EPCD File No. SF-19-004/CDR-20-012

Prepared For:

SR Land, LLC 20 Boulder Crescent, Suite 210 Colorado Springs, CO 80903

> June 16, 2021 Project No. 25188.00

Prepared By:
JR Engineering, LLC
5475 Tech Center Drive, Suite 235
Colorado Springs, CO 80919
719-593-2593



ENGINEER'S STATEMENT:

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by El Paso County for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors, or omissions on my part in preparing this report.

Mike Bramlett, Colorado P.E. # 32314
For and On Behalf of JR Engineering, LLC

32314 GOVE BRAME 32314 GOVAL ENGINE

DEVELOPER'S STATEMENT:

I, the developer, have read and will comply with all of the requirements specified in this drainage report and plan.

Business Name: SR Land, LLC

By:

Title: Address:

20 Boulder Crescent, Suite 210

Colorado Springs, CO 80903

El Paso County:

Filed in accordance with the requirements of the El Paso County Land Development Code, Drainage Criteria Manual, Volumes 1 and 2 and Engineering Criteria Manual, as amended.

APPROVED Engineering Department 04/14/2022 2:38:52 PM dsdnijkamp

EPC Planning & Community Development Department

Jennifer Irvine, P.E.

County Engineer/ ECM Administrator

Date

Conditions:



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MHFD Detention workbook Sand Filter 1

MHFD Detention workbook Sand Filter 2

Proposed basin map (limited to Basins X1, X2, W1, & Y1)



PURPOSE

This document is an Addendum to the Final Drainage Report for Homestead at Sterling Ranch Filing No. 2. The purpose of this report is to update the approved "Final Drainage Report for Homestead at Sterling Ranch Filing No. 2". The scope of the updates included in this addendum are limited to proposed Basins W1, X1, X2, & Y1. More specifically, this Addendum proposes to replace the proposed individual lot Sand Filters for lots 13-24, 28-35, and 36-41 with two common Sand Filters, one to serve basin X1, lots 36-41, and one to serve basins W1, X2, & Y1, lots 13-24 & 28-35.

The text below replaces the original corresponding text from the Final Drainage Report for Homestead at Sterling Ranch Filing No. 2. The revised sections of the original report are marked in the table of contents below, and also crossed out/highlighted in the attached original report. Crossed out text is replaced and highlighted text is modified or discussed further herein.

PROPSED DRAINAGE CHARACTERISTICS

DETAILED DRAINAGE DISCUSSION (DESIGN POINTS)

BASIN X1 (0.78 acres), consists of proposed residential backyards of lots 36-41 along the eastern boundary of the site with runoff coefficients of 0.22 for the 5 year and 0.46 for the 100 year. Runoff in this basin will be directed via backyard swales/berms towards the rear of the lots where it will be collected in a 12" Nyoplast Drain Basin w/ a 12" dome grate placed in the rear southwest corner of each lot. Each lot will have a half foot berm/swale along the rear and low side of lot that directs water to each inlet, see the detail included on the drainage map, GESC, and Storm plans. Should the inlet in any lot become clogged, the berm will overtop, and flow will continue to Sand Creek. Per the original drainage report by MandS, the estimated flows per each lot in basin X1 = 0.2 cfs for the 100 year storm. The 12" Nyoplast Drain Basins are sized to collect all flows (Q5 = 0.6 cfs, Q100 = 2.3 cfs) in both the 5 and 100 year storms. Collected flows will then be piped to a proposed full-spectrum sand filter, with a 12-hour drain time and a 4" perforated underdrain. The treated flows from the sand filter will be discharged via an outlet structure to the adjacent Sand Creek.

BASIN X2 (1.04 acres), consists of proposed residential backyards of lots 28-35 along the southern boundary of the site with runoff coefficients of 0.22 for the 5 year and 0.46 for the 100 year. Runoff in this basin will be directed via backyard swales/berm towards the rear of the lots where it will be collected in a 12" Nyoplast Drain Basin w/ a 12" dome grate placed in the rear southwest corner of each lot (DP2). Each lot will have a half foot berm/swale along the rear and low side of lot that directs water to each inlet, see the detail included on the drainage map, GESC, and Storm plans. Should the inlet in any lot become clogged, the berm will overtop, and flow will continue to Sand Creek, per existing drainage patterns. The 12" Nyoplast Drain Basins are sized to collect all flows



(Q5 = 0.9 cfs, Q100 = 3.0 cfs) in both the 5 and 100 year storms. Collected flows will then be piped west via 12" HDPE pipe following the rear lot lines towards DP3.1, where flows in the pipe combine with collected flows from Basin W1. See below for DP 3.1 flows.

BASIN W1 (0.86 acres), consists of proposed residential backyards of lots 19-24 along the southeastern boundary of the site with runoff coefficients of 0.22 for the 5 year and 0.46 for the 100 year. Runoff in this basin will be directed via backyard swales towards the rear of the lots where it will be collected in a 12" Nyoplast Drain Basin w/ a 12" dome grate placed in the rear corner of each lot (DP3). Each lot will have a half foot berm/swale along the rear and low side of lot that directs water to each inlet, see the detail included on the drainage map, GESC, and Storm plans. Should the inlet in any lot become clogged, the berm will overtop, and flow will continue to Sand Creek per existing drainage patterns. The 12" Nyoplast Drain Basins are sized to collect all flows (Q5 = 0.6 cfs, Q100 = 2.2 cfs) in both the 5 and 100 year storms. Collected flows will then be piped southwest via 12" HDPE pipe following the rear lot lines towards DP3.1, where flows in the pipe combine with collected flows from Basin X2 (Q5 = 1.3 cfs, Q100 = 4.6 cfs).

Flows in the pipe at DP3.1 are then piped to DP4.1 where they combine with collected flows from Basin Y1 (Q5 = 1.7 cfs, Q100 = 6.4 cfs).

BASIN Y1 (0.84 acres), consists of proposed residential backyards of lots 13-18 along the southeastern boundary of the site with runoff coefficients of 0.22 for the 5 year and 0.46 for the 100 year. Runoff in this basin will be directed via backyard swales towards the rear of the lots where it will be collected in a 12" Nyoplast Drain Basin w/ a 12" dome grate placed in the rear corner of each lot (DP4). Each lot will have a half foot berm/swale along the rear and low side of lot that directs water to each inlet, see the detail included on the drainage map, GESC, and Storm plans. Should the inlet in any lot become clogged, the berm will overtop, and flow will continue to Sand Creek per existing drainage patterns. The 12" Nyoplast Drain Basins are sized to collect all flows (Q5 = 0.7 cfs, Q100 = 2.5 cfs) in both the 5 and 100 year storms. Collected flows will then be piped southwest via 12" HDPE pipe following the rear lot lines to a proposed full spectrum sand filter at DP4.1, where flows combine with collected flows from Basin X2 and W1 (Q5 = 1.7 cfs, Q100 = 6.4 cfs).

The basin characteristics, hydrologic parameters, runoff and rational calcs for Basins X1, X2, W1, and Y1 have remained consistent with the approved Final Drainage Report for Homestead at Sterling Ranch Filing No. 2. However, the routing of the basins has changed and therefore revised SF-2 & SF-3 forms are included in the appendix section of this report. A revised basin map, showing the changes within the above described basins is also attached to this report.

WATER QUALITY PROVISIONS

Runoff produced within the residential backyard lots, of Basin X1 will be conveyed in backyard swales, collected in drain basins and directed to a full-spectrum sand filter (sand filter 1). The treated



flows will be collected by private storm sewer systems and discharged into the Sand Creek Channel. Sand filter basin 1 is designed to provide 0.007 ac-ft of water quality storage (WQCV), 0.013 ac-feet of excess urban runoff volume (EURV) and 0.03 ac-ft of 100-year storage for a total design volume of 0.027 ac-ft. Sand filter basin 1 was designed to have a 12 hour WQCV drain time and a peak outflow for the 100 year design storm of 0.7 cfs which roughly equates to 90% of pre-development peak flows. The sand filter will outfall via an orifice controlled 12" HDPE pipe and FES directly to the adjacent Sand Creek channel. Sand filter basin 1 will also include a 4" perforated underdrain system and emergency overflow spillway designed to pass the undetained peak 100-yr flow rate with one foot of freeboard above the design water surface elevation. The peak discharge rate of the proposed sand filter is at or below the historic flows for the basin which it serves.

Runoff produced within the residential backyard lots, of Basins X2, W1, and Y1 will be conveyed in backyard swales, collected in drain basins and directed to a full-spectrum sand filter (sand filter 2). The treated flows will be collected by private storm sewer systems and discharged, ultimately, into the Sand Creek Channel. The sand filter will outfall via an orifice controlled 15" HDPE pipe that is directly connected to the existing 60" RCP storm sewer outfall pipe of existing "Pond 4".

Sand filter basin 2 is designed to provide 0.025 ac-ft of water quality storage (WQCV), 0.045 ac-feet of excess urban runoff volume (EURV) and 0.094 ac-ft of 100-year storage for a total minimum design volume of 0.163 ac-ft. Sand filter basin 2 was designed to have a 12 hour WQCV drain time and a peak outflow for the 100 year design storm of 2.7 cfs which is less than or equal to predevelopment peak flow rates. The sand filter will outfall via an orifice controlled 15" HDPE pipe directly connected to the existing 60" RCP pipe to the south that serves as the outfall to "Pond 4" constructed with Sterling Ranch Filing No. 1. Sand filter basin 2 will also include a 4" perforated underdrain system and emergency overflow spillway designed to pass the peak 100-yr flow rate with one foot of freeboard above the design water surface elevation. The peak discharge rate of the proposed sand filter is at or below the historic flows for the basins which it serves.

MAINTENANCE ENTITY

Both proposed sand filters are contained within existing Tract D, of the Homestead at Sterling Ranch Filing No. 2 development. The proposed sand filter facilities are to be maintained by the Sterling Ranch Metropolitan District. Access to maintain these sand filter basins is from the forthcoming maintenance access road that is being designed as part of the naturalized channel design being completed by JR Engineering.

The proposed sand filters were sized using the MHFD Detention workbook and printouts are included in the Hydraulic Calculations section of this report.

CONSTRUCTION COST OPINION – HOMESTEAD AT STERLING RANCH FIL. NO. 2



Drainage improvements are planned with the development of Homestead at Sterling Ranch Filing No. 2. A majority of the construction costs have been accounted for in the "Master Development Drainage Report for Sterling Ranch Filing Nos. 1&2, and Final Drainage Report for Sterling Ranch Filing No.1" prepared by MS Civil Consultants, dated April 2017. Any additional improvements and costs are listed below.

The following list of drainage improvements is Non-Reimbursable.

ltem	Description	Quantity Prev	Quantity Now	Unit	Uı	nit Cost		Cost
1	18" RCP	31	31	LF	\$	40	\$	1,24
2	24" RCP	127	127	LF	\$	50	\$	6,35
3	30" RCP	998	998	LF	\$	85	\$	84,83
4	36" RCP	8	8	LF	\$	105	\$	84
5	42" RCP	699	699	LF	\$	185	\$1	129,31
6	24" FES	1	1	EA	\$	750	\$	75
8	42" FES	1	1	EA	\$	1,250	\$	1,25
9	5.0'x4.5' CDOT Type R Sump Inlet	1	1	EA	\$	4,000	\$	4,00
10	10' CDOT Type R Sump Inlet	4	4	EA	\$	4,700	\$	18,80
11	15' CDOT Type R At-Grade Inlet	2	2	EA	\$	6,000	\$	12,00
12	4.0' Type II MH	1	1	EA	\$	3,500	\$	3,50
13	5.0' Type II MH	2	2	EA	\$	4,000	\$	8,00
14	6.0' Type II MH	1	1	EA	\$	4,500	\$	4,50
17	5.0'x6.0' MH	2	2	EA	\$	6,500	\$	13,00
18	5.5'x5.5' MH	1	1	EA	\$	6,500	\$	6,50
19	Headwall/Wingwall	1	1	EA	\$	6,000	\$	6,00
20	Full Spectrum Det. Pond 1	1	1	EA	\$	15,000	\$	15,00
21	FSD Pond 1 Outlet Structure	1	1	EA	\$	12,600	\$	12,60
22	Ind. Lot Sand filter	26	0	EA	\$	2,000	\$	-
23	18" Drain basin MH	27	0	EA	\$	1,000	\$	-
24	12" Storm pipe	1,658	1,960	LF	\$	26	\$	50,96
25	15" Storm pipe	0	473	LF	\$	32	\$	15,13
26	12" Nyloplast Drain basin w/ 12" dome grate	0	28	EA	\$	1,000	\$	28,00
27	Sand Filter Basin 1	0	1	LS	\$	4,000	\$	4,00
28	Sand Filter Basin 2	0	1	LS	\$	6,000	\$	6,00
29	12"- 15" FES	0	4	EA	\$	350	\$	1,40
						TOTAL	\$4	133,97



REVISED APPENDIX MATERIALS



STANDARD FORM SF-2 TIME OF CONCENTRATION

Subdivision: Homestead at Sterling Ranch Filing No. 2 **Location:** Colorado Springs

Project Name: Homestead at Sterling Ranch Filing No. 2 Project No.: 2000-5188.00 Calculated By: REB Checked By: **Date:** 3/18/21

		SUB-	BASIN			INITI	AL/OVERI	LAND			TRAVEL TII	ME	tc CHECK								
		D/	ATA				(T _i)			(T _t) (URBANIZED BASINS)					(T _t)					SINS)	FINAL
BASIN	D.A.	Hydrologic	Impervious	C ₅	C ₁₀₀	L	S _o	t,	L _t	S _t	К	VEL.	t t	COMP. t _c	TOTAL	Urbanized t_c	t _c				
ID	(ac)	Soils Group	(%)			(ft)	(%)	(min)	(ft)	(%)		(ft/s)	(min)	(min)	LENGTH (ft)	(min)	(min)				
W1	0.86	В	25%	0.22	0.46	100	2.0%	12.6	50	0.0%	20.0	0.2	4.2	16.8	150.0	28.4	16.8				
X1	0.78	В	25%	0.22	0.46	100	2.0%	12.6	50	2.5%	20.0	3.2	0.3	12.9	150.0	22.2	12.9				
X2	1.04	В	25%	0.22	0.46	100	2.0%	12.6	50	2.5%	20.0	3.2	0.3	12.9	150.0	22.2	12.9				
Y1	0.84	В	25%	0.22	0.46	100	2.0%	12.6	50	2.5%	20.0	3.2	0.3	12.9	150.0	22.2	12.9				

NOTES:

 $t_c = t_i + t_t$

Equation 6-2

$$t_i = \frac{0.395(1.1 - C_5)\sqrt{L_i}}{S_o^{0.33}}$$

Equation 6-3

Where:

 t_c = computed time of concentration (minutes)

 t_i = overland (initial) flow time (minutes)

 t_t = channelized flow time (minutes).

$$t_t = \frac{L_t}{60K_0/S_c} = \frac{L_t}{60V_0}$$

Where:

 t_i = overland (initial) flow time (minutes)

 L_1 = overland (initial) row talk (initials) L_2 = runoff coefficient for 5-year frequency (from Table 6-4) L_3 = length of overland flow (ft)

 S_0 = average slope along the overland flow path (ft/ft).

$$=\frac{L_t}{60K\sqrt{S_o}}=\frac{L_t}{60V_t}$$

Equation 6-4

$$t_c = (26 - 17i) + \frac{L_t}{60(14i + 9)\sqrt{S_t}}$$

Equation 6-5

 t_t = channelized flow time (travel time, min)

 L_t = waterway length (ft)

 $S_o = \text{waterway slope (ft/ft)}$

 V_t = travel time velocity (ft/sec) = K $\sqrt{S_o}$ K = NRCS conveyance factor (see Table 6-2). Where:

 t_c = minimum time of concentration for first design point when less than t_c from Equation 6-1.

 L_t = length of channelized flow path (ft)

i = imperviousness (expressed as a decimal) $S_t = \text{slope of the channelized flow path (ft/ft)}.$

Use a minimum t_c value of 5 minutes for urbanized areas and a minimum t_c value of 10 minutes for areas that are not considered urban. Use minimum values even when calculations result in a lesser time of concentration

Table 6-2. NRCS Conveyance factors, K

	.,
Type of Land Surface	Conveyance Factor, K
Heavy meadow	2.5
Tillage/field	5
Short pasture and lawns	7
Nearly bare ground	10
Grassed waterway	15
Paved areas and shallow paved swales	20

STANDARD FORM SF-3

STORM DRAINAGE SYSTEM DESIGN

(RATIONAL METHOD PROCEDURE)

	Project Name:	Homestead at Sterling Ranch Filing No. 2
Subdivision: Homestead at Sterling Ranch Filing No. 2	Project No.:	2000-5188.
Location: Colorado Springs	Calculated By:	REB
Design Storm: 5-Year	Checked By:	
	Date:	3/18/21

				DIRE	CT RUI	NOFF			TO	OTAL I	RUNO	FF		PIP	E		TRAV	EL TIN	ΛE	
STREET	Design Point	Basin ID	Area (Ac)	Runoff Coeff.	t_c (min)	C* A (Ac)	(in/hr)	Q (cfs)	tc (min)	C* A (ac)	/ (in/hr)	Q (cfs)	Q _{pipe} (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	$t_{ m r}$ (min)	REMARKS
	1	X1	0.78	0.22	12.9	0.17	3.75	0.6					0.6	0.17	0.5	18	250	1.7	2.5	Runoff from Basin X1, collected by private 12" Nyoplast Drain Basins, Piped via 12" HDPE to pvt. sand filter @ DP1.1
	2	X2	1.04	0.22	12.9	0.23	3.75	0.9					0.9	0.23	1.5	12	950	2.8	5.6	Runoff from Basin X2, collected by private 12" Nyoplast Drain Basins, Piped via 12" HDPE to DP3.1
	3	W1	0.86	0.22	16.8	0.19	3.35	0.6					0.6	0.19	1.5	12	250	2.6	1.6	Runoff from Basin W1, collected by private 12" Nyoplast Drain Basins, Piped via 12" HDPE to DP3.1
	3.1								20.1	0.42	3.08	1.3								Combined flow in private 12" HDPE pipe @ DP3.1, piped to private sand filter @ DP-4.1
	4	Y1	0.84	0.22	12.9	0.18	3.75	0.7					0.7	0.18	1.5	15	350	2.4		Runoff from Basin Y1, collected by private 12" Nyoplast Drain Basins, Piped via 15" HDPE to DP4.1
	4.1								22.5	0.60	2.91	1.7								Combined flow in private 15" HDPE pipe @ DP4.1, inflow to proposed private sand filter

Notes:

Street and Pipe C*A values are determined by Q/i using the catchment's intensity value All pipes are private and RCP unless otherwise noted. Pipe size shown in table column.

STANDARD FORM SF-3

STORM DRAINAGE SYSTEM DESIGN

(RATIONAL METHOD PROCEDURE)

	Project Name: Homestead at Sterling Ranch Filing No. 2	
Subdivision: Homestead at Sterling Ranch Filing No. 2	Project No.: 2000-5188.	
Location: Colorado Springs	Calculated By: REB	
Design Storm: 100-Year	Checked By:	
	Date: 3/18/21	

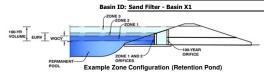
				DIR	ECT RI	JNOFF			TO	OTAL R	UNOF	F		PII	PE		TRAV	EL TIN	ME	
Description	Design Point	Basin ID	Area (ac)	Runoff Coeff.	t_c (min)	C*A (ac)	/ (in/hr)	Q (cfs)	tc (min)	C*A (ac)	(in/hr)	Q (cfs)	Q _{pipe} (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	t _t (min)	REMARKS
	1	X1	0.78	0.46	12.9	0.36	6.29	2.3					2.3	0.36	0.5		250	2.2		Runoff from Basin X1, collected by private 12" Nyoplast Drain Basins, Piped via 12" HDPE to pvt. sand filter @ DP1.1
	2	X2	1.04	0.46	12.9	0.48	6.29	3.0					3.0	0.48	1.0	12	950	3.1	5.1	Runoff from Basin X2, collected by private 12" Nyoplast Drain Basins, Piped via 12" HDPE to DP3.1
	3	W1	0.86	0.46	16.8	0.40	5.62	2.2					2.2	0.40	1.0	12	250	2.9	1.4	Runoff from Basin W1, collected by private 12" Nyoplast Drain Basins, Piped via 12" HDPE to DP3.1
	3.1								19.4	0.88	5.26	4.6								Combined flow in private 12" HDPE pipe @ DP3.1, piped to private sand filter @ DP-4.1
	4	Y1	0.84	0.46	12.9	0.39	6.29	2.5					2.5	0.39	1.5	15	350	3.3	1.8	Runoff from Basin Y1, collected by private 15" Nyoplast Drain Basins, Piped via 12" HDPE to DP4.1
1	4.1								21.1	1.27	5.05	6.4								Combined flow in private 15" HDPE pipe @ DP4.1, inflow to proposed private sand filter

Notes:
Street and Pipe C*A values are determined by Q/i using the catchment's intensity value.
All pipes are private and RCP unless otherwise noted. Pipe size shown in table column.

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.04 (February 2021)

Project: Homestead at Sterling Ranch Filing No. 2



Watershed Information

Selected BMP Type =	SF	
Watershed Area =	0.78	acres
Watershed Length =	450	ft
Watershed Length to Centroid =	225	ft
Watershed Slope =	0.020	ft/ft
Watershed Imperviousness =	25.00%	percent
Percentage Hydrologic Soil Group A =	0.0%	percent
Percentage Hydrologic Soil Group B =	100.0%	percent
Percentage Hydrologic Soil Groups C/D =	0.0%	percent
Target WQCV Drain Time =	12.0	hours
Location for 1-hr Rainfall Depths =	User Input	

After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

the embedded Colorado Urban Hydro	graph Procedu	re.
Water Quality Capture Volume (WQCV) =	0.007	acre-feet
Excess Urban Runoff Volume (EURV) =	0.020	acre-feet
2-yr Runoff Volume (P1 = 1.19 in.) =	0.020	acre-feet
5-yr Runoff Volume (P1 = 1.5 in.) =	0.035	acre-feet
10-yr Runoff Volume (P1 = 1.75 in.) =	0.048	acre-feet
25-yr Runoff Volume (P1 = 2 in.) =	0.069	acre-feet
50-yr Runoff Volume (P1 = 2.25 in.) =	0.085	acre-feet
100-yr Runoff Volume (P1 = 2.52 in.) =	0.106	acre-feet
500-yr Runoff Volume (P1 = 3.14 in.) =	0.146	acre-feet
Approximate 2-yr Detention Volume =	0.014	acre-feet
Approximate 5-yr Detention Volume =	0.020	acre-feet
Approximate 10-yr Detention Volume =	0.031	acre-feet
Approximate 25-yr Detention Volume =	0.037	acre-feet
Approximate 50-yr Detention Volume =	0.039	acre-feet
Approximate 100-yr Detention Volume =	0.046	acre-feet

Optional User Overrides

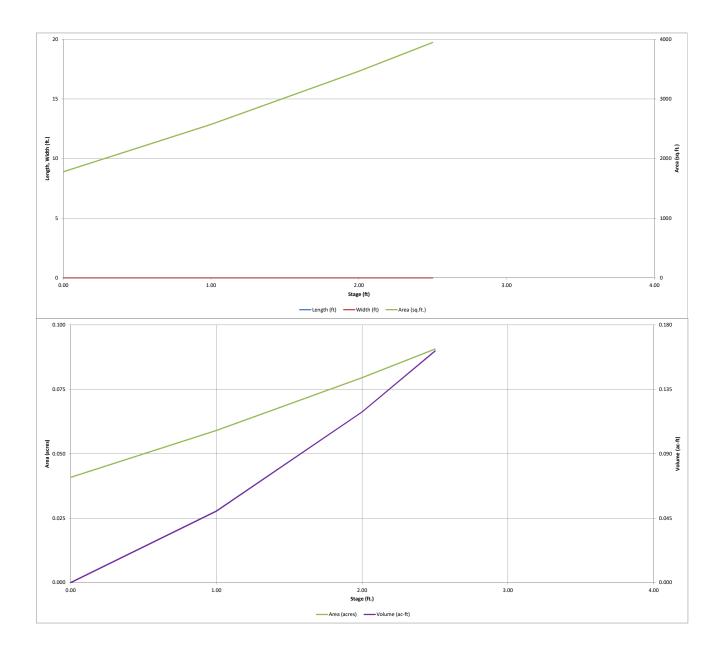
Optional osci	Overrides
	acre-feet
	acre-feet
1.19	inches
1.50	inches
1.75	inches
2.00	inches
2.25	inches
2.52	inches
	inches

Define Zones and Basin Geometry

acre-feet	0.007	Zone 1 Volume (WQCV) =
acre-feet	0.013	Zone 2 Volume (EURV - Zone 1) =
acre-feet	0.027	Zone 3 Volume (100-year - Zones 1 & 2) =
acre-feet	0.046	Total Detention Basin Volume =
ft ³	N/A	Initial Surcharge Volume (ISV) =
ft	N/A	Initial Surcharge Depth (ISD) =
ft	user	Total Available Detention Depth (Htotal) =
ft	N/A	Depth of Trickle Channel (H_{TC}) =
ft/ft	N/A	Slope of Trickle Channel $(S_{TC}) =$
H:V	user	Slopes of Main Basin Sides (S _{main}) =
	user	Basin Length-to-Width Ratio (R _{L/W}) =

Initial Surcharge Area $(A_{ISV}) =$	user	ft ²
Surcharge Volume Length $(L_{ISV}) =$	user	ft
Surcharge Volume Width $(W_{ISV}) =$	user	ft
Depth of Basin Floor $(H_{FLOOR}) =$	user	ft
Length of Basin Floor $(L_{FLOOR}) =$	user	ft
Width of Basin Floor $(W_{FLOOR}) =$	user	ft
Area of Basin Floor $(A_{FLOOR}) =$	user	ft ²
Volume of Basin Floor $(V_{FLOOR}) =$	user	ft ³
Depth of Main Basin (H _{MAIN}) =	user	ft
Length of Main Basin $(L_{MAIN}) =$	user	ft
Width of Main Basin $(W_{MAIN}) =$	user	ft
Area of Main Basin $(A_{MAIN}) =$	user	ft ²
Volume of Main Basin (V _{MAIN}) =	user	ft ³
Calculated Total Basin Volume (V _{total}) =	user	acre-fe

Double Townson		ft							
Depth Increment =		Optional				Optional			
Stage - Storage Description	Stage (ft)	Override Stage (ft)	Length (ft)	Width (ft)	Area (ft 2)	Override Area (ft ²)	Area (acre)	Volume (ft ³)	Volume (ac-ft)
Media Surface		0.00				1,780	0.041	, , ,	(30.0)
7088.5		1.00				2,572	0.059	2,176	0.050
7089.5	1	2.00	1	1	1	3,463	0.079	5,193	0.119
7090	-	2.50	-		-	3,947	0.091	7,046	0.162
	-		-		-				
	-		-		-				
	-		-		-				
	-		-	-	1				
					-				
	-		-		-				
	-		-		-				
	-		-		-				
	-		-	-	1				
	-		-						
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DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.04 (February 2021)

Project: Homestead at Sterling Ranch Filing No. 2 Rasin ID: Sand Filter - Basin X1

	240111 221 24114 1 11461 240111 7/12
100-YR EURY WOCY PERMANENT POOL	ZONE 3 ZONE 2 ZONE 1 ZONE 1 AND 2 ORIFICES ORIFICE
POOL	Example Zone Configuration (Retention Pond)

	Estimated	Estimated	
	Stage (ft)	Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	0.17	0.007	Filtration Media
Zone 2 (EURV)	0.44	0.013	Rectangular Orifice
Zone 3 (100-year)	0.94	0.027	Weir&Pipe (Restrict)
•	Total (all zones)	0.046	

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth = ft (distance below the filtration media surface) 2.10 Underdrain Orifice Diameter = 0.42

Calculated Parameters for Underdrain Underdrain Orifice Area 0.0 Underdrain Orifice Centroid = 0.02

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP) ft (relative to basin bottom at Stage = 0 ft) Invert of Lowest Orifice = N/A

Depth at top of Zone using Orifice Plate = N/A ft (relative to basin bottom at Stage = 0 ft) Orifice Plate: Orifice Vertical Spacing = N/A inches Orifice Plate: Orifice Area per Row = N/A

Calculated Parameters for Plate WQ Orifice Area per Row = N/A Elliptical Half-Width = N/A feet Elliptical Slot Centroid = N/A feet Elliptical Slot Area = N/A

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

Row 1 (optional) Row 2 (optional) Row 3 (optional) Row 4 (optional) Row 5 (optional) Row 6 (optional) Row 7 (optional) Row 8 (optional) Stage of Orifice Centroid (ft) N/A N/A N/A N/A N/A N/A N/A N/A Orifice Area (sq. inches) N/A N/A N/A N/A N/A

Row 9 (optional) Row 10 (optional) Row 11 (optional) Row 12 (optional) Row 13 (optional) Row 14 (optional) Row 15 (optional) Row 16 (optional) Stage of Orifice Centroid (ft) N/A Orifice Area (sq. inches) N/A N/A N/A N/A

User Input: Vertical Orifice (Circular or Rectangular)

Calculated Parameters for Vertical Orifice Zone 2 Rectangula Not Selected Zone 2 Rectangula Not Selected Invert of Vertical Orifice = 0.35 N/A ft (relative to basin bottom at Stage = 0 ft) Vertical Orifice Area = 0.06 N/A 0.44 Depth at top of Zone using Vertical Orifice = N/A ft (relative to basin bottom at Stage = 0 ft) Vertical Orifice Centroid = 0.08 N/A Vertical Orifice Height = 2.00 N/A Vertical Orifice Width = 4.00 inches

User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe) Zone 3 Weir Not Selected

Overflow Weir Front Edge Height, Ho 0.75 N/A Overflow Weir Front Edge Length = 2.21 N/A Overflow Weir Grate Slope = H:V 0.00 N/A Horiz. Length of Weir Sides = 2.21 N/A feet Overflow Grate Type : N/A Type C Grate Debris Clogging % = 50% N/A

Height of Grate Upper Edge, H. ft (relative to basin bottom at Stage = 0 ft) Overflow Weir Slope Length Grate Open Area / 100-yr Orifice Area Overflow Grate Open Area w/o Debris Overflow Grate Open Area w/ Debris

	Calculated Paramet	ters for Overflow V	Veir
	Zone 3 Weir	Not Selected	
=	0.75	N/A	fee
=	2.21	N/A	fee
=	42.55	N/A	
=	3.40	N/A	ft ²
=	1.70	N/A	ft²

feet

feet

acres

acre-ft

feet

radians

500 Year

3 14

0.146

0.146

1.0

1.30

1.2

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

Zone 3 Restrictor Not Selected Depth to Invert of Outlet Pipe N/A 2.10 ft (distance below basin bottom at Stage = 0 ft) Outlet Pipe Diameter 12.00 N/A inches Restrictor Plate Height Above Pipe Invert = 1.90 inches

Zone 3 Restrictor Not Selected Outlet Orifice Area 0.08 N/A Outlet Orifice Centroid 0.09 N/A Half-Central Angle of Restrictor Plate on Pipe = N/A 0.82

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage= ft (relative to basin bottom at Stage = 0 ft) 2.50 Spillway Crest Length = 5.00 feet Spillway End Slopes = 4.00 H:V Freeboard above Max Water Surface = eet

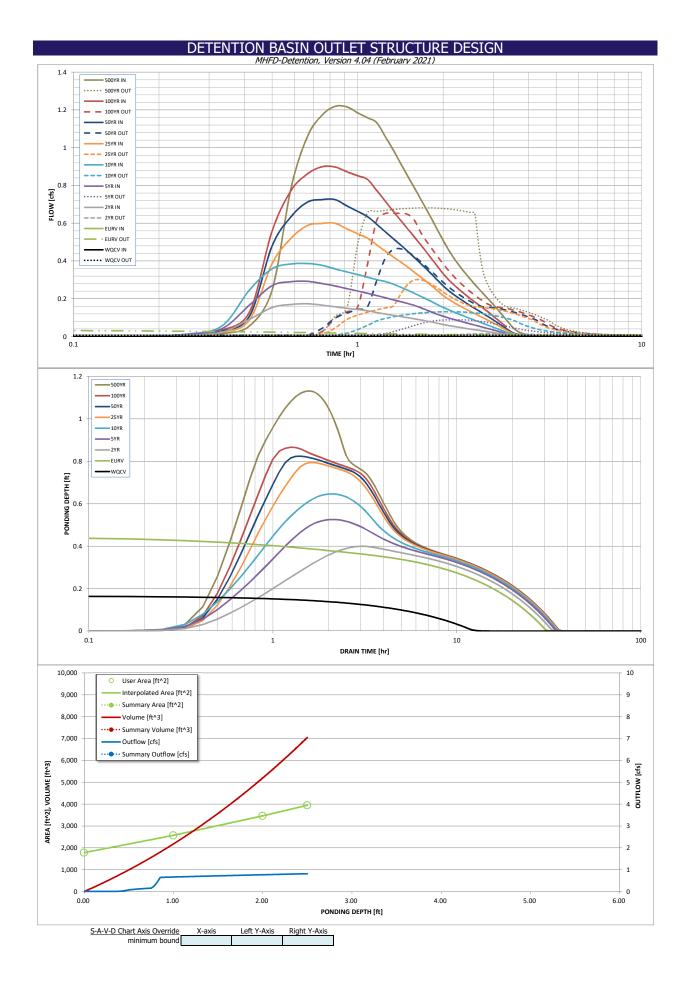
Calculated Parameters for Spillway Spillway Design Flow Depth= 0.14 Stage at Top of Freeboard = 4.14 Basin Area at Top of Freeboard = 0.09 Basin Volume at Top of Freeboard = 0.16

ophs table (Columns W through Al Routed Hydrograph Results aphs and runoff volumes by ring new values in the Inflow Hvdi Design Storm Return Period WQCV **EURV** 2 Year 5 Year 10 Year 25 Year 50 Year 100 Year One-Hour Rainfall Depth (in) N/A N/A 1.19 1 50 2.00 CUHP Runoff Volume (acre-ft) 0.007 0.020 0.020 0.035 0.048 0.069 0.085 0.106 Inflow Hydrograph Volume (acre-ft) N/A N/A 0.020 0.035 0.048 0.069 0.085 0.106 CUHP Predevelopment Peak Q (cfs) N/A N/A 0.2 0.2 0.4 0.7 0.1 0.6 OPTIONAL Override Predevelopment Peak Q (cfs) N/A N/A Predevelopment Unit Peak Flow, q (cfs/acre) N/A N/A 0.07 0.20 0.31 0.58 0.72 0.93 N/A Peak Inflow O (cfs) N/A 0.3 0.4 0.6 0.7 0.9 0.2 Peak Outflow Q (cfs) Ratio Peak Outflow to Predevelopment Q

Structure Controlling Flow Max Velocity through Grate 1 (fps) Max Velocity through Grate 2 (fps) Time to Drain 97% of Inflow Volume (hours) Time to Drain 99% of Inflow Volume (hours) Maximum Ponding Depth (ft)

Area at Maximum Ponding Depth (acres)

o Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	0.6	0.5	0.7	0.8	0.9	0.7
Structure Controlling Flow =	Filtration Media	Vertical Orifice 1	Vertical Orifice 1	Vertical Orifice 1	Vertical Orifice 1	Overflow Weir 1	Overflow Weir 1	Outlet Plate 1	Outlet Plate 1
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	N/A	N/A	0.0	0.1	0.1	0.1
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Drain 97% of Inflow Volume (hours) =	12	30	32	33	33	32	31	30	28
Drain 99% of Inflow Volume (hours) =	13	31	33	34	34	35	34	34	34
Maximum Ponding Depth (ft) =	0.17	0.45	0.40	0.53	0.65	0.79	0.82	0.87	1.13
a at Maximum Ponding Depth (acres) =	0.04	0.05	0.05	0.05	0.05	0.06	0.06	0.06	0.06
Maximum Volume Stored (acre-ft) =	0.007	0.020	0.017	0.024	0.030	0.038	0.040	0.042	0.058



DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename:

Inflow Hydrographs

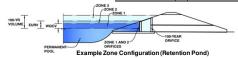
The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

İ								in a separate pro		CHILD
	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:15:00	0.00	0.00	0.01	0.01	0.01	0.01	0.01	0.01	0.02
	0:20:00	0.00	0.00	0.02	0.04	0.06	0.02	0.03	0.03	0.06
	0:25:00 0:30:00	0.00	0.00	0.09	0.17	0.25	0.09	0.11	0.13	0.25
	0:35:00	0.00	0.00	0.15 0.17	0.27 0.29	0.36 0.38	0.39 0.52	0.48	0.56 0.77	0.79 1.06
	0:40:00	0.00	0.00	0.17	0.29	0.39	0.59	0.03	0.77	1.17
	0:45:00	0.00	0.00	0.17	0.28	0.38	0.60	0.73	0.90	1.22
	0:50:00	0.00	0.00	0.16	0.27	0.36	0.60	0.73	0.90	1.22
	0:55:00	0.00	0.00	0.15	0.25	0.34	0.57	0.69	0.87	1.18
	1:00:00	0.00	0.00	0.14	0.24	0.33	0.54	0.66	0.85	1.16
	1:05:00	0.00	0.00	0.14	0.23	0.31	0.52	0.64	0.83	1.13
	1:10:00	0.00	0.00	0.13	0.22	0.30	0.49	0.59	0.77	1.06
	1:15:00	0.00	0.00	0.12	0.21	0.29	0.45	0.56	0.72	0.99
	1:20:00	0.00	0.00	0.11	0.20	0.28	0.42	0.52	0.66	0.92
	1:25:00	0.00	0.00	0.11	0.18	0.26	0.39	0.49	0.62	0.85
	1:30:00 1:35:00	0.00	0.00	0.10	0.17 0.16	0.25 0.23	0.37 0.34	0.45 0.42	0.57 0.53	0.79 0.73
	1:40:00	0.00	0.00	0.09	0.15	0.23	0.34	0.42	0.53	0.73
	1:45:00	0.00	0.00	0.09	0.13	0.21	0.32	0.39	0.49	0.62
	1:50:00	0.00	0.00	0.08	0.13	0.18	0.26	0.33	0.41	0.56
	1:55:00	0.00	0.00	0.07	0.12	0.17	0.24	0.30	0.37	0.51
	2:00:00	0.00	0.00	0.06	0.11	0.15	0.22	0.27	0.33	0.46
	2:05:00	0.00	0.00	0.06	0.10	0.14	0.20	0.24	0.30	0.42
	2:10:00	0.00	0.00	0.05	0.09	0.13	0.18	0.22	0.28	0.39
	2:15:00	0.00	0.00	0.05	0.08	0.12	0.17	0.21	0.26	0.36
	2:20:00	0.00	0.00	0.05	0.08	0.11	0.16	0.19	0.24	0.33
	2:25:00	0.00	0.00	0.04	0.07	0.10	0.14	0.18	0.22	0.30
	2:30:00	0.00	0.00	0.04	0.07	0.09	0.13	0.16	0.20	0.28
	2:35:00 2:40:00	0.00	0.00	0.04	0.06	0.09	0.12	0.15	0.18	0.25
	2:45:00	0.00	0.00	0.03	0.06	0.08 0.07	0.11 0.10	0.14	0.17 0.15	0.23 0.21
	2:50:00	0.00	0.00	0.03	0.03	0.06	0.10	0.12	0.13	0.19
	2:55:00	0.00	0.00	0.02	0.04	0.06	0.08	0.10	0.12	0.17
	3:00:00	0.00	0.00	0.02	0.03	0.05	0.07	0.09	0.11	0.15
	3:05:00	0.00	0.00	0.02	0.03	0.04	0.06	0.08	0.09	0.13
	3:10:00	0.00	0.00	0.02	0.03	0.04	0.05	0.06	0.08	0.11
	3:15:00	0.00	0.00	0.01	0.02	0.03	0.04	0.05	0.07	0.09
	3:20:00	0.00	0.00	0.01	0.02	0.02	0.03	0.04	0.05	0.07
	3:25:00	0.00	0.00	0.01	0.01	0.02	0.03	0.03	0.04	0.05
	3:30:00	0.00	0.00	0.01	0.01	0.01	0.02	0.02	0.03	0.04
	3:35:00 3:40:00	0.00	0.00	0.00	0.01	0.01	0.01	0.02	0.02	0.03
	3:45:00	0.00	0.00	0.00	0.01	0.01	0.01	0.01	0.01	0.02
	3:50:00	0.00	0.00	0.00	0.00	0.01	0.01	0.01	0.01	0.02
	3:55:00	0.00	0.00	0.00	0.00	0.01	0.00	0.01	0.01	0.01
	4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.01
	4:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:15:00 4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:20:00 4:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:40:00 4:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:05:00 5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:30:00 5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:55:00 6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
l.										

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.04 (February 2021)

Project: <u>Homestead at Sterling Ranch Filing No. 2</u> Basin ID: <u>Sand Filter - Basin Y1, W1, X2</u>



Watershed Information

coronica zinormacion		
Selected BMP Type =	SF	
Watershed Area =	2.74	acres
Watershed Length =	900	ft
Watershed Length to Centroid =	300	ft
Watershed Slope =	0.020	ft/ft
Watershed Imperviousness =	25.00%	percent
Percentage Hydrologic Soil Group A =	0.0%	percent
Percentage Hydrologic Soil Group B =	100.0%	percent
Percentage Hydrologic Soil Groups C/D =	0.0%	percent
Target WQCV Drain Time =	12.0	hours
Location for 1-hr Rainfall Denths =	User Innut	

After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure

the embedded Colorado Urban Hydrograph Procedure.					
Water Quality Capture Volume (WQCV) =	0.025	acre-feet			
Excess Urban Runoff Volume (EURV) =	0.069	acre-feet			
2-yr Runoff Volume (P1 = 1.19 in.) =	0.072	acre-feet			
5-yr Runoff Volume (P1 = 1.5 in.) =	0.123	acre-feet			
10-yr Runoff Volume (P1 = 1.75 in.) =	0.170	acre-feet			
25-yr Runoff Volume (P1 = 2 in.) =	0.245	acre-feet			
50-yr Runoff Volume (P1 = 2.25 in.) =	0.300	acre-feet			
100-yr Runoff Volume (P1 = 2.52 in.) =	0.374	acre-feet			
500-yr Runoff Volume (P1 = 3.14 in.) =	0.516	acre-feet			
Approximate 2-yr Detention Volume =	0.049	acre-feet			
Approximate 5-yr Detention Volume =	0.071	acre-feet			
Approximate 10-yr Detention Volume =	0.108	acre-feet			
Approximate 25-yr Detention Volume =	0.128	acre-feet			
Approximate 50-yr Detention Volume =	0.135	acre-feet			
Approximate 100-yr Detention Volume =	0.163	acre-feet			
		ē'			

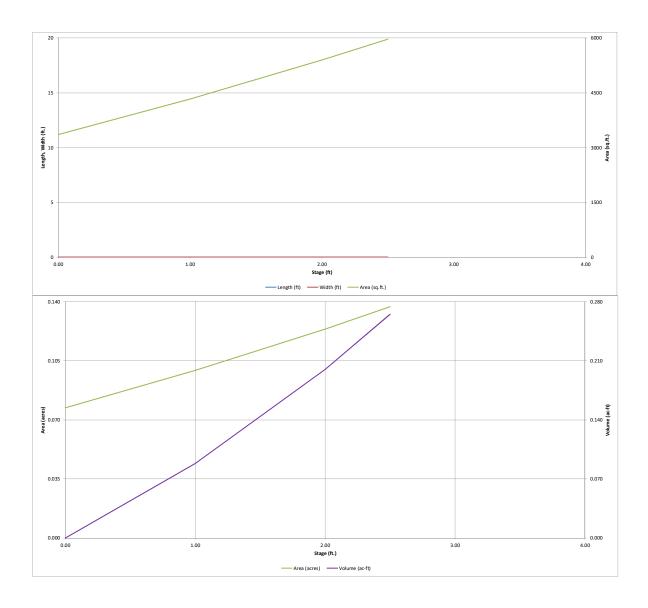
Optional User Overrides					
	acre-feet				
	acre-feet				
1.19	inches				
1.50	inches				
1.75	inches				
2.00	inches				
2.25	inches				
2.52	inches				
	inches				

Define Zones and Basin Geometry

erine Zones and Basin Geometry		
Zone 1 Volume (WQCV) =	0.025	acre-f
Zone 2 Volume (EURV - Zone 1) =	0.045	acre-f
Zone 3 Volume (100-year - Zones 1 & 2) =	0.094	acre-f
Total Detention Basin Volume =	0.163	acre-f
Initial Surcharge Volume (ISV) =	N/A	ft ³
Initial Surcharge Depth (ISD) =	N/A	ft
Total Available Detention Depth (H _{total}) =	user	ft
Depth of Trickle Channel $(H_{TC}) =$	N/A	ft
Slope of Trickle Channel $(S_{TC}) =$	N/A	ft/ft
Slopes of Main Basin Sides (Smain) =	user	H:V
Basin Length-to-Width Ratio (R _{L/W}) =	user	1

Initial Surcharge Area $(A_{ISV}) =$	user	ft ²
Surcharge Volume Length $(L_{ISV}) =$	user	ft
Surcharge Volume Width $(W_{ISV}) =$	user	ft
Depth of Basin Floor $(H_{FLOOR}) =$	user	ft
Length of Basin Floor (L_{FLOOR}) =	user	ft
Width of Basin Floor $(W_{FLOOR}) =$		ft
Area of Basin Floor $(A_{FLOOR}) =$		ft ²
Volume of Basin Floor $(V_{FLOOR}) =$	user	ft ³
Depth of Main Basin (H _{MAIN}) =	user	ft
Length of Main Basin $(L_{MAIN}) =$	user	ft
Width of Main Basin $(W_{MAIN}) =$	user	ft
Area of Main Basin (A _{MAIN}) =		ft ²
Volume of Main Basin (V _{MAIN}) =	user	ft ³
Calculated Total Basin Volume $(V_{total}) =$	user	acre-feet

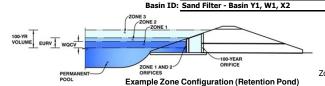
Depth Increment =		ft							
		Optional		145 (1)		Optional		Makama	M. I
Stage - Storage Description	Stage (ft)	Override Stage (ft)	Length (ft)	Width (ft)	Area (ft 2)	Override Area (ft ²)	Area (acre)	Volume (ft 3)	Volume (ac-ft)
Media Surface		0.00				3,358	0.077	()	(GC IL)
7062		1.00	_		-		0.099	3,842	0.088
						4,326			
7063		2.00	-		-	5,395	0.124	8,702	0.200
7063.5		2.50	-		-	5,967	0.137	11,543	0.265
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DETENTION BASIN OUTLET STRUCTURE

MHFD-Detention, Version 4.04 (February 2021)

Project: Homestead at Sterling Ranch Filing No. 2



	Estimated	Estimated	
	Stage (ft)	Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	0.31	0.025	Filtration Media
Zone 2 (EURV)	0.81	0.045	Rectangular Orifice
one 3 (100-year)	1.70	0.094	Weir&Pipe (Restrict)
•	Total (all zones)	0.163	

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

ft (distance below the filtration media surface) Underdrain Orifice Invert Depth = 2.10 Underdrain Orifice Diameter = 0.80 inches

<u> </u>	Calculated Paramet	ters for Underdrain
Underdrain Orifice Area =	0.0	ft ²
Underdrain Orifice Centroid =	0.03	feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice = N/A ft (relative to basin bottom at Stage = 0 ft) Depth at top of Zone using Orifice Plate = N/A ft (relative to basin bottom at Stage = 0 ft) Orifice Plate: Orifice Vertical Spacing = N/A inches Orifice Plate: Orifice Area per Row = N/A inches

<u>IP)</u>	Calculated Paramet	ters for Plate
Q Orifice Area per Row =	N/A	ft ²
Elliptical Half-Width =		feet
Elliptical Slot Centroid =	N/A	feet
Elliptical Slot Area =	N/A	ft ²

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (optional)	Row 2 (optional)	Row 3 (optional)	onal) Row 4 (optional) Row 5 (optio		Row 6 (optional)	Row 7 (optional)	nal) Row 8 (optional)	
Stage of Orifice Centroid (ft)	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	
Orifice Area (sq. inches)	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	

	Row 9 (optional)	Row 10 (optional) Row 11 (optional) Row 12 (optional)		Row 13 (optional) Row 14 (optional)		Row 15 (optional)	Row 16 (optional)	
Stage of Orifice Centroid (ft)	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Orifice Area (sq. inches)	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A

User Input: Vertical Orifice (Circular or Rectangular)

Zone 2 Rectangula Not Selected Invert of Vertical Orifice : N/A ft (relative to basin bottom at Stage = 0 ft) 0.33 Depth at top of Zone using Vertical Orifice = N/A ft (relative to basin bottom at Stage = 0 ft) 0.81 Vertical Orifice Height = 2.00 N/A inches Vertical Orifice Width = 4.00

	Calculated Paramet	ers for Vertical Orif	<u>îce</u>
	Zone 2 Rectangular	Not Selected	
Vertical Orifice Area =	0.06	N/A	ft ²
Vertical Orifice Centroid =	0.08	N/A	feet

User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe)

input: ordinor tres (bropber marriage)	Diopea Grace and	outlet i ipe on nee	tangalar, mapezolaar men (ana no oatiet npe)
	Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	1.00	N/A	ft (relative to basin bottom at Stage = 0 ft) Height of Grate Upper Edge, H_t
Overflow Weir Front Edge Length =	2.21	N/A	feet Overflow Weir Slope Length
Overflow Weir Grate Slope =	0.00	N/A	H:V Grate Open Area / 100-yr Orifice Area
Horiz. Length of Weir Sides =	2.21	N/A	feet Overflow Grate Open Area w/o Debris
Overflow Grate Type =	Type C Grate	N/A	Overflow Grate Open Area w/ Debris
Debris Clogging % =	50%	N/A	%

	Calculated Parameters for Overflow We						
	Zone 3 Weir	Not Selected					
$H_t =$	1.00	N/A	feet				
th =	2.21	N/A	feet				
ea =	10.98	N/A					
is =	3.40	N/A	ft ²				
is =	1.70	N/A	ft ²				

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

	Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	2.10	N/A	ft (dista
Outlet Pipe Diameter =	15.00	N/A	inches
Restrictor Plate Height Above Pipe Invert =	4.50		inches

ft (distance below basin bottom at Stage = 0 ft) inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate Outlet Orifice Area Outlet Orifice Centroid Half-Central Angle of Restrictor Plate on Pipe

	Zone 3 Restrictor	Not Selected	
=	0.31	N/A	ft ²
=	0.22	N/A	feet
=	1.16	N/A	radians
	`		

User Input: Emergency Spillway (Rectangular or Trapezoidal)

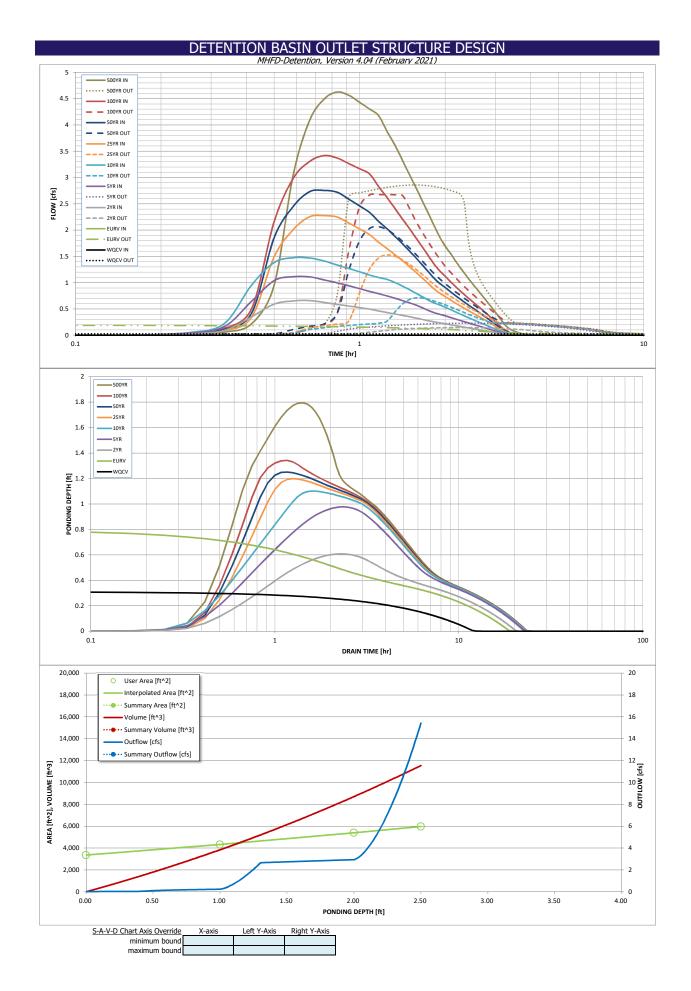
ft (relative to basin bottom at Stage = 0 ft) Spillway Invert Stage= 2.00 Spillway Crest Length = 10.00 feet Spillway End Slopes = H:V 4.00 Freeboard above Max Water Surface = 1.50 feet

Calculated Parameters for Spillway Spillway Design Flow Depth= 0.22 feet Stage at Top of Freeboard = feet 3.72 Basin Area at Top of Freeboard = 0.14 acres Basin Volume at Top of Freeboard = 0.26 acre-ft

Routed Hydrograph Results Design Storm Return Perio One-Hour Rainfall Depth (in CUHP Runoff Volume (acre-fi Inflow Hydrograph Volume (acre-fi CUHP Predevelopment Peak Q (cf: OPTIONAL Override Predevelopment Peak Q (cfs Predevelopment Unit Peak Flow, q (cfs/acre Peak Inflow Q (cf

Peak Outflow Q (cfs Ratio Peak Outflow to Predevelopment Structure Controlling Flow Max Velocity through Grate 1 (fps Max Velocity through Grate 2 (fp. Time to Drain 97% of Inflow Volume (hours Time to Drain 99% of Inflow Volume (hour Maximum Ponding Depth (f Area at Maximum Ponding Depth (acres

ograph Results	The user can overr	ide the default CUF	HP hydrographs and	runoff volumes by	entering new value	s in the Inflow Hyd	rographs table (Col	lumns W through A	F).
Design Storm Return Period =	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
One-Hour Rainfall Depth (in) =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52	3.14
CUHP Runoff Volume (acre-ft) =	0.025	0.069	0.072	0.123	0.170	0.245	0.300	0.374	0.516
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	0.072	0.123	0.170	0.245	0.300	0.374	0.516
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A	0.2	0.6	0.9	1.7	2.1	2.7	3.8
verride Predevelopment Peak Q (cfs) =	N/A	N/A							
lopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.08	0.22	0.34	0.62	0.78	1.00	1.40
Peak Inflow Q (cfs) =	N/A	N/A	0.7	1.1	1.5	2.3	2.8	3.4	4.6
Peak Outflow Q (cfs) =	0.0	0.2	0.1	0.2	0.7	1.5	2.1	2.7	2.9
o Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	0.4	0.8	0.9	1.0	1.0	0.7
Structure Controlling Flow =	Filtration Media	Vertical Orifice 1	Vertical Orifice 1	Vertical Orifice 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Outlet Plate 1	Outlet Plate 1
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	N/A	0.1	0.4	0.5	0.7	0.7
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Drain 97% of Inflow Volume (hours) =	12	18	20	21	21	20	19	18	16
Drain 99% of Inflow Volume (hours) =	12	19	20	22	22	22	22	22	21
Maximum Ponding Depth (ft) =	0.32	0.81	0.61	0.98	1.10	1.20	1.25	1.34	1.80
a at Maximum Ponding Depth (acres) =	0.08	0.10	0.09	0.10	0.10	0.10	0.11	0.11	0.12
Maximum Volume Stored (acre-ft) =	0.026	0.070	0.050	0.085	0.098	0.108	0.114	0.123	0.174



DETENTION BASIN OUTLET STRUCTURE DESIGN

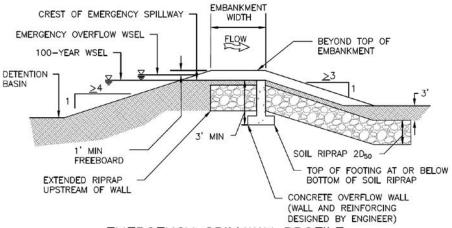
Outflow Hydrograph Workbook Filename:

Inflow Hydrographs

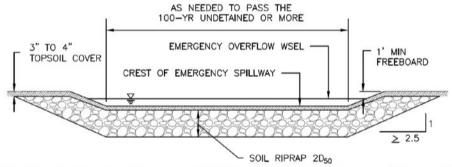
The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]		25 Year [cfs]	50 Year [cfs]		500 Year [cfs]
	0:00:00									
5.00 min	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.01
	0:20:00	0.00	0.00	0.02	0.16	0.03	0.03	0.04	0.04	0.06
	0:25:00	0.00	0.00	0.35	0.65	0.95	0.34	0.42	0.50	0.95
	0:30:00	0.00	0.00	0.59	1.04	1.38	1.49	1.85	2.16	3.04
	0:35:00	0.00	0.00	0.65	1.11	1.47	2.01	2.45	2.98	4.09
	0:40:00	0.00	0.00	0.66	1.11	1.47	2.25	2.73	3.30	4.49
	0:45:00	0.00	0.00	0.62	1.05	1.41	2.28	2.75	3.42	4.63
	0:50:00	0.00	0.00	0.59	1.00	1.33	2.25	2.72	3.37	4.56
	0:55:00	0.00	0.00	0.55	0.94	1.27	2.13	2.59	3.26	4.43
	1:00:00 1:05:00	0.00	0.00	0.53	0.89	1.21	2.02	2.46	3.17 3.07	4.30
	1:10:00	0.00	0.00	0.50 0.46	0.83 0.79	1.15 1.10	1.91 1.77	2.34	2.83	4.18 3.87
	1:15:00	0.00	0.00	0.43	0.75	1.06	1.65	2.02	2.62	3.61
	1:20:00	0.00	0.00	0.40	0.70	1.00	1.53	1.88	2.41	3.32
	1:25:00	0.00	0.00	0.38	0.66	0.93	1.42	1.74	2.21	3.05
	1:30:00	0.00	0.00	0.35	0.62	0.86	1.30	1.60	2.02	2.79
	1:35:00	0.00	0.00	0.33	0.57	0.80	1.19	1.46	1.84	2.54
	1:40:00	0.00	0.00	0.30	0.52	0.73	1.08	1.33	1.67	2.30
	1:45:00	0.00	0.00	0.27	0.47	0.66	0.98	1.20	1.50	2.07
	1:50:00	0.00	0.00	0.25	0.43	0.61	0.88	1.08	1.34	1.86
	1:55:00 2:00:00	0.00	0.00	0.23 0.22	0.40	0.57 0.54	0.80	0.98 0.91	1.22	1.70 1.56
	2:05:00	0.00	0.00	0.22	0.34	0.49	0.67	0.91	1.12	1.43
	2:10:00	0.00	0.00	0.18	0.31	0.45	0.62	0.76	0.94	1.30
	2:15:00	0.00	0.00	0.17	0.28	0.41	0.56	0.70	0.85	1.19
	2:20:00	0.00	0.00	0.15	0.26	0.37	0.51	0.63	0.78	1.08
	2:25:00	0.00	0.00	0.14	0.23	0.33	0.47	0.58	0.70	0.98
	2:30:00	0.00	0.00	0.13	0.21	0.30	0.42	0.52	0.64	0.88
	2:35:00	0.00	0.00	0.11	0.19	0.27	0.38	0.47	0.57	0.79
	2:40:00	0.00	0.00	0.10	0.16	0.24	0.34	0.41	0.51	0.70
	2:45:00 2:50:00	0.00	0.00	0.09	0.14 0.12	0.21 0.18	0.30 0.25	0.36 0.31	0.45	0.62 0.53
	2:55:00	0.00	0.00	0.07	0.12	0.15	0.23	0.31	0.32	0.55
	3:00:00	0.00	0.00	0.05	0.08	0.12	0.17	0.21	0.26	0.36
	3:05:00	0.00	0.00	0.04	0.06	0.09	0.13	0.16	0.20	0.27
	3:10:00	0.00	0.00	0.03	0.05	0.07	0.10	0.12	0.15	0.20
	3:15:00	0.00	0.00	0.02	0.03	0.05	0.07	0.08	0.10	0.14
	3:20:00	0.00	0.00	0.02	0.03	0.04	0.05	0.06	0.07	0.10
	3:25:00	0.00	0.00	0.01	0.02	0.04	0.04	0.05	0.05	0.08
	3:30:00	0.00	0.00	0.01	0.02	0.03	0.03	0.04	0.04	0.06
	3:35:00 3:40:00	0.00	0.00	0.01	0.02	0.03	0.02	0.03	0.03 0.02	0.04
	3:45:00	0.00	0.00	0.01	0.01	0.02	0.02	0.02	0.02	0.03
	3:50:00	0.00	0.00	0.01	0.01	0.01	0.01	0.01	0.01	0.02
	3:55:00	0.00	0.00	0.00	0.01	0.01	0.01	0.01	0.01	0.01
	4:00:00	0.00	0.00	0.00	0.01	0.01	0.01	0.01	0.01	0.01
	4:05:00	0.00	0.00	0.00	0.00	0.01	0.01	0.01	0.01	0.01
	4:10:00 4:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.01
	4:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:35:00 4:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:55:00 5:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:15:00 5:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:40:00 5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Chapter 12 Storage



EMERGENCY SPILLWAY PROFILE



EMERGENCY SPILLWAY SECTION AND SPILLWAY CHANNEL

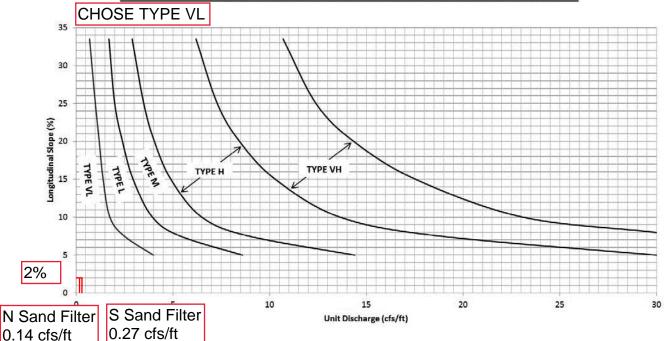
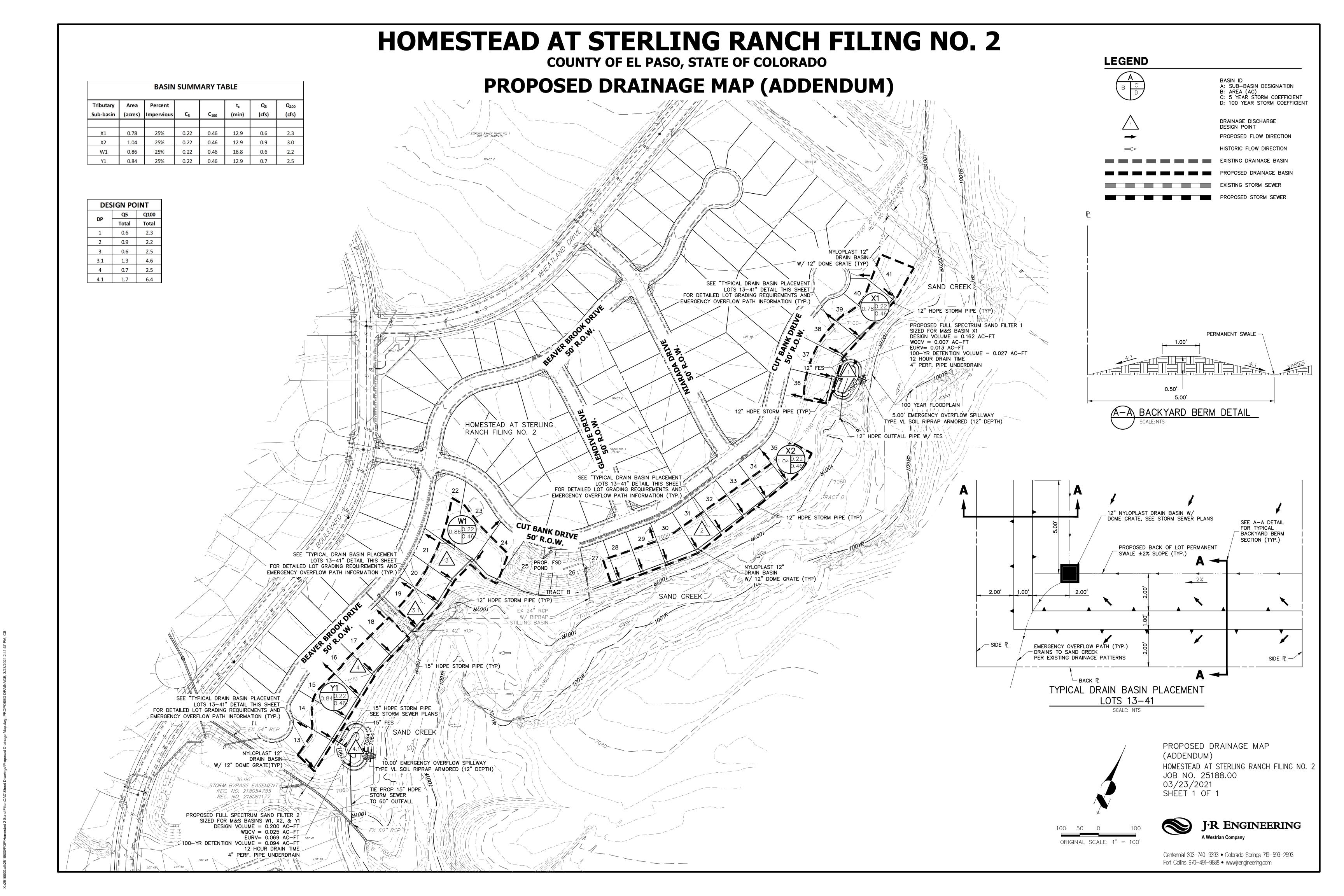


Figure 12-21. Embankment protection details and rock sizing chart (adapted from Arapahoe County)



FINAL DRAINAGE REPORT FOR HOMESTEAD AT STERLING RANCH FILING NO.2

EL PASO COUNTY, COLORADO

March 2020

Prepared for: SR Land, LLC 20 Boulder Crescent, Suite 210 Colorado Springs, CO 80903

Prepared by:



102 E. Pikes Peak, Suite 500 Colorado Springs, CO 80903 (719) 955-5485

> Project #09-007 SF-19-004

FINAL DRAINAGE REPORT FOR HOMESTEAD AT STERLING RANCH FILING NO. 2

DRAINAGE PLAN STATEMENTS

ENGINEERS STATEMENT

The attached drainage plan and report was prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the County for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.

	3/160	
Virgil A. Sanchez, P.E. #37160 For and on Behalf of M&S Civil Consultants, Inc	THE SONAL ENGINEERING	ī

DEVELOPER'S STATEMENT

I, the developer have read and will comply with all the requirements specified in this drain age report and plan.

BY: Jams May	
James F Morley	
TITLE: Manager	
DATE: 3-31-12020	

ADDRESS: SR Land, LLC

20 Boulder Crescent, Suite 210 ColoradoSprings, CO80903

EL PASO COUNTY'S STATEMENT

Filedinaccordancewith the requirements of El Paso County Land Development Code, Drainage Criteria Manual Volumes 1 and 2, and the Engineering Criteria Manual, as amended.

BY:	DATE:	
Jennifer Irvine, P.E.		
County Engineer / ECM A	dministrator	

FINAL DRAINAGE REPORT FOR HOMESTEAD AT STERLING RANCH FILING NO. 2

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APPENDIX

VicinityMap
SoilsMap
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HydrologicCalculations
HydraulicCalculations
DrainageMaps

FINAL DRAINAGE REPORT FOR HOMESTEAD AT STERLING RANCH FILING NO. 2

PURPOSE

Additional language added in Addendum above

This document is the Final Drainage Report for Homestead at Sterling Ranch Filing No. 2. This report was previously discussed, as a preliminary drainage report, in the "Master Development Drainage Report for Sterling Ranch Filing No.1" prepared by MS Civil Consultants, dated April 2017. The purpose of this document is to identify and analyze the on and offsite drainage patterns and to ensure that post development runoff is routed through the site safely and in a manner that satisfies the requirements set forth by the El Paso County Drainage Criteria Manual. The following report is an analysis of the drainage for Homestead at Sterling Ranch Filing No. 2, single family lots, onsite and offsite drainage.

GENERAL LOCATION AND DESCRIPTION

Homestead at Sterling Ranch Filing No. 2 is located in the SE ¼ of the NW ¼, the SW ¼ of the NE ¼, andthe NW ¼ of the NE ¼ of Section 33, Township 12 South, Range 65 West of the 6th Principal Meridian, and the NE ¼ of the SW ¼ of Section 33, Township 12 South, Range 65 West of the 6th Principal Meridianwithin unincorporated El Paso County, Colorado. The site is bound on the south by an existing detention pond, to the north by Briargate Parkway and to the east by Sand Creek. ExistingDines Boulevard runs along the western site boundary. An existing residential development, Homestead at Sterling Ranch Filing No. 1, bounds the site to the west and a future commercial parcel bounds the site to the northwest. Sterling Ranch lies within the Sand Creek Drainage Basin. Flows from this site are tributary to Sand Creek.

Homestead at Sterling Ranch Filing No. 2consists of 29.658 acresand is presently undeveloped. Vegetation is sparse, consisting of native grasses. Existing site terrain generally slopes from north to southwest at grade rates that vary between 2% and 6%.

Land use for Homestead at Sterling Ranch Filing No. 2is currently listed as AG(Grazing Land). Improvements proposed for the site include pavedstreets, trails, a full spectrum detention pond, and utilities as normally constructed for a residential development.

SOILS

Soils for this project are delineated by the map in the appendix as Pring Coarse Sandy Loam (71) and is characterized as Hydrologic Soil Types "B". Soils in the study area are shown as mapped by S.C.S. in the "Soils Survey of El Paso County Area". Vegetation is sparse, consisting of native grasses and weeds.

HYDROLOGIC CALCULATIONS

Hydrologic calculations were performed using the El Paso County and City of Colorado Springs Storm Drainage Design Criteria manual and where applicable the Urban Storm Drainage Criteria Manual. The Rational Method was used to estimate stormwater runoff anticipated from design storms with 5-year and 100-year recurrence intervals.

HYDRAULIC CALCULATIONS

Hydraulic calculations were estimated using the Manning's Formula and the methods described in the El Paso County and City of Colorado Springs Storm Drainage Design Criteria manual. The relevant data sheets can be found in the "Master Development Drainage Report for Sterling Ranch Filing Nos. 1&2, and Final Drainage Report for Sterling Ranch Filing No.1" prepared by MS Civil Consultants, dated April 2017 and in the appendix of this report.

FLOODPLAIN STATEMENT

No portion of this site is within a designated F.E.M.A. floodplain as determined by the Federal Emergency Management Agency (FEMA) Flood Insurance Rate Map (FIRM) Panel No. 08041C0533G, effective date December 7, 2018.An annotated FIRM Panel is included in the Appendix.

DRAINAGE CRITERIA

This drainage analysis has been prepared in accordance with the current City of Colorado Springs/El Paso County Drainage Criteria Manual, Volumes I & II, dated November 1991, including subsequent updates. El Paso County has also adopted Chapter 6 and Section 3.2.1 of Chapter 13 in the City of Colorado Springs & El Paso County Drainage Criteria Manual Volumes I and II, dated May 2014. (Appendix I of the El Paso County's Engineering Criteria Manual (ECM), 2008). In addition to the ECM, the Urban Storm Drainage Criteria Manuals, Volumes 1-3, published by the Urban Drainage and Flood Control District (Volumes 1 & 2 dated January 2016, Volume 3 dated November 2010 and updates. Calculations were performed to determine runoff quantities for the 5-year and 100-year frequency storms for developed conditions using the Rational Method.July 2019 ECM updated for MS4 permit.

FOUR STEP PROCESS

- **Step 1 Employ Runoff Reduction Practices**. Roof drains will be directed to side yard swales and as possible to grass lined swales to aid in minimizing direct connection of impervious surfaces.
- **Step 2 Implement BMPs that provide a water quality capture volume with slow release.** An existing Full Spectrum Detention Facility (see Sterling Ranch Filing Nos. 1&2 MDDP, Pond 4)was planned and constructed to handle tributary flows for the southwest portion of the site. All remaining tributary areas from the site will be treated in a proposed temporary Full Spectrum Detention Facility, Interim Pond 1. Both ponds will incorporate water quality capture volumes that are intended to slowly drain in 40 hours and excess urban runoff volumes that are intended to drain within 72 hours.
- **Step 3 Stabilize streams.** With the full spectrum detention facilities in place, the runoff from the proposed residential development will be reduced to predevelopment conditions. The developed discharge from the site is less that existing and therefore is not anticipated to have negative effects on downstream drainageways. Additionally, the Sand Creek Channel will be reinforced with selected areas of rip rap bank protection, vegetative slope stabilization, check structures and drop structures.
- **Step 4** Consider need for Industrial and Commercial BMPs. No industrial or commercial land uses are proposed with this development. The proposed residential development area will implement a Stormwater Management Plan (SWMP) incorporation proper housekeeping procedures. Onsite drainage will be routed through proposed private temporary Full Spectrum Detention Facility (FSD), Interim Pond 1, to minimize introduction of contaminates to the county's public drainage systems.

EXISTING DRAINAGE CONDITIONS

The Homestead at Sterling Ranch Filing No. 2 site consists of 29.658 acres and is situated west of the Sand Creek Watershed. This area was previously studied in the "Sand Creek Drainage Basin Planning Study" (DBPS) prepared by Kiowa Corporation, revised March 1996. More recently the area was studied in the "Master Development Drainage Report for Sterling Ranch Filing Nos. 1&2, and Final Drainage Report for Sterling Ranch Filing No.1" prepared by MS Civil Consultants, dated April 2017 (henceforth referred to as "Sterling Ranch Filing Nos. 1&2 MDDP").

See the Historic conditions map, the Homestead at Sterling Ranch Filing No. 2 site lies within the Basin EX-4 (Q5 = 71 cfs, Q100 = 352 cfs) and is a 330 acre area of land located on the western portion of the site, including the Sand Creek channel. A portion of this basin extends off-site to the northwest of Vollmer Road, and at the time this map was created was undeveloped property. Runoff from the basin generally travels from north to south until it reaches the northern boundary of the site, being conveyed in the Sand Creek channel. Homestead at Sterling Ranch Filing No. 2 and the surrounding areas, with the exception of the existing Barbarick Subdivision; have already been graded during the overlot of the subdivision. Please refer to the Sterling Ranch Filing Nos. 1&2 MDDP by MS Civil Consultants for information on existing conditions and overlot drainage patterns. A copy of the historic and existing conditions map has been provided in the appendix.

PROPOSED DRAINAGE CHARACTERISTICS

General Concept Drainage Discussion

The following is a description of the onsite basins, offsite bypass flows and the overall drainage characteristics for the development of Sterling Ranch Filing No. 2. The development of Sterling Ranch Filing No. 2 consists of residential streets and cul-de-sacs, proposedstorm drainage improvements, and lots located within the filing boundary. The proposed development results in drainage patterns and flow values that the same or less thanthose in the Sterling Ranch Filing Nos. 1&2 MDDP. Surface flow is designated as Design Points (DP). The following DPs and Basins were determined using the Rational Method since this method offers a more conservative approach to drainage. It should be noted that all calculations and drainage basins have been revised to reflect the new criteria updates by the El Paso County/City of Colorado Springs Drainage Criteria Manual. For comparison, the **asterisk** (*) symbol in the detailed drainage discussions below represents each Basin or Design Point as labeled in the Sterling Ranch Filing Nos. 1&2 MDDP. Asterisk symbols on the Proposed Drainage Map in the appendix also represent Basins, Design Points and Pipe Runs as presented in the Sterling Ranch Filing Nos. 1&2 MDDP.

Detailed Drainage Discussion (Design Points)

DP2*, 5.39 acres, consists ofBasin B*planned residential lots and streets with runoff coefficients of 0.38 for the 5-year and 0.55 for the 100-year. Developed runoff of Q5=8.0 cfs and Q100=19.3 cfs has been calculated for DP2*. The surface runoff is routed via overlot grading and planned swales to two existing 15' CDOT Type R at-grade inlets. The flows are routed east via a 36" RCP to DP5.

DP3*, 2.92 acres, consists ofBasin C* residential lots within Homestead at Sterling Ranch Filing No. 1, and streets with runoff coefficients of 0.38 for the 5-year and 0.55 for the 100-year. Developed runoff of Q5=4.2 cfs and Q100=10.1 cfs has been calculated for DP3*. The surface runoff is routed via overlot grading and proposed swales to an existing 5' CDOT type R sump inlet. The flows captured by the inlet are routed to existing Detention Pond 4.

DP4*, 9.36 acres, consists ofBasin D* and Basin E*residential lots within Homestead at Sterling Ranch Filing No. 1 and streets with runoff coefficients of 0.38 for the 5-year and 0.55 for the 100-year and BasinF* (Dines Boulevard) with runoff coefficients of 0.90 for the 5-year and 0.96 for the 100-year. Developed runoff of Q5=16.1 cfs and Q100=36.7 cfs has been calculated for DP4. The surface runoff is routed via overlot grading and curb and gutter to DP4* which will be collected by a 15' CDOT type R atgrade inlet. The intercepted flow (Q5=13.3 cfs and Q100=20.0 cfs) will combine with flows from DP3* and be routed east via a 30" RCP (PR6*, Q5=16.8 cfs and Q100=29.4 cfs) to existing Detention Pond 4.

DP5*,0.80 acres, consists ofBasin G* residential lots with runoff coefficients of 0.22 for the 5-year and 0.46 for the 100-year, Basin H* existing Dines Boulevard, with runoff coefficients of 0.90 for the 5-year and 0.96 for the 100-year and flowby from Sterling Ranch Filing Nos. 1&2 MDDP DP4*. Developed runoff of Q5=4.2 and Q100=19.7cfs has been calculated for DP5*. The surface runoff is routed via overlot grading and curb and gutter to DP5* which is collected by an existing 15' CDOT type R at-grade inlet. DP5* has an intercepted flow of (Q5=4.2cfs and Q100=14.7cfs) and of flowby of (Q5=0.0cfs and Q100=5.0cfs). Flowby from DP5* continues on toPond FSD13, east of Dines Boulevard.See, Sterling Ranch Filing MDDP Proposed Hydrologic Conditions Map.

DP6*, 4.68 acres, consists of Sterling Ranch Filing Nos. 1&2 MDDP Basins J* and K*planned residential lots with runoff coefficients of 0.22 for the 5-year and 0.46 for the 100-year, Sterling Ranch Filing Nos. 1&2 MDDP Basin I* (Wheatland Drive) and Basin L*(Dines Boulevard) with runoff coefficients of 0.90 for the 5-year and 0.96 for the 100-year. Developed runoff of Q5=14.1 cfs and Q100=26.7cfs has been calculated for DP6*. The surface runoff is routed via overlot grading and curb and gutter to DP6* which is collected by an existing 15' CDOT type R at-grade inlet. DP6* has an intercepted flow of (Q5=12.1cfs and Q100=17.2cfs) and of flowby of (Q5=2.0 cfs and Q100=9.5cfs). Flowby from DP6* continues on to Pond FSD13, east of Dines Boulevard. See, Sterling Ranch Filing MDDP Proposed Hydrologic Conditions Map.

DP7,4.42 acres, consists ofBasin Pproposed residential lots with runoff coefficients of 0.38 for the 5-year and 0.55 for the 100-year. Developed runoff of Q5=5.7 and Q100=13.8cfs has been calculated for DP7. Surface runoff is routed via overlot grading and curb and gutter to DP7 which is collected by a proposed 10' CDOT type R sump inlet. Flows captured by the proposed 10' CDOT type R sump inlet are routed to existing Detention Pond 4 by proposed RCP storm sewer. The flows from DP7 were anticipated in the sizing of Pond 4 per the Sterling Ranch Filing No. 1 Final Drainage Report.

DP8,3.78, acres, consists ofBasin Qproposed residential lots with runoff coefficients of 0.38 for the 5-year and 0.55 for the 100-year. Developed runoff of Q5=4.9 and Q100=11.8cfs has been calculated for DP8. Surface runoff is routed via overlot grading and curb and gutter to DP8 which is collected by a proposed 10' CDOT type R sump inlet. Flows captured by the proposed 10' CDOT type R sump inlet are routed to existing Detention Pond 4 by proposed RCP storm sewer. The flows from DP8 were anticipated in the sizing of Pond 4 per the Sterling Ranch Filing No. 1 Final Drainage Report.

DP9, acres, consists ofBasin Rproposed residential lots with runoff coefficients of 0.38 for the 5-year and 0.55 for the 100-year. Developed runoff of Q5=2.2 and Q100=5.4cfs has been calculated for DP9. Surface runoff is routed via overlot grading and curb and gutter to DP9 which is collected by a proposed 5' CDOT type R sump inlet. Flows captured by the proposed 10' CDOT type R sump inletcombine with capturedflows contributed from Design Points 7 & 8 and are routed to existing Detention Pond 4 by Pipe Run 4 (Q5=12.4 and Q100=30.1cfs). Pipe Run 4 connects to existing Sterling Ranch Filing Nos. 1&2 MDDP Pipe Run 10* (Q5=12.5 and Q100=30.4 cfs) and is discharged into the forebay of existing Detention Pond 4. Flows contributed to the forebay of existing Pond 4 are approximately equal to those anticipated by the MDDP, therefore Pond 4 has the capacity for SWQ and Full Spectrum Detention for these flows.

DP10, 9.14, acres, consists ofBasin T proposed residential lots with runoff coefficients of 0.30 for the 5-year and 0.50 for the 100-year. Developed runoff of Q5=9.4 and Q100=15.6cfs has been calculated for

DP10. Surface runoff is routed via overlot grading and curb and gutter to DP10 which is collected by a proposed 15' CDOT type R at-grade inlet. DP10 has an intercepted flow of (Q5=9.1 cfs and Q100=12.7cfs) and of flowby of (Q5=0.3cfs and Q100=2.9cfs). Flows captured by the proposed 15' CDOT type R at-grade inletare routed southwest to the proposed full spectrum detention Pond 1 by proposed RCP storm sewer.

DP11,1.48, acres, consists ofBasin V1proposed residential lots with runoff coefficients of 0.38 for the 5-year and 0.55 for the 100-year. Developed runoff of Q5=1.9 and Q100=15.6 cfs has been calculated for DP11. Surface runoff is routed via overlot grading and curb and gutter to DP11 which is collected by a proposed 15' CDOT type R at-grade inlet. DP11 has an intercepted flow of (Q5=1.9cfs and Q100=12.7cfs) and of flowby of (Q5=0.0cfs and Q100=2.9cfs). Flows captured by the proposed 15' CDOT type R at-grade inlet are routed southwest to the proposed full spectrum detention Pond 1 by proposed RCP storm sewer.

DP12,4.50, acres, consists ofBasin Uproposed residential lots with runoff coefficients of 0.38 for the 5-year and 0.55 for the 100-year and flowby from DP10. Developed runoff of Q5=6.2cfs and Q100=17.2 cfs has been calculated for DP12. Surface runoff is routed via overlot grading and curb and gutter to DP12 which is collected by a proposed 10' CDOT type R sump inlet. Flows captured by the proposed 10' CDOT type R sump inlet are routed to the proposed full spectrum detention Pond 1 by proposed RCP storm sewer.

DP13,0.83, acres, consists ofBasin V2proposed residential lots with runoff coefficients of 0.38 for the 5-year and 0.55 for the 100-year and flowby from DP11. Developed runoff of Q5=1.2 and Q100=5.9cfs has been calculated for DP13. Surface runoff is routed via overlot grading and curb and gutter to DP13 which is collected by a proposed modified 5' length by 4.5' wide CDOT type R sump inlet.

DP14,0.56, acres, consists ofBasin W3proposed full spectrum detention Pond 1with runoff coefficients of 0.08 for the 5-year and 0.35 for the 100-year and contributed flow from pipe run 9. Developed runoff of Q5=19.6cfs and Q100=52.4cfs has been calculated for DP14. All flows captured by inlets at Design Points DP10, DP11, DP12 and DP13 are routed by Pipe Run 9 (PR9, Q5=17.9 and Q100=47.1 cfs) to the forebay inPond 1 and combine withsurface runoff within Basin W1. An outlet structure with an orifice plate and restrictor plate regulates release rates and provides treatment to all flows tributary to DP14. See the Water Quality Provisions discussion in this report for more information on Pond 1.

Basins labeled on the Proposed Drainage Map marked with a "*", were previously analyzed and shown in the Final Drainage report for Sterling Ranch Filing No. 1. These basins are; B*, C*, D*, E*, F*, G*, H*, I*, L*, &S*. They are shown on the Proposed Drainage Map for continuity. Basins K & J additionally contribute to Design Points 3, 4, 5 &6. Therefore, the inlets sizing at these design points has been verified.

Detailed Drainage Discussion (Drainage Basins)

Basins X1, X2,W1, and Y1(0.78, 1.04, 0.86 and 0.084 acres respectively), consists of proposedresidential backyard lotslocated along the eastern boundary of the sitewith runoff coefficients of 0.22for the 5-year and 0.46for the 100-year. Developed runoff of (Q5=0.8, 1.1, 0.2, and 0.8cfs and Q100=2.8, 3.7, 1.7, and 3.0 cfsrespectively has been calculated for the basins. Runoff produced within the residential backyard lots, of Basins X1, X2, W1 and Y1 will be conveyed in backyard swalesand as sheet flow to a Sand Filter Basin within each lot. The treated flows will be collected by private storm sewer systems and discharged into the Sand Creek Channel. A 20' wide typical drainage easement is provided within the lots to accommodate the BMP's. The facilities constructed are to be privately maintained by the Sterling Ranch metro district.

Basins X, W2, and Y (0.22, 0.26, and 0.09 acres respectively), consists primarily of vegetated tracts and portion of residential backyards that will discharge as sheet flow to the Sand Creek Channel. The developed flow rates from Basins X, W2, and Y are Q5=0.2, 0.1, 0.1 cfs andQ100=0.8, 0.8, and 0.3 respectively. The total combined developed area being discharge to the channel is less than one acre. It

is not practicable to provide WQCV for these areas, as stated earlier in this paragraph, areas consists primarily of vegetated tracts with no development.

CHANNEL IMPROVEMENTS

Slope grading and intermittent channel bank lining has been proposed for portions of the developable areas adjacent to Sand Creek to protect the developed lots and prevent excessive erosion until the DBPS recommended Sand Creek Channel improvements are installed. The proposed slope grading is intended to reduce outer bankgrades and bring uniformity to areas where significant riling and destabilization has occurred. Proposed channel stabilization improvements includes placement of soil riprap and turf reinforcement matting along embankment toes and along embankment slopes, both of which will function to retain soils and vegetation during heavy rains or larger flood flow events. All disturbed areas, not hardscaped will be re-vegetated with native species grasses, per El Paso County erosion control standards. Storm sewer outfalls into Sand Creek shall be protected by low-tailwater riprap basins. The outfall protection is shown on the accompanying drainage map in the appendix. Refer to the Homestead Filing No.2 Grading and Erosion Control Plans for riprap and turf reinforcement map placement and construction details.

Permanently installed check structures and rip-rap channel lining will be installed within Sand Creek Channel to handle the runoff from fully developed Sterling Ranch and up-gradient watershed in accordance with the Sand Creek DBPS. A discussion regarding the timing of these channel improvements is provided in a subsequent paragraph titled Sterling Ranch Filing No. 1 Subdivision Improvement agreement which follows the Construction Costs segment of this report. Financial Assurance shall be posted for the proposed Sand Creek Channel Improvements and Bank Stabilization (Slope Protection and grade control structures).

WATER QUALITY PROVISIONS

The proposed Full Spectrum Detention Facility, Pond 1 functions to provide detention storage and water quality facility facility from tributary Basins T, U, V1, V2 and W3. This water quality facility is designed to treat 0.245 ac-ft of water quality storage (WQCV), 0.741 ac-feet of excess urban runoff volume (EURV) and 1.331 ac-ft of 100-year storage. A rolled erosion control blanketed emergency spillway, concrete forebay, trickle channel and outlet structure, and gravel maintenance access road has been designed for Pond 1.

A 24" RCP pipeextending from the proposed modified 6'x2.9' CDOT Type D sump inlet (see Design Point 13) will convey discharge from the pond to Sand Creek. Runoff discharged to Sand Creek is anticipated to reach peak flow rates of Q5=0.7 cfs and Q100=23.4 cfs. A soil riprap stilling basin has been provided at the termination of the pipe to arrest erosion.

Runoff produced within the residential backyard lots, of Basins X1, X2, W1 and Y1 will be conveyed in backyard swales and as sheet flow to a Sand Filter Basin within each lot. The <u>treated</u> flows will be collected by private storm sewer systems and discharged into the Sand Creek Channel. This water quality facility, for each Sand Filter Basin, is designed to treat 0.001 ac-ft of water quality storage (WQCV), 0.005 ac-feet of excess urban runoff volume (EURV) and 0.014 ac-ft of 100-year storage. A 20' wide typical drainage easement is provided within the lots to accommodate the BMP's. The facilities constructed are to be privately maintained by the Sterling Ranch Metropolitan District. Access to maintain these sand filter basins is from the regional trail along sand creek.

The WQCV and EURV required for the site has been determined using the guidelines set forth in the City of Colorado Springs/El Paso County Drainage Criteria Manual - Volume II. Refer to the water quality

facility sizing calculations located within the appendix of this report(see UD-Detention Worksheet in appendix).

As previously discussed, refer to Sterling Ranch Filing Nos. 1&2 MDDP for additional information regarding existing FSD Pond 4. The previously approved FSD Pond was constructed with the Sterling Ranch Filing No. 1 construction drawings in 2018-2019.

EROSION CONTROL

It is the policy of the El Paso County that a grading and erosion control plan be submitted with the drainage report. EPC approved "Early Grading Plan for Sterling Ranch Phase I <u>Onsite</u> Grading & Erosion Control", November 18, 2015. And "Early Grading Plan for Sterling Ranch Phase I <u>Offsite</u> Grading & Erosion Control", December 3, 2015. Grading and Erosion control operations are currently underway (July 2019). Grading and Erosion Control will cease with the final development of the site in the next 6-12 months.

CONSTRUCTION COST OPINION – HOMESTEAD AT STERLING RANCH FIL. NO. 2

Drainage Facilities:

Updated Cost Opinion included in Addendum above

Drainage improvements are planned with the development of Homestead at Sterling Ranch Filing No. 2. A majority of the construction costs have been accounted for in the "Master Development Drainage Report for Sterling Ranch Filing No. 1&2, and Final Drainage Report for Sterling Ranch Filing No.1" prepared by MS Civil Consultants, dated April 2017. Any additional improvements and costs are listed below.

The following list of drainage improvements are **Non-Reimbursable**. The Reimbursable facilities are outlined in the Sterling Ranch Filing No. 1 Final Drainage Report and Sterling Ranch MDDP. Refer to the MDDP for Sterling Ranch Cost and Fee Analysis Report (February 2019).

Item	Description	Quantity	Unit Cost	Cost
1.	18" RCP	31 LF	\$40 /LF	\$1,240.00
2.	24" RCP	127 LF	\$50 /LF	\$6,350.00
3.	30" RCP	998 LF	\$85 /LF	\$84,830.00
4.	36" RCP	8 LF	\$105 /LF	\$840.00
5.	42" RCP	699 LF	\$185 /LF	\$129,315.00
6.—	24" FES	1 EA	\$750 /EA	\$750.00
8.	42" FES	1 EA	\$1,250 /EA	\$1,250.00
9.	5.0'x4.5' CDOT Type R Sump Inlet	1 EA	\$4,000 /EA	\$4,000.00
10.	10' CDOT Type R Sump Inlet	4 EA	\$4,700 /EA	\$18,800.00
11.	15' CDOT Type R At-Grade Inlet	2 EA	\$6,000 /EA	\$12,000.00
12.	4.0' Type II MH	1 EA	\$3,500 /EA	\$3,500.00
13 .	5.0' Type II MH	2 EA	\$4,000 /EA	\$8,000.00
14.	6.0' Type II MH	1 EA	\$4,500 /EA	\$4,500.00
17.	5.0'x6.0' MH	2 EA	\$6,500 /EA	\$13,000.00
18.	5.5'x5.5' MH	1 EA	\$6,500 /EA	\$6,500.00
19.	Headwall/Wingwall	1 EA	\$6,000 /EA	\$6,000.00
20.	Full Spectrum Det. Pond 1	1 EA	\$15,000 /EA	\$15,000.00

21.	FSD Pond 1 Outlet Structure	1	EA	\$12,600	/EA		\$12,600.00
22.	Ind. Lot Sand Filter Basins w/6" Pipe	26	EA	\$2,000	/EA		\$52,000.00
23	18" Drain Basin Manholes w/Lids	27	EA	\$1,000	/EA		27,000.00
24	12" ADS Pipe	1,658		\$26	/LF		43,108.00
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The following list of drainage improvements are **Reimbursable** for the improvements to the Sand Creek Channel adjacent to Homestead at Sterling Ranch Filing No.2. The reimbursement is up to the amount as shown in the DBPS or as adjusted through the City/EPC Drainage Board.

Sand Creek Channel Improvements

Item	Description	Quar	Quantity		ost		Cost
1.	Rip Rap Protection	390	Ton	\$80	/Ton		\$31,200.00
2.	Drop/Check Structures	5	EA	\$75,000	/EA		\$375,000.00
3.	Slope Stabilization Blankets	7,435	SY	\$6	/SY	_	\$44,610.00
						Total	\$450,810.00

DRAINAGE & BRIDGE FEES – HOMESTEAD AT STERLING RANCH FIL. NO. 2

This site is within the Sand Creek Drainage Basin. The 2019 Drainageand BridgeFees per El Paso County for the HOMESTEAD AT STERLING RANCH FILING NO. 2site are as follows:

Per Homesteadat Sterling Ranch Filing No. 2 Plat –					Total Area	29.658 Acres		
HOMESTEAD AT STERLING RANCH FILING NO. 2 FEES:								
Drainage Fees:	29.658	X	46%	\$	18,940.00	=	\$ 258,392.36	
Bridge Fees:	29.658	X	46%	\$	5,559.00	=	\$ 75,839.66	
_							Total \$ 334,232.02	

STERLING RANCH FILING NO. 1 - SUBDIVISION IMPROVEMENTS AGREEEMENT

Sterling Ranch Filing No. 1 final plat and SIA has been recorded, and addressed the following drainage improvements Not located/and located in the Sand Creek Channel. The following SIA paragraphs outlined drainage for Sterling Ranch in the following manner;

2. Drainage and Landscaping Tracts: Improvements on Tracts A, B, F, H, I, J, L, M, N, O, P, Q, R, S, T, U, V, W, X, Y, Z, AA and CC as identified on the final plat of Filing No. 1 will be completed to the satisfaction of the County and District and, upon said completion, the improvements will be dedicated to and accepted by the District. Improvements on Tract D (Sand Creek) will be completed to the satisfaction of the County and upon said completion; the improvements will be dedicated to and accepted by the County. The ownership and maintenance of storm drain facilities and structures not located on the foregoing tracts shall be determined as follows. All storm pipes shall be owned and maintained by the District except where located in County road rights of way (see Paragraph 5 below), in which case the County shall own and maintain the storm drain facilities and structures, including but not limited to, inlets and manholes. A typical cross section describing the ownership and maintenance responsibilities of drainage improvements within County rights of way is attached as Exhibit C hereto.

7. Timing of Construction and Acceptance:

a. **Drainage Improvements Not Located in Sand Creek Channel**: Except as set forth below in subsection 6.b. (drainage improvements located in Sand Creek Channel), all drainage improvements described in <u>Exhibit A</u> and constructed within the Drainage and Landscaping Tracts identified in paragraph 2 above shall be completed by the

Subdivider and District, meeting all applicable standards for preliminary acceptance, prior to the recording of the first replat of Tracts C, E, G, K or BB. In the event that a portion of the drainage improvements are not completed prior to the recording of the first replat, then prior to such recording collaterial sufficient in the opinion of the County to assure completion of the improvements must be posted by the Subdivider and a deadline by which such drainage improvements shall be completed shall be established by written agreement.

- b. **Drainage Improvements Located in Sand Creek Channel (Tract D):** The District agrees that it will construct or cause the construction of all drainage improvements to be located in Tract D as well as future tracts within Sterling Ranch containing the Sand Creek Channel in accordance with the following:
- i. Bank stabilization of the Sand Creek channel shall be required prior to any replats or other final plats adjacent to the channel. The design and installation of said improvements shall be accomplished and guaranteed through the normal subdivision review and collateralization process.
- ii. Other drainage improvements in Tract D and future tracts containing the Sand Creek Channel, such as drop structures, check structures and similar stabilization or protection improvements, will be designed and constructed by the District with the final construction drawings to be approved by the County no later than the final platting of the 700th single family lot within the boundaries of the approved Sterling Ranch Sketch Plan and the completion of all said improvements no later than the 800th single family lot with the boundaries of the approved Sterling Ranch Sketch Plan.
- iii. In order to assure completion of the drainage improvements required in Subsection 6.b.ii above as well as a fair apportionment of the costs of said drainage improvements amongst adjacent Sterling Ranch subdividers, the District agrees to establish a Sand Creek Channel Drainage Fee to be paid into a District Escrow Fund by adjacent subdividers at the time of final platting. The amount of the fee shall be a minimum of One Thousand Dollars (\$1,000.00) per single family lot. The details of the proposed Sand Creek Channel Drainage Fee and the District Escrow Fund shall be agreed to by the parties in advance of the submittal of the first replat of or subdivision of the Master Pad Sites or other property located within Sterling Ranch.

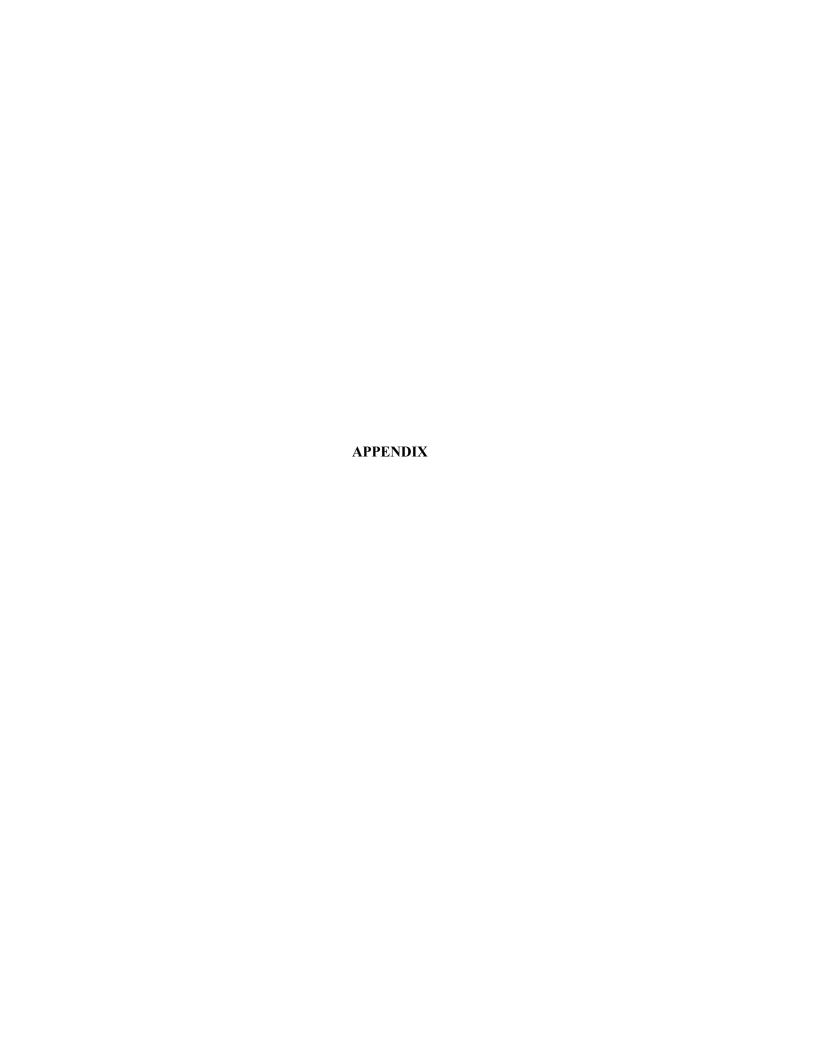
A full copy of the recorded SIA is located in the files of El Paso County and EPC Clerk and Recorders office under Reception No. 218714151

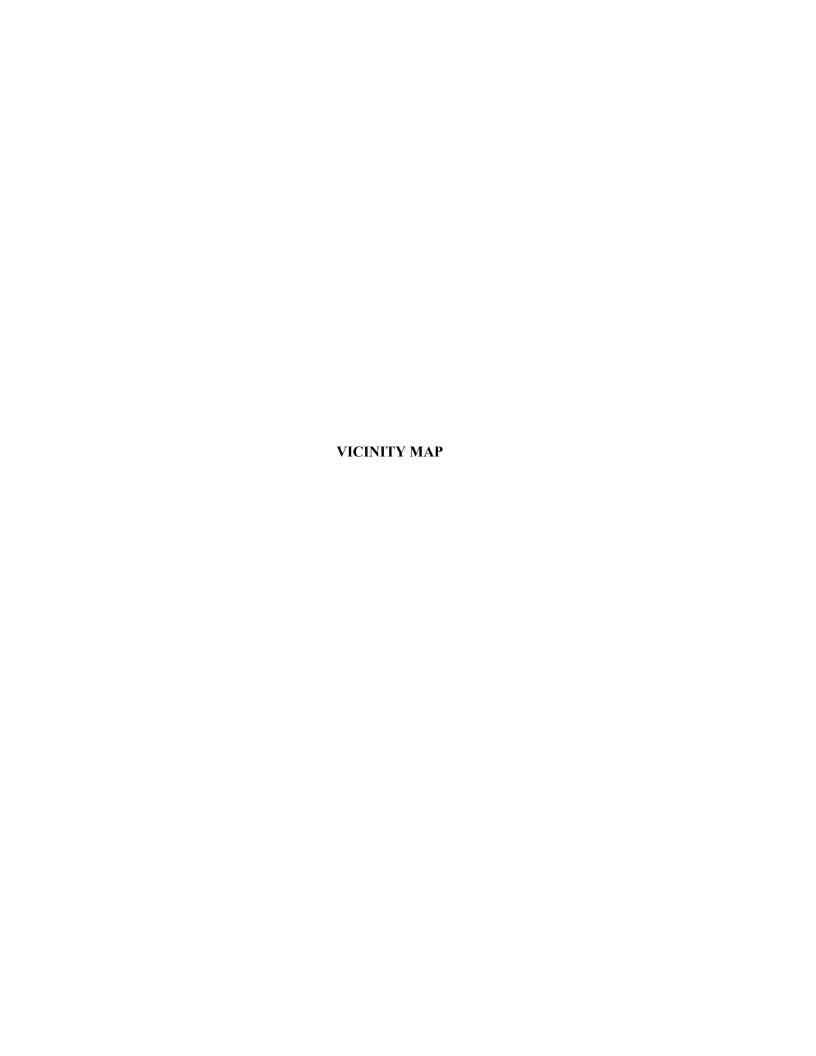
SUMMARY

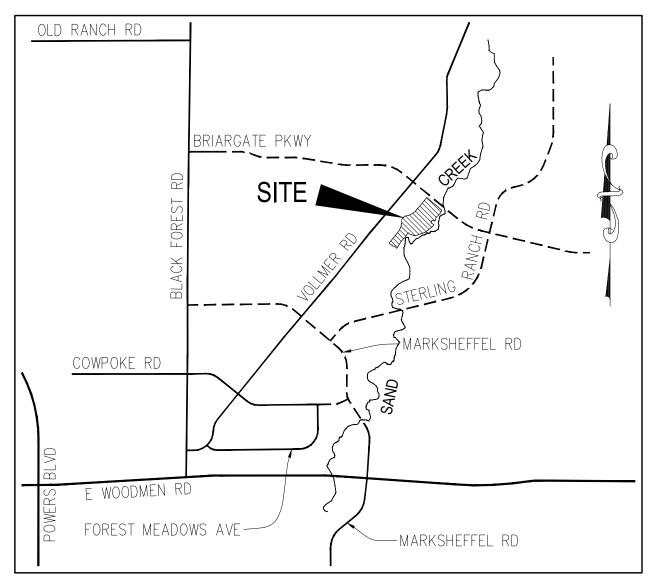
Development of this site will not adversely affect the surrounding development per this final drainage report with no negative impacts to the neighboring developments. The existing and proposed drainage facilities will adequately convey, detain and route runoff from tributary and onsite flows to the Sand Creek Drainage channel. Full Spectrum Detention and Water Quality Ponds will be used to discharge developed flows into Sand Creek per the Urban Drainage criteria flow rates, which are at or less than the historic flow. Care will be taken during construction to accommodate overland flow routes onsite and temporary drainage conditions. The development of the HOMESTEAD AT STERLING RANCH FILING NO. 2project(s)shall not adversely affect adjacent or downstream property.

REFERENCES

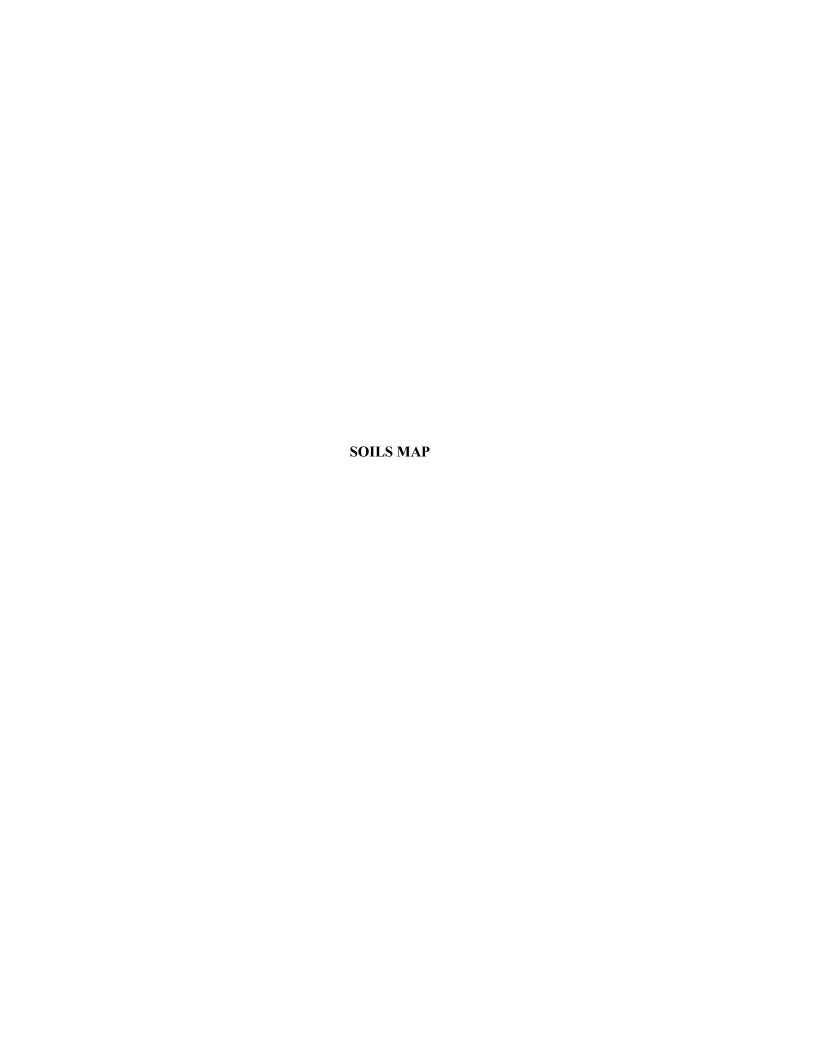
- 1.) "El Paso County and City of Colorado Springs Drainage Criteria Manual, Vol I & II".
- 2.) "Urban Storm Drainage Criteria Manuals, Volumes 1-3"
- 3.) NRSC Web Soil Survey Map for El Paso County. http://websoilsurvey.nrcs.usda.gov
- 4.) Flood Insurance Rate Map (FIRM), Federal Emergency Management Agency, Effective date December 7, 2018.
- 5.) "Sand Creek Drainage Basin Planning Study" (DBPS) prepared by Kiowa Corporation, revised March 1996
- 6.) "Sterling Ranch-Phase 1 Offsite Grading, Early Grading & Erosion Control Plans", prepared by M&S Civil Consultants, Inc., dated November 2015
- 7.) "Sterling Ranch-Phase 1 Onsite Grading, Early Grading & Erosion Control Plans", prepared by M&S Civil Consultants, Inc., dated November 2015
- 8.) "Master Development Drainage Report for Sterling Ranch Filing Nos. 1&2 and Final Drainage Report for Sterling Ranch Filing No. 1", prepared by M&S Civil Consultants, Inc., dated April 2017
- 9.) "Sterling Ranch Filing Nos. 1&2 MDDP" prepared by MS Civil Consultants, Inc., dated October 2018.

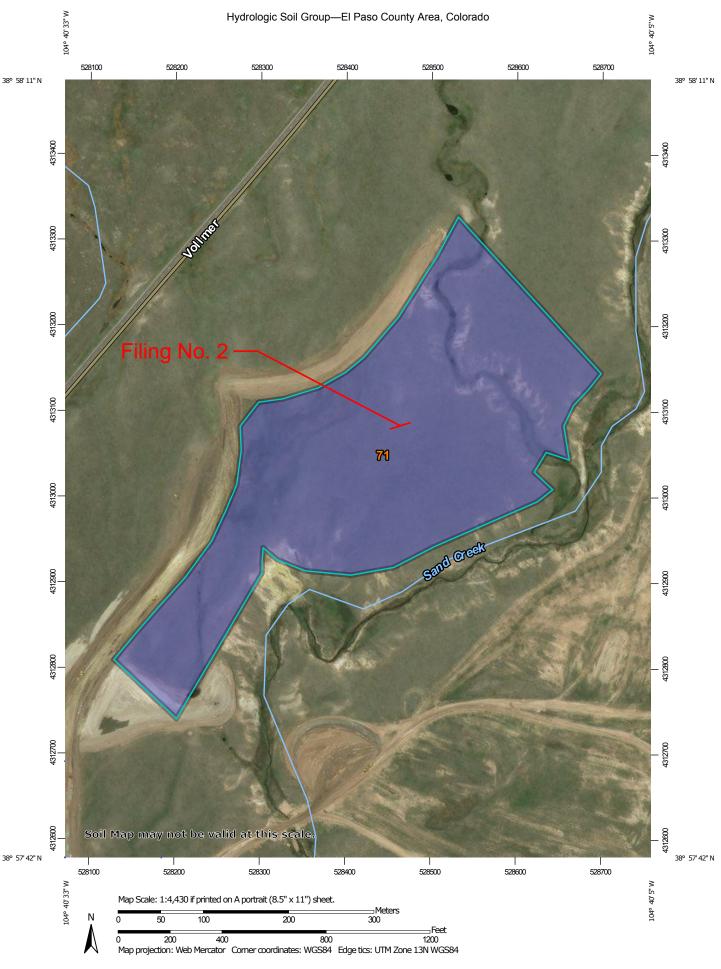






VICINITY MAP N.T.S.





MAP LEGEND MAP INFORMATION The soil surveys that comprise your AOI were mapped at Area of Interest (AOI) С 1:24.000. Area of Interest (AOI) C/D Soils Warning: Soil Map may not be valid at this scale. D **Soil Rating Polygons** Enlargement of maps beyond the scale of mapping can cause Not rated or not available Α misunderstanding of the detail of mapping and accuracy of soil **Water Features** line placement. The maps do not show the small areas of A/D Streams and Canals contrasting soils that could have been shown at a more detailed В Transportation B/D Rails ---Please rely on the bar scale on each map sheet for map measurements. Interstate Highways C/D Source of Map: Natural Resources Conservation Service **US Routes** Web Soil Survey URL: D Major Roads Coordinate System: Web Mercator (EPSG:3857) Not rated or not available -Local Roads Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts Soil Rating Lines Background distance and area. A projection that preserves area, such as the Aerial Photography Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required. This product is generated from the USDA-NRCS certified data as of the version date(s) listed below. B/D Soil Survey Area: El Paso County Area, Colorado Survey Area Data: Version 15, Oct 10, 2017 C/D Soil map units are labeled (as space allows) for map scales 1:50,000 or larger. D Not rated or not available Date(s) aerial images were photographed: May 22, 2016—Mar 9. 2017 **Soil Rating Points** The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background A/D imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident. B/D

Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
71	Pring coarse sandy loam, 3 to 8 percent slopes	В	29.0	100.0%
Totals for Area of Intere	est	29.0	100.0%	

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

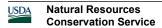
Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

Rating Options

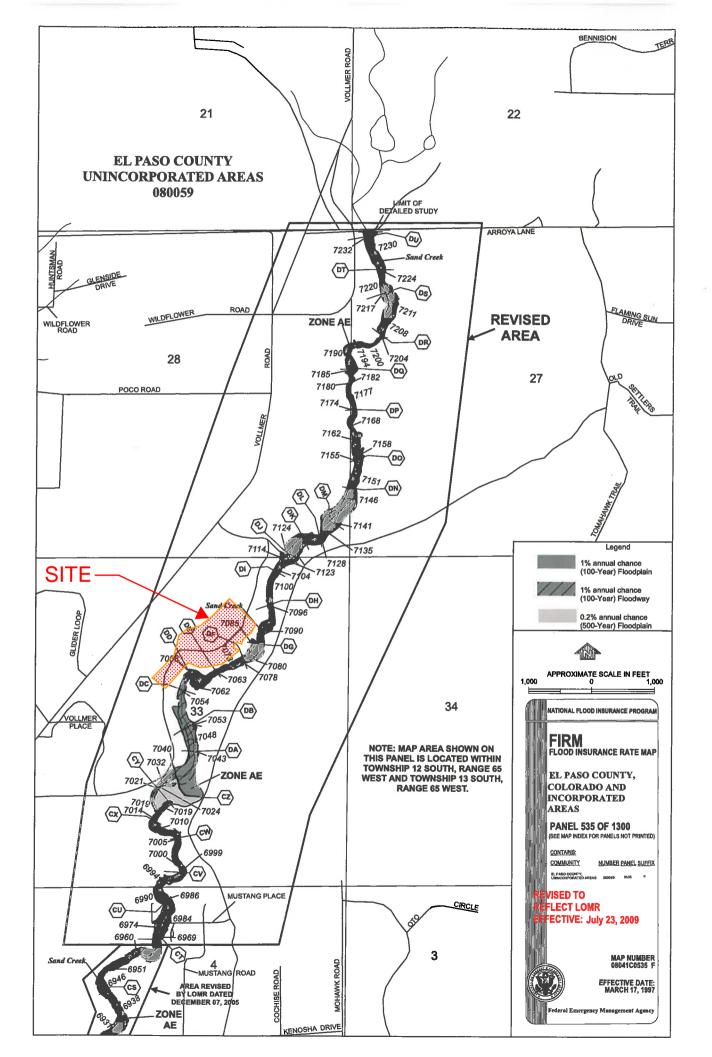
Aggregation Method: Dominant Condition



Component Percent Cutoff: None Specified

Tie-break Rule: Higher



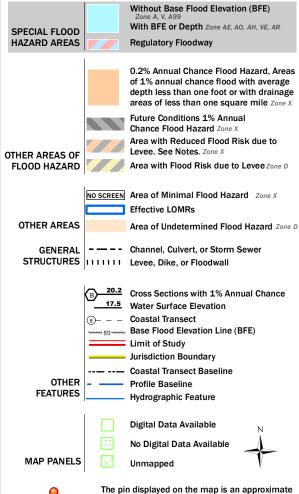


National Flood Hazard Layer FIRMette



Legend

SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT

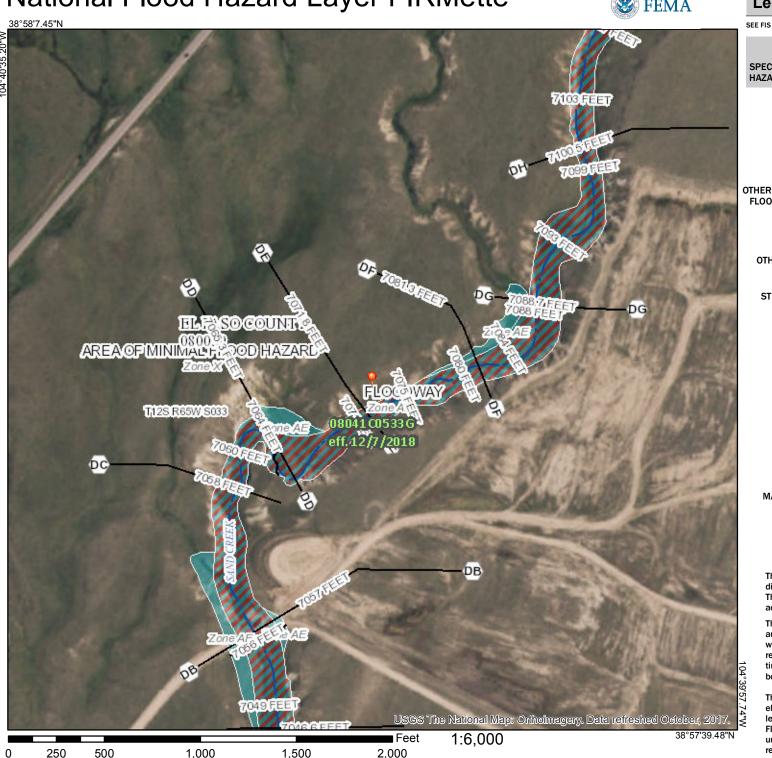


The pin displayed on the map is an approximate point selected by the user and does not represent an authoritative property location.

This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The basemap shown complies with FEMA's basemap accuracy standards

The flood hazard information is derived directly from the authoritative NFHL web services provided by FEMA. This map was exported on 1/23/2019 at 7:09:44 PM and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or become superseded by new data over time.

This map image is void if the one or more of the following map elements do not appear: basemap imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for unmapped and unmodernized areas cannot be used for regulatory purposes.



Latitude: 38.964784

Longitude: 104.67180

NGVD 29 height:

Datum shift(NAVD 88 minus NGVD 29): 1.196 meter

1.196 meters = 3.92 feet

NAVD88 - 3.92 feet = NGVD29

STORM 4 Outfall to Sand Creek Channel

Cross Section DE = 7071.8 NAVD88

7071.8 NAVD88 - 3.92 feet = 7067.88 NGVD29



HOMESTEAD AT STERLING RANCH FILING NO. 2 FINAL DRAINAGE REPORT

(Area Drainage Summary)

From Area Runoff Coe	ficient Summa	ıry			OVER.	LAND		STRE	ET / CH	ANNEL F	LOW	Time of T	Fravel (T_t)	INTENS	INTENSITY **		TOTAL FLOWS	
BASIN	AREA TOTAL	C ₅	C ₁₀₀	C ₅	Length	Height	T_{C}	Length	Slope	Velocity	T _t	TOTAL	СНЕСК	I ₅	I ₁₀₀	Q ₅	Q ₁₀₀	
	(Acres)	From DCI	A Table 5-1		(ft)	(ft)	(min)	(ft)	(%)	(fps)	(min)	(min)	(min)	(in/hr)	(in/hr)	(c.f.s.)	(c.f.s.)	
					Propo	osed Ar	ea Dra	inage S	ummai	ry								
ONSITE BASINS																		
J	0.43	0.22	0.46	0.22	90	1.8	12.0	0	2.0%	3.0	0.0	12.0	10.5	4.1	6.8	0.4	1.3	
<u>K</u>	0.61	0.22	0.46	0.22	75	1.5	10.9	0	2.0%	3.0	0.0	10.9	10.4	4.1	6.8	0.5	1.9	
P	4.42	0.38	0.55	0.38	100	2	10.3	1100	2.5%	3.0	6.0	16.4	16.7	3.4	5.7	5.7	13.8	
Q	3.78	0.38	0.55	0.38	100	2	10.3	1100	2.5%	3.0	6.0	16.4	16.7	3.4	5.7	4.9	11.8	
R	1.57	0.38	0.55	0.38	100	2	10.3	450	1.6%	3.0	2.5	12.8	13.1	3.8	6.3	2.2	5.4	
T	9.14	0.30	0.50	0.30	100	2	11.5	942	2.1%	3.0	5.2	16.7	15.8	3.4	5.8	9.4	26.4	
U	4.50	0.38	0.55	0.38	100	2	10.3	457	1.5%	3.0	2.5	12.9	13.1	3.8	6.3	6.4	15.6	
V1	1.48	0.38	0.55	0.38	100	2	10.3	600	2.0%	3.0	3.3	13.6	13.9	3.7	6.2	2.1	5.0	
V2	0.83	0.38	0.55	0.38	100	2	10.3	360	1.6%	3.0	2.0	12.3	12.6	3.8	6.4	1.2	2.9	
W1	0.86	0.22	0.46	0.22	80	6	7.3	0	0.0%	2.3	0.0	7.3	10.4	4.6	7.7	0.9	3.1	
W2	0.26	0.08	0.35	0.08	35	8	3.9	0	0.3%	2.3	0.0	5.0	10.2	5.2	8.7	0.1	0.8	
W3	0.56	0.08	0.35	0.08	35	8	3.9	160	0.5%	2.3	1.2	5.1	11.1	5.2	8.7	0.2	1.7	
X	0.22	0.22	0.46	0.22	80	6	7.3	0	2.5%	2.3	0.0	7.3	10.4	4.6	7.7	0.2	0.8	
X1	0.78	0.22	0.46	0.22	80	6	7.3	0	2.5%	2.3	0.0	7.3	10.4	4.6	7.7	0.8	2.8	
X2	1.04	0.22	0.46	0.22	80	6	7.3	0	2.5%	2.3	0.0	7.3	10.4	4.6	7.7	1.1	3.7	
Y	0.09	0.22	0.46	0.22	80	6	7.3	0	2.5%	2.3	0.0	7.3	10.4	4.6	7.7	0.1	0.3	
Y1	0.84	0.22	0.46	0.22	80	6	7.3	0	2.5%	2.3	0.0	7.3	10.4	4.6	7.7	0.8	3.0	
Y2	0.21	0.22	0.46	0.22	80	6	7.3	0	2.5%	2.3	0.0	7.3	10.4	4.6	7.7	0.2	0.7	
OFFSITE BASINS*													•		•			
B *	5.39	0.38	0.55	0.38	60	1.2	8.0	1381	2.8%	3.0	7.6	16.3	18.0	3.4	5.7	8.0	19.3	
C*	2.92	0.38	0.55	0.38	100	1.2	12.2	411	3.0%	3.0	2.3	14.5	12.8	3.8	6.3	4.2	10.1	
D*	2.90	0.38	0.55	0.38	100	2	10.3	245	2.1%	3.0	1.3	11.7	11.9	3.9	6.5	4.3	10.4	
E*	5.34	0.38	0.55	0.38	100	2	10.3	61	3.3%	3.0	0.3	10.7	10.9	4.0	6.8	8.2	19.9	
F*	1.12	0.90	0.96	0.90	10	0.2	0.9	1525	2.8%	3.0	8.4	9.3	18.5	4.2	7.1	4.3	7.7	
G*	0.61	0.22	0.46	0.22	100	2	12.6	0	2.2%	3.0	0.0	12.6	10.6	4.0	6.8	0.5	1.9	
H*	0.19	0.90	0.96	0.90	10	0.2	0.9	280	2.1%	3.0	1.5	5.0	11.6	5.2	8.7	0.9	1.6	
I*	2.10	0.90	0.96	0.90	10	0.2	0.9	1082	2.5%	3.0	5.9	6.9	16.1	4.7	7.9	8.9	15.9	
L^*	1.54	0.90	0.96	0.90	10	0.2	0.9	1805	2.1%	3.0	9.9	10.8	20.1	4.0	6.7	5.6	10.0	
S*	1.97	0.08	0.35	0.08	60	10	5.6	270	0.5%	2.3	2.0	7.6	11.8	4.5	7.6	0.7	5.3	

^{*} For detailed information on Desing Points, Basins, Flowby, or Pipe Runs see Sterling Ranch Filing Nos. 1&2 MDDP prepared by MS Civil Consultants, dated April 2017

Calculated by: ET/CMN
Date: 1/14/2020

Checked by: VAS

^{**} Intensity equations assume a minimum travel time of 5 minutes.

HOMESTEAD AT STERLING RANCH FILING NO. 2 FINAL DRAINAGE REPORT

(Basin Routing Summary)

			- 1-	1			8					I					Tr
	From Area Runoff Coefficient Summary					RLAND				NNEL FLO		Time of Travel (T_t)		SITY **	TOTAL .		J
DESIGN POINT	CONTRIBUTING BASINS	CA ₅	CA ₁₀₀	C ₅	Length	Height	T_{C}	Length	Slope	Velocity	T _t	TOTAL	I ₅	I ₁₀₀	Q_5	Q_{100}	COMMENTS
					(ft)	(ft)	(min)	(ft)	(%)	(fps)	(min)	(min)	(in/hr)	(in/hr)	(c.f.s.)	(c.f.s.)	
		P.	ROPOS	ED L	PRAIN A	IGE BA	SIN R	OUTIN	G SUM	MARY							
2*	B*	2.34	3.39									16.3	3.4	5.7	8.0	19.3	(2) EX. 15' AT-GRADE INLETS
3*	C*	1.11	1.61									12.8	3.8	6.3	4.2	10.1	EX. 6' SUMP INLET
4.5	De De De												2.0		1/1	26.7	
4*	D*, E*, F*	4.14	5.61									11.7	3.9	6.5	16.1	36. 7	EX. 15' AT-GRADE INLET
5*	G*, H*, FLOWBY DP4*	1.07	3.02									11.7	3.9	6.5	4.2	10 7	EX. 15' AT-GRADE INLET
,	G , II , FLOWBI DI 4	1.07	3.02									11.7	3.9	0.5	4.2	17./	EX. 15 A1-GRADE INLET
6*	I*, J, K, L*	3.50	3.97									10.8	4.0	6.7	14.1	26.7	EX. 15' AT-GRADE INLET
	, , ,																
7	P	1.68	2.43									16.4	3.4	5.7	5.7	13.8	PROP. 10' SUMP INLET
8	Q	1.44	2.08									16.4	3.4	5.7	4.9	11.8	PROP. 10' SUMP INLET
	D	0.60	0.06									12.0	3.8	6.2	2.2		
9	R	0.60	0.86									12.8	3.8	6.3	2.2	5.4	PROP. 10' SUMP INLET
10	T	2.74	2.69									15.8	3.4	5.8	9.4	15.6	PROP. 15' AT-GRADE INLET
10	•	2.71	2.07									15.0	5.1	2.0	7.4		Total CA100=3.86 Split Between
																	DP10 & DP11 For Crown Overflow
11	V1	0.56	2.69									15.8	3.4	5.8	1.9	15.6	PROP. 15' AT-GRADE INLET
																	Total CA100=3.86 Split Between
														<u> </u>			DP10 & DP11 For Crown Overflow
12	U, FLOWBY DP10	1.80	2.98									15.8	3.4	5.8	6.2	17.2	PROP. 10' SUMP INLET
																	Į
13	V2, FLOWBY DP11	0.32	0.96									13.6	3.7	6.2	1.2	5.9	PROP. MODIFIED
																	5'x4.5' SUMP INLET
14	W3, PR9	5.25	0.52									13.6	2.7	(2	10.6	52.1	
14	ws, rky	5.35	8.52									13.6	3.7	6.2	19.6	32.4	CUMULATIVE DETENTION DOND
																	DETENTION POND
													0.1	1 . 11	ETT/CLOL		IL

^{*} For detailed information on Desing Points, Basins, Flowby, or Pipe Runs see Sterling Ranch Filing Nos. 1&2 MDDP prepared by MS Civil Consultants, dated April 2017

** Intensity equations assume a minimum travel time of 5 minutes.

Calculated by: ET/CMN Date: 1/14/2020 Checked by: VAS

HOMESTEAD AT STERLING RANCH FILING NO. 2 DRAINAGE CALCULATIONS

(Storm Sewer Routing Summary)

					In	tensity**	Fle)w	PIPE SIZE
PIPE RUN	Contributing Pipes/Design Points	Equivalent CA 5	Equivalent CA ₁₀₀	Maximum T _C	I_5	I 100	Q 5	Q 100	
1	DP7	1.68	2.43	16.4	3.4	5.7	5.7	13.8	24" RCP
2	DP8	1.44	2.08	16.4	3.4	5.7	4.9	11.8	18" RCP
3	PR1, PR2	3.12	4.51	16.4	3.4	5.7	10.6	25.7	24" RCP
4	DP9, PR3	3.71	5.37	17.0	3.3	5.6	12.4	30.1	30" RCP
5	DP10	2.64	2.20	15.8	3.4	5.8	9.1	12.7	18" RCP
6	DP11	0.55	2.20	15.8	3.4	5.8	1.9	12.7	18" RCP
7	PR5, PR6	3.19	4.39	16.0	3.4	5.7	10.9	25.3	30" RCP
8	DP12	1.80	2.98	15.8	3.4	5.8	6.2	17.2	24" RCP
9	DP13, PR7, PR8	5.31	8.33	16.6	3.4	5.7	17.9	47.1	42" RCP
10	UD-Detention_v3.07						0. 7	23.4	Outlet Structure & 18" CMP
11	Pipe Run continued from MDDP DP1	5* to Sand Creek	. Flow values ar	e that of MDDF	Pipe Run	15* (PR15*).	42.1	76.8	42" RCP
12	Lots 36-41						0.0	1.3	12" ADS
13	Lots 28-35			0.0	1.6	12" ADS			
14	Lots 19-24			0.0	1.5	12" ADS			
<u>15</u>	Lots 13-18						0.0	1.4	12" ADS

^{*} For detailed information on Desing Points, Basins, Flowby, or Pipe Runs see Sterling Ranch Filing Nos. 1&2 MDDP prepared by MS Civil Consultants, dated April 2017

DP - Design Point EX - Existing Design Point FB- Flow By from Design Point INT- Intercepted Flow from Design Point

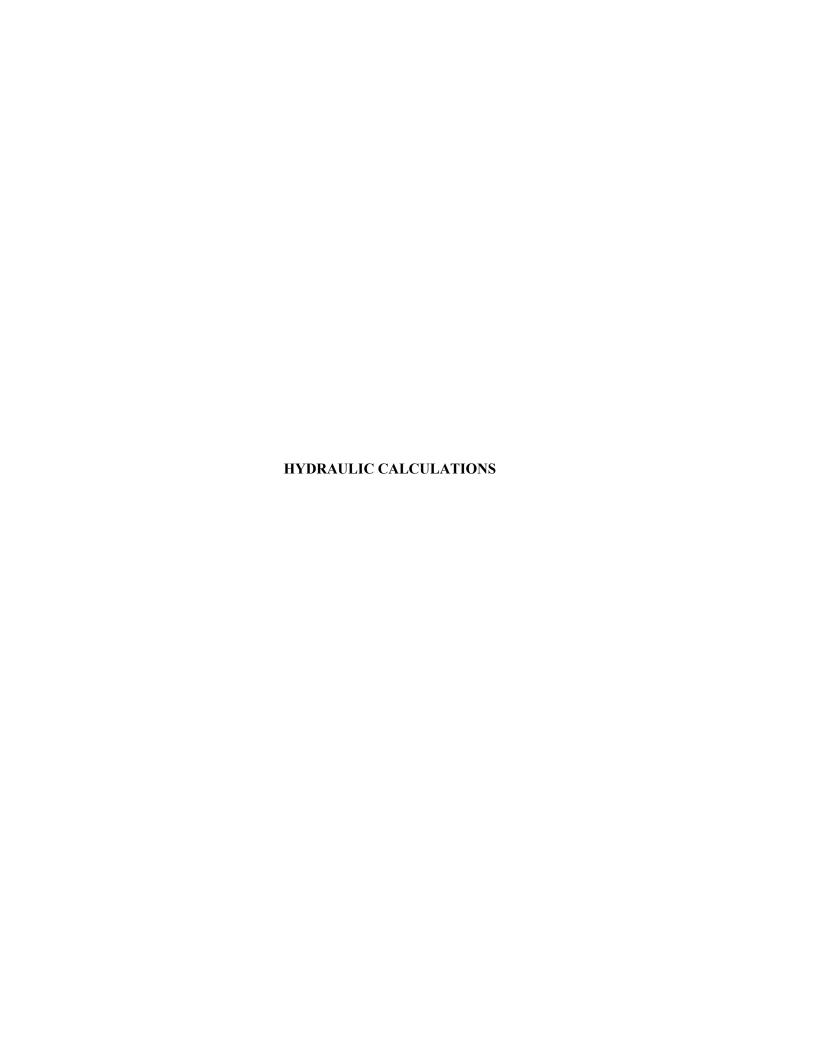
Calculated by: <u>CMN</u>

Date: <u>1/14/2020</u>

Checked by: <u>VAS</u>

Updated SF-3 routing for Basins X1, X2, W1, & Y1 included in Addendum above.

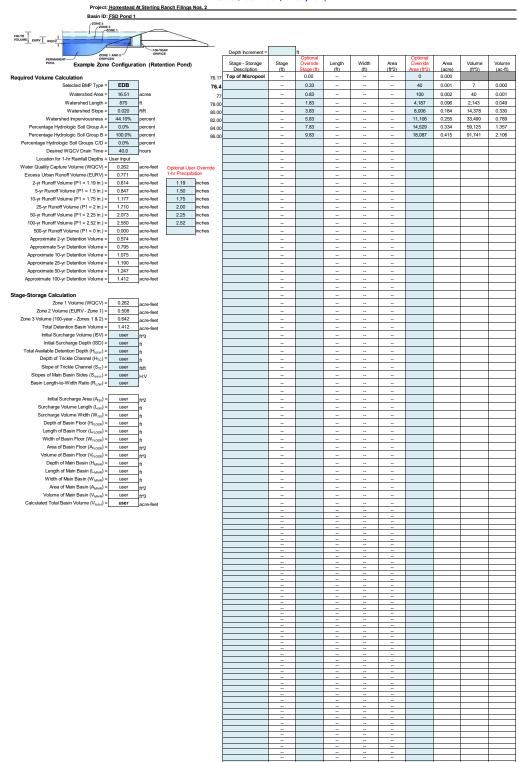
^{**} Intensity equations assume a minimum travel time of 5 minutes.



Weig	Weighted Percent Imperviousness of FSD Pond 1									
Contributing Basins	Area (Acres)	C 5	Impervious % (I)	(Acres)*(I)						
T	9.14	0.30	40	365.60						
$oldsymbol{U}$	4.50	0.38	53	238.50						
V1	1.48	0.38	53	78.44						
V2	0.83	0.38	53	43.99						
W1	0.56	0.08	2	1.12						
Totals	16.51			727.65						
Imperviousness of FSD Pond 1	44.1	%								

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

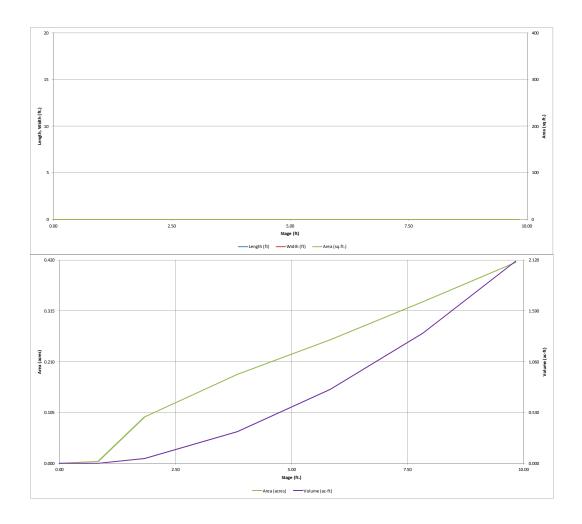
UD-Detention, Version 3.07 (February 2017)



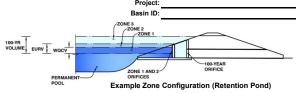
UD-Peterition_v3.07.x/sm, Basin 7/31/2019, 9:30 AM

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

UD-Detention, Version 3.07 (February 2017)



UD-Detention, Version 3.07 (February 2017)



	Stage (ft)	Zone Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	3.45	0.262	Orifice Plate
Zone 2 (EURV)	5.84	0.508	Orifice Plate
!one 3 (100-year)	8.00	0.642	Weir&Pipe (Restrict)
•		1.412	Total

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth = ft (distance below the filtration media surface) N/A Underdrain Orifice Diameter = N/A inches

Calculate	ed Parameters for Un	derdrai
Underdrain Orifice Area =	N/A	ft ²
Underdrain Orifice Centroid =	N/A	feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice =	0.00	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Orifice Plate =	5.84	ft (relative to basin bottom at Stage = 0 ft)
Orifice Plate: Orifice Vertical Spacing =	23.40	inches
Orifice Plate: Orifice Area per Row =	1.19	sq. inches (diameter = 1-3/16 inches)

Calculated Parameters for Plat								
WQ Orifice Area per Row =	8.264E-03	ft ²						
Elliptical Half-Width =	N/A	feet						
Elliptical Slot Centroid =	N/A	feet						
Elliptical Slot Area =	N/A	ft ²						

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	1.95	3.89					
Orifice Area (sq. inches)	1.19	1.19	1.19					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

	Not Selected	Not Selected	
Invert of Vertical Orifice =	N/A	N/A	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Vertical Orifice =	N/A	N/A	ft (relative to basin bottom at Stage = 0 ft)
Vertical Orifice Diameter =	N/A	N/A	inches

Calculated Parameters for Vertical Orifice					
	Not Selected	Not Selected			
Vertical Orifice Area =	N/A	N/A	ft ²		
Vertical Orifice Centroid =	N/A	N/A	feet		

User Input: Overflow Weir (Dropbox) and Grate (Flat or Sloped)

	Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	5.84	N/A	ft (relative to basin bottom at Stage = 0 ft
Overflow Weir Front Edge Length =	6.00	N/A	feet
Overflow Weir Slope =	3.00	N/A	H:V (enter zero for flat grate)
Horiz. Length of Weir Sides =	2.91	N/A	feet
Overflow Grate Open Area % =	70%	N/A	%, grate open area/total area
Debris Clogging % =	50%	N/A	%

Calculated			
Height of Grate Upper Edge, H_t =	6.81	N/A	feet
Over Flow Weir Slope Length =	3.07	N/A	feet
Grate Open Area / 100-yr Orifice Area =	7.21	N/A	should be ≥ 4
Overflow Grate Open Area w/o Debris =	12.88	N/A	ft ²
Overflow Grate Open Area w/ Debris =	6.44	N/A	ft ²
-			_

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

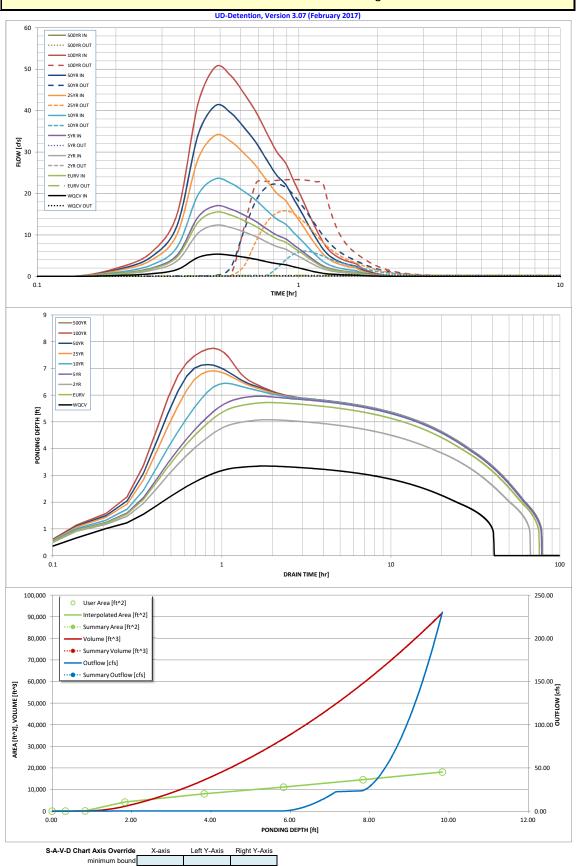
put: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectan			gular Orifice)	Calculated Parameters for Outlet Pipe w/ Flow Restriction P			te
	Zone 3 Restrictor	Not Selected			Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	0.25	N/A	ft (distance below basin bottom at Stage = 0 ft)	Outlet Orifice Area =	1.79	N/A	ft ²
Outlet Pipe Diameter =	24.00	N/A	inches	Outlet Orifice Centroid =	0.63	N/A	feet
Restrictor Plate Height Above Pipe Invert =	13.30	•	inches Half-Central Angle o	f Restrictor Plate on Pipe =	1.68	N/A	radians

User Input: Emerg	gency Spillway	(Rectangular or	Trapezoidal)

oser input zine.Benej spiniaj (nestanj	Saidi oi itapezoidai,	
Spillway Invert Stage=	7.80	ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length =	17.00	feet
Spillway End Slopes =	4.00	H:V
Freeboard above Max Water Surface =	1.00	feet

Calcula	ted Parameters for S	pillway
Spillway Design Flow Depth=	0.89	feet
Stage at Top of Freeboard =	9.69	feet
sin Area at Top of Freeboard =	0.41	acres

Routed Hydrograph Results									
Design Storm Return Period =	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
One-Hour Rainfall Depth (in) =	0.53	1.07	1.19	1.50	1.75	2.00	2.25	2.52	0.00
Calculated Runoff Volume (acre-ft) =	0.262	0.771	0.614	0.847	1.177	1.710	2.073	2.550	0.000
OPTIONAL Override Runoff Volume (acre-ft) =									
Inflow Hydrograph Volume (acre-ft) =	0.262	0.771	0.614	0.847	1.176	1.710	2.074	2.551	#N/A
Predevelopment Unit Peak Flow, q (cfs/acre) =	0.00	0.00	0.02	0.03	0.27	0.84	1.16	1.55	0.00
Predevelopment Peak Q (cfs) =	0.0	0.0	0.3	0.4	4.4	13.9	19.2	25.5	0.0
Peak Inflow Q (cfs) =	5.3	15.5	12.4	17.0	23.5	34.1	41.2	50.5	#N/A
Peak Outflow Q (cfs) =	0.1	0.2	0.2	0.7	6.0	15.8	22.3	23.4	#N/A
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	1.5	1.4	1.1	1.2	0.9	#N/A
Structure Controlling Flow =	Plate	Plate	Plate	Overflow Grate 1	Overflow Grate 1	Overflow Grate 1	Outlet Plate 1	Outlet Plate 1	#N/A
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	0.0	0.4	1.2	1.7	1.8	#N/A
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	#N/A
Time to Drain 97% of Inflow Volume (hours) =	39	69	62	71	69	66	63	61	#N/A
Time to Drain 99% of Inflow Volume (hours) =	40	73	65	76	75	74	73	72	#N/A
Maximum Ponding Depth (ft) =	3.35	5.72	5.08	5.96	6.44	6.91	7.15	7.75	#N/A
Area at Maximum Ponding Depth (acres) =	0.16	0.25	0.23	0.26	0.28	0.30	0.31	0.33	#N/A
Maximum Volume Stored (acre-ft) =	0.245	0.741	0.588	0.802	0.932	1.067	1.137	1.331	#N/A



maximum bound

Outflow Hydrograph Workbook Filename:

Storm Inflow Hydrographs

UD-Detention, Version 3.07 (February 2017)

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

SOURCE WORKBOOK WORKBOOK WORKBOOK WORKBOOK WORKBOOK WORKBOOK WORKBOOK WORKBOOK WORKBOOK #N/A

	SOURCE	WORKBOOK	WORKBOOK	WORKBOOK	WORKBOOK	WORKBOOK	WORKBOOK	WORKBOOK	WORKBOOK	#N/A
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
4.40	0:00:00		0.00	0.00			0.00		0.00	401/0
4.12 min		0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	0:04:07	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
Hydrograph	0:08:14	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
Constant	0:12:22	0.24	0.68	0.55	0.75	1.03	1.47	1.77	2.15	#N/A
1.214	0:16:29	0.64	1.85	1.48	2.02	2.79	4.01	4.84	5.91	#N/A
	0:20:36	1.65	4.74	3.79	5.20	7.16	10.30	12.42	15.18	#N/A
	0:24:43	4.55	13.03	10.43	14.28	19.66	28.29	34.10	41.64	#N/A
	0:28:50	5.34	15.51	12.37	17.02	23.54	34.08	41.22	50.54	#N/A
	0:32:58	5.08	14.81	11.80	16.25	22.50	32.61	39.48	48.45	#N/A
	0:37:05	4.62	13.48	10.75	14.80	20.49	29.69	35.94	44.09	#N/A
	0:41:12	4.11	12.05	9.59	13.23	18.35	26.64	32.27	39.64	#N/A
	0:45:19	3.53	10.41	8.28	11.44	15.90	23.13	28.07	34.53	#N/A
	0:49:26	3.08	9.07	7.22	9.96	13.83	20.09	24.40	30.06	#N/A
	0:53:34	2.79	8.22	6.54	9.03	12.54	18.22	22.11	27.22	#N/A
	0:57:41	2.73	6.79	5.39	7.47	10.41	15.18	18.44	22.73	#N/A
	1:01:48									
		1.84	5.56	4.40	6.12	8.55	12.50	15.21	18.77	#N/A
	1:05:55	1.40	4.29	3.39	4.73	6.64	9.78	11.93	14.77	#N/A
	1:10:02	1.02	3.21	2.52	3.54	5.01	7.43	9.10	11.31	#N/A
	1:14:10	0.75	2.32	1.83	2.56	3.64	5.45	6.70	8.37	#N/A
	1:18:17	0.59	1.79	1.42	1.97	2.79	4.15	5.08	6.32	#N/A
	1:22:24	0.48	1.47	1.16	1.62	2.29	3.38	4.13	5.12	#N/A
	1:26:31	0.41	1.25	0.99	1.38	1.94	2.86	3.49	4.32	#N/A
	1:30:38	0.36	1.10	0.87	1.21	1.70	2.50	3.05	3.77	#N/A
	1:34:46	0.33	0.99	0.78	1.09	1.52	2.24	2.73	3.38	#N/A
	1:38:53	0.30	0.91	0.72	1.00	1.40	2.06	2.51	3.10	#N/A
	1:43:00	0.22	0.67	0.53	0.73	1.03	1.52	1.85	2.29	#N/A
	1:47:07	0.16	0.49	0.39	0.54	0.75	1.11	1.35	1.67	#N/A
	1:51:14	0.12	0.36	0.28	0.40	0.55	0.81	0.99	1.23	#N/A
	1:55:22	0.09	0.26	0.21	0.29	0.41	0.60	0.74	0.91	#N/A
	1:59:29	0.06	0.19	0.15	0.21	0.30	0.44	0.53	0.66	#N/A
	2:03:36	0.04	0.13	0.11	0.15	0.21	0.31	0.38	0.47	#N/A
	2:07:43	0.03	0.10	0.08	0.11	0.15	0.23	0.28	0.34	#N/A
	2:11:50	0.03	0.06	0.05	0.07	0.10	0.25	0.19	0.24	#N/A
	2:15:58									
	2:20:05	0.01	0.04	0.03	0.04	0.06	0.10	0.12	0.15	#N/A
		0.00	0.02	0.01	0.02	0.03	0.05	0.06	0.08	#N/A
	2:24:12	0.00	0.01	0.00	0.01	0.01	0.02	0.03	0.04	#N/A
	2:28:19	0.00	0.00	0.00	0.00	0.00	0.00	0.01	0.01	#N/A
	2:32:26	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	2:36:34	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	2:40:41	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	2:44:48	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	2:48:55	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	2:53:02	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	2:57:10	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	3:01:17	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	3:05:24	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	3:09:31	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	3:13:38	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	3:17:46	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	3:21:53	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	3:26:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	3:30:07	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	3:34:14	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	3:38:22	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	3:42:29	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	3:46:36	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	3:50:43	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	3:54:50	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	3:58:58	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	4:03:05	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	4:07:12 4:11:19	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A #N/A
	4:11:19	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A #N/A
	4:19:34	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	4:23:41	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	4:27:48	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	4:31:55	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	4:36:02	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	4:40:10	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	4:44:17	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	4:48:24	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	4:52:31	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	4:56:38	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A



PROJECT:	Homestead Filing No. 2
DATE:	

Micropool Surface Area	Tribm	tag Area	= 16.51 AC	
TIA IXA			= 44.1%	
(0.441 x 1451)				
TIA = 7.3 ~ 8.0	, in			
From Micropool Sizing Chan	of (SA)	Micropoof	SA = 40 st	2
				2
Foreboy Volume for PSD Pa	_			
Topontary Area - 16.51.				
Min. Forebuy Voiume - 3	1 1		WOFED 7-5,	, EDB
Wacv for FoD Pond = a.	262 Ac-	A		Management and the second seco
Total Volume Regid. = 0.0	3 (0.242	13540	= 342cf	
Arca = 283 - 7 (wall) =				
		Footb	a 15 1 H	
(forebay) (dust) (10/10		70.00	y 15 depth	TO THE PARTY OF TH
(torchan) (dysta) (volun proud				
		to 207 +1		1000
Since notch in Forebry to Q100 = 47.1 cfs => 0.02 x 5	a comman	CUOPEL	T-5 EDS	
(4100 = 41.1 cts = 0.02 x 5	7.7 = 0.99	LUR		9 ,
Using Ret. Weir Egn.	Q = 3.24	1121.118	7	<i>H.</i> /
Solve for L = 2.6" 0	= 0,94	// % ~		continues animateur
		use a 2.	6"notch	- Annual Control
			The state of the s	



PROJECT:	Homestead Filing No. 2	
PROJECT:	North Control of the	_
DATE:		

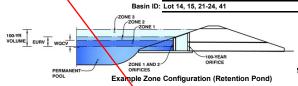
Q: os.	Apron For	Panel 1	
Riprop Sizina) which I w	Panel 1	
Q100 = 47.1 cfs	(Ping Bung)		
D ₂ = 42° = 3.5′			
01.5 < 6 The	n use Figure	9-38 (UDFC	D Nol 5)
47.1 = 2.05	< 6 Therefore county	re use Figure	9-38 01.5 - 17.1 = 7.19 01.5 (3.5)" = 7.19
Use Type L	D ₅₀ =9"		(3, 5)
Rioras Deptin			
T=2-0s			
Law Teinheater Ripre			
FES	9' 1-w=7'-1	6 1 X00	
Toewall	11.5'		

DETENTION BASIN STAGE-STORAGE TABLE BUILDER UD-Detention, Version 3.07 (February 2017) Project: Homestead at Sterling Ranch Filing No.2 Basin ID: Lots 14, 15, 21-24, 41 Lot size 10,319 sq ft-15,049 sq ft Depth Increment = Example Zone Configuration (Retention Pond) Stage - Storage Stage Override Length Width Area Override Volume Volume Description (ft) (ft^2) (ac-ft) Media Surface 0.00 77 0.002 7065.27 **Required Volume Calculation** 152 Selected BMP Type = 0.50 0.003 0.001 7065.5 Watershed Area : 0.18 1.00 328 0.004 ------0.008 174 ote: L / W R 7066 82 1.50 543 0.012 390 0.009 Watershed Length = 7066.50 L/W.Ratio = Watershed Slope = 0.080 ft/ft 2.00 796 0.018 722 0.017 7067.00 Watershed Imperviousness = 42.00% --Percentage Hydrologic Soil Group A = Percentage Hydrologic Soil Group B = 100.0% percent Percentage Hydrologic Soil Groups C/D = ercent Desired WQCV Drain Time = 12.0 hours Location for 1-hr Rainfall Depths = User Input --Water Quality Capture Volume (WQCV) = 0.002 acre-feet Optional User Override 1-hr Precipitation Excess Urban Runoff Volume (EURV) = 0.008 acre-feet 2-yr Runoff Volume (P1 = 1.19 in.) = 0.006 acre-feet 1.19 inches 5-yr Runoff Volume (P1 = 1.5 in.) = 0.009 acre-feet 1.50 inches ------10-yr Runoff Volume (P1 = 1.75 in.) = 0.012 acre-feet 1.75 inches --25-yr Runoff Volume (P1 = 2 in.) = 0.018 acre-feet 2 00 inches 50-yr Runoff Volume (P1 = 2.25 in.) = 0.022 acre-feet 2.25 inches 100-yr Runoff Volume (P1 = 2.52 in.) = 0.027 acre-feet 2.52 inches ----500-yr Runoff Volume (P1 = 0 in.) = acre-feet Approximate 2-yr Detention Volume = 0.006 -acre-feet Approximate 5-yr Detention Volume = 0.008 acre-feet Approximate 10-yr Detention Volume = 0.011 acre-feet --Approximate 25-yr Detention Volume = 0.012 acre-feet --Approximate 50-yr Detention Volume = 0.013 acre-feet __ --__ Approximate 100-yr Detention Volume 0.015 acre-feet Stage-Storage Calculation ------Zone 1 Volume (WQCV) = 0.002 acre-feet Zone 2 Volume (EURV - Zone 1) = 0.006 acre-feet Zone 3 Volume (100-year - Zones 1 & 2) = 0.007 Total Detention Basin Volume 0.015 --Initial Surcharge Volume (ISV) = N/A Initial Surcharge Depth (ISD) = N/A ------Total Available Detention Depth (H_{total}) = user Depth of Trickle Channel (H_{TC}) = N/A --Slope of Trickle Channel (STC) = N/A ft/ft Slopes of Main Basin Sides (Smain)

UD-Detention v3.07 LOT 15.xlsm, Basin

UD-Detention, Version 3.07 (February 2017)

Project: Homestead at Sterling Ranch Filing No.2



	Stage (ft)	Zone Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	0.71	0.002	Filtration Media
Zone 2 (EURV)	1.41	0.006	Rectangular Orifice
one 3 (100-year)	1.90	0.007	Rectangular Orifice
•		0.015	Total

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Death 2.10 ft (distance below the filtration media surface)
Underdrain Orifice Diamete 0.13 inches

Calculate	ca i arameters for	<u>Onucian</u>
Underdrain Orifice Area =	0.0	5 6 ²
Underdrain Orifice Centroid =	0.01	feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice =	N/A		ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Orifice Plate =	W/A		ft (relative to basin bottom at Stage = 0 ft)
Orifice Plate: Orifice Vertical Spacing =	N/X		inches
Orifice Plate: Orifice Area per Row =	N/A	$\overline{}$	inches

Calcu	Calculated Parameters for Pla					
WQ Orifice Area per Row =	N/A	ft ²				
Elliptical Half-Width =	N/A	feet				
Elliptical Slot Centroid =	N/A	feet				
Elliptical Slot Area =	N/A	ft ²				
· ·		_				

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (optional)	Row 2	(optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row	(optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	N/A	1	N/A	N/A	N/A	N/A		N/A	N/A	N/A
Orifice Area (sq. inches)	N/A	ì	W A	N/A	N/A	N/A	_	N/A	N/A	N/A

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Orifice Area (sq. inches)	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A

User Input: Vertical Orifice (Circular or Rectangular)

	Zone 2 Rectangular	Zone 3 Rectangular		
Invert of Vertical Orifice =	0.71	1.41	ft (relative to	basin bottom at Stage = 0 ft)
Depth at top of Zone using Vertical Orifice =	1.41	1.90	ft (relative to	basin bottom at Stage = 0 ft)
Vertical Orifice Height =	2.00	2.00	inches	\ /
Vertical Orifice Width =	1.00	6.00	inches	

Calculated Parameters for Vertical Orifice						
	Zone 2 Rectangular	Zone 3 Rectangular				
Vertical Orifice Area =	0.01	0.08	ft ²			
Vertical Orifice Centroid =	0.08	0.08	feet			

User Input: Overflow Weir (Dropbox) and Grate (Flat or Sloped)

	Not Selected	Not Selected	Y
Overflow Weir Front Edge Height, Ho =	1.88	N/A	ft (relative to basin bottom at Stage = 0 ft)
Overflow Weir Front Edge Length =	1.00	N/A	feet
Overflow Weir Slope =	0.00	N/A	H:V (enter zero for flet grate)
Horiz. Length of Weir Sides =	1.00	N/A	feet /
Overflow Grate Open Area % =	70%	N/A	%, grate open area/total area
Debris Clogging % =	50%	N/A	%

Not Selected

Calculated F	Calculated Parameters for Overflow Weir				
	Not Selected	Not Selected			
Height of Grate Upper Edge, H _t =	1.88	N/A	feet		
Over Flow Weir Slope Length =	1.00	N/A	feet		
Grate Open Area / 100-yr Orifice Area =	N/A	N/A	should be		
Overflow Grate Open Area w/o Debris =	0.70	N/A	ft ²		
Overflow Grate Open Area w/ Debris =	0.35	N/A	ft ²		
<u> </u>			_		

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

Depth to Invert of Outlet Pipe =	N/A	N/A	ft (distance below basin bottom at Stage = 0 ft)
Circular Orifice Diameter =	N/A	N/A	inches
-			Half-Cen

Not Selected

	Not Selected	Not Selected	
Outlet Orifice Area =	N/A	N/A	ft ²
Outlet Orifice Centroid =	N/A	N/A	feet
of Restrictor Plate on Pipe =	N/A	N/A	radians

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage=	1.90	ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length =	2.00	feet
Spillway End Slopes =	4.00	H √
Freeboard above Max Water Surface =	0.25	feet
•		•

Calcula	ted Parameters for S	pillway
Spillway Design Flow Depth=	0.14	feet
Stage at Top of Preeboard =	2.29	feet
sin Area at Top of Freeboard =	0.02	acres
	0.00	

Ва

Routed Hydrograph Results							\		
Design Storm Return Period =	WQQV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
One-Hour Rainfall Depth (in) =	0.53	1.07	1.19	1.50	1.75	2.00	2.25	2.52	0.00
Calculated Runoff Volume (acre-ft) =	0.002	0.008	0.006	0.009	0.012	0.018	0.022	0.027	0.000
OPTIONAL Override Runoff Volume (acre-ft) =									
Inflow Hydrograph Volume (acre-ft) =	0.001	0.007	0.006	0.008	0.012	0.018	0.021	0.027	#N/A
Predevelopment Unit Peak Flow, q (cfs/acre) =	0.00	0.00	0.02	0.03	0.32	0.97	1.34	1.78	0.00
Predevelopment Peak Q (cfs) =	0.0	0.0	0.0	0.0	0.1	0.2	0.2	0.3	0.0
Peak Inflow Q (ofs) =	0.0	0.2	0.2	0.2	0.3	0.5	0.6	0.8	#N/A
Peak Outflow Q (cfs) =	0.0	0.0	0.0	0.0	0.1	0.2	0.3	0.3	#N/A
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	8.1	1.4	1.2	1.1	1.0	#N/A
Structure Controlling Flow =	Filtration Media	Vertical Orifice 1	Vertical Orifice 1	Vertical Orifice 1	Vertical Orifice 2	Vertical Orifice 2	Vertical Orifice 2	Vertical Orifice 2	#N/A
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	#N/A
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N)A	#N/A
Time to Drain 97% of Inflow Volume (hours) =	12	40	40	39	38	35	33	30	#N/A
Time to Drain 99% of Inflow Volume (hours) =	12	43	43	43	43	42	41	40	#N/A
Maximum Ponding Depth (ft) =	0.27	1.17	1.01	1.24	1.47	1.62	1.72	1.88	#N/A
Area at Maximum Ponding Depth (acres) =	0.00	0.01	0.01	0.01	0.01	0.01	0.02	0.02	#N/A
Maxipum Volume Stored (acre-ft) =	0.001	0.005	0.004	0.006	0.009	0.011	0.012	0.014	#N/A
<i>'</i>									

Detention Basin Outlet Structure Design UD-Detention, Version 3.07 (February 2017) - 500YR IN ----- 500YR OUT 0.7 - - 100YR OUT = 50YR IN - - 50YR OUT 0.6 - 25YR IN 25YR OUT 0.5 10YR OUT FLOW [cfs] 6.0 = 2YR IN === 2YR OUT - EURV IN 0.3 - EURV OUT ••••• WQCV OUT 0.2 0.1 TIME [hr] 1.8 1.6 -10YR -SYR —2YR 1.4 EURV -wqcv DONDING DEPTH [#] 1.2 0.6 0.4 0.2 0.1 100 DRAIN TIME [hr] 1.00 O User Area [ft^2] Interpolated Area [ft^2] 0.90 800 ··• ·· Summary Area [ft^2] Volume [ft^3] 0.80 700 ···• ·· Summary Volume [ft^3] 0.70 Outflow [cfs] AREA [ft^2], VOLUME [ft^3] 0.60 [cfs] 09:0 0.40 0.30 200 0.20 0.10 0.00 0.00

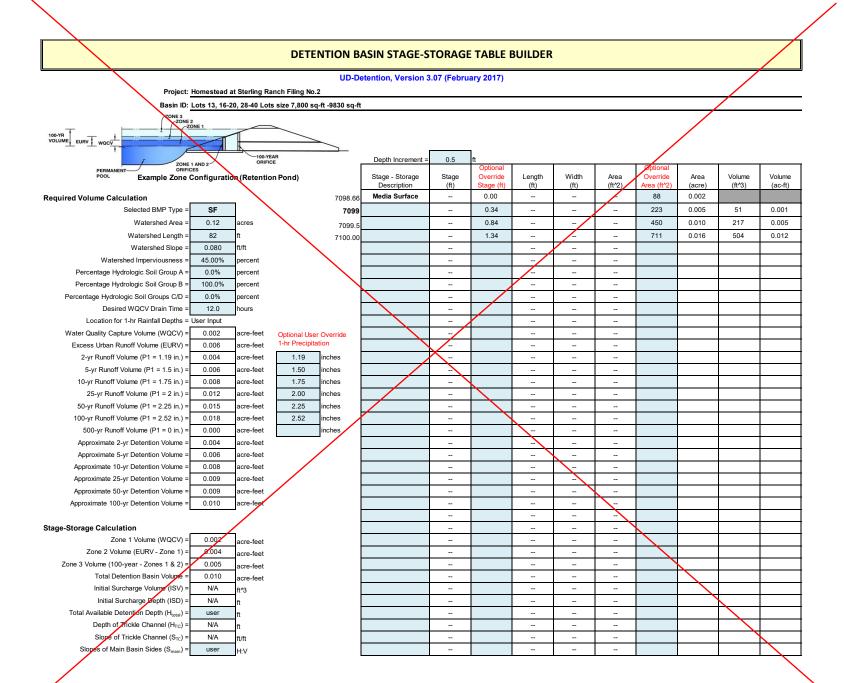
2.00

S-A-V-D Chart Axis Override Right Y-Axis minimum bound maximum bound

1.00

PONDING DEPTH [ft]

0.50

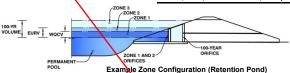


UD-Detention_v3.07_vOT 40.xlsm, Basin

UD-Detention, Version 3.07 (February 2017)

Project: Homestead at Sterling Ranch Filing No.2

Basin ID: Lots 13, 16-20, 28-40 Lots size 7,800 sq-ft -9830 sq-ft



	Stage (ft)	Zone Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	0.40	0.002	Filtration Media
Zone 2 (EURV)	0.89	0.004	Rectangular Orifice
one 3 (100-year)	1.24	0.005	Rectangular Orifice
•		0.010	Total

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depti = 2.10 ft (distance below the filtration media surface)
Underdrain Orifice Diameter 0.13 inches

Calculated Parameters for Underdrain

Underdrain Orifice Area = 0.0 ft²

Underdrain Orifice Centroid = 0.01 feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice =	y	N/A		ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Orifice Plate =	١	VΑ		ft (relative to basin bottom at Stage = 0 ft)
Orifice Plate: Orifice Vertical Spacing =	١	N/A	\	inches
Orifice Plate: Orifice Area per Row =	1	N/A	1	inches

Caicu	iated Paramete	ers for Plate
WQ Orifice Area per Row =	N/A	ft ²
Elliptical Half-Width =	N/A	feet
Elliptical Slot Centroid =	N/A	feet
Elliptical Slot Area =	N/A	ft ²

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (optional)	Row	2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row	6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	N/A		WA	N/A	N/A	N/A		N/A	N/A	N/A
Orifice Area (sq. inches)	N/A		N/A	N/A	N/A	N/A	\	N/A	N/A	N/A

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Orifice Area (sq. inches)	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A

User Input: Vertical Orifice (Circular or Rectangular)

	Zone 2 Rectangular	Zone 3 Rectangular		
Invert of Vertical Orifice =	0.40	0.89	ft (relative to	asin bottom at Stage = 0 ft)
Depth at top of Zone using Vertical Orifice =	0.89	1.24	ft (relative to b	asin bottom at Stage = 0 ft)
Vertical Orifice Height =	2.00	2.00	inches	\ /
Vertical Orifice Width =	1.00	3.50	inches	\ /

Calculated Parameters for Vertical Orifice						
	Zone 2 Rectangular	Zone 3 Rectangular				
Vertical Orifice Area =	0.01	0.05	ft ²			
Vertical Orifice Centroid =	0.08	0.08	fee			

User Input: Overflow Weir (Dropbox) and Grate (Flat or Sloped)

	Not Selected	Not Selected	
Overflow Weir Front Edge Height, Ho =	1.24	N/A	ft (relative to basin bottom at Stage =
Overflow Weir Front Edge Length =	1.00	N/A	feet
Overflow Weir Slope =	0.00	N/A	H:V (enter zero for f/at grate)
Horiz. Length of Weir Sides =	1.00	N/A	feet
Overflow Grate Open Area % =	70%	N/A	%, grate open rea/total area
Debris Clogging % =	50%	N/A	%

Calculated	Parameters for Ove	rflow Weir	
	Not Selected	Not Selected	
Height of Grate Upper Edge, H_t =	1.24	N/A	feet
Over Flow Weir Slope Length =	1.00	N/A	feet
Grate Open Area / 100-yr Orifice Area =	N/A	N/A	should be ≥ 4
Overflow Grate Open Area w/o Debris =	0.70	N/A	ft ²
Overflow Grate Open Area w/ Debris =	0.35	N/A	ft ²
_			_

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

	Not Selected	Not Selected		\
Depth to Invert of Outlet Pipe =	N/A	N/A	ft (distance below basin bottom at Stage = 0 ft)	_/
Circular Orifice Diameter =	N/A	N/A	inches	o
			Half-Central Angle	of Re

	Not Selected	Not Selected	
Outlet Orifice Area =	N/A	N/A	ft ²
Outlet Orifice Centroid =	N/A	N/A	feet
Restrictor Plate on Pipe =	N/A	N/A	radians

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate

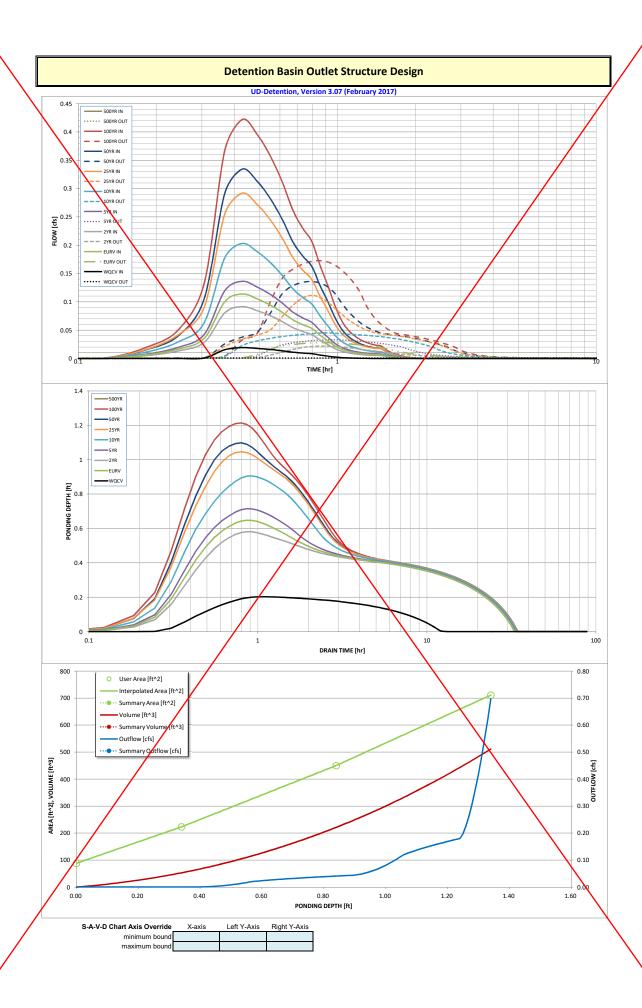
User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage=	1.24	ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length =	2.00	feet /
Spillway End Slopes =	4.00	ну
Freeboard above Max Water Surface =	0.25	reet

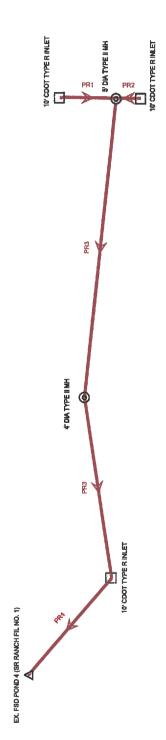
ted Parameters for S	pillway
0.14	feet
1.63	feet
0.02	acres
	0.14 1.63

Ва

Routed Hydrograph Results									
Design Storm Return Period =	WQC	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
One-Hour Rainfall Depth (in) =	0,83	1.07	1.19	1.50	1.75	2.00	2.25	2.52	0.00
Calculated Runoff Volume (acre-ft) =	Ø.002	0.006	0.004	0.006	0.008	0.012	0.015	0.018	0.000
OPTIONAL Override Runoff Volume (acre-ft) =									
Inflow Hydrograph Volume (acre-ft) =	0.001	0.005	0.004	0.006	0.008	0.012	0.014	0.018	#N/A
Predevelopment Unit Peak Flow, q (cfs/acre) =	0.00	0.00	0.02	0.03	0.28	0.88	1.21	1.61	0.00
Predevelopment Peak Q (cfs)	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.2	0.0
Peak Inflow Q (cfs) =	0.0	0.1	0.1	0.1	0.2	0.3	0.3	0.4	#N/A
Peak Outflow Q (cfs) =	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.2	#N/A
Ratio Peak Outflow to Predeveloppent Q =	N/A	N/A	N/A	10.1	1.4	1.1	1.0	0.9	#N/A
Structure Controlling Flow =	Filtration Media	Vertical Orifice 1	Vertical Orifice 1	Vertical Orifice 1	Vertical Orifice 2	Vertical Orifice 2	Vertical Orifice 2	Vertical Orifice 2	#N/A
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	#N/A
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	#N/A
Time to Drain 97% of Inflow Volume (hours) =	12	31	31	30	29	28	27	25	#N/A
Time to Drain 99% of Inflow Volume (hours) =	12	32	32	32	33	32	32	31	#N/A
Maximum Ponding Depth (ft) =	0.20	0.65	0.58	0.71	0.91	1.05	1.10	1.21	#N/A
Area at Maximum Ponding Depth (acres) =	0.00	0.01	0.01	0.01	0.01	0.01	0.01	0.01	#N/A
Maximum Volume Stored (acre-ft) =	0.001	0.003	0.003	0.004	0.006	0.007	0.008	0.010	#N/A
/									



4

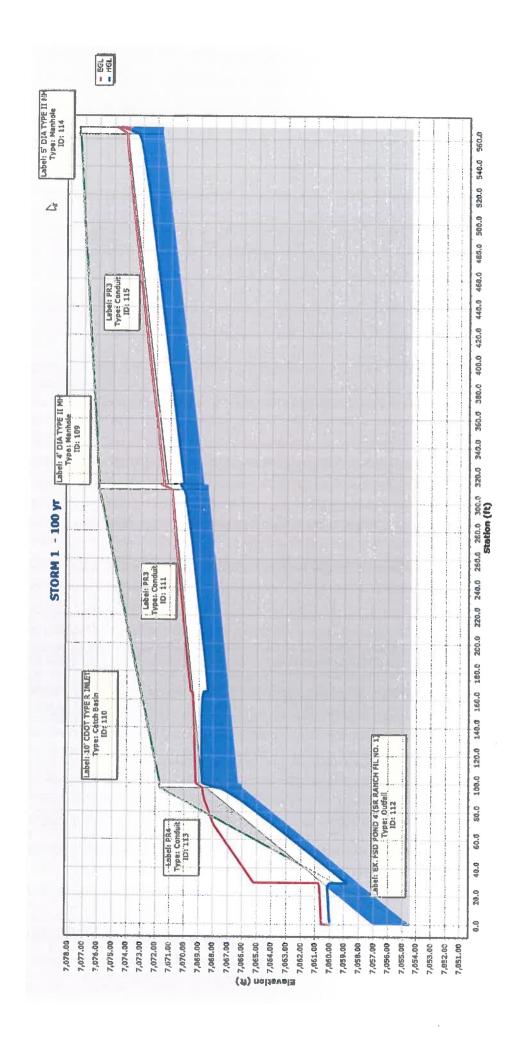


Bentley StormCAD CONNECT Edition [10.01.01.04] Page 1 of 1

> Bentley Systems, Inc. Haestad Methods Solution Center 27 Siemon Company Drive Suite 200 W Watertown, CT 06795 USA +1-203-755-1666

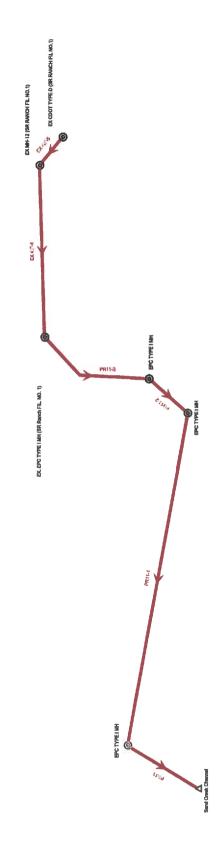
Conduit FlexTable: Table - 1 STRM 18.2

				I ICA I ANICI	CONTRACTOR I ADDICTOR I OF INTERIOR	TO MINICA			
Label	Upstream Structure	Rise (ft)	How (cfs)	How / Capacity (Design) (%)	Length (Unified) (ft)	Velocity (ft/s)	Froude Number (Normal)	Depth (Normal) (ft)	Depth (Critical) (ft)
PR3	4' DIA TYPE II MH		25.70	62.7	213.1	8.82	1.432	1.43	1.73
PR4	10' CDOT TYPE R INLET		30.10	21.5	68.7	22.71	5.300	0.79	1.87
PR3	5' DIA TYPE II MH		25.70	58.4	254.1	9.31	1.557	1.37	1.73
PR2.	10' CDOT TYPE R INLET		11.80	37.9	3.2	3.76	2.023	0.85	1.23
PR1	10' CDOT TYPE R INLET		13.80	26.6	27.2	13.97	3,425	0.70	1.34
Hydraulic Grade Line (In) (ft)	Hydraulic Grade Line (Out) (ft)	Headloss (ft)	Upstream Structure Hydraulic Grade Line (In)	Upstream Structure Velocity (In- Governing) (ft/s)	Upstream Structure Headloss Coefficient	Upstream Structure Headloss (ft)	Elevation Ground (Start) (ft)	Invert (Start) (ft)	Invert (Stop) (ft)
7,070.13	7,068.77	1.36	7,070.34	9.31	0.270	0.21	7,075.93	7,068.40	7,066.27
7,067.84		7.84	7,068.77	5.24	1.020	0.93	7,071.69	7,065.97	7,054.50
7,073.35		3.27	7,074.54	4.39	1.520	1.19	7,077.37	7,071.62	7,068.70
7,074.55		10.0	7,075.57	3.76	1.000	1.02	7,077.10	7,072.18	7,072.12
7,074.89	7,074.54	0.35	7,075.49	6.18	1.020	0.61	7,077.10	7,073.55	7,072.12



Scenario: 100 yr

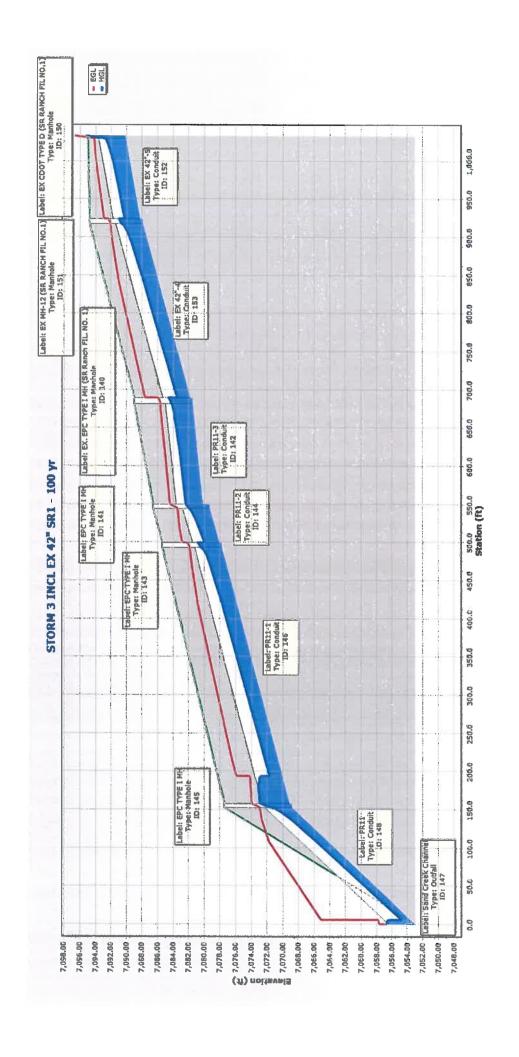
STEM 3 THEL EXHZ" SRI



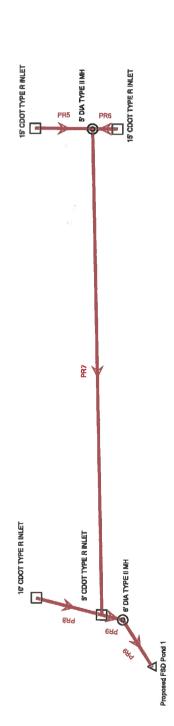
Bertley StormCAD CONNECT Edition [10.01.01.04] Page 1 of 1

Conduit FlexTable: Table - 1 STRM 3 INCL 42" SR1

									_								
Depth (Critical)	(£)	2.74	2.74	2.74	2.74	2.74		2.74	Invert (Stop)	£		7,080.11	7,078.00	7,069.11	7,053.00	7,088.21	7,081.79
Depth (Normal)	(£)	2.29	1.70	1.71	1.16	1.93		1.69	Invert (Start)	£		7,081.49	7,079.31	7,077.70	7,068.81	7,090,07	7,087.91
Froude Number	(Normal)	1.432	2.541	2.507	5.244	1.992		2.553	Elevation Ground	(Start)		7,088.97	7,086.56	7,085.36	7,077.40	7,095.00	7,094.77
Velocity	(trys)	11.50	16.58	16.43	27.41	14.12		16.64	Upstream	Structure	(F)	0.38	0.38	0.38	1.43	2.48	0.38
Length (Unified)	(ft)	138.4	20.8	341.2	155.1	110.4		235.2	Upstream	Structure	Coefficient	0.270	0.270	0.270	1.020	1.770	0.270
Flow / Capacity	(Design) (%)	76.4	47.5	48.1	23.9	58.8		47.3	Upstream	Structure Velocity (In-	Governing) (ft/s)	9.24	11.32	9.24	7.98	9.50	9.24
How	(ds)	76.80	76.80	76.80	76.80	76.80		76.80	Upstream	Structure	Line (In)	7,084.61	7,082.43	7,080.82	7,072.98	7,095.29	7,091.03
Rise	(ft)								Headloss	€		1.80	1.23	7.46	14.85	1.78	6.04
Upstream	Structure	EX. EPC TYPE I MH (SR Ranch EII NO 1)	EPC TYPE I MH	EPC TYPE I MH	EPC TYPE I MH	EX CDOT TYPE D (SR RANCH	EX MH-12 (SR	RANCH FIL NO.1)	Hydraulic Grade	Line (Out)	3	7,082.43	7,080.82	7,072.98	7,056.70	7,091.03	7,084.61
Label		PR11-3	PR11-2	PR11-1	PR11	EX 42"-5		EX 42"-4	Hydraulic Grade	Line (In)	3	7,084.23	7,082.05	7,080.44	7,071.55	7,092.81	7,090.65



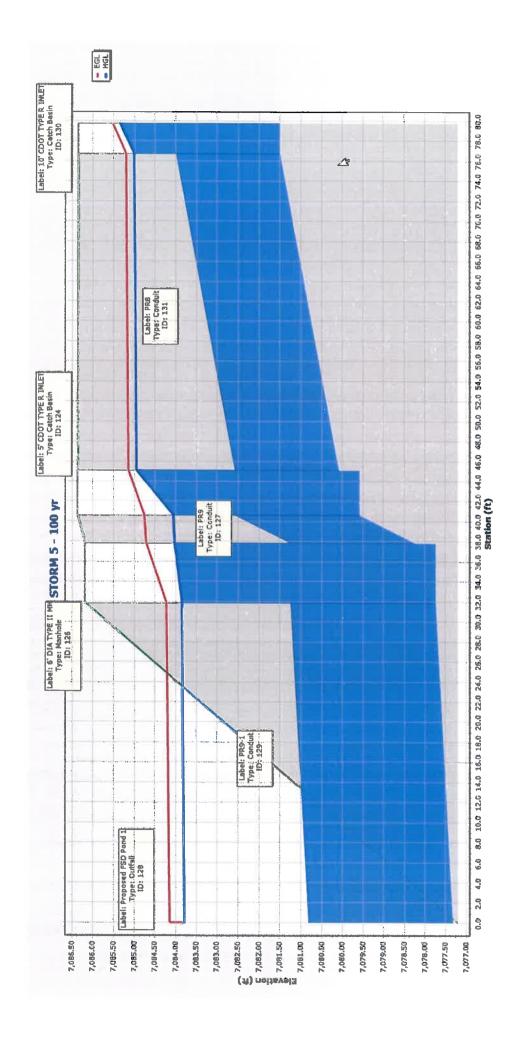
STRM 5,6,7

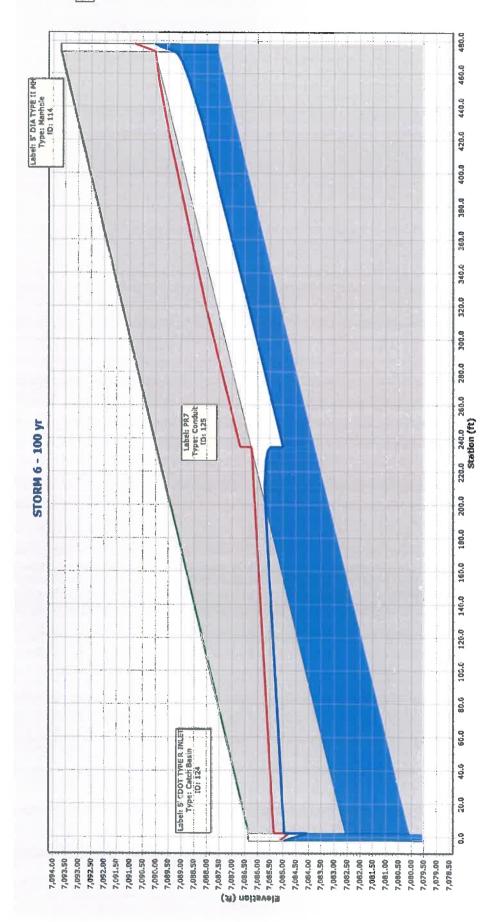


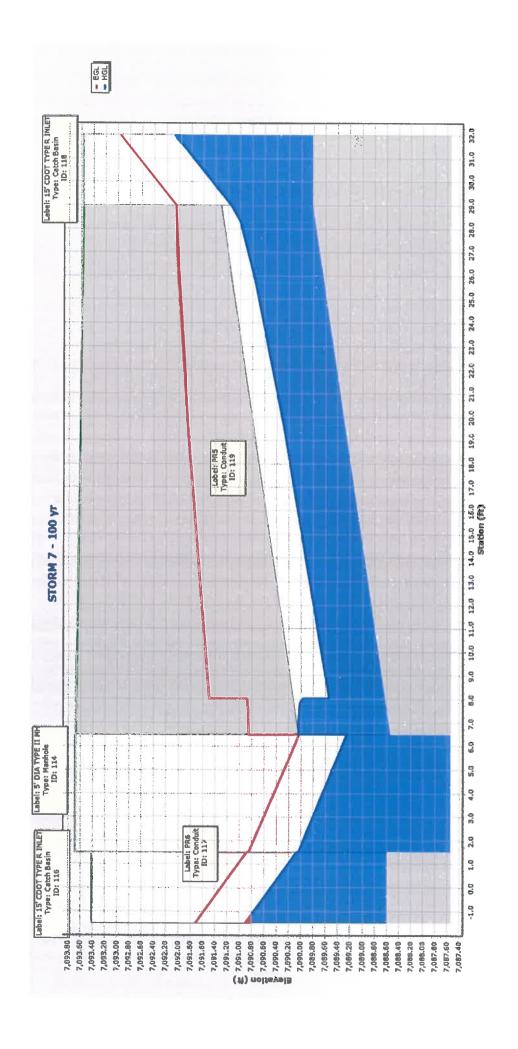
Conduit FlexTable: Table - 1 STRM 5,6,7

Depth (Critical) (ft)	1.34	1.34	1.71	2.24	2.14	1.40	Invert (Stop) (ft)	7,088.54	7,088.54	7,080.07	7,078.23	7,077.31	7,080.07
Depth (Normal) (ft)	1.07	08.0	1.24	0.84	1.60	0.78	Invert (Start) (ft)	7,088.59	7,089.81	7,087.54	7,079.57	7,077.73	7,081.49
Froude Number (Normal)	1.674	2.948	1.867	6.560	1.755	3.114	Elevation Ground (Start) (ft)	7,093.41	7,093.57	7,093.68	7,086.36	7,086.18	7,086.34
Velocity (ft/s)	7.19	13.34	10.43	99'9	4.90	3.50	Upstream Structure Headloss (ft)	0.82	0.92	1.17	0.88	0.18	0.34
How / Capacity Length (Unified) Velocity (ft) (ft)	2.5	26.5	475.5	8.0	34.9	35.4	Upstream Structure Headloss Coefficient	1.020	1.020	1.520	1.280	0.470	1.770
Flow / Capacity (Design)	(%)	55.2	49.2	17.3	42.6	20.9	Upstream Structure Velocity (In- Governing) (ft/s)	7.19	7.62	7.19	3.50	99'9	3.50
Flow (cfs)	12.70	12.70	25.30	47.10	47.10	17.20	Upstream Structure Hydraulic Grade Line (In) (ft)	7,091.28	7,092.07	7,090.43	7,084.94	7,084.02	7,085.34
Rise (ft)							Headloss (ft)	0.04	0.72	4.31	0.04	0.08	90.0
Upstream Structure	15' CDOT TYPE R INLET	15' CDOT TYPE R INLET	5' DIA TYPE II MH	5' CDOT TYPE R INLET	6' DIA TYPE II MH	10' CDOT TYPE R INLET	Hydraulic Grade Line (Out) (ft)	7,090.43	7,090.43	7,084,94	7,084.02	7,083.77	7,084.94
Label	PR6	PR5	PR7	PR9	PR9-1	PR8	Hydraulic Grade Line (In) (ft)	7,090.47	7,091.15	7,089.25	7,084.06	7,083.85	7,085.01

Storm 5, Storm 6, Storm 7.stsw 2/21/2019







STRM 4 POND 1 OUTFALL INDEX MAP

Outlet Structure (FSD Pond 1)

PR10

Sand Creek Channel

Conduit FlexTable: STRM 4 POND 1 7-30-19

Label	ID	Upstream Structure	Flow (cfs)	Flow / Capacity (Design) (%)	Length (Unified) (ft)	Velocity (ft/s)	Froude Number (Normal)	Depth (Normal) (ft)	Depth (Critical) (ft)	Energy Grade Line (In) (ft)	Energy Grade Line (Out) (ft)	Hydraulic Grade Line (In) (ft)	Hydraulic Grade Line (Out) (ft)	Headloss (ft)	Upstream Structure Hydraulic Grade Line (In) (ft)
PR10	129	Outlet Structure (FSD Pond 1)	23.50	40.3	78.2	17.56	3.772	0.88	1.72	7,078.68	7,074.39	7,077.64	7,069.91	7.73	7,079.20
Upstream Structure Velocity (In- Governing)	Upstream Structure Headloss Coefficient	Upstream Structure Headloss (ft)	Elevation Ground (Start) (ft)	Invert (Start) (ft)	Invert (Stop) (ft)										

(ft/s)

8.17

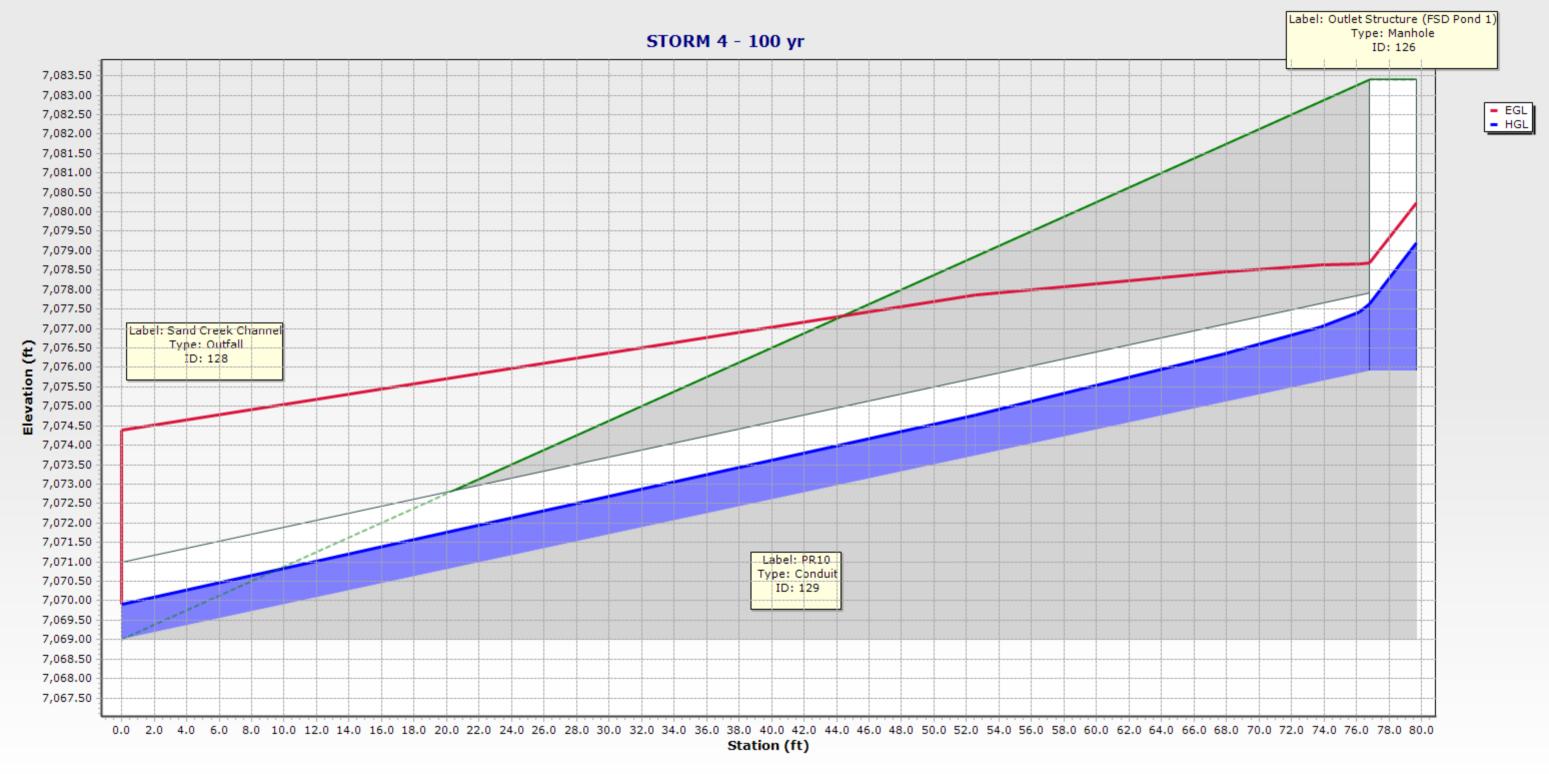
1.500

1.56

7,083.40

7,075.92

7,069.00

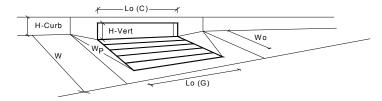


ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) Project: Enter Your Project Name Here Inlet ID: Inlet DP 7 CRONN Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb 8.0 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) 0.020 ft/ft Manning's Roughness Behind Curb (typically between 0.012 and 0.020) 0.020 Height of Curb at Gutter Flow Line H_{CURB} 6.00 Distance from Curb Face to Street Crown T_{CROWN} 17.0 Gutter Width w: 2.00 Street Transverse Slope S_X : 0.020 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) S_W 0.083 ft/ft S_o : Street Longitudinal Slope - Enter 0 for sump condition 0.000 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) n_{STREET} : 0.020 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm 17.0 17.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm 5.1 Check boxes are not applicable in SUMP conditions MINOR STORM Allowable Capacity is based on Depth Criterion Minor Storm Major Storm

SUMP

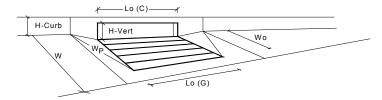
SUMP

MAJOR STORM Allowable Capacity is based on Depth Criterion



Design Information (Input) CDOT Type R Curb Opening	-		MINOR	MAJOR	_
Type of Inlet		Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a' fro	m above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)		No =	2	2	
Water Depth at Flowline (outside of local depression)		Ponding Depth =	5.1	7.8	inches
Grate Information			MINOR	MAJOR	Override Depths
Length of a Unit Grate		L ₀ (G) =	N/A	N/A	feet
Width of a Unit Grate		W _o =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)		A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)		$C_f(G) =$	N/A	N/A	Ī
Grate Weir Coefficient (typical value 2.15 - 3.60)		C _w (G) =	N/A	N/A	1
Grate Orifice Coefficient (typical value 0.60 - 0.80)		C _o (G) =	N/A	N/A	7
Curb Opening Information		_	MINOR	MAJOR	_
Length of a Unit Curb Opening		L ₀ (C) =	5.00	5.00	feet
Height of Vertical Curb Opening in Inches		H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches		H _{throat} =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)		Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)		W _p =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)		$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)		C _w (C) =	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)		C _o (C) =	0.67	0.67]
Low Head Performance Reduction (Calculated)			MINOR	MAJOR	
Depth for Grate Midwidth		d _{Grate} =	N/A	N/A	ft
Depth for Curb Opening Weir Equation		d _{Curb} =	0.26	0.48	ft
Combination Inlet Performance Reduction Factor for Long Inlets		RF _{Combination} =	0.48	0.74	
Curb Opening Performance Reduction Factor for Long Inlets		RF _{Curb} =	0.88	1.00	
Grated Inlet Performance Reduction Factor for Long Inlets		RF _{Grate} =	N/A	N/A	
		_	MINOR	MAJOR	_
Total Inlet Interception Capacity (assumes clogge	l condition)	Q _a =	6.7	18.7	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK		Q PEAK REQUIRED =	5.7	13.8	cfs

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) Project: **Enter Your Project Name Here** Inlet ID: Inlet DP 8 CRONN Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb 8.0 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) 0.020 ft/ft Manning's Roughness Behind Curb (typically between 0.012 and 0.020) 0.020 Height of Curb at Gutter Flow Line H_{CURB} 6.00 Distance from Curb Face to Street Crown T_{CROWN} 17.0 Gutter Width w: 2.00 Street Transverse Slope S_X : 0.020 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) S_W 0.083 ft/ft S_o : Street Longitudinal Slope - Enter 0 for sump condition 0.000 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) n_{STREET} : 0.020 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm 17.0 17.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm 5.1 Check boxes are not applicable in SUMP conditions MINOR STORM Allowable Capacity is based on Depth Criterion Minor Storm Major Storm MAJOR STORM Allowable Capacity is based on Depth Criterion SUMP SUMP



Design Information (Input) CDOT Type R Curb Opening ▼		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	2	2	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	5.1	7.8	inches
Grate Information		MINOR	MAJOR	Override Depths
Length of a Unit Grate	L ₀ (G) =	N/A	N/A	feet
Width of a Unit Grate	W _o =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	C _f (G) =	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C _w (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	C _o (G) =	N/A	N/A	
Curb Opening Information	_	MINOR	MAJOR	_
Length of a Unit Curb Opening	L ₀ (C) =	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H _{throat} =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W _p =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	C _w (C) =	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	C _o (C) =	0.67	0.67]
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d _{Curb} =	0.26	0.48	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	0.48	0.74	
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	0.88	1.00	
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A	
		MINOR	MAJOR	_
Total Inlet Interception Capacity (assumes clogged condition)	$Q_a =$	6.7	18.7	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	4.9	11.8	cfs

Version 4.05 Released March 2017 ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) Project: **Enter Your Project Name Here** Inlet ID: Inlet DP 9 CRONN Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb 8.0 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) 0.020 ft/ft Manning's Roughness Behind Curb (typically between 0.012 and 0.020) 0.020 Height of Curb at Gutter Flow Line H_{CURB} 6.00 Distance from Curb Face to Street Crown T_{CROWN} 17.0 Gutter Width w: 2.00 Street Transverse Slope S_X : 0.020 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) S_W 0.083 ft/ft S_o : Street Longitudinal Slope - Enter 0 for sump condition 0.000 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) n_{STREET} : 0.020 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm 17.0 17.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm 5.1 Check boxes are not applicable in SUMP conditions

Minor Storm

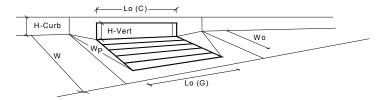
SUMP

Major Storm

SUMP

MINOR STORM Allowable Capacity is based on Depth Criterion

MAJOR STORM Allowable Capacity is based on Depth Criterion

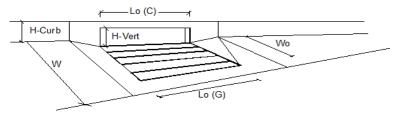


Design Information (Input)		MINOR	MAJOR	
Type of Inlet CDOT Type R Curb Opening	Type =	CDOT Type F	Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	5.1	7.8	inches
Grate Information		MINOR	MAJOR	Override Depths
Length of a Unit Grate	L ₀ (G) =	N/A	N/A	feet
Width of a Unit Grate	W _o =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_f(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C_w (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	C ₀ (G) =	N/A	N/A	
Curb Opening Information		MINOR	MAJOR	_
Length of a Unit Curb Opening	L ₀ (C) =	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H _{throat} =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W _p =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	C _o (C) =	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d _{Curb} =	0.26	0.48	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	0.65	1.00	
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	1.00	1.00	
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A	
		MINOR	MAJOR	
Total Inlet Interception Capacity (assumes clogged condition)	$Q_a =$	3.7	9.0	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q _{PEAK REQUIRED} =	2.2	5.4	cfs

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) Project: **Enter Your Project Name Here** Inlet ID: Inlet DP 10 CRONN Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb 8.0 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) 0.020 ft/ft Manning's Roughness Behind Curb (typically between 0.012 and 0.020) 0.020 Height of Curb at Gutter Flow Line H_{CURB} 6.00 Distance from Curb Face to Street Crown 17.0 T_{CROWN} Gutter Width w: 2.00 S_X : Street Transverse Slope 0.020 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) S_W 0.083 ft/ft S_o : Street Longitudinal Slope - Enter 0 for sump condition 0.022 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) n_{STREET} : 0.020 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm 17.0 17.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm 5.1 Allow Flow Depth at Street Crown (leave blank for no) check = yes MINOR STORM Allowable Capacity is based on Depth Criterion Minor Storm Major Storm MAJOR STORM Allowable Capacity is based on Depth Criterion 29.1 Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Manage

lajor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Manager

INLET ON A CONTINUOUS GRADE

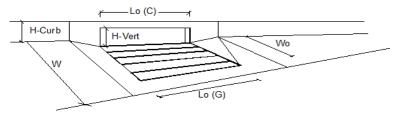


Design Information (Input) CDOT Type R Curb Opening		MINOR	MAJOR	_
Type of Inlet	Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L ₀ =	15.00	15.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	9.1	12.7	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.3	2.9	cfs
Capture Percentage = Q _a /Q _o =	C% =	97	82	%

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) Project: **Enter Your Project Name Here** Inlet ID: Inlet DP 11 CRONN Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb 8.0 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) 0.020 ft/ft Manning's Roughness Behind Curb (typically between 0.012 and 0.020) 0.020 Height of Curb at Gutter Flow Line H_{CURB} 6.00 Distance from Curb Face to Street Crown 17.0 T_{CROWN} Gutter Width w: 2.00 S_X : Street Transverse Slope 0.020 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) S_W 0.083 ft/ft S_o : Street Longitudinal Slope - Enter 0 for sump condition 0.022 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) n_{STREET} : 0.020 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm 17.0 17.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm 5.1 Allow Flow Depth at Street Crown (leave blank for no) check = yes MINOR STORM Allowable Capacity is based on Depth Criterion Minor Storm Major Storm MAJOR STORM Allowable Capacity is based on Depth Criterion 29.1 Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Manage

lajor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Manager

INLET ON A CONTINUOUS GRADE



Design Information (Input)		MINOR	MAJOR	
Type of Inlet CDOT Type R Curb Opening	Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	15.00	15.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	1.9	12.7	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	2.9	cfs
Capture Percentage = Q _a /Q _o =	C% =	100	82	%

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) Project: Enter Your Project Name Here Inlet ID: Inlet DP 12 CRONN Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb 8.0 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) 0.020 ft/ft Manning's Roughness Behind Curb (typically between 0.012 and 0.020) 0.020 Height of Curb at Gutter Flow Line H_{CURB} 6.00 Distance from Curb Face to Street Crown T_{CROWN} 17.0 Gutter Width w: 2.00 Street Transverse Slope S_X : 0.020 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) S_W 0.083 ft/ft S_o : Street Longitudinal Slope - Enter 0 for sump condition 0.000 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) n_{STREET} : 0.020 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm 17.0 17.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm 5.1 Check boxes are not applicable in SUMP conditions

Minor Storm

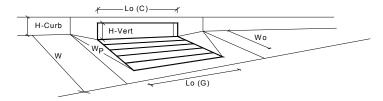
SUMP

Major Storm

SUMP

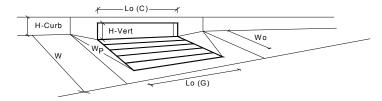
MINOR STORM Allowable Capacity is based on Depth Criterion

MAJOR STORM Allowable Capacity is based on Depth Criterion



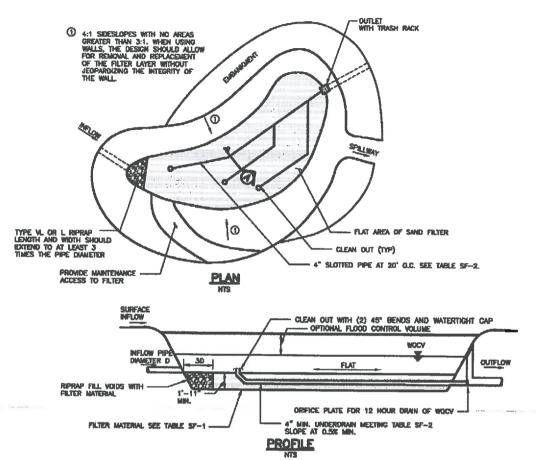
Design Information (Input) CDOT Type R Curb Opening ▼		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	7
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	2	2	
Nater Depth at Flowline (outside of local depression)	Ponding Depth =	5.1	7.8	inches
Grate Information		MINOR	MAJOR	Override Depths
ength of a Unit Grate	L ₀ (G) =	N/A	N/A	feet
Nidth of a Unit Grate	W _o =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_f(G) =$	N/A	N/A	Ī
Grate Weir Coefficient (typical value 2.15 - 3.60)	C _w (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	C _o (G) =	N/A	N/A	
Curb Opening Information	_	MINOR	MAJOR	_
ength of a Unit Curb Opening	L ₀ (C) =	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H _{throat} =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W _p =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	C _w (C) =	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	C _o (C) =	0.67	0.67]
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d _{Curb} =	0.26	0.48	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	0.48	0.74	
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	0.88	1.00	
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A]
	_	MINOR	MAJOR	_
Total Inlet Interception Capacity (assumes clogged condition)	$Q_a =$	6.7	18.7	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	6.2	17.2	cfs

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) Project: Enter Your Project Name Here Inlet ID: Inlet DP 13 CRONN Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb 8.0 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) 0.020 ft/ft Manning's Roughness Behind Curb (typically between 0.012 and 0.020) 0.020 Height of Curb at Gutter Flow Line H_{CURB} 6.00 Distance from Curb Face to Street Crown T_{CROWN} 17.0 Gutter Width w: 2.00 Street Transverse Slope S_X : 0.020 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) S_W 0.083 ft/ft S_o : Street Longitudinal Slope - Enter 0 for sump condition 0.000 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) n_{STREET} : 0.020 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm 17.0 17.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm 5.1 Check boxes are not applicable in SUMP conditions MINOR STORM Allowable Capacity is based on Depth Criterion Minor Storm Major Storm MAJOR STORM Allowable Capacity is based on Depth Criterion SUMP SUMP

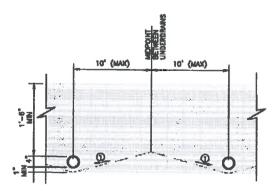


Design Information (Input)	ODOT To a DiOurk On suring		MINOR	MAJOR	
Type of Inlet	CDOT Type R Curb Opening	Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to co	ontinuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or C	urb Opening)	No =	1	1	
Water Depth at Flowline (outside	of local depression)	Ponding Depth =	5.1	7.8	inches
Grate Information			MINOR	MAJOR	Override Depths
Length of a Unit Grate		L ₀ (G) =	N/A	N/A	feet
Width of a Unit Grate		W _o =	N/A	N/A	feet
Area Opening Ratio for a Grate (t	ypical values 0.15-0.90)	A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grat	e (typical value 0.50 - 0.70)	$C_f(G) =$	N/A	N/A	
Grate Weir Coefficient (typical va	lue 2.15 - 3.60)	C_w (G) =	N/A	N/A	
Grate Orifice Coefficient (typical v	/alue 0.60 - 0.80)	C ₀ (G) =	N/A	N/A	
Curb Opening Information			MINOR	MAJOR	_
Length of a Unit Curb Opening		L _o (C) =	5.00	5.00	feet
Height of Vertical Curb Opening i	n Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Ir	nches	H _{throat} =	6.00	6.00	inches
Angle of Throat (see USDCM Fig	ure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (t	ypically the gutter width of 2 feet)	W _p =	2.00	2.00	feet
Clogging Factor for a Single Curb	Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (t	ypical value 2.3-3.7)	C _w (C) =	3.60	3.60	
Curb Opening Orifice Coefficient	(typical value 0.60 - 0.70)	C _o (C) =	0.67	0.67]
Low Head Performance Reduct	tion (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth		d _{Grate} =	N/A	N/A	ft
Depth for Curb Opening Weir Equ	uation	d _{Curb} =	0.26	0.48	ft
Combination Inlet Performance R	leduction Factor for Long Inlets	RF _{Combination} =	0.65	1.00	
Curb Opening Performance Redu	uction Factor for Long Inlets	RF _{Curb} =	1.00	1.00	
Grated Inlet Performance Reduct	ion Factor for Long Inlets	RF _{Grate} =	N/A	N/A]
			MINOR	MAJOR	_
Total Inlet Interception Ca	apacity (assumes clogged condition)	Q _a =	3.7	9.0	cfs
Inlet Capacity IS GOOD for Min	or and Major Storms(>Q PEAK)	Q _{PEAK REQUIRED} =	1.2	5.9	cfs

EDB AND SFB DETAILS



NOTE: THS DETAIL SHOWS A PARTIAL INFILTRATION SECTION. FOR FULL INFILTRATION ELIMINATE UNDERDRAIN AND PROVIDE 1'-6' OF FILTER MATERIAL FOR NO INFILTRATION PROVIDE IMPERIMEMBLE MEMBRANE SECURED TO CAST—IN-PLACE CONCRETE WALL SEE DETAILS SF-2 AND SF-3.



() SLOPE (STRAIGHT GRADE) SUBGRADE (2—10%) TO UNDERDRAIN TO REDUCE SATURATED SOIL CONDITIONS BETWEEN STORM EVENTS (OPTIONAL)



Figure SF-1. Sand Filter Plan and Sections

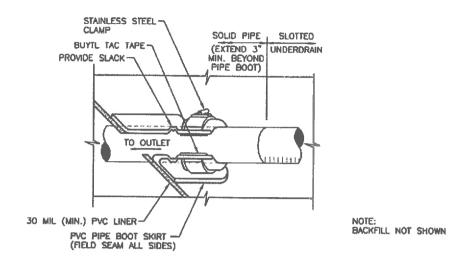


Figure SF-2. Geomembrane Liner/Underdrain Penetration Detail

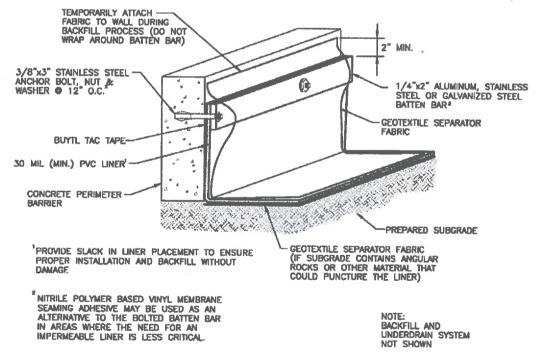


Figure SF-3. Geomembrane Liner/Concrete Connection Detail

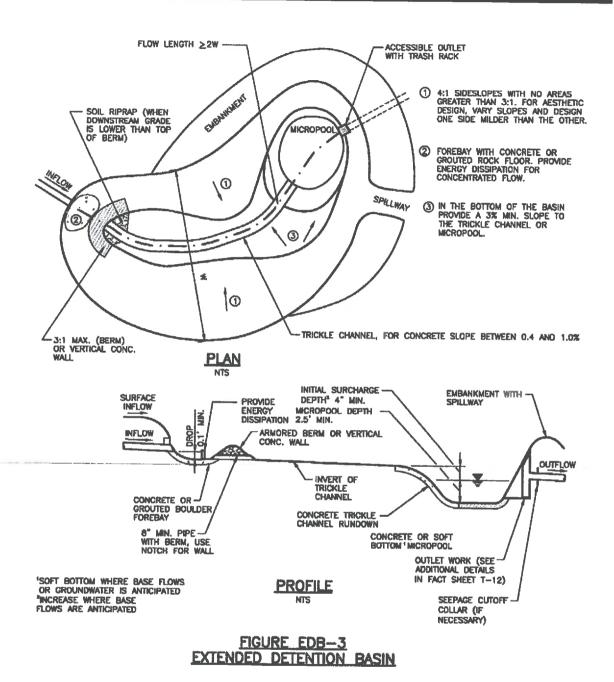
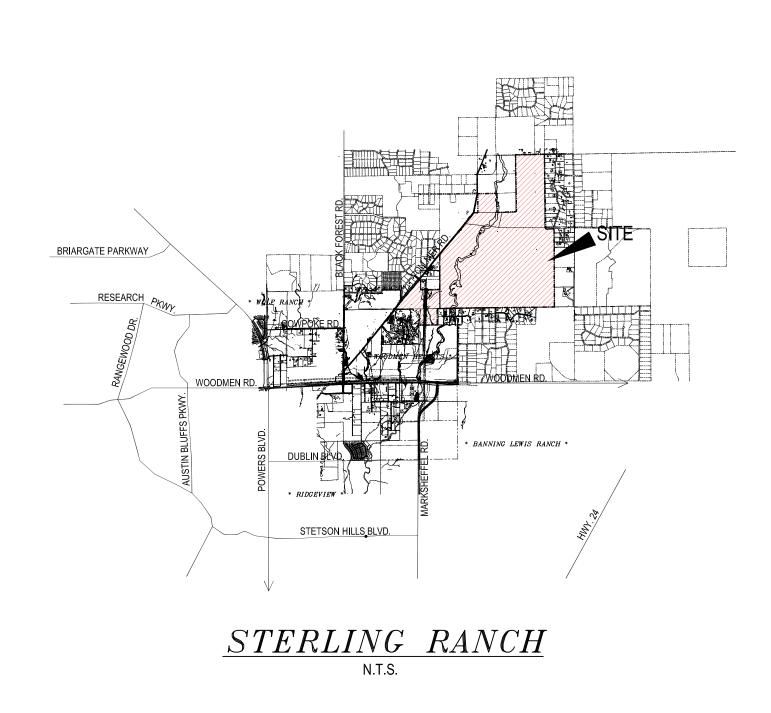
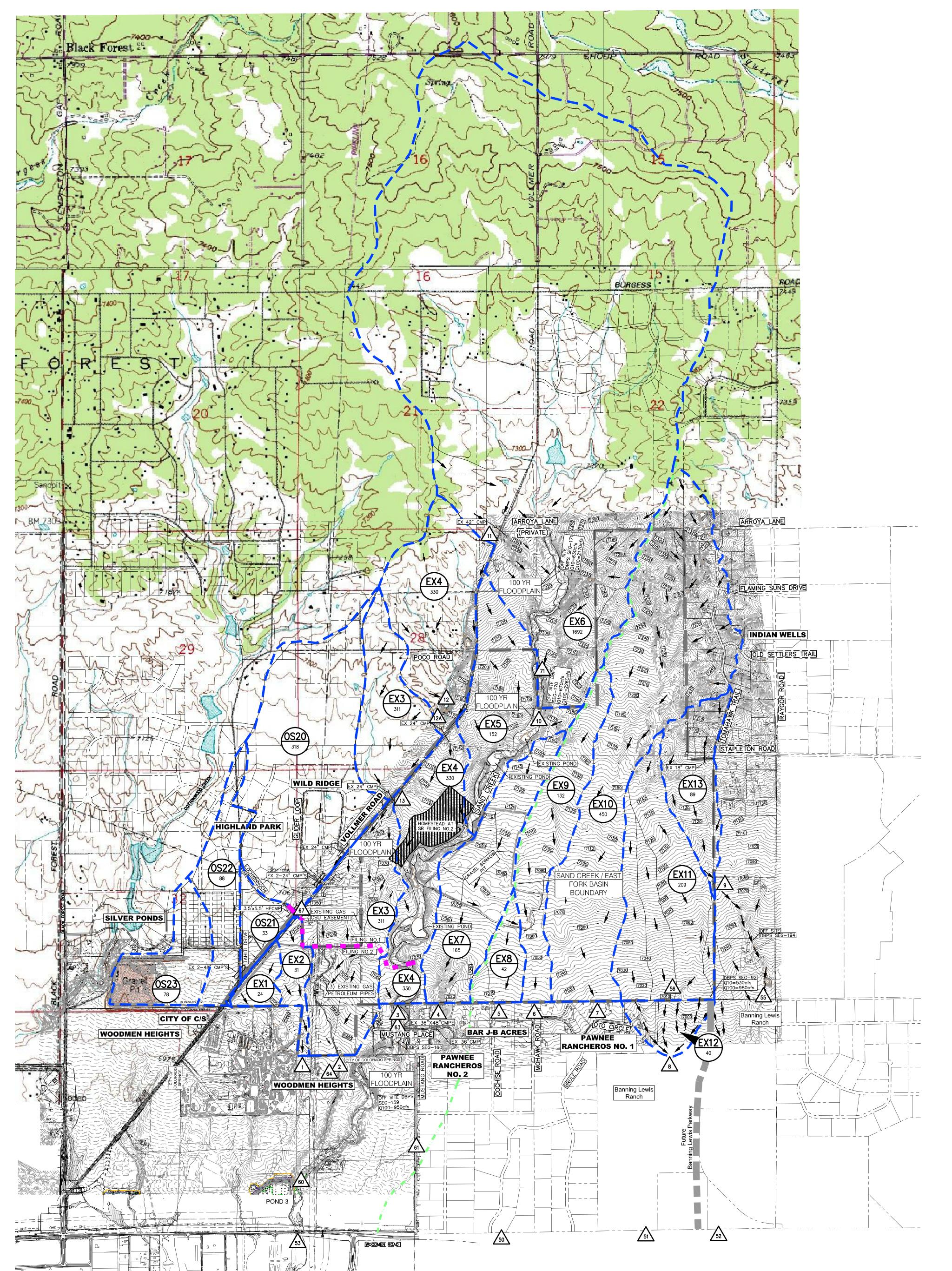


Figure EDB-3. Extended Detention Basin (EDB) Plan and Profile

Additional Details are provided in BMP Fact Sheet T-12. This includes outlet structure details including orifice plates and trash racks.

HISTORIC, EXISTING AND PROPOSED DRAINAGE MAPS





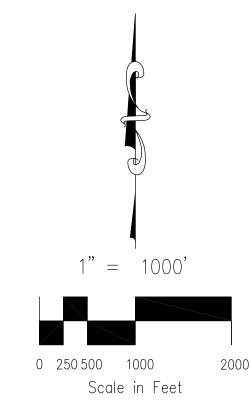
HISTORIC CONDITION

В	ASIN S	UMMAR`	Y
BASIN	AREA (acres)	Q ₅ (CFS)	Q100 (CFS)
EX-1	24	3	40
EX-2	31	3	45
EX-3	311	49	341
EX-4	330	71	352
EX-5	152	14	209
EX-6	1692	118	2168
EX-7	165	12	197
EX-8	42	4	64
EX-9	132	11	149
EX-10	450	48	474
EX-11	209	17	261
EX-12	40	5	65
EX-13	89	6	114
OS-20	318	61	310
OS-21	33	8	38
OS-22	88	18	91
OS-23	78	34	84

* NOTE: BASIN S OS-22 & OS-23 NOT PART OF THIS REPORT. FLOWS FOLLOW HISTORIC PATTERNS ON THE WEST SIDE OF VOLLMER ROAD.

HISTORIC CONDITION

		<u> </u>	<u> </u>	<u>ST NIC</u>)	
DESIGN POINT	SQ. MI.	Q ₅ (CFS)	Q ₁₀₀ (CFS)	SQ. MI.	DBPS Q ₁₀₀	DBPS DP/ID
1	0.09	5	84			,
2	0.49	49	341	0.74	465	64
3	0.52	139	2610	4.33	2552	63
4	0.26	12	197			
5	0.07	4	64			
6	0.21	11	149			
7	0.70	48	474			
8	0.39	18	305			
9	0.14	6	114			
10	2.64	122	2245	3.27	2245	71
11	0.09	5	83			
12A	0.01	3	16			
12	0.27	10	200			
13	0.17	6	126			
* NOTE:		I A D [- NOT	0.48	#	55
INO IL.	SQ. M Stant		E NOT ACH	0.53	1210	56
DESIG			-DBPS	5.38	2629	60



<u>LEGEND</u>





EXISTING FLOW RELEASE POINT



FILING NO.1 & NO.2 DIVISION LINE PROPERTY BOUNDARY -----6920----- EXISTING CONTOUR

CHECKED BY: VAS VERT: N/A

CULVERT PIPE

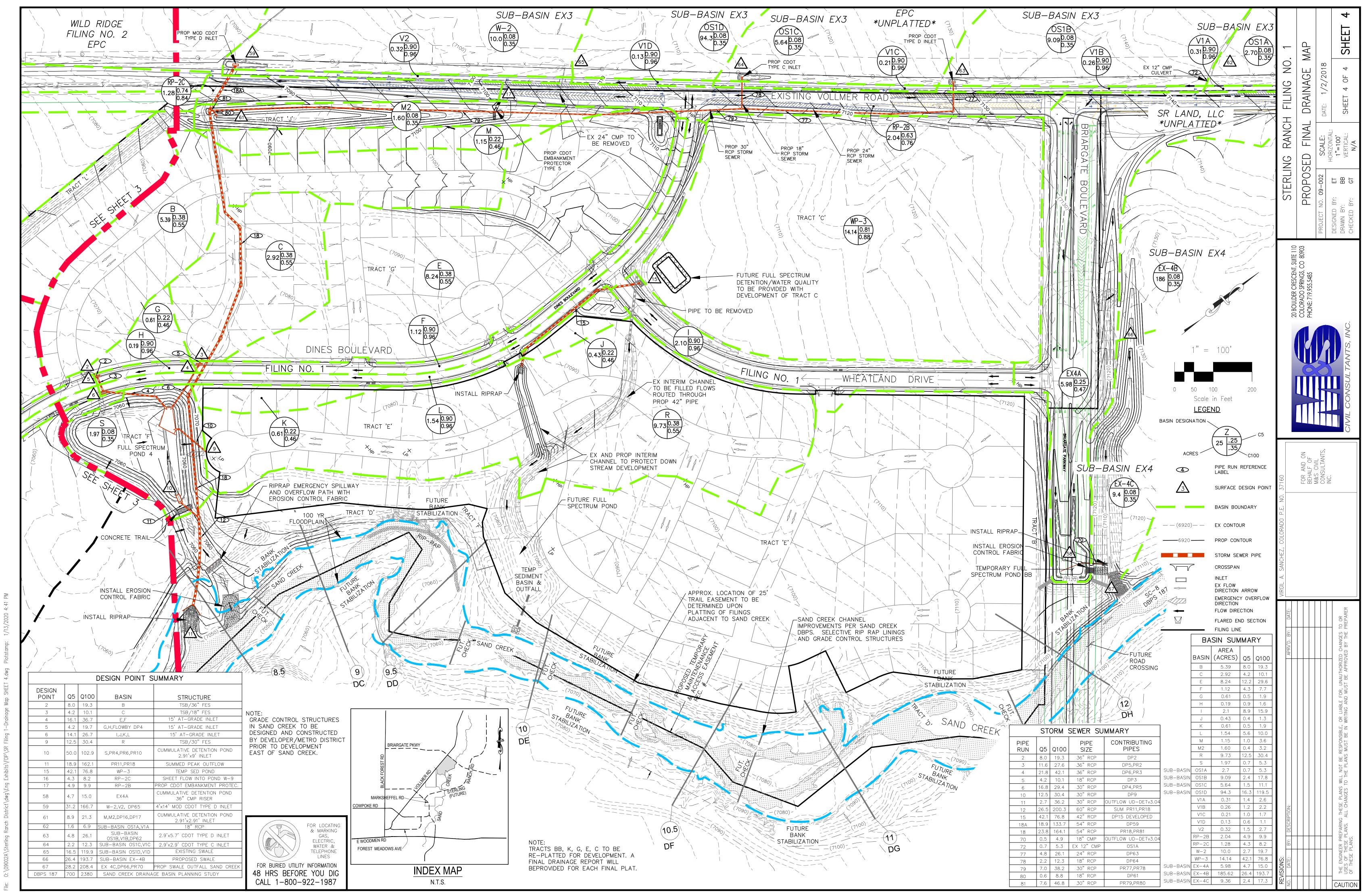


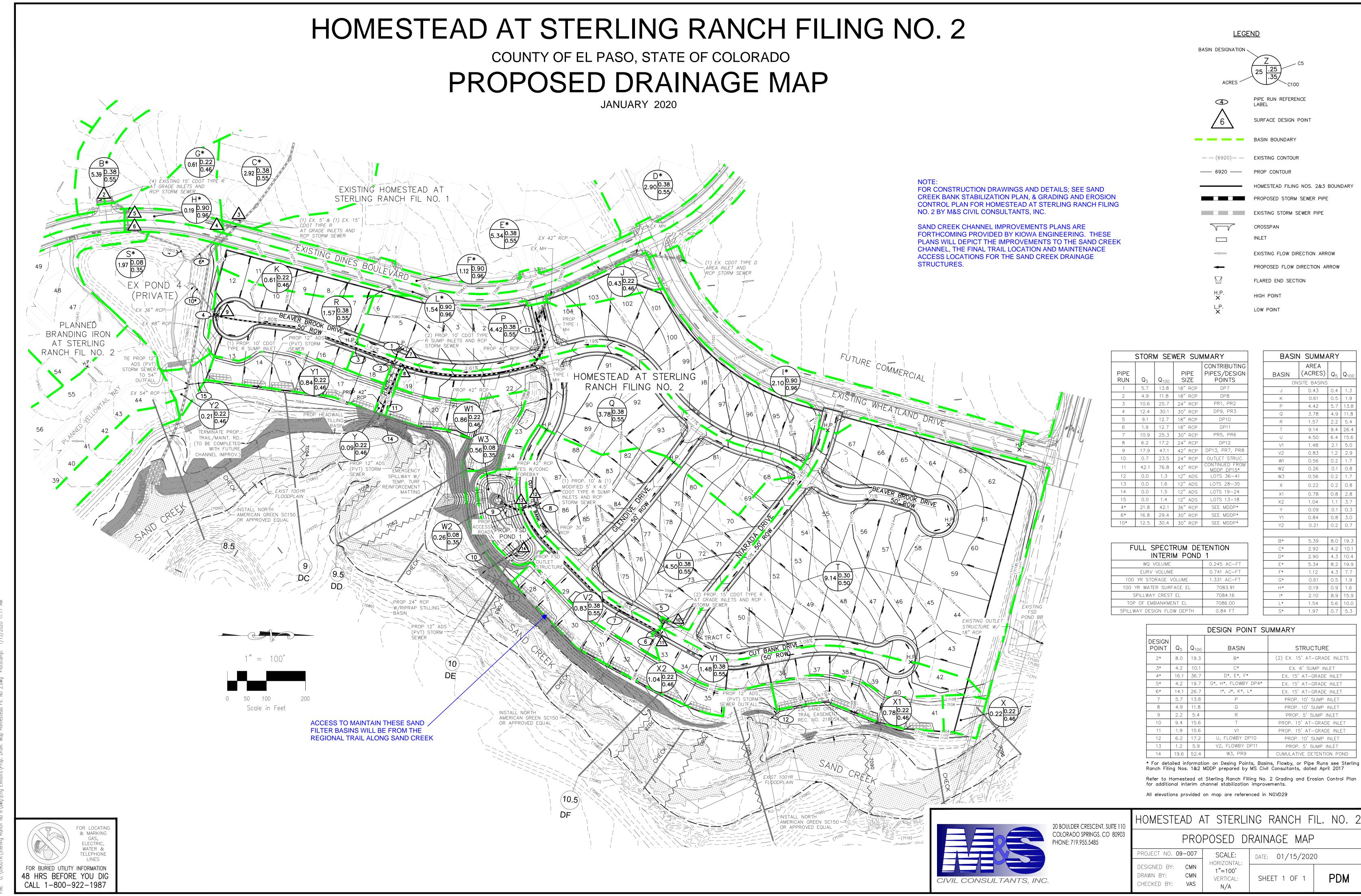
STERLING RANCH

HISTORIC - DRAINAGE MAP

PROJECT NO. 09-002 | FILE: O: \\dwg\Eng Exhibits\MDDP HISTORIC DATE: 2/6/17 DESIGNED BY: VAS VAS | HORIZ: 1"=1000' DRAWN BY:

SHEET 1 OF 1





File: 0:\09007A\Sterling Banch No 6\dwa\Fna Fxhibits\Prop. Drain. Map Homestead Fil. No 2.dwa Plotstamp: