PRELIMINARY/FINAL DRAINAGE REPORT

FOR

CROSSROADS MIXED USE FILING NO. 2 EL PASO COUNTY, COLORADO

NOVEMBER 2022

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The File Number has been added to the document.

FINAL DRAINAGE REPORT FOR CROSSROADS MIXED USE FILING NO. 2

DRAINAGE PLAN STATEMENTS

ENGINEERS STATEMENT

The attached drainage plan and report was prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the County for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.

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Update report contents to change any mention of the FSD pond to the new BMP that is being used throughout the report.

The report has been updated to change any mention of FSD to the new UGD.

FOR CROSSROADS MIXED USE FILING NO. 2

Purpose

This Final Drainage Report for Crossroads Mixed Use Filing No. 2 is in support of the Final Plat, Preliminary Plan, and Construction Drawings of the subject site. This report functions to identify the existing and proposed runoff patterns and recommend proposed drainage improvements which are intended to safely convey runoff through the proposed development, while minimizing impacts to downstream facilities and adjacent properties.

The Final Plat and Construction Drawings for this site will be submitted concurrently with this report. Individual drainage letters and/or reports shall be required with the development of each lot not otherwise clearly analyzed by this report for Crossroads Mixed Use Filing No. 2.

Project Location and Description

The subject site is located in the south half of Section 8, Township 14 South, Range 65 West of the 6th P.M. in El Paso County, Colorado. The 12.016 Acre site is currently undeveloped. The site is bound to the west by the planned Southern Rail Point, to the north by the Meadowbrook Parkway, south by Highway 24, and to the east by Newt Drive. The proposed site will be developed into two (2) commercial lots, three (3) tracts, and two (2) private roadways through the site.

The majority of the existing site is covered with native grasses with fair to good cover. Known earthwork operations for "borrow material" have occurred over a small area of the eastern portion of the site in early to mid-2019, but have since stabilized. Generally, the site slopes from east to west slightly greater than 1% with some localized depressions. Some of these may be the results of previous earthwork activities. The site lies within the Sand Creek Drainage Basin. No existing drainage facilities or improvements are onsite, however, surrounding drainage facilities are planned and will connect onsite. No known irrigation systems or wells are present.

Soils

Soils in the project area have been determined to be Blakeland Loamy Sand (8) and Blendon Sandy Loam (10), which are characterized to be part of Hydrologic Soil Types "A" & "B" as determined from the United States Department of Agriculture (USDA) Natural Resources Conservation Service (NRCS) "Web Soils Survey". A soils map illustrating the site location and soil types is provided in the appendix of this report.

Floodplain Statement

According to the Federal Emergency Management Agency (FEMA) Flood Insurance Rate Map (FIRM) Nos. 08041C0754 G & 08041C0752 G, effective date December 7th, 2018, none of the site lies within a designated floodplain. A copy of these annotated maps can be found in the appendix. The Sand Creek East Fork Channel is located to the northwest of the adjacent Meadowbrook Crossing subdivision.

Previous Studies

The area which encompasses Crossroads Mixed Use Filing No. 2 has been previously studied. Below is a short outline of the assumptions regarding the lands of the subject site and those based upon the previously assembled and approved drainage reports and how the assumptions within them impact the subject site.

"Crossroads Mixed Use Filing No.1 Final Drainage Report, prepared by M&S Civil Consultants, Inc., dated February 2021, revised February 2022.

• Establishes all historic, existing, and future drainage patterns and detailed drainage information for the proposed site and adjacent properties.

"Sand Creek Drainage Basin Planning Study, Preliminary Design Report", prepared by Kiowa Engineering Corporation, dated January 1993, revised March 1996.

- Establishes that the subject site falls within the East Fork Sand Creek Drainage Basin, a portion of the larger Sand Creek Watershed
- Establishes that there are no requirements for major infrastructure improvements and subsequently no drainage-improvement related reimbursements with the development of this parcel
- Drainage fees shall be required to plat the subdivision

"Claremont Business Park Filing No.2 prepared by Matrix Design Group, revised November 2006

- Establishes the drainage patterns of offsite Basins 0S-4 and E2 which are to be conveyed within the Meadowbrook Rights of Way
- Established up-gradient offsite drainage to be directed under Meadowbrook north to offsite East Fork Sand Creek Channel, and away from the subject site

"Final Drainage Report, Lot 1 24/94 Business Park Filing No.1 prepared by Core Engineering Group, dated July 14, 2016

• The development of the 24/94 Business Park FDR shows future curb inlets along the future Meadowbrook Parkway extension on the south and west corners of the intersection to

- capture runoff from up-gradient watersheds in addition to a proposed inlet which was to be located above the intersection at the northwest corner of the subject site.
- Establishes that flows from the parcel upstream of the convenience store (29/94 FDR Basin OS4) EX-B now to be collected by the extension of a 36" RCP along the south side of Meadowbrook Parkway. Runoff within the right of way/roadway separated out as Basin EX-A2.
- Continues assumption that flows from Newt Drive be conveyed north to East Fork Sand Creek.
- Evaluated pre-development drainage patterns for subject site including direct discharge flow rates to the CDOT rights of way of 1.9 and 14.5 cfs for the 5 and 100 year events, respectively. (Basin EX-E).

"Preliminary and Final Drainage Report Meadowbrook Crossing Filing No. 1 and Filing 2, El Paso County, Colorado prepared by Kiowa Engineering Corporation, dated July 25, 2017

- Proposed the installation of a future 10' Type R inlet at the southeast corner of Newt Drive and Meadowbrook Parkway with the extension of Meadowbrook Parkway to the west (along the northern boundary of the subject site). The inlet was to function to collect offsite runoff from a portion of the south half of Meadowbrook Parkway and Newt Drive north of Hwy 24. Intercepted runoff would be conveyed via a proposed 24" storm sewer to the existing storm sewer system within the Meadowbrook Crossings development.
- Proposed the installation of a 10' Type R inlet at the west end of future Meadowbrook Parkway. The inlet was to collect runoff from the north half of the future roadway. An 18" storm drain was proposed to convey collected runoff to the existing water quality pond located within the Meadowbrook Crossings Development. The report indicates a separate forebay or the modification of an existing forebay would be required.
- Shifted the location of the existing 10' Type R curb inlet to be installed upstream of the intersection of Newt Drive (as shown with the 24/94 Business Park FDR), flows in excess of the inlet capacity are to continue within the future Meadowbrook.

"Final Drainage Report for Meadowbrook Dirt Borrow Site, El Paso County Colorado, prepared by M&S Civil Consultants, November 2018.

- Evaluated onsite drainage patterns
- Excluded offsite runoff impacts from areas to the east of site.
- Allowed site to be utilized as a "borrow site" for offsite earthwork activities.

Hydrologic Calculations

Hydrologic calculations were performed using the El Paso County and City of Colorado Springs Storm Drainage Design Criteria manual and where applicable the Mile High Flood District Manual. The Rational Method was used to estimate stormwater runoff anticipated from design storms with 5-year and 100-year recurrence intervals.

Hydraulic Calculations

Hydraulic calculations were estimated using the Manning's Formula and the methods described in the El Paso County and City of Colorado Springs Storm Drainage Design Criteria manual. Storm drains were designed using parameters and criteria summarized in Chapter 8 of El Paso County's Drainage Criteria Manual Vol. 1 and the City of Colorado Springs Drainage Criteria Manuals. Parameters such as Manning's values of 0.13 were used for concrete pipe flow, and design considerations for minimum freeboard and maximum velocities were applied. The relevant data sheets are included in the appendix of this report. Hydraulic grade line calculations for the storm system in the ultimate (future) condition are provided in the Appendix of this Final Drainage report.

Drainage Criteria

This drainage analysis has been prepared in accordance with current El Paso County Drainage Criteria Manual and, where applicable, City of Colorado Springs and Mile High Flood District Criteria Manuals. Calculations were performed to determine runoff quantities for the 5-year and 100-year frequency storms for developed conditions using the Rational Method as required for basins having areas less than 100 acres. See Appendix for supporting calculations.

Existing Drainage Characteristics

The subject site has been utilized as a "borrow site" to provide surplus earthwork to offsite developments in the area. This recent grading effort occurred during the spring and summer of 2019. At the request of El Paso County, an existing conditions drainage analysis has been provided to show the changes to the topography and drainage patterns as a result of this effort. As the only changes between the two conditions are onsite, the offsite drainage patterns calculations and assumptions determined within the historical analysis will remain the same. Specifically, historical basins E2, EX-A2, OS-A, and OS-1 correlate to existing DP1, DP2, and DP3, respectively. It should be noted that the subject site was not disturbed to the full extent of the approved plan, with limited excavation primarily occurring within the eastern side of the site. For historic (pre-grading) drainage information, refer to the Crossroads Mixed Use Filing No. 1 FDR/MDDP (CMU1 MDDP) by M&S Civil Consultants, Inc (see appendix).

In the existing condition, vegetation remains sparse, consisting primarily of native grasses and weeds with good to fair cover. Areas disturbed by grading activities were reseeded and have since stabilized. With regards to historic versus existing drainage basin delineation, the bisecting parcel ridgeline has been relocated further to the south, which results in redirecting more of the runoff to the southwestern part of the site and less to the CDOT rights of way. The few small depressions remain on site, near the west boundary. For the purposes of hydrologic analysis, these small depressions will continue to not be evaluated for their ability to detain runoff. Ultimately, all runoff from the parcel is conveyed to the west towards existing drainage facilities located under Peterson Road and ultimately the East Fork of Sand Creek as in the historic condition.

This section only discusses the changes in basin geometry and drainage pattern and provides a direct comparison of the historic versus existing conditions, utilizing the same outfall (design) points, which have remained undisturbed.

Design Point 1

Basins E2 and EX-A2 geometry were derived from their respective reports. Flow velocity equations, conveyance coefficients, and time of concentration equations have been modified since these reports were approved, therefore, these parameters were remodeled with El Paso's hydrologic criteria current to this report's date. Excerpts of reported calculations for these basins are provided in the Appendix for comparison. Basin E2 (Claremont Business Park Filing No.2) consists of a reported 3.86 developed acres of development located along the southeastern half of existing Meadowbrook Parkway, some 1200' northeast of the subject site. Runoff produced by the offsite development (CBPF2 Lot 46) is conveyed to Meadowbrook Parkway at flow rates of Q5=15.1 and Q100=28.6 cfs in the 5 and 100-year storm events respectively. The collected flows combine with runoff from Basin EX-A2 (Lot 1 24/94 Business Park Filing No.1) (Q5=2.5, Q100=4.5 cfs) which consists of 0.59 acres of the southeastern half of Meadowbrook Parkway, and is located immediately east of existing Newt Drive. The collected flows from the two basins culminate at **Design Point 1** at peak rates of Q5=14.2 and Q100=26.5 cfs. An existing 10' CDOT Type R atgrade inlet (Inlet 1) intercepts flows of Q5=8.4 and Q100=11.1 cfs, with subsequent by-pass flows of 5.8 and 15.4 cfs in the 5 and 100 year events. Surface flows continue west within the south half of existing Meadowbrook Parkway.

Design Point 2

Basin OS-A (Meadowbrook Crossing Filing 1 and 2) consists of 1.29 acres of the northern half of existing Meadowbrook Parkway located immediately east of Newt Drive. Runoff produced within this basin totals Q5=3.1 and Q100=6.0 cfs. These calculated flows differ 0.1 cfs from reported flows due to the significant digits used for the basin acreage in the flow calculation, yet can be viewed as conservative values since they are higher. An existing 10' CDOT Type R at grade inlet (**Inlet 2**) collects runoff of Q5=3.1 and Q100=5.3 cfs, with subsequent by-pass flows in only the 100 year event of 0.7 cfs. Runoff leaving the design point continuing west within the north half of existing Meadowbrook Parkway.

Design Point 3

Basin OS-1 consists of approximately 1.28 developed acres of existing Newt Drive located along the eastern boundary of the site. Runoff produced within the basin (Q5=5.8 cfs, Q100=10.5 cfs) combine with flow-by from **DP1** in the intersection at peak flow rates of 9.8 cfs, and 22.5 cfs in the 5 and 100-year storm events.

Surface runoff and by-pass flows from both **DP2** and **DP3** enter **Basin A** in the undeveloped rights of way of future Meadowbrook Parkway, at the northeast corner of the site.

Design Point 4

Basin A (Q5=1.5, Q100=11.1 cfs) currently consists of 11.02 acres which continues to drain from east to west eventually discharging along the western boundary of the site, approximately 250'

south of the northern property line. Peak runoff, post-grading, is 7.1 and 25.5 cfs in the 5-year and 100-year events respectively.

Design Point 5

Basin B (Q5=2.0, Q100=14.5 cfs) consists of 17.31 acres that drains from northeast to southwest, eventually discharging along the western boundary of the site, approximately 200' north of the southern property line. Peak runoff rates at this location are 2.0 cfs and 14.5 cfs in the 5-year and 100-year events respectively.

Design Point 6

Basin C consists of 3.99 undeveloped Right of Way at the southern bounders in the 5-year and 100-year event

Provide narrative for DP 6.5, DP 8, DP 9 and DP 12. The "existing drainage map" has different

The "existing drainage map" has different design points that do not effectively correlate to the design points mentioned above from the "proposed drainage map".

Design Point 7

Basin OS-2 (Q5=8.7, Q100=19.6 cfs) consists of 4.98 acres of the northern half of the US HWY 24 roadway and adjoining native grass lined barrow ditch. Runoff produced within the basin combines with runoff from **DP6** at lower cumulative peak runoff rates of 9.9 and 28.0 cfs in the 5 and 100-year storm events at **DP7**. A cross section of the ditch at the M&S has clarified that the UGD will event for comparison purposes and is provided in the appendix be completed as part of Filing No.1.

Four Step Process

Clarify that this being done in Filing 1.

Step 1 Employ Runoff Reduction Practices – Approx. 2.54 acres of the proposed development is being set aside for a Full Spectrum Detention (FSD) Pond. Whenever possible, runoff produced within developable area containing impervious surfaces will be routed through landscaped areas or earthen swales (grass-lined where slope exceeds 2%) to minimize direct connection of impervious surfaces. In the interim, runoff will be reduced through the use of (4) temporary sediments ponds until the ground has been stabilized with proceedings of the TSBs (one Show location on plans). Show location on plans

Step 2 Stabilize Drainageways The development for the Filing No. 2 site plans. In the interim, the site proposes four temporary sedimentation ponds, before discharging at the southwest property corner of the site and onto an adjacent undeveloped property via riprap-lined spillways. This ensures that in this stage of the development negative effects on the downstream drainage ways will be avoided.

In the proposed and future conditions, the flow is discharged to the same location offsite through an RCP pipe outfall lined with rip rap. From here it continues southwest in CDOT's man-made roadside ditch until it reaches Peterson Road. It is then conveyed to the other side of the road, into a similar earthen channel, via a 36" CMP culvert. The drainage continues southwest in the right of way, until it reaches the East Fork Sand Creek Channel. Existing rip rap barriers are lined throughout this portion of the pathway approximately every 90-100 feet within the ditch to the channel bank. The Drainageway Exhibit provided in the Drainage Maps section of the Appendix provides a visual representation of this information. Roadside ditch calculations for various storm events are provided

for the selected suitable downstream outfall (project site's discharge location) to ensure the facility can adequately contain and convey the flows.

Step 3 Provide Water Quality Capture Volume (WQCV)— The site will use a Full Spectrum Detention (FSD) Pond to control developed runoff that is discharging into an existing CDOT ROW roadside ditch and ultimately into Sand Creek. The FSD pond's outlet structure will be designed to drain the water quality event storm in 40 hours, while reducing the 100 year peak discharge to approximately 90% of the predevelopment conditions.

Step 4 Consider Need For Selecting Industrial And Commercial BMP's – The proposed development will implement a Stormwater Management Plan including property housekeeping practices, spill containment procedures, and coverage of storage/handling areas. Specialized BMP's are not required since the vertical development of the commercial areas are unknown at this time.

Proposed Drainage Characteristics

The future site will be developed into two (2) commercial lots, three (3) tracts, and two (2) private roadways. The proposed development will extend Pacific Rail Point and Central Rail Way into the site to provide access and a utility corridor to both the commercial and residential developments. At this time, it is anticipated that the development and design of Lot 1 and Lot 2 (by others) is planned to occur following the construction of the proposed utilities and infrastructure provided by this plan. A separate drainage letter or report will be required for that portion of the development.

The following summary generalizes the proposed drainage patterns and drainage improvements required to safely route developed runoff to downstream facilities.

Off-site flows within the existing Meadowbrook Parkway will be collected by a pair of sump inlets located at the west end of the roadway, then routed south to the planned off-site FSD. Pacific Rail Point(private) and Central Rail Way(private) will provide access and utility corridors for development. Private storm sewer mains, stubs, and inlets will be extended along these corridors to serve the development. The extension of these facilities beyond what is shown by this plan is likely with future development. All onsite storm sewer and drainage improvements shall be private. Storm sewer pipes and inlets will be constructed along, and tie in at the southwest boundary of the proposed Central Rail Way to aid in collecting runoff from the site. These facilities will connect at the west side of the proposed site to the planned system located east of the planned Southern Rail Point. Runoff collected by the infrastructure will be conveyed west and south, then off-site through a 36" storm pipe. Proposed on-site flows will continue off-site through planned storm pipes, where the flows will combine with adjacent lot flows and continue through planned storm pipes to the planned single full spectrum detention pond loc. The section has been updated to include all of the outfall from the pond will discharge into the exi requested information regarding the UGD proposed the existing CDOT Right of Way as per the CM in Filing No.1 for water quality and detention.

Update entire section to discuss the proposed underground water quality system. Include information on TSS removal and/or WQCV, whichever is being used to meet WQ criteria. For TSS information make sure to include provided rate vs what is required per criteria. Include project number and name for submitted deviation request and cdr project.

Proposed Detailed Drainage Discussion

Design Point 1*

Off-site Basin E2 (Claremont Business Park Filing No.2) consists of a reported 3.86 acres of development located along the southeastern half of existing Meadowbrook Parkway some 1200' northeast of the subject site. Runoff produced by the offsite development (CBPF2 Lot 46) is conveyed to Meadowbrook Parkway at flow rates of Q5=15.1 and Q100=28.6 cfs in the 5 and 100-year storm events respectively. The collected flows combine with runoff from Basin EX-A2 (Lot 1 24/94 Business Park Filing No.1) (Q5=2.5, Q100=4.5 cfs) which consists of 0.59 acres of the southeastern half of Meadowbrook Parkway located immediately east of existing Newt Drive. The collected flows from the two basins culminate at Design Point 1 at peak rates of Q5=14.2 and Q100=26.5 cfs. An existing 10' CDOT Type R at-grade inlet (Inlet 1) intercepts flows of Q5=8.4 and Q100=11.1 cfs, with subsequent by-pass flows of 5.8 and 15.4 cfs in the 5 and 100 year events. Surface flows continue west within the south half of existing Meadowbrook Parkway. Flows at DP1 are consistent with planned flows at this location from the CMU1 MDDP.

Design Point 2*

Off-site Basin OS-A (Meadowbrook Crossing Filing 1 and 2) consists of 1.29 acres of the northern half of existing Meadowbrook Parkway located immediately east of existing Newt Drive. Runoff produced within this basin totals Q5=3.1 and Q100=6.0 cfs. An existing 10' CDOT Type R at grade inlet (Inlet 2) collects runoff of Q5=3.1 and Q100=5.3 cfs, with subsequent by-pass flows in only the 100 year event of 0.7 cfs. Runoff leaving the design point continuing west within the north half of existing Meadowbrook Parkway. Flows at DP2 are consistent with planned flows at this location from the CMU1 MDDP.

Design Point 3*

In accordance with the assumptions outlined within the Meadowbrook Subdivision Final Drainage Report, an offsite public storm sewer pipe and inlet will be constructed at the southwest corner of the proposed roundabout to aid in collecting runoff from a portion of the offsite watershed located to the east of the site. A new manhole is not anticipated to be required to connect the outfall to the existing pipe located inside the existing Meadowbrook Subdivision. As this area is already paved, increases to the imperviousness of this area are not anticipated.

Off-site **Basin OS-1** consists of approximately 1.40 acres of existing Newt Drive that will be retrofitted with new raised median as part of an intersection conversion to a roundabout. Runoff produced within the basin (Q5=6.4 and Q100=11.5 cfs) will combine with flow-by from **DP1** at peak rates of Q5=10.2 and Q100=23.3 cfs at a proposed public 10' at-grade inlet (**Inlet 3**: Q5=6.7, Q100=9.8 cfs intercepted; Q5=3.5, Q100=13.5 cfs flowby) located at **DP3**. A proposed public 24" storm sewer (**PR1**) will convey water across the intersection to the existing 42" storm sewer with Meadowbrook Crossings in accordance with that subdivision's drainage report. The existing manhole connection has been determined to be sufficient following construction of this proposed inlet and storm sewer. It is important to note that this connection also remains feasible as the roundabout is not anticipated to significantly increase the overall imperviousness of the area above that of the existing condition. Runoff in excess of the inlet capacity will continue westward via the

curb and gutter of existing Meadowbrook Parkway. Flows at **DP3** are consistent with planned flows at this location from the CMU1 MDDP.

Design Point 4*

Off-site **Basin A** consists of 1.67 acres of the north half of existing Meadowbrook Parkway. Runoff within this basin (Q5=6.5 and Q100=11.6 cfs) combines with flow by from **DP2** for total flows of 6.5 and 12.4 cfs in the 5 year and 100 year events, respectively. A proposed 15' at-grade inlet (**Inlet 4:** Q5=6.5, Q100=10.6 cfs intercepted; Q5=0.0, Q100=1.8 cfs flowby) is located at the west end of the roadway just before the proposed temporary cul-de-sac. This inlet conveys intercepted flows to **PR1.5**, a proposed 24" RCP public storm sewer. Flowby from the 100 year event continues west to downstream infrastructure. Flows at **DP4** are consistent with planned flows at this location from the CMU1 MDDP.

Design Point 4.5*

1.8 cfs of flowby in the 100 year event continues west from **DP4** towards off-site **Inlet 4.5**, a **NEENAH R-2501 Type C Grate** lid and frame at the low point of the cul-de-sac. Supporting calculations for this non-standard inlet are provided in the Appendix. This inlet is anticipated to reach a maximum depth of 0.5' in order to convey this flow underneath the roadway via a proposed public 24" storm sewer (**PR2**). The NEENAH inlet is to be removed and replaced with a standard CDOT 5' Type R inlet when the roadway cul de sac is removed and the roadway is extended to the west with future development. In the case of inlet clogging, overflow will collect at **DP5**, which has an additional 13.3 cfs capacity. Flows at **DP4.5** are consistent with planned flows at this location from the CMU1 MDDP.

Design Point 5*

Off-site **Basin B** consists of 1.48 acres of the southern half of existing Meadowbrook Parkway. Runoff produced within this basin (Q5=5.8 and Q100=10.3 cfs) combines with flow-by leaving **DP3** at peak flowrates of Q5=9.9, Q100=25.8 cfs. A proposed public 15' sump inlet (**Inlet 5**: Q5=10.1, Q100=26.3 cfs intercepted; no flowby) located at west end of the roadway will prevent developed flows from leaving exiting the roadway corridor. The intercepted runoff will combine with **PR2** flows in a 36" private storm sewer system (**PR3**, **by others**). Combined flows within the planned system are calculated to reach peak rates of 16.5 and 38.4 cfs. The storm sewer system is to be planned by others through the multi-family site (Lot 11) but ultimately will tie back into the system at **DP15**. In case of inlet clogging, overflows will overtop the curb on the southern side onto the apartment site and be conveyed to the swale on the west side of the site. Flows at **DP5** are consistent with planned flows at this location from the CMU1 MDDP.

Design Point 6

Basin C (Q5=9.3, Q100=17.4 cfs) consists of 2.36 acres of the northern portion of commercial Tract C located along the east side of the site. A proposed private 30" storm sewer (**PR4**) is provided to collect and convey flows of Q5=9.3 and Q100=17.4 cfs in the 5 and 100-year storm event, respectively. Intercepted flows are conveyed west underground within the roadway tract. **PR4** was treated as a flared end pipe for rational method calculation purposes, to account for future development.

Design Point 6.5

Basin C1 (Q5=9.3, Q100=17.4 cfs) consists of 2.19 acres of the southern portion of commercial Tract C located along the east side of the site. A proposed private 30" storm sewer (**PR4.5**) is provided to collect and convey flows of Q5=9.3 and Q100=17.4 cfs in the 5 and 100-year storm event, respectively. Intercepted flows from **PR4** and **PR4.5** are conveyed west underground within the roadway tract through **PR5-PR7** at flow rates of Q5=18.7 and Q100=34.7 cfs.

Design Point 7

Basin D consists of 2.21 acres of commercial Tract B located between existing Meadowbrook Parkway, proposed Central Rail Way, proposed Pacific Rail Point, and planned Southern Rail Point. **Basin D**, which includes portions of Lots 9 and 10, will require a private 24" storm drain (**PR8**) to collect peak flows of Q5=9.3 and Q100=16.9 cfs from this basin in the 5 and 100 year storm events, respectively.

Design Point 8

Basin E (Q5=3.3, Q100=6.0 cfs) consists of 0.84 acres of a portion of commercial lots, the northern half of proposed Central Rail Way and the western half of proposed Pacific Rail Point. A private 10' CDOT Type R at-grade inlet (**Inlet 6:** Q5=4.0, Q100=6.0 cfs intercepted; Q5=0.0, Q100=0.0 cfs flowby in proposed conditions) is located on the north side of the roadway to intercept flows. Runoff bypassing this inlet continues to downstream infrastructure. Flows collected from the inlet combine with **PR8** and are conveyed to a box base manhole in the center of the proposed Central Rail Way via a proposed private 30" (**PR9**) storm drain at flow rates of Q5=12.4 and Q100=21.4 cfs. Within the manhole, flows from **PR9** then combine with flows from **PR7** and continue to flow through a proposed private 36" (**PR10**) storm drain at flow rates of Q5=29.5 and Q100=53.0 cfs.

Design Point 9

Basin E1 (Q5=6.3, Q100=11.4 cfs) consists of 1.62 acres of commercial lots, the southern half of Central Rail Way, and the eastern half of Pacific Rail Point. A private 10' CDOT Type R at-grade inlet (**Inlet 7:** Q5=5.5, Q100=7.7 cfs intercepted; Q5=0.8, Q100=3.7 cfs flowby) is located on the south side of the Central Rail Way to intercept flows. Runoff bypassing this inlet continues to downstream infrastructure. Flows collected from the inlet combine with flows from (**PR10**) and are conveyed south to a box base manhole on the south side of the roadway via a private 36" (**PR11**) storm drain and continue west underground at flow rates of Q5=35.0 and Q100=60.7 cfs. **PR12**, a planned 42" private storm sewer, then directs the system south from another manhole. Pipe flows at Q5=6.9 and Q100=13.8 cfs from the neighboring planned apartment site (**PR11.5**, private 24" RCP) combine with flows from **PR12** in a planned private 48" storm drain (**PR12.5**) at flow rates of Q5=43.2 and Q100=77.4 cfs. The proposed flows exiting the site through **PR11** are 0.1 and 0.3 cfs less than the planned flows from the CMU1 MDDP for the 5 and 100-year events, respectively.

Design Point 10*

Off-site **Basin G** (Q5=2.1, Q100=3.8 cfs) consists of 0.46 acres of multi-family lots and roadway located southwest of the proposed site at the southwest edge of planned Southern Rail Point. A private 10' CDOT Type R sump inlet (**Inlet 8**: Q5=2.1, Q100=3.8 cfs; no flowby) located on the west side of the street functions to collect the runoff from **Basin G. PR13**, a proposed 18" private storm sewer, will direct runoff east to a box base manhole at peak flow rates of 2.1 cfs and 3.8 cfs in

the minor and major storm events, respectively. In the case of inlet clogging, overflow is directed to the swale at **DP13**. Flows at **DP10** are consistent with planned flows at this location from the CMU1 MDDP.

Design Point 11*

Off-site **Basin G1** (Q5=2.7, Q100=4.9 cfs) consists of 0.59 acres of commercial lots and roadway located southwest of the proposed site at the southeast edge of planned Southern Rail Point. A private 15' CDOT Type R sump inlet (**Inlet 9:** Q5=3.5, Q100=8.7 cfs intercepted; no flowby), located on the east side of planned Southern Rail Point to collect the runoff from **Basin G1** as well as bypass flows from **DP8 and DP9**, totaling Q5=3.5 and Q100=8.7 cfs. **PR14**, a proposed 30" private storm sewer, will direct runoff west to an underground box base manhole at peak flow rates of 3.5 cfs and 8.7 cfs in the minor and major storm events, respectively. From the junction, flows from **PR12.5**, **PR13**, and **PR14** combine at **PR15** (Q5=47.7, Q100=87.7 cfs), a 48" private storm sewer, and are directed south. In the case of inlet clogging, overflows will overtop the curb and collect in the rip rap protected depression at **DP12**.

Design Point 12*

Basin F consists of 2.72 acres of on-site commercial lots (Lot 1 and portions of Lot 2) located along the southwestern boundary of the site. A private planned 24" storm drain (**PR16**) is provided to collect the basin flows of Q5=11.4 and Q100=20.8 cfs at **DP12** in the 5 and 100 year events, respectively. Intercepted flows are conveyed west underground to the main line where they combine with flows from **PR15** at a manhole junction. **PR17**, a private 48" RCP storm sewer directs the collected runoff at rates of Q5=57.3 and Q100=105.1 cfs to a manhole which joins with a private 30" RCP, **PR21** (Q5=2.1, Q100=4.2) at combined peak flow rates of Q5=58.2 and Q100=107.3 cfs. The collected flows are conveyed southwest via **PR18** (Private 48" RCP) until discharging into the planned forebay at **DP15**. Flows at **DP12** are greater than planned flows at this location from the CMU1 MDDP.

Design Point 13*

Off-site **DP13** consists of a 2' bottom earthen swale that is designed to convey overflow runoff from the planned apartment complex site, west of the proposed site (**Basin A-5 Overflow**: Q5=0.9, Q100=7.8 cfs, **Basin Z-1**: Q5=0.47, Q100=1.27 cfs, and **Basin D-1 Overflow**: Q5=0.0, Q100=1.5 cfs) to the northwest corner of the pond. This swale joins another on the west end of the property (**DP14**) that ultimately conveys flows into the pond. Overflows from the apartment site were obtained by using flowby from the "Final Drainage Report for Aura at Crossroads" MHFD inlet sheets, which are provided in the appendix. The maximum runoff expected at **DP13** is 1.3 and 10.9 cfs in the 5 and 100 year events, respectively.

Design Point 14*

Off-site **DP14** represents the v-shaped, earthen swale located west of the proposed site that collects flows not anticipated to be collected by the planned apartment site's storm sewer (**Basin Z-2**: Q5=0.57, Q100=1.43 cfs), and combines with flows from **Design Point 13**. Runoff collected within this swale (maximum Q5=2.0 cfs, Q100=9.7 cfs) is conveyed from north to south to the planned FSD pond at **DP15**. Calculations for this swale before (Section B-B') and after (Section D-D') the junction are provided in the appendix of this report. Anticipated flows for **Basin Z-2**

from "Final Drainage Report for Aura at Crossroads" were used to determine swale cross section prior to the junction location, and combined flows with **DP13** were used for after. North American Green SC-250 erosion control blanketing or approved equal shall be used as swale protection and was selected based on flow velocity.

Design Point 15*

Off-site **Basin J** consists of 3.21 acres of the planned Tract for the full spectrum detention pond located southwest of the proposed site. Runoff produced within this basin reaches peak runoff rates (Q5=2.3 and Q100=10.0 cfs) combines with flows from **DP14** and **PR18** (planned 48" private RCP) in the pond. **PR19** (planned 48" private RCP) represents the tie in point for the apartment site storm sewer, and conveys collected flows into the planned forebay. The cumulative flows at **FSD Pond 1** are Q5=117.0 and Q100=229.7 cfs. Flow exiting the pond will be routed to the existing 5' bottom earthen swale (Planned Section A-A' Analyses) in CDOT's Right of Way at **DP16** via 18" private **PR20** (Q5=1.2 and Q100=11.4 cfs). A rip rap pad (Type L, D50=9") is provided as outlet protection. Flows at **DP15** are 0.3 cfs greater and 7.3 cfs less than the planned flows at this location from the CMU1 MDDP for the 5 and 100-year events, respectively.

Design Point 16*

Off-site **Basin OS-2** consists of 4.98 acres. Approximately half of this basin is comprised of the paved surface of U.S. Highway 24, while the other half is comprised of the 5 foot bottom earthen swale in CDOT's Right of Way. Runoff produced within this basin (Q5=8.7 and Q100=19.6 cfs) flows from northeast to southwest, combining with outfall flows from **DP15**. This combination of runoff collects in the existing swale in the right of way. According to the CMU1 MDDP, the pond releases flows at Q5=1.2, Q100=11.4 cfs. Thus, the cumulative flows at **DP16** are the same as the planned flows in the CMU1 MDDP at Q5=9.9 and Q100=31.0 cfs. Flows from this design point continue to downstream infrastructure.

*See Crossroads Mixed Use Filing No.1 FDR/MDDP ("CMU1 MDDP") by M&S Civil Consultants, Inc. dated February 2022, in the appendix for predevelopment, historic, and future condition comparison for the intermediate events at these locations.

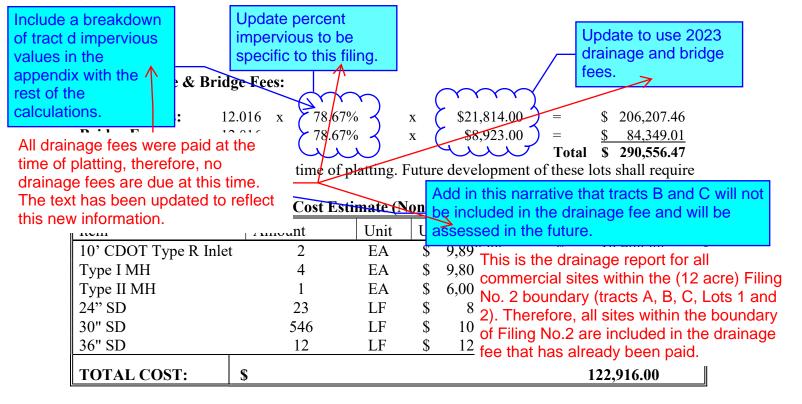
Water Quality Provisions and Maintenance

See comment on step #3 on four step process and update this narrative accordingly to include system being used and maintenance of BMP.

The off-site planned full spectrum detention (FSD) pond tunctions to provide detention and water quality for the proposed development. Refer to the CMU This section has been updated for the use calculations regarding this planned full spectrum detention of the new BMP (UGD) from Filing No.1.

Erosion Control

It is the policy of the El Paso County that M&S Civil Consultants submit a grading and erosion control plan with the drainage report. The plan includes proposed silt fence and vehicle tracking control as proposed erosion control measures. The plan also includes provisions for stockpiling, staging, and concrete washout areas. A stormwater management plan is provided to accompany the plans.



M & S Civil Consultants, Inc. (M & S) cannot and does not guarantee the construction cost will not vary from these opinions of probable costs. These opinions represent our best judgment as design professionals familiar with the construction industry and this development in particular. The above is only an estimate of the facility cost and drainage basin fee amounts in 2022.

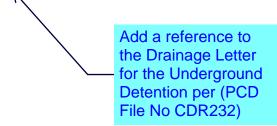
Summary:

The construction of this site is for the purposes of creating a commercial site (Lots 1, 2, Tract A, Tract B and Tract C) in the proposed condition. The site will be graded and all disturbed areas will be seeded. Proposed post construction runoff will be discharged from the site at **DP9** and At **DP9**, the proposed runoff is 0.1 and 0.3 cfs less than the planned runoff from the CMU1 MDDP for the 5 and 100-year events, respectively. At **DP12**, the proposed runoff is 0.6 and 1.2 cfs greater than the planned runoff from the CMU1 MDDP for the 5 and 100-year events, respectively. This difference is due to the area adjustment of **Basin F** from the planned CMU1 MDDP to this site's drainage report. Though there is an increase in proposed runoff from **DP12**, the amount of runoff that reaches the planned FSD from adjacent lots and the proposed site is 0.3 cfs greater and 7.3 cfs less than the planned flows at this location from the CMU1 MDDP for the 5 and 100-year events, respectively. Thus, the runoff from the proposed site does not affect the size of the planned FSD. Proposed post construction runoff will be discharged from the pond at rates that are 2.0 cfs greater in the 100-year event than existing discharge rates, but are equal to the planned discharge rates for the 5 and 100 year design events from the CMU1 MDDP. Thus, the development of the proposed site will not further impact the flows that are planned to be released from the planned FSD in the CMU1 MDDP (see appendix).

The construction of Crossroads Mixed Use Filing No. 2 shall not adversely affect adjacent or downstream property. Subsequent drainage reports will be required when the site is developed further than the uses defined within this report.

References

- 1.) "El Paso County and City of Colorado Springs Drainage Criteria Manual".
- 2.) "Urban Storm Drainage Criteria Manual"
- 3.) SCS Soils Map for El Paso County.
- 4.) Flood Insurance Rate Map (FIRM), Federal Emergency Management Agency, Revised date December 7th, 2018.
- 5.) "Final Drainage Report for Claremont Business Park Filing No. 2", dated November 2006, by Matrix Design Group, Inc.
- 6.) "Preliminary and Final Drainage Report Meadowbrook Crossing Filing 1 and Filing 2", dated July 25, 2017, by Kiowa Engineering Corporation.
- 7.) "Final Drainage Report Lot 1 24/94 Business Park Filing No. 1 on Platte Avenue and Meadowbrook Parkway", dated April 28, 2016 and revised July 14, 2016, by Core Engineering Group, LLC.
- 8.) "Final Drainage Report for Meadowbrook Dirt Borrow Site", dated November 2018, by M&S Civil Consultants, Inc.
- 9.) "Sand Creek Drainage Basin Planning Study", revised March 1996, by Kiowa Engineering Corporation.
- 10.) "Final Drainage Report for Aura at Crossroads", dated April 4th, 2022, by Harris Kocher Smith.
- 11.) "Final Drainage Report for Crossroads Mixed Use Filing No.1", dated February 2022, by M&S Civil Consultants, Inc.



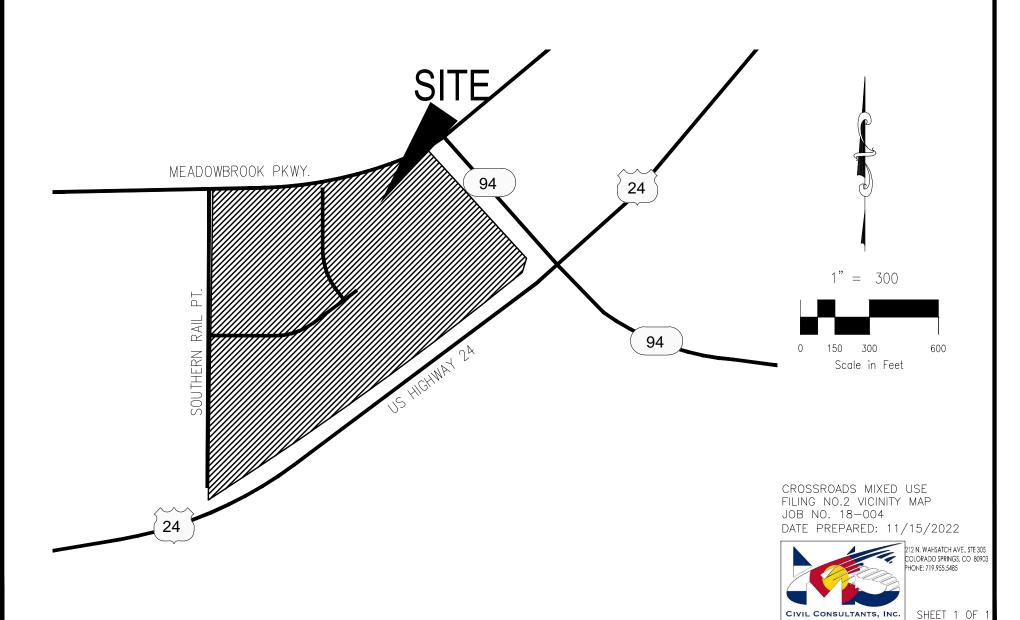
This reference was added to the report.

APPENDIX

VICINITY MAP

VICINITY MAP

CROSSROADS MIXED USE FILING NO.2



SOILS MAP

Totals for Area of Interest

SOILS MAP

385.6

100.0%

1" = 300

Scale in Feet

212 N. WAHSATCH AVE., STE 305 COLORADO SPRINGS, CO 80903 PHONE: 719.955.5485

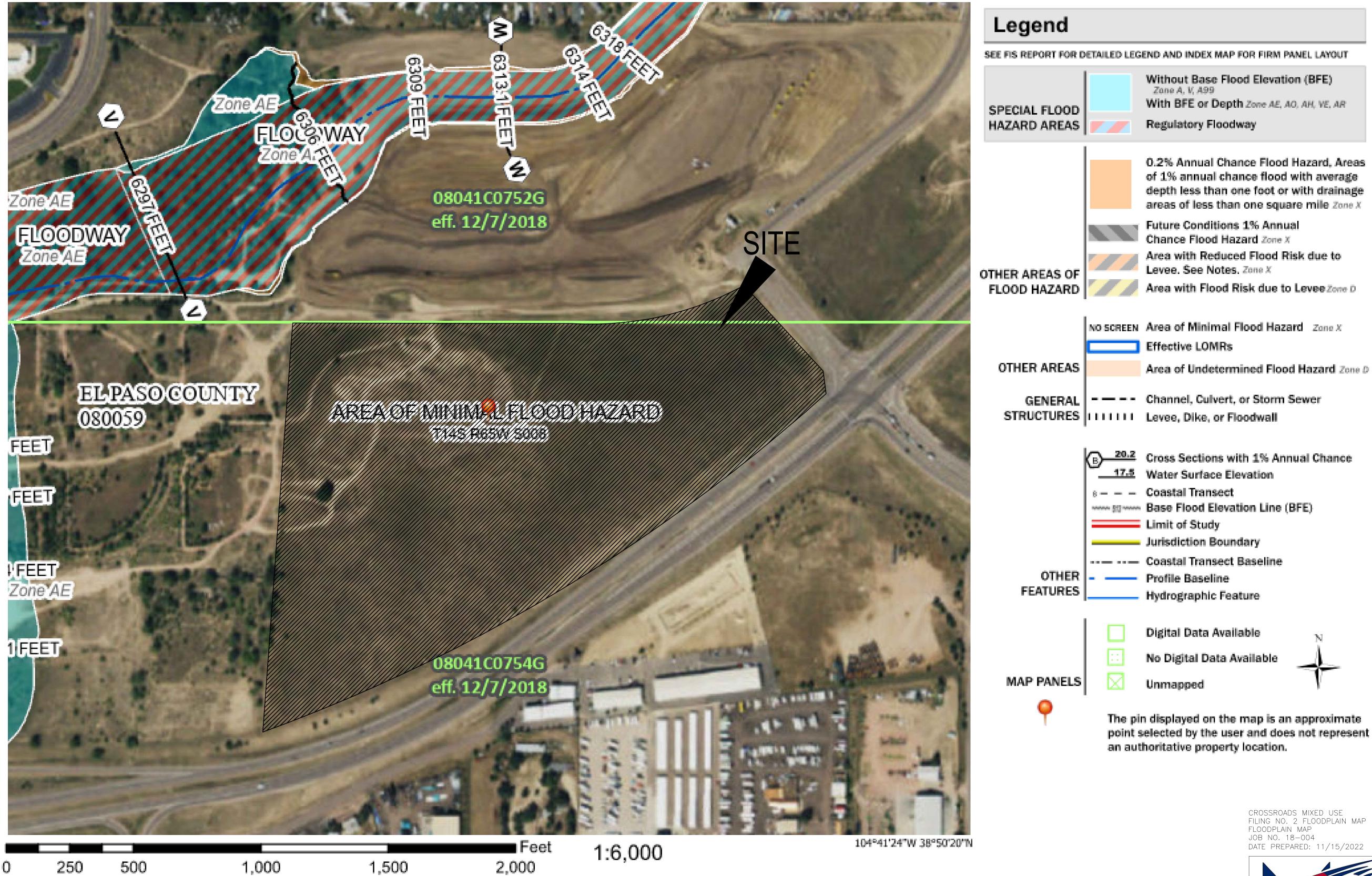
SHEET 1 OF 1

CIVIL CONSULTANTS, INC.

FIRM PANELS

FLOODPLAIN MAP

CROSSROADS MIXED USE FILING NO. 2



Basemap: USGS National Map: Ortholmagery: Data refreshed October, 2020

CROSSROADS MIXED USE FILING NO. 2 FLOODPLAIN MAP FLOODPLAIN MAP JOB NO. 18-004 DATE PREPARED: 11/15/2022



HYDROLOGIC CALCULATIONS

Crossroads Mixed Use Filing No. 2 FINAL DRAINAGE REPORT (Existing Area Runoff Coefficient Summary)

			STREE	TS / DEVE	ELOPED	OVERI	LAND / DEVI	ELOPED	WEIG	HTED
BASIN	TOTAL AREA (SF)	TOTAL AREA (Acres)	AREA (Acres)	C ₅	C ₁₀₀	AREA (Acres)	C ₅	C_{100}	C ₅	C ₁₀₀
C	173960	3.99	0.00	0.90	0.96	5.89	0.08	0.35	0.08	0.35
A	480166.8	11.02	0.00	0.90	0.96	11.02	0.08	0.35	0.08	0.35
В	754121.6	17.31	0.00	0.90	0.96	17.31	0.08	0.35	0.08	0.35
OS-1	55560.16	1.28	1.28	0.90	0.96	0.00	0.08	0.35	0.90	0.96
OS-2	216993.7	4.98	2.49	0.90	0.96	2.49	0.08	0.35	0.49	0.66
EX-A2***		0.59	0.59	0.90	0.96	0.00	0.08	0.35	0.90	0.96
OS-A**		1.29	1.29	0.62	0.72	0.00	0.08	0.35	0.62	0.72
E2*		3.86	3.86	0.80	0.90	0.00	0.08	0.35	0.80	0.90

^{*}FROM FDR FOR CLAREMONT BUSINESS PARK FILING NO. 2

^{**}FROM TO FDR MEADOWBROOK CROSSING FILING 1 AND FILING 2

^{***}FROM FDR LOT 1 24/94 BUSINESS PARK FILING NO. 1 ON PLATTE AVENUE AND MEADOWBROOK PARKWAY

Crossroads Mixed Use Filing No. 2 FINAL DRAINAGE REPORT

(Existing Area Drainage Summary)

Fron	n Area Runoff Co	efficient Summar	у		OVERLA.	1ND		ST	REET / CH	ANNEL FLO	OW .	Time of Trave	$l(T_t)$	INTEN	SITY ^	TOTAL	FLOWS
BASIN	AREA TOTAL	C ₅	C ₁₀₀	C ₅	Length	Height	T_{C}	Length	Slope	Velocity	T _t	TOTAL	CHECK	I ₅	I ₁₀₀	Q ₅	Q ₁₀₀
	(Acres)	From DCI	A Table 5-1		(ft)	(ft)	(min)	(ft)	(%)	(fps)	(min)	(min)	(min)	(in/hr)	(in/hr)	(c.f.s.)	(c.f.s.)
C	3.99	0.08	0.35	0.08	120	2.8	15.3	555	1.5%	0.9	10.6	25.9	13.8	2.7	4.5	0.9	6.3
A	11.02	0.08	0.35	0.08	165	8	13.8	1730	1.3%	0.8	36.3	50.1	20.5	1.7	2.9	1.5	11.1
В	17.31	0.08	0.35	0.08	300	3	30.9	1390	1.2%	0.8	29.7	60.6	19.4	1.4	2.4	2.0	14.5
OS-1	1.28	0.90	0.96	0.90	100	3	2.5	490	2.2%	3.0	2.8	5.3	13.3	5.1	8.5	5.8	10.5
OS-2	4.98	0.49	0.66	0.49	85	8	4.8	1165	1.8%	2.0	9.6	14.5	16.9	3.6	6.0	8.7	19.6
EX-A2***	0.59	0.90	0.96	0.90	10	0.2	0.9	916	1.9%	2.7	5.6	6.5	15.1	4.8	8.0	2.5	4.5
OS-A**	1.29	0.62	0.72	0.62	40	0.8	4.4	1310	1.9%	2.8	7.9	12.3	17.5	3.8	6.4	3.1	6.0
E2*	3.86	0.80	0.90	0.80	50	1	3.0	400	1.3%	2.3	2.9	6.0	12.5	4.9	8.2	15.1	28.6

[^] Intensity equations assume a minimum travel time of 5 minutes.

Calculated by: CVW

Date: 1/31/2022

^{*}VALUES DERIVED USING DATA FROM FDR FOR CLAREMONT BUSINESS PARK FILING NO. 2

^{**}VALUES DERIVED USING DATA FROM FDR FOR MEADOWBROOK CROSSING FILING 1 AND FILING 2 PAGE 31

^{***}VALUES DERIVED USING DATA FROM FDR FOR LOT 1 24/94 BUSINESS PARK FILING NO. 1 ON PLATTE AVENUE AND MEADOWBROOK PARKWAY

Crossroads Mixed Use Filing No. 2 FINAL DRAINAGE REPORT (Existing Basin Routing Summary)

	From Area Runoff Coefficient Summar	v			OVI	ERLAND		PIPE	/ CHA	NNEL FLO)W	Time of Travel (T _t)	INTEN	VSITY *	TOTAL I	FLOWS	
DESIGN POINT	CONTRIBUTING BASINS	CA ₅	CA ₁₀₀	C ₅	Length	Height	T _C	Length	Slope	Velocity	T _t	TOTAL	I ₅	I ₁₀₀	Q ₅	Q ₁₀₀	COMMENTS
			•		(ft)	(ft)	(min)	(ft)	(%)	(fps)	(min)	(min)	(in/hr)	(in/hr)	(c.f.s.)	(c.f.s.)	
1	E2	3.09	3.47				6.0	916	1.9%	2.7	5.6	11.6	3.9	6.6	14.2	26.5	
	EX-A2	0.53	0.57									1					
																	EXISTING 10' CDOT TYPE R AT
		3.62	4.04		Te fe	or E2 Used											GRADE INLET
2	OS-A	0.80	0.93									12.3	3.8	6.4	3.1	6.0	
																	EXISTING 10' CDOT TYPE R AT
				Se	e Area Drai	nage Sheet t	for Input										GRADE INLET
3	OS-1	1.15	1.22				11.6	150	1.0%	2.0	1.3	12.8	3.8	6.3	9.8	22.5	
	FB-DP1	1.47	2.35														
		2.62	3.57		Tc fo	r DP1 Used											END OF PAVEMENT
4	A	0.88	3.86				12.8	1470	1.6%	0.9	28.0	40.8	2.0	3.4	7.1	25.5	
	FB-DP2	0.00	0.10														
	DP3	2.62	3.57														
		3.50	7.54		Tc fo	r DP3 Used											ADJACENT PARCEL (LOT 1)
5	В	1.38	6.06									60.6	1.4	2.4	2.0	14.5	
				Se	e Area Drai	nage Sheet i	or Input										ADJACENT PARCEL (LOT 2)
6	C	0.32	1.40									25.9	2.7	4.5	0.9	6.3	
				Se	e Area Drai	nage Sheet 1	or Input										DISCHARGE TO CDOT ROW
7	OS2	2.44	3.26									14.5	3.6	6.0	9.9	28.0	
	DP6	0.32	1.40														BARROW DITCH
		2.76	4.66		Tc fo	r OS2 Used											SW CORNER OF SITE/CDOT ROW

Calculated by: CVW

Date: 1/31/2022

CROSSROADS MIXED USE FILING NO. 2 FINAL DRAINAGE CALCULATIONS

(Proposed Area Runoff Coefficient Summary)

			STREE	TS / COM	MERC.	MULTI-FA	AMILY/PA	RKLAND	OVERLAN.	D / UNDE	/ELOPED	WEIG	HTED
BASIN	TOTAL AREA (Sq Ft)	TOTAL AREA (Acres)	AREA (Acres)	C ₅	C ₁₀₀	AREA (Acres)	C ₅	C ₁₀₀	AREA (Acres)	C ₅	C ₁₀₀	C ₅	C ₁₀₀
					PROPOS	ED BASINS							
OS-A**		1.29	1.29	0.62	0.72	0.00	0.49	0.62	0.00	0.08	0.35	0.62	0.72
E2*		3.86	3.86	0.80	0.90	0.00	0.49	0.62	0.00	0.08	0.35	0.80	0.90
EX-A2***		0.59	0.59	0.90	0.96	0.00	0.49	0.62	0.00	0.08	0.35	0.90	0.96
OS-1	60793.3017	1.40	1.40	0.90	0.96	0.00	0.49	0.62	0.00	0.08	0.35	0.90	0.96
OS-2	217071.1816	4.98	2.49	0.90	0.96	0.00	0.49	0.62	2.49	0.08	0.35	0.49	0.66
A	72787.0873	1.67	1.67	0.90	0.96	0.00	0.49	0.62	0.00	0.08	0.35	0.90	0.96
В	64538.8381	1.48	1.48	0.90	0.96	0.00	0.49	0.62	0.00	0.08	0.35	0.90	0.96
C	102868.78	2.36	2.22	0.81	0.88	0.00	0.49	0.62	0.15	0.08	0.35	0.76	0.85
D	96317.6781	2.21	2.21	0.81	0.88	0.00	0.49	0.62	0.00	0.08	0.35	0.81	0.88
E	36526.0967	0.84	0.24	0.90	0.96	0.60	0.81	0.88	0.00	0.08	0.35	0.84	0.90
E1	70476.5132	1.62	0.24	0.90	0.96	1.38	0.81	0.88	0.00	0.08	0.35	0.82	0.89
F	118628.9595	2.72	2.72	0.81	0.88	0.00	0.49	0.62	0.00	0.08	0.35	0.81	0.88
G	20057.4496	0.46	0.46	0.90	0.96	0.00	0.49	0.62	0.00	0.08	0.35	0.90	0.96
J	139924.2472	3.21	0.00	0.90	0.96	3.21	0.16	0.41	0.00	0.08	0.35	0.16	0.41
A-5***	159865.2	3.67	0.00	0.90	0.96	3.67	0.68	0.79	0.00	0.08	0.35	0.68	0.79
Z-1***	16117.2	0.37	0.00	0.90	0.96	0.37	0.33	0.52	0.00	0.08	0.35	0.33	0.52
D-1****	33976.8	0.78	0.00	0.90	0.96	0.78	0.62	0.75	0.00	0.08	0.35	0.62	0.75
Z-2***	16552.8	0.38	0.00	0.90	0.96	0.38	0.38	0.56	0.00	0.08	0.35	0.38	0.56
G1	25617.769	0.59	0.59	0.90	0.96	0.00	0.16	0.41	0.00	0.08	0.35	0.90	0.96
CI	95425.7528	2.19	2.04	0.81	0.88	0.00	0.49	0.62	0.15	0.08	0.35	0.76	0.84

^{*}FROM FDR FOR CLAREMONT BUSINESS PARK FILING NO. 2

Calculated by: TAU

Date: 11/22/2022

^{**}FROM FDR FOR MEADOWBROOK CROSSING FILING 1 AND FILING 2

^{***}FROM FDR FOR LOT 1 24/94 BUSINESS PARK FILING NO. 1 ON PLATTE AVENUE AND MEADOWBROOK PARKWAY

^{****}FROM FDR FOR AURA AT CROSSROADS, DATED OCTOBER 29TH, 2021

CROSSROADS MIXED USE FILING NO. 2 FINAL DRAINAGE REPORT

(Proposed Drainage Summary)

From Area Rui	noff Coefficient S	Summary			OVER	LAND		STRE	ET / CH	ANNEL F	FLOW	Time of T	Fravel (T_t)	INTEN	SITY#	TOTAL	FLOWS
BASIN	AREA TOTAL	C ₅	C ₁₀₀	C ₅	Length	Height	T_{C}	Length	Slope	Velocity	T _t	TOTAL	CHECK	I_5	I ₁₀₀	Q_5	Q ₁₀₀
	(Acres)	From DCM	1 Table 5-1		(ft)	(ft)	(min)	(ft)	(%)	(fps)	(min)	(min)	(min)	(in/hr)	(in/hr)	(c.f.s.)	(c.f.s.)
					I	Proposed	d Area I	Drainag	e Sumi	nary							
OS-A**	1.29	0.62	0.72	0.62	40	0.8	4.4	1310	1.9%	2.8	7.9	12.3	17.5	3.8	6.4	3.1	6.0
E2*	3.86	0.80	0.90	0.80	50	1	3.0	400	1.3%	2.3	2.9	6.0	12.5	4.9	8.2	15.1	28.6
EX-A2***	0.59	0.90	0.96	0.90	10	0.2	0.9	916	1.9%	2.7	5.6	6.5	15.1	4.8	8.0	2.5	4.5
OS-1	1.40	0.90	0.96	0.90	100	3	2.5	490	2.2%	3.0	2.7	5.2	13.3	5.1	8.6	6.4	11.5
OS-2	4.98	0.49	0.66	0.49	85	8	4.8	1165	1.8%	2.0	9.6	14.5	16.9	3.6	6.0	8.7	19.6
A	1.67	0.90	0.96	0.90	30	0.6	1.6	1325	0.7%	1.7	7.3	8.9	17.5	4.3	7.2	6.5	11.6
В	1.48	0.90	0.96	0.90	25	0.5	1.4	1335	0.7%	1.7	7.3	8.8	17.6	4.3	7.3	5.8	10.3
C	2.36	0.76	0.85	0.76	50	1	3.4	260	1.5%	2.4	1.4	5.0	11.7	5.2	8.7	9.3	17.4
D	2.21	0.81	0.88	0.81	50	1	2.9	200	1.5%	2.4	1.1	5.0	11.4	5.2	8.7	9.3	16.9
E	0.84	0.84	0.90	0.84	60	1.2	2.9	700	1.0%	2.0	3.8	6.8	14.2	4.7	7.9	3.3	6.0
E1	1.62	0.82	0.89	0.82	60	1.2	2.9	700	1.0%	2.0	3.8	6.8	14.2	4.7	7.9	6.3	11.4
F	2.72	0.81	0.88	0.81	50	0.8	3.2	300	1.3%	2.3	1.6	5.0	11.9	5.2	8.7	11.4	20.8
G	0.46	0.90	0.96	0.90	50	1	2.0	466	1.1%	2.1	2.6	5.0	12.9	5.2	8.7	2.1	3.8
J	3.21	0.16	0.41	0.16	50	2	7.6	0	0.0%	0.0	0.0	7.6	10.3	4.5	7.6	2.3	10.0
A-5****	3.67	0.68	0.79	0.68			REF	ER TO "FD	R FOR AU	JRA AT CR	.OSSROAI	OS" FOR DE	ETAILS			8.72	17.06
Z-1****	0.37	0.33	0.52	0.33			REF	ER TO "FD	R FOR AL	JRA AT CR	OSSROAI	OS" FOR DE	ETAILS			0.47	1.27
D-1****	0.78	0.62	0.75	0.62			REF	ER TO "FD	R FOR AL	JRA AT CR	OSSROAI	OS" FOR DE	ETAILS			2.08	4.20
Z-2****	0.38	0.38	0.56	0.38			REF	ER TO "FD	R FOR AL	JRA AT CR	OSSROAI	OS" FOR DE	ETAILS			0.57	1.43
G1	0.59	0.90	0.96	0.90	50	1	2.0	466	1.1%	2.1	2.6	5.0	12.9	5.2	8.7	2.7	4.9
C1	2.19	0.76	0.84	0.76	50	1	3.4	260	1.5%	2.4	1.4	5.0	11.7	5.2	8.7	9.3	17.4

[#] Intensity equations assume a minimum travel time of 5 minutes.

Calculated by: TAU

Date: 11/22/2022

^{*}VALUES DERIVED USING DATA FROM FDR FOR CLAREMONT BUSINESS PARK FILING NO. 2

^{**}VALUES DERIVED USING DATA FROM FDR MEADOWBROOK CROSSING FILING 1 AND FILING 2 PAGE 31

^{***}VALUES DERIVED USING DATA FROM FDR LOT 1 24/94 BUSINESS PARK FILING NO. 1 ON PLATTE AVENUE AND MEADOWBROOK PARKWAY

^{****}FROM FDR FOR AURA AT CROSSROADS, DATED OCTOBER 29th, 2021

CROSSROADS MIXED USE FILING NO. 2 FINAL DRAINAGE REPORT (Proposed Basin Routing Summary)

							(Pro	opose	ed Be	isin I	Rout	ing Summ	ary)				
	From Area Runoff Coefficient Summary				O1	ERLAND				NNEL FLO		Time of Travel (T1)		VSITY *	TOTAL	FLOWS	
DESIGN POINT	CONTRIBUTING BASINS	CA ₅	CA ₁₀₀	C ₅	Lengt	h Height	T _C	Length (ft)	Slope (%)	Velocity (fps)	T _t	TOTAL (min)	I ₅ (in/hr)	I ₁₀₀ (in/hr)	Q ₅ (c.f.s.)	Q ₁₀₀ (c.f.s.)	COMMENTS
		•	I	ROP	OSED	DRAIN	AGE BA	ASIN RO			IARY	•	•				
1	E2, EX-A2	3.62	4.04				6.0	916	1.9%	2.7	5.6	11.6	3.9	6.6	14.2	26.5	Existing 10' CDOT Type R At-Grade Inlet
								_									(Public)
	00.4	0.00		-	Tc	for E2 Used						40.0			2.1		
2	OS-A	0.80	0.93	l								12.3	3.8	6.4	3.1	6.0	Existing 10' CDOT Type R At-Grade Inlet (Public)
					Tc fo	or OS-A Used	-	1									(i doic)
3	OS-1, FB-DP1	2.73	3.69				11.6	150	1.0%	2.0	1.3	12.8	3.8	6.3	10.2	23.3	Proposed 10' CDOT Type R At-Grade Inlet
				<u> </u>	Т- 6	or DP1 Used		4									(Public)
4	A, FB-DP2	1.50	1.71	 	101	or Dr r oscu	Т					8.9	4.3	7.2	6.5	12.4	Proposed 15' CDOT Type R At-Grade Inlet
,	,			l										,	0.5	12	(Public)
					Tc fo	Basin A use	d										
4.5	FB-DP4	0.00	0.24	l								8.9	4.3	7.2	0.0	1.8	Proposed NEENAH R-2501 MH Lid and Frame
				<u> </u>	Tet	for DP4 used		1									(Public)
5	B, FB-DP3	2.28	3.56									8.8	4.3	7.3	9.9	25.8	Proposed 15' CDOT Type R Sump Inlet
																	(Public)
	~	1.81		<u> </u>	Te for	Basin B Use	d						5.2	0.0			
6	C	1.81	2.00	l								5.0	5.2	8.7	9.3	17.4	Future 30" RCP or PP Storm Sewer, Rip Rap Pad (Private)
					Tc for	Basin C Use	d	1									(Pilvale)
6.5	C1	1.81	2.00									5.0	5.2	8.7	9.3	17.4	Future 30" RCP or PP Storm Sewer, Rip Rap Pad
				<u> </u>	T. C	Basin C1 Uso	<u> </u>	4									(Private)
7	D	1.79	1.95	\vdash	1 c for	Basin CT Use	ea I					5.0	5.2	8.7	9.3	16.9	Future 24" RCP or PP Storm Sewer, Rip Rap Pad
′	D	1,	1.75									3.0	5.2	0.7	7.3	10.7	(Private)
					Tc for	Basin D Use	d										ì
8	E	0.70	0.76									6.8	4.7	7.9	3.3	6.0	Future 10' CDOT Type R At-Grate Inlet
				├	Tc for	Basin E Use	d	1									(Private)
9	E1	1.33	1.44									6.8	4.7	7.9	6.3	11.4	Future 10' CDOT Type R At-Grade Inlet
																	(Private)
10	G	0.41	0.44	-	Tc for	Basin E1 Uso	ed T					5.0	5.2	8.7	2.1	3.8	h Haranama Na VI
10	G	0.41	0.44	l								5.0	5.2	8.7	2.1	3.8	Proposed 10' CDOT Type R Sump Inlet (Private)
					Te for	Basin G Use	d	1									(Titule)
11	G1	0.53	0.56									5.6	5.0	8.4	3.5	8.7	Proposed 15' CDOT Type R Sump Inlet
	FB-DP8 FB-DP9	-0.15 0.16	0.00														(Private)
	rb-Dry	0.10	1.03	 	Weis	ghted Tc Used		1									
12	F	2.21	2.40		$\overline{}$	1	T					5.0	5.2	8.7	11.4	20.8	Proposed 24" RCP or PP Storm Sewer
					L_												(Private)
13	Basin A-5 (Overflow)	0.23	1.32	-	Tc for	Basin F Use	d					12.8	3.8	6.3	1.3	10.9	n lan a Fid C I n' n n
13	Basin A-5 (Overflow) Basin Z-1	0.23	0.20									12.0	3.0	0.3	1.3	10.9	Proposed 2' Bottom Earthen Swale, Rip Rap Rundown
	Basin D-1 (Overflow)	0.00	0.21														
		0.36	1.72		Weiş	thted Tc Used											
14	Basin Z-2 DP 13	0.14 0.36	0.03 1.43	I				1				11.1	4.0	6.7	2.0	9.7	Proposed Triangular Earthen Swale
	Dr 15	0.50	1.45	\vdash	Tc for	Basin Z-2 Us	ed	1									(Private)
15	J, DP14, PR19,	24.21	28.30									6.3	4.8	8.1	117.0	229.7	Full Spectrum Extended Detention Basin
	PR18							1									(Private)
16	DOND OUTFALL	2.77	5.16	-	Weiş	ghted Tc Used						14.5	3.6	6.0	0.0	21.0	HISTORIC PLOW BUSDOT DARROW DITCH
16	POND OUTFALL OS-2	2.11	5.16	1								14.5	3.0	6.0	9.9	31.0	HISTORIC FLOW IN CDOT BARROW DITCH Q5= 10.4 CFS, Q100 = 31.9 CFS
	~~ -	1			Tc for l	Basin OS-2 U	sed	1	l		1	1	I			1	PER HISTORIC DRAINAGE ANALYSIS

Intensity equations assume a minimum travel time of 5 minutes.

Overflow- obtain flows from inlet sheets provided in Background Information Section of Appendix

Date: TAU 11/22/2022
Checked by: DLM

CROSSROADS MIXED USE FILING NO. 2 FINAL DRAINAGE CALCULATIONS

(Proposed Storm Sewer Routing Summary)

		1	I		т.	•, 4	r.]
					Inter	isity*	FI	ow	PIPE SIZE
PIPE RUN	Contributing Pipes/Design Points	Equivalent CA 5	Equivalent CA ₁₀₀	Maximum T _C	I_5	I 100	Q 5	Q 100	
1	DP3 (INLET 3)	1.78	1.55	12.8	3.8	6.3	6.7	9.8	24" SD
1.5	DP4 (INLET 4)	1.50	1.46	8.9	4.3	7.2	6.5	10.6	24" SD
2	PR1.5, DP4.5 (INLET 4.5)	1.50	1.71	9.0	4.3	7.2	6.4	12.3	24" SD
3	PR2, DP5 (INLET 5)	3.78	5.27	9.0	4.3	7.2	16.2	37.9	36" SD
4	DP6	1.81	2.00	5.0	5.2	8.7	9.3	17.4	30" SD
4.5	DP6.5	1.81	2.00	5.0	5.2	8.7	9.3	17.4	30" SD
5	PR4, PR4.5	3.61	4.00	5.0	5.2	8.7	18.7	34.7	30" SD
6	PR5	3.61	4.00	5.0	5.2	8.7	18.7	34.7	30" SD
7	PR6	3.61	4.00	5.0	5.2	8.7	18.7	34.7	30" SD
8	DP7	1.79	1.95	5.0	5.2	8.7	9.3	16.9	24" SD
9	PR8, DP8 (Inlet 6)	2.64	2.70	6.8	4.7	7.9	12.4	21.4	30" SD
10	PR7, PR9	6.25	6.71	6.8	4.7	7.9	29.5	53.0	36" SD
11	PR10, DP9 (Inlet 7)	7.42	7.68	6.8	4.7	7.9	35.0	60.7	36" SD
11.5*	SEE FDR FOR AURA AT CROSSROADS	1.93	2.30	14.6	3.6	6.0	6.9	13.8	30" SD
12	PR11	7.42	7.68	7.0	4.7	7.8	34.6	60.1	42" SD
12.5	PR12, PR11.5	9.35	9.98	7.2	4.6	7.8	43.2	77.4	48" SD
13	DP10 (Inlet 8)	0.41	0.44	5.0	5.2	8.7	2.1	3.8	18" SD
14	DP11 (Inlet 9)	0.69	1.03	5.6	5.0	8.4	3.5	8. 7	30" SD
15	PR12.5, PR13, PR14	10.46	11.45	7.5	4.6	7.7	47.7	87.7	48" SD
16	DP12	2.21	2.40	5.0	5.2	8.7	11.4	20.8	24" SD
17	PR15, PR16	12.66	13.85	7.7	4.5	7.6	57.3	105.1	48" SD
18	PR17, PR21	13.14	14.43	8.2	4.4	7.4	58.2	107.3	48" SD
19*	SEE FDR FOR AURA AT CROSSROADS	10.05	11.09	15.0	3.5	5.9	35.4	65.5	48" SD
20	POND OUTFALL	PER	MHFD	WKSHT			1.2	11.4	18" SD
21*	SEE FDR FOR AURA AT CROSSROADS O FDR FOR AURA AT CROSSROADS FOR	0.48	0.58	8.8	4.3	7.3	2.1	4.2	30" SD

*REFER TO FOR FOR AURA AT CROSSROADS FOR CONTRIBUTING PIPE FLOW DETAILS

DP - Design Point

EX - Existing Design Point

FB- Flow By from Design Point INT- Intercepted Flow from Design Point
 Calculated by:
 TAU

 Date:
 11/22/2022

 Checked by:
 DLM

Page 1

Version 4.06 Released August 2018

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Crossroads Mixed Use
Inlet 6 Project: Inlet ID: STREET

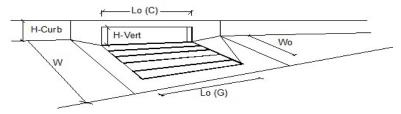
T _{BACK} =	7.5	ft	
S _{BACK} =	0.020	ft/ft	
n _{BACK} =	0.020]	
House =	6.00	linghag	
_		-1	
_		- 111	
		-1	
_	0.020	ft/ft	
S _W =	0.083	ft/ft	
S _o =	0.020	ft/ft	
n _{STREET} =	0.016		
	Minor Storm	Major Storm	
T _{MAX} =	14.0	14.0	ft
d _{MAX} =	4.4	8.8	inches
_		✓	check = yes
_	Minor Storm	Major Storm	
y =	3.36	3.36	inches
d _C =	2.0	2.0	inches
	SBACK = nBACK = HCURB = TCROWN = SX = SW = SO = NSTREET = TMAX = dMAX =	$\begin{array}{c} S_{BACK} = \\ n_{BACK} = \\ \end{array} \begin{array}{c} 0.020 \\ 0.020 \\ \end{array}$ $\begin{array}{c} H_{CURB} = \\ T_{CROWN} = \\ \end{array} \begin{array}{c} 0.00 \\ 14.0 \\ W = \\ 0.020 \\ S_X = \\ 0.020 \\ S_W = \\ 0.083 \\ S_O = \\ 0.020 \\ n_{STREET} = \\ \end{array} \begin{array}{c} 0.020 \\ 0.016 \\ \end{array}$ $\begin{array}{c} M_{INOT} Storm \\ T_{MAX} = \\ d_{MAX} = \\ \end{array} \begin{array}{c} 4.4 \\ 0.00 \\ 0.00 \\ \end{array}$	S _{BACK} = 0.020 ft/ft n _{BACK} = 0.020 ft/ft H _{CURB} = 6.00 inches T _{CROWN} = 14.0 ft W = 2.00 ft S _X = 0.020 ft/ft S _W = 0.083 ft/ft S _O = 0.020 ft/ft Minor Storm Major Storm T _{MAX} = 14.0 14.0 d _{MAX} = 4.4 8.8

Maximum Capacity for 1/2 Street based on Allowable Spread	_	WIII OF STOTT	Major Otorni	_
Water Depth without Gutter Depression (Eq. ST-2)	y =	3.36	3.36	inches
Vertical Depth between Gutter Lip and Gutter Flowline (usually 2")	d _C =	2.0	2.0	inches
Gutter Depression (d _C - (W * S _x * 12))	a =	1.51	1.51	inches
Water Depth at Gutter Flowline	d =	4.87	4.87	inches
Allowable Spread for Discharge outside the Gutter Section W (T - W)	T _X =	12.0	12.0	ft
Gutter Flow to Design Flow Ratio by FHWA HEC-22 method (Eq. ST-7)	Eo =	0.425	0.425	1
Discharge outside the Gutter Section W, carried in Section T _X	Q _X =	5.5	5.5	cfs
Discharge within the Gutter Section W (Q _T - Q _X)	Q _W =	4.1	4.1	cfs
Discharge Behind the Curb (e.g., sidewalk, driveways, & lawns)	Q _{BACK} =	0.0	0.0	cfs
Maximum Flow Based On Allowable Spread	$Q_T =$	9.6	9.6	cfs
Flow Velocity within the Gutter Section	V =	6.3	6.3	fps
V*d Product: Flow Velocity times Gutter Flowline Depth	V*d =	2.6	2.6	
ll				_

various control valous, amos cultar riomino Dopar		2.0	2.0
	_		
Maximum Capacity for 1/2 Street based on Allowable Depth		Minor Storm	Major Storm
Theoretical Water Spread	T _{TH} =	11.8	30.4
Theoretical Spread for Discharge outside the Gutter Section W (T - W)	T _{X TH} =	9.8	28.4
Gutter Flow to Design Flow Ratio by FHWA HEC-22 method (Eq. ST-7)	E _o =	0.498	0.191
Theoretical Discharge outside the Gutter Section W, carried in Section TXTH	$Q_{XTH} =$	3.2	54.6
Actual Discharge outside the Gutter Section W, (limited by distance T _{CROWN})	Q _X =	3.2	42.0
Discharge within the Gutter Section W (Q _d - Q _X)	Q _W =	3.2	12.9
Discharge Behind the Curb (e.g., sidewalk, driveways, & lawns)	Q _{BACK} =	0.0	3.8
Total Discharge for Major & Minor Storm (Pre-Safety Factor)	Q =	6.4	58.7
Average Flow Velocity Within the Gutter Section	V =	5.7	9.9
V*d Product: Flow Velocity Times Gutter Flowline Depth	V*d =	2.1	7.3
Slope-Based Depth Safety Reduction Factor for Major & Minor (d ≥ 6") Storm	R =	1.00	0.83
Max Flow Based on Allowable Depth (Safety Factor Applied)	$Q_d =$	6.4	49.0
Resultant Flow Depth at Gutter Flowline (Safety Factor Applied)	d =	4.35	8.26
Resultant Flow Depth at Street Crown (Safety Factor Applied)	d _{CROWN} =	0.00	3.39
MINOR STORM Allowable Capacity is based on Depth Criterion		Minor Storm	Major Storn
MAJOR STORM Allowable Capacity is based on Depth Criterion	Q _{allow} =	6.4	49.0
Minor storm max. allowable capacity GOOD - greater than the design flow given on	•		
Major storm max. allowable capacity GOOD - greater than the design flow given on s	sheet 'Inlet Managemen	<u>t'</u>	

INLET ON A CONTINUOUS GRADE

Version 4.06 Released August 2018



Design Information (Input) Type of Inlet CDOT Type R Curb Opening ▼	Type =	MINOR CDOT Type R	MAJOR Curb Opening	1
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	10.00	10.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	4.0	6.0	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.1	1.4	cfs
Capture Percentage = Q _a /Q _o =	C% =	98	81	%

18-004 Proposed Inlet Calcs.xlsm, Inlet 6

Version 4.06 Released August 2018

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Crossroads Mixed Use
Inlet 7 Project: Inlet ID: STREET

/				
Gutter Geometry (Enter data in the blue cells)	_		_	
Maximum Allowable Width for Spread Behind Curb	T _{BACK} =	7.5	ft	
Side Slope Behind Curb (leave blank for no conveyance credit behind curb)	S _{BACK} =	0.020	ft/ft	
Manning's Roughness Behind Curb (typically between 0.012 and 0.020)	n _{BACK} =	0.020]	
Height of Curb at Gutter Flow Line	H _{CURB} =	6.00	inches	
Distance from Curb Face to Street Crown	T _{CROWN} =	14.0	ft	
Gutter Width	W =	2.00	ft	
Street Transverse Slope	S _X =	0.020	ft/ft	
Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)	S _W =	0.083	ft/ft	
Street Longitudinal Slope - Enter 0 for sump condition	S _o =	0.020	ft/ft	
Manning's Roughness for Street Section (typically between 0.012 and 0.020)	n _{STREET} =	0.016]	
		Minor Storm	Major Storm	
Max. Allowable Spread for Minor & Major Storm	T _{MAX} =	14.0	14.0	ft
Max. Allowable Depth at Gutter Flowline for Minor & Major Storm	d _{MAX} =	4.4	8.8	inches
Allow Flow Depth at Street Crown (leave blank for no)	_		✓	check = yes
Maximum Capacity for 1/2 Street based On Allowable Spread		Minor Storm	Major Storm	_
Water Depth without Gutter Depression (Eq. ST-2)	y =	3.36	3.36	inches
Vertical Depth between Gutter Lip and Gutter Flowline (usually 2")	d _C =	2.0	2.0	inches

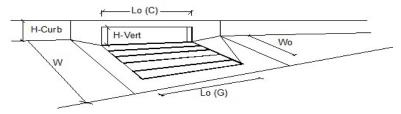
Maximum Capacity for 1/2 Street based On Allowable Spread		Minor Storm	iviajor Storm	
Water Depth without Gutter Depression (Eq. ST-2)	y =	3.36	3.36	inches
Vertical Depth between Gutter Lip and Gutter Flowline (usually 2")	d _C =	2.0	2.0	inches
Gutter Depression (d _C - (W * S _x * 12))	a =	1.51	1.51	inches
Water Depth at Gutter Flowline	d =	4.87	4.87	inches
Allowable Spread for Discharge outside the Gutter Section W (T - W)	T _X =	12.0	12.0	ft
Gutter Flow to Design Flow Ratio by FHWA HEC-22 method (Eq. ST-7)	Eo =	0.425	0.425	
Discharge outside the Gutter Section W, carried in Section T _x	Q _X =	5.5	5.5	cfs
Discharge within the Gutter Section W (Q _T - Q _X)	Q _W =	4.1	4.1	cfs
Discharge Behind the Curb (e.g., sidewalk, driveways, & lawns)	Q _{BACK} =	0.0	0.0	cfs
Maximum Flow Based On Allowable Spread	$Q_T =$	9.6	9.6	cfs
Flow Velocity within the Gutter Section	V =	6.3	6.3	fps
V*d Product: Flow Velocity times Gutter Flowline Depth	V*d =	2.6	2.6	
	_			

· · · · · · · · · · · · · · ·			
Marianum Canada, for 1/2 Street based on Alleunble Donth	_	Minor Ctorn	Major Ctorm
Maximum Capacity for 1/2 Street based on Allowable Depth	- r	Minor Storm	Major Storm
Theoretical Water Spread	T _{TH} =	12.0	30.4
Theoretical Spread for Discharge outside the Gutter Section W (T - W)	T _{X TH} =	10.0	28.4
Gutter Flow to Design Flow Ratio by FHWA HEC-22 method (Eq. ST-7)	E _o =	0.490	0.191
Theoretical Discharge outside the Gutter Section W, carried in Section T _{X TH}	Q _{X TH} =	3.4	54.6
Actual Discharge outside the Gutter Section W, (limited by distance T _{CROWN})	Q _X =	3.4	42.0
Discharge within the Gutter Section W (Q _d - Q _X)	Q _W =	3.3	12.9
Discharge Behind the Curb (e.g., sidewalk, driveways, & lawns)	Q _{BACK} =	0.0	3.8
Total Discharge for Major & Minor Storm (Pre-Safety Factor)	Q =	6.7	58.7
Average Flow Velocity Within the Gutter Section	V =	5.8	9.9
V*d Product: Flow Velocity Times Gutter Flowline Depth	V*d =	2.1	7.3
Slope-Based Depth Safety Reduction Factor for Major & Minor (d ≥ 6") Storm	R =	1.00	0.83
Max Flow Based on Allowable Depth (Safety Factor Applied)	$Q_d =$	6.7	49.0
Resultant Flow Depth at Gutter Flowline (Safety Factor Applied)	d =	4.40	8.26
Resultant Flow Depth at Street Crown (Safety Factor Applied)	d _{CROWN} =	0.00	3.39
MINOR STORM Allowable Capacity is based on Depth Criterion		Minor Storm	Major Storm
MAJOR STORM Allowable Capacity is based on Depth Criterion	Q _{allow} =	6.7	49.0
Minor storm max. allowable capacity GOOD - greater than the design flow given on s	•		
Major storm max. allowable capacity GOOD - greater than the design flow given on s	sheet 'Inlet Managemen	t'	

18-004 Proposed Inlet Calcs.xlsm, Inlet 7

INLET ON A CONTINUOUS GRADE

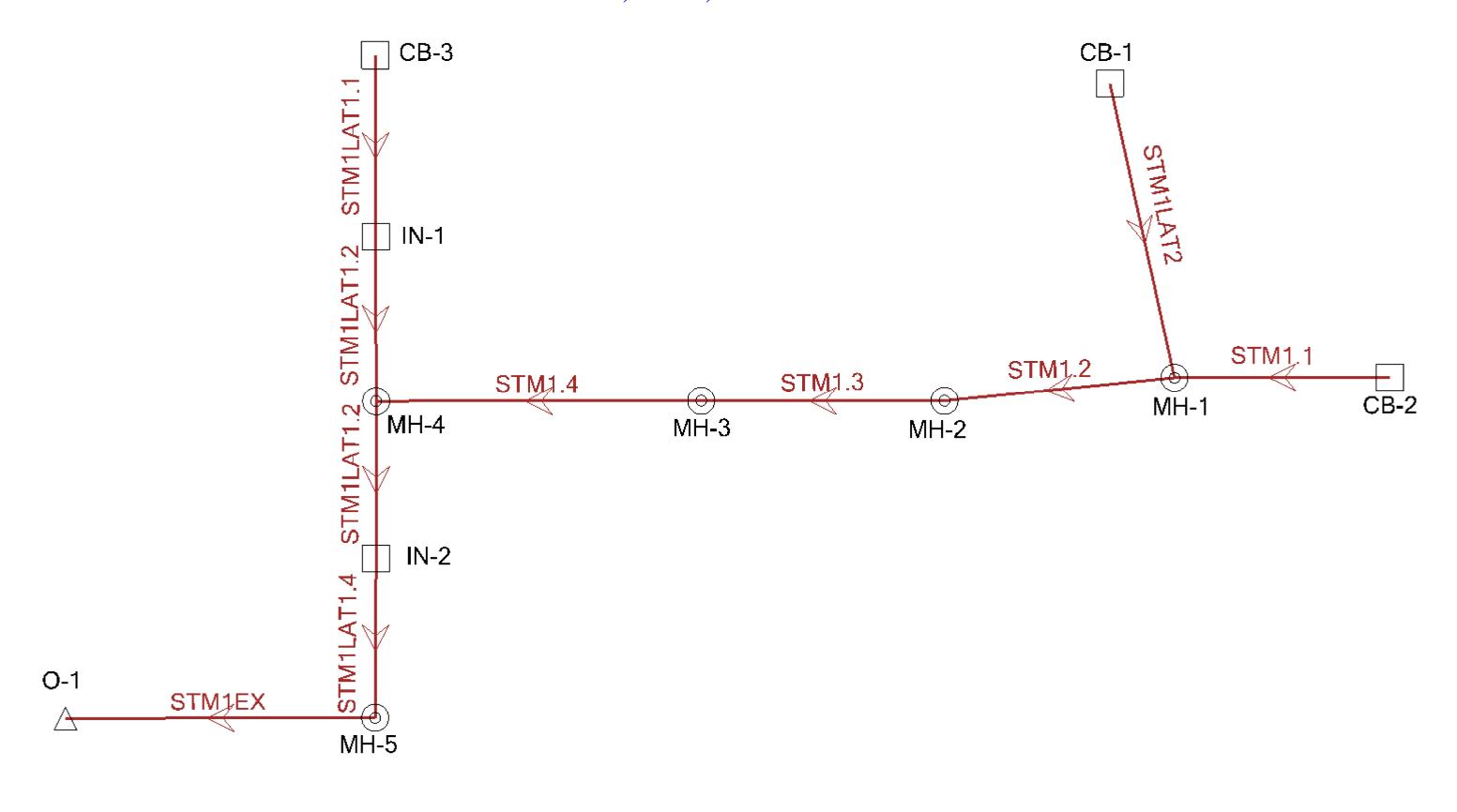
Version 4.06 Released August 2018



Design Information (Input)		MINOR	MAJOR	
Type of Inlet CDOT Type R Curb Opening	Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	10.00	10.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	5.5	7.7	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.9	4.0	cfs
Capture Percentage = Q _a /Q _o =	C% =	86	66	%

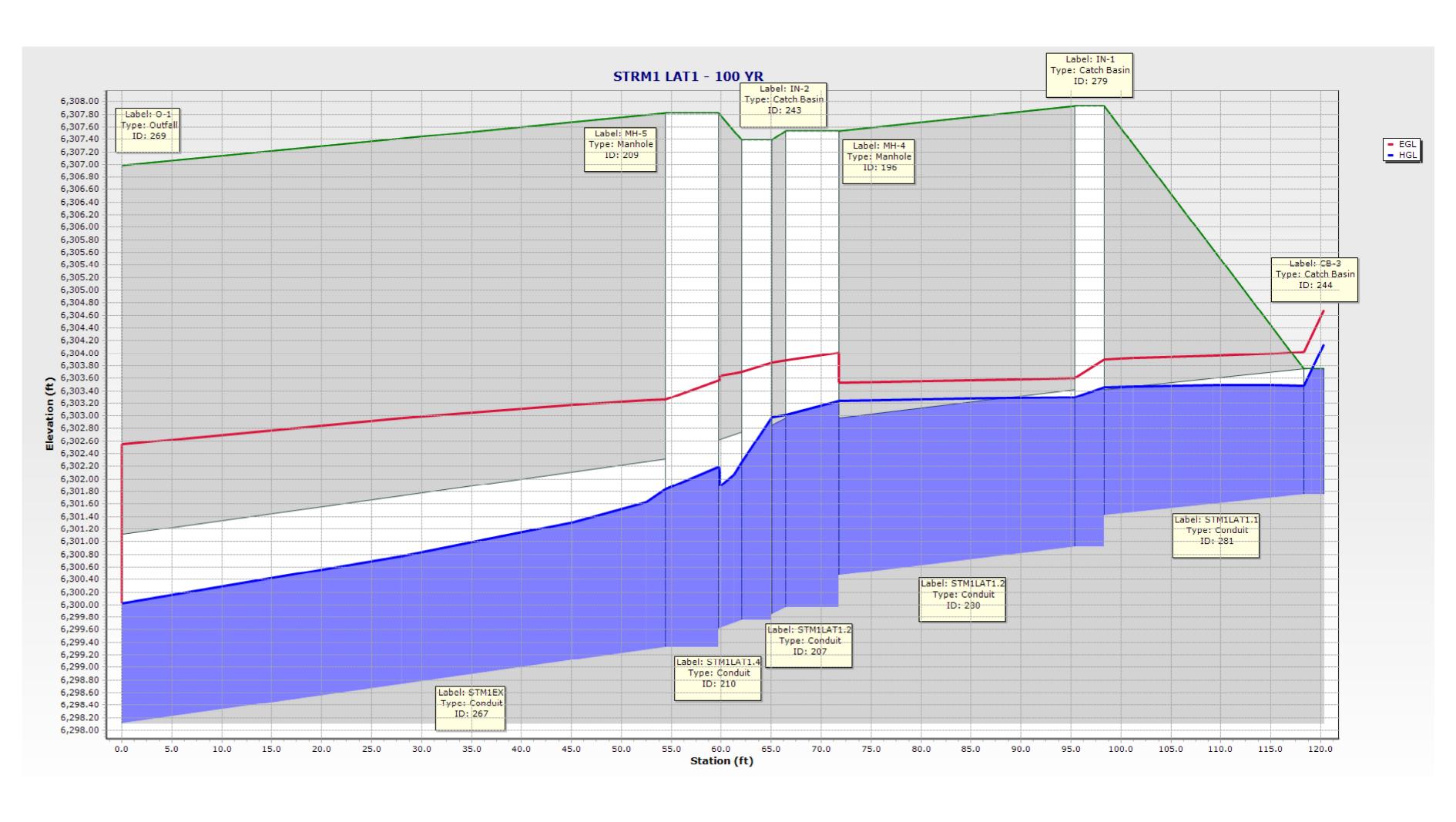
HYDRAULIC CALCULATIONS

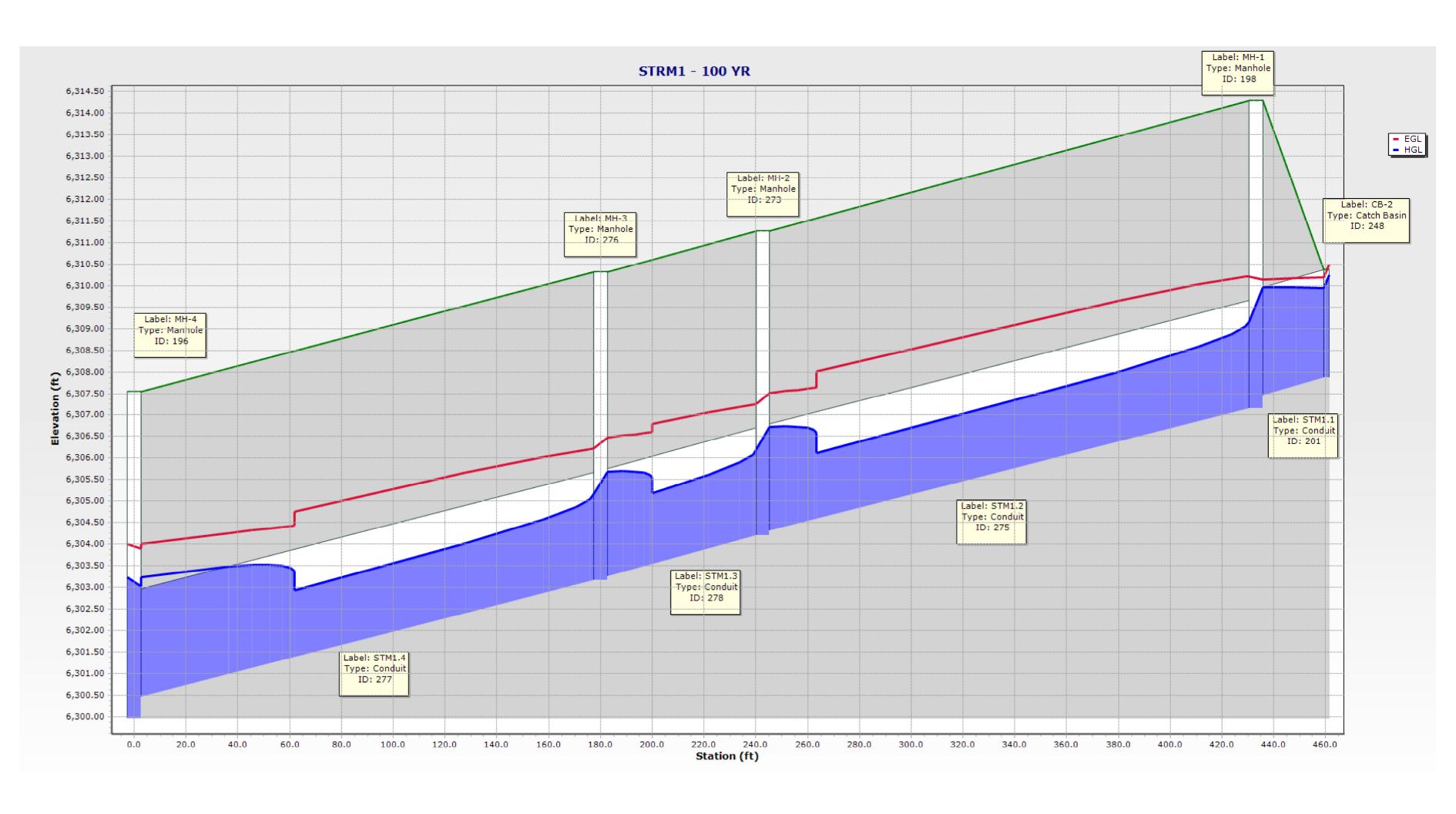
STORM 1, LAT 1, LAT 2 INDEX MAP

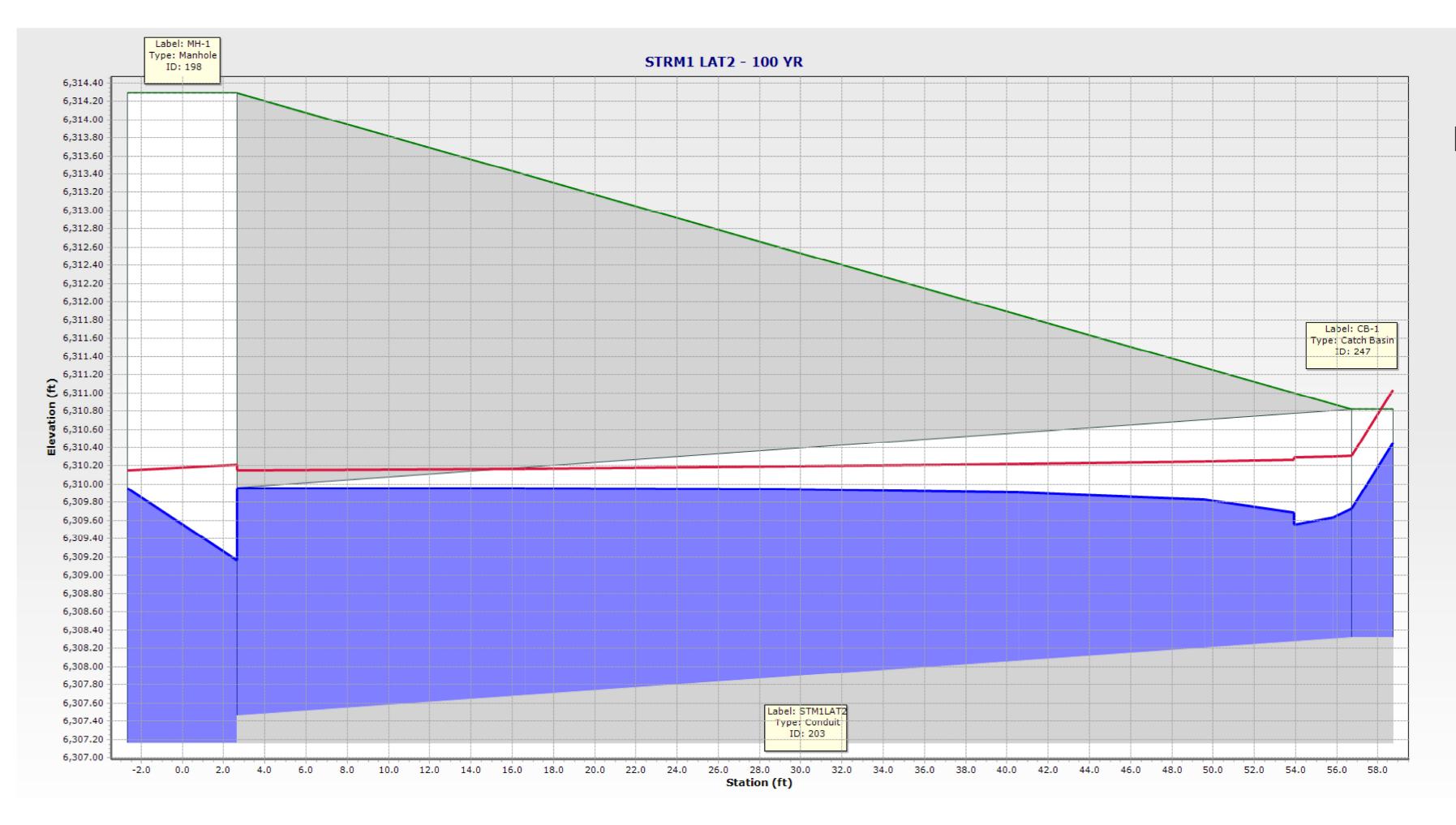


Conduit FlexTable: STRM1-LAT1-LAT2 100 YR

Label	ID	Upstream Structure	Flow (cfs)	Flow / Capacity (Design) (%)	Length (Unified) (ft)	Velocity (ft/s)	Depth (Normal) (ft)	Depth (Critical) (ft)	Energy Grade Line (In) (ft)	Energy Grade Line (Out) (ft)	Hydraulic Grade Line (In) (ft)	Hydraulic Grade Line (Out) (ft)	Headloss (ft)	Upstream Structure Hydraulic Grade Line (In) (ft)
STM1.1	201	CB-2	17.40	34.6	27.4	9.30	1.02	1.41	6,310.19	6,310.15	6,309.94	6,309.95	-0.01	6,310.25
STM1L1	203	CB-1	17.40	34.8	57.7	9.28	1.02	1.41	6,310.31	6,310.15		6,309.95	-0.22	6,310.45
STM1LAT1.2	207	MH-4	53.00	56.5	5.6	7.50	1.61	2.37	6,303.89	6,303.85	6,303.01	6,302.98	0.04	6,303.23
STM1LAT1.4	210	IN-2	60.70	64.0	6.4	14.23	1.74	2.51	6,303.70	6,303.57	6,302.26	6,302.19	0.07	6,302.98
STM1EX 11.1	267	MH-5	60.70	62.5	57.1	14.49	1.72	2.51	6,303.27	6,302.55	6,301.83	6,300.02	1.81	6,302.19
STM1.2		MH-1	34.70	69.0	190.2	11.05	1.53	2.00	6,310.22	6,307.52	6,309.16	6,306.73	2.43	6,309.95
STM1.4	277	MH-3	34.70	69.1	180.1	11.04	1.53	2.00	6,306.22	6,304.01	6,305.16	6,303.23	1.93	6,305.69
STM1.3		MH-2	34.70	69.1	62.6	11.04	1.53	2.00	6,307.26	6,306.48	6,306.20	6,305.69	0.51	6,306.73
STM1LAT1.2	280	IN-1	21.40	40.5	27.8	10.19	1.11	1.57	6,303.60	6,303.53	6,303.30	6,303.23	0.06	6,303.45
STM1LAT1.1		CB-3	16.90	61.6	22.5	9.18	1.14	1.48	6,304.01	6,303.90		6,303.45	0.04	6,304.15
Upstream Structure	Upstream	Upstream	Elevation Ground	Elevation Ground	Invert (Start)	Invert (Stop)	Conduit	Manning's n	Friction Slope	Slope				
Velocity (In- Governing) (ft/s)	Structure Headloss Coefficient	Structure Headloss (ft)	(Start) (ft)	(Stop) (ft)	(ft)	(ft)	Description	Ĵ	(ft/ft)	(Calculated) (ft/ft)				
Velocity (In- Governing)	Headloss	Headloss			(ft) 6,307.46	(ft)	Description Circle - 30.0 in	0.013		(Calculated)				
Velocity (In- Governing) (ft/s)	Headloss Coefficient	Headloss (ft)	(ft)	(ft)		(ft) 6,307.87		-	(ft/ft)	(Calculated) (ft/ft)				
Velocity (In- Governing) (ft/s)	Headloss Coefficient 1.250	Headloss (ft)	(ft) 6,314.29	(ft) 6,310.37	6,307.46	6,307.87 6,308.32	Circle - 30.0 in	0.013	(ft/ft) 0.002	(Calculated) (ft/ft) -0.015				
Velocity (In- Governing) (ft/s) 4.00 6.09	Headloss Coefficient 1.250 1.250	Headloss (ft) 0.31 0.72	(ft) 6,314.29 6,314.29	(ft) 6,310.37 6,310.82	6,307.46 6,307.46	6,307.87 6,308.32 6,299.96	Circle - 30.0 in Circle - 30.0 in	0.013 0.013	(ft/ft) 0.002 0.003	(Calculated) (ft/ft) -0.015 -0.015				
Velocity (In- Governing) (ft/s) 4.00 6.09 7.07 7.50 9.41	Headloss Coefficient 1.250 1.250 0.250	Headloss (ft) 0.31 0.72 0.22	6,314.29 6,314.29 6,307.39	6,310.37 6,310.82 6,307.54	6,307.46 6,307.46 6,299.85	6,307.87 6,308.32 6,299.96 6,299.75	Circle - 30.0 in Circle - 30.0 in Circle - 36.0 in	0.013 0.013 0.013	0.002 0.003 0.006	(Calculated) (ft/ft) -0.015 -0.020				
Velocity (In- Governing) (ft/s) 4.00 6.09 7.07 7.50	1.250 1.250 0.250 0.500	Headloss (ft) 0.31 0.72 0.22 0.72 0.36 0.79	6,314.29 6,314.29 6,307.39 6,307.82	6,310.37 6,310.82 6,307.54 6,307.39	6,307.46 6,307.46 6,299.85 6,299.62	6,307.87 6,308.32 6,299.96 6,299.75 6,299.32	Circle - 30.0 in Circle - 30.0 in Circle - 36.0 in Circle - 36.0 in	0.013 0.013 0.013 0.013	0.002 0.003 0.006 0.020	(Calculated) (ft/ft) -0.015 -0.015 -0.020 -0.020				
Velocity (In- Governing) (ft/s) 4.00 6.09 7.07 7.50 9.41 3.55 7.13	1.250 1.250 0.250 0.500 0.250 0.750 0.500	Headloss (ft) 0.31 0.72 0.22 0.72 0.36 0.79 0.53	6,314.29 6,314.29 6,307.39 6,307.82 6,306.99	6,310.37 6,310.82 6,307.54 6,307.39 6,307.82 6,314.29 6,310.31	6,307.46 6,307.46 6,299.85 6,299.62 6,298.11 6,304.30 6,300.46	6,307.87 6,308.32 6,299.96 6,299.75 6,299.32 6,307.16 6,303.16	Circle - 30.0 in Circle - 30.0 in Circle - 36.0 in Circle - 36.0 in Circle - 36.0 in Circle - 30.0 in Circle - 30.0 in	0.013 0.013 0.013 0.013 0.013 0.013	0.002 0.003 0.006 0.020 0.013 0.014 0.012	-0.015 -0.020 -0.020 -0.021 -0.015 -0.015				
Velocity (In- Governing) (ft/s) 4.00 6.09 7.07 7.50 9.41 3.55 7.13 7.13	1.250 1.250 0.250 0.500 0.750 0.500 0.500	Headloss (ft) 0.31 0.72 0.22 0.72 0.36 0.79 0.53 0.53	6,314.29 6,314.29 6,307.39 6,307.82 6,306.99 6,311.27	(ft) 6,310.37 6,310.82 6,307.54 6,307.39 6,307.82 6,314.29 6,310.31 6,311.27	6,307.46 6,307.46 6,299.85 6,299.62 6,298.11 6,304.30	6,307.87 6,308.32 6,299.96 6,299.75 6,299.32 6,307.16 6,303.16 6,304.20	Circle - 30.0 in Circle - 30.0 in Circle - 36.0 in Circle - 36.0 in Circle - 36.0 in Circle - 30.0 in Circle - 30.0 in Circle - 30.0 in	0.013 0.013 0.013 0.013 0.013 0.013 0.013	0.002 0.003 0.006 0.020 0.013 0.014 0.012 0.012	-0.015 -0.015 -0.020 -0.020 -0.021 -0.015 -0.015 -0.015				
Velocity (In- Governing) (ft/s) 4.00 6.09 7.07 7.50 9.41 3.55 7.13	1.250 1.250 0.250 0.500 0.250 0.750 0.500	Headloss (ft) 0.31 0.72 0.22 0.72 0.36 0.79 0.53	6,314.29 6,314.29 6,307.39 6,307.82 6,306.99 6,311.27 6,307.54	6,310.37 6,310.82 6,307.54 6,307.39 6,307.82 6,314.29 6,310.31	6,307.46 6,307.46 6,299.85 6,299.62 6,298.11 6,304.30 6,300.46	6,307.87 6,308.32 6,299.96 6,299.75 6,299.32 6,307.16 6,303.16 6,304.20 6,300.92	Circle - 30.0 in Circle - 30.0 in Circle - 36.0 in Circle - 36.0 in Circle - 36.0 in Circle - 30.0 in Circle - 30.0 in	0.013 0.013 0.013 0.013 0.013 0.013	0.002 0.003 0.006 0.020 0.013 0.014 0.012	-0.015 -0.020 -0.020 -0.021 -0.015 -0.015				



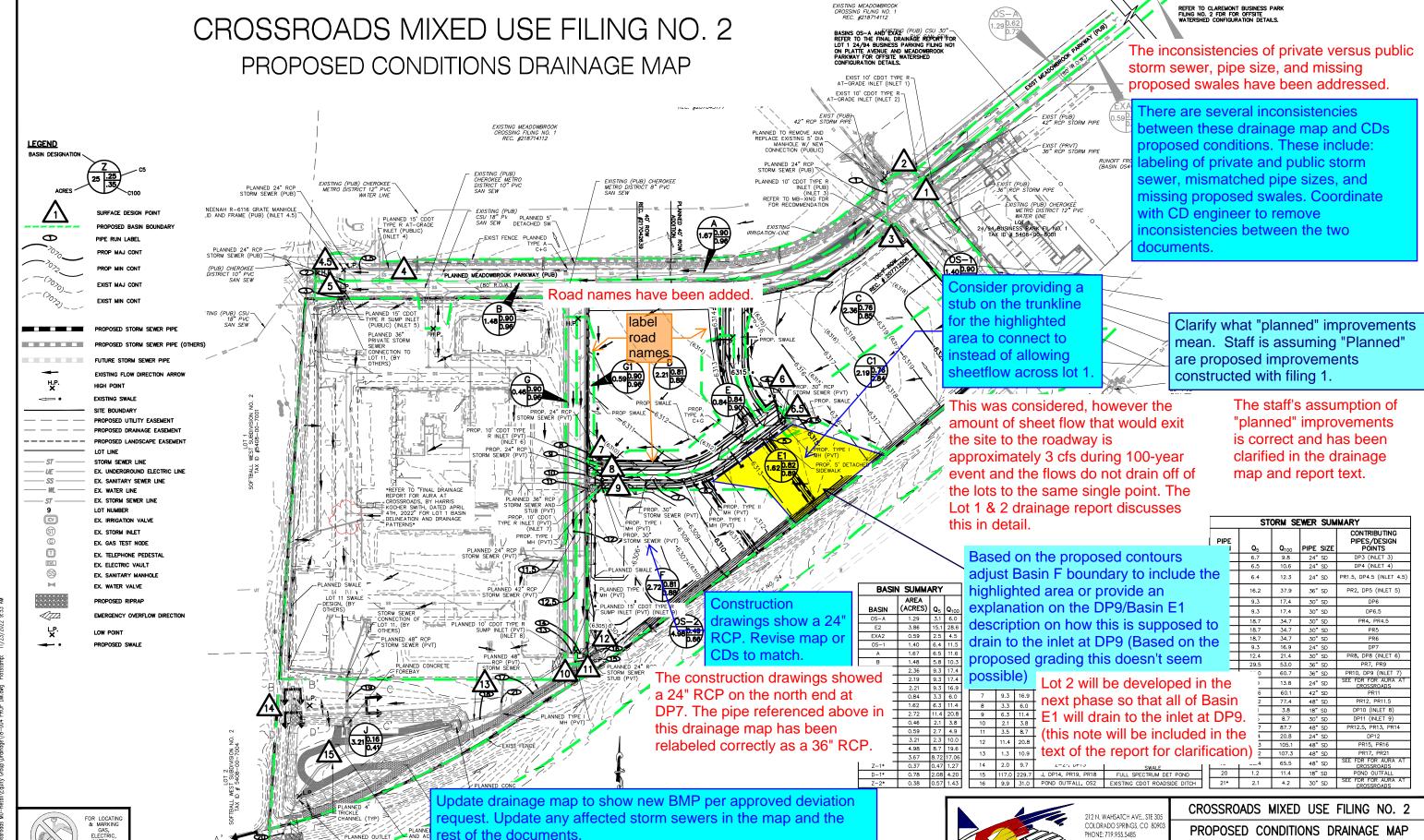






BACKGROUND

DRAINAGE MAPS



The drainage map, drainage calculations and drainage report have

been updated to reflect the BMP modification from Filing No.1.

48 HRS BEFORE YOU DIG

CALL 1-800-922-1987

SCALE: DATE: 11/23/2022 DESIGNED BY TAU DRAWN BY: SHEET 1 OF 1 **PDM**

CHECKED BY:

V1_Drainage Report - Final.pdf Markup Summary

dsdlaforce (5)



Subject: Text Box

Page Label: [1] DRAINAGE

Lock: Unlocked Author: dsdlaforce

Date: 2/6/2023 5:17:38 PM

Status: Color: Layer: Space: Clarify what "planned" improvements mean. Staff is assuming "Planned" are proposed improvements constructed with filing 1.

1.) "Final Drainage Report for Crossroads Mixed Use Fi M&S Civil Consultants, Inc.

Add a reference to the Drainage Letter for the Underground Detention per (PCD Subject: Callout Page Label: 17 Lock: Unlocked

Author: dsdlaforce

Date: 2/9/2023 10:08:15 AM

Status: Color: Layer: Space: Add a reference to the Drainage Letter for the Underground Detention per (PCD File No CDR232)



Subject: Text Box Page Label: 9

Lock: Unlocked Author: dsdlaforce

Date: 2/9/2023 10:58:23 AM

Status: Color: Layer: Space: Provide narrative for DP 6.5, DP 8, DP 9 and DP



Subject: Polygon

Page Label: [1] DRAINAGE

Lock: Unlocked
Author: dsdlaforce

Date: 2/9/2023 10:58:47 AM

Status: Color: Layer: Space:



Subject: Callout

Page Label: [1] DRAINAGE

Lock: Unlocked Author: dsdlaforce

Date: 2/9/2023 11:10:54 AM

Status: Color: Layer: Space: Based on the proposed contours adjust Basin F boundary to include the highlighted area or provide an explanation on the DP9/Basin E1 description on how this is supposed to drain to the inlet at DP9 (Based on the proposed grading this doesn't seem possible)

Glenn Reese - EPC Stormwater (6)

The second section of the section of t

Subject: SW - Highlight

Page Label: 9 Lock: Unlocked

Author: Glenn Reese - EPC Stormwater

Date: 2/2/2023 12:19:00 PM

Status: Color: Layer: Space: Approx. 2.54 acres of the proposed

developmen

rates of 9.9 and 28.0 cfs in the 5 and 100 at this location was analyzed in the 100 y sendix.

Subject: SW - Textbox with Arrow

Page Label: 9 Lock: Unlocked

Author: Glenn Reese - EPC Stormwater

Date: 2/2/2023 12:19:38 PM

Status:
Color: Layer:
Space:

Clarify that this being done in Filing 1.

Subject: SW - Highlight

Page Label: 9 Lock: Unlocked

Author: Glenn Reese - EPC Stormwater

Date: 2/2/2023 12:22:38 PM

Status: Color: Layer: Space: In the interim, runoff will be reduced through the

use of (4)

temporary sediments ponds

icco wrann or copuses area containing impervious surfaces wat areas or earthen swales (grass-lined where slope exceeds 2%) t of impervious surfaces. In the interim, ranoff will be reduced three ediments ponds until the ground has been stabilized with vogetatis

exts on downstream drainage ways since flows released will be below the site proposes. four temperary sedimentation posdle, before is repeny comes of the site and onto an adjacent undeveloped proper his essuares that in this stage of the development negative efficies c a will be avoided.

tfall lined with rip rap. From here it continues southwest in CDOT's reaches Peterson Road. It is then conveyed to the other side of the road win a No CMP reducer. The designant continues weathward in the r

Subject: SW - Highlight

Page Label: 9 Lock: Unlocked

Author: Glenn Reese - EPC Stormwater

Date: 2/2/2023 12:23:39 PM

Status: Color: Layer: Space: proposes four temporary sedimentation ponds

reas or earthen swales (grass-lined where :
impervious surfaces. In the interim, runoff
diments ponds until the ground has been sta

Stabilize Drainageways - The development its on downstream drainage ways since flows the the site proposes four temporary sedimental operty corner of the site and onto an adjacent is ensures that in this stage of the development Subject: SW - Textbox with Arrow

Page Label: 9 Lock: Unlocked

Author: Glenn Reese - EPC Stormwater

Date: 2/2/2023 12:23:43 PM

Status: Color: ■ Layer: Space: Show location on plans



Subject: SW - Textbox with Arrow

Page Label: [1] DRAINAGE

Lock: Unlocked

Author: Glenn Reese - EPC Stormwater

Date: 2/2/2023 12:30:35 PM

Status: Color: Layer: Space: label road names

lpackman (12)



Subject: Text Box

Page Label: [1] DRAINAGE

Lock: Unlocked Author: lpackman

Date: 1/31/2023 2:57:15 PM

Status: Color: Layer: Space: There are several inconsistencies between these drainage map and CDs proposed conditions. These include: labeling of private and public storm sewer, mismatched pipe sizes, and missing proposed swales. Coordinate with CD engineer to remove inconsistencies between the two

documents.



Subject: Cloud+ Page Label: 10 Lock: Unlocked Author: lpackman

Date: 2/1/2023 1:06:29 PM

Status: Color: Layer: Space: Update entire section to discuss the proposed underground water quality system. Include information on TSS removal and/or WQCV, whichever is being used to meet WQ criteria. For TSS information make sure to include provided rate vs what is required per criteria. Include project number and name for submitted deviation request and cdr project.



Subject: Callout Page Label: 15 Lock: Unlocked Author: lpackman

Date: 2/1/2023 1:08:19 PM

Status: Color: Layer: Space: See comment on step #3 on four step process and update this narrative accordingly to include system being used and maintenance of BMP.



Subject: Cloud+ Page Label: 16 Lock: Unlocked Author: Ipackman

Date: 2/1/2023 1:17:16 PM

Status: Color: Layer: Space: Update to use 2023 drainage and bridge fees.



Subject: Cloud+ Page Label: 16 Lock: Unlocked Author: Ipackman

Date: 2/1/2023 1:30:35 PM

Status: Color: Layer: Space: Update percent impervious to be specific to this filing.



Subject: Callout Page Label: 16 Lock: Unlocked Author: Ipackman

Date: 2/1/2023 1:54:59 PM **Status:**

Status: Color: Layer: Space: Include a breakdown of tract d impervious values in the appendix with the rest of the calculations.



Subject: Text Box Page Label: 4 Lock: Unlocked Author: lpackman

Date: 2/1/2023 2:01:38 PM

Status: Color: Layer: Space: Update report contents to change any mention of the FSD pond to the new BMP that is being used throughout the report.



Subject: Text Box

Page Label: [1] DRAINAGE

Lock: Unlocked Author: lpackman

Date: 2/1/2023 2:12:40 PM

Status: Color: Layer: Space: Update drainage map to show new BMP per approved deviation request. Update any affected storm sewers in the map and the rest of the documents.



Subject: Callout Page Label: 16 Lock: Unlocked

Author: lpackman **Date:** 2/1/2023 3:26:24 PM

Status: Color: Layer: Space: Add in this narrative that tracts B and C will not be included in the drainage fee and will be assessed

in the future.



Subject: Callout Page Label: 1 Lock: Unlocked Author: Ipackman

Date: 2/2/2023 12:34:19 PM

Status: Color: Layer: Space: EPC's EDARP File Number: SF2238 (with no dashes or extras zeros or extra spaces in the file

number)



Subject: Callout

Page Label: [1] DRAINAGE

Lock: Unlocked Author: lpackman

Date: 2/6/2023 5:06:45 PM

Status: Color: Layer: Space: Construction drawings show a 24" RCP. Revise map or CDs to match.



Subject: Callout

Page Label: [1] DRAINAGE

Lock: Unlocked Author: lpackman

Date: 2/9/2023 1:19:18 PM

Status: Color: Layer: Space: Consider providing a stub on the trunkline for the highlighted area to connect to instead of allowing

sheetflow across lot 1.