

**FINAL DRAINAGE REPORT  
FOR  
CLOVERLEAF FILING NO. 2**

**PCD File No. SF2123**

**Prepared For:**

**PT Cloverleaf, LLC.  
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**August 20<sup>th</sup>, 2021  
Project No. 25158.01**

**Prepared By:  
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Colorado Springs, CO 80919  
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**ENGINEER'S STATEMENT:**

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by El Paso County for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors, or omissions on my part in preparing this report.

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Mike Bramlett, Colorado P.E. # 32314  
For and On Behalf of JR Engineering, LLC

**DEVELOPER'S STATEMENT:**

I, the developer, have read and will comply with all of the requirements specified in this drainage report and plan.

Business Name: PT Cloverleaf, LLC.

By: \_\_\_\_\_

Title: \_\_\_\_\_

Address: 1864 Woodmoor Drive, Suite 100  
Monument, CO 80920

**El Paso County:**

Filed in accordance with the requirements of the El Paso County Land Development Code, Drainage Criteria Manual, Volumes 1 and 2 and Engineering Criteria Manual, as amended.

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Jennifer Irvine, P.E.  
County Engineer/ ECM Administrator

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Date

Conditions:

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### APPENDIX

- Appendix A – Vicinity Map, Soil Descriptions, FEMA Floodplain Map
- Appendix B – Rational Hydrologic Calculations
- Appendix C – CUHP/SWMM Hydrologic Calculations
- Appendix D – Water Quality & Detention and Hydraulic Calculations
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- Appendix F – Drainage Maps



## **PURPOSE**

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This document is the Final Drainage Report for Cloverleaf Filing No. 2. The purpose of this report is to identify on-site and off-site drainage patterns, storm sewer, culvert and inlet locations, areas tributary to the site, and to safely route developed storm water to adequate outfall facilities.

## **GENERAL SITE DESCRIPTION**

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### **GENERAL LOCATION**

The proposed Cloverleaf Filing No. 2, known as “Cloverleaf F2” from herein, is a parcel of land located in Section 23 and 24, Township 11 South, Range 67 West of the 6th Principal Meridian in El Paso County, Colorado. The subdivision will replat Tract H of Woodmoor Greens and a Portion of Tract B of Woodmoor Placer. Cloverleaf F2 is a 37.28 acre, single family-development and is comprised of 132 lots and associated infrastructure. Cloverleaf F2 will be an urban subdivision proposed for RS-5000 zoning. The site is bounded by Walters Commons Townhomes and Country Ridge Condos to the south, Bowstring Road to the west, Woodmoor Greens and Woodmoor Placer subdivision to the north and Cloverleaf Road to the east. A vicinity map of the area is presented in Appendix A.

No major drainageways or irrigation wells exist on the site.

### **DESCRIPTION OF PROPERTY**

Cloverleaf F2 is currently unoccupied and undeveloped. The existing ground cover is sparse vegetation and open space, typical of a Colorado rolling range land condition. In general, Cloverleaf F2 slopes from northeast to southwest.

Per an NRCS web soil survey of the area, Cloverleaf F2 is made up of Type B soils. This Type B soil is a Tomah-Crowfoot loamy sand. This soil type has a moderate infiltration rate when thoroughly wet. It also consists of moderately deep or deep, moderately well drained or well-drained soil. A soil survey map has been presented in Appendix A.

There are no major drainageways or known irrigation facilities located on the project site. Woodmoor Water and Sanitation District does have various easements for both sanitary and water lines run parallel to existing property lines or cross the site as shown on the drainage map in Appendix F.

### **FLOODPLAIN STATEMENT**

Based on the FEMA Firm Map Number 08041CO278G, revised December 7, 2018, the entire development is located within Zone X, or areas area outside the Special Flood Hazard Area (SFHA)

and higher than the elevation of the 0.2-percent-annual-chance (or 500-year) flood. The FEMA map containing the site has been presented in Appendix A.

## **EXISTING DRAINAGE CONDITIONS**

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### **MAJOR BASIN DESCRIPTIONS**

Cloverleaf F2 lies within the upper reaches of the Teachout Creek watershed basin. Although no DBPS currently exists for Teachout Creek, basin fees have been listed in the Interim Basin Section of the 2021 El Paso County Drainage Basin Fee list. Existing vegetation on the proposed site consists primarily of native grasses. The terrain is sloped generally from northeast to southwest and ranges from 3% to 15%. Drainage from the site currently discharges both west through existing culverts to Lewis Palmer High School and south under Higby Road through existing culverts.

### **EXISTING SUB-BASIN DRAINAGE**

Existing basin drainage patterns are generally from northeast to southwest by way of sheet flow. Woodmoor Placer and Woodmoor Greens subdivisions were platted in the 1970's with half acre or larger lots served by asphalt roads with roadside ditches and culverts. Woodmoor Placer and Woodmoor Greens also had a large somewhat connected series of open space tracts that were envisioned as a golf course. Any excess drainage flows generated by Woodmoor Greens or Woodmoor Place were not detained except in natural depressions within the open space.

The upper Woodmoor drainage flows above Caribou Drive have been collected in the roadside ditches and historically discharged through the lower lots via side lot swales and into the open space where the flow dispersed as sheet flow. The open space flows drain to lower Woodmoor developments; Leggins Way, County Ridge Condos, and Walters Commons Townhomes. Leggins Way accepts the upstream flows via gentle side lot swales that drain to Leggins Way roadside swales discharge through a 28"x42" culvert under Bowstring Road and continue into the Lewis-Palmer High School drainage system. Upstream flows onto Country Ridge pass through the condos and exit into Magic Lamp Way which discharges as gutter flow at the high point of Bowstring Road with half the flows entering the high school at Leggins Way and half the flows entering the Higby Road storm sewer system. Leggins Way and Country Ridge do not provide detention. Walters Commons Townhomes was developed in the 2000's also accepts some of the Woodmoor Place and Woodmoor Greens upstream developed flows but it does provide for stormwater detention which discharges to the Higby Road storm sewer system.

A meeting was held with the school district in January 2020 and the district reported no periodic flooding or drainage concerns.



## **CUHP/SWMM EXISTING SUB-BASIN DRAINAGE**

The Cloverleaf Filing No. 2 Site contains 3 separate areas. The main area, totaling approximately 37.24 acres will contain lots 1 – 126. The main site area has approximately 136 tributary acres upstream of it represented by Basins TX-1, TX-2 in the SWMM model. The site also has flows combining with the development's flows from the existing roadside swale along Bowstring Road. These flows are represented by Basin SX-6 with a total additional area of 49.1 acres. Due to the total analysis area being over 200 acres, the historic, existing, and proposed conditions hydrology were analyzed using CUHP/SWMM. Further discussions regarding these basins can be found below.

As seen in the “Existing Conditions CUHP/SWMM Basins & Routing Map” drainage map, the offsite and on-site areas can be broken into six sub-basins: TX-1, TX-2, SX-3, SX-4, SX-5, and SX-6.

Existing Basin TX-1 is approximately 108.7 acres and consists of prairie grasses, public streets and single family lots. Flow from this basin ( $Q_5=46.8$  cfs,  $Q_{100}=124.8$  cfs) flows through an existing side yard swale and enters the open space at Node/DP-1 ( $Q_5=46.8$  cfs,  $Q_{100}=124.8$  cfs), eventually reaching the Cloverleaf F2 site as sheet flow at Node/DP-3.

Existing Basin TX-2 is approximately 27.2 acres and consists of prairie grasses, public streets and single family lots. Flow from this basin ( $Q_5=10.9$  cfs,  $Q_{100}=31.4$  cfs) flows through an existing side yard swale and enters the open space at Node/DP-2 ( $Q_5=10.9$  cfs,  $Q_{100}=31.4$  cfs), eventually reaching the Cloverleaf F2 site as sheet flow into Basin SX-4.

Existing Basin SX-3 is approximately 27.6 acres and consists of prairie grasses. Flow from this basin ( $Q_5=9.1$  cfs,  $Q_{100}=33.0$  cfs) combines with flows from Basins TX-1 and TX-2 at Node/DP-3 and flows ultimately to the roadside swale along the east side of Leggins Way at DP-9. The areas included in existing SWMM basin SX-3 were included in the Walters Commons FDR as portions of basins OS-5(32.05 ac) and OS-4 (5.68 ac).

Existing Basin SX-4 is approximately 5.2 acres and consists of prairie grasses and a portion of Walters Point (an existing private road access to Walters Commons. Flow from this basin ( $Q_5=1.7$  cfs,  $Q_{100}=5.6$  cfs) sheet flows south into Walters Commons at Node/DP-4. This flow continues to the southwest through the Walters Commons F1 site until it reaches the existing 1.83 ac-ft detention pond part of the Walters Commons development. This pond was sized for the offsite tributary areas that are now part of the Cloverleaf development site and included a total of 9.31 tributary acres to the existing 1.83 ac-ft detention from the Cloverleaf site in basins OS-9, OS-10, and OS-11.

The existing Walters Commons detention pond limits flows to historic rates, and ultimately discharges to the existing 2.3' diameter CMP culvert pipe those outfalls to the ditch on the south side of Higby Road.

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Existing Basin SX-5 is approximately 4.3 acres and consists of prairie grasses and a portion of Walters Point. Flow from this basin ( $Q_5=1.7$  cfs,  $Q_{100}=5.8$  cfs) sheet flows to the south and enters the roadside ditch for Cloverleaf Road at Node/DP-5. Flows in the roadside ditch are collected at a Type C area inlet and enter the Walters Commons Storm Sewer System at Node/DP-11 and are then piped to the existing 1.83 ac-ft detention pond part of the Walters Commons development. This pond was sized for the offsite tributary areas that are now part of the Cloverleaf F2 development site and included a total of 9.31 tributary acres to the existing 1.83 ac-ft detention from the Cloverleaf F2 site in basins OS-9, OS-10, and OS-11.

The existing Walters Commons detention pond limits flows to historic rates, and ultimately discharges to the existing 2.3' diameter CMP culvert pipe that outfalls to the ditch on the south side of Higby Road.

Basins OS-9, OS-10, and OS-11 form the Walters Commons FDR are reasonably consistent in area, flow patterns and runoff quantities with existing basins SX-4 and SX-5 detailed in this report.

Existing Basin SX-6 is approximately 49.1 acres and consists of prairie grasses, Leggins Way, and single family lots. Flow from this basin ( $Q_5=22.3$  cfs,  $Q_{100}=63.1$  cfs) sheet flows to the roadside swales along Bowstring Road at DP-6 and continue in the roadside swale to the southeast until they reach the EX-28"X42" CMP culvert at outfall O1.

### **CUHP/SWMM HISTORIC SUB-BASIN DRAINAGE**

Two basins were analyzed for historic flows. The first basins H1, consists of 163.4 acres of open space/fields (2% impervious). This basin roughly encompasses the same area as the proposed basins TX-1, TX-2, and S-3 from the CUHP/SWMM proposed conditions model. The intent of the historical flow analysis was to quantify pre-development flow rates for the area congruent with Pond P2's tributary area (Proposed basins TX-1, TX-2, and S-3) to determine allowable release rates for the proposed pond. This pond needed to be modeled in SWMM as it is in series with the proposed volume attenuation pond P1. Historic Basin H1 generates runoff rates of  $Q_5 = 32.6$  cfs and  $Q_{100} = 124.8$  cfs.

Historic Basin H2 was provided for informational purposes only and was not used to determine allowable release rates to any pond. Basin H2 consists of 9.62 acres in the southeast corner of the proposed development site. Basin H2 generates runoff rates of  $Q_5 = 2.8$  cfs and  $Q_{100} = 31.4$  cfs. Proposed Pond 3 lies within the historic basin H2, but was sized and designed using the UDFCD UD-detention workbook as its tributary is very small, and in our opinion best modeled through methods other than SWMM and CUHP.

## PROPOSED DRAINAGE CONDITIONS

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### PROPOSED SUB-BASIN DRAINAGE (RATIONAL METHOD)

The proposed site was broken into 21 sub-basins: Basins A through O, and OS-1 through OS-5. The proposed and sub-basin delineation is shown on the drainage basin map in Appendix F. Four ponds and a sand filter are proposed as part of this development. Pond P1 is a private volume attenuation pond that receives all flow from offsite basins that are tributary to the project site, as well as Basin OS-1. Pond P2 is a private full spectrum detention extended detention basin that receives flow from Basins A through K, which make up the majority of the project site. Pond 3 is a private full spectrum detention extended detention basin that receives flow from Basin L in the southeast side of the project site. Pond 4 is a private water quality pond that receives flow from Basins M, N, and O on the western side of the project site. The proposed sand filter will be located behind lots 67-68 and will treat runoff from Sub-Basin OS-4.

The proposed Cloverleaf F2 basin delineation is described below. Refer to the basin and design point summary tables at the end of this section for basin and design point flows.

Proposed Basin A is approximately 4.39 acres in area and includes portions of twenty two proposed single family residential lots, proposed open space, and proposed roadway. Runoff from Basin A ( $Q_5=7.8$  cfs,  $Q_{100}=17.3$  cfs) sheet flows to the proposed roads and is routed via proposed El Paso County Type C curb and gutter to a proposed public 15' Type R on-grade inlet at DP 1. Once in the inlet, the captured flow is piped via proposed public storm sewer to a DP 4.1, where it combines with the flow from Basin D.

Proposed Basin B is approximately 3.11 acres in area and includes portions of twenty one proposed single family residential lots. Runoff from Basin B ( $Q_5=4.2$  cfs,  $Q_{100}=10.1$  cfs) sheet flows to the back of the proposed lots and is routed via a proposed swale to a proposed private Type C area inlet at DP 2. The proposed swale will be within a drainage easement, which will restrict the installation of fencing, structures, or storage of materials within the easement. Once in the inlet, the captured flow is piped via proposed public storm sewer to DP 4.2, where it combines with the flow from DP 4.1. In the event that the inlet at DP 2 becomes clogged, the flow will be routed directly into the proposed private water quality pond 4 at DP 15 via a proposed swale. The proposed routing reduces the runoff to the adjacent site and instead routes the flow to the proposed pond P2, which releases flow at or below the historic rates.

Proposed Basin C is approximately 1.77 acres in area and includes portions of sixteen proposed single family residential lots and proposed roadway. Runoff from Basin C ( $Q_5=4.2$  cfs,  $Q_{100}=8.7$  cfs) sheet flows to the proposed road and is routed via proposed El Paso County Type C curb and gutter to a proposed public 15' Type R on-grade inlet at DP 3. The captured flow is piped via proposed private storm sewer to DP 4.3, where it combines with flow from DP 4.2.

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Proposed Basin D is approximately 3.38 acres in area and includes portions of twenty proposed single family residential lots, proposed open space, and proposed roadway. Runoff from Basin D ( $Q_5=5.9$  cfs,  $Q_{100}=13.0$  cfs) sheet flows to the proposed road and is routed via proposed El Paso County Type C curb and gutter to a proposed public 15' Type R on-grade inlet at DP 4. Once in the inlet, the captured flow is piped via proposed public storm sewer to a proposed public manhole at DP 4.1, where it combines with the flow from Basin A.

All flow at DP 4.1 ( $Q_5=13.1$  cfs,  $Q_{100}=24.6$  cfs) is piped via proposed public storm sewer to DP 4.2.

All flow at DP 4.2 ( $Q_5=16.7$  cfs,  $Q_{100}=33.7$  cfs) is piped via proposed public storm sewer to DP 4.3.

All flow at DP 4.3 ( $Q_5=20.1$  cfs,  $Q_{100}=40.4$  cfs) is piped via proposed public storm sewer to DP 5.1.

Proposed Basin E is approximately 0.30 acres in area and includes portions of four proposed single family residential lots and proposed roadway. Runoff from Basin E ( $Q_5=1.0$  cfs,  $Q_{100}=2.0$  cfs) sheet flows to the proposed road and is routed via proposed El Paso County Type C curb and gutter to a proposed public 10' Type R on-grade inlet at DP 5. Once in the inlet, the captured flow combines with flow from DP 4.3 at DP 5.1.

All flow at DP 5.1 ( $Q_5=20.8$  cfs,  $Q_{100}=41.7$  cfs) is piped via proposed public storm sewer to proposed private Pond P2, where it combines with flow from Basin K and DP 10.1 at DP 11.

Proposed Basin F is approximately 1.40 acres in area and includes portions of eight proposed single family residential lots and proposed roadway. Runoff from Basin F ( $Q_5=3.4$  cfs,  $Q_{100}=6.9$  cfs) sheet flows to the proposed roads and is routed via proposed El Paso County Type C curb and gutter to a proposed public 10' Type R on-grade inlet at DP 6. Once in the inlet, the captured flow is piped via proposed public storm sewer to a proposed public manhole at DP 8.3, where it combines with the flow from tributary basins routed through Pond P1 (DP TB) and DP 8.2.

All flow from tributary basins is routed through Pond P1 and throttled in a proposed private outlet structure at DP TB to release into the proposed storm system at rates of  $Q_5=47.4$  cfs,  $Q_{100}=84.8$  cfs. This flow is routed via proposed public storm sewer to DP 8.3, where it combines with flow from Basin F and DP 8.2. In the event that the proposed private outlet structure becomes clogged, flow will overtop the proposed pond embankment and travel down through proposed open space to the proposed public 15' Type R sump inlet at DP 8.

Proposed Basin IA is approximately 1.71 acres in area and includes portions of eighteen proposed single family residential lots and proposed roadway. Runoff from Basin IA ( $Q_5=3.5$  cfs,  $Q_{100}=7.3$  cfs) sheet flows to the proposed roads and is routed via proposed El Paso County Type C curb and gutter to a proposed public 10' Type R on-grade inlet at DP 7A. Once in the inlet, the captured flow



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is piped via proposed public storm sewer to a proposed public manhole at DP 8.2, where it combines with the flow from DP 8.1.

Proposed Basin G is approximately 0.90 acres in area and includes portions of four proposed single family residential lots, proposed open space, and proposed roadway. Runoff from Basin G ( $Q_5=2.4$  cfs,  $Q_{100}=5.1$  cfs) sheet flows to the proposed roads and is routed via proposed El Paso County Type C curb and gutter to a proposed public 5' Type R on-grade inlet at DP 7. Once in the inlet, the captured flow is piped via proposed public storm sewer to a proposed public manhole at DP 8.1, where it combines with the flow from Basin H.

Proposed Basin H is approximately 4.18 acres in area and includes portions of eighteen proposed single family residential lots, proposed open space, and proposed roadway. Runoff from Basin H ( $Q_5=6.6$  cfs,  $Q_{100}=15.2$  cfs) sheet flows to the proposed roads and is routed via proposed El Paso County Type C curb and gutter to a proposed public 15' Type R sump inlet at DP 8. Once in the inlet, the captured flow is piped via proposed public storm sewer to a proposed public manhole at DP 8.1, where it combines with the flow from Basin G. In the event that the proposed public sump inlet becomes clogged, flow will overtop the local depression in the road and travel in the proposed curb and gutter along the northwest side of Crimson Clover Drive in Basin J to the proposed public 10' Type R sump inlet at DP 10.

All flow at DP 8.1 ( $Q_5=8.2$  cfs,  $Q_{100}=18.3$  cfs) is piped via proposed public storm sewer to DP 8.2, where it combines with flow from DP 7A.

All flow at DP 8.2 ( $Q_5=11.6$  cfs,  $Q_{100}=24.2$  cfs) is piped via proposed public storm sewer to DP 8.3, where it combines with flow from DP TB and DP 6.

All flow at DP 8.3 ( $Q_5=47.5$  cfs,  $Q_{100}=88.8$  cfs) is piped via proposed public storm sewer to DP 9.1, where it combines with flow from DP 9.

Proposed Basin I is approximately 2.76 acres in area and includes portions of eighteen proposed single family residential lots and proposed roadway. Runoff from Basin I ( $Q_5=5.6$  cfs,  $Q_{100}=12.0$  cfs) sheet flows to the proposed roads and is routed via proposed El Paso County Type C curb and gutter to a proposed public 10' Type R sump inlet at DP 9. This inlet was sized to capture all flow in the 5 and 100-year events. Once in the inlet, the captured flow combines with flow from DP 8.3 at DP 9.1. In the event that the proposed public sump inlet becomes clogged, flow will overtop the crown in the road and enter the proposed public 10' Type R sump inlet at DP 10.

All flow at DP 9.1 ( $Q_5=51.2$  cfs,  $Q_{100}=95.6$  cfs) is piped via proposed public storm sewer to DP 10.1, where it combines with flow from DP 10.

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Proposed Basin J is approximately 1.39 acres in area and includes portions of 12 proposed single family residential lots and proposed roadway. Runoff from Basin J ( $Q_5=3.5$  cfs,  $Q_{100}=7.2$  cfs) sheet flows to the proposed roads and is routed via proposed El Paso County Type C curb and gutter to a proposed public 10' Type R sump inlet at DP 10. This inlet was sized to capture all flow in the 5 and 100-year events. Once in the inlet, the captured flow combines with flow from DP 9.1 at DP 10.1. In the event that the proposed public sump inlet becomes clogged, flow will overtop the proposed curb and travel down the proposed open space into Pond P2 at DP 11.

All flow at DP 10.1 ( $Q_5=53.7$  cfs,  $Q_{100}=99.6$  cfs) is piped via proposed private storm sewer to Pond P2, where it combines with flow from Basin K and DP 5.1 at DP 10.2.

Proposed Basin K is approximately 5.29 acres in area and includes portions of 20 proposed single-family residential lots, proposed private full spectrum extended detention Pond P2, and proposed open space. Runoff from Basin K ( $Q_5=5.3$  cfs,  $Q_{100}=15.5$  cfs) sheet flows to the back of the proposed lots and is routed via a proposed swale to the proposed Pond P2, where it combines with flow from DP 5.1 and DP 10.1. A proposed swale along the western property line ensures that all flow from Basin K is routed to Pond P2 at DP 11. The proposed swale will be within a tract, which will restrict the installation of fencing, structures, or storage of materials within the tract. The flow from DP 11 is routed via proposed private storm sewer to DP 15.2, where it combines with the flow from DP 15 (Pond 4).

Proposed Basin L is approximately 1.97 acres in area and includes portions of six proposed single family residential lots, proposed private full spectrum extended detention Pond 3, proposed open space, and existing roadway (Walters Point). Runoff from Basin L ( $Q_5=2.7$  cfs,  $Q_{100}=6.9$  cfs) sheet flows to the back of the proposed lots and into Pond 3 at DP 12. Proposed swales ensure that the runoff will be routed to the pond. The proposed swales will be within tracts, which will restrict the installation of fencing, structures, or storage of materials within the tracts.

Proposed Basin M is approximately 0.54 acres in area and includes portions of two proposed single family residential lots, proposed open space, and proposed roadway. Runoff from Basin M ( $Q_5=1.4$  cfs,  $Q_{100}=2.9$  cfs) sheet flows to the proposed road and is routed via proposed El Paso County Type C curb and gutter to a proposed public 10' Type R on-grade inlet at DP-13. This inlet was sized to capture all flow in the 5 and 100-year events. Once in the inlet, the captured flow is piped via proposed public storm sewer to a proposed public 10' Type R on-grade inlet at DP 14.1, where it combines with the flow from Basin N.

Proposed Basin N is approximately 0.53 acres in area and includes portions of eight proposed single family residential lots and proposed roadway. Runoff from Basin N ( $Q_5=1.4$  cfs,  $Q_{100}=2.8$  cfs) sheet flows to the proposed road and is routed via proposed El Paso County Type C curb and gutter to a proposed public 10' Type R on-grade inlet at DP 14. This inlet was sized to capture all flow in the 5

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and 100-year events. Once in the inlet, the captured flow is piped to DP 14.1, where it combines with the flow from Basin M.

All flow at DP 14.1 ( $Q_5=2.7$  cfs,  $Q_{100}=4.0$  cfs) is piped via proposed public storm sewer to Pond 4 at DP 15, where it combines with flow from Basin O.

Proposed Basin O is approximately 0.98 acres in area and includes portions of seven proposed single family residential lots, proposed private water quality Pond 4, and proposed open space. The emergency spillway from Pond 4 will overflow to the southwest off the property and enter into an existing swale within Walters Commons Filing No. 1. The existing swale will prevent the overflow runoff from impacting the existing buildings. Runoff from Basin O ( $Q_5=1.5$  cfs,  $Q_{100}=3.8$  cfs) sheet flows to the back of the proposed lots and into the proposed swale that routes the flow to Pond 4 at DP 15 where it combines with flow from DP 14.1. The proposed swale will be within a drainage easement, which will restrict the installation of fencing, structures, or storage of materials within the easement. The flow from DP 15 is routed via proposed private storm sewer to DP 15.2, where it combines with the flow from DP 11 (Pond P2).

All flow at DP 15.2 ( $Q_5=64.1$  cfs,  $Q_{100}=120.1$  cfs) is piped via proposed public storm sewer to the outfall on the northeast corner of Bowstring Road and Leggins Way.

Proposed Basin OS-1 is approximately 0.41 acres in area and includes portions of three proposed single family residential lots and proposed open space. Runoff from Basin OS-1 ( $Q_5=0.8$  cfs,  $Q_{100}=1.9$  cfs) sheet flows to the back of the proposed lots and into Pond P1 at DP 16. The flow continues through the pond and combines with the flow from tributary basins at DP TB.

Proposed Basin OS-2 is approximately 0.79 acres in area and includes proposed open space and proposed roadway. Runoff from Basin OS-2 ( $Q_5=1.2$  cfs,  $Q_{100}=3.6$  cfs) sheet flows to the proposed road and is routed via proposed El Paso County Type C curb and gutter to DP L1, where the flow exits the site at Leggins Way and is captured by a proposed Type C inlet. Due to the low existing grade along Leggins Way, the runoff from Basin OS-2 could not be feasibly routed to a proposed pond. Basin OS-2 meets the criteria to exclude water quality capture volume for up to 20% of the applicable site, not to exceed one acre per ECM Appendix I Section I.7.1.C.1.a.

Proposed Basin OS-3 is approximately 0.31 acres in area and includes proposed open space and existing roadway (Walters Point). Runoff from Basin OS-3 ( $Q_5=0.6$  cfs,  $Q_{100}=1.6$  cfs) sheet flows to the existing road and is routed via existing curb and gutter to DP-18, where the flow exits the site along Walters Point. The runoff from Basin OS-3 is received by the existing 1.83-acre foot detention pond to the southwest in the adjacent Walters Commons development, per the approved *Final Drainage Report for Walters Commons*, dated 2005. Flows tributary to the Walters Commons F1 subdivision from the proposed Cloverleaf development are consistent with the approved *Final Drainage Report for Walters Commons*, dated 2005.

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The Walters Commons FDR delineates a basin (OS-9) that discharges to the same point as Basin OS-3 in this report. The runoff from Basin OS-9 ( $Q_5=2$  cfs,  $Q_{100}=4$  cfs) is greater than the runoff expected from the proposed Basin OS-3. Therefore, the existing adjacent Walters Commons development has accounted for the runoff from Basin OS-3 in its existing 1.83-acre foot detention pond and stormwater infrastructure.

Proposed Basin OS-4 is approximately 1.00 acres in area and includes the back portion of four proposed lots, proposed open space, and existing roadway (Walters Point). The back of the proposed lots are assumed to consist mainly of undeveloped and landscaped areas. Runoff from Basin OS-4 ( $Q_5=1.8$  cfs,  $Q_{100}=4.3$  cfs) is routed via proposed swales to a proposed sand filter in the back of lots 67-68. The sand filter releases stormwater via an underdrain to the roadside swale along Cloverleaf Road immediately upstream of the existing 24" RCP culvert underneath Walters Point at DP 19. From the existing culvert, the flow continues south via an existing roadside swale along Cloverleaf Road to the existing Type C inlet on the northwest corner of Higby Road and Cloverleaf Road. The flow is then routed via the existing stormwater system to the existing 1.83-acre foot detention pond in the Walters Commons development. The Walters Commons FDR delineates a basin (OS-10) that discharges to the same point as Basin OS-4 in this report. The runoff from Walters Commons F1 FDR Basin OS-10 ( $Q_5=2$  cfs,  $Q_{100}=5$  cfs) is reasonably consistent with the runoff expected from the proposed Basin OS-4. Therefore, the existing adjacent Walters Commons development has accounted for the runoff from Basin OS-4 in its existing 1.83-acre foot detention pond and stormwater infrastructure. However, the 1.83-acre foot existing detention pond was designed only to accommodate flood control, not water quality. The proposed sand filter will provide the water quality necessary for Basin OS-4. In the case that the sand filter becomes full, the overtopping flow will enter the adjacent ditch and flow through the existing 24" RCP culvert underneath Walters Point.

The site is anticipated to send runoff ( $Q_5=2.8$  cfs,  $Q_{100}=8.8$  cfs) to the existing 1.83-acre foot Walters Commons detention pond from Basin OS-3, Basin OS-4, and proposed Pond 3. Flows tributary to the Walters Commons F1 subdivision from the proposed Cloverleaf F2 development are consistent with the approved *Final Drainage Report for Walters Commons*, dated 2005. Per the approved Walters Commons FDR, the 1.83-acre foot detention pond was designed to accommodate more flow ( $Q_5=7$  cfs,  $Q_{100}=17$  cfs) than the proposed site is anticipated to send to the pond. See the table below for a comparison in the flows proposed in this report and the flows in the Walters Commons FDR.

| Walters Commons 1.83-Acre Foot Detention Pond Flow Comparison |                   |            |                    |            |                      |            |          |            |
|---|-------------------|------------|--------------------|------------|----------------------|------------|----------|------------|
|   | Basin OS-3 / OS-9 |            | Basin OS-4 / OS-10 |            | Pond 3 / Basin OS-11 |            | Sum      |            |
|   | Q5 [cfs]          | Q100 [cfs] | Q5 [cfs]           | Q100 [cfs] | Q5 [cfs]             | Q100 [cfs] | Q5 [cfs] | Q100 [cfs] |
| This Report   | 0.6               | 1.6        | 1.8                | 4.3        | 0.4                  | 2.9        | 2.8      | 8.8        |
| <i>Final Drainage Report for Walters Commons</i>              | 2                 | 4          | 2                  | 5          | 3                    | 8          | 7        | 17         |

### **PROPOSED SUB-BASIN DRAINAGE (CUHP/SWMM METHOD)**

The areas tributary to proposed ponds P1 and P2 were analyzed for the proposed conditions utilizing CUHP/SWMM. Due to the large tributary areas to the ponds and the ponds being in series (P1 drains to P2) a CUHP/SWMM analysis was required.

Pond 3 and its tributary area (quantified as proposed rational basin L) were not included in the CUHP/SWMM proposed conditions analysis, as the ponds tributary areas is only 1.97 acres and it was analyzed and designed using the rational method and UDFCD's UD-Detention workbook. Flows from pond 3 are limited to historic rates through the full spectrum design outlet structure and outfall to Walters Commons Filing 1, along with proposed rational basins OS-3 & OS-4. The flows generated from these three basins are consistent with the Walters Commons Filing 1 FDR. See the proposed conditions rational method section above for more detail.

Proposed Pond 4's tributary area was included in proposed SWMM basin S-6 in order to quantify the total flows at the existing 28" by 42" CMP pipe at the intersection of Leggins Way and Bowstring Road. However, Pond 4 is proposed to provide water quality only for its tributary area, and therefore, a controlled release was not modeled in SWMM. Pond 4 was analyzed/designed using the rational method and UDFCD's UD-Detention workbook.

Proposed Basin TX-1 is approximately 108.7 acres and consists of prairie grasses, public streets and single family lots. Flow from this basin (Node 1,  $Q_5=46.8$  cfs,  $Q_{100}=124.8$  cfs) flow through an existing side yard swale and enter proposed volume attenuation Pond P1 at Storage Unit/Node P1 where they combine with flows from proposed basin TX-2.

Proposed Basin TX-2 is approximately 27.2 acres and consists of prairie grasses, public streets and single family lots (2/3 acre+). Flow from this basin (Node 2,  $Q_5=10.9$  cfs,  $Q_{100}=31.4$  cfs) flows through an existing side yard swale and enters the proposed volume attenuation Pond P1 at Storage Unit/Node P1 where they combine with flows from proposed basin TX-1. The total flow tributary to Storage Unit/Node P1 is  $Q_5 = 57.6$  cfs,  $Q_{100} = 155.8$  cfs.

Storage Unit P1 was designed to limit the release rates to  $Q_5 = 45$  cfs and  $Q_{100} = 79$  cfs. Storage Unit P1 will outfall through a 42" RCP pipe (link 1) and is connected to the on-site storm sewer system which collects all onsite flows from basin S-3 and transports them directly to Pond P2, a full spectrum extended detention basin. The DP06 run was sized based on the pond peak 100-yr release rate and used a time of concentration closer to the peak as shown in the SWMM model.

Proposed Basin S-3 consists of 30.6 acres of single family residential lots, roadways and walks, and open space. Its area and composite percent imperviousness is consistent with rational basins A-K. Basin S-3 generates runoff rates of  $Q_5 = 42$  cfs and  $Q_{100} = 82$  cfs. Runoff from basin S-3 is collected via the proposed Type C curb and gutter system, and proposed on-site storm sewer system and transported to the proposed full spectrum extended detention basin, Pond P2. See the proposed



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rational basin descriptions for on-site routing. The total flow tributary to Storage Unit P2 is  $Q_5 = 74$  cfs and  $Q_{100} = 130$  cfs per the SWMM model as shown in the appendices.

Pond/Storage Unit P2 will release through a full-spectrum outlet structure into a 42" RCP outfall pipe (link 2,  $Q_5 = 63$  cfs,  $Q_{100} = 109$  cfs). The proposed outfall pipe will transport flow to the existing roadside swale on the northeast corner of Leggins Way and Bowstring Road where flows will combine with proposed Basin S-6 runoff at the EX\_28x42\_CMP node in the SWMM model.

Proposed Basin S-6 is approximately 49.1 acres and consists of prairie grasses, Leggins Way, portions of 9 proposed residential lots (6 lots are approximately 7200 s.f., 2 lots are approximately 6000 s.f. each and one is 7500 s.f.) and existing single family lots (2/3 acre+). Flow from this basin ( $Q_5=25.1$  cfs,  $Q_{100}=69.5$  cfs) sheet flows to the roadside swales along Bowstring Road at DP 6 and continue in the roadside swale to the southeast until they reach the EX-28"X42" CMP culvert at outfall O1 where flows combine with the controlled release of Pond/Storage Unit P2, and the existing Walters Commons Flows ( $Q_5 = 12$  cfs,  $Q_{100} = 26$  cfs) for a total flow of  $Q_5 = 91.7$  cfs &  $Q_{100} = 199.2$  cfs.

Due to the large offsite developed areas that currently have no detention facilities that are tributary to the proposed full-spectrum extended detention basin Pond P2, it was not feasible to limit the pond's release rate to the historic flows for the entire basin. Therefore, the design goals for the site were to provide water quality for all new development part of this project, to provide detention for all new developed areas part of the project, and to provide as much additional detention for the offsite areas as practical to limit the flows downstream of the project site to as close to historic levels as possible. Flows from the three CUHP/SWMM models were compared at different design points. The first comparison shown below is for the areas tributary to the proposed full-spectrum extended detention basin Pond P2. This tributary area includes Basin H-1 in the historic conditions model, Basins TX-1, TX-2, and SX-3 in the existing conditions model, and Basins TX-1, TX-2, and S-3 in the proposed conditions model.

The next flow comparison shown compares the existing present day conditions to the proposed conditions for the flow tributary to the existing 18 inch CMP pipe at the intersection of Leggins Way and Bowstring Road. The proposed swale at the back of lots 1-71 captures flows on-site and limits flows tributary to the neighboring Walters Commons development as shown in the table below.

The third flow comparison is for the flow tributary to the existing 28" by 42" CMP pipe located at the intersection of Leggins Way and Bowstring Road. This pipe contains all flows from Ponds P2 and 4, including the offsite tributary areas described above, and proposed basin S-6's flows. Refer to the appendix for a HY-8 analysis of this culvert. The results indicate that, despite the decrease in flow from existing to proposed, Bowstring Road will be overtopped in the 5 and 100-year storms and does not meet the crossing criteria described in EPC DCM Volume 1 Table 6-1 for a Type A (local with a roadside ditch) for both storms. Proposed basin S-6 includes a single 0.5 acre lot that will be



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developed for a single family residence. As shown in the tables below, the proposed detention facilities limit the proposed release rates to below existing conditions, and thus provide detention for all proposed development, and some additional detention for the existing offsite developed tributary areas.

| Existing 28" x 42" CMP Culvert Analysis (Bowstring & Leggins) |          |            |                                   |                                     |
|---|----------|------------|-----------------------------------|-------------------------------------|
|   | Q5 [cfs] | Q100 [cfs] | 5-year Flow Depth at Shoulder[ft] | 100-year Flow Depth at Shoulder[ft] |
| Existing  | 102      | 282        | 0.73                              | 1.23                                |
| Proposed  | 92       | 199        | 0.68                              | 1.06                                |

Bowstring Road shoulder elevation is 6992.74 per existing El Paso County contours.

The last row in the table compares the existing and proposed conditions flows tributary to the existing 1.83 ac-ft detention pond part of the Walter Commons F1 development. The existing flows shown are per the Walters Commons F1 FDR and are further explained in the proposed rational method section above. The proposed flows are per the proposed rational analysis and the proposed Pond 3 release rates. Pond 3 outfalls to Walters Commons F1 at or below historic rates as shown in the table below.

| CUHP OUTFALL/DESIGN POINT COMPARISON TABLE                             |          |            |          |            |          |            |
|--|----------|------------|----------|------------|----------|------------|
| Outfall/Design Point   | Historic |            | Existing |            | Proposed |            |
|  | Q5 (cfs) | Q100 (cfs) | Q5 (cfs) | Q100 (cfs) | Q5 (cfs) | Q100 (cfs) |
| 01, 9, P2_OUT  | 33       | 125        | 67       | 188        | 63       | 109        |
| EX18CMP  | n/a      | n/a        | 14       | 32         | 12       | 26         |
| EX28X42  |          |            | 102      | 282        | 92       | 199        |
| Pond 3*  | 0        | 1.9        | N/A      | N/A        | 0        | 2.9        |
| Areas tributary to Walters Commons F1 1.83-ac-ft pond                  | N/A      | N/A        | 7        | 17         | 2.8      | 8.8        |
| * Flows per UD-Detention Basin and Outlet Worksheets, see Appendix D   |          |            |          |            |          |            |
| From rational calculations, prior reports, and UD-Detention worksheets |          |            |          |            |          |            |

## **DRAINAGE DESIGN CRITERIA**

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### **DEVELOPMENT CRITERIA REFERENCE**

Storm drainage analysis and design criteria for this project were taken from the “*City of Colorado Springs/El Paso County Drainage Criteria Manual*” Volumes 1 and 2 (EPCDCM), dated October 12, 1994, the “*Urban Storm Drainage Criteria Manual*” Volumes 1 to 3 (USDCM) and Chapter 6 and Section 3.2.1 of Chapter 13 of the “*Colorado Springs Drainage Criteria Manual*” (CSDCM), dated May 2014, as adopted by El Paso County.

### **HYDROLOGIC CRITERIA**

All hydrologic data was obtained from the “*El Paso Drainage Criteria Manual*” Volumes 1 and 2, and the “*Urban Drainage and Flood Control District Urban Storm Drainage Criteria Manual*” Volumes 1, 2, and 3. Onsite drainage improvements were designed based on the 5 year (minor) storm event and the 100-year (major) storm event. Existing Basin Runoff (offsite and on-site) were calculated with Colorado Urban Hydrograph Program (CUHP) due to basin size and Stormwater Management Model (SWMM) was used routing the flows through the offsite pond and the larger on-site pond. On-site developed condition runoff was calculated using the Rational Method, and rainfall intensities for the 5-year and the 100-year storm return frequencies were obtained from Table 6-2 of the CSDCM. One hour point rainfall data for the storm events is identified in the chart below. Runoff coefficients were determined based on proposed land use and from data in Table 6-6 from the CSDCM. Time of concentrations were developed using equations from CSDCM. All runoff calculations and applicable charts and graphs are included in the Appendices.

**Table 2 - 1-hr Point Rainfall Data**

| <b>Storm</b> | <b>Rainfall (in.)</b> |
|--------------|-----------------------|
| 5-year       | 1.50                  |
| 100-year     | 2.52                  |

### **HYDRAULIC CRITERIA**

The Rational Method and USDCM’s SF-2 and SF-3 forms were used to determine the runoff from the minor and major storms on the site, and the UDFCD UD-Detention v4.03 spreadsheet was utilized for evaluating proposed detention and water quality for Pond 3, Pond 4, and the proposed sand filter. The UDFCD UD-Detention v4.03 spreadsheet was also used with EPA SWMM 5.1 to model Pond P1 (peak attenuation pond) and Pond P2 (full-spectrum EDB) which are in series. The UD-Detention spreadsheet was used to input the stage storage information which was then added to the SWMM model for each pond. Then the 5-year and 100-year SWMM models were run to create inflow hydrographs for Pond P2. Those hydrographs were then transferred back to the UD-Detention spreadsheet for the 5-year and 100-year storms where they were used to design the outlet structure for Pond P2. Once the outlet structure was determined in the UD-Detention, the stage-discharge



information was then transferred to SWMM models. Sump and on-grade inlets were sized using UDFCD UD-Inlet v4.06. Using Storm StormCAD V8i, a modeling program for stormwater drainage, the hydraulic grade lines and energy grade lines were determined for the storm sewer network. Manhole and pipe losses for the model were obtained from the Urban Storm Drainage Criteria Manual. Hydraulic grade lines for the Cloverleaf F2 development shall in no case be closer than one foot to the ground or street surface. Storm CAD results can be found in Appendix D.

## **DRAINAGE FACILITY DESIGN**

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### **FOUR STEP PROCESS TO MINIMIZE ADVERSE IMPACTS OF URBANIZATION**

In accordance with the El Paso County Drainage Criteria Manual Volume 2, this site has implemented the four step process to minimize adverse impacts of urbanization. The four step process includes reducing runoff volumes, treating the water quality capture volume (WQCV), stabilizing drainage ways, and implementing long-term source controls.

**Step 1 – Reducing Runoff Volumes:** The Cloverleaf Filing No. 2 development project consists of 132 single family lots with open spaces and lawn areas interspersed within the development which helps disconnect impervious areas and reduce runoff volumes. Roof drains from the structures will discharge to lawn areas, where feasible, to allow for infiltration and runoff volume reduction. The site also uses grass lined swales to transport runoff to the proposed storm sewer system and detention ponds which allows for additional infiltration and runoff reduction above pipe conveyance systems.

**Step 2 – Stabilize Drainageways:** The site lies within the Teachout Creek Drainage Basin. Basin and bridge fees will be paid at time of platting. These funds will be used on future projects within the basin to stabilize drainageways. The site does not discharge directly into the open drainageway of Teachout Creek, therefore no downstream stabilization will be accomplished with this project.

**Step 3 – Treat the WQCV:** Water Quality treatment for this site is provided in two proposed full spectrum extended detention basins: Pond P2 and Pond 3, proposed water-quality pond 4, and a proposed sand filter. The runoff from this site will be collected within inlets and conveyed to the proposed ponds via storm sewer. Upon entrance to the ponds, flows will be captured in a forebay designed to promote settlement of suspended solids. A trickle channel is also incorporated into the ponds to minimize the amount of standing water. The outlet structure has been designed to detain the water quality capture volume (WQCV) for 40 hours, and the extended urban runoff volume (EURV) for 72 hours. The sand filter was designed to have a volume above the sand bed of the basin equal to the WQCV based on a 12-hour drain time. The sand filter does not include an impermeable liner but includes an underdrain, so some infiltration is allowed (see the description for “Partial Infiltration Section” sand filter in *Urban Storm Drainage Criteria Manual Volume 3*, page SF-4).



Step 4 – Consider Need for Industrial and Commercial BMPs: BMPs will be utilized to minimize off-site contaminants and to protect the downstream receiving waters. Site specific temporary source control BMPs that will be implemented include, but are not limited to, silt fencing placed around downstream areas of disturbance, construction vehicle tracking pads at the entrances, designated concrete truck washout basin, designated vehicle fueling areas, covered storage areas, spill containment and control, etc. The permanent erosion control BMPs include asphalt streets, storm inlets and storm pipe, two full spectrum water quality and detention ponds, and permanent vegetation.

### **WATER QUALITY/DETENTION**

The site is split by a natural ridge, therefore; a full spectrum water quality and detention pond is provided on both sides. Basins A through K, located north of the natural ridge, will discharge to the pond at DP 10.2 (Pond P2). Basins M, N, and O, also located north of the natural ridge, will discharge to the pond at DP 15 (Pond 4). Basin L, south of the natural ridge, will discharge to the pond at DP 12 (Pond 3). Both full-spectrum ponds P2 and P3 have been designed per Section 13.3.2.1 of the City of Colorado Springs' Drainage Criteria Manual Volume 1, as revised in May 2014.

As previously discussed, two large off-site basins (TX-1 and TX-2) are tributary to the site and currently have no engineered detention or water quality features. Due to space constraints on-site, detention for the off-site basins TX-1 and TX-2 was not feasible on-site. Therefore, a volume attenuation pond, Pond P1, is proposed upstream of the site along the site's northeastern border to reduce the peak flows tributary to the site. Pond P1 is intended to provide volume attenuation only, and is connected to proposed on-site Pond P2 (ponds in series). Both ponds were modeled using SWMM version 5.1.

As shown in the attached CUHP/SWMM models(existing & proposed), basins TX-1 and TX-2 produce a total tributary flow to proposed Pond/node P1 of  $Q_5 = 58$  cfs, &  $Q_{100} = 156$  cfs. The proposed peak outflow of Pond P1 (link 1), is  $Q_5 = 45$  cfs &  $Q_{100} = 79$  cfs and is piped directly to Pond P2 via proposed reinforced concrete pipe (RCP).

Pond P2 receives flows from the controlled release of Pond P1, via the storm sewer system described above, and from on-site tributary basins (rational basins A-K, and CUHP/SWMM basin S-3/Node 3). Basin S3/Node 3 produces a peak flow of  $Q_5 = 42$  cfs, &  $Q_{100} = 82$  cfs which combines with the controlled release from Pond P1 (which is  $Q_5 = 45$  cfs &  $Q_{100} = 79$  cfs) for a total peak flow into Pond P2 of  $Q_5 = 74$  cfs, and  $Q_{100} = 130$  cfs (as shown in the SWMM model). The proposed full-spectrum outlet structure will limit Pond P2's release to a maximum of  $Q_5 = 63$  cfs, and  $Q_{100} = 109$  cfs.

## FINAL DRAINAGE REPORT FOR CLOVERLEAF FILING NO. 2

For comparison purposes, a Historic CUHP/SWMM model was created to quantify the pre-development flows from the entire area tributary to Pond P2. Basin H1 in the Historic Model encompasses 163.4 acres, in roughly the same area as basins TX-1, TX-2, and S-3/SX-3. This model assumed all area to be undeveloped open space with a composite percent impervious value of 2%. Basin H1 produced peak flows of  $Q_5 = 33$  cfs, and  $Q_{100} = 125$  cfs. As shown above, Pond P2's maximum release rate is approximately equal to the historic peak flow for the 100 year storm, and slightly more than the historic peak flow for the 5 year storm. These flow comparisons are more fully discussed in the "Proposed Sub-Basin Drainage (CUHP/SWMM)" section above.

Pond P2's required WQCV and EURV was calculated using the UDFCD UD-Detention v4.03 spreadsheet for the on-site tributary basins A-K, totaling 30.6 acres.

- Required WQCV: 0.594 ac-ft
- Required EURV: 1.948 ac-ft

The pond was designed for a 40-hour WQCV drain time and a 72-hour EURV drain time (see appendix D for supporting calculations). As described above, Pond P2 was also sized to provide detention for both the on-site and off-site tributary areas and has a total volume of 3.34 ac-ft. The pond totally drains in less than 79 hours as shown in the SWMM model.

Both Ponds P1 and P2 will include an emergency overflow spillway sized for the undetained peak 100-year flow rate tributary to each pond. Both spillways will consist of buried soil riprap w/ a grade control concrete weir installed in the crest of the spillway. Both Pond P1 and Pond P2 will have cutoff walls to ensure proper design due to their size and peak undetained flow rate. Both spillways will provide a minimum of one foot of freeboard from the design water surface elevation to the top of embankment.

Pond P1's emergency overflow spillway will be centered on the open space tract between lots 101 and 102 where a trapezoidal channel will be graded in to direct flows westward into the proposed street. Flows will then follow the overflow routing described in the rational basins G and J description above.

Pond P2's spillway will direct water from the southwestern corner of the pond where the outlet structure is proposed to the adjacent proposed street to the south. Flows will then travel down the proposed street to the west to the existing Leggins Way, and ultimately to the existing 28"x42" CMP beneath Bowstring Road.

Pond 3 receives flows from proposed Basin L. The proposed full-spectrum outlet structure will limit Pond 3's release rate to below predevelopment peaks. The Pond 3 design includes a forebay, trickle channel, and a full spectrum detention outlet structure.

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Pond 3's required WQCV and EURV was calculated using UDFCD UD-Detention workbook for the on-site tributary Basin L, totaling 1.97 acres.

- Required WQCV: 0.031 ac-ft
- Required EURV: 0.088 ac-ft

The pond was designed for a 40-hour WQCV drain time and a 72-hour EURV drain time (see appendix D for supporting calculations). Pond 3 was also sized to provide detention for the 100-yr storm and below and has a total volume of 0.164 ac-ft. The pond totally drains in 77 hours for a 100-year event.

Pond 3 will include an emergency overflow spillway sized for the undetained peak 100 year flow rate tributary to the pond. The spillway will consist of buried soil riprap. The spillway will provide a minimum of one foot of freeboard from the design water surface elevation to the top of embankment.

The overflow path for the stormwater that crests the spillway extends from the Pond 3 spillway southeast to the existing roadside swale along the west side of Cloverleaf Road. The flow will then enter the existing Type C inlet at the northwest corner of Cloverleaf Road and Higby Road. The existing offsite pond and structures are functioning as intended, has sufficient capacity, and is not in need of any maintenance.

Pond 4 receives flows from proposed Basins M, N, and O. The proposed outlet structure will limit Pond 4's water quality capture volume to release in 40 hours. The Pond 4 design includes a trickle channel and an outlet structure.

Pond 4's required WQCV was calculated using UDFCD UD-Detention workbook as well as the UD-BMP v3.07 workbook for the on-site tributary Basins M, N, and O, totaling 2.05 acres. The UD-BMP workbook was used to reduce the percent impervious value that was used in the UD-Detention workbook.

- Required WQCV: 0.030ac-ft

The pond was designed for a 40-hour WQCV drain time (see appendix D for supporting calculations).

The Pond 4 emergency spillway will be routed to the existing swale in Walters Commons Filing 1 to the southwest of the pond's outlet structure, consistent with existing drainage patterns. The flow will travel to the existing roadside ditch along Bowstring Road, which will route the flow northwest to the existing 18" RCP culvert under Leggins Way. The proposed spillway outfall point onto Walters Commons Filing 1 is consistent with the Basin OS-4 discharge included in the approved *Final Drainage Report for Walters Commons*. The proposed peak 100-year spillway discharge from Pond 4 (6.1 cfs) is less than the anticipated flow from the aforementioned Basin OS-4 (per Walters Commons FDR) (9 cfs).

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A sand filter is proposed in the back of lots 67 & 68 to provide water quality for the proposed Basin OS-4 runoff. The existing 1.83 acre-foot detention pond within Walters Commons Filing 1 receives runoff from this basin and provides detention but no water quality. The sand filter was designed to have a volume above the sand bed of the basin equal to Basin OS-4's WQCV (0.010 acre-feet) based on a 12-hour drain time. Refer to Appendix D for the sand filter sizing calculation. The sand filter does not include an impermeable liner but includes an underdrain, so some infiltration is allowed (see the description for "Partial Infiltration Section" sand filter in *Urban Storm Drainage Criteria Manual Volume 3*, page SF-4). The underdrain discharges directly into the adjacent roadside swale along Cloverleaf Road, immediately upstream of the existing 24" RCP culvert underneath Walters Point. In the event that the sand filter becomes full, the overtopping flow will enter the adjacent roadside swale and flow through the existing 24" RCP culvert underneath Walters Point and continue to the existing 1.83 acre-foot detention pond within Walters Commons Filing 1.

Three isolated lots were part of the overall Cloverleaf Preliminary plan and the drainage analysis for these lots has been completed with the *Small Subdivision Final Drainage Report for Cloverleaf Filing No. 1*, by JR Engineering, dated December 1, 2020 (PCD File No. SF2114).

### **EROSION CONTROL PLAN**

We respectfully request that the Erosion Control Plan and Cost Estimate be submitted in conjunction with the grading and erosion control plan and construction assurances posted prior to obtaining a grading permit. The CD plan set includes a final grading plan.

### **OPERATION & MAINTENANCE**

In order to ensure the function and effectiveness of the stormwater infrastructure, maintenance activities such as inspection, routine maintenance, restorative maintenance, rehabilitation and repair, are required. Cloverleaf Metropolitan District shall be responsible for the inspection, maintenance, rehabilitation and repair of stormwater and erosion control facilities located on the property, unless another party accepts such responsibility in writing and responsibility is properly assigned through legal documentation. Access is provided from onsite facilities and easements for proposed infrastructure located offsite. Access to Pond 3 is provided through the existing access easements centered around Walters Point.

### **DRAINAGE AND BRIDGE FEES**

The site lies within the Teachout Creek Drainage Basin. Anticipated drainage and bridge fees are presented below and will be paid at time of platting (depending on date of plat submittal):

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| 2021 DRAINAGE AND BRIDGE FEES – CLOVERLEAF FILING NO. 2 |                              |                            |                         |                       |
|---|------------------------------|----------------------------|-------------------------|-----------------------|
| Impervious Acres (ac)                                   | Drainage Fee (Per Imp. Acre) | Bridge Fee (Per Imp. Acre) | Cloverleaf Drainage Fee | Cloverleaf Bridge Fee |
| 22.02   | \$5,429                      | \$816                      | \$119,547               | \$17,968              |

## SUMMARY

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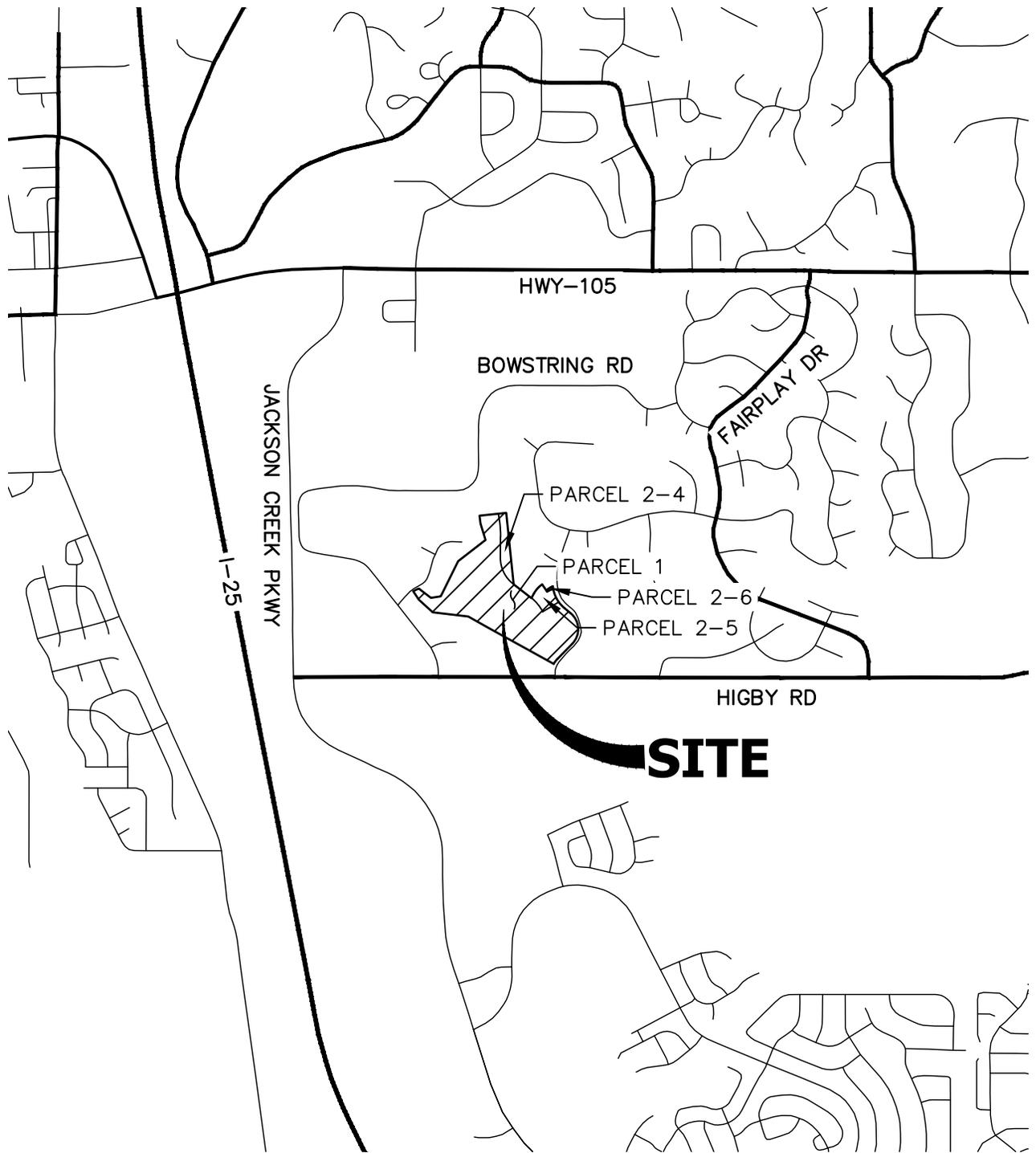
The proposed Cloverleaf Filing No. 2 development drainage improvements, including storm sewer and two full spectrum water quality and detention ponds were designed to meet or exceed the El Paso County Drainage Criteria. The proposed development will not adversely affect the offsite drainageways or surrounding development. This report is in conformance and meets the latest El Paso County Storm Drainage Criteria requirements for this site.

## REFERENCES

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1. El Paso County Drainage Criteria Manual Volume 1, El Paso County, CO, 1994.
  2. Urban Storm Drainage Criteria Manual (Volumes 1, 2, and 3), Urban Drainage and Flood Control District, June 2001.
  3. Flood Insurance Study- El Paso County, Colorado & Incorporated Areas Vol 7 of 8, Federal Emergency Management Agency, December 7, 2018.
  4. Walters Commons Final Drainage Report, prepared by JR Engineering, 2005.
  5. Preliminary Drainage Report for Cloverleaf Subdivision Preliminary Plan, prepared by JR Engineering, 2020. (PCD File No. SP202)
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**Appendix A**  
**Vicinity Map, Soil Descriptions, FEMA Floodplain Map**



2000 1000 0 2000



ORIGINAL SCALE: 1" = 2000'

VICINITY MAP  
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JOB NO. 25158.01  
08/19/2021  
SHEET 1 OF 1

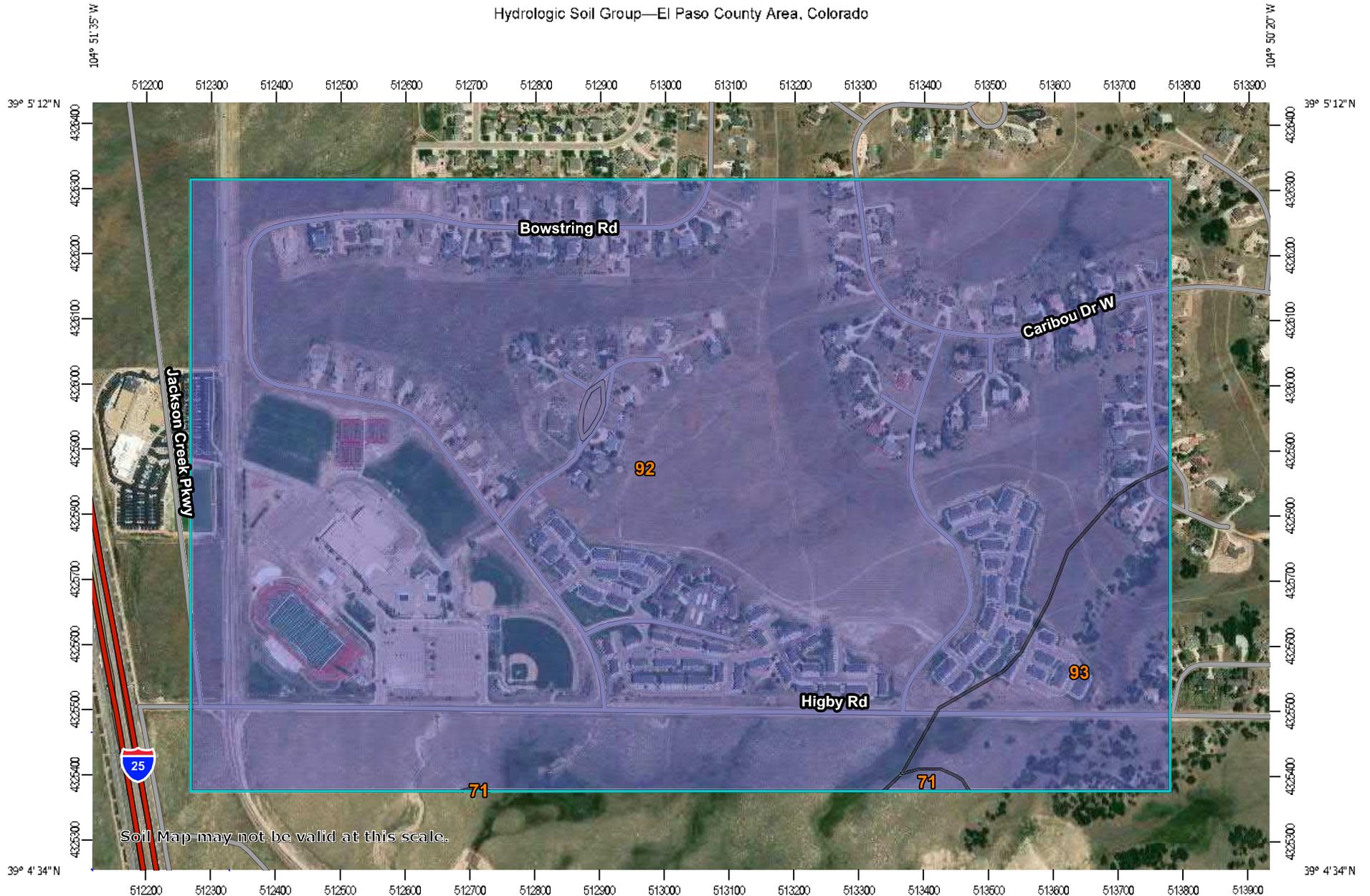


**J·R ENGINEERING**

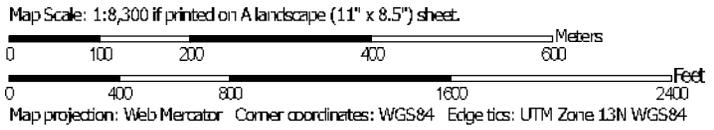
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Hydrologic Soil Group—El Paso County Area, Colorado



Soil Map may not be valid at this scale.



### MAP LEGEND

- Area of Interest (AOI)**  
 Area of Interest (AOI)
- Soils**
- Soil Rating Polygons**
-  A
  -  A/D
  -  B
  -  B/D
  -  C
  -  C/D
  -  D
  -  Not rated or not available
- Soil Rating Lines**
-  A
  -  A/D
  -  B
  -  B/D
  -  C
  -  C/D
  -  D
  -  Not rated or not available
- Soil Rating Points**
-  A
  -  A/D
  -  B
  -  B/D
- Water Features**
-  Streams and Canals
- Transportation**
-  Rails
  -  Interstate Highways
  -  US Routes
  -  Major Roads
  -  Local Roads
- Background**
-  Aerial Photography
- Soil Rating Legend**
-  C
  -  C/D
  -  D
  -  Not rated or not available

### MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24,000.

**Warning: Soil Map may not be valid at this scale.**

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service  
 Web Soil Survey URL:  
 Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: El Paso County Area, Colorado  
 Survey Area Data: Version 16, Sep 10, 2018

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Jul 4, 2010—Oct 16, 2017

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

## Hydrologic Soil Group

| Map unit symbol                    | Map unit name                                     | Rating | Acres in AOI | Percent of AOI |
|------------------------------------|---|--------|--------------|----------------|
| 71                                 | Pring coarse sandy loam, 3 to 8 percent slopes    | B      | 0.8          | 0.2%           |
| 92                                 | Tomah-Crowfoot loamy sands, 3 to 8 percent slopes | B      | 323.0        | 91.8%          |
| 93                                 | Tomah-Crowfoot complex, 8 to 15 percent slopes    | B      | 28.1         | 8.0%           |
| <b>Totals for Area of Interest</b> |   |        | <b>352.0</b> | <b>100.0%</b>  |

## Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

**Group A.** Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

**Group B.** Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

**Group C.** Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

**Group D.** Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

## Rating Options

*Aggregation Method:* Dominant Condition

*Component Percent Cutoff:* None Specified

*Tie-break Rule:* Higher

# National Flood Hazard Layer FIRMette



## Legend

SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT

- |                                    |  |  |
|------------------------------------|--|--|
| <b>SPECIAL FLOOD HAZARD AREAS</b>  |  | Without Base Flood Elevation (BFE)<br><i>Zone A, V, A99</i>  |
|                                    |  | With BFE or Depth <i>Zone AE, AO, AH, VE, AR</i>   |
|                                    |  | Regulatory Floodway  |
| <b>OTHER AREAS OF FLOOD HAZARD</b> |  | 0.2% Annual Chance Flood Hazard, Areas of 1% annual chance flood with average depth less than one foot or with drainage areas of less than one square mile <i>Zone X</i> |
|                                    |  | Future Conditions 1% Annual Chance Flood Hazard <i>Zone X</i>  |
|                                    |  | Area with Reduced Flood Risk due to Levee. See Notes. <i>Zone X</i>  |
|                                    |  | Area with Flood Risk due to Levee <i>Zone D</i>  |
| <b>OTHER AREAS</b>                 |  | Area of Minimal Flood Hazard <i>Zone X</i>   |
|                                    |  | Effective LOMRs  |
| <b>GENERAL STRUCTURES</b>          |  | Area of Undetermined Flood Hazard <i>Zone D</i>  |
|                                    |  | Channel, Culvert, or Storm Sewer   |
|                                    |  | Levee, Dike, or Floodwall  |
| <b>OTHER FEATURES</b>              |  | 20.2 Cross Sections with 1% Annual Chance Water Surface Elevation  |
|                                    |  | 17.5 Coastal Transect  |
|                                    |  | Base Flood Elevation Line (BFE)  |
|                                    |  | Limit of Study   |
|                                    |  | Jurisdiction Boundary  |
|                                    |  | Coastal Transect Baseline  |
| <b>MAP PANELS</b>                  |  | Digital Data Available   |
|                                    |  | No Digital Data Available  |
|                                    |  | Unmapped   |



The pin displayed on the map is an approximate point selected by the user and does not represent an authoritative property location.

This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The basemap shown complies with FEMA's basemap accuracy standards

The flood hazard information is derived directly from the authoritative NFHL web services provided by FEMA. This map was exported on 4/4/2020 at 4:42:39 PM and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or become superseded by new data over time.

This map image is void if the one or more of the following map elements do not appear: basemap imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for unmapped and unmodernized areas cannot be used for regulatory purposes.



USGS The National Map: Orthoimagery. Data refreshed April, 2019.

0 250 500 1,000 1,500 2,000 Feet

1:6,000

39°4'44.34"N

39°5'12.27"N

104°51'15.23"W

104°50'37.78"W

## **Appendix B**

### **Hydrologic Calculations (Rational)**

## COMPOSITE % IMPERVIOUS & COMPOSITE RUNOFF COEFFICIENT CALCULATIONS

Subdivision: Cloverleaf Subdivision  
 Location: Colorado Springs

Project Name: Cloverleaf Subdivision - Proposed  
 Project No.: 2000-5158.01  
 Calculated By: GAG  
 Checked By: \_\_\_\_\_  
 Date: 8/18/21

| Basin ID        | Total Area (ac) | Paved Streets (100% Imp.) |                  |           |                 | Residential (6k SF min) (62% Imp.) |                  |           |                 | Parks/Open Space (7% Imp.) |                  |           |                 | Basins Total Weighted C Values |                  | Basins Total Weighted % Imp. |
|-----------------|-----------------|---------------------------|------------------|-----------|-----------------|------------------------------------|------------------|-----------|-----------------|----------------------------|------------------|-----------|-----------------|--------------------------------|------------------|------------------------------|
|                 |                 | C <sub>5</sub>            | C <sub>100</sub> | Area (ac) | Weighted % Imp. | C <sub>5</sub>                     | C <sub>100</sub> | Area (ac) | Weighted % Imp. | C <sub>5</sub>             | C <sub>100</sub> | Area (ac) | Weighted % Imp. | C <sub>5</sub>                 | C <sub>100</sub> |                              |
| A               | 4.39            | 0.90                      | 0.96             | 0.69      | 15.8%           | 0.43                               | 0.58             | 3.13      | 44%             | 0.12                       | 0.39             | 0.57      | 0.9%            | 0.47                           | 0.62             | 61.2%                        |
| B               | 3.11            | 0.90                      | 0.96             | 0.00      | 0.0%            | 0.43                               | 0.58             | 2.52      | 51%             | 0.12                       | 0.39             | 0.59      | 1.3%            | 0.38                           | 0.54             | 51.9%                        |
| C               | 1.77            | 0.90                      | 0.96             | 0.41      | 23.3%           | 0.43                               | 0.58             | 1.36      | 48%             | 0.12                       | 0.39             | 0.00      | 0.0%            | 0.54                           | 0.67             | 71.2%                        |
| D               | 3.38            | 0.90                      | 0.96             | 0.40      | 11.8%           | 0.43                               | 0.58             | 2.77      | 51%             | 0.12                       | 0.39             | 0.21      | 0.4%            | 0.47                           | 0.61             | 63.5%                        |
| E               | 0.30            | 0.90                      | 0.96             | 0.14      | 46.5%           | 0.43                               | 0.58             | 0.16      | 33%             | 0.12                       | 0.39             | 0.00      | 0.0%            | 0.65                           | 0.76             | 79.9%                        |
| F               | 1.40            | 0.90                      | 0.96             | 0.32      | 22.9%           | 0.43                               | 0.58             | 1.08      | 48%             | 0.12                       | 0.39             | 0.00      | 0.0%            | 0.54                           | 0.67             | 71.0%                        |
| G               | 0.90            | 0.90                      | 0.96             | 0.31      | 35.2%           | 0.43                               | 0.58             | 0.51      | 36%             | 0.12                       | 0.39             | 0.07      | 0.6%            | 0.57                           | 0.70             | 71.3%                        |
| H               | 4.18            | 0.90                      | 0.96             | 0.48      | 11.5%           | 0.43                               | 0.58             | 2.95      | 44%             | 0.12                       | 0.39             | 0.75      | 1.3%            | 0.43                           | 0.59             | 56.8%                        |
| IA              | 1.71            | 0.90                      | 0.96             | 0.39      | 22.8%           | 0.43                               | 0.58             | 1.32      | 48%             | 0.12                       | 0.39             | 0.00      | 0.0%            | 0.54                           | 0.67             | 71.0%                        |
| I               | 2.76            | 0.90                      | 0.96             | 0.32      | 11.6%           | 0.43                               | 0.58             | 2.44      | 55%             | 0.12                       | 0.39             | 0.00      | 0.0%            | 0.49                           | 0.62             | 66.8%                        |
| J               | 1.39            | 0.90                      | 0.96             | 0.33      | 23.5%           | 0.43                               | 0.58             | 1.07      | 48%             | 0.12                       | 0.39             | 0.00      | 0.0%            | 0.54                           | 0.67             | 71.3%                        |
| K               | 5.29            | 0.90                      | 0.96             | 0.00      | 0.0%            | 0.43                               | 0.58             | 2.75      | 32%             | 0.12                       | 0.39             | 2.54      | 3.4%            | 0.28                           | 0.49             | 35.8%                        |
| Pond 2 Subtotal | 30.6            |                           |                  |           |                 |                                    |                  |           |                 |                            |                  |           |                 |                                |                  | 58.5%                        |
| L               | 1.97            | 0.90                      | 0.96             | 0.14      | 7.1%            | 0.43                               | 0.58             | 1.02      | 32%             | 0.12                       | 0.39             | 0.81      | 2.9%            | 0.34                           | 0.53             | 42.3%                        |
| Pond 3 Subtotal | 1.97            |                           |                  |           |                 |                                    |                  |           |                 |                            |                  |           |                 |                                |                  | 42.3%                        |
| M               | 0.54            | 0.90                      | 0.96             | 0.12      | 21.8%           | 0.43                               | 0.58             | 0.41      | 48%             | 0.12                       | 0.39             | 0.01      | 0.1%            | 0.53                           | 0.66             | 69.6%                        |
| N               | 0.53            | 0.90                      | 0.96             | 0.15      | 28.5%           | 0.43                               | 0.58             | 0.37      | 44%             | 0.12                       | 0.39             | 0.01      | 0.1%            | 0.56                           | 0.69             | 72.1%                        |
| O               | 0.98            | 0.90                      | 0.96             | 0.00      | 0.0%            | 0.43                               | 0.58             | 0.71      | 45%             | 0.12                       | 0.39             | 0.27      | 1.9%            | 0.35                           | 0.53             | 47.2%                        |
| Pond 4 Subtotal | 2.05            |                           |                  |           |                 |                                    |                  |           |                 |                            |                  |           |                 |                                |                  | 59.5%                        |
| OS-1            | 0.41            | 0.90                      | 0.96             | 0.00      | 0.0%            | 0.43                               | 0.58             | 0.41      | 38%             | 0.12                       | 0.39             | 0.00      | 0.0%            | 0.43                           | 0.58             | 37.5%                        |
| OS-2            | 0.79            | 0.90                      | 0.96             | 0.18      | 22.5%           | 0.43                               | 0.58             | 0.00      | 0%              | 0.12                       | 0.39             | 0.61      | 5.4%            | 0.30                           | 0.52             | 28.0%                        |
| OS-3            | 0.31            | 0.90                      | 0.96             | 0.10      | 32.1%           | 0.43                               | 0.58             | 0.00      | 0%              | 0.12                       | 0.39             | 0.21      | 4.8%            | 0.37                           | 0.57             | 36.8%                        |
| OS-4            | 1.00            | 0.90                      | 0.96             | 0.08      | 7.5%            | 0.43                               | 0.58             | 0.65      | 19%             | 0.12                       | 0.39             | 0.27      | 1.9%            | 0.38                           | 0.56             | 28.4%                        |
| OS-5            | 6.12            | 0.90                      | 0.96             | 0.32      | 5.2%            | 0.43                               | 0.58             | 2.30      | 11%             | 0.12                       | 0.39             | 3.50      | 4.0%            | 0.28                           | 0.49             | 20.1%                        |
| TOTAL           | 43.2            |                           |                  |           |                 |                                    |                  |           |                 |                            |                  |           |                 |                                |                  | 50.8%                        |

## STANDARD FORM SF-2 TIME OF CONCENTRATION

Subdivision: Cloverleaf Subdivision  
Location: Colorado Springs

Project Name: Cloverleaf Subdivision - Proposed  
Project No.: 2000-5158.01  
Calculated By: GAG  
Checked By: \_\_\_\_\_  
Date: 8/18/21

| SUB-BASIN |           |                        |                |                |                  | INITIAL/OVERLAND  |                    |                      | TRAVEL TIME         |                    |      |             |                      | tc CHECK                   |                   |                                | FINAL |
|-----------|-----------|------------------------|----------------|----------------|------------------|-------------------|--------------------|----------------------|---------------------|--------------------|------|-------------|----------------------|----------------------------|-------------------|--------------------------------|-------|
| DATA      |           |                        |                |                |                  | (T <sub>i</sub> ) |                    |                      | (T <sub>t</sub> )   |                    |      |             |                      | (URBANIZED BASINS)         |                   |                                |       |
| BASIN ID  | D.A. (ac) | Hydrologic Soils Group | Impervious (%) | C <sub>s</sub> | C <sub>100</sub> | L (ft)            | S <sub>o</sub> (%) | t <sub>i</sub> (min) | L <sub>t</sub> (ft) | S <sub>t</sub> (%) | K    | VEL. (ft/s) | t <sub>t</sub> (min) | COMP. t <sub>c</sub> (min) | TOTAL LENGTH (ft) | Urbanized t <sub>c</sub> (min) |       |
| A         | 4.4       | B                      | 61%            | 0.47           | 0.62             | 115               | 2.4%               | 9.2                  | 688                 | 3.2%               | 20.0 | 3.6         | 3.2                  | 12.4                       | 803.0             | 19.2                           | 12.4  |
| B         | 3.1       | B                      | 52%            | 0.38           | 0.54             | 147               | 8.6%               | 7.8                  | 1156                | 3.5%               | 15.0 | 2.8         | 6.9                  | 14.7                       | 1303.0            | 23.5                           | 14.7  |
| C         | 1.8       | B                      | 71%            | 0.54           | 0.67             | 50                | 5.9%               | 3.9                  | 1001                | 3.3%               | 20.0 | 3.6         | 4.6                  | 8.5                        | 1051.0            | 18.7                           | 8.5   |
| D         | 3.4       | B                      | 63%            | 0.47           | 0.61             | 162               | 3.4%               | 9.7                  | 690                 | 2.9%               | 20.0 | 3.4         | 3.4                  | 13.0                       | 852.0             | 19.0                           | 13.0  |
| E         | 0.3       | B                      | 80%            | 0.65           | 0.76             | 30                | 1.6%               | 3.8                  | 300                 | 4.4%               | 20.0 | 4.2         | 1.2                  | 5.0                        | 330.0             | 13.6                           | 5.0   |
| F         | 1.4       | B                      | 71%            | 0.54           | 0.67             | 60                | 3.0%               | 5.4                  | 553                 | 2.7%               | 20.0 | 3.3         | 2.8                  | 8.2                        | 613.0             | 16.9                           | 8.2   |
| G         | 0.9       | B                      | 71%            | 0.57           | 0.70             | 60                | 9.9%               | 3.5                  | 530                 | 2.1%               | 20.0 | 2.9         | 3.0                  | 6.5                        | 590.0             | 17.1                           | 6.5   |
| H         | 4.2       | B                      | 57%            | 0.43           | 0.59             | 100               | 2.7%               | 8.7                  | 716                 | 1.5%               | 20.0 | 2.4         | 4.9                  | 13.6                       | 816.0             | 22.1                           | 13.6  |
| IA        | 1.7       | B                      | 71%            | 0.54           | 0.67             | 59                | 2.5%               | 5.7                  | 969                 | 1.5%               | 20.0 | 2.4         | 6.6                  | 12.3                       | 1028.0            | 20.9                           | 12.3  |
| I         | 2.8       | B                      | 67%            | 0.49           | 0.62             | 215               | 11.0%              | 7.3                  | 301                 | 1.1%               | 20.0 | 2.1         | 2.4                  | 9.7                        | 516.0             | 17.2                           | 9.7   |
| J         | 1.4       | B                      | 71%            | 0.54           | 0.67             | 60                | 2.5%               | 5.7                  | 405                 | 4.3%               | 20.0 | 4.2         | 1.6                  | 7.4                        | 465.0             | 15.6                           | 7.4   |
| K         | 5.3       | B                      | 36%            | 0.28           | 0.49             | 100               | 6.6%               | 7.9                  | 1073                | 3.2%               | 15.0 | 2.7         | 6.7                  | 14.6                       | 1173.0            | 27.0                           | 14.6  |
| L         | 2.0       | B                      | 42%            | 0.34           | 0.53             | 60                | 2.5%               | 7.9                  | 652                 | 5.0%               | 15.0 | 3.4         | 3.2                  | 11.1                       | 712.0             | 22.1                           | 11.1  |
| M         | 0.5       | B                      | 70%            | 0.53           | 0.66             | 34                | 2.5%               | 4.4                  | 365                 | 5.6%               | 20.0 | 4.7         | 1.3                  | 5.7                        | 399.0             | 15.5                           | 5.7   |
| N         | 0.5       | B                      | 72%            | 0.56           | 0.69             | 60                | 2.5%               | 5.6                  | 365                 | 5.6%               | 20.0 | 4.7         | 1.3                  | 6.9                        | 425.0             | 15.1                           | 6.9   |
| O         | 1.0       | B                      | 47%            | 0.35           | 0.53             | 97                | 15.0%              | 5.5                  | 601                 | 4.1%               | 15.0 | 3.0         | 3.3                  | 8.8                        | 698.0             | 21.2                           | 8.8   |
| OS-1      | 0.4       | B                      | 38%            | 0.43           | 0.58             | 100               | 5.4%               | 6.9                  | 0                   | 1.0%               | 20.0 | 2.0         | 0.0                  | 6.9                        | 100.0             | 19.6                           | 6.9   |
| OS-2      | 0.8       | B                      | 28%            | 0.30           | 0.52             | 13                | 2.0%               | 0.0                  | 205                 | 4.7%               | 20.0 | 4.3         | 0.8                  | 0.8                        | 218.0             | 22.5                           | 5.0   |
| OS-3      | 0.3       | B                      | 37%            | 0.37           | 0.57             | 48                | 9.1%               | 4.4                  | 134                 | 8.0%               | 20.0 | 5.7         | 0.4                  | 4.8                        | 182.0             | 20.3                           | 5.0   |
| OS-4      | 1.0       | B                      | 28%            | 0.38           | 0.56             | 90                | 8.1%               | 6.1                  | 215                 | 5.0%               | 15.0 | 3.4         | 1.1                  | 7.2                        | 305.0             | 22.4                           | 7.2   |
| OS-5      | 6.1       | B                      | 20%            | 0.28           | 0.49             | 300               | 4.1%               | 16.1                 | 955                 | 4.0%               | 15.0 | 3.0         | 5.3                  | 21.4                       | 1255.0            | 29.3                           | 21.4  |

**NOTES:**

$$t_c = t_i + t_t$$

Where:

- t<sub>c</sub> = computed time of concentration (minutes)
- t<sub>i</sub> = overland (initial) flow time (minutes)
- t<sub>t</sub> = channelized flow time (minutes).

$$t_t = \frac{L_t}{60K\sqrt{S_o}} = \frac{L_t}{60V_t}$$

Where:

- t<sub>t</sub> = channelized flow time (travel time, min)
- L<sub>t</sub> = waterway length (ft)
- S<sub>o</sub> = waterway slope (ft/ft)
- V<sub>t</sub> = travel time velocity (ft/sec) = K√S<sub>o</sub>
- K = NRCS conveyance factor (see Table 6-2).

Use a minimum t<sub>t</sub> value of 5 minutes for urbanized areas and a minimum t<sub>c</sub> value of 10 minutes for areas that are not considered urban. Use minimum values even when calculations result in a lesser time of concentration.

Equation 6-2

$$t_i = \frac{0.395(1.1 - C_s)\sqrt{L_i}}{S_o^{0.33}}$$

Equation 6-3

Where:

- t<sub>i</sub> = overland (initial) flow time (minutes)
- C<sub>s</sub> = runoff coefficient for 5-year frequency (from Table 6-4)
- L<sub>i</sub> = length of overland flow (ft)
- S<sub>o</sub> = average slope along the overland flow path (ft/ft).

Equation 6-4

$$t_t = (26 - 17t) + \frac{L_t}{60(14t + 9)\sqrt{S_o}}$$

Equation 6-5

Where:

- t<sub>t</sub> = minimum time of concentration for first design point when less than t<sub>c</sub> from Equation 6-1.
- L<sub>t</sub> = length of channelized flow path (ft)
- t = imperviousness (expressed as a decimal)
- S<sub>o</sub> = slope of the channelized flow path (ft/ft).

Table 6-2. NRCS Conveyance factors, K

| Type of Land Surface                 | Conveyance Factor, K |
|--------------------------------------|----------------------|
| Heavy meadow                         | 2.5                  |
| Tillage/field                        | 5                    |
| Short pasture and lawns              | 7                    |
| Nearly bare ground                   | 10                   |
| Grassed waterway                     | 15                   |
| Paved areas and shallow paved swales | 20                   |

**STANDARD FORM SF-3**  
**STORM DRAINAGE SYSTEM DESIGN**  
**(RATIONAL METHOD PROCEDURE)**

Subdivision: Cloverleaf Subdivision  
 Location: Colorado Springs  
 Design Storm: 5-Year

Project Name: Cloverleaf Subdivision - Proposed  
 Project No.: 2000-5158.01  
 Calculated By: GAG  
 Checked By:  
 Date: 8/18/21

| Design Point | DIRECT RUNOFF |           |               |                      |          |           |         |                      | TOTAL RUNOFF |           |         |                           | STREET   |           |                         | PIPE     |           |                    | TRAVEL TIME |                |                      | REMARKS   |   |
|--------------|---------------|-----------|---------------|----------------------|----------|-----------|---------|----------------------|--------------|-----------|---------|---------------------------|----------|-----------|-------------------------|----------|-----------|--------------------|-------------|----------------|----------------------|---|---|
|              | Basin ID      | Area (Ac) | Runoff Coeff. | t <sub>c</sub> (min) | C*A (Ac) | t (in/hr) | Q (cfs) | t <sub>c</sub> (min) | C*A (ac)     | t (in/hr) | Q (cfs) | Q <sub>street</sub> (cfs) | C*A (ac) | Slope (%) | Q <sub>pipe</sub> (cfs) | C*A (ac) | Slope (%) | Pipe Size (inches) | Length (ft) | Velocity (fps) | t <sub>t</sub> (min) |   |   |
| 1            | A             | 4.39      | 0.47          | 12.4                 | 2.05     | 3.81      | 7.8     |                      |              |           |         | 0.2                       | 0.05     | 2.6       | 7.6                     | 2.00     | 2.0       | 30                 | 1010<br>716 | 3.2<br>8.0     | 5.2<br>1.5           | On-grade Inlet, Carryover flow to DP 3<br>Piped to DP 4.1   |   |
| 4            | D             | 3.38      | 0.47          | 13.0                 | 1.59     | 3.73      | 5.9     |                      |              |           |         |                           |          |           | 5.9                     | 1.59     | 1.0       | 18                 | 48          | 6.1            | 0.1                  | On-grade Inlet, Carryover flow to DP 9<br>Piped to DP 4.1   |   |
| 4.1          |               |           |               |                      |          |           |         | 13.9                 | 3.59         | 3.64      | 13.0    |                           |          |           | 13.0                    | 3.59     | 2.0       | 30                 | 223         | 9.5            | 0.4                  | Sum of DP 1 & DP 4, piped to DP 4.2   |   |
| 2            | B             | 3.11      | 0.38          | 14.7                 | 1.17     | 3.55      | 4.2     |                      |              |           |         |                           |          |           | 4.2                     | 1.17     | 2.0       | 24                 | 147         | 7.0            | 0.4                  | Type C Inlet<br>Piped to DP 4.2   |   |
| 4.2          |               |           |               |                      |          |           |         | 15.0                 | 4.76         | 3.52      | 16.7    |                           |          |           | 16.7                    | 4.76     | 2.0       | 36                 | 223         | 10.0           | 0.4                  | Sum of DP 4.1 & DP 2, piped to DP 4.3   |   |
| 3            | C             | 1.77      | 0.54          | 8.5                  | 0.96     | 4.37      | 4.2     | 8.5                  | 1.01         | 4.37      | 4.4     |                           |          |           | 4.4                     | 1.01     | 2.0       | 18                 | 31          | 7.2            | 0.1                  | On-Grade Inlet, Sum of carryover flow from DP 1 and Sub-Basin C, Carryover flow to DP 14<br>Piped to DP 4.3 |   |
| 4.3          |               |           |               |                      |          |           |         | 15.4                 | 5.77         | 3.48      | 20.1    |                           |          |           | 20.1                    | 5.77     | 2.0       | 36                 | 5           | 10.6           | 0.0                  | Sum of DP 4.2 & DP 3, piped to DP 5.1   |   |
| 5            | E             | 0.30      | 0.65          | 5.0                  | 0.19     | 5.17      | 1.0     |                      |              |           |         |                           |          |           | 1.0                     | 0.19     | 2.0       | 36                 | 0           | 4.2            | 0.0                  | On-grade Inlet<br>Piped to DP 5.1   |   |
| 5.1          |               |           |               |                      |          |           |         | 15.4                 | 5.96         | 3.48      | 20.7    |                           |          |           | 20.7                    | 5.96     | 2.0       | 36                 | 148         | 10.6           | 0.2                  | Sum of DP 4.3 & DP5, piped to DP 10.2   |   |
| 6            | F             | 1.40      | 0.54          | 8.2                  | 0.76     | 4.42      | 3.4     |                      |              |           |         |                           |          |           | 3.4                     | 0.76     | 1.0       | 18                 | 515         | 5.2            | 1.7                  | On-grade Inlet, Carryover flow to DP 8<br>Piped to DP 8.3   |   |
| TB           | TB            | 135.90    | #N/A          | 79.0                 | 43.96    | 1.03      | 45.2    |                      |              |           |         |                           |          |           | 45.2                    | 43.96    | 1.0       | 42                 | 182         | 10.1           | 0.3                  | Proposed Attenuation Pond Outlet Structure Release<br>Piped to DP 8.3                                       |   |
| 7            | G             | 0.90      | 0.57          | 6.5                  | 0.51     | 4.77      | 2.4     |                      |              |           |         | 0.3                       | 0.07     | 4.3       | 2.1                     | 0.44     | 1.0       | 18                 | 470<br>62   | 4.1<br>4.6     | 1.9<br>0.2           | On-grade Inlet, Carryover flow to DP 10<br>Piped to DP 8.1  |   |
| 8            | H             | 4.18      | 0.43          | 13.6                 | 1.80     | 3.67      | 6.6     |                      |              |           |         |                           |          |           | 6.6                     | 1.80     | 1.0       | 24                 | 5           | 6.3            | 0.0                  | Sump Inlet, sum of carryover flow from DP 6 and Sub-Basin H<br>Piped to DP 8.1                              |   |
| 8.1          |               |           |               |                      |          |           |         | 13.6                 | 2.24         | 3.67      | 8.2     |                           |          |           | 8.2                     | 2.24     | 0.7       | 24                 | 37          | 5.8            | 0.1                  | Sum of DP 7 & DP 8, piped to DP 8.2   |   |
| 7A           | IA            | 1.71      | 0.54          | 12.3                 | 0.92     | 3.82      | 3.5     |                      |              |           |         |                           |          |           | 3.5                     | 0.92     | 1.0       | 18                 | 29          | 5.3            | 0.1                  | On-grade Inlet, Carryover flow to DP 9<br>Piped to DP 8.2   |   |
| 8.2          |               |           |               |                      |          |           |         | 13.7                 | 3.16         | 3.66      | 11.6    |                           |          |           | 11.6                    | 3.16     | 1.4       | 30                 | 171         | 8.1            | 0.4                  | Sum of DP 8.1 & DP 7A, piped to DP 8.3  |   |
| 8.3          |               |           |               |                      |          |           |         | 79.3                 | 47.88        | 1.02      | 49.0    |                           |          |           | 49.0                    | 47.88    | 2.0       | 42                 | 293         | 13.4           | 0.4                  | Sum of DP 8.2, DP 6, & DP TB, piped to DP 9.1   |   |
| 9            | I             | 2.76      | 0.49          | 9.7                  | 1.35     | 4.17      | 5.6     |                      |              |           |         |                           |          |           | 5.6                     | 1.35     | 1.0       | 18                 | 0           | 6.0            | 0.0                  | Sump Inlet, sum of carryover flow from DP 4, DP 7A, and Sub-Basin I<br>Piped to DP 9.1                      |   |
| 9.1          |               |           |               |                      |          |           |         | 79.7                 | 49.23        | 1.02      | 50.0    |                           |          |           | 50.0                    | 49.23    | 2.3       | 42                 | 35          | 14.2           | 0.0                  | Sum of DP 8.3 & DP 9, piped to DP 10.1  |   |
| 10           | J             | 1.39      | 0.54          | 7.4                  | 0.76     | 4.59      | 3.5     | 8.4                  | 0.83         | 4.39      | 3.6     |                           |          |           | 3.6                     | 0.83     | 2.0       | 42                 | 0           | 6.2            | 0.0                  | Sump Inlet, sum of carryover flow from DP 7 and Sub-Basin J<br>Piped to DP 10.1                             |   |
| 10.1         |               |           |               |                      |          |           |         | 79.7                 | 50.06        | 1.02      | 50.8    |                           |          |           | 50.8                    | 50.06    | 1.6       | 42                 | 140         | 12.5           | 0.2                  | Sum of DP 9.1 & DP 10, piped to DP 10.2   |   |
| 11           | K             | 5.29      | 0.28          | 14.6                 | 1.50     | 3.56      | 5.3     |                      |              |           |         | 5.3                       | 1.5      | 1.0       |                         |          |           |                    |             |                |                      |   | Swale<br>Swale/Pond conveyance to DP 10.2                   |
| 10.2         |               |           |               |                      |          |           |         | 79.9                 | 57.52        | 1.01      | 58.2    |                           |          |           |                         |          |           |                    |             |                |                      |   | Sum of DP 5.1, DP 10.1, & DP 11<br>Pond P2 Outlet Structure |
| P2           |               |           |               |                      |          |           |         | 80.0                 | 62.08        | 1.01      | 62.7    |                           |          |           | 62.7                    | 62.08    | 2.0       | 42                 | 454         | 14.3           | 0.5                  | Pond P2 Outlet Structure Release<br>Piped to DP 15.2  |   |
| 13           | M             | 0.54      | 0.53          | 5.7                  | 0.28     | 4.97      | 1.4     |                      |              |           |         |                           |          |           | 1.4                     | 0.28     | 1.0       | 18                 | 34          | 4.1            | 0.1                  | On-Grade Inlet, sum of carryover flow from DP 5 and Sub-Basin M<br>Piped to DP 14.1                         |   |
| 14           | N             | 0.53      | 0.56          | 6.9                  | 0.30     | 4.70      | 1.4     |                      |              |           |         |                           |          |           | 1.4                     | 0.30     | 1.0       | 18                 | 0           | 4.0            | 0.0                  | On-Grade Inlet, sum of carryover flow from DP 3 and Sub-Basin N<br>Piped to DP 14.1                         |   |
| 14.1         |               |           |               |                      |          |           |         | 6.9                  | 0.58         | 4.70      | 2.7     |                           |          |           | 2.7                     | 0.58     | 1.0       | 18                 | 31          | 4.9            | 0.1                  | Sum of DP 13 & DP 14<br>Piped to DP 15.1  |   |
| 15           | O             | 0.98      | 0.35          | 8.8                  | 0.34     | 4.33      | 1.5     |                      |              |           |         | 1.5                       | 0.34     | 0.5       |                         |          |           |                    |             |                |                      |   | Swale<br>Swale/pond conveyance to DP 15.1                   |

STANDARD FORM SF-3  
STORM DRAINAGE SYSTEM DESIGN  
(RATIONAL METHOD PROCEDURE)

Subdivision: Cloverleaf Subdivision  
Location: Colorado Springs  
Design Storm: 5-Year

Project Name: Cloverleaf Subdivision - Proposed  
Project No.: 2000-5158.01  
Calculated By: GAG  
Checked By:  
Date: 8/18/21

| Design Point | DIRECT RUNOFF |           |               |                      |          |           |         |                      | TOTAL RUNOFF |           |         |                           | STREET   |           |                         | PIPE     |           |                    | TRAVEL TIME |                |                      | REMARKS   |   |
|--------------|---------------|-----------|---------------|----------------------|----------|-----------|---------|----------------------|--------------|-----------|---------|---------------------------|----------|-----------|-------------------------|----------|-----------|--------------------|-------------|----------------|----------------------|---|---|
|              | Basin ID      | Area (Ac) | Runoff Coeff. | t <sub>c</sub> (min) | C*A (Ac) | I (in/hr) | Q (cfs) | t <sub>c</sub> (min) | C*A (ac)     | I (in/hr) | Q (cfs) | Q <sub>street</sub> (cfs) | C*A (ac) | Slope (%) | Q <sub>pipe</sub> (cfs) | C*A (ac) | Slope (%) | Pipe Size (inches) | Length (ft) | Velocity (fps) | t <sub>t</sub> (min) |   |   |
| 15.1         |               |           |               |                      |          |           |         | 8.8                  | 0.92         | 4.33      | 4.0     |                           |          |           | 4.0                     | 0.92     | 0.5       | 18                 | 80          | 4.2            | 0.3                  | Sum of DP 14.1 & DP 15<br>Water quality pond outlet structure<br>Sum of DP P2 and DP 15.1<br>Piped to DP L1.1 |   |
| 15.2         |               |           |               |                      |          |           |         | 80.5                 | 63.00        | 1.00      | 63.0    |                           |          |           | 63.0                    | 63.00    | 2.5       | 48                 | 116         | 15.5           | 0.1                  | Type C Inlet<br>Swale flows offsite along Leggins Way to DP L1. Piped to DP L1.0                              |   |
| L1           | OS-5          | 6.12      | 0.28          | 21.4                 | 1.71     | 2.99      | 5.1     |                      |              |           |         | 5.1                       | 1.71     | 4.0       |                         |          |           |                    |             |                |                      |   | Type C Inlet<br>Sheet flows offsite to DP L1, Piped to DP L1.0                    |
| L1           | OS-2          | 0.79      | 0.30          | 5.0                  | 0.23     | 5.17      | 1.2     |                      |              |           |         | 1.2                       | 0.23     | 1.0       |                         |          |           |                    |             |                |                      |   | Sheet flows offsite to DP L1, Piped to DP L1.0                                    |
| L1.0         |               |           |               |                      |          |           |         | 21.4                 | 1.94         | 2.99      | 5.8     |                           |          |           | 5.8                     | 1.94     | 1.2       | 24                 | 51          | 6.4            | 0.1                  | Sum of Sub-Basin OS-2 and Sub-Basin OS-5<br>Piped to DP L1.1  |   |
| L1.1         |               |           |               |                      |          |           |         | 80.7                 | 64.94        | 1.00      | 64.8    |                           |          |           | 64.8                    | 64.94    | 1.8       | 48                 | 116         | 13.8           | 0.1                  | Sum of DP 15.2 and DP L1.0<br>Piped to outfall O1   |   |
| 12           | L             | 1.97      | 0.34          | 11.1                 | 0.67     | 3.97      | 2.7     |                      |              |           |         | 2.7                       | 0.67     | 1.0       |                         |          |           |                    |             |                |                      |   | Swale<br>Swale/Pond conveyance to DP 12   |
| 16           | US-1          | 0.41      | 0.43          | 6.9                  | 0.18     | 4.69      | 0.8     |                      |              |           |         | 0.8                       | 0.18     | 1.0       |                         |          |           |                    |             |                |                      |   | Overland Flow<br>Sheet flows offsite to DP 16 to the proposed attenuation pond P1 |
| 18           | OS-3          | 0.31      | 0.37          | 5.0                  | 0.11     | 5.17      | 0.6     |                      |              |           |         | 0.6                       | 0.11     | 1.0       |                         |          |           |                    |             |                |                      |   | Overland Flow<br>Sheet flows offsite to DP 18                                     |
| 19           | OS-4          | 1.00      | 0.38          | 7.2                  | 0.38     | 4.62      | 1.8     |                      |              |           |         | 1.8                       | 0.38     | 1.0       |                         |          |           |                    |             |                |                      |   | Overland Flow<br>Sheet flows offsite to DP 19                                     |

STANDARD FORM SF-3  
 STORM DRAINAGE SYSTEM DESIGN  
 (RATIONAL METHOD PROCEDURE)

Subdivision: Cloverleaf Subdivision  
 Location: Colorado Springs  
 Design Storm: 100-Year

Project Name: Cloverleaf Subdivision - Proposed  
 Project No.: 2000-5158  
 Calculated By: GAG  
 Checked By:  
 Date: 8/18/21

| Design Point | DIRECT RUNOFF |           |               |                      |          |           |         | TOTAL RUNOFF         |          |           | STREET  |                           |          | PIPE      |                         |          | TRAVEL TIME |                    |             | REMARKS |                |   |
|--------------|---------------|-----------|---------------|----------------------|----------|-----------|---------|----------------------|----------|-----------|---------|---------------------------|----------|-----------|-------------------------|----------|-------------|--------------------|-------------|---------|----------------|---|
|              | Basin ID      | Area (ac) | Runoff Coeff. | t <sub>c</sub> (min) | C*A (ac) | Q (in/hr) | Q (cfs) | t <sub>c</sub> (min) | C*A (ac) | Q (in/hr) | Q (cfs) | Q <sub>street</sub> (cfs) | C*A (ac) | Slope (%) | Q <sub>pipe</sub> (cfs) | C*A (ac) | Slope (%)   | Pipe Size (inches) | Length (ft) |         | Velocity (fps) | t <sub>t</sub> (min)  |
| 1            | A             | 4.39      | 0.62          | 12.4                 | 2.70     | 6.39      | 17.3    |                      |          |           |         | 3.4                       | 0.53     | 2.6       | 13.9                    | 2.17     | 2.0         | 30                 | 1010        | 3.2     | 5.2            | On-grade Inlet, Carryover flow to DP 3<br>Piped to DP 4.1   |
| 4            | D             | 3.38      | 0.61          | 13.0                 | 2.07     | 6.26      | 13.0    |                      |          |           |         | 1.6                       | 0.25     | 1.1       | 11.4                    | 1.82     | 1.0         | 18                 | 339         | 2.1     | 2.7            | On-grade Inlet, Carryover flow to DP 9<br>Piped to DP 4.1   |
| 4.1          |               |           |               |                      |          |           |         | 13.6                 | 3.99     | 6.15      | 24.6    |                           |          |           | 24.6                    | 3.99     | 2.0         | 30                 | 223         | 11.3    | 0.3            | Sum of DP 1 & DP 4, piped to DP 4.2<br>Type C Inlet<br>Piped to DP 4.2  |
| 2            | B             | 3.11      | 0.54          | 14.7                 | 1.69     | 5.97      | 10.1    |                      |          |           |         |                           |          |           | 10.1                    | 1.69     | 2.0         | 24                 | 147         | 8.9     | 0.3            | Piped to DP 4.2   |
| 4.2          |               |           |               |                      |          |           |         | 14.9                 | 5.68     | 5.92      | 33.6    |                           |          |           | 33.6                    | 5.68     | 2.0         | 36                 | 223         | 12.2    | 0.3            | Sum of DP 4.1 & DP 2, piped to DP 4.3   |
| 3            | C             | 1.77      | 0.67          | 8.5                  | 1.18     | 7.33      | 8.7     | 17.6                 | 1.71     | 5.51      | 9.4     | 0.2                       | 0.04     | 5.5       | 9.2                     | 1.67     | 2.0         | 18                 | 377         | 4.7     | 1.3            | On-Grade Inlet, Sum of carryover flow from DP 1 and Sub-Basin C, Carryover flow to DP 14<br>Piped to DP 4.3                             |
| 4.3          |               |           |               |                      |          |           |         | 17.7                 | 7.35     | 5.50      | 40.4    |                           |          |           | 40.4                    | 7.35     | 2.0         | 36                 | 5           | 12.7    | 0.0            | Sum of DP 4.2 & DP 3, piped to DP 5.1<br>On-grade Inlet<br>Piped to DP 5.1  |
| 5            | E             | 0.30      | 0.76          | 5.0                  | 0.23     | 8.68      | 2.0     |                      |          |           |         |                           |          |           | 2.0                     | 0.23     | 2.0         | 36                 | 0           | 5.2     | 0.0            | On-grade Inlet<br>Piped to DP 5.1   |
| 5.1          |               |           |               |                      |          |           |         | 17.7                 | 7.58     | 5.50      | 41.7    |                           |          |           | 41.7                    | 7.58     | 2.0         | 36                 | 148         | 12.9    | 0.2            | Sum of DP 4.3 & DP 5, piped to DP 10.2<br>On-grade Inlet, Carryover flow to DP 8<br>Piped to DP 8.3                                     |
| 6            | F             | 1.40      | 0.67          | 8.24                 | 0.93     | 7.42      | 6.9     |                      |          |           |         | 0.9                       | 0.12     | 1.5       | 6.0                     | 0.81     | 1.0         | 18                 | 722         | 2.4     | 4.9            | On-grade Inlet, Carryover flow to DP 8<br>Piped to DP 8.3   |
| TB           | TB            | 135.90    | #N/A          | 106                  | 79.88    | 0.98      | 78.5    |                      |          |           |         |                           |          |           | 78.5                    | 79.88    | 1.0         | 42                 | 182         | 11.5    | 0.3            | Proposed Attenuation Pond Outlet Structure Release<br>Piped to DP 8.3   |
| 7            | G             | 0.90      | 0.70          | 6.5                  | 0.63     | 8.02      | 5.1     |                      |          |           |         | 2.1                       | 0.26     | 6.5       | 3.0                     | 0.37     | 2.0         | 18                 | 470         | 5.1     | 1.5            | On-grade Inlet, Carryover flow to DP 10<br>Piped to DP 8.1  |
| 8            | H             | 4.18      | 0.59          | 13.6                 | 2.47     | 6.16      | 15.2    | 13.6                 | 2.59     | 6.16      | 16.0    |                           |          |           | 16.0                    | 2.59     | 1.0         | 24                 | 5           | 7.8     | 0.0            | Sump Inlet, sum of carryover flow from DP 6 and Sub-Basin H<br>Piped to DP 8.1  |
| 8.1          |               |           |               |                      |          |           |         | 13.6                 | 2.97     | 6.16      | 18.3    |                           |          |           | 18.3                    | 2.97     | 0.7         | 24                 | 37          | 6.9     | 0.1            | Sum of DP 7 & DP 8, piped to DP 8.2<br>On-grade Inlet, Carryover flow to DP 9<br>Piped to DP 8.2  |
| 7A           | IA            | 1.71      | 0.67          | 12.3                 | 1.14     | 6.41      | 7.3     |                      |          |           |         | 1.1                       | 0.17     | 6.5       | 6.2                     | 0.97     | 5.4         | 18                 | 423         | 5.1     | 1.4            | On-grade Inlet, Carryover flow to DP 9<br>Piped to DP 8.2   |
| 8.2          |               |           |               |                      |          |           |         | 13.7                 | 3.93     | 6.15      | 24.2    |                           |          |           | 24.2                    | 3.93     | 1.4         | 30                 | 171         | 9.9     | 0.3            | Sum of DP 8.1 & DP 7A, piped to DP 8.3  |
| 8.3          |               |           |               |                      |          |           |         | 106.3                | 84.62    | 0.98      | 82.7    |                           |          |           | 82.7                    | 84.62    | 2.0         | 42                 | 293         | 15.3    | 0.3            | Sum of DP 8.2, DP 6, & DP TB, piped to DP 9.1<br>Sump Inlet, sum of carryover flow from DP 4, DP 7A, and Sub-Basin I<br>Piped to DP 9.1 |
| 9            | I             | 2.76      | 0.62          | 9.7                  | 1.72     | 7.00      | 12.0    | 15.7                 | 2.14     | 5.79      | 12.4    |                           |          |           | 12.4                    | 2.14     | 1.0         | 18                 | 0           | 7.0     | 0.0            | Sum of DP 8.3 & DP 9, piped to DP 10.1<br>Sump Inlet, sum of carryover flow from DP 7 and Sub-Basin J<br>Piped to DP 10.1               |
| 9.1          |               |           |               |                      |          |           |         | 106.6                | 86.76    | 0.97      | 84.1    |                           |          |           | 84.1                    | 86.76    | 2.3         | 42                 | 35          | 16.2    | 0.0            | Sum of DP 8.3 & DP 9, piped to DP 10.1  |
| 10           | J             | 1.39      | 0.67          | 7.4                  | 0.93     | 7.70      | 7.2     | 8.0                  | 1.19     | 7.48      | 8.9     |                           |          |           | 8.9                     | 1.19     | 2.0         | 42                 | 0           | 8.1     | 0.0            | Sump Inlet, sum of carryover flow from DP 7 and Sub-Basin J<br>Piped to DP 10.1   |
| 10.1         |               |           |               |                      |          |           |         | 106.6                | 87.95    | 0.97      | 85.2    |                           |          |           | 85.2                    | 87.95    | 1.6         | 42                 | 140         | 14.1    | 0.2            | Sum of DP 9.1 & DP 10, piped to DP 10.2<br>Swale<br>Swale/Pond conveyance to DP 10.2  |
| 11           | K             | 5.29      | 0.49          | 14.6                 | 2.59     | 5.98      | 15.5    |                      |          |           |         | 15.5                      | 2.59     | 1.0       |                         |          |             |                    | 366         | 2.0     | 3.1            | Swale<br>Swale/Pond conveyance to DP 10.2   |
| 10.2         |               |           |               |                      |          |           |         | 106.8                | 98.12    | 0.96      | 94.6    |                           |          |           |                         |          |             |                    |             |         |                | Sum of DP 5.1, DP 10.1, & DP 11<br>Pond P2 Outlet Structure<br>Pond P2 Outlet Structure Release<br>Piped to DP 15.2                     |
| P2           |               |           |               |                      |          |           |         | 78.0                 | 61.97    | 1.76      | 108.8   |                           |          |           | 108.8                   | 61.97    | 2.0         | 42                 | 454         | 16.3    | 0.5            | Sum of DP 5.1, DP 10.1, & DP 11<br>Pond P2 Outlet Structure<br>Pond P2 Outlet Structure Release<br>Piped to DP 15.2                     |
| 13           | M             | 0.54      | 0.66          | 5.7                  | 0.35     | 8.34      | 2.9     |                      |          |           |         |                           |          |           | 2.9                     | 0.35     | 1.0         | 18                 | 34          | 5.1     | 0.1            | On-Grade Inlet, sum of carryover flow from DP 5 and Sub-Basin M<br>Piped to DP 14.1   |
| 14           | N             | 0.53      | 0.69          | 6.9                  | 0.36     | 7.88      | 2.8     | 18.9                 | 0.40     | 5.32      | 2.1     |                           |          |           | 2.1                     | 0.40     | 1.0         | 18                 | 0           | 4.6     | 0.0            | On-Grade Inlet, sum of carryover flow from DP 3 and Sub-Basin N<br>Piped to DP 14.1   |
| 14.1         |               |           |               |                      |          |           |         | 18.9                 | 0.75     | 5.32      | 4.0     |                           |          |           | 4.0                     | 0.75     | 1.0         | 18                 | 31          | 5.5     | 0.1            | Sum of DP 13 & DP 14<br>Piped to DP 15.1  |
| 15           | O             | 0.98      | 0.53          | 8.8                  | 0.52     | 7.26      | 3.8     |                      |          |           |         | 3.8                       | 0.52     | 0.5       |                         |          |             |                    |             |         |                | Swale<br>Swale/pond conveyance to DP 15.1   |

STANDARD FORM SF-3  
STORM DRAINAGE SYSTEM DESIGN  
(RATIONAL METHOD PROCEDURE)

Subdivision: Cloverleaf Subdivision  
Location: Colorado Springs  
Design Storm: 100-Year

Project Name: Cloverleaf Subdivision - Proposed  
Project No.: 2000-5158  
Calculated By: GAG  
Checked By:  
Date: 8/18/21

| Design Point | DIRECT RUNOFF |           |               |             |          |             |           |             | TOTAL RUNOFF |             |           |                    | STREET   |           |                  | PIPE     |           |                    | TRAVEL TIME |                |             | REMARKS   |   |
|--------------|---------------|-----------|---------------|-------------|----------|-------------|-----------|-------------|--------------|-------------|-----------|--------------------|----------|-----------|------------------|----------|-----------|--------------------|-------------|----------------|-------------|---|---|
|              | Basin ID      | Area (ac) | Runoff Coeff. | $t_c$ (min) | C*A (ac) | $I$ (in/hr) | $Q$ (cfs) | $t_c$ (min) | C*A (ac)     | $I$ (in/hr) | $Q$ (cfs) | $Q_{street}$ (cfs) | C*A (ac) | Slope (%) | $Q_{pipe}$ (cfs) | C*A (ac) | Slope (%) | Pipe Size (inches) | Length (ft) | Velocity (fps) | $t_t$ (min) |   |   |
| 15.1         |               |           |               |             |          |             |           | 19.0        | 1.27         | 5.31        | 6.7       |                    |          |           | 6.7              | 1.27     | 0.5       | 18                 | 80          | 4.8            | 0.3         | Sum of DP 14.1 & DP 15<br>Water quality pond outlet structure<br>Sum of DP P2 and DP 15.1<br>Piped to DP L1.1 |   |
| 15.2         |               |           |               |             |          |             |           | 78.5        | 63.23        | 1.74        | 110.1     |                    |          |           | 110.1            | 63.23    | 2.5       | 48                 | 116         | 17.9           | 0.1         | Type C Inlet<br>Swale flows offsite along Leggins Way to DP L1, Piped to DP L1.0                              |   |
| L1           | OS-5          | 6.12      | 0.49          | 21.4        | 3.01     | 5.01        | 15.1      |             |              |             |           | 15.1               | 3.01     | 1.0       |                  |          |           |                    |             |                |             |   | Type C Inlet<br>Sheet flows offsite to DP L1, Piped to DP L1.0                    |
| L1           | OS-2          | 0.79      | 0.52          | 5.0         | 0.41     | 8.68        | 3.6       |             |              |             |           | 3.6                | 0.41     | 1.0       |                  |          |           |                    |             |                |             |   | Type C Inlet<br>Sheet flows offsite to DP L1, Piped to DP L1.0                    |
| L1.0         |               |           |               |             |          |             |           | 21.4        | 3.42         | 5.01        | 17.1      |                    |          |           | 17.1             | 3.42     | 1.2       | 24                 | 51          | 8.5            | 0.1         | Sum of Sub-Basin OS-2 and Sub-Basin OS-5<br>Piped to DP L1.1  |   |
| L1.1         |               |           |               |             |          |             |           | 78.6        | 66.65        | 1.74        | 115.8     |                    |          |           | 115.8            | 66.65    | 1.8       | 48                 | 116         | 16.0           | 0.1         | Sum of DP T5.2 and DP L1.0<br>Piped to outfall O1   |   |
| 12           | L             | 1.97      | 0.53          | 11.1        | 1.04     | 6.67        | 6.9       |             |              |             |           | 6.9                | 1.04     | 1.0       |                  |          |           |                    |             |                |             |   | Swale<br>Swale/Pond conveyance to DP 12   |
| 16           | OS-1          | 0.41      | 0.58          | 6.9         | 0.24     | 7.87        | 1.9       |             |              |             |           | 1.9                | 0.24     | 1.0       |                  |          |           |                    |             |                |             |   | Overland Flow<br>Sheet flows offsite to DP 16 to the proposed attenuation pond P1 |
| 18           | OS-3          | 0.31      | 0.57          | 5.0         | 0.18     | 8.68        | 1.6       |             |              |             |           | 1.6                | 0.18     | 1.0       |                  |          |           |                    |             |                |             |   | Overland Flow<br>Sheet flows offsite to DP 18                                     |
| 19           | OS-4          | 1.00      | 0.56          | 7.2         | 0.56     | 7.76        | 4.3       |             |              |             |           | 4.3                | 0.56     | 1.0       |                  |          |           |                    |             |                |             |   | Overland Flow<br>Sheet flows offsite to DP 19                                     |

**Appendix C**  
**Hydrologic Calculations (CUHP/SWMM)**

**Summary of CUHP Input Parameters (Version 2.0.1)**  
**Existing Condition - 5yr**

| Catchment Name/ID | SWMM Node/ID | Raingage Name/ID         | Area (sq.mi.) | Dist. to Centroid (miles) | Length (miles) | Slope (ft./ft.) | Percent Imperv. | Depression Storage |                  | Horton's Infiltration Parameters |                      |                       | DCIA Level and Fractions |                              |                        | Percent Eff. Imperv. |
|-------------------|--------------|--------------------------|---------------|---------------------------|----------------|-----------------|-----------------|--------------------|------------------|----------------------------------|----------------------|-----------------------|--------------------------|------------------------------|------------------------|----------------------|
|                   |              |                          |               |                           |                |                 |                 | Pervious (inches)  | Imperv. (inches) | Initial Rate (in./hr.)           | Final Rate (in./hr.) | Decay Coeff. (1/sec.) | DCIA Level               | Dir. Con'ct Imperv. Fraction | Receiv. Perv. Fraction |                      |
| TX-1              | 1            | 2-HOUR DESIGN STORM 5 YR | 0.170         | 0.665                     | 1.056          | 0.060           | 23.5            | 0.50               | 0.10             | 4.50                             | 0.60                 | 0.0018                | 2.00                     | 0.12                         | 0.38                   | 18.41                |
| TX-2              | 2            | 2-HOUR DESIGN STORM 5 YR | 0.043         | 0.263                     | 0.544          | 0.060           | 16.0            | 0.50               | 0.10             | 4.50                             | 0.60                 | 0.0018                | 2.00                     | 0.08                         | 0.34                   | 12.08                |
| SX-3              | 3            | 2-HOUR DESIGN STORM 5 YR | 0.043         | 0.234                     | 0.323          | 0.040           | 0.0             | 0.50               | 0.10             | 4.50                             | 0.60                 | 0.0018                | 2.00                     | 0.00                         | 0.00                   | 0.00                 |
| SX-4              | 4            | 2-HOUR DESIGN STORM 5 YR | 0.008         | 0.132                     | 0.200          | 0.060           | 4.8             | 0.50               | 0.10             | 4.50                             | 0.60                 | 0.0018                | 2.00                     | 0.00                         | 0.14                   | 3.41                 |
| SX-5              | 5            | 2-HOUR DESIGN STORM 5 YR | 0.007         | 0.086                     | 0.144          | 0.060           | 4.0             | 0.50               | 0.10             | 4.50                             | 0.60                 | 0.0018                | 2.00                     | 0.00                         | 0.12                   | 2.84                 |
| SX-6              | 6            | 2-HOUR DESIGN STORM 5 YR | 0.077         | 0.259                     | 0.698          | 0.050           | 16.9            | 0.50               | 0.10             | 4.50                             | 0.60                 | 0.0018                | 2.00                     | 0.08                         | 0.34                   | 12.82                |

**Summary of Unit Hydrograph Parameters Used By Program and Calculated Results (Version 2.0.1)**

**Existing Condition - 5yr**

| Catchment Name/ID | User Comment for Catchment | Unit Hydrograph Parameters and Results |       |               |                       |               |                       |                           |            |                 | Excess Precip.     |                  | Storm Hydrograph          |                    |                           |                                       |
|-------------------|----------------------------|--|-------|---------------|-----------------------|---------------|-----------------------|---------------------------|------------|-----------------|--------------------|------------------|---------------------------|--------------------|---------------------------|---------------------------------------|
|                   |                            | CT                                     | Cp    | W50<br>(min.) | W50<br>Before<br>Peak | W75<br>(min.) | W75<br>Before<br>Peak | Time to<br>Peak<br>(min.) | Peak (cfs) | Volume<br>(c.f) | Excess<br>(inches) | Excess<br>(c.f.) | Time to<br>Peak<br>(min.) | Peak<br>Flow (cfs) | Total<br>Volume<br>(c.f.) | Runoff per<br>Unit Area<br>(cfs/acre) |
| TX-1              |                            | 0.113                                  | 0.165 | 53.0          | 7.02                  | 27.6          | 4.96                  | 11.7                      | 96         | 394,581         | 0.54               | 213,183          | 60.0                      | 47                 | 213,182                   | 0.43                                  |
| TX-2              |                            | 0.122                                  | 0.092 | 48.3          | 3.70                  | 25.1          | 2.62                  | 6.2                       | 26         | 98,736          | 0.46               | 45,815           | 56.0                      | 11                 | 45,815                    | 0.40                                  |
| SX-3              |                            | 0.163                                  | 0.118 | 40.5          | 3.98                  | 21.0          | 2.81                  | 6.6                       | 32         | 100,188         | 0.31               | 31,003           | 55.0                      | 9                  | 31,001                    | 0.33                                  |
| SX-4              |                            | 0.150                                  | 0.052 | 46.7          | 2.16                  | 24.3          | 1.52                  | 3.6                       | 5          | 18,876          | 0.35               | 6,696            | 54.0                      | 2                  | 6,696                     | 0.32                                  |
| SX-5              |                            | 0.152                                  | 0.048 | 35.5          | 1.61                  | 18.5          | 1.14                  | 2.7                       | 6          | 15,609          | 0.35               | 5,419            | 51.0                      | 2                  | 5,418                     | 0.40                                  |
| SX-6              |                            | 0.121                                  | 0.119 | 43.1          | 4.23                  | 22.4          | 2.99                  | 7.1                       | 53         | 178,233         | 0.47               | 84,305           | 55.0                      | 22                 | 84,302                    | 0.45                                  |

**Summary of CUHP Input Parameters (Version 2.0.1)**

**Existing Condition - 100yr**

| Catchment Name/ID | SWMM Node/ID | Raingage Name/ID    | Area (sq.mi.) | Dist. to Centroid (miles) | Length (miles) | Slope (ft./ft.) | Percent Imperv. | Depression Storage |                  | Horton's Infiltration Parameters |                      |                       | DCIA Level and Fractions |                              |                        | Percent Eff. Imperv. |
|-------------------|--------------|---------------------|---------------|---------------------------|----------------|-----------------|-----------------|--------------------|------------------|----------------------------------|----------------------|-----------------------|--------------------------|------------------------------|------------------------|----------------------|
|                   |              |                     |               |                           |                |                 |                 | Pervious (inches)  | Imperv. (inches) | Initial Rate (in./hr.)           | Final Rate (in./hr.) | Decay Coeff. (1/sec.) | DCIA Level               | Dir. Con'ct Imperv. Fraction | Receiv. Perv. Fraction |                      |
| TX-1              | 1            | 2-HOUR DESIGN STORM | 0.170         | 0.665                     | 1.056          | 0.060           | 23.5            | 0.50               | 0.10             | 4.50                             | 0.60                 | 0.0018                | 2.00                     | 0.12                         | 0.38                   | 20.24                |
| TX-2              | 2            | 2-HOUR DESIGN STORM | 0.043         | 0.263                     | 0.544          | 0.060           | 16.0            | 0.50               | 0.10             | 4.50                             | 0.60                 | 0.0018                | 2.00                     | 0.08                         | 0.34                   | 13.47                |
| SX-3              | 3            | 2-HOUR DESIGN STORM | 0.043         | 0.234                     | 0.323          | 0.040           | 0.0             | 0.50               | 0.10             | 4.50                             | 0.60                 | 0.0018                | 2.00                     | 0.00                         | 0.00                   | 0.00                 |
| SX-4              | 4            | 2-HOUR DESIGN STORM | 0.008         | 0.132                     | 0.200          | 0.060           | 4.8             | 0.50               | 0.10             | 4.50                             | 0.60                 | 0.0018                | 2.00                     | 0.00                         | 0.14                   | 3.89                 |
| SX-5              | 5            | 2-HOUR DESIGN STORM | 0.007         | 0.086                     | 0.144          | 0.060           | 4.0             | 0.50               | 0.10             | 4.50                             | 0.60                 | 0.0018                | 2.00                     | 0.00                         | 0.12                   | 3.24                 |
| SX-6              | 6            | 2-HOUR DESIGN STORM | 0.077         | 0.259                     | 0.698          | 0.050           | 16.9            | 0.50               | 0.10             | 4.50                             | 0.60                 | 0.0018                | 2.00                     | 0.08                         | 0.34                   | 14.27                |

**Summary of Unit Hydrograph Parameters Used By Program and Calculated Results (Version 2.0.1)**

**Existing Condition - 100yr**

| Catchment Name/ID | User Comment for Catchment | Unit Hydrograph Parameters and Results |       |               |                       |               |                       |                           |            |                 | Excess Precip.     |                  | Storm Hydrograph          |                    |                           |                                       |
|-------------------|----------------------------|--|-------|---------------|-----------------------|---------------|-----------------------|---------------------------|------------|-----------------|--------------------|------------------|---------------------------|--------------------|---------------------------|---------------------------------------|
|                   |                            | CT                                     | Cp    | W50<br>(min.) | W50<br>Before<br>Peak | W75<br>(min.) | W75<br>Before<br>Peak | Time to<br>Peak<br>(min.) | Peak (cfs) | Volume<br>(c.f) | Excess<br>(inches) | Excess<br>(c.f.) | Time to<br>Peak<br>(min.) | Peak<br>Flow (cfs) | Total<br>Volume<br>(c.f.) | Runoff per<br>Unit Area<br>(cfs/acre) |
| TX-1              |                            | 0.110                                  | 0.164 | 52.2          | 6.87                  | 27.1          | 4.86                  | 11.5                      | 98         | 394,581         | 1.46               | 577,723          | 59.0                      | 125                | 577,720                   | 1.15                                  |
| TX-2              |                            | 0.120                                  | 0.091 | 47.9          | 3.64                  | 24.9          | 2.57                  | 6.1                       | 27         | 98,736          | 1.38               | 136,205          | 55.0                      | 31                 | 136,206                   | 1.15                                  |
| SX-3              |                            | 0.163                                  | 0.118 | 40.5          | 3.98                  | 21.0          | 2.81                  | 6.6                       | 32         | 100,188         | 1.21               | 121,642          | 54.0                      | 33                 | 121,635                   | 1.20                                  |
| SX-4              |                            | 0.149                                  | 0.051 | 46.7          | 2.13                  | 24.3          | 1.51                  | 3.6                       | 5          | 18,876          | 1.26               | 23,820           | 53.0                      | 6                  | 23,818                    | 1.08                                  |
| SX-5              |                            | 0.151                                  | 0.048 | 35.5          | 1.60                  | 18.5          | 1.13                  | 2.7                       | 6          | 15,609          | 1.25               | 19,573           | 51.0                      | 6                  | 19,570                    | 1.35                                  |
| SX-6              |                            | 0.119                                  | 0.118 | 42.7          | 4.16                  | 22.2          | 2.94                  | 6.9                       | 54         | 178,233         | 1.39               | 247,637          | 54.0                      | 63                 | 247,623                   | 1.28                                  |

\*\*\*\*\*  
NOTE: The summary statistics displayed in this report are based on results found at every computational time step, not just on results from each reporting time step.  
\*\*\*\*\*

\*\*\*\*\*  
Analysis Options

\*\*\*\*\*  
Flow Units ..... CFS  
Process Models:  
  Rainfall/Runoff ..... NO  
  RDII ..... NO  
  Snowmelt ..... NO  
  Groundwater ..... NO  
  Flow Routing ..... YES  
  Ponding Allowed ..... NO  
  Water Quality ..... NO  
Flow Routing Method ..... KINWAVE  
Starting Date ..... 01/01/2005 00:00:00  
Ending Date ..... 01/04/2005 06:00:00  
Antecedent Dry Days ..... 0.0  
Report Time Step ..... 00:15:00  
Routing Time Step ..... 30.00 sec

|                            | Volume<br>acre-feet | Volume<br>10 <sup>6</sup> gal |
|----------------------------|---------------------|-------------------------------|
| Flow Routing Continuity    |                     |                               |
| Dry Weather Inflow .....   | 38.674              | 12.603                        |
| Wet Weather Inflow .....   | 0.000               | 0.000                         |
| Groundwater Inflow .....   | 0.000               | 0.000                         |
| RDII Inflow .....          | 0.000               | 0.000                         |
| External Inflow .....      | 8.871               | 2.891                         |
| External Outflow .....     | 47.545              | 15.493                        |
| Flooding Loss .....        | 0.000               | 0.000                         |
| Evaporation Loss .....     | 0.000               | 0.000                         |
| Exfiltration Loss .....    | 0.000               | 0.000                         |
| Initial Stored Volume .... | 0.000               | 0.000                         |
| Final Stored Volume .....  | 0.000               | 0.000                         |
| Continuity Error (%) ..... | 0.000               |                               |

\*\*\*\*\*  
Highest Flow Instability Indexes

\*\*\*\*\*  
All links are stable.

\*\*\*\*\*  
Routing Time Step Summary

\*\*\*\*\*  
Minimum Time Step : 30.00 sec  
Average Time Step : 30.00 sec  
Maximum Time Step : 30.00 sec  
Percent in Steady State : 0.00  
Average Iterations per Step : 1.00  
Percent Not Converging : 0.00

\*\*\*\*\*  
Node Depth Summary  
\*\*\*\*\*

| Node         | Type     | Average Depth Feet | Maximum Depth Feet | Maximum HGL Feet | Time of Max Occurrence days hr:min | Reported Max Depth Feet |
|--------------|----------|--------------------|--------------------|------------------|------------------------------------|-------------------------|
| 1            | JUNCTION | 0.00               | 0.00               | 7409.00          | 0 00:00                            | 0.00                    |
| 2            | JUNCTION | 0.00               | 0.00               | 7226.00          | 0 00:00                            | 0.00                    |
| 3            | JUNCTION | 0.00               | 0.00               | 7065.00          | 0 00:00                            | 0.00                    |
| 4            | JUNCTION | 0.00               | 0.00               | 7101.00          | 0 00:00                            | 0.00                    |
| 5            | JUNCTION | 0.00               | 0.00               | 7108.00          | 0 00:00                            | 0.00                    |
| 6            | JUNCTION | 0.00               | 0.00               | 7160.00          | 0 00:00                            | 0.00                    |
| 9            | JUNCTION | 0.00               | 0.00               | 7003.00          | 0 00:00                            | 0.00                    |
| EX_28X42_CMP | JUNCTION | 0.00               | 0.00               | 6992.00          | 0 00:00                            | 0.00                    |
| EX_18_CMP    | JUNCTION | 0.00               | 0.00               | 6996.00          | 0 00:00                            | 0.00                    |
| 10           | OUTFALL  | 0.00               | 0.00               | 6988.00          | 0 00:00                            | 0.00                    |
| 11           | OUTFALL  | 0.00               | 0.00               | 7042.00          | 0 00:00                            | 0.00                    |

\*\*\*\*\*  
Node Inflow Summary  
\*\*\*\*\*

| Node         | Type     | Maximum Lateral Inflow CFS | Maximum Total Inflow CFS | Time of Max Occurrence days hr:min | Lateral Inflow Volume 10^6 gal | Total Inflow Volume 10^6 gal | Flow Balance Error Percent |
|--------------|----------|----------------------------|--------------------------|------------------------------------|--------------------------------|------------------------------|----------------------------|
| 1            | JUNCTION | 46.77                      | 46.77                    | 0 01:00                            | 1.59                           | 1.59                         | 0.000                      |
| 2            | JUNCTION | 10.94                      | 10.94                    | 0 00:56                            | 0.343                          | 0.343                        | 0.000                      |
| 3            | JUNCTION | 9.13                       | 66.47                    | 0 00:58                            | 0.232                          | 2.17                         | 0.000                      |
| 4            | JUNCTION | 1.69                       | 1.69                     | 0 00:54                            | 0.0501                         | 0.0501                       | 0.000                      |
| 5            | JUNCTION | 1.74                       | 1.74                     | 0 00:51                            | 0.0405                         | 0.0405                       | 0.000                      |
| 6            | JUNCTION | 22.27                      | 22.27                    | 0 00:55                            | 0.631                          | 0.631                        | 0.000                      |
| 9            | JUNCTION | 0.00                       | 66.47                    | 0 00:58                            | 0                              | 2.17                         | 0.000                      |
| EX_28X42_CMP | JUNCTION | 0.00                       | 96.20                    | 0 00:57                            | 0                              | 15.5                         | 0.000                      |
| EX_18_CMP    | JUNCTION | 6.00                       | 7.69                     | 0 00:54                            | 12.6                           | 12.7                         | 0.000                      |
| 10           | OUTFALL  | 0.00                       | 96.20                    | 0 00:57                            | 0                              | 15.5                         | 0.000                      |
| 11           | OUTFALL  | 0.00                       | 1.74                     | 0 00:51                            | 0                              | 0.0405                       | 0.000                      |

\*\*\*\*\*  
Node Flooding Summary  
\*\*\*\*\*

No nodes were flooded.

\*\*\*\*\*  
Outfall Loading Summary  
\*\*\*\*\*

| Outfall Node | Flow Freq Pcnt | Avg Flow CFS | Max Flow CFS | Total Volume 10^6 gal |
|--------------|----------------|--------------|--------------|-----------------------|
| 10           | 100.00         | 7.36         | 96.20        | 15.451                |
| 11           | 3.23           | 0.60         | 1.74         | 0.041                 |
| System       | 51.61          | 7.95         | 97.85        | 15.492                |

\*\*\*\*\*  
 Link Flow Summary  
 \*\*\*\*\*

| Link | Type  | Maximum<br> Flow <br>CFS | Time of Max<br>Occurrence<br>days hr:min | Maximum<br> Veloc <br>ft/sec | Max/<br>Full<br>Flow | Max/<br>Full<br>Depth |
|------|-------|--------------------------|--|------------------------------|----------------------|-----------------------|
| 4    | DUMMY | 10.94                    | 0 00:56                                  |                              |                      |                       |
| 5    | DUMMY | 66.47                    | 0 00:58                                  |                              |                      |                       |
| 6    | DUMMY | 22.27                    | 0 00:55                                  |                              |                      |                       |
| 7    | DUMMY | 1.69                     | 0 00:54                                  |                              |                      |                       |
| 8    | DUMMY | 7.69                     | 0 00:54                                  |                              |                      |                       |
| 9    | DUMMY | 96.20                    | 0 00:57                                  |                              |                      |                       |
| 10   | DUMMY | 1.74                     | 0 00:51                                  |                              |                      |                       |
| 13   | DUMMY | 66.47                    | 0 00:58                                  |                              |                      |                       |
| 14   | DUMMY | 46.77                    | 0 01:00                                  |                              |                      |                       |

\*\*\*\*\*  
 Conduit Surcharge Summary  
 \*\*\*\*\*

No conduits were surcharged.

Analysis begun on: Thu May 13 10:36:51 2021  
 Analysis ended on: Thu May 13 10:36:51 2021  
 Total elapsed time: < 1 sec

\*\*\*\*\*  
 NOTE: The summary statistics displayed in this report are based on results found at every computational time step, not just on results from each reporting time step.  
 \*\*\*\*\*

\*\*\*\*\*  
 Analysis Options

\*\*\*\*\*  
 Flow Units ..... CFS  
 Process Models:  
 Rainfall/Runoff ..... NO  
 RDII ..... NO  
 Snowmelt ..... NO  
 Groundwater ..... NO  
 Flow Routing ..... YES  
 Ponding Allowed ..... NO  
 Water Quality ..... NO  
 Flow Routing Method ..... KINWAVE  
 Starting Date ..... 01/01/2005 00:00:00  
 Ending Date ..... 01/04/2005 06:00:00  
 Antecedent Dry Days ..... 0.0  
 Report Time Step ..... 00:15:00  
 Routing Time Step ..... 30.00 sec

|                            | Volume<br>acre-feet | Volume<br>10 <sup>6</sup> gal |
|----------------------------|---------------------|-------------------------------|
| Flow Routing Continuity    |                     |                               |
| Dry Weather Inflow .....   | 167.588             | 54.611                        |
| Wet Weather Inflow .....   | 0.000               | 0.000                         |
| Groundwater Inflow .....   | 0.000               | 0.000                         |
| RDII Inflow .....          | 0.000               | 0.000                         |
| External Inflow .....      | 25.862              | 8.427                         |
| External Outflow .....     | 193.450             | 63.039                        |
| Flooding Loss .....        | 0.000               | 0.000                         |
| Evaporation Loss .....     | 0.000               | 0.000                         |
| Exfiltration Loss .....    | 0.000               | 0.000                         |
| Initial Stored Volume .... | 0.000               | 0.000                         |
| Final Stored Volume .....  | 0.000               | 0.000                         |
| Continuity Error (%) ..... | 0.000               |                               |

\*\*\*\*\*  
 Highest Flow Instability Indexes

\*\*\*\*\*  
 All links are stable.

\*\*\*\*\*  
 Routing Time Step Summary

\*\*\*\*\*  
 Minimum Time Step : 30.00 sec  
 Average Time Step : 30.00 sec  
 Maximum Time Step : 30.00 sec  
 Percent in Steady State : 0.00  
 Average Iterations per Step : 1.00  
 Percent Not Converging : 0.00

\*\*\*\*\*  
Node Depth Summary  
\*\*\*\*\*

| Node         | Type     | Average<br>Depth<br>Feet | Maximum<br>Depth<br>Feet | Maximum<br>HGL<br>Feet | Time of Max<br>Occurrence<br>days hr:min | Reported<br>Max Depth<br>Feet |
|--------------|----------|--------------------------|--------------------------|------------------------|--|-------------------------------|
| 1            | JUNCTION | 0.00                     | 0.00                     | 7409.00                | 0 00:00                                  | 0.00                          |
| 2            | JUNCTION | 0.00                     | 0.00                     | 7226.00                | 0 00:00                                  | 0.00                          |
| 3            | JUNCTION | 0.00                     | 0.00                     | 7065.00                | 0 00:00                                  | 0.00                          |
| 4            | JUNCTION | 0.00                     | 0.00                     | 7101.00                | 0 00:00                                  | 0.00                          |
| 5            | JUNCTION | 0.00                     | 0.00                     | 7108.00                | 0 00:00                                  | 0.00                          |
| 6            | JUNCTION | 0.00                     | 0.00                     | 7160.00                | 0 00:00                                  | 0.00                          |
| 9            | JUNCTION | 0.00                     | 0.00                     | 7003.00                | 0 00:00                                  | 0.00                          |
| EX_28X42_CMP | JUNCTION | 0.00                     | 0.00                     | 6992.00                | 0 00:00                                  | 0.00                          |
| EX_18_CMP    | JUNCTION | 0.00                     | 0.00                     | 6996.00                | 0 00:00                                  | 0.00                          |
| 10           | OUTFALL  | 0.00                     | 0.00                     | 6988.00                | 0 00:00                                  | 0.00                          |
| 11           | OUTFALL  | 0.00                     | 0.00                     | 7042.00                | 0 00:00                                  | 0.00                          |

\*\*\*\*\*  
Node Inflow Summary  
\*\*\*\*\*

| Node         | Type     | Maximum<br>Lateral<br>Inflow<br>CFS | Maximum<br>Total<br>Inflow<br>CFS | Time of Max<br>Occurrence<br>days hr:min | Lateral<br>Inflow<br>Volume<br>10^6 gal | Total<br>Inflow<br>Volume<br>10^6 gal | Flow<br>Balance<br>Error<br>Percent |
|--------------|----------|-------------------------------------|-----------------------------------|--|---|---------------------------------------|-------------------------------------|
| 1            | JUNCTION | 124.80                              | 124.80                            | 0 00:59                                  | 4.32                                    | 4.32                                  | 0.000                               |
| 2            | JUNCTION | 31.41                               | 31.41                             | 0 00:55                                  | 1.02                                    | 1.02                                  | 0.000                               |
| 3            | JUNCTION | 33.04                               | 188.19                            | 0 00:57                                  | 0.91                                    | 6.25                                  | 0.000                               |
| 4            | JUNCTION | 5.63                                | 5.63                              | 0 00:53                                  | 0.178                                   | 0.178                                 | 0.000                               |
| 5            | JUNCTION | 5.81                                | 5.81                              | 0 00:51                                  | 0.146                                   | 0.146                                 | 0.000                               |
| 6            | JUNCTION | 63.07                               | 63.07                             | 0 00:54                                  | 1.85                                    | 1.85                                  | 0.000                               |
| 9            | JUNCTION | 0.00                                | 188.19                            | 0 00:57                                  | 0                                       | 6.25                                  | 0.000                               |
| EX_28X42_CMP | JUNCTION | 0.00                                | 282.29                            | 0 00:56                                  | 0                                       | 62.9                                  | 0.000                               |
| EX_18_CMP    | JUNCTION | 26.00                               | 31.63                             | 0 00:53                                  | 54.6                                    | 54.8                                  | 0.000                               |
| 10           | OUTFALL  | 0.00                                | 282.29                            | 0 00:56                                  | 0                                       | 62.9                                  | 0.000                               |
| 11           | OUTFALL  | 0.00                                | 5.81                              | 0 00:51                                  | 0                                       | 0.146                                 | 0.000                               |

\*\*\*\*\*  
Node Flooding Summary  
\*\*\*\*\*

No nodes were flooded.

\*\*\*\*\*  
Outfall Loading Summary  
\*\*\*\*\*

| Outfall Node | Flow<br>Freq<br>Pcnt | Avg<br>Flow<br>CFS | Max<br>Flow<br>CFS | Total<br>Volume<br>10^6 gal |
|--------------|----------------------|--------------------|--------------------|-----------------------------|
| 10           | 100.00               | 29.94              | 282.29             | 62.887                      |
| 11           | 3.50                 | 1.99               | 5.81               | 0.146                       |
| System       | 51.75                | 31.93              | 287.83             | 63.034                      |

\*\*\*\*\*  
 Link Flow Summary  
 \*\*\*\*\*

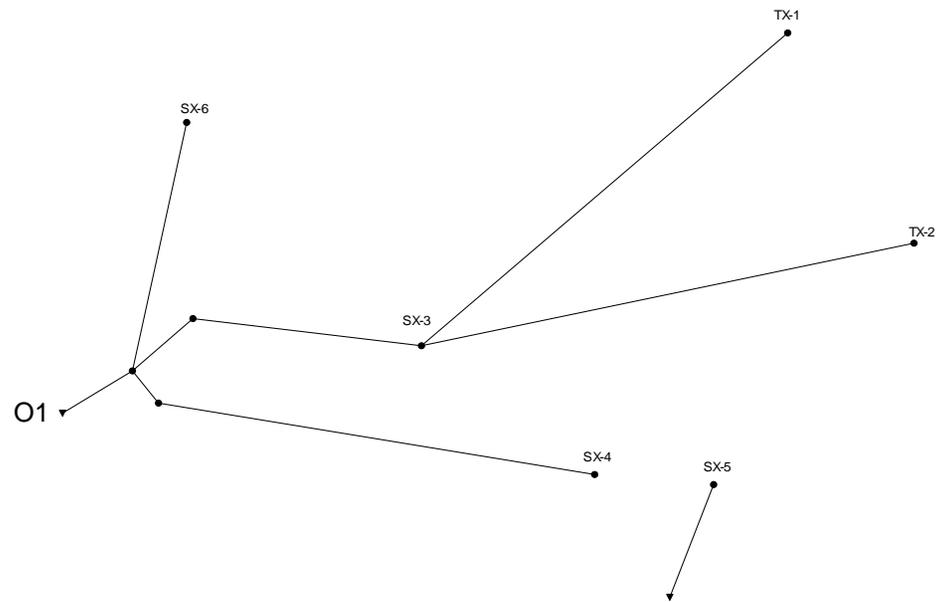
| Link | Type  | Maximum<br> Flow <br>CFS | Time of Max<br>Occurrence<br>days hr:min | Maximum<br> Veloc <br>ft/sec | Max/<br>Full<br>Flow | Max/<br>Full<br>Depth |
|------|-------|--------------------------|--|------------------------------|----------------------|-----------------------|
| 4    | DUMMY | 31.41                    | 0 00:55                                  |                              |                      |                       |
| 5    | DUMMY | 188.19                   | 0 00:57                                  |                              |                      |                       |
| 6    | DUMMY | 63.07                    | 0 00:54                                  |                              |                      |                       |
| 7    | DUMMY | 5.63                     | 0 00:53                                  |                              |                      |                       |
| 8    | DUMMY | 31.63                    | 0 00:53                                  |                              |                      |                       |
| 9    | DUMMY | 282.29                   | 0 00:56                                  |                              |                      |                       |
| 10   | DUMMY | 5.81                     | 0 00:51                                  |                              |                      |                       |
| 13   | DUMMY | 188.19                   | 0 00:57                                  |                              |                      |                       |
| 14   | DUMMY | 124.80                   | 0 00:59                                  |                              |                      |                       |

\*\*\*\*\*  
 Conduit Surcharge Summary  
 \*\*\*\*\*

No conduits were surcharged.

Analysis begun on: Thu May 13 10:41:48 2021  
 Analysis ended on: Thu May 13 10:41:49 2021  
 Total elapsed time: 00:00:01

# EXISTING CONDITIONS MODEL



**Summary of CUHP Input Parameters (Version 2.0.1)**

**Proposed Condition - 5YR**

| Catchment Name/ID | SWMM Node/ID | Raingage Name/ID         | Area (sq.mi.) | Dist. to Centroid (miles) | Length (miles) | Slope (ft./ft.) | Percent Imperv. | Depression Storage |                  | Horton's Infiltration Parameters |                      |                       | DCIA Level and Fractions |                              |                        | Percent Eff. Imperv. |
|-------------------|--------------|--------------------------|---------------|---------------------------|----------------|-----------------|-----------------|--------------------|------------------|----------------------------------|----------------------|-----------------------|--------------------------|------------------------------|------------------------|----------------------|
|                   |              |                          |               |                           |                |                 |                 | Pervious (inches)  | Imperv. (inches) | Initial Rate (in./hr.)           | Final Rate (in./hr.) | Decay Coeff. (1/sec.) | DCIA Level               | Dir. Con'ct Imperv. Fraction | Receiv. Perv. Fraction |                      |
| TX-1              | 1            | 2-HOUR DESIGN STORM 5 YR | 0.170         | 0.665                     | 1.056          | 0.060           | 23.5            | 0.50               | 0.10             | 4.50                             | 0.60                 | 0.0018                | 2.00                     | 0.12                         | 0.38                   | 18.41                |
| TX-2              | 2            | 2-HOUR DESIGN STORM 5 YR | 0.043         | 0.263                     | 0.544          | 0.060           | 16.0            | 0.50               | 0.10             | 4.50                             | 0.60                 | 0.0018                | 2.00                     | 0.08                         | 0.34                   | 12.08                |
| S-3               | 3            | 2-HOUR DESIGN STORM 5 YR | 0.048         | 0.279                     | 0.460          | 0.040           | 59.3            | 0.40               | 0.10             | 4.50                             | 0.60                 | 0.0018                | 1.00                     | 0.69                         | 0.42                   | 55.33                |
| S-6               | 6            | 2-HOUR DESIGN STORM 5 YR | 0.081         | 0.259                     | 0.698          | 0.050           | 18.9            | 0.50               | 0.10             | 4.50                             | 0.60                 | 0.0018                | 2.00                     | 0.09                         | 0.35                   | 14.49                |

**Summary of Unit Hydrograph Parameters Used By Program and Calculated Results (Version 2.0.1)**

**Proposed Condition - 5YR**

| Catchment Name/ID | User Comment for Catchment | Unit Hydrograph Parameters and Results |       |               |                       |               |                       |                           |            |                 | Excess Precip.     |                  | Storm Hydrograph          |                    |                           |                                       |
|-------------------|----------------------------|--|-------|---------------|-----------------------|---------------|-----------------------|---------------------------|------------|-----------------|--------------------|------------------|---------------------------|--------------------|---------------------------|---------------------------------------|
|                   |                            | CT                                     | Cp    | W50<br>(min.) | W50<br>Before<br>Peak | W75<br>(min.) | W75<br>Before<br>Peak | Time to<br>Peak<br>(min.) | Peak (cfs) | Volume<br>(c.f) | Excess<br>(inches) | Excess<br>(c.f.) | Time to<br>Peak<br>(min.) | Peak Flow<br>(cfs) | Total<br>Volume<br>(c.f.) | Runoff per<br>Unit Area<br>(cfs/acre) |
| TX-1              |                            | 0.113                                  | 0.165 | 53.0          | 7.02                  | 27.6          | 4.96                  | 11.7                      | 96         | 394,581         | 0.54               | 213,183          | 60.0                      | 47                 | 213,182                   | 0.43                                  |
| TX-2              |                            | 0.122                                  | 0.092 | 48.3          | 3.70                  | 25.1          | 2.62                  | 6.2                       | 26         | 98,736          | 0.46               | 45,815           | 56.0                      | 11                 | 45,815                    | 0.40                                  |
| S-3               |                            | 0.086                                  | 0.145 | 22.5          | 2.80                  | 11.7          | 1.98                  | 4.7                       | 64         | 110,715         | 1.02               | 112,490          | 47.0                      | 42                 | 112,483                   | 1.37                                  |
| S-6               |                            | 0.118                                  | 0.120 | 41.6          | 4.15                  | 21.6          | 2.93                  | 6.9                       | 58         | 188,034         | 0.49               | 92,731           | 55.0                      | 25                 | 92,727                    | 0.48                                  |

**Summary of CUHP Input Parameters (Version 2.0.1)**  
**Proposed Condition - 100YR**

| Catchment Name/ID | SWMM Node/ID | Raingage Name/ID    | Area (sq.mi.) | Dist. to Centroid (miles) | Length (miles) | Slope (ft./ft.) | Percent Imperv. | Depression Storage |                  | Horton's Infiltration Parameters |                      |                       | DCIA Level and Fractions |                              |                        | Percent Eff. Imperv. |
|-------------------|--------------|---------------------|---------------|---------------------------|----------------|-----------------|-----------------|--------------------|------------------|----------------------------------|----------------------|-----------------------|--------------------------|------------------------------|------------------------|----------------------|
|                   |              |                     |               |                           |                |                 |                 | Pervious (inches)  | Imperv. (inches) | Initial Rate (in./hr.)           | Final Rate (in./hr.) | Decay Coeff. (1/sec.) | DCIA Level               | Dir. Con'ct Imperv. Fraction | Receiv. Perv. Fraction |                      |
| TX-1              | 1            | 2-HOUR DESIGN STORM | 0.170         | 0.665                     | 1.056          | 0.060           | 23.5            | 0.50               | 0.10             | 4.50                             | 0.60                 | 0.0018                | 2.00                     | 0.12                         | 0.38                   | 20.24                |
| TX-2              | 2            | 2-HOUR DESIGN STORM | 0.043         | 0.263                     | 0.544          | 0.060           | 16.0            | 0.50               | 0.10             | 4.50                             | 0.60                 | 0.0018                | 2.00                     | 0.08                         | 0.34                   | 13.47                |
| S-3               | 3            | 2-HOUR DESIGN STORM | 0.048         | 0.279                     | 0.460          | 0.040           | 58.5            | 0.40               | 0.10             | 4.50                             | 0.60                 | 0.0018                | 1.00                     | 0.69                         | 0.41                   | 55.97                |
| S-6               | 6            | 2-HOUR DESIGN STORM | 0.081         | 0.259                     | 0.698          | 0.050           | 18.9            | 0.50               | 0.10             | 4.50                             | 0.60                 | 0.0018                | 2.00                     | 0.09                         | 0.35                   | 16.06                |

**Summary of Unit Hydrograph Parameters Used By Program and Calculated Results (Version 2.0.1)**

**Proposed Condition - 100YR**

| Catchment Name/ID | User Comment for Catchment | Unit Hydrograph Parameters and Results |       |               |                       |               |                       |                           |            |                 | Excess Precip.     |                  | Storm Hydrograph          |                    |                           |                                       |
|-------------------|----------------------------|--|-------|---------------|-----------------------|---------------|-----------------------|---------------------------|------------|-----------------|--------------------|------------------|---------------------------|--------------------|---------------------------|---------------------------------------|
|                   |                            | CT                                     | Cp    | W50<br>(min.) | W50<br>Before<br>Peak | W75<br>(min.) | W75<br>Before<br>Peak | Time to<br>Peak<br>(min.) | Peak (cfs) | Volume<br>(c.f) | Excess<br>(inches) | Excess<br>(c.f.) | Time to<br>Peak<br>(min.) | Peak Flow<br>(cfs) | Total<br>Volume<br>(c.f.) | Runoff per<br>Unit Area<br>(cfs/acre) |
| TX-1              |                            | 0.110                                  | 0.164 | 52.2          | 6.87                  | 27.1          | 4.86                  | 11.5                      | 98         | 394,581         | 1.46               | 577,723          | 59.0                      | 125                | 577,720                   | 1.15                                  |
| TX-2              |                            | 0.120                                  | 0.091 | 47.9          | 3.64                  | 24.9          | 2.57                  | 6.1                       | 27         | 98,736          | 1.38               | 136,205          | 55.0                      | 31                 | 136,206                   | 1.15                                  |
| S-3               |                            | 0.086                                  | 0.146 | 22.2          | 2.79                  | 11.6          | 1.97                  | 4.6                       | 64         | 111,078         | 2.00               | 222,496          | 47.0                      | 82                 | 222,471                   | 2.68                                  |
| S-6               |                            | 0.116                                  | 0.119 | 41.1          | 4.07                  | 21.4          | 2.88                  | 6.8                       | 59         | 188,034         | 1.41               | 265,448          | 54.0                      | 69                 | 265,434                   | 1.34                                  |

Peak attenuation pond P1 input values.

| Property                | Value                         |
|-------------------------|-------------------------------|
| Name                    | P2                            |
| X-Coordinate            | 4479.272                      |
| Y-Coordinate            | 5360.212                      |
| Description             | ON-SITE DETENTION AND WQ POND |
| Tag                     |                               |
| Inflows                 | NO                            |
| Treatment               | NO                            |
| Invert El.              | 7025                          |
| Max. Depth              | 6.33                          |
| Initial Depth           | 0                             |
| Surcharge Depth         | 0                             |
| Evap. Factor            | 0                             |
| Seepage Loss            | NO                            |
| Storage Curve           | TABULAR                       |
| <b>Functional Curve</b> |                               |
| Coefficient             | 1000                          |
| Exponent                | 0                             |
| Constant                | 0                             |
| <b>Tabular Curve</b>    |                               |
| Curve Name              | P2_VOLUME                     |

Name of storage curve to use (after specifying a curve, you can double-click to edit it)

| Depth (ft) | Area (ft2) |
|------------|------------|
| 1          | 0          |
| 2          | 4          |
| 3          | 7257       |
| 4          | 25248      |
| 5          | 43939      |
| 6          | 60500      |
| 7          | 71527      |
| 8          | 78278      |
| 9          | 84848      |
| 10         | 92117      |
| 11         |            |

Pond P1 Stage-Storage from UD-Detention

Full spectrum EDB pond P2 input values.

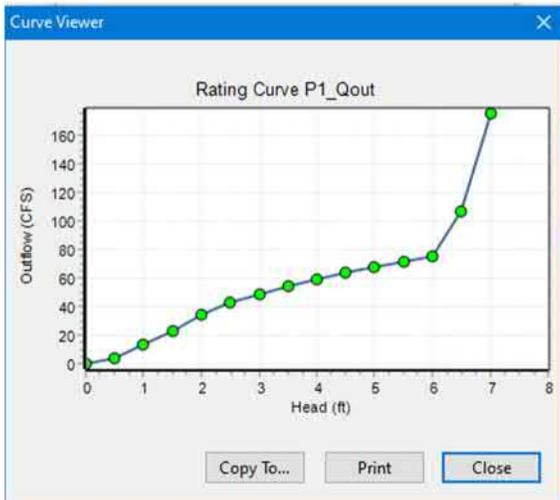
| Property                | Value                            |
|-------------------------|----------------------------------|
| Name                    | P1                               |
| X-Coordinate            | 4924.166                         |
| Y-Coordinate            | 5420.880                         |
| Description             | OFF-SITE VOLUME ATTENUATION POND |
| Tag                     |                                  |
| Inflows                 | NO                               |
| Treatment               | NO                               |
| Invert El.              | 7066                             |
| Max. Depth              | 6.08                             |
| Initial Depth           | 0                                |
| Surcharge Depth         | 0                                |
| Evap. Factor            | 0                                |
| Seepage Loss            | NO                               |
| Storage Curve           | TABULAR                          |
| <b>Functional Curve</b> |                                  |
| Coefficient             | 1000                             |
| Exponent                | 0                                |
| Constant                | 0                                |
| <b>Tabular Curve</b>    |                                  |
| Curve Name              | P1_VOLUME                        |

B-value in expression Area = A\*Depth^B + C for Depth in ft.

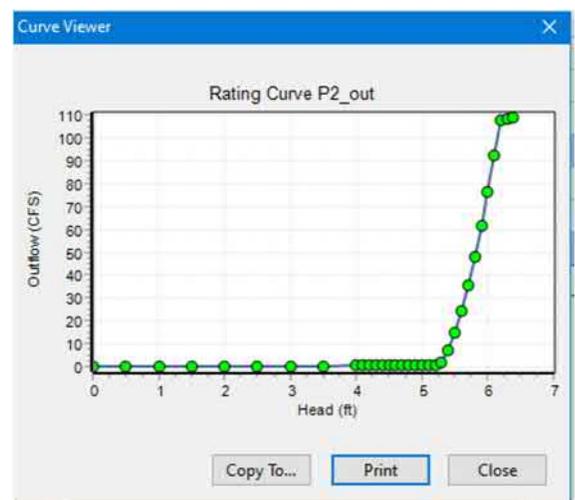
| Depth (ft) | Area (ft2) |
|------------|------------|
| 1          | 0          |
| 2          | 0          |
| 3          | 1379       |
| 4          | 7541       |
| 5          | 18733      |
| 6          | 35627      |
| 7          | 51267      |
| 8          | 55882      |
| 9          | 60677      |
| 10         | 65444      |
| 11         |            |

Pond P2 Stage-Storage from UD-Detention

Link 1 Stage-Discharge from UD-Detention



Link 2 Stage-Discharge from UD-Detention



# 5-YR Proposed Condition

EPA STORM WATER MANAGEMENT MODEL - VERSION 5.1 (Build 5.1.015)

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### Element Count

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Number of rain gages ..... 0  
 Number of subcatchments ... 0  
 Number of nodes ..... 10  
 Number of links ..... 9  
 Number of pollutants ..... 0  
 Number of land uses ..... 0

\*\*\*\*\*

### Node Summary

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| Name         | Type     | Invert El ev. | Max. Depth | Ponded Area | External Inflow |
|--------------|----------|---------------|------------|-------------|-----------------|
| 1            | JUNCTION | 7409.00       | 0.00       | 0.0         |                 |
| 2            | JUNCTION | 7226.00       | 0.00       | 0.0         |                 |
| 3            | JUNCTION | 7065.00       | 0.00       | 0.0         |                 |
| 6            | JUNCTION | 7160.00       | 0.00       | 0.0         |                 |
| P2_out       | JUNCTION | 7003.00       | 0.00       | 0.0         |                 |
| EX_28X42_CMP | JUNCTION | 6992.00       | 0.00       | 0.0         |                 |
| EX18CMP      | JUNCTION | 6993.00       | 0.00       | 0.0         | Yes             |
| 01           | OUTFALL  | 6988.00       | 0.00       | 0.0         |                 |
| P1           | STORAGE  | 7066.00       | 6.08       | 0.0         |                 |
| P2           | STORAGE  | 7025.00       | 6.33       | 0.0         |                 |

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### Link Summary

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| Name    | From Node    | To Node      | Type    | Length |
|---------|--------------|--------------|---------|--------|
| 4       | 2            | P1           | CONDUIT | 400.0  |
| 43.6436 | 0.0100       |              |         |        |
| 5       | 3            | P2           | CONDUIT | 400.0  |
| 10.0504 | 0.0100       |              |         |        |
| 6       | 6            | EX_28X42_CMP | CONDUIT | 400.0  |
| 46.2798 | 0.0100       |              |         |        |
| 9       | EX_28X42_CMP | 01           | CONDUIT | 400.0  |
| 1.0001  | 0.0100       |              |         |        |
| 13      | P2_out       | EX_28X42_CMP | CONDUIT | 400.0  |

|          |        |         |              |         |       |
|----------|--------|---------|--------------|---------|-------|
| 2.7510   | 0.0100 |         |              |         |       |
| 14       |        | 1       | P1           | CONDUIT | 400.0 |
| 166.6719 | 0.0100 |         |              |         |       |
| 15       |        | EX18CMP | EX_28X42_CMP | CONDUIT | 400.0 |
| 0.2500   | 0.0100 |         |              |         |       |
| 1        |        | P1      | P2           | OUTLET  |       |
| 2        |        | P2      | P2_out       | OUTLET  |       |

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Cross Section Summary  
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| Full<br>Conduit<br>Flow | Shape | Full<br>Depth | Full<br>Area | Hyd.<br>Rad. | Max.<br>Width | No. of<br>Barrels |
|-------------------------|-------|---------------|--------------|--------------|---------------|-------------------|
| -----                   |       |               |              |              |               |                   |
| 4<br>0.00               | DUMMY | 0.00          | 0.00         | 0.00         | 0.00          | 1                 |
| 5<br>0.00               | DUMMY | 0.00          | 0.00         | 0.00         | 0.00          | 1                 |
| 6<br>0.00               | DUMMY | 0.00          | 0.00         | 0.00         | 0.00          | 1                 |
| 9<br>0.00               | DUMMY | 0.00          | 0.00         | 0.00         | 0.00          | 1                 |
| 13<br>0.00              | DUMMY | 0.00          | 0.00         | 0.00         | 0.00          | 1                 |
| 14<br>0.00              | DUMMY | 0.00          | 0.00         | 0.00         | 0.00          | 1                 |
| 15<br>0.00              | DUMMY | 0.00          | 0.00         | 0.00         | 0.00          | 1                 |

\*\*\*\*\*  
NOTE: The summary statistics displayed in this report are based on results found at every computational time step, not just on results from each reporting time step.  
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\*\*\*\*\*  
Analysis Options  
\*\*\*\*\*

Flow Units ..... CFS  
Process Models:  
Rainfall/Runoff ..... NO  
RDI ..... NO  
Snowmelt ..... NO  
Groundwater ..... NO

Flow Routing ..... YES  
 Ponding Allowed ..... NO  
 Water Quality ..... NO  
 Flow Routing Method ..... KINWAVE  
 Starting Date ..... 01/01/2005 00:00:00  
 Ending Date ..... 01/05/2005 06:00:00  
 Antecedent Dry Days ..... 0.0  
 Report Time Step ..... 00:15:00  
 Routing Time Step ..... 30.00 sec

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Control Actions Taken

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| Flow Routing Continuity    | Volume<br>acre-feet | Volume<br>10 <sup>6</sup> gal |
|----------------------------|---------------------|-------------------------------|
| *****                      | -----               | -----                         |
| Dry Weather Inflow .....   | 0.000               | 0.000                         |
| Wet Weather Inflow .....   | 0.000               | 0.000                         |
| Groundwater Inflow .....   | 0.000               | 0.000                         |
| RDII Inflow .....          | 0.000               | 0.000                         |
| External Inflow .....      | 111.806             | 36.433                        |
| External Outflow .....     | 111.783             | 36.426                        |
| Flooding Loss .....        | 0.000               | 0.000                         |
| Evaporation Loss .....     | 0.000               | 0.000                         |
| Exfiltration Loss .....    | 0.000               | 0.000                         |
| Initial Stored Volume .... | 0.000               | 0.000                         |
| Final Stored Volume .....  | 0.000               | 0.000                         |
| Continuity Error (%) ..... | 0.020               |                               |

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Highest Flow Instability Indexes

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All links are stable.

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Routing Time Step Summary

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|                             |   |           |
|-----------------------------|---|-----------|
| Minimum Time Step           | : | 30.00 sec |
| Average Time Step           | : | 30.00 sec |
| Maximum Time Step           | : | 30.00 sec |
| Percent in Steady State     | : | 0.00      |
| Average Iterations per Step | : | 1.00      |
| Percent Not Converging      | : | 0.00      |

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Node Depth Summary  
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| Node         | Type     | Average Depth Feet | Maximum Depth Feet | Maximum HGL Feet | Time of Max Occurrence days hr: min | Reported Max Depth Feet |
|--------------|----------|--------------------|--------------------|------------------|-------------------------------------|-------------------------|
| 1            | JUNCTION | 0.00               | 0.00               | 7409.00          | 0 00:00                             | 0.00                    |
| 2            | JUNCTION | 0.00               | 0.00               | 7226.00          | 0 00:00                             | 0.00                    |
| 3            | JUNCTION | 0.00               | 0.00               | 7065.00          | 0 00:00                             | 0.00                    |
| 6            | JUNCTION | 0.00               | 0.00               | 7160.00          | 0 00:00                             | 0.00                    |
| P2_out       | JUNCTION | 0.00               | 0.00               | 7003.00          | 0 00:00                             | 0.00                    |
| EX_28X42_CMP | JUNCTION | 0.00               | 0.00               | 6992.00          | 0 00:00                             | 0.00                    |
| EX18CMP      | JUNCTION | 0.00               | 0.00               | 6993.00          | 0 00:00                             | 0.00                    |
| O1           | OUTFALL  | 0.00               | 0.00               | 6988.00          | 0 00:00                             | 0.00                    |
| P1           | STORAGE  | 0.05               | 2.69               | 7068.69          | 0 01:19                             | 2.68                    |
| P2           | STORAGE  | 2.68               | 5.91               | 7030.91          | 0 01:20                             | 5.89                    |

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 Node Inflow Summary  
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| Total Inflow Volume gal | Flow Balance Error Percent | Type     | Maximum Lateral Inflow CFS | Maximum Total Inflow CFS | Time of Max Occurrence days hr: min | Lateral Inflow Volume 10^6 gal |
|-------------------------|----------------------------|----------|----------------------------|--------------------------|-------------------------------------|--------------------------------|
| 1                       |                            | JUNCTION | 46.77                      | 46.77                    | 0 01:00                             | 1.59                           |
| 1.59                    | 0.000                      |          |                            |                          |                                     |                                |
| 2                       |                            | JUNCTION | 10.94                      | 10.94                    | 0 00:56                             | 0.343                          |
| 0.343                   | 0.000                      |          |                            |                          |                                     |                                |
| 3                       |                            | JUNCTION | 41.63                      | 41.63                    | 0 00:47                             | 0.841                          |
| 0.841                   | 0.000                      |          |                            |                          |                                     |                                |
| 6                       |                            | JUNCTION | 25.11                      | 25.11                    | 0 00:55                             | 0.694                          |
| 0.694                   | 0.000                      |          |                            |                          |                                     |                                |
| P2_out                  |                            | JUNCTION | 0.00                       | 62.70                    | 0 01:20                             | 0                              |
| 2.77                    | 0.000                      |          |                            |                          |                                     |                                |
| EX_28X42_CMP            |                            | JUNCTION | 0.00                       | 91.70                    | 0 01:18                             | 0                              |
| 36.4                    | 0.000                      |          |                            |                          |                                     |                                |
| EX18CMP                 |                            | JUNCTION | 12.00                      | 12.00                    | 0 00:00                             | 33                             |

|      |       |         |      |       |   |       |  |   |
|------|-------|---------|------|-------|---|-------|--|---|
| 33   | 0.000 |         |      |       |   |       |  |   |
| 01   |       | OUTFALL | 0.00 | 91.70 | 0 | 01:18 |  | 0 |
| 36.4 | 0.000 |         |      |       |   |       |  |   |
| P1   |       | STORAGE | 0.00 | 57.56 | 0 | 00:59 |  | 0 |
| 1.94 | 0.112 |         |      |       |   |       |  |   |
| P2   |       | STORAGE | 0.00 | 74.01 | 0 | 00:57 |  | 0 |
| 2.78 | 0.190 |         |      |       |   |       |  |   |

\*\*\*\*\*  
Node Flooding Summary  
\*\*\*\*\*

No nodes were flooded.

\*\*\*\*\*  
Storage Volume Summary  
\*\*\*\*\*

| of Max Occurrence | Maximum Storage Unit | Average Volume | Avg Pcnt Full | Evap Pcnt Loss | Exfil Pcnt Loss | Maximum Volume | Max Pcnt Full | Time days |
|-------------------|----------------------|----------------|---------------|----------------|-----------------|----------------|---------------|-----------|
| hr: min           | Outflow CFS          | 1000 ft3       |               |                |                 | 1000 ft3       |               |           |
| P1<br>01:19       | 45.23                | 0.292          | 0             | 0              | 0               | 30.252         | 13            | 0         |
| P2<br>01:20       | 62.70                | 24.141         | 17            | 0              | 0               | 119.342        | 84            | 0         |

\*\*\*\*\*  
Outfall Loading Summary  
\*\*\*\*\*

| Outfall Node | Flow Freq Pcnt | Avg Flow CFS | Max Flow CFS | Total Volume 10^6 gal |
|--------------|----------------|--------------|--------------|-----------------------|
| 01           | 100.00         | 13.26        | 91.70        | 36.423                |
| System       | 100.00         | 13.26        | 91.70        | 36.423                |

\*\*\*\*\*

Link Flow Summary

\*\*\*\*\*

| Link | Type  | Maximum<br> Flow <br>CFS | Time of Max<br>Occurrence<br>days hr: min | Maximum<br> Velocity <br>ft/sec | Max/<br>Full<br>Flow | Max/<br>Full<br>Depth |
|------|-------|--------------------------|---|---------------------------------|----------------------|-----------------------|
| 4    | DUMMY | 10.94                    | 0 00: 56                                  |                                 |                      |                       |
| 5    | DUMMY | 41.63                    | 0 00: 47                                  |                                 |                      |                       |
| 6    | DUMMY | 25.11                    | 0 00: 55                                  |                                 |                      |                       |
| 9    | DUMMY | 91.70                    | 0 01: 18                                  |                                 |                      |                       |
| 13   | DUMMY | 62.70                    | 0 01: 20                                  |                                 |                      |                       |
| 14   | DUMMY | 46.77                    | 0 01: 00                                  |                                 |                      |                       |
| 15   | DUMMY | 12.00                    | 0 00: 00                                  |                                 |                      |                       |
| 1    | DUMMY | 45.23                    | 0 01: 19                                  |                                 |                      |                       |
| 2    | DUMMY | 62.70                    | 0 01: 20                                  |                                 |                      |                       |

\*\*\*\*\*

Conduit Surcharge Summary

\*\*\*\*\*

No conduits were surcharged.

Analysis begun on: Thu Aug 19 14:09:37 2021

Analysis ended on: Thu Aug 19 14:09:38 2021

Total elapsed time: 00:00:01

100-YR Proposed Condition

EPA STORM WATER MANAGEMENT MODEL - VERSION 5.1 (Build 5.1.015)

\*\*\*\*\*

Element Count

\*\*\*\*\*

Number of rain gages ..... 0  
 Number of subcatchments ... 0  
 Number of nodes ..... 10  
 Number of links ..... 9  
 Number of pollutants ..... 0  
 Number of land uses ..... 0

\*\*\*\*\*

Node Summary

\*\*\*\*\*

| Name         | Type     | Invert El ev. | Max. Depth | Ponded Area | External Inflow |
|--------------|----------|---------------|------------|-------------|-----------------|
| 1            | JUNCTION | 7409.00       | 0.00       | 0.0         |                 |
| 2            | JUNCTION | 7226.00       | 0.00       | 0.0         |                 |
| 3            | JUNCTION | 7065.00       | 0.00       | 0.0         |                 |
| 6            | JUNCTION | 7160.00       | 0.00       | 0.0         |                 |
| P2_out       | JUNCTION | 7003.00       | 0.00       | 0.0         |                 |
| EX_28X42_CMP | JUNCTION | 6992.00       | 0.00       | 0.0         |                 |
| EX18CMP      | JUNCTION | 6993.00       | 0.00       | 0.0         | Yes             |
| 01           | OUTFALL  | 6988.00       | 0.00       | 0.0         |                 |
| P1           | STORAGE  | 7066.00       | 6.08       | 0.0         |                 |
| P2           | STORAGE  | 7025.00       | 8.33       | 0.0         |                 |

\*\*\*\*\*

Link Summary

\*\*\*\*\*

| Name    | From Node    | To Node      | Type    | Length |
|---------|--------------|--------------|---------|--------|
| 4       | 2            | P1           | CONDUIT | 400.0  |
| 43.6436 | 0.0100       |              |         |        |
| 5       | 3            | P2           | CONDUIT | 400.0  |
| 10.0504 | 0.0100       |              |         |        |
| 6       | 6            | EX_28X42_CMP | CONDUIT | 400.0  |
| 46.2798 | 0.0100       |              |         |        |
| 9       | EX_28X42_CMP | 01           | CONDUIT | 400.0  |
| 1.0001  | 0.0100       |              |         |        |
| 13      | P2_out       | EX_28X42_CMP | CONDUIT | 400.0  |

|          |        |         |              |         |       |
|----------|--------|---------|--------------|---------|-------|
| 2.7510   | 0.0100 |         |              |         |       |
| 14       |        | 1       | P1           | CONDUIT | 400.0 |
| 166.6719 | 0.0100 |         |              |         |       |
| 15       |        | EX18CMP | EX_28X42_CMP | CONDUIT | 400.0 |
| 0.2500   | 0.0100 |         |              |         |       |
| 1        |        | P1      | P2           | OUTLET  |       |
| 2        |        | P2      | P2_out       | OUTLET  |       |

\*\*\*\*\*  
Cross Section Summary  
\*\*\*\*\*

| Full<br>Conduit<br>Flow | Shape | Full<br>Depth | Full<br>Area | Hyd.<br>Rad. | Max.<br>Width | No. of<br>Barrels |
|-------------------------|-------|---------------|--------------|--------------|---------------|-------------------|
| -----                   |       |               |              |              |               |                   |
| 4<br>0.00               | DUMMY | 0.00          | 0.00         | 0.00         | 0.00          | 1                 |
| 5<br>0.00               | DUMMY | 0.00          | 0.00         | 0.00         | 0.00          | 1                 |
| 6<br>0.00               | DUMMY | 0.00          | 0.00         | 0.00         | 0.00          | 1                 |
| 9<br>0.00               | DUMMY | 0.00          | 0.00         | 0.00         | 0.00          | 1                 |
| 13<br>0.00              | DUMMY | 0.00          | 0.00         | 0.00         | 0.00          | 1                 |
| 14<br>0.00              | DUMMY | 0.00          | 0.00         | 0.00         | 0.00          | 1                 |
| 15<br>0.00              | DUMMY | 0.00          | 0.00         | 0.00         | 0.00          | 1                 |

\*\*\*\*\*  
NOTE: The summary statistics displayed in this report are based on results found at every computational time step, not just on results from each reporting time step.  
\*\*\*\*\*

\*\*\*\*\*  
Analysis Options  
\*\*\*\*\*

Flow Units ..... CFS  
Process Models:  
Rainfall/Runoff ..... NO  
RDI ..... NO  
Snowmelt ..... NO  
Groundwater ..... NO

Flow Routing ..... YES  
 Ponding Allowed ..... NO  
 Water Quality ..... NO  
 Flow Routing Method ..... KINWAVE  
 Starting Date ..... 01/01/2005 00: 00: 00  
 Ending Date ..... 01/05/2005 06: 00: 00  
 Antecedent Dry Days ..... 0.0  
 Report Time Step ..... 00: 15: 00  
 Routing Time Step ..... 30.00 sec

\*\*\*\*\*

Control Actions Taken

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| Flow Routing Continuity    | Volume<br>acre-feet | Volume<br>10 <sup>6</sup> gal |
|----------------------------|---------------------|-------------------------------|
| *****                      | -----               | -----                         |
| Dry Weather Inflow .....   | 0.000               | 0.000                         |
| Wet Weather Inflow .....   | 0.000               | 0.000                         |
| Groundwater Inflow .....   | 0.000               | 0.000                         |
| RDII Inflow .....          | 0.000               | 0.000                         |
| External Inflow .....      | 246.746             | 80.406                        |
| External Outflow .....     | 246.718             | 80.397                        |
| Flooding Loss .....        | 0.000               | 0.000                         |
| Evaporation Loss .....     | 0.000               | 0.000                         |
| Exfiltration Loss .....    | 0.000               | 0.000                         |
| Initial Stored Volume .... | 0.000               | 0.000                         |
| Final Stored Volume .....  | 0.000               | 0.000                         |
| Continuity Error (%) ..... | 0.011               |                               |

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Highest Flow Instability Indexes

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All links are stable.

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Routing Time Step Summary

\*\*\*\*\*

|                             |   |           |
|-----------------------------|---|-----------|
| Minimum Time Step           | : | 30.00 sec |
| Average Time Step           | : | 30.00 sec |
| Maximum Time Step           | : | 30.00 sec |
| Percent in Steady State     | : | 0.00      |
| Average Iterations per Step | : | 1.00      |
| Percent Not Converging      | : | 0.00      |

\*\*\*\*\*

Node Depth Summary  
 \*\*\*\*\*

| Node         | Type     | Average Depth Feet | Maximum Depth Feet | Maximum HGL Feet | Time of Max Occurrence days hr: min | Reported Max Depth Feet |
|--------------|----------|--------------------|--------------------|------------------|-------------------------------------|-------------------------|
| 1            | JUNCTION | 0.00               | 0.00               | 7409.00          | 0 00:00                             | 0.00                    |
| 2            | JUNCTION | 0.00               | 0.00               | 7226.00          | 0 00:00                             | 0.00                    |
| 3            | JUNCTION | 0.00               | 0.00               | 7065.00          | 0 00:00                             | 0.00                    |
| 6            | JUNCTION | 0.00               | 0.00               | 7160.00          | 0 00:00                             | 0.00                    |
| P2_out       | JUNCTION | 0.00               | 0.00               | 7003.00          | 0 00:00                             | 0.00                    |
| EX_28X42_CMP | JUNCTION | 0.00               | 0.00               | 6992.00          | 0 00:00                             | 0.00                    |
| EX18CMP      | JUNCTION | 0.00               | 0.00               | 6993.00          | 0 00:00                             | 0.00                    |
| 01           | OUTFALL  | 0.00               | 0.00               | 6988.00          | 0 00:00                             | 0.00                    |
| P1           | STORAGE  | 0.14               | 6.05               | 7072.05          | 0 01:46                             | 6.05                    |
| P2           | STORAGE  | 2.72               | 6.38               | 7031.38          | 0 01:18                             | 6.37                    |

\*\*\*\*\*  
 Node Inflow Summary  
 \*\*\*\*\*

| Total Inflow Volume gal | Flow Balance Error Percent | Type     | Maximum Lateral Inflow CFS | Maximum Total Inflow CFS | Time of Max Occurrence days hr: min | Lateral Inflow Volume 10^6 gal | 10^6 |
|-------------------------|----------------------------|----------|----------------------------|--------------------------|-------------------------------------|--------------------------------|------|
| 1                       |                            | JUNCTION | 124.80                     | 124.80                   | 0 00:59                             | 4.32                           |      |
| 4.32                    | 0.000                      |          |                            |                          |                                     |                                |      |
| 2                       |                            | JUNCTION | 31.41                      | 31.41                    | 0 00:55                             | 1.02                           |      |
| 1.02                    | 0.000                      |          |                            |                          |                                     |                                |      |
| 3                       |                            | JUNCTION | 81.88                      | 81.88                    | 0 00:47                             | 1.66                           |      |
| 1.66                    | 0.000                      |          |                            |                          |                                     |                                |      |
| 6                       |                            | JUNCTION | 69.49                      | 69.49                    | 0 00:54                             | 1.99                           |      |
| 1.99                    | 0.000                      |          |                            |                          |                                     |                                |      |
| P2_out                  |                            | JUNCTION | 0.00                       | 108.82                   | 0 01:18                             | 0                              |      |
| 7                       | 0.000                      |          |                            |                          |                                     |                                |      |
| EX_28X42_CMP            |                            | JUNCTION | 0.00                       | 199.21                   | 0 01:01                             | 0                              |      |
| 80.4                    | 0.000                      |          |                            |                          |                                     |                                |      |
| EX18CMP                 |                            | JUNCTION | 26.00                      | 26.00                    | 0 00:00                             | 71.4                           |      |

|      |       |         |      |        |   |       |  |   |
|------|-------|---------|------|--------|---|-------|--|---|
| 71.4 | 0.000 |         |      |        |   |       |  |   |
| 01   |       | OUTFALL | 0.00 | 199.21 | 0 | 01:01 |  | 0 |
| 80.4 | 0.000 |         |      |        |   |       |  |   |
| P1   |       | STORAGE | 0.00 | 155.84 | 0 | 00:58 |  | 0 |
| 5.34 | 0.010 |         |      |        |   |       |  |   |
| P2   |       | STORAGE | 0.00 | 130.33 | 0 | 00:52 |  | 0 |
| 7    | 0.120 |         |      |        |   |       |  |   |

\*\*\*\*\*  
Node Flooding Summary  
\*\*\*\*\*

No nodes were flooded.

\*\*\*\*\*  
Storage Volume Summary  
\*\*\*\*\*

| of Max Occurrence | Maximum Storage Unit | Average Volume | Avg Pcnt Full | Evap Pcnt Loss | Exfil Pcnt Loss | Maximum Volume | Max Pcnt Full | Time |
|-------------------|----------------------|----------------|---------------|----------------|-----------------|----------------|---------------|------|
| hr: min           | Outflow CFS          | 1000 ft3       |               |                |                 | 1000 ft3       |               | days |
| P1<br>01:46       | 78.53                | 4.090          | 2             | 0              | 0               | 226.009        | 99            | 0    |
| P2<br>01:17       | 108.82               | 25.265         | 10            | 0              | 0               | 145.272        | 55            | 0    |

\*\*\*\*\*  
Outfall Loading Summary  
\*\*\*\*\*

| Outfall Node | Flow Freq Pcnt | Avg Flow CFS | Max Flow CFS | Total Volume 10^6 gal |
|--------------|----------------|--------------|--------------|-----------------------|
| 01           | 100.00         | 29.27        | 199.21       | 80.391                |
| System       | 100.00         | 29.27        | 199.21       | 80.391                |

\*\*\*\*\*  
 Link Flow Summary  
 \*\*\*\*\*

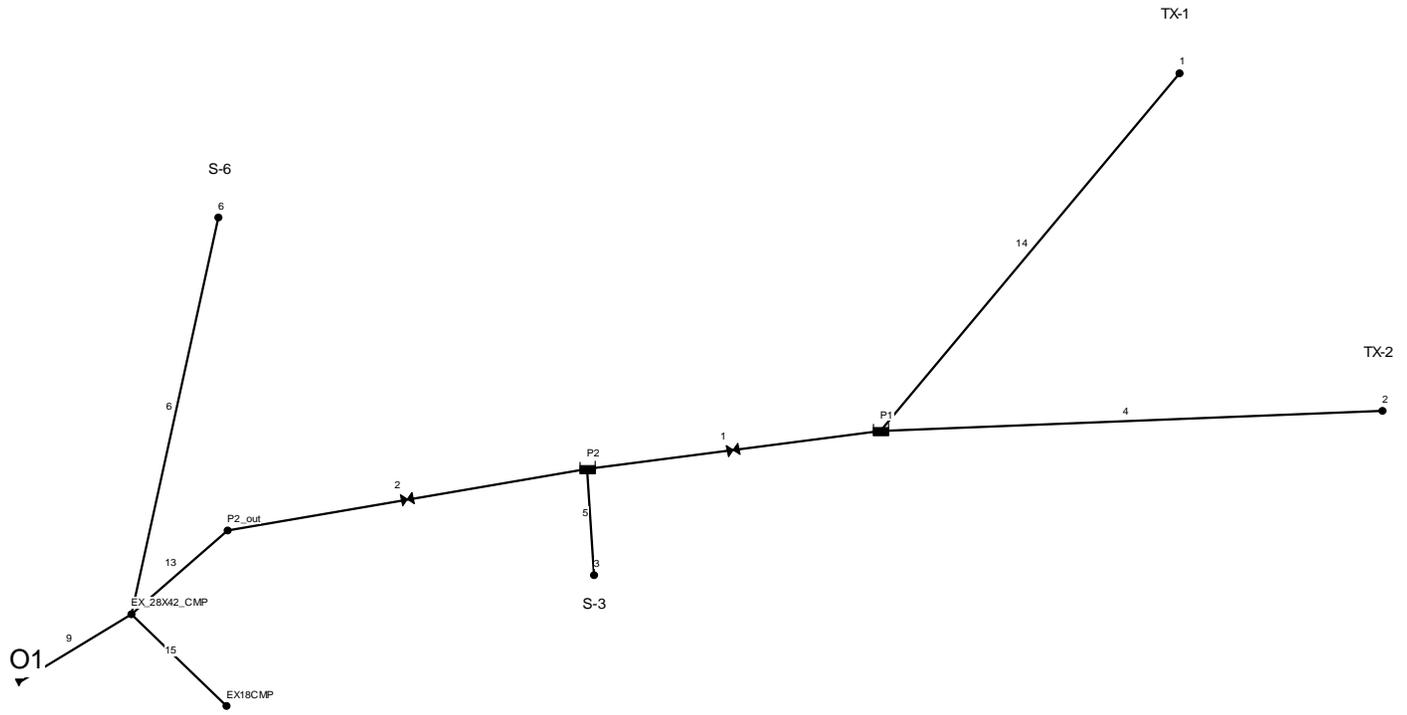
| Link | Type  | Maximum<br> Flow <br>CFS | Time of Max<br>Occurrence<br>days hr: min | Maximum<br> Veloc <br>ft/sec | Max/<br>Full<br>Flow | Max/<br>Full<br>Depth |
|------|-------|--------------------------|---|------------------------------|----------------------|-----------------------|
| 4    | DUMMY | 31.41                    | 0 00: 55                                  |                              |                      |                       |
| 5    | DUMMY | 81.88                    | 0 00: 47                                  |                              |                      |                       |
| 6    | DUMMY | 69.49                    | 0 00: 54                                  |                              |                      |                       |
| 9    | DUMMY | 199.21                   | 0 01: 01                                  |                              |                      |                       |
| 13   | DUMMY | 108.82                   | 0 01: 18                                  |                              |                      |                       |
| 14   | DUMMY | 124.80                   | 0 00: 59                                  |                              |                      |                       |
| 15   | DUMMY | 26.00                    | 0 00: 00                                  |                              |                      |                       |
| 1    | DUMMY | 78.53                    | 0 01: 46                                  |                              |                      |                       |
| 2    | DUMMY | 108.82                   | 0 01: 18                                  |                              |                      |                       |

\*\*\*\*\*  
 Conduit Surcharge Summary  
 \*\*\*\*\*

No conduits were surcharged.

Analysis begun on: Thu Aug 19 14:07:31 2021  
 Analysis ended on: Thu Aug 19 14:07:32 2021  
 Total elapsed time: 00:00:01

# PROPOSED CONDITIONS MODEL



**Summary of CUHP Input Parameters (Version 2.0.1)**  
**Historic Conditions 5 yr**

| Catchment Name/ID | SWMM Node/ID | Raingage Name/ID         | Area (sq.mi.) | Dist. to Centroid (miles) | Length (miles) | Slope (ft./ft.) | Percent Imperv. | Depression Storage |                  | Horton's Infiltration Parameters |                      |                       | DCIA Level and Fractions |                              |                        | Percent Eff. Imperv. |
|-------------------|--------------|--------------------------|---------------|---------------------------|----------------|-----------------|-----------------|--------------------|------------------|----------------------------------|----------------------|-----------------------|--------------------------|------------------------------|------------------------|----------------------|
|                   |              |                          |               |                           |                |                 |                 | Pervious (inches)  | Imperv. (inches) | Initial Rate (in./hr.)           | Final Rate (in./hr.) | Decay Coeff. (1/sec.) | DCIA Level               | Dir. Con'ct Imperv. Fraction | Receiv. Perv. Fraction |                      |
| H-1               | H1           | 2-HOUR DESIGN STORM 5 YR | 0.255         | 0.576                     | 1.269          | 0.060           | 2.0             | 0.60               | 0.10             | 4.50                             | 0.60                 | 0.0018                | 2.00                     | 0.01                         | 0.06                   | 1.42                 |
| H-2               | H2           | 2-HOUR DESIGN STORM 5 YR | 0.015         | 0.115                     | 0.185          | 0.060           | 2.0             | 0.60               | 0.10             | 4.50                             | 0.60                 | 0.0018                | 2.00                     | 0.00                         | 0.06                   | 1.42                 |

**Summary of Unit Hydrograph Parameters Used By Program and Calculated Results (Version 2.0.1)**  
**Historic Conditions 5 yr**

| Catchment Name/ID | User Comment for Catchment | Unit Hydrograph Parameters and Results |       |            |                 |            |                 |                     |            |              | Excess Precip.  |               | Storm Hydrograph    |                 |                     |                                 |
|-------------------|----------------------------|--|-------|------------|-----------------|------------|-----------------|---------------------|------------|--------------|-----------------|---------------|---------------------|-----------------|---------------------|---------------------------------|
|                   |                            | CT                                     | Cp    | W50 (min.) | W50 Before Peak | W75 (min.) | W75 Before Peak | Time to Peak (min.) | Peak (cfs) | Volume (c.f) | Excess (inches) | Excess (c.f.) | Time to Peak (min.) | Peak Flow (cfs) | Total Volume (c.f.) | Runoff per Unit Area (cfs/acre) |
| H-1               |                            | 0.158                                  | 0.241 | 51.9       | 9.90            | 27.0       | 6.99            | 16.5                | 148        | 592,979      | 0.23            | 136,599       | 64.0                | 33              | 136,600             | 0.20                            |
| H-2               |                            | 0.158                                  | 0.071 | 32.1       | 2.06            | 16.7       | 1.45            | 3.4                 | 14         | 34,938       | 0.23            | 8,047         | 53.0                | 3               | 8,046               | 0.29                            |

**Summary of CUHP Input Parameters (Version 2.0.1)**

**Historic Conditions 100 yr**

| Catchment Name/ID | SWMM Node/ID | Raingage Name/ID    | Area (sq.mi.) | Dist. to Centroid (miles) | Length (miles) | Slope (ft./ft.) | Percent Imperv. | Depression Storage |                  | Horton's Infiltration Parameters |                     |                       | DCIA Level and Fractions |                              |                        |                      |
|-------------------|--------------|---------------------|---------------|---------------------------|----------------|-----------------|-----------------|--------------------|------------------|----------------------------------|---------------------|-----------------------|--------------------------|------------------------------|------------------------|----------------------|
|                   |              |                     |               |                           |                |                 |                 | Pervious (inches)  | Imperv. (inches) | Initial Rate (in./hr.)           | Final Rate (in.hr.) | Decay Coeff. (1/sec.) | DCIA Level               | Dir. Con'ct Imperv. Fraction | Receiv. Perv. Fraction | Percent Eff. Imperv. |
| H-1               | H1           | 2-HOUR DESIGN STORM | 0.255         | 0.576                     | 1.269          | 0.060           | 2.0             | 0.60               | 0.10             | 4.50                             | 0.60                | 0.0018                | 2.00                     | 0.01                         | 0.06                   | 1.62                 |
| H-2               | H2           | 2-HOUR DESIGN STORM | 0.015         | 0.115                     | 0.185          | 0.060           | 2.0             | 0.60               | 0.10             | 4.50                             | 0.60                | 0.0018                | 2.00                     | 0.00                         | 0.06                   | 1.62                 |

**Summary of Unit Hydrograph Parameters Used By Program and Calculated Results (Version 2.0.1)**

**Historic Conditions 100 yr**

| Catchment Name/ID | User Comment for Catchment                                       | Unit Hydrograph Parameters and Results |       |            |                 |            |                 |                     |            |              | Excess Precip.  |               | Storm Hydrograph    |                 |                     |                                 |
|-------------------|--|--|-------|------------|-----------------|------------|-----------------|---------------------|------------|--------------|-----------------|---------------|---------------------|-----------------|---------------------|---------------------------------|
|                   |  | CT                                     | Cp    | W50 (min.) | W50 Before Peak | W75 (min.) | W75 Before Peak | Time to Peak (min.) | Peak (cfs) | Volume (c.f) | Excess (inches) | Excess (c.f.) | Time to Peak (min.) | Peak Flow (cfs) | Total Volume (c.f.) | Runoff per Unit Area (cfs/acre) |
| H-1               | Historic flow for comparison to basins TX-1, TX-2, and SX-3/S-3  | 0.157                                  | 0.240 | 51.8       | 9.85            | 27.0       | 6.96            | 16.4                | 148        | 592,979      | 1.14            | 673,696       | 63.0                | 152             | 673,702             | 0.93                            |
| H-2               | Historic flow for comparison to Basin S-4 (for information only) | 0.157                                  | 0.071 | 32.1       | 2.05            | 16.7       | 1.45            | 3.4                 | 14         | 34,938       | 1.14            | 39,691        | 51.0                | 13              | 39,687              | 1.33                            |

-----  
WARNING 08: elevation drop exceeds length for Conduit 1

\*\*\*\*\*  
NOTE: The summary statistics displayed in this report are based on results found at every computational time step, not just on results from each reporting time step.  
\*\*\*\*\*

\*\*\*\*\*  
Analysis Options  
\*\*\*\*\*

Flow Units ..... CFS  
Process Models:  
  Rainfall/Runoff ..... NO  
  RDII ..... NO  
  Snowmelt ..... NO  
  Groundwater ..... NO  
  Flow Routing ..... YES  
  Ponding Allowed ..... NO  
  Water Quality ..... NO  
Flow Routing Method ..... KINWAVE  
Starting Date ..... 01/01/2005 00:00:00  
Ending Date ..... 01/04/2005 06:00:00  
Antecedent Dry Days ..... 0.0  
Report Time Step ..... 00:15:00  
Routing Time Step ..... 30.00 sec

| *****                      | Volume    | Volume   |
|----------------------------|-----------|----------|
| Flow Routing Continuity    | acre-feet | 10^6 gal |
| *****                      | -----     | -----    |
| Dry Weather Inflow .....   | 0.000     | 0.000    |
| Wet Weather Inflow .....   | 0.000     | 0.000    |
| Groundwater Inflow .....   | 0.000     | 0.000    |
| RDII Inflow .....          | 0.000     | 0.000    |
| External Inflow .....      | 3.320     | 1.082    |
| External Outflow .....     | 3.320     | 1.082    |
| Flooding Loss .....        | 0.000     | 0.000    |
| Evaporation Loss .....     | 0.000     | 0.000    |
| Exfiltration Loss .....    | 0.000     | 0.000    |
| Initial Stored Volume ...  | 0.000     | 0.000    |
| Final Stored Volume .....  | 0.000     | 0.000    |
| Continuity Error (%) ..... | 0.000     |          |

\*\*\*\*\*  
Highest Flow Instability Indexes  
\*\*\*\*\*  
All links are stable.

\*\*\*\*\*  
Routing Time Step Summary  
\*\*\*\*\*

Minimum Time Step : 30.00 sec  
Average Time Step : 30.00 sec  
Maximum Time Step : 30.00 sec  
Percent in Steady State : 0.00  
Average Iterations per Step : 1.00  
Percent Not Converging : 0.00

\*\*\*\*\*  
Node Depth Summary  
\*\*\*\*\*

| Node | Type     | Average Depth Feet | Maximum Depth Feet | Maximum HGL Feet | Time of Max Occurrence days hr:min | Reported Max Depth Feet |
|------|----------|--------------------|--------------------|------------------|------------------------------------|-------------------------|
| H1   | JUNCTION | 0.00               | 0.00               | 7409.00          | 0 00:00                            | 0.00                    |
| H2   | JUNCTION | 0.00               | 0.00               | 7108.00          | 0 00:00                            | 0.00                    |
| 1    | OUTFALL  | 0.00               | 0.00               | 7004.00          | 0 00:00                            | 0.00                    |
| 2    | OUTFALL  | 0.00               | 0.00               | 7047.00          | 0 00:00                            | 0.00                    |

\*\*\*\*\*  
Node Inflow Summary  
\*\*\*\*\*

| Node | Type     | Maximum Lateral Inflow CFS | Maximum Total Inflow CFS | Time of Max Occurrence days hr:min | Lateral Inflow Volume 10^6 gal | Total Inflow Volume 10^6 gal | Flow Balance Error Percent |
|------|----------|----------------------------|--------------------------|------------------------------------|--------------------------------|------------------------------|----------------------------|
| H1   | JUNCTION | 32.57                      | 32.57                    | 0 01:04                            | 1.02                           | 1.02                         | 0.000                      |
| H2   | JUNCTION | 2.84                       | 2.84                     | 0 00:53                            | 0.0602                         | 0.0602                       | 0.000                      |
| 1    | OUTFALL  | 0.00                       | 32.57                    | 0 01:04                            | 0                              | 1.02                         | 0.000                      |
| 2    | OUTFALL  | 0.00                       | 2.84                     | 0 00:53                            | 0                              | 0.0602                       | 0.000                      |

\*\*\*\*\*  
Node Flooding Summary  
\*\*\*\*\*

No nodes were flooded.

\*\*\*\*\*  
Outfall Loading Summary  
\*\*\*\*\*

| Outfall Node | Flow Freq Pcnt | Avg Flow CFS | Max Flow CFS | Total Volume 10^6 gal |
|--------------|----------------|--------------|--------------|-----------------------|
| 1            | 4.99           | 9.75         | 32.57        | 1.022                 |
| 2            | 2.97           | 0.96         | 2.84         | 0.060                 |
| System       | 3.98           | 10.71        | 34.93        | 1.082                 |

\*\*\*\*\*  
Link Flow Summary  
\*\*\*\*\*

| Link | Type  | Maximum  Flow  CFS | Time of Max Occurrence days hr:min | Maximum  Veloc  ft/sec | Max/ Full Flow | Max/ Full Depth |
|------|-------|--------------------|------------------------------------|------------------------|----------------|-----------------|
| 2    | DUMMY | 2.84               | 0 00:53                            |                        |                |                 |
| 1    | DUMMY | 32.57              | 0 01:04                            |                        |                |                 |

\*\*\*\*\*  
Conduit Surcharge Summary  
\*\*\*\*\*

No conduits were surcharged.

Analysis begun on: Thu May 13 10:50:02 2021  
Analysis ended on: Thu May 13 10:50:02 2021  
Total elapsed time: < 1 sec

WARNING 08: elevation drop exceeds length for Conduit 1

\*\*\*\*\*  
 NOTE: The summary statistics displayed in this report are based on results found at every computational time step, not just on results from each reporting time step.  
 \*\*\*\*\*

\*\*\*\*\*  
 Analysis Options  
 \*\*\*\*\*

Flow Units ..... CFS  
 Process Models:  
 Rainfall/Runoff ..... NO  
 RDII ..... NO  
 Snowmelt ..... NO  
 Groundwater ..... NO  
 Flow Routing ..... YES  
 Ponding Allowed ..... NO  
 Water Quality ..... NO  
 Flow Routing Method ..... KINWAVE  
 Starting Date ..... 01/01/2005 00:00:00  
 Ending Date ..... 01/04/2005 06:00:00  
 Antecedent Dry Days ..... 0.0  
 Report Time Step ..... 00:15:00  
 Routing Time Step ..... 30.00 sec

| *****                      | Volume    | Volume              |
|----------------------------|-----------|---------------------|
| Flow Routing Continuity    | acre-feet | 10 <sup>6</sup> gal |
| *****                      | -----     | -----               |
| Dry Weather Inflow .....   | 0.000     | 0.000               |
| Wet Weather Inflow .....   | 0.000     | 0.000               |
| Groundwater Inflow .....   | 0.000     | 0.000               |
| RDII Inflow .....          | 0.000     | 0.000               |
| External Inflow .....      | 16.389    | 5.341               |
| External Outflow .....     | 16.389    | 5.341               |
| Flooding Loss .....        | 0.000     | 0.000               |
| Evaporation Loss .....     | 0.000     | 0.000               |
| Exfiltration Loss .....    | 0.000     | 0.000               |
| Initial Stored Volume ...  | 0.000     | 0.000               |
| Final Stored Volume .....  | 0.000     | 0.000               |
| Continuity Error (%) ..... | 0.000     |                     |

\*\*\*\*\*  
 Highest Flow Instability Indexes  
 \*\*\*\*\*  
 All links are stable.

\*\*\*\*\*  
 Routing Time Step Summary  
 \*\*\*\*\*

Minimum Time Step : 30.00 sec  
 Average Time Step : 30.00 sec  
 Maximum Time Step : 30.00 sec  
 Percent in Steady State : 0.00  
 Average Iterations per Step : 1.00  
 Percent Not Converging : 0.00

\*\*\*\*\*  
Node Depth Summary  
\*\*\*\*\*

| Node | Type     | Average Depth Feet | Maximum Depth Feet | Maximum HGL Feet | Time of Max Occurrence days hr:min | Reported Max Depth Feet |
|------|----------|--------------------|--------------------|------------------|------------------------------------|-------------------------|
| H1   | JUNCTION | 0.00               | 0.00               | 7409.00          | 0 00:00                            | 0.00                    |
| H2   | JUNCTION | 0.00               | 0.00               | 7108.00          | 0 00:00                            | 0.00                    |
| 1    | OUTFALL  | 0.00               | 0.00               | 7004.00          | 0 00:00                            | 0.00                    |
| 2    | OUTFALL  | 0.00               | 0.00               | 7047.00          | 0 00:00                            | 0.00                    |

\*\*\*\*\*  
Node Inflow Summary  
\*\*\*\*\*

| Node | Type     | Maximum Lateral Inflow CFS | Maximum Total Inflow CFS | Time of Max Occurrence days hr:min | Lateral Inflow Volume 10^6 gal | Total Inflow Volume 10^6 gal | Flow Balance Error Percent |
|------|----------|----------------------------|--------------------------|------------------------------------|--------------------------------|------------------------------|----------------------------|
| H1   | JUNCTION | 0.00                       | 0.00                     | 0 00:00                            | 0                              | 0                            | 0.000                      |
| H2   | JUNCTION | 0.00                       | 0.00                     | 0 00:00                            | 0                              | 0                            | 0.000                      |
| 1    | OUTFALL  | 124.80                     | 124.80                   | 0 00:59                            | 4.32                           | 4.32                         | 0.000                      |
| 2    | OUTFALL  | 31.41                      | 31.41                    | 0 00:55                            | 1.02                           | 1.02                         | 0.000                      |

\*\*\*\*\*  
Node Flooding Summary  
\*\*\*\*\*

No nodes were flooded.

\*\*\*\*\*  
Outfall Loading Summary  
\*\*\*\*\*

| Outfall Node | Flow Freq Pcnt | Avg Flow CFS | Max Flow CFS | Total Volume 10^6 gal |
|--------------|----------------|--------------|--------------|-----------------------|
| 1            | 6.39           | 32.20        | 124.80       | 4.321                 |
| 2            | 5.72           | 8.49         | 31.41        | 1.019                 |
| System       | 6.05           | 40.69        | 155.84       | 5.340                 |

\*\*\*\*\*  
Link Flow Summary  
\*\*\*\*\*

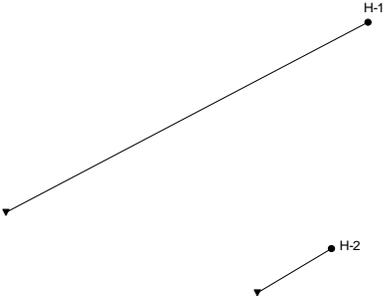
| Link | Type  | Maximum  Flow  CFS | Time of Max Occurrence days hr:min | Maximum  Veloc  ft/sec | Max/ Full Flow | Max/ Full Depth |
|------|-------|--------------------|------------------------------------|------------------------|----------------|-----------------|
| 2    | DUMMY | 0.00               | 0 00:00                            |                        |                |                 |
| 1    | DUMMY | 0.00               | 0 00:00                            |                        |                |                 |

\*\*\*\*\*  
Conduit Surcharge Summary  
\*\*\*\*\*

No conduits were surcharged.

Analysis begun on: Thu May 13 10:50:56 2021  
Analysis ended on: Thu May 13 10:50:56 2021  
Total elapsed time: < 1 sec

# HISTORIC CONDITIONS MODEL



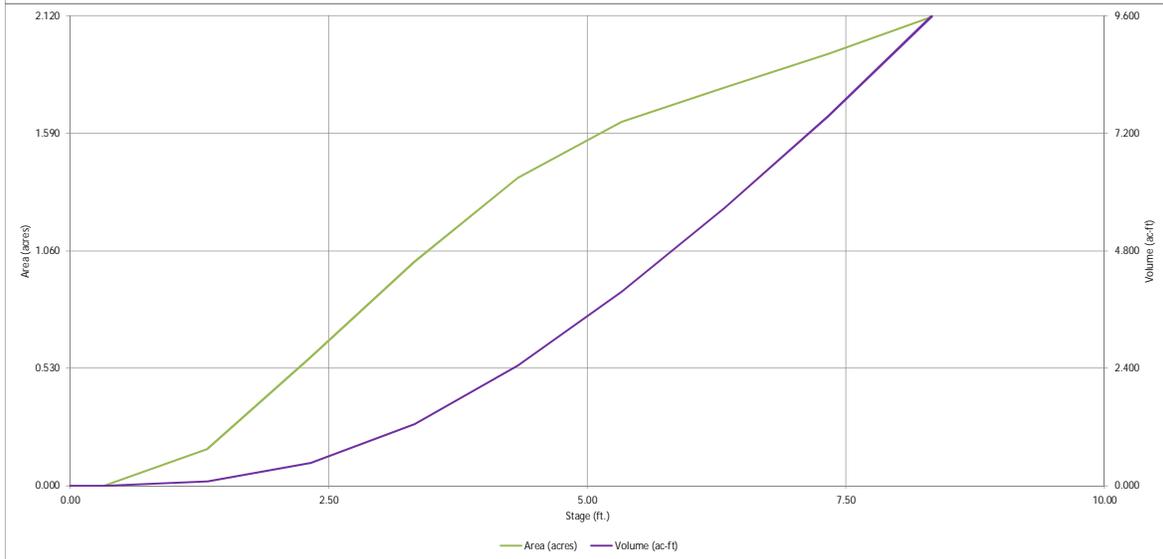
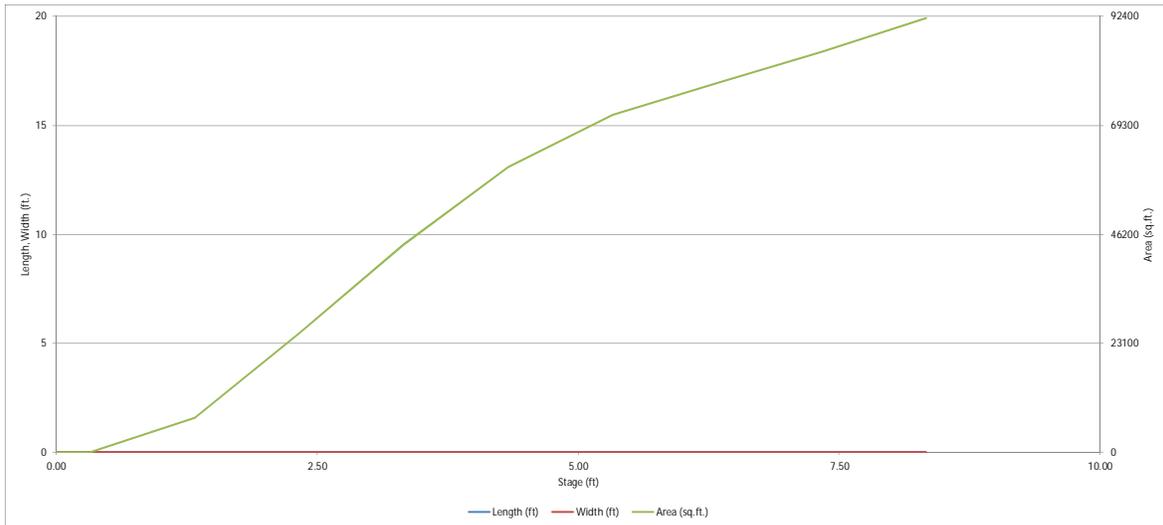
## **Appendix D**

### **Hydraulic Calculations**



# DETENTION BASIN STAGE-STORAGE TABLE BUILDER

*MHFD-Detention, Version 4.03 (May 2020)*

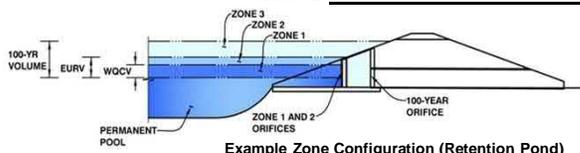


# DETENTION BASIN OUTLET STRUCTURE DESIGN

*MHFD-Detention, Version 4.03 (May 2020)*

Project: Cloverleaf Filling No. 1

Basin I D: Attenuation Pond P1



|                          | Estimated Stage (ft) | Estimated Volume (ac-ft) | Outlet Type            |
|--------------------------|----------------------|--------------------------|------------------------|
| Zone 1 (100-year)        | 7.31                 | 7.514                    | Weir & Pipe (Restrict) |
| Zone 2                   |                      |                          |                        |
| Zone 3                   |                      |                          |                        |
| <b>Total (all zones)</b> |                      | 7.514                    |                        |

User Input: Orifice at Underdrain Outlet (typically used to drain WOCV in a Filtration BMP)

Underdrain Orifice Invert Depth =  ft (distance below the filtration media surface)  
 Underdrain Orifice Diameter =  inches

Calculated Parameters for Underdrain

Underdrain Orifice Area =  ft<sup>2</sup>  
 Underdrain Orifice Centroid =  feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WOCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice =  ft (relative to basin bottom at Stage = 0 ft)  
 Depth at top of Zone using Orifice Plate =  ft (relative to basin bottom at Stage = 0 ft)  
 Orifice Plate: Orifice Vertical Spacing =  inches  
 Orifice Plate: Orifice Area per Row =  inches

Calculated Parameters for Plate

WQ Orifice Area per Row =  ft<sup>2</sup>  
 Elliptical Half-Width =  feet  
 Elliptical Slot Centroid =  feet  
 Elliptical Slot Area =  ft<sup>2</sup>

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

|                                | Row 1 (optional) | Row 2 (optional) | Row 3 (optional) | Row 4 (optional) | Row 5 (optional) | Row 6 (optional) | Row 7 (optional) | Row 8 (optional) |
|--------------------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|
| Stage of Orifice Centroid (ft) | N/A              |
| Orifice Area (sq. inches)      | N/A              |

|                                | Row 9 (optional) | Row 10 (optional) | Row 11 (optional) | Row 12 (optional) | Row 13 (optional) | Row 14 (optional) | Row 15 (optional) | Row 16 (optional) |
|--------------------------------|------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| Stage of Orifice Centroid (ft) | N/A              | N/A               | N/A               | N/A               | N/A               | N/A               | N/A               | N/A               |
| Orifice Area (sq. inches)      | N/A              | N/A               | N/A               | N/A               | N/A               | N/A               | N/A               | N/A               |

User Input: Vertical Orifice (Circular or Rectangular)

Invert of Vertical Orifice =   ft (relative to basin bottom at Stage = 0 ft)  
 Depth at top of Zone using Vertical Orifice =   ft (relative to basin bottom at Stage = 0 ft)  
 Vertical Orifice Diameter =   inches

Calculated Parameters for Vertical Orifice

Vertical Orifice Area =   ft<sup>2</sup>  
 Vertical Orifice Centroid =   feet

User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe))

Overflow Weir Front Edge Height, Ho =  ft (relative to basin bottom at Stage = 0 ft)  
 Overflow Weir Front Edge Length =  feet  
 Overflow Weir Grate Slope =  H:V  
 Horiz. Length of Weir Sides =  feet  
 Overflow Grate Open Area % =  % , grate open area/total area  
 Debris Clogging % =  %

Calculated Parameters for Overflow Weir

Height of Grate Upper Edge, H<sub>1</sub> =  feet  
 Overflow Weir Slope Length =  feet  
 Grate Open Area / 100-yr Orifice Area =   
 Overflow Grate Open Area w/o Debris =  ft<sup>2</sup>  
 Overflow Grate Open Area w/ Debris =  ft<sup>2</sup>

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

Depth to Invert of Outlet Pipe =  ft (distance below basin bottom at Stage = 0 ft)  
 Outlet Pipe Diameter =  inches  
 Restrictor Plate Height Above Pipe Invert =  inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate

Outlet Orifice Area =  ft<sup>2</sup>  
 Outlet Orifice Centroid =  feet  
 Half-Central Angle of Restrictor Plate on Pipe =   radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage =  ft (relative to basin bottom at Stage = 0 ft)  
 Spillway Crest Length =  feet  
 Spillway End Slopes =  H:V  
 Freeboard above Max Water Surface =  feet

Calculated Parameters for Spillway

Spillway Design Flow Depth =  feet  
 Stage at Top of Freeboard =  feet  
 Basin Area at Top of Freeboard =  acres  
 Basin Volume at Top of Freeboard =  acre-ft

## Routed Hydrograph Results

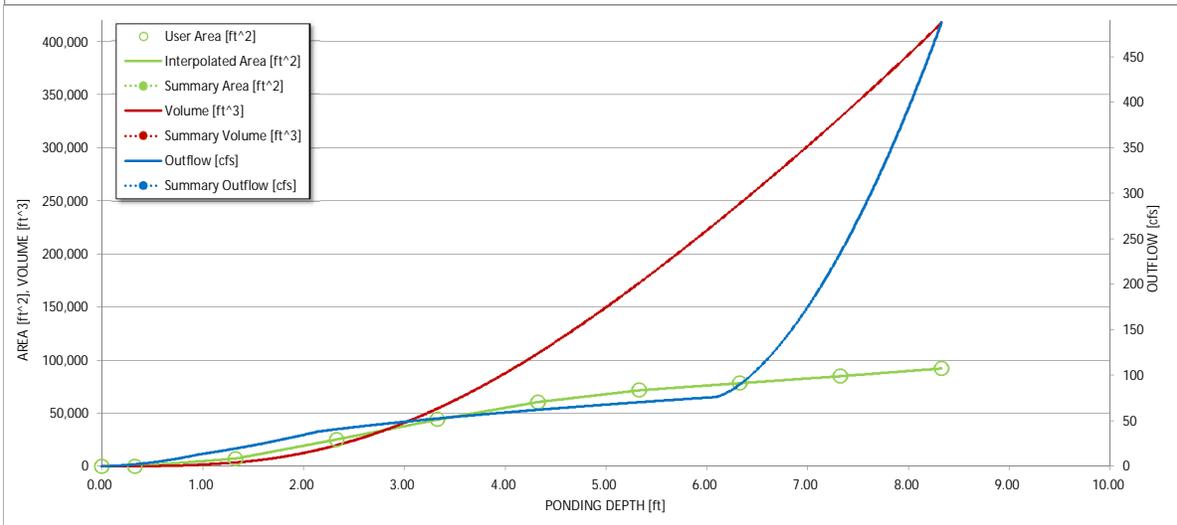
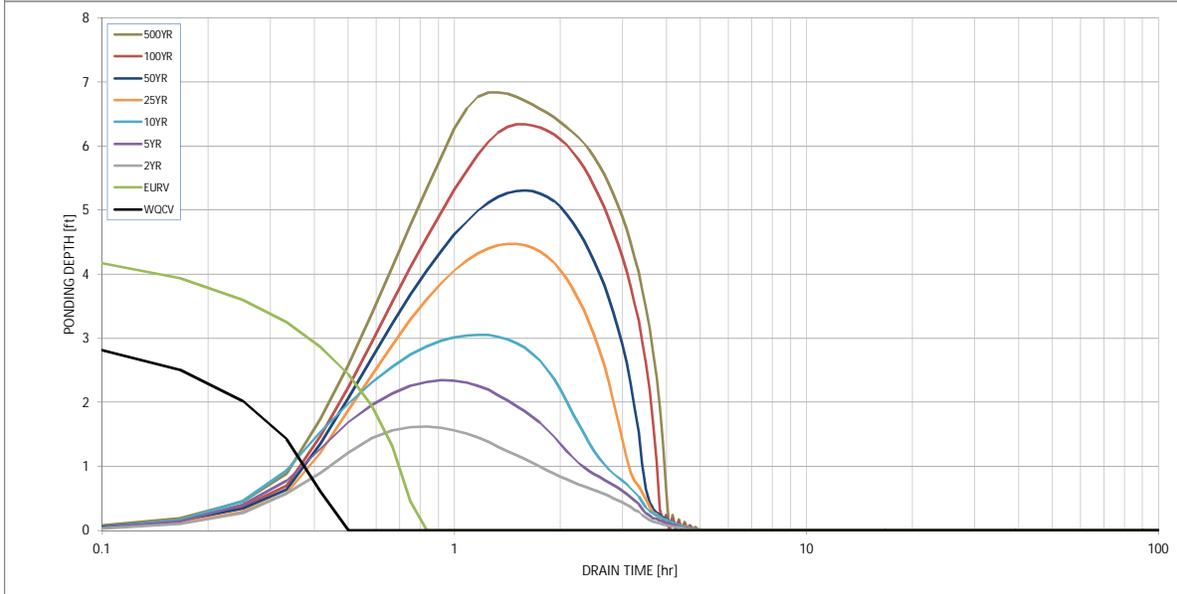
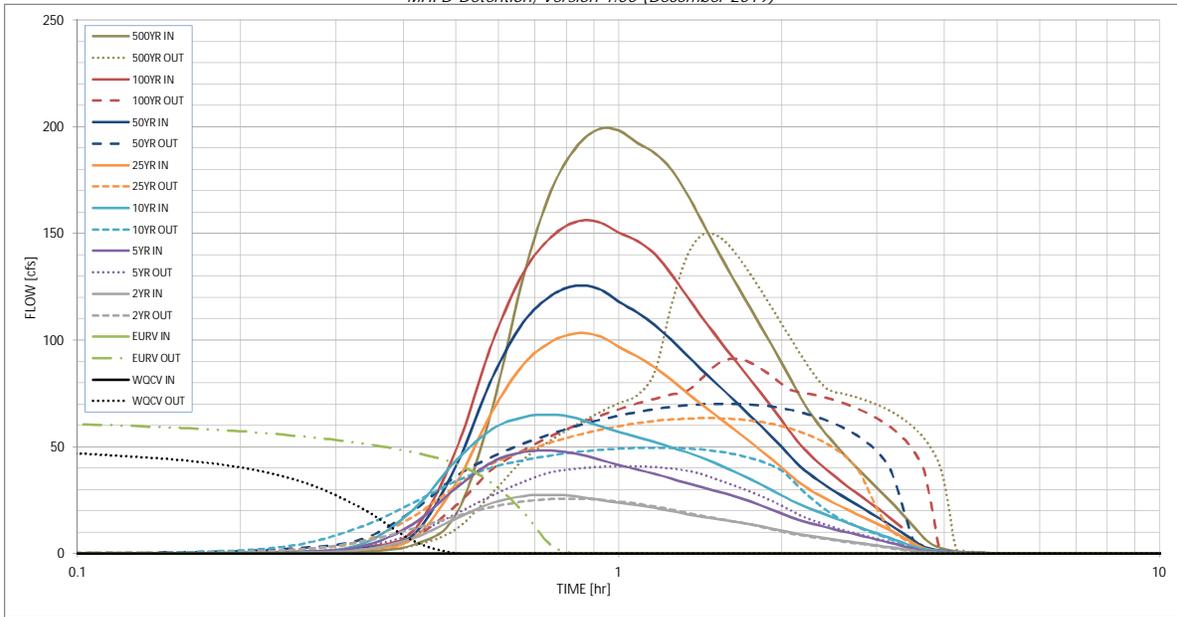
*The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).*

|   | WOCV           | EURV           | 2 Year         | 5 Year         | 10 Year        | 25 Year        | 50 Year        | 100 Year            | 500 Year |
|---|----------------|----------------|----------------|----------------|----------------|----------------|----------------|---------------------|----------|
| Design Storm Return Period                    | N/A            | N/A            | 1.19           | 1.50           | 1.75           | 2.00           | 2.25           | 2.52                | 3.00     |
| One-Hour Rainfall Depth (in)                  | N/A            | N/A            | 1.19           | 1.50           | 1.75           | 2.00           | 2.25           | 2.52                | 3.00     |
| CUHP Runoff Volume (acre-ft)                  | 1.401          | 2.993          | 3.226          | 5.717          | 8.074          | 11.847         | 14.582         | 18.346              | 23.804   |
| Inflow Hydrograph Volume (acre-ft)            | N/A            | N/A            | 3.226          | 5.717          | 8.074          | 11.847         | 14.582         | 18.346              | 23.804   |
| CUHP Predevelopment Peak Q (cfs)              | N/A            | N/A            | 9.9            | 27.9           | 43.4           | 80.3           | 101.1          | 129.9               | 170.2    |
| OPTIONAL Override Predevelopment Peak Q (cfs) | N/A            | N/A            |                |                |                |                |                |                     |          |
| Predevelopment Unit Peak Flow, q (cfs/acre)   | N/A            | N/A            | 0.07           | 0.21           | 0.32           | 0.59           | 0.74           | 0.96                | 1.25     |
| Peak Inflow Q (cfs)                           | N/A            | N/A            | 27.5           | 48.1           | 65.1           | 103.1          | 125.4          | 155.4               | 198.7    |
| Peak Outflow Q (cfs)                          | 52.2           | 64.1           | 25.7           | 40.9           | 49.5           | 63.3           | 70.2           | 91.1                | 149.6    |
| Ratio Peak Outflow to Predevelopment Q        | N/A            | N/A            | N/A            | 1.5            | 1.1            | 0.8            | 0.7            | 0.7                 | 0.9      |
| Structure Controlling Flow                    | Outlet Plate 1 | <del>Spillway</del> | Spillway |
| Max Velocity through Gate 1 (fps)             | 0.76           | 0.92           | 0.36           | 0.6            | 0.7            | 0.9            | 1.0            | 1.1                 | 1.1      |
| Max Velocity through Gate 2 (fps)             | N/A                 | N/A      |
| Time to Drain 97% of Inflow Volume (hours)    | 0              | 1              | 1              | 2              | 2              | 3              | 3              | 4                   | 4        |
| Time to Drain 99% of Inflow Volume (hours)    | 0              | 1              | 2              | 2              | 3              | 3              | 3              | 4                   | 4        |
| Maximum Ponding Depth (ft)                    | 3.48           | 4.71           | 1.63           | 2.34           | 3.06           | 4.48           | 5.31           | 6.34                | 6.84     |
| Area at Maximum Ponding Depth (acres)         | 1.07           | 1.49           | 0.29           | 0.58           | 0.89           | 1.42           | 1.63           | 1.80                | 1.87     |
| Maximum Volume Stored (acre-ft)               | 1.406          | 2.995          | 0.149          | 0.462          | 0.985          | 2.646          | 3.916          | 5.702               | 6.602    |

Pond Depth Per SWMM Model = 6.05'

# DETENTION BASIN OUTLET STRUCTURE DESIGN

*MHFD-Detention, Version 4.00 (December 2019)*



| S-A-V-D Chart Axis Override | X-axis | Left Y-Axis | Right Y-Axis |
|-----------------------------|--------|-------------|--------------|
| minimum bound               |        |             |              |
| maximum bound               |        |             |              |

# DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename: \_\_\_\_\_

## Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

| Time Interval | SOURCE  | CUHP       | CUHP       | CUHP         | CUHP         | CUHP          | CUHP          | CUHP          | CUHP           | CUHP           |
|---------------|---------|------------|------------|--------------|--------------|---------------|---------------|---------------|----------------|----------------|
|               | TIME    | WOCV [cfs] | EURV [cfs] | 2 Year [cfs] | 5 Year [cfs] | 10 Year [cfs] | 25 Year [cfs] | 50 Year [cfs] | 100 Year [cfs] | 500 Year [cfs] |
| 5.00_min      | 0:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 0:05:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 0:10:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.04          | 0.00           | 0.10           |
|               | 0:15:00 | 0.00       | 0.00       | 0.34         | 0.56         | 0.69          | 0.47          | 0.63          | 0.58           | 0.88           |
|               | 0:20:00 | 0.00       | 0.00       | 1.61         | 3.09         | 4.17          | 1.75          | 2.24          | 2.60           | 3.98           |
|               | 0:25:00 | 0.00       | 0.00       | 7.03         | 13.68        | 20.35         | 7.00          | 8.68          | 10.63          | 18.02          |
|               | 0:30:00 | 0.00       | 0.00       | 16.33        | 30.59        | 43.34         | 32.65         | 40.82         | 48.21          | 67.71          |
|               | 0:35:00 | 0.00       | 0.00       | 23.65        | 42.79        | 58.20         | 66.30         | 82.08         | 98.53          | 129.76         |
|               | 0:40:00 | 0.00       | 0.00       | 26.87        | 47.50        | 63.86         | 88.51         | 108.37        | 131.60         | 169.95         |
|               | 0:45:00 | 0.00       | 0.00       | 27.50        | 48.14        | 65.05         | 99.07         | 120.69        | 148.20         | 190.10         |
|               | 0:50:00 | 0.00       | 0.00       | 26.72        | 46.78        | 63.42         | 103.12        | 125.42        | 155.40         | 198.66         |
|               | 0:55:00 | 0.00       | 0.00       | 25.20        | 44.10        | 59.87         | 101.98        | 124.06        | 155.26         | 198.18         |
|               | 1:00:00 | 0.00       | 0.00       | 23.72        | 41.44        | 56.86         | 96.85         | 118.04        | 150.33         | 192.34         |
|               | 1:05:00 | 0.00       | 0.00       | 22.57        | 39.29        | 54.43         | 92.22         | 112.81        | 146.32         | 187.54         |
|               | 1:10:00 | 0.00       | 0.00       | 21.30        | 37.22        | 52.06         | 87.16         | 106.97        | 140.12         | 180.06         |
|               | 1:15:00 | 0.00       | 0.00       | 19.88        | 35.09        | 49.78         | 81.47         | 100.30        | 131.04         | 169.11         |
|               | 1:20:00 | 0.00       | 0.00       | 18.52        | 33.01        | 47.52         | 75.46         | 93.11         | 120.99         | 156.78         |
|               | 1:25:00 | 0.00       | 0.00       | 17.36        | 31.21        | 45.10         | 70.14         | 86.63         | 111.65         | 145.01         |
|               | 1:30:00 | 0.00       | 0.00       | 16.35        | 29.58        | 42.53         | 65.32         | 80.72         | 103.27         | 134.24         |
|               | 1:35:00 | 0.00       | 0.00       | 15.39        | 27.99        | 39.93         | 60.77         | 75.11         | 95.57          | 124.28         |
|               | 1:40:00 | 0.00       | 0.00       | 14.47        | 26.26        | 37.35         | 56.45         | 69.77         | 88.51          | 115.08         |
|               | 1:45:00 | 0.00       | 0.00       | 13.55        | 24.38        | 34.81         | 52.27         | 64.61         | 81.72          | 106.23         |
|               | 1:50:00 | 0.00       | 0.00       | 12.63        | 22.46        | 32.33         | 48.20         | 59.60         | 75.14          | 97.69          |
|               | 1:55:00 | 0.00       | 0.00       | 11.66        | 20.55        | 29.84         | 44.20         | 54.67         | 68.72          | 89.36          |
|               | 2:00:00 | 0.00       | 0.00       | 10.65        | 18.68        | 27.27         | 40.28         | 49.86         | 62.51          | 81.31          |
|               | 2:05:00 | 0.00       | 0.00       | 9.66         | 16.94        | 24.84         | 36.33         | 44.99         | 56.33          | 73.40          |
|               | 2:10:00 | 0.00       | 0.00       | 8.83         | 15.53        | 22.84         | 32.79         | 40.68         | 50.90          | 66.51          |
|               | 2:15:00 | 0.00       | 0.00       | 8.16         | 14.38        | 21.12         | 30.01         | 37.27         | 46.56          | 60.90          |
|               | 2:20:00 | 0.00       | 0.00       | 7.56         | 13.32        | 19.52         | 27.66         | 34.35         | 42.84          | 56.02          |
|               | 2:25:00 | 0.00       | 0.00       | 7.00         | 12.33        | 18.03         | 25.56         | 31.72         | 39.48          | 51.60          |
|               | 2:30:00 | 0.00       | 0.00       | 6.47         | 11.39        | 16.62         | 23.63         | 29.30         | 36.41          | 47.54          |
|               | 2:35:00 | 0.00       | 0.00       | 5.97         | 10.50        | 15.28         | 21.85         | 27.07         | 33.57          | 43.79          |
|               | 2:40:00 | 0.00       | 0.00       | 5.49         | 9.64         | 14.00         | 20.14         | 24.93         | 30.91          | 40.28          |
|               | 2:45:00 | 0.00       | 0.00       | 5.03         | 8.81         | 12.78         | 18.51         | 22.90         | 28.43          | 37.00          |
|               | 2:50:00 | 0.00       | 0.00       | 4.59         | 8.01         | 11.61         | 16.94         | 20.94         | 26.06          | 33.86          |
|               | 2:55:00 | 0.00       | 0.00       | 4.16         | 7.23         | 10.49         | 15.40         | 19.03         | 23.72          | 30.80          |
|               | 3:00:00 | 0.00       | 0.00       | 3.74         | 6.48         | 9.42          | 13.89         | 17.16         | 21.41          | 27.77          |
|               | 3:05:00 | 0.00       | 0.00       | 3.32         | 5.74         | 8.36          | 12.39         | 15.30         | 19.11          | 24.76          |
|               | 3:10:00 | 0.00       | 0.00       | 2.91         | 5.01         | 7.32          | 10.91         | 13.47         | 16.82          | 21.77          |
|               | 3:15:00 | 0.00       | 0.00       | 2.50         | 4.30         | 6.29          | 9.44          | 11.65         | 14.54          | 18.79          |
|               | 3:20:00 | 0.00       | 0.00       | 2.10         | 3.59         | 5.27          | 7.98          | 9.83          | 12.27          | 15.83          |
|               | 3:25:00 | 0.00       | 0.00       | 1.71         | 2.90         | 4.27          | 6.52          | 8.04          | 10.02          | 12.89          |
|               | 3:30:00 | 0.00       | 0.00       | 1.33         | 2.22         | 3.30          | 5.10          | 6.28          | 7.81           | 10.01          |
|               | 3:35:00 | 0.00       | 0.00       | 0.97         | 1.59         | 2.43          | 3.71          | 4.57          | 5.67           | 7.28           |
|               | 3:40:00 | 0.00       | 0.00       | 0.70         | 1.17         | 1.89          | 2.49          | 3.12          | 3.88           | 5.11           |
|               | 3:45:00 | 0.00       | 0.00       | 0.54         | 0.95         | 1.56          | 1.78          | 2.28          | 2.77           | 3.72           |
|               | 3:50:00 | 0.00       | 0.00       | 0.45         | 0.78         | 1.30          | 1.32          | 1.71          | 2.02           | 2.75           |
|               | 3:55:00 | 0.00       | 0.00       | 0.37         | 0.65         | 1.08          | 1.00          | 1.31          | 1.46           | 2.03           |
|               | 4:00:00 | 0.00       | 0.00       | 0.31         | 0.54         | 0.89          | 0.76          | 1.00          | 1.05           | 1.48           |
|               | 4:05:00 | 0.00       | 0.00       | 0.26         | 0.44         | 0.73          | 0.59          | 0.78          | 0.75           | 1.06           |
|               | 4:10:00 | 0.00       | 0.00       | 0.21         | 0.35         | 0.58          | 0.46          | 0.60          | 0.52           | 0.75           |
|               | 4:15:00 | 0.00       | 0.00       | 0.17         | 0.28         | 0.45          | 0.35          | 0.46          | 0.38           | 0.56           |
|               | 4:20:00 | 0.00       | 0.00       | 0.14         | 0.22         | 0.35          | 0.28          | 0.36          | 0.31           | 0.44           |
|               | 4:25:00 | 0.00       | 0.00       | 0.11         | 0.17         | 0.27          | 0.22          | 0.28          | 0.24           | 0.34           |
|               | 4:30:00 | 0.00       | 0.00       | 0.09         | 0.12         | 0.20          | 0.17          | 0.22          | 0.19           | 0.27           |
|               | 4:35:00 | 0.00       | 0.00       | 0.07         | 0.09         | 0.15          | 0.13          | 0.17          | 0.15           | 0.21           |
|               | 4:40:00 | 0.00       | 0.00       | 0.05         | 0.06         | 0.11          | 0.10          | 0.12          | 0.11           | 0.16           |
|               | 4:45:00 | 0.00       | 0.00       | 0.03         | 0.04         | 0.08          | 0.07          | 0.09          | 0.08           | 0.11           |
|               | 4:50:00 | 0.00       | 0.00       | 0.02         | 0.03         | 0.05          | 0.04          | 0.06          | 0.05           | 0.07           |
|               | 4:55:00 | 0.00       | 0.00       | 0.01         | 0.02         | 0.03          | 0.03          | 0.03          | 0.03           | 0.04           |
|               | 5:00:00 | 0.00       | 0.00       | 0.01         | 0.01         | 0.01          | 0.01          | 0.02          | 0.01           | 0.02           |
|               | 5:05:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.01           |
|               | 5:10:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:15:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:20:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:25:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:30:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:35:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:40:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:45:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:50:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:55:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 6:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |

# Weir Report

## Pond P1 Spillway

### Trapezoidal Weir

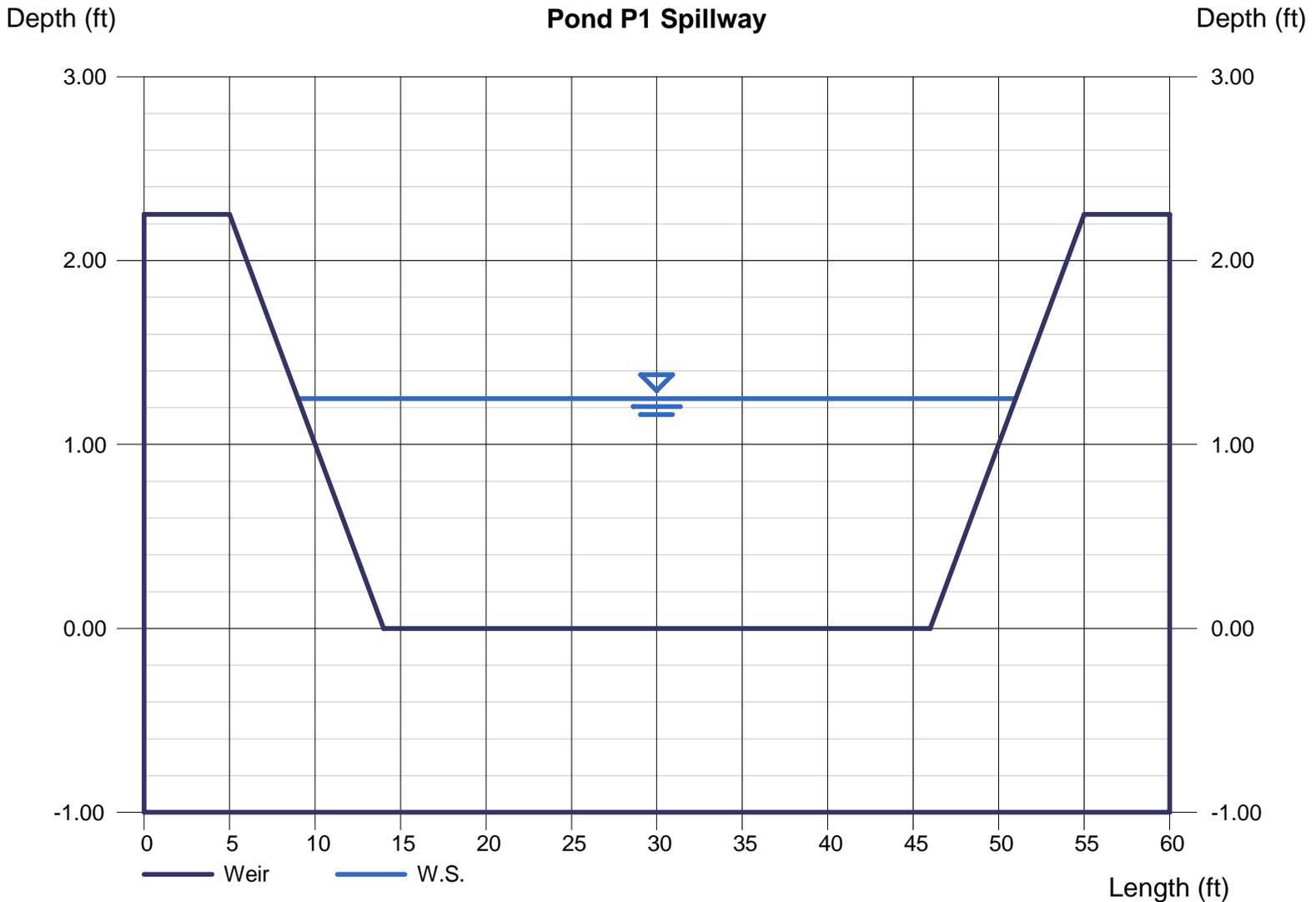
Crest = Sharp  
Bottom Length (ft) = 32.00  
Total Depth (ft) = 2.25  
Side Slope (z:1) = 4.00

### Highlighted

Depth (ft) = 1.25  
Q (cfs) = 155.80  
Area (sqft) = 46.25  
Velocity (ft/s) = 3.37  
Top Width (ft) = 42.00

### Calculations

Weir Coeff. Cw = 3.10  
Compute by: Known Q  
Known Q (cfs) = 155.80



# Channel Report

## Pond P1 Overflow Channel

### Trapezoidal

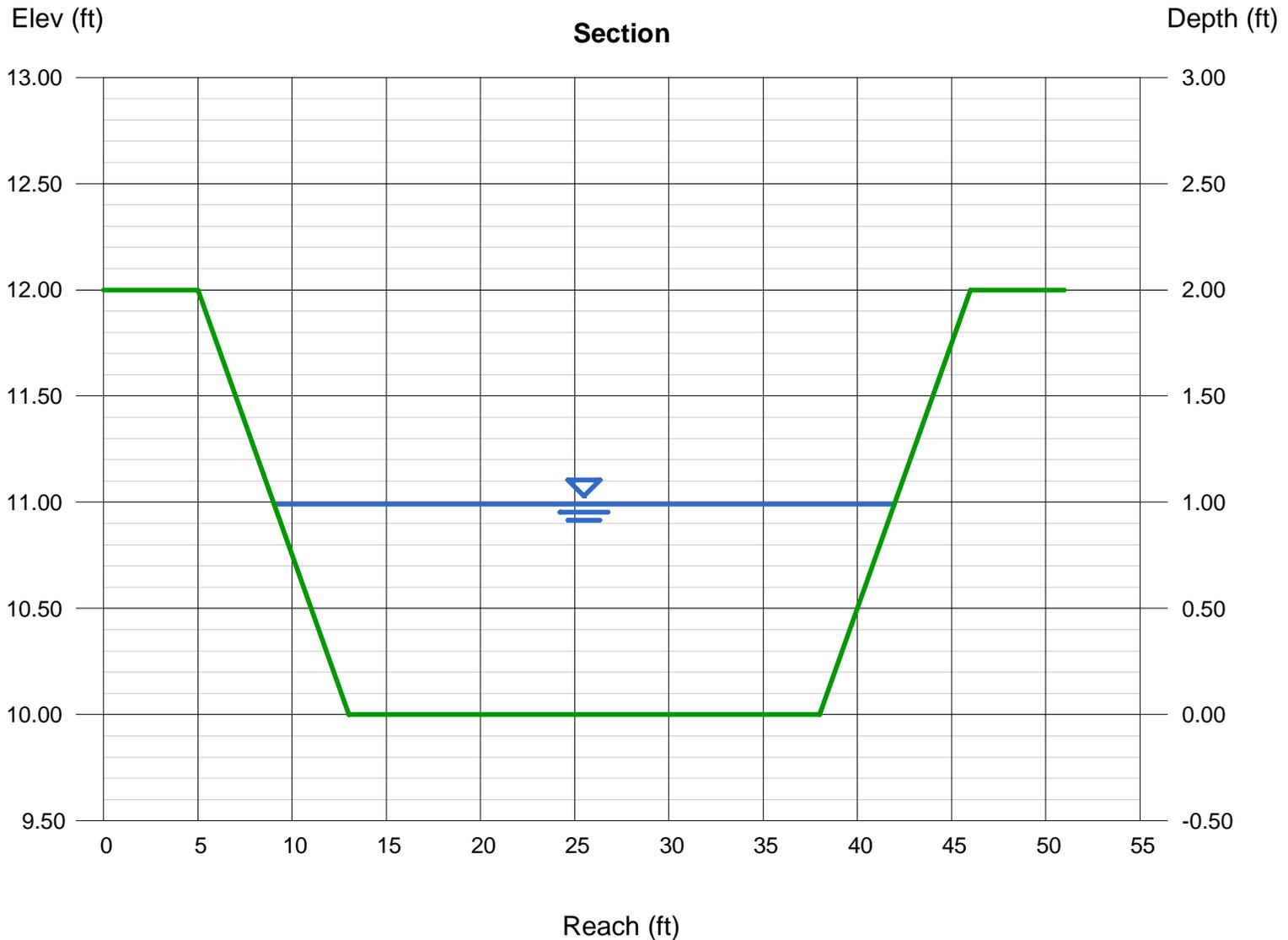
Bottom Width (ft) = 25.00  
Side Slopes (z:1) = 4.00, 4.00  
Total Depth (ft) = 2.00  
Invert Elev (ft) = 10.00  
Slope (%) = 1.50  
N-Value = 0.030

### Highlighted

Depth (ft) = 0.99  
Q (cfs) = 155.80  
Area (sqft) = 28.67  
Velocity (ft/s) = 5.43  
Wetted Perim (ft) = 33.16  
Crit Depth,  $Y_c$  (ft) = 1.01  
Top Width (ft) = 32.92  
EGL (ft) = 1.45

### Calculations

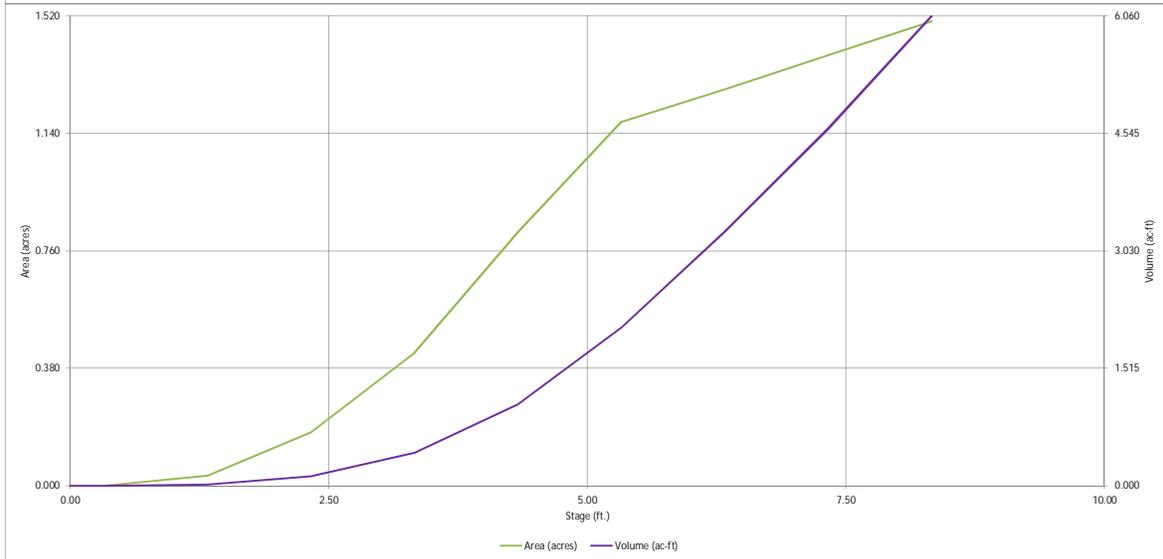
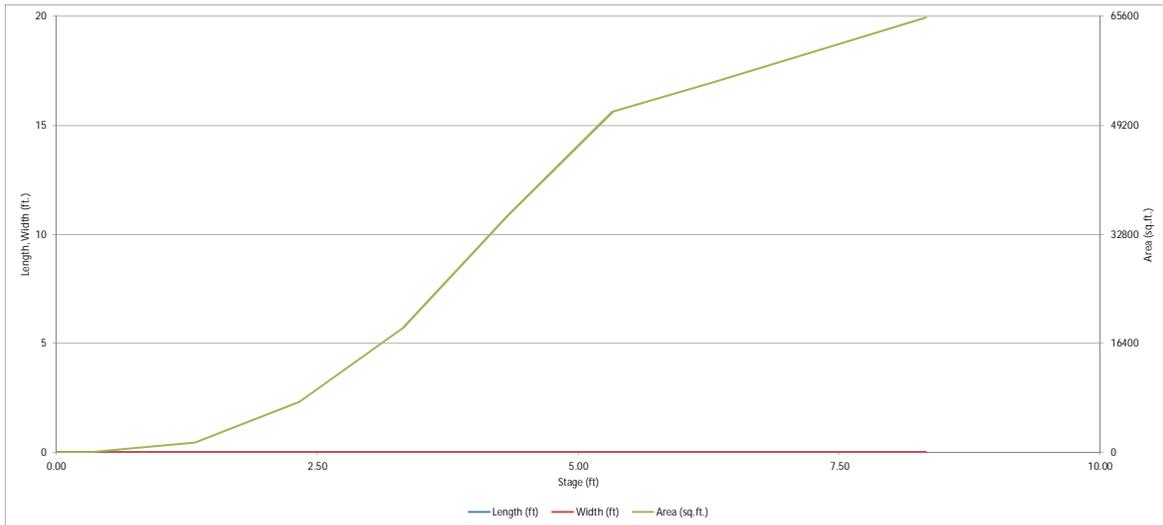
Compute by: Known Q  
Known Q (cfs) = 155.80





# DETENTION BASIN STAGE-STORAGE TABLE BUILDER

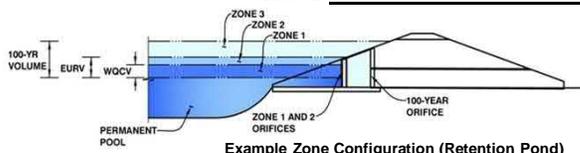
*MHFD-Detention, Version 4.03 (May 2020)*



# DETENTION BASIN OUTLET STRUCTURE DESIGN

*MHFD-Detention, Version 4.03 (May 2020)*

Project: Cloverleaf Filling No. 2  
Basin I.D.: Pond P2



|                          | Estimated Stage (ft) | Estimated Volume (ac-ft) | Outlet Type          |
|--------------------------|----------------------|--------------------------|----------------------|
| Zone 1 (WOCV)            | 3.68                 | 0.590                    | Orifice Plate        |
| Zone 2 (EURV)            | 5.25                 | 1.348                    | Circular Orifice     |
| Zone 3 (100-year)        | 6.29                 | 1.279                    | Weir&Pipe (Restrict) |
| <b>Total (all zones)</b> |                      | <b>3.216</b>             |                      |

User Input: Orifice at Underdrain Outlet (typically used to drain WOCV in a Filtration BMP)

|                                   |     |  |
|-----------------------------------|-----|--|
| Underdrain Orifice Invert Depth = | N/A | ft (distance below the filtration media surface) |
| Underdrain Orifice Diameter =     | N/A | inches   |

Calculated Parameters for Underdrain

|                               |     |                 |
|-------------------------------|-----|-----------------|
| Underdrain Orifice Area =     | N/A | ft <sup>2</sup> |
| Underdrain Orifice Centroid = | N/A | feet            |

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WOCV and/or EURV in a sedimentation BMP)

|  |      |   |
|--|------|---|
| Invert of Lowest Orifice =                 | 0.00 | ft (relative to basin bottom at Stage = 0 ft) |
| Depth at top of Zone using Orifice Plate = | 3.68 | ft (relative to basin bottom at Stage = 0 ft) |
| Orifice Plate: Orifice Vertical Spacing =  | N/A  | inches  |
| Orifice Plate: Orifice Area per Row =      | N/A  | inches  |

Calculated Parameters for Plate

|                            |     |                 |
|----------------------------|-----|-----------------|
| WQ Orifice Area per Row =  | N/A | ft <sup>2</sup> |
| Elliptical Half-Width =    | N/A | feet            |
| Elliptical Slot Centroid = | N/A | feet            |
| Elliptical Slot Area =     | N/A | ft <sup>2</sup> |

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

|                                | Row 1 (required) | Row 2 (optional) | Row 3 (optional) | Row 4 (optional) | Row 5 (optional) | Row 6 (optional) | Row 7 (optional) | Row 8 (optional) |
|--------------------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|
| Stage of Orifice Centroid (ft) | 0.00             | 1.20             | 2.40             |                  |                  |                  |                  |                  |
| Orifice Area (sq. inches)      | 1.59             | 1.59             | 1.59             |                  |                  |                  |                  |                  |

|                                | Row 9 (optional) | Row 10 (optional) | Row 11 (optional) | Row 12 (optional) | Row 13 (optional) | Row 14 (optional) | Row 15 (optional) | Row 16 (optional) |
|--------------------------------|------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| Stage of Orifice Centroid (ft) |                  |                   |                   |                   |                   |                   |                   |                   |
| Orifice Area (sq. inches)      |                  |                   |                   |                   |                   |                   |                   |                   |

User Input: Vertical Orifice (Circular or Rectangular)

|   | Zone 2 Circular | Not Selected |   |
|---|-----------------|--------------|---|
| Invert of Vertical Orifice =                  | 3.60            | N/A          | ft (relative to basin bottom at Stage = 0 ft) |
| Depth at top of Zone using Vertical Orifice = | 5.25            | N/A          | ft (relative to basin bottom at Stage = 0 ft) |
| Vertical Orifice Diameter =                   | 3.25            | N/A          | inches  |

Calculated Parameters for Vertical Orifice

|                             | Zone 2 Circular | Not Selected |                 |
|-----------------------------|-----------------|--------------|-----------------|
| Vertical Orifice Area =     | 0.06            | N/A          | ft <sup>2</sup> |
| Vertical Orifice Centroid = | 0.14            | N/A          | feet            |

User Input: Overflow Weir (Dropbox with Flat or Sloped Gate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe))

|                                       | Zone 3 Weir | Not Selected |   |
|---------------------------------------|-------------|--------------|---|
| Overflow Weir Front Edge Height, Ho = | 5.26        | N/A          | ft (relative to basin bottom at Stage = 0 ft) |
| Overflow Weir Front Edge Length =     | 10.00       | N/A          | feet  |
| Overflow Weir Gate Slope =            | 0.00        | N/A          | H:V   |
| Horiz. Length of Weir Sides =         | 17.50       | N/A          | feet  |
| Overflow Gate Open Area % =           | 70%         | N/A          | % , gate open area/total area                 |
| Debris Clogging % =                   | 50%         | N/A          | %   |

Calculated Parameters for Overflow Weir

|   | Zone 3 Weir | Not Selected |                 |
|---|-------------|--------------|-----------------|
| Height of Gate Upper Edge, H <sub>1</sub> = | 5.26        | N/A          | feet            |
| Overflow Weir Slope Length =                | 17.50       | N/A          | feet            |
| Gate Open Area / 100-yr Orifice Area =      | 14.68       | N/A          |                 |
| Overflow Gate Open Area w/o Debris =        | 122.50      | N/A          | ft <sup>2</sup> |
| Overflow Gate Open Area w/ Debris =         | 61.25       | N/A          | ft <sup>2</sup> |

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

|   | Zone 3 Restrictor | Not Selected |  |
|---|-------------------|--------------|--|
| Depth to Invert of Outlet Pipe =            | 2.50              | N/A          | ft (distance below basin bottom at Stage = 0 ft) |
| Outlet Pipe Diameter =                      | 42.00             | N/A          | inches   |
| Restrictor Plate Height Above Pipe Invert = | 34.00             |              | inches   |

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate

|  | Zone 3 Restrictor | Not Selected |                 |
|--|-------------------|--------------|-----------------|
| Outlet Orifice Area =                            | 8.34              | N/A          | ft <sup>2</sup> |
| Outlet Orifice Centroid =                        | 1.54              | N/A          | feet            |
| Half-Central Angle of Restrictor Plate on Pipe = | 2.24              | N/A          | radians         |

User Input: Emergency Spillway (Rectangular or Trapezoidal)

|                                     |       |   |
|-------------------------------------|-------|---|
| Spillway Invert Stage =             | 6.45  | ft (relative to basin bottom at Stage = 0 ft) |
| Spillway Crest Length =             | 45.00 | feet  |
| Spillway End Slopes =               | 4.00  | H:V   |
| Freeboard above Max Water Surface = | 1.00  | feet  |

Calculated Parameters for Spillway

|                                    |      |         |
|------------------------------------|------|---------|
| Spillway Design Flow Depth =       | 0.79 | feet    |
| Stage at Top of Freeboard =        | 8.24 | feet    |
| Basin Area at Top of Freeboard =   | 1.49 | acres   |
| Basin Volume at Top of Freeboard = | 5.92 | acre-ft |

## Routed Hydrograph Results

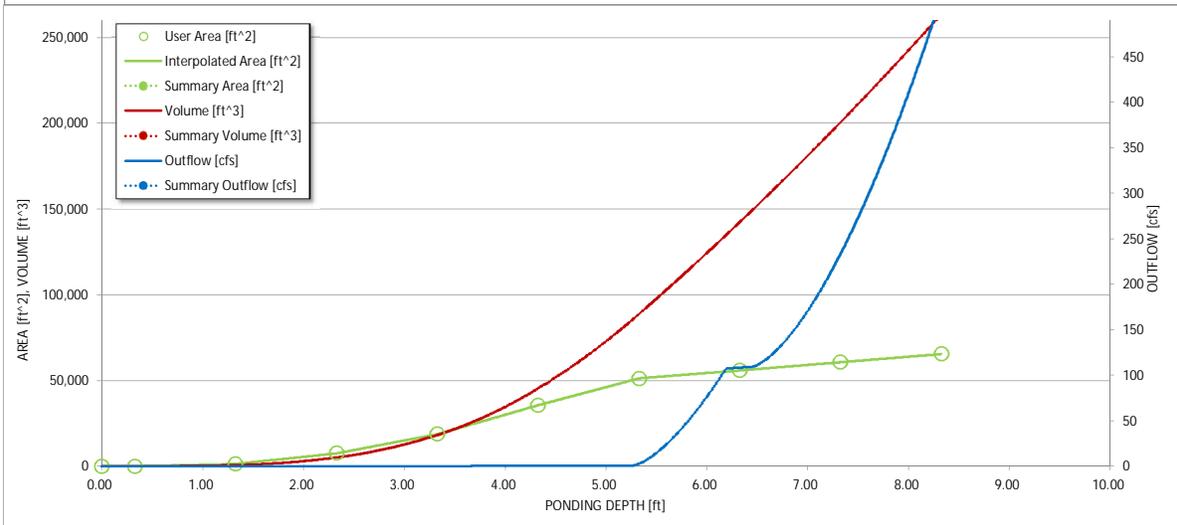
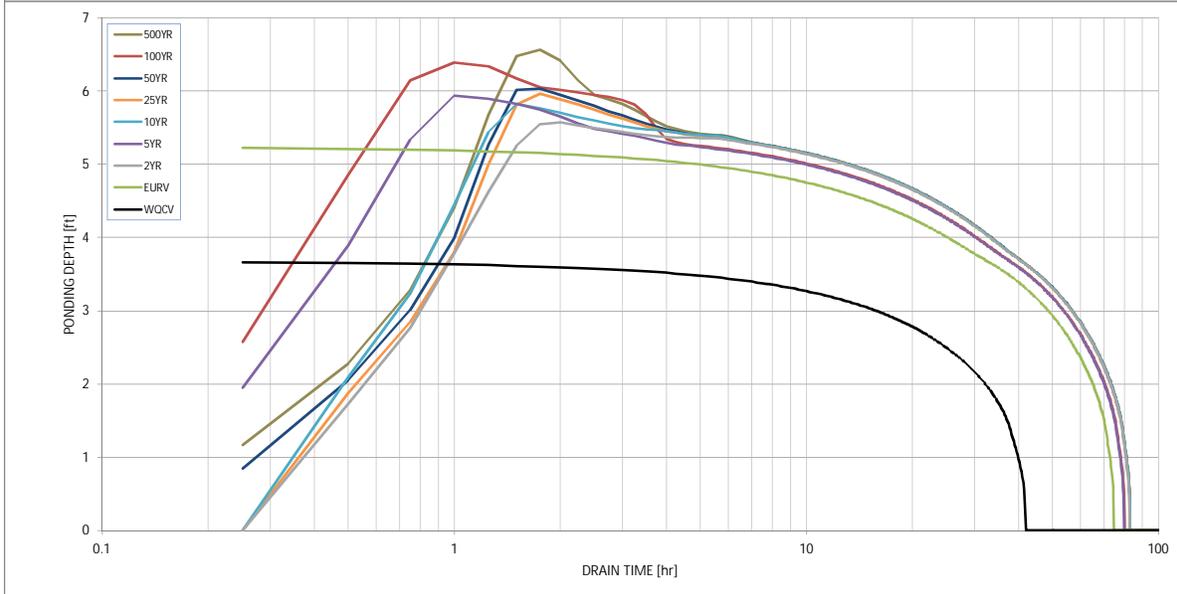
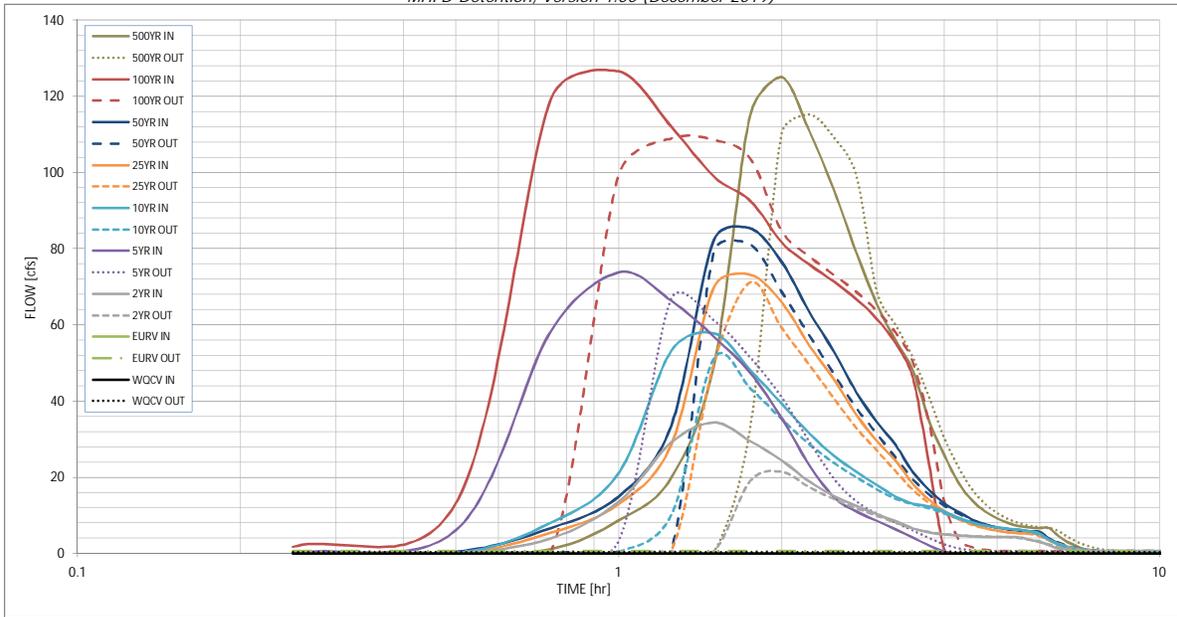
*The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).*

|  | WOCV               | EURV               | 2 Year          | 5 Year          | 10 Year         | 25 Year         | 50 Year         | 100 Year       | 500 Year |
|--|--------------------|--------------------|-----------------|-----------------|-----------------|-----------------|-----------------|----------------|----------|
| Design Storm Return Period                       | N/A                | N/A                | 1.19            | 1.50            | 1.75            | 2.00            | 2.25            | 2.52           | 3.00     |
| One-Hour Rainfall Depth (in)                     | N/A                | N/A                | 1.19            | 1.50            | 1.75            | 2.00            | 2.25            | 2.52           | 3.00     |
| CUHP Runoff Volume (acre-ft)                     | 0.590              | 1.938              | 1.760           | 2.442           | 3.030           | 3.781           | 4.411           | 5.191          | 6.432    |
| User Override Inflow Hydrograph Volume (acre-ft) | N/A                | N/A                | 5.280           | 8.575           | 9.090           | 11.343          | 13.233          | 21.621         |          |
| CUHP Predevelopment Peak Q (cfs)                 | N/A                | N/A                | 4.0             | 11.4            | 17.1            | 30.1            | 37.8            | 47.3           | 61.5     |
| OPTIONAL Override Predevelopment Peak Q (cfs)    | N/A                | N/A                |                 |                 |                 |                 |                 |                |          |
| Predevelopment Unit Peak Flow, q (cfs/acre)      | N/A                | N/A                | 0.13            | 0.37            | 0.56            | 0.98            | 1.24            | 1.55           | 2.01     |
| Peak Inflow Q (cfs)                              | N/A                | N/A                | 34.3            | 73.7            | 57.8            | 73.1            | 85.3            | 126.5          | 125.0    |
| Peak Outflow Q (cfs)                             | 0.3                | 0.7                | 21.4            | 66.8            | 51.2            | 71.2            | 81.1            | 108.9          | 115.2    |
| Ratio Peak Outflow to Predevelopment Q           | N/A                | N/A                | N/A             | 5.9             | 3.0             | 2.4             | 2.1             | 2.3            | 1.9      |
| Structure Controlling Flow                       | Vertical Orifice 1 | Vertical Orifice 1 | Overflow Weir 1 | Outlet Plate 1 | Spillway |
| Max Velocity through Gate 1 (fps)                | N/A                | N/A                | 0.17            | 0.5             | 0.4             | 0.6             | 0.7             | 0.9            | 0.9      |
| Max Velocity through Gate 2 (fps)                | N/A                | N/A                | N/A             | N/A             | N/A             | N/A             | N/A             | N/A            | N/A      |
| Time to Drain 97% of Inflow Volume (hours)       | 30                 | 66                 | 65              | 56              | 58              | 54              | 51              | 36             | 42       |
| Time to Drain 99% of Inflow Volume (hours)       | 40                 | 71                 | 75              | 69              | 71              | 69              | 68              | 59             | 63       |
| Maximum Ponding Depth (ft)                       | 3.68               | 5.25               | 5.57            | 5.94            | 5.83            | 5.97            | 6.03            | 6.39           | 6.56     |
| Area at Maximum Ponding Depth (acres)            | 0.57               | 1.15               | 1.20            | 1.24            | 1.23            | 1.24            | 1.25            | 1.29           | 1.31     |
| Maximum Volume Stored (acre-ft)                  | 0.594              | 1.948              | 2.327           | 2.766           | 2.631           | 2.804           | 2.891           | 3.335          | 3.569    |

Drain time shown in SWMM Model Results

# DETENTION BASIN OUTLET STRUCTURE DESIGN

*MHFD-Detention, Version 4.00 (December 2019)*



| S-A-V-D Chart Axis Override | X-axis | Left Y-Axis | Right Y-Axis |
|-----------------------------|--------|-------------|--------------|
| minimum bound               |        |             |              |
| maximum bound               |        |             |              |

Values from 5-yr SWMM model

Values from 100-yr SWMM model

## DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename: \_\_\_\_\_

**Inflow Hydrographs**

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program

| User-Defined  | SOURCE   | CUHP       | CUHP       | CUHP         | USER         | CUHP          | CUHP          | CUHP          | USER           | CUHP           |
|---------------|----------|------------|------------|--------------|--------------|---------------|---------------|---------------|----------------|----------------|
| Time Interval | TIME     | WOCV [cfs] | EURV [cfs] | 2 Year [cfs] | 5 Year [cfs] | 10 Year [cfs] | 25 Year [cfs] | 50 Year [cfs] | 100 Year [cfs] | 500 Year [cfs] |
| 15.00 min     | 0:00:00  | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 0:15:00  | 0.00       | 0.00       | 0.00         | 0.11         | 0.00          | 0.00          | 0.00          | 1.73           | 0.00           |
|               | 0:30:00  | 0.00       | 0.00       | 0.00         | 6.05         | 0.00          | 0.00          | 0.45          | 13.14          | 1.13           |
|               | 0:45:00  | 0.00       | 0.00       | 3.99         | 58.42        | 8.07          | 5.42          | 6.68          | 119.28         | 8.64           |
|               | 1:00:00  | 0.00       | 0.00       | 13.54        | 73.74        | 21.08         | 12.93         | 14.96         | 126.49         | 19.77          |
|               | 1:15:00  | 0.00       | 0.00       | 29.09        | 66.33        | 53.09         | 28.50         | 33.46         | 112.06         | 49.39          |
|               | 1:30:00  | 0.00       | 0.00       | 34.32        | 56.86        | 57.77         | 69.83         | 82.32         | 98.86          | 115.02         |
|               | 1:45:00  | 0.00       | 0.00       | 29.47        | 47.39        | 48.16         | 73.15         | 85.31         | 92.61          | 125.01         |
|               | 2:00:00  | 0.00       | 0.00       | 24.43        | 35.56        | 39.27         | 65.91         | 76.55         | 81.62          | 110.96         |
|               | 2:15:00  | 0.00       | 0.00       | 18.86        | 23.22        | 31.54         | 54.62         | 63.42         | 75.86          | 95.29          |
|               | 2:30:00  | 0.00       | 0.00       | 15.06        | 14.72        | 25.59         | 45.66         | 52.94         | 71.31          | 78.98          |
|               | 2:45:00  | 0.00       | 0.00       | 12.49        | 11.00        | 21.44         | 36.35         | 42.30         | 66.75          | 65.47          |
|               | 3:00:00  | 0.00       | 0.00       | 10.31        | 8.57         | 17.92         | 29.55         | 34.50         | 61.57          | 55.86          |
|               | 3:15:00  | 0.00       | 0.00       | 8.53         | 6.31         | 14.93         | 24.27         | 28.40         | 55.14          | 47.93          |
|               | 3:30:00  | 0.00       | 0.00       | 6.57         | 4.19         | 13.03         | 18.13         | 21.27         | 45.91          | 34.67          |
|               | 3:45:00  | 0.00       | 0.00       | 5.49         | 2.03         | 12.32         | 14.10         | 16.64         | 23.07          | 25.75          |
|               | 4:00:00  | 0.00       | 0.00       | 4.97         | 0.45         | 10.97         | 11.10         | 13.08         | 0.90           | 18.54          |
|               | 4:15:00  | 0.00       | 0.00       | 4.66         | 0.03         | 9.28          | 9.25          | 10.88         | 0.12           | 13.89          |
|               | 4:30:00  | 0.00       | 0.00       | 4.50         | 0.02         | 8.14          | 7.65          | 8.93          | 0.02           | 11.11          |
|               | 4:45:00  | 0.00       | 0.00       | 4.38         | 0.01         | 7.36          | 6.60          | 7.62          | 0.02           | 9.22           |
|               | 5:00:00  | 0.00       | 0.00       | 4.30         | 0.00         | 6.84          | 5.95          | 6.82          | 0.00           | 8.00           |
|               | 5:15:00  | 0.00       | 0.00       | 4.25         | 0.00         | 6.49          | 5.51          | 6.27          | 0.00           | 7.20           |
|               | 5:30:00  | 0.00       | 0.00       | 4.23         | 0.00         | 6.23          | 5.25          | 5.94          | 0.00           | 6.81           |
|               | 5:45:00  | 0.00       | 0.00       | 3.56         | 0.00         | 5.85          | 5.10          | 5.76          | 0.00           | 6.66           |
|               | 6:00:00  | 0.00       | 0.00       | 3.08         | 0.00         | 5.21          | 5.02          | 5.65          | 0.00           | 6.61           |
|               | 6:15:00  | 0.00       | 0.00       | 2.09         | 0.00         | 3.52          | 3.40          | 3.83          | 0.00           | 4.50           |
|               | 6:30:00  | 0.00       | 0.00       | 1.37         | 0.00         | 2.33          | 2.25          | 2.53          | 0.00           | 2.98           |
|               | 6:45:00  | 0.00       | 0.00       | 0.89         | 0.00         | 1.52          | 1.48          | 1.66          | 0.00           | 1.96           |
|               | 7:00:00  | 0.00       | 0.00       | 0.55         | 0.00         | 0.95          | 0.93          | 1.04          | 0.00           | 1.22           |
|               | 7:15:00  | 0.00       | 0.00       | 0.32         | 0.00         | 0.58          | 0.58          | 0.65          | 0.00           | 0.77           |
|               | 7:30:00  | 0.00       | 0.00       | 0.16         | 0.00         | 0.31          | 0.33          | 0.37          | 0.00           | 0.43           |
|               | 7:45:00  | 0.00       | 0.00       | 0.07         | 0.00         | 0.13          | 0.15          | 0.17          | 0.00           | 0.19           |
|               | 8:00:00  | 0.00       | 0.00       | 0.02         | 0.00         | 0.03          | 0.04          | 0.04          | 0.00           | 0.05           |
|               | 8:15:00  | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 8:30:00  | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 8:45:00  | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 9:00:00  | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 9:15:00  | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 9:30:00  | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 9:45:00  | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 10:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 10:15:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 10:30:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 10:45:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 11:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 11:15:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 11:30:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 11:45:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 12:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 12:15:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 12:30:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 12:45:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 13:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 13:15:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 13:30:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 13:45:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 14:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 14:15:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 14:30:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 14:45:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 15:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 15:15:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 15:30:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 15:45:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 16:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 16:15:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 16:30:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 16:45:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 17:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 17:15:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 17:30:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 17:45:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 18:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |

SWMM Model Results

Controlled Release From Pond 2

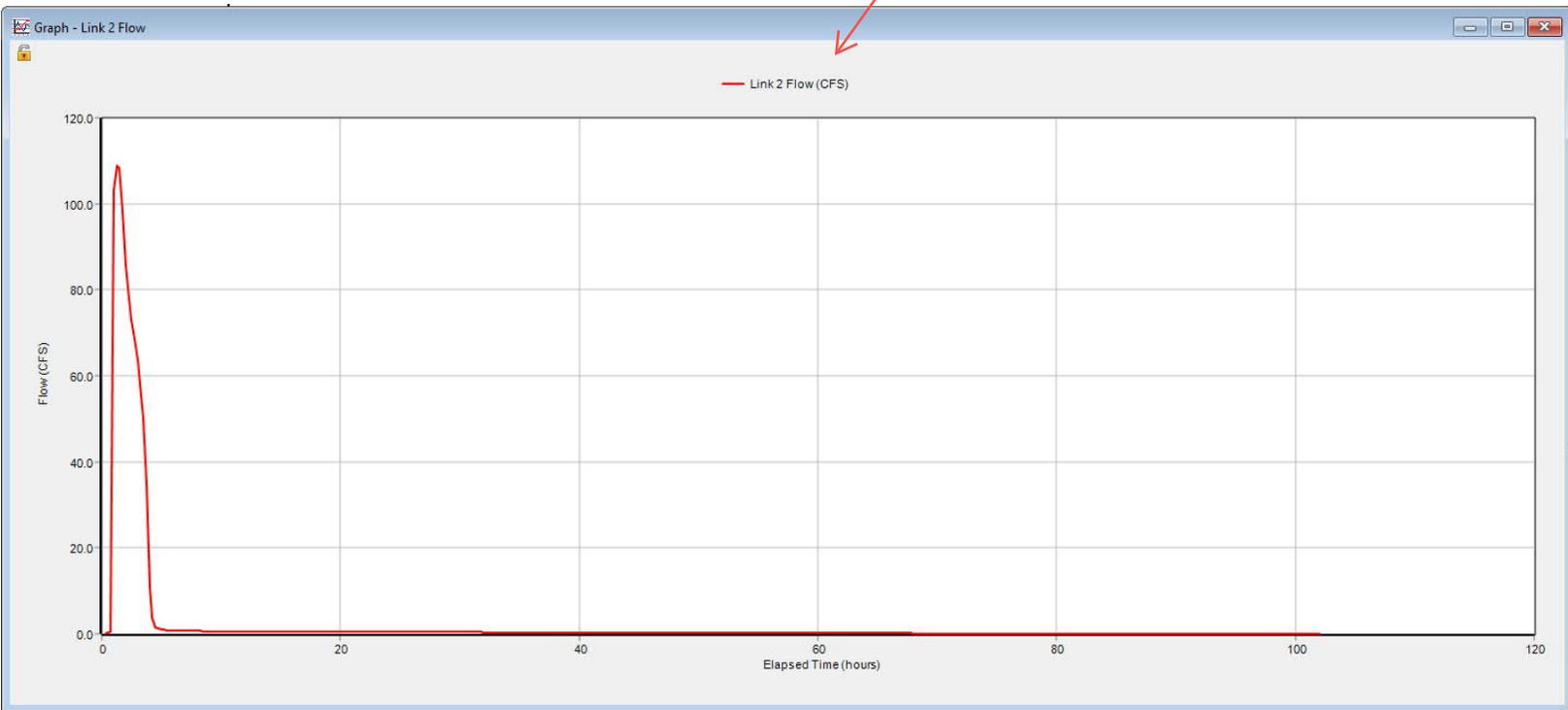
Table - Link 2

| Days | Hours    | Flow (CFS) | Days | Hours    | Flow (CFS) | Days | Hours    | Flow (CFS) |
|------|----------|------------|------|----------|------------|------|----------|------------|
| 0    | 0:15:00  | 0.05       | 0    | 11:15:00 | 0.61       | 0    | 22:15:00 | 0.51       |
| 0    | 0:30:00  | 0.15       | 0    | 11:30:00 | 0.6        | 0    | 22:30:00 | 0.51       |
| 0    | 0:45:00  | 0.56       | 0    | 11:45:00 | 0.6        | 0    | 22:45:00 | 0.5        |
| 0    | 1:00:00  | 103.24     | 0    | 12:00:00 | 0.6        | 0    | 23:00:00 | 0.5        |
| 0    | 1:15:00  | 108.78     | 0    | 12:15:00 | 0.6        | 0    | 23:15:00 | 0.5        |
| 0    | 1:30:00  | 108.32     | 0    | 12:30:00 | 0.6        | 0    | 23:30:00 | 0.5        |
| 0    | 1:45:00  | 98.26      | 0    | 12:45:00 | 0.6        | 0    | 23:45:00 | 0.49       |
| 0    | 2:00:00  | 85.7       | 0    | 13:00:00 | 0.6        | 1    | 0:00:00  | 0.49       |
| 0    | 2:15:00  | 77.89      | 0    | 13:15:00 | 0.59       | 1    | 0:15:00  | 0.49       |
| 0    | 2:30:00  | 73.07      | 0    | 13:30:00 | 0.59       | 1    | 0:30:00  | 0.48       |
| 0    | 2:45:00  | 68.56      | 0    | 13:45:00 | 0.59       | 1    | 0:45:00  | 0.48       |
| 0    | 3:00:00  | 63.64      | 0    | 14:00:00 | 0.59       | 1    | 1:00:00  | 0.48       |
| 0    | 3:15:00  | 57.91      | 0    | 14:15:00 | 0.59       | 1    | 1:15:00  | 0.47       |
| 0    | 3:30:00  | 50.04      | 0    | 14:30:00 | 0.59       | 1    | 1:30:00  | 0.47       |
| 0    | 3:45:00  | 34.77      | 0    | 14:45:00 | 0.58       | 1    | 1:45:00  | 0.46       |
| 0    | 4:00:00  | 11.01      | 0    | 15:00:00 | 0.58       | 1    | 2:00:00  | 0.46       |
| 0    | 4:15:00  | 3.84       | 0    | 15:15:00 | 0.58       | 1    | 2:15:00  | 0.46       |
| 0    | 4:30:00  | 1.6        | 0    | 15:30:00 | 0.58       | 1    | 2:30:00  | 0.45       |
| 0    | 4:45:00  | 1.34       | 0    | 15:45:00 | 0.57       | 1    | 2:45:00  | 0.45       |
| 0    | 5:00:00  | 1.13       | 0    | 16:00:00 | 0.57       | 1    | 3:00:00  | 0.45       |
| 0    | 5:15:00  | 0.95       | 0    | 16:15:00 | 0.57       | 1    | 3:15:00  | 0.44       |
| 0    | 5:30:00  | 0.79       | 0    | 16:30:00 | 0.57       | 1    | 3:30:00  | 0.44       |
| 0    | 5:45:00  | 0.66       | 0    | 16:45:00 | 0.56       | 1    | 3:45:00  | 0.44       |
| 0    | 6:00:00  | 0.65       | 0    | 17:00:00 | 0.56       | 1    | 4:00:00  | 0.43       |
| 0    | 6:15:00  | 0.65       | 0    | 17:15:00 | 0.56       | 1    | 4:15:00  | 0.43       |
| 0    | 6:30:00  | 0.65       | 0    | 17:30:00 | 0.56       | 1    | 4:30:00  | 0.43       |
| 0    | 6:45:00  | 0.65       | 0    | 17:45:00 | 0.55       | 1    | 4:45:00  | 0.42       |
| 0    | 7:00:00  | 0.64       | 0    | 18:00:00 | 0.55       | 1    | 5:00:00  | 0.42       |
| 0    | 7:15:00  | 0.64       | 0    | 18:15:00 | 0.55       | 1    | 5:15:00  | 0.42       |
| 0    | 7:30:00  | 0.64       | 0    | 18:30:00 | 0.55       | 1    | 5:30:00  | 0.42       |
| 0    | 7:45:00  | 0.64       | 0    | 18:45:00 | 0.54       | 1    | 5:45:00  | 0.41       |
| 0    | 8:00:00  | 0.64       | 0    | 19:00:00 | 0.54       | 1    | 6:00:00  | 0.41       |
| 0    | 8:15:00  | 0.64       | 0    | 19:15:00 | 0.54       | 1    | 6:15:00  | 0.41       |
| 0    | 8:30:00  | 0.63       | 0    | 19:30:00 | 0.54       | 1    | 6:30:00  | 0.4        |
| 0    | 8:45:00  | 0.63       | 0    | 19:45:00 | 0.53       | 1    | 6:45:00  | 0.4        |
| 0    | 9:00:00  | 0.63       | 0    | 20:00:00 | 0.53       | 1    | 7:00:00  | 0.4        |
| 0    | 9:15:00  | 0.63       | 0    | 20:15:00 | 0.53       | 1    | 7:15:00  | 0.39       |
| 0    | 9:30:00  | 0.62       | 0    | 20:30:00 | 0.53       | 1    | 7:30:00  | 0.39       |
| 0    | 9:45:00  | 0.62       | 0    | 20:45:00 | 0.52       | 1    | 7:45:00  | 0.38       |
| 0    | 10:00:00 | 0.62       | 0    | 21:00:00 | 0.52       | 1    | 8:00:00  | 0.38       |
| 0    | 10:15:00 | 0.62       | 0    | 21:15:00 | 0.52       | 1    | 8:15:00  | 0.38       |
| 0    | 10:30:00 | 0.61       | 0    | 21:30:00 | 0.52       | 1    | 8:30:00  | 0.37       |
| 0    | 10:45:00 | 0.61       | 0    | 21:45:00 | 0.51       | 1    | 8:45:00  | 0.37       |
| 0    | 11:00:00 | 0.61       | 0    | 22:00:00 | 0.51       | 1    | 9:00:00  | 0.36       |

| Days | Hours    | Flow (CFS) | Days | Hours    | Flow (CFS) | Days | Hours    | Flow (CFS) |
|------|----------|------------|------|----------|------------|------|----------|------------|
| 1    | 9:15:00  | 0.36       | 1    | 20:30:00 | 0.23       | 2    | 7:45:00  | 0.19       |
| 1    | 9:30:00  | 0.36       | 1    | 20:45:00 | 0.23       | 2    | 8:00:00  | 0.19       |
| 1    | 9:45:00  | 0.35       | 1    | 21:00:00 | 0.23       | 2    | 8:15:00  | 0.19       |
| 1    | 10:00:00 | 0.35       | 1    | 21:15:00 | 0.23       | 2    | 8:30:00  | 0.18       |
| 1    | 10:15:00 | 0.34       | 1    | 21:30:00 | 0.23       | 2    | 8:45:00  | 0.18       |
| 1    | 10:30:00 | 0.34       | 1    | 21:45:00 | 0.23       | 2    | 9:00:00  | 0.18       |
| 1    | 10:45:00 | 0.34       | 1    | 22:00:00 | 0.22       | 2    | 9:15:00  | 0.18       |
| 1    | 11:00:00 | 0.33       | 1    | 22:15:00 | 0.22       | 2    | 9:30:00  | 0.18       |
| 1    | 11:15:00 | 0.33       | 1    | 22:30:00 | 0.22       | 2    | 9:45:00  | 0.18       |
| 1    | 11:30:00 | 0.32       | 1    | 22:45:00 | 0.22       | 2    | 10:00:00 | 0.18       |
| 1    | 11:45:00 | 0.32       | 1    | 23:00:00 | 0.22       | 2    | 10:15:00 | 0.18       |
| 1    | 12:00:00 | 0.32       | 1    | 23:15:00 | 0.22       | 2    | 10:30:00 | 0.18       |
| 1    | 12:15:00 | 0.31       | 1    | 23:30:00 | 0.22       | 2    | 10:45:00 | 0.18       |
| 1    | 12:30:00 | 0.31       | 1    | 23:45:00 | 0.22       | 2    | 11:00:00 | 0.17       |
| 1    | 12:45:00 | 0.31       | 2    | 0:00:00  | 0.22       | 2    | 11:15:00 | 0.17       |
| 1    | 13:00:00 | 0.3        | 2    | 0:15:00  | 0.22       | 2    | 11:30:00 | 0.17       |
| 1    | 13:15:00 | 0.3        | 2    | 0:30:00  | 0.22       | 2    | 11:45:00 | 0.17       |
| 1    | 13:30:00 | 0.29       | 2    | 0:45:00  | 0.21       | 2    | 12:00:00 | 0.17       |
| 1    | 13:45:00 | 0.29       | 2    | 1:00:00  | 0.21       | 2    | 12:15:00 | 0.17       |
| 1    | 14:00:00 | 0.29       | 2    | 1:15:00  | 0.21       | 2    | 12:30:00 | 0.17       |
| 1    | 14:15:00 | 0.28       | 2    | 1:30:00  | 0.21       | 2    | 12:45:00 | 0.17       |
| 1    | 14:30:00 | 0.28       | 2    | 1:45:00  | 0.21       | 2    | 13:00:00 | 0.16       |
| 1    | 14:45:00 | 0.28       | 2    | 2:00:00  | 0.21       | 2    | 13:15:00 | 0.16       |
| 1    | 15:00:00 | 0.27       | 2    | 2:15:00  | 0.21       | 2    | 13:30:00 | 0.16       |
| 1    | 15:15:00 | 0.27       | 2    | 2:30:00  | 0.21       | 2    | 13:45:00 | 0.16       |
| 1    | 15:30:00 | 0.26       | 2    | 2:45:00  | 0.21       | 2    | 14:00:00 | 0.16       |
| 1    | 15:45:00 | 0.26       | 2    | 3:00:00  | 0.21       | 2    | 14:15:00 | 0.16       |
| 1    | 16:00:00 | 0.26       | 2    | 3:15:00  | 0.21       | 2    | 14:30:00 | 0.16       |
| 1    | 16:15:00 | 0.25       | 2    | 3:30:00  | 0.2        | 2    | 14:45:00 | 0.16       |
| 1    | 16:30:00 | 0.25       | 2    | 3:45:00  | 0.2        | 2    | 15:00:00 | 0.16       |
| 1    | 16:45:00 | 0.25       | 2    | 4:00:00  | 0.2        | 2    | 15:15:00 | 0.15       |
| 1    | 17:00:00 | 0.24       | 2    | 4:15:00  | 0.2        | 2    | 15:30:00 | 0.15       |
| 1    | 17:15:00 | 0.24       | 2    | 4:30:00  | 0.2        | 2    | 15:45:00 | 0.15       |
| 1    | 17:30:00 | 0.24       | 2    | 4:45:00  | 0.2        | 2    | 16:00:00 | 0.15       |
| 1    | 17:45:00 | 0.24       | 2    | 5:00:00  | 0.2        | 2    | 16:15:00 | 0.15       |
| 1    | 18:00:00 | 0.24       | 2    | 5:15:00  | 0.2        | 2    | 16:30:00 | 0.15       |
| 1    | 18:15:00 | 0.24       | 2    | 5:30:00  | 0.2        | 2    | 16:45:00 | 0.15       |
| 1    | 18:30:00 | 0.24       | 2    | 5:45:00  | 0.2        | 2    | 17:00:00 | 0.14       |
| 1    | 18:45:00 | 0.24       | 2    | 6:00:00  | 0.19       | 2    | 17:15:00 | 0.14       |
| 1    | 19:00:00 | 0.23       | 2    | 6:15:00  | 0.19       | 2    | 17:30:00 | 0.14       |
| 1    | 19:15:00 | 0.23       | 2    | 6:30:00  | 0.19       | 2    | 17:45:00 | 0.14       |
| 1    | 19:30:00 | 0.23       | 2    | 6:45:00  | 0.19       | 2    | 18:00:00 | 0.14       |
| 1    | 19:45:00 | 0.23       | 2    | 7:00:00  | 0.19       | 2    | 18:15:00 | 0.14       |
| 1    | 20:00:00 | 0.23       | 2    | 7:15:00  | 0.19       | 2    | 18:30:00 | 0.14       |
| 1    | 20:15:00 | 0.23       | 2    | 7:30:00  | 0.19       | 2    | 18:45:00 | 0.13       |

| Days | Hours    | Flow (CFS) | Days | Hours   | Flow (CFS) |
|------|----------|------------|------|---------|------------|
| 2    | 19:00:00 | 0.13       | 3    | 6:15:00 | 0.04       |
| 2    | 19:15:00 | 0.13       | 3    | 6:30:00 | 0.04       |
| 2    | 19:30:00 | 0.13       | 3    | 6:45:00 | 0.04       |
| 2    | 19:45:00 | 0.13       | 3    | 7:00:00 | 0          |
| 2    | 20:00:00 | 0.13       | 3    | 7:15:00 | 0          |
| 2    | 20:15:00 | 0.13       |      |         |            |
| 2    | 20:30:00 | 0.12       |      |         |            |
| 2    | 20:45:00 | 0.12       |      |         |            |
| 2    | 21:00:00 | 0.12       |      |         |            |
| 2    | 21:15:00 | 0.12       |      |         |            |
| 2    | 21:30:00 | 0.12       |      |         |            |
| 2    | 21:45:00 | 0.12       |      |         |            |
| 2    | 22:00:00 | 0.12       |      |         |            |
| 2    | 22:15:00 | 0.11       |      |         |            |
| 2    | 22:30:00 | 0.11       |      |         |            |
| 2    | 22:45:00 | 0.11       |      |         |            |
| 2    | 23:00:00 | 0.11       |      |         |            |
| 2    | 23:15:00 | 0.11       |      |         |            |
| 2    | 23:30:00 | 0.11       |      |         |            |
| 2    | 23:45:00 | 0.11       |      |         |            |
| 3    | 0:00:00  | 0.11       |      |         |            |
| 3    | 0:15:00  | 0.1        |      |         |            |
| 3    | 0:30:00  | 0.1        |      |         |            |
| 3    | 0:45:00  | 0.1        |      |         |            |
| 3    | 1:00:00  | 0.1        |      |         |            |
| 3    | 1:15:00  | 0.1        |      |         |            |
| 3    | 1:30:00  | 0.1        |      |         |            |
| 3    | 1:45:00  | 0.09       |      |         |            |
| 3    | 2:00:00  | 0.09       |      |         |            |
| 3    | 2:15:00  | 0.09       |      |         |            |
| 3    | 2:30:00  | 0.09       |      |         |            |
| 3    | 2:45:00  | 0.08       |      |         |            |
| 3    | 3:00:00  | 0.08       |      |         |            |
| 3    | 3:15:00  | 0.08       |      |         |            |
| 3    | 3:30:00  | 0.07       |      |         |            |
| 3    | 3:45:00  | 0.07       |      |         |            |
| 3    | 4:00:00  | 0.07       |      |         |            |
| 3    | 4:15:00  | 0.06       |      |         |            |
| 3    | 4:30:00  | 0.06       |      |         |            |
| 3    | 4:45:00  | 0.05       |      |         |            |
| 3    | 5:00:00  | 0.05       |      |         |            |
| 3    | 5:15:00  | 0.05       |      |         |            |
| 3    | 5:30:00  | 0.05       |      |         |            |
| 3    | 5:45:00  | 0.05       |      |         |            |
| 3    | 6:00:00  | 0.05       |      |         |            |

SWMM Model Results



SWMM Model Results

Pond 2 - Stage, Volume  
(100 - yr)

Table - Node P2

| Days | Hours    | Depth (ft) | Volume (ft3) |             | Days | Hours    | Depth (ft) | Volume (ft3) |
|------|----------|------------|--------------|-------------|------|----------|------------|--------------|
| 0    | 0:15:00  | 0.88       | 207.27       |             | 0    | 11:15:00 | 4.94       | 69920.08     |
| 0    | 0:30:00  | 2.39       | 5625.17      |             | 0    | 11:30:00 | 4.92       | 69374.63     |
| 0    | 0:45:00  | 4.66       | 58101.26     |             | 0    | 11:45:00 | 4.91       | 68831.36     |
| 0    | 1:00:00  | 6.17       | 133927.7     |             | 0    | 12:00:00 | 4.9        | 68290.27     |
| 0    | 1:15:00  | 6.37       | 145008.9     | Max Volume  | 0    | 12:15:00 | 4.89       | 67750.81     |
| 0    | 1:30:00  | 6.31       | 141243.6     |             | 0    | 12:30:00 | 4.88       | 67212.45     |
| 0    | 1:45:00  | 6.14       | 131806.9     |             | 0    | 12:45:00 | 4.86       | 66675.2      |
| 0    | 2:00:00  | 6.06       | 127440.5     |             | 0    | 13:00:00 | 4.85       | 66139.03     |
| 0    | 2:15:00  | 6.01       | 124806.4     |             | 0    | 13:15:00 | 4.84       | 65603.97     |
| 0    | 2:30:00  | 5.98       | 123081.3     |             | 0    | 13:30:00 | 4.83       | 65070.01     |
| 0    | 2:45:00  | 5.95       | 121427.4     |             | 0    | 13:45:00 | 4.81       | 64537.15     |
| 0    | 3:00:00  | 5.91       | 119624.4     |             | 0    | 14:00:00 | 4.8        | 64005.41     |
| 0    | 3:15:00  | 5.87       | 117412.5     |             | 0    | 14:15:00 | 4.79       | 63475.16     |
| 0    | 3:30:00  | 5.82       | 114293.7     |             | 0    | 14:30:00 | 4.78       | 62947.12     |
| 0    | 3:45:00  | 5.69       | 107816.9     |             | 0    | 14:45:00 | 4.76       | 62421.3      |
| 0    | 4:00:00  | 5.45       | 95070.08     |             | 0    | 15:00:00 | 4.75       | 61897.72     |
| 0    | 4:15:00  | 5.34       | 89440.33     |             | 0    | 15:15:00 | 4.74       | 61376.36     |
| 0    | 4:30:00  | 5.3        | 87214.48     |             | 0    | 15:30:00 | 4.73       | 60857.22     |
| 0    | 4:45:00  | 5.27       | 85910.59     |             | 0    | 15:45:00 | 4.72       | 60340.32     |
| 0    | 5:00:00  | 5.25       | 84804.8      | EURV + WQCV | 0    | 16:00:00 | 4.7        | 59825.64     |
| 0    | 5:15:00  | 5.23       | 83871.57     |             | 0    | 16:15:00 | 4.69       | 59313.2      |
| 0    | 5:30:00  | 5.21       | 83088.35     |             | 0    | 16:30:00 | 4.68       | 58802.98     |
| 0    | 5:45:00  | 5.2        | 82432.74     |             | 0    | 16:45:00 | 4.67       | 58295        |
| 0    | 6:00:00  | 5.19       | 81847.23     |             | 0    | 17:00:00 | 4.65       | 57789.25     |
| 0    | 6:15:00  | 5.18       | 81263.7      |             | 0    | 17:15:00 | 4.64       | 57285.73     |
| 0    | 6:30:00  | 5.17       | 80681.24     |             | 0    | 17:30:00 | 4.63       | 56784.44     |
| 0    | 6:45:00  | 5.15       | 80099.86     |             | 0    | 17:45:00 | 4.62       | 56285.39     |
| 0    | 7:00:00  | 5.14       | 79519.55     |             | 0    | 18:00:00 | 4.6        | 55788.57     |
| 0    | 7:15:00  | 5.13       | 78940.32     |             | 0    | 18:15:00 | 4.59       | 55294        |
| 0    | 7:30:00  | 5.12       | 78362.18     |             | 0    | 18:30:00 | 4.58       | 54801.65     |
| 0    | 7:45:00  | 5.11       | 77785.12     |             | 0    | 18:45:00 | 4.57       | 54311.55     |
| 0    | 8:00:00  | 5.09       | 77209.29     |             | 0    | 19:00:00 | 4.55       | 53823.68     |
| 0    | 8:15:00  | 5.08       | 76635.52     |             | 0    | 19:15:00 | 4.54       | 53338.06     |
| 0    | 8:30:00  | 5.07       | 76063.92     |             | 0    | 19:30:00 | 4.53       | 52854.67     |
| 0    | 8:45:00  | 5.06       | 75494.5      |             | 0    | 19:45:00 | 4.52       | 52373.52     |
| 0    | 9:00:00  | 5.05       | 74927.25     |             | 0    | 20:00:00 | 4.5        | 51894.62     |
| 0    | 9:15:00  | 5.03       | 74362.19     |             | 0    | 20:15:00 | 4.49       | 51417.96     |
| 0    | 9:30:00  | 5.02       | 73799.3      |             | 0    | 20:30:00 | 4.48       | 50943.54     |
| 0    | 9:45:00  | 5.01       | 73238.59     |             | 0    | 20:45:00 | 4.47       | 50471.37     |
| 0    | 10:00:00 | 5          | 72680.05     |             | 0    | 21:00:00 | 4.45       | 50001.45     |
| 0    | 10:15:00 | 4.98       | 72123.7      |             | 0    | 21:15:00 | 4.44       | 49533.76     |
| 0    | 10:30:00 | 4.97       | 71569.52     |             | 0    | 21:30:00 | 4.43       | 49068.33     |
| 0    | 10:45:00 | 4.96       | 71017.53     |             | 0    | 21:45:00 | 4.42       | 48605.14     |
| 0    | 11:00:00 | 4.95       | 70467.71     |             | 0    | 22:00:00 | 4.4        | 48144.21     |

| Days | Hours    | Depth (ft) | Volume (ft3) |
|------|----------|------------|--------------|
| 0    | 22:15:00 | 4.39       | 47685.52     |
| 0    | 22:30:00 | 4.38       | 47229.09     |
| 0    | 22:45:00 | 4.37       | 46774.9      |
| 0    | 23:00:00 | 4.35       | 46322.97     |
| 0    | 23:15:00 | 4.34       | 45873.3      |
| 0    | 23:30:00 | 4.33       | 45425.88     |
| 0    | 23:45:00 | 4.32       | 44980.71     |
| 1    | 0:00:00  | 4.3        | 44537.8      |
| 1    | 0:15:00  | 4.29       | 44097.4      |
| 1    | 0:30:00  | 4.28       | 43660.31     |
| 1    | 0:45:00  | 4.27       | 43226.61     |
| 1    | 1:00:00  | 4.25       | 42796.29     |
| 1    | 1:15:00  | 4.24       | 42369.33     |
| 1    | 1:30:00  | 4.23       | 41945.74     |
| 1    | 1:45:00  | 4.22       | 41525.51     |
| 1    | 2:00:00  | 4.2        | 41108.63     |
| 1    | 2:15:00  | 4.19       | 40695.1      |
| 1    | 2:30:00  | 4.18       | 40284.91     |
| 1    | 2:45:00  | 4.17       | 39878.06     |
| 1    | 3:00:00  | 4.15       | 39474.53     |
| 1    | 3:15:00  | 4.14       | 39074.33     |
| 1    | 3:30:00  | 4.13       | 38677.44     |
| 1    | 3:45:00  | 4.12       | 38283.86     |
| 1    | 4:00:00  | 4.11       | 37893.59     |
| 1    | 4:15:00  | 4.09       | 37506.46     |
| 1    | 4:30:00  | 4.08       | 37121.68     |
| 1    | 4:45:00  | 4.07       | 36739.08     |
| 1    | 5:00:00  | 4.06       | 36358.69     |
| 1    | 5:15:00  | 4.04       | 35980.5      |
| 1    | 5:30:00  | 4.03       | 35604.51     |
| 1    | 5:45:00  | 4.02       | 35230.73     |
| 1    | 6:00:00  | 4.01       | 34859.16     |
| 1    | 6:15:00  | 4          | 34489.88     |
| 1    | 6:30:00  | 3.98       | 34124.01     |
| 1    | 6:45:00  | 3.97       | 33761.89     |
| 1    | 7:00:00  | 3.96       | 33403.49     |
| 1    | 7:15:00  | 3.95       | 33048.82     |
| 1    | 7:30:00  | 3.93       | 32697.84     |
| 1    | 7:45:00  | 3.92       | 32350.56     |
| 1    | 8:00:00  | 3.91       | 32006.96     |
| 1    | 8:15:00  | 3.9        | 31667.02     |
| 1    | 8:30:00  | 3.89       | 31330.73     |
| 1    | 8:45:00  | 3.88       | 30998.09     |
| 1    | 9:00:00  | 3.86       | 30669.06     |
| 1    | 9:15:00  | 3.85       | 30343.65     |

| Days | Hours    | Depth (ft) | Volume (ft3) |
|------|----------|------------|--------------|
| 1    | 9:30:00  | 3.84       | 30021.83     |
| 1    | 9:45:00  | 3.83       | 29703.6      |
| 1    | 10:00:00 | 3.82       | 29388.93     |
| 1    | 10:15:00 | 3.8        | 29077.82     |
| 1    | 10:30:00 | 3.79       | 28770.25     |
| 1    | 10:45:00 | 3.78       | 28466.2      |
| 1    | 11:00:00 | 3.77       | 28165.66     |
| 1    | 11:15:00 | 3.76       | 27868.62     |
| 1    | 11:30:00 | 3.75       | 27575.05     |
| 1    | 11:45:00 | 3.74       | 27284.95     |
| 1    | 12:00:00 | 3.73       | 26998.3      |
| 1    | 12:15:00 | 3.71       | 26715.08     |
| 1    | 12:30:00 | 3.7        | 26435.28     |
| 1    | 12:45:00 | 3.69       | 26158.88     |
| 1    | 13:00:00 | 3.68       | 25885.86     |
| 1    | 13:15:00 | 3.67       | 25616.22     |
| 1    | 13:30:00 | 3.66       | 25349.92     |
| 1    | 13:45:00 | 3.65       | 25086.96     |
| 1    | 14:00:00 | 3.64       | 24827.32     |
| 1    | 14:15:00 | 3.63       | 24570.99     |
| 1    | 14:30:00 | 3.62       | 24317.93     |
| 1    | 14:45:00 | 3.6        | 24068.15     |
| 1    | 15:00:00 | 3.59       | 23821.61     |
| 1    | 15:15:00 | 3.58       | 23578.31     |
| 1    | 15:30:00 | 3.57       | 23338.21     |
| 1    | 15:45:00 | 3.56       | 23101.32     |
| 1    | 16:00:00 | 3.55       | 22867.61     |
| 1    | 16:15:00 | 3.54       | 22637.05     |
| 1    | 16:30:00 | 3.53       | 22409.63     |
| 1    | 16:45:00 | 3.52       | 22185.34     |
| 1    | 17:00:00 | 3.51       | 21964.15     |
| 1    | 17:15:00 | 3.5        | 21746.04     |
| 1    | 17:30:00 | 3.49       | 21530.23     |
| 1    | 17:45:00 | 3.48       | 21315.18     |
| 1    | 18:00:00 | 3.47       | 21100.85     |
| 1    | 18:15:00 | 3.46       | 20887.25     |
| 1    | 18:30:00 | 3.45       | 20674.39     |
| 1    | 18:45:00 | 3.44       | 20462.26     |
| 1    | 19:00:00 | 3.43       | 20250.88     |
| 1    | 19:15:00 | 3.42       | 20040.23     |
| 1    | 19:30:00 | 3.41       | 19830.34     |
| 1    | 19:45:00 | 3.4        | 19621.19     |
| 1    | 20:00:00 | 3.39       | 19412.8      |
| 1    | 20:15:00 | 3.38       | 19205.17     |
| 1    | 20:30:00 | 3.37       | 18998.3      |

WQCV

| Days | Hours    | Depth (ft) | Volume (ft3) |
|------|----------|------------|--------------|
| 1    | 20:45:00 | 3.36       | 18792.21     |
| 1    | 21:00:00 | 3.35       | 18586.88     |
| 1    | 21:15:00 | 3.34       | 18382.33     |
| 1    | 21:30:00 | 3.32       | 18178.55     |
| 1    | 21:45:00 | 3.31       | 17975.57     |
| 1    | 22:00:00 | 3.3        | 17773.37     |
| 1    | 22:15:00 | 3.29       | 17571.96     |
| 1    | 22:30:00 | 3.28       | 17371.34     |
| 1    | 22:45:00 | 3.27       | 17171.51     |
| 1    | 23:00:00 | 3.26       | 16972.48     |
| 1    | 23:15:00 | 3.25       | 16774.24     |
| 1    | 23:30:00 | 3.24       | 16576.81     |
| 1    | 23:45:00 | 3.23       | 16380.17     |
| 2    | 0:00:00  | 3.21       | 16184.34     |
| 2    | 0:15:00  | 3.2        | 15989.32     |
| 2    | 0:30:00  | 3.19       | 15795.11     |
| 2    | 0:45:00  | 3.18       | 15601.71     |
| 2    | 1:00:00  | 3.17       | 15409.13     |
| 2    | 1:15:00  | 3.16       | 15217.36     |
| 2    | 1:30:00  | 3.15       | 15026.41     |
| 2    | 1:45:00  | 3.13       | 14836.29     |
| 2    | 2:00:00  | 3.12       | 14646.99     |
| 2    | 2:15:00  | 3.11       | 14458.52     |
| 2    | 2:30:00  | 3.1        | 14270.88     |
| 2    | 2:45:00  | 3.09       | 14084.07     |
| 2    | 3:00:00  | 3.08       | 13898.1      |
| 2    | 3:15:00  | 3.07       | 13712.98     |
| 2    | 3:30:00  | 3.05       | 13528.69     |
| 2    | 3:45:00  | 3.04       | 13345.25     |
| 2    | 4:00:00  | 3.03       | 13162.67     |
| 2    | 4:15:00  | 3.02       | 12980.93     |
| 2    | 4:30:00  | 3.01       | 12800.05     |
| 2    | 4:45:00  | 2.99       | 12620.03     |
| 2    | 5:00:00  | 2.98       | 12440.88     |
| 2    | 5:15:00  | 2.97       | 12262.59     |
| 2    | 5:30:00  | 2.96       | 12085.18     |
| 2    | 5:45:00  | 2.95       | 11908.63     |
| 2    | 6:00:00  | 2.93       | 11732.97     |
| 2    | 6:15:00  | 2.92       | 11558.19     |
| 2    | 6:30:00  | 2.91       | 11384.3      |
| 2    | 6:45:00  | 2.9        | 11211.29     |
| 2    | 7:00:00  | 2.88       | 11039.19     |
| 2    | 7:15:00  | 2.87       | 10867.98     |
| 2    | 7:30:00  | 2.86       | 10697.68     |
| 2    | 7:45:00  | 2.85       | 10528.28     |

| Days | Hours    | Depth (ft) | Volume (ft3) |
|------|----------|------------|--------------|
| 2    | 8:00:00  | 2.83       | 10359.8      |
| 2    | 8:15:00  | 2.82       | 10192.23     |
| 2    | 8:30:00  | 2.81       | 10025.59     |
| 2    | 8:45:00  | 2.79       | 9859.88      |
| 2    | 9:00:00  | 2.78       | 9695.1       |
| 2    | 9:15:00  | 2.77       | 9531.26      |
| 2    | 9:30:00  | 2.76       | 9368.37      |
| 2    | 9:45:00  | 2.74       | 9206.43      |
| 2    | 10:00:00 | 2.73       | 9045.44      |
| 2    | 10:15:00 | 2.72       | 8885.41      |
| 2    | 10:30:00 | 2.7        | 8726.36      |
| 2    | 10:45:00 | 2.69       | 8568.28      |
| 2    | 11:00:00 | 2.67       | 8411.18      |
| 2    | 11:15:00 | 2.66       | 8255.07      |
| 2    | 11:30:00 | 2.65       | 8099.95      |
| 2    | 11:45:00 | 2.63       | 7945.84      |
| 2    | 12:00:00 | 2.62       | 7792.75      |
| 2    | 12:15:00 | 2.6        | 7640.67      |
| 2    | 12:30:00 | 2.59       | 7489.62      |
| 2    | 12:45:00 | 2.58       | 7339.6       |
| 2    | 13:00:00 | 2.56       | 7190.64      |
| 2    | 13:15:00 | 2.55       | 7042.72      |
| 2    | 13:30:00 | 2.53       | 6895.87      |
| 2    | 13:45:00 | 2.52       | 6750.1       |
| 2    | 14:00:00 | 2.5        | 6605.41      |
| 2    | 14:15:00 | 2.49       | 6461.82      |
| 2    | 14:30:00 | 2.47       | 6319.34      |
| 2    | 14:45:00 | 2.46       | 6177.98      |
| 2    | 15:00:00 | 2.44       | 6037.75      |
| 2    | 15:15:00 | 2.42       | 5898.67      |
| 2    | 15:30:00 | 2.41       | 5760.75      |
| 2    | 15:45:00 | 2.39       | 5624.01      |
| 2    | 16:00:00 | 2.37       | 5488.46      |
| 2    | 16:15:00 | 2.36       | 5354.12      |
| 2    | 16:30:00 | 2.34       | 5221         |
| 2    | 16:45:00 | 2.32       | 5089.14      |
| 2    | 17:00:00 | 2.3        | 4958.53      |
| 2    | 17:15:00 | 2.29       | 4829.19      |
| 2    | 17:30:00 | 2.27       | 4701.13      |
| 2    | 17:45:00 | 2.25       | 4574.34      |
| 2    | 18:00:00 | 2.23       | 4448.85      |
| 2    | 18:15:00 | 2.22       | 4324.64      |
| 2    | 18:30:00 | 2.2        | 4201.74      |
| 2    | 18:45:00 | 2.18       | 4080.15      |
| 2    | 19:00:00 | 2.16       | 3959.87      |

| Days | Hours    | Depth (ft) | Volume (ft3) |
|------|----------|------------|--------------|
| 2    | 19:15:00 | 2.14       | 3840.92      |
| 2    | 19:30:00 | 2.12       | 3723.3       |
| 2    | 19:45:00 | 2.11       | 3607.03      |
| 2    | 20:00:00 | 2.09       | 3492.11      |
| 2    | 20:15:00 | 2.07       | 3378.55      |
| 2    | 20:30:00 | 2.05       | 3266.36      |
| 2    | 20:45:00 | 2.03       | 3155.56      |
| 2    | 21:00:00 | 2.01       | 3046.15      |
| 2    | 21:15:00 | 1.99       | 2938.1       |
| 2    | 21:30:00 | 1.97       | 2831.17      |
| 2    | 21:45:00 | 1.95       | 2725.31      |
| 2    | 22:00:00 | 1.93       | 2620.55      |
| 2    | 22:15:00 | 1.91       | 2516.9       |
| 2    | 22:30:00 | 1.89       | 2414.37      |
| 2    | 22:45:00 | 1.87       | 2312.99      |
| 2    | 23:00:00 | 1.84       | 2212.76      |
| 2    | 23:15:00 | 1.82       | 2113.73      |
| 2    | 23:30:00 | 1.8        | 2015.89      |
| 2    | 23:45:00 | 1.78       | 1919.29      |
| 3    | 0:00:00  | 1.75       | 1823.93      |
| 3    | 0:15:00  | 1.73       | 1729.86      |
| 3    | 0:30:00  | 1.7        | 1637.11      |
| 3    | 0:45:00  | 1.68       | 1545.7       |
| 3    | 1:00:00  | 1.65       | 1455.68      |
| 3    | 1:15:00  | 1.63       | 1367.09      |
| 3    | 1:30:00  | 1.6        | 1279.97      |
| 3    | 1:45:00  | 1.57       | 1194.4       |
| 3    | 2:00:00  | 1.54       | 1110.43      |
| 3    | 2:15:00  | 1.51       | 1028.15      |
| 3    | 2:30:00  | 1.47       | 947.82       |
| 3    | 2:45:00  | 1.44       | 870          |
| 3    | 3:00:00  | 1.4        | 794.89       |
| 3    | 3:15:00  | 1.35       | 722.74       |
| 3    | 3:30:00  | 1.31       | 653.92       |
| 3    | 3:45:00  | 1.26       | 588.68       |
| 3    | 4:00:00  | 1.21       | 527.03       |
| 3    | 4:15:00  | 1.16       | 468.95       |
| 3    | 4:30:00  | 1.11       | 414.43       |
| 3    | 4:45:00  | 1.06       | 363.47       |
| 3    | 5:00:00  | 1.01       | 316.05       |
| 3    | 5:15:00  | 0.96       | 271.28       |
| 3    | 5:30:00  | 0.91       | 227.48       |
| 3    | 5:45:00  | 0.85       | 184.66       |
| 3    | 6:00:00  | 0.79       | 142.9        |
| 3    | 6:15:00  | 0.72       | 102.33       |

| Days | Hours   | Depth (ft) | Volume (ft3) |
|------|---------|------------|--------------|
| 3    | 6:30:00 | 0.64       | 63.11        |
| 3    | 6:45:00 | 0.53       | 25.56        |
| 3    | 7:00:00 | 0          | 0            |
| 3    | 7:15:00 | 0          | 0            |

# Weir Report

## Pond P2 Spillway

### Trapezoidal Weir

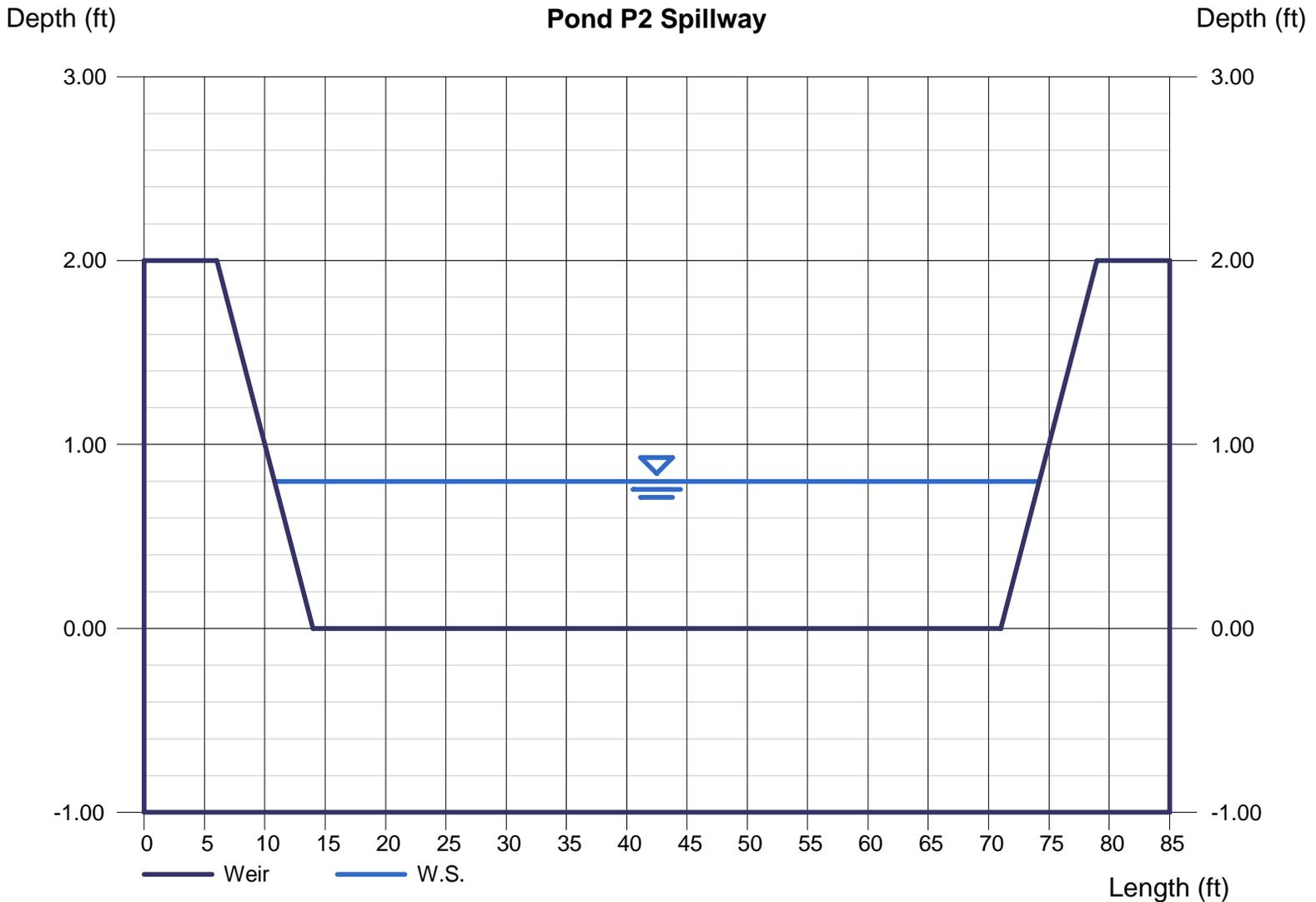
Crest = Sharp  
Bottom Length (ft) = 57.00  
Total Depth (ft) = 2.00  
Side Slope (z:1) = 4.00

### Highlighted

Depth (ft) = 0.80  
Q (cfs) = 130.30  
Area (sqft) = 48.16  
Velocity (ft/s) = 2.71  
Top Width (ft) = 63.40

### Calculations

Weir Coeff. Cw = 3.10  
Compute by: Known Q  
Known Q (cfs) = 130.30



# Channel Report

## Pond P2 Overflow Channel

### Trapezoidal

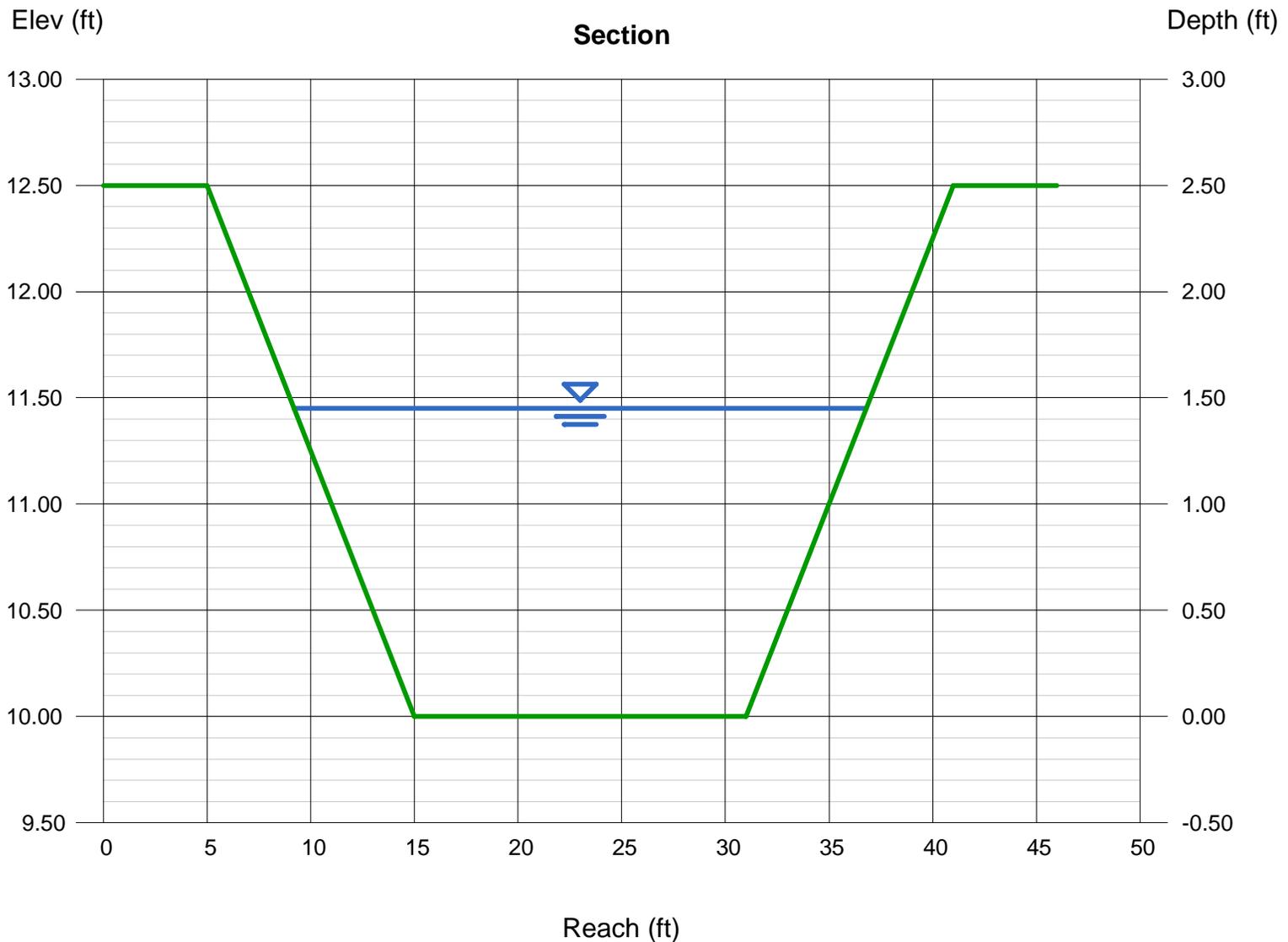
Bottom Width (ft) = 16.00  
Side Slopes (z:1) = 4.00, 4.00  
Total Depth (ft) = 2.50  
Invert Elev (ft) = 10.00  
Slope (%) = 0.60  
N-Value = 0.030

### Highlighted

Depth (ft) = 1.45  
Q (cfs) = 130.30  
Area (sqft) = 31.61  
Velocity (ft/s) = 4.12  
Wetted Perim (ft) = 27.96  
Crit Depth, Yc (ft) = 1.16  
Top Width (ft) = 27.60  
EGL (ft) = 1.71

### Calculations

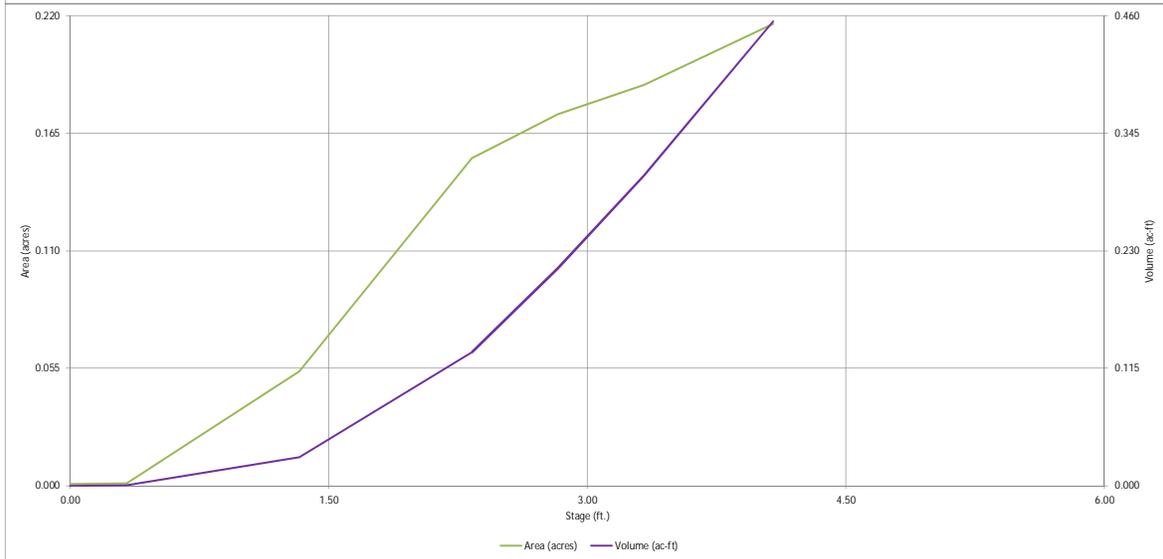
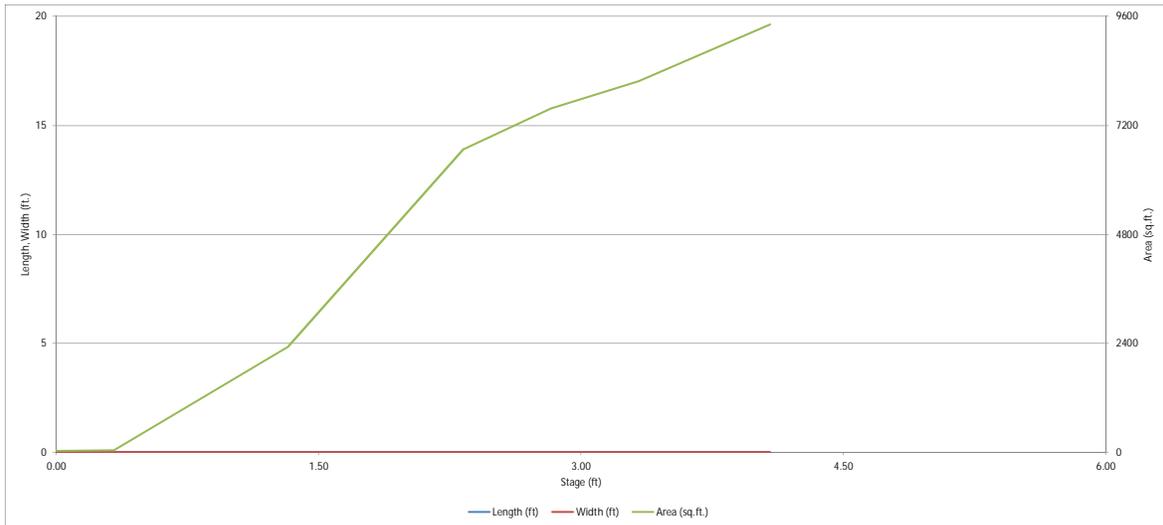
Compute by: Known Q  
Known Q (cfs) = 130.30





# DETENTION BASIN STAGE-STORAGE TABLE BUILDER

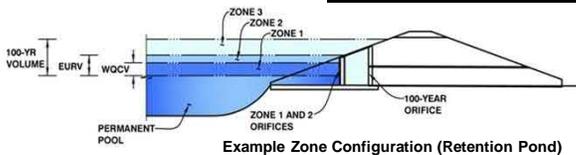
*MHFD-Detention, Version 4.03 (May 2020)*



# DETENTION BASIN OUTLET STRUCTURE DESIGN

*MHFD-Detention, Version 4.03 (May 2020)*

Project: Cloverleaf Subdivision  
Basin I.D.: P3 (Private FSD EDB for Basin L)



|                          | Estimated Stage (ft) | Estimated Volume (ac-ft) | Outlet Type          |
|--------------------------|----------------------|--------------------------|----------------------|
| Zone 1 (WOCV)            | 1.39                 | 0.031                    | Orifice Plate        |
| Zone 2 (EURV)            | 2.02                 | 0.057                    | Circular Orifice     |
| Zone 3 (100-year)        | 2.54                 | 0.076                    | Weir&Pipe (Restrict) |
| <b>Total (all zones)</b> |                      | <b>0.164</b>             |                      |

User Input: Orifice at Underdrain Outlet (typically used to drain WOCV in a Filtration BMP)

|                                   |     |  |
|-----------------------------------|-----|--|
| Underdrain Orifice Invert Depth = | N/A | ft (distance below the filtration media surface) |
| Underdrain Orifice Diameter =     | N/A | inches   |

Calculated Parameters for Underdrain

|                               |     |                 |
|-------------------------------|-----|-----------------|
| Underdrain Orifice Area =     | N/A | ft <sup>2</sup> |
| Underdrain Orifice Centroid = | N/A | feet            |

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WOCV and/or EURV in a sedimentation BMP)

Calculated Parameters for Plate

|  |      |   |                            |     |                 |
|--|------|---|----------------------------|-----|-----------------|
| Invert of Lowest Orifice =                 | 0.00 | ft (relative to basin bottom at Stage = 0 ft) | WQ Orifice Area per Row =  | N/A | ft <sup>2</sup> |
| Depth at top of Zone using Orifice Plate = | 1.69 | ft (relative to basin bottom at Stage = 0 ft) | Elliptical Half-Width =    | N/A | feet            |
| Orifice Plate: Orifice Vertical Spacing =  | N/A  | inches  | Elliptical Slot Centroid = | N/A | feet            |
| Orifice Plate: Orifice Area per Row =      | N/A  | inches  | Elliptical Slot Area =     | N/A | ft <sup>2</sup> |

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

|                                | Row 1 (required) | Row 2 (optional) | Row 3 (optional) | Row 4 (optional) | Row 5 (optional) | Row 6 (optional) | Row 7 (optional) | Row 8 (optional) |
|--------------------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|
| Stage of Orifice Centroid (ft) | 0.00             | 0.66             | 1.13             |                  |                  |                  |                  |                  |
| Orifice Area (sq. inches)      | 0.20             | 0.12             | 0.12             |                  |                  |                  |                  |                  |

|                                | Row 9 (optional) | Row 10 (optional) | Row 11 (optional) | Row 12 (optional) | Row 13 (optional) | Row 14 (optional) | Row 15 (optional) | Row 16 (optional) |
|--------------------------------|------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| Stage of Orifice Centroid (ft) |                  |                   |                   |                   |                   |                   |                   |                   |
| Orifice Area (sq. inches)      |                  |                   |                   |                   |                   |                   |                   |                   |

User Input: Vertical Orifice (Circular or Rectangular)

Calculated Parameters for Vertical Orifice

|   | Zone 2 Circular | Not Selected |   | Zone 2 Circular             | Not Selected |                 |
|---|-----------------|--------------|---|-----------------------------|--------------|-----------------|
| Invert of Vertical Orifice =                  | 1.55            | N/A          | ft (relative to basin bottom at Stage = 0 ft) | Vertical Orifice Area =     | 0.01         | ft <sup>2</sup> |
| Depth at top of Zone using Vertical Orifice = | 2.02            | N/A          | ft (relative to basin bottom at Stage = 0 ft) | Vertical Orifice Centroid = | 0.05         | feet            |
| Vertical Orifice Diameter =                   | 1.25            | N/A          | inches  |                             |              |                 |

User Input: Overflow Weir (Dropbox with Flat or Sloped Gate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe))

Calculated Parameters for Overflow Weir

|                                       | Zone 3 Weir | Not Selected |   | Zone 3 Weir                                 | Not Selected |                 |
|---------------------------------------|-------------|--------------|---|---|--------------|-----------------|
| Overflow Weir Front Edge Height, Ho = | 2.37        | N/A          | ft (relative to basin bottom at Stage = 0 ft) | Height of Gate Upper Edge, H <sub>1</sub> = | 2.37         | feet            |
| Overflow Weir Front Edge Length =     | 3.00        | N/A          | feet  | Overflow Weir Slope Length =                | 3.00         | feet            |
| Overflow Weir Gate Slope =            | 0.00        | N/A          | H:V   | Grate Open Area / 100-yr Orifice Area =     | 17.68        | N/A             |
| Horiz. Length of Weir Sides =         | 3.00        | N/A          | feet  | Overflow Grate Open Area w/o Debris =       | 6.30         | ft <sup>2</sup> |
| Overflow Grate Open Area % =          | 70%         | N/A          | % , grate open area/total area                | Overflow Grate Open Area w/ Debris =        | 6.30         | ft <sup>2</sup> |
| Debris Clogging % =                   | 0%          | N/A          | %   |   |              |                 |

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate

|   | Zone 3 Restrictor | Not Selected |  | Zone 3 Restrictor                                | Not Selected |                 |
|---|-------------------|--------------|--|--|--------------|-----------------|
| Depth to Invert of Outlet Pipe =            | 0.50              | N/A          | ft (distance below basin bottom at Stage = 0 ft) | Outlet Orifice Area =                            | 0.36         | ft <sup>2</sup> |
| Outlet Pipe Diameter =                      | 18.00             | N/A          | inches   | Outlet Orifice Centroid =                        | 0.23         | feet            |
| Restrictor Plate Height Above Pipe Invert = | 4.60              |              | inches   | Half-Central Angle of Restrictor Plate on Pipe = | 1.06         | radians         |

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Calculated Parameters for Spillway

|                                     |       |   |                                    |      |         |
|-------------------------------------|-------|---|------------------------------------|------|---------|
| Spillway Invert Stage =             | 2.83  | ft (relative to basin bottom at Stage = 0 ft) | Spillway Design Flow Depth =       | 0.25 | feet    |
| Spillway Crest Length =             | 14.00 | feet  | Stage at Top of Freeboard =        | 4.08 | feet    |
| Spillway End Slopes =               | 4.00  | H:V   | Basin Area at Top of Freeboard =   | 0.22 | acres   |
| Freeboard above Max Water Surface = | 1.00  | feet  | Basin Volume at Top of Freeboard = | 0.45 | acre-ft |

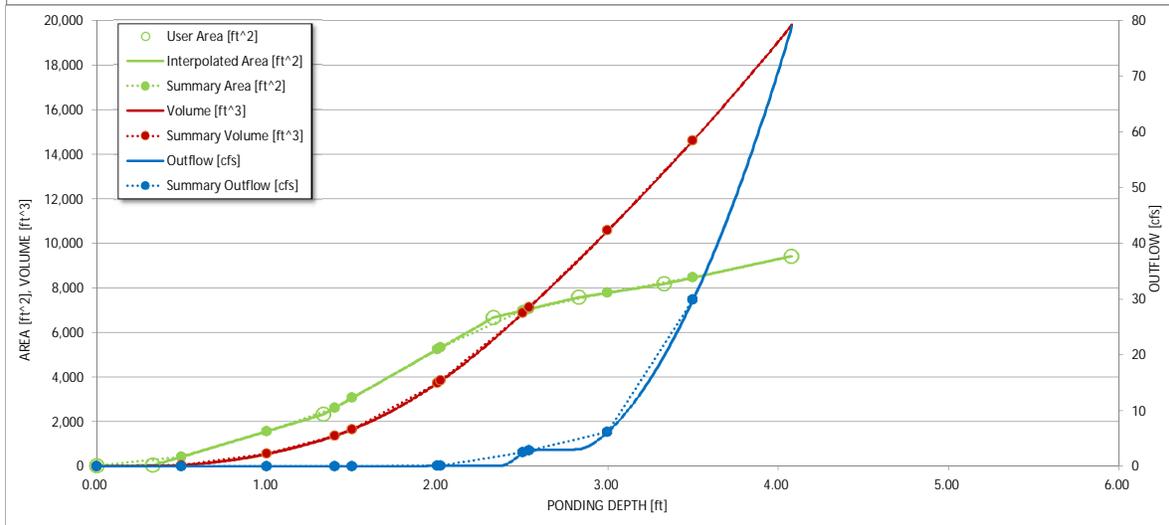
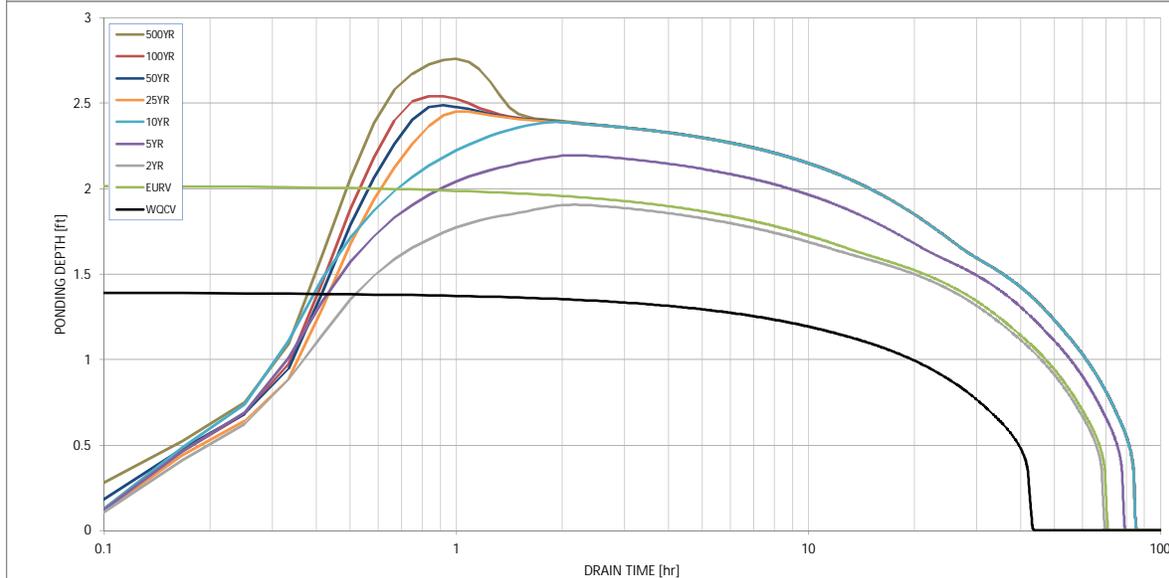
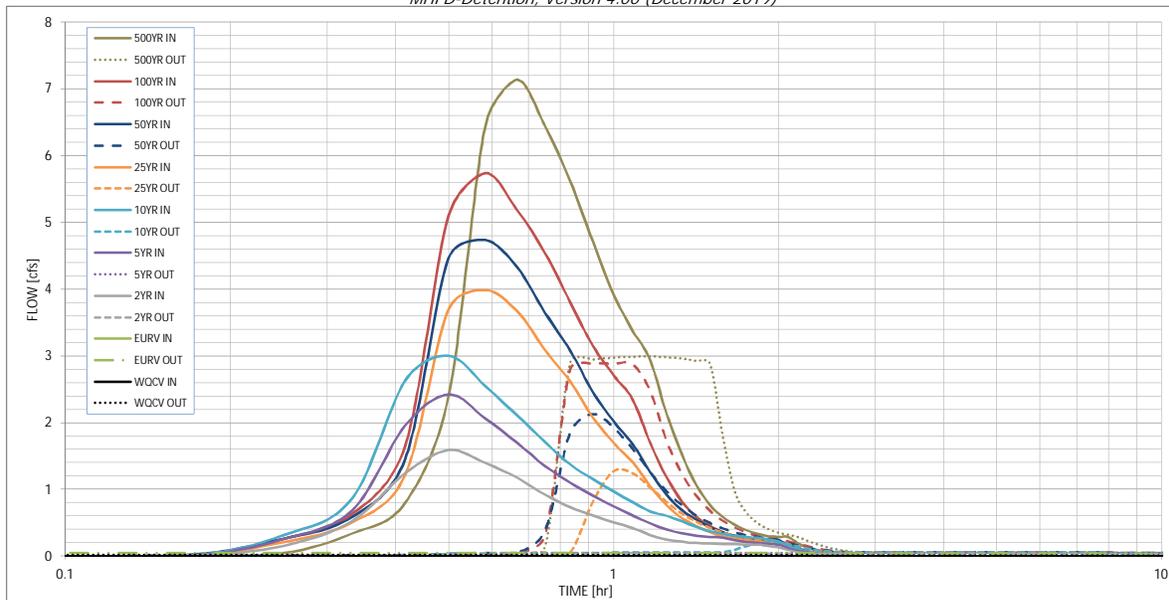
## Routed Hydrograph Results

*The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).*

|   | WOCV  | EURV               | 2 Year             | 5 Year             | 10 Year         | 25 Year         | 50 Year         | 100 Year       | 500 Year       |
|---|-------|--------------------|--------------------|--------------------|-----------------|-----------------|-----------------|----------------|----------------|
| Design Storm Return Period =                  | N/A   | N/A                | 1.19               | 1.50               | 1.75            | 2.00            | 2.25            | 2.52           | 3.00           |
| One-Hour Rainfall Depth (in)                  | N/A   | N/A                | 1.19               | 1.50               | 1.75            | 2.00            | 2.25            | 2.52           | 3.00           |
| CUHP Runoff Volume (acre-ft)                  | 0.031 | 0.088              | 0.080              | 0.118              | 0.153           | 0.201           | 0.239           | 0.288          | 0.364          |
| Inflow Hydrograph Volume (acre-ft)            | N/A   | N/A                | 0.080              | 0.118              | 0.153           | 0.201           | 0.239           | 0.288          | 0.364          |
| CUHP Predevelopment Peak Q (cfs)              | N/A   | N/A                | 0.3                | 0.8                | 1.2             | 2.1             | 2.7             | 3.3            | 4.3            |
| OPTIONAL Override Predevelopment Peak Q (cfs) | N/A   | N/A                |                    |                    |                 |                 |                 |                |                |
| Predevelopment Unit Peak Flow, q (cfs/acre)   | N/A   | N/A                | 0.15               | 0.42               | 0.63            | 1.08            | 1.35            | 1.69           | 2.20           |
| Peak Inflow Q (cfs)                           | N/A   | N/A                | 1.6                | 2.4                | 3.0             | 4.0             | 4.7             | 5.7            | 7.1            |
| Peak Outflow Q (cfs)                          | 0.0   | 0.0                | 0.0                | 0.1                | 0.2             | 1.3             | 2.1             | 2.9            | 3.0            |
| Ratio Peak Outflow to Predevelopment Q        | N/A   | N/A                | N/A                | 0.1                | 0.2             | 0.6             | 0.8             | 0.9            | 0.7            |
| Structure Controlling Flow                    | Plate | Vertical Orifice 1 | Vertical Orifice 1 | Vertical Orifice 1 | Overflow Weir 1 | Overflow Weir 1 | Overflow Weir 1 | Outlet Plate 1 | Outlet Plate 1 |
| Max Velocity through Gate 1 (fps)             | N/A   | N/A                | N/A                | N/A                | 0.0             | 0.2             | 0.3             | 0.4            | 0.5            |
| Max Velocity through Gate 2 (fps)             | N/A   | N/A                | N/A                | N/A                | N/A             | N/A             | N/A             | N/A            | N/A            |
| Time to Drain 97% of Inflow Volume (hours)    | 40    | 64                 | 63                 | 70                 | 74              | 71              | 70              | 67             | 64             |
| Time to Drain 99% of Inflow Volume (hours)    | 42    | 68                 | 67                 | 75                 | 81              | 79              | 79              | 77             | 76             |
| Maximum Ponding Depth (ft)                    | 1.40  | 2.02               | 1.91               | 2.20               | 2.39            | 2.45            | 2.49            | 2.54           | 2.76           |
| Area at Maximum Ponding Depth (acres)         | 0.06  | 0.12               | 0.11               | 0.14               | 0.16            | 0.16            | 0.16            | 0.16           | 0.17           |
| Maximum Volume Stored (acre-ft)               | 0.031 | 0.088              | 0.074              | 0.110              | 0.140           | 0.150           | 0.154           | 0.164          | 0.201          |

# DETENTION BASIN OUTLET STRUCTURE DESIGN

*MHFD-Detention, Version 4.00 (December 2019)*



S-A-V-D Chart Axis Override

|               | X-axis | Left Y-Axis | Right Y-Axis |
|---------------|--------|-------------|--------------|
| minimum bound |        |             |              |
| maximum bound |        |             |              |

# DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename: \_\_\_\_\_

## Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

| Time Interval | SOURCE  | CUHP       | CUHP       | CUHP         | CUHP         | CUHP          | CUHP          | CUHP          | CUHP           | CUHP           |      |
|---------------|---------|------------|------------|--------------|--------------|---------------|---------------|---------------|----------------|----------------|------|
|               | TIME    | WOCV [cfs] | EURV [cfs] | 2 Year [cfs] | 5 Year [cfs] | 10 Year [cfs] | 25 Year [cfs] | 50 Year [cfs] | 100 Year [cfs] | 500 Year [cfs] |      |
| 5.00_min      | 0:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |      |
|               | 0:05:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |      |
|               | 0:10:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.02           | 0.00           | 0.04 |
|               | 0:15:00 | 0.00       | 0.00       | 0.15         | 0.25         | 0.31          | 0.21          | 0.26          | 0.26           | 0.26           | 0.34 |
|               | 0:20:00 | 0.00       | 0.00       | 0.52         | 0.68         | 0.86          | 0.50          | 0.58          | 0.63           | 0.63           | 0.80 |
|               | 0:25:00 | 0.00       | 0.00       | 1.24         | 1.95         | 2.63          | 1.22          | 1.45          | 1.65           | 1.65           | 2.40 |
|               | 0:30:00 | 0.00       | 0.00       | 1.59         | 2.42         | 3.00          | 3.69          | 4.46          | 5.10           | 5.10           | 6.44 |
|               | 0:35:00 | 0.00       | 0.00       | 1.39         | 2.06         | 2.55          | 3.99          | 4.73          | 5.73           | 5.73           | 7.14 |
|               | 0:40:00 | 0.00       | 0.00       | 1.17         | 1.70         | 2.11          | 3.67          | 4.33          | 5.19           | 5.19           | 6.44 |
|               | 0:45:00 | 0.00       | 0.00       | 0.92         | 1.35         | 1.71          | 3.09          | 3.64          | 4.54           | 4.54           | 5.62 |
|               | 0:50:00 | 0.00       | 0.00       | 0.73         | 1.10         | 1.37          | 2.62          | 3.08          | 3.80           | 3.80           | 4.71 |
|               | 0:55:00 | 0.00       | 0.00       | 0.61         | 0.90         | 1.15          | 2.07          | 2.46          | 3.15           | 3.15           | 3.92 |
|               | 1:00:00 | 0.00       | 0.00       | 0.51         | 0.75         | 0.97          | 1.70          | 2.02          | 2.71           | 2.71           | 3.38 |
|               | 1:05:00 | 0.00       | 0.00       | 0.42         | 0.61         | 0.81          | 1.40          | 1.68          | 2.35           | 2.35           | 2.93 |
|               | 1:10:00 | 0.00       | 0.00       | 0.32         | 0.49         | 0.67          | 1.05          | 1.25          | 1.69           | 1.69           | 2.13 |
|               | 1:15:00 | 0.00       | 0.00       | 0.25         | 0.40         | 0.60          | 0.76          | 0.92          | 1.18           | 1.18           | 1.51 |
|               | 1:20:00 | 0.00       | 0.00       | 0.21         | 0.34         | 0.52          | 0.57          | 0.69          | 0.81           | 0.81           | 1.05 |
|               | 1:25:00 | 0.00       | 0.00       | 0.20         | 0.31         | 0.43          | 0.45          | 0.55          | 0.59           | 0.59           | 0.76 |
|               | 1:30:00 | 0.00       | 0.00       | 0.19         | 0.29         | 0.37          | 0.36          | 0.43          | 0.45           | 0.45           | 0.58 |
|               | 1:35:00 | 0.00       | 0.00       | 0.18         | 0.27         | 0.33          | 0.30          | 0.35          | 0.36           | 0.36           | 0.46 |
|               | 1:40:00 | 0.00       | 0.00       | 0.18         | 0.24         | 0.31          | 0.26          | 0.31          | 0.29           | 0.29           | 0.39 |
|               | 1:45:00 | 0.00       | 0.00       | 0.17         | 0.21         | 0.29          | 0.24          | 0.27          | 0.25           | 0.25           | 0.33 |
|               | 1:50:00 | 0.00       | 0.00       | 0.17         | 0.19         | 0.27          | 0.22          | 0.25          | 0.23           | 0.23           | 0.30 |
|               | 1:55:00 | 0.00       | 0.00       | 0.15         | 0.18         | 0.25          | 0.21          | 0.24          | 0.22           | 0.22           | 0.29 |
|               | 2:00:00 | 0.00       | 0.00       | 0.13         | 0.17         | 0.22          | 0.21          | 0.24          | 0.22           | 0.22           | 0.28 |
|               | 2:05:00 | 0.00       | 0.00       | 0.09         | 0.12         | 0.15          | 0.14          | 0.16          | 0.15           | 0.15           | 0.20 |
|               | 2:10:00 | 0.00       | 0.00       | 0.06         | 0.08         | 0.10          | 0.10          | 0.11          | 0.10           | 0.10           | 0.13 |
|               | 2:15:00 | 0.00       | 0.00       | 0.04         | 0.05         | 0.07          | 0.07          | 0.07          | 0.07           | 0.07           | 0.09 |
|               | 2:20:00 | 0.00       | 0.00       | 0.03         | 0.03         | 0.05          | 0.04          | 0.05          | 0.05           | 0.05           | 0.06 |
|               | 2:25:00 | 0.00       | 0.00       | 0.02         | 0.02         | 0.03          | 0.03          | 0.03          | 0.03           | 0.03           | 0.04 |
|               | 2:30:00 | 0.00       | 0.00       | 0.01         | 0.01         | 0.02          | 0.02          | 0.02          | 0.02           | 0.02           | 0.02 |
|               | 2:35:00 | 0.00       | 0.00       | 0.00         | 0.01         | 0.01          | 0.01          | 0.01          | 0.01           | 0.01           | 0.01 |
|               | 2:40:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           | 0.00 |
|               | 2:45:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           | 0.00 |
|               | 2:50:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           | 0.00 |
|               | 2:55:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           | 0.00 |
|               | 3:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           | 0.00 |
|               | 3:05:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           | 0.00 |
|               | 3:10:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           | 0.00 |
|               | 3:15:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           | 0.00 |
|               | 3:20:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           | 0.00 |
|               | 3:25:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           | 0.00 |
|               | 3:30:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           | 0.00 |
|               | 3:35:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           | 0.00 |
|               | 3:40:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           | 0.00 |
|               | 3:45:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           | 0.00 |
|               | 3:50:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           | 0.00 |
|               | 3:55:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           | 0.00 |
|               | 4:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           | 0.00 |
|               | 4:05:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           | 0.00 |
|               | 4:10:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           | 0.00 |
|               | 4:15:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           | 0.00 |
|               | 4:20:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           | 0.00 |
|               | 4:25:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           | 0.00 |
|               | 4:30:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           | 0.00 |
|               | 4:35:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           | 0.00 |
|               | 4:40:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           | 0.00 |
|               | 4:45:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           | 0.00 |
|               | 4:50:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           | 0.00 |
|               | 4:55:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           | 0.00 |
| 5:00:00       | 0.00    | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |      |
| 5:05:00       | 0.00    | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |      |
| 5:10:00       | 0.00    | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |      |
| 5:15:00       | 0.00    | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |      |
| 5:20:00       | 0.00    | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |      |
| 5:25:00       | 0.00    | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |      |
| 5:30:00       | 0.00    | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |      |
| 5:35:00       | 0.00    | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |      |
| 5:40:00       | 0.00    | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |      |
| 5:45:00       | 0.00    | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |      |
| 5:50:00       | 0.00    | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |      |
| 5:55:00       | 0.00    | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |      |
| 6:00:00       | 0.00    | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |      |



# Weir Report

## Pond 3 Spillway

### Trapezoidal Weir

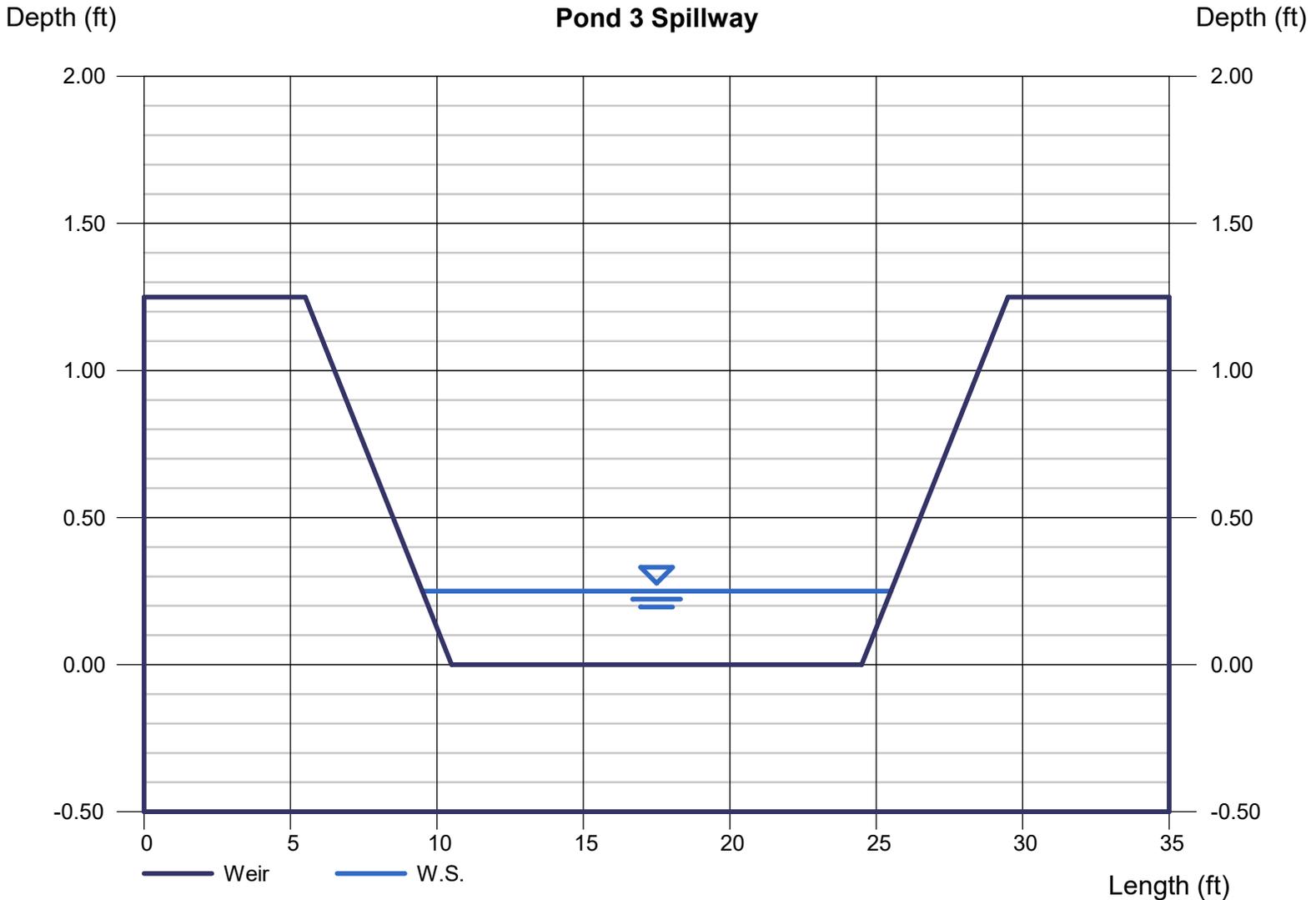
Crest = Sharp  
Bottom Length (ft) = 14.00  
Total Depth (ft) = 1.25  
Side Slope (z:1) = 4.00

### Highlighted

Depth (ft) = 0.25  
Q (cfs) = 5.700  
Area (sqft) = 3.75  
Velocity (ft/s) = 1.52  
Top Width (ft) = 16.00

### Calculations

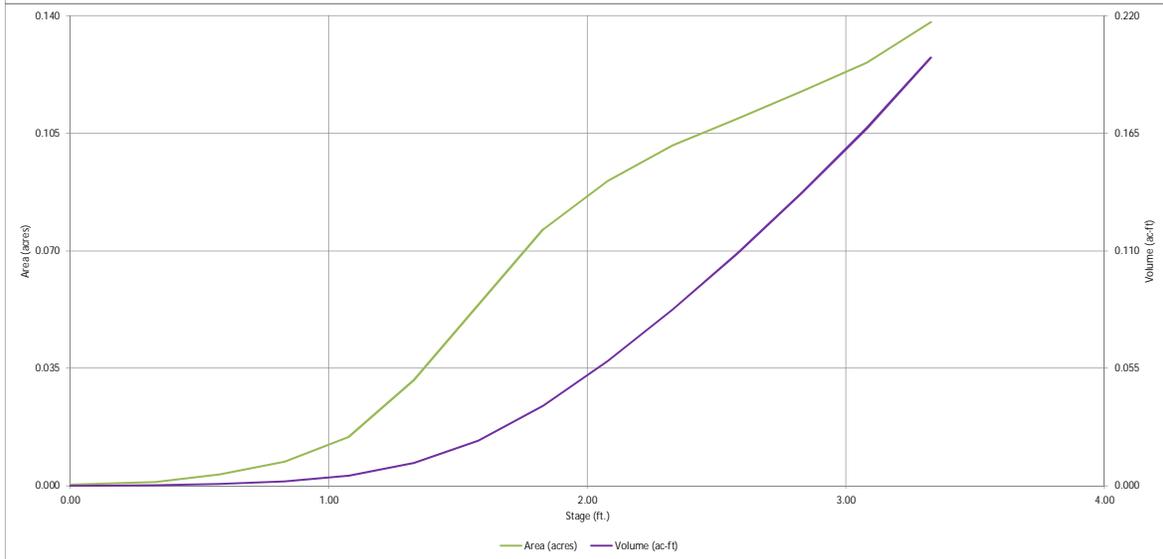
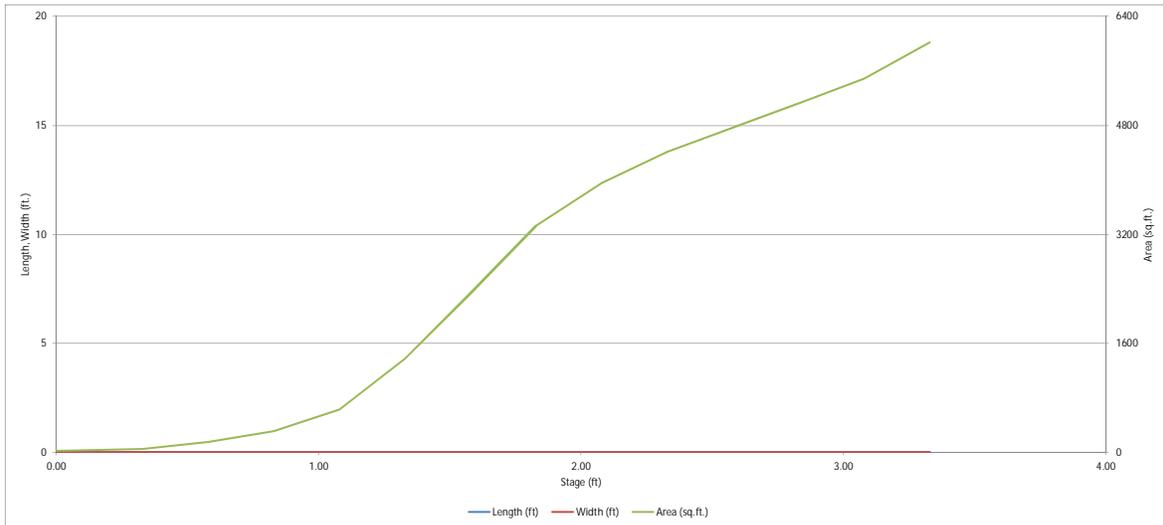
Weir Coeff. Cw = 3.10  
Compute by: Known Q  
Known Q (cfs) = 5.70





# DETENTION BASIN STAGE-STORAGE TABLE BUILDER

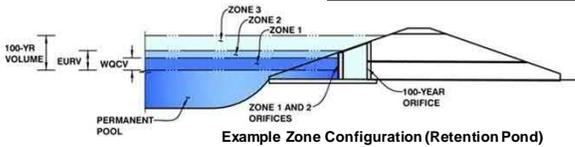
*MHFD-Detention, Version 4.03 (May 2020)*



# DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-*Detention, Version 4.03 (May 2020)*

Project: Cloverleaf Subdivision  
Basin ID: P4 (Private Water Quality Only Pond)



**Example Zone Configuration (Retention Pond)**

|                          | Estimated Stage (ft) | Estimated Volume (ac-ft) | Outlet Type          |
|--------------------------|----------------------|--------------------------|----------------------|
| Zone 1 (WOCV)            | 1.71                 | 0.029                    | Orifice Plate        |
| Zone 2                   |                      |                          | Weir&Pipe (Circular) |
| Zone 3                   |                      |                          |                      |
| <b>Total (all zones)</b> |                      | <b>0.029</b>             |                      |

User Input: Orifice at Underdrain Outlet (typically used to drain WOCV in a Filtration BMP)

|                                   |     |  |
|-----------------------------------|-----|--|
| Underdrain Orifice Invert Depth = | N/A | ft (distance below the filtration media surface) |
| Underdrain Orifice Diameter =     | N/A | inches   |

Calculated Parameters for Underdrain

|                               |     |                 |
|-------------------------------|-----|-----------------|
| Underdrain Orifice Area =     | N/A | ft <sup>2</sup> |
| Underdrain Orifice Centroid = | N/A | feet            |

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WOCV and/or EURV in a sedimentation BMP)

|  |      |   |
|--|------|---|
| Invert of Lowest Orifice =                 | 0.00 | ft (relative to basin bottom at Stage = 0 ft) |
| Depth at top of Zone using Orifice Plate = | 1.71 | ft (relative to basin bottom at Stage = 0 ft) |
| Orifice Plate: Orifice Vertical Spacing =  | N/A  | inches  |
| Orifice Plate: Orifice Area per Row =      | N/A  | inches  |

Calculated Parameters for Plate

|                            |     |                 |
|----------------------------|-----|-----------------|
| WO Orifice Area per Row =  | N/A | ft <sup>2</sup> |
| Elliptical Half-Width =    | N/A | feet            |
| Elliptical Slot Centroid = | N/A | feet            |
| Elliptical Slot Area =     | N/A | ft <sup>2</sup> |

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

|                                | Row 1 (required) | Row 2 (optional) | Row 3 (optional) | Row 4 (optional) | Row 5 (optional) | Row 6 (optional) | Row 7 (optional) | Row 8 (optional) |
|--------------------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|
| Stage of Orifice Centroid (ft) | 0.00             | 0.83             |                  |                  |                  |                  |                  |                  |
| Orifice Area (sq. inches)      | 0.13             | 0.18             |                  |                  |                  |                  |                  |                  |

|                                | Row 9 (optional) | Row 10 (optional) | Row 11 (optional) | Row 12 (optional) | Row 13 (optional) | Row 14 (optional) | Row 15 (optional) | Row 16 (optional) |
|--------------------------------|------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| Stage of Orifice Centroid (ft) |                  |                   |                   |                   |                   |                   |                   |                   |
| Orifice Area (sq. inches)      |                  |                   |                   |                   |                   |                   |                   |                   |

User Input: Vertical Orifice (Circular or Rectangular)

|   | Not Selected | Not Selected |   |
|---|--------------|--------------|---|
| Invert of Vertical Orifice =                  |              |              | ft (relative to basin bottom at Stage = 0 ft) |
| Depth at top of Zone using Vertical Orifice = |              |              | ft (relative to basin bottom at Stage = 0 ft) |
| Vertical Orifice Diameter =                   |              |              | inches  |

Calculated Parameters for Vertical Orifice

|                             | Not Selected | Not Selected |                 |
|-----------------------------|--------------|--------------|-----------------|
| Vertical Orifice Area =     |              |              | ft <sup>2</sup> |
| Vertical Orifice Centroid = |              |              | feet            |

User Input: Overflow Weir (Dropbox with Flat or Sloped Gate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe))

|                                       | Zone 2 Weir | Not Selected |   |
|---------------------------------------|-------------|--------------|---|
| Overflow Weir Front Edge Height, Ho = | 1.72        |              | ft (relative to basin bottom at Stage = 0 ft) |
| Overflow Weir Front Edge Length =     | 4.00        |              | feet  |
| Overflow Weir Gate Slope =            | 0.00        |              | H:V   |
| Horiz. Length of Weir Sides =         | 4.00        |              | feet  |
| Overflow Gate Open Area % =           | 70%         |              | %, gate open area/total area                  |
| Debris Clogging % =                   | 0%          |              | %   |

Calculated Parameters for Overflow Weir

|  | Zone 2 Weir | Not Selected |                 |
|--|-------------|--------------|-----------------|
| Height of Gate Upper Edge, Hi =        | 1.72        |              | feet            |
| Overflow Weir Slope Length =           | 4.00        |              | feet            |
| Gate Open Area / 100-yr Orifice Area = | 6.34        |              |                 |
| Overflow Gate Open Area w/o Debris =   | 11.20       |              | ft <sup>2</sup> |
| Overflow Gate Open Area w/ Debris =    | 11.20       |              | ft <sup>2</sup> |

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

|                                  | Zone 2 Circular | Not Selected |  |
|----------------------------------|-----------------|--------------|--|
| Depth to Invert of Outlet Pipe = | 0.50            |              | ft (distance below basin bottom at Stage = 0 ft) |
| Circular Orifice Diameter =      | 18.00           |              | inches   |

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate

|  | Zone 2 Circular | Not Selected |                 |
|--|-----------------|--------------|-----------------|
| Outlet Orifice Area =                            | 1.77            |              | ft <sup>2</sup> |
| Outlet Orifice Centroid =                        | 0.75            |              | feet            |
| Half-Central Angle of Restrictor Plate on Pipe = | N/A             | N/A          | radians         |

User Input: Emergency Spillway (Rectangular or Trapezoidal)

|                                     |       |   |
|-------------------------------------|-------|---|
| Spillway Invert Stage =             | 2.13  | ft (relative to basin bottom at Stage = 0 ft) |
| Spillway Crest Length =             | 22.00 | feet  |
| Spillway End Slopes =               | 4.00  | H:V   |
| Freeboard above Max Water Surface = | 1.00  | feet  |

Calculated Parameters for Spillway

|                                    |      |         |
|------------------------------------|------|---------|
| Spillway Design Flow Depth =       | 0.19 | feet    |
| Stage at Top of Freeboard =        | 3.32 | feet    |
| Basin Area at Top of Freeboard =   | 0.14 | acres   |
| Basin Volume at Top of Freeboard = | 0.20 | acre-ft |

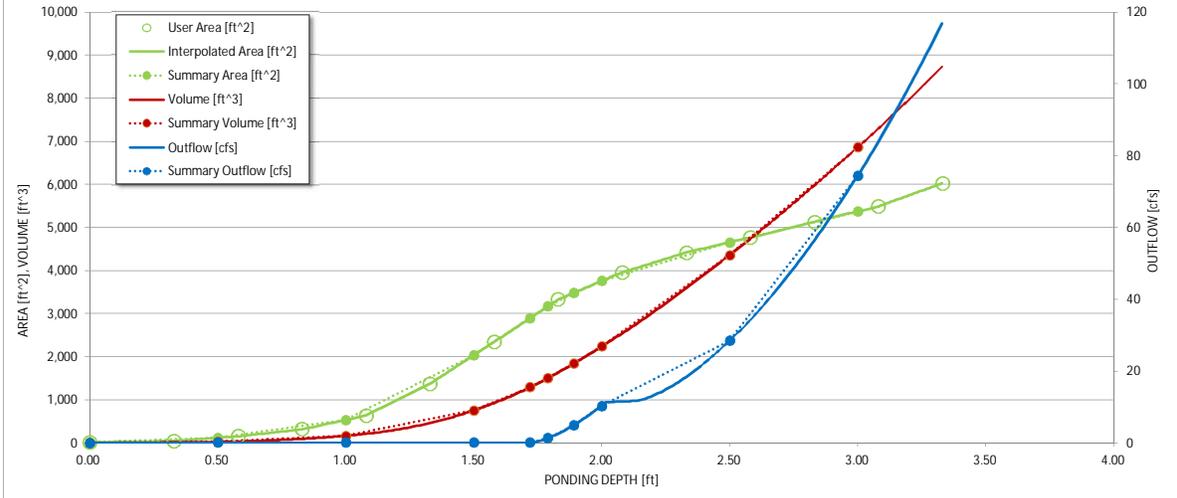
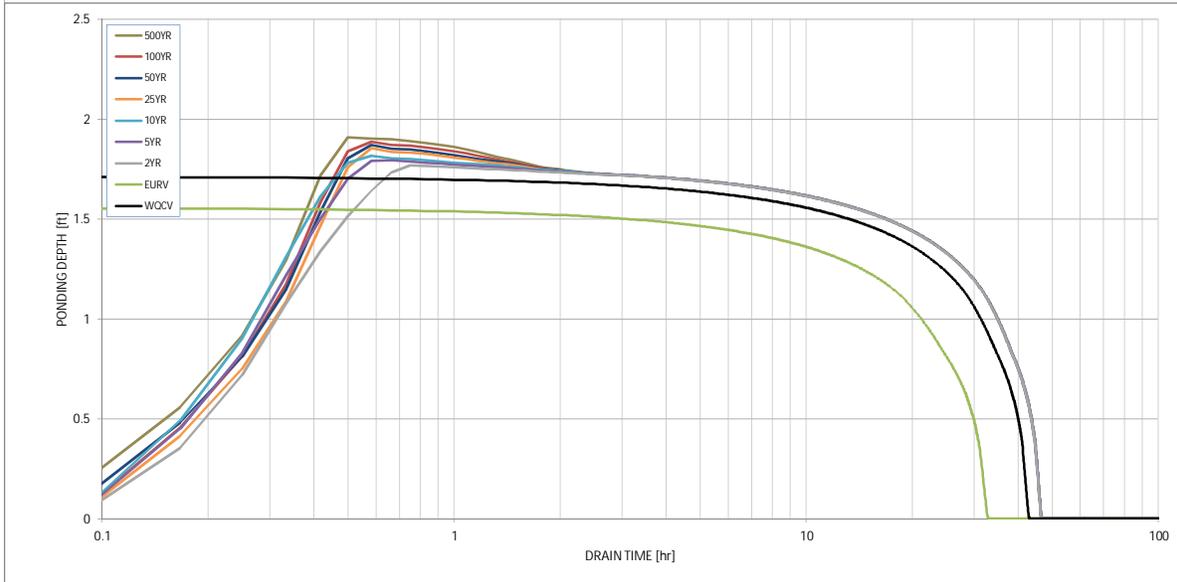
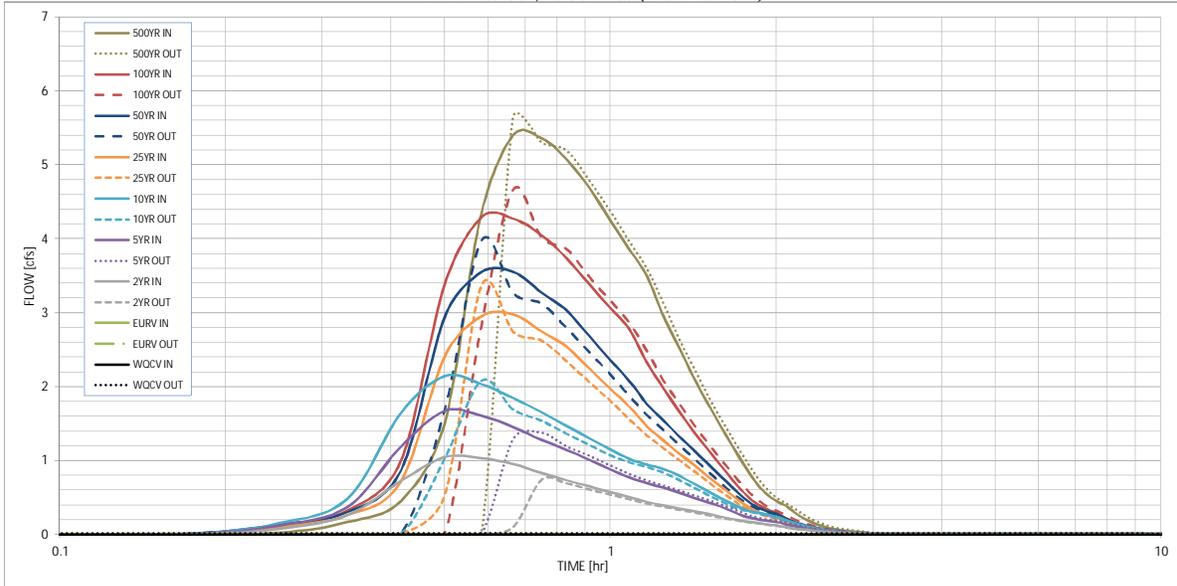
## Routed Hydrograph Results

*The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).*

|   | WOCV            | EURV     | 2 Year          | 5 Year          | 10 Year         | 25 Year         | 50 Year         | 100 Year        | 500 Year        |
|---|-----------------|----------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|
| Design Storm Return Period                    |                 |          |                 |                 |                 |                 |                 |                 |                 |
| One-Hour Rainfall Depth (in)                  | N/A             | N/A      | 1.19            | 1.50            | 1.75            | 2.00            | 2.25            | 2.52            | 3.00            |
| CUHP Runoff Volume (acre-ft)                  | 0.029           | 0.076    | 0.073           | 0.113           | 0.149           | 0.202           | 0.243           | 0.297           | 0.378           |
| Inflow Hydrograph Volume (acre-ft)            | N/A             | N/A      | 0.073           | 0.113           | 0.149           | 0.202           | 0.243           | 0.297           | 0.378           |
| CUHP Predevelopment Peak Q (cfs)              | N/A             | N/A      | 0.2             | 0.7             | 1.0             | 1.7             | 2.2             | 2.7             | 3.5             |
| OPTIONAL Override Predevelopment Peak Q (cfs) | N/A             | N/A      |                 |                 |                 |                 |                 |                 |                 |
| Predevelopment Unit Peak Flow, q (cfs/acre)   | N/A             | N/A      | 0.11            | 0.32            | 0.48            | 0.85            | 1.06            | 1.33            | 1.73            |
| Peak Inflow Q (cfs)                           | N/A             | N/A      | 1.0             | 1.7             | 2.1             | 3.0             | 3.5             | 4.3             | 5.4             |
| Peak Outflow Q (cfs)                          | 0.0             | 8.2      | 0.7             | 1.4             | 2.1             | 3.4             | 4.0             | 4.7             | 5.6             |
| Ratio Peak Outflow to Predevelopment Q        | N/A             | N/A      | N/A             | 2.1             | 2.1             | 1.9             | 1.8             | 1.7             | 1.6             |
| Structure Controlling Flow                    | Overflow Weir 1 | Spillway | Overflow Weir 1 |
| Max Velocity through Gate 1 (fps)             | N/A             | 1.08     | 0.07            | 0.1             | 0.2             | 0.3             | 0.4             | 0.4             | 0.5             |
| Max Velocity through Gate 2 (fps)             | N/A             | N/A      | N/A             | N/A             | N/A             | N/A             | N/A             | N/A             | N/A             |
| Time to Drain 97% of Inflow Volume (hours)    | 39              | 27       | 38              | 36              | 34              | 31              | 30              | 27              | 24              |
| Time to Drain 99% of Inflow Volume (hours)    | 41              | 30       | 43              | 41              | 40              | 39              | 38              | 36              | 35              |
| Maximum Ponding Depth (ft)                    | 1.72            | 2.27     | 1.77            | 1.79            | 1.82            | 1.85            | 1.87            | 1.89            | 1.91            |
| Area at Maximum Ponding Depth (acres)         | 0.07            | 0.10     | 0.07            | 0.07            | 0.07            | 0.08            | 0.08            | 0.08            | 0.08            |
| Maximum Volume Stored (acre-ft)               | 0.030           | 0.076    | 0.032           | 0.034           | 0.036           | 0.039           | 0.040           | 0.041           | 0.043           |

# DETENTION BASIN OUTLET STRUCTURE DESIGN

*MHFD-Detention, Version 4.00 (December 2019)*



| S-A-V-D Chart Axis Override | X-axis | Left Y-Axis | Right Y-Axis |
|-----------------------------|--------|-------------|--------------|
| minimum bound               |        |             |              |
| maximum bound               |        |             |              |

# DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename: \_\_\_\_\_

## Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

| Time Interval | SOURCE  | WQCV [cfs] | EURV [cfs] | 2 Year [cfs] | 5 Year [cfs] | 10 Year [cfs] | 25 Year [cfs] | 50 Year [cfs] | 100 Year [cfs] | 500 Year [cfs] |
|---------------|---------|------------|------------|--------------|--------------|---------------|---------------|---------------|----------------|----------------|
| 5.00 min      | 0:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 0:05:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 0:10:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.01          | 0.00           | 0.02           |
|               | 0:15:00 | 0.00       | 0.00       | 0.07         | 0.12         | 0.15          | 0.10          | 0.13          | 0.12           | 0.17           |
|               | 0:20:00 | 0.00       | 0.00       | 0.26         | 0.37         | 0.48          | 0.26          | 0.30          | 0.32           | 0.45           |
|               | 0:25:00 | 0.00       | 0.00       | 0.72         | 1.19         | 1.64          | 0.72          | 0.86          | 0.99           | 1.49           |
|               | 0:30:00 | 0.00       | 0.00       | 1.05         | 1.67         | 2.14          | 2.40          | 2.93          | 3.37           | 4.34           |
|               | 0:35:00 | 0.00       | 0.00       | 1.03         | 1.61         | 2.03          | 2.95          | 3.54          | 4.28           | 5.40           |
|               | 0:40:00 | 0.00       | 0.00       | 0.95         | 1.45         | 1.84          | 2.97          | 3.55          | 4.27           | 5.36           |
|               | 0:45:00 | 0.00       | 0.00       | 0.83         | 1.28         | 1.65          | 2.74          | 3.27          | 4.05           | 5.07           |
|               | 0:50:00 | 0.00       | 0.00       | 0.73         | 1.15         | 1.47          | 2.54          | 3.03          | 3.73           | 4.68           |
|               | 0:55:00 | 0.00       | 0.00       | 0.65         | 1.01         | 1.30          | 2.24          | 2.68          | 3.38           | 4.25           |
|               | 1:00:00 | 0.00       | 0.00       | 0.57         | 0.88         | 1.15          | 1.97          | 2.36          | 3.07           | 3.85           |
|               | 1:05:00 | 0.00       | 0.00       | 0.51         | 0.77         | 1.02          | 1.73          | 2.08          | 2.77           | 3.49           |
|               | 1:10:00 | 0.00       | 0.00       | 0.44         | 0.70         | 0.94          | 1.46          | 1.76          | 2.32           | 2.95           |
|               | 1:15:00 | 0.00       | 0.00       | 0.39         | 0.63         | 0.89          | 1.27          | 1.54          | 1.98           | 2.53           |
|               | 1:20:00 | 0.00       | 0.00       | 0.35         | 0.56         | 0.80          | 1.10          | 1.33          | 1.67           | 2.13           |
|               | 1:25:00 | 0.00       | 0.00       | 0.31         | 0.50         | 0.69          | 0.95          | 1.15          | 1.40           | 1.79           |
|               | 1:30:00 | 0.00       | 0.00       | 0.28         | 0.44         | 0.59          | 0.80          | 0.96          | 1.16           | 1.48           |
|               | 1:35:00 | 0.00       | 0.00       | 0.24         | 0.38         | 0.50          | 0.66          | 0.79          | 0.94           | 1.20           |
|               | 1:40:00 | 0.00       | 0.00       | 0.21         | 0.31         | 0.41          | 0.53          | 0.64          | 0.74           | 0.94           |
|               | 1:45:00 | 0.00       | 0.00       | 0.18         | 0.25         | 0.34          | 0.41          | 0.49          | 0.57           | 0.72           |
|               | 1:50:00 | 0.00       | 0.00       | 0.16         | 0.21         | 0.30          | 0.32          | 0.38          | 0.43           | 0.56           |
|               | 1:55:00 | 0.00       | 0.00       | 0.14         | 0.19         | 0.27          | 0.26          | 0.32          | 0.35           | 0.46           |
|               | 2:00:00 | 0.00       | 0.00       | 0.12         | 0.17         | 0.24          | 0.23          | 0.28          | 0.29           | 0.39           |
|               | 2:05:00 | 0.00       | 0.00       | 0.10         | 0.14         | 0.19          | 0.18          | 0.22          | 0.22           | 0.29           |
|               | 2:10:00 | 0.00       | 0.00       | 0.08         | 0.11         | 0.15          | 0.13          | 0.17          | 0.16           | 0.22           |
|               | 2:15:00 | 0.00       | 0.00       | 0.06         | 0.09         | 0.12          | 0.10          | 0.13          | 0.12           | 0.16           |
|               | 2:20:00 | 0.00       | 0.00       | 0.05         | 0.07         | 0.09          | 0.08          | 0.10          | 0.09           | 0.12           |
|               | 2:25:00 | 0.00       | 0.00       | 0.04         | 0.05         | 0.07          | 0.06          | 0.07          | 0.06           | 0.09           |
|               | 2:30:00 | 0.00       | 0.00       | 0.03         | 0.04         | 0.05          | 0.05          | 0.06          | 0.05           | 0.07           |
|               | 2:35:00 | 0.00       | 0.00       | 0.02         | 0.03         | 0.04          | 0.03          | 0.04          | 0.04           | 0.05           |
|               | 2:40:00 | 0.00       | 0.00       | 0.02         | 0.02         | 0.03          | 0.03          | 0.03          | 0.03           | 0.04           |
|               | 2:45:00 | 0.00       | 0.00       | 0.01         | 0.02         | 0.02          | 0.02          | 0.02          | 0.02           | 0.03           |
|               | 2:50:00 | 0.00       | 0.00       | 0.01         | 0.01         | 0.02          | 0.01          | 0.02          | 0.02           | 0.02           |
|               | 2:55:00 | 0.00       | 0.00       | 0.01         | 0.01         | 0.01          | 0.01          | 0.01          | 0.01           | 0.01           |
|               | 3:00:00 | 0.00       | 0.00       | 0.00         | 0.01         | 0.01          | 0.01          | 0.01          | 0.01           | 0.01           |
|               | 3:05:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.01           |
|               | 3:10:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:15:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:20:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:25:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:30:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:35:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:40:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:45:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:50:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:55:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:05:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:10:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:15:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:20:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:25:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:30:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:35:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:40:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:45:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:50:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:55:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:05:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:10:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:15:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:20:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:25:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:30:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:35:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:40:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:45:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:50:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:55:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 6:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |



## Site-Level Low Impact Development (LID) Design Effective Impervious Calculator LID Credit by Impervious Reduction Factor (IRF) Method

UD-BMP (Version 3.06, November 2016)

|  |                |      |
|--|----------------|------|
| User Input   |                |      |
| Calculated cells   |                |      |
| ---Design Storm: 1-Hour Rain Depth                                     | WQCV Event     | 0.60 |
| ---Minor Storm: 1-Hour Rain Depth                                      | 5-Year Event   | 1.50 |
| ---Major Storm: 1-Hour Rain Depth                                      | 100-Year Event | 2.52 |
| Optional User Defined Storm  | CUHP           |      |
| (CUHP) NOAA 1 Hour Rainfall Depth and Frequency for User Defined Storm | 100-Year Event |      |
| Max Intensity for Optional User Defined Storm                          |                | 0    |

**Designer:** REB  
**Company:** JR Engineering  
**Date:** August 18, 2021  
**Project:** Cloverleaf Filing No. 2  
**Location:** El Paso County

**SITE INFORMATION (USER-INPUT)**

| Sub-basin Identifier   | O             | N             | M             |               |               |               |               |               |               |               |               |  |  |  |
|--|---------------|---------------|---------------|---------------|---------------|---------------|---------------|---------------|---------------|---------------|---------------|--|--|--|
| Receiving Pervious Area Soil Type  | Sandy Loam    | Sandy Loam    | Sandy Loam    |               |               |               |               |               |               |               |               |  |  |  |
| Total Area (ac., Sum of DCIA, UIA, RPA, & SPA)                             | 0.980         | 0.530         | 0.540         |               |               |               |               |               |               |               |               |  |  |  |
| Directly Connected Impervious Area (DCIA, acres)                           | 0.235         | 0.150         | 0.120         |               |               |               |               |               |               |               |               |  |  |  |
| Unconnected Impervious Area (UIA, acres)                                   | 0.319         | 0.160         | 0.200         |               |               |               |               |               |               |               |               |  |  |  |
| Receiving Pervious Area (RPA, acres)                                       | 0.426         | 0.220         | 0.220         |               |               |               |               |               |               |               |               |  |  |  |
| Separate Pervious Area (SPA, acres)  | 0.000         | 0.000         | 0.000         |               |               |               |               |               |               |               |               |  |  |  |
| RPA Treatment Type: Conveyance (C), Volume (V), or Permeable Pavement (PP) | V             | C             | C             | C             | C             | C             | C             | C             | C             | C             | C             |  |  |  |
|  | MISSING INPUT |  |  |  |

**CALCULATED RESULTS (OUTPUT)**

|  |       |       |       |  |  |  |  |  |  |  |  |  |  |  |
|--|-------|-------|-------|--|--|--|--|--|--|--|--|--|--|--|
| Total Calculated Area (ac, check against input)                | 0.980 | 0.530 | 0.540 |  |  |  |  |  |  |  |  |  |  |  |
| Directly Connected Impervious Area (DCIA, %)                   | 24.0% | 28.3% | 22.2% |  |  |  |  |  |  |  |  |  |  |  |
| Unconnected Impervious Area (UIA, %)                           | 32.6% | 30.2% | 37.0% |  |  |  |  |  |  |  |  |  |  |  |
| Receiving Pervious Area (RPA, %)                               | 43.5% | 41.5% | 40.7% |  |  |  |  |  |  |  |  |  |  |  |
| Separate Pervious Area (SPA, %)                                | 0.0%  | 0.0%  | 0.0%  |  |  |  |  |  |  |  |  |  |  |  |
| A <sub>w</sub> (RPA / UIA)                                     | 1.335 | 1.375 | 1.100 |  |  |  |  |  |  |  |  |  |  |  |
| I <sub>a</sub> Check   | 0.430 | 0.420 | 0.480 |  |  |  |  |  |  |  |  |  |  |  |
| f / I for WQCV Event:  | 1.7   | 1.7   | 1.7   |  |  |  |  |  |  |  |  |  |  |  |
| f / I for 5-Year Event:  | 0.5   | 0.5   | 0.5   |  |  |  |  |  |  |  |  |  |  |  |
| f / I for 100-Year Event:                                      | 0.3   | 0.3   | 0.3   |  |  |  |  |  |  |  |  |  |  |  |
| f / I for Optional User Defined Storm CUHP:                    |       |       |       |  |  |  |  |  |  |  |  |  |  |  |
| IRF for WQCV Event:  | 0.00  | 0.62  | 0.65  |  |  |  |  |  |  |  |  |  |  |  |
| IRF for 5-Year Event:  | 0.87  | 0.88  | 0.89  |  |  |  |  |  |  |  |  |  |  |  |
| IRF for 100-Year Event:  | 0.92  | 0.92  | 0.93  |  |  |  |  |  |  |  |  |  |  |  |
| IRF for Optional User Defined Storm CUHP:                      |       |       |       |  |  |  |  |  |  |  |  |  |  |  |
| Total Site Imperviousness: I <sub>total</sub>                  | 56.5% | 58.5% | 59.3% |  |  |  |  |  |  |  |  |  |  |  |
| Effective Imperviousness for WQCV Event:                       | 24.0% | 47.1% | 46.3% |  |  |  |  |  |  |  |  |  |  |  |
| Effective Imperviousness for 5-Year Event:                     | 52.3% | 55.0% | 55.3% |  |  |  |  |  |  |  |  |  |  |  |
| Effective Imperviousness for 100-Year Event:                   | 53.9% | 56.1% | 56.6% |  |  |  |  |  |  |  |  |  |  |  |
| Effective Imperviousness for Optional User Defined Storm CUHP: |       |       |       |  |  |  |  |  |  |  |  |  |  |  |

**LID / EFFECTIVE IMPERVIOUSNESS CREDITS**

|  |      |       |       |  |  |  |  |  |  |  |  |  |     |     |     |
|--|------|-------|-------|--|--|--|--|--|--|--|--|--|-----|-----|-----|
| WQCV Event CREDIT: Reduce Detention By:        | N/A  | 14.2% | 16.0% |  |  |  |  |  |  |  |  |  | N/A | N/A | N/A |
| This line only for 10-Year Event               | N/A  | N/A   | N/A   |  |  |  |  |  |  |  |  |  | N/A | N/A | N/A |
| 100-Year Event CREDIT**: Reduce Detention By:  | 4.5% | 4.0%  | 4.4%  |  |  |  |  |  |  |  |  |  | N/A | N/A | N/A |
| User Defined CUHP CREDIT: Reduce Detention By: |      |       |       |  |  |  |  |  |  |  |  |  |     |     |     |

|   |       |
|---|-------|
| Total Site Imperviousness:  | 57.8% |
| Total Site Effective Imperviousness for WQCV Event:                       | 35.8% |
| Total Site Effective Imperviousness for 5-Year Event:                     | 53.8% |
| Total Site Effective Imperviousness for 100-Year Event:                   | 55.2% |
| Total Site Effective Imperviousness for Optional User Defined Storm CUHP: |       |

**Notes:**

- \* Use Green-Ampt average infiltration rate values from Table 3-3.
- \*\* Flood control detention volume credits based on empirical equations from Storage Chapter of USDCM.
- \*\*\* Method assumes that 1-hour rainfall depth is equivalent to 1-hour intensity for calculation purposed

# Weir Report

## Pond 4 Spillway

### Trapezoidal Weir

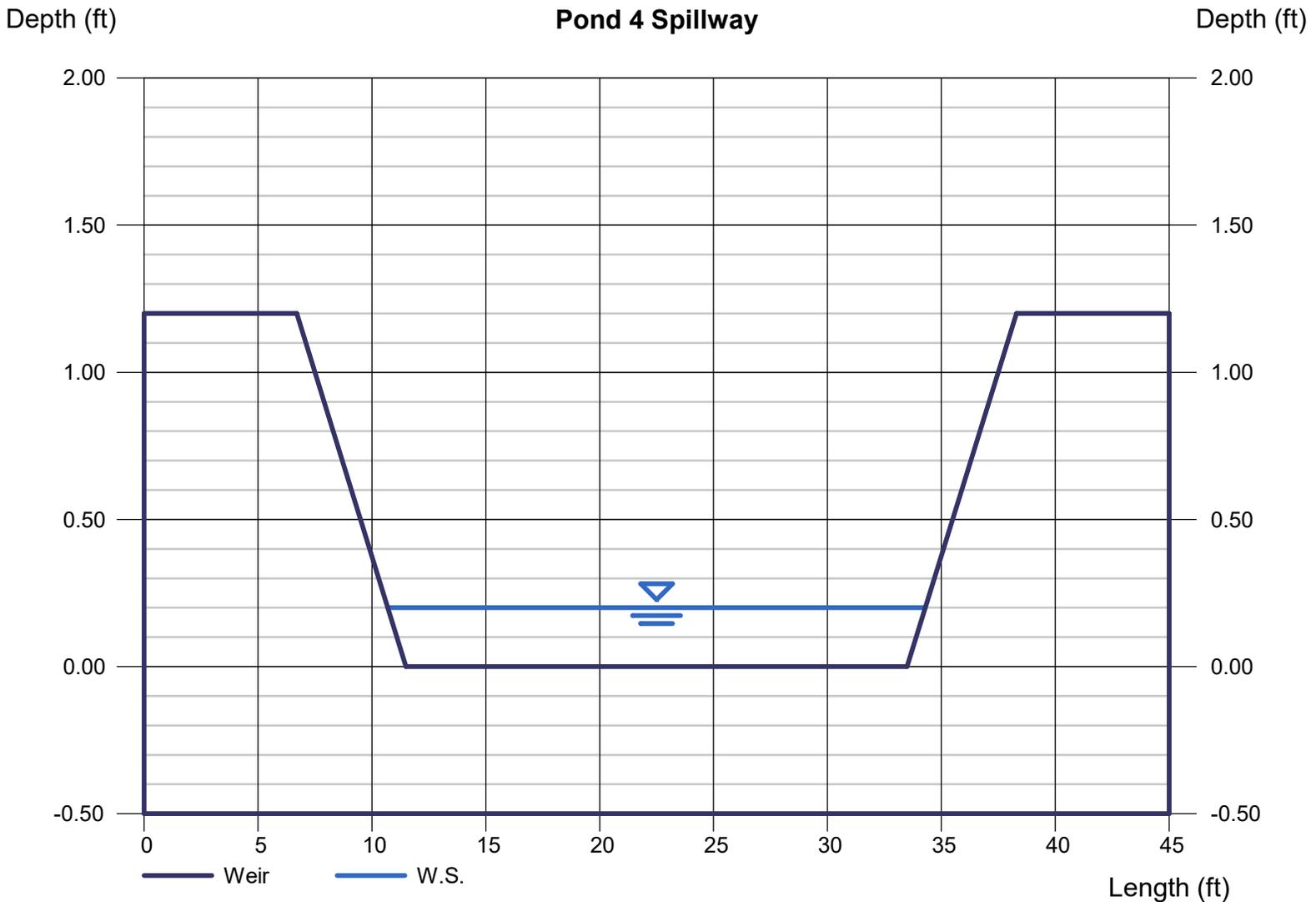
Crest = Sharp  
Bottom Length (ft) = 22.00  
Total Depth (ft) = 1.20  
Side Slope (z:1) = 4.00

### Highlighted

Depth (ft) = 0.20  
Q (cfs) = 6.100  
Area (sqft) = 4.56  
Velocity (ft/s) = 1.34  
Top Width (ft) = 23.60

### Calculations

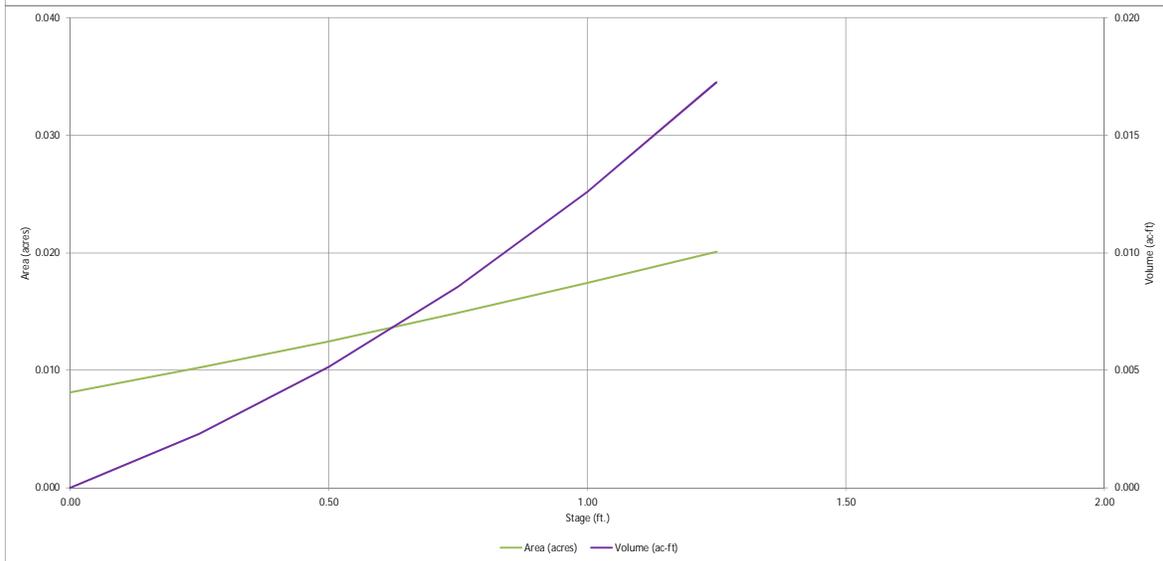
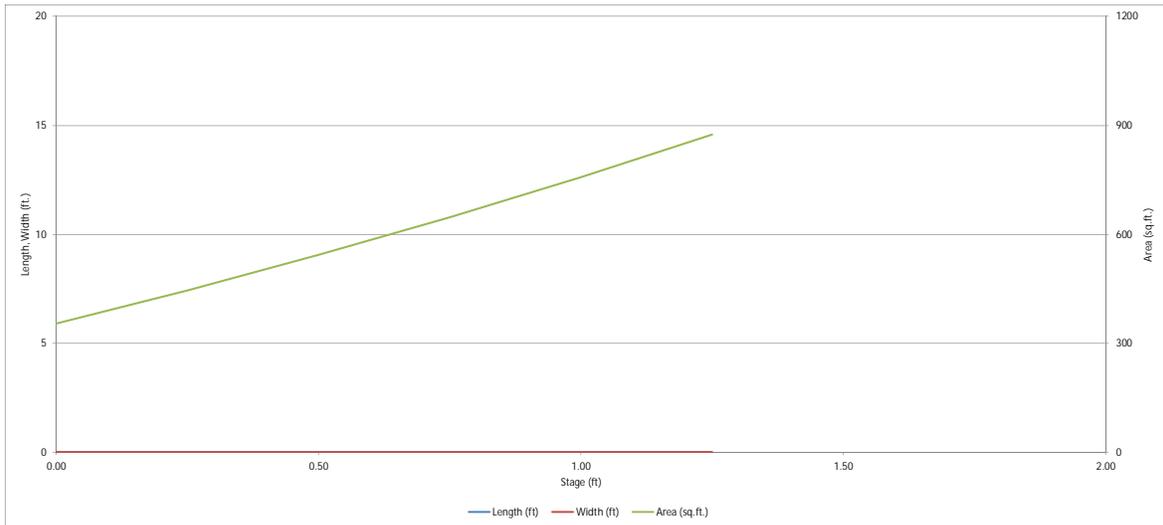
Weir Coeff. Cw = 3.10  
Compute by: Known Q  
Known Q (cfs) = 6.10





# DETENTION BASIN STAGE-STORAGE TABLE BUILDER

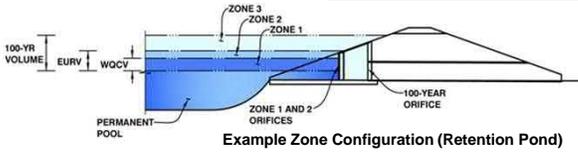
*MHFD-Detention, Version 4.03 (May 2020)*



# DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.03 (May 2020)

Project: Cloverleaf Subdivision  
Basin ID: OS4 (Sand Filter)



**Example Zone Configuration (Retention Pond)**

|                   | Estimated Stage (ft) | Estimated Volume (ac-ft) | Outlet Type          |
|-------------------|----------------------|--------------------------|----------------------|
| Zone 1 (WOCV)     | 0.83                 | 0.010                    | Filtration Media     |
| Zone 2            |                      |                          | Weir&Pipe (Circular) |
| Zone 3            |                      |                          |                      |
| Total (all zones) |                      | 0.010                    |                      |

User Input: Orifice at Underdrain Outlet (typically used to drain WOCV in a Filtration BMP)

Underdrain Orifice Invert Depth = 1.50 ft (distance below the filtration media surface)  
Underdrain Orifice Diameter = 0.53 inches

Calculated Parameters for Underdrain

Underdrain Orifice Area = 0.0 ft<sup>2</sup>  
Underdrain Orifice Centroid = 0.02 feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WOCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice = N/A ft (relative to basin bottom at Stage = 0 ft)  
Depth at top of Zone using Orifice Plate = N/A ft (relative to basin bottom at Stage = 0 ft)  
Orifice Plate: Orifice Vertical Spacing = N/A inches  
Orifice Plate: Orifice Area per Row = N/A inches

Calculated Parameters for Plate

WO Orifice Area per Row = N/A ft<sup>2</sup>  
Elliptical Half-Width = N/A feet  
Elliptical Slot Centroid = N/A feet  
Elliptical Slot Area = N/A ft<sup>2</sup>

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

|                                | Row 1 (optional) | Row 2 (optional) | Row 3 (optional) | Row 4 (optional) | Row 5 (optional) | Row 6 (optional) | Row 7 (optional) | Row 8 (optional) |
|--------------------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|
| Stage of Orifice Centroid (ft) | N/A              |
| Orifice Area (sq. inches)      | N/A              |

|                                | Row 9 (optional) | Row 10 (optional) | Row 11 (optional) | Row 12 (optional) | Row 13 (optional) | Row 14 (optional) | Row 15 (optional) | Row 16 (optional) |
|--------------------------------|------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| Stage of Orifice Centroid (ft) | N/A              | N/A               | N/A               | N/A               | N/A               | N/A               | N/A               | N/A               |
| Orifice Area (sq. inches)      | N/A              | N/A               | N/A               | N/A               | N/A               | N/A               | N/A               | N/A               |

User Input: Vertical Orifice (Circular or Rectangular)

Invert of Vertical Orifice = Not Selected ft (relative to basin bottom at Stage = 0 ft)  
Depth at top of Zone using Vertical Orifice = Not Selected ft (relative to basin bottom at Stage = 0 ft)  
Vertical Orifice Diameter = Not Selected inches

Calculated Parameters for Vertical Orifice

Vertical Orifice Area = Not Selected ft<sup>2</sup>  
Vertical Orifice Centroid = Not Selected feet

User Input: Overflow Weir (Dropbox with Flat or Sloped Gate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe))

Overflow Weir Front Edge Height, Ho = 0.86 ft (relative to basin bottom at Stage = 0 ft)  
Overflow Weir Front Edge Length = 3.00 feet  
Overflow Weir Gate Slope = 0.00 H:V  
Horiz. Length of Weir Sides = 3.00 feet  
Overflow Gate Open Area % = 70%  
Debris Clogging % = 50%

Calculated Parameters for Overflow Weir

Height of Gate Upper Edge, H<sub>1</sub> = 0.86 feet  
Overflow Weir Slope Length = 3.00 feet  
Gate Open Area / 100-yr Orifice Area = 3.57  
Overflow Gate Open Area w/o Debris = 6.30 ft<sup>2</sup>  
Overflow Gate Open Area w/ Debris = 3.15 ft<sup>2</sup>

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

Depth to Invert of Outlet Pipe = 2.00 ft (distance below basin bottom at Stage = 0 ft)  
Circular Orifice Diameter = 18.00 inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate

Outlet Orifice Area = 1.77 ft<sup>2</sup>  
Outlet Orifice Centroid = 0.75 feet  
Half-Central Angle of Restrictor Plate on Pipe = N/A radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage = Not Selected ft (relative to basin bottom at Stage = 0 ft)  
Spillway Crest Length = Not Selected feet  
Spillway End Slopes = Not Selected H:V  
Freeboard above Max Water Surface = Not Selected feet

Calculated Parameters for Spillway

Spillway Design Flow Depth = Not Selected feet  
Stage at Top of Freeboard = Not Selected feet  
Basin Area at Top of Freeboard = Not Selected acres  
Basin Volume at Top of Freeboard = Not Selected acre-ft

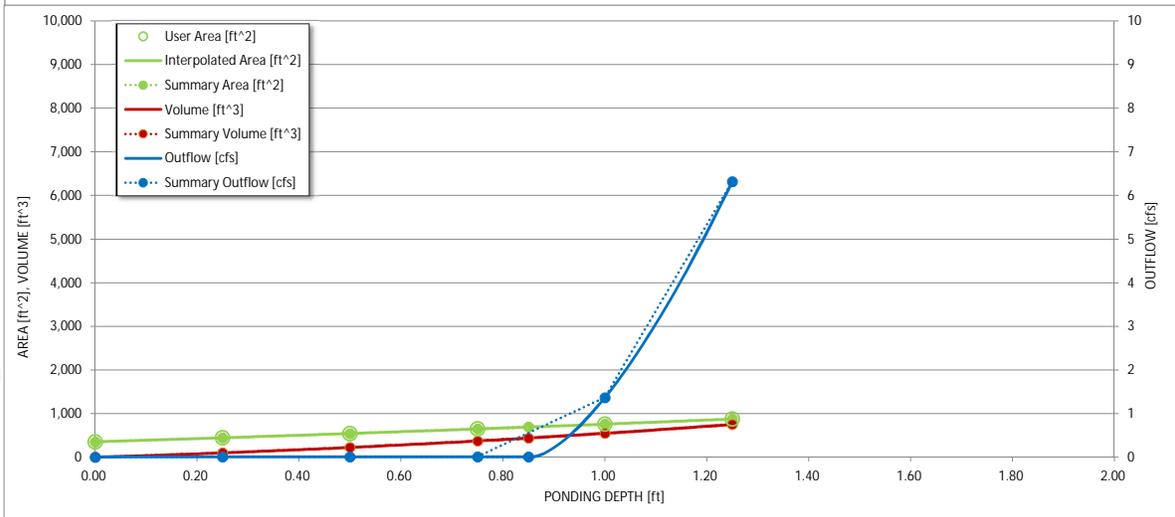
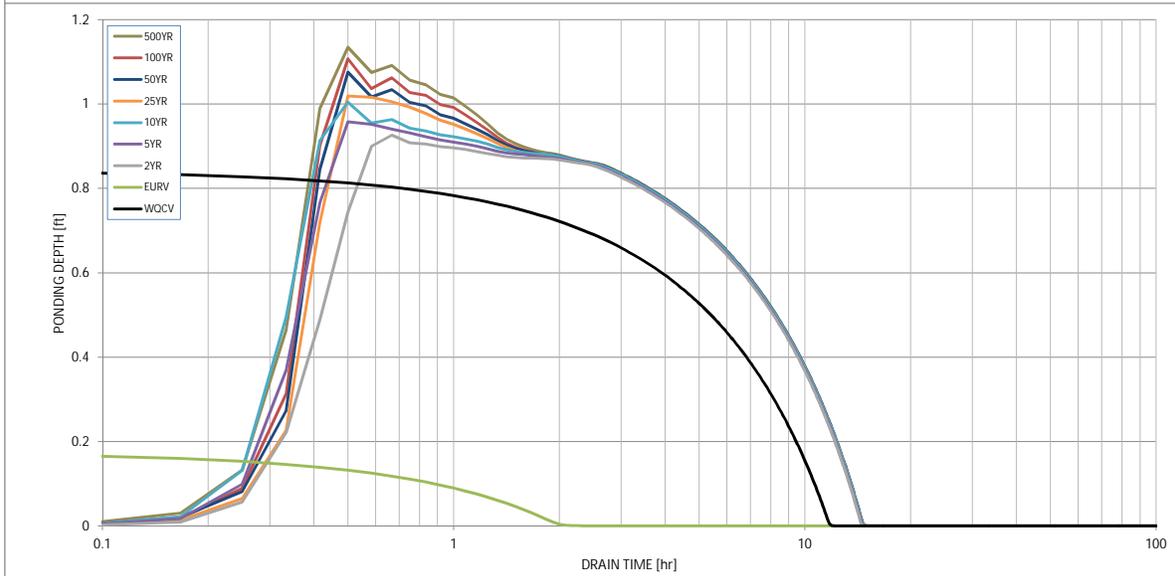
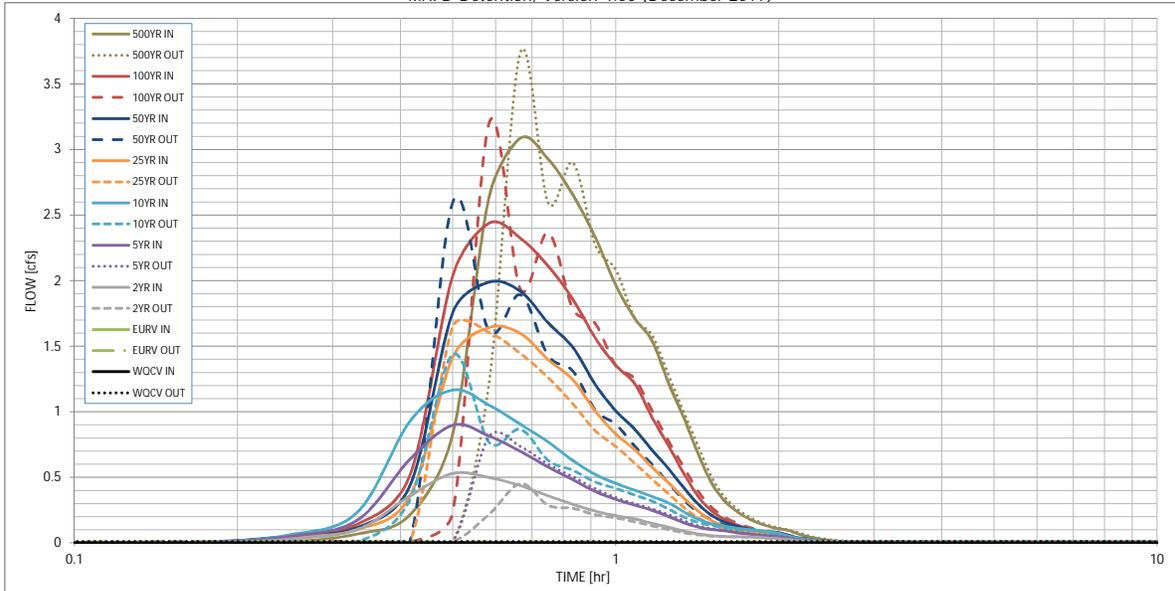
## Routed Hydrograph Results

The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).

|   | WOCV             | EURV             | 2 Year          | 5 Year          | 10 Year         | 25 Year         | 50 Year         | 100 Year        | 500 Year        |
|---|------------------|------------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|
| Design Storm Return Period                    | N/A              | N/A              | 1.19            | 1.50            | 1.75            | 2.00            | 2.25            | 2.52            | 3.00            |
| One-Hour Rainfall Depth (in)                  | N/A              | N/A              | 0.028           | 0.046           | 0.063           | 0.088           | 0.107           | 0.133           | 0.171           |
| CUHP Runoff Volume (acre-ft)                  | N/A              | N/A              | 0.028           | 0.046           | 0.063           | 0.088           | 0.107           | 0.133           | 0.171           |
| Inflow Hydrograph Volume (acre-ft)            | N/A              | N/A              | 0.2             | 0.5             | 0.7             | 1.2             | 1.5             | 1.9             | 2.5             |
| CUHP Predevelopment Peak Q (cfs)              | N/A              | N/A              | 0.17            | 0.47            | 0.72            | 1.20            | 1.50            | 1.88            | 2.45            |
| OPTIONAL Override Predevelopment Peak Q (cfs) | N/A              | N/A              | 0.5             | 0.9             | 1.2             | 1.6             | 2.0             | 2.4             | 3.1             |
| Predevelopment Unit Peak Flow, q (cfs/acre)   | N/A              | N/A              | 0.5             | 0.8             | 1.4             | 1.6             | 2.6             | 3.2             | 3.7             |
| Peak Inflow Q (cfs)                           | N/A              | N/A              | N/A             | 1.7             | 2.0             | 1.4             | 1.7             | 1.7             | 1.5             |
| Peak Outflow Q (cfs)                          | N/A              | N/A              | N/A             | 0.08            | 0.1             | 0.2             | 0.3             | 0.4             | 0.6             |
| Ratio Peak Outflow to Predevelopment Q        | N/A              | N/A              | N/A             | N/A             | N/A             | N/A             | N/A             | N/A             | N/A             |
| Structure Controlling Flow                    | Filtration Media | Filtration Media | Overflow Weir 1 |
| Max Velocity through Gate 1 (fps)             | N/A              | N/A              | 11              | 13              | 12              | 11              | 11              | 10              | 8               |
| Max Velocity through Gate 2 (fps)             | N/A              | N/A              | 12              | 14              | 14              | 14              | 13              | 13              | 13              |
| Time to Drain 97% of Inflow Volume (hours)    | 0.85             | 0.17             | 0.93            | 0.96            | 1.00            | 1.02            | 1.08            | 1.11            | 1.13            |
| Time to Drain 99% of Inflow Volume (hours)    | 0.02             | 0.01             | 0.02            | 0.02            | 0.02            | 0.02            | 0.02            | 0.02            | 0.02            |
| Maximum Ponding Depth (ft)                    | 0.010            | 0.001            | 0.011           | 0.012           | 0.013           | 0.013           | 0.014           | 0.014           | 0.015           |
| Area at Maximum Ponding Depth (acres)         |                  |                  |                 |                 |                 |                 |                 |                 |                 |
| Maximum Volume Stored (acre-ft)               |                  |                  |                 |                 |                 |                 |                 |                 |                 |

# DETENTION BASIN OUTLET STRUCTURE DESIGN

*MHFD-Detention, Version 4.00 (December 2019)*



| S-A-V-D Chart Axis Override | X-axis | Left Y-Axis | Right Y-Axis |
|-----------------------------|--------|-------------|--------------|
| minimum bound               |        |             |              |
| maximum bound               |        |             |              |

# DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename: \_\_\_\_\_

## Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

| Time Interval | SOURCE  | CUHP       | CUHP       | CUHP         | CUHP         | CUHP          | CUHP          | CUHP          | CUHP           | CUHP           |
|---------------|---------|------------|------------|--------------|--------------|---------------|---------------|---------------|----------------|----------------|
|               | TIME    | WOCV [cfs] | EURV [cfs] | 2 Year [cfs] | 5 Year [cfs] | 10 Year [cfs] | 25 Year [cfs] | 50 Year [cfs] | 100 Year [cfs] | 500 Year [cfs] |
| 5.00 min      | 0:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 0:05:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 0:10:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.01           |
|               | 0:15:00 | 0.00       | 0.00       | 0.03         | 0.05         | 0.06          | 0.04          | 0.05          | 0.05           | 0.07           |
|               | 0:20:00 | 0.00       | 0.00       | 0.10         | 0.17         | 0.23          | 0.10          | 0.12          | 0.14           | 0.21           |
|               | 0:25:00 | 0.00       | 0.00       | 0.36         | 0.64         | 0.93          | 0.36          | 0.44          | 0.52           | 0.83           |
|               | 0:30:00 | 0.00       | 0.00       | 0.53         | 0.90         | 1.17          | 1.42          | 1.76          | 2.04           | 2.63           |
|               | 0:35:00 | 0.00       | 0.00       | 0.50         | 0.82         | 1.05          | 1.64          | 1.99          | 2.44           | 3.09           |
|               | 0:40:00 | 0.00       | 0.00       | 0.44         | 0.70         | 0.90          | 1.60          | 1.92          | 2.32           | 2.93           |
|               | 0:45:00 | 0.00       | 0.00       | 0.36         | 0.58         | 0.77          | 1.40          | 1.68          | 2.11           | 2.65           |
|               | 0:50:00 | 0.00       | 0.00       | 0.29         | 0.48         | 0.63          | 1.24          | 1.49          | 1.86           | 2.33           |
|               | 0:55:00 | 0.00       | 0.00       | 0.24         | 0.39         | 0.52          | 1.00          | 1.21          | 1.56           | 1.97           |
|               | 1:00:00 | 0.00       | 0.00       | 0.21         | 0.33         | 0.45          | 0.83          | 1.01          | 1.35           | 1.71           |
|               | 1:05:00 | 0.00       | 0.00       | 0.18         | 0.29         | 0.40          | 0.71          | 0.87          | 1.21           | 1.54           |
|               | 1:10:00 | 0.00       | 0.00       | 0.15         | 0.25         | 0.35          | 0.58          | 0.71          | 0.96           | 1.23           |
|               | 1:15:00 | 0.00       | 0.00       | 0.12         | 0.20         | 0.31          | 0.46          | 0.57          | 0.74           | 0.96           |
|               | 1:20:00 | 0.00       | 0.00       | 0.09         | 0.16         | 0.24          | 0.35          | 0.42          | 0.54           | 0.69           |
|               | 1:25:00 | 0.00       | 0.00       | 0.07         | 0.12         | 0.18          | 0.25          | 0.30          | 0.36           | 0.46           |
|               | 1:30:00 | 0.00       | 0.00       | 0.06         | 0.10         | 0.15          | 0.17          | 0.21          | 0.25           | 0.33           |
|               | 1:35:00 | 0.00       | 0.00       | 0.05         | 0.09         | 0.13          | 0.13          | 0.16          | 0.18           | 0.25           |
|               | 1:40:00 | 0.00       | 0.00       | 0.05         | 0.08         | 0.11          | 0.10          | 0.13          | 0.14           | 0.19           |
|               | 1:45:00 | 0.00       | 0.00       | 0.05         | 0.07         | 0.10          | 0.09          | 0.11          | 0.11           | 0.15           |
|               | 1:50:00 | 0.00       | 0.00       | 0.04         | 0.06         | 0.10          | 0.07          | 0.09          | 0.09           | 0.13           |
|               | 1:55:00 | 0.00       | 0.00       | 0.04         | 0.05         | 0.09          | 0.07          | 0.09          | 0.08           | 0.11           |
|               | 2:00:00 | 0.00       | 0.00       | 0.03         | 0.05         | 0.07          | 0.06          | 0.08          | 0.07           | 0.10           |
|               | 2:05:00 | 0.00       | 0.00       | 0.02         | 0.04         | 0.05          | 0.05          | 0.06          | 0.05           | 0.07           |
|               | 2:10:00 | 0.00       | 0.00       | 0.02         | 0.03         | 0.04          | 0.03          | 0.04          | 0.04           | 0.05           |
|               | 2:15:00 | 0.00       | 0.00       | 0.01         | 0.02         | 0.03          | 0.02          | 0.03          | 0.03           | 0.04           |
|               | 2:20:00 | 0.00       | 0.00       | 0.01         | 0.01         | 0.02          | 0.02          | 0.02          | 0.02           | 0.03           |
|               | 2:25:00 | 0.00       | 0.00       | 0.01         | 0.01         | 0.01          | 0.01          | 0.01          | 0.01           | 0.02           |
|               | 2:30:00 | 0.00       | 0.00       | 0.00         | 0.01         | 0.01          | 0.01          | 0.01          | 0.01           | 0.01           |
|               | 2:35:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.01          | 0.01          | 0.01          | 0.01           | 0.01           |
|               | 2:40:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.01           |
|               | 2:45:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 2:50:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 2:55:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:05:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:10:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:15:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:20:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:25:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:30:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:35:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:40:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:45:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:50:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:55:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:05:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:10:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:15:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:20:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:25:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:30:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:35:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:40:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:45:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:50:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:55:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:05:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:10:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:15:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:20:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:25:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:30:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:35:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:40:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:45:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:50:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:55:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 6:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |

## FOREBAY VOLUME REQUIREMENTS

Equation 3-1  $WQCV = a(0.91I^3 - 1.19I^2 + 0.781I)$   
 $a=1$  (40 hour drain time)

|                  |             |                    |
|------------------|-------------|--------------------|
| Pond 2 Forebay 1 | $I = .6137$ | $WQCV = 0.2408332$ |
| Pond 2 Forebay 2 | $I = .6531$ | $WQCV = 0.2553373$ |
| Pond 4 Forebay   | $I = .7084$ | $WQCV = 0.2788757$ |

Equation 3-3  $V = (WQCV/12)A$

|                  |                  |              |
|------------------|------------------|--------------|
| Pond 2 Forebay 1 | $A = 12.9$ Acres | $V = 0.2589$ |
| Pond 2 Forebay 2 | $A = 12.3$ Acres | $V = 0.2617$ |
| Pond 4 Forebay   | $A = 1.07$ Acres | $V = 0.0249$ |

3% OF WQCV  
 FOREBAY TOTAL VOLUME =  $.03(V)$

|   |        |       |        |
|---|--------|-------|--------|
| Volume Required For Pond P2 Forebay 1 = | 0.0078 | AC-FT | 338 CF |
| Volume Required For Pond P2 Forebay 2 = | 0.0079 | AC-FT | 342 CF |
| Volume Required For Pond 4 Forebay =    | 0.0007 | AC-FT | 32 CF  |

|   |     |    |
|---|-----|----|
| Volume Provided For Pond P2 Forebay 1 = | 366 | CF |
| Volume Provided For Pond P2 Forebay 2 = | 404 | CF |
| Volume Provided For Pond 4 Forebay =    | 74  | CF |

|                            |  |
|----------------------------|--|
| $Q_{100}$ Discharges       | 2% OF $Q_{100}$                              |
| $Q_{100}$ P2 Forebay 1 =   | $.02 * 41.7 \text{ CFS} = 0.834 \text{ CFS}$ |
| $Q_{100}$ P2 Forebay 2 =   | $.02 * 99.6 \text{ CFS} = 1.99 \text{ CFS}$  |
| $Q_{100}$ Pond 4 Forebay = | $.02 * 6.1 \text{ CFS} = 0.122 \text{ CFS}$  |

# Weir Report

## Pond P2 Forebay 1 Notch

### Rectangular Weir

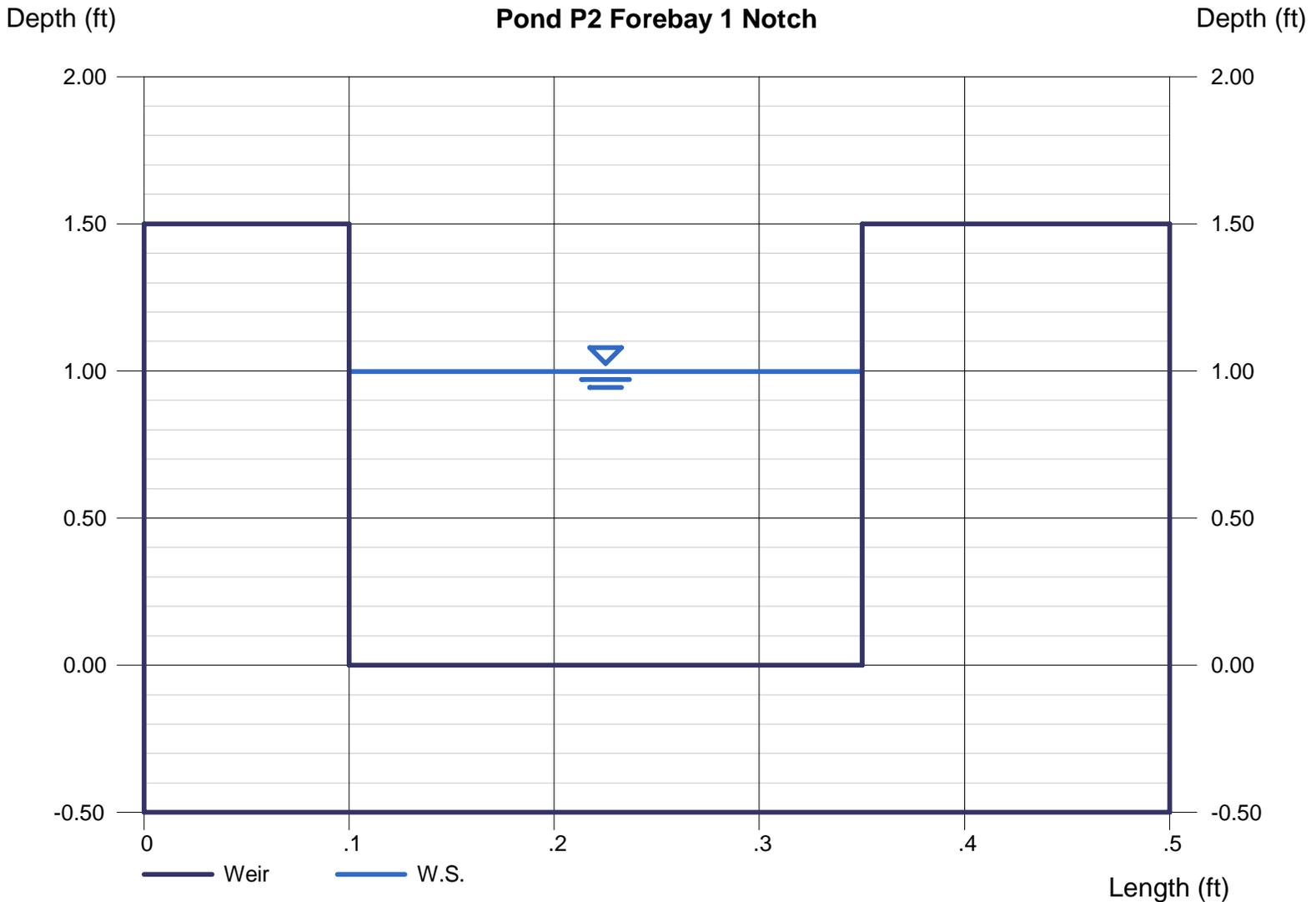
Crest = Sharp  
Bottom Length (ft) = 0.25  
Total Depth (ft) = 1.50

### Highlighted

Depth (ft) = 1.00  
Q (cfs) = 0.830  
Area (sqft) = 0.25  
Velocity (ft/s) = 3.33  
Top Width (ft) = 0.25

### Calculations

Weir Coeff. Cw = 3.33  
Compute by: Known Q  
Known Q (cfs) = 0.83



# Weir Report

## Pond P2 Forebay 2 Notch

### Rectangular Weir

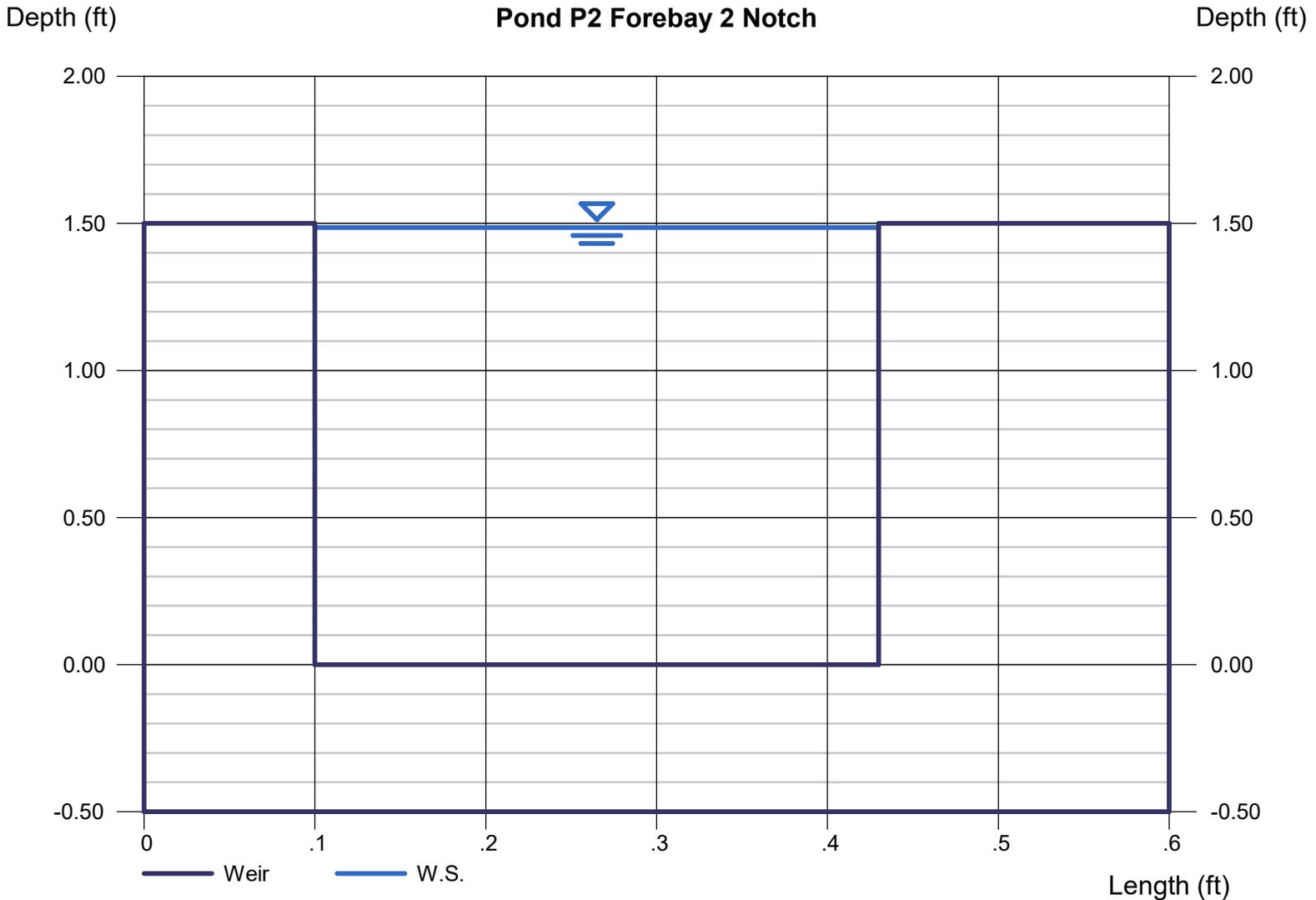
Crest = Sharp  
Bottom Length (ft) = 0.33  
Total Depth (ft) = 1.50

### Highlighted

Depth (ft) = 1.49  
Q (cfs) = 1.990  
Area (sqft) = 0.49  
Velocity (ft/s) = 4.06  
Top Width (ft) = 0.33

### Calculations

Weir Coeff. Cw = 3.33  
Compute by: Known Q  
Known Q (cfs) = 1.99



# Weir Report

## Pond 4 Forebay Notch

### Rectangular Weir

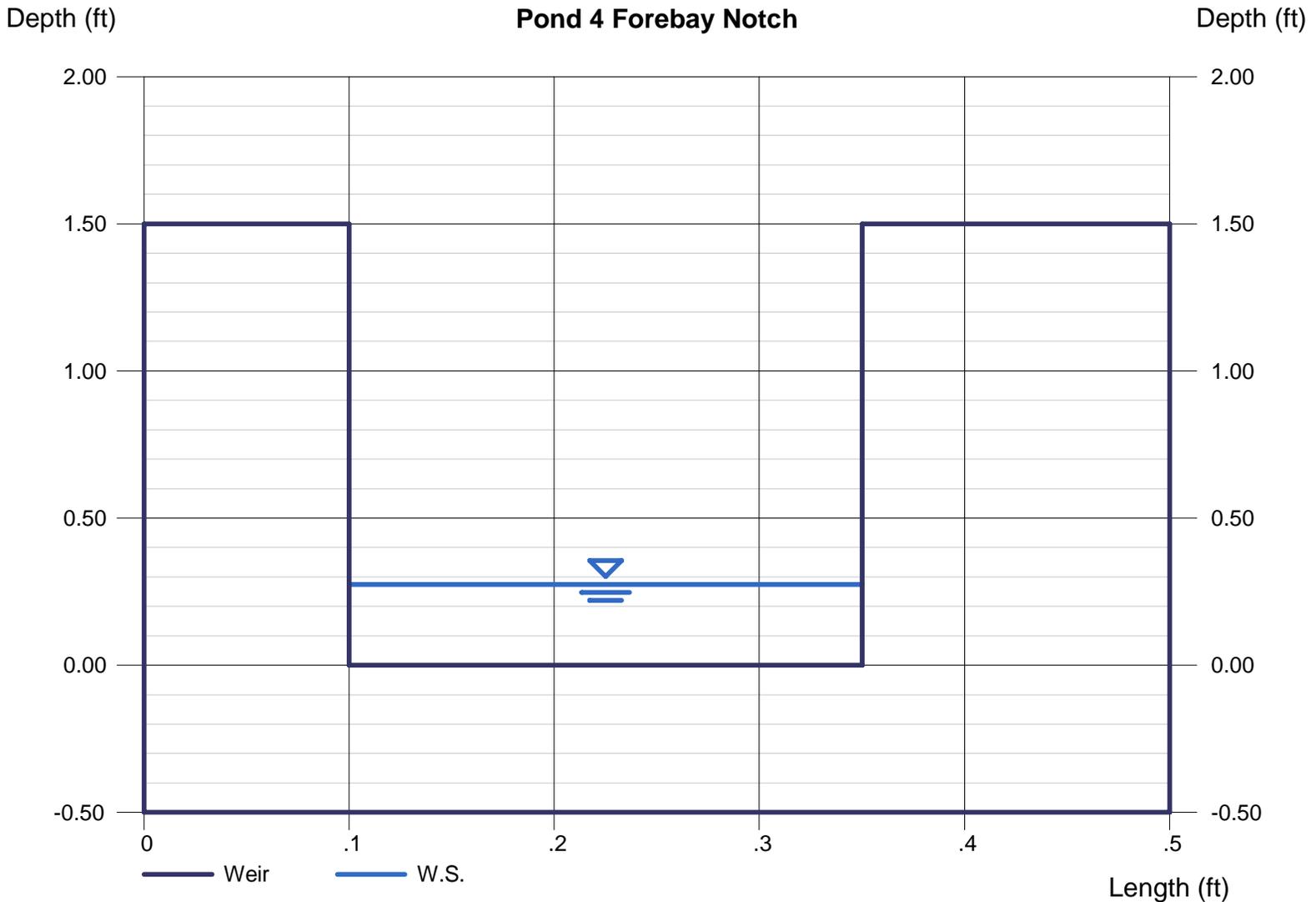
Crest = Sharp  
Bottom Length (ft) = 0.25  
Total Depth (ft) = 1.50

### Highlighted

Depth (ft) = 0.27  
Q (cfs) = 0.120  
Area (sqft) = 0.07  
Velocity (ft/s) = 1.75  
Top Width (ft) = 0.25

### Calculations

Weir Coeff. Cw = 3.33  
Compute by: Known Q  
Known Q (cfs) = 0.12



POND 1 SPILLWAY RIPRAP CALCULATION

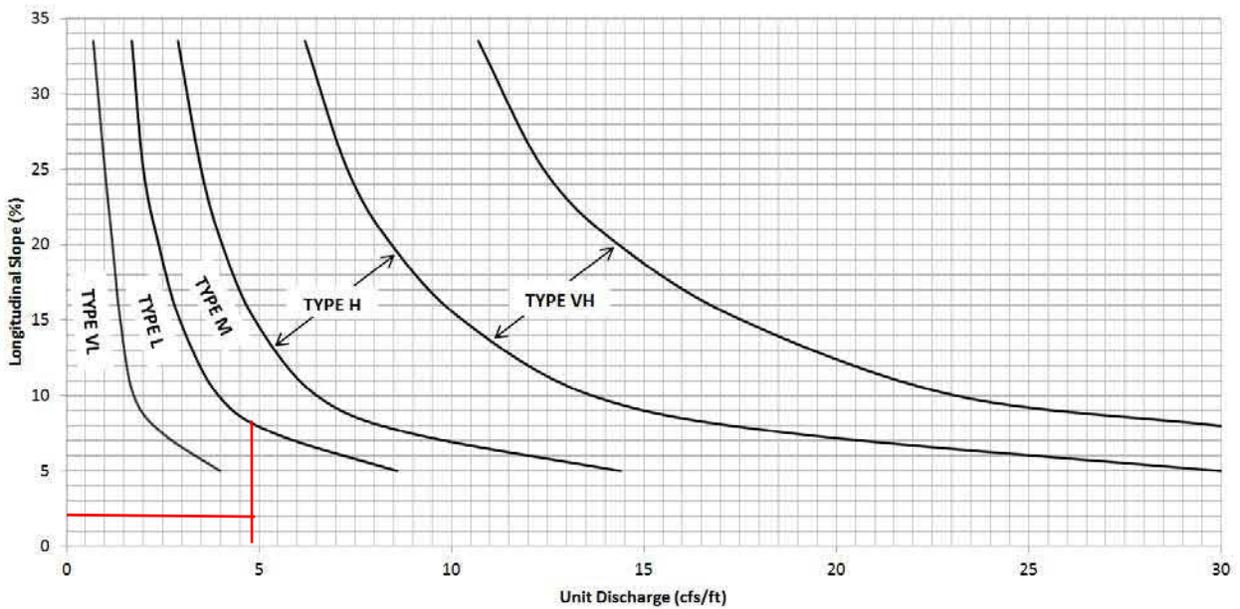
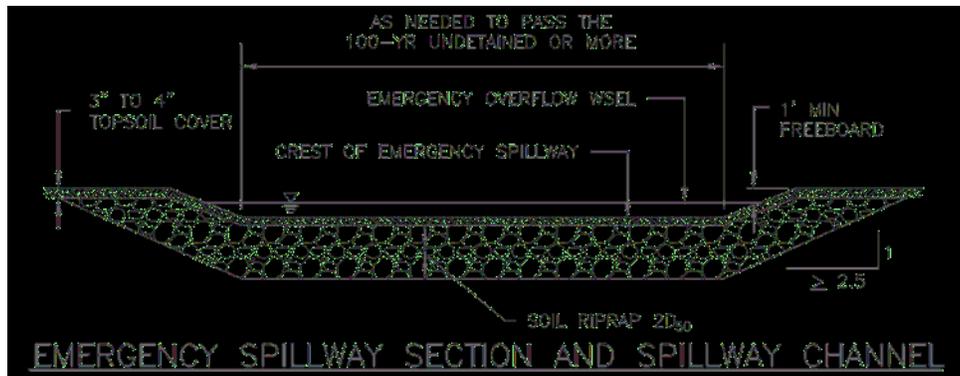
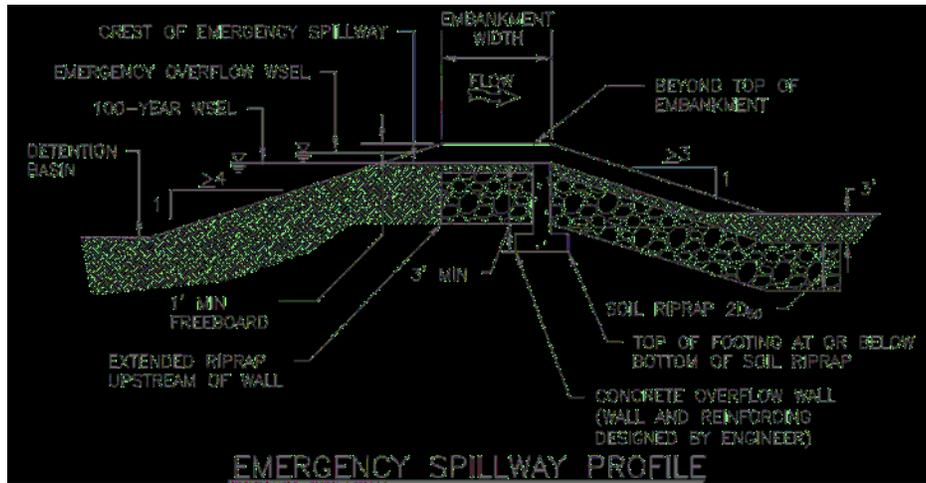


Figure 12-21. Embankment protection details and rock sizing chart (adapted from Arapahoe County)

POND 2 SPILLWAY RIPRAP CALCULATION

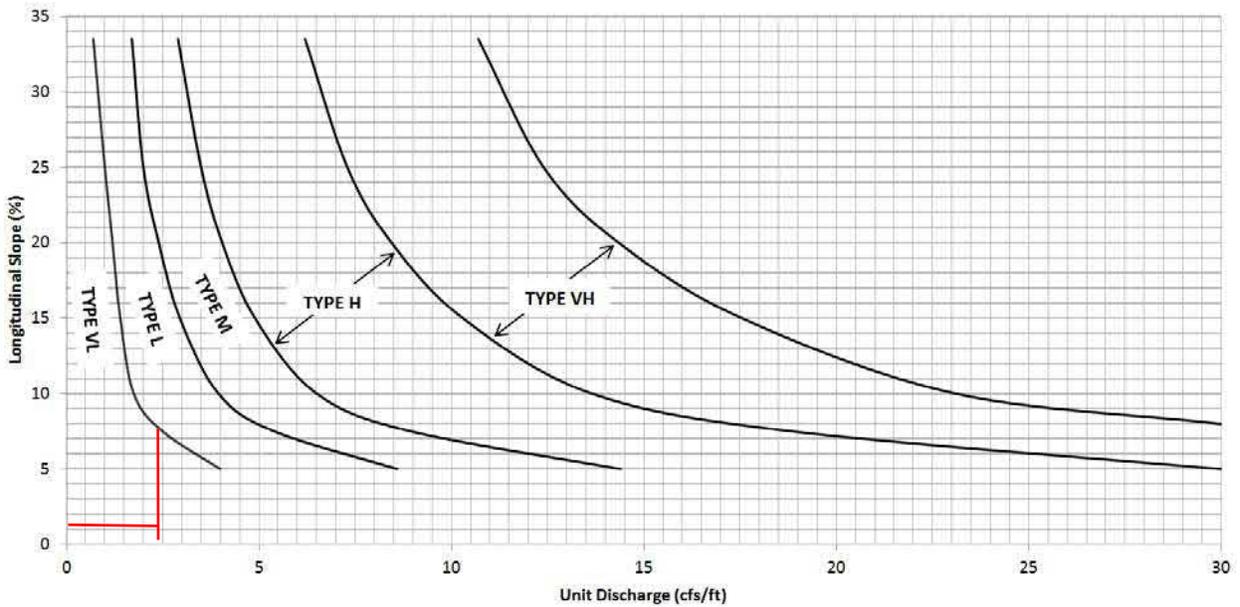
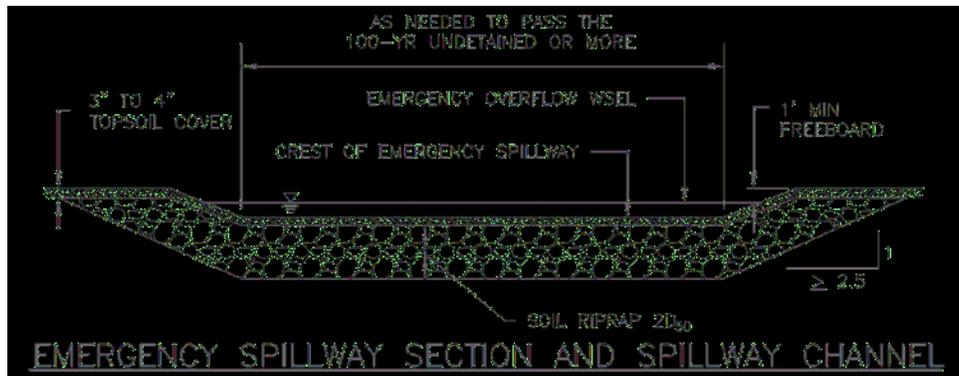
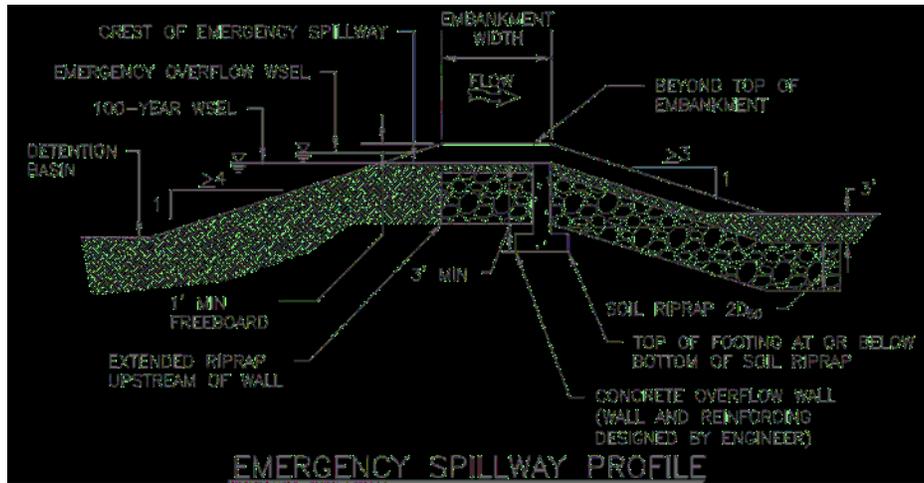


Figure 12-21. Embankment protection details and rock sizing chart (adapted from Arapahoe County)

### POND 3 SPILLWAY RIPRAP CALCULATION

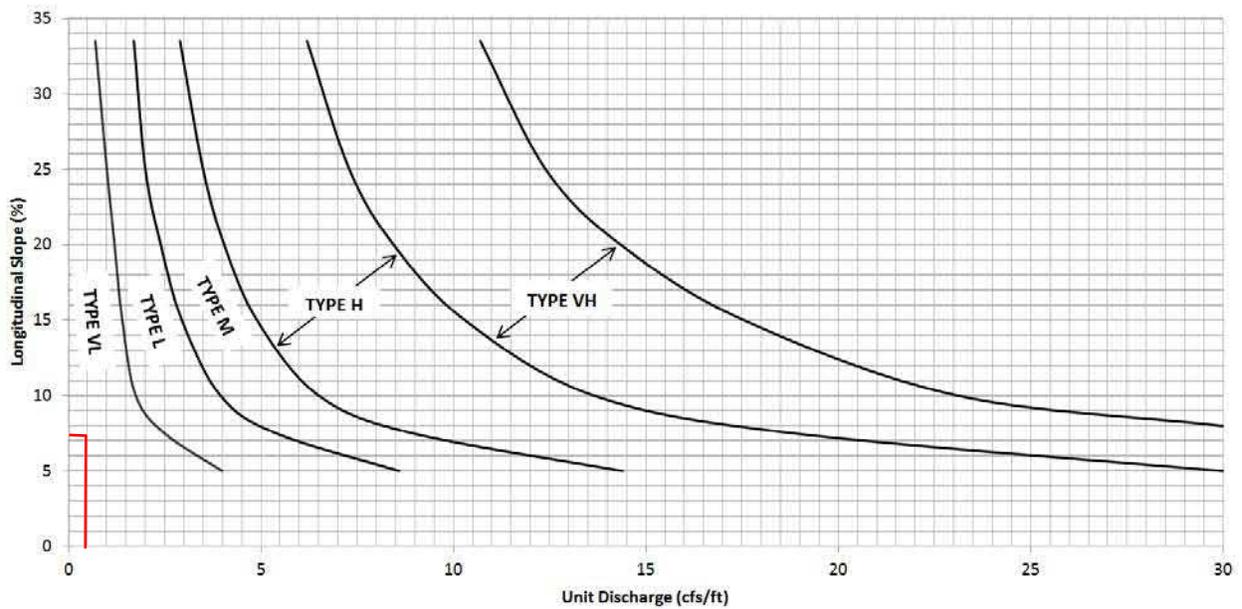
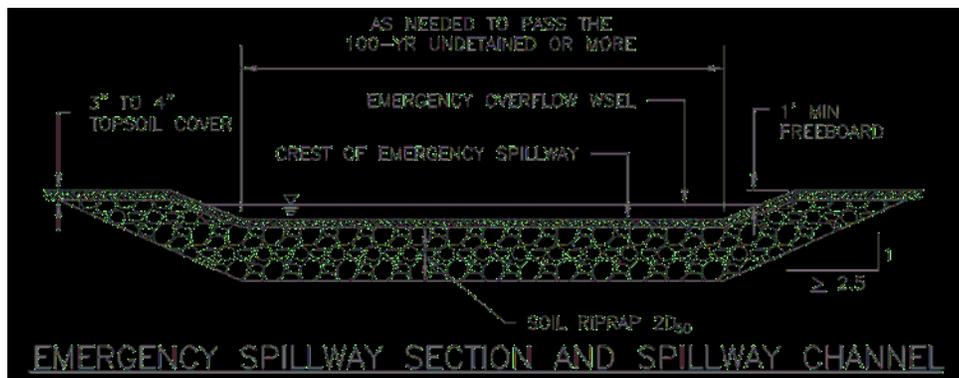
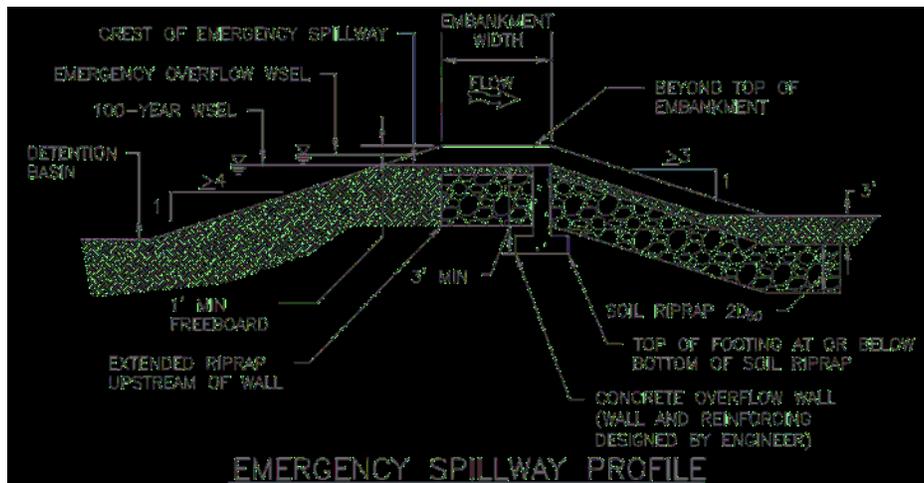


Figure 12-21. Embankment protection details and rock sizing chart (adapted from Arapahoe County)

POND 4 SPILLWAY RIPRAP CALCULATION

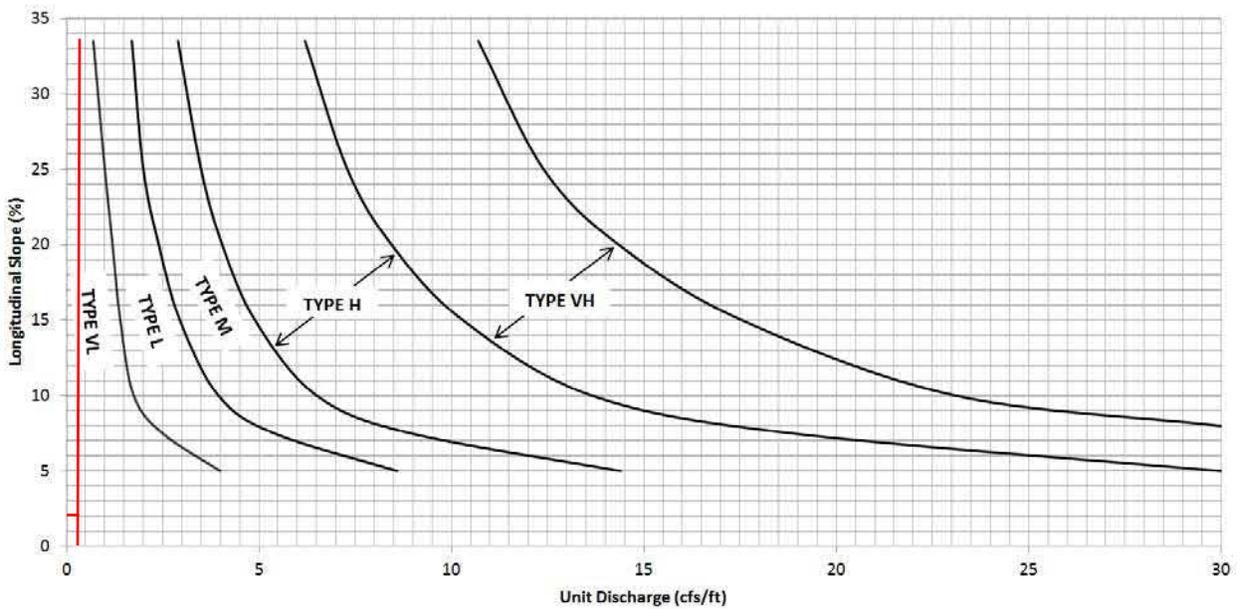
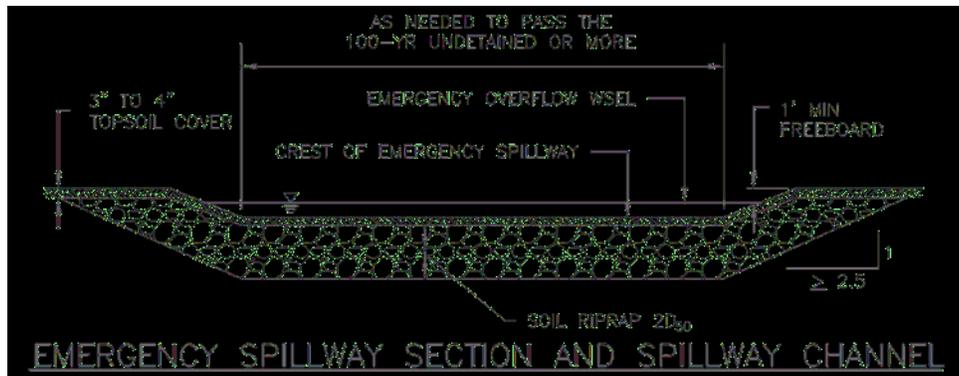
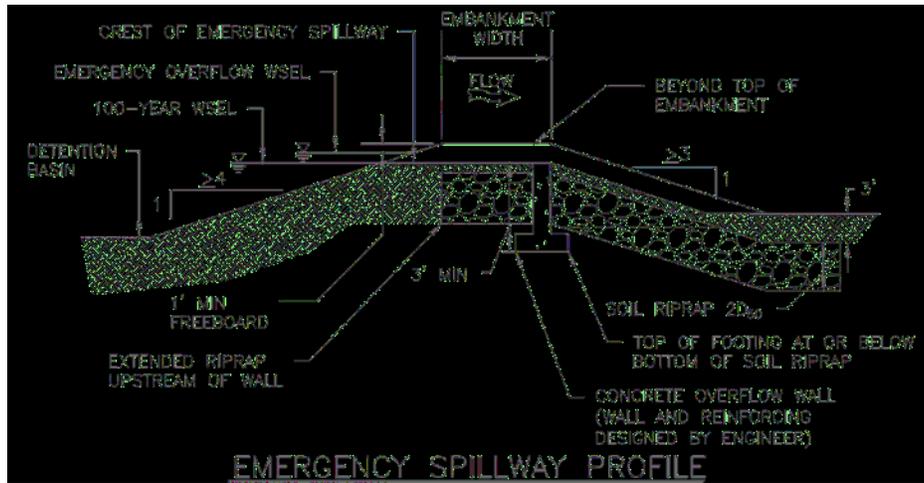


Figure 12-21. Embankment protection details and rock sizing chart (adapted from Arapahoe County)

# Channel Report

## Emergency Overflow - Pond P1 to Pond P2

### User-defined

Invert Elev (ft) = 0.25  
Slope (%) = 3.00  
N-Value = Composite

### Highlighted

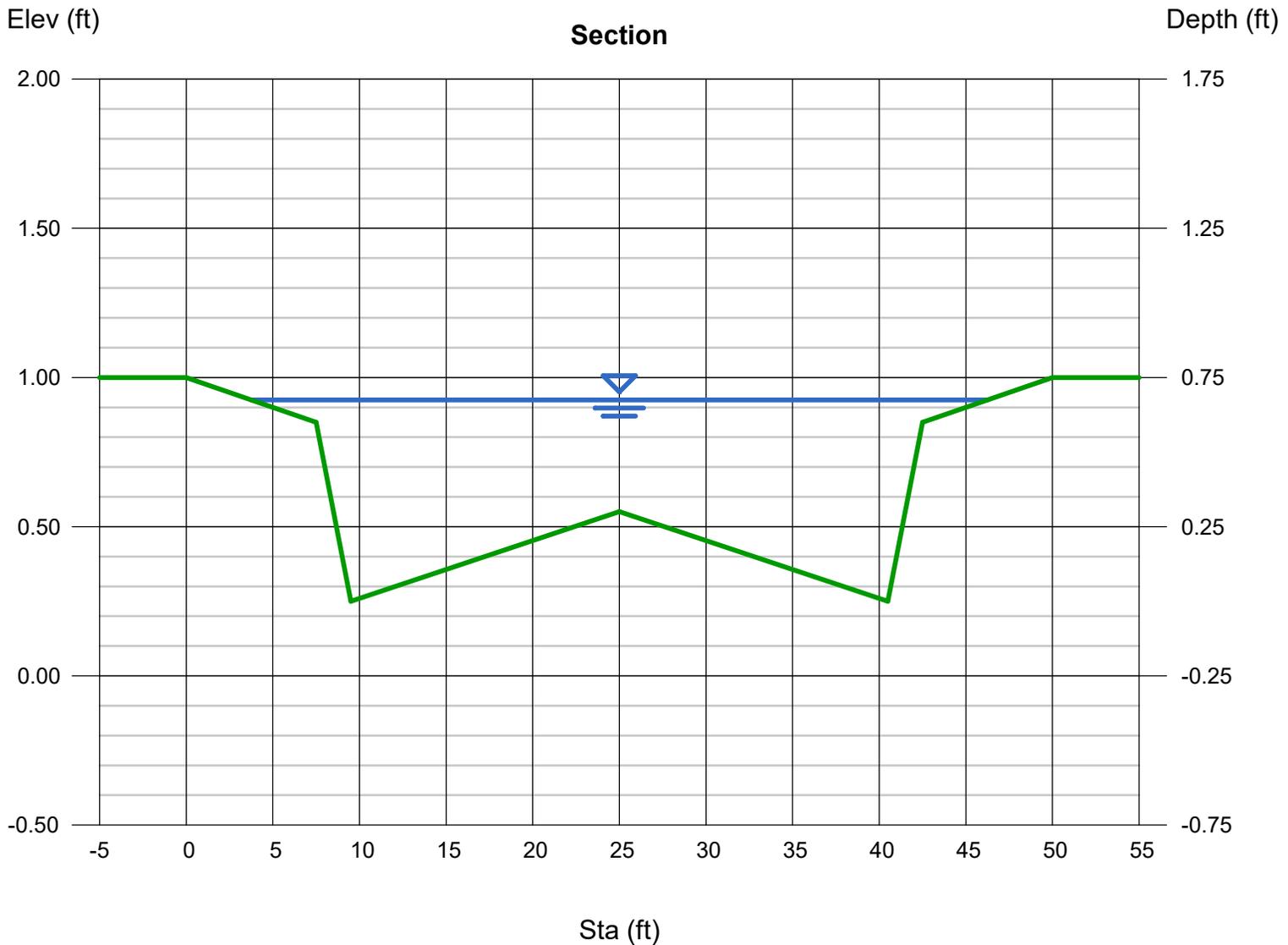
Depth (ft) = 0.68  
Q (cfs) = 158.23  
Area (sqft) = 18.06  
Velocity (ft/s) = 8.76  
Wetted Perim (ft) = 42.68  
Crit Depth, Yc (ft) = 0.75  
Top Width (ft) = 42.50  
EGL (ft) = 1.87

### Calculations

Compute by: Q vs Depth  
No. Increments = 10

### (Sta, El, n)-(Sta, El, n)...

(0.00, 1.00)-(7.50, 0.85, 0.030)-(9.50, 0.25, 0.013)-(25.00, 0.55, 0.013)-(40.50, 0.25, 0.013)-(42.50, 0.85, 0.013)-(50.00, 1.00, 0.030)



# Channel Report

## Emergency Overflow - Pond P2 to Leggins Way

### User-defined

Invert Elev (ft) = 7021.34  
Slope (%) = 5.42  
N-Value = 0.014

### Highlighted

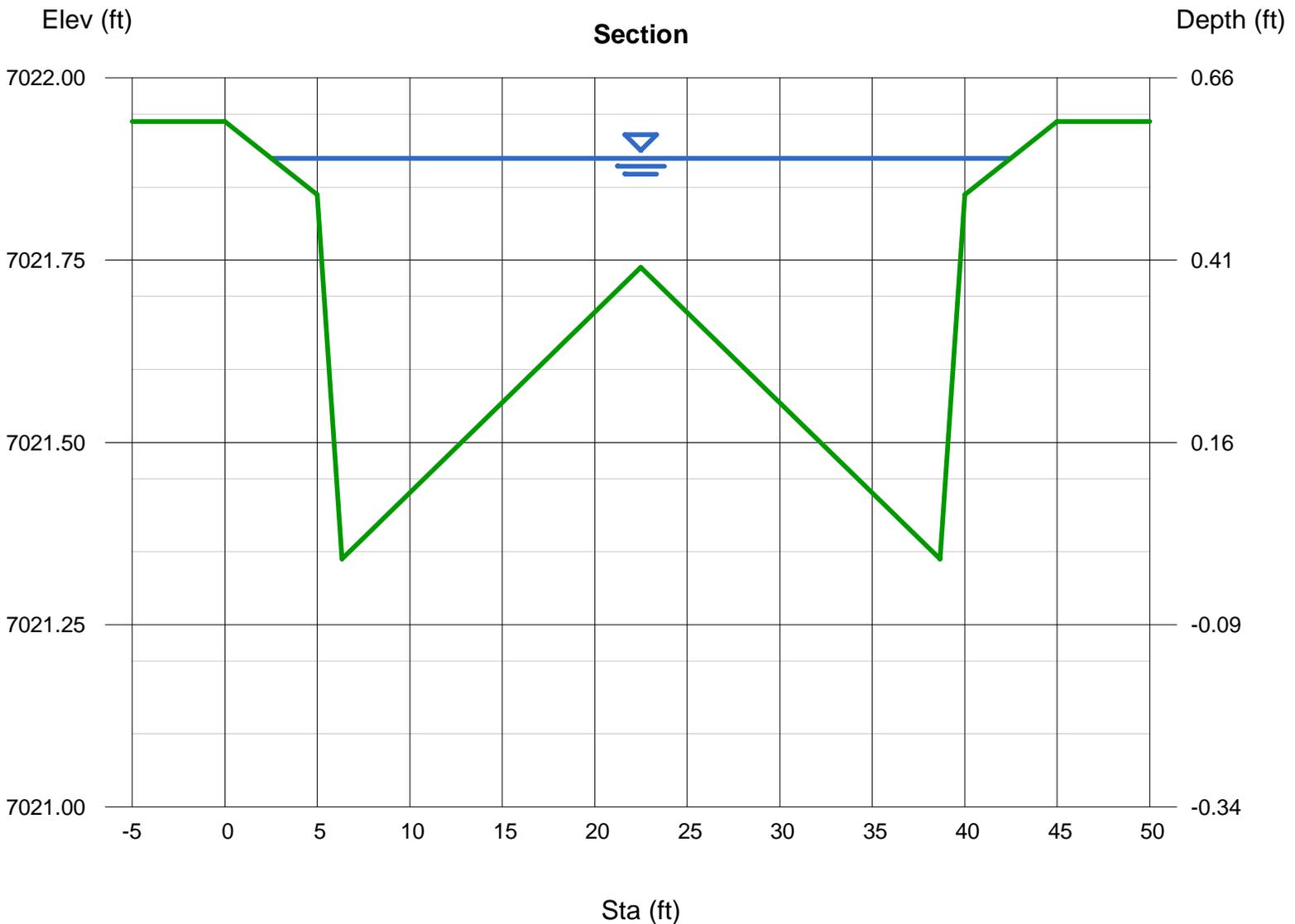
Depth (ft) = 0.55  
Q (cfs) = 130.30  
Area (sqft) = 12.23  
Velocity (ft/s) = 10.66  
Wetted Perim (ft) = 40.17  
Crit Depth, Yc (ft) = 0.60  
Top Width (ft) = 39.98  
EGL (ft) = 2.32

### Calculations

Compute by: Known Q  
Known Q (cfs) = 130.30

### (Sta, El, n)-(Sta, El, n)...

(0.00, 7021.94) -(5.00, 7021.84, 0.013) -(6.33, 7021.34, 0.013) -(22.50, 7021.74, 0.016) -(38.67, 7021.34, 0.013) -(40.00, 7021.84, 0.013) -(45.00, 7021.94, 0.013)



# Channel Report

## Emergency Overflow Into Pond P2

### Trapezoidal

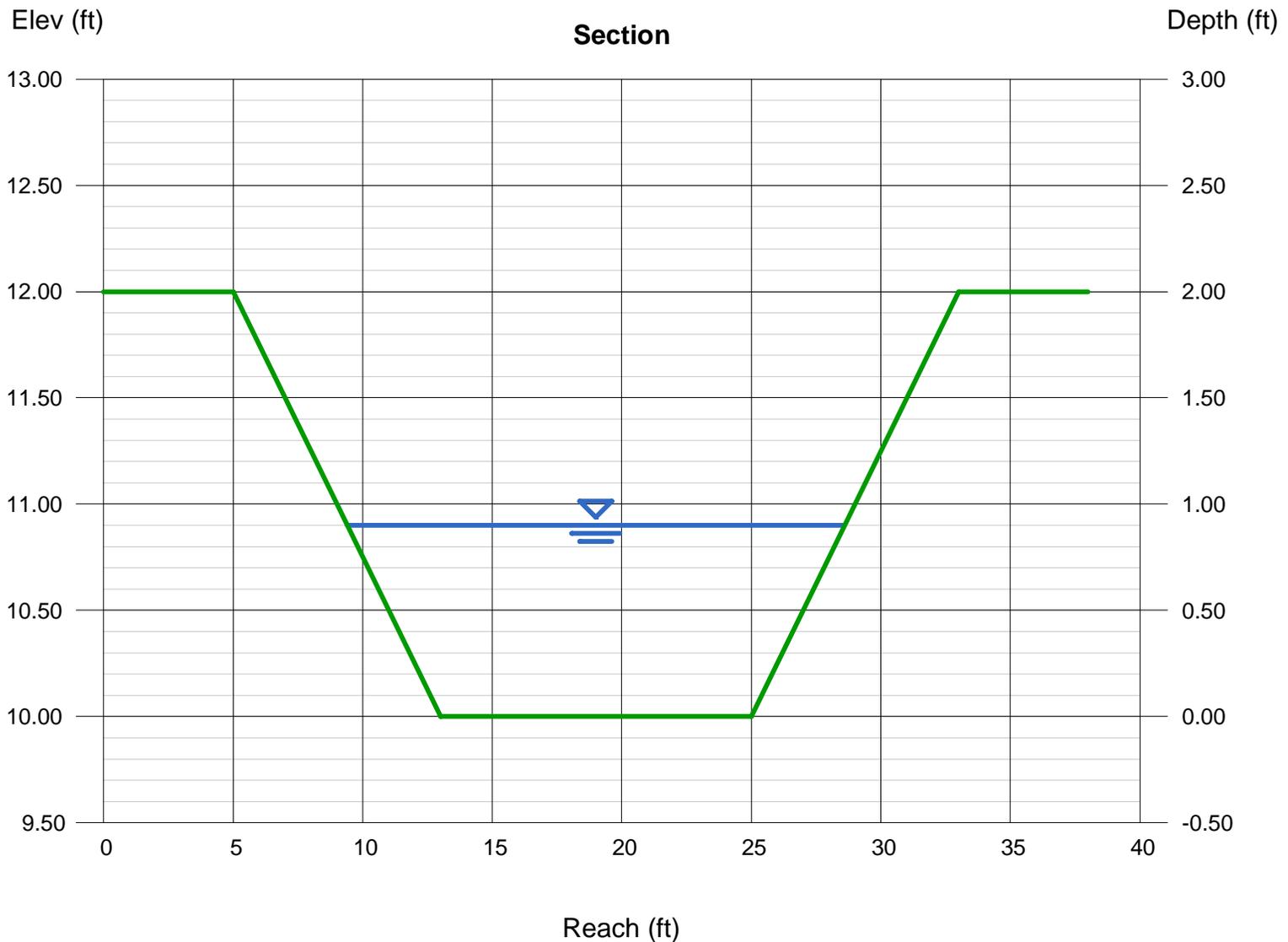
Bottom Width (ft) = 12.00  
Side Slopes (z:1) = 4.00, 4.00  
Total Depth (ft) = 2.00  
Invert Elev (ft) = 10.00  
Slope (%) = 8.00  
N-Value = 0.030

### Highlighted

Depth (ft) = 0.90  
Q (cfs) = 155.80  
Area (sqft) = 14.04  
Velocity (ft/s) = 11.10  
Wetted Perim (ft) = 19.42  
Crit Depth, Yc (ft) = 1.47  
Top Width (ft) = 19.20  
EGL (ft) = 2.81

### Calculations

Compute by: Known Q  
Known Q (cfs) = 155.80



**USACE Steep slope Method (2%-20% Channel Slope)**

**Emergency Overflow into Pond P2**

|                         |                          |
|-------------------------|--------------------------|
| Slope of Bed            | 0.08 ft/ft               |
| Bottom width of Channel | 12 ft                    |
| Channel Flow            | 155.8 ft <sup>3</sup> /S |
| Gravity constant (g)    | 32.2 ft/s                |
| Unit Discharge (q)      | 16.22917                 |
| d30                     | 0.967153                 |
| D30 INCHES              | 11.60583                 |

In cases where unit discharge is low, riprap can be used on steep slopes ranging from 2 to 20 percent. A typical application is a rock-lined chute. The stone size equation is

$$D_{30} = \frac{1.95 S^{0.555} q^{2/3}}{g^{1/3}} \quad (3-5)$$

where

$S$  = slope of bed

$q$  = unit discharge

Equation 3-5 is applicable to thickness = 1.5  $D_{100}$ , angular rock, unit weight of 167 pcf,  $D_{85}/D_{15}$  from 1.7 to 2.7, slopes from 2 to 20 percent, and uniform flow on a down-slope with no tailwater. The following steps should be used in application of Equation 3-5:

- (1) Estimate  $q = Q/b$  where  $b$  = bottom width of chute.
- (2) Multiply  $q$  by flow concentration factor of 1.25. Use greater factor if approach flow is skewed.
- (3) Compute  $D_{30}$  using Equation 3-5.
- (4) Use uniform gradation having  $D_{85}/D_{15} \leq 2$  such as Table 3-1.
- (5) Restrict application to straight channels with side slope of 1V:2.5H or flatter.
- (6) Use filter fabric beneath rock.

The guidance for steep slope riprap generally results in large riprap sizes. Grouted riprap is often used instead of loose riprap in steep slope applications. \*

| RIPRAP DESIGNATION | % SMALLER THAN GIVEN SIZE BY WEIGHT | INTERMEDIATE ROCK DIMENSION (INCHES) | $D_{50}$ * (INCHES) |
|--------------------|-------------------------------------|--------------------------------------|---------------------|
| TYPE VL            | 70 - 100                            | 12                                   | 6                   |
|                    | 50 - 70                             | 9                                    |                     |
|                    | 35 - 50                             | 6                                    |                     |
|                    | 2 - 10                              | 2                                    |                     |
| TYPE L             | 70 - 100                            | 15                                   | 9                   |
|                    | 50 - 70                             | 12                                   |                     |
|                    | 35 - 50                             | 9                                    |                     |
|                    | 2 - 10                              | 3                                    |                     |
| TYPE M             | 70 - 100                            | 21                                   | 12                  |
|                    | 50 - 70                             | 18                                   |                     |
|                    | 35 - 50                             | 12                                   |                     |
|                    | 2 - 10                              | 4                                    |                     |
| TYPE H             | 70 - 100                            | 30                                   | 18                  |
|                    | 50 - 70                             | 24                                   |                     |
|                    | 35 - 50                             | 18                                   |                     |
|                    | 2 - 10                              | 6                                    |                     |

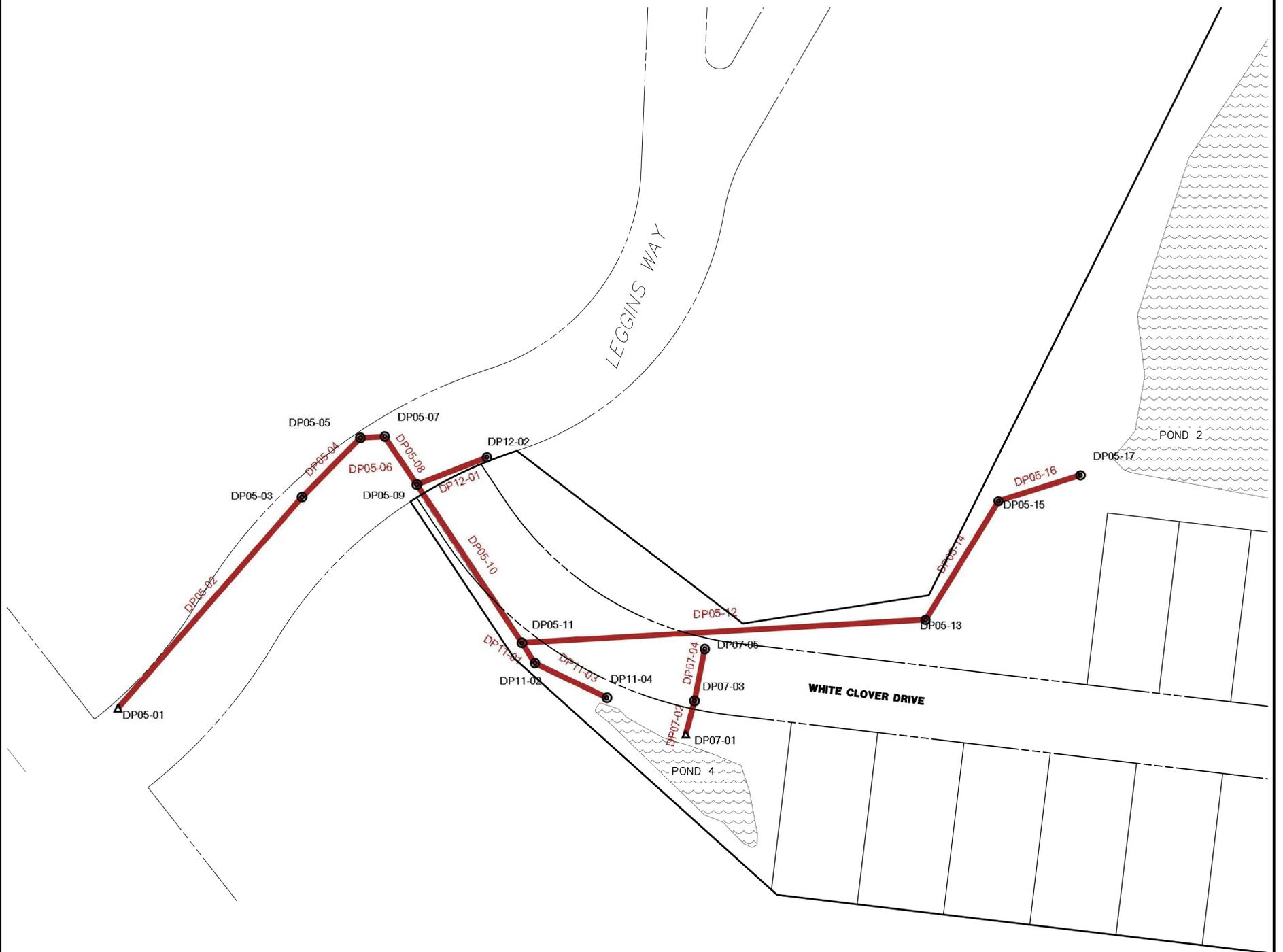
\* $D_{50}$  = MEAN ROCK SIZE

NOTE: MIX ON SITE AND PRIOR TO PLACEMENT

Use Type M Riprap

# CLOVERLEAF FILING 2

## STORMCAD MAP 1



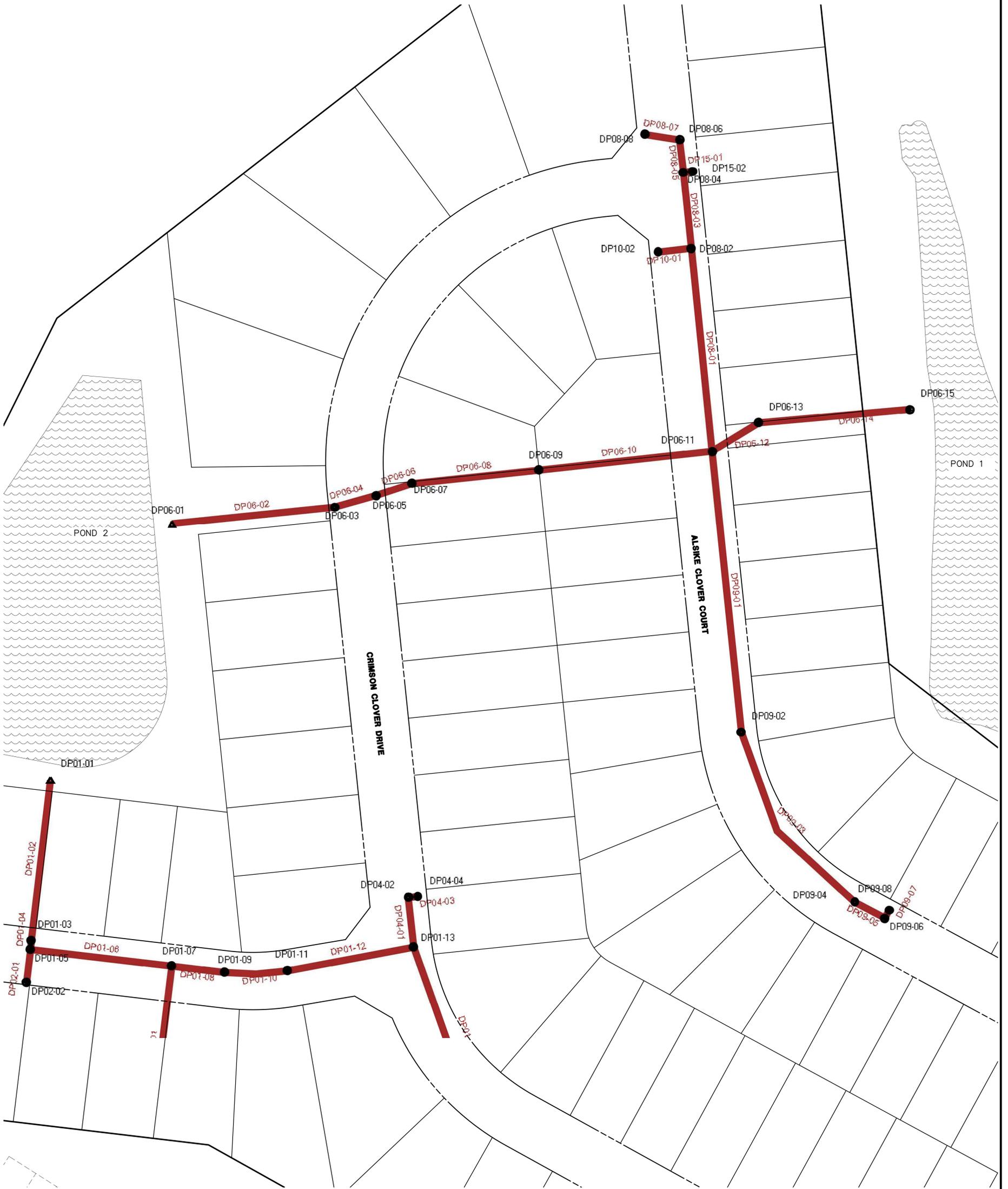
STORMCAD MAP 1  
CLOVERLEAF FILING 2  
2000-5158.01  
08/20/2021  
SHEET 1 OF 4



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# CLOVERLEAF FILING 2

## STORMCAD MAP 2



40 20 0 40 80  
ORIGINAL SCALE: 1" = 40'

STORMCAD MAP 2  
CLOVERLEAF FILING 2  
2000-5158.01  
08/20/2021  
SHEET 2 OF 4

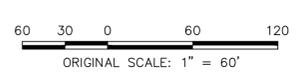
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X:\2010\000\20115801\Drawings\Presentations\2021-08-20\_StormCAD-Map.dwg, PDF2, 8/20/2021 11:48:40 AM, CS

# CLOVERLEAF FILING 2

## STORMCAD MAP 3



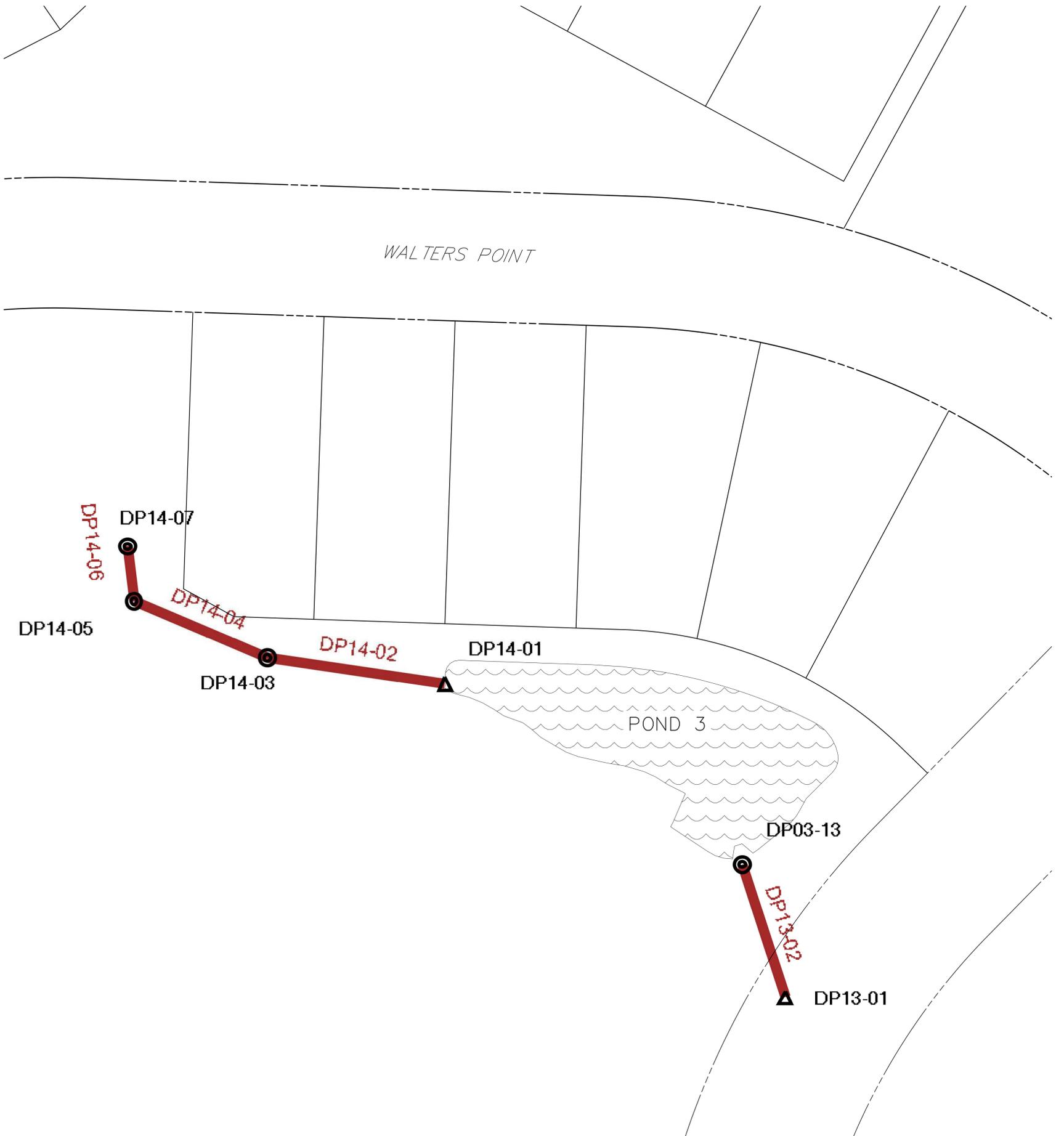
STORMCAD MAP 3  
CLOVERLEAF FILING 2  
JOB NO. 2000-5158.01  
08/20/2021  
SHEET 3 OF 4



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# CLOVERLEAF FILING 2

## STORMCAD MAP 4



STORMCAD MAP 4  
CLOVERLEAF FILING 2  
JOB NO. 2000-5158.01  
08/20/2021  
SHEET 4 OF 4



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**Scenario: 5-YR**  
**Current Time Step: 0.000 h**  
**Conduit FlexTable: Combined Pipe/Node Report**

| Upstream Structure | Label   | Flow (cfs) | Capacity (Full Flow) (cfs) | Diameter (in) | Length (User Defined) (ft) | Slope (Calculated) (ft/ft) | Velocity (ft/s) | Invert (Start) (ft) | Invert (Stop) (ft) | Elevation Ground (Start) (ft) | Elevation Ground (Stop) (ft) | Hydraulic Grade Line (In) (ft) | Hydraulic Grade Line (Out) (ft) | Energy Grade Line (In) (ft) | Energy Grade Line (Out) (ft) | Upstream Structure Headloss Coefficient | Manning's n |
|--------------------|---------|------------|----------------------------|---------------|----------------------------|----------------------------|-----------------|---------------------|--------------------|-------------------------------|------------------------------|--------------------------------|---------------------------------|-----------------------------|------------------------------|---|-------------|
| DP01-03            | DP01-02 | 20.80      | 72.58                      | 36.0          | 139.8                      | 0.012                      | 8.86            | 7,025.83            | 7,024.17           | 7,034.33                      | 7,027.51                     | 7,027.29                       | 7,025.27                        | 7,027.87                    | 7,026.49                     | 0.050                                   | 0.013       |
| DP01-05            | DP01-04 | 20.10      | 81.68                      | 36.0          | 7.8                        | 0.015                      | 9.56            | 7,026.05            | 7,025.94           | 7,034.02                      | 7,034.33                     | 7,027.49                       | 7,027.17                        | 7,028.05                    | 7,028.00                     | 1.020                                   | 0.013       |
| DP01-07            | DP01-06 | 16.70      | 47.16                      | 36.0          | 122.5                      | 0.005                      | 6.10            | 7,026.97            | 7,026.35           | 7,040.66                      | 7,034.02                     | 7,028.27                       | 7,028.06                        | 7,028.77                    | 7,028.31                     | 1.020                                   | 0.013       |
| DP01-09            | DP01-08 | 13.10      | 87.15                      | 30.0          | 46.0                       | 0.045                      | 12.78           | 7,036.08            | 7,034.01           | 7,043.14                      | 7,040.66                     | 7,037.30                       | 7,034.72                        | 7,037.77                    | 7,036.76                     | 0.050                                   | 0.013       |
| DP01-11            | DP01-10 | 13.10      | 87.15                      | 30.0          | 54.5                       | 0.045                      | 12.78           | 7,038.64            | 7,036.18           | 7,045.71                      | 7,043.14                     | 7,039.86                       | 7,036.88                        | 7,040.33                    | 7,039.03                     | 0.050                                   | 0.013       |
| DP01-13            | DP01-12 | 13.10      | 61.05                      | 30.0          | 110.7                      | 0.022                      | 9.91            | 7,041.39            | 7,038.94           | 7,047.66                      | 7,045.71                     | 7,042.61                       | 7,039.73                        | 7,043.08                    | 7,041.25                     | 1.770                                   | 0.013       |
| DP01-15            | DP01-14 | 7.80       | 64.72                      | 30.0          | 182.4                      | 0.025                      | 8.90            | 7,046.23            | 7,041.69           | 7,052.32                      | 7,047.66                     | 7,047.16                       | 7,043.45                        | 7,047.51                    | 7,043.52                     | 0.050                                   | 0.013       |
| DP01-17            | DP01-16 | 7.80       | 65.71                      | 30.0          | 323.4                      | 0.026                      | 9.00            | 7,054.73            | 7,046.43           | 7,060.80                      | 7,052.32                     | 7,055.66                       | 7,047.02                        | 7,056.01                    | 7,048.27                     | 0.100                                   | 0.013       |
| DP01-19            | DP01-18 | 7.80       | 89.92                      | 30.0          | 210.8                      | 0.048                      | 11.24           | 7,064.96            | 7,054.83           | 7,070.53                      | 7,060.80                     | 7,065.89                       | 7,055.33                        | 7,066.24                    | 7,057.29                     | 1.320                                   | 0.013       |
| DP01-21            | DP01-20 | 7.80       | 41.91                      | 30.0          | 27.3                       | 0.010                      | 6.53            | 7,065.55            | 7,065.26           | 7,070.83                      | 7,070.53                     | 7,066.47                       | 7,066.35                        | 7,066.82                    | 7,066.57                     | 0.000                                   | 0.013       |
| DP02-02            | DP02-01 | 4.40       | 30.33                      | 18.0          | 28.9                       | 0.083                      | 12.23           | 7,030.27            | 7,027.85           | 7,034.34                      | 7,034.02                     | 7,031.07                       | 7,028.27                        | 7,031.39                    | 7,030.21                     | 0.000                                   | 0.013       |
| DP03-02            | DP03-01 | 4.20       | 16.00                      | 24.0          | 145.5                      | 0.005                      | 4.29            | 7,028.69            | 7,027.97           | 7,031.94                      | 7,040.66                     | 7,029.41                       | 7,028.78                        | 7,029.68                    | 7,028.97                     | 0.000                                   | 0.013       |
| DP04-02            | DP04-01 | 5.90       | 7.43                       | 18.0          | 43.3                       | 0.005                      | 4.66            | 7,042.61            | 7,042.39           | 7,047.18                      | 7,047.66                     | 7,043.63                       | 7,043.45                        | 7,043.96                    | 7,043.76                     | 1.320                                   | 0.013       |
| DP04-04            | DP04-03 | 5.90       | 7.43                       | 18.0          | 8.1                        | 0.005                      | 3.34            | 7,042.95            | 7,042.91           | 7,047.18                      | 7,047.50                     | 7,044.14                       | 7,044.07                        | 7,044.37                    | 7,044.34                     | 0.000                                   | 0.013       |
| DP05-03            | DP05-02 | 64.80      | 146.12                     | 48.0          | 191.3                      | 0.010                      | 11.28           | 6,992.35            | 6,990.37           | 7,000.91                      | 6,995.01                     | 6,994.78                       | 6,992.25                        | 6,995.80                    | 6,994.18                     | 0.050                                   | 0.013       |
| DP05-05            | DP05-04 | 64.80      | 168.57                     | 48.0          | 53.0                       | 0.014                      | 12.54           | 6,994.08            | 6,993.35           | 7,002.66                      | 7,000.91                     | 6,996.51                       | 6,995.26                        | 6,997.53                    | 6,997.12                     | 0.400                                   | 0.013       |
| DP05-07            | DP05-06 | 64.80      | 163.91                     | 48.0          | 13.1                       | 0.013                      | 12.28           | 6,995.25            | 6,995.08           | 7,003.44                      | 7,002.66                     | 6,997.68                       | 6,997.20                        | 6,998.70                    | 6,998.63                     | 0.640                                   | 0.013       |
| DP05-09            | DP05-08 | 64.80      | 187.75                     | 48.0          | 38.0                       | 0.017                      | 13.57           | 6,996.90            | 6,996.25           | 7,003.95                      | 7,003.44                     | 6,999.33                       | 6,998.14                        | 7,000.35                    | 7,000.05                     | 1.020                                   | 0.013       |
| DP05-11            | DP05-10 | 63.00      | 227.33                     | 48.0          | 128.9                      | 0.025                      | 15.47           | 7,000.23            | 6,997.00           | 7,006.38                      | 7,003.95                     | 7,002.62                       | 7,000.37                        | 7,003.63                    | 7,000.86                     | 0.640                                   | 0.013       |
| DP05-13            | DP05-12 | 62.70      | 150.89                     | 42.0          | 279.2                      | 0.022                      | 14.96           | 7,006.81            | 7,000.53           | 7,017.53                      | 7,006.38                     | 7,009.30                       | 7,003.27                        | 7,010.44                    | 7,004.21                     | 0.640                                   | 0.013       |
| DP05-15            | DP05-14 | 62.70      | 155.51                     | 42.0          | 96.6                       | 0.024                      | 15.29           | 7,011.92            | 7,009.61           | 7,025.12                      | 7,017.53                     | 7,014.40                       | 7,011.28                        | 7,015.55                    | 7,014.24                     | 0.400                                   | 0.013       |
| DP05-17            | DP05-16 | 62.70      | 159.13                     | 42.0          | 59.3                       | 0.025                      | 15.56           | 7,019.18            | 7,017.70           | 7,023.27                      | 7,025.12                     | 7,021.67                       | 7,019.44                        | 7,022.81                    | 7,022.12                     | 0.000                                   | 0.013       |
| DP06-03            | DP06-02 | 50.80      | 127.25                     | 42.0          | 140.5                      | 0.016                      | 12.48           | 7,027.89            | 7,025.64           | 7,043.80                      | 7,029.73                     | 7,030.12                       | 7,027.23                        | 7,031.08                    | 7,029.48                     | 0.075                                   | 0.013       |
| DP06-05            | DP06-04 | 50.00      | 159.04                     | 42.0          | 35.0                       | 0.025                      | 14.64           | 7,038.10            | 7,037.23           | 7,043.80                      | 7,043.80                     | 7,040.31                       | 7,038.84                        | 7,041.26                    | 7,040.92                     | 0.050                                   | 0.013       |
| DP06-07            | DP06-06 | 49.00      | 159.04                     | 42.0          | 29.4                       | 0.025                      | 14.56           | 7,038.93            | 7,038.20           | 7,044.44                      | 7,043.80                     | 7,041.12                       | 7,039.82                        | 7,042.05                    | 7,041.78                     | 0.075                                   | 0.013       |
| DP06-09            | DP06-08 | 49.00      | 159.04                     | 42.0          | 105.5                      | 0.025                      | 14.56           | 7,041.67            | 7,039.04           | 7,058.13                      | 7,044.44                     | 7,043.86                       | 7,040.45                        | 7,044.79                    | 7,043.26                     | 0.050                                   | 0.013       |
| DP06-11            | DP06-10 | 49.00      | 157.66                     | 42.0          | 148.1                      | 0.025                      | 14.46           | 7,055.55            | 7,051.91           | 7,067.52                      | 7,058.13                     | 7,057.73                       | 7,053.29                        | 7,058.67                    | 7,056.29                     | 1.300                                   | 0.013       |
| DP06-13            | DP06-12 | 45.20      | 123.59                     | 42.0          | 36.2                       | 0.015                      | 11.85           | 7,061.36            | 7,060.81           | 7,067.78                      | 7,067.52                     | 7,063.46                       | 7,062.47                        | 7,064.33                    | 7,064.05                     | 0.075                                   | 0.013       |
| DP06-15            | DP06-14 | 45.20      | 138.70                     | 42.0          | 143.3                      | 0.019                      | 12.89           | 7,064.18            | 7,061.46           | 7,068.27                      | 7,067.78                     | 7,066.28                       | 7,062.87                        | 7,067.16                    | 7,065.28                     | 0.000                                   | 0.013       |
| DP07-03            | DP07-02 | 2.70       | 20.25                      | 18.0          | 24.3                       | 0.037                      | 7.97            | 7,005.82            | 7,004.92           | 7,014.46                      | 7,004.92                     | 7,006.45                       | 7,005.31                        | 7,006.68                    | 7,006.17                     | 0.050                                   | 0.013       |
| DP07-05            | DP07-04 | 1.40       | 20.49                      | 18.0          | 36.7                       | 0.038                      | 6.63            | 7,010.57            | 7,009.17           | 7,014.44                      | 7,014.46                     | 7,011.01                       | 7,009.44                        | 7,011.17                    | 7,010.12                     | 0.000                                   | 0.013       |
| DP08-02            | DP08-01 | 11.60      | 38.02                      | 30.0          | 177.0                      | 0.009                      | 6.80            | 7,058.07            | 7,056.55           | 7,064.95                      | 7,067.52                     | 7,059.21                       | 7,058.95                        | 7,059.65                    | 7,059.04                     | 1.020                                   | 0.013       |
| DP08-04            | DP08-03 | 8.20       | 18.34                      | 24.0          | 66.3                       | 0.007                      | 5.68            | 7,059.00            | 7,058.56           | 7,064.37                      | 7,064.95                     | 7,060.02                       | 7,059.66                        | 7,060.42                    | 7,060.00                     | 1.020                                   | 0.013       |
| DP08-06            | DP08-05 | 2.40       | 13.18                      | 18.0          | 28.6                       | 0.016                      | 5.67            | 7,059.94            | 7,059.49           | 7,064.52                      | 7,064.37                     | 7,060.53                       | 7,060.43                        | 7,060.74                    | 7,060.50                     | 0.980                                   | 0.013       |
| DP08-08            | DP08-07 | 2.40       | 12.47                      | 18.0          | 29.4                       | 0.014                      | 5.45            | 7,060.65            | 7,060.24           | 7,064.83                      | 7,064.52                     | 7,061.24                       | 7,060.69                        | 7,061.46                    | 7,061.14                     | 0.000                                   | 0.013       |
| DP09-02            | DP09-01 | 3.40       | 10.42                      | 18.0          | 244.8                      | 0.010                      | 5.27            | 7,065.22            | 7,062.81           | 7,070.22                      | 7,067.52                     | 7,065.93                       | 7,063.40                        | 7,066.20                    | 7,063.84                     | 0.100                                   | 0.013       |
| DP09-04            | DP09-03 | 3.40       | 11.46                      | 18.0          | 183.8                      | 0.012                      | 5.65            | 7,067.51            | 7,065.33           | 7,072.64                      | 7,070.22                     | 7,068.22                       | 7,065.89                        | 7,068.49                    | 7,066.38                     | 0.100                                   | 0.013       |
| DP09-06            | DP09-05 | 3.40       | 11.17                      | 18.0          | 29.4                       | 0.011                      | 5.55            | 7,067.95            | 7,067.62           | 7,073.01                      | 7,072.64                     | 7,068.65                       | 7,068.19                        | 7,068.92                    | 7,068.65                     | 1.320                                   | 0.013       |
| DP09-08            | DP09-07 | 3.40       | 13.33                      | 18.0          | 8.1                        | 0.016                      | 6.30            | 7,068.37            | 7,068.24           | 7,073.31                      | 7,073.01                     | 7,069.08                       | 7,069.01                        | 7,069.35                    | 7,069.23                     | 0.000                                   | 0.013       |
| DP10-02            | DP10-01 | 3.50       | 24.16                      | 18.0          | 27.4                       | 0.053                      | 9.74            | 7,060.51            | 7,059.06           | 7,065.24                      | 7,064.95                     | 7,061.23                       | 7,059.47                        | 7,061.50                    | 7,060.73                     | 0.000                                   | 0.013       |
| DP11-02            | DP11-01 | 4.00       | 7.85                       | 18.0          | 15.4                       | 0.006                      | 4.46            | 7,002.62            | 7,002.53           | 7,007.08                      | 7,006.38                     | 7,003.39                       | 7,003.29                        | 7,003.69                    | 7,003.60                     | 1.000                                   | 0.013       |
| DP11-04            | DP11-03 | 4.00       | 7.98                       | 18.0          | 56.1                       | 0.006                      | 4.52            | 7,002.93            | 7,002.61           | 7,005.30                      | 7,007.08                     | 7,003.70                       | 7,003.64                        | 7,004.00                    | 7,003.79                     | 0.000                                   | 0.013       |
| DP12-02            | DP12-01 | 5.80       | 23.56                      | 24.0          | 50.7                       | 0.011                      | 6.21            | 7,001.45            | 7,000.90           | 7,004.67                      | 7,003.95                     | 7,002.30                       | 7,001.58                        | 7,002.62                    | 7,002.17                     | 0.000                                   | 0.013       |
| DP03-13            | DP13-02 | 2.70       | 13.85                      | 18.0          | 54.2                       | 0.017                      | 6.08            | 7,049.68            | 7,048.74           | 7,051.49                      | 7,050.45                     | 7,050.31                       | 7,049.19                        | 7,050.54                    | 7,049.76                     | 0.000                                   | 0.013       |
| DP14-03            | DP14-02 | 1.40       | 3.69                       | 12.0          | 69.3                       | 0.011                      | 4.38            | 7,051.43            | 7,050.69           | 7,054.43                      | 7,051.86                     | 7,051.93                       | 7,051.12                        | 7,052.13                    | 7,051.41                     | 0.075                                   | 0.013       |
| DP14-05            | DP14-04 | 1.40       | 3.69                       | 12.0          | 55.8                       | 0.011                      | 4.38            | 7,052.03            | 7,051.43           | 7,054.73                      | 7,054.43                     | 7,052.54                       | 7,051.95                        | 7,052.73                    | 7,052.13                     | 0.640                                   | 0.013       |
| DP14-07            | DP14-06 | 1.40       | 3.69                       | 12.0          | 21.4                       | 0.011                      | 4.38            | 7,052.26            | 7,052.03           | 7,053.43                      | 7,054.73                     | 7,052.76                       | 7,052.66                        | 7,052.96                    | 7,052.77                     | 0.000                                   | 0.013       |
| DP15-02            | DP15-01 | 6.60       | 44.58                      | 24.0          | 7.0                        | 0.039                      | 10.17           | 7,059.57            | 7,059.30           | 7,064.65                      | 7,064.37                     | 7,060.48                       | 7,060.43                        | 7,060.83                    | 7,060.63                     | 0.000                                   | 0.013       |

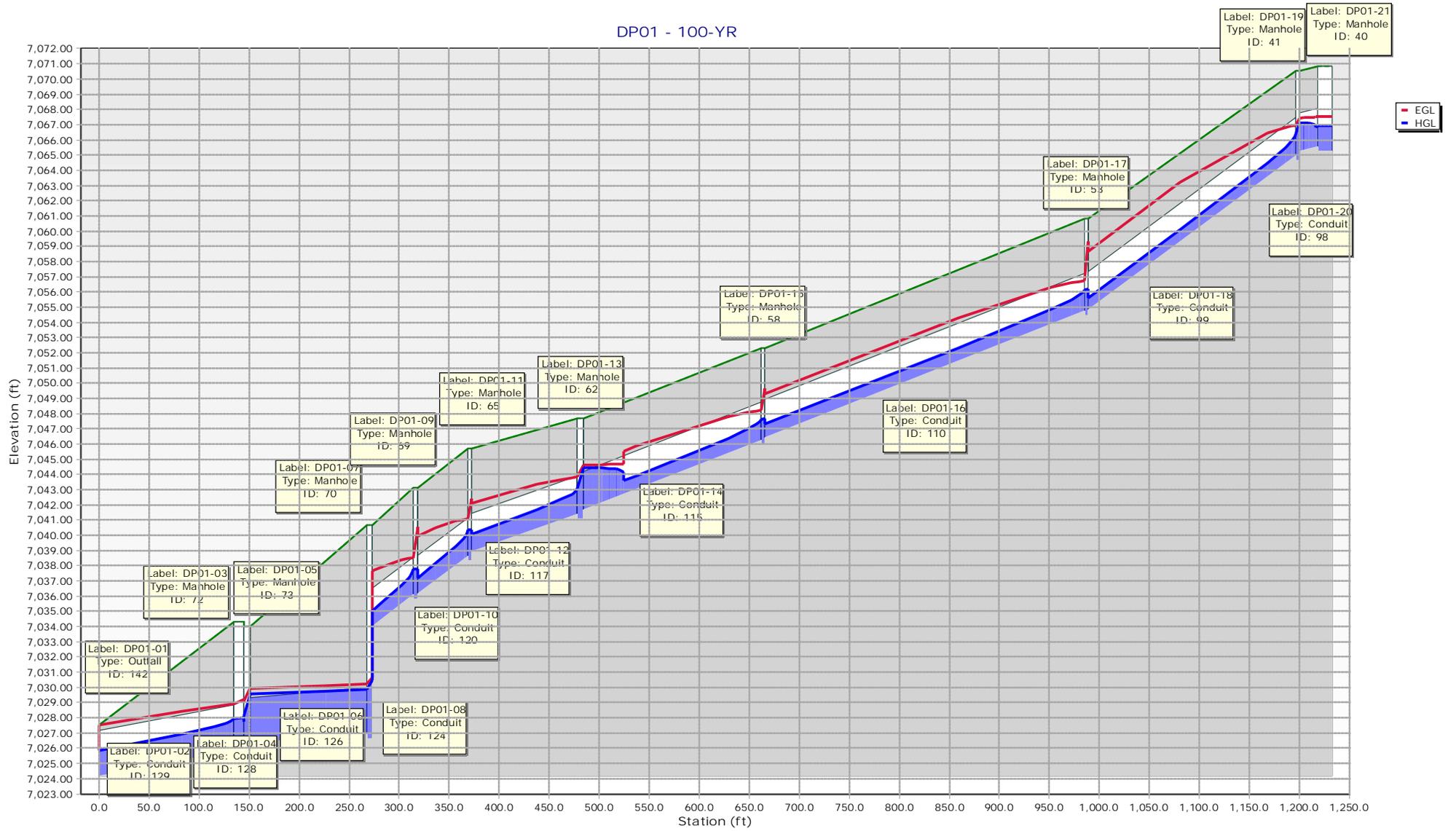
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**Scenario: 100-YR**  
**Current Time Step: 0.000 h**  
**Conduit FlexTable: Combined Pipe/Node Report**

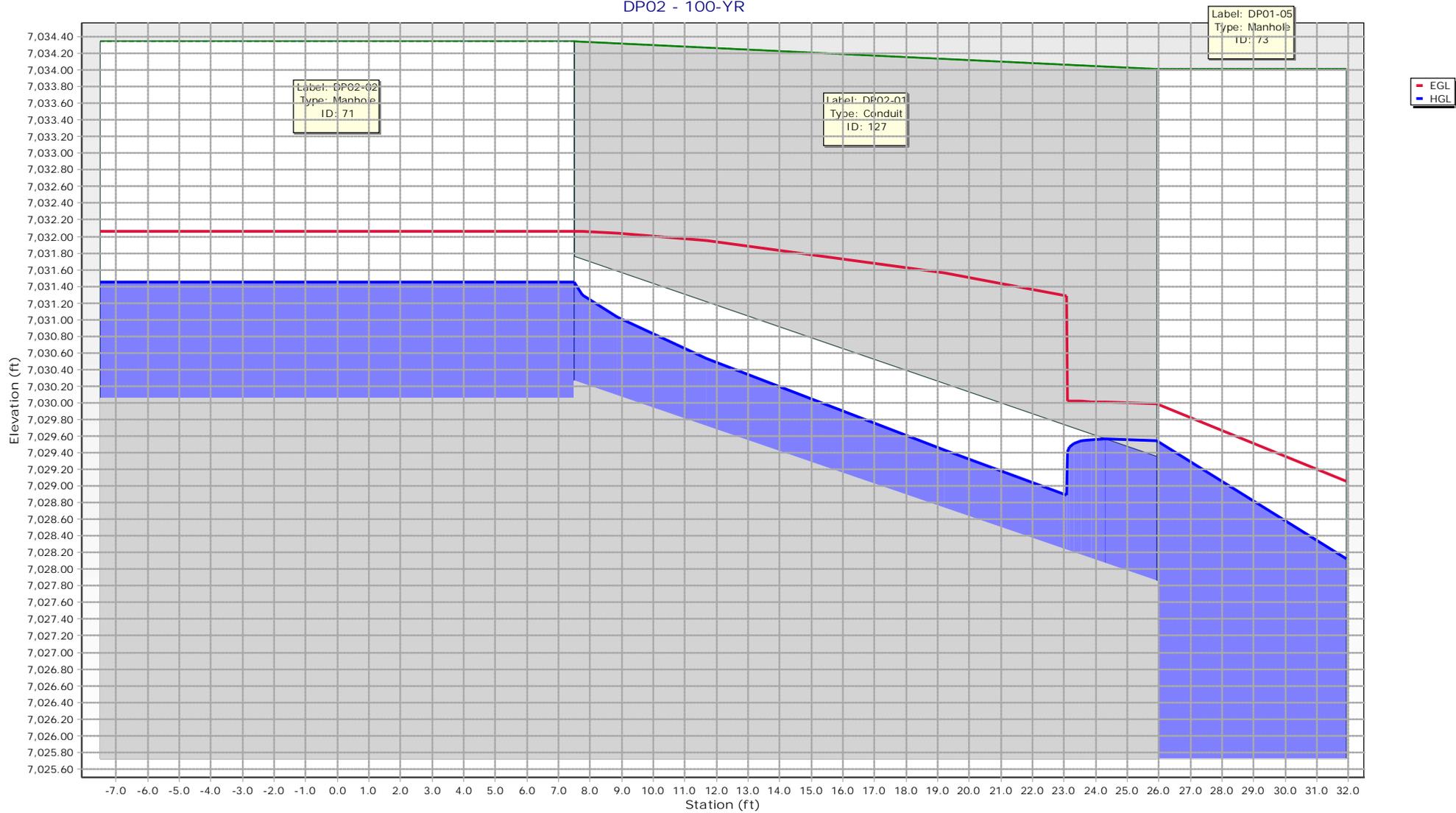
| Upstream Structure | Label   | Flow (cfs) | Capacity (Full Flow) (cfs) | Diameter (in) | Length (User Defined) (ft) | Slope (Calculated) (ft/ft) | Velocity (ft/s) | Invert (Start) (ft) | Invert (Stop) (ft) | Elevation Ground (Start) (ft) | Elevation Ground (Stop) (ft) | Hydraulic Grade Line (In) (ft) | Hydraulic Grade Line (Out) (ft) | Energy Grade Line (In) (ft) | Energy Grade Line (Out) (ft) | Upstream Structure Headloss Coefficient | Manning's n |
|--------------------|---------|------------|----------------------------|---------------|----------------------------|----------------------------|-----------------|---------------------|--------------------|-------------------------------|------------------------------|--------------------------------|---------------------------------|-----------------------------|------------------------------|---|-------------|
| DP01-03            | DP01-02 | 41.70      | 72.58                      | 36.0          | 139.8                      | 0.012                      | 10.62           | 7,025.83            | 7,024.17           | 7,034.33                      | 7,027.51                     | 7,027.93                       | 7,025.82                        | 7,028.90                    | 7,027.53                     | 0.050                                   | 0.013       |
| DP01-05            | DP01-04 | 40.40      | 81.68                      | 36.0          | 7.8                        | 0.015                      | 11.52           | 7,026.05            | 7,025.94           | 7,034.02                      | 7,034.33                     | 7,028.12                       | 7,027.77                        | 7,029.06                    | 7,029.01                     | 1.520                                   | 0.013       |
| DP01-07            | DP01-06 | 33.70      | 47.16                      | 36.0          | 122.5                      | 0.005                      | 7.25            | 7,026.97            | 7,026.35           | 7,040.66                      | 7,034.02                     | 7,029.84                       | 7,029.55                        | 7,030.21                    | 7,029.90                     | 1.770                                   | 0.013       |
| DP01-09            | DP01-08 | 24.60      | 87.15                      | 30.0          | 46.0                       | 0.045                      | 15.26           | 7,036.08            | 7,034.01           | 7,043.14                      | 7,040.66                     | 7,037.77                       | 7,035.04                        | 7,038.53                    | 7,037.64                     | 0.050                                   | 0.013       |
| DP01-11            | DP01-10 | 24.60      | 87.15                      | 30.0          | 54.5                       | 0.045                      | 15.26           | 7,038.64            | 7,036.18           | 7,045.71                      | 7,043.14                     | 7,040.33                       | 7,037.19                        | 7,041.09                    | 7,039.94                     | 0.050                                   | 0.013       |
| DP01-13            | DP01-12 | 24.60      | 61.05                      | 30.0          | 110.7                      | 0.022                      | 11.77           | 7,041.39            | 7,038.94           | 7,047.66                      | 7,045.71                     | 7,043.08                       | 7,040.07                        | 7,043.84                    | 7,042.10                     | 1.770                                   | 0.013       |
| DP01-15            | DP01-14 | 17.30      | 64.72                      | 30.0          | 182.4                      | 0.025                      | 11.17           | 7,046.23            | 7,041.69           | 7,052.32                      | 7,047.66                     | 7,047.64                       | 7,044.42                        | 7,048.22                    | 7,044.61                     | 0.050                                   | 0.013       |
| DP01-17            | DP01-16 | 17.30      | 65.71                      | 30.0          | 323.4                      | 0.026                      | 11.29           | 7,054.73            | 7,046.43           | 7,060.80                      | 7,052.32                     | 7,056.14                       | 7,047.31                        | 7,056.72                    | 7,049.29                     | 0.100                                   | 0.013       |
| DP01-19            | DP01-18 | 17.30      | 89.92                      | 30.0          | 210.8                      | 0.048                      | 14.15           | 7,064.96            | 7,054.83           | 7,070.53                      | 7,060.80                     | 7,066.37                       | 7,055.57                        | 7,066.95                    | 7,058.68                     | 1.320                                   | 0.013       |
| DP01-21            | DP01-20 | 17.30      | 41.91                      | 30.0          | 27.3                       | 0.010                      | 8.13            | 7,065.55            | 7,065.26           | 7,070.83                      | 7,070.53                     | 7,066.95                       | 7,067.13                        | 7,067.53                    | 7,067.43                     | 0.000                                   | 0.013       |
| DP02-02            | DP02-01 | 9.40       | 30.33                      | 18.0          | 28.9                       | 0.083                      | 15.13           | 7,030.27            | 7,027.85           | 7,034.34                      | 7,034.02                     | 7,031.45                       | 7,029.55                        | 7,032.06                    | 7,029.99                     | 0.000                                   | 0.013       |
| DP03-02            | DP03-01 | 10.10      | 16.00                      | 24.0          | 145.5                      | 0.005                      | 3.21            | 7,028.69            | 7,027.97           | 7,031.94                      | 7,040.66                     | 7,030.78                       | 7,030.49                        | 7,030.94                    | 7,030.65                     | 0.000                                   | 0.013       |
| DP04-02            | DP04-01 | 13.00      | 7.43                       | 18.0          | 43.3                       | 0.005                      | 7.36            | 7,042.61            | 7,042.39           | 7,047.18                      | 7,047.66                     | 7,045.08                       | 7,044.42                        | 7,045.92                    | 7,045.26                     | 1.320                                   | 0.013       |
| DP04-04            | DP04-03 | 13.00      | 7.43                       | 18.0          | 8.1                        | 0.005                      | 7.36            | 7,042.95            | 7,042.91           | 7,047.18                      | 7,047.50                     | 7,046.32                       | 7,046.19                        | 7,047.16                    | 7,047.03                     | 0.000                                   | 0.013       |
| DP05-03            | DP05-02 | 115.80     | 146.12                     | 48.0          | 191.3                      | 0.010                      | 12.90           | 6,992.35            | 6,990.37           | 7,000.91                      | 6,995.01                     | 6,995.60                       | 6,993.09                        | 6,997.34                    | 6,995.61                     | 0.050                                   | 0.013       |
| DP05-05            | DP05-04 | 115.80     | 168.57                     | 48.0          | 53.0                       | 0.014                      | 14.46           | 6,994.08            | 6,993.35           | 7,002.66                      | 7,000.91                     | 6,997.33                       | 6,996.06                        | 6,999.07                    | 6,998.60                     | 0.400                                   | 0.013       |
| DP05-07            | DP05-06 | 115.80     | 163.91                     | 48.0          | 13.1                       | 0.013                      | 14.14           | 6,995.25            | 6,995.08           | 7,003.44                      | 7,002.66                     | 6,998.50                       | 6,998.02                        | 7,000.24                    | 7,000.14                     | 0.640                                   | 0.013       |
| DP05-09            | DP05-08 | 115.80     | 187.75                     | 48.0          | 38.0                       | 0.017                      | 15.72           | 6,996.90            | 6,996.25           | 7,003.95                      | 7,003.44                     | 7,000.15                       | 6,999.61                        | 7,001.89                    | 7,001.25                     | 1.335                                   | 0.013       |
| DP05-11            | DP05-10 | 110.10     | 227.33                     | 48.0          | 128.9                      | 0.025                      | 17.95           | 7,000.23            | 6,997.00           | 7,006.38                      | 7,003.95                     | 7,003.40                       | 7,002.48                        | 7,005.05                    | 7,003.67                     | 0.640                                   | 0.013       |
| DP05-13            | DP05-12 | 108.80     | 150.89                     | 42.0          | 279.2                      | 0.022                      | 17.07           | 7,006.81            | 7,000.53           | 7,017.53                      | 7,006.38                     | 7,009.97                       | 7,004.46                        | 7,012.18                    | 7,006.45                     | 0.640                                   | 0.013       |
| DP05-15            | DP05-14 | 108.80     | 155.51                     | 42.0          | 96.6                       | 0.024                      | 17.49           | 7,011.92            | 7,009.61           | 7,025.12                      | 7,017.53                     | 7,015.08                       | 7,011.98                        | 7,017.28                    | 7,015.82                     | 0.400                                   | 0.013       |
| DP05-17            | DP05-16 | 108.80     | 159.13                     | 42.0          | 59.3                       | 0.025                      | 17.80           | 7,019.18            | 7,017.70           | 7,023.27                      | 7,025.12                     | 7,022.34                       | 7,020.15                        | 7,024.55                    | 7,023.71                     | 0.000                                   | 0.013       |
| DP06-03            | DP06-02 | 85.20      | 127.25                     | 42.0          | 140.5                      | 0.016                      | 14.17           | 7,027.89            | 7,025.64           | 7,043.80                      | 7,029.73                     | 7,030.77                       | 7,027.82                        | 7,032.34                    | 7,030.67                     | 0.075                                   | 0.013       |
| DP06-05            | DP06-04 | 84.10      | 159.04                     | 42.0          | 35.0                       | 0.025                      | 16.76           | 7,038.10            | 7,037.23           | 7,043.80                      | 7,043.80                     | 7,040.96                       | 7,039.43                        | 7,042.52                    | 7,042.13                     | 0.050                                   | 0.013       |
| DP06-07            | DP06-06 | 82.60      | 159.04                     | 42.0          | 29.4                       | 0.025                      | 16.69           | 7,038.93            | 7,038.20           | 7,044.44                      | 7,043.80                     | 7,041.77                       | 7,041.04                        | 7,043.29                    | 7,042.56                     | 0.075                                   | 0.013       |
| DP06-09            | DP06-08 | 82.60      | 159.04                     | 42.0          | 105.5                      | 0.025                      | 16.69           | 7,041.67            | 7,039.04           | 7,058.13                      | 7,044.44                     | 7,044.51                       | 7,041.88                        | 7,046.03                    | 7,043.39                     | 0.050                                   | 0.013       |
| DP06-11            | DP06-10 | 82.60      | 157.66                     | 42.0          | 148.1                      | 0.025                      | 16.58           | 7,055.55            | 7,051.91           | 7,067.52                      | 7,058.13                     | 7,058.38                       | 7,053.81                        | 7,059.90                    | 7,057.56                     | 1.300                                   | 0.013       |
| DP06-13            | DP06-12 | 78.50      | 123.59                     | 42.0          | 36.2                       | 0.015                      | 13.60           | 7,061.36            | 7,060.81           | 7,067.78                      | 7,067.52                     | 7,064.13                       | 7,063.12                        | 7,065.57                    | 7,065.24                     | 0.075                                   | 0.013       |
| DP06-15            | DP06-14 | 78.50      | 138.70                     | 42.0          | 143.3                      | 0.019                      | 14.86           | 7,064.18            | 7,061.46           | 7,068.27                      | 7,067.78                     | 7,066.95                       | 7,064.24                        | 7,068.39                    | 7,065.67                     | 0.000                                   | 0.013       |
| DP07-03            | DP07-02 | 4.00       | 20.25                      | 18.0          | 24.3                       | 0.037                      | 8.92            | 7,005.82            | 7,004.92           | 7,014.46                      | 7,004.92                     | 7,006.59                       | 7,005.41                        | 7,006.89                    | 7,006.42                     | 0.050                                   | 0.013       |
| DP07-05            | DP07-04 | 2.90       | 20.49                      | 18.0          | 36.7                       | 0.038                      | 8.20            | 7,010.57            | 7,009.17           | 7,014.44                      | 7,014.46                     | 7,011.22                       | 7,009.56                        | 7,011.46                    | 7,010.55                     | 0.000                                   | 0.013       |
| DP08-02            | DP08-01 | 24.20      | 38.02                      | 30.0          | 177.0                      | 0.009                      | 4.93            | 7,058.07            | 7,056.55           | 7,064.95                      | 7,067.52                     | 7,060.98                       | 7,060.36                        | 7,061.35                    | 7,060.74                     | 1.770                                   | 0.013       |
| DP08-04            | DP08-03 | 18.30      | 18.34                      | 24.0          | 66.3                       | 0.007                      | 5.83            | 7,059.00            | 7,058.56           | 7,064.37                      | 7,064.95                     | 7,062.08                       | 7,061.64                        | 7,062.61                    | 7,062.17                     | 1.770                                   | 0.013       |
| DP08-06            | DP08-05 | 5.10       | 13.18                      | 18.0          | 28.6                       | 0.016                      | 2.89            | 7,059.94            | 7,059.49           | 7,064.52                      | 7,064.37                     | 7,063.08                       | 7,063.01                        | 7,063.21                    | 7,063.14                     | 0.980                                   | 0.013       |
| DP08-08            | DP08-07 | 5.10       | 12.47                      | 18.0          | 29.4                       | 0.014                      | 2.89            | 7,060.65            | 7,060.24           | 7,064.83                      | 7,064.52                     | 7,063.27                       | 7,063.21                        | 7,063.40                    | 7,063.34                     | 0.000                                   | 0.013       |
| DP09-02            | DP09-01 | 6.90       | 10.42                      | 18.0          | 244.8                      | 0.010                      | 6.30            | 7,065.22            | 7,062.81           | 7,070.22                      | 7,067.52                     | 7,066.24                       | 7,063.71                        | 7,066.70                    | 7,064.32                     | 0.100                                   | 0.013       |
| DP09-04            | DP09-03 | 6.90       | 11.46                      | 18.0          | 183.8                      | 0.012                      | 6.78            | 7,067.51            | 7,065.33           | 7,072.64                      | 7,070.22                     | 7,068.53                       | 7,066.17                        | 7,068.99                    | 7,066.88                     | 0.100                                   | 0.013       |
| DP09-06            | DP09-05 | 6.90       | 11.17                      | 18.0          | 29.4                       | 0.011                      | 6.65            | 7,067.95            | 7,067.62           | 7,073.01                      | 7,072.64                     | 7,068.97                       | 7,068.49                        | 7,069.42                    | 7,069.14                     | 1.320                                   | 0.013       |
| DP09-08            | DP09-07 | 6.90       | 13.33                      | 18.0          | 8.1                        | 0.016                      | 7.61            | 7,068.37            | 7,068.24           | 7,073.31                      | 7,073.01                     | 7,069.52                       | 7,069.57                        | 7,069.87                    | 7,069.84                     | 0.000                                   | 0.013       |
| DP10-02            | DP10-01 | 7.30       | 24.16                      | 18.0          | 27.4                       | 0.053                      | 11.98           | 7,060.51            | 7,059.06           | 7,065.24                      | 7,064.95                     | 7,061.60                       | 7,061.64                        | 7,062.04                    | 7,061.91                     | 0.000                                   | 0.013       |
| DP11-02            | DP11-01 | 6.70       | 7.85                       | 18.0          | 15.4                       | 0.006                      | 3.79            | 7,002.62            | 7,002.53           | 7,007.08                      | 7,006.38                     | 7,004.52                       | 7,004.46                        | 7,004.74                    | 7,004.68                     | 0.250                                   | 0.013       |
| DP11-04            | DP11-03 | 6.70       | 7.98                       | 18.0          | 56.1                       | 0.006                      | 3.79            | 7,002.93            | 7,002.61           | 7,005.30                      | 7,007.08                     | 7,004.80                       | 7,004.58                        | 7,005.03                    | 7,004.80                     | 0.000                                   | 0.013       |
| DP12-02            | DP12-01 | 17.10      | 23.56                      | 24.0          | 50.7                       | 0.011                      | 8.18            | 7,001.45            | 7,000.90           | 7,004.67                      | 7,003.95                     | 7,002.94                       | 7,002.48                        | 7,003.66                    | 7,003.12                     | 0.000                                   | 0.013       |
| DP03-13            | DP13-02 | 6.90       | 13.85                      | 18.0          | 54.2                       | 0.017                      | 7.83            | 7,049.68            | 7,048.74           | 7,051.49                      | 7,050.45                     | 7,050.70                       | 7,049.50                        | 7,051.16                    | 7,050.42                     | 0.000                                   | 0.013       |
| DP14-03            | DP14-02 | 3.30       | 3.69                       | 12.0          | 69.3                       | 0.011                      | 5.32            | 7,051.43            | 7,050.69           | 7,054.43                      | 7,051.86                     | 7,052.21                       | 7,051.43                        | 7,052.61                    | 7,051.87                     | 0.075                                   | 0.013       |
| DP14-05            | DP14-04 | 3.30       | 3.69                       | 12.0          | 55.8                       | 0.011                      | 5.32            | 7,052.03            | 7,051.43           | 7,054.73                      | 7,054.43                     | 7,052.81                       | 7,052.24                        | 7,053.21                    | 7,052.61                     | 0.640                                   | 0.013       |
| DP14-07            | DP14-06 | 3.30       | 3.69                       | 12.0          | 21.4                       | 0.011                      | 5.32            | 7,052.26            | 7,052.03           | 7,053.43                      | 7,054.73                     | 7,053.24                       | 7,053.06                        | 7,053.52                    | 7,053.34                     | 0.000                                   | 0.013       |
| DP15-02            | DP15-01 | 16.00      | 44.58                      | 24.0          | 7.0                        | 0.039                      | 5.09            | 7,059.57            | 7,059.30           | 7,064.65                      | 7,064.37                     | 7,063.05                       | 7,063.01                        | 7,063.45                    | 7,063.41                     | 0.000                                   | 0.013       |

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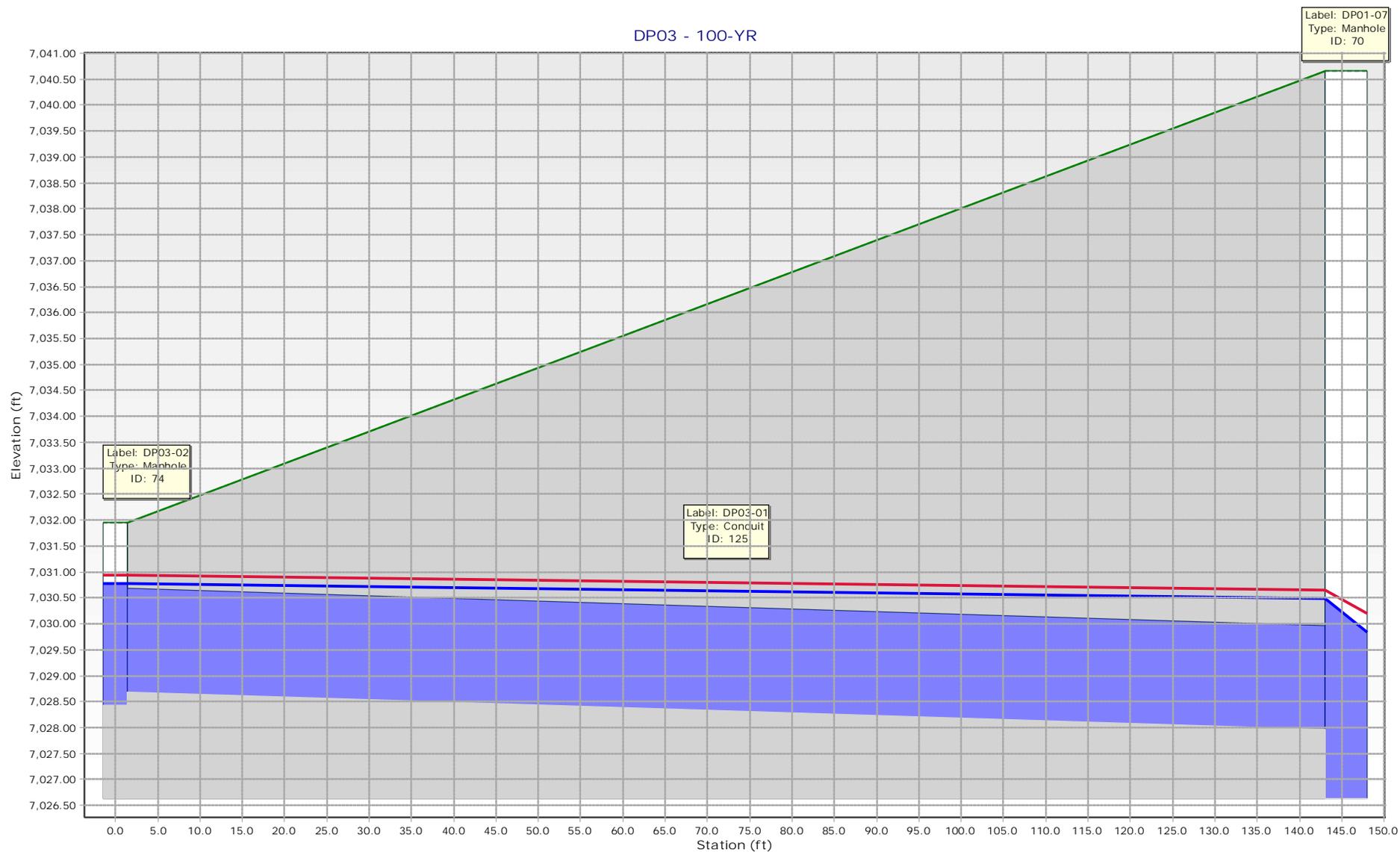
DP01 - 100-YR



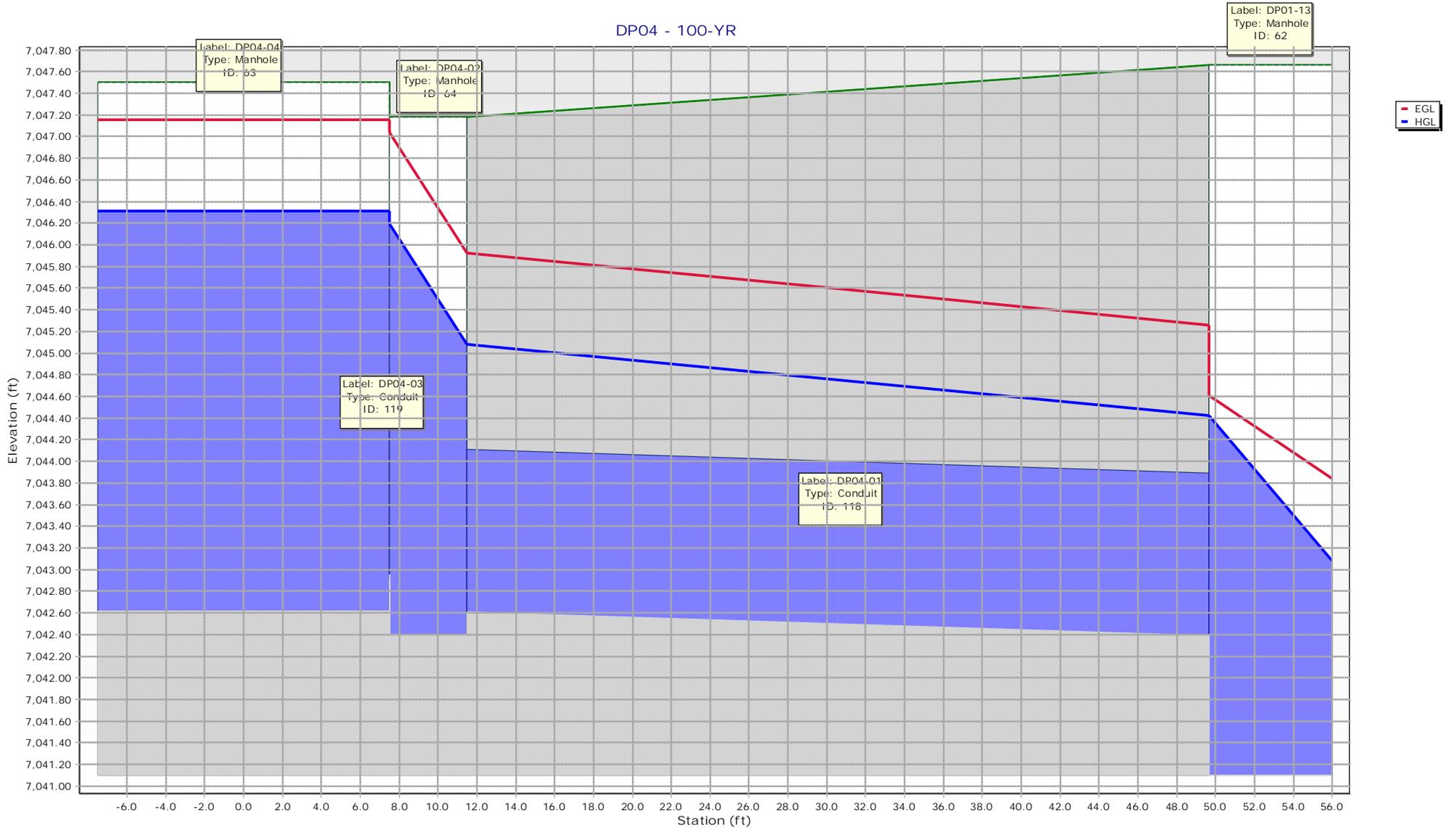
DPO2 - 100-YR



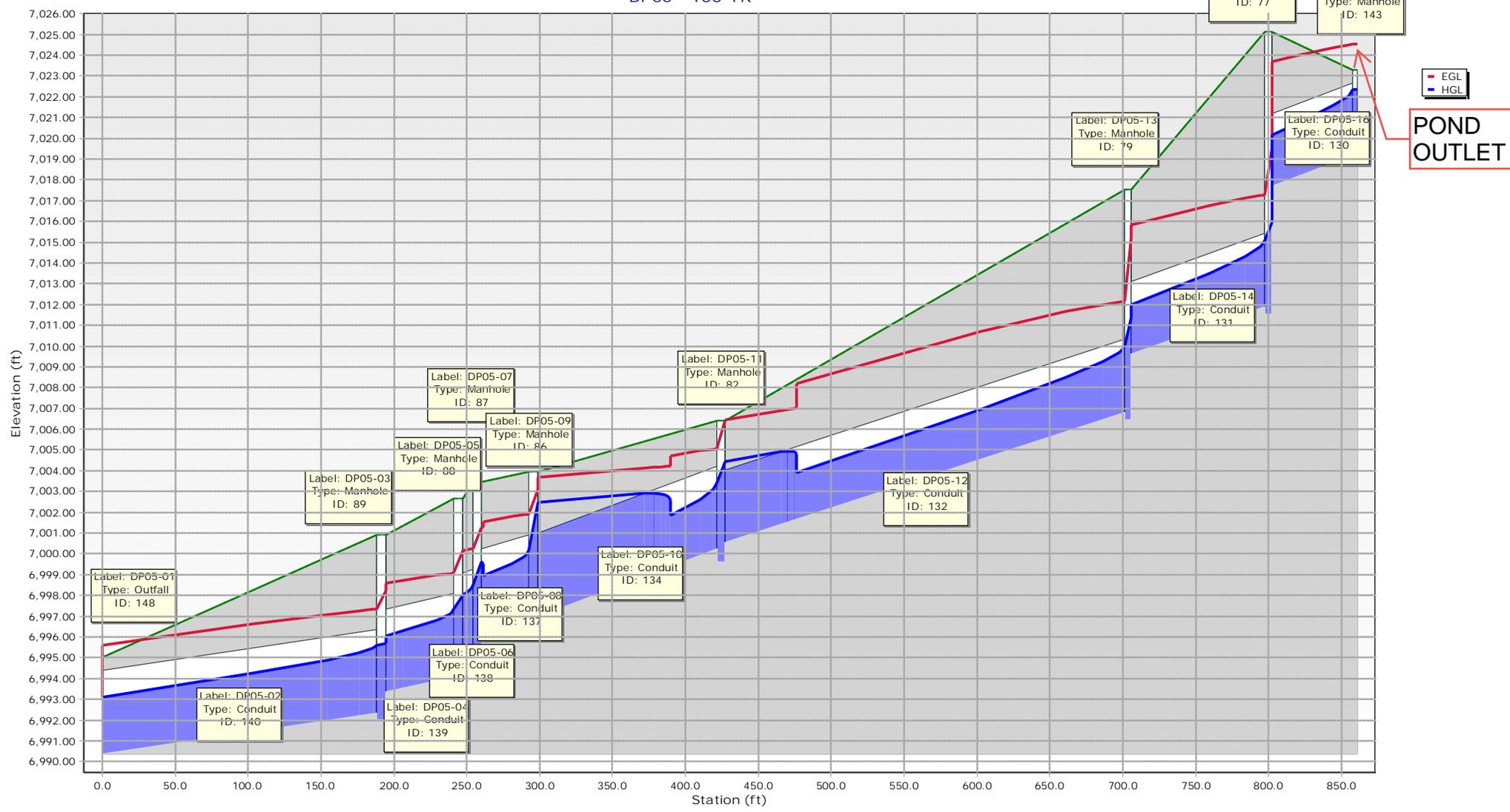
DPO3 - 100-YR



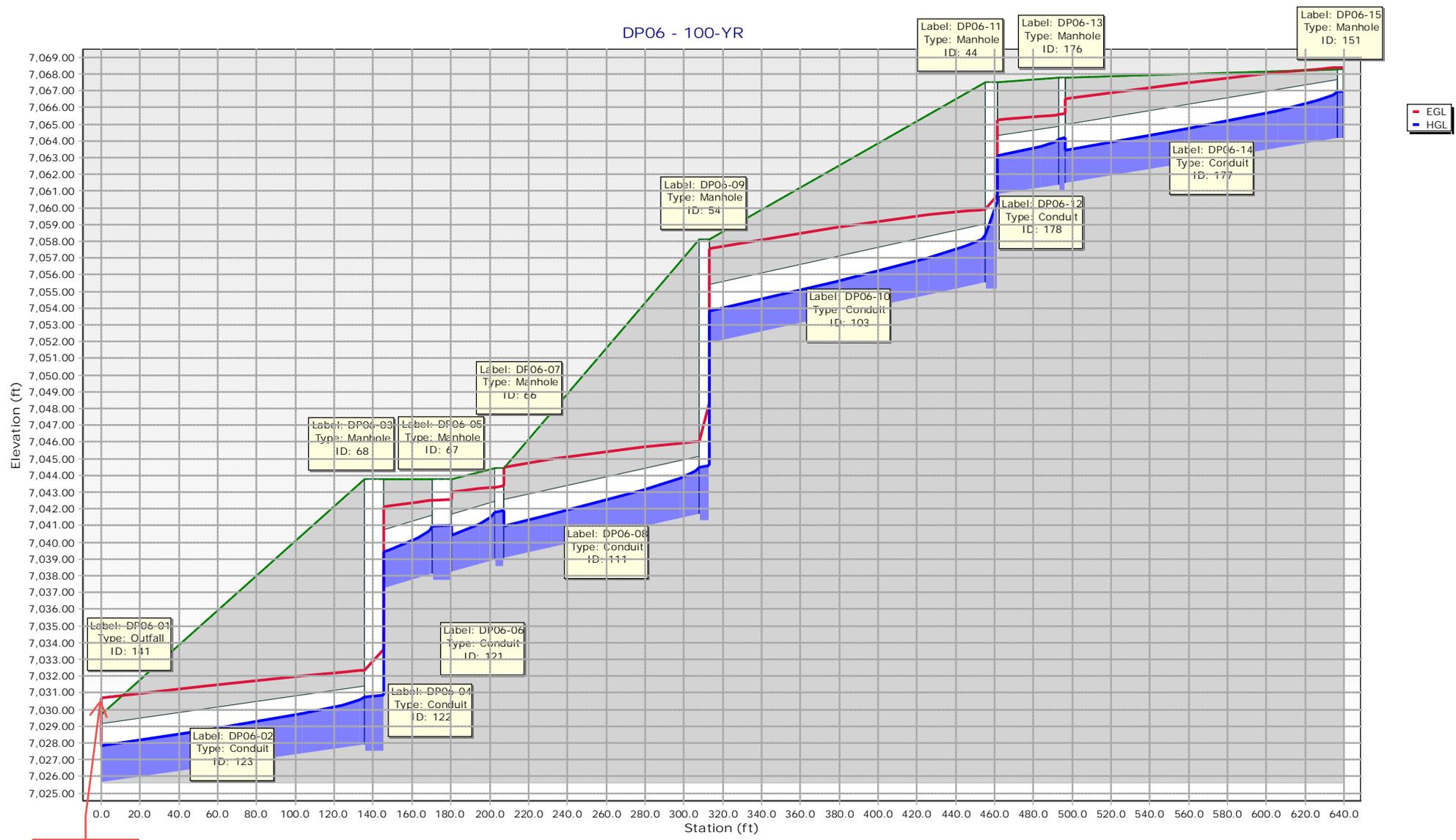
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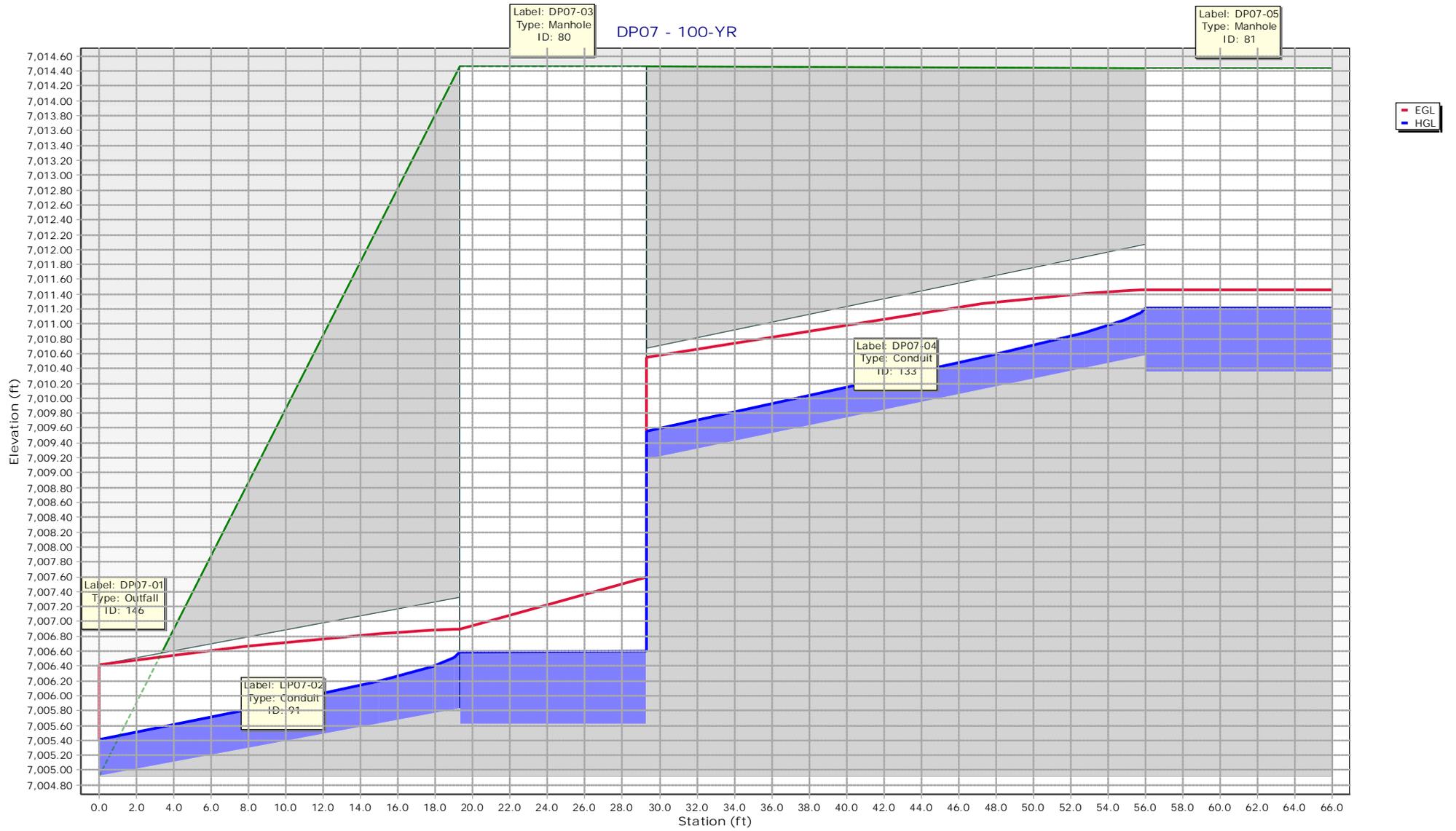
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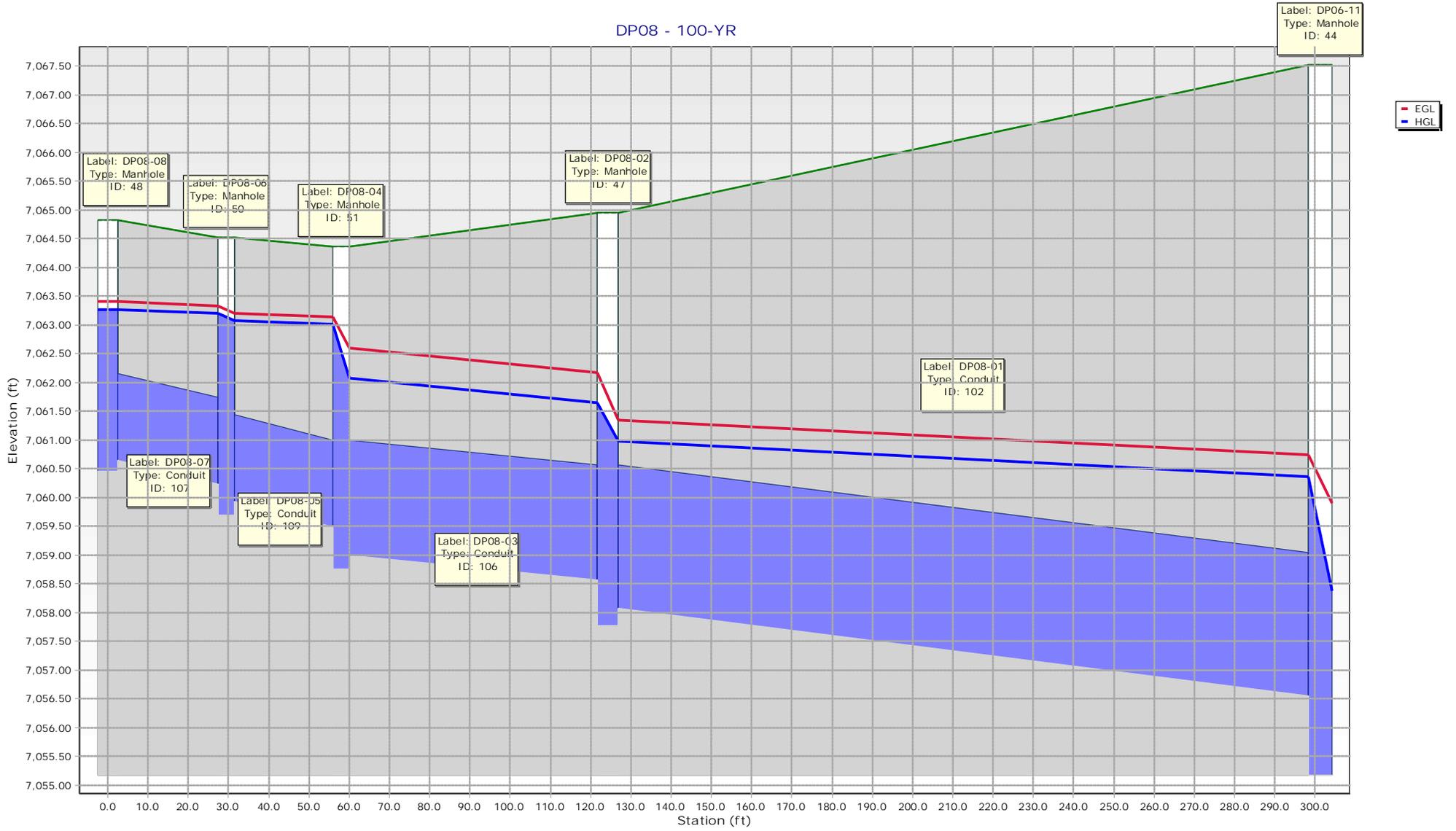
DPO6 - 100-YR



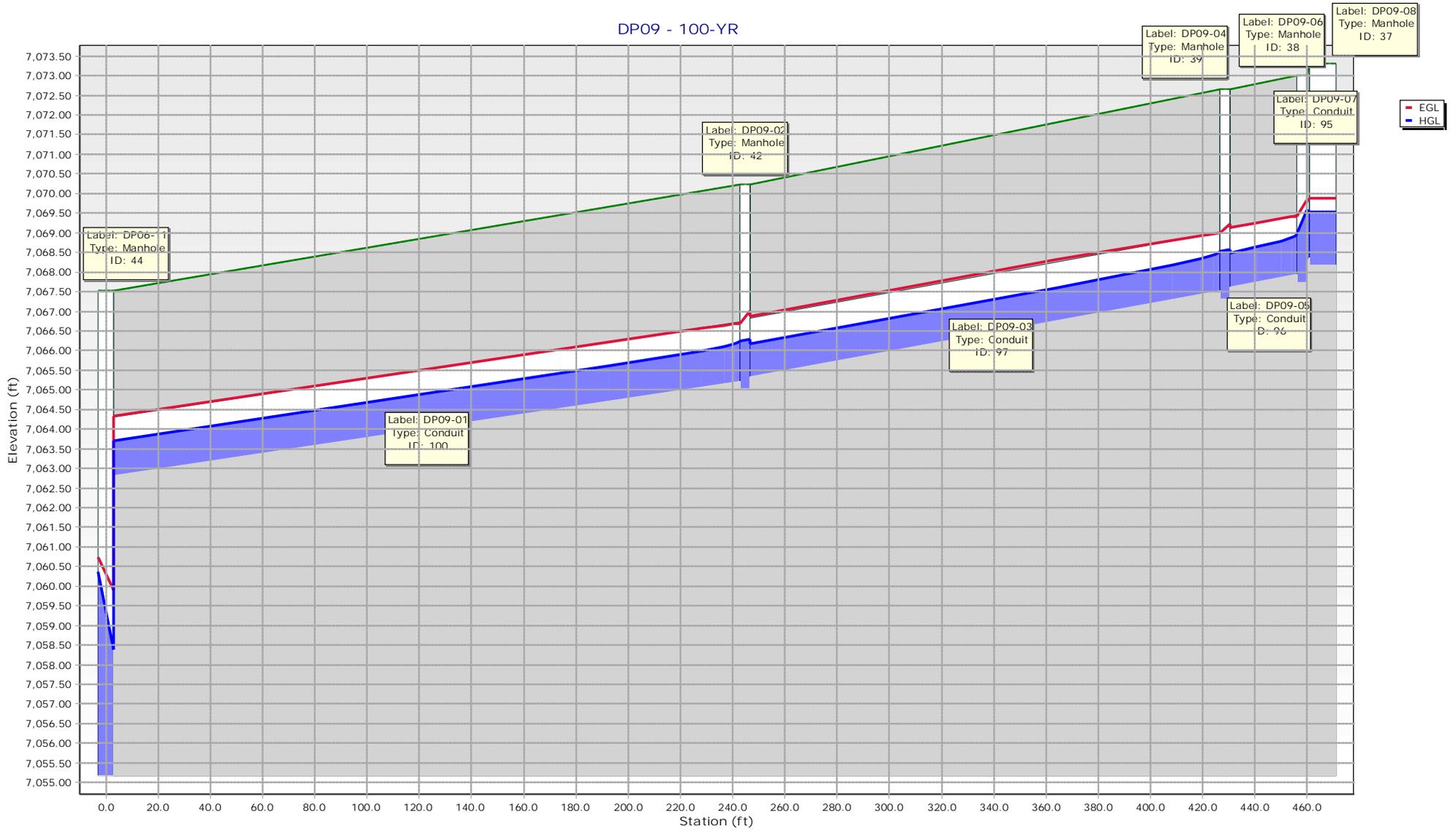
POND  
OUTLET



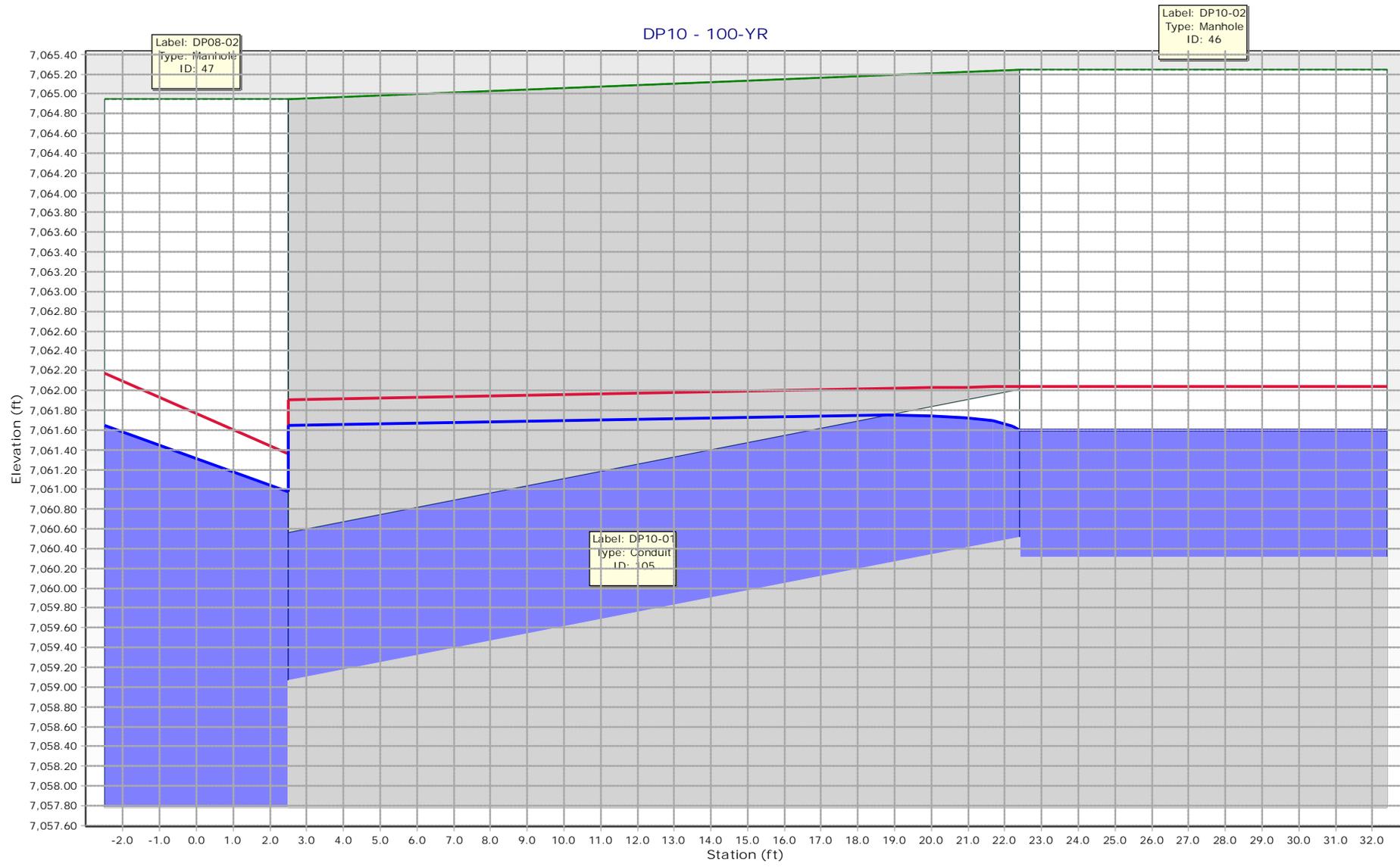
DPO8 - 100-YR



DPO9 - 100-YR

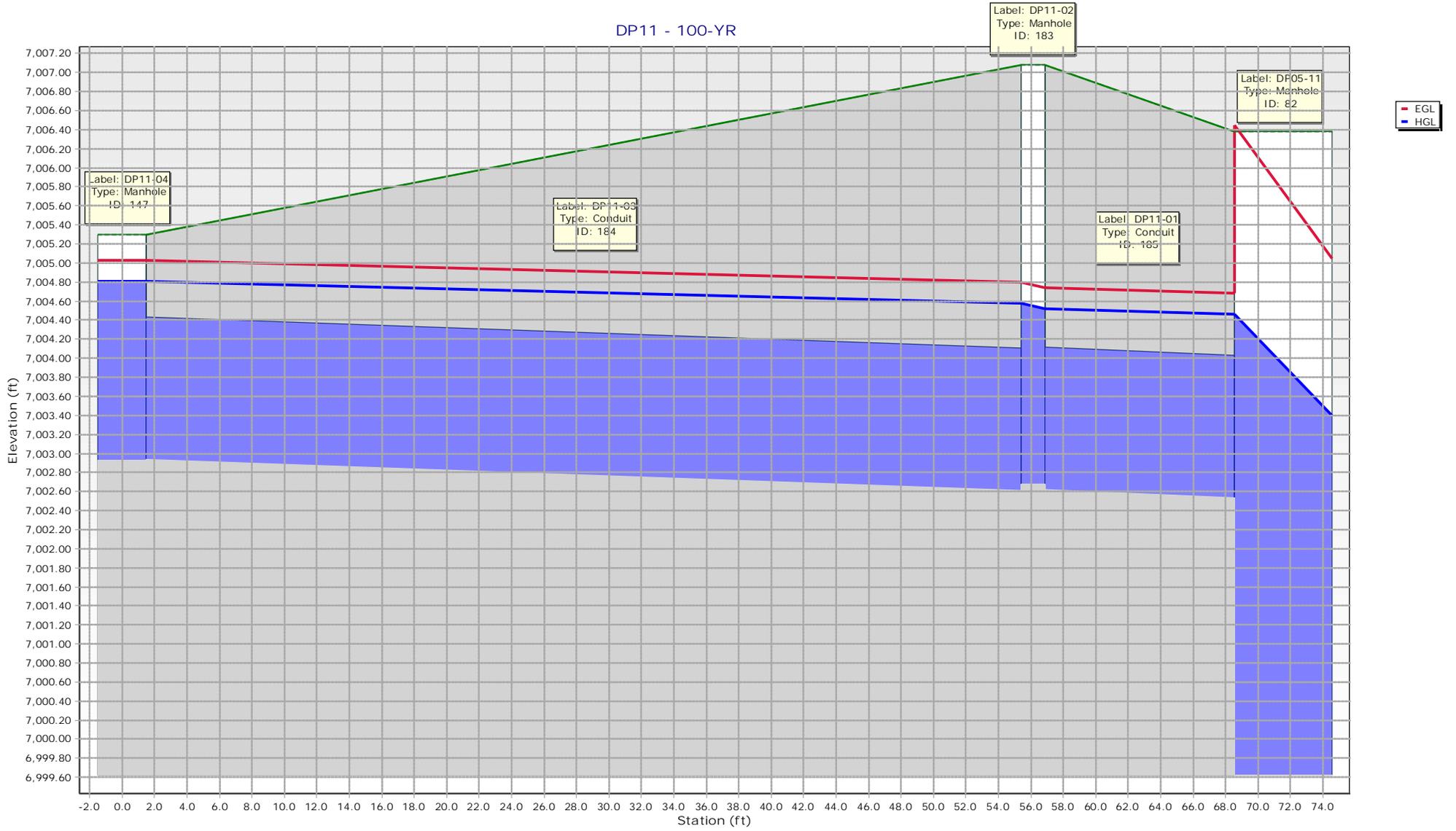


DP10 - 100-YR

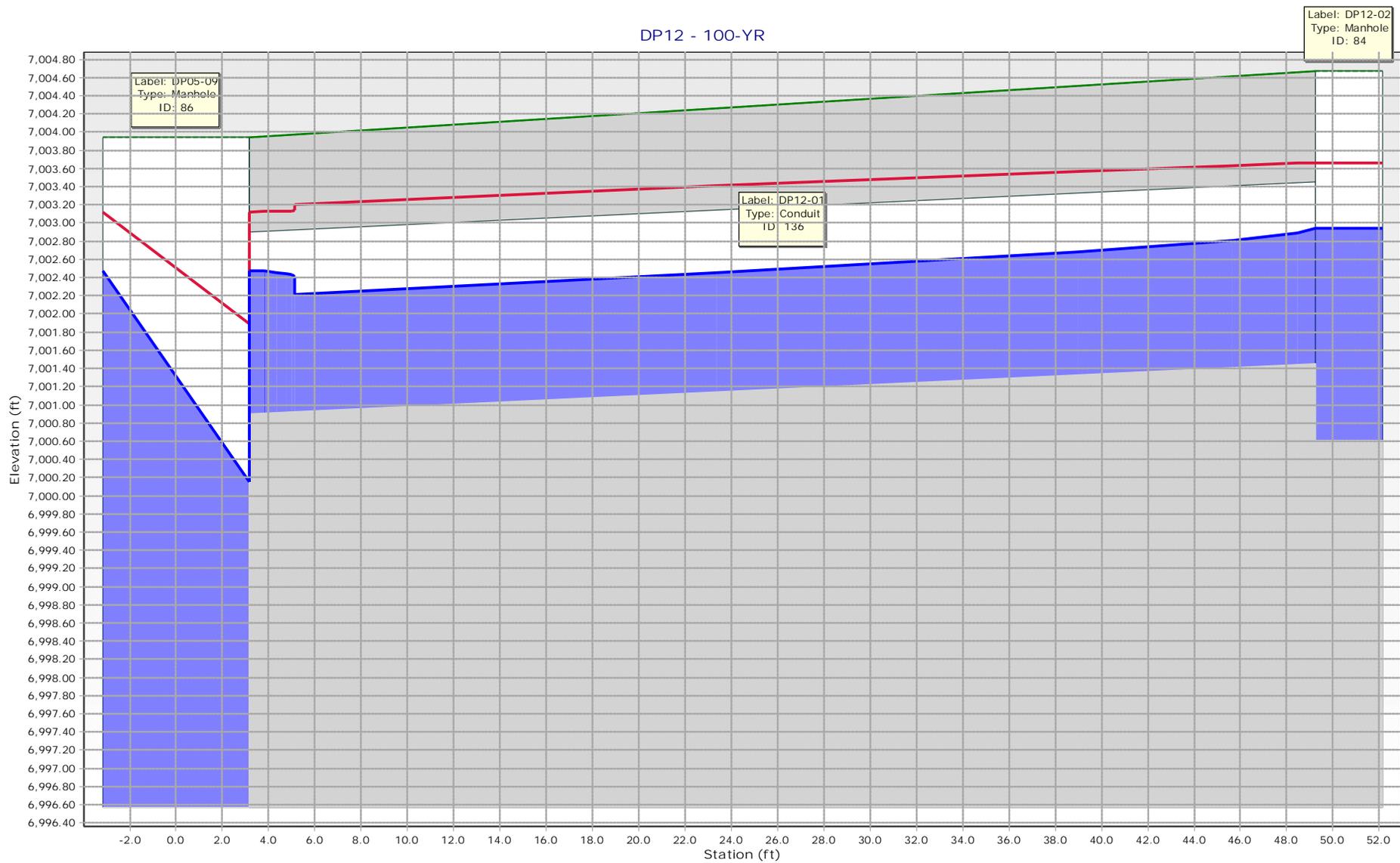


EGL  
HGL

DP11 - 100-YR

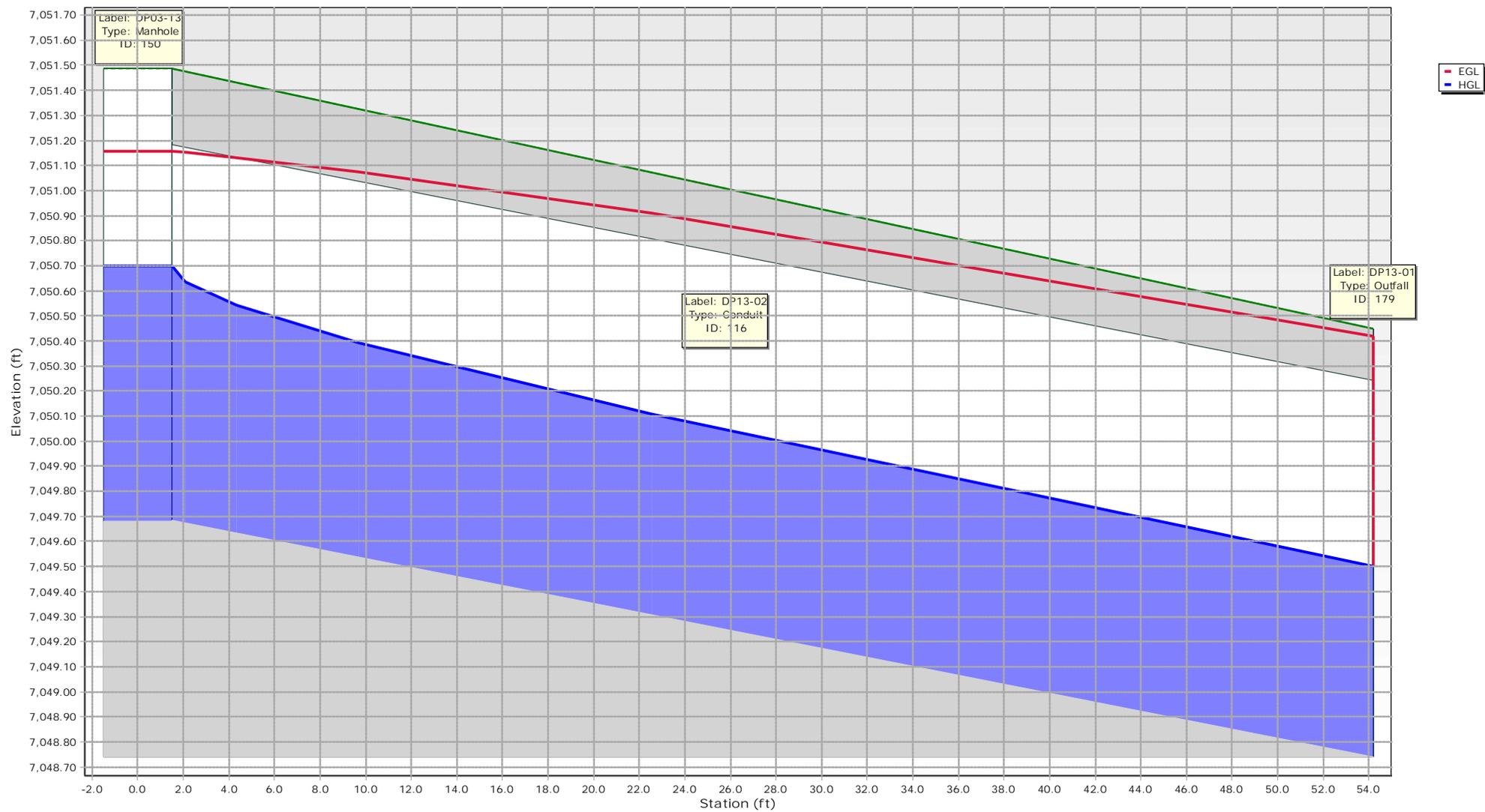


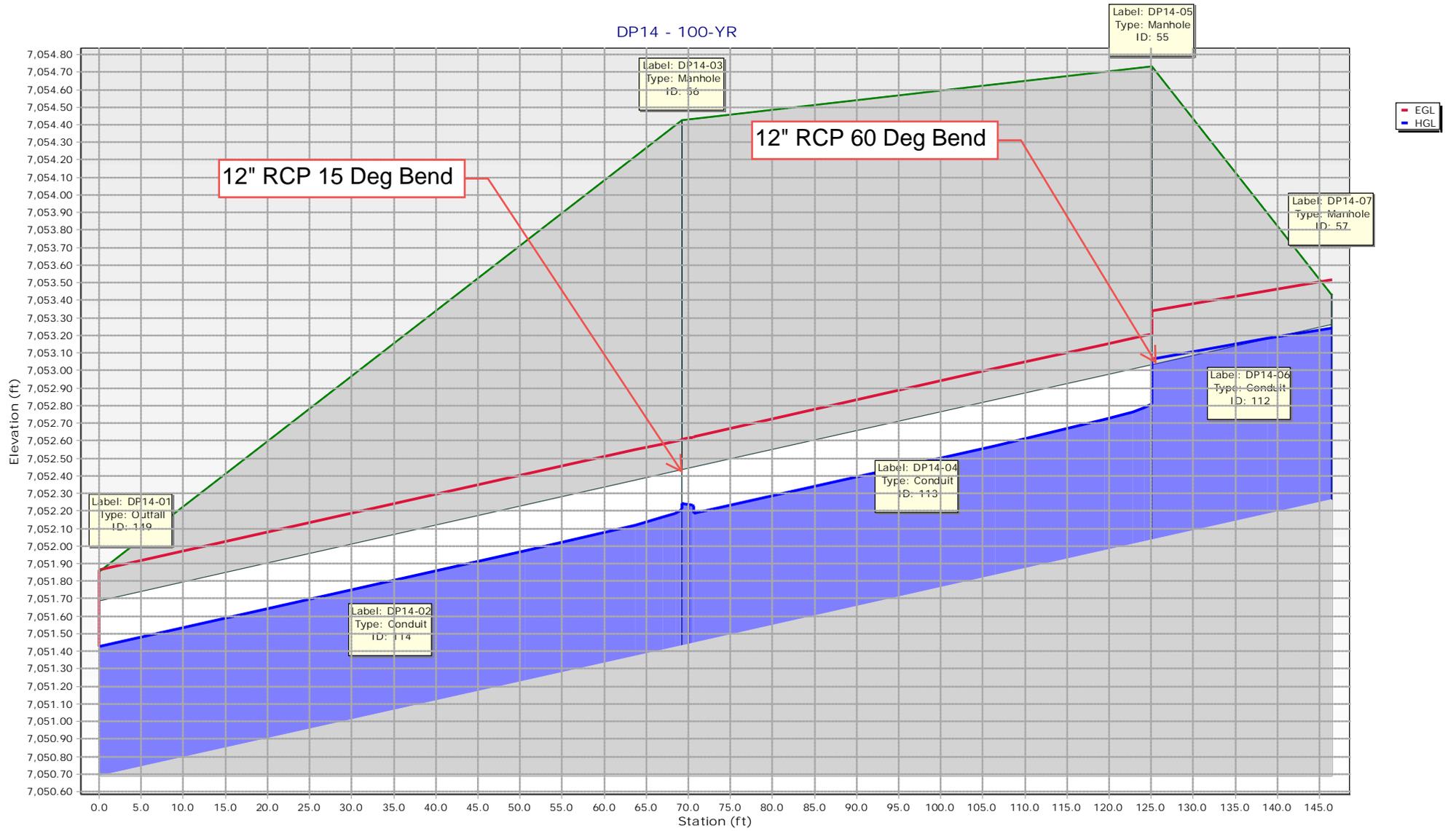
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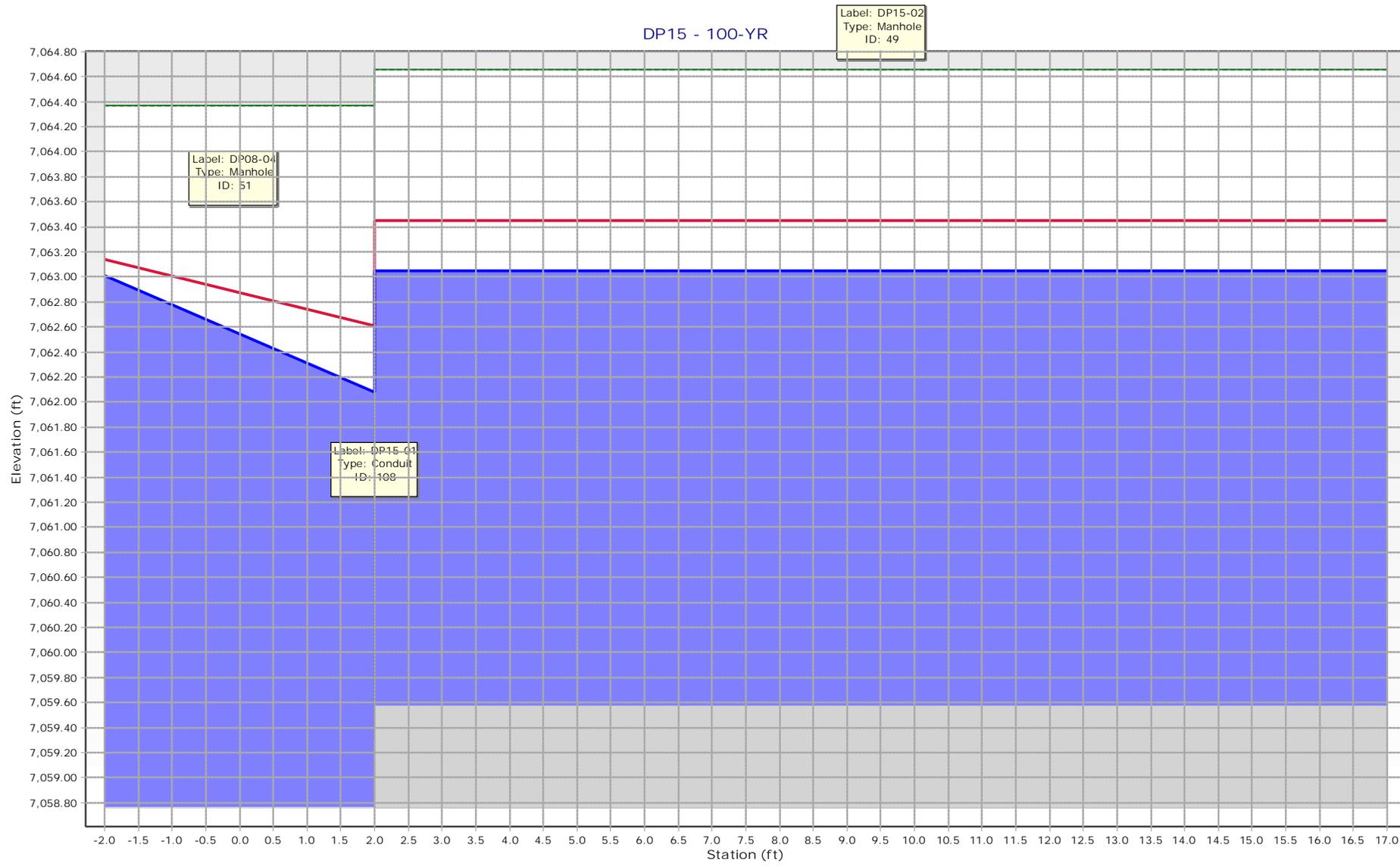
EGL  
HGL

DP13 - 100-YR



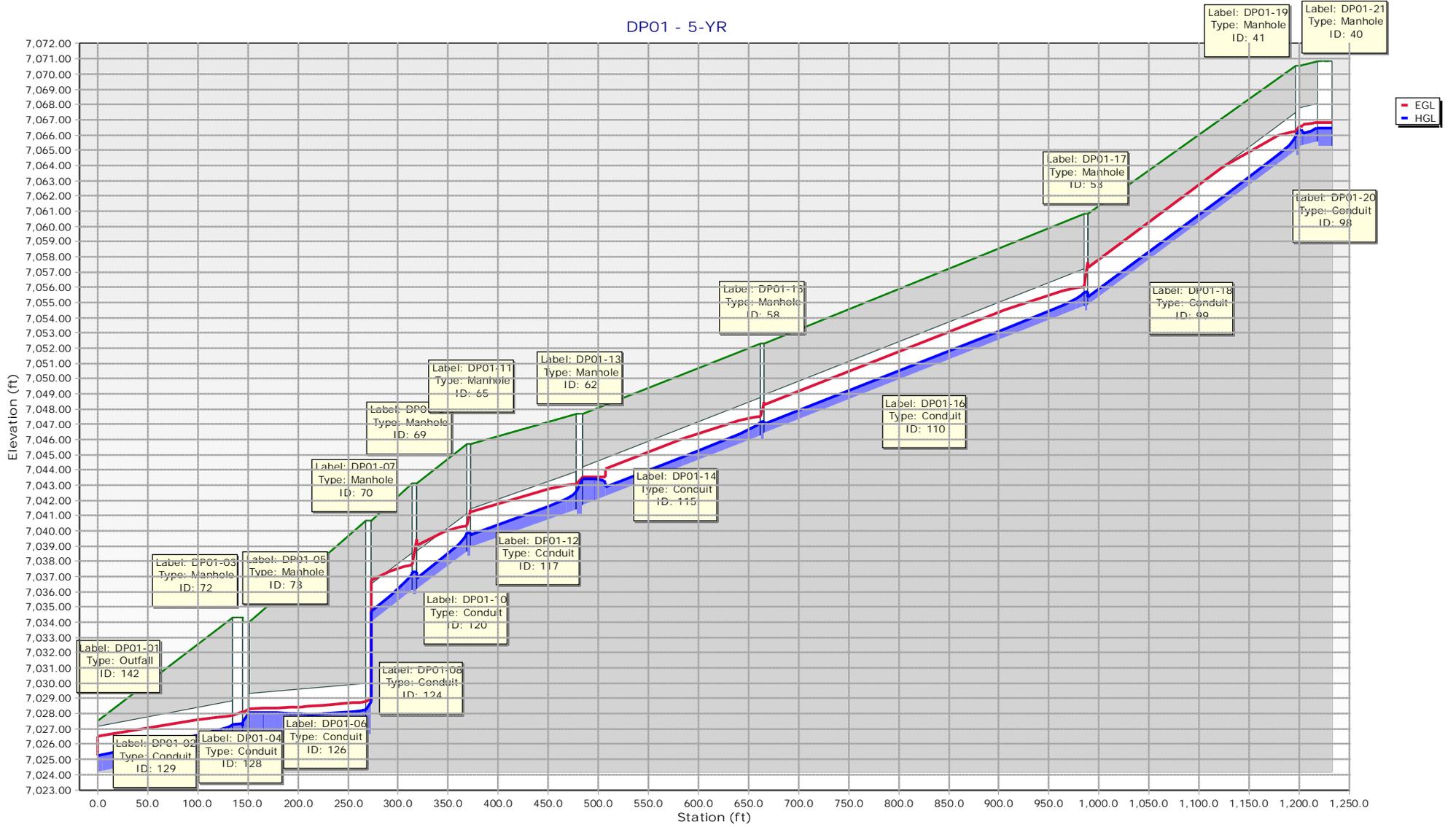


DP15 - 100-YR



EGL  
HGL

DPO1 - 5-YR



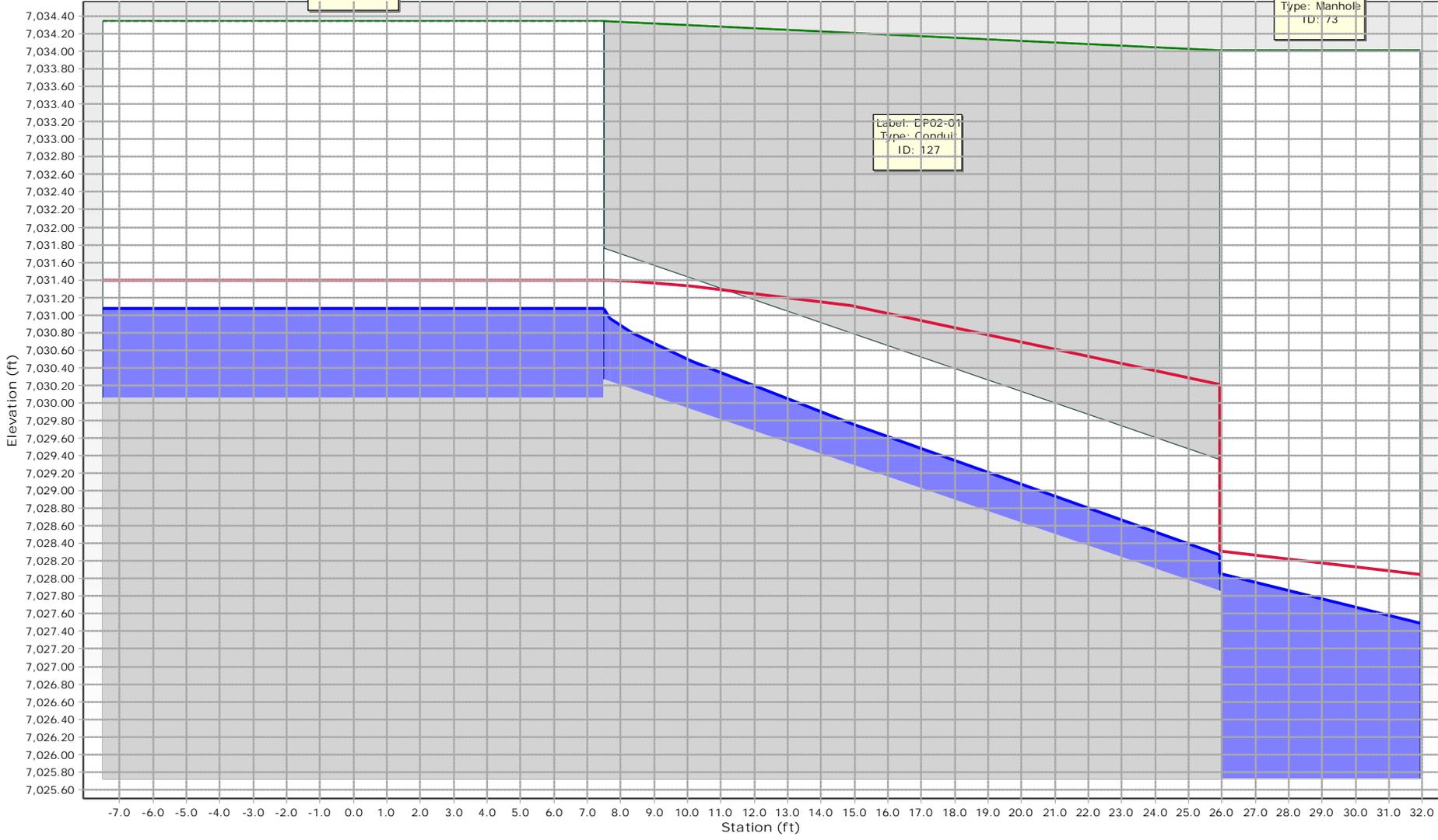
Label: DP02-02  
Type: Manhole  
ID: 71

DPO2 - 5-YR

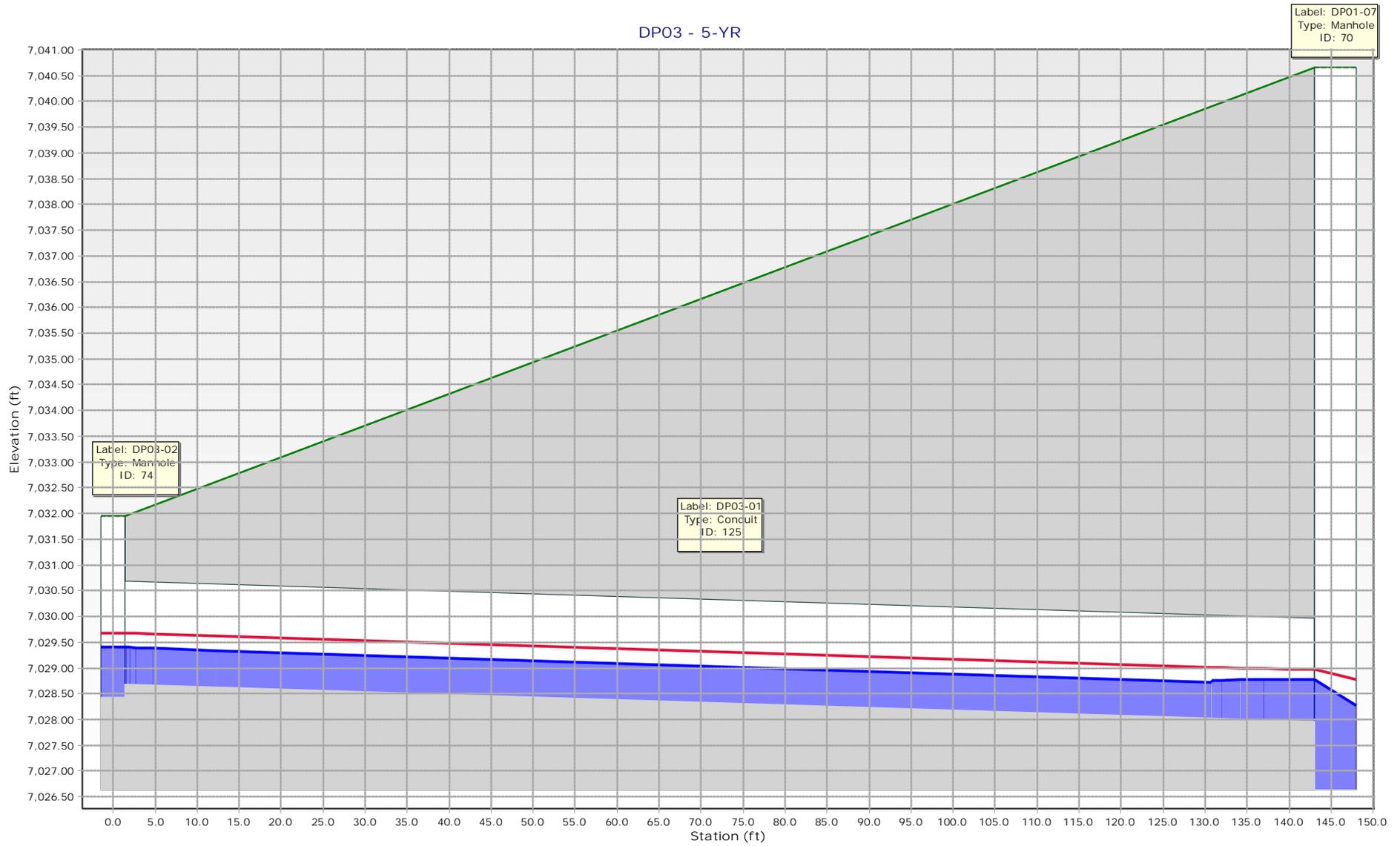
Label: DP01-05  
Type: Manhole  
ID: 73

Label: DP02-01  
Type: Conduit  
ID: 127

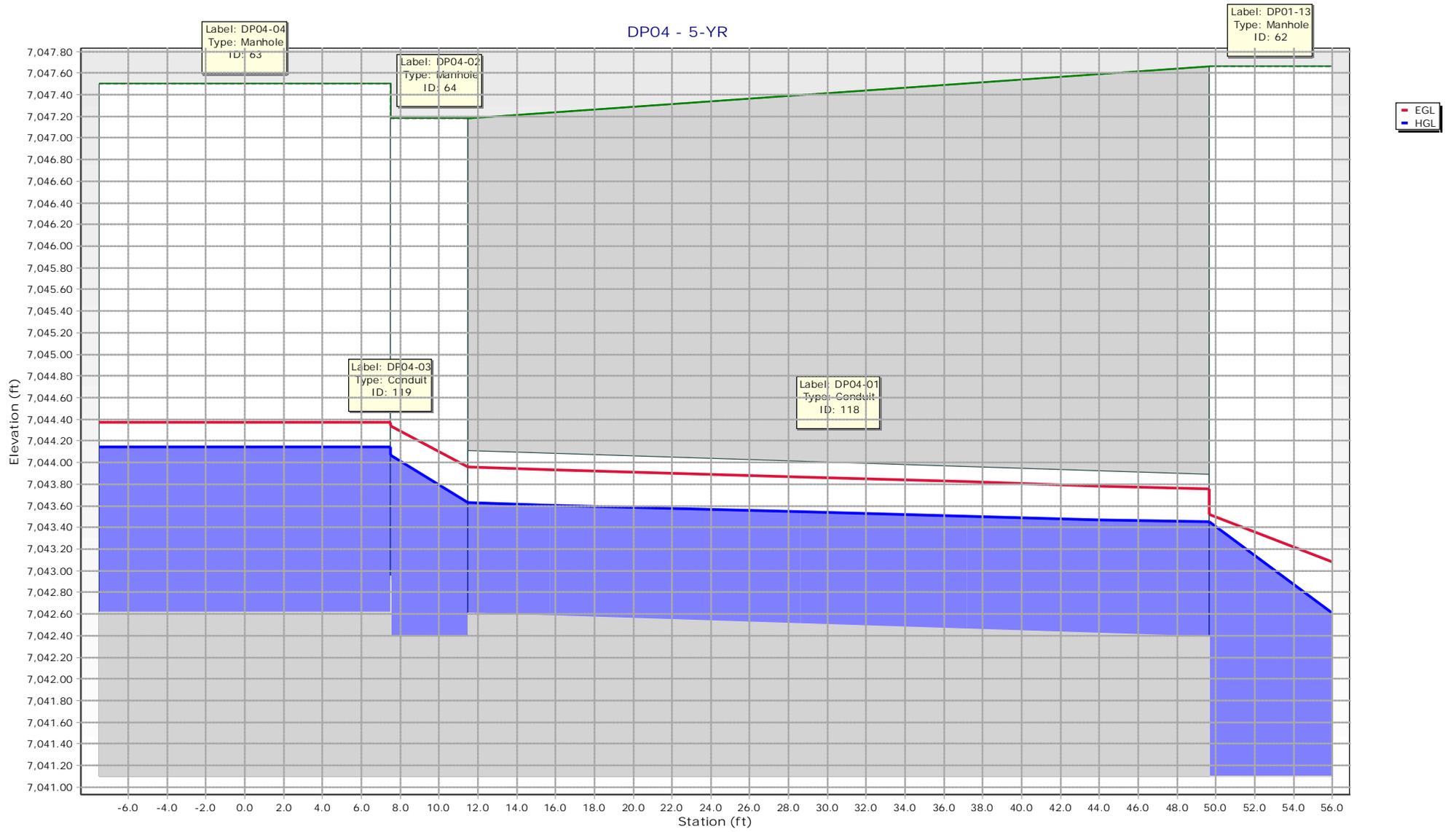
EGL  
HGL



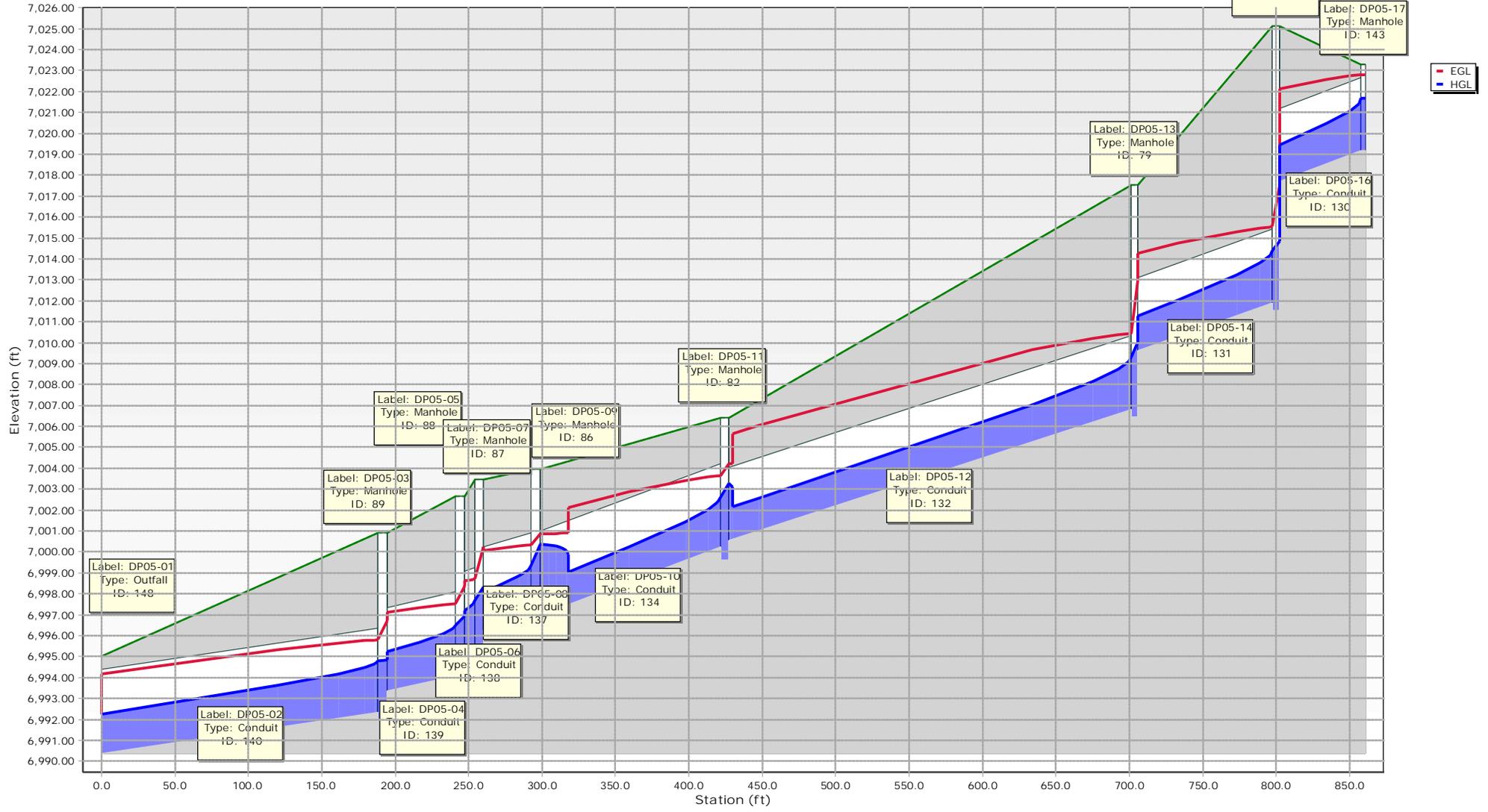
DPO3 - 5-YR



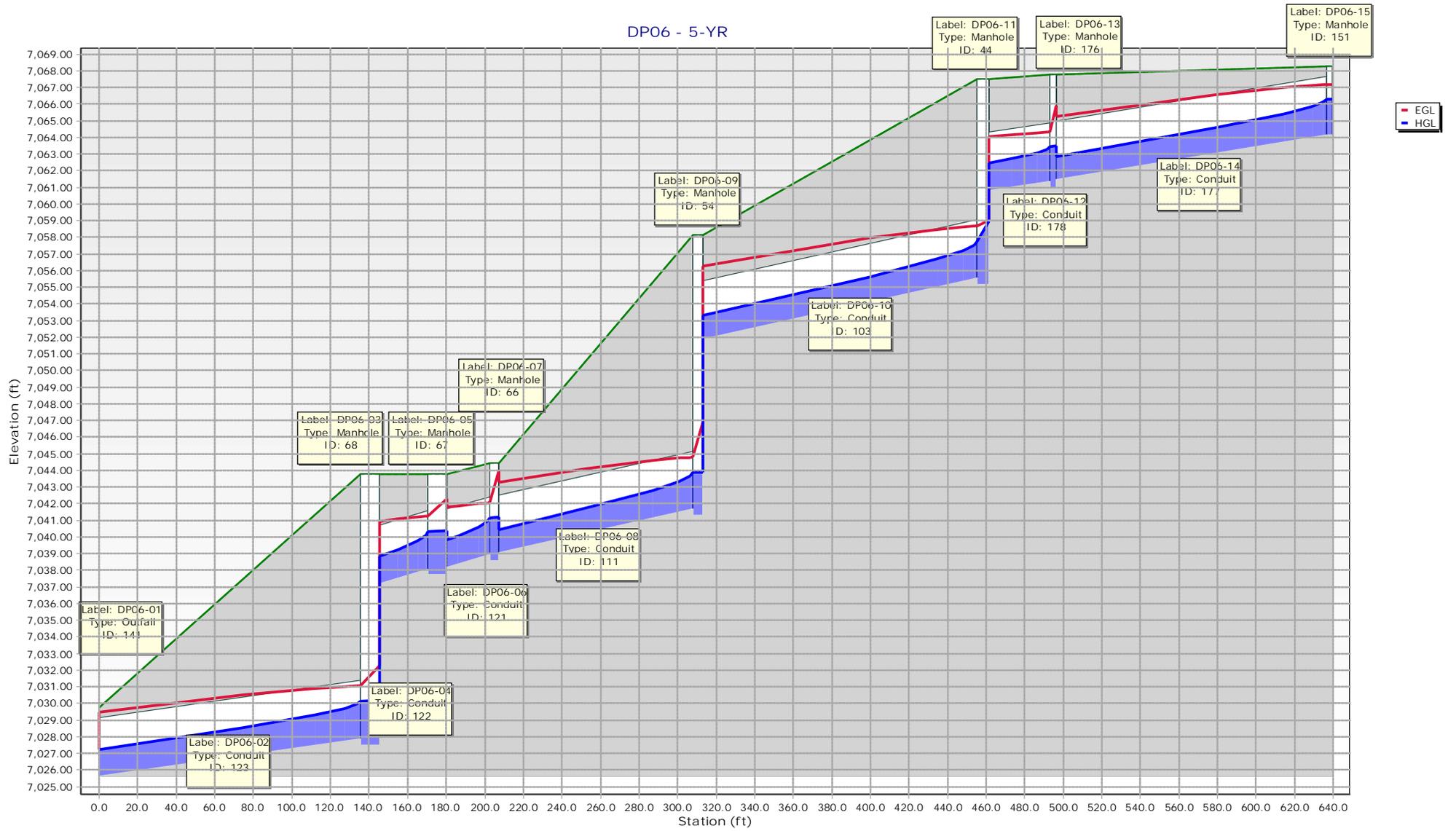
DPO4 - 5-YR

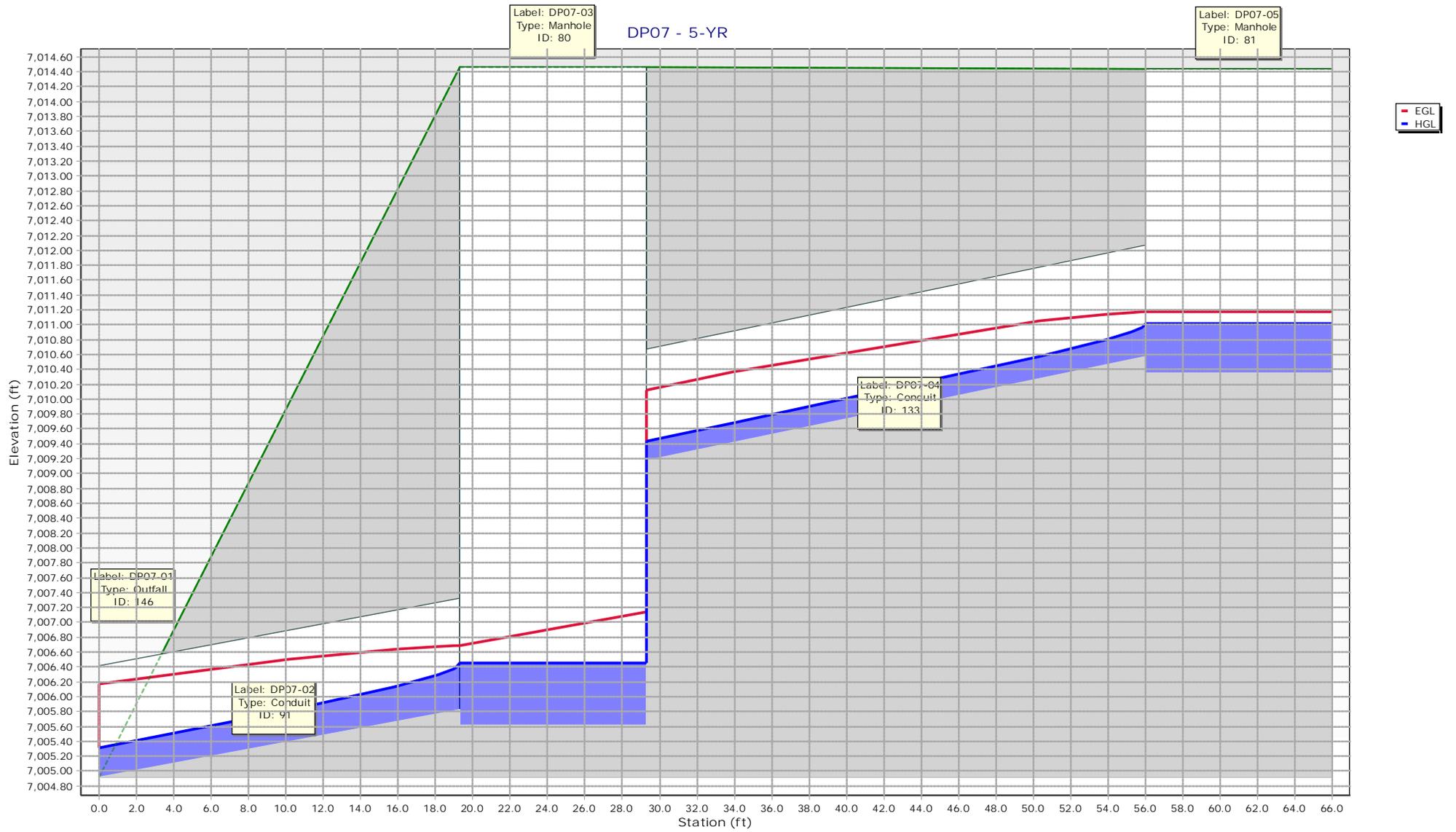


DPO5 - 5-YR

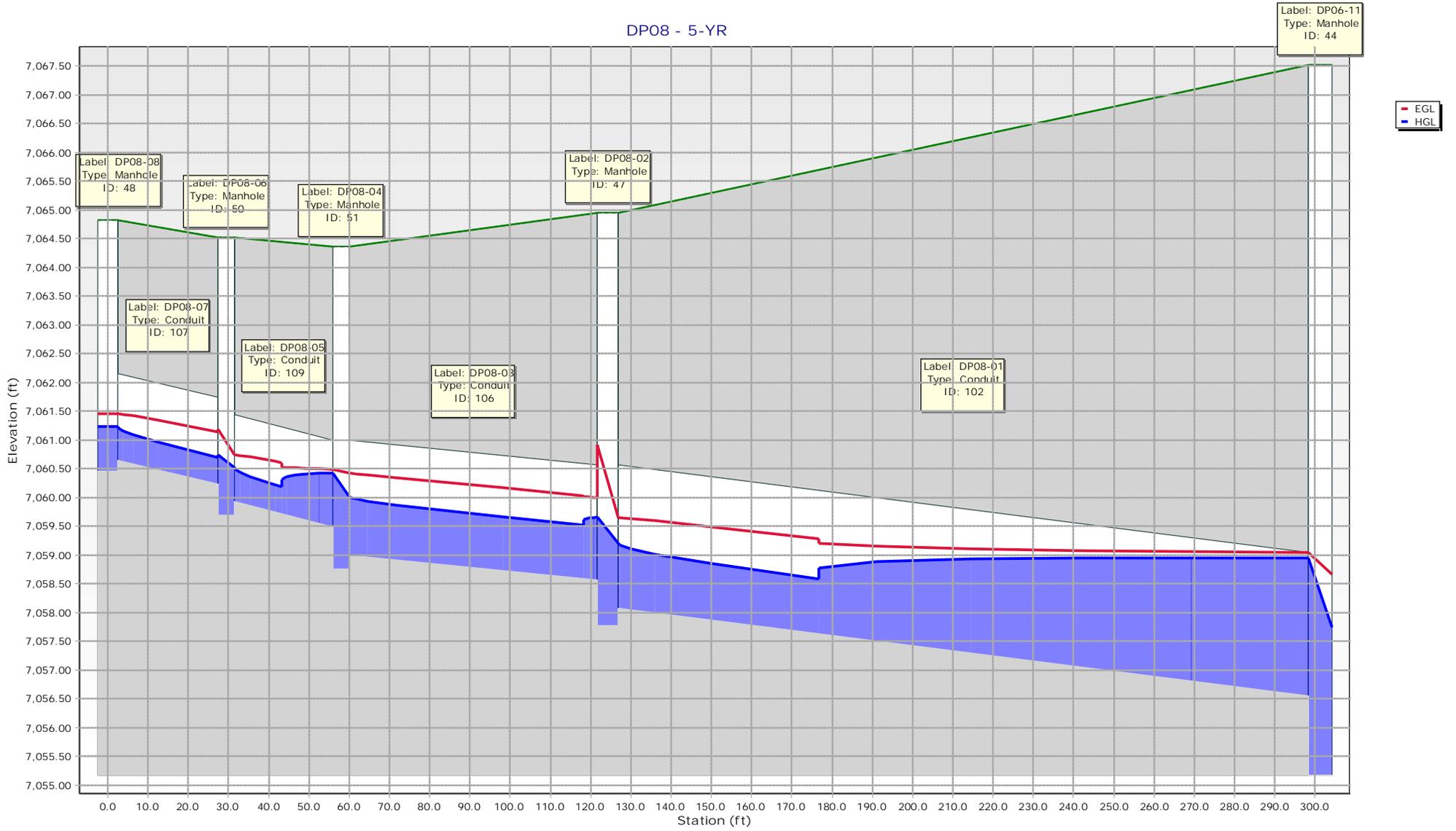


DPO6 - 5-YR

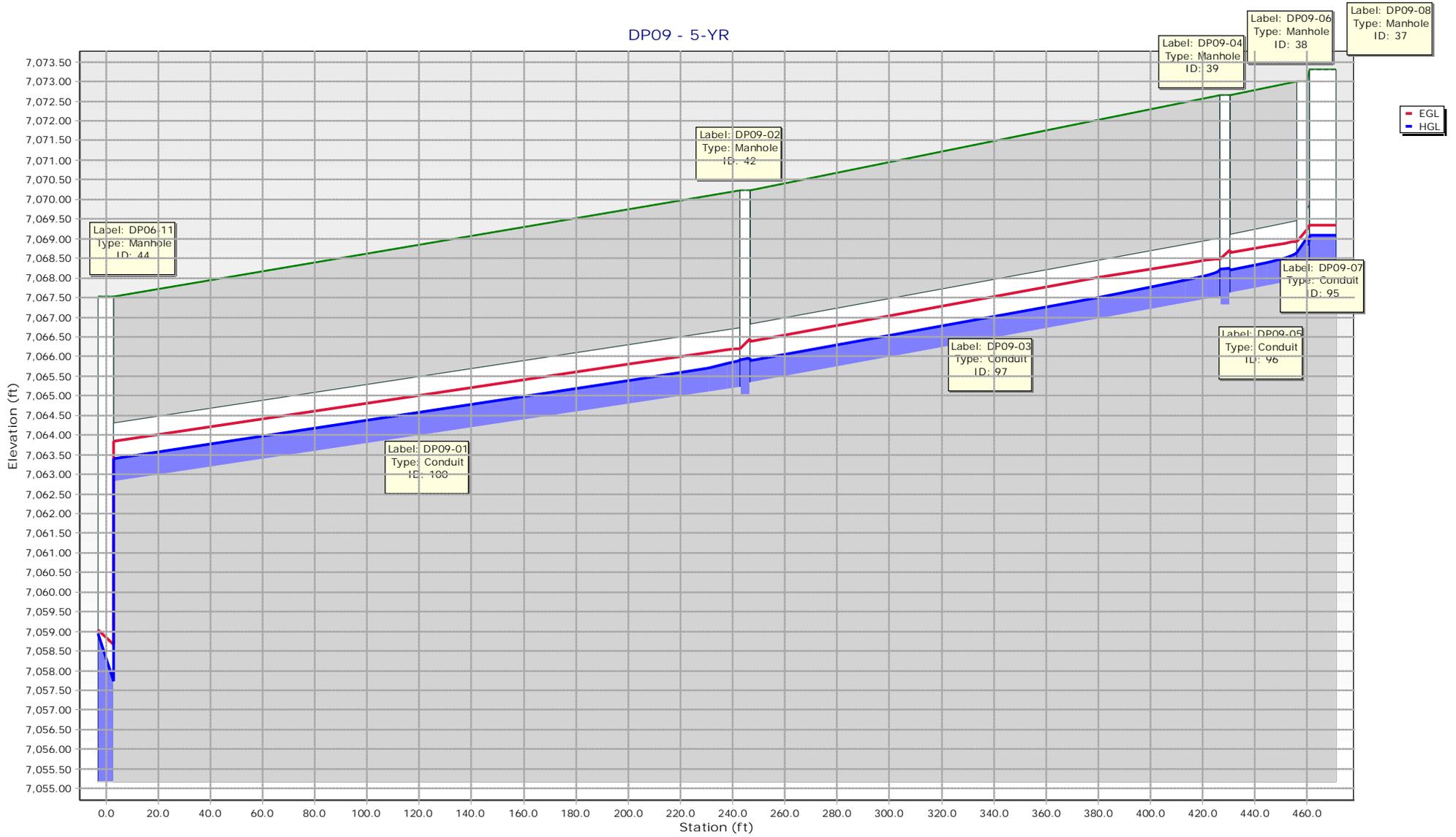




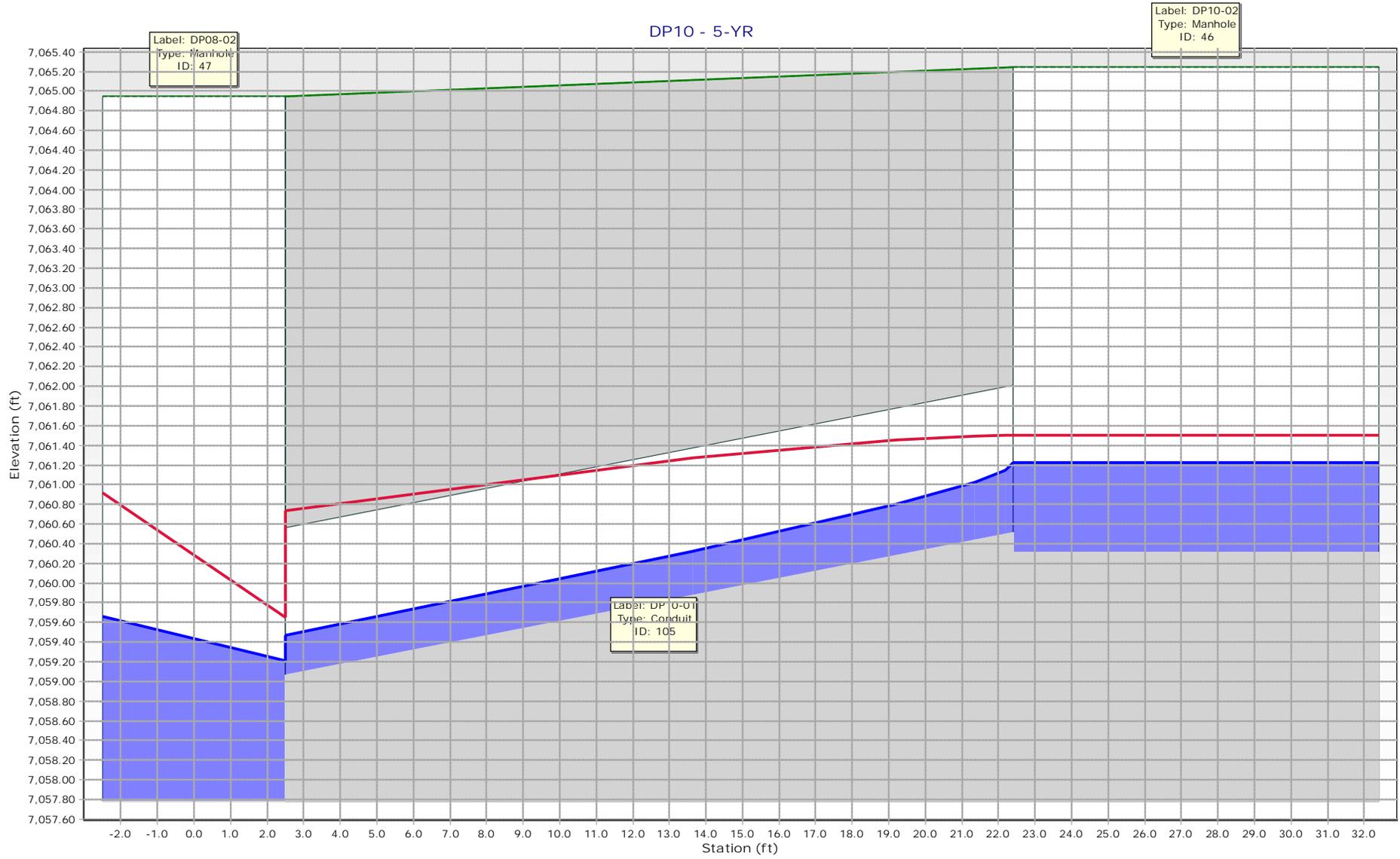
DPO8 - 5-YR



DPO9 - 5-YR

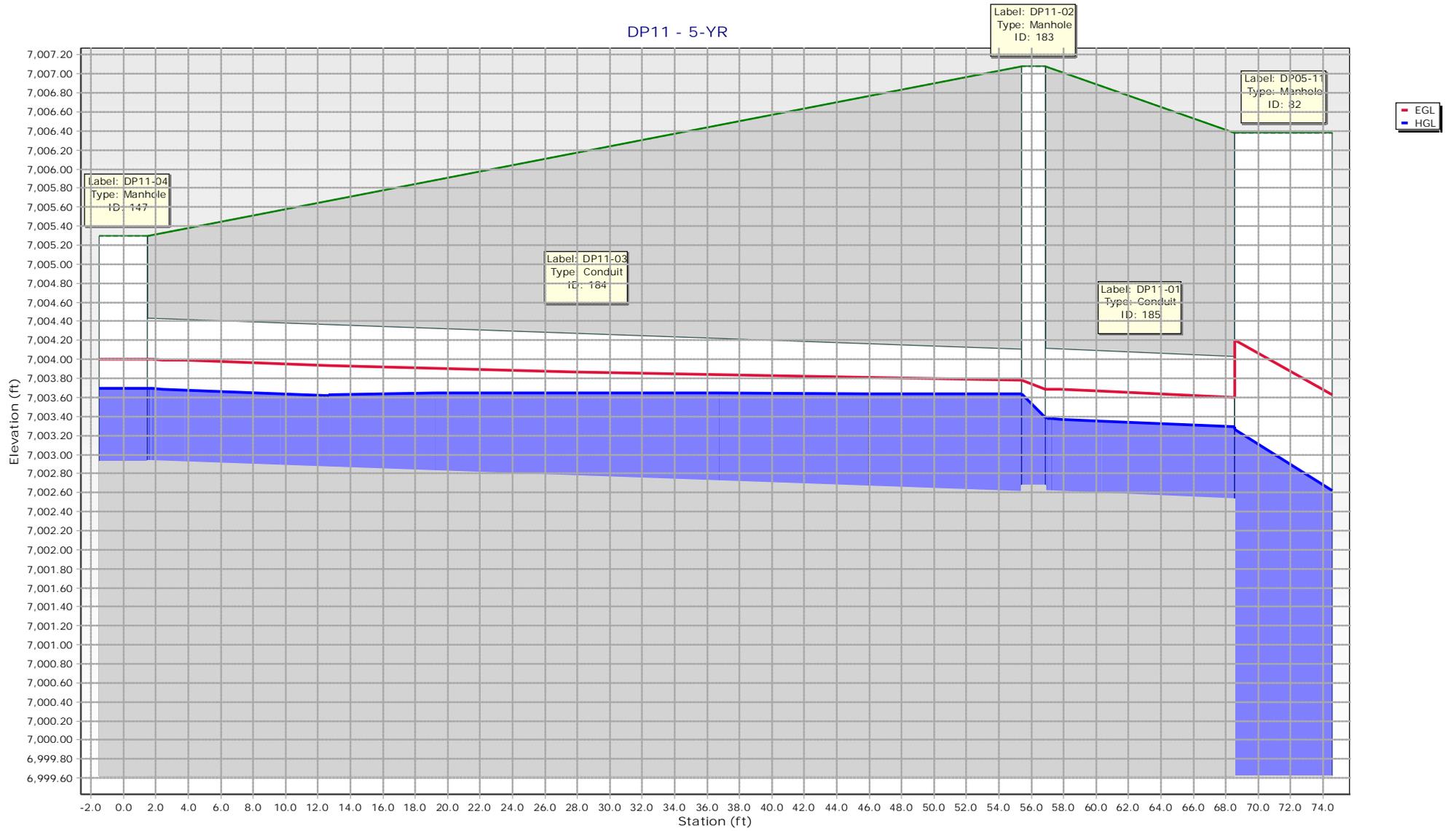


DP10 - 5-YR

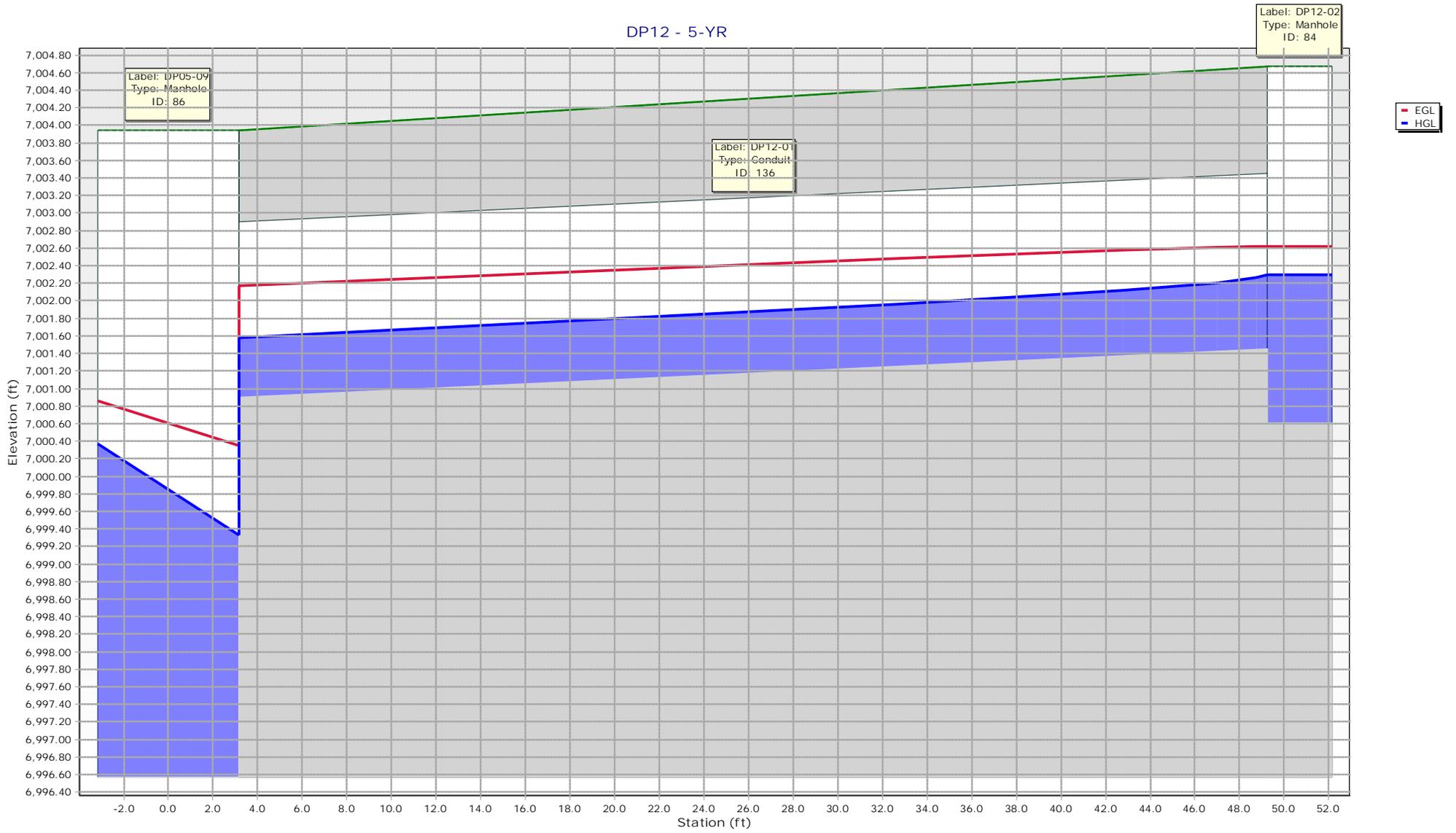


EGL  
HGL

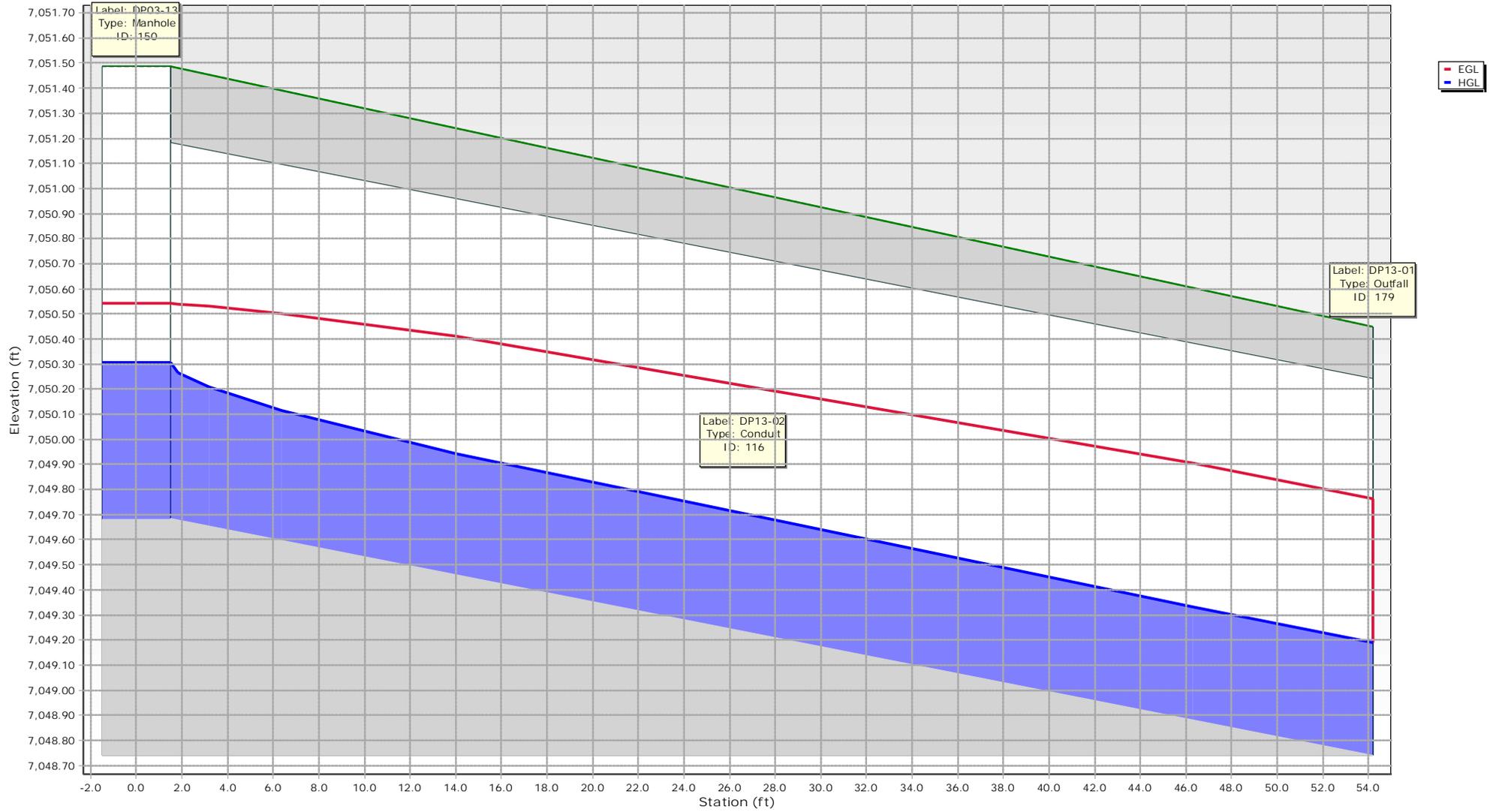
DP11 - 5-YR

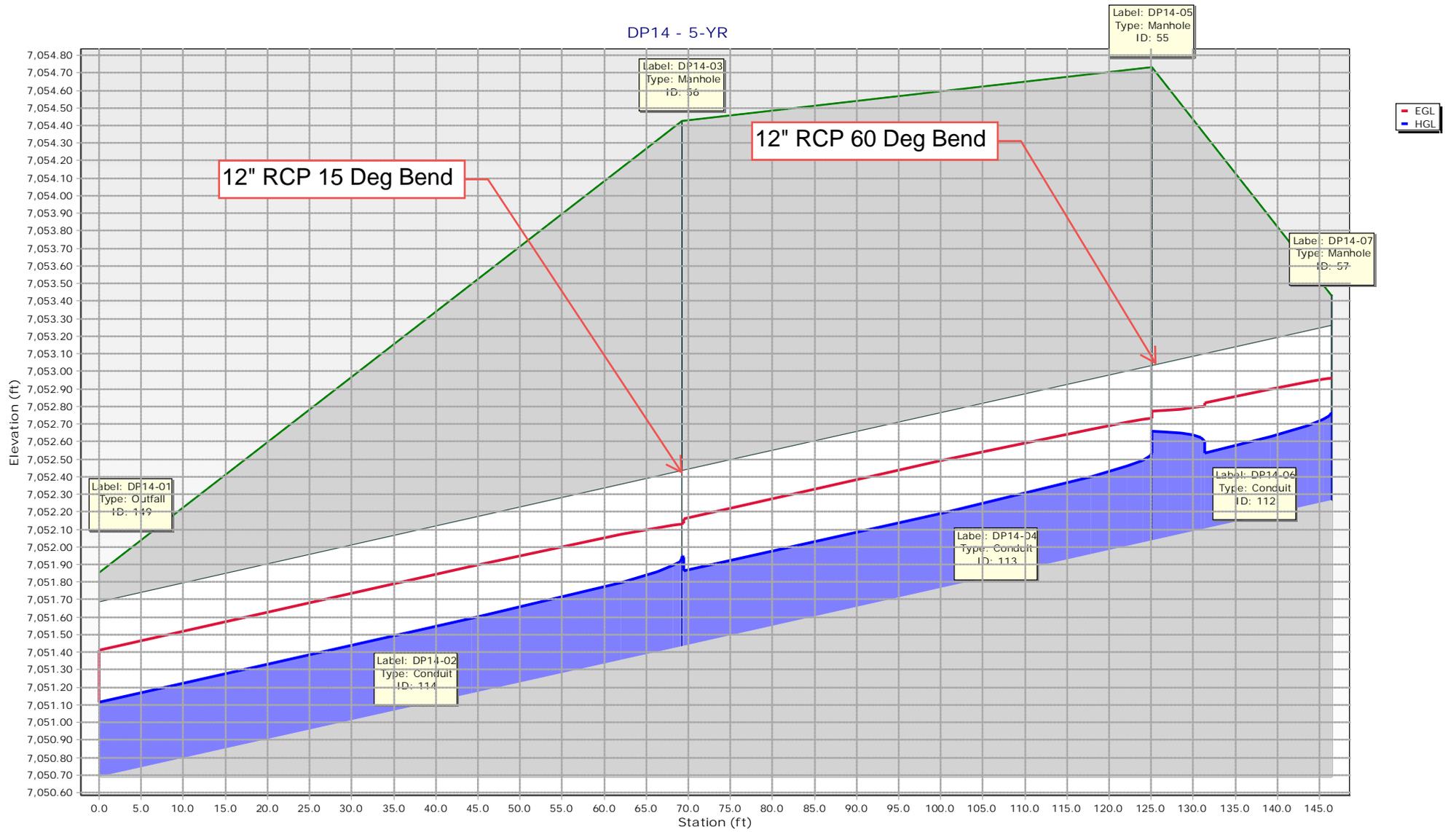


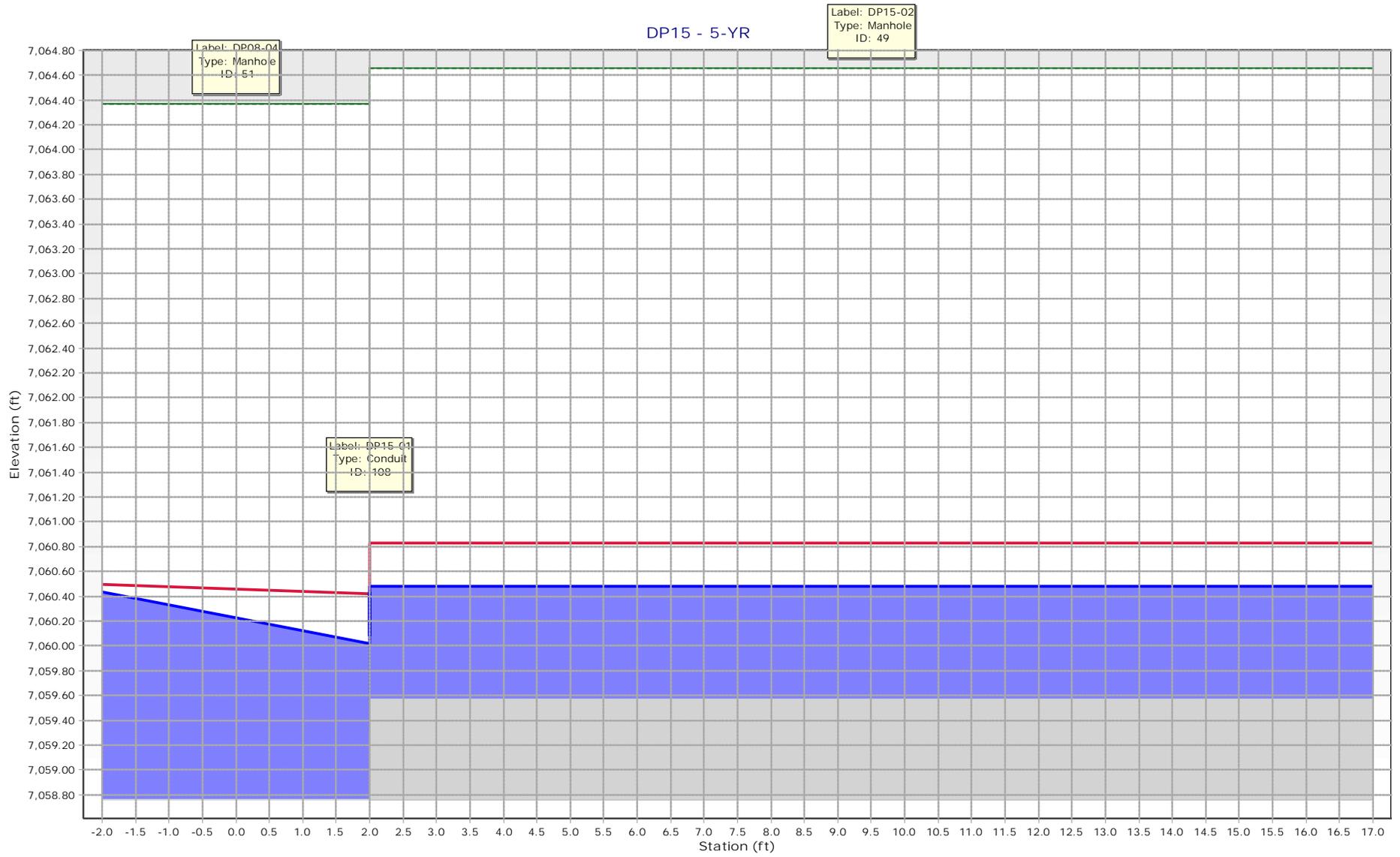
DP12 - 5-YR



DP13 - 5-YR







Label: DP08-04  
Type: Manhole  
ID: 51

Label: DP15-01  
Type: Conduit  
ID: 108

Label: DP15-02  
Type: Manhole  
ID: 49

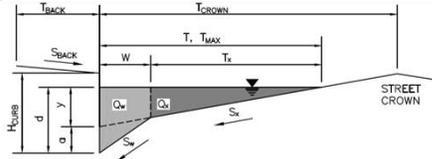
**ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)**

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project:  
Inlet ID:

Cloverleaf Subdivision

A



**Gutter Geometry (Enter data in the blue cells)**

Maximum Allowable Width for Spread Behind Curb  
 Side Slope Behind Curb (leave blank for no conveyance credit behind curb)  
 Manning's Roughness Behind Curb (typically between 0.012 and 0.020)  
 Height of Curb at Gutter Flow Line  
 Distance from Curb Face to Street Crown  
 Gutter Width  
 Street Transverse Slope  
 Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)  
 Street Longitudinal Slope - Enter 0 for sump condition  
 Manning's Roughness for Street Section (typically between 0.012 and 0.020)

$T_{BACK} = 7.5$  ft  
 $S_{BACK} = 0.020$  ft/ft  
 $n_{BACK} = 0.016$   
 $H_{CURB} = 4.00$  inches  
 $T_{CROWN} = 15.0$  ft  
 $W = 1.00$  ft  
 $S_x = 0.045$  ft/ft  
 $S_w = 0.083$  ft/ft  
 $S_o = 0.020$  ft/ft  
 $n_{STREET} = 0.016$

Max. Allowable Spread for Minor & Major Storm  
 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm  
 Allow Flow Depth at Street Crown (leave blank for no)

|             | Minor Storm              | Major Storm              |             |
|-------------|--------------------------|--------------------------|-------------|
| $T_{MAX} =$ | 15.0                     | 15.0                     | ft          |
| $d_{MAX} =$ | 4.0                      | 12.0                     | inches      |
|             | <input type="checkbox"/> | <input type="checkbox"/> | check = yes |

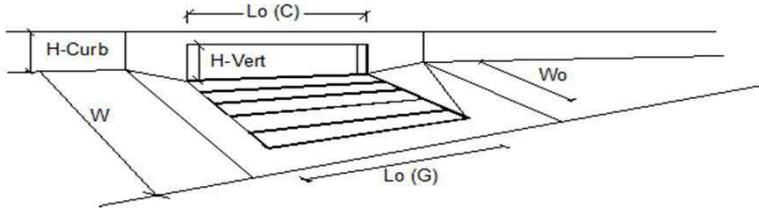
**MINOR STORM** Allowable Capacity is based on Depth Criterion  
**MAJOR STORM** Allowable Capacity is based on Spread Criterion

|               | Minor Storm | Major Storm |     |
|---------------|-------------|-------------|-----|
| $Q_{allow} =$ | 4.4         | 52.7        | cfs |

**WARNING: MINOR STORM max. allowable capacity is less than the design flow given on sheet 'Inlet Management'**  
**Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'**

## INLET ON A CONTINUOUS GRADE

Version 4.06 Released August 2018



| Design Information (Input)  | MINOR                    | MAJOR |        |
|---|--------------------------|-------|--------|
| Type of Inlet   | CDOT Type R Curb Opening |       |        |
| Local Depression (additional to continuous gutter depression 'a')         | 5.0                      | 5.0   | inches |
| Total Number of Units in the Inlet (Grate or Curb Opening)                | 1                        | 1     |        |
| Length of a Single Unit Inlet (Grate or Curb Opening)                     | 15.00                    | 15.00 | ft     |
| Width of a Unit Grate (cannot be greater than W, Gutter Width)            | N/A                      | N/A   | ft     |
| Clogging Factor for a Single Unit Grate (typical min. value = 0.5)        | N/A                      | N/A   |        |
| Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1) | 0.10                     | 0.10  |        |
| <b>Street Hydraulics: WARNING: Q &gt; ALLOWABLE Q FOR MINOR STORM!</b>    |                          |       |        |
| Total Inlet Interception Capacity   | 7.6                      | 13.9  | cfs    |
| Total Inlet Carry-Over Flow (flow bypassing inlet)                        | 0.2                      | 3.4   | cfs    |
| Capture Percentage = $Q_i/Q_o$ =  | 98                       | 80    | %      |

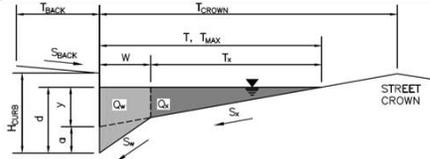
**ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)**

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project:  
Inlet ID:

Cloverleaf Subdivision

D



**Gutter Geometry (Enter data in the blue cells)**

Maximum Allowable Width for Spread Behind Curb  
 Side Slope Behind Curb (leave blank for no conveyance credit behind curb)  
 Manning's Roughness Behind Curb (typically between 0.012 and 0.020)  
 Height of Curb at Gutter Flow Line  
 Distance from Curb Face to Street Crown  
 Gutter Width  
 Street Transverse Slope  
 Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)  
 Street Longitudinal Slope - Enter 0 for sump condition  
 Manning's Roughness for Street Section (typically between 0.012 and 0.020)

$T_{BACK} = 7.5$  ft  
 $S_{BACK} = 0.020$  ft/ft  
 $n_{BACK} = 0.016$   
 $H_{CURB} = 4.00$  inches  
 $T_{CROWN} = 15.0$  ft  
 $W = 1.00$  ft  
 $S_x = 0.020$  ft/ft  
 $S_w = 0.083$  ft/ft  
 $S_o = 0.025$  ft/ft  
 $n_{STREET} = 0.016$

Max. Allowable Spread for Minor & Major Storm  
 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm  
 Allow Flow Depth at Street Crown (leave blank for no)

|             | Minor Storm              | Major Storm                         |             |
|-------------|--------------------------|-------------------------------------|-------------|
| $T_{MAX} =$ | 15.0                     | 15.0                                | ft          |
| $d_{MAX} =$ | 4.0                      | 12.0                                | inches      |
|             | <input type="checkbox"/> | <input checked="" type="checkbox"/> | check = yes |

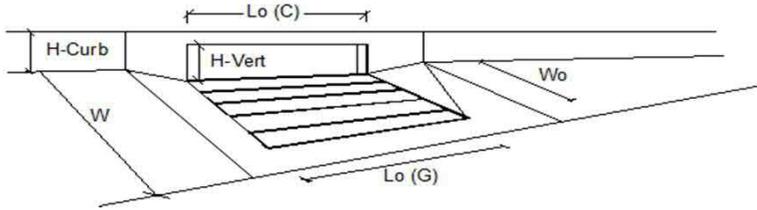
**MINOR STORM Allowable Capacity is based on Depth Criterion**  
**MAJOR STORM Allowable Capacity is based on Depth Criterion**

|               | Minor Storm | Major Storm |     |
|---------------|-------------|-------------|-----|
| $Q_{allow} =$ | 8.8         | 137.1       | cfs |

**Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'**  
**Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'**

## INLET ON A CONTINUOUS GRADE

Version 4.06 Released August 2018



| Design Information (Input)  | MINOR                    | MAJOR |        |
|---|--------------------------|-------|--------|
| Type of Inlet   | CDOT Type R Curb Opening |       |        |
| Local Depression (additional to continuous gutter depression 'a')         | 5.0                      | 5.0   | inches |
| Total Number of Units in the Inlet (Grate or Curb Opening)                | 1                        | 1     |        |
| Length of a Single Unit Inlet (Grate or Curb Opening)                     | 15.00                    | 15.00 | ft     |
| Width of a Unit Grate (cannot be greater than W, Gutter Width)            | N/A                      | N/A   | ft     |
| Clogging Factor for a Single Unit Grate (typical min. value = 0.5)        | N/A                      | N/A   |        |
| Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1) | 0.10                     | 0.10  |        |
| <b>Street Hydraulics: OK - Q &lt; Allowable Street Capacity</b>           |                          |       |        |
| Total Inlet Interception Capacity   | 5.9                      | 11.4  | cfs    |
| Total Inlet Carry-Over Flow (flow bypassing inlet)                        | 0.0                      | 1.6   | cfs    |
| Capture Percentage = $Q_i/Q_o$ =  | 100                      | 87    | %      |

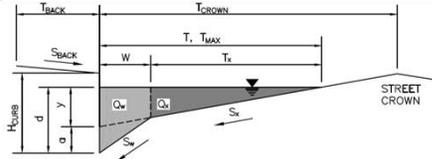
**ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)**

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project:  
Inlet ID:

Cloverleaf Subdivision

C



**Gutter Geometry (Enter data in the blue cells)**

Maximum Allowable Width for Spread Behind Curb  
 Side Slope Behind Curb (leave blank for no conveyance credit behind curb)  
 Manning's Roughness Behind Curb (typically between 0.012 and 0.020)  
 Height of Curb at Gutter Flow Line  
 Distance from Curb Face to Street Crown  
 Gutter Width  
 Street Transverse Slope  
 Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)  
 Street Longitudinal Slope - Enter 0 for sump condition  
 Manning's Roughness for Street Section (typically between 0.012 and 0.020)

$T_{BACK} = 7.5$  ft  
 $S_{BACK} = 0.020$  ft/ft  
 $n_{BACK} = 0.016$   
 $H_{CURB} = 4.00$  inches  
 $T_{CROWN} = 15.0$  ft  
 $W = 1.00$  ft  
 $S_X = 0.020$  ft/ft  
 $S_W = 0.083$  ft/ft  
 $S_O = 0.066$  ft/ft  
 $n_{STREET} = 0.016$

Max. Allowable Spread for Minor & Major Storm  
 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm  
 Allow Flow Depth at Street Crown (leave blank for no)

|           | Minor Storm              | Major Storm              |             |
|-----------|--------------------------|--------------------------|-------------|
| $T_{MAX}$ | 15.0                     | 15.0                     | ft          |
| $d_{MAX}$ | 4.0                      | 16.0                     | inches      |
|           | <input type="checkbox"/> | <input type="checkbox"/> | check = yes |

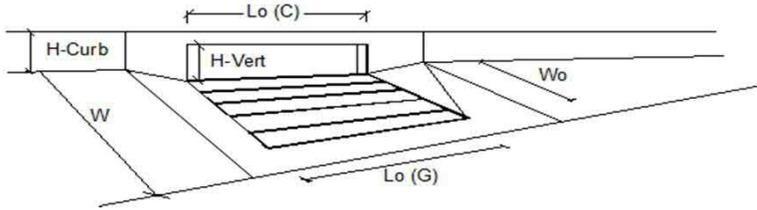
**MINOR STORM Allowable Capacity is based on Depth Criterion**  
**MAJOR STORM Allowable Capacity is based on Spread Criterion**

|             | Minor Storm | Major Storm |     |
|-------------|-------------|-------------|-----|
| $Q_{allow}$ | 14.3        | 18.8        | cfs |

**Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'**  
**Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'**

## INLET ON A CONTINUOUS GRADE

Version 4.06 Released August 2018



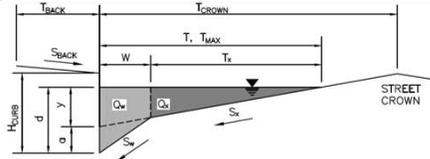
| <b>Design Information (Input)</b>   | MINOR                    | MAJOR |        |
|---|--------------------------|-------|--------|
| Type of Inlet   | CDOT Type R Curb Opening |       |        |
| Local Depression (additional to continuous gutter depression 'a')         | 5.0                      | 5.0   | inches |
| Total Number of Units in the Inlet (Grate or Curb Opening)                | 1                        | 1     |        |
| Length of a Single Unit Inlet (Grate or Curb Opening)                     | 15.00                    | 15.00 | ft     |
| Width of a Unit Grate (cannot be greater than W, Gutter Width)            | N/A                      | N/A   | ft     |
| Clogging Factor for a Single Unit Grate (typical min. value = 0.5)        | N/A                      | N/A   |        |
| Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1) | 0.10                     | 0.10  |        |
| <b>Street Hydraulics: OK - Q &lt; Allowable Street Capacity</b>           |                          |       |        |
| Total Inlet Interception Capacity   | 4.4                      | 9.2   | cfs    |
| Total Inlet Carry-Over Flow (flow bypassing inlet)                        | 0.0                      | 0.2   | cfs    |
| Capture Percentage = $Q_i/Q_o$ =  | 100                      | 97    | %      |

**ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)**

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: Cloverleaf Subdivision

Inlet ID: 1



**Gutter Geometry (Enter data in the blue cells)**

Maximum Allowable Width for Spread Behind Curb  
 Side Slope Behind Curb (leave blank for no conveyance credit behind curb)  
 Manning's Roughness Behind Curb (typically between 0.012 and 0.020)  
 Height of Curb at Gutter Flow Line  
 Distance from Curb Face to Street Crown  
 Gutter Width  
 Street Transverse Slope  
 Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)  
 Street Longitudinal Slope - Enter 0 for sump condition  
 Manning's Roughness for Street Section (typically between 0.012 and 0.020)

$T_{BACK} = 7.5$  ft  
 $S_{BACK} = 0.020$  ft/ft  
 $n_{BACK} = 0.016$   
 $H_{CURB} = 4.00$  inches  
 $T_{CROWN} = 15.0$  ft  
 $W = 1.00$  ft  
 $S_x = 0.020$  ft/ft  
 $S_w = 0.083$  ft/ft  
 $S_o = 0.000$  ft/ft  
 $n_{STREET} = 0.016$

**Warning 02** Max. Allowable Spread for Minor & Major Storm  
 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm  
 Check boxes are not applicable in SUMP conditions

|             | Minor Storm              | Major Storm              |        |
|-------------|--------------------------|--------------------------|--------|
| $T_{MAX} =$ | 15.0                     | 15.0                     | ft     |
| $d_{MAX} =$ | 5.0                      | 12.0                     | inches |
|             | <input type="checkbox"/> | <input type="checkbox"/> |        |

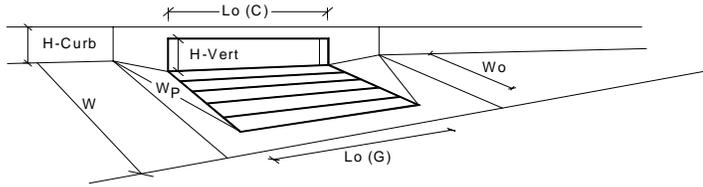
**MINOR STORM** Allowable Capacity is based on Depth Criterion  
**MAJOR STORM** Allowable Capacity is based on Depth Criterion

$Q_{allow} =$ 

| Minor Storm | Major Storm |     |
|-------------|-------------|-----|
| SUMP        | SUMP        | cfs |

## INLET IN A SUMP OR SAG LOCATION

Version 4.06 Released August 2018



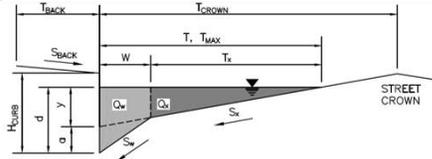
| <b>Design Information (Input)</b>  | MINOR                    | MAJOR |   |
|--|--------------------------|-------|---|
| Type of Inlet  | CDOT Type R Curb Opening |       |   |
| Local Depression (additional to continuous gutter depression 'a' from above) | 5.00                     | 5.00  | inches  |
| Number of Unit Inlets (Grate or Curb Opening)                                | 1                        | 1     |   |
| Water Depth at Flowline (outside of local depression)                        | 4.6                      | 6.6   | inches  |
| <b>Grate Information</b>   | MINOR                    | MAJOR | <input checked="" type="checkbox"/> Override Depths |
| Length of a Unit Grate   | N/A                      | N/A   | feet  |
| Width of a Unit Grate  | N/A                      | N/A   | feet  |
| Area Opening Ratio for a Grate (typical values 0.15-0.90)                    | N/A                      | N/A   |   |
| Clogging Factor for a Single Grate (typical value 0.50 - 0.70)               | N/A                      | N/A   |   |
| Grate Weir Coefficient (typical value 2.15 - 3.60)                           | N/A                      | N/A   |   |
| Grate Orifice Coefficient (typical value 0.60 - 0.80)                        | N/A                      | N/A   |   |
| <b>Curb Opening Information</b>  | MINOR                    | MAJOR |   |
| Length of a Unit Curb Opening  | 10.00                    | 10.00 | feet  |
| Height of Vertical Curb Opening in Inches                                    | 6.00                     | 6.00  | inches  |
| Height of Curb Orifice Throat in Inches                                      | 6.00                     | 6.00  | inches  |
| Angle of Throat (see USDCM Figure ST-5)                                      | 63.40                    | 63.40 | degrees   |
| Side Width for Depression Pan (typically the gutter width of 2 feet)         | 1.00                     | 1.00  | feet  |
| Clogging Factor for a Single Curb Opening (typical value 0.10)               | 0.10                     | 0.10  |   |
| Curb Opening Weir Coefficient (typical value 2.3-3.7)                        | 3.60                     | 3.60  |   |
| Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)                 | 0.67                     | 0.67  |   |
| <b>Low Head Performance Reduction (Calculated)</b>                           | MINOR                    | MAJOR |   |
| Depth for Grate Midwidth   | N/A                      | N/A   | ft  |
| Depth for Curb Opening Weir Equation   | 0.30                     | 0.47  | ft  |
| Combination Inlet Performance Reduction Factor for Long Inlets               | 0.44                     | 0.63  |   |
| Curb Opening Performance Reduction Factor for Long Inlets                    | 0.84                     | 0.97  |   |
| Grated Inlet Performance Reduction Factor for Long Inlets                    | N/A                      | N/A   |   |
| <b>Total Inlet Interception Capacity (assumes clogged condition)</b>         | MINOR                    | MAJOR |   |
| <b>Q<sub>a</sub></b>   | 5.6                      | 12.5  | cfs   |
| Q <sub>PEAK REQUIRED</sub>   | 5.6                      | 12.4  | cfs   |

**ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)**

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: **Cloverleaf Subdivision**

Inlet ID: **E**



**Gutter Geometry (Enter data in the blue cells)**

Maximum Allowable Width for Spread Behind Curb  
 Side Slope Behind Curb (leave blank for no conveyance credit behind curb)  
 Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

$T_{BACK} = 7.5$  ft  
 $S_{BACK} = 0.020$  ft/ft  
 $n_{BACK} = 0.016$

Height of Curb at Gutter Flow Line  
 Distance from Curb Face to Street Crown  
 Gutter Width  
 Street Transverse Slope  
 Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)  
 Street Longitudinal Slope - Enter 0 for sump condition  
 Manning's Roughness for Street Section (typically between 0.012 and 0.020)

$H_{CURB} = 4.00$  inches  
 $T_{CROWN} = 15.0$  ft  
 $W = 1.00$  ft  
 $S_x = 0.020$  ft/ft  
 $S_w = 0.083$  ft/ft  
 $S_o = 0.055$  ft/ft  
 $n_{STREET} = 0.016$

Max. Allowable Spread for Minor & Major Storm  
 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm  
 Allow Flow Depth at Street Crown (leave blank for no)

|           | Minor Storm | Major Storm |        |
|-----------|-------------|-------------|--------|
| $T_{MAX}$ | 15.0        | 15.0        | ft     |
| $d_{MAX}$ | 4.0         | 12.0        | inches |

check = yes

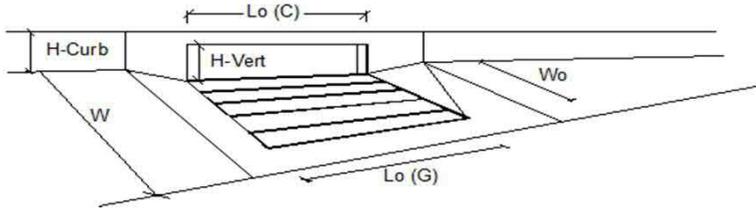
**MINOR STORM Allowable Capacity is based on Depth Criterion**  
**MAJOR STORM Allowable Capacity is based on Spread Criterion**

|             | Minor Storm | Major Storm |     |
|-------------|-------------|-------------|-----|
| $Q_{allow}$ | 13.0        | 17.1        | cfs |

Minor storm max. allowable capacity **GOOD** - greater than the design flow given on sheet 'Inlet Management'  
 Major storm max. allowable capacity **GOOD** - greater than the design flow given on sheet 'Inlet Management'

## INLET ON A CONTINUOUS GRADE

Version 4.06 Released August 2018



| <b>Design Information (Input)</b>   | MINOR                           | MAJOR |        |
|---|---------------------------------|-------|--------|
| Type of Inlet   | Type = CDOT Type R Curb Opening |       |        |
| Local Depression (additional to continuous gutter depression 'a')         | 5.0                             | 5.0   | inches |
| Total Number of Units in the Inlet (Grate or Curb Opening)                | 1                               | 1     |        |
| Length of a Single Unit Inlet (Grate or Curb Opening)                     | 5.00                            | 5.00  | ft     |
| Width of a Unit Grate (cannot be greater than W, Gutter Width)            | N/A                             | N/A   | ft     |
| Clogging Factor for a Single Unit Grate (typical min. value = 0.5)        | N/A                             | N/A   |        |
| Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1) | 0.10                            | 0.10  |        |
| <b>Street Hydraulics: OK - Q &lt; Allowable Street Capacity</b>           |                                 |       |        |
| Total Inlet Interception Capacity   | Q = 1.0                         | 1.9   | cfs    |
| Total Inlet Carry-Over Flow (flow bypassing inlet)                        | Q <sub>b</sub> = 0.0            | 0.1   | cfs    |
| Capture Percentage = Q <sub>i</sub> /Q <sub>b</sub> =                     | C% = 100                        | 93    | %      |

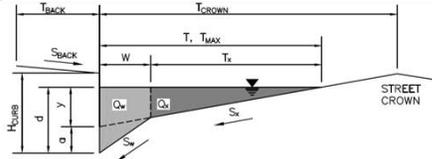
**ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)**

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project:  
Inlet ID:

Cloverleaf Subdivision

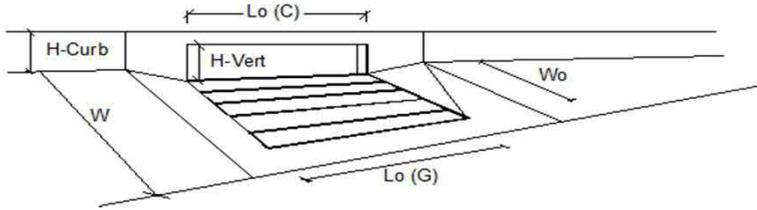
F



| Gutter Geometry (Enter data in the blue cells)   |   |             |             |  |                   |        |        |
|--|---|-------------|-------------|--|-------------------|--------|--------|
| Maximum Allowable Width for Spread Behind Curb   | $T_{BACK} = 7.5$ ft   |             |             |  |                   |        |        |
| Side Slope Behind Curb (leave blank for no conveyance credit behind curb)  | $S_{BACK} = 0.020$ ft/ft  |             |             |  |                   |        |        |
| Manning's Roughness Behind Curb (typically between 0.012 and 0.020)  | $n_{BACK} = 0.016$  |             |             |  |                   |        |        |
| Height of Curb at Gutter Flow Line   | $H_{CURB} = 4.00$ inches  |             |             |  |                   |        |        |
| Distance from Curb Face to Street Crown  | $T_{CROWN} = 15.0$ ft   |             |             |  |                   |        |        |
| Gutter Width   | $W = 1.00$ ft   |             |             |  |                   |        |        |
| Street Transverse Slope  | $S_X = 0.020$ ft/ft   |             |             |  |                   |        |        |
| Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)  | $S_W = 0.083$ ft/ft   |             |             |  |                   |        |        |
| Street Longitudinal Slope - Enter 0 for sump condition   | $S_O = 0.015$ ft/ft   |             |             |  |                   |        |        |
| Manning's Roughness for Street Section (typically between 0.012 and 0.020)                                       | $n_{STREET} = 0.016$  |             |             |  |                   |        |        |
| Max. Allowable Spread for Minor & Major Storm  | <table style="width: 100%; border: none;"> <tr> <td style="width: 50%; text-align: center;">Minor Storm</td> <td style="width: 50%; text-align: center;">Major Storm</td> <td style="width: 10%;"></td> </tr> <tr> <td style="border: 1px solid black; text-align: center;"><math>T_{MAX} = 15.0</math></td> <td style="border: 1px solid black; text-align: center;"><math>15.0</math></td> <td style="text-align: right;">ft</td> </tr> </table>    | Minor Storm | Major Storm |  | $T_{MAX} = 15.0$  | $15.0$ | ft     |
| Minor Storm  | Major Storm   |             |             |  |                   |        |        |
| $T_{MAX} = 15.0$   | $15.0$  | ft          |             |  |                   |        |        |
| Max. Allowable Depth at Gutter Flowline for Minor & Major Storm  | <table style="width: 100%; border: none;"> <tr> <td style="width: 50%; text-align: center;">Minor Storm</td> <td style="width: 50%; text-align: center;">Major Storm</td> <td style="width: 10%;"></td> </tr> <tr> <td style="border: 1px solid black; text-align: center;"><math>d_{MAX} = 4.0</math></td> <td style="border: 1px solid black; text-align: center;"><math>12.0</math></td> <td style="text-align: right;">inches</td> </tr> </table> | Minor Storm | Major Storm |  | $d_{MAX} = 4.0$   | $12.0$ | inches |
| Minor Storm  | Major Storm   |             |             |  |                   |        |        |
| $d_{MAX} = 4.0$  | $12.0$  | inches      |             |  |                   |        |        |
| Allow Flow Depth at Street Crown (leave blank for no)  | <input type="checkbox"/> <input type="checkbox"/> check = yes   |             |             |  |                   |        |        |
| <b>MINOR STORM Allowable Capacity is based on Depth Criterion</b>  |   |             |             |  |                   |        |        |
| <b>MAJOR STORM Allowable Capacity is based on Spread Criterion</b>   |   |             |             |  |                   |        |        |
| <b>Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'</b> |   |             |             |  |                   |        |        |
| <b>Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'</b> |   |             |             |  |                   |        |        |
| Allowable Capacity   | <table style="width: 100%; border: none;"> <tr> <td style="width: 50%; text-align: center;">Minor Storm</td> <td style="width: 50%; text-align: center;">Major Storm</td> <td style="width: 10%;"></td> </tr> <tr> <td style="border: 1px solid black; text-align: center;"><math>Q_{allow} = 6.8</math></td> <td style="border: 1px solid black; text-align: center;"><math>8.9</math></td> <td style="text-align: right;">cfs</td> </tr> </table>   | Minor Storm | Major Storm |  | $Q_{allow} = 6.8$ | $8.9$  | cfs    |
| Minor Storm  | Major Storm   |             |             |  |                   |        |        |
| $Q_{allow} = 6.8$  | $8.9$   | cfs         |             |  |                   |        |        |

## INLET ON A CONTINUOUS GRADE

Version 4.06 Released August 2018



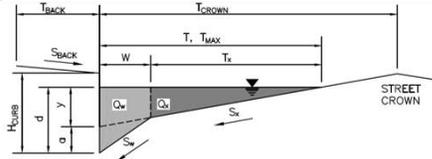
| <b>Design Information (Input)</b>   | MINOR                    | MAJOR |        |
|---|--------------------------|-------|--------|
| Type of Inlet   | CDOT Type R Curb Opening |       |        |
| Local Depression (additional to continuous gutter depression 'a')         | 5.0                      | 5.0   | inches |
| Total Number of Units in the Inlet (Grate or Curb Opening)                | 1                        | 1     |        |
| Length of a Single Unit Inlet (Grate or Curb Opening)                     | 10.00                    | 10.00 | ft     |
| Width of a Unit Grate (cannot be greater than W, Gutter Width)            | N/A                      | N/A   | ft     |
| Clogging Factor for a Single Unit Grate (typical min. value = 0.5)        | N/A                      | N/A   |        |
| Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1) | 0.10                     | 0.10  |        |
| <b>Street Hydraulics: OK - Q &lt; Allowable Street Capacity</b>           |                          |       |        |
| Total Inlet Interception Capacity   | 3.4                      | 6.0   | cfs    |
| Total Inlet Carry-Over Flow (flow bypassing inlet)                        | 0.0                      | 0.9   | cfs    |
| Capture Percentage = $Q_i/Q_o$ =  | 100                      | 87    | %      |

**ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)**

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project:  
Inlet ID:

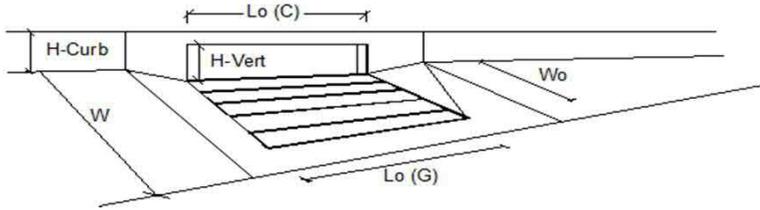
Cloverleaf Subdivision  
IA



| Gutter Geometry (Enter data in the blue cells)   |  |             |             |        |      |      |  |
|--|--|-------------|-------------|--------|------|------|--|
| Maximum Allowable Width for Spread Behind Curb   | $T_{BACK} = 7.5$ ft  |             |             |        |      |      |  |
| Side Slope Behind Curb (leave blank for no conveyance credit behind curb)  | $S_{BACK} = 0.020$ ft/ft   |             |             |        |      |      |  |
| Manning's Roughness Behind Curb (typically between 0.012 and 0.020)  | $n_{BACK} = 0.016$   |             |             |        |      |      |  |
| Height of Curb at Gutter Flow Line   | $H_{CURB} = 4.00$ inches   |             |             |        |      |      |  |
| Distance from Curb Face to Street Crown  | $T_{CROWN} = 15.0$ ft  |             |             |        |      |      |  |
| Gutter Width   | $W = 1.00$ ft  |             |             |        |      |      |  |
| Street Transverse Slope  | $S_x = 0.020$ ft/ft  |             |             |        |      |      |  |
| Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)  | $S_w = 0.083$ ft/ft  |             |             |        |      |      |  |
| Street Longitudinal Slope - Enter 0 for sump condition   | $S_o = 0.015$ ft/ft  |             |             |        |      |      |  |
| Manning's Roughness for Street Section (typically between 0.012 and 0.020)                                       | $n_{STREET} = 0.016$   |             |             |        |      |      |  |
| Max. Allowable Spread for Minor & Major Storm  | <table border="1"> <tr> <th>Minor Storm</th> <th>Major Storm</th> <th>ft</th> </tr> <tr> <td>15.0</td> <td>15.0</td> <td></td> </tr> </table>    | Minor Storm | Major Storm | ft     | 15.0 | 15.0 |  |
| Minor Storm  | Major Storm  | ft          |             |        |      |      |  |
| 15.0   | 15.0   |             |             |        |      |      |  |
| Max. Allowable Depth at Gutter Flowline for Minor & Major Storm  | <table border="1"> <tr> <th>Minor Storm</th> <th>Major Storm</th> <th>inches</th> </tr> <tr> <td>4.0</td> <td>12.0</td> <td></td> </tr> </table> | Minor Storm | Major Storm | inches | 4.0  | 12.0 |  |
| Minor Storm  | Major Storm  | inches      |             |        |      |      |  |
| 4.0  | 12.0   |             |             |        |      |      |  |
| Allow Flow Depth at Street Crown (leave blank for no)  | <input type="checkbox"/> <input type="checkbox"/> check = yes  |             |             |        |      |      |  |
| <b>MINOR STORM Allowable Capacity is based on Depth Criterion</b>  |  |             |             |        |      |      |  |
| <b>MAJOR STORM Allowable Capacity is based on Spread Criterion</b>   |  |             |             |        |      |      |  |
| <b>Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'</b> |  |             |             |        |      |      |  |
| <b>Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'</b> |  |             |             |        |      |      |  |
| $Q_{allow} =$  | <table border="1"> <tr> <th>Minor Storm</th> <th>Major Storm</th> <th>cfs</th> </tr> <tr> <td>6.8</td> <td>8.9</td> <td></td> </tr> </table>     | Minor Storm | Major Storm | cfs    | 6.8  | 8.9  |  |
| Minor Storm  | Major Storm  | cfs         |             |        |      |      |  |
| 6.8  | 8.9  |             |             |        |      |      |  |

## INLET ON A CONTINUOUS GRADE

Version 4.06 Released August 2018



| Design Information (Input)  | MINOR                    | MAJOR |        |
|---|--------------------------|-------|--------|
| Type of Inlet   | CDOT Type R Curb Opening |       |        |
| Local Depression (additional to continuous gutter depression 'a')         | 5.0                      | 5.0   | inches |
| Total Number of Units in the Inlet (Grate or Curb Opening)                | 1                        | 1     |        |
| Length of a Single Unit Inlet (Grate or Curb Opening)                     | 10.00                    | 10.00 | ft     |
| Width of a Unit Grate (cannot be greater than W, Gutter Width)            | N/A                      | N/A   | ft     |
| Clogging Factor for a Single Unit Grate (typical min. value = 0.5)        | N/A                      | N/A   |        |
| Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1) | 0.10                     | 0.10  |        |
| <b>Street Hydraulics: OK - Q &lt; Allowable Street Capacity</b>           |                          |       |        |
| Total Inlet Interception Capacity   | 3.5                      | 6.2   | cfs    |
| Total Inlet Carry-Over Flow (flow bypassing inlet)                        | 0.0                      | 1.1   | cfs    |
| Capture Percentage = $Q_i/Q_o$ =  | 100                      | 85    | %      |

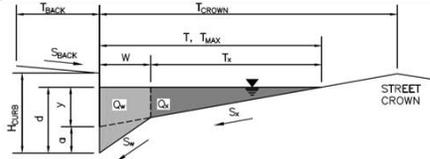
**ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)**

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project:  
Inlet ID:

Cloverleaf Subdivision

G



**Gutter Geometry (Enter data in the blue cells)**

Maximum Allowable Width for Spread Behind Curb  
Side Slope Behind Curb (leave blank for no conveyance credit behind curb)  
Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

$T_{BACK} = 7.5$  ft  
 $S_{BACK} = 0.020$  ft/ft  
 $n_{BACK} = 0.016$

Height of Curb at Gutter Flow Line  
Distance from Curb Face to Street Crown  
Gutter Width  
Street Transverse Slope  
Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)  
Street Longitudinal Slope - Enter 0 for sump condition  
Manning's Roughness for Street Section (typically between 0.012 and 0.020)

$H_{CURB} = 4.00$  inches  
 $T_{CROWN} = 15.0$  ft  
 $W = 1.00$  ft  
 $S_x = 0.020$  ft/ft  
 $S_w = 0.083$  ft/ft  
 $S_o = 0.020$  ft/ft  
 $n_{STREET} = 0.016$

Max. Allowable Spread for Minor & Major Storm  
Max. Allowable Depth at Gutter Flowline for Minor & Major Storm  
Allow Flow Depth at Street Crown (leave blank for no)

|             | Minor Storm              | Major Storm              |             |
|-------------|--------------------------|--------------------------|-------------|
| $T_{MAX} =$ | 15.0                     | 15.0                     | ft          |
| $d_{MAX} =$ | 4.0                      | 12.0                     | inches      |
|             | <input type="checkbox"/> | <input type="checkbox"/> | check = yes |

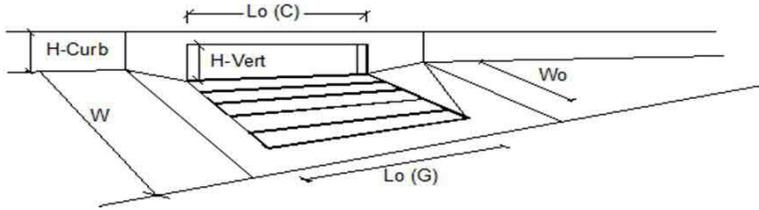
**MINOR STORM Allowable Capacity is based on Depth Criterion**  
**MAJOR STORM Allowable Capacity is based on Spread Criterion**

|               | Minor Storm | Major Storm |     |
|---------------|-------------|-------------|-----|
| $Q_{allow} =$ | 7.9         | 10.3        | cfs |

**Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'**  
**Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'**

## INLET ON A CONTINUOUS GRADE

Version 4.06 Released August 2018

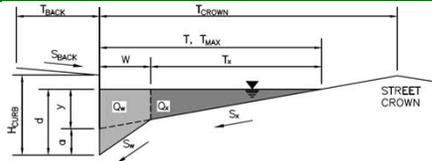


| Design Information (Input)  | MINOR                    | MAJOR |        |
|---|--------------------------|-------|--------|
| Type of Inlet   | CDOT Type R Curb Opening |       |        |
| Local Depression (additional to continuous gutter depression 'a')         | 5.0                      | 5.0   | inches |
| Total Number of Units in the Inlet (Grate or Curb Opening)                | 1                        | 1     |        |
| Length of a Single Unit Inlet (Grate or Curb Opening)                     | 5.00                     | 5.00  | ft     |
| Width of a Unit Grate (cannot be greater than W, Gutter Width)            | N/A                      | N/A   | ft     |
| Clogging Factor for a Single Unit Grate (typical min. value = 0.5)        | N/A                      | N/A   |        |
| Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1) | 0.10                     | 0.10  |        |
| <b>Street Hydraulics: OK - Q &lt; Allowable Street Capacity</b>           |                          |       |        |
| Total Inlet Interception Capacity   | 2.1                      | 3.0   | cfs    |
| Total Inlet Carry-Over Flow (flow bypassing inlet)                        | 0.3                      | 2.1   | cfs    |
| Capture Percentage = $Q_i/Q_o$ =  | 86                       | 60    | %      |

**ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)**

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: \_\_\_\_\_  
 Inlet ID: \_\_\_\_\_  
 Cloverleaf Subdivision  
 H

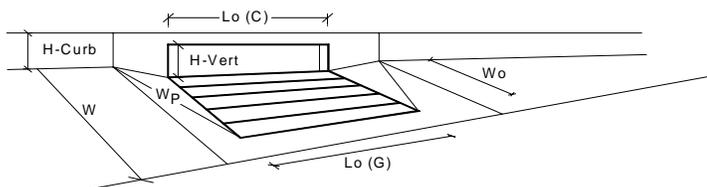


| Gutter Geometry (Enter data in the blue cells)                             |  |             |             |        |                           |                           |  |
|--|--|-------------|-------------|--------|---------------------------|---------------------------|--|
| Maximum Allowable Width for Spread Behind Curb                             | $T_{BACK} = 7.5$ ft  |             |             |        |                           |                           |  |
| Side Slope Behind Curb (leave blank for no conveyance credit behind curb)  | $S_{BACK} = 0.020$ ft/ft   |             |             |        |                           |                           |  |
| Manning's Roughness Behind Curb (typically between 0.012 and 0.020)        | $n_{BACK} = 0.016$   |             |             |        |                           |                           |  |
| Height of Curb at Gutter Flow Line   | $H_{CURB} = 4.00$ inches   |             |             |        |                           |                           |  |
| Distance from Curb Face to Street Crown                                    | $T_{CROWN} = 15.0$ ft  |             |             |        |                           |                           |  |
| Gutter Width   | $W = 1.00$ ft  |             |             |        |                           |                           |  |
| Street Transverse Slope  | $S_x = 0.020$ ft/ft  |             |             |        |                           |                           |  |
| Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)      | $S_w = 0.083$ ft/ft  |             |             |        |                           |                           |  |
| Street Longitudinal Slope - Enter 0 for sump condition                     | $S_o = 0.000$ ft/ft  |             |             |        |                           |                           |  |
| Manning's Roughness for Street Section (typically between 0.012 and 0.020) | $n_{STREET} = 0.016$   |             |             |        |                           |                           |  |
| Max. Allowable Spread for Minor & Major Storm                              | <table border="1"> <tr> <th>Minor Storm</th> <th>Major Storm</th> <th>ft</th> </tr> <tr> <td><math>T_{MAX} = 15.0</math></td> <td><math>T_{MAX} = 15.0</math></td> <td></td> </tr> </table>                    | Minor Storm | Major Storm | ft     | $T_{MAX} = 15.0$          | $T_{MAX} = 15.0$          |  |
| Minor Storm  | Major Storm  | ft          |             |        |                           |                           |  |
| $T_{MAX} = 15.0$   | $T_{MAX} = 15.0$   |             |             |        |                           |                           |  |
| Max. Allowable Depth at Gutter Flowline for Minor & Major Storm            | <table border="1"> <tr> <th>Minor Storm</th> <th>Major Storm</th> <th>inches</th> </tr> <tr> <td><math>d_{MAX} = 5.0</math></td> <td><math>d_{MAX} = 12.0</math></td> <td></td> </tr> </table>                 | Minor Storm | Major Storm | inches | $d_{MAX} = 5.0$           | $d_{MAX} = 12.0$          |  |
| Minor Storm  | Major Storm  | inches      |             |        |                           |                           |  |
| $d_{MAX} = 5.0$  | $d_{MAX} = 12.0$   |             |             |        |                           |                           |  |
| Check boxes are not applicable in SUMP conditions                          | <input type="checkbox"/> <input type="checkbox"/>  |             |             |        |                           |                           |  |
| <b>MINOR STORM Allowable Capacity is based on Depth Criterion</b>          |  |             |             |        |                           |                           |  |
| <b>MAJOR STORM Allowable Capacity is based on Depth Criterion</b>          |  |             |             |        |                           |                           |  |
|  | <table border="1"> <tr> <th>Minor Storm</th> <th>Major Storm</th> <th>cfs</th> </tr> <tr> <td><math>Q_{allow} = \text{SUMP}</math></td> <td><math>Q_{allow} = \text{SUMP}</math></td> <td></td> </tr> </table> | Minor Storm | Major Storm | cfs    | $Q_{allow} = \text{SUMP}$ | $Q_{allow} = \text{SUMP}$ |  |
| Minor Storm  | Major Storm  | cfs         |             |        |                           |                           |  |
| $Q_{allow} = \text{SUMP}$  | $Q_{allow} = \text{SUMP}$  |             |             |        |                           |                           |  |

Warning 02

## INLET IN A SUMP OR SAG LOCATION

Version 4.06 Released August 2018



| Design Information (Input)   | MINOR                    | MAJOR |   |
|--|--------------------------|-------|---|
| Type of Inlet  | CDOT Type R Curb Opening |       |   |
| Local Depression (additional to continuous gutter depression 'a' from above) | 5.00                     | 5.00  | inches  |
| Number of Unit Inlets (Grate or Curb Opening)                                | 1                        | 1     |   |
| Water Depth at Flowline (outside of local depression)                        | 4.6                      | 6.7   | inches  |
| <b>Grate Information</b>   | MINOR                    | MAJOR | <input checked="" type="checkbox"/> Override Depths |
| Length of a Unit Grate   | N/A                      | N/A   | feet  |
| Width of a Unit Grate  | N/A                      | N/A   | feet  |
| Area Opening Ratio for a Grate (typical values 0.15-0.90)                    | N/A                      | N/A   |   |
| Clogging Factor for a Single Grate (typical value 0.50 - 0.70)               | N/A                      | N/A   |   |
| Grate Weir Coefficient (typical value 2.15 - 3.60)                           | N/A                      | N/A   |   |
| Grate Orifice Coefficient (typical value 0.60 - 0.80)                        | N/A                      | N/A   |   |
| <b>Curb Opening Information</b>  | MINOR                    | MAJOR |   |
| Length of a Unit Curb Opening  | 15.00                    | 15.00 | feet  |
| Height of Vertical Curb Opening in Inches                                    | 6.00                     | 6.00  | inches  |
| Height of Curb Orifice Throat in Inches                                      | 6.00                     | 6.00  | inches  |
| Angle of Throat (see USDCM Figure ST-5)                                      | 63.40                    | 63.40 | degrees   |
| Side Width for Depression Pan (typically the gutter width of 2 feet)         | 1.00                     | 1.00  | feet  |
| Clogging Factor for a Single Curb Opening (typical value 0.10)               | 0.10                     | 0.10  |   |
| Curb Opening Weir Coefficient (typical value 2.3-3.7)                        | 3.60                     | 3.60  |   |
| Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)                 | 0.67                     | 0.67  |   |
| <b>Low Head Performance Reduction (Calculated)</b>                           | MINOR                    | MAJOR |   |
| Depth for Grate Midwidth   | N/A                      | N/A   | ft  |
| Depth for Curb Opening Weir Equation   | 0.30                     | 0.48  | ft  |
| Combination Inlet Performance Reduction Factor for Long Inlets               | 0.44                     | 0.64  |   |
| Curb Opening Performance Reduction Factor for Long Inlets                    | 0.69                     | 0.83  |   |
| Grated Inlet Performance Reduction Factor for Long Inlets                    | N/A                      | N/A   |   |
| <b>Total Inlet Interception Capacity (assumes clogged condition)</b>         | MINOR                    | MAJOR |   |
| <b>Q<sub>a</sub></b>   | 6.7                      | 16.0  | cfs   |
| Q <sub>PEAK REQUIRED</sub>   | 6.6                      | 16.0  | cfs   |

Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)

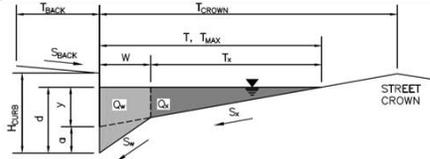
**ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)**

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project:  
Inlet ID:

Cloverleaf Subdivision

J



**Gutter Geometry (Enter data in the blue cells)**

Maximum Allowable Width for Spread Behind Curb  
 Side Slope Behind Curb (leave blank for no conveyance credit behind curb)  
 Manning's Roughness Behind Curb (typically between 0.012 and 0.020)  
 Height of Curb at Gutter Flow Line  
 Distance from Curb Face to Street Crown  
 Gutter Width  
 Street Transverse Slope  
 Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)  
 Street Longitudinal Slope - Enter 0 for sump condition  
 Manning's Roughness for Street Section (typically between 0.012 and 0.020)

$T_{BACK} = 7.5$  ft  
 $S_{BACK} = 0.020$  ft/ft  
 $n_{BACK} = 0.016$   
 $H_{CURB} = 4.00$  inches  
 $T_{CROWN} = 15.0$  ft  
 $W = 1.00$  ft  
 $S_x = 0.020$  ft/ft  
 $S_w = 0.083$  ft/ft  
 $S_o = 0.000$  ft/ft  
 $n_{STREET} = 0.016$

**Warning 02** Max. Allowable Spread for Minor & Major Storm  
 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm  
 Check boxes are not applicable in SUMP conditions

|             | Minor Storm              | Major Storm              |        |
|-------------|--------------------------|--------------------------|--------|
| $T_{MAX} =$ | 15.0                     | 15.0                     | ft     |
| $d_{MAX} =$ | 5.0                      | 12.0                     | inches |
|             | <input type="checkbox"/> | <input type="checkbox"/> |        |

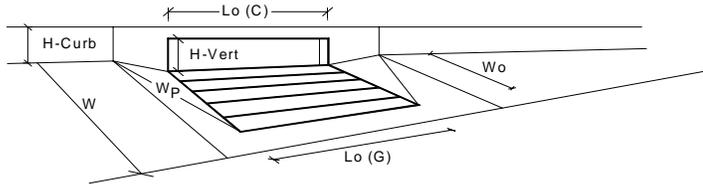
**MINOR STORM** Allowable Capacity is based on Depth Criterion  
**MAJOR STORM** Allowable Capacity is based on Depth Criterion

$Q_{allow} =$ 

| Minor Storm | Major Storm |     |
|-------------|-------------|-----|
| SUMP        | SUMP        | cfs |

## INLET IN A SUMP OR SAG LOCATION

Version 4.06 Released August 2018



| <b>Design Information (Input)</b>  | MINOR                    | MAJOR |   |
|--|--------------------------|-------|---|
| Type of Inlet  | CDOT Type R Curb Opening |       |   |
| Local Depression (additional to continuous gutter depression 'a' from above) | 5.00                     | 5.00  | inches  |
| Number of Unit Inlets (Grate or Curb Opening)                                | 1                        | 1     |   |
| Water Depth at Flowline (outside of local depression)                        | 3.9                      | 5.7   | inches  |
| <b>Grate Information</b>   | MINOR                    | MAJOR | <input checked="" type="checkbox"/> Override Depths |
| Length of a Unit Grate   | N/A                      | N/A   | feet  |
| Width of a Unit Grate  | N/A                      | N/A   | feet  |
| Area Opening Ratio for a Grate (typical values 0.15-0.90)                    | N/A                      | N/A   |   |
| Clogging Factor for a Single Grate (typical value 0.50 - 0.70)               | N/A                      | N/A   |   |
| Grate Weir Coefficient (typical value 2.15 - 3.60)                           | N/A                      | N/A   |   |
| Grate Orifice Coefficient (typical value 0.60 - 0.80)                        | N/A                      | N/A   |   |
| <b>Curb Opening Information</b>  | MINOR                    | MAJOR |   |
| Length of a Unit Curb Opening  | 10.00                    | 10.00 | feet  |
| Height of Vertical Curb Opening in Inches                                    | 6.00                     | 6.00  | inches  |
| Height of Curb Orifice Throat in Inches                                      | 6.00                     | 6.00  | inches  |
| Angle of Throat (see USDCM Figure ST-5)                                      | 63.40                    | 63.40 | degrees   |
| Side Width for Depression Pan (typically the gutter width of 2 feet)         | 1.00                     | 1.00  | feet  |
| Clogging Factor for a Single Curb Opening (typical value 0.10)               | 0.10                     | 0.10  |   |
| Curb Opening Weir Coefficient (typical value 2.3-3.7)                        | 3.60                     | 3.60  |   |
| Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)                 | 0.67                     | 0.67  |   |
| <b>Low Head Performance Reduction (Calculated)</b>                           | MINOR                    | MAJOR |   |
| Depth for Grate Midwidth   | N/A                      | N/A   | ft  |
| Depth for Curb Opening Weir Equation   | 0.25                     | 0.40  | ft  |
| Combination Inlet Performance Reduction Factor for Long Inlets               | 0.37                     | 0.54  |   |
| Curb Opening Performance Reduction Factor for Long Inlets                    | 0.78                     | 0.92  |   |
| Grated Inlet Performance Reduction Factor for Long Inlets                    | N/A                      | N/A   |   |
| <b>Total Inlet Interception Capacity (assumes clogged condition)</b>         | MINOR                    | MAJOR |   |
| <b>Q<sub>a</sub></b>   | 3.8                      | 9.1   | cfs   |
| Q <sub>PEAK REQUIRED</sub>   | 3.6                      | 8.9   | cfs   |

Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)

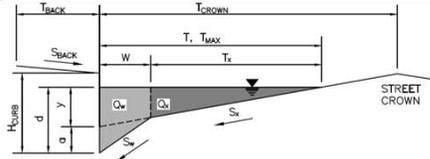
**ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)**

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project:  
Inlet ID:

Cloverleaf Subdivision

M



**Gutter Geometry (Enter data in the blue cells)**

Maximum Allowable Width for Spread Behind Curb  
 Side Slope Behind Curb (leave blank for no conveyance credit behind curb)  
 Manning's Roughness Behind Curb (typically between 0.012 and 0.020)  
 Height of Curb at Gutter Flow Line  
 Distance from Curb Face to Street Crown  
 Gutter Width  
 Street Transverse Slope  
 Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)  
 Street Longitudinal Slope - Enter 0 for sump condition  
 Manning's Roughness for Street Section (typically between 0.012 and 0.020)

$T_{BACK} = 7.5$  ft  
 $S_{BACK} = 0.020$  ft/ft  
 $n_{BACK} = 0.016$   
 $H_{CURB} = 4.00$  inches  
 $T_{CROWN} = 15.0$  ft  
 $W = 1.00$  ft  
 $S_x = 0.020$  ft/ft  
 $S_w = 0.083$  ft/ft  
 $S_o = 0.055$  ft/ft  
 $n_{STREET} = 0.016$

Max. Allowable Spread for Minor & Major Storm  
 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm  
 Allow Flow Depth at Street Crown (leave blank for no)

|           | Minor Storm              | Major Storm              |             |
|-----------|--------------------------|--------------------------|-------------|
| $T_{MAX}$ | 15.0                     | 15.0                     | ft          |
| $d_{MAX}$ | 4.0                      | 12.0                     | inches      |
|           | <input type="checkbox"/> | <input type="checkbox"/> | check = yes |

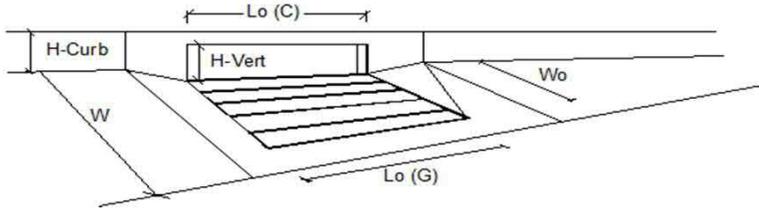
**MINOR STORM Allowable Capacity is based on Depth Criterion**  
**MAJOR STORM Allowable Capacity is based on Spread Criterion**

|             | Minor Storm | Major Storm |     |
|-------------|-------------|-------------|-----|
| $Q_{allow}$ | 13.0        | 17.1        | cfs |

**Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'**  
**Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'**

## INLET ON A CONTINUOUS GRADE

Version 4.06 Released August 2018



| Design Information (Input)  | MINOR                    | MAJOR |        |
|---|--------------------------|-------|--------|
| Type of Inlet   | CDOT Type R Curb Opening |       |        |
| Local Depression (additional to continuous gutter depression 'a')         | 5.0                      | 5.0   | inches |
| Total Number of Units in the Inlet (Grate or Curb Opening)                | 1                        | 1     |        |
| Length of a Single Unit Inlet (Grate or Curb Opening)                     | 10.00                    | 10.00 | ft     |
| Width of a Unit Grate (cannot be greater than W, Gutter Width)            | N/A                      | N/A   | ft     |
| Clogging Factor for a Single Unit Grate (typical min. value = 0.5)        | N/A                      | N/A   |        |
| Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1) | 0.10                     | 0.10  |        |
| <b>Street Hydraulics: OK - Q &lt; Allowable Street Capacity</b>           |                          |       |        |
| Total Inlet Interception Capacity   | 1.4                      | 3.0   | cfs    |
| Total Inlet Carry-Over Flow (flow bypassing inlet)                        | 0.0                      | 0.0   | cfs    |
| Capture Percentage = $Q_i/Q_o$ =  | 100                      | 100   | %      |

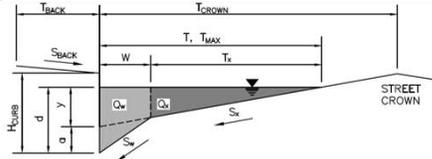
**ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)**

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project:  
Inlet ID:

Cloverleaf Subdivision

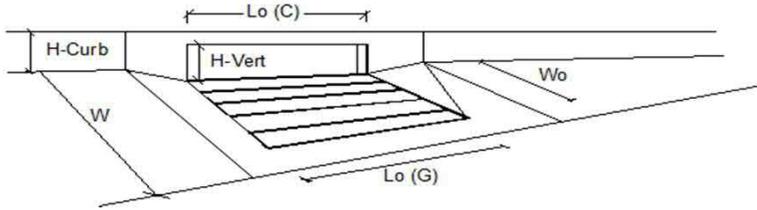
N



| Gutter Geometry (Enter data in the blue cells)   |  |             |             |        |                  |                  |  |
|--|--|-------------|-------------|--------|------------------|------------------|--|
| Maximum Allowable Width for Spread Behind Curb   | $T_{BACK} = 7.5$ ft  |             |             |        |                  |                  |  |
| Side Slope Behind Curb (leave blank for no conveyance credit behind curb)  | $S_{BACK} = 0.020$ ft/ft   |             |             |        |                  |                  |  |
| Manning's Roughness Behind Curb (typically between 0.012 and 0.020)  | $n_{BACK} = 0.016$   |             |             |        |                  |                  |  |
| Height of Curb at Gutter Flow Line   | $H_{CURB} = 4.00$ inches   |             |             |        |                  |                  |  |
| Distance from Curb Face to Street Crown  | $T_{CROWN} = 15.0$ ft  |             |             |        |                  |                  |  |
| Gutter Width   | $W = 1.00$ ft  |             |             |        |                  |                  |  |
| Street Transverse Slope  | $S_X = 0.020$ ft/ft  |             |             |        |                  |                  |  |
| Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)  | $S_W = 0.083$ ft/ft  |             |             |        |                  |                  |  |
| Street Longitudinal Slope - Enter 0 for sump condition   | $S_O = 0.055$ ft/ft  |             |             |        |                  |                  |  |
| Manning's Roughness for Street Section (typically between 0.012 and 0.020)                                       | $n_{STREET} = 0.016$   |             |             |        |                  |                  |  |
| Max. Allowable Spread for Minor & Major Storm  | <table border="1"> <tr> <th>Minor Storm</th> <th>Major Storm</th> <th>ft</th> </tr> <tr> <td><math>T_{MAX} = 15.0</math></td> <td><math>T_{MAX} = 15.0</math></td> <td></td> </tr> </table>    | Minor Storm | Major Storm | ft     | $T_{MAX} = 15.0$ | $T_{MAX} = 15.0$ |  |
| Minor Storm  | Major Storm  | ft          |             |        |                  |                  |  |
| $T_{MAX} = 15.0$   | $T_{MAX} = 15.0$   |             |             |        |                  |                  |  |
| Max. Allowable Depth at Gutter Flowline for Minor & Major Storm  | <table border="1"> <tr> <th>Minor Storm</th> <th>Major Storm</th> <th>inches</th> </tr> <tr> <td><math>d_{MAX} = 4.0</math></td> <td><math>d_{MAX} = 12.0</math></td> <td></td> </tr> </table> | Minor Storm | Major Storm | inches | $d_{MAX} = 4.0$  | $d_{MAX} = 12.0$ |  |
| Minor Storm  | Major Storm  | inches      |             |        |                  |                  |  |
| $d_{MAX} = 4.0$  | $d_{MAX} = 12.0$   |             |             |        |                  |                  |  |
| Allow Flow Depth at Street Crown (leave blank for no)  | <input type="checkbox"/> <input type="checkbox"/> check = yes  |             |             |        |                  |                  |  |
| <b>MINOR STORM Allowable Capacity is based on Depth Criterion</b>  |  |             |             |        |                  |                  |  |
| <b>MAJOR STORM Allowable Capacity is based on Spread Criterion</b>   |  |             |             |        |                  |                  |  |
| <b>Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'</b> |  |             |             |        |                  |                  |  |
| <b>Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'</b> |  |             |             |        |                  |                  |  |
| $Q_{allow} =$  | <table border="1"> <tr> <th>Minor Storm</th> <th>Major Storm</th> <th>cfs</th> </tr> <tr> <td><math>13.0</math></td> <td><math>17.1</math></td> <td></td> </tr> </table>                       | Minor Storm | Major Storm | cfs    | $13.0$           | $17.1$           |  |
| Minor Storm  | Major Storm  | cfs         |             |        |                  |                  |  |
| $13.0$   | $17.1$   |             |             |        |                  |                  |  |

## INLET ON A CONTINUOUS GRADE

Version 4.06 Released August 2018



| Design Information (Input)  | MINOR                    | MAJOR |        |
|---|--------------------------|-------|--------|
| Type of Inlet   | CDOT Type R Curb Opening |       |        |
| Local Depression (additional to continuous gutter depression 'a')         | 5.0                      | 5.0   | inches |
| Total Number of Units in the Inlet (Grate or Curb Opening)                | 1                        | 1     |        |
| Length of a Single Unit Inlet (Grate or Curb Opening)                     | 10.00                    | 10.00 | ft     |
| Width of a Unit Grate (cannot be greater than W, Gutter Width)            | N/A                      | N/A   | ft     |
| Clogging Factor for a Single Unit Grate (typical min. value = 0.5)        | N/A                      | N/A   |        |
| Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1) | 0.10                     | 0.10  |        |
| <b>Street Hydraulics: OK - Q &lt; Allowable Street Capacity</b>           |                          |       |        |
| Total Inlet Interception Capacity   | 1.4                      | 3.9   | cfs    |
| Total Inlet Carry-Over Flow (flow bypassing inlet)                        | 0.0                      | 0.0   | cfs    |
| Capture Percentage = $Q_i/Q_o$ =  | 100                      | 100   | %      |

### HY-8 Analysis Results - Bowstring & Leggins

| Condition       | Headwater Elevation (ft) | Total Discharge (cfs) | Ex 28"x42" CMP Discharge (cfs) | Roadway Discharge (cfs) | Iterations |
|-----------------|--------------------------|-----------------------|--------------------------------|-------------------------|------------|
| 5-yr Proposed   | 6993.42                  | 92                    | 53.67                          | 38.08                   | 8          |
| 5-yr Existing   | 6993.47                  | 102                   | 54.27                          | 47.49                   | 8          |
| 100-yr Proposed | 6993.8                   | 199                   | 57.97                          | 140.62                  | 4          |
| 100-yr Existing | 6993.97                  | 282                   | 59.81                          | 222.07                  | 3          |

Proposed 100-year results shown below:

Crossing Data - Bowstring & Leggins
— □ ×

**Crossing Properties**

Name:

| Parameter                | Value                        | Units |
|--------------------------|------------------------------|-------|
| <b>DISCHARGE DATA</b>    |                              |       |
| Discharge Method         | Minimum, Design, and Maximum |       |
| Minimum Flow             | 50.000                       | cfs   |
| Design Flow              | 165.000                      | cfs   |
| Maximum Flow             | 300.000                      | cfs   |
| <b>TAILWATER DATA</b>    |                              |       |
| Channel Type             | Trapezoidal Channel          |       |
| Bottom Width             | 12.000                       | ft    |
| Side Slope (H:V)         | 4.000                        | _: 1  |
| Channel Slope            | 0.0370                       | ft/ft |
| Manning's n (channel)    | 0.040                        |       |
| Channel Invert Elevation | 6987.800                     | ft    |
| Rating Curve             | <a href="#">View...</a>      |       |
| <b>ROADWAY DATA</b>      |                              |       |
| Roadway Profile Shape    | Irregular                    |       |
| Irregular Shape          | <a href="#">Define...</a>    |       |
| Roadway Surface          | Paved                        |       |
| Top Width                | 24.000                       | ft    |

**Culvert Properties**

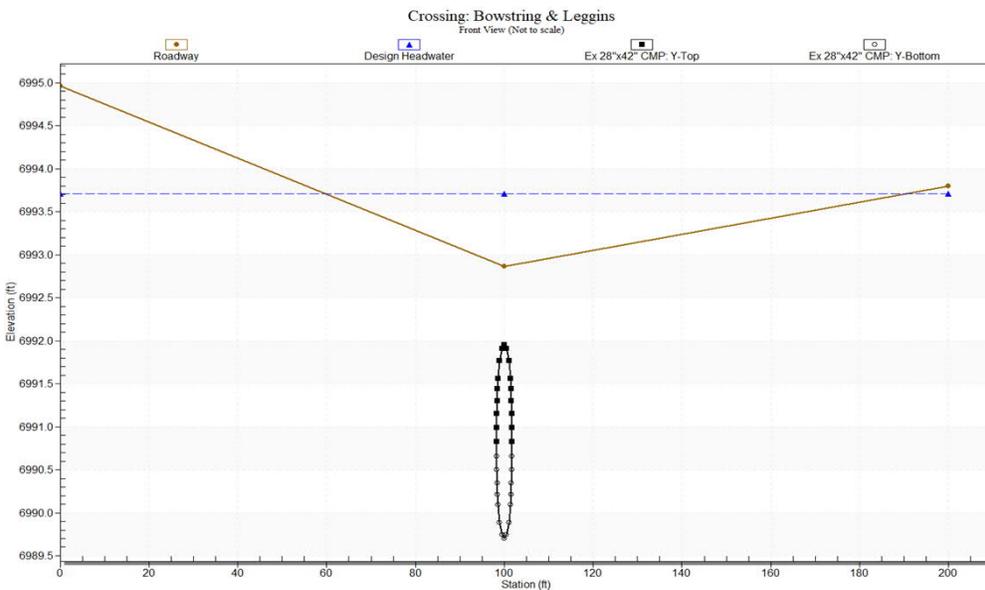
[Add Culvert](#)

[Duplicate Culvert](#)

[Delete Culvert](#)

| Parameter              | Value                     | Units |
|------------------------|---------------------------|-------|
| <b>CULVERT DATA</b>    |                           |       |
| Name                   | Ex 28"x42" CMP            |       |
| Shape                  | Elliptical                |       |
| Material               | Concrete                  |       |
| Size                   | <a href="#">Define...</a> |       |
| Span                   | 42.000                    | in    |
| Rise                   | 27.000                    | in    |
| Embedment Depth        | 0.000                     | in    |
| Manning's n            | 0.024                     |       |
| Culvert Type           | Straight                  |       |
| Inlet Configuration    | Grooved Edge Projecting   |       |
| Inlet Depression?      | No                        |       |
| <b>SITE DATA</b>       |                           |       |
| Site Data Input Option | Culvert Invert Data       |       |
| Inlet Station          | 0.000                     | ft    |
| Inlet Elevation        | 6989.700                  | ft    |
| Outlet Station         | 44.000                    | ft    |
| Outlet Elevation       | 6988.000                  | ft    |
| Number of Barrels      | 1                         |       |

Help
Click on any icon for help on a specific topic
Low Flow
AOP
Energy Dissipation
Analyze Crossing
OK
Cancel



# Channel Report

## Swale B (5-Year)

### Triangular

Side Slopes (z:1) = 4.00, 4.00

Total Depth (ft) = 1.00

Invert Elev (ft) = 10.00

Slope (%) = 2.00

N-Value = 0.030

### Calculations

Compute by: Known Q

Known Q (cfs) = 4.20

### Highlighted

Depth (ft) = 0.59

Q (cfs) = 4.200

Area (sqft) = 1.39

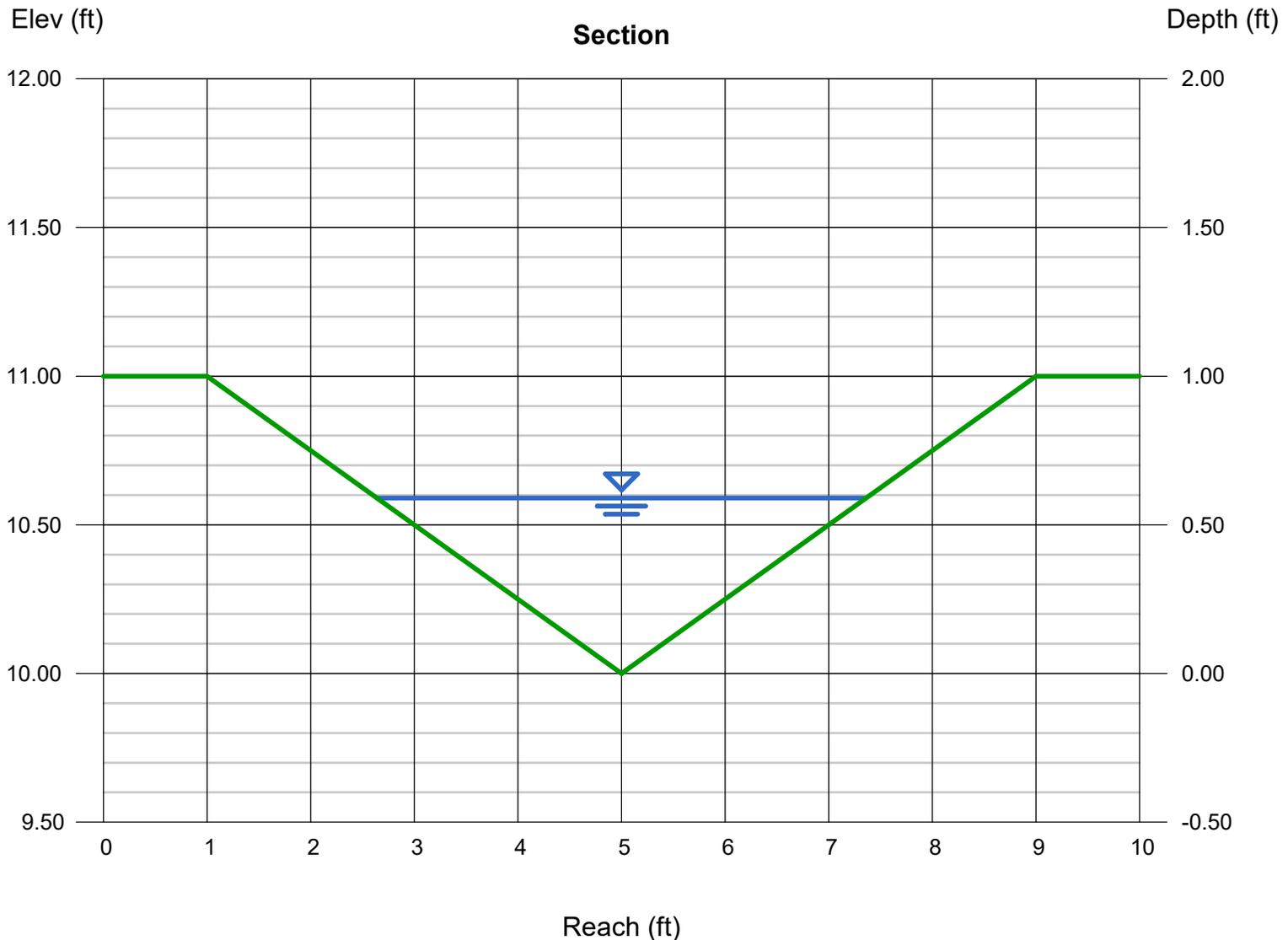
Velocity (ft/s) = 3.02

Wetted Perim (ft) = 4.87

Crit Depth, Yc (ft) = 0.59

Top Width (ft) = 4.72

EGL (ft) = 0.73



# Channel Report

## Swale B (100-Year)

### Triangular

Side Slopes (z:1) = 4.00, 4.00

Total Depth (ft) = 1.00

Invert Elev (ft) = 10.00

Slope (%) = 2.00

N-Value = 0.030

### Calculations

Compute by: Known Q

Known Q (cfs) = 10.10

### Highlighted

Depth (ft) = 0.82

Q (cfs) = 10.10

Area (sqft) = 2.69

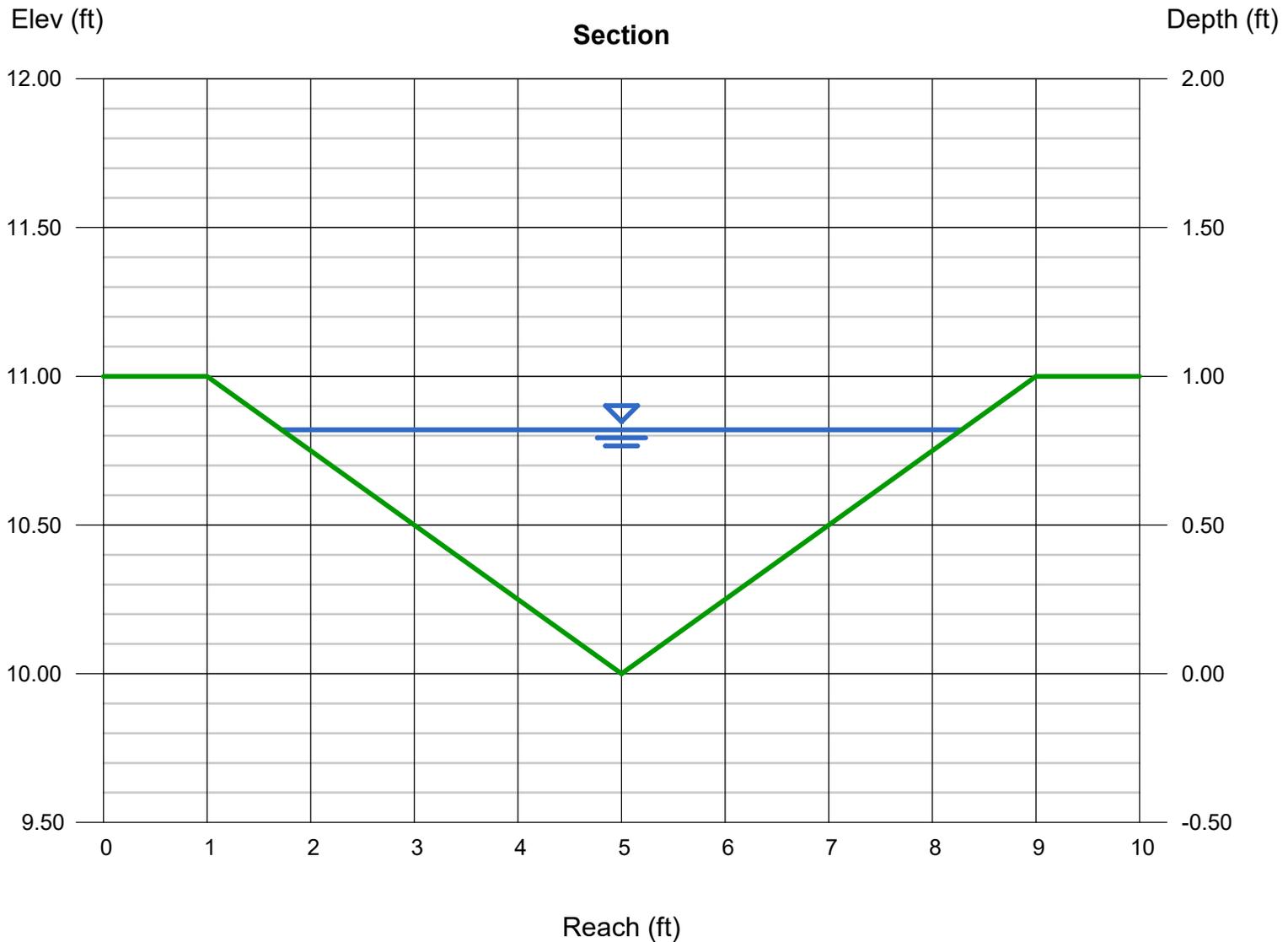
Velocity (ft/s) = 3.76

Wetted Perim (ft) = 6.76

Crit Depth, Yc (ft) = 0.84

Top Width (ft) = 6.56

EGL (ft) = 1.04



# Channel Report

## Swale K (5-Year)

### Triangular

Side Slopes (z:1) = 4.00, 4.00  
Total Depth (ft) = 1.50

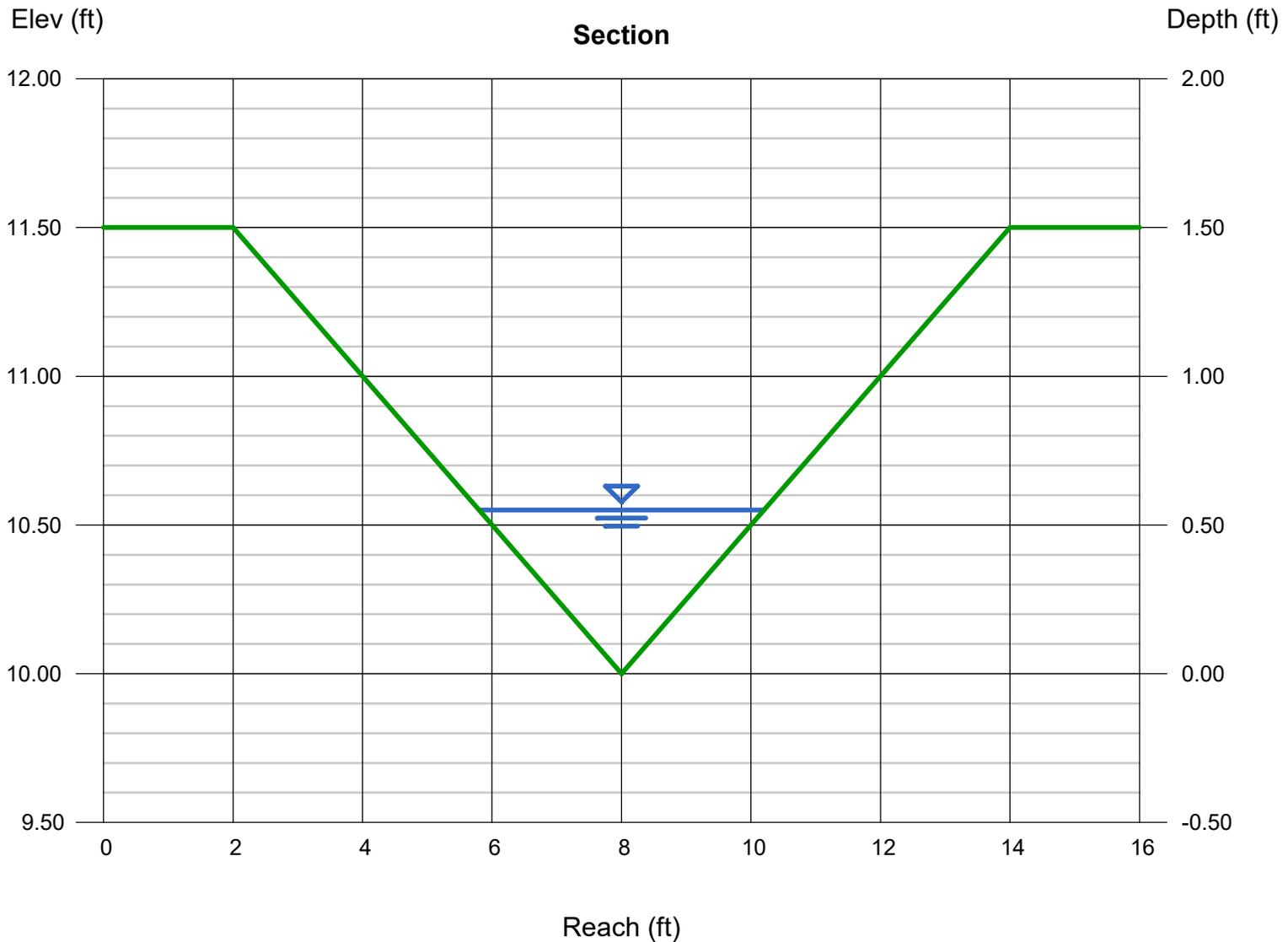
Invert Elev (ft) = 10.00  
Slope (%) = 5.00  
N-Value = 0.030

### Calculations

Compute by: Known Q  
Known Q (cfs) = 5.30

### Highlighted

Depth (ft) = 0.55  
Q (cfs) = 5.300  
Area (sqft) = 1.21  
Velocity (ft/s) = 4.38  
Wetted Perim (ft) = 4.54  
Crit Depth, Yc (ft) = 0.65  
Top Width (ft) = 4.40  
EGL (ft) = 0.85



# Channel Report

## Swale K (100-Year)

### Triangular

Side Slopes (z:1) = 4.00, 4.00  
Total Depth (ft) = 1.50

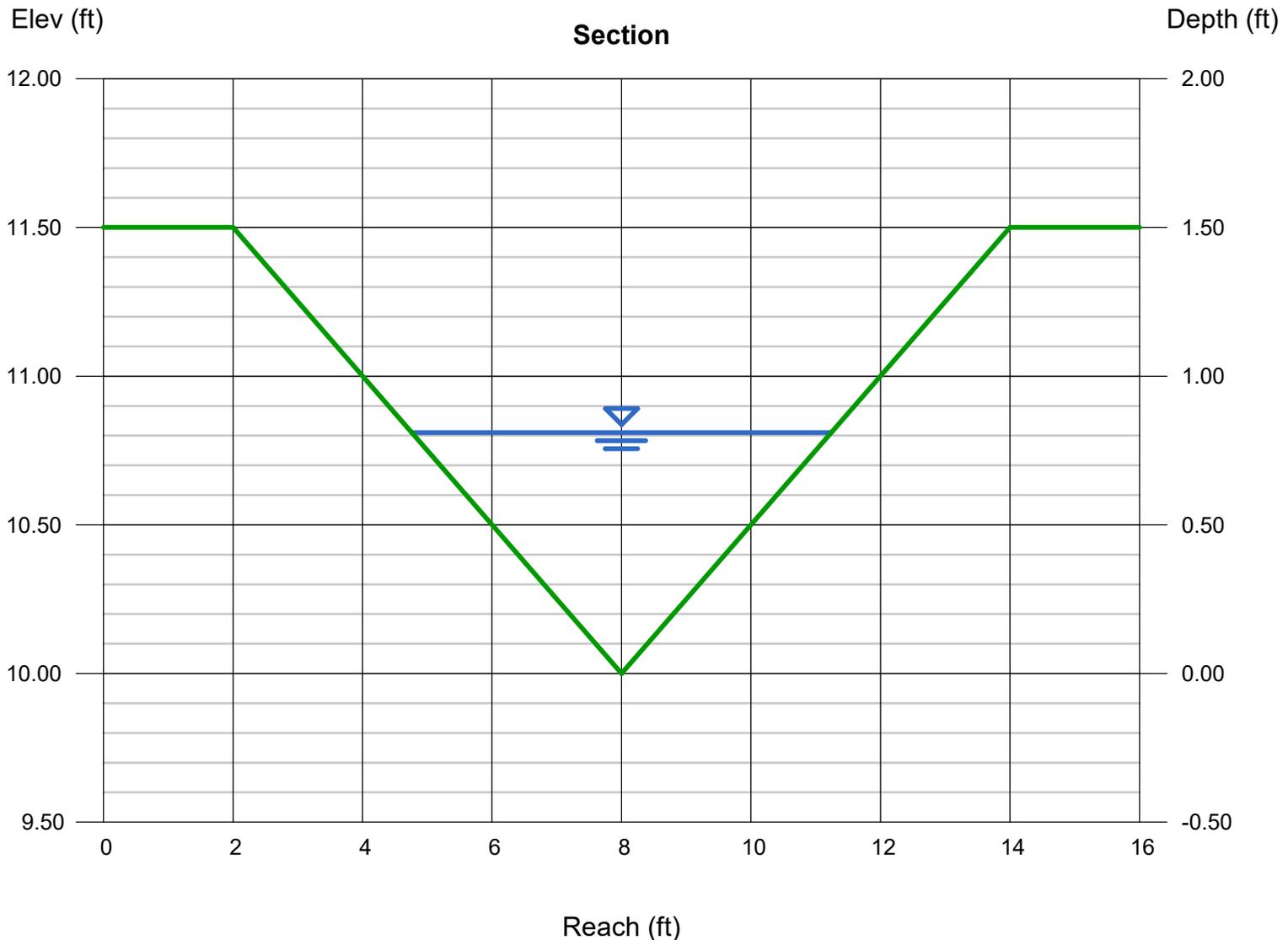
Invert Elev (ft) = 10.00  
Slope (%) = 5.00  
N-Value = 0.030

### Calculations

Compute by: Known Q  
Known Q (cfs) = 15.50

### Highlighted

Depth (ft) = 0.81  
Q (cfs) = 15.50  
Area (sqft) = 2.62  
Velocity (ft/s) = 5.91  
Wetted Perim (ft) = 6.68  
Crit Depth, Yc (ft) = 0.99  
Top Width (ft) = 6.48  
EGL (ft) = 1.35



# Channel Report

## Swale L1 (5-Year)

### Triangular

Side Slopes (z:1) = 4.00, 4.00  
Total Depth (ft) = 1.00

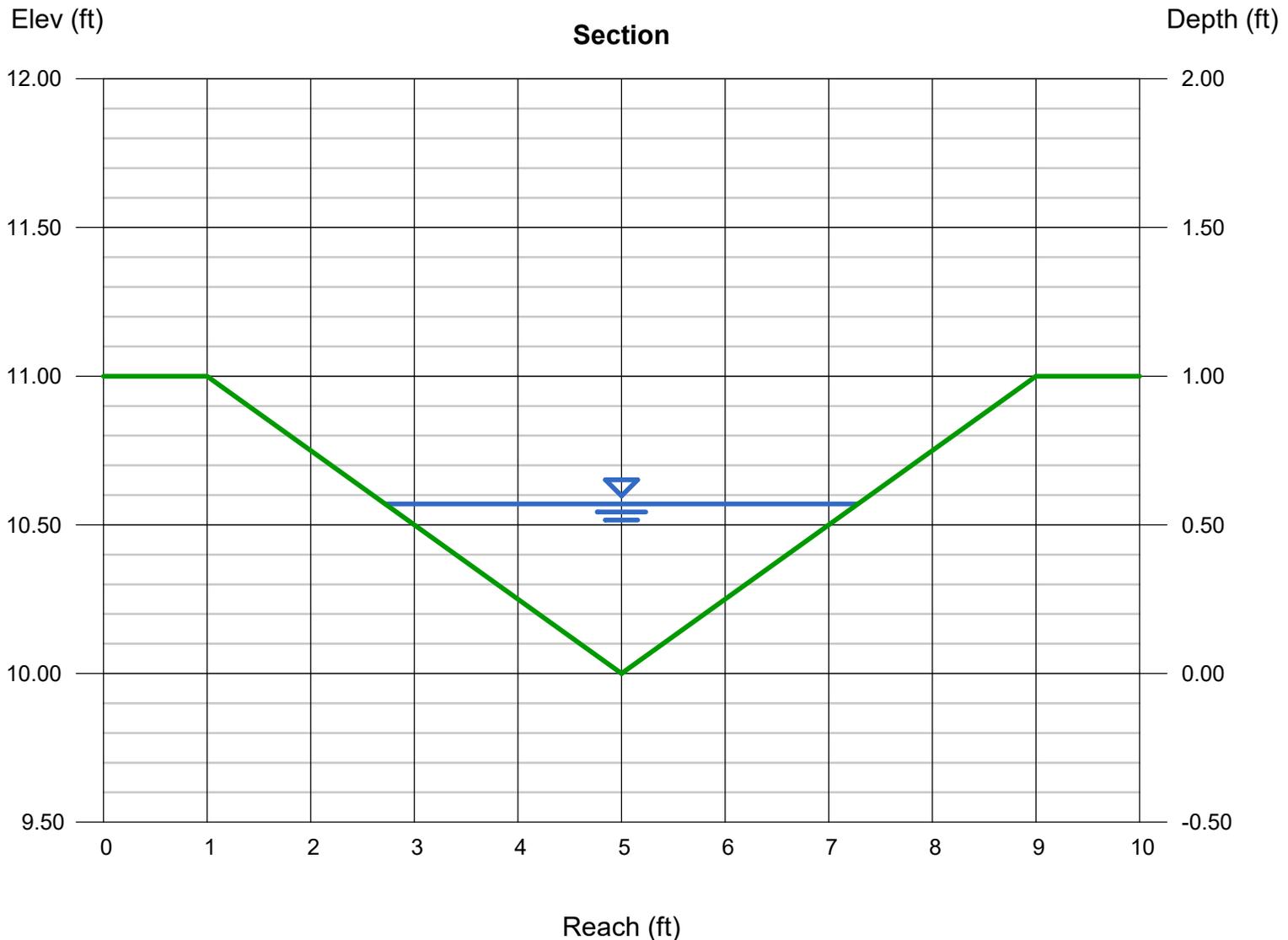
Invert Elev (ft) = 10.00  
Slope (%) = 1.00  
N-Value = 0.030

### Calculations

Compute by: Known Q  
Known Q (cfs) = 2.70

### Highlighted

Depth (ft) = 0.57  
Q (cfs) = 2.700  
Area (sqft) = 1.30  
Velocity (ft/s) = 2.08  
Wetted Perim (ft) = 4.70  
Crit Depth, Yc (ft) = 0.50  
Top Width (ft) = 4.56  
EGL (ft) = 0.64



# Channel Report

## Swale L1 (100-Year)

### Triangular

Side Slopes (z:1) = 4.00, 4.00

Total Depth (ft) = 1.00

Invert Elev (ft) = 10.00

Slope (%) = 1.00

N-Value = 0.030

### Calculations

Compute by: Known Q

Known Q (cfs) = 6.90

### Highlighted

Depth (ft) = 0.81

Q (cfs) = 6.900

Area (sqft) = 2.62

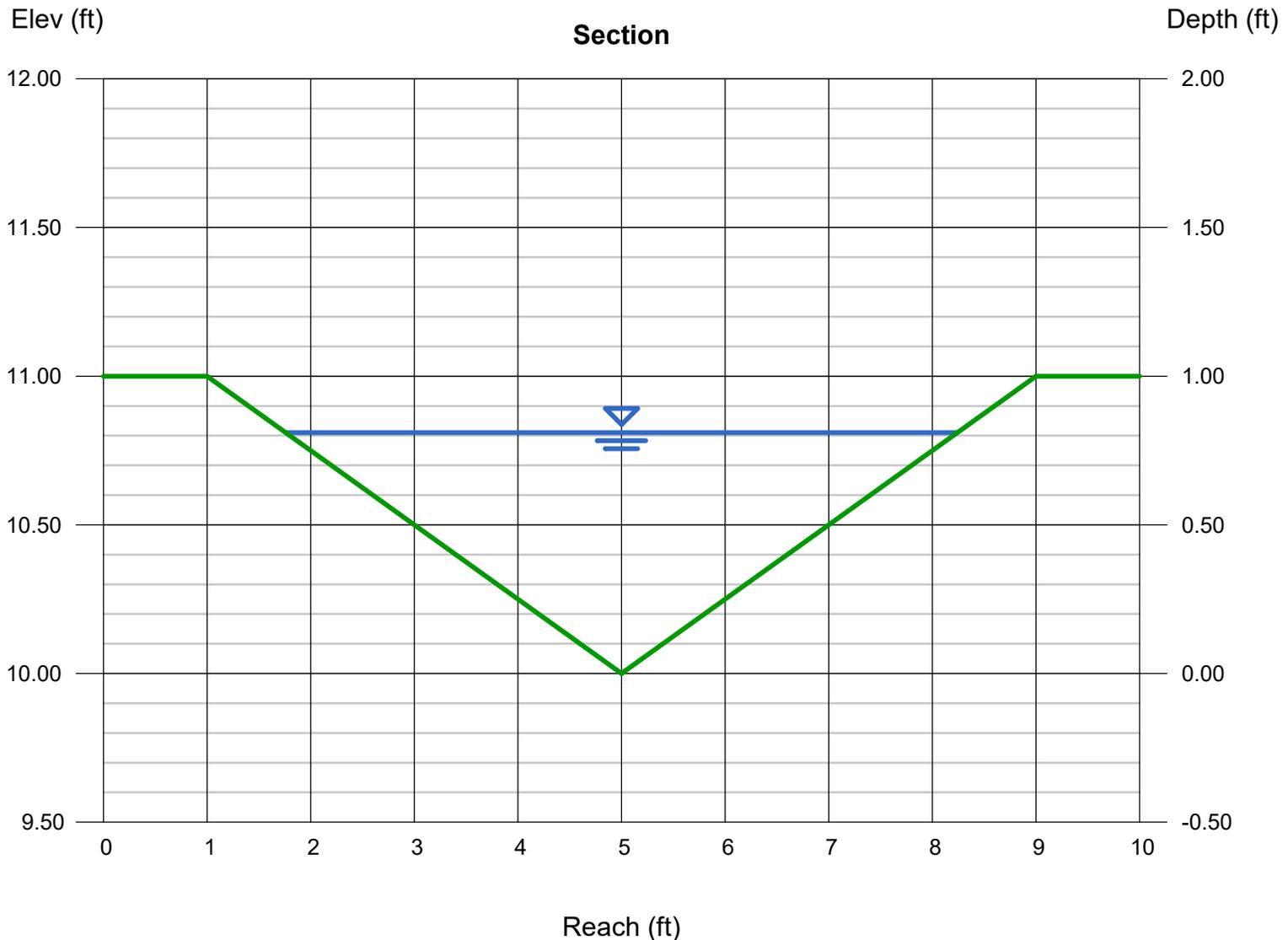
Velocity (ft/s) = 2.63

Wetted Perim (ft) = 6.68

Crit Depth, Yc (ft) = 0.72

Top Width (ft) = 6.48

EGL (ft) = 0.92



# Channel Report

## Swale L2 (5-Year)

### Triangular

Side Slopes (z:1) = 4.00, 4.00

Total Depth (ft) = 1.00

Invert Elev (ft) = 10.00

Slope (%) = 7.31

N-Value = 0.030

### Calculations

Compute by: Known Q

Known Q (cfs) = 2.70

### Highlighted

Depth (ft) = 0.40

Q (cfs) = 2.700

Area (sqft) = 0.64

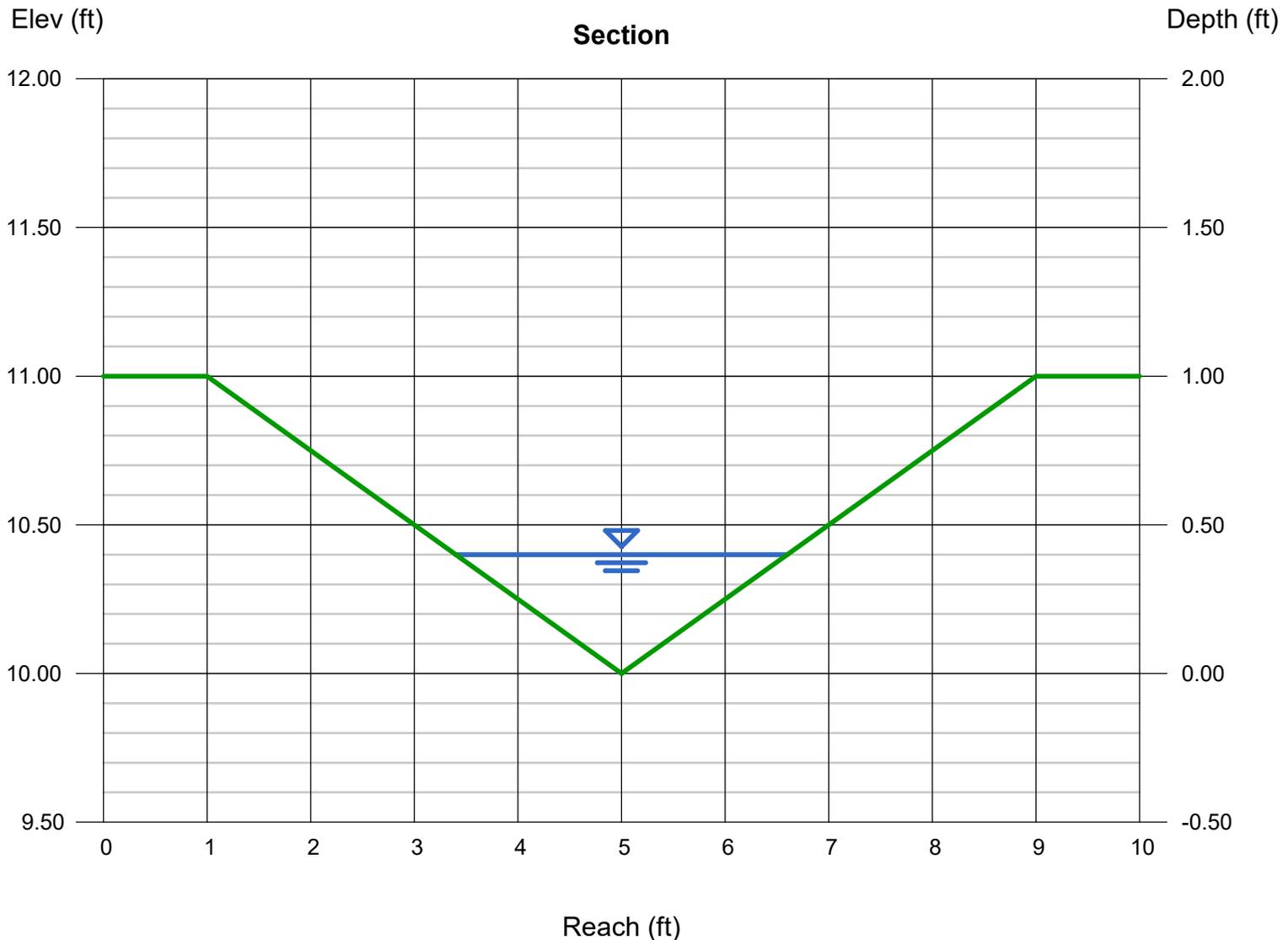
Velocity (ft/s) = 4.22

Wetted Perim (ft) = 3.30

Crit Depth, Yc (ft) = 0.50

Top Width (ft) = 3.20

EGL (ft) = 0.68



# Channel Report

## Swale L2 (100-Year)

### Triangular

Side Slopes (z:1) = 4.00, 4.00

Total Depth (ft) = 1.00

Invert Elev (ft) = 10.00

Slope (%) = 7.31

N-Value = 0.030

### Calculations

Compute by: Known Q

Known Q (cfs) = 6.90

### Highlighted

Depth (ft) = 0.56

Q (cfs) = 6.900

Area (sqft) = 1.25

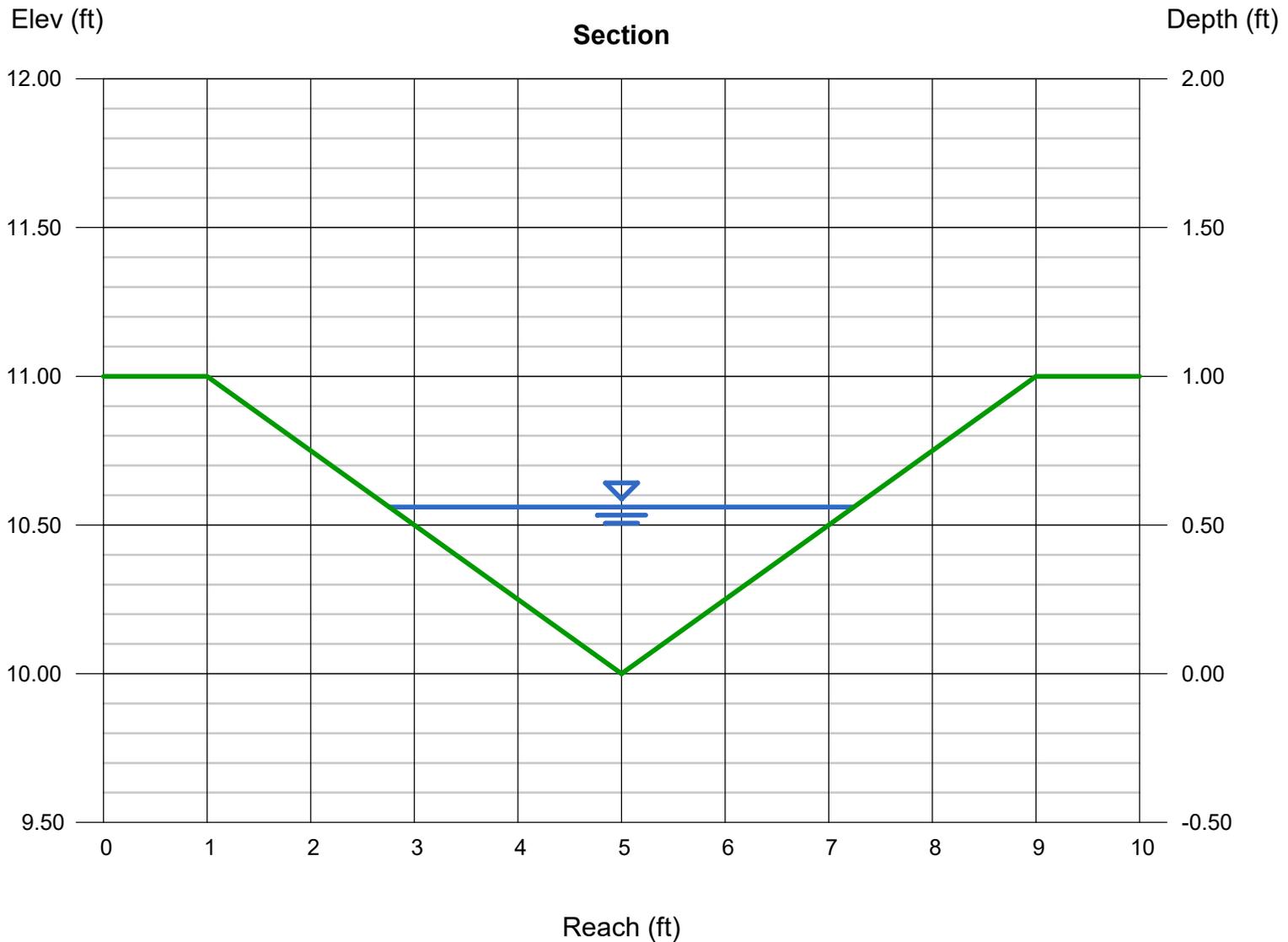
Velocity (ft/s) = 5.50

Wetted Perim (ft) = 4.62

Crit Depth, Yc (ft) = 0.72

Top Width (ft) = 4.48

EGL (ft) = 1.03



# Channel Report

## Swale OS-4 (5-Year)

### Triangular

Side Slopes (z:1) = 4.00, 13.00

Total Depth (ft) = 1.00

Invert Elev (ft) = 10.00

Slope (%) = 5.00

N-Value = 0.030

### Calculations

Compute by: Known Q

Known Q (cfs) = 1.80

### Highlighted

Depth (ft) = 0.28

Q (cfs) = 1.800

Area (sqft) = 0.67

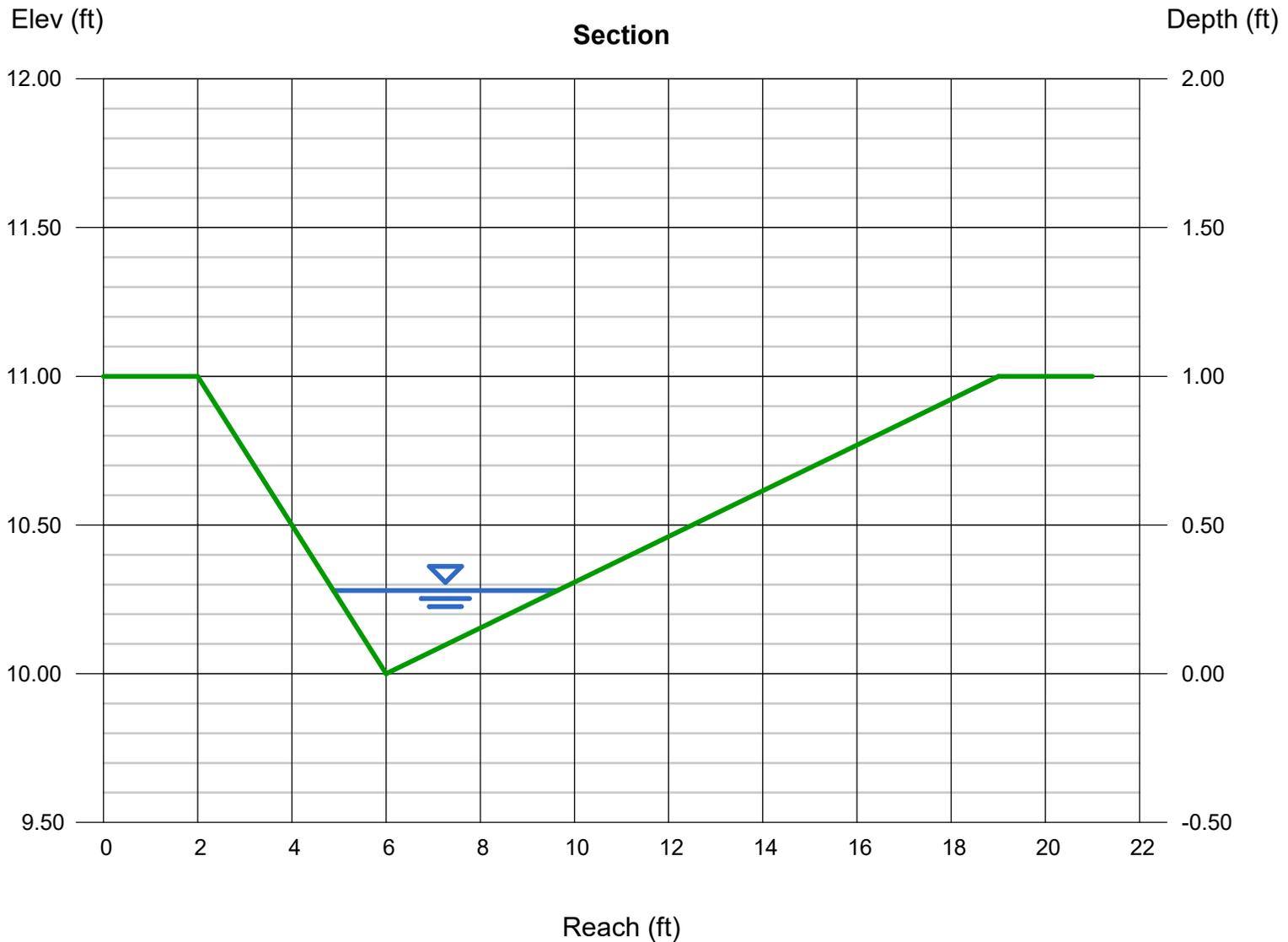
Velocity (ft/s) = 2.70

Wetted Perim (ft) = 4.81

Crit Depth, Yc (ft) = 0.31

Top Width (ft) = 4.76

EGL (ft) = 0.39



# Channel Report

## Swale OS-4 (100-Year)

### Triangular

Side Slopes (z:1) = 4.00, 13.00  
Total Depth (ft) = 1.00

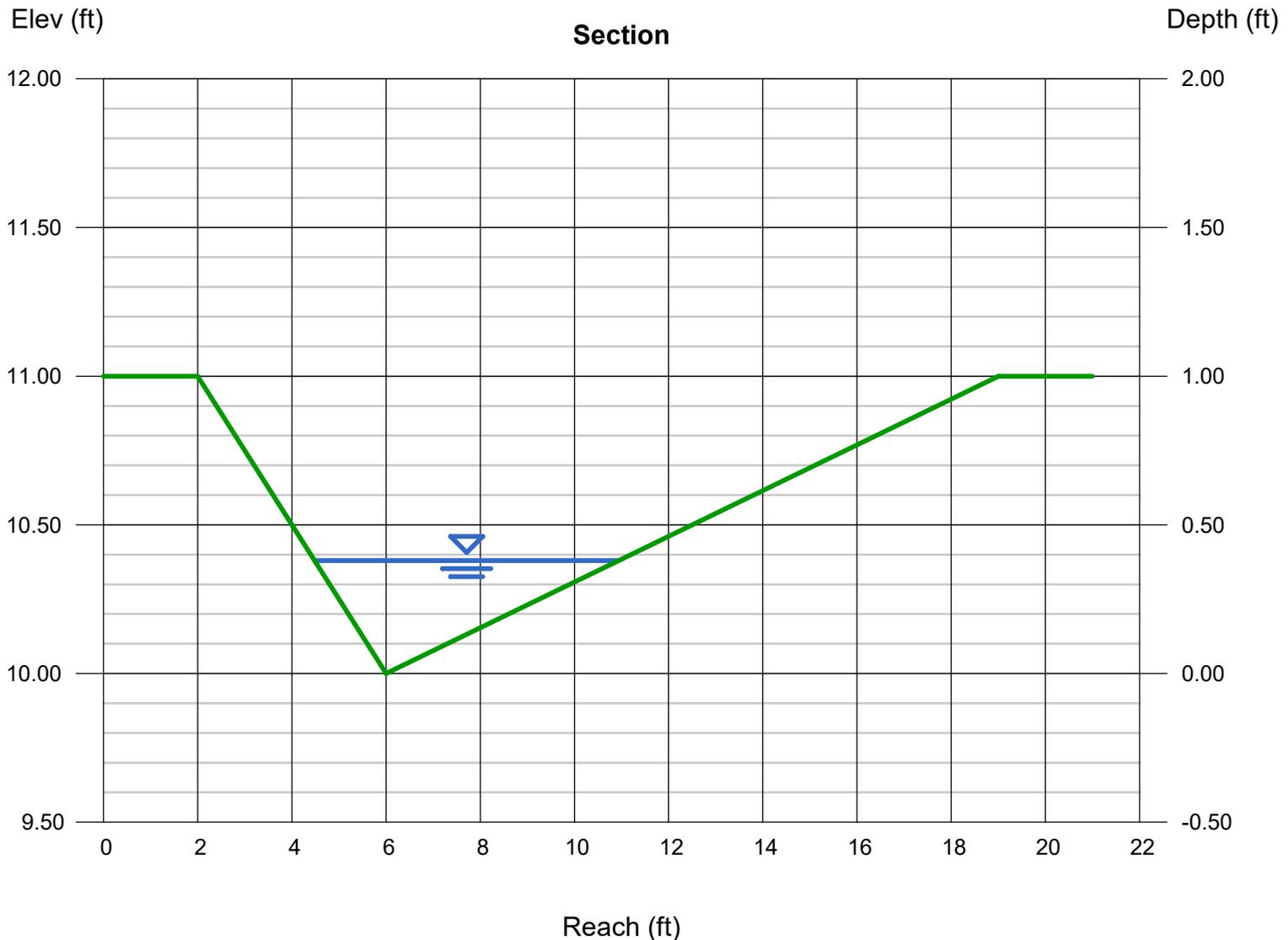
Invert Elev (ft) = 10.00  
Slope (%) = 5.00  
N-Value = 0.030

### Calculations

Compute by: Known Q  
Known Q (cfs) = 4.30

### Highlighted

Depth (ft) = 0.38  
Q (cfs) = 4.300  
Area (sqft) = 1.23  
Velocity (ft/s) = 3.50  
Wetted Perim (ft) = 6.52  
Crit Depth, Yc (ft) = 0.44  
Top Width (ft) = 6.46  
EGL (ft) = 0.57



# Rock Chute Design Data

(Version 4.01 - 04/23/03, Based on Design of Rock Chutes by Robinson, Rice, Kadavy, ASAE, 1998)

**Project:** Cloverleaf-Pond 1 Rundown  
**Designer:** GAG  
**Date:** 8/18/2021

**County:** El Paso  
**Checked by:** \_\_\_\_\_  
**Date:** \_\_\_\_\_

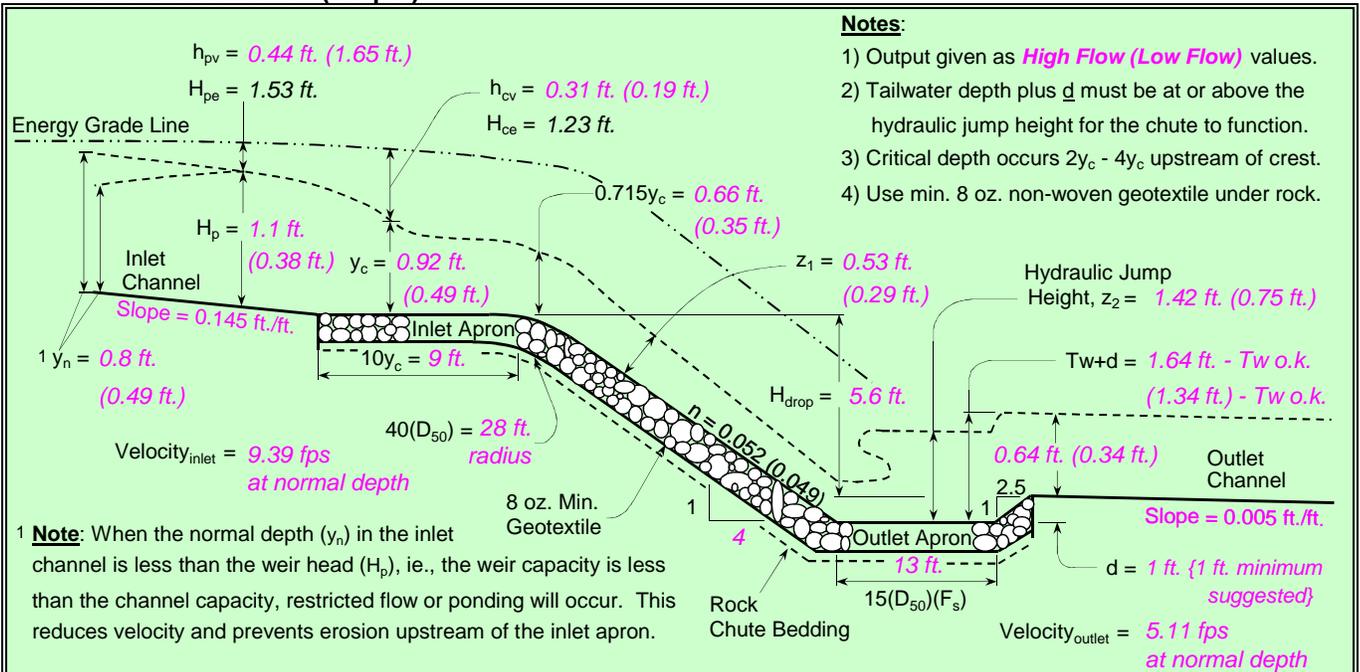
### Input Channel Geometry

| Inlet Channel              | Chute   | Outlet Channel             |
|----------------------------|---|----------------------------|
| Bw = 1.0 ft.               | Bw = 4.0 ft.  | Bw = 7.0 ft.               |
| Side slopes = 4.0 (m:1)    | Factor of safety = 1.20 (F <sub>s</sub> )           | Side slopes = 4.0 (m:1)    |
| n-value = 0.035            | Side slopes = 4.0 (m:1) → <b>2.0:1 max.</b>         | n-value = 0.013            |
| Bed slope = 0.1450 ft./ft. | Bed slope (4:1) = 0.250 ft./ft. → <b>2.5:1 max.</b> | Bed slope = 0.0050 ft./ft. |
| Freeboard = 1.0 ft.        | Outlet apron depth, d = 1.0 ft.                     | Base flow = 0.0 cfs        |

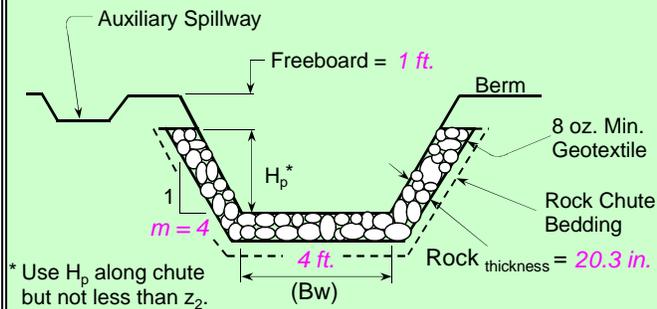
### Design Storm Data (Table 2, NHCP, NRCS Grade Stabilization Structure No. 410)

|  |  |   |
|--|--|---|
| Drainage area = 27.2 acres   | Rainfall = <input checked="" type="radio"/> 0 - 3 in. <input type="radio"/> 3 - 5 in. <input type="radio"/> 5+ in. | <b>Note:</b> The total required capacity is routed through the chute (principal spillway) or in combination with an auxiliary spillway. |
| Apron elev. --- Inlet = 7072.4 ft. --- Outlet = 7065.8 ft. --- (H <sub>drop</sub> = 5.6 ft.) |  | <b>Input tailwater (Tw):</b>  |
| Chute capacity = Q <sub>10</sub> -year   | Minimum capacity (based on a 5-year, 24-hour storm with a 0 - 3 inch rainfall)                                     |   |
| Total capacity = Q <sub>25</sub> -year   |  |   |
| Q <sub>high</sub> = 31.4 cfs   | High flow storm through chute  | Tw (ft.) = Program 0.25   |
| Q <sub>low</sub> = 10.1 cfs  | Low flow storm through chute   | Tw (ft.) = Program  |

### Profile and Cross Section (Output)



### Profile Along Centerline of Chute



|  |                                 |
|--|---------------------------------|
| $q_t = 4.98$ cfs/ft.   | Equivalent unit discharge       |
| $F_s = 1.20$   | Factor of safety (multiplier)   |
| $z_1 = 0.53$ ft.   | Normal depth in chute           |
| n-value = 0.052  | Manning's roughness coefficient |
| $D_{50}(F_s) = 10.2$ in. (77 lbs. - 50% round / 50% angular) | Rock chute thickness            |
| $2(D_{50})(F_s) = 20.3$ in.                                  | Rock chute thickness            |
| $Tw + d = 1.64$ ft.  | Tailwater above outlet apron    |
| $z_2 = 1.42$ ft.   | Hydraulic jump height           |
| <b>*** The outlet will function adequately</b>               |                                 |

**Typical Cross Section**

**High Flow Storm Information**

## **Appendix E**

### **Reference Material**

**RECEIVED**

MAY 03 2005

**EPC DEVELOPMENT SERVICES**



**J·R ENGINEERING**  
A Westrian Company

**FINAL DRAINAGE REPORT  
FOR  
WALTERS COMMONS**

APRIL 2005

Prepared For:

**PULTE HOME CORPORATION**  
1975 Research Parkway  
Colorado Springs, CO 80920  
(719) 536-4200

Prepared By:

**JR ENGINEERING**  
4310 ArrowsWest Drive  
Colorado Springs, CO 80907  
(719) 593-2593

Job No. 9170.72

FINAL DRAINAGE REPORT  
FOR  
WALTERS COMMONS

DRAINAGE REPORT STATEMENT



J-R ENGINEERING  
A Westrian Company

ENGINEER'S STATEMENT:

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the County for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors, or omissions on my part in preparing this report.



Troy D. Keen, Colorado P.E. #35996  
For and On Behalf of JR Engineering

5/2/05  
Date

DEVELOPER'S STATEMENT:

I, the developer, have read and will comply with all of the requirements specified in this drainage report and plan.

Business Name: Pulte Homes

By: [Signature]

Title: Senior Project Manager

Address: 1975 Research Parkway

Colorado Springs, CO 80920

EL PASO COUNTY ONLY:

Filed in accordance with Section 51.1 of the El Paso Land Development Code, as amended.

[Signature]  
John McCarty  
County Engineer/Director

5-4-05  
Date

Conditions:

As indicated in the Basin Summary on the previous page, the rational method yields higher runoff amounts in all cases. This is consistent with what would be expected when applying the two methodologies to the same basin.

### **PROPOSED DRAINAGE CONDITIONS**

Walters Commons is a proposed 291-unit townhome project on 32.3 acres. Filing 1 consists of 178 units on 18.7 acres. Proposed drainage patterns are as identified on the PROPOSED DRAINAGE MAP located in the Appendix. The general drainage concept is to collect developed runoff via a proposed R.C.P. storm sewer system and transport the runoff to two private on-site detention ponds located on the south and southwest sides of the proposed development.

The proposed private storm sewer and detention pond system will be designed to release storm water at historic rates into the Higby Road right-of-way and existing storm drain facilities under Higby Road. (See the EXISTING DRAINAGE MAP in the Appendix).

The proposed Walters Commons Development has been divided into 13 on-site sub-basins labeled A-M. Twelve off-site basins with the prefix "OS" have been identified to account for the remaining drainage from the existing sub-basins that flow through the site to four critical design points.

Proposed on-site Drainage Basin A ( $Q_5=1$  cfs,  $Q_{100}=3$  cfs), Basin B ( $Q_5=3$  cfs,  $Q_{100}=6$  cfs), Basin C ( $Q_5=5$  cfs,  $Q_{100}=10$  cfs) and Basin D ( $Q_5=1$  cfs,  $Q_{100}=2$  cfs) are comprised of a multi-family residential development and will drain to the northwest. Storm water from OS-3, Basins C and D flows through the north ditch of Magic Lamp Way to the east roadside ditch of Bowstring Road toward DP4. Proposed flows at DP4 combine with flows from Basin A in the ditch east of Bowstring and flow toward DP1. Existing flows from OS-4 will be intercepted on-site by an area inlet at DP3 and flow via an 24" storm pipe to DP2. The developed flows of Basin B are intercepted by a proposed private inlet at DP2, combine with pipe flows from DP3, and travel through a proposed private 24" R.C.P. storm sewer to DP1. The total developed flows from Basins A, B, C, D, OS-2, OS-3 and OS-4 at DP1 are  $Q_5=12$  cfs and  $Q_{100}=27$  cfs. The existing flow at DP1 is  $Q_5=6$  cfs,  $Q_{100}=16$  cfs. The flows from DP1 travel north along Bowstring Road to an existing 24" CMP

storm drain under Leggins Way and then through an existing 36" CMP storm drain under Bowstring Road and outlet into a 6' wide by 4' deep grass ditch on the Lewis Palmer High School property. These pipes and grass ditch have adequate capacity to carry the developed flows and will not need to be modified. (See Existing Facility Hydraulic Calculations in the Appendix). Existing Roadside ditches along Magic Lamp Way and Bowstring Road has 10 cfs capacity. The east ditch of Bowstring Road will be regarded from Magic Lamp Way to the north property line as part of the Bowstring Road paving improvements. This regarded ditch will direct flows from Magic Lamp Way, under Timber Run through the proposed 24" RCP culvert to the existing ditch north of the property line. The capacity of this ditch will be 13 cfs, developed flows in the 100-year condition through this ditch are 12 cfs.

Off-site Drainage Basin OS-5 ( $Q_5=19$  cfs,  $Q_{100}=47$  cfs) is comprised primarily of undeveloped area and a small portion of street. This off-site basin is part of EB1b. (See EXISTING DRAINAGE MAP in the Appendix). OS-5 flows travel through Country Ridge Estates and combine with OS-6 ( $Q_5=3$  cfs,  $Q_{100}=7$  cfs) and travel along the south ditch of Magic Lamp Way to the east ditch of Bowstring Road to DP7 in the southwest corner of the site (See Proposed Drainage Map in the Appendix).

Offsite flows from OS-7 ( $Q_5=4$  cfs,  $Q_{100}=10$  cfs) combine with on-site basin I ( $Q_5=0.2$  cfs,  $Q_{100}=1$  cfs), flow through the southern portion of the existing Country Ridge Estates and flow onto the proposed development at Basin G ( $Q_5=5$  cfs,  $Q_{100}=10$  cfs). A proposed private 20' At-Grade inlet at DP5 intercepts these flows. The intercepted flows will be routed through an 18" RCP storm sewer to the proposed sump inlet at DP6. (See Proposed Drainage Map.)

Bypass flow from the inlet at DP5 ( $Q_5=2$  cfs,  $Q_{100}=6$  cfs) continues into Basin F in the curb and gutter of Yellow Dogwood Heights and is intercepted at DP6 by a proposed 20' private sump inlet (See Inlet Sizing Calculations in the Appendix). The developed flows at DP6 sump inlet at ( $Q_5=15$  cfs,  $Q_{100}=30$  cfs). Combined flows from DP5 and DP6 will be routed to a proposed private detention pond through a proposed private 24" R.C.P. storm pipe. This 0.79 acre-foot detention facility will have an allowable outflow equal to or less than 78 cfs to ensure that peak drainage flows at Design Point 7 (DP7) are reduced to the historic rates of  $Q_5=33$  cfs and  $Q_{100}=78$  cfs. (See EXISTING

HYDROLOGIC CALCULATIONS in the Appendix). Developed Flows at DP7 include drainage from DP5, DP6, Basin E, Basin M, OS-6 and OS-5. The total developed flows in the proposed detention pond (DP6a) are  $Q_5 = 17$  cfs and  $Q_{100} = 36$  cfs. As mentioned above, the outfall structure will restrict 100-year flow from the proposed detention pond to ensure that DP7 flows are 78 cfs or less. Calculations for the outfall structure for this detention facility can be found in the "Storm Sewer Routing and Proposed Drainage Structures" section of this report.

Flows from Basin OS-9 ( $Q_5 = 2$  cfs,  $Q_{100} = 4$  cfs) travel on-site to Proposed Basin H ( $Q_5 = 10$  cfs,  $Q_{100} = 20$  cfs). A proposed curb opening and concrete swale at DP8 intercept flows from these basins. Flows from DP8 are routed through the swale to a 24" RCP storm sewer and outlet into the proposed 1.83 acre-ft detention pond on the south-central portion of the development. Bypass flows at DP8 ( $Q_5 = 5$  cfs,  $Q_{100} = 8$  cfs) will continue along Yellow Dogwood Heights to the sump inlet at DP6. (See Proposed Drainage Map in the Appendix.)

At Design Point 9, drainage from Basin OS-11 ( $Q_5 = 2$  cfs,  $Q_{100} = 4$  cfs) and Basin L ( $Q_5 = 1$  cfs,  $Q_{100} = 2$  cfs), Basin K ( $Q_5 = 8$  cfs,  $Q_{100} = 17$  cfs) combines for a resultant flow of  $Q_5 = 9$  cfs and  $Q_{100} = 19$  cfs. This water is intercepted by a proposed 10' private sump inlet on Burning Bush Point and routed to the proposed 1.83 acre-ft detention facility by a proposed private 24" R.C.P. storm sewer. This proposed detention facility will have an allowable outflow equal to or less than 30 cfs to ensure that peak drainage flows at DP10 are reduced to the historic rate of  $Q_{100} = 30$  cfs. The outfall structure for this detention facility is detailed in the "Storm Sewer Routing and Proposed Drainage Structures" section of this report.

A 30" proposed private RCP storm sewer will transport developed flows from future Filing 2 of the Walters Commons development to the proposed 1.83 acre-foot detention pond mentioned above. Proposed flows through this storm sewer are  $Q_{100} = 35$  cfs. The capacity of this proposed storm drain is 83 cfs. This storm drain will have a temporary plug installed in the southeast corner of Filing 1. (See Proposed Drainage Map in the Appendix.) The total developed flows to the above mentioned detention pond are  $Q_5 = 37$  cfs and  $Q_{100} = 77$  cfs. The outfall structure from this pond is designed to limit flows at DP10 to the historic rate of  $Q_{100} = 30$  cfs. Detention pond and outfall structure sizing will be discussed in a later portion of this report.

primarily undeveloped with the exception of a small portion of Cloverleaf Road on the east side of the basin. The calculations for the 5-year and 100-year storm flows for Basin EB2 can be found in the Appendix, EXISTING HYDROLOGIC CALCULATIONS. The existing flows at DP10 are 12 cfs for the 5-year storm and 30 cfs for the 100-year storm. Proposed Drainage Basins J,K OS-10, OS-11 and Future Filing 2 Developed Flows will result in  $Q_5 = 37$  cfs and  $Q_{100} = 77$  cfs at DP10 after the site is developed. The existing structure at DP10 is a 24" storm sewer that flows under Higby Road. This storm sewer has a capacity of 40 cfs at its current slope. Because development and proposed flow patterns will significantly increase flow quantities at DP10 ( $Q_{100} = 77$  cfs), a proposed 1.83 acre-ft, on-site detention pond will be designed to maintain historical flows ( $Q_{100}=30$  cfs) at DP10 through the existing 24" storm outfall facility. (See PROPOSED DRAINAGE MAP in the Appendix). The proposed outfall structure linking the detention pond to the existing 24" storm drain is a 30" private RCP storm sewer at 1% slope. This outfall structure is further detailed in the "Storm Sewer Routing and Proposed Drainage Structures" section of this report. Future storm drain improvements per the "Drainage Master Plan for Jackson Creek, Teachout Creek and No Name Creek Final Report" will include an extension of the existing 24" storm facility under Higby Road to the south. (See PROPOSED OFF-SITE DRAINAGE MAP in the Appendix). As this future storm drain facility may be several years from construction, the existing swale south of Higby Road will be adequate to handle the developed flows from Walters Commons. (See EXISTING FACILITY HYDRAULIC CALCULATIONS in the Appendix). The existing swale that flows from the highpoint in Cloverleaf Road and continues along the north side of Higby Road to DP10 has an existing capacity of 28 cfs. The proposed developed flows through this swale are 10 cfs in the 100-yr condition, therefore the existing swale has adequate capacity (See EXISITING FACILITY HYDRAULIC CALCULATIONS in the Appendix.)

### **Design Point 11**

Design Point 11 will connect to the future Walters Commons Filing 2 development and transport developed flows from a proposed Filing 2 inlet to the 1.83 acre-ft detention pond in Filing 1 via a proposed 24" and 30" private RCP storm sewer. The developed flows at DP11 from future Filing 2 are  $Q_5 = 18$  cfs and  $Q_{100} = 35$  cfs as calculated in the approved Preliminary Drainage Report for Walters Commons. The storm drain sizing calculations can be found in the Proposed Facility Hydraulic Calculations in the Appendix of this report.

### **Design Point 12**

Design Point 12 is located in the NW corner of the proposed Cloverleaf Road and Walters Point intersection. The existing flows at DP12 are  $Q_5 = 2$  cfs and  $Q_{100} = 4$  cfs. Developed flows at DP12 from Basin OS-3 and a small portion of the proposed Walters Point will be  $Q_5 = 2$  cfs and  $Q_{100} = 5$  cfs. Flows from DP12 are will move under Walters Point via a proposed private 24" culvert and travel to the south through Basin OS -11 in the roadside ditch west of Cloverleaf Road and continue along Higby Road to the proposed type C inlet at DP-10. Developed Flows at DP12 are 1 cfs higher than historic flows, therefore the existing swales will be adequate for increase developed flows (See EXISTING FACILITY HYDRAULIC CALCULATIONS in the Appendix). Calculations for the proposed culvert under Walters Point can be found in the Proposed Facility Hydraulic Calculations in the Appendix. The capacity of the existing swale from DP12 to DP7 is discussed above in "Design Point 10."

The two existing swales that receive developed flows from DP7 and DP10 mentioned above meet capacity for the 100-year storm event. Riprap dissipaters will reduce and disperse discharges to non-erosive velocities. The existing swales have established vegetation, therefore bank erosion and sedimentation down stream will not be significant as developed flows are only slightly higher than existing. Future improvements detailed in the Master Drainage Report include underground culverts connecting to the culverts under Higby Road and discharging to Teachout Creek.

## **STORM SEWER ROUTING AND PROPOSED DRAINAGE STRUCTURES**

### *Pipe Design Point 101*

The proposed storm drain facility at DP3 will collect off-site flows from basin OS-4 ( $Q_5 = 4$  cfs and  $Q_{100} = 8$  cfs) in a proposed area-inlet in the north portion of basin B. Flows will be diverted to DP1 via a proposed private 24" RCP storm drain. The total flow through pipe 101 is  $Q_5 = 4$  cfs and  $Q_{100} = 8$  cfs.

### *Pipe Design Point 102*

Flows at DP2 are collected in a proposed 5' sump inlet and travel via a proposed 24" RCP private storm drain and combine with flows from DP3 at a WYE in the northwest corner of the site. Flows

the pond to restrict the flows consists of four parts. There will be a 4' diameter manhole structure connected to the 36" culvert exiting the pond. This manhole structure will have two orifices to accept flows: a 1.2' diameter pipe with invert 6992', and a 1.4' diameter pipe with invert 6996'. The emergency overflow weir is located at 6999.5', just above the 100-year water surface elevation. Storms greater than the 100-year storm will overtop the pond and flow into the existing elliptical CMP flowing west under Bowstring Road. Both the 1.4' diameter pipe and the 1.2' diameter pipe will have a trash rack grate. Pond calculations can be found in the Proposed Detention Pond Calculations in the Appendix.

Another pond will be built at DP 10 to maintain historic rates for flows existing the site at the existing 2.3' diameter CMP flowing under Higby Road. The historic flows at this point are 12 cfs and 30 cfs for the 5 and 100-year storms respectively. Developed flows at the point are proposed to be 37 cfs and 77 cfs. To maintain historic flows, the required storage for this pond is 1.833 acre-feet.

The 5 and 100-year water surface elevations in the pond as shown on the proposed drainage map are approximately 7009.5' and 7012'.

The outlet structure that will be built in the pond to restrict the flows consists of four parts. There will be a 4' diameter manhole structure connected to the 30" culvert exiting the pond. This manhole structure will have two orifices to accept flows: a 1.1' diameter pipe with invert 7002', and a 2.0' diameter pipe with invert 7009.5'. The emergency overflow weir is located at 7012', just above the 100-year water surface elevation. Storms greater than the 100-year storm will overtop the pond and flow into the existing pipe under Higby Road. Both the 1.1' diameter pipe and the 2.0' diameter pipe will have a trash rack grate. Pond calculations can be found in the Proposed Detention Pond Calculations in the Appendix.

**PROPOSED BASIN PARAMETERS**

**WALTERS COMMONS**  
**FINAL DRAINAGE REPORT~ FILING NO. 1**  
**(Area Runoff Summary)**

| BASIN | TOTAL AREA   |              |        | IMPERVIOUS AREA |      |        | PERVIOUS AREA |      |        | WEIGHTED |        |
|-------|--------------|--------------|--------|-----------------|------|--------|---------------|------|--------|----------|--------|
|       | AREA (Acres) | AREA (Acres) | C(100) | AREA (Acres)    | C(5) | C(100) | AREA (Acres)  | C(5) | C(100) | C(5)     | C(100) |
| OS-1  | 0.5          | 0.1          | 0.90   | 0.90            | 0.90 | 0.95   | 0.4           | 0.25 | 0.35   | 0.34     | 0.43   |
| OS-2  | 0.2          | 0.2          | 0.90   | 0.90            | 0.95 | 0.95   | 0.0           | 0.25 | 0.35   | 0.90     | 0.95   |
| OS-3  | 0.4          | 0.2          | 0.90   | 0.90            | 0.95 | 0.95   | 0.2           | 0.25 | 0.35   | 0.59     | 0.67   |
| OS-4  | 5.7          | 0.0          | 0.90   | 0.90            | 0.95 | 0.95   | 5.7           | 0.25 | 0.35   | 0.25     | 0.35   |
| OS-5  | 32.1         | 0.0          | 0.35   | 0.35            | 0.45 | 0.45   | 32.1          | 0.25 | 0.35   | 0.25     | 0.35   |
| OS-6  | 1.1          | 0.6          | 0.90   | 0.90            | 0.95 | 0.95   | 0.6           | 0.25 | 0.35   | 0.57     | 0.64   |
| OS-7  | 6.8          | 0.0          | 0.90   | 0.90            | 0.95 | 0.95   | 6.8           | 0.25 | 0.35   | 0.25     | 0.35   |
| OS-8  | 0.3          | 0.0          | 0.90   | 0.90            | 0.95 | 0.95   | 0.3           | 0.25 | 0.35   | 0.25     | 0.35   |
| OS-9  | 2.3          | 0.0          | 0.90   | 0.90            | 0.95 | 0.95   | 2.3           | 0.25 | 0.35   | 0.25     | 0.35   |
| OS-10 | 3.2          | 0.0          | 0.90   | 0.90            | 0.95 | 0.95   | 3.2           | 0.25 | 0.35   | 0.25     | 0.35   |
| OS-11 | 1.7          | 0.0          | 0.90   | 0.90            | 0.95 | 0.95   | 1.7           | 0.25 | 0.35   | 0.25     | 0.35   |
| OS-12 | 1.5          | 0.8          | 0.90   | 0.90            | 0.95 | 0.95   | 0.8           | 0.25 | 0.35   | 0.58     | 0.65   |
| A     | 0.9          | 0.3          | 0.90   | 0.90            | 0.95 | 0.95   | 0.6           | 0.25 | 0.35   | 0.49     | 0.57   |
| B     | 1.8          | 0.6          | 0.90   | 0.90            | 0.95 | 0.95   | 1.2           | 0.25 | 0.35   | 0.48     | 0.56   |
| C     | 2.7          | 1.5          | 0.90   | 0.90            | 0.95 | 0.95   | 1.3           | 0.25 | 0.35   | 0.60     | 0.68   |
| D     | 0.4          | 0.2          | 0.90   | 0.90            | 0.95 | 0.95   | 0.2           | 0.25 | 0.35   | 0.62     | 0.70   |
| E     | 0.7          | 0.1          | 0.90   | 0.90            | 0.95 | 0.95   | 0.6           | 0.25 | 0.35   | 0.35     | 0.44   |
| F     | 2.2          | 1.2          | 0.90   | 0.90            | 0.95 | 0.95   | 1.0           | 0.25 | 0.35   | 0.60     | 0.68   |
| G     | 1.6          | 1.2          | 0.90   | 0.90            | 0.95 | 0.95   | 0.4           | 0.25 | 0.35   | 0.72     | 0.78   |
| H     | 4.6          | 1.6          | 0.90   | 0.90            | 0.95 | 0.95   | 3.1           | 0.25 | 0.35   | 0.47     | 0.55   |
| I     | 0.2          | 0.0          | 0.90   | 0.90            | 0.95 | 0.95   | 0.2           | 0.25 | 0.35   | 0.25     | 0.35   |
| J     | 6.2          | 0.1          | 0.90   | 0.90            | 0.95 | 0.95   | 6.1           | 0.25 | 0.35   | 0.26     | 0.36   |
| K     | 3.3          | 1.2          | 0.90   | 0.90            | 0.95 | 0.95   | 2.1           | 0.25 | 0.35   | 0.49     | 0.57   |
| L     | 0.2          | 0.2          | 0.90   | 0.90            | 0.95 | 0.95   | 0.0           | 0.25 | 0.35   | 0.90     | 0.95   |
| M     | 0.3          | 0.0          | 0.90   | 0.90            | 0.95 | 0.95   | 0.3           | 0.25 | 0.35   | 0.25     | 0.35   |

**DRAINAGE MAPS**

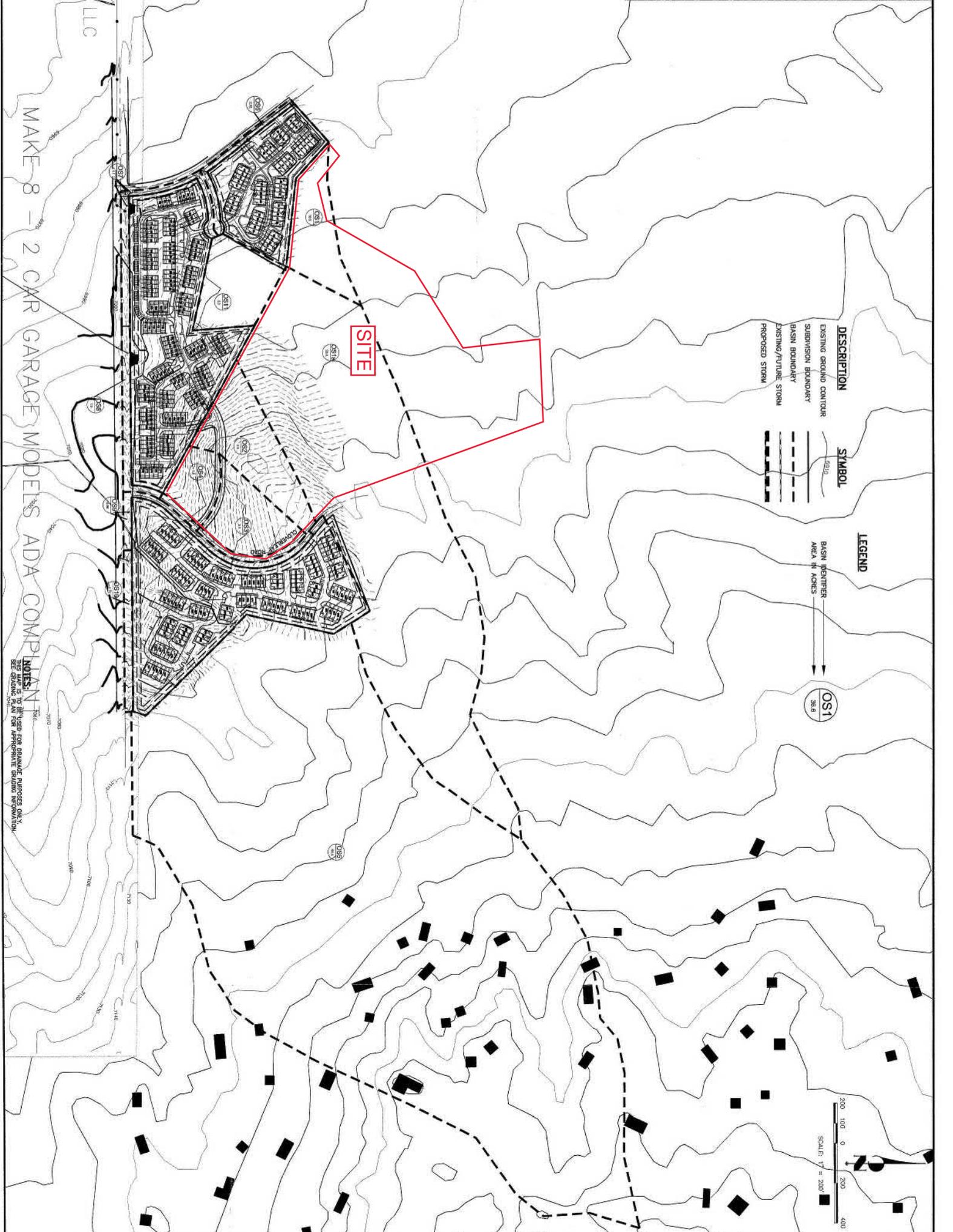
PROPOSED OFF-SITE DRAINAGE MAP

PROPOSED ON-SITE DRAINAGE MAP

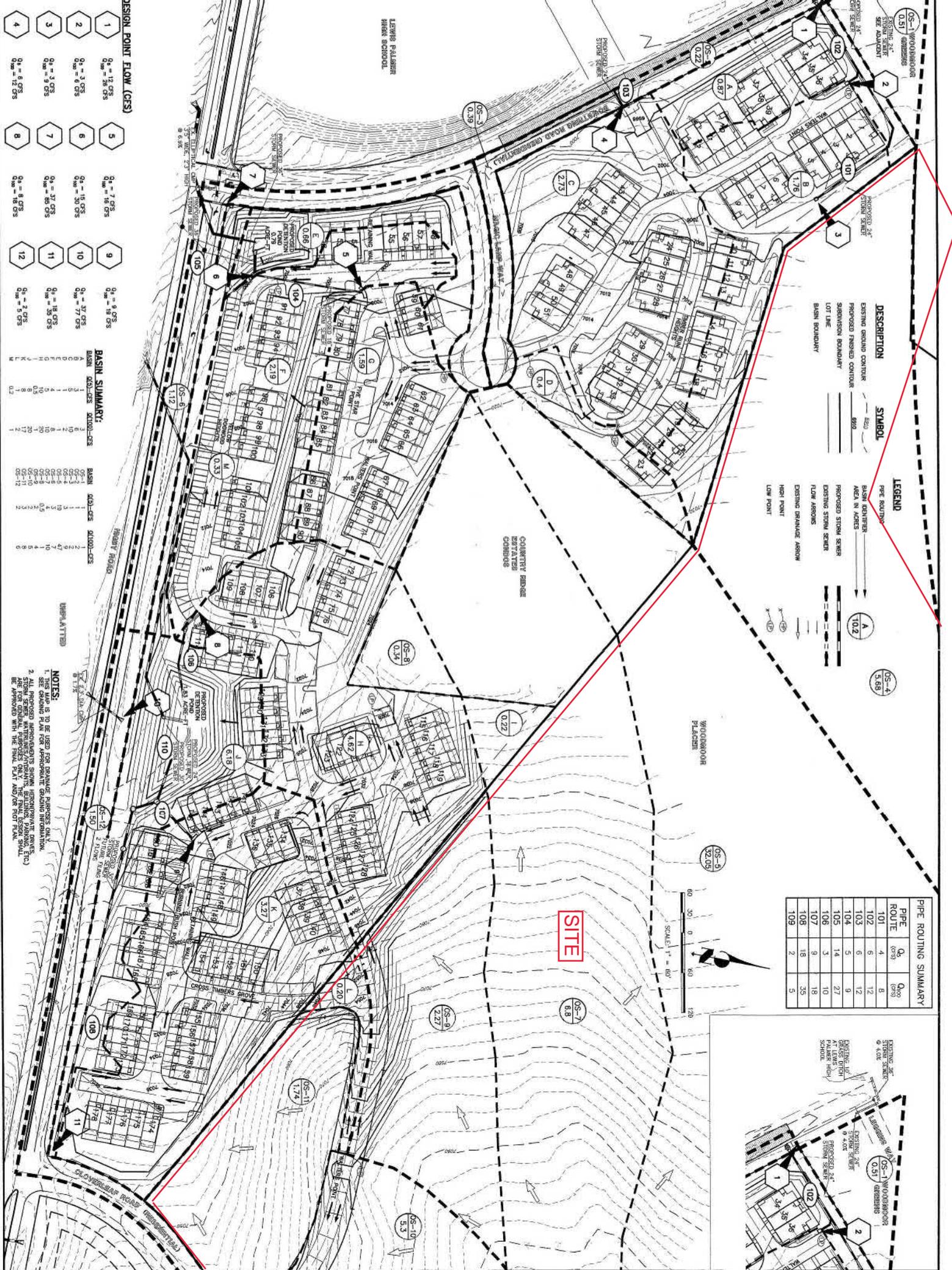
EXISTING DRAINAGE MAP

MAKE 8 - 2 CR GARAGE MODELS ADA COMPLIANT

LLC



NOTES:  
THIS PLAN IS TO BE USED FOR BROWNE PURPOSES ONLY.  
SEE GROUND PLAN FOR APPROPRIATE DRAINAGE INFORMATION.



**DESIGN POINT FLOW (GFS)**

|    |   |
|----|---|
| 1  | Q <sub>1</sub> = 12 GFS<br>Q <sub>10</sub> = 26 GFS |
| 2  | Q <sub>1</sub> = 3 GFS<br>Q <sub>10</sub> = 6 GFS   |
| 3  | Q <sub>1</sub> = 3 GFS<br>Q <sub>10</sub> = 9 GFS   |
| 4  | Q <sub>1</sub> = 6 GFS<br>Q <sub>10</sub> = 12 GFS  |
| 5  | Q <sub>1</sub> = 7 GFS<br>Q <sub>10</sub> = 16 GFS  |
| 6  | Q <sub>1</sub> = 15 GFS<br>Q <sub>10</sub> = 30 GFS |
| 7  | Q <sub>1</sub> = 37 GFS<br>Q <sub>10</sub> = 50 GFS |
| 8  | Q <sub>1</sub> = 18 GFS<br>Q <sub>10</sub> = 37 GFS |
| 9  | Q <sub>1</sub> = 18 GFS<br>Q <sub>10</sub> = 37 GFS |
| 10 | Q <sub>1</sub> = 37 GFS<br>Q <sub>10</sub> = 50 GFS |
| 11 | Q <sub>1</sub> = 18 GFS<br>Q <sub>10</sub> = 37 GFS |
| 12 | Q <sub>1</sub> = 2 GFS<br>Q <sub>10</sub> = 7 GFS   |

**PIPE ROUTING SUMMARY**

| PIPE ROUTE | Q <sub>1</sub> (GFS) | Q <sub>10</sub> (GFS) |
|------------|----------------------|-----------------------|
| 101        | 4                    | 8                     |
| 102        | 6                    | 12                    |
| 103        | 6                    | 12                    |
| 104        | 5                    | 9                     |
| 105        | 14                   | 27                    |
| 106        | 3                    | 10                    |
| 107        | 9                    | 18                    |
| 108        | 18                   | 35                    |
| 109        | 2                    | 5                     |

**LEGEND**

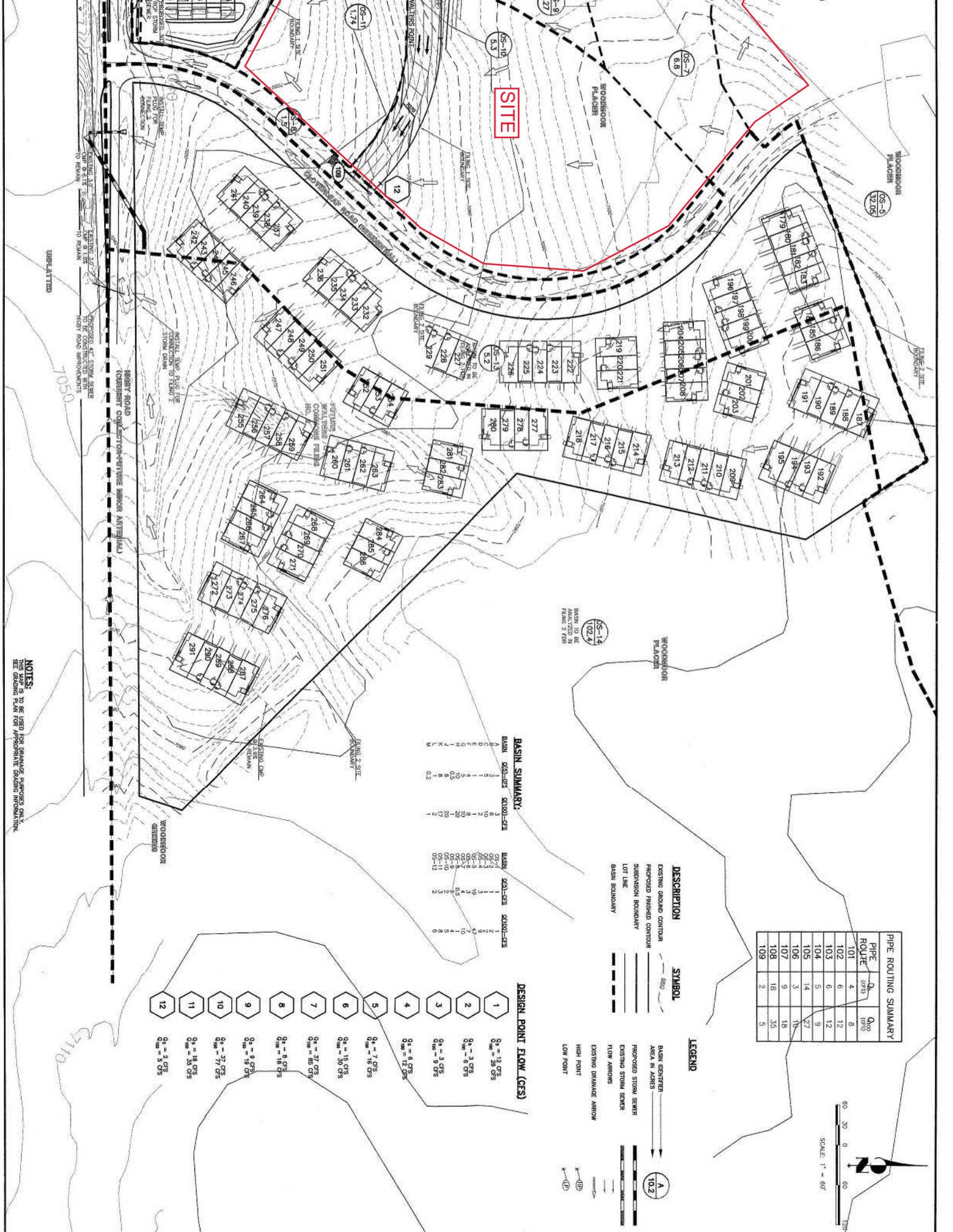
- EXISTING GROUND CONTOUR
- PROPOSED FINISHED CONTOUR
- SUBDIVISION BOUNDARY
- LOT LINE
- BASEIN BOUNDARY
- PIPE ROUTING
- BASEIN DIVERTER
- FEEL IN FEET
- PROPOSED STORM SEWER
- EXISTING STORM SEWER
- FLOW ARROWS
- EXISTING DRAINAGE ARROW
- HIGH POINT
- LOW POINT

**BASEIN SUMMARY:**

| BASEIN | NO. LOTS | Q <sub>100</sub> -GFS | BASEIN | NO. LOTS | Q <sub>100</sub> -GFS |
|--------|----------|-----------------------|--------|----------|-----------------------|
| A      | 1        | 10                    | 1      | 2        | 2                     |
| B      | 2        | 10                    | 2      | 3        | 3                     |
| C      | 3        | 10                    | 3      | 4        | 4                     |
| D      | 4        | 10                    | 4      | 5        | 5                     |
| E      | 5        | 10                    | 5      | 6        | 6                     |
| F      | 6        | 10                    | 6      | 7        | 7                     |
| G      | 7        | 10                    | 7      | 8        | 8                     |
| H      | 8        | 10                    | 8      | 9        | 9                     |
| I      | 9        | 10                    | 9      | 10       | 10                    |
| J      | 10       | 10                    | 10     | 11       | 11                    |
| K      | 11       | 10                    | 11     | 12       | 12                    |
| L      | 12       | 10                    | 12     | 13       | 13                    |
| M      | 13       | 10                    | 13     | 14       | 14                    |
| N      | 14       | 10                    | 14     | 15       | 15                    |
| O      | 15       | 10                    | 15     | 16       | 16                    |
| P      | 16       | 10                    | 16     | 17       | 17                    |
| Q      | 17       | 10                    | 17     | 18       | 18                    |
| R      | 18       | 10                    | 18     | 19       | 19                    |
| S      | 19       | 10                    | 19     | 20       | 20                    |
| T      | 20       | 10                    | 20     | 21       | 21                    |
| U      | 21       | 10                    | 21     | 22       | 22                    |
| V      | 22       | 10                    | 22     | 23       | 23                    |
| W      | 23       | 10                    | 23     | 24       | 24                    |
| X      | 24       | 10                    | 24     | 25       | 25                    |
| Y      | 25       | 10                    | 25     | 26       | 26                    |
| Z      | 26       | 10                    | 26     | 27       | 27                    |
| AA     | 27       | 10                    | 27     | 28       | 28                    |
| AB     | 28       | 10                    | 28     | 29       | 29                    |
| AC     | 29       | 10                    | 29     | 30       | 30                    |
| AD     | 30       | 10                    | 30     | 31       | 31                    |
| AE     | 31       | 10                    | 31     | 32       | 32                    |
| AF     | 32       | 10                    | 32     | 33       | 33                    |
| AG     | 33       | 10                    | 33     | 34       | 34                    |
| AH     | 34       | 10                    | 34     | 35       | 35                    |
| AI     | 35       | 10                    | 35     | 36       | 36                    |
| AJ     | 36       | 10                    | 36     | 37       | 37                    |
| AK     | 37       | 10                    | 37     | 38       | 38                    |
| AL     | 38       | 10                    | 38     | 39       | 39                    |
| AM     | 39       | 10                    | 39     | 40       | 40                    |
| AN     | 40       | 10                    | 40     | 41       | 41                    |
| AO     | 41       | 10                    | 41     | 42       | 42                    |
| AP     | 42       | 10                    | 42     | 43       | 43                    |
| AQ     | 43       | 10                    | 43     | 44       | 44                    |
| AR     | 44       | 10                    | 44     | 45       | 45                    |
| AS     | 45       | 10                    | 45     | 46       | 46                    |
| AT     | 46       | 10                    | 46     | 47       | 47                    |
| AU     | 47       | 10                    | 47     | 48       | 48                    |
| AV     | 48       | 10                    | 48     | 49       | 49                    |
| AW     | 49       | 10                    | 49     | 50       | 50                    |
| AX     | 50       | 10                    | 50     | 51       | 51                    |
| AY     | 51       | 10                    | 51     | 52       | 52                    |
| AZ     | 52       | 10                    | 52     | 53       | 53                    |
| BA     | 53       | 10                    | 53     | 54       | 54                    |
| BB     | 54       | 10                    | 54     | 55       | 55                    |
| BC     | 55       | 10                    | 55     | 56       | 56                    |
| BD     | 56       | 10                    | 56     | 57       | 57                    |
| BE     | 57       | 10                    | 57     | 58       | 58                    |
| BF     | 58       | 10                    | 58     | 59       | 59                    |
| BG     | 59       | 10                    | 59     | 60       | 60                    |
| BH     | 60       | 10                    | 60     | 61       | 61                    |
| BI     | 61       | 10                    | 61     | 62       | 62                    |
| BJ     | 62       | 10                    | 62     | 63       | 63                    |
| BK     | 63       | 10                    | 63     | 64       | 64                    |
| BL     | 64       | 10                    | 64     | 65       | 65                    |
| BM     | 65       | 10                    | 65     | 66       | 66                    |
| BN     | 66       | 10                    | 66     | 67       | 67                    |
| BO     | 67       | 10                    | 67     | 68       | 68                    |
| BP     | 68       | 10                    | 68     | 69       | 69                    |
| BQ     | 69       | 10                    | 69     | 70       | 70                    |
| BR     | 70       | 10                    | 70     | 71       | 71                    |
| BS     | 71       | 10                    | 71     | 72       | 72                    |
| BT     | 72       | 10                    | 72     | 73       | 73                    |
| BU     | 73       | 10                    | 73     | 74       | 74                    |
| BV     | 74       | 10                    | 74     | 75       | 75                    |
| BW     | 75       | 10                    | 75     | 76       | 76                    |
| BX     | 76       | 10                    | 76     | 77       | 77                    |
| BY     | 77       | 10                    | 77     | 78       | 78                    |
| BZ     | 78       | 10                    | 78     | 79       | 79                    |
| CA     | 79       | 10                    | 79     | 80       | 80                    |
| CB     | 80       | 10                    | 80     | 81       | 81                    |
| CC     | 81       | 10                    | 81     | 82       | 82                    |
| CD     | 82       | 10                    | 82     | 83       | 83                    |
| CE     | 83       | 10                    | 83     | 84       | 84                    |
| CF     | 84       | 10                    | 84     | 85       | 85                    |
| CG     | 85       | 10                    | 85     | 86       | 86                    |
| CH     | 86       | 10                    | 86     | 87       | 87                    |
| CI     | 87       | 10                    | 87     | 88       | 88                    |
| CJ     | 88       | 10                    | 88     | 89       | 89                    |
| CK     | 89       | 10                    | 89     | 90       | 90                    |
| CL     | 90       | 10                    | 90     | 91       | 91                    |
| CM     | 91       | 10                    | 91     | 92       | 92                    |
| CN     | 92       | 10                    | 92     | 93       | 93                    |
| CO     | 93       | 10                    | 93     | 94       | 94                    |
| CP     | 94       | 10                    | 94     | 95       | 95                    |
| CQ     | 95       | 10                    | 95     | 96       | 96                    |
| CR     | 96       | 10                    | 96     | 97       | 97                    |
| CS     | 97       | 10                    | 97     | 98       | 98                    |
| CT     | 98       | 10                    | 98     | 99       | 99                    |
| CU     | 99       | 10                    | 99     | 100      | 100                   |
| CV     | 100      | 10                    | 100    | 101      | 101                   |
| CU     | 101      | 10                    | 101    | 102      | 102                   |
| CV     | 102      | 10                    | 102    | 103      | 103                   |
| CW     | 103      | 10                    | 103    | 104      | 104                   |
| CV     | 104      | 10                    | 104    | 105      | 105                   |
| CW     | 105      | 10                    | 105    | 106      | 106                   |
| CV     | 106      | 10                    | 106    | 107      | 107                   |
| CW     | 107      | 10                    | 107    | 108      | 108                   |
| CV     | 108      | 10                    | 108    | 109      | 109                   |
| CW     | 109      | 10                    | 109    | 110      | 110                   |
| CV     | 110      | 10                    | 110    | 111      | 111                   |
| CW     | 111      | 10                    | 111    | 112      | 112                   |
| CV     | 112      | 10                    | 112    | 113      | 113                   |
| CW     | 113      | 10                    | 113    | 114      | 114                   |
| CV     | 114      | 10                    | 114    | 115      | 115                   |
| CW     | 115      | 10                    | 115    | 116      | 116                   |
| CV     | 116      | 10                    | 116    | 117      | 117                   |
| CW     | 117      | 10                    | 117    | 118      | 118                   |
| CV     | 118      | 10                    | 118    | 119      | 119                   |
| CW     | 119      | 10                    | 119    | 120      | 120                   |
| CV     | 120      | 10                    | 120    | 121      | 121                   |
| CW     | 121      | 10                    | 121    | 122      | 122                   |
| CV     | 122      | 10                    | 122    | 123      | 123                   |
| CW     | 123      | 10                    | 123    | 124      | 124                   |
| CV     | 124      | 10                    | 124    | 125      | 125                   |
| CW     | 125      | 10                    | 125    | 126      | 126                   |
| CV     | 126      | 10                    | 126    | 127      | 127                   |
| CW     | 127      | 10                    | 127    | 128      | 128                   |
| CV     | 128      | 10                    | 128    | 129      | 129                   |
| CW     | 129      | 10                    | 129    | 130      | 130                   |
| CV     | 130      | 10                    | 130    | 131      | 131                   |
| CW     | 131      | 10                    | 131    | 132      | 132                   |
| CV     | 132      | 10                    | 132    | 133      | 133                   |
| CW     | 133      | 10                    | 133    | 134      | 134                   |
| CV     | 134      | 10                    | 134    | 135      | 135                   |
| CW     | 135      | 10                    | 135    | 136      | 136                   |
| CV     | 136      | 10                    | 136    | 137      | 137                   |
| CW     | 137      | 10                    | 137    | 138      | 138                   |
| CV     | 138      | 10                    | 138    | 139      | 139                   |
| CW     | 139      | 10                    | 139    | 140      | 140                   |
| CV     | 140      | 10                    | 140    | 141      | 141                   |
| CW     | 141      | 10                    | 141    | 142      | 142                   |
| CV     | 142      | 10                    | 142    | 143      | 143                   |
| CW     | 143      | 10                    | 143    | 144      | 144                   |
| CV     | 144      | 10                    | 144    | 145      | 145                   |
| CW     | 145      | 10                    | 145    | 146      | 146                   |
| CV     | 146      | 10                    | 146    | 147      | 147                   |
| CW     | 147      | 10                    | 147    | 148      | 148                   |
| CV     | 148      | 10                    | 148    | 149      | 149                   |
| CW     | 149      | 10                    | 149    | 150      | 150                   |

**NOTES:**

- ALL PROPOSED IMPROVEMENTS SHOWN HEREON (PRIVATE DRAINAGE, STORM SEWER, WATER MAINS, PLUMBING, GAS, ETC.) ARE SUBJECT TO THE FINAL APPROVED GRADING INFORMATION.
- ALL PROPOSED IMPROVEMENTS SHOWN HEREON (PRIVATE DRAINAGE, STORM SEWER, WATER MAINS, PLUMBING, GAS, ETC.) BE APPROVED WITH THE FINAL PLAN AND/OR FLOOD PLAN.



**SITE**

| PIPE ROUTE | Q <sub>100</sub> (CFS) | Q <sub>50</sub> (CFS) |
|------------|------------------------|-----------------------|
| 101        | 4                      | 8                     |
| 102        | 6                      | 12                    |
| 103        | 5                      | 12                    |
| 104        | 5                      | 9                     |
| 105        | 14                     | 27                    |
| 106        | 3                      | 11                    |
| 107        | 9                      | 18                    |
| 108        | 18                     | 35                    |
| 109        | 2                      | 5                     |

**BASIN SUMMARY:**

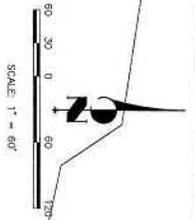
| BASIN | Q <sub>100</sub> -CFS | ACTUAL-CFS |
|-------|-----------------------|------------|
| A     | 1                     | 1          |
| B     | 1                     | 1          |
| C     | 1                     | 1          |
| D     | 1                     | 1          |
| E     | 1                     | 1          |
| F     | 1                     | 1          |
| G     | 1                     | 1          |
| H     | 1                     | 1          |
| I     | 1                     | 1          |
| J     | 1                     | 1          |
| K     | 1                     | 1          |
| L     | 0.2                   | 0.2        |

**DESIGN POINT FLOW (CFS)**

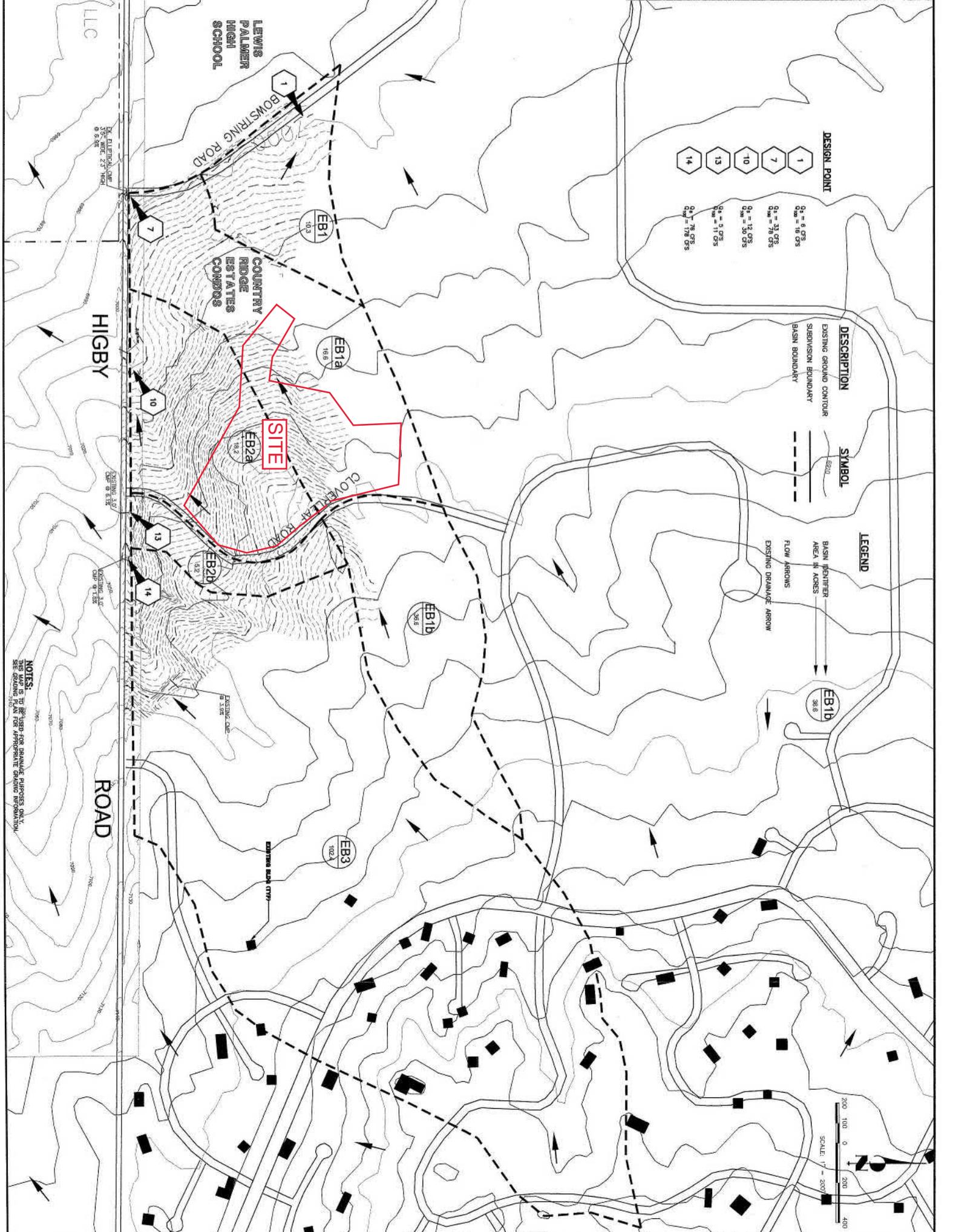
- 1 Q<sub>1</sub> = 12 CFS  
Q<sub>50</sub> = 26 CFS
- 2 Q<sub>1</sub> = 3 CFS  
Q<sub>50</sub> = 8 CFS
- 3 Q<sub>1</sub> = 3 CFS  
Q<sub>50</sub> = 9 CFS
- 4 Q<sub>1</sub> = 6 CFS  
Q<sub>50</sub> = 12 CFS
- 5 Q<sub>1</sub> = 7 CFS  
Q<sub>50</sub> = 16 CFS
- 6 Q<sub>1</sub> = 18 CFS  
Q<sub>50</sub> = 30 CFS
- 7 Q<sub>1</sub> = 37 CFS  
Q<sub>50</sub> = 66 CFS
- 8 Q<sub>1</sub> = 8 CFS  
Q<sub>50</sub> = 16 CFS
- 9 Q<sub>1</sub> = 9 CFS  
Q<sub>50</sub> = 19 CFS
- 10 Q<sub>1</sub> = 37 CFS  
Q<sub>50</sub> = 77 CFS
- 11 Q<sub>1</sub> = 18 CFS  
Q<sub>50</sub> = 35 CFS
- 12 Q<sub>1</sub> = 3 CFS  
Q<sub>50</sub> = 9 CFS

| DESCRIPTION                  | SYMBOL |
|------------------------------|--------|
| EXISTING GROUND CONTOUR      |        |
| PROPOSED FINISHED CONTOUR    |        |
| SUBDIVISION BOUNDARY         |        |
| LOT LINE                     |        |
| BASIN BOUNDARY               |        |
| BASIN ENGINEER AREA IN ACRES |        |
| PROPOSED STORM SEWER         |        |
| EXISTING STORM SEWER         |        |
| FLOW ARROWS                  |        |
| EXISTING RENAISSANCE ARROW   |        |
| HIGH POINT                   |        |
| LOW POINT                    |        |

**LEGEND**



**NOTES:**  
THIS PLAN IS TO BE USED FOR DRAINAGE PURPOSES ONLY.  
SEE SHEETS FOR APPROPRIATE DRAINAGE INFORMATION.



**DESIGN POINT**

|    |  |
|----|--|
| 1  | $Q_{in} = 8.075$<br>$Q_{out} = 10.075$   |
| 7  | $Q_{in} = 33.075$<br>$Q_{out} = 78.075$  |
| 10 | $Q_{in} = 12.075$<br>$Q_{out} = 30.075$  |
| 13 | $Q_{in} = 5.075$<br>$Q_{out} = 11.075$   |
| 14 | $Q_{in} = 78.075$<br>$Q_{out} = 178.075$ |

**DESCRIPTION**

|                         |  |
|-------------------------|--|
| EXISTING GROUND CONTOUR |  |
| SUBDIVISION BOUNDARY    |  |
| BASIN BOUNDARY          |  |

**SYMBOL**

**LEGEND**

|                         |  |
|-------------------------|--|
| BASIN IDENTIFIER        |  |
| AREA IN ACRES           |  |
| FLOW ARROWS             |  |
| EXISTING DRAINAGE ARROW |  |

**NOTES:**  
THIS PLAN IS TO BE USED FOR DRAINAGE PURPOSES ONLY.  
IT IS NOT TO BE USED FOR ANY OTHER PURPOSES WITHOUT THE WRITTEN CONSENT OF THE ENGINEER.





**J·R ENGINEERING**  
A Westrian Company

**ADDENDUM TO  
FINAL DRAINAGE REPORT  
FOR  
WALTERS COMMONS**

November 2006

Prepared For:

**PULTE HOME CORPORATION**  
1975 Research Parkway  
Colorado Springs, CO 80920  
(719) 536-4200

Prepared By:

**JR ENGINEERING**  
4310 ArrowsWest Drive  
Colorado Springs, CO 80907  
(719) 593-2593

Job No. 9170.72

ADDENDUM TO  
FINAL DRAINAGE REPORT  
FOR  
WALTERS COMMONS  
DRAINAGE REPORT STATEMENT



J-R ENGINEERING  
A Westrian Company

ENGINEER'S STATEMENT:

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the County for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors, or omissions on my part in preparing this report.

  
Mike A. Bramlett, Colorado P.E. #32314  
For and On Behalf of JR Engineering  


11/20/06  
Date

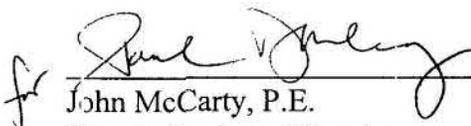
DEVELOPER'S STATEMENT:

I, the developer, have read and will comply with all of the requirements specified in this drainage report and plan.

Business Name: Pulte Homes  
By:   
Title: Vice President of Land  
Address: 1975 Research Parkway  
Colorado Springs, CO 80920

EL PASO COUNTY ONLY:

Filed in accordance with Section 51.1 of the El Paso Land Development Code, as amended.

  
John McCarty, P.E.  
County Engineer/Director

11-22-06  
Date

Conditions:

## **ADDENDUM TO FINAL DRAINAGE REPORT FOR WALTERS COMMONS**

### **PURPOSE**

The purpose of this addendum is to identify changes to the approved final drainage report, as a result of construction procedures and current drainage conditions at the intersection of Cloverleaf Rd. and Higby Rd. The previously approved drainage patterns for drainage basin A-1, referred to as OS-10 and OS-8 in the approved Final Drainage Report for Walters Commons, have been revised from the original design. See attached Proposed On-Site Drainage Area Map for more information. It is the intent of this report to calculate the revised storm water runoff quantities as a result of revisions to the Walters Commons development. In addition, recommend proposed drainage facilities and calculate impacts to current storm sewer routing.

### **GENERAL DESCRIPTION**

The general description for this project has remained the same, except that the project is now platted as Walter Commons Filing 1. For more information, see the approved Final Drainage Report for Walters Commons Filing 1.

### **PROPOSED DRAINAGE ADDENDUM**

In the previously approved drainage report for Walters Commons Filing 1, runoff from Basin A-1 (see Proposed On-Site Drainage Map) was captured by a drainage ditch along the west side of Cloverleaf Rd. The runoff was then conveyed south paralleling the road to the intersection of Cloverleaf Rd. and Higby Rd. At this point the runoff was routed west in a drainage ditch along the north side of Higby Rd to DP-10 of the previously approved drainage report for Walters Commons Filing 1. The drainage ditch along the north side of Higby Rd. was never constructed. In it's place, a curb line was constructed and the ditch was removed to prevent relocating utilities in this area. As a result, the runoff from basin A-1 currently discharges into Higby Rd. at the intersection of Cloverleaf Rd. and Higby Rd., resulting in concentrated storm water entering Higby Rd.

This Addendum proposes that a Type-C CDOT inlet be constructed at the northwest corner of the intersection of Cloverleaf Road and Higby Road to collect the additional storm water from basin A-1 ( $Q_5 = 4$  cfs and  $Q_{100} = 10$  cfs). The runoff collected by the inlet will be routed south via 15' of 18" RCP to the existing 30" RCP, (Design point 11) installed with the original design. From this point the runoff is routed to the proposed 1.83 acre-ft detention pond.

The pond's current design does not accommodate basin A-1, but the effects of the increased runoff ( $Q_5 = 4$  cfs and  $Q_{100} = 10$  cfs) will be negligible to the function of the pond. The pond will function as previously approved except in the most extreme 100-yr event. During this storm event, the pond will overtop the spillway ( $Q_{100} = 7$  cfs) and be collected by the existing 24" storm sewer pipe located at DP-10. Since DP-10 was the original collection point of basin A-1, we feel that the impacts are minimal to this system. In addition, the existing 24" storm sewer pipe has a capacity of 17.8 cfs, which is more than adequate to convey the additional runoff that will overtop the spillway. See Appendix for backup calculations.

## **ADDENDUM IMPACTS TO FACILITIES**

### **Design Point 10**

Design Point 10 is in the same location as in the previously approved drainage report for Walters Commons Filing 1. Only minimal flows that overtop the existing detention pond weir ( $Q_{100} = 7$  cfs) will be captured by the existing 24" storm sewer and conveyed under Higby Rd. The existing storm sewer pipe has a full flow capacity of 17.8 cfs, which is more than adequate to convey the discharge. See Appendix for backup calculations.

### **Design Point 11**

Design Point 11 is in the same location as in the previously approved drainage report for Walters Commons Filing 1, but now incorporates the additional flow captured at DP-13 as well as the existing flows at DP 14. Anticipated flows at this location will be  $Q_5 = 32$  cfs and  $Q_{100} = 66$  cfs.

### **Design Point 13**

Design Point 13 is located at the northwest corner of the intersection of Cloverleaf Road and Higby

Road. A proposed Type-C CDOT inlet will be installed at this location to capture the existing flows from drainage basin A-1. The flows will be approximately  $Q_5 = 4$  cfs and  $Q_{100} = 10$  cfs.

#### **Design Point 14**

Design Point 14 is the same design point as design point 6 in the previously approved drainage report for Walters Commons Filing 2. The flows at this design point will be generated by the Walters Commons Filing 2 project. Flows in this existing pipe are  $Q_5 = 28$  cfs and  $Q_{100} = 56$  cfs.

### **STORM SEWER ROUTING AND PROPOSED DRAINAGE STRUCTURES**

#### **Pipe Design Point 108**

Incorporates the developed flows from Walters Commons Filing 2 (DP-14) and the rerouted flows from drainage basin A-1 (DP-13). The runoff will travel to the existing 1.83 arce-ft detention pond in Filing 1 via an existing 30" RCP storm sewer. The existing facility will now convey  $Q_5 = 32$  cfs and  $Q_{100} = 66$  cfs. The existing pipe has adequate capacity (Full flow capacity = 66 CFS) to convey this additional runoff. See Proposed Facility Hydraulic Calculations for more information.

#### **Pipe Design Point 200**

This design point incorporates the flows at DP-13 from drainage basin A-1. The flows will be conveyed via an 18" RCP storm sewer (Full flow capacity = 70 CFS) from the proposed Type-C CDOT inlet to the existing 30" RCP storm sewer. This proposed facility will carry  $Q_5 = 4$  cfs and  $Q_{100} = 10$  cfs. See Proposed Facility Hydraulic Calculations for more information.

#### **Pipe Design Point 201**

This design point incorporates the flows that overtop the existing detention pond's weir in the most extreme event. Per the revised pond calculations located in the Appendix, 7cfs will overtop the spillway for roughly 35 minutes. The runoff will be conveyed under Higby Rd. by an existing 24" storm sewer (Full Flow Capacity = 17.8cfs). See Proposed Facility Hydraulic Calculations and Proposed Detention Pond Calculations for more information.

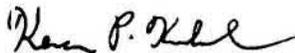
All other conditions will remain consistent with the previously approved Final Drain Report for Walters Commons.

## **SUMMARY**

We conclude that the installation of a Type-C CDOT inlet at the intersection of Cloverleaf Rd. and Higby Rd. will be adequate to collect and convey the existing runoff from drainage basin A-1. This conclusion is based on the fact that the existing storm sewer has adequate capacity for the increased flow. In addition, the existing detention pond will face minimal impacts, except in the most extreme event, due to the increased runoff. In the event of a 100-yr storm, the pond will overtop via the emergency spillway and be conveyed under Higby Rd. through the existing 24" CMP storm sewer. Finally, the proposed improvement will eliminate the concentrated runoff that is currently entering into Higby Rd.

PREPARED BY:

**JR Engineering**



Kevan P. Kuhnel, E.I.  
Engineer II

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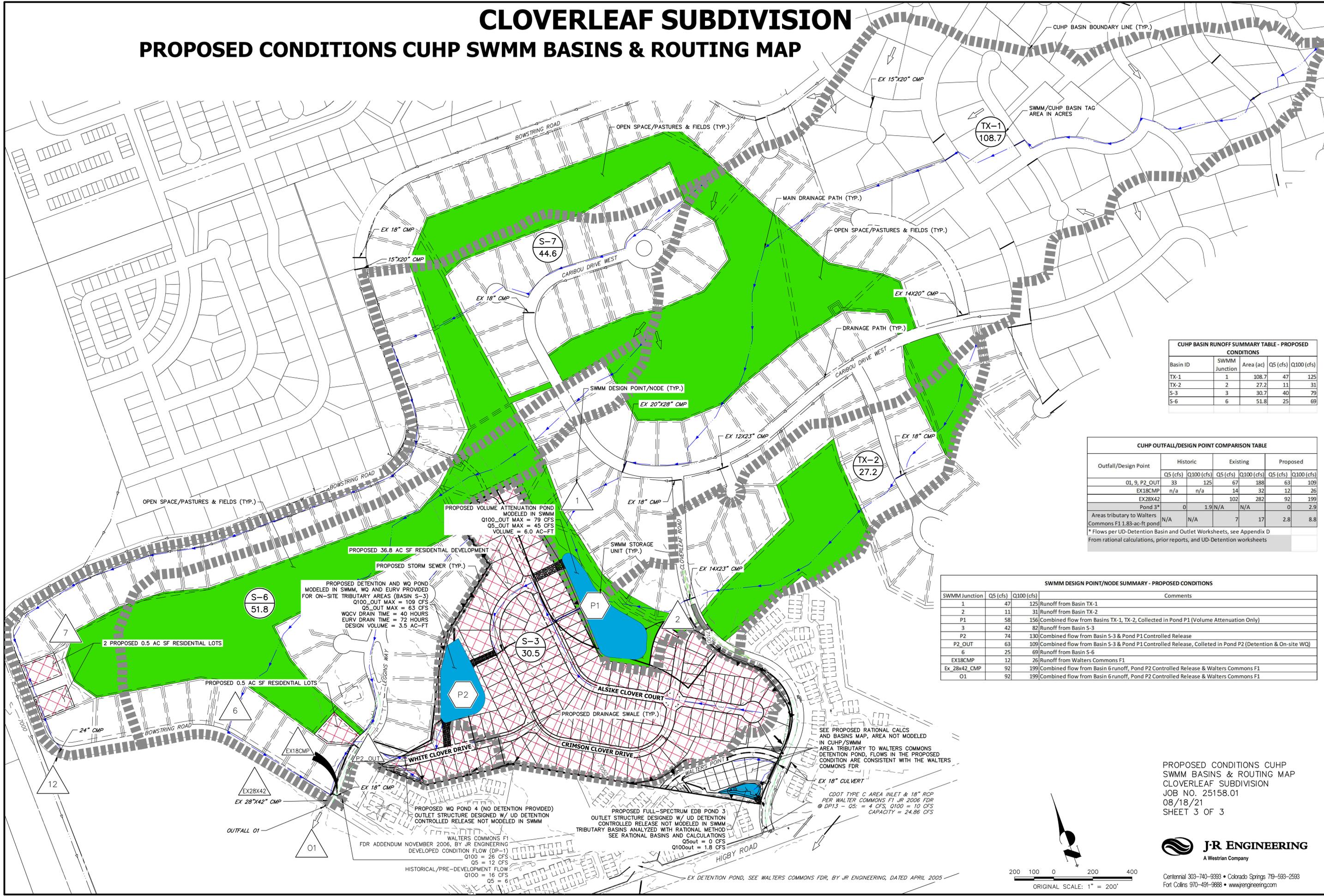
## **Appendix F**

### **Drainage Maps**



# CLOVERLEAF SUBDIVISION

## PROPOSED CONDITIONS CUHP SWMM BASINS & ROUTING MAP



**CUHP BASIN RUNOFF SUMMARY TABLE - PROPOSED CONDITIONS**

| Basin ID | SWMM Junction | Area (ac) | Q5 (cfs) | Q100 (cfs) |
|----------|---------------|-----------|----------|------------|
| TX-1     | 1             | 108.7     | 47       | 125        |
| TX-2     | 2             | 27.2      | 11       | 31         |
| S-3      | 3             | 30.7      | 40       | 79         |
| S-6      | 6             | 51.8      | 25       | 69         |

**CUHP OUTFALL/DESIGN POINT COMPARISON TABLE**

| Outfall/Design Point                                  | Historic |            | Existing |            | Proposed |            |
|---|----------|------------|----------|------------|----------|------------|
|   | Q5 (cfs) | Q100 (cfs) | Q5 (cfs) | Q100 (cfs) | Q5 (cfs) | Q100 (cfs) |
| O1, 9, P2_OUT   | 33       | 125        | 67       | 188        | 63       | 109        |
| EX18CMP   | n/a      | n/a        | 14       | 32         | 12       | 26         |
| EX28X42   |          |            | 102      | 282        | 92       | 299        |
| Pond 3*   | 0        | 1.9        | N/A      | N/A        | 0        | 2.9        |
| Areas tributary to Walters Commons F1 1.83-ac-ft pond | N/A      | N/A        | 7        | 17         | 2.8      | 8.8        |

\* Flows per UD-Detention Basin and Outlet Worksheets, see Appendix D  
From rational calculations, prior reports, and UD-Detention worksheets

**SWMM DESIGN POINT/NODE SUMMARY - PROPOSED CONDITIONS**

| SWMM Junction | Q5 (cfs) | Q100 (cfs) | Comments   |
|---------------|----------|------------|--|
| 1             | 47       | 125        | Runoff from Basin TX-1   |
| 2             | 11       | 31         | Runoff from Basin TX-2   |
| P1            | 58       | 156        | Combined flow from Basins TX-1, TX-2, Collected in Pond P1 (Volume Attenuation Only)                     |
| 3             | 42       | 82         | Runoff from Basin S-3  |
| P2            | 74       | 130        | Combined flow from Basin S-3 & Pond P1 Controlled Release  |
| P2_OUT        | 63       | 109        | Combined flow from Basin S-3 & Pond P1 Controlled Release, Collected in Pond P2 (Detention & On-site WQ) |
| 6             | 25       | 69         | Runoff from Basin S-6  |
| EX18CMP       | 12       | 26         | Runoff from Walters Commons F1   |
| Ex 28x42 CMP  | 92       | 199        | Combined flow from Basin 6 runoff, Pond P2 Controlled Release & Walters Commons F1                       |
| O1            | 92       | 199        | Combined flow from Basin 6 runoff, Pond P2 Controlled Release & Walters Commons F1                       |

**PROPOSED VOLUME ATTENUATION POND**  
 MODELED IN SWMM  
 Q100\_OUT MAX = 79 CFS  
 Q5\_OUT MAX = 45 CFS  
 VOLUME = 6.0 AC-FT

**PROPOSED DETENTION AND WQ POND**  
 MODELED IN SWMM, WQ AND EURV PROVIDED FOR ON-SITE TRIBUTARY AREAS (BASIN S-3)  
 Q100\_OUT MAX = 109 CFS  
 Q5\_OUT MAX = 63 CFS  
 WQV DRAIN TIME = 40 HOURS  
 EURV DRAIN TIME = 72 HOURS  
 DESIGN VOLUME = 3.5 AC-FT

**PROPOSED WQ POND 4 (NO DETENTION PROVIDED)**  
 OUTLET STRUCTURE DESIGNED W/ UD DETENTION CONTROLLED RELEASE NOT MODELED IN SWMM

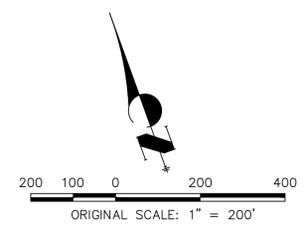
**PROPOSED FULL-SPECTRUM EDB POND 3**  
 OUTLET STRUCTURE DESIGNED W/ UD DETENTION CONTROLLED RELEASE NOT MODELED IN SWMM  
 TRIBUTARY BASINS ANALYZED WITH RATIONAL METHOD  
 SEE RATIONAL BASINS AND CALCULATIONS  
 Q5out = 0 CFS  
 Q100out = 1.8 CFS

SEE PROPOSED RATIONAL CALCS AND BASINS MAP, AREA NOT MODELED IN CUHP/SWMM  
 AREA TRIBUTARY TO WALTERS COMMONS DETENTION POND, FLOWS IN THE PROPOSED CONDITION ARE CONSISTENT WITH THE WALTERS COMMONS FDR

CDOT TYPE C AREA INLET & 18" RCP PER WALTERS COMMONS F1 JR 2006 FDR  
 @ DP13 - Q5 = 4 CFS, Q100 = 10 CFS  
 CAPACITY = 24.86 CFS

WALTERS COMMONS F1  
 FDR ADDENDUM NOVEMBER 2006, BY JR ENGINEERING  
 DEVELOPED CONDITION FLOW (DP-1)  
 Q100 = 26 CFS  
 Q5 = 12 CFS  
 HISTORICAL/PRE-DEVELOPMENT FLOW  
 Q100 = 16 CFS  
 Q5 = 6

EX DETENTION POND, SEE WALTERS COMMONS FDR, BY JR ENGINEERING, DATED APRIL 2005

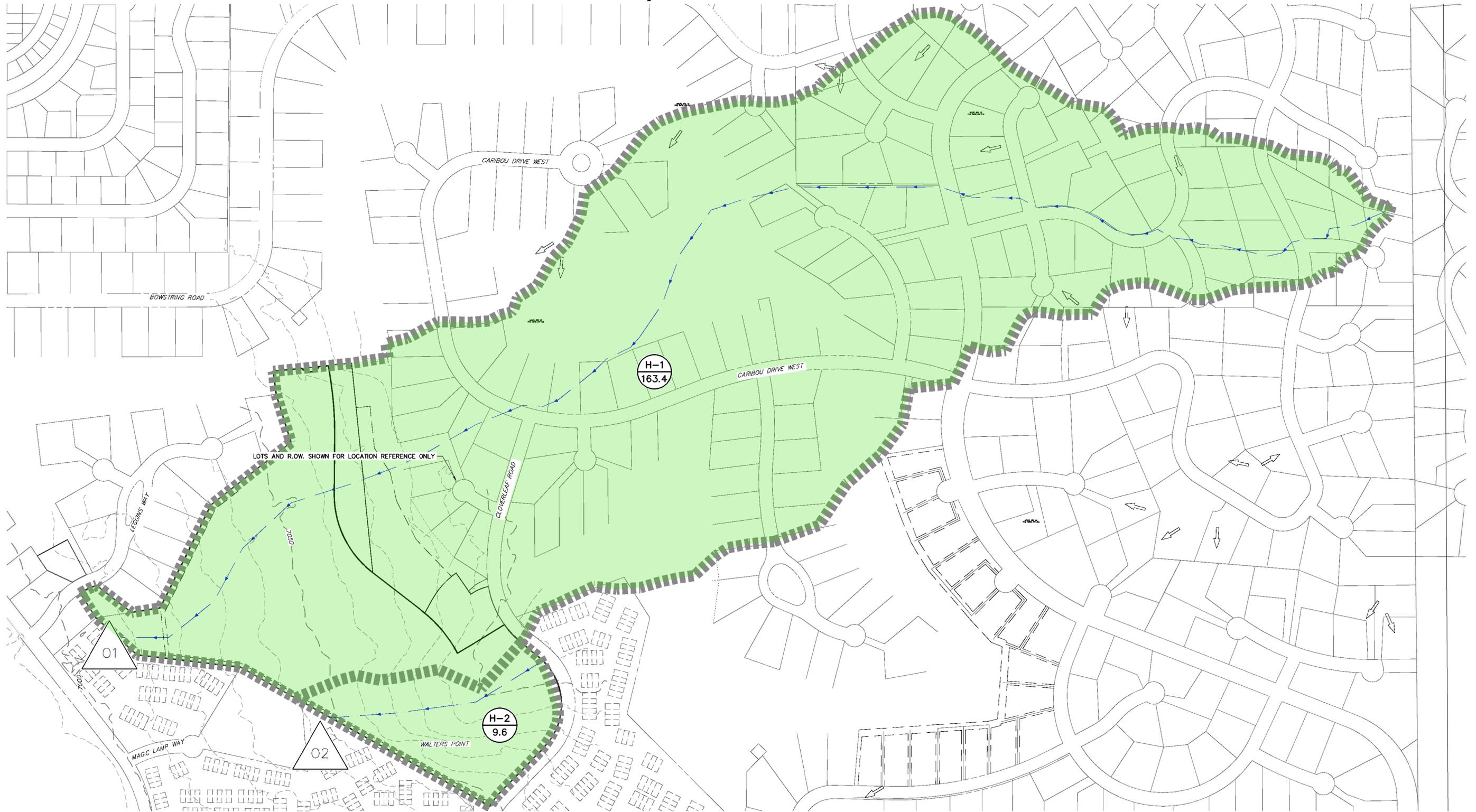


PROPOSED CONDITIONS CUHP  
 SWMM BASINS & ROUTING MAP  
 CLOVERLEAF SUBDIVISION  
 JOB NO. 25158.01  
 08/18/21  
 SHEET 3 OF 3



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# HISTORICAL CONDITIONS CUHP/SWMM BASINS MAP



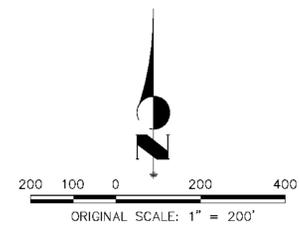
**CUHP BASIN RUNOFF SUMMARY TABLE - HISTORIC CONDITIONS**

| Basin ID | SWMM Junction | Area (ac) | Q5 (cfs) | Q100 (cfs) |
|----------|---------------|-----------|----------|------------|
| H-1      | 1             | 163.36    | 32.6     | 124.8      |
| H-2      | 2             | 9.62      | 2.8      | 31.4       |

**SWMM DESIGN POINT/NODE SUMMARY - HISTORIC CONDITIONS**

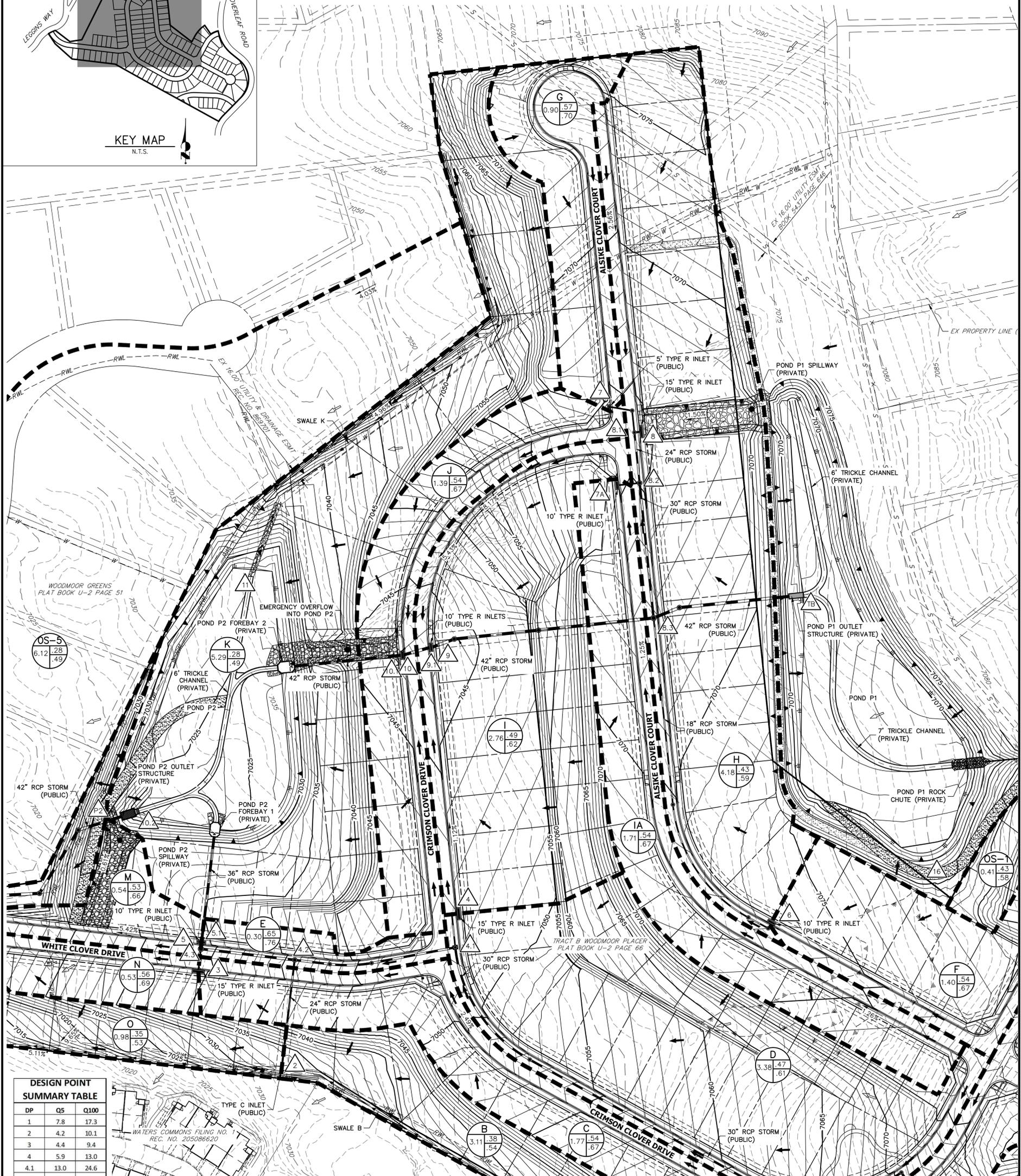
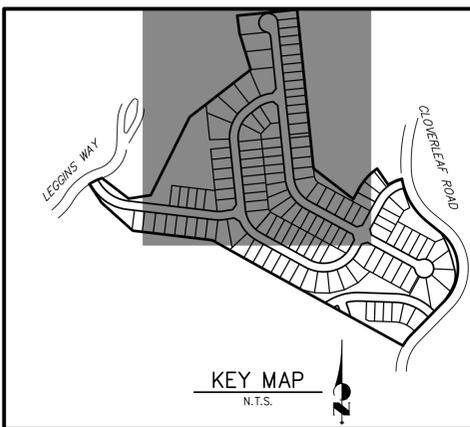
| SWMM Junction | Q5 (cfs) | Q100 (cfs) | Comments              |
|---------------|----------|------------|-----------------------|
| OUTFALL 1     | 32.6     | 124.8      | Runoff from Basin H-1 |
| OUTFALL 2     | 2.8      | 31.4       | Runoff from Basin H-2 |

25158.01  
CLOVERLEAF  
HISTORICAL CONDITIONS CUHP BASINS  
5/14/21  
SHEET 1 OF 1



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# CLOVERLEAF DRAINAGE MAPS



**DESIGN POINT SUMMARY TABLE**

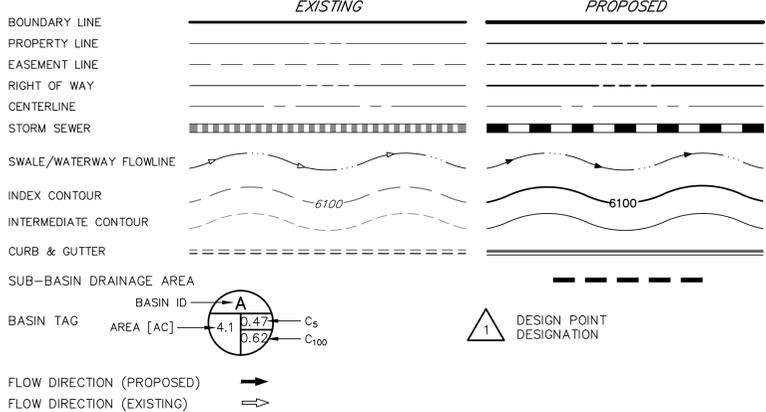
| DP   | Q5   | Q100  |
|------|------|-------|
| 1    | 7.8  | 17.3  |
| 2    | 4.2  | 10.1  |
| 3    | 4.4  | 9.4   |
| 4    | 5.9  | 13.0  |
| 4.1  | 13.0 | 24.6  |
| 4.2  | 16.7 | 33.6  |
| 4.3  | 20.1 | 40.4  |
| 5    | 1.0  | 2.0   |
| 5.1  | 20.7 | 41.7  |
| 6    | 3.4  | 6.9   |
| TB   | 45.2 | 78.5  |
| 7    | 2.4  | 5.1   |
| 7A   | 3.5  | 7.3   |
| 8    | 6.6  | 16.0  |
| 8.1  | 8.2  | 18.3  |
| 8.2  | 11.6 | 24.2  |
| 8.3  | 49.0 | 82.7  |
| 9    | 5.6  | 12.4  |
| 9.1  | 50.0 | 84.1  |
| 10   | 3.6  | 8.9   |
| 10.1 | 50.8 | 85.2  |
| 10.2 | 58.2 | 94.6  |
| 11   | 5.3  | 15.5  |
| 12   | 2.7  | 6.9   |
| 13   | 1.4  | 2.9   |
| 14   | 1.4  | 2.8   |
| 14.1 | 2.7  | 4.0   |
| 15   | 1.5  | 3.8   |
| 15.1 | 4.0  | 6.7   |
| 15.2 | 63.0 | 110.1 |
| 16   | 0.8  | 1.9   |
| 18   | 0.6  | 1.6   |
| 19   | 1.8  | 4.3   |
| L1   | 5.1  | 15.1  |
| L1.0 | 5.8  | 17.1  |
| L1.1 | 64.8 | 115.8 |
| P2   | 62.7 | 108.8 |



**BASIN SUMMARY TABLE**

| Tributary Sub-basin | Area (acres) | Percent Impervious | C <sub>s</sub> | C <sub>100</sub> | t <sub>c</sub> (min) | Q <sub>c</sub> (cfs) | Q <sub>100</sub> (cfs) |
|---------------------|--------------|--------------------|----------------|------------------|----------------------|----------------------|------------------------|
| A                   | 4.39         | 61%                | 0.47           | 0.62             | 12.4                 | 7.8                  | 17.3                   |
| B                   | 3.11         | 52%                | 0.38           | 0.54             | 14.7                 | 4.2                  | 10.1                   |
| C                   | 1.77         | 71%                | 0.54           | 0.67             | 8.5                  | 4.2                  | 8.7                    |
| D                   | 3.38         | 63%                | 0.47           | 0.61             | 13.0                 | 5.9                  | 13.0                   |
| E                   | 0.30         | 80%                | 0.65           | 0.76             | 5.0                  | 1.0                  | 2.0                    |
| F                   | 1.40         | 71%                | 0.54           | 0.67             | 8.2                  | 3.4                  | 6.9                    |
| G                   | 0.90         | 71%                | 0.57           | 0.70             | 6.5                  | 2.4                  | 5.1                    |
| H                   | 4.18         | 57%                | 0.43           | 0.59             | 13.6                 | 6.6                  | 15.2                   |
| I                   | 2.76         | 67%                | 0.49           | 0.62             | 9.7                  | 5.6                  | 12.0                   |
| IA                  | 1.71         | 71%                | 0.54           | 0.67             | 12.3                 | 3.5                  | 7.3                    |
| J                   | 1.39         | 71%                | 0.54           | 0.67             | 7.4                  | 3.5                  | 7.2                    |
| K                   | 5.29         | 36%                | 0.28           | 0.49             | 14.6                 | 5.3                  | 15.5                   |
| L                   | 1.97         | 42%                | 0.34           | 0.53             | 11.1                 | 2.7                  | 6.9                    |
| M                   | 0.54         | 70%                | 0.53           | 0.66             | 5.7                  | 1.4                  | 2.9                    |
| N                   | 0.53         | 72%                | 0.56           | 0.69             | 6.9                  | 1.4                  | 2.8                    |
| O                   | 0.98         | 47%                | 0.35           | 0.53             | 8.8                  | 1.5                  | 3.8                    |
| OS-1                | 0.41         | 38%                | 0.43           | 0.58             | 6.9                  | 0.8                  | 1.9                    |
| OS-2                | 0.79         | 28%                | 0.30           | 0.52             | 5.0                  | 1.2                  | 3.6                    |
| OS-3                | 0.31         | 37%                | 0.37           | 0.57             | 5.0                  | 0.6                  | 1.6                    |
| OS-4                | 1.00         | 28%                | 0.38           | 0.56             | 7.2                  | 1.8                  | 4.3                    |
| OS-5                | 6.12         | 20%                | 0.28           | 0.49             | 21.4                 | 5.1                  | 15.1                   |

**LAYER LINETYPE LEGEND**

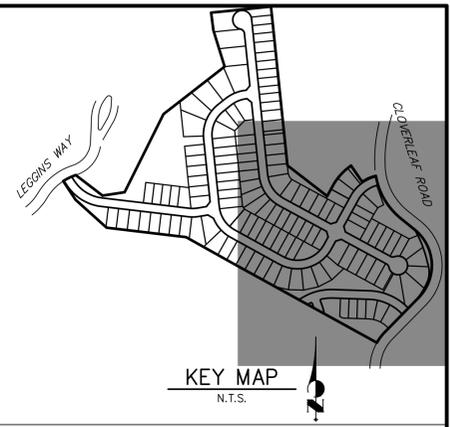


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# CLOVERLEAF DRAINAGE MAPS



## LAYER LINETYPE LEGEND

|                           | EXISTING | PROPOSED |
|---------------------------|----------|----------|
| BOUNDARY LINE             | —        | —        |
| PROPERTY LINE             | —        | —        |
| EASEMENT LINE             | —        | —        |
| RIGHT OF WAY              | —        | —        |
| CENTERLINE                | —        | —        |
| STORM SEWER               | —        | —        |
| SWALE/WATERWAY FLOWLINE   | —        | —        |
| INDEX CONTOUR             | —        | —        |
| INTERMEDIATE CONTOUR      | —        | —        |
| CURB & GUTTER             | —        | —        |
| SUB-BASIN DRAINAGE AREA   | —        | —        |
| BASIN TAG                 |          |          |
| FLOW DIRECTION (PROPOSED) | →        | →        |
| FLOW DIRECTION (EXISTING) | →        | →        |

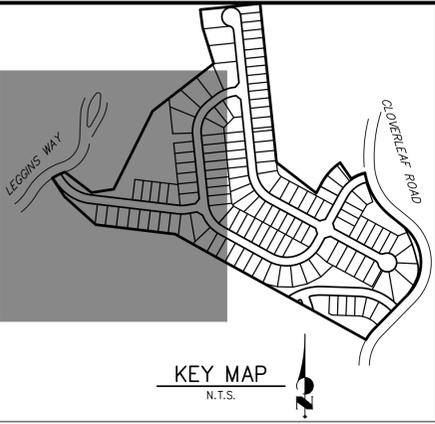
CLOVERLEAF FILING NO. 2  
JOB NO. 25158.01  
8/18/21  
SHEET 2 OF 3

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# CLOVERLEAF DRAINAGE MAPS



## LAYER LINETYPE LEGEND

|                           | EXISTING | PROPOSED |
|---------------------------|----------|----------|
| BOUNDARY LINE             | ---      | ---      |
| PROPERTY LINE             | ---      | ---      |
| EASEMENT LINE             | ---      | ---      |
| RIGHT OF WAY              | ---      | ---      |
| CENTERLINE                | ---      | ---      |
| STORM SEWER               | ---      | ---      |
| SWALE/WATERWAY FLOWLINE   | ---      | ---      |
| INDEX CONTOUR             | ---      | ---      |
| INTERMEDIATE CONTOUR      | ---      | ---      |
| CURB & GUTTER             | ---      | ---      |
| SUB-BASIN DRAINAGE AREA   | ---      | ---      |
| BASIN TAG                 |          |          |
| DESIGN POINT DESIGNATION  |          |          |
| FLOW DIRECTION (PROPOSED) | →        | →        |
| FLOW DIRECTION (EXISTING) | →        | →        |

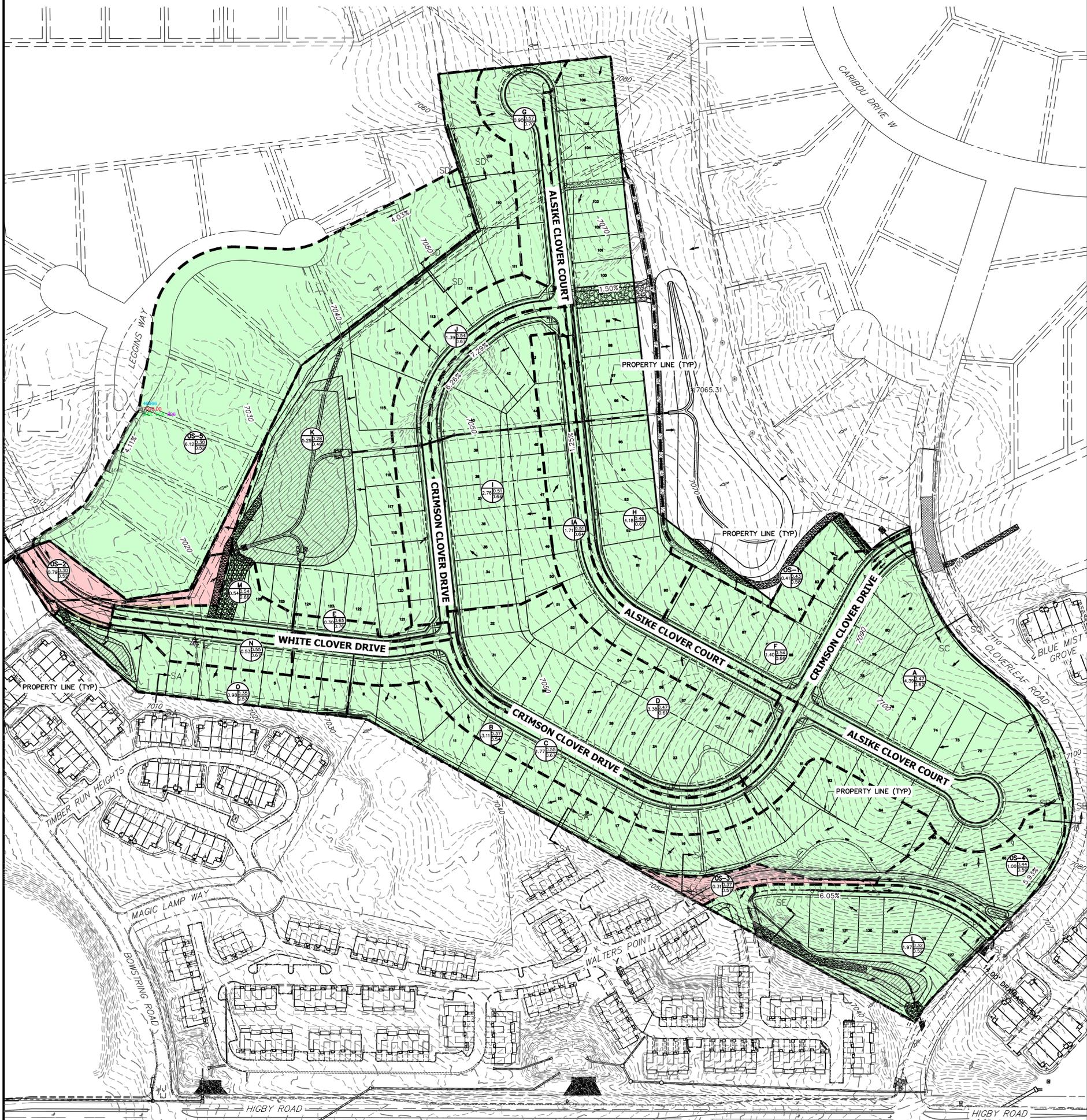
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JOB NO. 25158.01  
8/18/21  
SHEET 3 OF 3

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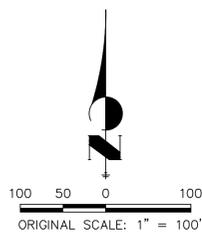
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# CLOVERLEAF SUBDIVISION PERMANENT BMP APPLICABILITY MAP



## LEGEND

- |  |  |
|--|--|
|  | BASIN DESIGNATION  |
|  | I.D.: BASIN IDENTIFIER   |
|  | A: BASIN AREA  |
|  | B: C <sub>s</sub>  |
|  | C: C <sub>100</sub>  |
|  | BASIN DELINEATION  |
|  | EXISTING INDEX CONTOURS  |
|  | EXISTING INTERMEDIATE CONTOURS   |
|  | PROPOSED INDEX CONTOURS  |
|  | PROPOSED INTERMEDIATE CONTOURS   |
|  | EXISTING FLOW DIRECTION  |
|  | PROPOSED FLOW DIRECTION  |
|  | AREA DETAINED IN PBMP  |
|  | AREA NOT DETAINED IN PBMP<br>(20% UP TO 1 AC. OF DEVELOPMENT<br>SITE CAN BE EXCLUDED -<br>DUE TO TOPOGRAPHY) |
|  | TOP OF DETENTION POND  |



CLOVERLEAF FILING NO. 2  
MS4 PERMIT EXCLUSION AREAS  
JOB NO. 25158.01  
05/11/2021  
SHEET 1 OF 1

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