FINAL DRAINAGE REPORT FOR COLORADO CENTRE METROPOLITAN DISTRICT ADMINISTRATION BUILDING

PCD FILE # PPR-21-51

PREPARED BY

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PREPARED FOR

Colorado Centre Metropolitan District 4770 Horizonview Drive Colorado Springs, CO 80925

April 2023

Project 247.07





ENGINEER'S STATEMENT

This report and plan for the drainage design of Colorado Centre Metropolitan District Administration Building, was prepared by me (or under my direct supervision) and is correct to the best of my knowledge and belief. Said report and plan has been prepared according to the criteria established by the County for drainage reports and said report is in conformity with the master plan of the drainage basin. I understand that El Paso County does not, and will not, assume liability for drainage facilities designed by others. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.

Richard Gallegos, P.E.

Registered Professional Engineer State of Colorado No. 36247

OWNER/DEVELOPER'S STATEMENT

THE SCIONAL ENGINE

3624

Jackie McClintock, President Colorado Centre Metropolitan District 4770 Horizonview Drive, Colorado Springs, CO 80925

County Engineer/ECM Administrator

EL PASO COUNTY STATEMENT

Filed in accordance with the requirements of the County Engineering Criteria Manual and Land De	e Drainage Criteria Manual, Volumes 1 and 2, El Pa evelopment Code as amended.	S
Joshua Palmer, P.E.	Date	



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1.0 PURPOSE

This drainage report is for the design of the Colorado Centre Metropolitan District Administration Building. The site is located at 9696 Flagstone Street, Colorado Springs, Colorado in central El Paso County. See Vicinity Map in the Appendix below for reference. It is further described as the Northeast One-Quarter of the Southwest One-Quarter of Section 3, Township 15 South, Range 65 West of the 6th P.M.

One County-approved Drainage Report was found within the County's files that included the project site:

 Drainage Report for Colorado Centro Metropolitan District Water Treatment Facility by JDS-Hydro Consultants Inc. approved in August 2015.

This 7.73-acre site is located within the Jimmy Camp Creek – FOFO2000 basin. Work will include the construction of a 4,542 square foot (sf) administration building, asphalt driveway, and a parking lot. In order to accommodate an area of disturbance greater than 1 acre, a 0.207-acre-foot detention basin will be constructed in the southwest portion of the site to detain all flows directed to the south. No portion of the site is located within a FEMA designated 100-year floodplain per Map No. 08041C0769G that was effective on December 7th, 2018.

2.0 SOIL CONDITIONS

According to the El Paso County Area Soil Survey, the soil on the site is classified as follows:

SOIL#	SOIL TYPE	HYDROLOGIC	PERCENT OF SITE
		CLASSIFICATION	
28	Ellicot Loamy Coarse Sand, 0 to 5	Α	0.0%
	Percent Slopes		
101	Ustic Torrifluvents, Loamy	В	100.0%

The Ustic Torrifluvents soil can be described as having a high permeability, low surface runoff, and slight hazard of erosion. The Ellicot soils is described as having very high permeability and very low surface runoff. The hydrologic soil classification used for this study is 'B'. See Soils Map in the Appendix for reference.

3.0 HYDROLOGIC CRITERIA

The methodology utilized for this report is in accordance with the *El Paso County Drainage Criteria Manual*. All references from the *El Paso County Drainage Criteria Manual* can be found in Appendix C. The Rational Method for computation of runoff was used.



Q = cia Where

Q = maximum rate of runoff in cubic feet per second

c = runoff coefficient representing drainage area characteristics

i = average rainfall intensity, in inches per hour, for the duration required for the runoff

to become established

a = drainage basin size in acres

The storm recurrence intervals used for this study were the 5-year storm and the 100-year storm. The detention discharge for the proposed 0.207-acre-foot Full Spectrum Extended Detention Basin is 0.5 cfs for the 5-year storm and 5.5 cfs for the 100-year storm. The Colorado Urban Hydrograph Procedure (CUHP) was used to route flows through the proposed private detention basin. This procedure is described in more detail in the *Mile High Flood District Urban Storm Drainage Criteria Manual Volume 1*, shown below in Appendix C – Colorado Urban Hydrograph Procedure Summary.

The Mile High Flood District – Detention Version 4.05 (January 2022) spreadsheet was used to determine the required detention basin storage volume and outlet structure design. ManningSolver Version 1.019, also, was used in this analysis to calculate the Manning's normal depth within the pond inlet channel.

4.0 EXISTING DRAINAGE CONDITIONS

The overall site consists of 7.73 acres. The site includes an existing 3725 sf water treatment plant and an asphalt driveway. The areas of the site not covered by the water treatment plant or asphalt driveway are covered with nearly bare ground. These undeveloped areas include slopes that range from 0.5% to 19.3%. The overall existing site is 4.6% impervious. See Existing Drainage Map for reference.

Flows from Sub-basin Aex through Sub-basin Dex are tributary to the Jimmy Camp Creek (FOFO2000) basin.

Sub-basin Aex contains 2.05 acres and drains south towards a grated inlet in the southwest corner of the site. This sub-basin produces existing flows of 0.6 cfs for the 5-year storm and 3.4 cfs for the 100-year storm. Flows from Aex are ultimately drained by flowing to an existing graged inlet near Flagstone Street, and discharged to the existing Flagstone Channel located to the east via a 24" CMP pipe. At the 24" CMP discharge point, a riprap pad was installed. Based on site observations, the existing riprap is adequate to protect the outfall point and can be considered scour stable. The scour stable assessment is based upon deposition of sediment at the outfall point, and the establishment of vegetation, both of which would not occur if the discharge point was unstable. A photograph showing the outfall point is included within the appendix of this report. As part of the project, the sediment and any excessive vegetation should be removed.

Sub-basin Bex contains 0.17 acres and drains south along East Anvil Drive. This sub-basin produces existing flows of 0.8 cfs for the 5-year storm and 1.5 cfs for the 100-year storm. These flows move south into and along curb and gutter as channelized flow.



Sub-basin Cex contains 2.87 acres and drains east towards Jimmy Camp Creek. This sub-basin produces existing flows of 1.0 cfs for the 5-year storm and 5.4 cfs for the 100-year storm. These flows sheetflow to the east.

Sub-basin Dex contains 0.71 acres and drains east towards Jimmy Camp Creek. It produces flows of 0.2 cfs for the 5-year storm and 1.5 cfs for the 100-year storm. These flows sheetflow to the east, ultimately ending up in Jimmy Camp Creek.

Sub-basin Eex contains 1.65 acres and drains east towards Jimmy Camp Creek. It produces flows of 0.4 cfs for the 5-year storm and 2.8 cfs for the 100-year storm. These flows sheetflow to the east into Jimmy Camp Creek.

Sub-basin Fex contains 0.09 acres and drains northeast into Jimmy Camp Creek. It produces flows of less than 0.1 cfs for the 5-year storm and 0.3 cfs for the 100-year storm. These flows sheetflow to the east into Jimmy Camp Creek.

Sub-basin Gex contains 0.07 acres and drains south towards Flagstone Street. It produces flows of less than 0.1 cfs for the 5-year storm and 0.2 cfs for the 100-year storm. These flows sheetflow to the south onto Flagstone Street.

Sub-basin OS1 contains 0.50 acres and drains southwest towards Sub-basin Aex. It produces flows of 0.1 cfs for the 5-year storm and 0.9 cfs for the 100-year storm. These flows sheetflow to the southwest into Sub-basin Aex.

Sub-basin OS2 contains 0.37 acres and drains southeast towards Sub-basin Eex. It produces flows of 0.1 cfs for the 5-year storm and 0.8 cfs for the 100-year storm. These flows sheetflow to the southeast into Sub-basin Eex.

Sub-basin OS3 contains 0.01 acres and drains east towards Sub-basin Aex. It produces flows of less than 0.1 cfs for the 5-year storm and less than 0.1 cfs for the 100-year storm. These flows sheetflow to the east into Sub-basin Aex.

The estimated runoff amounts produced for the project under Existing Conditions are shown in Table 1 below.

TABLE 1 – EXISTING CONDITIONS											
Sub-basin Q_5 (CFS) Q_{100} (CFS)											
Aex	0.6	3.4									
Bex	0.8	1.5									
Cex	1.0	5.4									
Dex	0.2	1.5									
Eex	0.4	2.8									
Fex	<0.1	0.3									
Gex	<0.1	0.2									
0\$1	0.1	0.9									
OS2	0.1	0.8									
OS3	<0.1	<0.1									



5.0 DEVELOPED DRAINAGE CONDITIONS

The overall site consists of 7.73 acres, of which 2.65 acres will be disturbed as part of this project. A 4,542 sf administration building and asphalt driveway is proposed on the west side of the site. A 0.20-acre-foot Full Spectrum Extended Detention basin size will accommodate the area of disturbance greater than 1 acre. Proposed Conditions Map is located below in the Back Pocket for reference. Proposed site imperviousness is 19.6%, versus 4.6% in the existing conditions. Proposed flows are tributary to the Jimmy Camp Creek Basin (FOFO2000).

Sub-basin A contains 2.78 acres and south towards a 0.20-acre-foot Full Spectrum Extended Detention Basin located in the southwest corner of the site. It produces flows of 3.7 cfs for the 5-year storm and 9.1 cfs for the 100-year storm. These flows sheetflow to the south into the proposed 0.20-acre-foot Full Spectrum Extended Detention Basin. A portion of these flows drain through an existing 4' wide curb opening located on the along East Anvil Drive. A conservative approach was used in calculating the curb opening capacity and the total 100-year flow of 9.1 cfs was used. The 9.1 cfs accounts for 0.33 feet of depth, with minimum of 0.5' of freeboard. No flows will bypass the existing curb opening. More details on this calculation can be found in Appendix B below.

Sub-basin B contains 0.17 acres and drains south along East Anvil Drive. This sub-basin produces flows of 0.8 cfs for the 5-year storm and 1.5 cfs for the 100-year storm. These flows move south into and along curb and gutter as channelized flow. No water quality control measures are proposed within Subbasin B per the El Paso County Engineering Criteria Manual (ECM) Section I.7.1.C.1., which allows for the County to exclude up to 20 percent when the County has determined that it is not practicable to capture runoff from portions of the site that will not drain towards control measures. Sub-basin B is to remain the same as existing conditions.

Sub-basin C contains 2.14 acres and drains east towards Jimmy Camp Creek. This sub-basin produces flows of 0.8 cfs for the 5-year storm and 4.2 cfs for the 100-year storm. These flows sheetflow to the east. No water quality control measures are proposed within Sub-basin C because the land is to remain undeveloped. Water quality is not required for this sub-basin per El Paso County ECM Section I.7.1.B.7.

Sub-basin D contains 0.65 acres and drains east towards Jimmy Camp Creek. It produces flows of 0.2 cfs for the 5-year storm and 1.4 cfs for the 100-year storm. These flows sheetflow to the east, draining into Jimmy Camp Creek. No water quality control measures are proposed within Sub-basin D because the land is to remain undeveloped. Water quality is not required for this sub-basin per El Paso County ECM Section I.7.1.B.7.

Sub-basin E contains 1.65 acres and drains east towards Jimmy Camp Creek. It produces flows of 0.4 cfs for the 5-year storm and 2.8 cfs for the 100-year storm. These flows sheetflow to the east into Jimmy Camp Creek. No water quality control measures are proposed within Sub-basin E because the land is to remain undeveloped. Water quality is not required for this sub-basin per El Paso County ECM Section I.7.1.B.7.

Sub-basin F contains 0.09 acres and drains northeast into Jimmy Camp Creek. It produces flows of less than 0.1 cfs for the 5-year storm and 0.3 cfs for the 100-year storm. These flows sheetflow to the



east into Jimmy Camp Creek. No water quality control measures are proposed within Sub-basin F because the land is to remain undeveloped. Water quality is not required for this sub-basin per El Paso County ECM Section I.7.1.B.7.

Sub-basin OS1 contains 0.50 acres and drains southwest towards Sub-basin A. It produces flows of 0.1 cfs for the 5-year storm and 0.9 cfs for the 100-year storm. These flows sheetflow to the southwest into Sub-basin A. Flows combine with flows from Sub-basin A at Design Point 1 (DP1) to produce total flows of 3.3 cfs for the 5-year storm and 8.8 cfs for the 100-year storm. Flows were computed at this point to determine the capacity and freeboard within the proposed swale and trickle channel.

Sub-basin OS2 contains 0.37 acres and drains southeast towards Sub-basin E. It produces flows of 0.1 cfs for the 5-year storm and 0.8 cfs for the 100-year storm. These flows sheetflow to the southeast into Sub-basin E.

Sub-basin OS3 contains 0.01 acres and drains east towards Sub-basin A. It produces flows of less than 0.1 cfs for the 5-year storm and less than 0.1 cfs for the 100-year storm. These flows sheetflow to the east into Sub-basin A.

One existing rock check dam is to be removed to allow for the installation of the concrete forebay. All other existing rock check dams are to remain onsite. The removal of all other rock check dams is deemed unnecessary, and therefore, should remain as to slow runoff.

The estimated runoff amounts produced for the project under Proposed Conditions are shown in Table 2 below. The proposed design point information for the project are shown in Table 3 below.

TABLE 2 - PROPOSED CONDITIONS									
Sub-basin	Q ₅ (CFS)	Q ₁₀₀ (CFS)							
A*	3.7	9.1							
В	0.8	1.5							
С	0.8	4.2							
D	0.2	1.4							
E	0.4	2.8							
F	<0.1	0.3							
0\$1	0.1	0.9							
O\$2	0.1	0.8							
0\$3	<0.1	<0.1							

^{*}Note that detained flows are 0.6 cfs for the 5-year event and 5.0 cfs for the 100-year event

TABLE 3 - DESIGN POINTS								
DESIGN POINT	Q₅(CFS)	Q ₁₀₀ (CFS)						
DP1 (A + OS1)	3.3	8.8						



6.0 FOUR STEP PROCESS

The proposed development follows the "Four Step Process" as mandated by the *El Paso County Drainage Criteria Manual* as follows:

Step 1: Reduce runoff by disconnecting impervious area, eliminating "unnecessary" impervious area and encouraging infiltration into soils that are suitable.

Runoff has been reduced by disconnecting impervious areas where possible, eliminating "unnecessary" impervious areas and encouraging infiltration into suitable soils. IRF Spreadsheets utilized for design.

Step 2: Treat and slowly release the WQCV.

- All new developed flows have been routed to the water quality basin with impervious area less than one acre.
- Drain time for the water quality basin is as follows: Full Spectrum Extended Detention Basin (EDB) is 40 hours.

Step 3: Stabilize stream channels.

Although Jimmy Camp Creek drainageway is adjacent to the project, no work will be done in the drainageway.

- Site flows from the project have been directed to the concrete curb and gutters along the roadways and transported to public drainage facilities which direct them into the water quality/detention facility.
- All new and re-developed projects are required to construct or participate in the funding of channel stabilization measures. Drainage basin fees paid at the time of platting go towards channel stabilization within the drainage basin.

Step 4: Implement source controls.

Erosion control measures will be in place during initial construction to provide source control of sediment with landscaping placed within the proposed development and permanent seeding of all disturbed areas. No other potential pollutants are anticipated with this site post construction. The development of this site will have no adverse impact on downstream properties.

7.0 DETENTION BASIN

To accommodate the area of disturbance greater than 1 acre, a private 0.20-acre-foot Full Spectrum Detention Basin is proposed on the southwest corner of the site (See Proposed Drainage Plan in the Back Pocket). An proposed ditch beginning in the west end of Sub-basin A will direct flows towards the proposed private detention basin in the southwest corner of the site, as seen in Back Pocket – Proposed Drainage Plan. The detention basin, with a depth of 5.17ft and a volume of 0.20-acre-feet, will detain a flow of 3.3 cfs for the 5-year storm and 8.8 cfs for the 100-year storm in Sub-basin A (according to the CUHP procedure), seen below in Appendix B – Developed Detention for Colorado Centre.



A triangular channel located on the west end of the site discharges flows into the 0.20-acre-foot Full Spectrum Extended Detention Basin. These flows produce a velocity of 3.04 feet per second (fps) and a depth of 0.50 feet for the 5-year storm and a velocity of 3.89 fps and a depth of 0.72 feet for the 100-year storm within the channel. This is 1.95 feet of freeboard for the 5-year storm and 1.73 feet of freeboard for the 100-year storm within the channel. More details on the Manning's normal depth calculation for the inlet channel are provided below in Appendix B.

The detention basin will have post-detention peak flows of 0.6 cfs for the 5-year storm and 5.0 cfs for the 100-year storm. This detention basin will outlet 5-year flows through a series of orifices spaced at 0, 0.71, and 1.41 feet above the bottom of the basin. The detention basin will, conversely, outlet 100-year flows through a proposed Type OS2 outlet structure and tied into an existing 24" diameter CMP outlet pipe with a flow restrictor plate set at 6.0" above the pipe invert. More details can be found in the Appendix B – Outlet Structure Design. Basin drain times and stage versus volume figures are shown below in Appendix B – Developed Detention for Colorado Centre.

8.0 WATER QUALITY

Water quality for the site will be achieved through a 0.20-acre-foot proposed private Full Spectrum Extended Detention Basin (FS/EDB). A 2' wide trickle channel located in the detention basin will carry flows towards a private 'Type OS2' Outlet Structure tied into an existing private 24" corrugated metal pipe outlet (See *MHFD Detention Basin Stage-Storage Table Builder* in Appendix B for reference). The existing grated inlet located in Sub-basin Aex will be removed during construction. The outlet pipe to be tied into is in a stable and working condition, flowing and outfalling east into Flagstone Channel (See the Proposed Drainage Plan in the Back Pocket for reference). The outfall is protected with existing riprap and vegetation, which is seen below in a provided photo found in Appendix A. For these reasons, no improvements to the existing pipe are proposed. The private EDB drains an area of 3.28 acres that is 35.4% impervious and will have a volume of 0.20-acre-ft. The Water Quality capture volume will be 0.047 acre-ft. Calculations for the private EDB and outlet structure design are included in Appendix B of this report.

9.0 EROSION CONTROL PLAN

The site construction consists of constructing a new administration building and asphalt drive, disturbing 2.65 acres of area. This requires an Erosion and Stormwater Quality Control Permit. The Grading and Erosion Control Plan will be submitted in separate Construction Plans.

10.0 FLOODPLAIN STATEMENT

No portion of the developed site is located within a designated FEMA 100-year floodplain according to the information published in the Federal Emergency Management Agency Flood Plain Map No. 08041C0769G dated December 7th, 2018.



11.0 DRAINAGE BASIN FEES

The proposed development is located within the Jimmy Camp Creek Drainage Basin.

2022 Jimmy Camp Creek Drainage Fees

Drainage fees are waived because Colorado Centre Metropolitan District owns and maintains the drainage infrastructure within its boundaries.

2022 Jimmy Camp Creek Bridge Fees

Bridge fees are waived because Colorado Centre Metropolitan District owns and maintains the bridges within its boundaries.

12.0 CONSTRUCTION COST OPINION

The private, non-reimbursable Control Measures (CM) Financial Assurances costs of construction are as follows:

Description	Quantity	Unit Cost	Amount
·	•		
OUTLET STRUCTURE	1 EA	\$3,000	\$3,000
CONCRETE FOREBAY	1 LS	\$500	\$500
2' CONC. PAN	120 LF	\$20	\$2,400
FSD/EDB GRADING	1350 CY	\$10	\$13,500
CONCRETE STILLING BASIN	1 EA	\$2,500	\$2,500
RETAINING WALL	90 SF	\$20	\$1,800
		Sub-Total	\$23,700
	Engineering & Cor	ntingencies 10%	\$2,370
		Total	\$26,070

13.0 CONCLUSIONS

For this 7.73-acre site, work will include constructing a 4,542 sf administration building and asphalt driveway. In order to accommodate an area of disturbance greater than 1 acre, a 0.20-acre-foot Full Spectrum Extended Detention Basin is proposed that detains flows from Sub-basin A and releases 5-year storm and 100-year storm flows through a Type OS2 Outlet Structure that is tied into an existing 24" corrugated metal pipe.

Sediment and vegetation surrounding the existing 24" corrugated metal pipe outfall point in Flagstone Channel will be removed. Riprap pad will be re-established at this outfall point. The outfall point is currently scour stable. All areas disturbed by construction will be repaired, and erosion control measures will be installed during construction of the proposed site per the approved Grading and Erosion Control Plan to be submitted separately for review and approval. Site runoff, storm drains, and appurtenances associated with the development of the Colorado Centre Metropolitan District Administration building will not adversely affect the downstream and surrounding developments.



14.0 REFERENCES

Drainage Report for Colorado Centre Metropolitan District Water Treatment Facility, prepared by JDS-Hydro Consultants Inc in August 2015.

Flood Insurance Rate Map Number 08041C0769G, Federal Emergency Management Agency Floodplain Data, revised December 7, 2018

Municipal Code Corporation (2018). Drainage Criteria Manual of El Paso County, Colorado (DPM)

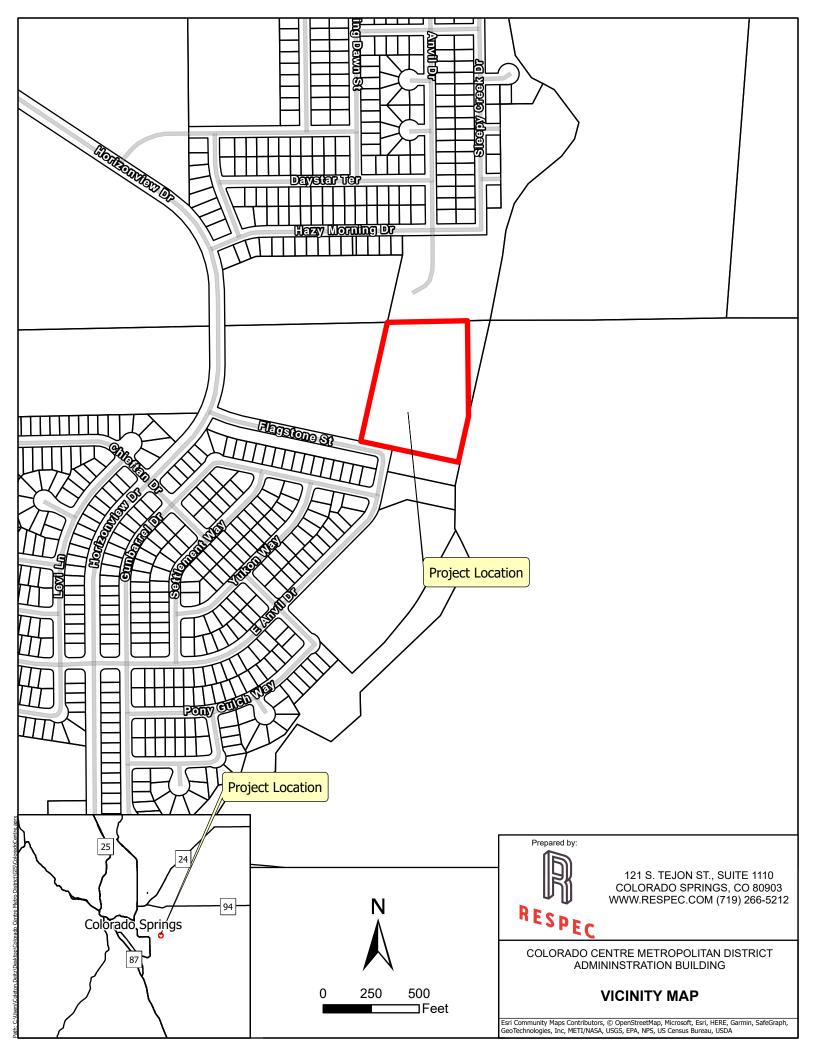
Urban Drainage and Flood Control District (June 2017). *Urban Storm Drainage Criteria Manual, Volume 1-3.*

USDA, NRCS. Soil Survey of El Paso County Area, Colorado.



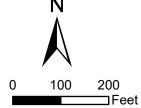
APPENDIX A

MAPS





Map Unit Symbol	Map Unit Name	Rating	Percent of Site, %
28	Ellicot loamy coarse sand,	۸	0
	0 to 5 percent slopes	ζ	0
101	Ustic Torrifluvents, loamy	В	100.0



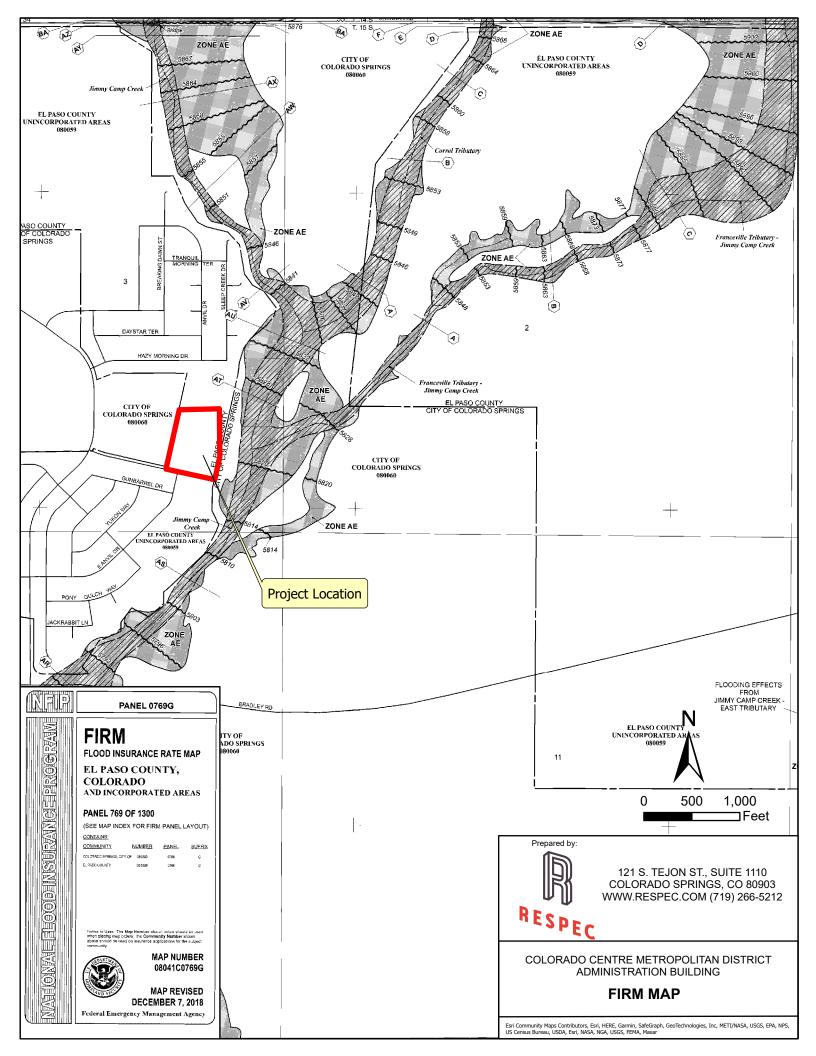


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COLORADO CENTRE METROPOLITAN DISTRICT ADMINISTRATION BUILDING

SOILS MAP

Maxar, Microsoft, Esri Community Maps Contributors, © OpenStreetMap, Microsoft, Esri, HERE, Garmin, SafeGraph, GeoTechnologies, Inc, METI/NASA, USGS, EPA, NPS, US Census Bureau, USDA





APPENDIX B

CALCULATIONS

Colorado Cer	ntre Metropolita	n District Ad	dminstration	Building					
PROJ.247.07									
C FACTOR C	ALCULATION S	HEET							
EXISTING CONDITIONS									
RUNOFF CO									
TYPE A/B SO	ILS								
LAND USE		Imperv %	5 YR	100 YR					
UNDEV		0							
GRAVEL ROA		80		0.7					
ASPHALT RO	AD	100							
ROOFS		90	0.73	0.81					
				XISTING CO	NDITIONS				
	ITOTAL	CLIDEAC	E CONDITIO		NUTTIONS	CALCIII	ATED C		
AREA	AREA	UNDEV	GRAVEL	ASPHALT	ROOFS	5	100	% IMPE	DVIOLIS
DESIG.	(acre)	ONDEV	ROAD	ROAD	ROOFS	YR	YR	70 IIVIFE	KV1003
Aex	2.05	2.01			0.00		0.36		1.8
Bex	0.17	0.00		0.07	0.00	0.90	0.96		100.0
Cex	2.87	2.72			0.08		0.38		4.9
Dex	0.71	0.71		0.00	0.00		0.35		0.0
Eex	1.65			0.00	0.00		0.35		0.0
Fex	0.09	0.09		0.00	0.00	0.08	0.35		0.0
Gex	0.07	0.07	0.00	0.00	0.00		0.35		0.0
OS1	0.50		1	0.00	0.00	0.08	0.35		0.0
OS2	0.37	0.37	0.00	0.00	0.00	0.08	0.35		0.0
OS3	0.01	0.01	0.00	0.00	0.00	0.08	0.35		0.0
Site Percent Ir	mpervious, %	4.6							

PROPOSED (CONDITIONS								
RUNOFF COE									
TYPE A/B SO	ILS								
LAND USE		Imperv %	5 YR	100 YR					
UNDEV		0							
GRAVEL ROA		80							
ASPHALT RO	AD	100		0.96					
ROOFS		90	0.73	0.81					
			PR	OPOSED CO	NDITIONS				
	TOTAL	SURFACE CONDITION				CALCUL	ATED C		
AREA	AREA	UNDEV	GRAVEL	ASPHALT	ROOFS	5	100	% IMPEI	RVIOUS
DESIG.	(acre)		ROAD	ROAD		YR	YR		
A	2.78		0.00		0.12	0.42	0.60		41.8
В	0.17	0.00	0.00	0.17	0.00	0.90	0.96		100.0
С	2.14	1.99	0.00	0.07	0.08	0.13	0.39		6.9
D	0.65	0.65	0.00	0.00	0.00	0.08	0.35		0.0
E	1.65	1.65	0.00	0.00	0.00	0.08	0.35		0.0
F	0.09	0.09	0.00	0.00	0.00	0.08	0.35		0.0
G	0.07	0.07	0.00	0.00	0.00	0.08	0.35		0.0
OS1	0.50	0.50	0.00	0.00	0.00	0.08	0.35		0.0
OS2	0.37	0.37	0.00	0.00	0.00	0.08	0.35		0.0
OS3	0.01	0.01	0.00	0.00	0.00	0.08	0.35		0.0
Site Percent Ir	npervious, %	19.6							

CCMD Admin Building																		
PROJ.247.07																		
DRAINAGE CALCULAT	TON SHEE	T																
file:Colorado Centre Adr	min Building	g.xlsx																
MARCH 2023																		
							Initial Tci			Travel Ti	me							
AREA	AREA	C5	C100	C5 X A	C100 X A	. (5:)	Slope	ti		Slope	V	Tt	TC	15	I100	Q5		AREA
DESIG.	(acre)	(5 yr)	(100 yr)			L (ft)	(%)	(min)	L (ft)	(%)	(fps)	(min)	(min)	(in/hr)	(in/hr)	(cfs)	(cfs)	DESIG.
EVICTING																		
EXISTING																		
CONDITIONS		0.00		0.10	0.74	400		40.0	700		4 -	0.0	00.0		4.0	2.0		ļ
Aex	2.05	0.09	0.36	0.18	0.74	100	1.4	16.9	700	3.3	1.7	6.9	23.8	2.7	4.6	0.6	3.4	Aex
Bex	0.17	0.90	0.96	0.15	0.16	65	4.4	1.8	90	4.4	4.2	0.4	5.0	5.2	9.1	0.8	1.5	Bex
Cex	2.87	0.12	0.38	0.34	1.09	100	1.5	16.0	585	4.5	2.0	4.9	20.9	2.8	5.0	1.0	5.4	Cex
Dex	0.71	0.08	0.35	0.06	0.25	100	6.5	10.3	320	1.9	1.4	3.8	14.1	3.5	6.1	0.2	1.5	Dex
Eex	1.65	0.08 0.08	0.35 0.35	0.13 0.01	0.58	100 70	0.8 10.8	20.5 7.3	140	10.7 0.0	3.1	0.8	21.3	2.8	4.9	0.4 <0.1	2.8 0.3	Eex
Fex Gex	0.09 0.07	0.08	0.35	0.01	0.03 0.02	55	10.8	6.5	0	0.0	0.0	0.0	7.3 6.5	4.6 4.8	8.0 8.3	<0.1	0.3	Fex Gex
OS1	0.07	0.08	0.35	0.01	0.02	100	0.8	20.5	40	0.0	0.0	0.0	21.3	2.8	4.9	0.1	0.2	OS1
OS2	0.37	0.08	0.35	0.04	0.18	100	5.4	10.9	70	0.8	0.9	1.4	12.3	3.7	6.5	0.1	0.8	OS2
OS3	0.01	0.08	0.35	0.00	0.00	15	16.2	2.9	0	0.0	0.9	0.0	5.0	5.2	9.1	<0.1	<0.1	OS3
000	0.01	0.00	0.55	0.00	0.00	10	10.2	2.5	0	0.0	0.0	0.0	3.0	0.2	0.1	\0.1	\0.1	000
PROPOSED																		
CONDITIONS																		
A	2.78	0.42	0.60	1.17	1.67	100	1.0	12.7	710	1.6	2.5	4.7	17.4	3.1	5.5	3.7	9.1	Α
В	0.17	0.90	0.96	0.15	0.16	65	4.4	1.8	90	4.4	4.2	0.4	5.0	5.2	9.1	8.0	1.5	В
C	2.14	0.13	0.39	0.28	0.83	100	1.5	15.9	585	4.5	2.0	4.9	20.7	2.9	5.0	0.8	4.2	C
D	0.65	0.08	0.35	0.05	0.23	100	6.5	10.3	320	1.9	1.4	3.8	14.1	3.5	6.1	0.2	1.4	D
E	1.65	0.08	0.35	0.13	0.58	100	0.8	20.5	140	10.7	3.1	0.8	21.3	2.8	4.9	0.4	2.8	<u> </u>
F	0.09	0.08	0.35	0.01	0.03	70	10.8	7.3	0	0.0	0.0	0.0	7.3	4.6	8.0	<0.1	0.3	F
OS1	0.50	0.08	0.35	0.04	0.18	100	0.8	20.5	40	0.8	0.9	0.8	21.3	2.8	4.9	0.1	0.9	OS1
OS2	0.37	0.08	0.35	0.03	0.13	100	5.4	10.9	70	0.8	0.9	1.4	12.3	3.7	6.5	0.1	0.8	OS2
OS3 DP1 (A + OS1)	0.01	0.08 0.37	0.35 0.56	0.00 1.21	0.00 1.84	15	16.2	2.9 21.3	0 580	0.0 2.8	0.0 1.6	0.0	5.0	5.2	9.1 4.8	<0.1 3.3	<0.1 8.8	OS3 DP1 (A + OS1)
DP1 (A + US1)	3.28	0.37	0.50	1.∠1	1.04			21.3	300	2.0	1.0	1.0	22.3	2.7	4.0	ა.ა	0.0	DFT (A + UST)
	-t		-1	1	1	I	1	I.	l.	1	I	1	I	-1	1	1	I.	

Colorado Centre Metropolitan District Proposed Full Spectrum Detention Basin Stage-Area Curve

Elevation (ft)	Depth (ft)	Area (sf)	Area (ac)	Inc. Vol. (ac-ft)	Total Vol. (ac-ft)
5818.83	0	0	0	0.00	0.00
5819	5819	419	0.01	0.00	0.00
5820	5820	3075	0.07	0.04	0.04
5821	5821	4378	0.10	0.09	0.13
5822	5822	5338	0.12	0.11	0.24
5823	5823	6484	0.15	0.14	0.37
5824	5824	6940	0.16	0.15	0.53

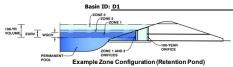
DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.05 (January 2022)

Project: Colorado Centre Metro District Admin Building

acre-feet
1.19 inches
1.50 inches
1.75 inches
2.00 inches

2.25 inches 2.52 inches 3.01 inches



Watershed Information

Selected BMP Type =	EDB				
Watershed Area =	3.28	acres			
Watershed Length =	500	ft			
Watershed Length to Centroid =	200	ft			
Watershed Slope =	0.050	ft/ft			
Watershed Imperviousness =	35.40%	percent			
Percentage Hydrologic Soil Group A =	0.0%	percent			
Percentage Hydrologic Soil Group B =	100.0%	percent			
Percentage Hydrologic Soil Groups C/D =	0.0%	percent			
Target WQCV Drain Time =	40.0	hours			
Location for 1-hr Rainfall Depths = Denver - Capitol Building					

After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Libba Notaconado Parado

the embedded Colorado Urban Hydrograph Procedure.					
Water Quality Capture Volume (WQCV) =	0.046	acre-feet			
Excess Urban Runoff Volume (EURV) =	0.121	acre-feet			
2-yr Runoff Volume (P1 = 1.19 in.) =	0.114	acre-feet			
5-yr Runoff Volume (P1 = 1.5 in.) =	0.175	acre-feet			
10-yr Runoff Volume (P1 = 1.75 in.) =	0.232	acre-feet			
25-yr Runoff Volume (P1 = 2 in.) =	0.314	acre-feet			
50-yr Runoff Volume (P1 = 2.25 in.) =	0.378	acre-feet			
100-yr Runoff Volume (P1 = 2.52 in.) =	0.461	acre-feet			
500-yr Runoff Volume (P1 = 3.01 in.) =	0.590	acre-feet			
Approximate 2-yr Detention Volume =	0.088	acre-feet			
Approximate 5-yr Detention Volume =	0.124	acre-feet			
Approximate 10-yr Detention Volume =	0.175	acre-feet			
Approximate 25-yr Detention Volume =	0.198	acre-feet			
Approximate 50-yr Detention Volume =	0.208	acre-feet			
Approximate 100-yr Detention Volume =	0.242	acre-feet			

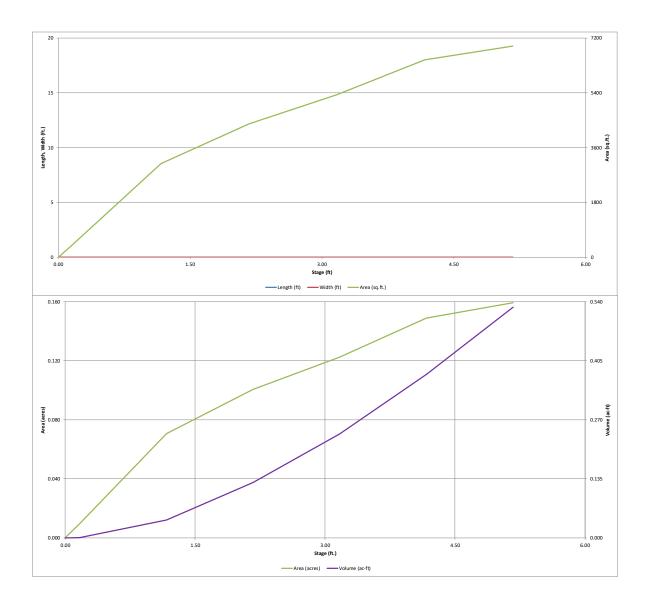
Define Zones and Basin Geometry

Zone 1 Volume (WQCV) =	0.046	acre-feet
Zone 2 Volume (EURV - Zone 1) =	0.075	acre-feet
Zone 3 Volume (100-year - Zones 1 & 2) =	0.121	acre-feet
Total Detention Basin Volume =	0.242	acre-feet
Initial Surcharge Volume (ISV) =	user	ft ³
Initial Surcharge Depth (ISD) =	user	ft
Total Available Detention Depth (H _{total}) =	user	ft
Depth of Trickle Channel (H _{TC}) =	user	ft
Slope of Trickle Channel $(S_{TC}) =$	user	ft/ft
Slopes of Main Basin Sides (Smain) =	user	H:V
Basin Length-to-Width Ratio (R _{L/W}) =	user	

Initial Surcharge Area $(A_{ISV}) =$	user	ft ²
Surcharge Volume Length $(L_{ISV}) =$	user	ft
Surcharge Volume Width $(W_{ISV}) =$	user	ft
Depth of Basin Floor (H_{FLOOR}) =	user	ft
Length of Basin Floor (L_{FLOOR}) =	user	ft
Width of Basin Floor $(W_{FLOOR}) =$	user	ft
Area of Basin Floor $(A_{FLOOR}) =$	user	ft²
Volume of Basin Floor $(V_{FLOOR}) =$	user	ft ³
Depth of Main Basin $(H_{MAIN}) =$	user	ft
Length of Main Basin $(L_{MAIN}) =$	user	ft
Width of Main Basin $(W_{MAIN}) =$	user	ft
Area of Main Basin $(A_{MAIN}) =$	user	ft²
Volume of Main Basin $(V_{MAIN}) =$	user	ft ³
Calculated Total Basin Volume (V_{total}) =	user	acre-feet

	D. II	0.40	l.							
г	Depth Increment =	0.10	ft Optional				Optional			
	Stage - Storage	Stage	Override	Length	Width	Area	Override	Area	Volume	Volume
L	Description	(ft)	Stage (ft)	(ft)	(ft)	(ft 2)	Area (ft 2)	(acre)	(ft 3)	(ac-ft)
	Top of Micropool	-	0.00	-		-	0	0.000		
	5819		0.17	-		-	419	0.010	36	0.001
	5820		1.17			-	3,075	0.071	1,783	0.041
	5821		2.17	-			4,378	0.101	5,509	0.126
	5822		3.17	-		-	5,338	0.123	10,367	0.238
	5823		4.17	-		-	6,484	0.149	16,278	0.374
	5824		5.17	-		-	6,940	0.159	22,990	0.528
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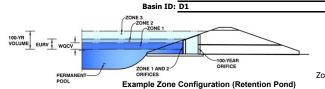
Colorado Centre - M-IFD Detention V3, Basin 4/12/2023, 7:29 AM



Colorado Centre - M-IFD Detention V3, Basin 4/12/2023, 7:29 AM

MHFD-Detention, Version 4.05 (January 2022)

Project: Colorado Centre Metro District Admin Building



	Estimated	Estimated	
	Stage (ft)	Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	1.24	0.046	Orifice Plate
Zone 2 (EURV)	2.12	0.075	Orifice Plate
one 3 (100-year)	3.21	0.121	Weir&Pipe (Restrict)
·-	Total (all zones)	0.242	

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

ft (distance below the filtration media surface) Underdrain Orifice Invert Depth = Underdrain Orifice Diameter = inches

Calculated Parameters for Underdrain Underdrain Orifice Area Underdrain Orifice Centroid = feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP) Centroid of Lowest Orifice = 0.00 ft (relative to basin bottom at Stage = 0 ft) Depth at top of Zone using Orifice Plate = 2.12 ft (relative to basin bottom at Stage = 0 ft)

Orifice Plate: Orifice Vertical Spacing = 8.50 inches Orifice Plate: Orifice Area per Row = 0.38 sq. inches (diameter = 11/16 inch)

Calculated Parameters for Plate WQ Orifice Area per Row 2.639E-03 ft^2 Elliptical Half-Width = N/A feet Elliptical Slot Centroid = N/A feet ft² Elliptical Slot Area = N/A

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	0.71	1.41					
Orifice Area (sq. inches)	0.38	0.38	0.38					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

	Not Selected	Not Selected	
Invert of Vertical Orifice =	N/A	N/A	ft (rela
Depth at top of Zone using Vertical Orifice =	N/A	N/A	ft (relat
Vertical Orifice Diameter =	N/A	N/A	inches

ft (relative to basin bottom at Stage = 0 ft) ft (relative to basin bottom at Stage = 0 ft)

Vertical Orifice Area = Vertical Orifice Centroid =

	Calculated Parameters for Vertical Orifice					
	Not Selected	Not Selected				
=	N/A	N/A	ft²			
=	N/A	N/A	fee			

Calculated Parameters for Overflow Weir

Not Selected

N/A

N/A

N/A

N/A

N/A

ns W through AF

100 Year

0.461

0.461

5.6

1.72

8.8

0.9

N/A

N/A

64

2.86

Outlet Plate

500 Year

3.01

0.590

0.590

7.3

2.24

10.8

5.4

0.7

Spillway

N/A

N/A

63

feet

feet

ft²

Zone 3 Weir

2.15

0.00

0.00

0.00

0.00

User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir and No Outlet Pipe)

	Zone 3 Weir	Not Selected]
Overflow Weir Front Edge Height, Ho =	2.15	N/A	ft (ı
Overflow Weir Front Edge Length =	4.00	N/A	fee
Overflow Weir Grate Slope =	0.00	N/A	Н:۷
Horiz. Length of Weir Sides =	0.00	N/A	fee
Overflow Grate Type =	Type C Grate	N/A	
Debris Clogging % =	50%	N/A	%

Height of Grate Upper Edge, Ht = (relative to basin bottom at Stage = 0 ft) Overflow Weir Slope Length = Grate Open Area / 100-yr Orifice Area = Overflow Grate Open Area w/o Debris = Overflow Grate Open Area w/ Debris =

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

	Zone 3 Restrictor	Not Selected
Depth to Invert of Outlet Pipe =	0.25	N/A
Outlet Pipe Diameter =	24.00	N/A
Restrictor Plate Height Above Pipe Invert =	6.00	

ft (distance below basin bottom at Stage = 0 ft) inches inches

Outlet Orifice Area = Outlet Orifice Centroid = Half-Central Angle of Restrictor Plate on Pipe =

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate Zone 3 Restrictor Not Selected 0.61 N/A 0.29 N/A feet N/A radians 1.05

<u>User Input: Emergency Spillway (Rectangular or Trapezoidal)</u>

Spillway Invert Stage=	3.35	ft (rel
Spillway Crest Length =	4.00	feet
Spillway End Slopes =	4.00	H:V
Freeboard above Max Water Surface =	1.00	feet

lative to basin bottom at Stage = 0 ft)

Spillway Design Flow Depth= Stage at Top of Freeboard = Basin Area at Top of Freeboard = Basin Volume at Top of Freeboard =

Calculated Parameters for Spillway 0.62 feet 4.97 feet acres 0.16 0.50 acre-ft

50 Year

0.378

0.378

4.5

7.0

4.5

Overflow Weir 1

N/A

N/A

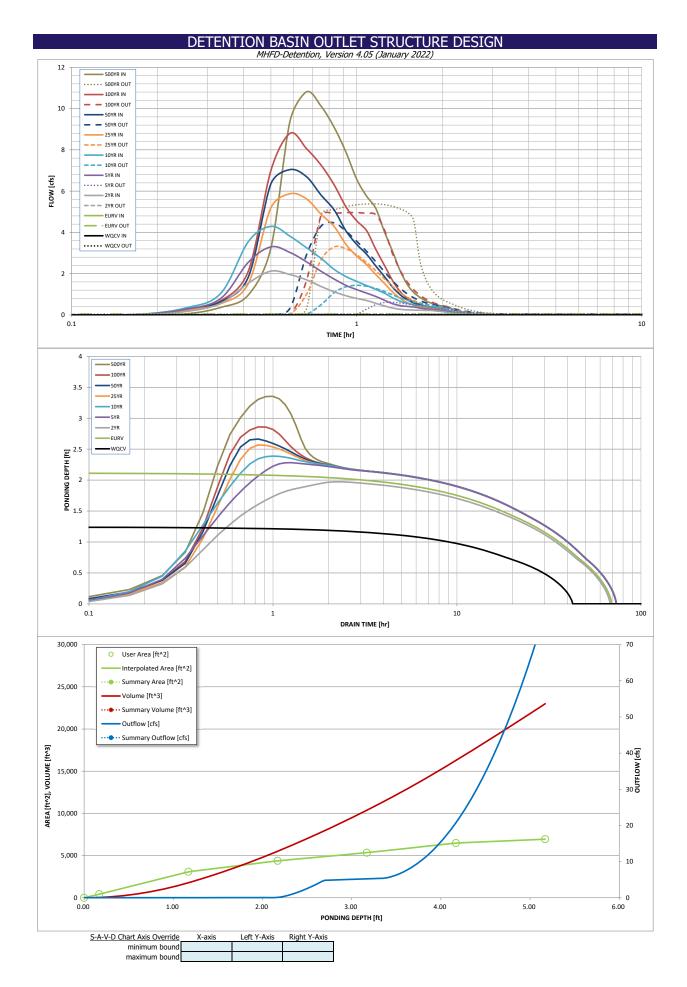
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2.66

Routed Hydrograph Results Design Storm Return Perio One-Hour Rainfall Depth (in CUHP Runoff Volume (acre-f User Override Inflow Hydrograph Volume (acre-f CUHP Predevelopment Peak Q (cfs OPTIONAL Override Predevelopment Peak Q (cf. Predevelopment Unit Peak Flow, g (cfs/acre Peak Inflow Q (cfs Peak Outflow Q (cf Ratio Peak Outflow to Predevelopment Structure Controlling Flor Max Velocity through Grate 1 (fps

Design Storm Return Period =	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	
One-Hour Rainfall Depth (in) =	N/A	N/A	1.19	1.50	1.75	2.00	Ĺ
CUHP Runoff Volume (acre-ft) =	0.046	0.121	0.114	0.175	0.232	0.314	Ĺ
r Override Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	0.114	0.175	0.232	0.314	Ĺ
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A	0.5	1.4	2.1	3.6	
PTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A					Ī
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.16	0.42	0.64	1.10	
Peak Inflow Q (cfs) =	N/A	N/A	2.1	3.3	4.3	5.9	_
Peak Outflow Q (cfs) =	0.0	0.0	0.0	0.6	1.4	3.3	
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	0.4	0.7	0.9	
Structure Controlling Flow =	Plate	Plate	Plate	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	
Time to Drain 97% of Inflow Volume (hours) =	39	62	61	63	61	58	_
Time to Drain 99% of Inflow Volume (hours) =	41	66	65	69	68	67	
Maximum Ponding Depth (ft) =	1.25	2.12	1.97	2.28	2.39	2.57	
Area at Maximum Ponding Depth (acres) =	0.07	0.10	0.09	0.10	0.11	0.11	_
Maximum Volume Stored (acre-ft) =	0.047	0.121	0.107	0.138	0.148	0.167	

4/12/2023, 7:27 AM Colorado Centre - MHFD Detention V3, Outlet Structure



DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename:

Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

	SOURCE	CUHP	CUHP	CUHP	USER	CUHP	CUHP	CUHP	USER	CUHP
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]		10 Year [cfs]		50 Year [cfs]		500 Year [cfs]
	0:00:00									
5.00 min		0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00 0:15:00	0.00	0.00	0.00 0.16	0.00 0.27	0.00	0.00	0.02 0.28	0.00	0.05 0.37
	0:20:00	0.00	0.00	0.16	0.80	1.04	0.55	0.28	0.28	0.37
	0:25:00	0.00	0.00	1.54	2.56	3.55	1.53	1.84	2.13	3.25
	0:30:00	0.00	0.00	2.12	3.30	4.29	5.20	6.35	7.00	9.39
	0:35:00	0.00	0.00	1.96	3.03	3.82	5.87	7.04	8.80	10.81
	0:40:00	0.00	0.00	1.70	2.57	3.25	5.63	6.70	8.06	10.12
	0:45:00	0.00	0.00	1.38	2.12	2.74	4.88	5.81	7.26	9.09
	0:50:00	0.00	0.00	1.12	1.74	2.21	4.29	5.09	6.31	7.89
	0:55:00	0.00	0.00	0.93	1.43	1.86	3.42	4.07	5.24	6.58
	1:00:00	0.00	0.00	0.80	1.23	1.63	2.85	3.42	4.56	5.76
	1:05:00 1:10:00	0.00	0.00	0.70 0.56	1.06 0.90	1.43 1.24	2.44 1.96	2.94 2.37	4.08 3.18	5.16 4.05
	1:15:00	0.00	0.00	0.44	0.72	1.06	1.54	1.87	2.42	3.11
	1:20:00	0.00	0.00	0.34	0.55	0.84	1.13	1.36	1.69	2.18
	1:25:00	0.00	0.00	0.28	0.46	0.67	0.81	0.99	1.15	1.51
	1:30:00	0.00	0.00	0.25	0.41	0.57	0.61	0.74	0.83	1.10
	1:35:00	0.00	0.00	0.23	0.39	0.50	0.48	0.59	0.64	0.85
	1:40:00	0.00	0.00	0.23	0.33	0.45	0.40	0.49	0.51	0.68
	1:45:00	0.00	0.00	0.22	0.30	0.42	0.34	0.42	0.42	0.56
	1:50:00	0.00	0.00	0.22	0.27	0.39	0.31	0.38	0.36	0.48
	1:55:00	0.00	0.00	0.19	0.25	0.36	0.28	0.35	0.32	0.43
	2:00:00 2:05:00	0.00	0.00	0.16 0.12	0.22	0.31	0.27	0.33	0.30 0.22	0.40
	2:10:00	0.00	0.00	0.12	0.16 0.12	0.22	0.19 0.14	0.24	0.22	0.29
	2:15:00	0.00	0.00	0.06	0.08	0.11	0.10	0.17	0.13	0.15
	2:20:00	0.00	0.00	0.04	0.06	0.08	0.07	0.08	0.08	0.10
	2:25:00	0.00	0.00	0.03	0.04	0.05	0.05	0.06	0.05	0.07
	2:30:00	0.00	0.00	0.02	0.03	0.04	0.03	0.04	0.04	0.05
	2:35:00	0.00	0.00	0.01	0.02	0.02	0.02	0.03	0.02	0.03
	2:40:00	0.00	0.00	0.01	0.01	0.01	0.01	0.01	0.01	0.02
	2:45:00	0.00	0.00	0.00	0.00	0.01	0.01	0.01	0.01	0.01
	2:50:00 2:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:45:00 3:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:20:00 4:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:40:00 4:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:00:00 5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:25:00 5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:45:00 5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
			·					· · · · · · · · · · · · · · · · · · ·		·

Rock_Chute.xls Page 1 of 3

Rock Chute Design Data

(Version WI-July-2010, Based on Design of Rock Chutes by Robinson, Rice, Kadavy, ASAE, 1998)

County: El Paso, Colorado

Project: Colorado Centre Admin Building
Designer: CTD Che

igner: CTD Checked by: RGG
Date: December 1, 2022 Date:

Input Geometry:

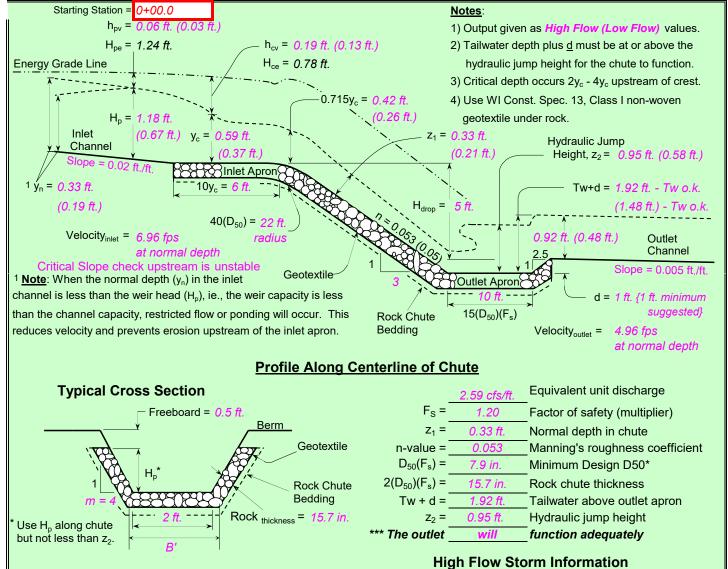
Upstream Channel Chute Downstream Channel Bw = 4.0 ft. Bw = 2.0Bw = 2.0Side slopes = 0.0 (m:1) Factor of safety = 1.20 (F_s) Side slopes = 0.0 (m:1) Side slopes = 4.0 (m:1) \rightarrow 2.0:1 max. Velocity n-value = 0.013 Velocity n-value = 0.013Bed slope = 0.0200 ft./ft. Bed slope (3:1) = 0.333 ft./ft $\rightarrow 3.0:1$ max. Bed slope = 0.0050 ft./ft. Note: n value = a) velocity n from waterway program Freeboard = 0.5 ft. or b) computed mannings n for channel Outlet apron depth, d = 1.0 ft. Base flow = 0.0 cfs

Design Storm Data (Table 2, FOTG, WI-NRCS Grade Stabilization Structure No. 410):

Apron elev. --- Inlet =5826.0 ft. ---- Outle\$820.0 ft. --- ($\mathsf{H}_{\mathsf{drop}} = 5$ ft.)

Apron elev. --- Inlet =5826.0 ft. ----- Outle\$820.0 ft. --- ($\mathsf{H}_{\mathsf{drop}} = 5$ ft.) Note : The total required capacity is routed through the chute (principal spillway) or in combination with an auxiliary spillway. $\mathsf{Q}_{\mathsf{high}} = \mathsf{Runofff}$ from a 5-year,24-hour storm. $\mathsf{Q}_{\mathsf{high}} = 9.1$ cfs High flow storm through chute $\mathsf{Tw} = 1.20$ Tw (ft.) = Program $\mathsf{Q}_{\mathsf{high}} = 1.20$ Tw (ft.) = Program

Profile and Cross Section (Output):



Project: Colorado Centre Admin Building



Water Quality Capture Volume (WQCV) Calculator

Drain Time (hrs)	40
Coefficient, a	1.0
Imperviousness, I	35.4%
WQCV (watershed inches)	0.17
WQCV (ft)	0.01
Watershed Area (ac)	3.3
WQCV (ac-ft)	0.046



Forebay Calculator

WQCV (ac-ft)	0.046
2% of WQCV (ac-ft)	0.0009
2% of WQCV (cf)	40
Depth (ft)	1.00
Width (ft)	6
Length (ft)	8
Volume (cf)	48
Is Volume greater than 2% of WQCV?	YES



Forebay Notch Calculator

Q ₁₀₀ (cfs)	8.8
2% of Q ₁₀₀ (cfs)	0.18
D (ft)	1
W (ft)	0.06

$$W = \frac{2\% \ of \ Q}{D^{1.5} * C}$$



Trickle Channel Calculator

Q ₁₀₀ (cfs)	8.8
2% of Q ₁₀₀ (cfs)	0.18
Slope (ft/ft)	0.005
Bottom Width (ft)	2
Side Slopes (Vertical)	0
Depth of Trickle Channel (ft)	0.5
Depth of 2% of 100-Year (ft)	0.07
Velocity (ft/s)	1.3
Froude Number	0.9
Type of Flow	Subcritical
(Subcritcal/Supercritical)	Subcritical

Project: Colorado Centre Admin Building



Proposed Detention Basin Spillway

Slope (ft/ft)	0.1
Cf	2
Q ₁₀₀ (cfs)	8.8
Width (ft)	4.0
q (cfs/ft)	2.20
Calculated D ₅₀ (in)	5.3
D ₅₀ used (in)	6.0

RESPEC	Detention Basin Outlet
100-Year Peak Outflow (cfs)	5.6
Y _t (ft)	0.59
D _c (ft)	2.0
D ₅₀ (ft)	0.2
D ₅₀ Used (ft)	6.0

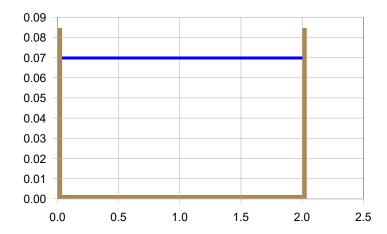
Rectangular Channel

Input

Flow 0.18 cfs
Slope 0.005 ft/ft
Manning's n 0.013
Base Width 2 ft
Right Side Slope 0:1
Left Side Slope 0:1

Output

Depth 0.069 ft Flow Area 0.138 sf Velocity 1.30 fps Velocity Head 0.0263 ft Top Width 2.00 ft Froude Number 0.873 Critical Depth 0.063 ft Critical Slope 0.00671 ft/ft



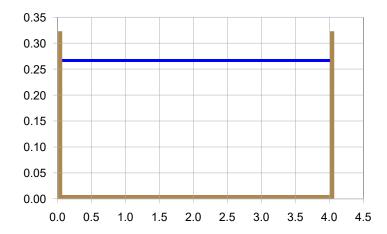
Rectangular Channel

Input

Flow 9.1 cfs
Slope 0.04 ft/ft
Manning's n 0.013
Base Width 4 ft
Right Side Slope 0:1
Left Side Slope 0:1

Output

Depth 0.263 ft Flow Area 1.05 sf 8.65 fps Velocity Velocity Head 1.16 ft Top Width 4.00 ft Froude Number 2.97 Critical Depth 0.544 ft Critical Slope 0.00416 ft/ft



Irregular Section

Input

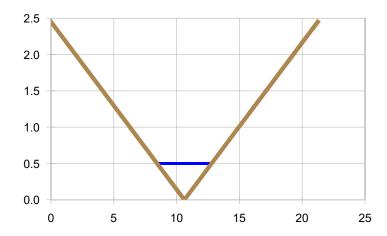
Flow 3.3 cfs Slope 0.044 ft/ft

Sta **n** 0.04 Elev n Sta Elev Sta Elev n Sta Elev n 0.04 2.45 10.62 21.24 0.04 0 2.45

Output

WSElev 0.500 ft 1.09 sf Flow Area 3.04 fps Velocity Velocity Head 0.144 ft Top Width 4.34 ft Froude Number 1.07 Critical WSElev 0.514 ft Critical Slope ft/ft

Note: 1.95' of Freeboard.



Manning Formula:

Irregular Section

Input

Flow 8.8 cfs Slope 0.044 ft/ft

Sta Elev n Sta Elev Sta Elev n Sta Elev n 0.04 0.04 2.45 10.62 21.24 0.04 0 2.45

Output

WSElev 0.723 ft Flow Area 2.26 sf 3.89 fps Velocity Velocity Head 0.235 ft Top Width 6.27 ft Froude Number 1.14 Critical WSElev 0.762 ft Critical Slope ft/ft

Note: 1.73' of Freeboard.

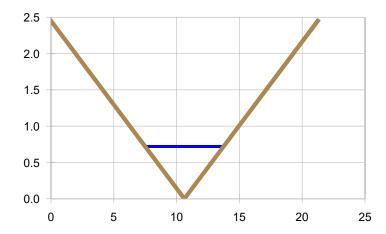




Image taken looking southeast at the existing outfall configuration of the 24" CMP storm sewer line beginning onsite and terminating in Flagstone Channel.



APPENDIX C

DESIGN CHARTS

3.1. - Rational Method Runoff Coefficient (C)

The runoff coefficient represents the integrated effects of infiltration, detention storage, evaporation, retention, flow routing, and interception, all of which affect the time distribution and peak rate of runoff. Runoff coefficients are based on the imperviousness of a particular land use and the hydrologic soil type of the area and are to be selected in accordance with Table 6-6.

The procedure for determining the runoff coefficient includes these steps:

- 1. Categorize the site area into one or more similar land uses, each with a representative imperviousness, according to the information in Table 6-6.
- 2. Based on the dominant hydrologic soil type in the area, use Table 6-6 to estimate the runoff coefficient for the particular land use category for the design storms of interest.
- 3. Calculate an area-weighted average runoff coefficient for the site based on the runoff coefficients from individual land use areas of the site.

When analyzing an area for design purposes, urbanization of the full watershed, including both on-site and off-site areas, shall be assumed.

Gravel parking areas, storage areas, and access drives proposed on Site Improvement Plans shall be analyzed based on an imperviousness of 80%. This is due to the potential for gravel areas being paved over time by property owners and the resulting adverse impacts on the stormwater management facilities and adjacent properties.

There are some circumstances where the selection of impervious percentage values may require additional investigation due to unique land characteristics (e.g., recent burn areas). When these circumstances arise, it is the designer's responsibility to verify that the correct land use assumptions are made.

When multiple sub-basins are delineated, the composite C value calculation is:

$$C_c = (C_1 A_1 + C_2 A_2 + C_3 A_3 + ... C_i A_i)/A_t$$
 (Eq. 6-6)

Where:

C_c = composite runoff coefficient for total area

C_i = runoff coefficient for subarea corresponding to surface type or land use

A i = area of surface type corresponding to Ci (units must be the same as those used for total area)

A t = total area of all subareas for which composite runoff coefficient applies

i = number of surface types in the drainage area

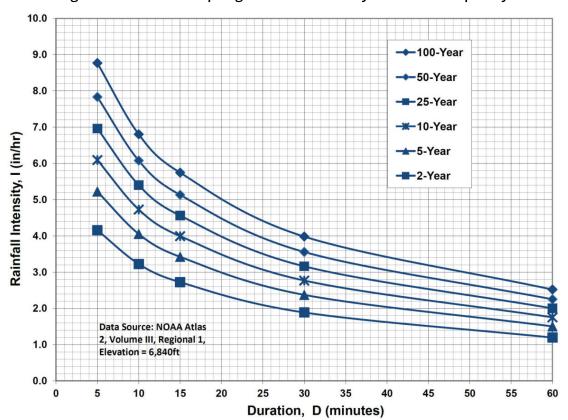
Table 6-6. Runoff Coefficients for Rational Method (Source: UDFCD 2001)

Land Use or	Percent	Runoff Coef	ficients				
Surface Characteristics	Impervious	2-year	5-year	10-year	25-year	50-year	100-year

		HSG A&B	HSG C&D										
Business													
Commercial Areas	95	0.79	0.80	0.81	0.82	0.83	0.84	0.85	0.87	0.87	0.88	0.88	0.89
Neighborhood Areas	70	0.45	0.49	0.49	0.53	0.53	0.57	0.58	0.62	0.60	0.65	0.62	0.68
Residential													
⅓ Acre or less	65	0.41	0.45	0.45	0.49	0.49	0.54	0.54	0.59	0.57	0.62	0.59	0.65
¼ Acre	40	0.23	0.28	0.30	0.35	0.36	0.42	0.42	0.50	0.46	0.54	0.50	0.58
⅓ Acre	30	0.18	0.22	0.25	0.30	0.32	0.38	0.39	0.47	0.43	0.52	0.47	0.57
½ Acre	25	0.15	0.20	0.22	0.28	0.30	0.36	0.37	0.46	0.41	0.51	0.46	0.56
1 Acre	20	0.12	0.17	0.20	0.26	0.27	0.34	0.35	0.44	0.40	0.50	0.44	0.55
Industrial													
Light Areas	80	0.57	0.60	0.59	0.63	0.63	0.66	0.66	0.70	0.68	0.72	0.70	0.74
Heavy Areas	90	0.71	0.73	0.73	0.75	0.75	0.77	0.78	0.80	0.80	0.82	0.81	0.83
Parks and Cemeteries	7	0.05	0.09	0.12	0.19	0.20	0.29	0.30	0.40	0.34	0.46	0.39	0.52
Playgrounds	13	0.07	0.13	0.16	0.23	0.24	0.31	0.32	0.42	0.37	0.48	0.41	0.54
Railroad Yard Areas	40	0.23	0.28	0.30	0.35	0.36	0.42	0.42	0.50	0.46	0.54	0.50	0.58
Undeveloped Areas													

Historic Flow Analysis— Greenbelts, Agriculture	2	0.03	0.05	0.09	0.16	0.17	0.26	0.26	0.38	0.31	0.45	0.36	0.51
Pasture/Meadow	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50
Forest	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50
Exposed Rock	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Offsite Flow Analysis (when landuse is undefined)	45	0.26	0.31	0.32	0.37	0.38	0.44	0.44	0.51	0.48	0.55	0.51	0.59
Streets													
Paved	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Gravel	80	0.57	0.60	0.59	0.63	0.63	0.66	0.66	0.70	0.68	0.72	0.70	0.74
Drive and Walks	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Roofs	90	0.71	0.73	0.73	0.75	0.75	0.77	0.78	0.80	0.80	0.82	0.81	0.83
Lawns	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50

Figure 6-5. Colorado Springs Rainfall Intensity Duration Frequency



IDF Equations

$$I_{100} = -2.52 \ln(D) + 12.735$$

$$I_{50} = -2.25 \ln(D) + 11.375$$

$$I_{25} = -2.00 \ln(D) + 10.111$$

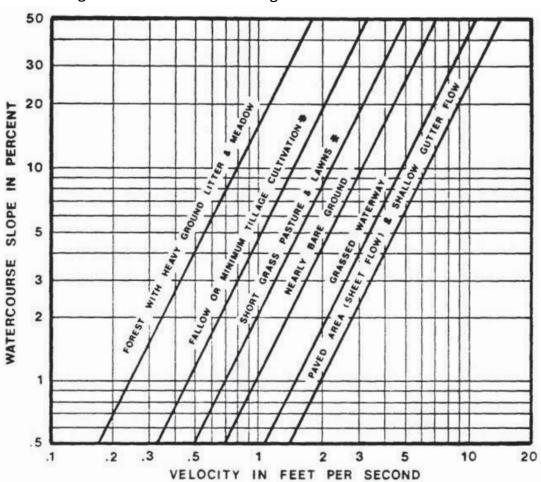
$$I_{10} = -1.75 \ln(D) + 8.847$$

$$I_5 = -1.50 \ln(D) + 7.583$$

$$I_2 = -1.19 \ln(D) + 6.035$$

Note: Values calculated by equations may not precisely duplicate values read from figure.

Figure 6-25. Estimate of Average Concentrated Shallow Flow



Chapter 6 Runoff

Colorado Urban Hydrograph Procedure 3.0

3.1 **Background**

The Colorado Urban Hydrograph Procedure (CUHP) is a method of hydrologic analysis based upon the unit hydrograph principle. A unit hydrograph is defined as the hydrograph of one inch of direct runoff from the tributary area resulting from a storm of a given duration. The unit hydrograph thus represents the integrated effects of factors such as tributary area, shape, street pattern, channel capacities, and street and land slopes. The basic premise of the unit hydrograph is that individual hydrographs resulting from the successive increments of excess rainfall that occur throughout a storm period will be proportional in discharge throughout their runoff period. Thus, the hydrograph of total storm discharge is obtained by summing the ordinates of the individual sub-hydrographs.

CUHP has been developed and calibrated using rainfall-runoff data collected in Colorado (mostly in the Denver/Boulder metropolitan area). This section provides a general background in the use of the computer version of CUHP to perform stormwater runoff calculations. A detailed description of the CUHP method and the assumptions and equations used, including a hand calculation example, are provided in the CUHP User Manual. The latest version of the CUHP 2005 macro-enabled Excel workbook and User Manual are available for download from www.udfcd.org.

3.2 **Effective Rainfall for CUHP**

Effective rainfall is that portion of precipitation during a storm event that runs off the land to streams. Those portions of precipitation that do not reach a stream are called abstractions and include interception by vegetation, evaporation, infiltration, storage in all surface depressions, and extended duration surface retention. The total design rainfall depth for use with CUHP should be obtained from the Rainfall chapter of the USDCM. This chapter illustrates a method for estimating the amount of rainfall that actually becomes surface runoff whenever a design rainstorm is used.

3.2.1 **Pervious-Impervious Areas**

As described in Section 2.5.1, the urban landscape is comprised of pervious and impervious surfaces. The degree of imperviousness is the primary variable that affects the volumes and rates of runoff calculated using CUHP. When analyzing a watershed for design purposes, the probable future percent of impervious area must first be estimated. A complete tabulation of recommended values of total percentage imperviousness is provided in Table 6-3 and Figures 6-1 through 6-3. References to impervious area and all calculations in this chapter are based on the input of total impervious areas. The pervious-impervious area relationship can be further refined for use in CUHP as follows:

- **DCIA**: Impervious area portion directly connected to the drainage system.
- **UIA:** Impervious area portion that drains onto or across pervious surfaces.
- **RPA**: The portion of pervious area receiving runoff from impervious portions.
- **SPA:** The separate pervious area portion not receiving runoff from impervious surfaces.

This further refinement is explained in more detail in the CUHP User Manual and in Chapter 3 of the USDCM Volume 3.



APPENDIX D

GEC PLANSET

- STORMWATER DISCHARGES FROM CONSTRUCTION SITES SHALL NOT CAUSE OR THREATEN TO CAUSE POLLUTION, CONTAMINATION, OR DEGRADATION OF STATE WATERS. ALL WORK AND EARTH DISTURBANCE SHALL BE DONE IN A MANNER THAT MINIMIZES POLLUTION OF ANY ON-SITE OR OFF-SITE WATERS, INCLUDING
- NOTWITHSTANDING ANYTHING DEPICTED IN THESE PLANS IN WORDS OR GRAPHIC REPRESENTATION, ALL DESIGN AND CONSTRUCTION RELATED TO ROADS, STORM DRAINAGE, AND EROSION CONTROL SHALL CONFORM TO THE STANDARDS AND REQUIREMENTS OF THE MOST RECENT VERSION OF THE RELEVANT ADOPTED EL PASO COUNTY STANDARDS, INCLUDING THE LAND DEVELOPMENT CODE, THE ENGINEERING CRITERIA MANUAL, THE DRAINAGE CRITERIA MANUAL, AND THE DRAINAGE CRITERIA MANUAL VOLUME 2. ANY DEVIATIONS FROM REGULATIONS AND STANDARDS MUST BE REQUESTED, AND APPROVED, IN WRITING.
- A SEPARATE STORMWATER MANAGEMENT PLAN (SWMP) FOR THIS PROJECT SHALL BE COMPLETED AND AN EROSION AND STORMWATER QUALITY CONTROL PERMIT (ESQCP) ISSUED PRIOR TO COMMENCING CONSTRUCTION, MANAGEMENT OF THE SWMP DURING CONSTRUCTION IS THE RESPONSIBILITY OF THE DESIGNATED QUALIFIED STORMWATER MANAGER OR CERTIFIED EROSION CONTROL INSPECTOR. THE SWMP SHALL BE LOCATED ON SITE AT ALL TIMES DURING CONSTRUCTION AND SHALL BE KEPT UP TO DATE WITH WORK PROGRESS
- ONCE THE ESQCP IS APPROVED AND A "NOTICE TO PROCEED" HAS BEEN ISSUED, THE CONTRACTOR MAY INSTALL THE INITIAL STAGE EROSION AND SEDIMENT CONTROL MEASURES AS INDICATED ON THE APPROVED GEC. A PRECONSTRUCTION MEETING BETWEEN THE CONTRACTOR, ENGINEER, AND EL PASO COUNTY WILL BE HELD PRIOR TO ANY CONSTRUCTION. IT IS THE RESPONSIBILITY OF THE APPLICANT TO COORDINATE THE MEETING TIME AND PLACE WITH COUNTY STAFF.
- CONTROL MEASURES MUST BE INSTALLED PRIOR TO COMMENCEMENT OF ACTIVITIES THAT COULD CONTRIBUTE POLLUTANTS TO STORMWATER. CONTROL MEASURES FOR ALL SLOPES, CHANNELS, DITCHES, AND DISTURBED LAND AREAS SHALL BE INSTALLED IMMEDIATELY UPON COMPLETION OF THE DISTURBANCE.
- ALL TEMPORARY SEDIMENT AND FROSION CONTROL MEASURES SHALL BE MAINTAINED AND REMAIN IN FEFFCTIVE OPERATING CONDITION UNTIL PERMANENT SOIL FROSION CONTROL MEASURES ARE IMPLEMENTED AND FINAL STABILIZATION IS ESTABLISHED. ALL PERSONS ENGAGED IN LAND DISTURBANCE ACTIVITIES SHALL ASSESS THE ADEQUACY OF CONTROL MEASURES AT THE SITE AND IDENTIFY IF CHANGES TO THOSE CONTROL MEASURES ARE NEEDED TO ENSURE THE CONTINUED EFFECTIVE PERFORMANCE OF THE CONTROL MEASURES. ALL CHANGES TO TEMPORARY SEDIMENT AND EROSION CONTROL MEASURES MUST BE INCORPORATED INTO THE STORMWATER MANAGEMENT PLAN.
- TEMPORARY STABILIZATION SHALL BE IMPLEMENTED ON DISTURBED AREAS AND STOCKPILES WHERE GROUND-DISTURBING CONSTRUCTION ACTIVITY HAS PERMANENTLY CEASED OR TEMPORARILY CEASED FOR LONGER THAN 14 DAYS.
- FINAL STABILIZATION MUST BE IMPLEMENTED AT ALL APPLICABLE CONSTRUCTION SITES, FINAL STABILIZATION IS ACHIEVED WHEN ALL GROUND-DISTURBING ACTIVITIES ARE COMPLETE AND ALL DISTURBED AREAS EITHER HAVE A UNIFORM VEGETATIVE COVER WITH INDIVIDUAL PLANT DENSITY OF 70 PERCENT OF PRE-DISTURBANCE LEVELS ESTABLISHED OR EQUIVALENT PERMANENT ALTERNATIVE STABILIZATION METHOD IS IMPLEMENTED. ALL TEMPORARY SEDIMENT AND EROSION CONTROL MEASURES SHALL BE REMOVED UPON FINAL
- ALL PERMANENT STORMWATER MANAGEMENT FACILITIES SHALL BE INSTALLED AS DESIGNED IN THE APPROVED PLANS, ANY PROPOSED CHANGES THAT EFFECT THE DESIGN OR FUNCTION OF PERMANENT STORMWATER MANAGEMENT STRUCTURES MUST BE APPROVED BY THE ECM ADMINISTRATOR PRIOR TO IMPLEMENTATION.
- EARTH DISTURBANCES SHALL BE CONDUCTED IN SUCH A MANNER SO AS TO EFFECTIVELY MINIMIZE ACCELERATED SOIL EROSION AND RESULTING SEDIMENTATION. ALL DISTURBANCES SHALL BE DESIGNED, CONSTRUCTED, AND COMPLETED SO THAT THE EXPOSED AREA OF ANY DISTURBED LAND SHALL BE LIMITED TO THE SHORTEST PRACTICAL PERIOD OF TIME. PRE-EXISTING VEGETATION SHALL BE PROTECTED AND MAINTAINED WITHIN 50 HORIZONTAL FEET OF A WATERS OF THE STATE UNLESS SHOWN TO BE INFEASIBLE AND SPECIFICALLY REQUESTED AND APPROVED.
- COMPACTION OF SOIL MUST BE PREVENTED IN AREAS DESIGNATED FOR INFILTRATION CONTROL MEASURES OR WHERE FINAL STABILIZATION WILL BE ACHIEVED BY VEGETATIVE COVER. AREAS DESIGNATED FOR INFILTRATION CONTROL MEASURES SHALL ALSO BE PROTECTED FROM SEDIMENTATION DURING CONSTRUCTION UNTIL FINAL STABILIZATION IS ACHIEVED. IF COMPACTION PREVENTION IS NOT FEASIBLE DUE TO SITE CONSTRAINTS, ALL AREAS DESIGNATED FOR INFILTRATION AND VEGETATION CONTROL MEASURES MUST BE LOOSENED PRIOR TO INSTALLATION OF THE CONTROL MEASURE(S).
- ANY TEMPORARY OR PERMANENT FACILITY DESIGNED AND CONSTRUCTED FOR THE CONVEYANCE OF STORMWATER AROUND, THROUGH, OR FROM THE EARTH DISTURBANCE AREA SHALL BE A STABILIZED CONVEYANCE DESIGNED TO MINIMIZE EROSION AND THE DISCHARGE OF SEDIMENT OFF SITE.
- CONCRETE WASH WATER SHALL BE CONTAINED AND DISPOSED OF IN ACCORDANCE WITH THE SWMP. NO WASH WATER SHALL BE DISCHARGE TO OR ALLOWED TO ENTER STATE WATERS, INCLUDING ANY SURFACE OR SUBSURFACE STORM DRAINAGE SYSTEM OR FACILITIES. CONCRETE WASHOUTS SHALL NOT BE LOCATED IN AN AREA WHERE SHALLOW GROUNDWATER MAY BE PRESENT, OR WITHIN 50 FEET OF A SURFACE WATER BODY, CREEK, OR STREAM.
- DURING DEWATERING OPERATIONS OF UNCONTAMINATED GROUND WATER MAY BE DISCHARGED ON SITE. BUT SHALL NOT LEAVE THE SITE IN THE FORM OF SURFACE RUNOFF UNLESS AN APPROVED STATE DEWATERING PERMIT IS IN PLACE.
- EROSION CONTROL BLANKETING OR OTHER PROTECTIVE COVERING SHALL BE USED ON SLOPES 3:1 AND STEEPER,
- CONTRACTOR SHALL BE RESPONSIBLE FOR THE REMOVAL OF ALL WASTES FROM THE CONSTRUCTION SITE FOR DISPOSAL IN ACCORDANCE WITH LOCAL AND STATE REGULATORY REQUIREMENTS. NO CONSTRUCTION DEBRIS, TREE SLASH, BUILDING MATERIAL WASTES, OR UNUSED BUILDING MATERIALS SHALL BE BURIED, DUMPED, OR DISCHARGED AT THE
- WASTE MATERIALS SHALL NOT BE TEMPORARILY PLACED OR STORED IN THE STREET, ALLEY, OR OTHER PUBLIC WAY, UNLESS IN ACCORDANCE WITH AN APPROVED TRAFFIC CONTROL PLAN. CONTROL MEASURES MAY BE REQUIRED BY EL PASO COUNTY ENGINEERING IF DEEMED NECESSARY, BASED ON SPECIFIC CONDITIONS AND CIRCUMSTANCES.
- TRACKING OF SOILS AND CONSTRUCTION DEBRIS OFF SITE SHALL BE MINIMIZED. MATERIALS TRACKED OFF SITE SHALL BE CLEANED UP AND PROPERLY DISPOSED OF
- THE OWNER/DEVELOPER SHALL BE RESPONSIBLE FOR THE REMOVAL OF ALL CONSTRUCTION DEBRIS, DIRT, TRASH, ROCK, SEDIMENT, SOIL, AND SAND THAT MAY ACCUMULATE IN ROADS, STORM DRAINS, AND OTHER DRAINAGE CONVEYANCE SYSTEMS AND STORMWATER APPURTENANCES AS A RESULT OF SITE DEVELOPMENT
- THE QUANTITY OF MATERIALS STORED ON THE PROJECT SITE SHALL BE LIMITED, AS MUCH AS PRACTICAL, TO THAT QUANTITY REQUIRED TO PERFORM THE WORK IN AN ORDERLY SEQUENCE, ALL MATERIALS STORED ON SITE SHALL BE STORED IN A NEAT, ORDERLY MANNER, IN THEIR ORIGINAL CONTAINERS, AND WITH ORIGINAL MANUFACTURER'S LABELS.
- NO CHEMICAL(S) HAVING THE POTENTIAL TO BE RELEASED IN STORMWATER ARE TO BE STORED OR USED ON SITE UNLESS PERMISSION FOR THE USE OF SUCH CHEMICAL(S) IS GRANTED IN WRITING BY THE ECM ADMINISTRATOR, IN GRANTING APPROVAL FOR THE USE OF SUCH CHEMICAL(S), SPECIAL CONDITIONS AND MONITORING MAY BE REQUIRED
- BULK STORAGE OF ALLOWED PETROLEUM PRODUCTS OR OTHER ALLOWED LIQUID CHEMICALS IN EXCESS OF 55 GALLONS SHALL REQUIRE ADEQUATE SECONDARY CONTAINMENT PROTECTION TO CONTAIN ALL SPILLS ON SITE AND TO PREVENT ANY SPILLED MATERIALS FROM ENTERING STATE WATERS, ANY SURFACE OR SUBSURFACE STORM DRAINAGE SYSTEM, OR OTHER FACILITIES.
- NO PERSON SHALL CAUSE THE IMPEDIMENT OF STORMWATER FLOW IN THE CURB AND GUTTER OR DITCH EXCEPT WITH APPROVED SEDIMENT CONTROL MEASURES.
- OWNER/DEVELOPER AND THEIR AGENTS SHALL COMPLY WITH THE "COLORADO WATER QUALITY CONTROL ACT" (TITLE 25, ARTICLE 8, CRS) AND THE "CLEAN WATER ACT" (33 USC 1344), IN ADDITION TO THE REQUIREMENTS OF THE LAND DEVELOPMENT CODE, DCM VOLUME II AND THE ECM APPENDIX I. ALL APPROPRIATE PERMITS MUST BE OBTAINED BY THE CONTRACTOR PRIOR TO CONSTRUCTION (1041, NPDES, FLOODPLAIN, 404, FUGITIVE DUST, ETC.). IN THE EVENT OF CONFLICTS BETWEEN THESE REQUIREMENTS AND OTHER LAWS, RULES, OR REGULATIONS OF OTHER FEDERAL, STATE, LOCAL, OR COUNTY AGENCIES, THE MOST RESTRICTIVE LAWS, RULES, OR REGULATIONS SHALL APPLY.
- ALL CONSTRUCTION TRAFFIC MUST ENTER/EXIT THE SITE ONLY AT APPROVED CONSTRUCTION ACCESS POINTS
- 26. PRIOR TO CONSTRUCTION, THE PERMITTEE SHALL VERIFY THE LOCATION OF EXISTING UTILITIES.
- 27. A WATER SOURCE SHALL BE AVAILABLE ON SITE DURING EARTHWORK OPERATIONS AND SHALL BE UTILIZED AS REQUIRED TO MINIMIZE DUST FROM EARTHWORK EQUIPMENT AND
- 28. THE SOILS REPORT FOR THIS SITE WAS PREPARED BY EARTH ENGINEERING CONSULTANTS, LLC (DATED 09/08/14) AND SHALL BE CONSIDERED A PART OF THESE PLANS.
- AT LEAST TEN (10) DAYS PRIOR TO THE ANTICIPATED START OF CONSTRUCTION, FOR PROJECTS THAT WILL DISTURB ONE (1) ACRE OR MORE, THE OWNER OR OPERATOR OF CONSTRUCTION ACTIVITY SHALL SUBMIT A PERMIT APPLICATION FOR STORMWATER DISCHARGE TO THE COLORADO DEPARTMENT OF PUBLIC HEALTH AND ENVIRONMENT, WATER QUALITY DIVISION. THE APPLICATION CONTAINS CERTIFICATION OF COMPLETION OF A STORMWATER MANAGEMENT PLAN (SWMP), OF WHICH THIS GRADING AND EROSION CONTROL PLAN MAY BE A PART. FOR INFORMATION OR APPLICATIONS MATERIALS, CONTACT:

COLORADO DEPARTMENT OF PUBLIC HEALTH AND ENVIRONMENT WATER QUALITY CONTROL DIVISION WOCD - PERMITS 4300 CHERRY CREEK DRIVE SOUTH DENVER, CO 80246-1530 ATTN PERMITS LINIT

EROSION CONTROL NOTES (CONT'D):

- 30. SEED AND MULCH ALL DISTURBED AREAS THAT WILL NOT HAVE IMPROVEMENTS (I.E. PAVED ROADS, RIPRAP, ETC.).
- 31. NO BATCH PLANTS ARE PROPOSED AS A PART OF THIS PROJECT
- 32. THERE ARE NO STREAM CROSSINGS WITHIN THE LIMITS OF THIS PROJECT.
- 33. BMPs MUST BE INSTALLED PRIOR TO LAND DISTURBANCE. SEE LEGEND FOR PHASED BMPs (INITIAL/INTERIM/FINAL) FOR THIS PROJECT.
- 34. PROPOSED BUILDING SITE/LANDSCAPING IS LOCATED OUTSIDE OF FLOODPLAIN
- 35. J-HOOKS TO BE INSTALLED WHEREVER SILT FENCE IS INSTALLED PERPENDICULAR TO CONTOURS.
- THE PARTIES RESPONSIBLE FOR THIS PLAN HAVE FAMILIARIZED THEMSELVES WITH ALL CURRENT ACCESSIBILITY CRITERIA AND SPECIFICATIONS AND THE PROPOSED PLAN REFLECTS ALL SITE ELEMENTS REQUIRED BY THE APPLICABLE ADA DESIGN STANDARDS AND GUIDELINES AS PUBLISHED BY THE UNITED STATES DEPARTMENT OF JUSTICE. APPROVAL OF THIS PLAN BY EL PASO COUNTY DOES NOT ASSURE COMPLIANCE WITH THE ADA OR ANY REGULATIONS OR GUIDELINES ENACTED OR PROMULGATED UNDER OR WITH RESPECT TO SUCH LAWS.
- 37. EXISTING VEGETATION CONSISTS OF NATIVE GRASSES/WEEDS WITH APPROXIMATELY 75% GROUND COVER

TIMING, CONSTRUCTION STAGING, AND SEQUENCING:

EXPECTED START DATE: FALL 2022 INSTALL TEMPORARY EROSION CONTROL: 2-4 DAYS - PERIMETER SILT FENCING

- VEHICLE TRACKING CONTROL PAD
- CONCRETE WASHOUT

ROUGH GRADING - 5 DAYS INSTALL FINAL SITE IMPROVEMENTS - 10 MONTHS REMOVE TEMPORARY EROSION CONTROL - 5 DAYS

EARTHWORK SUMMARY:

PROPOSED SITE: CUT - 3,855.2 CY <u>FILL - 1,688.6 (*1.15) = 1,941.9 CY</u> NET - 1,913.3 CY CUT

DISTURBED AREA - 152,246 SF, 3.50 AC

EROSION CONTROL FACILITIES:

SILT FENCE - 1337 LF VEHICLE TRACKING PAD (VT) - 1 CURB SOCK LOCATIONS -ROCK CHECK DAMS - 4 CONCRETE WASHOUT - 1 EROSION CONTROL BLANKET - 884 SY TEMPORARY SEDIMENT BASIN -

OVERALL LOT COVERAGE

AREA OF TRACT	336,719
AREA OF BUILDING (EXISTING REATMENT FACILITY)	3,727±
AREA OF BUILDING (PROPOSED ADMIN. BLDG.)	4,542
6 TRACT COVERAGE WITH MPROVEMENTS (INCLUDING PROPOSED ADMIN. BLDG.)	15%
OTAL IMPERVIOUS AREA (PROPOSED MPROVEMENTS)	36,376

MINIMUM BEST MANAGEMENT PRACTICES ELEMENTS:

- STEP 1- EROSION AND SEDIMENT CONTROL
- INSTALL SEDIMENT TRAPPING DEVICES (PERIMETER CONTROLS) PRIOR TO THE START OF CONSTRUCTION.
- PREVENTION AND RESPONSE
- STEP 3- MATERIAL MANAGEMENT
 - MATERIAL AND EQUIPMENT STORAGE AREAS SHALL BE SECURE AND CONTAINED TO PREVENT DISCHARGE OF ANY MATERIAL IN RUNOFF, WASTE SHALL BE CONTAINED AND DISPOSED OF PROPERLY. MAINTAIN BMP'S DURING BUILDING AND UTILITY CONSTRUCTION.
- STEP 4- INSPECTION AND MAINTENANCE (SEE EROSION CONTROL NOTES)
 STEP 5- INSTALL FINAL STABILIZATION PAVEMENT, LANDSCAPING, EROSION CONTROL BLANKETS, AND SEEDING
- REMOVE TEMPORARY CONTROLS SILT FENCING, CURB SOCK AFTER PERMANENT FEATURES ARE INSTALLED.

FINAL STABILIZATION AND LONG-TERM STORMWATER MANAGEMENT:

FINAL STABILIZATION MEASURES INCLUDE PAVEMENT, PARTIAL LANDSCAPE, AND REVEGETATION.

ALL AREAS DISTURBED BY EARTHWORK SHALL BE PERMANENTLY REVEGETATED WITH GRASS MIX BY <u>DRILL SEEDING</u>. SEED MIX FOR THIS PROJECT SHALL BE AS FOLLOWS (SEE BELOW):

RECOMMENDED VARIETY	% OF SEED MIX	PLS RATE PER ACRE, DOUBLE IF BROADCAST
KAW, BISON, CHAMP	20.0%	1.08
LOVINGTON, HACHITA, ALMA	10.0%	0.12
LODORM	10.0%	0.48
ARRIBA, BARTON	20.0%	1.60
VAUGHN, BUTTE, EL RENO, NINER	10.0%	0.46
BLACKWELL, GREENVILLE	10.0%	0.20
GOSHEN, PRONGHORN	10.0%	0.32
CHEYENNE, HOLT, LLANO	10.0%	0.51
	VARIETY KAW, BISON, CHAMP LOVINGTON, HACHITA, ALMA LODORM ARRIBA, BARTON VAUGHN, BUTTE, EL RENO, NINER BLACKWELL, GREENVILLE GOSHEN, PRONGHORN CHEYENNE,	VARIETY MIX KAW, BISON, CHAMP 20.0% LOVINGTON, HACHITA, ALMA 10.0% ARRIBA, BARTON 20.0% VAUGHN, BUTTE, EL RENO, NINER BLACKWELL, GREENVILLE GOSHEN, PRONGHORN 10.0% CHEYENNE, 10.0%

GENERAL GRASS SEEDING NOTES:

- AN ESTABLISHED STAND OF GRASS IN THIS COLORADO CLIMATE IS DEFINED AS 2 TO 3 PLANTS IN A SQUARE FOOT AREA.
 GRASSES MUST BE PLANTED IN A FIRM, WEED-FREE SEEDBED, PRIMARILY BECAUSE SUCCESS DEPENDS UPON GOOD SOIL-TO-SEED CONTACT. IF YOU ARE BROADCASTING SEED, IT MUST BE RAKED INTO THE SOIL. NATIVE GRASS SEED IS PLANTED ONLY 1/4 TO 1/2 INCHES DEEP. LOOSE SOIL DRIES OUT QUICKLY AT THE SURFACE COMPARED TO FIRM SOIL.
- MOST GRASSES SHOULD BE PLANTED WITH A GRASS DRILL, BUT BROADCASTING CAN ALSO BE USED. A DOUBLE DISC DRILL WITH AN AGITATOR IS RECOMMENDED FOR SEEDING. IF USING A GRASS DRILL, THE AMOUNT OF SEED NEEDED WILL BE CUT IN HALF SINCE THE METHOD OF PLANTING
- IN MOST CASES, A GRASS SEEDLING NEEDS NO FERTILIZER DURING ESTABLISHMENT. HOWEVER, ON DISTURBED SITES, SUCH AS AREAS AROUND A NEW HOUSE, WATER LINES, TRENCHING, ETC., SOIL AMENDMENTS MAY BE REQUIRED TO MAINTAIN THE VIGOR OF THE GRASSES.
 RECOMMENDED SEEDING DATES FOR COLORADO ARE NOVEMBER 1 TO MAY 1, WHEN THE SOIL IS NOT FROZEN. GRASSES SHOULD BE SEEDED
- WHEN SOIL MOISTURE AND TEMPERATURE ARE OPTIMUM FOR GERMINATION. GRASSES ARE DESIGNATED EITHER 'COOL' OR 'WARM' SEASON BASED ON THEIR GROWTH CYCLE. COOL—SEASON GRASSES CAN BE PLANTED WHEN TEMPERATURES ARE COOLER AND DAY LENGTHS ARE SHORT. WARM—SEASON GRASSES NEED WARMER TEMPERATURES AND LONGER DAY LENGTHS TO GROW.
- A PROPER SEEDBED IS FIRM AND FREE OF COMPETING VEGETATION. CORRECT FIRMNESS IS WHEN AN ADULT FOOTPRINT IS ONLY SLIGHTLY VISIBLE ON THE PREPARED BED PRIOR TO THE SEEDING OPERATION. THE SEEDBED CAN BE FIRMED, IF NEEDED, BY PULLING A COMMERCIAL OR HOMEMADE PACKER OR ROLLER, A FIRM SEEDBED IS ESSENTIAL FOR PROPER SEEDING DEPTH, A LOOSE, FLUFFY BED WILL PLACE SEEDS TOO DEEP FOR PROPER GERMINATION.
- DEEP FOR PROPER GERMINATION.

 SEEDING NATIVE GRASSES IN A SUITABLE COVER CROP IS RECOMMENDED. A SUITABLE COVER CROP DECREASES EVAPORATION TO RETAIN SOIL

 MOISTURE, AND KEEPS SOIL TEMPERATURES LOWER BECAUSE OF SHADING. IT PROTECTS YOUNG GRASS SEEDLINGS FROM STRONG WINDS,
 COLLECTS SNOW DURING WINTER, AND MINIMIZES THE WEED PROBLEM. THE COVER CROP SHOULD BE PLANTED IN THE SPRING MAY 15 THROUGH
 JULY 15 BUT PREFERABLY BEFORE JUNE 15. GRASS IS SEEDED DIRECTLY INTO THE STANDING STUBBLE IN THE FALL. IF YOU ARE HAVING THE
 COVER CROP, LEAVE 18 INCHES ON SANDY SOIL AND 12 INCHES ON LOAMY OR HEAVIER SOILS. RECOMMENDED COVER CROPS ARE STERILE
 FORACE SORGHUM, LONG—SEASON MILO, MILLET, OATS, SUDAN GRASS, ETC.
 MOST GROWERS OF NATIVE GRASSES ARE CONVINCED THEY HAVE A FAILURE THE FIRST YEAR. MOST OF THE TIME THEY ACTUALLY HAVE A GOOD
 STAND. NATIVE GRASSES GROW DOWN, NOT UP, DURING THE ESTRADISHMENT YEAR. THE TOP GROWTH NORMALLY AMOUNTS TO A NARROW,
- STRAIGHT LEAF UNTIL LATE SUMMER. THESE SEEDLINGS CAN BE HARD TO SEE, EVEN FOR THE EXPERIENCED GROWER. BE PATIENT. DO NOT GRAZE FOR AT LEAST 2 TO 3 GROWING SEASONS AND AFTER THE GRASS IS ESTABLISHED.

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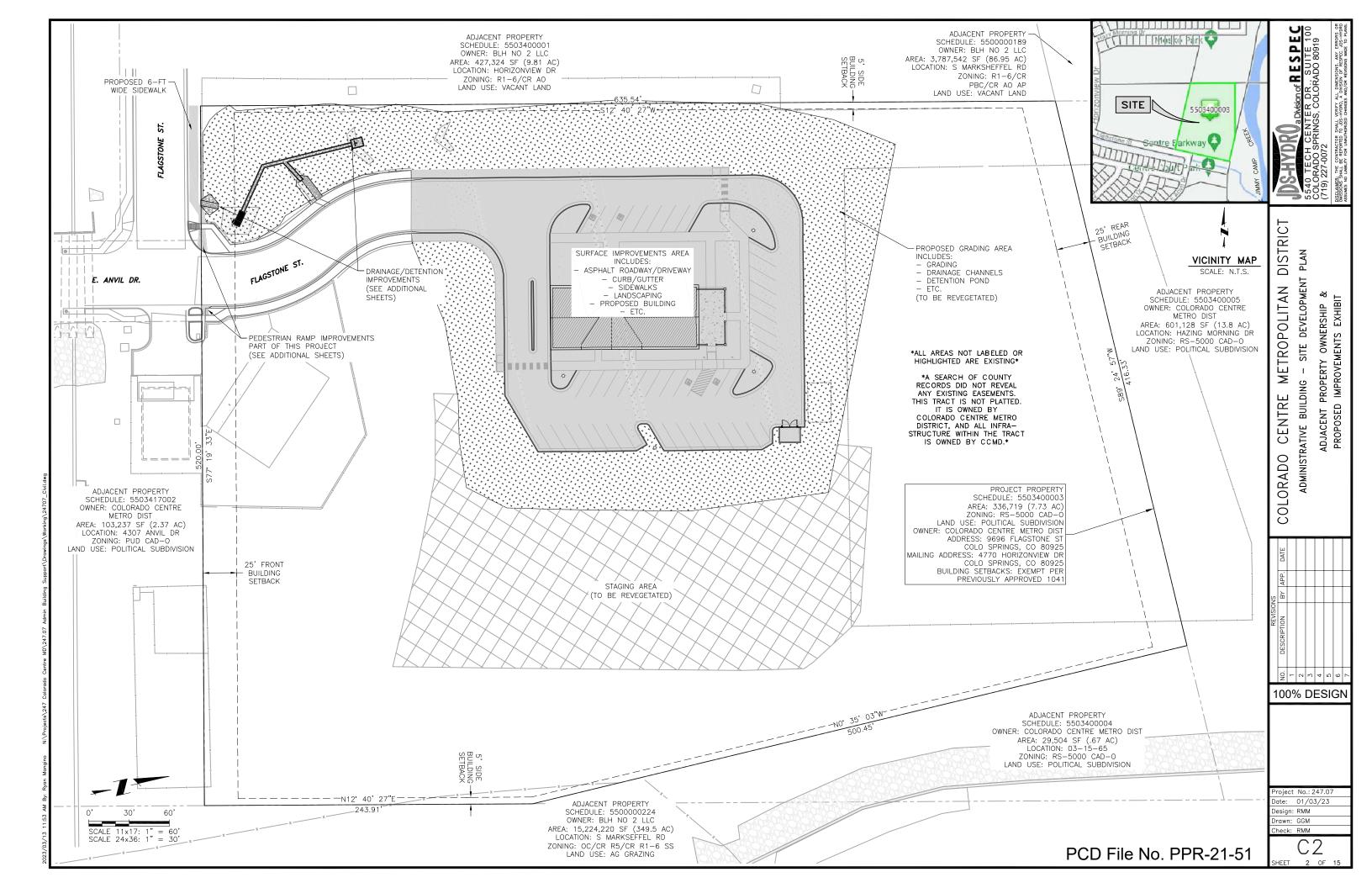
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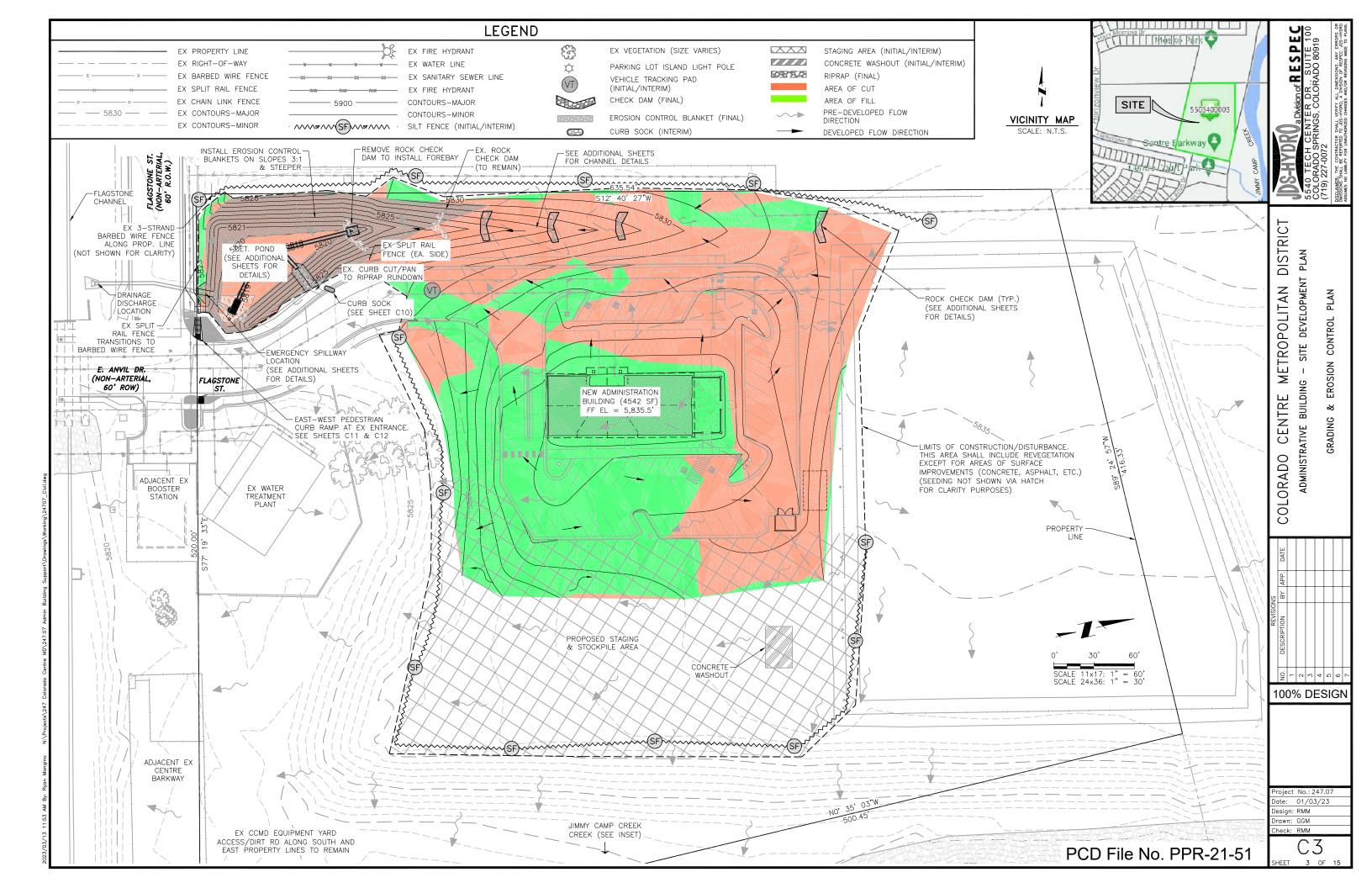
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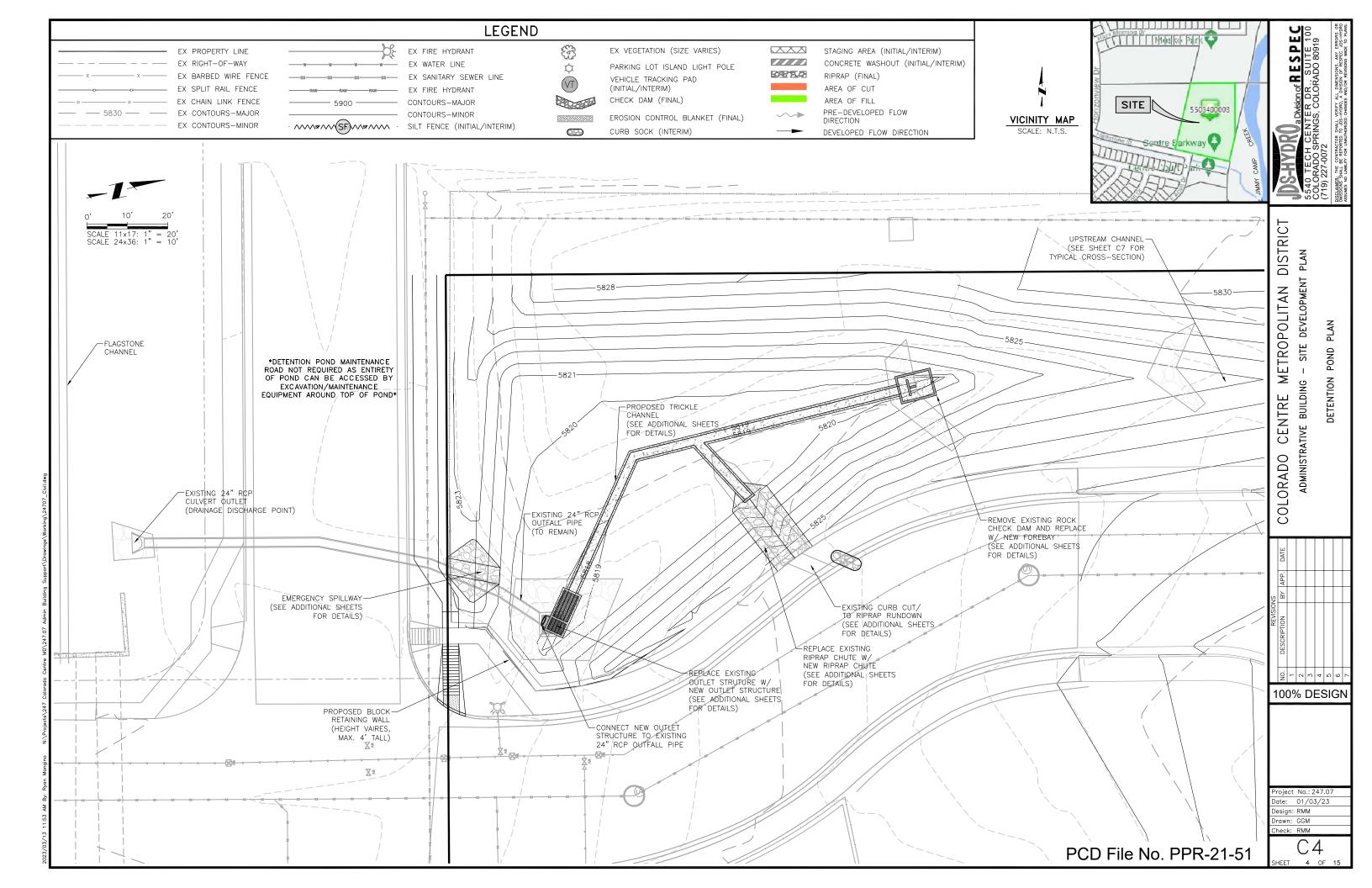
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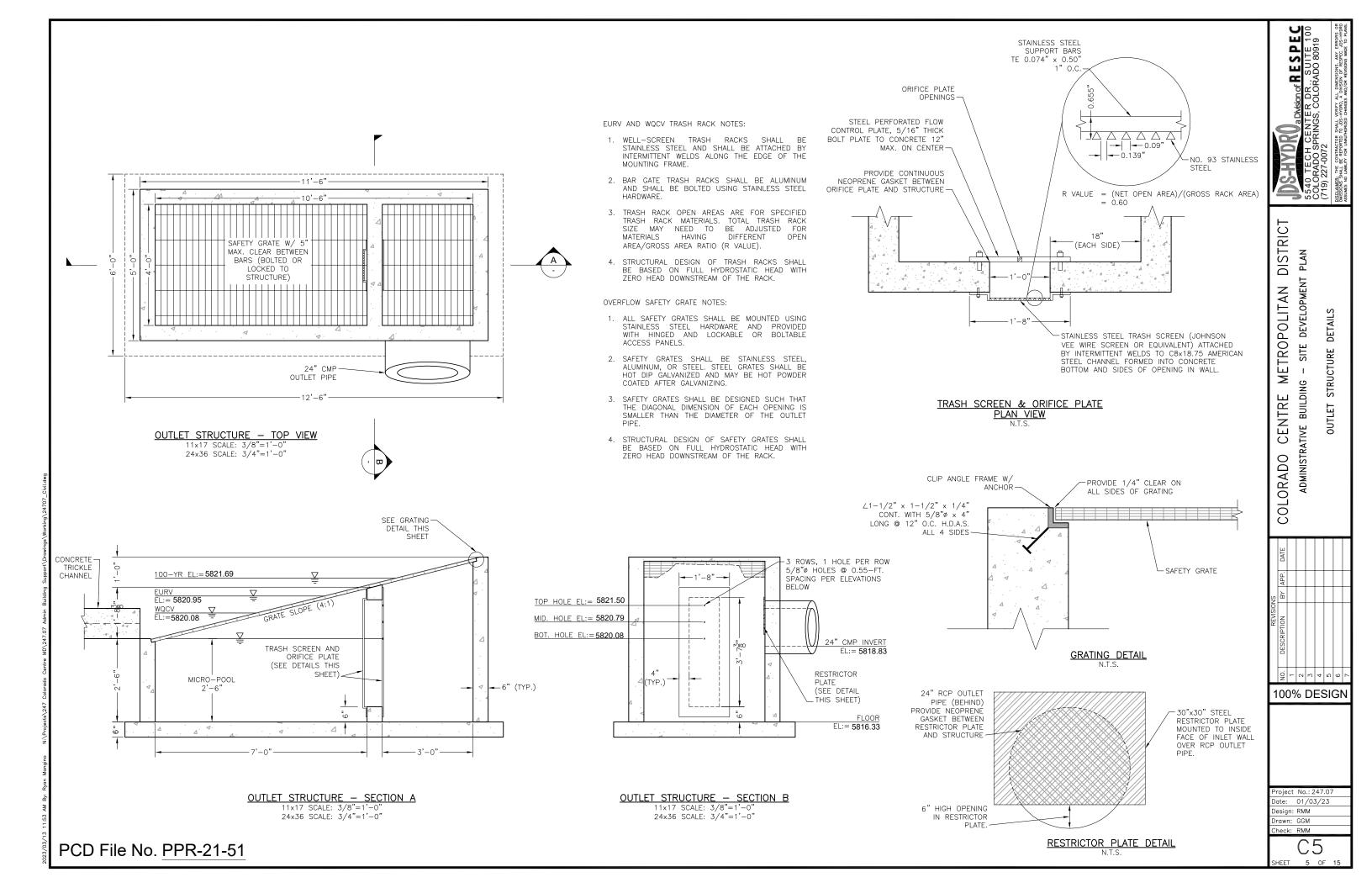
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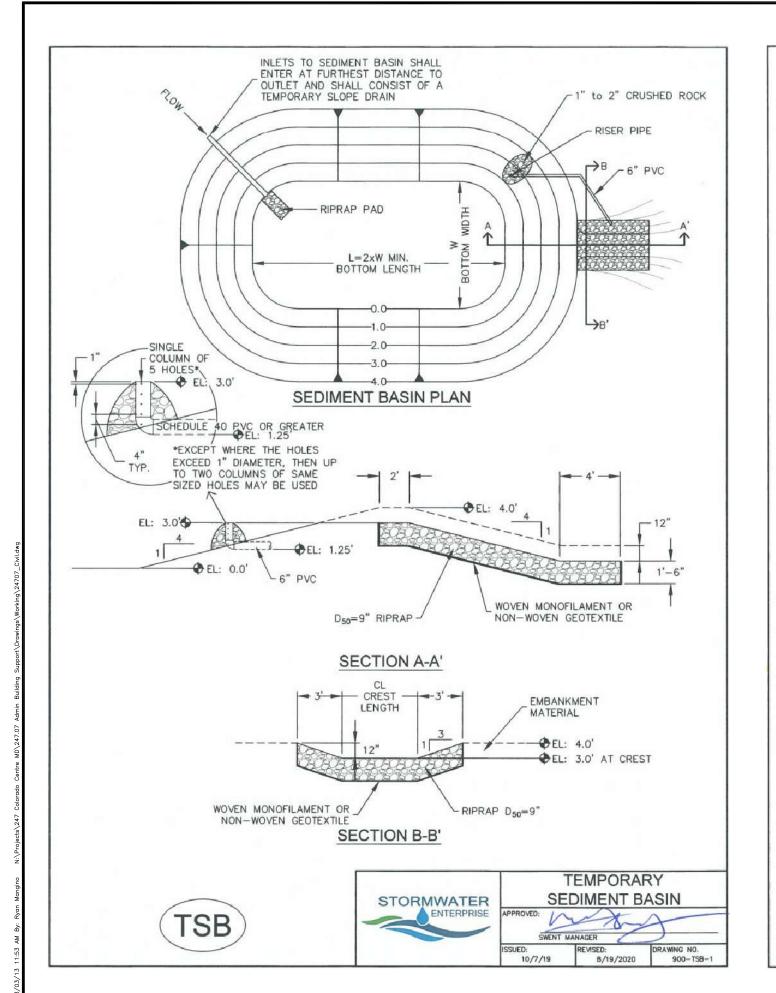


TABLE SB-1, SIZING INFORMATION FOR STANDARD SEDIMENT BASIN UPSTREAM DRAINAGE HOLE BASIN BOTTOM WIDTH SPILLWAY CREST AREA (ROUNDED TO DIAMETER LENGTH (CL), (FT) (W), (FT) (HD), (IN) NEAREST ACRE), (AC) 12½ %2 13/6 1/2 1/6 28 33% 38½ 43 2/32 2/32 25/32 25/32 27/32 7/8 471/4 51 12 55 13 5814 15 61 16 3/32 64 18 13 67% 19 1/16 70% 21 11/8 22 13/16 731/4

INSTALLATION NOTES

- FOR STANDARD BASIN, BOTTOM DIMENSION MAY BE MODIFIED AS LONG AS BOTTOM AREA IS NOT REDUCED.
- 2. EMBANKMENT MATERIAL SHALL CONSIST OF SOIL FREE OF DEBRIS, ORGANIC MATERIAL, AND ROCKS OR CONCRETE GREATER THAN 3 INCHES. AND SHALL HAVE A MINIMUM OF 15 PERCENT BY WEIGHT PASSING THE No. 200 SIEVE
- EMBANKMENT MATERIAL SHALL BE COMPACTED TO AT LEAST 95 PERCENT OF MAXIMUM DENSITY IN ACCORDANCE WITH ASTM D-698.
- PIPE SCHEDULE 40 OR GREATER SHALL BE USED.
- THE DETAILS SHOWN ON THESE SHEETS PERTAIN TO STANDARD SEDIMENT BASIN(S) FOR DRAINAGE AREAS LESS THAN 15 ACRES. SEE CONSTRUCTION DRAWINGS FOR EMBANKMENT, STORAGE VOLUME, SPILLWAY, OUTLET, AND OUTLET PROTECTION DETAILS FOR ANY SEDIMENT BASIN(S) THAT HAVE BEEN INDIVIDUALLY DESIGNED FOR DRAINAGE AREAS LARGER THAN 15 ACRES. DESIGN CALCULATIONS MUST BE APPROVED PRIOR TO IMPLEMENTATION.

MAINTENANCE NOTES

- FREQUENT OBSERVATIONS AND MAINTENANCE ARE NECESSARY TO MAINTAIN CONTROL MEASURES IN EFFECTIVE OPERATING CONDITION. INSPECTIONS AND CORRECTIVE MEASURES SHOULD BE DOCUMENTED THOROUGHLY.
- SEDIMENT ACCUMULATED IN BASIN SHALL BE REMOVED AS NEEDED TO MAINTAIN CONTROL MEASURE EFFECTIVENESS, TYPICALLY WHEN SEDIMENT DEPTH REACHES ONE FOOT (I.E. TWO FEET BELOW SPILLWAY CREST)
- SEDIMENT BASINS ARE TO REMAIN IN PLACE UNTIL THE UPSTREAM DISTURBED AREA IS PERMANENTLY
- PERMANENTLY STABILIZE AREA AFTER SEDIMENT BASIN REMOVAL.

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COLORADO



TEMPORARY SEDIMENT BASIN

PCD File No. PPR-21-51

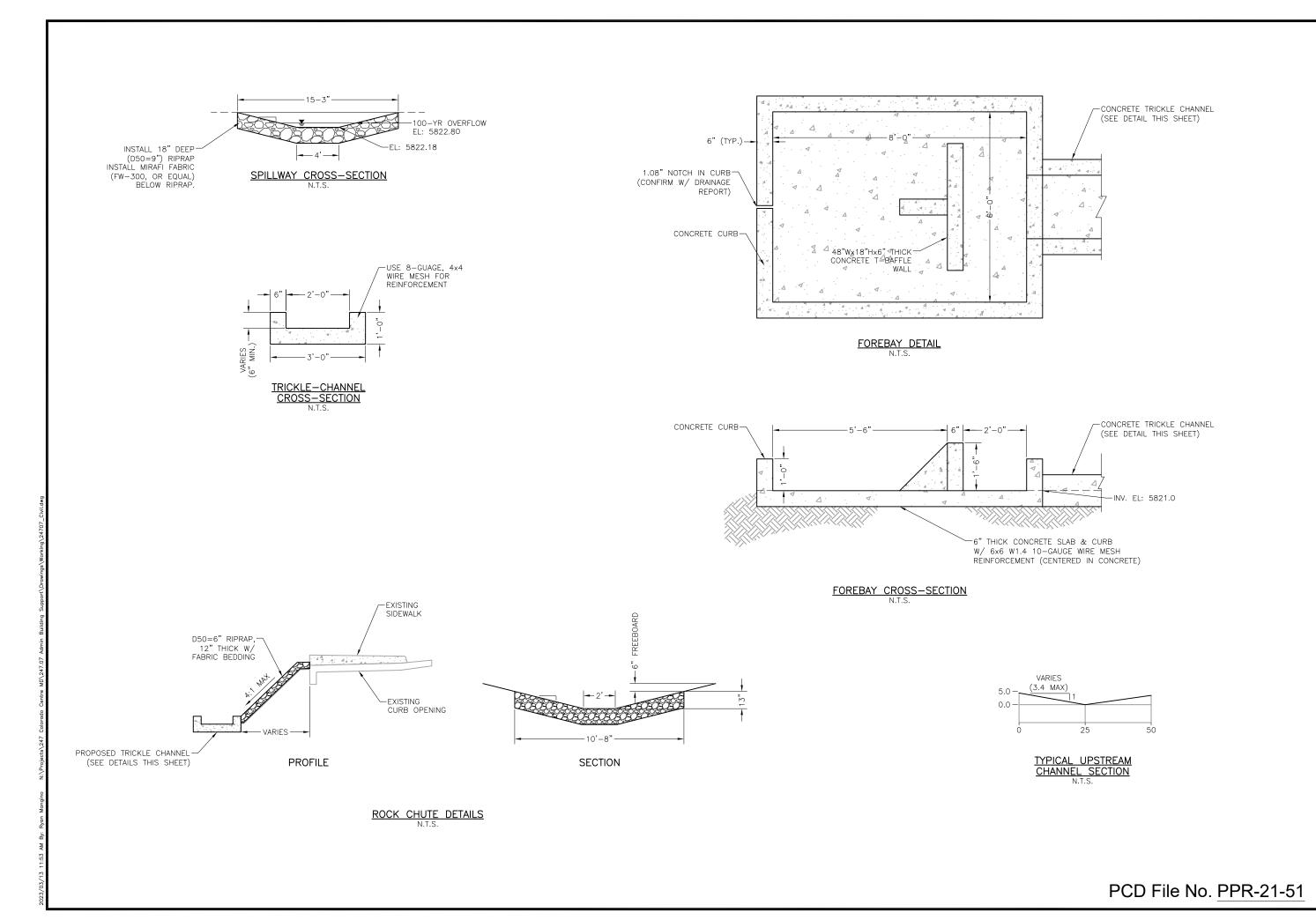
DISTRICT PLAN METROPOLITAN SEDIMENTATION BUILDING CENTRE

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COLORADO 80919

CENTRE METROPOLITAN DISTRICT SITE DEVELOPMENT PLAN ADMINISTRATIVE BUILDING COLORADO

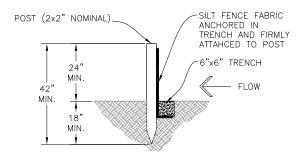
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Project No.: 247.07 Date: 01/03/23

Design: RMM Drawn: GGM Check: RMM



SILT FENCE DETAIL

INSTALLATION REQUIREMENTS:

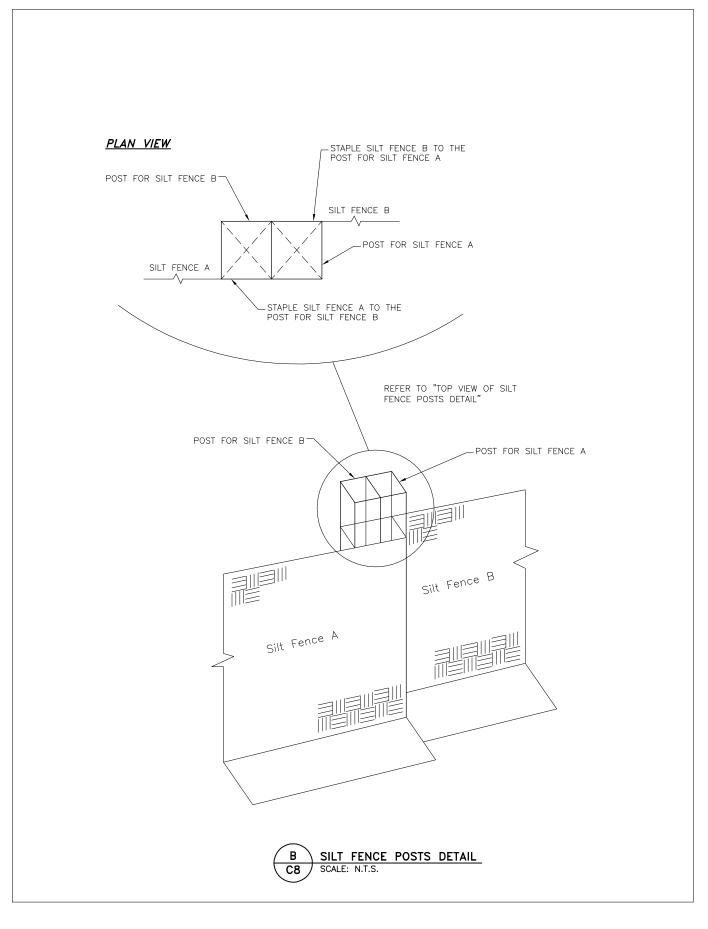
- SILT FENCES SHALL BE INSTALLED PRIOR TO ANY LAND DISTURBING ACTIVITIES.
- 2. WHEN JOINTS ARE NECESSARY, SILT FENCE GEOTEXTILE SHALL BE SPLICED TOGETHER ONLY AT SUPPORT POST AND SECURELY SEALED.
- 3. METAL POSTS SHALL BE "STUDDED TEE" OR "U" TYPE WITH MINIMUM WEIGHT OF 1.33 POUNDS PER LINEAR FOOT. WOOD POSTS SHALL HAVE A MINIMUM DIAMETER OR CROSS SECTION DIMENSION OF 2 INCHES.
- 4. THE FILTER MATERIAL SHALL BE FASTENED SECURELY TO METAL POSTS USING WIRE TIES, OR TO WOOD POSTS WITH 3/4" LONG #9 HEAVY—DUTY STAPLES. THE SILT FENCE GEOTEXTILE SHALL NOT BE STAPLED TO EXISTING TREES.
- 5. WHILE NOT REQUIRED, WIRE MESH FENCE MAY BE USED TO SUPPORT THE GEOTEXTILE. WIRE FENCE SHALL BE FASTENED SECURELY TO THE UPSLOPE SIDE OF THE POSTS USING HEAVY-DUTY WIRE STAPLES AT LEAST 3/4" LONG, TIE WIRES OR HOG RINGS. THE WIRE SHALL EXTEND INTO THE TRENCH A MINIMUM OF 6 INCHES AND SHALL NOT EXTEND MORE THAN 3 FEET ABOVE THE ORIGINAL GROUND SURFACE.

- 6. ALONG THE TOE OF FILLS, INSTALL THE SILT FENCE ALONG A LEVEL CONTOUR AND PROVIDE AN AREA BEHIND THE FENCE FOR RUNOFF TO POND AND SEDIMENT TO SETTLE. A MINIMUM DISTANCE OF 5 FEET FROM THE TOE OF THE FILL IS RECOMMENDED.
- 7. THE HEIGHT OF THE SILT FENCE FROM THE GROUND SURFACE SHALL BE MINIMUM OF 24 INCHES AND SHALL NOT EXCEED 36 INCHES. HIGHER FENCES MAY IMPOUND VOLUMES OF WATER SUFFICIENT TO CAUSE FAILURE OF THE STRUCTURE.

MAINTENANCE REQUIREMENTS:

- 1. CONTRACTOR SHALL INSPECT SILT FENCES IMMEDIATELY AFTER EACH RAINFALL, AT LEAST DAILY DURING PROLONGED RAINFALL, AND WEEKLY DURING PERIODS OF NO RAINFALL. DAMAGED, COLLAPSED, UNENTRENCHED OR INEFFECTIVE SILT FENCES SHALL BE PROMPTLY REPAIRED OR REPLACED.
- 2. SEDIMENT SHALL BE REMOVED FROM BEHIND SILT FENCE WHEN IT ACCUMULATES TO HALF THE EXPOSED GEOTEXTILE HEIGHT.
- 3. SILT FENCES SHALL BE REMOVED WHEN ADEQUATE VEGETATIVE COVER IS ATTAINED.





PCD File No. PPR-21-51

S540 TECH CENTER DR., SUITE 100 COLORADO SPRINGS, COLORADO 80919 (719) 227-0072 DESLAMER. THE CONTRACTOR SHALL VERIFY ALL DIMENSIONS, ANY ERRORS (DUSSIANLE RE PROMITMENTE ON DESPRENCE) A DESPRENCE SPRINGS AND VERSEN SAND WESTER OF SERVICE AND SERVICE SPRINGS AND VERSEN SAND VERSEN

COLORADO CENTRE METROPOLITAN DISTRICT ADMINISTRATIVE BUILDING - SITE DEVELOPMENT PLAN

DETAILS

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Project No.: 247.07 Date: 01/03/23

Design: RMM
Drawn: GGM
Check: RMM

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VEHICLE TRACKING PAD DETAIL

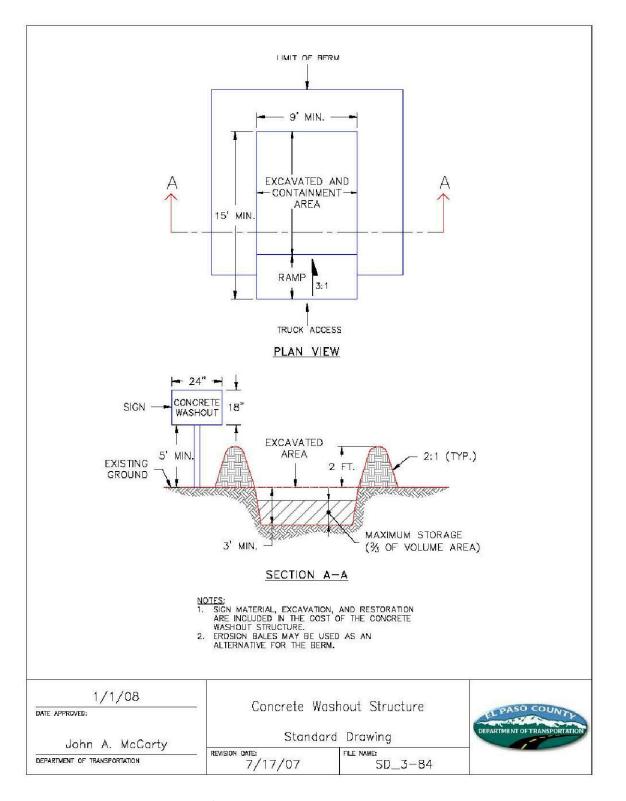
INSTALLATION REQUIREMENTS:

- ALL ENTRANCES TO THE CONSTRUCTION SITE ARE TO BE STABILIZED PRIOR TO COMMENCEMENT OF CONSTRUCTION.
- CONSTRUCTION ENTRANCES ARE TO BE BUILT WITH AN APRON TO ALLOW FOR TURNING TRAFFIC, BUT SHOULD NOT BE BUILT OVER EXISTING PAVEMENT EXCEPT FOR A SLIGHT OVERLAP.
- 3. AREAS TO BE STABILIZED ARE TO BE PROPERLY GRADED AND COMPACTED.
- 4. CONSTRUCTION ROADS, PARKING AREAS, LOADING/UNLOADING ZONES, STORAGE AREAS, AND STAGING AREAS ARE TO BE STABILIZED.
- 5. CONSTRUCTION ROADS ARE TO BE BUILT TO CONFORM TO SITE GRADES, BUT SHOULD NOT HAVE SIDE SLOPES OR ROAD GRADES THAT ARE EXCESSIVELY STEEP.

MAINTENANCE REQUIREMENTS

- REGULAR INSPECTIONS ARE TO BE MADE OF ALL STABILIZED AREAS, ESPECIALLY AFTER STORM EVENTS.
- 2. STONES ARE TO BE REAPPLIED PERIODICALLY AND WHEN REPAIR IS NECESSARY.
- 3. SEDIMENT TRACKED ONTO PAVED ROADS IS TO BE REMOVED DAILY BY SHOVELING OR SWEEPING. SEDIMENT IS NOT TO BE WASHED DOWN STORM SEWER DRAINS.
- 4. OTHER ASSOCIATED SEDIMENT CONTROL MEASURES ARE TO BE INSPECTED TO ENSURE GOOD WORKING CONDITION.
- 5. TO BE REMOVED JUST PRIOR TO FINAL SURFACING AND STABILIZATION.





B CONCRETE WASHOUT STRUCTURE DETAIL
C9 SCALE: N.T.S.

PCD File No. PPR-21-51

5540 TECH CENTER DR., SUITE 10 COLORADO SPRINGS, COLORADO 80919 (719) 227-0072

COLORADO CENTRE METROPOLITAN DISTRICT ADMINISTRATIVE BUILDING - SITE DEVELOPMENT PLAN

DETAILS

CONTROL

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Project No.: 247.07 Date: 01/03/23 Design: RMM

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CHECK DAM AND CURB SOCK INLET PROTECTION

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DETAILS

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GRADING

DR., SUITE 100 LORADO 80919

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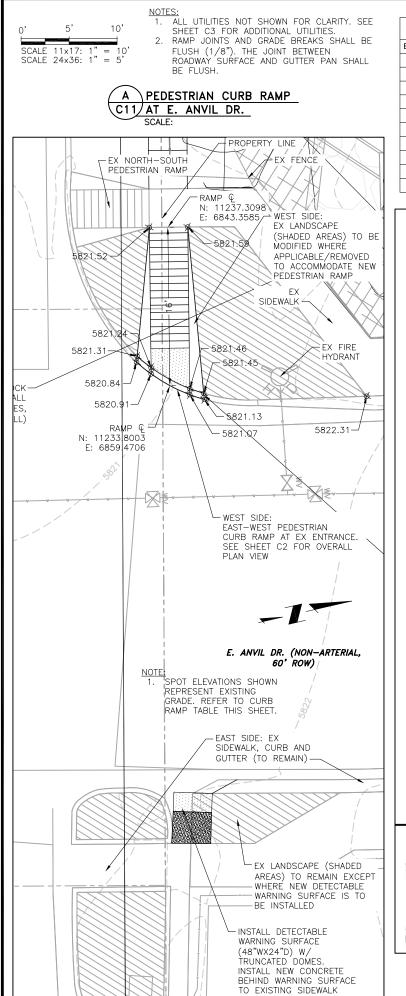
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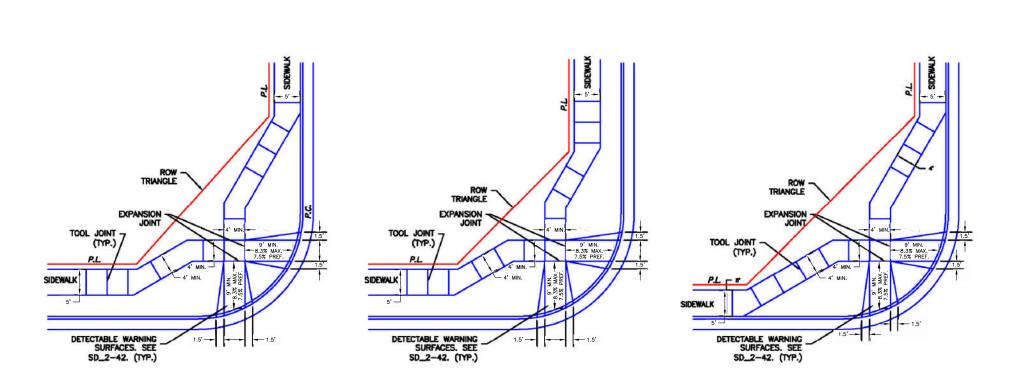
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EAST-WEST PEDESTRIAN CURB RAMP						
EXISTING EL	PROPOSED EL					
5821.59						
5821.46	5821.04					
5821.45	5821.40					
5821.13	5821.40					
5821.07						
5820.91						
5820.84	5821.24					
5821.31	5821.24					
5821.24	5821.04					
5821.52						



SCALE: NOT TO SCALE

Pedestrian Curb 6/23/20 Ramp Detail DATE APPROVED: Standard Drawing Jennifer E. Irvine REVISION DATE: 6/23/20 DEPARTMENT OF PUBLIC WORKS

SD_2-40

PEDESTRIAN CURB RAMP STANDARD C11 SCALE: N.T.S.



Project No.: 247.07 Date: 01/03/23 Design: RMM Drawn: GGM

100% DESIGN

sion of **RESPEC**N DR., SUITE 100
COLORADO 80919

DISTRICT

METROPOLITAN

CENTRE

COLORADO

DEVELOPMENT PLAN

BUILDING

DETAILS

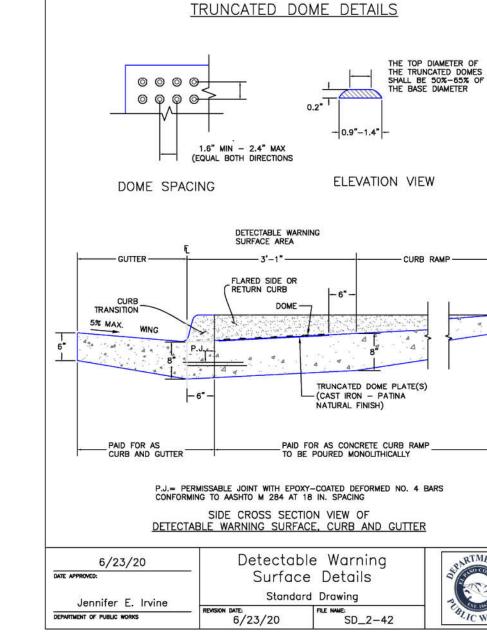
CONTROL

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GRADING

Check: RMM

PCD File No. PPR-21-51



DETECTABLE WARNING SURFACE C12 SCALE: N.T.S.

PEDESTRIAN CURB RAMP SCALE: N.T.S.

6/23/20

Pedestrian Curb

Ramp Detail

Standard Drawing

SD_2-41

THE COUNTER SLOPE OF THE GUTTER OR ROAD AT THE FOOT OF A RAMP SHALL NOT EXCEED 5%.

6/23/20

Jennifer E. Irvine

DATE APPROVED:

DEPARTMENT OF PUBLIC WORKS

nof **RESPE** DR., SUITE 10 LORADO 80919 DISTRICT PLAN METROPOLITAN BUILDING CENTRE COLORADO

CONTROL

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100% DESIGN

Project No.: 247.07 Date: 01/03/23 Design: RMM Drawn: GGM

> Check: RMM C 1 HEET 12 OF 15

Temporary and Permanent Seeding (TS/PS)

be otherwise stabilized. Effective seeding proper planting techniques, and protection of the seeded area with mulch, geotextiles,

EC-2

Photograph TS/PS -1. Equipment used to drill seed. Photo courtesy of Douglas County.

Appropriate Uses When the soil surface is disturbed and

or other appropriate measures.

Description

Temporary seeding can be used to

inactive for an extended period.

stabilize disturbed areas that will be

Permanent seeding should be used to

includes preparation of a seedbed,

stabilize areas at final grade that will not

selection of an appropriate seed mixture,

will remain inactive for an extended period (typically 30 days or longer),

proactive stabilization measures should be implemented. If the inactive period is short-lived (on the order of two weeks), techniques such as surface roughening may be appropriate. For longer periods of inactivity, temporary seeding and mulching can provide effective erosion control. Permanent seeding should be used on finished areas that have not been otherwise stabilized.

Typically, local governments have their own seed mixes and timelines for seeding. Check jurisdictional requirements for seeding and temporary stabilization.

Design and Installation

Effective seeding requires proper seedbed preparation, selection of an appropriate seed mixture, use of appropriate seeding equipment to ensure proper coverage and density, and protection with mulch or fabric

The USDCM Volume 2 Revegetation Chapter contains detailed seed mix, soil preparations, and seeding and mulching recommendations that may be referenced to supplement this Fact Sheet.

Drill seeding is the preferred seeding method. Hydroseeding is not recommended except in areas where steep slopes prevent use of drill seeding equipment, and even in these instances it is preferable to hand seed and mulch. Some jurisdictions do not allow hydroseeding or hydromulching.

Seedbed Preparation

Prior to seeding ensure that areas to be revegetated have soil conditions capable of supporting vegetation. Overlot grading can result in loss of topsoil, resulting in poor quality subsoils at the ground surface that have low nutrient value, little organic matter content, few soil microorganisms, rooting restrictions, and conditions less conducive to infiltration of precipitation. As a result, it is typically necessary to provide stockpiled topsoil, compost, or other

Temporary and Permanen	t Seeding
Functions	
Erosion Control	Yes
Sediment Control	No
Site/Material Management	No

TS/PS-1

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EC-2 Temporary and Permanent Seeding (TS/PS)

soil amendments and rototill them into the soil to a depth of 6 inches or more.

Topsoil should be salvaged during grading operations for use and spread on areas to be revegetated later. Topsoil should be viewed as an important resource to be utilized for vegetation establishment, due to its water-holding capacity, structure, texture, organic matter content, biological activity, and nutrient content The rooting depth of most native grasses in the semi-arid Denver metropolitan area is 6 to 18 inches. At a minimum, the upper 6 inches of topsoil should be stripped, stockpiled, and ultimately respread across

Where topsoil is not available, subsoils should be amended to provide an appropriate plant-growth medium. Organic matter, such as well digested compost, can be added to improve soil characteristics conducive to plant growth. Other treatments can be used to adjust soil pH conditions when needed. Soil testing, which is typically inexpensive, should be completed to determine and optimize the types and amounts of amendments that are required.

If the disturbed ground surface is compacted, rip or rototill the surface prior to placing topsoil. If adding compost to the existing soil surface, rototilling is necessary. Surface roughening will assist in placemen of a stable topsoil layer on steeper slopes, and allow infiltration and root penetration to greater depth.

Prior to seeding, the soil surface should be rough and the seedbed should be firm, but neither too loose nor compacted. The upper layer of soil should be in a condition suitable for seeding at the proper depth and conducive to plant growth. Seed-to-soil contact is the key to good germination.

Seed Mix for Temporary Vegetation

To provide temporary vegetative cover on disturbed areas which will not be paved, built upon, or fully landscaped or worked for an extended period (typically 30 days or more), plant an annual grass appropriate for the time of planting and mulch the planted areas. Annual grasses suitable for the Denver metropolitan area are listed in Table TS/PS-1. These are to be considered only as general recommendations when specific design guidance for a particular site is not available. Local governments typically specify seed mixes appropriate for their jurisdiction.

Seed Mix for Permanent Revegetation

To provide vegetative cover on disturbed areas that have reached final grade, a perennial grass mix should be established. Permanent seeding should be performed promptly (typically within 14 days) after reaching final grade. Each site will have different characteristics and a landscape professional or the local jurisdiction should be contacted to determine the most suitable seed mix for a specific site. In lieu of a specific recommendation, one of the perennial grass mixes appropriate for site conditions and growth season listed in Table TS/PS-2 can be used. The pure live seed (PLS) rates of application recommended in these tables are considered to be absolute minimum rates for seed applied using proper drill-seeding

If desired for wildlife habitat or landscape diversity, shrubs such as rubber rabbitbrush (Chrysothamnus nauseosus), fourwing saltbush (Atriplex canescens) and skunkbrush sumac (Rhus trilobata) could be added to the upland seedmixes at 0.25, 0.5 and 1 pound PLS/acre, respectively. In riparian zones, planting root stock of such species as American plum (Prunus americana), woods rose (Rosa woodsii). plains cottonwood (Populus sargentii), and willow (Populus spp.) may be considered. On non-topsoiled upland sites, a legume such as Ladak alfalfa at 1 pound PLS/acre can be included as a source of nitrogen

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Temporary and Permanent Seeding (TS/PS)

Seeding dates for the highest success probability of perennial species along the Front Range are generally in the spring from April through early May and in the fall after the first of September until the ground freezes. If the area is irrigated, seeding may occur in summer months, as well. See Table TS/PS-3 for appropriate seeding dates.

Table TS/PS-1. Minimum Drill Seeding Rates for Various Temporary Annual Grasses

Species ^a (Common name)	Growth Season	Pounds of Pure Live Seed (PLS)/acre	Planting Depth (inches)
1. Oats	Cool	35 - 50	1 - 2
2. Spring wheat	Cool	25 - 35	1 - 2
3. Spring barley	Cool	25 - 35	1 - 2
4. Annual ryegrass	Cool	10 - 15	1/2
5. Millet	Warm	3 - 15	¹ / ₂ - ³ / ₄
6. Sudangrass	Warm	5-10	1/2 - 3/4
7. Sorghum	Warm	5-10	1/2 - 3/4
8. Winter wheat	Cool	20-35	1 - 2
9. Winter barley	Cool	20-35	1 - 2
10. Winter rye	Coo1	20-35	1 - 2
11. Triticale	Cool	25-40	1 - 2

Successful seeding of annual grass resulting in adequate plant growth will usually produce enough dead-plant residue to provide protection from wind and water erosion for an additional year. This assumes that the cover is not disturbed or mowed closer than 8 inches.

Hydraulic seeding may be substituted for drilling only where slopes are steeper than 3:1 or where access limitations exist. When hydraulic seeding is used, hydraulic mulching should be applied as a separate operation, when practical, to prevent the seeds from being encapsulated in

- See Table TS/PS-3 for seeding dates. Irrigation, if consistently applied, may extend the use of cool season species during the summer mo
- Seeding rates should be doubled if seed is broadcast, or increased by 50 percent if done using a Brillion Drill or by hydraulic seeding.

June 2012

June 2012

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BUILDING

ADMINISTRATIVE

DETAILS

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GRADING

Project No.: 247.07 ate: 01/03/23 esign: RMM Drawn: GGM

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PCD File No. PPR-21-51

Drawn: GGM Check: RMM C14 HEET 14 OF 15

Temporary and Permanent Seeding (TS/PS)

Table TS/PS-2. Minimum Drill Seeding Rates for Perennial Grasses

Common ^a Name	Botanical Name	Growth Season ^b	Growth Form	Seeds/ Pound	Pounds of PLS/acre
Alakali Soil Seed Mix					
Alkali sacaton	Sporobolus airoides	Cool	Bunch	1,750,000	0.25
Basin wildrye	Elymus cinereus	Cool	Bunch	165,000	2.5
Sodar streambank wheatgrass	Agropyron riparium 'Sodar'	Cool	Sod	170,000	2.5
Jose tall wheatgrass	Agropyron elongatum 'Jose'	Cool	Bunch	79,000	7.0
Arriba western wheatgrass	Agropyron smithii 'Arriba'	Cool	Sod	110,000	5.5
Total					17.75
Fertile Loamy Soil Seed Mix			Ďi.		***
Ephriam crested wheatgrass	Agropyron cristatum 'Ephriam'	Cool	Sod	175,000	2.0
Dural hard fescue	Festuca ovina 'duriuscula'	Cool	Bunch	565,000	1.0
Lincoln smooth brome	Bromus inermis leyss 'Lincoln'	Cool	Sod	130,000	3.0
Sodar streambank wheatgrass	Agropyron riparium 'Sodar'	Cool	Sod	170,000	2.5
Arriba western wheatgrass	Agropyron smithii 'Arriba'	Cool	Sod	110,000	7.0
Total				1	15.5
High Water Table Soil Seed Mix	r			***	.
Meadow foxtail	Alopecurus pratensis	Cool	Sod	900,000	0.5
Redtop	Agrostis alba	Warm	Open sod	5,000,000	0.25
Reed canarygrass	Phalaris arundinacea	Cool	Sod	68,000	0.5
Lincoln smooth brome	Bromus inermis leyss 'Lincoln'	Cool	Sod	130,000	3.0
Pathfinder switchgrass	Panicum virgatum 'Pathfinder'	Warm	Sod	389,000	1.0
Alkar tall wheatgrass	Agropyron elongatum 'Alkar'	Cool	Bunch	79,000	5.5
Total					10.75
Transition Turf Seed Mix			16	78	5
Ruebens Canadian bluegrass	Poa compressa 'Ruebens'	Cool	Sod	2,500,000	0.5
Dural hard fescue	Festuca ovina 'duriuscula'	Cool	Bunch	565,000	1.0
Citation perennial ryegrass	Lolium perenne 'Citation'	Cool	Sod	247,000	3.0
Lincoln smooth brome	Bromus inermis leyss 'Lincoln'	Cool	Sod	130,000	3.0
Total					7.5

Temporary and Permanent Seeding (TS/PS)

Table TS/PS-2. Minimum Drill Seeding Rates for Perennial Grasses (cont.)

Common Name	Botanical Name	Growth Season ^b	Growth Form	Seeds/ Pound	Pounds of PLS/acre
Sandy Soil Seed Mix					
Blue grama	Bouteloua gracilis	Warm	Sod-forming bunchgrass	825,000	0.5
Camper little bluestem	Schizachyrium scoparium 'Camper'	Warm	Bunch	240,000	1.0
Prairie sandreed	Calamovilfa longifolia	Warm	Open sod	274,000	1.0
Sand dropseed	Sporobolus cryptandrus	Cool	Bunch	5,298,000	0.25
Vaughn sideoats grama	Boutelous curtipenduls 'Vaughn'	Warm	Sod	191,000	2.0
Arriba western wheatgrass	Agropyron smithii 'Arriba'	Cool	Sod	110,000	5.5
Total					10.25
Heavy Clay, Rocky Foothill Seed	Mix			. As	70
Ephriam crested wheatgrass ^d	Agropyron cristatum 'Ephriam'	Cool	Sod	175,000	1.5
Oahe Intermediate wheatgrass	Agropyron intermedium 'Oahe'	Cool	Sod	115,000	5.5
Vaughn sideoats grama*	Bouteloua curtipendula 'Vaughn'	Warm	Sod	191,000	2.0
Lincoln smooth brome	Bromus inermis leyss 'Lincoln'	Cool	Sod	130,000	3.0
Arriba western wheatgrass	Agropyron smithii 'Arriba'	Cool	Sod	110,000	5.5
Total					17.5

All of the above seeding mixes and rates are based on drill seeding followed by crimped straw mulch. These rates should be doubled if seed is broadcast and should be increased by 50 percent if the seeding is done using a Brillion Drill or is applied through hydraulic seeding. Hydraulic seeding may be substituted for drilling only where slopes are steeper than 3:1. If hydraulic seeding is used, hydraulic mulching thould be done as a separate operation.

- See Table TS/PS-3 for seeding dates.
- If site is to be irrigated, the transition turf seed rates should be doubled.
- Crested wheatgrass should not be used on slopes steeper than 6H to 1V.
- Can substitute 0.5 lbs PLS of blue grama for the 2.0 lbs PLS of Vaughn sideoats grama.

EC-2 Temporary and Permanent Seeding (TS/PS)

Table TS/PS-3. Seeding Dates for Annual and Perennial Grasses

	(Numbers in	l Grasses table reference able TS/PS-1)	Perennial Grasses		
Seeding Dates	Warm	Cool	Warm	Cool	
January 1–March 15			✓	1	
March 16-April 30	4	1,2,3	· ·	1	
May 1–May 15	4		~		
May 16–June 30	4,5,6,7				
July 1–July 15	5,6,7		e e		
July 16-August 31					
September 1-September 30		8,9,10,11			
October 1-December 31			✓	1	

Cover seeded areas with mulch or an appropriate rolled erosion control product to promote establishment of vegetation. Anchor mulch by crimping, netting or use of a non-toxic tackifier. See the Mulching BMP Fact Sheet for additional guidance.

Maintenance and Removal

Monitor and observe seeded areas to identify areas of poor growth or areas that fail to germinate. Reseed and mulch these areas, as needed.

An area that has been permanently seeded should have a good stand of vegetation within one growing season if irrigated and within three growing seasons without irrigation in Colorado. Reseed portions of the site that fail to germinate or remain bare after the first growing season.

Seeded areas may require irrigation, particularly during extended dry periods. Targeted weed control may also be necessary.

Protect seeded areas from construction equipment and vehicle access.

TS/PS-4

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EC-4

Mulch can be applied either using standard mechanical dry application methods or using hydromulching equipment that hydraulically applies a slurry of water, wood fiber mulch, and often a tackifier.



Photograph MU-1. An area that was recently seeded, mulched, and crimped.

Appropriate Uses

Use mulch in conjunction with seeding to help protect the seedbed and stabilize the soil. Mulch can also be used as a temporary cover on low to mild slopes to help temporarily stabilize disturbed areas where growing season constraints prevent effective reseeding. Disturbed areas should be properly mulched and tacked, or seeded, mulched and tacked promptly after final grade is reached (typically within no longer than 14 days) on portions of the site not otherwise permanently stabilized.

Standard dry mulching is encouraged in most jurisdictions; however, hydromulching may not be allowed in certain jurisdictions or may not be allowed near waterways.

Do not apply mulch during windy conditions

Design and Installation

Prior to mulching, surface-roughen areas by rolling with a crimping or punching type roller or by track walking. Track walking should only be used where other methods are impractical because track walking with heavy equipment typically compacts the soil.

A variety of mulches can be used effectively at construction sites. Consider the following:

Mulch						
Functions						
Erosion Control	Yes					
Sediment Control	Moderate					
Site/Material Management	No					

MU-1

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• Clean, weed-free and seed-free cereal grain straw should be applied evenly at a rate of 2 tons per acre and must be tacked or fastened by a method suitable for the condition of the site. Straw mulch must be anchored (and not merely placed) on the surface. This can be accomplished mechanically by crimping or with the aid of tackifiers or nets. Anchoring with a crimping implement is preferred, and is the recommended method for areas flatter than 3:1. Mechanical crimpers must be capable of tucking the long mulch fibers into the soil to a depth of 3 inches without cutting them. An agricultural disk, while not an ideal substitute, may work if the disk blades are dull or blunted and set vertically; however, the frame may have to be weighted to afford proper soil penetration.

- Grass hay may be used in place of straw; however, because hay is comprised of the entire plant including seed, mulching with hay may seed the site with non-native grass species which might in turn out-compete the native seed. Alternatively, native species of grass hay may be purchased, but can be difficult to find and are more expensive than straw. Purchasing and utilizing a certified weed-free straw is an easier and less costly mulching method. When using grass hay, follow the same guidelines as for straw (provided above).
- On small areas sheltered from the wind and heavy runoff, spraying a tackifier on the mulch is satisfactory
 for holding it in place. For steep slopes and special situations where greater control is needed, erosion
 control blankets anchored with stakes should be used instead of mulch.
- Hydraulic mulching consists of wood cellulose fibers mixed with water and a tackifying agent and should be applied at a rate of no less than 1,500 pounds per acre (1,425 lbs of fibers mixed with at least 75 lbs of tackifier) with a hydraulic mulcher. For steeper slopes, up to 2000 pounds per acre may be required for effective hydroseeding. Hydromulch typically requires up to 24 hours to dry; therefore, it should not be applied immediately prior to inclement weather. Application to roads, waterways and existing vegetation should be avoided.
- Erosion control mats, blankets, or nets are recommended to help stabilize steep slopes (generally 3:1 and steeper) and waterways. Depending on the product, these may be used alone or in conjunction with grass or straw mulch. Normally, use of these products will be restricted to relatively small areas.
 Biodegradable mats made of straw and jute, straw-coconut, coconut fiber, or excelsior can be used instead of mulch. (See the ECM/TRM BMP for more information.)
- Some tackifiers or binders may be used to anchor mulch. Check with the local jurisdiction for allowed tackifiers. Manufacturer's recommendations should be followed at all times. (See the Soil Binder BMP for more information on general types of tackifiers.)
- Rock can also be used as mulch. It provides protection of exposed soils to wind and water erosion and
 allows infiltration of precipitation. An aggregate base course can be spread on disturbed areas for
 temporary or permanent stabilization. The rock mulch layer should be thick enough to provide full
 coverage of exposed soil on the area it is applied.

Maintenance and Removal

After mulching, the bare ground surface should not be more than 10 percent exposed. Reapply mulch, as needed, to cover bare areas:

U-2 Urban Drainage and Flood Control District June 2012 Urban Storm Drainage Criteria Manual Volume 3 COLORADO CENTRE METROPOLITAN DISTRICT ADMINISTRATIVE BUILDING - SITE DEVELOPMENT PLAN

DETAILS

CONTROL

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GRADING

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Project No.: 247.07 Date: 01/03/23

Design: RMM
Drawn: GGM
Check: RMM

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SHEET 15 OF 15



BACK POCKET

