

[See comment letter](#)

FINAL DRAINAGE REPORT
for
FALCON MARKETPLACE

El Paso County, Colorado

December 21, 2018

SF-19-001

Prepared for:

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FALCON MARKETPLACE
Falcon, Colorado

1.0 CERTIFICATION STATEMENTS

ENGINEER'S STATEMENT

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by El Paso County for drainage reports, and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omission on my part in preparing this report.

Tim D. McConnell, P.E.
Colorado P.E. License No. 33797
For and on Behalf of Drexel, Barrell & Co.

Date

DEVELOPER'S STATEMENT

I, the developer have read and will comply with all the requirements specified in this drainage report and plan.

Business Name: LG HI Falcon, LLC.

By:

Ben Hummel

Date

Title:

Owner

Address:

3953 Maple Ave, #290
Dallas, TX 75219

EL PASO COUNTY

Filed in accordance with the requirements of the El Paso County Land Development Code, Drainage Criteria Manual Volumes 1 and 2, and the Engineering Criteria Manual, as amended.

For the County Engineer
CONDITIONS:

Date

FINAL DRAINAGE REPORT
for
FALCON MARKETPLACE
Falcon, Colorado

2.0 PURPOSE

This report is prepared by Drexel, Barrel & Co in support of the Falcon Marketplace project. The purpose of this report is to identify onsite and offsite drainage patterns, storm sewer, inlet locations, and areas tributary to the site, and to safely route developed storm water runoff to adequate outfall facilities.

3.0 GENERAL SITE DESCRIPTION

Location

The site is located at the northwest corner of E. Woodmen Road and Meridian Road - the SE 1/4 of the SE 1/4 of Section 1, Township 13 S, Range 65 W of the 6th P.M., El Paso County, Colorado.

There is one existing home on the site, and several out buildings. The site is bounded on the north by Falcon Ranchettes single family residential, the west by Courtyards at Woodmen Hills West single family residential, the east by Meridian Road, and on the south by E. Woodmen Road.

There are no existing irrigation facilities on the project site.

Existing Site Conditions

The site is approximately 35.7 acres in size and is proposed as commercial use, with one large anchor lot and several smaller outlying lots. The majority of the site is currently undeveloped and is covered with native grass and vegetation. It is gently sloping from the north to south. Offsite flows concentrate into the Unnamed Tributary to Black Squirrel Creek (UTBSC) through the center of the site, and on to a double set of triple 48" diameter culverts under E. Woodmen Road.

Proposed Site Conditions

Falcon Marketplace is a proposed commercial development, consisting of a main anchor, junior anchor and several outlying lots. Falcon Market Place bisects the project, providing access from E. Woodmen Road, Woodmen Frontage Road and Eastonville Road to the north east.

Soils

According to the Soil Survey of El Paso County Area, Colorado, prepared by the U.S. Department of Agriculture Soil Conservation Service, the site is partially underlain by the Blakeland loamy sand (Soil No. 8), and predominantly by the Blakeland-Fluvaquentic Haplaquolis (Soil No. 9), and the Columbine gravelly sandy loam (Soil No. 19). All soils are type 'A' hydrologic soil group. See appendix for map.

Climate

This area of El Paso County can be described as the foothills, with total precipitation amounts typical of a semi-arid region. Winters are generally cold and dry, and summers relatively warm and dry. Precipitation ranges from 12 to 14 inches per year, with the majority of this moisture occurring in the spring and summer in the form of rainfall. Thunderstorms are common during the summer months.

Floodplain Statement

The effective floodplain, Zone A limits, for the Unnamed Tributary to Black Squirrel Creek (UTBSC), in the vicinity of the Falcon Marketplace project, are defined on the FIRM for El Paso County, Colorado and Unincorporated Areas, Map Number 8041CO575F, Effective Date March 17, 1997.

The effective floodplain, Zone A limits, for the UTBSC, in the vicinity of the Falcon Marketplace development, were modified by a LOMR, Case No. 12-08-0579P, Woodmen Road Widening Project – Powers Boulevard to US-24, Effective Date February 28, 2013.

FEMA issued Preliminary FIS and FIRM documents for El Paso County, Colorado and Incorporated Areas dated July 29, 2015. The preliminary FIRM, Map Number 08041CO553G, incorporates the LOMR revised Zone A floodplain identified above. See appendix for supporting information.

A CLOMR to modify the effective floodplain was approved by FEMA, Case No. 17-08-0074R (May 26, 2017).

Previous Drainage Studies

The site is located within the Middle Tributary Basin of the Falcon Drainage Basin, as studied in the Falcon Drainage Basin Planning Study, prepared by Matrix Design Group, September, 2015. DBPS recommendations are presented later in this report.

Update to Dec
2018

4.0 DBPS ANALYSIS

Existing Conditions

The Falcon DBPS completed hydrologic analysis for the Falcon Basin Watershed, using HEC-HMS v.3.5 software, for historical, existing and future land use conditions by applying a 24-hour storm event with 2-, 5-, 10-, 25-, 50-, and 100-year recurrence intervals and current drainage conveyance infrastructure.

As mentioned earlier, offsite flows from two unnamed tributaries to Black Squirrel Creek (West Branch and East Branch) converge and combine with onsite flows from the Falcon Marketplace site, and travel on to a double set of triple 48" diameter culverts under E. Woodmen Road.

The following table details the HEC-HMS analysis of existing conditions across the Falcon Marketplace development.

Peak Discharges for the Existing Condition at Points of Interest in vicinity of Falcon Marketplace Development (DBPS)

Location	Existing Conditions (source: Falcon Basin, Drainage Planning Study, HEC-HMS model)								
	HEC-HMS Element	Area (sq mi)	Basin/ Design Point	Peak Flow (cfs)					
				2-yr	5-yr	10-yr	25-yr	50-yr	100-yr
West Branch at North Property Line of Falcon Marketplace	RMT062	0.29	1	1	11	25	62	110	160
East Branch at North Property Line of Falcon Marketplace	RMT064	0.67	2	50	140	230	390	490	580
Local Basin	MT060	0.19	MT060	8	21	33	62	80	99
Convergence of West and East Branch at Falcon Marketplace	JMT060	1.16	3	54	160	250	450	560	670
Local Basin	MT070	0.2	MT070	10	23	34	61	77	93
E. Woodmen Road, South Property Line of Falcon Marketplace	JMT070	1.36	4	61	180	280	510	630	760

The DBPS flow rates shown in the table above were used as the basis of the existing condition analysis of the Falcon Marketplace development. Site specific basins have been allocated, and referenced on the existing conditions map in the appendix.

Future Conditions

The DBPS also studied the future condition, with the existing drainage infrastructure currently in place. To accommodate the future condition, the DBPS recommends drainage infrastructure improvements, including Sub-Regional Pond SR4 which was identified to be installed on the Falcon Marketplace property. Pond SR4 will be renamed Pond #1 for the purposes of this report, and was conceptually sized with the parameters shown below:

Falcon DBPS, Pond #1 (SR4) – Sizing Parameters

Parameter	Value
100-year storage volume	19 ac-ft
Q _{2in}	130 cfs
Q _{2out}	27 cfs
Q _{100in}	1,000 cfs
Q _{100out}	730 cfs

The DBPS model was updated to reflect the proposed site design and Pond #1's stage/storage/discharge characteristics were updated using Urban Drainage UD-Detention software. This analysis was then input into the HEC-HMS hydrologic model.

Peak Discharges for the Future Developed Conditions at Points of Interest in vicinity of Falcon Marketplace Development (DBPS)

Location	Future Conditions, with existing drainage infrastructure and Pond SR4 (Pond #1) (source: Falcon Basin, DBPS, HEC-HMS model)								
	HEC-HMS Element	Area (sq mi)	Basin/ Design Point	Peak Flow (cfs)					
				2-yr	5-yr	10-yr	25-yr	50-yr	100-yr
West Branch at North Property Line of Falcon Marketplace	RMT062	0.29	1	5	21	34	64	81	99
East Branch at North Property Line of Falcon Marketplace	RMT064	0.67	2	121	273	373	591	712	847
Local Basin	MT060	0.19	MT060	30	59	83	137	167	199
Sub Regional Pond SR4 (Pond #1) Inflow		1.16		133	310	431	697	847	1016
Sub Regional Pond SR4 (Pond #1) Outflow	JMT060	1.16	3	27	142	246	467	595	727
Local Basin	MT070	0.2	MT070	25	50	69	114	139	165
E. Woodmen Road, South Property Line of Falcon Marketplace	JMT070	1.36	4	31	162	281	535	685	844

As shown in the above table, the 100-year discharge to E. Woodmen Road at the south property line, with pond #1 is 844-cfs. To be in conformance with the DBPS recommendations, the allowable 100-year discharge from the Falcon Marketplace development can be no greater than 844-cfs.

Proposed Development & CLOMR Study

On October 17, 2016 a CLOMR, prepared by Drexel, Barrell & Co., was submitted to FEMA. The CLOMR specifically details how the Falcon Marketplace development proposes filling the site and rerouting the UTBSC. This will be accomplished by intercepting the existing creek at the north property line and conveying it via a rundown into a sub-regional detention pond (SR4 - Pond #1), as recommended by the DBPS.

Pond #1 Inflow/Outflow/Stage/Storage Parameters

Recurrence Interval	Pond Inflow (cfs)	Pond Outflow (cfs)	Water Surface Elevation (ft)	Storage Volume (ac-ft)
100-year	1,016	644	6897.0	26.6
50-year	847	481	6896.4	24.5
25-year	697	338	6895.8	22.5
10-year	431	106	6894.6	18.3
5-year	310	52	6894.2	17.0
2-year	133	12	6891.8	10.0

Peak discharges resulting from proposed Pond #1 are summarized above.

Pond #1 will discharge to a new 96" RCP storm drainage system which will flow from south to east across the property and discharge to a section of grass-lined channel that parallels the south perimeter of the property.

Onsite runoff generated from the site, represented as a portion of MT070 in the HEC-HMS model, will be conveyed via curb and gutter, and storm sewer to proposed water quality basins at the south end of the site. The water quality basins will discharge into the open grass-lined channel along the south perimeter of the site.

Specific developed runoff quantities for the site were determined using the Rational Method and are discussed further in section 5.0 of this report.

The open grass-lined channel will then discharge into two sets of existing triple 48" culverts under E. Woodmen Road. Detention pond #1, 96" pipe and open channel are all designed to convey the full 100-year discharge.

No changes to the existing culverts under E. Woodmen Road are proposed. HY-8 software was used to quantify a 765-cfs total capacity of the existing culverts with the culvert headwater at the elevation of the north edge of the roadway pavement.

Specific developed runoff quantities for the site were determined using the Rational Method and are discussed further in section 5.0 of this report.

Peak Discharges at Points of Interest of Falcon Marketplace

Location	Future Conditions, with existing drainage infrastructure + Falcon Marketplace Development (Source: Falcon Marketplace, HEC-HMS model)							
	HEC-HMS Element	Area (sq mi)	Peak Flow (cfs)					
			2-yr	5-yr	10-yr	25-yr	50-yr	100-yr
West branch at North Property Line of Falcon Marketplace	RMT062	0.29	5	21	34	64	81	99
East branch at North Property Line of Falcon Marketplace	RMT064	0.67	121	273	373	591	712	847
Local Basin	MT060	0.19	30	59	83	137	167	199
Sub Regional Pond SR4 Inflow	-	1.16	133	310	431	697	847	1016
Sub Regional Pond SR4 Outflow	JMT060	1.16	12	52	106	338	481	644
Local Basin	MT070	0.20	30	57	79	129	157	186
E. Woodmen Road, South Property Line of Falcon Marketplace	JMT070	1.36	32	62	119	398	562	757

Per the above table, the 100-year discharge at the south property line is 757-cfs, which is less than the capacity of the existing culverts (765-cfs), and also less than the maximum allowable 100-year discharge (844-cfs) identified by the DBPS.

5.0 EXISTING CONDITION HYDROLOGY SUMMARY

In addition to the DBPS, a site specific analysis of the existing conditions was completed. The flows determined by the DBPS for the creek tributary entering the site from the north, were used in combination with rational method analysis for the surrounding onsite/offsite flows.

O1 represents 20.7 acres of 5-acre lots to the north of the Courtyards at Woodmen Hills West, northwest of the Falcon Marketplace site. A swale along the northern boundary of the Courtyards at Woodmen Hills West development is proposed to capture runoff from the north. Runoff rates of $Q_5=6.6$ cfs and $Q_{100}=19.4$ cfs discharge on to the northwest corner of the Falcon Marketplace site. This flow is to be routed into the proposed pond SR4.

O1A represents the easterly boundary of the Courtyards at Woodmen Hills West and is currently graded to discharge to the east, onto the Falcon Marketplace site as overland flow.

Basin O2 covers the westerly lanes of Meridian Road that discharge into a roadside swale and travel southerly towards a curb cut. The curb cut discharges into the SE corner of the Falcon Marketplace site.

Existing storm sewer infrastructure in the median of Meridian Road was identified as part of this project. Currently, flows generated in the Meridian Road median travel in open landscaped swales, and culverts under roadway intersections, from Woodmen Hills Road to approximately 500 ft north of E. Woodmen Road. The flow approaching E. Woodmen Road is intercepted by a Type D inlet and piped to the south.

Basin O3 generates flows along E. Woodmen Road adjacent to the Falcon Marketplace project site, and from a high point approximately 500 ft to the west, traveling easterly via roadside ditch towards the existing triple 48" culverts.

Existing Design Point 1 combines the flows, to result in $Q_5=196.7$ cfs and $Q_{100}=780.4$ cfs culminating at the existing triple 48" culverts under E. Woodmen Road. This value is comparable to the DBPS determined $Q_{100}=757$ cfs determined for the same location.

The two sets of existing triple 48" RCP culverts discharge to the south across E. Woodmen Road, into an existing storm sewer system. A Type D grate inlet in the median of E. Woodmen Road intercepts median flows and also discharges to the south.

6.0 PROPOSED HYDROLOGY (RATIONAL METHOD) & HYDRAULIC SUMMARY

For the purposes of site specific analysis, the project site has been divided into several grouped drainage basins as shown on the proposed drainage plan. Five Design Points have been analyzed for sizing of the drainage facilities.

The Rational Method was used to determine runoff quantities for the 5- and 100-year storm recurrence intervals. Urban Drainage UD-Detention, UD-Inlet and UD-Sewer were also used to identify pond and storm system sizing (see appendix for calculations), and below for a summary runoff table.

Rational Method Runoff Summary

BASIN	DP	Area (Ac.)	Q ₅ (CFS)	Q ₁₀₀ (CFS)
A1		0.69	0.2	1.3
A2		1.50	4.8	9.5
	DP1	2.19	3.5	7.7
A3		4.82	1.4	10.2
	DP2	7.01	4.6	16.5
A4	DP3	1.52	5.6	10.1
B1		0.54	2.1	3.9
B2		1.18	4.9	8.9
B3		1.17	4.7	8.6
	DP4	2.89	11.4	20.9
B4	DP5	3.32	10.7	19.5
B5		0.32	1.3	2.4
	DP6	6.53	20.6	37.6
B6		0.31	1.3	2.3
B7		0.72	2.8	5.1
	DP7	1.03	4.0	7.4
B8		0.17	0.7	1.3
	DP8	7.73	24.0	43.8
B9	DP9	2.25	9.2	16.7
B10		0.18	0.7	1.4
	DP10	10.16	31.0	56.5
B11		0.20	0.8	1.5
	DP11	10.36	31.5	57.4
B12	DP12	1.76	6.3	11.5
B13		0.21	0.9	1.6
	DP13	1.97	7.0	12.8

BASIN	DP	Area (Ac.)	Q ₅ (CFS)	Q ₁₀₀ (CFS)
B14	DP14	4.34	15.7	28.6
B15		0.16	0.7	1.2
	DP15	6.47	22.6	41.2
B16		0.34	1.4	2.6
	DP16	6.81	23.6	43.2
	DP16a	17.17	52.0	94.8
B17	DP17	2.16	8.9	16.2
B18	DP18	2.90	11.4	20.8
	DP19	22.23	66.7	121.7
B19	DP20	2.02	5.5	11.3
B20		1.65	0.5	3.9
C1		0.11	0.0	0.2
C2		0.29	1.1	2.0
	DP21	0.40	0.9	1.8
C3		1.88	0.5	3.8
C4		2.43	10.0	18.3
	DP22	4.31	7.2	16.0
C5	DP23	0.64	0.5	1.9
C6		0.45	0.2	1.2
C7	DP24	0.16	0.6	1.2
C8		1.08	2.5	5.3
	DP25	1.24	3.1	6.3
C9	DP26	0.19	0.8	1.5
C10		3.43	7.3	16.2
	DPO1	32.50	10.3	30.2

A-group basins represent flows at the northern portion of the site that will be intercepted by Pond #1, and the 96" outfall. Flows generated from offsite basins have already been established by the aforementioned CLOMR study.

DP 1 (Q₅ =3.5 cfs, Q₁₀₀ =7.7 cfs) is located at a low point just west of the Meridian Road and Eastonville Road intersection. A 10' Type R Inlet IA1 is sited at the low point and sized to intercept flows from Basin A1 and A2. A Type C Area Inlet IA3 is designed to intercept runoff generated by the depressed roundabout circle, the intention is to utilize the circle

How does this drain backwards? Is this lot owner to provide their own WQCV?

for snow stockpiling during winter storms. Flows will then travel by 24" storm sewer on to pond SR4 to the west and DP 2 ($Q_5 = 4.6$ cfs, $Q_{100} = 16.5$ cfs).

DP 3 represents flows from basin A4 ($Q_5 = 5.6$ cfs, $Q_{100} = 10.1$ cfs), that are intended to enter the 96" storm pipe through 24" stub from manhole MA1. Design of the internal storm sewer at this location will be determined by the individual lot developer at a later date.

DP O1 covers the 10' swale along the Courtyards at Woodmen Hills West northern boundary that discharges offsite flows ($Q_5 = 10.3$ cfs and $Q_{100} = 30.2$ cfs) onto the Falcon Marketplace site. These flows will be directed into Pond SR4 via 24" RCP slope drain.

B-group basins represent the bulk of the site, with flows generally travelling southwards via curb and gutter, and storm sewer towards Pond #2. Pond #2 has been designed as a 2.7 ac-ft basin, sufficient to detain and release the WQCV generated by the site.

DP4 ($Q_5 = 10.9$ cfs, $Q_{100} = 19.8$ cfs) is located at the confluence of basins B1-B3. An at-grade 10' Type R Inlet IB1 is located north of the intersection of Falcon Market Place and the RI/RO access road to capture flows from the roadway basin B1. Design of the internal storm sewer/drainage configuration for Lots 3 and 4 will be determined by the individual lot developer at a later date. Piped flows travel to the west via 18" storm sewer.

DP5 ($Q_5 = 10.7$ cfs, $Q_{100} = 19.5$ cfs) represents flow from basin B4, that are intended to enter the 18" storm pipe the runs along Falcon Market Place. Design of the internal storm sewer for Lot 2 will be determined by the individual lot developer at a later date. Piped flows travel to the south via 18" storm sewer.

DP6 ($Q_5 = 20.6$ cfs, $Q_{100} = 37.6$ cfs) is located at a proposed at-grade 10' Type R inlet IB2, west of the intersection of Falcon Market Place and the RI/RO access road. The inlet is designed to capture flows from Basin B5. Flows travel from north to south through proposed 24" storm pipe.

DP7 ($Q_5 = 4.0$ cfs, $Q_{100} = 7.4$ cfs) is located north of the curve in Falcon Marketplace. An at-grade 10' Type R Inlet IB3 captures flows from the roadway basin B6. Design of the internal storm sewer/drainage configuration for Lot 5, will be determined by the individual lot developer at a later date. Piped flows travel to the west via 18" storm sewer.

DP8 ($Q_5 = 24.0$ cfs, $Q_{100} = 43.8$ cfs) is located at a proposed at-grade 10' Type R inlet IB4, just north of the curve in Falcon Market Place. The inlet is designed to capture flows from Basin B8. Flows travel from north to south through proposed 36" storm pipe.

DP9 ($Q_5 = 9.2$ cfs, $Q_{100} = 16.7$ cfs) is located at a stub to the north (basin B9) for Lot 2 drainage system to connect to the site system. Configuration of the internal lot system will be by the individual lot owner at a later date. Flows travel to the south via 24" storm pipe.

DP10 ($Q_5 = 31.0$ cfs, $Q_{100} = 56.5$ cfs) is located at the north side of the low-point on Falcon Market Place. A 10' Type R sump inlet IB5 collects flow from basin B10 and any flow bypass from upstream inlets. Flows travel to the south via 36" storm pipe.

DP11 ($Q_5 = 31.5$ cfs, $Q_{100} = 57.4$ cfs) is located at the south side of the low-point on Falcon

Will there be an easement through Lot 6?

Market Place. A 10' Type R sump inlet IB6 collects flow from basin B11 and any flow bypass from upstream inlets. Flows travel to the southwest via 42" storm pipe.

DP12 ($Q_5 = 9.2$ cfs, $Q_{100} = 16.7$ cfs) is located at a stub to the north (basin B12) for Lot 2 drainage system to connect to the site system. Configuration of the internal lot system will be by the individual lot owner at a later date. Flows travel to the south via 24" storm pipe.

DP13 ($Q_5 = 7.0$ cfs, $Q_{100} = 12.8$ cfs) is located to the south of DP12. An at-grade 10' Type R inlet IB7 captures flows from Basin B13. Flows travel to the east via 18" storm pipe.

DP14 ($Q_5 = 15.7$ cfs, $Q_{100} = 28.6$ cfs) is located at a stub to the north (basin B14) for Lot 2 drainage system to connect to the site system. Configuration of the internal lot system will be by the individual lot owner at a later date. Flows travel to the south via 24" storm pipe.

DP15 ($Q_5 = 22.6$ cfs, $Q_{100} = 41.2$ cfs) is located at the north side of the low-point on Falcon Market Place. A 10' Type R sump inlet IB8 collects flow from basin B15 and any flow bypass from upstream inlets. Flows travel to the south via 30" storm pipe.

DP16 ($Q_5 = 23.6$ cfs, $Q_{100} = 43.2$ cfs) is located at the south side of the low-point on Falcon Market Place. A 10' Type R sump inlet IB9 collects flow from basin B16. Flows travel to the southeast via 30" storm pipe.

Dp16a ($Q_5 = 52.0$ cfs, $Q_{100} = 94.8$ cfs) is located at the proposed box base manhole MB1. Flows from DP11 and DP16 combine at this point and travel to the south via 42" storm pipe.

DP17 ($Q_5 = 8.9$ cfs, $Q_{100} = 16.2$ cfs) is located at a stub to the west to accommodate basin B17, for ot drainage system to connect to the site system. Configuration of the internal lot system will be by the individual lot owner at a later date. Flows travel to the east via 24" storm pipe.

DP18 ($Q_5 = 11.4$ cfs, $Q_{100} = 20.8$ cfs) is located at a stub to the east to accommodate basin B18, for ot drainage system to connect to the site system. Configuration of the internal lot system will be by the individual lot owner at a later date. Flows travel to the west via 24" storm pipe.

DP19 ($Q_5 = 66.7$ cfs, $Q_{100} = 121.7$ cfs) is located at the proposed box base manhole MB2. Flows from DP16a, DP17 and DP18 combine at this point and travel to the south via 42" storm pipe into Water Quality pond #2.

DP20 covers flows generated by Meridian Road, basin B19 ($Q_5 = 5.5$ cfs, $Q_{100} = 11.3$ cfs). Flows will be intercepted via a relocated curb cut, and directed to Pond #2 via riprap swale/rundown.

C-group basins cover the western and southern portions of the site, along with flows off E. Woodmen Road that will discharge into the open channel.

DP 21 ($Q_5 = 0.9$ cfs, $Q_{100} = 1.8$ cfs) is located at the low point on the west side of the SW roundabout. A type C inlet is located in the depressed roundabout island. A 5' Type R

sump inlet will capture flows from Basin C2 and direct them to the west via 18" storm pipe.

DP22 ($Q_5 = 7.2$ cfs, $Q_{100} = 16.0$ cfs) is located at a proposed low point on the exit roadway from Lot 11. This inlet is design to capture flows from Basin C3 and C4 which will then discharge to the south via 24" storm pipe into Water Quality pond #3.

DP23 ($Q_5 = 0.5$ cfs, $Q_{100} = 1.9$ cfs) is located at a proposed culvert that ultimately discharges into Pond #3.

Water Quality Pond #3 has been designed as a 0.17 ac-ft basin, sufficient to detain and release the WQCV generated by the C-group portion of the site. Discharge from the pond travels to the east via 18" storm pipe, and ultimately into the 96" storm pipe.

DP24 covers flows ($Q_5 = 0.6$ cfs, $Q_{100} = 1.2$ cfs) is located at a low point on the south side of the SW roundabout. Flows exit the roadway via curb cut and travel to the south via a riprap swale.

DP25 ($Q_5 = 3.1$ cfs, $Q_{100} = 6.3$ cfs) is located at a proposed culvert under the access road off E. Woodmen Road. Flows travel by swale and are directed to the northeast by 12" culvert in to the open channel adjacent to E. Woodmen Road.

DP26 ($Q_5 = 0.8$ cfs, $Q_{100} = 1.5$ cfs) is located at a proposed low point on the east side of the SW roundabout. Flows will be intercepted by curb cut and directed to the east via riprap swale directly into Pond #2.

The HEC-HMS study determined that allowable flow generated by the site (B & C-group basins) cannot exceed $Q_{100} = 113$ -cfs. This represents the difference between the open channel flow and discharge from the 96" pipe (757 cfs – 644 cfs = 113 cfs).

Outflow from the 96" storm pipe, and discharge from Ponds 2 & 3 are combined with DP25 and basin C10, to generate flows of 730 cfs. This flow is within the HEC-HMS design parameter of 757 cfs and as such will not negatively impact the downstream facilities.

HY-8 software was used to analyze the hydraulic performance of the existing culverts. The table below lists the discharge/headwater relationship for the two sets of culverts, and identifies the assumed maximum allowable discharge through each of the two sets of culverts assuming the maximum allowable headwater elevation is equal to the elevation of the edge of roadway asphalt along the north side of E. Woodmen Road.

E. Woodmen Road Culverts, Headwater/Discharge Data

West Set of 3-48" RCP Culverts		East Set of 3-48" RCP Culverts	
Headwater Elevation (ft)	Total Discharge (cfs)	Headwater Elevation (ft)	Total Discharge (cfs)
6871.20	0	6867.80	0
6873.04	50	6869.44	50
6873.88	100	6870.26	100
6874.60	150	6870.95	150
6875.27	200	6871.58	200
6875.96	250	6872.41	250
6876.84	300	6873.01	300
6877.87	350	6873.88	350
6877.99	355	6875.00	400
6878.0*	355.5*	6875.12	405
6878.59	450	6875.2*	408.4*
6878.80	500	6875.78	500

* maximum allowable discharge through each of the two sets of culverts assuming the maximum allowable headwater elevation is equal to the elevation of the edge of roadway asphalt along the north side of E. Woodmen Road.

The proposed grass-lined channel, which parallels the south property line, contains a check dam, located immediately downstream (east) of the westerly set of 3-48" culverts under E. Woodmen Road. The check dam will help to more evenly divide flows between the westerly and easterly sets of 3-48" culverts. The check dam will be constructed of earthen material armored with riprap. The check dam was modeled as an obstruction at CLOMR XS535 with a crest elevation of 6875.9 which was chosen to maximize flow to the westerly set of culverts without exceeding the allowable headwater elevation. The HEC-RAS model results indicate that of the total 100-year discharge = 757 cfs, in the main channel, 351 cfs is diverted to the westerly set of culverts and 406 cfs remain in the main channel. See appendix for supporting information.

In addition to the onsite storm sewer system, a proposed 24" RCP line is to be installed between the existing grate inlet at the Meridian Road/Eastonville Road intersection and the existing grate inlet approximately 600 ft to the south. Median grading in Meridian Road necessitates replacing the existing landscaped median flow with pipe in this location. The southerly inlet will be replaced with a storm sewer manhole.

Private maintenance agreements will be established for the private storm system, prior to Final Plat recording.

for turn lane?

Address Eastonville Road, Meridian Road, Woodmen Frontage Road at southwest corner

7.0 PROPOSED DETENTION/WATER QUALITY FACILITIES

As previously mentioned, three separate detention/water quality facilities are proposed with this development:

Pond #1 (DBPS – SR4), a 26.7 ac-ft sub-regional detention facility is proposed along the northern boundary of the project site, to intercept flows from the UTBSC, and release it at a reduced flow rate into the 96" pipe. In accordance with El Paso County criteria, a 12'x8' modified type D outlet structure with a permanent micropool will release the WQCV over a 40-hour period. A gravel maintenance access road will be constructed in to, and around the entire perimeter of the pond. Pond #1 will be owned and maintained by El Paso County.

Pond #2, a 2.7 ac-ft water-quality basin will intercept the flows generated by the site, south of the proposed sub-regional pond #1. As with pond #1, in accordance with El Paso County criteria, an outlet structure with permanent micropool will release the WQCV over a 40-hour period, to the open channel along E. Woodmen Road. A gravel maintenance access road will be constructed in to, and around the southern perimeter of the pond.

Pond #3, is a small 0.17 ac-ft water-quality basin intended to intercept the flows generated by the western portion of the site. As with pond #1, in accordance with El Paso County criteria, an outlet structure with permanent micropool will release the WQCV over a 40-hour period. Flows will discharge into the 96" RCP, and ultimately reach the open channel along E. Woodmen Road.

MA1 PBMP?

Private maintenance agreements and O&M manuals will be established for Ponds 2 and 3, prior to Final Plat recording.

8.0 FOUR-STEP PROCESS

In conformance with the Four-Step Process, outlined in the DCM, Volume 2, the site development design is focused on reducing runoff volumes, treating the water quality capture volume, and creating stabilized drainage ways.

Proposed sub-regional pond SR4 (Pond #1), and both onsite water quality facilities (Ponds #2 & #3) will capture and slowly release the WQCV, aiding in water quality treatment.

Construction and stabilization of a natural channel along E. Woodmen Road will also take place, allowing water quality benefits, through infiltration and vegetation pollutant uptake. A proposed grade structure will also reduce channel velocities and assist in preventing bed and bank erosion.

Future individual lot owners will be required to address the four-step process, and implement further water quality features as necessary.

Grass-lined?

9.0 GEOTECHNICAL HAZARDS

In accordance with geotechnical recommendations, the project design is intended to direct runoff away from structures, and into the receiving water quality basins. This will be accomplished by a variety of means, i.e. curb and gutter and storm sewer. The individual building pads will be developed by others, and further analysis will need to be addressed in the lot-specific geotechnical reports for those lots.

After consulting with the State of Colorado Dam Safety Branch, it was determined that the design of Pond #1 (SR4) allows for the structure to be considered non-jurisdictional. Given the length of the buried outlet, the downstream toe is to be used as the datum for measuring dam height.

During construction of the embankment, settlement monitoring plates will be installed. Regular measurements will be recorded, documenting the amount of settlement in the embankment, and when it becomes negligible.

Groundwater mitigation measures for the pond, will consist of installation of a 12-inch thick impervious clay liner, to resolve the potential for vertical groundwater seepage. Liner specifications will be based on the Colorado Department of Natural Resources specifications.

10.0 EXISTING ONSITE UTILITY INFRASTRUCTURE

Along the southern site boundary, a number of existing utilities are being considered as part of the final project design. Utility providers have been consulted and communication will continue as the project design progresses.

Mountain View Electric

An existing overhead transmission line runs along Meridian Road, and continues underground along E. Woodmen Road. These lines, both overhead and underground are proposed to be relocated through the project site, following the proposed main access road.

Woodmen Hills Metropolitan District

An existing 10" sanitary sewer line runs along E. Woodmen Road, and an existing 12" sanitary sewer line runs along Meridian Road, but both are minimally impacted by the project development.

An existing 10" water main, and 6" non-potable raw water main run along the southern boundary of the site. These lines will be relocated along the project main road through the site. Existing lines will be removed when encountered during grading of the open channel.

Nustar Energy

An existing 10" high-pressure petroleum pipeline also runs along the southern boundary of the site. It is anticipated that this line will remain in place.

11.0 CONDITIONAL LETTER OF MAP REVISION (CLOMR)

As mentioned above, a Conditional Letter of Map Revision (CLOMR) was approved by FEMA (Case No. 17-08-0074R) on May 26, 2017. The CLOMR takes a large portion of the project site out of the floodplain, by constructing a sub-regional detention pond, and open channel along E. Woodmen Road.

Referenced portions of the CLOMR are included in the appendix.

12.0 DRAINAGE/BRIDGE FEES

Drainage and Bridge Fees

The project lies within the Falcon Drainage Basin, and is previously unplatted. The following fees are required:

The percent imperviousness for this subdivision is calculated as follows:

27.7 Acres Commercial	95% Impervious
8.7 Acres Open Space	0% Impervious
Weighted Average	72.3% Impervious

36.4 Acres at 72.3% Impervious = 26.3 Impervious Acres

The following calculations are based on the 2018 drainage/bridge fees for the Falcon Basin:

Drainage Fees

\$27,762 x 26.3 Impervious Ac = \$730,140.60*

Bridge Fees

\$3,814 x 26.3 Impervious Ac. = \$101,018.30*

***Pond Reimbursement**

Full reimbursement for construction of the sub-regional detention pond (Pond #1 – SR4) and outfall in accordance with DCM Section 3.3, is anticipated. Construction costs are listed below and the drainage basin fee is requested to be adjusted accordingly. Fees will be based upon the Final Plat submittal date.

13.0 CONSTRUCTION COST ESTIMATE

Item	Qty	Unit	Unit Price	Cost
<i>Public Non-Reimbursable</i>				
Type C Inlet	2	EA	\$4,500.00	\$9,000.00
5' Type R Inlet	1	EA	\$5,500.00	\$5,500.00
10' Type R Inlet	11	EA	\$6,800.00	\$74,800.00
18" RCP	1064	LF	\$25.00	\$26,600.00
24" RCP	1664	LF	\$35.00	\$58,240.00
30" RCP	153	LF	\$50.00	\$7,650.00
36" RCP	274	LF	\$75.00	\$20,550.00
42" RCP	194	LF	\$95.00	\$18,430.00
<i>Public facilities subtotal</i>				<i>\$220,770.00</i>
<i>Private</i>				
2.7 ac-ft WQCVF	1	EA	\$75,000.00	\$75,000.00
0.2 ac-ft WQCVF	1	EA	\$35,000.00	\$35,000.00
<i>Public facilities subtotal</i>				<i>\$110,000.00</i>
<i>10% Contingency</i>				<i>\$33,077.00</i>
Cost Estimate Total				\$363,847.00

Provide all drainage costs

14.0 CONCLUSIONS

The Falcon Marketplace project has been designed in accordance with El Paso County criteria. The detention pond and water quality basins have been designed to limit the release of storm runoff to historic flows. This development will not negatively impact the downstream facilities.

A portion of the site will remain in the 100-year floodplain after grading is complete. A LOMR will be submitted to FEMA after construction to revise the FIRM map and remove the majority of the site from the floodplain. Future buildings will not be constructed in the floodplain, or downstream of the Pond SR4 spillway in the potential overtopping inundation area.

15.0 REFERENCES

The sources of information used in the development of this study are listed below:

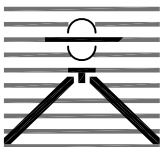
1. City of Colorado Springs/El Paso County Drainage Criteria Manual, May 2014.
2. Urban Storm Drainage Criteria Manuals, Urban Drainage and Flood Control District. June 2001, Revised April 2008.
3. Request for Conditional Letter of Map Revision, Unnamed Tributary to Black Squirrel Creek, Falcon Marketplace. Prepared by Drexel, Barrell & Co., October 17, 2016.
4. Final Drainage & Erosion Control Plan for The Courtyards at Woodmen Hills West. Prepared by JDS-Hydro, December 1, 2003.
5. Natural Resources Conservation Service (NRCS) Web Soil Survey
6. Federal Emergency Management Agency, Flood Insurance Rate Map, El Paso County, Colorado and Unincorporated Areas, Map Number 8041CO575F, Effective Date March 17, 1997.
7. EL Paso County Board Resolution No 15-042: El Paso County adoption of Chapter 6 and Section 3.2.1, Chapter 13 of the City of Colorado Springs Drainage Criteria Manual, May 2014.
8. Falcon Drainage Basin Planning Study. Prepared by Matrix Design Group, September 2015.
9. Preliminary Geotechnical Investigation. Prepared by Ground Engineering, August 25, 2015, with Addenda #1, dated March 17, 2017.
10. Colorado Department of Natural Resources – Pond Liner Specifications.
11. PSI Pond Liner Memo, June 23, 2017.

Vicinity Map



Vicinity Map

NTS



FALCON MARKETPLACE VICINITY MAP

Drexel, Barrell & Co.
Engineers • Surveyors

DATE:
8/18/16

JOB NO:
20988-00

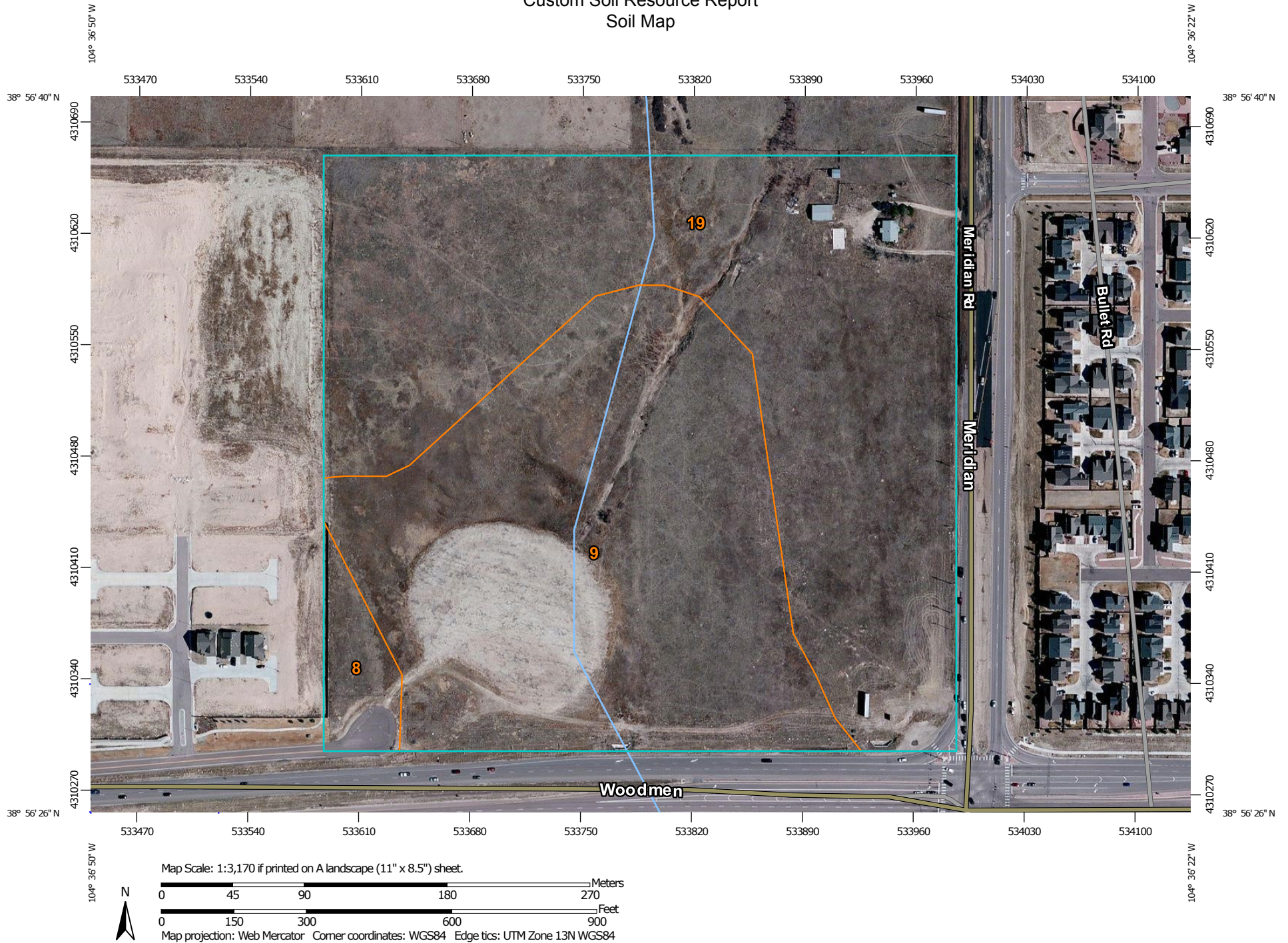
DWG. NO.

VMAP

SHEET 1 OF 1

Soils Map


Custom Soil Resource Report Soil Map



Custom Soil Resource Report

MAP LEGEND

Area of Interest (AOI)

 Area of Interest (AOI)

Soils

 Soil Map Unit Polygons

 Soil Map Unit Lines

 Soil Map Unit Points

Special Point Features

 Blowout

 Borrow Pit


 Clay Spot


 Closed Depression

 Gravel Pit

 Gravelly Spot

 Landfill

 Lava Flow

 Marsh or swamp

 Mine or Quarry

 Miscellaneous Water


 Perennial Water

 Rock Outcrop


 Saline Spot

 Sandy Spot

 Severely Eroded Spot


 Sinkhole


 Slide or Slip

 Sodic Spot

 Spoil Area

 Stony Spot


 Very Stony Spot

 Wet Spot

 Other

 Special Line Features

Water Features

 Streams and Canals


Transportation

 Rails

 Interstate Highways

 US Routes

 Major Roads

 Local Roads

Background

 Aerial Photography

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24,000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service
Web Soil Survey URL: <http://websoilsurvey.nrcs.usda.gov>
Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: El Paso County Area, Colorado
Survey Area Data: Version 13, Sep 22, 2015

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Apr 15, 2011—Sep 22, 2011

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Map Unit Legend

El Paso County Area, Colorado (CO625)			
Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
8	Blakeland loamy sand, 1 to 9 percent slopes	1.2	3.2%
9	Blakeland-Fluvaquentic Haplaquolls	16.3	43.9%
19	Columbine gravelly sandy loam, 0 to 3 percent slopes	19.6	52.9%
Totals for Area of Interest		37.1	100.0%

Map Unit Descriptions

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The delineation of such segments

on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An *association* is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

El Paso County Area, Colorado

8—Blakeland loamy sand, 1 to 9 percent slopes

Map Unit Setting

National map unit symbol: 369v

Elevation: 4,600 to 5,800 feet

Mean annual precipitation: 14 to 16 inches

Mean annual air temperature: 46 to 48 degrees F

Frost-free period: 125 to 145 days

Farmland classification: Not prime farmland

Map Unit Composition

Blakeland and similar soils: 85 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Blakeland

Setting

Landform: Flats, hills

Landform position (three-dimensional): Side slope, tal

Down-slope shape: Linear

Across-slope shape: Linear

Parent material: Alluvium derived from sedimentary rock and/or eolian deposits
derived from sedimentary rock

Typical profile

A - 0 to 11 inches: loamy sand

AC - 11 to 27 inches: loamy sand

C - 27 to 60 inches: sand

Properties and qualities

Slope: 1 to 9 percent

Depth to restrictive feature: More than 80 inches

Natural drainage class: Somewhat excessively drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): High to very high (5.95
to 19.98 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None

Frequency of ponding: None

Calcium carbonate, maximum in profile: 5 percent

Available water storage in profile: Low (about 4.5 inches)

Interpretive groups

Land capability classification (irrigated): 3e

Land capability classification (nonirrigated): 6e

Hydrologic Soil Group: A

Ecological site: Sandy Foothill (R049BY210CO)

Minor Components

Other soils

Percent of map unit:

Pleasant

Percent of map unit:

Landform: Depressions

9—Blakeland-Fluvaquentic Haplaquolls

Map Unit Setting

National map unit symbol: 36b6

Elevation: 3,500 to 5,800 feet

Mean annual precipitation: 13 to 17 inches

Mean annual air temperature: 46 to 55 degrees F

Frost-free period: 110 to 165 days

Farmland classification: Not prime farmland

Map Unit Composition

Blakeland and similar soils: 60 percent

Fluvaquentic haplaquolls and similar soils: 30 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Blakeland

Setting

Landform: Flats, hills

Landform position (three-dimensional): Side slope, tal

Down-slope shape: Linear

Across-slope shape: Linear

Parent material: Sandy alluvium derived from arkose and/or eolian deposits derived from arkose

Typical profile

A - 0 to 11 inches: loamy sand

AC - 11 to 27 inches: loamy sand

C - 27 to 60 inches: sand

Properties and qualities

Slope: 1 to 9 percent

Depth to restrictive feature: More than 80 inches

Natural drainage class: Somewhat excessively drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): High to very high (5.95 to 19.98 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None

Frequency of ponding: None

Calcium carbonate, maximum in profile: 5 percent

Available water storage in profile: Low (about 4.5 inches)

Interpretive groups

Land capability classification (irrigated): 3e

Land capability classification (nonirrigated): 6e

Custom Soil Resource Report

Hydrologic Soil Group: A

Ecological site: Sandy Foothill (R049BY210CO)

Description of Fluvaquentic Haplaquolls

Setting

Landform: Swales

Down-slope shape: Linear

Across-slope shape: Linear

Parent material: Alluvium

Typical profile

H1 - 0 to 12 inches: variable

Properties and qualities

Slope: 1 to 2 percent

Depth to restrictive feature: More than 80 inches

Natural drainage class: Poorly drained

Runoff class: Very high

*Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high
(0.20 to 6.00 in/hr)*

Depth to water table: About 0 to 24 inches

Frequency of flooding: Occasional

Frequency of ponding: None

Salinity, maximum in profile: Nonsaline to slightly saline (0.0 to 4.0 mmhos/cm)

Interpretive groups

Land capability classification (irrigated): 6w

Land capability classification (nonirrigated): 6w

Hydrologic Soil Group: D

Minor Components

Other soils

Percent of map unit:

Pleasant

Percent of map unit:

Landform: Depressions

19—Columbine gravelly sandy loam, 0 to 3 percent slopes

Map Unit Setting

National map unit symbol: 367p

Elevation: 6,500 to 7,300 feet

Mean annual precipitation: 14 to 16 inches

Mean annual air temperature: 46 to 50 degrees F

Frost-free period: 125 to 145 days

Farmland classification: Not prime farmland

Map Unit Composition

Columbine and similar soils: 85 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Columbine

Setting

Landform: Fans, flood plains, fan terraces

Down-slope shape: Linear

Across-slope shape: Linear

Parent material: Alluvium

Typical profile

A - 0 to 14 inches: gravelly sandy loam

C - 14 to 60 inches: very gravelly loamy sand

Properties and qualities

Slope: 0 to 3 percent

Depth to restrictive feature: More than 80 inches

Natural drainage class: Well drained

Runoff class: Very low

Capacity of the most limiting layer to transmit water (Ksat): High to very high (5.95 to 19.98 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None

Frequency of ponding: None

Available water storage in profile: Very low (about 2.5 inches)

Interpretive groups

Land capability classification (irrigated): 4e

Land capability classification (nonirrigated): 6e

Hydrologic Soil Group: A

Ecological site: Gravelly Foothill (R049BY214CO)

Minor Components

Fluvaquentic haplaquolls

Percent of map unit:

Landform: Swales

Other soils

Percent of map unit:

Pleasant

Percent of map unit:

Landform: Depressions

Floodplain Map

Hydrology Calculations

(Not checked on 1st review)

PROJECT INFORMATION

PROJECT: Falcon Marketplace
 PROJECT NO: 20988-00CSCV
 DESIGN BY: KGV
 REV. BY: TDM
 AGENCY: El Paso County
 REPORT TYPE: Final
 DATE: 12/21/2018



Drexel, Barrell & Co.

	C2*	C5*	C10*	C100*	% IMPERV
Commercial Development		0.81		0.88	95
Open Space		0.08		0.35	0
Asphalt Roadway		0.90		0.96	100

*C-Values and Basin Imperviousness based on Table 5-1, City of Colorado Springs and El Paso County "Drainage Criteria Manual"

SUB-BASIN	SURFACE DESIGNATION	AREA ACRE	COMPOSITE RUNOFF COEFFICIENTS				% IMPERV
			C2	C5	C10	C100	
A1	Commercial Development	0.00		0.81		0.88	95
	Open Space	0.69		0.08		0.35	0
	Asphalt Roadway	0.00		0.90		0.96	100
TOTAL A1	WEIGHTED AVERAGE	0.69		0.08		0.35	0
A2	Commercial Development	0.00		0.81		0.88	95
	Open Space	0.40		0.08		0.35	0
	Asphalt Roadway	1.10		0.90		0.96	100
TOTAL A2	WEIGHTED AVERAGE	1.50		0.68		0.80	73
A3	Commercial Development	0.00		0.81		0.88	95
	Open Space	4.82		0.08		0.35	0
	Asphalt Roadway	0.00		0.90		0.96	100
TOTAL A3	WEIGHTED AVERAGE	4.82		0.08		0.35	0
A4	Commercial Development	1.52		0.81		0.88	95
	Open Space	0.00		0.08		0.35	0
	Asphalt Roadway	0.00		0.90		0.96	100
TOTAL A4	WEIGHTED AVERAGE	1.52		0.81		0.88	95
B1	Commercial Development	0.54		0.81		0.88	95
	Open Space	0.00		0.08		0.35	0
	Asphalt Roadway	0.00		0.90		0.96	100
TOTAL B1	WEIGHTED AVERAGE	0.54		0.81		0.88	95
B2	Commercial Development	1.18		0.81		0.88	95
	Open Space	0.00		0.08		0.35	0
	Asphalt Roadway	0.00		0.90		0.96	100
TOTAL B2	WEIGHTED AVERAGE	1.18		0.81		0.88	95
B3	Commercial Development	1.17		0.81		0.88	95
	Open Space	0.00		0.08		0.35	0
	Asphalt Roadway	0.00		0.90		0.96	100
TOTAL B3	WEIGHTED AVERAGE	1.17		0.81		0.88	95
B4	Commercial Development	3.32		0.81		0.88	95
	Open Space	0.00		0.08		0.35	0
	Asphalt Roadway	0.00		0.90		0.96	100
TOTAL B4	WEIGHTED AVERAGE	3.32		0.81		0.88	95

PROJECT INFORMATION

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 AGENCY: El Paso County
 REPORT TYPE: Final
 DATE: 12/21/2018



Drexel, Barrell & Co.

	C2*	C5*	C10*	C100*	% IMPERV
Commercial Development		0.81		0.88	95
Open Space		0.08		0.35	0
Asphalt Roadway		0.90		0.96	100

*C-Values and Basin Imperviousness based on Table 5-1, City of Colorado Springs and El Paso County "Drainage Criteria Manual"

B5	Commercial Development	0.32		0.81		0.88	95
	Open Space	0.00		0.08		0.35	0
	Asphalt Roadway	0.00		0.90		0.96	100
TOTAL B5	WEIGHTED AVERAGE	0.32		0.81		0.88	95
B6	Commercial Development	0.31		0.81		0.88	95
	Open Space	0.00		0.08		0.35	0
	Asphalt Roadway	0.00		0.90		0.96	100
TOTAL B6	WEIGHTED AVERAGE	0.31		0.81		0.88	95
B7	Commercial Development	0.72		0.81		0.88	95
	Open Space	0.00		0.08		0.35	0
	Asphalt Roadway	0.00		0.90		0.96	100
TOTAL B7	WEIGHTED AVERAGE	0.72		0.81		0.88	95
B8	Commercial Development	0.17		0.81		0.88	95
	Open Space	0.00		0.08		0.35	0
	Asphalt Roadway	0.00		0.90		0.96	100
TOTAL B8	WEIGHTED AVERAGE	0.17		0.81		0.88	95
B9	Commercial Development	2.25		0.81		0.88	95
	Open Space	0.00		0.08		0.35	0
	Asphalt Roadway	0.00		0.90		0.96	100
TOTAL B9	WEIGHTED AVERAGE	2.25		0.81		0.88	95
B10	Commercial Development	0.18		0.81		0.88	95
	Open Space	0.00		0.08		0.35	0
	Asphalt Roadway	0.00		0.90		0.96	100
TOTAL B10	WEIGHTED AVERAGE	0.18		0.81		0.88	95
B11	Commercial Development	0.20		0.81		0.88	95
	Open Space	0.00		0.08		0.35	0
	Asphalt Roadway	0.00		0.90		0.96	100
TOTAL B11	WEIGHTED AVERAGE	0.20		0.81		0.88	95
B12	Commercial Development	1.76		0.81		0.88	95
	Open Space	0.00		0.08		0.35	0
	Asphalt Roadway	0.00		0.90		0.96	100
TOTAL B12	WEIGHTED AVERAGE	1.76		0.81		0.88	95
B13	Commercial Development	0.21		0.81		0.88	95
	Open Space	0.00		0.08		0.35	0
	Asphalt Roadway	0.00		0.90		0.96	100

PROJECT INFORMATION

PROJECT: Falcon Marketplace
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Drexel, Barrell & Co.

	C2*	C5*	C10*	C100*	% IMPERV
Commercial Development		0.81		0.88	95
Open Space		0.08		0.35	0
Asphalt Roadway		0.90		0.96	100

*C-Values and Basin Imperviousness based on Table 5-1, City of Colorado Springs and El Paso County "Drainage Criteria Manual"

TOTAL B13	WEIGHTED AVERAGE	0.21		0.81		0.88	95
B14	Commercial Development	4.34		0.81		0.88	95
	Open Space	0.00		0.08		0.35	0
	Asphalt Roadway	0.00		0.90		0.96	100
TOTAL B14	WEIGHTED AVERAGE	4.34		0.81		0.88	95
B15	Commercial Development	0.16		0.81		0.88	95
	Open Space	0.00		0.08		0.35	0
	Asphalt Roadway	0.00		0.90		0.96	100
TOTAL B15	WEIGHTED AVERAGE	0.16		0.81		0.88	95
B16	Commercial Development	0.34		0.81		0.88	95
	Open Space	0.00		0.08		0.35	0
	Asphalt Roadway	0.00		0.90		0.96	100
TOTAL B16	WEIGHTED AVERAGE	0.34		0.81		0.88	95
B17	Commercial Development	2.16		0.81		0.88	95
	Open Space	0.00		0.08		0.35	0
	Asphalt Roadway	0.00		0.90		0.96	100
TOTAL B17	WEIGHTED AVERAGE	2.16		0.81		0.88	95
B18	Commercial Development	2.90		0.81		0.88	95
	Open Space	0.00		0.08		0.35	0
	Asphalt Roadway	0.00		0.90		0.96	100
TOTAL B18	WEIGHTED AVERAGE	2.90		0.81		0.88	95
B19	Commercial Development	0.00		0.81		0.88	95
	Open Space	0.73		0.08		0.35	0
	Asphalt Roadway	1.29		0.90		0.96	100
TOTAL B19	WEIGHTED AVERAGE	2.02		0.60		0.74	64
B20	Commercial Development	0.00		0.81		0.88	95
	Open Space	1.65		0.08		0.35	0
	Asphalt Roadway	0.00		0.90		0.96	100
TOTAL B20	WEIGHTED AVERAGE	1.65		0.08		0.35	0
C1	Commercial Development	0.00		0.81		0.88	95
	Open Space	0.11		0.08		0.35	0
	Asphalt Roadway	0.00		0.90		0.96	100
TOTAL C1	WEIGHTED AVERAGE	0.11		0.08		0.35	0
C2	Commercial Development	0.29		0.81		0.88	95
	Open Space	0.00		0.08		0.35	0

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Drexel, Barrell & Co.

	C2*	C5*	C10*	C100*	% IMPERV
Commercial Development		0.81		0.88	95
Open Space		0.08		0.35	0
Asphalt Roadway		0.90		0.96	100

*C-Values and Basin Imperviousness based on Table 5-1, City of Colorado Springs and El Paso County "Drainage Criteria Manual"

	Asphalt Roadway	0.00		0.90		0.96	100
TOTAL C2	WEIGHTED AVERAGE	0.29		0.81		0.88	95
C3	Commercial Development	0.00		0.81		0.88	95
	Open Space	1.88		0.08		0.35	0
	Asphalt Roadway	0.00		0.90		0.96	100
TOTAL C3	WEIGHTED AVERAGE	1.88		0.08		0.35	0
C4	Commercial Development	2.43		0.81		0.88	95
	Open Space	0.00		0.08		0.35	0
	Asphalt Roadway	0.00		0.90		0.96	100
TOTAL C4	WEIGHTED AVERAGE	2.43		0.81		0.88	95
C5	Commercial Development	0.00		0.81		0.88	95
	Open Space	0.54		0.08		0.35	0
	Asphalt Roadway	0.10		0.90		0.96	100
TOTAL C5	WEIGHTED AVERAGE	0.64		0.21		0.45	16
C6	Commercial Development	0.00		0.81		0.88	95
	Open Space	0.45		0.08		0.35	0
	Asphalt Roadway	0.00		0.90		0.96	100
TOTAL C6	WEIGHTED AVERAGE	0.45		0.08		0.35	0
C7	Commercial Development	0.16		0.81		0.88	95
	Open Space	0.00		0.08		0.35	0
	Asphalt Roadway	0.00		0.90		0.96	100
TOTAL C7	WEIGHTED AVERAGE	0.16		0.81		0.88	95

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Drexel, Barrell & Co.

RATIONAL METHOD CALCULATIONS FOR STORM WATER RUNOFF

DEVELOPED TIME OF CONCENTRATION STANDARD FORM SF-2

SUB-BASIN DATA				INITIAL/OVERLAND TIME (t_i)							TIME OF CONC. t_c		FINAL t_c
BASIN	DESIGN PT:	C_5	C_{100}	AREA	LENGTH	SLOPE	t_i	LENGTH	SLOPE	VEL.	t_i	COMP.	<i>MINIMUM</i>
				Ac	Ft	%	Min	Ft	%	FPS	Min	t_c	t_c
	(1)	(2)		(3)	(4)	(5)	(6)	(7)	(8)	(9)*	(11)	(12)	(13)
A1		0.08	0.35	0.69	100	2.0	15.1	600	2.0	6.1	1.6	16.8	5.0
A2		0.68	0.80	1.50	100	2.7	5.6	355	0.6	7.1	0.8	6.5	5.0
	DP1	0.49	0.66	2.19			16.8	100	0.6	7.1	0.2	17.0	5.0
A3		0.08	0.35	4.82	100	25.0	6.5	900	0.5	2.2	6.8	13.3	5.0
	DP2	0.21	0.45	7.01			17.0	200	1.0	5.9	0.6	17.6	5.0
A4	DP3	0.81	0.88	1.52	100	0.7	6.1	300	0.7	3.6	1.4	7.5	5.0
B1		0.81	0.88	0.54	75	1.8	3.9	660	1.7	5.8	1.9	5.8	5.0
B2		0.81	0.88	1.18	100	2.5	4.0	250	2.5	6.8	0.6	4.6	5.0
B3		0.81	0.88	1.17	100	1.5	4.7	250	1.5	5.3	0.8	5.5	5.0
	DP4	0.81	0.88	2.89			5.0	250	1.5	5.3	0.8	5.8	5.0
B4	DP5	0.81	0.88	3.32	100	0.5	6.8	660	0.5	3.0	3.7	10.5	5.0
B5		0.81	0.88	0.32	40	20.0	1.3	480	1.3	5.4	1.5	2.7	5.0
	DP6	0.81	0.88	6.53			10.5	200	1.0	5.9	0.6	11.1	5.0
B6		0.81	0.88	0.31	40	2.0	2.7	380	1.1	4.9	1.3	4.0	5.0
B7		0.81	0.88	0.72	100	1.0	5.4	150	1.3	4.3	0.6	6.0	5.0
	DP7	0.81	0.88	1.03			6.0				0.0	6.0	5.0
B8		0.81	0.88	0.17	30	2.0	2.4	275	1.5	6.1	0.8	3.1	5.0

	DP8	0.81	0.88	7.73			11.1	200	1.0	7.2	0.5	11.5	5.0	11.5
B9	DP9	0.81	0.88	2.25	100	2.0	4.3	355	2.5	6.5	0.9	5.2	5.0	5.2
B10		0.81	0.88	0.18	25	2.0	2.2	325	1.2	5.8	0.9	3.1	5.0	5.0
	DP10	0.81	0.88	10.16			11.5	250	1.0	8.4	0.5	12.0	5.0	12.0
B11		0.81	0.88	0.20	25	2.0	2.2	400	1.8	5.8	1.1	3.3	5.0	5.0
	DP11	0.81	0.88	10.36			12.0	50	1.0	8.4	0.1	12.1	5.0	12.1
B12	DP12	0.81	0.88	1.76	100	1.0	5.4	675	1.0	4.3	2.6	8.0	5.0	8.0
B13		0.81	0.88	0.21	25	2.0	2.2	350	1.0	4.3	1.4	3.5	5.0	5.0
	DP13	0.81	0.88	1.97			8.0	10	1.0	8.4	0.0	8.1	5.0	8.1
B14	DP14	0.81	0.88	4.34	100	1.0	5.4	675	1.3	4.9	2.3	7.7	5.0	7.7
B15		0.81	0.88	0.16	25	2.0	2.2	300	0.7	4.3	1.2	3.3	5.0	5.0
	DP15	0.81	0.88	6.47			8.1	250	1.0	8.4	0.5	8.6	5.0	8.6
B16		0.81	0.88	0.34	25	2.0	2.2	655	0.9	4.3	2.5	4.7	5.0	5.0
	DP16	0.81	0.88	6.81			8.6	50	1.0	8.4	0.1	8.7	5.0	8.7
	DP16a	0.81	0.88	17.17			12.1	50	1.0	8.4	0.1	12.2	5.0	12.2
B17	DP17	0.81	0.88	2.16	100	5.0	3.2	280	1.1	4.5	1.0	4.2	5.0	5.0
B18	DP18	0.81	0.88	2.90	100	2.0	4.3	450	1.1	4.5	1.7	6.0	5.0	6.0
	DP19	0.81	0.88	22.23			12.1	200	1.0	9.4	0.4	12.5	5.0	12.5
B19	DP20	0.60	0.74	2.02	50	2.0	5.2	650	1.1	4.5	2.4	7.6	5.0	7.6
B20		0.08	0.35	1.65	50	25.0	4.6	1050	1.0	3.1	5.6	10.3	5.0	10.3
C1		0.08	0.35	0.11	40	1.0	12.1	0	0.0	0.0	0.0	12.1	5.0	12.1
C2		0.81	0.88	0.29	100	1.0	5.4	170	1.0	3.1	0.9	6.3	5.0	6.3
	DP21	0.61	0.73	0.40			12.1	50	1.0	5.9	0.1	12.2	5.0	12.2
C3		0.08	0.35	1.88	100	4.0	12.0	965	2.0	5.2	3.1	15.1	5.0	15.1
C4		0.81	0.88	2.43	100	25.0	1.9	765	2.0	5.6	2.3	4.1	5.0	5.0
	DP22	0.49	0.65	4.31			15.1				0.0	15.1	5.0	15.1
C5	DP23	0.21	0.45	0.64	100	5.0	9.8	295	1.0	5.9	0.8	10.6	5.0	10.6
C6		0.08	0.35	0.45	50	5.0	7.9	120	5.0	8.4	0.2	8.1	5.0	8.1
C7	DP24	0.81	0.88	0.16	100	1.0	5.4	150	1.0	5.9	0.4	5.8	5.0	5.8
C8		0.57	0.71	1.08	100	2.0	7.9	325	1.0	3.4	1.6	9.5	5.0	9.5
	DP25	0.60	0.73	1.24			9.5				0.0	9.5	5.0	9.5
C9	DP26	0.81	0.88	0.19	50	1.0	3.8	50	1.0	5.2	0.2	4.0	5.0	5.0
C10		0.50	0.66	3.43	100	2.0	8.9	50	33.0	15.6	0.1	8.9	5.0	8.9

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RATIONAL METHOD CALCULATIONS FOR STORM WATER RUNOFF

DEVELOPED	RUNOFF			5 YR	STORM				P1=		1.50	
BASIN (S)	DIRECT RUNOFF								TOTAL RUNOFF			
	DESIGN POINT	AREA	AREA (AC)	RUNOFF COEFF	t _c (MIN)	C * A	I (IN/HR)	Q (CFS)	t _c (MIN)	S (C * A)	I (IN/HR)	Q (CFS)
	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)
A1			0.69	0.08	16.8	0.06	3.23	0.2				
A2			1.50	0.68	6.5	1.02	4.73	4.8				
	DP1		2.19	0.49	17.0	1.08	3.20	3.5				
A3			4.82	0.08	13.3	0.39	3.59	1.4				
	DP2		7.01	0.21	17.6	1.46	3.15	4.6				
A4	DP3		1.52	0.81	7.5	1.23	4.51	5.6				
B1			0.54	0.81	5.8	0.44	4.89	2.1				
B2			1.18	0.81	5.0	0.96	5.09	4.9				
B3			1.17	0.81	5.5	0.95	4.95	4.7				
	DP4		2.89	0.81	5.8	2.34	4.89	11.4				
B4	DP5		3.32	0.81	10.5	2.69	3.98	10.7				
B5			0.32	0.81	5.0	0.26	5.09	1.3				
	DP6		6.53	0.81	11.1	5.29	3.90	20.6				
B6			0.31	0.81	5.0	0.25	5.09	1.3				
B7			0.72	0.81	6.0	0.58	4.84	2.8				
	DP7		1.03	0.81	6.0	0.83	4.84	4.0				
B8			0.17	0.81	5.0	0.14	5.09	0.7				

	DP8		7.73	0.81	11.5	6.26	3.83	24.0				
B9	DP9		2.25	0.81	5.2	1.82	5.03	9.2				
B10			0.18	0.81	5.0	0.15	5.09	0.7				
	DP10		10.16	0.81	12.0	8.23	3.76	31.0				
B11			0.20	0.81	5.0	0.16	5.09	0.8				
	DP11		10.36	0.81	12.1	8.39	3.75	31.5				
B12	DP12		1.76	0.81	8.0	1.43	4.40	6.3				
B13			0.21	0.81	5.0	0.17	5.09	0.9				
	DP13		1.97	0.81	8.1	1.60	4.40	7.0				
B14	DP14		4.34	0.81	7.7	3.52	4.46	15.7				
B15			0.16	0.81	5.0	0.13	5.09	0.7				
	DP15		6.47	0.81	8.6	5.24	4.30	22.6				
B16			0.34	0.81	5.0	0.28	5.09	1.4				
	DP16		6.81	0.81	8.7	5.52	4.29	23.6				
	DP16a		17.17	0.81	12.2	13.91	3.74	52.0				
B17	DP17		2.16	0.81	5.0	1.75	5.09	8.9				
B18	DP18		2.90	0.81	6.0	2.35	4.84	11.4				
	DP19		22.23	0.81	12.5	18.01	3.70	66.7				
B19	DP20		2.02	0.60	7.6	1.22	4.48	5.5				
B20			1.65	0.08	10.3	0.13	4.02	0.5				
C1			0.11	0.08	12.1	0.01	3.76	0.0				
C2			0.29	0.81	6.3	0.24	4.76	1.1				
	DP21		0.40	0.61	12.2	0.24	3.74	0.9				
C3			1.88	0.08	15.1	0.15	3.39	0.5				
C4			2.43	0.81	5.0	1.97	5.09	10.0				
	DP22		4.31	0.49	15.1	2.12	3.39	7.2				
C5	DP23		0.64	0.21	10.6	0.13	3.97	0.5				
C6			0.45	0.08	8.1	0.04	4.38	0.2				
C7	DP24		0.16	0.81	5.8	0.13	4.87	0.6				
C8			1.08	0.57	9.5	0.61	4.14	2.5				
	DP25		1.24	0.60	9.5	0.74	4.14	3.1				
C9	DP26		0.19	0.81	5.0	0.16	5.09	0.8				
C10			3.43	0.50	8.9	1.72	4.24	7.3				

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Drexel, Barrell & Co.

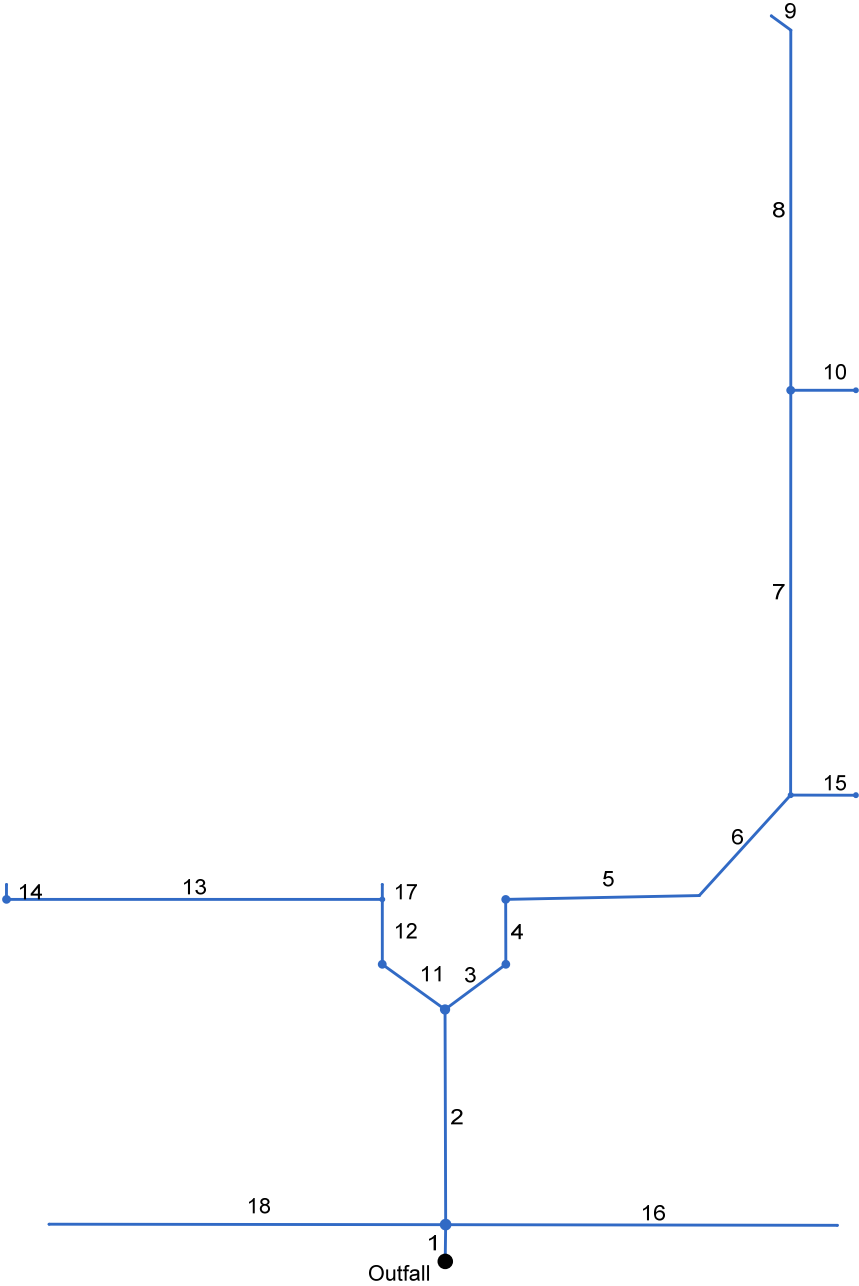
RATIONAL METHOD CALCULATIONS FOR STORM WATER RUNOFF

DEVELOPED	RUNOFF			5 YR	STORM				P1=			
BASIN (S)	DIRECT RUNOFF								TOTAL RUNOFF			
	DESIGN POINT	AREA	AREA (AC)	RUNOFF COEFF	t _c (MIN)	C * A	I (IN/HR)	Q (CFS)	t _c (MIN)	S (C * A)	I (IN/HR)	Q (CFS)
	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)
A1			0.69	0.35	16.8	0.24	5.42	1.3				
A2			1.50	0.80	6.5	1.20	7.95	9.5				
	DP1		2.19	0.66	17.0	1.44	5.38	7.7				
A3			4.82	0.35	13.3	1.69	6.04	10.2				
	DP2		7.01	0.45	17.6	3.12	5.30	16.5				
A4	DP3		1.52	0.88	7.5	1.34	7.57	10.1				
B1			0.54	0.88	5.8	0.48	8.22	3.9				
B2			1.18	0.88	5.0	1.04	8.55	8.9				
B3			1.17	0.88	5.5	1.03	8.32	8.6				
	DP4		2.89	0.88	5.8	2.54	8.21	20.9				
B4	DP5		3.32	0.88	10.5	2.92	6.69	19.5				
B5			0.32	0.88	5.0	0.28	8.55	2.4				
	DP6		6.53	0.88	11.1	5.75	6.55	37.6				
B6			0.31	0.88	5.0	0.27	8.55	2.3				
B7			0.72	0.88	6.0	0.63	8.12	5.1				
	DP7		1.03	0.88	6.0	0.91	8.12	7.4				
B8			0.17	0.88	5.0	0.15	8.55	1.3				

	DP8		7.73	0.88	11.5	6.80	6.43	43.8				
B9	DP9		2.25	0.88	5.2	1.98	8.45	16.7				
B10			0.18	0.88	5.0	0.16	8.55	1.4				
	DP10		10.16	0.88	12.0	8.94	6.32	56.5				
B11			0.20	0.88	5.0	0.18	8.55	1.5				
	DP11		10.36	0.88	12.1	9.12	6.30	57.4				
B12	DP12		1.76	0.88	8.0	1.55	7.39	11.5				
B13			0.21	0.88	5.0	0.18	8.55	1.6				
	DP13		1.97	0.88	8.1	1.73	7.39	12.8				
B14	DP14		4.34	0.88	7.7	3.82	7.50	28.6				
B15			0.16	0.88	5.0	0.14	8.55	1.2				
	DP15		6.47	0.88	8.6	5.69	7.23	41.2				
B16			0.34	0.88	5.0	0.30	8.55	2.6				
	DP16		6.81	0.88	8.7	5.99	7.20	43.2				
	DP16a		17.17	0.88	12.2	15.11	6.28	94.8				
B17	DP17		2.16	0.88	5.0	1.90	8.55	16.2				
B18	DP18		2.90	0.88	6.0	2.55	8.14	20.8				
	DP19		22.23	0.88	12.5	19.56	6.22	121.7				
B19	DP20		2.02	0.74	7.6	1.49	7.53	11.3				
B20			1.65	0.35	10.3	0.58	6.75	3.9				
C1			0.11	0.35	12.1	0.04	6.31	0.2				
C2			0.29	0.88	6.3	0.26	7.99	2.0				
	DP21		0.40	0.73	12.2	0.29	6.28	1.8				
C3			1.88	0.35	15.1	0.66	5.70	3.8				
C4			2.43	0.88	5.0	2.14	8.55	18.3				
	DP22		4.31	0.65	15.1	2.80	5.70	16.0				
C5	DP23		0.64	0.45	10.6	0.29	6.66	1.9				
C6			0.45	0.35	8.1	0.16	7.37	1.2				
C7	DP24		0.16	0.88	5.8	0.14	8.19	1.2				
C8			1.08	0.71	9.5	0.77	6.95	5.3				
	DP25		1.24	0.73	9.5	0.91	6.95	6.3				
C9	DP26		0.19	0.88	5.0	0.17	8.55	1.5				
C10			3.43	0.66	8.9	2.28	7.12	16.2				

Hydraulic Calculations

Hydraflow Storm Sewers Extension for Autodesk® AutoCAD® Civil 3D® Plan



Storm Sewer Inventory Report

Line No.	Alignment				Flow Data				Physical Data								Line ID
	Dnstr Line No.	Line Length (ft)	Defl angle (deg)	Junc Type	Known Q (cfs)	Drng Area (ac)	Runoff Coeff (C)	Inlet Time (min)	Invert El Dn (ft)	Line Slope (%)	Invert El Up (ft)	Line Size (in)	Line Shape	N Value (n)	J-Loss Coeff (K)	Inlet/ Rim El (ft)	
1	End	25.128	-89.363	MH	0.00	0.00	0.00	0.0	6874.00	0.99	6874.25	48	Cir	0.012	1.00	6882.05	PB16
2	1	146.947	-0.786	MH	0.00	0.00	0.00	0.0	6874.25	1.00	6875.72	48	Cir	0.012	0.84	6883.35	PB13
3	2	51.602	53.397	Curb	14.30	0.00	0.00	0.0	6876.22	1.01	6876.74	42	Cir	0.012	1.25	6883.20	PB7
4	3	44.332	-53.375	Curb	11.20	0.00	0.00	0.0	6877.24	0.99	6877.68	36	Cir	0.012	1.50	6883.20	PB6
5	4	131.739	88.983	None	0.00	0.00	0.00	0.0	6877.68	1.00	6879.00	36	Cir	0.012	0.77	6884.84	PB5B
6	5	92.553	-46.653	Curb	1.40	0.00	0.00	0.0	6879.00	0.99	6879.92	36	Cir	0.012	1.17	6886.62	PB5A
7	6	276.549	-42.201	Curb	2.60	0.00	0.00	0.0	6880.42	1.00	6883.19	30	Cir	0.012	1.50	6890.30	PB3
8	7	245.950	0.000	None	0.00	0.00	0.00	0.0	6883.69	1.00	6886.15	24	Cir	0.012	0.84	6893.40	PB1B
9	8	16.464	-53.625	None	17.60	0.00	0.00	0.0	6886.15	0.97	6886.31	24	Cir	0.012	1.00	6893.70	PB1A
10	7	44.336	89.981	Curb	9.30	0.00	0.00	0.0	6884.19	0.99	6884.63	18	Cir	0.012	1.00	6890.30	PB2
11	2	52.706	-53.988	Curb	9.40	0.00	0.00	0.0	6876.22	1.01	6876.75	42	Cir	0.012	1.26	6883.04	PB12
12	11	44.330	54.116	Curb	9.40	0.00	0.00	0.0	6877.25	0.99	6877.69	36	Cir	0.012	1.50	6883.04	PB11
13	12	255.617	-89.979	Curb	1.70	0.00	0.00	0.0	6878.69	1.00	6881.25	24	Cir	0.012	1.50	6885.40	PB9
14	13	10.167	89.940	None	11.20	0.00	0.00	0.0	6881.25	0.98	6881.35	24	Cir	0.012	1.00	6885.60	PB8
15	6	44.335	47.813	Curb	9.10	0.00	0.00	0.0	6881.42	0.99	6881.86	18	Cir	0.012	1.00	6886.88	PB4
16	1	266.443	89.475	None	20.70	0.00	0.00	0.0	6876.25	1.00	6878.92	24	Cir	0.012	1.00	6882.04	PB15
17	12	10.167	-0.039	None	29.60	0.00	0.00	0.0	6878.19	0.98	6878.29	30	Cir	0.012	1.00	6883.24	PB10
18	1	269.817	-90.576	None	16.20	0.00	0.00	0.0	6876.25	1.00	6878.95	24	Cir	0.012	1.00	6882.06	PB14
Project File: FM 3-7-17 HF.stm												Number of lines: 18				Date: 3/16/2017	

Structure Report

Struct No.	Structure ID	Junction Type	Rim Elev (ft)	Structure			Line Out			Line In		
				Shape	Length (ft)	Width (ft)	Size (in)	Shape	Invert (ft)	Size (in)	Shape	Invert (ft)
1	MB2	Manhole	6882.05	Cir	6.00	6.00	48	Cir	6874.25	48 24 24	Cir Cir Cir	6874.25 6876.25 6876.25
2	MB1	Manhole	6883.35	Cir	5.00	5.00	48	Cir	6875.72	42 42	Cir Cir	6876.22 6876.22
3	IB6	Curb-	6883.20	Cir	4.00	4.00	42	Cir	6876.74	36	Cir	6877.24
4	IB5	Curb-	6883.20	Cir	4.00	4.00	36	Cir	6877.68	36	Cir	6877.68
5	NB3	None	6884.84	n/a	n/a	n/a	36	Cir	6879.00	36	Cir	6879.00
6	IB4	Curb-	6886.62	Cir	2.00	2.00	36	Cir	6879.92	30 18	Cir Cir	6880.42 6881.42
7	IB2	Curb-	6890.30	Cir	4.00	4.00	30	Cir	6883.19	24 18	Cir Cir	6883.69 6884.19
8	NB2	None	6893.40	n/a	n/a	n/a	24	Cir	6886.15	24	Cir	6886.15
9	NB1	None	6893.70	n/a	n/a	n/a	24	Cir	6886.31			
10	IB1	Curb-	6890.30	Cir	2.00	2.00	18	Cir	6884.63			
11	IB9	Curb-	6883.04	Cir	4.00	4.00	42	Cir	6876.75	36	Cir	6877.25
12	IB8	Curb-	6883.04	Cir	2.00	2.00	36	Cir	6877.69	24 30	Cir Cir	6878.69 6878.19
13	IB7	Curb-	6885.40	Cir	4.00	4.00	24	Cir	6881.25	24	Cir	6881.25
14	NB4	None	6885.60	n/a	n/a	n/a	24	Cir	6881.35			
15	IB3	Curb-	6886.88	Cir	2.00	2.00	18	Cir	6881.86			
16	NB7	None	6882.04	n/a	n/a	n/a	24	Cir	6878.92			
17	NB5	None	6883.24	n/a	n/a	n/a	30	Cir	6878.29			
18	NB6	None	6882.06	n/a	n/a	n/a	24	Cir	6878.95			
Project File: FM 3-7-17 HF.stm							Number of Structures: 18			Run Date: 3/16/2017		

Storm Sewer Summary Report

Line No.	Line ID	Flow rate (cfs)	Line Size (in)	Line shape	Line length (ft)	Invert EL Dn (ft)	Invert EL Up (ft)	Line Slope (%)	HGL Down (ft)	HGL Up (ft)	Minor loss (ft)	HGL Junct (ft)	Dns Line No.	Junction Type
1	PB16	163.7	48	Cir	25.128	6874.00	6874.25	0.995	6877.69	6877.94	n/a	6877.94	End	Manhole
2	PB13	126.8	48	Cir	146.947	6874.25	6875.72	1.001	6877.94	6879.10	1.64	6879.10	1	Manhole
3	PB7	65.50	42	Cir	51.602	6876.22	6876.74	1.008	6879.10	6879.28	1.50	6879.28	2	Curb-
4	PB6	51.20	36	Cir	44.332	6877.24	6877.68	0.992	6879.28	6880.01	n/a	6880.01	3	Curb-
5	PB5B	40.00	36	Cir	131.739	6877.68	6879.00	1.002	6880.01	6881.06	n/a	6881.06 j	4	None
6	PB5A	40.00	36	Cir	92.553	6879.00	6879.92	0.994	6881.06	6881.98	n/a	6881.98	5	Curb-
7	PB3	29.50	30	Cir	276.549	6880.42	6883.19	1.002	6881.98	6885.04	1.34	6885.04	6	Curb-
8	PB1B	17.60	24	Cir	245.950	6883.69	6886.15	1.000	6885.04	6887.66	n/a	6887.66	7	None
9	PB1A	17.60	24	Cir	16.464	6886.15	6886.31	0.973	6887.66	6887.82	n/a	6887.82	8	None
10	PB2	9.30	18	Cir	44.336	6884.19	6884.63	0.992	6885.22	6885.81	n/a	6885.81	7	Curb-
11	PB12	61.30	42	Cir	52.706	6876.22	6876.75	1.005	6879.10	6879.20	n/a	6879.20	2	Curb-
12	PB11	51.90	36	Cir	44.330	6877.25	6877.69	0.992	6879.20	6880.03	n/a	6880.03	11	Curb-
13	PB9	12.90	24	Cir	255.617	6878.69	6881.25	1.002	6880.03	6882.54	n/a	6882.54 j	12	Curb-
14	PB8	11.20	24	Cir	10.167	6881.25	6881.35	0.985	6882.54	6882.55	n/a	6882.55	13	None
15	PB4	9.10	18	Cir	44.335	6881.42	6881.86	0.992	6882.44	6883.03	0.59	6883.03	6	Curb-
16	PB15	20.70	24	Cir	266.443	6876.25	6878.92	1.002	6877.94	6880.55	n/a	6880.55 j	1	None
17	PB10	29.60	30	Cir	10.167	6878.19	6878.29	0.985	6880.03	6880.14	0.89	6880.14	12	None
18	PB14	16.20	24	Cir	269.817	6876.25	6878.95	1.001	6877.94	6880.40	n/a	6880.40 j	1	None

Project File: FM 3-7-17 HF.stm

Number of lines: 18

Run Date: 3/16/2017

NOTES: Known Qs only ; j - Line contains hyd. jump.

Storm Sewer Tabulation

Label design storm on these sheets.

Station		Len	Drng Area		Rnoff coeff	Area x C		Tc		Rain (I)	Total flow	Cap full	Vel	Pipe		Invert Elev		HGL Elev		Grnd / Rim Elev		Line ID
Line	To Line		Incr	Total		Incr	Total	Inlet	Syst					Size	Slope	Dn	Up	Dn	Up	Dn	Up	
		(ft)	(ac)	(ac)	(C)			(min)	(min)	(in/hr)	(cfs)	(cfs)	(ft/s)	(in)	(%)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	
1	End	25.128	0.00	0.00	0.00	0.00	0.00	0.0	2.7	0.0	163.7	155.2	13.51	48	0.99	6874.00	6874.25	6877.69	6877.94	6878.66	6882.05	PB16
2	1	146.947	0.00	0.00	0.00	0.00	0.00	0.0	2.4	0.0	126.8	155.7	10.84	48	1.00	6874.25	6875.72	6877.94	6879.10	6882.05	6883.35	PB13
3	2	51.602	0.00	0.00	0.00	0.00	0.00	0.0	2.3	0.0	65.50	109.4	8.26	42	1.01	6876.22	6876.74	6879.10	6879.28	6883.35	6883.20	PB7
4	3	44.332	0.00	0.00	0.00	0.00	0.00	0.0	2.2	0.0	51.20	71.98	9.37	36	0.99	6877.24	6877.68	6879.28	6880.01	6883.20	6883.20	PB6
5	4	131.739	0.00	0.00	0.00	0.00	0.00	0.0	1.8	0.0	40.00	72.32	7.27	36	1.00	6877.68	6879.00	6880.01	6881.06	6883.20	6884.84	PB5B
6	5	92.553	0.00	0.00	0.00	0.00	0.00	0.0	1.5	0.0	40.00	72.03	7.74	36	0.99	6879.00	6879.92	6881.06	6881.98	6884.84	6886.62	PB5A
7	6	276.549	0.00	0.00	0.00	0.00	0.00	0.0	0.8	0.0	29.50	44.47	8.38	30	1.00	6880.42	6883.19	6881.98	6885.04	6886.62	6890.30	PB3
8	7	245.950	0.00	0.00	0.00	0.00	0.00	0.0	0.0	0.0	17.60	24.50	7.36	24	1.00	6883.69	6886.15	6885.04	6887.66	6890.30	6893.40	PB1B
9	8	16.464	0.00	0.00	0.00	0.00	0.00	0.0	0.0	0.0	17.60	24.17	6.92	24	0.97	6886.15	6886.31	6887.66	6887.82	6893.40	6893.70	PB1A
10	7	44.336	0.00	0.00	0.00	0.00	0.00	0.0	0.0	0.0	9.30	11.33	6.70	18	0.99	6884.19	6884.63	6885.22	6885.81	6890.30	6890.30	PB2
11	2	52.706	0.00	0.00	0.00	0.00	0.00	0.0	1.2	0.0	61.30	109.3	7.88	42	1.01	6876.22	6876.75	6879.10	6879.20	6883.35	6883.04	PB12
12	11	44.330	0.00	0.00	0.00	0.00	0.00	0.0	1.1	0.0	51.90	71.98	9.72	36	0.99	6877.25	6877.69	6879.20	6880.03	6883.04	6883.04	PB11
13	12	255.617	0.00	0.00	0.00	0.00	0.00	0.0	0.0	0.0	12.90	24.52	5.89	24	1.00	6878.69	6881.25	6880.03	6882.54	6883.04	6885.40	PB9
14	13	10.167	0.00	0.00	0.00	0.00	0.00	0.0	0.0	0.0	11.20	24.31	5.46	24	0.98	6881.25	6881.35	6882.54	6882.55	6885.40	6885.60	PB8
15	6	44.335	0.00	0.00	0.00	0.00	0.00	0.0	0.0	0.0	9.10	11.33	6.65	18	0.99	6881.42	6881.86	6882.44	6883.03	6886.62	6886.88	PB4
16	1	266.443	0.00	0.00	0.00	0.00	0.00	0.0	0.0	0.0	20.70	24.53	7.43	24	1.00	6876.25	6878.92	6877.94	6880.55	6882.05	6882.04	PB15
17	12	10.167	0.00	0.00	0.00	0.00	0.00	0.0	0.0	0.0	29.60	44.09	7.61	30	0.98	6878.19	6878.29	6880.03	6880.14	6883.04	6883.24	PB10
18	1	269.817	0.00	0.00	0.00	0.00	0.00	0.0	0.0	0.0	16.20	24.51	6.18	24	1.00	6876.25	6878.95	6877.94	6880.40	6882.05	6882.06	PB14
Project File: FM 3-7-17 HF.stm																Number of lines: 18				Run Date: 3/16/2017		
NOTES:Known Qs only ; c = cir e = ellip b = box																						

Inlet Report

Line No	Inlet ID	Q = CIA	Q carry	Q capt	Q Byp	Junc Type	Curb Inlet		Grate Inlet			Gutter							Inlet			Byp Line No
		(cfs)	(cfs)	(cfs)	(cfs)		Ht (in)	L (ft)	Area (sqft)	L (ft)	W (ft)	So (ft/ft)	W (ft)	Sw (ft/ft)	Sx (ft/ft)	n	Depth (ft)	Spread (ft)	Depth (ft)	Spread (ft)	Depr (in)	
1	MB2	0.00	0.00	0.00	0.00	MH	0.0	0.00	0.00	0.00	0.00	Sag	0.00	0.000	0.000	0.013	0.00	0.00	0.00	0.00	0.0	Off
2	MB1	0.00	0.00	0.00	0.00	MH	0.0	0.00	0.00	0.00	0.00	Sag	0.00	0.000	0.000	0.013	0.00	0.00	0.00	0.00	0.0	Off
3	IB6	14.30*	0.00	14.30	0.00	Curb	6.0	10.00	0.00	0.00	0.00	Sag	2.00	0.083	0.020	0.013	0.61	24.20	0.61	24.20	0.0	Off
4	IB5	11.20*	0.00	11.20	0.00	Curb	6.0	10.00	0.00	0.00	0.00	Sag	2.00	0.083	0.020	0.013	0.52	19.62	0.52	19.62	0.0	Off
5	NB3	0.00	0.00	0.00	0.00	None	0.0	0.00	0.00	0.00	0.00	0.000	0.00	0.000	0.000	0.013	0.00	0.00	0.00	0.00	0.0	Off
6	IB4	1.40*	0.00	1.40	0.00	Curb	6.0	10.00	0.00	0.00	0.00	0.010	2.00	0.083	0.020	0.013	0.25	5.95	0.01	0.12	0.0	Off
7	IB2	2.60*	0.00	2.31	0.29	Curb	6.0	10.00	0.00	0.00	0.00	0.010	2.00	0.083	0.020	0.013	0.29	8.35	0.15	1.81	0.0	Off
8	NB2	0.00	0.00	0.00	0.00	None	0.0	0.00	0.00	0.00	0.00	0.000	0.00	0.000	0.000	0.013	0.00	0.00	0.00	0.00	0.0	Off
9	NB1	17.60*	0.00	0.00	17.60	None	0.0	0.00	0.00	0.00	0.00	0.000	0.00	0.000	0.000	0.013	0.00	0.00	0.00	0.00	0.0	Off
10	IB1	9.30*	0.00	4.91	4.39	Curb	6.0	10.00	0.00	0.00	0.00	0.010	2.00	0.083	0.020	0.013	0.42	14.70	0.34	10.70	0.0	Off
11	IB9	9.40*	0.00	9.40	0.00	Curb	6.0	10.00	0.00	0.00	0.00	Sag	2.00	0.050	0.020	0.013	0.46	20.06	0.46	20.06	0.0	Off
12	IB8	9.40*	0.00	9.40	0.00	Curb	6.0	10.00	0.00	0.00	0.00	Sag	2.00	0.083	0.020	0.013	0.46	16.76	0.46	16.76	0.0	Off
13	IB7	1.70*	0.00	1.67	0.03	Curb	6.0	10.00	0.00	0.00	0.00	0.010	2.00	0.083	0.020	0.013	0.26	6.70	0.07	0.84	0.0	Off
14	NB4	11.20*	0.00	0.00	11.20	None	0.0	0.00	0.00	0.00	0.00	0.000	0.00	0.000	0.000	0.013	0.00	0.00	0.00	0.00	0.0	Off
15	IB3	9.10*	0.00	4.85	4.25	Curb	6.0	10.00	0.00	0.00	0.00	0.010	2.00	0.083	0.020	0.013	0.42	14.55	0.34	10.70	0.0	Off
16	NB7	20.70*	0.00	0.00	20.70	None	0.0	0.00	0.00	0.00	0.00	0.000	0.00	0.000	0.000	0.013	0.00	0.00	0.00	0.00	0.0	Off
17	NB5	29.60*	0.00	0.00	29.60	None	0.0	0.00	0.00	0.00	0.00	0.000	0.00	0.000	0.000	0.013	0.00	0.00	0.00	0.00	0.0	Off
18	NB6	16.20*	0.00	0.00	16.20	None	0.0	0.00	0.00	0.00	0.00	0.000	0.00	0.000	0.000	0.013	0.00	0.00	0.00	0.00	0.0	Off
Project File: FM 3-7-17 HF.stm														Number of lines: 18				Run Date: 3/16/2017				
NOTES: Inlet N-Values = 0.016; Known Qs only; * Indicates Known Q added. All curb inlets are throat.																						

FL-DOT Report

Line No	To Line	Type of struc	n - Value	Len	Drainage Area			Time of conc	Time of Flow in sect	Inten (I)	Total CA	Add Q	Inlet elev	Elev of HGL			Rise	HGL	ADD		Date: 3/16/2017
					C1 = 0.2 C2 = 0.5 C3 = 0.9							Total Flow		Elev of Crown			Span	Pipe	Full Flow		Frequency: (n/a)
												Proj: FM 3-7-17 HF.stm									
					Increment (ac)	Sub-Total (ac)	Sum CA					Q (cfs)		Up (ft)	Down (ft)	Fall (ft)	Size (in)	Slope (%)	Vel (ft/s)	Cap (cfs)	Line description
1	End	MH	0.012	25.128	0.00 0.00 0.00	0.00 0.00 0.00	0.00 0.00 0.00	2.68	0.03	0.00	0.00	0.00 163.7	6882.05	6877.94 6878.25 6874.25	6877.69 6878.00 6874.00	0.25 0.25	48 48 Cir	0.99 0.99	13.51 12.35	163.7 155.2	PB16
2	1	MH	0.012	146.947	0.00 0.00 0.00	0.00 0.00 0.00	0.00 0.00 0.00	2.44	0.24	0.00	0.00	0.00 126.8	6883.35	6879.10 6879.72 6875.72	6877.94 6878.25 6874.25	1.16 1.47	48 48 Cir	0.79 1.00	10.84 12.39	126.8 155.7	PB13
3	2	Curb	0.012	51.602	0.00 0.00 0.00	0.00 0.00 0.00	0.00 0.00 0.00	2.31	0.13	0.00	0.00	14.30 65.50	6883.20	6879.28 6880.24 6876.74	6879.10 6879.72 6876.22	0.18 0.52	42 42 Cir	0.35 1.01	8.26 11.37	65.50 109.4	PB7
4	3	Curb	0.012	44.332	0.00 0.00 0.00	0.00 0.00 0.00	0.00 0.00 0.00	2.21	0.10	0.00	0.00	11.20 51.20	6883.20	6880.01 6880.68 6877.68	6879.28 6880.24 6877.24	0.73 0.44	36 36 Cir	1.65 0.99	9.37 10.18	51.20 71.98	PB6
5	4	None	0.012	131.739	0.00 0.00 0.00	0.00 0.00 0.00	0.00 0.00 0.00	1.82	0.39	0.00	0.00	0.00 40.00	6884.84	6881.06 6882.00 6879.00	6880.01 6880.68 6877.68	1.05 1.32	36 36 Cir	0.80 1.00	7.27 10.23	40.00 72.32	PB5B
6	5	Curb	0.012	92.553	0.00 0.00 0.00	0.00 0.00 0.00	0.00 0.00 0.00	1.55	0.27	0.00	0.00	1.40 40.00	6886.62	6881.98 6882.92 6879.92	6881.06 6882.00 6879.00	0.92 0.92	36 36 Cir	0.99 0.99	7.74 10.19	40.00 72.03	PB5A
7	6	Curb	0.012	276.549	0.00 0.00 0.00	0.00 0.00 0.00	0.00 0.00 0.00	0.78	0.77	0.00	0.00	2.60 29.50	6890.30	6885.04 6885.69 6883.19	6881.98 6882.92 6880.42	3.06 2.77	30 30 Cir	1.11 1.00	8.38 9.06	29.50 44.47	PB3
8	7	None	0.012	245.950	0.00 0.00 0.00	0.00 0.00 0.00	0.00 0.00 0.00	0.05	0.73	0.00	0.00	0.00 17.60	6893.40	6887.66 6888.15 6886.15	6885.04 6885.69 6883.69	2.62 2.46	24 24 Cir	1.07 1.00	7.36 7.80	17.60 24.50	PB1B
9	8	None	0.012	16.464	0.00 0.00 0.00	0.00 0.00 0.00	0.00 0.00 0.00	0.00	0.05	0.00	0.00	17.60 17.60	6893.70	6887.82 6888.31 6886.31	6887.66 6888.15 6886.15	0.16 0.16	24 24 Cir	0.97 0.97	6.92 7.69	17.60 24.17	PB1A
10	7	Curb	0.012	44.336	0.00 0.00 0.00	0.00 0.00 0.00	0.00 0.00 0.00	0.00	0.14	0.00	0.00	9.30 9.30	6890.30	6885.81 6886.13 6884.63	6885.22 6885.69 6884.19	0.58 0.44	18 18 Cir	1.32 0.99	6.70 6.41	9.30 11.33	PB2

NOTES: Known Qs only ; Time of flow in section is based on full flow.

Project File: FM 3-7-17 HF.stm

FL-DOT Report

Line No	To Line	Type of struc	n - Value	Len	Drainage Area			Time of conc	Time of Flow in sect	Inten (I)	Total CA	Add Q	Inlet elev	Elev of HGL			Rise	HGL	ADD		Date: 3/16/2017	
					C1 = 0.2 C2 = 0.5 C3 = 0.9							Total Flow		Elev of Crown			Span	Pipe	Full Flow		Frequency: (n/a)	
												Elev of Invert			Proj: FM 3-7-17 HF.stm							
				Q	Up	Down	Fall	Size	Slope	Vel	Cap	Line description										
(cfs)	(ft)	(ft)	(ft)	(in)	(%)	(ft/s)	(cfs)															
11	2	Curb	0.012	52.706	0.00 0.00 0.00	0.00 0.00 0.00	0.00 0.00 0.00	1.19	0.14	0.00	0.00	9.40 61.30	6883.04	6879.20 6880.25 6876.75	6879.10 6879.72 6876.22	0.11 0.53	42 42 Cir	0.20 1.01	7.88 11.36	61.30 109.3	PB12	
12	11	Curb	0.012	44.330	0.00 0.00 0.00	0.00 0.00 0.00	0.00 0.00 0.00	1.09	0.10	0.00	0.00	9.40 51.90	6883.04	6880.03 6880.69 6877.69	6879.20 6880.25 6877.25	0.83 0.44	36 36 Cir	1.87 0.99	9.72 10.18	51.90 71.98	PB11	
13	12	Curb	0.012	255.617	0.00 0.00 0.00	0.00 0.00 0.00	0.00 0.00 0.00	0.05	1.04	0.00	0.00	1.70 12.90	6885.40	6882.54 6883.25 6881.25	6880.03 6880.69 6878.69	2.51 2.56	24 24 Cir	0.98 1.00	5.89 7.81	12.90 24.52	PB9	
14	13	None	0.012	10.167	0.00 0.00 0.00	0.00 0.00 0.00	0.00 0.00 0.00	0.00	0.05	0.00	0.00	11.20 11.20	6885.60	6882.55 6883.35 6881.35	6882.54 6883.25 6881.25	0.01 0.10	24 24 Cir	0.08 0.98	5.46 7.74	11.20 24.31	PB8	
15	6	Curb	0.012	44.335	0.00 0.00 0.00	0.00 0.00 0.00	0.00 0.00 0.00	0.00	0.14	0.00	0.00	9.10 9.10	6886.88	6883.03 6883.36 6881.86	6882.44 6882.92 6881.42	0.59 0.44	18 18 Cir	1.33 0.99	6.65 6.41	9.10 11.33	PB4	
16	1	None	0.012	266.443	0.00 0.00 0.00	0.00 0.00 0.00	0.00 0.00 0.00	0.00	0.67	0.00	0.00	20.70 20.70	6882.04	6880.55 6880.92 6878.92	6877.94 6878.25 6876.25	2.61 2.67	24 24 Cir	0.98 1.00	7.43 7.81	20.70 24.53	PB15	
17	12	None	0.012	10.167	0.00 0.00 0.00	0.00 0.00 0.00	0.00 0.00 0.00	0.00	0.03	0.00	0.00	29.60 29.60	6883.24	6880.14 6880.79 6878.29	6880.03 6880.69 6878.19	0.11 0.10	30 30 Cir	1.11 0.98	7.61 8.98	29.60 44.09	PB10	
18	1	None	0.012	269.817	0.00 0.00 0.00	0.00 0.00 0.00	0.00 0.00 0.00	0.00	0.87	0.00	0.00	16.20 16.20	6882.06	6880.40 6880.95 6878.95	6877.94 6878.25 6876.25	2.46 2.70	24 24 Cir	0.91 1.00	6.18 7.80	16.20 24.51	PB14	

NOTES: Known Qs only ; Time of flow in section is based on full flow.

Project File: FM 3-7-17 HF.stm

Line No.	Area Dn (sqft)	Area Up (sqft)	Byp Ln No	Coeff C1 (C)	Coeff C2 (C)	Coeff C3 (C)	Capac Full (cfs)	Crit Depth (ft)	Cross SI, Sw (ft/ft)	Cross SI, Sx (ft/ft)	Curb Len (ft)	Defl Ang (Deg)	Depth Dn (ft)	Depth Up (ft)	DnStm Ln No	Drng Area (ac)	Easting X (ft)	EGL Dn (ft)	EGL Up (ft)	Energy Loss (ft)	
1	12.12	12.11	n/a	0.20	0.50	0.90	155.22	3.69	-89.363	3.69	3.69**	Outfall	0.00	9422.28	6880.53	6880.78	0.000	
2	11.31	11.31	n/a	0.20	0.50	0.90	155.66	3.37	-0.786	3.69	3.37**	1	0.00	9421.90	6879.89	6881.05	0.000	
3	7.46	7.46	Sag	0.20	0.50	0.90	109.41	2.53	0.083	0.020	10.00	53.397	2.87	2.54**	2	0.00	9463.25	6880.29	6880.47	0.000	
4	5.11	5.88	Sag	0.20	0.50	0.90	71.98	2.33	0.083	0.020	10.00	-53.375	2.04	2.33**	3	0.00	9463.15	6880.46	6881.19	0.000	
5	5.17	5.17	n/a	0.20	0.50	0.90	72.32	2.06	88.983	2.33	2.06**	4	0.00	9594.86	6880.94	6881.99	0.000	
6	5.17	5.17	Offsite	0.20	0.50	0.90	72.03	2.06	0.083	0.020	10.00	-46.653	2.06	2.06**	5	0.00	9657.03	6881.99	6882.91	0.000	
7	3.21	3.89	Offsite	0.20	0.50	0.90	44.47	1.85	0.083	0.020	10.00	-42.201	1.56	1.85**	6	0.00	9657.04	6882.87	6885.93	0.000	
8	2.26	2.55	n/a	0.20	0.50	0.90	24.50	1.51	0.000	1.35	1.51**	7	0.00	9657.05	6885.78	6888.40	0.000	
9	2.55	2.55	n/a	0.20	0.50	0.90	24.17	1.51	-53.625	1.51	1.51**	8	0.00	9643.80	6888.40	6888.56	0.000	
10	1.30	1.49	Offsite	0.20	0.50	0.90	11.33	1.18	0.083	0.020	10.00	89.981	1.03	1.18**	7	0.00	9701.38	6885.83	6886.42	0.000	
11	7.20	7.20	Sag	0.20	0.50	0.90	109.27	2.45	0.050	0.020	10.00	-53.988	2.87	2.45**	2	0.00	9379.19	6880.22	6880.33	0.000	
12	4.87	5.92	Sag	0.20	0.50	0.90	71.98	2.34	0.083	0.020	10.00	54.116	1.95	2.34**	11	0.00	9379.17	6880.40	6881.23	0.000	
13	2.14	2.14	Offsite	0.20	0.50	0.90	24.52	1.29	0.083	0.020	10.00	-89.979	1.34	1.29**	12	0.00	9123.56	6880.59	6883.10	0.000	
14	1.97	1.97	n/a	0.20	0.50	0.90	24.31	1.20	89.940	1.29	1.20**	13	0.00	9123.54	6883.05	6883.05	0.000	
15	1.28	1.47	Offsite	0.20	0.50	0.90	11.33	1.17	0.083	0.020	10.00	47.813	1.02	1.17**	6	0.00	9701.37	6883.03	6883.62	0.000	
16	2.74	2.74	n/a	0.20	0.50	0.90	24.53	1.63	89.475	1.69	1.63**	1	0.00	9688.73	6878.83	6881.44	0.000	
17	3.87	3.90	n/a	0.20	0.50	0.90	44.09	1.85	-0.039	1.84	1.85**	12	0.00	9379.16	6880.93	6881.04	0.000	
18	2.44	2.44	n/a	0.20	0.50	0.90	24.51	1.45	-90.576	1.69	1.45**	1	0.00	9152.47	6878.63	6881.09	0.000	

Project File: FM 3-7-17 HF.stm

Number of lines: 18

Date: 3/16/2017

NOTES: ** Critical depth

MyReport

Flow Rate	Sf Ave	Sf Dn	Grate Area	Grate Len	Grate Width	Gnd/Rim El Dn	Gnd/Rim El Up	Gutter Depth	Gutter Slope	Gutter Spread	Gutter Width	HGL Dn	HGL Up	HGL Jnct	HGL Jmp Dn	HGL Jmp Up	Incr CxA	Incr Q	Inlet Depth	Inlet Eff
(cfs)	(ft/ft)	(ft/ft)	(sqft)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft/ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)		(cfs)	(ft)	(%)
163.70	0.000	0.000	6878.66	6882.05	6877.69	6877.94	6877.94	0.00	0.00
126.80	0.000	0.000	6882.05	6883.35	6877.94	6879.10	6879.10	0.00	0.00
65.50	0.000	0.000	6883.35	6883.20	0.61	Sag	24.20	2.00	6879.10	6879.28	6879.28	0.00	14.30	0.61	100
51.20	0.000	0.000	6883.20	6883.20	0.52	Sag	19.62	2.00	6879.28	6880.01	6880.01	0.00	11.20	0.52	100
40.00	0.000	0.000	6883.20	6884.84	6880.01	6881.06 j	6881.06	6879.88	6879.75	0.00	0.00
40.00	0.000	0.000	6884.84	6886.62	0.25	0.010	5.95	2.00	6881.06	6881.98	6881.98	0.00	1.40	0.25	100
29.50	0.000	0.000	6886.62	6890.30	0.29	0.010	8.35	2.00	6881.98	6885.04	6885.04	0.00	2.60	0.29	89
17.60	0.000	0.000	6890.30	6893.40	6885.04	6887.66	6887.66	0.00	0.00
17.60	0.000	0.000	6893.40	6893.70	6887.66	6887.82	6887.82	0.00	17.60
9.30	0.000	0.000	6890.30	6890.30	0.42	0.010	14.70	2.00	6885.22	6885.81	6885.81	0.00	9.30	0.42	53
61.30	0.000	0.000	6883.35	6883.04	0.46	Sag	20.06	2.00	6879.10	6879.20	6879.20	0.00	9.40	0.46	100
51.90	0.000	0.000	6883.04	6883.04	0.46	Sag	16.76	2.00	6879.20	6880.03	6880.03	0.00	9.40	0.46	100
12.90	0.000	0.000	6883.04	6885.40	0.26	0.010	6.70	2.00	6880.03	6882.54 j	6882.54	6880.24	6880.10	0.00	1.70	0.26	98
11.20	0.000	0.000	6885.40	6885.60	6882.54	6882.55	6882.55	0.00	11.20
9.10	0.000	0.000	6886.62	6886.88	0.42	0.010	14.55	2.00	6882.44	6883.03	6883.03	0.00	9.10	0.42	53
20.70	0.000	0.000	6882.05	6882.04	6877.94	6880.55 j	6880.55	6878.15	6878.06	0.00	20.70
29.60	0.000	0.000	6883.04	6883.24	6880.03	6880.14	6880.14	0.00	29.60
16.20	0.000	0.000	6882.05	6882.06	6877.94	6880.40 j	6880.40	6877.97	6877.83	0.00	16.20

Project File: FM 3-7-17 HF.stm

Number of lines: 18

Date: 3/16/2017

NOTES: ** Critical depth

Inlet ID	Inlet Loc		Inlet Time	i Sys	i Inlet	Invert Dn	Invert Up	Jump Loc	Jump Len	Vel Hd Jmp Dn	Vel Hd Jmp Up	J-Loss Coeff	Junct Type	Known Q	Cost RCP	Cost CMP	Cost PVC	Line ID	
		(ft)	(min)	(in/hr)	(in/hr)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)			(cfs)					
MB2	Sag		0.0	0.00	0.00	6874.00	6874.25	0.00	0.00	1.00 z	MH	0.00	1,646	1,481	1,399	PB16	
MB1	Sag		0.0	0.00	0.00	6874.25	6875.72	0.00	0.00	0.84 z	MH	0.00	9,506	8,555	8,080	PB13	
IB6	Sag		0.0	0.00	0.00	6876.22	6876.74	0.00	0.00	1.25 z	Curb	14.30	3,323	2,991	2,825	PB7	
IB5	Sag		0.0	0.00	0.00	6877.24	6877.68	0.00	0.00	1.50 z	Curb	11.20	2,408	2,167	2,047	PB6	
NB3	On Grade		0.0	0.00	0.00	6877.68	6879.00	13.17	10.32	0.92	1.21	0.77 z	None	0.00	6,958	6,262	5,914	PB5B	
IB4	On Grade		0.0	0.00	0.00	6879.00	6879.92	0.00	0.00	1.17 z	Curb	1.40	5,544	4,990	4,712	PB5A	
IB2	On Grade		0.0	0.00	0.00	6880.42	6883.19	0.00	0.00	1.50 z	Curb	2.60	15,614	14,053	13,272	PB3	
NB2	On Grade		0.0	0.00	0.00	6883.69	6886.15	0.00	0.00	0.84 z	None	0.00	12,896	11,606	10,962	PB1B	
NB1	On Grade		0.0	0.00	0.00	6886.15	6886.31	0.00	0.00	1.00 z	None	17.60	962	866	818	PB1A	
IB1	On Grade		0.0	0.00	0.00	6884.19	6884.63	0.00	0.00	1.00 z	Curb	9.30	1,935	1,742	1,645	PB2	
IB9	Sag		0.0	0.00	0.00	6876.22	6876.75	0.00	0.00	1.26 z	Curb	9.40	3,385	3,047	2,877	PB12	
IB8	Sag		0.0	0.00	0.00	6877.25	6877.69	0.00	0.00	1.50 z	Curb	9.40	2,408	2,167	2,047	PB11	
IB7	On Grade		0.0	0.00	0.00	6878.69	6881.25	25.56	6.46	0.56	0.86	1.50 z	Curb	1.70	11,362	10,226	9,658	PB9	
NB4	On Grade		0.0	0.00	0.00	6881.25	6881.35	0.00	0.00	1.00 z	None	11.20	560	504	476	PB8	
IB3	On Grade		0.0	0.00	0.00	6881.42	6881.86	0.00	0.00	1.00 z	Curb	9.10	1,880	1,692	1,598	PB4	
NB7	On Grade		0.0	0.00	0.00	6876.25	6878.92	26.64	8.15	0.89	1.11	1.00 z	None	20.70	11,104	9,994	9,438	PB15	
NB5	On Grade		0.0	0.00	0.00	6878.19	6878.29	0.00	0.00	1.00 z	None	29.60	600	540	510	PB10	
NB6	On Grade		0.0	0.00	0.00	6876.25	6878.95	26.98	7.25	0.69	0.97	1.00 z	None	16.20	11,246	10,121	9,559	PB14	
Project File: FM 3-7-17 HF.stm													Number of lines: 18			Date: 3/16/2017			
NOTES: Known Qs only. ; ** Critical depth																			

Line Length	Line Size	Line Slope	Line Type	Local Depr	n-val Gutter	n-val Pipe	Minor Loss	Northing Y	Pipe Travel	Q Byp	Q Capt	Q Carry	Line Rise	Runoff Coeff	Line Span	Area A1	Area A2	Area A3	Tc	Throat Ht	Total Area	Total CxA
(ft)	(in)	(%)		(in)			(ft)	(ft)	(min)	(cfs)	(cfs)	(cfs)	(in)	(C)	(in)	(ac)	(ac)	(ac)	(min)	(in)	(ac)	
25.128	48	0.99	Cir	0.012	n/a	15205.44	0.03	48	0.00	48	0.00	0.00	0.00	2.7	0.00	0.00
146.947	48	1.00	Cir	0.012	1.64	15352.39	0.24	48	0.00	48	0.00	0.00	0.00	2.4	0.00	0.00
51.602	42	1.01	Cir	0.0	0.012	1.50	15383.27	0.13	0.00	14.30	0.00	42	0.00	42	0.00	0.00	0.00	2.3	6.0	0.00	0.00
44.332	36	0.99	Cir	0.0	0.012	n/a	15427.60	0.10	0.00	11.20	0.00	36	0.00	36	0.00	0.00	0.00	2.2	6.0	0.00	0.00
131.739	36	1.00	Cir	0.012	n/a	15430.23	0.39	36	0.00	36	0.00	0.00	0.00	1.8	0.00	0.00
92.553	36	0.99	Cir	0.0	0.013	0.012	n/a	15498.79	0.27	0.00	1.40	0.00	36	0.00	36	0.00	0.00	0.00	1.5	6.0	0.00	0.00
276.549	30	1.00	Cir	0.0	0.013	0.012	1.34	15775.34	0.77	0.29	2.31	0.00	30	0.00	30	0.00	0.00	0.00	0.8	6.0	0.00	0.00
245.950	24	1.00	Cir	0.012	n/a	16021.29	0.73	24	0.00	24	0.00	0.00	0.00	0.0	0.00	0.00
16.464	24	0.97	Cir	0.012	n/a	16031.05	0.05	24	0.00	24	0.00	0.00	0.00	0.0	0.00	0.00
44.336	18	0.99	Cir	0.0	0.013	0.012	n/a	15775.35	0.14	4.39	4.91	0.00	18	0.00	18	0.00	0.00	0.00	0.0	6.0	0.00	0.00
52.706	42	1.01	Cir	0.0	0.012	n/a	15383.27	0.14	0.00	9.40	0.00	42	0.00	42	0.00	0.00	0.00	1.2	6.0	0.00	0.00
44.330	36	0.99	Cir	0.0	0.012	n/a	15427.60	0.10	0.00	9.40	0.00	36	0.00	36	0.00	0.00	0.00	1.1	6.0	0.00	0.00
255.617	24	1.00	Cir	0.0	0.013	0.012	n/a	15427.60	1.04	0.03	1.67	0.00	24	0.00	24	0.00	0.00	0.00	0.0	6.0	0.00	0.00
10.167	24	0.98	Cir	0.012	n/a	15437.77	0.05	24	0.00	24	0.00	0.00	0.00	0.0	0.00	0.00
44.335	18	0.99	Cir	0.0	0.013	0.012	0.59	15498.78	0.14	4.25	4.85	0.00	18	0.00	18	0.00	0.00	0.00	0.0	6.0	0.00	0.00
266.443	24	1.00	Cir	0.012	n/a	15204.93	0.67	24	0.00	24	0.00	0.00	0.00	0.0	0.00	0.00
10.167	30	0.98	Cir	0.012	0.89	15437.77	0.03	30	0.00	30	0.00	0.00	0.00	0.0	0.00	0.00
269.817	24	1.00	Cir	0.012	n/a	15205.73	0.87	24	0.00	24	0.00	0.00	0.00	0.0	0.00	0.00
Project File: FM 3-7-17 HF.stm													Number of lines: 18					Date: 3/16/2017				
NOTES: ** Critical depth																						

Total Runoff	Vel Ave	Vel Dn	Vel Hd Dn	Vel Hd Up	Vel Up	Cover Dn	Cover Up	Storage					
(cfs)	(ft/s)	(ft/s)	(ft)	(ft)	(ft/s)	(ft)	(ft)	(cft)					
0.00	13.51	13.51	2.84	2.84	13.51	0.66	3.80	304.43					
0.00	10.84	10.47	1.95	1.95	11.21	3.80	3.63	1723.89					
0.00	8.26	7.75	1.20	1.20	8.78	3.63	2.96	411.33					
0.00	9.37	10.03	1.18	1.18	8.71	2.96	2.52	243.81					
0.00	7.27	6.80	0.93	0.93	7.74	2.52	2.84	728.38					
0.00	7.74	7.74	0.93	0.93	7.74	2.84	3.70	478.15					
0.00	8.38	9.18	0.89	0.89	7.57	3.70	4.61	984.74					
0.00	7.36	7.80	0.74	0.74	6.92	4.61	5.25	590.95					
0.00	6.92	6.92	0.74	0.74	6.92	5.25	5.39	41.90					
0.00	6.70	7.16	0.61	0.61	6.25	4.61	4.17	61.86					
0.00	7.88	7.25	1.13	1.13	8.52	3.63	2.79	413.49					
0.00	9.72	10.66	1.20	1.20	8.77	2.79	2.35	239.62					
0.00	5.89	5.76	0.56	0.56	6.02	2.35	2.15	560.42					
0.00	5.46	5.22	0.50	0.50	5.70	2.15	2.25	20.90					
0.00	6.65	7.13	0.59	0.59	6.17	3.70	3.52	61.05					
0.00	7.43	7.31	0.89	0.89	7.55	3.80	1.12	742.30					
0.00	7.61	7.64	0.89	0.89	7.59	2.35	2.45	39.52					
0.00	6.18	5.72	0.69	0.69	6.64	3.80	1.11	712.62					
Project File: FM 3-7-17 HF.stm								Number of lines: 18				Date: 3/16/2017	
NOTES: ** Critical depth													

Storm Sewer Inlet Time Tabulation

Line No.	Line ID	Tc Method	Sheet Flow					Shallow Concentrated Flow					Channel Flow							Total
			n-Value	flow Length (ft)	2-yr 24h P (in)	Land Slope (%)	Travel Time (min)	flow Length (ft)	Water Slope (%)	Surf Descr	Ave Vel (ft/s)	Travel Time (min)	X-sec Area (sqft)	Wetted Perim (ft)	Chan Slope (%)	n-Value	Vel	flow Length (ft)	Travel Time (min)	Travel Time (min)
1	PB16	User																		0.00
2	PB13	User																		0.00
3	PB7	User																		0.00
4	PB6	User																		0.00
5	PB5B	User																		0.00
6	PB5A	User																		0.00
7	PB3	User																		0.00
8	PB1B	User																		0.00
9	PB1A	User																		0.00
10	PB2	User																		0.00
11	PB12	User																		0.00
12	PB11	User																		0.00
13	PB9	User																		0.00
14	PB8	User																		0.00
15	PB4	User																		0.00
16	PB15	User																		0.00
17	PB10	User																		0.00
18	PB14	User																		0.00
Project File: FM 3-7-17 HF.stm					Min. Tc used for intensity calculations = 5 min							Number of lines: 18				Date: 3/16/2017				

Hydraulic Grade Line Computations

Line	Size	Q	Downstream								Len	Upstream								Check		JL coeff	Minor loss
			Invert elev (ft)	HGL elev (ft)	Depth (ft)	Area (sqft)	Vel (ft/s)	Vel head (ft)	EGL elev (ft)	Sf (%)		Invert elev (ft)	HGL elev (ft)	Depth (ft)	Area (sqft)	Vel (ft/s)	Vel head (ft)	EGL elev (ft)	Sf (%)	Ave Sf (%)	Enrgy loss (ft)		
(1)	(in) (2)	(cfs) (3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(ft) (12)	(13)	(14)	(15)	(16)	(17)	(18)	(19)	(20)	(21)	(22)	(K) (23)	(ft) (24)
1	48	163.7	6874.00	6877.69	3.69	12.12	13.51	2.84	6880.53	0.000	25.128	6874.25	6877.94	3.69**	12.11	13.51	2.84	6880.78	0.000	0.000	n/a	1.00	n/a
2	48	126.8	6874.25	6877.94	3.69	11.31	10.47	1.95	6879.89	0.000	146.947	6875.72	6879.10	3.37**	11.31	11.21	1.95	6881.05	0.000	0.000	n/a	0.84	1.64
3	42	65.50	6876.22	6879.10	2.87	7.46	7.75	1.20	6880.29	0.000	51.602	6876.74	6879.28	2.54**	7.46	8.78	1.20	6880.47	0.000	0.000	n/a	1.25	1.50
4	36	51.20	6877.24	6879.28	2.04	5.11	10.03	1.18	6880.46	0.000	44.332	6877.68	6880.01	2.33**	5.88	8.71	1.18	6881.19	0.000	0.000	n/a	1.50	n/a
5	36	40.00	6877.68	6880.01	2.33	5.17	6.80	0.93	6880.94	0.000	131.739	6879.00	6881.06 j	2.06**	5.17	7.74	0.93	6881.99	0.000	0.000	n/a	0.77	n/a
6	36	40.00	6879.00	6881.06	2.06*	5.17	7.74	0.93	6881.99	0.000	92.553	6879.92	6881.98	2.06**	5.17	7.74	0.93	6882.91	0.000	0.000	n/a	1.17	n/a
7	30	29.50	6880.42	6881.98	1.56	3.21	9.18	0.89	6882.87	0.000	276.549	6883.19	6885.04	1.85**	3.89	7.57	0.89	6885.93	0.000	0.000	n/a	1.50	1.34
8	24	17.60	6883.69	6885.04	1.35	2.26	7.80	0.74	6885.78	0.000	245.950	6886.15	6887.66	1.51**	2.55	6.92	0.74	6888.40	0.000	0.000	n/a	0.84	n/a
9	24	17.60	6886.15	6887.66	1.51*	2.55	6.92	0.74	6888.40	0.000	16.464	6886.31	6887.82	1.51**	2.55	6.92	0.74	6888.56	0.000	0.000	n/a	1.00	n/a
10	18	9.30	6884.19	6885.22	1.03*	1.30	7.16	0.61	6885.83	0.000	44.336	6884.63	6885.81	1.18**	1.49	6.25	0.61	6886.42	0.000	0.000	n/a	1.00	n/a
11	42	61.30	6876.22	6879.10	2.87	7.20	7.25	1.13	6880.22	0.000	52.706	6876.75	6879.20	2.45**	7.20	8.52	1.13	6880.33	0.000	0.000	n/a	1.26	n/a
12	36	51.90	6877.25	6879.20	1.95	4.87	10.66	1.20	6880.40	0.000	44.330	6877.69	6880.03	2.34**	5.92	8.77	1.20	6881.23	0.000	0.000	n/a	1.50	n/a
13	24	12.90	6878.69	6880.03	1.34	2.14	5.76	0.56	6880.59	0.000	255.617	6881.25	6882.54 j	1.29**	2.14	6.02	0.56	6883.10	0.000	0.000	n/a	1.50	0.84
14	24	11.20	6881.25	6882.54	1.29	1.97	5.22	0.50	6883.05	0.000	10.167	6881.35	6882.55	1.20**	1.97	5.70	0.50	6883.05	0.000	0.000	n/a	1.00	n/a
15	18	9.10	6881.42	6882.44	1.02*	1.28	7.13	0.59	6883.03	0.000	44.335	6881.86	6883.03	1.17**	1.47	6.17	0.59	6883.62	0.000	0.000	n/a	1.00	0.59
16	24	20.70	6876.25	6877.94	1.69	2.74	7.31	0.89	6878.83	0.000	266.443	6878.92	6880.55 j	1.63**	2.74	7.55	0.89	6881.44	0.000	0.000	n/a	1.00	n/a
17	30	29.60	6878.19	6880.03	1.84	3.87	7.64	0.89	6880.93	0.000	10.167	6878.29	6880.14	1.85**	3.90	7.59	0.89	6881.04	0.000	0.000	n/a	1.00	0.89
18	24	16.20	6876.25	6877.94	1.69	2.44	5.72	0.69	6878.63	0.000	269.817	6878.95	6880.40 j	1.45**	2.44	6.64	0.69	6881.09	0.000	0.000	n/a	1.00	n/a
Project File: FM 3-7-17 HF.stm														Number of lines: 18					Run Date: 3/16/2017				
Notes: * depth assumed; ** Critical depth.; j-Line contains hyd. jump ; c = cir e = ellip b = box																							

General Procedure:

Hydraflow computes the HGL using the Bernoulli energy equation. Manning's equation is used to determine energy losses due to pipe friction. In a standard step, iterative procedure, Hydraflow assumes upstream HGLs until the energy equation balances. If the energy equation cannot balance, supercritical flow exists and critical depth is temporarily assumed at the upstream end. A supercritical flow Profile is then computed using the same procedure in a downstream direction using momentum principles.

Col. 1 The line number being computed. Calculations begin at Line 1 and proceed upstream.

Col. 2 The line size. In the case of non-circular pipes, the line rise is printed above the span.

Col. 3 Total flow rate in the line.

Col. 4 The elevation of the downstream invert.

Col. 5 Elevation of the hydraulic grade line at the downstream end. This is computed as the upstream HGL + Minor loss of this line's downstream line.

Col. 6 The downstream depth of flow inside the pipe (HGL - Invert elevation) but not greater than the line size.

Col. 7 Cross-sectional area of the flow at the downstream end.

Col. 8 The velocity of the flow at the downstream end, (Col. 3 / Col. 7).

Col. 9 Velocity head (Velocity squared / 2g).

Col. 10 The elevation of the energy grade line at the downstream end, HGL + Velocity head, (Col. 5 + Col. 9).

Col. 11 The friction slope at the downstream end (the S or Slope term in Manning's equation).

Col. 12 The line length.

Col. 13 The elevation of the upstream invert.

Col. 14 Elevation of the hydraulic grade line at the upstream end.

Col. 15 The upstream depth of flow inside the pipe (HGL - Invert elevation) but not greater than the line size.

Col. 16 Cross-sectional area of the flow at the upstream end.

Col. 17 The velocity of the flow at the upstream end, (Col. 3 / Col. 16).

Col. 18 Velocity head (Velocity squared / 2g).

Col. 19 The elevation of the energy grade line at the upstream end, HGL + Velocity head, (Col. 14 + Col. 18) .

Col. 20 The friction slope at the upstream end (the S or Slope term in Manning's equation).

Col. 21 The average of the downstream and upstream friction slopes.

Col. 22 Energy loss. Average $S_f/100 \times \text{Line Length}$ (Col. 21/100 x Col. 12). Equals (EGL upstream - EGL downstream) +/- tolerance.

Col. 23 The junction loss coefficient (K).

Col. 24 Minor loss. (Col. 23 x Col. 18). Is added to upstream HGL and used as the starting HGL for the next upstream line(s).

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

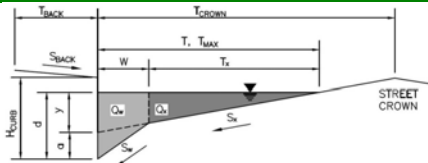
(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project:

FALCON MARKETPLACE

Inlet ID:

IB1

**Gutter Geometry (Enter data in the blue cells)**

Maximum Allowable Width for Spread Behind Curb

 $T_{BACK} = 7.0$ ft

Side Slope Behind Curb (leave blank for no conveyance credit behind curb)

 $S_{BACK} = 0.020$ ft/ft

Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

 $n_{BACK} = 0.020$

Height of Curb at Gutter Flow Line

 $H_{CURB} = 6.00$ inches

Distance from Curb Face to Street Crown

 $T_{CROWN} = 20.0$ ft

Gutter Width

 $W = 2.00$ ft

Street Transverse Slope

 $S_X = 0.020$ ft/ft

Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)

 $S_W = 0.083$ ft/ft

Street Longitudinal Slope - Enter 0 for sump condition

 $S_O = 0.010$ ft/ft

Manning's Roughness for Street Section (typically between 0.012 and 0.020)

 $n_{STREET} = 0.013$

Max. Allowable Spread for Minor & Major Storm

	Minor Storm	Major Storm	
$T_{MAX} =$	20.0	20.0	ft
$d_{MAX} =$	6.0	7.5	inches

Max. Allowable Depth at Gutter Flowline for Minor & Major Storm

Allow Flow Depth at Street Crown (leave blank for no)

☐ ☐ check = yes
MINOR STORM Allowable Capacity is based on Depth Criterion**MAJOR STORM Allowable Capacity is based on Spread Criterion**

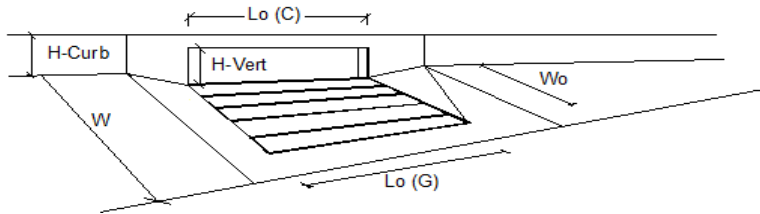
	Minor Storm	Major Storm	
$Q_{allow} =$	17.0	20.1	cfs

Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

INLET ON A CONTINUOUS GRADE

Version 4.04 Released November 2016



Design Information (Input)		MINOR		MAJOR	
Type of Inlet	CDOT Type R Curb Opening	Type =	CDOT Type R Curb Opening		
Local Depression (additional to continuous gutter depression 'a')		a_{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)		No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)		L_o =	10.00	10.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)		W_o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)		$C_r G$ =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)		$C_r C$ =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity		MINOR		MAJOR	
Total Inlet Interception Capacity		Q =	7.0	9.3	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)		Q_b =	3.9	10.5	cfs
Capture Percentage = Q_i/Q_o =		$C\%$ =	64	47	%

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

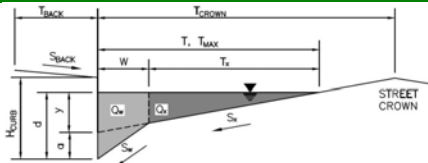
(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project:

FALCON MARKETPLACE

Inlet ID:

IB2

**Gutter Geometry (Enter data in the blue cells)**

Maximum Allowable Width for Spread Behind Curb

 $T_{BACK} = 7.0$ ft

Side Slope Behind Curb (leave blank for no conveyance credit behind curb)

 $S_{BACK} = 0.020$ ft/ft

Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

 $n_{BACK} = 0.020$

Height of Curb at Gutter Flow Line

 $H_{CURB} = 6.00$ inches

Distance from Curb Face to Street Crown

 $T_{CROWN} = 20.0$ ft

Gutter Width

 $W = 2.00$ ft

Street Transverse Slope

 $S_x = 0.020$ ft/ft

Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)

 $S_w = 0.083$ ft/ft

Street Longitudinal Slope - Enter 0 for sump condition

 $S_o = 0.010$ ft/ft

Manning's Roughness for Street Section (typically between 0.012 and 0.020)

 $n_{STREET} = 0.013$

Max. Allowable Spread for Minor & Major Storm

	Minor Storm	Major Storm	
$T_{MAX} =$	20.0	20.0	ft
$d_{MAX} =$	6.0	7.5	inches

Max. Allowable Depth at Gutter Flowline for Minor & Major Storm

Allow Flow Depth at Street Crown (leave blank for no)

☐ ☐ check = yes
MINOR STORM Allowable Capacity is based on Depth Criterion**MAJOR STORM Allowable Capacity is based on Spread Criterion**

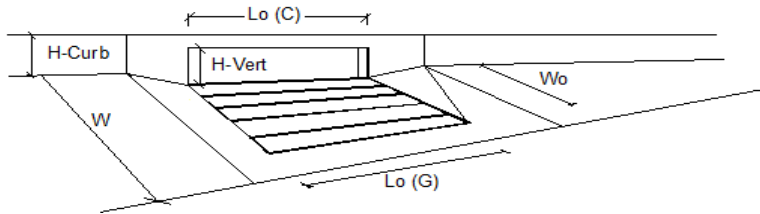
	Minor Storm	Major Storm	
$Q_{allow} =$	17.0	20.1	cfs

Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

INLET ON A CONTINUOUS GRADE

Version 4.04 Released November 2016



Design Information (Input)	MINOR	MAJOR	
Type of Inlet	CDOT Type R Curb Opening		
Local Depression (additional to continuous gutter depression 'a')	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	10.00	10.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity			
Total Inlet Interception Capacity	1.5	2.6	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	0.0	0.0	cfs
Capture Percentage = Q_i/Q_o =	100	100	%

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

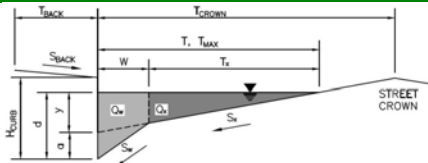
(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project:

FALCON MARKETPLACE

Inlet ID:

IB3

**Gutter Geometry (Enter data in the blue cells)**

Maximum Allowable Width for Spread Behind Curb

 $T_{BACK} = 7.0$ ft

Side Slope Behind Curb (leave blank for no conveyance credit behind curb)

 $S_{BACK} = 0.020$ ft/ft

Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

 $n_{BACK} = 0.020$

Height of Curb at Gutter Flow Line

 $H_{CURB} = 6.00$ inches

Distance from Curb Face to Street Crown

 $T_{CROWN} = 20.0$ ft

Gutter Width

 $W = 2.00$ ft

Street Transverse Slope

 $S_X = 0.020$ ft/ft

Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)

 $S_W = 0.083$ ft/ft

Street Longitudinal Slope - Enter 0 for sump condition

 $S_O = 0.010$ ft/ft

Manning's Roughness for Street Section (typically between 0.012 and 0.020)

 $n_{STREET} = 0.013$

Max. Allowable Spread for Minor & Major Storm

	Minor Storm	Major Storm	
$T_{MAX} =$	20.0	20.0	ft
$d_{MAX} =$	6.0	7.5	inches

Max. Allowable Depth at Gutter Flowline for Minor & Major Storm

Allow Flow Depth at Street Crown (leave blank for no)

☐ ☐ check = yes
MINOR STORM Allowable Capacity is based on Depth Criterion**MAJOR STORM Allowable Capacity is based on Spread Criterion**

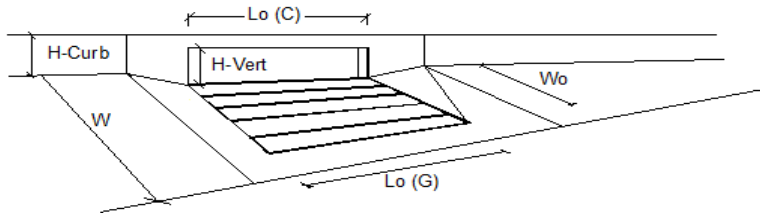
	Minor Storm	Major Storm	
$Q_{allow} =$	17.0	20.1	cfs

Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

INLET ON A CONTINUOUS GRADE

Version 4.04 Released November 2016



Design Information (Input)	MINOR	MAJOR	
Type of Inlet	CDOT Type R Curb Opening		
Local Depression (additional to continuous gutter depression 'a')	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	10.00	10.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity			
Total Inlet Interception Capacity	6.2	9.1	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	2.3	10.0	cfs
Capture Percentage = Q_i/Q_o =	73	48	%

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

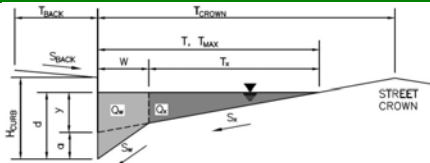
(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project:

FALCON MARKETPLACE

Inlet ID:

IB4

**Gutter Geometry (Enter data in the blue cells)**

Maximum Allowable Width for Spread Behind Curb

T_{BACK} = 7.0 ft

Side Slope Behind Curb (leave blank for no conveyance credit behind curb)

S_{BACK} = 0.020 ft/ft

Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

n_{BACK} = 0.020

Height of Curb at Gutter Flow Line

H_{CURB} = 6.00 inches

Distance from Curb Face to Street Crown

T_{CROWN} = 20.0 ft

Gutter Width

W = 2.00 ft

Street Transverse Slope

S_X = 0.020 ft/ft

Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)

S_W = 0.083 ft/ft

Street Longitudinal Slope - Enter 0 for sump condition

S_O = 0.010 ft/ft

Manning's Roughness for Street Section (typically between 0.012 and 0.020)

n_{STREET} = 0.013

Max. Allowable Spread for Minor & Major Storm

	Minor Storm	Major Storm	
T _{MAX}	20.0	20.0	ft
d _{MAX}	6.0	7.5	inches

Max. Allowable Depth at Gutter Flowline for Minor & Major Storm

Allow Flow Depth at Street Crown (leave blank for no)

☐ ☐ check = yes
MINOR STORM Allowable Capacity is based on Depth Criterion**MAJOR STORM Allowable Capacity is based on Spread Criterion**

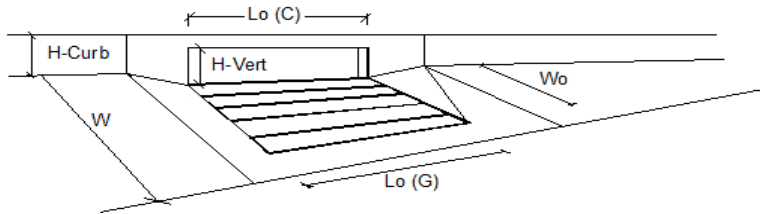
	Minor Storm	Major Storm	
Q _{allow}	17.0	20.1	cfs

Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

INLET ON A CONTINUOUS GRADE

Version 4.04 Released November 2016



Design Information (Input)		MINOR		MAJOR	
Type of Inlet	CDOT Type R Curb Opening	Type =	CDOT Type R Curb Opening		
Local Depression (additional to continuous gutter depression 'a')		a_{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)		N_o =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)		L_o =	10.00	10.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)		W_o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)		$C_r G$ =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)		$C_r C$ =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity		MINOR		MAJOR	
Total Inlet Interception Capacity		Q =	0.8	1.4	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)		Q_b =	0.0	0.0	cfs
Capture Percentage = Q_i/Q_o =		C% =	100	100	%

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

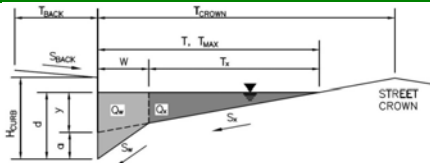
(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project:

FALCON MARKETPLACE

Inlet ID:

IB5

**Gutter Geometry (Enter data in the blue cells)**

Maximum Allowable Width for Spread Behind Curb

 $T_{BACK} = 7.0$ ft

Side Slope Behind Curb (leave blank for no conveyance credit behind curb)

 $S_{BACK} = 0.020$ ft/ft

Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

 $n_{BACK} = 0.020$

Height of Curb at Gutter Flow Line

 $H_{CURB} = 6.00$ inches

Distance from Curb Face to Street Crown

 $T_{CROWN} = 20.0$ ft

Gutter Width

 $W = 2.00$ ft

Street Transverse Slope

 $S_X = 0.020$ ft/ft

Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)

 $S_W = 0.083$ ft/ft

Street Longitudinal Slope - Enter 0 for sump condition

 $S_O = 0.000$ ft/ft

Manning's Roughness for Street Section (typically between 0.012 and 0.020)

 $n_{STREET} = 0.013$

Max. Allowable Spread for Minor & Major Storm

	Minor Storm	Major Storm	
$T_{MAX} =$	20.0	20.0	ft
$d_{MAX} =$	6.0	7.5	inches

Max. Allowable Depth at Gutter Flowline for Minor & Major Storm

Allow Flow Depth at Street Crown (leave blank for no)

☐ ☐ check = yes

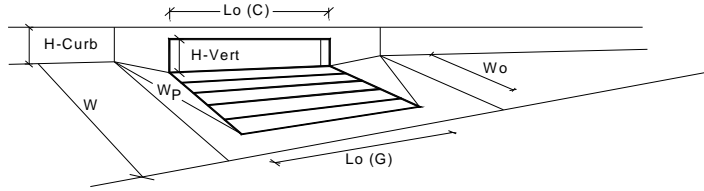
MINOR STORM Allowable Capacity is based on Depth Criterion

	Minor Storm	Major Storm	
$Q_{allow} =$	SUMP	SUMP	cfs

MAJOR STORM Allowable Capacity is based on Depth Criterion

INLET IN A SUMP OR SAG LOCATION

Version 4.04 Released November 2016



Design Information (Input)

Type of Inlet CDOT Type R Curb Opening

Local Depression (additional to continuous gutter depression 'a' from 'Q-Allow')

Number of Unit Inlets (Grate or Curb Opening)

Water Depth at Flowline (outside of local depression)

Grate Information

Length of a Unit Grate

Width of a Unit Grate

Area Opening Ratio for a Grate (typical values 0.15-0.90)

Clogging Factor for a Single Grate (typical value 0.50 - 0.70)

Grate Weir Coefficient (typical value 2.15 - 3.60)

Grate Orifice Coefficient (typical value 0.60 - 0.80)

Curb Opening Information

Length of a Unit Curb Opening

Height of Vertical Curb Opening in Inches

Height of Curb Orifice Throat in Inches

Angle of Throat (see USDCM Figure ST-5)

Side Width for Depression Pan (typically the gutter width of 2 feet)

Clogging Factor for a Single Curb Opening (typical value 0.10)

Curb Opening Weir Coefficient (typical value 2.3-3.7)

Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)

Low Head Performance Reduction (Calculated)

Depth for Grate Midwidth

Depth for Curb Opening Weir Equation

Combination Inlet Performance Reduction Factor for Long Inlets

Curb Opening Performance Reduction Factor for Long Inlets

Grated Inlet Performance Reduction Factor for Long Inlets

Total Inlet Interception Capacity (assumes clogged condition)

WARNING: Inlet Capacity less than Q Peak for Major Storm

	MINOR	MAJOR	
Type =	CDOT Type R Curb Opening		
a_{local} =	3.00	3.00	inches
No =	1	1	
Ponding Depth =	6.0	6.3	inches
	MINOR	MAJOR	<input checked="" type="checkbox"/> Override Depths
L_o (G) =	N/A	N/A	feet
W_o =	N/A	N/A	feet
A_{ratio} =	N/A	N/A	
C_r (G) =	N/A	N/A	
C_w (G) =	N/A	N/A	
C_o (G) =	N/A	N/A	
	MINOR	MAJOR	
L_o (C) =	15.00	15.00	feet
H_{vert} =	6.00	6.00	inches
H_{throat} =	6.00	6.00	inches
Theta =	63.40	63.40	degrees
W_p =	2.00	2.00	feet
C_r (C) =	0.10	0.10	
C_w (C) =	3.60	3.60	
C_o (C) =	0.67	0.67	
	MINOR	MAJOR	
d_{Grate} =	N/A	N/A	ft
d_{Curb} =	0.33	0.36	ft
$RF_{Combination}$ =	0.57	0.60	
RF_{Curb} =	0.79	0.81	
RF_{Grate} =	N/A	N/A	
	MINOR	MAJOR	
Q_a =	9.7	11.2	cfs
$Q_{PEAK REQUIRED}$ =	9.6	17.5	cfs

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

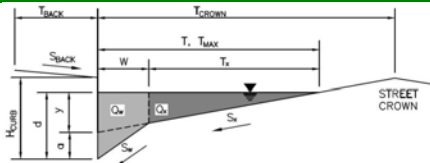
(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project:

FALCON MARKETPLACE

Inlet ID:

IB6

**Gutter Geometry (Enter data in the blue cells)**

Maximum Allowable Width for Spread Behind Curb

 $T_{BACK} = 7.0$ ft

Side Slope Behind Curb (leave blank for no conveyance credit behind curb)

 $S_{BACK} = 0.020$ ft/ft

Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

 $n_{BACK} = 0.020$

Height of Curb at Gutter Flow Line

 $H_{CURB} = 6.00$ inches

Distance from Curb Face to Street Crown

 $T_{CROWN} = 20.0$ ft

Gutter Width

 $W = 2.00$ ft

Street Transverse Slope

 $S_X = 0.020$ ft/ft

Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)

 $S_W = 0.083$ ft/ft

Street Longitudinal Slope - Enter 0 for sump condition

 $S_O = 0.000$ ft/ft

Manning's Roughness for Street Section (typically between 0.012 and 0.020)

 $n_{STREET} = 0.013$

Max. Allowable Spread for Minor & Major Storm

	Minor Storm	Major Storm	
$T_{MAX} =$	20.0	20.0	ft
$d_{MAX} =$	6.0	7.5	inches

Max. Allowable Depth at Gutter Flowline for Minor & Major Storm

Allow Flow Depth at Street Crown (leave blank for no)

☐ ☐ check = yes

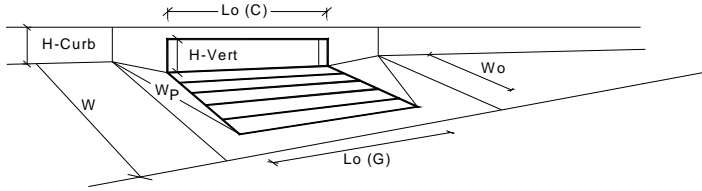
MINOR STORM Allowable Capacity is based on Depth Criterion

	Minor Storm	Major Storm	
$Q_{allow} =$	SUMP	SUMP	cfs

MAJOR STORM Allowable Capacity is based on Depth Criterion

INLET IN A SUMP OR SAG LOCATION

Version 4.04 Released November 2016



Design Information (Input)

Type of Inlet

Local Depression (additional to continuous gutter depression 'a' from 'Q-Allow')

Number of Unit Inlets (Grate or Curb Opening)

Water Depth at Flowline (outside of local depression)

Grate Information

Length of a Unit Grate

Width of a Unit Grate

Area Opening Ratio for a Grate (typical values 0.15-0.90)

Clogging Factor for a Single Grate (typical value 0.50 - 0.70)

Grate Weir Coefficient (typical value 2.15 - 3.60)

Grate Orifice Coefficient (typical value 0.60 - 0.80)

Curb Opening Information

Length of a Unit Curb Opening

Height of Vertical Curb Opening in Inches

Height of Curb Orifice Throat in Inches

Angle of Throat (see USDCM Figure ST-5)

Side Width for Depression Pan (typically the gutter width of 2 feet)

Clogging Factor for a Single Curb Opening (typical value 0.10)

Curb Opening Weir Coefficient (typical value 2.3-3.7)

Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)

Low Head Performance Reduction (Calculated)

Depth for Grate Midwidth

Depth for Curb Opening Weir Equation

Combination Inlet Performance Reduction Factor for Long Inlets

Curb Opening Performance Reduction Factor for Long Inlets

Grated Inlet Performance Reduction Factor for Long Inlets

Total Inlet Interception Capacity (assumes clogged condition)

Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)

	MINOR	MAJOR	
Type =	CDOT Type R Curb Opening		
a_{local} =	3.00	3.00	inches
No =	1	1	
Ponding Depth =	6.0	7.5	inches
	MINOR	MAJOR	<input checked="" type="checkbox"/> Override Depths
$L_o (G)$ =	N/A	N/A	feet
W_o =	N/A	N/A	feet
A_{ratio} =	N/A	N/A	
$C_r (G)$ =	N/A	N/A	
$C_w (G)$ =	N/A	N/A	
$C_o (G)$ =	N/A	N/A	
	MINOR	MAJOR	
$L_o (C)$ =	10.00	10.00	feet
H_{vert} =	6.00	6.00	inches
H_{throat} =	6.00	6.00	inches
Theta =	63.40	63.40	degrees
W_p =	2.00	2.00	feet
$C_r (C)$ =	0.10	0.10	
$C_w (C)$ =	3.60	3.60	
$C_o (C)$ =	0.67	0.67	
	MINOR	MAJOR	
d_{Grate} =	N/A	N/A	ft
d_{Curb} =	0.33	0.46	ft
$RF_{Combination}$ =	0.57	0.71	
RF_{Curb} =	0.93	1.00	
RF_{Grate} =	N/A	N/A	
	MINOR	MAJOR	
Q_a =	8.3	14.3	cfs
$Q_{PEAK REQUIRED}$ =	3.2	11.6	cfs

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

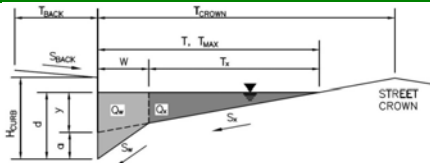
(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project:

FALCON MARKETPLACE

Inlet ID:

IB7

**Gutter Geometry (Enter data in the blue cells)**

Maximum Allowable Width for Spread Behind Curb

 $T_{BACK} = 7.0$ ft

Side Slope Behind Curb (leave blank for no conveyance credit behind curb)

 $S_{BACK} = 0.020$ ft/ft

Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

 $n_{BACK} = 0.020$

Height of Curb at Gutter Flow Line

 $H_{CURB} = 6.00$ inches

Distance from Curb Face to Street Crown

 $T_{CROWN} = 20.0$ ft

Gutter Width

 $W = 2.00$ ft

Street Transverse Slope

 $S_x = 0.020$ ft/ft

Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)

 $S_w = 0.083$ ft/ft

Street Longitudinal Slope - Enter 0 for sump condition

 $S_o = 0.010$ ft/ft

Manning's Roughness for Street Section (typically between 0.012 and 0.020)

 $n_{STREET} = 0.013$

Max. Allowable Spread for Minor & Major Storm

	Minor Storm	Major Storm	
$T_{MAX} =$	20.0	20.0	ft
$d_{MAX} =$	6.0	7.5	inches

Max. Allowable Depth at Gutter Flowline for Minor & Major Storm

	Minor Storm	Major Storm	
$d_{MAX} =$	6.0	7.5	inches

Allow Flow Depth at Street Crown (leave blank for no)

☐ ☐ check = yes
MINOR STORM Allowable Capacity is based on Depth Criterion

	Minor Storm	Major Storm	
$Q_{allow} =$	17.0	20.1	cfs

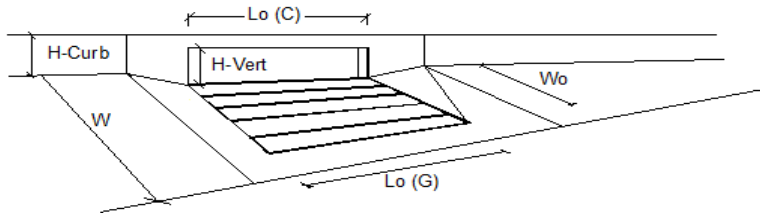
MAJOR STORM Allowable Capacity is based on Spread Criterion

Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

INLET ON A CONTINUOUS GRADE

Version 4.04 Released November 2016



Design Information (Input)	MINOR	MAJOR	
Type of Inlet	CDOT Type R Curb Opening		
Local Depression (additional to continuous gutter depression 'a')	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	10.00	10.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity			
Total Inlet Interception Capacity	1.0	1.7	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	0.0	0.0	cfs
Capture Percentage = Q_i/Q_o =	100	100	%

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

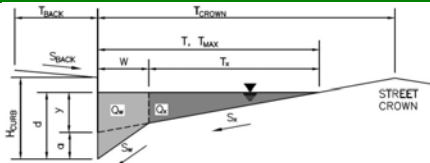
(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project:

FALCON MARKETPLACE

Inlet ID:

IB8

**Gutter Geometry (Enter data in the blue cells)**

Maximum Allowable Width for Spread Behind Curb

 $T_{BACK} = 7.0$ ft

Side Slope Behind Curb (leave blank for no conveyance credit behind curb)

 $S_{BACK} = 0.020$ ft/ft

Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

 $n_{BACK} = 0.020$

Height of Curb at Gutter Flow Line

 $H_{CURB} = 6.00$ inches

Distance from Curb Face to Street Crown

 $T_{CROWN} = 20.0$ ft

Gutter Width

 $W = 2.00$ ft

Street Transverse Slope

 $S_X = 0.020$ ft/ft

Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)

 $S_W = 0.083$ ft/ft

Street Longitudinal Slope - Enter 0 for sump condition

 $S_O = 0.000$ ft/ft

Manning's Roughness for Street Section (typically between 0.012 and 0.020)

 $n_{STREET} = 0.013$

Max. Allowable Spread for Minor & Major Storm

	Minor Storm	Major Storm	
$T_{MAX} =$	20.0	20.0	ft
$d_{MAX} =$	6.0	7.5	inches

Max. Allowable Depth at Gutter Flowline for Minor & Major Storm

Allow Flow Depth at Street Crown (leave blank for no)



check = yes

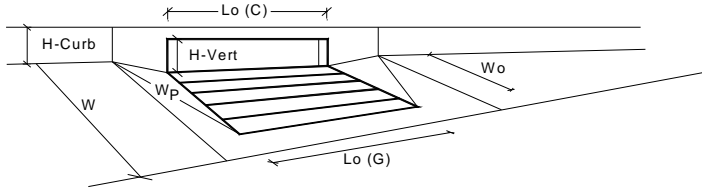
MINOR STORM Allowable Capacity is based on Depth Criterion

MAJOR STORM Allowable Capacity is based on Depth Criterion

	Minor Storm	Major Storm	
$Q_{allow} =$	SUMP	SUMP	cfs

INLET IN A SUMP OR SAG LOCATION

Version 4.04 Released November 2016



Design Information (Input)

Type of Inlet CDOT Type R Curb Opening
 Local Depression (additional to continuous gutter depression 'a' from 'Q-Allow')
 Number of Unit Inlets (Grate or Curb Opening)
 Water Depth at Flowline (outside of local depression)
Grate Information
 Length of a Unit Grate
 Width of a Unit Grate
 Area Opening Ratio for a Grate (typical values 0.15-0.90)
 Clogging Factor for a Single Grate (typical value 0.50 - 0.70)
 Grate Weir Coefficient (typical value 2.15 - 3.60)
 Grate Orifice Coefficient (typical value 0.60 - 0.80)

Curb Opening Information

Length of a Unit Curb Opening
 Height of Vertical Curb Opening in Inches
 Height of Curb Orifice Throat in Inches
 Angle of Throat (see USDCM Figure ST-5)
 Side Width for Depression Pan (typically the gutter width of 2 feet)
 Clogging Factor for a Single Curb Opening (typical value 0.10)
 Curb Opening Weir Coefficient (typical value 2.3-3.7)
 Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)

Low Head Performance Reduction (Calculated)

Depth for Grate Midwidth
 Depth for Curb Opening Weir Equation
 Combination Inlet Performance Reduction Factor for Long Inlets
 Curb Opening Performance Reduction Factor for Long Inlets
 Grated Inlet Performance Reduction Factor for Long Inlets

Total Inlet Interception Capacity (assumes clogged condition)

Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)

	MINOR	MAJOR	
Type =	CDOT Type R Curb Opening		
a_{local} =	3.00	3.00	inches
No =	1	1	
Ponding Depth =	6.0	6.3	inches
	MINOR	MAJOR	Override Depths
L_o (G) =	N/A	N/A	feet
W_o =	N/A	N/A	feet
A_{ratio} =	N/A	N/A	
C_r (G) =	N/A	N/A	
C_w (G) =	N/A	N/A	
C_o (G) =	N/A	N/A	
	MINOR	MAJOR	
L_o (C) =	10.00	10.00	feet
H_{vert} =	6.00	6.00	inches
H_{throat} =	6.00	6.00	inches
Theta =	63.40	63.40	degrees
W_p =	2.00	2.00	feet
C_r (C) =	0.10	0.10	
C_w (C) =	3.60	3.60	
C_o (C) =	0.67	0.67	
	MINOR	MAJOR	
d_{Grate} =	N/A	N/A	ft
d_{Curb} =	0.33	0.36	ft
$RF_{Combination}$ =	0.57	0.60	
RF_{Curb} =	0.93	0.95	
RF_{Grate} =	N/A	N/A	
	MINOR	MAJOR	
Q_a =	8.3	9.4	cfs
$Q_{PEAK REQUIRED}$ =	2.1	6.4	cfs

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

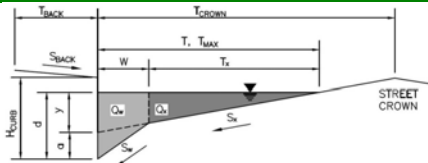
(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project:

FALCON MARKETPLACE

Inlet ID:

IB9

**Gutter Geometry (Enter data in the blue cells)**

Maximum Allowable Width for Spread Behind Curb

 $T_{BACK} = 7.0$ ft

Side Slope Behind Curb (leave blank for no conveyance credit behind curb)

 $S_{BACK} = 0.020$ ft/ft

Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

 $n_{BACK} = 0.020$

Height of Curb at Gutter Flow Line

 $H_{CURB} = 6.00$ inches

Distance from Curb Face to Street Crown

 $T_{CROWN} = 20.0$ ft

Gutter Width

 $W = 2.00$ ft

Street Transverse Slope

 $S_X = 0.020$ ft/ft

Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)

 $S_W = 0.083$ ft/ft

Street Longitudinal Slope - Enter 0 for sump condition

 $S_O = 0.000$ ft/ft

Manning's Roughness for Street Section (typically between 0.012 and 0.020)

 $n_{STREET} = 0.013$

Max. Allowable Spread for Minor & Major Storm

	Minor Storm	Major Storm	
$T_{MAX} =$	20.0	20.0	ft
$d_{MAX} =$	6.0	7.5	inches

Max. Allowable Depth at Gutter Flowline for Minor & Major Storm

Allow Flow Depth at Street Crown (leave blank for no)

☐ ☐ check = yes

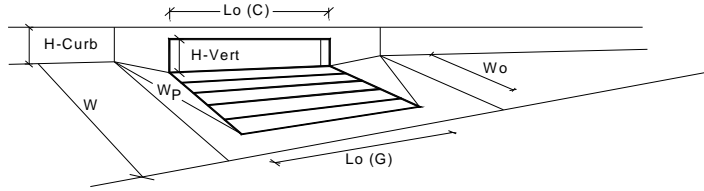
MINOR STORM Allowable Capacity is based on Depth Criterion

	Minor Storm	Major Storm	
$Q_{allow} =$	SUMP	SUMP	cfs

MAJOR STORM Allowable Capacity is based on Depth Criterion

INLET IN A SUMP OR SAG LOCATION

Version 4.04 Released November 2016



Design Information (Input)

CDOT Type R Curb Opening

Type of Inlet

Local Depression (additional to continuous gutter depression 'a' from 'Q-Allow')

Number of Unit Inlets (Grate or Curb Opening)

Water Depth at Flowline (outside of local depression)

Grate Information

Length of a Unit Grate

Width of a Unit Grate

Area Opening Ratio for a Grate (typical values 0.15-0.90)

Clogging Factor for a Single Grate (typical value 0.50 - 0.70)

Grate Weir Coefficient (typical value 2.15 - 3.60)

Grate Orifice Coefficient (typical value 0.60 - 0.80)

Curb Opening Information

Length of a Unit Curb Opening

Height of Vertical Curb Opening in Inches

Height of Curb Orifice Throat in Inches

Angle of Throat (see USDCM Figure ST-5)

Side Width for Depression Pan (typically the gutter width of 2 feet)

Clogging Factor for a Single Curb Opening (typical value 0.10)

Curb Opening Weir Coefficient (typical value 2.3-3.7)

Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)

Low Head Performance Reduction (Calculated)

Depth for Grate Midwidth

Depth for Curb Opening Weir Equation

Combination Inlet Performance Reduction Factor for Long Inlets

Curb Opening Performance Reduction Factor for Long Inlets

Grated Inlet Performance Reduction Factor for Long Inlets

Total Inlet Interception Capacity (assumes clogged condition)

Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)

	MINOR	MAJOR	
Type =	CDOT Type R Curb Opening		
a_{local} =	3.00	3.00	inches
No =	1	1	
Ponding Depth =	6.0	6.3	inches
	MINOR	MAJOR	Override Depths
L_o (G) =	N/A	N/A	feet
W_o =	N/A	N/A	feet
A_{ratio} =	N/A	N/A	
C_r (G) =	N/A	N/A	
C_w (G) =	N/A	N/A	
C_o (G) =	N/A	N/A	
	MINOR	MAJOR	
L_o (C) =	10.00	10.00	feet
H_{vert} =	6.00	6.00	inches
H_{throat} =	6.00	6.00	inches
Theta =	63.40	63.40	degrees
W_p =	2.00	2.00	feet
C_r (C) =	0.10	0.10	
C_w (C) =	3.60	3.60	
C_o (C) =	0.67	0.67	
	MINOR	MAJOR	
d_{Grate} =	N/A	N/A	ft
d_{Curb} =	0.33	0.36	ft
$RF_{Combination}$ =	0.57	0.60	
RF_{Curb} =	0.93	0.95	
RF_{Grate} =	N/A	N/A	
	MINOR	MAJOR	
Q_a =	8.3	9.4	cfs
$Q_{PEAK REQUIRED}$ =	1.5	2.6	cfs

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

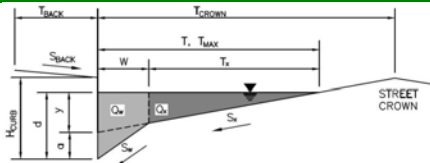
(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project:

FALCON MARKETPLACE

Inlet ID:

IB10

**Gutter Geometry (Enter data in the blue cells)**

Maximum Allowable Width for Spread Behind Curb

 $T_{BACK} = 10.0$ ft

Side Slope Behind Curb (leave blank for no conveyance credit behind curb)

 $S_{BACK} = 0.020$ ft/ft

Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

 $n_{BACK} = 0.020$

Height of Curb at Gutter Flow Line

 $H_{CURB} = 6.00$ inches

Distance from Curb Face to Street Crown

 $T_{CROWN} = 24.0$ ft

Gutter Width

 $W = 2.00$ ft

Street Transverse Slope

 $S_x = 0.020$ ft/ft

Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)

 $S_w = 0.083$ ft/ft

Street Longitudinal Slope - Enter 0 for sump condition

 $S_o = 0.010$ ft/ft

Manning's Roughness for Street Section (typically between 0.012 and 0.020)

 $n_{STREET} = 0.013$

Max. Allowable Spread for Minor & Major Storm

	Minor Storm	Major Storm	
$T_{MAX} =$	24.0	24.0	ft
$d_{MAX} =$	6.0	8.0	inches

Max. Allowable Depth at Gutter Flowline for Minor & Major Storm

Allow Flow Depth at Street Crown (leave blank for no)

☐ ☐ check = yes
MINOR STORM Allowable Capacity is based on Depth Criterion**MAJOR STORM Allowable Capacity is based on Spread Criterion**

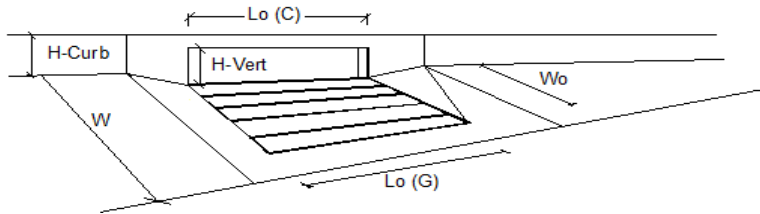
	Minor Storm	Major Storm	
$Q_{allow} =$	17.0	32.3	cfs

Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

INLET ON A CONTINUOUS GRADE

Version 4.04 Released November 2016



Design Information (Input)	MINOR	MAJOR	
Type of Inlet	CDOT Type R Curb Opening		
Local Depression (additional to continuous gutter depression 'a')	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	10.00	10.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity			
Total Inlet Interception Capacity	4.1	6.2	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	0.2	2.3	cfs
Capture Percentage = Q_i/Q_o =	95	73	%

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

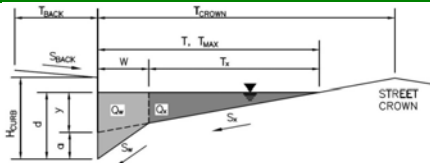
(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project:

FALCON MARKETPLACE

Inlet ID:

IA1

**Gutter Geometry (Enter data in the blue cells)**

Maximum Allowable Width for Spread Behind Curb

 $T_{BACK} = 10.0$ ft

Side Slope Behind Curb (leave blank for no conveyance credit behind curb)

 $S_{BACK} = 0.020$ ft/ft

Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

 $n_{BACK} = 0.020$

Height of Curb at Gutter Flow Line

 $H_{CURB} = 6.00$ inches

Distance from Curb Face to Street Crown

 $T_{CROWN} = 24.0$ ft

Gutter Width

 $W = 2.00$ ft

Street Transverse Slope

 $S_x = 0.020$ ft/ft

Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)

 $S_w = 0.083$ ft/ft

Street Longitudinal Slope - Enter 0 for sump condition

 $S_o = 0.010$ ft/ft

Manning's Roughness for Street Section (typically between 0.012 and 0.020)

 $n_{STREET} = 0.013$

Max. Allowable Spread for Minor & Major Storm

	Minor Storm	Major Storm	
$T_{MAX} =$	24.0	24.0	ft
$d_{MAX} =$	6.0	8.0	inches

Max. Allowable Depth at Gutter Flowline for Minor & Major Storm

	Minor Storm	Major Storm	
$d_{MAX} =$	6.0	8.0	inches

Allow Flow Depth at Street Crown (leave blank for no)

☐ ☐ check = yes

MINOR STORM Allowable Capacity is based on Depth Criterion

	Minor Storm	Major Storm	
$Q_{allow} =$	17.0	32.3	cfs

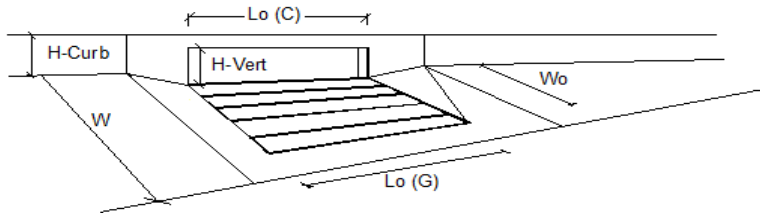
MAJOR STORM Allowable Capacity is based on Spread Criterion

Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

INLET ON A CONTINUOUS GRADE

Version 4.04 Released November 2016



Design Information (Input)	MINOR	MAJOR	
Type of Inlet	CDOT Type R Curb Opening		
Local Depression (additional to continuous gutter depression 'a')	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	10.00	10.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity			
Total Inlet Interception Capacity	2.4	4.7	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	0.0	0.6	cfs
Capture Percentage = Q_i/Q_o =	100	89	%

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

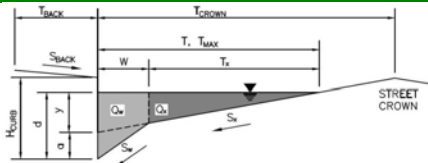
(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project:

FALCON MARKETPLACE

Inlet ID:

IA2

**Gutter Geometry (Enter data in the blue cells)**

Maximum Allowable Width for Spread Behind Curb

 $T_{BACK} = 5.0$ ft

Side Slope Behind Curb (leave blank for no conveyance credit behind curb)

 $S_{BACK} = 0.020$ ft/ft

Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

 $n_{BACK} = 0.020$

Height of Curb at Gutter Flow Line

 $H_{CURB} = 6.00$ inches

Distance from Curb Face to Street Crown

 $T_{CROWN} = 28.0$ ft

Gutter Width

 $W = 2.00$ ft

Street Transverse Slope

 $S_x = 0.020$ ft/ft

Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)

 $S_w = 0.083$ ft/ft

Street Longitudinal Slope - Enter 0 for sump condition

 $S_o = 0.000$ ft/ft

Manning's Roughness for Street Section (typically between 0.012 and 0.020)

 $n_{STREET} = 0.013$

Max. Allowable Spread for Minor & Major Storm

	Minor Storm	Major Storm	
$T_{MAX} =$	28.0	28.0	ft
$d_{MAX} =$	6.0	7.5	inches

Max. Allowable Depth at Gutter Flowline for Minor & Major Storm

Allow Flow Depth at Street Crown (leave blank for no)

☐ ☐ check = yes

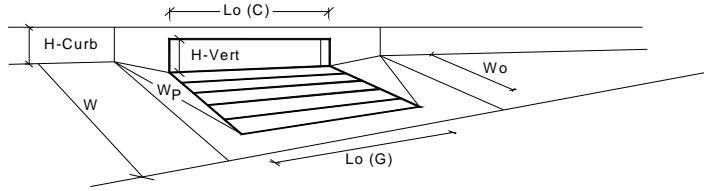
MINOR STORM Allowable Capacity is based on Depth Criterion

	Minor Storm	Major Storm	
$Q_{allow} =$	SUMP	SUMP	cfs

MAJOR STORM Allowable Capacity is based on Depth Criterion

INLET IN A SUMP OR SAG LOCATION

Version 4.04 Released November 2016



Design Information (Input)

Type of Inlet

Local Depression (additional to continuous gutter depression 'a' from 'Q-Allow')

Number of Unit Inlets (Grate or Curb Opening)

Water Depth at Flowline (outside of local depression)

Grate Information

Length of a Unit Grate

Width of a Unit Grate

Area Opening Ratio for a Grate (typical values 0.15-0.90)

Clogging Factor for a Single Grate (typical value 0.50 - 0.70)

Grate Weir Coefficient (typical value 2.15 - 3.60)

Grate Orifice Coefficient (typical value 0.60 - 0.80)

Curb Opening Information

Length of a Unit Curb Opening

Height of Vertical Curb Opening in Inches

Height of Curb Orifice Throat in Inches

Angle of Throat (see USDCM Figure ST-5)

Side Width for Depression Pan (typically the gutter width of 2 feet)

Clogging Factor for a Single Curb Opening (typical value 0.10)

Curb Opening Weir Coefficient (typical value 2.3-3.7)

Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)

Low Head Performance Reduction (Calculated)

Depth for Grate Midwidth

Depth for Curb Opening Weir Equation

Combination Inlet Performance Reduction Factor for Long Inlets

Curb Opening Performance Reduction Factor for Long Inlets

Grated Inlet Performance Reduction Factor for Long Inlets

Total Inlet Interception Capacity (assumes clogged condition)

Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)

	MINOR	MAJOR	
Type =	CDOT Type R Curb Opening		
a_{local} =	3.00	3.00	inches
No =	1	1	
Ponding Depth =	6.0	7.5	inches
	MINOR	MAJOR	Override Depths
$L_o (G)$ =	N/A	N/A	feet
W_o =	N/A	N/A	feet
A_{ratio} =	N/A	N/A	
$C_r (G)$ =	N/A	N/A	
$C_w (G)$ =	N/A	N/A	
$C_o (G)$ =	N/A	N/A	
	MINOR	MAJOR	
$L_o (C)$ =	10.00	10.00	feet
H_{vert} =	6.00	6.00	inches
H_{throat} =	6.00	6.00	inches
Theta =	63.40	63.40	degrees
W_p =	2.00	2.00	feet
$C_r (C)$ =	0.10	0.10	
$C_w (C)$ =	3.60	3.60	
$C_o (C)$ =	0.67	0.67	
	MINOR	MAJOR	
d_{Grate} =	N/A	N/A	ft
d_{Curb} =	0.33	0.46	ft
$RF_{Combination}$ =	0.57	0.71	
RF_{Curb} =	0.93	1.00	
RF_{Grate} =	N/A	N/A	
	MINOR	MAJOR	
Q_a =	8.3	14.3	cfs
$Q_{PEAK REQUIRED}$ =	2.0	4.6	cfs

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

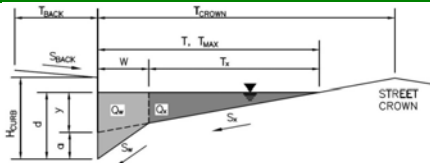
(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project:

FALCON MARKETPLACE

Inlet ID:

IC1

**Gutter Geometry (Enter data in the blue cells)**

Maximum Allowable Width for Spread Behind Curb

 $T_{BACK} = 10.0$ ft

Side Slope Behind Curb (leave blank for no conveyance credit behind curb)

 $S_{BACK} = 0.200$ ft/ft

Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

 $n_{BACK} = 0.020$

Height of Curb at Gutter Flow Line

 $H_{CURB} = 6.00$ inches

Distance from Curb Face to Street Crown

 $T_{CROWN} = 20.0$ ft

Gutter Width

 $W = 2.00$ ft

Street Transverse Slope

 $S_X = 0.020$ ft/ft

Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)

 $S_W = 0.083$ ft/ft

Street Longitudinal Slope - Enter 0 for sump condition

 $S_O = 0.000$ ft/ft

Manning's Roughness for Street Section (typically between 0.012 and 0.020)

 $n_{STREET} = 0.013$

Max. Allowable Spread for Minor & Major Storm

	Minor Storm	Major Storm	
$T_{MAX} =$	20.0	20.0	ft
$d_{MAX} =$	6.0	8.0	inches

Max. Allowable Depth at Gutter Flowline for Minor & Major Storm

Allow Flow Depth at Street Crown (leave blank for no)

☐ ☐ check = yes

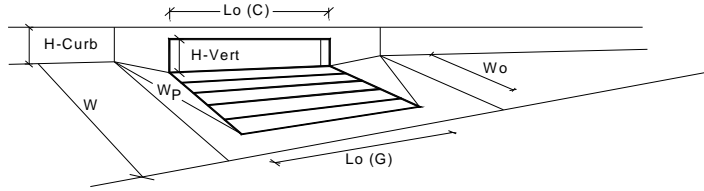
MINOR STORM Allowable Capacity is based on Depth Criterion

MAJOR STORM Allowable Capacity is based on Depth Criterion

	Minor Storm	Major Storm	
$Q_{allow} =$	SUMP	SUMP	cfs

INLET IN A SUMP OR SAG LOCATION

Version 4.04 Released November 2016



Design Information (Input)

Type of Inlet
Local Depression (additional to continuous gutter depression 'a' from 'Q-Allow')
Number of Unit Inlets (Grate or Curb Opening)
Water Depth at Flowline (outside of local depression)
Grate Information
Length of a Unit Grate
Width of a Unit Grate
Area Opening Ratio for a Grate (typical values 0.15-0.90)
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)
Grate Weir Coefficient (typical value 2.15 - 3.60)
Grate Orifice Coefficient (typical value 0.60 - 0.80)

Curb Opening Information

Length of a Unit Curb Opening
Height of Vertical Curb Opening in Inches
Height of Curb Orifice Throat in Inches
Angle of Throat (see USDCM Figure ST-5)
Side Width for Depression Pan (typically the gutter width of 2 feet)
Clogging Factor for a Single Curb Opening (typical value 0.10)
Curb Opening Weir Coefficient (typical value 2.3-3.7)
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)

Low Head Performance Reduction (Calculated)

Depth for Grate Midwidth
Depth for Curb Opening Weir Equation
Combination Inlet Performance Reduction Factor for Long Inlets
Curb Opening Performance Reduction Factor for Long Inlets
Grated Inlet Performance Reduction Factor for Long Inlets

Total Inlet Interception Capacity (assumes clogged condition)

WARNING: Inlet Capacity less than Q Peak for Major Storm

	MINOR	MAJOR	
Type =	CDOT Type R Curb Opening		
a_{local} =	3.00	3.00	inches
No =	1	1	
Ponding Depth =	6.0	7.5	inches
	MINOR	MAJOR	<input checked="" type="checkbox"/> Override Depths
$L_o (G)$ =	N/A	N/A	feet
W_o =	N/A	N/A	feet
A_{ratio} =	N/A	N/A	
$C_r (G)$ =	N/A	N/A	
$C_w (G)$ =	N/A	N/A	
$C_o (G)$ =	N/A	N/A	
	MINOR	MAJOR	
$L_o (C)$ =	15.00	15.00	feet
H_{vert} =	6.00	6.00	inches
H_{throat} =	6.00	6.00	inches
Theta =	63.40	63.40	degrees
W_p =	2.00	2.00	feet
$C_r (C)$ =	0.10	0.10	
$C_w (C)$ =	3.60	3.60	
$C_o (C)$ =	0.67	0.67	
	MINOR	MAJOR	
d_{Grate} =	N/A	N/A	ft
d_{Curb} =	0.33	0.46	ft
$RF_{Combination}$ =	0.57	0.71	
RF_{Curb} =	0.79	0.87	
RF_{Grate} =	N/A	N/A	
	MINOR	MAJOR	
Q_a =	9.7	17.3	cfs
$Q_{PEAK REQUIRED}$ =	9.3	20.6	cfs

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

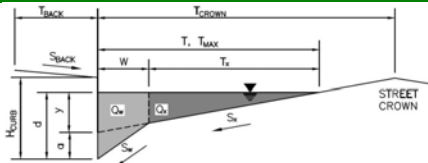
(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project:

FALCON MARKETPLACE

Inlet ID:

IC2

**Gutter Geometry (Enter data in the blue cells)**

Maximum Allowable Width for Spread Behind Curb

 $T_{BACK} = 7.0$ ft

Side Slope Behind Curb (leave blank for no conveyance credit behind curb)

 $S_{BACK} = 0.020$ ft/ft

Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

 $n_{BACK} = 0.020$

Height of Curb at Gutter Flow Line

 $H_{CURB} = 6.00$ inches

Distance from Curb Face to Street Crown

 $T_{CROWN} = 20.0$ ft

Gutter Width

 $W = 2.00$ ft

Street Transverse Slope

 $S_X = 0.020$ ft/ft

Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)

 $S_W = 0.083$ ft/ft

Street Longitudinal Slope - Enter 0 for sump condition

 $S_O = 0.000$ ft/ft

Manning's Roughness for Street Section (typically between 0.012 and 0.020)

 $n_{STREET} = 0.013$

Max. Allowable Spread for Minor & Major Storm

	Minor Storm	Major Storm	
$T_{MAX} =$	20.0	20.0	ft
$d_{MAX} =$	6.0	7.5	inches

Max. Allowable Depth at Gutter Flowline for Minor & Major Storm

Allow Flow Depth at Street Crown (leave blank for no)

☐ ☐ check = yes

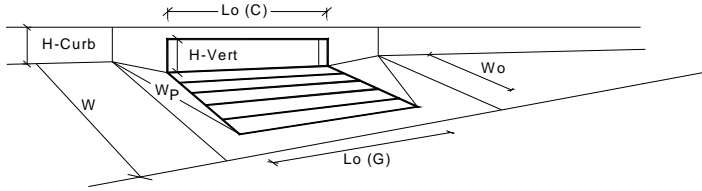
MINOR STORM Allowable Capacity is based on Depth Criterion

MAJOR STORM Allowable Capacity is based on Depth Criterion

	Minor Storm	Major Storm	
$Q_{allow} =$	SUMP	SUMP	cfs

INLET IN A SUMP OR SAG LOCATION

Version 4.04 Released November 2016



Design Information (Input)

Type of Inlet

Local Depression (additional to continuous gutter depression 'a' from 'Q-Allow')

Number of Unit Inlets (Grate or Curb Opening)

Water Depth at Flowline (outside of local depression)

Grate Information

Length of a Unit Grate

Width of a Unit Grate

Area Opening Ratio for a Grate (typical values 0.15-0.90)

Clogging Factor for a Single Grate (typical value 0.50 - 0.70)

Grate Weir Coefficient (typical value 2.15 - 3.60)

Grate Orifice Coefficient (typical value 0.60 - 0.80)

Curb Opening Information

Length of a Unit Curb Opening

Height of Vertical Curb Opening in Inches

Height of Curb Orifice Throat in Inches

Angle of Throat (see USDCM Figure ST-5)

Side Width for Depression Pan (typically the gutter width of 2 feet)

Clogging Factor for a Single Curb Opening (typical value 0.10)

Curb Opening Weir Coefficient (typical value 2.3-3.7)

Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)

Low Head Performance Reduction (Calculated)

Depth for Grate Midwidth

Depth for Curb Opening Weir Equation

Combination Inlet Performance Reduction Factor for Long Inlets

Curb Opening Performance Reduction Factor for Long Inlets

Grated Inlet Performance Reduction Factor for Long Inlets

Total Inlet Interception Capacity (assumes clogged condition)

Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)

	MINOR	MAJOR	
Type =	CDOT Type R Curb Opening		
a_{local} =	3.00	3.00	inches
No =	1	1	
Ponding Depth =	6.0	6.3	inches
	MINOR	MAJOR	Override Depths
$L_o (G)$ =	N/A	N/A	feet
W_o =	N/A	N/A	feet
A_{ratio} =	N/A	N/A	
$C_r (G)$ =	N/A	N/A	
$C_w (G)$ =	N/A	N/A	
$C_o (G)$ =	N/A	N/A	
	MINOR	MAJOR	
$L_o (C)$ =	10.00	10.00	feet
H_{vert} =	6.00	6.00	inches
H_{throat} =	6.00	6.00	inches
Theta =	63.40	63.40	degrees
W_p =	2.00	2.00	feet
$C_r (C)$ =	0.10	0.10	
$C_w (C)$ =	3.60	3.60	
$C_o (C)$ =	0.67	0.67	
	MINOR	MAJOR	
d_{Grate} =	N/A	N/A	ft
d_{Curb} =	0.33	0.36	ft
$RF_{Combination}$ =	0.57	0.60	
RF_{Curb} =	0.93	0.95	
RF_{Grate} =	N/A	N/A	
	MINOR	MAJOR	
Q_a =	8.3	9.4	cfs
$Q_{PEAK REQUIRED}$ =	0.4	5.7	cfs

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

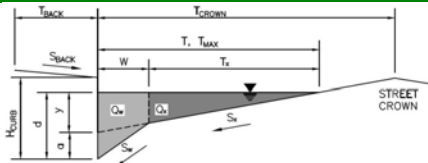
(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project:

FALCON MARKETPLACE

Inlet ID:

IC3

**Gutter Geometry (Enter data in the blue cells)**

Maximum Allowable Width for Spread Behind Curb

 $T_{BACK} = 7.0$ ft

Side Slope Behind Curb (leave blank for no conveyance credit behind curb)

 $S_{BACK} = 0.020$ ft/ft

Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

 $n_{BACK} = 0.020$

Height of Curb at Gutter Flow Line

 $H_{CURB} = 6.00$ inches

Distance from Curb Face to Street Crown

 $T_{CROWN} = 20.0$ ft

Gutter Width

 $W = 2.00$ ft

Street Transverse Slope

 $S_X = 0.020$ ft/ft

Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)

 $S_W = 0.083$ ft/ft

Street Longitudinal Slope - Enter 0 for sump condition

 $S_O = 0.000$ ft/ft

Manning's Roughness for Street Section (typically between 0.012 and 0.020)

 $n_{STREET} = 0.013$

Max. Allowable Spread for Minor & Major Storm

	Minor Storm	Major Storm	
$T_{MAX} =$	20.0	20.0	ft
$d_{MAX} =$	6.0	7.5	inches

Max. Allowable Depth at Gutter Flowline for Minor & Major Storm

Allow Flow Depth at Street Crown (leave blank for no)

☐ ☐ check = yes

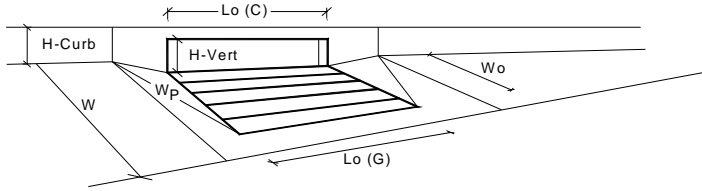
MINOR STORM Allowable Capacity is based on Depth Criterion

	Minor Storm	Major Storm	
$Q_{allow} =$	SUMP	SUMP	cfs

MAJOR STORM Allowable Capacity is based on Depth Criterion

INLET IN A SUMP OR SAG LOCATION

Version 4.04 Released November 2016



Design Information (Input)

Type of Inlet

Local Depression (additional to continuous gutter depression 'a' from 'Q-Allow')

Number of Unit Inlets (Grate or Curb Opening)

Water Depth at Flowline (outside of local depression)

Grate Information

Length of a Unit Grate

Width of a Unit Grate

Area Opening Ratio for a Grate (typical values 0.15-0.90)

Clogging Factor for a Single Grate (typical value 0.50 - 0.70)

Grate Weir Coefficient (typical value 2.15 - 3.60)

Grate Orifice Coefficient (typical value 0.60 - 0.80)

Curb Opening Information

Length of a Unit Curb Opening

Height of Vertical Curb Opening in Inches

Height of Curb Orifice Throat in Inches

Angle of Throat (see USDCM Figure ST-5)

Side Width for Depression Pan (typically the gutter width of 2 feet)

Clogging Factor for a Single Curb Opening (typical value 0.10)

Curb Opening Weir Coefficient (typical value 2.3-3.7)

Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)

Low Head Performance Reduction (Calculated)

Depth for Grate Midwidth

Depth for Curb Opening Weir Equation

Combination Inlet Performance Reduction Factor for Long Inlets

Curb Opening Performance Reduction Factor for Long Inlets

Grated Inlet Performance Reduction Factor for Long Inlets

Total Inlet Interception Capacity (assumes clogged condition)

Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)

	MINOR	MAJOR	
Type =	CDOT Type R Curb Opening		
a _{local} =	3.00	3.00	inches
No =	1	1	
Ponding Depth =	6.0	6.3	inches
	MINOR	MAJOR	Override Depths
L _o (G) =	N/A	N/A	feet
W _o =	N/A	N/A	feet
A _{ratio} =	N/A	N/A	
C _r (G) =	N/A	N/A	
C _w (G) =	N/A	N/A	
C _o (G) =	N/A	N/A	
	MINOR	MAJOR	
L _o (C) =	10.00	10.00	feet
H _{vert} =	6.00	6.00	inches
H _{throat} =	6.00	6.00	inches
Theta =	63.40	63.40	degrees
W _p =	2.00	2.00	feet
C _r (C) =	0.10	0.10	
C _w (C) =	3.60	3.60	
C _o (C) =	0.67	0.67	
	MINOR	MAJOR	
d _{Grate} =	N/A	N/A	ft
d _{Curb} =	0.33	0.36	ft
RF _{Combination} =	0.57	0.60	
RF _{Curb} =	0.93	0.95	
RF _{Grate} =	N/A	N/A	
	MINOR	MAJOR	
Q _a =	8.3	9.4	cfs
Q _{PEAK REQUIRED} =	2.1	3.7	cfs

DETENTION VOLUME BY THE FULL SPECTRUM METHOD

Project: _____

Basin ID: _____

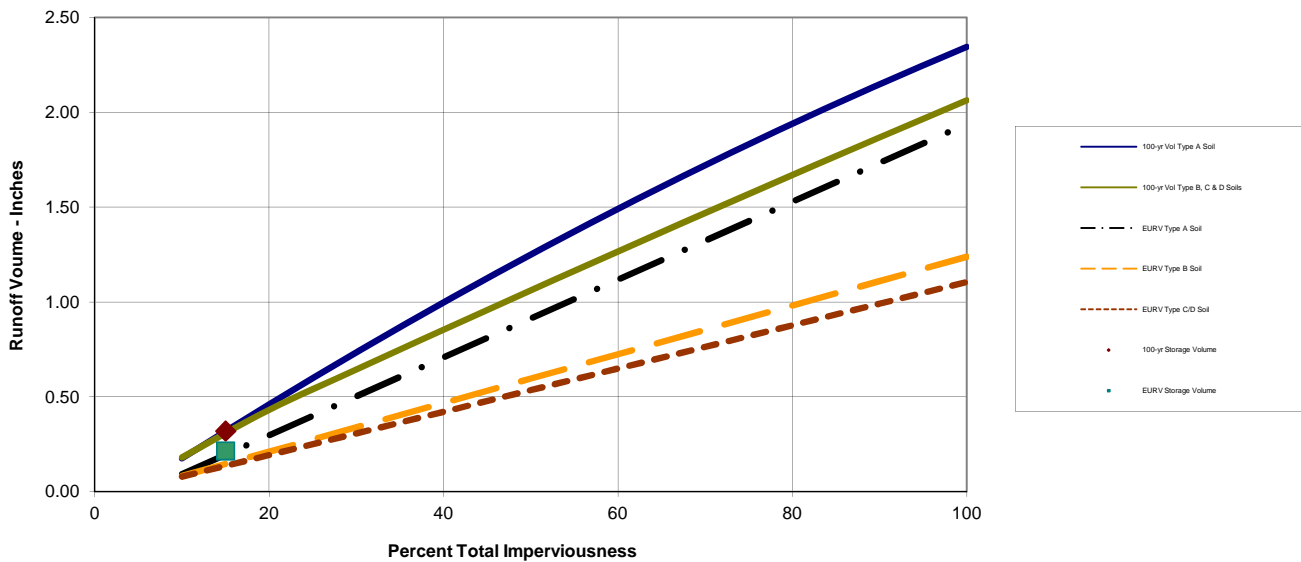
* User input data
shown in blue.

Area of Watershed (acres)	740.00	
Subwatershed Imperviousness	15.0%	
Level of Minimizing Directly Connected Impervious Area (MDCIA)	0	0 ▼
Effective Imperviousness ¹	15.0%	
Hydrologic Soil Type	Percentage of Area	Area (acres)
Type A	100.0%	740.0
Type B		0.0
Type C or D		0.0

Recommended Horton's Equation Parameters for CUHP		
Infiltration (inches per hour)		Decay Coefficient-- α
Initial-- f_i	Final-- f_o	
5	1.0	0.0007
Detention Volumes ^{2,5}		Maximum Allowable Release Rate, cfs ³
(watershed inches)	(acre-feet)	
0.22	13.30	Design Outlet to Empty EURV in 72 Hours
0.32	19.72	370.00

Excess Urban Runoff Volume⁴

100-year Detention Volume Including WQCV⁵



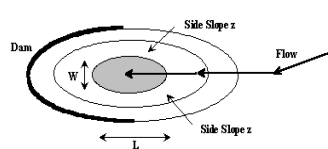
Notes:

- 1) Effective imperviousness is based on Figure ND-1 of the Urban Storm Drainage Criteria Manual (USDCM).
- 2) Results shown reflect runoff reduction from Level 1 or 2 MDCIA and are plotted at the watershed's total imperviousness value; the impact of MDCIA is reflected by the results being below the curves.
- 3) Maximum allowable release rates for 100-year event are based on Table SO-1. Outlet for the Excess Urban Runoff Volume (EURV) to be designed to empty out the EURV in 72 hours. Outlet design is similar to one for the WQCV outlet of an extended detention basin (i.e., perforated plate with a micro-pool) and extends to top of EURV water surface elevation.
- 4) EURV approximates the difference between developed and pre-developed runoff volume.
- 5) 100-yr detention volume includes EURV. No need to add more volume for WQCV or EURV

STAGE-STORAGE SIZING FOR DETENTION BASINS	
---	--

Project: FALCON MARKETPLACE

Basin ID: NORTH POND #1



Design Information (Input): _____ **Check Basin Shape** _____

Design Information (Input)		Select Basin Shape	
Width of Basin Bottom, W =	<input type="text"/> ft	Right Triangle	OR...
Length of Basin Bottom, L =	<input type="text"/> ft	Isosceles Triangle	OR...
Dam Side-slope (H:V), Z _d =	<input type="text"/> ft/ft	Rectangle	OR...

Check Basin Shape

Shape		
Right Triangle		OR...
Isosceles Triangle		OR...
Rectangle		OR...
Circle / Ellipse		OR...
Irregular		(Use Override values in cells G32:G52)

Stage-Storage Relationship:	Storage Requirement from Sheet 'Moduled PAA':			acre-ft.
	Storage Requirement from Sheet 'Hydrograph':			acre-ft.

	MINOR	MAJOR	
Storage Requirement from Sheet 'Modified FAA':			acre-ft.
Storage Requirement from Sheet 'Hydrograph':			acre-ft.
Storage Requirement from Sheet 'Full-Spectrum':	13.30	19.72	acre-ft.

[illegible]

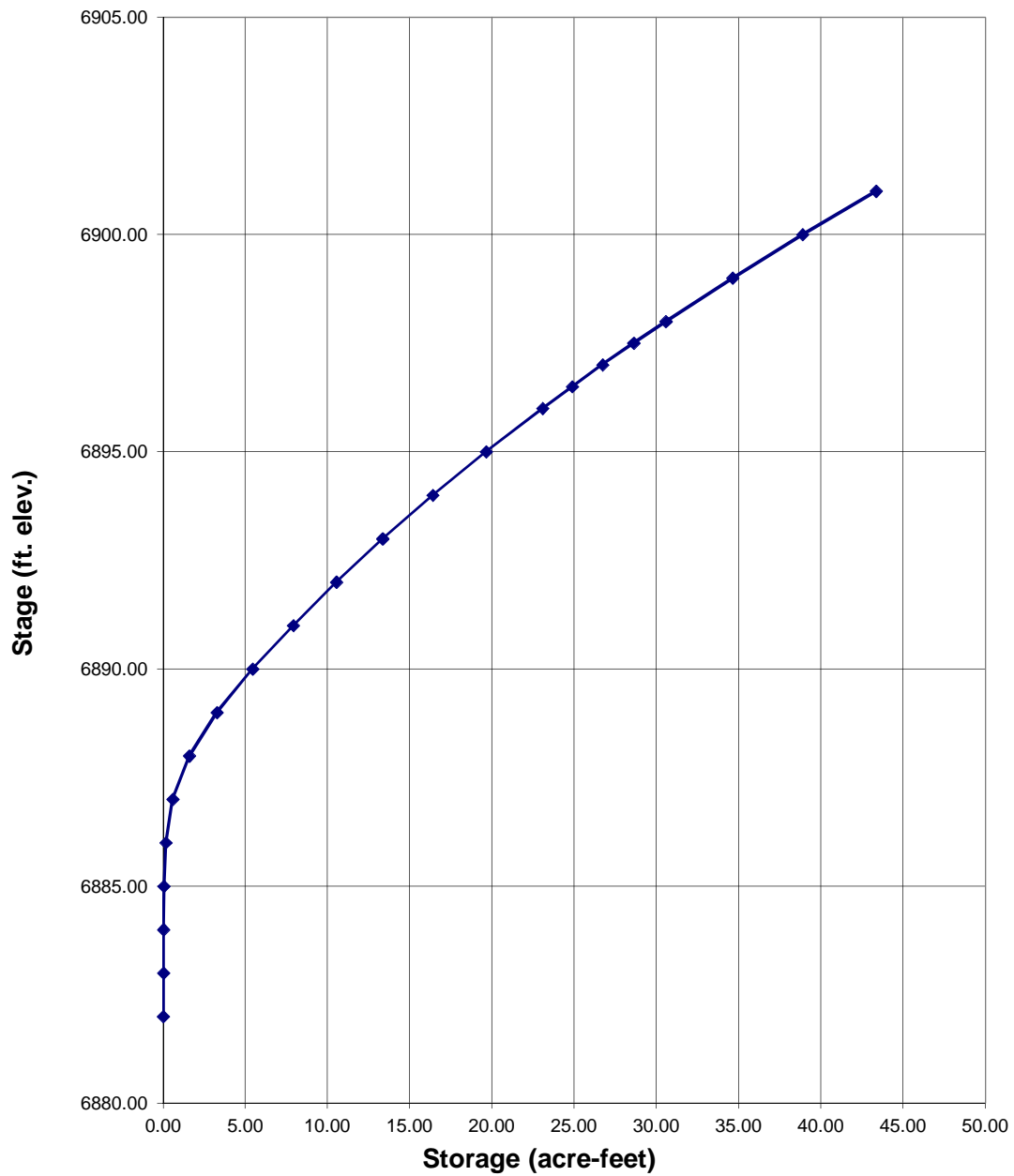
provide labels

STAGE-STORAGE SIZING FOR DETENTION BASINS

Project: _____

Basin ID: _____

STAGE-STORAGE CURVE FOR THE POND



STAGE-DISCHARGE SIZING OF THE WATER QUALITY CAPTURE VOLUME (WQCV) OUTLET	
--	--

Project: **FALCON MARKETPLACE**

Basin ID: **NORTH POND #1**

WQCV Design Volume (Input):

OR

Watershed Design Information (Input):

Perforated Plate Examples

Outlet Design Information (Output):

[illegible]

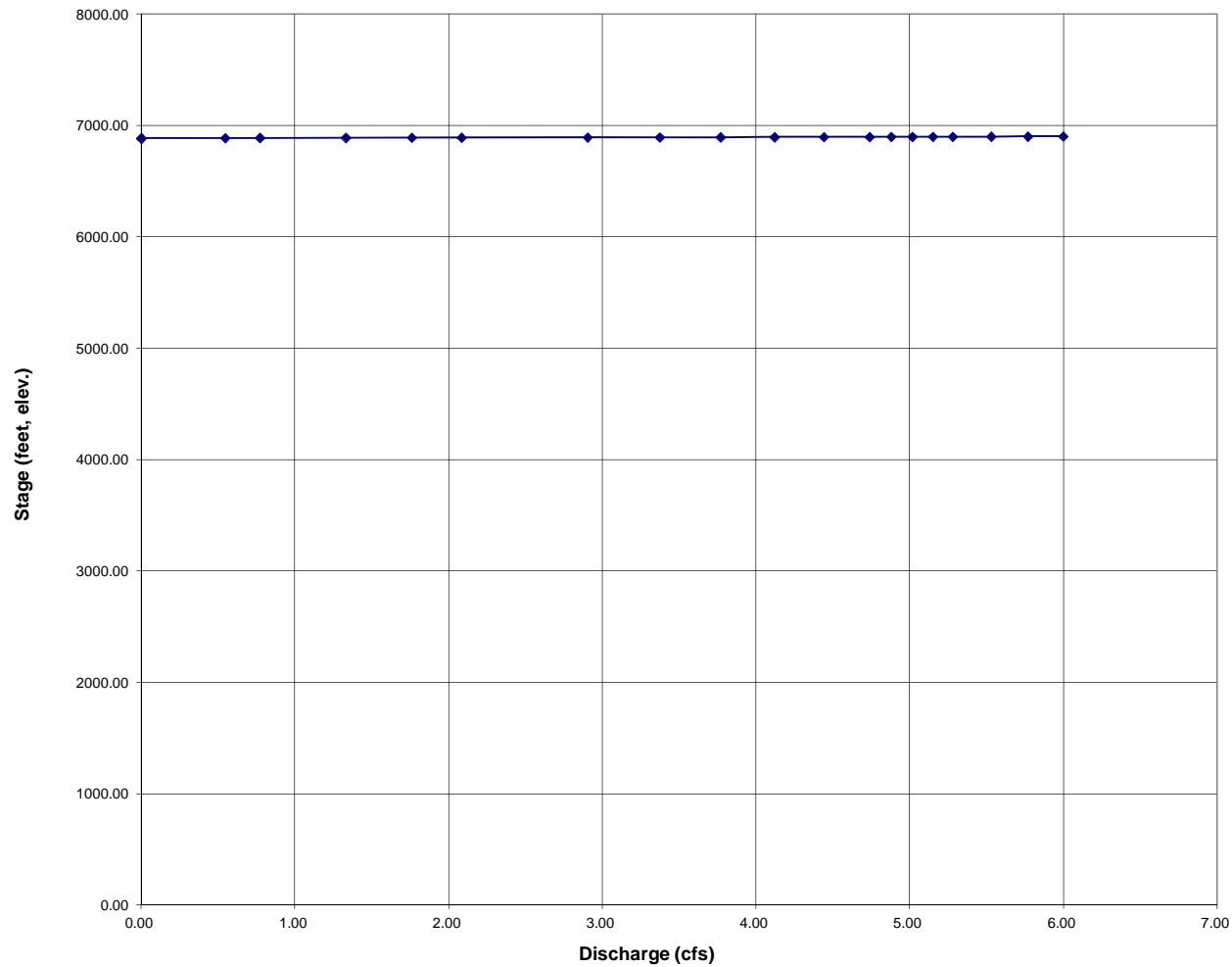
STAGE-DISCHARGE SIZING OF THE WATER QUALITY CAPTURE VOLUME (WQCV) OUTLET

Worksheet Protected

Project: **FALCON MARKETPLACE**

Basin ID: **NORTH POND #1**

STAGE-DISCHARGE CURVE FOR THE WQCV OUTLET STRUCTURE



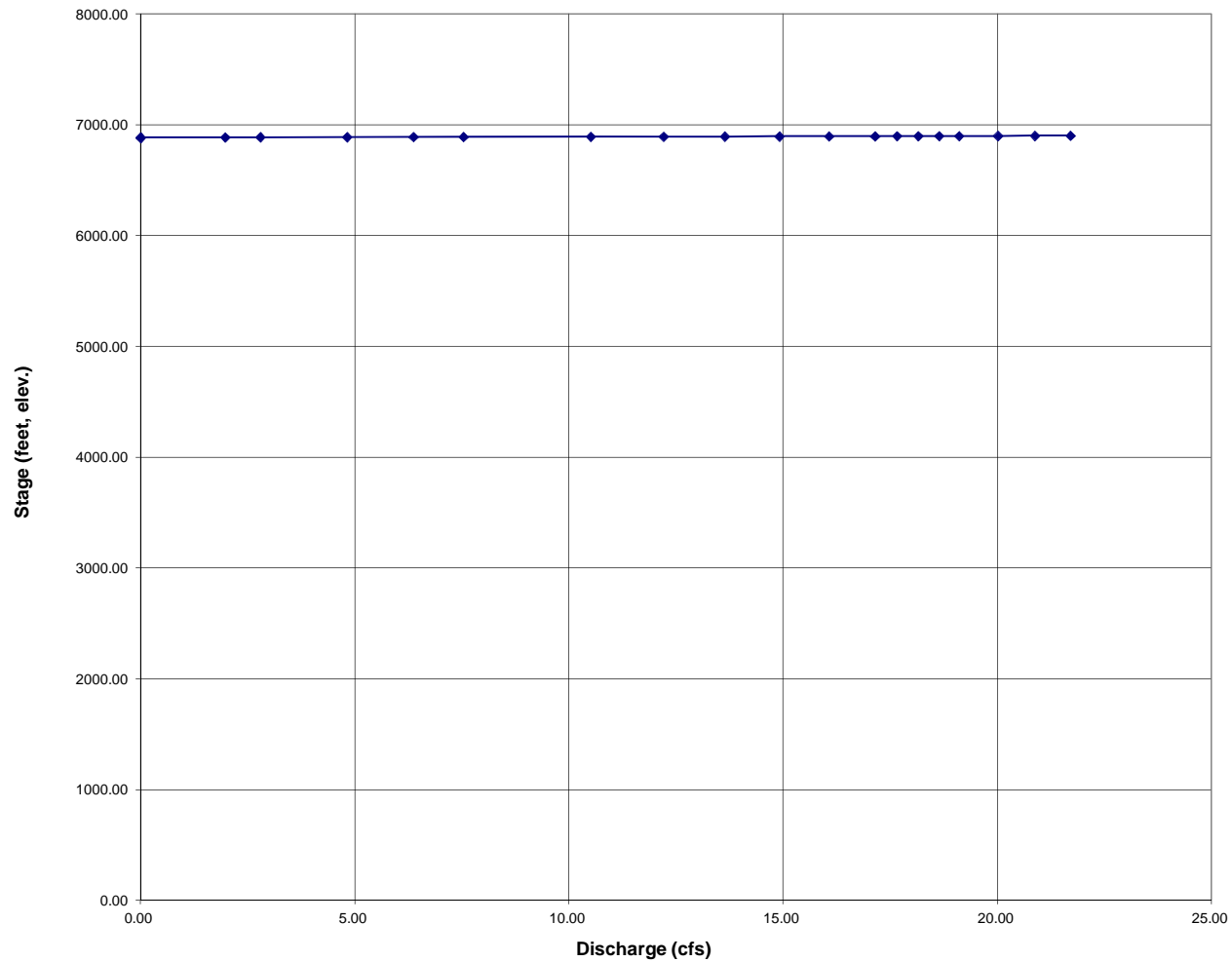
STAGE-DISCHARGE SIZING OF THE WATER QUALITY CAPTURE VOLUME (WQCV) OUTLET

Worksheet Protected

Project: **FALCON MARKETPLACE**

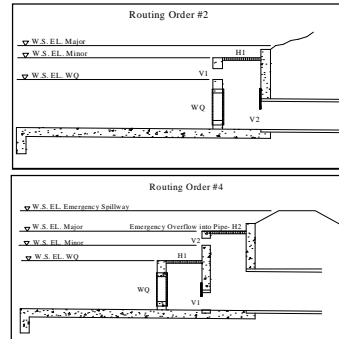
Basin ID: **NORTH POND #1**

STAGE-DISCHARGE CURVE FOR THE WQCV OUTLET STRUCTURE



STAGE-DISCHARGE SIZING OF THE WEIRS AND ORIFICES (INLET CONTROL)

Project: Falcon Marketplace #1
Basin ID: NORTH POND #1



Design Information (Input):

	#1 Horiz.	#2 Horiz.	#1 Vert.	#2 Vert.	
Dia. =			96.00		inches
W =	8.00				ft.
L or H =	12.00				ft.
% open =	80		100		%
C _o =	0.75		0.75		
C _w =	3.00				
E _o =	6893.80		6,881.97		ft.

Calculation of Collection Capacity:

$A_o = 76.80$ 50.27 sq. ft.
 $A_o =$ sq. ft.
 $L_w = 36.80$ ft.
 $L_w =$ ft.
 Top Elevation of Vertical Orifice Opening, Top = 6889.97 ft.
 Center Elevation of Vertical Orifice Opening, Cen = 6885.97 ft.

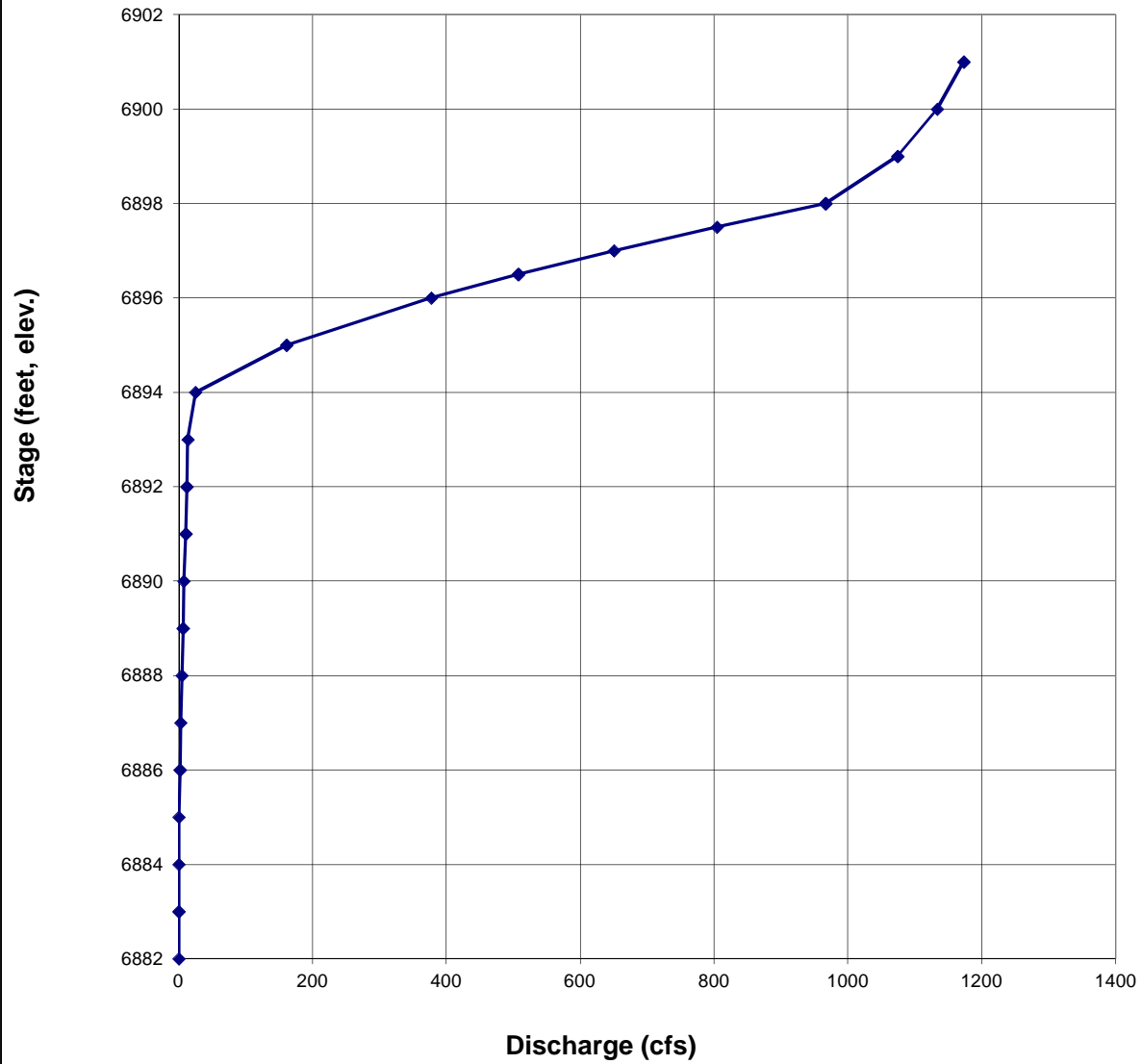
Routing 3: Single Stage - Water flows through WQCV plate and #1 horizontal opening into #1 vertical opening. This flow will be applied to culvert sheet (#2 vertical & horizontal openings is not used).

[illegible]

STAGE-DISCHARGE SIZING OF THE WEIRS AND ORIFICES (INLET CONTROL)

Project: Falcon Marketplace #1
Basin ID: NORTH POND #1

STAGE-DISCHARGE CURVE FOR THE OUTLET STRUCTURE



Project: **FALCON MARKETPLACE**
Basin ID: **NORTH POND #1**

D = 96 in
Grooved End with Headwall

Height (Rise) = ft
Width (Span) = ft
Square Edge w/ 90-15 deg. Flared Wingwall

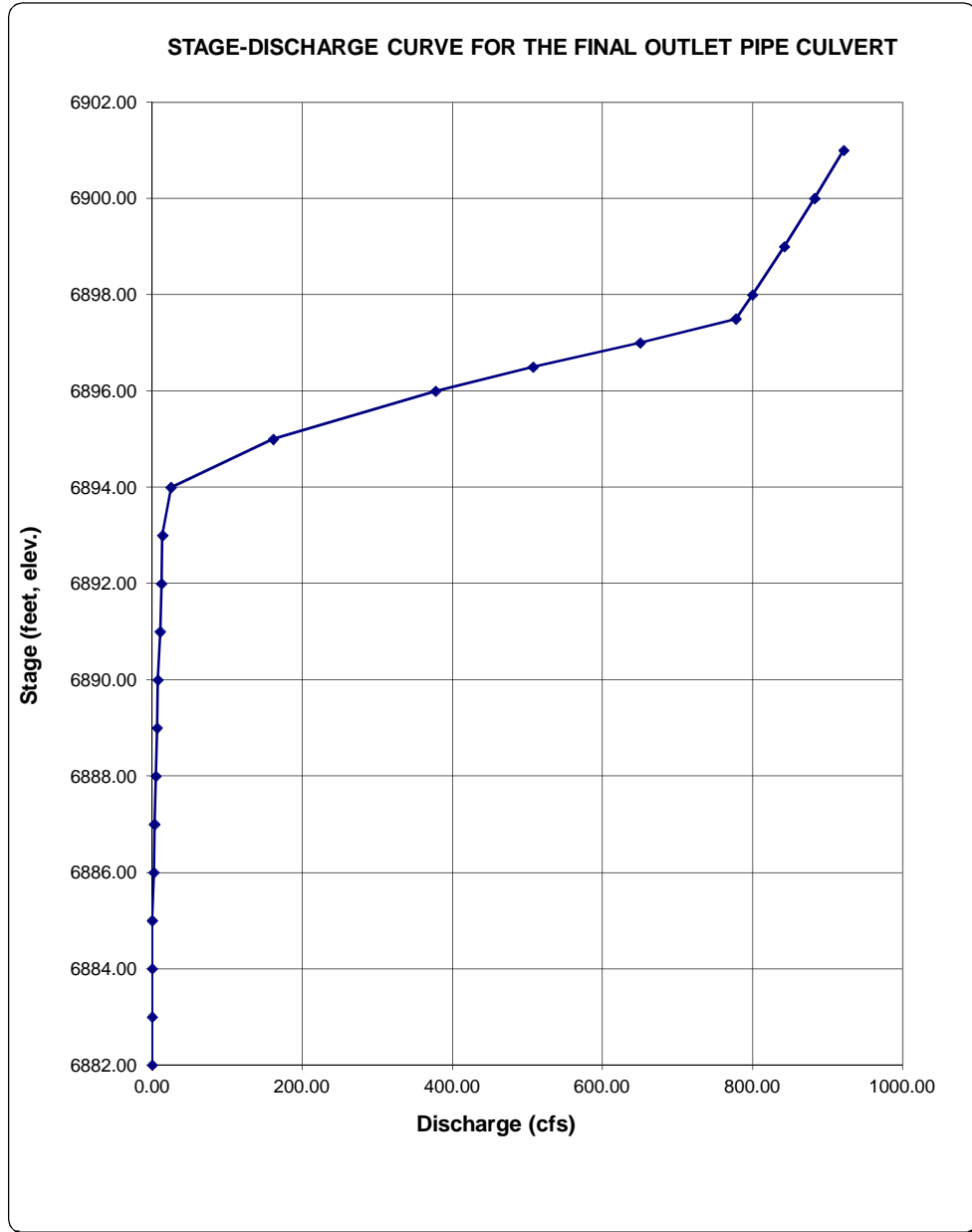
No =	1	
I_{elev} =	6881.97	ft. elev.
O_{elev} =	6880.85	ft. elev.
L =	78.0	ft.
n =	0.0120	
K_D =	0.00	
K_{s_k} =	1.00	

$K_g =$	0.20
$K_f =$	0.13
$K_s =$	1.33
$C_d =$	0.99
$KE_{low} =$	-0.04

[illegible]

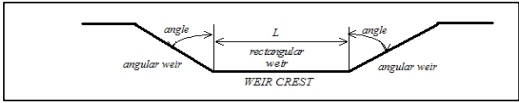
STAGE-DISCHARGE SIZING OF THE OUTLET CULVERT (INLET vs. OUTLET CONTROL WITH TAILWATER EFFECTS)

Project: FALCON MARKETPLACE
Basin ID: NORTH POND #1



STAGE-DISCHARGE SIZING OF THE SPILLWAY

Basin ID: NORTH POND #1



Design Information (input):

Bottom Length of Weir
Angle of Side Slope Weir
Elev. for Weir Crest
Coef. for Rectangular Weir
Coef. for Trapezoidal Weir

L =	160.00	feet
Angle =	75.96	degrees
EL. Crest =	6,898.00	feet
C _w =		
C _t =	3.50	

Calculation of Spillway Capacity (output):

[illegible]

PROJECT INFORMATION

PROJECT: Falcon Marketplace
PROJECT NO: 20988-00CSCV
DESIGN BY: KGV
REV. BY: TDM
AGENCY: El Paso County
REPORT TYPE: Preliminary
DATE: 6/19/2017



Drexel, Barrell & Co.

SPILLWAY CALCULATIONS

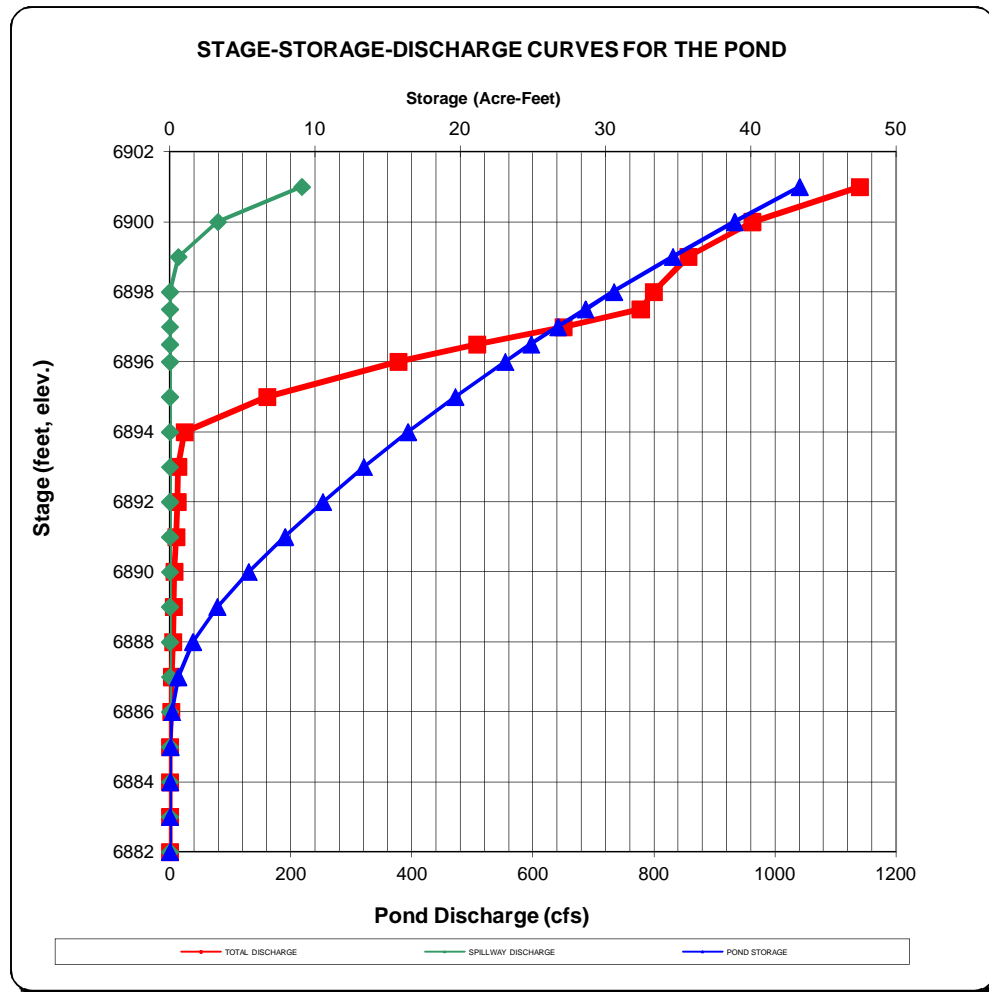
$$Q = CL(H^{2/3})$$

Weir coefficient C: 3.5
Depth H, ft: 1.5
Flowrate Q, cfs: 1016

Required L, ft: 158.01

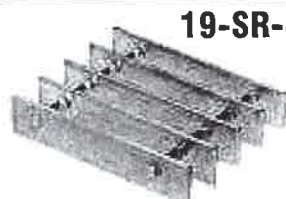
STAGE-DISCHARGE SIZING OF THE SPILLWAY

Project: FALCON MARKETPLACE
Basin ID: NORTH POND #1

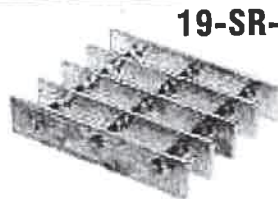


TRASH RACK GRATE
AT FRONT OF BOX

RECTANGULAR BAR SWAGE-LOCKED 1-3/16" C/C Bearing Bars

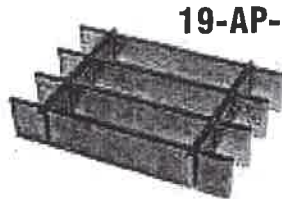


Cross Rods 4" C/C

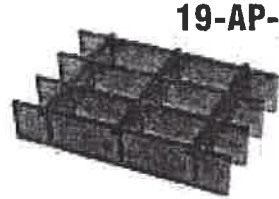


Cross Rods 2" C/C

PRESS-LOCKED 1-3/16" C/C Bearing Bars



Cross Bars 4" C/C



Cross Bars 2" C/C

NON-SERRATED & SERRATED

LOAD & DEFLECTION TABLE

Bar Size	Symbol	Approx. Wt./psf	Sec. Mod Per Ft. Of Width	SPAN (Direction of Bearing Bar)															
				24"	30"	36"	42"	48"	54"	60"	66"	72"	78"	84"	96"	108"			
3/4" x 1/8"	19-SR-4	1.4	0.118	U	237	152	105	77											
	19-SR-2	1.6		D	0.192	0.300	0.432	0.588											
	19-AP-4	1.5		C	237	189	158	135.											
	19-AP-2	1.8		D	0.154	0.240	0.346	0.470											
3/4" x 3/16"	19-SR-4	1.9	0.178	U	355	227	158	116											
	19-SR-2	2.1		D	0.192	0.300	0.432	0.588											
	19-AP-4	2.2		C	355	284	237	203											
	19-AP-2	2.7		D	0.154	0.240	0.346	0.470	48"										
1" x 1/8"	19-SR-4	1.7	0.211	U	421	269	187	137	105										
	19-SR-2	1.9		D	0.144	0.225	0.324	0.441	0.576										
	19-AP-4	1.8		C	421	337	281	241	211										
	19-AP-2	2.2		D	0.115	0.180	0.259	0.353	0.461	54"									
1" x 3/16"	19-SR-4	2.5	0.316	U	632	404	281	206	158	125									
	19-SR-2	2.7		D	0.144	0.225	0.324	0.441	0.576	0.729									
	19-AP-4	2.8		C	632	505	421	361	316	281									
	19-AP-2	3.3		D	0.115	0.180	0.259	0.353	0.461	0.583									
1-1/4" x 1/8"	19-SR-4	2.1	0.329	U	658	421	292	215	164	130									
	19-SR-2	2.3		D	0.115	0.180	0.259	0.353	0.461	0.583									
	19-AP-4	2.4		C	658	526	439	376	329	292									
	19-AP-2	2.8		D	0.092	0.144	0.207	0.282	0.369	0.467	60"								
1-1/4" x 3/16"	19-SR-4	3.1	0.493	U	987	632	439	322	247	195	158								
	19-SR-2	3.3		D	0.115	0.180	0.259	0.353	0.461	0.583	0.720								
	19-AP-4	3.5		C	987	789	658	564	493	439	395								
	19-AP-2	4.2		D	0.092	0.144	0.207	0.282	0.369	0.467	0.576								
1-1/2" x 1/8"	19-SR-4	2.5	0.474	U	947	606	421	309	237	187	152								
	19-SR-2	2.7		D	0.096	0.150	0.216	0.294	0.384	0.486	0.600								
	19-AP-4	2.8		C	947	758	632	541	474	421	379								
	19-AP-2	3.2		D	0.077	0.120	0.173	0.235	0.307	0.389	0.480	66"							
1-1/2" x 3/16"	19-SR-4	3.7	0.711	U	1421	909	632	464	355	281	227	188							
	19-SR-2	3.9		D	0.096	0.150	0.216	0.294	0.384	0.486	0.600	0.726							
	19-AP-4	4.1		C	1421	1137	947	812	711	632	568	517							
	19-AP-2	4.8		D	0.077	0.120	0.173	0.235	0.307	0.389	0.480	0.581	72"	78"					
1-3/4" x 3/16"	19-SR-4	4.2	0.967	U	1934	1238	860	632	484	382	309	256	215	183					
	19-SR-2	4.4		D	0.082	0.129	0.185	0.252	0.329	0.417	0.514	0.622	0.741	0.869					
	19-AP-4	4.7		C	1934	1547	1289	1105	967	860	774	703	645	595	545				
	19-AP-2	5.3		D	0.066	0.103	0.148	0.202	0.263	0.333	0.411	0.498	0.592	0.695	0.819	84"			
2" x 3/16"	19-SR-4	4.8	1.263	U	2526	1617	1123	825	632	499	404	334	281	239	206				
	19-SR-2	5.0		D	0.072	0.113	0.162	0.221	0.288	0.365	0.450	0.545	0.648	0.761	0.882				
	19-AP-4	5.3		C	2526	2021	1684	1444	1263	1123	1011	919	842	777	722				
	19-AP-2	5.9		D	0.058	0.090	0.130	0.176	0.230	0.292	0.360	0.436	0.518	0.608	0.706	96"			
2-1/4" x 3/16"	19-SR-4	5.4	1.599	U	3197	2046	1421	1044	799	632	512	423	355	303	261	200			
	19-SR-2	5.6		D	0.064	0.100	0.144	0.196	0.256	0.324	0.400	0.484	0.576	0.676	0.784	1.024			
	19-AP-4	5.8		C	3197	2558	2132	1827	1599	1421	1279	1163	1066	984	914	799			
	19-AP-2	6.5		D	0.051	0.080	0.115	0.157	0.205	0.259	0.320	0.387	0.461	0.541	0.627	0.819	108"		
2-1/2" x 3/16"	19-SR-4	5.9	1.974	U	3947	2526	1754	1289	987	780	632	522	439	374	322	247	195		
	19-SR-2	6.1		D	0.058	0.090	0.130	0.176	0.230	0.292	0.360	0.436	0.518	0.608	0.706	0.922	1.166		
	19-AP-4	6.4		C	3947	3158	2632	2256	1974	1754	1579	1435	1316	1215	1128	987	877		
	19-AP-2	7.1		D	0.046	0.072	0.104	0.141	0.184	0.233	0.288	0.348	0.415	0.487	0.564	0.737	0.933		

U = uniform load, psf (page 1)

C = safe concentrated load, psf (page 1)

D = deflection, inches

E = modulus of elasticity, 10,000,000 psi

F = fiber stress, 12,000 psi

Material: ASTM B-221, 6063 or 6061

Deflection: Spans and loads to be applied shall not exceed 1/4" deflection under full load of 100 psf which provides pedestrian comfort. These can be used for other types of loads with engineering approval.

Serrated Bars: For serrated gratings deeper than that shown in the table.

General: Loads and deflections are based on static loading.

Finish: Mill finish unless otherwise specified.

FALCON MARK

15-FT Head x 62

U = safe uniform load, psf (page 93)

C = safe concentrated load, psf (page 93)

D = deflection, inches

E = modulus of elasticity, 10,000,000 psi

F = fiber stress, 12,000 psi

Material: ASTM B-221, 6063 or 6061

Deflection: Spans and loads to the right of the bold line exceed 1/4" deflection for uniform load of 100 psf which provides safe pedestrian comfort. These can be exceeded for other types of loads with engineer's approval.

Serrated Bars: For serrated grating, the depth of grating required for a specified load is 1/4" deeper than that shown in the table.

General: Loads and deflections are theoretical and based on static loading.

Finish: Mill finish unless otherwise specified.

FALCON MARKETPLACE

$$15\text{-FT Head} \times 62.4 = 936 \text{ psf}$$

SR/AP-19 PANEL WIDTH (inches)

No. of Bars	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16
1/8" Bar	1 ⁹ / ₁₆	2 ³ / ₄	3 ¹⁵ / ₁₆	5 ¹ / ₈	6 ⁵ / ₁₆	7 ¹ / ₂	8 ¹¹ / ₁₆	9 ⁷ / ₈	11 ¹ / ₁₆	12 ¹ / ₄	13 ⁷ / ₁₆	14 ⁵ / ₈	15 ¹³ / ₁₆	17	18 ³ / ₁₆
3/16" Bar	1 ⁵ / ₈	2 ¹³ / ₁₆	4	5 ³ / ₁₆	6 ³ / ₈	7 ⁹ / ₁₆	8 ³ / ₄	9 ¹⁵ / ₁₆	11 ¹ / ₈	12 ⁵ / ₁₆	13 ¹ / ₂	14 ¹¹ / ₁₆	15 ⁷ / ₈	17 ¹ / ₁₆	18 ¹ / ₄
No. of Bars	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
1/8" Bar	19 ³ / ₈	20 ⁹ / ₁₆	21 ³ / ₄	22 ¹⁵ / ₁₆	24 ¹ / ₈	25 ⁵ / ₁₆	26 ¹ / ₂	27 ¹¹ / ₁₆	28 ⁷ / ₈	30 ¹ / ₁₆	31 ¹ / ₄	32 ⁷ / ₁₆	33 ⁵ / ₈	34 ¹³ / ₁₆	36
3/16" Bar	19 ⁷ / ₁₆	20 ⁵ / ₈	21 ¹³ / ₁₆	23	24 ³ / ₁₆	25 ³ / ₈	26 ⁹ / ₁₆	27 ³ / ₄	28 ¹⁵ / ₁₆	30 ¹ / ₈	31 ⁵ / ₁₆	32 ¹ / ₂	33 ¹ / ₁₆	34 ⁷ / ₈	36 ¹ / ₁₆

Note: Includes 1/4" (1/8" each side) for extended cross rods on swage-locked (SR) and extended cross bars on press-locked (AP).

Flow depths entering Pond SR4

CLOMR

Min Ch El	6895.98
WS Elev	6898.75
Max flow depth (north)	2.8 ft

NORTHWEST SWALE

Assuming trapezoidal channelized flow at riprap entry

Q100	30.2 cfs
Width	8 ft
Side Slopes	5 :1
Slope	1.6 %
n	0.020

Calculated flow depth	0.5 ft
-----------------------	---------------

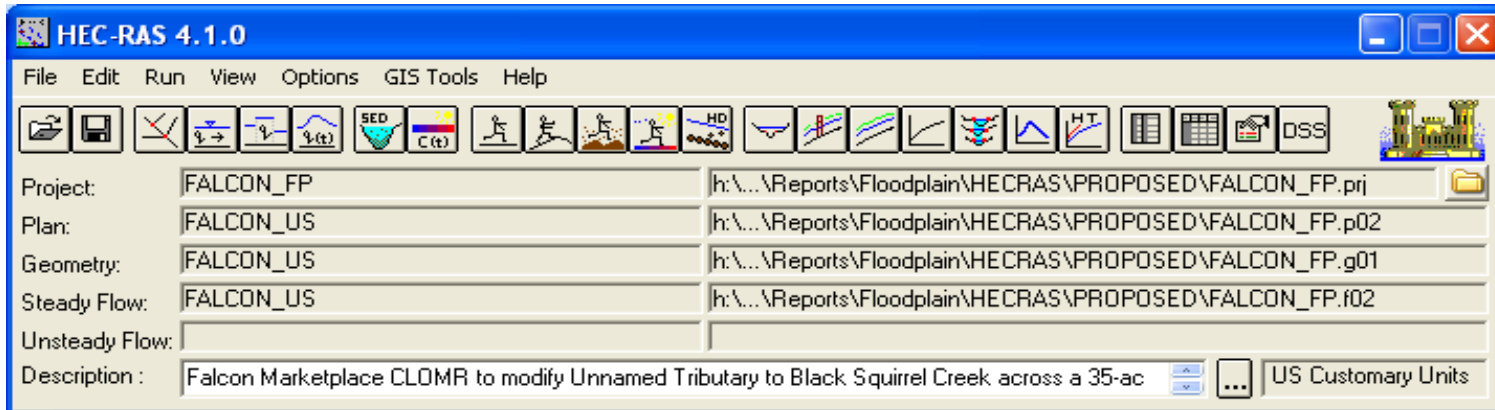
Project: Falcon Marketplace
Project No.: 20988-00

HEC-RAS Data Output

Proposed Conditions Model, North (Drexel Barrell Model)

File: H:\20988-00CSCV\Reports\Floodplain\HECRAS\PROPOSED\FALCON_FP.prj

Plan: FALCON_US



Date: 10/17/16
100-year Output, Standard Tabel 1
Cross Sections: 2926-2842

Reach	River Sta	Profile	Q Total (cfs)	Min Ch El (ft)	W.S. Elev (ft)	Crit W.S. (ft)	E.G. Elev (ft)	E.G. Slope (ft/ft)	Vel Chnl (ft/s)	Flow Area (sq ft)	Top Width (ft)	Froude #	
												Chl	
FALCON_US	2926	100-YR	1016	6895.98	6898.75	6898.75	6899.12	0.025538	6.71	306.22	403.31	0.91	
FALCON_US	2842	100-YR	1016	6888.58	6897	6889.37	6897	0.000001	0.15	6775.42	897.89	0.01	

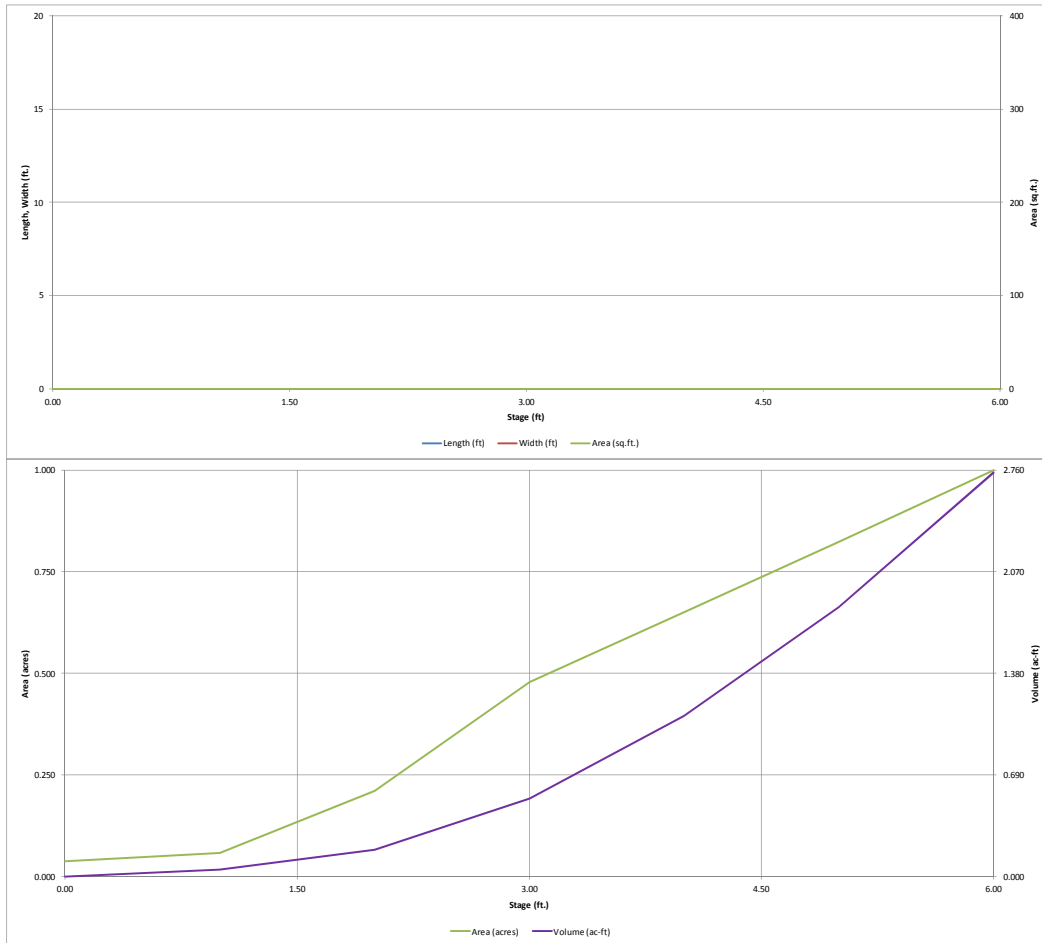
Drexel, Barrell Co.

H:\20988-00CSCV\Reports\Floodplain\CLOMR\Appendix 5 - HEC-RAS Modeling\parts\HEC-RAS Output 100YR_20988.xlsx

10/17/2016

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

UD-Detention, Version 3.07 (February 2017)

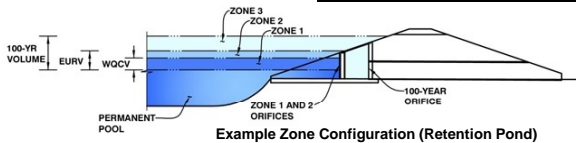


Detention Basin Outlet Structure Design

UD-Detention, Version 3.07 (February 2017)

Project: **Falcon Marketplace Pond #2**

Basin ID: _____



Example Zone Configuration (Retention Pond)

	Stage (ft)	Zone Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	3.38	0.718	Orifice Plate
Zone 2			Weir&Pipe (Circular)
Zone 3			
		0.718	Total

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth = ft (distance below the filtration media surface)
Underdrain Orifice Diameter = inches

Calculated Parameters for Underdrain

Underdrain Orifice Area = ft²
Underdrain Orifice Centroid = feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice = ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Orifice Plate = ft (relative to basin bottom at Stage = 0 ft)
Orifice Plate: Orifice Vertical Spacing = inches
Orifice Plate: Orifice Area per Row = sq. inches (diameter = 1-13/16 inches)

Calculated Parameters for Plate

WQ Orifice Area per Row = ft²
Elliptical Half-Width = feet
Elliptical Slot Centroid = feet
Elliptical Slot Area = ft²

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	1.20	2.40					
Orifice Area (sq. inches)	2.69	2.69	2.69					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

Invert of Vertical Orifice = ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Vertical Orifice = ft (relative to basin bottom at Stage = 0 ft)
Vertical Orifice Diameter = inches

Calculated Parameters for Vertical Orifice

Vertical Orifice Area = ft²
Vertical Orifice Centroid = feet

User Input: Overflow Weir (Dropbox) and Grate (Flat or Sloped)

	Zone 2 Weir	Not Selected	
Overflow Weir Front Edge Height, H _o =	3.38		ft (relative to basin bottom at Stage = 0 ft)
Overflow Weir Front Edge Length =	7.00		feet
Overflow Weir Slope =	0.00		H:V (enter zero for flat grate)
Horiz. Length of Weir Sides =	5.00		feet
Overflow Grate Open Area % =	70%		%, grate open area/total area
Debris Clogging % =	50%		%

Calculated Parameters for Overflow Weir

	Zone 2 Weir	Not Selected	
Height of Grate Upper Edge, H ₁ =	3.38		feet
Over Flow Weir Slope Length =	5.00		feet
Grate Open Area / 100-yr Orifice Area =	4.99		should be ≥ 4
Overflow Grate Open Area w/o Debris =	24.50		ft ²
Overflow Grate Open Area w/ Debris =	12.25		ft ²

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

	Zone 2 Circular	Not Selected	
Depth to Invert of Outlet Pipe =	0.00		ft (distance below basin bottom at Stage = 0 ft)
Circular Orifice Diameter =	30.00		inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate

	Zone 2 Circular	Not Selected	
Outlet Orifice Area =	4.91		ft ²
Outlet Orifice Centroid =	1.25		feet
Half-Central Angle of Restrictor Plate on Pipe =	N/A	N/A	radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage = ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length = feet
Spillway End Slopes = H:V
Freeboard above Max Water Surface = feet

Calculated Parameters for Spillway

Spillway Design Flow Depth = feet
Stage at Top of Freeboard = feet
Basin Area at Top of Freeboard = acres

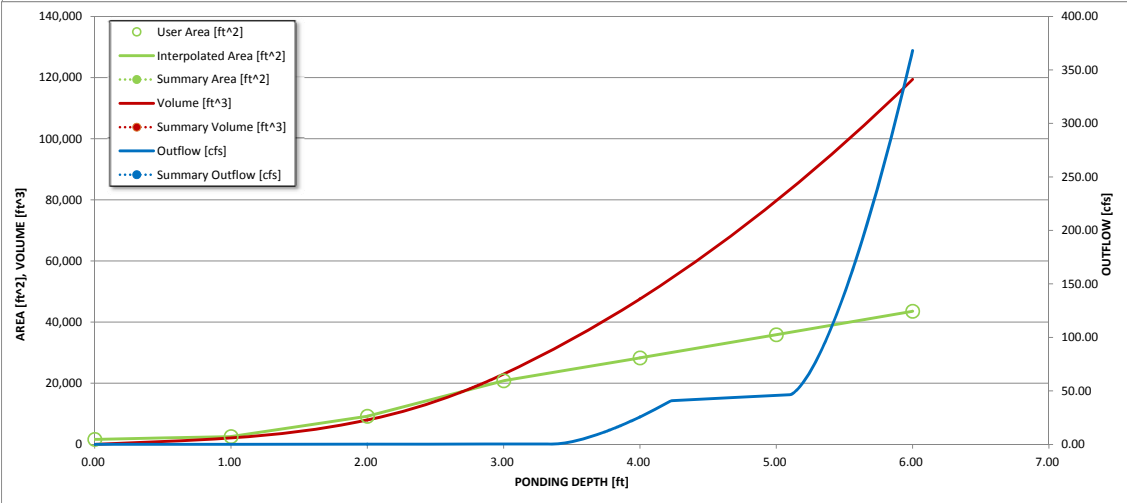
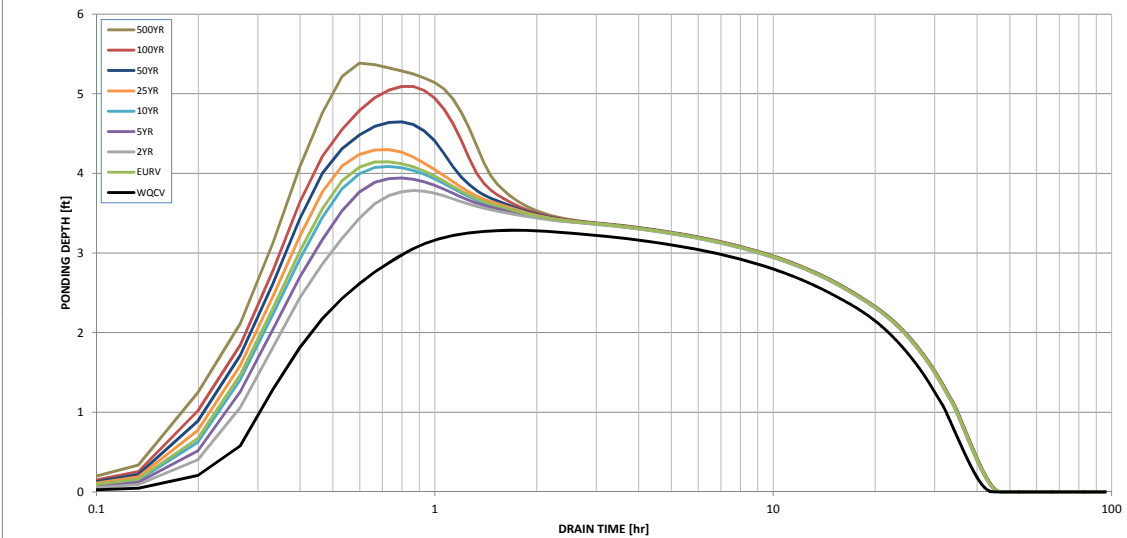
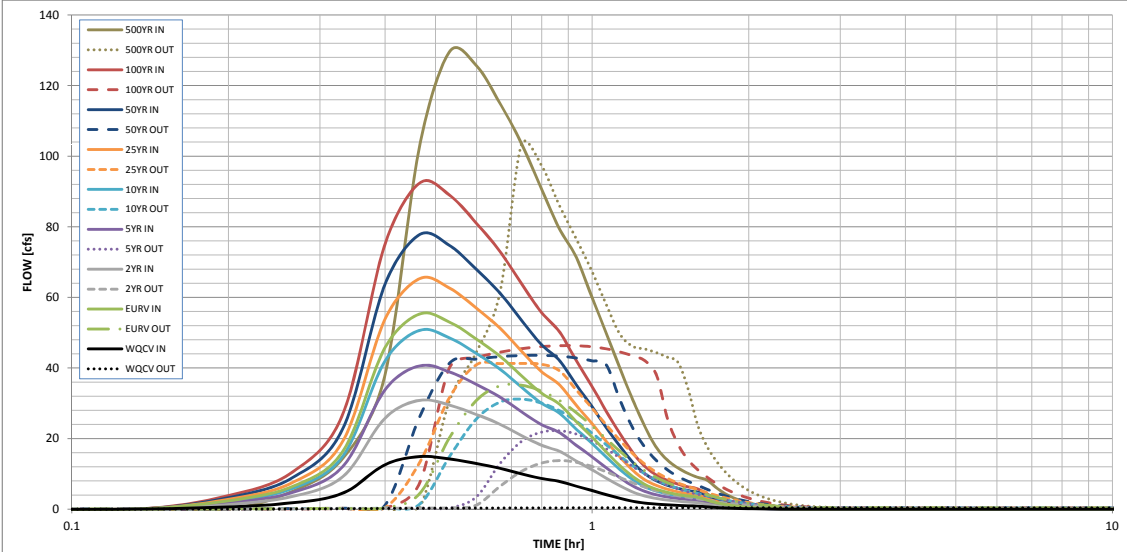
Routed Hydrograph Results

	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =									
One-Hour Rainfall Depth (in) =	0.53	1.07	0.95	1.22	1.48	1.86	2.19	2.54	3.46
Calculated Runoff Volume (acre-ft) =	0.718	2.706	1.498	1.979	2.476	3.204	3.826	4.561	6.456
OPTIONAL Override Runoff Volume (acre-ft) =									
Inflow Hydrograph Volume (acre-ft) =	0.717	2.703	1.496	1.976	2.473	3.200	3.821	4.556	6.445
Predevelopment Unit Peak Flow, q (cfs/acre) =	0.00	0.00	0.00	0.01	0.01	0.03	0.26	0.65	1.56
Predevelopment Peak Q (cfs) =	0.0	0.0	0.0	0.1	0.3	0.8	6.2	15.4	37.2
Peak Inflow Q (cfs) =	14.9	55.3	30.8	40.6	50.6	65.3	77.7	92.3	129.6
Peak Outflow Q (cfs) =	0.4	35.1	13.8	22.2	31.2	41.3	43.6	46.3	103.3
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	165.0	95.6	51.7	7.0	3.0	2.8
Structure Controlling Flow =	Plate	Overflow Grate 1	Overflow Grate 1	Overflow Grate 1	Overflow Grate 1	Outlet Plate 1	Outlet Plate 1	Outlet Plate 1	Spillway
Max Velocity through Grate 1 (fps) =	N/A	1.43	0.53	0.9	1.3	1.7	1.8	1.9	1.9
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	37	31	35	33	32	30	29	28	24
Time to Drain 99% of Inflow Volume (hours) =	40	38	40	39	37	36	35	35	33
Maximum Ponding Depth (ft) =	3.29	4.15	3.78	3.94	4.09	4.30	4.65	5.09	5.38
Area at Maximum Ponding Depth (acres) =	0.53	0.67	0.61	0.64	0.66	0.70	0.76	0.84	0.89
Maximum Volume Stored (acre-ft) =	0.669	1.185	0.954	1.054	1.145	1.288	1.544	1.904	2.155

The WQCV needs to be released over 40 hours with the EDB design.

Detention Basin Outlet Structure Design

UD-Detention, Version 3.07 (February 2017)



S-A-V-D Chart Axis Override	X-axis	Left Y-Axis	Right Y-Axis
minimum bound			
maximum bound			

Detention Basin Outlet Structure Design

UD-Detention, Version 3.07 (February 2017)

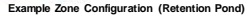
The user can create a summary S-A-V-D by entering the desired stage increments and the remainder of the table will populate automatically.

The user should graphically compare the summary S-A-V-D table to the full S-A-V-D table in the chart to confirm it captures all key transition points.

	Stage	Area	Area	Volume	Volume	Total
--	-------	------	------	--------	--------	-------

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DETENTION BASIN STAGE-STORAGE TABLE BUILDER

Basin ID: POND #3

Selected BMP Type =

Optional User Override
1-hr Precipitation

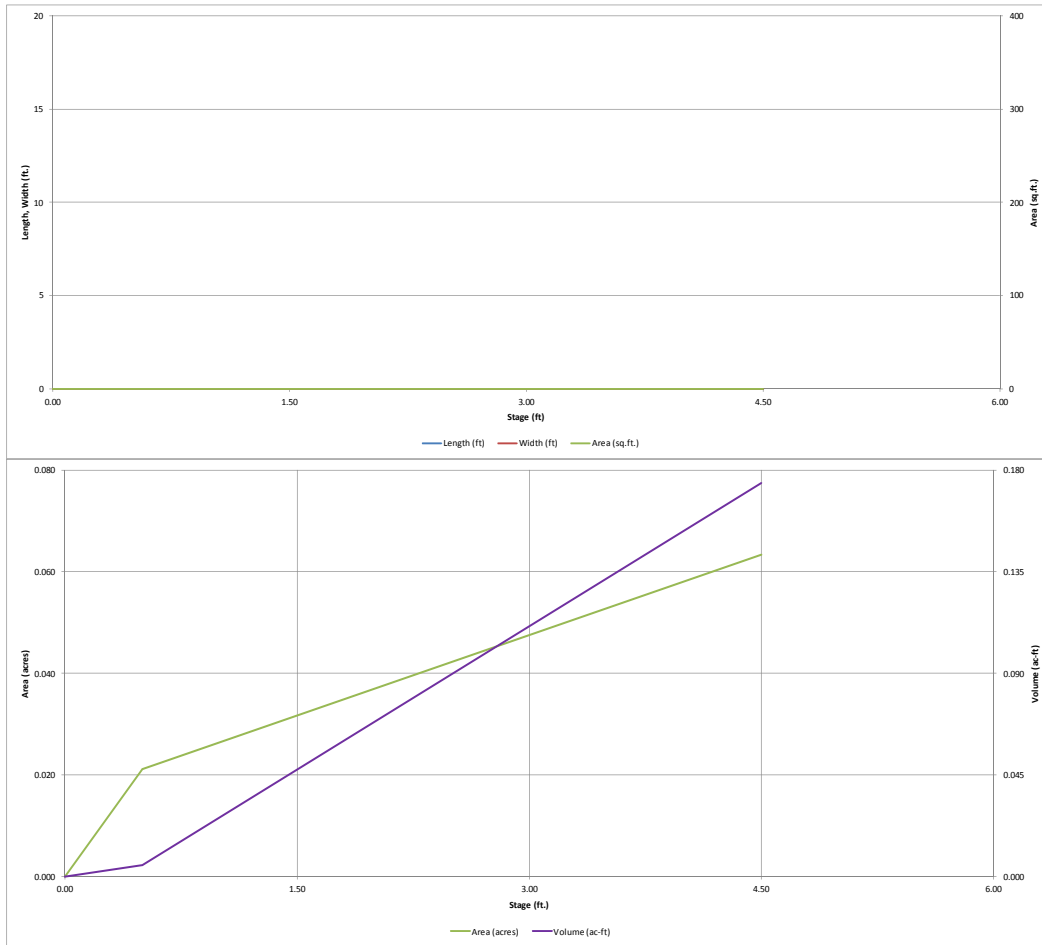
0.95	inches
1.22	inches
1.48	inches
1.86	inches
2.19	inches
2.54	inches
3.46	inches

Zone 1 Volume (WOCV) =	0.096	acre-feet
Zone 2 Volume (User Defined - Zone 1) =	0.015	acre-feet
Select Zone 3 Storage Volume (Optional) =		acre-feet
Total Detention Basin Volume =	0.111	acre-feet
Initial Surcharge Volume (ISV) =	user	ft ³
Initial Surcharge Depth (ISD) =	user	ft
Total Available Detention Depth (H_{total}) =	user	ft
Depth of Trickle Channel (H_{TC}) =	user	ft
Slope of Trickle Channel (S_{TC}) =	user	ft/ft
Slopes of Main Basin Sides (S_{main}) =	user	H:V
Basin Length-to-Width Ratio ($R_{L/W}$) =	user	

Total detention volume is less than 100-year volume.

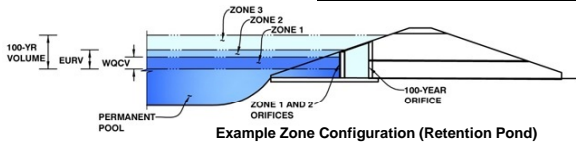
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DETENTION BASIN STAGE-STORAGE TABLE BUILDER



Detention Basin Outlet Structure Design

Project: **FALCON MARKETPLACE**
Basin ID: **POND #3**



Example Zone Configuration (Retention Pond)

	Stage (ft)	Zone Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	3.11	0.096	Orifice Plate
Zone 2 (User)	3.41	0.015	Weir&Pipe (Circular)
Zone 3			
		0.111	Total

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth = ft (distance below the filtration media surface)
Underdrain Orifice Diameter = inches

Calculated Parameters for Underdrain

Underdrain Orifice Area = ft²
Underdrain Orifice Centroid = feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice = ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Orifice Plate = ft (relative to basin bottom at Stage = 0 ft)
Orifice Plate: Orifice Vertical Spacing = inches
Orifice Plate: Orifice Area per Row = sq. inches (diameter = 3/4 inch)

Calculated Parameters for Plate

WQ Orifice Area per Row = ft²
Elliptical Half-Width = feet
Elliptical Slot Centroid = feet
Elliptical Slot Area = ft²

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	<input type="text" value="0.00"/>	<input type="text" value="1.04"/>	<input type="text" value="2.07"/>					
Orifice Area (sq. inches)	<input type="text" value="0.48"/>	<input type="text" value="0.48"/>	<input type="text" value="0.48"/>					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

Invert of Vertical Orifice = ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Vertical Orifice = ft (relative to basin bottom at Stage = 0 ft)
Vertical Orifice Diameter = inches

Calculated Parameters for Vertical Orifice

Vertical Orifice Area = ft²
Vertical Orifice Centroid = feet

User Input: Overflow Weir (Dropbox) and Grate (Flat or Sloped)

Overflow Weir Front Edge Height, H_o = ft (relative to basin bottom at Stage = 0 ft)
Overflow Weir Front Edge Length = feet
Overflow Weir Slope = H:V (enter zero for flat grate)
Horiz. Length of Weir Sides = feet
Overflow Grate Open Area % = %
Debris Clogging % = %

Calculated Parameters for Overflow Weir

Height of Grate Upper Edge, H₁ = feet
Over Flow Weir Slope Length = feet
Grate Open Area / 100-yr Orifice Area = should be ≥ 4
Overflow Grate Open Area w/o Debris = ft²
Overflow Grate Open Area w/ Debris = ft²

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

Depth to Invert of Outlet Pipe = ft (distance below basin bottom at Stage = 0 ft)
Circular Orifice Diameter = inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate

Outlet Orifice Area = ft²
Outlet Orifice Centroid = feet
Half-Central Angle of Restrictor Plate on Pipe = radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage = ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length = feet
Spillway End Slopes = H:V
Freeboard above Max Water Surface = feet

Calculated Parameters for Spillway

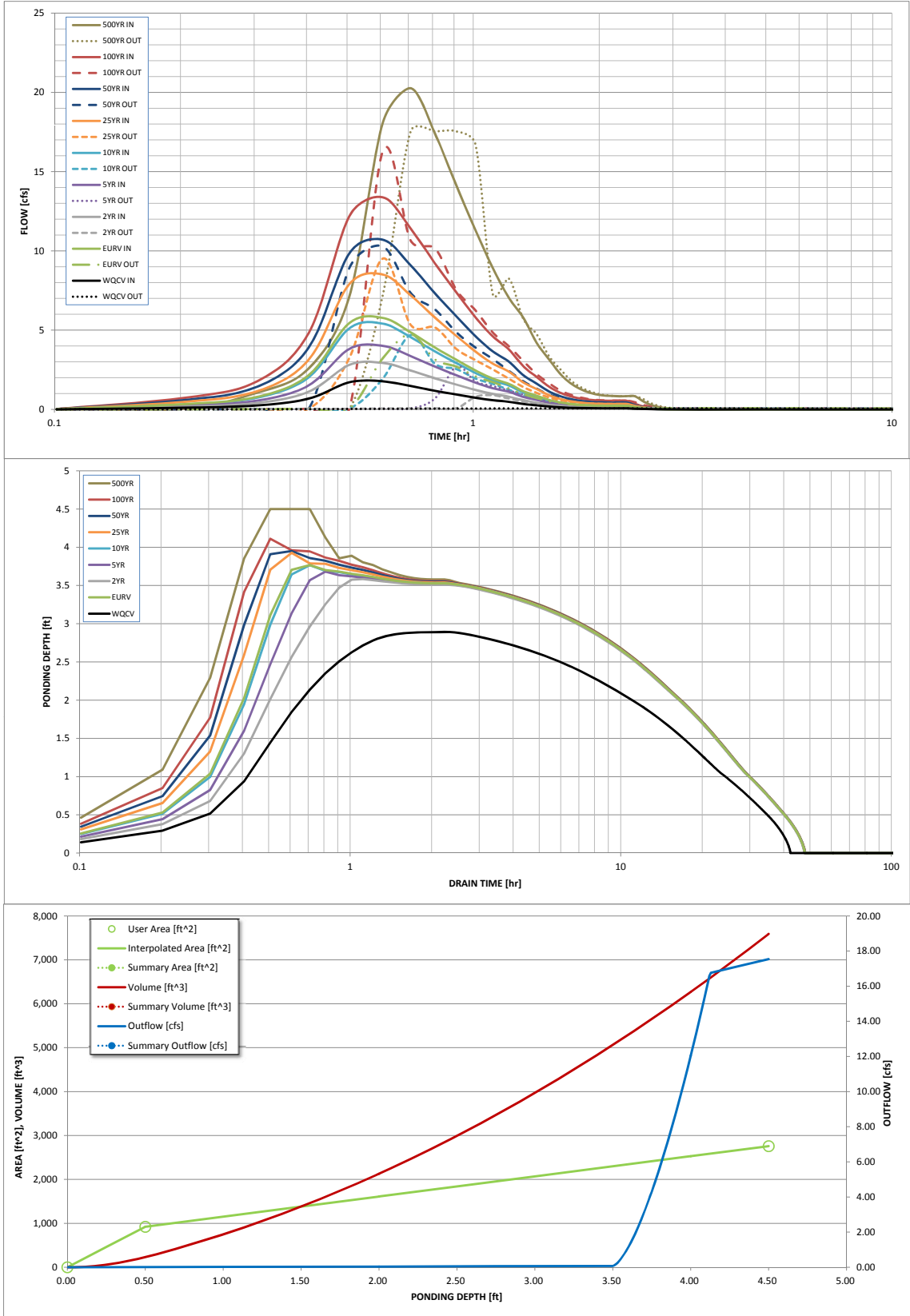
Spillway Design Flow Depth = feet
Stage at Top of Freeboard = feet
Basin Area at Top of Freeboard = acres

Routed Hydrograph Results

	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =	0.53	1.07	0.95	1.22	1.48	1.86	2.19	2.54	3.46
One-Hour Rainfall Depth (in) =	0.59	0.315	0.160	0.219	0.296	0.465	0.586	0.732	1.110
Calculated Runoff Volume (acre-ft) =									
OPTIONAL Override Runoff Volume (acre-ft) =									
Inflow Hydrograph Volume (acre-ft) =	0.096	0.315	0.159	0.218	0.295	0.464	0.585	0.732	1.109
Predevelopment Unit Peak Flow, q (cfs/acre) =	0.00	0.00	0.00	0.01	0.01	0.16	0.33	0.54	0.99
Predevelopment Peak Q (cfs) =	0.0	0.0	0.0	0.0	0.1	0.9	1.9	3.1	5.7
Peak Inflow Q (cfs) =	1.8	5.8	2.9	4.0	5.4	8.5	10.7	13.4	20.3
Peak Outflow Q (cfs) =	0.1	4.7	0.9	2.7	4.7	9.5	10.3	16.3	17.5
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	58.6	61.5	10.5	5.5	5.3	3.1
Structure Controlling Flow =	Plate	Overflow Grate 1	Overflow Grate 1	Overflow Grate 1	Overflow Grate 1	Overflow Grate 1	Overflow Grate 1	Overflow Grate 1	N/A
Max Velocity through Grate 1 (fps) =	N/A	0.44	0.07	0.2	0.4	0.9	0.9	1.5	1.6
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	38	36	41	39	37	33	30	27	22
Time to Drain 99% of Inflow Volume (hours) =	40	43	45	44	43	41	40	38	35
Maximum Ponding Depth (ft) =	2.89	3.77	3.58	3.68	3.77	3.93	3.95	4.11	4.50
Area at Maximum Ponding Depth (acres) =	0.05	0.06	0.05	0.05	0.06	0.06	0.06	0.06	0.06
Maximum Volume Stored (acre-ft) =	0.086	0.130	0.120	0.126	0.130	0.139	0.141	0.150	0.174

The WQCV needs to be released over 40 hours with the EDB design.

Detention Basin Outlet Structure Design



Detention Basin Outlet Structure Design

Summary Stage-Area-Volume-Discharge Relationships

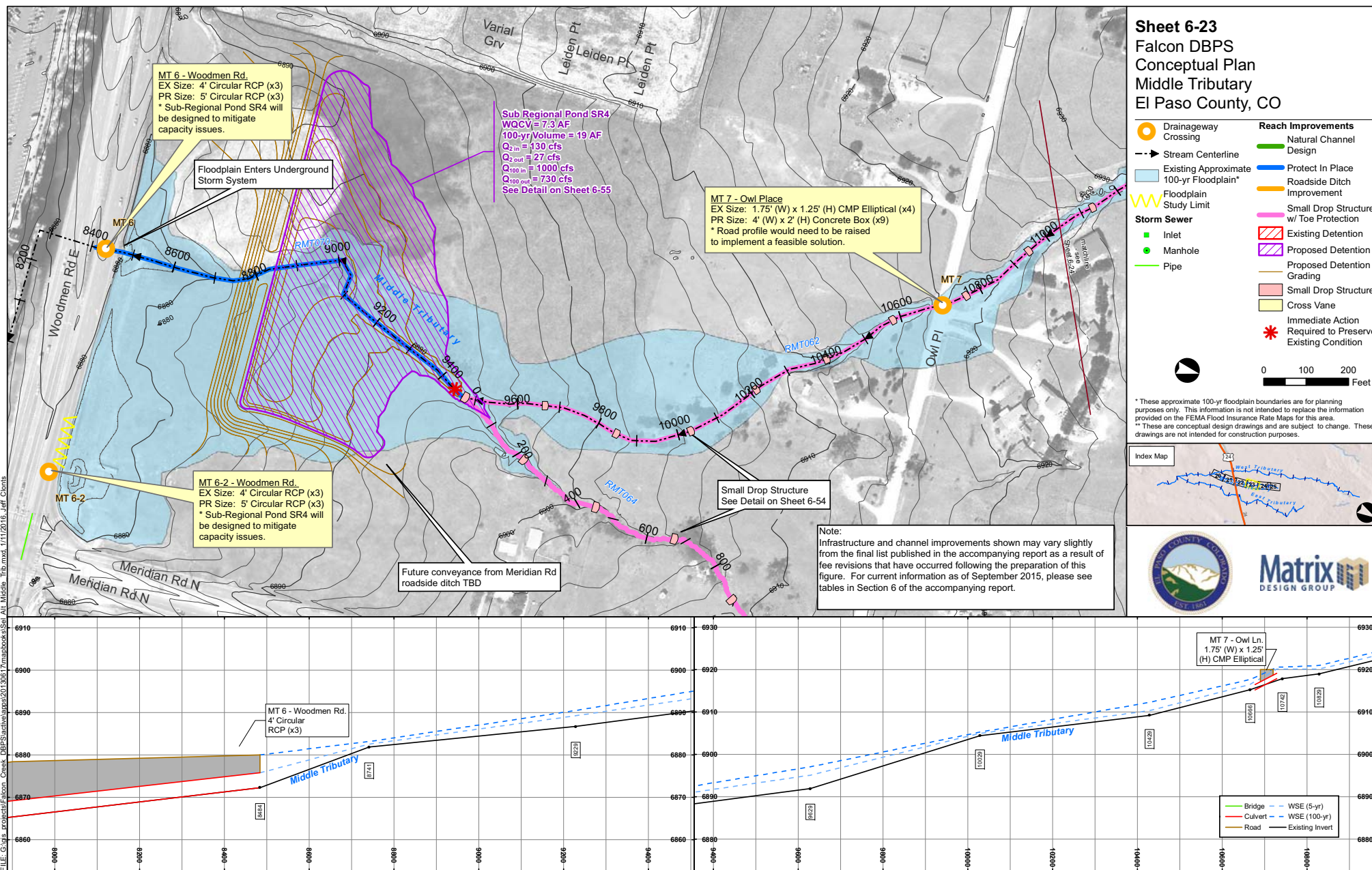
The user can create a summary S-A-V-D by entering the desired stage increments and the remainder of the table will populate automatically.

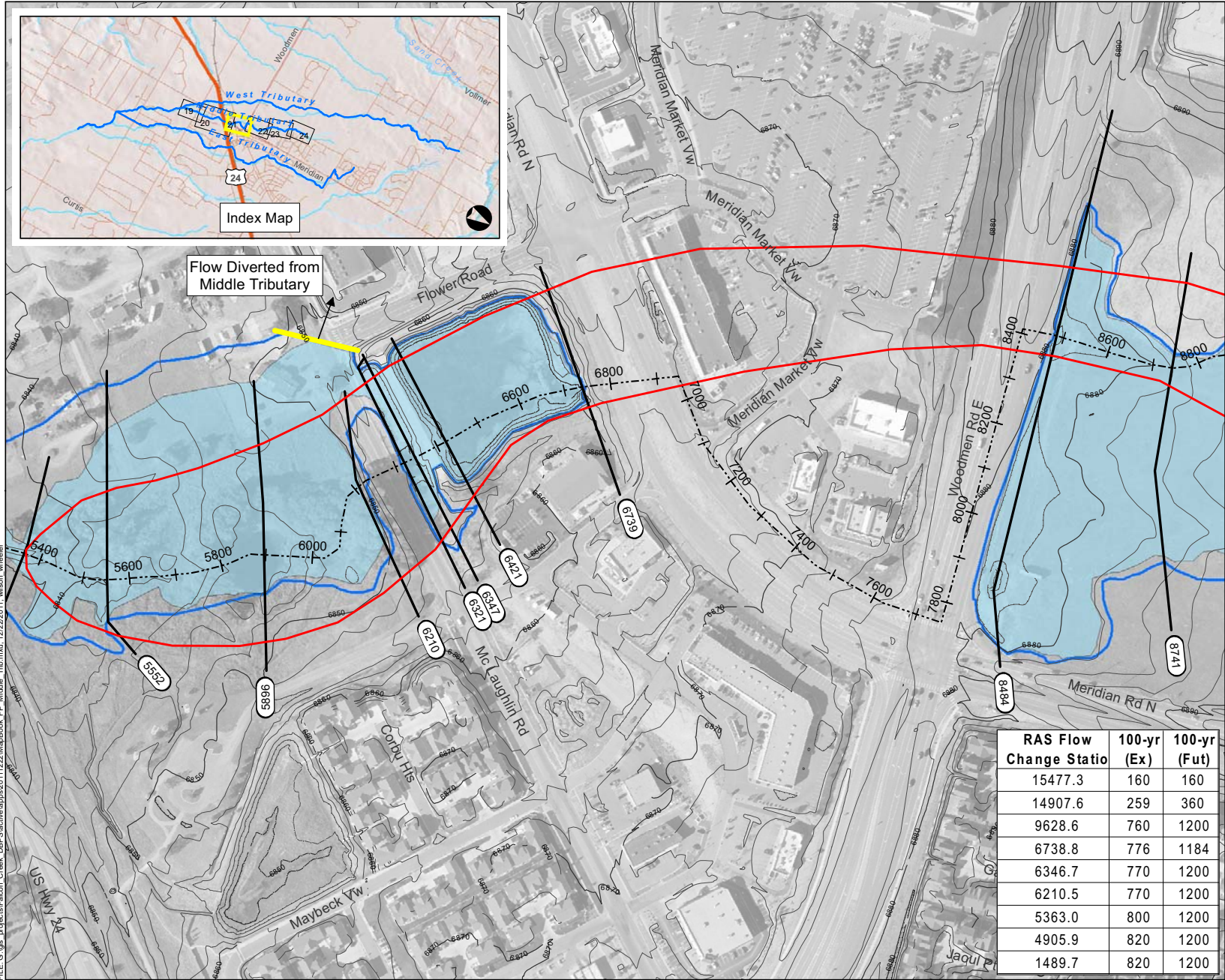
The user should graphically compare the summary S-A-V-D table to the full S-A-V-D table in the chart to confirm it captures all key transition points.

[illegible]

Falcon DBPS Excerpts

FILE: G:\gis_projects\Falcon_DBPS\active\appa20130817\mapbooks\Sat All Middle Trib.mxd, 1/11/2016, Jeff. Conts





Sheet 4-21

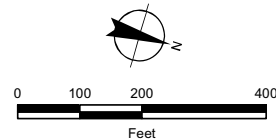
Middle Tributary Floodplain

Falcon DBPS

El Paso County, CO

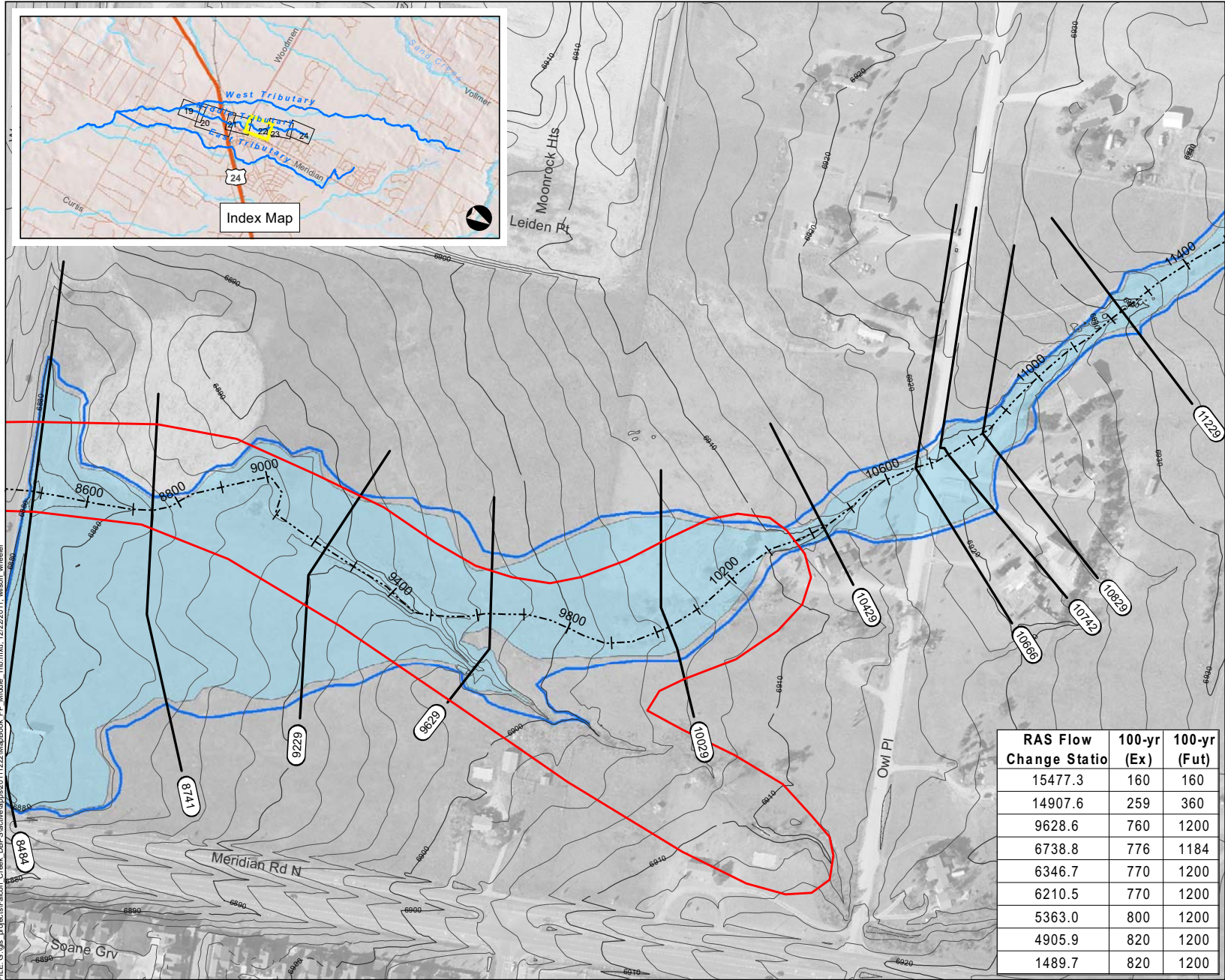
- Legend**
- Approximate 100-yr Floodplain Existing
 - Approximate 100-yr Floodplain Existing (Based on Assumed Split Flow Condition)
 - Approximate 100-yr Floodplain Future
 - Approximate 100-yr Floodplain Future (Based on Assumed Split Flow Condition)
 - Shallow Flooding
 - HEC-RAS Centerline
 - XSCutLines (Middle Trib)
 - FEMA Regulatory Floodplain (Effective as of 1999)*
 - Study Limit

*Letters of Map Change completed after 1999 are not shown



RAS Flow Change Statio	100-yr (Ex)	100-yr (Fut)
15477.3	160	160
14907.6	259	360
9628.6	760	1200
6738.8	776	1184
6346.7	770	1200
6210.5	770	1200
5363.0	800	1200
4905.9	820	1200
1489.7	820	1200





Sheet 4-22

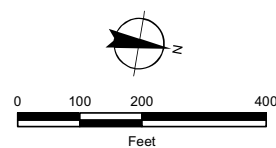
Middle Tributary Floodplain

Falcon DBPS

El Paso County, CO

- Legend**
- Approximate 100-yr Floodplain Existing
 - Approximate 100-yr Floodplain Existing (Based on Assumed Split Flow Condition)
 - Approximate 100-yr Floodplain Future
 - Approximate 100-yr Floodplain Future (Based on Assumed Split Flow Condition)
 - Shallow Flooding
 - HEC-RAS Centerline
 - XSCutLines (Middle Trib)
 - FEMA Regulatory Floodplain (Effective as of 1999)*
 - Study Limit

*Letters of Map Change completed after 1999 are not shown

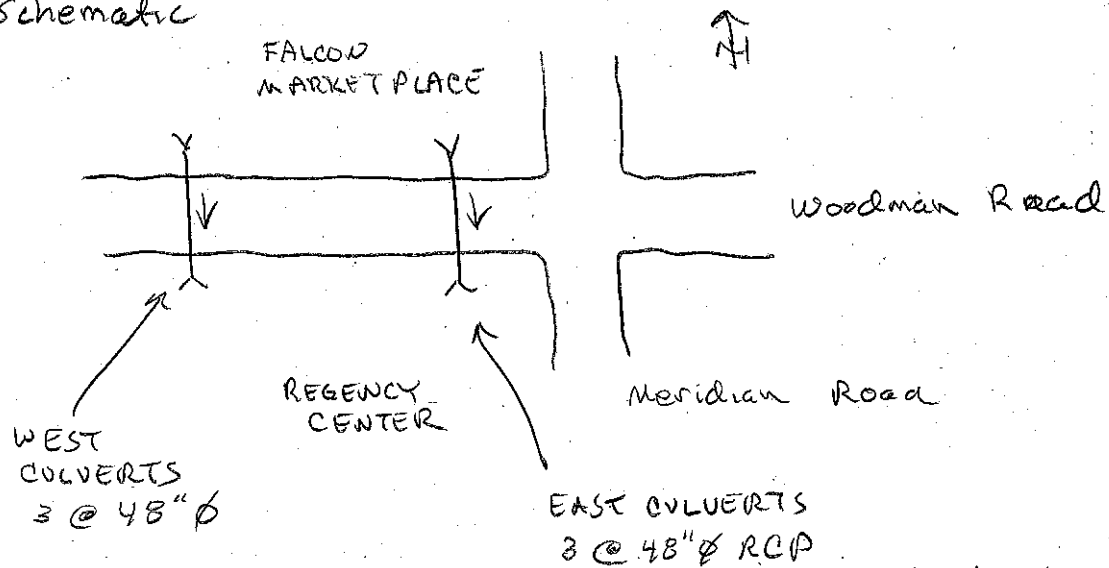


RAS Flow Change Statio	100-yr (Ex)	100-yr (Fut)
15477.3	160	160
14907.6	259	360
9628.6	760	1200
6738.8	776	1184
6346.7	770	1200
6210.5	770	1200
5363.0	800	1200
4905.9	820	1200
1489.7	820	1200



CLOMR Excerpts

① Schematic



② Use FHWA HY-8 software to check culvert capacity

③ Model input based on 3 sources of information

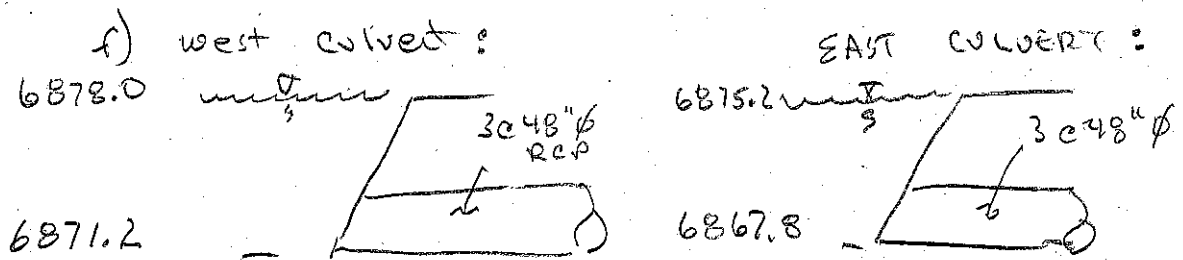
a) project surveys by DBC for Falcon Marketplace
email 9/26/16

b) Design drawing from Regency Center
URS 8/24/04

c) Design drawing for culvert extension on
north side of Woodman
DMJM Harris/AECOM 9/11/2007

d) See HY-8 model output files
file: HY-8-Woodman Culverts.hy8

e) Design flow rate varied until allowable headwater elevation reached. Allowable headwater elevation = to north edge of Woodman Road Asphalt.



g) The Woodman Road culverts discharge to large 84" culvert & 8' x 8' culvert on the Regency Center property that are @ a significantly lower elevation.

than the invert of the 48" ϕ pipes;
therefore inlet control conditions are
anticipate w/ no backwater from
downstream

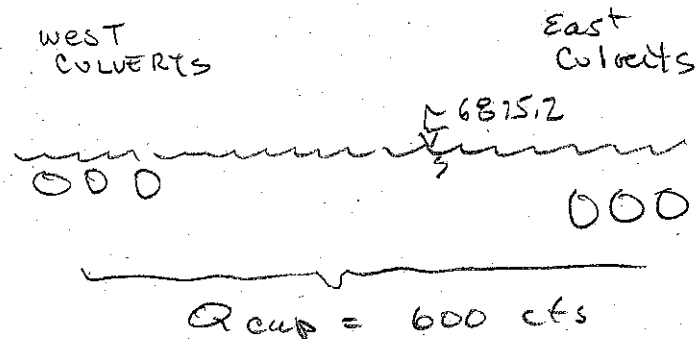
④ See HY-8 output

a) West Culvert: $Q_{cap} = 355$ cfs w/ HW @ 6877.99
 ≈ 6878

b) East Culvert: $Q_{cap} = 405$ cfs w/ HW @ 6875.12
 ≈ 6875.2

c) Total Capacity 760 cfs

d) Also looked @ capacity of both
culverts with the lower allowable
headwater elevation



HY-8 Culvert Analysis Report

Project Notes

Project Title:

Designer:

Project Date: Wednesday, September 28, 2016

Notes:

Project Units: U.S. Customary Units

Outlet Control Option: Profiles

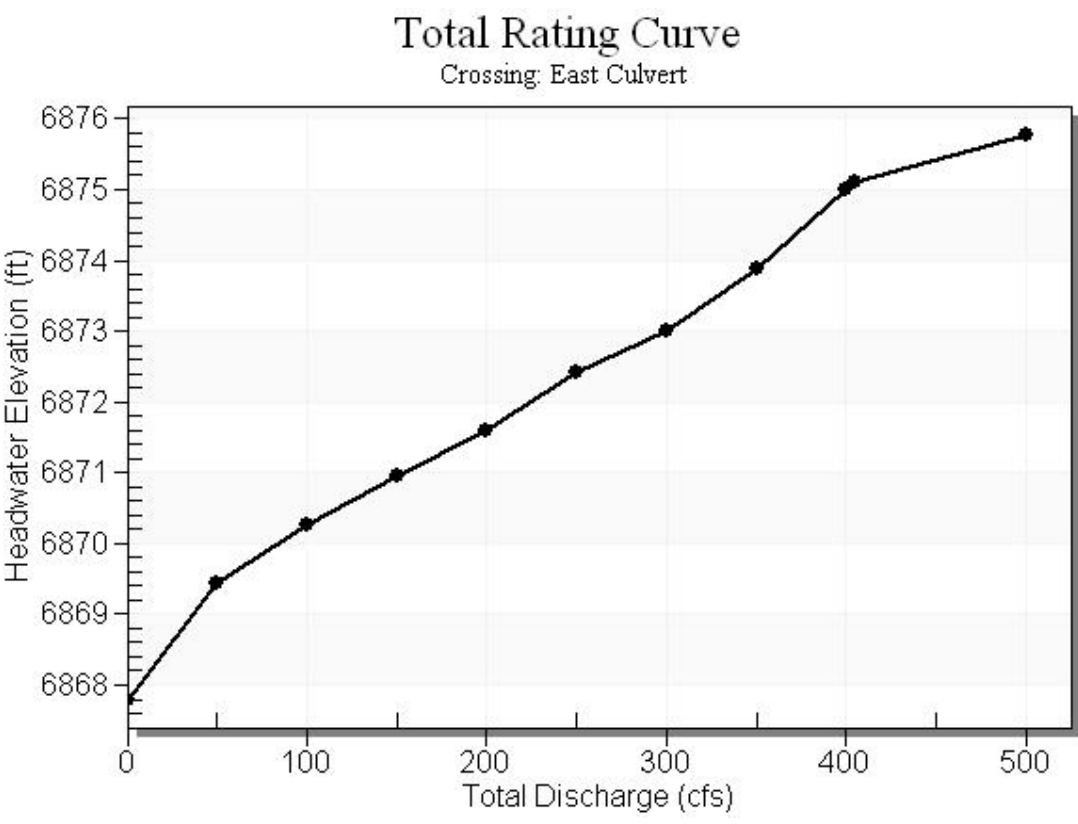
Exit Loss Option: Standard Method

Crossing Notes: East Culvert

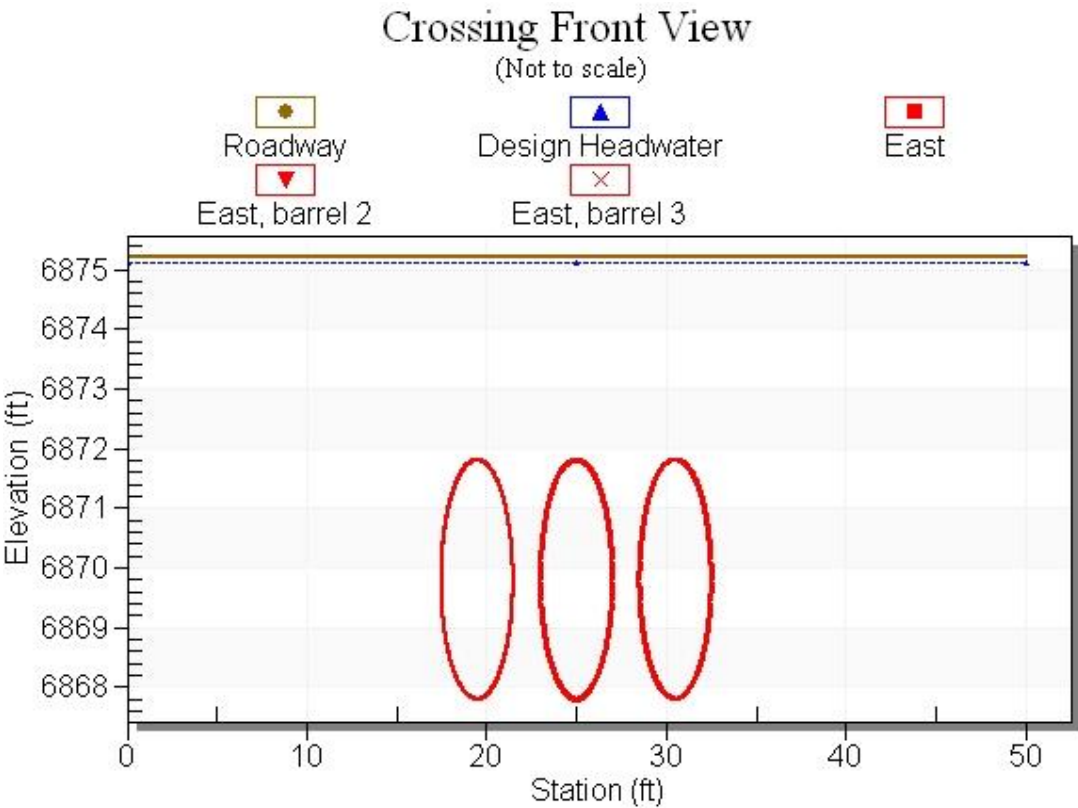
Table 1 - Summary of Culvert Flows at Crossing: East Culvert

Headwater Elevation (ft)	Total Discharge (cfs)	East Discharge (cfs)	Roadway Discharge (cfs)	Iterations
6867.80	0.00	0.00	0.00	1
6869.44	50.00	50.00	0.00	1
6870.26	100.00	100.00	0.00	1
6870.95	150.00	150.00	0.00	1
6871.58	200.00	200.00	0.00	1
6872.41	250.00	250.00	0.00	1
6873.01	300.00	300.00	0.00	1
6873.88	350.00	350.00	0.00	1
6875.00	400.00	400.00	0.00	1
6875.12	405.00	405.00	0.00	1
6875.78	500.00	432.38	67.60	5
6875.20	408.39	408.39	0.00	Overtopping

Rating Curve Plot for Crossing: East Culvert



Crossing Front View (Roadway Profile): East Culvert



Culvert Notes: East

Table 2 - Culvert Summary Table: East

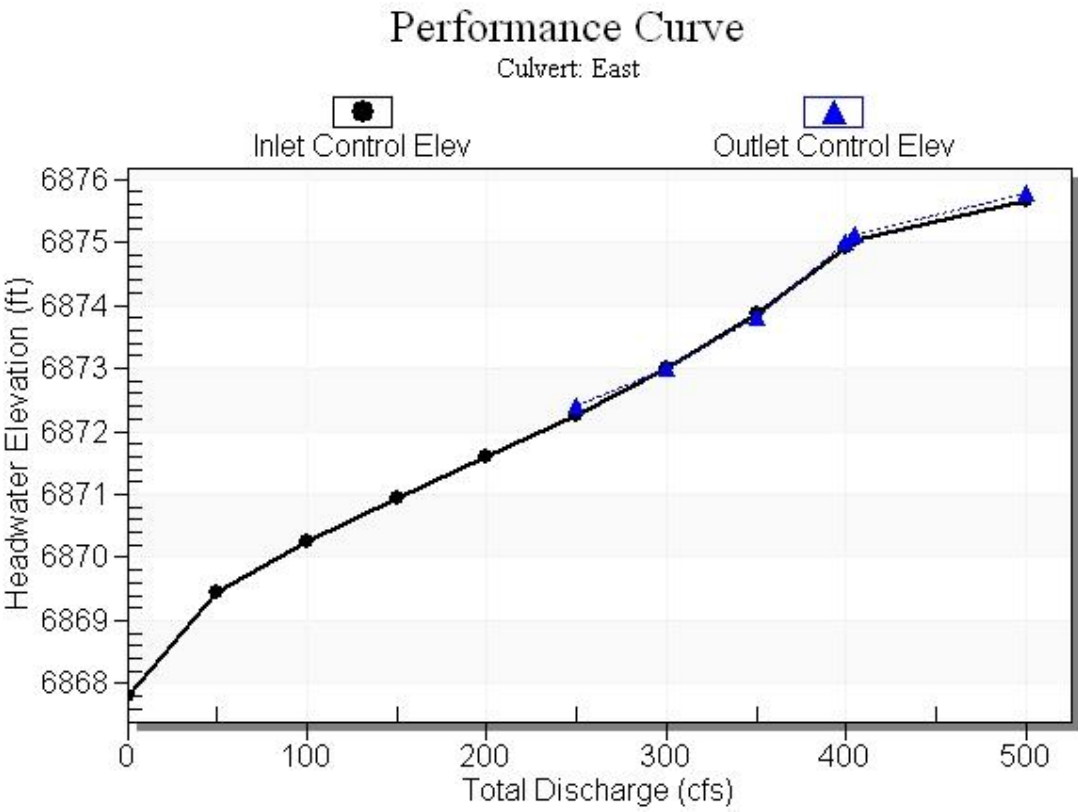
Total Discharge (cfs)	Culvert Discharge (cfs)	Headwater Elevation (ft)	Inlet Control Depth (ft)	Outlet Control Depth (ft)	Flow Type	Normal Depth (ft)	Critical Depth (ft)	Outlet Depth (ft)	Tailwater Depth (ft)	Outlet Velocity (ft/s)	Tailwater Velocity (ft/s)
0.00	0.00	6867.80	0.000	0.0*	0-NF	0.000	0.000	0.000	0.000	0.000	0.000
50.00	50.00	6869.44	1.645	0.0*	1-S2n	1.114	1.197	1.117	0.745	5.778	8.385
100.00	100.00	6870.26	2.457	0.0*	1-S2n	1.620	1.708	1.622	1.169	6.978	10.692
150.00	150.00	6870.95	3.153	0.0*	1-S2n	2.042	2.114	2.043	1.532	7.747	12.238
200.00	200.00	6871.58	3.785	0.0*	1-S2n	2.445	2.461	2.445	1.864	8.280	13.414
250.00	250.00	6872.41	4.445	4.610	2-M2c	2.874	2.763	2.766	2.175	8.989	14.366
300.00	300.00	6873.01	5.196	5.208	2-M2c	3.464	3.018	3.030	2.473	9.792	15.165
350.00	350.00	6873.88	6.077	6.001	2-M2c	4.000	3.246	3.258	2.760	10.663	15.852
400.00	400.00	6875.00	7.109	7.200	7-M2c	4.000	3.420	3.447	3.039	11.579	16.454
405.00	405.00	6875.12	7.221	7.318	7-M2c	4.000	3.437	3.464	3.066	11.676	16.509
500.00	432.38	6875.78	7.861	7.984	7-M2c	4.000	3.533	3.544	3.578	12.241	17.466

* theoretical depth is impractical. Depth reported is corrected.

Inlet Elevation (invert): 6867.80 ft, Outlet Elevation (invert): 6866.90 ft

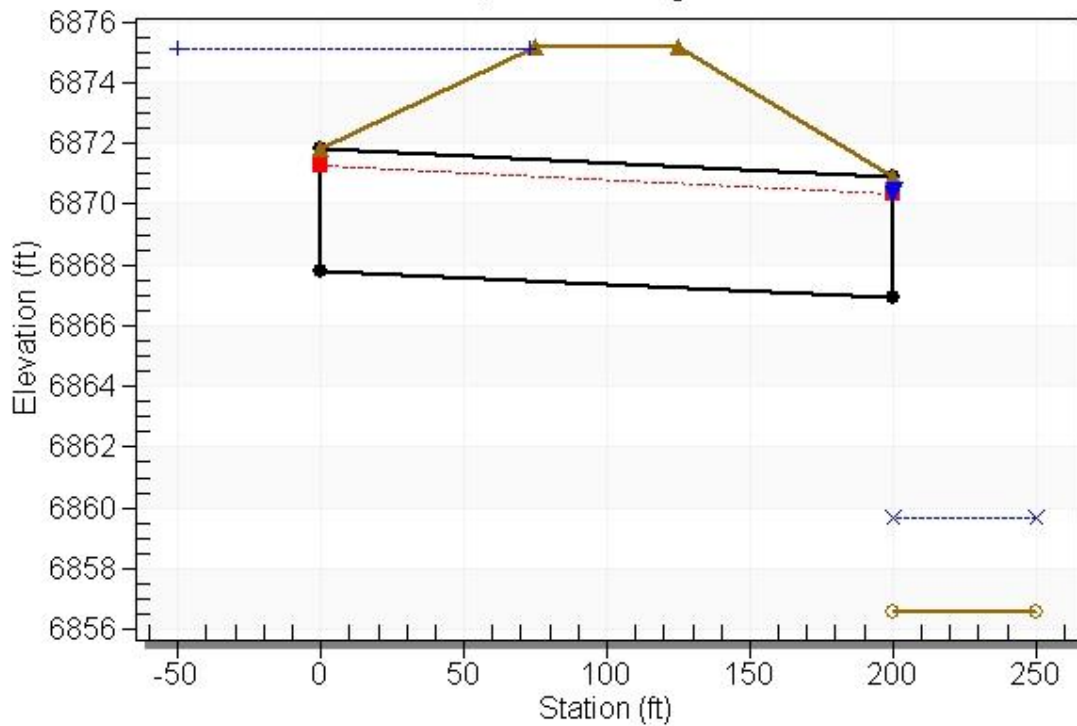
Culvert Length: 200.00 ft, Culvert Slope: 0.0045

Culvert Performance Curve Plot: East



Water Surface Profile Plot for Culvert: East

Crossing - East Culvert , Design Discharge - 405.0 cfs
Culvert - East, Culvert Discharge - 405.0 cfs



Site Data - East

Site Data Option: Culvert Invert Data

Inlet Station: 0.00 ft

Inlet Elevation: 6867.80 ft

Outlet Station: 200.00 ft

Outlet Elevation: 6866.90 ft

Number of Barrels: 3

Culvert Data Summary - East

Barrel Shape: Circular

Barrel Diameter: 4.00 ft

Barrel Material: Concrete

Embedment: 0.00 in

Barrel Manning's n: 0.0130

Inlet Type: Conventional

Inlet Edge Condition: Square Edge with Headwall

Inlet Depression: NONE

Table 3 - Downstream Channel Rating Curve (Crossing: East Culvert)

Flow (cfs)	Water Surface Elev (ft)	Depth (ft)	Velocity (ft/s)	Shear (psf)	Froude Number
0.00	6856.60	0.00	0.00	0.00	0.00
50.00	6857.35	0.75	8.39	0.47	1.71
100.00	6857.77	1.17	10.69	0.73	1.74
150.00	6858.13	1.53	12.24	0.96	1.74
200.00	6858.46	1.86	13.41	1.16	1.73
250.00	6858.78	2.18	14.37	1.36	1.72
300.00	6859.07	2.47	15.17	1.54	1.70
350.00	6859.36	2.76	15.85	1.72	1.68
400.00	6859.64	3.04	16.45	1.90	1.66
405.00	6859.67	3.07	16.51	1.91	1.66
500.00	6860.18	3.58	17.47	2.23	1.63

Tailwater Channel Data - East Culvert

Tailwater Channel Option: Rectangular Channel

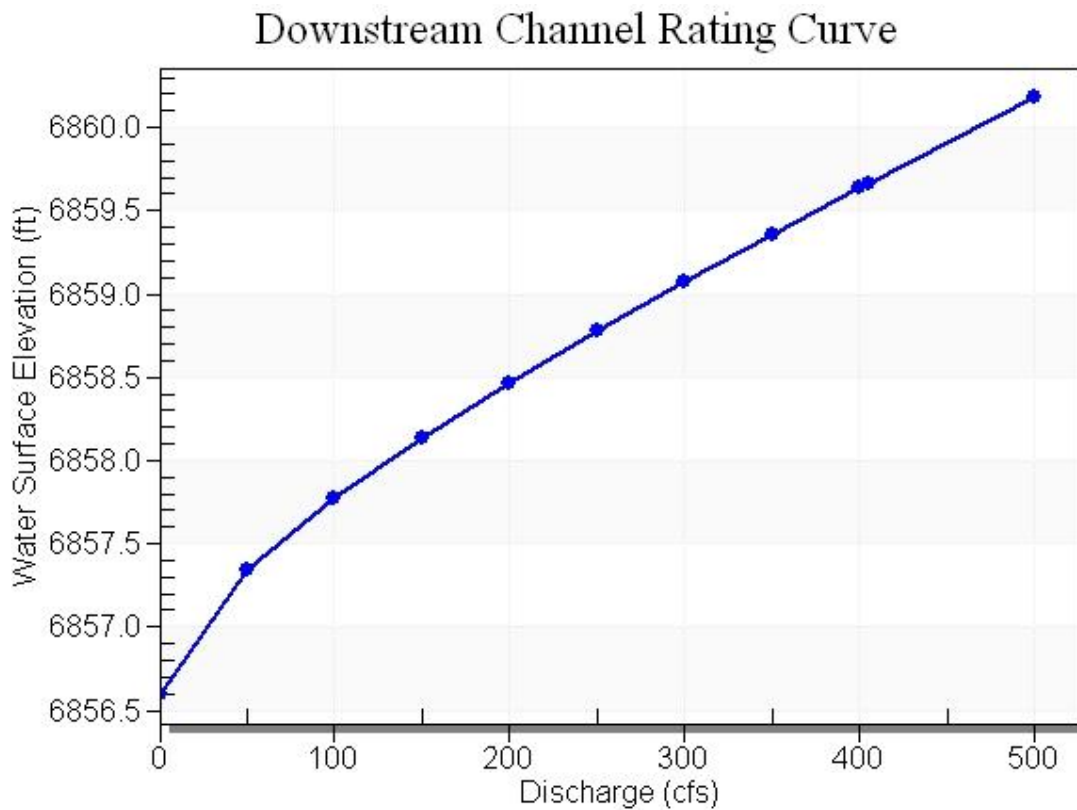
Bottom Width: 8.00 ft

Channel Slope: 0.0100

Channel Manning's n: 0.0130

Channel Invert Elevation: 6856.60 ft

Tailwater Rating Curve Plot for Crossing: East Culvert



Roadway Data for Crossing: East Culvert

Roadway Profile Shape: Irregular Roadway Shape (coordinates)

Irregular Roadway Cross-Section:

Coord No.	Station (ft)	Elevation (ft)
0	0.00	6875.20
1	25.00	6875.20
2	50.00	6875.20

Roadway Surface: Paved

Roadway Top Width: 50.00 ft

HY-8 Culvert Analysis Report

Project Notes

Project Title:

Designer:

Project Date: Wednesday, September 28, 2016

Notes:

Project Units: U.S. Customary Units

Outlet Control Option: Profiles

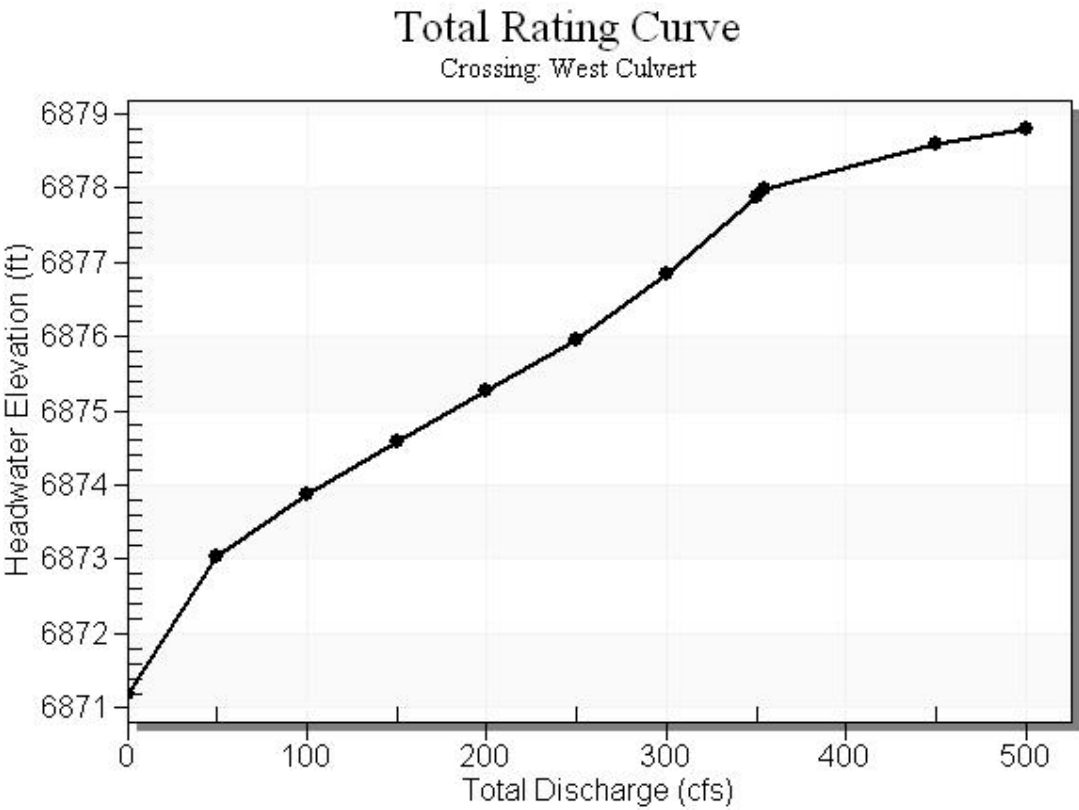
Exit Loss Option: Standard Method

Crossing Notes: West Culvert

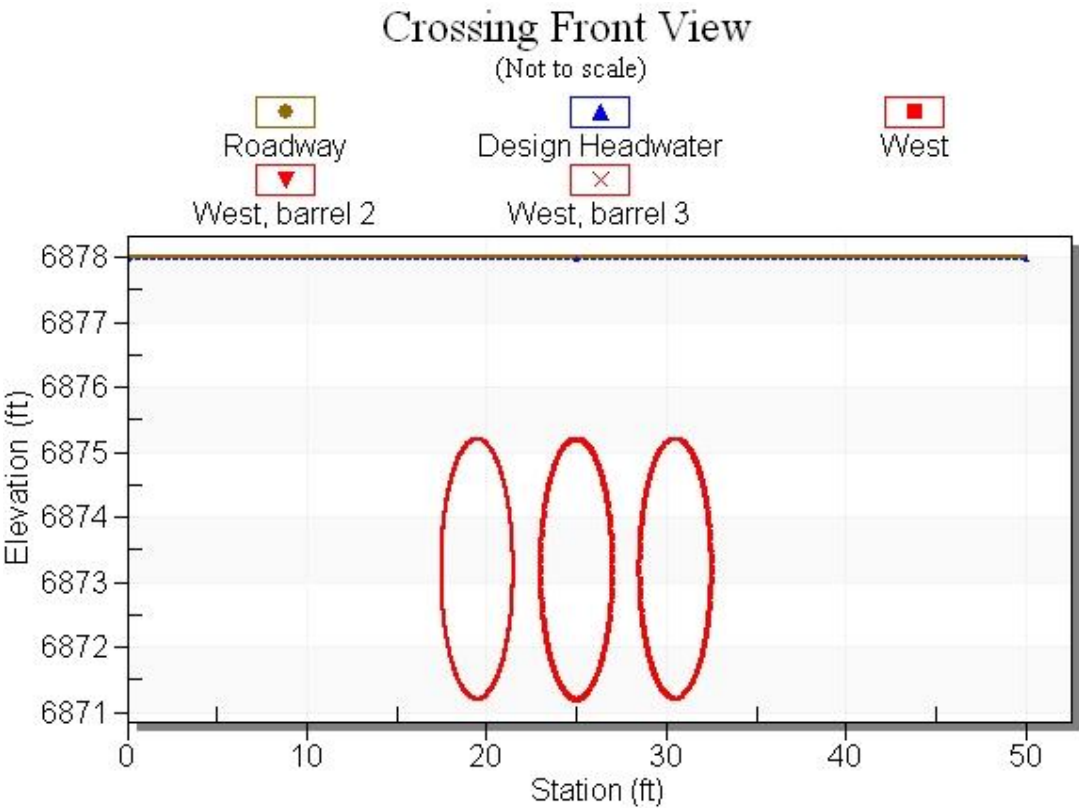
Table 1 - Summary of Culvert Flows at Crossing: West Culvert

Headwater Elevation (ft)	Total Discharge (cfs)	West Discharge (cfs)	Roadway Discharge (cfs)	Iterations
6871.20	0.00	0.00	0.00	1
6873.04	50.00	50.00	0.00	1
6873.88	100.00	100.00	0.00	1
6874.60	150.00	150.00	0.00	1
6875.27	200.00	200.00	0.00	1
6875.96	250.00	250.00	0.00	1
6876.84	300.00	300.00	0.00	1
6877.87	350.00	350.00	0.00	1
6877.99	355.00	355.00	0.00	1
6878.59	450.00	381.65	68.32	5
6878.80	500.00	390.91	108.90	4
6878.00	355.54	355.54	0.00	Overtopping

Rating Curve Plot for Crossing: West Culvert



Crossing Front View (Roadway Profile): West Culvert



Culvert Notes: West

Table 2 - Culvert Summary Table: West

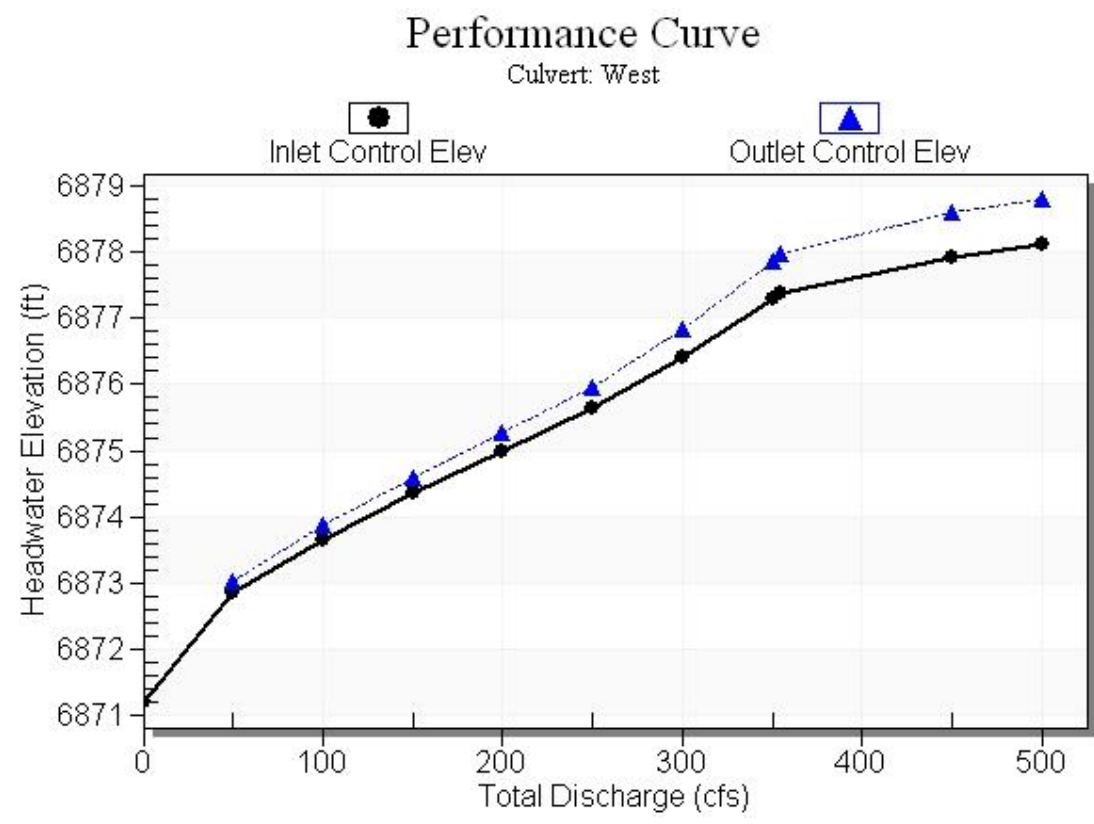
Total Discharge (cfs)	Culvert Discharge (cfs)	Headwater Elevation (ft)	Inlet Control Depth (ft)	Outlet Control Depth (ft)	Flow Type	Normal Depth (ft)	Critical Depth (ft)	Outlet Depth (ft)	Tailwater Depth (ft)	Outlet Velocity (ft/s)	Tailwater Velocity (ft/s)
0.00	0.00	6871.20	0.000	0.0*	0-NF	0.000	0.000	0.000	0.000	0.000	0.000
50.00	50.00	6873.04	1.649	1.836	2-M2c	1.492	1.197	1.197	0.821	5.273	8.705
100.00	100.00	6873.88	2.463	2.685	2-M2c	2.228	1.708	1.716	1.297	6.473	11.017
150.00	150.00	6874.60	3.159	3.396	2-M2c	2.970	2.114	2.121	1.709	7.390	12.536
200.00	200.00	6875.27	3.791	4.071	2-M2c	4.000	2.461	2.465	2.090	8.203	13.674
250.00	250.00	6875.96	4.451	4.755	2-M2c	4.000	2.763	2.766	2.449	8.989	14.582
300.00	300.00	6876.84	5.202	5.642	7-M2c	4.000	3.018	3.030	2.795	9.792	15.335
350.00	350.00	6877.87	6.083	6.665	7-M2c	4.000	3.246	3.258	3.130	10.646	15.976
355.00	355.00	6877.99	6.179	6.787	7-M2c	4.000	3.264	3.278	3.163	10.735	16.035
450.00	381.65	6878.59	6.718	7.388	7-M2c	4.000	3.356	3.380	3.777	11.230	17.019
500.00	390.91	6878.80	6.916	7.602	7-M2c	4.000	3.388	3.413	4.093	11.410	17.453

* theoretical depth is impractical. Depth reported is corrected.

Inlet Elevation (invert): 6871.20 ft, Outlet Elevation (invert): 6870.90 ft

Culvert Length: 200.00 ft, Culvert Slope: 0.0015

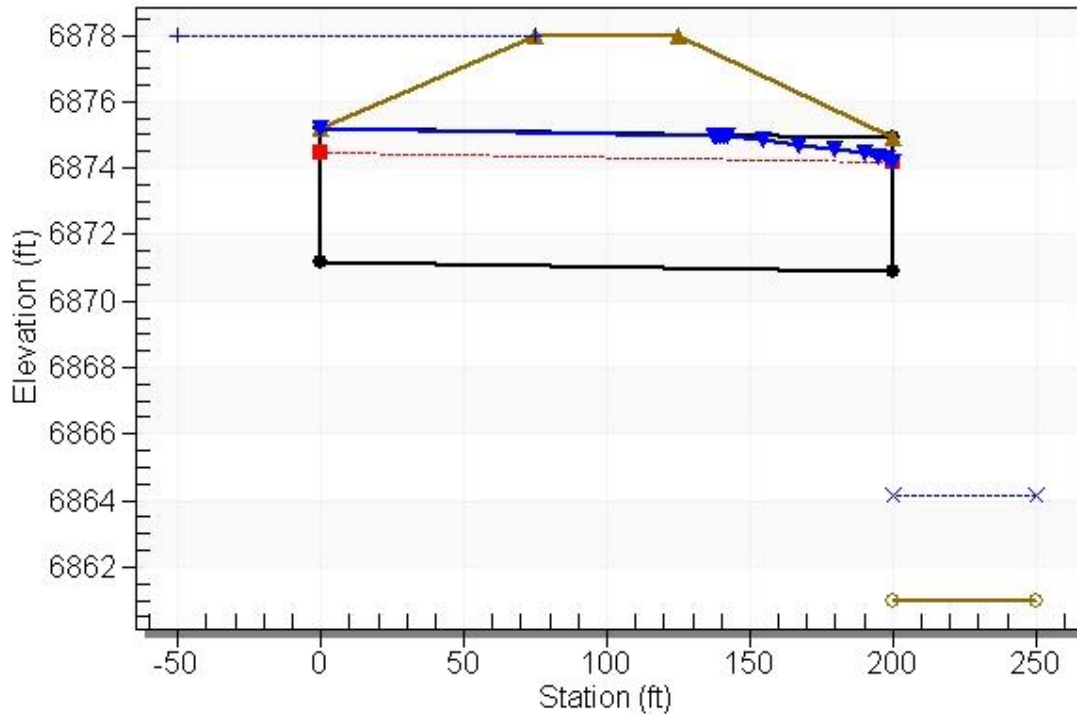
Culvert Performance Curve Plot: West



Water Surface Profile Plot for Culvert: West

Crossing - West Culvert, Design Discharge - 355.0 cfs

Culvert - West, Culvert Discharge - 355.0 cfs



Site Data - West

Site Data Option: Culvert Invert Data

Inlet Station: 0.00 ft

Inlet Elevation: 6871.20 ft

Outlet Station: 200.00 ft

Outlet Elevation: 6870.90 ft

Number of Barrels: 3

Culvert Data Summary - West

Barrel Shape: Circular

Barrel Diameter: 4.00 ft

Barrel Material: Concrete

Embedment: 0.00 in

Barrel Manning's n: 0.0130

Inlet Type: Conventional

Inlet Edge Condition: Square Edge with Headwall

Inlet Depression: NONE

Table 3 - Downstream Channel Rating Curve (Crossing: West Culvert)

Flow (cfs)	Water Surface Elev (ft)	Depth (ft)	Velocity (ft/s)	Shear (psf)	Froude Number
0.00	6861.00	0.00	0.00	0.00	0.00
50.00	6861.82	0.82	8.71	0.51	1.69
100.00	6862.30	1.30	11.02	0.81	1.71
150.00	6862.71	1.71	12.54	1.07	1.69
200.00	6863.09	2.09	13.67	1.30	1.67
250.00	6863.45	2.45	14.58	1.53	1.64
300.00	6863.79	2.79	15.34	1.74	1.62
350.00	6864.13	3.13	15.98	1.95	1.59
355.00	6864.16	3.16	16.03	1.97	1.59
450.00	6864.78	3.78	17.02	2.36	1.54
500.00	6865.09	4.09	17.45	2.55	1.52

Tailwater Channel Data - West Culvert

Tailwater Channel Option: Rectangular Channel

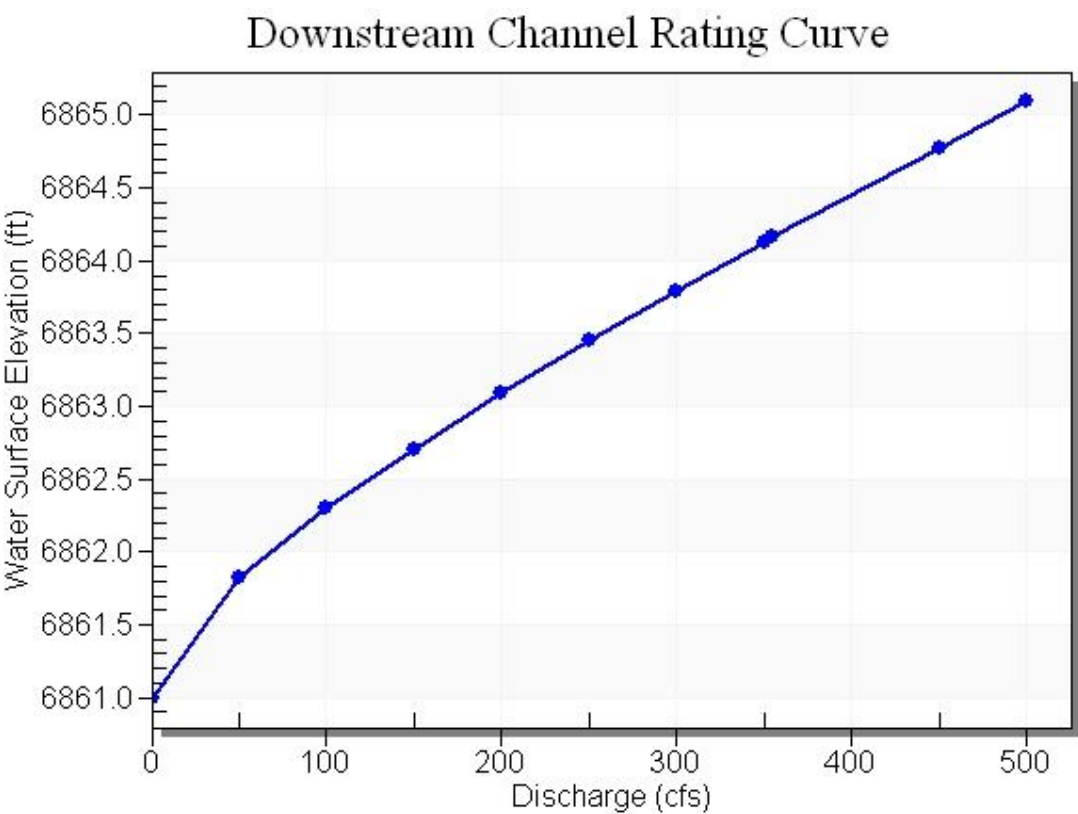
Bottom Width: 7.00 ft

Channel Slope: 0.0100

Channel Manning's n: 0.0130

Channel Invert Elevation: 6861.00 ft

Tailwater Rating Curve Plot for Crossing: West Culvert



Roadway Data for Crossing: West Culvert

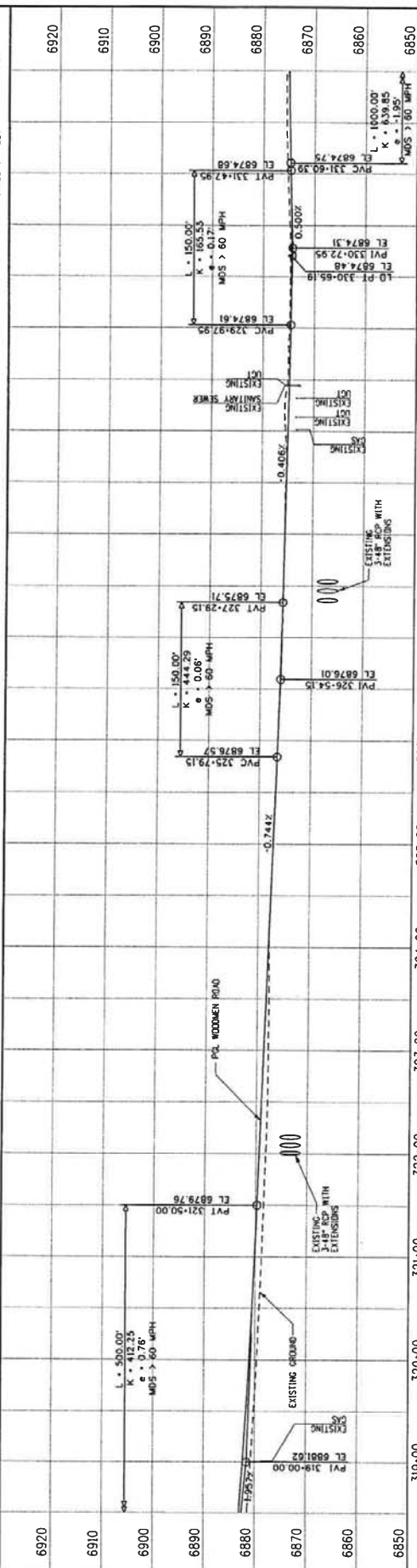
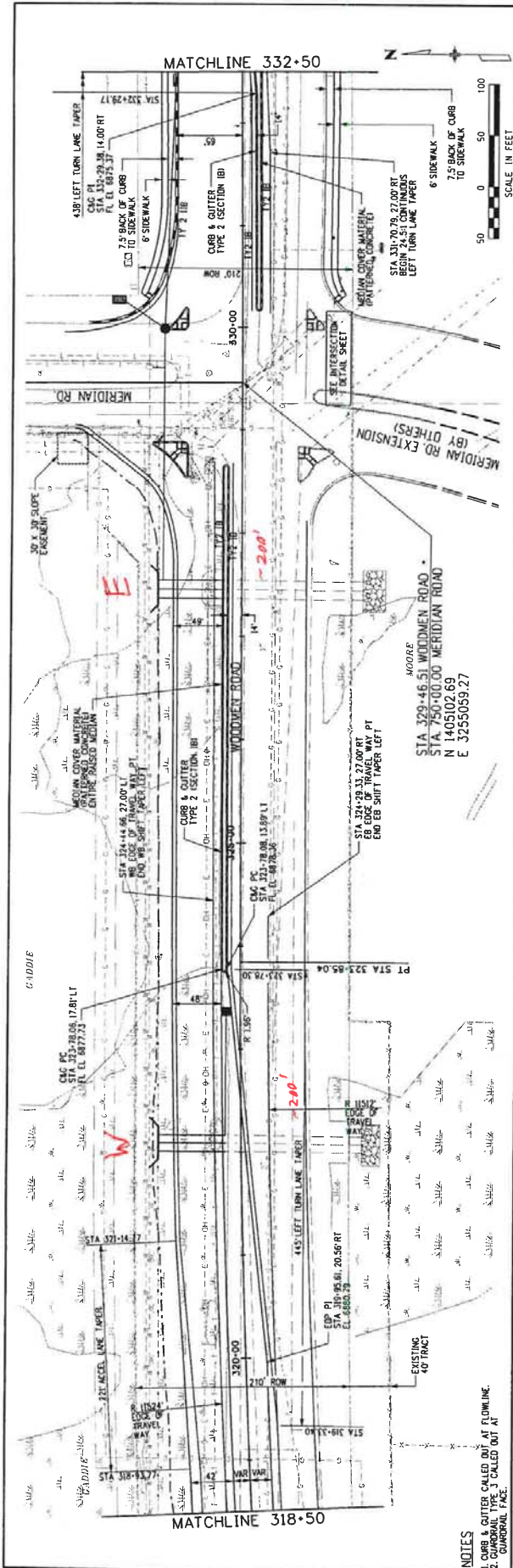
Roadway Profile Shape: Irregular Roadway Shape (coordinates)

Irregular Roadway Cross-Section:

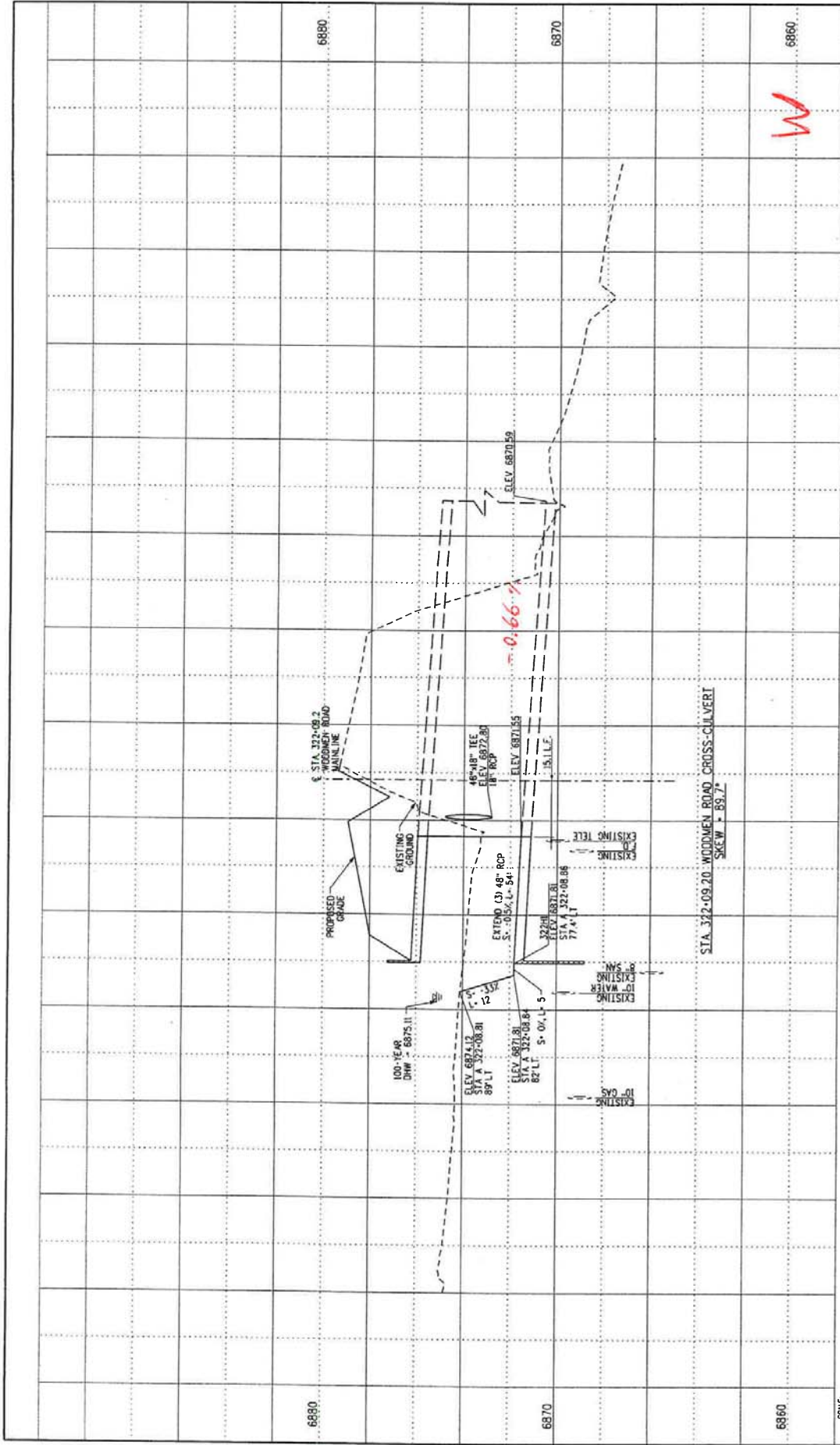
Coord No.	Station (ft)	Elevation (ft)
0	0.00	6878.00
1	25.00	6878.00
2	50.00	6878.00

Roadway Surface: Paved

Roadway Top Width: 50.00 ft



Computer File Information				Sheet Revisions				As Constructed				Project No./Code			
Creation Date:	02/07/06	Initials:	LPS					No Revisions:				WOODMEN ROAD			
Last Modification Date:	9/11/2007	Initials:	LPS					Revised:				PLAN & PROFILE-WOODMEN ROAD			
Full Path:	\\P:\P\1454\1454_0004\Roadway\1400PP24.dgn														
Drawing Scale:	1"=50'	Units:	ENGLISH					Drawn:				13263			
VB Ver:	08.00.01.19							Checked:				Roadway Subst: R0PP23 of 38			
								Sheet Number				91			



SCALE:
1" = 40' HORIZONTAL
1" = 4' VERTICAL

Computer File Information				Sheet Revisions		As Constructed		WOODMEN ROAD STORM SEWER PROFILE - WOODMEN RD. STA. 322+09.20		Project No./Code	
Creation Date:	02/20/06	Initials:	LPS			No Revisions:	-	Designer:	CLP	STU M240-062	
Last Modification Date:	9/17/2007	Initials:	LPS			Revised:	-	Checker:	CLP	13263	
Full Path:	\\V951\951_0604\ood\Woodmen\144RSTR45.dgn					Mod:	-	Sheet Subset:	DR45	Sheet Number	193
Drawing Scale:	1=20	Units: ENGLISH									
VB Ver:	08.00.01.19										

CLOMR Approval



Federal Emergency Management Agency

Washington, D.C. 20472

May 26, 2017

CERTIFIED MAIL
RETURN RECEIPT REQUESTED

The Honorable Darryl Glenn
Chairman, El Paso County
Board of Commissioners
200 South Cascade Avenue, Suite 100
Colorado Springs, CO 80903

IN REPLY REFER TO:

Case No.: 17-08-0074R
Community Name: El Paso County, CO
Community No.: 080059

Dear Mr. Glenn:

The Flood Insurance Study Report and Flood Insurance Rate Map for your community have been revised by this Letter of Map Revision (LOMR). Please use the enclosed annotated map panel(s) revised by this LOMR for floodplain management purposes and for all flood insurance policies and renewals issued in your community.

Additional documents are enclosed that provide information regarding this LOMR. Please see the List of Enclosures below to determine which documents are included. Other attachments specific to this request may be included as referenced in the Determination Document. If you have any questions regarding floodplain management regulations for your community or the National Flood Insurance Program (NFIP) in general, please contact the Consultation Coordination Officer for your community. If you have any technical questions regarding this LOMR, please contact the Director, Mitigation Division of the Department of Homeland Security's Federal Emergency Management Agency (FEMA) in Denver, Colorado, at (303) 235-4830, or the FEMA Map Information eXchange (FMIX) toll free at 1-877-336-2627 (1-877-FEMA MAP). Additional information about the NFIP is available on our website at <http://www.fema.gov/national-flood-insurance-program>.

Sincerely,

Patrick "Rick" F. Sacbibit, P.E., Branch Chief
Engineering Services Branch
Federal Insurance and Mitigation Administration

List of Enclosures:

Letter of Map Revision Determination Document
Annotated Flood Insurance Rate Map
Annotated Flood Insurance Study Report

cc: Mr. Keith Curtis, P.E., CFM
Floodplain Administrator
El Paso County

Mr. Steven Leslie, P.E., CFM
Project Engineer
Drexell, Barrell & CO



Federal Emergency Management Agency

Washington, D.C. 20472

CONDITIONAL LETTER OF MAP REVISION COMMENT DOCUMENT

COMMUNITY INFORMATION		PROPOSED PROJECT DESCRIPTION	BASIS OF CONDITIONAL REQUEST
COMMUNITY	El Paso County Colorado (Unincorporated Areas)	CHANNELIZATION BRIDGE	HYDRAULIC ANALYSIS UPDATED TOPOGRAPHIC DATA HYDROLOGIC ANALYSIS
	COMMUNITY NO.: 080059		
IDENTIFIER	Falcon Marketplace	APPROXIMATE LATITUDE & LONGITUDE: 38.9426, -104.610 SOURCE: USGS QUADRANGLE DATUM: NAD 83	
AFFECTED MAP PANELS			
TYPE: FIRM* NO.: 08041C0575F DATE: March 17, 1997		* FIRM - Flood Insurance Rate Map	

FLOODING SOURCE(S) AND REACH DESCRIPTION

Unnamed Tributary to Black Squirrel Creek- from Woodmen Road to approximately 2,280 feet upstream of Woodmen Road

PROPOSED PROJECT DESCRIPTION

Flooding Source	Proposed Project	Location of Proposed Project
Unnamed Tributary to Black Squirrel Creek	Channelization	From Woodmen Road to approximately 2,820 feet upstream of Woodmen Road
	Bridge Modification	At Woodmen Road

SUMMARY OF IMPACTS TO FLOOD HAZARD DATA

Flooding Source	Effective Flooding	Proposed Flooding	Increases	Decreases
Unnamed Tributary to Black Squirrel Creek	Zone A	Zone AE	Yes	Yes
	No BFEs	BFEs	Yes	None

* BFEs - Base (1-percent-annual-chance) Flood Elevations

COMMENT

This document provides the Federal Emergency Management Agency's (FEMA's) comment regarding a request for a CLOMR for the project described above. This document is not a final determination; it only provides our comment on the proposed project in relation to the flood hazard information shown on the effective National Flood Insurance Program (NFIP) map. We reviewed the submitted data and the data used to prepare the effective flood hazard information for your community and determined that the proposed project meets the minimum floodplain management criteria of the NFIP. Your community is responsible for approving all floodplain development and for ensuring that all permits required by Federal or State/Commonwealth law have been received. State/Commonwealth, county, and community officials, based on their knowledge of local conditions and in the interest of safety, may set higher standards for construction in the Special Flood Hazard Area (SFHA), the area subject to inundation by the base flood). If the State/Commonwealth, county, or community has adopted more restrictive or comprehensive floodplain management criteria, these criteria take precedence over the minimum NFIP criteria.

This comment is based on the flood data presently available. If you have any questions about this document, please contact the FEMA Map Information eXchange (FMIX) toll free at 1-877-336-2627 (1-877-FEMA MAP) or by letter addressed to the LOMC Clearinghouse, 3601 Eisenhower Avenue, Suite 500, Alexandria, VA 22304-6426. Additional information about the NFIP is available on the FEMA website at <http://www.fema.gov/national-flood-insurance-program>.

Patrick "Rick" F. Sacbitt, P.E., Branch Chief
Engineering Services Branch
Federal Insurance and Mitigation Administration



Federal Emergency Management Agency

Washington, D.C. 20472

CONDITIONAL LETTER OF MAP REVISION COMMENT DOCUMENT (CONTINUED)

COMMUNITY INFORMATION

USE PARAGRAPH BELOW WHEN REQUEST IS FOR ZONE A ONLY

To determine the changes in flood hazards that will be caused by the proposed project, we compared the hydraulic modeling reflecting the proposed project (referred to as the proposed conditions model) to the hydraulic modeling reflecting the existing conditions.

The table below shows the changes in the base flood water-surface elevations (WSELs).

Base Flood WSEL Comparison Table

Flooding Source: Unnamed Tributary to Black Squirrel Creek		Base Flood WSEL Change (feet)	Location of maximum change
Proposed vs.	Maximum increase	None	N/A
Existing	Maximum decrease	7.3	Approximately 880 feet upstream of Woodmen Road

NFIP regulations Subparagraph 60.3(b)(7) requires communities to ensure that the flood-carrying capacity within the altered or relocated portion of any watercourse is maintained. This provision is incorporated into your community's existing floodplain management ordinances; therefore, responsibility for maintenance of the altered or relocated watercourse, including any related appurtenances such as bridges, culverts, and other drainage structures, rests with your community. We may request that your community submit a description and schedule of maintenance activities necessary to ensure this requirement.

This comment is based on the flood data presently available. If you have any questions about this document, please contact the FEMA Map Information eXchange (FMIX) toll free at 1-877-336-2627 (1-877-FEMA MAP) or by letter addressed to the LOMC Clearinghouse, 3601 Eisenhower Avenue, Suite 500, Alexandria, VA 22304-6426. Additional information about the NFIP is available on the FEMA website at <http://www.fema.gov/national-flood-insurance-program>.

Patrick "Rick" F. Sacibit, P.E., Branch Chief
Engineering Services Branch
Federal Insurance and Mitigation Administration



Federal Emergency Management Agency

Washington, D.C. 20472

CONDITIONAL LETTER OF MAP REVISION COMMENT DOCUMENT (CONTINUED)

COMMUNITY INFORMATION (CONTINUED)

DATA REQUIRED FOR FOLLOW-UP LOMR

Upon completion of the project, your community must submit the data listed below and request that we make a final determination on revising the effective FIRM. If the project is built as proposed and the data below are received, a revision to the FIRM would be warranted.

- Detailed application and certification forms must be used for requesting final revisions to the maps. Therefore, when the map revision request for the area covered by this letter is submitted, Form 1, entitled "Overview and Concurrence Form," must be included. A copy of this form may be accessed at http://www.fema.gov/plan/prevent/fhm/dl_mt-2.shtm.

- The detailed application and certification forms listed below may be required if as-built conditions differ from the proposed plans. If required, please submit new forms, which may be accessed at http://www.fema.gov/plan/prevent/fhm/dl_mt-2.shtm, or annotated copies of the previously submitted forms showing the revised information.

Form 2, entitled "Riverine Hydrology and Hydraulics Form." Hydraulic analyses for as-built conditions of the base flood must be submitted with Form 2.

Form 3, entitled "Riverine Structures Form."

- A certified topographic work map showing the revised and effective base floodplain boundaries. Please ensure that the revised information ties-in with the current effective information at the downstream and upstream ends of the revised reach.

- An annotated copy of the FIRM, at the scale of the effective FIRM, that shows the revised base floodplain boundary delineations shown on the submitted work map and how they tie-in to the base floodplain boundary delineations shown on the current effective FIRM at the downstream and upstream ends of the revised reach.

- As-built plans, certified by a registered Professional Engineer, of all proposed project elements.

- Documentation of the individual legal notices sent to property owners who will be affected by any widening or shifting of the base floodplain and/or any BFE increases along the Unnamed Tributary to Black Squirrel Creek.

This comment is based on the flood data presently available. If you have any questions about this document, please contact the FEMA Map Information eXchange (FMIX) toll free at 1-877-336-2627 (1-877-FEMA MAP) or by letter addressed to the LOMC Clearinghouse, 3601 Eisenhower Avenue, Suite 500, Alexandria, VA 22304-6426. Additional information about the NFIP is available on the FEMA website at <http://www.fema.gov/national-flood-insurance-program>.

Patrick "Rick" F. Sacibit, P.E., Branch Chief
Engineering Services Branch
Federal Insurance and Mitigation Administration



Federal Emergency Management Agency

Washington, D.C. 20472

CONDITIONAL LETTER OF MAP REVISION COMMENT DOCUMENT (CONTINUED)

COMMUNITY INFORMATION (CONTINUED)

COMMUNITY REMINDERS

We have designated a Consultation Coordination Officer (CCO) to assist your community. The CCO will be the primary liaison between your community and FEMA. For information regarding your CCO, please contact:

Ms. Jeanine P. Petterson
Director, Mitigation Division
Federal Emergency Management Agency, Region VIII
Denver Federal Center, Building 710
P.O. Box 25267
Denver, CO 80225-0267
(303) 235-4830

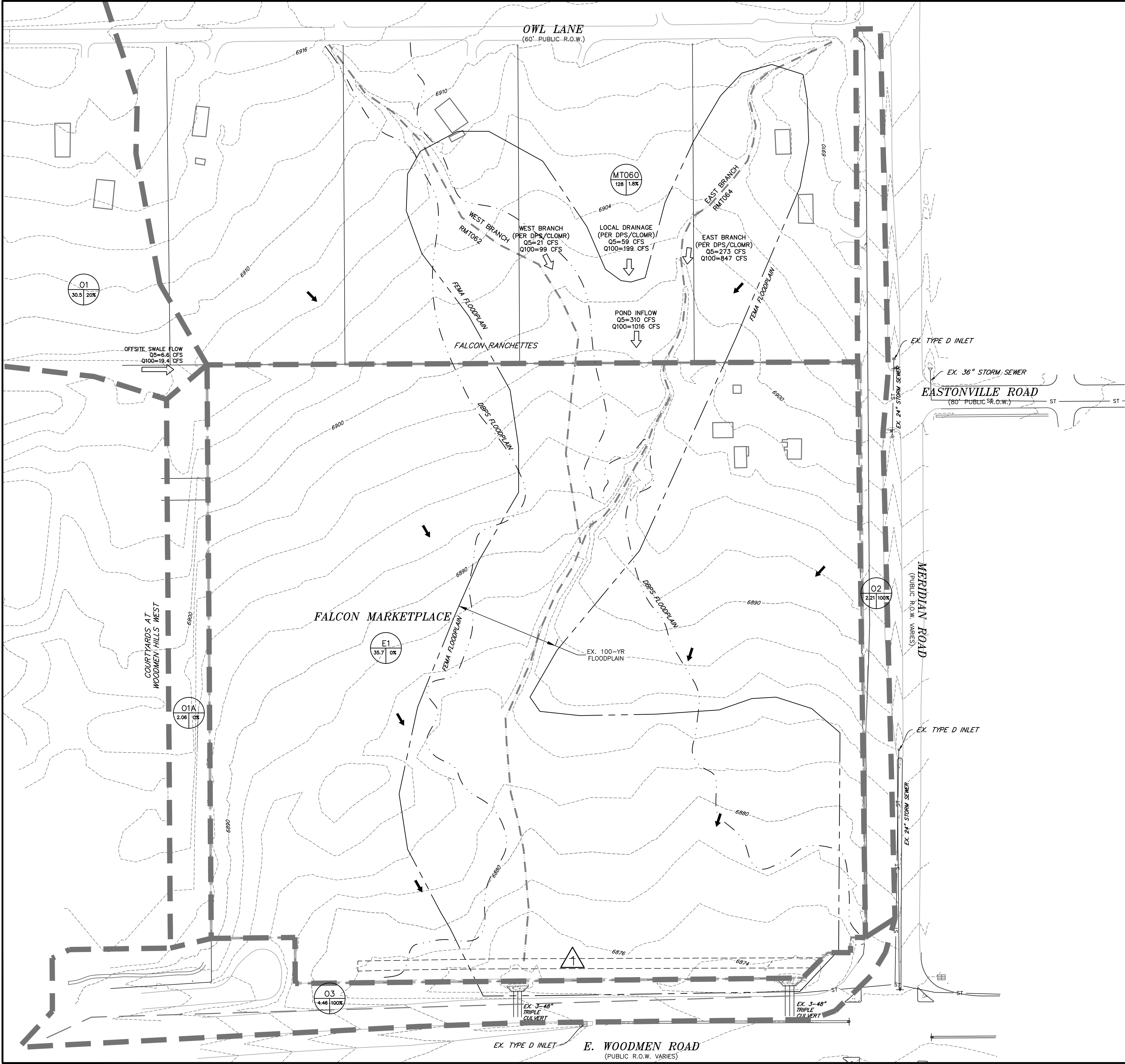
WHEN PRELIMINARY STUDY HAS BEEN SUBMITTED TO COMMUNITY FOR REVIEW

A preliminary study is being conducted for El Paso County. Preliminary copies of the revised FIRM and FIS report were submitted to your community for review on July 29, 2015, and may become effective before the revision request following this CLOMR is submitted. Please ensure that the data submitted for the revision ties into the data effective at the time of the submittal.

This comment is based on the flood data presently available. If you have any questions about this document, please contact the FEMA Map Information eXchange (FMIX) toll free at 1-877-336-2627 (1-877-FEMA MAP) or by letter addressed to the LOMC Clearinghouse, 3601 Eisenhower Avenue, Suite 500, Alexandria, VA 22304-6426. Additional Information about the NFIP is available on the FEMA website at <http://www.fema.gov/national-flood-insurance-program>.

Patrick "Rick" F. Sacbibit, P.E., Branch Chief
Engineering Services Branch
Federal Insurance and Mitigation Administration

Drainage Map



LEGEND

PROPERTY LINE.....

EX. MINOR CONTOUR.....

EX. MAJOR CONTOUR.....

BASIN BOUNDARY.....

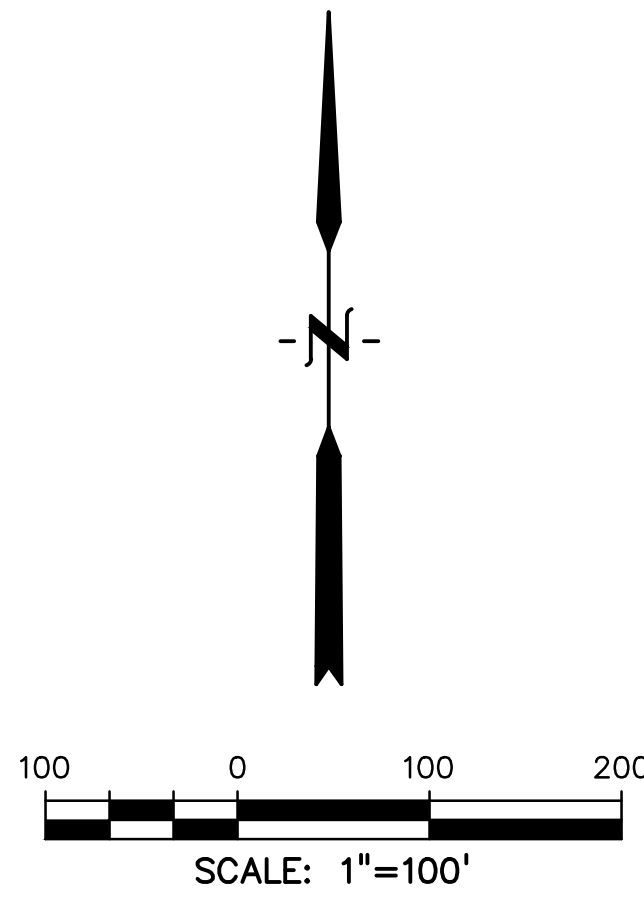
FLOW DIRECTION.....

DESIGN POINT.....

BASIN DESCRIPTION.....

BASIN AREA (ACRES)

BASIN IMPERVIOUS COVERAGE PERCENTAGE



RUNOFF SUMMARY

BASIN	Area (Ac.)	Q ₅ (CFS)	Q ₁₀₀ (CFS)
MT060	128	310	1016
O1	32.50	10.3	30.2
O1A	2.06	0.7	4.9
O2	2.21	6.7	12.0
O3	4.46	14.2	25.4
E1	35.70	6.3	46.3
DP1		348.1	1134.7

PREPARED BY:



DREXEL, BARRELL & CO.
Engineers • Surveyors
3 SOUTH 7TH STREET
COLORADO SPGS, COLORADO 80905
CONTACT: TIM D. McCONNELL, P.E.
(719)260-0887
BOULDER • COLORADO SPRINGS

CLIENT:

HUMMEL INVESTMENTS, LLC
8117 PRESTON ROAD, SUITE 120
DALLAS, TEXAS 75225
(214) 416-9820

PRELIMINARY PLAN FOR

FALCON MARKETPLACE

FALCON, COLORADO

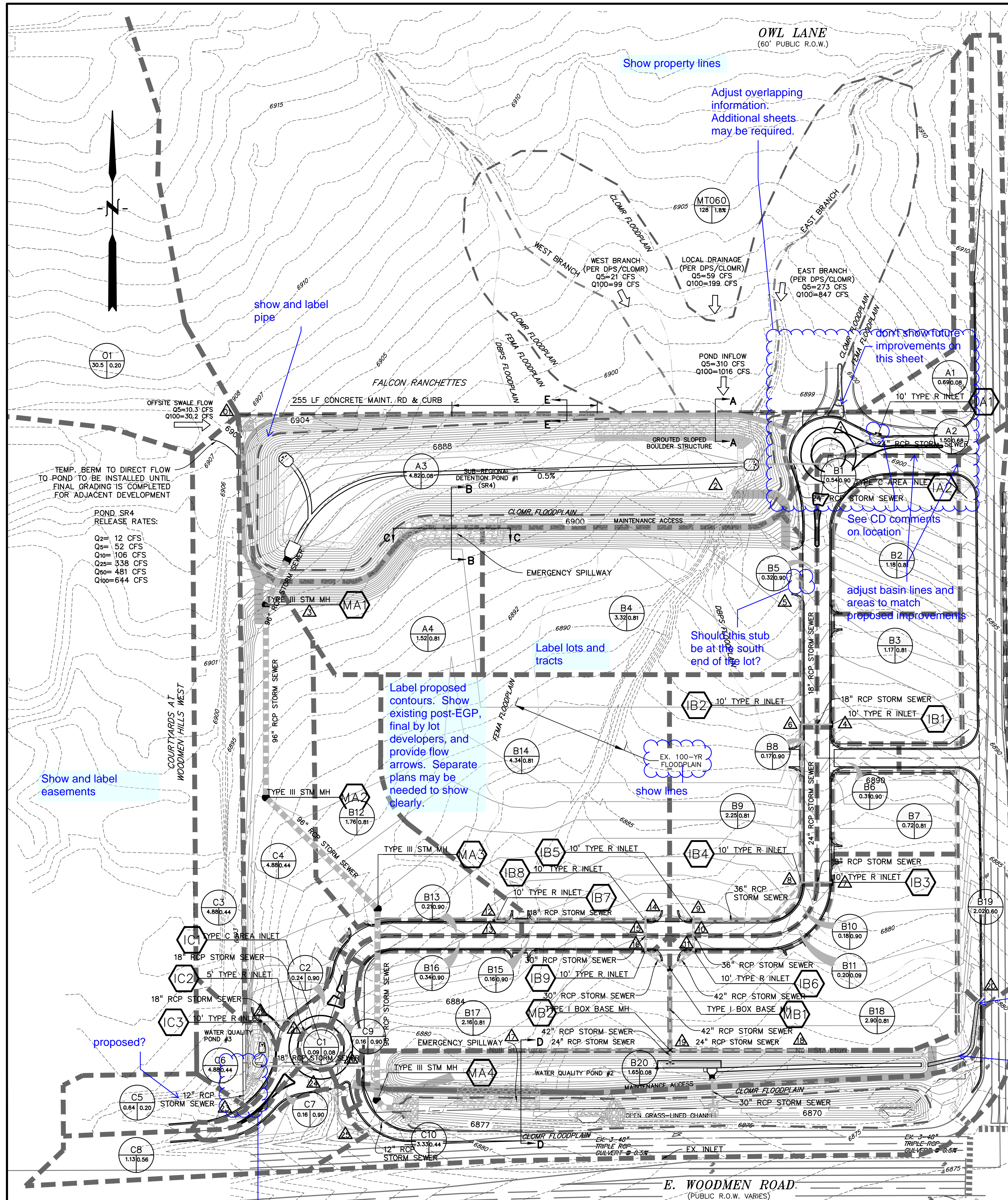
ISSUE	DATE
INITIAL ISSUE	3-23-17
REVISION	9-27-18
DESIGNED BY:	TDM
DRAWN BY:	KGV
CHECKED BY:	TDM
FILE NAME:	

PREPARED UNDER MY DIRECT SUPERVISION FOR AND ON BEHALF OF DREXEL, BARRELL & CO.

DRAWING SCALE:
HORIZONTAL: 1"=100'
VERTICAL: N/A

EXISTING DRAINAGE CONDITIONS

PROJECT NO. 20988-00CSCV
DRAWING NO.



RUNOFF SUMMARY											
BASIN	DP	Area (Ac.)	Q ₂ (CFS)	Q ₅ (CFS)	Q ₁₀₀ (CFS)	BASIN	DP	Area (Ac.)	Q ₂ (CFS)	Q ₅ (CFS)	Q ₁₀₀ (CFS)
A1		0.69	0.2	1.3		B14	DP14	4.34	15.7	28.6	
A2		1.50	4.8	9.5		B15		0.16	0.7	1.2	
A3	DP1	2.19	3.5	7.7		B16	DP15	6.47	22.6	41.2	
A4	DP2	4.82	1.4	10.2		B17	DP16	0.34	1.4	2.6	
B1	DP3	7.01	4.6	16.5		B18	DP16a	17.17	52.0	94.8	
B2		1.52	5.6	10.1		B19	DP17	2.16	8.9	16.2	
B3		0.54	2.1	3.9		B20	DP18	2.90	11.4	20.8	
B4		1.18	4.9	8.9		B21	DP19	22.23	66.7	121.7	
B5		1.17	4.7	8.6		B22	DP20	2.02	5.5	13.4	
B6	DP4	2.89	11.4	20.9		B23		1.65	0.5	8.2	
B7		3.32	10.7	19.5		C1		0.11	0.0	0.2	
B8	DP5	0.32	1.3	2.4		C2		0.29	1.1	0.8	
B9		6.53	20.6	37.6		C3	DP21	0.40	0.9	2.2	
B10		0.31	1.3	2.3		C4		1.88	0.5	7.9	
B11	DP6	0.72	2.8	5.1		C5	DP22	2.43	10.0	7.3	
B12	DP7	1.03	4.0	7.4		C6	DP23	4.31	7.2	21.6	
B13		0.17	0.7	1.3		C7	DP24	0.64	0.5	2.8	
		DP8	7.73	24.0	43.8	C8		0.45	0.2	1.5	
		DP9	2.25	9.2	16.7	C9	DP25	0.16	0.6	0.5	
		DP10	0.18	0.7	1.4	C10		1.08	2.5	6.6	
		DP11	0.20	0.8	1.5			1.24	3.1	6.1	
		DP12	10.36	31.5	57.4			0.19	0.8	1.2	
		DP13	1.76	6.3	11.5			3.43	7.3	21.5	
			0.21	0.9	1.6						
			1.97	7.0	12.8						

LEGEND

PROPERTY LINE.....

LOT LINE.....

PROPOSED STORM SEWER.....

EX. MINOR CONTOUR.....

EX. MAJOR CONTOUR.....

PR. MINOR CONTOUR.....

PR. MAJOR CONTOUR.....

BASIN BOUNDARY.....

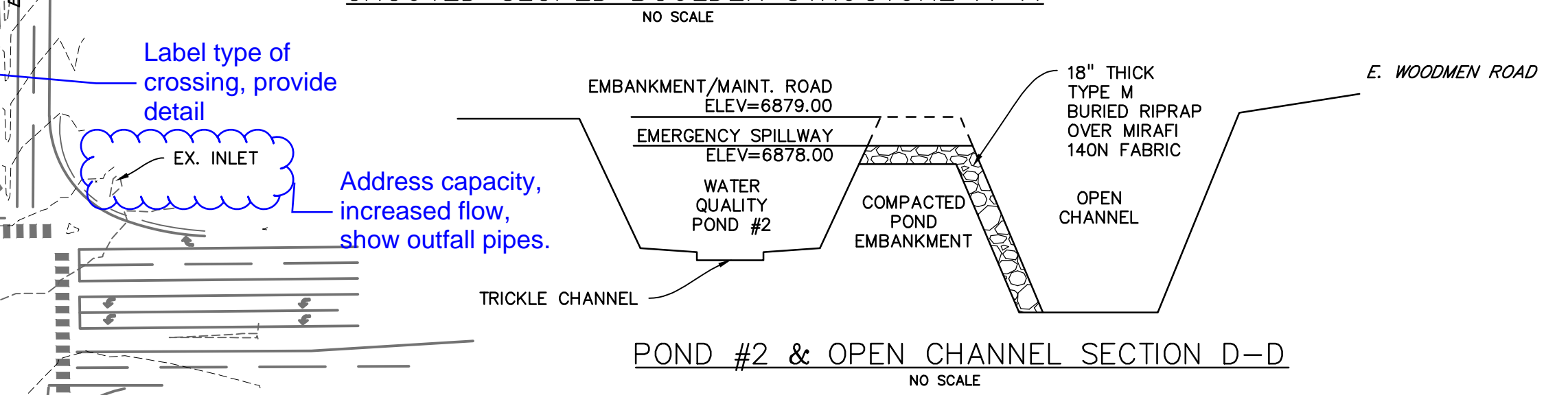
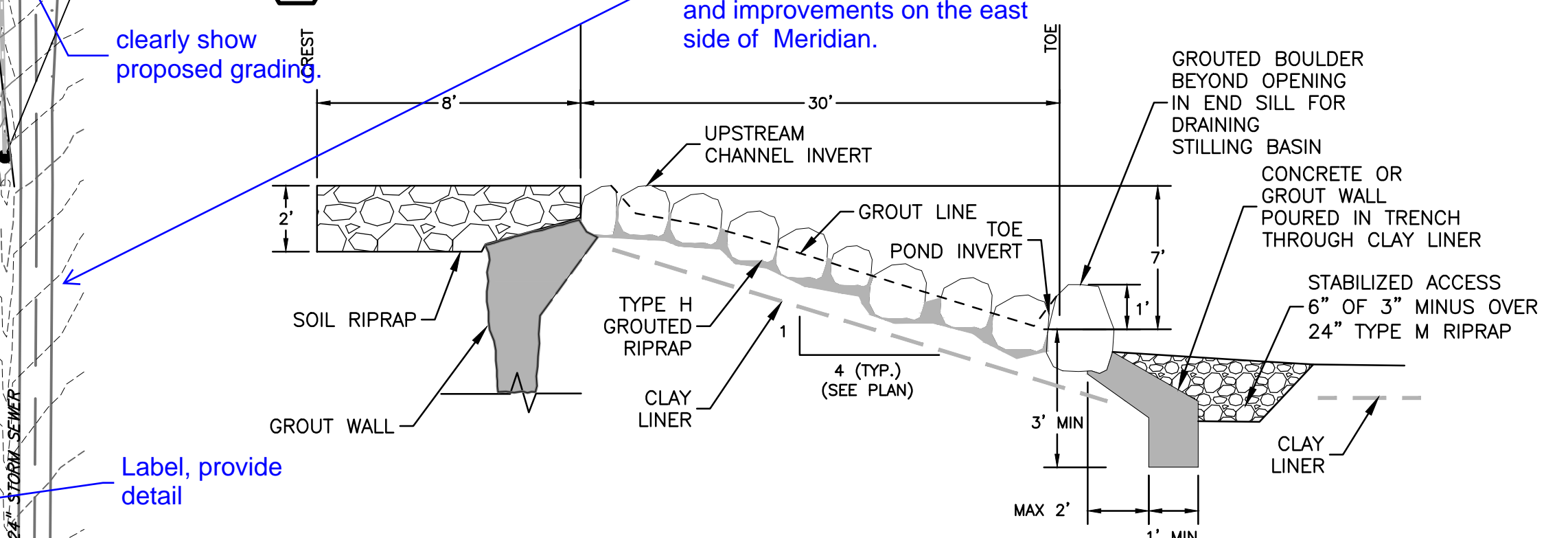
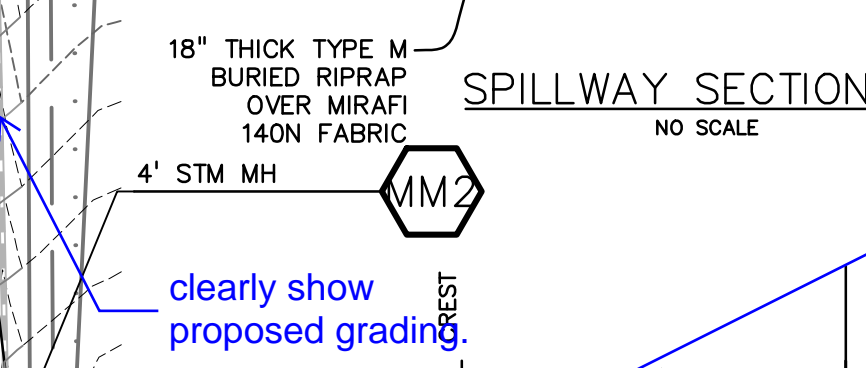
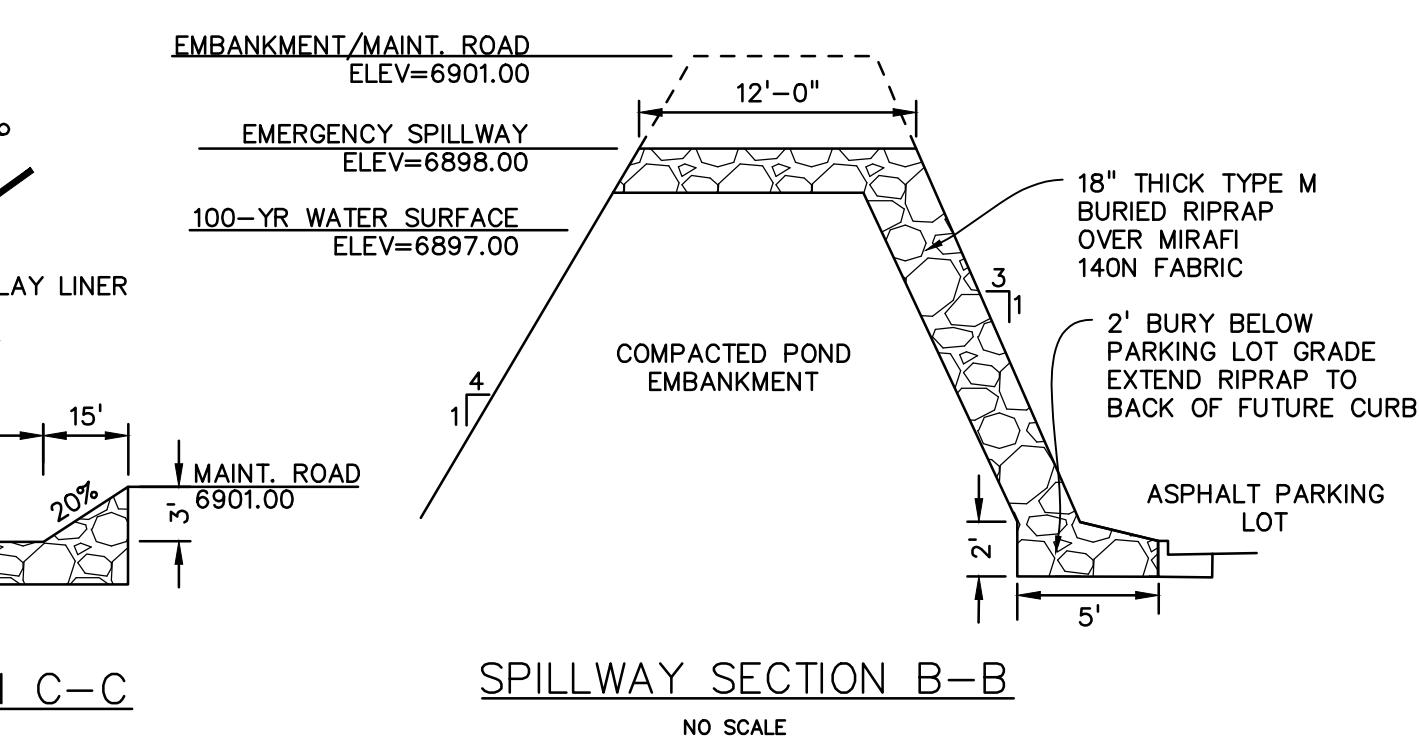
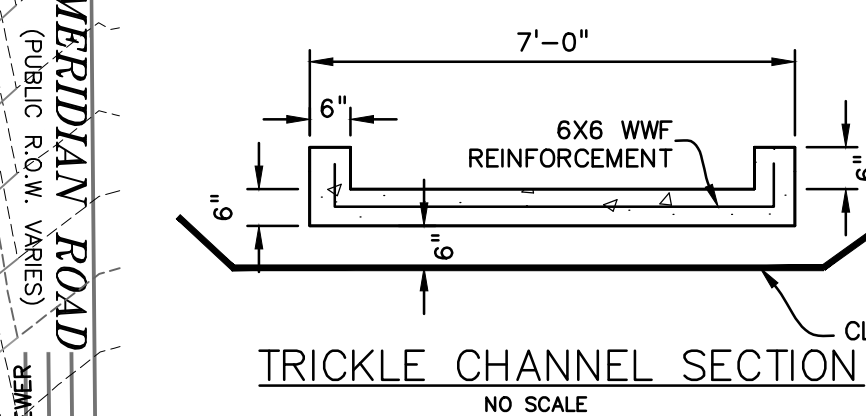
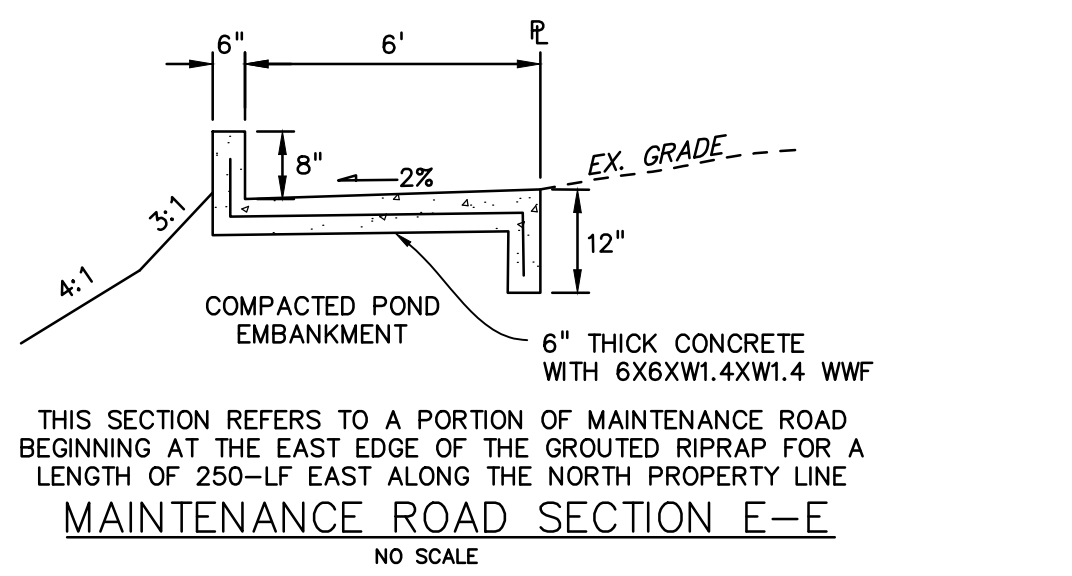
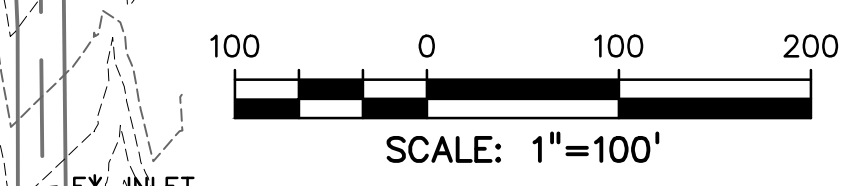
FLOW DIRECTION.....

DESIGN POINT.....

BASIN DESCRIPTION.....

BASIN AREA (ACRES).....

PRO. INLET LABEL.....



PREPARED BY:

DREXEL, BARRELL & CO.
Engineers-Surveyors
3 SOUTH 7TH STREET
COLORADO SPGS, COLORADO 80905
CONTACT: TIM D. McCONNELL, P.E.
(719)260-0887
BOULDER • COLORADO SPRINGS

CLIENT:

HUMMEL INVESTMENTS, LLC
8117 PRESTON ROAD, SUITE 120
DALLAS, TEXAS 75225
(214) 416-9820

PRELIMINARY PLAN FOR

FALCON MARKETPLACE

FALCON, COLORADO

ISSUE	DATE
INITIAL ISSUE	1-17-17
FDR	12-21-18

DESIGNED BY: TDM
DRAWN BY: KGV
CHECKED BY: TDM
FILE NAME:

PREPARED UNDER MY DIRECT SUPERVISION FOR AND ON BEHALF OF DREXEL, BARRELL & CO.

DRAWING SCALE:
HORIZONTAL: 1"=100'
VERTICAL: N/A

PROPOSED DRAINAGE CONDITIONS

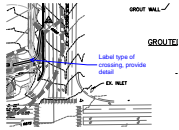
PROJECT NO. 20988-00CSCV
DRAWING NO.

D-1

SHEET: 1 OF 1

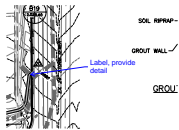
Markup Summary

dsdrice (43)



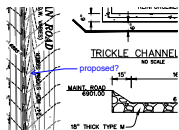
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Page Label: 159
Author: dsdrice
Date: 2/12/2019 9:27:29 PM
Color: ■

Label type of crossing, provide detail



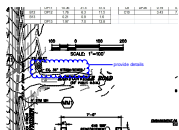
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Page Label: 159
Author: dsdrice
Date: 2/12/2019 9:27:46 PM
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Label, provide detail



Subject: Callout
Page Label: 159
Author: dsdrice
Date: 2/12/2019 9:30:02 PM
Color: ■

proposed?



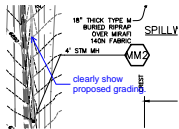
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Author: dsdrice
Date: 2/12/2019 9:30:45 PM
Color: ■

provide details



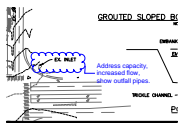
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Page Label: 159
Author: dsdrice
Date: 2/12/2019 9:33:06 PM
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Address existing and proposed drainage conditions and improvements on the east side of Meridian.



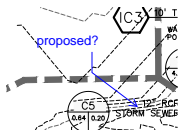
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Page Label: 159
Author: dsdrice
Date: 2/12/2019 9:33:09 PM
Color: ■

clearly show proposed grading.



Subject: Cloud+
Page Label: 159
Author: dsdrice
Date: 2/12/2019 9:34:09 PM
Color: ■

Address capacity, increased flow, show outfall pipes.



Subject: Callout
Page Label: 159
Author: dsdrice
Date: 2/12/2019 9:34:32 PM
Color: ■

proposed?

DECEMBER 21, 2019

SF-19-001

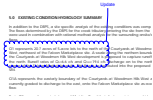
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SF-19-001



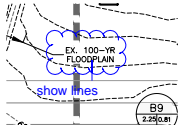
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Update to Dec 2018



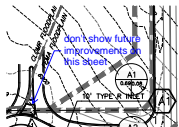
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Author: dsdrice
Date: 2/13/2019 3:10:49 PM
Color: ■

Update



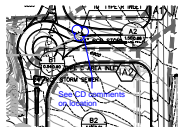
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Author: dsdrice
Date: 2/13/2019 3:13:47 PM
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show lines



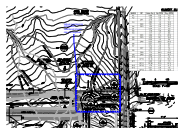
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Page Label: 159
Author: dsdrice
Date: 2/13/2019 3:15:51 PM
Color: ■

don't show future improvements on this sheet



Subject: Cloud+
Page Label: 159
Author: dsdrice
Date: 2/13/2019 3:16:24 PM
Color: ■

See CD comments on location



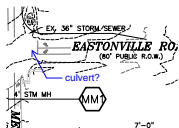
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Page Label: 159
Author: dsdrice
Date: 2/13/2019 3:17:25 PM
Color: ■

Adjust overlapping information. Additional sheets may be required.



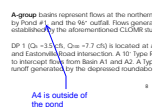
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Page Label: 159
Author: dsdrice
Date: 2/13/2019 3:18:03 PM
Color: ■

Show property lines



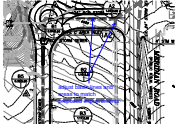
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Author: dsdrice
Date: 2/13/2019 3:20:40 PM
Color: ■

culvert?



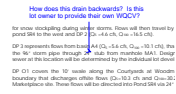
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Page Label: 11
Author: dsdrice
Date: 2/13/2019 3:21:26 PM
Color: ■

A4 is outside of the pond



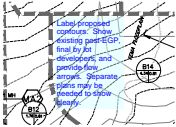
Subject: Callout
Page Label: 159
Author: dsdrice
Date: 2/13/2019 3:23:41 PM
Color: ■

adjust basin lines and areas to match proposed improvements



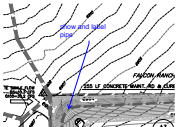
Subject: Callout
Page Label: 12
Author: dsdrice
Date: 2/13/2019 3:30:49 PM
Color: ■

How does this drain backwards? Is this lot owner to provide their own WQCV?



Subject: Text Box
Page Label: 159
Author: dsdrice
Date: 2/13/2019 3:33:32 PM
Color: ■

Label proposed contours. Show existing post-EGP, final by lot developers, and provide flow arrows. Separate plans may be needed to show clearly.



Subject: Callout
Page Label: 159
Author: dsdrice
Date: 2/13/2019 3:34:48 PM
Color: ■

show and label pipe



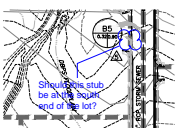
Subject: Text Box
Page Label: 159
Author: dsdrice
Date: 2/13/2019 3:37:28 PM
Color: ■

Label lots and tracts



Subject: Text Box
Page Label: 159
Author: dsdrice
Date: 2/13/2019 3:38:02 PM
Color: ■

Show and label easements



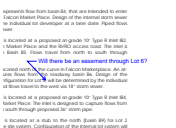
Subject: Cloud+
Page Label: 159
Author: dsdrice
Date: 2/13/2019 3:43:28 PM
Color: ■

Should this stub be at the south end of the lot?



Subject: Text Box
Page Label: 1
Author: dsdrice
Date: 2/14/2019 10:13:52 AM
Color: ■

See comment letter



Subject: Callout
Page Label: 12
Author: dsdrice
Date: 2/14/2019 11:34:16 AM
Color: ■

Will there be an easement through Lot 6?

Flows travel to the south via 24" storm pipe.
at the north side of the low point on Falcon
collects flow from boxes 010 and any flow
to south via 30" storm pipe.
at the south side of the low point on Falcon

End of cursory review.

Subject: Text Box
Page Label: 12
Author: dsdrice
Date: 2/14/2019 11:35:49 AM
Color: ■

End of cursory review.



Subject: Highlight
Page Label: 12
Author: dsdrice
Date: 2/14/2019 11:35:52 AM
Color: ■

In addition to the water main system, a proposed 24" RCP line is to be installed
to intercept the flow from the 24" RCP line to the south. This line will be installed
along the north side of the low point on Falcon
collects flow from boxes 010 and any flow
to south via 30" storm pipe.
at the south side of the low point on Falcon

Address Eastonville Road, Meridian Road, Woodmen
Frontage Road at southwest corner

Subject: Text Box
Page Label: 15
Author: dsdrice
Date: 2/14/2019 11:37:35 AM
Color: ■

Address Eastonville Road, Meridian Road,
Woodmen Frontage Road at southwest corner

water system, a proposed 24" RCP line is to be installed
at the Meridian Road/Astonville Road intersection
along 400 ft to the south. Median grading to the
existing landscaped median flow will be replaced
with a storm sewer manhole.
will be established for the private storm system, pr

for turn lane?

Subject: Callout
Page Label: 15
Author: dsdrice
Date: 2/14/2019 11:37:41 AM
Color: ■

for turn lane?

city basin intended to intercept the flow
at site. As with pond #1, in accordance with (1)
with permanent micropipe will release the WQCV
into the 18" RCP, and ultimately reach the
d.

MA1 PBMP?

OMM manuals will be established for Pond 2 and

Subject: Text Box
Page Label: 16
Author: dsdrice
Date: 2/14/2019 11:38:30 AM
Color: ■

MA1 PBMP?

a natural c
y benefits,

Subject: Delete
Page Label: 16
Author: dsdrice
Date: 2/14/2019 11:38:53 AM
Color: ■

Delete

the maximum average depth
1.5 ft (Pond #1) and basin under water quality facilities (Pond
only release the WQCV, adding to water quality treatment
and a regular maintenance program. The water flow will also
quality facilities through filtration and expansion pollution
detention. The water quality facilities will be installed in
water.
will be required to conduct the flow step process, and
city facilities as necessary.

Grass-lined?

Subject: Callout
Page Label: 16
Author: dsdrice
Date: 2/14/2019 11:39:18 AM
Color: ■

Grass-lined?

1	EA	\$75,000.00	\$75,000.00
1	EA	\$35,000.00	\$35,000.00
Public facilities subtotal			\$710,000.00
NCE Contingency			\$22,077.00
Cost Estimate Total			\$363,847.00

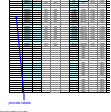
Falcon Marketplace
20988-00CSCV
KGV
TDM
ET Power Center

(Not checked on 1st review)

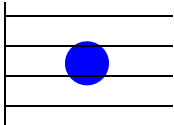
n Label design storm on these sheets.

Model	Yr	Scale	Total	Cap	Net	Price	Short Run	Long
Trade	Scale	Price	Trade	Cap	Net	Trade	Scale	Price
1000	1000	2.7	1000	1000	1000	1000	1000	1000
1000	1000	2.4	1000	1000	1000	1000	1000	1000

Label design storm on these sheets.

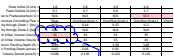


provide labels

[illegible]

The WQCV needs to be released over 40 hours with the EDB design.

The WQCV needs to be released over 40 hours with the EDB design.



The WQCV needs to be released over 40 hours with the EDB design.

The WQCV needs to be released over 40 hours with the EDB design.



provide details and forebay