

FINAL DRAINAGE REPORT FOR ELDORADO SPRINGS PPR-19-032

Engineering Review

03/25/2020 10:02:17 AM
dsdkuehster
stevekuehster@elpasoco.com
(719) 520-6813
EPC Planning & Community
Development Department

November 5, 2019 Revised February 5, 2020

Prepared for:

Emery Chukly 5671 North Oracle Road Suite 1102 Tucson, AZ 85704

WestWorks Job #91807

FINAL DRAINAGE REPORT FOR ELDORADO SPRINGS

Engineer's Statement:

Conditions:

| The attached drainage plan and report were prepared correct to the best of my knowledge and belief. Said the criteria established by the City/County for drain with the master plan of the drainage basin. I accept negligent acts, errors, or omissions on my part in pre- | drainage report has been prepared according nage reports and said report is in conformity responsibility for any liability caused by any |
|---|--|
| Chad D. Kuzbek, Colorado PE #35751 For and on behalf of WestWorks Engineering | Date |
| <u>Developer's Statement:</u> I, the developer have read and will comply with all report and plan. | of the requirements specified in this drainage |
| Business Name | • |
| By: Title: | |
| Address: | · |
| El Paso County, Colorado: Filed in accordance with requirements of the Draina County Engineering Criteria Manual, and Land Dev | • |
| Jennifer Irvine, P.E. County Engineer/ECM Administrator | Date |

FINAL DRAINAGE REPORT FOR ELDORADO SPRINGS

Engineer's Statement:

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the established criteria for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.

Certification Statement "This report and plan for the final drainage design of Eldorado Springs was prepared by me (or under my direct supervision) in accordance with the provisions of the City of Colorado Springs Drainage Criteria Manual Volumes 1 & 2 Drainage Design and Technical Criteria for the owners thereof. I understand that the City Colorado Springs does not and will not assume liability for drainage facilities designed by others." SIGNATURE: (affix seal) Registered Professional Engineer State of Colorado No. 35751 **Developer's Statement** I, the developer have read and will comply with all of the requirements specified in this drainage report and plan. "ESH Development, LLC hereby certifies that the drainage facilities for Eldorado Springs shall be constructed according to the design presented in this report. I understand that the City Colorado Springs does not and will not assume liability for the drainage facilities designed and/or certified by my engineer and that the City of Colorado Springs reviews drainage plans pursuant to Colorado Revised Statutes, Title 30, Article 28; but cannot, on behalf of Eldorado Springs, guarantee that final drainage design review will absolve ESH Development, LLC and/or their successors and/or assigns of future liability for improper design. I further understand that approval of the final plat does not imply approval of my engineer's drainage design." Name of Developer Authorized Signature

City of Colorado Springs Only: Filed in accordance with Section 7.7.906 of the Code of the City of Colorado Springs, 2001, as amended. For the City Engineer Date

Conditions:

FINAL DRAINAGE REPORT FOR ELDORADO SPRINGS

TABLE OF CONTENTS

| Purpose | Page 1 |
|----------------------------------|---------|
| General Location and Description | Page 1 |
| Drainage Basins and Subbasins | Page 1 |
| Existing Conditions | Page 1 |
| Developed Conditions | Page 10 |
| 4-Step Process Discussion | Page 13 |
| Summary | Page 14 |
| Drainage Design Criteria | Page 14 |
| Drainage Facility Design | Page 14 |
| Floodplain Statement | Page 14 |
| Erosion Control Plan | Page 15 |
| Opinion of Probable Cost | Page 15 |
| Drainage Fees | Page 16 |
| Reference List | Page 16 |

APPENDIX

Vicinity Map Soils Map Floodplain Map Hydrologic Calculations (5-YR and 100-YR) Hydraulic Calculations Stormwater Facility Calculations Previous Drainage Study Maps Drainage Map

FINAL DRAINAGE REPORT FOR ELDORADO SPRINGS

PURPOSE

The purpose of this final drainage report (FDR) is to identify specific solutions to drainage problems on site and off-site resulting from the development and platting of this subdivision.

GENERAL LOCATION AND DESCRIPTION

Eldorado Springs includes 15.5 acres located in a portion of the southwest corner of Section 33, Township 14 South and in the northwest corner of Section 4, Township 15 South, Range 66 West of the 6th P.M. in El Paso County, Colorado. More specifically, the site is located near the southeast corner of Venetucci Boulevard and Bob Johnson Drive, south of the World Arena facility. The site is bounded by unplatted land to the east and west, single family residential Stratmoor Subdivision to the south, and Venetucci Boulevard to the north.

The site is currently undeveloped and drains from south to north over moderate slopes. Proposed development includes a multi-family apartment complex. Existing soils in the study area consist mostly of Schamber-Razor complex (SCS Map Unit Symbol 82 - Hydrologic Soil Group A) with a small portion being Nunn Clay loam (SCS Map Unit Symbol 59 - Hydrologic Soil Group C). The site is located in the Stratton Drainage Basin.

DRAINAGE BASINS AND SUB-BASINS

The site has been part of multiple drainage studies. Most recently, the site was previously studied in the, "Final Drainage Report for Independence Place at Cheyenne Mountain Filing No. 1," prepared by Classic Consulting Engineers & Surveyors, dated 1/27/2011. The existing conditions drainage map and description is taken directly from this previous study and quoted below:

"Existing Drainage Characteristics:

The site is located within the Stratton Drainage Basin. This site was originally studied as a part of the "Master Drainage Plan Harrison Street — 1-25 Vicinity Cheyenne Mountain Ranch," by Hartzell — Pfeiffenberger and Associates, Inc. dated November 15, 1973. Since then the site was included in additional basin analysis reports; "Stratton and Fischer's Canyon Drainage Basin Planning Study, Draft Hydraulic Analysis," by Muller Engineering Co. dated May 31, 1990; the "Master Drainage Report for Cheyenne Mountain Center and Final Drainage Report for Cheyenne Mountain Center Filing No. 1 and Cheyenne Meadows Road," by Drexel Barrell, dated October 1985; the "Hydrology Report Stratton Drainage Basin Outfall Study," by Drexel Barrell, dated June 1994; and the "Preliminary and Final Drainage Report and Plan for World Arena Subdivision No. 1," by Obering, Wurth & Associates, August 1994 revised March 1995.

The most recent master study drainage report for this area that included the proposed site was the "Hydrology Report Stratton Drainage Basin Outfall Study El Paso County, Colorado," by Drexel Barrell, dated June 9, 1994. This Hydrology Report by Drexel Barrell conforms to current El Paso County criteria and was performed based on minor modifications and revisions to TR-20 data prepared in the 1990 study by Muller Engineering Co. This Hydrology Report also updated the hydrologic modeling completed in the 1985 study by Drexel Barrell with the correct 2 hour and 24 hour storms that are utilized in the current criteria. This report provides the basis for the proposed site's allowable release rate since it sized and described the 90"/102" RCP storm outfall system (Sinton Outfall). This system runs parallel with the eastern site boundary, along the opposite site of Venetucci Blvd. A Drainage Map from the Drexel Barrell Hydrology Study is included in the appendix of this report for reference.

The proposed 15.46 acre site is included within Basin 009 of this previous study. At the time of the Drexel Barrell Hydrology Study, existing box culverts conveyed the runoff from Basin 009 under Venetucci Blvd./Old Hwy 85-87 to the existing 14' x 11.7' box culvert crossing under Interstate 25 and to the east into Fountain Creek. The development of Cheyenne Mountain Center constructed the 'Sinton Outfall' RCP storm sewer system that accepts the allowable release rates of the upstream parcels and conveys them along the historic drainage pattern of under I-25 and into the Sinton Channel, which connects to Fountain Creek. This large storm system consists of 102" RCP and 90" RCP storm main, with appropriate sized storm laterals to account for the flows quantified within the Drexel Barrell Hydrology Report. Basin 009 of this previous report consists of 0.147 square miles (94.08 acres) and was modeled using a CN value of 81 (SCS Method since entire study area was over 100 acres). Per the Drainage Criteria Manual Vol. 1 Table 5-5 a CN of 81 is equivalent to 1/3 acre home lots with all Group C soils, or about 1/6 acre home lots with all Group B soils. The existing Stratmoor Hills subdivision is also located within this Basin 009, with homes slightly over 2 lots per acre; and since these homes are within Group B soils, a more accurate CN value for the existing development would be around 71. Therefore, the remaining area of Basin 009 (the proposed Independence Place at Chevenne Mountain Filing No. 1 site) is allowed to be substantially higher density than the calculated CN of 81. Also, runoff from Basin 008 of the previous report overflows the existing curb storm inlets and a portion drains onto the Venetucci Blvd. right-of-way within the Basin 009 area. Thus the actual total release from the developed site can be higher than the assumed Basin 009 flows $(Q_{100} = 270 \text{ cfs}, 24 \text{ hour duration storm event}).$

When the World Arena was constructed to the immediate north of the proposed site, street improvements were made to Venetucci Blvd. that expanded the existing storm sewer facilities constructed with the Sinton Outfall main (Drexel Barrell Report). Many curb inlets were placed along the improved roadways at the Cheyenne Meadows Road intersection and Bob Johnson Drive intersection. Using the "Preliminary and Final Drainage Report and Plan for World Arena Subdivision No. 1," by Obering, Wurth & Associates, August 1994 revised March 1995 and the "Roadway Improvement Package and Storm Sewer Package for US Highway 85187 (Venetucci Boulevard)," by Drexel Barrell including the as-built revisions; these storm modifications have been incorporated into this report and construction drawings

for the proposed development. The following will describe the existing runoff quantities and existing facilities in more detail at each of the existing design points.

Design Point 1 ($Q_5 = 25.0$ cfs, $Q_{100} = 61.1$ cfs) consists of flows from Basins EX-1, EX-2, and EX-3 all of which are within the existing Stratmoor Hills subdivision to the south-west of the proposed site. Basin EX-1 is 6.13 acres of existing home lots that drains to the east, overtops Stratmoor Drive and into Basin EX-2. The combined flows from EX-1 & EX-2 continue on the surface to the east and overtop Westcott Ave. drain into Basin EX-3. Roadside ditches along Chamberlin Ave. route all of the runoff from the three basins to DP-1, where an existing concrete storm pipe collects the water and routes it under Chamberlin Ave. and into the ravine to the east, within Basin EX-4. Although the density of the existing Stratmoor Hills subdivision is closer to 2 DU/Ac., C values corresponding with 3 DU/Ac. are used to conservatively estimate the runoff from the upstream basins ($C_5 = 0.40$, $C_{100} = 0.55$, Group B soils).

Design Point 2 ($Q_5 = 38.2$ cfs, $Q_{100} = 92.1$ cfs) consists of flows from DP-1 and Basins EX-4, EX-5, and EX-6. Basin EX-4 is 4.57 acres (B soils) of existing home lots that drains to the south into the outfall ravine from DP-1. Basin EX-5 is 4.93 acres (C soils) of existing roadway and home lots that drains into one of two ravines that meet at DP-2. Basin EX-6 is 3.96 acres (C soils) of existing home lots that drains to the north-east to DP-2. C soils were used throughout EX-5 & EX-6 to calculate the storm runoff higher and therefore more conservatively. See soils map in Appendix for separation of B and C soil groups. All of the runoff from these basins combine at this confluence point and continue north-east onto the proposed site and toward DP-3.

Design Point 3 (Qs = 45.2 cfs, $Q_{100} = 107.9$ cfs) consists of flows &om DP-2 and Basins EX-7 and EX-8. Slightly upstream and west of DP-3, manmade berms were constructed at some point in the past that prevents the runoff &om DP-2 &om continuing north to the existing culverts under Venetucci Blvd (as the Stratton Basin Hydrology Study anticipated). This man made berm instead routes the entire flow from DP-2 onto Westmark Ave. (DP-3) where the flow combines with the runoff &om Basins EX-7 & EX-8. This runoff continues north-east as surface flow on Westmark Ave. to DP-4. Documentation of why and when this berm, along with others located on the actual proposed site, does not exist as a drainage report for this existing Stratmoor Hills subdivision is not on file with E1 Paso County and there is no mention of diverting the flows with the Hydrology Report or any of the World Arena Subdivision drainage reports.

Design Point 4 ($Q_5 = 49.6 \text{ cfs}$, $Q_{100} = 118.3 \text{ cfs}$) consists of flows &om DP-3 and Basins EX-9 and EX-10. Basin EX-9 is 3.54 acres (C soils) of existing home lots and Westmark Ave. that drains down Westmark via curb and gutter and surface flow to the intersection of Venetucci Blvd. and Westmark Ave. (DP-4). Basin EX-10 is 1.11 acres (C soils) of on-site, undeveloped land that drains to this intersection and onto the roadway prior to the small culvert at DP-5. This combined runoff &om DP-4 flows onto Venetucci Blvd. and the adjacent roadside swale to Design Point 8.

Design Point 5 (Q_5 = 7.1 cfs, Q_{100} = 16.7 cfs) consists of runoff & om Basin EX-11, 3.83 acres (C soils) of mostly on-site, undeveloped land with a small portion of existing Stratmoor Hills homes and a portion of the western half of existing Venetucci Blvd. This runoff sheet flows to an existing 12" CMP storm pipe culvert that routes the runoff under Venetucci Blvd. and continues in the existing drainage pattern towards Interstate 25. This runoff combines with that from DP-8 and continues around the future World Arena Subd. Lot 2, Fil. 5 site to the existing 48" RCP I-25 crossing. The final drainage report for this World Arena parcel does not acknowledge or quantify the off-site tributary flows.

Design Point 6 ($Q_5 = 10.4$ cfs, $Q_{100} = 25.3$ cfs) consists of runoff & om Basin EX-12, 7.01 acres (C soils) of mostly on-site, undeveloped land with a small portion of existing Stratmoor Hills homes and a portion of the western half of existing Venetucci Blvd. This runoff sheet flows to this existing low point at DP-6. Previous reports drainage documents show an existing box culvert at this location that routes any runoff at this point under Venetucci Blvd. and directly toward the 1-25 box culvert (Sinton Outfall). However, this box culvert has since been covered, or filled, with soil and is no longer functioning. Documentation on why this was done cannot be found on file with El Paso County. The Sinton Outfall storm system shown on the Drainage Map does provide a 48" RCP stub off the junction box that points directly to the DP-6 and this filled in box culvert. It is our understanding that this 48" stub was meant to connect to this low-point at DP-6, which would then leave the existing box culvert not needed. A field inspection of the manhole does indeed show only a capped 48" lateral toward DP-6, and it appears this runoff simply infiltrates into the ground at this location.

Design Point 7 (Qs = 30.5 cfs, $Q_{100} = 83.9$ cfs) consists of runoff from Basins EX-13 & EX-14 and the flow by from DP-11. Basin EX-13 is 8.63 acres (C soils) of mostly on-site, undeveloped land, a portion of the western half of Venetucci Blvd. and a small portion of existing Stratmoor Hills homes. Basin EX-14 is 13.75 acres that consists of mostly undeveloped land and a small portion of the existing homes as well as a portion of the adjacent Stratmoor Hills United Methodist Church and the western half of Venetucci Blvd. A substantial amount of runoff at this point ($Q_5 = 3.1$ cfs, $Q_{100} = 21.2$ cfs) comes from the water not intercepted by the inlets at Design Points 9 - 11. The existing curb along the west side of Venetucci Blvd. from the Cheyenne Meadows Rd. intersection ends just after the inlet at DP-11, thus the flow by drains into the roadside ditch to DP-7. The combined runoff is intercepted by an existing CDOT Type D storm inlet (3.5' x 8.5' inlet dimensions). This inlet was installed with the construction of the Sinton Outfall Storm System and an existing 48" RCP storm pipe conveys the intercepted runoff across Venetucci Blvd. and connects to the 90" main.

Design Point 8 ($Q_5 = 52.1$ cfs, $Q_{100} = 124.2$ cfs) consists of flows from DP-4 and Basin EX-15. Basin EX-15 is 2.64 acres (C soils) of off-site, undeveloped land, including a portion of existing Venetucci Blvd. An existing elliptical CMP culvert conveys this runoff under Venetucci Blvd. to the north and into the existing drainage pattern. This culvert is very under-sized for 120+ cfs and it can be assumed that significant ponding takes place at this location prior to flowing to the downstream facilities. The parcel to the north of DP-8 (across Venetucci Blvd.) is planned to be a hotel with surrounding parking. The development

of the site will maintain the historic drainage pattern around the future development, but does change the overall outfall of the existing runoff. This World Arena Lot 2, Filing No. 5 (hotel site) construction was stopped after overlot grading and utility infrastructure was completed. Per the "Final Drainage Report for World Arena Subdivision Filing No. 5, Lot #2," by Matrix Design Group, Inc. (April 2008) the construction of Detention Pond #1 was to be outside of the existing drainage path to the existing 48" RCP under I-25. However, a site visit confirmed that the outlet pipe for this Pond 1 has been connected to the existing 48" interstate crossing and the existing low point (entry into the 48") has been filled in. Now, the existing drainage ponds approximately 2.0' and overtops into Pond #1, where a D-9 grate inlet within the pond intercepts the flows and passes them into the existing culvert.

Design Point 9a $(Q_5 = 22.3 \text{ cfs}, Q_{100} = 47.6 \text{ cfs})$ consists of runoff from Basin EX-20, 14.70 acres of existing single family subdivision and Cheyenne Meadows Road. An existing 8' D-10R at-grade curb inlet (4.5% street slope) intercepts a portion of this runoff $(Q_5 = 5.7 \text{ cfs}, Q_5)$, while the rest continues down Cheyenne Meadows Rd. to the intersection with Venetucci Blvd.

Design Point 9b ($Q_5 = 47.8 \text{ cfs}$, $Q_{100} = 102.0 \text{ cfs}$) consists of runoff from Basin EX-16, 31.48 acres of existing single family subdivision and Cheyenne Meadows Road. An existing 8' D-10R at-grade curb inlet (4.5% street slope) intercepts a portion of this runoff ($Q_5 = 5.9 \text{ cfs}$, $Q_5 = 12.7 \text{ cfs}$), while the rest continues down Cheyenne Meadows Rd. to the intersection with Venetucci Blvd. The combined intercepted runoff from DP-9a & DP-9b is routed in an existing 36" RCP storm pipe to the north to an existing channel, away from the Venetucci Blvd. and Cheyenne Meadows Rd. intersection. The large amount of flow-by ($Q_5 = 41.9 \text{ cfs}$, $Q_{100} = 89.3 \text{ cfs}$) continues to the submerged inlets at DP-9c.

Design Point 9c (Q5 = 85.3 cfs, Q100 = 186.7 cfs) consists of runoff from Basins EX-21 and EX-22, as well as the flow by from DP-9a & DP-9b. Basin EX-21 is 14.83 acres of the existing single family Huckleberry Knoll Subdivision and Cheyenne Meadows Rd. Basin EX-22 is 4.46 acres of existing Stratmoor Hills Subdivision, existing Stratmoor Hills United Methodist Church, and existing Cheyenne Meadows Rd. Two existing D10-R curb inlets (20' & 30') exist on Cheyenne Meadows, west of Venetucci Blvd. The storm water at this point overtops the crown of the Cheyenne Meadows and completely submerges the inlets, thus changing the calculation used in quantifying the intercepted flow (See Calculations in Appendix). The total area of opening of the two combined inlets is 33.5 square feet (50.0' x 0'67), and based upon field as-builts of the curb return, the inlets only have 0.35' of depth before overtopping south down Venetucci Blvd. This results in both inlets only intercepting 57 cfs of both 5 and 100 year flows. The flow by from these inlets next hits the inlet at DP-10.

Design Point 10 ($Q_5 = 28.3$ cfs, $Q_{100} = 129.7$ cfs) has a 20' at-grade D10-R curb inlet that intercepts a large portion of the flow-by from DP-9c. Venetucci Blvd. has a slope of 1.3% at this inlet based upon field as-builts of the constructed curb. This 20' inlet intercepts $Q_5 = 16.3$ cfs and $Q_{100} = 75.6$, while the remainder continues to the next existing inlet at DP-11.

Design Point 11 ($Q_5 = 12.0$ cfs, $Q_{100} = 54.1$ cfs) has a 20' at-grade CDOT Type R curb inlet that intercepts a portion of the remaining flow-by from DP-9c & DP-10. Venetucci Blvd. has a slope of 2.8% at this inlet based upon field as-builts of the constructed curb. This 20' inlet intercepts $Q_5 = 8.9$ cfs and $Q_{100} = 32.9$ cfs while the remainder continues south down Venetucci Blvd. The existing curb and gutter along Venetucci ends just downstream of DP-11, therefore the flow-by ($Q_5 = 3.1$ cfs, $Q_{100} = 21.2$ cfs) runs off the edge of asphalt and enters the roadside ditch, which drains to the grated inlet at DP-7.

Design Point 12 ($Q_5 = 3.1$ cfs, $Q_{100} = 6.0$ cfs) consists of runoff from Basin EX-17, 0.80 acres of existing Venetucci Blvd. and adjacent landscape area that drains to an existing 5' at-grade CDOT Type R curb inlet Based upon field as-builts Venetucci Blvd. has a slope of 3.0% at this inlet, resulting in intercepting $Q_5 = 1.9$ cfs and $Q_{100} = 2.3$, while the remainder continues within the curb to DP-13.

Design Point 13 ($Q_5 = 3.4$ cfs, $Q_{100} = 8.2$ cfs) consists of runoff from the flow-by of DP-12 and Basin EX-18, 0.68 acres of existing Venetucci Blvd. and adjacent landscape area that drains to an existing 5' at-grade CDOT Type R curb inlet. Based upon field as-builts Venetucci Blvd. has a slope of 0.7% at this inlet, resulting in intercepting $Q_5 = 2.2$ cfs and $Q_{100} = 3.5$ cfs. The non-intercepted runoff ($Q_5 = 1.2$ cfs, $Q_{100} = 4.7$ cfs) continues within the curb and gutter onto Bob Johnson Drive and west toward the overall basin outfall corridor.

Design Point 14 ($Q_5 = 1.4$ cfs, $Q_{100} = 3.2$ cfs) consists of runoff from Basin EX-19, 0.58 acres of existing Venetucci Blvd. and adjacent undeveloped right of way area. An existing modified Type D grated inlet drains this area and conveys the runoff into the 90" RCP Sinton Outfall system via a 48" RCP storm lateral. As mentioned previously, the existing alignments and storm facilities have been established through the "Roadway Improvement Package and Storm Sewer Package for US Highway 85/87 (Venetucci Boulevard)," by Drexel Barrell including the as-built revisions and field survey data.

Summary of Existing Conditions

The existing Sinton Outfall Storm system was planned to intercept all of the Stratton Basin runoff at rates specified within the "Hydrology Report Stratton Drainage Basin Outfall Study El Paso County, Colorado," by Drexel Barrell, dated June 9, 1994. The construction of the large storm main system appears to have been completed in two separate phases, per the "M.D.D.P. for Cheyenne Mountain Center." The second phase included extending storm sewer laterals off of the main alignment to our proposed site location in order to convey the existing runoff as well as a future allowable runoff rate per the Hydrology Study. This extension of a 48" storm lateral was completed at the northernmost existing roadway crossing (Design Point 7). However, at Design Point 6, no such storm sewer extension off the main line was completed and it appears that the existing roadway culvert was filled in and does not pass historic runoff under Venetucci Blvd./Old Hwy 85/87. The construction plans for the 102"-90" RCP storm main show a 48" RCP stub pointed toward the filled in box culvert, but capped 8.0' outside of the manhole. It is our assumption that this 48" stub is meant to convey the runoff at this DP-6 location. Therefore, our proposed conditions will discuss extending this lateral under Venetucci Blvd. and into our proposed site. Drainage reports completed for the immediate downstream World Arena Subdivisions do not discuss any

off-site flows from the tributary area, including our site and the upstream Stratmoor Hills Subdivision, or mention extending this 48" stub to the edge of the Venetucci Blvd. right-of-way. The Hydrology Report specifies a developable 100-year flow rate from the proposed site and upstream Stratmoor Hills Subdivision as 270 cfs. The calculated combined 100-year existing flow rate at design points 6, 7, and 8 is 198 cfs. Therefore, substantial more development can be constructed with this Basin 009 before storm water detention is required.

Also, the construction of the diversion berms on the proposed site that re-route the upstream tributary area (Stratmoor Hills) runoff directly to the Westmark Ave. and Venetucci Blvd. intersection are un-documented and seem to have been completed to eliminate the historic runoff to the 'filled in' culvert at DP-6. The existing CMP culverts at DP-5 and DP-8 are not adequately sized to convey all of the existing storm runoff that they currently receive. However, since it appears this drainage path is not natural and not per the previous drainage studies, we are proposing intercepting the upstream, existing runoff and conveying it through the proposed site's public storm system and directly to the 90"/102" RCP Sinton Outfall system."

Developed Drainage Characteristics:

Development of the site is a multi-family residential apartment complex with clubhouse, park space, pool and amenity areas, garages, paved parking and drive aisles, and landscaping. Development of this site also includes adjacent public roadway improvements along Venetucci Boulevard and a portion of Westmark Avenue.

Developed drainage overview:

On site runoff along with some off-site tributary runoff will be collected on site and routed into 2 private full-spectrum detention and stormwater quality facilities (Pond A and Pond B). A limited portion of the existing downstream drainage infrastructure has been adequately designed for developed runoff from this site (102" RCP). However, the existing 102" RCP combines with an existing 78"RCP and connects to an undersized existing 72" RCP. This scenario is believed through witness accounts to have caused flooding in the one-way road underpass under I-25. For this reason, Pond A and B will be full-spectrum detention facilities so as not to contribute excess runoff to this condition.

Details of Ponds A and B shall be included with the Site Construction Drawings. Details include dissipation basins, trickle channels, outfall structures, emergency overflows, and maintenance access.

Basins with designations of EX are taken directly from the existing conditions analysis. Basins with designations of OS are off-site basins. Basins with designations of A drain to Pond A. Basins with designations of B drain to Pond B. Basins with designations C do not drain to pond facility.

Developed Drainage Design Point Descriptions:

$DP-25 [Q_5 = 5 CFS/Q_{100} = 15 CFS]$

DP-25 is a proposed CDOT Type C grated inlet in sump. DP-25 collects mostly off-site runoff from Basin OS-13C. Collected flows will by-pass Pond A and are routed via SD28 to SD25.

Design Point 1 (DP-1) $[Q_5 = 2 \text{ CFS/}Q_{100} = 4 \text{ CFS}]$

DP-1 is a proposed 5' wide Type R curb inlet in sump. DP-1 collects runoff from Basins OS-13B and A1. Collected flows are routed via storm drain design point SD1 to SD2.

DP-2 $[Q_5 = 2 \text{ CFS}/Q_{100} = 3 \text{ CFS}]$

DP-2 is a proposed 5' wide Type R curb inlet in sump. DP-1 collects runoff from Basin A2. Collected flows are routed via SD2 to SD3.

DP-3 $[Q_5 = 2 \text{ CFS}/Q_{100} = 3 \text{ CFS}]$

DP-3 is a proposed CDOT Type C grate inlet in sump. DP-3 collects runoff from Basin A3. Collected flows are routed via SD3 to SD4.

$DP-4 [Q_5 = 1 CFS/Q_{100} = 2 CFS]$

DP-4 is a proposed 5' wide Type R curb inlet in sump. DP-4 collects runoff from Basin A4. Collected flows are routed via SD4 to SD5.

$DP-5 [Q_5 = 1 CFS/Q_{100} = 2 CFS]$

DP-5 is a proposed 5' wide Type R curb inlet in sump. DP-5 collects runoff from Basin A5. Collected flows are routed via SD6 ($Q_5 = 7$ CFS/ $Q_{100} = 14$ CFS) into Pond A. The discharge point into Pond A shall have a concrete energy dissipater.

$DP-6 | Q_5 = 4 | CFS/Q_{100} = 11 | CFS |$

DP-6 is a proposed 15' wide Type R curb inlet at grade. DP-6 collects runoff from Basins OS-13A and A6. Collected flows are routed via SD7 to SD8. Flow-by of $Q_5 = 0$ CFS/ $Q_{100} = 1.5$ CFS will continue to DP-22.

DP-7 $[Q_5 = 1 \text{ CFS/}Q_{100} = 3 \text{ CFS}]$

DP-7 is a proposed system of landscape drains, pool deck grates, and roof drain collection for the clubhouse. DP-7 collects runoff from Basin A7. Collected flows are routed to the inlet at DP6.

DP-8 $[Q_5 = 0.5 \text{ CFS/}Q_{100} = 1 \text{ CFS}]$

DP-8 is a proposed 5' wide Type R curb inlet at grade. DP-8 collects runoff from Basin A8. Collected flows are routed via SD8 ($Q_5 = 6$ CFS/ $Q_{100} = 12$ CFS) into Pond A. The discharge point into Pond A shall have a concrete energy dissipater.

DP-9 $[Q_5 = 0.3 \text{ CFS/}Q_{100} = 2 \text{ CFS}]$

DP-9 represents the sheet flow into Pond A.

DP-10 $[Q_5 = 2 \text{ CFS/}Q_{100} = 3 \text{ CFS}]$

DP-10 is a proposed CDOT Type C grate inlet in sump. DP-10 collects runoff from Basin B1. Collected flows are routed via SD10 to SD12.

DP-11 $[Q_5 = 1 \text{ CFS/}Q_{100} = 3 \text{ CFS}]$

DP-11 is a proposed 5' wide Type R curb inlet in sump. DP-11 collects runoff from Basin B2. Collected flows are routed via SD11 to SD12.

DP-12 $[Q_5 = 2 \text{ CFS/}Q_{100} = 3 \text{ CFS}]$

DP-12 is a proposed CDOT Type C grate inlet in sump. DP-12 collects runoff from Basin B3. Collected flows are routed via SD13 to SD16.

DP-13 $[Q_5 = 10 \text{ CFS/}Q_{100} = 20 \text{ CFS}]$

DP-13 is a proposed 20' wide Type R curb inlet in sump. DP-13 collects runoff from Basins OS-11 and B4. Collected flows are routed via SD14 to SD15.

DP-14 $[Q_5 = 2 \text{ CFS/}Q_{100} = 3 \text{ CFS}]$

DP-14 is a proposed 5' wide Type R curb inlet in sump. DP-14 collects runoff from Basin B5. Collected flows are routed via SD16 to SD18.

DP-15 $[Q_5 = 2 CFS/Q_{100} = 4 CFS]$

DP-15 is a proposed CDOT Type C grate inlet in sump. DP-15 collects runoff from Basin B6. Collected flows are routed via SD18 ($Q_5 = 23$ CFS/ $Q_{100} = 44$ CFS) into Pond B. The discharge point into Pond B shall have a concrete energy dissipater.

DP-16 $[Q_5 = 6 \text{ CFS/}Q_{100} = 11 \text{ CFS}]$

DP-16 is a proposed 10' wide Type R curb inlet in sump. DP-16 collects runoff from Basins OS-12 and B7. Collected flows are routed via SD17 to SD18.

$DP-24 [Q_5 = 2 CFS/Q_{100} = 4 CFS]$

DP-24 represents a series of landscape drains running behind the buildings along Venetucci Blvd. These landscape drains are intended to collect runoff and roofdrains in Basin B11. Collected flows are routed via SD27 to Pond B.

DP-17 $[Q_5 = 2 CFS/Q_{100} = 4 CFS]$

DP-17 is a proposed 10' wide Type R curb inlet at grade. DP-17 collects runoff from Basin B8. Collected flows are routed via SD19 to SD20. Flow-by of $Q_5 = 0$ CFS/ $Q_{100} = 0.1$ CFS will continue into Westmark Avenue.

DP-18 $[Q_5 = 0.7 \text{ CFS/}Q_{100} = 1 \text{ CFS}]$

DP-18 is a proposed 5' wide Type R curb inlet at grade. DP-18 collects runoff from Basin B9. Collected flows are routed via SD20 ($Q_5 = 2$ CFS/ $Q_{100} = 4$ CFS) into Pond B. The discharge point into Pond B shall have a concrete energy dissipater. Flow-by of $Q_5 = 0$ CFS/ $Q_{100} = 0.1$ CFS will continue into Westmark Avenue.

DP-19 $[Q_5 = 1 \text{ CFS}/Q_{100} = 2 \text{ CFS}]$

DP-19 represents the sheet flow into Pond B.

$DP-20 [Q_5 = 40 CFS/Q_{100} = 100 CFS]$

DP-20 is a proposed 48" RCP culvert to pick up off-site flows tributary to the existing drainageway south of the site. The collected runoff is not routed through a Pond facility. Instead it bypasses the site via SD21. Flows in SD21 are combined with the discharge from Pond B in SD22 ($Q_5 = 40 \text{ CFS/}Q_{100} = 105 \text{ CFS}$) will be routed under Venetucci Boulevard in a proposed 48" RCP storm tying to and existing 48" RCP stub that connects to an existing 102" RCP storm drain.

DP-21 $[Q_5 = 29 \text{ CFS}/Q_{100} = 59 \text{ CFS}]$

DP-21 is a proposed pair of 20' wide Type R curb inlets at grade. DP-21 collects runoff from Basin OS-14 and existing flow-by from DP-OS11. DP-OS11 is the last in a series of at-grade inlets in or near Cheyenne Meadows Road. Venetucci Boulevard does not have capacity to carry all of the existing runoff. Runoff to the inlets at DP-21 is modeled at maximum street capacity. Collected flows are routed via SD24 to SD25. Flow-by of $Q_5 = 0.2$ CFS/ $Q_{100} = 12$ CFS will continue to DP-22.

DP-22 $[Q_5 = 1 \text{ CFS/}Q_{100} = 14 \text{ CFS}]$

DP-22 is a proposed 15' wide Type R curb inlet in sump. DP-22 collects runoff from Basin C1 and flow-by from DP-6 and DP-21. Collected flows are routed via SD23 to SD25. Flows in SD25 ($Q_5 = 33 \text{ CFS/}Q_{100} = 73 \text{ CFS}$) are a combination of flows from SD9, SD23, and SD24. These combined storm pipes will tie to the existing CDOT Type D grate inlet in the roadside ditch near the site entrance. SD25 is an existing 48" RCP under Venetucci Boulevard connecting to the existing 90" RCP running along the north side of Venetucci Boulevard.

DP-23 $[Q_5 = 1 \text{ CFS/}Q_{100} = 6 \text{ CFS}]$

DP-23 is street flow in Venetucci Boulevard near the intersection with Westmark Avenue. This flow is less than the historic flow at existing conditions DP-5 ($Q_5 = 7 \text{ CFS/}Q_{100} = 17 \text{ CFS}$).

DP-009 $[Q_5 = 67 \text{ CFS/}Q_{100} = 172 \text{ CFS}]$

DP-009 represents the total flow from Basin 009 as referenced in the Drexel Barrell Report. The storm drain outfall infrastructure installed based on the Drexel Barrell Report anticipated flows of $Q_{100} = 270$ CFS. This means that the downstream infrastructure will not be additionally burdened by runoff from this site and even additional development in the Basin.

4-Step Process Discussion:

Step 1. Employ Runoff Reduction Practices.

The site layout was done to minimize paving and includes park and amenity areas. Site impervious area calculations are shown in the IRF spreadsheet in the Appendix.

Step 2. Implement BMPs That Provide WQCV with Slow Release.

Development of this site includes a full-spectrum detention facility providing WQCV and an outfall structure with a 40-hour drain time.

Step 3. Stabilize Drainageways.

There are no natural drainageways associated with this site. Drainage fees were be paid with the platting of this subdivision. These fees contribute to any necessary channel improvements within the major drainage basin.

Step 4. Implement Site Specific and Other Source Control BMPs. There is no permanent outside storage associated with this site.

Summary:

The development of the Eldorado Springs apartment site accounts for up-stream off-site flows, on-site flows, and adjacent flows for a solution that can handle these flows and safely discharge them to adequately sized downstream stormwater infrastructure. The grading and drainage of this site is such that less than 1-acre of developed property drains off the site without going through a full-spectrum detention and stormwater quality facility.

DRAINAGE DESIGN CRITERIA

This drainage report was prepared in accordance to the criteria established in the County Drainage Criteria Manual, updated in May 2014.

WestWorks Engineering uses the rational method for drainage basin study areas of less than 90 acres. This methodology is implemented in accordance with the County Drainage Criteria Manual Guidelines.

For the Rational Method, flows are calculated for the 5-year and 100-year recurrence intervals. The average runoff coefficients, 'C' values, are taken from Table 6-6 and the Intensity-Duration-Frequency curves are taken from Figure 6-5 of the County Drainage Criteria Manual. Time of concentration for overland flow and storm drain or gutter flow are calculated per Section 3.2 of the County Drainage Criteria Manual. Calculations for the Rational Method are shown in the Appendix of this report. Detention volume is calculated in accordance with the County Drainage Criteria Manual Guidelines.

DRAINAGE FACILITY DESIGN

All inlets, storm drains, culverts, and open channels are sized using the procedures outlined in the City Drainage Criteria Manual. All of the drainage systems, including the streets, are designed to safely route the 5-year and 100-year storm flows. Hydraulic grade line calculations for the proposed storm drain design will be included with the storm drain constructions drawings.

FLOODPLAIN STATEMENT

No portion of this site is within a F.E.M.A. designated floodplain per Flood Insurance Rate Map Community Panel No. 08041C0741 G, effective December 7, 2018.

EROSION CONTROL PLAN

The El Paso County Drainage Criteria Manual specifies that an Erosion Control Plan and associated cost estimate be submitted in conjunction with the Final Drainage Report. WestWorks Engineering respectfully requests the Erosion Control Plan be submitted in conjunction with the Overlot Grading Plan and construction assurances posted prior to obtaining a grading permit.

OPINION OF PROBABLE COST

Private Drainage Facilities (non-reimbursable):

| Item | Quantity | Unit Cost | Total Cost |
|------------------------|----------|-----------------|------------|
| 18" RCP Storm Drain | 1,549 LF | \$65/LF | \$100,425 |
| 24" RCP Storm Drain | 1,041 LF | \$78/LF | \$ 81,198 |
| 30" RCP Storm Drain | 376 LF | \$97/LF | \$ 36,472 |
| 5' Type R Inlet | 8 EA | \$4,000/EA | \$ 32,000 |
| 10' Type R Inlet | 2 EA | \$5,500/EA | \$ 11,000 |
| 15' Type R Inlet | 1 EA | \$8,000/EA | \$ 8,000 |
| 20' Type R Inlet | 1 EA | \$8,000/EA | \$ 8,000 |
| CDOT Type C Inlet | 5 EA | \$3,300/EA | \$ 16,500 |
| Storm Manhole | 8 EA | \$4,600/EA | \$ 36,800 |
| Pond Outfall Structure | 2 EA | \$7,500/EA | \$ 15,000 |
| Riprap | 33 CY | \$75/CY | \$ 2,475 |
| | | Sub-Total | \$347,870 |
| | | 20% Contingency | \$ 69,574 |
| | | TOTAL | \$417,444 |

Public Drainage Facilities (non-reimbursable):

| | (11011 1 011110 111 201 | | | |
|------------------------|-------------------------|-----------------|------------|--|
| Item | Quantity | Unit Cost | Total Cost | |
| 24" RCP Storm Drain | 20 LF | \$84/LF | \$ 1,680 | |
| 30" RCP Storm Drain | 11 LF | \$94/LF | \$ 1,034 | |
| 36" RCP Storm Drain | 146 LF | \$124/LF | \$ 18,104 | |
| 48" RCP Storm Drain | 1,225 LF | \$178/LF | \$218,050 | |
| 15' Type R Inlet | 1 EA | \$8,000/EA | \$ 8,000 | |
| 20' Type R Inlet | 2 EA | \$8,000/EA | \$ 16,000 | |
| Storm Manhole (Type 1) | 4 EA | \$8,600/EA | \$ 34,400 | |
| | | Sub-Total | \$297,268 | |
| | | 20% Contingency | \$ 59,454 | |
| | | TOTAL | \$356,722 | |

This opinion of probable cost is made on the basis of experience and qualifications and represents WestWorks Engineering's best judgment as an experienced and qualified professional firm, familiar with the construction industry. WestWorks Engineering cannot and will not guarantee that actual construction costs will not vary from this opinion of probable cost.

DRAINAGE FEES

The study area is in the Stratton Drainage Basin. The site has already been platted and drainage fees paid at that time.

REFERENCE LIST

"Soil Survey of El Paso County Area, Colorado," prepared by United States Department of Agriculture Soil Conservation Service, issued June 1981

"FIRM Flood Insurance Rate Map," prepared by Federal Emergency Management Agency, effective date March 17, 1997

El Paso County Drainage Criteria Manual, updated May 2014

"Master Drainage Plan Harrison Street- I-25 Vicinity Cheyenne Mountain Ranch", by Hartzell-Pfeiffenberger and Associates, Inc. dated November 15, 1973

"Stratton and Fischer's Canyon Drainage Basin Planning Study, Draft Hydraulic Analysis," by Muller Engineering Co. dated May 31, 1990

"Master Drainage Report for Cheyenne Mountain Center and Final Drainage Report for Cheyenne Mountain Center Filing No. 1 and Cheyenne Meadows Road," by Drexel Barrell, dated October 1985

"Hydrology Report Stratton Drainage Basin Outfall Study," by Drexel Barrell, dated June 1994

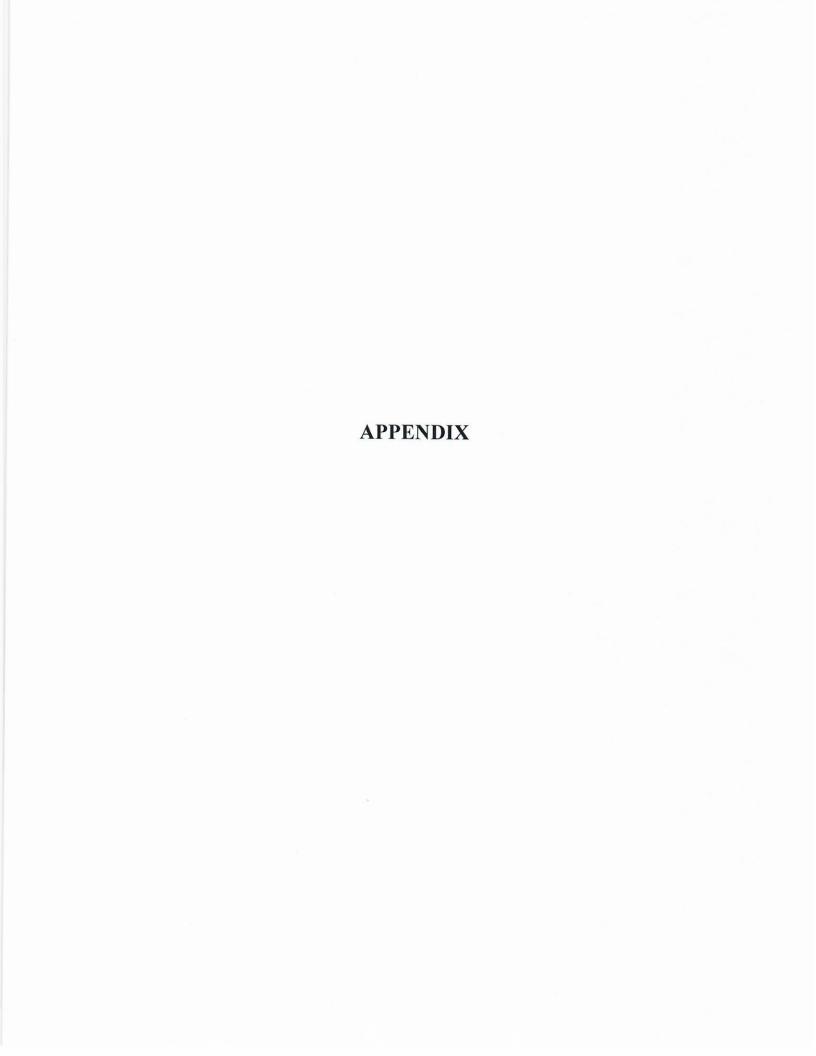
"Prediminary and Final Drainage Report and Plan for World Arena Subdivision No. 1," by Obering, Wurth & Associates, August 1994 revised March 1995

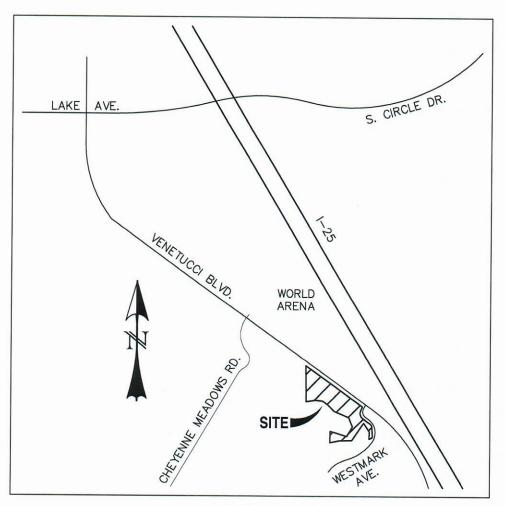
"Final Drainage Report for World Arena Subdivision Filing No. 5, Lot #2," by Matrix Design Group, Inc., April 2008

"Drainage Report for Huckleberry Knoll Subdivision," by Drexel Barrell & Company, dated June 15, 1983

"Roadway Improvement Package and Storm Sewer Package for US Highway 85/87 (Venetucci Boulevard)," by Drexel Barrell including the as-built revisions

"Final Drainage Report for Independence Place at Cheyenne Mountain Filing No. 1," prepared by Classic Consulting Engineers & Surveyors, dated 1/27/2011





VICINITY MAP SCALE: N.T.S.



Hydrologic Soil Group

| Map unit symbol | Map unit name | Rating | Acres in AOI | Percent of AOI |
|--------------------------|--|--------|--------------|----------------|
| 59 | Nunn clay loam, 0 to 3 percent slopes | С | 0.6 | 4.0% |
| 82 | Schamber-Razor complex, 8 to 50 percent slopes | Α | 14.7 | 96.0% |
| Totals for Area of Inter | rest | | 15.3 | 100.0% |

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

National Flood Hazard Layer FIRMette





Legend

SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT

With BFE or Depth Zone AE, AO, AH, VE, AR Without Base Flood Elevation (BFE) Regulatory Floodway SPECIAL FLOOD HAZARD AREAS

0.2% Annual Chance Flood Hazard, Area of 1% annual chance flood with average depth less than one foot or with drainage areas of less than one square mile zone Future Conditions 1% Annual Chance Flood Hazard Zone

Area with Reduced Flood Risk due to Levee. See Notes. Zone

Area with Flood Risk due to Levee Zone D

NO SCREEN Area of Minimal Flood Hazard Zone Effective LOMRs

Area of Undetermined Flood Hazard Zon

- - - Channel, Culvert, or Storm Sewer STRUCTURES IIIIIII Levee, Dike, or Floodwall GENERAL

Cross Sections with 1% Annual Chance Water Surface Elevation 17.5

Base Flood Elevation Line (BFE) Coastal Transect

Limit of Study

Coastal Transect Baseline Jurisdiction Boundary

Hydrographic Feature Profile Baseline

OTHER FEATURES

No Digital Data Available Digital Data Available

Unmapped

MAP PANELS

The pin displayed on the map is an approximate point selected by the user and does not represe an authoritative property location.

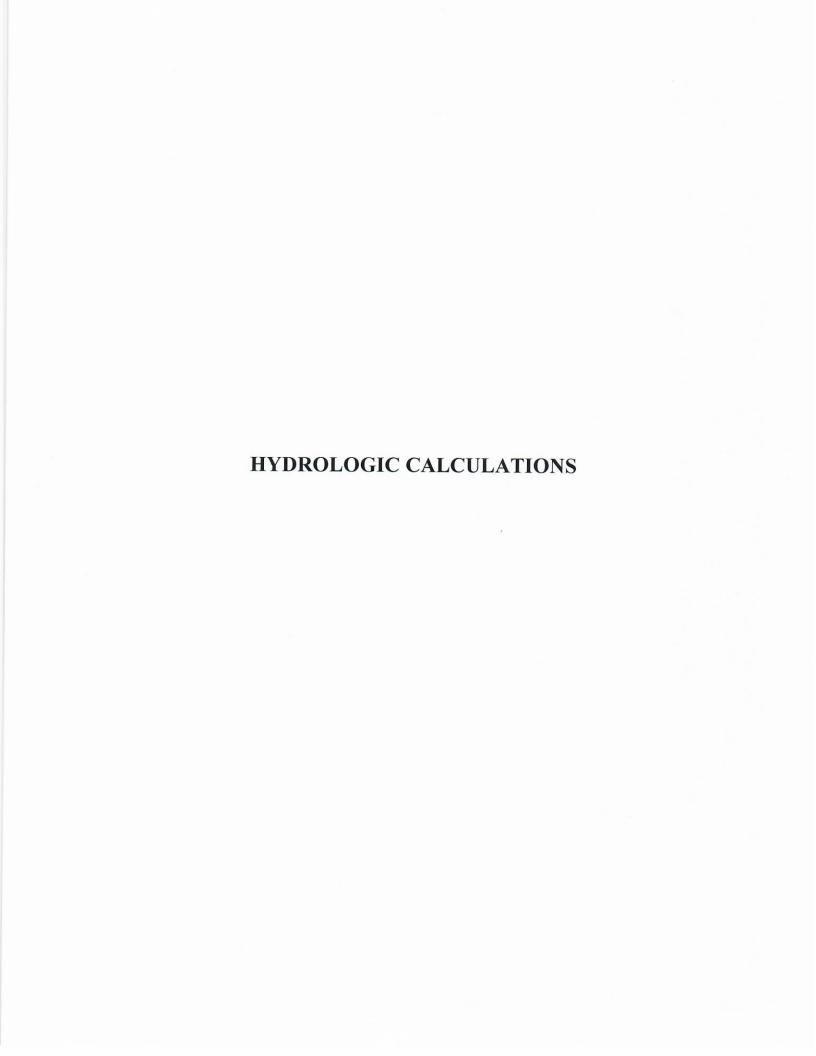
authoritative NFHL web services provided by FEMA. This map was exported on 5/24/2019 at 2:39:54 PM and does not The flood hazard information is derived directly from the This map complies with FEMA's standards for the use of The basemap shown complies with FEMA's basemap digital flood maps if it is not void as described below.

reflect changes or amendments subsequent to this date and

time. The NFHL and effective information may change or

become superseded by new data over time.

This map image is void if the one or more of the following map legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for elements do not appear: basemap imagery, flood zone labels, unmapped and unmodernized areas cannot be used for



Time of Concentration Calcuations

| Sub-Basin | Time Flowline | of Co L [ft.] | ncentrat H [ft.] | Time of Concentration, \mathbf{Tc} [min.] line $ L[ft.] H[ft.] v[ft/s] \mathbf{Tc} p$ | Time of Concentration, Tc [min.] Flowline L [ft.] V [ft/s] Tc [min.] | Sub-Basin | Time Flowline | of Col L[ft.] | ncentrat H [ft.] | Time of Concentration, \mathbf{Tc} [min.] line $ L$ [ft.] $ H$ [ft.] $ \mathbf{r}$ | Time of Concentration, Tc [min.] Flowline L [ft.] H [ft.] v [ft/s] Tc [min.] | Sub-Basin | Time of Concentration, Tc Flowline L fft.1 H fft.1 v fft/s1 | e of Co L [ft.] | ncentra H [ft.] | Time of Concentration, \mathbf{Tc} [min.] dine L [ft.] H [ft.] \mathbf{v} [ft/s] \mathbf{Tc} In | [min.] |
|-----------|------------------|------------------|---------------------|---|---|-----------------|------------------|------------------|---------------------|--|---|-----------|--|--------------------|--------------------|---|--------|
| | overland | 1 | 1.0 | | 0.3 | | overland | 110 | 4.0 | | 10.8 | | overland | 10 | 0.5 | | 2.9 |
| AI | channel | 80 | 1.0 | 4 | 0.3 | <u>A6</u> | channel | 170 | 12.0 | 6 | 0.3 | <u>B1</u> | channel | 30 | 1.0 | 9 | 0.1 |
| | | | Tot | Total Tc = | 2 | | | | Toi | Total Tc = | 111 | | | | To | Total Tc = | S |
| | overland | 70 | 10.0 | | 5.5 | | overland | 30 | 2.0 | | 4.6 | | overland | 70 | 8.0 | | 5.9 |
| A2 | channel | 50 | 1.0 | 5 | 0.2 | <u>A7</u> | channel | 130 | 0.5 | 2 | 1.0 | <u>B2</u> | channel | 50 | 1.0 | 5 | 0.2 |
| | | | Tot | Total Tc = | 9 | | | | Tol | Total Tc = | 9 | | | | To | Total Tc = | 9 |
| | overland | 20 | 0.5 | | 5.2 | | overland | 140 | 42.0 | | 6.1 | | overland | 20 | 1.0 | | 4.2 |
| <u>A3</u> | channel | 09 | 9.0 | 4 | 0.3 | $\overline{48}$ | channel | 120 | 4.0 | 9 | 0.3 | B3 | channel | 10 | 0.2 | S | 0.0 |
| | | | Tot | Total Tc = | 9 | | | | Tot | Total Tc = | 9 | | | | То | Total Tc = | w |
| | overland | 10 | 0.5 | | 2.9 | | overland | 250 | 48.0 | | 9.4 | | overland | 20 | 1.0 | | 4.2 |
| A4 | channel | 50 | 1.5 | 9 | 0.1 | <u>A9</u> | channel | - | 1.0 | 35 | 0.0 | B4 | channel | 160 | 2.0 | 4 | 0.7 |
| | | | Tot | Total Tc = | S | | | | Tot | Total Tc = | 6 | | | | Toi | Total Tc = | s, |
| | overland | 40 | 0.9 | | 4.1 | | overland | 1 | 1.0 | | 0.3 | | overland | 70 | 8.0 | | 5.9 |
| <u>A5</u> | channel | 06 | 2.0 | 5 | 0.3 | | channel | - | 1.0 | 35 | 0.0 | B5 | channel | 20 | 1.0 | 5 | 0.2 |
| | | | Tot | Total Tc = | S | | | | Tot | Total Tc = | v | | | | Tol | Total Tc = | 9 |



Project: Eldorado Springs

Job No.: 91807
Engineer: Chad Kuzbek, PE
Date: 5/24/2019

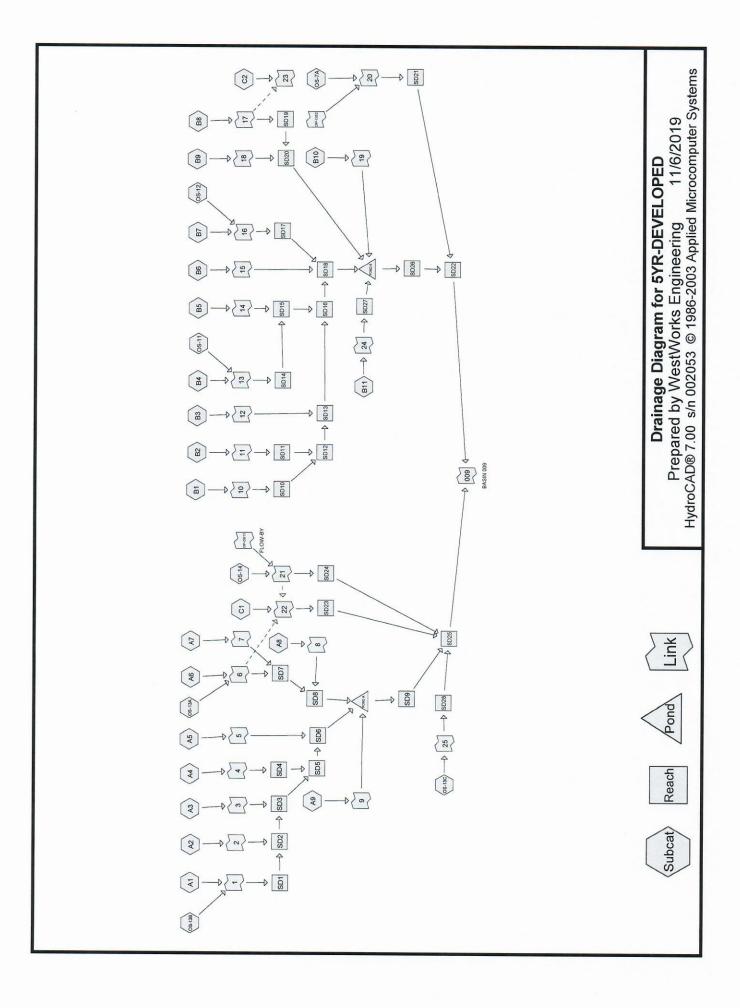
Time of Concentration Calcuations

| Flowline L [ft.] H [ft.] v [ft/s] Te min. Flowline L [ft.] H [ft.] v [ft/s] Te min. | Sub-Basin | Time | ofCon | centrati | Time of Concentration, Tc [min.] | | Sub-Basin | Time | of Con | centrat | Time of Concentration, Tc [min.] | min.] | Sub-Basin | Time | of Col | ncentrat | Time of Concentration, Tc [min.] | [min.] |
|--|-----------|----------|---------|----------|----------------------------------|-----------|-----------|----------|---------|---------|----------------------------------|-----------|-----------|-----------------------------------|---------|----------|----------------------------------|-----------|
| overland 20 1.0 4.2 overland 100 12.0 3 channel 30 0.5 5 0.1 CI channel 320 3.0 3 overland 50 8.0 4 5 CZ channel 630 8.0 4 overland 60 14.0 4.3 channel 1 1.0 35 channel 60 4.0 9 0.1 channel 1 1.0 35 overland 40 4.0 9 0.1 channel 1 1.0 35 channel 60 4.0 9 0.1 channel 1 1.0 35 channel 60 4.0 9 0.1 channel 1 1.0 35 channel 60 4.0 9 0.1 channel 1 1.0 35 channel 60 4.0 9 0.1 channel | | Flowline | C [ft.] | H [ft.] | v [ft/s] | Tc [min.] | | Flowline | L [ft.] | H [ft.] | | Tc [min.] | | Flowline L [ft.] H [ft.] v [ft/s] | L [ft.] | H [ft.] | v [ft/s] | Tc [min.] |
| channel 30 0.5 5 0.1 CI channel 320 3.0 3 overland 50 8.0 4.5 channel 630 8.0 4 channel 70 1.0 4 0.3 CZ channel 630 8.0 4 overland 60 14.0 4.3 channel 1 1.0 35 channel 60 4.0 9 0.1 channel 1 1.0 35 overland 40 4.0 9 0.1 channel 1 1.0 35 channel 60 4.0 9 0.1 channel 1 1.0 35 channel 60 4.0 9 0.1 channel 1 1.0 35 achannel 60 4.0 9 0.1 channel 1 1.0 35 channel 60 4.0 9 0.1 channel | | overland | 20 | 1.0 | | 4.2 | | overland | 100 | 12.0 | | 6.9 | | overland | - | 1.0 | | 0.3 |
| overland 50 8.0 4.5 overland 110 10.0 4 channel 70 1.0 4 60.3 C2 channel 630 8.0 4 channel 60 14.0 4.3 overland 1 1.0 35 channel 60 4.0 9 0.1 channel 1 1.0 35 channel 60 4.0 9 0.1 channel 1 1.0 35 channel 60 4.0 9 0.1 channel 1 1.0 35 channel 60 4.0 9 0.1 channel 1 1.0 35 result 60 4.0 9 0.1 channel 1 1.0 35 result 1 1 1 1 1 1 1 | B6 | channel | 30 | 0.5 | 5 | 0.1 | IJ | channel | 320 | 3.0 | 3 | 1.6 | | channel | - | 1.0 | 35 | 0.0 |
| overland 50 8.0 4.5 overland 110 10.0 4 channel 70 1.0 4 0.3 CZ channel 630 8.0 4 overland 60 14.0 4.3 overland 1 1.0 35 channel 60 4.0 9 0.1 channel 1 1.0 35 channel 60 4.0 9 0.1 channel 1 1.0 35 channel 60 4.0 9 0.1 channel 1 1.0 35 channel 60 4.0 9 0.1 channel 1 1.0 35 | | | | Tot | | S | | | | Tot | al Tc = | 6 | | | | To | Total Tc = | S |
| channel 70 1.0 4 0.3 C2 channel 630 8.0 4 overland 60 14.0 4.3 overland 1 1.0 35 channel 60 4.0 9 0.1 channel 1 1.0 35 overland 40 4.0 9 0.1 1.0 35 channel 60 4.0 9 0.1 channel 1 1.0 35 channel 60 4.0 9 0.1 channel 1 1.0 35 rotalTc = 5 7 channel 1 1.0 35 | 5-112 | overland | 50 | 8.0 | | 4.5 | | overland | 110 | 10.0 | | 8.0 | | overland | _ | 1.0 | | 0.3 |
| overland 60 14.0 4.3 overland 1 1.0 35 channel 60 4.0 9 0.1 channel 1 1.0 35 overland 40 4.0 4.7 overland 1 1.0 35 channel 60 4.0 9 0.1 channel 1 1.0 35 channel 60 4.0 9 0.1 channel 1 1.0 35 Total Tc = 5 Total Tc = 7 Total Tc = | | channel | 70 | 1.0 | 4 | 0.3 | C7 | channel | 630 | 8.0 | 4 | 2.7 | | channel | - | 1.0 | 35 | 0.0 |
| overland channel 60 14.0 4.3 overland channel 1 1.0 35 channel 60 4.0 9 0.1 channel 1 1.0 35 channel 40 4.0 9 0.1 channel 1 1.0 35 channel 60 4.0 9 0.1 channel 1 1.0 35 Total Tc = 5 Total Tc = Total Tc = | | | | Tot | al Tc = | 2 | | | | Tot | al Tc = | 11 | | | | Toi | Total Tc = | S |
| channel 60 4.0 9 0.1 channel 1 1.0 35 overland 40 4.0 4.7 overland 1 1.0 35 channel 60 4.0 9 0.1 channel 1 1.0 35 Total Tc = 5 Total Tc = Total Tc = | | overland | 09 | 14.0 | | 4.3 | | overland | - | 1.0 | | 0.3 | | overland | - | 1.0 | | 0.3 |
| overland channel 40 4.0 9 0.1 channel 1 1.0 35 Total Tc = 5 Total Tc = 5 Total Tc = | | channel | 09 | 4.0 | 6 | 0.1 | | channel | - | 1.0 | 35 | 0.0 | | channel | 1 | 1.0 | 35 | 0.0 |
| overland 40 4.0 4.7 overland 1 1.0 35 channel 60 4.0 9 0.1 channel 1 1.0 35 Total Tc = Total Tc = | | | - | Tot | al Tc = | 2 | | | | Tot | al Tc = | S | | | | Tot | Total Tc = | 5 |
| channel 60 4.0 9 0.1 channel 1 1.0 35 Total Tc = Total Tc = | | overland | 40 | 4.0 | | 4.7 | | overland | - | 1.0 | | 0.3 | | overland | П | 1.0 | | 0.3 |
| 5 Total Tc = | | channel | 09 | 4.0 | 6 | 0.1 | | channel | - | 1.0 | 35 | 0.0 | | channel | 1 | 1.0 | 35 | 0.0 |
| | | | | Tot | al Tc = | v. | | | | Tot | al Tc = | 3 | | | | Tot | Total Tc = | S |
| overland 90 14.0 6.0 overland 20 2.0 3.3 | | overland | 06 | 14.0 | | 0.9 | | overland | 20 | 2.0 | | 3.3 | | overland | - | 1.0 | | 0.3 |
| $\overline{B10}$ channel 60 5.0 10 0.1 $\overline{B11}$ channel 30 1.0 6 $\overline{0.1}$ | | channel | 09 | 5.0 | 10 | 0.1 | B11 | channel | 30 | 1.0 | 9 | 0.1 | | channel | _ | 1.0 | 35 | 0.0 |
| Total $Tc = 6$ Total $Tc = 5$ | | | | Tota | al Tc = | 9 | | | | Tot | al Tc = | w | | | | Tot | Total Tc = | w |



Project: Eldorado Springs

Job No.: 91807
Engineer: Chad Kuzbek, PE
Date: 5/24/2019



El Paso County 5-Year Duration=5 min, Inten=5.17 in/hr

Prepared by WestWorks Engineering

Page 1

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Subcatchment A1:

Runoff

=

1.33 cfs @

0.08 hrs, Volume=

0.009 af, Depth= 0.38"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 5-Year Duration=5 min, Inten=5.17 in/hr

| Area (ac) | С | Description |
|-----------|------|-----------------|
| 0.100 | 0.73 | ROOFTOPS |
| 0.200 | 0.96 | PAVEMENT |
| 0.000 | 0.00 | |

0.300 0.88 Weighted Average

Tc Length (feet) (min)

Slope (ft/ft)

Velocity (cfs)

Capacity Description

(ft/sec) 5.0

Direct Entry,

Subcatchment A4:

Runoff

1.27 cfs @

0.08 hrs, Volume=

0.009 af, Depth= 0.36"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 5-Year Duration=5 min, Inten=5.17 in/hr

| _ | Area (ac) | C | Description |
|---|-----------------|------|-----------------|
| | 0.100 | 0.73 | ROOFTOP |
| _ | 0.200 | 0.90 | PAVEMENT |
| | 150 1 El 2010 V | | |

0.300 0.84 Weighted Average

Tc Length Slope (feet) (min) (ft/ft)

Velocity Capacity

Description (cfs)

(ft/sec)

5.0

Direct Entry,

Subcatchment A5:

Runoff

0.95 cfs @

0.08 hrs, Volume=

0.007 af, Depth= 0.27"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 5-Year Duration=5 min, Inten=5.17 in/hr

| Area (ac) | С | Description |
|-----------|------|-------------|
| 0.100 | 0.08 | LANDSCAPE |
| 0.200 | 0.90 | PAVEMENT |

0.300 0.63 Weighted Average

Tc Length Slope Velocity Capacity Description (min) (feet) (ft/ft) (ft/sec) (cfs)

5.0

Direct Entry,

El Paso County 5-Year Duration=5 min, Inten=5.17 in/hr

Prepared by WestWorks Engineering

Page 2

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Subcatchment B1:

Runoff = 1.73 cfs

1.73 cfs @ 0.08 hrs, Volume=

0.012 af, Depth= 0.37"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 5-Year Duration=5 min, Inten=5.17 in/hr

| Area (ac) | С | Description |
|-----------|------|-------------|
| 0.100 | 0.73 | ROOFTOP |
| 0.300 | 0.90 | PAVEMENT |

0.400 0.86 Weighted Average

| Tc | Length | Slope | Velocity | Capacity | Description |
|----|--------|-------|----------|----------|-------------|
| | | | | (cfs) | |

5.0

Direct Entry,

Subcatchment B11:

Runoff =

1.68 cfs @

0.08 hrs, Volume=

0.012 af, Depth= 0.16"

Runoff by Rational method, Rise/Fall= $1.0/1.0 \, xTc$, Time Span= $0.00-3.00 \, hrs$, dt= $0.01 \, hrs$ El Paso County 5-Year Duration= $5 \, min$, Inten= $5.17 \, in/hr$

| Area (a | ic) | С | Description |
|---------|-----|------|-------------|
| 0.40 | 00 | 0.73 | ROOFTOP |
| 0.50 | 00 | 0.08 | LANDSCAPE |
| | | | |

0.900 0.37 Weighted Average

| Tc | Length | Slope | Velocity | Capacity | Description |
|----|--------|-------|----------|----------|-------------|
| | | | | (cfs) | |

5.0

Direct Entry,

Subcatchment B3:

Runoff

1.73 cfs @

0.08 hrs, Volume=

0.012 af, Depth= 0.37"

Runoff by Rational method, Rise/Fall= $1.0/1.0 \, xTc$, Time Span= $0.00-3.00 \, hrs$, dt= $0.01 \, hrs$ El Paso County 5-Year Duration= $5 \, min$, Inten= $5.17 \, in/hr$

| Area (ac) | C | Description | |
|-----------|------|-----------------|--|
| 0.100 | 0.73 | ROOFTOP | |
| 0.300 | 0.90 | PAVEMENT | |

0.400 0.86 Weighted Average

| Tc | Length | Slope | Velocity | Capacity | Description |
|----|--------|-------|----------|----------|-------------|
| | (feet) | | (ft/sec) | | |

5.0

Direct Entry,

El Paso County 5-Year Duration=5 min, Inten=5.17 in/hr

Prepared by WestWorks Engineering

Page 3

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Subcatchment B4:

Runoff

=

3.40 cfs @ 0

0.08 hrs, Volume=

0.024 af, Depth= 0.32"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 5-Year Duration=5 min, Inten=5.17 in/hr

| Area (ac) | С | Description | |
|-----------|------|------------------|--|
| 0.100 | 0.08 | LANDSCAPE | |
| 0.300 | 0.73 | ROOFTOP | |
| 0.500 | 0.90 | PAVEMENT | |
| 0.900 | 0.75 | Weighted Average | |

| | | | | Capacity (cfs) | Description |
|-----|--------|--------|----------|-------------------|-------------|
| 5.0 | (ICCL) | (IUIL) | (II/Sec) | (CIS) | D: |

5.0

Direct Entry,

Subcatchment B5:

Runoff

1.51 cfs @

0.08 hrs, Volume=

0.011 af, Depth= 0.32"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 5-Year Duration=5 min, Inten=5.17 in/hr

| | Area (ac) | С | Description | |
|----|-----------|------|------------------|--|
| | 0.050 | 0.08 | LANDSCAPE | |
| | 0.100 | 0.73 | ROOFTOP | |
| _ | 0.250 | 0.90 | PAVEMENT | |
| 12 | 0.400 | 0.75 | Weighted Average | |
| | | | | |

| (min) | Length (feet) | , | Description | |
|-------|------------------|-------|--------------|--|
| 5.0 | | | Direct Entry | |

Direct Entry,

Subcatchment B7:

Runoff

2.47 cfs @

0.08 hrs, Volume=

0.018 af, Depth= 0.30"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 5-Year Duration=5 min, Inten=5.17 in/hr

| _ | Area (ac) | С | Description | |
|---|-----------|------|------------------|--|
| | 0.150 | 0.08 | LANDSCAPE | |
| | 0.100 | 0.73 | ROOFTOP | |
| | 0.450 | 0.90 | PAVEMENT | |
| | 0.700 | 0.70 | Weighted Average | |

| 5Y | DD | | | - |
|-----|-----|--|---|---|
| OIL | K-1 | | O |) |

El Paso County 5-Year Duration=5 min, Inten=5.17 in/hr

Prepared by WestWorks Engineering

Page 4

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

| | | | | . , | Description |
|------------|--------|---------|---------|-------|-------------|
| (min) (fee | et) (f | t/ft) (| ft/sec) | (cfs) | 24 |

5.0

Direct Entry,

Subcatchment B8:

Runoff

= 1.94 cfs @

0.08 hrs, Volume=

0.014 af, Depth= 0.24"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 5-Year Duration=5 min, Inten=5.17 in/hr

| _ | Area (ac) | С | Description |
|---|-----------|------|-----------------|
| | 0.300 | 0.08 | LANDSCAPE |
| | 0.400 | 0.90 | PAVEMENT |
| | 0.700 | 0.55 | \\\/-:- - - |

0.700 0.55 Weighted Average

Tc Length Slope Velocity Capacity Description (min) (feet) (ft/ft) (ft/sec) (cfs)

5.0

Direct Entry,

Subcatchment B9:

Runoff

0.65 cfs @

0.08 hrs, Volume=

0.005 af, Depth= 0.28"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 5-Year Duration=5 min, Inten=5.17 in/hr

| | Area (ac) | С | Description | |
|---|-----------|------|------------------|--|
| | 0.050 | 0.08 | LANDSCAPE | |
| | 0.050 | 0.73 | ROOFTOP | |
| _ | 0.100 | 0.90 | PAVEMENT | |
| | 0.200 | 0.65 | Weighted Average | |

| | | | | | Description |
|-------|--------|---------|----------|-------|-------------|
| (min) | (feet) | (ft/ft) | (ft/sec) | (cfs) | |

5.0

Direct Entry,

Subcatchment OS-7A:

Runoff

7.04 cfs @

0.08 hrs, Volume=

0.050 af, Depth= 0.22"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 5-Year Duration=5 min, Inten=5.17 in/hr

| Area (ac) | С | Description |
|-----------|------|-------------|
| 2.800 | 0.50 | FROM FDR |

El Paso County 5-Year Duration=5 min, Inten=5.17 in/hr

Prepared by WestWorks Engineering

Page 5

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

| (min) (feet) (ft/ft) (ft/sec) (cfs) | | | | | Capacity (cfs) | Description |
|-------------------------------------|--|--|--|--|----------------|-------------|
|-------------------------------------|--|--|--|--|----------------|-------------|

5.0

Direct Entry, FROM FDR

Reach SD10:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.400 ac, Inflow Depth = 0.37" for 5-Year event 1.73 cfs @ 0.08 hrs, Volume= 0.012 af

Outflow = 1.73 cfs @ 0.08 hrs, Volume= 0.012 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Reach SD19:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.700 ac, Inflow Depth = 0.23" for 5-Year event 1.60 cfs @ 0.07 hrs, Volume= 0.013 af

Outflow = 1.60 cfs @ 0.07 hrs, Volume= 0.013 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Reach SD20:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.900 ac, Inflow Depth = 0.24" for 5-Year event 2.25 cfs @ 0.08 hrs, Volume= 0.018 af

Outflow = 2.25 cfs @ 0.08 hrs, Volume= 0.018 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Reach SD27:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.900 ac, Inflow Depth = 0.16" for 5-Year event 1.68 cfs @ 0.08 hrs, Volume= 0.012 af

Outflow = 1.68 cfs @ 0.08 hrs, Volume= 0.012 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

El Paso County 5-Year Duration=5 min, Inten=5.17 in/hr

Prepared by WestWorks Engineering

Page 6

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Reach SD4:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.300 ac, Inflow Depth = 0.36" for 5-Year event 1.27 cfs @ 0.08 hrs, Volume= 0.009 af

Outflow = 1.27 cfs @ 0.08 hrs, Volume= 0.009 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 4:

Inflow Area = 0.300 ac, Inflow Depth = 0.36" for 5-Year event 1.27 cfs @ 0.08 hrs, Volume= 0.009 af

Primary = 1.27 cfs @ 0.08 hrs, Volume= 0.009 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 5:

Inflow Area = 0.300 ac, Inflow Depth = 0.27" for 5-Year event 0.95 cfs @ 0.08 hrs. Volume= 0.007 af

Primary = 0.95 cfs @ 0.08 hrs, Volume= 0.007 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 10:

Inflow Area = 0.400 ac, Inflow Depth = 0.37" for 5-Year event 1.73 cfs @ 0.08 hrs, Volume= 0.012 af

Primary = 1.73 cfs @ 0.08 hrs, Volume= 0.012 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 12:

Inflow Area = 0.400 ac, Inflow Depth = 0.37" for 5-Year event 1.73 cfs @ 0.08 hrs, Volume= 0.012 af

Primary = 1.73 cfs @ 0.08 hrs, Volume= 0.012 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-3.00 hrs. dt= 0.01 hrs.

Link 14:

Inflow Area = 0.400 ac, Inflow Depth = 0.32" for 5-Year event 1.51 cfs @ 0.08 hrs, Volume= 0.011 af

Primary = 1.51 cfs @ 0.08 hrs, Volume= 0.011 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

El Paso County 5-Year Duration=5 min, Inten=5.17 in/hr

Prepared by WestWorks Engineering

Page 7

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Link 17:

Inflow Area = 0.700 ac, Inflow Depth = 0.24" for 5-Year event 1.94 cfs @ 0.08 hrs, Volume= 0.014 af

Primary = 1.60 cfs @ 0.07 hrs, Volume= 0.013 af, Atten= 17%, Lag= 0.0 min

Secondary = 0.34 cfs @ 0.08 hrs, Volume= 0.001 af

Primary outflow = Inflow below 1.60 cfs, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 18:

Inflow Area = 0.200 ac, Inflow Depth = 0.28" for 5-Year event 0.65 cfs @ 0.08 hrs, Volume= 0.005 af

Primary = 0.65 cfs @ 0.08 hrs, Volume= 0.005 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-3.00 hrs. dt= 0.01 hrs.

Link 24:

Inflow Area = 0.900 ac, Inflow Depth = 0.16" for 5-Year event 1.68 cfs @ 0.08 hrs, Volume= 0.012 af

Primary = 1.68 cfs @ 0.08 hrs, Volume= 0.012 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

El Paso County 5-Year Duration=6 min, Inten=4.90 in/hr

Prepared by WestWorks Engineering

Page 1

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Subcatchment A2:

Runoff = 1.66 cfs @ 0.10 hrs, Volume=

0.014 af, Depth= 0.41"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 5-Year Duration=6 min, Inten=4.90 in/hr

| Area (ac) | С | Description |
|-----------|------|-------------|
| 0.150 | 0.73 | ROOFTOP |
| 0.250 | 0.90 | PAVEMENT |

0.400 0.84 Weighted Average

| Tc | Length | Slope | Velocity | Capacity | Description |
|----|--------|-------|----------|----------|-------------|
| | | | | (cfs) | |

6.0

Direct Entry,

Subcatchment A3:

Runoff = 1.62 cfs

1.62 cfs @ 0.10 hrs, Volume=

0.013 af, Depth= 0.40"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 5-Year Duration=6 min, Inten=4.90 in/hr

| Area (ac) | С | Description |
|-----------|------|-----------------|
| 0.200 | 0.73 | ROOFTOP |
| 0.200 | 0.90 | PAVEMENT |
| | | |

0.400 0.82 Weighted Average

| Tc | Length | Slope | Velocity | Capacity | Description |
|----|--------|-------|----------|----------|-------------|
| | (feet) | | (ft/sec) | (cfs) | |

6.0

Direct Entry,

Subcatchment A7:

Runoff

1.28 cfs @

0.10 hrs, Volume=

0.011 af, Depth= 0.32"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 5-Year Duration=6 min, Inten=4.90 in/hr

| Area (ac) | С | Description |
|-----------|------|-------------|
| 0.100 | 0.08 | LANDSCAPE |
| 0.100 | 0.73 | ROOFTOP |
| 0.200 | 0.90 | PAVEMENT |

0.400 0.65 Weighted Average

| Tc | Length | Slope | Velocity | Capacity | Description |
|----|--------|-------|----------|----------|-------------|
| | (feet) | | (ft/sec) | | |

6.0

Direct Entry,

6.0

El Paso County 5-Year Duration=6 min, Inten=4.90 in/hr

Prepared by WestWorks Engineering

Page 2

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Subcatchment A8:

Runoff = 0.52 cfs @ 0.10 hrs, Volume=

0.004 af, Depth= 0.17"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 5-Year Duration=6 min, Inten=4.90 in/hr

| _ | Area (| (ac) | С | Des | cription | | | | |
|---|-------------|--------------|------|------------------|----------------------|----------|-------------|--|----|
| | 0.2 | 200 | 0.08 | LAN | IDSCAPE | | | | |
| | 0. | 100 | 0.90 | PA\ | /EMENT | | | | |
| | 0.3 | 300 | 0.35 | Wei | ighted Ave | rage | | | i. |
| | Tc (min) | Leng (fee | | Slope (ft/ft) | Velocity (ft/sec) | Capacity | Description | | |

Direct Entry,

Subcatchment B10:

Runoff = 0.71 cfs @ 0.10 hrs, Volume= 0.006 af, Depth= 0.12"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 5-Year Duration=6 min, Inten=4.90 in/hr

| Area | (ac) | С | Des | cription | | | |
|-------------|-------------|------|------------------|----------------------|-------------------|-------------|--|
| 0. | 450 | 0.08 | LAN | IDSCAPE | | | |
| 0. | 150 | 0.73 | RO | OFTOP | | | |
| 0. | 600 | 0.24 | Wei | ghted Ave | rage | | |
| Tc (min) | Leng (fe | | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description | |

6.0 (ff/ft) (ft/sec) (cfs) Direct Entry,

Subcatchment B2:

Runoff = 1.44 cfs @ 0.10 hrs, Volume= 0.012 af, Depth= 0.36"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 5-Year Duration=6 min, Inten=4.90 in/hr

| Area | (ac) | С | Des | scription | | | |
|-------------|--------------|------|------------------|----------------------|-------------------|-------------|--|
| 0. | 050 | 0.08 | LAN | NDSCAPE | VIII. | | |
| 0. | 150 | 0.73 | RO | OFTOP | | | |
| 0. | 200 | 0.90 | PA | JEMENT | | | |
| 0. | 400 | 0.73 | We | ighted Ave | rage | | |
| Tc (min) | Leng (fee | | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description | |

6.0 Direct Entry,

El Paso County 5-Year Duration=6 min, Inten=4.90 in/hr

Prepared by WestWorks Engineering

Page 3

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Subcatchment B6:

Runoff

=

1.90 cfs @

0.10 hrs, Volume=

0.016 af, Depth= 0.38"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 5-Year Duration=6 min, Inten=4.90 in/hr

| Area (ac) | С | Description |
|-----------|------|-------------|
| 0.050 | 0.08 | LANDSCAPE |
| 0.150 | 0.73 | ROOFTOP |
| 0.300 | 0.90 | PAVEMENT |

0.500 0.77 Weighted Average

| Tc | Length | Slope | Velocity | Capacity | Description |
|----|--------|-------|----------|----------|-------------|
| | | | | | |

6.0

Direct Entry,

Subcatchment OS-12:

Runoff

3.21 cfs @

0.10 hrs, Volume=

0.027 af, Depth= 0.24"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 5-Year Duration=6 min, Inten=4.90 in/hr

| Area (ac) | С | Description |
|-----------|------|-------------|
| 1.300 | 0.50 | FROM FDR |

| Tc | Length | Slope | Velocity | Capacity | Description |
|----|--------|-------|----------|----------|-------------|
| | | | | (cfs) | |

6.0

Direct Entry, FROM FDR

Subcatchment OS-13A:

Runoff

1.82 cfs @

0.10 hrs, Volume=

0.015 af, Depth= 0.11"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 5-Year Duration=6 min, Inten=4.90 in/hr

| Area (ac) | С | Description |
|-----------|------|---------------|
| 0.300 | 0.90 | PAVEMENT/ROOF |
| 1.300 | 0.08 | LANDSCAPE |

| 1.600 | 0.23 | Weighted Average |
|-------|------|------------------|
| | | |

| Tc | Length | Slope | Velocity | Capacity | Description |
|----|--------|-------|----------|----------|-------------|
| | (feet) | | (ft/sec) | (cfs) | 1989 |

6.0

Direct Entry, FROM FDR

El Paso County 5-Year Duration=6 min, Inten=4.90 in/hr

Prepared by WestWorks Engineering

Page 4

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Subcatchment OS-13B:

Runoff

=

0.37 cfs @

0.10 hrs, Volume=

0.003 af, Depth= 0.07"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 5-Year Duration=6 min, Inten=4.90 in/hr

Area (ac)

C Description

0.500 0.15 LANDSCAPE

Tc Length (min) (feet)

Slope Velocity (ft/ft) (ft/sec)

Capacity Description (cfs)

6.0

Direct Entry,

Subcatchment OS-13C:

Runoff

4.69 cfs @

0.10 hrs, Volume=

0.039 af. Depth= 0.12"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 5-Year Duration=6 min, Inten=4.90 in/hr

| Area (ac) | С | Description |
|-----------|------|---------------|
| 0.800 | 0.90 | PAVEMENT/ROOF |

3.000 0.08 LANDSCAPE

3.800 0.25 Weighted Average

Slope

(ft/ft)

(min)

Tc Length

(feet)

Velocity Capacity (ft/sec)

Description

(cfs)

6.0

Direct Entry, FROM FDR

Reach SD1:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area =

0.800 ac, Inflow Depth = 0.21" for 5-Year event

Inflow

1.69 cfs @

0.10 hrs. Volume=

0.014 af

Outflow

1.69 cfs @

0.10 hrs, Volume=

0.014 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Reach SD11:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area =

0.400 ac, Inflow Depth = 0.36"

for 5-Year event

Inflow

1.44 cfs @

0.10 hrs, Volume=

0.012 af

Outflow =

1.44 cfs @

0.10 hrs, Volume=

0.012 af, Atten= 0%, Lag= 0.0 min

El Paso County 5-Year Duration=6 min, Inten=4.90 in/hr

Prepared by WestWorks Engineering

Page 5

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Reach SD12:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area =

0.800 ac, Inflow Depth = 0.39" for 5-Year event

Inflow

3.15 cfs @ 0.10 hrs, Volume=

0.026 af

Outflow

3.15 cfs @ 0.10 hrs, Volume=

0.026 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs. dt= 0.01 hrs.

Reach SD13:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area =

1.200 ac, Inflow Depth = 0.40" for 5-Year event

Inflow

4.87 cfs @ 0.10 hrs, Volume=

0.040 af

Outflow

4.87 cfs @

0.10 hrs, Volume=

0.040 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs.

Reach SD17:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area =

2.000 ac, Inflow Depth = 0.28" for 5-Year event

Inflow

5.64 cfs @ 0.10 hrs, Volume=

0.047 af

Outflow

5.64 cfs @ 0.10 hrs. Volume=

0.047 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Reach SD2:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area =

1.200 ac, Inflow Depth = 0.28"

for 5-Year event

Inflow

3.34 cfs @ 0.10 hrs, Volume=

0.028 af

Outflow

3.34 cfs @ 0.10 hrs, Volume=

0.028 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Reach SD28:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area =

3.800 ac, Inflow Depth = 0.12" for 5-Year event

Inflow

4.69 cfs @ 0.10 hrs, Volume=

0.039 af

Outflow =

4.69 cfs @ 0.10 hrs, Volume=

0.039 af, Atten= 0%, Lag= 0.0 min

El Paso County 5-Year Duration=6 min, Inten=4.90 in/hr

Prepared by WestWorks Engineering

Page 6

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Reach SD3:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 1.600 ac, Inflow Depth = 0.31" for 5-Year event 4.96 cfs @ 0.10 hrs, Volume= 0.041 af

Outflow = 4.96 cfs @ 0.10 hrs, Volume= 0.041 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Reach SD5:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 1.900 ac, Inflow Depth = 0.32" for 5-Year event 6.21 cfs @ 0.10 hrs, Volume= 0.051 af

Outflow = 6.21 cfs @ 0.10 hrs, Volume= 0.051 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Reach SD6:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 2.200 ac, Inflow Depth = 0.32" for 5-Year event 7.15 cfs @ 0.10 hrs, Volume= 0.059 af

Outflow = 7.15 cfs @ 0.10 hrs, Volume= 0.059 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 1:

Inflow Area = 0.800 ac, Inflow Depth = 0.21" for 5-Year event 1.69 cfs @ 0.10 hrs, Volume= 0.014 af

Primary = 1.69 cfs @ 0.10 hrs, Volume= 0.014 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 2:

Inflow Area = 0.400 ac, Inflow Depth = 0.41" for 5-Year event 1.66 cfs @ 0.10 hrs, Volume= 0.014 af

Primary = 1.66 cfs @ 0.10 hrs, Volume= 0.014 af, Atten= 0%, Lag= 0.0 min

El Paso County 5-Year Duration=6 min, Inten=4.90 in/hr

Prepared by WestWorks Engineering

Page 7

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Link 3:

Inflow Area = 0.400 ac, Inflow Depth = 0.40" for 5-Year event 1.62 cfs @ 0.10 hrs, Volume= 0.013 af

Primary = 1.62 cfs @ 0.10 hrs, Volume= 0.013 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 7:

Inflow Area = 0.400 ac, Inflow Depth = 0.32" for 5-Year event 1.28 cfs @ 0.10 hrs, Volume= 0.011 af

Primary = 1.28 cfs @ 0.10 hrs, Volume= 0.011 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 8:

Inflow Area = 0.300 ac, Inflow Depth = 0.17" for 5-Year event Inflow = 0.52 cfs @ 0.10 hrs, Volume= 0.004 af

Primary = 0.52 cfs @ 0.10 hrs, Volume= 0.004 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 11:

Inflow Area = 0.400 ac, Inflow Depth = 0.36" for 5-Year event 1.44 cfs @ 0.10 hrs, Volume= 0.012 af

Primary = 1.44 cfs @ 0.10 hrs, Volume= 0.012 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 15:

Inflow Area = 0.500 ac, Inflow Depth = 0.38" for 5-Year event 1.90 cfs @ 0.10 hrs, Volume= 0.016 af

Primary = 1.90 cfs @ 0.10 hrs, Volume= 0.016 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 16:

Inflow Area = 2.000 ac, Inflow Depth = 0.28" for 5-Year event Inflow = 5.64 cfs @ 0.10 hrs. Volume= 0.047 af

Primary = 5.64 cfs @ 0.10 hrs, Volume= 0.047 af, Atten= 0%, Lag= 0.0 min

El Paso County 5-Year Duration=6 min, Inten=4.90 in/hr

Prepared by WestWorks Engineering

Page 8

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Link 19:

Inflow Area =

0.600 ac, Inflow Depth = 0.12" for 5-Year event

Inflow

0.71 cfs @ 0.10 hrs, Volume= 0.006 af

Primary

0.71 cfs @ 0.10 hrs, Volume=

0.006 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 25:

Inflow Area =

3.800 ac, Inflow Depth = 0.12" for 5-Year event

Inflow Primary 4.69 cfs @ 4.69 cfs @

0.10 hrs, Volume= 0.10 hrs, Volume=

0.039 af 0.039 af, Atten= 0%, Lag= 0.0 min

Prepared by WestWorks Engineering

Page 1

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Subcatchment OS-11:

Runoff = 7.06 cfs @ 0.12 hrs, Volume= 0.070 af, Depth= 0.30"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 5-Year Duration=7 min, Inten=4.66 in/hr

Area (ac) C Description
2.800 0.55 FROM FDR

Tc Length Slope Velocity Capacity Description (min) (feet) (ft/ft) (ft/sec) (cfs)

7.0

Direct Entry, FROM FDR

Reach SD14:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 3.700 ac, Inflow Depth = 0.33" for 5-Year event 10.17 cfs @ 0.12 hrs, Volume= 0.100 af

Outflow = 10.17 cfs @ 0.12 hrs, Volume= 0.100 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Reach SD15:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 4.100 ac, Inflow Depth = 0.33" for 5-Year event 11.57 cfs @ 0.12 hrs, Volume= 0.114 af

Outflow = 11.57 cfs @ 0.12 hrs, Volume= 0.114 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Reach SD16:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 5.300 ac, Inflow Depth = 0.36" for 5-Year event 16.04 cfs @ 0.11 hrs, Volume= 0.158 af

Outflow = 16.04 cfs @ 0.11 hrs, Volume= 0.158 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

El Paso County 5-Year Duration=7 min, Inten=4.66 in/hr

Prepared by WestWorks Engineering

Page 2

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Reach SD18:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 7.800 ac, Inflow Depth = 0.35" for 5-Year event 1nflow = 23.18 cfs @ 0.11 hrs, Volume= 0.227 af

Outflow = 23.18 cfs @ 0.11 hrs, Volume= 0.227 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Reach SD26:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 10.200 ac, Inflow Depth = 0.04" for 5-Year event
Inflow = 0.16 cfs @ 0.23 hrs, Volume= 0.037 af

Outflow = 0.16 cfs @ 0.23 hrs, Volume= 0.037 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 13:

Inflow Area = 3.700 ac, Inflow Depth = 0.33" for 5-Year event 10.17 cfs @ 0.12 hrs, Volume= 0.100 af

Primary = 10.17 cfs @ 0.12 hrs, Volume= 0.100 af, Atten= 0%, Lag= 0.0 min

El Paso County 5-Year Duration=9 min, Inten=4.29 in/hr

Prepared by WestWorks Engineering

Page 1

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Subcatchment A9:

Runoff

=

0.32 cfs @

0.15 hrs. Volume=

0.004 af. Depth= 0.10"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 5-Year Duration=9 min, Inten=4.29 in/hr

Area (ac)

C Description

0.500 0.15 LANDSCAPE

Tc Length (min)

9.0

Slope

Velocity Capacity (ft/sec)

Description

(feet)

(ft/ft)

(cfs)

Direct Entry,

Subcatchment C1:

Runoff

1.27 cfs @

0.15 hrs, Volume=

0.016 af, Depth= 0.32"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 5-Year Duration=9 min, Inten=4.29 in/hr

| Area (ac) | С | Description |
|-----------|------|-------------|
| 0.300 | 0.08 | LANDSCAPE |

0.300 0.90 **PAVEMENT**

Weighted Average 0.600 0.49

Tc Length

Slope Velocity Capacity (ft/ft)

Description

(min) (feet) (ft/sec)

(cfs)

9.0

Direct Entry,

Link 9:

Inflow Area =

=

0.500 ac, Inflow Depth = 0.10" for 5-Year event

Inflow

0.32 cfs @

0.15 hrs, Volume=

0.004 af

Primary

0.32 cfs @

0.15 hrs, Volume=

0.004 af, Atten= 0%, Lag= 0.0 min

El Paso County 5-Year Duration=11 min, Inten=3.99 in/hr

Prepared by WestWorks Engineering

Page 1

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Subcatchment A6:

Runoff = 2.87 cfs @ 0.181

0.18 hrs, Volume= 0.044 af, Depth= 0.48"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 5-Year Duration=11 min, Inten=3.99 in/hr

| Area (ac) | C | Description |
|--|---|--|
| 0.300 | 0.08 | LANDSCAPE |
| 0.100 | 0.73 | ROOFTOP |
| 0.700 | 0.90 | PAVEMENT |
| The second secon | The book of the second of the | The second of th |

1.100 0.66 Weighted Average

| Tc | Length | Slope | Velocity | Capacity | Description |
|----|--------|-------|----------|----------|--|
| | (feet) | | (ft/sec) | | 201 20 20 20 20 20 20 20 20 20 20 20 20 20 |

11.0

Direct Entry,

Subcatchment C2:

Runoff =

2.33 cfs @ 0.18 hrs, Volume=

0.036 af, Depth= 0.36"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 5-Year Duration=11 min, Inten=3.99 in/hr

| Area (a | ac) | C | escription |
|---------|------|-------|------------|
| 0.6 | 00 0 | .08 L | ANDSCAPE |
| 0.6 | 00 0 | .90 P | AVEMENT |
| | | | |

1.200 0.49 Weighted Average

| IC | Length | Slope | Velocity | Capacity |
|-------|--------|---------|----------|----------|
| (min) | (feet) | (ft/ft) | (ft/sec) | (cfs) |

11.0

Direct Entry,

Description

Reach SD7:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 3.100 ac, Inflow Depth = 0.32" for 5-Year event Inflow = 5.40 cfs @ 0.18 hrs, Volume= 0.083 af

Outflow = 5.40 cfs @ 0.18 hrs, Volume= 0.083 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs. dt= 0.01 hrs.

Reach SD8:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 3.400 ac, Inflow Depth = 0.31" for 5-Year event Inflow = 5.82 cfs @ 0.18 hrs, Volume= 0.089 af

Outflow = 5.82 cfs @ 0.18 hrs, Volume= 0.089 af, Atten= 0%, Lag= 0.0 min

El Paso County 5-Year Duration=11 min, Inten=3.99 in/hr

Prepared by WestWorks Engineering

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

Page 2 11/6/2019

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Reach SD9:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 6.100 ac, Inflow Depth = 0.05" for 5-Year event 0.11 cfs @ 0.36 hrs, Volume= 0.024 af

Outflow = 0.11 cfs @ 0.36 hrs, Volume= 0.024 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 6:

Inflow Area = 2.700 ac, Inflow Depth = 0.30" for 5-Year event

Inflow = 4.35 cfs @ 0.18 hrs, Volume= 0.067 af

Primary = 4.35 cfs @ 0.18 hrs, Volume= 0.067 af, Atten= 0%, Lag= 0.0 min

Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Primary outflow = Inflow below 4.40 cfs, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 23:

Inflow Area = 1.200 ac, Inflow Depth = 0.36" for 5-Year event Inflow = 2.33 cfs @ 0.18 hrs, Volume= 0.036 af

Primary = 2.33 cfs @ 0.18 hrs, Volume= 0.036 af, Atten= 0%, Lag= 0.0 min

El Paso County 5-Year Duration=20 min, Inten=3.09 in/hr

Prepared by WestWorks Engineering

Page 1

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Reach SD23:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.600 ac, Inflow Depth = 0.50" for 5-Year event 0.92 cfs @ 0.15 hrs, Volume= 0.025 af

Outflow = 0.92 cfs @ 0.15 hrs, Volume= 0.025 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Reach SD24:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 78.100 ac, Inflow Depth = 0.12" for 5-Year event 28.57 cfs @ 0.33 hrs, Volume= 0.781 af

Outflow = 28.57 cfs @ 0.33 hrs, Volume= 0.781 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Reach SD25:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 88.600 ac, Inflow Depth = 0.12" for 5-Year event 32.59 cfs @ 0.33 hrs, Volume= 0.920 af

Outflow = 32.59 cfs @ 0.33 hrs, Volume= 0.920 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs. dt= 0.01 hrs.

Link 21:

Inflow Area = 78.100 ac, Inflow Depth = 0.12" for 5-Year event 28.57 cfs @ 0.33 hrs, Volume= 0.781 af

Primary = 28.57 cfs @ 0.33 hrs, Volume= 0.781 af, Atten= 0%, Lag= 0.0 min

Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Primary outflow = Inflow below 28.80 cfs, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 22:

Inflow Area = 0.600 ac, Inflow Depth = 0.50" for 5-Year event 0.92 cfs @ 0.15 hrs, Volume= 0.025 af

Primary = 0.92 cfs @ 0.15 hrs, Volume= 0.025 af, Atten= 0%, Lag= 0.0 min

El Paso County 5-Year Duration=20 min, Inten=3.09 in/hr

Prepared by WestWorks Engineering

Page 2

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Link DP-OS11: FLOW-BY

Inflow Area = 65.500 ac, Inflow Depth = 0.06" for 5-Year event Inflow = 0.327 af

12.00 cfs @ 0.33 hrs, Volume= 12.00 cfs @ 0.33 hrs, Volume= Primary = 0.327 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

23 Point hydrograph entered manually, To= 0.00 hrs, dt= 0.03 hrs, Area= 65.500 ac, cfs =

| 0.00 | 1.10 | 2.20 | 3.30 | 4.40 | 5.50 | 6.50 | 7.60 | 8.70 | 9.80 |
|-------|-------|-------|------|------|------|------|------|------|------|
| 10.90 | 12.00 | 10.90 | 9.80 | 8.70 | 7.60 | 6.50 | 5.50 | 4.40 | 3.30 |
| 2.20 | 1.10 | 0.00 | | | | | | | |

El Paso County 5-Year Duration=25 min, Inten=2.75 in/hr

Prepared by WestWorks Engineering

Page 1

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Reach SD21:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 2.800 ac, Inflow Depth = 5.96" for 5-Year event Inflow = 39.95 cfs @ 0.42 hrs, Volume= 1.390 af

Outflow = 39.95 cfs @ 0.42 hrs, Volume= 1.390 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Reach SD22:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 13.000 ac, Inflow Depth = 1.35" for 5-Year event 40.26 cfs @ 0.42 hrs, Volume= 1.464 af

Outflow = 40.26 cfs @ 0.42 hrs, Volume= 1.464 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 009: BASIN 009

Inflow Area = 101.600 ac, Inflow Depth = 0.29" for 5-Year event Inflow = 66.86 cfs @ 0.41 hrs, Volume= 2.452 af

Primary = 66.86 cfs @ 0.41 hrs, Volume= 2.452 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 20:

Inflow Area = 2.800 ac, Inflow Depth = 5.96" for 5-Year event Inflow = 39.95 cfs @ 0.42 hrs, Volume= 1.390 af

Primary = 39.95 cfs @ 0.42 hrs, Volume= 1.390 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-3.00 hrs. dt= 0.01 hrs.

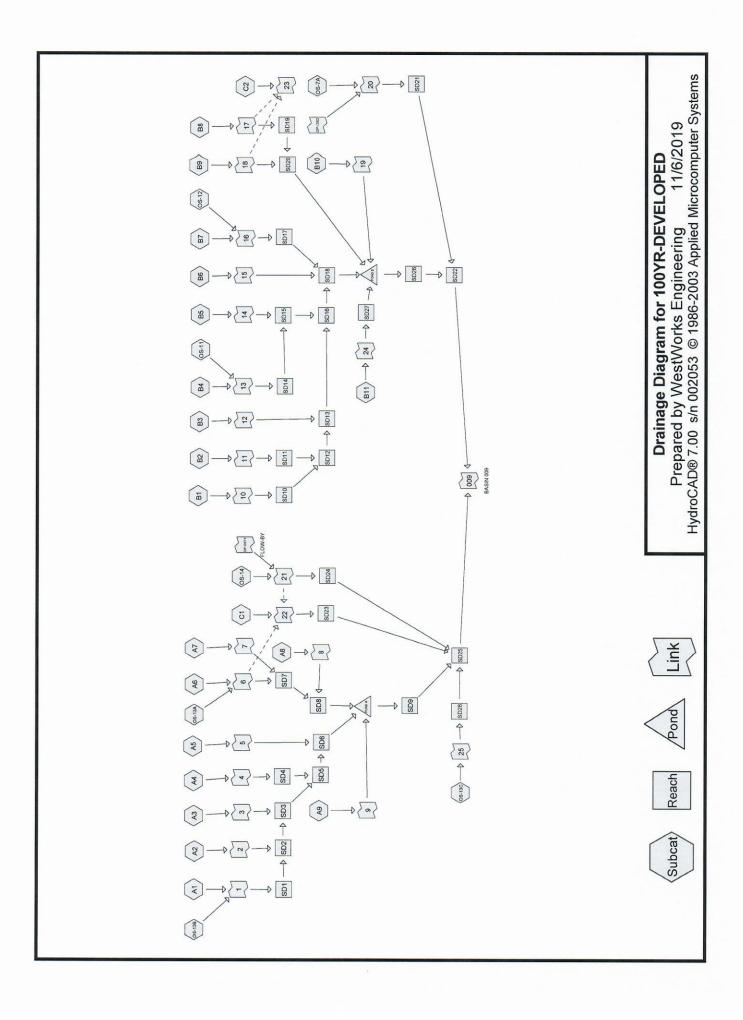
Link DP-OS2:

Inflow = 36.20 cfs @ 0.42 hrs, Volume= 1.257 af

Primary = 36.20 cfs @ 0.42 hrs, Volume= 1.257 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

29 Point hydrograph entered manually, To= 0.00 hrs, dt= 0.03 hrs, Area= 0.000 ac, cfs = 0.00 2.60 5.20 7.80 10.30 12.90 15.50 18.10 20.70 23.30 25.90 28.40 31.00 33.60 36.20 33.60 31.00 28.40 25.90 23.30 20.70 18.10 15.50 12.90 10.30 7.80 5.20 2.60 0.00



El Paso County 100-Year Duration=5 min, Inten=8.68 in/hr

Prepared by WestWorks Engineering

Page 1

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Subcatchment A1:

Runoff

= 2.31 cfs @

@ 0.08 hrs, Volume=

0.016 af, Depth= 0.66"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 100-Year Duration=5 min, Inten=8.68 in/hr

| Area (ac) | С | Description |
|-----------|------|-----------------|
| 0.100 | 0.81 | ROOFTOPS |
| 0.200 | 0.96 | PAVEMENT |

0.300 0.91 Weighted Average

Tc Length Slope Velocity Capacity Description (min) (feet) (ft/ft) (ft/sec) (cfs)

5.0

Direct Entry,

Subcatchment A4:

Runoff

= 2.31 cfs @

0.08 hrs, Volume=

0.016 af, Depth= 0.66"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 100-Year Duration=5 min, Inten=8.68 in/hr

| | Area (ac) | С | Description |
|---|-----------|------|-----------------|
| | 0.100 | 0.81 | ROOFTOP |
| _ | 0.200 | 0.96 | PAVEMENT |
| | | | |

0.300 0.91 Weighted Average

| Tc | Length | Slope | Velocity | Capacity | Description |
|----|--------|-------|----------|----------|-------------|
| | | | | (cfs) | |

5.0

Direct Entry,

Subcatchment A5:

Runoff

= 1.93 cfs @

0.08 hrs, Volume=

0.014 af, Depth= 0.55"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 100-Year Duration=5 min, Inten=8.68 in/hr

| Area (ac) | С | Description |
|-----------|------|-------------|
| 0.100 | 0.35 | LANDSCAPE |
| 0.200 | 0.96 | PAVEMENT |

0.300 0.76 Weighted Average

Tc Length Slope Velocity Capacity Description (min) (feet) (ft/ft) (ft/sec) (cfs)

5.0

Direct Entry,

El Paso County 100-Year Duration=5 min, Inten=8.68 in/hr

Prepared by WestWorks Engineering

Page 2

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Subcatchment B1:

Runoff

= 3.1

3.11 cfs @

0.08 hrs, Volume=

0.022 af, Depth= 0.66"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 100-Year Duration=5 min, Inten=8.68 in/hr

| Area (ac) | С | Description |
|-----------|------|-------------|
| 0.100 | 0.81 | ROOFTOP |
| 0.200 | 0.00 | DAVENTENT |

Tc Length Slope Velocity Capacity Description (min) (feet) (ft/ft) (ft/sec) (cfs)

5.0

Direct Entry,

Subcatchment B11:

Runoff

= 4.18 cfs @

0.08 hrs, Volume=

0.030 af, Depth= 0.40"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 100-Year Duration=5 min, Inten=8.68 in/hr

| Area (ac) | С | Description |
|-----------|------|-------------|
| 0.400 | 0.81 | ROOFTOP |
| 0.500 | 0.35 | LANDSCAPE |
| | | |

0.900 0.55 Weighted Average

| Tc | Length | Slope | Velocity | Capacity | Description |
|-------|--------|---------|----------|----------|--|
| (min) | (feet) | (ft/ft) | (ft/sec) | (cfs) | 50 |
| - | | | | | AND MARKET AND ADDRESS OF THE PARTY OF THE P |

5.0

Direct Entry,

Subcatchment B3:

Runoff

3.11 cfs @

0.08 hrs, Volume=

0.022 af. Depth= 0.66"

Runoff by Rational method, Rise/Fall= $1.0/1.0 \, xTc$, Time Span= $0.00-3.00 \, hrs$, dt= $0.01 \, hrs$ El Paso County 100-Year Duration= $5 \, min$, Inten= $8.68 \, in/hr$

| Area (ac) | С | Description |
|-----------|------|-------------|
| 0.100 | 0.81 | ROOFTOP |

0.300 0.96 PAVEMENT

0.400 0.92 Weighted Average

Tc Length Slope Velocity Capacity Description (min) (feet) (ft/ft) (ft/sec) (cfs)

5.0

Direct Entry,

El Paso County 100-Year Duration=5 min, Inten=8.68 in/hr

Prepared by WestWorks Engineering

Page 3

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Subcatchment B4:

Runoff

= 6.39

6.39 cfs @ 0.08 hrs, Volume=

0.045 af, Depth= 0.61"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 100-Year Duration=5 min, Inten=8.68 in/hr

| Area (ac) | С | Description |
|-----------|------|-------------|
| 0.100 | 0.35 | LANDSCAPE |
| 0.300 | 0.81 | ROOFTOP |
| 0.500 | 0.96 | PAVEMENT |

0.900 0.84 Weighted Average

| Tc | Length | Slope | Slope Velocity | | Description |
|----|--------|-------|----------------|--|-------------|
| | | | (ft/sec) | | |

5.0

Direct Entry,

Subcatchment B5:

Runoff

2.87 cfs @

0.08 hrs, Volume=

0.020 af, Depth= 0.61"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 100-Year Duration=5 min, Inten=8.68 in/hr

| Area (ac) | С | Description |
|-----------|------|-------------|
| 0.050 | 0.35 | LANDSCAPE |
| 0.100 | 0.81 | ROOFTOP |
| 0.250 | 0.96 | PAVEMENT |
| 0.400 | 0.05 | 10/-: |

0.400 0.85 Weighted Average

| Tc | Length | Slope | Velocity | Capacity | Description |
|----|--------|-------|----------|----------|-------------|
| | | | (ft/sec) | | |

5.0

Direct Entry,

Subcatchment B7:

Runoff

4.79 cfs @

0.08 hrs, Volume=

0.034 af, Depth= 0.58"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 100-Year Duration=5 min, Inten=8.68 in/hr

| Area (ac) | С | Description | |
|-----------|------|------------------|--|
| 0.150 | 0.35 | LANDSCAPE | |
| 0.100 | 0.81 | ROOFTOP | |
| 0.450 | 0.96 | PAVEMENT | |
| 0.700 | 0.81 | Weighted Average | |

| 10 | NYR | -DE\ | /FI | OP | FD |
|----|-----|------|-----|----|----|
| | | | | | |

El Paso County 100-Year Duration=5 min, Inten=8.68 in/hr

Prepared by WestWorks Engineering

Page 4

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

| | | Capacity (cfs) | Description |
|-----|--|----------------|--------------|
| 5.0 | | | Direct Entry |

Direct Entry,

Subcatchment B8:

Runoff 4.14 cfs @

0.08 hrs, Volume=

0.029 af, Depth= 0.51"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 100-Year Duration=5 min, Inten=8.68 in/hr

| Area | (ac) | С | Des | cription | | | |
|-------------|--------------|--------|------------------|----------------------|-------------------|-------------|--|
| 0. | 300 | 0.35 | LAN | IDSCAPE | | | |
| 0. | 400 | 0.96 | PA | /EMENT | | | |
| 0. | 700 | 0.70 | Wei | ghted Ave | rage | | |
| Tc (min) | Leng (fee | 100000 | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description | |

Direct Entry,

Subcatchment B9:

Runoff

5.0

1.30 cfs @

0.08 hrs, Volume=

0.009 af, Depth= 0.56"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 100-Year Duration=5 min, Inten=8.68 in/hr

| Area (ac) | С | Description | |
|-----------|------|------------------|--|
| 0.050 | 0.35 | LANDSCAPE | |
| 0.050 | 0.81 | ROOFTOP | |
| 0.100 | 0.96 | PAVEMENT | |
| 0.200 | 0.77 | Weighted Average | |
| | | | |

| 20 20 20 | Length (feet) | | Velocity (ft/sec) | Capacity (cfs) | Description | |
|----------|---------------|----------|-------------------|-------------------|--------------|--|
| 5.0 | () | (1.2.13) | () | (5.5) | Direct Entry | |

Direct Entry,

Subcatchment OS-7A:

Runoff 14.19 cfs @ 0.08 hrs, Volume= 0.101 af, Depth= 0.43"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 100-Year Duration=5 min, Inten=8.68 in/hr

| Area (ac) | С | Description | |
|-----------|------|-------------|--|
| 2.800 | 0.60 | FROM FDR | |

El Paso County 100-Year Duration=5 min, Inten=8.68 in/hr

Prepared by WestWorks Engineering

Page 5

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

| Tc | Length | Slope | Velocity | Capacity | Description |
|----|--------|-------|----------|----------|-------------|
| | | | | (cfs) | |

5.0

Direct Entry, FROM FDR

Reach SD10:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.400 ac, Inflow Depth = 0.66" for 100-Year event

Inflow = 3.11 cfs @ 0.08 hrs, Volume= 0.022 af

Outflow = 3.11 cfs @ 0.08 hrs, Volume= 0.022 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Reach SD19:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.700 ac, Inflow Depth = 0.41" for 100-Year event

Inflow = 2.40 cfs @ 0.05 hrs, Volume= 0.024 af

Outflow = 2.40 cfs @ 0.05 hrs, Volume= 0.024 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Reach SD20:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.900 ac, Inflow Depth = 0.44" for 100-Year event

Inflow = 3.61 cfs @ 0.08 hrs, Volume= 0.033 af

Outflow = 3.61 cfs @ 0.08 hrs, Volume= 0.033 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Reach SD27:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.900 ac, Inflow Depth = 0.40" for 100-Year event Inflow = 0.030 af 0.08 hrs, Volume= 0.030 af

Outflow = 4.18 cfs @ 0.08 hrs, Volume= 0.030 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

El Paso County 100-Year Duration=5 min. Inten=8.68 in/hr

Prepared by WestWorks Engineering

Page 6

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Reach SD4:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area =

0.300 ac, Inflow Depth = 0.66" for 100-Year event

Inflow

2.31 cfs @ 0.08 hrs, Volume=

0.016 af

Outflow

2.31 cfs @

0.08 hrs, Volume=

0.016 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 4:

Inflow Area =

0.300 ac, Inflow Depth = 0.66" for 100-Year event

0.016 af

Inflow Primary 2.31 cfs @ 0.08 hrs. Volume=

2.31 cfs @ 0.08 hrs, Volume=

0.016 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 5:

Inflow Area =

0.300 ac, Inflow Depth = 0.55" for 100-Year event

Inflow Primary 1.93 cfs @

0.08 hrs, Volume= 1.93 cfs @ 0.08 hrs, Volume= 0.014 af 0.014 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-3.00 hrs. dt= 0.01 hrs.

Link 10:

Inflow Area =

0.400 ac, Inflow Depth = 0.66" for 100-Year event

Inflow

3.11 cfs @ 0.08 hrs. Volume=

0.022 af

Primary

3.11 cfs @ 0.08 hrs, Volume=

0.022 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-3.00 hrs. dt= 0.01 hrs.

Link 12:

Inflow Area =

0.400 ac, Inflow Depth = 0.66" for 100-Year event 3.11 cfs @ 0.08 hrs, Volume=

0.022 af

Inflow Primary

3.11 cfs @ 0.08 hrs, Volume=

0.022 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 14:

Inflow Area =

0.400 ac. Inflow Depth = 0.61" for 100-Year event

Inflow

2.87 cfs @

0.08 hrs. Volume=

0.020 af

Primary =

2.87 cfs @ 0.08 hrs, Volume=

0.020 af, Atten= 0%, Lag= 0.0 min

El Paso County 100-Year Duration=5 min, Inten=8.68 in/hr

Prepared by WestWorks Engineering
HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

Page 7

11/6/2019

Link 17:

Inflow Area = 0.700 ac, Inflow Depth = 0.51" for 100-Year event Inflow = 0.029 af

Primary = 2.40 cfs @ 0.05 hrs, Volume= 0.024 af, Atten= 42%, Lag= 0.0 min

Secondary = 1.74 cfs @ 0.08 hrs, Volume= 0.006 af

Primary outflow = Inflow below 2.40 cfs, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 18:

Inflow Area = 0.200 ac, Inflow Depth = 0.56" for 100-Year event 1.30 cfs @ 0.08 hrs, Volume= 0.009 af

Primary = 1.21 cfs @ 0.08 hrs, Volume= 0.009 af, Atten= 7%, Lag= 0.1 min

Secondary = 0.10 cfs @ 0.08 hrs, Volume= 0.000 af

Primary outflow = Inflow below 1.20 cfs, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 24:

Inflow Area = 0.900 ac, Inflow Depth = 0.40" for 100-Year event
Inflow = 0.030 af
0.900 ac, Inflow Depth = 0.40" for 100-Year event
0.030 af

Primary = 4.18 cfs @ 0.08 hrs, Volume= 0.030 af, Atten= 0%, Lag= 0.0 min

El Paso County 100-Year Duration=6 min, Inten=8.22 in/hr

Prepared by WestWorks Engineering

Page 1

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Subcatchment A2:

Runoff

= 2.98 cfs @

0.10 hrs, Volume=

0.025 af, Depth= 0.74"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 100-Year Duration=6 min. Inten=8.22 in/hr

| Area (ac) | С | Description |
|-----------|------|-------------|
| 0.150 | 0.81 | ROOFTOP |
| 0.250 | 0.96 | PAVEMENT |

0.400 0.90 Weighted Average

Tc Length Slope Velocity Capacity Description (min) (feet) (ft/ft) (ft/sec) (cfs)

6.0

Direct Entry,

Subcatchment A3:

Runoff

2.92 cfs @

0.10 hrs, Volume=

0.024 af, Depth= 0.72"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 100-Year Duration=6 min, Inten=8.22 in/hr

| Area (ac) | С | Description |
|-----------|------|-------------|
| 0.200 | 0.81 | ROOFTOP |
| 0.200 | 0.96 | PAVEMENT |

0.400 0.88 Weighted Average

Tc Length Slope Velocity Capacity Description (min) (feet) (ft/ft) (ft/sec) (cfs)

6.0

Direct Entry,

Subcatchment A7:

Runoff

2.55 cfs @

0.10 hrs, Volume=

0.021 af, Depth= 0.63"

Runoff by Rational method, Rise/Fall= $1.0/1.0 \, xTc$, Time Span= $0.00-3.00 \, hrs$, dt= $0.01 \, hrs$ El Paso County 100-Year Duration= $6 \, min$, Inten= $8.22 \, in/hr$

| Area | (ac) | С | Description |
|------|------|------|-------------|
| 0 | .100 | 0.35 | LANDSCAPE |
| 0 | .100 | 0.81 | ROOFTOP |

 0.200
 0.96
 PAVEMENT

 0.400
 0.77
 Weighted Average

| Tc | Lenath | Slope | Velocity | Capacity | Description |
|----|--------|-------|----------|----------|-------------|
| | | | | (cfs) | Becomption |

6.0

Direct Entry,

El Paso County 100-Year Duration=6 min, Inten=8.22 in/hr

Prepared by WestWorks Engineering

Page 2 11/6/2019

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

Subcatchment A8:

Runoff

= 1.37

1.37 cfs @ 0.10 hrs, Volume=

0.011 af, Depth= 0.45"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 100-Year Duration=6 min, Inten=8.22 in/hr

| Area (ac) | С | Description |
|-----------|------|------------------|
| 0.200 | 0.35 | LANDSCAPE |
| 0.100 | 0.96 | PAVEMENT |
| 0.300 | 0.55 | Weighted Average |

| Tc | Length | Slope | Velocity | Capacity | Description |
|----|--------|-------|----------|----------|-------------|
| | | | (ft/sec) | | |

6.0

Direct Entry.

Subcatchment B10:

Runoff

2.34 cfs @

0.10 hrs, Volume=

0.019 af, Depth= 0.39"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 100-Year Duration=6 min, Inten=8.22 in/hr

| Area (ac) | С | Description |
|-----------|------|-------------|
| 0.450 | 0.35 | LANDSCAPE |
| 0.150 | 0.81 | ROOFTOP |
| | | |

0.600 0.47 Weighted Average

| (min) (feet) (ft/ft) (ft/sec) (cfs) | | | | | | Description |
|-------------------------------------|--|--|--|--|--|-------------|
|-------------------------------------|--|--|--|--|--|-------------|

6.0

Direct Entry,

Subcatchment B2:

Runoff

_

2.75 cfs @

0.10 hrs, Volume=

0.023 af, Depth= 0.68"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 100-Year Duration=6 min, Inten=8.22 in/hr

| Area (ac) | С | Description |
|-----------|------|-----------------|
| 0.050 | 0.35 | LANDSCAPE |
| 0.150 | 0.81 | ROOFTOP |
| 0.200 | 0.96 | PAVEMENT |
| | | |

0.400 0.83 Weighted Average

| Tc | Length | Slope | Velocity | Capacity | Description |
|-------|--------|-------|----------|----------|-------------|
| (min) | (feet) | | (ft/sec) | | |

6.0

Direct Entry,

El Paso County 100-Year Duration=6 min, Inten=8.22 in/hr

Prepared by WestWorks Engineering

Page 3

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Subcatchment B6:

Runoff

= 3.52 cfs @ 0.10 hrs, Volume=

0.029 af, Depth= 0.70"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 100-Year Duration=6 min, Inten=8.22 in/hr

| Area (ac) | С | Description |
|-----------|------|-----------------|
| 0.050 | 0.35 | LANDSCAPE |
| 0.150 | 0.81 | ROOFTOP |
| 0.300 | 0.96 | PAVEMENT |
| | | |

0.500 0.85 Weighted Average

| | | | Velocity (ft/sec) | | Description |
|--|--|--|-------------------|--|-------------|
|--|--|--|-------------------|--|-------------|

6.0

Direct Entry,

Subcatchment OS-12:

Runoff

6.47 cfs @

0.10 hrs, Volume=

0.053 af, Depth= 0.49"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs. dt= 0.01 hrs. El Paso County 100-Year Duration=6 min. Inten=8.22 in/hr

| Area (ac) | C | Description |
|-----------|------|-------------|
| 1.300 | 0.60 | FROM FDR |

| Tc | Length | Slope | Velocity | Capacity | Description |
|----|--------|-------|----------|----------|-------------|
| | | | | (cfs) | |

6.0

Direct Entry, FROM FDR

Subcatchment OS-13A:

Runoff

6.10 cfs @ 0.10 hrs, Volume=

0.050 af, Depth= 0.38"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 100-Year Duration=6 min, Inten=8.22 in/hr

| _ | Area (ac) | С | Description |
|---|-----------|------|------------------|
| | 0.300 | 0.96 | PAVEMENT/ROOF |
| | 1.300 | 0.35 | LANDSCAPE |
| | 1.600 | 0.46 | Weighted Average |

| - | | | | 12 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 | |
|----|--------|-------|----------|--|-------------|
| IC | Length | Slope | Velocity | Capacity | Description |
| | | | | (cfc) | 1800 |

6.0

Direct Entry, FROM FDR

El Paso County 100-Year Duration=6 min, Inten=8.22 in/hr

Prepared by WestWorks Engineering

Page 4

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Subcatchment OS-13B:

Runoff

= 1.66 cfs @ 0.10 hrs. Volume=

0.014 af, Depth= 0.33"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 100-Year Duration=6 min, Inten=8.22 in/hr

Area (ac)

C Description

0.500 0.40

LANDSCAPE

Velocity

Capacity Description

Tc Length (min) (feet) Slope (ft/ft)

(ft/sec)

(cfs)

Direct Entry,

Subcatchment OS-13C:

Runoff

6.0

15.12 cfs @

0.10 hrs, Volume=

0.125 af, Depth= 0.39"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 100-Year Duration=6 min, Inten=8.22 in/hr

| Area | (ac) | С | Description |
|------|------|---|-------------|
| | | | |

0.800 0.96 PAVEMENT/ROOF

3.000 0.35 LANDSCAPE

3.800 0.48 Weighted Average

Tc Length

Slope Velocity (ft/ft) (ft/sec)

Capacity Description

(min) (feet) 6.0

(cfs) Direct Entry, FROM FDR

Subcatchment OS-14:

Runoff

54.58 cfs @

0.10 hrs, Volume=

0.451 af. Depth= 0.43"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 100-Year Duration=6 min, Inten=8.22 in/hr

Area (ac)

C Description

12.600 0.54 FROM FDR

Tc Length

Slope Velocity Capacity

Description

(feet) (min)

(ft/ft)

(ft/sec)

(cfs)

6.2

Direct Entry, FROM FDR

El Paso County 100-Year Duration=6 min, Inten=8.22 in/hr

Prepared by WestWorks Engineering

Page 5

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Reach SD1:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area =

0.800 ac, Inflow Depth = 0.49" for 100-Year event

Inflow

3.94 cfs @

0.10 hrs, Volume=

0.032 af

Outflow

3.94 cfs @

0.10 hrs, Volume=

0.032 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Reach SD11:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area =

=

0.400 ac, Inflow Depth = 0.68" for 100-Year event

Inflow Outflow

2.75 cfs @ 2.75 cfs @

0.10 hrs, Volume= 0.10 hrs, Volume=

0.023 af 0.023 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Reach SD12:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area =

0.800 ac, Inflow Depth = 0.72" for 100-Year event

Inflow

5.82 cfs @ 0.10 hrs, Volume= 0.048 af

Outflow

5.82 cfs @ 0.10 hrs, Volume=

0.048 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Reach SD13:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area =

1.200 ac, Inflow Depth = 0.73" for 100-Year event

Inflow

8.90 cfs @

0.10 hrs, Volume=

0.073 af

Outflow

8.90 cfs @

0.10 hrs, Volume=

0.073 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Reach SD17:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area =

2.000 ac. Inflow Depth = 0.55" for 100-Year event

0.092 af

Inflow Outflow 11.19 cfs @ 11.19 cfs @

0.10 hrs, Volume= 0.10 hrs, Volume=

0.092 af, Atten= 0%, Lag= 0.0 min

El Paso County 100-Year Duration=6 min, Inten=8.22 in/hr

Prepared by WestWorks Engineering

Page 6

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Reach SD2:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 1.200 ac, Inflow Depth = 0.57" for 100-Year event Inflow = 0.057 af

Outflow = 6.91 cfs @ 0.10 hrs, Volume= 0.057 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Reach SD28:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 3.800 ac, Inflow Depth = 0.39" for 100-Year event 15.12 cfs @ 0.10 hrs, Volume= 0.125 af

Outflow = 15.12 cfs @ 0.10 hrs, Volume= 0.125 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Reach SD3:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 1.600 ac, Inflow Depth = 0.61" for 100-Year event Inflow = 9.83 cfs @ 0.10 hrs, Volume= 0.081 af

Outflow = 9.83 cfs @ 0.10 hrs, Volume= 0.081 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Reach SD5:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 1.900 ac, Inflow Depth = 0.63" for 100-Year event 12.10 cfs @ 0.10 hrs, Volume= 0.100 af

Outflow = 12.10 cfs @ 0.10 hrs, Volume= 0.100 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Reach SD6:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 2.200 ac, Inflow Depth = 0.63" for 100-Year event 14.01 cfs @ 0.10 hrs, Volume= 0.115 af

Outflow = 14.01 cfs @ 0.10 hrs, Volume= 0.115 af, Atten= 0%, Lag= 0.0 min

El Paso County 100-Year Duration=6 min, Inten=8.22 in/hr

Prepared by WestWorks Engineering

Page 7

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 1:

Inflow Area = 0.800 ac, Inflow Depth = 0.49" for 100-Year event

Inflow = 3.94 cfs @ 0.10 hrs, Volume= 0.032 af

Primary = 3.94 cfs @ 0.10 hrs, Volume= 0.032 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-3.00 hrs. dt= 0.01 hrs.

Link 2:

Inflow Area = 0.400 ac, Inflow Depth = 0.74" for 100-Year event

Inflow = 2.98 cfs @ 0.10 hrs, Volume= 0.025 af

Primary = 2.98 cfs @ 0.10 hrs, Volume= 0.025 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 3:

Inflow Area = 0.400 ac, Inflow Depth = 0.72" for 100-Year event 2.92 cfs @ 0.10 hrs, Volume= 0.024 af

Primary = 2.92 cfs @ 0.10 hrs, Volume= 0.024 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 7:

Inflow Area = 0.400 ac, Inflow Depth = 0.63" for 100-Year event 2.55 cfs @ 0.10 hrs, Volume= 0.021 af

Primary outflow = Inflow, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 8:

Inflow Area = 0.300 ac, Inflow Depth = 0.45" for 100-Year event

Inflow = 1.37 cfs @ 0.10 hrs, Volume= 0.011 af

Primary = 1.37 cfs @ 0.10 hrs, Volume= 0.011 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 11:

Inflow Area = 0.400 ac, Inflow Depth = 0.68" for 100-Year event Inflow = 0.75 cfs @ 0.10 hrs. Volume= 0.023 af

Primary = 2.75 cfs @ 0.10 hrs, Volume= 0.023 af, Atten= 0%, Lag= 0.0 min

El Paso County 100-Year Duration=6 min, Inten=8.22 in/hr

Prepared by WestWorks Engineering

Page 8

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Link 15:

Inflow Area = 0.500 ac, Inflow Depth = 0.70" for 100-Year event Inflow 3.52 cfs @ 0.10 hrs, Volume=

0.029 af Primary 3.52 cfs @ 0.10 hrs, Volume= 0.029 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 16:

Inflow Area = 2.000 ac, Inflow Depth = 0.55" for 100-Year event Inflow 11.19 cfs @ 0.10 hrs, Volume= 0.092 af

Primary 11.19 cfs @ 0.10 hrs, Volume= 0.092 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 19:

Inflow Area = 0.600 ac, Inflow Depth = 0.39" for 100-Year event Inflow

2.34 cfs @ 0.10 hrs, Volume= 0.019 af

Primary 2.34 cfs @ 0.10 hrs, Volume= 0.019 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 25:

Inflow Area = 3.800 ac, Inflow Depth = 0.39" for 100-Year event Inflow = 15.12 cfs @ 0.10 hrs, Volume= 0.125 af

Primary = 15.12 cfs @ 0.10 hrs, Volume= 0.125 af, Atten= 0%, Lag= 0.0 min

El Paso County 100-Year Duration=7 min, Inten=7.83 in/hr

Prepared by WestWorks Engineering

Page 1

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Subcatchment OS-11:

Runoff

13.79 cfs @

0.12 hrs, Volume=

0.136 af. Depth= 0.58"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 100-Year Duration=7 min, Inten=7.83 in/hr

Area (ac)

C Description

2.800 0.64

FROM FDR

Tc Length

Slope (ft/ft)

Velocity

Capacity Description (cfs)

(min) (feet) 7.0

(ft/sec)

Direct Entry, FROM FDR

Reach SD14:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area =

3.700 ac, Inflow Depth = 0.63" for 100-Year event

Inflow

19.66 cfs @

0.12 hrs, Volume=

0.194 af

Outflow

19.66 cfs @

0.12 hrs, Volume=

0.194 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Reach SD15:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area =

4.100 ac, Inflow Depth = 0.64" for 100-Year event

Inflow

22.31 cfs @

0.12 hrs, Volume=

0.220 af

Outflow

22.31 cfs @

0.12 hrs, Volume=

0.220 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Reach SD16:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area =

5.300 ac, Inflow Depth = 0.68" for 100-Year event

Inflow

30.50 cfs @

0.11 hrs, Volume=

0.301 af

Outflow

30.50 cfs @

0.11 hrs, Volume=

0.301 af. Atten= 0%. Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

El Paso County 100-Year Duration=7 min, Inten=7.83 in/hr

Prepared by WestWorks Engineering

Page 2

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Reach SD18:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 7.800 ac, Inflow Depth = 0.67" for 100-Year event

Inflow = 44.43 cfs @ 0.11 hrs, Volume= 0.436 af

Outflow = 44.43 cfs @ 0.11 hrs, Volume= 0.436 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Reach SD26:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 10.200 ac, Inflow Depth = 0.09" for 100-Year event

Inflow = 0.32 cfs @ 0.23 hrs, Volume= 0.074 af

Outflow = 0.32 cfs @ 0.23 hrs, Volume= 0.074 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 13:

Inflow Area = 3.700 ac, Inflow Depth = 0.63" for 100-Year event 19.66 cfs @ 0.12 hrs, Volume= 0.194 af

Inflow = 19.66 cfs @ 0.12 hrs, Volume= 0.194 af Primary = 19.66 cfs @ 0.12 hrs, Volume= 0.194 af, Atten= 0%, Lag= 0.0 min

El Paso County 100-Year Duration=9 min, Inten=7.20 in/hr

Prepared by WestWorks Engineering

Page 1

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Subcatchment A9:

Runoff

1.82 cfs @

0.15 hrs, Volume=

0.023 af, Depth= 0.54"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 100-Year Duration=9 min, Inten=7.20 in/hr

Area (ac)

C Description

0.500 0.50

LANDSCAPE

Tc Length (min)

Slope Velocity Capacity

Description

(feet)

(ft/ft) (ft/sec) (cfs)

9.0

Direct Entry,

Subcatchment C1:

Runoff

2.83 cfs @

0.15 hrs, Volume=

0.035 af, Depth= 0.70"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 100-Year Duration=9 min, Inten=7.20 in/hr

| Area (ac) | С | Description |
|-----------|------|-------------|
| 0.000 | 0.0= | |

LANDSCAPE 0.35 0.300 **PAVEMENT** 0.300 0.96

0.600 0.65 Weighted Average

(min)

Slope Velocity

Description

(feet) (ft/ft)

Tc Length

(ft/sec)

(cfs)

Capacity

9.0

Direct Entry,

Link 9:

Inflow Area =

0.500 ac, Inflow Depth = 0.54" for 100-Year event

0.023 af

Inflow Primary 1.82 cfs @

1.82 cfs @

0.15 hrs, Volume= 0.15 hrs, Volume=

0.023 af, Atten= 0%, Lag= 0.0 min

El Paso County 100-Year Duration=11 min, Inten=6.69 in/hr

Prepared by WestWorks Engineering

Page 1

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Subcatchment A6:

Runoff

5.70 cfs @

0.18 hrs, Volume=

0.088 af, Depth= 0.96"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 100-Year Duration=11 min. Inten=6.69 in/hr

| Area (ac) | С | Description |
|-----------|------|-------------|
| 0.300 | 0.35 | LANDSCAPE |
| 0.100 | 0.81 | ROOFTOP |
| 0.700 | 0.96 | PAVEMENT |

1.100 0.78 Weighted Average

| Tc | Length | Slope | Velocity | Capacity | Description |
|----|--------|-------|----------|----------|-------------|
| | (feet) | | (ft/sec) | | |

11.0

Direct Entry,

Subcatchment C2:

Runoff

5.18 cfs @

0.18 hrs. Volume=

0.080 af, Depth= 0.80"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 100-Year Duration=11 min, Inten=6.69 in/hr

| _ | Area (ac) | C | Description |
|---|-----------|------|-----------------|
| | 0.600 | 0.35 | LANDSCAPE |
| _ | 0.600 | 0.96 | PAVEMENT |
| | 4 200 | 0.05 | \A/-: |

1.200 0.65 Weighted Average

| Tc | Length | Slope | Velocity | Capacity | Description |
|----|--------|-------|----------|----------|-------------|
| | | | (ft/sec) | | |

11.0

Direct Entry,

Reach SD7:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 3.100 ac, Inflow Depth = 0.74" for 100-Year event

Inflow Outflow

11.28 cfs @ 0.14 hrs, Volume= 11.28 cfs @ 0.14 hrs, Volume=

0.190 af 0.190 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Reach SD8:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 3.400 ac, Inflow Depth = 0.73" for 100-Year event Inflow 12.39 cfs @ 0.14 hrs, Volume= 0.207 af

Outflow 12.39 cfs @ 0.14 hrs, Volume= 0.207 af, Atten= 0%, Lag= 0.0 min

El Paso County 100-Year Duration=11 min, Inten=6.69 in/hr

Prepared by WestWorks Engineering

Page 2

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Reach SD9:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area =

6.100 ac, Inflow Depth = 0.15" for 100-Year event

Inflow

1.83 cfs @

0.32 hrs, Volume=

0.074 af

Outflow

1.83 cfs @

0.32 hrs, Volume=

0.074 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 6:

Inflow Area =

2.700 ac, Inflow Depth = 0.72" for 100-Year event

Inflow = Primary

10.65 cfs @ 9.20 cfs @

0.18 hrs, Volume= 0.14 hrs, Volume=

0.159 af, Atten= 14%, Lag= 0.0 min

Secondary =

1.45 cfs @

0.18 hrs, Volume=

0.004 af

0.163 af

Primary outflow = Inflow below 9.20 cfs, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 23:

Inflow Area =

1.200 ac, Inflow Depth = 0.89" for 100-Year event

Inflow =

6.07 cfs @ 0.18 hrs, Volume=

0.089 af

Primary

6.07 cfs @ 0.18 hrs, Volume=

0.089 af, Atten= 0%, Lag= 0.0 min

El Paso County 100-Year Duration=20 min, Inten=5.19 in/hr

Prepared by WestWorks Engineering

Page 1

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Reach SD23:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area =

0.600 ac, Inflow Depth = 5.92" for 100-Year event

Inflow = 14.15 cfs @

0.15 hrs, Volume=

0.296 af

Outflow

14.15 cfs @

0.15 hrs, Volume=

0.296 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Reach SD24:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area =

78.100 ac, Inflow Depth = 0.27" for 100-Year event

1.741 af

Inflow = Outflow =

46.90 cfs @ 46.90 cfs @

0.10 hrs, Volume= 0.10 hrs, Volume=

1.741 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs. dt= 0.01 hrs.

Reach SD25:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area =

88.600 ac. Inflow Depth = 0.34" for 100-Year event

Inflow

=

72.52 cfs @

0.33 hrs. Volume=

2.528 af

Outflow

72.52 cfs @ 0.33 hrs, Volume=

2.528 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 21:

Inflow Area =

78.100 ac, Inflow Depth = 0.30" for 100-Year event

Inflow Primary

59.01 cfs @ 46.90 cfs @

0.15 hrs. Volume= 0.10 hrs, Volume= 1.981 af

Secondary =

12.11 cfs @

0.15 hrs, Volume=

1.741 af, Atten= 21%, Lag= 0.0 min 0.240 af

Primary outflow = Inflow below 46.90 cfs, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 22:

Inflow Area =

0.600 ac, Inflow Depth = 5.92" for 100-Year event

Inflow =

14.15 cfs @

0.15 hrs, Volume=

0.296 af

Primary

14.15 cfs @ 0.15 hrs, Volume=

0.296 af, Atten= 0%, Lag= 0.0 min

El Paso County 100-Year Duration=20 min, Inten=5.19 in/hr

Prepared by WestWorks Engineering

Page 2

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Link DP-OS11: FLOW-BY

Inflow Area = 65.500 ac, Inflow Depth = 0.27" for 100-Year event

Inflow 54.10 cfs @ 0.33 hrs, Volume= 1.475 af

Primary = 23.40 cfs @ 0.15 hrs, Volume= 1.000 af, Atten= 57%, Lag= 0.0 min

Secondary = 30.70 cfs @ 0.33 hrs, Volume= 0.475 af

Primary outflow = Inflow below 23.40 cfs, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

23 Point hydrograph entered manually, To= 0.00 hrs, dt= 0.03 hrs, Area= 65.500 ac, cfs =

0.00 4.90 9.80 14.80 19.70 24.60 29.50 34.40 39.30 44.30 49.20 54.10 49.20 44.30 39.30 34.40 29.50 24.60 19.70 14.80

9.80 4.90 0.00

100YR-DEVELOPED

El Paso County 100-Year Duration=25 min. Inten=4.62 in/hr

Prepared by WestWorks Engineering

Page 1

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Reach SD21:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area =

2.800 ac, Inflow Depth = 14.86" for 100-Year event

Inflow = 99.65 cfs @

0.42 hrs, Volume=

3.466 af

Outflow

99.65 cfs @

0.42 hrs, Volume=

3.466 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Reach SD22:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area =

13.000 ac, Inflow Depth = 3.68" for 100-Year event

Inflow Outflow = 104.88 cfs @

104.88 cfs @

0.42 hrs, Volume= 0.42 hrs. Volume= 3.983 af

3.983 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 009: BASIN 009

Inflow Area =

101.600 ac, Inflow Depth = 0.79" for 100-Year event

Inflow

171.59 cfs @

0.42 hrs, Volume=

6.715 af

Primary = 171.59 cfs @ 0.42 hrs, Volume=

6.715 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-3.00 hrs. dt= 0.01 hrs.

Link 20:

Inflow Area =

2.800 ac, Inflow Depth = 14.86" for 100-Year event

Inflow = 99.65 cfs @

0.42 hrs, Volume=

3.466 af

Primary

99.65 cfs @

0.42 hrs, Volume=

3.466 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-3.00 hrs. dt= 0.01 hrs.

Link DP-OS2:

Inflow

92.10 cfs @

0.42 hrs, Volume=

3.197 af

Primary =

92.10 cfs @

0.42 hrs, Volume=

3.197 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

29 Point hydrograph entered manually, To= 0.00 hrs, dt= 0.03 hrs, Area= 0.000 ac, cfs = 0.00 6.60

19.70 26.30 32.90 39.50

46.10 52.60

59.20

65.80 72.40 13.20 78.90

85.50

85.50

78.90

52.60

92.10 26.30

19.70

65.80

0.00

59.20

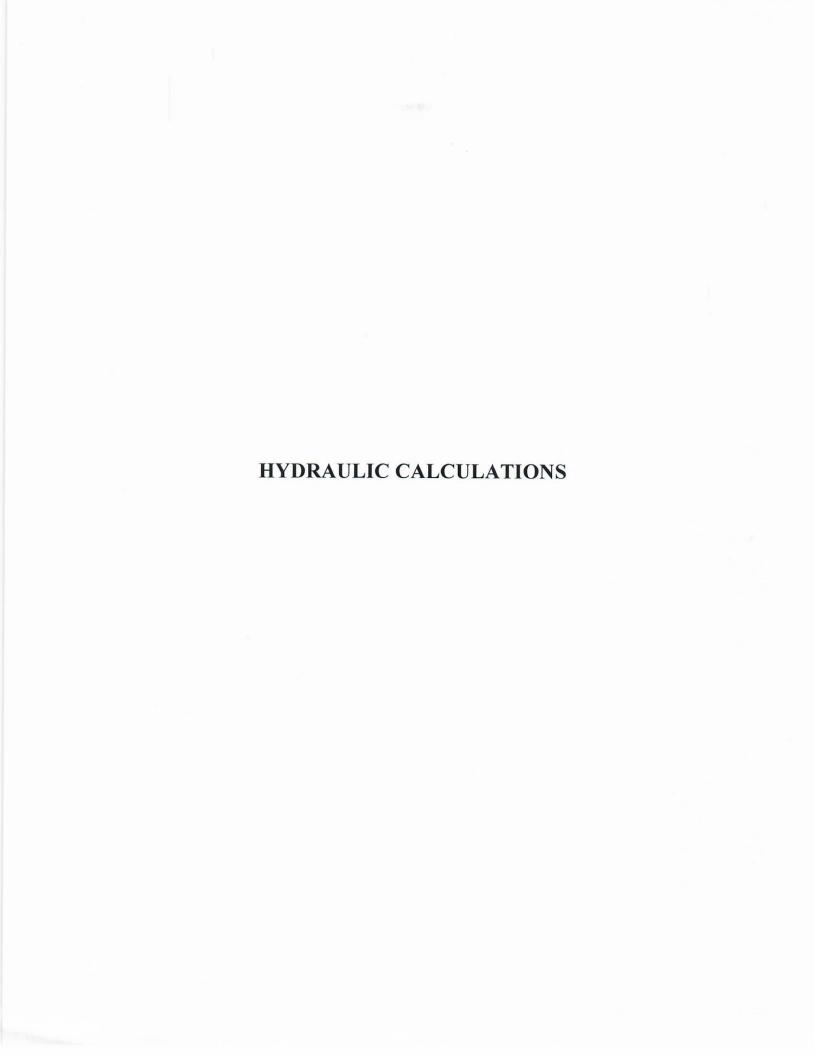
46.10

39.50

32.90

13.20

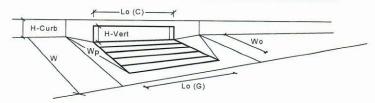
72.40 6.60



ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

ELDORADO SPRINGS

DP-1 Project: Inlet ID: STREET Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb TBACK = 5.0 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) SBACK = 0.020 ft/ft Manning's Roughness Behind Curb (typically between 0.012 and 0.020) nBACK : Height of Curb at Gutter Flow Line H_{CURB} : 6.00 Distance from Curb Face to Street Crown TCROWN : 24.0 Gutter Width W= 2.00 Street Transverse Slope Sx = 0.020 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) S_W = 0.083 ft/ft Street Longitudinal Slope - Enter 0 for sump condition So: 0.000 Manning's Roughness for Street Section (typically between 0.012 and 0.020) n_{STREET} = 0.012 Major Storm Max. Allowable Spread for Minor & Major Storm 24.0 24.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm Check boxes are not applicable in SUMP conditions MINOR STORM Allowable Capacity is based on Depth Criterion MAJOR STORM Allowable Capacity is based on Depth Criterion Major Storm SUMP SUMP



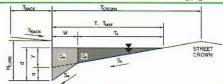
| Design Information (Input) CDOT Type R Curb Opening | | MINOR | MAJOR | |
|--|-----------------------------|-------------|--------------|-----------------|
| ype of inlet | Type = | CDOT Type R | Curb Opening | 7 |
| Local Depression (additional to continuous gutter depression 'a' from above) | a _{local} = | 3.00 | 3 00 | inches |
| Number of Unit Inlets (Grate or Curb Opening) | No = | 1 | 1 | |
| Nater Depth at Flowline (outside of local depression) | Ponding Depth = | 6.0 | 6.0 | inches |
| Grate Information | _ | MINOR | MAJOR | Override Depths |
| ength of a Unit Grate | L _o (G) = | N/A | N/A | feet |
| Nidth of a Unit Grate | W _o = | N/A | N/A | feet |
| Area Opening Ratio for a Grate (typical values 0.15-0.90) | A _{ratio} = | N/A | N/A | |
| Clogging Factor for a Single Grate (typical value 0.50 - 0.70) | C _f (G) = | N/A | N/A | 7 |
| Grate Weir Coefficient (typical value 2.15 - 3.60) | C _w (G) = | N/A | N/A | |
| Grate Orifice Coefficient (typical value 0.60 - 0.80) | C _o (G) = | N/A | N/A | |
| Curb Opening Information | | MINOR | MAJOR | _ |
| ength of a Unit Curb Opening | L _o (C) = | 5.00 | 5.00 | feet |
| Height of Vertical Curb Opening in Inches | H _{vert} = | 6.00 | 6.00 | inches |
| Height of Curb Orifice Throat in Inches | H _{throat} = | 6.00 | 6.00 | inches |
| Angle of Throat (see USDCM Figure ST-5) | Theta = | 63.40 | 63.40 | degrees |
| Side Width for Depression Pan (typically the gutter width of 2 feet) | W _p = | 2.00 | 2.00 | feet |
| Clogging Factor for a Single Curb Opening (typical value 0.10) | $C_{f}(C) =$ | 0.10 | 0.10 | |
| Curb Opening Weir Coefficient (typical value 2.3-3.7) | C _w (C) = | 3.60 | 3,60 | |
| Curb Opening Orifice Coefficient (typical value 0.60 - 0.70) | C _o (C) = | 0.67 | 0.67 | |
| ow Head Performance Reduction (Calculated) | | MINOR | MAJOR | |
| Depth for Grate Midwidth | d _{Grate} = | N/A | N/A | T ft |
| Pepth for Curb Opening Weir Equation | d _{Curb} = | 0.33 | 0.33 | ft |
| Combination Inlet Performance Reduction Factor for Long Inlets | RF _{Combination} = | 0.77 | 0.77 | |
| Curb Opening Performance Reduction Factor for Long Inlets | RF _{Curb} = | 1.00 | 1.00 | 1 |
| Grated Inlet Performance Reduction Factor for Long Inlets | RF _{Grate} = | N/A | N/A |] |
| | | MINOR | MAJOR | |
| Total Inlet Interception Capacity (assumes clogged condition) | $Q_a =$ | 5.4 | 5.4 | cfs |
| nlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK) | Q PEAK REQUIRED = | 2.0 | 4.0 | cfs |

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)
ELDORADO SPRINGS

Project: Inlet ID:

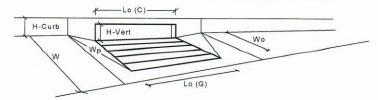
DP-2



Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb TBACK = 5.0 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) SBACK = 0.020 ft/ft Manning's Roughness Behind Curb (typically between 0.012 and 0.020) **NBACK** 0.020 Height of Curb at Gutter Flow Line H_{CURB} = 6.00 inches Distance from Curb Face to Street Crown TCROWN 24.0 Gutter Width W= 2.00 Street Transverse Slope Sx = 0.020 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) S_W = 0.083 ft/ft Street Longitudinal Slope - Enter 0 for sump condition So: 0.000 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) n_{STREET} = 0.012 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm Max. Allowable Depth at Gutter Flowline for Minor & Major Storm 6.0 6.0 Check boxes are not applicable in SUMP conditions MINOR STORM Allowable Capacity is based on Depth Criterion MAJOR STORM Allowable Capacity is based on Depth Criterion Minor Storm Major Storm

SUMP

SUMP



| Design Information (Input) CDOT Type R Curb Opening ▼ | | MINOR | MAJOR | |
|---|-----------------------------|-------------|--------------|-----------------|
| Type of Inlet CDOT Type R Curb Opening | Type = | CDOT Type R | Curb Opening | 7 |
| ocal Depression (additional to continuous gutter depression 'a' from above) | a _{local} = | 3.00 | 3.00 | inches |
| Number of Unit Inlets (Grate or Curb Opening) | No = | 1 | 1 | |
| Nater Depth at Flowline (outside of local depression) | Ponding Depth = | 6.0 | 6.0 | inches |
| Grate Information | | MINOR | MAJOR | Override Depths |
| ength of a Unit Grate | L _o (G) = | N/A | N/A | feet |
| Nidth of a Unit Grate | W _o = | N/A | N/A | feet |
| Area Opening Ratio for a Grate (typical values 0.15-0.90) | A _{ratio} = | N/A | N/A | |
| Clogging Factor for a Single Grate (typical value 0.50 - 0.70) | C _f (G) = | N/A | N/A | |
| Grate Weir Coefficient (typical value 2.15 - 3.60) | C _w (G) = | N/A | N/A | |
| Grate Orifice Coefficient (typical value 0.60 - 0.80) | C _o (G) = | N/A | N/A | |
| Curb Opening Information | | MINOR | MAJOR | _ |
| ength of a Unit Curb Opening | L _o (C) = | 5.00 | 5.00 | feet |
| Height of Vertical Curb Opening in Inches | H _{vert} = | 6.00 | 6.00 | inches |
| Height of Curb Orifice Throat in Inches | H _{throat} = | 6.00 | 6.00 | inches |
| Angle of Throat (see USDCM Figure ST-5) | Theta = | 63.40 | 63.40 | degrees |
| Side Width for Depression Pan (typically the gutter width of 2 feet) | W _p = | 2.00 | 2.00 | feet |
| Clogging Factor for a Single Curb Opening (typical value 0.10) | $C_{f}(C) =$ | 0.10 | 0.10 | |
| Curb Opening Weir Coefficient (typical value 2.3-3.7) | C _w (C) = | 3.60 | 3,60 | |
| Curb Opening Orifice Coefficient (typical value 0.60 - 0.70) | C _o (C) = | 0.67 | 0.67 | |
| Low Head Performance Reduction (Calculated) | | MINOR | MAJOR | |
| Depth for Grate Midwidth | d _{Grate} = | N/A | N/A | ft |
| Depth for Curb Opening Weir Equation | d _{Curb} = | 0.33 | 0.33 | ft |
| Combination Inlet Performance Reduction Factor for Long Inlets | RF _{Combination} = | 0.77 | 0.77 | |
| Curb Opening Performance Reduction Factor for Long Inlets | RF _{Curb} = | 1.00 | 1.00 | |
| Grated Inlet Performance Reduction Factor for Long Inlets | RF _{Grate} = | N/A | N/A | |
| | | MINOR | MAJOR | |
| Total Inlet Interception Capacity (assumes clogged condition) | $Q_a =$ | 5.4 | 5.4 | cfs |
| nlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK) | Q PEAK REQUIRED = | 2.0 | 3.0 | cfs |

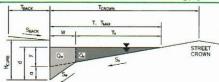
ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

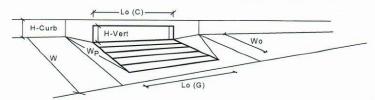
ELDORADO SPRINGS

DP-3

Project: Inlet ID:



| Gutter Geometry (Enter data in the blue cells) | | | _ | |
|--|-----------------------|-------------|---------------------|--------|
| Maximum Allowable Width for Spread Behind Curb | T _{BACK} = | 5.0 | ft | |
| Side Slope Behind Curb (leave blank for no conveyance credit behind curb) | S _{BACK} = | 0.020 | ft/ft | |
| Manning's Roughness Behind Curb (typically between 0.012 and 0.020) | n _{BACK} = | 0.020 |] | |
| Height of Curb at Gutter Flow Line | H _{CURB} = | 6.00 | inches | |
| Distance from Curb Face to Street Crown | T _{CROWN} = | 24.0 | ft | |
| Gutter Width | W= | 3.00 | ft | |
| Street Transverse Slope | S _X = | 0.020 | ft/ft | |
| Sutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) | S _W = | 0.083 | ft/ft | |
| Street Longitudinal Slope - Enter 0 for sump condition | So = | 0.000 | ft/ft | |
| Manning's Roughness for Street Section (typically between 0.012 and 0.020) | n _{street} = | 0.012 | | |
| | | Minor Storm | Major Storm | |
| Max. Allowable Spread for Minor & Major Storm | T _{MAX} = | 24.0 | 24.0 | ft |
| Max. Allowable Depth at Gutter Flowline for Minor & Major Storm | d _{MAX} = | 6.0 | 6.0 | inches |
| Check boxes are not applicable in SUMP conditions | _ | Г | Г | _ |
| MINOR STORM Allowable Capacity is based on Depth Criterion | | Minor Storm | Major Storm | |
| INIOR STORM Allowable Capacity is based on Depth Criterion IAJOR STORM Allowable Capacity is based on Depth Criterion | Q _{allow} = | SUMP | Major Storm SUMP | cfs |



| Design Information (Input) | CDOT Type C Grate ▼ | | MINOR | MAJOR | |
|------------------------------------|--|-----------------------------|---------|------------|-----------------|
| Type of Inlet | 1 | Type = | CDOT Ty | oe C Grate | |
| Local Depression (additional to | continuous gutter depression 'a' from above) | a _{local} = | 6.00 | 6.00 | inches |
| Number of Unit Inlets (Grate or | Curb Opening) | No = | 1 | 1 | |
| Water Depth at Flowline (outsid | e of local depression) | Ponding Depth = | 6.0 | 6.0 | inches |
| Grate Information | | | MINOR | MAJOR | Override Depths |
| Length of a Unit Grate | | L _o (G) = | 2.92 | 2.92 | feet |
| Width of a Unit Grate | | W _o = | 2.92 | 2.92 | feet |
| Area Opening Ratio for a Grate | , , | A _{ratio} = | 0.70 | 0.70 | |
| Clogging Factor for a Single Gra | ate (typical value 0.50 - 0.70) | $C_f(G) =$ | 0.50 | 0.50 | |
| Grate Weir Coefficient (typical v | alue 2.15 - 3.60) | C _w (G) = | 2.41 | 2.41 | |
| Grate Orifice Coefficient (typical | value 0.60 - 0.80) | C _o (G) = | 0.67 | 0.67 | |
| Curb Opening Information | | | MINOR | MAJOR | _ |
| Length of a Unit Curb Opening | | L _o (C) = | N/A | N/A | feet |
| Height of Vertical Curb Opening | in Inches | H _{vert} = | N/A | N/A | inches |
| Height of Curb Orifice Throat in | Inches | H _{throat} = | N/A | N/A | inches |
| Angle of Throat (see USDCM Fi | gure ST-5) | Theta = | N/A | N/A | degrees |
| Side Width for Depression Pan (| (typically the gutter width of 2 feet) | W _p = | N/A | N/A | feet |
| Clogging Factor for a Single Cur | rb Opening (typical value 0.10) | $C_f(C) =$ | N/A | N/A | |
| Curb Opening Weir Coefficient (| typical value 2.3-3.7) | C _w (C) = | N/A | N/A | - |
| Curb Opening Orifice Coefficien | t (typical value 0.60 - 0.70) | C _o (C) = | N/A | N/A | |
| Low Head Performance Reduc | ction (Calculated) | | MINOR | MAJOR | |
| Depth for Grate Midwidth | | d _{Grate} = | 0.635 | 0.635 | ft |
| Depth for Curb Opening Weir Ed | quation | d _{Curb} = | N/A | N/A | ft |
| | Reduction Factor for Long Inlets | RF _{Combination} = | N/A | N/A | |
| Curb Opening Performance Rec | | RF _{Curb} = | N/A | N/A | |
| Grated Inlet Performance Reduc | tion Factor for Long Inlets | RF _{Grate} = | 0.95 | 0.95 | |
| | | 2.1 | MINOR | MAJOR | |
| Total Inlet Interception C | apacity (assumes clogged condition) | Q _a = | 4.2 | 4.2 | cfs |
| nlet Capacity IS GOOD for Min | nor and Major Storms(>Q PEAK) | Q PEAK REQUIRED = | 2.0 | 3.0 | cfs |

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) ELDORADO SPRINGS Project: Inlet ID: DP-4 STREET Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb TBACK = 5.0 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) Manning's Roughness Behind Curb (typically between 0.012 and 0.020) SBACK 0.020 ft/ft 0.020 Height of Curb at Gutter Flow Line H_{CURB} 6.00 inches Distance from Curb Face to Street Crown TCROWN 24.0 Gutter Width W= 2.00 Street Transverse Slope Sx = 0.020 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) S_W : 0.083 ft/ft Street Longitudinal Slope - Enter 0 for sump condition So 0.000 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) n_{STREET} = 0.012 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm 24.0 24.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm 6.0 6.0 Check boxes are not applicable in SUMP conditions

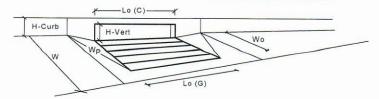
Minor Storm

SUMP

Major Storm

SUMP

MINOR STORM Allowable Capacity is based on Depth Criterion MAJOR STORM Allowable Capacity is based on Depth Criterion



| Design Information (Input) CDOT Type R Curb Opening | | MINOR | MAJOR | |
|--|-----------------------------|-------------|--------------|-----------------|
| Type of Inlet | Type = | CDOT Type R | Curb Opening | |
| Local Depression (additional to continuous gutter depression 'a' from above) | a _{local} = | 3.00 | 3.00 | inches |
| Number of Unit Inlets (Grate or Curb Opening) | No = | 1 | 1 | |
| Water Depth at Flowline (outside of local depression) | Ponding Depth = | 6.0 | 6.0 | inches |
| Grate Information | | MINOR | MAJOR | Override Depths |
| Length of a Unit Grate | L _o (G) = | N/A | N/A | feet |
| Width of a Unit Grate | W _o = | N/A | N/A | feet |
| Area Opening Ratio for a Grate (typical values 0.15-0.90) | A _{ratio} = | N/A | N/A | |
| Clogging Factor for a Single Grate (typical value 0.50 - 0.70) | C _f (G) = | N/A | N/A | 7 |
| Grate Weir Coefficient (typical value 2.15 - 3.60) | C _w (G) = | N/A | N/A | |
| Grate Orifice Coefficient (typical value 0.60 - 0.80) | C _o (G) = | N/A | N/A | |
| Curb Opening Information | | MINOR | MAJOR | _ |
| Length of a Unit Curb Opening | L _o (C) = | 5.00 | 5.00 | feet |
| Height of Vertical Curb Opening in Inches | H _{vert} = | 6.00 | 6.00 | inches |
| Height of Curb Orifice Throat in Inches | H _{throat} = | 6.00 | 6.00 | inches |
| Angle of Throat (see USDCM Figure ST-5) | Theta = | 63.40 | 63.40 | degrees |
| Side Width for Depression Pan (typically the gutter width of 2 feet) | W _p = | 2.00 | 2.00 | feet |
| Clogging Factor for a Single Curb Opening (typical value 0.10) | $C_{f}(C) =$ | 0.10 | 0.10 | |
| Curb Opening Weir Coefficient (typical value 2.3-3.7) | C _w (C) = | 3.60 | 3.60 | |
| Curb Opening Orifice Coefficient (typical value 0.60 - 0.70) | C _o (C) = | 0.67 | 0.67 | |
| Low Head Performance Reduction (Calculated) | | MINOR | MAJOR | |
| Depth for Grate Midwidth | d _{Grate} = | N/A | N/A | Tft . |
| Depth for Curb Opening Weir Equation | d _{Curb} = | 0.33 | 0.33 | ft |
| Combination Inlet Performance Reduction Factor for Long Inlets | RF _{Combination} = | 0.77 | 0.77 | |
| Curb Opening Performance Reduction Factor for Long Inlets | RF _{Curb} = | 1.00 | 1.00 | |
| Grated Inlet Performance Reduction Factor for Long Inlets | RF _{Grate} = | N/A | N/A | |
| | _ | MINOR | MAJOR | |
| Total Inlet Interception Capacity (assumes clogged condition) | Q _a = | 5.4 | 5.4 | cfs |
| nlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK) | Q PEAK REQUIRED = | 1.0 | 2.0 | cfs |

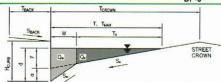
ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

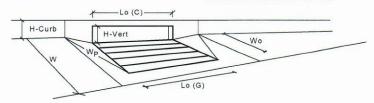
ELDORADO SPRINGS

DP-5

Project: Inlet ID:



| Gutter Geometry (Enter data in the blue cells) | | | | |
|--|-----------------------|-------------|-------------|--------------------|
| Maximum Allowable Width for Spread Behind Curb | TBACK = | 5.0 | ft | |
| Side Slope Behind Curb (leave blank for no conveyance credit behind curb) | S _{BACK} = | 0.020 | ft/ft | |
| Manning's Roughness Behind Curb (typically between 0.012 and 0.020) | n _{BACK} = | 0.020 | | |
| Height of Curb at Gutter Flow Line | H _{CURB} = | 6.00 | inches | |
| Distance from Curb Face to Street Crown | T _{CROWN} = | 24.0 | ft | |
| Gutter Width | W = | 2.00 | ft | |
| Street Transverse Slope | S _X = | 0.020 | ft/ft | |
| Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) | S _W = | 0.083 | ft/ft | |
| Street Longitudinal Slope - Enter 0 for sump condition | So= | 0.000 | ft/ft | |
| Manning's Roughness for Street Section (typically between 0.012 and 0.020) | n _{street} = | 0.012 | | |
| | | Minor Storm | Major Storm | |
| Max. Allowable Spread for Minor & Major Storm | T _{MAX} = | 24.0 | 24.0 | ft |
| Max. Allowable Depth at Gutter Flowline for Minor & Major Storm | d _{MAX} = | 6.0 | 6.0 | inches |
| Check boxes are not applicable in SUMP conditions | _ | Г | | ## (Fig. 2) States |
| MINOR STORM Allowable Capacity is based on Depth Criterion | | Minor Storm | Major Storm | |
| | Q _{allow} = | SUMP | SUMP | cfs |



| Design Information (Input) | | MINOR | MAJOR | |
|--|-----------------------------|-------------|--------------|-----------------|
| Type of Inlet CDOT Type R Curb Opening | Type = | CDOT Type R | Curb Opening | |
| Local Depression (additional to continuous gutter depression 'a' from above) | a _{local} = | 3.00 | 3 00 | inches |
| Number of Unit Inlets (Grate or Curb Opening) | No = | 1 | 1 | |
| Nater Depth at Flowline (outside of local depression) | Ponding Depth = | 6.0 | 6.0 | inches |
| Grate Information | | MINOR | MAJOR | Override Depths |
| Length of a Unit Grate | L _o (G) = | N/A | N/A | feet |
| Width of a Unit Grate | W _o = | N/A | N/A | feet |
| Area Opening Ratio for a Grate (typical values 0.15-0.90) | A _{ratio} = | N/A | N/A | |
| Clogging Factor for a Single Grate (typical value 0.50 - 0.70) | $C_{f}(G) =$ | N/A | N/A | |
| Grate Weir Coefficient (typical value 2.15 - 3.60) | C _w (G) = | N/A | N/A | |
| Grate Orifice Coefficient (typical value 0.60 - 0.80) | C _o (G) = | N/A | N/A | |
| Curb Opening Information | 12- | MINOR | MAJOR | |
| Length of a Unit Curb Opening | L _o (C) = | 5.00 | 5 00 | feet |
| Height of Vertical Curb Opening in Inches | H _{vert} = | 6.00 | 6.00 | inches |
| Height of Curb Orifice Throat in Inches | H _{throat} = | 6.00 | 6.00 | inches |
| Angle of Throat (see USDCM Figure ST-5) | Theta = | 63.40 | 63.40 | degrees |
| Side Width for Depression Pan (typically the gutter width of 2 feet) | W _p = | 2.00 | 2.00 | feet |
| Clogging Factor for a Single Curb Opening (typical value 0.10) | $C_f(C) =$ | 0.10 | 0.10 | |
| Curb Opening Weir Coefficient (typical value 2.3-3.7) | C _w (C) = | 3.60 | 3.60 | |
| Curb Opening Orifice Coefficient (typical value 0.60 - 0.70) | C _o (C) = | 0.67 | 0.67 | |
| ow Head Performance Reduction (Calculated) | | MINOR | MAJOR | |
| Depth for Grate Midwidth | d _{Grate} = | N/A | N/A | ft |
| Depth for Curb Opening Weir Equation | d _{Curb} = | 0.33 | 0.33 | ft |
| Combination Inlet Performance Reduction Factor for Long Inlets | RF _{Combination} = | 0.77 | 0.77 | |
| Curb Opening Performance Reduction Factor for Long Inlets | RF _{Curb} = | 1.00 | 1.00 | |
| Grated Inlet Performance Reduction Factor for Long Inlets | RF _{Grate} = | N/A | N/A | |
| | - | MINOR | MAJOR | _ |
| Total Inlet Interception Capacity (assumes clogged condition) | Q _a = | 5.4 | 5.4 | cfs |
| nlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK) | Q PEAK REQUIRED = | 1.0 | 2.0 | cfs |

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) ELDORADO SPRINGS Project: Inlet ID: DP-6 STREET Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb 10.0 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) SBACK : 0.020 ft/ft Manning's Roughness Behind Curb (typically between 0.012 and 0.020) 0.020 Height of Curb at Gutter Flow Line H_{CURB} : 6.00 inches Distance from Curb Face to Street Crown 26.0 Gutter Width W= 2.00 S_x = Street Transverse Slope ft/ft 0.020 Sw: Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) 0.083 ft/ft Street Longitudinal Slope - Enter 0 for sump condition So 0.030 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) 0.012 n_{STREET} = Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm T_{MAX} 26.0 26.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm

6.0

Minor Storm 23.7

8.0

Major Storm

50.4

inches

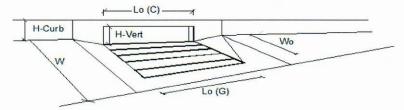
check = yes

Allow Flow Depth at Street Crown (leave blank for no)

MINOR STORM Allowable Capacity is based on Depth Criterion MAJOR STORM Allowable Capacity is based on Depth Criterion

Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management' Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

INLET ON A CONTINUOUS GRADE

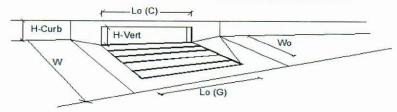


| Design Information (Input) | CODOT T B C C | 9 | MINOR | MAJOR | |
|--|---|-------------------------|-------------|--------------|--------|
| Type of Inlet | CDOT Type R Curb Opening | Type = | CDOT Type R | Curb Opening | |
| Local Depression (additional to o | ontinuous gutter depression 'a') | a _{LOCAL} = | 3.0 | 3.0 | inches |
| Total Number of Units in the Inle | t (Grate or Curb Opening) | No = | 1 | 1 | |
| Length of a Single Unit Inlet (Gra | te or Curb Opening) | L _o = | 15.00 | 15.00 | ft |
| Width of a Unit Grate (cannot be | greater than W, Gutter Width) | W _o = | N/A | N/A | ft |
| Clogging Factor for a Single Unit Grate (typical min. value = 0.5) | | CrG = | N/A | N/A | |
| Clogging Factor for a Single Uni | t Curb Opening (typical min. value = 0.1) | C _r -C = | 0.10 | 0.10 | |
| Street Hydraulics: OK - Q < All | owable Street Capacity' | | MINOR | MAJOR | |
| Total Inlet Interception Capaci | ty | Q= | 4.4 | 9.2 | cfs |
| Total Inlet Carry-Over Flow (flo | ow bypassing inlet) | Q _b = | 0.0 | 1.5 | cfs |
| Capture Percentage = Q ₃ /Q ₀ = | | C% = | 100 | 86 | % |

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) ELDORADO SPRINGS Project: Inlet ID: DP-8 STREET Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb TBACK 10.0 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) SBACK 0.020 ft/ft Manning's Roughness Behind Curb (typically between 0.012 and 0.020) 0.020 Height of Curb at Gutter Flow Line H_{CURB} 6.00 inches Distance from Curb Face to Street Crown TCROWN 26.0 Gutter Width W= 2.00 Street Transverse Slope Sx = 0.020 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) Sw = 0.083 ft/ft Street Longitudinal Slope - Enter 0 for sump condition So= 0.030 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) n_{STREET} = 0.012 Minor Storm Max. Allowable Spread for Minor & Major Storm 26.0 26.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm 6.0 inches Allow Flow Depth at Street Crown (leave blank for no) check = yes MINOR STORM Allowable Capacity is based on Depth Criterion Minor Storm Major Storm MAJOR STORM Allowable Capacity is based on Depth Criterion 23.7 50.4 Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

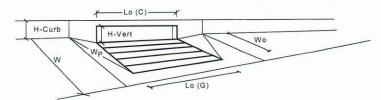
flajor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

INLET ON A CONTINUOUS GRADE



| Design Information (Input) | CDOT Type R Curb Opening | - | 100 | MINOR | MAJOR | |
|---|---|------------------|----------------------|-------------|--------------|--------|
| Type of Inlet | CDO1 Type R Curb Opening | | Type = | CDOT Type R | Curb Opening | |
| Local Depression (additional to c | ontinuous gutter depression 'a') | | a _{LOCAL} = | 3.0 | 3.0 | inches |
| Total Number of Units in the Inlet | (Grate or Curb Opening) | | No = | 1 | 1 | |
| Length of a Single Unit Inlet (Gra | te or Curb Opening) | | L _o = | 5.00 | 5,00 | ft |
| Width of a Unit Grate (cannot be greater than W, Gutter Width) Clogging Factor for a Single Unit Grate (typical min. value = 0.5) | | W _o = | N/A | N/A | ft | |
| | | | CrG = | N/A | N/A | 7 |
| Clogging Factor for a Single Unit | Curb Opening (typical min. value = 0.1) | | C _C C = | 0.10 | 0.10 | 7 |
| Street Hydraulics: OK - Q < Alle | owable Street Capacity' | | | MINOR | MAJOR | |
| Total Inlet Interception Capacit | у | | Q = | 0.5 | 1.2 | cfs |
| Total Inlet Carry-Over Flow (flo | w bypassing inlet) | | Q _b = | 0.0 | 0.1 | cfs |
| Capture Percentage = Q _a /Q _o = | | | C% = | 100 | 94 | % |

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) ELDORADO SPRINGS Project: Inlet ID: DP-10 STREET Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb 0.0 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) SBACK : 0.020 ft/ft Manning's Roughness Behind Curb (typically between 0.012 and 0.020) 0.020 Height of Curb at Gutter Flow Line H_{CURB} 6.00 Distance from Curb Face to Street Crown 24.0 Gutter Width W= 3.00 Street Transverse Slope S_X = 0.020 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) Sw: 0.083 ft/ft Street Longitudinal Slope - Enter 0 for sump condition So: 0.000 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) n_{STREET} 0.012 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm 24.0 24.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm 6.0 6.0 Check boxes are not applicable in SUMP conditions MINOR STORM Allowable Capacity is based on Depth Criterion MAJOR STORM Allowable Capacity is based on Depth Criterion Minor Storm Major Storm SUMP SUMP

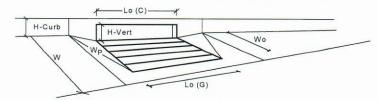


| Design Information (Input) | | MINOR | MAJOR | |
|--|-----------------------------|----------|-----------|-----------------|
| Type of Inlet CDOT Type C Grate | Type = | CDOT Typ | e C Grate | |
| Local Depression (additional to continuous gutter depression 'a' from above) | a _{local} = | 6.00 | 6.00 | inches |
| Number of Unit Inlets (Grate or Curb Opening) | No = | 1 | 1 | |
| Water Depth at Flowline (outside of local depression) | Ponding Depth = | 6.0 | 6.0 | inches |
| Grate Information | | MINOR | MAJOR | Override Depths |
| Length of a Unit Grate | L _o (G) = | 2.92 | 2.92 | feet |
| Width of a Unit Grate | W _o = | 2.92 | 2.92 | feet |
| Area Opening Ratio for a Grate (typical values 0.15-0.90) | A _{ratio} = | 0.70 | 0.70 | |
| Clogging Factor for a Single Grate (typical value 0.50 - 0.70) | C _f (G) = | 0.50 | 0.50 | |
| Grate Weir Coefficient (typical value 2.15 - 3.60) | C _w (G) = | 2.41 | 2.41 | |
| Grate Orifice Coefficient (typical value 0.60 - 0.80) | C _o (G) = | 0.67 | 0.67 | |
| Curb Opening Information | | MINOR | MAJOR | |
| Length of a Unit Curb Opening | L _o (C) = | N/A | N/A | feet |
| Height of Vertical Curb Opening in Inches | H _{vert} = | N/A | N/A | inches |
| Height of Curb Orifice Throat in Inches | H _{throat} = | N/A | N/A | inches |
| Angle of Throat (see USDCM Figure ST-5) | Theta = | N/A | N/A | degrees |
| Side Width for Depression Pan (typically the gutter width of 2 feet) | W _p = | N/A | N/A | feet |
| Clogging Factor for a Single Curb Opening (typical value 0.10) | $C_{f}(C) =$ | N/A | N/A | |
| Curb Opening Weir Coefficient (typical value 2.3-3.7) | C _w (C) = | N/A | N/A | |
| Curb Opening Orifice Coefficient (typical value 0.60 - 0.70) | C _o (C) = | N/A | N/A | |
| Low Head Performance Reduction (Calculated) | | MINOR | MAJOR | |
| Depth for Grate Midwidth | d _{Grate} = | 0.635 | 0.635 | ft |
| Depth for Curb Opening Weir Equation | d _{Curb} = | N/A | N/A | ft |
| Combination Inlet Performance Reduction Factor for Long Inlets | RF _{Combination} = | N/A | N/A | |
| Curb Opening Performance Reduction Factor for Long Inlets | RF _{Curb} = | N/A | N/A | |
| Grated Inlet Performance Reduction Factor for Long Inlets | RF _{Grate} = | 0.95 | 0.95 | |
| and the second s | | MINOR | MAJOR | _ |
| Total Inlet Interception Capacity (assumes clogged condition) | Q _a = | 4.2 | 4.2 | cfs |
| Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK) | Q PEAK REQUIRED = | 1.7 | 3.1 | cfs |

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) ELDORADO SPRINGS DP-11 Project: Inlet ID: STREET Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb 5.0 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) SBACK = 0.020 ft/ft Manning's Roughness Behind Curb (typically between 0.012 and 0.020) 0.020 Height of Curb at Gutter Flow Line 6.00 inches Distance from Curb Face to Street Crown TCROWN 24.0 Gutter Width W= 2.00 Street Transverse Slope Sx = 0.020 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) Sw 0.083 ft/ft Street Longitudinal Slope - Enter 0 for sump condition So 0.000 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) n_{STREET} = 0.012 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm 24.0 24.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm 6.0 6.0 Check boxes are not applicable in SUMP conditions MINOR STORM Allowable Capacity is based on Depth Criterion MAJOR STORM Allowable Capacity is based on Depth Criterion Minor Storm Major Storm

SUMP

SUMP



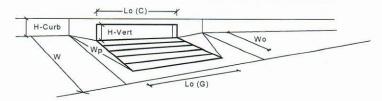
| Design Information (Input) | CDOT Type R Curb Opening ▼ | 95 | MINOR | MAJOR | |
|------------------------------------|--|-----------------------------|-------------|--------------|-----------------|
| Type of Inlet | CDOT Type R Curb Opening | Type = | CDOT Type R | Curb Opening | |
| Local Depression (additional to d | continuous gutter depression 'a' from above) | a _{local} = | 3.00 | 3.00 | inches |
| Number of Unit Inlets (Grate or 0 | Curb Opening) | No = | 1 | 1 | |
| Water Depth at Flowline (outside | of local depression) | Ponding Depth = | 6.0 | 6.0 | inches |
| Grate Information | | _ | MINOR | MAJOR | Override Depths |
| Length of a Unit Grate | | L _o (G) = | N/A | N/A | feet |
| Width of a Unit Grate | | W _o = | N/A | N/A | feet |
| Area Opening Ratio for a Grate (| typical values 0.15-0.90) | A _{ratio} = | N/A | N/A | |
| Clogging Factor for a Single Gra | te (typical value 0.50 - 0.70) | C _f (G) = | N/A | N/A | 1 |
| Grate Weir Coefficient (typical va | alue 2.15 - 3.60) | C _w (G) = | N/A | N/A | 7 |
| Grate Orifice Coefficient (typical | value 0.60 - 0.80) | C _o (G) = | N/A | N/A | 7 |
| Curb Opening Information | | | MINOR | MAJOR | _ |
| Length of a Unit Curb Opening | | L _o (C) = | 5.00 | 5 00 | feet |
| Height of Vertical Curb Opening | in Inches | H _{vert} = | 6.00 | 6.00 | inches |
| Height of Curb Orifice Throat in I | nches | H _{throat} = | 6.00 | 6.00 | inches |
| Angle of Throat (see USDCM Fig | gure ST-5) | Theta = | 63.40 | 63.40 | degrees |
| Side Width for Depression Pan (| typically the gutter width of 2 feet) | W _p = | 2.00 | 2.00 | feet |
| Clogging Factor for a Single Cur | b Opening (typical value 0.10) | $C_{f}(C) =$ | 0.10 | 0.10 | |
| Curb Opening Weir Coefficient (| typical value 2.3-3.7) | C _w (C) = | 3.60 | 3.60 | |
| Curb Opening Orifice Coefficient | (typical value 0.60 - 0.70) | C _o (C) = | 0.67 | 0.67 | |
| Low Head Performance Reduc | tion (Calculated) | | MINOR | MAJOR | |
| Depth for Grate Midwidth | | d _{Grate} = | N/A | N/A | ft |
| Depth for Curb Opening Weir Ed | uation | d _{Curb} = | 0.33 | 0.33 | ft |
| Combination Inlet Performance F | Reduction Factor for Long Inlets | RF _{Combination} = | 0.77 | 0.77 | |
| Curb Opening Performance Red | | RF _{Curb} = | 1.00 | 1.00 | |
| Grated Inlet Performance Reduc | tion Factor for Long Inlets | RF _{Grate} = | N/A | N/A | |
| | | _ | MINOR | MAJOR | |
| Total Inlet Interception C | apacity (assumes clogged condition) | Q _a = | 5.4 | 5.4 | cfs |
| nlet Capacity IS GOOD for Mir | or and Major Storms(>Q PEAK) | Q PEAK REQUIRED = | 1.0 | 3.0 | cfs |

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) ELDORADO SPRINGS Project: Inlet ID: DP-12 STREET Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb 0.0 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) 0.020 ft/ft Manning's Roughness Behind Curb (typically between 0.012 and 0.020) H_{CURB} Height of Curb at Gutter Flow Line 6.00 Distance from Curb Face to Street Crown 24.0 Gutter Width W Street Transverse Slope S_X = 0.020 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) Sw 0.083 ft/ft Street Longitudinal Slope - Enter 0 for sump condition 0.000 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) n_{STREET} = 0.012 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm 24.0 24.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm 6.0 6.0 Check boxes are not applicable in SUMP conditions MINOR STORM Allowable Capacity is based on Depth Criterion Major Storm Minor Storm

SUMP

SUMP

MAJOR STORM Allowable Capacity is based on Depth Criterion



| Design Information (Input) | and the same of th | MINOR | MAJOR | |
|---|--|---------|------------|-----------------|
| ype of Inlet | Type = | CDOT Ty | pe C Grate | |
| ocal Depression (additional to continuous gutter depression 'a' from above) | a _{local} = | 6.00 | 6.00 | inches |
| lumber of Unit Inlets (Grate or Curb Opening) | No = | 1 | 1 | |
| Vater Depth at Flowline (outside of local depression) | Ponding Depth = | 6.0 | 6.0 | inches |
| Grate Information | A 1000 | MINOR | MAJOR | Override Depths |
| ength of a Unit Grate | L ₀ (G) = | 2.92 | 2.92 | feet |
| Vidth of a Unit Grate | W _o = | 2.92 | 2,92 | feet |
| krea Opening Ratio for a Grate (typical values 0.15-0.90) | A _{ratio} = | 0.70 | 0.70 | |
| Clogging Factor for a Single Grate (typical value 0.50 - 0.70) | $C_f(G) =$ | 0.50 | 0.50 | |
| Grate Weir Coefficient (typical value 2.15 - 3.60) | C _w (G) = | 2.41 | 2.41 | |
| Grate Orifice Coefficient (typical value 0.60 - 0.80) | C _o (G) = | 0.67 | 0.67 | |
| Curb Opening Information | | MINOR | MAJOR | |
| ength of a Unit Curb Opening | L _o (C) = | N/A | N/A | feet |
| leight of Vertical Curb Opening in Inches | H _{vert} = | N/A | N/A | inches |
| leight of Curb Orifice Throat in Inches | H _{throat} = | N/A | N/A | inches |
| Angle of Throat (see USDCM Figure ST-5) | Theta = | N/A | N/A | degrees |
| Side Width for Depression Pan (typically the gutter width of 2 feet) | W _p = | N/A | N/A | feet |
| Clogging Factor for a Single Curb Opening (typical value 0.10) | $C_f(C) =$ | N/A | N/A | |
| Curb Opening Weir Coefficient (typical value 2.3-3.7) | C _w (C) = | N/A | N/A | |
| Curb Opening Orifice Coefficient (typical value 0.60 - 0.70) | C _o (C) = | N/A | N/A | |
| ow Head Performance Reduction (Calculated) | | MINOR | MAJOR | |
| Pepth for Grate Midwidth | d _{Grate} = | 0.635 | 0.635 | T ft |
| lepth for Curb Opening Weir Equation | d _{Curb} = | N/A | N/A | ft |
| combination Inlet Performance Reduction Factor for Long Inlets | RF _{Combination} = | N/A | N/A | |
| urb Opening Performance Reduction Factor for Long Inlets | RF _{Curb} = | N/A | N/A | |
| erated inlet Performance Reduction Factor for Long Inlets | RF _{Grate} = | 0.95 | 0.95 | |
| | 19 | MINOR | MAJOR | |
| otal Inlet Interception Capacity (assumes clogged condition) | Q _a = | 4.2 | 4.2 | cfs |
| nlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK) | Q PEAK REQUIRED = | 1.7 | 3.0 | cfs |

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) ELDORADO SPRINGS Project: Inlet ID: DP-13 STREET Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb TBACK 5.0 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) SBACK 0.020 ft/ft Manning's Roughness Behind Curb (typically between 0.012 and 0.020) 0.020 Height of Curb at Gutter Flow Line H_{CURB} : 6.00 inches Distance from Curb Face to Street Crown 24.0 Gutter Width W: 2.00 Street Transverse Slope S_X = 0.020 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) Sw = 0.083 ft/ft Street Longitudinal Slope - Enter 0 for sump condition So= 0.000 Manning's Roughness for Street Section (typically between 0.012 and 0.020) n_{STREET} = 0.012 Major Storm Max. Allowable Spread for Minor & Major Storm 24.0 24.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm 6.0 Check boxes are not applicable in SUMP conditions

Minor Storm

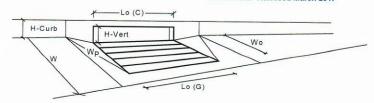
SUMP

Major Storm

SUMP

MINOR STORM Allowable Capacity is based on Depth Criterion

MAJOR STORM Allowable Capacity is based on Depth Criterion

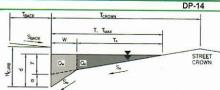


| Design Information (Input) Type of Inlet CDOT Type R Curb Opening | | MINOR | MAJOR | |
|--|-----------------------------|-------------|--------------|-----------------|
| Type of fillet | Type = | CDOT Type R | Curb Opening | - |
| Local Depression (additional to continuous gutter depression 'a' from above) | a _{local} = | 3.00 | 3.00 | inches |
| Number of Unit Inlets (Grate or Curb Opening) | No = | 1 | 1 | - Contract |
| Water Depth at Flowline (outside of local depression) | Ponding Depth = | 6.0 | 7.3 | inches |
| Grate Information | _ | MINOR | MAJOR | Override Depths |
| Length of a Unit Grate | L _o (G) = | N/A | N/A | feet |
| Width of a Unit Grate | W _o = | N/A | N/A | feet |
| Area Opening Ratio for a Grate (typical values 0.15-0.90) | A _{ratio} = | N/A | N/A | |
| Clogging Factor for a Single Grate (typical value 0.50 - 0.70) | C _f (G) = | N/A | N/A | 1 |
| Grate Weir Coefficient (typical value 2.15 - 3.60) | C _w (G) = | N/A | N/A | - |
| Grate Orifice Coefficient (typical value 0.60 - 0.80) | C _o (G) = | N/A | N/A | - |
| Curb Opening Information | | MINOR | MAJOR | _ |
| Length of a Unit Curb Opening | L _o (C) = | 20.00 | 20.00 | feet |
| Height of Vertical Curb Opening in Inches | H _{vert} = | 6.00 | 6.00 | inches |
| Height of Curb Orifice Throat in Inches | H _{throat} = | 6.00 | 6.00 | inches |
| Angle of Throat (see USDCM Figure ST-5) | Theta = | 63.40 | 63.40 | degrees |
| Side Width for Depression Pan (typically the gutter width of 2 feet) | W _p = | 2.00 | 2 00 | feet |
| Clogging Factor for a Single Curb Opening (typical value 0.10) | $C_f(C) =$ | 0.10 | 0.10 | - |
| Curb Opening Weir Coefficient (typical value 2.3-3.7) | C _w (C) = | 3.60 | 3,60 | |
| Curb Opening Orifice Coefficient (typical value 0.60 - 0.70) | C _o (C) = | 0.67 | 0,67 | |
| _ow Head Performance Reduction (Calculated) | | MINOR | MAJOR | |
| Depth for Grate Midwidth | d _{Grate} = | N/A | N/A | T ft |
| Depth for Curb Opening Weir Equation | d _{Curb} = | 0.33 | 0.44 | ft |
| Combination Inlet Performance Reduction Factor for Long Inlets | RF _{Combination} = | 0.57 | 0.69 | 1 |
| Curb Opening Performance Reduction Factor for Long Inlets | RF _{Curb} = | 0.79 | 0.86 | |
| Grated Inlet Performance Reduction Factor for Long Inlets | RF _{Grate} = | N/A | N/A |] |
| | _ | MINOR | MAJOR | _ |
| Total Inlet Interception Capacity (assumes clogged condition) | Q _a = | 12.5 | 20.6 | cfs |
| nlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK) | Q PEAK REQUIRED = | 10.0 | 20.0 | cfs |

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) ELDORADO SPRINGS

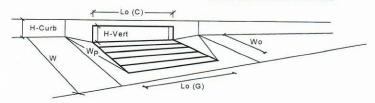
Project: Inlet ID:



Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb TBACK = 0.0 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) SBACK = 0.020 ft/ft Manning's Roughness Behind Curb (typically between 0.012 and 0.020) n_{BACK} : 0.020 Height of Curb at Gutter Flow Line 6.00 Distance from Curb Face to Street Crown 24.0 Gutter Width W= 2.00 Street Transverse Slope S_X = 0.020 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) Sw = 0.083 ft/ft Street Longitudinal Slope - Enter 0 for sump condition So= 0.000 Manning's Roughness for Street Section (typically between 0.012 and 0.020) 0.012 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm 24.0 24.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm 6.0 Check boxes are not applicable in SUMP conditions MINOR STORM Allowable Capacity is based on Depth Criterion

SUMP

SUMP

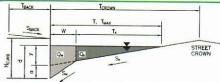


| Design Information (Input) CDOT Type R Curb Opening | 7 | MINOR | MAJOR | |
|---|-----------------------------|-------------|--------------|-----------------|
| ype of inlet | Type = | CDOT Type F | Curb Opening | |
| ocal Depression (additional to continuous gutter depression 'a' from above) | a _{local} = | 3.00 | 3.00 | inches |
| Number of Unit Inlets (Grate or Curb Opening) | No = | 1 | 1 | |
| Water Depth at Flowline (outside of local depression) | Ponding Depth = | 6.0 | 6.0 | inches |
| Grate Information | PORC LA CHARACTE A | MINOR | MAJOR | Override Depths |
| Length of a Unit Grate | L _o (G) = | N/A | N/A | feet |
| Width of a Unit Grate | W _o = | N/A | N/A | feet |
| Area Opening Ratio for a Grate (typical values 0.15-0.90) | A _{ratio} = | N/A | N/A | |
| Clogging Factor for a Single Grate (typical value 0.50 - 0.70) | $C_f(G) =$ | N/A | N/A | |
| Grate Weir Coefficient (typical value 2.15 - 3.60) | C _w (G) = | N/A | N/A | 7 |
| Grate Orifice Coefficient (typical value 0.60 - 0.80) | C _o (G) = | N/A | N/A | 7 |
| Curb Opening Information | _ | MINOR | MAJOR | |
| Length of a Unit Curb Opening | L _o (C) = | 5.00 | 5.00 | feet |
| Height of Vertical Curb Opening in Inches | H _{vert} = | 6.00 | 6.00 | inches |
| Height of Curb Orifice Throat in Inches | H _{throat} = | 6.00 | 6.00 | inches |
| Angle of Throat (see USDCM Figure ST-5) | Theta = | 63.40 | 63.40 | degrees |
| Side Width for Depression Pan (typically the gutter width of 2 feet) | W _p = | 2.00 | 2.00 | feet |
| Clogging Factor for a Single Curb Opening (typical value 0.10) | $C_{t}(C) =$ | 0.10 | 0.10 | |
| Curb Opening Weir Coefficient (typical value 2.3-3.7) | C _w (C) = | 3.60 | 3.60 | |
| Curb Opening Orifice Coefficient (typical value 0.60 - 0.70) | C _o (C) = | 0.67 | 0.67 | |
| ow Head Performance Reduction (Calculated) | | MINOR | MAJOR | |
| Depth for Grate Midwidth | d _{Grate} = | N/A | N/A | T ft |
| Depth for Curb Opening Weir Equation | d _{Curb} = | 0.33 | 0.33 | ft |
| Combination Inlet Performance Reduction Factor for Long Inlets | RF _{Combination} = | 0.77 | 0.77 | |
| Curb Opening Performance Reduction Factor for Long Inlets | RF _{Curb} = | 1.00 | 1.00 | |
| Grated Inlet Performance Reduction Factor for Long Inlets | RF _{Grate} = | N/A | N/A | |
| | _ | MINOR | MAJOR | |
| Total Inlet Interception Capacity (assumes clogged condition) | $Q_a =$ | 5.4 | 5.4 | cfs |
| nlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK) | Q PEAK REQUIRED = | 1.5 | 3.0 | cfs |

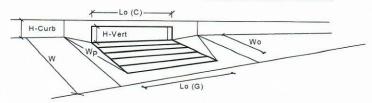
ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)
ELDORADO SPRINGS

Project: Inlet ID:



Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb 0.0 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) 0.020 ft/ft Manning's Roughness Behind Curb (typically between 0.012 and 0.020) n_{BACK} 0.020 Height of Curb at Gutter Flow Line H_{CURB} 6.00 Distance from Curb Face to Street Crown 24.0 Gutter Width W= 3.00 Street Transverse Slope S_X = 0.020 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) Sw = 0.083 ft/ft Street Longitudinal Slope - Enter 0 for sump condition So 0.000 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) n_{STREET} = 0.012 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm 24.0 24.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm 6.0 6.0 Check boxes are not applicable in SUMP conditions MINOR STORM Allowable Capacity is based on Depth Criterion MAJOR STORM Allowable Capacity is based on Depth Criterion Minor Storm Major Storm SUMP



| Design Information (Input) CDOT Type C Grate ▼ | | MINOR | MAJOR | -10 |
|--|-----------------------------|---------|------------|-----------------|
| Type of Inlet | Type = | CDOT Ty | pe C Grate | |
| Local Depression (additional to continuous gutter depression 'a' from above) | a _{local} = | 6.00 | 6.00 | inches |
| Number of Unit Inlets (Grate or Curb Opening) | No = | 1 | 1 | |
| Water Depth at Flowline (outside of local depression) | Ponding Depth = | 6.0 | 6.0 | inches |
| Grate Information | | MINOR | MAJOR | Override Depths |
| Length of a Unit Grate | L _o (G) = | 2.92 | 2,92 | feet |
| Width of a Unit Grate | W _o = | 2.92 | 2.92 | feet |
| Area Opening Ratio for a Grate (typical values 0.15-0.90) | A _{ratio} = | 0.70 | 0.70 | |
| Clogging Factor for a Single Grate (typical value 0.50 - 0.70) | $C_f(G) =$ | 0.50 | 0.50 | |
| Grate Weir Coefficient (typical value 2.15 - 3.60) | C _w (G) = | 2.41 | 2.41 | |
| Grate Orifice Coefficient (typical value 0.60 - 0.80) | C _o (G) = | 0.67 | 0.67 | - |
| Curb Opening Information | | MINOR | MAJOR | |
| Length of a Unit Curb Opening | L ₀ (C) = | N/A | N/A | feet |
| Height of Vertical Curb Opening in Inches | H _{vert} = | N/A | N/A | inches |
| Height of Curb Orifice Throat in Inches | H _{throat} = | N/A | N/A | inches |
| Angle of Throat (see USDCM Figure ST-5) | Theta = | N/A | N/A | degrees |
| Side Width for Depression Pan (typically the gutter width of 2 feet) | W _p = | N/A | N/A | feet |
| Clogging Factor for a Single Curb Opening (typical value 0.10) | $C_{f}(C) =$ | N/A | N/A | |
| Curb Opening Weir Coefficient (typical value 2.3-3.7) | C _w (C) = | N/A | N/A | |
| Curb Opening Orifice Coefficient (typical value 0.60 - 0.70) | C _o (C) = | N/A | N/A | |
| Low Head Performance Reduction (Calculated) | | MINOR | MAJOR | |
| Depth for Grate Midwidth | d _{Grate} = | 0.635 | 0.635 | 7ft |
| Depth for Curb Opening Weir Equation | d _{Curb} = | N/A | N/A | ft |
| Combination Inlet Performance Reduction Factor for Long Inlets | RF _{Combination} = | N/A | N/A | |
| Curb Opening Performance Reduction Factor for Long Inlets | RF _{Curb} = | N/A | N/A | |
| Grated Inlet Performance Reduction Factor for Long Inlets | RF _{Grate} = | 0.95 | 0.95 | |
| | | MINOR | MAJOR | |
| Total Inlet Interception Capacity (assumes clogged condition) | Q _a = | 4.2 | 4.2 | cfs |
| nlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK) | Q PEAK REQUIRED = | 1.5 | 4.0 | cfs |

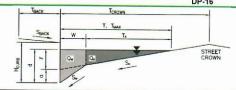
ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

ELDORADO SPRINGS

DP-16

Project: Inlet ID:

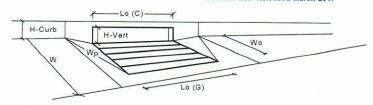


Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb TBACK = 0.0 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) 0.020 ft/ft Manning's Roughness Behind Curb (typically between 0.012 and 0.020) 0.020 Height of Curb at Gutter Flow Line H_{CURB} : 6.00 inches Distance from Curb Face to Street Crown TCROWN 24.0 Gutter Width W= 3.00 Street Transverse Slope Sx = 0.020 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) Sw

| Street Longitudinal Slope - Enter 0 for sump condition Manning's Roughness for Street Section (typically between 0.012 and 0.020) | S _O = | 0.000 | ft/ft |
|--|------------------|-------------|---------|
| | V- | Minor Storm | Maior S |
| Max. Allowable Spread for Minor & Major Storm | Turn = | 24.0 | O.4 |

| to bell to | Minor Storm | Major Storm | |
|--------------------|-------------|-------------------------|------------------------------|
| T _{MAX} = | 24.0 | 24.0 | ft |
| d _{MAX} = | 6.0 | 6.0 | inches |
| | F | Г | |
| | | T _{MAX} = 24.0 | T _{MAX} = 24.0 24.0 |

| MINOR STORM Allowable Capacity is based on Depth Criterion | _ | Minor Storm | Major Storm | |
|--|----------------------|-------------|-------------|-----|
| MAJOR STORM Allowable Capacity is based on Depth Criterion | Q _{allow} = | SUMP | SUMP | cfs |



| Design Information (Input) CDOT Type R Curb Opening ▼ | | MINOR | MAJOR | |
|---|-----------------------------|-------------|--------------|-----------------|
| ype of inlet | Type = | CDOT Type R | Curb Opening | |
| ocal Depression (additional to continuous gutter depression 'a' from above) | a _{local} = | 3.00 | 3.00 | inches |
| Number of Unit Inlets (Grate or Curb Opening) | No = | 1 | 1 | |
| Water Depth at Flowline (outside of local depression) | Ponding Depth = | 6.0 | 6.0 | inches |
| Grate Information | | MINOR | MAJOR | Override Depths |
| ength of a Unit Grate | L _o (G) = | N/A | N/A | feet |
| Nidth of a Unit Grate | W _o = | N/A | N/A | feet |
| Area Opening Ratio for a Grate (typical values 0.15-0.90) | A _{ratio} = | N/A | N/A | |
| Clogging Factor for a Single Grate (typical value 0.50 - 0.70) | C _f (G) = | N/A | N/A | 1 |
| Grate Weir Coefficient (typical value 2.15 - 3.60) | C _w (G) = | N/A | N/A | - |
| Grate Orifice Coefficient (typical value 0.60 - 0.80) | C _o (G) = | N/A | N/A | |
| Curb Opening Information | | MINOR | MAJOR | _ |
| ength of a Unit Curb Opening | L _o (C) = | 10.00 | 10.00 | feet |
| Height of Vertical Curb Opening in Inches | H _{vert} = | 6.00 | 6.00 | inches |
| Height of Curb Orifice Throat in Inches | H _{throat} = | 6.00 | 6.00 | inches |
| Angle of Throat (see USDCM Figure ST-5) | Theta = | 63.40 | 63.40 | degrees |
| Side Width for Depression Pan (typically the gutter width of 2 feet) | W _p = | 3.00 | 3.00 | feet |
| Clogging Factor for a Single Curb Opening (typical value 0.10) | $C_f(C) =$ | 0.10 | 0.10 | |
| Curb Opening Weir Coefficient (typical value 2.3-3.7) | C _w (C) = | 3.60 | 3.60 | |
| Curb Opening Orifice Coefficient (typical value 0.60 - 0.70) | C _o (C) = | 0.67 | 0.67 | |
| ow Head Performance Reduction (Calculated) | | MINOR | MAJOR | |
| Depth for Grate Midwidth | d _{Grate} = | N/A | N/A | T ft |
| Pepth for Curb Opening Weir Equation | d _{Curb} = | 0.25 | 0.25 | ft |
| Combination Inlet Performance Reduction Factor for Long Inlets | RF _{Combination} = | 0.57 | 0.57 | 1 |
| Curb Opening Performance Reduction Factor for Long Inlets | RF _{Curb} = | 0.93 | 0.93 | 1 |
| Grated Inlet Performance Reduction Factor for Long Inlets | RF _{Grate} = | N/A | N/A | |
| | | MINOR | MAJOR | |
| otal Inlet Interception Capacity (assumes clogged condition) | Q _a = | 6.1 | 6.1 | cfs |
| VARNING: Inlet Capacity less than Q Peak for Major Storm | Q PEAK REQUIRED = | 5.6 | 11.0 | cfs |

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) ELDORADO SPRINGS Project: Inlet ID: DP-17 STREET Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb TBACK = 5.0 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) SBACK 0.020 ft/ft Manning's Roughness Behind Curb (typically between 0.012 and 0.020) 0.020 Height of Curb at Gutter Flow Line H_{CURB} = 6.00 Distance from Curb Face to Street Crown T_{CROWN} 12.0 Gutter Width W= 2.00 Street Transverse Slope S_X = 0.020 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) S_W = 0.083 ft/ft Street Longitudinal Slope - Enter 0 for sump condition So = 0.040 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) n_{STREET} = 0.012 Major Storm Max. Allowable Spread for Minor & Major Storm 12.0 12.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm Allow Flow Depth at Street Crown (leave blank for no) check = yes MINOR STORM Allowable Capacity is based on Spread Criterion Minor Storn Major Storm

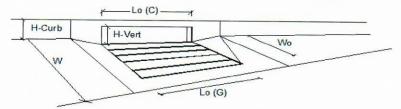
12.6

12.6

MAJOR STORM Allowable Capacity is based on Spread Criterion

Minor storm max, allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management' Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

INLET ON A CONTINUOUS GRADE Version 4.05 Released March 2017



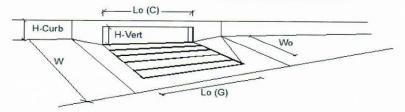
| Design Information (Input) | CDOT Type R Curb Opening | -1 | | MINOR | MAJOR | |
|---|---|-------------------------------------|----------------------|-------------|--------------|--------|
| Type of Inlet | Obot Type it dails opening | | Type = | CDOT Type R | Curb Opening | |
| Local Depression (additional to c | ontinuous gutter depression 'a') | | a _{LOCAL} = | 3.0 | 3.0 | inches |
| Total Number of Units in the Inlet | (Grate or Curb Opening) | | No = | 1 | 1 | |
| Length of a Single Unit Inlet (Gra | te or Curb Opening) | | L _o = | 10.00 | 10.00 | ft |
| Width of a Unit Grate (cannot be greater than W, Gutter Width) Clogging Factor for a Single Unit Grate (typical min. value = 0.5) | | W _o = C _r G = | N/A N/A | N/A | ft | |
| | | | | N/A | | |
| Clogging Factor for a Single Unit | Curb Opening (typical min. value = 0.1) | | CrC = | 0.10 | 0.10 | |
| Street Hydraulics: OK - Q < Alle | wable Street Capacity' | | | MINOR | MAJOR | |
| Total Inlet Interception Capacit | y | | Q = | 2.0 | 3.9 | cfs |
| Total Inlet Carry-Over Flow (flo | w bypassing inlet) | | Q _b = | 0.0 | 0.1 | cfs |
| Capture Percentage = Q _a /Q _o = | | | C% = | 100 | 96 | % |

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) Project: **ELDORADO SPRINGS** Inlet ID: DP-18 STREET Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb TBACK = 5.0 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) SBACK = 0.020 ft/ft Manning's Roughness Behind Curb (typically between 0.012 and 0.020) n_{BACK} 0.020 Height of Curb at Gutter Flow Line Distance from Curb Face to Street Crown H_{CURB} = 6.00 inches TCROWN 12.0 Gutter Width W= 2.00 Street Transverse Slope S_X = 0.020 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) S_W = 0.083 ft/ft Street Longitudinal Slope - Enter 0 for sump condition So 0.040 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) 0.012 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm 12.0 12.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm 6.0 6.0 inches Allow Flow Depth at Street Crown (leave blank for no) check = ves MINOR STORM Allowable Capacity is based on Spread Criterion MAJOR STORM Allowable Capacity is based on Spread Criterion Minor Storm Major Storm

Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management' 12.6

12.6

INLET ON A CONTINUOUS GRADE



| Design Information (Input) | CDOT Type R Curb Opening | | | MINOR | MAJOR | |
|--|---|------------------|----------------------|-------------|--------------|--------|
| Type of Inlet | 1 ODOT Type it Guib Opening | | Type = | CDOT Type R | Curb Opening | |
| Local Depression (additional to co | ontinuous gutter depression 'a') | | a _{LOCAL} = | 3.0 | 3.0 | inches |
| Total Number of Units in the Inlet (Grate or Curb Opening) Length of a Single Unit Inlet (Grate or Curb Opening) Width of a Unit Grate (cannot be greater than W, Gutter Width) Clogging Factor for a Single Unit Grate (typical min. value = 0.5) | | | No = | 1 | 1 | 1 |
| | | L _o = | 5.00 N/A | 5.00 | ft | |
| | | | | N/A | ft | |
| | | | CrG = | N/A | N/A | |
| Clogging Factor for a Single Unit | Curb Opening (typical min. value = 0.1) | | C _C C = | 0.10 | 0.10 | |
| Street Hydraulics: OK - Q < Allo | wable Street Capacity' | | | MINOR | MAJOR | |
| Total Inlet Interception Capacity | / | | Q= | 0.7 | 1.2 | cfs |
| Total Inlet Carry-Over Flow (flo | w bypassing inlet) | | Q _b = | 0.0 | 0.1 | cfs |
| Capture Percentage = Q _a /Q _o = | | | C% = | 100 | 94 | % |

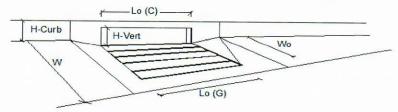
ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) ELDORADO SPRINGS Project: Inlet ID: STREET Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb 10.0 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) 0.020 ft/ft Manning's Roughness Behind Curb (typically between 0.012 and 0.020) 0.020 Height of Curb at Gutter Flow Line H_{CURB} 6.00 Distance from Curb Face to Street Crown 34.0 Gutter Width W= 2.00 Street Transverse Slope S_X = 0.020 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) S_W = 0.083 ft/ft Street Longitudinal Slope - Enter 0 for sump condition So 0.015 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) n_{STREET} = 0.012 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm TMAX 22.0 34.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm 6.0 8.0 inches Allow Flow Depth at Street Crown (leave blank for no) check = yes MINOR STORM Allowable Capacity is based on Depth Criterion Minor Storm Major Storm

22.5

MAJOR STORM Allowable Capacity is based on Depth Criterion

WARNING: MINOR STORM max. allowable capacity is less than the design flow given on sheet 'Inlet Management' Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

INLET ON A CONTINUOUS GRADE Version 4.05 Released March 2017



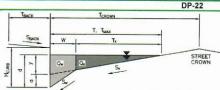
| Design Information (Input) | CDOT Type R Curb Opening | -1 | | MINOR | MAJOR | |
|---|---|----|----------------------|-------------|--------------|--------|
| Type of Inlet | | | Type = | CDOT Type R | Curb Opening | |
| Local Depression (additional to co | ontinuous gutter depression 'a') | | a _{LOCAL} = | 3.0 | 3.0 | inches |
| Total Number of Units in the Inlet | (Grate or Curb Opening) | | No = | 2 | 2 | |
| Length of a Single Unit Inlet (Gra | e or Curb Opening) | | L _o = | 20.00 | 20 00 | ft |
| Width of a Unit Grate (cannot be | greater than W, Gutter Width) | | W _o = | N/A | N/A | ft |
| Clogging Factor for a Single Unit | Grate (typical min. value = 0.5) | | CrG = | N/A | N/A | |
| Clogging Factor for a Single Unit | Curb Opening (typical min. value = 0.1) | | CrC = | 0.10 | 0.10 | 7 |
| Street Hydraulics: WARNING: 0 | > ALLOWABLE Q FOR MINOR STORM | | | MINOR | MAJOR | |
| Total Inlet Interception Capacit | / | | Q= | 28.8 | 46.9 | cfs |
| Total Inlet Carry-Over Flow (flo | w bypassing inlet) | | Q _b = | 0.2 | 12.1 | cfs |
| Capture Percentage = Q _a /Q _o = | | | C% = | 99 | 79 | % |

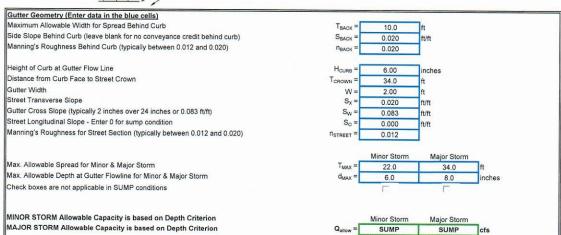
Version 4.05 Released March 2017

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) ELDORADO SPRINGS

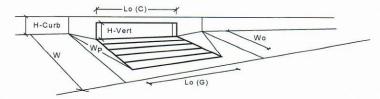
Project Inlet ID:





INLET IN A SUMP OR SAG LOCATION

Version 4.05 Released March 2017



| Design Information (Input) CDOT Type R Curb Opening | | MINOR | MAJOR | |
|--|-----------------------------|-------------|--------------|-------------------|
| Type of Inlet | Type = | CDOT Type R | Curb Opening | |
| Local Depression (additional to continuous gutter depression 'a' from above) | a _{local} = | 3.00 | 3.00 | inches |
| Number of Unit Inlets (Grate or Curb Opening) | No = | 1 | 1 | |
| Water Depth at Flowline (outside of local depression) | Ponding Depth = | 6.0 | 8.2 | inches |
| Grate Information | | MINOR | MAJOR | ✓ Override Depths |
| Length of a Unit Grate | L _o (G) = | N/A | N/A | feet |
| Width of a Unit Grate | W _o = | N/A | N/A | feet |
| Area Opening Ratio for a Grate (typical values 0.15-0.90) | A _{ratio} = | N/A | N/A | |
| Clogging Factor for a Single Grate (typical value 0.50 - 0.70) | C _f (G) = | N/A | N/A | |
| Grate Weir Coefficient (typical value 2.15 - 3.60) | C _w (G) = | N/A | N/A | |
| Grate Orifice Coefficient (typical value 0.60 - 0.80) | C _o (G) = | N/A | N/A | 7 |
| Curb Opening Information | _ | MINOR | MAJOR | _ |
| Length of a Unit Curb Opening | L _o (C) = | 15.00 | 15.00 | feet |
| Height of Vertical Curb Opening in Inches | H _{vert} = | 6.00 | 6.00 | inches |
| Height of Curb Orifice Throat in Inches | H _{throat} = | 6.00 | 6.00 | inches |
| Angle of Throat (see USDCM Figure ST-5) | Theta = | 63.40 | 63.40 | degrees |
| Side Width for Depression Pan (typically the gutter width of 2 feet) | W _p = | 2.00 | 2.00 | feet |
| Clogging Factor for a Single Curb Opening (typical value 0.10) | $C_{f}(C) =$ | 0.10 | 0.10 | |
| Curb Opening Weir Coefficient (typical value 2.3-3.7) | C _w (C) = | 3.60 | 3,60 | |
| Curb Opening Orifice Coefficient (typical value 0.60 - 0.70) | C _o (C) = | 0.67 | 0.67 | _ |
| Low Head Performance Reduction (Calculated) | | MINOR | MAJOR | |
| Depth for Grate Midwidth | d _{Grate} = | N/A | N/A | Tft. |
| Depth for Curb Opening Weir Equation | d _{Curb} = | 0.33 | 0.52 | ft |
| Combination Inlet Performance Reduction Factor for Long Inlets | RF _{Combination} = | 0.57 | 0.77 | |
| Curb Opening Performance Reduction Factor for Long Inlets | RF _{Curb} = | 0.79 | 0.90 | |
| Grated Inlet Performance Reduction Factor for Long Inlets | RF _{Grate} = | N/A | N/A | |
| | _ | MINOR | MAJOR | |
| Total Inlet Interception Capacity (assumes clogged condition) | Q _a = | 9.7 | 21.5 | cfs |
| nlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK) | Q PEAK REQUIRED = | 1.0 | 14.0 | cfs |

AREA INLET IN A SWALE

ELDORADO SPRINGS

DP-25

T_{MAX}
T
d
MAX
d
MAX

This worksheet uses the NRCS vegetal retardance method to determine Manning's n.

For more information see Section 7.2.3 of the USDCM.

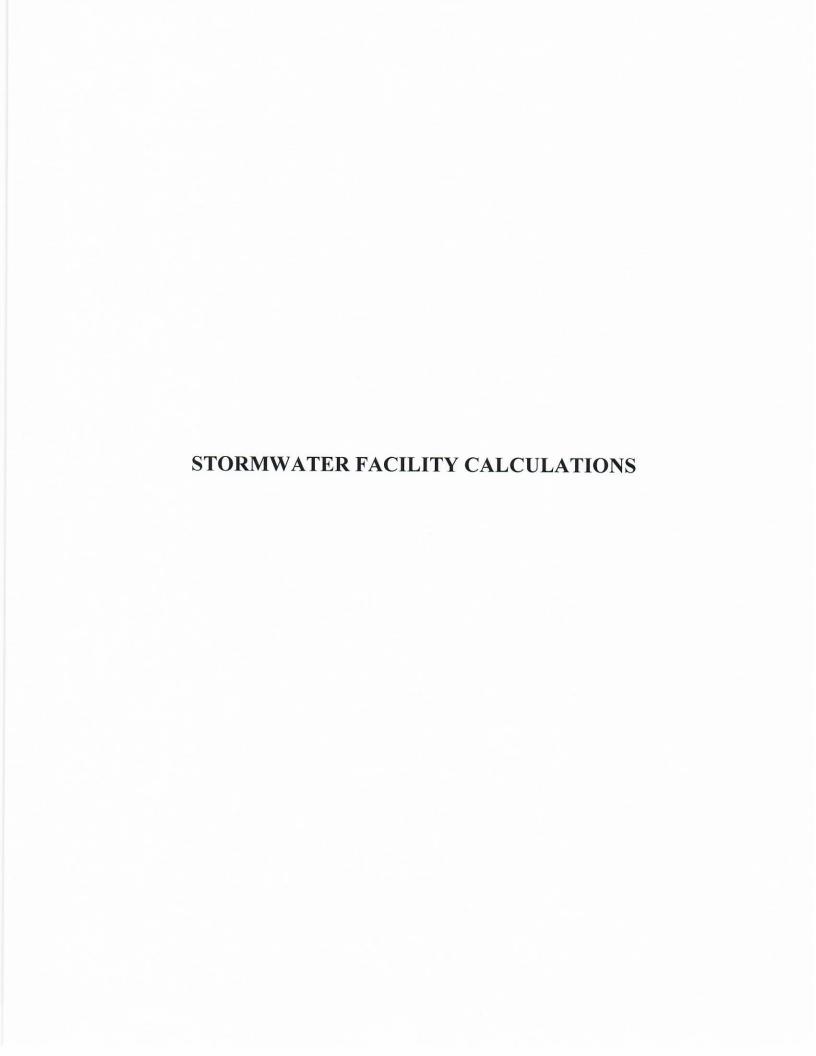
Analysis of Trapezoidal Grass-Lined Channel Using SCS Method NRCS Vegetal Retardance (A, B, C, D, or E) A, B, C, D or E Manning's n (Leave cell D16 blank to manually enter an n value) 0.022 n= Channel Invert Slope So = 0.0100 ft/ft Bottom Width B = 0.00 Left Side Slope Z1 = 3.00 ft/ft Right Side Slope Z2 = 3.00 ft/ft Check one of the following soil types: Choose One:

Non-Cohesive Soil Type: Max. Velocity (V_{MAX}) Max Froude No. (F_{MAX}) Non-Cohesive 5.0 fps · Cohesive Cohesive 7.0 fps 0.80 C Paved Paved N/A N/A Minor Storm Major Storn Max. Allowable Top Width of Channel for Minor & Major Storm 8.00 8.00 Max. Allowable Water Depth in Channel for Minor & Major Storm d_{MAX} 1.50 Allowable Channel Capacity Based On Channel Geometry
MINOR STORM Allowable Capacity is based on Top Width Criterion Minor Storm Major Storm 26.6 cfs 26.6 MAJOR STORM Allowable Capacity is based on Top Width Criterion dallow 1.33 1.33 Water Depth in Channel Based On Design Peak Flow Design Peak Flow Q_o = 5.0 15.0 cfs Water Depth 0.71 1.08 Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management' Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

AREA INLET IN A SWALE

ELDORADO SPRINGS DP-25 Inlet Design Information (Input) Type of Inlet CDOT Type C (Depressed) Inlet Type = CDOT Type C (Depressed) -Angle of Inclined Grate (must be <= 30 degrees) θ= 0.00 Width of Grate W= 3.00 Length of Grate L= 3.00 feet Open Area Ratio A_{RATIO} = 0.70 Height of Inclined Grate HB = 0.00 Clogging Factor C, = 0.50 Grate Discharge Coefficient C_d = 0.84 Orifice Coefficient Co: Weir Coefficient 1.81 MINOR Water Depth at Inlet (for depressed inlets, 1 foot is added for depression) 1.71 2.08 Total Inlet Interception Capacity (assumes clogged condition) Q_a = 18.6 20.5 cfs Bypassed Flow, Q_b = 0.0 0.0 cfs Capture Percentage = Q_a/Q_o = C% 100 100 %

Warning 04: Froude No. exceeds USDCM Volume I recommendation.



Site-Level Low Impact Development (LID) Design Effective Impervious Calculator

LID Credit by Impervious Reduction Factor (IRF) Method

UD-BMP (Version 3.06, November 2016)

User Input

inches

inches

Calculated cells

2.51496

 Designer:
 Chad Kuzbek, PE

 Company:
 WestWorks Engineering

 Date:
 November 5, 2019

 Project:
 EL DORADO SPRINGS

 Location:
 POND A

SITE INFORMATION (USER-INPUT)

Max Intensity for Optional User Defined Storm

| Sub-basin Identifier | A1 | A2 | A3 | A4 | A5 | A6 | A7 | A8 | A9 | OS-13A | OS-13B | | | |
|---|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|------------|------------|------------|
| Receiving Pervious Area Soil Type | Clay Loam | Sandy Loam | Sandy Loam | Sandy Loam |
| Total Area (ac., Sum of DCIA, UIA, RPA, & SPA) | 0.300 | 0.400 | 0.400 | 0.300 | 0.300 | 1.100 | 0.400 | 0.300 | 0.500 | 1.600 | 0.500 | | | |
| Directly Connected Impervious Area (DCIA, acres) | 0.300 | 0.400 | 0.400 | 0.300 | 0.200 | 0.800 | 0.300 | 0.100 | 0.000 | 0.300 | 0.100 | | | |
| Unconnected Impervious Area (UIA, acres) | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | | | |
| Receiving Pervious Area (RPA, acres) | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | | | |
| Separate Pervious Area (SPA, acres) | 0.000 | 0.000 | 0.000 | 0.000 | 0.100 | 0.300 | 0.100 | 0.200 | 0.500 | 1.300 | 0.400 | | | |
| RPA Treatment Type: Conveyance (C), Volume (V), or Permeable Pavement (PP) | v | ٧ | v | V | v | v | v | V | ٧ | V | ٧ | | | |

| volume (v), or remineable ravelment (r) | | | ALCOHOLD TO | A CONTRACTOR OF THE PARTY | | - | Maria Caracteria | | | The second | the state of the s | | | |
|--|--------|--------|-------------|---------------------------|-------|-------|------------------|-------|--------|------------|--|------------------|------------------|---------|
| | | | | | | | | | | | | MISSING INPUT | MISSING INPUT | MISSING |
| CALCULATED RESULTS (OUTPUT) | | | | | | | | | | | | | | |
| Total Calculated Area (ac, check against input) | 0.300 | 0.400 | 0.400 | 0.300 | 0.300 | 1.100 | 0.400 | 0.300 | 0.500 | 1.600 | 0.500 | | | |
| Directly Connected Impervious Area (DCIA, %) | 100.0% | 100.0% | 100.0% | 100.0% | 66.7% | 72.7% | 75.0% | 33.3% | 0.0% | 18.8% | 20.0% | | | |
| Unconnected Impervious Area (UIA, %) | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | | | |
| Receiving Pervious Area (RPA, %) | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | | | |
| Separate Pervious Area (SPA, %) | 0.0% | 0.0% | 0.0% | 0.0% | 33.3% | 27.3% | 25.0% | 66.7% | 100.0% | 81.3% | 80.0% | | | |
| A _R (RPA / UIA) | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | | | |
| I _a Check | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | | | |
| f / I for WQCV Event: | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 | | | |
| f / I for 10-Year Event: | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | | | |
| f / I for 100-Year Event: | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | | | |
| f / I for Optional User Defined Storm CUHP: | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 | | | |
| IRF for WQCV Event: | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | | | |
| IRF for 10-Year Event: | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | |
| IRF for 100-Year Event: | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | |
| IRF for Optional User Defined Storm CUHP: | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | |
| Total Site Imperviousness: I _{total} | 100.0% | 100.0% | 100.0% | 100.0% | 66.7% | 72.7% | 75.0% | 33.3% | 0.0% | 18.8% | 20.0% | | | |
| Effective Imperviousness for WQCV Event: | 100.0% | 100.0% | 100.0% | 100.0% | 66.7% | 72.7% | 75.0% | 33.3% | 0.0% | 18.8% | 20.0% | | | |
| Effective Imperviousness for 10-Year Event: | 100.0% | 100.0% | 100.0% | 100.0% | 66.7% | 72.7% | 75.0% | 33.3% | 0.0% | 18.8% | 20.0% | | | |
| Effective Imperviousness for 100-Year Event: | 100.0% | 100.0% | 100.0% | 100.0% | 66.7% | 72.7% | 75.0% | 33.3% | 0.0% | 18.8% | 20.0% | | | |
| Effective Imperviousness for Optional User Defined Storm CUHP: | 100.0% | 100.0% | 100.0% | 100.0% | 66.7% | 72.7% | 75.0% | 33.3% | 0.0% | 18.8% | 20.0% | | | |

LID / EFFECTIVE IMPERVIOUSNESS CREDITS WQCV Event CREDIT: Reduce Detention By:

| 10-Year Event CREDIT**: | Reduce Detention By: |
|---------------------------|----------------------|
| 100-Year Event CREDIT**: | Reduce Detention By: |
| User Defined CUHP CREDIT: | Reduce Detention By: |

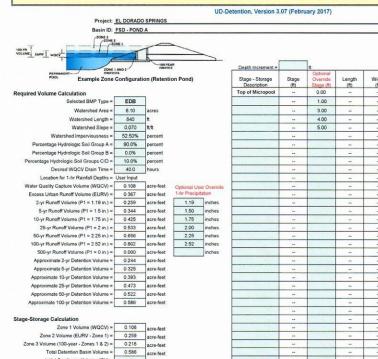
| | N/A | | | |
|---|------|------|------|------|------|------|------|------|------|------|------|---|---|--|
| L | 0.0% | 0.0% | 0.0% | 0.0% | 0.1% | 0.0% | 0.0% | 0.2% | N/A | 0.1% | 0.2% | - | V | |
| | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.1% | N/A | 0.0% | 0.1% | | | |
| | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | | | |

| Total Site Imperviousness: | 52.5% |
|--|-------|
| Total Site Effective Imperviousness for WQCV Event: | 52.5% |
| Total Site Effective Imperviousness for 10-Year Event: | 52.5% |
| Total Site Effective Imperviousness for 100-Year Event: | 52.5% |
| otal Site Effective Imperviousness for Optional User Defined Storm CUHP: | 52.5% |

Notes:

- * Use Green-Ampt average infiltration rate values from Table 3-3.
- Flood control detention volume credits based on empirical equations from Storage Chapter of USDCM.
 *** Method assumes that 1-hour rainfall depth is equivalent to 1-hour intensity for calculation purposed

DETENTION BASIN STAGE-STORAGE TABLE BUILDER



| Zone 2 Volume (EURV - Zone 1) = | 0.259 | acre-feet |
|--|---|---|
| Zone 3 Volume (100-year - Zones 1 & 2) = | 0.218 | acre-feet |
| Total Detention Basin Volume = | 0.586 | acre-feet |
| Initial Surcharge Volume (ISV) = | user | ft^3 |
| Initial Surcharge Depth (ISD) = | user | ft |
| Total Available Detention Depth (Htotal) = | user | ft |
| | Zone 3 Volume (100-year - Zones 1 & 2) = Total Detention Basin Volume = Initial Surcharge Volume (ISV) = Initial Surcharge Depth (ISD) = | Zone 3 Volume (100-year - Zones 1 & 2) = 0.218 Total Detention Basin Volume = 0.586 Initial Surcharge Volume (ISV) = user Initial Surcharge Depth (ISD) = user |

| ft^3 | user | Initial Surcharge Volume (ISV) = |
|-------|------|---|
| ft | user | Initial Surcharge Depth (ISD) = |
| ft | user | Total Available Detention Depth (H _{total}) = |
| ft | user | Depth of Trickle Channel (H _{TC}) = |
| ft/ft | user | Slope of Trickle Channel (Stc) = |
| H:V | user | Slopes of Main Basin Sides (Smain) = |
| | user | Basin Length-to-Width Ratio (R _{L/W}) = |

| Surcharge Volume Length (L _{15v}) = | user | ft |
|---|------|-----------|
| Surcharge Volume Width (Wigu) = | user | ft |
| Depth of Basin Floor (HFLOOR) = | user | ft |
| Length of Basin Floor (L _{FLOOR}) = | user | ft |
| Width of Basin Floor (W _{FLOOR}) = | user | ft |
| Area of Basin Floor (A _{FLOOR}) = | user | ft^2 |
| Volume of Basin Floor (VFLOOR) = | user | ft^3 |
| Depth of Main Basin (H _{MAIN}) = | user | ft |
| Length of Main Basin (L _{MAIN}) = | user | ft |
| Width of Main Basin (W _{MAIN}) = | user | ft |
| Area of Main Basin (A _{MAIN}) = | user | ft^2 |
| Volume of Main Basin (V _{MAIN}) = | user | ft^3 |
| Calculated Total Basin Volume (Vtotal) = | user | acre-feet |

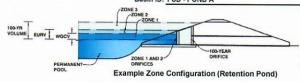
| Top Micropool | Stage - Storage Description | Stage (ft) | Optional Override Stage (ft) | Length (ft) | Width (ft) | Area (ft^2) | Optional Override Area (ft*2) | Area (acre) | Volume (ft^3) | Volume (ac-ft) |
|--|--------------------------------|---------------|------------------------------------|----------------|---------------|----------------|-------------------------------------|----------------|------------------|-------------------|
| - 300 5500 1377 14300 3328 | Top of Micropool | | 10.5000 | | | | | | | |
| | | | | | | | | | | |
| | | _ | | | | | | | | |
| | | | | | | | | | | |
| | | | 5.00 | | | | 8,070 | 0.185 | 28,380 | 0.652 |
| | | | | | | | | | | _ |
| | | | | | | | | | | |
| | | | - | | | | | | | |
| | | | - | | | | | - | _ | |
| | | | | | | | | | | |
| | | | | | | | | | | |
| | | | | | | | | | | |
| | | | | | | | | | | |
| | | 20 | | | - | _ | | | | |
| | | ** | | | | | Control of the | | | |
| | | | | | | | | | | |
| | | | | | | | | | | |
| | | ** | | | | - | | | | |
| | | 24 | | | ** | ** | | | | |
| | The second second | | Decree of the second | | | | | | | |
| | | | | | | | | | | |
| | | | | | | | | | | |
| | | | | | | | | | | |
| | | | | | | | | | | |
| | | | | | | | | | | |
| | | | | | | | | | | |
| | | | | | | | | | | |
| | | | | | | | | | | |
| | | | | | | - | | | | |
| | | | | | | | - | | | |
| | | | | | | | | | | |
| | | | | | | | | | | |
| | | | | | | | | | | |
| | | | | | | | | | | |
| | | | | | | | - | | _ | |
| | | | | | | | | | | |
| | | | | | | | | | | |
| | | ** | | - | - | | | | | |
| | | - | | - | - | - | | | | |
| | | | | | ** | - | | | | |
| | | ** | | | ** | | | | | |
| | | | | - | 343 | | | | | |
| | | | | | - | - | | | | |
| | | | | | | | | | | |
| | | | | | | | | | | |
| | | | | | | | | | | |
| | | | | | | | | | | |
| 1 | | | | | | | | | | |
| 1 | | | | | | | | | | |
| 1 | | | | _ | | | | | | |
| 10 | | | | 2.0 | | | | | | |
| 1 | | | | | | | | | | - |
| 1 | | 22 | | | | ** | | | | |
| 1 | | - | | - | | | | | | |
| 1 | | | | | | - | | 6 | | |
| 1 | | | | | | | | | | |
| 1 | | | - | | ** | | | | | |
| 1 | | | | | | - | | | | |
| 1 | | ** | | | | | | | | |
| 10 | | | | | | | | | | |
| 1 | | | | | | - | | - | | |
| 10 | | | 100 | - | | | | | | |
| 1 | | | | | ** | | | | | |
| 1 | | - | | - :- | | | | | | |
| 10 | | | | | | | | 7 | | 111 |
| 1 | | | | | ** | ** | | | | |
| 10 10 10 10 10 10 10 10 10 10 10 10 10 1 | | | | | | | | | | |
| 10 10 10 10 10 10 10 10 10 10 10 10 10 1 | | - | | | - :- | - | | | | |
| 10 10 10 10 10 10 10 10 10 10 10 10 10 1 | - | | | ** | | - | | | | |
| 10 10 10 10 10 10 10 10 10 10 10 10 10 1 | | - | | | | | | 4 | | |
| 1 | | | | | | | | | | |
| | | | | ** | 44 | | | | | |
| 1 | | | | | | - | | | | |
| | | | | | ** | - | | | | |
| 10 | | | | | | - | | | | |
| | | | | ** | | - | - | | | |
| 10 | | | | - | - | - | | | | |
| 10 10 10 10 10 10 10 10 10 10 10 10 10 1 | | - | | | - | | | | | |
| 10 10 10 10 10 10 10 10 10 10 10 10 10 1 | | | | - | - | - | - | | | |
| 1 | | - " | | ** | | | | | | |
| | | | | - | | | | | | |
| | | | | | | | | | | |

Detention Basin Outlet Structure Design

UD-Detention, Version 3.07 (February 2017)

Project: EL DORADO SPRINGS

Basin ID: FSD - POND A



| | Stage (ft) | Zone Volume (ac-ft) | Outlet Type |
|-------------------|------------|---------------------|----------------------|
| Zone 1 (WQCV) | 1.19 | 0.108 | Orifice Plate |
| Zone 2 (EURV) | 3.28 | 0.259 | Orifice Plate |
| 'one 3 (100-year) | 4.64 | 0.218 | Weir&Pipe (Restrict) |
| | | 0.586 | Total |

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth = ft (distance below the filtration media surface) N/A Underdrain Orifice Diameter N/A inches

| Calculated P | arameters fo | r Underdra |
|-------------------------------|--------------|-----------------|
| Underdrain Orifice Area = | N/A | ft ² |
| Underdrain Orifice Centroid = | N/A | feet |

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice = ft (relative to basin bottom at Stage = 0 ft) 0.00 Depth at top of Zone using Orifice Plate = 3.28 ft (relative to basin bottom at Stage = 0 ft) Orifice Plate: Orifice Vertical Spacing = 13.10 inches Orifice Plate: Orifice Area per Row = N/A

| Calculated Parameters for | | | | | |
|----------------------------|-----|-----------------|--|--|--|
| WQ Orifice Area per Row = | N/A | ft ² | | | |
| Elliptical Half-Width = | N/A | feet | | | |
| Elliptical Slot Centroid = | N/A | feet | | | |
| Elliptical Slot Area = | N/A | ft ² | | | |

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

| CONTRACTOR | Row 1 (required) | Row 2 (optional) | Row 3 (optional) | Row 4 (optional) | Row 5 (optional) | Row 6 (optional) | Row 7 (optional) | Row 8 (optional) |
|---|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|
| Stage of Orifice Centroid (ft) | 0.00 | 1.09 | 2.19 | | | | | |
| Orifice Area (sq. inches) | 1.45 | 1.45 | 1.45 | | | | | |

| | Row 9 (optional) | Row 10 (optional) | Row 11 (optional) | Row 12 (optional) | Row 13 (optional) | Row 14 (optional) | Row 15 (optional) | Row 16 (optional) |
|--------------------------------|------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| Stage of Orifice Centroid (ft) | | | | | | | | |
| Orifice Area (sq. inches) | | | | | | | | |

User Input: Vertical Orifice (Circular or Rectangular)

| | Not Selected | Not Selected | |
|---|--------------|--------------|---|
| Invert of Vertical Orifice = | N/A | N/A | ft (relative to basin bottom at Stage = 0 ft) |
| Depth at top of Zone using Vertical Orifice = | N/A | N/A | ft (relative to basin bottom at Stage = 0 ft) |
| Vertical Orifice Diameter = | N/A | N/A | inches |

| Calculated F | arameters for Vert | ical Orifice | |
|-----------------------------|--------------------|--------------|-----------------|
| | Not Selected | Not Selected | |
| Vertical Orifice Area = | N/A | N/A | ft ² |
| Vertical Orifice Centroid = | N/A | N/A | feet |

User Input: Overflow Weir (Dropbox) and Grate (Flat or Sloped)

| | Zone 3 Weir | Not Selected | |
|-------------------------------------|-------------|--------------|---|
| Overflow Weir Front Edge Height, Ho | 3.28 | N/A | ft (relative to basin bottom at Stage = 0 ft) |
| Overflow Weir Front Edge Length : | 2.92 | N/A | feet |
| Overflow Weir Slope : | 0.00 | N/A | H:V (enter zero for flat grate) |
| Horiz. Length of Weir Sides : | 2.92 | N/A | feet |
| Overflow Grate Open Area % : | 85% | N/A | %, grate open area/total area |
| Debris Clogging % : | 50% | N/A | % |

| Calculated | arameters for Ove | mow weir | 17 |
|--|-------------------|--------------|-----------------|
| | Zone 3 Weir | Not Selected | |
| Height of Grate Upper Edge, H _t = | 3.28 | N/A | feet |
| Over Flow Weir Slope Length = | 2.92 | N/A | feet |
| Grate Open Area / 100-yr Orifice Area = | 28.80 | N/A | should be ≥ 4 |
| Overflow Grate Open Area w/o Debris = | 7.25 | N/A | ft ² |
| Overflow Grate Open Area w/ Debris = | 3.62 | N/A | ft ² |

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

| | Zone 3 Restrictor | Not Selected | | | Zone 3 Restrictor | Not Selected | 7 |
|---|-------------------|---------------------|--|-----------------------------------|-------------------|--------------|-----------------|
| Depth to Invert of Outlet Pipe = | 2.50 | N/A | ft (distance below basin bottom at Stage = 0 ft) | Outlet Orifice Area = | 0.25 | N/A | ft ² |
| Outlet Pipe Diameter = | 18.00 | N/A | inches | Outlet Orifice Centroid = | 0.18 | N/A | feet |
| Restrictor Plate Height Above Pipe Invert = | 3.60 | | inches Half-Central Ar | gle of Restrictor Plate on Pipe = | 0.93 | N/A | radians |

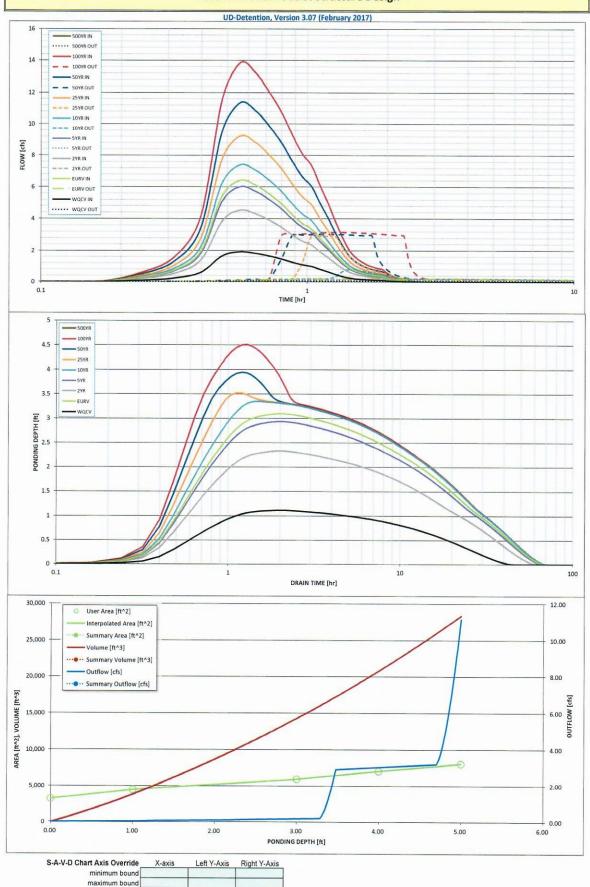
User Input: Emergency Spillway (Rectangular or Trapezoidal)

| | Spillway Invert Stage= | 4.70 | ft (relative to basin bottom at Stage = 0 ft) |
|--------------|-------------------------|-------|---|
| | Spillway Crest Length = | 15.00 | feet |
| | Spillway End Slopes = | 4.00 | H:V |
| Freeboard ab | ove Max Water Surface = | 1.00 | feet |

| Calculated | Parameters : | for Spillwa |
|----------------------------------|--------------|-------------|
| Spillway Design Flow Depth= | 0.43 | feet |
| Stage at Top of Freeboard = | 6.13 | feet |
| Basin Area at Top of Freeboard = | 0.19 | acres |

| Routed Hydrograph Results | | | | | | | | | |
|---|-------|-------|--------|--------|------------------|----------------|----------------|----------------|----------|
| Design Storm Return Period = | WQCV | EURV | 2 Year | 5 Year | 10 Year | 25 Year | 50 Year | 100 Year | 500 Year |
| One-Hour Rainfall Depth (in) = | 0.53 | 1.07 | 1.19 | 1.50 | 1.75 | 2.00 | 2.25 | 2.52 | 0.00 |
| Calculated Runoff Volume (acre-ft) = | 0.108 | 0.367 | 0.259 | 0.344 | 0.425 | 0.533 | 0.656 | 0.802 | 0.000 |
| OPTIONAL Override Runoff Volume (acre-ft) = | | | | | | | | | 0,000 |
| Inflow Hydrograph Volume (acre-ft) = | 0.108 | 0.367 | 0.258 | 0.344 | 0.425 | 0.533 | 0.656 | 0.802 | #N/A |
| Predevelopment Unit Peak Flow, q (cfs/acre) = | 0.00 | 0.00 | 0.00 | 0.02 | 0.05 | 0.11 | 0.29 | 0.58 | 0.00 |
| Predevelopment Peak Q (cfs) = | 0.0 | 0.0 | 0.0 | 0.1 | 0.3 | 0.6 | 1.7 | 3.5 | 0.0 |
| Peak Inflow Q (cfs) = | 1.9 | 6.4 | 4.5 | 6.0 | 7.4 | 9.3 | 11.4 | 13.9 | #N/A |
| Peak Outflow Q (cfs) = | 0.1 | 0.2 | 0.1 | 0.2 | 0.8 | 2.9 | 3.0 | 3.2 | #N/A |
| Ratio Peak Outflow to Predevelopment Q = | N/A | N/A | N/A | 1.8 | 2.8 | 4.6 | 1.7 | 0.9 | #N/A |
| Structure Controlling Flow = | Plate | Plate | Plate | Plate | Overflow Grate 1 | Outlet Plate 1 | Outlet Plate 1 | Outlet Plate 1 | #N/A |
| Max Velocity through Grate 1 (fps) = | N/A | N/A | N/A | N/A | 0.1 | 0.4 | 0.4 | 0.4 | #N/A |
| Max Velocity through Grate 2 (fps) = | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | #N/A |
| Time to Drain 97% of Inflow Volume (hours) = | 39 | 57 | 52 | 56 | 58 | 56 | 54 | 52 | #N/A |
| Time to Drain 99% of Inflow Volume (hours) = | 43 | 63 | 57 | 62 | 64 | 63 | 62 | 61 | #N/A |
| Maximum Ponding Depth (ft) = | 1.12 | 3.10 | 2.33 | 2.94 | 3.35 | 3.52 | 3.95 | 4.52 | #N/A |
| Area at Maximum Ponding Depth (acres) = | 0.10 | 0.14 | 0.13 | 0.14 | 0.15 | 0.15 | 0.16 | 0.17 | #N/A |
| Maximum Volume Stored (acre-ft) = | 0.100 | 0.341 | 0.239 | 0.319 | 0.378 | 0.403 | 0.468 | 0.563 | #N/A |

Detention Basin Outlet Structure Design



Prepared by WestWorks Engineering

Page 1

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Pond POND A:

Inflow Area = 6.100 ac, Inflow Depth = 0.36" for 5-Year event Inflow 0.18 hrs, Volume= 11.97 cfs @ 0.181 af 0.36 hrs, Volume= Outflow 0.11 cfs @ 0.024 af, Atten= 99%, Lag= 11.0 min Primary = 0.11 cfs @ 0.36 hrs, Volume= 0.024 af Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs Peak Elev= 5,860.76' @ 0.36 hrs Surf.Area= 0.116 ac Storage= 0.180 af Plug-Flow detention time= 89.9 min calculated for 0.024 af (13% of inflow) Center-of-Mass det. time= 83.8 min (92.8 - 9.0)

| # | Invert | Avail.Storage | Storage Description |
|---|-----------|---------------|--|
| 1 | 5,859.00' | 0.652 af | Custom Stage Data (Prismatic) Listed below |

| Elevation (feet) | Surf.Area (acres) | Inc.Store (acre-feet) | Cum.Store (acre-feet) |
|---------------------|-------------------|-----------------------|-----------------------|
| 5,859.00 | 0.074 | 0.000 | 0.000 |
| 5,860.00 | 0.103 | 0.089 | 0.089 |
| 5,862.00 | 0.137 | 0.240 | 0.329 |
| 5,863.00 | 0.162 | 0.150 | 0.478 |
| 5,864.00 | 0.185 | 0.173 | 0.652 |

| # | Routing | Invert | Outlet Devices |
|---|----------|-------------|---|
| 1 | Primary | 5,856.50' | 6.8" x 120.0' long OUTLET W/ RESTRICTOR PLATE |
| | | | RCP, square edge headwall, Ke= 0.500 |
| | | | Outlet Invert= 5,854.29' S= 0.0184 '/' n= 0.013 Cc= 0.900 |
| 2 | Device 1 | 5,859.00' | 1.4" Vert. WQ ORIFICE C= 0.600 |
| 3 | Device 1 | 5,860.10' | 1.4" Vert. WQ ORIFICE C= 0.600 |
| 4 | Primary | 5,861.20' | 1.4" Vert. WQ ORIFICE C= 0.600 |
| 5 | Device 1 | 5,862.28' | 2.92' x 2.92' Horiz. CDOT TYPE C INLET W/ MESH GRATE |
| | | | Limited to weir flow C= 0.600 |
| 6 | Secondar | y 5,863.70' | 15.0' long x 10.4' breadth EMERGENCY OVERFLOW |
| | | | Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 |
| | | | Coef. (English) 2.51 2.57 2.70 2.69 2.68 2.69 2.67 2.64 |

Primary OutFlow Max=0.11 cfs @ 0.36 hrs HW=5,860.76' (Free Discharge)

1=OUTLET W/ RESTRICTOR PLATE (Passes 0.11 cfs of 1.59 cfs potential flow)

2=WQ ORIFICE (Orifice Controls 0.07 cfs @ 6.3 fps)

-3=WQ ORIFICE (Orifice Controls 0.04 cfs @ 3.7 fps)

-5=CDOT TYPE C INLET W/ MESH GRATE (Controls 0.00 cfs)

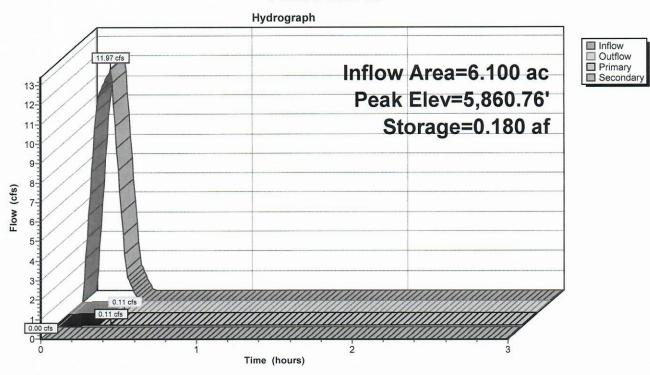
-4=WQ ORIFICE (Controls 0.00 cfs)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=5,859.00' (Free Discharge) 6=EMERGENCY OVERFLOW (Controls 0.00 cfs)

Page 2 11/6/2019

Prepared by WestWorks Engineering
HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

Pond POND A:



Prepared by WestWorks Engineering

Page 1

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Pond POND A:

Inflow Area = 6.100 ac, Inflow Depth = 0.80" for 100-Year event Inflow 25.45 cfs @ 0.15 hrs, Volume= 0.405 af 1.83 cfs @ Outflow = 0.32 hrs, Volume=

0.074 af, Atten= 93%, Lag= 9.9 min

Primary 1.83 cfs @ = 0.32 hrs, Volume= 0.074 af Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs Peak Elev= 5,862.42' @ 0.32 hrs Surf.Area= 0.147 ac Storage= 0.391 af Plug-Flow detention time= 66.8 min calculated for 0.074 af (18% of inflow)

Center-of-Mass det. time= 61.2 min (70.2 - 9.0)

Invert Avail.Storage Storage Description

5,859.00' 0.652 af Custom Stage Data (Prismatic) Listed below

| Elevation (feet) | Surf.Area (acres) | Inc.Store (acre-feet) | Cum.Store (acre-feet) |
|---------------------|-------------------|-----------------------|-----------------------|
| 5,859.00 | 0.074 | 0.000 | 0.000 |
| 5,860.00 | 0.103 | 0.089 | 0.089 |
| 5,862.00 | 0.137 | 0.240 | 0.329 |
| 5,863.00 | 0.162 | 0.150 | 0.478 |
| 5,864.00 | 0.185 | 0.173 | 0.652 |

| # | Routing | Invert | Outlet Devices |
|---|---------|-----------|---|
| 1 | Primary | 5,856.50' | 6.8" x 120.0' long OUTLET W/ RESTRICTOR PLATE |

RCP, square edge headwall, Ke= 0.500 Outlet Invert= 5,854.29' S= 0.0184 '/' n= 0.013 Cc= 0.900

2 Device 1 5,859.00' 1.4" Vert. WQ ORIFICE C= 0.600

3 Device 1 5.860.10' 1.4" Vert. WQ ORIFICE C= 0.600 4 Primary 5,861.20' 1.4" Vert. WQ ORIFICE C= 0.600

5 Device 1 5,862.28' 2.92' x 2.92' Horiz. CDOT TYPE C INLET W/ MESH GRATE

Limited to weir flow C= 0.600

6 Secondary 5,863.70' 15.0' long x 10.4' breadth EMERGENCY OVERFLOW

Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 Coef. (English) 2.51 2.57 2.70 2.69 2.68 2.69 2.67 2.64

Primary OutFlow Max=1.86 cfs @ 0.32 hrs HW=5,862.42' (Free Discharge)

-1=OUTLET W/ RESTRICTOR PLATE (Barrel Controls 1.80 cfs @ 7.1 fps)

-2=WQ ORIFICE (Passes < 0.09 cfs potential flow) -3=WQ ORIFICE (Passes < 0.08 cfs potential flow)

-5=CDOT TYPE C INLET W/ MESH GRATE (Passes < 1.90 cfs potential flow)

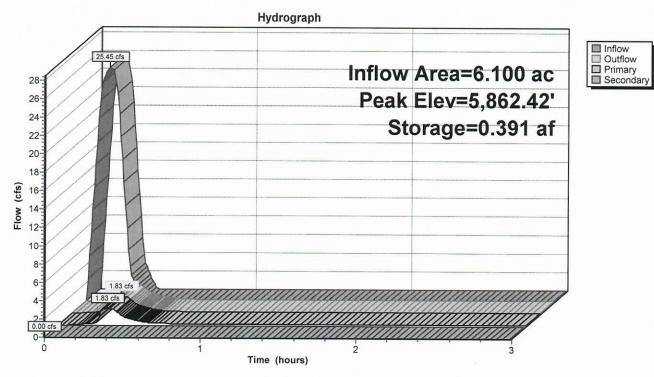
4=WQ ORIFICE (Orifice Controls 0.06 cfs @ 5.2 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=5,859.00' (Free Discharge) 6=EMERGENCY OVERFLOW (Controls 0.00 cfs)

Page 2 11/6/2019

Prepared by WestWorks Engineering
HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

Pond POND A:



Site-Level Low Impact Development (LID) Design Effective Impervious Calculator

LID Credit by Impervious Reduction Factor (IRF) Method

UD-BMP (Version 3.06, November 2016)

inches

inches

User Input Calculated cells

2.51496

***Design Storm: 1-Hour Rain Depth WQCV Event 0.60 ***Minor Storm: 1-Hour Rain Depth 10-Year Event 1.75 ***Major Storm: 1-Hour Rain Depth 2.52 Optional User Defined Storm CUHP (CUHP) NOAA 1 Hour Rainfall Depth and Frequency for User Defined Storm 2.52 100-Year Event

Designer: Chad Kuzbek, PE WestWorks Engineering Company: Date: November 5, 2019 ELDORADO SPRINGS Project: Location: POND B

Max Intensity for Optional User Defined Storm

| SITE INFORMATION (USER-INPUT) | | | | | | | | | | | | | | |
|---|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| Sub-basin Identifier | B1 | B2 | B3 | B4 | B5 | B6 | B7 | B8 | B9 | B10 | OS-11 | OS-12 | B11 | |
| Receiving Pervious Area Soil Type | Clay Loam |
| Total Area (ac., Sum of DCIA, UIA, RPA, & SPA) | 0.400 | 0.400 | 0.400 | 0.900 | 0.400 | 0.500 | 0.700 | 0.700 | 0.200 | 0.600 | 2.800 | 1.300 | 0.900 | |
| Directly Connected Impervious Area (DCIA, acres) | 0.400 | 0.350 | 0,400 | 0.800 | 0.350 | 0.450 | 0.550 | 0.400 | 0.150 | 0.150 | 0.800 | 0.300 | 0.400 | |
| Unconnected Impervious Area (UIA, acres) | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | |
| Receiving Pervious Area (RPA, acres) | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | |
| Separate Pervious Area (SPA, acres) | 0.000 | 0.050 | 0.000 | 0.100 | 0.050 | 0.050 | 0.150 | 0.300 | 0.050 | 0.450 | 2.000 | 1.000 | 0.500 | |
| RPA Treatment Type: Conveyance (C), Volume (V), or Permeable Pavement (PP) | ٧ | ٧ | v | v | V | v | V | V | ٧ | v | v | ٧ | V | |

0.0%

| Δ | LCUI | ATED | RESULTS | (OUTPUT) |
|---|------|------|---------|----------|

| LATED RESULTS (OUTPUT) | | | | | | | | | | | | | | |
|--|--------|-------|--------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|--|
| Total Calculated Area (ac, check against input) | 0.400 | 0.400 | 0.400 | 0.900 | 0.400 | 0.500 | 0.700 | 0.700 | 0.200 | 0.600 | 2.800 | 1.300 | 0.900 | |
| Directly Connected Impervious Area (DCIA, %) | 100.0% | 87.5% | 100.0% | 88.9% | 87.5% | 90.0% | 78.6% | 57.1% | 75.0% | 25.0% | 28.6% | 23.1% | 44.4% | |
| Unconnected Impervious Area (UIA, %) | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | |
| Receiving Pervious Area (RPA, %) | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | |
| Separate Pervious Area (SPA, %) | 0.0% | 12.5% | 0.0% | 11.1% | 12.5% | 10.0% | 21.4% | 42.9% | 25.0% | 75.0% | 71.4% | 76.9% | 55.6% | |
| A _R (RPA / UIA) | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | |
| I _a Check | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | |
| f / I for WQCV Event: | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 | |
| f / I for 10-Year Event: | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | |
| f / I for 100-Year Event: | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | |
| f / I for Optional User Defined Storm CUHP: | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 | |
| IRF for WQCV Event: | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| IRF for 10-Year Event: | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| IRF for 100-Year Event: | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| IRF for Optional User Defined Storm CUHP: | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Total Site Imperviousness: I _{total} | 100.0% | 87.5% | 100.0% | 88.9% | 87.5% | 90.0% | 78.6% | 57.1% | 75.0% | 25.0% | 28.6% | 23.1% | 44.4% | |
| Effective Imperviousness for WQCV Event: | 100.0% | 87.5% | 100.0% | 88.9% | 87.5% | 90.0% | 78.6% | 57.1% | 75.0% | 25.0% | 28.6% | 23.1% | 44.4% | |
| Effective Imperviousness for 10-Year Event: | 100.0% | 87.5% | 100.0% | 88.9% | 87.5% | 90.0% | 78.6% | 57.1% | 75.0% | 25.0% | 28.6% | 23.1% | 44.4% | |
| Effective Imperviousness for 100-Year Event: | 100.0% | 87.5% | 100.0% | 88.9% | 87.5% | 90.0% | 78.6% | 57.1% | 75.0% | 25.0% | 28.6% | 23.1% | 44.4% | |
| Effective Imperviousness for Optional User Defined Storm CUHP: | 100.0% | 87.5% | 100.0% | 88,9% | 87.5% | 90.0% | 78.6% | 57.1% | 75.0% | 25.0% | 28.6% | 23.1% | 44.4% | |

LID / EFFECTIVE IMPERVIOUSNESS CREDITS

| WQCV Event CREDIT: Reduce Detention By: | N/A | N/A | N/A | N/A | ĺ |
|--|------|------|------|------|------|------|------|--|------|------|------|---|
| 10-Year Event CREDIT**: Reduce Detention By: | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.1% | 0.1% | 0.0% | ſ |
| 100-Year Event CREDIT**: Reduce Detention By: | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.1% | 0.1% | 0.0% | İ |
| User Defined CUHP CREDIT: Reduce Detention By: | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | ľ |
| | | | | | | | | A. The state of th | • | | | ۰ |

| Total Site Imperviousness: | 53.9% |
|---|-------|
| Total Site Effective Imperviousness for WQCV Event: | 53.9% |
| Total Site Effective Imperviousness for 10-Year Event: | 53.9% |
| Total Site Effective Imperviousness for 100-Year Event: | 53.9% |
| Total Site Effective Imperviousness for Optional User Defined Storm CUHP: | 53.9% |

Notes:

- * Use Green-Ampt average infiltration rate values from Table 3-3.
- Flood control detention volume credits based on empirical equations from Storage Chapter of USDCM.

 **** Method assumes that 1-hour rainfall depth is equivalent to 1-hour intensity for calculation purposed

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

UD-Detention, Version 3.07 (February 2017)



| Required Volume Calculation | | -23 | |
|---|------------|-----------|---------------------|
| Selected BMP Type = | EDB | | |
| Watershed Area = | 10.20 | acres | |
| Watershed Length = | 840 | n | |
| Watershed Slope = | 0.060 | ft/ft | |
| Watershed Imperviousness = | 53.90% | percent | |
| Percentage Hydrologic Soil Group A = | 100.0% | percent | |
| Percentage Hydrologic Soil Group B = | 0.0% | percent | |
| Percentage Hydrologic Soil Groups C/D = | 0.0% | percent | |
| Desired WQCV Drain Time = | 40.0 | hours | |
| Location for 1-hr Rainfall Depths = | User Input | | |
| Water Quality Capture Volume (WQCV) = | 0.185 | acre-feet | Optional User Overr |
| Excess Urban Runoff Volume (EURV) = | 0.647 | acre-feet | 1-hr Precipitation |
| | | | |

| Excess Urban Runoff Volume (EURV) = | 0.647 | acre-feet |
|--|-------|-----------|
| 2-yr Runoff Volume (P1 = 1.19 in.) = | 0.443 | acre-feet |
| 5-yr Runoff Volume (P1 = 1.5 in.) = | 0.581 | acre-feet |
| 10-yr Runoff Volume (P1 = 1.75 in.) = | 0.713 | acre-feet |
| 25-yr Runoff Volume (P1 = 2 in.) = | 0.881 | acre-feet |
| 50-yr Runoff Volume (P1 = 2.25 in.) = | 1.085 | acre-feet |
| 100-yr Runoff Volume (P1 = 2.52 in.) = | 1.324 | acre-feet |
| 500-yr Runoff Volume (P1 = 0 in.) = | 0.000 | acre-feet |
| Approximate 2-yr Detention Volume = | 0.418 | acre-feet |
| Approximate 5-yr Detention Volume = | 0.549 | acre-feet |
| Approximate 10-yr Detention Volume = | 0.667 | acre-feet |
| Approximate 25-yr Detention Volume = | 0.813 | acre-feet |
| Approximate 50-yr Detention Volume = | 0.903 | acre-feet |
| Approximate 100-yr Detention Volume = | 1.009 | acre-feet |
| | | |

Stage-Storage Calculation

| Zone 1 Volume (WQCV) = | 0.185 | acre-feet |
|---|-------|-----------|
| Zone 2 Volume (EURV - Zone 1) = | 0.463 | acre-feet |
| Zone 3 Volume (100-year - Zones 1 & 2) = | 0.362 | acre-feet |
| Total Detention Basin Volume = | 1.009 | acre-feet |
| Initial Surcharge Volume (ISV) = | user | ft^3 |
| Initial Surcharge Depth (ISD) = | user | ft |
| Total Available Detention Depth (H _{total}) = | user | ft |
| Depth of Trickle Channel (H _{TC}) = | user | ft |
| Slope of Trickle Channel (S _{TC}) = | user | n/n |
| Slopes of Main Basin Sides (Smain) = | user | H:V |
| Basin Length-to-Width Ratio (R _{UW}) = | user | |

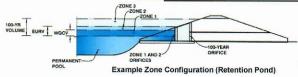
| | 1000 | - |
|---|------|------|
| Initial Surcharge Area (A _{ISV}) = | user | ft^2 |
| Surcharge Volume Length (L _{rpv}) = | user | ft |
| Surcharge Volume Width (W _{rpv}) = | user | ft |
| Depth of Basin Floor (H _{FLOOR}) = | user | ft |
| Length of Basin Floor (L _{FLOOR}) = | user | ft |
| Width of Basin Floor (W _{FLOOR}) = | user | ft |
| Area of Basin Floor (A _{FLOOR}) = | user | ft^2 |
| Volume of Basin Floor (V _{FLOOR}) = | user | ft^3 |
| Depth of Main Basin (H _{MAIN}) = | user | ft |
| Length of Main Basin (L _{MAIN}) = | user | n |
| Width of Main Basin (W _{MAIN}) = | user | ft |
| Area of Main Basin (A _{MAIN}) = | user | ft^2 |
| Volume of Main Basin (V _{MAIN}) = | user | ft^3 |
| Calculated Total Basin Volume (V) = | user | |

| Stage - Storage | Stage | Optional Override | Length | Width | Area | Optional Override | Area | Volume | Volume |
|------------------------------|-------|----------------------|----------|----------|--------|----------------------|-----------------|--------|---------|
| Description Top of Micropool | (ft) | Stage (ft) 0.00 | (ft) | (ft) | (ft^2) | Area (ft^2) 5,400 | (acre) 0.124 | (ft^3) | (ac-ft) |
| | | 1.00 | - | - | - | 6,320 | 0.145 | 5,797 | 0.133 |
| | | 3.00 | | - | - | 8,320 | 0.191 | 20,500 | 0.471 |
| | | 5.00 | | | - | 10,410 | 0.239 | 39,230 | 0.901 |
| | | 6.00 | - | | - | 11,700 | 0.269 | 50,285 | 1.154 |
| | | 7.00 | - | - | | 12,570 | 0.289 | 62,420 | 1.433 |
| | | | | | | | | 02,120 | 1,400 |
| | | | | - | | | | | |
| | | | | - | - | | | | |
| | ** | | - | | | | | | |
| | - | | ** | ** | - | | | | |
| | | | ** | - | | | | | |
| | ** | | - 4 | - | | | | | |
| | | | | - | - | | | | |
| | - | | | | - | | | | |
| | ** | | | - | - | | | | |
| - | | - | | | - | | | | _ |
| | - | | | - | | | | - | |
| | 10.0 | | 2. | - 2 | - | | | | |
| | | | | ** | - | | | | |
| | - | | - | - | - | | | | |
| 2 - 1 - 2 - 2 | - | | - | | ** | | | | |
| | ** | | | - | - | | | | |
| | - | | | | - | | - | | |
| | | | - | - | | | | | |
| | | | - | | - | | | | |
| | | | | | | | | | |
| | - | | ** | ** | - | | | | |
| | (88) | | - 2 | | - | | | | |
| | - | | | 44 | - 2 | | | | |
| | ** | | | | | | | | |
| | | | | ** | - | | | | |
| | ** | | | ** | - | | | | |
| | - | | - | | - | | | | |
| | ** | | | ** | - | | | | |
| | - | _ | | - | | _ | | | - |
| | | - | | | - | | | | _ |
| | - | | - | - | | | | - | |
| | ** | | | - | - | | | | |
| | ** | To the same | - | ** | - | - | | | |
| | ** | | | | | | | | |
| | | | ** | | - | Control of | | | |
| | - | | | - | - | | | | |
| 18 | | | | | | | | | |
| | | | | | | | | | |
| | | | | - | - | | | | |
| | | | | | | | | | |
| | | | | | | | | | |
| | | | | - | | | | | |
| and the second | | | ** | - | | | | | |
| | | | | | | | | | |
| | | | - | | - | | | _ | |
| | = : | | | | ** | | | | |
| | | | | | | | | | |
| | ** | | - | | *** | - Taraban 18 | | | |
| | | | | | - | | _ | - | |
| | | | | - :- | | | | | |
| | | | | | - | | | | |
| | ** | | ** | ** | | | | | |
| | | | | | - | | | | |
| | - : | | ** | ** | - | | | | |
| | - | | | | | | | | |
| | | | | | | | | | |
| | | | | - | | | | | |
| | | | | | - | | | | |
| | ** | | - | | | | | | |
| | -:- | | | | | | | | |
| | - | | - | - | | | | | |
| | - | | - | -:- | | | | | |
| | ** | | | | | | | | |
| | | | | | | - | | | |
| - | | | - | | - | | | | |
| | - 1 | | - | | ** | | | | |
| | | | | | | | | | |
| | | | | - : | - | | | | |
| | | | - | -: | | | | | |
| | | | | - | - | | | | |
| | | | | - | - | | | | |
| | | | - | | - | | | | |
| | | | - | ** | ** | | | | |
| | | | | | | | | | |
| | | | | | - | | | | |

Detention Basin Outlet Structure Design

UD-Detention, Version 3.07 (February 2017)

Project: ELDORADO SPRINGS
Basin ID: FSD - POND B



| | Stage (ft) | Zone Volume (ac-ft) | Outlet Type |
|------------------|------------|---------------------|----------------------|
| Zone 1 (WQCV) | 1.34 | 0.185 | Orifice Plate |
| Zone 2 (EURV) | 3.88 | 0.463 | Orifice Plate |
| one 3 (100-year) | 5.45 | 0.362 | Weir&Pipe (Restrict) |
| | | 1.009 | Total |

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth = N/A ft (distance below the filtration media surface)

Underdrain Orifice Diameter = N/A inches

| Calculated P | arameters fo | r Underdrain |
|-------------------------------|--------------|-----------------|
| Underdrain Orifice Area = | N/A | ft ² |
| Underdrain Orifice Centroid = | N/A | feet |

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

| | to the terminal and the second and the second of the secon |
|-------|--|
| 0.00 | ft (relative to basin bottom at Stage = 0 ft) |
| 3.24 | ft (relative to basin bottom at Stage = 0 ft) |
| 13.00 | inches |
| 2.49 | sq. inches (diameter = 1-3/4 inches) |
| | 0.00 3.24 13.00 |

| Calculat | ed Parameters | for Plat |
|----------------------------|---------------|-----------------|
| WQ Orifice Area per Row = | 1.729E-02 | ft ² |
| Elliptical Half-Width = | N/A | feet |
| Elliptical Slot Centroid = | N/A | feet |
| Elliptical Slot Area = | N/A | ft ² |

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

| | Row 1 (required) | Row 2 (optional) | Row 3 (optional) | Row 4 (optional) | Row 5 (optional) | Row 6 (optional) | Row 7 (optional) | Row 8 (optional) |
|--------------------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|
| Stage of Orifice Centroid (ft) | 0.00 | 1.08 | 2.16 | | | | | |
| Orifice Area (sq. inches) | 2.49 | 2.49 | 2.49 | | | | | |

| | Row 9 (optional) | Row 10 (optional) | Row 11 (optional) | Row 12 (optional) | Row 13 (optional) | Row 14 (optional) | Row 15 (optional) | Row 16 (optional) |
|----------------------------|------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| e of Orifice Centroid (ft) | | | | | | | | |
| Orifice Area (sq. inches) | | | | | | | | |

User Input: Vertical Orifice (Circular or Rectangular)

| | Not Selected | Not Selected | | |
|---|--------------|--------------|---|------------|
| Invert of Vertical Orifice = | N/A | N/A | ft (relative to basin bottom at Stage = 0 ft) | Vertic |
| Depth at top of Zone using Vertical Orifice = | N/A | N/A | ft (relative to basin bottom at Stage = 0 ft) | Vertical O |
| Vertical Orifice Diameter = | N/A | N/A | inches | |

| Calculated P | arameters for Vert | ical Orifice | |
|----------------------|--------------------|--------------|-----------------|
| | Not Selected | Not Selected | |
| tical Orifice Area = | N/A | N/A | ft ² |
| Orifice Centroid = | N/A | N/A | feet |

User Input: Overflow Weir (Dropbox) and Grate (Flat or Sloped)

Stage

| | Zone 3 Weir | Not Selected | |
|---------------------------------------|-------------|--------------|---|
| Overflow Weir Front Edge Height, Ho = | 3.90 | N/A | ft (relative to basin bottom at Stage = 0 ft) |
| Overflow Weir Front Edge Length = | 2.92 | N/A | feet |
| Overflow Weir Slope = | 0.00 | N/A | H:V (enter zero for flat grate) |
| Horiz. Length of Weir Sides = | 2.92 | N/A | feet |
| Overflow Grate Open Area % = | 85% | N/A | %, grate open area/total area |
| Debris Clogging % = | 50% | N/A | % |

| Calculated F | Parameters for Ove | rflow Weir | |
|--|--------------------|--------------|-----------------|
| | Zone 3 Weir | Not Selected | |
| Height of Grate Upper Edge, H _t = | 3.90 | N/A | feet |
| Over Flow Weir Slope Length = | 2.92 | N/A | feet |
| Grate Open Area / 100-yr Orifice Area = | 17.13 | N/A | should be ≥ 4 |
| Overflow Grate Open Area w/o Debris = | 7.25 | N/A | ft ² |
| Overflow Grate Open Area w/ Debris = | 3.62 | N/A | ft ² |

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

| | to the control of the state | tor ridte, or medic | mgarar ormee, | carculated i di diffeter | ieters for Outlet ripe w/ riow Restriction riate | | | |
|---|-----------------------------|---------------------|--|-------------------------------------|--|--------------|-----------------|--|
| | Zone 3 Restrictor | Not Selected | | | Zone 3 Restrictor | Not Selected | 7 | |
| Depth to Invert of Outlet Pipe = | 2.50 | N/A | ft (distance below basin bottom at Stage = 0 ft) | Outlet Orifice Area = | 0.42 | N/A | ft ² | |
| Outlet Pipe Diameter = | 18.00 | N/A | inches | Outlet Orifice Centroid = | 0.25 | N/A | feet | |
| strictor Plate Height Above Pipe Invert = | 5.20 | | inches Half-Central A | Angle of Restrictor Plate on Pipe = | 1.13 | N/A | radians | |

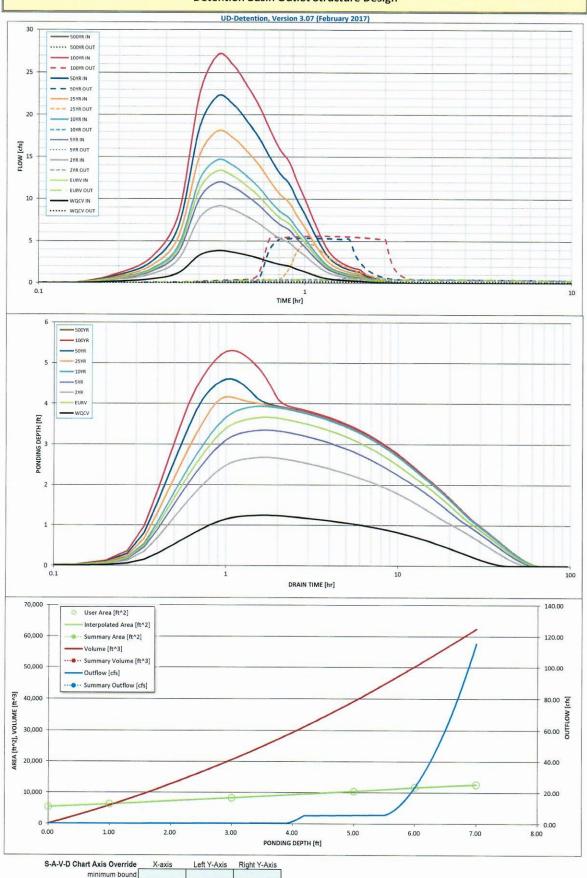
| 5.50 | ft (relative to basin bottom at Stage = 0 ft) |
|-------|---|
| 15.00 | feet |
| 4.00 | H:V |
| 1.00 | feet |
| | 15.00 4.00 |

| Calculated | Calculated Parameters for Spillw | | | | |
|--------------------------------|----------------------------------|-------|--|--|--|
| Spillway Design Flow Depth= | 0.65 | feet | | | |
| Stage at Top of Freeboard = | 7.15 | feet | | | |
| sin Area at Top of Freeboard = | 0.29 | acres | | | |

Basin Area

| Routed Hydrograph Results | | | | | | | | | |
|---|-------|-------|--------|--------|------------------|------------------|----------------|----------------|----------|
| Design Storm Return Period = | WQCV | EURV | 2 Year | 5 Year | 10 Year | 25 Year | 50 Year | 100 Year | 500 Year |
| One-Hour Rainfall Depth (in) = | 0.53 | 1.07 | 1.19 | 1.50 | 1.75 | 2.00 | 2.25 | 2.52 | 0.00 |
| Calculated Runoff Volume (acre-ft) = | 0.185 | 0.647 | 0.443 | 0.581 | 0.713 | 0.881 | 1.085 | 1.324 | 0.000 |
| OPTIONAL Override Runoff Volume (acre-ft) = | | | | | | | | | |
| Inflow Hydrograph Volume (acre-ft) = | 0.184 | 0.647 | 0.441 | 0.580 | 0.712 | 0.880 | 1.083 | 1.322 | #N/A |
| Predevelopment Unit Peak Flow, q (cfs/acre) = | 0.00 | 0.00 | 0.00 | 0.01 | 0.02 | 0.03 | 0.25 | 0.61 | 0.00 |
| Predevelopment Peak Q (cfs) = | 0.0 | 0.0 | 0.0 | 0.1 | 0.2 | 0.4 | 2.6 | 6.2 | 0.0 |
| Peak Inflow Q (cfs) = | 3.9 | 13.4 | 9.2 | 12.0 | 14.7 | 18.1 | 22.2 | 27.1 | #N/A |
| Peak Outflow Q (cfs) = | 0.1 | 0.4 | 0.3 | 0.4 | 0.7 | 4.7 | 5.3 | 5.6 | #N/A |
| Ratio Peak Outflow to Predevelopment Q = | N/A | N/A | N/A | 5.5 | 4.4 | 13.2 | 2.1 | 0.9 | #N/A |
| Structure Controlling Flow = | Plate | Plate | Plate | Plate | Overflow Grate 1 | Overflow Grate 1 | Outlet Plate 1 | Outlet Plate 1 | #N/A |
| Max Velocity through Grate 1 (fps) = | N/A | N/A | N/A | N/A | 0.0 | 0.6 | 0.7 | 0.7 | #N/A |
| Max Velocity through Grate 2 (fps) = | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | #N/A |
| Time to Drain 97% of Inflow Volume (hours) = | 37 | 52 | 47 | 50 | 52 | 51 | 49 | 47 | #N/A |
| Time to Drain 99% of Inflow Volume (hours) = | 40 | 58 | 52 | 56 | 59 | 58 | 57 | 56 | #N/A |
| Maximum Ponding Depth (ft) = | 1.25 | 3.67 | 2.68 | 3.36 | 3.94 | 4.17 | 4.61 | 5.31 | #N/A |
| Area at Maximum Ponding Depth (acres) = | 0.15 | 0.21 | 0.18 | 0.20 | 0.21 | 0.22 | 0.23 | 0.25 | #N/A |
| Maximum Volume Stored (acre-ft) = | 0.170 | 0.602 | 0.409 | 0.539 | 0.661 | 0.708 | 0.807 | 0.976 | #N/A |

Detention Basin Outlet Structure Design



maximum bound

Prepared by WestWorks Engineering

Page 1

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Pond POND B:

Inflow Area = 10.200 ac, Inflow Depth = 0.32" for 5-Year event Inflow 27.63 cfs @ 0.11 hrs, Volume= 0.271 af Outflow 0.23 hrs, Volume= = 0.16 cfs @ 0.037 af, Atten= 99%, Lag= 7.4 min Primary 0.16 cfs @ 0.23 hrs, Volume= 0.037 af Secondary = 0.00 cfs @ 0.00 hrs. Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs Peak Elev= 5,856.80' @ 0.23 hrs Surf.Area= 0.163 ac Storage= 0.270 af Plug-Flow detention time= 89.0 min calculated for 0.036 af (13% of inflow) Center-of-Mass det. time= 85.1 min (91.5 - 6.4)

Invert Avail.Storage Storage Description

1 5,855.00' 1.164 af Custom Stage Data (Prismatic) Listed below

| Elevation (feet) | Surf.Area (acres) | Inc.Store (acre-feet) | Cum.Store (acre-feet) |
|---------------------|-------------------|-----------------------|-----------------------|
| 5,855.00 | 0.124 | 0.000 | 0.000 |
| 5,856.00 | 0.145 | 0.134 | 0.134 |
| 5,858.00 | 0.191 | 0.336 | 0.470 |
| 5,860.00 | 0.239 | 0.430 | 0.900 |
| 5,861.00 | 0.289 | 0.264 | 1 164 |

| # | Routing | Invert | Outlet Devices |
|---|----------|-------------|--|
| 1 | Primary | 5,852.50' | 8.8" x 38.0' long OUTLET W/ RESTRICTOR PLATE |
| | | | RCP, square edge headwall, Ke= 0.500 |
| | | | Outlet Invert= 5,851.67' S= 0.0218 '/' n= 0.013 Cc= 0.900 |
| 2 | Device 1 | 5,855.00' | 1.7" Vert. WQ ORIFICE C= 0.600 |
| 3 | Device 1 | 5,856.10 | 1.7" Vert. WQ ORIFICE C= 0.600 |
| 4 | Device 1 | 5,857.16' | 1.7" Vert. WQ ORIFICE C= 0.600 |
| 5 | Device 1 | | 2.92' x 2.92' Horiz. CDOT TYPE C INLET W/ MESH GRATE |
| | | | Limited to weir flow C= 0.600 |
| 6 | Secondar | y 5,860.50' | 12.0' long x 6.0' breadth EMERGENCY OVERFLOW |
| | | | Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 |
| | | | 3.00 3.50 4.00 4.50 5.00 5.50 |
| | | | Coef. (English) 2.37 2.51 2.70 2.68 2.68 2.67 2.65 2.65 2.65 2.65 2.66 |
| | | | 2.66 2.67 2.69 2.72 2.76 2.83 |

Primary OutFlow Max=0.16 cfs @ 0.23 hrs HW=5,856.80' (Free Discharge)
1=OUTLET W/ RESTRICTOR PLATE (Passes 0.16 cfs of 3.91 cfs potential flow)

2=WQ ORIFICE (Orifice Controls 0.10 cfs @ 6.3 fps)

3=WQ ORIFICE (Orifice Controls 0.06 cfs @ 3.8 fps)

-4=WQ ORIFICE (Controls 0.00 cfs)

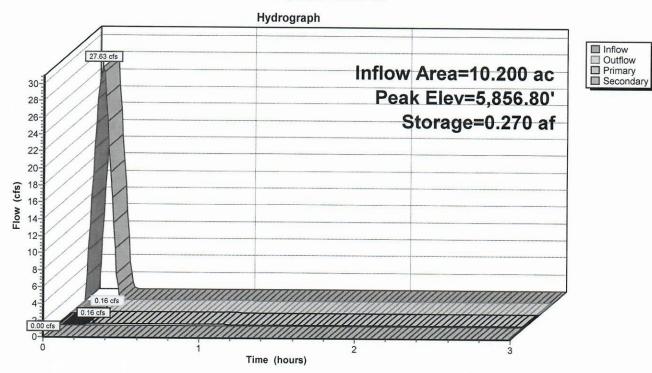
-5=CDOT TYPE C INLET W/ MESH GRATE (Controls 0.00 cfs)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=5,855.00' (Free Discharge) 6=EMERGENCY OVERFLOW (Controls 0.00 cfs)

Page 2 11/6/2019

Prepared by WestWorks Engineering
HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

Pond POND B:



Prepared by WestWorks Engineering

Page 1

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Pond POND B:

Inflow Area = 10.200 ac, Inflow Depth = 0.63" for 100-Year event Inflow 54.15 cfs @ 0.11 hrs, Volume= 0.536 af Outflow = 0.32 cfs @ 0.23 hrs, Volume= 0.074 af, Atten= 99%, Lag= 7.4 min Primary = 0.32 cfs @ 0.23 hrs, Volume= 0.074 af Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs
Peak Elev= 5,858.29' @ 0.23 hrs Surf.Area= 0.198 ac Storage= 0.532 af
Plug-Flow detention time= 89.6 min calculated for 0.074 af (14% of inflow)
Center-of-Mass det. time= 85.4 min (91.8 - 6.4)

| #_ | Invert | Avail.Storage | Storage Description |
|----|-----------|---------------|--|
| 1 | 5,855.00' | 1.164 af | Custom Stage Data (Prismatic) Listed below |

| Elevation (feet) | Surf.Area (acres) | Inc.Store (acre-feet) | Cum.Store (acre-feet) |
|---------------------|-------------------|-----------------------|-----------------------|
| 5,855.00 | 0.124 | 0.000 | 0.000 |
| 5,856.00 | 0.145 | 0.134 | 0.134 |
| 5,858.00 | 0.191 | 0.336 | 0.470 |
| 5,860.00 | 0.239 | 0.430 | 0.900 |
| 5,861.00 | 0.289 | 0.264 | 1.164 |

| # | Routing | Invert | Outlet Devices |
|---|----------|-------------|--|
| 1 | Primary | 5,852.50' | 8.8" x 38.0' long OUTLET W/ RESTRICTOR PLATE |
| | | | RCP, square edge headwall, Ke= 0.500 |
| | | | Outlet Invert= 5,851.67' S= 0.0218 '/' n= 0.013 Cc= 0.900 |
| 2 | Device 1 | 5,855.00' | 1.7" Vert. WQ ORIFICE C= 0.600 |
| 3 | Device 1 | 5,856.10' | 1.7" Vert. WQ ORIFICE C= 0.600 |
| 4 | Device 1 | 5,857.16' | 1.7" Vert. WQ ORIFICE C= 0.600 |
| 5 | Device 1 | 5,858.90' | 2.92' x 2.92' Horiz. CDOT TYPE C INLET W/ MESH GRATE |
| | | | Limited to weir flow C= 0.600 |
| 6 | Secondar | y 5,860.50' | 12.0' long x 6.0' breadth EMERGENCY OVERFLOW |
| | | | Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 |
| | | | 3.00 3.50 4.00 4.50 5.00 5.50 |
| | | | Coef. (English) 2.37 2.51 2.70 2.68 2.68 2.67 2.65 2.65 2.65 2.65 2.66 |
| | | | 2.66 2.67 2.69 2.72 2.76 2.83 |

Primary OutFlow Max=0.32 cfs @ 0.23 hrs HW=5,858.29' (Free Discharge)
1=OUTLET W/ RESTRICTOR PLATE (Passes 0.32 cfs of 4.52 cfs potential flow)

—2=WQ ORIFICE (Orifice Controls 0.14 cfs @ 8.6 fps) —3=WQ ORIFICE (Orifice Controls 0.11 cfs @ 7.0 fps)

-4=WQ ORIFICE (Orifice Controls 0.08 cfs @ 4.9 fps)

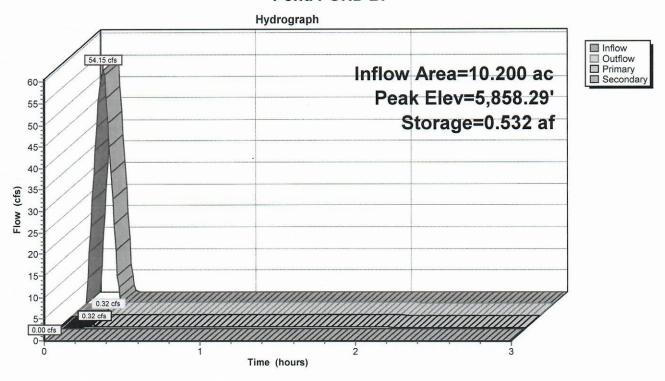
-5=CDOT TYPE C INLET W/ MESH GRATE (Controls 0.00 cfs)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=5,855.00' (Free Discharge) 6=EMERGENCY OVERFLOW (Controls 0.00 cfs)

Page 2 11/6/2019

Prepared by WestWorks Engineering
HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

Pond POND B:



User Defined

User Defined

User Defined

User Defined

Stormwater Facility Name: ELDORADO SPRINGS - POND A

Facility Location & Jurisdiction: EL PASO COUNTY

User Input: Watershed Characteristics

| Watershed Slope = | 0.070 | ft/ft |
|---|------------|---------|
| Watershed Length = | 840 | ft |
| Watershed Area = | 6.10 | acres |
| Watershed Imperviousness = | 52.5% | percent |
| Percentage Hydrologic Soil Group A = | 90.0% | percent |
| Percentage Hydrologic Soil Group B = | 0.0% | percent |
| Percentage Hydrologic Soil Groups C/D = | 10.0% | percent |
| Location for 1-hr Rainfall Depths (us | e dropdowr | 1): |

Location for 1-hr Rainfall Depths (use dropdown):

User Input

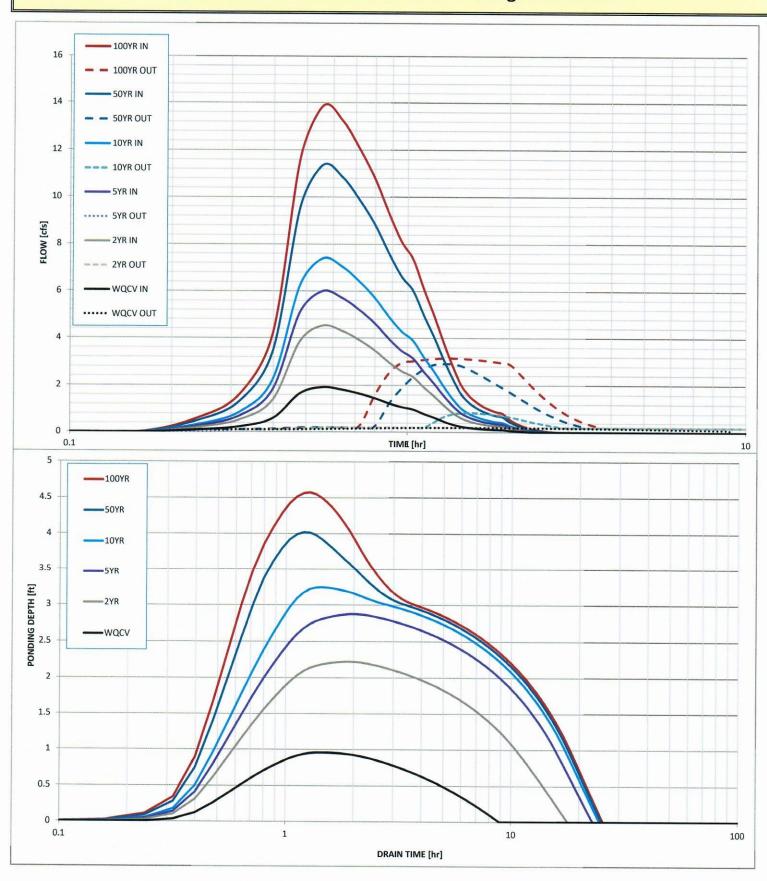
WQCV Treatment Method = Extended Detention

Stage [ft] Area [ft^2] Stage [ft] Discharge [cfs] 0.00 3,230 0.00 0.10 0.20 1.00 4,490 1.00 3.00 0.20 3.00 5,950 4.00 7,070 4.00 2.90 4.70 7,800 4.70 3.20

After completing and printing this worksheet to a pdf, go to: https://maperture.digitaldataservices.com/gvh/?viewer=cswdif create a new stormwater facility, and attach the pdf of this worksheet to that record.

Routed Hydrograph Results

| _ <u>_</u> | outeu nyuro | graph results | | | | | |
|--------------------------------------|-------------|---------------|--------|---------|---------|----------|---------|
| Design Storm Return Period = | WQCV | 2 Year | 5 Year | 10 Year | 50 Year | 100 Year | |
| One-Hour Rainfall Depth = | 0.53 | 1.19 | 1.50 | 1.75 | 2.25 | 2.52 | in |
| Calculated Runoff Volume = | 0.108 | 0.259 | 0.344 | 0.425 | 0.656 | 0.802 | acre-ft |
| OPTIONAL Override Runoff Volume = | | | | | | | acre-ft |
| Inflow Hydrograph Volume = | 0.108 | 0.258 | 0.344 | 0.424 | 0.656 | 0.802 | acre-ft |
| Time to Drain 97% of Inflow Volume = | 8.5 | 17.0 | 21.9 | 23.2 | 23.1 | 23.1 | hours |
| Time to Drain 99% of Inflow Volume = | 8.8 | 17.6 | 22.6 | 24.2 | 24.5 | 24.7 | hours |
| Maximum Ponding Depth = | 0.96 | 2.22 | 2.88 | 3.25 | 4.02 | 4.57 | ft |
| Maximum Ponded Area = | 0.10 | 0.12 | 0.13 | 0.14 | 0.16 | 0.18 | acres |
| Maximum Volume Stored = | 0.084 | 0.227 | 0.311 | 0.362 | 0.481 | 0.574 | acre-ft |
| | | | | | | | |



Stormwater Facility Name: ELDORADO SPRINGS - POND B

Facility Location & Jurisdiction: EL PASO COUNTY

User Input: Watershed Characteristics

| Watershed Slope = | 0.060 | ft/ft |
|---|------------|-----------|
| Watershed Length = | 840 | ft |
| Watershed Area = | 10.20 | acres |
| Watershed Imperviousness = | 53.9% | percent |
| Percentage Hydrologic Soil Group A = | 100.0% | percent |
| Percentage Hydrologic Soil Group B = | 0.0% | percent |
| Percentage Hydrologic Soil Groups C/D = | 0.0% | percent |
| Location for 1-hr Rainfall Depths (us | e dropdown | <u>):</u> |

User Input

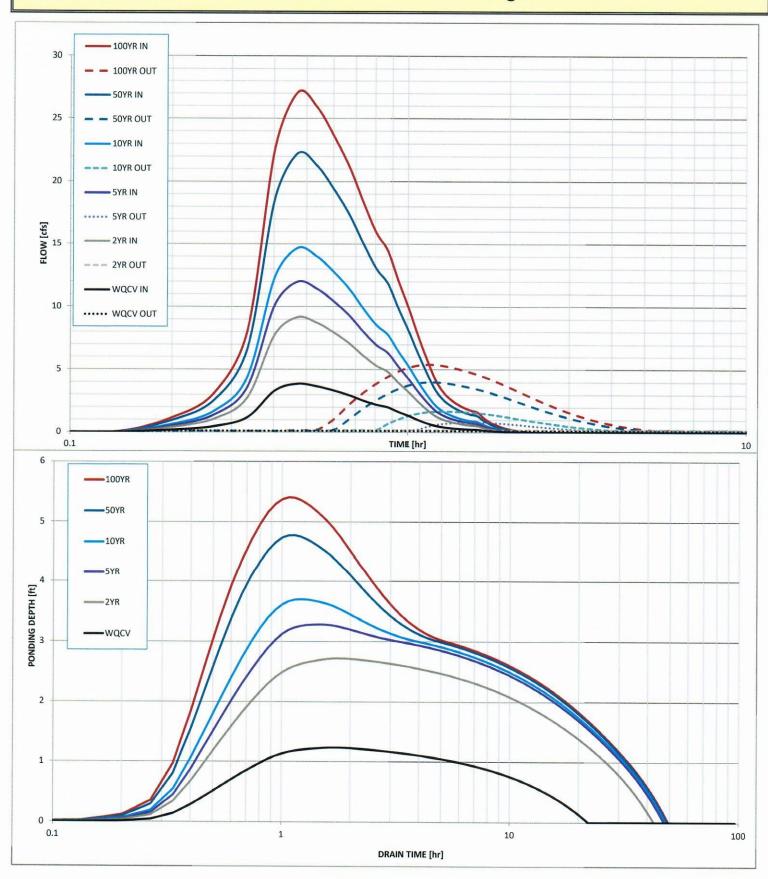
WQCV Treatment Method = Extended Detention

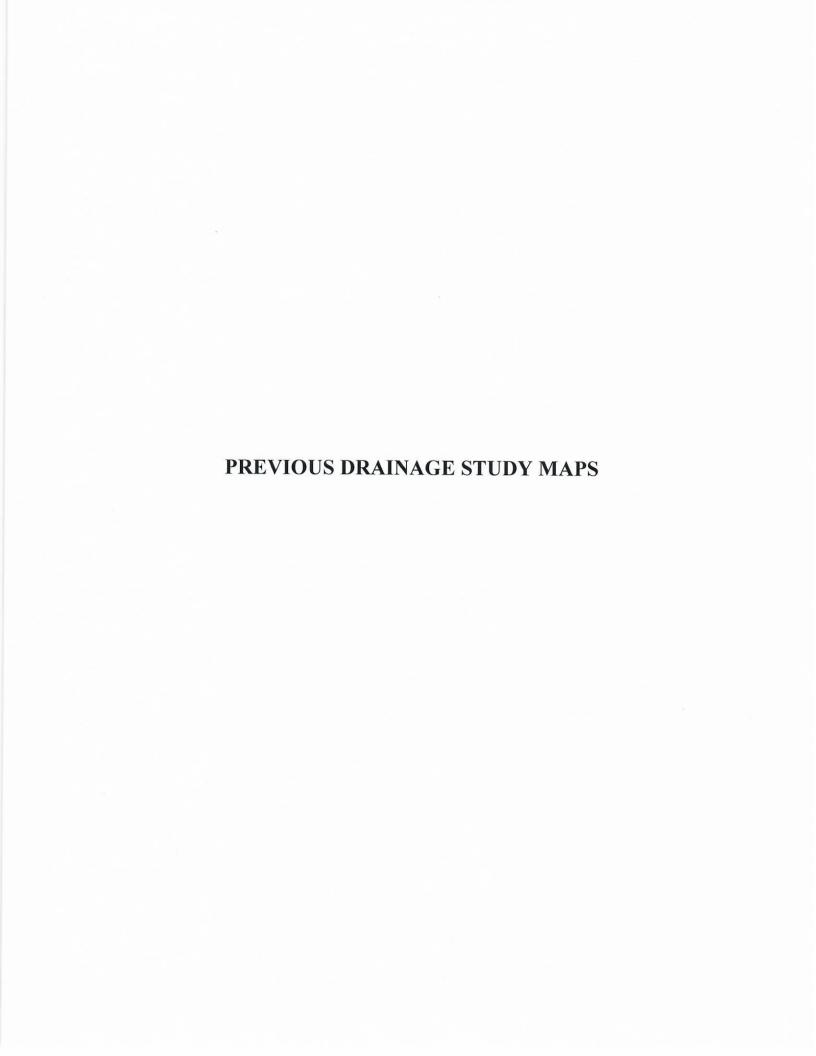
User Defined User Defined User Defined User Defined Stage [ft] Area [ft^2] Stage [ft] Discharge [cfs] 0.00 5,400 0.00 0.10 1.00 6,320 1.00 0.10 3.00 8,320 3.00 0.20 5.00 10,410 5.00 4.50 5.50 11,100 5.50 5.60 7.00 12,570 7.00 10.00

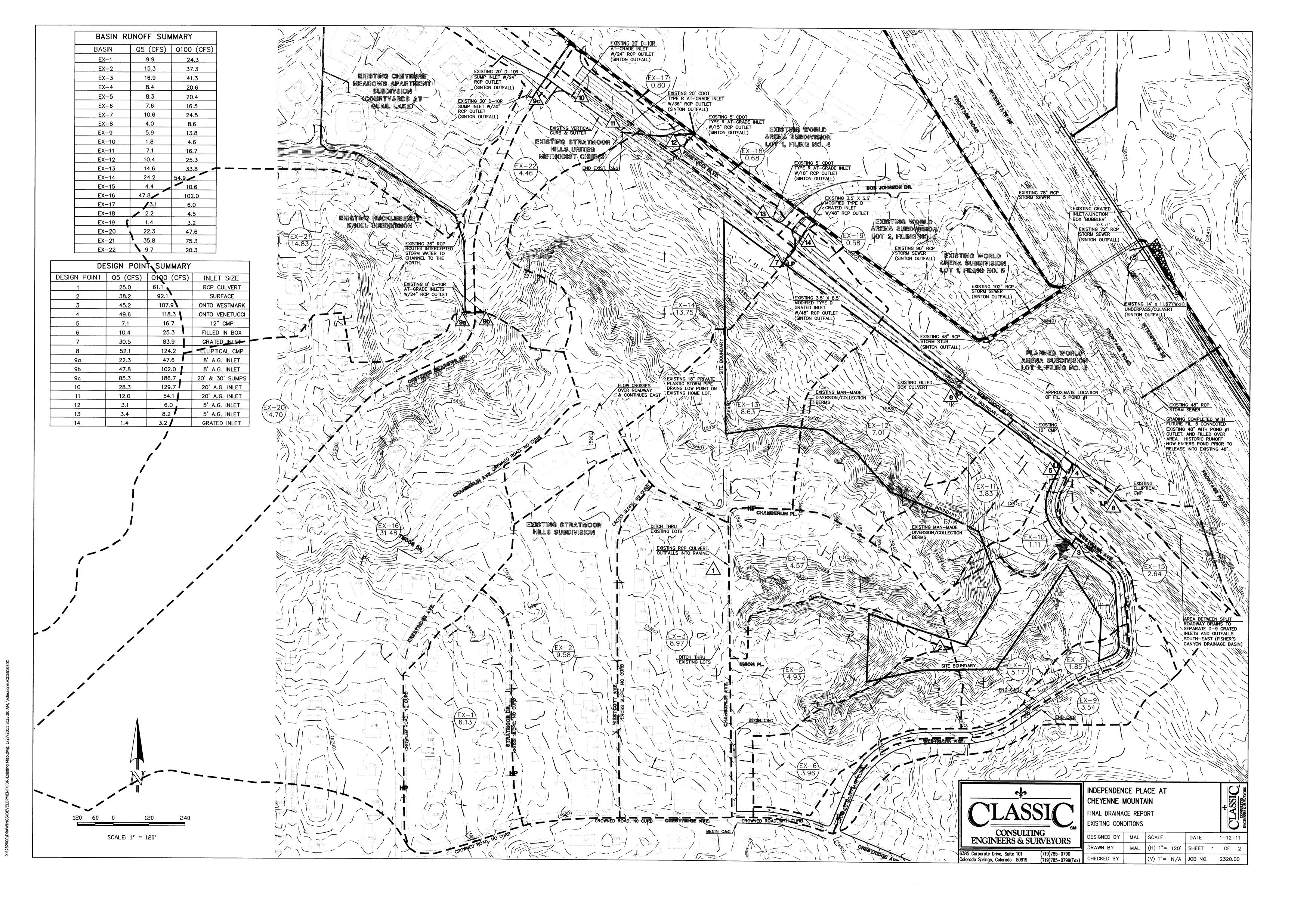
After completing and printing this worksheet to a pdf, go to: https://maperture.digitaldataservices.com/gvh/?viewer=cswdif create a new stormwater facility, and attach the pdf of this worksheet to that record.

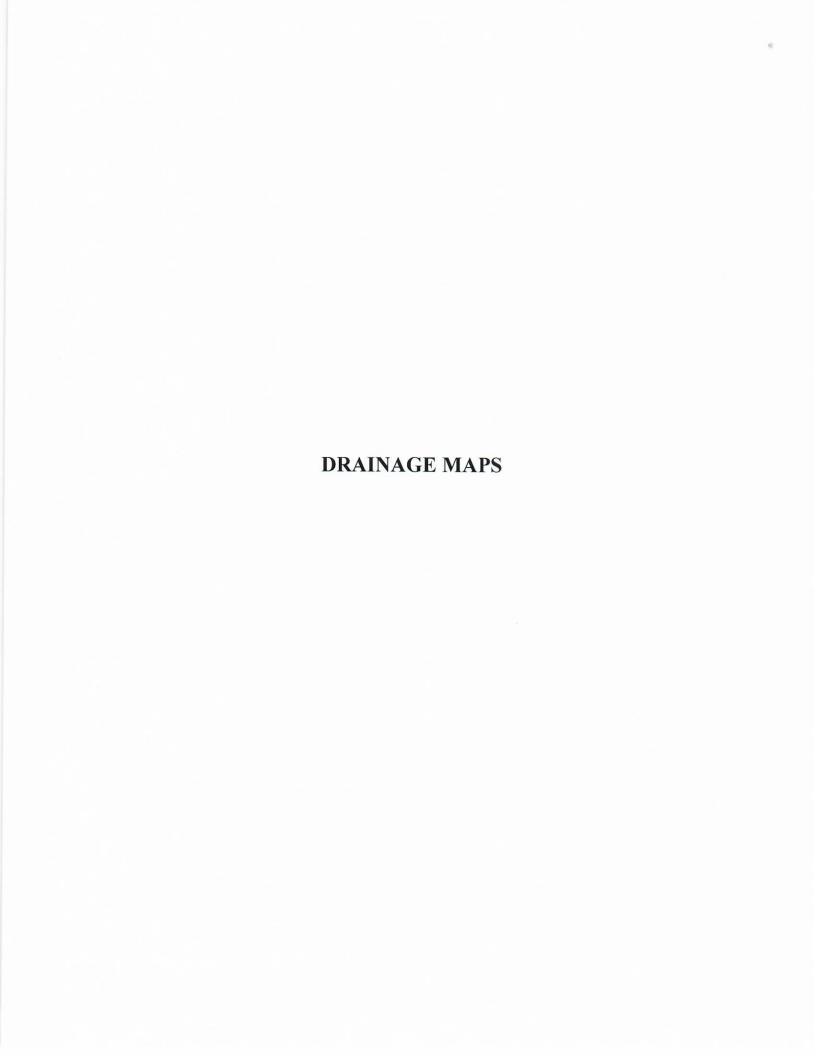
Routed Hydrograph Results

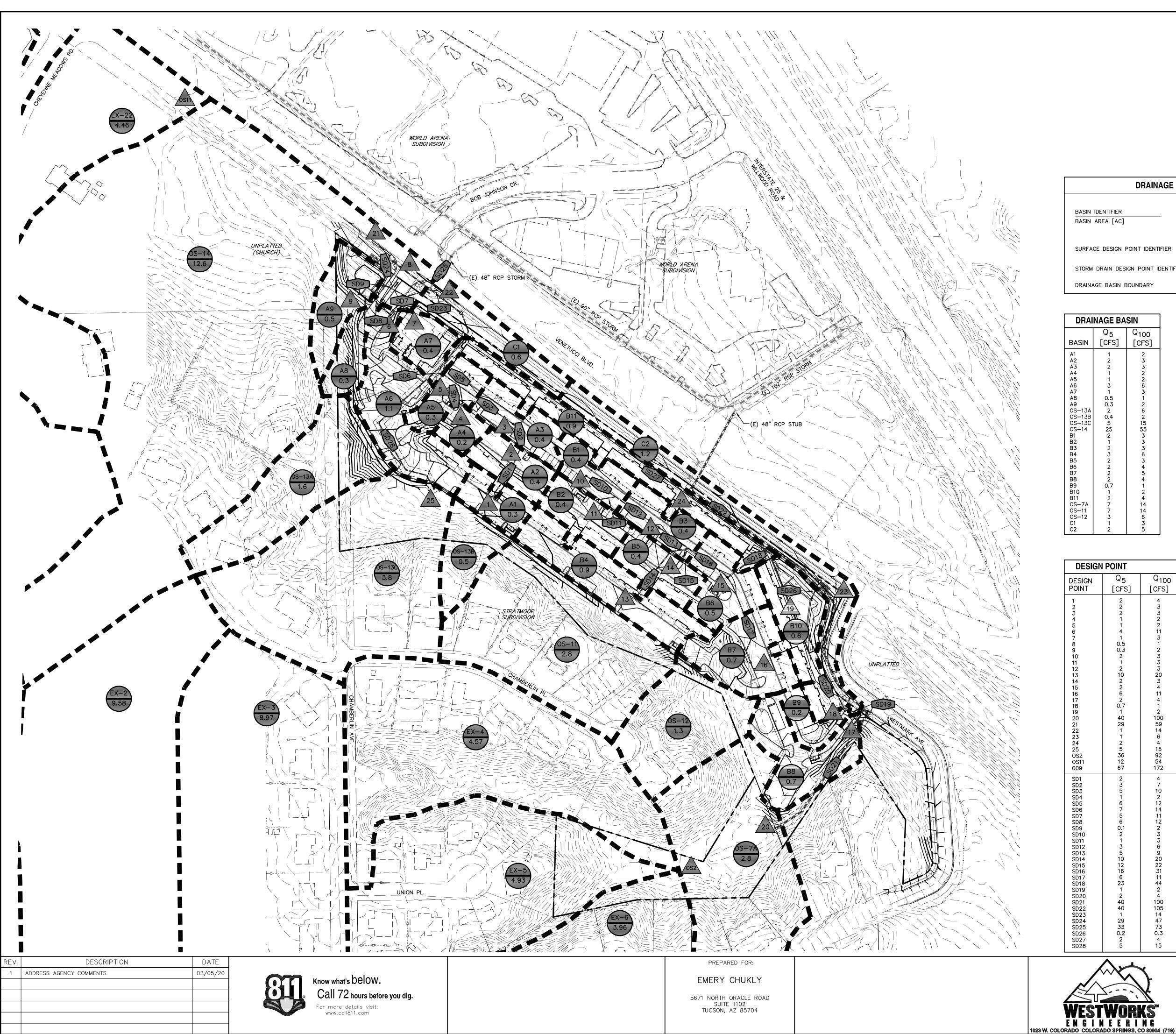
| | outed Hydro | graph Results | | | | | |
|--------------------------------------|-------------|---------------|--------|---------|---------|----------|---------|
| Design Storm Return Period = | WQCV | 2 Year | 5 Year | 10 Year | 50 Year | 100 Year | |
| One-Hour Rainfall Depth = | 0.53 | 1.19 | 1.50 | 1.75 | 2.25 | 2.52 | in |
| Calculated Runoff Volume = | 0.185 | 0.443 | 0.581 | 0.713 | 1.085 | 1.324 | acre-ft |
| OPTIONAL Override Runoff Volume = | | | | | | | acre-ft |
| Inflow Hydrograph Volume = | 0.184 | 0.442 | 0.580 | 0.712 | 1.084 | 1.323 | acre-ft |
| Time to Drain 97% of Inflow Volume = | 21.5 | 41.2 | 45.3 | 45.5 | 45.1 | 44.6 | hours |
| Time to Drain 99% of Inflow Volume = | 21.9 | 42.2 | 46.7 | 47.2 | 47.7 | 47.7 | hours |
| Maximum Ponding Depth = | 1.23 | 2.72 | 3.28 | 3.70 | 4.78 | 5.41 | ft |
| Maximum Ponded Area = | 0.15 | 0.18 | 0.20 | 0.21 | 0.23 | 0.25 | acres |
| Maximum Volume Stored = | 0.169 | 0.417 | 0.525 | 0.609 | 0.846 | 1.000 | acre-ft |











<u>LEGEND</u> EXISTING PROPOSED FUTURE C&G CURB AND GUTTER EASEMENT ESMT RIGHT-OF-WAY BOUNDARY RIGHT-OF-WAY LOT LINE EASEMENT (E) CONTOUR, INDEX (E) CONTOUR (P) CONTOUR, INDEX (P) CONTOUR (E) STORM SEWER, INLET, MH

DRAINAGE LEGEND

BASIN IDENTIFIER BASIN AREA [AC]

STORM DRAIN DESIGN POINT IDENTIFIER

DRAINAGE BASIN BOUNDARY

| DUAI | Dhainage Basin | | | |
|---|--|---------------------------|--|--|
| BASIN | Q ₅ [CFS] | Q ₁₀₀ [CFS] | | |
| A1 A2 A3 A4 A5 A6 A7 A8 A9 OS-13A OS-13B OS-13C OS-14 B1 B2 B3 B4 B5 B6 B7 B8 B9 B10 B11 | 1 2 2 1 1 3 1 0.5 0.4 5 2 5 2 2 2 2 2 2 2 2 2 7 1 2 7 1 2 7 1 7 | 2332263126215533363454124 | | |

| FSD EDB WQ POND A | | | | |
|---------------------|-----------------|-------------------|-------|--|
| DESCRIPTION | 5 _{YR} | 100 _{YR} | UNITS | |
| INFLOW (*1) | 12 | 25 | [CFS] | |
| OUTFLOW | 0.1 | 2 | [CFS] | |
| WATER SURFACE ELEV. | 5,860.8 | 5,862.4 | [FT] | |
| OVERFLOW WEIR ELEV. | 5,863.7 | 5,863.7 | [FT] | |
| STORAGE VOLUME | 0.18 | 0.39 | [AF] | |

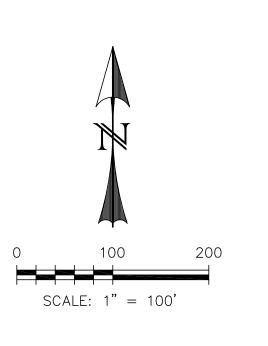
(P) STORM SEWER, INLET, MH

*1 - INFLOW AREA = 10.2 AC

| FSD EDB WQ POND B | | | | |
|---------------------|-----------------|-------------------|-------|--|
| DESCRIPTION | 5 _{YR} | 100 _{YR} | UNITS | |
| INFLOW (*2) | 28 | 54 | [CFS] | |
| OUTFLOW | 0.2 | 0.3 | [CFS] | |
| WATER SURFACE ELEV. | 5,856.8 | 5,858.3 | [FT] | |
| OVERFLOW WEIR ELEV. | 5,860.5 | 5,860.5 | [FT] | |
| STORAGE VOLUME | 0.27 | 0.53 | [AF] | |

*2 - INFLOW AREA = 6.1 AC

| DESIGN POINT | | | |
|---|--|--|--|
| DESIGN POINT | Q ₅ [CFS] | Q ₁₀₀ [CFS] | DESCRIPTION |
| 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 OS2 OS2 OS9 | 2 2 2 1 1 4 1 0.5 0.3 2 1 2 10 2 2 6 2 0.7 1 40 29 1 1 2 5 36 12 67 | 4 3 3 2 2 11 3 1 2 3 3 3 3 20 3 4 11 4 1 2 100 59 14 6 4 15 9 9 17 9 17 9 17 9 17 9 17 9 17 9 17 | (P) 5' TYPE R CURB INLET IN SUMP [PRIVATE] (P) 5' TYPE R CURB INLET IN SUMP [PRIVATE] (P) CDOT TYPE C GRATE INLET IN SUMP [PRIVATE] (P) 5' TYPE R CURB INLET IN SUMP [PRIVATE] (P) 5' TYPE R CURB INLET IN SUMP [PRIVATE] (P) 15' TYPE R CURB INLET AT GRADE [PRIVATE] (P) AREA AND LANDSCAPE DRAINS [PRIVATE] (P) AREA AND LANDSCAPE DRAINS [PRIVATE] (P) 5' TYPE R CURB INLET AT GRADE [PRIVATE] SHEET FLOW INTO POND A (P) CDOT TYPE C GRATE INLET IN SUMP [PRIVATE] (P) 5' TYPE R CURB INLET IN SUMP [PRIVATE] (P) CDOT TYPE C GRATE INLET IN SUMP [PRIVATE] (P) 20' TYPE R CURB INLET IN SUMP [PRIVATE] (P) 5' TYPE R CURB INLET IN SUMP [PRIVATE] (P) 10' TYPE R CURB INLET IN SUMP [PRIVATE] (P) 10' TYPE R CURB INLET AT GRADE [PRIVATE] (P) 5' TYPE R CURB INLET AT GRADE [PRIVATE] (P) 5' TYPE R CURB INLET AT GRADE [PRIVATE] (P) 5' TYPE R CURB INLET AT GRADE [PUBLIC] (P) 15' TYPE R CURB INLET IN SUMP [PUBLIC] (P) 15' TYPE R CURB INLET IN SUMP [PUBLIC] (P) 15' TYPE R CURB INLET IN SUMP [PUBLIC] (P) SERIES OF LANDSCAPE DRAINS (P) CDOT TYPE C GRATE INLET IN SUMP [PRIVATE] (E) FLOW IN DRAINAGE WAY (E) FLOW-BY FROM MULTIPLE INLETS (P) TOTAL FLOW TO HISTORIC BOX CULVERT UNDER VENETUCCI |
| SD1 SD2 SD3 SD4 SD5 SD6 SD7 SD8 SD9 SD10 SD11 SD12 SD13 SD14 SD15 SD16 SD17 SD18 SD19 SD20 SD21 SD20 SD21 SD22 SD23 SD24 SD25 SD26 SD27 SD28 | 2 35 1 67 5 6 0.1 2 1 3 5 10 12 16 6 23 1 2 40 40 1 2 3 3 0.2 2 5 | 4 7 10 2 12 14 11 12 2 3 6 9 20 22 31 11 44 2 4 100 105 14 47 73 0.3 4 15 | (P) 18" RCP STORM DRAIN [PRIVATE] (P) 24" RCP STORM DRAIN [PRIVATE] (P) 24" RCP STORM DRAIN [PRIVATE] (P) 18" RCP STORM DRAIN [PRIVATE] (P) 24" RCP STORM DRAIN [PRIVATE] (P) 18" RCP STORM DRAIN [PRIVATE] (P) 48" RCP STORM DRAIN [PRIVATE] (P) 48" RCP STORM DRAIN [PUBLIC] (P) 48" RCP STORM DRAIN [PUBLIC] (P) 36" RCP STORM DRAIN [PUBLIC] (P) 36" RCP STORM DRAIN [PUBLIC] (P) 18" RCP STORM DRAIN [PUBLIC] (P) 18" RCP STORM DRAIN [PUBLIC] (P) 18" RCP STORM DRAIN [PRIVATE] (P) 12" HDPE STORM DRAIN [PRIVATE] (P) 12" HDPE STORM DRAIN [PRIVATE] |



| ELDORADO SPRINGS | | DRAWN BY: CDK |
|-----------------------------------|----------------|---------------|
| | SCALE: 1"=100' | DATE: 02/05/2 |
| | JOB NUMBER | SHEET |
| DRAINAGE MAP DEVELOPED CONDITIONS | 91807 | 1 OF 1 |



Engineering Review

EPC Planning & Community Development Department

PPR-19-032

November 5, 2019

Prepared for:

Emery Chukly 5671 North Oracle Road Suite 1102 Tucson, AZ 85704

WestWorks Job #91807



November 5, 2019

Prepared for:

Emery Chukly 5671 North Oracle Road Suite 1102 Tucson, AZ 85704

Duplicate Page.

WestWorks Job #91807

| Engineer's Statement: The attached drainage plan and report were prepared correct to the best of my knowledge and belief. Said the criteria established by the City/County for draina with the master plan of the drainage basin. I accept r negligent acts, errors, or omissions on my part in prepared | drainage report has been prepared according age reports and said report is in conformity exponsibility for any liability caused by any |
|--|--|
| Chad D. Kuzbek, Colorado PE #35751 | Date |
| For and on behalf of WestWorks Engineering | Date |
| | |
| Developer's Statement: I, the developer have read and will comply with all or report and plan. | f the requirements specified in this drainage |
| | 1 |
| Business Name | |
| By: | |
| Title: | |
| Address: | |
| | |
| | |
| El Paso County, Colorado: Filed in accordance with requirements of the Drainage County Engineering Criteria Manual, and Land Develo | Criteria Manual Volumes 1 and 2, El Paso opment Code, as amended. |

Jennifer Irvine, P.E.
County Engineer/ECM Administrator

Date

Conditions:

Engineer's Statement:

For the City Engineer

Conditions:

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the established criteria for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.

Certification Statement "This report and plan for the final drainage design of Eldorado Springs was prepared by me (or under my direct supervision) in accordance with the provisions of the City of Colorado Springs Drainage Criteria Manual Volumes 1 & 2 Drainage Design and Technical Criteria for the owners thereof. I understand that the City Colorado Springs does not and will not assume liability for drainage facilities designed by others." SIGNATURE: (affix seal) Registered Professional Engineer State of Colorado No. 35751 **Developer's Statement** I, the developer have read and will comply with all of the requirements specified in this drainage report and plan. "ESH Development, LLC hereby certifies that the drainage facilities for Eldorado Springs shall be constructed according to the design presented in this report. I understand that the City Colorado Springs does not and will not assume liability for the drainage facilities designed and/or certified by my engineer and that the City of Colorado Springs reviews drainage plans pursuant to Colorado Revised Statutes, Title 30, Article 28; but cannot, on behalf of Eldorado Springs, guarantee that final drainage design review will absolve ESH Development, LLC and/or their successors and/or assigns of future liability for improper design. I further understand that approval of the final plat does not imply approval of my engineer's drainage design." Name of Developer Authorized Signature City of Colorado Springs Only: Filed in accordance with Section 7.7.906 of the Code of the City of Colorado Springs, 2001, as amended.

Date

TABLE OF CONTENTS

| Page 1 |
|---------|
| Page 1 |
| Page 1 |
| Page 1 |
| Page 10 |
| Page 13 |
| Page 14 |
| Page 14 |
| Page 14 |
| Page 14 |
| Page 15 |
| Page 15 |
| Page 16 |
| Page 16 |
| |

APPENDIX

Vicinity Map Soils Map Floodplain Map Hydrologic Calculations (5-YR and 100-YR) Hydraulic Calculations Stormwater Facility Calculations Previous Drainage Study Maps Drainage Map

PURPOSE

The purpose of this final drainage report (FDR) is to identify specific solutions to drainage problems on site and off-site resulting from the development and platting of this subdivision.

GENERAL LOCATION AND DESCRIPTION

Eldorado Springs includes 15.5 acres located in a portion of the southwest corner of Section 33, Township 14 South and in the northwest corner of Section 4, Township 15 South, Range 66 West of the 6th P.M. in El Paso County, Colorado. More specifically, the site is located near the southeast corner of Venetucci Boulevard and Bob Johnson Drive, south of the World Arena facility. The site is bounded by unplatted land to the east and west, single family residential Stratmoor Subdivision to the south, and Venetucci Boulevard to the north.

The site is currently undeveloped and drains from south to north over moderate slopes. Proposed development includes a multi-family apartment complex. Existing soils in the study area consist mostly of Schamber-Razor complex (SCS Map Unit Symbol 82 - Hydrologic Soil Group A) with a small portion being Nunn Clay loam (SCS Map Unit Symbol 59 - Hydrologic Soil Group C). The site is located in the Stratton Drainage Basin.

DRAINAGE BASINS AND SUB-BASINS

The site has been part of multiple drainage studies. Most recently, the site was previously studied in the, "Final Drainage Report for Independence Place at Cheyenne Mountain Filing No. 1," prepared by Classic Consulting Engineers & Surveyors, dated 1/27/2011. The existing conditions drainage map and description is taken directly from this previous study and quoted below:

"Existing Drainage Characteristics:

The site is located within the Stratton Drainage Basin. This site was originally studied as a part of the "Master Drainage Plan Harrison Street — 1-25 Vicinity Cheyenne Mountain Ranch," by Hartzell — Pfeiffenberger and Associates, Inc. dated November 15, 1973. Since then the site was included in additional basin analysis reports; "Stratton and Fischer's Canyon Drainage Basin Planning Study, Draft Hydraulic Analysis," by Muller Engineering Co. dated May 31, 1990; the "Master Drainage Report for Cheyenne Mountain Center and Final Drainage Report for Cheyenne Mountain Center Filing No. 1 and Cheyenne Meadows Road," by Drexel Barrell, dated October 1985; the "Hydrology Report Stratton Drainage Basin Outfall Study," by Drexel Barrell, dated June 1994; and the "Preliminary and Final Drainage Report and Plan for World Arena Subdivision No. 1," by Obering, Wurth & Associates, August 1994 revised March 1995.

The most recent master study drainage report for this area that included the proposed site was the "Hydrology Report Stratton Drainage Basin Outfall Study El Paso County, Colorado," by Drexel Barrell, dated June 9, 1994. This Hydrology Report by Drexel Barrell conforms to current El Paso County criteria and was performed based on minor modifications and revisions to TR-20 data prepared in the 1990 study by Muller Engineering Co. This Hydrology Report also updated the hydrologic modeling completed in the 1985 study by Drexel Barrell with the correct 2 hour and 24 hour storms that are utilized in the current criteria. This report provides the basis for the proposed site's allowable release rate since it sized and described the 90"/102" RCP storm outfall system (Sinton Outfall). This system runs parallel with the eastern site boundary, along the opposite site of Venetucci Blvd. A Drainage Map from the Drexel Barrell Hydrology Study is included in the appendix of this report for reference.

The proposed 15.46 acre site is included within Basin 009 of this previous study. At the time of the Drexel Barrell Hydrology Study, existing box culverts conveyed the runoff from Basin 009 under Venetucci Blvd./Old Hwy 85-87 to the existing 14' x 11.7' box culvert crossing under Interstate 25 and to the east into Fountain Creek. The development of Cheyenne Mountain Center constructed the 'Sinton Outfall' RCP storm sewer system that accepts the allowable release rates of the upstream parcels and conveys them along the historic drainage pattern of under I-25 and into the Sinton Channel, which connects to Fountain Creek. This large storm system consists of 102" RCP and 90" RCP storm main, with appropriate sized storm laterals to account for the flows quantified within the Drexel Barrell Hydrology Report. Basin 009 of this previous report consists of 0.147 square miles (94.08 acres) and was modeled using a CN value of 81 (SCS Method since entire study area was over 100 acres). Per the Drainage Criteria Manual Vol. 1 Table 5-5 a CN of 81 is equivalent to 1/3 acre home lots with all Group C soils, or about 1/6 acre home lots with all Group B soils. The existing Stratmoor Hills subdivision is also located within this Basin 009, with homes slightly over 2 lots per acre; and since these homes are within Group B soils, a more accurate CN value for the existing development would be around 71. Therefore, the remaining area of Basin 009 (the proposed Independence Place at Cheyenne Mountain Filing No. 1 site) is allowed to be substantially higher density than the calculated CN of 81. Also, runoff from Basin 008 of the previous report overflows the existing curb storm inlets and a portion drains onto the Venetucci Blvd. right-of-way within the Basin 009 area. Thus the actual total release from the developed site can be higher than the assumed Basin 009 flows $(O_{100} = 270 \text{ cfs}, 24 \text{ hour duration storm event}).$

When the World Arena was constructed to the immediate north of the proposed site, street improvements were made to Venetucci Blvd. that expanded the existing storm sewer facilities constructed with the Sinton Outfall main (Drexel Barrell Report). Many curb inlets were placed along the improved roadways at the Cheyenne Meadows Road intersection and Bob Johnson Drive intersection. Using the "Preliminary and Final Drainage Report and Plan for World Arena Subdivision No. 1," by Obering, Wurth & Associates, August 1994 revised March 1995 and the "Roadway Improvement Package and Storm Sewer Package for US Highway 85187 (Venetucci Boulevard)," by Drexel Barrell including the as-built revisions; these storm modifications have been incorporated into this report and construction drawings

for the proposed development. The following will describe the existing runoff quantities and existing facilities in more detail at each of the existing design points.

Design Point 1 ($Q_5 = 25.0$ cfs, $Q_{100} = 61.1$ cfs) consists of flows from Basins EX-1, EX-2, and EX-3 all of which are within the existing Stratmoor Hills subdivision to the south-west of the proposed site. Basin EX-1 is 6.13 acres of existing home lots that drains to the east, overtops Stratmoor Drive and into Basin EX-2. The combined flows from EX-1 & EX-2 continue on the surface to the east and overtop Westcott Ave. drain into Basin EX-3. Roadside ditches along Chamberlin Ave. route all of the runoff from the three basins to DP-1, where an existing concrete storm pipe collects the water and routes it under Chamberlin Ave. and into the ravine to the east, within Basin EX-4. Although the density of the existing Stratmoor Hills subdivision is closer to 2 DU/Ac., C values corresponding with 3 DU/Ac. are used to conservatively estimate the runoff from the upstream basins ($C_5 = 0.40$, $C_{100} = 0.55$, Group B soils).

Design Point 2 ($Q_5 = 38.2$ cfs, $Q_{100} = 92.1$ cfs) consists of flows from DP-1 and Basins EX-4, EX-5, and EX-6. Basin EX-4 is 4.57 acres (B soils) of existing home lots that drains to the south into the outfall ravine from DP-1. Basin EX-5 is 4.93 acres (C soils) of existing roadway and home lots that drains into one of two ravines that meet at DP-2. Basin EX-6 is 3.96 acres (C soils) of existing home lots that drains to the north-east to DP-2. C soils were used throughout EX-5 & EX-6 to calculate the storm runoff higher and therefore more conservatively. See soils map in Appendix for separation of B and C soil groups. All of the runoff from these basins combine at this confluence point and continue north-east onto the proposed site and toward DP-3.

Design Point 3 (Q_5 = 45.2 cfs, Q_{100} = 107.9 cfs) consists of flows &om DP-2 and Basins EX-7 and EX-8. Slightly upstream and west of DP-3, manmade berms were constructed at some point in the past that prevents the runoff &om DP-2 &om continuing north to the existing culverts under Venetucci Blvd (as the Stratton Basin Hydrology Study anticipated). This man made berm instead routes the entire flow from DP-2 onto Westmark Ave. (DP-3) where the flow combines with the runoff &om Basins EX-7 & EX-8. This runoff continues north-east as surface flow on Westmark Ave. to DP-4. Documentation of why and when this berm, along with others located on the actual proposed site, does not exist as a drainage report for this existing Stratmoor Hills subdivision is not on file with E1 Paso County and there is no mention of diverting the flows with the Hydrology Report or any of the World Arena Subdivision drainage reports.

Design Point 4 ($Q_5 = 49.6$ cfs, $Q_{100} = 118.3$ cfs) consists of flows &om DP-3 and Basins EX-9 and EX-10. Basin EX-9 is 3.54 acres (C soils) of existing home lots and Westmark Ave. that drains down Westmark via curb and gutter and surface flow to the intersection of Venetucci Blvd. and Westmark Ave. (DP-4). Basin EX-10 is 1.11 acres (C soils) of on-site, undeveloped land that drains to this intersection and onto the roadway prior to the small culvert at DP-5. This combined runoff &om DP-4 flows onto Venetucci Blvd. and the adjacent roadside swale to Design Point 8.

Please call out the drainage structure in Westmark Avenue and indicate it adequacy.



? There is no drainage structure in Westmark. **Design Point 5** (Q_5 = 7.1 cfs, Q_{100} = 16.7 cfs) consists of runoff &om Basin EX-11, 3.83 acres (C soils) of mostly on-site, undeveloped land with a small portion of existing Stratmoor Hills homes and a portion of the western half of existing Venetucci Blvd. This runoff sheet flows to an existing 12" CMP storm pipe culvert that routes the runoff under Venetucci Blvd. and continues in the existing drainage pattern towards Interstate 25. This runoff combines with that from DP-8 and continues around the future World Arena Subd. Lot 2, Fil. 5 site to the existing 48" RCP I-25 crossing. The final drainage report for this World Arena parcel does not acknowledge or quantify the off-site tributary flows.

Design Point 6 ($Q_5 = 10.4$ cfs, $Q_{100} = 25.3$ cfs) consists of runoff &om Basin EX-12, 7.01 acres (C soils) of mostly on-site, undeveloped land with a small portion of existing Stratmoor Hills homes and a portion of the western half of existing Venetucci Blvd. This runoff sheet flows to this existing low point at DP-6. Previous reports drainage documents show an existing box culvert at this location that routes any runoff at this point under Venetucci Blvd. and directly toward the I-25 box culvert (Sinton Outfall). However, this box culvert has since been covered, or filled, with soil and is no longer functioning. Documentation on why this was done cannot be found on file with El Paso County. The Sinton Outfall storm system shown on the Drainage Map does provide a 48" RCP stub off the junction box that points directly to the DP-6 and this filled in box culvert. It is our understanding that this 48" stub was meant to connect to this low-point at DP-6, which would then leave the existing box culvert not needed. A field inspection of the manhole does indeed show only a capped 48" lateral toward DP-6, and it appears this runoff simply infiltrates into the ground at this location.

Design Point 7 ($Q_5 = 30.5$ cfs, $Q_{100} = 83.9$ cfs) consists of runoff from Basins EX-13 & EX-14 and the flow by from DP-11. Basin EX-13 is 8.63 acres (C soils) of mostly on-site, undeveloped land, a portion of the western half of Venetucci Blvd. and a small portion of existing Stratmoor Hills homes. Basin EX-14 is 13.75 acres that consists of mostly undeveloped land and a small portion of the existing homes as well as a portion of the adjacent Stratmoor Hills United Methodist Church and the western half of Venetucci Blvd. A substantial amount of runoff at this point ($Q_5 = 3.1$ cfs, $Q_{100} = 21.2$ cfs) comes from the water not intercepted by the inlets at Design Points 9 - 11. The existing curb along the west side of Venetucci Blvd. from the Cheyenne Meadows Rd. intersection ends just after the inlet at DP-11, thus the flow by drains into the roadside ditch to DP-7. The combined runoff is intercepted by an existing CDOT Type D storm inlet (3.5' x 8.5' inlet dimensions). This inlet was installed with the construction of the Sinton Outfall Storm System and an existing 48" RCP storm pipe conveys the intercepted runoff across Venetucci Blvd. and connects to the 90" main.

Design Point 8 ($Q_5 = 52.1$ cfs, $Q_{100} = 124.2$ cfs) consists of flows from DP-4 and Basin EX-15. Basin EX-15 is 2.64 acres (C soils) of off-site, undeveloped land, including a portion of existing Venetucci Blvd. An existing elliptical CMP culvert conveys this runoff under Venetucci Blvd. to the north and into the existing drainage pattern. This culvert is very under-sized for 120+ cfs and it can be assumed that significant ponding takes place at this location prior to flowing to the downstream facilities. The parcel to the north of DP-8 (across Venetucci Blvd.) is planned to be a hotel with surrounding parking. The development

of the site will maintain the historic drainage pattern around the future development, but does change the overall outfall of the existing runoff. This World Arena Lot 2, Filing No. 5 (hotel site) construction was stopped after overlot grading and utility infrastructure was completed. Per the "Final Drainage Report for World Arena Subdivision Filing No. 5, Lot #2," by Matrix Design Group, Inc. (April 2008) the construction of Detention Pond #1 was to be outside of the existing drainage path to the existing 48" RCP under I-25. However, a site visit confirmed that the outlet pipe for this Pond 1 has been connected to the existing 48" interstate crossing and the existing low point (entry into the 48") has been filled in. Now, the existing drainage ponds approximately 2.0' and overtops into Pond #1, where a D-9 grate inlet within the pond intercepts the flows and passes them into the existing culvert.

Design Point 9a $(Q_5 = 22.3 \text{ cfs}, Q_{100} = 47.6 \text{ cfs})$ consists of runoff from Basin EX-20, 14.70 acres of existing single family subdivision and Cheyenne Meadows Road. An existing 8' D-10R at-grade curb inlet (4.5% street slope) intercepts a portion of this runoff $(Q_5 = 5.7 \text{ cfs}, Q_5 = 5.9 \text{ cfs})$, while the rest continues down Cheyenne Meadows Rd. to the intersection with Venetucci Blvd.

Design Point 9b ($Q_5 = 47.8 \text{ cfs}$, $Q_{100} = 102.0 \text{ cfs}$) consists of runoff from Basin EX-16, 31.48 acres of existing single family subdivision and Cheyenne Meadows Road. An existing 8' D-10R at-grade curb inlet (4.5% street slope) intercepts a portion of this runoff ($Q_5 = 5.9 \text{ cfs}$, $Q_5 = 12.7 \text{ cfs}$), while the rest continues down Cheyenne Meadows Rd. to the intersection with Venetucci Blvd. The combined intercepted runoff from DP-9a & DP-9b is routed in an existing 36" RCP storm pipe to the north to an existing channel, away from the Venetucci Blvd. and Cheyenne Meadows Rd. intersection. The large amount of flow-by ($Q_5 = 41.9 \text{ cfs}$, $Q_{100} = 89.3 \text{ cfs}$) continues to the submerged inlets at DP-9c.

Design Point 9c ($Q_5 = 85.3$ cfs, $Q_{100} = 186.7$ cfs) consists of runoff from Basins EX-21 and EX-22, as well as the flow by from DP-9a & DP-9b. Basin EX-21 is 14.83 acres of the existing single family Huckleberry Knoll Subdivision and Cheyenne Meadows Rd. Basin EX-22 is 4.46 acres of existing Stratmoor Hills Subdivision, existing Stratmoor Hills United Methodist Church, and existing Cheyenne Meadows Rd. Two existing D10-R curb inlets (20' & 30') exist on Cheyenne Meadows, west of Venetucci Blvd. The storm water at this point overtops the crown of the Cheyenne Meadows and completely submerges the inlets, thus changing the calculation used in quantifying the intercepted flow (See Calculations in Appendix). The total area of opening of the two combined inlets is 33.5 square feet (50.0' x 0'67), and based upon field as-builts of the curb return, the inlets only have 0.35' of depth before overtopping south down Venetucci Blvd. This results in both inlets only intercepting 57 cfs of both 5 and 100 year flows. The flow by from these inlets next hits the inlet at DP-10.

Design Point 10 ($Q_5 = 28.3$ cfs, $Q_{100} = 129.7$ cfs) has a 20' at-grade D10-R curb inlet that intercepts a large portion of the flow-by from DP-9c. Venetucci Blvd. has a slope of 1.3% at this inlet based upon field as-builts of the constructed curb. This 20' inlet intercepts $Q_5 = 16.3$ cfs and $Q_{100} = 75.6$, while the remainder continues to the next existing inlet at DP-11.

Design Point 11 ($Q_5 = 12.0 \text{ cfs}$, $Q_{100} = 54.1 \text{ cfs}$) has a 20' at-grade CDOT Type R curb inlet that intercepts a portion of the remaining flow-by from DP-9c & DP-10. Venetucci Blvd. has a slope of 2.8% at this inlet based upon field as-builts of the constructed curb. This 20' inlet intercepts $Q_5 = 8.9 \text{ cfs}$ and $Q_{100} = 32.9 \text{ cfs}$ while the remainder continues south down Venetucci Blvd. The existing curb and gutter along Venetucci ends just downstream of DP-11, therefore the flow-by ($Q_5 = 3.1 \text{ cfs}$, $Q_{100} = 21.2 \text{ cfs}$) runs off the edge of asphalt and enters the roadside ditch, which drains to the grated inlet at DP-7.

Design Point 12 ($Q_5 = 3.1$ cfs, $Q_{100} = 6.0$ cfs) consists of runoff from Basin EX-17, 0.80 acres of existing Venetucci Blvd. and adjacent landscape area that drains to an existing 5' at-grade CDOT Type R curb inlet Based upon field as-builts Venetucci Blvd. has a slope of 3.0% at this inlet, resulting in intercepting $Q_5 = 1.9$ cfs and $Q_{100} = 2.3$, while the remainder continues within the curb to DP-13.

Design Point 13 ($Q_5 = 3.4$ cfs, $Q_{100} = 8.2$ cfs) consists of runoff from the flow-by of DP-12 and Basin EX-18, 0.68 acres of existing Venetucci Blvd. and adjacent landscape area that drains to an existing 5' at-grade CDOT Type R curb inlet. Based upon field as-builts Venetucci Blvd. has a slope of 0.7% at this inlet, resulting in intercepting $Q_5 = 2.2$ cfs and $Q_{100} = 3.5$ cfs. The non-intercepted runoff ($Q_5 = 1.2$ cfs, $Q_{100} = 4.7$ cfs) continues within the curb and gutter onto Bob Johnson Drive and west toward the overall basin outfall corridor.

Design Point 14 ($Q_5 = 1.4$ cfs, $Q_{100} = 3.2$ cfs) consists of runoff from Basin EX-19, 0.58 acres of existing Venetucci Blvd. and adjacent undeveloped right of way area. An existing modified Type D grated inlet drains this area and conveys the runoff into the 90" RCP Sinton Outfall system via a 48" RCP storm lateral. As mentioned previously, the existing alignments and storm facilities have been established through the "Roadway Improvement Package and Storm Sewer Package for US Highway 85/87 (Venetucci Boulevard)," by Drexel Barrell including the as-built revisions and field survey data.

Summary of Existing Conditions

The existing Sinton Outfall Storm system was planned to intercept all of the Stratton Basin runoff at rates specified within the "Hydrology Report Stratton Drainage Basin Outfall Study El Paso County, Colorado," by Drexel Barrell, dated June 9, 1994. The construction of the large storm main system appears to have been completed in two separate phases, per the "M.D.D.P. for Cheyenne Mountain Center." The second phase included extending storm sewer laterals off of the main alignment to our proposed site location in order to convey the existing runoff as well as a future allowable runoff rate per the Hydrology Study. This extension of a 48" storm lateral was completed at the northernmost existing roadway crossing (Design Point 7). However, at Design Point 6, no such storm sewer extension off the main line was completed and it appears that the existing roadway culvert was filled in and does not pass historic runoff under Venetucci Blvd./Old Hwy 85/87. The construction plans for the 102"-90" RCP storm main show a 48" RCP stub pointed toward the filled in box culvert, but capped 8.0' outside of the manhole. It is our assumption that this 48" stub is meant to convey the runoff at this DP-6 location. Therefore, our proposed conditions will discuss extending this lateral under Venetucci Blvd. and into our proposed site. Drainage reports completed for the immediate downstream World Arena Subdivisions do not discuss any

off-site flows from the tributary area, including our site and the upstream Stratmoor Hills Subdivision, or mention extending this 48" stub to the edge of the Venetucci Blvd. right-of-way. The Hydrology Report specifies a developable 100-year flow rate from the proposed site and upstream Stratmoor Hills Subdivision as 270 cfs. The calculated combined 100-year existing flow rate at design points 6, 7, and 8 is 198 cfs. Therefore, substantial more development can be constructed with this Basin 009 before storm water detention is required.

Also, the construction of the diversion berms on the proposed site that re-route the upstream tributary area (Stratmoor Hills) runoff directly to the Westmark Ave. and Venetucci Blvd. intersection are un-documented and seem to have been completed to eliminate the historic runoff to the 'filled in' culvert at DP-6. The existing CMP culverts at DP-5 and DP-8 are not adequately sized to convey all of the existing storm runoff that they currently receive. However, since it appears this drainage path is not natural and not per the previous drainage studies, we are proposing intercepting the upstream, existing runoff and conveying it through the proposed site's public storm system and directly to the 90"/102" RCP Sinton Outfall system."

Developed Drainage Characteristics:

Development of the site is a multi-family residential apartment complex with clubhouse, park space, pool and amenity areas, garages, paved parking and drive aisles, and landscaping. Development of this site also includes adjacent public roadway improvements along Venetucci Boulevard and a portion of Westmark Avenue.

Developed drainage overview:

On site runoff along with some off-site tributary runoff will be collected on site and routed into 2 private full-spectrum detention and stormwater quality facilities (Pond A and Pond B). A limited portion of the existing downstream drainage infrastructure has been adequately designed for developed runoff from this site (102" RCP). However, the existing 102" RCP combines with an existing 78"RCP and connects to an undersized existing 72" RCP. This scenario is believed through witness accounts to have caused flooding in the one-way road underpass under I-25. For this reason, Pond A and B will be full-spectrum detention facilities so as not to contribute excess runoff to this condition.

Details of Ponds A and B shall be included with the Site Construction Drawings. Details include dissipation basins, trickle channels, outfall structures, emergency overflows, and maintenance access.

Basins with designations of EX are taken directly from the existing conditions analysis. Basins with designations of OS are off-site basins. Basins with designations of A drain to Pond A. Basins with designations of B drain to Pond B. Basins with designations C do not drain to pond facility.

Developed Drainage Design Point Descriptions: **DP-25** [Q₅ = 5 CFS/Q₁₀₀ = 15 CFS]

DP-25 is a proposed CDOT Type C grated inlet in sump. DP-25 collects mostly off-site runoff from Basin OS-13C. Collected flows will by-pass Pond A and are routed via SD28 to SD25.

Design Point 1 (DP-1) $[Q_5 = 2 \text{ CFS/}Q_{100} = 4 \text{ CFS}]$

DP-1 is a proposed 5' wide Type R curb inlet in sump. DP-1 collects runoff from Basins OS-13B and A1. Collected flows are routed via storm drain design point SD1 to SD2.

DP-2 $[Q_5 = 2 \text{ CFS/}Q_{100} = 3 \text{ CFS}]$

DP-2 is a proposed 5' wide Type R curb inlet in sump. DP-1 collects runoff from Basin A2. Collected flows are routed via SD2 to SD3.

DP-3 $[Q_5 = 2 \text{ CFS/}Q_{100} = 3 \text{ CFS}]$

DP-3 is a proposed CDOT Type C grate inlet in sump. DP-3 collects runoff from Basin A3. Collected flows are routed via SD3 to SD4.

DP-4 $[Q_5 = 1 \text{ CFS/}Q_{100} = 2 \text{ CFS}]$

DP-4 is a proposed 5' wide Type R curb inlet in sump. DP-4 collects runoff from Basin A4. Collected flows are routed via SD4 to SD5.

DP-5 $[Q_5 = 1 \text{ CFS}/Q_{100} = 2 \text{ CFS}]$

DP-5 is a proposed 5' wide Type R curb inlet in sump. DP-5 collects runoff from Basin A5. Collected flows are routed via SD6 ($Q_5 = 7$ CFS/ $Q_{100} = 14$ CFS) into Pond A. The discharge point into Pond A shall have a concrete energy dissipater.

DP-6 $[Q_5 = 4 \text{ CFS/}Q_{100} = 11 \text{ CFS}]$

DP-6 is a proposed 15' wide Type R curb inlet at grade. DP-6 collects runoff from Basins OS-13A and A6. Collected flows are routed via SD7 to SD8. Flow-by of $Q_5 = 0$ CFS/ $Q_{100} = 1.5$ CFS will continue to DP-22.

DP-7 $[Q_5 = 1 \text{ CFS/}Q_{100} = 3 \text{ CFS}]$

DP-7 is a proposed system of landscape drains, pool deck grates, and roof drain collection for the clubhouse. DP-7 collects runoff from Basin A7. Collected flows are routed to the inlet at DP6.

DP-8 $[Q_5 = 0.5 \text{ CFS/}Q_{100} = 1 \text{ CFS}]$

DP-8 is a proposed 5' wide Type R curb inlet at grade. DP-8 collects runoff from Basin A8. Collected flows are routed via SD8 ($Q_5 = 6$ CFS/ $Q_{100} = 12$ CFS) into Pond A. The discharge point into Pond A shall have a concrete energy dissipater.

DP-9 $[Q_5 = 0.3 \text{ CFS/}Q_{100} = 2 \text{ CFS}]$

DP-9 represents the sheet flow into Pond A.

DP-10 $[Q_5 = 2 \text{ CFS/}Q_{100} = 3 \text{ CFS}]$

DP-10 is a proposed CDOT Type C grate inlet in sump. DP-10 collects runoff from Basin B1. Collected flows are routed via SD10 to SD12.

DP-11 $[Q_5 = 1 \text{ CFS/}Q_{100} = 3 \text{ CFS}]$

DP-11 is a proposed 5' wide Type R curb inlet in sump. DP-11 collects runoff from Basin B2. Collected flows are routed via SD11 to SD12.

DP-12 $[Q_5 = 2 \text{ CFS/}Q_{100} = 3 \text{ CFS}]$

DP-12 is a proposed CDOT Type C grate inlet in sump. DP-12 collects runoff from Basin B3. Collected flows are routed via SD13 to SD16.

DP-13 $[Q_5 = 10 \text{ CFS}/Q_{100} = 20 \text{ CFS}]$

DP-13 is a proposed 20' wide Type R curb inlet in sump. DP-13 collects runoff from Basins OS-11 and B4. Collected flows are routed via SD14 to SD15.

DP-14 $[Q_5 = 2 \text{ CFS/}Q_{100} = 3 \text{ CFS}]$

DP-14 is a proposed 5' wide Type R curb inlet in sump. DP-14 collects runoff from Basin B5. Collected flows are routed via SD16 to SD18.

DP-15 $[Q_5 = 2 \text{ CFS/}Q_{100} = 4 \text{ CFS}]$

DP-15 is a proposed CDOT Type C grate inlet in sump. DP-15 collects runoff from Basin B6. Collected flows are routed via SD18 ($Q_5 = 23$ CFS/ $Q_{100} = 44$ CFS) into Pond B. The discharge point into Pond B shall have a concrete energy dissipater.

DP-16 $[Q_5 = 6 \text{ CFS/}Q_{100} = 11 \text{ CFS}]$

DP-16 is a proposed 10' wide Type R curb inlet in sump. DP-16 collects runoff from Basins OS-12 and B7. Collected flows are routed via SD17 to SD18.

DP-24 $[Q_5 = 2 \text{ CFS/}Q_{100} = 4 \text{ CFS}]$

DP-24 represents a series of landscape drains running behind the buildings along Venetucci Blvd. These landscape drains are intended to collect runoff and roofdrains in Basin B11. Collected flows are routed via SD27 to Pond B.

DP-17 $[Q_5 = 2 \text{ CFS/}Q_{100} = 4 \text{ CFS}]$

DP-17 is a proposed 10' wide Type R curb inlet at grade. DP-17 collects runoff from Basin B8. Collected flows are routed via SD19 to SD20. Flow-by of $Q_5 = 0$ CFS/ $Q_{100} = 0.1$ CFS will continue into Westmark Avenue.

DP-18 $[Q_5 = 0.7 \text{ CFS/}Q_{100} = 1 \text{ CFS}]$

DP-18 is a proposed 5' wide Type R curb inlet at grade. DP-18 collects runoff from Basin B9. Collected flows are routed via SD20 ($Q_5 = 2$ CFS/ $Q_{100} = 4$ CFS) into Pond B. The discharge point into Pond B shall have a concrete energy dissipater. Flow-by of $Q_5 = 0$ CFS/ $Q_{100} = 0.1$ CFS will continue into Westmark Avenue.

DP-19 $[Q_5 = 1 \text{ CFS/}Q_{100} = 2 \text{ CFS}]$

DP-19 represents the sheet flow into Pond B.

DP-20 [$Q_5 = 40 \text{ CFS/}Q_{100} = 100 \text{ CFS}$]

DP-20 is a proposed 48" RCP culvert to pick up off-site flows tributary to the existing drainageway south of the site. The collected runoff is not routed through a Pond facility. Instead

it bypasses the site via SD21. Flows in SD21 are combined with the discharge from Pond B in SD22 ($Q_5 = 40~\text{CFS/Q}_{100} = 105~\text{CFS}$) will be routed under Venetucci Boulevard in a proposed 48" RCP storm tying to and existing 48" RCP stub that connects to an existing 102" RCP storm drain.

DP-21 $[Q_5 = 29 \text{ CFS/}Q_{100} = 59 \text{ CFS}]$

DP-21 is a proposed pair of 20' wide Type R curb inlets at grade. DP-21 collects runoff from Basin OS-14 and existing flow-by from DP-OS11. DP-OS11 is the last in a series of at-grade inlets in or near Cheyenne Meadows Road. Venetucci Boulevard does not have capacity to carry all of the existing runoff. Runoff to the inlets at DP-21 is modeled at maximum street capacity. Collected flows are routed via SD24 to SD25. Flow-by of $Q_5 = 0.2$ CFS/ $Q_{100} = 12$ CFS will continue to DP-22.

DP-22 $[Q_5 = 1 \text{ CFS/}Q_{100} = 14 \text{ CFS}]$

DP-22 is a proposed 15' wide Type R curb inlet in sump. DP-22 collects runoff from Basin C1 and flow-by from DP-6 and DP-21. Collected flows are routed via SD23 to SD25. Flows in SD25 ($Q_5 = 33 \text{ CFS/}Q_{100} = 73 \text{ CFS}$) are a combination of flows from SD9, SD23, and SD24. These combined storm pipes will tie to the existing CDOT Type D grate inlet in the roadside ditch near the site entrance. SD25 is an existing 48" RCP under Venetucci Boulevard connecting to the existing 90" RCP running along the north side of Venetucci Boulevard.

DP-23 $[Q_5 = 1 \text{ CFS/}Q_{100} = 6 \text{ CFS}]$

DP-23 is street flow in Venetucci Boulevard near the intersection with Westmark Avenue. This flow is less than the historic flow at existing conditions DP-5 ($Q_5 = 7 \text{ CFS/}Q_{100} = 17 \text{ CFS}$).

DP-009 $[Q_5 = 67 \text{ CFS/}Q_{100} = 172 \text{ CFS}]$

DP-009 represents the total flow from Basin 009 as referenced in the Drexel Barrell Report. The storm drain outfall infrastructure installed based on the Drexel Barrell Report anticipated flows of $Q_{100} = 270$ CFS. This means that the downstream infrastructure will not be additionally burdened by runoff from this site and even additional development in the Basin.

4-Step Process Discussion:

Step 1. Employ Runoff Reduction Practices.

The site layout was done to minimize paving and includes park and amenity areas. Site impervious area calculations are shown in the IRF spreadsheet in the Appendix.

Step 2. Implement BMPs That Provide WQCV with Slow Release.

Development of this site includes a full-spectrum detention facility providing WQCV and an outfall structure with a 40-hour drain time.

Step 3. Stabilize Drainageways.

There are no natural drainageways associated with this site. Drainage fees were be paid with the platting of this subdivision. These fees contribute to any necessary channel improvements within the major drainage basin.

Step 4. Implement Site Specific and Other Source Control BMPs.

There is no permanent outside storage associated with this site.

Summary:

The development of the Eldorado Springs apartment site accounts for up-stream off-site flows, on-site flows, and adjacent flows for a solution that can handle these flows and safely discharge them to adequately sized downstream stormwater infrastructure.

No more than one acre of your development site can

DRAINAGE DESIGN CRITERIA

flow off site without receiving SWQ treatment. Provide a statement here that demonstrates the amount of development area has been accounted for in the

This drainage report was prepared in accordance to the criteria established in the County Drainage Criteria Manual, updated in May 2014.

WestWorks Engineering uses the rational method for drainage basin study areas of less than 90 acres. This methodology is implemented in accordance with the County Drainage Criteria Manual Guidelines. Perimeter area that

drains off-site is

For the Rational Me 0.8-acres - 0.7-AC The average runoff of it is landscape Frequency curves at area and 0.1-AC is concentration for ov the main entrance. the County Drainage

Appendix of this rep

ited for the 5-year and 100-year recurrence intervals. are taken from Table 6-6 and the Intensity-Duration-5 of the County Drainage Criteria Manual. Time of drain or gutter flow are calculated per Section 3.2 of lculations for the Rational Method are shown in the is calculated in accordance with the County Drainage

Criteria Manual Guidelines.

DRAINAGE FACILITY DESIGN

All inlets, storm drains, culverts, and open channels are sized using the procedures outlined in the City Drainage Criteria Manual. All of the drainage systems, including the streets, are designed to safely route the 5-year and 100-year storm flows. Hydraulic grade line calculations for the proposed storm drain design will be included with the storm drain constructions drawings.

FLOODPLAIN STATEMENT

No portion of this site is within a F.E.M.A. designated floodplain per Flood Insurance Rate Map Community Panel No. 08041C0741 G, effective December 7, 2018.

EROSION CONTROL PLAN

The El Paso County Drainage Criteria Manual specifies that an Erosion Control Plan and associated cost estimate be submitted in conjunction with the Final Drainage Report. WestWorks Engineering respectfully requests the Erosion Control Plan be submitted in conjunction with the Overlot Grading Plan and construction assurances posted prior to obtaining a grading permit.

OPINION OF PROBABLE COST

Private Drainage Facilities (non-reimbursable):

| Item | Quantity | Unit Cost | Total Cost |
|------------------------|----------|-----------------|------------|
| 18" RCP Storm Drain | 1,549 LF | \$65/LF | \$100,425 |
| 24" RCP Storm Drain | 1,041 LF | \$78/LF | \$ 81,198 |
| 30" RCP Storm Drain | 376 LF | \$97/LF | \$ 36,472 |
| 5' Type R Inlet | 8 EA | \$4,000/EA | \$ 32,000 |
| 10' Type R Inlet | 2 EA | \$5,500/EA | \$ 11,000 |
| 15' Type R Inlet | 1 EA | \$8,000/EA | \$ 8,000 |
| 20' Type R Inlet | 1 EA | \$8,000/EA | \$ 8,000 |
| CDOT Type C Inlet | 5 EA | \$3,300/EA | \$ 16,500 |
| Storm Manhole | 8 EA | \$4,600/EA | \$ 36,800 |
| Pond Outfall Structure | 2 EA | \$7,500/EA | \$ 15,000 |
| Riprap | 33 CY | \$75/CY | \$ 2,475 |
| | | Sub-Total | \$347,870 |
| | | 20% Contingency | \$ 69,574 |
| | | TOTAL | \$417,444 |

Public Drainage Facilities (non-reimbursable):

| Item | Quantity | Unit Cost | Total Cost |
|------------------------|----------|-----------------|------------|
| 24" RCP Storm Drain | 20 LF | \$84/LF | \$ 1,680 |
| 30" RCP Storm Drain | 11 LF | \$94/LF | \$ 1,034 |
| 36" RCP Storm Drain | 146 LF | \$124/LF | \$ 18,104 |
| 48" RCP Storm Drain | 1,225 LF | \$178/LF | \$218,050 |
| 15' Type R Inlet | 1 EA | \$8,000/EA | \$ 8,000 |
| 20' Type R Inlet | 2 EA | \$8,000/EA | \$ 16,000 |
| Storm Manhole (Type 1) | 4 EA | \$8,600/EA | \$ 34,400 |
| | | Sub-Total | \$297,268 |
| | | 20% Contingency | \$ 59,454 |
| | | TOTAL | \$356,722 |

This opinion of probable cost is made on the basis of experience and qualifications and represents WestWorks Engineering's best judgment as an experienced and qualified professional firm, familiar with the construction industry. WestWorks Engineering cannot and will not guarantee that actual construction costs will not vary from this opinion of probable cost.

DRAINAGE FEES

The study area is in the Stratton Drainage Basin. The site has already been platted and drainage fees paid at that time.

REFERENCE LIST

"Soil Survey of El Paso County Area, Colorado," prepared by United States Department of Agriculture Soil Conservation Service, issued June 1981

"FIRM Flood Insurance Rate Map," prepared by Federal Emergency Management Agency, effective date March 17, 1997

El Paso County Drainage Criteria Manual, updated May 2014

"Master Drainage Plan Harrison Street- I-25 Vicinity Cheyenne Mountain Ranch", by Hartzell-Pfeiffenberger and Associates, Inc. dated November 15, 1973

"Stratton and Fischer's Canyon Drainage Basin Planning Study, Draft Hydraulic Analysis," by Muller Engineering Co. dated May 31, 1990

"Master Drainage Report for Cheyenne Mountain Center and Final Drainage Report for Cheyenne Mountain Center Filing No. 1 and Cheyenne Meadows Road," by Drexel Barrell, dated October 1985

"Hydrology Report Stratton Drainage Basin Outfall Study," by Drexel Barrell, dated June 1994

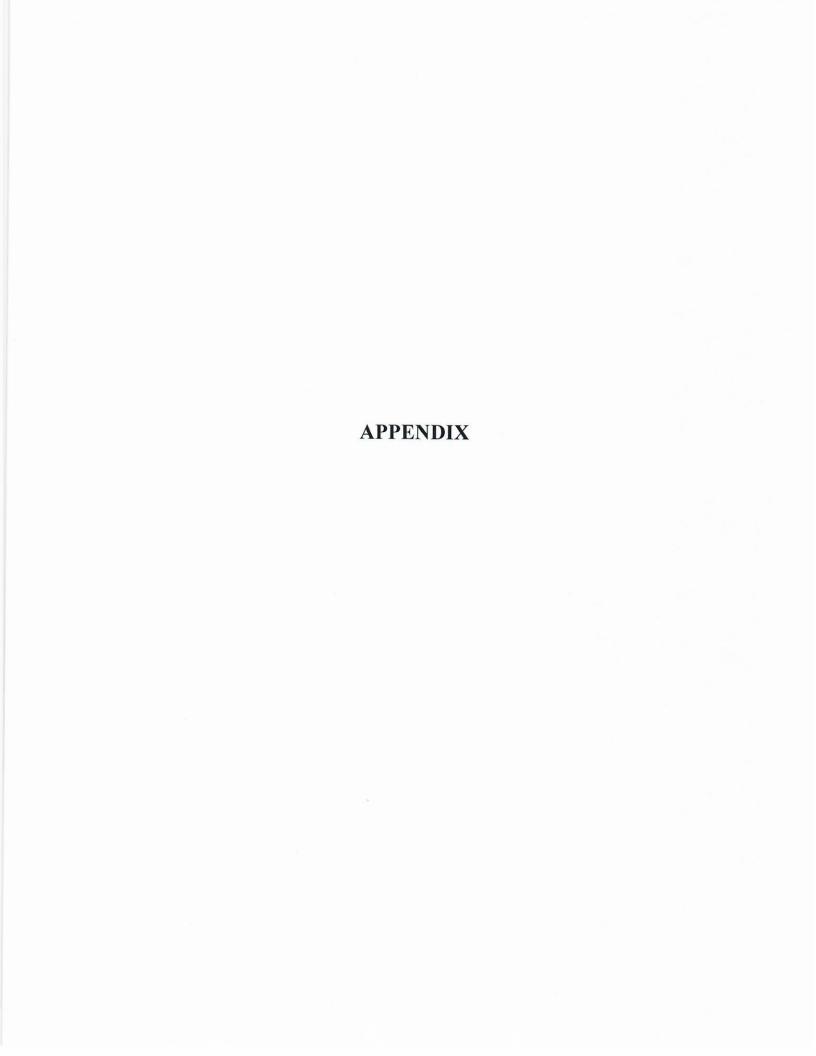
"Preliminary and Final Drainage Report and Plan for World Arena Subdivision No. 1," by Obering, Wurth & Associates, August 1994 revised March 1995

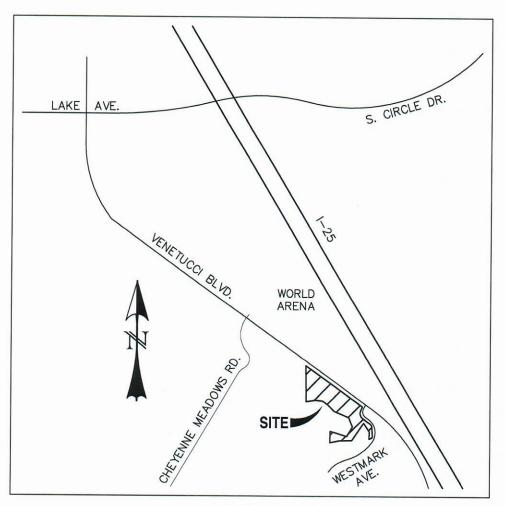
"Final Drainage Report for World Arena Subdivision Filing No. 5, Lot #2," by Matrix Design Group, Inc., April 2008

"Drainage Report for Huckleberry Knoll Subdivision," by Drexel Barrell & Company, dated June 15, 1983

"Roadway Improvement Package and Storm Sewer Package for US Highway 85/87 (Venetucci Boulevard)," by Drexel Barrell including the as-built revisions

"Final Drainage Report for Independence Place at Cheyenne Mountain Filing No. 1," prepared by Classic Consulting Engineers & Surveyors, dated 1/27/2011





VICINITY MAP SCALE: N.T.S.



Hydrologic Soil Group

| Map unit symbol | Map unit name | Rating | Acres in AOI | Percent of AOI |
|--------------------------|--|--------|--------------|----------------|
| 59 | Nunn clay loam, 0 to 3 percent slopes | С | 0.6 | 4.0% |
| 82 | Schamber-Razor complex, 8 to 50 percent slopes | Α | 14.7 | 96.0% |
| Totals for Area of Inter | rest | | 15.3 | 100.0% |

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

National Flood Hazard Layer FIRMette





Legend

SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT

With BFE or Depth Zone AE, AO, AH, VE, AR Without Base Flood Elevation (BFE) Regulatory Floodway SPECIAL FLOOD HAZARD AREAS

0.2% Annual Chance Flood Hazard, Area of 1% annual chance flood with average depth less than one foot or with drainage areas of less than one square mile zone Future Conditions 1% Annual Chance Flood Hazard Zone

Area with Reduced Flood Risk due to Levee. See Notes. Zone

Area with Flood Risk due to Levee Zone D

NO SCREEN Area of Minimal Flood Hazard Zone Effective LOMRs

Area of Undetermined Flood Hazard Zon

- - - Channel, Culvert, or Storm Sewer STRUCTURES | 1111111 Levee, Dike, or Floodwall GENERAL

Cross Sections with 1% Annual Chance Water Surface Elevation 17.5

Base Flood Elevation Line (BFE) Coastal Transect

Limit of Study

Coastal Transect Baseline Jurisdiction Boundary

Hydrographic Feature Profile Baseline

OTHER FEATURES

No Digital Data Available Digital Data Available

Unmapped

MAP PANELS

The pin displayed on the map is an approximate point selected by the user and does not represe an authoritative property location.

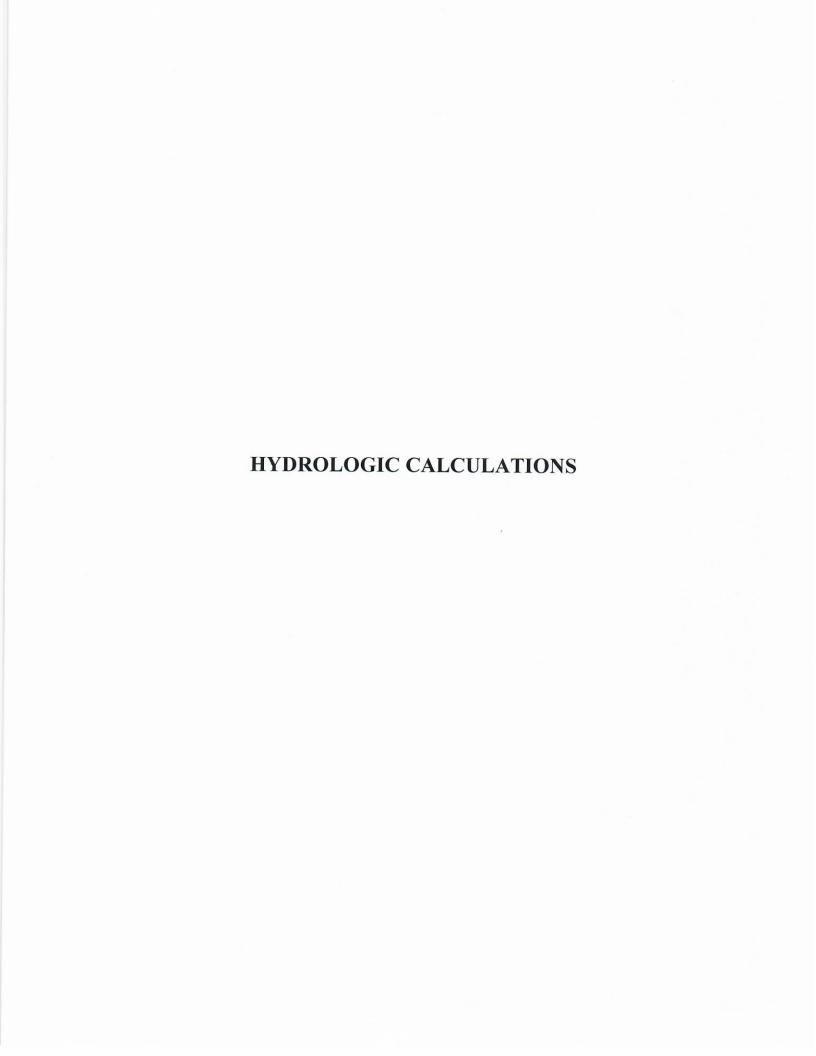
authoritative NFHL web services provided by FEMA. This map was exported on 5/24/2019 at 2:39:54 PM and does not The flood hazard information is derived directly from the This map complies with FEMA's standards for the use of The basemap shown complies with FEMA's basemap digital flood maps if it is not void as described below.

reflect changes or amendments subsequent to this date and

time. The NFHL and effective information may change or

become superseded by new data over time.

This map image is void if the one or more of the following map legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for elements do not appear: basemap imagery, flood zone labels, unmapped and unmodernized areas cannot be used for



Time of Concentration Calcuations

| Sub-Basin | Time Flowline | of Co L [ft.] | ncentrat H [ft.] | Time of Concentration, \mathbf{Tc} [min.] line $ L[ft.] H[ft.] v[ft/s] \mathbf{Tc} p$ | Time of Concentration, Tc [min.] Flowline L [ft.] V [ft/s] Tc [min.] | Sub-Basin | Time Flowline | of Col L[ft.] | ncentrat H [ft.] | Time of Concentration, \mathbf{Tc} [min.] line $ L$ [ft.] $ H$ [ft.] $ \mathbf{r}$ | Time of Concentration, Tc [min.] Flowline L [ft.] H [ft.] v [ft/s] Tc [min.] | Sub-Basin | Time of Concentration, Tc Flowline L fft.1 H fft.1 v fft/s1 | e of Co L [ft.] | ncentra H [ft.] | Time of Concentration, \mathbf{Tc} [min.] dine L [ft.] H [ft.] \mathbf{v} [ft/s] \mathbf{Tc} In | [min.] |
|-----------|------------------|------------------|---------------------|---|---|-----------|------------------|------------------|---------------------|--|---|-----------|--|--------------------|--------------------|---|--------|
| | overland | 1 | 1.0 | | 0.3 | | overland | 110 | 4.0 | | 10.8 | | overland | 10 | 0.5 | | 2.9 |
| AI | channel | 80 | 1.0 | 4 | 0.3 | <u>A6</u> | channel | 170 | 12.0 | 6 | 0.3 | <u>B1</u> | channel | 30 | 1.0 | 9 | 0.1 |
| | | | Tot | Total Tc = | 2 | | | | Toi | Total Tc = | 111 | | | | To | Total Tc = | S |
| | overland | 70 | 10.0 | | 5.5 | | overland | 30 | 2.0 | | 4.6 | | overland | 70 | 8.0 | | 5.9 |
| A2 | channel | 50 | 1.0 | 5 | 0.2 | <u>A7</u> | channel | 130 | 0.5 | 2 | 1.0 | <u>B2</u> | channel | 50 | 1.0 | 5 | 0.2 |
| | | | Tot | Total Tc = | 9 | | | | Tol | Total Tc = | 9 | | | | To | Total Tc = | 9 |
| | overland | 20 | 0.5 | | 5.2 | | overland | 140 | 42.0 | | 6.1 | | overland | 20 | 1.0 | | 4.2 |
| <u>A3</u> | channel | 09 | 9.0 | 4 | 0.3 | <u>A8</u> | channel | 120 | 4.0 | 9 | 0.3 | B3 | channel | 10 | 0.2 | S | 0.0 |
| | | | Tot | Total Tc = | 9 | | | | Tot | Total Tc = | 9 | | | | То | Total Tc = | w |
| | overland | 10 | 0.5 | | 2.9 | | overland | 250 | 48.0 | | 9.4 | | overland | 20 | 1.0 | | 4.2 |
| A4 | channel | 50 | 1.5 | 9 | 0.1 | <u>A9</u> | channel | - | 1.0 | 35 | 0.0 | B4 | channel | 160 | 2.0 | 4 | 0.7 |
| | | | Tot | Total Tc = | S | | | | Tot | Total Tc = | 6 | | | | Toi | Total Tc = | s, |
| | overland | 40 | 0.9 | | 4.1 | | overland | 1 | 1.0 | | 0.3 | | overland | 70 | 8.0 | | 5.9 |
| <u>A5</u> | channel | 06 | 2.0 | 5 | 0.3 | | channel | - | 1.0 | 35 | 0.0 | B5 | channel | 20 | 1.0 | 5 | 0.2 |
| | | | Tot | Total Tc = | S | | | | Tot | Total Tc = | S | | | | Tol | Total Tc = | 9 |



Project: Eldorado Springs

Job No.: 91807
Engineer: Chad Kuzbek, PE
Date: 5/24/2019

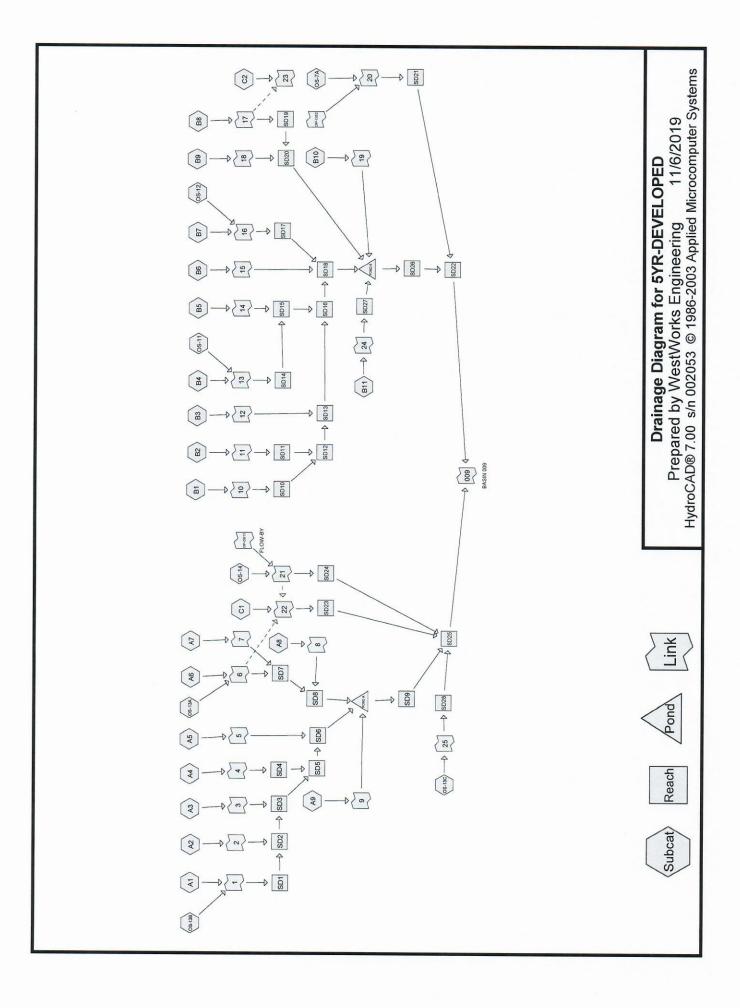
Time of Concentration Calcuations

| Flowline L [ft.] H [ft.] v [ft/s] Te min. Flowline L [ft.] H [ft.] v [ft/s] Te min. | Sub-Basin | Time | ofCon | centrati | Time of Concentration, Tc [min.] | | Sub-Basin | Time | of Con | centrat | Time of Concentration, Tc [min.] | min.] | Sub-Basin | Time | of Col | ncentrat | Time of Concentration, Tc [min.] | [min.] |
|--|-----------|----------|---------|----------|----------------------------------|-----------|-----------|----------|---------|---------|----------------------------------|-----------|-----------|-----------------------------------|---------|----------|----------------------------------|-----------|
| overland 20 1.0 4.2 overland 100 12.0 3 channel 30 0.5 5 0.1 CI channel 320 3.0 3 overland 50 8.0 4 5 CZ channel 630 8.0 4 overland 60 14.0 4.3 channel 1 1.0 35 channel 60 4.0 9 0.1 channel 1 1.0 35 overland 40 4.0 9 0.1 channel 1 1.0 35 channel 60 4.0 9 0.1 channel 1 1.0 35 channel 60 4.0 9 0.1 channel 1 1.0 35 channel 60 4.0 9 0.1 channel 1 1.0 35 channel 60 4.0 9 0.1 channel | | Flowline | C [ft.] | H [ft.] | v [ft/s] | Tc [min.] | | Flowline | L [ft.] | H [ft.] | | Tc [min.] | | Flowline L [ft.] H [ft.] v [ft/s] | L [ft.] | H [ft.] | v [ft/s] | Tc [min.] |
| channel 30 0.5 5 0.1 CI channel 320 3.0 3 overland 50 8.0 4.5 channel 630 8.0 4 channel 70 1.0 4 0.3 CZ channel 630 8.0 4 overland 60 14.0 4.3 channel 1 1.0 35 channel 60 4.0 9 0.1 channel 1 1.0 35 overland 40 4.0 9 0.1 channel 1 1.0 35 channel 60 4.0 9 0.1 channel 1 1.0 35 channel 60 4.0 9 0.1 channel 1 1.0 35 achannel 60 4.0 9 0.1 channel 1 1.0 35 channel 60 4.0 9 0.1 channel | | overland | 20 | 1.0 | | 4.2 | | overland | 100 | 12.0 | | 6.9 | | overland | - | 1.0 | | 0.3 |
| overland 50 8.0 4.5 overland 110 10.0 4 channel 70 1.0 4 0.3 C2 channel 630 8.0 4 overland 60 14.0 4.3 overland 1 1.0 35 channel 60 4.0 9 0.1 channel 1 1.0 35 channel 60 4.0 9 0.1 channel 1 1.0 35 channel 60 4.0 9 0.1 channel 1 1.0 35 channel 60 4.0 9 0.1 channel 1 1.0 35 rannel 60 4.0 9 0.1 channel 1 1.0 35 rannel 60 4.0 9 0.1 channel 1 1.0 35 | B6 | channel | 30 | 0.5 | 5 | 0.1 | IJ | channel | 320 | 3.0 | 3 | 1.6 | | channel | - | 1.0 | 35 | 0.0 |
| overland 50 8.0 4.5 overland 110 10.0 4 channel 70 1.0 4 0.3 CZ channel 630 8.0 4 overland 60 14.0 4.3 overland 1 1.0 35 channel 60 4.0 9 0.1 channel 1 1.0 35 channel 60 4.0 9 0.1 channel 1 1.0 35 channel 60 4.0 9 0.1 channel 1 1.0 35 channel 60 4.0 9 0.1 channel 1 1.0 35 | | | | Tot | | S | | | | Tot | al Tc = | 6 | | | | To | Total Tc = | S |
| channel 70 1.0 4 0.3 C2 channel 630 8.0 4 overland 60 14.0 4.3 overland 1 1.0 35 channel 60 4.0 9 0.1 channel 1 1.0 35 overland 40 4.0 9 0.1 1.0 35 channel 60 4.0 9 0.1 channel 1 1.0 35 channel 60 4.0 9 0.1 channel 1 1.0 35 rotalTc = 5 7 channel 1 1.0 35 | 5-112 | overland | 50 | 8.0 | | 4.5 | | overland | 110 | 10.0 | | 8.0 | | overland | _ | 1.0 | | 0.3 |
| overland 60 14.0 4.3 overland 1 1.0 35 channel 60 4.0 9 0.1 channel 1 1.0 35 overland 40 4.0 4.7 overland 1 1.0 35 channel 60 4.0 9 0.1 channel 1 1.0 35 channel 60 4.0 9 0.1 channel 1 1.0 35 Total Tc = 5 Total Tc = 7 Total Tc = | | channel | 70 | 1.0 | 4 | 0.3 | C7 | channel | 630 | 8.0 | 4 | 2.7 | | channel | - | 1.0 | 35 | 0.0 |
| overland channel 60 14.0 4.3 overland channel 1 1.0 35 channel 60 4.0 9 0.1 channel 1 1.0 35 channel 40 4.0 9 0.1 channel 1 1.0 35 channel 60 4.0 9 0.1 channel 1 1.0 35 Total Tc = 5 Total Tc = Total Tc = | | | | Tot | al Tc = | 2 | | | | Tot | al Tc = | 11 | | | | Toi | Total Tc = | S |
| channel 60 4.0 9 0.1 channel 1 1.0 35 overland 40 4.0 4.7 overland 1 1.0 35 channel 60 4.0 9 0.1 channel 1 1.0 35 Total Tc = 5 Total Tc = Total Tc = | | overland | 09 | 14.0 | | 4.3 | | overland | - | 1.0 | | 0.3 | | overland | - | 1.0 | | 0.3 |
| overland channel 40 4.0 9 0.1 channel 1 1.0 35 Total Tc = 5 Total Tc = 5 Total Tc = | | channel | 09 | 4.0 | 6 | 0.1 | | channel | - | 1.0 | 35 | 0.0 | | channel | 1 | 1.0 | 35 | 0.0 |
| overland 40 4.0 4.7 overland 1 1.0 35 channel 60 4.0 9 0.1 channel 1 1.0 35 Total Tc = Total Tc = | | | - | Tot | al Tc = | 2 | | | | Tot | al Tc = | S | | | | Tot | Total Tc = | 5 |
| channel 60 4.0 9 0.1 channel 1 1.0 35 Total Tc = Total Tc = | | overland | 40 | 4.0 | | 4.7 | | overland | - | 1.0 | | 0.3 | | overland | П | 1.0 | | 0.3 |
| 5 Total Tc = | | channel | 09 | 4.0 | 6 | 0.1 | | channel | - | 1.0 | 35 | 0.0 | | channel | 1 | 1.0 | 35 | 0.0 |
| | | | | Tot | al Tc = | v. | | | | Tot | al Tc = | 3 | | | | Tot | Total Tc = | S |
| overland 90 14.0 6.0 overland 20 2.0 3.3 | | overland | 06 | 14.0 | | 0.9 | | overland | 20 | 2.0 | | 3.3 | | overland | - | 1.0 | | 0.3 |
| $\overline{B10}$ channel 60 5.0 10 0.1 $\overline{B11}$ channel 30 1.0 6 $\overline{0.1}$ | | channel | 09 | 5.0 | 10 | 0.1 | B11 | channel | 30 | 1.0 | 9 | 0.1 | | channel | _ | 1.0 | 35 | 0.0 |
| Total $Tc = 6$ Total $Tc = 5$ | | | | Tota | al Tc = | 9 | | | | Tot | al Tc = | w | | | | Tot | Total Tc = | w |



Project: Eldorado Springs

Job No.: 91807
Engineer: Chad Kuzbek, PE
Date: 5/24/2019



El Paso County 5-Year Duration=5 min, Inten=5.17 in/hr

Prepared by WestWorks Engineering

Page 1

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Subcatchment A1:

Runoff

=

1.33 cfs @

0.08 hrs, Volume=

0.009 af, Depth= 0.38"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 5-Year Duration=5 min, Inten=5.17 in/hr

| Area (ac) | С | Description |
|-----------|------|-----------------|
| 0.100 | 0.73 | ROOFTOPS |
| 0.200 | 0.96 | PAVEMENT |
| 0.000 | 0.00 | |

0.300 0.88 Weighted Average

Tc Length (feet) (min)

Slope (ft/ft)

Velocity (cfs)

Capacity Description

(ft/sec) 5.0

Direct Entry,

Subcatchment A4:

Runoff

1.27 cfs @

0.08 hrs, Volume=

0.009 af, Depth= 0.36"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 5-Year Duration=5 min, Inten=5.17 in/hr

| _ | Area (ac) | C | Description |
|---|-----------------|------|-----------------|
| | 0.100 | 0.73 | ROOFTOP |
| _ | 0.200 | 0.90 | PAVEMENT |
| | 150 1 El 2010 V | | |

0.300 0.84 Weighted Average

Tc Length Slope (feet) (min) (ft/ft)

Velocity Capacity

Description (cfs)

(ft/sec)

5.0

Direct Entry,

Subcatchment A5:

Runoff

0.95 cfs @

0.08 hrs, Volume=

0.007 af, Depth= 0.27"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 5-Year Duration=5 min, Inten=5.17 in/hr

| Area (ac) | С | Description |
|-----------|------|-------------|
| 0.100 | 0.08 | LANDSCAPE |
| 0.200 | 0.90 | PAVEMENT |

0.300 0.63 Weighted Average

Tc Length Slope Velocity Capacity Description (min) (feet) (ft/ft) (ft/sec) (cfs)

5.0

Direct Entry,

El Paso County 5-Year Duration=5 min, Inten=5.17 in/hr

Prepared by WestWorks Engineering

Page 2

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Subcatchment B1:

Runoff = 1.73 cfs

1.73 cfs @ 0.08 hrs, Volume=

0.012 af, Depth= 0.37"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 5-Year Duration=5 min, Inten=5.17 in/hr

| Area (ac) | С | Description |
|-----------|------|-------------|
| 0.100 | 0.73 | ROOFTOP |
| 0.300 | 0.90 | PAVEMENT |

0.400 0.86 Weighted Average

| Tc | Length | Slope | Velocity | Capacity | Description |
|----|--------|-------|----------|----------|-------------|
| | | | | (cfs) | |

5.0

Direct Entry,

Subcatchment B11:

Runoff =

1.68 cfs @

0.08 hrs, Volume=

0.012 af, Depth= 0.16"

Runoff by Rational method, Rise/Fall= $1.0/1.0 \, xTc$, Time Span= $0.00-3.00 \, hrs$, dt= $0.01 \, hrs$ El Paso County 5-Year Duration= $5 \, min$, Inten= $5.17 \, in/hr$

| Area (a | ic) | С | Description |
|---------|-----|------|-------------|
| 0.40 | 00 | 0.73 | ROOFTOP |
| 0.50 | 00 | 0.08 | LANDSCAPE |
| | | | |

0.900 0.37 Weighted Average

| Tc | Length | Slope | Velocity | Capacity | Description |
|----|--------|-------|----------|----------|-------------|
| | | | | (cfs) | |

5.0

Direct Entry,

Subcatchment B3:

Runoff

1.73 cfs @

0.08 hrs, Volume=

0.012 af, Depth= 0.37"

Runoff by Rational method, Rise/Fall= $1.0/1.0 \, xTc$, Time Span= $0.00-3.00 \, hrs$, dt= $0.01 \, hrs$ El Paso County 5-Year Duration= $5 \, min$, Inten= $5.17 \, in/hr$

| Area (ac) | C | Description | |
|-----------|------|-----------------|--|
| 0.100 | 0.73 | ROOFTOP | |
| 0.300 | 0.90 | PAVEMENT | |

0.400 0.86 Weighted Average

| Tc | Length | Slope | Velocity | Capacity | Description |
|----|--------|-------|----------|----------|-------------|
| | (feet) | | (ft/sec) | | |

5.0

Direct Entry,

El Paso County 5-Year Duration=5 min, Inten=5.17 in/hr

Prepared by WestWorks Engineering

Page 3

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Subcatchment B4:

Runoff

=

3.40 cfs @ 0

0.08 hrs, Volume=

0.024 af, Depth= 0.32"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 5-Year Duration=5 min, Inten=5.17 in/hr

| Area (ac) | С | Description | |
|-----------|------|------------------|--|
| 0.100 | 0.08 | LANDSCAPE | |
| 0.300 | 0.73 | ROOFTOP | |
| 0.500 | 0.90 | PAVEMENT | |
| 0.900 | 0.75 | Weighted Average | |

| | | | | Capacity (cfs) | Description |
|-----|--------|--------|----------|-------------------|-------------|
| 5.0 | (ICCL) | (IUIL) | (II/Sec) | (CIS) | D: |

5.0

Direct Entry,

Subcatchment B5:

Runoff

1.51 cfs @

0.08 hrs, Volume=

0.011 af, Depth= 0.32"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 5-Year Duration=5 min, Inten=5.17 in/hr

| | Area (ac) | С | Description | |
|----|-----------|------|------------------|--|
| | 0.050 | 0.08 | LANDSCAPE | |
| | 0.100 | 0.73 | ROOFTOP | |
| _ | 0.250 | 0.90 | PAVEMENT | |
| 12 | 0.400 | 0.75 | Weighted Average | |
| | | | | |

| (min) | Length (feet) | , | Description | |
|-------|------------------|-------|--------------|--|
| 5.0 | | | Direct Entry | |

Direct Entry,

Subcatchment B7:

Runoff

2.47 cfs @

0.08 hrs, Volume=

0.018 af, Depth= 0.30"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 5-Year Duration=5 min, Inten=5.17 in/hr

| _ | Area (ac) | С | Description | |
|---|-----------|------|------------------|--|
| | 0.150 | 0.08 | LANDSCAPE | |
| | 0.100 | 0.73 | ROOFTOP | |
| | 0.450 | 0.90 | PAVEMENT | |
| | 0.700 | 0.70 | Weighted Average | |

| 5Y | DD | | | - |
|-----|-----|--|----|---|
| OIL | K-1 | | () |) |

El Paso County 5-Year Duration=5 min, Inten=5.17 in/hr

Prepared by WestWorks Engineering

Page 4

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

| | | | | . , | Description |
|------------|--------|---------|---------|-------|-------------|
| (min) (fee | et) (f | t/ft) (| ft/sec) | (cfs) | 24 |

5.0

Direct Entry,

Subcatchment B8:

Runoff

= 1.94 cfs @

0.08 hrs, Volume=

0.014 af, Depth= 0.24"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 5-Year Duration=5 min, Inten=5.17 in/hr

| _ | Area (ac) | С | Description | |
|---|-----------|------|-----------------|--|
| | 0.300 | 0.08 | LANDSCAPE | |
| | 0.400 | 0.90 | PAVEMENT | |
| | 0.700 | 0.55 | \\\/-:- - - | |

0.700 0.55 Weighted Average

Tc Length Slope Velocity Capacity Description (min) (feet) (ft/ft) (ft/sec) (cfs)

5.0

Direct Entry,

Subcatchment B9:

Runoff

0.65 cfs @

0.08 hrs, Volume=

0.005 af, Depth= 0.28"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 5-Year Duration=5 min, Inten=5.17 in/hr

| | Area (ac) | С | Description | |
|---|-----------|------|------------------|--|
| | 0.050 | 0.08 | LANDSCAPE | |
| | 0.050 | 0.73 | ROOFTOP | |
| _ | 0.100 | 0.90 | PAVEMENT | |
| | 0.200 | 0.65 | Weighted Average | |

| | | | | | Description |
|-------|--------|---------|----------|-------|-------------|
| (min) | (feet) | (ft/ft) | (ft/sec) | (cfs) | |

5.0

Direct Entry,

Subcatchment OS-7A:

Runoff

7.04 cfs @

0.08 hrs, Volume=

0.050 af, Depth= 0.22"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 5-Year Duration=5 min, Inten=5.17 in/hr

| Area (ac) | С | Description |
|-----------|------|-------------|
| 2.800 | 0.50 | FROM FDR |

El Paso County 5-Year Duration=5 min, Inten=5.17 in/hr

Prepared by WestWorks Engineering

Page 5

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

| (min) (feet) (ft/ft) (ft/sec) (cfs) | | | | | Capacity (cfs) | Description |
|-------------------------------------|--|--|--|--|----------------|-------------|
|-------------------------------------|--|--|--|--|----------------|-------------|

5.0

Direct Entry, FROM FDR

Reach SD10:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.400 ac, Inflow Depth = 0.37" for 5-Year event 1.73 cfs @ 0.08 hrs, Volume= 0.012 af

Outflow = 1.73 cfs @ 0.08 hrs, Volume= 0.012 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Reach SD19:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.700 ac, Inflow Depth = 0.23" for 5-Year event 1.60 cfs @ 0.07 hrs, Volume= 0.013 af

Outflow = 1.60 cfs @ 0.07 hrs, Volume= 0.013 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Reach SD20:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.900 ac, Inflow Depth = 0.24" for 5-Year event 2.25 cfs @ 0.08 hrs, Volume= 0.018 af

Outflow = 2.25 cfs @ 0.08 hrs, Volume= 0.018 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Reach SD27:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.900 ac, Inflow Depth = 0.16" for 5-Year event 1.68 cfs @ 0.08 hrs, Volume= 0.012 af

Outflow = 1.68 cfs @ 0.08 hrs, Volume= 0.012 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

El Paso County 5-Year Duration=5 min, Inten=5.17 in/hr

Prepared by WestWorks Engineering

Page 6

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Reach SD4:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.300 ac, Inflow Depth = 0.36" for 5-Year event 1.27 cfs @ 0.08 hrs, Volume= 0.009 af

Outflow = 1.27 cfs @ 0.08 hrs, Volume= 0.009 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 4:

Inflow Area = 0.300 ac, Inflow Depth = 0.36" for 5-Year event 1.27 cfs @ 0.08 hrs, Volume= 0.009 af

Primary = 1.27 cfs @ 0.08 hrs, Volume= 0.009 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 5:

Inflow Area = 0.300 ac, Inflow Depth = 0.27" for 5-Year event 0.95 cfs @ 0.08 hrs. Volume= 0.007 af

Primary = 0.95 cfs @ 0.08 hrs, Volume= 0.007 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 10:

Inflow Area = 0.400 ac, Inflow Depth = 0.37" for 5-Year event 1.73 cfs @ 0.08 hrs, Volume= 0.012 af

Primary = 1.73 cfs @ 0.08 hrs, Volume= 0.012 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 12:

Inflow Area = 0.400 ac, Inflow Depth = 0.37" for 5-Year event 1.73 cfs @ 0.08 hrs, Volume= 0.012 af

Primary = 1.73 cfs @ 0.08 hrs, Volume= 0.012 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-3.00 hrs. dt= 0.01 hrs.

Link 14:

Inflow Area = 0.400 ac, Inflow Depth = 0.32" for 5-Year event 1.51 cfs @ 0.08 hrs, Volume= 0.011 af

Primary = 1.51 cfs @ 0.08 hrs, Volume= 0.011 af, Atten= 0%, Lag= 0.0 min

El Paso County 5-Year Duration=5 min, Inten=5.17 in/hr

Prepared by WestWorks Engineering

Page 7

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Link 17:

Inflow Area = 0.700 ac, Inflow Depth = 0.24" for 5-Year event 1.94 cfs @ 0.08 hrs, Volume= 0.014 af

Primary = 1.60 cfs @ 0.07 hrs, Volume= 0.013 af, Atten= 17%, Lag= 0.0 min

Secondary = 0.34 cfs @ 0.08 hrs, Volume= 0.001 af

Primary outflow = Inflow below 1.60 cfs, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 18:

Inflow Area = 0.200 ac, Inflow Depth = 0.28" for 5-Year event 0.65 cfs @ 0.08 hrs, Volume= 0.005 af

Primary = 0.65 cfs @ 0.08 hrs, Volume= 0.005 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-3.00 hrs. dt= 0.01 hrs.

Link 24:

Inflow Area = 0.900 ac, Inflow Depth = 0.16" for 5-Year event 1.68 cfs @ 0.08 hrs, Volume= 0.012 af

Primary = 1.68 cfs @ 0.08 hrs, Volume= 0.012 af, Atten= 0%, Lag= 0.0 min

El Paso County 5-Year Duration=6 min, Inten=4.90 in/hr

Prepared by WestWorks Engineering

Page 1

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Subcatchment A2:

Runoff = 1.66 cfs @ 0.10 hrs, Volume=

0.014 af, Depth= 0.41"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 5-Year Duration=6 min, Inten=4.90 in/hr

| Area (ac) | С | Description |
|-----------|------|-------------|
| 0.150 | 0.73 | ROOFTOP |
| 0.250 | 0.90 | PAVEMENT |

0.400 0.84 Weighted Average

| Tc | Length | Slope | Velocity | Capacity | Description |
|----|--------|-------|----------|----------|-------------|
| | | | | (cfs) | |

6.0

Direct Entry,

Subcatchment A3:

Runoff = 1.62 cfs

1.62 cfs @ 0.10 hrs, Volume=

0.013 af, Depth= 0.40"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 5-Year Duration=6 min, Inten=4.90 in/hr

| Area (ac) | С | Description |
|-----------|------|-----------------|
| 0.200 | 0.73 | ROOFTOP |
| 0.200 | 0.90 | PAVEMENT |
| | | |

0.400 0.82 Weighted Average

| Tc | Length | Slope | Velocity | Capacity | Description |
|----|--------|-------|----------|----------|-------------|
| | (feet) | | (ft/sec) | (cfs) | |

6.0

Direct Entry,

Subcatchment A7:

Runoff

1.28 cfs @

0.10 hrs, Volume=

0.011 af, Depth= 0.32"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 5-Year Duration=6 min, Inten=4.90 in/hr

| Area (ac) | С | Description |
|-----------|------|-------------|
| 0.100 | 0.08 | LANDSCAPE |
| 0.100 | 0.73 | ROOFTOP |
| 0.200 | 0.90 | PAVEMENT |

0.400 0.65 Weighted Average

| Tc | Length | Slope | Velocity | Capacity | Description |
|----|--------|-------|----------|----------|-------------|
| | (feet) | | (ft/sec) | | |

6.0

Direct Entry,

6.0

El Paso County 5-Year Duration=6 min, Inten=4.90 in/hr

Prepared by WestWorks Engineering

Page 2

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Subcatchment A8:

Runoff = 0.52 cfs @ 0.10 hrs, Volume=

0.004 af, Depth= 0.17"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 5-Year Duration=6 min, Inten=4.90 in/hr

| _ | Area (| (ac) | С | Des | cription | | | | |
|---|-------------|--------------|------|------------------|----------------------|----------|-------------|--|----|
| | 0.2 | 200 | 0.08 | LAN | IDSCAPE | | | | |
| | 0. | 100 | 0.90 | PA\ | /EMENT | | | | |
| | 0.3 | 300 | 0.35 | Wei | ighted Ave | rage | | | i. |
| | Tc (min) | Leng (fee | | Slope (ft/ft) | Velocity (ft/sec) | Capacity | Description | | |

Direct Entry,

Subcatchment B10:

Runoff = 0.71 cfs @ 0.10 hrs, Volume= 0.006 af, Depth= 0.12"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 5-Year Duration=6 min, Inten=4.90 in/hr

| Area | (ac) | С | Des | cription | | | |
|-------------|-------------|------|------------------|----------------------|-------------------|-------------|--|
| 0. | 450 | 0.08 | LAN | IDSCAPE | | | |
| 0. | 150 | 0.73 | RO | OFTOP | | | |
| 0. | 600 | 0.24 | Wei | ghted Ave | rage | | |
| Tc (min) | Leng (fe | | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description | |

6.0 (ff/ft) (ft/sec) (cfs) Direct Entry,

Subcatchment B2:

Runoff = 1.44 cfs @ 0.10 hrs, Volume= 0.012 af, Depth= 0.36"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 5-Year Duration=6 min, Inten=4.90 in/hr

| Area | (ac) | С | Des | scription | | | |
|-------------|--------------|------|------------------|----------------------|-------------------|-------------|--|
| 0. | 050 | 0.08 | LAN | NDSCAPE | VIII. | | |
| 0. | 150 | 0.73 | RO | OFTOP | | | |
| 0. | 200 | 0.90 | PA | JEMENT | | | |
| 0. | 400 | 0.73 | We | ighted Ave | rage | | |
| Tc (min) | Leng (fee | | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description | |

6.0 Direct Entry,

El Paso County 5-Year Duration=6 min, Inten=4.90 in/hr

Prepared by WestWorks Engineering

Page 3

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Subcatchment B6:

Runoff

=

1.90 cfs @

0.10 hrs, Volume=

0.016 af, Depth= 0.38"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 5-Year Duration=6 min, Inten=4.90 in/hr

| Area (ac) | С | Description |
|-----------|------|-------------|
| 0.050 | 0.08 | LANDSCAPE |
| 0.150 | 0.73 | ROOFTOP |
| 0.300 | 0.90 | PAVEMENT |

0.500 0.77 Weighted Average

| Tc | Length | Slope | Velocity | Capacity | Description |
|----|--------|-------|----------|----------|-------------|
| | | | | | |

6.0

Direct Entry,

Subcatchment OS-12:

Runoff

3.21 cfs @

0.10 hrs, Volume=

0.027 af, Depth= 0.24"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 5-Year Duration=6 min, Inten=4.90 in/hr

| Area (ac) | С | Description |
|-----------|------|-------------|
| 1.300 | 0.50 | FROM FDR |

| Tc | Length | Slope | Velocity | Capacity | Description |
|----|--------|-------|----------|----------|-------------|
| | | | | (cfs) | |

6.0

Direct Entry, FROM FDR

Subcatchment OS-13A:

Runoff

1.82 cfs @

0.10 hrs, Volume=

0.015 af, Depth= 0.11"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 5-Year Duration=6 min, Inten=4.90 in/hr

| Area (ac) | С | Description |
|-----------|------|---------------|
| 0.300 | 0.90 | PAVEMENT/ROOF |
| 1.300 | 0.08 | LANDSCAPE |

| 1.600 | 0.23 | Weighted Average |
|-------|------|------------------|
| | | |

| Tc | Length | Slope | Velocity | Capacity | Description |
|----|--------|-------|----------|----------|-------------|
| | (feet) | | (ft/sec) | (cfs) | 1989 |

6.0

Direct Entry, FROM FDR

El Paso County 5-Year Duration=6 min, Inten=4.90 in/hr

Prepared by WestWorks Engineering

Page 4

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Subcatchment OS-13B:

Runoff

= 0.37 cfs @ 0.10 hrs, Volume=

0.003 af, Depth= 0.07"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 5-Year Duration=6 min, Inten=4.90 in/hr

Area (ac)

C Description

0.500 0.15 LANDSCAPE

Tc Length (min) (feet)

Slope Velocity (ft/ft)

Capacity Description

6.0

(ft/sec) (cfs)

Direct Entry,

Subcatchment OS-13C:

Runoff

4.69 cfs @

0.10 hrs, Volume=

0.039 af. Depth= 0.12"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 5-Year Duration=6 min, Inten=4.90 in/hr

| Area (ac) | С | Description | |
|-----------|------|-------------|--|
| 0.000 | 0.00 | DAY/ENACHI | |

PAVEMENT/ROOF 0.800 0.90 3.000 0.08 LANDSCAPE

3.800 0.25 Weighted Average

Tc Length

Slope Velocity Capacity

Description

(min) (feet) (ft/ft) (ft/sec) (cfs)

Direct Entry, FROM FDR

Reach SD1:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area =

6.0

0.800 ac, Inflow Depth = 0.21" for 5-Year event

Inflow

1.69 cfs @

0.10 hrs. Volume=

0.014 af

Outflow

1.69 cfs @

0.10 hrs, Volume=

0.014 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Reach SD11:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area =

0.400 ac, Inflow Depth = 0.36"

for 5-Year event

Inflow

1.44 cfs @

0.10 hrs, Volume=

0.012 af

Outflow = 1.44 cfs @

0.10 hrs, Volume=

0.012 af, Atten= 0%, Lag= 0.0 min

El Paso County 5-Year Duration=6 min, Inten=4.90 in/hr

Prepared by WestWorks Engineering

Page 5

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Reach SD12:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area =

0.800 ac, Inflow Depth = 0.39" for 5-Year event

Inflow

3.15 cfs @ 0.10 hrs, Volume=

0.026 af

Outflow

3.15 cfs @ 0.10 hrs, Volume=

0.026 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs. dt= 0.01 hrs.

Reach SD13:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area =

1.200 ac, Inflow Depth = 0.40" for 5-Year event

Inflow

4.87 cfs @ 0.10 hrs, Volume=

0.040 af

Outflow

4.87 cfs @

0.10 hrs, Volume=

0.040 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs.

Reach SD17:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area =

2.000 ac, Inflow Depth = 0.28" for 5-Year event

Inflow

5.64 cfs @ 0.10 hrs, Volume=

0.047 af

Outflow

5.64 cfs @ 0.10 hrs. Volume=

0.047 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Reach SD2:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area =

1.200 ac, Inflow Depth = 0.28"

for 5-Year event

Inflow Outflow

3.34 cfs @ 0.10 hrs, Volume= 3.34 cfs @ 0.10 hrs, Volume= 0.028 af 0.028 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Reach SD28:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area =

=

3.800 ac, Inflow Depth = 0.12" for 5-Year event

Inflow Outflow

4.69 cfs @ 0.10 hrs, Volume=

4.69 cfs @ 0.10 hrs, Volume=

0.039 af 0.039 af, Atten= 0%, Lag= 0.0 min

El Paso County 5-Year Duration=6 min, Inten=4.90 in/hr

Prepared by WestWorks Engineering

Page 6

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Reach SD3:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 1.600 ac, Inflow Depth = 0.31" for 5-Year event 4.96 cfs @ 0.10 hrs, Volume= 0.041 af

Outflow = 4.96 cfs @ 0.10 hrs, Volume= 0.041 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Reach SD5:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 1.900 ac, Inflow Depth = 0.32" for 5-Year event for 5-Year event 0.051 af

Outflow = 6.21 cfs @ 0.10 hrs, Volume= 0.051 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs. dt= 0.01 hrs.

Reach SD6:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 2.200 ac, Inflow Depth = 0.32" for 5-Year event 7.15 cfs @ 0.10 hrs, Volume= 0.059 af

Outflow = 7.15 cfs @ 0.10 hrs, Volume= 0.059 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 1:

Inflow Area = 0.800 ac, Inflow Depth = 0.21" for 5-Year event 1.69 cfs @ 0.10 hrs, Volume= 0.014 af

Primary = 1.69 cfs @ 0.10 hrs, Volume= 0.014 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 2:

Inflow Area = 0.400 ac, Inflow Depth = 0.41" for 5-Year event 1.66 cfs @ 0.10 hrs, Volume= 0.014 af

Primary = 1.66 cfs @ 0.10 hrs, Volume= 0.014 af, Atten= 0%, Lag= 0.0 min

El Paso County 5-Year Duration=6 min, Inten=4.90 in/hr

Prepared by WestWorks Engineering

Page 7

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Link 3:

Inflow Area = 0.400 ac, Inflow Depth = 0.40" for 5-Year event 1.62 cfs @ 0.10 hrs, Volume= 0.013 af

Primary = 1.62 cfs @ 0.10 hrs, Volume= 0.013 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 7:

Inflow Area = 0.400 ac, Inflow Depth = 0.32" for 5-Year event 1.28 cfs @ 0.10 hrs, Volume= 0.011 af

Primary = 1.28 cfs @ 0.10 hrs, Volume= 0.011 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 8:

Inflow Area = 0.300 ac, Inflow Depth = 0.17" for 5-Year event Inflow = 0.52 cfs @ 0.10 hrs. Volume= 0.004 af

Primary = 0.52 cfs @ 0.10 hrs, Volume= 0.004 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 11:

Inflow Area = 0.400 ac, Inflow Depth = 0.36" for 5-Year event 1.44 cfs @ 0.10 hrs, Volume= 0.012 af

Primary = 1.44 cfs @ 0.10 hrs, Volume= 0.012 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 15:

Inflow Area = 0.500 ac, Inflow Depth = 0.38" for 5-Year event 1.90 cfs @ 0.10 hrs, Volume= 0.016 af

Primary = 1.90 cfs @ 0.10 hrs, Volume= 0.016 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 16:

Inflow Area = 2.000 ac, Inflow Depth = 0.28" for 5-Year event Inflow = 5.64 cfs @ 0.10 hrs. Volume= 0.047 af

Primary = 5.64 cfs @ 0.10 hrs, Volume= 0.047 af, Atten= 0%, Lag= 0.0 min

El Paso County 5-Year Duration=6 min, Inten=4.90 in/hr

Prepared by WestWorks Engineering

Page 8

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Link 19:

Inflow Area =

0.600 ac, Inflow Depth = 0.12" for 5-Year event

Inflow

0.71 cfs @ 0.10 hrs, Volume= 0.006 af

Primary

0.71 cfs @ 0.10 hrs, Volume=

0.006 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 25:

Inflow Area =

3.800 ac, Inflow Depth = 0.12" for 5-Year event

Inflow

4.69 cfs @

0.10 hrs, Volume=

0.039 af

Primary

4.69 cfs @

0.10 hrs, Volume=

0.039 af, Atten= 0%, Lag= 0.0 min

Prepared by WestWorks Engineering

Page 1

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Subcatchment OS-11:

Runoff = 7.06 cfs @ 0.12 hrs, Volume= 0.070 af, Depth= 0.30"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 5-Year Duration=7 min, Inten=4.66 in/hr

Area (ac) C Description
2.800 0.55 FROM FDR

Tc Length Slope Velocity Capacity Description (min) (feet) (ft/ft) (ft/sec) (cfs)

7.0

Direct Entry, FROM FDR

Reach SD14:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 3.700 ac, Inflow Depth = 0.33" for 5-Year event 10.17 cfs @ 0.12 hrs, Volume= 0.100 af

Outflow = 10.17 cfs @ 0.12 hrs, Volume= 0.100 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Reach SD15:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 4.100 ac, Inflow Depth = 0.33" for 5-Year event 11.57 cfs @ 0.12 hrs, Volume= 0.114 af

Outflow = 11.57 cfs @ 0.12 hrs, Volume= 0.114 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Reach SD16:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 5.300 ac, Inflow Depth = 0.36" for 5-Year event 16.04 cfs @ 0.11 hrs, Volume= 0.158 af

Outflow = 16.04 cfs @ 0.11 hrs, Volume= 0.158 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

El Paso County 5-Year Duration=7 min, Inten=4.66 in/hr

Prepared by WestWorks Engineering

Page 2

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Reach SD18:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 7.800 ac, Inflow Depth = 0.35" for 5-Year event 1nflow = 23.18 cfs @ 0.11 hrs, Volume= 0.227 af

Outflow = 23.18 cfs @ 0.11 hrs, Volume= 0.227 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Reach SD26:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 10.200 ac, Inflow Depth = 0.04" for 5-Year event
Inflow = 0.16 cfs @ 0.23 hrs, Volume= 0.037 af

Outflow = 0.16 cfs @ 0.23 hrs, Volume= 0.037 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 13:

Inflow Area = 3.700 ac, Inflow Depth = 0.33" for 5-Year event 10.17 cfs @ 0.12 hrs, Volume= 0.100 af

Primary = 10.17 cfs @ 0.12 hrs, Volume= 0.100 af, Atten= 0%, Lag= 0.0 min

El Paso County 5-Year Duration=9 min, Inten=4.29 in/hr

Prepared by WestWorks Engineering

Page 1

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Subcatchment A9:

Runoff

=

0.32 cfs @

0.15 hrs. Volume=

0.004 af. Depth= 0.10"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 5-Year Duration=9 min, Inten=4.29 in/hr

Area (ac)

C Description

0.500 0.15 LANDSCAPE

Tc Length (min)

9.0

Slope

Velocity Capacity (ft/sec)

Description

(feet)

(ft/ft)

(cfs)

Direct Entry,

Subcatchment C1:

Runoff

1.27 cfs @

0.15 hrs, Volume=

0.016 af, Depth= 0.32"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 5-Year Duration=9 min, Inten=4.29 in/hr

| Area (ac) | С | Description |
|-----------|------|-------------|
| 0.300 | 0.08 | LANDSCAPE |

0.300 0.90 **PAVEMENT**

Weighted Average 0.600 0.49

Tc Length

Slope Velocity Capacity (ft/ft)

Description

(min) (feet) (ft/sec)

(cfs)

9.0

Direct Entry,

Link 9:

Inflow Area =

=

0.500 ac, Inflow Depth = 0.10" for 5-Year event

Inflow

0.32 cfs @

0.15 hrs, Volume=

0.004 af

Primary

0.32 cfs @

0.15 hrs, Volume=

0.004 af, Atten= 0%, Lag= 0.0 min

El Paso County 5-Year Duration=11 min, Inten=3.99 in/hr

Prepared by WestWorks Engineering

Page 1

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Subcatchment A6:

Runoff = 2.87 cfs @ 0.181

0.18 hrs, Volume= 0.044 af, Depth= 0.48"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 5-Year Duration=11 min, Inten=3.99 in/hr

| Area (ac) | C | Description |
|--|---|--|
| 0.300 | 0.08 | LANDSCAPE |
| 0.100 | 0.73 | ROOFTOP |
| 0.700 | 0.90 | PAVEMENT |
| The second secon | The book of the second of the | Company of the second s |

1.100 0.66 Weighted Average

| Tc | Length | Slope | Velocity | Capacity | Description |
|----|--------|-------|----------|----------|--|
| | (feet) | | (ft/sec) | | 201 20 20 20 20 20 20 20 20 20 20 20 20 20 |

11.0

Direct Entry,

Subcatchment C2:

Runoff =

2.33 cfs @ 0.18 hrs, Volume=

0.036 af, Depth= 0.36"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 5-Year Duration=11 min, Inten=3.99 in/hr

| Area (a | ac) | C | escription |
|---------|------|-------|------------|
| 0.6 | 00 0 | .08 L | ANDSCAPE |
| 0.6 | 00 0 | .90 P | AVEMENT |
| | | | |

1.200 0.49 Weighted Average

| IC | Length | Slope | Velocity | Capacity |
|-------|--------|---------|----------|----------|
| (min) | (feet) | (ft/ft) | (ft/sec) | (cfs) |

11.0

Direct Entry,

Description

Reach SD7:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 3.100 ac, Inflow Depth = 0.32" for 5-Year event Inflow = 5.40 cfs @ 0.18 hrs, Volume= 0.083 af

Outflow = 5.40 cfs @ 0.18 hrs, Volume= 0.083 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs. dt= 0.01 hrs.

Reach SD8:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 3.400 ac, Inflow Depth = 0.31" for 5-Year event Inflow = 5.82 cfs @ 0.18 hrs, Volume= 0.089 af

Outflow = 5.82 cfs @ 0.18 hrs, Volume= 0.089 af, Atten= 0%, Lag= 0.0 min

El Paso County 5-Year Duration=11 min, Inten=3.99 in/hr

Prepared by WestWorks Engineering

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

Page 2 11/6/2019

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Reach SD9:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 6.100 ac, Inflow Depth = 0.05" for 5-Year event 0.11 cfs @ 0.36 hrs, Volume= 0.024 af

Outflow = 0.11 cfs @ 0.36 hrs, Volume= 0.024 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 6:

Inflow Area = 2.700 ac, Inflow Depth = 0.30" for 5-Year event

Inflow = 4.35 cfs @ 0.18 hrs, Volume= 0.067 af

Primary = 4.35 cfs @ 0.18 hrs, Volume= 0.067 af, Atten= 0%, Lag= 0.0 min

Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Primary outflow = Inflow below 4.40 cfs, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 23:

Inflow Area = 1.200 ac, Inflow Depth = 0.36" for 5-Year event Inflow = 2.33 cfs @ 0.18 hrs, Volume= 0.036 af

Primary = 2.33 cfs @ 0.18 hrs, Volume= 0.036 af, Atten= 0%, Lag= 0.0 min

El Paso County 5-Year Duration=20 min, Inten=3.09 in/hr

Prepared by WestWorks Engineering

Page 1

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Reach SD23:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.600 ac, Inflow Depth = 0.50" for 5-Year event 0.92 cfs @ 0.15 hrs, Volume= 0.025 af

Outflow = 0.92 cfs @ 0.15 hrs, Volume= 0.025 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Reach SD24:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 78.100 ac, Inflow Depth = 0.12" for 5-Year event 28.57 cfs @ 0.33 hrs, Volume= 0.781 af

Outflow = 28.57 cfs @ 0.33 hrs, Volume= 0.781 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Reach SD25:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 88.600 ac, Inflow Depth = 0.12" for 5-Year event 32.59 cfs @ 0.33 hrs, Volume= 0.920 af

Outflow = 32.59 cfs @ 0.33 hrs, Volume= 0.920 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs. dt= 0.01 hrs.

Link 21:

Inflow Area = 78.100 ac, Inflow Depth = 0.12" for 5-Year event 28.57 cfs @ 0.33 hrs, Volume= 0.781 af

Primary = 28.57 cfs @ 0.33 hrs, Volume= 0.781 af, Atten= 0%, Lag= 0.0 min

Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Primary outflow = Inflow below 28.80 cfs, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 22:

Inflow Area = 0.600 ac, Inflow Depth = 0.50" for 5-Year event 0.92 cfs @ 0.15 hrs, Volume= 0.025 af

Primary = 0.92 cfs @ 0.15 hrs, Volume= 0.025 af, Atten= 0%, Lag= 0.0 min

El Paso County 5-Year Duration=20 min, Inten=3.09 in/hr

Prepared by WestWorks Engineering

Page 2

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Link DP-OS11: FLOW-BY

Inflow Area = 65.500 ac, Inflow Depth = 0.06" for 5-Year event Inflow = 0.327 af

12.00 cfs @ 0.33 hrs, Volume= 12.00 cfs @ 0.33 hrs, Volume= Primary = 0.327 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

23 Point hydrograph entered manually, To= 0.00 hrs, dt= 0.03 hrs, Area= 65.500 ac, cfs =

| 0.00 | 1.10 | 2.20 | 3.30 | 4.40 | 5.50 | 6.50 | 7.60 | 8.70 | 9.80 |
|-------|-------|-------|------|------|------|------|------|------|------|
| 10.90 | 12.00 | 10.90 | 9.80 | 8.70 | 7.60 | 6.50 | 5.50 | 4.40 | 3.30 |
| 2.20 | 1.10 | 0.00 | | | | | | | |

El Paso County 5-Year Duration=25 min, Inten=2.75 in/hr

Prepared by WestWorks Engineering

Page 1

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Reach SD21:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 2.800 ac, Inflow Depth = 5.96" for 5-Year event Inflow = 39.95 cfs @ 0.42 hrs, Volume= 1.390 af

Outflow = 39.95 cfs @ 0.42 hrs, Volume= 1.390 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Reach SD22:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 13.000 ac, Inflow Depth = 1.35" for 5-Year event 40.26 cfs @ 0.42 hrs, Volume= 1.464 af

Outflow = 40.26 cfs @ 0.42 hrs, Volume= 1.464 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 009: BASIN 009

Inflow Area = 101.600 ac, Inflow Depth = 0.29" for 5-Year event Inflow = 66.86 cfs @ 0.41 hrs, Volume= 2.452 af

Primary = 66.86 cfs @ 0.41 hrs, Volume= 2.452 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 20:

Inflow Area = 2.800 ac, Inflow Depth = 5.96" for 5-Year event Inflow = 39.95 cfs @ 0.42 hrs, Volume= 1.390 af

Primary = 39.95 cfs @ 0.42 hrs, Volume= 1.390 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-3.00 hrs. dt= 0.01 hrs.

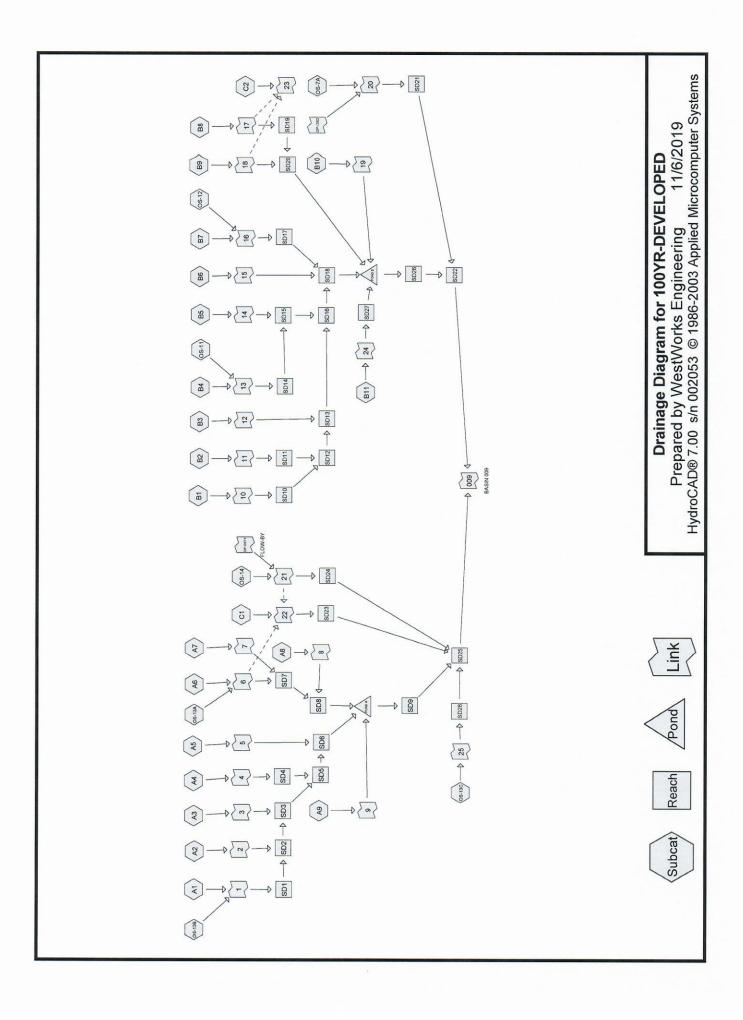
Link DP-OS2:

Inflow = 36.20 cfs @ 0.42 hrs, Volume= 1.257 af

Primary = 36.20 cfs @ 0.42 hrs, Volume= 1.257 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

29 Point hydrograph entered manually, To= 0.00 hrs, dt= 0.03 hrs, Area= 0.000 ac, cfs = 0.00 2.60 5.20 7.80 10.30 12.90 15.50 18.10 20.70 23.30 25.90 28.40 31.00 33.60 36.20 33.60 31.00 28.40 25.90 23.30 20.70 18.10 15.50 12.90 10.30 7.80 5.20 2.60 0.00



El Paso County 100-Year Duration=5 min, Inten=8.68 in/hr

Prepared by WestWorks Engineering

Page 1

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Subcatchment A1:

Runoff

= 2.3

2.31 cfs @

0.08 hrs, Volume=

0.016 af, Depth= 0.66"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 100-Year Duration=5 min. Inten=8.68 in/hr

| Area (ac) | С | Description |
|-----------|------|-----------------|
| 0.100 | 0.81 | ROOFTOPS |
| 0.200 | 0.96 | PAVEMENT |

0.300 0.91 Weighted Average

Tc Length Slope Velocity Capacity Description (min) (feet) (ft/ft) (ft/sec) (cfs)

5.0

Direct Entry.

Subcatchment A4:

Runoff

= 2.31 cfs @

0.08 hrs, Volume=

0.016 af, Depth= 0.66"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 100-Year Duration=5 min, Inten=8.68 in/hr

| Area (ac) | С | Description |
|-------------------|------------|-------------|
| 0.100 | 0.81 | ROOFTOP |
| 0.200 | 0.96 | PAVEMENT |
| E E E E E | 550 500 50 | 15X X 5X 5 |

0.300 0.91 Weighted Average

| | Тс | Length | Slope | Velocity | Capacity | Description |
|----|----|--------|---------------|----------|----------|-------------|
| 70 | | (feet) | CASTER COLARS | (ft/sec) | | |

5.0

Direct Entry,

Subcatchment A5:

Runoff

= 1.93 cfs @

0.08 hrs, Volume=

0.014 af, Depth= 0.55"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 100-Year Duration=5 min, Inten=8.68 in/hr

| Area (ac) | С | Description |
|-----------|------|-------------|
| 0.100 | 0.35 | LANDSCAPE |
| 0.200 | 0.96 | PAVEMENT |

0.300 0.76 Weighted Average

| Tc | Length | Slope | Velocity | Capacity | Description |
|-------|--------|---------|----------|----------|-------------|
| (min) | (feet) | (ft/ft) | (ft/sec) | (cfs) | |

5.0

Direct Entry,

El Paso County 100-Year Duration=5 min, Inten=8.68 in/hr

Prepared by WestWorks Engineering

Page 2

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Subcatchment B1:

Runoff

= 3.1

3.11 cfs @

0.08 hrs, Volume=

0.022 af, Depth= 0.66"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 100-Year Duration=5 min, Inten=8.68 in/hr

| Area (ac) | С | Description |
|-----------|------|-------------|
| 0.100 | 0.81 | ROOFTOP |
| 0.200 | 0.00 | DAVENTENT |

Tc Length Slope Velocity Capacity Description (min) (feet) (ft/ft) (ft/sec) (cfs)

5.0

Direct Entry,

Subcatchment B11:

Runoff

= 4.18 cfs @

0.08 hrs, Volume=

0.030 af, Depth= 0.40"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 100-Year Duration=5 min, Inten=8.68 in/hr

| Area (ac) | С | Description |
|-----------|------|-------------|
| 0.400 | 0.81 | ROOFTOP |
| 0.500 | 0.35 | LANDSCAPE |
| | | |

0.900 0.55 Weighted Average

| Tc | Length | Slope | Velocity | Capacity | Description |
|-------|--------|---------|----------|----------|--|
| (min) | (feet) | (ft/ft) | (ft/sec) | (cfs) | 50 |
| - | | | | | AND MARKET AND ADDRESS OF THE PARTY OF THE P |

5.0

Direct Entry,

Subcatchment B3:

Runoff

3.11 cfs @

0.08 hrs, Volume=

0.022 af. Depth= 0.66"

Runoff by Rational method, Rise/Fall= $1.0/1.0 \, xTc$, Time Span= $0.00-3.00 \, hrs$, dt= $0.01 \, hrs$ El Paso County 100-Year Duration= $5 \, min$, Inten= $8.68 \, in/hr$

| Area (ac) | С | Description |
|-----------|------|-------------|
| 0.100 | 0.81 | ROOFTOP |

0.300 0.96 PAVEMENT

0.400 0.92 Weighted Average

Tc Length Slope Velocity Capacity Description (min) (feet) (ft/ft) (ft/sec) (cfs)

5.0

Direct Entry,

El Paso County 100-Year Duration=5 min, Inten=8.68 in/hr

Prepared by WestWorks Engineering

Page 3

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Subcatchment B4:

Runoff

= 6.39

6.39 cfs @ 0.08 hrs, Volume=

0.045 af, Depth= 0.61"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 100-Year Duration=5 min, Inten=8.68 in/hr

| Area (ac) | С | Description |
|-----------|------|-----------------|
| 0.100 | 0.35 | LANDSCAPE |
| 0.300 | 0.81 | ROOFTOP |
| 0.500 | 0.96 | PAVEMENT |

0.900 0.84 Weighted Average

| Tc | Length | Slope | Slope Velocity | | Description |
|----|--------|-------|----------------|--|-------------|
| | | | (ft/sec) | | |

5.0

Direct Entry,

Subcatchment B5:

Runoff

2.87 cfs @

0.08 hrs, Volume=

0.020 af, Depth= 0.61"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 100-Year Duration=5 min, Inten=8.68 in/hr

| Area (ac) | С | Description |
|-----------|------|-------------|
| 0.050 | 0.35 | LANDSCAPE |
| 0.100 | 0.81 | ROOFTOP |
| 0.250 | 0.96 | PAVEMENT |
| 0.400 | 0.05 | 10/-: |

0.400 0.85 Weighted Average

| Tc | Length | Slope | Velocity | Capacity | Description |
|----|--------|-------|----------|----------|-------------|
| | | | (ft/sec) | | |

5.0

Direct Entry,

Subcatchment B7:

Runoff

4.79 cfs @

0.08 hrs, Volume=

0.034 af, Depth= 0.58"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 100-Year Duration=5 min, Inten=8.68 in/hr

| Area (ac) | С | Description | |
|-----------|------|------------------|--|
| 0.150 | 0.35 | LANDSCAPE | |
| 0.100 | 0.81 | ROOFTOP | |
| 0.450 | 0.96 | PAVEMENT | |
| 0.700 | 0.81 | Weighted Average | |

| 10 | NYR | -DE\ | /FI | OP | FD |
|----|-----|------|-----|----|----|
| | | | | | |

El Paso County 100-Year Duration=5 min, Inten=8.68 in/hr

Prepared by WestWorks Engineering

Page 4

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

| | | Capacity (cfs) | Description |
|-----|--|----------------|--------------|
| 5.0 | | | Direct Entry |

Direct Entry,

Subcatchment B8:

Runoff 4.14 cfs @

0.08 hrs, Volume=

0.029 af, Depth= 0.51"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 100-Year Duration=5 min, Inten=8.68 in/hr

| Area | (ac) | С | Des | cription | | | |
|-------------|--------------|--------|------------------|----------------------|-------------------|-------------|--|
| 0. | 300 | 0.35 | LAN | IDSCAPE | | | |
| 0. | 400 | 0.96 | PA | /EMENT | | | |
| 0. | 700 | 0.70 | Wei | ghted Ave | rage | | |
| Tc (min) | Leng (fee | 100000 | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description | |

Direct Entry,

Subcatchment B9:

Runoff

5.0

1.30 cfs @

0.08 hrs, Volume=

0.009 af, Depth= 0.56"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 100-Year Duration=5 min, Inten=8.68 in/hr

| Area (ac) | С | Description | |
|-----------|------|------------------|--|
| 0.050 | 0.35 | LANDSCAPE | |
| 0.050 | 0.81 | ROOFTOP | |
| 0.100 | 0.96 | PAVEMENT | |
| 0.200 | 0.77 | Weighted Average | |
| | | | |

| 20 20 20 | Length (feet) | | Velocity (ft/sec) | Capacity (cfs) | Description | |
|----------|---------------|-----------|-------------------|-------------------|--------------|--|
| 5.0 | () | (1.2.1.5) | () | (5.5) | Direct Entry | |

Direct Entry,

Subcatchment OS-7A:

Runoff 14.19 cfs @ 0.08 hrs, Volume= 0.101 af, Depth= 0.43"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 100-Year Duration=5 min, Inten=8.68 in/hr

| Area (ac) | С | Description | |
|-----------|------|-------------|--|
| 2.800 | 0.60 | FROM FDR | |

El Paso County 100-Year Duration=5 min, Inten=8.68 in/hr

Prepared by WestWorks Engineering

Page 5

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

| Tc | Length | Slope | Velocity | Capacity | Description |
|----|--------|-------|----------|----------|-------------|
| | | | | (cfs) | |

5.0

Direct Entry, FROM FDR

Reach SD10:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.400 ac, Inflow Depth = 0.66" for 100-Year event

Inflow = 3.11 cfs @ 0.08 hrs, Volume= 0.022 af

Outflow = 3.11 cfs @ 0.08 hrs, Volume= 0.022 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Reach SD19:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.700 ac, Inflow Depth = 0.41" for 100-Year event

Inflow = 2.40 cfs @ 0.05 hrs, Volume= 0.024 af

Outflow = 2.40 cfs @ 0.05 hrs, Volume= 0.024 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Reach SD20:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.900 ac, Inflow Depth = 0.44" for 100-Year event

Inflow = 3.61 cfs @ 0.08 hrs, Volume= 0.033 af

Outflow = 3.61 cfs @ 0.08 hrs, Volume= 0.033 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Reach SD27:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.900 ac, Inflow Depth = 0.40" for 100-Year event Inflow = 0.030 af 0.08 hrs, Volume= 0.030 af

Outflow = 4.18 cfs @ 0.08 hrs, Volume= 0.030 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

El Paso County 100-Year Duration=5 min. Inten=8.68 in/hr

Prepared by WestWorks Engineering

Page 6

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Reach SD4:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area =

0.300 ac, Inflow Depth = 0.66" for 100-Year event

Inflow

2.31 cfs @ 0.08 hrs, Volume=

0.016 af

Outflow

2.31 cfs @

0.08 hrs, Volume=

0.016 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 4:

Inflow Area =

0.300 ac, Inflow Depth = 0.66" for 100-Year event

0.016 af

Inflow Primary 2.31 cfs @ 0.08 hrs. Volume=

2.31 cfs @ 0.08 hrs, Volume=

0.016 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 5:

Inflow Area =

0.300 ac, Inflow Depth = 0.55" for 100-Year event

0.014 af

Inflow Primary 1.93 cfs @

0.08 hrs, Volume= 1.93 cfs @ 0.08 hrs, Volume=

0.014 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-3.00 hrs. dt= 0.01 hrs.

Link 10:

Inflow Area =

0.400 ac, Inflow Depth = 0.66" for 100-Year event

Inflow

3.11 cfs @ 0.08 hrs. Volume=

0.022 af

Primary

3.11 cfs @ 0.08 hrs, Volume=

0.022 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-3.00 hrs. dt= 0.01 hrs.

Link 12:

Inflow Area =

0.400 ac, Inflow Depth = 0.66" for 100-Year event

0.022 af

Inflow Primary

3.11 cfs @ 0.08 hrs, Volume= 3.11 cfs @ 0.08 hrs, Volume=

0.022 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 14:

Inflow Area =

0.400 ac. Inflow Depth = 0.61" for 100-Year event

Inflow

2.87 cfs @

0.08 hrs. Volume=

0.020 af

Primary =

2.87 cfs @ 0.08 hrs, Volume=

0.020 af, Atten= 0%, Lag= 0.0 min

El Paso County 100-Year Duration=5 min, Inten=8.68 in/hr

Prepared by WestWorks Engineering
HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

Page 7

11/6/2019

Link 17:

Inflow Area = 0.700 ac, Inflow Depth = 0.51" for 100-Year event Inflow = 0.029 af

Primary = 2.40 cfs @ 0.05 hrs, Volume= 0.024 af, Atten= 42%, Lag= 0.0 min

Secondary = 1.74 cfs @ 0.08 hrs, Volume= 0.006 af

Primary outflow = Inflow below 2.40 cfs, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 18:

Inflow Area = 0.200 ac, Inflow Depth = 0.56" for 100-Year event 1.30 cfs @ 0.08 hrs, Volume= 0.009 af

Primary = 1.21 cfs @ 0.08 hrs, Volume= 0.009 af, Atten= 7%, Lag= 0.1 min

Secondary = 0.10 cfs @ 0.08 hrs, Volume= 0.000 af

Primary outflow = Inflow below 1.20 cfs, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 24:

Inflow Area = 0.900 ac, Inflow Depth = 0.40" for 100-Year event
Inflow = 0.030 af
0.900 ac, Inflow Depth = 0.40" for 100-Year event
0.030 af

Primary = 4.18 cfs @ 0.08 hrs, Volume= 0.030 af, Atten= 0%, Lag= 0.0 min

El Paso County 100-Year Duration=6 min, Inten=8.22 in/hr

Prepared by WestWorks Engineering

Page 1

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Subcatchment A2:

Runoff

= 2.98 cfs @

0.10 hrs, Volume=

0.025 af, Depth= 0.74"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 100-Year Duration=6 min. Inten=8.22 in/hr

| Area (ac) | С | Description |
|-----------|------|-------------|
| 0.150 | 0.81 | ROOFTOP |
| 0.250 | 0.96 | PAVEMENT |

0.400 0.90 Weighted Average

Tc Length Slope Velocity Capacity Description (min) (feet) (ft/ft) (ft/sec) (cfs)

6.0

Direct Entry,

Subcatchment A3:

Runoff

2.92 cfs @

0.10 hrs, Volume=

0.024 af, Depth= 0.72"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 100-Year Duration=6 min, Inten=8.22 in/hr

| Area (ac) | C | Description |
|-----------|------|-----------------|
| 0.200 | 0.81 | ROOFTOP |
| 0.200 | 0.96 | PAVEMENT |

0.400 0.88 Weighted Average

Tc Length Slope Velocity Capacity Description (min) (feet) (ft/ft) (ft/sec) (cfs)

6.0

Direct Entry,

Subcatchment A7:

Runoff

2.55 cfs @

0.10 hrs, Volume=

0.021 af, Depth= 0.63"

Runoff by Rational method, Rise/Fall= $1.0/1.0 \, xTc$, Time Span= $0.00-3.00 \, hrs$, dt= $0.01 \, hrs$ El Paso County 100-Year Duration= $6 \, min$, Inten= $8.22 \, in/hr$

| Area (ac) | С | Description |
|-----------|------|-------------|
| 0.100 | 0.35 | LANDSCAPE |

0.100 0.81 ROOFTOP

0.200 0.96 PAVEMENT

0.400 0.77 Weighted Average

Tc Length Slope Velocity Capacity Description (min) (feet) (ft/ft) (ft/sec) (cfs)

6.0

Direct Entry,

El Paso County 100-Year Duration=6 min, Inten=8.22 in/hr

Prepared by WestWorks Engineering

Page 2 11/6/2019

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

Subcatchment A8:

Runoff

= 1.37

1.37 cfs @ 0.10 hrs, Volume=

0.011 af, Depth= 0.45"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 100-Year Duration=6 min, Inten=8.22 in/hr

| Area (ac) | С | Description |
|-----------|------|------------------|
| 0.200 | 0.35 | LANDSCAPE |
| 0.100 | 0.96 | PAVEMENT |
| 0.300 | 0.55 | Weighted Average |

| Tc | Length | Slope | Velocity | Capacity | Description |
|----|--------|-------|----------|----------|-------------|
| | | | (ft/sec) | | |

6.0

Direct Entry.

Subcatchment B10:

Runoff

2.34 cfs @

0.10 hrs, Volume=

0.019 af, Depth= 0.39"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 100-Year Duration=6 min, Inten=8.22 in/hr

| _ | Area (ac) | С | Description |
|---|-----------|------|------------------|
| | 0.450 | 0.35 | LANDSCAPE |
| _ | 0.150 | 0.81 | ROOFTOP |
| | 0.600 | 0.47 | Weighted Average |

| Tc | Length | Slope | Velocity | Capacity | Description |
|----|--------|-------|----------|----------|-------------|
| | (feet) | | (ft/sec) | | |

6.0

Direct Entry,

Subcatchment B2:

Runoff

= 2.75 cfs @

0.10 hrs, Volume=

0.023 af, Depth= 0.68"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 100-Year Duration=6 min, Inten=8.22 in/hr

| Area (ac) | С | Description |
|-----------|------|------------------|
| 0.050 | 0.35 | LANDSCAPE |
| 0.150 | 0.81 | ROOFTOP |
| 0.200 | 0.96 | PAVEMENT |
| 0.400 | 0.83 | Weighted Average |

| Tc | Length | Slope | Velocity | Capacity | Description |
|----|--------|-------|----------|----------|-------------|
| | | | | (cfs) | 22 |

6.0

Direct Entry,

El Paso County 100-Year Duration=6 min, Inten=8.22 in/hr

Prepared by WestWorks Engineering

Page 3

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Subcatchment B6:

Runoff

= 3.52 cfs @

0.10 hrs, Volume=

0.029 af, Depth= 0.70"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 100-Year Duration=6 min, Inten=8.22 in/hr

| Area (ac) | С | Description |
|-----------|------|-----------------|
| 0.050 | 0.35 | LANDSCAPE |
| 0.150 | 0.81 | ROOFTOP |
| 0.300 | 0.96 | PAVEMENT |
| | | |

0.500 0.85 Weighted Average

| | | | | | Description |
|-------|--------|---------|----------|-------|-------------|
| (min) | (feet) | (ft/ft) | (ft/sec) | (cfs) | |

6.0

Direct Entry,

Subcatchment OS-12:

Runoff

6.47 cfs @

0.10 hrs, Volume=

0.053 af, Depth= 0.49"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 100-Year Duration=6 min, Inten=8.22 in/hr

| Area (ac) | С | Description |
|-----------|------|-------------|
| 1.300 | 0.60 | FROM FDR |

| Tc | Length | Slope | Velocity | Capacity | Description |
|----|--------|-------|----------|----------|-------------|
| | (feet) | | (ft/sec) | | |

6.0

Direct Entry, FROM FDR

Subcatchment OS-13A:

Runoff

6.10 cfs @

0.10 hrs, Volume=

0.050 af, Depth= 0.38"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 100-Year Duration=6 min, Inten=8.22 in/hr

| Area (ac) | C | Description |
|-----------|------|------------------|
| 0.300 | 0.96 | PAVEMENT/ROOF |
| 1.300 | 0.35 | LANDSCAPE |
| 1.600 | 0.46 | Weighted Average |

| Tc | Length | Slope | Velocity | Capacity | Description |
|----|--------|-------|----------|----------|-------------|
| | | | | (cfs) | |

6.0

Direct Entry, FROM FDR

El Paso County 100-Year Duration=6 min, Inten=8.22 in/hr

Prepared by WestWorks Engineering

Page 4

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Subcatchment OS-13B:

Runoff

= 1.66 cfs @ 0.10 hrs. Volume=

0.014 af, Depth= 0.33"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 100-Year Duration=6 min, Inten=8.22 in/hr

Area (ac)

Description

0.500 0.40 LANDSCAPE

C

Tc Length (min)

Slope Velocity

Capacity

Description

(feet)

(ft/ft)

(ft/sec)

(cfs)

6.0

Direct Entry,

Subcatchment OS-13C:

Runoff

15.12 cfs @

0.10 hrs. Volume=

0.125 af, Depth= 0.39"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 100-Year Duration=6 min, Inten=8.22 in/hr

| C Description | (ac) | Area | |
|---------------|------|------|--|
| C Des | (ac) | Area | |

0.800 0.96 PAVEMENT/ROOF

3.000 0.35 LANDSCAPE

3.800 0.48 Weighted Average

Slope

(ft/ft)

Tc Length (min) 6.0

Velocity Capacity Description

(ft/sec) (cfs)

Direct Entry, FROM FDR

Subcatchment OS-14:

Runoff

(feet)

54.58 cfs @

0.10 hrs, Volume=

0.451 af. Depth= 0.43"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 100-Year Duration=6 min, Inten=8.22 in/hr

(cfs)

Area (ac)

C Description

12.600 0.54 FROM FDR

Tc Length

Slope Velocity Capacity Description

(feet) (min)

(ft/ft)

(ft/sec)

Direct Entry, FROM FDR

6.2

El Paso County 100-Year Duration=6 min, Inten=8.22 in/hr

Prepared by WestWorks Engineering

Page 5

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Reach SD1:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area =

0.800 ac, Inflow Depth = 0.49" for 100-Year event

Inflow

3.94 cfs @

0.10 hrs, Volume=

0.032 af

Outflow

3.94 cfs @

0.10 hrs, Volume=

0.032 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Reach SD11:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area =

0.400 ac, Inflow Depth = 0.68" for 100-Year event

Inflow = Outflow

2.75 cfs @ 2.75 cfs @

0.10 hrs, Volume= 0.10 hrs, Volume=

0.023 af

0.023 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Reach SD12:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area =

0.800 ac, Inflow Depth = 0.72" for 100-Year event

Inflow

5.82 cfs @ 0.10 hrs, Volume= 0.048 af

Outflow

5.82 cfs @ 0.10 hrs, Volume=

0.048 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Reach SD13:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area =

1.200 ac, Inflow Depth = 0.73" for 100-Year event

Inflow

8.90 cfs @

0.10 hrs, Volume=

0.073 af

Outflow

8.90 cfs @

0.10 hrs, Volume=

0.073 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Reach SD17:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area =

2.000 ac. Inflow Depth = 0.55" for 100-Year event

Inflow

11.19 cfs @

0.10 hrs, Volume=

0.092 af

Outflow

11.19 cfs @

0.10 hrs, Volume=

0.092 af, Atten= 0%, Lag= 0.0 min

El Paso County 100-Year Duration=6 min, Inten=8.22 in/hr

Prepared by WestWorks Engineering

Page 6

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Reach SD2:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 1.200 ac, Inflow Depth = 0.57" for 100-Year event Inflow = 0.057 af

Outflow = 6.91 cfs @ 0.10 hrs, Volume= 0.057 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Reach SD28:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 3.800 ac, Inflow Depth = 0.39" for 100-Year event 15.12 cfs @ 0.10 hrs, Volume= 0.125 af

Outflow = 15.12 cfs @ 0.10 hrs, Volume= 0.125 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Reach SD3:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 1.600 ac, Inflow Depth = 0.61" for 100-Year event Inflow = 9.83 cfs @ 0.10 hrs, Volume= 0.081 af

Outflow = 9.83 cfs @ 0.10 hrs, Volume= 0.081 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Reach SD5:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 1.900 ac, Inflow Depth = 0.63" for 100-Year event 12.10 cfs @ 0.10 hrs, Volume= 0.100 af

Outflow = 12.10 cfs @ 0.10 hrs, Volume= 0.100 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Reach SD6:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 2.200 ac, Inflow Depth = 0.63" for 100-Year event 14.01 cfs @ 0.10 hrs, Volume= 0.115 af

Outflow = 14.01 cfs @ 0.10 hrs, Volume= 0.115 af, Atten= 0%, Lag= 0.0 min

El Paso County 100-Year Duration=6 min, Inten=8.22 in/hr

Prepared by WestWorks Engineering

Page 7

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 1:

Inflow Area = 0.800 ac, Inflow Depth = 0.49" for 100-Year event

Inflow = 3.94 cfs @ 0.10 hrs, Volume= 0.032 af

Primary = 3.94 cfs @ 0.10 hrs, Volume= 0.032 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-3.00 hrs. dt= 0.01 hrs.

Link 2:

Inflow Area = 0.400 ac, Inflow Depth = 0.74" for 100-Year event

Inflow = 2.98 cfs @ 0.10 hrs, Volume= 0.025 af

Primary = 2.98 cfs @ 0.10 hrs, Volume= 0.025 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 3:

Inflow Area = 0.400 ac, Inflow Depth = 0.72" for 100-Year event 2.92 cfs @ 0.10 hrs, Volume= 0.024 af

Primary = 2.92 cfs @ 0.10 hrs, Volume= 0.024 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 7:

Inflow Area = 0.400 ac, Inflow Depth = 0.63" for 100-Year event 2.55 cfs @ 0.10 hrs, Volume= 0.021 af

Primary outflow = Inflow, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 8:

Inflow Area = 0.300 ac, Inflow Depth = 0.45" for 100-Year event

Inflow = 1.37 cfs @ 0.10 hrs, Volume= 0.011 af

Primary = 1.37 cfs @ 0.10 hrs, Volume= 0.011 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 11:

Inflow Area = 0.400 ac, Inflow Depth = 0.68" for 100-Year event Inflow = 0.75 cfs @ 0.10 hrs. Volume= 0.023 af

Primary = 2.75 cfs @ 0.10 hrs, Volume= 0.023 af, Atten= 0%, Lag= 0.0 min

El Paso County 100-Year Duration=6 min, Inten=8.22 in/hr

Prepared by WestWorks Engineering

Page 8

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Link 15:

Inflow Area = 0.500 ac, Inflow Depth = 0.70" for 100-Year event Inflow = 0.500 ac, Inflow Depth = 0.70" for 100-Year event 0.029 af

Primary = 3.52 cfs @ 0.10 hrs, Volume= 0.029 af 0.029 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 16:

Inflow Area = 2.000 ac, Inflow Depth = 0.55" for 100-Year event 11.19 cfs @ 0.10 hrs, Volume= 0.092 af

Primary = 11.19 cfs @ 0.10 hrs, Volume= 0.092 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 19:

Inflow Area = 0.600 ac, Inflow Depth = 0.39" for 100-Year event

Inflow = 2.34 cfs @ 0.10 hrs, Volume= 0.019 af

Primary = 2.34 cfs @ 0.10 hrs, Volume= 0.019 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 25:

Inflow Area = 3.800 ac, Inflow Depth = 0.39" for 100-Year event Inflow = 15.12 cfs @ 0.10 hrs, Volume= 0.125 af

Primary = 15.12 cfs @ 0.10 hrs, Volume= 0.125 af, Atten= 0%, Lag= 0.0 min

El Paso County 100-Year Duration=7 min, Inten=7.83 in/hr

Prepared by WestWorks Engineering

Page 1

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Subcatchment OS-11:

Runoff

13.79 cfs @

0.12 hrs, Volume=

0.136 af. Depth= 0.58"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 100-Year Duration=7 min, Inten=7.83 in/hr

Area (ac)

C Description

2.800 0.64

FROM FDR

Tc Length

Slope

Velocity (ft/sec)

Capacity Description

(min) (feet) 7.0

(ft/ft)

(cfs)

Direct Entry, FROM FDR

Reach SD14:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area =

3.700 ac, Inflow Depth = 0.63" for 100-Year event

Inflow

19.66 cfs @

0.12 hrs, Volume=

0.194 af

Outflow

19.66 cfs @

0.12 hrs, Volume=

0.194 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Reach SD15:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area =

4.100 ac, Inflow Depth = 0.64" for 100-Year event

Inflow

22.31 cfs @

0.12 hrs, Volume=

0.220 af

Outflow

22.31 cfs @

0.12 hrs, Volume=

0.220 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Reach SD16:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area =

5.300 ac, Inflow Depth = 0.68" for 100-Year event

Inflow

30.50 cfs @

0.11 hrs, Volume=

0.301 af

Outflow

30.50 cfs @

0.11 hrs, Volume=

0.301 af. Atten= 0%. Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

El Paso County 100-Year Duration=7 min, Inten=7.83 in/hr

Prepared by WestWorks Engineering

Page 2

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Reach SD18:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 7.800 ac, Inflow Depth = 0.67" for 100-Year event

Inflow = 44.43 cfs @ 0.11 hrs, Volume= 0.436 af

Outflow = 44.43 cfs @ 0.11 hrs, Volume= 0.436 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Reach SD26:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 10.200 ac, Inflow Depth = 0.09" for 100-Year event

Inflow = 0.32 cfs @ 0.23 hrs, Volume= 0.074 af

Outflow = 0.32 cfs @ 0.23 hrs, Volume= 0.074 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 13:

Inflow Area = 3.700 ac, Inflow Depth = 0.63" for 100-Year event 19.66 cfs @ 0.12 hrs, Volume= 0.194 af

Inflow = 19.66 cfs @ 0.12 hrs, Volume= 0.194 af Primary = 19.66 cfs @ 0.12 hrs, Volume= 0.194 af, Atten= 0%, Lag= 0.0 min

El Paso County 100-Year Duration=9 min, Inten=7.20 in/hr

Prepared by WestWorks Engineering

Page 1

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Subcatchment A9:

Runoff

1.82 cfs @

0.15 hrs, Volume=

0.023 af, Depth= 0.54"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 100-Year Duration=9 min, Inten=7.20 in/hr

Area (ac)

C Description

0.500

0.50 LANDSCAPE

Tc Length

Slope Velocity Capacity

Description

(min) (feet) (ft/ft)

(ft/sec)

(cfs)

9.0

Direct Entry,

Subcatchment C1:

Runoff

2.83 cfs @

0.15 hrs, Volume=

0.035 af, Depth= 0.70"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 100-Year Duration=9 min, Inten=7.20 in/hr

| Area | (ac) | С | Description |
|------|------|---|-------------|
| • | | | |

LANDSCAPE 0.300 0.35 **PAVEMENT** 0.300 0.96

0.600 0.65 Weighted Average

(min)

Capacity Slope Velocity (ft/ft)

Description

Tc Length

(feet)

(ft/sec)

(cfs)

9.0

Direct Entry,

Link 9:

Inflow Area =

0.500 ac, Inflow Depth = 0.54" for 100-Year event

Inflow Primary 1.82 cfs @ 1.82 cfs @

0.15 hrs, Volume=

0.15 hrs, Volume=

0.023 af 0.023 af, Atten= 0%, Lag= 0.0 min

El Paso County 100-Year Duration=11 min, Inten=6.69 in/hr

Prepared by WestWorks Engineering

Page 1

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Subcatchment A6:

Runoff

= 5.7

5.70 cfs @

0.18 hrs, Volume=

0.088 af, Depth= 0.96"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 100-Year Duration=11 min. Inten=6.69 in/hr

| Area (ac) | С | Description |
|-----------|------|-------------|
| 0.300 | 0.35 | LANDSCAPE |
| 0.100 | 0.81 | ROOFTOP |
| 0.700 | 0.96 | PAVEMENT |

1.100 0.78 Weighted Average

| Tc | Length | Slope | Velocity | Capacity | Description |
|------------------|--|-------|----------|----------|-------------|
| | | | | (cfs) | |
| Version in terms | The second secon | 77 | | | |

11.0

Direct Entry,

Subcatchment C2:

Runoff

5.18 cfs @

s @ 0.18 hrs, Volume=

0.080 af, Depth= 0.80"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs El Paso County 100-Year Duration=11 min, Inten=6.69 in/hr

| | Area (ac) | С | Description |
|-----|-----------|------|------------------|
| | 0.600 | 0.35 | LANDSCAPE |
| | 0.600 | 0.96 | PAVEMENT |
| Res | 1 200 | O GE | Mainleted Avenue |

1.200 0.65 Weighted Average

| Tc | Length | Slope | Velocity | Capacity | Description |
|--------------|--------|---------|----------|----------|-------------|
| <u>(min)</u> | (feet) | (ft/ft) | (ft/sec) | (cfs) | |

11.0

Direct Entry,

Reach SD7:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 3.100 ac, Inflow Depth = 0.74" for 100-Year event

for 100-Year event 0.190 af

Inflow = 11.28 cfs @ Outflow = 11.28 cfs @

11.28 cfs @ 0.14 hrs, Volume= 11.28 cfs @ 0.14 hrs, Volume=

0.190 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Reach SD8:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 3.400 ac, Inflow Depth = 0.73" for 100-Year event 12.39 cfs @ 0.14 hrs, Volume= 0.207 af

Outflow = 12.39 cfs @ 0.14 hrs, Volume= 0.207 af, Atten= 0%, Lag= 0.0 min

El Paso County 100-Year Duration=11 min, Inten=6.69 in/hr

Prepared by WestWorks Engineering

Page 2

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Reach SD9:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area =

6.100 ac, Inflow Depth = 0.15" for 100-Year event

Inflow

1.83 cfs @

0.32 hrs, Volume=

0.074 af

Outflow

1.83 cfs @

0.32 hrs, Volume=

0.074 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 6:

Inflow Area =

2.700 ac, Inflow Depth = 0.72" for 100-Year event

Inflow = Primary

10.65 cfs @ 9.20 cfs @

0.18 hrs, Volume= 0.14 hrs, Volume=

0.159 af, Atten= 14%, Lag= 0.0 min

Secondary =

1.45 cfs @

0.18 hrs, Volume=

0.004 af

0.163 af

Primary outflow = Inflow below 9.20 cfs, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 23:

Inflow Area =

1.200 ac, Inflow Depth = 0.89" for 100-Year event

6.07 cfs @ 0.18 hrs, Volume=

Inflow = Primary

6.07 cfs @ 0.18 hrs, Volume=

0.089 af 0.089 af, Atten= 0%, Lag= 0.0 min

El Paso County 100-Year Duration=20 min, Inten=5.19 in/hr

Prepared by WestWorks Engineering

Page 1

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Reach SD23:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area =

0.600 ac, Inflow Depth = 5.92" for 100-Year event

Inflow =

14.15 cfs @

0.15 hrs, Volume=

0.296 af

Outflow

14.15 cfs @

0.15 hrs, Volume=

0.296 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Reach SD24:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area =

78.100 ac, Inflow Depth = 0.27" for 100-Year event

1.741 af

Inflow = Outflow =

46.90 cfs @ 46.90 cfs @

0.10 hrs, Volume= 0.10 hrs, Volume=

1.741 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs. dt= 0.01 hrs.

Reach SD25:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area =

88.600 ac. Inflow Depth = 0.34" for 100-Year event

Inflow

=

72.52 cfs @

0.33 hrs. Volume=

2.528 af

Outflow

72.52 cfs @ 0.33 hrs, Volume=

2.528 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 21:

Inflow Area =

78.100 ac, Inflow Depth = 0.30" for 100-Year event

Inflow Primary

59.01 cfs @ 46.90 cfs @

0.15 hrs. Volume= 0.10 hrs, Volume= 1.981 af

Secondary =

12.11 cfs @

0.15 hrs, Volume=

1.741 af, Atten= 21%, Lag= 0.0 min 0.240 af

Primary outflow = Inflow below 46.90 cfs, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 22:

Inflow Area =

0.600 ac, Inflow Depth = 5.92" for 100-Year event

Inflow =

14.15 cfs @

0.15 hrs, Volume=

0.296 af

Primary

14.15 cfs @ 0.15 hrs, Volume=

0.296 af, Atten= 0%, Lag= 0.0 min

El Paso County 100-Year Duration=20 min, Inten=5.19 in/hr

Prepared by WestWorks Engineering

Page 2

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Link DP-OS11: FLOW-BY

Inflow Area = 65.500 ac, Inflow Depth = 0.27" for 100-Year event

Inflow 54.10 cfs @ 0.33 hrs, Volume= 1.475 af

Primary = 23.40 cfs @ 0.15 hrs, Volume= 1.000 af, Atten= 57%, Lag= 0.0 min

Secondary = 30.70 cfs @ 0.33 hrs, Volume= 0.475 af

Primary outflow = Inflow below 23.40 cfs, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

23 Point hydrograph entered manually, To= 0.00 hrs, dt= 0.03 hrs, Area= 65.500 ac, cfs =

0.00 4.90 9.80 14.80 19.70 24.60 29.50 34.40 39.30 44.30 49.20 54.10 49.20 44.30 39.30 34.40 29.50 24.60 19.70 14.80

9.80 4.90 0.00

El Paso County 100-Year Duration=25 min. Inten=4.62 in/hr

Prepared by WestWorks Engineering

Page 1

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Reach SD21:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area =

2.800 ac, Inflow Depth = 14.86" for 100-Year event

Inflow =

99.65 cfs @

0.42 hrs, Volume=

3.466 af

Outflow

99.65 cfs @

0.42 hrs, Volume=

3.466 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Reach SD22:

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area =

13.000 ac, Inflow Depth = 3.68" for 100-Year event

Inflow Outflow =

104.88 cfs @ 104.88 cfs @

0.42 hrs, Volume= 0.42 hrs. Volume= 3.983 af

3.983 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 009: BASIN 009

Inflow Area =

=

101.600 ac, Inflow Depth = 0.79" for 100-Year event

Inflow

171.59 cfs @

0.42 hrs, Volume=

6.715 af

Primary

171.59 cfs @

0.42 hrs, Volume=

6.715 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-3.00 hrs. dt= 0.01 hrs.

Link 20:

Inflow Area =

2.800 ac, Inflow Depth = 14.86" for 100-Year event

Inflow = 99.65 cfs @

0.42 hrs, Volume=

3.466 af

Primary

99.65 cfs @

0.42 hrs, Volume=

3.466 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-3.00 hrs. dt= 0.01 hrs.

Link DP-OS2:

Inflow

92.10 cfs @

0.42 hrs, Volume=

3.197 af

Primary =

92.10 cfs @

0.42 hrs, Volume=

3.197 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

29 Point hydrograph entered manually, To= 0.00 hrs, dt= 0.03 hrs, Area= 0.000 ac, cfs = 0.00 6.60 13.20

19.70 85.50

26.30 32.90 92.10 85.50

39.50 78.90

46.10 72.40 52.60 59.20 65.80

72.40 78.90

32.90

13.20

6.60

65.80 52.60

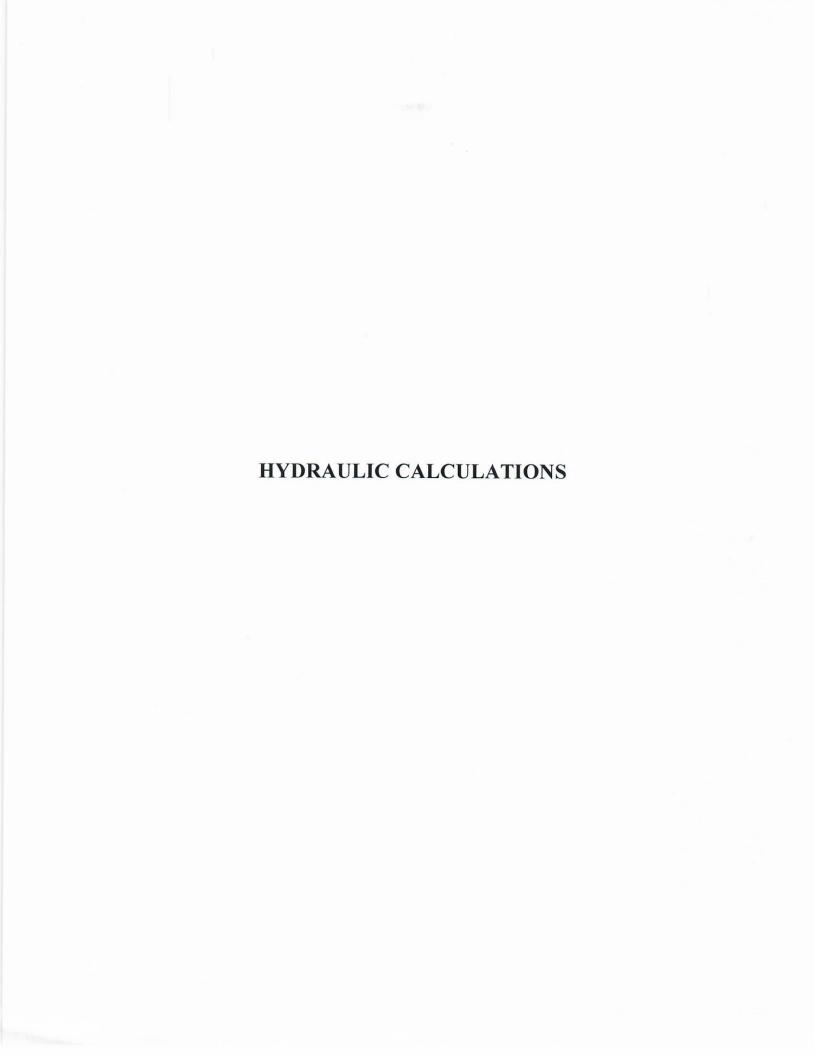
46.10 39.50

26.30

19.70

0.00

59.20



Version 4.05 Released March 2017

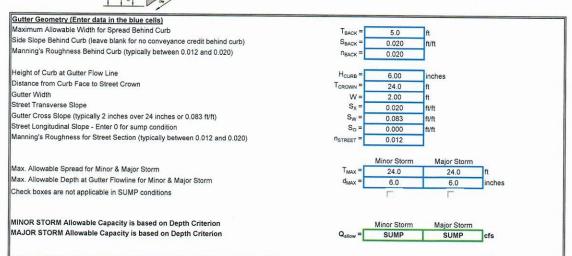
ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: ELDORADO SPRINGS
Inlet ID: DP-1

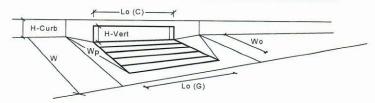
Tokon

Toko



INLET IN A SUMP OR SAG LOCATION

Version 4.05 Released March 2017



| Design Information (Input) CDOT Type R Curb Opening | | MINOR | MAJOR | |
|--|-----------------------------|--------------------------|-------|-----------------|
| ype of inlet | Type = | CDOT Type R Curb Opening | | 7 |
| Local Depression (additional to continuous gutter depression 'a' from above) | a _{local} = | 3.00 | 3 00 | inches |
| Number of Unit Inlets (Grate or Curb Opening) | No = | 1 | 1 | |
| Nater Depth at Flowline (outside of local depression) | Ponding Depth = | 6.0 | 6.0 | inches |
| Grate Information | _ | MINOR | MAJOR | Override Depths |
| ength of a Unit Grate | L _o (G) = | N/A | N/A | feet |
| Nidth of a Unit Grate | W _o = | N/A | N/A | feet |
| Area Opening Ratio for a Grate (typical values 0.15-0.90) | A _{ratio} = | N/A | N/A | |
| Clogging Factor for a Single Grate (typical value 0.50 - 0.70) | C _f (G) = | N/A | N/A | |
| Grate Weir Coefficient (typical value 2.15 - 3.60) | C _w (G) = | N/A | N/A | |
| Grate Orifice Coefficient (typical value 0.60 - 0.80) | C _o (G) = | N/A | N/A | - |
| Curb Opening Information | | MINOR | MAJOR | _ |
| ength of a Unit Curb Opening | L _o (C) = | 5.00 | 5 00 | Treet |
| leight of Vertical Curb Opening in Inches | H _{vert} = | 6.00 | 6.00 | inches |
| Height of Curb Orifice Throat in Inches | H _{throat} = | 6.00 | 6.00 | inches |
| Angle of Throat (see USDCM Figure ST-5) | Theta = | 63.40 | 63.40 | degrees |
| Side Width for Depression Pan (typically the gutter width of 2 feet) | W _p = | 2.00 | 2.00 | feet |
| Clogging Factor for a Single Curb Opening (typical value 0.10) | $C_{f}(C) =$ | 0.10 | 0.10 | |
| Curb Opening Weir Coefficient (typical value 2.3-3.7) | C _w (C) = | 3.60 | 3,60 | - |
| Curb Opening Orifice Coefficient (typical value 0.60 - 0.70) | C _o (C) = | 0.67 | 0.67 | |
| ow Head Performance Reduction (Calculated) | | MINOR | MAJOR | |
| Depth for Grate Midwidth | d _{Grate} = | N/A | N/A | T ft |
| Pepth for Curb Opening Weir Equation | d _{Curb} = | 0.33 | 0.33 | ft |
| Combination Inlet Performance Reduction Factor for Long Inlets | RF _{Combination} = | 0.77 | 0.77 | 1 |
| Curb Opening Performance Reduction Factor for Long Inlets | RF _{Curb} = | 1.00 | 1.00 | 1 |
| Grated Inlet Performance Reduction Factor for Long Inlets | RF _{Grate} = | N/A | N/A | 1 |
| | | MINOR | MAJOR | |
| otal Inlet Interception Capacity (assumes clogged condition) | $Q_a =$ | 5.4 | 5.4 | cfs |
| nlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK) | Q PEAK REQUIRED = | 2.0 | 4.0 | cfs |

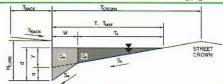
Version 4.05 Released March 2017

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)
ELDORADO SPRINGS

Project: Inlet ID:

DP-2



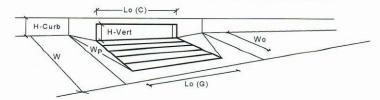
Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb TBACK = 5.0 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) SBACK = 0.020 ft/ft Manning's Roughness Behind Curb (typically between 0.012 and 0.020) **NBACK** 0.020 Height of Curb at Gutter Flow Line H_{CURB} = 6.00 inches Distance from Curb Face to Street Crown TCROWN 24.0 Gutter Width W= 2.00 Street Transverse Slope Sx = 0.020 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) S_W = 0.083 ft/ft Street Longitudinal Slope - Enter 0 for sump condition So: 0.000 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) n_{STREET} = 0.012 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm Max. Allowable Depth at Gutter Flowline for Minor & Major Storm 6.0 6.0 Check boxes are not applicable in SUMP conditions MINOR STORM Allowable Capacity is based on Depth Criterion MAJOR STORM Allowable Capacity is based on Depth Criterion Minor Storm Major Storm

SUMP

SUMP

INLET IN A SUMP OR SAG LOCATION

Version 4.05 Released March 2017



| Design Information (Input) CDOT Type R Curb Opening ▼ | | MINOR | MAJOR | |
|---|-----------------------------|--------------------------|-------|-----------------|
| Type of Inlet CDOT Type R Curb Opening | Type = | CDOT Type R Curb Opening | | 7 |
| ocal Depression (additional to continuous gutter depression 'a' from above) | a _{local} = | 3.00 | 3.00 | inches |
| Number of Unit Inlets (Grate or Curb Opening) | No = | 1 | 1 | |
| Nater Depth at Flowline (outside of local depression) | Ponding Depth = | 6.0 | 6.0 | inches |
| Grate Information | | MINOR | MAJOR | Override Depths |
| ength of a Unit Grate | L _o (G) = | N/A | N/A | feet |
| Nidth of a Unit Grate | W _o = | N/A | N/A | feet |
| Area Opening Ratio for a Grate (typical values 0.15-0.90) | A _{ratio} = | N/A | N/A | |
| Clogging Factor for a Single Grate (typical value 0.50 - 0.70) | C _f (G) = | N/A | N/A | |
| Grate Weir Coefficient (typical value 2.15 - 3.60) | C _w (G) = | N/A | N/A | |
| Grate Orifice Coefficient (typical value 0.60 - 0.80) | C _o (G) = | N/A | N/A | |
| Curb Opening Information | | MINOR | MAJOR | |
| ength of a Unit Curb Opening | L _o (C) = | 5.00 | 5.00 | feet |
| Height of Vertical Curb Opening in Inches | H _{vert} = | 6.00 | 6.00 | inches |
| Height of Curb Orifice Throat in Inches | H _{throat} = | 6.00 | 6.00 | inches |
| Angle of Throat (see USDCM Figure ST-5) | Theta = | 63.40 | 63.40 | degrees |
| Side Width for Depression Pan (typically the gutter width of 2 feet) | W _p = | 2.00 | 2.00 | feet |
| Clogging Factor for a Single Curb Opening (typical value 0.10) | $C_{f}(C) =$ | 0.10 | 0.10 | |
| Curb Opening Weir Coefficient (typical value 2.3-3.7) | C _w (C) = | 3.60 | 3,60 | |
| Curb Opening Orifice Coefficient (typical value 0.60 - 0.70) | C _o (C) = | 0.67 | 0.67 | |
| ow Head Performance Reduction (Calculated) | | MINOR | MAJOR | |
| Depth for Grate Midwidth | d _{Grate} = | N/A | N/A | ft |
| Depth for Curb Opening Weir Equation | d _{Curb} = | 0.33 | 0.33 | ft |
| Combination Inlet Performance Reduction Factor for Long Inlets | RF _{Combination} = | 0.77 | 0.77 | |
| Curb Opening Performance Reduction Factor for Long Inlets | RF _{Curb} = | 1.00 | 1.00 | |
| Grated Inlet Performance Reduction Factor for Long Inlets | RF _{Grate} = | N/A | N/A | |
| | | MINOR | MAJOR | |
| Total Inlet Interception Capacity (assumes clogged condition) | $Q_a =$ | 5.4 | 5.4 | cfs |
| nlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK) | Q PEAK REQUIRED = | 2.0 | 3.0 | cfs |

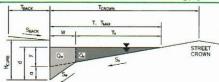
ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

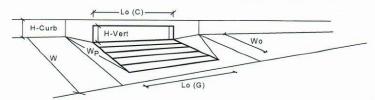
ELDORADO SPRINGS

DP-3

Project: Inlet ID:



| Gutter Geometry (Enter data in the blue cells) | | | _ | |
|--|-----------------------|-------------|------------------|--------|
| Maximum Allowable Width for Spread Behind Curb | T _{BACK} = | 5.0 | ft | |
| Side Slope Behind Curb (leave blank for no conveyance credit behind curb) | S _{BACK} = | 0.020 | ft/ft | |
| Manning's Roughness Behind Curb (typically between 0.012 and 0.020) | n _{BACK} = | 0.020 |] | |
| Height of Curb at Gutter Flow Line | H _{CURB} = | 6.00 | inches | |
| Distance from Curb Face to Street Crown | T _{CROWN} = | 24.0 | ft | |
| Gutter Width | W= | 3.00 | ft | |
| Street Transverse Slope | S _X = | 0.020 | ft/ft | |
| Sutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) | S _W = | 0.083 | ft/ft | |
| Street Longitudinal Slope - Enter 0 for sump condition | So = | 0.000 | ft/ft | |
| Manning's Roughness for Street Section (typically between 0.012 and 0.020) | n _{street} = | 0.012 | | |
| | | Minor Storm | Major Storm | |
| Max. Allowable Spread for Minor & Major Storm | T _{MAX} = | 24.0 | 24.0 | ft |
| Max. Allowable Depth at Gutter Flowline for Minor & Major Storm | d _{MAX} = | 6.0 | 6.0 | inches |
| Check boxes are not applicable in SUMP conditions | _ | Г | Г | _ |
| MINOR STORM Allowable Capacity is based on Depth Criterion | | Minor Storm | Major Storm | |
| MAJOR STORM Allowable Capacity is based on Depth Criterion | Q _{allow} = | SUMP | Major Storm SUMP | cfs |



| Design Information (Input) | CDOT Type C Grate ▼ | | MINOR | MAJOR | |
|------------------------------------|--|-----------------------------|---------|------------|-----------------|
| Type of Inlet | 1 | Type = | CDOT Ty | oe C Grate | |
| Local Depression (additional to | continuous gutter depression 'a' from above) | a _{local} = | 6.00 | 6.00 | inches |
| Number of Unit Inlets (Grate or | Curb Opening) | No = | 1 | 1 | |
| Water Depth at Flowline (outsid | e of local depression) | Ponding Depth = | 6.0 | 6.0 | inches |
| Grate Information | | | MINOR | MAJOR | Override Depths |
| Length of a Unit Grate | | L _o (G) = | 2.92 | 2.92 | feet |
| Width of a Unit Grate | | W _o = | 2.92 | 2.92 | feet |
| Area Opening Ratio for a Grate | , , | A _{ratio} = | 0.70 | 0.70 | |
| Clogging Factor for a Single Gra | ate (typical value 0.50 - 0.70) | $C_f(G) =$ | 0.50 | 0.50 | |
| Grate Weir Coefficient (typical v | alue 2.15 - 3.60) | C _w (G) = | 2.41 | 2.41 | |
| Grate Orifice Coefficient (typical | value 0.60 - 0.80) | C _o (G) = | 0.67 | 0.67 | |
| Curb Opening Information | | | MINOR | MAJOR | _ |
| Length of a Unit Curb Opening | | L _o (C) = | N/A | N/A | feet |
| Height of Vertical Curb Opening | in Inches | H _{vert} = | N/A | N/A | inches |
| Height of Curb Orifice Throat in | Inches | H _{throat} = | N/A | N/A | inches |
| Angle of Throat (see USDCM Fi | gure ST-5) | Theta = | N/A | N/A | degrees |
| Side Width for Depression Pan (| (typically the gutter width of 2 feet) | W _p = | N/A | N/A | feet |
| Clogging Factor for a Single Cur | rb Opening (typical value 0.10) | $C_f(C) =$ | N/A | N/A | |
| Curb Opening Weir Coefficient (| typical value 2.3-3.7) | C _w (C) = | N/A | N/A | - |
| Curb Opening Orifice Coefficien | t (typical value 0.60 - 0.70) | C _o (C) = | N/A | N/A | |
| Low Head Performance Reduc | ction (Calculated) | | MINOR | MAJOR | |
| Depth for Grate Midwidth | | d _{Grate} = | 0.635 | 0.635 | ft |
| Depth for Curb Opening Weir Ed | quation | d _{Curb} = | N/A | N/A | ft |
| | Reduction Factor for Long Inlets | RF _{Combination} = | N/A | N/A | |
| Curb Opening Performance Rec | | RF _{Curb} = | N/A | N/A | |
| Grated Inlet Performance Reduc | tion Factor for Long Inlets | RF _{Grate} = | 0.95 | 0.95 | |
| | | 2.1 | MINOR | MAJOR | |
| Total Inlet Interception C | apacity (assumes clogged condition) | Q _a = | 4.2 | 4.2 | cfs |
| nlet Capacity IS GOOD for Min | nor and Major Storms(>Q PEAK) | Q PEAK REQUIRED = | 2.0 | 3.0 | cfs |

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) ELDORADO SPRINGS Project: Inlet ID: DP-4 STREET Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb TBACK = 5.0 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) Manning's Roughness Behind Curb (typically between 0.012 and 0.020) SBACK 0.020 ft/ft 0.020 Height of Curb at Gutter Flow Line H_{CURB} 6.00 inches Distance from Curb Face to Street Crown TCROWN 24.0 Gutter Width W= 2.00 Street Transverse Slope Sx = 0.020 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) S_W : 0.083 ft/ft Street Longitudinal Slope - Enter 0 for sump condition So 0.000 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) n_{STREET} = 0.012 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm 24.0 24.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm 6.0 6.0 Check boxes are not applicable in SUMP conditions

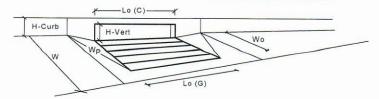
Minor Storm

SUMP

Major Storm

SUMP

MINOR STORM Allowable Capacity is based on Depth Criterion MAJOR STORM Allowable Capacity is based on Depth Criterion



| Design Information (Input) CDOT Type R Curb Opening | | MINOR | MAJOR | |
|--|-----------------------------|-------------|--------------|-----------------|
| Type of Inlet | Type = | CDOT Type R | Curb Opening | |
| Local Depression (additional to continuous gutter depression 'a' from above) | a _{local} = | 3.00 | 3.00 | inches |
| Number of Unit Inlets (Grate or Curb Opening) | No = | 1 | 1 | |
| Water Depth at Flowline (outside of local depression) | Ponding Depth = | 6.0 | 6.0 | inches |
| Grate Information | | MINOR | MAJOR | Override Depths |
| Length of a Unit Grate | L _o (G) = | N/A | N/A | feet |
| Width of a Unit Grate | W _o = | N/A | N/A | feet |
| Area Opening Ratio for a Grate (typical values 0.15-0.90) | A _{ratio} = | N/A | N/A | |
| Clogging Factor for a Single Grate (typical value 0.50 - 0.70) | C _f (G) = | N/A | N/A | 7 |
| Grate Weir Coefficient (typical value 2.15 - 3.60) | C _w (G) = | N/A | N/A | |
| Grate Orifice Coefficient (typical value 0.60 - 0.80) | C _o (G) = | N/A | N/A | |
| Curb Opening Information | | MINOR | MAJOR | _ |
| Length of a Unit Curb Opening | L _o (C) = | 5.00 | 5.00 | feet |
| Height of Vertical Curb Opening in Inches | H _{vert} = | 6.00 | 6.00 | inches |
| Height of Curb Orifice Throat in Inches | H _{throat} = | 6.00 | 6.00 | inches |
| Angle of Throat (see USDCM Figure ST-5) | Theta = | 63.40 | 63.40 | degrees |
| Side Width for Depression Pan (typically the gutter width of 2 feet) | W _p = | 2.00 | 2.00 | feet |
| Clogging Factor for a Single Curb Opening (typical value 0.10) | $C_{f}(C) =$ | 0.10 | 0.10 | |
| Curb Opening Weir Coefficient (typical value 2.3-3.7) | C _w (C) = | 3.60 | 3.60 | |
| Curb Opening Orifice Coefficient (typical value 0.60 - 0.70) | C _o (C) = | 0.67 | 0.67 | |
| Low Head Performance Reduction (Calculated) | | MINOR | MAJOR | |
| Depth for Grate Midwidth | d _{Grate} = | N/A | N/A | Tft . |
| Depth for Curb Opening Weir Equation | d _{Curb} = | 0.33 | 0.33 | ft |
| Combination Inlet Performance Reduction Factor for Long Inlets | RF _{Combination} = | 0.77 | 0.77 | |
| Curb Opening Performance Reduction Factor for Long Inlets | RF _{Curb} = | 1.00 | 1.00 | |
| Grated Inlet Performance Reduction Factor for Long Inlets | RF _{Grate} = | N/A | N/A | |
| | _ | MINOR | MAJOR | |
| Total Inlet Interception Capacity (assumes clogged condition) | Q _a = | 5.4 | 5.4 | cfs |
| nlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK) | Q PEAK REQUIRED = | 1.0 | 2.0 | cfs |

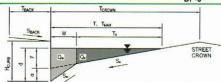
ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

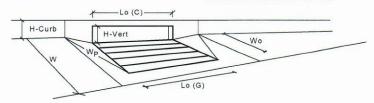
ELDORADO SPRINGS

DP-5

Project: Inlet ID:



| Gutter Geometry (Enter data in the blue cells) | | | | |
|--|-----------------------|-------------|-------------|-------------|
| Maximum Allowable Width for Spread Behind Curb | TBACK = | 5.0 | ft | |
| Side Slope Behind Curb (leave blank for no conveyance credit behind curb) | S _{BACK} = | 0.020 | ft/ft | |
| Manning's Roughness Behind Curb (typically between 0.012 and 0.020) | n _{BACK} = | 0.020 | | |
| Height of Curb at Gutter Flow Line | H _{CURB} = | 6.00 | inches | |
| Distance from Curb Face to Street Crown | T _{CROWN} = | 24.0 | ft | |
| Gutter Width | W = | 2.00 | ft | |
| Street Transverse Slope | S _X = | 0.020 | ft/ft | |
| Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) | S _W = | 0.083 | ft/ft | |
| Street Longitudinal Slope - Enter 0 for sump condition | So= | 0.000 | ft/ft | |
| Manning's Roughness for Street Section (typically between 0.012 and 0.020) | n _{street} = | 0.012 | | |
| | | Minor Storm | Major Storm | |
| Max. Allowable Spread for Minor & Major Storm | T _{MAX} = | 24.0 | 24.0 | ft |
| Max. Allowable Depth at Gutter Flowline for Minor & Major Storm | d _{MAX} = | 6.0 | 6.0 | inches |
| Check boxes are not applicable in SUMP conditions | _ | Г | | Proposition |
| MINOR STORM Allowable Capacity is based on Depth Criterion | | Minor Storm | Major Storm | |
| | Q _{allow} = | SUMP | SUMP | cfs |



| Design Information (Input) | | MINOR | MAJOR | |
|--|-----------------------------|-------------|--------------|-----------------|
| Type of Inlet CDOT Type R Curb Opening | Type = | CDOT Type R | Curb Opening | |
| Local Depression (additional to continuous gutter depression 'a' from above) | a _{local} = | 3.00 | 3 00 | inches |
| Number of Unit Inlets (Grate or Curb Opening) | No = | 1 | 1 | |
| Nater Depth at Flowline (outside of local depression) | Ponding Depth = | 6.0 | 6.0 | inches |
| Grate Information | | MINOR | MAJOR | Override Depths |
| Length of a Unit Grate | L _o (G) = | N/A | N/A | feet |
| Width of a Unit Grate | W _o = | N/A | N/A | feet |
| Area Opening Ratio for a Grate (typical values 0.15-0.90) | A _{ratio} = | N/A | N/A | |
| Clogging Factor for a Single Grate (typical value 0.50 - 0.70) | $C_{f}(G) =$ | N/A | N/A | |
| Grate Weir Coefficient (typical value 2.15 - 3.60) | C _w (G) = | N/A | N/A | |
| Grate Orifice Coefficient (typical value 0.60 - 0.80) | C _o (G) = | N/A | N/A | |
| Curb Opening Information | 12- | MINOR | MAJOR | |
| Length of a Unit Curb Opening | L _o (C) = | 5.00 | 5 00 | feet |
| Height of Vertical Curb Opening in Inches | H _{vert} = | 6.00 | 6.00 | inches |
| Height of Curb Orifice Throat in Inches | H _{throat} = | 6.00 | 6.00 | inches |
| Angle of Throat (see USDCM Figure ST-5) | Theta = | 63.40 | 63.40 | degrees |
| Side Width for Depression Pan (typically the gutter width of 2 feet) | W _p = | 2.00 | 2.00 | feet |
| Clogging Factor for a Single Curb Opening (typical value 0.10) | $C_f(C) =$ | 0.10 | 0.10 | |
| Curb Opening Weir Coefficient (typical value 2.3-3.7) | C _w (C) = | 3.60 | 3.60 | |
| Curb Opening Orifice Coefficient (typical value 0.60 - 0.70) | C _o (C) = | 0.67 | 0.67 | |
| ow Head Performance Reduction (Calculated) | | MINOR | MAJOR | |
| Depth for Grate Midwidth | d _{Grate} = | N/A | N/A | ft |
| Depth for Curb Opening Weir Equation | d _{Curb} = | 0.33 | 0.33 | ft |
| Combination Inlet Performance Reduction Factor for Long Inlets | RF _{Combination} = | 0.77 | 0.77 | |
| Curb Opening Performance Reduction Factor for Long Inlets | RF _{Curb} = | 1.00 | 1.00 | |
| Grated Inlet Performance Reduction Factor for Long Inlets | RF _{Grate} = | N/A | N/A | |
| | - | MINOR | MAJOR | _ |
| Total Inlet Interception Capacity (assumes clogged condition) | Q _a = | 5.4 | 5.4 | cfs |
| nlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK) | Q PEAK REQUIRED = | 1.0 | 2.0 | cfs |

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) ELDORADO SPRINGS Project: Inlet ID: DP-6 STREET Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb 10.0 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) SBACK : 0.020 ft/ft Manning's Roughness Behind Curb (typically between 0.012 and 0.020) 0.020 Height of Curb at Gutter Flow Line H_{CURB} : 6.00 inches Distance from Curb Face to Street Crown 26.0 Gutter Width W= 2.00 S_x = Street Transverse Slope ft/ft 0.020 Sw: Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) 0.083 ft/ft Street Longitudinal Slope - Enter 0 for sump condition So 0.030 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) 0.012 n_{STREET} = Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm T_{MAX} 26.0 26.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm

6.0

Minor Storm 23.7

8.0

Major Storm

50.4

inches

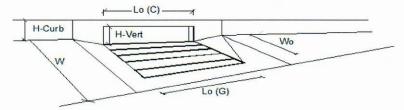
check = yes

Allow Flow Depth at Street Crown (leave blank for no)

MINOR STORM Allowable Capacity is based on Depth Criterion MAJOR STORM Allowable Capacity is based on Depth Criterion

Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management' Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

INLET ON A CONTINUOUS GRADE

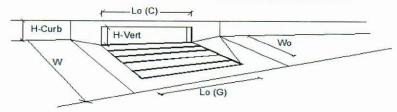


| Design Information (Input) | CODOT T B C C | 9 | MINOR | MAJOR | |
|---|---|----------------------|-------------|--------------|--------|
| Type of Inlet | CDOT Type R Curb Opening | Type = | CDOT Type R | Curb Opening | |
| Local Depression (additional to o | ontinuous gutter depression 'a') | a _{LOCAL} = | 3.0 | 3.0 | inches |
| Total Number of Units in the Inle | t (Grate or Curb Opening) | No = | 1 | 1 | |
| Length of a Single Unit Inlet (Gra | te or Curb Opening) | L _o = | 15.00 | 15.00 | ft |
| Width of a Unit Grate (cannot be | greater than W, Gutter Width) | W _o = | N/A | N/A | ft |
| Clogging Factor for a Single Un | it Grate (typical min. value = 0.5) | CrG = | N/A | N/A | |
| Clogging Factor for a Single Uni | t Curb Opening (typical min. value = 0.1) | CrC = | 0.10 | 0.10 | |
| Street Hydraulics: OK - Q < All | owable Street Capacity' | | MINOR | MAJOR | |
| Total Inlet Interception Capaci | ty | Q= | 4.4 | 9.2 | cfs |
| Total Inlet Carry-Over Flow (flo | ow bypassing inlet) | Q _b = | 0.0 | 1.5 | cfs |
| Capture Percentage = Q ₃ /Q ₀ = | | C% = | 100 | 86 | % |

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) ELDORADO SPRINGS Project: Inlet ID: DP-8 STREET Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb TBACK 10.0 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) SBACK 0.020 ft/ft Manning's Roughness Behind Curb (typically between 0.012 and 0.020) 0.020 Height of Curb at Gutter Flow Line H_{CURB} 6.00 inches Distance from Curb Face to Street Crown TCROWN 26.0 Gutter Width W= 2.00 Street Transverse Slope Sx = 0.020 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) Sw = 0.083 ft/ft Street Longitudinal Slope - Enter 0 for sump condition So= 0.030 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) n_{STREET} = 0.012 Minor Storm Max. Allowable Spread for Minor & Major Storm 26.0 26.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm 6.0 inches Allow Flow Depth at Street Crown (leave blank for no) check = yes MINOR STORM Allowable Capacity is based on Depth Criterion Minor Storm Major Storm MAJOR STORM Allowable Capacity is based on Depth Criterion 23.7 50.4 Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

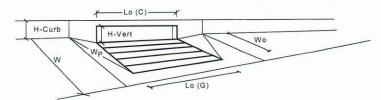
flajor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

INLET ON A CONTINUOUS GRADE



| Design Information (Input) | CDOT Type R Curb Opening | - | 100 | MINOR | MAJOR | |
|---|---|---|----------------------|-------------|--------------|--------|
| Type of Inlet | CDO1 Type R Curb Opening | | Type = | CDOT Type R | Curb Opening | |
| Local Depression (additional to c | ontinuous gutter depression 'a') | | a _{LOCAL} = | 3.0 | 3.0 | inches |
| Total Number of Units in the Inlet | (Grate or Curb Opening) | | No = | 1 | 1 | |
| Length of a Single Unit Inlet (Gra | te or Curb Opening) | | L _o = | 5.00 | 5,00 | ft |
| Width of a Unit Grate (cannot be | greater than W, Gutter Width) | | W _o = | N/A | N/A | ft |
| Clogging Factor for a Single Uni | t Grate (typical min. value = 0.5) | | CrG = | N/A | N/A | 7 |
| Clogging Factor for a Single Unit | Curb Opening (typical min. value = 0.1) | | CrC = | 0.10 | 0.10 | 7 |
| Street Hydraulics: OK - Q < Alle | owable Street Capacity' | | | MINOR | MAJOR | |
| Total Inlet Interception Capacit | у | | Q = | 0.5 | 1.2 | cfs |
| Total Inlet Carry-Over Flow (flo | w bypassing inlet) | | Q _b = | 0.0 | 0.1 | cfs |
| Capture Percentage = Q _a /Q _o = | | | C% = | 100 | 94 | % |

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) ELDORADO SPRINGS Project: Inlet ID: DP-10 STREET Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb 0.0 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) SBACK : 0.020 ft/ft Manning's Roughness Behind Curb (typically between 0.012 and 0.020) 0.020 Height of Curb at Gutter Flow Line H_{CURB} 6.00 Distance from Curb Face to Street Crown 24.0 Gutter Width W= 3.00 Street Transverse Slope S_X = 0.020 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) Sw: 0.083 ft/ft Street Longitudinal Slope - Enter 0 for sump condition So: 0.000 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) n_{STREET} 0.012 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm 24.0 24.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm 6.0 6.0 Check boxes are not applicable in SUMP conditions MINOR STORM Allowable Capacity is based on Depth Criterion MAJOR STORM Allowable Capacity is based on Depth Criterion Minor Storm Major Storm SUMP SUMP

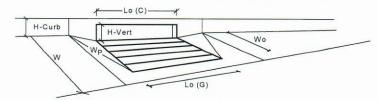


| Design Information (Input) | | MINOR | MAJOR | |
|--|-----------------------------|----------|-----------|-----------------|
| Type of Inlet CDOT Type C Grate | Type = | CDOT Typ | e C Grate | |
| Local Depression (additional to continuous gutter depression 'a' from above) | a _{local} = | 6.00 | 6.00 | inches |
| Number of Unit Inlets (Grate or Curb Opening) | No = | 1 | 1 | |
| Water Depth at Flowline (outside of local depression) | Ponding Depth = | 6.0 | 6.0 | inches |
| Grate Information | | MINOR | MAJOR | Override Depths |
| Length of a Unit Grate | L _o (G) = | 2.92 | 2.92 | feet |
| Width of a Unit Grate | W _o = | 2.92 | 2.92 | feet |
| Area Opening Ratio for a Grate (typical values 0.15-0.90) | A _{ratio} = | 0.70 | 0.70 | |
| Clogging Factor for a Single Grate (typical value 0.50 - 0.70) | C _f (G) = | 0.50 | 0.50 | |
| Grate Weir Coefficient (typical value 2.15 - 3.60) | C _w (G) = | 2.41 | 2.41 | |
| Grate Orifice Coefficient (typical value 0.60 - 0.80) | C _o (G) = | 0.67 | 0.67 | |
| Curb Opening Information | | MINOR | MAJOR | |
| Length of a Unit Curb Opening | L _o (C) = | N/A | N/A | feet |
| Height of Vertical Curb Opening in Inches | H _{vert} = | N/A | N/A | inches |
| Height of Curb Orifice Throat in Inches | H _{throat} = | N/A | N/A | inches |
| Angle of Throat (see USDCM Figure ST-5) | Theta = | N/A | N/A | degrees |
| Side Width for Depression Pan (typically the gutter width of 2 feet) | W _p = | N/A | N/A | feet |
| Clogging Factor for a Single Curb Opening (typical value 0.10) | $C_{f}(C) =$ | N/A | N/A | |
| Curb Opening Weir Coefficient (typical value 2.3-3.7) | C _w (C) = | N/A | N/A | |
| Curb Opening Orifice Coefficient (typical value 0.60 - 0.70) | C _o (C) = | N/A | N/A | |
| Low Head Performance Reduction (Calculated) | | MINOR | MAJOR | |
| Depth for Grate Midwidth | d _{Grate} = | 0.635 | 0.635 | ft |
| Depth for Curb Opening Weir Equation | d _{Curb} = | N/A | N/A | ft |
| Combination Inlet Performance Reduction Factor for Long Inlets | RF _{Combination} = | N/A | N/A | |
| Curb Opening Performance Reduction Factor for Long Inlets | RF _{Curb} = | N/A | N/A | |
| Grated Inlet Performance Reduction Factor for Long Inlets | RF _{Grate} = | 0.95 | 0.95 | |
| and the second s | | MINOR | MAJOR | _ |
| Total Inlet Interception Capacity (assumes clogged condition) | Q _a = | 4.2 | 4.2 | cfs |
| Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK) | Q PEAK REQUIRED = | 1.7 | 3.1 | cfs |

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) ELDORADO SPRINGS DP-11 Project: Inlet ID: STREET Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb 5.0 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) SBACK = 0.020 ft/ft Manning's Roughness Behind Curb (typically between 0.012 and 0.020) 0.020 Height of Curb at Gutter Flow Line 6.00 inches Distance from Curb Face to Street Crown TCROWN 24.0 Gutter Width W= 2.00 Street Transverse Slope Sx = 0.020 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) Sw 0.083 ft/ft Street Longitudinal Slope - Enter 0 for sump condition So 0.000 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) n_{STREET} = 0.012 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm 24.0 24.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm 6.0 6.0 Check boxes are not applicable in SUMP conditions MINOR STORM Allowable Capacity is based on Depth Criterion MAJOR STORM Allowable Capacity is based on Depth Criterion Minor Storm Major Storm

SUMP

SUMP



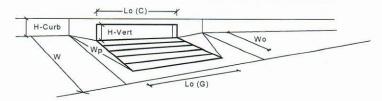
| Design Information (Input) | CDOT Type R Curb Opening ▼ | 95 | MINOR | MAJOR | |
|------------------------------------|--|-----------------------------|-------------|--------------|-----------------|
| Type of Inlet | CDOT Type R Curb Opening | Type = | CDOT Type R | Curb Opening | |
| Local Depression (additional to d | continuous gutter depression 'a' from above) | a _{local} = | 3.00 | 3.00 | inches |
| Number of Unit Inlets (Grate or 0 | Curb Opening) | No = | 1 | 1 | |
| Water Depth at Flowline (outside | of local depression) | Ponding Depth = | 6.0 | 6.0 | inches |
| Grate Information | | _ | MINOR | MAJOR | Override Depths |
| Length of a Unit Grate | | L _o (G) = | N/A | N/A | feet |
| Width of a Unit Grate | | W _o = | N/A | N/A | feet |
| Area Opening Ratio for a Grate (| typical values 0.15-0.90) | A _{ratio} = | N/A | N/A | |
| Clogging Factor for a Single Gra | te (typical value 0.50 - 0.70) | C _f (G) = | N/A | N/A | 1 |
| Grate Weir Coefficient (typical va | alue 2.15 - 3.60) | C _w (G) = | N/A | N/A | 7 |
| Grate Orifice Coefficient (typical | value 0.60 - 0.80) | C _o (G) = | N/A | N/A | 7 |
| Curb Opening Information | | | MINOR | MAJOR | _ |
| Length of a Unit Curb Opening | | L _o (C) = | 5.00 | 5 00 | feet |
| Height of Vertical Curb Opening | in Inches | H _{vert} = | 6.00 | 6.00 | inches |
| Height of Curb Orifice Throat in I | nches | H _{throat} = | 6.00 | 6.00 | inches |
| Angle of Throat (see USDCM Fig | gure ST-5) | Theta = | 63.40 | 63.40 | degrees |
| Side Width for Depression Pan (| typically the gutter width of 2 feet) | W _p = | 2.00 | 2.00 | feet |
| Clogging Factor for a Single Cur | b Opening (typical value 0.10) | $C_{f}(C) =$ | 0.10 | 0.10 | |
| Curb Opening Weir Coefficient (| typical value 2.3-3.7) | C _w (C) = | 3.60 | 3.60 | |
| Curb Opening Orifice Coefficient | (typical value 0.60 - 0.70) | C _o (C) = | 0.67 | 0.67 | |
| Low Head Performance Reduc | tion (Calculated) | | MINOR | MAJOR | |
| Depth for Grate Midwidth | | d _{Grate} = | N/A | N/A | ft |
| Depth for Curb Opening Weir Ed | uation | d _{Curb} = | 0.33 | 0.33 | ft |
| Combination Inlet Performance F | Reduction Factor for Long Inlets | RF _{Combination} = | 0.77 | 0.77 | |
| Curb Opening Performance Red | | RF _{Curb} = | 1.00 | 1.00 | |
| Grated Inlet Performance Reduc | tion Factor for Long Inlets | RF _{Grate} = | N/A | N/A | |
| | | _ | MINOR | MAJOR | |
| Total Inlet Interception C | apacity (assumes clogged condition) | Q _a = | 5.4 | 5.4 | cfs |
| nlet Capacity IS GOOD for Mir | or and Major Storms(>Q PEAK) | Q PEAK REQUIRED = | 1.0 | 3.0 | cfs |

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) ELDORADO SPRINGS Project: Inlet ID: DP-12 STREET Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb 0.0 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) 0.020 ft/ft Manning's Roughness Behind Curb (typically between 0.012 and 0.020) H_{CURB} Height of Curb at Gutter Flow Line 6.00 Distance from Curb Face to Street Crown 24.0 Gutter Width W Street Transverse Slope S_X = 0.020 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) Sw 0.083 ft/ft Street Longitudinal Slope - Enter 0 for sump condition 0.000 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) n_{STREET} = 0.012 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm 24.0 24.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm 6.0 6.0 Check boxes are not applicable in SUMP conditions MINOR STORM Allowable Capacity is based on Depth Criterion Major Storm Minor Storm

SUMP

SUMP

MAJOR STORM Allowable Capacity is based on Depth Criterion



| Design Information (Input) | and the same of th | MINOR | MAJOR | |
|---|--|---------|------------|-----------------|
| ype of Inlet | Type = | CDOT Ty | pe C Grate | |
| ocal Depression (additional to continuous gutter depression 'a' from above) | a _{local} = | 6.00 | 6.00 | inches |
| lumber of Unit Inlets (Grate or Curb Opening) | No = | 1 | 1 | |
| Vater Depth at Flowline (outside of local depression) | Ponding Depth = | 6.0 | 6.0 | inches |
| Grate Information | A 1000 | MINOR | MAJOR | Override Depths |
| ength of a Unit Grate | L ₀ (G) = | 2.92 | 2.92 | feet |
| Vidth of a Unit Grate | W _o = | 2.92 | 2,92 | feet |
| krea Opening Ratio for a Grate (typical values 0.15-0.90) | A _{ratio} = | 0.70 | 0.70 | |
| Clogging Factor for a Single Grate (typical value 0.50 - 0.70) | $C_f(G) =$ | 0.50 | 0.50 | |
| Grate Weir Coefficient (typical value 2.15 - 3.60) | C _w (G) = | 2.41 | 2.41 | |
| Grate Orifice Coefficient (typical value 0.60 - 0.80) | C _o (G) = | 0.67 | 0.67 | |
| Curb Opening Information | | MINOR | MAJOR | |
| ength of a Unit Curb Opening | L _o (C) = | N/A | N/A | feet |
| leight of Vertical Curb Opening in Inches | H _{vert} = | N/A | N/A | inches |
| leight of Curb Orifice Throat in Inches | H _{throat} = | N/A | N/A | inches |
| Angle of Throat (see USDCM Figure ST-5) | Theta = | N/A | N/A | degrees |
| Side Width for Depression Pan (typically the gutter width of 2 feet) | W _p = | N/A | N/A | feet |
| Clogging Factor for a Single Curb Opening (typical value 0.10) | $C_f(C) =$ | N/A | N/A | |
| Curb Opening Weir Coefficient (typical value 2.3-3.7) | C _w (C) = | N/A | N/A | |
| Curb Opening Orifice Coefficient (typical value 0.60 - 0.70) | C _o (C) = | N/A | N/A | |
| ow Head Performance Reduction (Calculated) | | MINOR | MAJOR | |
| Pepth for Grate Midwidth | d _{Grate} = | 0.635 | 0.635 | T ft |
| lepth for Curb Opening Weir Equation | d _{Curb} = | N/A | N/A | ft |
| combination Inlet Performance Reduction Factor for Long Inlets | RF _{Combination} = | N/A | N/A | |
| urb Opening Performance Reduction Factor for Long Inlets | RF _{Curb} = | N/A | N/A | |
| erated inlet Performance Reduction Factor for Long Inlets | RF _{Grate} = | 0.95 | 0.95 | |
| | 19 | MINOR | MAJOR | |
| otal Inlet Interception Capacity (assumes clogged condition) | Q _a = | 4.2 | 4.2 | cfs |
| nlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK) | Q PEAK REQUIRED = | 1.7 | 3.0 | cfs |

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) ELDORADO SPRINGS Project: Inlet ID: DP-13 STREET Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb TBACK 5.0 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) SBACK 0.020 ft/ft Manning's Roughness Behind Curb (typically between 0.012 and 0.020) 0.020 Height of Curb at Gutter Flow Line H_{CURB} : 6.00 inches Distance from Curb Face to Street Crown 24.0 Gutter Width W: 2.00 Street Transverse Slope S_X = 0.020 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) Sw = 0.083 ft/ft Street Longitudinal Slope - Enter 0 for sump condition So= 0.000 Manning's Roughness for Street Section (typically between 0.012 and 0.020) n_{STREET} = 0.012 Major Storm Max. Allowable Spread for Minor & Major Storm 24.0 24.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm 6.0 Check boxes are not applicable in SUMP conditions

Minor Storm

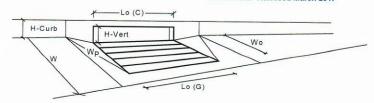
SUMP

Major Storm

SUMP

MINOR STORM Allowable Capacity is based on Depth Criterion

MAJOR STORM Allowable Capacity is based on Depth Criterion

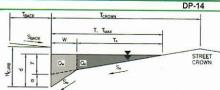


| Design Information (Input) Type of Inlet CDOT Type R Curb Opening | | MINOR | MAJOR | |
|--|-----------------------------|-------------|--------------|-----------------|
| Type of fillet | Type = | CDOT Type R | Curb Opening | |
| Local Depression (additional to continuous gutter depression 'a' from above) | a _{local} = | 3.00 | 3.00 | inches |
| Number of Unit Inlets (Grate or Curb Opening) | No = | 1 | 1 | - Contract |
| Water Depth at Flowline (outside of local depression) | Ponding Depth = | 6.0 | 7.3 | inches |
| Grate Information | _ | MINOR | MAJOR | Override Depths |
| Length of a Unit Grate | L _o (G) = | N/A | N/A | feet |
| Width of a Unit Grate | W _o = | N/A | N/A | feet |
| Area Opening Ratio for a Grate (typical values 0.15-0.90) | A _{ratio} = | N/A | N/A | |
| Clogging Factor for a Single Grate (typical value 0.50 - 0.70) | C _f (G) = | N/A | N/A | 1 |
| Grate Weir Coefficient (typical value 2.15 - 3.60) | C _w (G) = | N/A | N/A | - |
| Grate Orifice Coefficient (typical value 0.60 - 0.80) | C _o (G) = | N/A | N/A | - |
| Curb Opening Information | | MINOR | MAJOR | _ |
| Length of a Unit Curb Opening | L _o (C) = | 20.00 | 20.00 | feet |
| Height of Vertical Curb Opening in Inches | H _{vert} = | 6.00 | 6.00 | inches |
| Height of Curb Orifice Throat in Inches | H _{throat} = | 6.00 | 6.00 | inches |
| Angle of Throat (see USDCM Figure ST-5) | Theta = | 63.40 | 63.40 | degrees |
| Side Width for Depression Pan (typically the gutter width of 2 feet) | W _p = | 2.00 | 2 00 | feet |
| Clogging Factor for a Single Curb Opening (typical value 0.10) | $C_f(C) =$ | 0.10 | 0.10 | - |
| Curb Opening Weir Coefficient (typical value 2.3-3.7) | C _w (C) = | 3.60 | 3,60 | |
| Curb Opening Orifice Coefficient (typical value 0.60 - 0.70) | C _o (C) = | 0.67 | 0.67 | |
| _ow Head Performance Reduction (Calculated) | | MINOR | MAJOR | |
| Depth for Grate Midwidth | d _{Grate} = | N/A | N/A | T ft |
| Depth for Curb Opening Weir Equation | d _{Curb} = | 0.33 | 0.44 | ft |
| Combination Inlet Performance Reduction Factor for Long Inlets | RF _{Combination} = | 0.57 | 0.69 | 1 |
| Curb Opening Performance Reduction Factor for Long Inlets | RF _{Curb} = | 0.79 | 0.86 | |
| Grated Inlet Performance Reduction Factor for Long Inlets | RF _{Grate} = | N/A | N/A |] |
| | _ | MINOR | MAJOR | _ |
| Total Inlet Interception Capacity (assumes clogged condition) | Q _a = | 12.5 | 20.6 | cfs |
| nlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK) | Q PEAK REQUIRED = | 10.0 | 20.0 | cfs |

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) ELDORADO SPRINGS

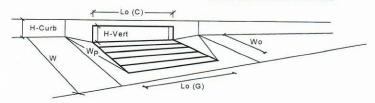
Project: Inlet ID:



Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb TBACK = 0.0 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) SBACK = 0.020 ft/ft Manning's Roughness Behind Curb (typically between 0.012 and 0.020) n_{BACK} : 0.020 Height of Curb at Gutter Flow Line 6.00 Distance from Curb Face to Street Crown 24.0 Gutter Width W= 2.00 Street Transverse Slope S_X = 0.020 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) Sw = 0.083 ft/ft Street Longitudinal Slope - Enter 0 for sump condition So= 0.000 Manning's Roughness for Street Section (typically between 0.012 and 0.020) 0.012 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm 24.0 24.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm 6.0 Check boxes are not applicable in SUMP conditions MINOR STORM Allowable Capacity is based on Depth Criterion

SUMP

SUMP

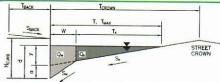


| Design Information (Input) CDOT Type R Curb Opening | | MINOR | MAJOR | |
|---|-----------------------------|-------------|--------------|-----------------|
| ype of inlet | Type = | CDOT Type F | Curb Opening | |
| ocal Depression (additional to continuous gutter depression 'a' from above) | a _{local} = | 3.00 | 3.00 | inches |
| Number of Unit Inlets (Grate or Curb Opening) | No = | 1 | 1 | |
| Water Depth at Flowline (outside of local depression) | Ponding Depth = | 6.0 | 6.0 | inches |
| Grate Information | PARK AND EMPORAL IN | MINOR | MAJOR | Override Depths |
| Length of a Unit Grate | L _o (G) = | N/A | N/A | feet |
| Width of a Unit Grate | W _o = | N/A | N/A | feet |
| Area Opening Ratio for a Grate (typical values 0.15-0.90) | A _{ratio} = | N/A | N/A | |
| Clogging Factor for a Single Grate (typical value 0.50 - 0.70) | $C_f(G) =$ | N/A | N/A | |
| Grate Weir Coefficient (typical value 2.15 - 3.60) | C _w (G) = | N/A | N/A | 7 |
| Grate Orifice Coefficient (typical value 0.60 - 0.80) | C _o (G) = | N/A | N/A | 7 |
| Curb Opening Information | | MINOR | MAJOR | |
| Length of a Unit Curb Opening | L _o (C) = | 5.00 | 5.00 | feet |
| Height of Vertical Curb Opening in Inches | H _{vert} = | 6.00 | 6.00 | inches |
| Height of Curb Orifice Throat in Inches | H _{throat} = | 6.00 | 6.00 | inches |
| Angle of Throat (see USDCM Figure ST-5) | Theta = | 63.40 | 63.40 | degrees |
| Side Width for Depression Pan (typically the gutter width of 2 feet) | W _p = | 2.00 | 2.00 | feet |
| Clogging Factor for a Single Curb Opening (typical value 0.10) | $C_{t}(C) =$ | 0.10 | 0.10 | |
| Curb Opening Weir Coefficient (typical value 2.3-3.7) | C _w (C) = | 3.60 | 3.60 | |
| Curb Opening Orifice Coefficient (typical value 0.60 - 0.70) | C _o (C) = | 0.67 | 0.67 | |
| ow Head Performance Reduction (Calculated) | | MINOR | MAJOR | |
| Depth for Grate Midwidth | d _{Grate} = | N/A | N/A | T ft |
| Depth for Curb Opening Weir Equation | d _{Curb} = | 0.33 | 0.33 | ft |
| Combination Inlet Performance Reduction Factor for Long Inlets | RF _{Combination} = | 0.77 | 0.77 | 1 |
| Curb Opening Performance Reduction Factor for Long Inlets | RF _{Curb} = | 1.00 | 1.00 | |
| Grated Inlet Performance Reduction Factor for Long Inlets | RF _{Grate} = | N/A | N/A | |
| | | MINOR | MAJOR | |
| Total Inlet Interception Capacity (assumes clogged condition) | Q _a = | 5.4 | 5.4 | cfs |
| nlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK) | Q PEAK REQUIRED = | 1.5 | 3.0 | cfs |

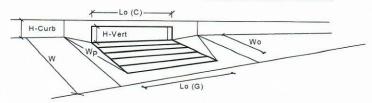
ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)
ELDORADO SPRINGS

Project: Inlet ID:



Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb 0.0 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) 0.020 ft/ft Manning's Roughness Behind Curb (typically between 0.012 and 0.020) n_{BACK} 0.020 Height of Curb at Gutter Flow Line H_{CURB} 6.00 Distance from Curb Face to Street Crown 24.0 Gutter Width W= 3.00 Street Transverse Slope S_X = 0.020 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) Sw = 0.083 ft/ft Street Longitudinal Slope - Enter 0 for sump condition So 0.000 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) n_{STREET} = 0.012 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm 24.0 24.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm 6.0 6.0 Check boxes are not applicable in SUMP conditions MINOR STORM Allowable Capacity is based on Depth Criterion MAJOR STORM Allowable Capacity is based on Depth Criterion Minor Storm Major Storm SUMP



| Design Information (Input) CDOT Type C Grate ▼ | | MINOR | MAJOR | |
|--|-----------------------------|---------|------------|-----------------|
| Type of Inlet | Type = | CDOT Ty | pe C Grate | |
| Local Depression (additional to continuous gutter depression 'a' from above) | a _{local} = | 6.00 | 6.00 | inches |
| Number of Unit Inlets (Grate or Curb Opening) | No = | 1 | 1 | |
| Water Depth at Flowline (outside of local depression) | Ponding Depth = | 6.0 | 6.0 | inches |
| Grate Information | | MINOR | MAJOR | Override Depths |
| Length of a Unit Grate | L _o (G) = | 2.92 | 2,92 | feet |
| Width of a Unit Grate | W _o = | 2.92 | 2.92 | feet |
| Area Opening Ratio for a Grate (typical values 0.15-0.90) | A _{ratio} = | 0.70 | 0.70 | |
| Clogging Factor for a Single Grate (typical value 0.50 - 0.70) | $C_f(G) =$ | 0.50 | 0.50 | |
| Grate Weir Coefficient (typical value 2.15 - 3.60) | C _w (G) = | 2.41 | 2.41 | |
| Grate Orifice Coefficient (typical value 0.60 - 0.80) | C _o (G) = | 0.67 | 0.67 | 7 |
| Curb Opening Information | | MINOR | MAJOR | |
| Length of a Unit Curb Opening | L ₀ (C) = | N/A | N/A | feet |
| Height of Vertical Curb Opening in Inches | H _{vert} = | N/A | N/A | inches |
| Height of Curb Orifice Throat in Inches | H _{throat} = | N/A | N/A | inches |
| Angle of Throat (see USDCM Figure ST-5) | Theta = | N/A | N/A | degrees |
| Side Width for Depression Pan (typically the gutter width of 2 feet) | W _p = | N/A | N/A | feet |
| Clogging Factor for a Single Curb Opening (typical value 0.10) | $C_{f}(C) =$ | N/A | N/A | |
| Curb Opening Weir Coefficient (typical value 2.3-3.7) | C _w (C) = | N/A | N/A | - |
| Curb Opening Orifice Coefficient (typical value 0.60 - 0.70) | C _o (C) = | N/A | N/A | |
| Low Head Performance Reduction (Calculated) | | MINOR | MAJOR | |
| Depth for Grate Midwidth | d _{Grate} = | 0.635 | 0.635 | T ft |
| Depth for Curb Opening Weir Equation | d _{Curb} = | N/A | N/A | ft |
| Combination Inlet Performance Reduction Factor for Long Inlets | RF _{Combination} = | N/A | N/A | |
| Curb Opening Performance Reduction Factor for Long Inlets | RF _{Curb} = | N/A | N/A | 7 |
| Grated Inlet Performance Reduction Factor for Long Inlets | RF _{Grate} = | 0.95 | 0.95 | |
| | | MINOR | MAJOR | |
| Total Inlet Interception Capacity (assumes clogged condition) | Q _a = | 4.2 | 4.2 | cfs |
| nlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK) | Q PEAK REQUIRED = | 1.5 | 4.0 | cfs |

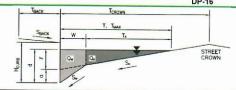
ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

ELDORADO SPRINGS

DP-16

Project: Inlet ID:

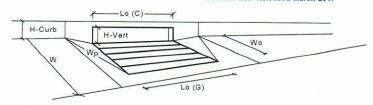


Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb TBACK = 0.0 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) 0.020 ft/ft Manning's Roughness Behind Curb (typically between 0.012 and 0.020) 0.020 Height of Curb at Gutter Flow Line H_{CURB} : 6.00 inches Distance from Curb Face to Street Crown TCROWN 24.0 Gutter Width W= 3.00 Street Transverse Slope Sx = 0.020 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) Sw

| Street Longitudinal Slope - Enter 0 for sump condition Manning's Roughness for Street Section (typically between 0.012 and 0.020) | S _O = | 0.000 | ft/ft |
|--|------------------|-------------|-----------|
| | | Minor Storm | Maior S |
| Max. Allowable Spread for Minor & Major Storm | Tuny = | 24.0 | iviajoi c |

| to bell to | Minor Storm | Major Storm | |
|--------------------|-------------|-------------------------|------------------------------|
| T _{MAX} = | 24.0 | 24.0 | ft |
| d _{MAX} = | 6.0 | 6.0 | inches |
| | F | Г | |
| | | T _{MAX} = 24.0 | T _{MAX} = 24.0 24.0 |

| MINOR STORM Allowable Capacity is based on Depth Criterion | _ | Minor Storm | Major Storm | |
|--|----------------------|-------------|-------------|-----|
| MAJOR STORM Allowable Capacity is based on Depth Criterion | Q _{allow} = | SUMP | SUMP | cfs |



| Design Information (Input) CDOT Type R Curb Opening ▼ | | MINOR | MAJOR | |
|---|-----------------------------|-------------|--------------|-----------------|
| ype of inlet | Type = | CDOT Type R | Curb Opening | |
| ocal Depression (additional to continuous gutter depression 'a' from above) | a _{local} = | 3.00 | 3.00 | inches |
| Number of Unit Inlets (Grate or Curb Opening) | No = | 1 | 1 | |
| Water Depth at Flowline (outside of local depression) | Ponding Depth = | 6.0 | 6.0 | inches |
| Grate Information | | MINOR | MAJOR | Override Depths |
| ength of a Unit Grate | L _o (G) = | N/A | N/A | feet |
| Nidth of a Unit Grate | W _o = | N/A | N/A | feet |
| Area Opening Ratio for a Grate (typical values 0.15-0.90) | A _{ratio} = | N/A | N/A | |
| Clogging Factor for a Single Grate (typical value 0.50 - 0.70) | C _f (G) = | N/A | N/A | 1 |
| Grate Weir Coefficient (typical value 2.15 - 3.60) | C _w (G) = | N/A | N/A | - |
| Grate Orifice Coefficient (typical value 0.60 - 0.80) | C _o (G) = | N/A | N/A | |
| Curb Opening Information | | MINOR | MAJOR | _ |
| ength of a Unit Curb Opening | L _o (C) = | 10.00 | 10.00 | feet |
| Height of Vertical Curb Opening in Inches | H _{vert} = | 6.00 | 6.00 | inches |
| Height of Curb Orifice Throat in Inches | H _{throat} = | 6.00 | 6.00 | inches |
| Angle of Throat (see USDCM Figure ST-5) | Theta = | 63.40 | 63.40 | degrees |
| Side Width for Depression Pan (typically the gutter width of 2 feet) | W _p = | 3.00 | 3.00 | feet |
| Clogging Factor for a Single Curb Opening (typical value 0.10) | $C_f(C) =$ | 0.10 | 0.10 | |
| Curb Opening Weir Coefficient (typical value 2.3-3.7) | C _w (C) = | 3.60 | 3.60 | |
| Curb Opening Orifice Coefficient (typical value 0.60 - 0.70) | C _o (C) = | 0.67 | 0.67 | |
| ow Head Performance Reduction (Calculated) | | MINOR | MAJOR | |
| Depth for Grate Midwidth | d _{Grate} = | N/A | N/A | T ft |
| Pepth for Curb Opening Weir Equation | d _{Curb} = | 0.25 | 0.25 | ft |
| Combination Inlet Performance Reduction Factor for Long Inlets | RF _{Combination} = | 0.57 | 0.57 | 1 |
| Curb Opening Performance Reduction Factor for Long Inlets | RF _{Curb} = | 0.93 | 0.93 | 1 |
| Grated Inlet Performance Reduction Factor for Long Inlets | RF _{Grate} = | N/A | N/A | |
| | | MINOR | MAJOR | |
| otal Inlet Interception Capacity (assumes clogged condition) | Q _a = | 6.1 | 6.1 | cfs |
| VARNING: Inlet Capacity less than Q Peak for Major Storm | Q PEAK REQUIRED = | 5.6 | 11.0 | cfs |

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) ELDORADO SPRINGS Project: Inlet ID: DP-17 STREET Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb TBACK = 5.0 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) SBACK 0.020 ft/ft Manning's Roughness Behind Curb (typically between 0.012 and 0.020) 0.020 Height of Curb at Gutter Flow Line H_{CURB} = 6.00 Distance from Curb Face to Street Crown T_{CROWN} 12.0 Gutter Width W= 2.00 Street Transverse Slope S_X = 0.020 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) S_W = 0.083 ft/ft Street Longitudinal Slope - Enter 0 for sump condition So = 0.040 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) n_{STREET} = 0.012 Major Storm Max. Allowable Spread for Minor & Major Storm 12.0 12.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm Allow Flow Depth at Street Crown (leave blank for no) check = yes MINOR STORM Allowable Capacity is based on Spread Criterion Minor Storn Major Storm

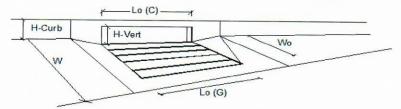
12.6

12.6

MAJOR STORM Allowable Capacity is based on Spread Criterion

Minor storm max, allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management' Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

INLET ON A CONTINUOUS GRADE Version 4.05 Released March 2017



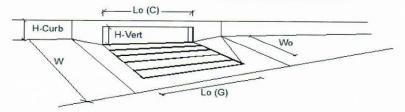
| Design Information (Input) | CDOT Type R Curb Opening | -1 | | MINOR | MAJOR | |
|---|---|----|----------------------|-------------|--------------|--------|
| Type of Inlet | Obot Type it dails opening | | Type = | CDOT Type R | Curb Opening | |
| Local Depression (additional to c | ontinuous gutter depression 'a') | | a _{LOCAL} = | 3.0 | 3.0 | inches |
| Total Number of Units in the Inlet | (Grate or Curb Opening) | | No = | 1 | 1 | |
| Length of a Single Unit Inlet (Gra | te or Curb Opening) | | L _o = | 10.00 | 10.00 | ft |
| Width of a Unit Grate (cannot be | greater than W, Gutter Width) | | W _o = | N/A | N/A | ft |
| Clogging Factor for a Single Uni | Grate (typical min. value = 0.5) | | CrG = | N/A | N/A | |
| Clogging Factor for a Single Unit | Curb Opening (typical min. value = 0.1) | | CrC = | 0.10 | 0.10 | |
| Street Hydraulics: OK - Q < Alle | wable Street Capacity' | | | MINOR | MAJOR | |
| Total Inlet Interception Capacit | y | | Q = | 2.0 | 3.9 | cfs |
| Total Inlet Carry-Over Flow (flo | w bypassing inlet) | | Q _b = | 0.0 | 0.1 | cfs |
| Capture Percentage = Q _a /Q _o = | | | C% = | 100 | 96 | % |

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) Project: **ELDORADO SPRINGS** Inlet ID: DP-18 STREET Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb TBACK = 5.0 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) SBACK = 0.020 ft/ft Manning's Roughness Behind Curb (typically between 0.012 and 0.020) n_{BACK} 0.020 Height of Curb at Gutter Flow Line Distance from Curb Face to Street Crown H_{CURB} = 6.00 inches TCROWN 12.0 Gutter Width W= 2.00 Street Transverse Slope S_X = 0.020 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) S_W = 0.083 ft/ft Street Longitudinal Slope - Enter 0 for sump condition So 0.040 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) 0.012 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm 12.0 12.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm 6.0 6.0 inches Allow Flow Depth at Street Crown (leave blank for no) check = ves MINOR STORM Allowable Capacity is based on Spread Criterion MAJOR STORM Allowable Capacity is based on Spread Criterion Major Storm

Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management' 12.6

12.6

INLET ON A CONTINUOUS GRADE



| Design Information (Input) | CDOT Type R Curb Opening | | | MINOR | MAJOR | |
|--|---|--|-------------------------------------|-------------|--------------|--------|
| Type of Inlet | 1 ODOT Type it Guib Opening | | Type = | CDOT Type R | Curb Opening | |
| Local Depression (additional to co | ontinuous gutter depression 'a') | | a _{LOCAL} = | 3.0 | 3.0 | inches |
| Total Number of Units in the Inlet | (Grate or Curb Opening) | | No = | 1 | 1 | 1 |
| Length of a Single Unit Inlet (Grat | e or Curb Opening) | | L _o = | 5.00 | 5.00 | ft |
| Width of a Unit Grate (cannot be greater than W, Gutter Width) Clogging Factor for a Single Unit Grate (typical min. value = 0.5) | | | W _o = C _C G = | N/A N/A | N/A N/A | ft |
| | | | | | | |
| Clogging Factor for a Single Unit | Curb Opening (typical min. value = 0.1) | | C _C C = | 0.10 | 0.10 | |
| Street Hydraulics: OK - Q < Allo | wable Street Capacity' | | | MINOR | MAJOR | |
| Total Inlet Interception Capacity | / | | Q= | 0.7 | 1.2 | cfs |
| Total Inlet Carry-Over Flow (flo | w bypassing inlet) | | Q _b = | 0.0 | 0.1 | cfs |
| Capture Percentage = Q _a /Q _o = | | | C% = | 100 | 94 | % |

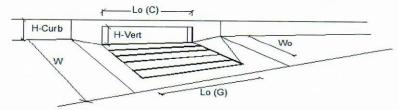
ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) ELDORADO SPRINGS Project: Inlet ID: STREET Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb 10.0 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) 0.020 ft/ft Manning's Roughness Behind Curb (typically between 0.012 and 0.020) 0.020 Height of Curb at Gutter Flow Line H_{CURB} 6.00 Distance from Curb Face to Street Crown 34.0 Gutter Width W= 2.00 Street Transverse Slope S_X = 0.020 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) S_W = 0.083 ft/ft Street Longitudinal Slope - Enter 0 for sump condition So 0.015 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) n_{STREET} = 0.012 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm TMAX 22.0 34.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm 6.0 8.0 inches Allow Flow Depth at Street Crown (leave blank for no) check = yes MINOR STORM Allowable Capacity is based on Depth Criterion Minor Storm Major Storm

22.5

MAJOR STORM Allowable Capacity is based on Depth Criterion

WARNING: MINOR STORM max. allowable capacity is less than the design flow given on sheet 'Inlet Management' Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

INLET ON A CONTINUOUS GRADE Version 4.05 Released March 2017

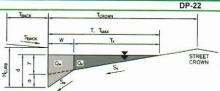


| Design Information (Input) CDOT Type R Curb Opening ▼ | | MINOR | MAJOR | |
|---|----------------------|-------------|--------------|--------|
| Type of Inlet | Type = | CDOT Type R | Curb Opening | |
| Local Depression (additional to continuous gutter depression 'a') | a _{LOCAL} = | 3.0 | 3.0 | inches |
| Total Number of Units in the Inlet (Grate or Curb Opening) | No = | 2 | 2 | |
| Length of a Single Unit Inlet (Grate or Curb Opening) | L _o = | 20.00 | 20 00 | ft |
| Width of a Unit Grate (cannot be greater than W, Gutter Width) | W _o = | N/A | N/A | ft |
| Clogging Factor for a Single Unit Grate (typical min. value = 0.5) | CrG = | N/A | N/A | 1 |
| Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1) | CrC = | 0.10 | 0.10 | |
| Street Hydraulics: WARNING: Q > ALLOWABLE Q FOR MINOR STORM | | MINOR | MAJOR | |
| Total Inlet Interception Capacity | Q = | 28.8 | 46.9 | cfs |
| Total Inlet Carry-Over Flow (flow bypassing inlet) | Q _b = | 0.2 | 12.1 | cfs |
| Capture Percentage = Q _a /Q _o = | C% = | 99 | 79 | % |

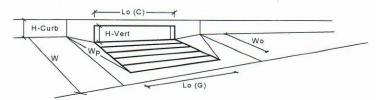
ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) ELDORADO SPRINGS

Project Inlet ID:



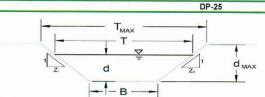
Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb TBACK = 10.0 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) SBACK = 0.020 ft/ft Manning's Roughness Behind Curb (typically between 0.012 and 0.020) n_{BACK} = 0.020 Height of Curb at Gutter Flow Line H_{CURB} = 6.00 inches Distance from Curb Face to Street Crown T_{CROWN} = 34.0 Gutter Width W= 2.00 Street Transverse Slope Sx = 0.020 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) Sw = 0.083 ft/ft Street Longitudinal Slope - Enter 0 for sump condition So: 0.000 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) n_{STREET} = 0.012 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm 22.0 34.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm 8.0 Check boxes are not applicable in SUMP conditions MINOR STORM Allowable Capacity is based on Depth Criterion Major Storm MAJOR STORM Allowable Capacity is based on Depth Criterion SUMP SUMP



| Design Information (Input) CDOT Type R Curb Opening | 7 | MINOR | MAJOR | |
|--|-----------------------------|-------------|--------------|-----------------|
| Type of Inlet | Type = | CDOT Type R | Curb Opening | |
| Local Depression (additional to continuous gutter depression 'a' from above) | a _{local} = | 3.00 | 3.00 | inches |
| Number of Unit Inlets (Grate or Curb Opening) | No = | 1 | 1 | |
| Water Depth at Flowline (outside of local depression) | Ponding Depth = | 6.0 | 8.2 | inches |
| Grate Information | | MINOR | MAJOR | Override Depths |
| Length of a Unit Grate | L _o (G) = | N/A | N/A | feet |
| Width of a Unit Grate | W _o = | N/A | N/A | feet |
| Area Opening Ratio for a Grate (typical values 0.15-0.90) | A _{ratio} = | N/A | N/A | |
| Clogging Factor for a Single Grate (typical value 0.50 - 0.70) | C _f (G) = | N/A | N/A | |
| Grate Weir Coefficient (typical value 2.15 - 3.60) | C _w (G) = | N/A | N/A | 7 |
| Grate Orifice Coefficient (typical value 0.60 - 0.80) | C _o (G) = | N/A | N/A | 7 |
| Curb Opening Information | _ | MINOR | MAJOR | _ |
| Length of a Unit Curb Opening | L ₀ (C) = | 15.00 | 15.00 | feet |
| Height of Vertical Curb Opening in Inches | H _{vert} = | 6.00 | 6.00 | inches |
| Height of Curb Orifice Throat in Inches | H _{throat} = | 6.00 | 6.00 | inches |
| Angle of Throat (see USDCM Figure ST-5) | Theta = | 63.40 | 63.40 | degrees |
| Side Width for Depression Pan (typically the gutter width of 2 feet) | W _p = | 2.00 | 2.00 | feet |
| Clogging Factor for a Single Curb Opening (typical value 0.10) | C _f (C) = | 0.10 | 0.10 | |
| Curb Opening Weir Coefficient (typical value 2.3-3.7) | C _w (C) = | 3.60 | 3,60 | |
| Curb Opening Orifice Coefficient (typical value 0.60 - 0.70) | C _o (C) = | 0.67 | 0.67 | _ |
| Low Head Performance Reduction (Calculated) | | MINOR | MAJOR | |
| Depth for Grate Midwidth | d _{Grate} = | N/A | N/A | ft |
| Depth for Curb Opening Weir Equation | d _{Curb} = | 0.33 | 0.52 | ft |
| Combination Inlet Performance Reduction Factor for Long Inlets | RF _{Combination} = | 0.57 | 0.77 | |
| Curb Opening Performance Reduction Factor for Long Inlets | RF _{Curb} = | 0.79 | 0.90 | |
| Grated Inlet Performance Reduction Factor for Long Inlets | RF _{Grate} = | N/A | N/A | |
| | _ | MINOR | MAJOR | |
| Total Inlet Interception Capacity (assumes clogged condition) | Q _a = | 9.7 | 21.5 | cfs |
| Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK) | Q PEAK REQUIRED = | 1.0 | 14.0 | cfs |

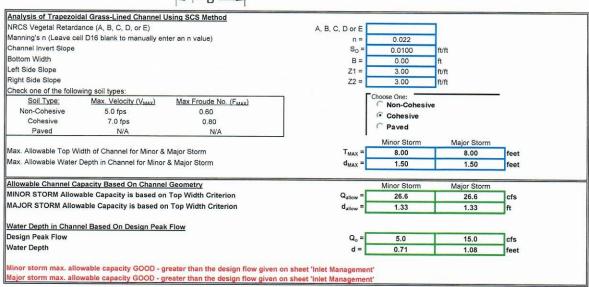
AREA INLET IN A SWALE

ELDORADO SPRINGS



This worksheet uses the NRCS vegetal retardance method to determine Manning's n.

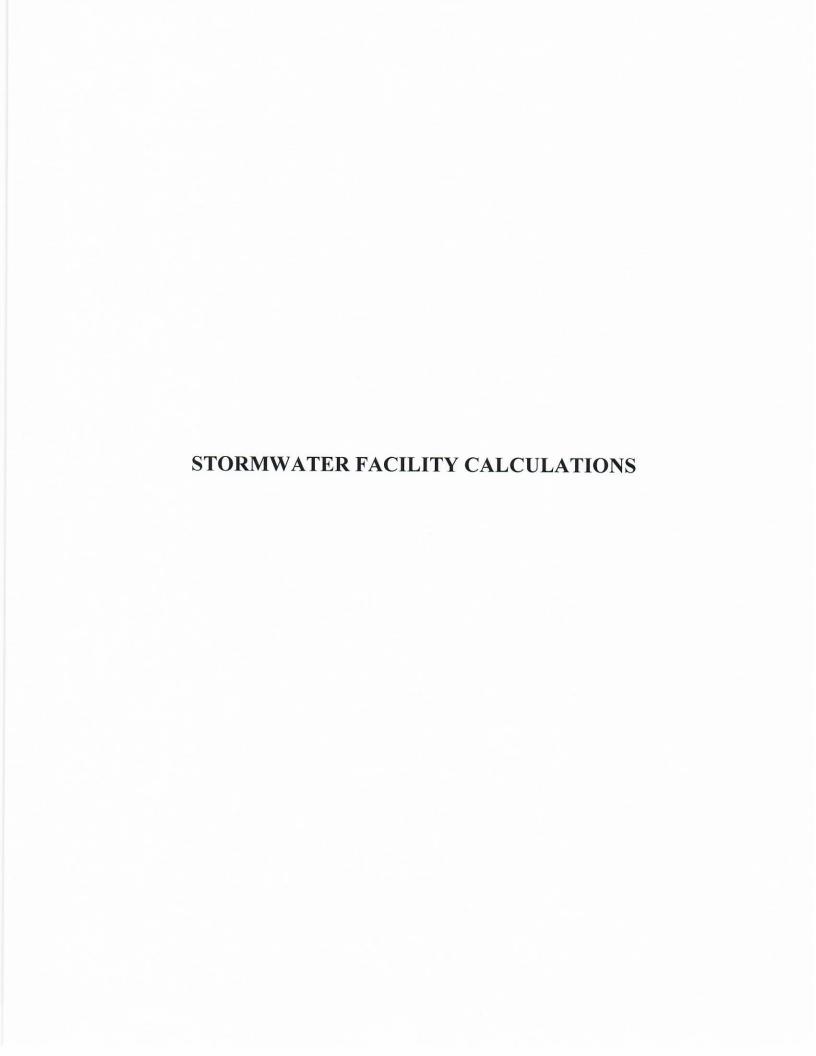
For more information see Section 7.2.3 of the USDCM.



AREA INLET IN A SWALE

ELDORADO SPRINGS DP-25 Inlet Design Information (Input) Type of Inlet CDOT Type C (Depressed) Inlet Type = CDOT Type C (Depressed) -Angle of Inclined Grate (must be <= 30 degrees) θ= 0.00 Width of Grate W= 3.00 Length of Grate L= 3.00 feet Open Area Ratio A_{RATIO} = 0.70 Height of Inclined Grate HB = 0.00 Clogging Factor C, = 0.50 Grate Discharge Coefficient C_d = 0.84 Orifice Coefficient Co: Weir Coefficient 1.81 MINOR Water Depth at Inlet (for depressed inlets, 1 foot is added for depression) 1.71 2.08 Total Inlet Interception Capacity (assumes clogged condition) Q_a = 18.6 20.5 cfs Bypassed Flow, Q_b = 0.0 0.0 cfs Capture Percentage = Q_a/Q_o = C% 100 100 %

Warning 04: Froude No. exceeds USDCM Volume I recommendation.



Site-Level Low Impact Development (LID) Design Effective Impervious Calculator

LID Credit by Impervious Reduction Factor (IRF) Method

UD-BMP (Version 3.06, November 2016)
User Input

inches

inches

 Designer:
 Chad Kuzbek, PE

 Company:
 WestWorks Engineering

 Date:
 November 5, 2019

 Project:
 EL DORADO SPRINGS

 Location:
 POND A

Max Intensity for Optional User Defined Storm 2.51496

| Sub-basin Identifier | A1 | A2 | А3 | A4 | A5 | A6 | A7 | A8 | A9 | OS-13A | OS-13B | | | |
|---|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|------------|------------|------------|
| Receiving Pervious Area Soil Type | Clay Loam | Sandy Loam | Sandy Loam | Sandy Loam |
| Total Area (ac., Sum of DCIA, UIA, RPA, & SPA) | 0.300 | 0.400 | 0.400 | 0.300 | 0.300 | 1.100 | 0.400 | 0.300 | 0.500 | 1.600 | 0.500 | | | |
| Directly Connected Impervious Area (DCIA, acres) | 0.300 | 0.400 | 0.400 | 0.300 | 0.200 | 0.800 | 0.300 | 0.100 | 0.000 | 0.300 | 0.100 | | | |
| Unconnected Impervious Area (UIA, acres) | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | | | |
| Receiving Pervious Area (RPA, acres) | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | | | |
| Separate Pervious Area (SPA, acres) | 0.000 | 0.000 | 0.000 | 0.000 | 0.100 | 0.300 | 0.100 | 0.200 | 0.500 | 1.300 | 0.400 | | | |
| RPA Treatment Type: Conveyance (C), Volume (V), or Permeable Pavement (PP) | V | V | v | V | V | V | v | V | ٧ | V | v | | | |

CALCULATED RESULTS (OUTPUT) Total Calculated Area (ac. check against input) 0.300 0.400 0.400 0.300 0.300 1.100 0.400 Directly Connected Impervious Area (DCIA, %) 100.0% 100.0% 100.0% 100.0% 66.7% 72.7% 75.0% 33.3% 0.0% 18.8% 20.0% Unconnected Impervious Area (UIA, %) 0.0% 0.0% 0.0% 0.0% 0.0% 0.0% 0.0% 0.0% 0.0% 0.0% 0.0% Receiving Pervious Area (RPA, %) 0.0% 0.0% 0.0% 0.0% 0.0% 0.0% 0.0% 0.0% 0.0% 0.0% 0.0% Separate Pervious Area (SPA, %) 0.0% 0.0% 0.0% 0.0% 33.3% 27.3% 25.0% 66.7% 100.0% 81.3% 80.0% A_R (RPA / UIA) 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0,000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 f / I for WQCV Event: 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 f / I for 10-Year Event: 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2 f / I for 100-Year Event: 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1 f / I for Optional User Defined Storm CUHP IRF for WQCV Event: 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 IRF for 10-Year Event: 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 IRF for 100-Year Event: 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 IRF for Optional User Defined Storm CUHP: Total Site Imperviousness: I_{total} 100.0% 100.0% 100.0% 100.0% 66.7% 72.7% 75.0% 33.3% 0.0% 18.8% 20.0% Effective Imperviousness for WQCV Event: 100.0% 100.0% 100.0% 100.0% 66.7% 72.7% 75.0% 33.3% 0.0% 18.8% 20.0% Effective Imperviousness for 10-Year Event: 100.0% 100.0% 100.0% 66.7% 72.7% 75.0% 33.3% 0.0% 18.8% 20.0% Effective Imperviousness for 100-Year Event: 100.0% 100.0% 100.0% 100.0% 66.7% 72.7% 75.0% 33.3% 0.0% 18.8% 20.0%

| LID / EFFECTIVE IMPERVIOUS | NESS CREDITS | |
|----------------------------|--------------------|----------------------|
| | WOCV Event CREDIT: | Reduce Detention By: |

| 10-Year Event CREDIT**: | Reduce Detention By |
|---------------------------|---------------------|
| 100-Year Event CREDIT**: | Reduce Detention By |
| User Defined CUHP CREDIT: | Reduce Detention By |
| | |

Effective Imperviousness for Optional User Defined Storm CUHP:

| N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | | |
|------|------|------|------|------|------|------|------|------|------|------|--|--|
| 0.0% | 0.0% | 0.0% | 0.0% | 0.1% | 0.0% | 0.0% | 0.2% | N/A | 0.1% | 0.2% | | |
| 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.1% | N/A | 0.0% | 0.1% | | |
| 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | | |

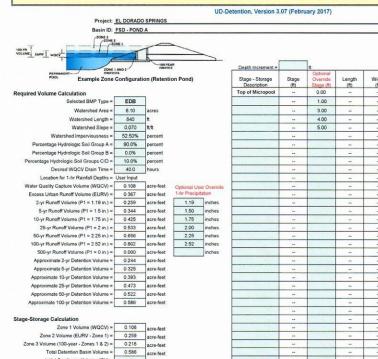
| Total Site Imperviousness: | 52.5% |
|---|-------|
| Total Site Effective Imperviousness for WQCV Event: | 52.5% |
| Total Site Effective Imperviousness for 10-Year Event: | 52.5% |
| Total Site Effective Imperviousness for 100-Year Event: | 52.5% |
| Total Site Effective Imperviousness for Optional User Defined Storm CUHP: | 52.5% |

Notes:

- * Use Green-Ampt average infiltration rate values from Table 3-3.
- Flood control detention volume credits based on empirical equations from Storage Chapter of USDCM.
 *** Method assumes that 1-hour rainfall depth is equivalent to 1-hour intensity for calculation purposed

20.0%

DETENTION BASIN STAGE-STORAGE TABLE BUILDER



| Zone 2 Volume (EURV - Zone 1) = | 0.259 | acre-feet |
|--|---|--|
| Zone 3 Volume (100-year - Zones 1 & 2) = | 0.218 | acre-feet |
| Total Detention Basin Volume = | 0.586 | acre-feet |
| Initial Surcharge Volume (ISV) = | user | ft^3 |
| Initial Surcharge Depth (ISD) = | user | ft |
| Total Available Detention Depth (Htotal) = | user | ft |
| | Zone 3 Volume (100-year - Zones 1 & 2) = Total Detention Basin Volume = Initial Surcharge Volume (ISV) = Initial Surcharge Depth (ISD) = | Zone 3 Volume (100-year - Zones 1 & 2) = |

| ft^3 | user | Initial Surcharge Volume (ISV) = |
|-------|------|---|
| ft | user | Initial Surcharge Depth (ISD) = |
| ft | user | Total Available Detention Depth (H _{total}) = |
| ft | user | Depth of Trickle Channel (H _{TC}) = |
| ft/ft | user | Slope of Trickle Channel (Stc) = |
| H:V | user | Slopes of Main Basin Sides (Smain) = |
| | user | Basin Length-to-Width Ratio (R _{L/W}) = |

| Surcharge Volume Length (L _{15v}) = | user | ft |
|---|------|-----------|
| Surcharge Volume Width (Wigu) = | user | ft |
| Depth of Basin Floor (HFLOOR) = | user | ft |
| Length of Basin Floor (L _{FLOOR}) = | user | ft |
| Width of Basin Floor (W _{FLOOR}) = | user | ft |
| Area of Basin Floor (A _{FLOOR}) = | user | ft^2 |
| Volume of Basin Floor (VFLOOR) = | user | ft^3 |
| Depth of Main Basin (H _{MAIN}) = | user | ft |
| Length of Main Basin (L _{MAIN}) = | user | ft |
| Width of Main Basin (W _{MAIN}) = | user | ft |
| Area of Main Basin (A _{MAIN}) = | user | ft^2 |
| Volume of Main Basin (V _{MAIN}) = | user | ft^3 |
| Calculated Total Basin Volume (Vtotal) = | user | acre-feet |

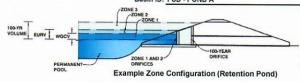
| Top Micropool | Stage - Storage Description | Stage (ft) | Optional Override Stage (ft) | Length (ft) | Width (ft) | Area (ft^2) | Optional Override Area (ft*2) | Area (acre) | Volume (ft^3) | Volume (ac-ft) |
|--|--------------------------------|---------------|------------------------------------|----------------|---------------|----------------|-------------------------------------|----------------|------------------|-------------------|
| - 300 5500 1377 14300 3328 | Top of Micropool | | 10.500 | | | | | | | |
| | | | | | | | | | | |
| | | _ | | | | | | | | |
| | | | | | | | | | | |
| | | | 5.00 | | | | 8,070 | 0.185 | 28,380 | 0.652 |
| | | | | | | | | | | _ |
| | | | | | | | | | | |
| | | | - | | | | | | | |
| | | | - | | | | | - | _ | |
| | | | | | | | | | | |
| | | | | | | | | | | |
| | | | | | | | | | | |
| | | | | | | | | | | |
| | | 20 | | | - | _ | | | | |
| | | ** | | | | | Control of the | | | |
| | | | | | | | | | | |
| | | | | | | | | | | |
| | | ** | | | | - | | | | |
| | | 24 | | | ** | ** | | | | |
| | The second second | | Decree of the second | | | | | | | |
| | | | | | | | | | | |
| | | | | | | | | | | |
| | | | | | | | | | | |
| | | | | | | | | | | |
| | | | | | | | | | | |
| | | | | | | | | | | |
| | | | | | | | | | | |
| | | | | | | | | | | |
| | | | | | | - | | | | |
| | | | | | | | - | | | |
| | | | | | | | | | | |
| | | | | | | | | | | |
| | | | | | | | | | | |
| | | | | | | | | | | |
| | | | | | | | - | | _ | |
| | | | | | | | | | | |
| | | | | | | | | | | |
| | | ** | | - | - | | | | | |
| | | - | | - | - | - | | | | |
| | | | | | ** | - | | | | |
| | | ** | | | ** | | | | | |
| | | | | - | 343 | | | | | |
| | | | | | - | - | | | | |
| | | | | | | | | | | |
| | | | | | | | | | | |
| | | | | | | | | | | |
| | | | | | | | | | | |
| 1 | | | | | | | | | | |
| 1 | | | | | | | | | | |
| 1 | | | | _ | | | | | | |
| 10 | | | | 2.0 | | | | | | |
| 1 | | | | | | | | | | - |
| 1 | | 22 | | | | ** | | | | |
| 1 | | - mar | | - | | | | | | |
| 1 | | | | | | - | | 6 | | |
| 1 | | | | | | | | | | |
| 1 | | | - | | ** | | | | | |
| 1 | | | | | | - | | | | |
| 1 | | ** | | | | | | | | |
| 10 | | | | | | | | | | |
| 1 | | | | | | - | | 2 | | |
| 10 | | | 100 | - | | | | | | |
| 1 | | | | | ** | | | | | |
| 1 | | - | | - :- | | | | | | |
| 10 | | | | | | | | 7 | | 111 |
| 1 | | | | | ** | ** | | | | |
| 10 10 10 10 10 10 10 10 10 10 10 10 10 1 | | | | | | | | | | |
| 10 10 10 10 10 10 10 10 10 10 10 10 10 1 | | - | | | - :- | - | | | | |
| 10 10 10 10 10 10 10 10 10 10 10 10 10 1 | - | | | ** | | - | | | | |
| 10 10 10 10 10 10 10 10 10 10 10 10 10 1 | | - | | | | | | 4 | | |
| 1 | | | | | | | | | | |
| | | | | ** | 44 | | | | | |
| 1 | | | | | | - | | | | |
| | | | | | ** | - | | | | |
| 10 | | | | | | - | | | | |
| | | | | ** | | - | - | | | |
| 10 | | | | - | - | - | | | | |
| 10 10 10 10 10 10 10 10 10 10 10 10 10 1 | | - | | | - | | | | | |
| 10 10 10 10 10 10 10 10 10 10 10 10 10 1 | | | | - | - | - | - | | | |
| 1 | | - " | | ** | | | | | | |
| | | | | - | | | | | | |
| | | | | - | | | | | | |

Detention Basin Outlet Structure Design

UD-Detention, Version 3.07 (February 2017)

Project: EL DORADO SPRINGS

Basin ID: FSD - POND A



| | Stage (ft) | Zone Volume (ac-ft) | Outlet Type |
|-------------------|------------|---------------------|----------------------|
| Zone 1 (WQCV) | 1.19 | 0.108 | Orifice Plate |
| Zone 2 (EURV) | 3.28 | 0.259 | Orifice Plate |
| 'one 3 (100-year) | 4.64 | 0.218 | Weir&Pipe (Restrict) |
| | | 0.586 | Total |

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth = ft (distance below the filtration media surface) N/A Underdrain Orifice Diameter N/A inches

| Calculated P | arameters fo | r Underdra |
|-------------------------------|--------------|-----------------|
| Underdrain Orifice Area = | N/A | ft ² |
| Underdrain Orifice Centroid = | N/A | feet |

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice = ft (relative to basin bottom at Stage = 0 ft) 0.00 Depth at top of Zone using Orifice Plate = 3.28 ft (relative to basin bottom at Stage = 0 ft) Orifice Plate: Orifice Vertical Spacing = 13.10 inches Orifice Plate: Orifice Area per Row = N/A

| Calculate | d Parameter | s for Plate |
|----------------------------|-------------|-----------------|
| WQ Orifice Area per Row = | N/A | ft ² |
| Elliptical Half-Width = | N/A | feet |
| Elliptical Slot Centroid = | N/A | feet |
| Elliptical Slot Area = | N/A | ft ² |

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

| CONTRACTOR | Row 1 (required) | Row 2 (optional) | Row 3 (optional) | Row 4 (optional) | Row 5 (optional) | Row 6 (optional) | Row 7 (optional) | Row 8 (optional) |
|---|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|
| Stage of Orifice Centroid (ft) | 0.00 | 1.09 | 2.19 | | | | | |
| Orifice Area (sq. inches) | 1.45 | 1.45 | 1.45 | | | | | |

| | Row 9 (optional) | Row 10 (optional) | Row 11 (optional) | Row 12 (optional) | Row 13 (optional) | Row 14 (optional) | Row 15 (optional) | Row 16 (optional) |
|--------------------------------|------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| Stage of Orifice Centroid (ft) | | | | | | | | |
| Orifice Area (sq. inches) | | | | | | | | |

User Input: Vertical Orifice (Circular or Rectangular)

| | Not Selected | Not Selected | |
|---|--------------|--------------|---|
| Invert of Vertical Orifice = | N/A | N/A | ft (relative to basin bottom at Stage = 0 ft) |
| Depth at top of Zone using Vertical Orifice = | N/A | N/A | ft (relative to basin bottom at Stage = 0 ft) |
| Vertical Orifice Diameter = | N/A | N/A | inches |

| Calculated F | arameters for Vert | ical Orifice | |
|-----------------------------|--------------------|--------------|-----------------|
| | Not Selected | Not Selected | |
| Vertical Orifice Area = | N/A | N/A | ft ² |
| Vertical Orifice Centroid = | N/A | N/A | feet |

User Input: Overflow Weir (Dropbox) and Grate (Flat or Sloped)

| | Zone 3 Weir | Not Selected | |
|-------------------------------------|-------------|--------------|---|
| Overflow Weir Front Edge Height, Ho | 3.28 | N/A | ft (relative to basin bottom at Stage = 0 ft) |
| Overflow Weir Front Edge Length : | 2.92 | N/A | feet |
| Overflow Weir Slope | 0.00 | N/A | H:V (enter zero for flat grate) |
| Horiz. Length of Weir Sides : | 2.92 | N/A | feet |
| Overflow Grate Open Area % : | 85% | N/A | %, grate open area/total area |
| Debris Clogging % : | 50% | N/A | % |

| Calculated | arameters for Ove | mow weir | 17 |
|--|-------------------|--------------|-----------------|
| | Zone 3 Weir | Not Selected | |
| Height of Grate Upper Edge, H _t = | 3.28 | N/A | feet |
| Over Flow Weir Slope Length = | 2.92 | N/A | feet |
| Grate Open Area / 100-yr Orifice Area = | 28.80 | N/A | should be ≥ 4 |
| Overflow Grate Open Area w/o Debris = | 7.25 | N/A | ft ² |
| Overflow Grate Open Area w/ Debris = | 3.62 | N/A | ft ² |

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

| | Zone 3 Restrictor | Not Selected | | | Zone 3 Restrictor | Not Selected | 7 | |
|---|-------------------|---------------------|--|-----------------------------------|-------------------|--------------|-----------------|--|
| Depth to Invert of Outlet Pipe = | 2.50 | N/A | ft (distance below basin bottom at Stage = 0 ft) | Outlet Orifice Area = | 0.25 | N/A | ft ² | |
| Outlet Pipe Diameter = | 18.00 | N/A | inches | Outlet Orifice Centroid = | 0.18 | N/A | feet | |
| Restrictor Plate Height Above Pipe Invert = | 3.60 | | inches Half-Central Ar | gle of Restrictor Plate on Pipe = | 0.93 | N/A | radians | |

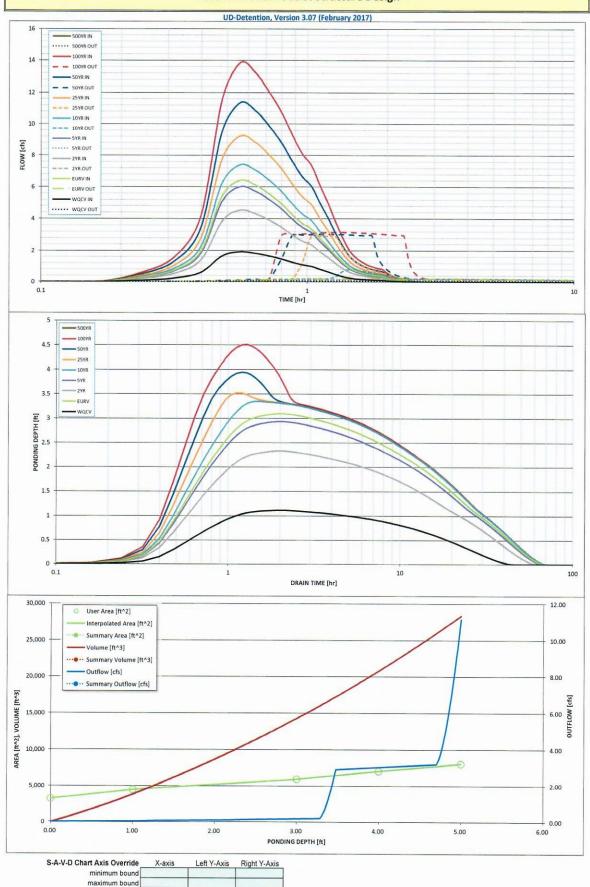
User Input: Emergency Spillway (Rectangular or Trapezoidal)

| | Spillway Invert Stage= | 4.70 | ft (relative to basin bottom at Stage = 0 ft) |
|--------------|-------------------------|-------|---|
| | Spillway Crest Length = | 15.00 | feet |
| | Spillway End Slopes = | 4.00 | H:V |
| Freeboard ab | ove Max Water Surface = | 1.00 | feet |

| Calculated | Parameters : | for Spillwa |
|----------------------------------|--------------|-------------|
| Spillway Design Flow Depth= | 0.43 | feet |
| Stage at Top of Freeboard = | 6.13 | feet |
| Basin Area at Top of Freeboard = | 0.19 | acres |

| Routed Hydrograph Results | | | | | | | | | |
|---|-------|-------|--------|--------|------------------|----------------|----------------|----------------|----------|
| Design Storm Return Period = | WQCV | EURV | 2 Year | 5 Year | 10 Year | 25 Year | 50 Year | 100 Year | 500 Year |
| One-Hour Rainfall Depth (in) = | 0.53 | 1.07 | 1.19 | 1.50 | 1.75 | 2.00 | 2.25 | 2.52 | 0.00 |
| Calculated Runoff Volume (acre-ft) = | 0.108 | 0.367 | 0.259 | 0.344 | 0.425 | 0.533 | 0.656 | 0.802 | 0.000 |
| OPTIONAL Override Runoff Volume (acre-ft) = | | | | | | | | | 0,000 |
| Inflow Hydrograph Volume (acre-ft) = | 0.108 | 0.367 | 0.258 | 0.344 | 0.425 | 0.533 | 0.656 | 0.802 | #N/A |
| Predevelopment Unit Peak Flow, q (cfs/acre) = | 0.00 | 0.00 | 0.00 | 0.02 | 0.05 | 0.11 | 0.29 | 0.58 | 0.00 |
| Predevelopment Peak Q (cfs) = | 0.0 | 0.0 | 0.0 | 0.1 | 0.3 | 0.6 | 1.7 | 3.5 | 0.0 |
| Peak Inflow Q (cfs) = | 1.9 | 6.4 | 4.5 | 6.0 | 7.4 | 9.3 | 11.4 | 13.9 | #N/A |
| Peak Outflow Q (cfs) = | 0.1 | 0.2 | 0.1 | 0.2 | 0.8 | 2.9 | 3.0 | 3.2 | #N/A |
| Ratio Peak Outflow to Predevelopment Q = | N/A | N/A | N/A | 1.8 | 2.8 | 4.6 | 1.7 | 0.9 | #N/A |
| Structure Controlling Flow = | Plate | Plate | Plate | Plate | Overflow Grate 1 | Outlet Plate 1 | Outlet Plate 1 | Outlet Plate 1 | #N/A |
| Max Velocity through Grate 1 (fps) = | N/A | N/A | N/A | N/A | 0.1 | 0.4 | 0.4 | 0.4 | #N/A |
| Max Velocity through Grate 2 (fps) = | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | #N/A |
| Time to Drain 97% of Inflow Volume (hours) = | 39 | 57 | 52 | 56 | 58 | 56 | 54 | 52 | #N/A |
| Time to Drain 99% of Inflow Volume (hours) = | 43 | 63 | 57 | 62 | 64 | 63 | 62 | 61 | #N/A |
| Maximum Ponding Depth (ft) = | 1.12 | 3.10 | 2.33 | 2.94 | 3.35 | 3.52 | 3.95 | 4.52 | #N/A |
| Area at Maximum Ponding Depth (acres) = | 0.10 | 0.14 | 0.13 | 0.14 | 0.15 | 0.15 | 0.16 | 0.17 | #N/A |
| Maximum Volume Stored (acre-ft) = | 0.100 | 0.341 | 0.239 | 0.319 | 0.378 | 0.403 | 0.468 | 0.563 | #N/A |

Detention Basin Outlet Structure Design



Prepared by WestWorks Engineering

Page 1

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Pond POND A:

Inflow Area = 6.100 ac, Inflow Depth = 0.36" for 5-Year event Inflow 0.18 hrs, Volume= 11.97 cfs @ 0.181 af 0.36 hrs, Volume= Outflow 0.11 cfs @ 0.024 af, Atten= 99%, Lag= 11.0 min Primary = 0.11 cfs @ 0.36 hrs, Volume= 0.024 af Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs Peak Elev= 5,860.76' @ 0.36 hrs Surf.Area= 0.116 ac Storage= 0.180 af Plug-Flow detention time= 89.9 min calculated for 0.024 af (13% of inflow) Center-of-Mass det. time= 83.8 min (92.8 - 9.0)

| # | Invert | Avail.Storage | Storage Description |
|---|-----------|---------------|--|
| 1 | 5,859.00' | 0.652 af | Custom Stage Data (Prismatic) Listed below |

| Elevation (feet) | Surf.Area (acres) | Inc.Store (acre-feet) | Cum.Store (acre-feet) |
|---------------------|-------------------|-----------------------|-----------------------|
| 5,859.00 | 0.074 | 0.000 | 0.000 |
| 5,860.00 | 0.103 | 0.089 | 0.089 |
| 5,862.00 | 0.137 | 0.240 | 0.329 |
| 5,863.00 | 0.162 | 0.150 | 0.478 |
| 5,864.00 | 0.185 | 0.173 | 0.652 |

| # | Routing | Invert | Outlet Devices |
|---|----------|-------------|---|
| 1 | Primary | 5,856.50' | 6.8" x 120.0' long OUTLET W/ RESTRICTOR PLATE |
| | | | RCP, square edge headwall, Ke= 0.500 |
| | | | Outlet Invert= 5,854.29' S= 0.0184 '/' n= 0.013 Cc= 0.900 |
| 2 | Device 1 | 5,859.00' | 1.4" Vert. WQ ORIFICE C= 0.600 |
| 3 | Device 1 | 5,860.10' | 1.4" Vert. WQ ORIFICE C= 0.600 |
| 4 | Primary | 5,861.20' | 1.4" Vert. WQ ORIFICE C= 0.600 |
| 5 | Device 1 | 5,862.28' | 2.92' x 2.92' Horiz. CDOT TYPE C INLET W/ MESH GRATE |
| | | | Limited to weir flow C= 0.600 |
| 6 | Secondar | y 5,863.70' | 15.0' long x 10.4' breadth EMERGENCY OVERFLOW |
| | | | Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 |
| | | | Coef. (English) 2.51 2.57 2.70 2.69 2.68 2.69 2.67 2.64 |

Primary OutFlow Max=0.11 cfs @ 0.36 hrs HW=5,860.76' (Free Discharge)

1=OUTLET W/ RESTRICTOR PLATE (Passes 0.11 cfs of 1.59 cfs potential flow)

2=WQ ORIFICE (Orifice Controls 0.07 cfs @ 6.3 fps)

-3=WQ ORIFICE (Orifice Controls 0.04 cfs @ 3.7 fps)

-5=CDOT TYPE C INLET W/ MESH GRATE (Controls 0.00 cfs)

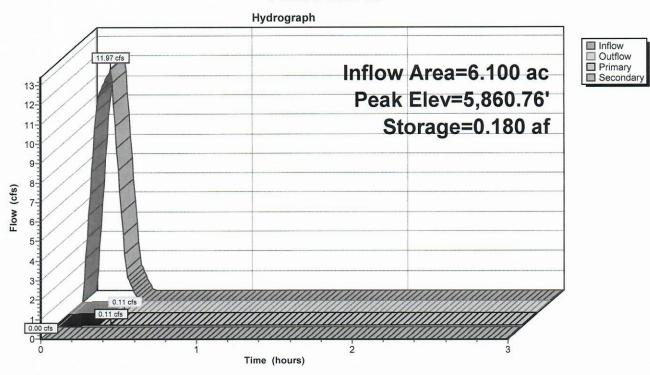
-4=WQ ORIFICE (Controls 0.00 cfs)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=5,859.00' (Free Discharge) 6=EMERGENCY OVERFLOW (Controls 0.00 cfs)

Page 2 11/6/2019

Prepared by WestWorks Engineering
HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

Pond POND A:



Prepared by WestWorks Engineering

Page 1

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Pond POND A:

Inflow Area = 6.100 ac, Inflow Depth = 0.80" for 100-Year event Inflow 25.45 cfs @ 0.15 hrs, Volume= 0.405 af 1.83 cfs @ Outflow = 0.32 hrs, Volume=

0.074 af, Atten= 93%, Lag= 9.9 min

Primary 1.83 cfs @ = 0.32 hrs, Volume= 0.074 af Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs Peak Elev= 5,862.42' @ 0.32 hrs Surf.Area= 0.147 ac Storage= 0.391 af Plug-Flow detention time= 66.8 min calculated for 0.074 af (18% of inflow)

Center-of-Mass det. time= 61.2 min (70.2 - 9.0)

Invert Avail.Storage Storage Description

5,859.00' 0.652 af Custom Stage Data (Prismatic) Listed below

| Elevation (feet) | Surf.Area (acres) | Inc.Store (acre-feet) | Cum.Store (acre-feet) |
|---------------------|-------------------|-----------------------|-----------------------|
| 5,859.00 | 0.074 | 0.000 | 0.000 |
| 5,860.00 | 0.103 | 0.089 | 0.089 |
| 5,862.00 | 0.137 | 0.240 | 0.329 |
| 5,863.00 | 0.162 | 0.150 | 0.478 |
| 5,864.00 | 0.185 | 0.173 | 0.652 |

| # | Routing | Invert | Outlet Devices |
|---|---------|-----------|---|
| 1 | Primary | 5,856.50' | 6.8" x 120.0' long OUTLET W/ RESTRICTOR PLATE |

RCP, square edge headwall, Ke= 0.500 Outlet Invert= 5,854.29' S= 0.0184 '/' n= 0.013 Cc= 0.900

2 Device 1 5,859.00' 1.4" Vert. WQ ORIFICE C= 0.600

3 Device 1 5.860.10' 1.4" Vert. WQ ORIFICE C= 0.600 4 Primary 5,861.20' 1.4" Vert. WQ ORIFICE C= 0.600

5 Device 1 5,862.28' 2.92' x 2.92' Horiz. CDOT TYPE C INLET W/ MESH GRATE

Limited to weir flow C= 0.600

6 Secondary 5,863.70' 15.0' long x 10.4' breadth EMERGENCY OVERFLOW

Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 Coef. (English) 2.51 2.57 2.70 2.69 2.68 2.69 2.67 2.64

Primary OutFlow Max=1.86 cfs @ 0.32 hrs HW=5,862.42' (Free Discharge)

-1=OUTLET W/ RESTRICTOR PLATE (Barrel Controls 1.80 cfs @ 7.1 fps)

-2=WQ ORIFICE (Passes < 0.09 cfs potential flow) -3=WQ ORIFICE (Passes < 0.08 cfs potential flow)

-5=CDOT TYPE C INLET W/ MESH GRATE (Passes < 1.90 cfs potential flow)

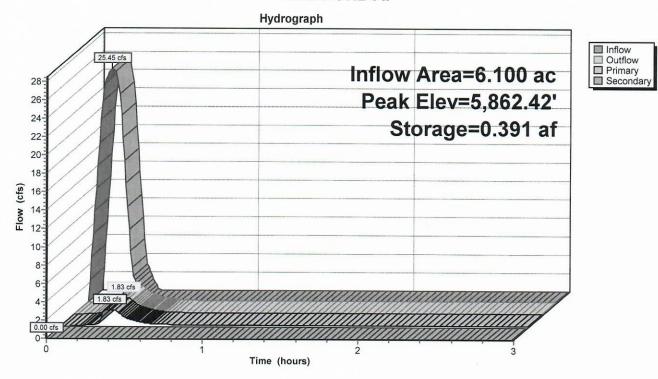
4=WQ ORIFICE (Orifice Controls 0.06 cfs @ 5.2 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=5,859.00' (Free Discharge) 6=EMERGENCY OVERFLOW (Controls 0.00 cfs)

Page 2 11/6/2019

Prepared by WestWorks Engineering
HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

Pond POND A:



Site-Level Low Impact Development (LID) Design Effective Impervious Calculator

LID Credit by Impervious Reduction Factor (IRF) Method UD-BMP (Version 3.06, November 2016)

User Input

inches

inches

Calculated cells

***Design Storm: 1-Hour Rain Depth WQCV Event 0.60 ***Minor Storm: 1-Hour Rain Depth 10-Year Event 1.75 ***Major Storm: 1-Hour Rain Depth 2.52 Optional User Defined Storm CUHP (CUHP) NOAA 1 Hour Rainfall Depth and Frequency for User Defined Storm 2.52 100-Year Event

Designer: Chad Kuzbek, PE WestWorks Engineering Company: Date: November 5, 2019 ELDORADO SPRINGS Project: Location: POND B

Max Intensity for Optional User Defined Storm 2.51496

| ITE | INFORMATION | (USER-INPUT) | |
|-----|-------------|--------------|--|
|-----|-------------|--------------|--|

| Sub-basin Identifier | B1 | B2 | B3 | B4 | B5 | B6 | B7 | B8 | B9 | B10 | OS-11 | OS-12 | B11 | |
|---|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| Receiving Pervious Area Soil Type | Clay Loam |
| Total Area (ac., Sum of DCIA, UIA, RPA, & SPA) | 0.400 | 0.400 | 0.400 | 0.900 | 0.400 | 0.500 | 0.700 | 0.700 | 0.200 | 0.600 | 2.800 | 1.300 | 0.900 | |
| irectly Connected Impervious Area (DCIA, acres) | 0.400 | 0.350 | 0,400 | 0.800 | 0.350 | 0.450 | 0.550 | 0.400 | 0.150 | 0.150 | 0.800 | 0.300 | 0.400 | |
| Unconnected Impervious Area (UIA, acres) | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | |
| Receiving Pervious Area (RPA, acres) | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | |
| Separate Pervious Area (SPA, acres) | 0.000 | 0.050 | 0.000 | 0.100 | 0.050 | 0.050 | 0.150 | 0.300 | 0.050 | 0.450 | 2.000 | 1.000 | 0.500 | |
| RPA Treatment Type: Conveyance (C), Volume (V), or Permeable Pavement (PP) | ٧ | ٧ | V | V | v | v | V | V | V | v | v | V | ٧ | |

CALCUL

| TED RESULTS (OUTPUT) | | | | | | | | | | | | | |
|--|--------|-------|--------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Total Calculated Area (ac, check against input) | 0.400 | 0.400 | 0.400 | 0.900 | 0.400 | 0.500 | 0.700 | 0.700 | 0.200 | 0.600 | 2.800 | 1.300 | 0.900 |
| Directly Connected Impervious Area (DCIA, %) | 100.0% | 87.5% | 100.0% | 88.9% | 87.5% | 90.0% | 78.6% | 57.1% | 75.0% | 25.0% | 28.6% | 23.1% | 44,4% |
| Unconnected Impervious Area (UIA, %) | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% |
| Receiving Pervious Area (RPA, %) | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% |
| Separate Pervious Area (SPA, %) | 0.0% | 12.5% | 0.0% | 11.1% | 12.5% | 10.0% | 21.4% | 42.9% | 25.0% | 75.0% | 71.4% | 76.9% | 55.6% |
| A _R (RPA / UIA) | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| I _a Check | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 |
| f / I for WQCV Event: | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 |
| f / I for 10-Year Event: | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 |
| f / I for 100-Year Event: | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 |
| f / I for Optional User Defined Storm CUHP: | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 |
| IRF for WQCV Event: | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| IRF for 10-Year Event: | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| IRF for 100-Year Event: | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| IRF for Optional User Defined Storm CUHP: | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Total Site Imperviousness: I _{total} | 100.0% | 87.5% | 100.0% | 88.9% | 87.5% | 90.0% | 78.6% | 57.1% | 75.0% | 25.0% | 28.6% | 23.1% | 44.4% |
| Effective Imperviousness for WQCV Event: | 100.0% | 87.5% | 100.0% | 88.9% | 87.5% | 90.0% | 78.6% | 57.1% | 75.0% | 25.0% | 28.6% | 23.1% | 44.4% |
| Effective Imperviousness for 10-Year Event: | 100.0% | 87.5% | 100.0% | 88.9% | 87.5% | 90.0% | 78.6% | 57.1% | 75.0% | 25.0% | 28.6% | 23.1% | 44.4% |
| Effective Imperviousness for 100-Year Event: | 100.0% | 87.5% | 100.0% | 88.9% | 87.5% | 90.0% | 78.6% | 57.1% | 75.0% | 25.0% | 28.6% | 23.1% | 44.4% |
| Effective Imperviousness for Optional User Defined Storm CUHP: | 100.0% | 87.5% | 100.0% | 88.9% | 87.5% | 90.0% | 78.6% | 57.1% | 75.0% | 25.0% | 28.6% | 23.1% | 44.4% |

LID / EFFECTIVE IMPERVIOUSNESS CREDITS

| 10-Year Event CREDIT**: Reduce Detention By: | 0.0% | 0.0% |
|--|------|------|
| 100-Year Event CREDIT**: Reduce Detention By: | 0.0% | 0.0% |
| User Defined CUHP CREDIT: Reduce Detention By: | 0.0% | 0.0% |
| Control of the Contro | | |

| N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | |
|------|------|------|------|------|------|------|------|------|------|------|------|------|--|
| 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.1% | 0.1% | 0.0% | 0.1% | 0.0% | |
| 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.1% | 0.1% | 0.0% | 0.0% | 0.0% | |
| 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | |

| Total Site Imperviousness: | 53.9% |
|---|-------|
| Total Site Effective Imperviousness for WQCV Event: | 53.9% |
| Total Site Effective Imperviousness for 10-Year Event: | 53.9% |
| Total Site Effective Imperviousness for 100-Year Event: | 53.9% |
| Site Effective Imperviousness for Optional User Defined Storm CUHP: | 53.9% |

Notes:

*Use Green-Ampt average infiltration rate values from Table 3-3.

*Flood control detention volume credits based on empirical equations from Storage Chapter of USDCM.

**** Method assumes that 1-hour rainfall depth is equivalent to 1-hour intensity for calculation purposed

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

UD-Detention, Version 3.07 (February 2017)



| Required Volume Calculation | | -23 | | |
|---|------------|-----------|---------------------|--|
| Selected BMP Type = | EDB | | | |
| Watershed Area = | 10.20 | acres | | |
| Watershed Length = | 840 | n | | |
| Watershed Slope = | 0.060 | ft/ft | | |
| Watershed Imperviousness = | 53.90% | percent | | |
| Percentage Hydrologic Soil Group A = | 100.0% | percent | | |
| Percentage Hydrologic Soil Group B = | 0.0% | percent | | |
| Percentage Hydrologic Soil Groups C/D = | 0.0% | percent | | |
| Desired WQCV Drain Time = | 40.0 | hours | | |
| Location for 1-hr Rainfall Depths = | User Input | | | |
| Water Quality Capture Volume (WQCV) = | 0.185 | acre-feet | Optional User Overr | |
| Excess Urban Runoff Volume (EURV) = | 0.647 | acre-feet | 1-hr Precipitation | |
| | | | | |

| Excess Urban Runoff Volume (EURV) = | 0.647 | acre-feet |
|--|-------|-----------|
| 2-yr Runoff Volume (P1 = 1.19 in.) = | 0.443 | acre-feet |
| 5-yr Runoff Volume (P1 = 1.5 in.) = | 0.581 | acre-feet |
| 10-yr Runoff Volume (P1 = 1.75 in.) = | 0.713 | acre-feet |
| 25-yr Runoff Volume (P1 = 2 in.) = | 0.881 | acre-feet |
| 50-yr Runoff Volume (P1 = 2.25 in.) = | 1.085 | acre-feet |
| 100-yr Runoff Volume (P1 = 2.52 in.) = | 1.324 | acre-feet |
| 500-yr Runoff Volume (P1 = 0 in.) = | 0.000 | acre-feet |
| Approximate 2-yr Detention Volume = | 0.418 | acre-feet |
| Approximate 5-yr Detention Volume = | 0.549 | acre-feet |
| Approximate 10-yr Detention Volume = | 0.667 | acre-feet |
| Approximate 25-yr Detention Volume = | 0.813 | acre-feet |
| Approximate 50-yr Detention Volume = | 0.903 | acre-feet |
| Approximate 100-yr Detention Volume = | 1.009 | acre-feet |
| | | |

Stage-Storage Calculation

| Zone 1 Volume (WQCV) = | 0.185 | acre-feet |
|---|-------|-----------|
| Zone 2 Volume (EURV - Zone 1) = | 0.463 | acre-feet |
| Zone 3 Volume (100-year - Zones 1 & 2) = | 0.362 | acre-feet |
| Total Detention Basin Volume = | 1.009 | acre-feet |
| Initial Surcharge Volume (ISV) = | user | ft^3 |
| Initial Surcharge Depth (ISD) = | user | ft |
| Total Available Detention Depth (H _{total}) = | user | ft |
| Depth of Trickle Channel (H _{TC}) = | user | ft |
| Slope of Trickle Channel (S _{TC}) = | user | n/n |
| Slopes of Main Basin Sides (Smain) = | user | H:V |
| Basin Length-to-Width Ratio (R _{UW}) = | user | |

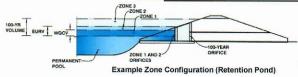
| | 1000 | - |
|---|------|------|
| Initial Surcharge Area (A _{ISV}) = | user | ft^2 |
| Surcharge Volume Length (L _{rpv}) = | user | ft |
| Surcharge Volume Width (W _{rpv}) = | user | ft |
| Depth of Basin Floor (H _{FLOOR}) = | user | ft |
| Length of Basin Floor (L _{FLOOR}) = | user | ft |
| Width of Basin Floor (W _{FLOOR}) = | user | ft |
| Area of Basin Floor (A _{FLOOR}) = | user | ft^2 |
| Volume of Basin Floor (V _{FLOOR}) = | user | ft^3 |
| Depth of Main Basin (H _{MAIN}) = | user | ft |
| Length of Main Basin (L _{MAIN}) = | user | n |
| Width of Main Basin (W _{MAIN}) = | user | ft |
| Area of Main Basin (A _{MAIN}) = | user | ft^2 |
| Volume of Main Basin (V _{MAIN}) = | user | ft^3 |
| Calculated Total Basin Volume (V) = | user | |

| Stage - Storage | Stage | Optional Override | Length | Width | Area | Optional Override | Area | Volume | Volume |
|------------------------------|-------|----------------------|----------|----------|--------|--|-----------------|--------|---------|
| Description Top of Micropool | (ft) | Stage (ft) 0.00 | (ft) | (ft) | (ft^2) | Area (ft^2) 5,400 | (acre) 0.124 | (ft^3) | (ac-ft) |
| | | 1.00 | - | - | - | 6,320 | 0.145 | 5,797 | 0.133 |
| | | 3.00 | | - | - | 8,320 | 0.191 | 20,500 | 0.471 |
| | | 5.00 | | | - | 10,410 | 0.239 | 39,230 | 0.901 |
| | | 6.00 | - | | - | 11,700 | 0.269 | 50,285 | 1.154 |
| | | 7.00 | - | - | | 12,570 | 0.289 | 62,420 | 1.433 |
| | | | | | | | | 02,120 | 1,100 |
| | | | | - | | | | | |
| | | | | - | - | | | | |
| | ** | | - | | | | | | |
| | - | | ** | ** | - | | | | |
| | | | ** | - | | | | | |
| | ** | | - 4 | - | | | | | |
| | | | | - | - | | | | |
| | - | | | | - | | | | |
| | ** | | | - | - | | | | |
| - | | - | | | - | | | | _ |
| | - | | | - | | | | - | |
| | 10.0 | | 2. | - 2 | - | | | | |
| | | | | ** | - | | | | |
| | - | | - | - | - | | | | |
| 2 - 1 - 2 - 2 | - | | - | | ** | | | | |
| | ** | | | - | - | | | | |
| | - | | | | - | | - | | |
| | | | - | - | | | | | |
| | | | - | | - | | | | |
| | | | | | | | | | |
| | - | | ** | ** | - | | | | |
| | (88) | | - 22 | | - | | | | |
| | - | | | 44 | - 2 | | | | |
| | ** | | | | | | | | |
| | | | | ** | - | | | | |
| | ** | | | | - | | | | |
| | - | | - | | - | | | | |
| | ** | | | ** | - | | | | |
| | - | _ | | - | | _ | | | - |
| | | - | | | - | | | | _ |
| | - | | - | - | | | | - | |
| | ** | | | - | - | | | | |
| | ** | To the same | - | ** | - | - | | | |
| | ** | | | | | | | | |
| | | | ** | | - | Control of | | | |
| | | | | - | - | | | | |
| 18 | | | | | | | | | |
| | | | | | | | | | |
| | | | | - | - | | | | |
| | | | | | | | | | |
| | | | | | | | | | |
| | | | | - | | | | | |
| 100 | | | ** | - | | | | | |
| | | | | | | | | | |
| | | | - | | - | | | _ | |
| | = : | | | | ** | | | | |
| | | | | | | | | | |
| | ** | | - | | *** | The same of the sa | | | |
| | | | | | - | | _ | - | |
| | | | | - :- | | | | | |
| | | | | | - | | | | |
| | ** | | ** | ** | | | | | |
| | | | | | - | | | | |
| | - : | | ** | ** | - | | | | |
| | - | | | | | | | | |
| | | | | | | | | | |
| | | | | - | | | | | |
| | | | | | - | | | | |
| | ** | | - | | | | | | |
| | -:- | | | | | | | | |
| | - | | - | - | | | | | |
| | - | | - | -:- | | | | | |
| | ** | | | | | | | | |
| | | | | | | - | | | |
| - | | | - | | - | | | | |
| | - 1 | | - | | ** | | | | |
| | | | | | | | | | |
| | | | | - : | | | | | |
| | | | - | -: | | | | | |
| | | | | - | - | | | | |
| | | | | - | - | | | | |
| | | | - | | - | | | | |
| | | | - | ** | ** | | | | |
| | | | | | | | | | |
| | | | | | - | | | | |

Detention Basin Outlet Structure Design

UD-Detention, Version 3.07 (February 2017)

Project: ELDORADO SPRINGS
Basin ID: FSD - POND B



| | Stage (ft) | Zone Volume (ac-ft) | Outlet Type |
|------------------|------------|---------------------|----------------------|
| Zone 1 (WQCV) | 1.34 | 0.185 | Orifice Plate |
| Zone 2 (EURV) | 3.88 | 0.463 | Orifice Plate |
| one 3 (100-year) | 5.45 | 0.362 | Weir&Pipe (Restrict) |
| | | 1.009 | Total |

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth = N/A ft (distance below the filtration media surface)

Underdrain Orifice Diameter = N/A inches

| Calculated Parameters for Underdra | | | | | | |
|------------------------------------|-----|-----------------|--|--|--|--|
| Underdrain Orifice Area = | N/A | ft ² | | | | |
| Underdrain Orifice Centroid = | N/A | feet | | | | |

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

| | to the transfer of the second |
|-------|---|
| 0.00 | ft (relative to basin bottom at Stage = 0 ft) |
| 3.24 | ft (relative to basin bottom at Stage = 0 ft) |
| 13.00 | inches |
| 2.49 | sq. inches (diameter = 1-3/4 inches) |
| | 0.00 3.24 13.00 |

| Calculated Parameters for | | | | | | |
|----------------------------|-----------|-----------------|--|--|--|--|
| WQ Orifice Area per Row = | 1.729E-02 | ft ² | | | | |
| Elliptical Half-Width = | N/A | feet | | | | |
| Elliptical Slot Centroid = | N/A | feet | | | | |
| Elliptical Slot Area = | N/A | ft ² | | | | |

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

| | Row 1 (required) | Row 2 (optional) | Row 3 (optional) | Row 4 (optional) | Row 5 (optional) | Row 6 (optional) | Row 7 (optional) | Row 8 (optional) |
|--------------------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|
| Stage of Orifice Centroid (ft) | 0.00 | 1.08 | 2.16 | | | | | |
| Orifice Area (sq. inches) | 2.49 | 2.49 | 2.49 | | | | | |

| | Row 9 (optional) | Row 10 (optional) | Row 11 (optional) | Row 12 (optional) | Row 13 (optional) | Row 14 (optional) | Row 15 (optional) | Row 16 (optional) |
|----------------------------|------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| e of Orifice Centroid (ft) | | | | | | | | |
| Orifice Area (sq. inches) | | | | | | | | |

User Input: Vertical Orifice (Circular or Rectangular)

| | Not Selected | Not Selected | | |
|---|--------------|--------------|---|------------|
| Invert of Vertical Orifice = | N/A | N/A | ft (relative to basin bottom at Stage = 0 ft) | Vertic |
| Depth at top of Zone using Vertical Orifice = | N/A | N/A | ft (relative to basin bottom at Stage = 0 ft) | Vertical O |
| Vertical Orifice Diameter = | N/A | N/A | inches | |

| Calculated P | arameters for Vert | ical Orifice | |
|----------------------|--------------------|--------------|-----------------|
| | Not Selected | Not Selected | |
| tical Orifice Area = | N/A | N/A | ft ² |
| Orifice Centroid = | N/A | N/A | feet |

User Input: Overflow Weir (Dropbox) and Grate (Flat or Sloped)

Stage

| | Zone 3 Weir | Not Selected | |
|---------------------------------------|-------------|--------------|---|
| Overflow Weir Front Edge Height, Ho = | 3.90 | N/A | ft (relative to basin bottom at Stage = 0 ft) |
| Overflow Weir Front Edge Length = | 2.92 | N/A | feet |
| Overflow Weir Slope = | 0.00 | N/A | H:V (enter zero for flat grate) |
| Horiz. Length of Weir Sides = | 2.92 | N/A | feet |
| Overflow Grate Open Area % = | 85% | N/A | %, grate open area/total area |
| Debris Clogging % = | 50% | N/A | % |

| Calculated F | Parameters for Ove | rflow Weir | |
|--|--------------------|--------------|-----------------|
| | Zone 3 Weir | Not Selected | |
| Height of Grate Upper Edge, H _t = | 3.90 | N/A | feet |
| Over Flow Weir Slope Length = | 2.92 | N/A | feet |
| Grate Open Area / 100-yr Orifice Area = | 17.13 | N/A | should be ≥ 4 |
| Overflow Grate Open Area w/o Debris = | 7.25 | N/A | ft ² |
| Overflow Grate Open Area w/ Debris = | 3.62 | N/A | ft ² |

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

| | to the control of the state | carculated i di diffeter | IOW RESUICION FIR | ate | | | |
|---|-----------------------------|--------------------------|--|-------------------------------------|-------------------|--------------|-----------------|
| | Zone 3 Restrictor | Not Selected | | | Zone 3 Restrictor | Not Selected | 7 |
| Depth to Invert of Outlet Pipe = | 2.50 | N/A | ft (distance below basin bottom at Stage = 0 ft) | Outlet Orifice Area = | 0.42 | N/A | ft ² |
| Outlet Pipe Diameter = | 18.00 | N/A | inches | Outlet Orifice Centroid = | 0.25 | N/A | feet |
| strictor Plate Height Above Pipe Invert = | 5.20 | | inches Half-Central A | Angle of Restrictor Plate on Pipe = | 1.13 | N/A | radians |

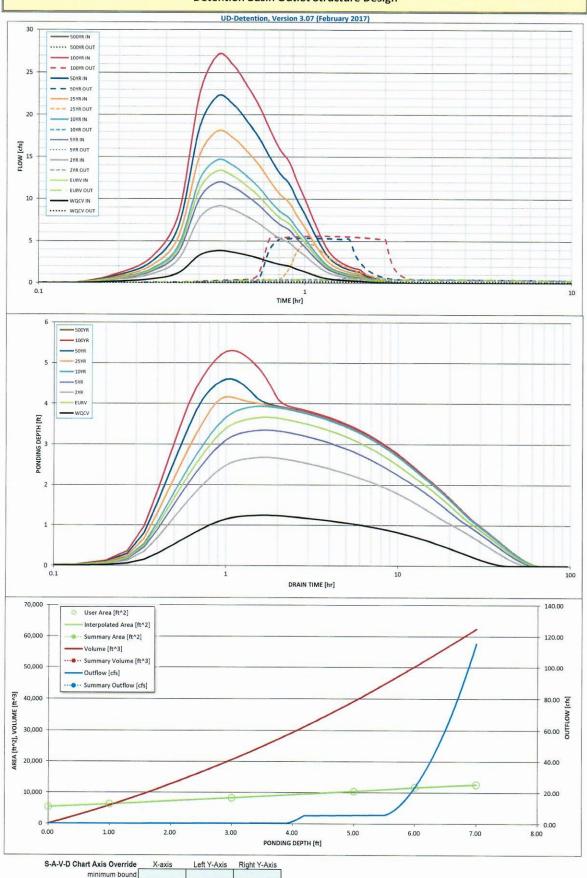
| 5.50 | ft (relative to basin bottom at Stage = 0 ft) |
|-------|---|
| 15.00 | feet |
| 4.00 | H:V |
| 1.00 | feet |
| | 15.00 4.00 |

| Calculated | Parameters 1 | for Spillway |
|--------------------------------|--------------|--------------|
| Spillway Design Flow Depth= | 0.65 | feet |
| Stage at Top of Freeboard = | 7.15 | feet |
| sin Area at Top of Freeboard = | 0.29 | acres |

Basin Area

| Routed Hydrograph Results | | | | | | | | | |
|---|-------|-------|--------|--------|------------------|------------------|----------------|----------------|----------|
| Design Storm Return Period = | WQCV | EURV | 2 Year | 5 Year | 10 Year | 25 Year | 50 Year | 100 Year | 500 Year |
| One-Hour Rainfall Depth (in) = | 0.53 | 1.07 | 1.19 | 1.50 | 1.75 | 2.00 | 2.25 | 2.52 | 0.00 |
| Calculated Runoff Volume (acre-ft) = | 0.185 | 0.647 | 0.443 | 0.581 | 0.713 | 0.881 | 1.085 | 1.324 | 0.000 |
| OPTIONAL Override Runoff Volume (acre-ft) = | | | | | | | | | |
| Inflow Hydrograph Volume (acre-ft) = | 0.184 | 0.647 | 0.441 | 0.580 | 0.712 | 0.880 | 1.083 | 1.322 | #N/A |
| Predevelopment Unit Peak Flow, q (cfs/acre) = | 0.00 | 0.00 | 0.00 | 0.01 | 0.02 | 0.03 | 0.25 | 0.61 | 0.00 |
| Predevelopment Peak Q (cfs) = | 0.0 | 0.0 | 0.0 | 0.1 | 0.2 | 0.4 | 2.6 | 6.2 | 0.0 |
| Peak Inflow Q (cfs) = | 3.9 | 13.4 | 9.2 | 12.0 | 14.7 | 18.1 | 22.2 | 27.1 | #N/A |
| Peak Outflow Q (cfs) = | 0.1 | 0.4 | 0.3 | 0.4 | 0.7 | 4.7 | 5.3 | 5.6 | #N/A |
| Ratio Peak Outflow to Predevelopment Q = | N/A | N/A | N/A | 5.5 | 4.4 | 13.2 | 2.1 | 0.9 | #N/A |
| Structure Controlling Flow = | Plate | Plate | Plate | Plate | Overflow Grate 1 | Overflow Grate 1 | Outlet Plate 1 | Outlet Plate 1 | #N/A |
| Max Velocity through Grate 1 (fps) = | N/A | N/A | N/A | N/A | 0.0 | 0.6 | 0.7 | 0.7 | #N/A |
| Max Velocity through Grate 2 (fps) = | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | #N/A |
| Time to Drain 97% of Inflow Volume (hours) = | 37 | 52 | 47 | 50 | 52 | 51 | 49 | 47 | #N/A |
| Time to Drain 99% of Inflow Volume (hours) = | 40 | 58 | 52 | 56 | 59 | 58 | 57 | 56 | #N/A |
| Maximum Ponding Depth (ft) = | 1.25 | 3.67 | 2.68 | 3.36 | 3.94 | 4.17 | 4.61 | 5.31 | #N/A |
| Area at Maximum Ponding Depth (acres) = | 0.15 | 0.21 | 0.18 | 0.20 | 0.21 | 0.22 | 0.23 | 0.25 | #N/A |
| Maximum Volume Stored (acre-ft) = | 0.170 | 0.602 | 0.409 | 0.539 | 0.661 | 0.708 | 0.807 | 0.976 | #N/A |

Detention Basin Outlet Structure Design



maximum bound

Prepared by WestWorks Engineering

Page 1

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Pond POND B:

Inflow Area = 10.200 ac, Inflow Depth = 0.32" for 5-Year event Inflow 27.63 cfs @ 0.11 hrs, Volume= 0.271 af Outflow 0.23 hrs, Volume= = 0.16 cfs @ 0.037 af, Atten= 99%, Lag= 7.4 min Primary 0.16 cfs @ 0.23 hrs, Volume= 0.037 af Secondary = 0.00 cfs @ 0.00 hrs. Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs Peak Elev= 5,856.80' @ 0.23 hrs Surf.Area= 0.163 ac Storage= 0.270 af Plug-Flow detention time= 89.0 min calculated for 0.036 af (13% of inflow) Center-of-Mass det. time= 85.1 min (91.5 - 6.4)

Invert Avail.Storage Storage Description

1 5,855.00' 1.164 af Custom Stage Data (Prismatic) Listed below

| Elevation (feet) | Surf.Area (acres) | Inc.Store (acre-feet) | Cum.Store (acre-feet) |
|---------------------|-------------------|-----------------------|-----------------------|
| 5,855.00 | 0.124 | 0.000 | 0.000 |
| 5,856.00 | 0.145 | 0.134 | 0.134 |
| 5,858.00 | 0.191 | 0.336 | 0.470 |
| 5,860.00 | 0.239 | 0.430 | 0.900 |
| 5,861.00 | 0.289 | 0.264 | 1 164 |

| # | Routing | Invert | Outlet Devices |
|---|----------|-------------|--|
| 1 | Primary | 5,852.50' | 8.8" x 38.0' long OUTLET W/ RESTRICTOR PLATE |
| | | | RCP, square edge headwall, Ke= 0.500 |
| | | | Outlet Invert= 5,851.67' S= 0.0218 '/' n= 0.013 Cc= 0.900 |
| 2 | Device 1 | 5,855.00' | 1.7" Vert. WQ ORIFICE C= 0.600 |
| 3 | Device 1 | 5,856.10 | 1.7" Vert. WQ ORIFICE C= 0.600 |
| 4 | Device 1 | 5,857.16' | 1.7" Vert. WQ ORIFICE C= 0.600 |
| 5 | Device 1 | | 2.92' x 2.92' Horiz. CDOT TYPE C INLET W/ MESH GRATE |
| | | | Limited to weir flow C= 0.600 |
| 6 | Secondar | y 5,860.50' | 12.0' long x 6.0' breadth EMERGENCY OVERFLOW |
| | | | Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 |
| | | | 3.00 3.50 4.00 4.50 5.00 5.50 |
| | | | Coef. (English) 2.37 2.51 2.70 2.68 2.68 2.67 2.65 2.65 2.65 2.65 2.66 |
| | | | 2.66 2.67 2.69 2.72 2.76 2.83 |

Primary OutFlow Max=0.16 cfs @ 0.23 hrs HW=5,856.80' (Free Discharge)
1=OUTLET W/ RESTRICTOR PLATE (Passes 0.16 cfs of 3.91 cfs potential flow)

2=WQ ORIFICE (Orifice Controls 0.10 cfs @ 6.3 fps)

3=WQ ORIFICE (Orifice Controls 0.06 cfs @ 3.8 fps)

-4=WQ ORIFICE (Controls 0.00 cfs)

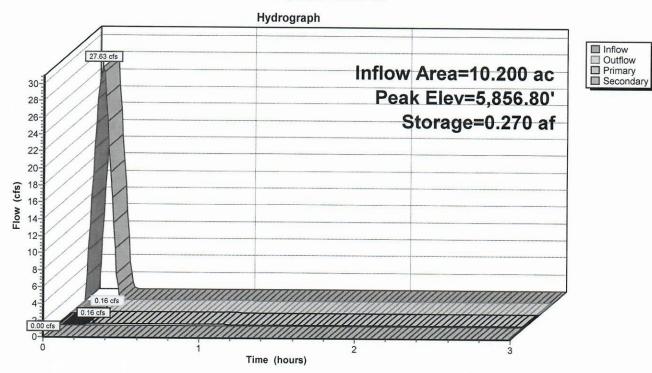
-5=CDOT TYPE C INLET W/ MESH GRATE (Controls 0.00 cfs)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=5,855.00' (Free Discharge) 6=EMERGENCY OVERFLOW (Controls 0.00 cfs)

Page 2 11/6/2019

Prepared by WestWorks Engineering
HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

Pond POND B:



Prepared by WestWorks Engineering

Page 1

HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

11/6/2019

Pond POND B:

Inflow Area = 10.200 ac, Inflow Depth = 0.63" for 100-Year event Inflow 54.15 cfs @ 0.11 hrs, Volume= 0.536 af Outflow = 0.32 cfs @ 0.23 hrs, Volume= 0.074 af, Atten= 99%, Lag= 7.4 min Primary = 0.32 cfs @ 0.23 hrs, Volume= 0.074 af Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs
Peak Elev= 5,858.29' @ 0.23 hrs Surf.Area= 0.198 ac Storage= 0.532 af
Plug-Flow detention time= 89.6 min calculated for 0.074 af (14% of inflow)
Center-of-Mass det. time= 85.4 min (91.8 - 6.4)

| #_ | Invert | Avail.Storage | Storage Description |
|----|-----------|---------------|--|
| 1 | 5,855.00' | 1.164 af | Custom Stage Data (Prismatic) Listed below |

| Elevation (feet) | Surf.Area (acres) | Inc.Store (acre-feet) | Cum.Store (acre-feet) |
|---------------------|-------------------|-----------------------|-----------------------|
| 5,855.00 | 0.124 | 0.000 | 0.000 |
| 5,856.00 | 0.145 | 0.134 | 0.134 |
| 5,858.00 | 0.191 | 0.336 | 0.470 |
| 5,860.00 | 0.239 | 0.430 | 0.900 |
| 5,861.00 | 0.289 | 0.264 | 1.164 |

| # | Routing | Invert | Outlet Devices |
|---|----------|-------------|--|
| 1 | Primary | 5,852.50' | 8.8" x 38.0' long OUTLET W/ RESTRICTOR PLATE |
| | | | RCP, square edge headwall, Ke= 0.500 |
| | | | Outlet Invert= 5,851.67' S= 0.0218 '/' n= 0.013 Cc= 0.900 |
| 2 | Device 1 | 5,855.00' | 1.7" Vert. WQ ORIFICE C= 0.600 |
| 3 | Device 1 | 5,856.10' | 1.7" Vert. WQ ORIFICE C= 0.600 |
| 4 | Device 1 | 5,857.16' | 1.7" Vert. WQ ORIFICE C= 0.600 |
| 5 | Device 1 | 5,858.90' | 2.92' x 2.92' Horiz. CDOT TYPE C INLET W/ MESH GRATE |
| | | | Limited to weir flow C= 0.600 |
| 6 | Secondar | y 5,860.50' | 12.0' long x 6.0' breadth EMERGENCY OVERFLOW |
| | | | Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 |
| | | | 3.00 3.50 4.00 4.50 5.00 5.50 |
| | | | Coef. (English) 2.37 2.51 2.70 2.68 2.68 2.67 2.65 2.65 2.65 2.65 2.66 |
| | | | 2.66 2.67 2.69 2.72 2.76 2.83 |

Primary OutFlow Max=0.32 cfs @ 0.23 hrs HW=5,858.29' (Free Discharge)
1=OUTLET W/ RESTRICTOR PLATE (Passes 0.32 cfs of 4.52 cfs potential flow)

—2=WQ ORIFICE (Orifice Controls 0.14 cfs @ 8.6 fps) —3=WQ ORIFICE (Orifice Controls 0.11 cfs @ 7.0 fps)

-4=WQ ORIFICE (Orifice Controls 0.08 cfs @ 4.9 fps)

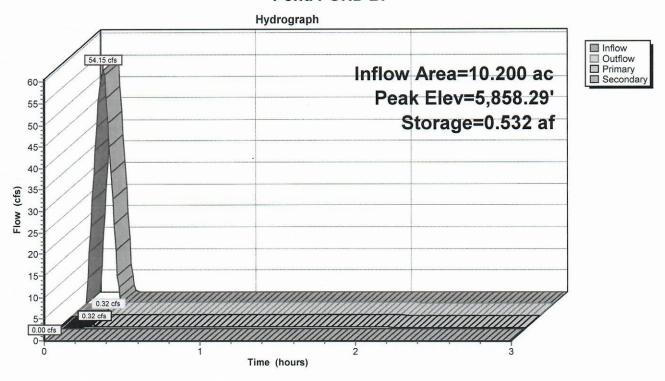
-5=CDOT TYPE C INLET W/ MESH GRATE (Controls 0.00 cfs)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=5,855.00' (Free Discharge) 6=EMERGENCY OVERFLOW (Controls 0.00 cfs)

Page 2 11/6/2019

Prepared by WestWorks Engineering
HydroCAD® 7.00 s/n 002053 © 1986-2003 Applied Microcomputer Systems

Pond POND B:



User Defined

User Defined

User Defined

User Defined

Stormwater Facility Name: ELDORADO SPRINGS - POND A

Facility Location & Jurisdiction: EL PASO COUNTY

User Input: Watershed Characteristics

| Watershed Slope = | 0.070 | ft/ft |
|---|------------|---------|
| Watershed Length = | 840 | ft |
| Watershed Area = | 6.10 | acres |
| Watershed Imperviousness = | 52.5% | percent |
| Percentage Hydrologic Soil Group A = | 90.0% | percent |
| Percentage Hydrologic Soil Group B = | 0.0% | percent |
| Percentage Hydrologic Soil Groups C/D = | 10.0% | percent |
| Location for 1-hr Rainfall Depths (us | e dropdowr | 1): |

Location for 1-hr Rainfall Depths (use dropdown):

User Input

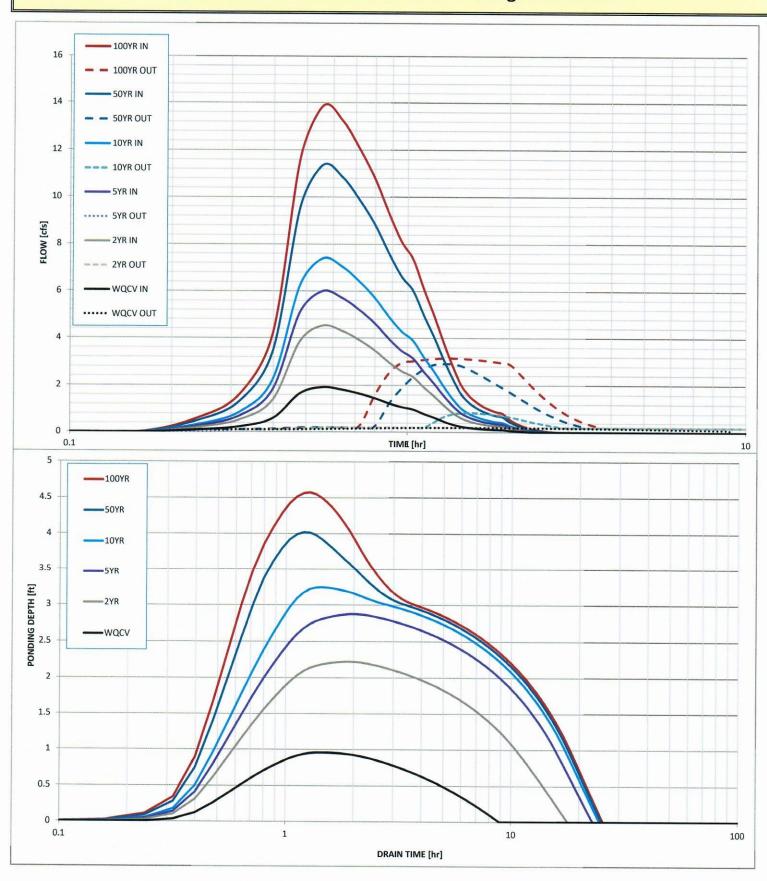
WQCV Treatment Method = Extended Detention

Stage [ft] Area [ft^2] Stage [ft] Discharge [cfs] 0.00 3,230 0.00 0.10 0.20 1.00 4,490 1.00 3.00 0.20 3.00 5,950 4.00 7,070 4.00 2.90 4.70 7,800 4.70 3.20

After completing and printing this worksheet to a pdf, go to: https://maperture.digitaldataservices.com/gvh/?viewer=cswdif create a new stormwater facility, and attach the pdf of this worksheet to that record.

Routed Hydrograph Results

| _ <u>_</u> | outeu nyuro | graph results | | | | | |
|--------------------------------------|-------------|---------------|--------|---------|---------|----------|---------|
| Design Storm Return Period = | WQCV | 2 Year | 5 Year | 10 Year | 50 Year | 100 Year | |
| One-Hour Rainfall Depth = | 0.53 | 1.19 | 1.50 | 1.75 | 2.25 | 2.52 | in |
| Calculated Runoff Volume = | 0.108 | 0.259 | 0.344 | 0.425 | 0.656 | 0.802 | acre-ft |
| OPTIONAL Override Runoff Volume = | | | | | | | acre-ft |
| Inflow Hydrograph Volume = | 0.108 | 0.258 | 0.344 | 0.424 | 0.656 | 0.802 | acre-ft |
| Time to Drain 97% of Inflow Volume = | 8.5 | 17.0 | 21.9 | 23.2 | 23.1 | 23.1 | hours |
| Time to Drain 99% of Inflow Volume = | 8.8 | 17.6 | 22.6 | 24.2 | 24.5 | 24.7 | hours |
| Maximum Ponding Depth = | 0.96 | 2.22 | 2.88 | 3.25 | 4.02 | 4.57 | ft |
| Maximum Ponded Area = | 0.10 | 0.12 | 0.13 | 0.14 | 0.16 | 0.18 | acres |
| Maximum Volume Stored = | 0.084 | 0.227 | 0.311 | 0.362 | 0.481 | 0.574 | acre-ft |
| | | | | | | | |



Stormwater Facility Name: ELDORADO SPRINGS - POND B

Facility Location & Jurisdiction: EL PASO COUNTY

User Input: Watershed Characteristics

| Watershed Slope = | 0.060 | ft/ft |
|---|------------|-----------|
| Watershed Length = | 840 | ft |
| Watershed Area = | 10.20 | acres |
| Watershed Imperviousness = | 53.9% | percent |
| Percentage Hydrologic Soil Group A = | 100.0% | percent |
| Percentage Hydrologic Soil Group B = | 0.0% | percent |
| Percentage Hydrologic Soil Groups C/D = | 0.0% | percent |
| Location for 1-hr Rainfall Depths (us | e dropdown | <u>):</u> |

User Input

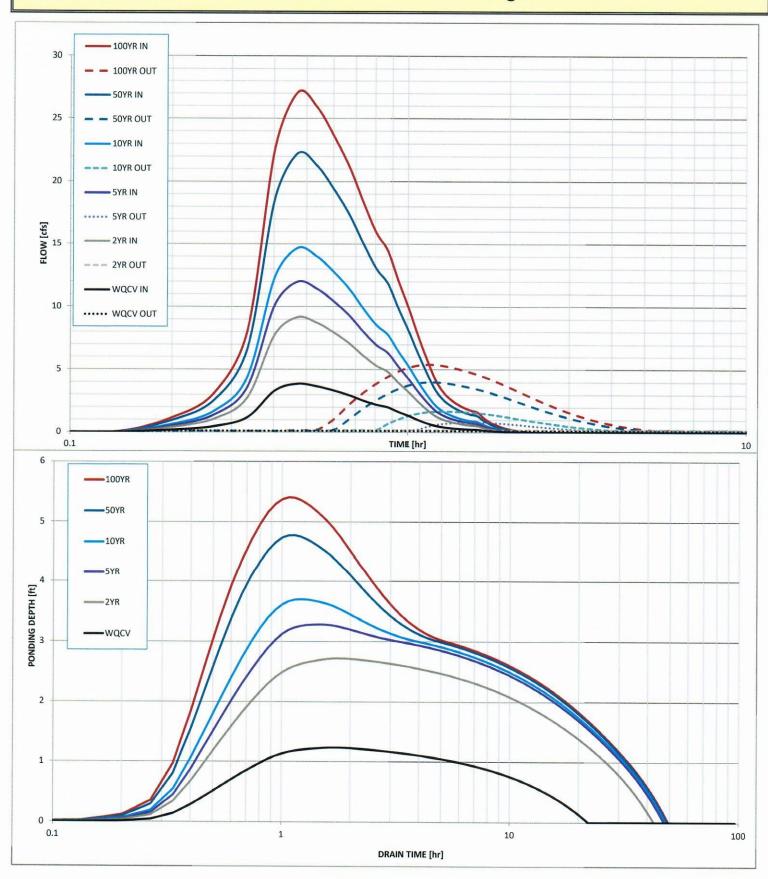
WQCV Treatment Method = Extended Detention

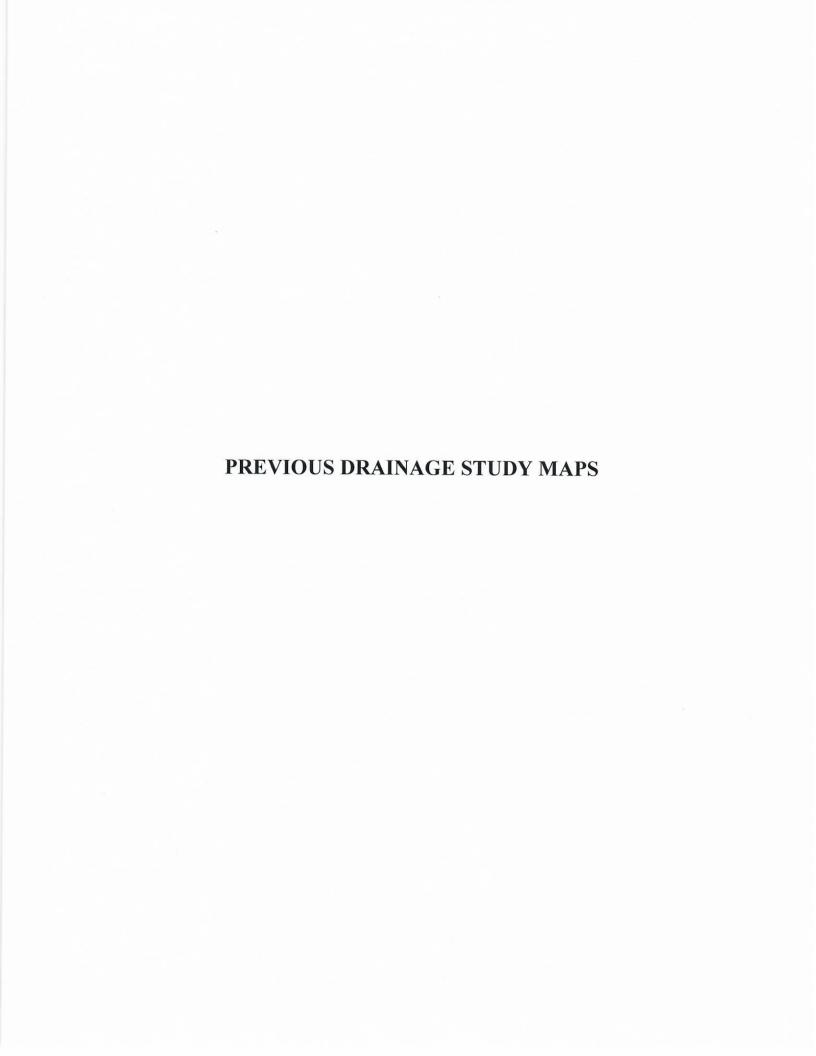
User Defined User Defined User Defined User Defined Stage [ft] Area [ft^2] Stage [ft] Discharge [cfs] 0.00 5,400 0.00 0.10 1.00 6,320 1.00 0.10 3.00 8,320 3.00 0.20 5.00 10,410 5.00 4.50 5.50 11,100 5.50 5.60 7.00 12,570 7.00 10.00

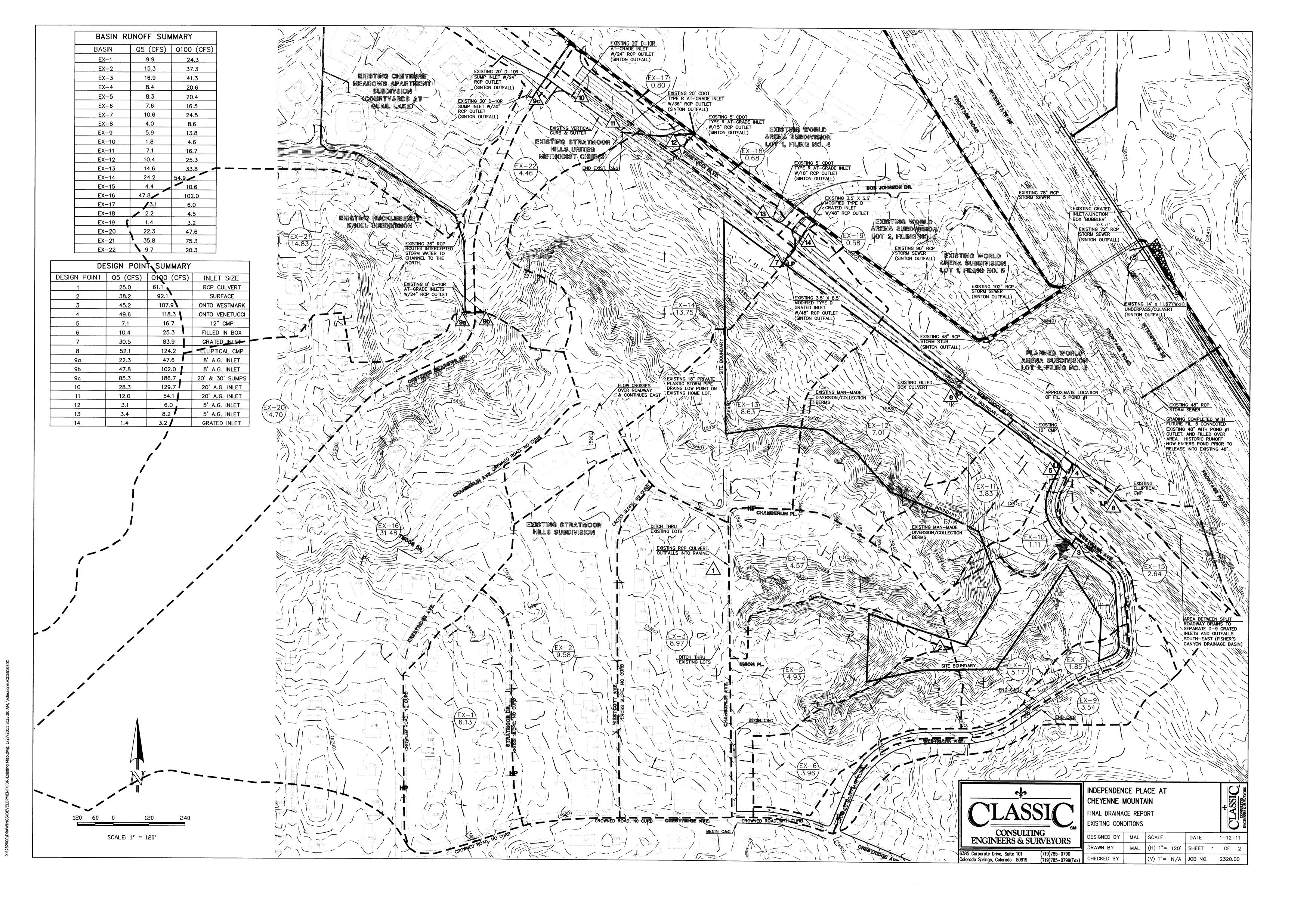
After completing and printing this worksheet to a pdf, go to: https://maperture.digitaldataservices.com/gvh/?viewer=cswdif create a new stormwater facility, and attach the pdf of this worksheet to that record.

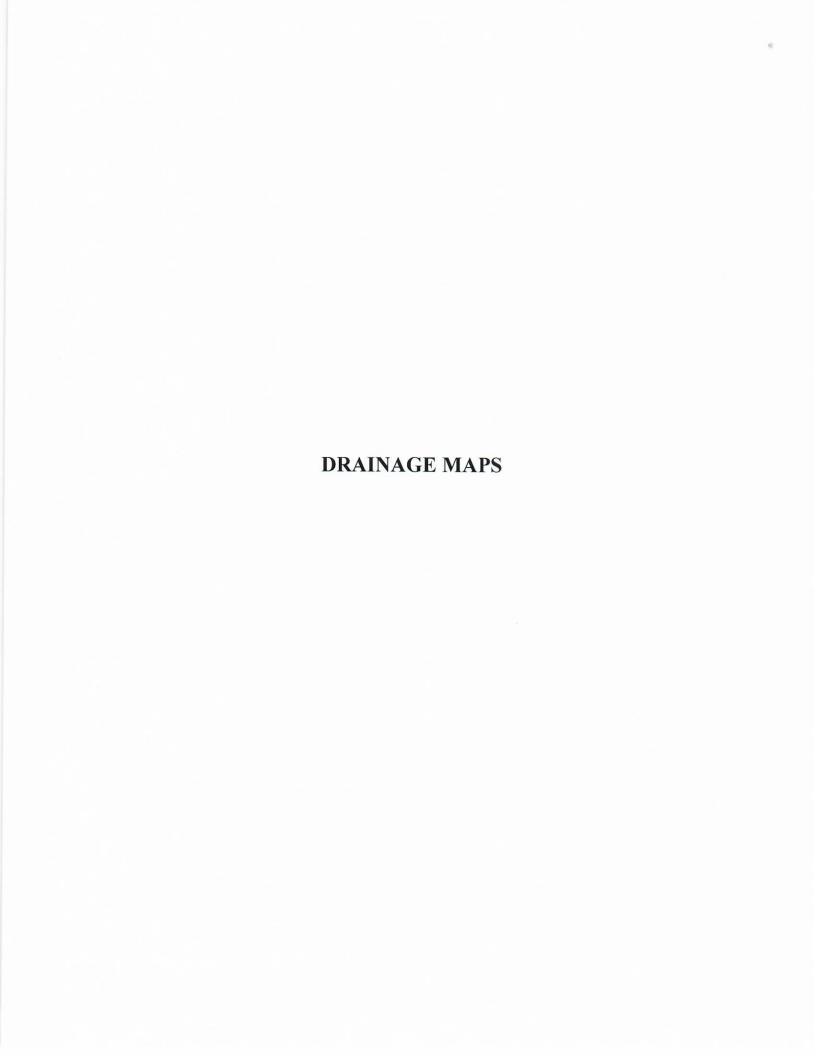
Routed Hydrograph Results

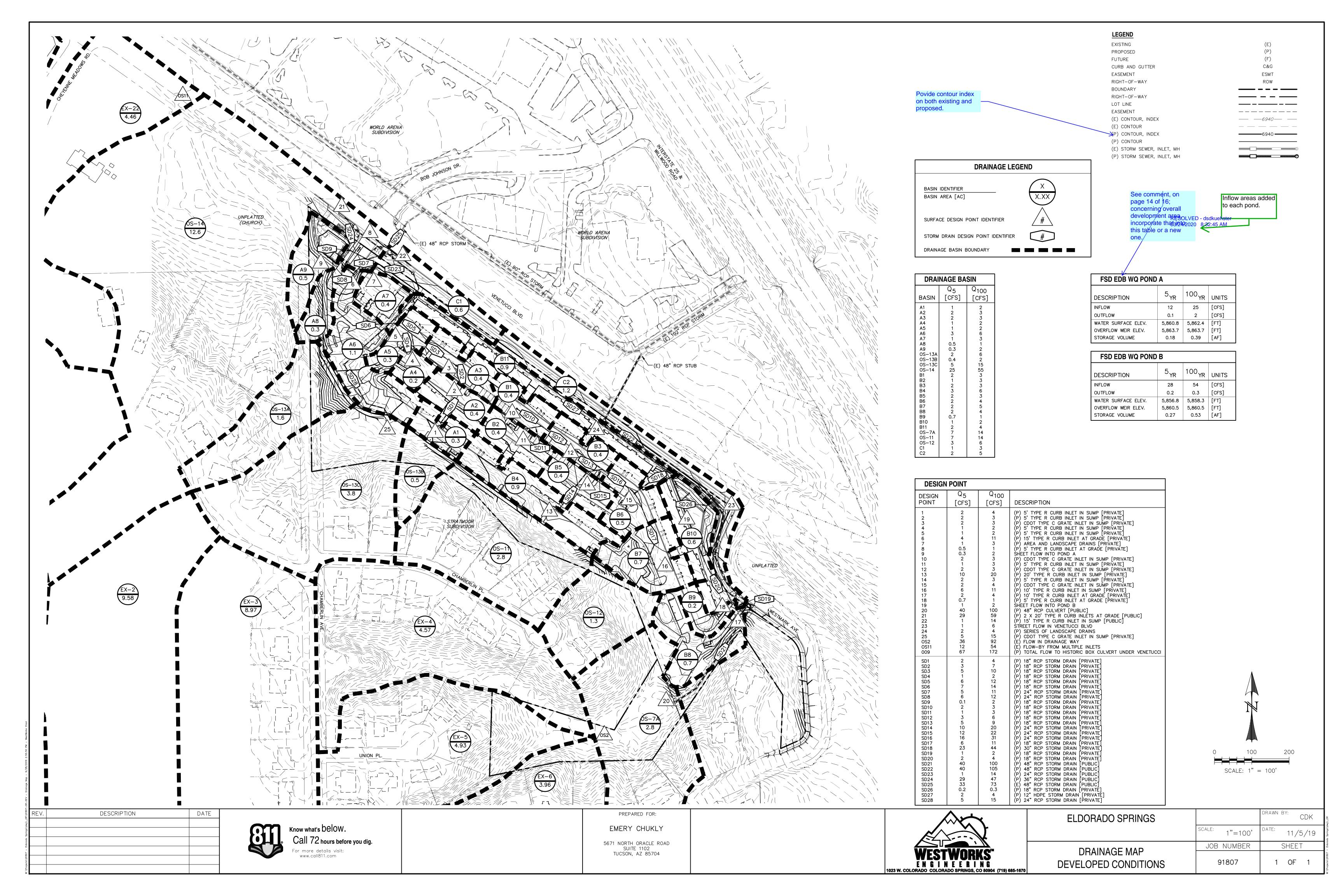
| Routed Hydrograph Results | | | | | | | |
|--------------------------------------|-------|--------|--------|---------|---------|----------|---------|
| Design Storm Return Period = | WQCV | 2 Year | 5 Year | 10 Year | 50 Year | 100 Year | |
| One-Hour Rainfall Depth = | 0.53 | 1.19 | 1.50 | 1.75 | 2.25 | 2.52 | in |
| Calculated Runoff Volume = | 0.185 | 0.443 | 0.581 | 0.713 | 1.085 | 1.324 | acre-ft |
| OPTIONAL Override Runoff Volume = | | | | | | | acre-ft |
| Inflow Hydrograph Volume = | 0.184 | 0.442 | 0.580 | 0.712 | 1.084 | 1.323 | acre-ft |
| Time to Drain 97% of Inflow Volume = | 21.5 | 41.2 | 45.3 | 45.5 | 45.1 | 44.6 | hours |
| Time to Drain 99% of Inflow Volume = | 21.9 | 42.2 | 46.7 | 47.2 | 47.7 | 47.7 | hours |
| Maximum Ponding Depth = | 1.23 | 2.72 | 3.28 | 3.70 | 4.78 | 5.41 | ft |
| Maximum Ponded Area = | 0.15 | 0.18 | 0.20 | 0.21 | 0.23 | 0.25 | acres |
| Maximum Volume Stored = | 0.169 | 0.417 | 0.525 | 0.609 | 0.846 | 1.000 | acre-ft |











Drainage Letter redlines_V2.pdf Markup Summary

1 (2)

ELD

Engineering Review

12/18/28/9778-18 AM

distributed to processor

Service being to groce com

FOR SERVICE TO SERVIC

Subject: EPC ENG Review

Page Label: 1

Author: Steve Kuehster Date: 12/18/2019 7:54:38 AM

Status: Color: E Layer: Space:

ORADO SPI PPR-19-032 Subject: text box Page Label: 1

Author: Steve Kuehster Date: 12/18/2019 7:57:06 AM

Status: Color: Layer: Space: PPR-19-032

2(1)



Subject: text box Page Label: 2

Author: Steve Kuehster Date: 12/18/2019 7:55:43 AM

Status: Color: Layer: Space: Duplicate Page.

3 (1)



Subject: text box Page Label: 3

Author: Steve Kuehster Date: 12/18/2019 7:37:09 AM

Status: Color: Layer: Space: Jennifer Irvine, P.E.

8 (3)



Subject: Highlight Page Label: 8

Author: Steve Kuehster Date: 12/18/2019 7:39:05 AM

Status: Color: Layer: Space:

Subject: text box Page Label: 8

Author: Steve Kuehster Date: 12/18/2019 7:39:12 AM

Status: Color: Layer: Space:

Please call out the drainage structure in Westmark Avenue and indicate it adequacy.

Subject: Highlight Page Label: 8

Author: Steve Kuehster Date: 12/18/2019 7:39:18 AM

Status: Color: Layer: Space:

16 (1)

Subject: text box Page Label: 16

Author: Steve Kuehster Date: 12/18/2019 8:44:23 AM

Status: Color: Layer: Space:

No more than one acre of your development site can flow off site without receiving SWQ treatment. Provide a statement here that demonstrates the amount of development area has been accounted for in the capture volume of the ponds.

138 (1)



Subject: arrow & box Page Label: 138 Author: Steve Kuehster Date: 12/18/2019 9:14:32 AM

Status: Color: Layer: Space:

See comment, on page 14 of 16; concerning overall development area, incorporate that into this table or a new one.

Drainage Letter_V3.pdf Markup Summary

Accepted (2)



Subject: Accepted Page Label: 138 Lock: Locked Author: Chad

Date: 3/25/2020 3:22:41 PM

Status: Color: Layer: Space:



Subject: Accepted Page Label: 140 Lock: Locked Author: Chad

Date: 3/25/2020 3:22:42 PM

Status: Color: Layer: Space:

arrow & box (2)



Subject: arrow & box Page Label: 275 Lock: Locked

Author: Steve Kuehster Date: 3/25/2020 3:22:34 PM

Status: Color: Layer: Space: See comment, on page 14 of 16; concerning overall development area, incorporate that into this table or a new one.



Subject: arrow & box Page Label: 275 Lock: Locked

Author: Steve Kuehster Date: 3/25/2020 3:22:44 PM

Status: Color: Layer: Space: Povide contour index on both existing and proposed.

Callout (3)

s cush and guster and surface flow to the interze tex (DP-4). Benin EX-10 is 1.11 acres (C saids) of this intersection and onto the readway prior to all ratioff death DP-4. Rons onto Festracel Blod. In Point S.

There is no drininge structure Subject: Callout Page Label: 145 Lock: Locked Author: Chad

Date: 3/25/2020 3:22:38 PM

Status: Color: Layer: Space: ? There is no drainage structure in Westmark.

Subject: Callout Page Label: 153

Lock: Locked Author: Chad

Date: 3/25/2020 3:22:39 PM

Status: Color: Layer: Space:

Perimeter area that drains off-site is 0.8-acres -0.7-AC of it is landscape area and 0.1-AC is the

main entrance.

Subject: Callout Page Label: 275 Lock: Locked

Author: Chad

Date: 3/25/2020 3:22:39 PM

Status: Color: Layer: Space:

Inflow areas added to each pond.

EPC ENG Review (2)



Subject: EPC ENG Review

Page Label: 138 Lock: Locked

Author: Steve Kuehster Date: 3/25/2020 3:22:32 PM

Status: Color: Layer: Space:

Subject: EPC ENG Review

Page Label: 1 Lock: Locked

Author: Steve Kuehster Date: 3/25/2020 3:22:48 PM

Status: Color: Layer: Space:

Highlight (2)



Subject: Highlight Page Label: 145 Lock: Locked

Author: Steve Kuehster Date: 3/25/2020 3:22:30 PM

Status: Color: Layer: Space:

Subject: Highlight Page Label: 145

Lock: Locked Author: Steve Kuehster Date: 3/25/2020 3:22:31 PM

Status: Color: Layer: Space:

Stamp Resolved (1)

RESOLVED - dsdkuehste 03/24/2020 8:32:45 AM Subject: Stamp Resolved

Page Label: 275 Lock: Locked

Author: Steve Kuehster Date: 3/25/2020 3:22:45 PM

Status: Color: Layer: Space:

text box (5)

Jennifer Irvine, P.E.
County Engineer/ECM Administrator
Conditions:

Subject: text box Page Label: 140

Lock: Locked

Author: Steve Kuehster Date: 3/25/2020 3:22:29 PM

Status: Color: Layer: Space: Jennifer Irvine, P.E.

recent roadside swale to Design Point 8.

Please call out the drainage structure in Westmark
Avenue and indicate it adequacy.

Subject: text box Page Label: 145 Lock: Locked

Author: Steve Kuehster Date: 3/25/2020 3:22:30 PM

Status: Color: Layer: Space: Please call out the drainage structure in Westmark Avenue and indicate it adequacy.

In integer annotated with this obs.

Loads Springs quarteest the associated for spotteress off-size foreign annotation of the second of the se

Subject: text box Page Label: 153 Lock: Locked Author: Steve Kuehster Date: 3/25/2020 3:22:31 PM

Status: Color: Layer: Space: No more than one acre of your development site can flow off site without receiving SWQ treatment. Provide a statement here that demonstrates the amount of development area has been accounted for in the capture volume of the ponds.

Suite 1102 Tucson, AZ 85704 Duplicate Page. WestWorks Job #91807 Subject: text box Page Label: 139 Lock: Locked

Author: Steve Kuehster Date: 3/25/2020 3:22:33 PM

Status: Color: Layer: Space: Duplicate Page.

ORADO SPI PPR-19-032 Subject: text box Page Label: 138 Lock: Locked

Author: Steve Kuehster Date: 3/25/2020 3:22:33 PM

Status: Color: Layer: Space: PPR-19-032