

FINAL DRAINAGE REPORT FOR SADDLEHORN RANCH – FILING 4

Prepared For: ROI Property Group, LLC 2495 Rigdon Street Napa, CA 94558 (707) 365-6891

> June 9, 2023 Project No. 25142.06

Prepared By: JR Engineering, LLC 5475 Tech Center Drive Colorado Springs, CO 80919 719-593-2593

El Paso County PCD File No.: SF-XX-XXX

SF-23-006

JR- Project # added.

ENGINEER'S STATEMENT:

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by El Paso County for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors, or omissions on my part in preparing this report.

Bryan Law, Colorado P. For and On Behalf of JR		Date	
DEVELOPER'S STA I, the developer, have re and plan.		the requirements specified in this drainage repo	ort
Business Name:	ROI Property Group,	LLC	
By:			
Title: Address:	2495 Rigdon Street Napa, CA 94558		
	n the requirements of the El Pas es 1 and 2 and Engineering Cri	so County Land Development Code, Drainage iteria Manual, as amended.	
Joshua Palmer, P.E. County Engineer/ ECM	Administrator	Date	
Conditions:			



CONTENTS

PURPOSE	1
GENERAL LOCATION AND DESCRIPTION	1
LOCATION DESCRIPTION OF PROPERTY FLOODPLAIN STATEMENT	2
DRAINAGE BASINS AND SUB-BASINS	2
Existing Major Basin Descriptions	4
DRAINAGE DESIGN CRITERIA	6
DEVELOPMENT CRITERIA REFERENCE HYDROLOGIC CRITERIA HYDRAULIC CRITERIA	6
DRAINAGE FACILITY DESIGN	6
GENERAL CONCEPT	7
Water Quality	8
Erosion Control Plan Operation & Maintenance	8
Drainage and Bridge Fees	
SUMMARY	9
REFERENCES: 1	.0

APPENDICES

- A. Figures and Exhibits
- B. Hydrologic Calculations
- C. Hydraulic Calculations
- D. Detention and Water Quality Calculations
- E. Reference Materials
- F. Drainage Maps

LIST OF TABLES:

- 1. Major Drainageway Naming Convention
- 2. Major Drainageway Ex. 100 Year Flow Comparison



PURPOSE

This document is the Final Drainage Report for Filing 4 of Saddlehorn Ranch. The purpose of this report is to:

- 1. Identify on-site and off-site drainage patterns.
- 2. Recommend storm water facilities to collect and convey storm runoff from the proposed development to appropriate discharge and/or detention locations.
- 3. Recommend water quality and detention facilities to control discharge release rates to below historic.
- 4. Demonstrate compliance with surrounding major drainage basin planning studies, master development drainage plans and flood insurance studies.

GENERAL LOCATION AND DESCRIPTION

Location

The proposed Saddlehorn Ranch Filing 4, known as "Filing 4" from herein, is a parcel of land located in Section 3 and 10, Township 13 South, Range 64 West of the 6th Principal Meridian in El Paso County, Colorado. Saddlehorn Ranch is an 824 acre, rural, single family-development. Filing 4 is 162.3 acres and is comprised of 42 lots of the overall Saddlehorn Ranch development. Saddlehorn Ranch is bound by Judge Orr Road to the North and Curtis Road to the West. To the East, Saddlehorn Ranch is bound by undeveloped land owned by Brent Houser Enterprises, LLC. To the south, Saddlehorn Ranch is bound by undeveloped properties owned by Carolyn Gudzunas and Faye Reynolds. Filing 4 is bound by undeveloped land owned by Brent Houser Enterprises, LLC to the east, future Saddlehorn Filing 5 to the south, Judge Orr Road to the north, and by Saddlehorn Filing 3 to the west. A vicinity map is presented in Appendix A.

Currently, there are two major drainageways that will receive flows from Filing 4: Gieck Ranch (WF-R7A) and Haegler Ranch Main Stem 6 (MS-06). These drainageways were analyzed, both hydrologically and hydraulically, in the following reports:

- Haegler Ranch Basin Drainage Basin Planning Study (DBPS), May 2009.
- Santa Fe Springs Haegler Ranch Drainage Basin Letter of Map Revision, June 2004.
- Master Development Drainage Plan and Preliminary Drainage Report for Saddlehorn Ranch, May 2020.
- Gieck Ranch Drainage Basin Planning Study (DBPS), October 2007
- Gieck Ranch Tributary West Fork Reach 7A Channel Analysis Report, March 2, 2022.

The impact of these drainageways and planning studies on the proposed development will be discussed later in the report.

Description of Property

Filing 4 is currently unoccupied and undeveloped. The existing ground cover is sparse vegetation and open space, typical of a Colorado rolling rangeland condition. In general, Filing slopes from south to southeast and the existing drainageways follows this topography.

Per a NRCS web soil survey of the area, Filing 4 is made up of Type A and D soils. Type A soils cover roughly 68% of Filing 4 while Type D soils cover 32% of Filing 4. Group A soils have a high infiltration rate when thoroughly wet. Type D soils have a very slow infiltration when thoroughly wet. A NRCS soil survey map has been presented in Appendix A.

Filing 4 is located in Zone A and Zone X per the No Rise Letter.

Floodplain Statement

Based on the FEMA FIRM Map number 08041C0558G, dated December 7, 2018, Filing 4 lies within Zone AE and Zone X. Zone AE is defined as area subject to inundation by the 1-percent-annual-chance flood event. Zone X is defined as area outside the Special Flood Hazard Area (SFHA) and higher than the elevation of the 0.2-percent-annual-chance (or 500-year) flood. All proposed residential development within Filing 4 will occur in Zone X. The FIRM Map has been presented in Appendix A.

DRAINAGE BASINS AND SUB-BASINS

Address LOMR requirements and BFEs to be approved by FEMA.

Existing Major Basin Descriptions

JR- BFE's were obtained from El Paso CO Floodplain Administrator. Drainage Maps have been updated.

Filing 4 lies within Haegler Ranch Drainage Basin based on the "*Haegler Ranch Drainage Basin Planning Study*" prepared by URS Corporation in May 2009, and the Gieck Ranch Drainage basin based on the "*Gieck Ranch Drainage Basin Planning Study*" prepared by Drexel, Barrell & Co in October 2007 (Not adopted by El Paso County as of July 2019).

The Haegler Ranch Drainage Basin covers approximately 16.6 square miles in unincorporated El Paso County, CO. The Haegler Ranch Drainage Basin is tributary to Black Squirrel Creek. In its existing condition, the basin is comprised of rolling rangeland with poor vegetative cover associated with Colorado's semi-arid climate. The natural Drainageways within the basin are typically shallow and wide with poorly defined flow paths in most areas. Anticipated land use for the basin includes residential and commercial development. Residential developments will range from 0.125 - 5 acre lots with a mix of low, medium and high density developments.

As part of its drainage research, JR Engineering reviewed the following drainage studies, reports and LOMRs:

- Haegler Ranch Drainage Basin Planning Study prepared by URS Corporation in May 2009
- Santa Fe Springs Haegler Ranch Drainage Basin Letter of Map Revision prepared by Tri-Core Engineering in June 2004.
- Master Development Drainage Plan and Preliminary Drainage Report for Saddlehorn Ranch, prepared by JR Engineering, May 2020.
- Gieck Ranch Drainage Basin Planning Study (DBPS), October 2007

Based on flood impacts, stream stability and cost effectiveness, this study recommended a sub-regional detention approach. This allows future development anywhere in the basin with the construction of an associated sub-regional pond. However, based on the *Master Development Drainage Plan and Preliminary Drainage Report for Saddlehorn Ranch*, Filing 4 will utilize three on-site full spectrum water quality and detention ponds instead. These full spectrum detention ponds will limit developed discharge into the MS-06 and WF-R7A Drainageways to less than historic rates.

The Santa Fe Springs – Haegler Ranch Drainage Basin LOMR was executed on Haegler Ranch Tributary 2, 3, and 4. The LOMR revised the onsite effective flood zone from Zone A to Zone AE. See FIRM Map Panel 08041C0558G for limits of LOMR study and revised flood zones, presented in Appendix E.

The Gieck Ranch Drainage Basin covers approximately 22 square miles and begins approximately five miles northeast of the Town of Falcon and travels approximately 15 miles to the southeast. The Gieck Ranch Drainage Basin is tributary to Black Squirrel Creek which drains south to the Arkansas River near the city of Pueblo, Colorado. The majority of the area within the basin is undeveloped and is characterized as rolling rangeland typically associated with Colorado's semi-arid climates. Anticipated land use for the basin includes residential, industrial, agricultural and commercial development. Residential developments will range from 0.125 - 5 acre lots with a mix of low, medium and high density developments.

Based upon provided drainage maps and analysis, Gieck Ranch discharges a total of 1,017 cfs onto the site within Major Drainageway Gieck Ranch West Fork Reach 7A (WF-R7A). An existing 66" CMP and 36" CMP convey the offsite flow across Judge Orr Road onto the site. The existing culverts at Judge Orr Road are undersized for existing and future flows resulting in localized overtopping. The DBPS recommends the culvert be upsized to four –12' x 5' box culverts. The culvert will not be upsized within the context of this report and development. The culvert is owned by El Paso County and timing of the recommended improvements will be controlled by the County. The overtopping at the intersection of WF-

R7A is not contained within the 100-year floodplain Clarify if there will be adverse effects to the development if the development is installed prior to the upsizing of the culverts.

See Table 2 for comparison of Drainageway identification and the namine context of this report. See Table 3 for a comparison of 100-year nows as calculated in the aforementioned DBPS and LOMR. An existing conditions drainage map is presented in Appendix E.

JR- Text moved to the next page.

Table 1: Major Drainageway Naming Convention Attach text to table on next page

Major Drainageway Naming Conventions									
Saddlehorn Ranch MDDP/PDR:	Per Haegler Ranch DBPS:	Per Gieck Ranch DBPS:	Per Sante Fe Springs LOMR:						
MS-06	Main Stem (MS- 06)	N/A*	Haegler Ranch Tributary 3						
WF-R7A	N/A*	West Fork (Middle)/WF-R7A	N/A*						

Table 2: Major Drainageway – Ex. 100-Year Flow Comparison

Major Drainageways: 100-Year Flow Comparison									
Drainageway Name	Contributing Area (sq. mi.)	Q ₁₀₀ Per Haegler Ranch DBPS:	Q ₁₀₀ Per Gieck Ranch DBPS:	Q ₁₀₀ Per Sante Fe Springs LOMR:					
MS-06 @ Curtis Road	@ Curtis Road 1.05 590 cfs		N/A*	505 cfs					
WF-R7A @ Judge Orr Road	1.50	N/A*	1,017 cfs	N/A*					

^{*}N/A: Flow regime outside limits of study.

The *Master Development Drainage Plan and Preliminary Drainage Report for Saddlehorn Ranch* proposed the overall drainage facility design for Saddlehorn Ranch. Within the context of this report, onsite drainage basins with associated full spectrum water quality ponds were established. As it pertains to Filing 4, three full spectrum water quality ponds are recommended. Roadside ditches and local street culverts will be utilized to capture and convey Filing 4's runoff to the water quality ponds. Three full spectrum water quality ponds were proposed with the Saddlehorn Filing 3 improvements. Saddlehorn Filing 4 will also utilize these three ponds. The ponds were sized for both the Filing 3 and Filing 4 improvements. Pond C and Pond E will discharge into Drainageway MS-06, while Pond D will release into Drainageway WF-R7A. All ponds are full spectrum and will release at less than historic rates. All pond calculations that were completed with the Filing 3 Drainage Report can be found in Appendix E.

Existing Sub-basin Drainage

PCD Filing No. SF234

On-site, existing sub-basin drainage patterns are generally from north JR- Project # added for reference. Drainageway MS-06 and Drainageway WF-R7A. On-site areas flow directly into these drainageways, which also bypass off-site flows through the site.

On-site, existing drainage basins were established based upon existing topography and the limits of the 100-year floodplain. These existing sub-basins were analyzed in the *Master Development Drainage Plan*

JR- Noted.

Final Drainage Report Filing 4 - Saddlehorn Ranch

and Preliminary Drainage Report for Saddlehorn Ranch. An existing drainage map and existing drainage calcs have been provided in Appendix E. A Filing 4 Existing Conditions Drainage Map has been provided in Appendix F. Please provide calculations corresponding to this map and add discussion

Proposed Sub-basin Drainag within report as well.

The proposed Filing 4 basin delineation is as follows;

JR- Existing basins discussion added to the report. Existing calculations can be found in Appendix E under hydraulic calculation for Saddlehorn Ranch Preliminary Drainage Report.

Basin C consists of Sub-Basins C1-C8 combining for a total of 46.69 acres. In its existing condition, Basin C is rolling rangeland and runoff generally flows southeast towards Drainageway MS-06. In the proposed condition, Basin C will be rural 2.5 acre lots, paved roadway, and will include Pond C. Runoff from this basin will be collected in road side ditches and conveyed to Pond C located in the southeast corner of the Filing 4 development. Pond C will be a full spectrum water quality and detention pond, and will release at less than historic rates into Drainageway MS-06.

Basin D consists of Sub-basins D1-D9 combining for a total of 53.78 acres. In its existing condition, Basin D is rolling rangeland and runoff generally flows east to Drainageway WF-R7A. In the proposed condition, Basin D will be rural 2.5 acre lots, paved roadway, and will include Pond D. Runoff from this basin will be collected in road side ditches and conveyed west to Pond D located in the northeast corner of the Filing 4 development. Pond D is a full spectrum water quality and detention pond, and will release at less than historic rates into Drainageway WF-R7A.

Basin UD consists of Sub-basins UD1-UD4 combining for a total of 65.86 acres. In their existing condition, these basins are rolling rangeland. Runoff from Basins UD1 & UD3 generally flow south and east to Drainageway WF-R7A. Basin UD3 represents Drainageway WF-R7A and the runoff generated along the Filing 4 boundary. Basin UD4 flows south to Drainageway MS-06. In the proposed condition, Basins UD1, UD3, and UD4 will be rural 2.5 acre lots with an imperviousness = 6.2%, and will be excluded from permanent stormwater quality management per Section I.7.1.B.5 of the ECM – Stormwater Quality Policy and Procedures.

Basin OS consists of Sub-basins OS1-OS2 combining for a total of 2.98 acres of offsite area. In their existing condition, these basins are paved roadway (Judge Orr Road) and undeveloped area. In the proposed condition, these basins will be improved with 8' of pavement width for the Judge Orr Road stretch. Basins OS1-OS2 will flow on-site prior to being captured in a roadside swale and conveyed to the Full Spectrum Detention Pond D prior to being released into Drainageway WF-R7A.

A summary table of proposed basin parameters and flow rates are presented in Appendix B.

Basin D and Basin OS runoff will be captured in roadside swales and conveyed to the proposed Pond D. This full spectrum pond will release treated flows at less than historic rates to minimize adverse impacts downstream. Basin C will be captured in roadside swales and conveyed to the proposed Pond C. Pond C discharges into Drainageway MS-06, and Pond D discharges into Drainageway WF-R7A.

All pond design parameters for Ponds C & D were completed with the Filing 3 report. These pond designs and parameters can be found in Appendix E. The proposed forebay calculations for the Filing 4 pond outfalls can be found in Appendix D. In the previous section, it states that Filing

JR- While Pond E is located along the boundary of filing 4. None of the filing 4 basins drain to Pond E as shown in the proposed drainage maps. The previous section was revised to state Filing 4 utilized 2 ponds.

In the previous section, it states that Filing 4 utilizes 3 ponds designed with Filing 3. The above section only makes references to 2 of the ponds. Include what areas use the third pond.

DRAINAGE DESIGN CRITERIA

Development Criteria Reference

Storm drainage analysis and design criteria for the project were taken from the "City of Colorado Spring/El Paso County Drainage Criteria Manual" Volumes 1 and 2 (EPCDCM), dated October 12, 1994, the "Urban Storm Drainage Criteria Manual" Volumes 1 - 3 (USDCM) and Chapter 6 and Section 3.2.1 of Chapter 13 of the "Colorado Springs Drainage Criteria Manual (CCSDCM), dated May 2014, as adopted by El Paso County.

Hydrologic Criteria

All hydrologic data was obtained from the "El Paso Drainage Criteria Manual" Volumes 1 and 2, and the "Urban Drainage and Flood Control District Urban Storm Drainage Criteria Manual" Volumes 1, 2, and 3. Onsite drainage improvements were designed based on the 5 year (minor) storm event and the 100-year (major) storm event. Rational Method calculations were prepared, in accordance with Section 13.3.2.1. of the CCSDCM, for the sub-basins that directly impact the sizing of ditches and local street culverts. Rational method calculations are presented in Appendix B.

Urban Drainage and Flood Control District's UD-Detention, Version 4.04 workbook was used for pond sizing with the Filing 3 report. Required detention volumes and allowable release rates were designed per USDCM and CCS/EPCDCM. Pond sizing spreadsheets that were completed with the Filing 3 improvements are presented in Appendix E.

Hydraulic Criteria

Autodesk Inc.'s Hydraflow Express Extension (Volume 10.5) was used for roadside ditch design. Ditches were checked for velocity and capacity per the CCS/EPCDCM Section 12.3.2.2. In order to check both capacity and velocity, a cross section analysis was performed on the roadside swales using the basin's maximum runoff Q and the proposed uniform slope of the swale. Swale cross sections have been presented in Appendix C.

Autodesk Inc.'s Hydraflow Express Extension (Volume 10.5) was used for local road crossing culvert design. Culvert size was determined based on 100-year flows and hydraulic criteria from EPCDCM Chapter 9 –Culvert Design. All local road crossing culvert design reports are presented in Appendix C.

DRAINAGE FACILITY DESIGN

General Concept

The proposed stormwater conveyance system was designed to convey the developed Filing 4 runoff to one of three full spectrum detention ponds via roadside ditches and local street culverts. These full spectrum ponds were designed to release at less than historic rates to minimize adverse impacts downstream.

Final Drainage Report Filing 4 - Saddlehorn Ranch

Improvements to Drainageway MS-06 within the Saddlehorn Filing 3 and Filing 4 improvements were completed with the Saddlehorn Filing 3 Drainage Report. A no rise study was conducted on the proposed Drainageway MS-06 improvements to ensure no rises to the floodplain occur as a result of the Filing 3 and 4 developments. All proposed drainageway improvements, including the San Isidro culvert crossing and channel sections were incorporated with the Saddlehorn Filing 3 improvements. A floodplain analysis was performed on Drainageway WF-R7A as part of the Saddlehorn Filing 4 development to ensure that the proposed improvements were not impacted by the existing 100-year floodplain and to ensure the improvements did not impact the drainageway. Pertinent information regarding this study can be found in Appendix E. Outfall protection from Pond D is the only improvement to Drainageway WF-R7A at this time. Further analysis of Drainageway WF-R7A regarding channel improvements will need to be revisited as this area develops. The remaining improvements to Drainageway MS-06 shall be implemented with the Filing 5 improvements.

Analysis needs to be within this report.

Specific Details

JR- BFE's and updated floodplain were received from FI Paso CO Floodplain manager

as development is occurring adjacent

to the channel reach.

Four Step Process to Minimize Adverse Impacts of I from El Paso CO Floodplain manager.

In accordance with the El Paso County Drainage Criteria Manual Volume 2, this site has implemented the four step process to minimize adverse impacts of urbanization. The four step process includes reducing runoff volumes, stabilizing drainageways, treating the water quality capture volume (WQCV), and consider the need for Industrial Commercial BMP's.

Step 1, Reducing Runoff Volumes: The development of the project site is proposed single family residential lots (2.5 ac. min.) with open spaces and lawn areas interspersed within the development which helps disconnect impervious areas and reduce runoff volumes. Roadways utilize soil riprap lined roadside ditches further disconnecting impervious areas. These practices will also allow for increased infiltration and reduce runoff volume.

Step 2, Stabilize Drainageways: Filing 4 utilizes roadside ditches with culvert crossings throughout. These roadside ditches direct the on-site development flows to the proposed detention ponds within the project that releases at or below historic rates into Drainageways MS-06 and WF-R7A. Based upon the proposed reduction in released flows compared to the pre-developed flows, no impacts to downstream Drainageway MS-06 or Drainageway WF-R7A are anticipated. Drainageway MS-06 was stabilized with the Filing 3 improvements.

Step 3, Provide WQCV: Runoff from this development is treated through capture and slow release of the WQCV in full spectrum water quality and detention ponds that are designed per current El Paso County drainage criteria. List the ponds that will treat filing 4 and clarify they were analyzed under filing 3. Based on the CD's ponds C and D are being modified (adding a forebay), clearly state the work on these pond that will be completed with filing 4. Step 4 Consider the need for Industrial and Commercial BMP's. No industrial or commercial uses are proposed within the need for Industrial and Commercial BMP's. No industrial or commercial uses are proposed within the need for Industrial and Commercial BMP's. No industrial or commercial uses are proposed within the need for Industrial and Commercial BMP's. No industrial or commercial uses are proposed within the need for Industrial and Commercial BMP's. No industrial or commercial uses are proposed within the need for Industrial and Commercial BMP's. No industrial or commercial uses are proposed within the need for Industrial and Commercial BMP's. No industrial or commercial uses are proposed within the need for Industrial and Commercial BMP's. No industrial or commercial uses are proposed within the need for Industrial and Commercial BMP's. No industrial or commercial uses are proposed within the need for Industrial and Commercial BMP's. No industrial or commercial uses are proposed within the need for Industrial and Commercial BMP's. No industrial or commercial uses are proposed within the need for Industrial and Commercial BMP's. No industrial or commercial uses are proposed within the need for Industrial and Commercial BMP's. No industrial or commercial uses are proposed within the need for Industrial and Commercial BMP's are detailed in this plan and narrative to protect receiving waters.

JR- Discussion regarding Pond D and the groundwater table have been added to this section.

Final Drainage Report

Filing 4 - Saddlehorn Ranch

Address specific design of Pond D, including how groundwater aspects are to be handled

Water Quality

In accordance with Section 13.3.2.1 of the CCS/EPCDCM, full spectrum water quality and detention are provided for all developed basins. Outlet structure release rates are limited to less than historic rates to minimize adverse impacts to downstream stormwater facilities.

Erosion Control Plan

The El Paso County Drainage Criteria Manual specifies an Erosion Control Plan and associated cost estimate must be submitted with each Final Drainage Report. The Erosion Control Plans for Filing 4 have been submitted concurrently with this report.

Operation & Maintenance

In order to ensure the function and effectiveness of the stormwater infrastructure, maintenance activities such as inspection, routine maintenance, restorative maintenance, rehabilitation and repair, are required. All proposed drainage structures within the any platted County ROW will be owned and maintained by El Paso County. All proposed drainage structures within easements or tracts will be owned and maintained by the Saddlehorn Ranch Metro District. An Inspection & Maintenance Plan is submitted concurrently with this drainage report that details the required maintenance activities and intervals to ensure proper function of all stormwater infrastructure in the future.

Drainage and Bridge Fees

Drainage and Bridge Fees are due at time of final platting. An estimate of basin fees for the proposed development within Haegler Ranch drainage basin is provided below. Fee reduction for low density lots are applied to the overall basin fees in the next section. Additionally, reimbursable expenses are detailed below.

Total Filing 4 Platted Acres: 162.3 ac

Total Filing 4 Impervious Acres = 16.2 ac (162.3 ac x 10%)

Filing 4 Fee Totals (Prior to Reductions):

Bridge Fees

 $$1,916/ac \times 16.2 ac = $31,039$

Drainage Fees

 $12,985/ac \times 16.2 ac = 10,357$

Filing 4 Drainage Fee Reduction: 25% Reduction for Low Density Lots: \$210,357 x 25% = \$52,589

Filing 4 Fee Totals (After Reductions):

Bridge Fees

 $1.916/ac \times 16.2 ac = $31,039$

Construction Cost Opinion

Cost opinion has been presented in Appendix A.

Drainage Fees

\$210,357 - \$31,039 = \$179,318

Should be subtracting the reduction in drainage fees, not the bridge fee.

JR- Calculation updated.

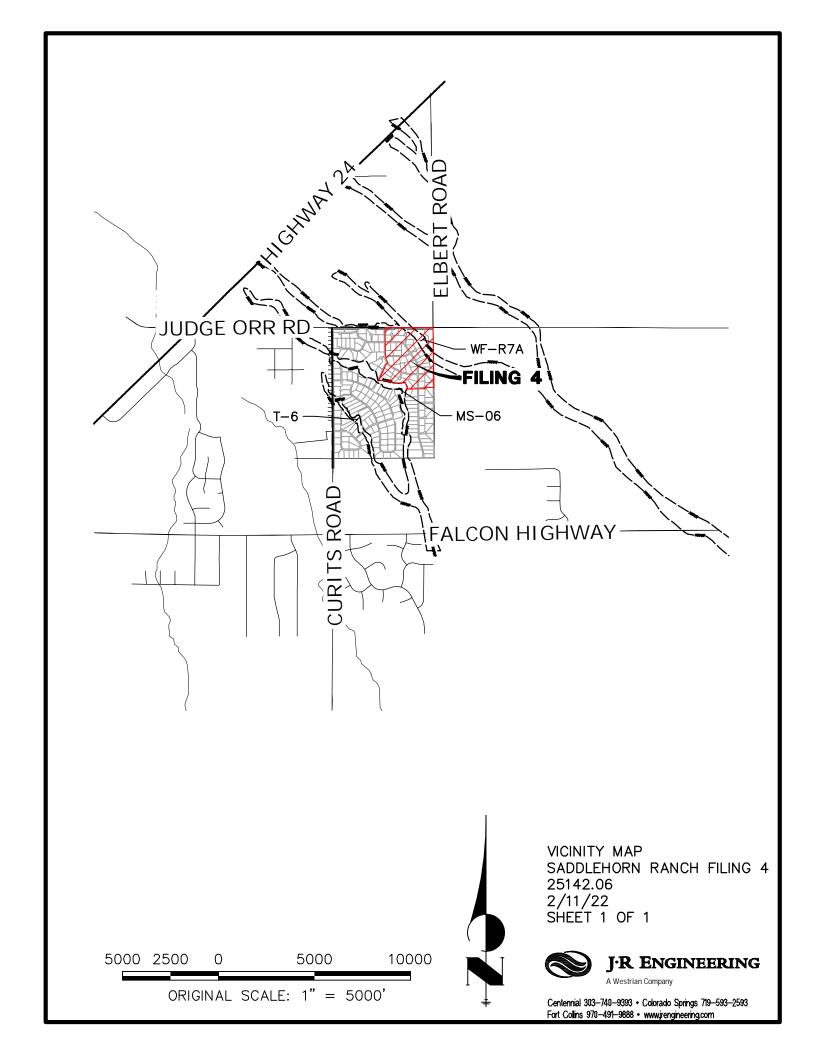
SUMMARY

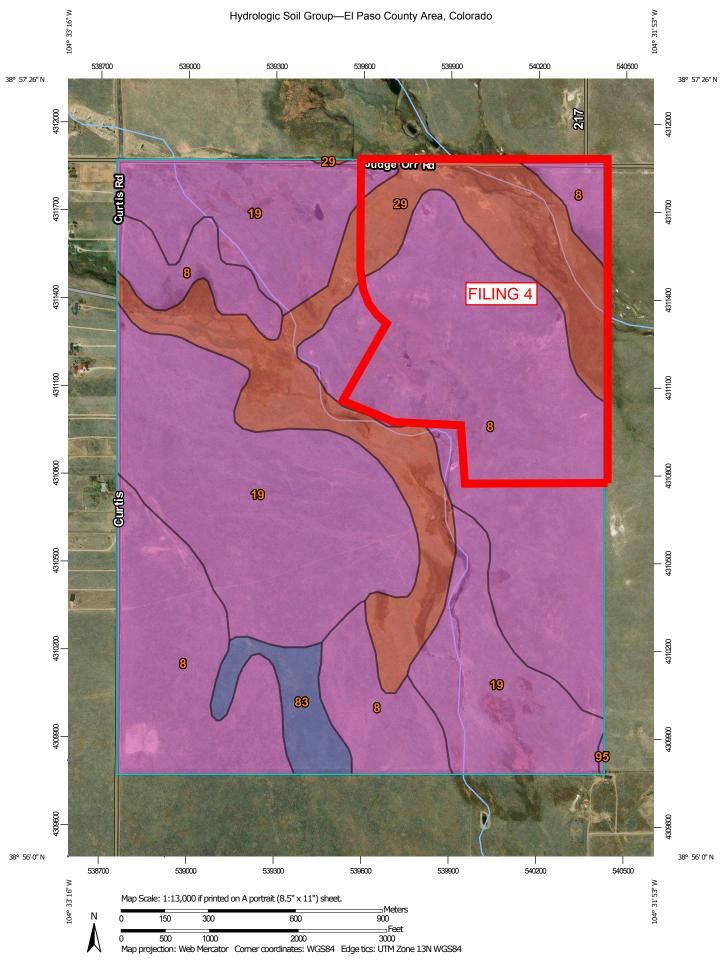
The proposed development remains consistent with pre-development drainage conditions with the construction of the recommended drainage improvements, including swales, culverts, detention ponds and drainage channel improvements. The proposed development will not adversely affect the offsite major drainageways or surrounding development. This report meets the latest El Paso County Drainage Criteria requirements for this site and is in accordance with the PDR/MDDP for Saddlehorn Ranch.

REFERENCES:

- 1. <u>City of Colorado Springs Drainage Criteria Manual Volume 1</u>, City of Colorado Springs, CO, May 2014.
- 2. <u>Urban Storm Drainage Criteria Manual</u>, Urban Drainage and Flood Control District, Latest Revision.
- 3. <u>Master Development Drainage Plan and Preliminary Drainage Report for Saddlehorn Ranch</u>, JR Engineering, May 2020.
- 4. Haegler Ranch Drainage Basin Planning Study, URS Corporation, May 2009.
- 5. <u>The Santa Fe Springs Haegler Ranch Drainage Basin LOMR</u>, Federal Emergency Management Agency, October 20, 2004.
- 6. Final Drainage Report for Saddlehorn Ranch Filing 3, JR Engineering, February 4, 2022
- 7. Gieck Ranch Tributary West Fork Reach 7A Channel Analysis Report For Saddlehorn Filing No. 4, JR Engineering, February 21, 2022

APPENDIX A FIGURES AND EXHIBITS





MAP LEGEND MAP INFORMATION The soil surveys that comprise your AOI were mapped at Area of Interest (AOI) С 1:24.000. Area of Interest (AOI) C/D Please rely on the bar scale on each map sheet for map Soils D measurements. Soil Rating Polygons Not rated or not available Α Source of Map: Natural Resources Conservation Service Web Soil Survey URL: **Water Features** A/D Coordinate System: Web Mercator (EPSG:3857) Streams and Canals В Maps from the Web Soil Survey are based on the Web Mercator Transportation projection, which preserves direction and shape but distorts B/D Rails --distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more Interstate Highways accurate calculations of distance or area are required. C/D **US Routes** This product is generated from the USDA-NRCS certified data as D Major Roads of the version date(s) listed below. Not rated or not available -Local Roads Soil Survey Area: El Paso County Area, Colorado Soil Rating Lines Survey Area Data: Version 16, Sep 10, 2018 Background Aerial Photography Soil map units are labeled (as space allows) for map scales 1:50,000 or larger. A/D Date(s) aerial images were photographed: May 22, 2016—Aug 17, 2017 B/D The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor C/D shifting of map unit boundaries may be evident. D Not rated or not available **Soil Rating Points** Α A/D B/D

Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
8	Blakeland loamy sand, 1 to 9 percent slopes	A	388.3	44.6%
19	Columbine gravelly sandy loam, 0 to 3 percent slopes	Α	307.3	35.3%
29	Fluvaquentic Haplaquolls, nearly level	D	150.0	17.2%
83	Stapleton sandy loam, 3 to 8 percent slopes	В	24.6	2.8%
95	Truckton loamy sand, 1 to 9 percent slopes	А	0.6	0.1%
Totals for Area of Interes	est		870.8	100.0%

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

Rating Options

Aggregation Method: Dominant Condition

Component Percent Cutoff: None Specified

Tie-break Rule: Higher

NOTES TO USERS

This map is for use in administering the National Flood Insurance Program. It does not necessarily identify all areas subject to flooding, particularly from local drainage sources of small size. The **community map repository** should be consulted for possible updated or additional flood hazard information.

To obtain more detailed information in areas where **Base Flood Elevations** (BFEs) and/or **floodways** have been determined, users are encouraged to consult the Flood Profiles and Floodway Data and/or Summary of Stillwater Elevations tables contained within the Flood Insurance Study (FIS) report that accompanies this FIRM. Users should be aware that BFEs shown on the FIRM represent rounded whole-foot elevations. These BFEs are intended for flood insurance rating purposes only and should not be used as the sole source of flood elevation information. Accordingly, flood elevation data presented in the FIS report should be utilized in conjunction with the FIRM for purposes of construction and/or floodplain management.

Coastal Base Flood Elevations shown on this map apply only landward of 0.0' North American Vertical Datum of 1988 (NAVD88). Users of this FIRM should be aware that coastal flood elevations are also provided in the Summary of Stillwater Elevations table in the Flood Insurance Study report for this jurisdiction. Elevations shown in the Summary of Stillwater Elevations table should be used for construction and/or floodplain management purposes when they are higher than the elevations shown on this FIRM

Boundaries of the **floodways** were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations with regard to requirements of the National Flood Insurance Program. Floodway widths and other pertinent floodway data are provided in the Flood Insurance Study report for this invisidiation.

Certain areas not in Special Flood Hazard Areas may be protected by **flood control structures**. Refer to section 2.4 "Flood Protection Measures" of the Flood Insurance Study report for information on flood control structures for this jurisdiction.

The **projection** used in the preparation of this map was Universal Transverse Mercator (UTM) zone 13. The **horizontal datum** was NAD83, GRS80 spheroid. Differences in datum, spheroid, projection or UTM zones zones used in the production of FIRMs for adjacent jurisdictions may result in slight positional differences in map features across jurisdiction boundaries. These differences do not affect the accuracy of this FIRM.

Flood elevations on this map are referenced to the North American Vertical Datum of 1988 (NAVD88). These flood elevations must be compared to structure and ground elevations referenced to the same vertical datum. For information regarding conversion between the National Geodetic Vertical Datum of 1929 and the North American Vertical Datum of 1988, visit the National Geodetic Survey website at http://www.ngs.noaa.gov/ or contact the National Geodetic Survey at the following address:

NGS Information Services NOAA, N/NGS12 National Geodetic Survey SSMC-3, #9202 1315 East-West Highway Silver Spring, MD 20910-3282

To obtain current elevation, description, and/or location information for **bench marks** shown on this map, please contact the Information Services Branch of the National Geodetic Survey at (301) 713-3242 or visit its website at http://www.ngs.noaa.gov/.

Base Map information shown on this FIRM was provided in digital format by El Paso County, Colorado Springs Utilities, and Anderson Consulting Engineers, Inc. These data are current as of 2008.

This map reflects more detailed and up-to-date **stream channel configurations and floodplain delineations** than those shown on the previous FIRM for this jurisdiction. The floodplains and floodways that were transferred from the previous FIRM may have been adjusted to conform to these new stream channel configurations. As a result, the Flood Profiles and Floodway Data tables in the Flood Insurance Study Report (which contains authoritative hydraulic data) may reflect stream channel distances that differ from what is shown on this map. The profile baselines depicted on this map represent the hydraulic modeling baselines that match the flood profiles and Floodway Data Tables if applicable, in the FIS report. As a result, the profile baselines may deviate significantly from the new base map channel representation and may appear outside of the floodplain.

Corporate limits shown on this map are based on the best data available at the time of publication. Because changes due to annexations or de-annexations may have occurred after this map was published, map users should contact appropriate community officials to verify current corporate limit locations.

Please refer to the separately printed **Map Index** for an overview map of the county showing the layout of map panels; community map repository addresses; and a Listing of Communities table containing National Flood Insurance Program dates for each community as well as a listing of the panels on which each community is

Contact **FEMA Map Service Center** (MSC) via the FEMA Map Information eXchange (FMIX) 1-877-336-2627 for information on available products associated with this FIRM. Available products may include previously issued Letters of Map Change, a Flood Insurance Study Report, and/or digital versions of this map. The MSC may also be reached by Fax at 1-800-358-9620 and its website at http://www.msc.fema.gov/.

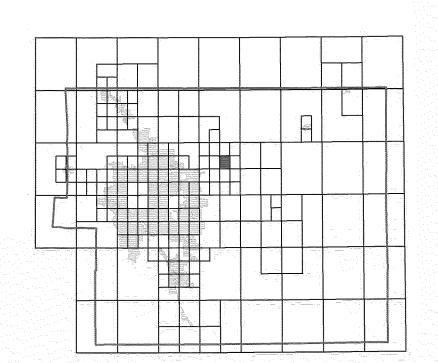
If you have **questions about this map** or questions concerning the National Flood Insurance Program in general, please call **1-877-FEMA MAP** (1-877-336-2627) or visit the FEMA website at http://www.fema.gov/business/nfip.

El Paso County Vertical Datum Offset Table

Flooding Source Vertical Datum Offset (ft)

REFER TO SECTION 3.3 OF THE EL PASO COUNTY FLOOD INSURANCE STUDY FOR STREAM BY STREAM VERTICAL DATUM CONVERSION INFORMATION

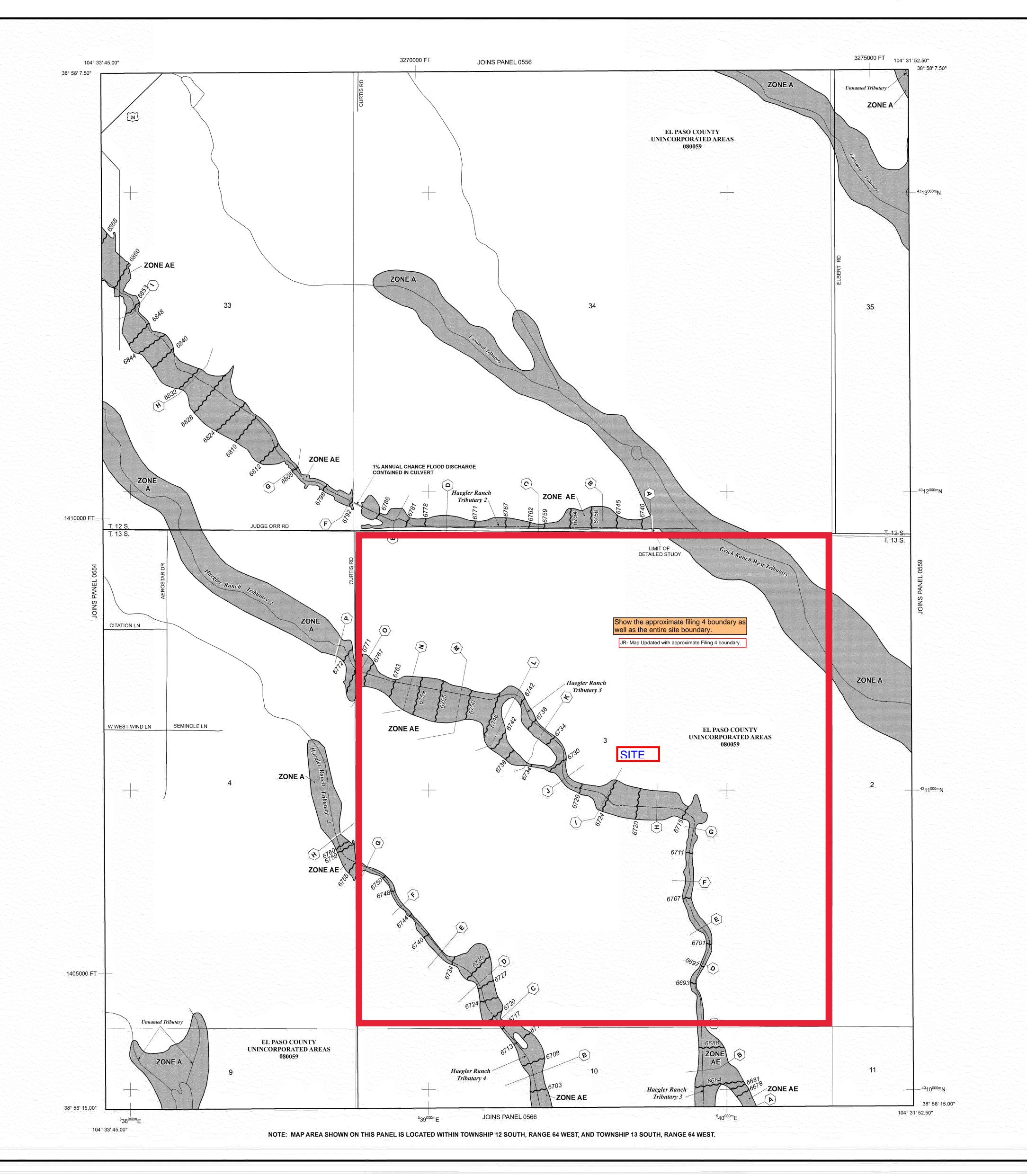
Panel Location Map



This Digital Flood Insurance Rate Map (DFIRM) was produced through a Cooperating Technical Partner (CTP) agreement between the State of Colorado Water Conservation Board (CWCB) and the Federal Emergency Management Agency (FEMA).



Additional Flood Hazard information and resources are available from local communities and the Colorado Water Conservation Board.



LEGEND

SPECIAL FLOOD HAZARD AREAS (SFHAS) SUBJECT TO INUNDATION BY THE 1% ANNUAL CHANCE FLOOD

The 1% annual chance flood (100-year flood), also known as the base flood, is the flood that has a 1% chance of being equaled or exceeded in any given year. The Special Flood Hazard Area is the area subject to flooding by the 1% annual chance flood. Areas of Special Flood Hazard include Zones A, AE, AH, AO, AR, A99, V, and VE. The Base Flood

Elevation is the water-surface elevation of the 1% annual chance flood.

ZONE A No Base Flood Elevations determined.

ZONE AE

Base Flood Elevations determined.

ZONE AH

Flood depths of 1 to 3 feet (usually areas of ponding); Base Flood Elevations determined.

ZONE AO Flood depths of 1 to 3 feet (usually sheet flow on sloping terrain); average depths determined. For areas of alluvial fan flooding, velocities also

depths determined. For areas of alluvial fan flooding, velocities also determined.

ZONE AR Special Flood Hazard Area Formerly protected from the 1% annual chance flood by a flood control system that was subsequently decertified. Zone AR

protection from the 1% annual chance or greater flood. **ZONE A99** Area to be protected from 1% annual chance flood by a Federal flood protection system under construction; no Base Flood Elevations

indicates that the former flood control system is being restored to provide

determined.

ZONE V Coastal flood zone with velocity hazard (wave action); no Base Flood

Elevations determined.

ZONE VE Coastal flood zone with velocity hazard (wave action); Base Flood Elevations determined.

FLOODWAY AREAS IN ZONE AE

The floodway is the channel of a stream plus any adjacent floodplain areas that must be kept free of encroachment so that the 1% annual chance flood can be carried without substantial increases in flood heights.

OTHER FLOOD AREAS

ZONE X Areas of 0.2% annual chance flood; areas of 1% annual chance flood with average depths of less than 1 foot or with drainage areas less than 1 square mile; and areas protected by levees from 1% annual chance flood.

OTHER AREAS

Areas determined to be outside the 0.2% annual chance floodplain.

Areas in which flood hazards are undetermined, but possible.

COASTAL BARRIER RESOURCES SYSTEM (CBRS) AREAS

OTHERWISE PROTECTED AREAS (OPAs)

CBRS areas and OPAs are normally located within or adjacent to Special Flood Hazard Areas.

Floodplain boundary
Floodway boundary

Zone D Boundary

CBRS and OPA boundary

Boundary dividing Special Flood Hazard Areas of different Base Flood Flevations, flood depths or flood velocities.

Flood Elevations, flood depths or flood velocities.

513 Base Flood Elevation line and value; elevation in feet*

(EL 987) Base Flood Elevation value where uniform within zone;

elevation in feet*

* Referenced to the North American Vertical Datum of 1988 (NAVD 88)

A Cross section line

----- **23** Transect line

97° 07' 30.00" Geographic coordinates referenced to the North American 32° 22' 30.00" Datum of 1983 (NAD 83)

4275^{000m}N 1000-meter Universal Transverse Mercator grid ticks, zone 13

6000000 FT 5000-foot grid ticks: Colorado State Plane coordinate system, central zone (FIPSZONE 0502),

DX5510 Bench mark (see explanation in Notes to Users section of

River Mile

this FIRM panel)

MAP REPOSITORIES
Refer to Map Repositories list on Map Index

EFFECTIVE DATE(S) OF REVISION(S) TO THIS PANEL

DECEMBER 7, 2018 - to update corporate limits, to change Base Flood Elevations and Special Flood Hazard Areas, to update map format, to add roads and road names, and to

EFFECTIVE DATE OF COUNTYWIDE

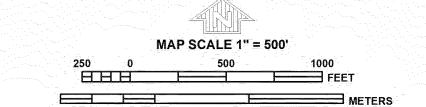
FLOOD INSURANCE RATE MAP

incorporate previously issued Letters of Map Revision.

For community map revision history prior to countywide mapping, refer to the Community

Map History Table located in the Flood Insurance Study report for this jurisdiction.

To determine if flood insurance is available in this community, contact your insurance agent or call the National Flood Insurance Program at 1-800-638-6620.



PANEL 0558G

FIRM

FLOOD INSURANCE RATE MAP

EL PASO COUNTY,

COLORADO

AND INCORPORATED AREAS

PANEL 558 OF 1300

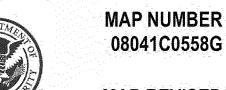
(SEE MAP INDEX FOR FIRM PANEL LAYOUT)

CONTAINS:

COMMUNITY EL PASO COUNTY

JNITY NUMBER PANEL SUFFIX
OUNTY 080059 0558 G

Notice to User. The **Map Number** shown below should be used when placing map orders: the **Community Number** shown above should be used on insurance applications for the subject



MAP REVISED DECEMBER 7, 2018

Federal Emergency Management Agency

2023 Financial Assurance Estimate Form (with pre-plat construction)

Use updated Filing 4 FAE and address the comments.

JR Response: FAE has been updated.

Updated: 12/8/2022

PROJECT INFORMATION								
Saddlehorn Filing 4	2/9/2023	EGP-22-004						
Project Name	Date	PCD File No.						

			Unit				(with Pre	-Plat	-Plat Construction)	
Description	Quantity	Units	Cost			Total	% Complete		Remaining	
SECTION 1 - GRADING AND EROSION CONTRO	(Construction	and Permar	ent BMPs)							
Earthwork										
less than 1,000; \$5,300 min		CY	\$ 8.00	=	\$	-		\$	-	
1,000-5,000; \$8,000 min		CY	\$ 6.00	=	\$	-		\$	-	
5,001-20,000; \$30,000 min		CY	\$ 5.00	=	\$	-		\$	-	
20,001-50,000; \$100,000 min		CY	\$ 3.50	=	\$	-		\$	-	
50,001-200,000; \$175,000 min	60,124	CY	\$ 2.50	=	\$	175,000.00		\$	175,000.00	
greater than 200,000; \$500,000 min		CY	\$ 2.00	=	\$	-		\$	-	
Permanent Erosion Control Blanket		SY	\$ 8.00	=	\$	-		\$	-	
Permanent Seeding (inc. noxious weed mgmnt.) & Mulching	41.00	AC	\$ 1,875.00	=	\$	76.875.00		\$	76,875.00	
Permanent Pond/BMP (provide engineer's estimate)		EA		=	\$	-		\$	-	
Concrete Washout Basin	1	EA	\$ 1,089.00	=	\$	1,089.00		\$	1,089.00	
Inlet Protection	10	EA	\$ 202.00	=	\$	2,020.00		\$	2,020.00	
Outlet Protection	10	EA	\$ 202.00	=	\$	2,020.00		\$	2,020.00	
Rock Check Dam	10	EA	\$ 605.00	=	\$	2,020.00		\$	2,020.00	
Safety Fence		LF	\$ 3.00		\$			\$		
Sediment Basin	2	EA	\$ 2,132.00		\$	4,264.00		\$	4,264.00	
Sediment Trap	2	EA	\$ 500.00		\$	4,204.00		\$	4,204.00	
Silt Fence	7 700	LF	\$ 3.00		\$	22 240 00		\$	22 240 00	
	7,780	LF		=	_	23,340.00			23,340.00	
Slope Drain			\$ 40.00		\$	-		\$	-	
Straw Bale		EA	\$ 31.00	=	\$	-		\$	-	
Straw Wattle/Erosion Logs		LF	\$ 7.00	=	\$	-		\$	-	
Surface Roughening		AC	\$ 250.00		\$	-		\$	-	
Temporary Erosion Control Blanket		SY	\$ 3.00	=	\$	-		\$	-	
Temporary Seeding and Mulching		AC	\$ 1,666.00	=	\$	-		\$	-	
Vehicle Tracking Control	3	EA	\$ 2,867.00	=	\$	8,601.00		\$	8,601.00	
				=	\$	-		\$	-	
[insert items not listed but part of construction plans]				=	\$	-		\$	-	
MAI	NTENANCE (35%	6 of Constru	iction BMPs)	=	\$	14,085.75		\$	14,085.75	
* - Subject to defect warranty financial assurance. A minimum of 20% shall be		•	40.1					_		
retained until final acceptance (MAXIMUM OF 80% COMPLETE ALLOWED)		Sectio	n 1 Subtotal	=	\$	307,294.75		\$	307,294.75	
retained until final acceptance (MAXIMOM OF 80% COMPLETE ALLOWED)				_	1 *	007/271170				
						007,271170				
SECTION 2 - PUBLIC IMPROVEMENTS *				_		007,271.70				
SECTION 2 - PUBLIC IMPROVEMENTS * ROADWAY IMPROVEMENTS	10								50 000 00	
SECTION 2 - PUBLIC IMPROVEMENTS * ROADWAY IMPROVEMENTS Construction Traffic Control	1.0	LS	\$ 50,000.00	=	\$	50,000.00		\$		
SECTION 2 - PUBLIC IMPROVEMENTS * ROADWAY IMPROVEMENTS Construction Traffic Control Aggregate Base Course (135 lbs/cf) 10" Thick	1.0 18,027.0	LS Tons	\$ 50,000.00 \$ 34.00		\$			\$		
SECTION 2 - PUBLIC IMPROVEMENTS * ROADWAY IMPROVEMENTS Construction Traffic Control Aggregate Base Course (135 lbs/cf) 10" Thick Aggregate Base Course (135 lbs/cf)		LS Tons CY	\$ 50,000.00 \$ 34.00 \$ 61.00	=	\$ \$ \$	50,000.00 612,918.00 -		\$ \$ \$	612,918.00 -	
SECTION 2 - PUBLIC IMPROVEMENTS * ROADWAY IMPROVEMENTS Construction Traffic Control Aggregate Base Course (135 lbs/cf) 10" Thick Aggregate Base Course (135 lbs/cf) Asphalt Pavement (3" thick)		LS Tons CY SY	\$ 50,000.00 \$ 34.00 \$ 61.00 \$ 17.00	=	\$ \$	50,000.00 612,918.00 - -		\$ \$ \$	612,918.00 - -	
ROADWAY IMPROVEMENTS * ROADWAY IMPROVEMENTS Construction Traffic Control Aggregate Base Course (135 lbs/cf) 10" Thick Aggregate Base Course (135 lbs/cf) Asphalt Pavement (3" thick) Asphalt Pavement (4" thick)		LS Tons CY SY	\$ 50,000.00 \$ 34.00 \$ 61.00 \$ 17.00 \$ 23.00	=	\$ \$ \$ \$	50,000.00 612,918.00 -		\$ \$ \$ \$	612,918.00 -	
ROADWAY IMPROVEMENTS * ROADWAY IMPROVEMENTS Construction Traffic Control Aggregate Base Course (135 lbs/cf) 10" Thick Aggregate Base Course (135 lbs/cf) Asphalt Pavement (3" thick) Asphalt Pavement (4" thick) Asphalt Pavement (6" thick)	18,027.0	LS Tons CY SY SY SY	\$ 50,000.00 \$ 34.00 \$ 61.00 \$ 17.00 \$ 23.00 \$ 35.00	= =	\$ \$ \$ \$ \$	50,000.00 612,918.00 - - -		\$ \$ \$ \$ \$	612,918.00 - - - -	
SECTION 2 - PUBLIC IMPROVEMENTS * ROADWAY IMPROVEMENTS Construction Traffic Control Aggregate Base Course (135 lbs/cf) 10" Thick Aggregate Base Course (135 lbs/cf) Asphalt Pavement (3" thick) Asphalt Pavement (4" thick) Asphalt Pavement (6" thick) Asphalt Pavement (147 lbs/cf) 7 " thick		LS Tons CY SY SY SY Tons	\$ 50,000.00 \$ 34.00 \$ 61.00 \$ 17.00 \$ 23.00 \$ 35.00 \$ 106.00	= =	\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	50,000.00 612,918.00 - -		\$ \$ \$ \$ \$	612,918.00 - -	
SECTION 2 - PUBLIC IMPROVEMENTS * ROADWAY IMPROVEMENTS Construction Traffic Control Aggregate Base Course (135 lbs/cf) 10" Thick Aggregate Base Course (135 lbs/cf) Asphalt Pavement (3" thick) Asphalt Pavement (4" thick) Asphalt Pavement (6" thick) Asphalt Pavement (147 lbs/cf) 7 thick Raised Median, Paved	18,027.0 12,754.0	LS Tons CY SY SY SY Tons SF	\$ 50,000.00 \$ 34.00 \$ 61.00 \$ 17.00 \$ 23.00 \$ 35.00 \$ 106.00 \$ 10.00	= =	\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	50,000.00 612,918.00 - - - - - 1,351,924.00		\$ \$ \$ \$ \$ \$	612,918.00 - - - - - 1,351,924.00	
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SECTION 2 - PUBLIC IMPROVEMENTS * ROADWAY IMPROVEMENTS Construction Traffic Control Aggregate Base Course (135 lbs/cf) 10" Thick Aggregate Base Course (135 lbs/cf) Asphalt Pavement (3" thick) Asphalt Pavement (4" thick) Asphalt Pavement (6" thick) Asphalt Pavement (6" thick) Raised Median, Paved Regulatory Sign/Advisory Sign Guide/Street Name Sign Epoxy Pavement Marking Thermoplastic Pavement Marking Barricade - Type 3 Delineator - Type I Curb and Gutter, Type A (6" Vertical)	12,754.0 21.0 22.0 9,005.0 116.0	LS Tons CY SY SY Tons SF EA EA SF EA EA	\$ 50,000.00 \$ 34.00 \$ 61.00 \$ 17.00 \$ 23.00 \$ 35.00 \$ 106.00 \$ 16.00 \$ 28.00 \$ 241.00 \$ 29.00 \$ 35.00	= = = = = = = = = = = = = = = = = = = =	\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	50,000.00 612,918.00 - - - - 1,351,924.00 - 7,644.00 - 144,080.00 3,248.00 964.00		\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	612,918.00 - - - 1,351,924.00 - 7,644.00 - 144,080.00 3,248.00 964.00	
SECTION 2 - PUBLIC IMPROVEMENTS * ROADWAY IMPROVEMENTS Construction Traffic Control Aggregate Base Course (135 lbs/cf) 10" Thick Aggregate Base Course (135 lbs/cf) Asphalt Pavement (3" thick) Asphalt Pavement (4" thick) Asphalt Pavement (6" thick) Asphalt Pavement (6" thick) Raised Median, Paved Regulatory Sign/Advisory Sign Guide/Street Name Sign Epoxy Pavement Marking Thermoplastic Pavement Marking Barricade - Type 3 Delineator - Type I Curb and Gutter, Type A (6" Vertical) Curb and Gutter, Type B (Median)	12,754.0 21.0 22.0 9,005.0 116.0	LS Tons CY SY SY SY Tons SF EA EA LF LF	\$ 50,000.00 \$ 34.00 \$ 61.00 \$ 17.00 \$ 23.00 \$ 35.00 \$ 106.00 \$ 16.00 \$ 364.00 \$ 28.00 \$ 241.00 \$ 29.00 \$ 35.00	= = = = = = = = = = = = = = = = = = = =	\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	50,000.00 612,918.00 - - - - 1,351,924.00 - 7,644.00 - 144,080.00 3,248.00 964.00		\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	612,918.00 - - - 1,351,924.00 - 7,644.00 - 144,080.00 3,248.00 964.00	
SECTION 2 - PUBLIC IMPROVEMENTS * ROADWAY IMPROVEMENTS Construction Traffic Control Aggregate Base Course (135 lbs/cf) 10" Thick Aggregate Base Course (135 lbs/cf) Asphalt Pavement (3" thick) Asphalt Pavement (4" thick) Asphalt Pavement (6" thick) Asphalt Pavement (6" thick) Asphalt Pavement (147 lbs/cf) Asphalt Pavement (147 lbs	12,754.0 21.0 22.0 9,005.0 116.0	LS Tons CY SY SY SY Tons SF EA EA LF LF	\$ 50,000.00 \$ 34.00 \$ 61.00 \$ 17.00 \$ 23.00 \$ 35.00 \$ 106.00 \$ 16.00 \$ 28.00 \$ 241.00 \$ 241.00 \$ 29.00 \$ 35.00 \$ 35.00	= = = = = = = = = = = = = = = = = = = =	\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	50,000.00 612,918.00 - - - 1,351,924.00 - 7,644.00 - 144,080.00 3,248.00 964.00		\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	612,918.00 1,351,924.00 - 7,644.00 - 144,080.00 3,248.00 964.00	
SECTION 2 - PUBLIC IMPROVEMENTS * ROADWAY IMPROVEMENTS Construction Traffic Control Aggregate Base Course (135 lbs/cf) 10" Thick Aggregate Base Course (135 lbs/cf) Asphalt Pavement (3" thick) Asphalt Pavement (4" thick) Asphalt Pavement (6" thick) Asphalt Pavement (6" thick) Asphalt Pavement (147 lbs/cf) Asphalt Pavement (147 lbs	12,754.0 21.0 22.0 9,005.0 116.0	LS Tons CY SY SY SY Tons EA EA LF LF LF SY	\$ 50,000.00 \$ 34.00 \$ 61.00 \$ 17.00 \$ 23.00 \$ 35.00 \$ 106.00 \$ 16.00 \$ 28.00 \$ 241.00 \$ 241.00 \$ 29.00 \$ 35.00 \$ 35.00 \$ 35.00 \$ 35.00 \$ 28.00		\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	50,000.00 612,918.00 - - - 1,351,924.00 - 7,644.00 - 144,080.00 3,248.00 964.00		\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	612,918.00 1,351,924.00 - 7,644.00 - 144,080.00 3,248.00 964.00	
SECTION 2 - PUBLIC IMPROVEMENTS * ROADWAY IMPROVEMENTS Construction Traffic Control Aggregate Base Course (135 lbs/cf) 10" Thick Aggregate Base Course (135 lbs/cf) Asphalt Pavement (3" thick) Asphalt Pavement (4" thick) Asphalt Pavement (6" thick) Asphalt Pavement (6" thick) Asphalt Pavement (147 lbs/cf) Asphalt Pavement (147 lbs/cf) Eq. (147 lbs/cf) T " thick Raised Median, Paved Regulatory Sign/Advisory Sign Guide/Street Name Sign Epoxy Pavement Marking Thermoplastic Pavement Marking Barricade - Type 3 Delineator - Type 1 Curb and Gutter, Type A (6" Vertical) Curb and Gutter, Type C (Ramp) 4" Sidewalk (common areas only) 5" Sidewalk	12,754.0 21.0 22.0 9,005.0 116.0	LS Tons CY SY SY SY Tons SF EA EA LF LF LF SY SY	\$ 50,000.00 \$ 34.00 \$ 61.00 \$ 17.00 \$ 23.00 \$ 35.00 \$ 106.00 \$ 10.00 \$ 364.00 \$ 28.00 \$ 241.00 \$ 29.00 \$ 35.00 \$ 35.00		\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	50,000.00 612,918.00 - - - 1,351,924.00 - 7,644.00 - 144,080.00 3,248.00 964.00 - -		\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	612,918.00 1,351,924.00 - 7,644.00 - 144,080.00 3,248.00 964.00	
ROADWAY IMPROVEMENTS ROADWAY IMPROVEMENTS Construction Traffic Control Aggregate Base Course (135 lbs/cf) 10" Thick Aggregate Base Course (135 lbs/cf) Asphalt Pavement (3" thick) Asphalt Pavement (6" thick) Asphalt Pavement (6" thick) Asphalt Pavement (6" thick) Asphalt Pavement (147 lbs/cf) Asphalt Pavement (147 lbs/cf) T" thick Raised Median, Paved Regulatory Sign/Advisory Sign Guide/Street Name Sign Epoxy Pavement Marking Thermoplastic Pavement Marking Barricade - Type 3 Delineator - Type 1 Curb and Gutter, Type A (6" Vertical) Curb and Gutter, Type B (Median) Curb and Gutter, Type B (Median) Curb and Gutter, Type C (Ramp) 4" Sidewalk (common areas only) 5" Sidewalk 6" Sidewalk	12,754.0 21.0 22.0 9,005.0 116.0	LS Tons CY SY SY SY Tons SF EA EA LF LF SY SY SY SF SY SF	\$ 50,000.00 \$ 34.00 \$ 61.00 \$ 17.00 \$ 23.00 \$ 35.00 \$ 106.00 \$ 10.00 \$ 28.00 \$ 241.00 \$ 29.00 \$ 35.00 \$ 35.00		\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	50,000.00 612,918.00 - - - 1,351,924.00 - 7,644.00 - 144,080.00 3,248.00 964.00 - -		\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	612,918.00 1,351,924.00 - 7,644.00 - 144,080.00 3,248.00 964.00	
SECTION 2 - PUBLIC IMPROVEMENTS * ROADWAY IMPROVEMENTS Construction Traffic Control Aggregate Base Course (135 lbs/cf) 10" Thick Aggregate Base Course (135 lbs/cf) Asphalt Pavement (3" thick) Asphalt Pavement (4" thick) Asphalt Pavement (6" thick) Asphalt Pavement (6" thick) Asphalt Pavement (147 lbs/cf) Raised Median, Paved Regulatory Sign/Advisory Sign Guide/Street Name Sign Epoxy Pavement Marking Barricade - Type 3 Delineator - Type I Curb and Gutter, Type A (6" Vertical) Curb and Gutter, Type B (Median) Curb and Gutter, Type C (Ramp) 4" Sidewalk (5" Sidewalk 6" Sidewalk 8" Sidewalk 8" Sidewalk	12,754.0 21.0 22.0 9,005.0 116.0	LS Tons CY SY SY SY Tons SF EA EA LF LF SY SY SY SY SY SY	\$ 50,000.00 \$ 34.00 \$ 61.00 \$ 17.00 \$ 23.00 \$ 35.00 \$ 106.00 \$ 10.00 \$ 28.00 \$ 241.00 \$ 29.00 \$ 35.00 \$ 35.00		\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	50,000.00 612,918.00 1,351,924.00 - 7,644.00 - 144,080.00 3,248.00 964.00		\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	612,918.00 1,351,924.00 - 7,644.00 - 144,080.00 3,248.00 964.00	
SECTION 2 - PUBLIC IMPROVEMENTS * ROADWAY IMPROVEMENTS Construction Traffic Control Aggregate Base Course (135 lbs/cf) 10" Thick Aggregate Base Course (135 lbs/cf) Asphalt Pavement (3" thick) Asphalt Pavement (4" thick) Asphalt Pavement (6" thick) Asphalt Pavement (6" thick) Asphalt Pavement (147 lbs/cf) Raised Median, Paved Regulatory Sign/Advisory Sign Guide/Street Name Sign Epoxy Pavement Marking Thermoplastic Pavement Marking Barricade - Type 3 Delineator - Type I Curb and Gutter, Type A (6" Vertical) Curb and Gutter, Type B (Median) Curb and Gutter, Type C (Ramp) 4" Sidewalk (common areas only) 5" Sidewalk 8" Sidewalk Pedestrian Ramp	12,754.0 21.0 22.0 9,005.0 116.0	LS Tons CY SY SY SY Tons SF EA EA LF LF LF LF SY SY SY SY SY SY SY SY SY	\$ 50,000.00 \$ 34.00 \$ 61.00 \$ 17.00 \$ 23.00 \$ 35.00 \$ 106.00 \$ 16.00 \$ 28.00 \$ 241.00 \$ 241.00 \$ 29.00 \$ 35.00 \$ 35.00 \$ 35.00 \$ 35.00 \$ 16.00		\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	50,000.00 612,918.00 - - - 1,351,924.00 - 7,644.00 3,248.00 964.00 - - - -		\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	612,918.00 1,351,924.00 - 7,644.00 - 144,080.00 3,248.00 964.00	
SECTION 2 - PUBLIC IMPROVEMENTS * ROADWAY IMPROVEMENTS Construction Traffic Control Aggregate Base Course (135 lbs/cf) 10" Thick Aggregate Base Course (135 lbs/cf) Asphalt Pavement (3" thick) Asphalt Pavement (6" thick) Asphalt Pavement (6" thick) Asphalt Pavement (6" thick) Asphalt Pavement (147 lbs/cf) Raised Median, Paved Regulatory Sign/Advisory Sign Guide/Street Name Sign Epoxy Pavement Marking Thermoplastic Pavement Marking Barricade - Type 3 Delineator - Type I Curb and Gutter, Type A (6" Vertical) Curb and Gutter, Type B (Median) Curb and Gutter, Type C (Ramp) 4" Sidewalk (common areas only) 5" Sidewalk 8" Sidewalk Pedestrian Ramp Cross Pan, local (8" thick, 6' wide to include return)	12,754.0 21.0 22.0 9,005.0 116.0	LS Tons CY SY SY SY Tons SF EA EA LF LF SY SY SY SF EA LF LF LF LF SY SY SY SY LF	\$ 50,000.00 \$ 34.00 \$ 61.00 \$ 17.00 \$ 23.00 \$ 35.00 \$ 10.00 \$ 364.00 \$ 28.00 \$ 241.00 \$ 29.00 \$ 35.00 \$ 35.00 \$ 35.00 \$ 35.00 \$ 16.00 \$ 10.00 \$ 24.00 \$ 24.00 \$ 24.00 \$ 35.00 \$ 35.00		\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	50,000.00 612,918.00 - - - 1,351,924.00 - 7,644.00 - 144,080.00 3,248.00 964.00 - - - -		\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	612,918.00 1,351,924.00 - 7,644.00 - 144,080.00 3,248.00 964.00	
SECTION 2 - PUBLIC IMPROVEMENTS * ROADWAY IMPROVEMENTS Construction Traffic Control Aggregate Base Course (135 lbs/cf) 10" Thick Aggregate Base Course (135 lbs/cf) Asphalt Pavement (3" thick) Asphalt Pavement (6" thick) Asphalt Pavement (6" thick) Asphalt Pavement (6" thick) Asphalt Pavement (147 lbs/cf) Asphalt Pavement (147 lbs	12,754.0 21.0 22.0 9,005.0 116.0	LS Tons CY SY SY SY Tons SF EA EA LF LF LF SY SY SY LF	\$ 50,000.00 \$ 34.00 \$ 61.00 \$ 17.00 \$ 23.00 \$ 35.00 \$ 106.00 \$ 16.00 \$ 28.00 \$ 241.00 \$ 241.00 \$ 241.00 \$ 25.00 \$ 35.00 \$ 35.00 \$ 35.00 \$ 116.00 \$ 72.00 \$ 1390.00 \$ 1390.00 \$ 1390.00 \$ 1390.00 \$ 73.00		\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	50,000.00 612,918.00 - - - 1,351,924.00 - 7,644.00 - 144,080.00 3,248.00 964.00 - - - -		\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	612,918.00 1,351,924.00 - 7,644.00 3,248.00 964.00	
SECTION 2 - PUBLIC IMPROVEMENTS * ROADWAY IMPROVEMENTS Construction Traffic Control Aggregate Base Course (135 lbs/cf) 10" Thick Aggregate Base Course (135 lbs/cf) Asphalt Pavement (3" thick) Asphalt Pavement (6" thick) Asphalt Pavement (6" thick) Asphalt Pavement (6" thick) Asphalt Pavement (6" thick) Asphalt Pavement (147 lbs/cf) Asphalt Pavement (147 lbs/c	12,754.0 21.0 22.0 9,005.0 116.0	LS Tons CY SY SY SY Tons EA EA SF EA LF LF LF SY SY SY SY LF	\$ 50,000.00 \$ 34.00 \$ 61.00 \$ 17.00 \$ 23.00 \$ 35.00 \$ 106.00 \$ 10.00 \$ 364.00 \$ 28.00 \$ 241.00 \$ 241.00 \$ 35.00 \$ 35.00 \$ 35.00 \$ 35.00 \$ 35.00 \$ 111.00 \$ 111.00 \$ 173.00 \$ 111.00 \$ 1,790.00		\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	50,000.00 612,918.00 - - - 1,351,924.00 - 7,644.00 - 144,080.00 3,248.00 964.00 - - - -		\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	612,918.00 1,351,924.00 - 7,644.00 - 144,080.00 3,248.00 964.00	
SECTION 2 - PUBLIC IMPROVEMENTS * ROADWAY IMPROVEMENTS Construction Traffic Control Aggregate Base Course (135 lbs/cf) 10" Thick Aggregate Base Course (135 lbs/cf) Asphalt Pavement (3" thick) Asphalt Pavement (6" thick) Asphalt Pavement (6" thick) Asphalt Pavement (6" thick) Asphalt Pavement (6" thick) Asphalt Pavement (147 lbs/cf) Asphalt Pavement (147 lbs/c	12,754.0 21.0 22.0 9,005.0 116.0	LS Tons CY SY SY SY Tons SF EA EA LF LF LF SY SY SY SY LF LF EA LF	\$ 50,000.00 \$ 34.00 \$ 61.00 \$ 17.00 \$ 23.00 \$ 35.00 \$ 106.00 \$ 10.00 \$ 28.00 \$ 241.00 \$ 241.00 \$ 29.00 \$ 35.00 \$ 35.00 \$ 35.00 \$ 35.00 \$ 35.00 \$ 35.00 \$ 116.00 \$ 1,390.00 \$ 11390.00 \$ 11,790.00 \$ 1,790.00 \$ 1,790.00 \$ 60.00		\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	50,000.00 612,918.00 - - - 1,351,924.00 - 7,644.00 - 144,080.00 3,248.00 964.00 - - - -		\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	612,918.00 1,351,924.00 - 7,644.00 3,248.00 964.00	
SECTION 2 - PUBLIC IMPROVEMENTS * ROADWAY IMPROVEMENTS Construction Traffic Control Aggregate Base Course (135 lbs/cf) 10" Thick Aggregate Base Course (135 lbs/cf) Asphalt Pavement (3" thick) Asphalt Pavement (6" thick) Asphalt Pavement (6" thick) Asphalt Pavement (6" thick) Asphalt Pavement (147 lbs/cf) Asphalt Pavement (147 lbs	12,754.0 21.0 22.0 9,005.0 116.0	LS Tons CY SY SY SY Tons EA EA SF EA LF LF LF SY SY SY SY LF	\$ 50,000.00 \$ 34.00 \$ 61.00 \$ 17.00 \$ 23.00 \$ 35.00 \$ 106.00 \$ 10.00 \$ 364.00 \$ 28.00 \$ 241.00 \$ 241.00 \$ 35.00 \$ 35.00 \$ 35.00 \$ 35.00 \$ 35.00 \$ 111.00 \$ 111.00 \$ 173.00 \$ 111.00 \$ 1,790.00		\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	50,000.00 612,918.00 1,351,924.00 - 7,644.00 - 144,080.00 3,248.00 964.00		\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	612,918.00 1,351,924.00 - 7,644.00 3,248.00 964.00	
SECTION 2 - PUBLIC IMPROVEMENTS * ROADWAY IMPROVEMENTS Construction Traffic Control Aggregate Base Course (135 lbs/cf) 10" Thick Aggregate Base Course (135 lbs/cf) Asphalt Pavement (3" thick) Asphalt Pavement (6" thick) Asphalt Pavement (6" thick) Asphalt Pavement (6" thick) Asphalt Pavement (6" thick) Asphalt Pavement (147 lbs/cf) Asphalt Pavement (147 lbs/c	12,754.0 21.0 22.0 9,005.0 116.0	LS Tons CY SY SY SY Tons SF EA EA LF LF LF SY SY SY SY LF LF EA LF	\$ 50,000.00 \$ 34.00 \$ 61.00 \$ 17.00 \$ 23.00 \$ 35.00 \$ 106.00 \$ 10.00 \$ 28.00 \$ 241.00 \$ 241.00 \$ 29.00 \$ 35.00 \$ 35.00 \$ 35.00 \$ 35.00 \$ 35.00 \$ 35.00 \$ 116.00 \$ 1,390.00 \$ 11390.00 \$ 11,790.00 \$ 1,790.00 \$ 1,790.00 \$ 60.00		\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	50,000.00 612,918.00 1,351,924.00 - 7,644.00 - 144,080.00 3,248.00 964.00		\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	612,918.00 1,351,924.00 - 7,644.00 - 144,080.00 3,248.00 964.00	
SECTION 2 - PUBLIC IMPROVEMENTS * ROADWAY IMPROVEMENTS Construction Traffic Control Aggregate Base Course (135 lbs/cf) 10" Thick Aggregate Base Course (135 lbs/cf) Asphalt Pavement (3" thick) Asphalt Pavement (4" thick) Asphalt Pavement (6" thick) Asphalt Pavement (6" thick) Asphalt Pavement (147 lbs/cf) Raised Median, Paved Regulatory Sign/Advisory Sign Guide/Street Name Sign Epoxy Pavement Marking Thermoplastic Pavement Marking Barricade - Type 3 Delineator - Type I Curb and Gutter, Type A (6" Vertical) Curb and Gutter, Type B (Median) Curb and Gutter, Type C (Ramp) 4" Sidewalk (common areas only) 5" Sidewalk 6" Sidewalk 8" Sidewalk Pedestrian Ramp Cross Pan, local (8" thick, 6' wide to include return) Curb Opening with Drainage Chase Guardrail Type 3 (W-Beam) Guardrail Type 7 (Concrete)	12,754.0 21.0 22.0 9,005.0 116.0	LS Tons CY SY SY SY Tons SF EA EA LF LF SY SY SY LF	\$ 50,000.00 \$ 34.00 \$ 61.00 \$ 17.00 \$ 23.00 \$ 35.00 \$ 106.00 \$ 10.00 \$ 28.00 \$ 241.00 \$ 29.00 \$ 35.00 \$ 35.00 \$ 35.00 \$ 35.00 \$ 35.00 \$ 116.00 \$ 116.00 \$ 1,390.00 \$ 111.00 \$ 17.790.00 \$ 17.790.00 \$ 87.00 \$ 17.790.00 \$ 87.00		\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	50,000.00 612,918.00 1,351,924.00 - 7,644.00 - 144,080.00 3,248.00 964.00		\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	612,918.00 1,351,924.00 - 7,644.00 - 144,080.00 3,248.00 964.00	
SECTION 2 - PUBLIC IMPROVEMENTS * ROADWAY IMPROVEMENTS Construction Traffic Control Aggregate Base Course (135 lbs/cf) 10" Thick Aggregate Base Course (135 lbs/cf) Asphalt Pavement (3" thick) Asphalt Pavement (4" thick) Asphalt Pavement (6" thick) Asphalt Pavement (6" thick) Asphalt Pavement (147 lbs/cf) Raised Median, Paved Regulatory Sign/Advisory Sign Guide/Street Name Sign Epoxy Pavement Marking Thermoplastic Pavement Marking Barricade - Type 3 Delineator - Type I Curb and Gutter, Type A (6" Vertical) Curb and Gutter, Type B (Median) Curb and Gutter, Type C (Ramp) 4" Sidewalk (common areas only) 5" Sidewalk 8" Sidewalk Pedestrian Ramp Cross Pan, local (8" thick, 6' wide to include return) Curb Opening with Drainage Chase Guardrail Type 7 (Concrete) Guardrail End Anchorage	12,754.0 21.0 22.0 9,005.0 116.0	LS Tons CY SY SY SY Tons SF EA EA LF	\$ 50,000.00 \$ 34.00 \$ 61.00 \$ 17.00 \$ 23.00 \$ 35.00 \$ 106.00 \$ 16.00 \$ 28.00 \$ 241.00 \$ 241.00 \$ 29.00 \$ 35.00 \$ 35.00 \$ 35.00 \$ 16.00 \$ 1.390.00 \$ 1.390.00 \$ 1.390.00 \$ 1.790.00 \$ 1.790.00 \$ 87.00 \$ 87.00 \$ 2.538.00		\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	50,000.00 612,918.00 1,351,924.00 - 7,644.00 - 144,080.00 3,248.00 964.00		\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	612,918.00 1,351,924.00 - 7,644.00 - 144,080.00 3,248.00 964.00	
SECTION 2 - PUBLIC IMPROVEMENTS * ROADWAY IMPROVEMENTS Construction Traffic Control Aggregate Base Course (135 lbs/cf) 10" Thick Aggregate Base Course (135 lbs/cf) Asphalt Pavement (3" thick) Asphalt Pavement (6" thick) Asphalt Pavement (6" thick) Asphalt Pavement (6" thick) Asphalt Pavement (147 lbs/cf) Raised Median, Paved Regulatory Sign/Advisory Sign Guide/Street Name Sign Epoxy Pavement Marking Thermoplastic Pavement Marking Barricade - Type 3 Delineator - Type I Curb and Gutter, Type A (6" Vertical) Curb and Gutter, Type B (Median) Curb and Gutter, Type C (Ramp) 4" Sidewalk 6" Sidewalk 8" Sidewalk Pedestrian Ramp Cross Pan, local (8" thick, 6' wide to include return) Cross Pan, collector (9" thick, 8' wide to include return) Curb Opening with Drainage Chase Guardrail Type 3 (V-Beam) Guardrail Type 7 (Concrete) Guardrail Impact Attenuator	12,754.0 21.0 22.0 9,005.0 116.0	LS Tons CY SY SY SY Tons SF EA EA LF	\$ 50,000.00 \$ 34.00 \$ 61.00 \$ 17.00 \$ 23.00 \$ 35.00 \$ 10.00 \$ 364.00 \$ 16.00 \$ 28.00 \$ 241.00 \$ 29.00 \$ 35.00 \$ 35.00 \$ 35.00 \$ 16.00 \$ 10.00 \$ 29.00 \$ 35.00 \$ 35.00		\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	50,000.00 612,918.00 - - - 1,351,924.00 - 7,644.00 3,248.00 964.00 - - - - - - - -		\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	612,918.00 1,351,924.00 - 7,644.00 - 144,080.00 3,248.00 964.00	
SECTION 2 - PUBLIC IMPROVEMENTS * ROADWAY IMPROVEMENTS Construction Traffic Control Aggregate Base Course (135 lbs/cf) 10" Thick Aggregate Base Course (135 lbs/cf) Asphalt Pavement (3" thick) Asphalt Pavement (6" thick) Asphalt Pavement (6" thick) Asphalt Pavement (6" thick) Asphalt Pavement (6" thick) Asphalt Pavement (147 lbs/cf) Asphalt Pavement (147 lbs/c	12,754.0 21.0 22.0 9,005.0 116.0	LS Tons CY SY SY SY Tons SF EA EA LF LF LF SY SY SY LF LF EA LF	\$ 50,000.00 \$ 34.00 \$ 61.00 \$ 17.00 \$ 23.00 \$ 35.00 \$ 106.00 \$ 10.00 \$ 364.00 \$ 28.00 \$ 241.00 \$ 241.00 \$ 29.00 \$ 35.00 \$ 35.00 \$ 35.00 \$ 135.00 \$ 116.00 \$ 1,390.00 \$ 72.00 \$ 111.00 \$ 1,790.00 \$ 60.00 \$ 25,38.00 \$ 25,38.00 \$ 95.00		\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	50,000.00 612,918.00 1,351,924.00 - 7,644.00 - 144,080.00 3,248.00 964.00		\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	- 1,351,924.00 - 7,644.00 - 144,080.00 3,248.00 	

PROJECT INFORMATION								
Saddlehorn Filing 4	2/9/2023	EGP-22-004						
Project Name	Date	PCD File No.						

				Unit				(with Pre-Pl	at Construction)
Description		Quantity	Units	Cost		Total		% Complete	Remaining
					=	\$	-	\$	-
[insert items not listed but part of construct	ion plans]				=	\$	-	\$	
STORM DRAIN IMPROVEMENTS									
Concrete Box Culvert (M Standard), Size (WxH)		LF		=	\$	-	\$	-
18" Reinforced Concrete Pipe		49	LF	\$ 76.00	=	\$ 3,7	724.00	\$	3,724.00
24" Reinforced Concrete Pipe		92	LF	\$ 91.00	=	\$ 8,3	372.00	\$	8,372.00
30" Reinforced Concrete Pipe		123	LF	\$ 114.00	=	\$ 14,0	022.00	\$	14,022.00
36" Reinforced Concrete Pipe			LF	\$ 140.00	=	\$	-	\$	-
42" Reinforced Concrete Pipe			LF	\$ 187.00	=	\$	-	\$	-
48" Reinforced Concrete Pipe			LF	\$ 228.00	=	\$	-	\$	-
54" Reinforced Concrete Pipe			LF	\$ 297.00	=	\$	-	\$	
60" Reinforced Concrete Pipe			LF	\$ 348.00	=	\$	-	\$	-
66" Reinforced Concrete Pipe			LF	\$ 402.00	=	\$	-	\$	-
72" Reinforced Concrete Pipe			LF	\$ 460.00	=	\$	-	\$	
18" Corrugated Steel Pipe		185	LF	\$ 98.00	=		130.00	\$	18,130.00
24" Corrugated Steel Pipe		66	LF	\$ 112.00	=		392.00	\$	7,392.00
30" Corrugated Steel Pipe		53	LF	\$ 143.00	=		579.00	\$	7,579.00
36" Corrugated Steel Pipe			LF	\$ 171.00	=	\$	-	\$	-
42" Corrugated Steel Pipe			LF	\$ 197.00	=	\$		\$	
48" Corrugated Steel Pipe			LF	\$ 207.00	=	\$		\$	
54" Corrugated Steel Pipe			LF	\$ 304.00	=	\$		\$	
60" Corrugated Steel Pipe			LF	\$ 328.00	=	\$		\$	
66" Corrugated Steel Pipe			LF	\$ 397.00		\$	-	\$	
72" Corrugated Steel Pipe			LF	\$ 467.00		\$		\$	
78" Corrugated Steel Pipe			LF	\$ 537.00		\$		\$	
84" Corrugated Steel Pipe			LF	\$ 642.00	_	\$	-	\$	
Flared End Section (FES) RCP Size =	18" RCP				_				
(unit cost = 6x pipe unit cost)	10 KGF	2	EA	\$ 402.00	=	\$ 8	304.00	\$	804.00
Flared End Section (FES) CSP Size =		4		\$ 486.00	=	\$ 1,9	944.00	\$	1,944.00
(unit cost = 6x pipe unit cost)	24" RCP	4	EA	\$ 400.00	_	J 1,7	744.00	J.	1,744.00
Flared End Section (FES) CSP Size = (unit cost = 6x pipe unit cost)	30" RCP	4	EA	\$ 600.00	=	\$ 2,4	100.00	\$	2,400.00
End Treatment- Headwall	00 1101		EA		=	\$		\$	
End Treatment- Wingwall			EA		_	\$		\$	
End Treatment - Cutoff Wall			EA		=	\$	-	\$	<u>-</u>
Curb Inlet (Type R) L=5', Depth <	E'		EA	\$ 6,703.00	=	\$	-	\$	
Curb Inlet (Type R) L=5', 5' ≤ Depth <			EA	\$ 8,715.00		\$	-	\$	
Curb Inlet (Type R) L = 5', 10' ≤ Depth <			EA	\$ 10,092.00		\$	-	\$	
Curb Inlet (Type R) L = 10', Depth <			EA	\$ 9,224.00		\$	-	\$	
			EA	\$ 9,507.00		\$	-	\$	
Curb Inlet (Type R) L =10', 5' ≤ Depth <			EA	\$ 9,307.00	=				-
Curb Inlet (Type R) L =10', 10' ≤ Depth <			EA	\$ 11,901.00	=	\$	-	\$	-
Curb Inlet (Type R) L =15', Depth <			EA	\$ 11,993.00	=	\$	-	\$	-
Curb Inlet (Type R) L =15', 5' ≤ Depth <				\$ 12,050.00	=	\$	-	\$	-
Curb Inlet (Type R) L =15', 10' ≤ Depth <			EA		=	\$	-	\$	-
Curb Inlet (Type R) L =20', Depth <			EA	\$ 12,783.00	=	\$	-	\$	-
Curb Inlet (Type R) L =20', 5' ≤ Depth <			EA	\$ 14,109.00	=	\$	-	\$	-
Grated Inlet (Type C), Depth <			EA	\$ 5,611.00	=	\$	-	\$	-
Grated Inlet (Type D), Depth <	5'		EA	\$ 6,931.00	=	\$	-	\$	-
Storm Sewer Manhole, Box Base			EA	\$ 14,061.00	=	\$	-	\$	•
Storm Sewer Manhole, Slab Base			EA	\$ 7,734.00	=	\$	-	\$	-
Geotextile (Erosion Control)			SY	\$ 8.00	=	\$	-	\$	-
Rip Rap, d50 size from 6" to 24"		1,402.0	Tons	\$ 97.00	=		994.00	\$	135,994.00
Rip Rap, Grouted			Tons	\$ 115.00	=	\$	-	\$	-
Drainage Channel Construction, Size (W	x H)		LF	\$ -	=	\$	-	\$	-
Drainage Channel Lining, Concrete			CY	\$ 689.00	=	\$	-	\$	-
Drainage Channel Lining, Rip Rap			CY	\$ 135.00	=	\$	-	\$	-
Drainage Channel Lining, Grass			AC	\$ 1,776.00	=	\$	-	\$	-
Drainage Channel Lining, Other Stabilization	on				=	\$	-	\$	-
					=	\$	-	\$	-
[insert items not listed but part of construct					=	\$	-	\$	-
 Subject to defect warranty financial assurance. A m retained until final acceptance (MAXIMUM OF 80% CO 			04'-	m 0 Cull-4-4-1		ф 0074.40	0.00	_	0.071.100.00
	IVIFLETE ALLOWED)		Sectio	n 2 Subtotal	=	\$ 2,371,139	Y ()()	\$	2,371,139.00

PROJECT INFORMATION							
Saddlehorn Filing 4	2/9/2023	EGP-22-004					
Project Name	Date	PCD File No.					

				Unit				(with Pre-	-Plat	Construction)
Description	Quantity	Units		Cost			Total	% Complete		Remaining
SECTION 3 - COMMON DEVELOPMENT IMPRO	VEMENTS (Priv	ate or Dis	tric	t and NC	T Mainta	ined	ov EPC)**			
ROADWAY IMPROVEMENTS							- , ,			
					=	\$	-		\$	-
					=	\$	-		\$	-
					=	\$	-		\$	-
					=	\$	-		\$	-
					=	\$	-		\$	-
					=	\$	-		\$	-
STORM DRAIN IMPROVEMENTS (Excep	tion: Permanent Pon	d/BMP shall	be it	emized und	er Section 1)				
					=	\$	-		\$	-
					=	\$	-		\$	-
					=	\$	-		\$	-
					=	\$	-		\$	-
					=	\$	-		\$	-
					=	\$	-		\$	-
WATER SYSTEM IMPROVEMENTS										
Water Main Pipe (PVC), Size 8"	8,825	LF	\$	78.00	=	\$	688,350.00		\$	688,350.00
Water Main Pipe (Ductile Iron), Size 8"		LF	\$	91.00	=	\$	-		\$	-
Gate Valves, 8"	12	EA	\$	2,247.00	=	\$	26,964.00		\$	26,964.00
Fire Hydrant Assembly, w/ all valves	18	EA	\$	7,978.00	=	\$	143,604.00		\$	143,604.00
Water Service Line Installation, inc. tap and valves	42	EA	\$	1,601.00	=	\$	67,242.00		\$	67,242.00
Fire Cistern Installation, complete		EA			=	\$	-		\$	-
					=	\$	-		\$	-
[insert items not listed but part of construction plans]					=	\$	-		\$	-
SANITARY SEWER IMPROVEMENTS										
Sewer Main Pipe (PVC), Size 8"		LF	\$	78.00	=	\$	-		\$	-
Sanitary Sewer Manhole, Depth < 15 feet		EA	\$	5,305.00	=	\$	-		\$	-
Sanitary Service Line Installation, complete		EA	\$	1,696.00	=	\$	-		\$	-
Sanitary Sewer Lift Station, complete		EA			=	\$	-		\$	-
					=	\$	-		\$	-
[insert items not listed but part of construction plans]					=	\$	-		\$	-
LANDSCAPING IMPROVEMENTS	(For subdivision spe		n of a	approval, or	PUD)					
		EA			=	\$	-		\$	-
		EA			=	\$	-		\$	-
		EA			=	\$	-		\$	-
		EA			=	\$	-		\$	-
		EA			=	\$	-		\$	-
** - Section 3 is not subject to defect warranty requirements		Sectio	n 3	Subtotal	=	\$	926,160.00		\$	926,160.00

	PI	ROJECTI	NEORIVIA I I C	אוע					
Saddlehorn Filing 4			2/9/2023				E	GP-2	22-004
Project Name			Date				PCD File No.		
			Unit				(with Pre	-Plat	Construction)
Description	Quantity	Units	Cost		1	Total	% Complete		Remaining
10 PUN T PL 100 (P 1 II)					•			•	
AS-BUILT PLANS (Public Improvements inc. Permanent WQC		LS		=	\$	-	_	\$	-
POND/BMP CERTIFICATION (inc. elevations and volume calc	ulations)	LS		=	\$	-	_	\$	-
				Total	Constructi	on Financia	I Assurance	\$	3,604,593.75
			(Sum of all se				MP certification)		
			(,		
	Total Remaini	ing Constr	uction Finan	icial Assu	rance (with	n Pre-Plat C	onstruction)	\$	3,604,593.75
							MP certification)		
				Total De	fect Warraı	nty Financia	I Assurance	\$	524,602.80
	(20	0% of all items	s identified as (*). To be coll	ateralized at ti	me of prelimina	ary acceptance)		
Approvals									
••									
I hereby certify that this is an accurate and complete estimate o	costs for the wor	k as shown o	n the Grading a	ind Erosion (Control Plan a	nd Constructio	n Drawings asso	ciated	d with the Project.
Engineer (P.E. Seal Required)		-							
z.ig.i.co. (i.e. ocui required)									

Date

Date

Approved by Owner / Applicant

Approved by El Paso County Engineer / ECM Administrator

APPENDIX B HYDROLOGIC CALCULATIONS

COMPOSITE % IMPERVIOUS CALCULATIONS

Subdivision: Saddlehorn Ranch Filing 4 Location: El Paso County

Project Name: Saddlehorn Ranch
Project No.: 25142.06
Calculated By: AAM
Checked By: Date: 3/1/22

			Paved Roads	S	2.5	Acre Rural l	.ots		Lawns		Basins Tota
Basin ID	Total Area (ac)	% Imp.	Area (ac)	Weighted % Imp.	% Imp.	Area (ac)	Weighted % Imp.	% Imp.	Area (ac)	Weighted % Imp.	Weighted % Imp.
C1	2.14	45%	1.00	21.0%	6.2%	1,14	3.3%	2%	0.00	0.0%	24.3%
C2	22.55	45%	2.21	4.4%	6.2%	20.34	5.6%	2%	0.00	0.0%	10.0%
C3	1.26	45%	0.61	21.8%	6.2%	0.65	3.2%	2%	0.00	0.0%	25.0%
C4	1.36	45%	1.36	45.0%	6.2%	0.00	0.0%	2%	0.00	0.0%	45.0%
C5	3.95	45%	1.59	18.1%	6.2%	2.36	3.7%	2%	0.00	0.0%	21.8%
C6	4.19	45%	0.93	10.0%	6.2%	3.26	4.8%	2%	0.00	0.0%	14.8%
C7	1.11	45%	1.11	45.0%	6.2%	0.00	0.0%	2%	0.00	0.0%	45.0%
C8	10.13	45%	0.00	0.0%	6.2%	8.07	4.9%	2%	2.06	0.4%	5.3%
D1	3.97	45%	1.22	13.8%	6.2%	2.75	4.3%	2%	0.00	0.0%	18.1%
D2	5.58	45%	1.55	12.5%	6.2%	4.03	4.5%	2%	0.00	0.0%	17.0%
D3	0.34	45%	0.34	45.0%	6.2%	0.00	0.0%	2%	0.00	0.0%	45.0%
D4	10.01	45%	0.35	1.6%	6.2%	8.21	5.1%	2%	1.45	0.3%	6.9%
D5	7.94	45%	0.00	0.0%	6.2%	5.15	4.0%	2%	2.79	0.7%	4.7%
D6	17.08	45%	2.29	6.0%	6.2%	14.79	5.4%	2%	0.00	0.0%	11.4%
D7	0.86	45%	0.86	45.0%	6.2%	0.00	0.0%	2%	0.00	0.0%	45.0%
D8	6.00	45%	1.96	14.7%	6.2%	4.04	4.2%	2%	0.00	0.0%	18.9%
D9	2.00	45%	1.94	43.7%	6.2%	0.06	0.2%	2%	0.00	0.0%	43.8%
UD1	20.70	45%	0.00	0.0%	6.2%	20.70	6.2%	2%	0.00	0.0%	6.2%
UD2	24.68	45%	0.00	0.0%	6.2%	0.00	0.0%	2%	24.68	2.0%	2.0%
UD3	7.68	45%	0.00	0.0%	6.2%	7.68	6.2%	2%	0.00	0.0%	6.2%
UD4	12.80	45%	0.00	0.0%	6.2%	12.80	6.2%	2%	0.00	0.0%	6.2%
OS1	2.26	100%	1.27	56.2%	6.2%	0.00	0.0%	2%	0.99	0.9%	57.1%
OS2	0.72	100%	0.24	33.3%	6.2%	0.00	0.0%	2%	0.48	1.3%	34.7%
TOTAL	169.31										10.7%

Land Use or Surface	Percent						Runoff Co	pefficients					
Characteristics	Impervious	2-1	year	5-1	ear	10-1	year	25-	year	50-	year	100	year
		HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG CBD
Business													
Commercial Areas	95	0.79	0.80	0.81	0.82	0.83	0.84	0.85	0.87	0.87	0.88	0.88	0.89
Neighborhood Areas	70	0.45	0.49	0.49	0.53	0.53	0.57	0.58	0.62	0.60	0.65	0.62	0.68
Residential					2								Ç.,
1/8 Acre or less	65	0.41	0.45	0.45	0.49	0.49	0.54	0.54	0.59	0.57	0.62	0.59	0.65
1/4 Acre	40	0.23	0.28	0.30	0.35	0.36	0.42	0.42	0.50	0.46	0.54	0.50	0.58
1/3 Acre	30	0.18	0.22	0.25	0.30	0.32	0.38	0.39	0.47	0.43	0.52	0.47	0.57
1/2 Acre	25	0.15	0.20	0.22	0.28	0.30	0.36	0.37	0.46	0.41	0.51	0.46	0.56
1 Acre	20	0.12	0.17	0.20	0.26	0.27	0.34	0.35	0.44	0.40	0.50	0.44	0.55
Industrial			—			k							·
Light Areas	80	0.57	0.60	0.59	0.63	0.63	0.66	0.66	0.70	0.68	0.72	0.70	0.74
Heavy Areas	90	0.71	0.73	0.73	0.75	0.75	0.77	0.78	0.80	0.80	0.82	0.81	0.83
Parks and Cemeteries	7	0.05	0.09	0.12	0.19	0.20	0.29	0.30	0.40	0.34	0.46	0.39	0.52
Playerounds	13	0.07	0.13	0.16	0.23	0.24	0.31	0.32	0.42	0.37	0.48	0.41	0.54
Railroad Yard Areas	40	0.23	0.28	0.30	0.35	0.36	0.42	0.42	0.50	0.46	0.54	0.50	0.58
Undeveloped Areas	-		 										
Historic Flow Analysis Greenbelts, Agriculture	2	0.08	0.05	0.09	0.16	0.17	0.26	0.26	0.38	0.31	0.45	0.36	0.51
Pasture/Meadow	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50
Forest	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50
Exposed Rock	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Offsite Flow Analysis (when landuse is undefined)	45	0.26	0.31	0.32	0.37	0.38	0.44	0.44	0.51	0.48	0.55	0.51	0.59
Streets			-										
Paved	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Gravel	80	0.57	0.60	0.59	0.63	0.63	0.66	0.66	0.70	0.68	0.72	0.70	0.74
Drive and Walks	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Roofs	90	0.71	0.73	0.73	0.75	0.75	0.77	0.78	0.80	0.80	0.82	0.81	0.83
Lawns	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50

2.5 A	Acre Rural Lots - Comp.	% Impervious Calculation	on
Total Area (ac)	Area (ac) - Roofs (90%)	Area (ac)- Drives (100%)	Area (ac) - Lawns (2%)
2.50	0.068	0.046	2.39
Comp % Imperviousness		6.20%	

Roads w/ Roadside [Ditches - Comp. % Impe	rvious Calculation											
Area* (ac)	Area* (ac) Area - Ditch (5%) Area - Roads (100%)												
0.2124													
Comp % Imperviousness	Comp % Imperviousness 0.41												

*Area based on 250 LF roadway from CL to outside edge of roadside ditch The above conservatively rounded to 45%.

COMPOSITE RUNOFF COEFFICIENT CALCULATIONS

bdivision: Saddlehorn Ranch Filing 4 Location: El Paso County

Project Name: Saddlehorn Ranch
Project No.: 25142.06

Calculated By: AAM Checked By: TBD

Date: 3/1/22

		Basins Total	Hydro	ologic Soil (Group	Hydro	ologic Soil (Group	Mir	nor Coeffici	ents	Maj	jor Coeffici	ents		Basins Total
Basin ID	Total Area (ac)	Weighted % Imp.	Area A (ac)	Area B (ac)	Area C/D (ac)	% A (ac)	% B (ac)	% C/D (ac)	C _{5,A}	C _{5,B}	C _{5,C/D}	C _{100,A}	C _{100,B}	C _{100,C/D}	Basins Total Weighted C ₅	Weighted C ₁₀₀
C1	2.14	24.3%	1.55	0.00	0.59	72%	0%	28%	0.14	0.19	0.23	0.30	0.54	0.58	0.17	0.38
C2	22.55	10.0%	22.55	0.00	0.00	100%	0%	0%	0.05	0.07	0.12	0.19	0.47	0.52	0.05	0.19
C3	1.26	25.0%	1.26	0.00	0.00	100%	0%	0%	0.15	0.19	0.24	0.31	0.54	0.59	0.15	0.31
C4	1.36	45.0%	1.36	0.00	0.00	100%	0%	0%	0.31	0.36	0.40	0.46	0.64	0.67	0.31	0.46
C5	3.95	21.8%	3.95	0.00	0.00	100%	0%	0%	0.12	0.16	0.21	0.28	0.53	0.57	0.12	0.28
C6	4.19	14.8%	4.19	0.00	0.00	100%	0%	0%	0.08	0.11	0.16	0.23	0.50	0.55	0.08	0.23
C7	1.11	45.0%	1.11	0.00	0.00	100%	0%	0%	0.31	0.36	0.40	0.46	0.64	0.67	0.31	0.46
C8	10.13	5.3%	10.13	0.00	0.00	100%	0%	0%	0.02	0.04	0.08	0.15	0.45	0.51	0.02	0.15
D1	3.97	18.1%	0.11	0.00	3.86	3%	0%	97%	0.10	0.13	0.18	0.25	0.51	0.56	0.18	0.55
D2	5.58	17.0%	3.65	0.00	1.93	65%	0%	35%	0.09	0.13	0.17	0.24	0.51	0.55	0.12	0.35
D3	0.34	45.0%	0.17	0.00	0.17	50%	0%	50%	0.31	0.36	0.40	0.46	0.64	0.67	0.36	0.57
D4	10.01	6.9%	3.16	0.00	6.85	32%	0%	68%	0.03	0.05	0.09	0.16	0.46	0.51	0.07	0.40
D5	7.94	4.7%	2.43	0.00	5.51	31%	0%	69%	0.02	0.03	0.07	0.15	0.45	0.50	0.06	0.39
D6	17.08	11.4%	13.71	0.00	3.37	80%	0%	20%	0.05	0.08	0.13	0.20	0.48	0.53	0.07	0.26
D7	0.86	45.0%	0.82	0.00	0.04	95%	0%	5%	0.31	0.36	0.40	0.46	0.64	0.67	0.31	0.47
D8	6.00	18.9%	6.00	0.00	0.00	100%	0%	0%	0.10	0.14	0.19	0.26	0.51	0.56	0.10	0.26
D9	2.00	43.8%	1.97	0.00	0.03	98%	0%	2%	0.30	0.35	0.39	0.45	0.63	0.66	0.30	0.46

UD1	20.70	6.2%	16.26	0.00	4.44	79%	0%	21%	0.03	0.04	0.09	0.16	0.46	0.51	0.04	0.23
UD2	24.68	2.0%	1.06	0.00	23.62	4%	0%	96%	0.01	0.01	0.05	0.13	0.44	0.49	0.05	0.48
UD3	7.68	6.2%	5.85	0.00	1.83	76%	0%	24%	0.03	0.04	0.09	0.16	0.46	0.51	0.04	0.24
UD4	12.80	6.2%	12.80	0.00	0.00	100%	0%	0%	0.03	0.04	0.09	0.16	0.46	0.51	0.03	0.16
OS1	2.26	57.1%	0.47	0.00	1.79	21%	0%	79%	0.42	0.47	0.50	0.56	0.69	0.72	0.49	0.68
OS2	0.72	34.7%	0.72	0.00	0.00	100%	0%	0%	0.22	0.27	0.32	0.38	0.59	0.63	0.22	0.38
TOTAL	169.31	10.7%	115.28	0.00	54.04	68%	0%	32%							0.07	0.30

Table 6-4. Runoff coefficient equations based on NRCS soil group and storm return period

NRCS				Storm Re	turn Period		
Soil Group	2-Year	5-Year	10-Year	25-Year	50-Year	100-Year	500-Year
A	C _A =	C _A =	C _A =	C _A =	C _A =	C _A =	C _A =
	0.84i ^{1.302}	0.86i ^{1.276}	0.87i ^{1.232}	0.84i ^{1.124}	0.85i+0.025	0.78i+0.110	0.65i+0.254
В	C _B = 0.84i ^{1.169}	$C_B = 0.86i^{1.088}$	C _B = 0.81 <i>i</i> +0.057	C _B = 0.63 <i>i</i> +0.249	C _B = 0.56 <i>t</i> +0.328	C _B = 0.47 <i>i</i> +0.426	C _B = 0.37 <i>i</i> +0.536
C/D	C _{C/D} =	C _{C/D} =	C _{CD} =	C _{C/D} =	C _{C/D} =	C _{C/D} =	C _{C/D} =
	0.83 <i>i</i> ^{1.122}	0.82i+0.035	0.74i+0.132	0.56i+0.319	0.49i+0.393	0.41 <i>i</i> +0.484	0.32i+0.588

Where:

i = % imperviousness (expressed as a decimal)

 C_A = Runoff coefficient for Natural Resources Conservation Service (NRCS) HSG A soils

 C_B = Runoff coefficient for NRCS HSG B soils

 $C_{C/D}$ = Runoff coefficient for NRCS HSG C and D soils.

STANDARD FORM SF-2 TIME OF CONCENTRATION

Subdivision: Saddlehorn Ranch Filing 4
Location: El Paso County

Project Name: Saddlehorn Ranch

Project No.: 25142.06

Calculated By: AAM

Checked By: TBD

Date: 3/1/22

		SUB-I	BASIN			INITI	AL/OVERI	LAND		T	RAVEL TIM	E			tc CHECK		
		DA	ATA				(T_i)				(T_t)			(U	IRBANIZED BA	SINS)	FINAL
BASIN	D.A.	Hydrologic	Impervious	C_5	C ₁₀₀	L	S_o	t_i	L_t	S_t	K	VEL.	t_t	COMP. t_c	TOTAL	Urbanized t_c	t_c
ID	(ac)	Soils Group	(%)			(ft)	(%)	(min)	(ft)	(%)		(ft/s)	(min)	(min)	LENGTH (ft)	(min)	(min)
C1	2.14	А	24%	0.17	0.38	52	7.5%	6.2	689	1.0%	15.0	1.5	7.7	13.9	741.0	31.1	13.9
C2	22.55	А	10%	0.05	0.19	300	1.9%	26.7	630	1.0%	15.0	1.5	7.0	33.7	930.0	34.4	33.7
C3	1.26	А	25%	0.15	0.31	143	2.4%	15.4	184	1.0%	15.0	1.5	2.0	17.5	327.0	24.2	17.5
C4	1.36	А	45%	0.31	0.46	28	13.8%	3.2	1210	1.6%	15.0	1.9	10.6	13.8	1238.0	28.8	13.8
C5	3.95	А	22%	0.12	0.28	97	1.4%	15.5	997	1.0%	15.0	1.5	11.1	26.6	1094.0	36.1	26.6
C6	4.19	А	15%	0.08	0.23	154	3.0%	16.0	455	1.0%	15.0	1.5	5.1	21.0	609.0	30.3	21.0
C7	1.11	А	45%	0.31	0.46	28	13.8%	3.2	673	1.0%	15.0	1.5	7.5	10.7	701.0	25.7	10.7
C8	10.13	А	5%	0.02	0.15	300	3.0%	23.5	557	1.0%	15.0	1.5	6.2	29.7	857.0	34.6	29.7
D1	3.97	D	18%	0.18	0.55	266	2.4%	20.3	354	1.0%	15.0	1.5	3.9	24.2	620.0	28.0	24.2
D2	5.58	Α	17%	0.12	0.35	83	3.0%	11.2	1382	2.2%	15.0	2.2	10.4	21.6	1465.0	36.8	21.6
D3	0.34	А	45%	0.36	0.57	46	8.0%	4.6	332	1.0%	15.0	1.5	3.7	8.3	378.0	22.0	8.3
D4	10.01	D	7%	0.07	0.40	300	1.8%	26.5	1201	1.0%	15.0	1.5	13.3	39.8	1501.0	44.9	39.8
D5	7.94	D	5%	0.06	0.39	300	2.0%	26.0	426	1.0%	7.0	0.7	10.1	36.1	726.0	32.5	32.5
D6	17.08	А	11%	0.07	0.26	300	4.0%	20.4	904	1.4%	15.0	1.8	8.4	28.8	1204.0	36.0	28.8
D7	0.86	А	45%	0.31	0.47	40	8.0%	4.5	857	1.0%	15.0	1.5	9.5	14.0	897.0	27.7	14.0
D8	6.00	А	19%	0.10	0.26	86	2.0%	13.3	1027	1.0%	15.0	1.5	11.4	24.7	1113.0	37.5	24.7
D9	2.00	Α	44%	0.30	0.46	110	3.0%	10.5	1823	1.0%	15.0	1.5	20.3	30.8	1933.0	38.6	30.8
UD1	20.70	Α	6%	0.04	0.23	300	3.0%	23.1	546	3.0%	7.0	1.2	7.5	30.6	846.0	30.3	30.3
UD2	24.68	D	2%	0.05	0.48	300	2.3%	25.0	1450	1.1%	15.0	1.6	15.4	40.3	1750.0	50.5	40.3
UD3	7.68	А	6%	0.04	0.24	300	2.5%	24.5	818	1.5%	7.0	0.9	15.9	40.4	1118.0	36.2	36.2
UD4	12.80	А	6%	0.03	0.16	300	1.6%	28.8	628	1.9%	7.0	1.0	10.8	39.6	928.0	32.6	32.6

STANDARD FORM SF-2 TIME OF CONCENTRATION

Subdivision: Saddlehorn Ranch Filing 4 Location: El Paso County

Project Name: Saddlehorn Ranch

Project No.: 25142.06

Calculated By: AAM

Checked By: TBD

Date: 3/1/22

		SUB-I	BASIN			INITI	AL/OVER	LAND		T	RAVEL TIM	E					
		DA	ATA				(T_i)				(T _t)			(U	RBANIZED BA	SINS)	FINAL
BASIN	D.A.	Hydrologic	Impervious	C ₅	C ₁₀₀	L	S_o	t _i	L_t	S_t	Κ	VEL.	t _t	COMP. t_c	TOTAL	Urbanized t_c	t _c
ID	(ac)	Soils Group	(%)			(ft)	(%)	(min)	(ft)	(%)		(ft/s)	(min)	(min)	LENGTH (ft)	(min)	(min)
OS1	2.26	D	57%	0.49	0.68	41	2.5%	5.2	45	1.1%	7.0	0.7	1.0	6.3	86.0	16.7	6.3
OS2	0.72	А	35%	0.22	0.38	41	2.5%	7.5	43	1.0%	7.0	0.7	1.0	8.5	84.0	20.6	8.5

NOTES:

Where:

Where:

 $t_c = t_i + t_t$

 t_c = computed time of concentration (minutes)

 t_i = overland (initial) flow time (minutes)

 t_t = channelized flow time (minutes).

$$t_t = \frac{L_t}{60K\sqrt{S_o}} = \frac{L_t}{60V_t}$$

Equation 6-2

Equation 6-4

Where:

 t_i = overland (initial) flow time (minutes)

C5 = runoff coefficient for 5-year frequency (from Table 6-4)

 $L_i = \text{length of overland flow (ft)}$

 S_0 = average slope along the overland flow path (ft/ft).

 $t_c = (26 - 17i) + \frac{\Sigma_t}{60(14i + 9)\sqrt{S_t}}$

Equation 6-3

Equation 6-5

Type of Land Surface	Conveyance Factor, K
Heavy meadow	2.5
Tillage/field	5
Short pasture and lawns	7
Nearly bare ground	10
Grassed waterway	15
Paved areas and shallow paved swales	20

Where:

 t_t = channelized flow time (travel time, min)

 L_t = waterway length (ft)

 S_0 = waterway slope (ft/ft) V_t = travel time velocity (ft/sec) = $K\sqrt{S_0}$

K = NRCS conveyance factor (see Table 6-2).

 t_c = minimum time of concentration for first design point when less than t_c from Equation 6-1.

 L_t = length of channelized flow path (ft)

i = imperviousness (expressed as a decimal)

 S_t = slope of the channelized flow path (ft/ft).

Use a minimum t_c value of 5 minutes for urbanized areas and a minimum t_c value of 10 minutes for areas that are not considered urban. Use minimum values even when calculations result in a lesser time of concentration.

Subdivision: Saddlehorn Ranch Filing 4
Location: El Paso County
Design Storm: 5-Year

 Project Name:
 Saddlehorn Ranch

 Project No.:
 25142.06

 Calculated By:
 AAM

 Checked By:
 TBD

 Date:
 3/1/22

				DIRE	CT RUI	NOFF			TC	OTAL F	RUNOF	F		SWALE			PI	PE		TRAV	EL TIN	1E	
																			0				
STREET	Design Point	Basin ID	Area (Ac)	Runoff Coeff.	t _c (min)	3*A (Ac)	(in/hr)	O (cfs)	tc (min)	C*A (ac)	(in/hr)	O (cfs)	O _{street} (cfs)	C*A (ac)	Slope (%)	O _{pipe} (cfs)	C*A (ac)	Slope (%)	oipe Size (inches)	ength (ft)	Velocity (fps)	t _t (min)	REMARKS
							_						2.7							387	2.0	3.2	Existing flows from Saddlehorn Filing 3
	EX1								34.7	1 19	2.26	2.7											Swale conveyance to DP 1.0
									0 1117	,	L.LO		2.0	0.72	1.0					0	2.0	0.0	Roadside Swale
	1	D1	3.97	0.18	24.2	0.72	2.80	2.0															Swale conveyance to DP 1.0
													4.1	1.91	1.7					1045	2.6	6.7	Sum of DP EX1 and DP 1
	1.0								37.9	1.91	2.13	4.1	2.0	0.77	1.0					0	2.0	0.0	Swale conveyance to DP 1.1
	2	D2	5.58	0.12	21.6	0.66	2 07	2.0					2.0	0.66	1.0					U	2.0	0.0	Roadside Swale Swale conveyance to DP 1.1
		DZ	3.30	0.12	21.0	0.00	2.71	2.0					0.5	0.12	1.0					0	2.0	0.0	Roadside Swale
	3	D3	0.34	0.36	8.3	0.12	4.41	0.5					0.0	0.12						Ŭ	2.0	0.0	Swale conveyance to DP 1.1
													5.1	2.69	1.0					117	2.0	1.0	Sum of DP 1.0, DP 2, & DP 3
	1.1								44.6	2.69	1.89	5.1											Swale conveyance to DP 1.2
	EV.0								07.0	4 (0	0.40		4.3	1.62	1.9					894	2.7	5.5	Existing flows from Saddlehorn Filing 3
	EX2								27.2	1.62	2.63	4.3	1.5	0.72	1.0					0	2.7	0.0	Swale conveyance to DP 1.2 Swale
	4	D4	10.01	0.07	30 S	0.72	2.06	1.5					1.5	0.72	1.9					U	2.1	0.0	Swale conveyance to DP 1.2
	7	DŦ	10.01	0.07	37.0	0.72	2.00	1.5					9.3	5.03	0.8					623	1.7	6.0	Sum of DP 1.1, DP EX2, and DP 4
	1.2								45.6	5.03	1.85	9.3											Swale/ Pond conveyance to DP 1.6
													3.0	1.17	1.1					430	2.1	3.4	Roadside Swale
	6	D6	17.08	0.07	28.8	1.17	2.54	3.0															Swale conveyance to DP 1.3
	7	D7	0.86	0.31	14.0	0.27	3.62	1.0					1.0	0.27	1.0					0	2.0	0.0	Roadside Swale
	,	וט	0.60	0.31	14.0	0.27	3.02	1.0					3.4	1.44	1.0					136	2.0	11	Swale conveyance to DP 1.3 Sum of DP 6 and DP 7
	1.3								32.3	1.44	2.37	3.4	5.4	1.44	1.0					130	2.0		Culvert conveyance to DP 1.5
													1.7	0.61	1.1					442	2.1		Roadside Swale
	8	D8	6.00	0.10	24.7	0.61	2.77	1.7															Swale conveyance to DP 1.4
													1.5	0.60	1.1					0	2.1	0.0	Roadside Swale
	9	D9	2.00	0.30	30.8	0.60	2.44	1.5					0.0	4.04	4.0					10/	0.0		Swale conveyance to DP 1.4
	1.4								30.8	1 21	2.44	3.0	3.0	1.21	1.0					136	2.0	1.1	Sum of DP 8 and DP 9 conveyance to DP 1.5
	1.4								30.0	1.21	2.44	3.0	6.1	2.65	0.5		-			153	1.4	1.8	Sum of DP 1.3 and DP 1.4
	1.5								33.4	2.65	2.32	6.1	0.1	2.00	0.5					100	1.4	1.0	Swale/ Pond conveyance to DP 1.6
													1.1	0.45	1.0	1				0	2.0	0.0	Roadside Swale
	5	D5	7.94	0.06	32.5	0.45	2.36	1.1															Swale conveyance to DP 1.6
													13.6	8.13	0.75					0	1.7	0.0	Sum of DP 1.2, DP 1.5, and DP 5
	1.6								51.6	8.13	1.67	13.6	10	0.27	1.0	!		ļ		1014	2.0	10.1	Outlet structure release into Drainageway MS-06
	11	C1	2.14	0 17	12.0	0.36	3 64	1.3					1.3	0.36	1.0					1214	2.0	10.1	Roadside Swale Swale conveyance to DP 2.0
		U1	2.14	0.17	13.9	0.30	3.04	1.3					2.4	1.04	1.0	1	+			n	2.0	0.0	Roadside Swale
	12	C2	22.55	0.05	33.7	1.04	2.31	2.4															Swale conveyance to DP 2.0

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Subdivision:	Saddlehorn Ranch Filing 4
Location:	El Paso County
Design Storm:	5-Year

 Project Name:
 Saddlehorn Ranch

 Project No.:
 25142.06

 Calculated By:
 AAM

 Checked By:
 TBD

 Date:
 371722

		DIRECT RUNOFF							TO	TAL F	RUNOF		SWALE			PI	PE		TRAV	EL TIN	ΊE			
STREET	Jesign Point	Basin ID	Area (Ac)	Runoff Coeff.	(min)	.*A (Ac)	(in/hr)	Q (cfs)	tc (min)	2*A (ac)	(in/hr)	Q (cfs)	O _{street} (cfs)	C*A (ac)	Slope (%)	O _{pipe} (cfs)	C*A (ac)	Slope (%)	lpe Size (inches)	ength (ft)	Velocity (fps)	(min)	REMARKS	
	ā	B	Ā	2	ئ	ت	_	O	tc	ت		0	3.2		0.5		ت	S	Ŀ	278	5 1.4	33	Sum of DP 11 & DP 12	
	2.0								33.7	1.40	2.31	3.2		1.40	0.5					270	1.4		wale conveyance to DP 2.2	
													6.8	4.61	1.0					1147	2.0		Existing flows from Saddlehorn Filing 3	
	EX3								58.3	4.61	1.48	6.8											Swale conveyance to DP 2.1 Roadside Swale	
													1.3	0.49	1.0					0	2.0			
	15	C5	3.95	0.12	26.6	0.49	2.66	1.3															Swale conveyance to DP 2.1	
	2.1								E0 2	5.10	1 /10	7.6				7.4	5.10	1.0	36	59	6.2	0.2	Sum of DP EX3 and DP 15 Culvert conveyance to DP 2.2	
	2.1								30.3	5.10	1.40	7.0	0.6	0.19	1.5		3.10	1.0	30	1071	2.4		Roadside Swale	
	13	C3	1.26	0.15	17.5	0.19	3.29	0.6					0.0	0.17	1.5					1071	2.7	7.5	Swale conveyance to DP 2.2	
	1												1.5	0.42	1.0					0	2.0	0.0	Roadside Swale Swale conveyance to DP 2.2 Sum of DP 13, DP 14, DP 2.0, & DP 2.1 Swale/ Pond conveyance to DP 2.4 Roadside Swale Swale conveyance to DP 2.3	
	14	C4	1.36	0.31	13.8	0.42	3.65	1.5																
													10.5	7.11	1.0					388	2.0	3.2		
	2.2								58.5	7.11	1.48	10.5												
													0.9	0.31	1.1					288	2.1	2.3		
	16	C6	4.19	0.08	21.0	0.31	3.01	0.9					1 /	0.24	1 1					0	2.1	0.0		
	17	C7	1.11	0.31	10.7	0.34	4.03	1.4					1.4	0.34	1.1					0	2.1	0.0	Roadside Swale Swale conveyance to DP 2.3	
	17	C/	1.11	0.31	10.7	0.34	4.03	1.4					1.9	0.65	1.0					649	2.0	5.4	Swale conveyance to DP 2.3 Sum of DP 16 and DP 17	
	2.3								23.3	0.65	2.86	1.9		0.00	1.0					017	2.0	0.1	Swale conveyance to DP 2.4	
													0.5	0.20	1.0					0	2.0	0.0	Existing Pond C, Filing 4 Lots, and Filing 4 roadways	
	18	C8	10.13	0.02	29.7	0.20	2.50	0.5															Overland flow, swale, and pond conveyance to DP 2.4	
													11.1	7.96	1.0					1147	2.0		Sum of DP 2.2, DP 2.3, and DP 18	
	2.4								61.7	7.96	1.40	11.1											Outlet structure release into Drainageway MS-06	
	LID1	LID1	20.70	0.04	20.2	0.70	2.47	1.0															Overland Flow	
	ועט	ועט	20.70	0.04	30.3	0.79	2.47	1.9															Sheet flow into Drainageway WF-R7A Overland Flow	
	UD2	UD2	24.68	0.05	40.3	1.21	2.04	2.5															Sheet flow into Drainageway WF-R7A	
	002	002	2 1.00	0.00	10.0		2.01	2.0															Overland Flow	
	UD3	UD3	7.68	0.04	36.2	0.30	2.20	0.7															Sheet flow into Drainageway WF-R7A	
																							Overland Flow	
	UD4	UD4	12.80	0.03	32.6	0.32	2.35	0.8															Sheet flow into Drainageway MS-06	
	001	001	2.24	0.40	4.2	1 10	4.02	E 2															Overland Flow	
	OS1	OS1	2.26	0.49	0.3	1.10	4.83	5.3										-	-				Sheet flow into Drainageway WF-R7A Overland Flow	
	OS2	OS2	0.72	0.22	8.5	0.16	4.37	0.7															Sheet flow into Drainageway WF-R7A	
	002		0.72	0.22	0.0	50		0.7									+						gonuj *** ****	

Notes

Street and Pipe C*A values are determined by Q/i using the catchment's intensity value.

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Subdivision: Saddlehorn Ranch Filing 4
Location: El Paso County
Design Storm: 100-Year

Project Name: Saddlehorn Ranch
Project No.: 25142.06

Calculated By: AAM
Checked By: TBD
Date: 3/1/22

		DIRECT RUNOFF							TC	SWALE				PI	PE		TRAV	EL TIN	ΛE				
																			(S)				
STREET	Design Point	Basin ID	Area (ac)	Runoff Coeff.	t _c (min)	C*A (ac)	l (in/hr)	O (cfs)	tc (min)	C*A (ac)	l (in/hr)	O (cfs)	O _{street} (cfs)	C*A (ac)	Slope (%)	O _{pipe} (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	t _t (min)	REMARKS
													15.4	4.05						387	2.0	3.2	Existing flows from Saddlehorn Filing 3
	EX1								34.7	4.05	3.80	15.4											Swale conveyance to DP 1.0
	1	D1	2.07	0.55	24.2	0.10	4.71	10.0					10.3	2.18	1.0					0	2.0	0.0	Roadside Swale
		D1	3.97	0.55	24.2	2.18	4./1	10.3					22.3	6.23	1.7					1045	2.6	6.7	Swale conveyance to DP 1.0 Sum of DP EX1 and DP 1
	1.0								37.9	6.23	3.57	22.3	22.3	0.23	1.7					1045	2.0	0.7	Swale conveyance to DP 1.1
													9.7	1.95	1.0					0	2.0	0.0	Roadside Swale
	2	D2	5.58	0.35	21.6	1.95	4.99	9.7															Swale conveyance to DP 1.1
	3	D3	0.34	0.57	83	N 10	7.41	1.4					1.4	0.19	1.0					0	2.0	0.0	Roadside Swale Swale conveyance to DP 1.1
	3	D3	0.34	0.37	0.3	0.17	7.41	1.4					26.5	8.37	1.0					117	2.0	1.0	Sum of DP 1.0, DP 2, & DP 3
	1.1								44.6	8.37	3.16	26.5	20.0	0.07							2.0		Swale conveyance to DP 1.2
													11.3	2.56	1.9					894	2.7	5.5	Existing flows from Saddlehorn Filing 3
	EX2								27.2	2.56	4.41	11.3											Swale conveyance to DP 1.2
													13.9	4.03	1.9					0	2.7	0.0	Swale
	4	D4	10.01	0.40	39.8	4.03	3.45	13.9					4/ 5	140/	0.0					(22	17	/ 0	Swale conveyance to DP 1.2 Sum of DP 1.1, DP EX2, and DP 4
	1.2								45.6	14 96	3.11	46.5	40.5	14.96	0.8					623	1.7	6.0	Sum of DP 1.1, DP EX2, and DP 4 Swale/ Pond conveyance to DP 1.6
	1.2								10.0		0	10.0	19.3	4.52	1.1					430	2.1	3.4	Roadside Swale
	6	D6	17.08	0.26	28.8	4.52	4.26	19.3															Swale conveyance to DP 1.3
													2.4	0.40	1.0					0	2.0	0.0	Roadside Swale
	7	D7	0.86	0.47	14.0	0.40	6.08	2.4															Swale conveyance to DP 1.3
	1 2								22.2	4.00	2.00	10 /	19.6	4.92	1.0					136	2.0		Sum of DP 6 and DP 7
	1.3								32.3	4.92	3.98	19.0	7.2	1.54	1.1					442	2.1		Culvert conveyance to DP 1.5 Roadside Swale
	8	D8	6.00	0.26	24.7	1.54	4.65	7.2					1.2	1.54	1.1					442	2.1	3.3	Swale conveyance to DP 1.4
	Ů	- 50	0.00	0.20	2	1101	1100	7.2					3.7	0.91	1.1					0	2.1	0.0	Roadside Swale
	9	D9	2.00	0.46	30.8	0.91	4.10	3.7															Swale conveyance to DP 1.4
													10.0	2.45	1.0					136	2.0	1.1	Sum of DP 8 and DP 9
	1.4								30.8	2.45	4.10	10.0											conveyance to DP 1.5
	1.5								22.4	7.07	2.00	20.7	28.7	7.37	0.5					153	1.4	1.8	Sum of DP 1.3 and DP 1.4
	1.5								33.4	1.51	3.89	Zö./	12.4	3.13	1.0			-		0	2.0	0.0	Swale/ Pond conveyance to DP 1.6 Roadside Swale
	5	D5	7.94	0.39	32.5	3.13	3.96	12.4					12.4	3.13	1.0						2.0	0.0	Swale conveyance to DP 1.6
													71.3	25.46	0.75					0	1.7	0.0	Sum of DP 1.2, DP 1.5, and DP 5
	1.6								51.6	25.46	2.80	71.3											Outlet structure release into Drainageway MS-06
		04	0.4:	0.00	40.5								4.9	0.81	1.0					1214	2.0		Roadside Swale
	11	C1	2.14	0.38	13.9	0.81	6.10	4.9					14 4	4.24	1.0					_	2.0		Swale conveyance to DP 2.0
	12	C2	22 55	0.10	33.7	4 24	3 87	16.4					16.4	4.24	1.0					0	2.0		Roadside Swale Swale conveyance to DP 2.0
	12	UZ	22.33	0.17	JJ.1	4.24	5.07	10.4										1					Swale conveyance to DF 2.0

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Subdivision:	Saddlehorn Ranch Filing 4
Location:	El Paso County
Design Storm:	100-Year

Project Name: Saddlehorn Ranch
Project No.: 25142.06
Calculated By: AAM
Checked By: TBD
Date: 3/1/22

		DIRECT RUNOFF							TO	SWALE				PI	PE		TRAV	EL TIN	ЛE						
	_			نے															ches)		()				
STREET	Design Point	Basin ID	Area (ac)	Runoff Coeff.	(min)	C*A (ac)	(in/hr)	O (cfs)	(min)	C*A (ac)	(in/hr)	O (cfs)	O _{street} (cfs)	C*A (ac)	Slope (%)	O _{pipe} (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	ength (ft)	Velocity (fps)	(min)	REMARKS		
	Des	Bas	Are	Rur	t _c (C* A	Ë	o (c	tc (ر* ک	ı.) a	Str	C* A	Slop	g	.×.	Slop	Pipe	Len	Velo	t _t (i			
													19.6							278	1.4	3.3	Sum of DP 11 & DP 12		
	2.0								33.7	5.05	3.87	19.6											Swale conveyance to DP 2.2		
	=>/*												32.2	12.95	1.0					1147	2.0		Existing flows from Saddlehorn Filing 3		
	EX3								58.3	12.95	2.49	32.2	г о	1 11	1.0					0	2.0		Swale conveyance to DP 2.1 Roadside Swale		
	15	C5	3.95	0.28	26.6	1.11	4.46	5.0					5.0	1.11	1.0					U	2.0		Roadside Swale Swale conveyance to DP 2.1		
	13	0.5	3.73	0.20	20.0	1.11	4.40	3.0															water Conveyance to DP 2.1 Sulvert conveyance to DP 2.2		
	2.1								58.3	14.06	2.49	35.0				35.0	14.06	1.0	36	59	9.5	0.1			
														0.38	1.5					1071	2.4		Roadside Swale		
	13	C3	1.26	0.31	17.5	0.38	5.53	2.1															Swale conveyance to DP 2.2 Roadside Swale		
													3.9	0.63	1.0					0	2.0	0.0			
	14	C4	1.36	0.46	13.8	0.63	6.12	3.9															Swale conveyance to DP 2.2		
													50.0	20.12	1.0					388	2.0		Sum of DP 13, DP 14, DP 2.0, & DP 2.1 Swale/ Pond conveyance to DP 2.4 Roadside Swale Swale conveyance to DP 2.3 Roadside Swale Swale conveyance to DP 2.3		
	2.2								58.4	20.12	2.49	50.0		0.05						000	0.4				
	1.	0/	4.10	0.00	21.0	0.05	F 0/	4.0					4.8	0.95	1.1					288	2.1				
	16	C6	4.19	0.23	21.0	0.95	5.06	4.8					2.5	0.51	11					0	2.1				
	17	C7	1 11	0.46	10.7	0.51	6.77	3.5					3.5	0.51	1.1					U	2.1				
	17	- 07	1.11	0.40	10.7	0.01	0.77	3.3					7.0	1.46	1.0					649	2.0		Sum of DP 16 and DP 17		
	2.3								23.3	1.46	4.80	7.0											Swale conveyance to DP 2.4		
														1.54	1.0					0	2.0	0.0	Existing Pond C, Filing 4 Lots, and Filing 4 roadways		
	18	C8	10.13	0.15	29.7	1.54	4.19	6.5															Overland flow, swale, and pond conveyance to DP 2.4		
													54.3	23.12	1.0					1147	2.0	9.6	Sum of DP 2.2, DP 2.3, and DP 18		
	2.4								61.6	23.12	2.35	54.3											Outlet structure release into Drainageway MS-06		
	LID1	LID1	20.70	0.00	20.2	4.00	4 1 4	20.0															Overland Flow		
	UD1	ועט	20.70	0.23	30.3	4.83	4.14	20.0															Sheet flow into Drainageway WF-R7A Overland Flow		
	UD2	UD2	24 68	0.48	40.3	11 75	3.42	40.2															Overland Flow Sheet flow into Drainageway WF-R7A		
	ODZ	ODZ	21.00	0.10	10.0	11.70	0.12	10.2															Overland Flow		
	UD3	UD3	7.68	0.24	36.2	1.86	3.69	6.9															Sheet flow into Drainageway WF-R7A		
																							Overland Flow		
	UD4	UD4	12.80	0.16	32.6	2.02	3.95	8.0															Sheet flow into Drainageway MS-06		
	OS1	OS1	2.26	0.68	6.2	1.55	8.11	12.6															Overland Flow		
	UST	UST	2.20	0.08	0.3	1.00	0.11	12.0			<u> </u>						_						Sheet flow into Drainageway WF-R7A Overland Flow		
	OS2	OS2	0.72	0.38	8.5	0.27	7.34	2.0															overland Flow Sheet flow into Drainageway WF-R7A		
			0.72	0.00	0.0	0.27	,	2.0															gonuj III IIII		

Notes: Street and Pipe C*A values are determined by Q/i using the catchment's intensity value.

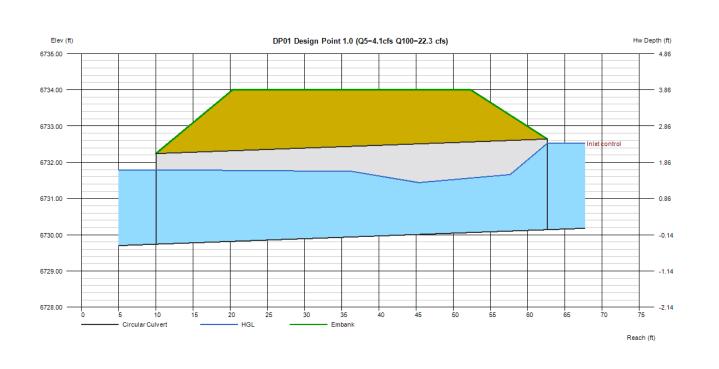
X:\2510000.all\2514206\Excel\Drainage\Filing 4 Drainage Calcs_v2.07.xlsm Page 2 of 2 3/1/2022

APPENDIX C HYDRAULIC CALCULATIONS

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

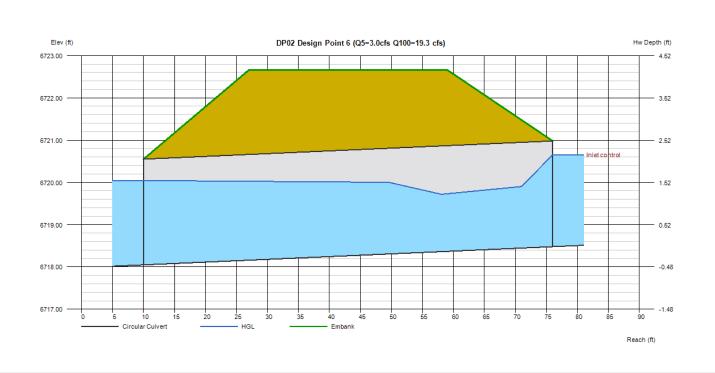
DP01 Design Point 1.0 (Q5=4.1cfs Q100=22.3 cfs)

Invert Elev Dn (ft)	= 6729.74	Calculations	
Pipe Length (ft)	= 52.63	Qmin (cfs)	= 4.10
Slope (%)	= 0.76	Qmax (cfs)	= 22.30
Invert Elev Up (ft)	= 6730.14	Tailwater Elev (ft)	= (dc+D)/2
Rise (in)	= 30.0		
Shape	= Circular	Highlighted	
Span (in)	= 30.0	Qtotal (cfs)	= 22.29
No. Barrels	= 1	Qpipe (cfs)	= 22.29
n-Value	= 0.012	Qovertop (cfs)	= 0.00
Culvert Type	Circular Concrete	Veloc Dn (ft/s)	= 5.17
Culvert Entrance	= Groove end projecting (C)	Veloc Up (ft/s)	= 6.67
Coeff. K,M,c,Y,k	= 0.0045, 2, 0.0317, 0.69, 0.2	HGL Dn (ft)	= 6731.79
		HGL Up (ft)	= 6731.75
Embankment		Hw Elev (ft)	= 6732.53
Top Elevation (ft)	= 6734.00	Hw/D (ft)	= 0.95
Top Width (ft)	= 32.00	Flow Regime	= Inlet Control
Crest Width (ft)	= 20.00		



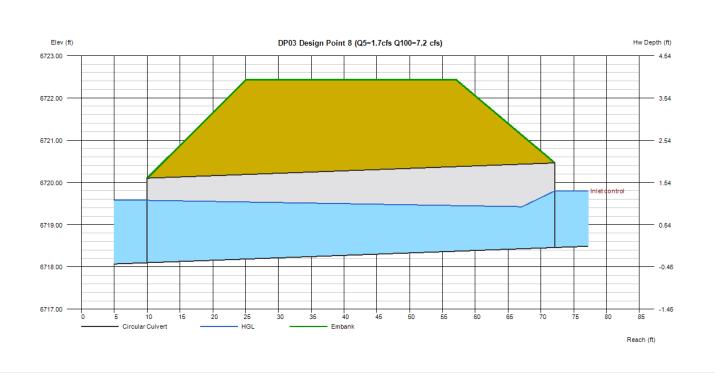
DP02 Design Point 6 (Q5=3.0cfs Q100=19.3 cfs)

Invert Elev Dn (ft)	= 6718.05	Calculations	
Pipe Length (ft)	= 66.01	Qmin (cfs)	= 3.00
Slope (%)	= 0.65	Qmax (cfs)	= 19.30
Invert Elev Up (ft)	= 6718.48	Tailwater Elev (ft)	= (dc+D)/2
Rise (in)	= 30.0		
Shape	= Circular	Highlighted	
Span (in)	= 30.0	Qtotal (cfs)	= 19.30
No. Barrels	= 1	Qpipe (cfs)	= 19.30
n-Value	= 0.012	Qovertop (cfs)	= 0.00
Culvert Type	Circular Concrete	Veloc Dn (ft/s)	= 4.60
Culvert Entrance	= Groove end projecting (C)	Veloc Up (ft/s)	= 6.30
Coeff. K,M,c,Y,k	= 0.0045, 2, 0.0317, 0.69, 0.2	HGL Dn (ft)	= 6720.04
		HGL Up (ft)	= 6719.98
Embankment		Hw Elev (ft)	= 6720.65
Top Elevation (ft)	= 6722.66	Hw/D (ft)	= 0.87
Top Width (ft)	= 32.00	Flow Regime	= Inlet Control
Crest Width (ft)	= 20.00		



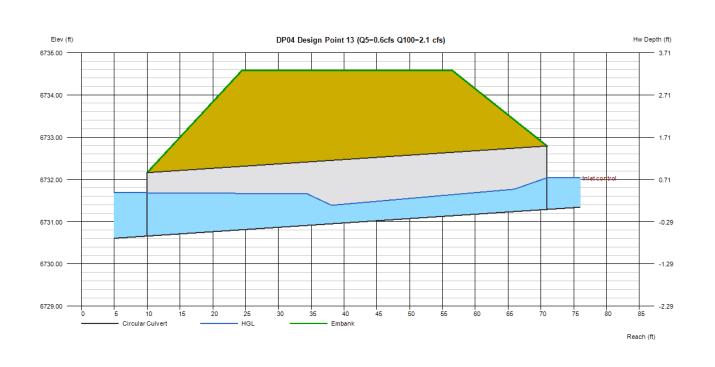
DP03 Design Point 8 (Q5=1.7cfs Q100=7.2 cfs)

Invert Elev Dn (ft)	= 6718.10	Calculations	
Pipe Length (ft)	= 62.13	Qmin (cfs)	= 1.70
Slope (%)	= 0.58	Qmax (cfs)	= 7.20
Invert Elev Up (ft)	= 6718.46	Tailwater Elev (ft)	= (dc+D)/2
Rise (in)	= 24.0		
Shape	= Circular	Highlighted	
Span (in)	= 24.0	Qtotal (cfs)	= 7.20
No. Barrels	= 1	Qpipe (cfs)	= 7.20
n-Value	= 0.012	Qovertop (cfs)	= 0.00
Culvert Type	= Circular Concrete	Veloc Dn (ft/s)	= 2.90
Culvert Entrance	= Groove end projecting (C)	Veloc Up (ft/s)	= 4.88
Coeff. K,M,c,Y,k	= 0.0045, 2, 0.0317, 0.69, 0.2	HGL Dn (ft)	= 6719.58
		HGL Up (ft)	= 6719.41
Embankment		Hw Elev (ft)	= 6719.80
Top Elevation (ft)	= 6722.43	Hw/D (ft)	= 0.67
Top Width (ft)	= 32.00	Flow Regime	= Inlet Control
Crest Width (ft)	= 20.00		



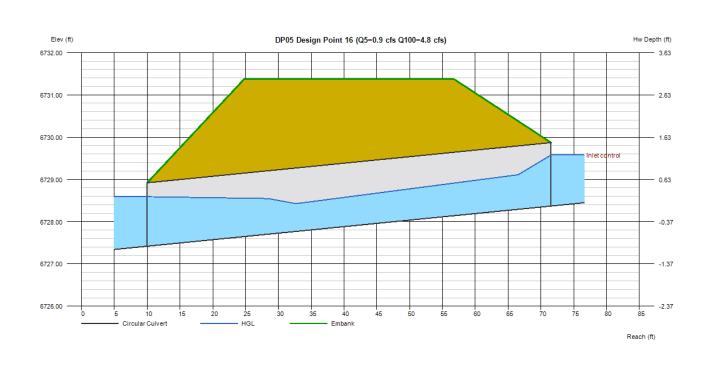
DP04 Design Point 13 (Q5=0.6cfs Q100=2.1 cfs)

Invert Elev Dn (ft)	= 6730.66	Calculations	
Pipe Length (ft)	= 60.93	Qmin (cfs)	= 0.60
Slope (%)	= 1.03	Qmax (cfs)	= 2.10
Invert Elev Up (ft)	= 6731.29	Tailwater Elev (ft)	= (dc+D)/2
Rise (in)	= 18.0		
Shape	= Circular	Highlighted	
Span (in)	= 18.0	Qtotal (cfs)	= 2.10
No. Barrels	= 1	Qpipe (cfs)	= 2.10
n-Value	= 0.012	Qovertop (cfs)	= 0.00
Culvert Type	Circular Concrete	Veloc Dn (ft/s)	= 1.63
Culvert Entrance	= Groove end projecting (C)	Veloc Up (ft/s)	= 3.61
Coeff. K,M,c,Y,k	= 0.0045, 2, 0.0317, 0.69, 0.2	HGL Dn (ft)	= 6731.68
		HGL Up (ft)	= 6731.84
Embankment		Hw Elev (ft)	= 6732.04
Top Elevation (ft)	= 6734.58	Hw/D (ft)	= 0.50
Top Width (ft)	= 32.00	Flow Regime	= Inlet Control
Crest Width (ft)	= 20.00		



DP05 Design Point 16 (Q5=0.9 cfs Q100=4.8 cfs)

Invert Elev Dn (ft)	= 6727.42	Calculations	
Pipe Length (ft)	= 61.54	Qmin (cfs)	= 0.90
Slope (%)	= 1.54	Qmax (cfs)	= 4.80
Invert Elev Up (ft)	= 6728.37	Tailwater Elev (ft)	= (dc+D)/2
Rise (in)	= 18.0	, ,	, ,
Shape	= Circular	Highlighted	
Span (in)	= 18.0	Qtotal (cfs)	= 4.80
No. Barrels	= 1	Qpipe (cfs)	= 4.80
n-Value	= 0.012	Qovertop (cfs)	= 0.00
Culvert Type	= Circular Concrete	Veloc Dn (ft/s)	= 3.24
Culvert Entrance	= Groove end projecting (C)	Veloc Up (ft/s)	= 4.70
Coeff. K,M,c,Y,k	= 0.0045, 2, 0.0317, 0.69, 0.2	HGL Dn (ft)	= 6728.59
		HGL Up (ft)	= 6729.21
Embankment		Hw Elev (ft)	= 6729.58
Top Elevation (ft)	= 6731.37	Hw/D (ft)	= 0.80
Top Width (ft)	= 32.00	Flow Regime	= Inlet Control
Crest Width (ft)	= 20.00	J	
• •			



Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Wednesday, Apr 19 2023

DP 1.0 Swale (5-Year)(FR:0.50)

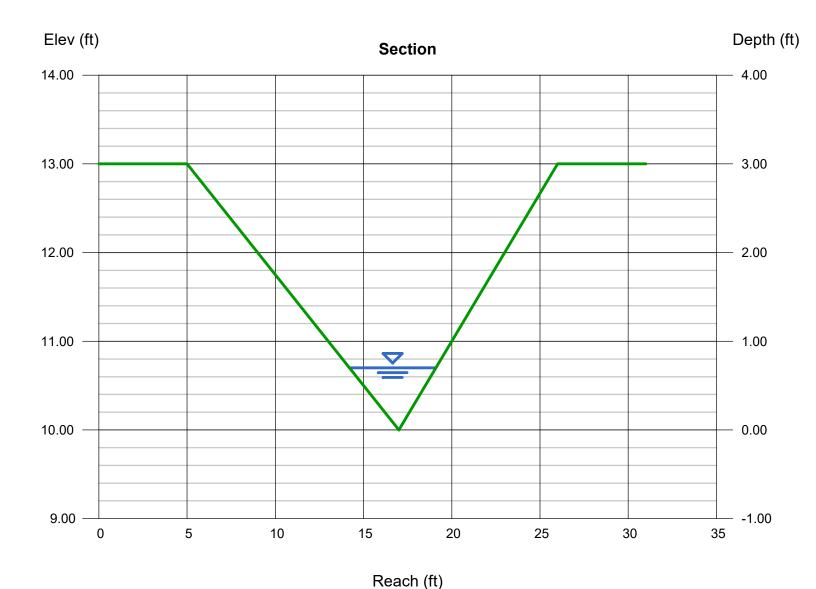
ırıangular	
Side Slopes (z:1)	= 4.00, 3.00
Total Depth (ft)	= 3.00

Invert Elev (ft) = 10.00 Slope (%) = 1.00 N-Value = 0.030

Calculations

Compute by: Known Q Known Q (cfs) = 4.10

Highlighted		
Depth (ft)	=	0.70
Q (cfs)	=	4.100
Area (sqft)	=	1.71
Velocity (ft/s)	=	2.39
Wetted Perim (ft)	=	5.10
Crit Depth, Yc (ft)	=	0.62
Top Width (ft)	=	4.90
EGL (ft)	=	0.79



Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Wednesday, Apr 19 2023

= 1.53

DP 1.0 Swale (100-Year)(FR:0.55)

Triangular	
Side Slopes (z:1)	= 4.00, 3.00
Total Depth (ft)	= 3.00

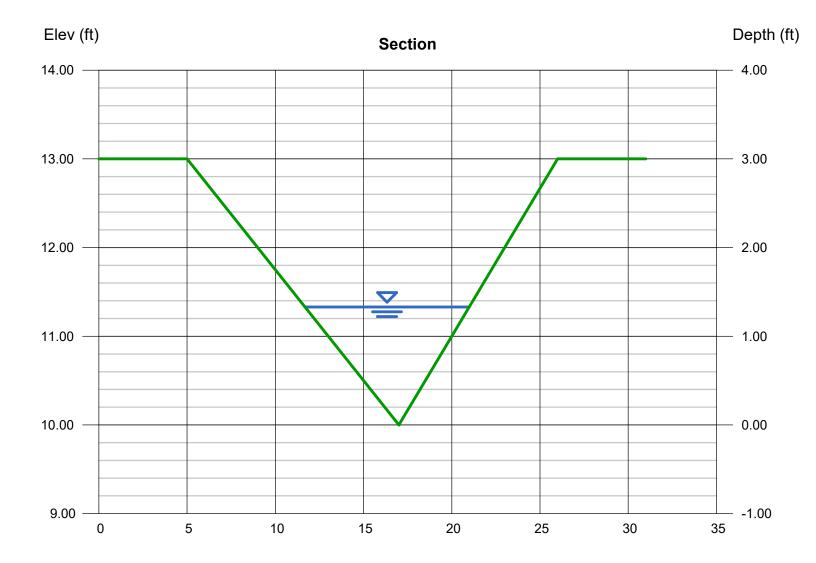
Invert Elev (ft) = 10.00 Slope (%) = 1.00 N-Value = 0.030

Calculations

Compute by: Known Q Known Q (cfs) = 22.30

Highlighted		
Depth (ft)	=	1.33
Q (cfs)	=	22.30
Area (sqft)	=	6.19
Velocity (ft/s)	=	3.60
Wetted Perim (ft)	=	9.69
Crit Depth, Yc (ft)	=	1.21
Top Width (ft)	=	9.31

EGL (ft)



Reach (ft)

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Wednesday, Apr 19 2023

DP 1.1 Swale (5-Year)(FR:0.63)

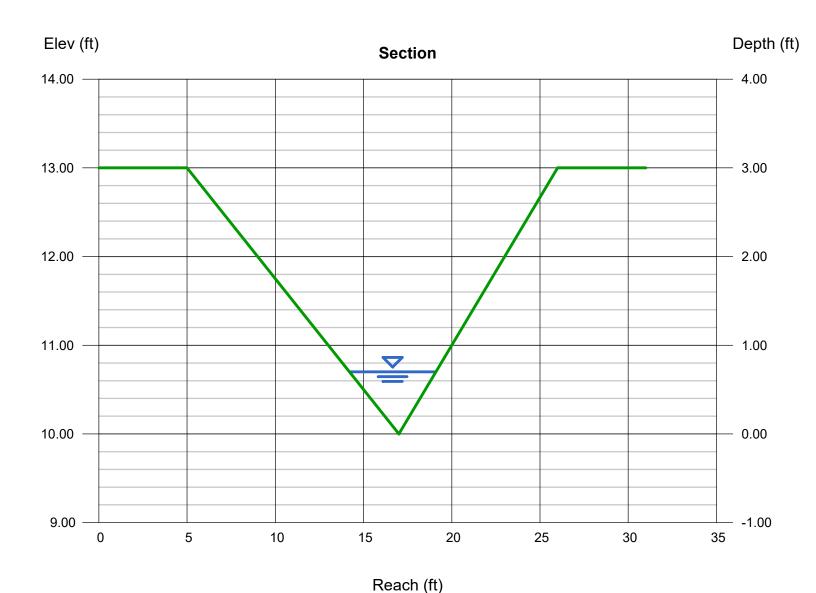
ırıangular	
Side Slopes (z:1)	= 4.00, 3.00
Total Depth (ft)	= 3.00
	40.00

Invert Elev (ft) = 10.00 Slope (%) = 1.60 N-Value = 0.030

Calculations

Compute by: Known Q Known Q (cfs) = 5.10

Highlighted		
Depth (ft)	=	0.70
Q (cfs)	=	5.100
Area (sqft)	=	1.71
Velocity (ft/s)	=	2.97
Wetted Perim (ft)	=	5.10
Crit Depth, Yc (ft)	=	0.67
Top Width (ft)	=	4.90
EGL (ft)	=	0.84



Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Wednesday, Apr 19 2023

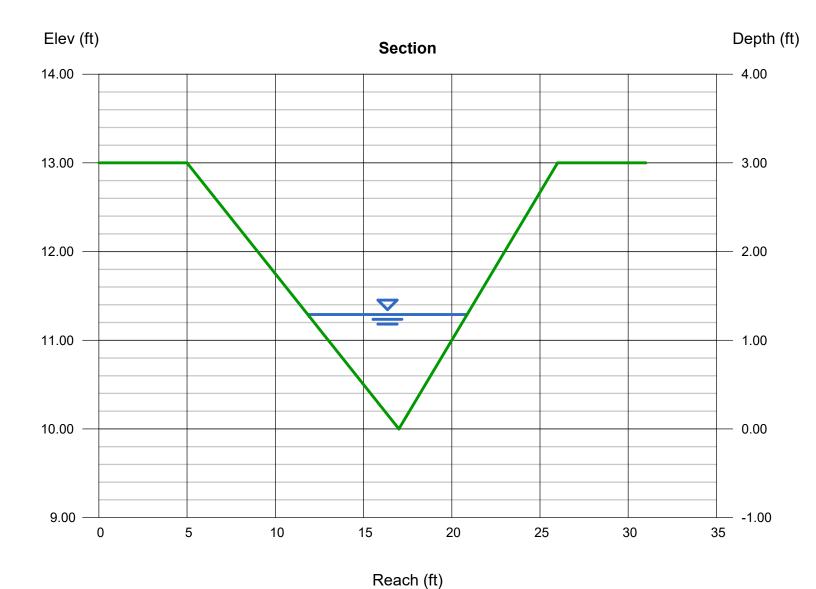
DP 1.1 Swale (100-Year)(FR:.70)

Triangular Side Slopes (z:1) Total Depth (ft)	= 4.00, 3.00 = 3.00
Invert Elev (ft)	= 10.00
Slope (%)	= 1.60
N-Value	= 0.030

Calculations

Compute by: Known Q Known Q (cfs) = 26.50

Highlighted	
Depth (ft)	= 1.29
Q (cfs)	= 26.50
Area (sqft)	= 5.82
Velocity (ft/s)	= 4.55
Wetted Perim (ft)	= 9.40
Crit Depth, Yc (ft)	= 1.29
Top Width (ft)	= 9.03
EGL (ft)	= 1.61



Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Wednesday, Apr 19 2023

DP 1.3 Swale (5-Year)(FR:0.52)

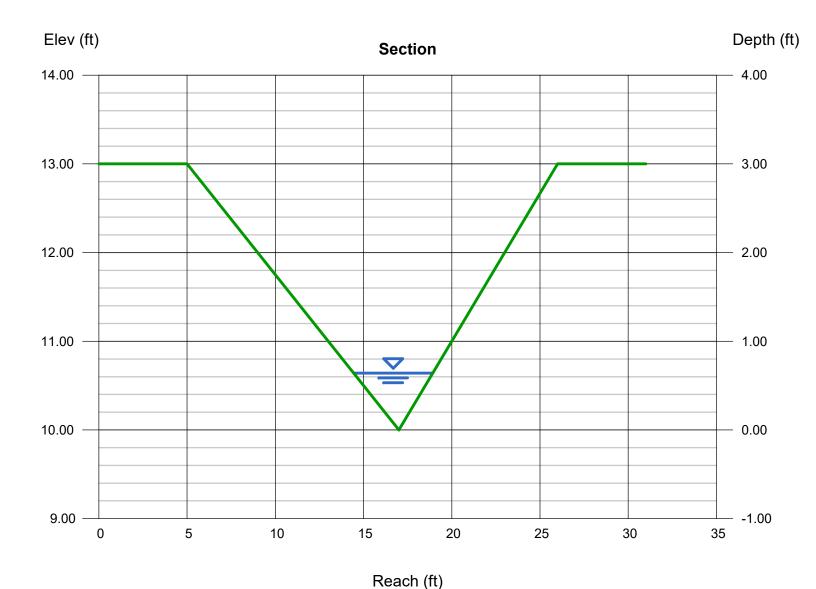
ırıangular	
Side Slopes (z:1)	= 4.00, 3.00
Total Depth (ft)	= 3.00
Invert Floy (ft)	- 10.00

Invert Elev (ft) = 10.00 Slope (%) = 1.17 N-Value = 0.030

Calculations

Compute by: Known Q Known Q (cfs) = 3.40

Highlighted		
Depth (ft)	=	0.64
Q (cfs)	=	3.400
Area (sqft)	=	1.43
Velocity (ft/s)	=	2.37
Wetted Perim (ft)	=	4.66
Crit Depth, Yc (ft)	=	0.57
Top Width (ft)	=	4.48
EGL (ft)	=	0.73



Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Wednesday, Apr 19 2023

DP 1.3 Swale (100-Year)(FR:0.58)

Triangular	
Side Slopes (z:1)	= 4.00, 3.00
Total Depth (ft)	= 3.00

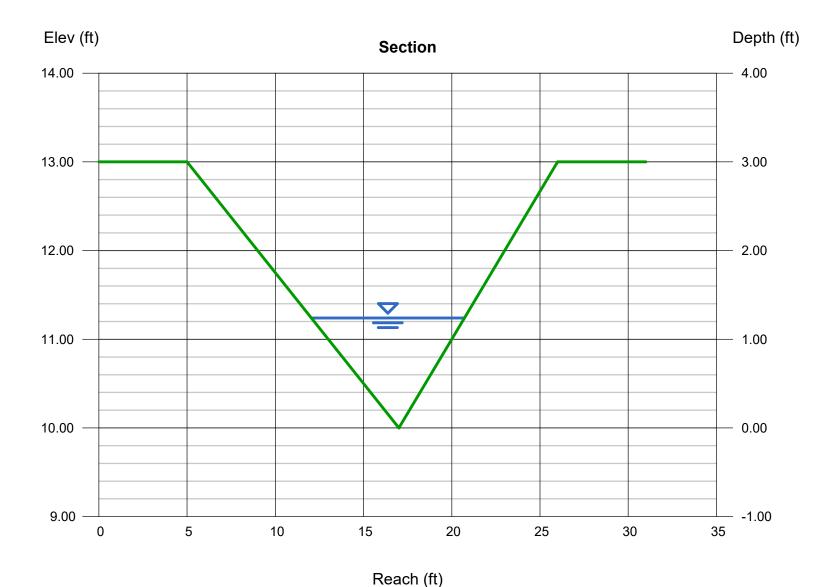
Invert Elev (ft) = 10.00 Slope (%) = 1.10 N-Value = 0.030

Calculations

Compute by: Known Q Known Q (cfs) = 19.60

Highlighted Depth (ft) = 1.24 Q (cfs) = 19.60 Area (sqft) = 5.38

Q (cfs) = 19.60 Area (sqft) = 5.38 Velocity (ft/s) = 3.64 Wetted Perim (ft) = 9.03 Crit Depth, Yc (ft) = 1.15 Top Width (ft) = 8.68 EGL (ft) = 1.45



Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Wednesday, Apr 19 2023

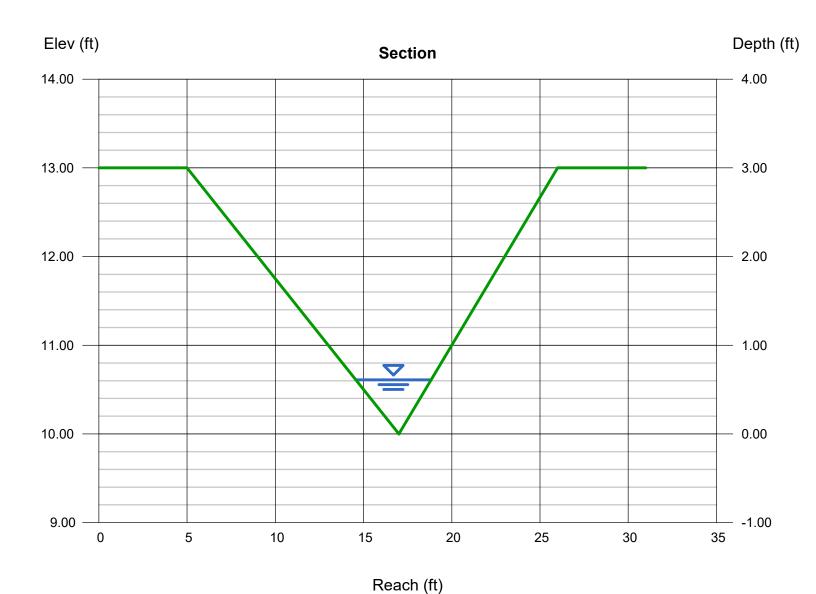
DP 1.4 Swale (5-Year)(FR:0.52)

Side Slopes (z:1) Total Depth (ft)	= 4.00, 3.00 = 3.00
Invert Elev (ft)	= 10.00
Slope (%)	= 1.17
N-Value	= 0.030

Calculations

Compute by: Known Q Known Q (cfs) = 3.00

Highlighted		
Depth (ft)	=	0.61
Q (cfs)	=	3.000
Area (sqft)	=	1.30
Velocity (ft/s)	=	2.30
Wetted Perim (ft)	=	4.44
Crit Depth, Yc (ft)	=	0.54
Top Width (ft)	=	4.27
EGL (ft)	=	0.69



Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Wednesday, Apr 19 2023

DP 1.4 Swale (100-Year)(FR:0.57)

T	ri	aı	าg	u	lar

Side Slopes (z:1) = 4.00, 3.00Total Depth (ft) = 3.00

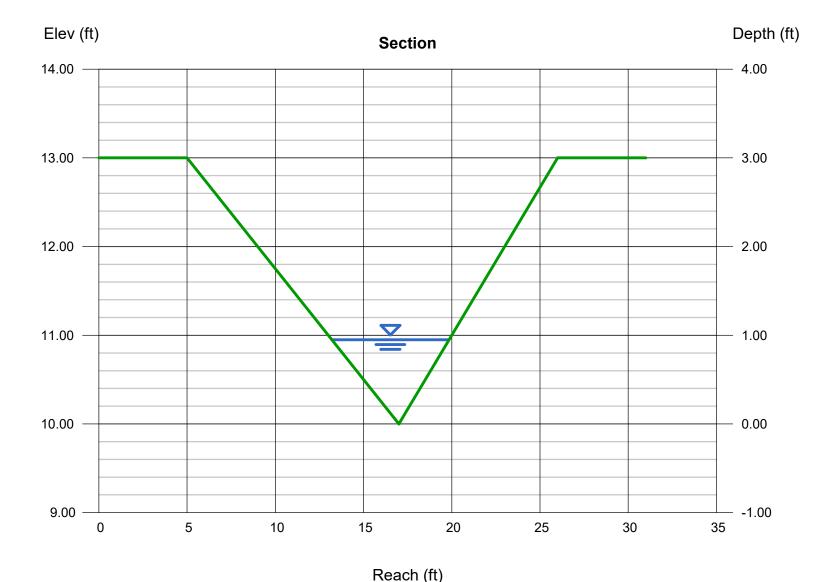
Invert Elev (ft) = 10.00 Slope (%) = 1.17 N-Value = 0.030

Calculations

Compute by: Known Q Known Q (cfs) = 10.00

Highlighted

Depth (ft) = 0.95Q (cfs) = 10.00Area (sqft) = 3.16Velocity (ft/s) = 3.17 Wetted Perim (ft) = 6.92Crit Depth, Yc (ft) = 0.88Top Width (ft) = 6.65EGL (ft) = 1.11



Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

= 0.030

Friday, Jun 9 2023

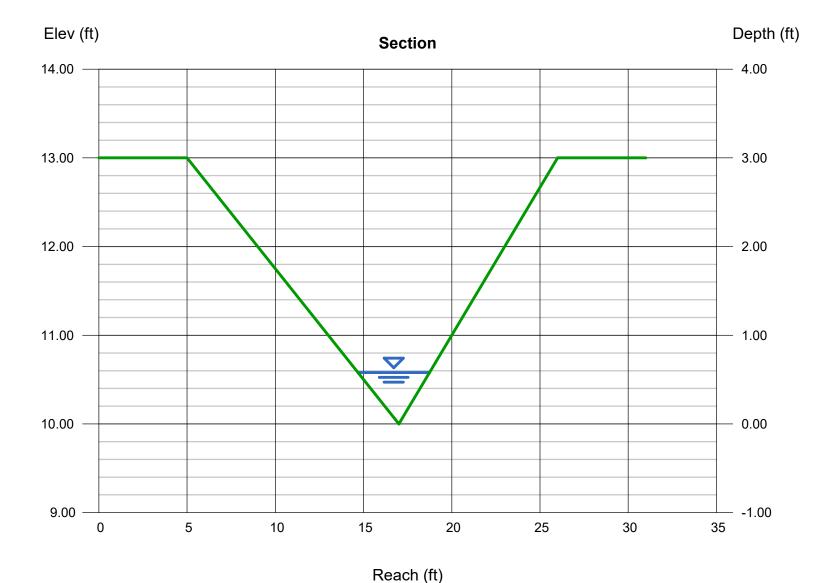
DP 2.0 Swale (5-Year)(FR:0.62)

Side Slopes (z:1) Total Depth (ft)	= 4.00, 3.00 = 3.00		
Invert Elev (ft)	= 10.00		
Slope (%)	= 1.74		

Calculations

N-Value

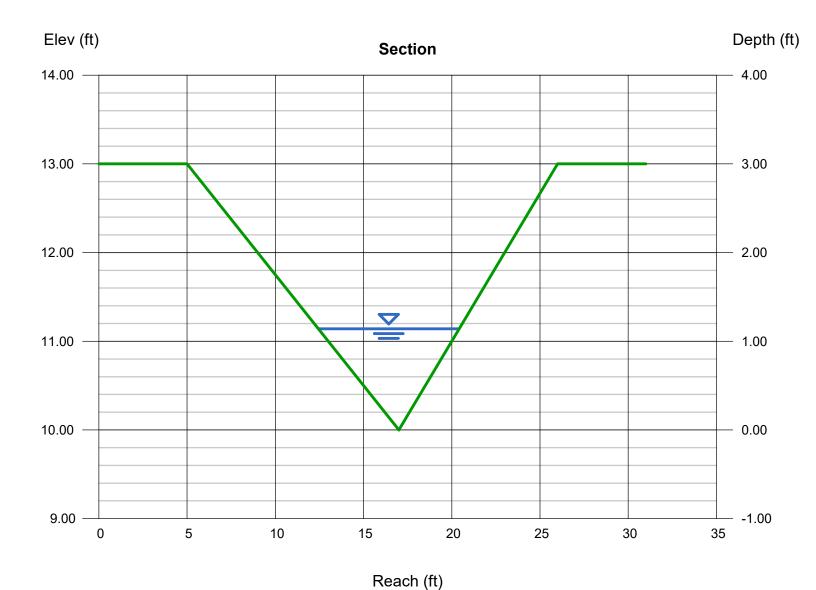
Compute by: Known Q Known Q (cfs) = 3.20 Highlighted Depth (ft) = 0.58Q (cfs) = 3.200Area (sqft) = 1.18 Velocity (ft/s) = 2.72Wetted Perim (ft) = 4.23Crit Depth, Yc (ft) = 0.56Top Width (ft) = 4.06EGL (ft) = 0.69



Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

DP 2.0 Swale (100-Year)(FR:0.71)

Triangular		Highlighted	
Side Slopes (z:1)	= 4.00, 3.00	Depth (ft)	= 1.14
Total Depth (ft)	= 3.00	Q (cfs)	= 19.60
		Area (sqft)	= 4.55
Invert Elev (ft)	= 10.00	Velocity (ft/s)	= 4.31
Slope (%)	= 1.74	Wetted Perim (ft) = 8.31
N-Value	= 0.030	Crit Depth, Yc (fi	t) = 1.15
		Top Width (ft)	= 7.98
Calculations		EĠL (ft)	= 1.43
Compute by:	Known Q	Drainage man shows a JR- Swale calcula	ation is
Known Q (cfs)	= 19.60	Drainage map shows a street slope of 1.0%	
, ,		flow conditions. T	·
		Please confirm swale Ct.) represents the	•
		section of swale the flow and Frou	
		highest.	iue # 15



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Wednesday, Apr 19 2023

DP 2.1 Swale (5-Year)(FR:0.51)

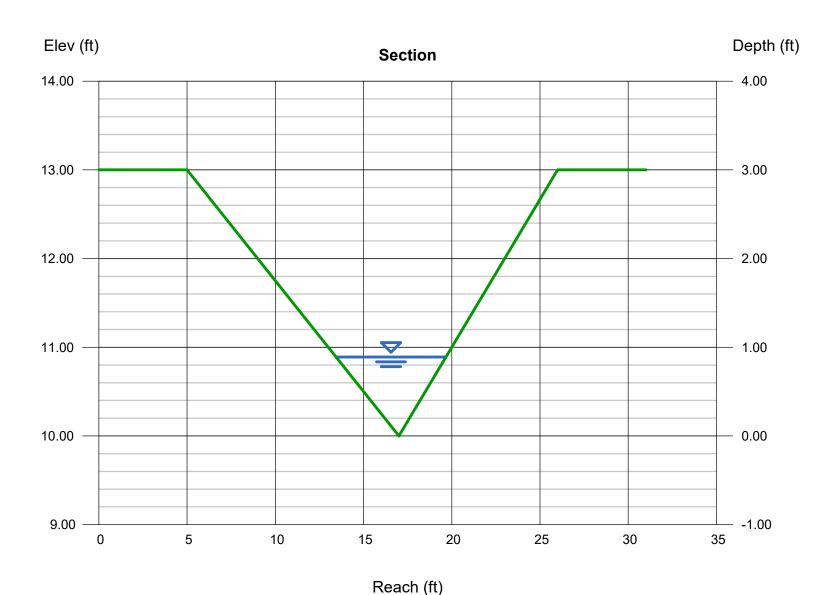
Triangular	
Side Slopes (z:1)	= 4.00, 3.00
Total Depth (ft)	= 3.00

Invert Elev (ft) = 10.00 Slope (%) = 1.00 N-Value = 0.030

Calculations

Compute by: Known Q Known Q (cfs) = 7.60

Highlighted		
Depth (ft)	=	0.89
Q (cfs)	=	7.600
Area (sqft)	=	2.77
Velocity (ft/s)	=	2.74
Wetted Perim (ft)	=	6.48
Crit Depth, Yc (ft)	=	0.79
Top Width (ft)	=	6.23
EGL (ft)	=	1.01



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Wednesday, Apr 19 2023

DP 2.1 Swale (100-Year)(FR:0.57)

T	r	ia	n	g	u	laı

Side Slopes (z:1) = 4.00, 3.00Total Depth (ft) = 3.00

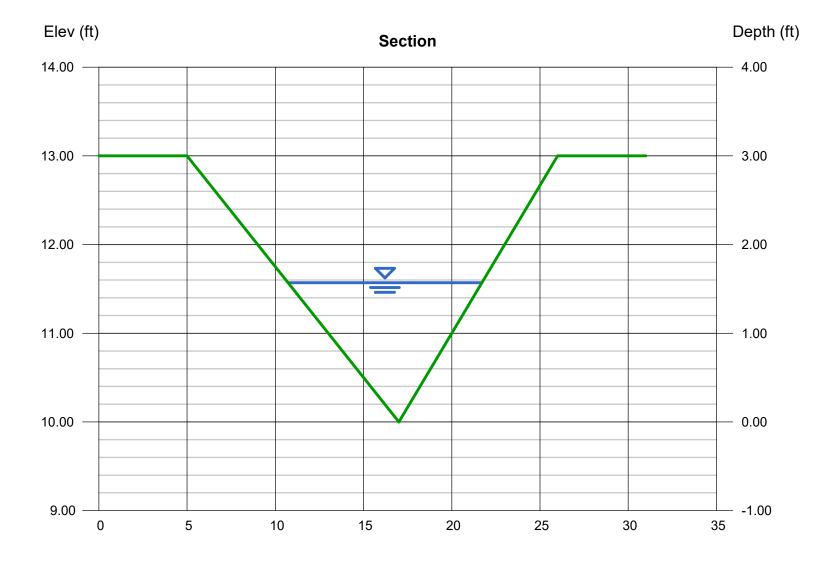
Invert Elev (ft) = 10.00 Slope (%) = 1.00 N-Value = 0.030

Calculations

Compute by: Known Q Known Q (cfs) = 35.00

Highlighted

Depth (ft) = 1.57 Q (cfs) = 35.00Area (sqft) = 8.63Velocity (ft/s) = 4.06 Wetted Perim (ft) = 11.44 Crit Depth, Yc (ft) = 1.45Top Width (ft) = 10.99EGL (ft) = 1.83



Reach (ft)

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Wednesday, Apr 19 2023

= 1.14

DP 2.2 Swale (5-Year)(FR:0.69)

Triangular	
Side Slopes (z:1)	= 4.00, 3.00
Total Depth (ft)	= 3.00

Invert Elev (ft) = 10.00 Slope (%) = 1.00 N-Value = 0.030

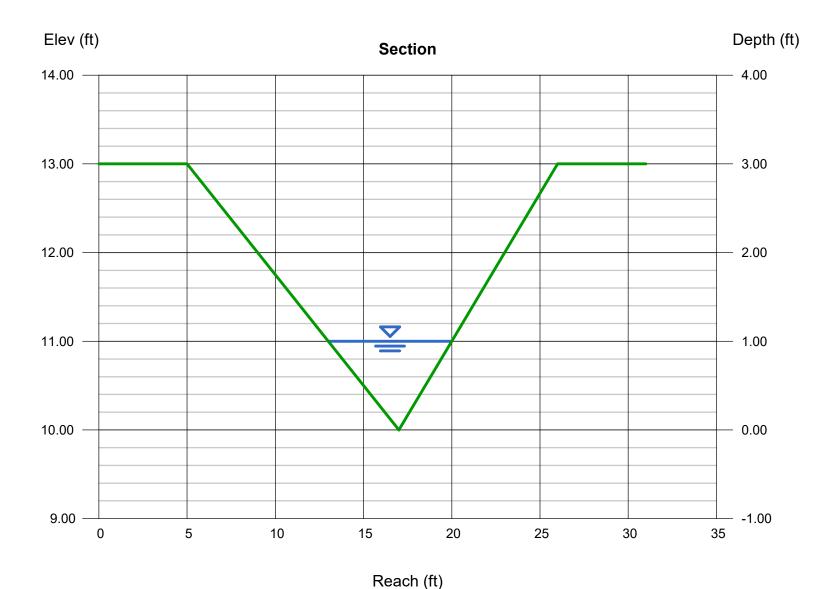
Calculations

Compute by: Known Q Known Q (cfs) = 10.50

rnginigitica	
Depth (ft)	= 1.00
Q (cfs)	= 10.50
Area (sqft)	= 3.50
Velocity (ft/s)	= 3.00
Wetted Perim (ft)	= 7.29
Crit Depth, Yc (ft)	= 0.90
Top Width (ft)	= 7.00

Highlighted

EGL (ft)

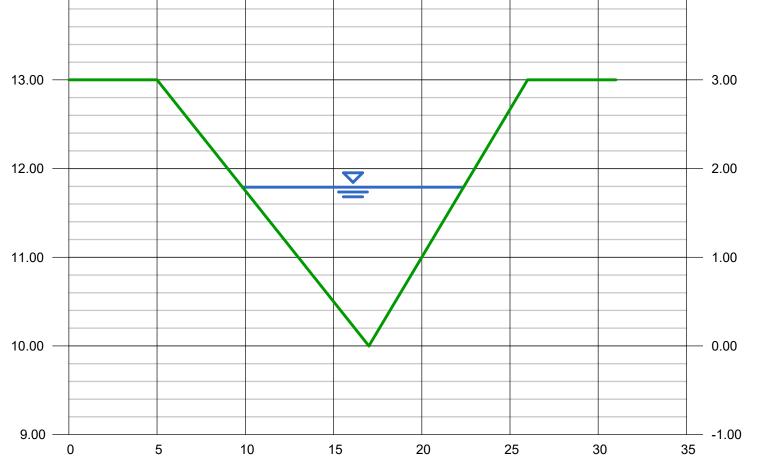


DP 2.2 Swale (100-Year)(FR:0.59)

Triangular Highlighted Side Slopes (z:1) = 4.00, 3.00Depth (ft) = 1.79Total Depth (ft) = 3.00Q (cfs) = 50.00Area (sqft) = 11.21Invert Elev (ft) Velocity (ft/s) = 10.00= 4.46Slope (%) Wetted Perim (ft) = 13.04= 1.00N-Value = 0.030Crit Depth, Yc (ft) = 1.67Top Width (ft) = 12.53EGL (ft) **Calculations** = 2.10Compute by: Known Q Drainage plan shows a Known Q (cfs) = 50.00street slope of 1.74%. Please confirm swale slope and revise as needed. JR- 1% represents the max flow condition near

Elev (ft)
Section
Depth (ft)
4.00

the outfall at DP2.2 along Mesilla Court. 1.74% is for Swale 2.0



Reach (ft)

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Wednesday, Apr 19 2023

DP 2.3 Swale (5-Year)(FR:0.70)

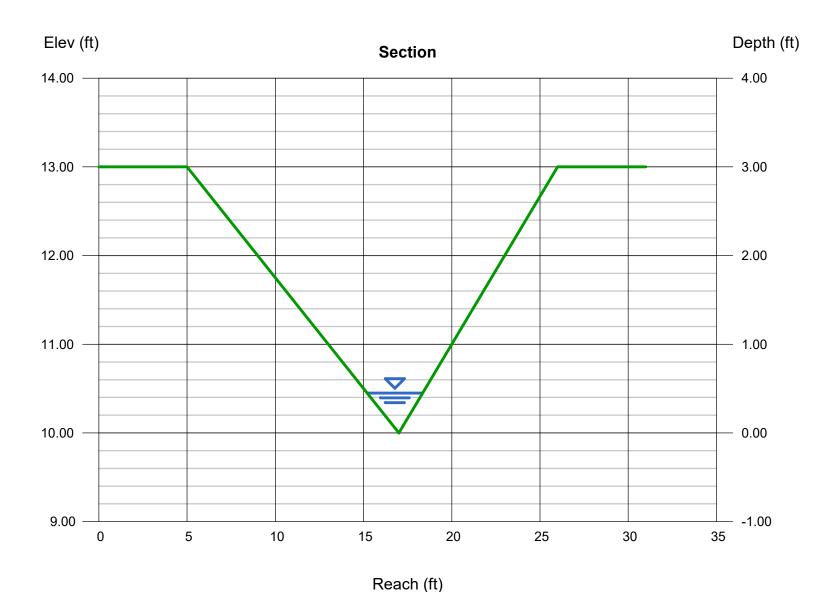
Triangular	
Side Slopes (z:1)	= 4.00, 3.00
Total Depth (ft)	= 3.00

Invert Elev (ft) = 10.00 Slope (%) = 2.33 N-Value = 0.030

Calculations

Compute by: Known Q Known Q (cfs) = 1.90

Highlighted	
Depth (ft)	= 0.45
Q (cfs)	= 1.900
Area (sqft)	= 0.71
Velocity (ft/s)	= 2.68
Wetted Perim (ft)	= 3.28
Crit Depth, Yc (ft)	= 0.45
Top Width (ft)	= 3.15
EGL (ft)	= 0.56



Known Q (cfs)

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= 7.00

DP 2.3 Swale (100-Year)(FR:0.77)

 Triangular

 Side Slopes (z:1)
 = 4.00, 3.00

 Total Depth (ft)
 = 3.00

 Invert Elev (ft)
 = 10.00

 Slope (%)
 = 2.33

 N-Value
 = 0.030

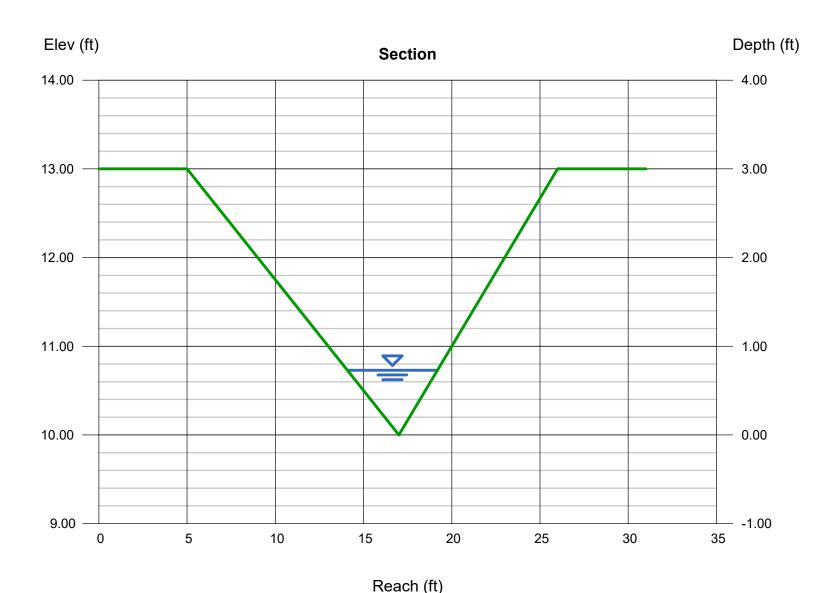
 Calculations

 Compute by:
 Known Q

Highlighted = 0.73Depth (ft) Q (cfs) = 7.000Area (sqft) = 1.87Velocity (ft/s) = 3.75Wetted Perim (ft) = 5.32Crit Depth, Yc (ft) = 0.76Top Width (ft) = 5.11EGL (ft) = 0.95

Drainage plan shows a street slope of 1.09%. Please confirm swale slope and revise as needed.

JR- 2.33% represents the max flow condition near the outfall at DP2.3 along Canelito PI.



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DP 3 Swale (5-Year)(FR:0.56)

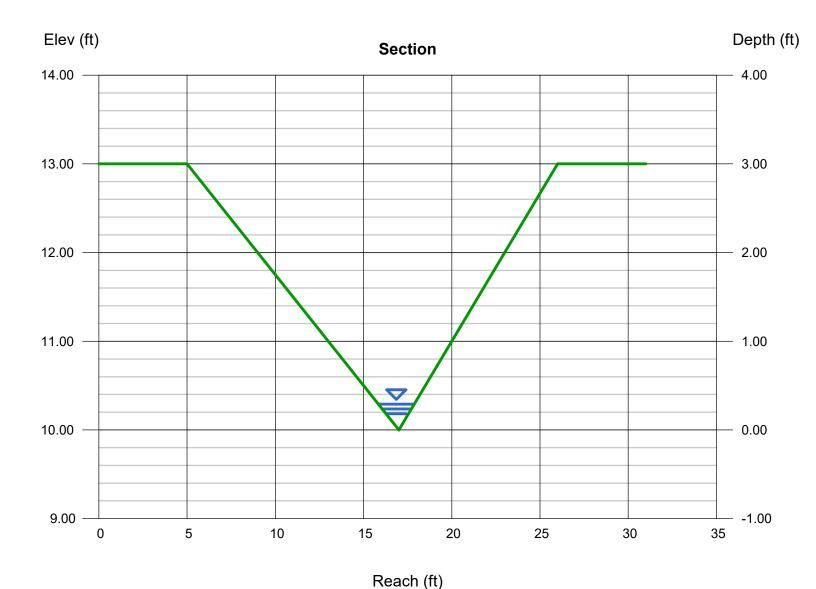
Triangular	
Side Slopes (z:1)	= 4.00, 3.00
Total Depth (ft)	= 3.00

Invert Elev (ft) = 10.00 Slope (%) = 1.94 N-Value = 0.030

Calculations

Compute by: Known Q Known Q (cfs) = 0.50

Highlighted		
Depth (ft)	=	0.29
Q (cfs)	=	0.500
Area (sqft)	=	0.29
Velocity (ft/s)	=	1.70
Wetted Perim (ft)	=	2.11
Crit Depth, Yc (ft)	=	0.27
Top Width (ft)	=	2.03
EGL (ft)	=	0.33



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Wednesday, Apr 19 2023

DP 3 Swale (100-Year)(FR:0.62)

Triangular
Side Slopes (z:1) = 4.00, 3.00
Total Depth (ft) = 3.00

Invert Elev (ft) = 10.00 Slope (%) = 1.94 N-Value = 0.030

Calculations

Elev (ft)

Compute by: Known Q Known Q (cfs) = 1.40

 Highlighted

 Depth (ft)
 = 0.42

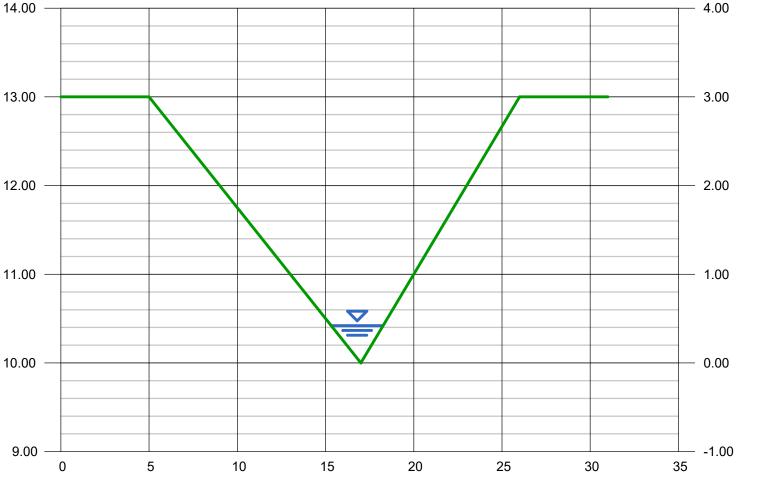
 Q (cfs)
 = 1.400

 Area (sqft)
 = 0.62

 Velocity (ft/s)
 = 2.27

Wetted Perim (ft) = 3.06Crit Depth, Yc (ft) = 0.40Top Width (ft) = 2.94EGL (ft) = 0.50

Depth (ft)



Section

Reach (ft)

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Friday, Jun 9 2023

DP 6 Swale (5-Year)(FR:0.56)

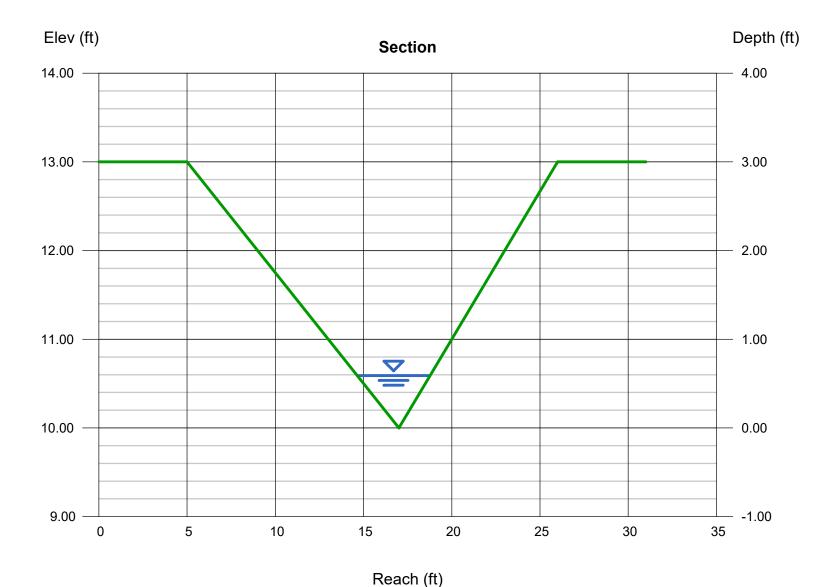
Side Slopes (z:1) Total Depth (ft)	= 4.00, 3.00 = 3.00
Invert Elev (ft)	= 10.00
Slope (%)	= 1.42

N-Value = 0.030

Calculations

Compute by: Known Q Known Q (cfs) = 3.00

Highlighted	
Depth (ft)	= 0.59
Q (cfs)	= 3.000
Area (sqft)	= 1.22
Velocity (ft/s)	= 2.46
Wetted Perim (ft)	= 4.30
Crit Depth, Yc (ft)	= 0.54
Top Width (ft)	= 4.13
EGL (ft)	= 0.68



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Friday, Jun 9 2023

DP 6 Swale (100-Year)(FR:0.64)

I	r	ia	n	g	Ju	laı	r

Side Slopes (z:1) = 4.00, 3.00Total Depth (ft) = 3.00

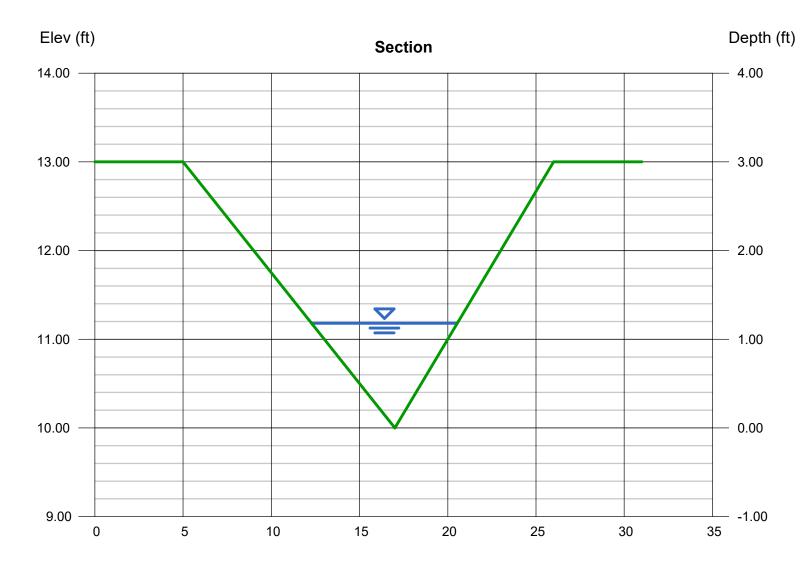
Invert Elev (ft) = 10.00 Slope (%) = 1.42 N-Value = 0.030

Calculations

Compute by: Known Q Known Q (cfs) = 19.30

Highlighted

Depth (ft) = 1.18 Q (cfs) = 19.30Area (sqft) = 4.87 Velocity (ft/s) = 3.96Wetted Perim (ft) = 8.60Crit Depth, Yc (ft) = 1.14 Top Width (ft) = 8.26 EGL (ft) = 1.42



Reach (ft)

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Friday, Jun 9 2023

DP 8 Swale (5-Year)(FR:0.54)

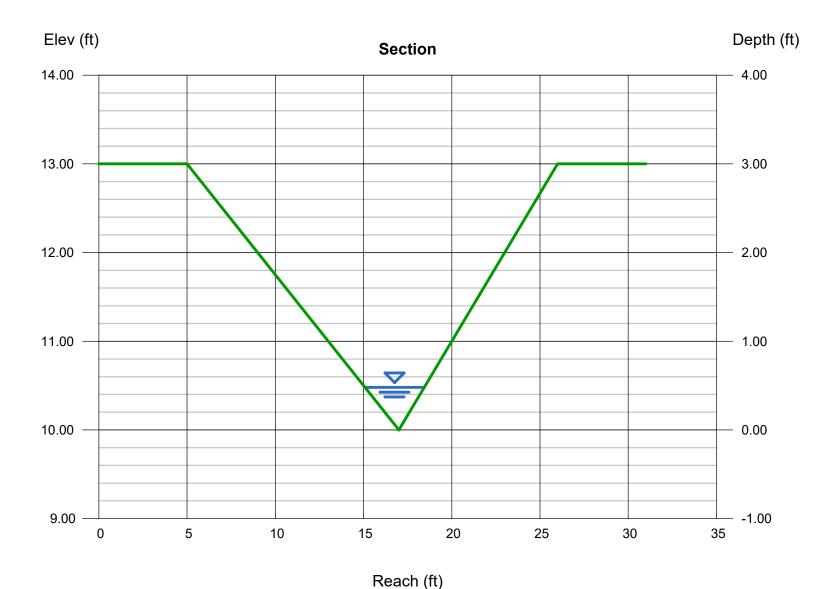
Triangular Side Slopes (z:1) Total Depth (ft)	= 4.00, 3.00 = 3.00
Invert Floy (ft)	- 10.00

Invert Elev (ft) = 10.00 Slope (%) = 1.42 N-Value = 0.030

Calculations

Compute by: Known Q Known Q (cfs) = 1.70

Highlighted		
Depth (ft)	=	0.48
Q (cfs)	=	1.700
Area (sqft)	=	0.81
Velocity (ft/s)	=	2.11
Wetted Perim (ft)	=	3.50
Crit Depth, Yc (ft)	=	0.43
Top Width (ft)	=	3.36
EGL (ft)	=	0.55



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Friday, Jun 9 2023

DP 8 Swale (100-Year)(FR:0.61)

ı	r	ıa	ngu	ııar
_				

Side Slopes (z:1) = 4.00, 3.00Total Depth (ft) = 3.00

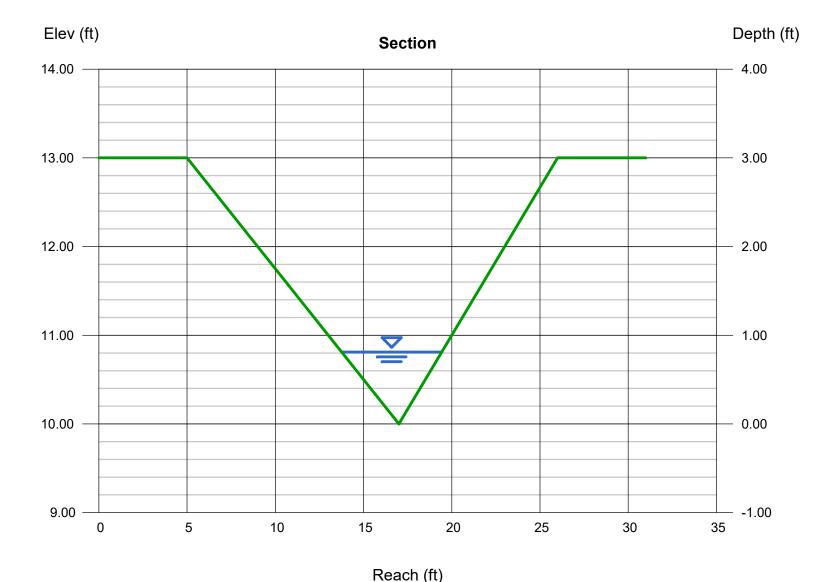
Invert Elev (ft) = 10.00 Slope (%) = 1.42 N-Value = 0.030

Calculations

Compute by: Known Q Known Q (cfs) = 7.20

Highlighted

Depth (ft) = 0.81Q (cfs) = 7.200Area (sqft) = 2.30Velocity (ft/s) = 3.14Wetted Perim (ft) = 5.90Crit Depth, Yc (ft) = 0.77Top Width (ft) = 5.67EGL (ft) = 0.96



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Wednesday, Apr 19 2023

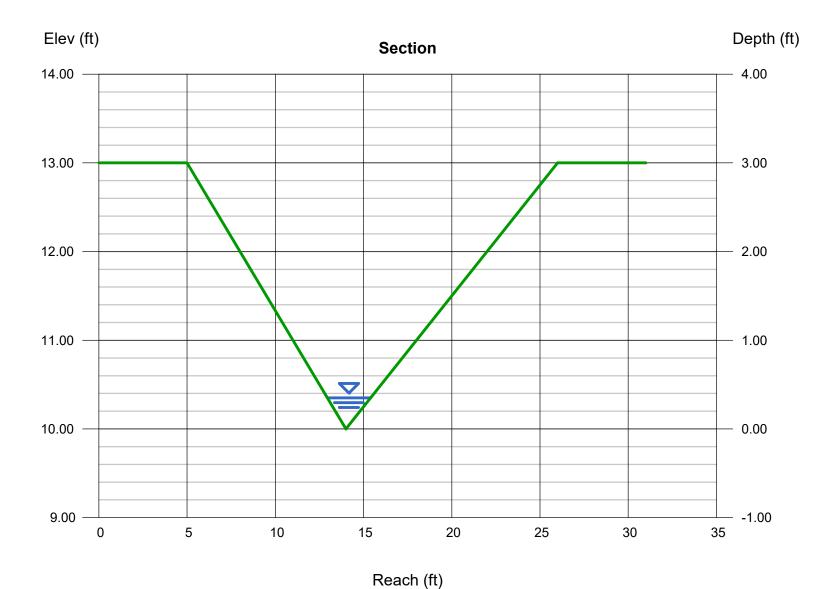
DP 13 Swale (5-Year)(FR:0.42)

Triangular Side Slopes (z:1) Total Depth (ft)	= 3.00, 4.00 = 3.00
Invert Elev (ft)	= 10.00
Slope (%)	= 1.00
N-Value	= 0.030

Calculations

Compute by: Known Q Known Q (cfs) = 0.60

Highlighted	
Depth (ft)	= 0.35
Q (cfs)	= 0.600
Area (sqft)	= 0.43
Velocity (ft/s)	= 1.40
Wetted Perim (ft)	= 2.55
Crit Depth, Yc (ft)	= 0.29
Top Width (ft)	= 2.45
EGL (ft)	= 0.38



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Wednesday, Apr 19 2023

DP 13 Swale (100-Year)(FR:0.47)

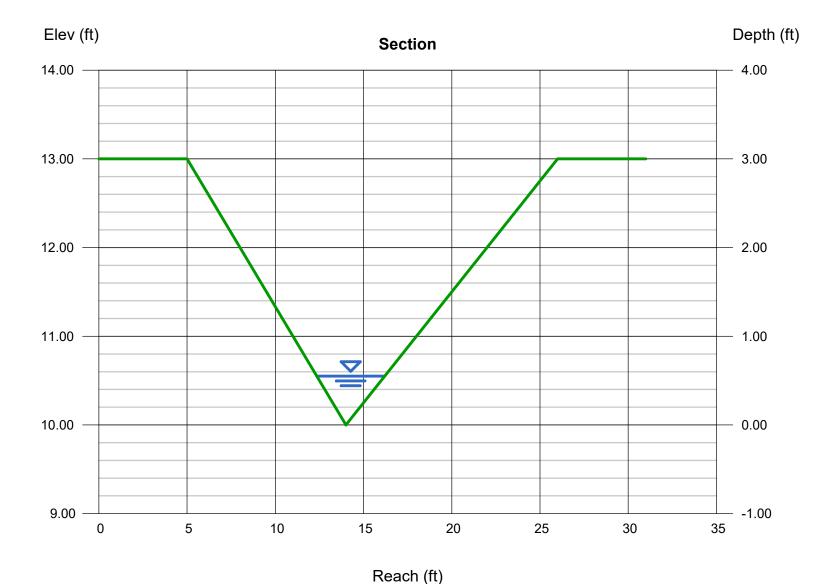
ırıangular	
Side Slopes (z:1)	= 3.00, 4.00
Total Depth (ft)	= 3.00

Invert Elev (ft) = 10.00 Slope (%) = 1.00 N-Value = 0.030

Calculations

Compute by: Known Q Known Q (cfs) = 2.10

Highlighted	
Depth (ft)	= 0.55
Q (cfs)	= 2.100
Area (sqft)	= 1.06
Velocity (ft/s)	= 1.98
Wetted Perim (ft)	= 4.01
Crit Depth, Yc (ft)	= 0.47
Top Width (ft)	= 3.85
EGL (ft)	= 0.61



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Wednesday, Apr 19 2023

DP 16 Swale (5-Year)(FR:0.48)

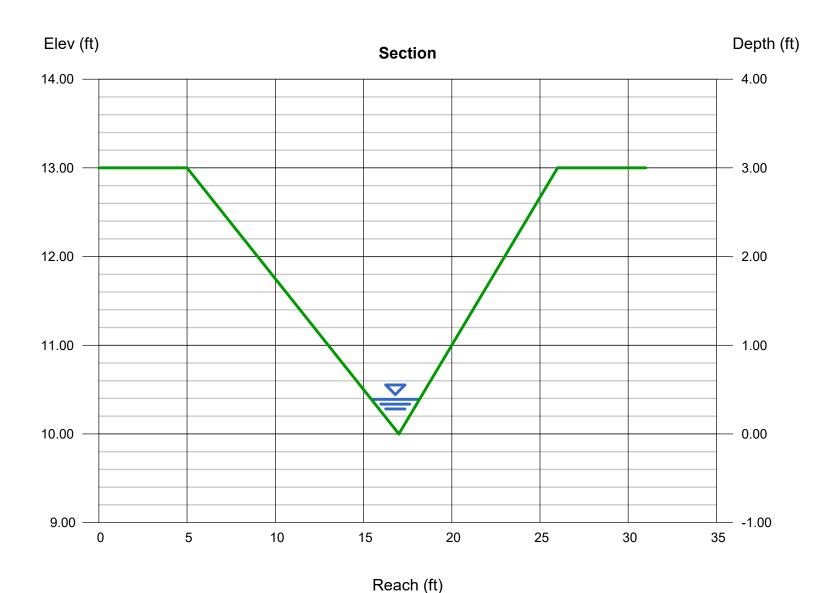
ırıangular	
Side Slopes (z:1)	= 4.00, 3.00
Total Depth (ft)	= 3.00
Invert Fley (ft)	= 10.00

Invert Elev (ft) = 10.00 Slope (%) = 1.09 N-Value = 0.030

Calculations

Compute by: Known Q Known Q (cfs) = 0.90

Highlighted		
Depth (ft)	=	0.39
Q (cfs)	=	0.900
Area (sqft)	=	0.53
Velocity (ft/s)	=	1.69
Wetted Perim (ft)	=	2.84
Crit Depth, Yc (ft)	=	0.34
Top Width (ft)	=	2.73
EGL (ft)	=	0.43



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Wednesday, Apr 19 2023

DP 16 Swale (100-Year)(FR:0.51)

Triangular	
Side Slopes (z:1)	

= 4.00, 3.00

Total Depth (ft)

= 3.00

Invert Elev (ft) Slope (%) N-Value

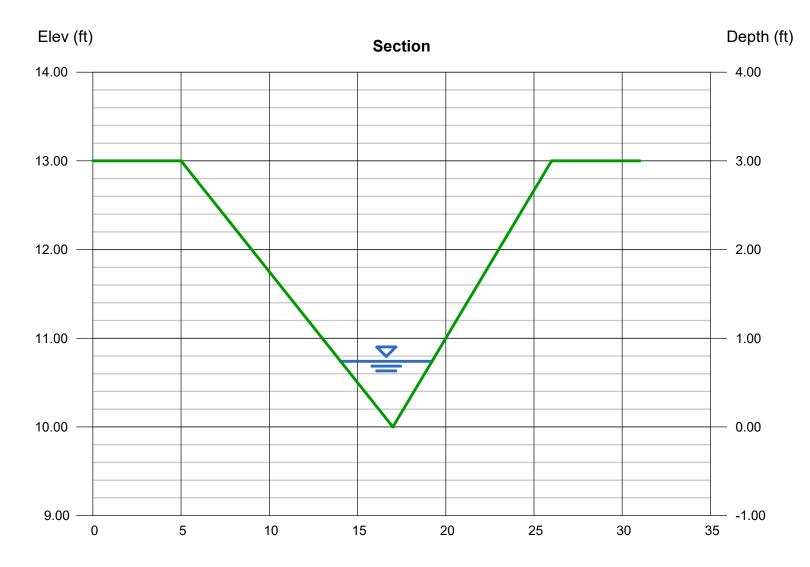
= 10.00= 1.09= 0.030

Calculations

Compute by: Known Q Known Q (cfs) = 4.80

Highlighted

Depth (ft) = 0.74Q (cfs) = 4.800Area (sqft) = 1.92Velocity (ft/s) = 2.50Wetted Perim (ft) = 5.39Crit Depth, Yc (ft) = 0.66Top Width (ft) = 5.18EGL (ft) = 0.84



Reach (ft)

PIPE OUTFALL RIPRAP SIZING CALCULATIONS

Subdivision: Saddlehorn Ranch Filing 4
Location: El Paso County

 Project Name:
 Saddlehorn Ranch

 Project No.:
 25142.06

 Calculated By:
 AAM

 Checked By:
 TBD

 Date:
 3/1/22

	STORM DRAIN SYSTEM			
	DESIGN POINT 1	DESIGN POINT 6	DESIGN POINT 8	Notes
Q ₁₀₀ (cfs):	10.3	19.3	7.2	Flows are the greater of proposed vs. future
Conduit	Pipe	Pipe	Pipe	
D_c , Pipe Diameter (in):	30	30	24	
W, Box Width (ft):	N/A	N/A	N/A	
H, Box Height (ft):	N/A	N/A	N/A	
Y_t , Tailwater Depth (ft):	1.95	1.95	1.55	If unknown, use Y_t/D_c (or H)=0.4
Y_t/Dc or Y_t/H	0.78	0.78	0.78	
Q/D ^{2.5} or Q/(WH ^{3/2})	1.04	1.95	1.27	
Supercritical?	No	No	No	
Y_n , Normal Depth (ft) [Supercritical]:	0.00	0.00	0.00	
D_a , H_a (in) [Supercritical]:	N/A	N/A	N/A	$D_a = (D_c + Y_n)/2$
Riprap d_{50} (in) [Supercritical]:	N/A	N/A	N/A	
Riprap d_{50} (in) [Subcritical]:	0.97	1.82	0.95	
Required Riprap Size:	L	L	L	Fig. 9-38 or Fig. 9-36
d ₅₀ (in):	9	9	9	
Expansion Factor, $1/(2 \tan \theta)$:	6.75	6.75	6.75	Read from Fig. 9-35 or 9-36
θ :	0.07	0.07	0.07	
Erosive Soils?	No	No	No	
Area of Flow, A_t (ft ²):	1.47	2.76	1.03	$A_t = Q/V$
Length of Protection, L_p (ft):	-11.8	-7.3	-9.0	$L=(1/(2 \tan \theta))(At/Yt - D)$
Min Length (ft)	7.5	7.5	6.0	Min L=3D or 3H
Max Length (ft)	25.0	25.0	20.0	Max L=10D or 10H
Min Bottom Width, T (ft):	0.8	1.4	0.7	$T=2*(L_p*tan\theta)+W$
Design Length (ft)	7.5	7.5	6.0	
Design Width (ft)	0.8	1.4	0.7	
Riprap Depth (in)	18	18	18	Depth=2(d ₅₀)
Type II Bedding Depth (in)*	6	6	6	*Not used if Soil Riprap
Cutoff Wall	No	No	No	
Cutoff Wall Depth (ft)				Depth of Riprap and Base
Cutoff Wall Width (ft)				

Note: No Type II Base to be used if Soil Riprap is specified within the plans

Add culvert name from plans to this table as well so it is easy to verify all culverts shown on the plans are located here. The plans show 7 culvert profiles, but there are only 5 in these tables. Verify all culverts are in this appendix.

JR- Culvert names added. Riprap calcs for Judge Orr culverts added.

^{*} For use when the flow in the culvert is supercritical (and less than full).

PIPE OUTFALL RIPRAP SIZING CALCULATIONS

Subdivision: Saddlehorn Ranch Filing 4
Location: El Paso County

 Project Name:
 Saddlehorn Ranch

 Project No.:
 25142.06

 Calculated By:
 AAM

 Checked By:
 TBD

 Date:
 3/1/22

	STORM DRAIN SYSTEM			
	DESIGN POINT 13	DESIGN POINT 16	DESIGN POINT	Notes
Q ₁₀₀ (cfs):	2.1	4.8		Flows are the greater of proposed vs. future
Conduit	Pipe	Pipe		
D_c , Pipe Diameter (in):	18	18		
W, Box Width (ft):	N/A	N/A		
H , Box Height (ft):	N/A	N/A		
Y_t , Tailwater Depth (ft):	1.05	1.20		If unknown, use Y_t/D_c (or H)=0.4
Y_t/Dc or Y_t/H	0.70	0.80		
$Q/D^{2.5}$ or $Q/(WH^{3/2})$	0.76	1.74		
Supercritical?	No	No		
Y_n , Normal Depth (ft) [Supercritical]:	0.00	0.00		
D_a , H_a (in) [Supercritical]:	N/A	N/A		$D_a = (D_c + Y_n)/2$
Riprap d_{50} (in) [Supercritical]:	N/A	N/A		
Riprap d_{50} (in) [Subcritical]:	0.48	0.94		
Required Riprap Size:	L	L		Fig. 9-38 or Fig. 9-36
d ₅₀ (in):	9	9		
Expansion Factor, $1/(2 \tan \theta)$:	6.75	6.75		Read from Fig. 9-35 or 9-36
θ :	0.07	0.07		
Erosive Soils?	No	No		
Area of Flow, A_t (ft ²):	0.30	0.69		$A_t = Q/V$
Length of Protection, L_p (ft):	-8.2	-6.3		L=(1/(2 tan θ))(At/Yt - D)
Min Length (ft)	4.5	4.5		Min L=3D or 3H
Max Length (ft)	15.0	15.0		Max L=10D or 10H
Min Bottom Width, \mathcal{T} (ft):	0.3	0.6		$T=2*(L_p*tan\theta)+W$
Design Length (ft)	4.5	4.5		
Design Width (ft)	0.3	0.6		
Riprap Depth (in)	18	18		Depth=2(d ₅₀)
Type II Bedding Depth (in)*	6	6		*Not used if Soil Riprap
Cutoff Wall	No	No		
Cutoff Wall Depth (ft)				Depth of Riprap and Base
Cutoff Wall Width (ft)				

Note: No Type II Base to be used if Soil Riprap is specified within the plans

^{*} For use when the flow in the culvert is supercritical (and less than full).

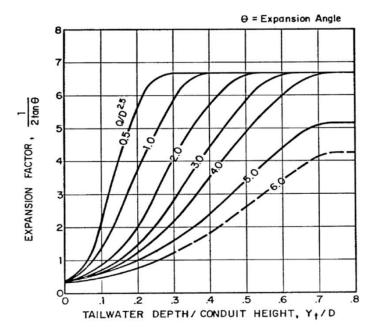


Figure 9-35. Expansion factor for circular conduits

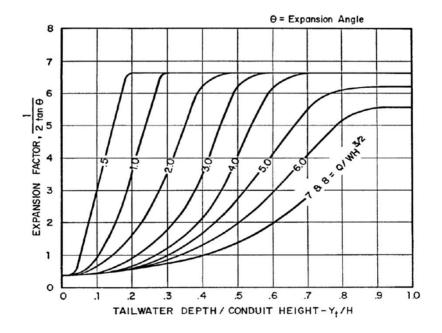


Figure 9-36. Expansion factor for rectangular conduits

APPENDIX D WATER QUALITY AND DETENTION CALCULATIONS

POND C FOREBAY VOLUME REQUIREMENTS

Equation 3-1 $WQCV = a(0.91I^3 - 1.19I^2 + 0.781I)$ a=1 (40 hour drain time)

PROPOSED FOREBAY I=.211 WQCV= 0.120148

Equation 3-3 V=(WQCV/12)A

PROPOSED FOREBAY A= 5.30 Acres V= 0.053

3% OF WQCV

FOREBAY TOTAL VOLUME= .03(V)

VOLUME REQUIRED FOR PROPOSED FOREBAY = 0.002 AC-FT 69 CF

VOLUME PROVIDED FOR PROPOSED FOREBAY = 0.005 AC-FT 210 CF

 Q_{100} DISCHARGES 2% OF Q_{100}

Q₁₀₀ PROPOSED FOREBAY= .02*7.0 CFS= 0.14 CFS

Weir Report

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Wednesday, Mar 2 2022

Pond C Forebay 1 Notch

V-Notch Weir	
Crest	= Sharp
Angle (Deg)	= 10
Total Depth (ft)	= 2.50

Calculations

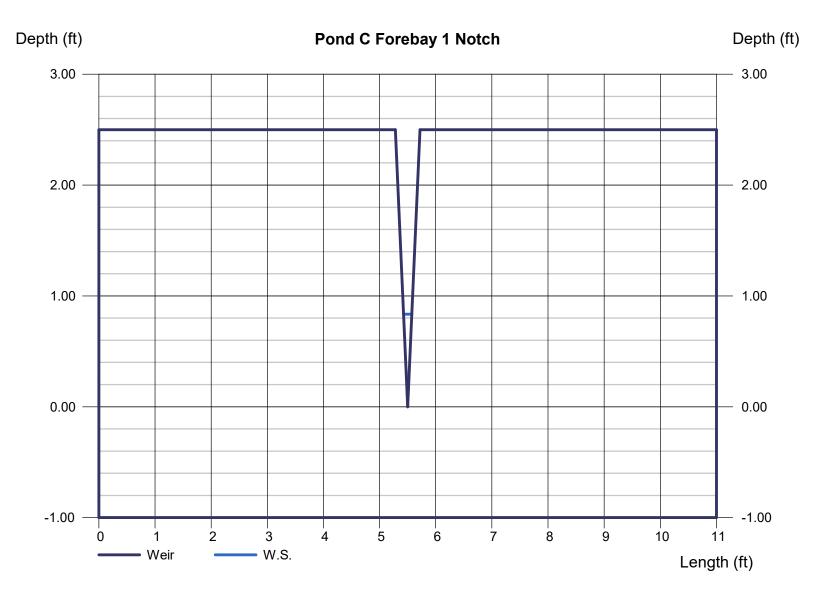
Weir Coeff. Cw = 0.22 Compute by: Known Q Known Q (cfs) = 0.14

 Highlighted

 Depth (ft)
 = 0.83

 Q (cfs)
 = 0.140

Area (sqft) = 0.06 Velocity (ft/s) = 2.30 Top Width (ft) = 0.15



POND D FOREBAY VOLUME REQUIREMENTS

WQCV= $a(0.91I^3-1.19I^2+0.781I)$ a=1 (40 hour drain time) Equation 3-1

Proposed Forebay I=.167 WQCV= 0.10131

Equation 3-3

V=(WQCV/12)A

Proposed Forebay A= 25.94 Acres 0.219

3% OF WQCV

FOREBAY TOTAL VOLUME= .03(V)

VOLUME REQUIRED FOR PROPOSED FOREBAY= 0.007 AC-FT 286 CF

VOLUME PROVIDED FOR PROPOSED FOREBAY = 0.014 AC-FT 615 CF

Q₁₀₀ Discharges 2% OF Q₁₀₀

Q₁₀₀ Proposed Forebay 1= .02*28.7 CFS= .57 CFS

Weir Report

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Wednesday, Mar 2 2022

Pond D Forebay 1 Notch

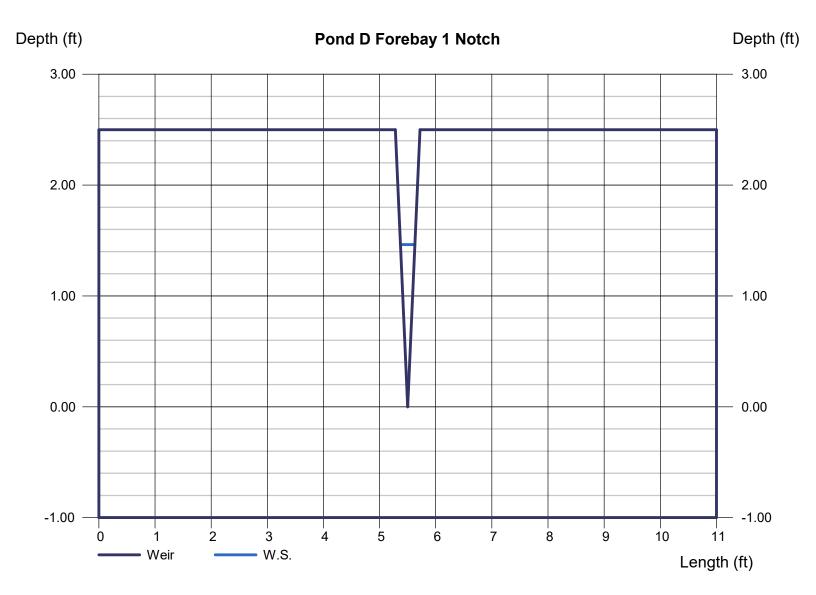
V-Notch Weir	
Crest	= Sharp
Angle (Deg)	= 10
Total Depth (ft)	= 2.50

Calculations

Weir Coeff. Cw = 0.22Compute by: Known Q Known Q (cfs) = 0.57

Highlighted Depth (ft)

= 1.46Q (cfs) = 0.570Area (sqft) = 0.19Velocity (ft/s) = 3.04Top Width (ft) = 0.26



APPENDIX E REFERENCE MATERIALS



Federal Emergency Management Agency

Washington, D.C. 20472

LETTER OF MAP REVISION **DETERMINATION DOCUMENT (CONTINUED)**

PUBLIC NOTIFICATION OF REVISION

Within 90 days of the second publication in the local newspaper, a citizen may request that we reconsider this determination. Any request for reconsideration must be based on scientific or technical data. Therefore, this letter will be effective only after the 90-day appeal period has elapsed and we have resolved any appeals that we receive during this appeal period. Until this LOMR is effective, the revised BFEs presented in this LOMR may be changed.

A notice of changes will be published in the Federal Register. This information also will be published in your local newspaper on or about the dates listed below.

LOCAL NEWSPAPER

Name: El Paso County News

Dates: 11/10/2004

11/17/2004

PUBLIC NOTIFICATION

		BFE (FEE	MAP PANEL	
FLOODING SOURCE	LOCATION OF REFERENCED ELEVATION	EFFECTIVE	REVISED	NUMBER(\$)
Haegler Ranch Tributary 2	Approximately 310 feet upstream of confluence with Geick Ranch West Tributary	None	6,735	08041C0575 F
	Approximately 3,140 feet upstream of confluence with Geick Ranch West Tributary	None	6,779	08041C0575 F
Haegler Ranch Tributary 3	Approximately 8,100 feet downstream of Curtis Road	None	6,672	08041C0575 F
	Approximately 300 feet upstream of Curtis Road	None	6,769	08041C0575 F
Haegler Ranch Tributary 4	Approximately 4,000 feet downstream of Curtis Road	None	6,688	08041C0575 F
	Approximately 300 feet upstream of Curtis Road	None	6,758	08041C0575 F

This determination is based on the flood data presently available. The enclosed documents provide additional information regarding this determination. If you have any questions about this document, please contact the FEMA Map Assistance Center toll free at 1-877-336-2677 (1-877-FEMA MAP) or by letter addressed to the LOMR Depot, 3601 Eisenhower Avenue, Alexandria, VA 22304. Additional information about the NFIP is available on our website at http://www.fema.gov/nfip.

Kevin C Jong

Kevin C. Long, CFM, Project Engineer Hagard Identification Section

Mitigation Division

Emergency Preparedness and Response Directorate 102929 101104080587 102IAC

CHANGES ARE MADE IN DETERMINATIONS OF BASE FLOOD ELEVATIONS FOR THE UNINCORPORATED AREAS OF EL PASO COUNTY, COLORADO, UNDER THE NATIONAL FLOOD INSURANCE PROGRAM

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On March 17, 1997, the Department of Homeland Security's Federal Emergency Management Agency identified Special Flood Hazard Areas (SFHAs) in the unincorporated areas of El Paso County, Colorado, through issuance of a Flood Insurance Rate Map (FIRM). The Mitigation Division has determined that modification of the elevations of the flood having a 1-percent chance of being equaled or exceeded in any given year (base flood) for certain locations in this community is appropriate. The modified Base Flood Elevations (BFEs) revise the FIRM for the community.

The changes are being made pursuant to Section 206 of the Flood Disaster Protection Act of 1973 (Public Law 93-234) and are in accordance with the National Flood Insurance Act of 1968, as amended (Title XIII of the Housing and Urban Development Act of 1968, Public Law 90-448), 42 U.S.C. 4001-4128, and 44 CFR Part 65.

A hydraulic analysis was performed to incorporate new hydrologic, hydraulic, and topographic data for Haegler Ranch Tributary 2 from approximately 310 feet upstream to approximately 3,140 feet upstream of the confluence with Geick Ranch West Tributary; for Haegler Ranch Tributary 3 from approximately 8,100 feet downstream to approximately 400 feet upstream of Curtis Road; and for Haegler Ranch Tributary 4 from approximately 4,100 feet downstream to approximately 400 feet upstream of Curtis Road. This has resulted in increases and decreases in SFHA width and increased BFEs for the above-mentioned tributaries. The table below indicates existing and modified BFEs for selected locations along the affected lengths of the flooding source(s) cited above.

Location	Existing BFE (feet)*	'Modified BFE (feet)*
Haegler Ranch Tributary 2:		
Approximately 310 feet upstream of confluence with		
Geick Ranch West Tributary	None	6,735
Approximately 3,140 feet upstream of confluence with		
Geick Ranch West Tributary	None	6,779
Haegler Ranch Tributary 3:		
Approximately 8,100 feet downstream of Curtis Road	None	6,672
Approximately 300 feet upstream of Curtis Road	None	6,769
Haegler Ranch Tributary 4:	•	
Approximately 4,000 feet downstream of Curtis Road	None	6,688
Approximately 300 feet upstream of Curtis Road	None	6,758

^{*}National Geodetic Vertical Datum, rounded to nearest whole foot

Under the above-mentioned Acts of 1968 and 1973, the Mitigation Division must develop criteria for floodplain management. To participate in the National Flood Insurance Program (NFIP), the community must use the modified BFEs to administer the floodplain management measures of the NFIP. These modified BFEs will also be used to calculate the appropriate flood insurance premium rates for new buildings and their contents and for the second layer of insurance on existing buildings and contents.

Upon the second publication of notice of these changes in this newspaper, any person has 90 days in which he or she can request, through the Chief Executive Officer of the community, that the Mitigation Division reconsider the determination. Any request for reconsideration must be based on knowledge of changed conditions or new scientific or technical data. All interested parties are on notice that until the 90-day period elapses, the Mitigation Division's determination to modify the BFEs may itself be changed.

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Any person having knowledge or wishing to comment on these changes should immediately notify:

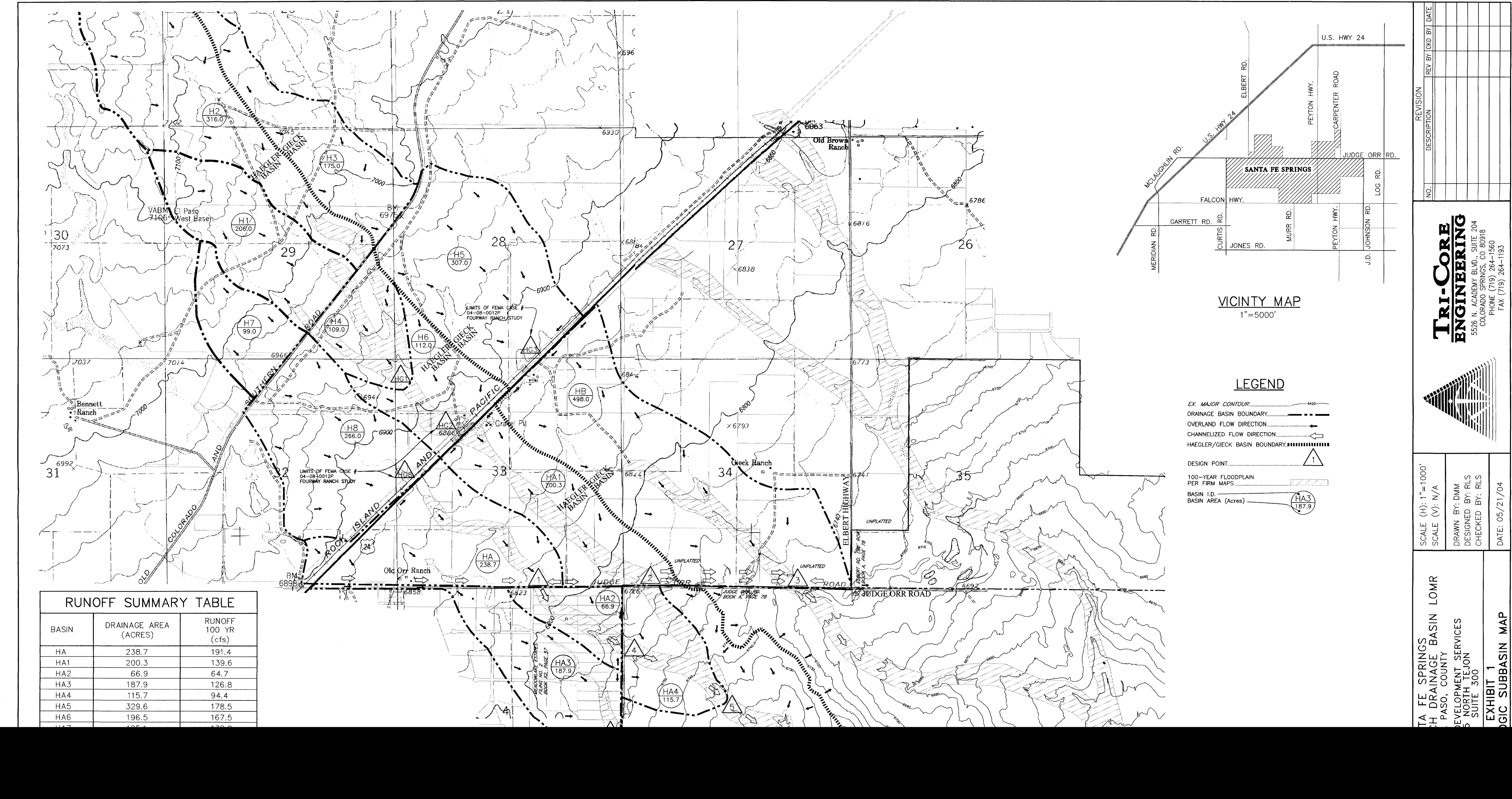
The Honorable Chuck Brown
Chairman, El Paso County
Board of Commissioners
27 Vermijo Avenue
Colorado Springs, CO 80903-2208

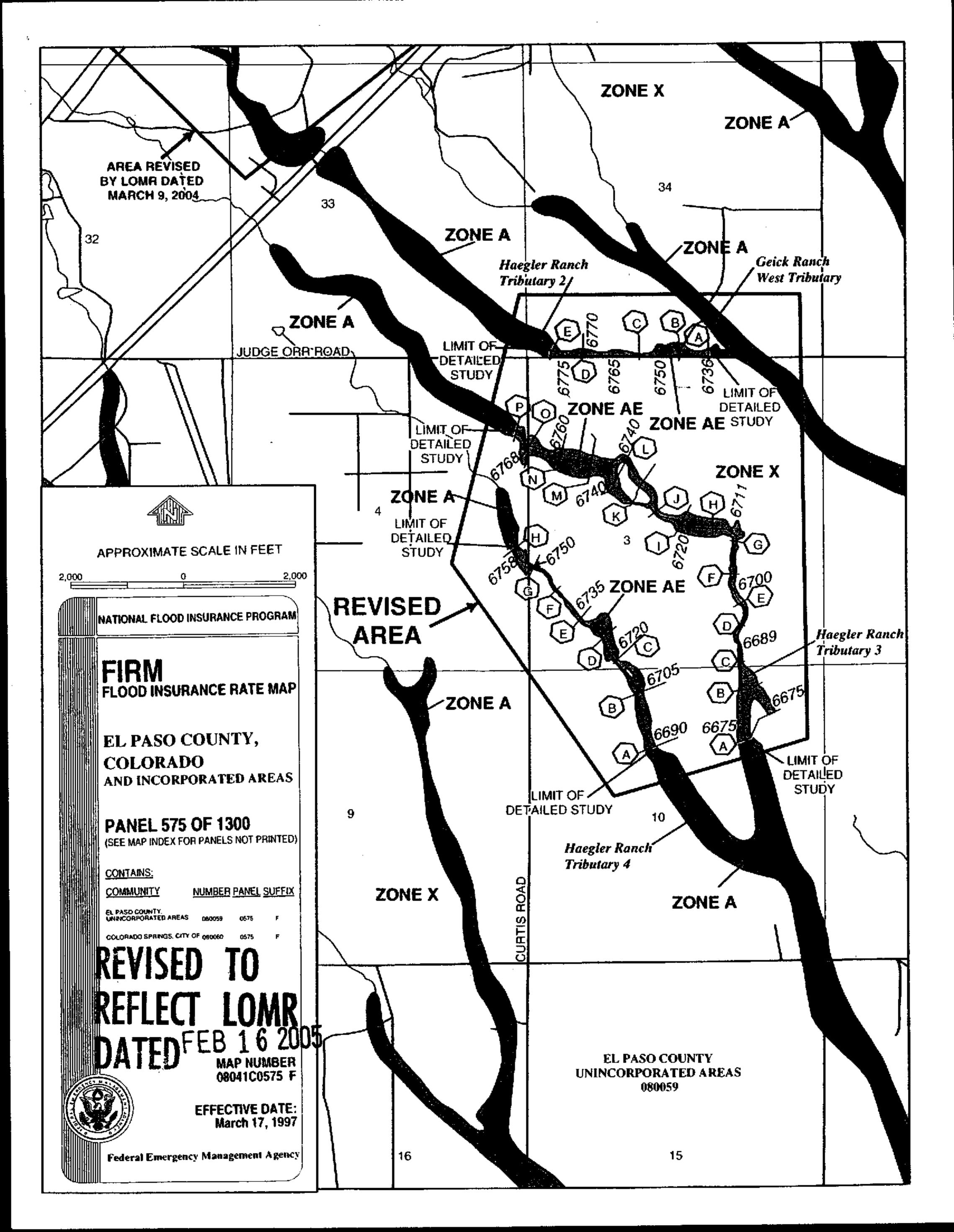
Table 3. Summary of Discharges

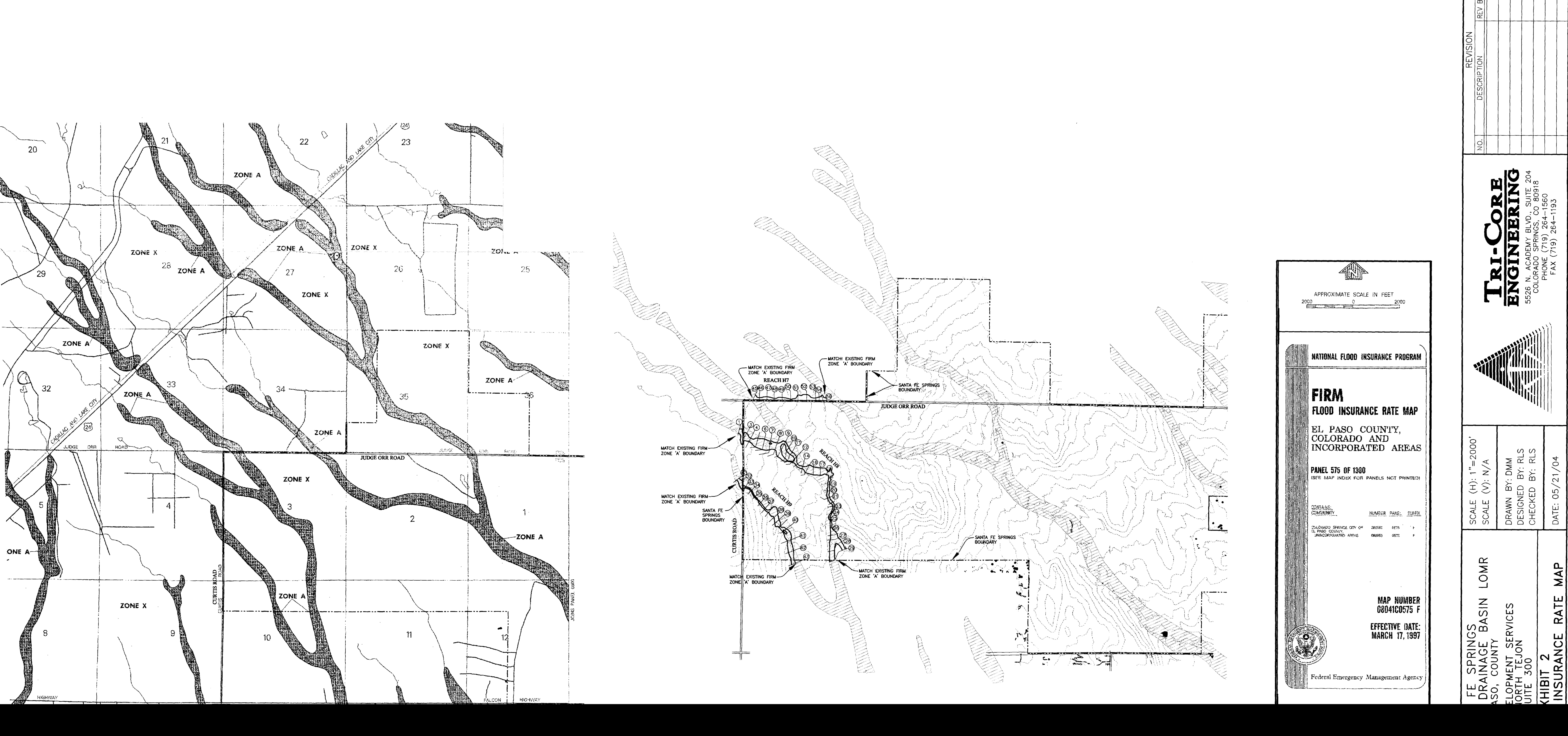
	Drainage Area	Pea	Peak Discharges (cubic feet per second)			
Flooding Source and Location	(square miles)	10-Year	50-Year	100-Year	500-Year	
Haegler Ranch Tributary 2 At the confluence with Geick						
Ranch West Tributary	1.47	1	1	592	11	
Haegler Ranch Tributary 3 At approximately 2,300 feet upstream of the confluence with Haegler Ranch Tributary 4	1.09	1	1	505	1	
Haegler Ranch Tributary 4 At approximately 3,700 feet upstream of the confluence with Haegler Ranch Tributary 3	0.60	1	1	130	1	

1 Data Not Available

REVISED TO REFLECT LOMR DATED FEB 1 6 2005

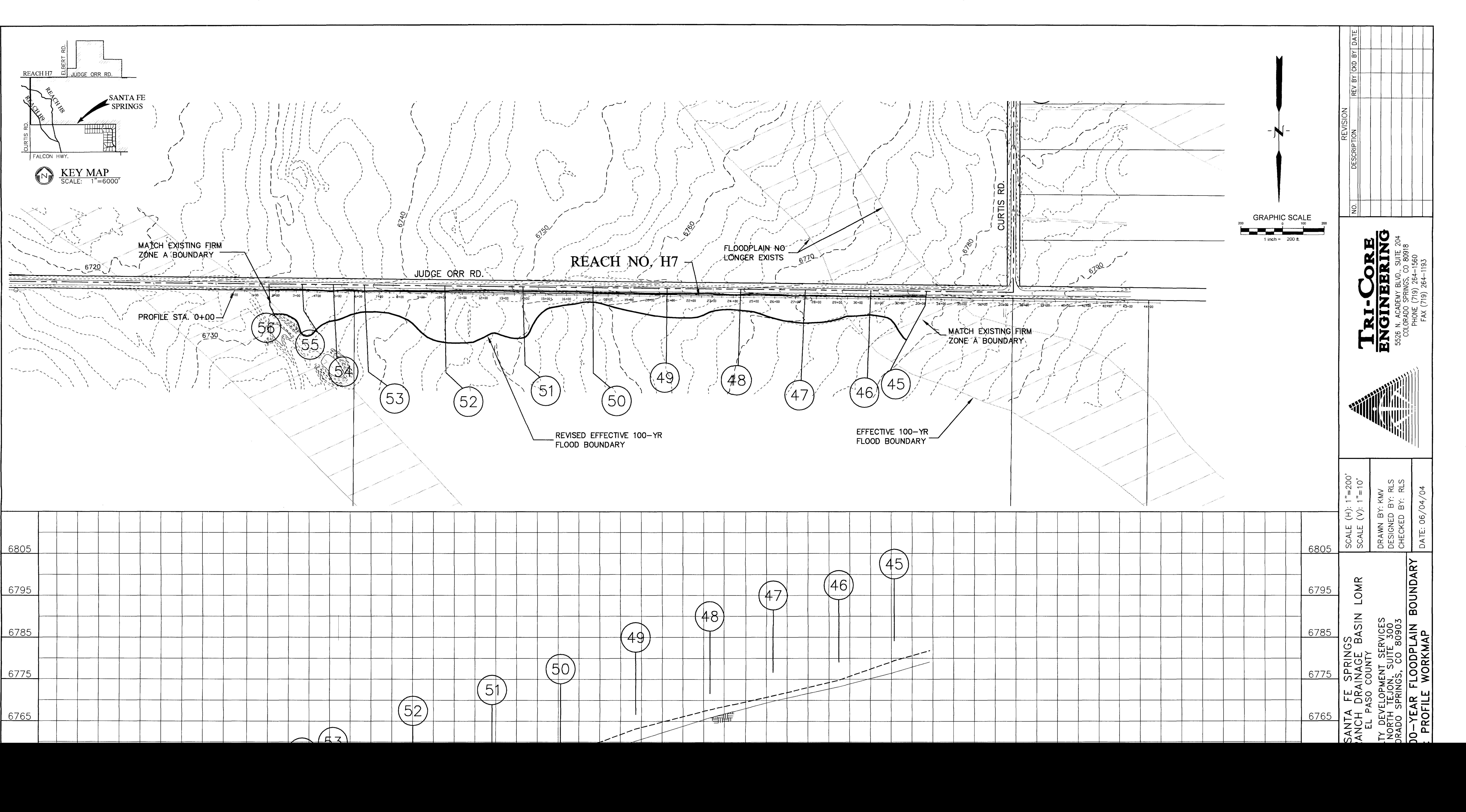


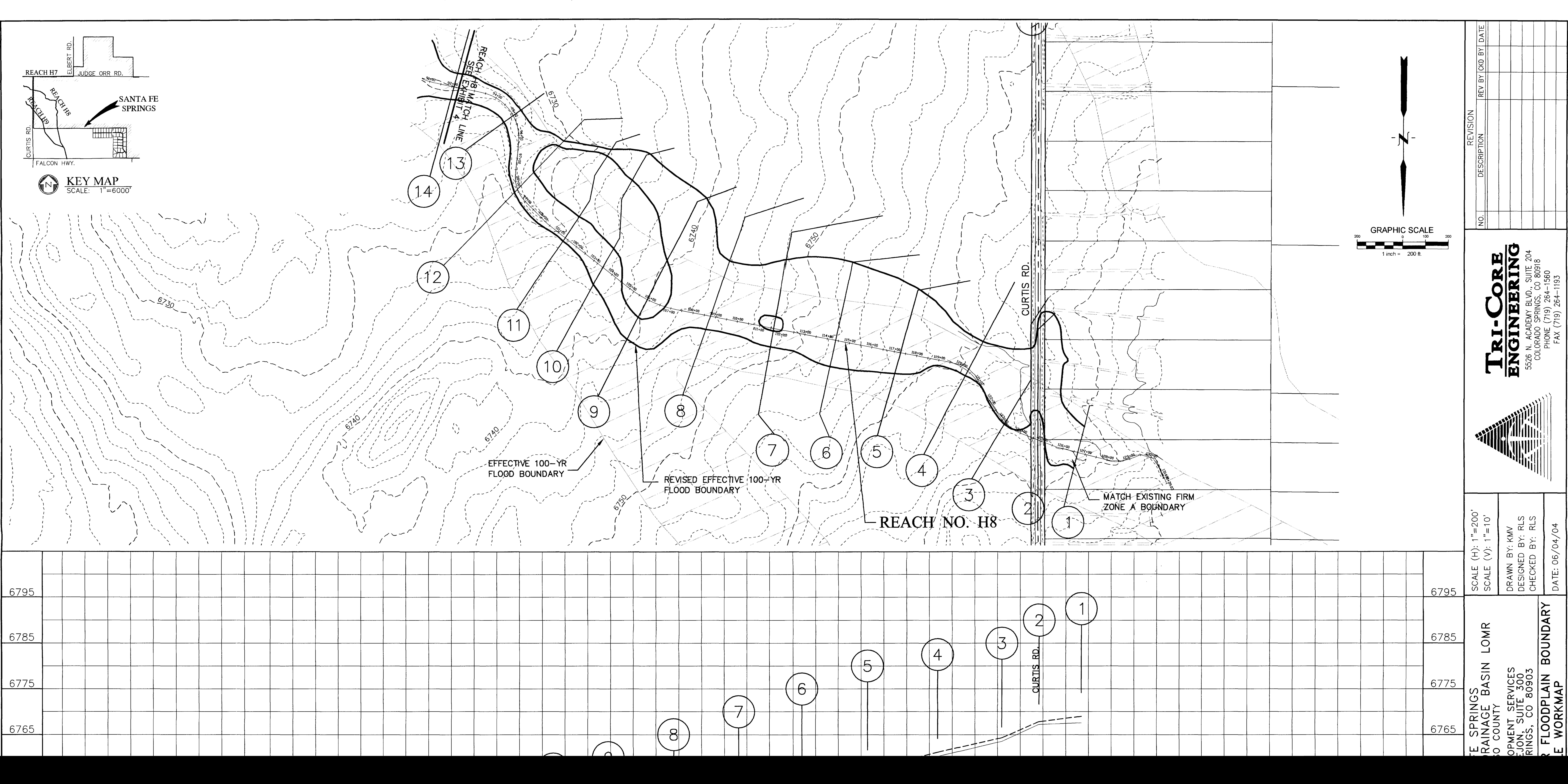


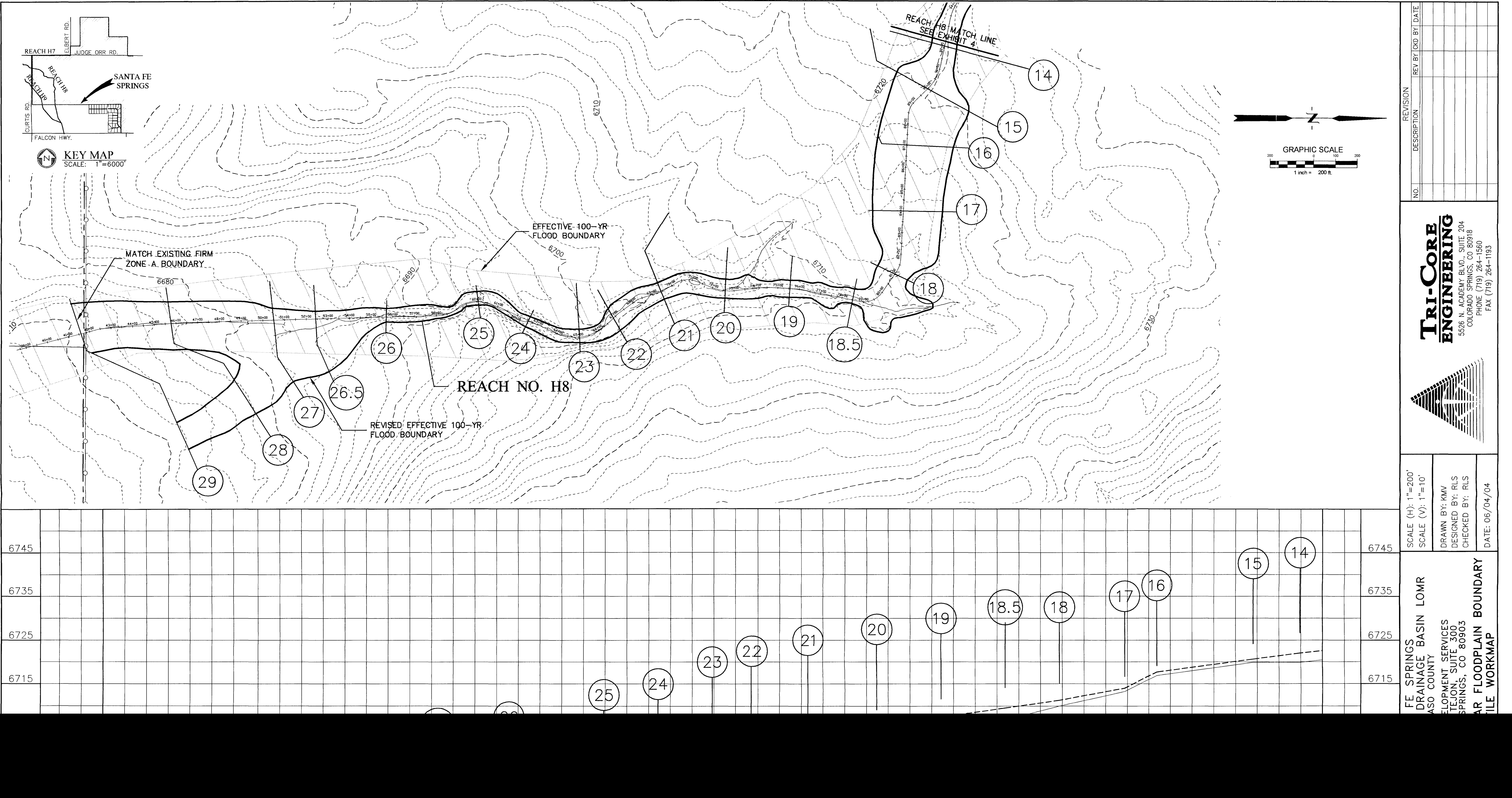


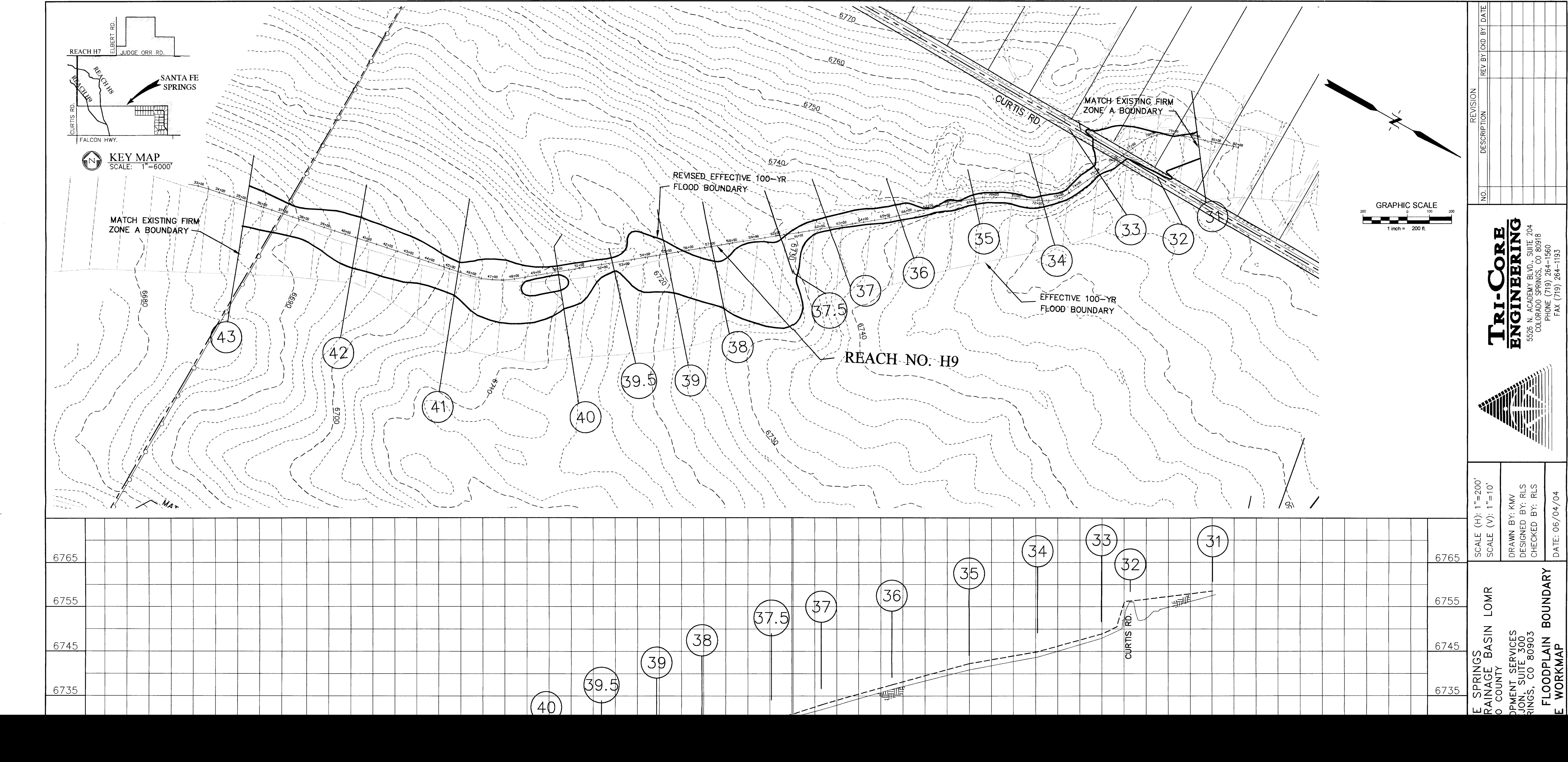
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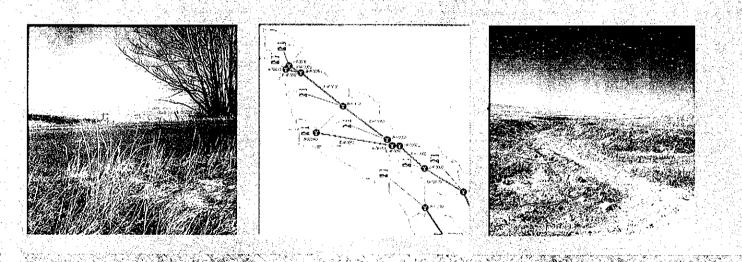
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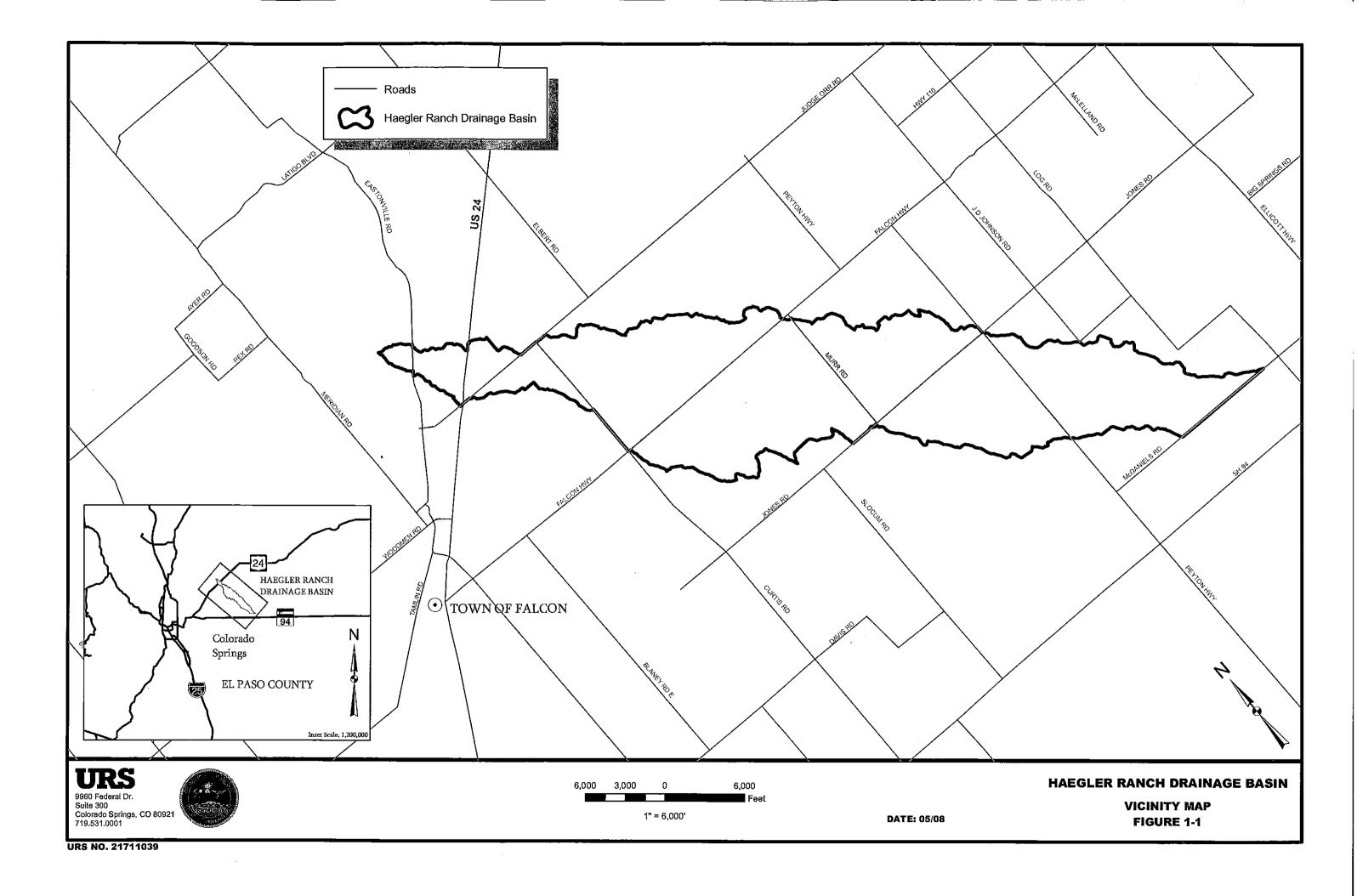


Howeviller Rowalder Bounder Study

May 2009







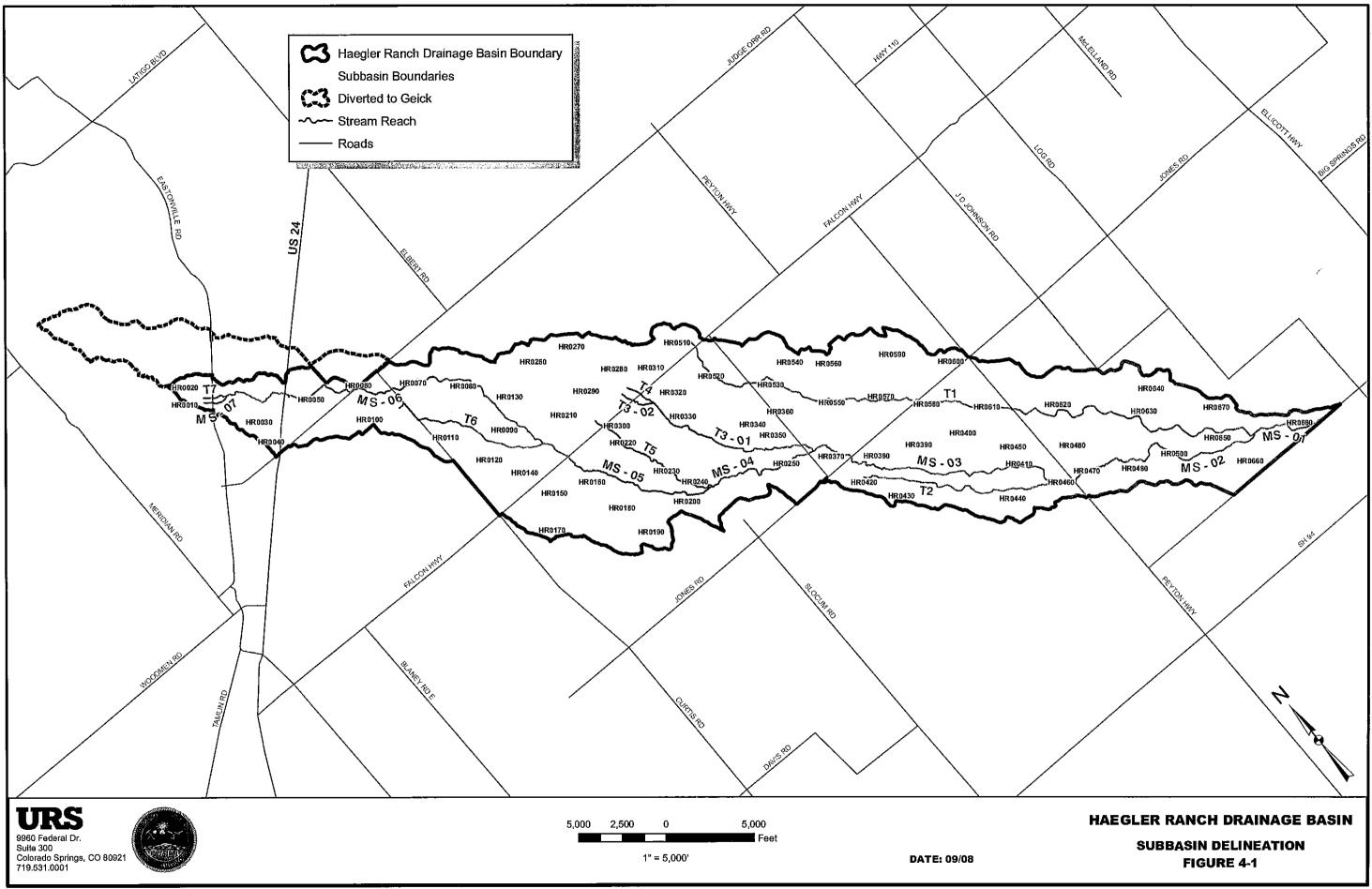


Table 5-3 Existing Hydraulic Deficiencies

Facility Number	Road Crossing	Channel	Existing Size	Existing 100-yr Flow (cfs)	Deficiency
633	Sagecreek Road	N/A	24" CMP	N/A	N/A
634	Sagecreek Road	N/A	24" CMP	N/A	N/A
701	Curtis Road	N/A	18" CMP	N/A	N/A
702	Curtis Road	Tributary 6 (T6)	36" CMP	120	Overtops
703	Curtis Road	Main Stem (MS-06)	24" CMP	590	Overtops
704	Judge Orr Road	Main Stem (MS-06)	Blocked Culvert	540	Overtops
705	Judge Orr Road	N/A	18" CMP	N/A	N/A
706	US 24	N/A	20" Steel Pipe	N/A	N/A
707	US 24	N/A	24" CMP	N/A	N/A
801	Pedestrain Bridge	Main Stem (MS-06)	Bridge	350	Meets Capacity
802	US24	Main Stem (MS-06)	2-66" CMPs	350	Meets Capacity
803	Eastonville Road	Main Stem (MS-07)	27"X21" CMP	25	Overtops
804	Eastonville Road	Tributary 7 (T7)	18" CMP	99	Overtops

Note: 69 Structures were cataloged and located. N/A indicates that the structure was not analyzed because it was not on one of the main channels.

5.14. Results

Hydraulic conditions from the hydraulic model results are summarized in Table 5-4. This includes channel velocity, flow depth, and top width for existing conditions at key locations. Water surface profiles for Haegler Ranch Drainage Basin for the 100-year recurrence interval flood for the existing conditions are presented in Figure 5-4 the HEC-RAS model for Haegler Ranch Drainage Basin for the existing conditions is provided in Appendix B.

The approximate 100-year floodplain as seen in Figure 5-4 varies from a contained floodplain with in a defined channel to a wide floodplain with shallow flooding. Three areas were designated as flooding: 1) the approximate 100-year floodplain as delineated by HEC-RAS, 2) split flow flooding that was estimated from HEC-RAS elevation upstream and contours, and 3) shallow areas connected to the floodplain with less than 1 foot of flooding.

Table 5-4 Existing Conditions HEC-RAS Model

	Reach and	each and HEC-RAS Result		Recurrence Intervals			
Key Location	Station	HEC-RAS RESUL	2-yr	5-yr	10-yr	100-yr	
		Channel velocity (ft/sec)	1.1	1.63	1.98	2.92	
Main stem at US 24	MS-06 72276	Water surface depth in channel (ft)	1.36	2.44	3.24	6.49	
	12210	Top width (ft)	18.23	24.85	29.7	255.62	
		Channel velocity (ft/sec)	3.33	4.09	1.76	3.48	
Main stem at Judge Orr Road	MS-06 67666	Water surface depth in channel (ft)	0.52	1.04	1.05	1.35	
	01000	Top width (ft)	174.53	534.34	535.52	569.34	
		Channel velocity (ft/sec)	1.05	1.6	2.04	3.59	
Main stem at Falcon Highway	MS-05 52353	Water surface depth in channel (ft)	1.79	3.69	4.96	5.74	
	3233	Top width (ft)	31.42	83.76	556.41	592.33	
	MS-03 33189	Channel velocity (ft/sec)	2.45	3.7	1.27	2.51	
Main stem at Jones Road		Water surface depth in channel (ft)	3.2	5.83	9.25	10.46	
		Top width (ft)	47.98	105.51	580.28	667.17	
	MS-02 18474	Channel velocity (ft/sec)	0.16	0.4	0.59	1.43	
Main stem at Peyton Highway		Water surface depth in channel (ft)	4.14	4.35	4.51	5.15	
		Top width (ft)	813.21	871.68	882.22	925.27	
	T1 22297	Channel velocity (ft/sec)	0.62	1.02	1.47	3.2	
Southeast Tributary at Jones Road		Water surface depth in channel (ft)	2.45	3.52	3.59	3.82	
		Top width (ft)	197.35	345.68	351.74	372.17	
		Channel velocity (ft/sec)	1.67	2.25	2.65	4.05	
Southeast Tributary at Peyton Highway	T1 16611	Water surface dcpth in channel (ft)	0.08	0.17	0.24	0.51	
- Angui (W)	10011	Top width (ft)	239.82	241.36	242.51	247.41	
		Channel velocity (ft/sec)	3.44	0.11	0.18	0.67	
Southeast Tributary at Confluence with Main stem	T1 410	Water surface depth in channel (ft)	1.69	2.01	2.01	2.01	
		Top width (ft)	31.89	1169.3	1169.3	1169.3	
		Channel velocity (ft/sec)	2.68	3.85	19.89	17.33	
At Confluence with Geick Basin	MS-01 82	Water surface depth in channel (ft)	1.45	2.17	1.11	2.36	
23011	<u>V</u>	Top width (ft)	75.88	255.32	60.67	262.84	

Grass channels are designed for depths and velocities to be within the limits of allowable shear stress. Grass lined channels are limited to 1.0 psf shear stress. If calculated shear stress is above this, drop structures must be added to flatten the natural slope of the channel.

Using these criteria, several channel sections were developed to accommodate a range of future flow rates from 100 cfs to 3500 cfs, as shown in Table 6-2. The approximate channel sections were used in the alternatives to accommodate future flows as necessary,

Table 6-2 Channel Dimensions based on Flow Rates

-2 Chaimei Dinichsions Dascu on Fio							
Λ	Grass						
Q (cfs)	Sideslope (h:v)	Bottom (ft)	Depth (ft)				
300	4	6	5				
500	4	8	5				
600	4	15	5				
800	4	20	5				
900	4	25	5				
1000	4	30	5				
1500	4	50	5				
2000	4	80	5				
3000	4	120	5				
3500	4	140	5				

6.2.2. Culvert Design

Culvert sizes for use in alternative evaluation were estimated based on full flow capacity of reinforced concrete pipe with a minimum slope of 0.50% and concrete end sections. For flows up to 300 cfs single RC pipe culverts with a maximum of 72" diameter were used. For greater flows, multiple RC pipes or 6-foot by 6-foot concrete box culverts with headwalls and flared wingwalls were used. Proposed culverts sizes based on existing flow rates are listed in Table 6-3.

Table 6-3 Existing Conditions Culvert Design

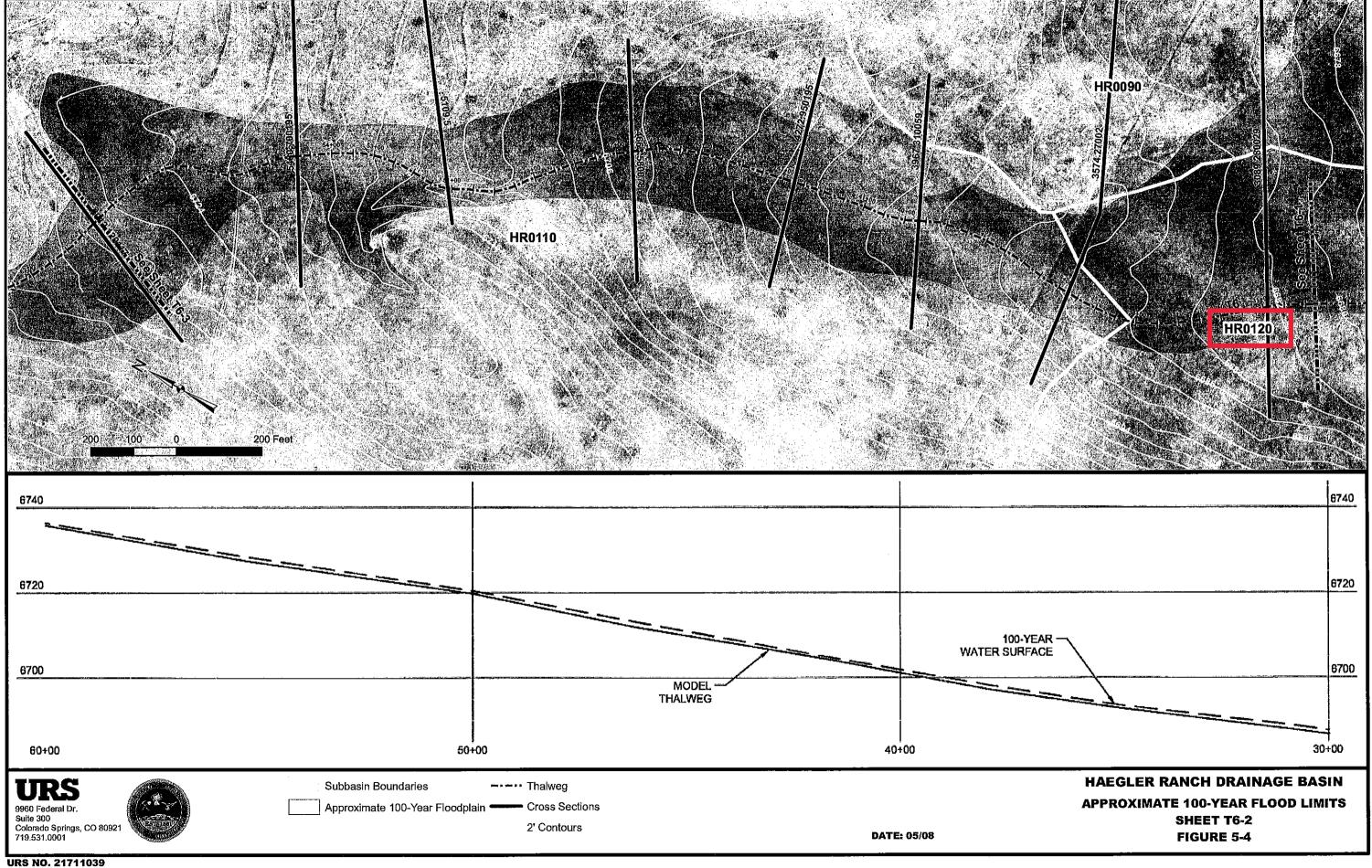
Facility Number	Road Crossing	Channel	Existing Size	Existing 100-yr Flow (cfs)	Deficiency	Necessary Facility
N/A	Peyton Highway	Tributary 1 (T1)	No Culvert	500	Overtops	2-72" RCPs
N/A	Falcon Highway	Tributary 1 (T1)	No Culvert	33	Overtops	36" RCP
301	Peyton Highway	Main Stem (MS-02)	2-33"X48" CMPs	2,500	Overtops	7-6'X6' RCBs
401	Jones Road	Tributary 1 (T1)	2-24" CMPs	370	Overtops	6'X6' RCB
403	Jones Road	Main Stem (MS-03)	3-60" CMPs	2,300	Overtops	6-6'X6' RCBs

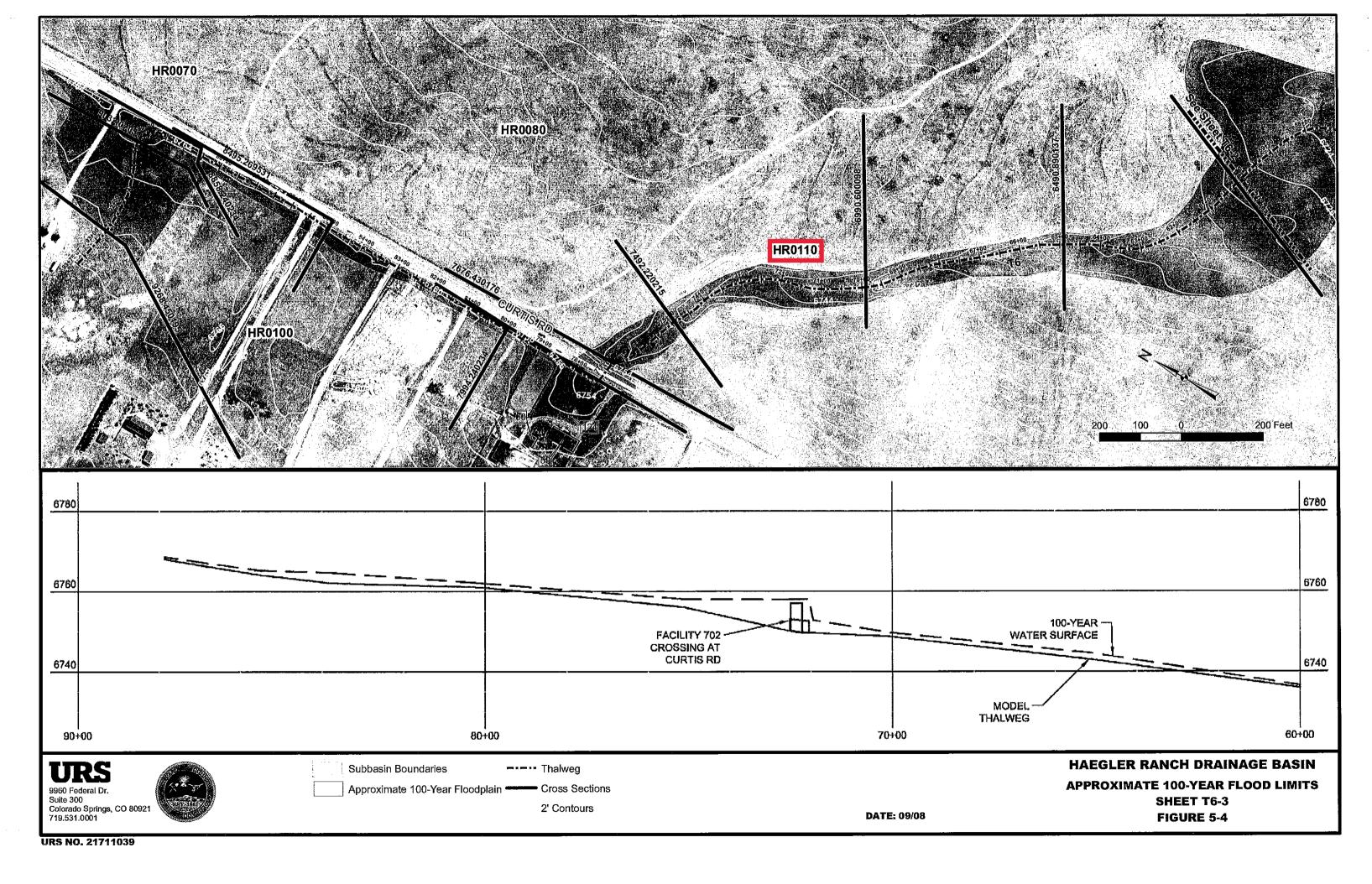
Facility Number	Road Crossing	Channel	Existing Size	Existing 100-yr Flow (cfs)	Deficiency	Necessary - Facility
405	Murr Road	Main Stem (MS-04)	66" RCP	1,700	Overtops	5-6'X6' RCBs
407	Murr Road	Tributary 3 (T3-01)	66" RCP	670	Overtops	2-6'X6' RCBs
507	Peerless Farms Road	Tributary 3 (T3-01)	60°, CMP	600	Overtops	2-6'X6' RCBs
509	Murr Road	Tributary 1 (T1)	2-15" RCPs	220	Overtops	66" RCP
601	Whiting Way	Tributary 1 (T1)	24" CMP	220	Overtops	66" RCP
604	Max Road	Tributary 1 (T1)	18" CMP	220	Overtops	66" RCP
609	Falcon Highway	Tributary 3 (T3-02)	18" CMP	180	Overtops	66" RCP
610	Falcon Highway	Tributary 4 (T4)	24" CMP	200	Overtops	66" RCP
612	Falcon Highway	Tributary 5 (T5)	24" CMP	150	Overtops	60" RCP
628	Falcon Highway	Main Stem (MS-05)	2-60" CMPs	1,000	Overtops	3-6'X6' RCBs
702	Curtis Road	Tributary 6 (T6)	36" CMP	120	Overtops	54" RCP
703	Curtis Road	Main Stem (MS-06)	24" CMP	590	Overtops	2-6'X6' RCBs
704	Judge Orr Road	Main Stem (MS-06)	Blocked Culvert	540	Overtops	2-72" RCPs
801	Pedestrain Bridge	Main Stem (MS-06)	Bridge	350	Meets Capacity	Existing Bridge
802	US24	Main Stem (MS-06)	2-66'' CMPs	350	Meets Capacity	Existing Culvert
803	Eastonville Road	Main Stem (MS-07)	27"X21" CMP	25	Overtops	30" RCP
804	Eastonville Road	Tributary 7 (T7)	18" CMP	99	Overtops	48" RCP

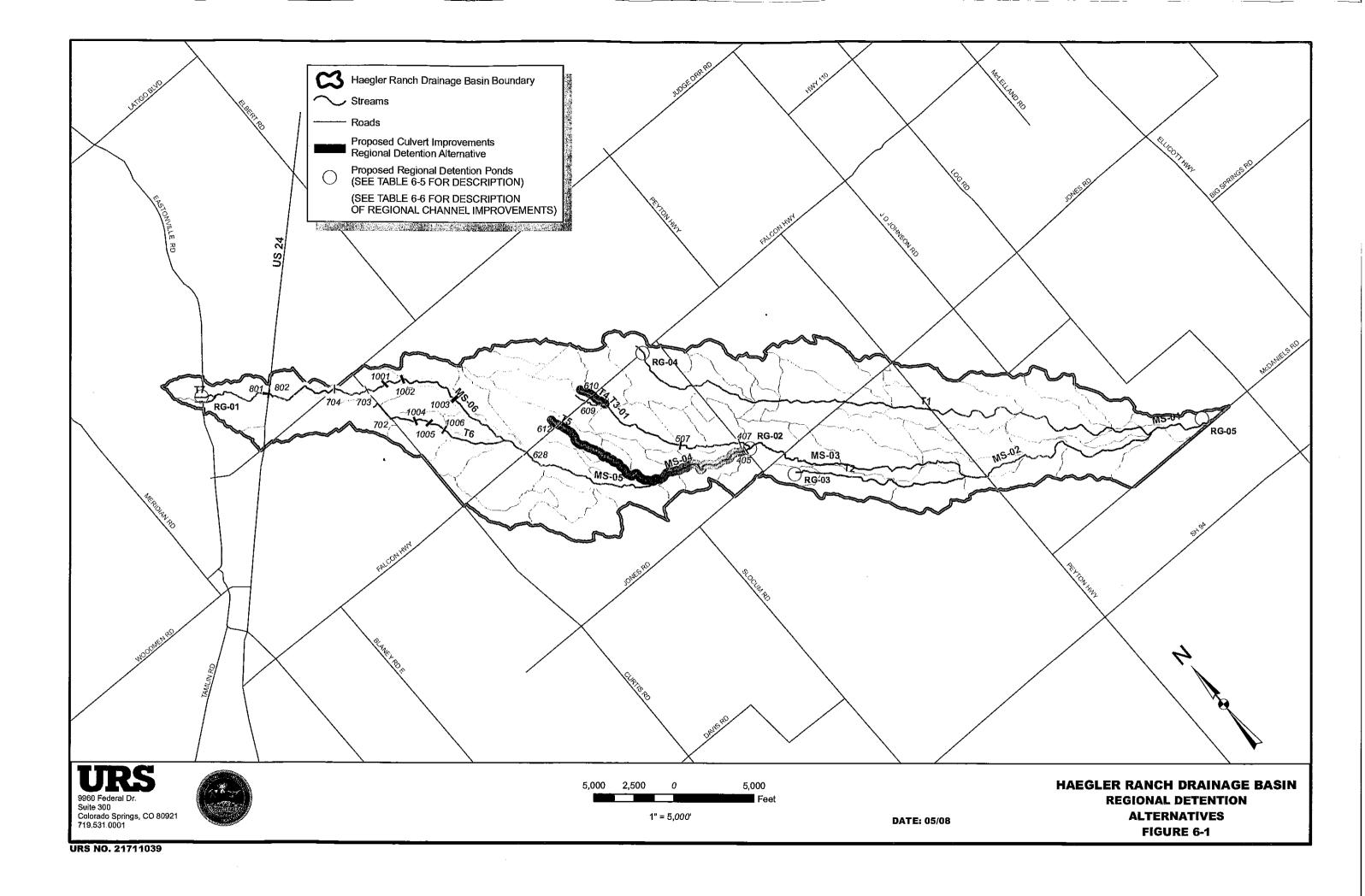
6.2.3. Detention Design

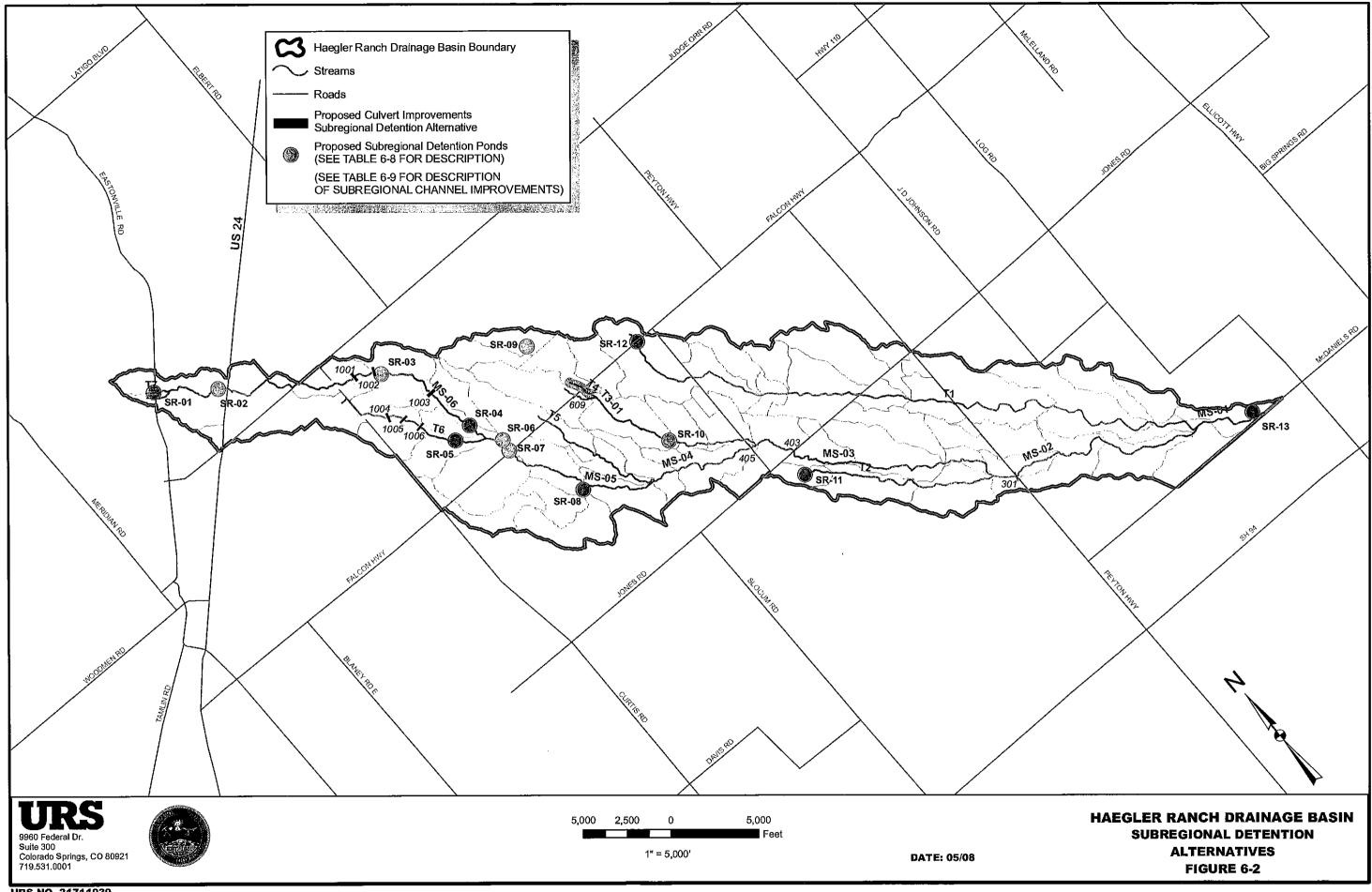
All detention pond design is based on Chapter 10, Storage, of the UDFCD SDCM. All ponds were assumed to be "full spectrum" per the SDCM. For final design to be performed later, some of the ponds may be separated into a water quality pond and an off-line major detention pond.

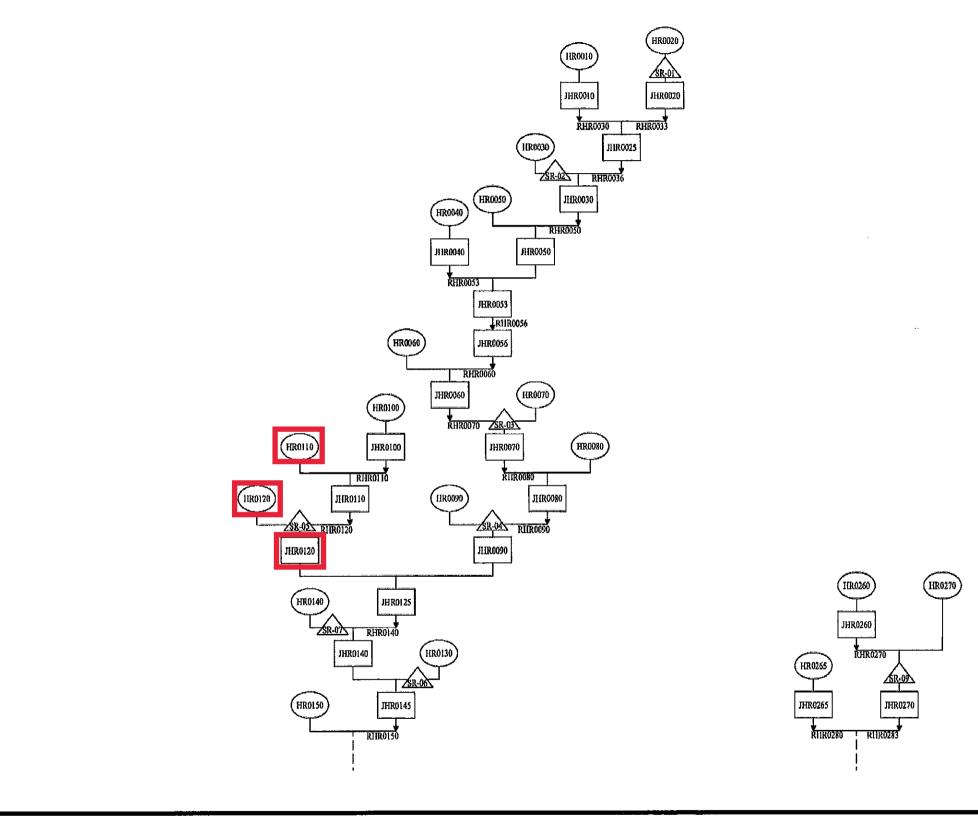
For the Regional Detention Alternative, either the simplified full spectrum sizing method or the hydrograph method was used to size the facility. If the contributing area is less than 160 acres and no











9960 Federal Dr. Sulte 300 Colorado Springs, CO 80921 719.531.0001



HAEGLER RANCH DRAINAGE BASIN
SUBREGIONAL DETENTION ALTERNATIVE
SHEET 1
FIGURE 6-3

6.4.1. Channel & Culvert Costs

Channel costs for each alternative are based on cubic yards of excavation, plus the cost of the channel lining and drop structures. These costs are presented in Table 6-13 and Table 6-14.

Table 6-13 Regional Detention Alternative Channel Cost Estimates

Channel	Design Flow (cfs)	-Channel Length (ft)	Total Cost	Drop Structure Cost
Main Stem (MS-04)	3,500	7,140	\$1,626,000	none
Main Stem (MS-05)	3,000	11,100	\$2,216,000	\$2,539,000
Main Stem (MS-06)	900	7,330	\$482,000	\$589,000
Main Stem (MS-06)	1,000	3,170	\$231,000	\$268,000
Main Stem (MS-06)	1,500	4,450	\$450,000	\$548,000
Main Stem (MS-06)	2,000	3,330	\$477,000	\$636,000
Tributary 3 (T3-01)	1,500	6,710	\$1,082,000	\$1,302,000
Tributary 4 (T4)	600	1,840	\$96,000	\$127,000
Tributary 5 (T5)	300	930	\$37,000	\$36,000
Tributary 5 (T5)	500	7,770	\$325,000	\$370,000
Tributary 6 (T6)	500	4,270	\$179,000	\$222,000
Tributary 6 (T6)	600	3,940	\$204,000	\$253,000
Sub-Total			\$7,405,000	\$6,888,000
30% Construction Cor	ntingency	\$2,222,000	\$2,066,000	
15% Engineering Contingency			\$1,110,000	\$1,033,000
Total			\$10,737,000	\$9,988,000

(See Tables C6 and C7 in Appendix C for details)

Table 6-14 Sub-Regional Detention Alternative Channel Cost Estimates

1 able 0-14 Sub-Regional Detention Alternative Chainlei Cost Estimates							
Channel	Design Flow (cfs)	Channel Length (ft)	Total Cost	Drop Structure Cost			
Main Stem (MS-05)	2,000	1,560	\$224,000	\$367,000			
Main Stem (MS-06)	600	3,120	\$162,000	\$295,000			
Main Stem (MS-06)	1,000	4,535	\$331,000	\$375,000			
Main Stem (MS-06)	800	3,190	\$188,000	\$368,000			
Tributary 3 (T3-01)	600	5,000	\$259,000	\$422,000			
Tributary 3 (T3-02)	500	420	\$18,000	\$37,000			
Tributary 4 (T4)	500	940	\$40,000	\$74,000			
Tributary 6 (T6)	500	4,280	\$179,000	\$333,000			
Tributary 6 (T6)	300	1,400	\$55,000	\$107,000			
Sub-Total			\$1,456,000	\$2,374,000			
30% Construction Contingency			\$430,000	\$712,000			
15% Engineering Contingency			\$218,000	\$356,000			
Total			\$2,111,000	\$3,442,000			

(See Tables C6 and C8 in Appendix C for details)

Culverts costs are based on a per linear foot of pipe with two flared end sections or two wing walls, as appropriate, complete-in-place. Culvert costs for each alternative are presented in Table 6-15 and Table 6-16.

Table 6-15 Regional Detention Alternative Roadway Crossing Cost Estimate Sumary

Facility Number	Road Crossing	Channel	Existing Size	Proposed 100-yr Flow (cfs)	Necessary Facility for Proposed 100- year Flow	Estimated Cost
405	Murr Road	Main Stem (MS-04)	66" RCP	3,400	9-6'X6' RCBs	\$256,000
507	Peerless Farms Road	Tributary 3 (T3-01)	60" CMP	1200	4-6'X6' RCBs	\$139,000
609	Falcon Highway	Tributary 3 (T3-02)	18" CMP	460	2-66" RCPs	\$51,600
610	Falcon Highway	Tributary 4 (T4)	24" CMP	570	2-72" RCPs	\$51,000
612	Falcon Highway	Tributary 5 (T5)	24" CMP	240	72" RCP	\$26,000
628	Falcon Highway	Main Stem (MS-05)	2-60" CMPs	2,200	6-6'X6' RCBs	\$243,000
702	Curtis Road	Tributary 6 (T6)	36" CMP	140	60" RCP	\$29,000
703	Curtis Road	Main Stem (MS-06)	24" CMP	890	3-6'X6' RCBs	\$142,000
704	Judge Orr Road	Main Stem (MS-06)	Blocked Culvert	830	3-6'X6' RCBs	\$185,000
1001	Future Pastura Street	Main Stem (MS-06)	N/A	930	3-6'X6' RCBs	\$99,000
1002	Future Arroyo Hondo Blvd. N.	Main Stem (MS-06)	N/A	930	3-6'X6' RCBs	\$99,000
1003	Future Arroyo Hondo Blvd. N	Main Stem (MS-06)	N/A	1500	4-6'X6' RCBs	\$143,000
1004	Future Pastura Street	Tributary 6 (T6)	N/A	440	2-66" RCPs	\$43,000
1005	Future El Vado Road	Tributary 6 (T6)	N/A	440	2-66" RCPs	\$43,000
1006	Future Socorro Trail	Tributary 6 (T6)	N/A	440	2-66" RCPs	\$43,000
Sub-Total						\$1,591,000
30% Construction Contingency						
15% Engi	neering Contingency					\$239,000
Total						\$2,307,000

(See Table C4 in Appendix C for details)

Table 6-16 Sub-Regional Detention Roadway Crossing Cost Estimate Summary

Facility Number	Road Crossing	Channel	Proposed 100-yr Flow (cfs)	Necessary Facility for Proposed 100-year Flow	Estimated Cost
301	Peyton Highway	Main Stem (MS-02)	3,370	9-6'X6' RCBs	\$402,000
403	Jones Road	Main Stem (MS-03)	2,970	8-6'X6' RCBs	\$358,000
405	Murr Road	Main Stem (MS-04)	2,870	8-6'X6' RCBs	\$283,000
609	Falcon Highway	Tributary 3 (T3-02)	460	2-6'X6' RCBs	\$106,000
N/A	Falcon Highway	Tributary 1 (T1)	110	2 - 36" RCP	\$20,000
1001	Future Pastura Street	Main Stem (MS-06)	610	2-6'X6' RCBs	\$107,000
1002	Future Arroyo Hondo Blvd. N.	Main Stem (MS-06)	610	2-6'X6' RCBs	\$87,000
1003	Future Arroyo Hondo Blvd. N.	Main Stem (MS-06)	530	2-6'X6' RCBs	\$87,000
1004	Future Pastura Street	Tributary 6 (T6)	440	2-66" RCPs	\$43,000
1005	Future El Vado Road	Tributary 6 (T6)	440	2-66" RCPs	\$43,000
1006	Future Socorro Trail	Tributary 6 (T6)	440	2-66" RCPs	\$43,000
Sub-Total					\$1,582,000
30% Constru	ction Contingency				\$475,000
15% Engine	ering Contingency				\$237,000
Total					\$2,294,000

(See Tables C5 in Appendix C for details)

6.4.2. Detention Pond Costs

The cost of detention ponds, both regional and subregional, is based on the cubic yards of excavation, an estimated outlet structure, and the cost of the land required for the facility. These costs are presented in Table 6-17 and Table 6-18.

Table 6-17 Regional Detention Pond Cost Summary

Two of T. Regional Doubleton I on a Copy Dulling				
Facility	Storage (AF)	Total Cost Including Construction and Engineering Contingencies		
RG-01 9.02	9.02	\$542,000		
RG-02 64.52	64.52	\$4,053,000		
RG-03 0.04	0.04	\$146,000		
RG-04 1.07	1.07	\$160,000		
RG-05 0.03	0.03	\$146,000		
Total	_	\$5,048,000		

(See Tables C1 in Appendix C for details)

Haegler Ranch Drainage Basin Planning Study Table 6-18 Sub-Regional Detention Pond Cost Summary

Facility	Storage (AF)	Total Cost Including Construction and Engineering Contingencies
SR-01	10	\$899,000
SR-02	5	\$640,000
SR-03	16	\$868,000
SR-04	25	\$1,453,000
SR-05	24	\$1,557,000
SR-06	9	\$547,000
SR-07	5	\$524,000
SR-08	5	\$326,000
SR-09	20	\$861,000
SR-10	23	\$1,069,000
SR-11	2	\$182,000
SR-12	9	\$477,000
SR-13	. 3	\$376,000
Total		\$9,780,000

(See Table C1 in Appendix C for details)

6.4.3. Other Costs

Design Engineering costs are also included as 15% of the construction costs. Construction contingencies (30%) include such items as utility relocations, mobilization, temporary erosion control, and construction engineering.

6.4.4. Conceptual Alternative Costs

The total estimated capital costs for each alternative are based on the sum of the cost of the proposed facilities, plus costs for engineering and construction contingencies. These costs are listed in Table 6-19.

Table 6-19 Concentual Alternative Costs

Table 0-17 Conceptual Atternative Costs				
	Regional Alternative	Subregional Alternative 😅		
Detention Ponds	\$5,048,000	\$9,780,000		
Channel Improvements	\$10,737,000	\$2,110,000		
Drop Structures	\$9,988,000	\$3,442,000		
Roadway Crossing Culverts	\$2,307,000	\$2,294,000		
Total	\$28,080,000	\$17,627,000		

impacted by site development, utility, roadway and landscape construction activities have in some cases negatively affected downstream areas.

El Paso County has enacted an erosion control ordinance to address these problems. In general, it is the responsibility of the entity conducting any land disturbance activity to properly control surface runoff, erosion and sedimentation during and after the activity. Technical criteria identifying measures which help mitigate the impacts of erosion and sedimentation are available and being used throughout the region. Minimum requirements must be developed to properly control erosion.

Erosion control is necessary to prevent environmental degradation caused by wind or water-borne soil. The following minimum criteria and standards are intended to prevent excessive erosion. El Paso County as well as other affected agencies will enforce the Clean Water Act standards if the planned erosion control measures fail to perform satisfactorily. Proper installation and maintenance is necessary to achieve the desired function of erosion control measures. By paying attention to quality, reinstallation can be avoided. General requirements for erosion control are as follows:

- 1. Any land disturbing activity shall be conducted so as to effectively reduce unacceptable erosion and resulting sedimentation.
- 2. All land disturbing activities shall be designed, constructed, and completed in such a manner that the exposure time of disturbed land shall be limited to the shortest possible period of time.
- 3. Sediment caused by accelerated soil erosion and runoff shall be intercepted by erosion control measures such as hay bales, silt fences and / or sediment ponds, and contained within the site.
- 4. Any facility designed and constructed to convey storm runoff shall be designed to be non-erosive.
- 5. Erosion control measures will be used prior to and during construction.

Temporary erosion control measures are required during construction, and permanent erosion control measures are required for all developments. Maintenance of erosion control measures is the responsibility of the property owner.

Various structures have been proposed in this plan to help control localized erosion and sedimentation problems. It is important that the erosion control plan for any land disturbing activity be strictly adhered to and maintained so that the above minimum criteria can be achieved in the Haegler Ranch Basin.

7.4. Operations and Maintenance

Maintenance of drainage way facilities is essential in preventing long term degradation of the creek and overbank areas. Along the drainageway, clearing of debris and dead vegetation should be considered within the low flow area of the creek and its tributaries. On the overbanks, limited maintenance of the existing vegetative cover is recommended. Semi-annual clearing of trash and debris at roadway crossings is also recommended to increase the effectiveness of the crossings. Sediments cleared from the channel or culvert should not be left on the overbank. This disturbs the native vegetation, creates a potential water quality concern if the dredgings are subsequently washed into the drainageway by natural erosion, and reduces the capacity of the overbank. In those reaches designated to be selectively

lined and the floodplain preserved, maintenance activities should be carried out with the least disturbances to native vegetation that is practical.

Similar practices should be employed when removing sediment from detention basins. Although some channels degrade and others agrade, all detention basins will collect sediment and agrade. The use of an easily accessible concrete lined forebay in the final design of a detention facility can make the cleaning of the larger debris and trash more easily accomplished with motorized equipment. If forebays are provided, they will need clearing semi-annually and after major storm events. More frequent routine maintenance may be required depending on the type of development upstream and the access provided to the public. Plan for annual removal of sediment and debris from the detention area of a facility with a forebay.

Deposition in drainage facilities of wind-blown trash and debris, should be expected in this region. This means that regular maintenance, even without rainfall events, should be performed.

7.5. Drainage and Bridge Fee Calculations

The cost estimates and basin fee calculation for the major drainageways, tributary drainageways, roadway culverts, regional detention basins, and related improvements for the Sub-Regional Detention Facilities are presented in Table 7-2. The sub-regional detention capital construction cost estimates include the cost for the construction of the embankment, water quality, and outlet structures. Bridges in the Sub-Regional Detention Alternative are presented in Table 7-3. The cost estimates include engineering and construction costs for the entire Haegler Ranch Basin as presented on the Conceptual Design Drawings in Appendix D. These estimates do not include costs for local or initial systems, and therefore no costs attributable to local or minor drainage systems have been computed in the estimation of the drainage basin fee. These systems are expected to be provided with proposed development. Costs associated with utility relocations have not been estimated but would be included in construction contingencies. A review of utility maps indicates that the majority of the potential relocations occur at the roadway crossings. Land acquisition costs for the detention facilities were not included for calculation of fees per Appendix L of the El Paso County Criteria Manual.

Unplatted acreage within Haegler Ranch was obtained from El Paso County, and is shown in Figure 7-I. A total of 8,953 acres is estimated to be currently unplatted and subject to future development. This unplatted land is projected to have an average imperviousness of approximately 15%, corresponding to approximately 1,343 unplatted impervious acres. All drainage and bridge fees are calculated per *impervious* acre. (See Appendix D for an unplatted area breakdown by subbasin and average imperviousness calculations.)

Reimbursable costs calculated for the Haegler Ranch Basin are listed in Table 7-4. These costs are based on improvements required under existing conditions. The term "reimbursable costs" used on Table 7-4 means those costs that have been used in estimation of drainage basin fees. Costs considered "non-reimbursable" are costs for the replacement of existing, undersized culverts, or costs to rehabilitate or maintain an existing lined segment of drainageway. For the most part, all of the drainageway costs for Haegler Ranch Basin are considered reimbursable.

The calculated drainage basin fee presented in Table 7-2 is \$ 7,633 per impervious acre, and the bridge fee is \$1,126 per impervious acre, as shown in Table 7-3.

Table 7-2 Drainage Basin Fec Calculations

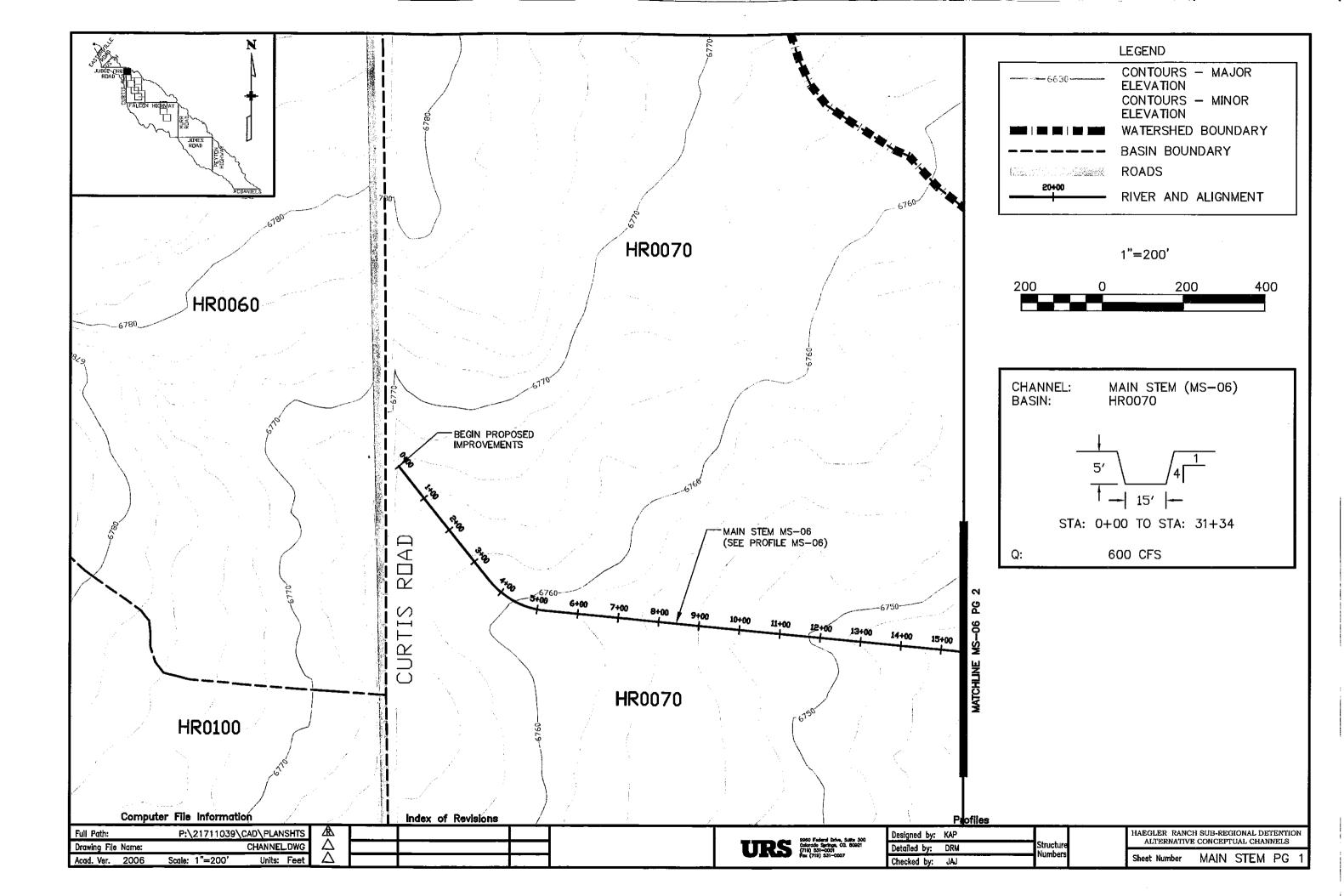
		Channel Improvemen				
			Drop Structure			
Channel	Basins	Channel Construction Cost	Construction Cost	Contingency Cost	Total Cost	
Main Stem (MS-05)	HR0200	\$224,000	\$363,600	\$264,420	\$852,020	
Main Stem (MS-06)	HR0070	\$162,000	\$295,400	\$205,830	\$633,230	
Main Stem (MS-06)	HR0080	\$331,000	\$374,500	\$317,475	\$1,022,975	
Main Stem (MS-06)	HR0090	\$188,000	\$368,000	\$250,200	\$806,200	
Tributary 3 (T3-01)	HR0330	\$259,000	\$422,000	\$306,450	\$987,450	
Tributary 3 (T3-02)	HR0300	\$18,000	\$37,000	\$24,750	\$79,750	
Tributary 4 (T4)	HR0300	\$40,000	\$74,000	\$51,300	\$165,300	
Tributary 4 (T4)	HR0110	\$179,000	\$333,000	\$230,400	\$742,400	
Tributary 6 (T6)	HR0120	\$55,000	\$106,500	\$72,675	\$234,175	
Subtotal Channel Costs						
		Culvert Improvement			\$5,553,500	
			Culvert			
			Construction	Contingency		
Culvert	Road Crossing	Channel	Cost	Cost	Total Cost	
609	Falcon Highway	Tributary 3 (T3-02)	\$106,301	\$47,836	\$154,137	
N/A	Falcon Highway	Tributary 1 (T1)	\$19,500	\$8,775	\$28,275	
1001	Future Pastura Street	Main Stem (MS-06)	\$106,301	\$47,836	\$154,137	
- 1002	Future Arroyo Hondo Blvd. N.	Main Stem (MS-06)	\$87,301	\$39,286	\$126,587	
1003	Future Arroyo Hondo Blvd. N.	Main Stem (MS-06)	\$87,301	\$39,286	\$126,587	
1004	Future Pasture Street	Tributary 6 (T6)	\$51,000	\$22,950	\$73,950	
1005	Future El Vado Road	Tributary 6 (T6)	\$19,500	\$8,775	\$28,275	
1006	Future Socorro Trail	Tributary 6 (T6)	\$42,800	\$19,260	\$62,060	
Subtotal Culvert Costs	<u> </u>		<u> </u>	·	\$754,007	
		etention Improvemen	its 🚟 💮			
				Contingency		
Facility	Storage (AF)	Construction Cost		Cost	Total Cost	
SR-01	10	\$296,701		\$133,516	\$430,217	
SR-02	5	\$207,949		\$93,577	\$301,525	
SR-03	16	\$186,252		\$83,814	\$270,066	
SR-04	25	\$390,182		\$175,582	\$565,764	
SR-05	24	\$455,235		\$204,856	\$660,091	
SR-06	9	\$140,670		\$63,301	\$203,971	
SR-07	5	\$162,046		\$72,921	\$234,967	
SR-08	5	\$87,489		\$39,370	\$126,860	
SR-09	20	\$188,250		\$84,713	\$272,963	
SR-10	23	\$331,635		\$149,236	\$480,871	
SR-11	2	\$56,880		\$25,596	\$82,476	
SR-12	9	\$108,987		\$49,044	\$158,031	
SR-13	3	\$107,812		\$48,515	\$156,327	
Subtotal Detention Cos	ets				\$3,944,129	
Total Cost					\$10,251,636	
Total Unplatted Impe	ervious Acres				1,343	
Fee Per Impervious Acre					\$7,633	
					+ + + + + + + + + + + + + + + + + + + +	

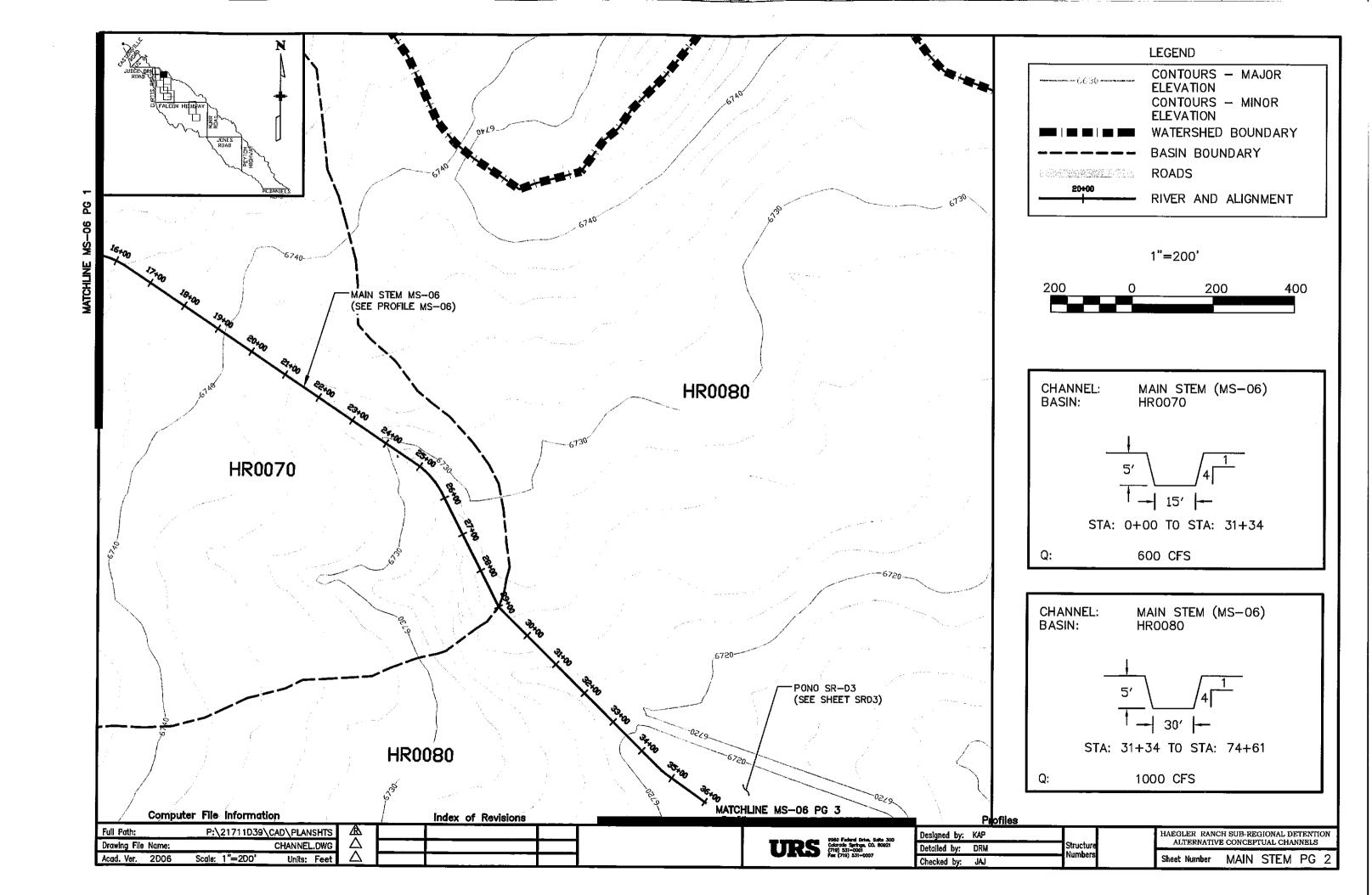
Table 7-3 Bridge Fce Calculation

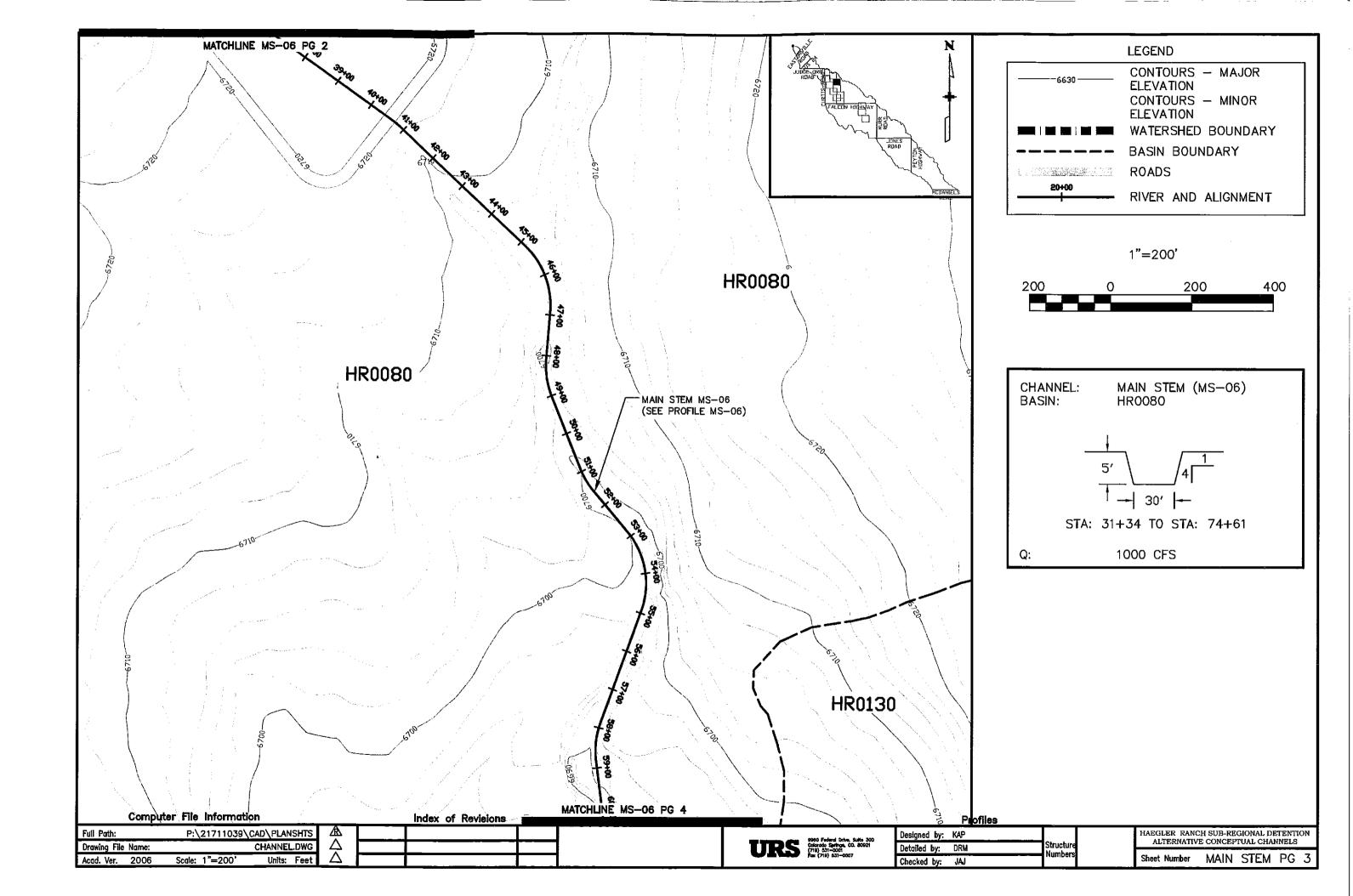
301	Peyton Highway	Main Stem (MS-02)	401,710	\$180,770	\$582,480
403	Jones Road	Main Stem (MS-03)	358,123	\$161,155	\$519,278
405	Murr Road	Main Stem (MS-04)	282,941	\$127,323	\$410,264
Subtotal	Bridge Costs				\$1,512,022
Total Co	st				\$1,512,022
Total Unplatted Impervious Acres					1,343
Bridge Fec Per Impervious Acre				\$1,126	

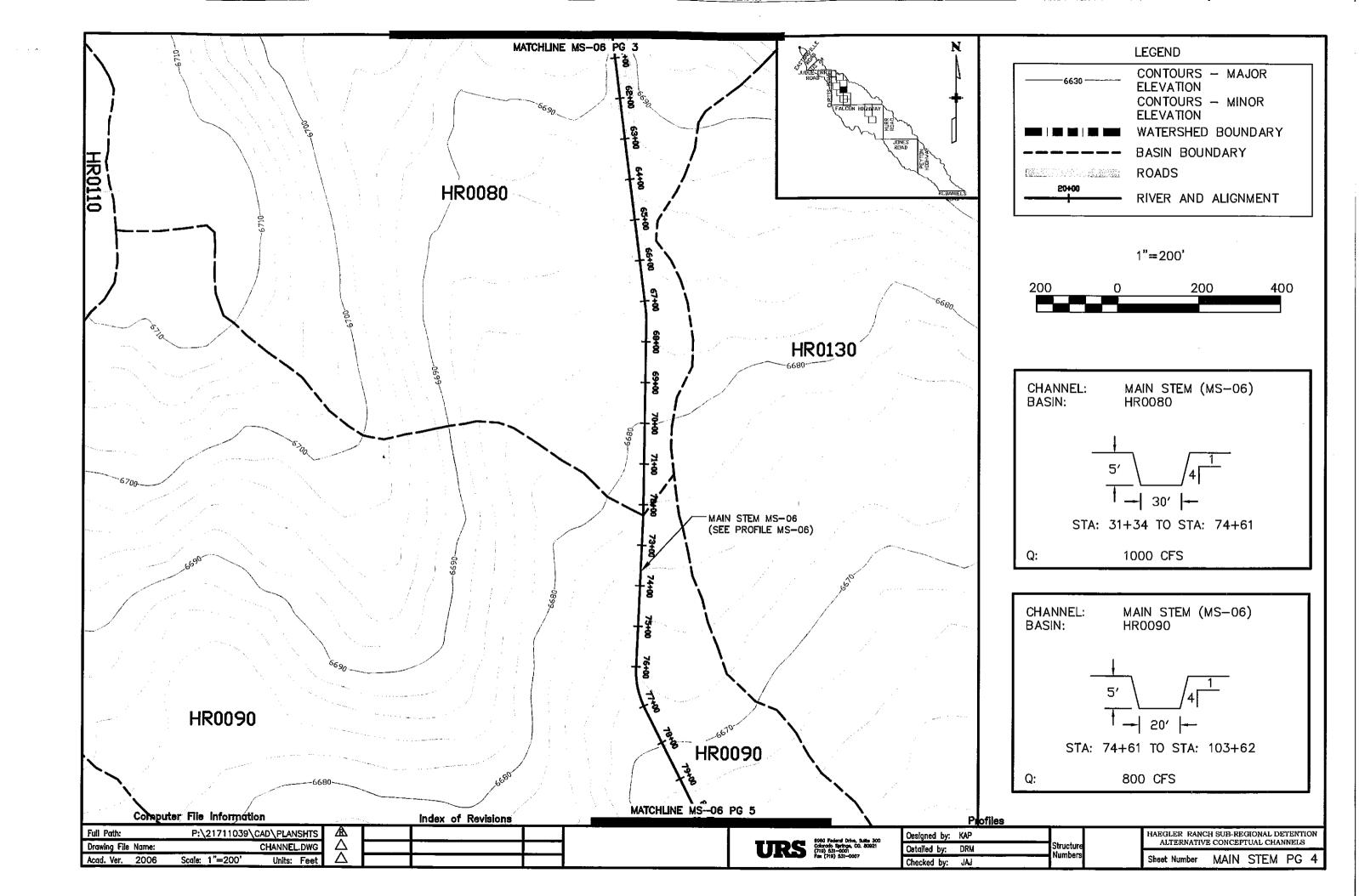
Table 7-4 Reimbursable Costs

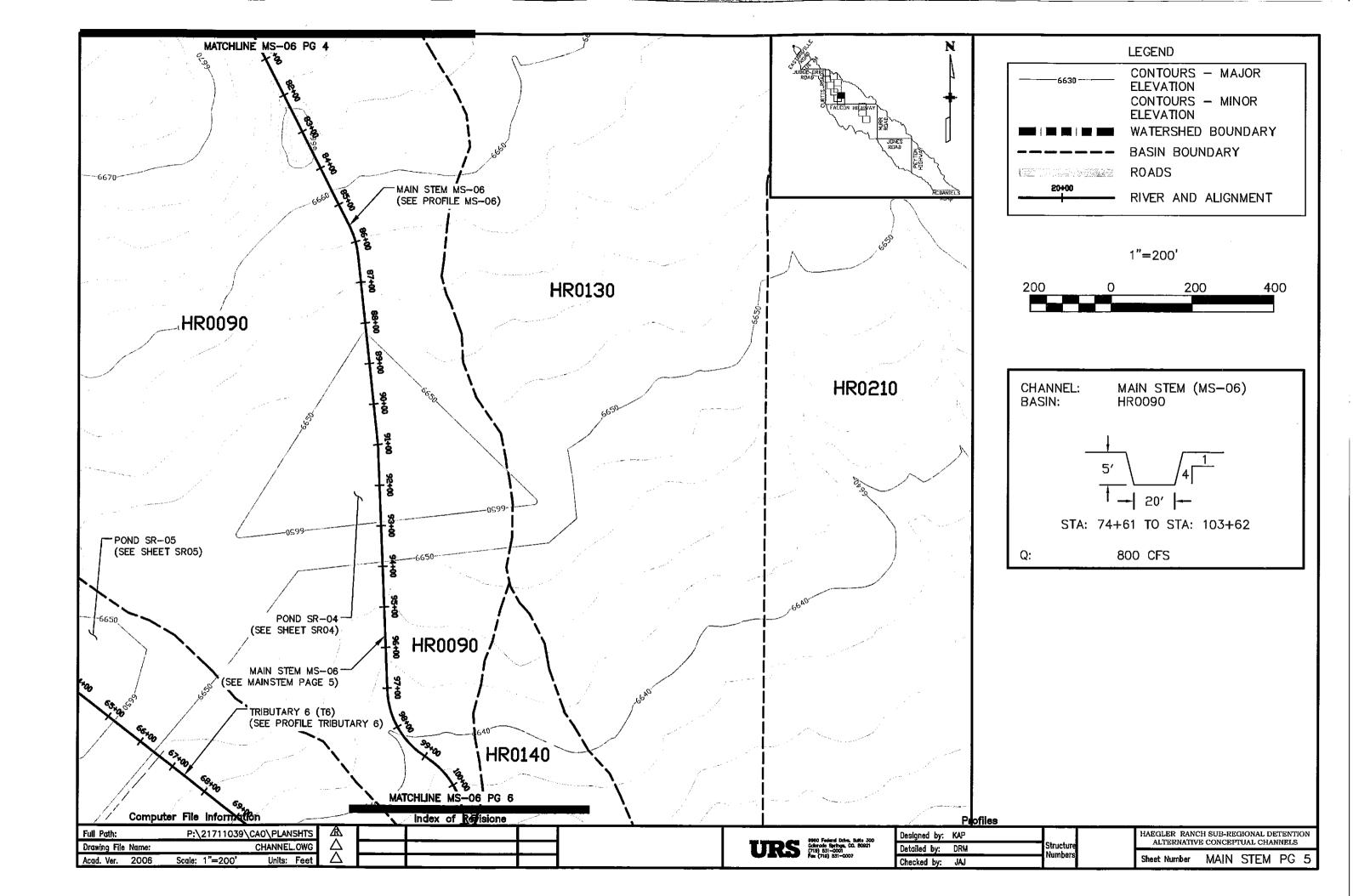
	Reim	bursable Culvert Impro	vements		
			Culvert Construction	Contingency	
Culvert	Road Crossing	Channel	Cost	Cost	Total Cost
N/A	Peyton Highway	Tributary 1 (T1)	\$51,000	\$22,950	\$73,950
N/A	Falcon Highway	Tributary 1 (T1)	\$9,7580	\$4,388	\$14,138
301	Peyton Highway	Main Stem (MS-02)	\$314,535	\$141,541	\$456,076
401	Jones Road	Tributary 1 (T1)	\$53,111	\$23,900	\$77,011
403	Jones Road	Main Stem (MS-03)	\$270,947	\$121,926	\$392,874
405	Murr Road	Main Stem (MS-04)	\$180,371	\$81,167	\$261,538
407	Murr Road	Tributary 3 (T3-01)	\$77,801	\$35,011	\$112,812
507	Peerless Farms Road	Tributary 3 (T3-01)	\$115,801	\$52,111	\$167,912
509	Murr Road	Tributary 1 (T1)	\$19,300	\$8,685	\$27,985
601	Whiting Way	Tributary 1 (T1)	\$23,500	\$10,575	\$34,075
604	Max Road	Tributary 1 (T1)	\$19,300	\$8,685	\$27,985
609	Falcon Highway	Tributary 3 (T3-02)	\$25,600	\$11,520	\$37,120
610	Falcon Highway	Tributary 4 (T4)	\$23,500	\$10,575	\$34,075
612	Falcon Highway	Tributary 5 (T5)	\$21,200	\$9,540	\$30,740
628	Falcon Highway	Main Stem (MS-05)	\$154,741	\$69,633	\$224,375
702	Curtis Road	Tributary 6 (T6)	\$23,150	\$10,418	\$33,568
703	Curtis Road	Main Stem (MS-06)	\$125,301	\$56,386	\$181,687
704	Judge Orr Road	Main Stem (MS-06)	\$83,200	\$37,440	\$120,640
803	Eastonville Road	Main Stem (MS±07)	\$9,680	\$4,356	\$14,036
804	Eastonville Road	Tributary 7 (T7)	\$14,980	\$6,741	\$21,721
Subtotal Channel Costs	S	<u> </u>	<u> </u>		\$2,344,315
	Reimb	ursable Detention Impr	ovements		
TO THE STATE OF TH	A CONTROL OF CONTROL COMMENT AND A SECOND CONTROL OF COMMENT	The second secon	and the state of t		
			A STATE OF THE STA	Contingency	
Facility	Storage (AF)	Construction Cost		Cost	Total Cost
SR-01	10	\$296,701		Cost \$133,516	\$430,217
SR-01 SR-02	10 5	\$296,701 \$207,949		Cost \$133,516 \$93,577	\$430,217 \$301,525
SR-01 SR-02 SR-03	10 5 16	\$296,701 \$207,949 \$186,252		Cost \$133,516 \$93,577 \$83,814	\$430,217 \$301,525 \$270,066
SR-01 SR-02 SR-03 SR-04	10 5 16 25	\$296,701 \$207,949 \$186,252 \$390,182		Cost \$133,516 \$93,577 \$83,814 \$175,582	\$430,217 \$301,525 \$270,066 \$565,764
SR-01 SR-02 SR-03 SR-04 SR-05	10 5 16 25 24	\$296,701 \$207,949 \$186,252 \$390,182 \$455,235		Cost \$133,516 \$93,577 \$83,814 \$175,582 \$204,856	\$430,217 \$301,525 \$270,066 \$565,764 \$660,091
SR-01 SR-02 SR-03 SR-04 SR-05 SR-06	10 5 16 25 24 9	\$296,701 \$207,949 \$186,252 \$390,182 \$455,235 \$140,670		\$133,516 \$93,577 \$83,814 \$175,582 \$204,856 \$63,301	\$430,217 \$301,525 \$270,066 \$565,764 \$660,091 \$203,971
SR-01 SR-02 SR-03 SR-04 SR-05 SR-06 SR-07	10 5 16 25 24 9 5	\$296,701 \$207,949 \$186,252 \$390,182 \$455,235 \$140,670 \$162,046		\$133,516 \$93,577 \$83,814 \$175,582 \$204,856 \$63,301 \$72,921	\$430,217 \$301,525 \$270,066 \$565,764 \$660,091 \$203,971 \$234,967
SR-01 SR-02 SR-03 SR-04 SR-05 SR-06 SR-07 SR-08	10 5 16 25 24 9 5	\$296,701 \$207,949 \$186,252 \$390,182 \$455,235 \$140,670 \$162,046 \$87,489		\$133,516 \$93,577 \$83,814 \$175,582 \$204,856 \$63,301 \$72,921 \$39,370	\$430,217 \$301,525 \$270,066 \$565,764 \$660,091 \$203,971 \$234,967 \$126,860
SR-01 SR-02 SR-03 SR-04 SR-05 SR-06 SR-07	10 5 16 25 24 9 5	\$296,701 \$207,949 \$186,252 \$390,182 \$455,235 \$140,670 \$162,046		Cost \$133,516 \$93,577 \$83,814 \$175,582 \$204,856 \$63,301 \$72,921 \$39,370 \$84,713	\$430,217 \$301,525 \$270,066 \$565,764 \$660,091 \$203,971 \$234,967 \$126,860 \$272,963
SR-01 SR-02 SR-03 SR-04 SR-05 SR-06 SR-07 SR-08 SR-09	10 5 16 25 24 9 5 5 5	\$296,701 \$207,949 \$186,252 \$390,182 \$455,235 \$140,670 \$162,046 \$87,489 \$188,250		Cost \$133,516 \$93,577 \$83,814 \$175,582 \$204,856 \$63,301 \$72,921 \$39,370 \$84,713 \$149,236	\$430,217 \$301,525 \$270,066 \$565,764 \$660,091 \$203,971 \$234,967 \$126,860 \$272,963 \$480,871
SR-01 SR-02 SR-03 SR-04 SR-05 SR-06 SR-07 SR-08 SR-09 SR-10 SR-11 SR-11	10 5 16 25 24 9 5 5 20 23 2	\$296,701 \$207,949 \$186,252 \$390,182 \$455,235 \$140,670 \$162,046 \$87,489 \$188,250 \$331,635		Cost \$133,516 \$93,577 \$83,814 \$175,582 \$204,856 \$63,301 \$72,921 \$39,370 \$84,713	\$430,217 \$301,525 \$270,066 \$565,764 \$660,091 \$203,971 \$234,967 \$126,860 \$272,963
SR-01 SR-02 SR-03 SR-04 SR-05 SR-06 SR-07 SR-08 SR-09 SR-10 SR-11 SR-12 SR-13	10 5 16 25 24 9 5 5 5 20 23 2 9 3	\$296,701 \$207,949 \$186,252 \$390,182 \$455,235 \$140,670 \$162,046 \$87,489 \$188,250 \$331,635 \$56,880		Cost \$133,516 \$93,577 \$83,814 \$175,582 \$204,856 \$63,301 \$72,921 \$39,370 \$84,713 \$149,236 \$25,596	\$430,217 \$301,525 \$270,066 \$565,764 \$660,091 \$203,971 \$234,967 \$126,860 \$272,963 \$480,871 \$82,476
SR-01 SR-02 SR-03 SR-04 SR-05 SR-06 SR-07 SR-08 SR-09 SR-10 SR-11 SR-11	10 5 16 25 24 9 5 5 20 23 2 9 3	\$296,701 \$207,949 \$186,252 \$390,182 \$455,235 \$140,670 \$162,046 \$87,489 \$188,250 \$331,635 \$56,880 \$108,987		\$133,516 \$93,577 \$83,814 \$175,582 \$204,856 \$63,301 \$72,921 \$39,370 \$84,713 \$149,236 \$25,596 \$49,044	\$430,217 \$301,525 \$270,066 \$565,764 \$660,091 \$203,971 \$234,967 \$126,860 \$272,963 \$480,871 \$82,476 \$158,031

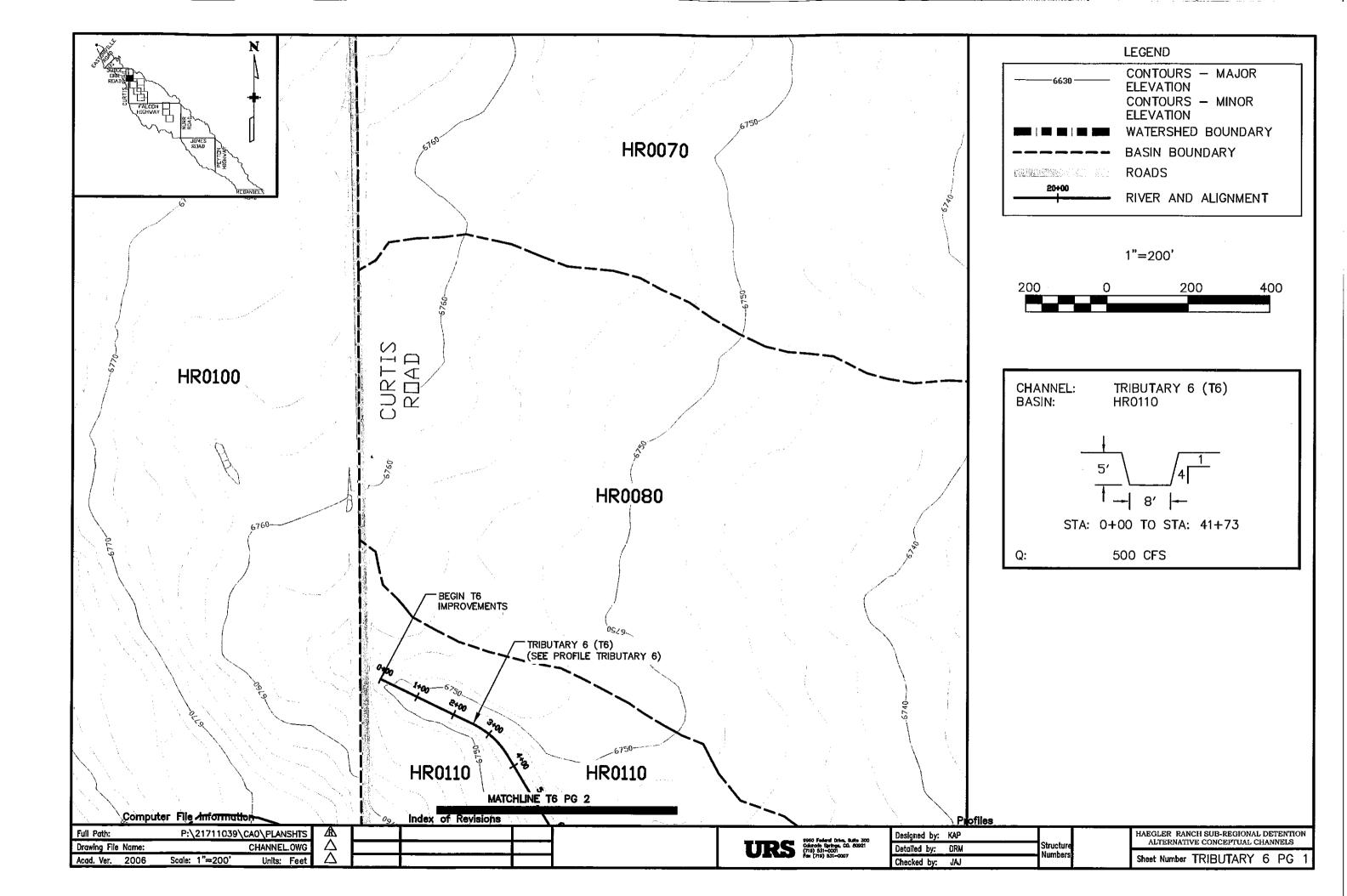


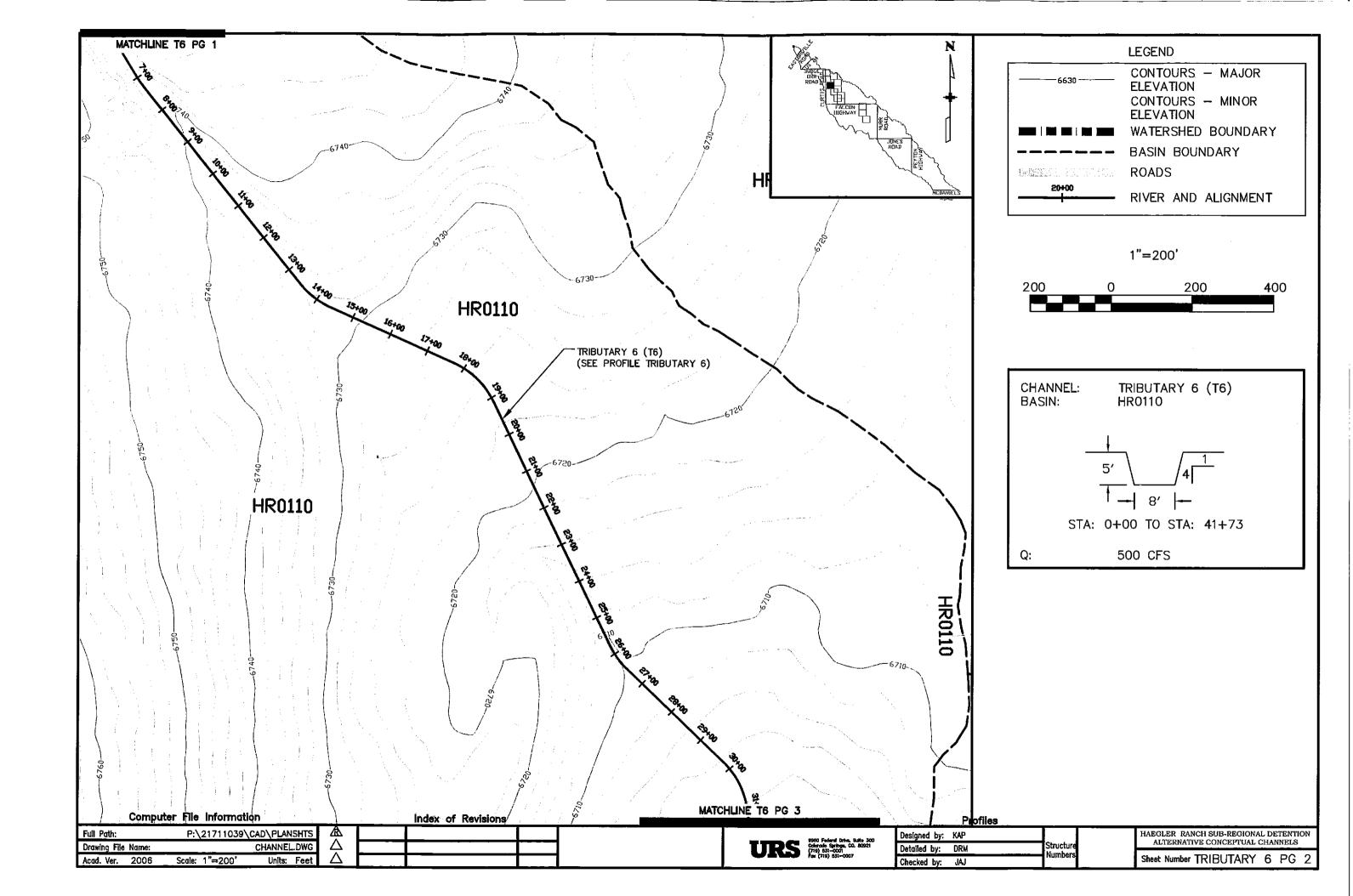


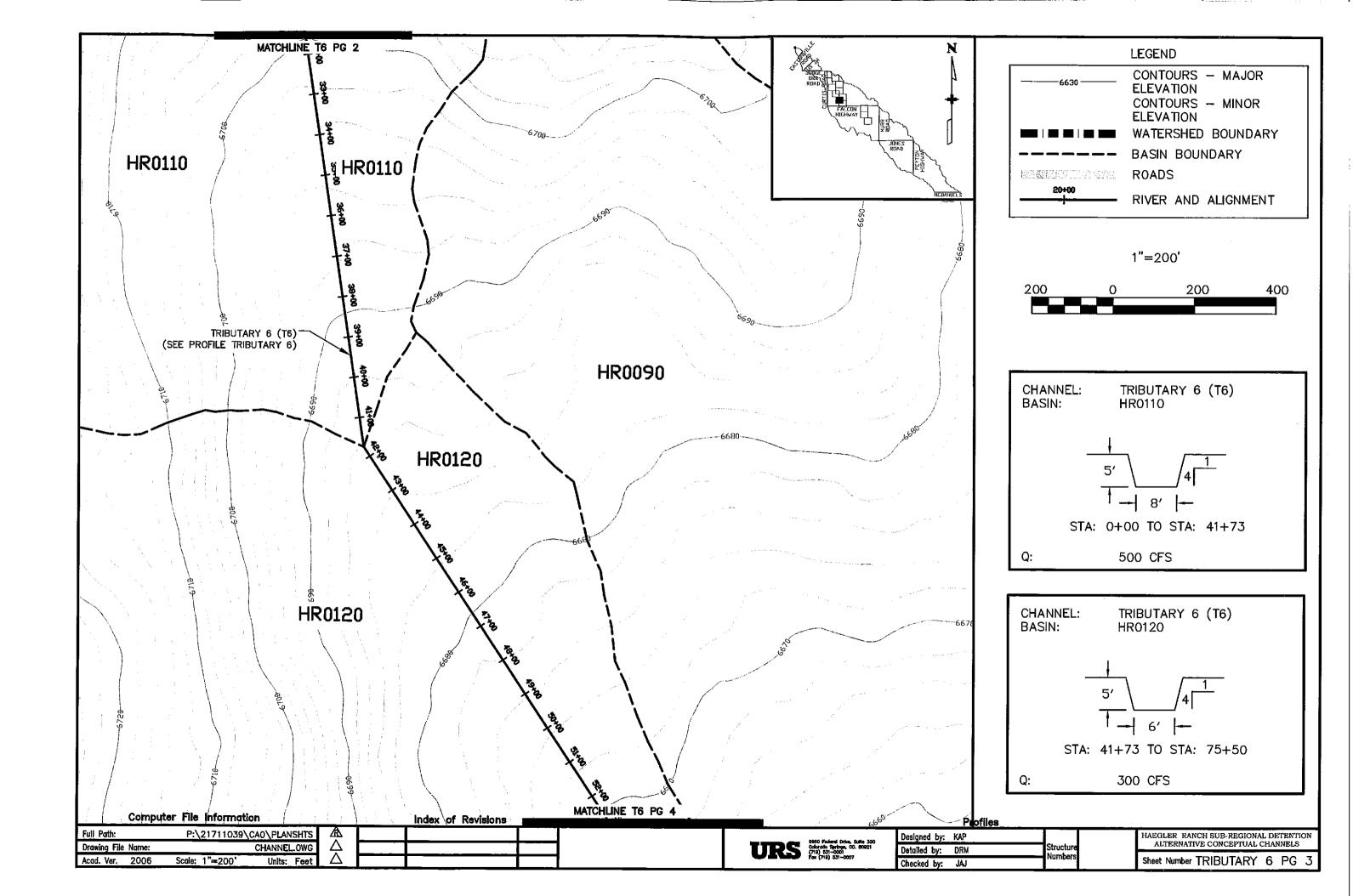


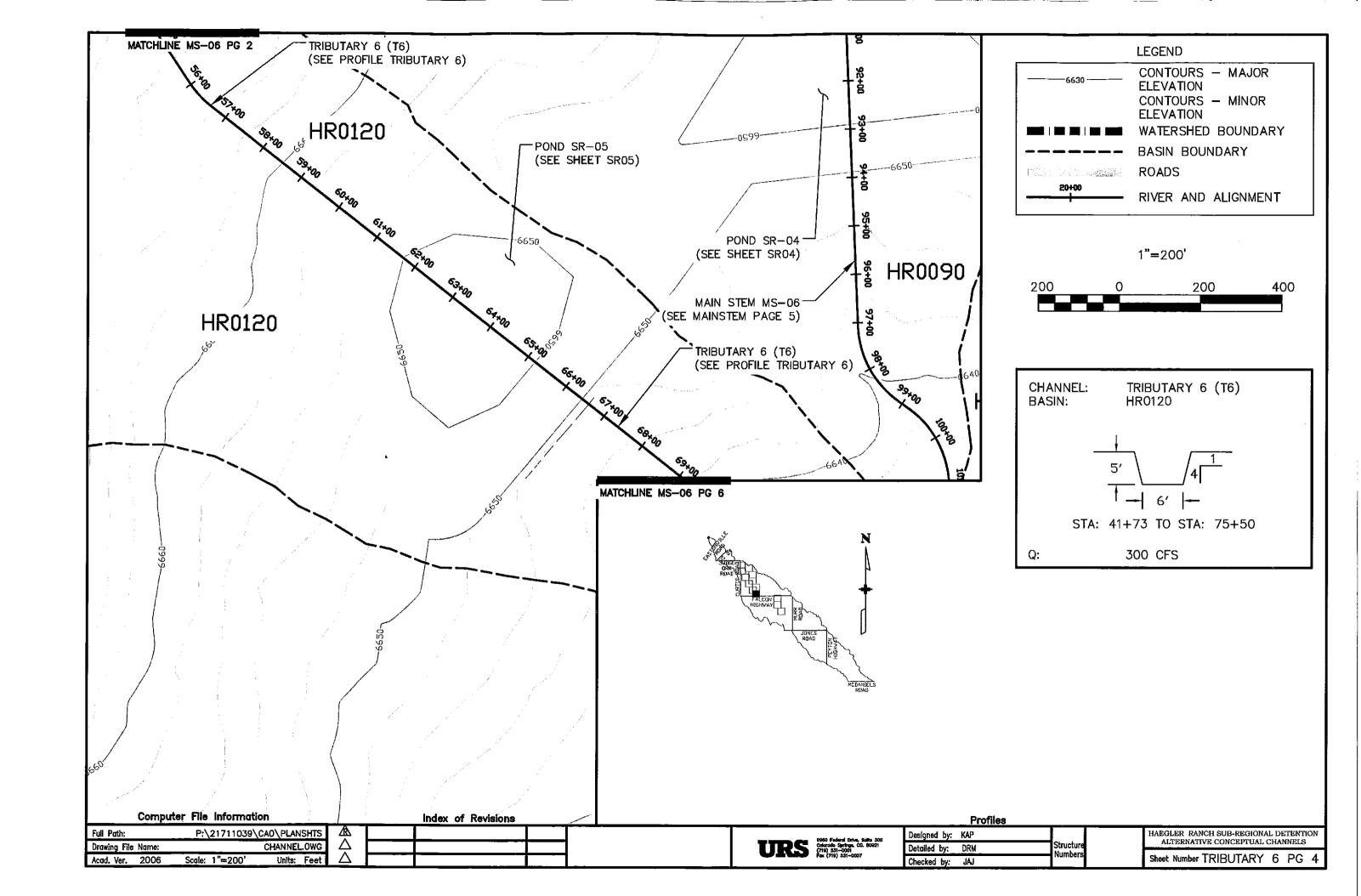












MS-06 HR0070

SLOPE = 0.60%

(7) 4' DROPS

MS-06 HR0080

SLOPE = 0.60%

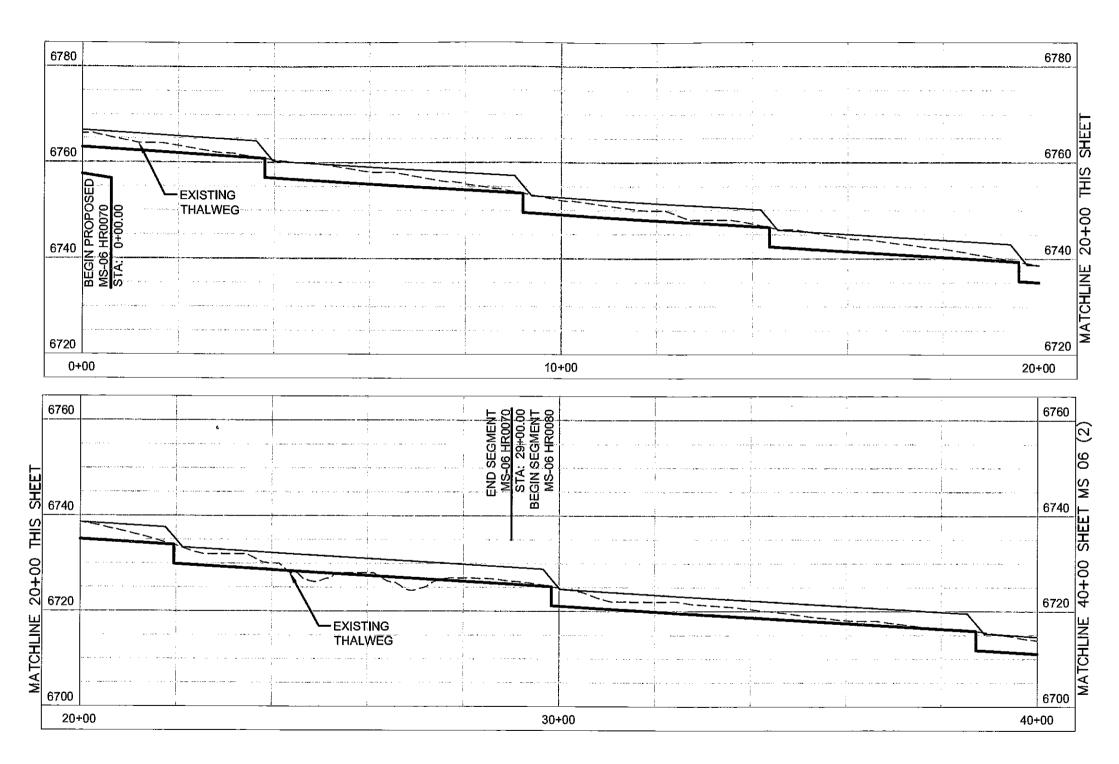
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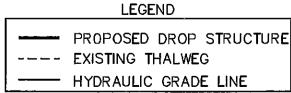
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Units: Feet

(7) 4' DROPS

PROFILE MAIN STEM (MS-06 & MS-05)





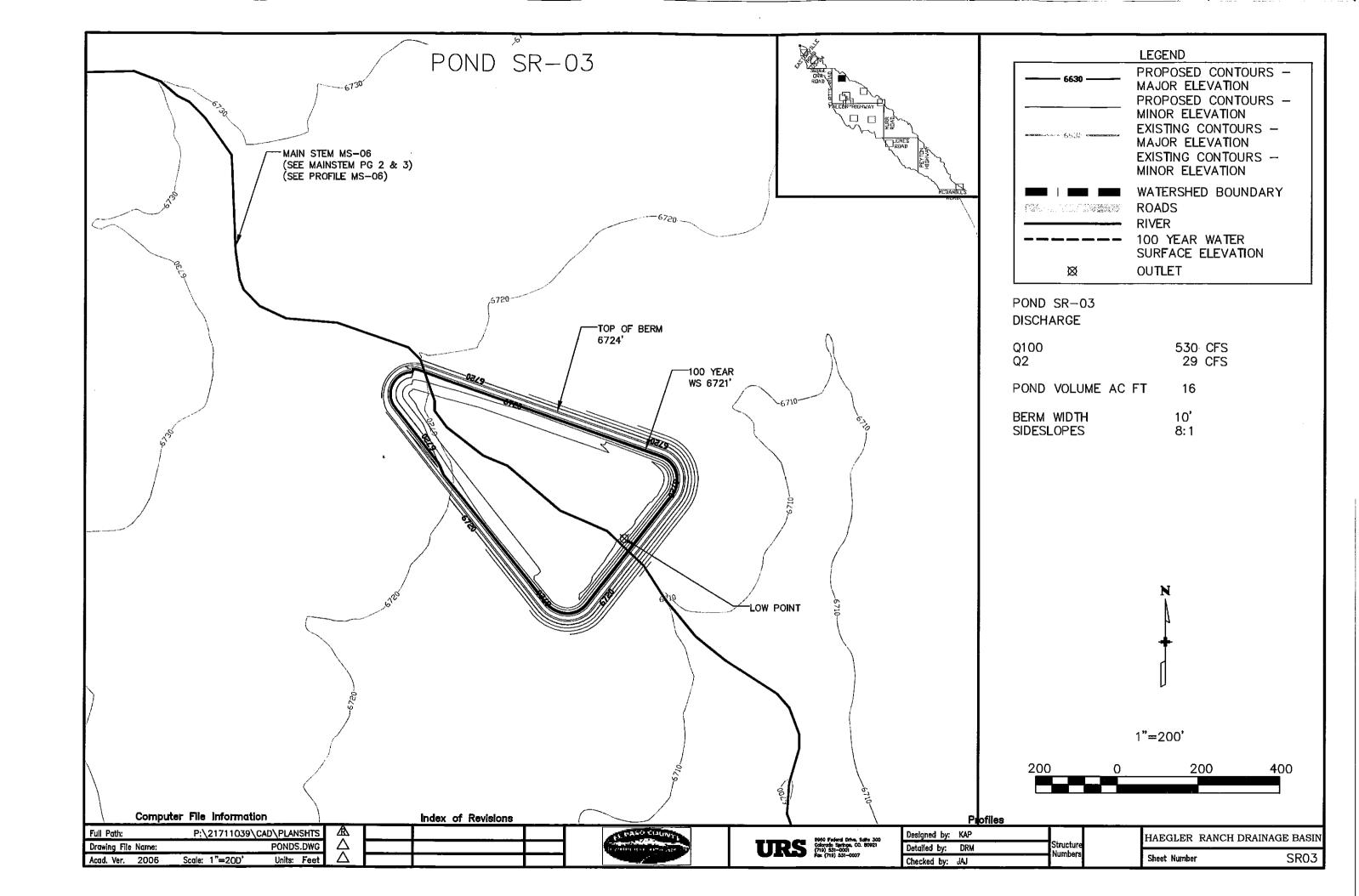
Computer File Information Index of Revisions **Profiles** P:\21711039\CAD\PLANSHTS Α. Δ. Designed by: KAP URS (749) 231-0007 Drawing File Name: MAINSTEM PROFILES_PROPOSED.DWG Detailed by: DRM

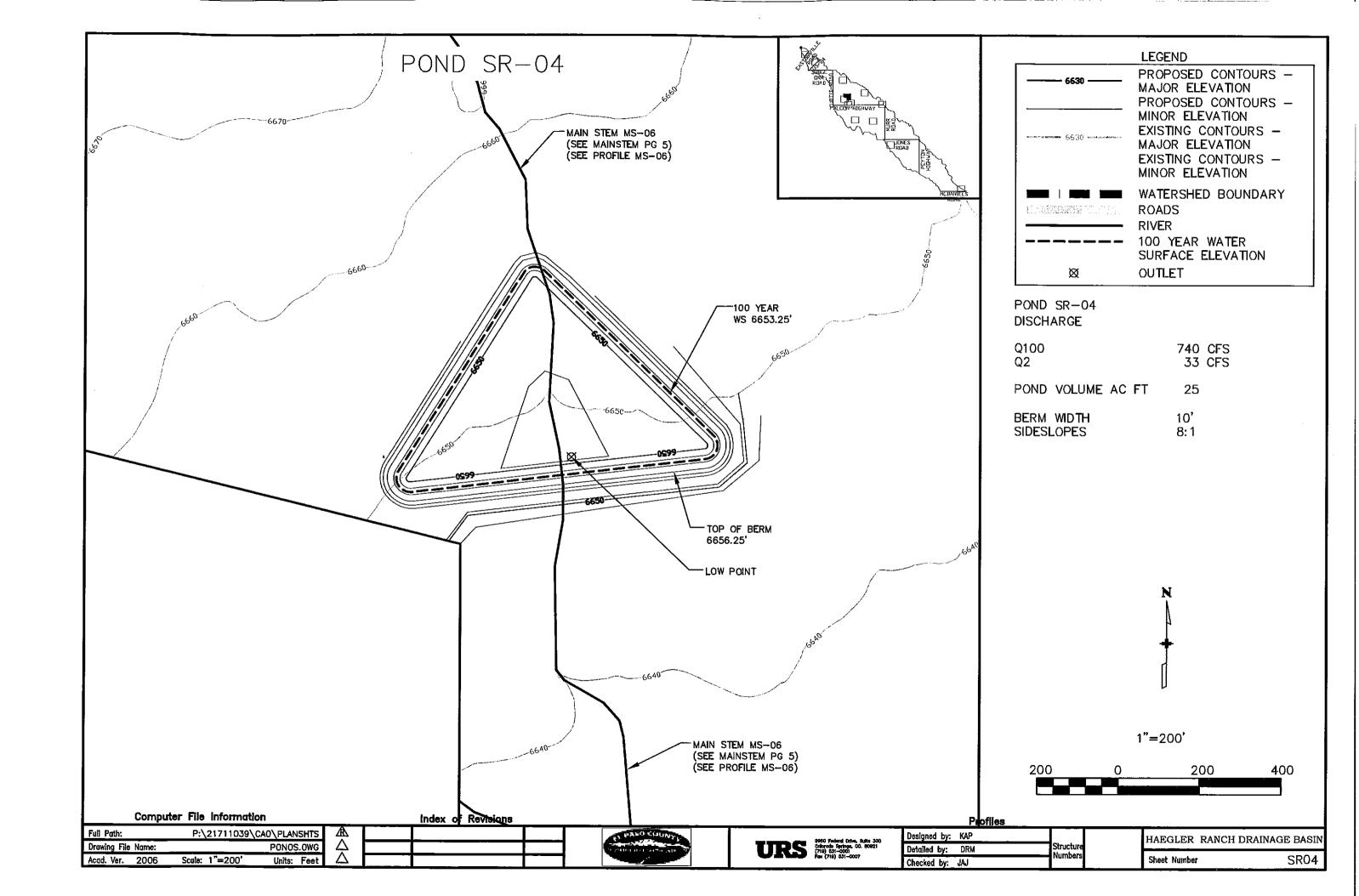
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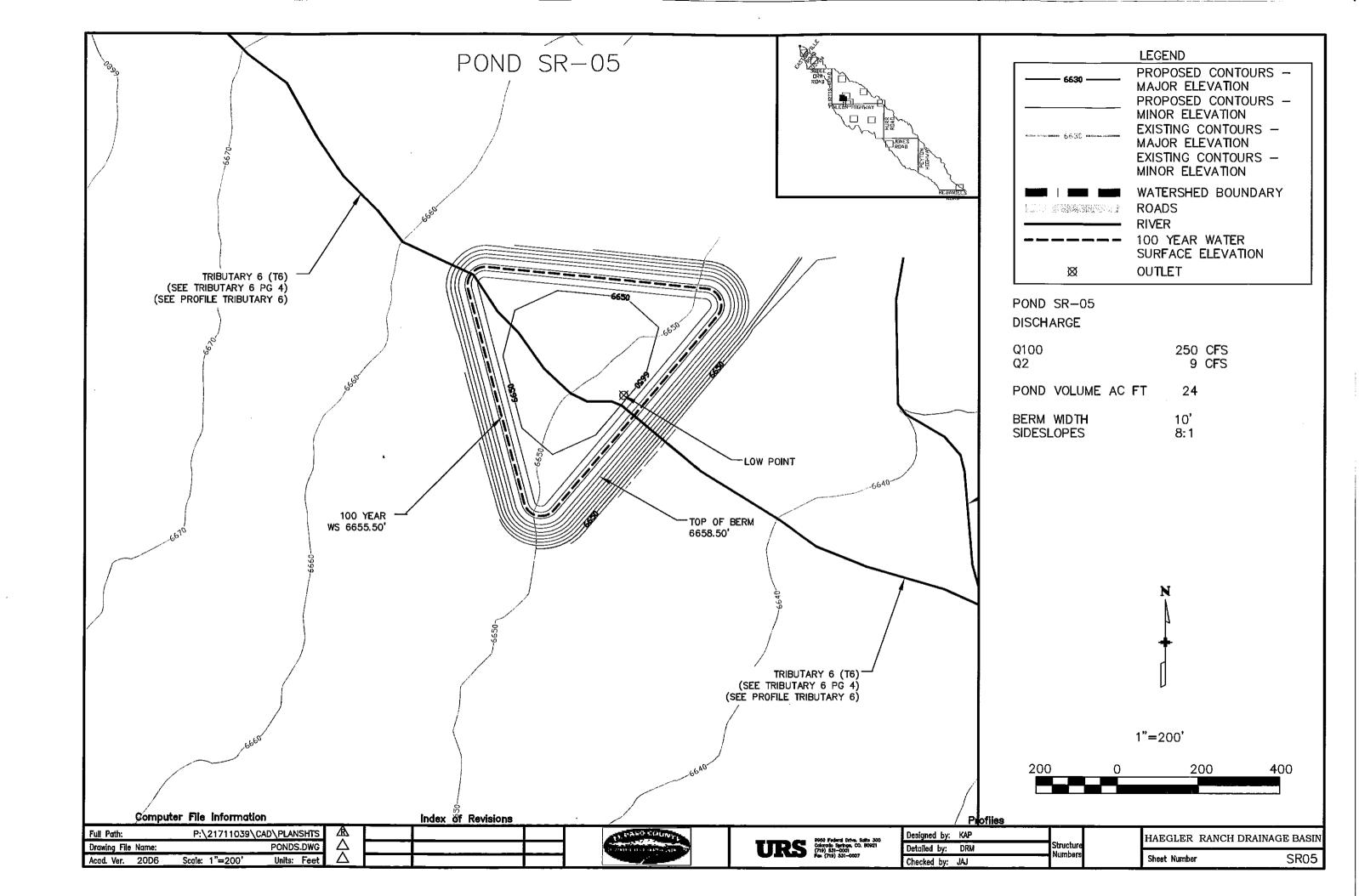
HAEGLER RANCH SUB-REGIONAL DETENTION ALTERNATIVE CONCEPTUAL PROFILES Structure Sheet Number MS 06

MS-06 HR0080 PROFILE MAIN STEM (MS-06 & MS-05) SLOPE = 0.60%(7) 4' DROPS 6720 6720 MS-06 HR0090 SLOPE = 0.60%EXISTING THALWEG S 8700 CF (8) 4' DROPS 40+00 SHEET N 6689 6680 6680 MATCHLINE MATCHLINE 6660 40+00 50+00 60+00 6700 6700 - EXISTING THALWEG SHEET 6680 SE SHEET SHEET THIS 00+09 6660 00+08 6660 MATCHLINE (MATCHLINE 6640 60+00 70+00 80+00 **LEGEND** PROPOSED DROP STRUCTURE EXISTING THALWEG HYDRAULIC GRADE LINE Computer File Information Index of Revisions **Profiles** P:\21711039\CAD\PLANSHTS Æ Designed by: KAP HAEGLER RANCH SUB-REGIONAL DETENTION ALTERNATIVE CONCEPTUAL PROFILES Δ Drawing File Name: MAINSTEM PROFILES_PROPOSEO.OWG Detailed by: DRM Sheet Number MS06 (2 Checked by:

MS-06 HR0090 PROFILE MAIN STEM (MS-06 & MS-05) SLOPE = 0.60%(8) 4' DROPS 6680 6680 MS 06 (2) HR0200 MS-05 SLOPE = 0.40%(4) 4' DROPS 6660 80+00 SHEET 6640 6660 MATCHLINE MATCHLINE **EXISTING** THALWEG 6620 6620 80+00 90+00 100+00 6660 6660 SHEET END SEGMENT MS-05 HR0200 STA: 11/9+46.00 6640 6640 -EXISTING 100+00 THALWEG 6620 6620 MATCHLINE 6600 6600 100+00 110+00 120+00 LEGEND PROPOSED DROP STRUCTURE EXISTING THALWEG HYDRAULIC GRADE LINE Computer File Information Index of Revisione **Profiles** <u>A</u> △ △ Full Path: P:\21711039\CAD\PLANSHTS HAEGLER RANCH SUB-REGIONAL DETENTION Designed by: KAP URS 9960 Federal Driva, Suita 300 Cederado Sertinga, Cú. 80921 (719) 831-0001 Fac (719) 831-0007 ALTERNATIVE CONCEPTUAL PROFILES Drawing File Name: MAINSTEM PROFILES_PROPOSED.DWG Detailed by: DRM Sheet Number MS06 & MS05 Acad. Ver. 2006 Scale: 1"=20' Units: Feet Checked by:





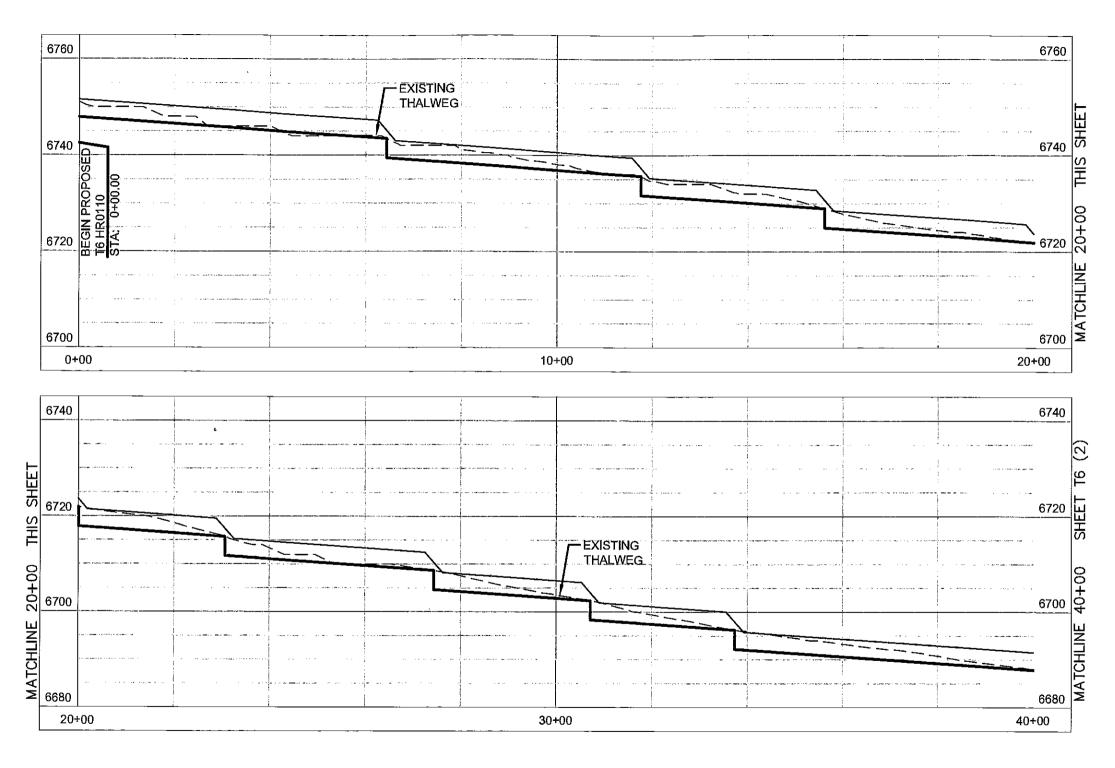


T6 HR0110

SLOPE = 0.70%

(9) 4' DROPS

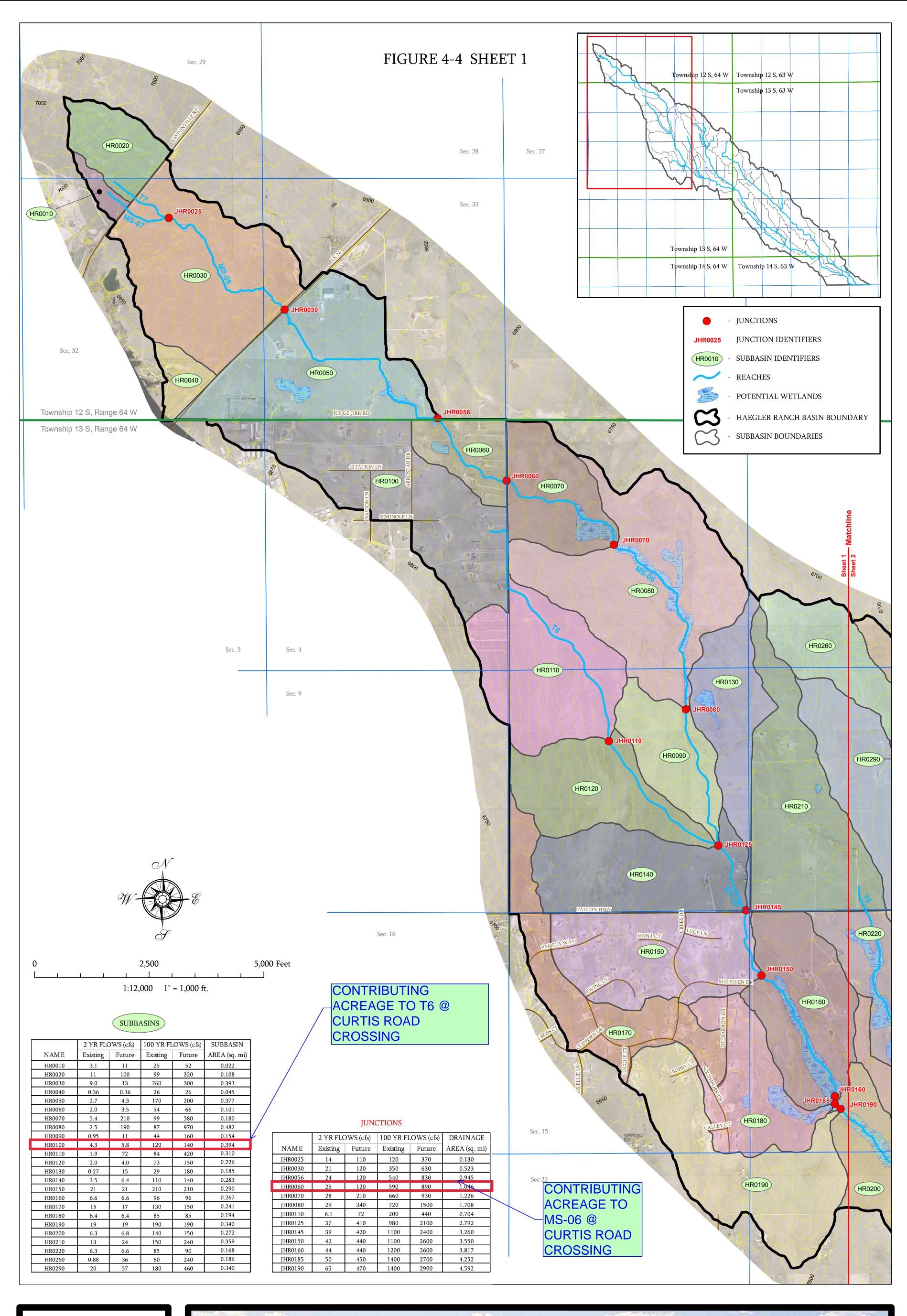
PROFILE TRIBUTARY 6 (T6)





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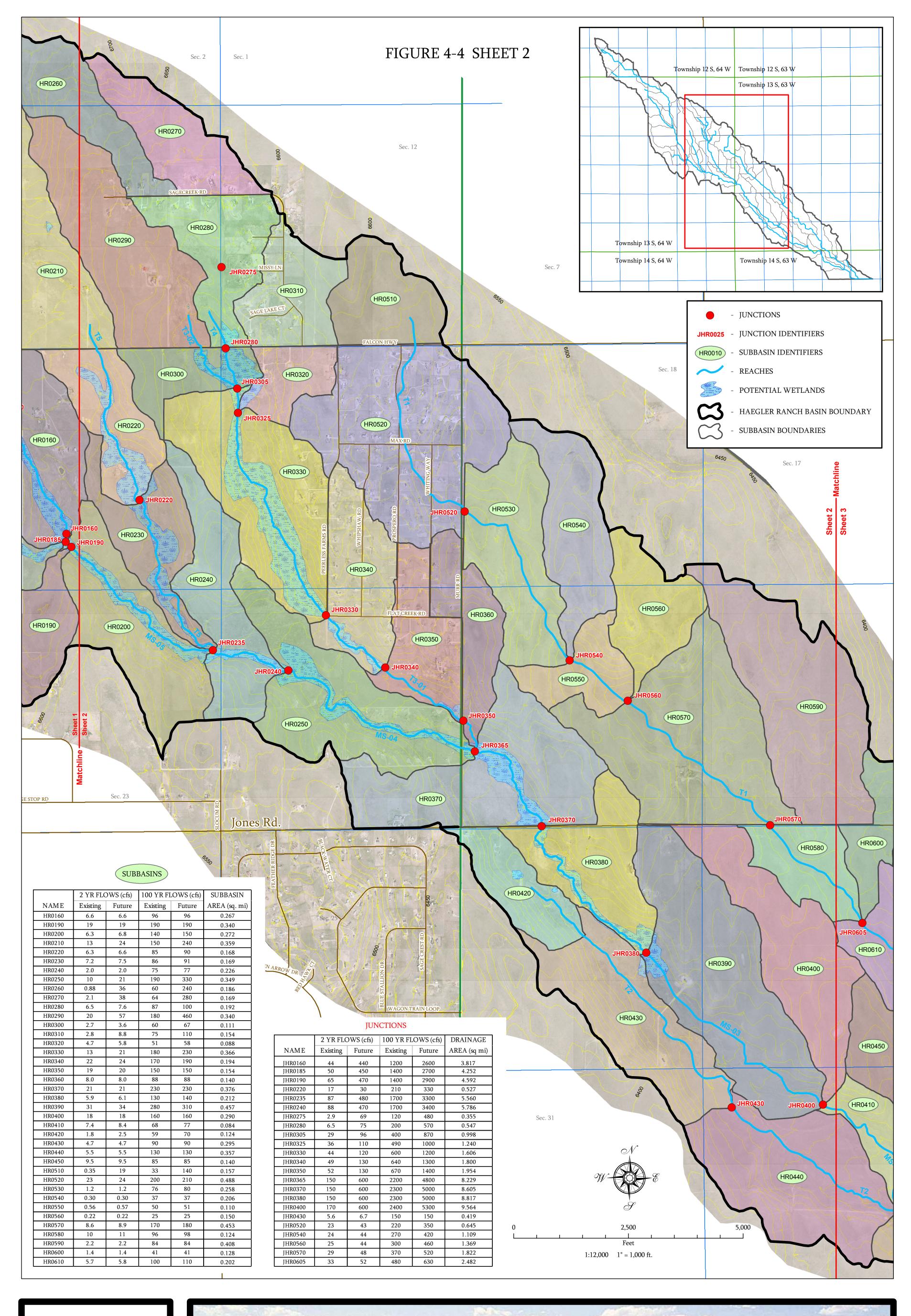




HAEGLER RANCH DRAINAGE BASIN

EXISTING AND FUTURE CONDITIONS HYDROLOGIC MODEL

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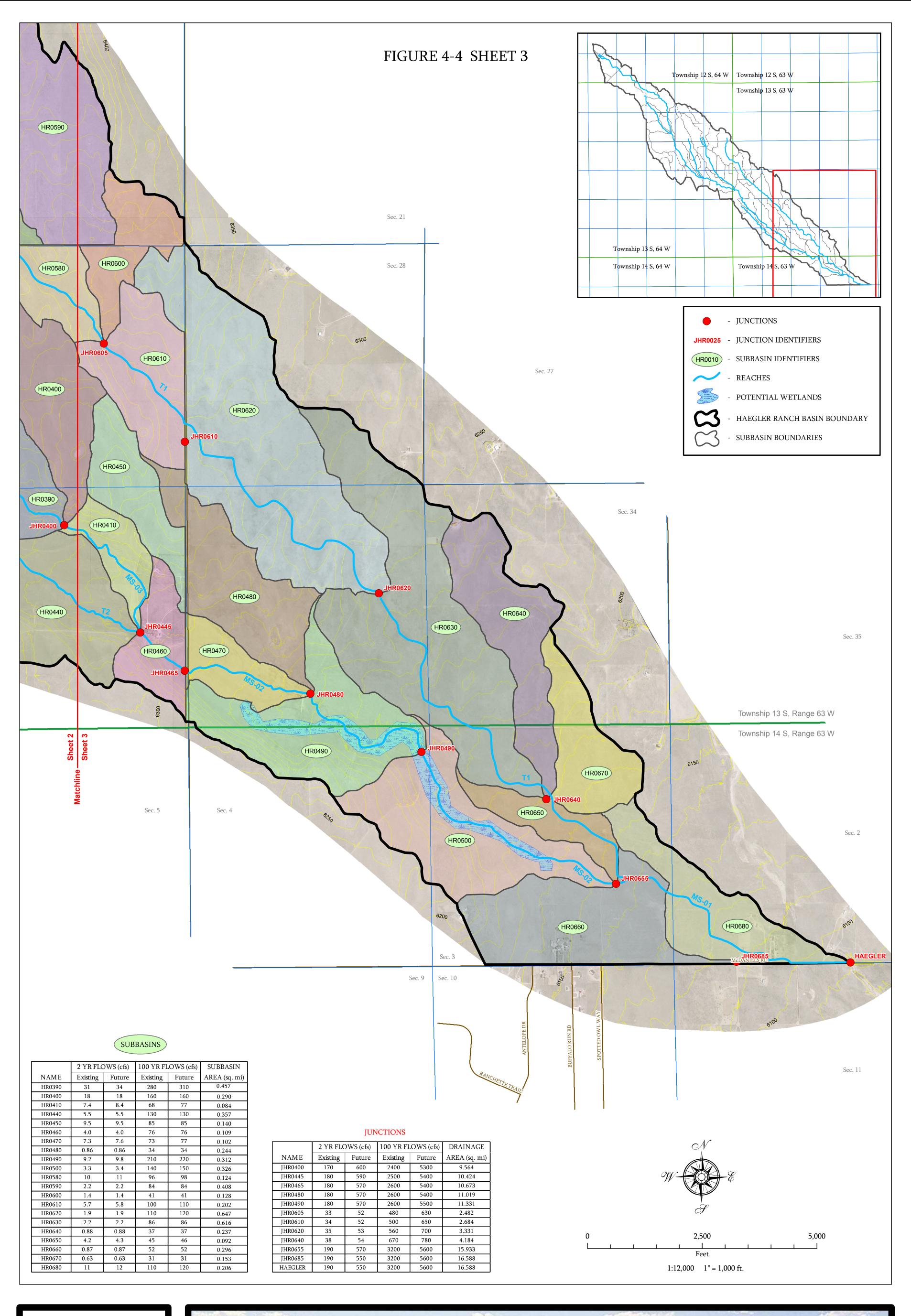




HAEGLER RANCH DRAINAGE BASIN

EXISTING AND FUTURE CONDITIONS HYDROLOGIC MODEL

URS NO. 21711039 DATE: 09/08





HAEGLER RANCH DRAINAGE BASIN

EXISTING AND FUTURE CONDITIONS HYDROLOGIC MODEL

URS NO. 21711039 DATE: 09/08

MASTER DEVELOPMENT DRAINAGE PLAN and PRELIMINARY DRAINAGE REPORT FOR SADDLEHORN RANCH

Prepared For: ROI Property Group, LLC 2495 Rigdon Street Napa, CA 94558 (707) 365-6891

> May 8, 2020 Project No. 25142.00

Prepared By: JR Engineering, LLC 5475 Tech Center Drive Colorado Springs, CO 80919 719-593-2593

El Paso County PCD File No. SP-19-006

ENGINEER'S STATEMENT:

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by El Paso County for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors, or omissions on my part in preparing this report.

Mike Bramlett, Colora For and On Behalf of J		Date
DEVELOPER'S STA I, the developer, have report and plan.		the requirements specified in this drainage
Business Name:	ROI Property Group, LI	<u>.C</u>
By:		
Title: Address:	2495 Rigdon Street Napa, CA 94558	
		so County Land Development Code, neering Criteria Manual, as amended.
Jennifer Irvine, P.E. County Engineer/ ECN	✓ Administrator	Date
Conditions:		



CONTENTS

PURPOSE	1
GENERAL LOCATION AND DESCRIPTION	1
LOCATION DESCRIPTION OF PROPERTY FLOODPLAIN STATEMENT	1
DRAINAGE BASINS AND SUBBASINS	2
Major Basin Descriptions Existing Sub-basin Drainage Proposed Sub-basin Drainage	5
DRAINAGE DESIGN CRITERIA	12
Development Criteria Reference Hydrologic Criteria Hydraulic Criteria	12
DRAINAGE FACILITY DESIGN	13
GENERAL CONCEPT SPECIFIC DETAILS Four Step Process to Minimize Adverse Impacts of Urbanization Water Quality Erosion Control Plan Operation & Maintenance Drainage and Bridge Fees. Construction Cost Opinion	
SUMMARY	17
REFERENCES:	18
APPENDICES A. Figures and Exhibits B. Hydrologic Calculations C. Hydraulic Calculations D. Detention and Water Quality Calculations E. Reference Materials F. Drainage Maps	
LIST OF TABLES:	
Existing Drainage Basin Summary	

- 2. Major Drainageway Naming Conventions
- 3. Major Drainageway Flow Comparison
- 4. Pond Summary
- 5. Site Composite Percent Imperviousness
- 6. Drainage & Bridge Fees



Page ii

PURPOSE

This document is the Master Development Drainage Plan (MDDP)/Preliminary Drainage Report (PDR) for the proposed Saddlehorn Ranch. The purpose of this report is to:

- 1. Identify on-site and off-site drainage patterns.
- 2. Recommend preliminary storm water facilities to collect and convey storm runoff from the proposed development to appropriate discharge and/or detention locations.
- 3. Recommend preliminary water quality and detention facilities to control discharge release rates to below historic.
- 4. Demonstrate compliance with surrounding major drainage basin planning studies, master plan and flood insurance studies.

GENERAL LOCATION AND DESCRIPTION

Location

The proposed Saddlehorn Ranch, known as "the site" from herein, is a parcel of land located in Section 3 and 10, Township 13 South, Range 65 West of the 6th Principal Meridian in El Paso County, Colorado. The proposed 824 acre, rural, single family-development is bound by Judge Orr Road to the North and Curtis Road to the West. To the East, the site is bound by undeveloped land owned by Brent Houser Enterprises, LLC. To the south, the site is bound by undeveloped properties owned by 7120 Sudiev, LLC and Faye Reyonlds. A vicinity map and property owner map is presented in Appendix A.

Currently, there are three major drainageways that run through the site: Haegler Ranch Main Stem 6 (MS-06), Haegler Ranch Tributary 6 (T-6), and Gieck Ranch West Fork – Reach 7A (WF-R7A). These drainageways were analyzed, both hydrologically and hydraulically, in the following reports:

- 1. Geick Ranch Drainage Basin Planning Study (DBPS), October 2007
- 2. Haegler Ranch Basin DBPS, May 2009
- Sante Fe Springs Haegler Ranch Drainage Basin Letter of Map Revision (LOMR), October 2004

The impact of these drainageways and planning studies on the proposed development will be discussed later in the report.

Description of Property

The proposed development contains approximately 824 acres and will be comprised of 227 rural 2.5 – 5 acre lots. The site is currently unoccupied and undeveloped. The existing ground cover is sparse vegetation and open space, typical of a Colorado rolling range land condition. In general, the site slopes from northwest to southeast and the existing drainageways follow this topography.

Per a NRCS web soil survey of the area, the site is made up of Type A, B and D soils. Type A soils cover roughly 80% of the site while Type B soils cover 3% and Type D cover the remaining 17% of the site. Group A soils have a high infiltration rate when thoroughly wet. Type B soils have a moderate infiltration when thoroughly wet. Type D soils have a very slow infiltration rate when thoroughly wet and have a high shrink-swell potential. A NRCS soil survey map has been presented in Appendix A.

Two existing wells are located in the southwest corner of the site. A 12" Cherokee Metropolitan District waterline runs through the site just south of the northern property line. Approximately a mile south of the Curtis Road and Judge Orr Road intersection, a two lane dirt road proceeds from Curtis Road east towards approximate center of the site. A water tank, pond and windmill are located within Major Drainageway MS-06 at the end of the dirt road.

Floodplain Statement

Based on the FEMA FIRM Map number 08041C0558G, dated December 7, 2018, the site lies within Zone A, Zone AE, and Zone X. Zone A is defined as areas subject to inundation by the 1-percent-annual-chance flood determined using approximate methodologies because BFEs have not been established. Zone AE is defined as area subject to inundation by the 1-percent-annual-chance flood event. Zone X is defined as area outside the Special Flood Hazard Area (SFHA) and higher than the elevation of the 0.2-percent-annual-chance (or 500-year) flood. All proposed development within the site will occur in Zone X.

In the northeast corner of the site, proposed development borders the Zone A boundary of the Geick Ranch West Tributary (WF-R7). At time of Final Drainage Report for this future phase of the development, a LOMR will be presented to establish base flood elevations (BFEs) for all lots that border the current Zone A boundary. The current FIRM Map has been presented in Appendix A.

Drainage Basins and Subbasins

Major Basin Descriptions

The site lies within two major drainage basins: the Gieck Ranch Drainage Basin based on the "Gieck Ranch Drainage Basin Planning Study" (DBPS) prepared by Drexel, Barrell & Co. in October, 2007 and revised in February 2010 and the Haegler Ranch Drainage Basin based on the "Haegler Ranch Drainage Basin Planning Study" prepared by URS Corporation in May 2009.

The Gieck Ranch Drainage Basin covers approximately 22 square miles and begins approximately five miles northeast of the Town of Falcon and travels approximately 15 miles to the southeast. The Gieck Ranch Drainage Basin is tributary to Black Squirrel Creek which drains south to the Arkansas River near the city of Pueblo, Colorado. The majority of the area within the basin is undeveloped and is characterized as rolling range land typically associated with Colorado's semi-arid climates.

Anticipated land use for the basin includes residential, industrial, agricultural and commercial development. Residential developments will range from 0.125 - 5 acre lots with a mix of low, medium and high density developments.

The Haegler Ranch Drainage Basin covers approximately 16.6 square miles in unincorporated El Paso County, CO. The Haegler Ranch Drainage Basin is tributary to Black Squirrel Creek. In its existing condition, the basin is comprised of rolling rangeland with poor vegetative cover associated with Colorado's semi-arid climate. The natural drainageways within the basin are typically shallow and wide with poorly defined flow paths in most areas. Anticipated land use for the basin includes residential and commercial development. Residential developments will range from 0.125 – 5 acre lots with a mix of low, medium and high density developments.

As part of its drainage research, JR Engineering reviewed the following drainage studies, reports and LOMRs:

- Gieck Ranch Drainage Basin Planning Study prepared by Drexel, Barrell & Co. in October, 2007 and revised in February 2010. (Not adopted by El Paso County as of July 2019)
- Haegler Ranch Drainage Basin Planning Study prepared by URS Corporation in May 2009
- Santa Fe Springs Haegler Ranch Drainage Basin Letter of Map Revision prepared by Tri-Core Engineering in June 2004.

Existing Gieck Ranch Drainage Basin

The "Gieck Ranch Drainage Basin Planning Study" evaluated existing and future drainage conditions, identified future improvements, and established basin and bridge fees for the Gieck Ranch Drainage Basin. It should be noted that as of today the "Gieck Ranch Drainage Basin Planning Study" has not yet been approved and adopted by the County. All referenced information from the aforementioned report is presented for information purposes only.

Based upon provided drainage maps and analysis, Gieck Ranch discharges a total of 1,017 cfs onto the site within Major Drainageway Gieck Ranch West Fork Reach 7A (WF-R7A). An existing 66" CMP and 36" CMP convey the offsite flow across Judge Orr Road onto the site. The existing culverts at Judge Orr Road are undersized for existing and future flows resulting in localized overtopping. The DBPS recommends the culvert be upsized to four –12' x 5' box culverts. The culvert will not be upsized within the context of this report and development. The culvert is owned by El Paso County and timing of the recommended improvements will be controlled by the County. The overtopping at the intersection of WF-R7A is not contained within the 100-year floodplain. Therefore, at time of Final Drainage Report, berming will be provided that will protect proposed lots from overtopping flows. An overtopping analysis is presented in Appendix D and the limits of overtopping are presented on the existing and proposed drainage maps in Appendix F.

Based on existing channel analysis, the *Gieck Ranch DBPS* recommends WF-R7A channel improvements approximately 200' upstream and 300' downstream of the culvert crossing at Judge Orr Road (50' bottom width, 10:1 side slopes and vegetative augmentation). The recommended

channel improvements result from upsizing the culvert at Judge Orr Road, requiring the channel to be lowered. The channel improvements were not recommended due to existing channel instability. Existing velocities in the channel were found to be 2.19 ft/s, as presented in Appendix E. Per the MS4 permit requirements, the onsite reach of WF-R7A will be analyzed for channel stability with the corresponding Final Drainage Report for that phase of the development. At the time of Final Drainage Report, any necessary improvements to WF-R7A to satisfy the MS4 permit will be evaluated. It should be noted that the onsite reach of WF-R7A, where the aforementioned channel improvements were recommended, is comprised of jurisdictional wetlands which will limit the allowable improvements. Coordination with the Army Corps of Engineers will be required to grant permission to disturb the jurisdictional wetlands. Recommended channel improvements from the *Gieck Ranch DBPS* are presented in Appendix E.

Existing Haegler Ranch Drainage Basin

The "Haegler Ranch Drainage Basin Planning Study" was used to establish a stormwater management plan for the existing and future stormwater infrastructure needs within the Haegler Ranch Drainage Basin. Based on provided drainage maps and analysis, in the existing condition Haegler Ranch contributes a total of 710 cfs onto the site. Of the 710 cfs, 590 cfs crosses Curtis Road in an existing 24" CMP onto the site. Major Drainageway MS-06 conveys the stormwater through the site and to its off-site confluence with Major Drainageway MS-05. The remaining 210 cfs crosses Curtis Road in an existing 36" CMP onto the site. Major Drainageway T-6 conveys the stormwater through the site and to its off-site confluence with Major Drainageway MS-05. Both Curtis Road culverts are undersized for existing and future flows and overtopping occurs locally near the culvert crossings. Overtopping at the intersection of Curtis Road and T-6 is contained within the 100-year floodplain and will not affect proposed lots. The overtopping at the intersection of MS-06 and Curtis Road is not contained within the 100-year floodplain limits. Therefore, at time of Final Drainage Report, berming will be provided that will protect proposed lots from overtopping flows. An overtopping analysis is presented in Appendix D and the limits of overtopping are presented on the existing and proposed drainage maps in Appendix F.

The culverts are not proposed to be upsized within the context of this report and development. The culverts are owned by El Paso County and timing of the recommended improvements will be controlled by the County.

Furthermore, the *Haegler Ranch DBPS* recommends channel improvements within drainageways MS-06 and T-6. Per the *Haegler Ranch DBPS*, all recommended channel sections are trapezoidal with side slopes of 4:1 and a maximum depth of five feet. Within the limits of the site, three (3) channel bottom widths are recommended for MS-06. The first reach, from station 0+00 – 31+34, is proposed with a 15' bottom width, the second reach from 31+34 to 74+61, MS-06 is proposed with a 30' bottom width, and the last reach from station 74+61 - 103+62 is proposed with a 20' channel bottom. The *Haegler Ranch DBPS* recommends Major Drainageway T-6 be improved to a trapezoidal channel with an 8' bottom width, 4:1 side slopes and depth of 5'. Drop structures have

also been recommended within MS-06 and T-6. These improvements will not occur within the context of this report or development. However, due to the addition of culvert crossings within MS-06 and T-6, channel improvements are anticipated up and downstream of the proposed culverts. The extent of these channel improvements will be addressed with corresponding Final Drainage Reports for those phases of the development. At that time, channel stability will be evaluated and any necessary improvements will be proposed. Recommended channel improvements from the *Haegler Ranch DBPS* are presented in Appendix E.

Based on flood impacts, stream stability and cost effectiveness, this study recommended a sub-regional detention approach. This allows future development anywhere in the basin with the construction of an associated sub-regional pond. Within the boundary of Saddlehorn Ranch, the DBPS recommended a total of three (3) sub-regional ponds. Based on discussion with El Paso County, the site will utilize full spectrum water quality and detention ponds instead. These full spectrum detention ponds will limit developed discharge into the drainageways to less than historic rates. Future, upstream development will also require full spectrum detention in accordance with current El Paso County criteria, which is an effective alternative to the sub-regional pond approach.

The Santa Fe Springs – Haegler Ranch Drainage Basin LOMR was executed on Haegler Ranch Tributary 2, 3, and 4. The LOMR revised the onsite effective flood zones from Zone A to Zone AE for the three drainageways. Upstream stretches of Tributary 3 and 4 are classified Zone A but those channel reaches are off site. All stretches of Tributary 3 and 4 onsite are Zone AE. See FIRM Map Panel 080059-0575G for limits of LOMR study and revised flood zones, presented in Appendix E.

Existing Sub-basin Drainage

On-site, existing drainage patterns are generally from northwest to southeast by way of existing, natural drainageways (MS-06, T-6, WF-R7A). On-site areas flow directly into these drainageways which also bypass off-site flows through the site. Offsite flows within the major drainageways that pass through the site will influence the on-site culvert designs and any channel improvements.

On-site, existing drainage basins were established based upon existing topography and the limits of 100-year floodplain. The site was divided into eleven existing sub-basins. See Table 1 below for summary of existing drainage sub-basins and corresponding peak flows. An existing drainage map is provided in Appendix F.

Table 1: Existing Drainage Basin Summary

EXIST	EXISTING BASIN SUMMARY TABLE					
Tributary Sub-Basin	Area (acres)	Percent Impervious	Q ₅ (cfs)	Q ₁₀₀ (cfs)		
G1	10.1	2.0%	0.00	0.1		
G2	87.6	2.0%	1.5	76.4		
H1	166.5	2.0%	0.1	81.0		
H2	111.1	2.0%	0.2	91.1		
Н3	118.9	2.0%	0.9	64.1		
H4	63.3	2.0%	1.4	73.2		
H5	53.2	2.0%	0.3	28.2		
H6	87.6	2.0%	0.2	110.1		
CH1	23.9	2.0%	5.4	21.0		
CH2	84.2	2.0%	2.6	33.7		
CH3	19.1	2.0%	0.1	6.5		
Total	825.4	N/A	12.7	585.4		

The existing condition of the three major drainageways are discussed below;

Existing Geick Ranch West Fork Reach 7A (WF-R7A)

The first major drainageway is the Gieck Ranch West Fork Reach 7A (WF-R7A), per the *Gieck Ranch DBPS*. WF-R7A crosses onto the site along Judge Orr Road, approximately ¼ mile west of the intersection with Elbert Road. Discharge from the developed site into this drainageway will be limited to historic rates via a full spectrum detention pond prior to discharge. This drainageway includes jurisdictional wetlands and the entire drainageway onsite is classified Zone A. Access to the drainage way will be provided from internal roadways and along an equestrian trail will be constructed adjacent to the drainageway. The equestrian train can be utilized for maintenance equipment as well.

Existing Haegler Ranch Main Stem (MS-06)

The second drainageway is the Haegler Ranch Main Stem (MS-06), per the *Haegler Ranch DBPS*, which crosses onto the site along Curtis Road, approximately 1,600' south of the intersection with Judge Orr Road. MS-06 flows south towards its offsite confluence with Black Squirrel Creek. MS-06 exits the site along the southern property line. Discharge from the developed site into this drainageway will be limited to historic rates via a full spectrum detention pond prior to discharge. This drainageway includes non-jurisdiction wetlands and the entire drainageway is classified Zone AE. Access to the channel will be provided at the culvert crossing of MS-06 and San Isidro Trail via

a 15' wide maintenance and access road that will proceed from San Isidro trail to the channel bottom. From here, access through the channel is achievable with existing grades within the channel. Furthermore, an equestrian trail will be constructed adjacent to the drainageway that can be utilized for maintenance equipment as well. The road alignments are displayed on the proposed drainage map presented in Appendix F.

Existing Haegler Ranch Tributary 6 (T-6)

The third drainageway is the Haegler Ranch Tributary 6 (T-6), per the *Haegler Ranch DBPS*, which crosses onto the site along Curtis Road, approximately ¾ mile south of the intersection with Judge Orr Road. T-6 conveys flows south through the site and towards its off-site confluence with Black Squirrel Creek. Discharge from the developed site into this drainageway will be limited to historic rates via a full spectrum detention pond prior to discharge. This drainageway is absent of any on-site wetlands and the entire drainageway is classified Zone AE. Access to the channel will be provided at the culvert crossing of T-6 and Del Cerro Trail via a 15' wide maintenance and access road that will proceed from Del Cerro Trail to the channel bottom. From here, access through the channel is achievable with existing grades within the channel. Furthermore, an equestrian trail will be constructed adjacent to the drainageway that can be utilized for maintenance equipment as well. The road alignments are displayed on the proposed drainage map presented in Appendix F.

The Santa Fe Springs – Haegler Ranch Drainage Basin LOMR was executed on three Haegler Ranch basin drainageways. Two of the drainageways that were evaluated pass through the proposed development. These drainageways are the: Haegler Ranch Tributary 3 & 4. Within the boundary of the proposed development, Haegler Ranch Tributary 3 and 4 are synonymous with Main Stem 6 and Tributary 6 from the Haegler Ranch DBPS. The purpose of the LOMR was to revise the flood hazard depicted in the current Flood Insurance Study. Additionally, the LOMR provided existing, 100-year velocities within the drainageways that will be utilized in the design of any potential channel improvements. A FIRM panel with the limits of the detailed study as well as BFEs has been presented in Appendix E.

See Table 2 for comparison of drainageway identification and the naming convention used within the context of this report. See Table 3 for a comparison of 100-year flows as calculated in the aforementioned DBPS' and LOMR. An existing conditions drainage map is presented in Appendix F.

Table 2: Major Drainageways

	•						
Major Drainageway Naming Conventions							
Saddlehorn Ranch MDDP/PDR:	Per Haegler Ranch DBPS:	Per Geick Ranch DBPS:	Per Sante Fe Springs LOMR:				
WF-R7A	N/A*	West Fork (Middle)/WF- R7A	N/A*				
MS-06	Main Stem (MS- 06)	N/A*	Haegler Ranch Tributary 3				
T-6	Tributary 6 (T-6)	N/A*	Haegler Ranch Tributary 4				

Table 3: Major Drainageways – Ex. 100-Year Flow Comparison

1	Major Drainageways: 100-Year Flow Comparison					
Drainageway Name	Contributing Area (sq. mi.)	Q ₁₀₀ Per Haegler Ranch DBPS:	Q ₁₀₀ Per Geick Ranch DBPS:	Q ₁₀₀ Per Sante Fe Springs LOMR:		
WF-R7A @ Judge Orr Road	Orr 1.50	N/A*	1,017 cfs	N/A*		
MS-06 @ Curtis Road	1.05	451 cfs	N/A*	505 cfs		
T-6 @ Curtis Road	0.39	120 cfs	N/A*	130 cfs		

^{*}N/A: Flow regime outside limits of study.

Proposed Sub-basin Drainage

The proposed basin delineation is as follows;

Basin A is approximately 9.2 acres and in its existing condition is rolling rangeland. Runoff generally flows southeast away from Drainageway MS-06. In the proposed condition, Basin A will be rural 2.5 acre lots and roadway. Runoff from this basin will be collected in road side swales and conveyed south along Barrosito Drive to Pond A. Pond A, while considered temporary in this MDDP, will need to meet Full Spectrum Detention Criteria unless deviations are approved in the Final Drainage Report for this future filing. It is anticipated that Barrosito Drive will be extended south as part of the development of the adjacent parcel to the south. The most logical place for a permanent Full Spectrum pond is located approximately 1,000 feet south at the future road crossing with MS-06. When that pond is constructed, the Saddlehorn Metropolitan District No. 1 will remove Pond A. The peak flow rate for Basin A in the 5 and 100-year storm are 9.5 cfs and 20.7 cfs, respectively. However, Pond A will discharge at less than historic rates.

Basin B is approximately 60.4 acres and in its existing condition is rolling rangeland. Runoff generally flows southwest across the basin towards Drainageway MS-06. In the proposed condition, Basin B will be rural 2.5 acre lots, paved roadway and will include Pond B. Runoff from this basin will be collected in road side swales and conveyed south along Barrosito Drive to Pond B. The peak flow rate for Basin B in the 5 and 100-year storm are 9.9 cfs and 46.3 cfs, respectively. However, Pond B will discharge at less than historic rates. A portion of Basin B is inundated by the existing 100-year floodplain, however; at time of final platting berming will be constructed to reduce the floodplain limits within the drainageway tract and a corresponding LOMR will be executed on this stretch of channel to establish the revised floodplain.

Basin C is approximately 102.5 acres and in its existing condition is rolling rangeland. Runoff generally flows southwest across the basin towards Drainageway MS-06. In the proposed condition, Basin C will be rural 2.5 acre lots, paved roadway and will include Pond C. Runoff from this basin will be collected in road side swales and conveyed south along Barrosito Drive and Del Cambre Drive to Pond C. The peak flow rate for Basin C in the 5 and 100-year storm are 15.8 cfs and 69.4 cfs, respectively. However, Pond C will discharge at less than historic rates.

Basin D is approximately 99.2 acres and in its existing condition is rolling rangeland. Runoff generally flows east across the basin towards Drainageway WF-R7A. In the proposed condition, Basin D will be rural 2.5 acre lots, paved roadway and will include Pond D. Runoff from this basin will be collected in road side swales and conveyed east along Barrosito drive to Pond D. The peak flow rate for Basin D in the 5 and 100-year storm are 29.4 cfs and 95.4 cfs, respectively. However, Pond D will discharge at less than historic rates. A portion of Basin D is inundated by the existing 100-year floodplain, however; at time of final platting berming will be constructed to reduce the floodplain limits within the drainageway tract and a corresponding LOMR will be executed on this stretch of channel to establish the base flood elevations.

Basin E is approximately 11.6 acres and in its existing condition is rolling rangeland. Runoff generally flows east across the basin towards Drainageway MS-06. In the proposed condition, Basin E will be rural 2.5 acre lots, paved roadway and will include Pond E. Runoff from this basin will be collected in road side swales and conveyed southwest along San Isidro Trail to Pond E. The peak flow rate for Basin E in the 5 and 100-year storm are 2.0 cfs and 9.9 cfs, respectively. However, Pond E will discharge at less than historic rates.

Basin F is approximately 117.4 acres and in its existing condition is rolling rangeland. Runoff generally flows southeast across the basin towards Drainageway MS-06. In the proposed condition, Basin F will be rural 2.5 acre lots, paved roadway and will include Pond F. Runoff from this basin will be collected in road side swales and conveyed southwest along Benito Wells Trail to Pond F. The peak flow rate for Basin F in the 5 and 100-year storm are 17.0 cfs and 69.9 cfs, respectively. However, Pond F will discharge at less than historic rates.

Basin G is approximately 39.9 acres and in its existing condition is rolling rangeland. Runoff generally flows south across the basin towards Drainageway T-6. In the proposed condition, Basin G will be rural 2.5 acre lots, paved roadway and will include Pond G. Runoff from this basin will be collected in road side swales and conveyed southwest along El Raiceno Trail to Pond G. The peak flow rate for Basin G in the 5 and 100-year storm are 6.1 cfs and 25.3, respectively. However, Pond G will discharge at less than historic rates.

Basin H is approximately 30.7 acres and in its existing condition is rolling rangeland. Runoff generally flows east across the basin towards Drainageway T-6. In the proposed condition, Basin H will be rural 2.5 acre lots, paved roadway and will include Pond H. Runoff from this basin will be collected in road side swales and conveyed north along Rosalia Place to Pond H. The peak flow rate for Basin H in the 5 and 100-year storm are 3.7 cfs and 17.9 cfs, respectively. However, Pond H will discharge at less than historic rates.

Basin I is approximately 46.6 acres and in its existing condition is rolling rangeland. Runoff generally flows east across the basin towards Drainageway T-6. In the proposed condition, Basin I will be rural 2.5 acre lots, paved roadway and will include Pond I. Runoff from this basin will be collected in road side swales and conveyed south down Carrizo Springs Trail and east down Zaragoza Trail to Pond I. The peak flow rate for Basin I in the 5 and 100-year storm are 15.9 cfs and 63.1 cfs, respectively. However, Pond I will discharge at less than historic rates.

Basin J is approximately 10.1 acres and in its existing condition is rolling rangeland. This basin will not be developed and will remain in its existing condition, per Section I.7.1.B.5 of the ECM Stormwater Quality Policy and Procedures this basin will not be detained in a full spectrum water quality and detention pond. Runoff generally flows east across the basin towards Drainageway T-6. In the proposed condition, Basin J will be an undeveloped tract. Undeveloped runoff from this basin will follow existing drainage patterns and sheet flow into Drainageway WF-R7A. The peak flow rate for Basin J in the 5 and 100-year storm are 3.0 cfs and 10.5 cfs, respectively.

Basins CH1, CH2 and CH3 are existing drainageway basins that will remain undeveloped in the proposed condition. There will be no development within Basin CH1-CH3, however; Basin CH2 & CH3 will require channel grading to accommodate proposed culverts. The scope of this grading will leave the channels in an undeveloped condition per Section I.7.1.B.7 and therefore will be excluded from permanent stormwater management. Basin CH1 contains jurisdictional wetlands. Basin CH2 contains non-jurisdictional wetlands. There are no wetlands located in Basin CH3. Peak flow rates for proposed undeveloped basins are presented in Appendix B.

Basins UD1-UD11 acre comprised of rural 2.5+ acre residential lots and will follow existing drainage patterns in the proposed condition. Development in these basins will be limited to a maximum of 10% impervious development via a plat covenant. Therefore, these basins can be excluded from permanent stormwater detention per Section I.7.1.B.5 of the ECM Stormwater Quality Policy and Procedures (2.5+ acre lots with imperviousness less than 10% can be excluded from

permanent stormwater management practices). Therefore, Basins UD1-UD11 will not be included in the developments permanent stormwater management facilities. A Permanent BMP applicability form is presented in Appendix D to justify these exclusions. A map detailing each development site and any exclusion is presented in Appendix F. Basin UD1 flows directly into Major Drainageway WF-R7A. Basins UD2, UD2.1, UD2.2, UD3, UD4, UD5 and UD8 flow directly into Major Drainageway MS-06. Basins UD6, UD7, UD9, and UD9.1 flow directly into Major Drainageway T-6. Basins UD8.1, UD10, and UD11 follow existing drainage patterns as well but flow directly off-site prior to being captured in major drainageways. A portion of Basin UD2.2 is inundated by the existing 100-yr floodplain. However, at time of final drainage report, lot lines will be adjusted outside floodplain limits. Furthermore, a portion of Basin UD10 is inundated by the existing 100-year floodplain, however; at time of final platting berming will be constructed to reduce the floodplain limits within the drainageway tract and a corresponding LOMR will be executed on this stretch of channel to establish the revised floodplain.

In addition to undeveloped lot areas, a small portion of Del Cerro Trail (portion of Basins UD9 & UD9.1) and San Isidro Trail (a portion of Basin UD5) will be allowed to directly discharge into Drainageway T-6 and MS-06, respectively, and excluded from the developments permanent stormwater management facilities. Per Section I.7.1.C.1, the County may exclude up to 20 percent, not to exceed 1 acre, of the applicable development site area from permanent stormwater management. Approximately, 16,240 ft² of Del Cerro Drive and 14,000 ft² square feet of San Isidro Trail, totaling 0.08% of the total development area, will be excluded from stormwater management, which is significantly less than the 20% limit.

A summary of all basin parameters has been presented in Appendix B.

Developed basin's runoff will be captured in roadside ditches and conveyed to a full spectrum water quality and detention pond per El Paso County DCM Volume 1. Each full spectrum pond will release treated flows at less than historic rates to minimize adverse impacts downstream. Pond D will discharge into Major Drainageway WF-7A, Pond B, C, E, and F will discharge into Major Drainageway T-6. Due to existing topography, Pond A will discharge into open space south of the site. Based on existing topography in the area, this flow will eventually be captured off-site by Major Drainageway MS-06.

See Table 4 for comparison of proposed pond parameters including a comparison of proposed basin discharge versus existing discharge.

Table 4: Pond Summary

POND SUMMARY TABLE							
Tributary Sub- Basin	Pond Name	Tributary Acres	WQ Volume (ac-ft)	100-Year Volume (ac-ft)	Provided Volume (ac-ft)	100-Year Peak Discharge (cfs)	Ex. 100- Year Peak Discharge (cfs)
Α	POND A	9.2	0.20	1.14	1.14	2.5	2.8
В	POND B	60.4	0.35	1.46	2.17	18.9	21.0
С	POND C	102.5	0.64	2.69	2.77	26.0	28.9
D	POND D	99.2	0.59	2.86	2.97	47.7	53.0
Е	POND E	11.6	0.05	0.23	0.39	4.7	5.2
F	POND F	117.4	0.65	3.20	3.35	50.7	56.3
G	POND G	39.9	0.34	1.36	1.62	10.1	11.2
Н	POND H	30.7	0.16	0.70	1.18	10.5	11.7
I	POND I	46.6	0.25	1.09	1.41	26.8	29.8

Drainage Design Criteria

Development Criteria Reference

Storm drainage analysis and design criteria for the project were taken from the "City of Colorado Spring/El Paso County Drainage Criteria Manual" Volumes 1 and 2 (EPCDCM), dated October 12, 1994, the "Urban Storm Drainage Criteria Manual" Volumes 1 - 3 (USDCM) and Chapter 6 and Section 3.2.1 of Chapter 13 of the "Colorado Springs Drainage Criteria Manual (CCSDCM), dated May 2014, as adopted by El Paso County, as well as the July 2019 El Paso County Engineering Criteria Manual update.

Hydrologic Criteria

All hydrologic data was obtained from the "El Paso Drainage Criteria Manual" Volumes 1 and 2, and the "Urban Drainage and Flood Control District Urban Storm Drainage Criteria Manual" Volumes 1, 2, and 3. Onsite drainage improvements were designed based on the 5 year (minor) storm event and the 100-year (major) storm event. Runoff was calculated using CUHP Version 2.0.0, developed by Urban Drainage and Flood Control District. The model utilizes the raingage classified as "a design storm by temporal distribution of one-hour rain depths with area correction factors". The following Colorado Springs rainfall depths were utilized in the model: 2.52 inches for 1-hour 100-year depth and 3.5 inches for 6-hour 100-year depth. EPA SWMM 5.1 was utilized to route runoff flow rates for the sizing of stormwater storage facilities. The CUHP calculations and SWMM model are presented in Appendix B.

Urban Drainage and Flood Control District's UD-Detention, Version 3.07 workbook was used for preliminary pond sizing. Required detention volumes and allowable release rates were designed per USDCM and CCS/EPCDCM. Pond sizing spreadsheets are presented in Appendix D.

Hydraulic Criteria

The Federal Highway Administration's HY-8 program (Volume 7.50) was used to analyze the proposed box culvert within Major Drainageways MS-06 and T-6. Per Section 14.3.2 of the CCS/EPCDCM, a maximum headwater-to-rise ratio of 1.5 was used for the sizing of box culverts. Furthermore, box culverts will be designed in conjunction with channel improvements to maintain the current floodplain and base flood elevations. Culvert sizing and corresponding channel improvements will be revised as roadway geometry becomes better defined. Preliminary culvert design sheets are presented in Appendix C.

Autodesk Inc.'s Hydraflow Express Extension (Volume 10.5) was used for preliminary roadside ditch design. For the purposes of this PDR/MDDP, the maximum roadside ditch size was determined based on peak 100-year flows and minimum roadway slopes within each basin. Swales were checked for velocity and Froude number per the EPC DCM Chapter 10, Section 10-7 and Table 10-4. Swale cross sections with a 100-year velocity greater than 5 ft/s or a Froude number greater than 0.9 will be lined with erosion control blanket and native grasses, or another approved method of stabilization, to limit erosive potential. Final swale designs and cross section details will be included with the Final Drainage Report. Preliminary swale design sheets are presented in Appendix C.

Autodesk Inc.'s Hydraflow Express Extension (Volume 10.5) will be used for final local road crossing culvert design with in the Final Drainage Report. All onsite, local road crossing culverts are assumed to be 18" or 24" CMP based on preliminary calculations. Culvert size was determined based on 100-year flows and hydraulic criteria from EPCDCM Chapter 9 –Culvert Design. The Final Drainage Report will provide final local road crossing culvert designs.

DRAINAGE FACILITY DESIGN

General Concept

The proposed stormwater conveyance system was designed to convey the developed Saddlehorn Ranch flows to full spectrum water quality and detention ponds. Water quality and detention ponds will be designed to release at less than historic rates to minimize adverse impacts downstream. All full spectrum water quality and detention ponds have been sized such that State Engineer review or approval is not required. Undeveloped basins are allowed to follow existing drainage patterns and discharge directly into major drainageways or off-site.

The undeveloped portion of developed lots will be allowed to discharge directly into Drainageways MS-06, T-6 and WF-R7A. Per the "Jurisdictional Determination Request for the 824 Acres Curtis Road subdivision Project" completed by Ecosystem System Services in October 2018, MS-06 and T-

6 are not waters of the state and WF-R7A is a water of the state however, any direct discharge into this drainageway will be historic, undeveloped flows. The direct discharge into drainageway situation occurs anywhere a lot naturally drains toward a drainageway rather than the street. It was determined for these lots that all development (i.e. house and driveway) will occur in the first 200' of the lot, measured from the street into the lot. The 200' developed region of the lot will drain towards the road and be conveyed to a full spectrum water quality pond, however; the remainder of the lot (undeveloped) will be allowed to follow historic drainage patterns and flow directly into the drainageways. Furthermore, at time of platting, a covenant will be established for the development that will limit imperviousness to 10% for areas draining directly to the drainageways in order to satisfy Section I.7.1.B.5 of the ECM Stormwater Quality Policy and Procedures.

A box culvert will be proposed within Major Drainageway MS-06 and T-6 to convey existing, off site and developed, on-site flows underneath proposed roadways and through the site, in accordance with the *Haegler Ranch DBPS*. Culverts will not be required in Major Drainageway WF-R7A to maintain the drainage patterns established in the *Gieck Ranch DBPS*.

Channel improvements will be proposed immediately up and downstream of culvert improvements in order to maintain the current floodplain. Further channel improvements may be required within the major drainageways and the need for these potential improvements will be evaluated in the Final Drainage Report for each Filing. Access roads will be provided from local roadways down into the drainageways to provide culvert and drainageway maintenance access. A proposed drainage map is presented in Appendix F showing locations of culvert improvements, approximate channel improvements and access roads.

Specific Details

Four Step Process to Minimize Adverse Impacts of Urbanization

In accordance with the El Paso County Drainage Criteria Manual, Volume 2 this site has implemented the four step process to minimize adverse impacts of urbanization. The four step process includes reducing runoff volumes; stabilizing drainageways, treating the water quality capture volume (WQCV), and consider the need for Industrial Commercial BMP's.

Step 1, Reducing Runoff Volumes: The development of the project site is proposed as single family residential (2.5 ac. min.) with open spaces and lawn areas interspersed within the development which helps disconnect impervious areas and reduce runoff volumes. Roadways will utilize roadside ditches further disconnecting impervious areas. These practices will also allow for increased infiltration and reduce runoff volume.

Step 2, Stabilize Drainageways: This site will utilize roadside ditches with culvert crossings throughout the site. These roadside ditches will then direct the on-site development flows to the multiple detention ponds within the project that will be designed to release at or below historic rates in the natural channels. The natural channels will be stabilized in reaches with high velocity by the

use of drop structures incorporated at each roadway culvert crossing and isolated grade control structures where warranted. Based upon the proposed reduction in released flows compared to the pre-developed flows, no impact to downstream drainageways is anticipated.

Step 3, Provide WQCV: Runoff from this development will be treated through capture and slow release of the WQCV in multiple permanent detention basins that will be designed per current El Paso County drainage criteria.

Step 4 Consider the need for Industrial and Commercial BMP's: No industrial or commercial uses are proposed within this development. However, a site specific storm water quality and erosion control plan and narrative will be prepared for each future Filing. Site specific temporary source control BMPs as well as permanent BMP's will be detailed in this plan and narrative to protect receiving waters.

Water Quality

In accordance with Section 13.3.2.1 of the CCS/EPCDCM, full spectrum water quality and detention will be provided for all of the development site not meeting exclusions present in the ECM - Stormwater Quality Policy and Procedures Section I.7.1.B and C. Any areas of the development site not being included in the site's permeant stormwater management are presented on the MS4 Development Site Map with their specific exclusion, presented in Appendix F. Outlet structure release rates will be limited to less than historic rates to minimize adverse impacts to downstream stormwater facilities. Complete pond and outlet structure designs will be provided with the Final Drainage Report. Preliminary pond design parameters are presented in Appendix D.

Erosion Control Plan

The El Paso County Drainage Criteria Manual specifies an Erosion Control Plan and associated cost estimate must be submitted with each Final Drainage Report. We respectfully request that the Erosion Control Plan and Cost Estimate be submitted in conjunction with the grading and erosion control plans and construction assurances posted prior to obtaining a grading permit.

Operation & Maintenance

In order to ensure the function and effectiveness of the stormwater infrastructure, maintenance activities such as inspection, routine maintenance, restorative maintenance, rehabilitation and repair, are required. All proposed drainage structures within the any platted County ROW (roadside ditches and local road culverts) will be owned and maintained by El Paso County. All proposed drainage structures within easements or tracts (full spectrum water quality ponds, drainageway culverts and drainageway improvements) will be owned and maintained by the Saddlehorn Ranch Metropolitan District No.1. Inspection access for El Paso County will be provided through a maintenance easement.

Drainage and Bridge Fees

An estimate of total basin fees for the proposed development within Haegler Ranch Drainage Basin is provided in Table 6. A portion of Saddlehorn Ranch (Basin J and CH1) is not within an approved

drainage basin, therefore; no drainage or bridge fees will be required for this area. Drainage and Bridge fees are for informational purposes only and do not include reductions for rural lots, permanent water quality facilities or reimbursable channel improvements. Final drainage reports for each phase of development will establish official drainage and bridge fees to be paid at time of platting.

Table 5: Site Composite Percent Imperviousness

Total Site Composite % Impervious for Basin Fees						
Daala	Area	%	(Area) *			
Basin	(ac)	Imperviousness	(% lmp.)			
Α	9.2	67%	6.13			
В	60.4	10%	6.28			
С	102.5	11%	11.69			
D	99.2	11%	10.71			
E	11.6	12%	1.35			
F	117.4	10%	11.62			
G	39.9	17%	6.70			
Н	30.7	9%	2.89			
I	46.6	9%	4.38			
J	10.1	9%	0.89			
UD1	12.4	2%	0.25			
UD2	12.8	2%	0.26			
UD2.1	14.8	2%	0.30			
UD2.2	7.2	2%	0.14			
UD3	13.4	2%	0.27			
UD4	4.8	2%	0.10			
UD5	36.4	2%	0.73			
UD6	22.1	2%	0.44			
UD7	9.3	2%	0.19			
UD8	4.6	2%	0.09			
UD8.1	5.3	2%	0.11			
UD9	4.8	2%	0.10			
UD9.1	6.4	2%	0.13			
UD10	10.4	2%	0.21			
UD11	6.0	2%	0.12			
CH1 23.9		2%	0.48			
CH2	84.2	2%	1.68			
CH3	19.0	2%	0.38			
Total	825.4	-	68.59			
Comp. % Imp. = 68.59%*ac/825.4 ac = 8.31%						

Table 6: Drainage Basin Fees

	El Paso County - Haegler Ranch Drainage Basin Fees								
Area (acre)	Composite % Impervious	Total Impervious Acreage	2019 Drainage Fee (per Impervious Acre)	2019 Bridge Fee (per Impervious Acre)	Saddlehorn Ranch Drainage Fee	Saddlehorn Ranch Bridge Fee			
825.4	8.31%	68.59	\$10,324	\$1,524	\$708,123	\$104,531			

Construction Cost Opinion

(For Information Only / Non-Reimbursable)

Cost opinion to be provided with Final Drainage Report.

SUMMARY

The proposed development remains consistent with pre-development drainage conditions with the construction of the recommended drainage improvements, including ditches, culverts, detention ponds and drainage channel improvements. The proposed development will not adversely affect the offsite major drainageways or surrounding development. This report meets the latest El Paso County Drainage Criteria requirements for this site.

REFERENCES:

- <u>City of Colorado Springs Drainage Criteria Manual Volume 1</u>, City of Colorado Springs,
 CO, May 2014.
- 2. <u>Urban Storm Drainage Criteria Manual</u>, Urban Drainage and Flood Control District, Latest Revision.
- 3. <u>Gieck Ranch Drainage Basin Planning Study</u>, Drexel, Barrell & Co., October 2007 and revised in February 2010.
- 4. Haegler Ranch Drainage Basin Planning Study, URS Corporation, May 2009.
- 5. <u>The Santa Fe Springs Haegler Ranch Drainage Basin LOMR</u>, Federal Emergency Management Agency, October 20, 2004.

APPENDIX A FIGURES AND EXHIBITS

Delete all extra Appendix divider sheets which are not needed.

JR Response: Extra sheets have been removed.

APPENDIX B HYDROLOGIC CALCULATIONS

Colorado Urban Hydrograph Procedure

Version 2.0.0 - Release Date: 9/9/2016

Urban Drainage and Flood Control District Denver, Colorado email: udfcd@udfcd.org

Purpose:	This program produces hydrographs using the Colorado Unit Hydrograph Procedure (CUHP)						
Functions:							
Edit Raingages	Add/Remove Raingages and change names						
Edit Subcatchments	Edit subcatchment parameters						
Edit Multiple Run Options	Edit the Multiple Run options (Advanced User Features)						
Import CUHP 2005 File	Import an older CUHP 2005 workbook into this updated version of CUHP						
Check Subcatchments	heck whether subcatchment inputs conform to UDFCD guidelines						
Check SWMM Nodes	Check whether all subcatchment target nodes are included in the SWMM .inp file						
Run CUHP	Calculate effective precipitation and generate hydrographs for each subcatchment						
Settings:	Fill in the blue cells to begin: Project Title: Saddlehorn Ranch Project Comment: Ex. Conditions Analysis Time Step Between Computations: 5 Minute(s); typically 5 or 1 (peak flow rate will differ slightly). Use Relative Path Names Output Workbook Filename: X:\2510000.all\2514200\CUHP-SWMM\Existing_CUHP_2002.xlsm.xlsx CUHP/SWMM Interface Filename (Optional): X:\2510000.all\2514200\CUHP-SWMM\Existing_CUHP_2002.xlsm.txt EPA SWMM 5 Input Filename (Optional): X:\2510000.all\2514200\CUHP-SWMM\Ex. Conditions Model.inp EPA SWMM 5 Application File (Optional): SWMM Hydrograph Start Time (Optional):						
Acknowledgements:	Thanks to Ben Urbonas, P.E., D.WRE and James C.Y.Guo, PhD, P.E., for the development of the CUHP project.						

CUHP SUBCATCHMENTS

Columns with this color heading are for required user-input

Columns with this color heading are for optional override values
Columns with this color heading are for program-calculated values

								Maximum Depre (Watershe	Но	DCIA			
Subcatchment Name	EPA SWMM Target Node	Raingage	Area (mi²)	Length to Centroid (mi)	Length (mi)	Slope (ft/ft)	Percent Imperviousness	Pervious	Impervious	Initial Rate (in/hr)	Decay Coefficient (1/seconds)	Rate	Level 0, 1, or 2
CH1	CH1	EPC	0.0373438	0.210994318	0.4289773	0.01	2	0.4	0	3	0.0018	0.5	2
CH2	CH2	EPC	0.1318594	0.930530303	1.4477273	0.015	2	0.4	0	4	0.0013	0.75	2
CH3	CH3	EPC	0.0329219	0.420583333	0.7320076	0.015	2	0.4	0	4.81	0.0011	0.85	2
H1	H1	EPC	0.2601406	0.229166666	0.821917	0.01	2	0.4	0	5	0.0007	1	2
H2	H2	EPC	0.1735781	0.129545454	0.4912879	0.025	2	0.4	0	5	0.0007	1	2
H3	H3	EPC	0.18325	0.490719697	0.932197	0.015	2	0.4	0	4.64	0.0009	0.73	2
H4	H4	EPC	0.0988906	0.085984848	0.5267045	0.0225	2	0.4	0	3.82	0.0008	0.74	2
H5	H5	EPC	0.0831875	0.236931818	0.7267045	0.02	2	0.4	0	4.93	0.0009	0.94	2
H6	H6	EPC	0.1367969	0.046022727	0.4	0.04	2	0.4	0	5	0.0007	1	2
G1	G1	EPC	0.01575	0.210606061	0.3015152	0.018	2	0.4	0	5	0.00007	1	2
G2	G2	EPC	0.1368125	0.235606061	0.6857955	0.02	2	0.4	0	4.32	0.0011	0.83	2

RUN MULTIPLE CUHP AND SWMM SCENARIOS

Columns with this color heading are for required user-input Columns with this color heading are for program-calculated values

SWMM Run Wait Time (sec) (Optional) SWMM Time Series Inflow "Modification Type" (LU, RP, or LU&RP)

Subcatchment Name	Existing Landuse % Imperviousness	Future Landuse % Imperviousness
CH1	2	2
CH2	2	2
CH3	2	2
H1	2	2
H2	2	2
H3	2	2
H4	2	2
H5	2	2
H6	2	2
G1	2	2
G2	2	2

Raingage	Return Period (Years)	1 Hr Depths (in)	6 Hr Depths (in)
	WQ	0.6	N/A
	2	1.19	2.1
	5	1.5	2.7
EPC	10	1.75	3.2
	25	2	3.6
	50	2.25	4.2
	100	2.52	4.6
-			

Enter "X" to Run Scenario	Scenario ID	Land Use (E or F)	Return Period (yr)	Correction Area (Sq.Mi.)
Х	WQ	E	WQ	0
	2-YR	E	2	1
X	5-YR	E	5	1
	10-YR	E	10	1
	25-YR	E	25	1
	50-YR	E	50	1
X	100-YR	E	100	1

(Optional) SWMM Time Series Inflow Table "NAME"

Comment	El Paso County F	Rainfall Depths		
1Hr Depth	2.52	inches	2hr Depth	2.86 inches
6Hr Depth	3.5	inches	3hr Depth	3.11 inches
Correction Area	1	Sq. Mi.		
Return Period	100	Years		
Time	Adjusted Depth	Unadjusted Depth		NOAA Atlas 14 Point Precipitation Frequency
0:05	0.0252	0.0252		
0:10	0.0756	0.0756		
0:15	0.1159	0.1159		
0:20	0.2016	0.2016		
0:25	0.3528	0.3528		
0:30	0.6300	0.6300		
0:35	0.3528	0.3528		
0:40	0.2016	0.2016		
0:45	0.1562	0.1562		
0:50	0.1260	0.1260		
0:55	0.1008	0.1008		
1:00	0.1008	0.1008		
1:05	0.1008	0.1008		
1:10	0.0504	0.0504		
1:15	0.0504	0.0504		
1:20	0.0302	0.0302		
1:25	0.0302	0.0302		
1:30	0.0302	0.0302		
1:35		0.0302		
1:40		0.0302		
1:45	0.0302	0.0302		
1:50		0.0302		
1:55		0.0302		
2:00		0.0302		
2:05		0.0000		
2:10		0.0000		
2:15		0.0000		
2:20		0.0000		
2:25	0.0000	0.0000		
2:30	0.0000	0.0000		
2:35	0.0000	0.0000		
2:40	0.0000	0.0000		
2:45	0.0000	0.0000		
2:50	0.0000	0.0000		
2:55	0.0000	0.0000		
3:00	0.0000	0.0000		
3:05	0.0000	0.0000		
3:10	0.0000	0.0000		
3:15	0.0000	0.0000		
3:20	0.0000	0.0000		
3:25	0.0000	0.0000		
3:30	0.0000	0.0000		
3:35	0.0000	0.0000		
3:40	0.0000	0.0000		
3:45	0.0000	0.0000		
3:50	0.0000	0.0000		
2.00	2.2200	2.2300		

SADDLEHORN RANCH - EX. 5-YEAR FLOW RESULTS

Node Inflow Summary

Node	Туре	Maximum Lateral Inflow CFS	Maximum Total Inflow CFS	Day of Maximum Inflow	Hour of Maximum Inflow	Lateral Inflow Volume 10^6 gal	Total Inflow Volume 10^6 gal	Flow Balance Error Percent
CH1	JUNCTION	5.40	5.40	0	00:50	0.232	0.232	0.000
CH2	JUNCTION	2.58	2.58	0	01:00	0.176	0.176	0.000
СНЗ	JUNCTION	0.11	0.11	0	00:45	0.00701	0.00701	0.000
DP1	JUNCTION	0.00	6.79	0	00:46	0	0.268	0.000
DP2	JUNCTION	0.00	1.46	0	00:40	0	0.0359	0.000
DP3	JUNCTION	0.00	0.13	0	00:40	0	0.00379	0.000
DP4	JUNCTION	0.00	0.16	0	00:35	0	0.00252	0.000
DP5	JUNCTION	0.00	0.90	0	00:45	0	0.0334	0.000
DP6	JUNCTION	0.00	1.35	0	00:35	0	0.0209	0.000
DP7	JUNCTION	0.00	4.06	0	01:05	0	0.237	0.000
DP8	JUNCTION	0.00	0.21	0	00:30	0	0.00194	0.000
DP9	JUNCTION	0.00	0.43	0	00:40	0	0.0172	0.000
G1	JUNCTION	0.00	0.00	0	00:00	0	0	0.000
G2	JUNCTION	1.46	1.46	0	00:40	0.0359	0.0359	0.000
H1	JUNCTION	0.13	0.13	0	00:40	0.00379	0.00379	0.000
H2	JUNCTION	0.16	0.16	0	00:35	0.00252	0.00252	0.000
Н3	JUNCTION	0.90	0.90	0	00:45	0.0334	0.0334	0.000

SWMM 5.1 Page 1

SADDLEHORN RANCH - EX. 5-YEAR FLOW RESULTS

Node	Туре	Maximum Lateral Inflow CFS	Maximum Total Inflow CFS	Day of Maximum Inflow	Hour of Maximum Inflow	Lateral Inflow Volume 10^6 gal	Total Inflow Volume 10^6 gal	Flow Balance Error Percent
H4	JUNCTION	1.35	1.35	0	00:35	0.0209	0.0209	0.000
H5	JUNCTION	0.33	0.33	0	00:40	0.0102	0.0102	0.000
Н6	JUNCTION	0.21	0.21	0	00:30	0.00194	0.00194	0.000
J13	JUNCTION	0.00	0.07	0	01:50	0	0.00485	0.000
J14	JUNCTION	0.00	0.06	0	02:28	0	0.00242	0.000
J15	JUNCTION	0.00	0.83	0	01:03	0	0.0333	0.000
J16	JUNCTION	0.00	0.09	0	00:49	0	0.00188	0.000

SWMM 5.1 Page 2

SADDLEHORN RANCH - EX. 100-YR FLOW RESULTS

Node Inflow Summary

Node	Туре	Maximum Lateral Inflow CFS	Maximum Total Inflow CFS	Day of Maximum Inflow	Hour of Maximum Inflow	Lateral Inflow Volume 10^6 gal	Total Inflow Volume 10^6 gal	Flow Balance Error Percent
CH1	JUNCTION	1038.04	1038.04	0	00:55	165	165	0.000
CH2	JUNCTION	485.11	485.11	0	01:15	75.2	75.2	0.000
СНЗ	JUNCTION	127.25	127.25	0	01:10	19.9	19.9	0.000
DP1	JUNCTION	0.00	1114.02	0	00:51	0	167	0.000
DP2	JUNCTION	0.00	76.38	0	00:50	0	2.23	0.000
DP3	JUNCTION	0.00	80.97	0	00:45	0	2.08	0.000
DP4	JUNCTION	0.00	91.06	0	00:40	0	1.38	0.000
DP5	JUNCTION	0.00	64.08	0	01:00	0	2.67	0.000
DP6	JUNCTION	0.00	73.15	0	00:40	0	1.47	0.000
DP7	JUNCTION	0.00	704.90	0	01:08	0	83	0.000
DP8	JUNCTION	0.00	110.05	0	00:35	0	1.06	0.000
DP9	JUNCTION	0.00	248.10	0	00:45	0	21.9	0.000
G1	JUNCTION	0.09	0.09	0	00:40	0.00364	0.00364	0.000
G2	JUNCTION	76.38	76.38	0	00:50	2.23	2.23	0.000
H1	JUNCTION	80.97	80.97	0	00:45	2.08	2.08	0.000
H2	JUNCTION	91.06	91.06	0	00:40	1.38	1.38	0.000
Н3	JUNCTION	64.08	64.08	0	01:00	2.67	2.67	0.000
H4	JUNCTION	73.15	73.15	0	00:40	1.47	1.47	0.000
Н5	JUNCTION	28.20	28.20	0	00:50	0.959	0.959	0.000
Н6	JUNCTION	110.05	110.05	0	00:35	1.06	1.06	0.000

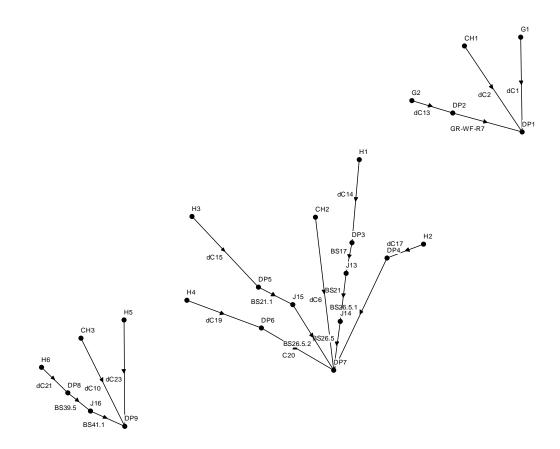
SADDLEHORN RANCH - EX. 100-YR FLOW RESULTS

Nodo	Tura	Maximum Lateral Inflow	Maximum Total Inflow	Day of Maximum	Hour of Maximum	Lateral Inflow Volume	Total Inflow Volume	Flow Balance Error
Node	Туре	CFS	CFS	Inflow	Inflow	10^6 gal	10^6 gal	Percent
J13	JUNCTION	0.00	69.43	0	01:03	0	2.18	0.000
J14	JUNCTION	0.00	68.26	0	01:09	0	2.19	0.000
J15	JUNCTION	0.00	63.63	0	01:07	0	2.68	0.000
J16	JUNCTION	0.00	103.79	0	00:38	0	1.08	0.000

SWMM 5.1 Page 2

SADDLEHORN RANCH - EX. CONDITIONS SWMM MODEL

01/01/2005 00:15:00



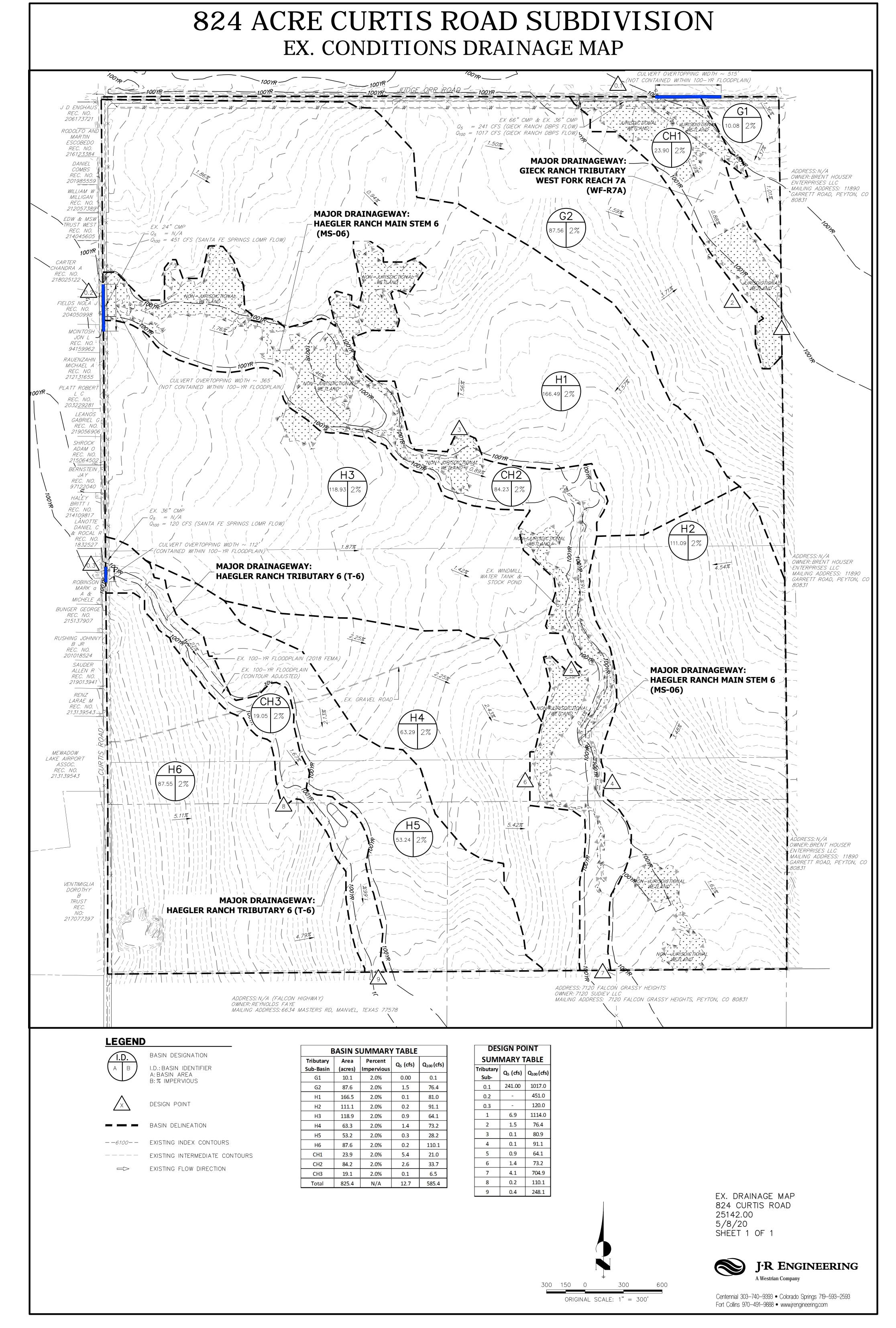
SWMM 5.1 Page 1

APPENDIX C HYDRAULIC CALCULATIONS

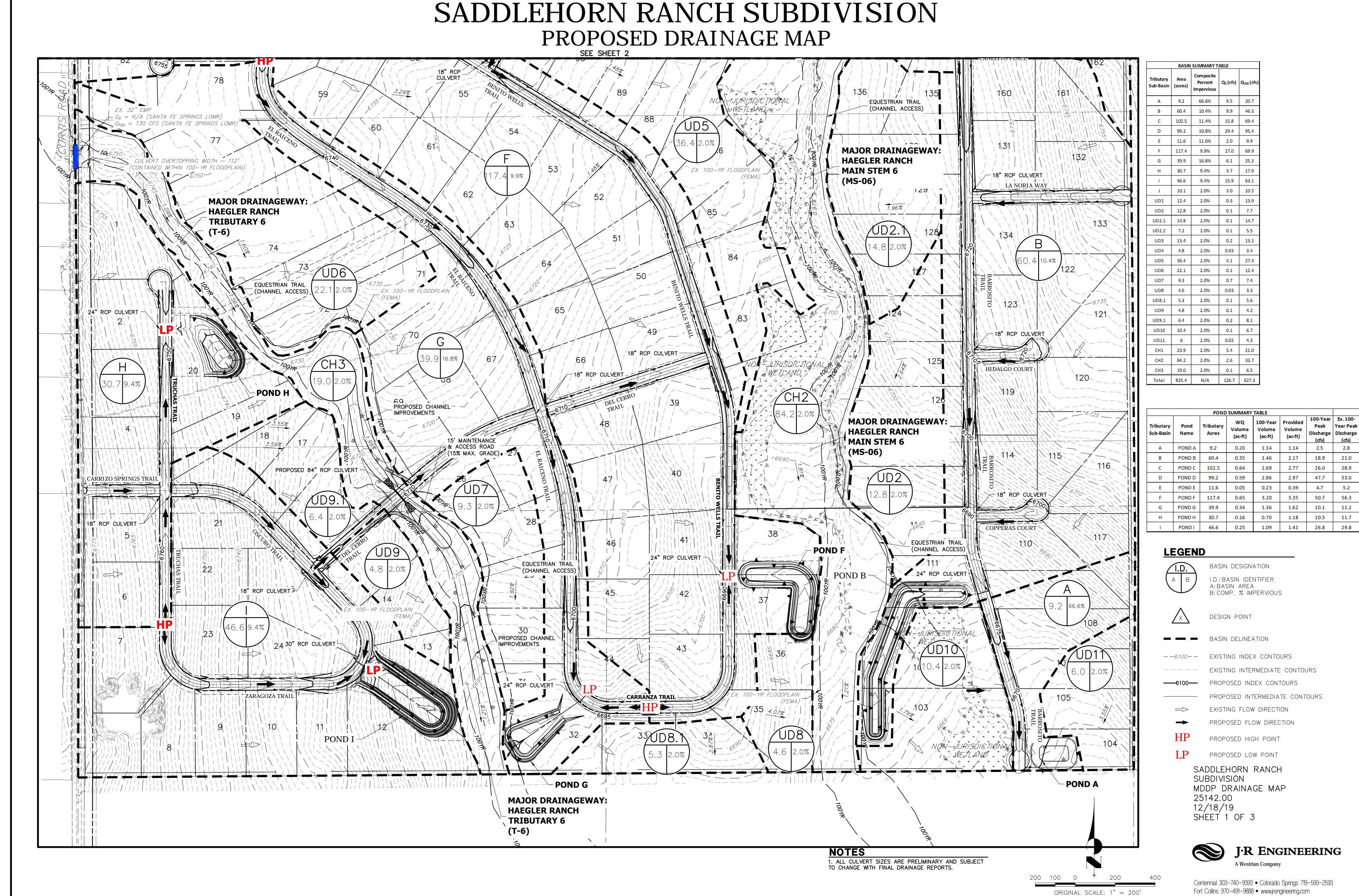
APPENDIX D WATER QUALITY AND DETENTION CALCULATIONS

APPENDIX E REFERENCE MATERIALS

APPENDIX F DRAINAGE MAPS

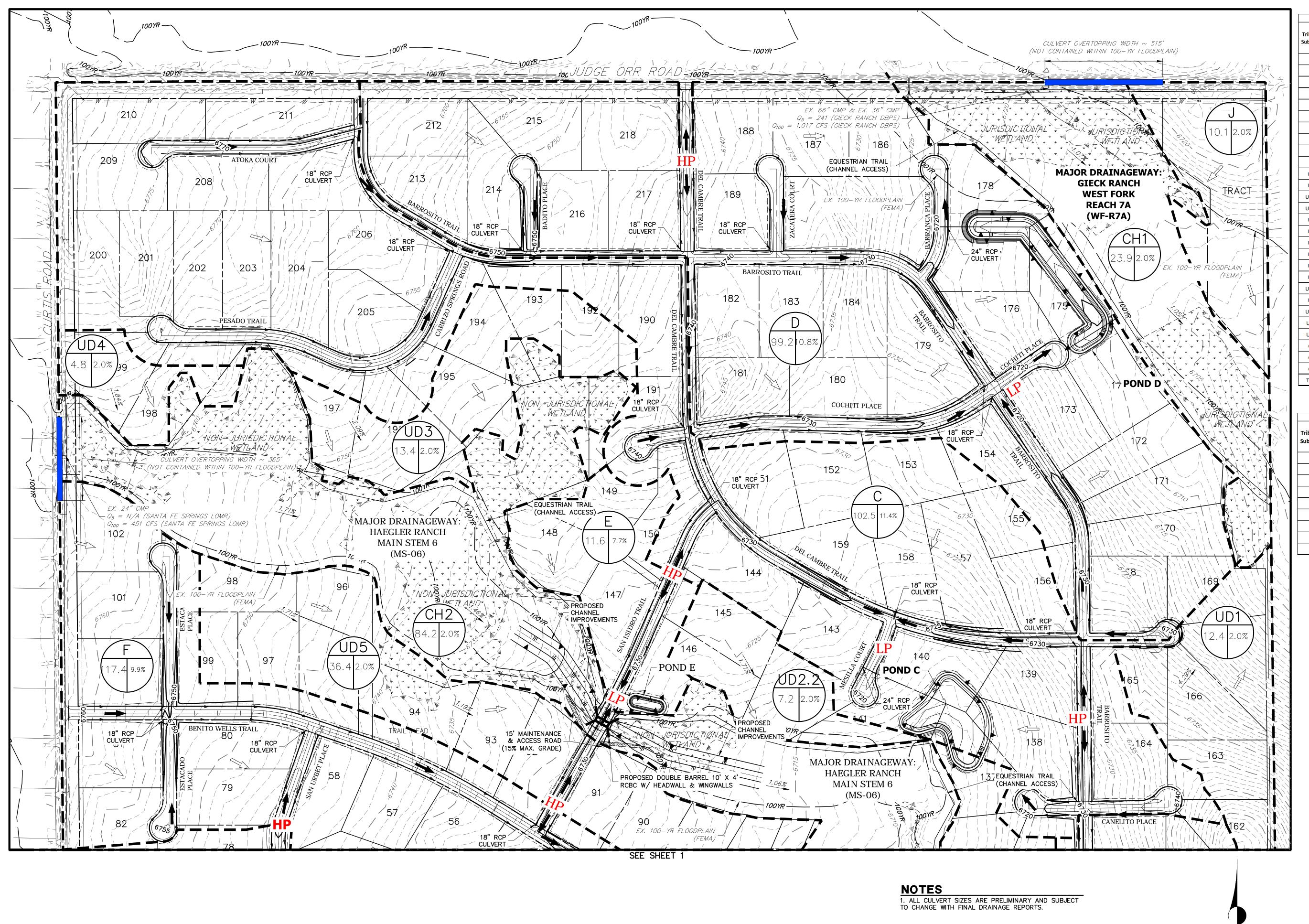


X:\2510000.all\2514200\Drawings\Sheet Dwgs_Drainage\2018-10-09_Ex.Drainage Map.dwg, EX. DR01, 5/8/20



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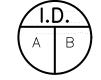
SADDLEHORN RANCH SUBDIVISION PROPOSED DRAINAGE MAP



Tributary Sub-Basin	Area (acres)	Composite Percent Impervious	Q₅ (cfs)	Q ₁₀₀ (cfs)
Α	9.2	66.6%	9.5	20.7
В	60.4	10.4%	9.9	46.3
С	102.5	11.4%	15.8	69.4
D	99.2	10.8%	29.4	95.4
E	11.6	11.6%	2.0	9.9
F	117.4	9.9%	17.0	69.9
G	39.9	16.8%	6.1	25.3
Н	30.7	9.4%	3.7	17.9
1	46.6	9.4%	15.9	63.1
J	10.1	2.0%	3.0	10.5
UD1	12.4	2.0%	0.3	13.9
UD2	12.8	2.0%	0.1	7.7
UD2.1	14.8	2.0%	0.1	14.7
UD2.2	7.2	2.0%	0.1	5.5
UD3	13.4	2.0%	0.2	13.1
UD4	4.8	2.0%	0.03	3.4
UD5	36.4	2.0%	4.1	27.4
UD6	22.1	2.0%	0.1	12.4
UD7	9.3	2.0%	0.7	7.4
UD8	4.6	2.0%	0.03	3.3
UD8.1	5.3	2.0%	0.1	5.6
UD9	4.8	2.0%	0.1	4.2
UD9.1	6.4	2.0%	0.2	8.1
UD10	10.4	2.0%	0.1	6.7
UD11	6	2.0%	0.02	4.3
CH1	23.9	2.0%	5.4	21.0
CH2	84.2	2.0%	2.6	33.7
CH3	19.0	2.0%	0.1	6.5
Total	825.4	N/A	126.7	627.3

	POND SUMMARY TABLE										
Tributary Sub-Basin	Pond Name	Tributary Acres	WQ Volume (ac-ft)	100-Year Volume (ac-ft)	Provided Volume (ac-ft)	100-Year Peak Discharge (cfs)	Ex. 100- Year Peak Discharge (cfs)				
Α	POND A	9.2	0.20	1.14	1.14	2.5	2.8				
В	POND B	60.4	0.35	1.46	2.17	18.9	21.0				
С	POND C	102.5	0.64	2.69	2.77	26.0	28.9				
D	POND D	99.2	0.59	2.86	2.97	47.7	53.0				
Е	POND E	11.6	0.05	0.23	0.39	4.7	5.2				
F	POND F	117.4	0.65	3.20	3.35	50.7	56.3				
G	POND G	39.9	0.34	1.36	1.62	10.1	11.2				
Н	POND H	30.7	0.16	0.70	1.18	10.5	11.7				
I	PONDI	46.6	0.25	1.09	1.41	26.8	29.8				

LEGEND



BASIN DESIGNATION

I.D.: BASIN IDENTIFIER

A: BASIN AREA

B: COMP. % IMPERVIOUS

X

ORIGINAL SCALE: 1" = 200'

DESIGN POINT

BASIN DELINEATION

--6100-- EXISTING INDEX CONTOURS
----- EXISTING INTERMEDIATE CONTOURS

—6100— PROPOSED INDEX CONTOURS— PROPOSED INTERMEDIATE CONTOURS

EXISTING FLOW DIRECTION

PROPOSED FLOW DIRECTION

P PROPOSED HIGH POINT

PROPOSED LOW POINT

SADDLEHORN RANCH MDDP DRAINAGE MAP 25142.00

25142.00 12/18/19 SHEET 2 OF 3



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April 25, 2023

Keith Curtis, PE, CFM Floodplain Administrator, PPRBD 2880 International Circle Colorado Springs, CO 80910

Re: Engineer's Certification of No Impact

Case No.:

Dear Mr. Curtis,

This letter serves as Certification of No Impact to the Floodplain for the project entitled "Saddlehorn Ranch – Filing 3." The project is located in the unincorporated El Paso County and involves a proposed rural 2.5 acre lot subdivision.

The Federal Emergency Management Agency (FEMA) Flood Insurance Rate Map (FIRM) shows the project area located on Panel No. 08041C0558G for El Paso County, Colorado dated December 7, 2018. The project area is located along Haegler Ranch MS-06 and is within a designated Zone AE Special Flood Hazard Area (SFHA).

JR Engineering has evaluated the effects of the proposed development on the Haegler Ranch floodplain using the effective modeling as a baseline. The HEC-RAS modeling was obtained in PDF format from the "Santa Fe Springs – Haegler Ranch Drainage Basin Letter of Map Revision (LOMR)" by Tri-Core Engineering, dated October 20, 2004, from the Federal Emergency Management Agency (FEMA). The effective model is the "Santa Fe Springs – Haegler DB. – Letter of Map Revision" prepared for FEMA by Tri-Core Engineering. The effective model was pared down to the stretch between Cross Sections 4 and 19 along Reach H8 (Haegler Ranch Tributary 3) for purposes of analysis within the context of this project.

JR Engineering utilized the calculated 100-year water surface from the aforementioned model to establish the existing 100-year floodplain. Proposed channel and culvert improvements were modeled utilizing the 100-year flow of 505 cfs established in the "Santa Fe Springs – Haegler Ranch Drainage Basin Letter of Map Revision (LOMR)". Cross sections for the proposed channel improvements were modeled using the CivilGeo HECRAS program. The program models the projects proposed dual 12'x4' RCBC, this also took into hydraulic head built at the culvert crossing to establish an accurate base flood elevation. The computed water surface elevation at each cross section was compared to the effective model to ensure a no rise scenario.

Select results of the analysis are presented in Table 1, on the following page:

Table 1: Base Flood Elevation Comparison

	Base Flood Elevation (ft)		
Cross Section	Ex. 100- Year	Pr. 100- Year	
13	6723.61	6723.60	
14	6722.03	6719.68	
15	6720.65	6718.33	
16	6717.71	6717.56	
17	6714.03	6714.03	

Based on the results of the CivilGeo HECRAS Analysis, no increase to either the floodplain width or water surface elevation will result from the proposed site development.

Sincerely,

Bryan Law PE Colorado P.E. #25043

No Rise Certification

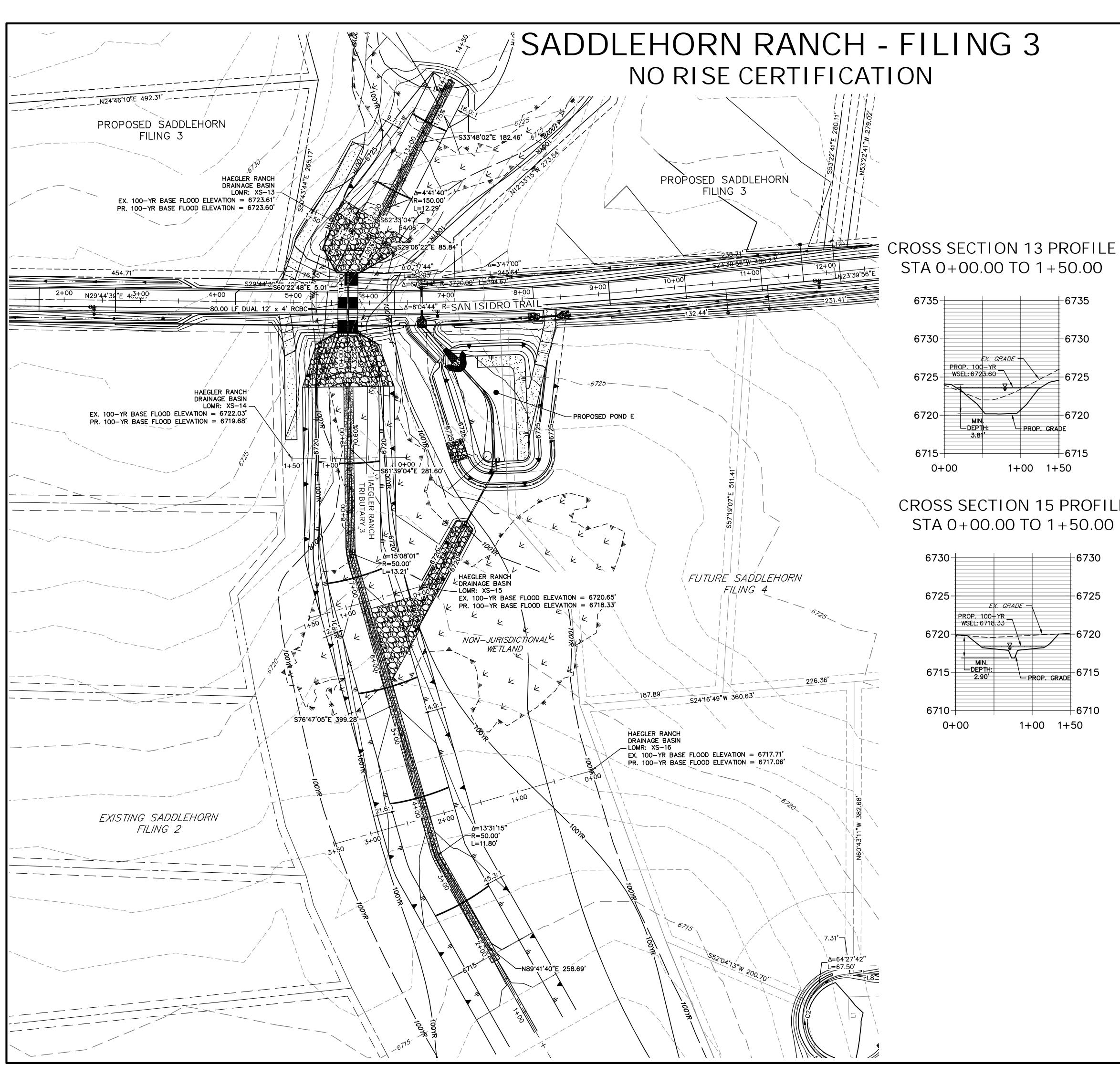
I certify that I am a duly qualified registered Professional Engineer in the State of Colorado.

I certify the proposed project, Saddlehorn Ranch Filing No. 3, as detailed on the following sheets and calculations will result in zero rise in the FEMA designated 100 year flood heights, and no increase in the 100-year discharge and no increase in the 100-year floodplain width, at published and unpublished cross sections of the current FEMA floodplain of Haegler Ranch MS-06 as shown on FEMA map 08041C0558G. This certification is intended as proof of meeting the requirements set forth in the Pikes Peak Regional Building Code RBC313.20.1.

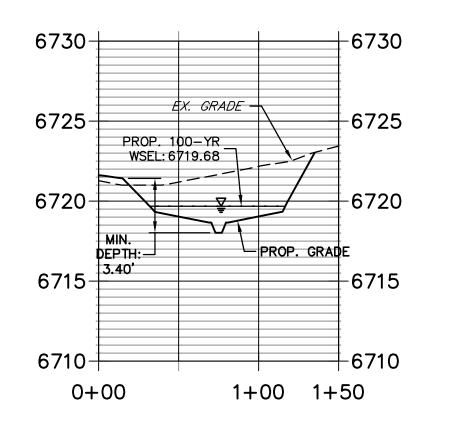
I further certify that the design conditions needed to meet the zero rise, box culvert and wing walls, are detailed in sufficient nature to allow for field confirmation and included among the supporting documentation.

I further certify that the structure in question will be securely anchored to prevent flotation, collapse or lateral movement in order to withstand the velocity of floodwaters as required by RCB313.18.1 and RBC313.21.2.

Bryan Law PE Colorado P.E. #25043



CROSS SECTION 14 PROFILE STA 0+00.00 TO 1+50.00

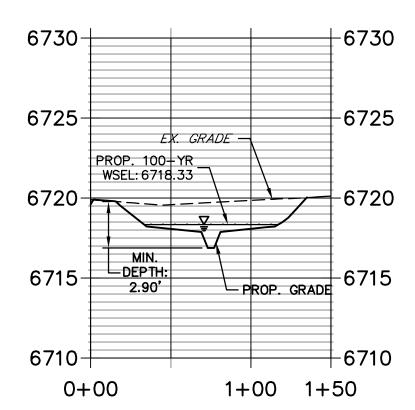


CROSS SECTION 15 PROFILE STA 0+00.00 TO 1+50.00

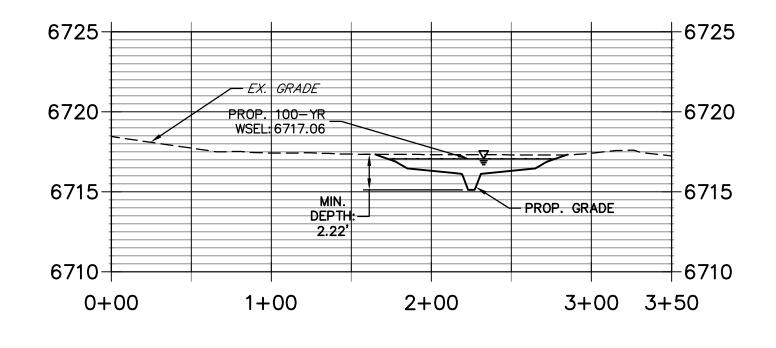
1+00 1+50

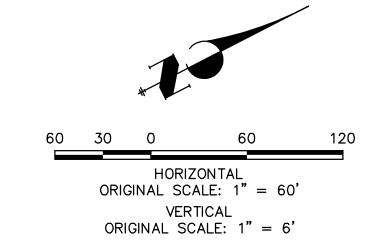
+6735

6730



CROSS SECTION 16 PROFILE STA 0+00.00 TO 3+50.00

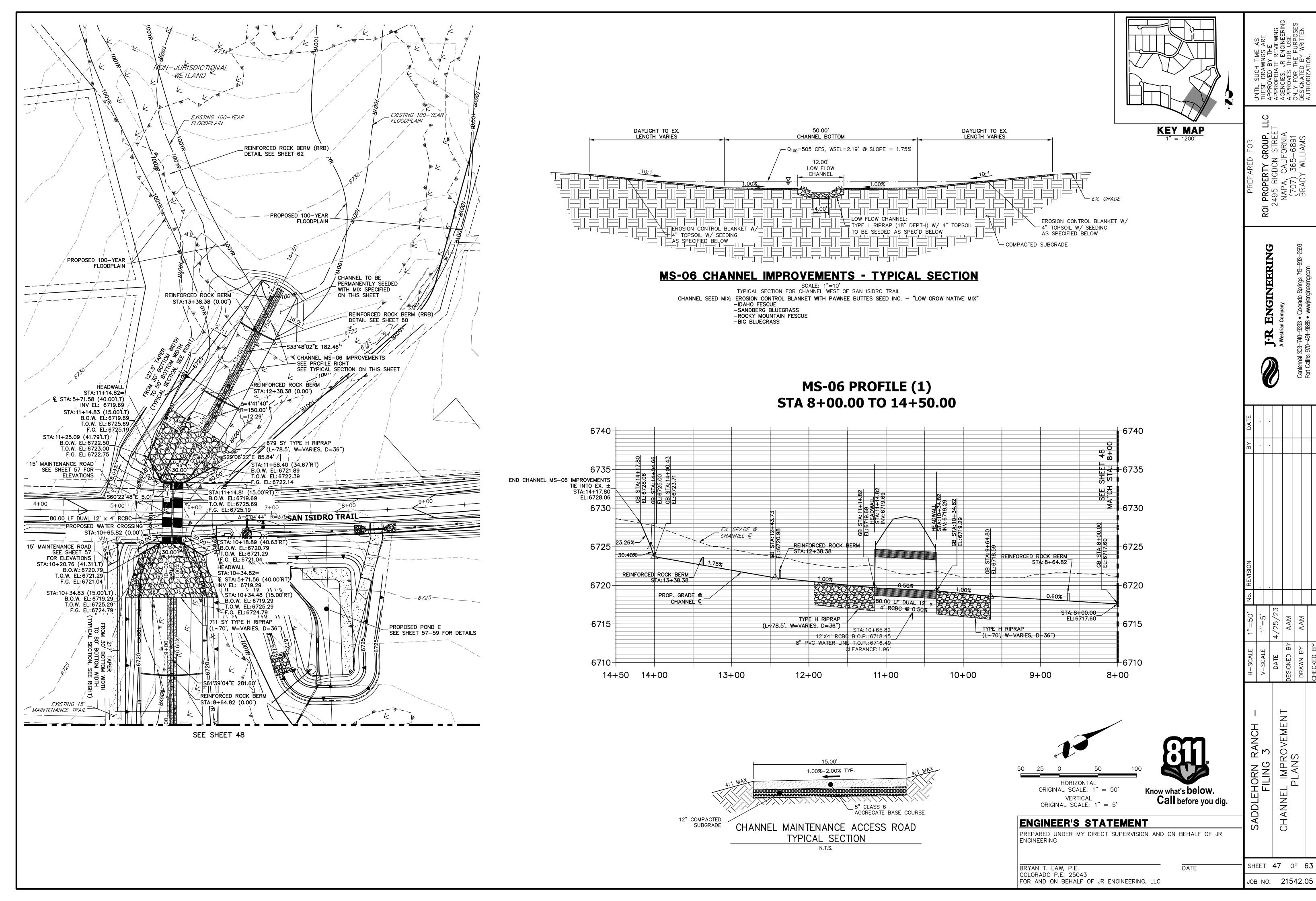


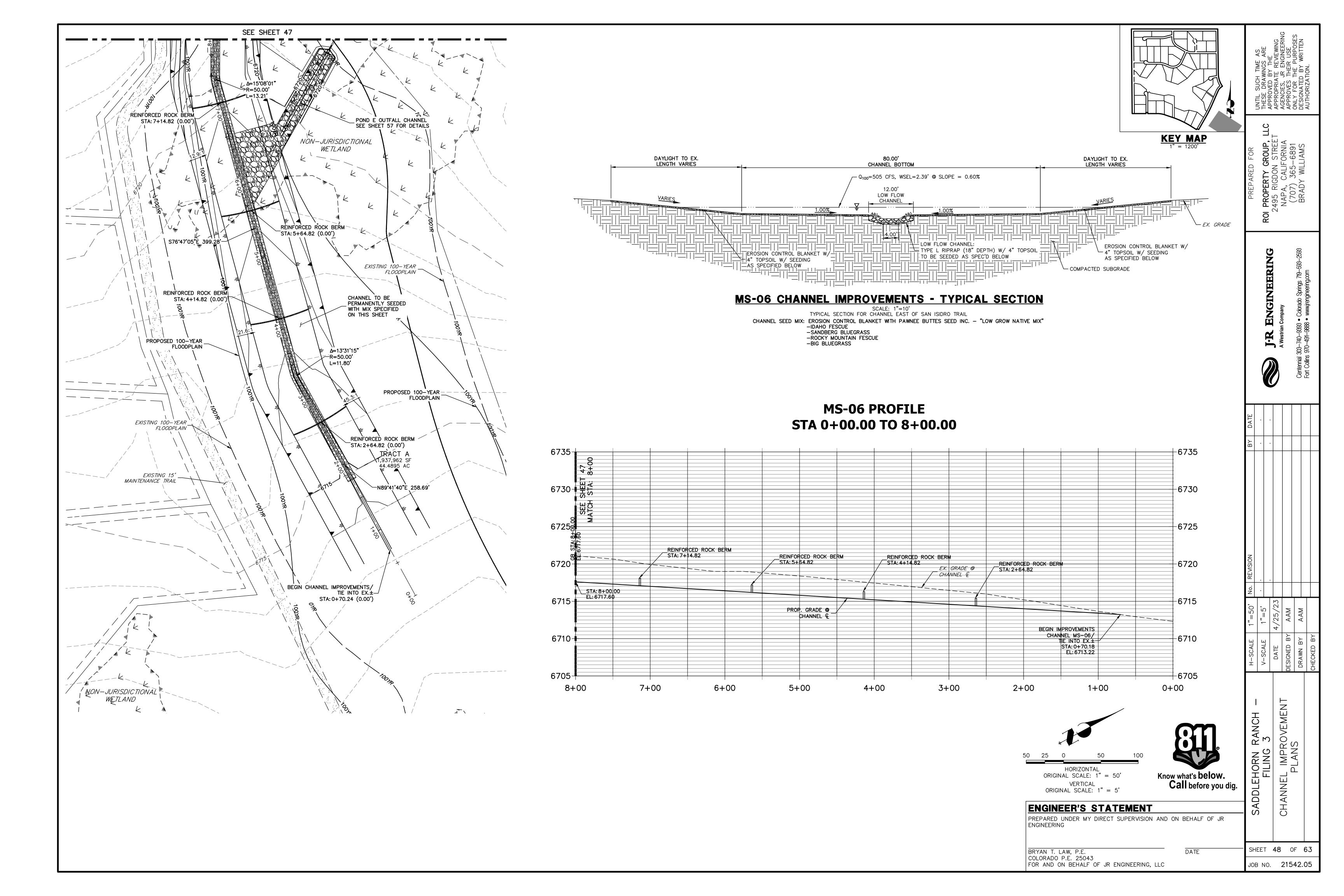


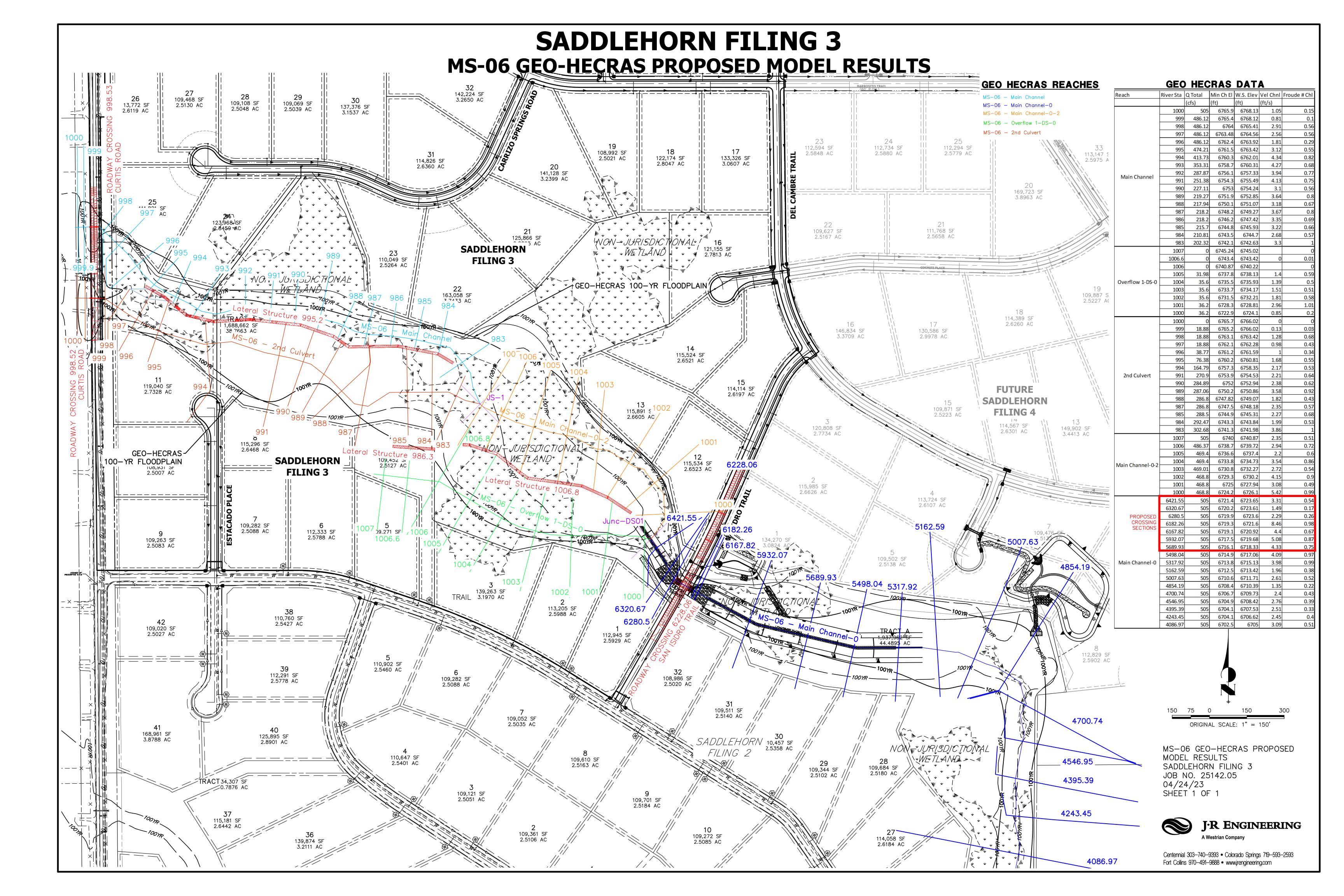
NO RISE CERTIFICATION SADDLEHORN RANCH - FILING 3 JOB NO. 25142.05 4/24/23 SHEET 1 OF 1



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HY-8 Culvert Analysis Report

Crossing Discharge Data

Discharge Selection Method: Specify Minimum, Design, and Maximum Flow

Minimum Flow: 400 cfs Design Flow: 505 cfs Maximum Flow: 600 cfs

Table 1 - Summary of Culvert Flows at Crossing: San Isidro Crossing

Headwater Elevation (ft)	Total Discharge (cfs)	San Isidro Crossing Discharge (cfs)	Roadway Discharge (cfs)	Iterations
6722.88	400.00	400.00	0.00	1
6722.99	420.00	420.00	0.00	1
6723.11	440.00	440.00	0.00	1
6723.22	460.00	460.00	0.00	1
6723.34	480.00	480.00	0.00	1
6723.48	505.00	505.00	0.00	1
6723.57	520.00	520.00	0.00	1
6723.68	540.00	540.00	0.00	1
6723.80	560.00	560.00	0.00	1
6723.91	580.00	580.00	0.00	1
6724.03	600.00	600.00	0.00	1
6728.59	1176.67	1176.67	0.00	Overtopping

Rating Curve Plot for Crossing: San Isidro Crossing

Total Rating Curve Crossing: San Isidro Crossing

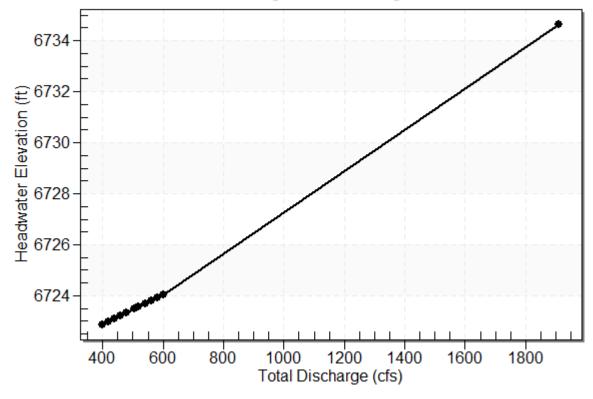


Table 2 - Culvert Summary Table: San Isidro Crossing

Total Discharge (cfs)	Culvert Discharge (cfs)	Headwater Elevation (ft)	Inlet Control Depth (ft)	Outlet Control Depth (ft)	Flow Type	Normal Depth (ft)	Critical Depth (ft)	Outlet Depth (ft)	Tailwater Depth (ft)	Outlet Velocity (ft/s)	Tailwater Velocity (ft/s)
400.00	400.00	6722.88	3.460	2.468	1-S2n	1.613	2.051	1.708	2.429	9.757	4.329
420.00	420.00	6722.99	3.575	2.556	1-S2n	1.666	2.119	1.767	2.470	9.901	4.394
440.00	440.00	6723.11	3.689	2.646	1-S2n	1.718	2.185	1.826	2.510	10.041	4.457
460.00	460.00	6723.22	3.803	2.737	1-S2n	1.769	2.251	1.884	2.550	10.176	4.517
480.00	480.00	6723.34	3.917	2.829	1-S2n	1.819	2.316	1.941	2.588	10.305	4.576
505.00	505.00	6723.48	4.060	2.947	5-S2n	1.881	2.396	2.011	2.635	10.462	4.646
520.00	520.00	6723.57	4.146	3.019	5-S2n	1.918	2.443	2.053	2.663	10.553	4.687
540.00	540.00	6723.68	4.261	3.116	5-S2n	1.967	2.505	2.108	2.699	10.672	4.740
560.00	560.00	6723.80	4.377	3.214	5-S2n	2.015	2.567	2.163	2.735	10.787	4.792
580.00	580.00	6723.91	4.494	3.315	5-S2n	2.063	2.627	2.218	2.769	10.894	4.842
600.00	600.00	6724.03	4.612	3.417	5-S2n	2.110	2.687	2.273	2.804	11.000	4.891

Straight Culvert

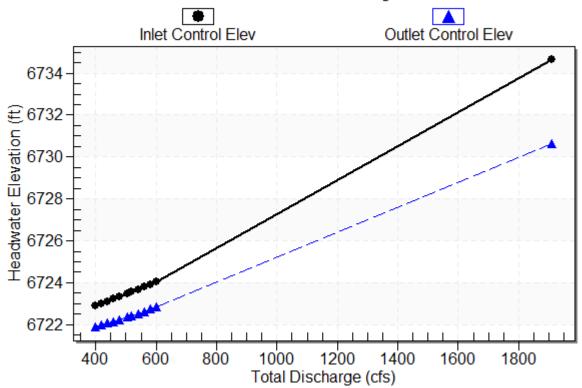
Inlet Elevation (invert): 6719.42 ft, Outlet Elevation (invert): 6719.00 ft

Culvert Length: 83.50 ft, Culvert Slope: 0.0050

Culvert Performance Curve Plot: San Isidro Crossing

Performance Curve

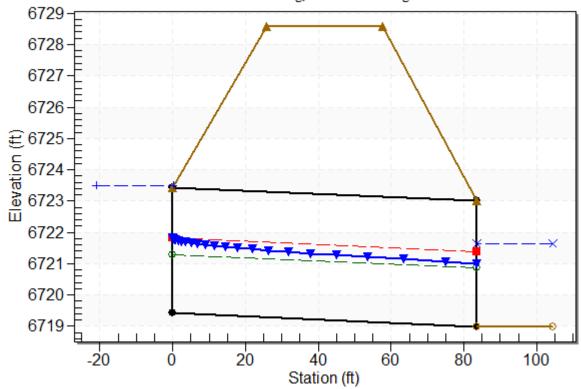
Culvert: San Isidro Crossing



Water Surface Profile Plot for Culvert: San Isidro Crossing

Crossing - San Isidro Crossing, Design Discharge - 505.0 cfs

Culvert - San Isidro Crossing, Culvert Discharge - 505.0 cfs



Site Data - San Isidro Crossing

Site Data Option: Culvert Invert Data

Inlet Station: 0.00 ft

Inlet Elevation: 6719.42 ft
Outlet Station: 83.50 ft
Outlet Elevation: 6719.00 ft

Number of Barrels: 2

Culvert Data Summary - San Isidro Crossing

Barrel Shape: Concrete Box

Barrel Span: 12.00 ft Barrel Rise: 4.00 ft

Barrel Material: Concrete Embedment: 0.00 in

Barrel Manning's n: 0.0120

Culvert Type: Straight

Inlet Configuration: Square Edge (90°) Headwall

Inlet Depression: None

Table 3 - Downstream Channel Rating Curve (Crossing: San Isidro Crossing)

Flow (cfs)	Water Surface Elev (ft)	Depth (ft)	Velocity (ft/s)	Shear (psf)	Froude Number
400.00	6721.43	2.43	4.33	0.91	0.70
420.00	6721.47	2.47	4.39	0.92	0.70
440.00	6721.51	2.51	4.46	0.94	0.70
460.00	6721.55	2.55	4.52	0.95	0.70
480.00	6721.59	2.59	4.58	0.97	0.70
505.00	6721.64	2.64	4.65	0.99	0.71
520.00	6721.66	2.66	4.69	1.00	0.71
540.00	6721.70	2.70	4.74	1.01	0.71
560.00	6721.73	2.73	4.79	1.02	0.71
580.00	6721.77	2.77	4.84	1.04	0.71
600.00	6721.80	2.80	4.89	1.05	0.72

Tailwater Channel Data - San Isidro Crossing

Tailwater Channel Option: Irregular Channel

Roadway Data for Crossing: San Isidro Crossing

Roadway Profile Shape: Constant Roadway Elevation

Crest Length: 6.00 ft

Crest Elevation: 6728.59 ft Roadway Surface: Paved Roadway Top Width: 32.00 ft

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Tuesday, Dec 21 2021

Section 13

Trapezoidal

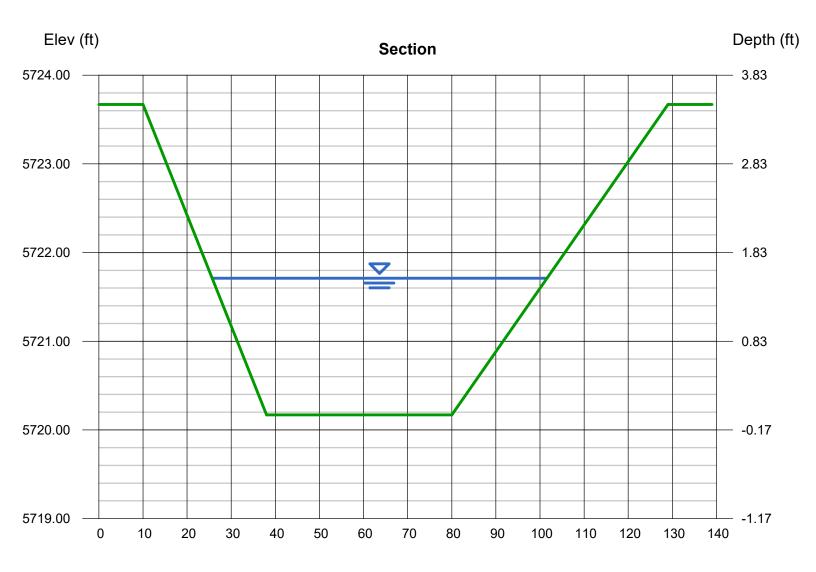
Bottom Width (ft) = 42.00 Side Slopes (z:1) = 8.00, 14.00 Total Depth (ft) = 3.50 Invert Elev (ft) = 5720.17

Slope (%) = 1.00 N-Value = 0.030

Calculations

Compute by: Known Q Known Q (cfs) = 505.00 Highlighted

Depth (ft) = 1.54Q (cfs) = 505.00Area (sqft) = 90.77Velocity (ft/s) = 5.56 Wetted Perim (ft) = 76.03 Crit Depth, Yc (ft) = 1.45Top Width (ft) = 75.88 EGL (ft) = 2.02



Reach (ft)

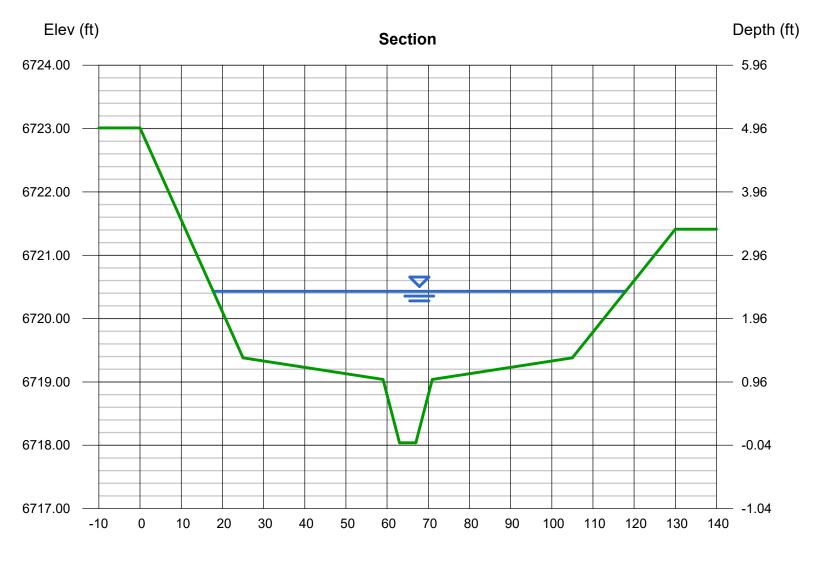
Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Tuesday, Dec 21 2021

Section 14

User-defined		Highlighted	
Invert Elev (ft)	= 6718.04	Depth (ft)	= 2.39
Slope (%)	= 0.60	Q (cfs)	= 505.00
N-Value	= 0.030	Area (sqft)	= 118.25
		Velocity (ft/s)	= 4.27
Calculations		Wetted Perim (ft)	= 100.53
Compute by:	Known Q	Crit Depth, Yc (ft)	= 2.11
Known Q (cfs)	= 505.00	Top Width (ft)	= 100.17
, ,		EGL (ft)	= 2.67

(Sta, EI, n)-(Sta, EI, n)... (0.00, 6723.01)-(25.00, 6719.38, 0.030)-(59.00, 6719.04, 0.030)-(63.00, 6718.04, 0.030)-(67.00, 6718.04, 0.030)-(71.00, 6719.04, 0.030)-(105.00, 6719.38, 0.030) -(130.00, 6721.41, 0.030)



Sta (ft)

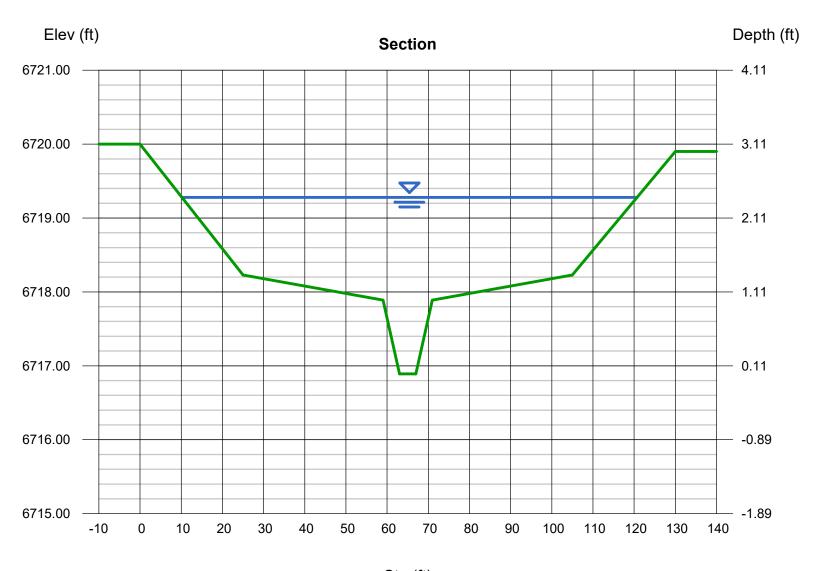
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Tuesday, Dec 21 2021

Section 15

User-defined		Highlighted	
Invert Elev (ft)	= 6716.89	Depth (ft)	= 2.39
Slope (%)	= 0.60	Q (cfs)	= 505.00
N-Value	= 0.030	Area (sqft)	= 123.70
		Velocity (ft/s)	= 4.08
Calculations		Wetted Perim (ft)	= 110.88
Compute by:	Known Q	Crit Depth, Yc (ft)	= 2.11
Known Q (cfs)	= 505.00	Top Width (ft)	= 110.56
		EGL (ft)	= 2.65

(Sta, EI, n)-(Sta, EI, n)... (0.00, 6720.00)-(25.00, 6718.23, 0.030)-(59.00, 6717.89, 0.030)-(63.00, 6716.89, 0.030)-(67.00, 6716.89, 0.030)-(71.00, 6717.89, 0.030)-(105.00, 6718.23, 0.030) -(130.00, 6719.90, 0.030)



Sta (ft)

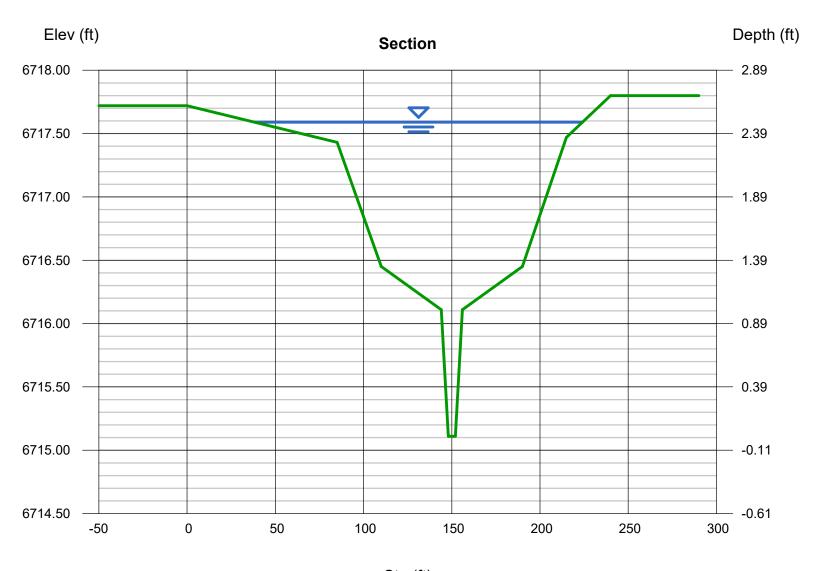
Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Tuesday, Dec 21 2021

Section 16

User-defined		Highlighted	
Invert Elev (ft)	= 6715.11	Depth (ft)	= 2.48
Slope (%)	= 0.60	Q (cfs)	= 505.00
N-Value	= 0.030	Area (sqft)	= 151.09
		Velocity (ft/s)	= 3.34
Calculations		Wetted Perim (ft)	= 186.16
Compute by:	Known Q	Crit Depth, Yc (ft)	= 2.10
Known Q (cfs)	= 505.00	Top Width (ft)	= 185.87
, ,		EGL (ft)	= 2.65

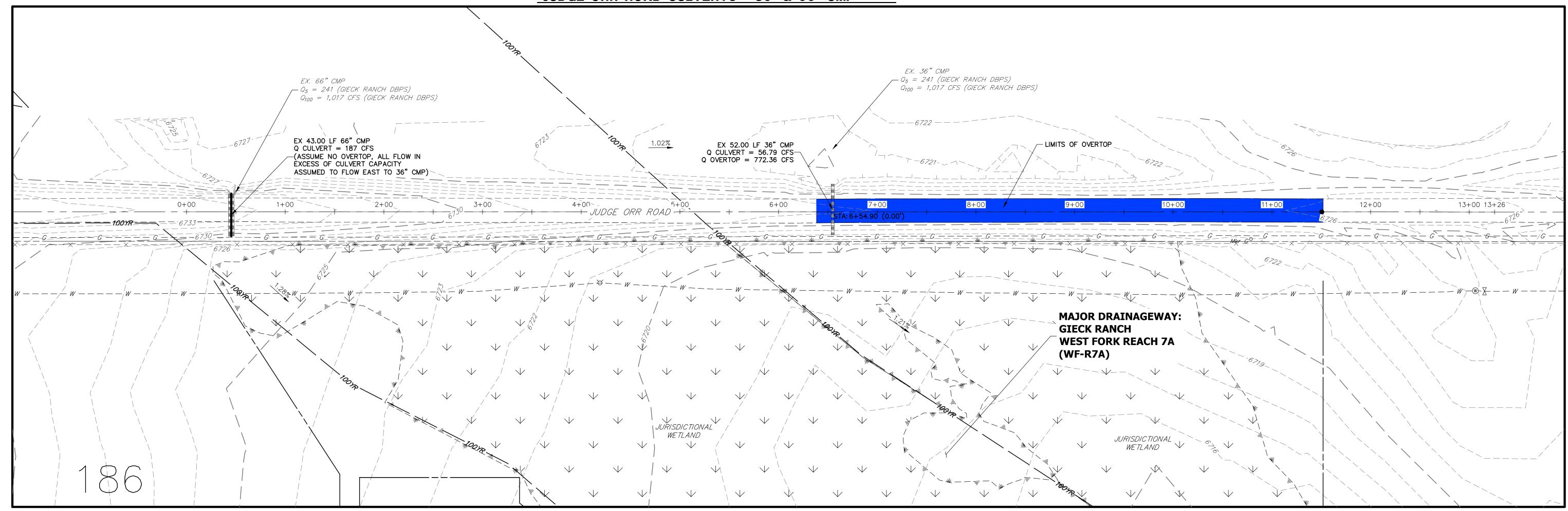
(Sta, El, n)-(Sta, El, n)... (0.00, 6717.72)-(85.00, 6717.43, 0.030)-(110.00, 6716.45, 0.030)-(144.00, 6716.11, 0.030)-(148.00, 6715.11, 0.030)-(152.00, 6715.11, 0.030)-(156.00, 6716.11, 0.030)-(156.00, 6716.11, 0.030)-(156.00, 6715.11, 0.030)-(1 -(190.00, 6716.45, 0.030)-(215.00, 6717.47, 0.030)-(240.00, 6717.80, 0.030)



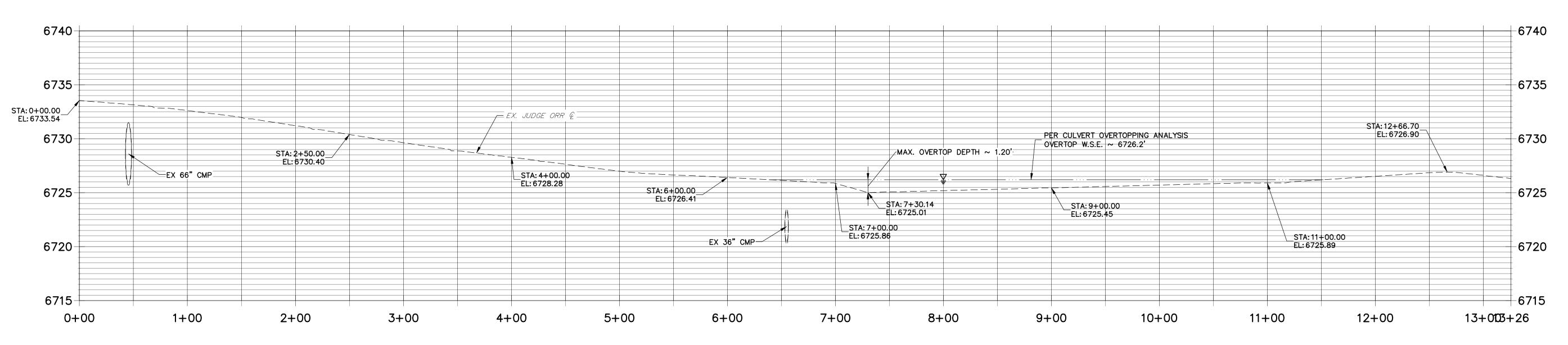
Sta (ft)

SADDLEHORN RANCH

JUDGE ORR ROAD CULVERTS - 36" & 66" CMP



JUDGE ORR ROAD WEST & EAST CULVERT ROAD PROFILE PROFILE STA 0+00.00 TO 13+25.72



SADDLEHORN RANCH EX CULVERT OVERTOPPING 2514200 11/27/19 SHEET 2 OF 2



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GIECK RANCH DRAINAGE BASIN PLANNING STUDY El Paso County, Colorado

Volume 1 – Final Report

October 1, 2007 Revised: February 10, 2010

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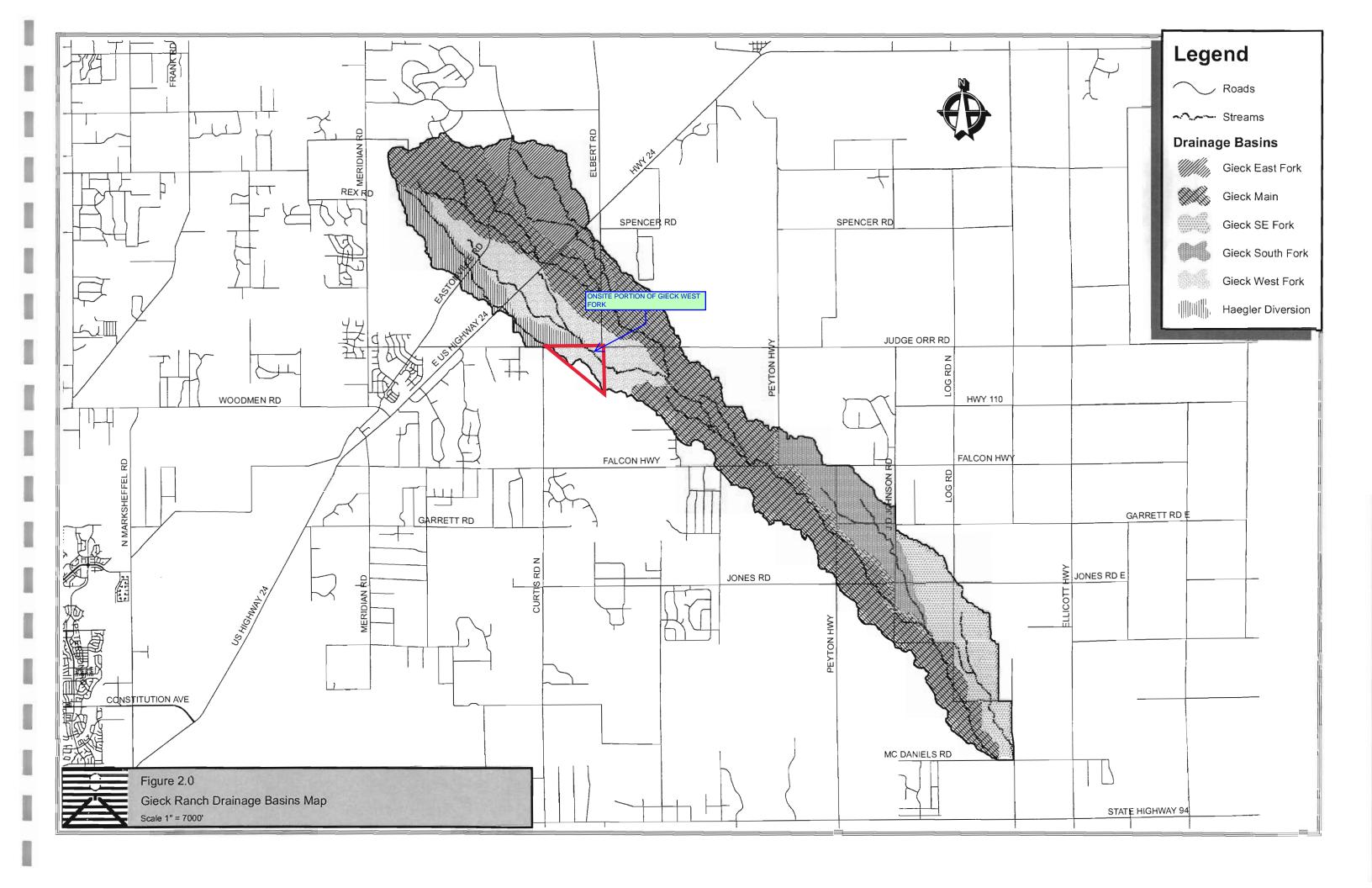


Table 6.4: Summary of Flows at Selected Design Points – 100-year Storm Event

	Summary of Flows at Science Design Forms 100 y		Accumulative	Existing	Future	%	Existing	Future	%
Design		Hydrologic	Accumulative	Existing Peak Flow	Peak Flow	Difference	Volume	Volume	Difference
Point ID	Design Point Location	Element	(mi ²)	(cfs)	(cfs)	Peak Flow	(ac-ft)	(ac-ft)	Volume
1	Haegler Diversion at Eastonville Road	HD-J2	0.8	431	1060	146%	77	96	25%
2	West Fork at Eastonville Road	WF-J1	0.3	146	389	166%	29	39	33%
3	Main Channel at Eastonville Road	MS-J4	1.3	730	1233	69%	112	135	20%
4	Haegler Diversion at Highway 24	HD-J4	1.3	521	1223	135%	97	121	24%
5	West Fork at Highway 24	WF-J3	0.4	224	605	170%	49	62	26%
6	Main Channel at Highway 24 CONTRIBUTING ACREAGE TO WE	MS-J6	2.5	997	1896	90%	194	225	16%
7	East Fork at Highway 24 R7A @ JUDGE ORR ROAD CROSSING	EF-J4	1.2	1054	1113	6%	124	126	1%
8	Main Channel at Elbert Road	MS-J7	3.0	1010	1896	88%	220	253	15%
9	Fast Fork at Filhert Road	FF-16	2.1	1120	1172	5%	183	187	2%
10	West Fork at Judge Orr Road	WF-J6	1.5	1017	2213	117%	244	291	19%
11	Confluence of East Fork and Main Channel	MS-J9	5.7	1817	3068	69%	429	467	9%
12	Main Channel at Judge Orr Road	MS-J11	6.7	1968	3383	72%	487	564	16%
13	Confluence of West Fork and Main Channel	MS-J12	11.2	2732	6104	123%	805	993	23%
14	Main Channel at Falcon Highway	MS-J16	13.4	3045	6784	123%	936	1191	27%
15	Main Channel at Peyton Highway	MS-J19	15.1	3200	6946	117%	1012	1269	25%
16	Main Channel at Jones Road	MS-J20	15.6	3250	7056	117%	1040	1308	26%
17	South Fork at Jones Road	SF-J4	1.3	454	454	0%	133	133	0%
18	Confluence of South Fork and Main Channel	MS-J22	17.9	3650	7392	103%	1210	1489	23%
19	Southeast Fork at McDaniels Road	SE-J3	2.4	547	546	0%	210	210	0%
20	Main Channel at McDaniels Road	MS-J29	19.6	3791	7525	99%	1293	1597	23%
21	Total Combined Outfall	SE-J3 plus MS-J29	22.0	4326	7687	78%	1503	1807	20%

The 100-year storm event future undetained peak flow is estimated to increase by 78% over the existing peak flow while the future volume of runoff is estimated to increase by 20%.

During the hydrologic analysis it was observed that the Black Squirrel Creek lies very close to the eastern boundary of the Gieck Ranch Basin from Falcon Highway downstream to Log Road. It is possible that flow from Black Squirrel Creek could spill into the Gieck Ranch Basin during extreme storm events. The flows in Black Squirrel Creek in this area are expected to be more than 5,000 cfs for the 100-year event. If the Black Squirrel Creek were to overflow its' banks and flow into the Gieck Ranch Basin it could increase the flows shown in the above tables. Possible improvements to address this potential problem include channel improvements to increase the Black Squirrel Creek conveyance in this area or constructing berms on the east bank to prevent overflow.

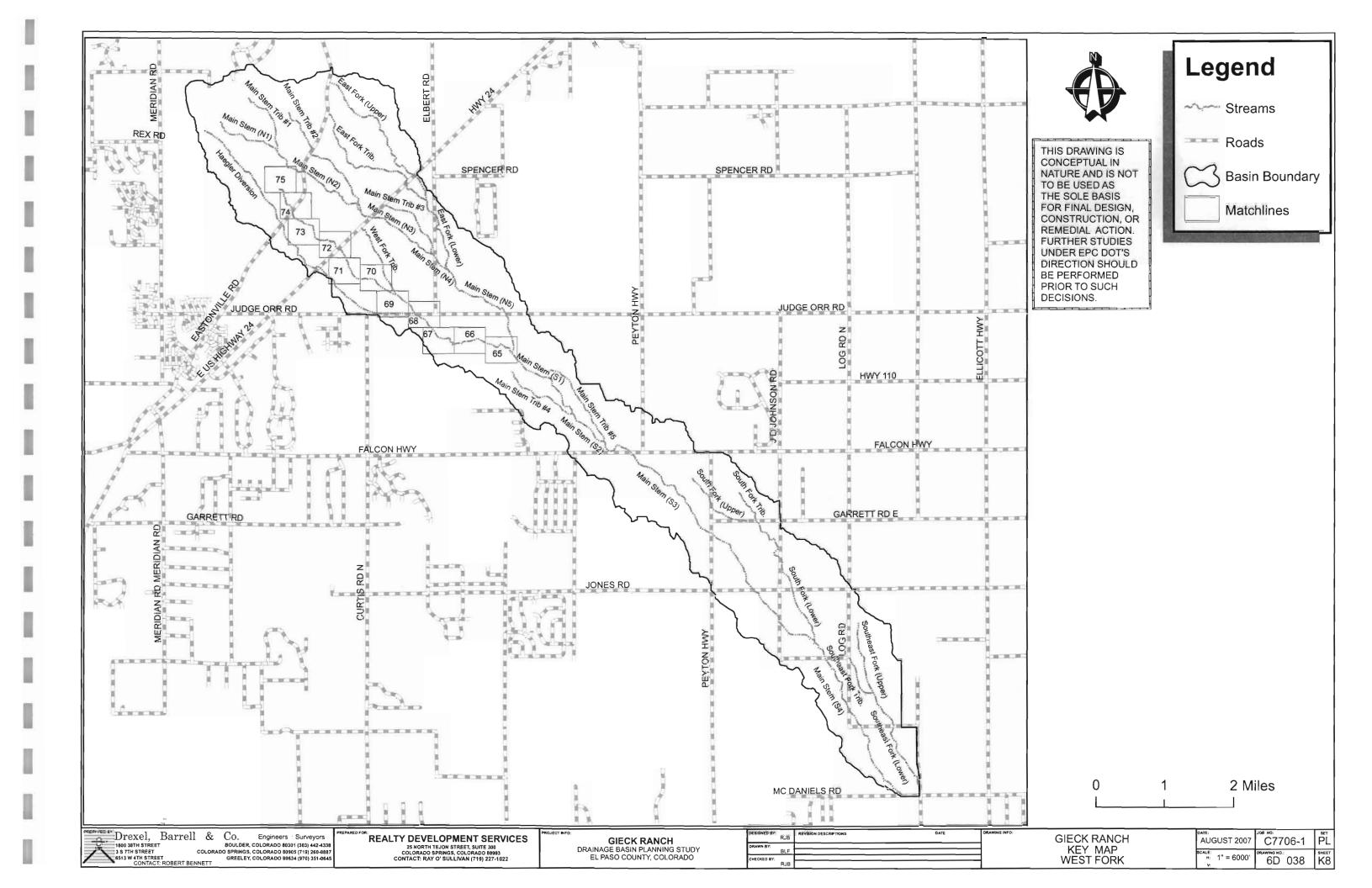
35	Elbert Road south of structure 34	24" CMP	Good	100%	Y	
36	Elbert Road at Main Channel	2 - 48" CMP	Good	19%	N	3 - 12' x 4' CB
37	Elbert Road south of structure 36	24" CMP	Poor	55%	Y	
		6711 -: 0511				
38	Judge Orr Road at West Fork	CMP	Good	20%	N	4 - 12' x 5' CB
39	Judge Orr Road east of structure 38	36" CMP	Good	100%	Y	
10	Judge Orr Road west of structure 41	24" CMP	Poor	90%	Y	
11	Judge Orr Road at Main Channel	Bridge	Good	100%	Y	
12	Falcon Hwy at Main Channel	Bridge	<u>G</u> ood	57%	N	85' Span
13	Peyton Road at headwaters of South Fork	24" CMP	Fair	75%	<u>Y</u>	
14	Peyton Road at Main Channel	4 - 24" RCP	Good	2%	N	5 - 12' x 7' CE
15	Peyton Road south of structure 44	36" CMP	Poor	100%	Y	
16	Peyton Road south of structure 45	24" CMP	Good	100%	Y	
7	East Garrett Road west of structure 48	24" CMP	Poor	100%	Y	
18	East Garrett Road at South Fork	48" CMP	Good	14%	N	2 - 5' x 4' CB
19	J.D. Johnson Road at South Fork	4 - 42" RCP	Good	63%	N	2 - 12' x 4' CF
0	J.D. Johnson Road south of structure 49	30" CMP	Fair	56%	N	36" CMP
51	J.D. Johnson Road south of structure 50	30" CMP	Fair	100%	Y	
52	Jones Road at Main Channel	60" CMP	Fair	4%	N	6 - 12' x 7' CE
53	J.D. Johnson Road at Jones Road	30" CMP	Fair	55%	Y	
54	Jones Road east of J.D. Johnson Road	30" CMP	Good	73%	Y	
55	Jones Road at South Fork	36" CMP	Good	6%	N	2 - 7' x 5' CB
56	Jones Road east of structure 55	30" CMP	Fair	67%	Y	
57	J.D. Johnson Road at Main Channel US of structure 58	3 - 60" RCP	Good	14%	N	85' Span
8	J.D. Johnson Road at Main Channel	30" CMP	Good	1%	N	120' Span
9	J.D. Johnson Road and Log Road	24" CMP	Fair	23%	N	2 - 6' x 3' CB
		48" CMP				
60	Main Channel at private driveway	(est.)	Unknown	2%	<u>N.E.</u>	
51	Log Road at Main Channel	Bridge	Good	36%	N	120' Span
(2	McDeviel Developed in Classic	30" x 48"	0 1	10/	3.7	1001.0
<u>62</u>	McDaniel Road at Main Channel	Oval CMP	Good	1%	N	120' Span
63	Log Road and McDaniels Road	24" CMP	Good	2%	N	5 - 6' x 3' C

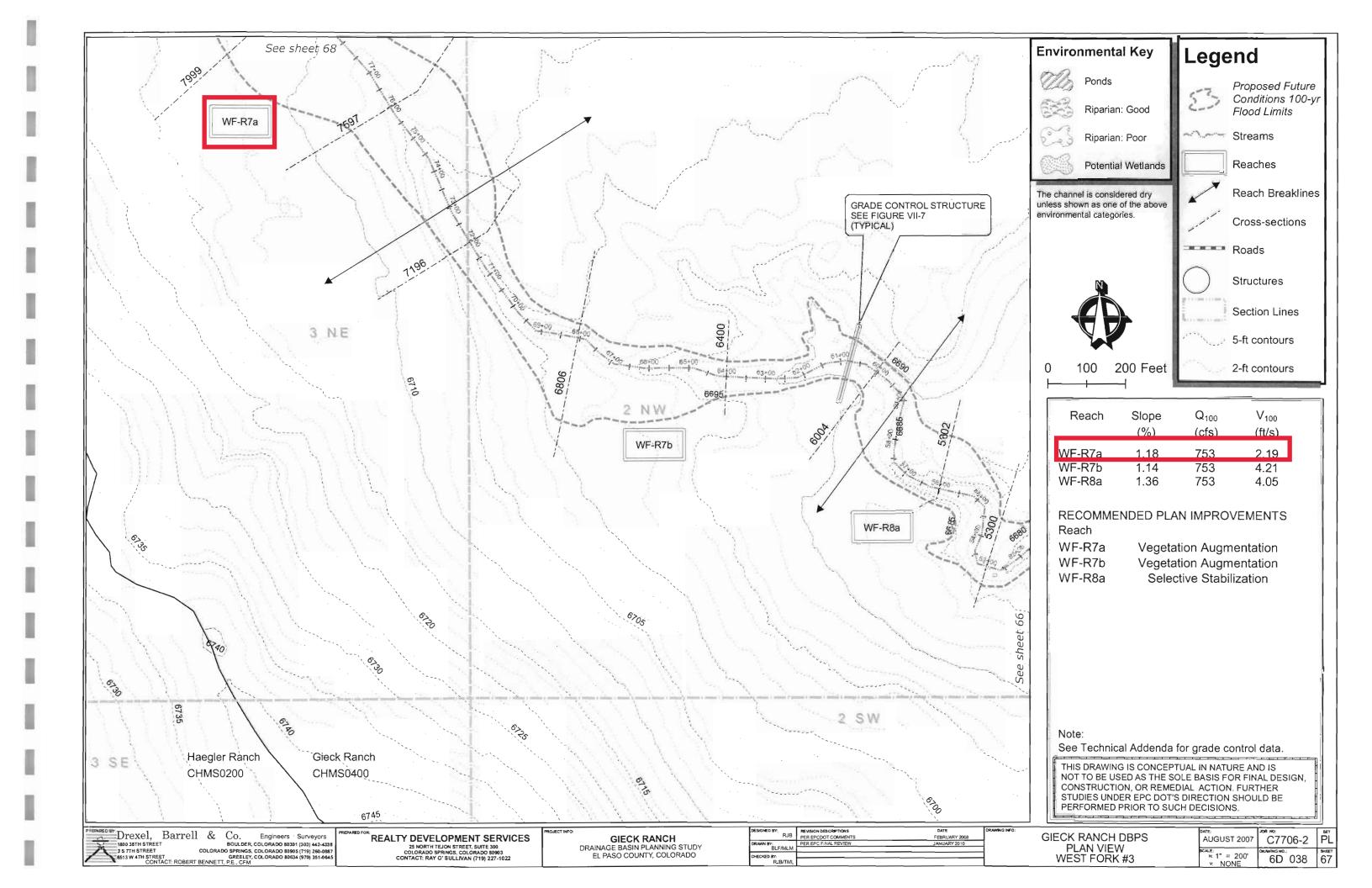
^{*} Road over-topping not included

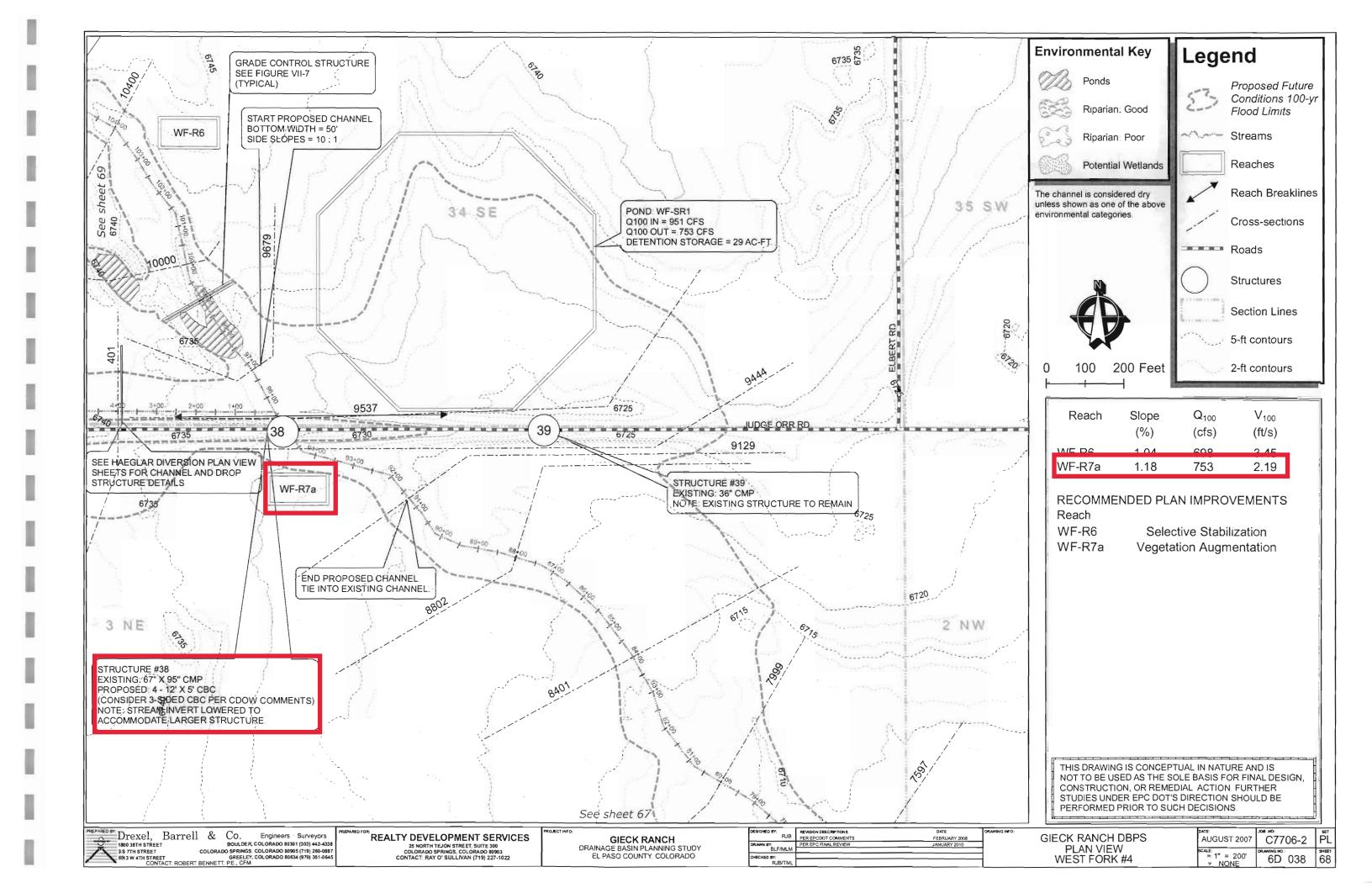
^{**} Allowable road over-topping included in adequacy analysis

^{***} Based on proposed (with selected drainage basin plan) flows

N.E. Not Evaluated, not EPCDOT responsibility

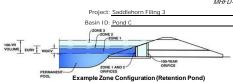






DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.04 (February 2021)



Watershe

itershed Information		
Selected BMP Type =	EDB	
Watershed Area =	96.84	acres
Watershed Length =	5,370	ft
Watershed Length to Centroid =	1,383	ft
Watershed Slope =	0.012	ft/ft
Watershed Imperviousness =	14.60%	percent
Percentage Hydrologic Soil Group A =	93.0%	percent
Percentage Hydrologic Soil Group B =	0.0%	percent
Percentage Hydrologic Soil Groups C/D =	7.0%	percent
Target WQCV Drain Time =	40.0	hours
Location for 1-hr Rainfall Depths =	User Input	

After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

the embedded Colorado Urban Hydrograph Procedure.					
Water Quality Capture Volume (WQCV) =	0.737	acre-feet			
Excess Urban Runoff Volume (EURV) =	1.159	acre-feet			
2-yr Runoff Volume (P1 = 1.19 in.) =	0.711	acre-feet			
5-yr Runoff Volume (P1 = 1.5 in.) =	1.074	acre-feet			
10-yr Runoff Volume (P1 = 1.75 in.) =	1.450	acre-feet			
25-yr Runoff Volume (P1 = 2 in.) =	3.279	acre-feet			
50-yr Runoff Volume (P1 = 2.25 in.) =	4.653	acre-feet			
100-yr Runoff Volume (P1 = 2.52 in.) =	6.705	acre-feet			
500-yr Runoff Volume (P1 = 3.14 in.) =	11.187	acre-feet			
Approximate 2-yr Detention Volume =	0.724	acre-feet			
Approximate 5-yr Detention Volume =	1.034	acre-feet			
Approximate 10-yr Detention Volume =	1.331	acre-feet			
Approximate 25-yr Detention Volume =	1.735	acre-feet			
Approximate 50-yr Detention Volume =	2.136	acre-feet			
Approximate 100-yr Detention Volume =	3.064	acre-feet			

Optional User Overrides				
	acre-feet			
	acre-feet			
1.19	inches			
1.50	inches			
1.75	inches			
2.00	inches			
2.25	inches			
2.52	inches			
	inches			

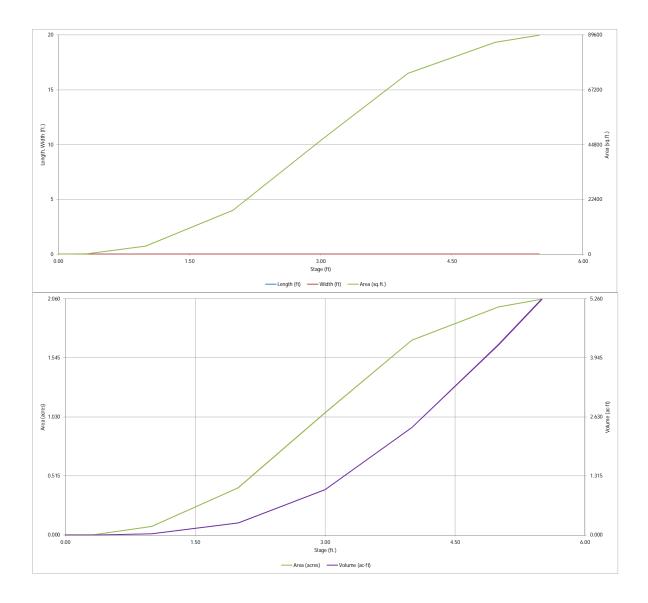
Define Zones and Basin Geometry

Define Zones and Basin Geometry		
Zone 1 Volume (WQCV) =	0.737	acre-f
Zone 2 Volume (EURV - Zone 1) =	0.422	acre-f
Zone 3 Volume (100-year - Zones 1 & 2) =	1.906	acre-f
Total Detention Basin Volume =	3.064	acre-f
Initial Surcharge Volume (ISV) =	user	ft ³
Initial Surcharge Depth (ISD) =	user	ft
Total Available Detention Depth (H _{total}) =	user	ft
Depth of Trickle Channel (H _{TC}) =	user	ft
Slope of Trickle Channel (S _{TC}) =	user	ft/ft
Slopes of Main Basin Sides (Smain) =	user	H:V
Basin Length-to-Width Ratio (R _{L/W}) =	user	

Initial Surcharge Area (A _{ISV}) =	user	ft ²
Surcharge Volume Length (L _{ISV}) =	user	ft
Surcharge Volume Width (W _{ISV}) =	user	ft
Depth of Basin Floor (H _{FLOOR}) =	user	ft
Length of Basin Floor (LFLOOR) =	user	ft
Width of Basin Floor (W _{FLOOR}) =	user	ft
Area of Basin Floor (A _{FLOOR}) =	user	ft ²
Volume of Basin Floor (V _{FLOOR}) =	user	ft ³
Depth of Main Basin (H _{MAIN}) =	user	ft
Length of Main Basin (L _{MAIN}) =	user	ft
Width of Main Basin (W _{MAIN}) =	user	ft
Area of Main Basin (A _{MAIN}) =	user	ft ²
Volume of Main Basin (V _{MAIN}) =	user	ft ³
Calculated Total Basin Volume (Vtotal) =	user	acre-feet

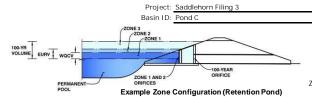
			1.							
	Depth Increment =		ft Optional				Optional			
	Stage - Storage Description	Stage (ft)	Override Stage (ft)	Length (ft)	Width (ft)	Area (ft 2)	Override Area (ft ²)	Area (acre)	Volume (ft 3)	Volume (ac-ft)
).67	Top of Micropool		0.00				32	0.001		
	6711		0.33				50	0.001	14	0.000
	6712 6713		1.00 2.00				3,260 17,980	0.075	1,122 11,742	0.026
	6714		3.00				46,439	1.066	43,952	1.009
	6715		4.00				73,964	1.698	104,153	2.391
	6716		5.00				86,681	1.990	184,476	4.235
	6716.5		5.50				89,520	2.055	228,526	5.246
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MHFD-Detention_v4 04_Pond C.xlsm, Basin 12/14/2021, 2:54 PM



M#FD-Detention_w4 04_Pond C.xlsm, Basin 12/14/2021, 2:54 PM

MHFD-Detention, Version 4.04 (February 2021)



	Estimated	Estimated	
	Stage (ft)	Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	2.73	0.737	Orifice Plate
Zone 2 (EURV)	3.14	0.422	Orifice Plate
Zone 3 (100-year)	4.39	1.906	Weir&Pipe (Restrict)
•	Total (all zones)	3.064	

<u>User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)</u>

Underdrain Orifice Invert Depth = N/A ft (distance below the filtration media surface)
Underdrain Orifice Diameter = N/A inches

	Calculated Paramet	ers for Underdrain
Underdrain Orifice Area =	N/A	ft ²
Underdrain Orifice Centroid =	N/A	feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice = 0.00 ft (relative to basin bottom at Stage = 0 ft)

Depth at top of Zone using Orifice Plate = 3.14 ft (relative to basin bottom at Stage = 0 ft)

Orifice Plate: Orifice Vertical Spacing = N/A inches

Orifice Plate: Orifice Area per Row = 2.44 sq. inches (diameter = 1-3/4 inches)

	Calculated Paramete	ers for Plate
VQ Orifice Area per Row =	1.694E-02	ft ²
Elliptical Half-Width =	N/A	feet
Elliptical Slot Centroid =	N/A	feet
Elliptical Slot Area =	N/A	ft ²
		•

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	0.91	1.82					
Orifice Area (sq. inches)	2.44	2.44	2.44					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

	Not Selected	Not Selected			
Invert of Vertical Orifice =	N/A	N/A	ft (relative to basin bottom at Stage = 0 ft)		
Depth at top of Zone using Vertical Orifice =	N/A	N/A	ft (relative to basin bottom at Stage = 0 ft)		
Vertical Orifice Diameter =	N/A	N/A	inches		

	Calculated Paramet	ers for Vertical Orific	e
	Not Selected	Not Selected	
Vertical Orifice Area =	N/A	N/A	ft ²
ertical Orifice Centroid =	N/A	N/A	feet
			-

User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe)

	Zone 3 weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	3.17	N/A	ft (relative to basin bottom at Stage = 0 f
Overflow Weir Front Edge Length =	6.00	N/A	feet
Overflow Weir Grate Slope =	0.00	N/A	H:V
Horiz. Length of Weir Sides =	5.00	N/A	feet
Overflow Grate Type =	Type C Grate	Type C Grate	
Debris Clogging % =	0%	N/A	%

Pipe)		Calculated Parameters for Overflow Weir			
		Zone 3 Weir	Not Selected		
ft)	Height of Grate Upper Edge, $H_t =$	3.17	N/A	feet	
	Overflow Weir Slope Length =	5.00	N/A	feet	
Grat	te Open Area / 100-yr Orifice Area =	4.25	N/A		
Ove	erflow Grate Open Area w/o Debris =	20.88	N/A	ft ²	
Ov	verflow Grate Open Area w/ Debris =	20.88	N/A	ft ²	
	•				

V

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

	Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	0.39	N/A	ft (distance below basin bottom at Stage = 0 ft)
Outlet Pipe Diameter =	30.00	N/A	inches
Restrictor Plate Height Above Pipe Invert =	30.00		inches Half-Central A

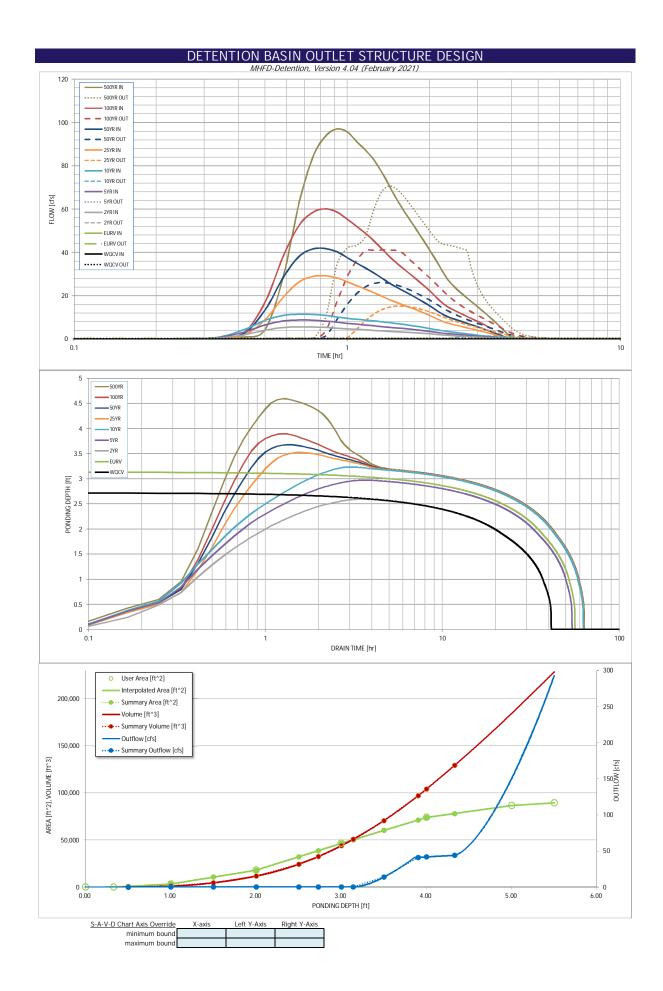
	Calculated Parameter	s for Outlet Pipe w/	Flow Restriction Plat	e
		Zone 3 Restrictor	Not Selected	
at Stage = 0 ft)	Outlet Orifice Area =	4.91	N/A	ft ²
	Outlet Orifice Centroid =	1.25	N/A	feet
Half-Central Angle	of Restrictor Plate on Pipe =	3.14	N/A	radia

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage=	4.33	ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length =	60.00	feet
Spillway End Slopes =	4.00	H:V
Freehoard above May Water Surface -	1.00	foot

	Calculated Paramet	ers for Spil
Spillway Design Flow Depth=	0.47	feet
Stage at Top of Freeboard =	5.80	feet
Basin Area at Top of Freeboard =	2.06	acres
Basin Volume at Top of Freeboard =	5.25	acre-ft

Routed Hydrograph Results Design Storm Return Period WOCV FURV 5 Year 50 Year 100 Yea 500 Year One-Hour Rainfall Depth (in) N/A N/A 1.19 1.50 1.75 2.00 2.25 2.52 3.14 CUHP Runoff Volume (acre-ft) 1.074 3.279 4.653 Inflow Hydrograph Volume (acre-ft) N/A N/A 0.711 1.074 1.450 3.279 4.653 6.705 11.187 CUHP Predevelopment Peak Q (cfs) N/A N/A 0.6 1.0 1.4 17.2 29.1 46.2 81.5 OPTIONAL Override Predevelopment Peak Q (cfs) N/A N/A Predevelopment Unit Peak Flow, q (cfs/acre) 0.01 0.01 0.18 0.84 N/A N/A 0.01 0.30 0.48 Peak Inflow Q (cfs) N/A N/A 8.8 11.5 41.8 60.2 97.1 Peak Outflow Q (cfs) 15.3 41.2 70.6 0.3 0.4 0.3 0.3 1.5 26.2 Ratio Peak Outflow to Predevelopment Q N/A N/A N/A 0.3 1.1 0.9 0.9 0.9 0.9 Structure Controlling Flow Plate Plate Plate Plate Overflow Weir 1 Overflow Weir 1 Overflow Weir 1 Outlet Plate Spillway Max Velocity through Grate 1 (fps) N/A N/A N/A N/A 0.0 0.7 Max Velocity through Grate 2 (fps) N/A N/A N/A N/A N/A N/A N/A N/A N/A Time to Drain 97% of Inflow Volume (hours) 49 38 51 38 53 50 46 39 Time to Drain 99% of Inflow Volume (hours) 40 54 40 52 60 58 57 55 52 Maximum Ponding Depth (ft) 2 73 3 14 2 59 2 97 3.68 3.90 4 60 Area at Maximum Ponding Depth (acres) 0.89 1.15 0.80 1.05 1.21 1.39 1.49 1.63 1.87 Maximum Volume Stored (acre-ft)



Outflow Hydrograph Workbook Filename:

Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

ĺ	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
	0:00:00									
5.00 min		0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00 0:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.01	0.00	0.04
	0:20:00	0.00	0.00	0.10	0.17	0.21	0.14	0.19	0.18	0.30
	0:25:00	0.00	0.00	1.97	3.17	4.25	1.80	2.42	2.78	4.35
	0:30:00	0.00	0.00	4.09	6.54	8.67	8.92	13.39	17.00	28.89
	0:35:00	0.00	0.00	5.34	8.37	10.93	19.40	28.58	38.34	63.01
	0:40:00	0.00	0.00	5.67	8.81	11.51	26.43	38.22	52.58	84.28
	0:45:00	0.00	0.00	5.63	8.71	11.43	28.97	41.67	58.62	93.78
	0:50:00	0.00	0.00	5.41	8.36	10.97	29.22	41.84	60.17	97.06
	0:55:00 1:00:00	0.00	0.00	5.09	7.81	10.24	28.29	40.33	58.73	95.68
	1:05:00	0.00	0.00	4.78 4.53	7.31 6.90	9.62 9.18	26.48 24.70	37.63 35.08	55.34 52.05	91.22 87.27
	1:10:00	0.00	0.00	4.30	6.53	8.80	23.10	32.81	48.89	82.89
	1:15:00	0.00	0.00	4.05	6.16	8.46	21.54	30.61	45.46	77.40
	1:20:00	0.00	0.00	3.80	5.77	8.05	19.95	28.35	41.94	71.50
	1:25:00	0.00	0.00	3.60	5.48	7.67	18.40	26.11	38.52	65.69
	1:30:00	0.00	0.00	3.45	5.23	7.28	17.12	24.29	35.66	60.79
	1:35:00	0.00	0.00	3.29	4.98	6.89	16.01	22.68	33.19	56.44
	1:40:00	0.00	0.00	3.14	4.72	6.50	14.98	21.19	30.91	52.44
	1:45:00	0.00	0.00	2.98	4.45 4.16	6.11 5.72	13.97 12.98	19.72 18.28	28.72 26.58	48.62 44.92
	1:55:00	0.00	0.00	2.66	3.88	5.72	12.98	16.85	24.45	41.27
	2:00:00	0.00	0.00	2.46	3.59	4.94	11.02	15.43	22.36	37.68
	2:05:00	0.00	0.00	2.25	3.28	4.51	10.01	13.99	20.25	34.12
	2:10:00	0.00	0.00	2.04	2.97	4.09	8.98	12.52	18.13	30.57
	2:15:00	0.00	0.00	1.88	2.75	3.78	8.07	11.25	16.28	27.54
	2:20:00	0.00	0.00	1.75	2.56	3.53	7.40	10.34	14.92	25.29
	2:25:00	0.00	0.00	1.63	2.39	3.28	6.89	9.63	13.86	23.44
	2:30:00	0.00	0.00	1.52	2.22	3.05	6.43	9.00	12.92	21.80
	2:40:00	0.00	0.00	1.41	2.06	2.83	6.01 5.60	7.83	12.06 11.24	20.29 18.86
	2:45:00	0.00	0.00	1.20	1.77	2.41	5.20	7.27	10.44	17.49
	2:50:00	0.00	0.00	1.11	1.62	2.21	4.81	6.73	9.67	16.20
	2:55:00	0.00	0.00	1.02	1.49	2.03	4.44	6.20	8.92	14.95
	3:00:00	0.00	0.00	0.93	1.36	1.85	4.07	5.67	8.18	13.71
	3:05:00	0.00	0.00	0.84	1.23	1.67	3.70	5.16	7.44	12.48
	3:10:00 3:15:00	0.00	0.00	0.75	1.10	1.50	3.33	4.64	6.71	11.26
	3:20:00	0.00	0.00	0.67	0.97	1.33	2.97 2.61	4.13 3.62	5.97 5.24	10.03 8.81
	3:25:00	0.00	0.00	0.51	0.73	1.00	2.25	3.11	4.51	7.60
	3:30:00	0.00	0.00	0.43	0.61	0.84	1.89	2.61	3.79	6.38
	3:35:00	0.00	0.00	0.35	0.49	0.68	1.54	2.10	3.06	5.17
	3:40:00	0.00	0.00	0.27	0.38	0.53	1.19	1.60	2.34	3.96
	3:45:00	0.00	0.00	0.20	0.27	0.39	0.85	1.12	1.63	2.78
	3:50:00	0.00	0.00	0.16	0.21	0.30	0.53	0.66	0.96	1.70
	3:55:00 4:00:00	0.00	0.00	0.13	0.17	0.25	0.33	0.41	0.58	0.75
	4:05:00	0.00	0.00	0.10	0.13	0.21	0.23	0.29	0.39	0.75
	4:10:00	0.00	0.00	0.08	0.11	0.16	0.14	0.17	0.20	0.35
	4:15:00	0.00	0.00	0.07	0.09	0.13	0.11	0.14	0.14	0.24
	4:20:00 4:25:00	0.00	0.00	0.06	0.08	0.11	0.09	0.11	0.10	0.15
	4:30:00	0.00	0.00	0.04	0.05	0.07	0.06	0.07	0.06	0.08
	4:35:00	0.00	0.00	0.03	0.04	0.05	0.05	0.05	0.05	0.06
	4:40:00 4:45:00	0.00	0.00	0.03	0.03	0.04	0.04	0.04	0.04	0.05
	4:50:00	0.00	0.00	0.01	0.02	0.02	0.02	0.02	0.02	0.03
	4:55:00	0.00	0.00	0.01	0.01	0.02	0.02	0.02	0.02	0.02
	5:00:00 5:05:00	0.00	0.00	0.01	0.01	0.01	0.01 0.01	0.01 0.01	0.01	0.01
	5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:20:00 5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:40:00 5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

MHFD-Detention, Version 4.04 (February 2021)

Summary Stage-Area-Volume-Discharge Relationships

The user can create a summary S-A-V-D by entering the desired stage increments and the remainder of the table will populate automatically. The user should graphically compare the summary S-A-V-D table to the full S-A-V-D table in the chart to confirm it captures all key transition points.

g	<u>'</u>	,					
Stage - Storage	Stage	Area	Area	Volume	Volume	Total	
Description		re. 21	[]	rs. 3a	F== 641	Outflow	
· ·	[ft]	[ft²]	[acres]	[ft ³]	[ac-ft]	[cfs]	_
	0.50	864	0.020	91	0.002	0.06	For
		3,260	0.075	1,122	0.026	0.11	stag
	1.00						chai
	1.50	10,620	0.244	4,592	0.105	0.16	fron
	2.00	17,980	0.413	11,742	0.270	0.24	She
	2.50	32,209	0.739	24,289	0.558	0.30	
WQCV	2.73	38,755	0.890	32,450	0.745	0.32	Also
	3.00	46,439	1.066	43,952	1.009	0.35	outl
FUDV		50,292	1.155	50,723	1.164	0.36	ove
EURV	3.14						whe
	3.50	60,201	1.382	70,612	1.621	13.83	+
100-YR	3.90	71,211	1.635	96,894	2.224	41.21	_
	4.00	73,964	1.698	104,153	2.391	41.88	
Spillway	4.33	78,161	1.794	129,254	2.967	44.03	
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For best results, include the stages of all grade slope changes (e.g. ISV and Floor) from the S-A-V table on Sheet 'Basin'.

Also include the inverts of all outlets (e.g. vertical orifice, overflow grate, and spillway, where applicable).

POND C FOREBAY VOLUME REQUIREMENTS

Equation 3-1 $WQCV = a(0.91I^3 - 1.19I^2 + 0.781I)$ a=1 (40 hour drain time)

Equation 3-3 V=(WQCV/12)A

PROPOSED FOREBAY A= 80.46 Acres V= 0.611 FUTURE FOREBAY A= 16.38 Acres V= 0.103

3% OF WQCV

FOREBAY TOTAL VOLUME= .03(V)

VOLUME REQUIRED FOR PROPOSED FOREBAY =0.018 AC-FT798 CFVOLUME REQUIRED FOR FUTURE FOREBAY =0.003 AC-FT134 CF

VOLUME PROVIDED FOR PROPOSED FOREBAY = 0.023 AC-FT 993 CF

Q₁₀₀ DISCHARGES 2% OF Q₁₀₀

 Q_{100} PROPOSED FOREBAY= .02*50.0 CFS= 1.00 CFS Q_{100} FUTURE FOREBAY= .02*14.3 CFS= 0.29 CFS

Weir Report

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Monday, Dec 13 2021

Pond C Forebay 1 Notch

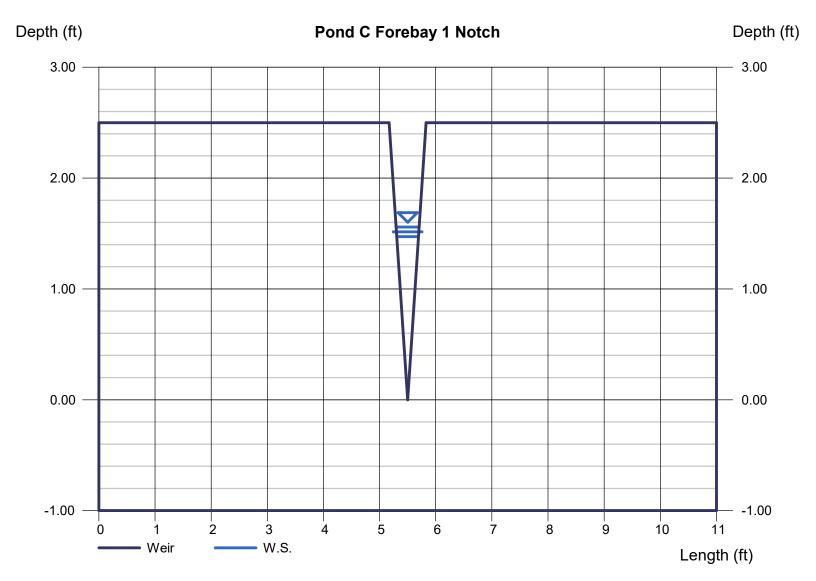
V-Notch Weir	
Crest	= Sharp
Angle (Deg)	= 15
Total Depth (ft)	= 2.50

Calculations

Weir Coeff. Cw = 0.33Compute by: Known Q Known Q (cfs) = 1.00

Highlighted

Depth (ft) = 1.56 Q (cfs) = 1.000 Area (sqft) = 0.32 Velocity (ft/s) = 3.13 Top Width (ft) = 0.41



Channel Report

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

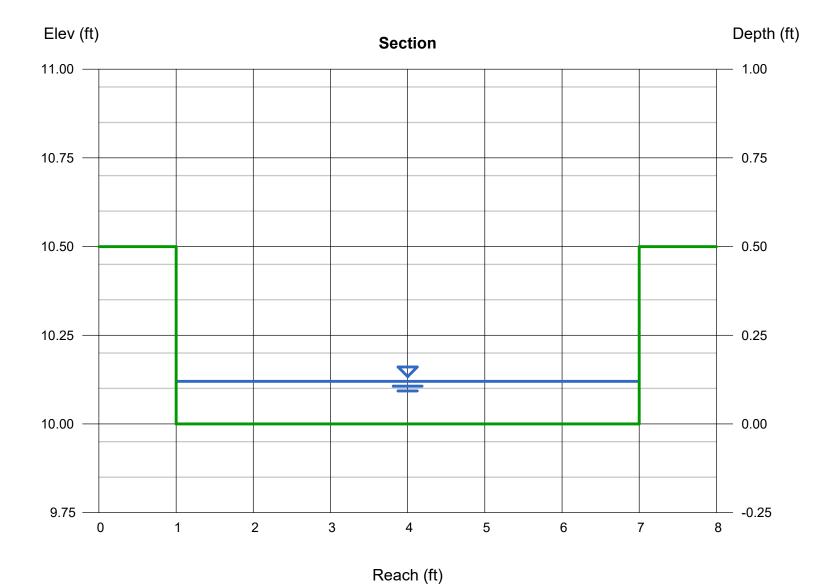
= 1.29

Monday, Dec 13 2021

Pond C Trickle Channel

Known Q (cfs)

	Highlighted	
= 6.00	Depth (ft)	= 0.12
= 0.50	Q (cfs)	= 1.290
	Area (sqft)	= 0.72
= 10.00	Velocity (ft/s)	= 1.79
= 0.50	Wetted Perim (ft)	= 6.24
= 0.013	Crit Depth, Yc (ft)	= 0.12
	Top Width (ft)	= 6.00
	EGL (ft)	= 0.17
Known Q		
	= 0.50 = 10.00 = 0.50 = 0.013	= 6.00 = 0.50 Depth (ft) Q (cfs) Area (sqft) Velocity (ft/s) = 0.50 Wetted Perim (ft) Crit Depth, Yc (ft) Top Width (ft) EGL (ft)



Weir Report

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Tuesday, Dec 14 2021

Pond C Spillway

Tra	pezo	oidal	Weir
	P 1		

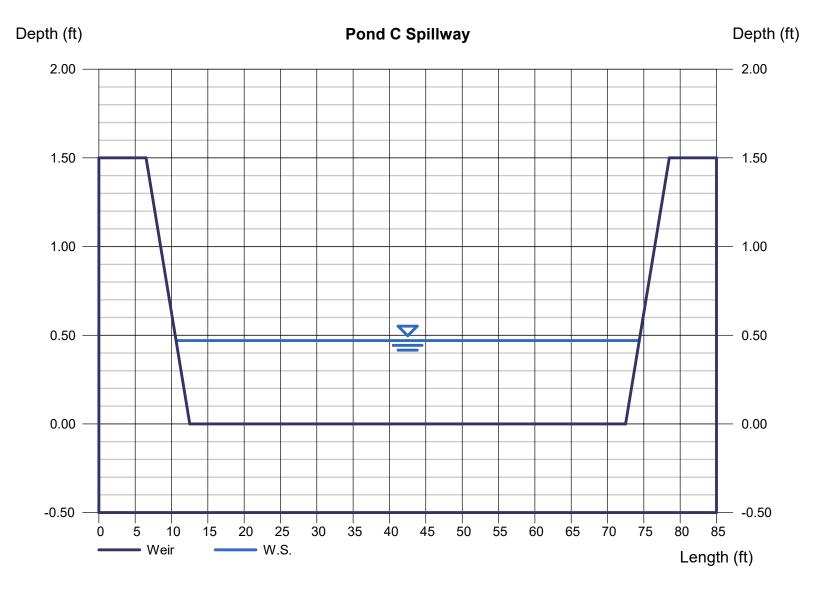
Crest = Sharp Bottom Length (ft) = 60.00 Total Depth (ft) = 1.50 Side Slope (z:1) = 4.00

Calculations

Weir Coeff. Cw = 3.10Compute by: Known Q Known Q (cfs) = 60.20

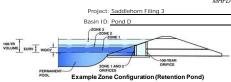
Highlighted

Depth (ft) = 0.47 Q (cfs) = 60.20 Area (sqft) = 29.08 Velocity (ft/s) = 2.07 Top Width (ft) = 63.76



DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.04 (February 2021)



Watershed Information

itersned Information		
Selected BMP Type =	EDB	
Watershed Area =	78.02	acres
Watershed Length =	3,473	ft
Watershed Length to Centroid =	970	ft
Watershed Slope =	0.012	ft/ft
Watershed Imperviousness =	15.40%	percent
Percentage Hydrologic Soil Group A =	70.0%	percent
Percentage Hydrologic Soil Group B =	0.0%	percent
Percentage Hydrologic Soil Groups C/D =	30.0%	percent
Target WQCV Drain Time =	40.0	hours
Location for 1-hr Rainfall Depths =	User Input	

After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

the embedded Colorado Urban Hydrograph Procedure.						
Water Quality Capture Volume (WQCV) =	0.619	acre-feet				
Excess Urban Runoff Volume (EURV) =	1.007	acre-feet				
2-yr Runoff Volume (P1 = 1.19 in.) =	0.755	acre-feet				
5-yr Runoff Volume (P1 = 1.5 in.) =	1.188	acre-feet				
10-yr Runoff Volume (P1 = 1.75 in.) =	2.116	acre-feet				
25-yr Runoff Volume (P1 = 2 in.) =	3.929	acre-feet				
50-yr Runoff Volume (P1 = 2.25 in.) =	5.225	acre-feet				
100-yr Runoff Volume (P1 = 2.52 in.) =	7.358	acre-feet				
500-yr Runoff Volume (P1 = 3.14 in.) =	11.183	acre-feet				
Approximate 2-yr Detention Volume =	0.683	acre-feet				
Approximate 5-yr Detention Volume =	1.098	acre-feet				
Approximate 10-yr Detention Volume =	1.393	acre-feet				
Approximate 25-yr Detention Volume =	1.747	acre-feet				
Approximate 50-yr Detention Volume =	2.024	acre-feet				
Approximate 100-yr Detention Volume =	2.808	acre-feet				
•						

Optional User Overrides				
acre-feet				
	acre-feet			
1.19	inches			
1.50	inches			
1.75	inches			
2.00	inches			
2.25	inches			
2.52	inches			
	inches			
	1.19 1.50 1.75 2.00 2.25			

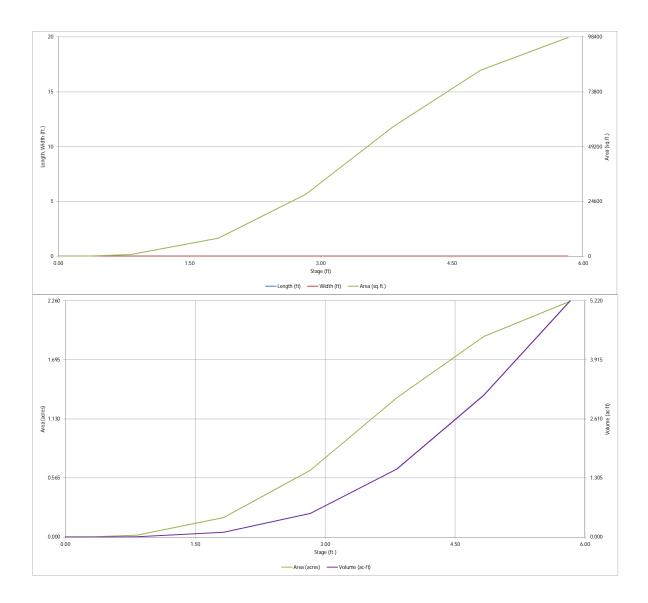
Define Zones and Basin Geometry

		Define Zuries and Dasin Geometry
acre-fe	0.619	Zone 1 Volume (WQCV) =
acre-fe	0.388	Zone 2 Volume (EURV - Zone 1) =
acre-fe	1.800	Zone 3 Volume (100-year - Zones 1 & 2) =
acre-fe	2.808	Total Detention Basin Volume =
ft 3	user	Initial Surcharge Volume (ISV) =
ft	user	Initial Surcharge Depth (ISD) =
ft	user	Total Available Detention Depth (H _{total}) =
ft	user	Depth of Trickle Channel (H _{TC}) =
ft/ft	user	Slope of Trickle Channel (S _{TC}) =
H:V	user	Slopes of Main Basin Sides (Smain) =
1	user	Basin Length-to-Width Ratio (R _{L/W}) =

Initial Surcharge Area (A _{ISV}) =	user	ft ²
Surcharge Volume Length (L _{ISV}) =	user	ft
Surcharge Volume Width (W _{ISV}) =	user	ft
Depth of Basin Floor (H _{FLOOR}) =	user	ft
Length of Basin Floor (LFLOOR) =	user	ft
Width of Basin Floor (W _{FLOOR}) =	user	ft
Area of Basin Floor (A _{FLOOR}) =	user	ft ²
Volume of Basin Floor (V _{FLOOR}) =	user	ft ³
Depth of Main Basin (H _{MAIN}) =	user	ft
Length of Main Basin (L _{MAIN}) =	user	ft
Width of Main Basin (W _{MAIN}) =	user	ft
Area of Main Basin (A _{MAIN}) =	user	ft ²
Volume of Main Basin (V _{MAIN}) =	user	ft ³
Calculated Total Basin Volume (Vtotal) =	user	acre-feet

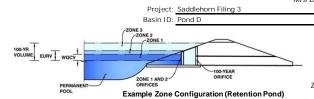
			1.							
ſ	Depth Increment =		ft Optional				Optional			
	Stage - Storage Description	Stage (ft)	Override Stage (ft)	Length (ft)	Width (ft)	Area (ft 2)	Override Area (ft ²)	Area (acre)	Volume (ft 3)	Volume (ac-ft)
.17	Top of Micropool		0.00				32	0.001		
ļ	6709.5		0.33				50	0.001	14	0.000
ļ	6710 6711		0.83				699 8,089	0.016 0.186	201 4,595	0.005
ŀ	6712		2.83				27,770	0.638	22,524	0.103
Ī	6713		3.83				58,037	1.332	65,427	1.502
	6714		4.83				83,546	1.918	136,219	3.127
ļ	6715		5.83				98,172	2.254	227,078	5.213
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M#FD-Detention_w4 04_Pond D.xlsm, Basin 12/14/2021, 3:08 PM



M#FD-Detention_w4 04_Pond D.xlsm, Basin 12/14/2021, 3:08 PM

MHFD-Detention, Version 4.04 (February 2021)



	Estimated	Estimated	
	Stage (ft)	Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	2.98	0.619	Orifice Plate
Zone 2 (EURV)	3.42	0.388	Circular Orifice
Zone 3 (100-year)	4.66	1.800	Weir&Pipe (Restrict)
	Total (all zones)	2.808	

<u>User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)</u>

Underdrain Orifice Invert Depth = N/A ft (distance below the filtration media surface)
Underdrain Orifice Diameter = N/A inches

	Calculated Parameters for Underdrain			
Underdrain Orifice Area =	N/A	ft ²		
Underdrain Orifice Centroid =	N/A	feet		

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice = 0.00 ft (relative to basin bottom at Stage = 0 ft)

Depth at top of Zone using Orifice Plate = 3.42 ft (relative to basin bottom at Stage = 0 ft)

Orifice Plate: Orifice Vertical Spacing = 13.70 inches

Orifice Plate: Orifice Area per Row = 2.05 sq. inches (diameter = 1-5/8 inches)

Calculated Parameters for Plate				
VQ Orifice Area per Row =	1.424E-02	ft ²		
Elliptical Half-Width =	N/A	feet		
Elliptical Slot Centroid =	N/A	feet		
Elliptical Slot Area =	N/A	ft ²		

<u>User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)</u>

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	1.14	2.28					
Orifice Area (sq. inches)	2.05	2.05	2.05					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

	Zone 2 Circular	Not Selected	
Invert of Vertical Orifice =	2.98	N/A	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Vertical Orifice =	3.42	N/A	ft (relative to basin bottom at Stage = 0 ft)
Vertical Orifice Diameter =	0.38	N/A	inches

	Calculated Paramet	ers for Vertical Orific	e
	Zone 2 Circular	Not Selected	
Vertical Orifice Area =	0.00	N/A	ft ²
ertical Orifice Centroid =	0.02	N/A	feet
			•

Calculated Darameters for Outlet Dine w/ Flow Destriction Diete

User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe)

	Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	3.42	N/A	ft (relative to basin bottom at Stage = 0
Overflow Weir Front Edge Length =	10.00	N/A	feet
Overflow Weir Grate Slope =	0.00	N/A	H:V
Horiz. Length of Weir Sides =	5.00	N/A	feet
Overflow Grate Type =	Type C Grate	N/A	
Debris Clogging % =	0%	N/A	%

<u>et Pip</u>	<u>e)</u>	Calculated Paramet	ers for Overflow We	<u>ir</u>
		Zone 3 Weir	Not Selected	
= 0 ft)	Height of Grate Upper Edge, $H_t =$	3.42	N/A	feet
	Overflow Weir Slope Length =	5.00	N/A	feet
(Grate Open Area / 100-yr Orifice Area =	4.92	N/A	
	Overflow Grate Open Area w/o Debris =	34.80	N/A	ft ²
	Overflow Grate Open Area w/ Debris =	34.80	N/A	ft ²
		<u> </u>		

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

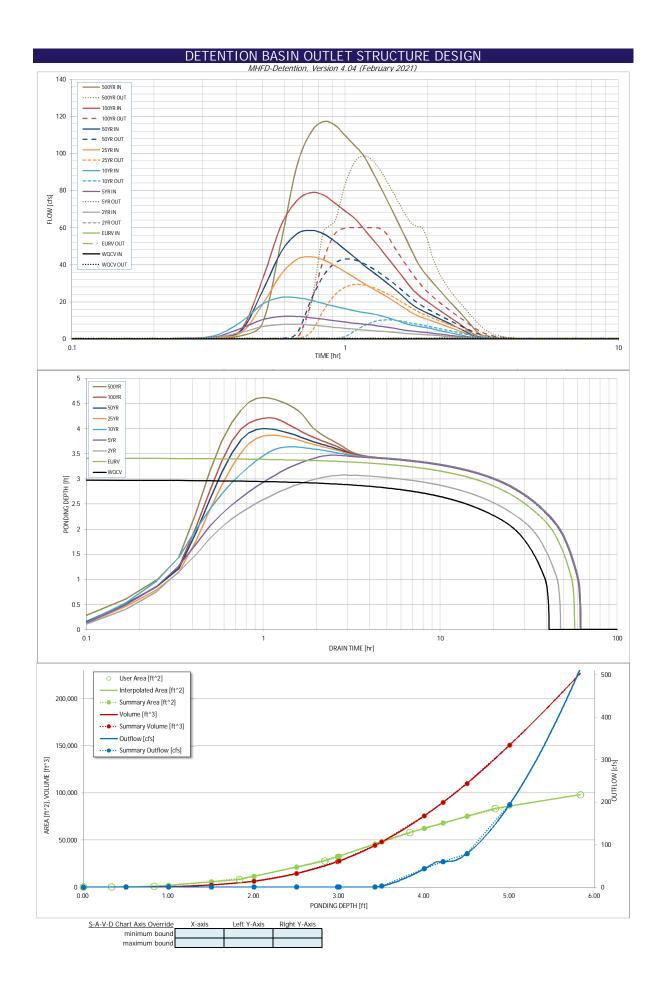
input. Outlet ripe w/ riow kestriction riate (c	iliculai Office, Resti	ictui Fiate, ui Rectai	rigular Office)	Calculated Faranneter	S for Outlet Fipe W/ I	TOW RESUICTION FIA	le
	Zone 3 Restrictor	Not Selected			Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	0.40	N/A	ft (distance below basin bottom at Stage = 0 ft)	Outlet Orifice Area =	7.07	N/A	ft ²
Outlet Pipe Diameter =	36.00	N/A	inches	Outlet Orifice Centroid =	1.50	N/A	feet
Restrictor Plate Height Above Pipe Invert =	36.00		inches Half-Central An	igle of Restrictor Plate on Pipe =	3.14	N/A	radian

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Emergency Spiliway (Rectangular or Tr	apezoidaij	
Spillway Invert Stage=	4.33	ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length =	75.00	feet
Spillway End Slopes =	4.00	H:V
Freeboard above Max Water Surface =	1.00	feet

	Calculated Paramet	ers for Spillway
Spillway Design Flow Depth=	0.49	feet
Stage at Top of Freeboard =	5.82	feet
Basin Area at Top of Freeboard =	2.25	acres
Basin Volume at Top of Freeboard =	5.19	acre-ft

Routed Hydrograph Results	The user can overr	ide the default CUHP	hydrographs and ru	noff volumes by ent	ering new values in	the Inflow Hydrogra	phs table (Columns V	V through AF).	
Design Storm Return Period =	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
One-Hour Rainfall Depth (in) =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52	3.14
CUHP Runoff Volume (acre-ft) =	0.619	1.007	0.755	1.188	2.116	3.929	5.225	7.358	11.183
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	0.755	1.188	2.116	3.929	5.225	7.358	11.183
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A	0.9	2.0	11.4	32.5	46.1	66.0	103.2
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A							
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.01	0.03	0.15	0.42	0.59	0.85	1.32
Peak Inflow Q (cfs) =	N/A	N/A	7.9	12.1	22.4	44.2	58.5	78.8	117.2
Peak Outflow Q (cfs) =	0.3	0.3	0.3	1.4	10.3	29.3	43.1	60.1	98.7
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	0.7	0.9	0.9	0.9	0.9	1.0
Structure Controlling Flow =	Plate	Overflow Weir 1	Vertical Orifice 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Outlet Plate 1	Spillway
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	0.0	0.3	0.8	1.2	1.7	1.8
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	38	53	44	56	54	49	47	42	35
Time to Drain 99% of Inflow Volume (hours) =	40	56	46	60	58	56	55	53	50
Maximum Ponding Depth (ft) =	2.98	3.42	3.07	3.47	3.64	3.87	4.00	4.22	4.62
Area at Maximum Ponding Depth (acres) =	0.74	1.05	0.80	1.08	1.20	1.35	1.43	1.55	1.79
Maximum Volume Stored (acre-ft) =	0.621	1.014	0.690	1.067	1.261	1.542	1.737	2.051	2.719



Outflow Hydrograph Workbook Filename:

Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

ĺ	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
	0:00:00									
5.00 min	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.02	0.00	0.07
	0:20:00	0.00	0.00	0.78	1.07	1.80	0.23	0.96	1.01	1.78
	0:25:00	0.00	0.00	3.62	5.77	9.24	3.35	4.42	5.02	8.89
	0:30:00	0.00	0.00	6.66	10.45	18.82	18.82	26.04	32.56	52.15
	0:35:00	0.00	0.00	7.84	12.08	22.42	34.80	46.75	61.06	93.07
	0:40:00	0.00	0.00	7.93	12.12	22.20	42.88	56.63	74.53	111.26
	0:45:00	0.00	0.00	7.48	11.45	20.90	44.25	58.54	78.84	117.15
	0:50:00	0.00	0.00	6.83	10.62	19.13	42.61	56.69	77.56	115.33
	0:55:00 1:00:00	0.00	0.00	6.26	9.86	17.62	39.50	52.70 48.27	73.29	109.78
	1:05:00	0.00	0.00	5.76 5.28	9.14 8.47	16.34 15.15	36.17 33.11	44.11	68.97 65.06	104.24 99.07
	1:10:00	0.00	0.00	4.89	7.99	14.25	30.04	39.97	59.68	91.26
	1:15:00	0.00	0.00	4.55	7.50	13.58	27.49	36.59	54.41	83.33
	1:20:00	0.00	0.00	4.22	6.95	12.74	25.14	33.49	49.45	75.69
	1:25:00	0.00	0.00	3.89	6.38	11.68	22.87	30.48	44.61	68.20
	1:30:00	0.00	0.00	3.56	5.81	10.53	20.61	27.48	40.05	61.16
	1:35:00	0.00	0.00	3.24	5.25	9.39	18.42	24.52	35.69	54.45
	1:40:00 1:45:00	0.00	0.00	2.93	4.70	8.31	16.26	21.61	31.44	47.94
	1:50:00	0.00	0.00	2.69	4.26 3.96	7.48 6.91	14.20 12.64	18.83 16.78	27.41 24.37	41.84 37.36
	1:55:00	0.00	0.00	2.39	3.70	6.44	11.50	15.25	22.06	33.85
	2:00:00	0.00	0.00	2.23	3.45	5.96	10.59	13.99	20.09	30.81
	2:05:00	0.00	0.00	2.04	3.15	5.44	9.68	12.77	18.25	27.94
	2:10:00	0.00	0.00	1.84	2.84	4.90	8.78	11.58	16.49	25.21
	2:15:00	0.00	0.00	1.65	2.54	4.37	7.91	10.44	14.82	22.61
	2:20:00	0.00	0.00	1.46	2.24	3.86	7.07	9.32	13.24	20.17
	2:25:00	0.00	0.00	1.28	1.96	3.37	6.25	8.23	11.74	17.88
	2:30:00	0.00	0.00	1.11 0.94	1.70	2.90 2.45	5.45 4.66	7.17 6.12	10.28 8.83	15.64 13.43
	2:40:00	0.00	0.00	0.74	1.19	2.43	3.88	5.09	7.40	11.24
	2:45:00	0.00	0.00	0.62	0.95	1.60	3.12	4.07	5.97	9.05
	2:50:00	0.00	0.00	0.47	0.72	1.19	2.36	3.06	4.55	6.89
	2:55:00	0.00	0.00	0.33	0.50	0.82	1.62	2.08	3.16	4.80
	3:00:00	0.00	0.00	0.25	0.39	0.60	0.98	1.26	2.00	3.10
	3:05:00	0.00	0.00	0.20	0.32	0.50	0.63	0.81	1.31	2.10
	3:10:00 3:15:00	0.00	0.00	0.17 0.15	0.26	0.41	0.43	0.56 0.41	0.89	1.46
	3:20:00	0.00	0.00	0.13	0.22	0.34	0.32	0.41	0.41	0.67
	3:25:00	0.00	0.00	0.11	0.15	0.22	0.19	0.23	0.28	0.44
	3:30:00	0.00	0.00	0.09	0.12	0.17	0.15	0.18	0.18	0.28
	3:35:00	0.00	0.00	0.07	0.09	0.13	0.11	0.14	0.12	0.19
	3:40:00	0.00	0.00	0.06	0.07	0.10	0.09	0.10	0.09	0.14
	3:45:00	0.00	0.00	0.05	0.06	0.08	0.07	0.08	0.07	0.11
	3:50:00	0.00	0.00	0.04	0.05	0.06	0.05	0.06	0.06	0.09
	3:55:00 4:00:00	0.00	0.00	0.03	0.03	0.04	0.04	0.05	0.04	0.07
	4:05:00	0.00	0.00	0.02	0.03	0.03	0.03	0.03	0.03	0.03
	4:10:00	0.00	0.00	0.01	0.01	0.01	0.01	0.02	0.01	0.02
	4:15:00 4:20:00	0.00	0.00	0.00	0.01	0.01	0.01	0.01	0.01	0.01
	4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:35:00 4:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:55:00 5:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:15:00 5:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:35:00 5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

MHFD-Detention, Version 4.04 (February 2021)

Summary Stage-Area-Volume-Discharge Relationships

The user can create a summary S-A-V-D by entering the desired stage increments and the remainder of the table will populate automatically. The user should graphically compare the summary S-A-V-D table to the full S-A-V-D table in the chart to confirm it captures all key transition points.

0.00 32 0.001 0 0.000 0.00 For be stages 1.00 1.00 1.955 0.045 426 0.010 0.07 from the stages 1.50 5.650 0.130 2.328 0.053 0.13 Sheet 2.00 11.435 0.263 6.254 0.144 0.16 2.50 21.275 0.488 14.432 0.331 0.22 Also in WQCV 2.98 32.310 0.742 27.030 0.621 0.27 outlets 2.00 32.915 0.756 27.682 0.635 0.27 overfice 2.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	Stage - Storage	Stage	Area	Area	Volume	Volume	Total Outflow	
0.50 271 0.006 41 0.001 0.05 stages stages 1.00 1.955 0.045 426 0.010 0.07 chang from t 1.50 5.650 0.130 2.328 0.053 0.13 Sheet 2.00 11,435 0.263 6.254 0.144 0.16 2.50 21,275 0.488 14,432 0.331 0.22 Also if where 3.00 32,915 0.756 27,682 0.635 0.27 overflag where 3.350 48,049 1.103 47,923 1.100 2.50 4.00 62,374 1.432 75,662 1.737 43.04 100-YR 4.22 67,986 1.561 90,002 2.066 60.12 4.50 75,128 1.725 110,038 2.526 78.64	Description	[ft]	[ft ²]	[acres]	[ft 3]	[ac-ft]		
0.50 271 0.006 41 0.001 0.05 stages 1.00 1,955 0.045 426 0.010 0.07 chang from the chang from the chang from the chang from the chang from the change f		0.00	32	0.001	0	0.000	0.00	For bes
1.00 1,955 0.045 426 0.010 0.07 chang from t from t sheet 1.50 5,650 0.130 2,328 0.053 0.13 Sheet 2.00 11,435 0.263 6,254 0.144 0.16 Sheet 2.50 21,275 0.488 14,432 0.331 0.22 Also ir WQCV 2.98 32,310 0.742 27,030 0.621 0.27 outlet 3.00 32,915 0.756 27,682 0.635 0.27 overfix EURV 3.42 45,628 1.047 44,176 1.014 0.31 where 4.00 62,374 1.432 75,662 1.737 43.04 100-YR 4.22 67,986 1.561 90,002 2.066 60.12 4.50 75,128 1.725 110,038 2.526 78.64			271	0.006	41	0.001	0.05	stages
1.50 5,680 0.130 2,328 0.053 0.13 Sheet 2.00 11,435 0.263 6,254 0.144 0.16 2.50 21,275 0.488 14,432 0.331 0.22 Also ir WQCV 2,98 32,310 0.742 27,030 0.621 0.27 outlet 3.00 32,915 0.756 27,682 0.635 0.27 overflow EURV 3.42 45,628 1.047 44,176 1.014 0.31 where 3.50 48,049 1.103 47,923 1.100 2.50 4.00 62,374 1.432 75,662 1.737 43.04 100-YR 4.22 67,986 1.561 90,002 2.066 60.12 4.50 75,128 1.725 110,038 2.526 78.64			1,955	0.045	426	0.010	0.07	change
2.00 11,435 0.263 6.254 0.144 0.16 2.50 21,275 0.488 14,432 0.331 0.22 Also ir WQCV 2.98 32,310 0.742 27,030 0.621 0.27 outlet: 3.00 32,915 0.756 27,682 0.635 0.27 overfic EURV 3.42 45,628 1.047 44,176 1.014 0.31 3.50 48,049 1.103 44,923 1.100 2.50 4.00 62,374 1.432 75,662 1.737 43.04 100-YR 4.22 67,986 1.561 90,002 2.066 60.12 4.50 75,128 1.725 110,038 2.526 78.64			5,650	0.130	2,328	0.053	0.13	Sheet 'I
WQCV 2.98 32,310 0.742 27,030 0.621 0.27 outlets overflow o		2.00						_
3.00 32,915 0.756 27,682 0.635 0.27 overflow there EURV 3.42 45,628 1.047 44,176 1.014 0.31 3.50 48,049 1.103 47,923 1.100 2.50 4.00 62,374 1.432 75,662 1.737 43.04 100-YR 4.22 67,986 1.561 90,002 2.066 60.12 4.50 75,128 1.725 110,038 2.526 78.64								Also inc
EURV 3.42 45,628 1.047 44,176 1.1014 0.31 Where 3.50 48,049 1.103 47,923 1.100 2.50 4.00 62,374 1.432 75,662 1.737 43.04 100-YR 4.22 67,986 1.561 90,002 2.066 60.12 4.50 75,128 1.725 110,038 2.526 78.64	WQCV							
3.50 48,049 1.103 47,923 1.100 2.50 4.00 62,374 1.432 75,662 1.737 43.04 100-YR 4.22 67,986 1.561 90,002 2.066 60.12 4.50 75,128 1.725 110,038 2.526 78.64	FUDV							where a
4.00 62,374 1.432 75,662 1.737 43.04 100-YR 4.22 67,986 1.561 90,002 2.066 60.12 4.50 75,128 1.725 110,038 2.526 78.64	EURV							
100-YR 4.22 67,986 1.561 90,002 2.066 60.12 4.50 75,128 1.725 110,038 2.526 78.64								
4.50 75,128 1.725 110,038 2.526 78.64	100-YR							
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For best results, include the stages of all grade slope changes (e.g. ISV and Floor) from the S-A-V table on Sheet 'Basin'.

Also include the inverts of all outlets (e.g. vertical orifice, overflow grate, and spillway, where applicable).

POND D FOREBAY VOLUME REQUIREMENTS

WQCV= $a(0.91I^3-1.19I^2+0.781I)$ a=1 (40 hour drain time) Equation 3-1

Proposed Forebay WQCV= 0.080158 I = .124Future Forebay I=.147 WQCV= 0.091836

> Equation 3-3 V=(WQCV/12)A

Proposed Forebay A= 40.72 Acres V= 0.272 Future Forebay A= 33.94 Acres V= 0.260

3% OF WQCV

FOREBAY TOTAL VOLUME= .03(V)

VOLUME REQUIRED FOR PROPOSED FOREBAY= 0.008 AC-FT 355 CF **VOLUME REQUIRED FOR FUTURE FOREBAY =** 339 CF 0.008 AC-FT

VOLUME PROVIDED FOR PROPOSED FOREBAY = 0.015 AC-FT 642 CF

Q₁₀₀ Discharges 2% OF Q₁₀₀

Q₁₀₀ Proposed Forebay 1= .02*51.7 CFS= 1.03 CFS Q₁₀₀ Future Forebay= .02*37.3 CFS= 0.75 CFS

Weir Report

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Wednesday, Mar 2 2022

Pond D Forebay 1 Notch

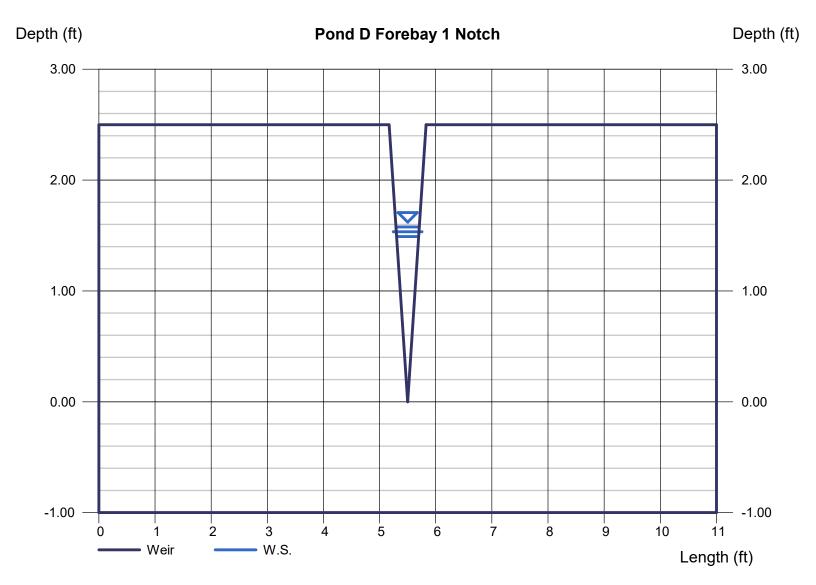
V-Notch Weir	
Crest	= Sharp
Angle (Deg)	= 15
Total Depth (ft)	= 2.50

Calculations

Weir Coeff. Cw = 0.33 Compute by: Known Q Known Q (cfs) = 1.03

Highlighted

Depth (ft) = 1.58 Q (cfs) = 1.030 Area (sqft) = 0.33 Velocity (ft/s) = 3.15 Top Width (ft) = 0.42



Channel Report

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Monday, Dec 13 2021

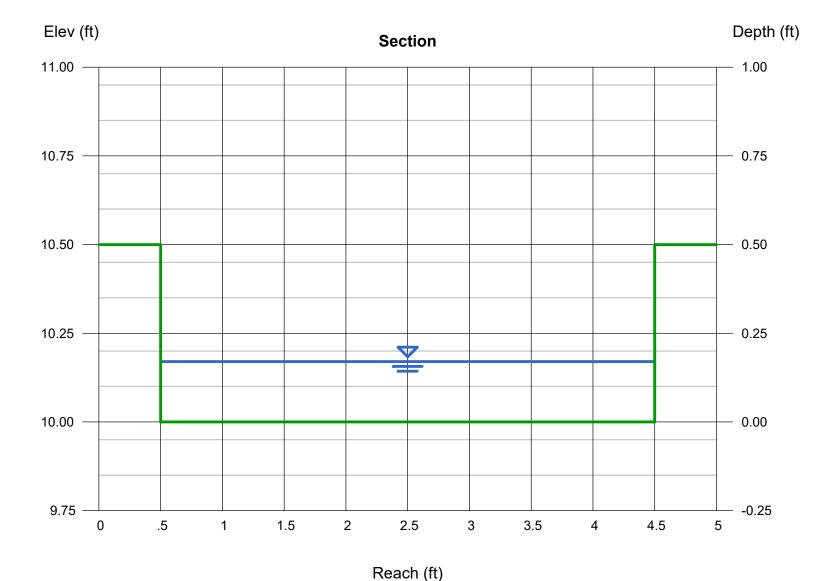
Pond D Trickle Channel

Rectangular Bottom Width (ft) Total Depth (ft)	= 4.00 = 0.50
Invert Elev (ft)	= 10.00
Slope (%)	= 0.50
N-Value	= 0.013

Compute by: Known Q Known Q (cfs) = 1.52

Calculations





Weir Report

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Tuesday, Dec 14 2021

Pond D Spillway

Tra	pez	oidal	l Weir

Crest = Sharp Bottom Length (ft) = 75.00 Total Depth (ft) = 1.50 Side Slope (z:1) = 4.00

Calculations

Weir Coeff. Cw = 3.10 Compute by: Known Q Known Q (cfs) = 78.80

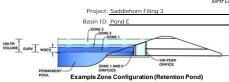
Highlighted

Depth (ft) = 0.48 Q (cfs) = 78.80 Area (sqft) = 36.92 Velocity (ft/s) = 2.13 Top Width (ft) = 78.84



DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.04 (February 2021)



Example 2011e Configuration (

Watershed Information

sica miornation		
Selected BMP Type =	EDB	
Watershed Area =	18.37	acres
Watershed Length =	1,810	ft
Watershed Length to Centroid =	803	ft
Watershed Slope =	0.012	ft/ft
Watershed Imperviousness =	8.10%	percent
Percentage Hydrologic Soil Group A =	83.0%	percent
Percentage Hydrologic Soil Group B =	0.0%	percent
rcentage Hydrologic Soil Groups C/D =	17.0%	percent
Target WQCV Drain Time =	40.0	hours
Location for 1-hr Rainfall Depths =	User Input	

After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using

the embedded Colorado Urban Hydro	graph Procedu	ure.
Water Quality Capture Volume (WQCV) =	0.086	acre-feet
Excess Urban Runoff Volume (EURV) =	0.106	acre-feet
2-yr Runoff Volume (P1 = 1.19 in.) =	0.065	acre-feet
5-yr Runoff Volume (P1 = 1.5 in.) =	0.106	acre-feet
10-yr Runoff Volume (P1 = 1.75 in.) =	0.204	acre-feet
25-yr Runoff Volume (P1 = 2 in.) =	0.592	acre-feet
50-yr Runoff Volume (P1 = 2.25 in.) =	0.859	acre-feet
100-yr Runoff Volume (P1 = 2.52 in.) =	1.292	acre-feet
500-yr Runoff Volume (P1 = 3.14 in.) =	2.174	acre-feet
Approximate 2-yr Detention Volume =	0.067	acre-feet
Approximate 5-yr Detention Volume =	0.113	acre-feet
Approximate 10-yr Detention Volume =	0.153	acre-feet
Approximate 25-yr Detention Volume =	0.199	acre-feet
Approximate 50-yr Detention Volume =	0.254	acre-feet
Approximate 100-yr Detention Volume =	0.419	acre-feet

	Optional User Overrides						
t		acre-feet					
t		acre-feet					
t	1.19	inches					
t	1.50	inches					
t	1.75	inches					
t	2.00	inches					
t	2.25	inches					
t	2.52	inches					
t		inches					

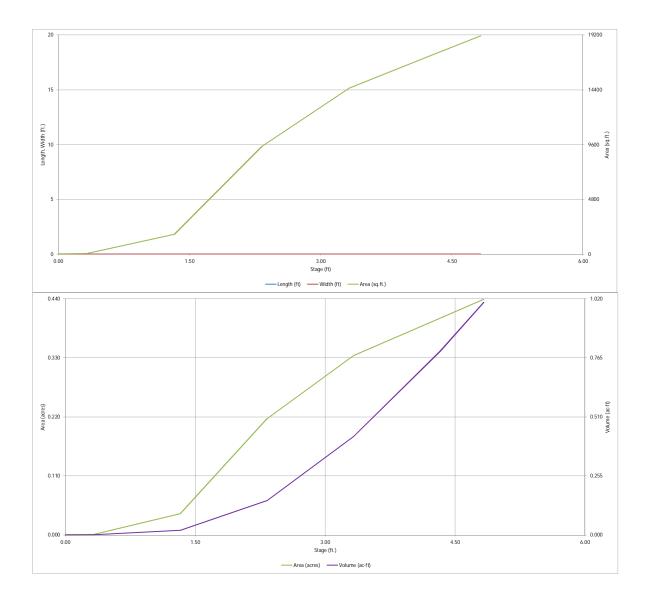
Define Zones and Basin Geometry

Jerine Zones and Basin Geometry		
Zone 1 Volume (WQCV) =	0.086	acre-feet
Zone 2 Volume (EURV - Zone 1) =	0.021	acre-feet
Zone 3 Volume (100-year - Zones 1 & 2) =	0.313	acre-feet
Total Detention Basin Volume =	0.419	acre-feet
Initial Surcharge Volume (ISV) =	user	ft ³
Initial Surcharge Depth (ISD) =	user	ft
Total Available Detention Depth (H _{total}) =	user	ft
Depth of Trickle Channel (H _{TC}) =	user	ft
Slope of Trickle Channel (S _{TC}) =	user	ft/ft
Slopes of Main Basin Sides (Smain) =	user	H:V
Basin Length-to-Width Ratio (R _{L/W}) =	user	

Initial Surcharge Area (A _{ISV}) =	user	ft ²
Surcharge Volume Length (L _{ISV}) =	user	ft
Surcharge Volume Width (W _{ISV}) =	user	ft
Depth of Basin Floor (H _{FLOOR}) =	user	ft
Length of Basin Floor (LFLOOR) =	user	ft
Width of Basin Floor (W _{FLOOR}) =	user	ft
Area of Basin Floor (A _{FLOOR}) =	user	ft ²
Volume of Basin Floor (V _{FLOOR}) =	user	ft ³
Depth of Main Basin (H _{MAIN}) =	user	ft
Length of Main Basin (L _{MAIN}) =	user	ft
Width of Main Basin (W _{MAIN}) =	user	ft
Area of Main Basin (A _{MAIN}) =	user	ft ²
Volume of Main Basin (V _{MAIN}) =	user	ft ³
Calculated Total Basin Volume (Vtotal) =	user	acre-feet

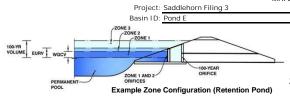
	D									
Γ	Depth Increment =		ft Optional				Optional			
	Stage - Storage Description	Stage (ft)	Override Stage (ft)	Length (ft)	Width (ft)	Area (ft ²)	Override Area (ft ²)	Area (acre)	Volume (ft 3)	Volume (ac-ft)
).67	Top of Micropool		0.00				32	0.001		
	6721		0.33				50	0.001	14	0.000
L	6722 6723		1.33				1,723 9,446	0.040	900 6,484	0.021
-	6724		3.33				14,566	0.334	18,490	0.424
Ī	6725		4.33				17,600	0.404	34,573	0.794
	6725.5		4.83				19,121	0.439	43,754	1.004
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M#FD-Detention_w4 04_Pond Extern, Basin 12/13/2021, 10:16 AM



M#FD-Detention_w4 04_Pond Extern, Basin 12/13/2021, 10:16 AM

MHFD-Detention, Version 4.04 (February 2021)



	Estimated Stage (ft)	Estimated Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	2.00	0.086	Orifice Plate
Zone 2 (EURV)	2.12	0.021	Orifice Plate
Zone 3 (100-year)	3.32	0.313	Weir&Pipe (Restrict)
•	Total (all zones)	0.419	

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth = N/A ft (distance below the filtration media surface)
Underdrain Orifice Diameter = N/A inches

	Calculated Parameters for Underdrain			
Underdrain Orifice Area =	N/A	ft ²		
Underdrain Orifice Centroid =	N/A	feet		

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP) Calculated Parameters for Plate ft (relative to basin bottom at Stage = 0 ft) WQ Orifice Area per Row 2 153F-03 ft² Invert of Lowest Orifice = 0.00 Depth at top of Zone using Orifice Plate = 2 12 ft (relative to basin bottom at Stage = 0 ft) Elliptical Half-Width N/A feet Orifice Plate: Orifice Vertical Spacing : N/A inches Elliptical Slot Centroid = N/A feet Orifice Plate: Orifice Area per Row = 0.31 sq. inches (diameter = 5/8 inch) Elliptical Slot Area N/A

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	0.60	1.20					
Orifice Area (sq. inches)	0.31	0.31	0.31					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular) Calculated Parameters for Vertical Orifice Not Selected Not Selected Not Selected Not Selected Invert of Vertical Orifice N/A N/A t (relative to basin bottom at Stage = 0 ft) Vertical Orifice Area N/A N/A Depth at top of Zone using Vertical Orifice : N/A N/A ft (relative to basin bottom at Stage = 0 ft) Vertical Orifice Centroid = N/A Vertical Orifice Diameter =

User Input: Overflow Weir (Dropbox with Flat or	Calculated Parameters for Overflow Weir					
	Zone 3 Weir	Not Selected		Zone 3 Weir	Not Selected	li .
Overflow Weir Front Edge Height, Ho =	2.30	N/A	ft (relative to basin bottom at Stage = 0 ft) Height of Grate Upper Edge, H_t =	3.55	N/A	feet
Overflow Weir Front Edge Length =	5.00	N/A	feet Overflow Weir Slope Length =	5.15	N/A	feet
Overflow Weir Grate Slope =	4.00	N/A	H:V Grate Open Area / 100-yr Orifice Area =	10.15	N/A	ı
Horiz. Length of Weir Sides =	5.00	N/A	feet Overflow Grate Open Area w/o Debris =	17.94	N/A	ft ²
Overflow Grate Type =	Type C Grate	N/A	Overflow Grate Open Area w/ Debris =	17.94	N/A	ft ²
Debris Clogging % =	0%	N/A	%			

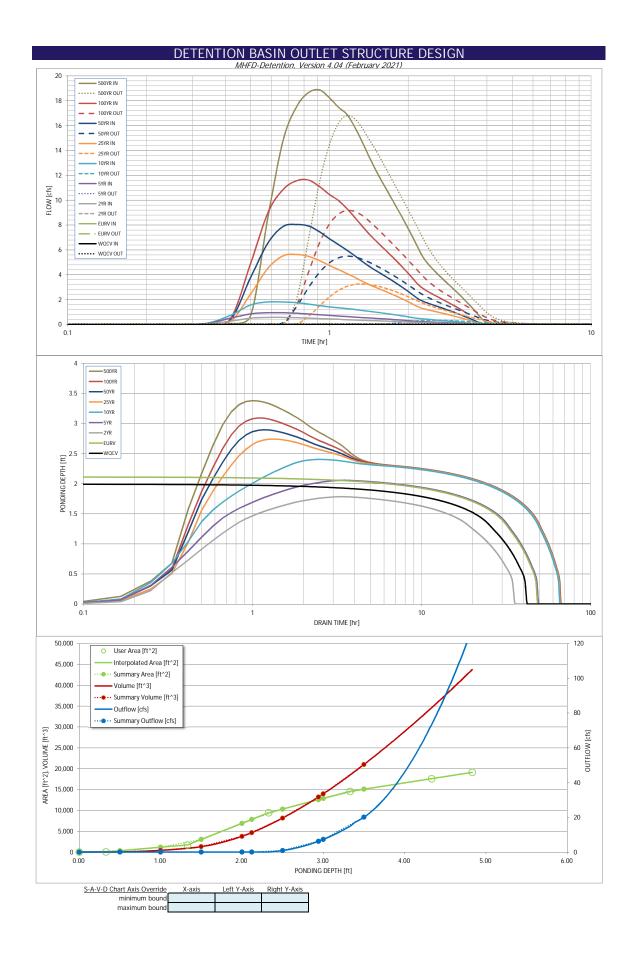
User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate

	Zone 3 Restrictor	Not Selected			Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	1.15	N/A	ft (distance below basin bottom at Stage = 0 ft)	Outlet Orifice Area =	1.77	N/A	ft ²
Outlet Pipe Diameter =	18.00	N/A	inches	Outlet Orifice Centroid =	0.75	N/A	feet
Restrictor Plate Height Above Pipe Invert =	18.00		inches Half-Central Angle	of Restrictor Plate on Pipe =	3.14	N/A	radians

User Input: Emergency Spillway (Rectangular or Trapezoidal) Calculated Parameters for Spillway Spillway Design Flow Depth= Spillway Invert Stage= 3.33 ft (relative to basin bottom at Stage = 0 ft) 0.38 feet Spillway Crest Length = 15.00 Stage at Top of Freeboard = 4.71 feet Spillway End Slopes 4.00 H:V Basin Area at Top of Freeboard = 0.43 acres Freeboard above Max Water Surface = 1.00 Basin Volume at Top of Freeboard = acre-ft

Routed Hydrograph Results	The user can over	ride the default CU	HP hydrographs and	d runoff volumes b	y entering new value	es in the Inflow Hyd	drographs table (Col	lumns W through Ai	-).
Design Storm Return Period =	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
One-Hour Rainfall Depth (in) =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52	3.14
CUHP Runoff Volume (acre-ft) =	0.086	0.106	0.065	0.106	0.204	0.592	0.859	1.292	2.174
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	0.065	0.106	0.204	0.592	0.859	1.292	2.174
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A	0.1	0.2	0.9	4.6	7.0	10.5	17.7
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A							
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.01	0.01	0.05	0.25	0.38	0.57	0.96
Peak Inflow Q (cfs) =	N/A	N/A	0.6	1.0	1.8	5.6	8.0	11.6	18.9
Peak Outflow Q (cfs) =	0.0	0.0	0.0	0.0	0.3	3.3	5.5	9.2	16.8
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	0.2	0.4	0.7	0.8	0.9	0.9
Structure Controlling Flow =	Plate	Plate	Plate	Plate	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Spillway
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	N/A	0.0	0.2	0.3	0.5	0.9
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	38	44	32	44	58	51	47	42	32
Time to Drain 99% of Inflow Volume (hours) =	40	46	34	47	62	59	57	54	49
Maximum Ponding Depth (ft) =	2.00	2.12	1.78	2.06	2.40	2.74	2.90	3.09	3.38
Area at Maximum Ponding Depth (acres) =	0.16	0.18	0.12	0.17	0.23	0.27	0.28	0.31	0.34
Maximum Volume Stored (acre-ft) =	0.087	0.107	0.056	0.095	0.164	0.248	0.289	0.348	0.438



DETENTION BASIN OUTLET STRUCTURE DESIGN Outflow Hydrograph Workbook Filename:

Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]		500 Year [cfs]
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:15:00	0.00	0.00	0.01	0.02	0.02	0.02	0.02	0.02	0.03
	0:20:00	0.00	0.00	0.04	0.06	0.07	0.04	0.05	0.06	0.07
	0:25:00	0.00	0.00	0.27	0.50	0.72	0.23	0.34	0.41	0.72
	0:30:00	0.00	0.00	0.51 0.57	0.86	1.57 1.81	2.46 4.55	3.79 6.58	4.91 9.03	8.73 14.87
	0:40:00	0.00	0.00	0.57	0.95	1.81	5.53	7.89	10.87	17.53
	0:45:00	0.00	0.00	0.55	0.91	1.75	5.64	8.05	11.57	18.66
	0:50:00	0.00	0.00	0.52	0.85	1.64	5.48	7.92	11.61	18.87
	0:55:00	0.00	0.00	0.48	0.78	1.52	5.14	7.46	11.09	18.24
	1:00:00	0.00	0.00	0.45	0.73	1.42	4.75	6.90	10.46	17.47
	1:10:00	0.00	0.00	0.42	0.69	1.35 1.28	4.42 4.11	6.43 5.98	9.97 9.32	16.90 15.88
	1:15:00	0.00	0.00	0.37	0.60	1.21	3.80	5.54	8.62	14.71
	1:20:00	0.00	0.00	0.34	0.56	1.14	3.49	5.08	7.92	13.52
	1:25:00	0.00	0.00	0.32	0.53	1.06	3.22	4.69	7.30	12.46
	1:30:00	0.00	0.00	0.31	0.50	1.00	2.99	4.36	6.76	11.55
	1:35:00	0.00	0.00	0.29	0.47	0.93	2.79	4.06 3.77	6.28 5.83	9.94
	1:45:00	0.00	0.00	0.26	0.44	0.87	2.41	3.49	5.83	9.94
	1:50:00	0.00	0.00	0.24	0.38	0.74	2.22	3.22	4.97	8.45
	1:55:00	0.00	0.00	0.22	0.35	0.68	2.03	2.94	4.54	7.72
	2:00:00	0.00	0.00	0.20	0.31	0.62	1.84	2.66	4.12	7.01
	2:05:00 2:10:00	0.00	0.00	0.18	0.28	0.55	1.65	2.38	3.70	6.31
	2:15:00	0.00	0.00	0.16 0.15	0.26	0.50	1.46	2.11 1.92	3.29 2.99	5.61 5.12
	2:20:00	0.00	0.00	0.14	0.22	0.44	1.23	1.78	2.77	4.73
	2:25:00	0.00	0.00	0.13	0.21	0.41	1.15	1.67	2.57	4.40
	2:30:00	0.00	0.00	0.12	0.20	0.38	1.08	1.56	2.40	4.09
	2:35:00	0.00	0.00	0.12	0.18	0.35	1.01	1.46	2.24	3.81
	2:40:00 2:45:00	0.00	0.00	0.11	0.17	0.33	0.94	1.36 1.27	2.09 1.94	3.54
	2:50:00	0.00	0.00	0.09	0.14	0.28	0.81	1.17	1.80	3.04
	2:55:00	0.00	0.00	0.08	0.13	0.25	0.74	1.07	1.65	2.80
	3:00:00	0.00	0.00	0.08	0.12	0.23	0.68	0.98	1.51	2.57
	3:05:00 3:10:00	0.00	0.00	0.07	0.11	0.21	0.61	0.89	1.37	2.33
	3:10:00	0.00	0.00	0.06	0.09	0.18	0.55 0.48	0.79	1.23	2.09 1.85
	3:20:00	0.00	0.00	0.03	0.07	0.14	0.42	0.60	0.95	1.62
	3:25:00	0.00	0.00	0.04	0.06	0.11	0.35	0.51	0.81	1.38
	3:30:00	0.00	0.00	0.03	0.05	0.09	0.29	0.42	0.67	1.14
	3:35:00	0.00	0.00	0.02	0.03	0.07	0.22	0.32	0.53	0.91
	3:40:00 3:45:00	0.00	0.00	0.02	0.02	0.05	0.16 0.10	0.23	0.39	0.67
	3:50:00	0.00	0.00	0.01	0.01	0.02	0.05	0.14	0.23	0.44
	3:55:00	0.00	0.00	0.01	0.01	0.02	0.03	0.04	0.08	0.17
	4:00:00	0.00	0.00	0.01	0.01	0.01	0.02	0.02	0.05	0.11
	4:05:00 4:10:00	0.00	0.00	0.01	0.01 0.01	0.01 0.01	0.01 0.01	0.02 0.01	0.03	0.07 0.04
	4:15:00	0.00	0.00	0.00	0.00	0.01	0.01	0.01	0.02	0.02
	4:20:00	0.00	0.00	0.00	0.00	0.01	0.01	0.01	0.01	0.01
	4:25:00 4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.01
	4:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:45:00 4:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:00:00 5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:20:00 5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:40:00 5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:55:00 6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

DETENTION BASIN OUTLET STRUCTURE DESIGN MHFD-Detention, Version 4.04 (February 2021)

Summary Stage-Area-Volume-Discharge Relationships
The user can create a summary S-A-V-D by entering the desired stage increments and the remainder of the table will populate automatically.
The user should graphically compare the summary S-A-V-D table to the full S-A-V-D table in the chart to confirm it captures all key transition points.

	Chann	0	A	Makima	Maliana	Total	7
Stage - Storage	Stage	Area	Area	Volume	Volume	Outflow	
Description	[ft]	[ft ²]	[acres]	[ft ³]	[ac-ft]	[cfs]	
	0.00	32	0.001	0	0.000	0.00	For best results, include the
		334	0.008			0.01	stages of all grade slope
	0.50			46	0.001		changes (e.g. ISV and Floor)
	1.00	1,171	0.027	423	0.010	0.02	from the S-A-V table on
	1.50	3,036	0.070	1,304	0.030	0.03	Sheet 'Basin'.
WQCV	2.00	6,897	0.158	3,788	0.087	0.04	Sheet Basiii.
EURV	2.12	7,824	0.180	4,671	0.107	0.04	Also include the inverts of all
LONG	2.50	10,316	0.237	8,164	0.187	0.91	outlets (e.g. vertical orifice,
							overflow grate, and spillway,
100-YR	2.94	12,569	0.289	13,199	0.303	6.22	where applicable).
	3.00	12,876	0.296	13,962	0.321	7.30	where аррисавіе).
	3.50	15,082	0.346	21,011	0.482	20.07	1
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POND E FOREBAY VOLUME REQUIREMENTS

Equation 3-1 $WQCV = a(0.91I^3 - 1.19I^2 + 0.781I)$ a=1 (40 hour drain time)

Equation 3-3 V=(WQCV/12)A

Forebay 1 A= 17.69 Acres V= 0.083

3% OF WQCV FOREBAY TOTAL VOLUME= .03(V)

VOLUME REQUIRED FOR FOREBAY 1 = 0.002 AC-FT 109 CF

VOLUME PROVIDED FOR FOREBAY 1 = 0.005 AC-FT 230 CF

Q₁₀₀ Discharges 2% OF Q₁₀₀

 Q_{100} Forebay 1= .02*12.6 CFS= 0.25 CFS

Weir Report

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Monday, Dec 13 2021

Pond E Forebay Notch

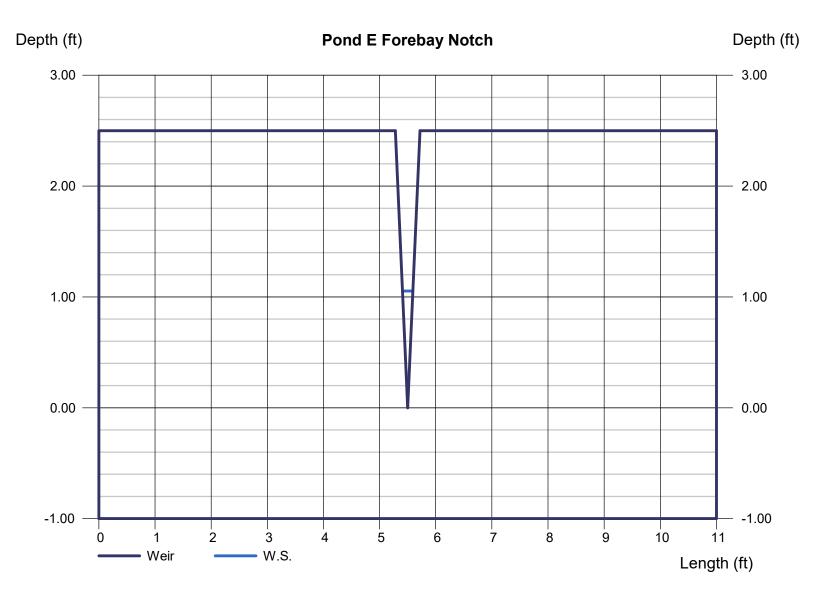
V-Notch Weir	
Crest	= Sharp
Angle (Deg)	= 10
Total Depth (ft)	= 2.50

Calculations

Weir Coeff. Cw = 0.22 Compute by: Known Q Known Q (cfs) = 0.25

Highlighted

Depth (ft) = 1.05 Q (cfs) = 0.250 Area (sqft) = 0.10 Velocity (ft/s) = 2.58 Top Width (ft) = 0.18



Channel Report

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

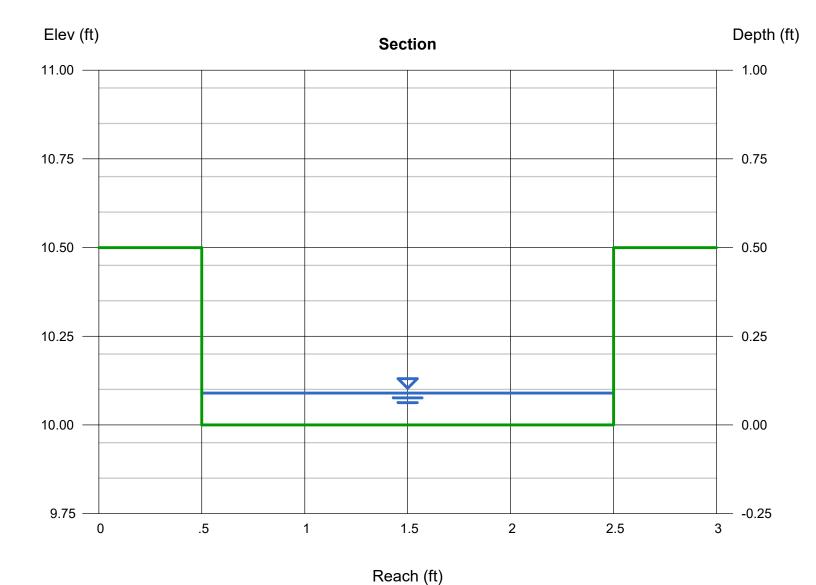
= 0.25

Monday, Dec 13 2021

Pond E Trickle Channel

Known Q (cfs)

	Highlighted	
= 2.00	Depth (ft)	= 0.09
= 0.50	Q (cfs)	= 0.250
	Area (sqft)	= 0.18
= 10.00	Velocity (ft/s)	= 1.39
= 0.50	Wetted Perim (ft)	= 2.18
= 0.013	Crit Depth, Yc (ft)	= 0.08
	Top Width (ft)	= 2.00
	EGL (ft)	= 0.12
Known Q		
	= 0.50 = 10.00 = 0.50 = 0.013	= 2.00 Depth (ft) = 0.50 Q (cfs) Area (sqft) = 10.00 Velocity (ft/s) = 0.50 Wetted Perim (ft) = 0.013 Crit Depth, Yc (ft) Top Width (ft) EGL (ft)



Weir Report

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Monday, Dec 13 2021

Pond E Spillway

Tra			

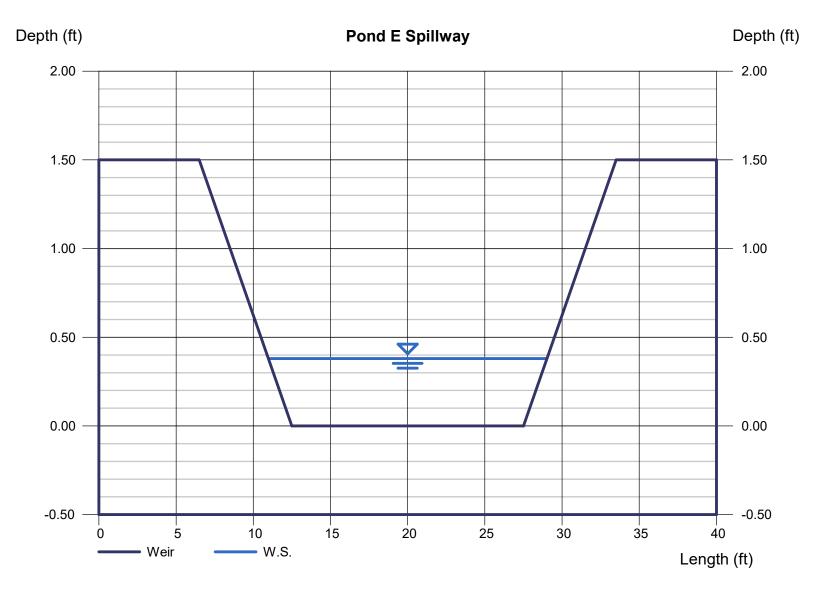
Crest = Sharp
Bottom Length (ft) = 15.00
Total Depth (ft) = 1.50
Side Slope (z:1) = 4.00

Calculations

Weir Coeff. Cw = 3.10 Compute by: Known Q Known Q (cfs) = 11.60

Highlighted

Depth (ft) = 0.38 Q (cfs) = 11.60 Area (sqft) = 6.28 Velocity (ft/s) = 1.85 Top Width (ft) = 18.04



Workhook Protected

Worksheet Protected

Stormwater Facility Name: Saddlehorn Filing 3 - Pond C

Facility Location & Jurisdiction: El Paso County - Saddlehorn Ranch Metropolitan District

User Input: Watershed Characteristics

Watershed Slope =	0.012	ft/ft
Watershed Length =	5370	ft
Watershed Area =	96.84	acres
Watershed Imperviousness =	14.6%	percent
Percentage Hydrologic Soil Group A =	93.0%	percent
Percentage Hydrologic Soil Group B =	0.0%	percent
Percentage Hydrologic Soil Groups C/D =	7.0%	percent

Location for 1-hr Rainfall Depths (use dropdown):

User Input

WQCV Treatment Method = Extended Detention

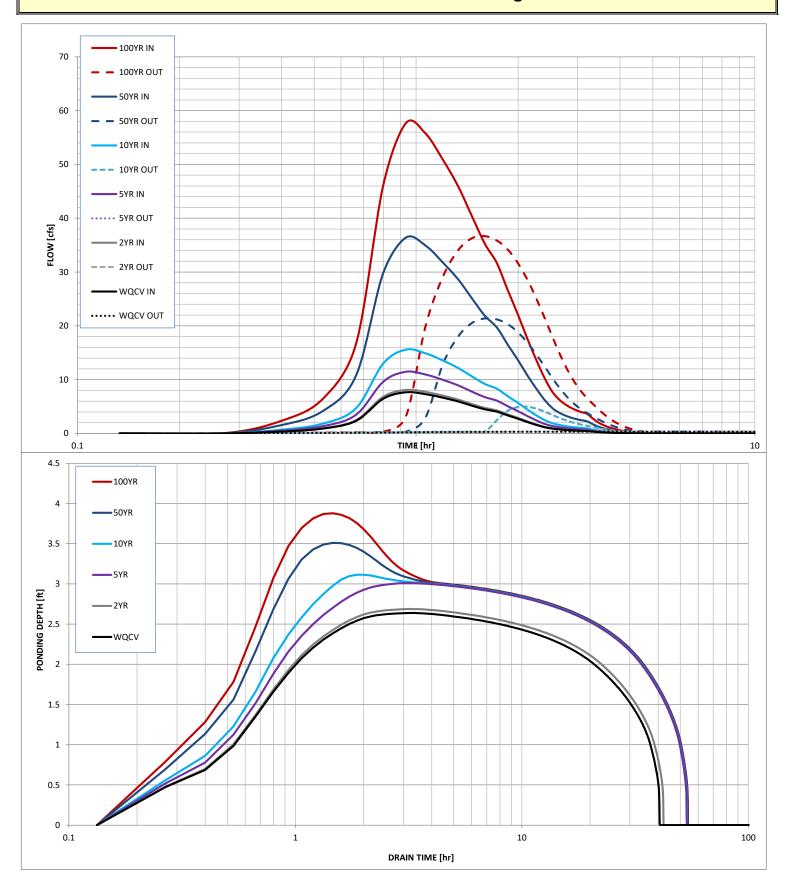
User Defined User Defined User Defined User Defined Area [ft^2] Discharge [cfs] Stage [ft] Stage [ft] 0.00 32 0.00 0.00 0.33 50 0.33 0.05 1.00 3,260 1.00 0.11 2.00 17,980 2.00 0.24 3.00 46,439 3.00 0.35 4.00 73,964 4.00 41.88 5.00 86,681 5.00 237.69 5.50 89,520 5.50 408.05

After completing and printing this worksheet to a pdf, go to: https://maperture.digitaldataservices.com/gvh/?viewer=cswdif create a new stormwater facility, and attach the pdf of this worksheet to that record.

Routed Hydrograph Results

	Routed Hydrograph Results						
Design Storm Return Period =	WQCV	2 Year	5 Year	10 Year	50 Year	100 Year	
One-Hour Rainfall Depth =	0.53	1.19	1.50	1.75	2.25	2.52	in
Calculated Runoff Volume =	0.737	0.780	1.110	1.513	3.577	5.724	acre-ft
OPTIONAL Override Runoff Volume =							acre-ft
Inflow Hydrograph Volume =	0.736	0.779	1.109	1.513	3.577	5.722	acre-ft
Time to Drain 97% of Inflow Volume =	37.4	38.9	49.0	48.1	43.7	39.8	hours
Time to Drain 99% of Inflow Volume =	39.3	40.9	51.6	51.2	49.4	47.7	hours
Maximum Ponding Depth =	2.64	2.69	3.01	3.11	3.51	3.88	ft
Maximum Ponded Area =	0.83	0.86	1.07	1.13	1.38	1.62	acres
Maximum Volume Stored =	0.662	0.702	1.014	1.127	1.624	2.180	acre-ft

SDI_Pond C.xlsm, Design Data 1/5/2022, 9:40 AM



SDI_Pond C.xlsm, Design Data 1/5/2022, 9:40 AM

Workhook Protected

Worksheet Protected

Stormwater Facility Name: Saddlehorn Ranch Filing 3 - Pond D

Facility Location & Jurisdiction: El Paso County - Saddlehorn Ranch Metropolitan District

User Input: Watershed Characteristics

Watershed Slope =	0.012	ft/ft
Watershed Length =	3473	ft
Watershed Area =	78.02	acres
Watershed Imperviousness =	15.4%	percent
Percentage Hydrologic Soil Group A =	70.0%	percent
Percentage Hydrologic Soil Group B =	0.0%	percent
Percentage Hydrologic Soil Groups C/D =	30.0%	percent
		1"

Location for 1-hr Rainfall Depths (use dropdown):

User Input

WQCV Treatment Method = Extended Detention

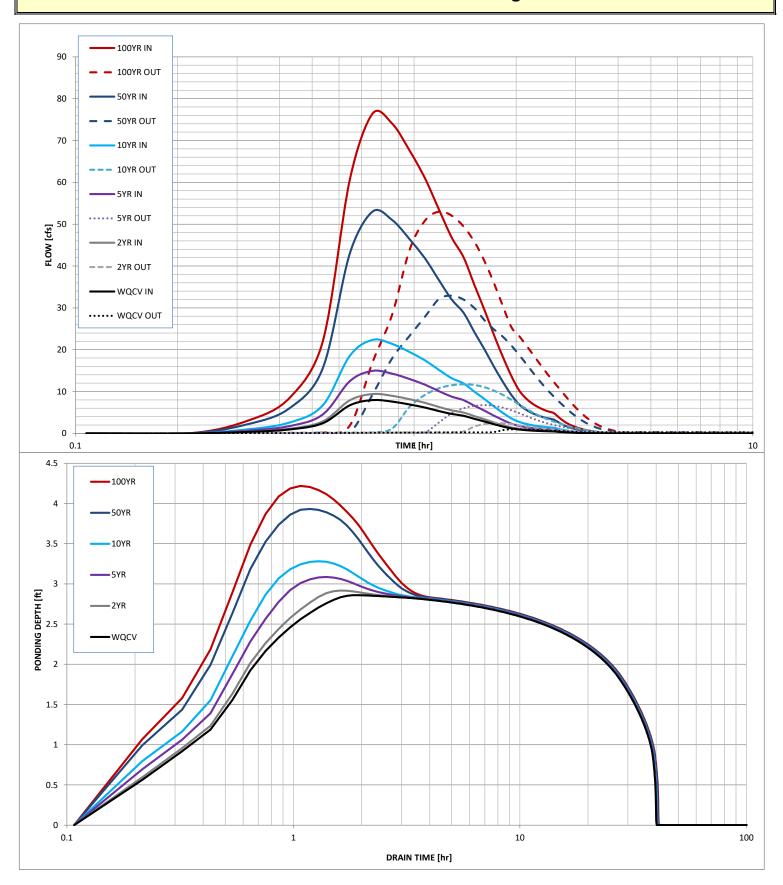
User Defined	User Defined	User Defined	User Defined
Stage [ft]	Area [ft^2]	Stage [ft]	Discharge [cfs]
0.00	32	0.00	0.00
0.33	50	0.33	0.04
0.83	699	0.83	0.06
1.83	8,089	1.83	0.15
2.83	27,770	2.83	0.26
3.83	58,037	3.83	25.71
4.33	70,791	4.33	61.17
4.83	83,546	4.83	146.98
5.83	98,172	5.83	513.83

After completing and printing this worksheet to a pdf, go to: https://maperture.digitaldataservices.com/gvh/?viewer=cswdif create a new stormwater facility, and attach the pdf of this worksheet to that record.

Routed Hydrograph Results

	Routeu Hyuro	graph Results					_
Design Storm Return Period =	WQCV	2 Year	5 Year	10 Year	50 Year	100 Year	
One-Hour Rainfall Depth =	0.53	1.19	1.50	1.75	2.25	2.52	in
Calculated Runoff Volume =	0.619	0.733	1.170	1.758	4.226	6.144	acre-ft
OPTIONAL Override Runoff Volume =							acre-ft
Inflow Hydrograph Volume =	0.619	0.733	1.170	1.758	4.226	6.142	acre-ft
Time to Drain 97% of Inflow Volume =	36.5	36.0	34.5	32.7	26.5	22.5	hours
Time to Drain 99% of Inflow Volume =	38.5	38.3	37.8	37.0	34.2	32.4	hours
Maximum Ponding Depth =	2.86	2.92	3.09	3.28	3.93	4.22	ft
Maximum Ponded Area =	0.65	0.70	0.81	0.95	1.39	1.56	acres
Maximum Volume Stored =	0.533	0.573	0.701	0.872	1.637	2.055	acre-ft

SDI_Pond D.xlsm, Design Data 1/5/2022, 9:56 AM



SDI_Pond D.xlsm, Design Data 1/5/2022, 9:56 AM

Workhook Protected

Worksheet Protected

Stormwater Facility Name: Saddlehorn Ranch Filing 3 - Pond E

Facility Location & Jurisdiction: El Paso County - Saddlehorn Ranch Metropolitan District

User Input: Watershed Characteristics

Watershed Slope =	0.012	ft/ft
Watershed Length =	1810	ft
Watershed Area =	18.37	acres
Watershed Imperviousness =	8.1%	percent
Percentage Hydrologic Soil Group A =	83.0%	percent
Percentage Hydrologic Soil Group B =	0.0%	percent
Percentage Hydrologic Soil Groups C/D =	17.0%	percent

Location for 1-hr Rainfall Depths (use dropdown):

User Input

WQCV Treatment Method = Extended Detention

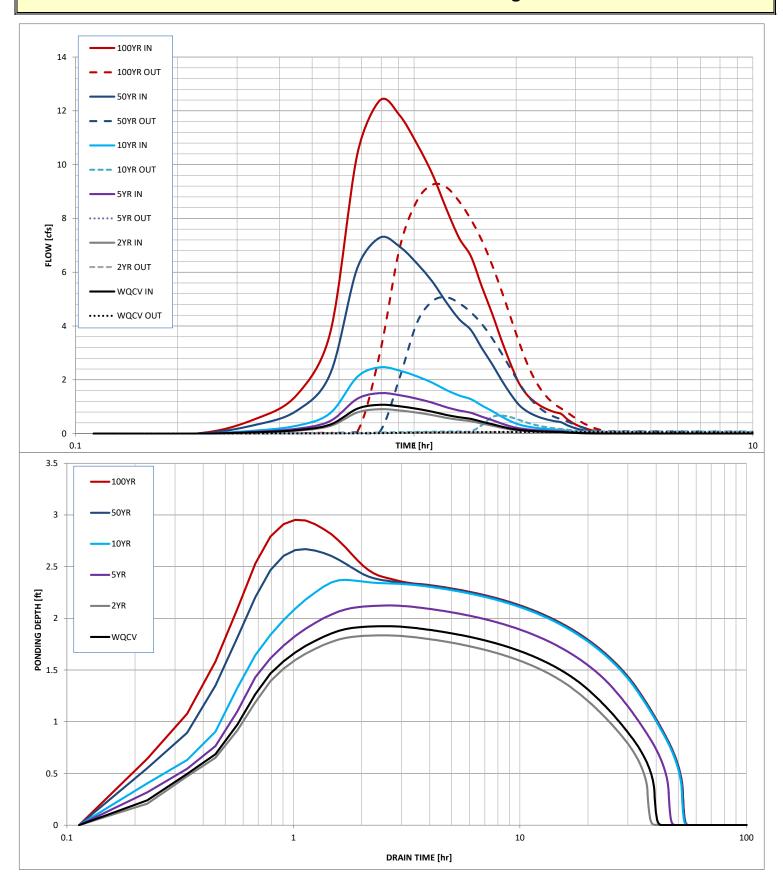
User Defined User Defined User Defined User Defined Area [ft^2] Discharge [cfs] Stage [ft] Stage [ft] 0.00 32 0.00 0.00 0.33 50 0.33 0.01 0.83 887 0.83 0.01 1.33 1.33 1,723 0.02 2.33 9,446 2.33 0.09 3.33 14,566 3.33 14.90 3.83 16,083 3.83 35.11 73.11 4.33 17,600 4.33 4.83 19,121 4.83 128.58

After completing and printing this worksheet to a pdf, go to: https://maperture.digitaldataservices.com/gvh/?viewer=cswdif create a new stormwater facility, and attach the pdf of this worksheet to that record.

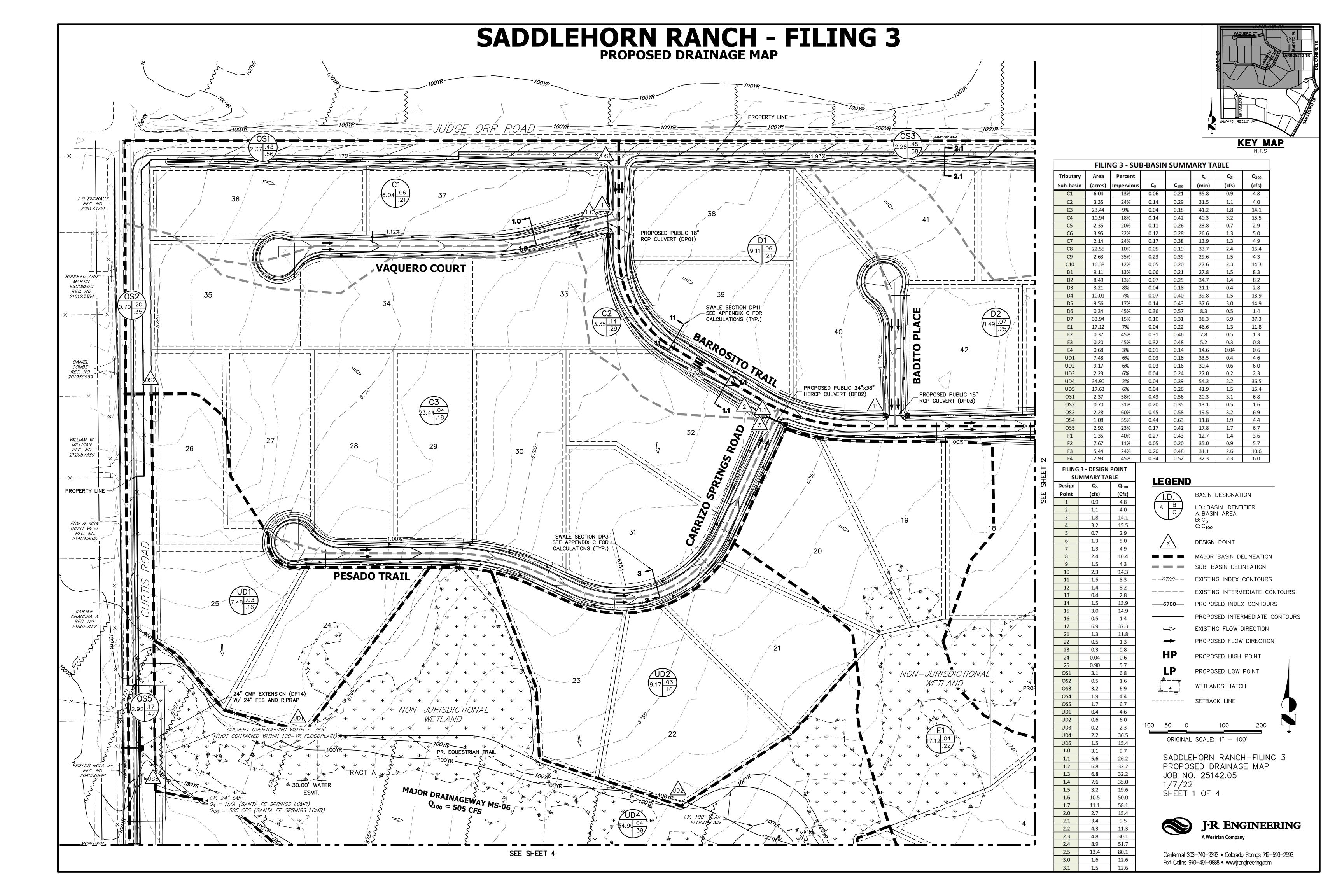
Routed Hydrograph Results

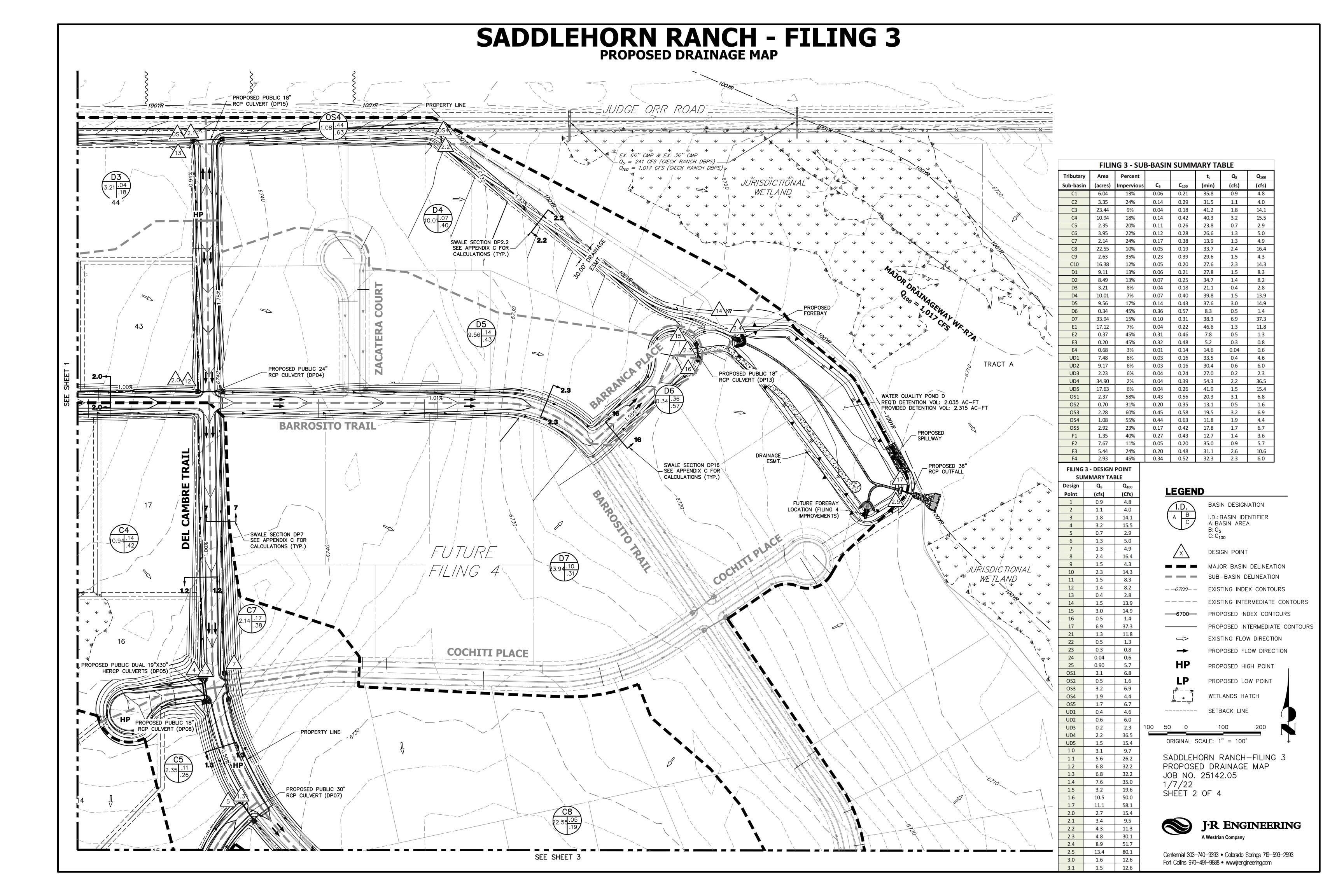
Routed Hydrograph Results							_
Design Storm Return Period =	WQCV	2 Year	5 Year	10 Year	50 Year	100 Year	
One-Hour Rainfall Depth =	0.53	1.19	1.50	1.75	2.25	2.52	in
Calculated Runoff Volume =	0.086	0.073	0.121	0.199	0.596	1.019	acre-ft
OPTIONAL Override Runoff Volume =							acre-ft
Inflow Hydrograph Volume =	0.085	0.072	0.120	0.199	0.596	1.019	acre-ft
Time to Drain 97% of Inflow Volume =	35.7	33.6	40.3	43.9	34.3	28.1	hours
Time to Drain 99% of Inflow Volume =	38.3	35.9	43.8	49.1	44.3	40.2	hours
Maximum Ponding Depth =	1.92	1.84	2.12	2.37	2.67	2.95	ft
Maximum Ponded Area =	0.14	0.13	0.18	0.22	0.26	0.29	acres
Maximum Volume Stored =	0.075	0.063	0.107	0.157	0.228	0.305	acre-ft

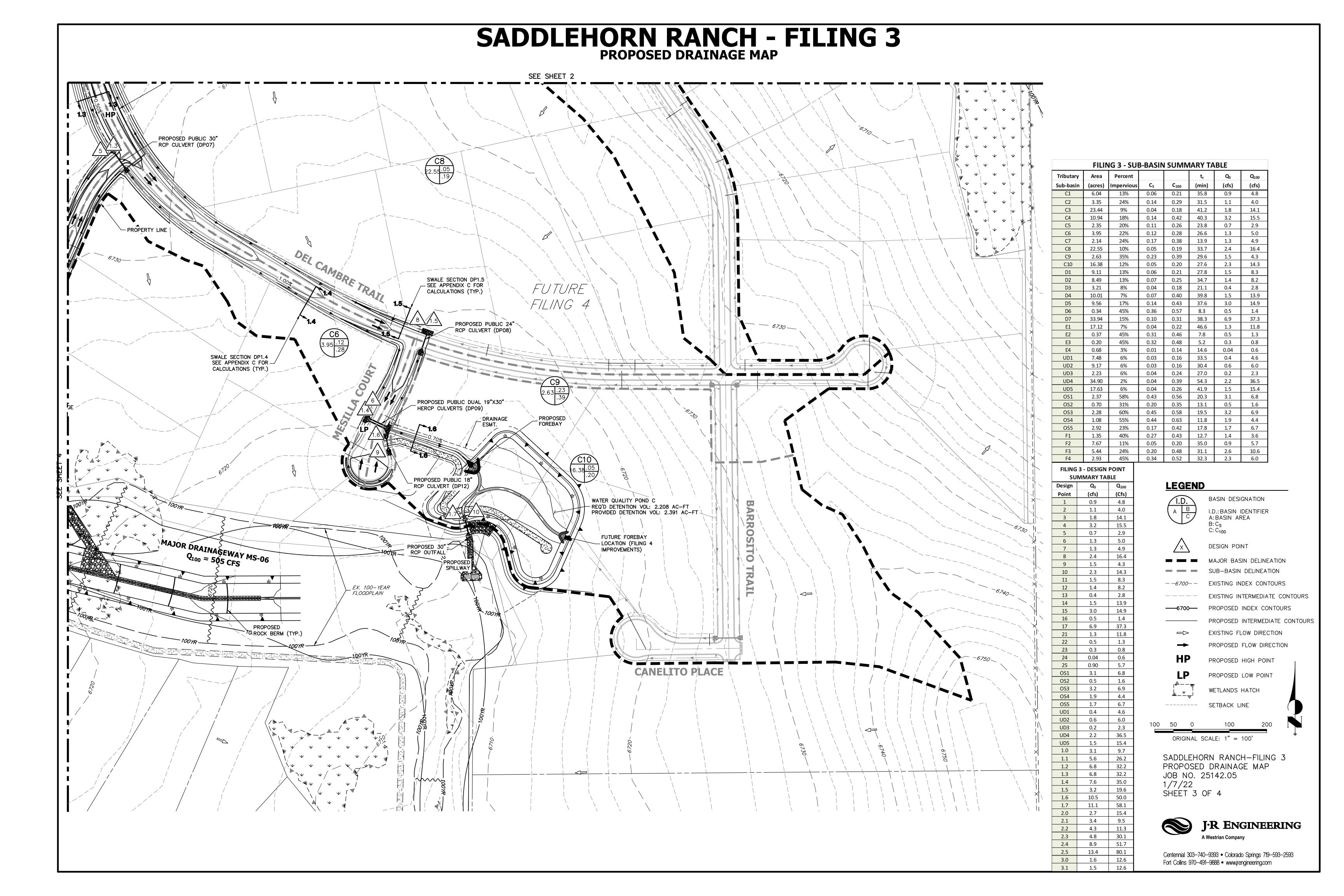
SDI_Pond E.xlsm, Design Data 1/5/2022, 10:14 AM

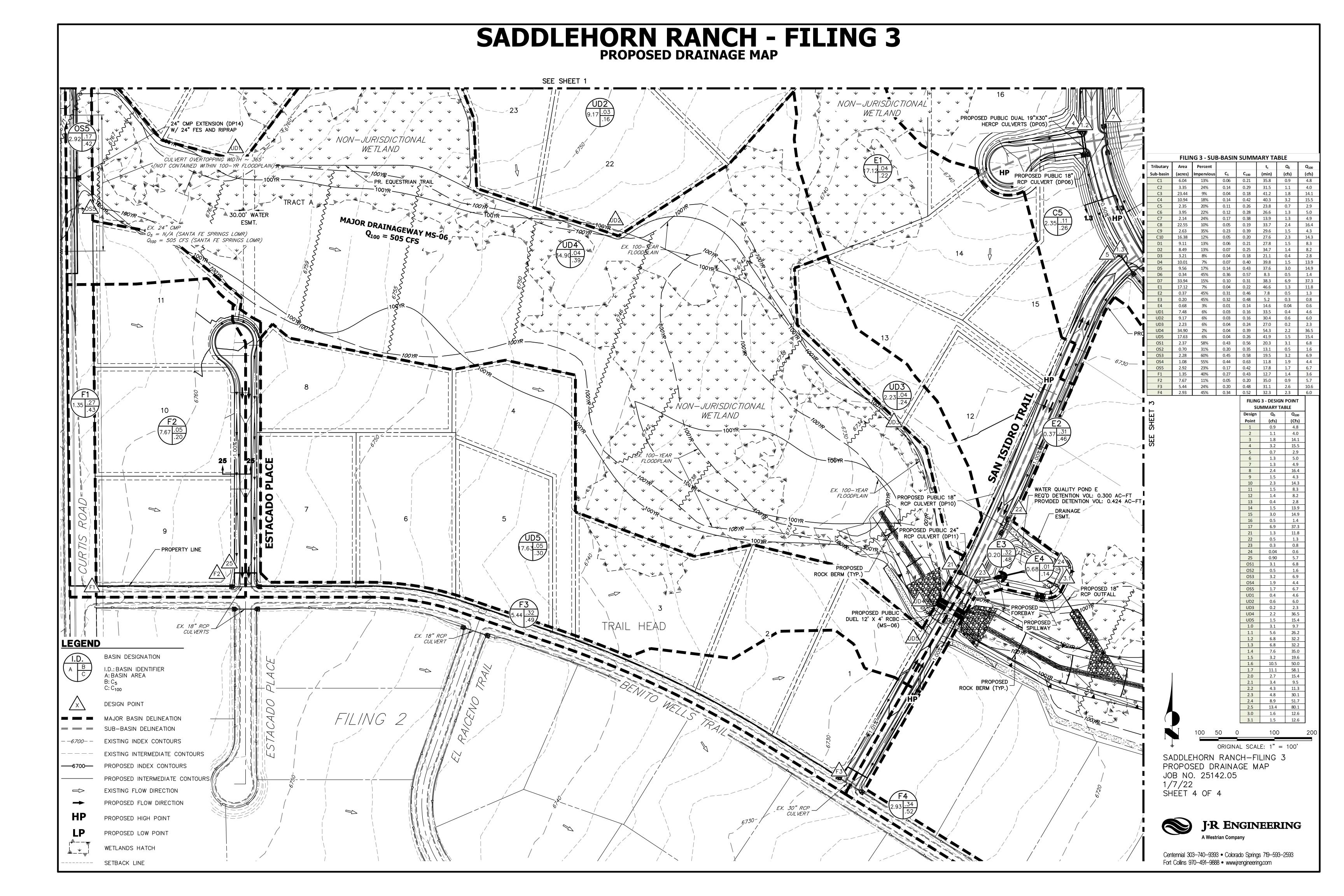


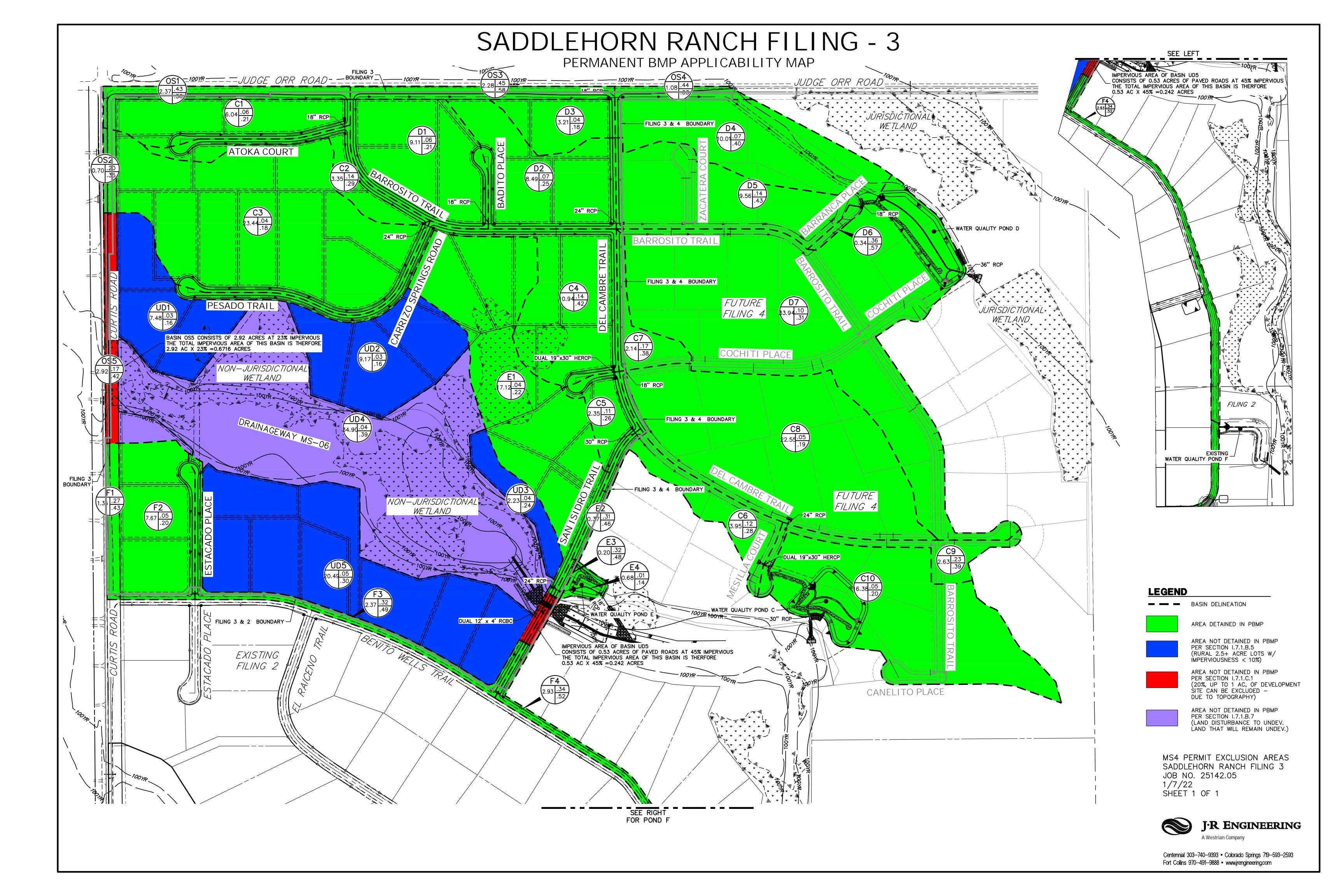
SDI_Pond E.xlsm, Design Data 1/5/2022, 10:14 AM











Subdivision: Saddlehorn Ranch Filing 3
Location: El Paso County

Project Name: Saddlehorn Ranch
Project No.: 25142.05
Calculated By: AAM
Checked By: Date: 174/22

	S	STORM DRAIN SYSTEM		
	DESIGN POINT 1.0	DESIGN POINT 1.1	DESIGN POINT 11	Notes
Q ₁₀₀ (cfs):	9.7	26.2	8.3	Flows are the greater of proposed vs. future
Conduit	Pipe	Pipe	Pipe	
D_c , Pipe Diameter (in):	18	30	18	
W, Box Width (ft):	N/A	N/A	N/A	
H, Box Height (ft):	N/A	N/A	N/A	
Y_t , Tailwater Depth (ft):	1.32	1.25	1.17	If unknown, use Y_t/D_c (or H)=0.4
Y_t/Dc or Y_t/H	0.88	0.50	0.78	
Q/D ^{2.5} or Q/(WH ^{3/2})	3.52	2.65	3.01	
Supercritical?	No	No	No	
Y_n , Normal Depth (ft) [Supercritical]:	0.00	0.00	0.00	
D_a , H_a (in) [Supercritical]:	N/A	N/A	N/A	$D_a = (D_c + Y_n)/2$
Riprap d_{50} (in) [Supercritical]:	N/A	N/A	N/A	
Riprap d_{50} (in) [Subcritical]:	1.70	4.20	1.68	
Required Riprap Size:	L	L	L	Fig. 9-38 or Fig. 9-36
d 50 (in):	9	9	9	
Expansion Factor, $1/(2 \tan \theta)$:	6.75	6.25	6.75	Read from Fig. 9-35 or 9-36
θ :	0.07	0.08	0.07	
Erosive Soils?	No	No	No	
Area of Flow, A_t (ft ²):	1.39	3.74	1.19	$A_t = Q/V$
Length of Protection, L_p (ft):	-3.0	3.1	-3.3	L=(1/(2 tan θ))(At/Yt - D)
Min Length (ft)	4.5	7.5	4.5	Min L=3D or 3H
Max Length (ft)	15.0	25.0	15.0	Max L=10D or 10H
Min Bottom Width, T (ft):	1.1	3.0	1.0	$T=2*(L_p*tan\theta)+W$
Design Length (ft)	4.5	7.5	4.5	
Design Width (ft)	1.1	3.0	1.0	
Riprap Depth (in)	18	18	18	Depth=2(d ₅₀)
Type II Bedding Depth (in)*	6	6	6	*Not used if Soil Riprap
Cutoff Wall	No	No	No	
Cutoff Wall Depth (ft)				Depth of Riprap and Base
Cutoff Wall Width (ft)				

^{*} For use when the flow in the culvert is supercritical (and less than full).

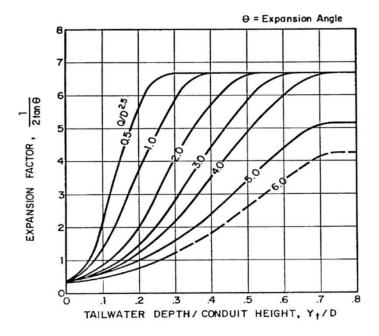


Figure 9-35. Expansion factor for circular conduits

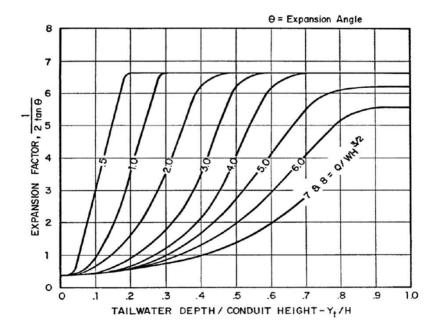


Figure 9-36. Expansion factor for rectangular conduits

Subdivision: Saddlehorn Ranch Filing 3

Location: El Paso County

Project Name: Saddlehorn Ranch

Project No.: 25142.05 Calculated By: AAM

Checked By: TBD

Date: 1/4/22

	S	TORM DRAIN SYSTEN		
	DESIGN POINT 2.0	DESIGN POINT 1.2	DESIGN POINT 7	Notes
Q ₁₀₀ (cfs):	15.4	32.2	4.9	Flows are the greater of proposed vs. future
Conduit	Pipe	Pipe	Pipe	
D_c , Pipe Diameter (in):	24	24	18	
W, Box Width (ft):	N/A	N/A	N/A	
H, Box Height (ft):	N/A	N/A	N/A	
Y_t , Tailwater Depth (ft):	1.08	1.34	0.39	If unknown, use Y_t/D_c (or H)=0.4
Y_t/Dc or Y_t/H	0.54	0.67	0.26	
$Q/D^{2.5}$ or $Q/(WH^{3/2})$	2.72	5.69	1.78	
Supercritical?	No	No	No	
Y_n , Normal Depth (ft) [Supercritical]:	0.00	0.00	0.00	
D_a , H_a (in) [Supercritical]:	N/A	N/A	N/A	$D_a = (D_c + Y_n)/2$
Riprap d_{50} (in) [Supercritical]:	N/A	N/A	N/A	
Riprap d ₅₀ (in) [Subcritical]:	3.15	5.08	3.71	
Required Riprap Size:	L	L	L	Fig. 9-38 or Fig. 9-36
d ₅₀ (in):	9	9	9	
Expansion Factor, $1/(2 \tan \theta)$:	6.75	4.25	3.50	Read from Fig. 9-35 or 9-36
θ :	0.07	0.12	0.14	
Erosive Soils?	No	No	No	
Area of Flow, A_t (ft ²):	2.20	4.60	0.70	$A_t = Q/V$
Length of Protection, L_p (ft):	0.3	6.1	1.0	L=(1/(2 tan θ))(At/Yt - D)
Min Length (ft)	6.0	6.0	4.5	Min L=3D or 3H
Max Length (ft)	20.0	20.0	15.0	Max L=10D or 10H
Min Bottom Width, T (ft):	2.0	3.4	1.8	$T=2*(L_p*tan\theta)+W$
Design Length (ft)	6.0	7.0	4.5	
Design Width (ft)	2.0	3.4	1.8	
Riprap Depth (in)	18	18	18	Depth=2(d ₅₀)
Type II Bedding Depth (in)*	6	6	6	*Not used if Soil Riprap
Cutoff Wall	No	No	No	
Cutoff Wall Depth (ft)				Depth of Riprap and Base
Cutoff Wall Width (ft)				

^{*} For use when the flow in the culvert is supercritical (and less than full).

Subdivision: Saddlehorn Ranch Filing 3

Location: El Paso County

Project Name: Saddlehorn Ranch

Project No.: 25142.05

Calculated By: AAM

Checked By: TBD

Date: 1/4/22

	S	TORM DRAIN SYSTEN		
	DESIGN POINT 1.3	DESIGN POINT 1.5	DESIGN POINT 1.4	Notes
Q ₁₀₀ (cfs):	32.2	19.6	35.0	Flows are the greater of proposed
				vs. future
Conduit	Pipe	Pipe	Pipe	
D_c , Pipe Diameter (in):	30	24	24	
W, Box Width (ft):	N/A	N/A	N/A	
H, Box Height (ft):	N/A	N/A	N/A	
Y_t , Tailwater Depth (ft):	1.24	1.30	1.46	If unknown, use Y_t/D_c (or H)=0.4
Y_t/Dc or Y_t/H	0.50	0.65	0.73	
Q/D ^{2.5} or Q/(WH ^{3/2})	3.26	3.46	6.19	
Supercritical?	No	No	No	
Y_n , Normal Depth (ft) [Supercritical]:	0.00	0.00	0.00	
D_a , H_a (in) [Supercritical]:	N/A	N/A	N/A	$D_a = (D_c + Y_n)/2$
Riprap d_{50} (in) [Supercritical]:	N/A	N/A	N/A	
Riprap d_{50} (in) [Subcritical]:	5.22	3.21	4.98	
Required Riprap Size:	L	L	L	Fig. 9-38 or Fig. 9-36
d 50 (in):	9	9	9	
Expansion Factor, $1/(2 \tan \theta)$:	5.50	6.75	4.25	Read from Fig. 9-35 or 9-36
θ :	0.09	0.07	0.12	
Erosive Soils?	No	No	No	
Area of Flow, A_t (ft ²):	4.60	2.80	5.00	$A_t = Q/V$
Length of Protection, L_p (ft):	6.7	1.0	6.1	L=(1/(2 tan θ))(At/Yt - D)
Min Length (ft)	7.5	6.0	6.0	Min L=3D or 3H
Max Length (ft)	25.0	20.0	20.0	Max L=10D or 10H
Min Bottom Width, T (ft):	3.7	2.2	3.4	$T=2*(L_p*tan\theta)+W$
Design Length (ft)	7.5	6.0	7.0	
Design Width (ft)	3.7	2.2	3.4	
Riprap Depth (in)	18	18	18	Depth=2(d ₅₀)
Type II Bedding Depth (in)*	6	6	6	*Not used if Soil Riprap
Cutoff Wall	No	No	No	
Cutoff Wall Depth (ft)				Depth of Riprap and Base
Cutoff Wall Width (ft)				

^{*} For use when the flow in the culvert is supercritical (and less than full).

Subdivision: Saddlehorn Ranch Filing 3

Location: El Paso County

Project Name: Saddlehorn Ranch

Project No.: <u>25142.05</u>

Calculated By: AAM
Checked By: TBD

Date: 1/4/22

	S	TORM DRAIN SYSTEN	Л	
	DESIGN POINT 22	DESIGN POINT 21	DESIGN POINT 9	Notes
Q ₁₀₀ (cfs):	1.3	11.8	4.3	Flows are the greater of proposed vs. future
Conduit	Pipe	Pipe	Pipe	
D_c , Pipe Diameter (in):	18	24	18	
W, Box Width (ft):	N/A	N/A	N/A	
H, Box Height (ft):	N/A	N/A	N/A	
Y_t , Tailwater Depth (ft):	0.39	0.94	0.77	If unknown, use Y_t/D_c (or H)=0.4
Y_t/Dc or Y_t/H	0.26	0.47	0.51	
Q/D ^{2.5} or Q/(WH ^{3/2})	0.47	2.09	1.56	
Supercritical?	No	No	No	
Y_n , Normal Depth (ft) [Supercritical]:	0.00	0.00	0.00	
D_a , H_a (in) [Supercritical]:	N/A	N/A	N/A	$D_a = (D_c + Y_n)/2$
Riprap d ₅₀ (in) [Supercritical]:	N/A	N/A	N/A	
Riprap d ₅₀ (in) [Subcritical]:	0.98	2.85	1.44	
Required Riprap Size:	L	L	L	Fig. 9-38 or Fig. 9-36
d ₅₀ (in):	9	9	9	
Expansion Factor, $1/(2 \tan \theta)$:	6.75	6.75	6.75	Read from Fig. 9-35 or 9-36
θ :	0.07	0.07	0.07	
Erosive Soils?	No	No	No	
Area of Flow, A_t (ft ²):	0.19	1.69	0.61	$A_t = Q/V$
Length of Protection, L_p (ft):	-6.9	-1.4	-4.7	L=(1/(2 tan θ))(At/Yt - D)
Min Length (ft)	4.5	6.0	4.5	Min L=3D or 3H
Max Length (ft)	15.0	20.0	15.0	Max L=10D or 10H
Min Bottom Width, T (ft):	0.5	1.8	0.8	$T=2*(L_p*tan\theta)+W$
Design Length (ft)	4.5	6.0	4.5	
Design Width (ft)	0.5	1.8	0.8	
Riprap Depth (in)	18	18	18	Depth=2(d ₅₀)
Type II Bedding Depth (in)*	6	6	6	*Not used if Soil Riprap
Cutoff Wall	No	No	No	
Cutoff Wall Depth (ft)				Depth of Riprap and Base
Cutoff Wall Width (ft)				

^{*} For use when the flow in the culvert is supercritical (and less than full).

Subdivision: Saddlehorn Ranch Filing 3

Location: El Paso County

Project Name: Saddlehorn Ranch

Project No.: <u>25142.05</u>

Calculated By: AAM
Checked By: TBD

Date: 1/4/22

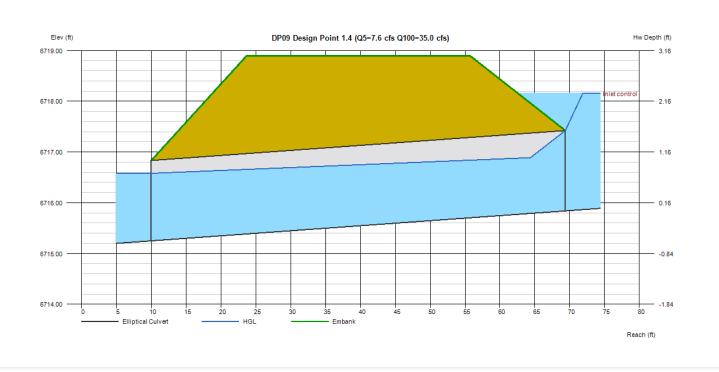
		STORM DRAIN SYSTEM	Л				
	DESIGN POINT 16	DESIGN POINT 2.1		Notes			
Q ₁₀₀ (cfs):	1.4	9.5		Flows are the greater of proposed vs. future			
Conduit	Pipe	Pipe					
D_c , Pipe Diameter (in):	18	30					
W, Box Width (ft):	N/A	N/A					
H, Box Height (ft):	N/A	N/A					
Y_t , Tailwater Depth (ft):	0.40	1.30	I	f unknown, use Y_t/D_c (or H)=0.4			
Y_t/Dc or Y_t/H	0.27	0.52					
$Q/D^{2.5}$ or $Q/(WH^{3/2})$	0.51	0.96					
Supercritical?	No	No					
Y_n , Normal Depth (ft) [Supercritical]:	0.00	0.00					
D_a , H_a (in) [Supercritical]:	N/A	N/A	1	$D_a = (D_c + Y_n)/2$			
Riprap d_{50} (in) [Supercritical]:	N/A	N/A					
Riprap d_{50} (in) [Subcritical]:	1.03	1.45					
Required Riprap Size:	L	L	F	Fig. 9-38 or Fig. 9-36			
d ₅₀ (in):	9	9					
Expansion Factor, $1/(2 \tan \theta)$:	6.75	6.75	F	Read from Fig. 9-35 or 9-36			
θ :	0.07	0.07					
Erosive Soils?	No	No					
Area of Flow, A_t (ft ²):	0.20	1.36	,	$A_t = Q/V$			
Length of Protection, L_p (ft):	-6.8	-9.8	L	_=(1/(2 tan θ))(At/Yt - D)			
Min Length (ft)	4.5	7.5		Min L=3D or 3H			
Max Length (ft)	15.0	25.0		Max L=10D or 10H			
Min Bottom Width, T (ft):	0.5	1.0	1	$\Gamma=2*(L_p*tan\theta)+W$			
Design Length (ft)	4.5	7.5					
Design Width (ft)	0.5	1.0					
Riprap Depth (in)	18	18		Depth=2(d ₅₀)			
Type II Bedding Depth (in)*	6	6	τ	*Not used if Soil Riprap			
Cutoff Wall	No	No					
Cutoff Wall Depth (ft)			[Depth of Riprap and Base			
Cutoff Wall Width (ft)							

^{*} For use when the flow in the culvert is supercritical (and less than full).

Tuesday, Dec 21 2021

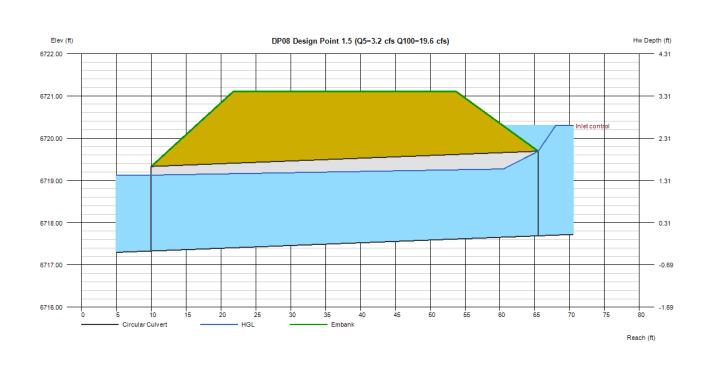
DP09 Design Point 1.4 (Q5=7.6 cfs Q100=35.0 cfs)

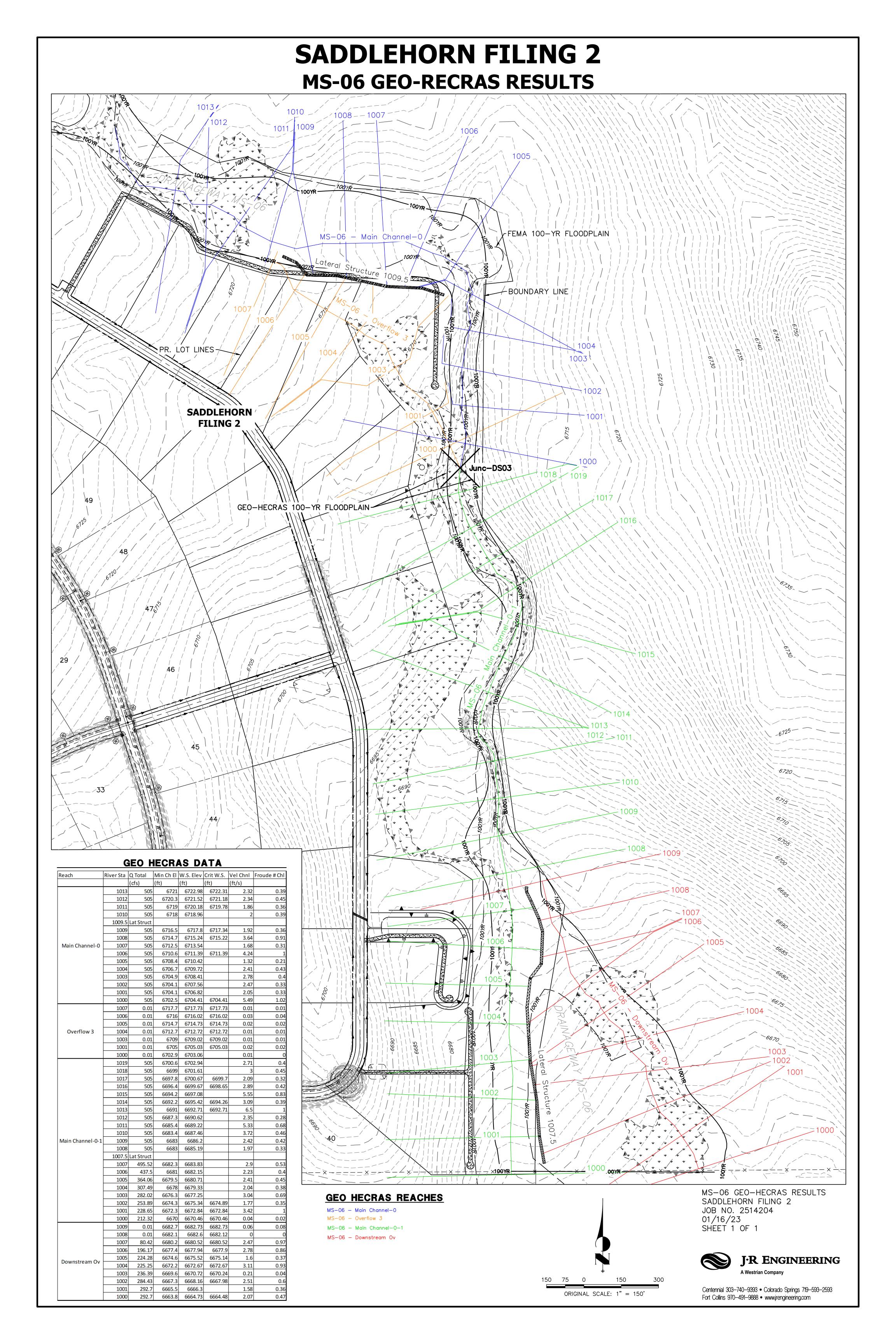
Invert Elev Dn (ft)	= 6715.25	Calculations	
Pipe Length (ft)	= 59.38	Qmin (cfs)	= 7.60
Slope (%)	= 0.99	Qmax (cfs)	= 35.00
Invert Elev Up (ft)	= 6715.84	Tailwater Élev (ft)	= (dc+D)/2
Rise (in)	= 19.0	, ,	,
Shape	= Elliptical	Highlighted	
Span (in)	= 30.0	Qtotal (cfs)	= 35.00
No. Barrels	= 2	Qpipe (cfs)	= 35.00
n-Value	= 0.012		= 0.00
Culvert Type	= Horizontal Ellipse Concrete	Veloc Dn (ft/s)	= 6.02
Culvert Entrance	= Square edge w/headwall (H)	Veloc Up (ft/s)	= 7.51
Coeff. K,M,c,Y,k	= 0.01, 2, 0.0398, 0.67, 0.5	HGL Dn (ft)	= 6716.58
		HGL Up (ft)	= 6716.92
Embankment		Hw Elev (ft)	= 6718.15
Top Elevation (ft)	= 6718.90	Hw/D (ft)	= 1.46
Top Width (ft)	= 32.00	Flow Regime	= Inlet Control
Crest Width (ft)	= 20.00	-	
Shape Span (in) No. Barrels n-Value Culvert Type Culvert Entrance Coeff. K,M,c,Y,k Embankment Top Elevation (ft) Top Width (ft)	= Elliptical = 30.0 = 2 = 0.012 = Horizontal Ellipse Concrete = Square edge w/headwall (H) = 0.01, 2, 0.0398, 0.67, 0.5 = 6718.90 = 32.00	Qpipe (cfs) Qovertop (cfs) Veloc Dn (ft/s) Veloc Up (ft/s) HGL Dn (ft) HGL Up (ft) Hw Elev (ft) Hw/D (ft)	= 35.00 = 0.00 = 6.02 = 7.51 = 6716.58 = 6716.92 = 6718.15 = 1.46



DP08 Design Point 1.5 (Q5=3.2 cfs Q100=19.6 cfs)

Invert Elev Dn (ft)	= 6717.33	Calculations	
Pipe Length (ft)	= 55.50	Qmin (cfs)	= 3.20
Slope (%)	= 0.65	Qmax (cfs)	= 19.60
Invert Elev Up (ft)	= 6717.69	Tailwater Elev (ft)	= (dc+D)/2
Rise (in)	= 24.0		·
Shape	= Circular	Highlighted	
Span (in)	= 24.0	Qtotal (cfs)	= 19.60
No. Barrels	= 1	Qpipe (cfs)	= 19.60
n-Value	= 0.012	Qovertop (cfs)	= 0.00
Culvert Type	Circular Concrete	Veloc Dn (ft/s)	= 6.59
Culvert Entrance	= Groove end projecting (C)	Veloc Up (ft/s)	= 7.30
Coeff. K,M,c,Y,k	= 0.0045, 2, 0.0317, 0.69, 0.2	HGL Dn (ft)	= 6719.13
		HGL Up (ft)	= 6719.28
Embankment		Hw Elev (ft)	= 6720.30
Top Elevation (ft)	= 6721.10	Hw/D (ft)	= 1.30
Top Width (ft)	= 32.00	Flow Regime	= Inlet Control
Crest Width (ft)	= 20.00		





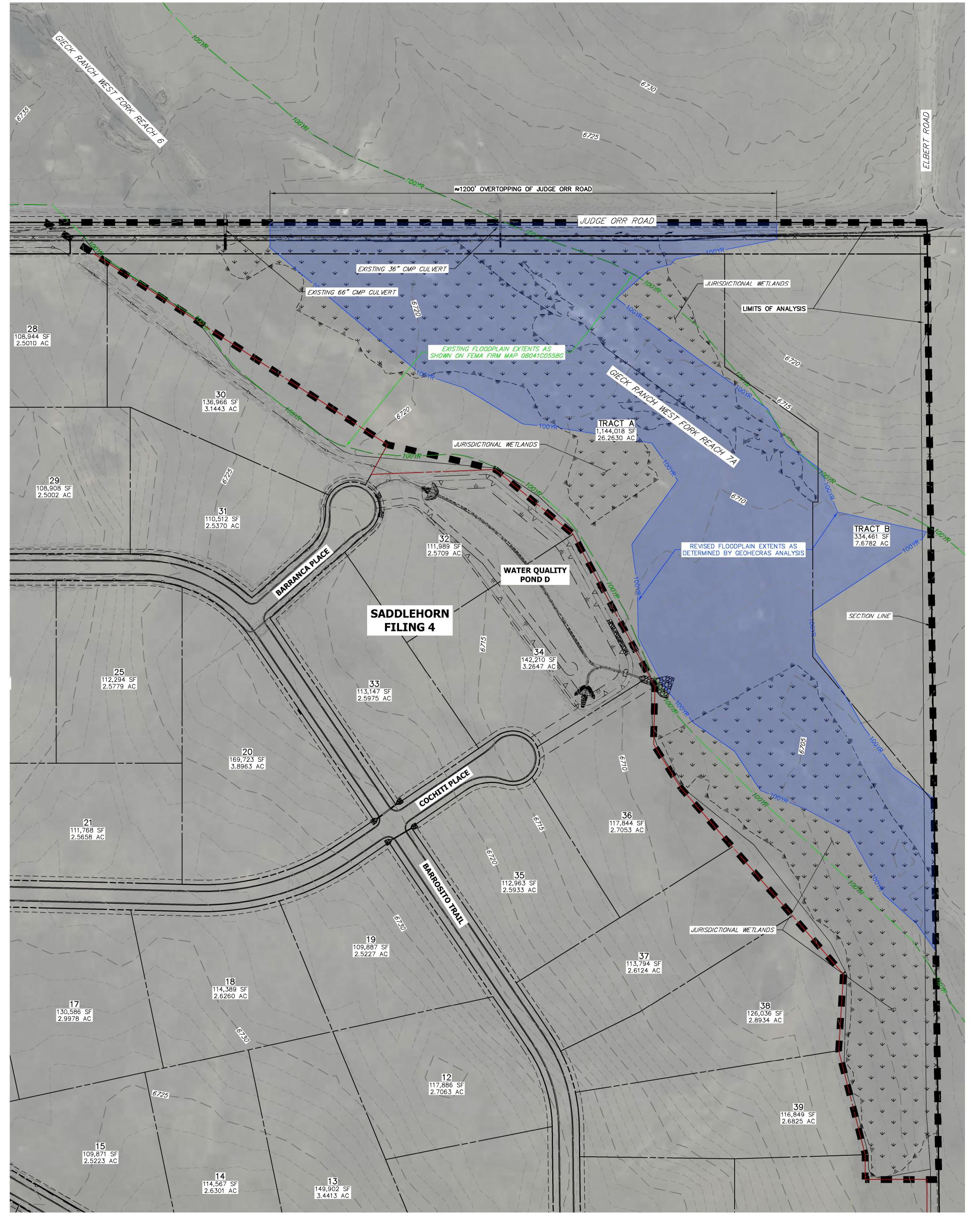
HEC-RAS Plan: Defa	ult Scenario P	rofile: 100 yr												
Reach	River Sta	Profile	Q Total	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope	Vel Chnl	Flow Area	Top Width	Froude # Chl	Shear Chan	Hydr Depth
			(cfs)	(ft)	(ft)	(ft)	(ft)	(ft/ft)	(ft/s)	(sq ft)	(ft)		(lb/sq ft)	(ft)
Main Channel-0	1014	100 yr	505.00	6721.50	6723.80		6724.00	0.002891	3.61	139.94	116.54	0.58	0.22	1.20
Main Channel-0	1013	100 yr	505.00	6721.00	6722.98	6722.31	6723.07	0.007902	2.32	217.55	200.88	0.39	0.53	1.08
Main Channel-0	1012	100 yr	505.00	6720.30	6721.52	6721.18	6721.61	0.011583	2.34	221.16	303.86	0.45	0.59	0.73
Main Channel-0	1011	100 yr	505.00	6719.00	6720.18	6719.78	6720.23	0.007171	1.86	280.35	393.62	0.36	0.37	0.71
Main Channel-0	1010	100 yr	505.00	6718.00	6718.96		6719.02	0.008246	2.00	256.25	332.21	0.39	0.43	0.77
Main Channel-0	1009.5		Lat Struct											
Main Channel-0	1009	100 yr	505.00	6716.50	6717.80	6717.34	6717.86	0.007267	1.92	266.02	329.30	0.36	0.39	0.81
Main Channel-0	1008	100 yr	505.00	6714.70	6715.24	6715.22	6715.45	0.054239	3.64	139.41	304.56	0.91	1.69	0.46
Main Channel-0	1007	100 yr	505.00	6712.50	6713.54		6713.58	0.005047	1.68	306.71	366.97	0.31	0.29	0.84
Main Channel-0	1006	100 yr	505.00	6710.60	6711.39	6711.39	6711.67	0.063578	4.24	119.11	214.06	1.00	2.22	0.56
Main Channel-0	1005	100 yr	505.00	6708.40	6710.42		6710.45	0.002217	1.32	382.27	353.43	0.21	0.17	1.08
Main Channel-0	1004	100 yr	505.00	6706.70	6709.72		6709.81	0.009820	2.41	209.21	214.32	0.43	0.60	0.98
Main Channel-0	1003	100 yr	505.00	6704.90	6708.41		6708.53	0.007229	2.78	181.66	119.49	0.40	0.68	1.52
Main Channel-0	1002	100 yr	505.00	6704.10	6707.56		6707.66	0.004579	2.47	204.77	114.46	0.33	0.51	1.79
Main Channel-0	1001	100 yr	505.00	6704.10	6706.82		6706.89	0.005420	2.05	246.08	205.82	0.33	0.40	1.20
Main Channel-0	1000	100 yr	505.00	6702.50	6704.41	6704.41	6704.88	0.056085	5.49	92.02	101.57	1.02	3.17	0.91
Overflow 3	1007	100 yr	0.01	6717.70	6717.73	6717.73	6717.73	0.000010	0.01	1.62	70.54	0.01	0.00	0.02
Overflow 3	1006	100 yr	0.01	6716.00	6716.02	6716.02	6716.02	0.000282	0.03	0.32	15.35	0.04	0.00	0.02
Overflow 3	1005	100 yr	0.01	6714.70	6714.73	6714.73	6714.73	0.000072	0.02	0.67	35.03	0.02	0.00	0.02
Overflow 3	1004	100 yr	0.01	6712.70	6712.72	6712.72	6712.72	0.000015	0.01	1.44	74.63	0.01	0.00	0.02
Overflow 3	1003	100 yr	0.01	6709.00	6709.02	6709.02	6709.02	0.000026	0.01	1.07	53.13	0.01	0.00	0.02
Overflow 3	1001	100 yr	0.01	6705.00	6705.03	6705.03	6705.03	0.000103	0.02	0.47	19.16	0.02	0.00	0.02
Overflow 3	1000	100 yr	0.01	6702.90	6703.06		6703.06	0.000002	0.01	1.35	14.20	0.00	0.00	0.10
Main Channel-0-1	1019	100 yr	505.00	6700.60	6702.94		6703.05	0.007686	2.71	186.12	133.11	0.40	0.67	1.40
Main Channel-0-1	1018	100 yr	505.00	6699.00	6701.61		6701.75	0.009469	3.00	168.56	121.49	0.45	0.82	1.39
Main Channel-0-1	1017	100 yr	505.00	6697.80	6700.67	6699.70	6700.74	0.004788	2.09	241.29	178.67	0.32	0.40	1.35
Main Channel-0-1	1016	100 yr	505.00	6696.40	6699.67	6698.65	6699.80	0.008234	2.89	174.95	119.90	0.42	0.75	1.46
Main Channel-0-1	1015	100 yr	505.00	6694.20	6697.08		6697.56	0.032246	5.55	90.95	64.93	0.83	2.81	1.40
Main Channel-0-1	1014	100 yr	505.00	6692.20	6695.42	6694.26	6695.56	0.006596	3.09	163.60	85.75	0.39	0.78	1.91
Main Channel-0-1	1013	100 yr	505.00	6691.00	6692.71	6692.71	6693.37	0.048628	6.50	77.64	59.48	1.00	3.95	1.31
Main Channel-0-1	1012	100 yr	505.00	6687.30	6690.62		6690.70	0.003297	2.35	215.12	101.03	0.28	0.44	2.13
Main Channel-0-1	1011	100 yr	505.00	6685.40	6689.22		6689.66	0.019635	5.33	94.80	49.06	0.68	2.33	1.93
Main Channel-0-1	1010	100 yr	505.00	6683.40	6687.46		6687.68	0.008729	3.72	135.84	66.04	0.46	1.11	2.06
Main Channel-0-1	1009	100 yr	505.00	6683.00	6686.20		6686.29	0.009054	2.42		238.49	0.42	0.59	0.90
Main Channel-0-1	1008	100 yr	505.00	6683.00	6685.19		6685.25	0.005416	1.97	258.32	242.87	0.33	0.38	1.06
Main Channel-0-1	1007.5		Lat Struct											
Main Channel-0-1	1007	100 yr	495.52	6682.30	6683.83		6683.96	0.015299	2.90	170.62	184.08	0.53	0.88	0.93
Main Channel-0-1	1006	100 yr	437.50	6681.00	6682.15		6682.23	0.008346	2.23	196.24	199.56	0.40	0.51	0.98
Main Channel-0-1	1005	100 yr	364.06	6679.50	6680.71		6680.80	0.011063	2.41	151.00	168.54	0.45	0.62	0.90
Main Channel-0-1	1004	100 yr	307.49	6678.00	6679.33		6679.39	0.007656	2.04	151.03	164.90	0.38	0.44	0.92
Main Channel-0-1	1003	100 yr	282.02	6676.30	6677.25		6677.40	0.029386	3.04	92.71	152.48	0.69	1.11	0.61
Main Channel-0-1	1002	100 yr	253.89	6674.30	6675.34	6674.89	6675.39	0.006976	1.77	143.71	181.22	0.35	0.34	0.79
Main Channel-0-1	1001	100 yr	228.65	6672.30	6672.84	6672.84	6673.03	0.072944	3.42	66.87	182.58	1.00	1.66	0.37
Main Channel-0-1	1000	100 yr	212.32	6670.00	6670.46	6670.46	6670.46	0.000021	0.04	848.73	536.15	0.02	0.00	1.58
Downstream Ov	1009	100 yr	0.01	6682.70	6682.73	6682.73	6682.73	0.001427	0.06	0.16	9.47	0.08	0.00	0.02
Downstream Ov	1008	100 yr	0.01	6682.10	6682.60	6682.12	6682.60	0.000000	0.00	36.84	116.11	0.00	0.00	0.32
Downstream Ov	1007	100 yr	80.42	6680.20	6680.52	6680.52	6680.62	0.083611	2.47	32.52	160.20	0.97	1.06	0.20
Downstream Ov	1006	100 yr	196.17	6677.40	6678.05		6678.12	0.025914	2.07	94.87	253.99	0.60	0.60	0.37
Downstream Ov	1005	100 yr	224.28	6674.60	6675.42	6675.14	6675.48	0.013081	1.89	118.53	217.09	0.45	0.45	0.55
Downstream Ov	1004	100 yr	225.25	6672.20	6672.80	6672.65	6672.88	0.023526	2.26	100.02	224.82	0.59	0.68	0.44
Downstream Ov	1003	100 yr	236.39	6669.60	6670.57	6670.25	6670.62	0.010463	1.78	133.13	228.33	0.41	0.38	0.58
Downstream Ov	1002	100 yr	284.43	6667.30	6668.16	6667.98	6668.26	0.023487	2.51	113.35	210.84	0.60	0.79	0.54
Downstream Ov	1001	100 yr	292.70	6665.50	6666.30		6666.34	0.007891	1.58	187.58	345.81	0.36	0.30	0.54
Downstream Ov	1000	100 yr	292.70	6663.80	6664.73	6664.48	6664.79	0.013917	2.07	142.83	254.26	0.47	0.52	0.56

Highlighted cross sections shall be further analyzed in the Saddlehorn Filing No. 3
Final Drainage Report and CDs.

SADDLEHORN RANCH - FILING 4

LOCATED IN SECTION 3
TOWNSHIP 13 SOUTH, RANGE 64 WEST OF THE 6TH P.M.,
EL PASO COUNTY, STATE OF COLORADO

FLOODPLAIN MAP



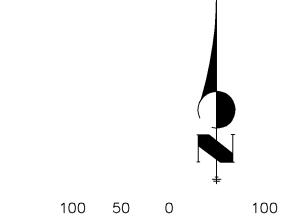
LEGEND

LIMITS OF ANALYSIS

FEMA FLOODPLAIN BOUNDARY

MODEL FLOODPLAIN BOUNDARY

PROPERTY/TRACT LINES



ORIGINAL SCALE: 1" = 100'

FLOODPLAIN MAP
SADDLEHORN RANCH — FILING 4
JOB NO. 25142.06
3/3/22
SHEET 1 OF 1



200

J-R ENGINEERING

A Westrian Company

Centennial 303-740-9393 • Colorado Springs 719-593-2593 Fort Collins 970-491-9888 • www.jrengineering.com HEC-RAS Plan: Default Scenario River: WF-R7a Reach: Geick West Fork Profile: PF# 1

Reach	River Sta	Profile	Q Total	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope	Vel Chnl	Flow Area	Top Width	Froude # Chl
			(cfs)	(ft)	(ft)	(ft)	(ft)	(ft/ft)	(ft/s)	(sq ft)	(ft)	
Geick West Fork	1001	PF# 1	1017.00	6726.00	6728.13	6728.13	6728.60	0.012973	5.96	438.12	397.94	1.16
Geick West Fork	1000 Judge Orr Up	PF# 1	1017.00	6720.00	6726.37	6721.47	6726.37	0.000004	0.26	3889.42	1111.97	0.02
Geick West Fork	999.5 Judge Orr		Culvert									
Geick West Fork	999 Judge Orr Down	PF# 1	1017.00	6719.80	6720.87	6720.52	6720.96	0.002576	2.52	403.97	529.88	0.51
Geick West Fork	998	PF# 1	1017.00	6719.40	6720.63	6720.25	6720.71	0.001945	2.30	441.84	536.92	0.45
Geick West Fork	997	PF# 1	1017.00	6719.10	6720.44	6720.04	6720.52	0.001859	2.26	450.68	545.49	0.44
Geick West Fork	996	PF# 1	1017.00	6718.80	6720.26	6719.85	6720.33	0.001676	2.17	467.93	554.33	0.42
Geick West Fork	995	PF# 1	1017.00	6718.70	6720.04	6719.72	6720.13	0.002459	2.45	414.93	547.12	0.50
Geick West Fork	994	PF# 1	1017.00	6718.40	6719.81	6719.52	6719.89	0.002406	2.18	465.67	718.13	0.48
Geick West Fork	993	PF# 1	1017.00	6717.10	6719.24	6719.13	6719.50	0.006808	4.05	251.34	335.22	0.82
Geick West Fork	992	PF# 1	1017.00	6716.50	6718.31	6718.31	6718.62	0.010988	4.47	227.47	374.18	1.01
Geick West Fork	991	PF# 1	1017.00	6715.80	6716.80	6716.80	6717.11	0.009872	4.48	227.07	343.78	0.97
Geick West Fork	990	PF# 1	1017.00	6714.10	6715.43	6715.43	6715.75	0.010075	4.54	224.20	338.15	0.98
Geick West Fork	989	PF# 1	1017.00	6711.60	6713.01	6713.01	6713.49	0.008936	5.58	182.30	184.22	0.99
Geick West Fork	988	PF# 1	1017.00	6710.50	6711.92	6711.85	6712.30	0.007314	4.93	206.25	215.85	0.89
Geick West Fork	987	PF# 1	1017.00	6709.70	6711.08	6711.08	6711.37	0.011058	4.35	233.78	402.60	1.01
Geick West Fork	986	PF# 1	1017.00	6709.10	6710.03	6710.03	6710.29	0.011722	4.15	245.02	473.01	1.02
Geick West Fork	985	PF# 1	1017.00	6707.90	6708.96	6708.77	6709.06	0.003673	2.57	396.30	659.07	0.58
Geick West Fork	984	PF# 1	1017.00	6707.50	6708.46		6708.60	0.006037	2.99	340.66	655.36	0.73
Geick West Fork	983	PF# 1	1017.00	6706.20	6707.48	6707.48	6707.81	0.010728	4.60	221.33	343.22	1.01
Geick West Fork	982	PF# 1	1017.00	6705.00	6706.55		6706.86	0.007584	4.48	226.93	281.65	0.88
Geick West Fork	981	PF# 1	1017.00	6703.90	6705.78	6705.69	6706.09	0.007768	4.47	227.46	288.41	0.89
Geick West Fork	980	PF# 1	1017.00	6703.30	6704.76	6704.76	6705.20	0.009771	5.33	190.89	221.02	1.01
Geick West Fork	979	PF# 1	1017.00	6700.90	6702.85	6702.83	6703.33	0.008365	5.60	181.64	173.74	0.97
Geick West Fork	978	PF# 1	1017.00	6700.20	6702.59	6702.12	6702.81	0.003102	3.74	271.90	226.33	0.60
Geick West Fork	977	PF# 1	1017.00	6700.20	6701.81	6701.81	6702.25	0.009728	5.35	190.07	217.93	1.01
Geick West Fork	976	PF# 1	1017.00	6697.60	6700.61	6700.61	6701.16	0.008512	5.96	170.59	150.32	0.99
Geick West Fork	975	PF# 1	1017.00	6696.00	6698.99	6698.99	6699.80	0.007457	7.21	141.14	84.57	0.98
Geick West Fork	974	PF# 1	1017.00	6695.20	6698.07	6698.07	6698.78	0.007976	6.74	150.91	105.32	0.99
Geick West Fork	973	PF# 1	1017.00	6692.00	6695.85	6695.85	6696.94	0.006901	8.40	121.05	53.73	0.99
Geick West Fork	972	PF# 1	1017.00	6691.00	6695.63	6694.53	6695.92	0.002960	4.30	236.97	163.36	0.61
Geick West Fork	971	PF# 1	1017.00	6692.00	6695.17	6695.17	6695.46	0.008554	4.44	381.90	519.60	0.92
Geick West Fork	970	PF# 1	1017.00	6690.00	6693.86	6693.58	6694.08	0.003757	3.80	413.50	498.11	0.65
Geick West Fork	969	PF# 1	1017.00	6690.30	6693.04	6693.04	6693.50	0.009005	5.45	186.44	195.90	0.99
Geick West Fork	968	PF# 1	1017.00	6685.70	6689.07	6689.07	6690.21	0.006986	8.59	118.37	51.34	1.00

Provide map showing where cross sections are in relation to channel & proposed development. Include 100-year water surface on map. Provide HEC-RAS input data as well as channel cross sections.

JR Response: BFE's were recieved for Drainageway WF-R7a from El Paso CO Floodplain manager. Data from our analysis has been removed from this report. Highlighted values are where FR #'s exceed the 0.90 criteria. Address what will be done to mitigate this within the channel.

APPENDIX F DRAINAGE MAPS & PLANS

