offsite 0.93 acres. It is anticipated that there will be no negative impacts to surrounding and downstream developments and infrastructure.

A. COMPLIANCE WITH STANDARDS

The criteria used to design the storm water runoff volumes are formulas and figures within the El Paso County Engineering Criteria Manual, the El Paso County Drainage Criteria Manual, the City of Colorado Springs Drainage Manuals (DCM) Volumes 1 and 2. Tables 6-6 and Appendix L Table 3-1 of the EPC DCM was used for runoff coefficients for the Rational Method.

Appendix calculations show drainage way section calculations using Bentley's Flowmaster software. Water Quality Capture Volume is provided for the developed gravel roadway and developed lots via grass buffers of the naturally vegetated meadow/pasture areas of the Site, as shown in the Appendix with UD-BMP Runoff Reduction calculations. No onsite stormwater detention is required as the major subdivision consists of relatively major imperviousness resulting in a relatively small increase to the stormwater runoff from the Site which is shown to have a stable outfall with capacity for the developed condition.

B. DRAINAGE BASIN AND BRIDGE FEES

The Site is located within the East Cherry Creek drainage basin which does not have a drainage basin fee listed within the 2023 El Paso County Drainage, Bridge, and Pond Fee Schedule. All outstanding County fees are to be paid at the time of platting.

VI. **REFERENCES**

El Paso County Engineering Criteria Manual, latest revision October 14, 2020

El Paso County Drainage Criteria Manual, latest revision October 31, 2018

City of Colorado Springs Drainage Manual Volumes I & II (May 2014, Revised January 2021)

Mile High Flood District Drainage Criteria Manual, Volume I (January 2016)

FEMA Flood Map Service Center

United States Department of Agriculture National Resources Conservation Service

Appendix A: Vicinity Map

VICINITY MAP MARIAH TRAIL FILING NO. 1 A PORTION OF THE NORTHWEST QUARTER OF SECTION 7, TOWNSHIP 11 SOUTH, RANGE 65 WEST, OF THE SIXTH PRINCIPAL MERIDIAN, EL PASO COUNTY, COLORADO



Appendix B: FEMA Floodplain Map

DWL RODO O RRG EDUGIZHU)51WWH

Fix heading and footer

HHQG

FEMA



% DHES 86 DWL RODO DS 20 WKRLEHU DWDUHUHKHG 28 WREHU

Appendix C: NRCS Soils Map

Hydrologic Soil Group—El Paso County Area, Colorado (Mariah Trail Filing No. 1 - Hydrologic Soils Map)



USDA Natural Resources Conservation Service Web Soil Survey National Cooperative Soil Survey





Hydrologic Soil Group

| Map unit symbol | Map unit name | Rating | Acres in AOI | Percent of AOI |
|---------------------------|---|--------|--------------|----------------|
| 15 | Brussett loam, 3 to 5 percent slopes | В | 44.8 | 50.6% |
| 69 | Peyton-Pring complex, 8 to 15 percent slopes | В | 43.7 | 49.4% |
| Totals for Area of Intere | st | 88.5 | 100.0% | |

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

Rating Options

Aggregation Method: Dominant Condition

USDA

Component Percent Cutoff: None Specified Tie-break Rule: Higher



Appendix D: Hydrology Calculations

| Project: | Mariah Trail Filing No. 1 |
|-----------|---------------------------------------|
| Engineer: | Carlos Serrano |
| Date: | 3/16/2023 |
| Address: | Mariah Trail El Paso County, Colorado |

CONDITION: EXISTING

Lot 1 Imperviousness Lot 2 Imperviousness

2452 3753.85 0.353926097 0.49890264 0.68115587

| Sub-Basin: | E1 | (IDF Curve Equations from Figure 6-5 of the DCM | | | | | | | | |
|--------------------------|----------------|---|-----------------|-----------------|------------------|--|--|--|--|--|
| t _t Duration: | 11.75 | Volume 1) | | | | | | | | |
| I ₂ | I ₅ | I ₁₀ | I ₂₅ | I ₅₀ | I ₁₀₀ | | | | | |
| 3.102718495 | 3.886846842 | 4.5348213 | 5.1827958 | 5.8307703 | 6.5254627 | | | | | |

Hydrologic Soil Type: B

| Coefficient (Table 6-6) | | | | | | | | | | | | | | | | | | |
|---------------------------------------|-------------|---------|---------------|---------------|----------------|----------------|----------------|-----------------|--|----------------------|-----------------------|---|-----------------------|------------------------|---------------------|---------------------|-------------|----------------------|
| Land Use or Surface Characteristic | Square Feet | Acreage | Coefficient 2 | Coefficient 5 | Coefficient 10 | Coefficient 25 | Coefficient 50 | Coefficient 100 | <u>2 Yr: C_i * A_i</u> | <u>5 Yr: C; * A;</u> | <u>10 Yr: C, * A,</u> | <u>25 Yr: C_i * A_i</u> | <u>50 Yr: C, * A,</u> | <u>100 Yr: C, * A,</u> | 2 Yr C _c | 5 Yr C _c | 10 Yr C_c | 25 Yr C _c |
| Roof + Hardscape | - | 0.000 | 0.71 | 0.73 | 0.75 | 0.78 | 0.80 | 0.81 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.020 | 0.080 | 0.150 | 0.250 |
| Gravel Roadway | - | 0.000 | 0.57 | 0.59 | 0.63 | 0.66 | 0.68 | 0.70 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | | | | |
| Pasture/Meadow | 80,586 | 1.850 | 0.02 | 0.08 | 0.15 | 0.25 | 0.30 | 0.35 | 0.037 | 0.148 | 0.278 | 0.463 | 0.555 | 0.648 | | | | |
| | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | |
| A _t : | 80,586 | 1.850 | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | |

| Sub-Basin: | E2 | (IDF Curve Equations from Figure 6-5 of the DCM | | | | | | | | |
|--------------------------|----------------|---|-----------------|-----------------|------------------|--|--|--|--|--|
| t _t Duration: | 17.57 | | Volur | ne 1) | | | | | | |
| I ₂ | I ₅ | I ₁₀ | I ₂₅ | I ₅₀ | I ₁₀₀ | | | | | |
| 2.62407407 | 3.283513534 | 3.8309325 | 4.3783514 | 4.9257703 | 5.5118627 | | | | | |

| r C _c 25 Yr C |
|--------------------------|
| 50 0.250 |
| |
| |
| |
| |
| |
| |
| |
| D Yr |

| Sub-Basin: | E3 | (IDF Curve Equations from Figure 6-5 of the DCM | | | | | | | | | |
|--------------------------|----------------|---|-----------------|-----------------|------------------|--|--|--|--|--|--|
| t _t Duration: | 9.31 | Volume 1) | | | | | | | | | |
| I ₂ | I ₅ | I ₁₀ | I ₂₅ | I ₅₀ | I ₁₀₀ | | | | | | |
| 3.379920008 | 4.236260515 | 4.9424706 | 5.6486807 | 6.3548908 | 7.1124777 | | | | | | |

Hydrologic Soil Type: B

Hydrologic Soil Type: B

| Coefficient (Table 6-6) | | | | | | | | | | | | | | | | | | |
|---------------------------------------|-------------|---------|---------------|---------------|----------------|----------------|----------------|-----------------|--|----------------------|---|---|-----------------------|------------------------|---------------------|---------------------|-------------------|-------|
| Land Use or Surface Characteristic | Square Feet | Acreage | Coefficient 2 | Coefficient s | Coefficient 10 | Coefficient 25 | Coefficient 50 | Coefficient 100 | <u>2 Yr: C_i * A_i</u> | <u>5 Yr: C; * A;</u> | <u>10 Yr: C_i * A_i</u> | <u>25 Yr: C_i * A_i</u> | <u>50 Yr: C, * A,</u> | <u>100 Yr: C, * A,</u> | 2 Yr C _c | 5 Yr C _c | 10 Yr $C_{\rm c}$ | 25 Yı |
| Roof + Hardscape | - | 0.000 | 0.71 | 0.73 | 0.75 | 0.78 | 0.80 | 0.81 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.020 | 0.080 | 0.150 | 0.25 |
| Gravel Roadway | - | 0.000 | 0.57 | 0.59 | 0.63 | 0.66 | 0.68 | 0.70 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | | | | |
| Pasture/Meadow | 36,155 | 0.830 | 0.02 | 0.08 | 0.15 | 0.25 | 0.30 | 0.35 | 0.017 | 0.066 | 0.125 | 0.208 | 0.249 | 0.291 | | | | |
| | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | |
| A _t : | 36,155 | 0.830 | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | |

| | Coefficient (Table 6-6) | | | | | | | | | | | | | | | | | | | |
|---------------------------------------|-------------------------|---------|---------------|----------------------|----------------|----------------|----------------|-----------------|--|----------------------|-----------------------|---|-----------------------|------------------------|---------------------|---------------------|-------------|----------------------|----------------------|-----------------------|
| Land Use or Surface Characteristic | Square Feet | Acreage | Coefficient 2 | <u>Coefficient s</u> | Coefficient 10 | Coefficient 25 | Coefficient 50 | Coefficient 100 | <u>2 Yr: C_i * A_i</u> | <u>5 Yr: C, * A,</u> | <u>10 Yr: C, * A,</u> | <u>25 Yr: C_i * A_i</u> | <u>50 Yr: C, * A,</u> | <u>100 Yr: C, * A,</u> | 2 Yr C _c | 5 Yr C _c | 10 Yr C_c | 25 Yr C _c | 50 Yr C _c | 100 Yr C _c |
| Roof + Hardscape | - | 0.000 | 0.71 | 0.73 | 0.75 | 0.78 | 0.80 | 0.81 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.020 | 0.080 | 0.150 | 0.250 | 0.300 | 0.350 |
| Gravel Roadway | - | 0.000 | 0.57 | 0.59 | 0.63 | 0.66 | 0.68 | 0.70 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | | | | | | |
| Pasture/Meadow | 169,884 | 3.900 | 0.02 | 0.08 | 0.15 | 0.25 | 0.30 | 0.35 | 0.078 | 0.312 | 0.585 | 0.975 | 1.170 | 1.365 | | | | | | |
| | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | |
| A _t : | 169,884 | 3.900 | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | |

| Sub-Basin: | OS1 | (IDF Curve Equations from Figure 6-5 of the DCM | | | | | | | |
|--------------------------|----------------|---|-----------------|-----------------|------------------|--|--|--|--|
| t _t Duration: | 13.19 | 19 Volume 1) | | | | | | | |
| I ₂ | I ₅ | I ₁₀ | I ₂₅ | I ₅₀ | I ₁₀₀ | | | | |
| 2.965055019 | 3.713321453 | 4.332375 | 4.9514286 | 5.5704822 | 6.23394 | | | | |

| Hydrologic Soil Type: | В |
|-----------------------|---|

| | Coefficient (Table 6-6) | | | | | | | | | | | | | | | | | | | |
|---------------------------------------|-------------------------|---------|---------------|---------------|----------------|----------------|----------------|-----------------|----------------------|----------------------|-----------------------|---|----------------------------------|------------------------|---------------------|---------------------|----------------------|----------------------|----------------------|-----------------------|
| Land Use or Surface Characteristic | Square Feet | Acreage | Coefficient 2 | Coefficient 5 | Coefficient 10 | Coefficient 25 | Coefficient 50 | Coefficient 100 | <u>2 Yr: C, * A,</u> | <u>5 Yr: C, * A,</u> | <u>10 Yr: C, * A,</u> | <u>25 Yr: C_i * A_i</u> | <u>50 Yr: C_i * Ai</u> | <u>100 Yr: C, * A,</u> | 2 Yr C _c | 5 Yr C _c | 10 Yr C _c | 25 Yr C _c | 50 Yr C _c | 100 Yr C _c |
| Roof + Hardscape | - | 0.000 | 0.71 | 0.73 | 0.75 | 0.78 | 0.80 | 0.81 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.020 | 0.080 | 0.150 | 0.250 | 0.300 | 0.350 |
| Gravel Roadway | - | 0.000 | 0.57 | 0.59 | 0.63 | 0.66 | 0.68 | 0.70 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | | | | | | |
| Pasture/Meadow | 27,878 | 0.640 | 0.02 | 0.08 | 0.15 | 0.25 | 0.30 | 0.35 | 0.013 | 0.051 | 0.096 | 0.160 | 0.192 | 0.224 | | | | | | |
| | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | |
| A _t : | 27,878 | 0.640 | | | | | | | | | | | | | | | | | | |

| : | E4 | (IDF Curve | (IDF Curve Equations from Figure 6-5 of the DCM | | | | | | |
|----------------|----------------|-----------------|---|-----------------|------------------|--|---|--|--|
| n: | 10.97 | | Volur | ne 1) | | | | | |
| l ₂ | I ₅ | I ₁₀ | I ₂₅ | I ₅₀ | I ₁₀₀ | | Ŀ | | |
| 3.184258474 | 3.989628328 | 4.654733 | 5.3198378 | 5.9849425 | 6.6981356 | | | | |
| | | | | | | | | | |
| | | | | | | | | | |

| Sub-Basin: | E4 | (IDF Curve | Equations fr |
|--------------------------|-------|------------|--------------|
| t _t Duration: | 10.97 | | Volu |
| h | le . | ha | lar. |

| I ₂ | I ₅ | 1 ₁₀ | 1 ₂₅ | 1 ₅₀ | |
|----------------|----------------|-----------------|-----------------|-----------------|-----|
| 3.184258474 | 3.989628328 | 4.654733 | 5.3198378 | 5.9849425 | 6.6 |
| | | | | | |

Hydrologic Soil Type: B

| 50 Yr C _c | 100 Yr C _c |
|----------------------|-----------------------|
| 0.300 | 0.350 |

| Q Peak Flow (cfs) | | | | | | | | | |
|-------------------|----------|-----------|-----------|-----------|------------|--|--|--|--|
| 2 Year Q | 5 Year Q | 10 Year Q | 25 Year Q | 50 Year Q | 100 Year Q | | | | |
| 0.11 | 0.58 | 1.26 | 2.40 | 3.24 | 4.23 | | | | |



| Q Peak Flow (cfs) | | | | | | | | | | | |
|-------------------|----------|-----------|-----------|-----------|------------|--|--|--|--|--|--|
| 2 Year Q | 5 Year Q | 10 Year Q | 25 Year Q | 50 Year Q | 100 Year Q | | | | | | |
| 1.76 | 8.84 | 19.33 | 36.82 | 49.71 | 64.91 | | | | | | |

| Yr C _c 50 Yr C _c 100 Yr C _c | 250 | 0.500 | 0.550 |
|--|-------------------|----------------------|-----------------------|
| Yr C _c 50 Yr C _c 100 Yr C _c | 250 | 0 200 | 0.250 |
| | Yr C _c | 50 Yr C _c | 100 Yr C _c |

| Q Peak Flow (cfs) | | | | | | | | | | |
|-------------------|----------|-----------|-----------|-----------|------------|--|--|--|--|--|
| 2 Year Q | 5 Year Q | 10 Year Q | 25 Year Q | 50 Year Q | 100 Year Q | | | | | |
| 0.05 | 0.26 | 0.56 | 1.08 | 1.45 | 1.90 | | | | | |

| Q Peak Flow (cfs) | | | | | | | | |
|-------------------|----------|-----------|-----------|-----------|------------|--|--|--|
| 2 Year Q | 5 Year Q | 10 Year Q | 25 Year Q | 50 Year Q | 100 Year Q | | | |
| 0.24 | 1.21 | 2.65 | 5.05 | 6.82 | 8.91 | | | |

| Q Peak Flow (cfs) | | | | | | | | | |
|-------------------|----------|-----------|-----------|-----------|------------|--|--|--|--|
| | | | | | | | | | |
| 2 Year Q | 5 Year Q | 10 Year Q | 25 Year Q | 50 Year Q | 100 Year Q | | | | |
| 0.04 | 0.20 | 0.44 | 0.83 | 1.12 | 1.46 | | | | |

| Sub-Basin: | OS2 | (IDF Curve Equations from Figure 6-5 of the DCM | | | | | | | | |
|--------------------------|----------------|---|-----------------|-----------------|------------------|--|--|--|--|--|
| t _t Duration: | 12.06 | Volume 1) | | | | | | | | |
| I ₂ | I ₅ | I ₁₀ | I ₂₅ | I _{SO} | I ₁₀₀ | | | | | |
| 3.071843389 | 3.847928642 | 4.4894167 | 5.1309049 | 5.772393 | 6.4600801 | | | | | |

Hydrologic Soil Type: B

| | Basin Summary | | | | | | | | | | |
|---------------|---------------|------------|----------------|------------------|--|--|--|--|--|--|--|
| Basin Summary | Design Point | Area (ac.) | Q ₅ | Q ₁₀₀ | | | | | | | |
| E1 | 1 | 1.85 | 0.58 | 4.23 | | | | | | | |
| E2 | 2 | 28.42 | 8.84 | 64.91 | | | | | | | |
| E3 | 3 | 0.83 | 0.26 | 1.90 | | | | | | | |
| E4 | 4 | 3.90 | 1.21 | 8.91 | | | | | | | |
| OS1 | 2 | 0.64 | 0.20 | 1.46 | | | | | | | |
| OS2 | 2 | 0.29 | 0.09 | 0.66 | | | | | | | |
| TOTAL ONSITE | | 35.00 | 10.88 | 79.94 | | | | | | | |
| TOTAL OFFSITE | | 0.93 | 0.29 | 2.12 | | | | | | | |
| TOTALS | | 35.93 | 11.17 | 82.06 | | | | | | | |

| Cumulative Design Daint Summany | | | | | | | | |
|---------------------------------|---------------------------------|------------|-------|------------------|--|--|--|--|
| <u></u> | Cumulative Design Point Summary | | | | | | | |
| Design Point | Basins | Area (ac.) | Q5 | Q ₁₀₀ | | | | |
| 1 | E1 | 1.85 | 9.50 | 69.80 | | | | |
| 2 | E2, OS1, OS2 | 29.35 | 9.13 | 67.03 | | | | |
| 3 | E3 | 0.83 | 0.26 | 1.90 | | | | |
| 4 | E4 | 3.90 | 1.21 | 8.91 | | | | |
| TOTAL ONSITE | E1-E4 | 35.00 | 10.88 | 79.94 | | | | |
| TOTAL OFFSITE | OS1, OS2 | 0.93 | 0.29 | 2.12 | | | | |

| | Coefficient (Table 6-6) | | | | | | | | | | | | | | | | | | | |
|---------------------------------------|-------------------------|---------|---------------|----------------------|----------------|----------------|----------------|-----------------|----------------------|----------------------|-----------------------|-----------------------|----------------------------------|------------------------|---------------------|---------------------|----------------------|----------------------|----------------------|--------------|
| Land Use or Surface Characteristic | Square Feet | Acreage | Coefficient 2 | <u>Coefficient s</u> | Coefficient 10 | Coefficient 25 | Coefficient 50 | Coefficient 100 | <u>2 Yr: C; * A;</u> | <u>5 Yr: C; * A;</u> | <u>10 Yr: C; * A;</u> | <u>25 Yr: C; * A;</u> | <u>50 Yr: C_i * Ai</u> | <u>100 Yr: C; * A;</u> | 2 Yr C _c | 5 Yr C _c | 10 Yr C _c | 25 Yr C _c | 50 Yr C _c | 100 Yr C_c |
| Roof + Hardscape | - | 0.000 | 0.71 | 0.73 | 0.75 | 0.78 | 0.80 | 0.81 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.020 | 0.080 | 0.150 | 0.250 | 0.300 | 0.350 |
| Gravel Roadway | - | 0.000 | 0.57 | 0.59 | 0.63 | 0.66 | 0.68 | 0.70 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | | | | | | |
| Pasture/Meadow | 12,632 | 0.290 | 0.02 | 0.08 | 0.15 | 0.25 | 0.30 | 0.35 | 0.006 | 0.023 | 0.044 | 0.073 | 0.087 | 0.102 | | | | | | |
| | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | |
| A _t : | 12,632 | 0.290 | | | | | | | | | | | | | | | | | | |

| Q Peak Flow (cfs) | | | | | | | | |
|-------------------|----------|-----------|-----------|-----------|------------|--|--|--|
| 2 Year Q | 5 Year Q | 10 Year Q | 25 Year Q | 50 Year Q | 100 Year Q | | | |
| 0.02 | 0.09 | 0.20 | 0.38 | 0.51 | 0.66 | | | |

3.2.1 - Overland (Initial) Flow Time

$$t_i = \frac{0.395(1.1 - C_5)\sqrt{L}}{S^{0.33}}$$
(Eq. 6-8)

Where:

 t_i = overland (initial) flow time (min) C_5 = runoff coefficient for 5-year frequency (see Table 6-6) L = length of overland flow (300 ft <u>maximum</u> for non-urban land uses, 100 ft <u>maximum</u> for urban land uses)

S = average basin slope (ft/ft)

Note that in some urban watersheds, the overland flow time may be very small because flows quickly concentrate and channelize.

| Sub-Basin or DP: | E1 | |
|------------------|-------|--|
| C ₅ : | 0.08 | [Table 6-6. Runoff Coefficients for Rational Method] |
| L: | 100 | ft |
| S: | 0.039 | ft/ft |

Composite Runoff Coefficient Calculation:

 $C_{c} = (C_{1}A_{1} + C_{2}A_{2} + C_{3}A_{3} + \dots C_{i}A_{i}) / A_{t}$

| Square Feet | Acreage | C₅ | |
|-------------|---|---|--|
| - | 0.00 | 0.73 | |
| - | 0.00 | 0.59 | |
| 80,586 | 1.85 | 0.08 | |
| 80,586 | 1.85 | | |
| | Square Feet - - 80,586 80,586 | Square Feet Acreage - 0.00 - 0.00 80,586 1.85 80,586 1.85 | |

 $C_c = (0.08*1.85) / 1.85 =$

0.08

11.75

mins

 $t_i = (0.395*(1.1-C_5)*sqrt(L))/(S^{0.33})$

```
t_i = (0.395*(1.1-0.08)*sqrt(100))/(0.039^{0.33}) =
```

3.2.2 Travel Time

For catchments with overland and channelized flow, the time of concentration needs to be considered in combination with the travel time, t_i , which is calculated using the hydraulic properties of the swale, ditch, or channel. For preliminary work, the overland travel time, t_n can be estimated with the help of Figure 6-25 or Equation 6-9 (Guo 1999).

 $V = C_v S_w^{0.5}$

(Eq. 6-9)

Where:

V = velocity (ft/s)

 $C_v =$ conveyance coefficient (from Table 6-7)

 S_w = watercourse slope (ft/ft)



| Table 6-7. | Conveyance Coefficie | nt, C _v |
|------------|----------------------|--------------------|
| Type of | С, | |

| Heavy meadow | 2.5 | | |
|---|-----|--|--|
| Tillage/field | 5 | | |
| Riprap (not buried)* | 6.5 | | |
| Short pasture and lawns | 7 | | |
| Nearly bare ground | 10 | | |
| Grassed waterway | 15 | | |
| Paved areas and shallow paved swales | 20 | | |
| For buried riprap, select Cv value based on type of vegetative cover. | | | |

 $t_{c} = t_{i} + t_{t} =$

11.75 min.

3.2.4 Minimum Time of Concentration

If the calculations result in a t_c of less than 10 minutes for undeveloped conditions, it is recommended that a minimum value of 10 minutes be used. The minimum t_c for urbanized areas is 5 minutes.

Final t_c:

11.75 min.

3.2.1 - Overland (Initial) Flow Time

$$t_i = \frac{0.395(1.1 - C_5)\sqrt{L}}{S^{0.33}}$$
(Eq. 6-8)

Where:

 t_i = overland (initial) flow time (min) C_5 = runoff coefficient for 5-year frequency (see Table 6-6) L = length of overland flow (300 ft <u>maximum</u> for non-urban land uses, 100 ft <u>maximum</u> for urban land uses)

S = average basin slope (ft/ft)

Note that in some urban watersheds, the overland flow time may be very small because flows quickly concentrate and channelize.

| Sub-Basin or DP: | E2 |] |
|------------------|------|--|
| C ₅ : | 0.08 | [Table 6-6. Runoff Coefficients for Rational Method] |
| L: | 300 | ft |
| S: | 0.07 | ft/ft |

Composite Runoff Coefficient Calculation:

 $C_{c} = (C_{1}A_{1} + C_{2}A_{2} + C_{3}A_{3} + \dots C_{i}A_{i}) / A_{t}$

| Square Feet | Acreage | C₅ |
|-------------|--|---|
| - | 0.00 | 0.73 |
| - | 0.00 | 0.59 |
| 1,237,975 | 28.42 | 0.08 |
| 1,237,975 | 28.42 | |
| | Square Feet - 1,237,975 1,237,975 | Square Feet Acreage - 0.00 - 0.00 1,237,975 28.42 1,237,975 28.42 |

 $C_c = (0.08 * 28.42) / 28.42 =$

0.08

16.78

mins

 $t_i = (0.395*(1.1-C_5)*sqrt(L))/(S^{0.33})$

 $t_i = (0.395*(1.1-0.08)*sqrt(300))/(0.07^0.33) =$

3.2.2 Travel Time

For catchments with overland and channelized flow, the time of concentration needs to be considered in combination with the travel time, t_n , which is calculated using the hydraulic properties of the swale, ditch, or channel. For preliminary work, the overland travel time, t_n can be estimated with the help of Figure 6-25 or Equation 6-9 (Guo 1999).

 $V = C_v S_w^{-0.5}$

(Eq. 6-9)

Where:

V = velocity (ft/s)

 C_v = conveyance coefficient (from Table 6-7)

 S_w = watercourse slope (ft/ft)



| Table 6-7. Conveyance Coefficie | nt, C _v |
|---------------------------------|--------------------|
| Type of Land Surface | C, |

| - / / | ~, |
|---|------------------|
| Heavy meadow | 2.5 |
| Tillage/field | 5 |
| Riprap (not buried)* | 6.5 |
| Short pasture and lawns | 7 |
| Nearly bare ground | 10 |
| Grassed waterway | 15 |
| Paved areas and shallow paved swales | 20 |
| * For buried riprap, select Cv value based on type of v | egetative cover. |

 $t_{c} = t_{i} + t_{t} =$

17.57 min.

3.2.4 Minimum Time of Concentration

If the calculations result in a t_c of less than 10 minutes for undeveloped conditions, it is recommended that a minimum value of 10 minutes be used. The minimum t_c for urbanized areas is 5 minutes.

Final t_c:

17.57 min.

3.2.1 - Overland (Initial) Flow Time

$$t_i = \frac{0.395(1.1 - C_5)\sqrt{L}}{S^{0.33}}$$
(Eq. 6-8)

Where:

 t_i = overland (initial) flow time (min) C_5 = runoff coefficient for 5-year frequency (see Table 6-6) L = length of overland flow (300 ft <u>maximum</u> for non-urban land uses, 100 ft <u>maximum</u> for urban land uses)

S = average basin slope (ft/ft)

Note that in some urban watersheds, the overland flow time may be very small because flows quickly concentrate and channelize.

| Sub-Basin or DP: | E3 |] |
|------------------|-------|--|
| C ₅ : | 0.08 | [Table 6-6. Runoff Coefficients for Rational Method] |
| L: | 100 | ft |
| S: | 0.079 | ft/ft |

Composite Runoff Coefficient Calculation:

 $C_{c} = (C_{1}A_{1} + C_{2}A_{2} + C_{3}A_{3} + \dots + C_{i}A_{i})/A_{t}$

| Land Use or Surface Characteristic | Square Feet | Acreage | C ₅ |
|---------------------------------------|-------------|---------|----------------|
| Roof + Hardscape | - | 0.00 | 0.73 |
| Gravel Roadway | - | 0.00 | 0.59 |
| Pasture/Meadow | 36,155 | 0.83 | 0.08 |
| At : | 36,155 | 0.83 | |

 $C_c = (0.08*0.83) / 0.83 =$

0.08

mins

 $t_i = (0.395*(1.1-C_5)*sqrt(L))/(S^{0.33})$

```
t_i = (0.395*(1.1-0.08)*sqrt(100))/(0.079^{0.33}) =
                                                       9.31
```

3.2.2 Travel Time

For catchments with overland and channelized flow, the time of concentration needs to be considered in combination with the travel time, t_{is} , which is calculated using the hydraulic properties of the swale, ditch, or channel. For preliminary work, the overland travel time, t_{is} can be estimated with the help of Figure 6-25 or Equation 6-9 (Guo 1999).

 $V = C_v S_w^{-0.5}$

(Eq. 6-9)

Where:

V = velocity (ft/s)

 C_v = conveyance coefficient (from Table 6-7)

 S_w = watercourse slope (ft/ft)



| $\mathbf{t}_{\mathbf{c}} = \mathbf{t}_{\mathbf{i}} + \mathbf{t}_{\mathbf{t}} =$ | 9.31 | min. |
|---|------|------|

3.2.4 Minimum Time of Concentration

If the calculations result in a t_c of less than 10 minutes for undeveloped conditions, it is recommended that a minimum value of 10 minutes be used. The minimum t_c for urbanized areas is 5 minutes.

Final t_c:

9.31 min. Table 6-7. Conveyance Coefficient, C_v

| Type of Land Surface | C, |
|---|------------------|
| Heavy meadow | 2.5 |
| Tillage/field | 5 |
| Riprap (not buried)* | 6.5 |
| Short pasture and lawns | 7 |
| Nearly bare ground | 10 |
| Grassed waterway | 15 |
| Paved areas and shallow paved swales | 20 |
| For buried riprap, select Cv value based on type of v | egetative cover. |

3.2.1 - Overland (Initial) Flow Time

$$t_i = \frac{0.395(1.1 - C_5)\sqrt{L}}{S^{0.33}}$$
(Eq. 6-8)

Where:

 t_i = overland (initial) flow time (min) C_5 = runoff coefficient for 5-year frequency (see Table 6-6) L = length of overland flow (300 ft <u>maximum</u> for non-urban land uses, 100 ft <u>maximum</u> for urban land uses)

S = average basin slope (ft/ft)

Note that in some urban watersheds, the overland flow time may be very small because flows quickly concentrate and channelize.

| Sub-Basin or DP: | E4 |] |
|------------------|-------|--|
| C ₅ : | 0.08 | [Table 6-6. Runoff Coefficients for Rational Method] |
| L: | 100 | ft |
| S: | 0.048 | ft/ft |

Composite Runoff Coefficient Calculation:

 $C_{c} = (C_{1}A_{1} + C_{2}A_{2} + C_{3}A_{3} + \dots C_{i}A_{i}) / A_{t}$

| Land Use or Surface Characteristic | Square Feet | Acreage | C₅ |
|---------------------------------------|-------------|---------|------|
| Roof + Hardscape | - | 0.00 | 0.73 |
| Gravel Roadway | - | 0.00 | 0.59 |
| Pasture/Meadow | 169,884 | 3.90 | 0.08 |
| At : | 169,884 | 3.90 | |

 $C_c = (0.08 * 3.90) / 3.90 =$

0.08

mins

 $t_i = (0.395*(1.1-C_5)*sqrt(L))/(S^{0.33})$

 $t_i = (0.395*(1.1-0.08)*sqrt(100))/(0.048^{0.33}) =$ 10.97

3.2.2 Travel Time

For catchments with overland and channelized flow, the time of concentration needs to be considered in combination with the travel time, t_{is} , which is calculated using the hydraulic properties of the swale, ditch, or channel. For preliminary work, the overland travel time, t_{is} can be estimated with the help of Figure 6-25 or Equation 6-9 (Guo 1999).

 $V = C_v S_w^{-0.5}$

(Eq. 6-9)

Where:

V = velocity (ft/s)

 C_v = conveyance coefficient (from Table 6-7)

 S_w = watercourse slope (ft/ft)



| Table 6-7. Conveyance Coefficient, C_v | | |
|--|-----|--|
| Type of Land Surface | C, | |
| vy meadow | 2.5 | |

| Heavy meadow | 2.5 |
|--|-----------------|
| Tillage/field | 5 |
| Riprap (not buried)* | 6.5 |
| Short pasture and lawns | 7 |
| Nearly bare ground | 10 |
| Grassed waterway | 15 |
| Paved areas and shallow paved swales | 20 |
| For buried riprap, select Cv value based on type of ve | getative cover. |

 $t_{c} = t_{i} + t_{t} =$

10.97 min.

3.2.4 Minimum Time of Concentration

If the calculations result in a t_c of less than 10 minutes for undeveloped conditions, it is recommended that a minimum value of 10 minutes be used. The minimum t_c for urbanized areas is 5 minutes.

Final t_c:

10.97 min.

3.2.1 - Overland (Initial) Flow Time

$$t_i = \frac{0.395(1.1 - C_5)\sqrt{L}}{S^{0.33}}$$
(Eq. 6-8)

Where:

 t_i = overland (initial) flow time (min) C_5 = runoff coefficient for 5-year frequency (see Table 6-6) L = length of overland flow (300 ft <u>maximum</u> for non-urban land uses, 100 ft <u>maximum</u> for urban land uses)

S = average basin slope (ft/ft)

Note that in some urban watersheds, the overland flow time may be very small because flows quickly concentrate and channelize.

| Sub-Basin or DP: | OS1 |] |
|------------------|-------|--|
| C ₅ : | 0.08 | [Table 6-6. Runoff Coefficients for Rational Method] |
| L: | 70 | ft |
| S: | 0.016 | ft/ft |

Composite Runoff Coefficient Calculation:

 $C_{c} = (C_{1}A_{1} + C_{2}A_{2} + C_{3}A_{3} + \dots C_{i}A_{i}) / A_{t}$

| Land Use or Surface Characteristic | Square Feet | Acreage | C₅ |
|---------------------------------------|-------------|---------|------|
| Roof + Hardscape | - | 0.00 | 0.73 |
| Gravel Roadway | - | 0.00 | 0.59 |
| Pasture/Meadow | 27,878 | 0.64 | 0.08 |
| At : | 27,878 | 0.64 | |

 $C_c = (0.08 * 0.64) / 0.64 =$

0.08

mins

 $t_i = (0.395*(1.1-C_5)*sqrt(L))/(S^{0.33})$

```
t_i = (0.395*(1.1-0.08)*sqrt(70))/(0.016^{0.33}) =
                                                       13.19
```

3.2.2 Travel Time

For catchments with overland and channelized flow, the time of concentration needs to be considered in combination with the travel time, t_{is} , which is calculated using the hydraulic properties of the swale, ditch, or channel. For preliminary work, the overland travel time, t_{is} can be estimated with the help of Figure 6-25 or Equation 6-9 (Guo 1999).

 $V = C_v S_w^{-0.5}$

(Eq. 6-9)

Where:

V = velocity (ft/s)

 C_v = conveyance coefficient (from Table 6-7)

 S_w = watercourse slope (ft/ft)



 $t_{c} = t_{i} + t_{t} =$



| Table 6-7. Conveyance Coefficient, C | |
|--------------------------------------|--|
|--------------------------------------|--|

| Type of Land Surface | C, |
|---|------------------|
| Heavy meadow | 2.5 |
| Tillage/field | 5 |
| Riprap (not buried)* | 6.5 |
| Short pasture and lawns | 7 |
| Nearly bare ground | 10 |
| Grassed waterway | 15 |
| Paved areas and shallow paved swales | 20 |
| For buried riprap, select Cv value based on type of v | egetative cover. |

3.2.4 Minimum Time of Concentration

13.19

min.

If the calculations result in a t_c of less than 10 minutes for undeveloped conditions, it is recommended that a minimum value of 10 minutes be used. The minimum t_c for urbanized areas is 5 minutes.

Final t_c:

13.19 min.

3.2.1 - Overland (Initial) Flow Time

$$t_i = \frac{0.395(1.1 - C_5)\sqrt{L}}{S^{0.33}}$$
(Eq. 6-8)

Where:

 t_i = overland (initial) flow time (min) C_5 = runoff coefficient for 5-year frequency (see Table 6-6) L = length of overland flow (300 ft <u>maximum</u> for non-urban land uses, 100 ft <u>maximum</u> for urban land uses)

S = average basin slope (ft/ft)

Note that in some urban watersheds, the overland flow time may be very small because flows quickly concentrate and channelize.

| Sub-Basin or DP: | OS2 | |
|------------------|-------|--|
| C ₅ : | 0.08 | [Table 6-6. Runoff Coefficients for Rational Method] |
| L: | 70 | ft |
| S: | 0.021 | ft/ft |

Composite Runoff Coefficient Calculation:

 $C_{c} = (C_{1}A_{1} + C_{2}A_{2} + C_{3}A_{3} + \dots + C_{i}A_{i})/A_{t}$

| Square Feet | Acreage | C₅ |
|-------------|---|---|
| - | 0.00 | 0.73 |
| - | 0.00 | 0.59 |
| 12,632 | 0.29 | 0.08 |
| 12,632 | 0.29 | |
| | Square Feet - - 12,632 12,632 | Square Feet Acreage - 0.00 - 0.00 12,632 0.29 12,632 0.29 |

 $C_c = (0.08 * 0.29) / 0.29 =$

0.08

mins

 $t_i = (0.395*(1.1-C_5)*sqrt(L))/(S^{0.33})$

 $t_i = (0.395*(1.1-0.08)*sqrt(70))/(0.021^{0.33}) =$ 12.06

3.2.2 Travel Time

For catchments with overland and channelized flow, the time of concentration needs to be considered in combination with the travel time, t_{is} , which is calculated using the hydraulic properties of the swale, ditch, or channel. For preliminary work, the overland travel time, t_{is} can be estimated with the help of Figure 6-25 or Equation 6-9 (Guo 1999).

 $V = C_v S_w^{-0.5}$

(Eq. 6-9)

Where:

V = velocity (ft/s)

 C_v = conveyance coefficient (from Table 6-7)

 S_w = watercourse slope (ft/ft)



| Table 6-7. Conveyance Coefficie | nt, C _v |
|---------------------------------|-----------------------|
| Type of Land Surface | <i>C</i> _v |

| Type of Land Surface | U _y |
|--|------------------|
| Heavy meadow | 2.5 |
| Tillage/field | 5 |
| Riprap (not buried)* | 6.5 |
| Short pasture and lawns | 7 |
| Nearly bare ground | 10 |
| Grassed waterway | 15 |
| Paved areas and shallow paved swales | 20 |
| *For buried riprap, select Cv value based on type of v | egetative cover. |

 $t_{c} = t_{i} + t_{t} =$

12.06 min.

3.2.4 Minimum Time of Concentration

If the calculations result in a t_c of less than 10 minutes for undeveloped conditions, it is recommended that a minimum value of 10 minutes be used. The minimum t_c for urbanized areas is 5 minutes.

Final t_c:

12.06 min.

| Project: | Mariah Trail Filing No. 1 |
|-----------|---------------------------------------|
| Engineer: | Carlos Serrano |
| Date: | 3/16/2023 |
| Address: | Mariah Trail El Paso County, Colorado |

CONDITION: DEVELOPED

Lot 1 Imperviousness Lot 2 Imperviousness

2452 3753.85 0.353926097 0.49890264 0.68115587

(IDF Curve Equations from Figure 6-5 of the DCM Volume 1) D1 11.75 ub-Basin: Duration: I₁₀₀ I₂ I_5 I_{10} I₂₅ I₅₀ 3.102718495 3.886846842 4.5348213 5.1827958 5.8307703 6.5254627

Hydrologic Soil Type: B

| | | | | | | | <u>Co</u> | pefficient (T | able 6-6) | | | | | | | | | |
|---------------------------------------|-------------|----------------|---------------|---------------|----------------|----------------|----------------|-----------------|--|----------------------|-----------------------|-----------------------|-----------------------|------------------------|---------------------|---------------------|----------------------|----------------------|
| Land Use or Surface Characteristic | Square Feet | <u>Acreage</u> | Coefficient 2 | Coefficient s | Coefficient 10 | Coefficient 25 | Coefficient 50 | Coefficient 100 | <u>2 Yr: C_i * A_i</u> | <u>5 Yr: C, * A,</u> | <u>10 Yr: C, * A,</u> | <u>25 Yr: C, * A,</u> | <u>50 Yr: C, * A,</u> | <u>100 Yr: C, * A,</u> | 2 Yr C _c | 5 Yr C _c | 10 Yr C _c | 25 Yr C _c |
| Roof + Hardscape | - | 0.000 | 0.71 | 0.73 | 0.75 | 0.78 | 0.80 | 0.81 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.020 | 0.080 | 0.150 | 0.250 |
| Gravel Roadway | - | 0.000 | 0.57 | 0.59 | 0.63 | 0.66 | 0.68 | 0.70 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | | | | |
| Pasture/Meadow | 80,586 | 1.850 | 0.02 | 0.08 | 0.15 | 0.25 | 0.30 | 0.35 | 0.037 | 0.148 | 0.278 | 0.463 | 0.555 | 0.648 | | | | |
| | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | |
| A _t : | 80,586 | 1.850 | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | |

| Sub-Basin: | D2 | (IDF Curve Equations from Figure 6-5 of the DCM | | | | | | | |
|--------------------------|----------------|---|-----------------|-----------------|------------------|--|--|--|--|
| t _t Duration: | 14.07 | Volume 1) | | | | | | | |
| I ₂ | I ₅ | I ₁₀ | I ₂₅ | I ₅₀ | I ₁₀₀ | | | | |
| 2.888222844 | 3.616474173 | 4.2193865 | 4.8222989 | 5.4252113 | 6.0712366 | | | | |

| | | | | | | | <u>Co</u> | pefficient (T | able 6-6) | | | | | | | | | |
|---------------------------------------|-------------|---------|---------------|---------------|----------------|----------------|----------------|-----------------|--|----------------------|-----------------------|-----------------------|-----------------------|----------------------|---------------------|---------------------|-------------|----------------------|
| Land Use or Surface Characteristic | Square Feet | Acreage | Coefficient 2 | Coefficient 5 | Coefficient 10 | Coefficient 25 | Coefficient 50 | Coefficient 100 | <u>2 Yr: C_i * A_i</u> | <u>5 Yr: C, * A,</u> | <u>10 Yr: C, * A,</u> | <u>25 Yr: C, * A,</u> | <u>50 Yr: C, * A,</u> | <u>100 Yr: Ç * A</u> | 2 Yr C _c | 5 Yr C _c | 10 Yr C_c | 25 Yr C _c |
| Roof + Hardscape | 32,139 | 0.738 | 0.71 | 0.73 | 0.75 | 0.78 | 0.80 | 0.81 | 0.524 | 0.539 | 0.553 | 0.575 | 0.590 | 0.598 | 0.098 | 0.153 | 0.218 | 0.310 |
| Gravel Roadway | 18,448 | 0.424 | 0.57 | 0.59 | 0.63 | 0.66 | 0.68 | 0.70 | 0.241 | 0.250 | 0.267 | 0.280 | 0.288 | 0.296 | | | | |
| Pasture/Meadow | 362,363 | 8.319 | 0.02 | 0.08 | 0.15 | 0.25 | 0.30 | 0.35 | 0.166 | 0.665 | 1.248 | 2.080 | 2.496 | 2.912 | | | | |
| | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | |
| A _t : | 412,949 | 9.480 | | | | | | | | | | | | | | | | |

| Sub-Basin: | D3 | (IDF Curve Equations from Figure 6-5 of the DCM | | | | | | | | |
|--------------------------|----------------|---|-----------------|-----------------|------------------|--|--|--|--|--|
| t _t Duration: | 9.31 | Volume 1) | | | | | | | | |
| I ₂ | I ₅ | I ₁₀ | I ₂₅ | I ₅₀ | I ₁₀₀ | | | | | |
| 3.379920008 | 4.236260515 | 4.9424706 | 5.6486807 | 6.3548908 | 7.1124777 | | | | | |

(IDF Curve Equations from Figure 6-5 of the DCM Volume 1)

Hydrologic Soil Type: B

D4 12.23

Hydrologic Soil Type: B

Sub-Basin: t_t Duration:

I₂

3.055134833

Hydrologic Soil Type: B

| | Coefficient (Table 6-6) | | | | | | | | | | | | | | | | | |
|---------------------------------------|-------------------------|---------|---------------|---------------|----------------|----------------|----------------|-----------------|----------------------|----------------------|-----------------------|---|-----------------------|------------------------|---------------------|---------------------|----------------------|----------------------|
| Land Use or Surface Characteristic | Square Feet | Acreage | Coefficient 2 | Coefficient s | Coefficient 10 | Coefficient 25 | Coefficient 50 | Coefficient 100 | <u>2 Yr: C, * A,</u> | <u>5 Yr: C, * A,</u> | <u>10 Yr: C, * A,</u> | <u>25 Yr: C_i * A_i</u> | <u>50 Yr: C, * A,</u> | <u>100 Yr: C, * A,</u> | 2 Yr C _c | 5 Yr C _c | 10 Yr C _c | 25 Yr C _c |
| Roof + Hardscape | - | 0.000 | 0.71 | 0.73 | 0.75 | 0.78 | 0.80 | 0.81 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.020 | 0.080 | 0.150 | 0.250 |
| Gravel Roadway | - | 0.000 | 0.57 | 0.59 | 0.63 | 0.66 | 0.68 | 0.70 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | | | | |
| Pasture/Meadow | 36,155 | 0.830 | 0.02 | 0.08 | 0.15 | 0.25 | 0.30 | 0.35 | 0.017 | 0.066 | 0.125 | 0.208 | 0.249 | 0.291 | | | | |
| | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | |
| A _t : | 36,155 | 0.830 | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | |

| | Coefficient (Table 6-6) | | | | | | | | | | | | | | | | | | | |
|---------------------------------------|-------------------------|---------|---------------|---------------|----------------|----------------|----------------|-----------------|--|----------------------|-----------------------|---|-----------------------|------------------------|---------------------|---------------------|----------------------|----------------------|----------------------|-----------------------|
| Land Use or Surface Characteristic | Square Feet | Acreage | Coefficient 2 | Coefficient 5 | Coefficient 10 | Coefficient 25 | Coefficient 50 | Coefficient 100 | <u>2 Yr: C_i * A_i</u> | <u>5 Yr: C, * A,</u> | <u>10 Yr: C, * A,</u> | <u>25 Yr: C_i * A_i</u> | <u>50 Yr: C, * A,</u> | <u>100 Yr: C, * A,</u> | 2 Yr C _c | 5 Yr C _c | 10 Yr C _c | 25 Yr C _c | 50 Yr C _c | 100 Yr C _c |
| Roof + Hardscape | 69,888 | 1.604 | 0.71 | 0.73 | 0.75 | 0.78 | 0.80 | 0.81 | 1.139 | 1.171 | 1.203 | 1.251 | 1.284 | 1.300 | 0.081 | 0.138 | 0.203 | 0.297 | 0.345 | 0.391 |
| Gravel Roadway | - | 0.000 | 0.57 | 0.59 | 0.63 | 0.66 | 0.68 | 0.70 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | | | | | | |
| Pasture/Meadow | 715,064 | 16.416 | 0.02 | 0.08 | 0.15 | 0.25 | 0.30 | 0.35 | 0.328 | 1.313 | 2.462 | 4.104 | 4.925 | 5.745 | | | | | | |
| | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | |
| A _t : | 784,951 | 18.020 | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | |

| Sub-Basin: | D5 | (IDF Curve Equations from Figure 6-5 of the DCM Volume 1) | | | | | | | | |
|--------------------------|----------------|--|-----------------|-----------------|------------------|--|--|--|--|--|
| t _t Duration: | 9.70 | | | | | | | | | |
| I ₂ | I ₅ | I ₁₀ | I ₂₅ | I ₅₀ | I ₁₀₀ | | | | | |
| 3.331467321 | 4.175185699 | 4.8712166 | 5.5672476 | 6.2632785 | 7.009872 | | | | | |

Hydrologic Soil Type: B

| | Coefficient (Table 6-6) | | | | | | | | | | | | | | | | | | | |
|-----------------------------|-------------------------|---------|---------------|---------------|----------------|----------------|----------------|-----------------|----------------------|--|-----------------------|---|---|------------------------|---------------------|---------------------|-------------|----------------------|----------------------|--------------|
| Land Use or S Characteri | urface Square Feet | Acreage | Coefficient 2 | Coefficient 5 | Coefficient 10 | Coefficient 25 | Coefficient 50 | Coefficient 100 | <u>2 Yr: C, * A,</u> | <u>5 Yr: C_i * A_i</u> | <u>10 Yr: C, * A,</u> | <u>25 Yr: C_i * A_i</u> | <u>50 Yr: C_i * A_i</u> | <u>100 Yr: C, * A,</u> | 2 Yr C _c | 5 Yr C _c | 10 Yr C_c | 25 Yr C _c | 50 Yr C _c | 100 Yr C_c |
| Roof + Hards | cape - | 0.000 | 0.71 | 0.73 | 0.75 | 0.78 | 0.80 | 0.81 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.273 | 0.315 | 0.371 | 0.439 | 0.475 | 0.511 |
| Gravel Road | way 18,448 | 0.424 | 0.57 | 0.59 | 0.63 | 0.66 | 0.68 | 0.70 | 0.241 | 0.250 | 0.267 | 0.280 | 0.288 | 0.296 | | | | | | |
| Pasture/Mea | dow 21,628 | 0.497 | 0.02 | 0.08 | 0.15 | 0.25 | 0.30 | 0.35 | 0.010 | 0.040 | 0.074 | 0.124 | 0.149 | 0.174 | | | | | | |
| | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | |
| | A _t : 40,075 | 0.920 | | | | | | | | | | | | | | | | | | |

| I ₅ | I ₁₀ | I ₂₅ | I ₅₀ | I ₁₀₀ | Land Use or Surface Characteristic | Square Feet | Acreage | Coet |
|----------------|-----------------|-----------------|-----------------|------------------|---------------------------------------|-------------|---------|------|
| 3.826867436 | 4.4648453 | 5.1028232 | 5.7408012 | 6.4246973 | Roof + Hardscape | 69,888 | 1.604 | (|
| | | | | | Gravel Roadway | - | 0.000 | (|
| | | _ | | | Pasture/Meadow | 715,064 | 16.416 | (|
| /pe: | В | | | | | | | |
| | | | | | | | | |
| | | | | | | | | |
| | | | | | | | | |

| 12 | 15 | '10 | 125 | ¹ 50 | 100 |
|-------------|-------------|-----------|-----------|-----------------|-------|
| 3.331467321 | 4.175185699 | 4.8712166 | 5.5672476 | 6.2632785 | 7.009 |
| | | | | | |
| | | | | | |
| | | | | | |

| 50 Yr C _c | 100 Yr C _c |
|----------------------|-----------------------|
| 0.300 | 0.350 |

| | Q Peak Flow (cfs) | | | | | | | | | | | |
|----------|-------------------|-----------|-----------|-----------|------------|--|--|--|--|--|--|--|
| 2 Year Q | 5 Year Q | 10 Year Q | 25 Year Q | 50 Year Q | 100 Year Q | | | | | | | |
| 0.11 | 0.58 | 1.26 | 2.40 | 3.24 | 4.23 | | | | | | | |



| | Q Peak Flow (cfs) | | | | | | | | | | | |
|----------|-------------------|-----------|-----------|-----------|------------|--|--|--|--|--|--|--|
| 2 Year Q | 5 Year Q | 10 Year Q | 25 Year Q | 50 Year Q | 100 Year Q | | | | | | | |
| 2.89 | 5.65 | 9.38 | 15.21 | 19.67 | 24.83 | | | | | | | |

| 250 | 0.300 | 0.350 |
|-------------------|----------------------|-----------------------|
| Yr C _c | 50 Yr C _c | 100 Yr C _c |
| | | |

| O Peak Flow (cfs) | | | | | | | | | | | |
|-------------------|----------|-----------|-----------|-----------|------------|--|--|--|--|--|--|
| | | Q Peak I | | | | | | | | | |
| 2 Year Q | 5 Year Q | 10 Year Q | 25 Year Q | 50 Year Q | 100 Year Q | | | | | | |
| 0.05 | 0.26 | 0.56 | 1.08 | 1.45 | 1.90 | | | | | | |

| | Q Peak Flow (cfs) | | | | | | | | | | | |
|----------|-------------------|-----------|-----------|-----------|------------|--|--|--|--|--|--|--|
| 2 Year Q | 5 Year Q | 10 Year Q | 25 Year Q | 50 Year Q | 100 Year Q | | | | | | | |
| 4.55 | 9.66 | 16.62 | 27.76 | 36.20 | 45.97 | | | | | | | |

| Q Peak Flow (cfs) | | | | | | | | | | | |
|-------------------|----------|-----------|-----------|-----------|------------|--|--|--|--|--|--|
| 2 Year Q | 5 Year Q | 10 Year Q | 25 Year Q | 50 Year Q | 100 Year Q | | | | | | |
| 0.78 | 1.13 | 1.55 | 2.09 | 2.55 | 3.07 | | | | | | |

| Sub-Basin: | D6 | (IDF Curve Equations from Figure 6-5 of the DCM | | | | | | | | |
|--------------------------|----------------|---|-----------------|-----------------|------------------|--|--|--|--|--|
| t _t Duration: | 10.97 | Volume 1) | | | | | | | | |
| I ₂ | I ₅ | I ₁₀ | I ₂₅ | I ₅₀ | I ₁₀₀ | | | | | |
| 3.184258474 | 3.989628328 | 4.654733 | 5.3198378 | 5.9849425 | 6.6981356 | | | | | |

Hydrologic Soil Type: B

| | Coefficient (Table 6-6) | | | | | | | | | | | | | | | | | | | |
|---------------------------------------|-------------------------|---------|---------------|---------------|----------------|----------------|----------------|-----------------|----------------------|--|---|-----------------------|---|------------------------|---------------------|---------------------|----------------------|----------------------|----------------------|-----------------------|
| Land Use or Surface Characteristic | Square Feet | Acreage | Coefficient 2 | Coefficient 5 | Coefficient 10 | Coefficient 25 | Coefficient so | Coefficient 100 | <u>2 Yr: C; * A;</u> | <u>5 Yr: C_i * A_i</u> | <u>10 Yr: C_i * A_i</u> | <u>25 Yr: C; * A;</u> | <u>50 Yr: C_i * A_i</u> | <u>100 Yr: Ci * Ai</u> | 2 Yr C _c | 5 Yr C _c | 10 Yr C _c | 25 Yr C _c | 50 Yr C _c | 100 Yr C _c |
| Roof + Hardscape | - | 0.000 | 0.71 | 0.73 | 0.75 | 0.78 | 0.80 | 0.81 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.020 | 0.080 | 0.150 | 0.250 | 0.300 | 0.350 |
| Gravel Roadway | - | 0.000 | 0.57 | 0.59 | 0.63 | 0.66 | 0.68 | 0.70 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | | | | | | |
| Pasture/Meadow | 169,884 | 3.900 | 0.02 | 0.08 | 0.15 | 0.25 | 0.30 | 0.35 | 0.078 | 0.312 | 0.585 | 0.975 | 1.170 | 1.365 | | | | | | |
| | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | |
| A _t : | 169,884 | 3.900 | | | | | | | | | | | | | | | | | | |
| | | | | | | | • | | | | | | | | | | | | | |

| Sub-Basin: | O\$1 | (IDF Curve Equations from Figure 6-5 of the DCM | | | | | | | | | |
|--------------------------|----------------|---|-----------------|-----------------|------------------|--|--|--|--|--|--|
| t _t Duration: | 13.19 | Volume 1) | | | | | | | | | |
| I ₂ | I ₅ | I ₁₀ | I ₂₅ | I ₅₀ | I ₁₀₀ | | | | | | |
| 2.965055019 | 3.713321453 | 4.332375 | 4.9514286 | 5.5704822 | 6.23394 | | | | | | |

| Hydrologic Soil Type: | В |
|-----------------------|---|
| | |

| | Coefficient (Table 6-6) | | | | | | | | | | | | | | | | | | | |
|---------------------------------------|-------------------------|---------|---------------|----------------------|----------------|----------------|----------------|-----------------|--|----------------------|---|-----------------------|-----------------------|------------------------|---------------------|---------------------|----------------------|----------------------|----------------------|-----------------------|
| Land Use or Surface Characteristic | Square Feet | Acreage | Coefficient 2 | <u>Coefficient s</u> | Coefficient 10 | Coefficient 25 | Coefficient 50 | Coefficient 100 | <u>2 Yr: C_i * A_i</u> | <u>5 Yr: C; * A;</u> | <u>10 Yr: C_i * A_i</u> | <u>25 Yr: C; * A;</u> | <u>50 Yr: C; * A;</u> | <u>100 Yr: C; * A;</u> | 2 Yr C _c | 5 Yr C _c | 10 Yr C _c | 25 Yr C _c | 50 Yr C _c | 100 Yr C _c |
| Roof + Hardscape | - | 0.000 | 0.71 | 0.73 | 0.75 | 0.78 | 0.80 | 0.81 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.020 | 0.080 | 0.150 | 0.250 | 0.300 | 0.350 |
| Gravel Roadway | - | 0.000 | 0.57 | 0.59 | 0.63 | 0.66 | 0.68 | 0.70 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | | | | | | |
| Pasture/Meadow | 27,878 | 0.640 | 0.02 | 0.08 | 0.15 | 0.25 | 0.30 | 0.35 | 0.013 | 0.051 | 0.096 | 0.160 | 0.192 | 0.224 | | | | | | |
| | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | |
| A _t : | 27,878 | 0.640 | | | | | | | | | | | _ | | | | | | | |

| Sub-Basin: OS2 (IDF Curve Equations from Figure 6-5 of the D | | | | | | | | |
|--|----------------|-----------------|-----------------|-----------------|------------------|--|--|--|
| t _t Duration: | 12.06 | Volume 1) | | | | | | |
| I ₂ | I ₅ | I ₁₀ | I ₂₅ | I _{SO} | I ₁₀₀ | | | |
| 3.071843389 | 3.847928642 | 4.4894167 | 5.1309049 | 5.772393 | 6.4600801 | | | |

| | Coefficient (Table 6-6) | | | | | | | | | | | | | | | | | | | |
|---------------------------------------|-------------------------|---------|---------------|---------------|----------------|----------------|----------------|-----------------|--|----------------------|-----------------------|---|---|------------------------|---------------------|---------------------|--------------------------------------|----------------------|----------------------|-----------------------|
| Land Use or Surface Characteristic | Square Feet | Acreage | Coefficient 2 | Coefficient 5 | Coefficient 10 | Coefficient 25 | Coefficient 50 | Coefficient 100 | <u>2 Yr: C_i * A_i</u> | <u>5 Yr: C; * A;</u> | <u>10 Yr: C, * A,</u> | <u>25 Yr: C_i * A_i</u> | <u>50 Yr: C_i * A_i</u> | <u>100 Yr: C, * A,</u> | 2 Yr C _c | 5 Yr C _c | $10 \text{Yr} \text{C}_{\text{c}}$ | 25 Yr C _c | 50 Yr C _c | 100 Yr C _c |
| Roof + Hardscape | - | 0.000 | 0.71 | 0.73 | 0.75 | 0.78 | 0.80 | 0.81 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.020 | 0.080 | 0.150 | 0.250 | 0.300 | 0.350 |
| Gravel Roadway | - | 0.000 | 0.57 | 0.59 | 0.63 | 0.66 | 0.68 | 0.70 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | | | | | | |
| Pasture/Meadow | 12,632 | 0.290 | 0.02 | 0.08 | 0.15 | 0.25 | 0.30 | 0.35 | 0.006 | 0.023 | 0.044 | 0.073 | 0.087 | 0.102 | | | | | | |
| | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | |
| A _t : | 12,632 | 0.290 | | | | | | | | | | | | | | | | | | |

| Hydrologic Soil Type: | В |
|-----------------------|---|

| Basin Summary | | | | | | | | | | | |
|---------------|--------------|---|------------|----------------|------------------|--|--|--|--|--|--|
| Basin Summary | Design Point | | Area (ac.) | Q ₅ | Q ₁₀₀ | | | | | | |
| D1 | | 1 | 1.85 | 0.58 | 4.23 | | | | | | |
| D2 | | 5 | 9.48 | 5.65 | 24.83 | | | | | | |
| D3 | | 3 | 0.83 | 0.26 | 1.90 | | | | | | |
| D4 | | 2 | 18.02 | 9.66 | 45.97 | | | | | | |
| D5 | | 2 | 0.92 | 1.13 | 3.07 | | | | | | |
| D6 | | 4 | 3.90 | 1.21 | 8.91 | | | | | | |
| OS1 | | 5 | 0.64 | 0.20 | 1.46 | | | | | | |
| OS2 | | 2 | 0.29 | 0.09 | 0.66 | | | | | | |
| TOTAL ONSITE | | | 35.00 | 18.48 | 88.90 | | | | | | |
| TOTAL OFFSITE | | | 0.93 | 0.29 | 2.12 | | | | | | |
| TOTALS | | | 35.93 | 18.77 | 91.03 | | | | | | |

| Cumulative Design Point Summary | | | | | | | | | | | |
|---------------------------------|----|------------------|---|------------|-------|------------------|--|--|--|--|--|
| Design Point | В | asins | | Area (ac.) | Qs | Q ₁₀₀ | | | | | |
| | 1 | D | 1 | 1.85 | 6.32 | 29.72 | | | | | |
| | 2 | DP5 + D4, D5, OS | 2 | 29.35 | 16.72 | 76.00 | | | | | |
| | 3 | D | 3 | 0.83 | 0.26 | 1.90 | | | | | |
| | 4 | D | 6 | 3.90 | 1.21 | 8.91 | | | | | |
| | 5 | D2, OS | 1 | 10.12 | 5.85 | 26.30 | | | | | |
| TOTAL ONSI | ΓE | D1-D | 6 | 35.00 | 18.48 | 88.90 | | | | | |
| TOTAL OFFSI | ΓE | OS1, OS | 2 | 0.93 | 0.29 | 2.12 | | | | | |

Unresolved from Submittal 1: Q5 = 10.88 and Q100 = 79.94cfs in the existing condition (per PDF pg 27 above). Per my comment on PDF pg 6 above, discuss this difference in the report text.

On page 6 it is stated that the flows do not increase nor decrease, but the proposed condition shows an increase in flows of about 10 cfs in the 100-year condition.

| Q Peak Flow (cfs) | | | | | | | | | | | |
|-------------------|----------|-----------|-----------|-----------|------------|--|--|--|--|--|--|
| 2 Year Q | 5 Year Q | 10 Year Q | 25 Year Q | 50 Year Q | 100 Year Q | | | | | | |
| 0.24 | 1.21 | 2.65 | 5.05 | 6.82 | 8.91 | | | | | | |

| Q Peak Flow (cfs) | | | | | |
|-------------------|----------|-----------|-----------|-----------|------------|
| 2 Year Q | 5 Year Q | 10 Year Q | 25 Year Q | 50 Year Q | 100 Year Q |
| 0.04 | 0.20 | 0.44 | 0.83 | 1.12 | 1.46 |

| Q Peak Flow (cfs) | | | | | |
|-------------------|----------|-----------|-----------|-----------|------------|
| 2 Year Q | 5 Year Q | 10 Year Q | 25 Year Q | 50 Year Q | 100 Year Q |
| 0.02 | 0.09 | 0.20 | 0.38 | 0.51 | 0.66 |

3.2.1 - Overland (Initial) Flow Time

$$t_i = \frac{0.395(1.1 - C_5)\sqrt{L}}{S^{0.33}}$$
(Eq. 6-8)

Where:

 t_i = overland (initial) flow time (min) C_5 = runoff coefficient for 5-year frequency (see Table 6-6) L = length of overland flow (300 ft <u>maximum</u> for non-urban land uses, 100 ft <u>maximum</u> for urban land uses)

S = average basin slope (ft/ft)

Note that in some urban watersheds, the overland flow time may be very small because flows quickly concentrate and channelize.

| Sub-Basin or DP: | D1 | |
|------------------|-------|--|
| C ₅ : | 0.08 | [Table 6-6. Runoff Coefficients for Rational Method] |
| L: | 100 | ft |
| S: | 0.039 | ft/ft |

Composite Runoff Coefficient Calculation:

 $C_{c} = (C_{1}A_{1} + C_{2}A_{2} + C_{3}A_{3} + \dots C_{i}A_{i}) / A_{t}$

| Land Use or Surface Characteristic | Square Feet | Acreage | C₅ |
|---------------------------------------|-------------|---------|------|
| Roof + Hardscape | - | 0.00 | 0.73 |
| Gravel Roadway | - | 0.00 | 0.59 |
| Pasture/Meadow | 80,586 | 1.85 | 0.08 |
| At : | 80,586 | 1.85 | |

 $C_c = (0.08*1.85) / 1.85 =$

0.08

11.75

mins

 $t_i = (0.395*(1.1-C_5)*sqrt(L))/(S^{0.33})$

 $t_i = (0.395*(1.1-0.08)*sqrt(100))/(0.039^{0.33}) =$

3.2.2 Travel Time

For catchments with overland and channelized flow, the time of concentration needs to be considered in combination with the travel time, t_i , which is calculated using the hydraulic properties of the swale, ditch, or channel. For preliminary work, the overland travel time, t_n can be estimated with the help of Figure 6-25 or Equation 6-9 (Guo 1999).

 $V = C_v S_w^{0.5}$

(Eq. 6-9)

Where:

V = velocity (ft/s)

 $C_v =$ conveyance coefficient (from Table 6-7)

 S_w = watercourse slope (ft/ft)



| Table 6-7. Conveyance Coefficie | nt, <i>C_v</i> |
|---------------------------------|--------------------------|
| Type of Land Surface | <i>C</i> _v |

| Heavy meadow | 2.5 |
|--|-----------------|
| Tillage/field | 5 |
| Riprap (not buried)* | 6.5 |
| Short pasture and lawns | 7 |
| Nearly bare ground | 10 |
| Grassed waterway | 15 |
| Paved areas and shallow paved swales | 20 |
| * For buried riprap, select Cv value based on type of ve | getative cover. |

 $t_{c} = t_{i} + t_{t} =$

11.75 min.

3.2.4 Minimum Time of Concentration

If the calculations result in a t_c of less than 10 minutes for undeveloped conditions, it is recommended that a minimum value of 10 minutes be used. The minimum t_c for urbanized areas is 5 minutes.

Final t_c:

11.75 min.

3.2.1 - Overland (Initial) Flow Time

$$t_i = \frac{0.395(1.1 - C_5)\sqrt{L}}{S^{0.33}}$$
(Eq. 6-8)

Where:

 t_i = overland (initial) flow time (min) C_5 = runoff coefficient for 5-year frequency (see Table 6-6) L = length of overland flow (300 ft <u>maximum</u> for non-urban land uses, 100 ft <u>maximum</u> for urban land uses)

S = average basin slope (ft/ft)

Note that in some urban watersheds, the overland flow time may be very small because flows quickly concentrate and channelize.

| Sub-Basin or DP: | D2 |] |
|------------------|-------|--|
| C ₅ : | 0.15 | [Table 6-6. Runoff Coefficients for Rational Method] |
| L: | 100 | ft |
| S: | 0.062 | ft/ft |

Composite Runoff Coefficient Calculation:

 $C_{c} = (C_{1}A_{1} + C_{2}A_{2} + C_{3}A_{3} + \dots C_{i}A_{i}) / A_{t}$

| Land Use or Surface Characteristic | Square Feet | Acreage | C ₅ |
|---------------------------------------|-------------|---------|----------------|
| Roof + Hardscape | 32,139 | 0.74 | 0.73 |
| Gravel Roadway | 18,448 | 0.42 | 0.59 |
| Pasture/Meadow | 362,363 | 8.32 | 0.08 |
| At : | 412,949 | 9.48 | |
| | | | |
| $C_c = (0.73*0.74 + 0.59)$ | 0.15 | | |

 $t_i = (0.395*(1.1-C_5)*sqrt(L))/(S^{0.33})$

| t ; = (0.395*(1.1-0.17)*sqrt(100))/(0.062^0.33) = | 9.36 | mins |
|---|------|------|

3.2.2 Travel Time

For catchments with overland and channelized flow, the time of concentration needs to be considered in combination with the travel time, t_{is} , which is calculated using the hydraulic properties of the swale, ditch, or channel. For preliminary work, the overland travel time, t_{is} can be estimated with the help of Figure 6-25 or Equation 6-9 (Guo 1999).

 $V = C_v S_w^{-0.5}$

(Eq. 6-9)

Where:

V = velocity (ft/s)

 C_v = conveyance coefficient (from Table 6-7)

 S_w = watercourse slope (ft/ft)



| Table 6-7. Conveyance Coefficient, C | |
|--------------------------------------|--|
|--------------------------------------|--|

| Type of Land Surface | <i>C</i> _v |
|---|-----------------------|
| Heavy meadow | 2.5 |
| Tillage/field | 5 |
| Riprap (not buried)* | 6.5 |
| Short pasture and lawns | 7 |
| Nearly bare ground | 10 |
| Grassed waterway | 15 |
| Paved areas and shallow paved swales 20 | |
| * For buried riprap, select Cv value based on type of v | egetative cover. |

3.2.4 Minimum Time of Concentration

14.07

min.

If the calculations result in a t_c of less than 10 minutes for undeveloped conditions, it is recommended that a minimum value of 10 minutes be used. The minimum t_c for urbanized areas is 5 minutes.

Final t_c:

 $t_{c} = t_{i} + t_{t} =$

14.07 min.

3.2.1 - Overland (Initial) Flow Time

$$t_i = \frac{0.395(1.1 - C_5)\sqrt{L}}{S^{0.33}}$$
(Eq. 6-8)

Where:

 t_i = overland (initial) flow time (min) C_5 = runoff coefficient for 5-year frequency (see Table 6-6) L = length of overland flow (300 ft <u>maximum</u> for non-urban land uses, 100 ft <u>maximum</u> for urban land uses)

S = average basin slope (ft/ft)

Note that in some urban watersheds, the overland flow time may be very small because flows quickly concentrate and channelize.

| Sub-Basin or DP: | D3 | |
|------------------|-------|--|
| C ₅ : | 0.08 | [Table 6-6. Runoff Coefficients for Rational Method] |
| L: | 100 | ft |
| S: | 0.079 | ft/ft |

Composite Runoff Coefficient Calculation:

 $C_{c} = (C_{1}A_{1} + C_{2}A_{2} + C_{3}A_{3} + \dots C_{i}A_{i}) / A_{t}$

| Land Use or Surface Characteristic | Square Feet | Acreage | C ₅ |
|---------------------------------------|-------------|---------|----------------|
| Roof + Hardscape | - | 0.00 | 0.73 |
| Gravel Roadway | - | 0.00 | 0.59 |
| Pasture/Meadow | 36,155 | 0.83 | 0.08 |
| At : | 36,155 | 0.83 | |

 $C_c = (0.08*0.83) / 0.83 =$

0.08

mins

 $t_i = (0.395*(1.1-C_5)*sqrt(L))/(S^{0.33})$

```
t_i = (0.395*(1.1-0.08)*sqrt(100))/(0.079^{0.33}) =
                                                       9.31
```

3.2.2 Travel Time

For catchments with overland and channelized flow, the time of concentration needs to be considered in combination with the travel time, t_{is} , which is calculated using the hydraulic properties of the swale, ditch, or channel. For preliminary work, the overland travel time, t_{is} can be estimated with the help of Figure 6-25 or Equation 6-9 (Guo 1999).

 $V = C_v S_w^{-0.5}$

(Eq. 6-9)

Where:

tc

V = velocity (ft/s)

 C_v = conveyance coefficient (from Table 6-7)

 S_w = watercourse slope (ft/ft)



| = t _i + t _t = | 9.31 | min. |
|-------------------------------------|------|------|

3.2.4 Minimum Time of Concentration

If the calculations result in a t_c of less than 10 minutes for undeveloped conditions, it is recommended that a minimum value of 10 minutes be used. The minimum t_c for urbanized areas is 5 minutes.

Final t_c:

9.31 min. Table 6-7. Conveyance Coefficient, C_v

| Type of Land Surface | <i>C_v</i> |
|--|----------------------|
| Heavy meadow | 2.5 |
| Tillage/field | 5 |
| Riprap (not buried)* | 6.5 |
| Short pasture and lawns | 7 |
| Nearly bare ground | 10 |
| Grassed waterway | 15 |
| Paved areas and shallow paved swales | 20 |
| * For buried riprap, select Cv value based on type of ve | egetative cover. |

3.2.1 - Overland (Initial) Flow Time

$$t_i = \frac{0.395(1.1 - C_5)\sqrt{L}}{S^{0.33}}$$
(Eq. 6-8)

Where:

 t_i = overland (initial) flow time (min) C_5 = runoff coefficient for 5-year frequency (see Table 6-6) L = length of overland flow (300 ft <u>maximum</u> for non-urban land uses, 100 ft <u>maximum</u> for urban land uses)

S = average basin slope (ft/ft)

Note that in some urban watersheds, the overland flow time may be very small because flows quickly concentrate and channelize.

| Sub-Basin or DP: | D4 | |
|------------------|-------|--|
| C ₅ : | 0.14 | [Table 6-6. Runoff Coefficients for Rational Method] |
| L: | 100 | ft |
| S: | 0.085 | ft/ft |

Composite Runoff Coefficient Calculation:

 $C_{c} = (C_{1}A_{1} + C_{2}A_{2} + C_{3}A_{3} + \dots + C_{i}A_{i})/A_{t}$

| Land Use or Surface Characteristic | Square Feet | Acreage | C ₅ |
|---|-------------|---------|----------------|
| Roof + Hardscape | 69,888 | 1.60 | 0.73 |
| Gravel Roadway | - | 0.00 | 0.59 |
| Pasture/Meadow | 715,064 | 16.42 | 0.08 |
| At : | 784,951 | 18.02 | |
| C _c = (0.73*1.60 + 0.08*16.42) / 18.02 = | | | 0.14 |

 $C_{c} = (0.73*1.60 + 0.08*16.42) / 18.02 =$

 $t_i = (0.395*(1.1-C_5)*sqrt(L))/(S^{0.33})$

```
t_i = (0.395*(1.1-0.14)*sqrt(100))/(0.085^{0.33}) =
                                                       8.57
```

3.2.2 Travel Time

For catchments with overland and channelized flow, the time of concentration needs to be considered in combination with the travel time, t_{is} , which is calculated using the hydraulic properties of the swale, ditch, or channel. For preliminary work, the overland travel time, t_{is} can be estimated with the help of Figure 6-25 or Equation 6-9 (Guo 1999).

mins

 $V = C_v S_w^{-0.5}$

(Eq. 6-9)

Where:

V = velocity (ft/s)

 C_v = conveyance coefficient (from Table 6-7)

 S_w = watercourse slope (ft/ft)



| Type of Land Surface | C _v |
|----------------------|----------------|
| | |

| Heavy meadow | 2.5 |
|---|-----|
| Tillage/field | 5 |
| Riprap (not buried)* | 6.5 |
| Short pasture and lawns | 7 |
| Nearly bare ground | 10 |
| Grassed waterway | 15 |
| Paved areas and shallow paved swales | 20 |
| For buried riprap, select Cv value based on type of vegetative cover. | |
| | |

Table 6-7. Conveyance Coefficient, C_v

 $t_{c} = t_{i} + t_{t} =$

12.23 min.

3.2.4 Minimum Time of Concentration

If the calculations result in a t_c of less than 10 minutes for undeveloped conditions, it is recommended that a minimum value of 10 minutes be used. The minimum t_c for urbanized areas is 5 minutes.

Final t_c:

12.23 min.

3.2.1 - Overland (Initial) Flow Time

$$t_i = \frac{0.395(1.1 - C_5)\sqrt{L}}{S^{0.33}}$$
(Eq. 6-8)

Where:

 t_i = overland (initial) flow time (min) C_5 = runoff coefficient for 5-year frequency (see Table 6-6) L = length of overland flow (300 ft <u>maximum</u> for non-urban land uses, 100 ft <u>maximum</u> for urban land uses)

S = average basin slope (ft/ft)

Note that in some urban watersheds, the overland flow time may be very small because flows quickly concentrate and channelize.

| Sub-Basin or DP: | D5 |] |
|------------------|------|--|
| C ₅ : | 0.31 | [Table 6-6. Runoff Coefficients for Rational Method] |
| L: | 28 | ft |
| S: | 0.04 | ft/ft |

Composite Runoff Coefficient Calculation:

 $C_{c} = (C_{1}A_{1} + C_{2}A_{2} + C_{3}A_{3} + \dots C_{i}A_{i}) / A_{t}$

| Square Feet | Acreage | C₅ |
|-------------|--|--|
| - | 0.00 | 0.73 |
| 18,448 | 0.42 | 0.59 |
| 21,628 | 0.50 | 0.08 |
| 40,075 | 0.92 | |
| | Square Feet - 18,448 21,628 40,075 | Square Feet Acreage - 0.00 18,448 0.42 21,628 0.50 40,075 0.92 |

 $C_c = (0.59*0.42 + 0.08*0.50) / 0.92 =$

 $t_i = (0.395*(1.1-C_5)*sqrt(L))/(S^{0.33})$

 $t_i = (0.395*(1.1-0.31)*sqrt(28))/(0.04^{0.33}) =$

3.2.2 Travel Time

For catchments with overland and channelized flow, the time of concentration needs to be considered in combination with the travel time, t_{is} , which is calculated using the hydraulic properties of the swale, ditch, or channel. For preliminary work, the overland travel time, t_{is} can be estimated with the help of Figure 6-25 or Equation 6-9 (Guo 1999).

0.31

4.75

mins

 $V = C_v S_w^{-0.5}$

(Eq. 6-9)

Where:

V = velocity (ft/s)

 C_v = conveyance coefficient (from Table 6-7)

 S_w = watercourse slope (ft/ft)



| $\mathbf{t}_{c} = \mathbf{t}_{i} + \mathbf{t}_{t} =$ | 9.70 | min. |
|--|------|------|

3.2.4 Minimum Time of Concentration

If the calculations result in a t_c of less than 10 minutes for undeveloped conditions, it is recommended that a minimum value of 10 minutes be used. The minimum t_c for urbanized areas is 5 minutes.

Final t_c:

9.70 min. Table 6-7. Conveyance Coefficient, C_v

| Type of Land Surface | <i>C</i> _v |
|--|-----------------------|
| Heavy meadow | 2.5 |
| Tillage/field | 5 |
| Riprap (not buried)* | 6.5 |
| Short pasture and lawns | 7 |
| Nearly bare ground | 10 |
| Grassed waterway | 15 |
| Paved areas and shallow paved swales | 20 |
| * For buried riprap, select Cv value based on type of ve | getative cover. |

3.2.1 - Overland (Initial) Flow Time

$$t_i = \frac{0.395(1.1 - C_5)\sqrt{L}}{S^{0.33}}$$
(Eq. 6-8)

Where:

 t_i = overland (initial) flow time (min) C_5 = runoff coefficient for 5-year frequency (see Table 6-6) L = length of overland flow (300 ft <u>maximum</u> for non-urban land uses, 100 ft <u>maximum</u> for urban land uses)

S = average basin slope (ft/ft)

Note that in some urban watersheds, the overland flow time may be very small because flows quickly concentrate and channelize.

| Sub-Basin or DP: | D6 |] |
|------------------|-------|--|
| C ₅ : | 0.08 | [Table 6-6. Runoff Coefficients for Rational Method] |
| L: | 100 | ft |
| S: | 0.048 | ft/ft |

Composite Runoff Coefficient Calculation:

 $C_{c} = (C_{1}A_{1} + C_{2}A_{2} + C_{3}A_{3} + \dots C_{i}A_{i}) / A_{t}$

| Square Feet | Acreage | C₅ | |
|-------------|---|---|--|
| - | 0.00 | 0.73 | |
| - | 0.00 | 0.59 | |
| 169,884 | 3.90 | 0.08 | |
| 169,884 | 3.90 | | |
| | Square Feet - - 169,884 169,884 | Square Feet Acreage - 0.00 - 0.00 169,884 3.90 169,884 3.90 | |

 $C_c = (0.08 * 3.90) / 3.90 =$

0.08

mins

 $t_i = (0.395*(1.1-C_5)*sqrt(L))/(S^{0.33})$

 $t_i = (0.395*(1.1-0.08)*sqrt(100))/(0.048^{0.33}) =$ 10.97

3.2.2 Travel Time

For catchments with overland and channelized flow, the time of concentration needs to be considered in combination with the travel time, t_{is} , which is calculated using the hydraulic properties of the swale, ditch, or channel. For preliminary work, the overland travel time, t_{is} can be estimated with the help of Figure 6-25 or Equation 6-9 (Guo 1999).

 $V = C_v S_w^{-0.5}$

(Eq. 6-9)

Where:

V = velocity (ft/s)

 C_v = conveyance coefficient (from Table 6-7)

 S_w = watercourse slope (ft/ft)



| Table 6-7. | Conveyance | Coefficient. | С. |
|------------|------------|--------------|----|

| Type of Land Surface | <i>C</i> _v |
|---|-----------------------|
| Heavy meadow | 2.5 |
| Tillage/field | 5 |
| Riprap (not buried)* | 6.5 |
| Short pasture and lawns | 7 |
| Nearly bare ground | 10 |
| Grassed waterway | 15 |
| Paved areas and shallow paved swales | 20 |
| * For buried riprap, select Cv value based on type of v | egetative cover. |

 $t_{c} = t_{i} + t_{t} =$

10.97 min.

3.2.4 Minimum Time of Concentration

If the calculations result in a t_c of less than 10 minutes for undeveloped conditions, it is recommended that a minimum value of 10 minutes be used. The minimum t_c for urbanized areas is 5 minutes.

Final t_c:

10.97 min.

3.2.1 - Overland (Initial) Flow Time

$$t_i = \frac{0.395(1.1 - C_5)\sqrt{L}}{S^{0.33}}$$
(Eq. 6-8)

Where:

 t_i = overland (initial) flow time (min) C_5 = runoff coefficient for 5-year frequency (see Table 6-6) L = length of overland flow (300 ft <u>maximum</u> for non-urban land uses, 100 ft <u>maximum</u> for urban land uses)

S = average basin slope (ft/ft)

Note that in some urban watersheds, the overland flow time may be very small because flows quickly concentrate and channelize.

| Sub-Basin or DP: | OS1 |] |
|------------------|-------|--|
| C ₅ : | 0.08 | [Table 6-6. Runoff Coefficients for Rational Method] |
| L: | 70 | ft |
| S: | 0.016 | ft/ft |

Composite Runoff Coefficient Calculation:

 $C_{c} = (C_{1}A_{1} + C_{2}A_{2} + C_{3}A_{3} + \dots C_{i}A_{i}) / A_{t}$

| Land Use or Surface Characteristic | Square Feet | Acreage | C₅ |
|---------------------------------------|-------------|---------|------|
| Roof + Hardscape | - | 0.00 | 0.73 |
| Gravel Roadway | - | 0.00 | 0.59 |
| Pasture/Meadow | 27,878 | 0.64 | 0.08 |
| At : | 27,878 | 0.64 | |

 $C_c = (0.08 * 0.64) / 0.64 =$

0.08

mins

 $t_i = (0.395*(1.1-C_5)*sqrt(L))/(S^{0.33})$

```
t_i = (0.395*(1.1-0.08)*sqrt(70))/(0.016^{0.33}) =
                                                       13.19
```

3.2.2 Travel Time

For catchments with overland and channelized flow, the time of concentration needs to be considered in combination with the travel time, t_{is} , which is calculated using the hydraulic properties of the swale, ditch, or channel. For preliminary work, the overland travel time, t_{is} can be estimated with the help of Figure 6-25 or Equation 6-9 (Guo 1999).

 $V = C_v S_w^{-0.5}$

(Eq. 6-9)

Where:

V = velocity (ft/s)

 C_v = conveyance coefficient (from Table 6-7)

 S_w = watercourse slope (ft/ft)



 $t_{c} = t_{i} + t_{t} =$



| Table 6-7. Conveyance Coefficient, C | |
|--------------------------------------|--|
|--------------------------------------|--|

| Type of Land Surface | C, |
|---|------------------|
| Heavy meadow | 2.5 |
| Tillage/field | 5 |
| Riprap (not buried)* | 6.5 |
| Short pasture and lawns | 7 |
| Nearly bare ground | 10 |
| Grassed waterway | 15 |
| Paved areas and shallow paved swales | 20 |
| For buried riprap, select Cv value based on type of v | egetative cover. |

3.2.4 Minimum Time of Concentration

13.19

min.

If the calculations result in a t_c of less than 10 minutes for undeveloped conditions, it is recommended that a minimum value of 10 minutes be used. The minimum t_c for urbanized areas is 5 minutes.

Final t_c:

13.19 min.

3.2.1 - Overland (Initial) Flow Time

$$t_i = \frac{0.395(1.1 - C_5)\sqrt{L}}{S^{0.33}}$$
(Eq. 6-8)

Where:

 t_i = overland (initial) flow time (min) C_5 = runoff coefficient for 5-year frequency (see Table 6-6) L = length of overland flow (300 ft <u>maximum</u> for non-urban land uses, 100 ft <u>maximum</u> for urban land uses)

S = average basin slope (ft/ft)

Note that in some urban watersheds, the overland flow time may be very small because flows quickly concentrate and channelize.

| Sub-Basin or DP: | OS2 | |
|------------------|-------|--|
| C ₅ : | 0.08 | [Table 6-6. Runoff Coefficients for Rational Method] |
| L: | 70 | ft |
| S: | 0.021 | ft/ft |

Composite Runoff Coefficient Calculation:

 $C_{c} = (C_{1}A_{1} + C_{2}A_{2} + C_{3}A_{3} + \dots + C_{i}A_{i})/A_{t}$

| Square Feet | Acreage | C₅ | |
|-------------|---|---|--|
| - | 0.00 | 0.73 | |
| - | 0.00 | 0.59 | |
| 12,632 | 0.29 | 0.08 | |
| 12,632 | 0.29 | | |
| | Square Feet - - 12,632 12,632 | Square Feet Acreage - 0.00 - 0.00 12,632 0.29 12,632 0.29 | |

 $C_c = (0.08 * 0.29) / 0.29 =$

0.08

mins

 $t_i = (0.395*(1.1-C_5)*sqrt(L))/(S^{0.33})$

 $t_i = (0.395*(1.1-0.08)*sqrt(70))/(0.021^{0.33}) =$ 12.06

3.2.2 Travel Time

For catchments with overland and channelized flow, the time of concentration needs to be considered in combination with the travel time, t_{is} , which is calculated using the hydraulic properties of the swale, ditch, or channel. For preliminary work, the overland travel time, t_{is} can be estimated with the help of Figure 6-25 or Equation 6-9 (Guo 1999).

 $V = C_v S_w^{-0.5}$

(Eq. 6-9)

Where:

V = velocity (ft/s)

 C_v = conveyance coefficient (from Table 6-7)

 S_w = watercourse slope (ft/ft)



| Table 6-7. Conveyance Coefficie | nt, C _v |
|---------------------------------|-----------------------|
| Type of Land Surface | <i>C</i> _v |

| Type of Land Surface | U _y |
|--|------------------|
| Heavy meadow | 2.5 |
| Tillage/field | 5 |
| Riprap (not buried)* | 6.5 |
| Short pasture and lawns | 7 |
| Nearly bare ground | 10 |
| Grassed waterway | 15 |
| Paved areas and shallow paved swales | 20 |
| *For buried riprap, select Cv value based on type of v | egetative cover. |

 $t_{c} = t_{i} + t_{t} =$

12.06 min.

3.2.4 Minimum Time of Concentration

If the calculations result in a t_c of less than 10 minutes for undeveloped conditions, it is recommended that a minimum value of 10 minutes be used. The minimum t_c for urbanized areas is 5 minutes.

Final t_c:

12.06 min. Appendix E: Hydraulic Calculations

| | | | De | esign Proc | edure Form | n: Runoff | Reduction | | | | |
|---|--------------------------|---------------------------|---------------|---------------|-----------------|-----------------|--------------|------------------------|-----------|---|--------------|
| | | | | UD-BMI | P (Version 3.07 | , March 2018) | | | | S | sheet 1 of 1 |
| Designer: | CARLOS SER | CARLOS SERRANO, PE | | | | | | | | | |
| Company: | ENGINEERING LOCAL XPERTS | | | | | | | | | | |
| Date: | July 31, 2023 | | | | | | | | | | |
| Project: | MARIAH TRA | IL FILING NO. | 1 | | | | | | | | |
| Location: | EL PASO CO | JNTY, COLOR | ADO | | | | | | | | |
| | | | | | | | | | | | |
| | | 0.11. | | | | | | | | | |
| SITE INFORMATION (US | | ainfall Denth | 0.60 | inches | | | | | | | |
| Depth of Average Ru | noff Producing | g Storm, d ₆ = | 0.43 | inches (for W | /atersheds Ou | utside of the D | enver Regior | n, Figure 3-1 in USDCM | 1 Vol. 3) | | |
| A | | | | | | | | 004 | | | |
| Area Type | | | | | | | | | | | |
| Area ID Downstroom Docign Boint ID | LOT 1 BOND | LUT Z | LUT 3 | LOT 4 | LUT 5 | LUT 6 | R.U.W. | | | | |
| Downstream Design Point ID | FOND | FUND | FUND | FUND | FUND | FUND | FUND | FOND | | | |
| DOWNStream Divir Type | EDB | EDB | EDB | EDB | EDB | EDB | EDB | EDB | | | |
| DCIA (IL) | 44 518 | 47 306 | 45 564 | 43 734 | 50.878 | 5 950 | 30 527 | | | | |
| DIA (IL) RDA (# ²) | 30.000 | 32,500 | 30.000 | 15.000 | 20.000 | 55.000 | 40.000 | | | | |
| SPA (ft ²) | | | | | | | | 1.033.622 | | | |
| HSG A (%) | 0% | 0% | 0% | 0% | 0% | 0% | 0% | 0% | | | |
| HSG B (%) | 100% | 100% | 100% | 100% | 100% | 100% | 100% | 100% | | | |
| HSG C/D (%) | 0% | 0% | 0% | 0% | 0% | 0% | 0% | 0% | | | |
| Average Slope of RPA (ft/ft) | 0.100 | 0.100 | 0.100 | 0.100 | 0.100 | 0.100 | 0.100 | | | | |
| UIA:RPA Interface Width (ft) | 200.00 | 200.00 | 200.00 | 100.00 | 400.00 | 600.00 | 800.00 | | | | |
| | | | | | | | | | | | |
| | | | | | | | | | | | |
| CALCULATED RUNOFF | RESULTS | | | | | | | | | | |
| Area ID | LOT 1 | LOT 2 | LOT 3 | LOT 4 | LOT 5 | LOT 6 | R.O.W. | UNDEVELOPED | | | |
| UIA:RPA Area (ft ²) | 74,518 | 79,806 | 75,564 | 58,734 | 70,878 | 60,950 | 70,527 | | | | |
| L / W Ratio | 1.86 | 2.00 | 1.89 | 5.87 | 0.44 | 0.17 | 0.11 | | | | |
| UIA / Area | 0.5974 | 0.5928 | 0.6030 | 0.7446 | 0.7178 | 0.0976 | 0.4328 | | | | |
| Runoff (in) | 0.00 | 0.00 | 0.00 | 0.08 | 0.05 | 0.00 | 0.00 | 0.00 | | | |
| Runoff (ft ³) | 0 | 0 | 0 | 406 | 307 | 0 | 0 | 0 | | | |
| Runoff Reduction (ft ³) | 1855 | 1971 | 1898 | 1417 | 1813 | 248 | 1272 | 51681 | | | |
| | | | | | | | | | | | |
| | | 1072 | LOT 3 | 1074 | LOT 5 | LOTE | ROW | | | | I |
| WOCV (#3) | 1855 | 1971 | 1898 | 1822 | 2120 | 248 | 1272 | 0 | | | |
| WOCV Reduction (ft ³) | 1855 | 1971 | 1898 | 1417 | 1813 | 248 | 1272 | 0 | | | |
| WQCV Reduction (%) | 100% | 100% | 100% | 78% | 86% | 100% | 100% | 0% | | | |
| Untreated WOCV (ft ³) | 0 | 0 | 0 | 406 | 307 | 0 | 0 | 0 | | | |
| | | | | | | | | | | • | / |
| CALCULATED DESIGN F | POINT RESUL | .TS (sums re | sults from al | I columns w | ith the same | Downstream | Design Poin | nt ID) | | | |
| Downstream Design Point ID | POND | | | | | | | | | | |
| DCIA (ft ²) | 0 | | | | | | | | | | |
| UIA (ft ²) | 268,478 | | | | | | | | | | |
| RPA (ft ²) | 222,500 | | | | | | | | | | |
| SPA (ft ²) | 1,033,622 | | | | | | | | | | |
| Total Area (ft ²) | 1,524,600 | | | | | | | | | | |
| Total Impervious Area (ft ²) | 268,478 | | | | | | | | | | |
| WQCV (ft ³) | 11,187 | | | | | | | | | | |
| WQCV Reduction (ft ³) | 10,474 | | | | | | | | | | |
| WQCV Reduction (%) | 94% | | | | | | | | | | |
| Untreated WQCV (ft ³) | /12 | | l | I | I | I | I | | | | |
| CALCULATED SITE RES | ULTS (sums | results from | all columns | in workshee | t) | | | | | | |
| Total Area (ft ²) | 1,524,600 | | | | | | | | | | |
| I otal Impervious Area (ft ²) | 268,478 | | | | | | | | | | |
| WQCV (ft ³) | 11,187 | | | | | | | | | | |
| WQCV Reduction (ft ³) | 10,474 | | | | | | | | | | |
| WQCV Reduction (%) | 94% | | | | | | | | | | |
| Untreated WQCV (ft ³) | /12 | | | | | | | | | | |
| | | | | | | | | | | | |
| | | | | | | | | | | | |

T FLOW (Normal & Critical Depth Computation CIRCULAR CONDUI

MHFD-Culvert, Version 4.00 (May 2020) Project: MARIAH TRAIL FILING NO. 1



VERTICAL PROFILE FOR THE CULVERT

MHFD-Culvert, Version 4.00 (May 2020)

Project = MARIAH TRAIL FILING NO.1 ID = PIPE 1 - 18" CULVERT PIPE UNDER ROADWAY



| Project Description | |
|--|--|
| Friction Method Solve For | Manning Formula Normal Depth |
| Input Data | |
| Channel Slope Normal Depth Discharge | 0.047 ft/ft 7.3 in 50.00 cfs |
| | 7431.00 7430.00 7429.00 7428.00 7427.00 7425.00 7425.00 7422.00 7422.00 7422.00 7422.00 7422.00 7422.00 7422.00 7422.00 7423.00 7425.00 |

Please input data of the channel sections such as bottom width, side slopes, n value used etc.

Mariah Trail sections.fm8 5/3/2023

Bentley Systems, Inc. Haestad Methods Solution Center 27 Siemon Company Drive Suite 200 W Watertown, CT 06795 USA +1-203-755-1666 FlowMaster [10.03.00.03] Page 1 of 1

Section A-A

Section B-B

| Project Description | |
|---------------------|-----------------------------------|
| Friction Method | Manning Formula |
| Solve For | Normal Depth |
| Input Data | |
| Channel Slope | 0.023 ft/ft |
| Normal Depth | 7.9 in |
| Discharge | 75.99 cfs |
| | 7412.00 |
| | 7411.50 |
| | 7411.00 |
| | 7410.50 |
| | 5 7410.00 |
| | 7409.50 |
| | 7409.00 |
| | 7408.50 |
| | 7408.00 |
| | 7407.50 |
| | 10+00 10+50 11+00 11+5 Station |

Mariah Trail sections.fm8 5/3/2023

Bentley Systems, Inc. Haestad Methods Solution Center 27 Siemon Company Drive Suite 200 W Watertown, CT 06795 USA +1-203-755-1666 FlowMaster [10.03.00.03] Page 1 of 1

Open Channel Flow

Left Side Ditch

$$V = \frac{1}{n} R^{\frac{2}{3}} s^{\frac{1}{2}}$$

Please verify the ditch calculations (left & right)as the velocities shown would require protection.

V = *Velocity or water mass flow rate*

n = Manning's roughness coefficient, 0.025 for grass

R = Hydraulic Radius, 0.35183

s = *Slope of channel's bottom surface*

$$V = \frac{1}{0.025} (0.35183)^{\frac{2}{3}} (2.5)^{\frac{1}{2}}$$
$$V = 3\frac{1.52 ft}{s}$$

Q = V * A

Q = *Volumetric Flow Rate*

V = Calculated Mass Flow Rate

A = Cross - sectional area of the water flow

Q = 31.52 * 0.79

 $Q = 24.83 \, cf/s$

Water Depth = 0.4 ft



Right Side Ditch

$$V = \frac{1}{n} R^{\frac{2}{3}} s^{\frac{1}{2}}$$

V = Velocity or water mass flow rate

n = Manning's roughness coefficient, 0.025 for grass

R = Hydraulic Radius, 0.16053

s = Slope of channel's bottom surface

$$V = \frac{1}{0.025} (0.16053)^{\frac{2}{3}} (2.5)^{\frac{1}{2}}$$
$$V = \frac{18.6811 \, ft/s}{18.6811 \, ft/s}$$

Q = V * A

Q = Volumetric Flow Rate

V = Calculated Mass Flow Rate

A = Cross - sectional area of the water flow

Q = 18.6811 * 0.16

 $Q = 3.07 \, cf/s$

Water Depth = 0.19 ft



| | | | | | 1 | |
|-----------------|----------|------------------------|----------------------|-----------------|-----------|----------|
| FROUDE NU | JMBER CA | LCULATIONS | CALCULATED BY: | ARP | DATE: | 8/2/2023 |
| PROJECT: MARIAH | FRAIL | | CHECKED BY: | RL | | |
| | | Froude Number C | Calculations: 100-YF | { | | |
| Section | Velocity | Gravitational Constant | Hydraulic depth | Xsectional Area | top Width | Froude # |
| - | ft/s | ft/s^2 | ft | ft^2 | ft | N/A |
| A-A | 5.74 | 32.17 | 0.61 | 23.28 | 38.27 | 1.30 |
| B-B | 5.74 | 32.17 | 0.66 | 37.24 | 56.56 | 1.25 |
| | | | | | | |

Per DCM Vol. 1 Section 3 Chapter 10.10 Riprap please provide calculations showing the type, width, and thickness of riprap required. Please reference Tables 10-6 through Table 10-7 for criteria. Fabric filter is required.

Per El Paso County DCM Vol. 1 Section 3 Chapter 10 Table 10-3 velocities exceed maximum permissible velocities for earth channels. Lining is required. Per Table 10-4 for a channel with a slope of 0-5% Bermuda Grass or Sodded Grass are the linings identified for flows higher than 5 ft/s. Please discuss the type of lining for the channel. Per the El Paso County DCM Vol. 1 Section 3 Chapter 10.7 Supercritical Flow channels should have a froude number of 0.9 or less to avoid supercritical flow.

TABLE 10-4 MAXIMUM PERMISSIBLE VELOCITIES FOR EARTH CHANNELS WITH VARIED GRASS LININGS AND SLOPES

| | | ∠ ^A EXPAND |
|---------------|----------------------|---|
| Channel Slope | Lining | Permissible Mean Channel Velocity* (ft/sec) |
| 0 - 5% | Sodded grass | 7 |
| | Bermudagrass | 6 |
| | Reed canarygrass | 5 |
| | Tall fescue | 5 |
| | Kentucky bluegrass | 5 |
| | Grass-legume mixture | 4 |

| S | HEAR STRESS & CHANNEL | LININGS | CALC | CULATED BY: | ARP | DATE: |
|---------|-----------------------|---------------------|-------|--------------|-----|---------|
| PRO. | JECT: MARIAH TRAIL | | CH | ECKED BY: | RL | |
| | Shear Stres | s Calculations: 100 | D-YR | | | |
| Section | unit weight of water | Depth of flow | Slope | Shear Stress | | |
| - | lb/ft^3 | ft | ft/ft | lb/ft^2 | | Section |
| A-A | 62.43 | 0.77 | 0.05 | 2.48 | | A-A |
| B-B | 62.43 | 0.55 | 0.05 | 1.77 | | B-B |

| | | Channel L | ining Determinati | on | |
|---------|-------------------|-----------|-------------------|----------|-----------------|
| | Calculated Values | S | P300 Max \ | /alues | |
| Section | Shear Stress | Velocity | Shear Stress | Velocity | Lining Required |
| A-A | 2.48 | 5.74 | 3 | 9 | P300 |
| B-B | 1.77 | 5.74 | 3 | 9 | P300 |

8/2/2023

Provide spec sheets of any proposed lining –

Appendix F: Drainage Maps

| Basin Summary | | | | | | | | |
|---------------|--------------|---|------------|-------|-------------------------|--|--|--|
| Basin Summary | Design Point | | Area (ac.) | Q₅ | Q ₁₀₀ | | | |
| E1 | | 1 | 1.85 | 0.58 | 4.23 | | | |
| E2 | | 2 | 28.42 | 8.84 | 64.91 | | | |
| E3 | | 3 | 0.83 | 0.26 | 1.90 | | | |
| E4 | | 4 | 3.90 | 1.21 | 8.91 | | | |
| OS1 | | 2 | 0.64 | 0.20 | 1.46 | | | |
| OS2 | | 2 | 0.29 | 0.09 | 0.66 | | | |
| TOTAL ONSITE | | | 35.00 | 10.88 | 79.94 | | | |
| TOTAL OFFSITE | | | 0.93 | 0.29 | 2.12 | | | |
| TOTALS | | | 35.93 | 11.17 | 82.06 | | | |

| <u></u> | mulativ | ve Design P | oint Sum | mary | | | | |
|---------------|---------|--------------|------------|-------|-------------------------|--|--|--|
| Design Point | Basins | | Area (ac.) | Q₅ | Q ₁₀₀ | | | |
| 1 | | E1 | 1.85 | 9.50 | 69.80 | | | |
| 2 | | E2, OS1, OS2 | 29.35 | 9.13 | 67.03 | | | |
| 3 | | E3 | 0.83 | 0.26 | 1.90 | | | |
| 4 | | E4 | 3.90 | 1.21 | 8.91 | | | |
| TOTAL ONSITE | | E1-E4 | 35.00 | 10.88 | 79.94 | | | |
| TOTAL OFFSITE | | OS1, OS2 | 0.93 | 0.29 | 2.12 | | | |



MAJOR SUBDIVISION FINAL DRAINAGE REPORT EXISTING CONDITIONS HYDROLOGY MAP

MARIAH TRAIL FILING NO. 1 A PORTION OF THE NORTHWEST QUARTER OF SECTION 7, TOWNSHIP 11 SOUTH, RANGE 65 WEST OF THE 6TH PRINCIPAL MERIDIAN, PASO COUNTY, COLORADO.



A TR OF LAND BEING IN A PORTION OF LOT 1 SEC 7-11-65...

REPLATTED LEGAL DESCRIPTION: LOTS 1-6 MARIAH TRAIL FILING NO. 1

PARCEL SCHEDULE NO .: 5100000

PROJECT DESCRIPTION: SMALL SUBDIVISION OF 6 LOTS FROM EX. 35-ACRE RR-5 ZONED PACEL

(IN FEET) 1 inch = 100 ft.

FLOODPLAIN STATEMENT: THE SUBJECT PROPERTY IS NOT LOCATED IN A DESIGNATED FLOODPLAIN AS SHOWN ON THE FEMA FLOOD INSURANCE RATE MAP 08041C0305G, EFFECTIVE DATE DECEMBER 7, 2018.

CONSTRUCTION ACTIVITIES:

THE SCOPE OF WORK INVOLVES DISTURBANCE AND CONSTRUCTION ACTIVITY FOR THE APPROXIMATE 1,050 FT. EXTENSION OF COUNTY RIGHT-OF-WAY INCLUDING THE EXTENSION OF THE GRAVEL ROADWAY OF MARIAH TRAIL.

ULTIMATE BUILDOUT OF THE SMALL SUBDIVISION IS FOR FIVE (LOTS 1-5) SINGLE-FAMILY RESIDENTS AT AN ASSUMED MAXIMUM COVERAGE FOR RR-5 ZONED LOTS (25%) WITH ALLOWABLE LAND USES.

TOTAL AREA TO BE CLEARED, EXCAVATED, OR GRADED: FOR ROADWAY: 1.54 ACRES

INCLUDING EROSION AND SEDIMENT CONTROL MEASURES

-THIS MAP SHOWS EXISTING CONDITIONS, NO DISTURBANCE HAS TAKEN PLACE-RECEIVING WATERS: EAST CHERRY CREEK, LOCATED APPROXIMATELY 1.5 MILES EAST OF THE PROPERTY OF INTEREST

SOIL TYPE: BRUSSETT LOAM AND PEYTON-PRINT COMPLEX - HYDROLOGIC SOIL GROUP B



NOTE:

THE PROPERTY INFORMATION AND LINEWORK SHOWN IS CONSIDERED APPROXIMATE AND BASED ON THE PRELIMINARY AND FINAL PLAT DOCUMENTS PREPARED BY MARR LAND SURVEYING DATED OCTOBER OF 2022. THERE IS NO PUBLIC OR PRIVATE STORMWATER INFRASTRUCTURE WITHIN THE VICINITY OF THE PROPERTY OF INTEREST TO DISPLAY ON THIS HYDROLOGY MAP.

THE PROPERTY OF INTEREST IS NOT WITHIN A STREAMSIDE ZONE, PRESERVATION AREA, OR NO-BUILD AREA.

THE PROPERTY OF INTEREST IS NOT WITHIN A FEMA FLOODPLAIN.





| DATE: | DESCRIPTION: |
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| 05/01/23 | SUBMITTAL 1 |
| 08/04/23 | SUBMITTAL 2 |
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SHEET NO .: C.01

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| | | | 1.90 | 0.26 | 0.83 | 3 | D3 |
| | I | | 45.97 | 9.66 | 18.02 | 2 | D4 |
| | I | | 3.07 8 a1 | 1.13 | 0.92 3 an | 2 | ט <u>5</u> D6 |
| | | | 1.46 | 0.20 | 0.64 | 5 | OS1 |
| | 67' | | 0.66 | 0.09 | 0.29 | 2 | DS2 |
| | 735. | | 88.90 2 12 | 18.48 0 29 | 35.00 0 92 | | |
| | ~ | | 91.03 | 18.77 | 35.93 | | OTALS |
| | ·14" / | | | | | | |
| | 20.00 | | 0 | <u>nary</u> 2₅Q₁ | o <mark>int Summ</mark> Area (ac.) | Basins A | Cun Design Point |
| | Z1 | | 29.72 | 6.32 | 1.85 | | 1 |
| | | | 1.90 | 0.26 | 0.83 | DF3 + D4, D3, O32 | 3 |
| | | | 8.91 | 1.21 | 3.90 | D6 | 4 |
| | | UNPLATIED | 26.30 | 5.85 | 10.12 | D2, OS1 | 5 |
| | | | 88.90 2.12 | <u> </u> | 35.00 | D1-D6 OS1. OS2 | TOTAL ONSITE TOTAL OFFSITE |
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| 67.23/" | / / | | | | | | |
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| -, / \ 9.48 | | FARM (40 AC.), | AREA: USE: DRY | LAND | | | |
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EXISTING LEGAL DESCRIPTION:

A TR OF LAND BEING IN A PORTION OF LOT 1 SEC 7-11-65...

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TOTAL AREA TO BE CLEARED, EXCAVATED, OR GRADED:

FOR ROADWAY: 1.54 ACRES INCLUDING EROSION AND SEDIMENT CONTROL MEASURES

RECEIVING WATERS: EAST CHERRY CREEK, LOCATED APPROXIMATELY 1.5 MILES EAST OF THE PROPERTY OF INTEREST

SOIL TYPE: BRUSSETT LOAM AND PEYTON-PRINT COMPLEX - HYDROLOGIC SOIL GROUP B



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JOB #: 100678

MAJOR SUBDIVISION CONSTRUCTION DRAWINGS

SHEET TITLE:

DEVELOPED CONDITIONS HYDROLOGY MAP

SHEET NO .:

C.01

PCD FIL. NO.: SF-231

REVIEWED BY: CDS PROJ. MNGR.: <u>CDS</u> PLAN SET:

MAJOR SUBDIVISION CONSTRUCTION DRAWINGS

SHEET TITLE:

DEVELOPED CONDITIONS HYDROLOGY MAP

SHEET NO .:

C.01