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Préliminary Drainage Report 4-Way Commercial El Paso County, Colorado

Final

September 2023 HR Green Project No: 2202654

Prepared For:

KO1515 Developments, LLC. PO Box 1385 Colorado Springs, CO 80901

Prepared By:

HR Green Development, LLC Contact: Colleen Monahan, PE cmonahan@hrgreen.com (719) 394-2433

PCD File No. TBD

PPR2347



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Note: additional comments will be provided on additional information needed with the next review



Engineer's Statement

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the County for drainage reports and said report is in conformity with the applicable master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.

Date

Colleen	Monahan	PF
Concert	wonanan,	

State of Colorado No.

For and on behalf of HR Green Development, LLC

Owner/Developer's Statement

I, the owner/developer have read and will comply with all of the requirements specified in this drainage report and plan.

By:

Address: KO1515, LLC PO Box 1385

Colorado Springs, CO 80903

El Paso County Statement

Filed in accordance with the requirements of the Drainage Criteria Manual, Volumes 1 and 2, El Paso County Engineering Criteria Manual and Land Development code, as amended.

Joshua Palmer, P.E.

County Engineer/ECM Administrator

Conditions:

Date

Date



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I. General Purpose, Location and Description

a. Purpose

The purpose of this Preliminary Drainage Report (PDR) for 4-Way Commercial is to describe onsite and offsite drainage patterns, size drainage and temporary erosion control measures to safely capture and convey stormwater runoff to temporary sediment basins during the initial phase of grading of designated areas of the site, size preliminary stormwater infrastructure and permanent control measures, and to safely route treated stormwater to adequate outfalls.

b. Location

The site lies within a part of the Southwest Quarter of Section 28 and the Northwest Quarter of Section 33, Township 12 South, Range 64 West of the 6th P.M., El Paso County, Colorado. The site is bound to the north by undeveloped unplatted land, to the east by State Highway 24 and land zoned A-35, to the west by 2.5-acre single-family properties that are part of 4-Way Ranch Filing No. 1, and to the south by land zoned A-35. A vicinity map is presented in Appendix A.

The overall 4-Way 67.1-acre property contains two tracts that are bisected by Stapleton Drive, with approximately 15.5 acres located north of Stapleton Drive and 51.6 acres south of Stapleton Drive. All of the property to the north (15.5 acres) and approximately 16.5 acres of the southern property will be portioned off for Overlot grading, with the southernmost part of the southern tract being developed with 2 warehouses, storage containers, and parking for trailer (approximately 32 acres total). The proposed improvements shown in the preliminary drainage plan (approximately 16.5 acres disturbed area) are on the southern area of the property, are referred to as 'the site' herein. The remaining area of the property will remain undeveloped.

c. Description of Property

The site that is being portioned off for Overlot grading contains 32 acres within two tracts that are bisected by Stapleton Drive. Both are currently undeveloped and unplatted with Commercial zoning. Stapleton Drive has its own storm sewer and stormwater detention ponds that are located on the overall 4-way property. One detention pond is located partially within 'the site' in the southwest corner of Stapleton Drive and Highway 24. Part of the site also drains into this detention pond. ______ except for the drainageway?

All of the property to the north (15.5 acres) and about 16.5 acres of the southern property will be portioned off for Overlot grading with the southernmost part of the southern tract being developed with 2 warehouses, storage containers, and parking for trailer (approximately 32 acres total) and are included in this project, referred to as 'the site' herein. The remaining 35.6 acres of the south tract will remain undeveloped. A total of 32 acres are expected to be disturbed during the Overlot grading phase, and 8 acres for the commercial development on the property.

The site lies within the Geick Ranch drainage basin and is tributary to Black Squirrel Creek. An unnamed tributary runs north-south through the southern tract and forms the west boundary of 'the site'. The portion of the site located east of this tributary drains southerly and easterly partially into this tributary, partially into a detention pond that provides treatment for Stapleton Drive, and partially into a swale that runs along the west side of Highway 24. The flows combine just south of the site where they flow easterly under Highway 24.

A second unnamed tributary traverses the northern boundary of the northern tract, and all initial grading will occur south of this tributary. Stormwater in this tract generally drains from west to east into the tributary or into the easterly adjacent property zoned A-35.

_ clarify and describe facilities under HWY 24



address capacities, - adequacy of the existing culverts

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There is existing stormwater infrastructure on the site from Stapleton Drive storm sewer. There are existing culverts for stormwater crossings under an existing dirt road that leads to an existing 1-story wood frame building and water well site that is located on the remaining undeveloped part of the 4-Way property. There is an existing overhead electric line that crosses the southern part of the property.

Existing vegetation and soils were determined from in-person field site visits and existing aerial inspection from Google Earth and the United States Department of Agriculture Natural Resources Conservation Service (NRCS) Web Soil Survey. The site currently contains vegetation consisting primarily of native grasses and weeds. Existing vegetation is estimated at 25% density by visual inspection during the in-person field site visit.

Per a NRCS web soil survey, the site's soil is comprised of Type A soils: Blakeland loamy sand and Columbine gravelly sandy loam, Type B soil Stapleton sandy loam. A NRCS soil survey is presented in Appendix A.

Existing topography within the site ranges from about 3% up to 10%.

d. Floodplain Statement

The westerly portion of the overall 4-Way property lies within a designated FEMA floodplain as determined by the flood insurance map panel '08041C0552G' effective date December 7, 2018. This part of the overall 4-Way property will remain undeveloped. The remainder of the overall 4-Way property including 'the site' for overlot grading is located outside of the floodplain, in Zone X, as shown on flood insurance map panels '08041C0552G' '08041C0556G' and '08041C0558G' effective date December 7, 2018. Zone X are areas determined to be outside the 0.2% annual chance flood. The Refer to Appendix A for Firmette.

Add a statement that the calculated 100-year floodplain for the drainageway within the north parcel is shown on all development plans II. Drainage Design Criteria

a. Drainage Criteria

Hydrologic data and calculations were performed using the El Paso County Drainage Criteria Manual Volume 1 & 2 (EPCDCM), with current revisions.

Onsite drainage improvements are designed for the 5-year storm (minor event) and 100-year storm (major event) using rainfall values from the NOAA Atlas 14 Point Precipitation Frequency Data Server. Runoff was calculated per CCSDCM Section 6.3.0 - Rational Method. Full spectrum pond design is to be completed in a future Final Drainage Report (FDR) for the fully developed proposed conditions using the latest version of Mile High Flood District's (MHFD) UD-Detention per CCSDCM Section 13.3.2.1. The detention pond allowable release rate will be limited to less than historic rates. Proposed private storm sewer calculations will be provided with the FDR and will be calculated in accordance with County criteria.

Rainfall Depths per NOAA Atlas 14						
Return Period (yr)	5	100				
1-hr Rainfall Depth (in)	1.22	2.51				



III. Drainage Basins and Subbasins

a. Previous Drainage Studies <

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please provide EDARP File #'s for all references (if/when applicable) so that they can be more easily referenced.

The site lies within the Geick Ranch drainage basin and is tributary to Black Squirrel Creek. The site's drainage characteristics were previously studied in the following reports:

1. "Final Drainage Report for 4 Way Ranch- Filing No. 1" prepared by JR Engineering, revised March 2006.

2. "Master Development Drainage Plan for 4-Way Ranch Phase 1" prepared by Associated Design Professionals, Inc, January 2012.

3. "MDDP Amendment/Preliminary Drainage Report for 4-Way Ranch Commercial" prepared by JR Engineering, revised February 2010.

4. "MDDP Amendment/Preliminary/Final Drainage Report for Stapleton Drive from Bandanero Drive to US Hwy 24' prepared by JR Engineering, revised May 2010.

6. Gieck Ranch Drainage Basin Planning Study (DBPS), 2008.

b. Major Basin Description

Gieck Ranch Drainage Basin is a 22.05 square mile watershed located in El Paso County, Colorado. Gieck Ranch Drainage Basin begins approximately five miles northeast of the Town of Falcon and travels approximately 15 miles to the southeast. It is tributary to Black Squirrel Creek which drains to the Arkansas River near the city of Pueblo, Colorado. The majority of the basin is undeveloped and is rolling range land typical of Colorado's semi-arid climates. Anticipated land use for the basin includes residential, industrial, agricultural, and commercial development.

c. Existing Subbasin Description

The existing conditions hydrology is shown on an Existing Conditions Drainage Map within Appendix D. The map and supporting calculations quantify the stormwater runoff per historical conditions prior to overlot grading permit disturbance. The existing conditions were analyzed in the MDDP Amendment/Preliminary/Final Drainage Report for Stapleton Drive from Bandanero Drive to US Hwy 24 prepared by JR Engineering, revised May 2010. This report described the improvements for the construction of Stapleton Drive which has since been completed.

South Tract:

Runoff within the south tract flows generally from a northwest to southeast direction where flows will eventually combine and pass underneath Highway 24 at one of its existing major crossings. As stated in the approved MDDP referenced above, these crossings are adequately sized for the existing Stapleton Drive and drainage improvements that were put in place as part of that construction. With future on-site drainage improvements releasing at or below the 100-year historic flow rate, these crossings will remain satisfactory.

Basin D is 16.83 acres of undeveloped area on-site. This basin generally drains from the northwest to the southeast via sheet flow to (2) existing public 26" CMP culverts under US HWY 24 at DP1 (DBPS 4 per the MDDP Amendment/Preliminary/Final Drainage Report for Stapleton Drive from Bandanero Drive to US Hwy



see drainage plan comments. Sub-basins will be reviewed with the additional information on the next review

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24). The calculated stormwater runoff generated from this basin is $Q_5 = 4.3$ cfs $Q_{100} = 31.3$ cfs in the minor and major storms. The calculated runoff flows in this report are higher than those in the "MDDP Amendment/Preliminary/Final Drainage Report for Stapleton Drive from Bandanero Drive to US Hwy 24' prepared by JR Engineering, revised May 2010" due to higher curve numbers for lawn areas specified in current criteria.

pasture/meadow?

Basin E is 9.64 acres of undeveloped area on-site. This basin generally drains from the north to the south via sheet flow to (2) existing public 26" CMP culverts under US HWY 24 at DP1 (DBPS 4 per the MDDP Amendment/Preliminary/Final Drainage Report for Stapleton Drive from Bandanero Drive to US Hwy 24). The calculated stormwater runoff generated from this basin is $Q_5 = 2.5$ cfs $Q_{100} = 18.2$ cfs in the minor and major storms. The calculated runoff flows in this report are higher than those in the "MDDP Amendment/Preliminary/Final Drainage Report for Stapleton Drive from Bandanero Drive to US Hwy 24' prepared by JR Engineering, revised May 2010" due to higher curve numbers for lawn areas specified in Discuss in greater detail in this Section or in current criteria.

Final Grading Conditions below.

Basin F is 5.83 acres of undeveloped area on-site. This basin generally drains from the northwest to the southeast via sheet flow to an existing temporary sediment and detention basin on the northwest side of US HWY 24. The calculated stormwater runoff generated from this basin is $Q_5 = 2.6$ cfs $Q_{100} = 13.5$ cfs in the minor and major storms. The calculated runoff flows in this report are higher than those in the "MDDP Amendment/Preliminary/Final Drainage Report for Stapleton Drive from Bandanero Drive to US Hwy 24' prepared by JR Engineering, revised May 2010" due to higher curve numbers for lawn areas specified in current criteria

North Tract:

Runoff within the north tract generally flows from west to east to the unnamed tributary bordering the north of this tract or into the adjacent lot to the east.

Basin NT1 is 1.45 acres of undeveloped area on the north edge of the north tract. This basin generally drains from the southwest to the northeast via sheet flow to an unnamed drainage channel on the north edge of the site. The unnamed channel drains to a public box culvert under US HWY 24 at DP2 (DBPS 5 per the MDDP Amendment/Preliminary/Final Drainage Report for Stapleton Drive from Bandanero Drive to US Hwy 24). The calculated stormwater runoff generated from this basin is $Q_5 = 0.5$ cfs $Q_{100} = 3.4$ cfs in the minor and major storms.

Basin NT2 is 10.65 acres of undeveloped area on the north tract. This basin generally drains from the west to the east via sheet flow/channelized flow to the east edge of the north tract area. Ultimately draining to the public box culvert under US HWY 24 at DP2 (DBPS 5 per the MDDP Amendment/Preliminary/Final Drainage Report for Stapleton Drive from Bandanero Drive to US Hwy 24). The calculated stormwater runoff generated from this basin is $Q_5 = 2.8$ cfs $Q_{100} = 20.8$ cfs in the minor and major storms.

Basin NT3 is 0.87 acres of undeveloped area on the south edge of the north tract. This basin generally drains from the northwest to the southeast via sheet flow onto the north side of Stapleton Drive. Ultimately draining to a public curb inlet near the intersection of Stapleton Dr and US HWY 24. Surface runoff captured by the public curb inlet drains through a series of public 24" RCP storm sewer pipes into an existing temporary sediment and detention basin on the northwest side of US HWY 24. The calculated stormwater runoff generated from this basin is $Q_5 = 0.3$ cfs $Q_{100} = 2.3$ cfs in the minor and major storms.

d. Final Grading Conditions

Within each basin paragraph, discuss how WQ treatment is achieved (or excluded if applicable) for each basin and/or parts of each basin.



Revise drainage map to match this. Drainage map shows all ponds as TSBs.

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The final grading conditions hydrology is shown on the Final Drainage Map within the Appendix. The map and supporting calculations quantify the stormwater runoff per final grading conditions which includes disturbance of particular areas of the site for paved roadway corridors, paved parking areas, the construction of two warehouses, a future commercial development area, and full spectrum detention pond

During final grading operations, runoff from the developed area of the site will be captured in sump inlets and conveyed into full spectrum detention Pond B. Runoff in the northern tract will remain as proposed in the overlot grading conditions and drain to a temporary sediment basin. The remaining area of the southern tract will remain undisturbed and will flow offsite based on historic drainage patterns.

North Tract

The GEC Plan states that it will have 1 column of 2 orifices at 3/4" dia. Revise to remove discrepancy.

Basin TSA is the northern portion of the site that is 11.46 acres in total with 11.46 acres disturbed as a part of overlot grading. This basin drains generally from the northeast to the southwest to Temporary Sediment Basin A (TSB A) at DP4. TSB A is designed to treat a tributary area of 11.46 acres with a disturbed area of 11.46 acres. The required volume of TSB A is 0.47 ac-ft below the spillway crest elevation. TSB A exceeds this with a provided volume of 1.27 ac-ft. TSB A is designed to drain its entire volume within 40 hours via a temporary outlet structure. This temporary outlet structure was designed as a singular column with five 1" dia holes allowing for water to drain. Outflows from TSB 1 will be restricted to 20.7 cfs in order to limit flows to its ultimate design point (DP2) at or less than historic values. Sediment basin design is per Table SB-1 SWENT Drawing No. 900-TSB-2. The sediment basin is owned and maintained by the Owner/Developer and is to remain in place until interim and final phases construct permanent full spectrum detention Pond A. The calculated stormwater runoff generated from this basin is $Q_5 = 3.1$ cfs $Q_{100} = 13.5$ cfs in the minor and major storms

Basin PNT1 is 0.13 acres of undeveloped area on-site and a small disturbed area from the proposed overlot grading improvements in the north tract. This subbasin represents the existing subbasin "NT1" under the proposed overlot grading conditions. There is no additional proposed impervious area proposed in this basin at the time of this report. This basin will maintain existing drainage patterns, while reducing the total peak flow drainage from existing conditions to its outfall location. This basin generally drains from the southwest to the northeast via sheet flow to an unnamed drainage channel on the north edge of the site. The unnamed channel drains to a public box culvert under US HWY 24 at DP2 (DBPS 5 per the MDDP Amendment/Preliminary/Final Drainage Report for Stapleton Drive from Bandanero Drive to US Hwy 24). The calculated stormwater runoff generated from this basin is $Q_5 = 0.04$ cfs $Q_{100} = 0.3$ cfs in the minor and major storms.

Basin PNT2 is 0.87 acres of undeveloped area on-site and a small disturbed area from the proposed overlot grading improvements in the north tract. This subbasin represents the existing subbasin "NT2" under the proposed overlot grading conditions. There is no additional proposed impervious area proposed in this basin at the time of this report. This basin will maintain existing drainage patterns, while reducing the total peak flow drainage from existing conditions to its outfall location. This basin generally drains from the west to the east via sheet flow/channelized flow to the east edge of the north tract area. Ultimately draining to the public box culvert under US HWY 24 at DP2 (DBPS 5 per the MDDP Amendment/Preliminary/Final Drainage Report for Stapleton Drive from Bandanero Drive to US Hwy 24). The calculated stormwater runoff generated from this basin is $Q_5 = 0.2$ cfs $Q_{100} = 1.7$ cfs in the minor and major storms.

Basin PNT3 is 0.56 acres of undeveloped area on-site and a small disturbed area from the proposed overlot grading improvements in the north tract. This subbasin represents the existing subbasin "NT3" under the



proposed overlot grading conditions. There is no additional proposed impervious area proposed in this basin at the time of this report. This basin will maintain existing drainage patterns, while reducing the total peak flow drainage from existing conditions to its outfall location. This basin generally drains from the northwest to the southeast via sheet flow onto the north side of Stapleton Drive. Ultimately draining to a public curb inlet near the intersection of Stapleton Dr and US HWY 24. Surface runoff captured by the public curb inlet drains through a series of public 24" RCP storm sewer pipes into an existing temporary sediment and detention basin on the northwest side of US HWY 24. The calculated stormwater runoff generated from this basin is Q_5 = 0.2 cfs Q_{100} = 1.4 cfs in the minor and major storms.

South Tract

Basin P1.1 is 0.78 acres of paved roadway. Stormwater ($Q_5 = 3.1$ cfs $Q_{100} = 5.6$ cfs) is captured at DP3.1 in a private 3' Type C sump inlet and is conveyed through a private 15" HDPE to DP3.2

Basin P1.2 is 0.26 acres of paved roadway. Stormwater ($Q_5 = 1.1$ cfs $Q_{100} = 2.0$ cfs) is captured at DP3.2 in a private 5' Type R sump inlet and is conveyed through a private 18" HDPE to DP3.3

Basin P1.3 is 0.4 acres of paved area and 0.19 acres of lawn area. Stormwater ($Q_5 = 1.9$ cfs $Q_{100} = 3.9$ cfs) is captured at DP3.3 in a private 5' Type R sump inlet and is conveyed through a private 18" HDPE to DP3.4

Basin P1.4 is 0.95 acres of paved area and 0.28 acres of roof area. Stormwater ($Q_5 = 5.5$ cfs $Q_{100} = 9.9$ cfs) is captured at DP3.4 in a private 5' Type R sump inlet and is conveyed through a private 24" HDPE to DP3.5

Basin P1.5 is 0.64 acres of paved area. Stormwater ($Q_5 = 3.0 \text{ cfs } Q_{100} = 5.3 \text{ cfs}$) is captured at DP3.1 in a private 5' Type R sump inlet and is conveyed through a private 24" HDPE to Pond B at DP3.12.

Basin P1.6A is 2.72 acres of undeveloped area. This area is designated to be a commercial site at a future date. Stormwater (Interim $Q_5 = 0.8$ cfs Interim $Q_{100} = 5.9$ cfs) is captured in a private stormsewer system to be connected to a private 30" HDPE stub at the western edge of the future development area. Flows are then conveyed to DP3.6. The stormwater flows from this basin after the build out of the future commercial site would be $Q_5 = 10.2$ cfs and $Q_{100} = 17.1$ cfs.

Basin P1.6B is 0.45 acres of paved area and 0.28 acres of roof area. Stormwater ($Q_5 = 3.1$ cfs $Q_{100} = 5.7$ cfs) is captured at DP3.6 in a private 5' Type R sump inlet and is conveyed through a private 30" HDPE to DP3.8

Basin P1.7A is 1.72 acres of undeveloped area. This area is designated to be a commercial site at a future date. Stormwater (Interim $Q_5 = 0.5$ cfs Interim $Q_{100} = 3.9$ cfs) is captured in a private 24" HDPE to be connected to a future stormwater system. Flows are then conveyed to DP3.7. The stormwater flows from this basin after the build out of the future commercial site would be $Q_5 = 6.3$ cfs and $Q_{100} = 10.6$ cfs.

Basin P1.7B is 0.31 acres of paved area and 0.28 acres of roof area. Stormwater ($Q_5 = 3.1$ cfs $Q_{100} = 5.7$ cfs) is captured at DP3.6 in a private 5' Type R sump inlet and is conveyed through a private 24" HDPE to DP3.9

Basin P1.8 is 0.76 acres of paved area. Stormwater ($Q_5 = 3.2$ cfs $Q_{100} = 5.7$ cfs) is captured at DP3.10 in a private 5' Type R sump inlet and is conveyed through a private 18" HDPE to DP3.11

Basin P1.9 is 0.20 acres of paved area. Stormwater ($Q_5 = 0.9$ cfs $Q_{100} = 1.7$ cfs) is captured at DP3.8 in a private a Duraslott XL trench drain and is conveyed to DP3.9

Basin P1.10 is 0.85 acres of paved area, 1.28 acres of lawn area, and 0.28 acres of roof area. Stormwater ($Q_5 = 5.5$ cfs $Q_{100} = 12.8$ cfs) is conveyed through sheet flow to Pond B at DP3.12



Basin PD is 14.99 acres of undeveloped area on-site and a small disturbed area from the proposed overlot grading improvements. Basin PD will not be disturbed past overlot grading conditions and will follow historic drainage patterns.

Basin PE is 2.56 acres of undeveloped area on-site and a small disturbed area from the proposed overlot grading improvements. Basin PE will not be disturbed past overlot grading conditions and will follow historic drainage patterns.

Basin PF is 2.73 acres of undeveloped area on-site and a small disturbed area from the proposed overlot grading improvements. Basin PF will not be disturbed past overlot grading conditions and will follow historic drainage patterns.

See Table 1 below for proposed TSB parameters. Table 1: TSB Summary these trees the second se

See my comment on the Proposed Drainage Map about summarizing WQ treatment more thoroughly. Adding to these tables would be acceptable.

Tributary Sub-Basin	Sediment Basin Name	Tributary Acres	Required Detention Volume below spillway crest (ac-ft)	Provided Volume up to spillway crest (ac-ft)	Total Provided Volume (ac-ft)
TSA	TSB A	11.46	0.47	0.95	1.27
TSB	TSB B	12.48	0.52	3.58	5.22

See Table 2 below for proposed full spectrum detention pond parameters.

Table 2: Pond Summary

Tributary Sub-Basin	Pond Name	Tributary Acres	Required Detention Volume (ac-ft)	Provided Volume (ac-ft)	Release Rate (cfs)
Basins P1.1- 1.11	Pond B	12.45	1.969	4.652	6

IV. Drainage Facility Design

See my comment about TSBs on the Drainage Map below.

a. General Concept

The drainage facilities for the overlot grading conditions will consist of the Temporary Sediment Basins (TSBs) only. The designed TSBs will be constructed in the area of future permanent detention ponds A and B which will be constructed at time of development of the commercial properties. The temporary sediment basins will not include construction of the inflow forebay, concrete trickle channel, the lower maintenance paths at the bottom of pond, and outlet structures with outlet pipes. Stormwater flows will be allowed to overtop the edge of the TSBs and flow through interim swales to historic drainage ways. Water volume in the pond will also infiltrate into the soil. The described natural release structure for each TSB will meet the minimum 40-hour drain/release time of storm water runoff from the property. Once the project progresses past this overlot grading phase, both TSB A and TSB B will be converted to full spectrum detention ponds. The final pond improvement for Pond B has been designed and will be constructed with the initial phase of

The GEC Plan and Drainage Map show the construction of two buildings and whatever the many rectangles around the buildings are (are those the storage containers?), which is more than just overlot grading. So this text does not match what is shown as proposed on those plans. Please revise as needed to remove discrepancies.



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initial

development described in this report. Further design details and improvements will be described in the FRD. Pond A will be designed at a later phase of development.

b. Water Quality & Detention

Water Quality is to be provided via future ponds A and B as a part of the interim and final phases of construction. As explained in earlier sections, Temporary Sediment Basins located at the future detention pond locations and constructed with similar basin geometry are to be implemented at the Overlot grading stage.

Water quality and full spectrum detention has been provided in Pond B.

c. Inspection and Maintenance

The private full spectrum detention ponds are to be owned and maintained by a metropolitan district, to be established with the project. Maintenance access for the full spectrum detention facilities will be provided through private drainage easements and tracts. The TSB's in Tracts A and B for the overlot grading phase are owned and maintained by the Owner or its assigns until the time of the full spectrum detention ponds.

V. Four Step Method to Minimize Adverse Impacts of Urbanization _____ this is not consistent with the site design

Step 1 – Reducing Runoff Volumes: Low impact development (LID) practices are utilized to reduce runoff at the source. In general, stormwater discharges are routed across pervious areas prior to capture in diversion ditches constructed at the Overlot grading stage. This practice promotes infiltration and reduces peak runoff rates. LID practices will also be utilized in future phases of development through the use of grass swales, and buffers.

Step 2 – Treat and slowly release the WQCV: This step utilizes full spectrum water quality and detention to capture the WQCV and slowly release runoff from the site. **Onsite full spectrum detention ponds** provide water quality treatment for the site. The WQCV is released over a period of 40 hours. Proposed and future ponds will provide full spectrum detention for improvements.

Step 3 – Stabilize stream channels: This step establishes practices to stabilize drainageways and provide scour protection at stormwater outfalls. There are no major drainageways affected by the Overlot grading of the commercial development phase of the development. No improvements to any downstream drainageways are required or anticipated at this time. Diversion ditches and swales are utilized to convey stormwater and sediment runoff to the temporary sediment basins. These are considered stabilized control measures.

Step 4 – Consider the need for source controls: Source controls are provided for the proposed initial development phase and the commercial development phase and are discussed in the Stormwater Management Report for this project.

provide the required analysis



\$50k is shown in the FAE for a PBMP. Remove from FAE or provide an itemized breakdown of that item here.

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VI. Opinion of Probable Cost

An engineer's opinion of probable cost is presented will be provided with a Final Drainage Report at time of development.

VII. Erosion Control Plan

The El Paso County Drainage Criteria Manual specifies an Erosion Control Plan and associated cost estimate must be submitted since this project is disturbing more than 1 acre. The Erosion Control Plan for 4-Way Commercial and for the initial phase of development have been submitted concurrently with this report.

VIII. Drainage and Bridge Fees — a site development plan

Drainage and Bridge Fees are not due with the preliminary drainage report. An estimate of basin fees for the proposed development will be calculated and provided with the FDR.

IX. Summary _____ delete - this is the FDR _____

The Preliminary Drainage Report discusses the site conditions at the time of initial overlot disturbance which includes preliminary undercut earthwork of the roadway corridors as well as the implementation of diversion ditches and temporary sediment basins as control measures for eros on and sediment control prior to interim and final construction phases. This report also discusses the preliminary development for the site and additional detail will be provided in the FDR. The proposed improvements will not adversely affect the offsite major drainageways or surrounding development. PBMPs are required on the south side

The basins will be owned and maintained by the Owner/Developer until such time that future construction of the permanent control measures will be owned and maintained by a Metropolitan District to be established with the project. All drainage facilities were sized per the El Paso County Drainage Criteria Manuals which include standards and details from the Mile High Flood District.

X. References

- 1. City of Colorado Springs Drainage Criteria Manual, May 2014, Revised January 2021.
- 2. Drainage Criteria Manual of El Paso, Colorado, October 2018.
- 3. Urban Storm Drainage Criteria Manual, Urban Drainage Flood Control District, January 2018.

XI. Drawings

Please refer to the appendices for vicinity and drainage basin maps.



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APPENDIX A - VICINITY MAP, SOIL MAP, FEMA MAP



National Flood Hazard Layer FIRMette



Legend

104°34'13"W 38°58'17"N SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT Without Base Flood Elevation (BFE) Zone A. V. A9 With BFE or Depth Zone AE, AO, AH, VE, AR SPECIAL FLOOD HAZARD AREAS **Regulatory Floodway** 0.2% Annual Chance Flood Hazard, Areas of 1% annual chance flood with average T12S R64W S028 depth less than one foot or with drainage areas of less than one square mile Zone X Future Conditions 1% Annual Chance Flood Hazard Zone X Area with Reduced Flood Risk due to 08041C0552G 08041C0556G Levee. See Notes. Zone X OTHER AREAS OF FLOOD HAZARD Area with Flood Risk due to Levee Zone D eff. 12/7/2018 еп. 12/7/2018 NO SCREEN Area of Minimal Flood Hazard Zone X Effective LOMRs OTHER AREAS Area of Undetermined Flood Hazard Zone D - — – – Channel, Culvert, or Storm Sewer GENERAL STRUCTURES LIIII Levee, Dike, or Floodwall AREAOFMINIMAL FLOOD HAZARD 20.2 Cross Sections with 1% Annual Chance 17.5 Water Surface Elevation ELPASO COUNTRY **Coastal Transect** Mase Flood Elevation Line (BFE) 080059 Limit of Study Jurisdiction Boundary **Coastal Transect Baseline** OTHER Profile Baseline FEATURES Hydrographic Feature **Digital Data Available** T12S R64W S033 No Digital Data Available MAP PANELS Unmapped The pin displayed on the map is an approximate point selected by the user and does not represent 08041C0554G 08041C0558G an authoritative property location. Zone A eff. 12/7/2018 /2018 This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The basemap shown complies with FEMA's basemap accuracy standards 65188FEFF Zone A The flood hazard information is derived directly from the authoritative NFHL web services provided by FEMA. This map was exported on 11/7/2022 at 6:05 PM and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or become superseded by new data over time. This map image is void if the one or more of the following map elements do not appear: basemap imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for 104°33'35"W 38°57'49"N Feet 1:6.000 unmapped and unmodernized areas cannot be used for regulatory purposes. 250 500 1,000 1,500 2.000 n

Basemap: USGS National Map: Orthoimagery: Data refreshed October, 2020



USDA Natural Resources

Conservation Service

8/31/2023 Page 1 of 4



		P		
Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
8	Blakeland loamy sand, 1 to 9 percent slopes	A	3.8	1
19	Columbine gravelly	А	212.8	77

в

Hydrologic Soil Group

percent slopes

Stapleton sandy loam, 3

to 8 percent slopes

Description

Totals for Area of Interest

83

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

1.4%

77.0%

21.6%

100.0%

59.8

276.4

Rating Options

Aggregation Method: Dominant Condition Component Percent Cutoff: None Specified Tie-break Rule: Higher





4-Way Commercial Early Grading Drainage Report Project No: 2202654

APPENDIX B – HYDROLOGIC CALCULATIONS

Precipitation Frequency Data Server

NOAA Atlas 14, Volume 8, Version 2 Location name: Peyton, Colorado, USA* Latitude: 38.968°, Longitude: -104.565° Elevation: 6900 ft** * source: ESRI Maps ** source: USGS



POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Deborah Martin, Sandra Pavlovic, Ishani Roy, Michael St. Laurent, Carl Trypaluk, Dale Unruh, Michael Yekta, Geoffery Bonnin

NOAA, National Weather Service, Silver Spring, Maryland

PF_tabular | PF_graphical | Maps_&_aerials

PF tabular

PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches) ¹											
Duration				Average	recurrence	interval (ye	ars)				
Duration	1	2	5	10	25	50	100	200	500	1000	
5-min	0.239 (0.190-0.302)	0.291 (0.232-0.368)	0.381 (0.302-0.484)	0.461 (0.363-0.587)	0.577 (0.442-0.767)	0.672 (0.502-0.903)	0.771 (0.557-1.06)	0.877 (0.607-1.24)	1.02 (0.682-1.48)	1.14 (0.738-1.67)	
10-min	0.350 (0.278-0.442)	0.426 (0.339-0.539)	0.559 (0.443-0.709)	0.675 (0.532-0.860)	0.845 (0.648-1.12)	0.984 (0.735-1.32)	1.13 (0.815-1.55)	1.28 (0.889-1.81)	1.50 (0.998-2.17)	1.67 (1.08-2.44)	
15-min	0.426 (0.340-0.539)	0.520 (0.414-0.658)	0.681 (0.540-0.864)	0.823 (0.649-1.05)	1.03 (0.790-1.37)	1.20 (0.897-1.61)	1.38 (0.994-1.89)	1.57 (1.08-2.21)	1.83 (1.22-2.65)	2.04 (1.32-2.98)	
30-min	0.609 (0.485-0.770)	0.742 (0.590-0.939)	0.971 (0.770-1.23)	1.17 (0.924-1.49)	1.46 (1.12-1.94)	1.70 (1.27-2.29)	1.95 (1.41-2.68)	2.22 (1.54-3.13)	2.59 (1.72-3.74)	2.88 (1.86-4.21)	
60-min	0.779 (0.620-0.985)	0.936 (0.745-1.18)	1.22 (0.964-1.54)	1.47 (1.16-1.87)	1.85 (1.42-2.47)	2.17 (1.62-2.92)	2.51 (1.81-3.46)	2.87 (1.99-4.07)	3.39 (2.26-4.92)	3.81 (2.47-5.57)	
2-hr	0.948 (0.761-1.19)	1.13 (0.906-1.42)	1.46 (1.17-1.84)	1.77 (1.40-2.23)	2.24 (1.74-2.97)	2.63 (1.99-3.53)	3.06 (2.24-4.20)	3.53 (2.47-4.97)	4.20 (2.83-6.06)	4.74 (3.10-6.89)	
3-hr	1.04 (0.838-1.30)	1.23 (0.987-1.53)	1.57 (1.26-1.97)	1.91 (1.52-2.40)	2.42 (1.90-3.22)	2.87 (2.19-3.85)	3.37 (2.48-4.62)	3.91 (2.76-5.50)	4.70 (3.18-6.77)	5.34 (3.50-7.73)	
6-hr	1.20 (0.977-1.49)	1.40 (1.14-1.74)	1.79 (1.45-2.22)	2.16 (1.74-2.70)	2.77 (2.19-3.67)	3.30 (2.54-4.40)	3.88 (2.88-5.30)	4.54 (3.23-6.35)	5.49 (3.76-7.88)	6.28 (4.16-9.04)	
12-hr	1.39 (1.14-1.70)	1.62 (1.32-1.98)	2.06 (1.68-2.53)	2.48 (2.01-3.07)	3.16 (2.52-4.14)	3.75 (2.91-4.96)	4.41 (3.30-5.96)	5.13 (3.69-7.13)	6.19 (4.28-8.82)	7.07 (4.72-10.1)	
24-hr	1.60 (1.32-1.94)	1.87 (1.54-2.28)	2.38 (1.96-2.90)	2.86 (2.34-3.50)	3.60 (2.89-4.66)	4.24 (3.31-5.54)	4.94 (3.72-6.61)	5.71 (4.13-7.85)	6.82 (4.74-9.62)	7.73 (5.21-11.0)	
2-day	1.85 (1.54-2.23)	2.18 (1.81-2.62)	2.76 (2.28-3.34)	3.29 (2.71-4.00)	4.11 (3.31-5.25)	4.79 (3.76-6.19)	5.53 (4.20-7.32)	6.33 (4.61-8.62)	7.48 (5.24-10.5)	8.40 (5.72-11.8)	
3-day	2.03 (1.70-2.43)	2.38 (1.99-2.86)	3.02 (2.51-3.63)	3.59 (2.98-4.34)	4.46 (3.61-5.66)	5.19 (4.09-6.66)	5.96 (4.54-7.85)	6.80 (4.98-9.21)	8.00 (5.63-11.1)	8.96 (6.12-12.6)	
4-day	2.18 (1.83-2.60)	2.55 (2.14-3.05)	3.22 (2.69-3.86)	3.82 (3.17-4.60)	4.72 (3.83-5.97)	5.48 (4.33-7.00)	6.28 (4.80-8.24)	7.16 (5.25-9.65)	8.39 (5.93-11.6)	9.38 (6.44-13.1)	
7-day	2.58 (2.18-3.06)	2.98 (2.51-3.53)	3.68 (3.10-4.38)	4.32 (3.62-5.17)	5.28 (4.32-6.62)	6.09 (4.85-7.73)	6.94 (5.35-9.04)	7.87 (5.82-10.5)	9.18 (6.54-12.7)	10.2 (7.08-14.3)	
10-day	2.93 (2.48-3.46)	3.36 (2.85-3.97)	4.13 (3.48-4.89)	4.81 (4.04-5.73)	5.83 (4.78-7.26)	6.67 (5.33-8.42)	7.57 (5.85-9.81)	8.54 (6.34-11.4)	9.89 (7.08-13.6)	11.0 (7.63-15.2)	
20-day	3.90 (3.34-4.57)	4.50 (3.85-5.27)	5.52 (4.70-6.48)	6.38 (5.40-7.53)	7.62 (6.26-9.33)	8.60 (6.91-10.7)	9.61 (7.48-12.3)	10.7 (7.97-14.1)	12.1 (8.72-16.4)	13.2 (9.28-18.3)	
30-day	4.69 (4.03-5.46)	5.43 (4.66-6.32)	6.64 (5.68-7.75)	7.65 (6.51-8.97)	9.04 (7.45-11.0)	10.1 (8.16-12.5)	11.2 (8.74-14.2)	12.3 (9.24-16.1)	13.8 (9.96-18.6)	14.9 (10.5-20.5)	
45-day	5.67 (4.89-6.56)	6.55 (5.65-7.58)	7.97 (6.85-9.25)	9.12 (7.80-10.6)	10.7 (8.81-12.8)	11.8 (9.58-14.5)	13.0 (10.2-16.3)	14.1 (10.6-18.3)	15.6 (11.3-20.9)	16.7 (11.8-22.8)	
60-day	6.49 (5.62-7.48)	7.47 (6.46-8.62)	9.02 (7.78-10.4)	10.3 (8.81-11.9)	11.9 (9.86-14.2)	13.1 (10.7-16.0)	14.3 (11.2-17.9)	15.5 (11.7-20.0)	16.9 (12.3-22.6)	18.0 (12.8-24.5)	

¹ Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values. Please refer to NOAA Atlas 14 document for more information.

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PF graphical



PDS-based depth-duration-frequency (DDF) curves







NOAA Atlas 14, Volume 8, Version 2

Created (GMT): Tue Oct 10 21:03:54 2023

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Maps & aerials

Small scale terrain

Precipitation Frequency Data Server







Large scale aerial

Precipitation Frequency Data Server



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US Department of Commerce National Oceanic and Atmospheric Administration National Weather Service National Water Center 1325 East West Highway Silver Spring, MD 20910 Questions?: HDSC.Questions@noaa.gov

Disclaimer



4-WAY COMMERCIAL

EXISTING CONDITIO

EL PASO COUNTY, CO HRGreen

-	<u>Calc'd by:</u>	SPC	
NS	<u>Checked by:</u>	СМ	
	Date:	10/12/2023	

SUMMARY RUNOFF TABLE

BASIN	AREA (ac)	% IMPERVIOUS	Q ₅ (cfs)	Q ₁₀₀ (cfs)
NT1	1.45	0	0.5	3.4
NT2	10.65	0	2.8	20.8
NT3	0.87	0	0.3	2.3
D	16.83	0	4.3	31.3
E	9.64	0	2.5	18.2
F	5.83	5	2.6	13.5

DESIGN POINT SUMMARY TABLE

DESIGN POINT	CONTRIBUTING BASINS	ΣQ_5 (cfs)	ΣQ_{100} (cfs)
1	D,E	6.5	47.4
2	NT1,NT2	2.8	20.7

Hydrologic calculations not checked in detail pending additional information per drainage plan redlines

Ex-Early_Grading

RBM 10/12/2023 4:29 PM

T V	4-WAY COMMERCIAL							<u>Calc'd by:</u>		SPC			
	EXISTING C	ONDITIC	DNS					<u>Chec</u> l	<u>ked by:</u>	СМ			
HRGreen	EL PASO COUNTY, CO							Date:		10/12/2023			
	COMPOSITE 'C' FACTORS												
BASIN	UNDEVELOPED	PAVED	TOTAL	SOIL	UNI	DEVEL	.OPED		PAVED		COMPOSITE IMPERVIOUSNESS & C		
	· · · · · · · · · · · · · · · · · · ·	ACRES		TYPE	%	C ₅	C ₁₀₀	%	C 5	C ₁₀₀	%I	C ₅	C ₁₀₀
NT1	1.45	0.00	1.45	A/B	0	0.08	0.35	100	0.90	0.96	0	0.08	0.35
NT2	10.65	0.00	10.65	A/B	0	0.08	0.35	100	0.90	0.96	0	0.08	0.35
NT3	0.87	0.00	0.87	A/B	0	0.08	0.35	100	0.90	0.96	0	0.08	0.35
		0.00	16.92	A/B	0	0.08	0.35	100	0.90	0.96	0	0.08	0.35
D	16.83	0.00	10.05	140	-								
D E	16.83 9.64	0.00	9.64	A/B	0	0.08	0.35	100	0.90	0.96	0	0.08	0.35
D E F	16.83 9.64 5.51	0.00 0.00 0.32	9.64	A/B A/B	0	0.08 0.08	0.35 0.35	100 100	0.90 0.90	0.96	0 5	0.08 0.13	0.35 0.38
D E F	16.83 9.64 5.51	0.00 0.00 0.32	9.64 5.83	A/B A/B	0	0.08	0.35 0.35	100 100	0.90 0.90	0.96 0.96	0 5	0.08 0.13	0.35 0.38



4-WAY COMMERCIAL EXISTING CONDITIONS DESIGN STORM: 5-YEAR

<u>Calc'd by:</u> Checked by: Date:

REMARKS **DIRECT RUNOFF TOTAL RUNOFF** SURFACE TRAVEL TIME PIPE TRAVEL TIME (min POINT PIPE SIZE (in) (FT) Q_{PIPE} (cfs) VEL. (FPS) Q_{street} (cfs) AREA (ac) / (in./ hr.) % **SLOPE** % C₅*A (ac) (in./ hr.) C₅*A (ac) SLOPE % C₅*A (ac) C₅*A (ac) ₽ LENGTH STREET t_c (min) t_c (min) DESIGN Q (cfs) Q (cfs) BASIN C5 NT1 1.45 0.08 10.6 0.12 4.05 0.5 0.5 0.12 739 1.04 11.85 1.1 NT2 10.65 0.08 17.1 0.85 3.33 2.8 2.8 0.85 19.4 460 4.40 1.74 Total flow to DP2 (DBPS 5 Per the MDDP Ammendment/Preliminary/Final Drainage 2 22.4 0.97 2.92 2.8 report for Stapleton Drive From Bandero DR to US HWY 24 NT3 0.08 0.07 4.40 0.87 8.3 0.3 4.3 1.35 2.0 125 1.41 1.47 D 16.83 0.08 19.1 1.35 3.16 4.3 18.3 0.77 3.22 2.5 Е 9.64 0.08 Total flow to D1 (DBPS 4 Per the MDDP Ammendment/Preliminary/Final Drainage report 20.5 2.12 3.05 6.5 1 for Stapleton Drive From Bandero DR to US HWY 24 F 5.83 0.13 14.4 0.73 3.59 2.6

SPC

СМ

10/12/2023

	4- W A`	Y COM	MERCIAI	-				Calc'd b	y:	SPC					
	EXIS	TING CO	ONDITIO	Checked	by:		СМ								
HRGreen	EL PAS		10/1	2/2023											
	$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$														
BAS	Length Length (tt) SLOPE % t_i (min) Cv Length (tt) SLOPE % V (tt/s) t_i (min) t_c (min) 0.08 1.45 100 4.2 11.6 10 0 0.00 0.00 0.0 11.2 0.08 10.65 100 2.3 14.1 10 1175 2.2 1.5 13.1 27.														
DESIGNATION	C ₅	AREA (ac)	LENGTH (ft)	SLOPE %	t _i (min)	C _V	LENGTH (ft)	SLOPE %	V (ft/s)	t _t (min)	t _c (min)				
NT1	0.08	1.45	100	4.2	11.6	10	0	0.0	0.0	0.0	11.6				
NT2	0.08	10.65	100	2.3	14.1	10	1175	2.2	1.5	13.1	27.2				
NT3	0.08	0.87	58	5.0	8.3	10	0	0.0	0.0	0.0	8.3				
D	0.08	16.83	200	1.5	23.1	10	1430	2.2	1.5	16.1	39.2				
E	0.08	9.64	200	2.0	21.0	10	1300	1.8	1.3	16.1	37.1				
F	0.13	5.83	200	2.5	18.6	10	585	4.4	2.1	4.6	23.3				

FORMULAS:

$$t_i = \frac{0.395(1.1 - C_5)\sqrt{s}}{S^{0.33}}$$

$$)\sqrt{L} \qquad V = C_v S_w^{0.5}$$

Table 6-7. Conveyance Coefficient, C_{ν}

Type of Land Surface	C_{ν}
Heavy meadow	2.5
Tillage/field	5
Riprap (not buried)*	6.5
Short pasture and lawns	7
Nearly bare ground	10
Grassed waterway	15
Paved areas and shallow paved swales	20

^{*} For buried riprap, select C_v value based on type of vegetative cover.



1									4-W	AY C	OMME	RCI	AL								Ca	lc'd by:	SPC
	\neg								EXIS	TING	G CONI	DITIC	DNS	;							Che	cked by	CM
									DESIG	SN ST	ORM: 1	00-Y	EAR								_	Date:	10/12/2023
HR	Gree	n																					·
				DI	RECT	RUNO	FF		т	OTAL	RUNOFF		S	URFAC	E		PI	PE		TR	AVEI	TIME	REMARKS
STREET	DESIGN POINT	BASIN ID	AREA (ac)	C ₁₀₀	t _c (min)	C ₁₀₀ *A (ac)	/ (in./ hr.)	Q (cfs)	t _e (min)	C ₁₀₀ *A (ac)	/ (in./ hr.)	Q (cfs)	Q _{street} (cfs)	C ₁₀₀ *A (ac)	SLOPE %	Q _{PIPE} (cfs)	C ₁₀₀ *A (ac)	SLOPE %	PIPE SIZE (in)	LENGTH (FT)	VEL. (FPS)	TRAVEL TIME (min	
			1 45	0.25	10.6	0.51	6 80	2.4					2.4	0.51	1 1					720	1.04	11.95	
		NT2	10.65	0.35	17.1	3.73	5.58	20.8					20.8	3.73	19.4					460	4.40	1.74	
	2								22.4	4.24	4.90	20.7											Total flow to DP2 (DBPS 5 Per the MDDP Ammendment/Preliminary/Final Drainage report for Stapleton Drive From Bandero DR to US HWY 24
		NT3	0.87	0.35	8.3	0.30	7.39	2.3										-					
		D	16.83	0.35	19.1	5.89	5.31	31.3					31.3	5.89	2.0					125	1.41	1.47	
		E	9.64	0.35	18.3	3.37	5.41	18.2															
	1								20.5	9.26	5.12	47.4											Total flow to D1 (DBPS 4 Per the MDDP Ammendment/Preliminary/Final Drainage report for Stapleton Drive From Bandero DR to US HWY 24
		F	5.83	0.38	14.4	2.24	6.02	13.5															

644
HRGreen

4-WAY COMMERCIAL PR. INTERIM GRADING CONDITIONS EL PASO COUNTY, CO

	SUMM	ARY RUNOFI	F TABLE	
BASIN	AREA (ac)	% IMPERVIOUS	Q ₅ (cfs)	Q ₁₀₀ (cfs)
TSA	11.46	0	3.1	13.5
PNT1	0.13	0	0.0	0.3
PNT2	0.87	0	0.2	1.7
PNT3	0.56	0	0.2	1.4
PD	14.99	0	3.8	27.8
PE	2.56	0	0.7	4.8
PF	2.73	12	1.7	6.9
P1.1	0.78	100	3.1	5.6
P1.2	0.26	100	1.1	2.0
P1.3	0.59	68	1.9	3.9
P1.4	1.23	98	5.5	9.9
P1.5	0.64	100	3.0	5.3
P1.6A	2.72	0	0.8	5.9
P1.6B	0.73	96	3.1	5.7
P1.7A	1.72	0	0.5	3.9
P1.7B	0.59	95	2.5	4.6
P1.8	0.76	100	3.2	5.7
P1.9	0.20	100	0.9	1.7
P1.10	2.41	46	5.5	12.8

DES	SIGN POINT SU	MMARY TA	ABLE
DESIGN POINT	CONTRIBUTING BASINS	ΣQ_5 (cfs)	ΣQ_{100} (cfs)
1	PD,PE	4.3	31.4
2	PNT1,PNT2	0.2	1.7
3.1	P1.3	3.1	5.6
3.2	P1.2,DP3.1	4.2	7.4
3.3	P1.3,DP3.2	5.8	10.8
3.4	P1.4,DP3.3	10.4	19.0
3.5	P1.5,DP1.4	8.4	15.2
3.6	P1.6A,P1.6B	4.0	5.7
3.7	P1.7A,P1.7B	3.0	8.4
3.8	P1.9,DP3.6	4.9	17.6
3.9	DP3.7,DP3.8	8.3	28.8
3.10	P1.8	3.1	5.6
3.11	DP3.9,DP3.10	10.8	23.6
3.12	DP3.5,DP3.11	27.6	53.9
4	TSA	3.1	13.5

<u>Calc'd by:</u>

Date:

Checked by:

SPC

СМ

10/12/2023

Pr_Drainage_Calcs_Interim

RBM 10/12/2023 4:30 PM

	4-WAY COMME	RCIAL	-										Calc'	d by:	SPC						
	PR. INTERIM	I GRA	DING CO	ONDITIONS	6								Chec	ked by:	СМ						
HRGreen	EL PASO COUNT	r, co											Date:	_	10/12/2023						
						СОМ	POS	TE '	C' FAC	CTORS	;						•				
	UNDEVELOPED/L	Deste		Commercial		6011	UND	EVEL	OPED/L		Deefe					Cor	nmei	rcial	CO	MPOSIT	ſE
BASIN	AWNS	ROOTS	PAVED	Area	IUIAL			AWN	S		ROOTS			P/			Area	1	IMPERV	IOUSNE	SS & C
						ITPE	% I	C ₅	C ₁₀₀	%I	C ₅	C ₁₀₀	%	C ₅	C ₁₀₀	%	C ₅	C ₁₀₀	%	C ₅	C ₁₀₀
TSA	11.46	0.00	0.00	0.00	11.46	A/B	0	0.08	0.35	90	0.73	0.81	100	0.90	0.96	95	0.81	0.88	0	0.08	0.35
PNT1	0.13	0.00	0.00	0.00	0.13	A/B	0	0.08	0.35	90	0.73	0.81	100	0.90	0.96	95	0.81	0.88	0	0.08	0.35
PNT2	0.87	0.00	0.00	0.00	0.87	A/B	0	0.08	0.35	90	0.73	0.81	100	0.90	0.96	95	0.81	0.88	0	0.08	0.35
PNT3	0.56	0.00	0.00	0.00	0.56	A/B	0	0.08	0.35	90	0.73	0.81	100	0.90	0.96	95	0.81	0.88	0	0.08	0.35
P1.1	0.00	0.00	0.78	0.00	0.78	A/B	0	0.08	0.35	90	0.73	0.81	100	0.90	0.96	95	0.81	0.88	100	0.90	0.96
P1.2	0.00	0.00	0.26	0.00	0.26	A/B	0	0.08	0.35	90	0.73	0.81	100	0.90	0.96	95	0.81	0.88	100	0.90	0.96
P1.3	0.19	0.00	0.40	0.00	0.59	A/B	0	0.08	0.35	90	0.73	0.81	100	0.90	0.96	95	0.81	0.88	68	0.64	0.76
P1.4	0.00	0.28	0.95	0.00	1.23	A/B	0	0.08	0.35	90	0.73	0.81	100	0.90	0.96	95	0.81	0.88	98	0.86	0.93
P1.5	0.00	0.00	0.64	0.00	0.64	A/B	0	0.08	0.35	90	0.73	0.81	100	0.90	0.96	95	0.81	0.88	100	0.90	0.96
P1.6A	2.72	0.00	0.00	0.00	2.72	A/B	0	0.08	0.35	90	0.73	0.81	100	0.90	0.96	95	0.81	0.88	0	0.08	0.35
P1.6B	0.00	0.28	0.45	0.00	0.73	A/B	0	0.08	0.35	90	0.73	0.81	100	0.90	0.96	95	0.81	0.88	96	0.83	0.90
P1.7A	1.72	0.00	0.00	0.00	1.72	A/B	0	0.08	0.35	90	0.73	0.81	100	0.90	0.96	95	0.81	0.88	0	0.08	0.35
P1.7B	0.00	0.28	0.31	0.00	0.59	A/B	0	0.08	0.35	90	0.73	0.81	100	0.90	0.96	95	0.81	0.88	95	0.82	0.89
P1.8	0.00	0.00	0.76	0.00	0.76	A/B	0	0.08	0.35	90	0.73	0.81	100	0.90	0.96	95	0.81	0.88	100	0.90	0.96
P1.9	0.00	0.00	0.20	0.00	0.20	A/B	0	0.08	0.35	90	0.73	0.81	100	0.90	0.96	95	0.81	0.88	100	0.90	0.96
P1.10	1.28	0.28	0.85	2.41	A/B	0	0.08	0.35	90	0.73	0.81	100	0.90	0.96	95	0.81	0.88	46	0.44	0.62	
PD	14.99	0.00	0.00	0.00	14.99	A/B	0	0.08	0.35	90	0.73	0.81	100	0.90	0.96	95	0.81	0.88	0	0.08	0.35
PE	2.56	0.00	0.00	0.00	2.56	A/B	0	0.08	0.35	90	0.73	0.81	100	0.90	0.96	95	0.81	0.88	0	0.08	0.35
PF	2.41	0.00	0.32	2.73	A/B	0	0.08	0.35	90	0.73	0.81	100	0.90	0.96	95	0.81	0.88	12	0.18	0.42	
																					_
Total					14.19																

	4-WA	у сомі	MERCIA	L				Calc'd b	y:	5	SPC		
	PR. II	NTERIM	GRADI	NG COM	NDITIO	NS		Checked	by:		СМ		
HRGreen	EL PAS		гү, со					Date:		10/1	2/2023		
				TIME O	F CONCE	NTRATI	ON						
BAS	SIN DATA		OVER	LAND TIM	E (T _i)		TRAV	EL TIME (T _t)		TOTAL	tc=(L/180)+10	Design tc
DESIGNATION	C ₅	AREA (ac)	LENGTH (ft)	SLOPE %	t _i (min)	Cv	LENGTH (ft)	SLOPE %	V (ft/s)	t _t (min)	t _c (min)	tc max	tc design (min)
TSA	0.08	11.46	100	1.5	16.3	10	1106	2.0	1.4	12.9	29.2	16.7	16.7
PNT1	0.08	0.13	100	4.2	11.6	10	0	0.0	0.0	0.0	11.6	10.6	10.6
PNT2	0.08	0.87	100	2.3	14.1	10	1175	2.2	1.5	13.1	27.2	17.1	17.1
PNT3	0.08	0.56	58	5.0	8.3	10	0	0.0	0.0	0.0	8.3	10.3	8.3
P1.1	0.90	0.78	75	3.0	2.2	20	694	1.0	2.0	5.8	8.0	14.3	8.0
P1.2	0.90	0.26	15	2.0	1.1	20	625	1.0	2.0	5.2	6.3	13.6	6.3
P1.3	0.64	0.59	15	2.0	2.6	20	155	1.0	2.0	1.3	5.0	10.9	5.0
P1.4	0.86	1.23	81	18.5	1.5	20	217	0.5	1.4	2.6	5.0	11.7	5.0
P1.5	0.90	0.64	100	1.0	3.7	20	171	1.0	2.0	1.4	5.1	11.5	5.1
P1.6A	0.08	2.72	300	2.0	25.7	10	315	0.5	0.7	7.4	33.1	13.4	13.4
P1.6B	0.83	0.73	81	18.5	1.7	20	225	1.6	2.5	1.5	5.0	11.7	5.0
P1.7A	0.08	1.72	300	0.5	40.8	10	115	1.1	1.0	1.8	42.6	12.3	12.3
P1.7B	0.82	0.59	81	18.5	1.8	20	87	1.7	2.6	0.6	5.0	10.9	5.0
P1.8	0.90	0.76	89	1.5	3.0	20	351	0.5	1.4	4.1	7.2	12.4	7.2
P1.9	0.90	0.20	28	1.0	1.9	20	161	0.5	1.4	1.9	5.0	11.1	5.0
P1.10	0.44	2.41	81	18.5	4.1	20	233	3.2	3.6	1.1	5.2	11.7	5.2
PD	0.08	14.99	200	1.5	23.1	10	1430	2.2	1.5	16.1	39.2	19.1	19.1
PE	0.08	2.56	200	2.0	21.0	10	1300	1.8	1.3	16.1	37.1	18.3	18.3
PF	0.18	2.73	200	2.5	17.7	10	585	5 4.4 2.1			22.3	14.4	14.4
FORMULAS:													

$$t_i = \frac{0.395(1.1)}{50}$$

$$= \frac{0.395(1.1 - C_5)\sqrt{L}}{S^{0.33}} \qquad V = C_v S_w^{0.5}$$

Table 6-7. Conveyance Coefficient, C_{ν}

Type of Land Surface	C_{ν}
Heavy meadow	2.5
Tillage/field	5
Riprap (not buried)*	6.5
Short pasture and lawns	7
Nearly bare ground	10
Grassed waterway	15
Paved areas and shallow paved swales	20

* For buried riprap, select Cv value based on type of vegetative cover.



4-WAY COMMERCIAL PR. INTERIM GRADING CONDITIONS

DESIGN STORM: 5-YEAR

Checked by: Date:

Calc'd by:

				DIR	ECT R	UNOF	F		тс	DTAL I	RUNOFF		SL	JRFA	CE		PIP	Έ		TR	AVEL	TIME	
STREET	DESIGN POINT	BASIN ID	AREA (ac)	C ₅	t _c (min)	C₅*A (ac)	/ (in./ hr.)	Q (cfs)	t _c (min)	C ₅ *A (ac)	/ (in./ hr.)	Q (cfs)	Q _{street} (cfs)	C ₅ *A (ac)	SLOPE %	Q _{PIPE} (cfs)	C ₅ *A (ac)	% BAODE	PIPE SIZE (in)	LENGTH (FT)	VEL. (FPS)	TRAVEL TIME (min	
	4	TSA	11 46	0.08	16.7	0 92	3 36	31															
			0.40	0.00	10.0	0.01	4.05	0.1						0.05		700.0				700	1.0	44.05	
	2	PNT1 PNT2 (PNT1, PNT2)	0.13	0.08	10.6 17.1	0.01	4.05 3.326	0.0	22.4	0.08	2.92	0.2	0.3 1.7	0.05	1.1 19.4	460.0				7 <u>39</u> 460	1.0 4.4	11.85 1.74	Total f
		PNT3	0.56	0.08	8.3	0.04	4 40	02															
		PD	14.99	0.08	19.1	1.20	3.16	3.8					3.8	1.20	2.0					125	1.4	1.47	
	1	PE (PD,PE)	2.56	0.08	18.3	0.20	3.22	0.7	20.5	1.40	3.05	4.3											Total
		PF	2.73	0.18	14.4	0.48	3.59	1.7															
	3.1	P1.1	0.78	0.90	8.0	0.70	4.47	3.1								3.1	0.70	0.5	15.0	60	5.9	0.17	B/
	3.2	P1.2	0.26	0.90	6.3	0.23	4.81	1.1	8.2	0.94	4.44	4.2				4.2	0.94	0.5	18.0	34	7.3	0.08	B/
	3.3	P1.3	0.59	0.64	5.0	0.38	5.17	1.9	8.2	1.31	4.42	5.8				5.8	1.31	0.5	18.0	100	7.3	0.23	B/
	3.4	P1.4	1.23	0.86	5.0	1.06	5.17	5.5	8.5	2.37	4.38	10.4				10.4	2.37	0.5	24.0	225	10.2	0.37	
	3.5	P1.5	0.64	0.90	5.1	0.58	5.14	3.0	5.4	2.95	5.06	8.4				8.4	2.95	0.5	24.0	31	10.2	0.05	
		P1.6A	2.72	0.08	13.4	0.22	3.69	0.8								0.8	0.22	0.5	30.0	10	13.2	0.01	BA
	3.6	P1.6B	0.73	0.83	5.0	0.61	5.17	3.1	5.0	1.11	5.17	4.0				4.0	1.11	0.5	30.0	175	13.2	0.22	BA
		P1.7A	1.72	0.08	12.3	0.14	3.82	0.5								0.5	0.14	0.5	24.0	10	10.2	0.02	BA
	3.7	P1.7B	0.59	0.82	5.0	0.48	5.17	2.5	5.0	0.62	5.17	3.0				3.0	0.62	0.5	24.0	450	10.2	0.74	BA
	3.8	P1.9	0.2	0.90	5.0	0.18	5.17	0.9	5.0	0.79	5.17	4.9				4.9	0.79	0.5	30.0	38	13.2	0.05	B/
	3.9								5.7	1.41	4.96	8.3				8.3	1.41	0.5	36.0	193	16.3	0.20	
	3.1	P1.8	0.76	0.90	7.2	0.68	4.63	3.2								3.2	0.68	0.5	18.0	228	7.3	0.52	BA
	3.11								7.7	2.09	4.52	10.8				10.8	2.09	0.5	36.0	24	16.3	0.02	
	3.12	P1.10	2.41	0.44	5.2	1.07	5.12	5.5	7.7	6.11	4.52	27.6											

SPC СМ 10/12/2023 REMARKS flow to DP2 (DBPS 5 Per the MDDP Ammendment/Preliminary/Final Drainage report for Stapleton Drive From Bandero DR to US HWY 24 flow to D1 (DBPS 4 Per the MDDP Ammendment/Preliminary/Final Drainage report for Stapleton Drive From Bandero DR to US HWY 24 ASIN P1.1 FLOW, CAPTURED IN 5' TYPE C SUMP INLET @ DP3.1, PIPE FLOW TO DP3.2 ASIN P1.2 FLOW, CAPTURED IN 5' TYPE R SUMP INLET @ DP3.2, PIPE FLOW TO DP3.3 ASIN P1.3 FLOW, CAPTURED IN 5' TYPE R SUMP INLET @ DP3.3, PIPE FLOW TO DP3.7 BASIN P1.4 FLOW, CAPTURED IN 5' TYPE C INLET @ DP3.4, PIPE FLOW TO DP3.5 BASIN P1.5 FLOW, CAPTURED IN XX' INLET @ DP3.5, PIPE TO POND B ASIN P1.6A FLOW, CAPTURED IN 5' TYPE R SUMP INLET @ DP3.6, PIPE FLOW TO DP3.8 ASIN P1.6B FLOW, CAPTURED IN 5' TYPE R SUMP INLET @ DP3.6, PIPE FLOW TO DP3.8 ASIN P1.7A FLOW, CAPTURED IN 5' TYPE R SUMP INLET @ DP3.7, PIPE FLOW TO DP3.9 ASIN P1.7B FLOW, CAPTURED IN 5' TYPE R SUMP INLET @ DP3.7, PIPE FLOW TO DP3.9 ASIN P1.9 FLOW, CAPTURED IN 5' TYPE R SUMP INLET @ DP3.8, PIPE FLOW TO DP3.9 DP3.9 FLOW, PIPE TO DP3.11 SIN P1.8 FLOW, CAPTURED IN 5' TYPE R SUMP INLET @ DP3.10, PIPE FLOW TO DP3.11 DP3.9 FLOW, PIPE TO POND B BASIN P1.10 SHEET FLOW TO DP3.12, POND B TOTAL FLOW



1 1	22								4-W/	AY C	ОММЕ	RCI	AL								<u>Cal</u>	c'd by:	SPC
							PR	r. IN	TERIN	/I GR	ADING	; CO	NDI.	ΓΙΟΝ	S						<u>Chec</u>	cked by	<u>:</u> CM
									DESIG	N STO	DRM: 1	00-YI	EAR								D	ate:	10/12/2023
HR	Gree	n											-										
				D	IRECT	RUNC	DFF		٦	OTAL	RUNOFF	•	S	URFAC	E		PIP	ΡE		TR	AVEL	TIME	REMARKS
STREET	DESIGN POINT	BASIN ID	AREA (ac)	C100	t _c (min)	C ₁₀₀ *A (ac)	/ (in./ hr.)	a (cfs)	f _c (min)	C ₁₀₀ *A (ac)	/ (in./ hr.)	Q (cfs)	Q _{street} (cfs)	C ₁₀₀ *A (ac)	SLOPE %	Q _{PIPE} (cfs)	C ₁₀₀ *A (ac)	SLOPE %	PIPE SIZE (in)	LENGTH (FT)	VEL. (FPS)	TRAVEL TIME (mi	
	Δ	TSA	11 46	0 35	16 7	4 01	3 36	135															
		TOA	11.40	0.00	10.7	4.01	0.00	10.0	,														
		PNT1	0.13	0.35	10.6	0.05	6.80	0.3	} •				0.3	0.05	1.1					739	1.0	11.85	
	2	(PNT1, PNT2)	0.07	0.35	17.1	0.30	5.56296		22.4	0.35	4.90	1.7	1.7	0.30	19.4					400	4.4	1.74	Total flow to DP2 (DBPS 5 Per the MDDP Ammendment/Preliminary/Final Drainage report for Stapleton Drive From Bandero DR to US HWY 24
			0.50	0.25	0.0	0.20	7.20	1 4															
		PNI3	0.50	0.35	0.3	0.20	7.39	1.4	•														
		PD	14.99	0.35	19.1	5.25	5.31	27.8	3				27.8	5.25	2.0					125	1.4	1.47	
	1	PE (PD,PE)	2.56	0.35	18.3	0.90	5.40502	4.8	20.5	6.14	5.12	31.4											Total flow to D1 (DBPS 4 Per the MDDP Ammendment/Preliminary/Final Drainage report for Stapleton Drive From Bandero DR to US HWY 24
		DE	0.70	0.40	44.4	4 45	C 00																
		PF	2.73	0.42	14.4	1.15	6.02	6.9	,							5.6	0.75	0.5	15.0	0 60	5.9	0.17	
	3.1	P1.1	0.78	0.96	8.0	0.75	7.50	5.6	5							7.4	1.00	0.5	40.0		7.0	0.00	BASIN P1.1 FLOW, CAPTURED IN 5' TYPE C SUMP INLET @ DP3.1, PIPE FLOW TO DP3.2
	3.2	P1.2	0.26	0.96	6.3	0.25	8.08	2.0	8.2	2 1.00	7.45	7.4				7.4	1.00	0.5	18.0	34	7.3	0.08	BASIN P1.2 FLOW, CAPTURED IN 5' TYPE R SUMP INLET @ DP3.2, PIPE FLOW TO DP3.3
						0.20										10.8	1.45	0.5	18.0	0 100	7.3	0.23	
	3.3	P1.3	0.59	0.76	5.0	0.45	8.68	3.9	8.2	2 1.45	7.42	10.8				19.0	2 59	0.5	24 () 225	10.2	0.37	BASIN P1.3 FLOW, CAPTURED IN 5' TYPE R SUMP INLET @ DP3.3, PIPE FLOW TO DP3.7
	3.4	P1.4	1.23	0.93	5.0	1.14	8.68	9.9	8.5	2.59	7.35	19.0				10.0	2.00	0.0	24.0	220	10.2	0.07	BASIN P1.4 FLOW, CAPTURED IN 5' TYPE C INLET @ DP3.4, PIPE FLOW TO DP3.5
	2.5	D1 5	0.64	0.06	5 1	0.61	9 62	5.2	5	2 20	9 50	15.0				15.2	3.20	0.5	24.0	31	10.2	0.05	
	5.5	F1.5	0.04	0.90	5.1	0.01	0.03	5 5.5	5 5.4	5.20	0.50	10.2				5.9	0.95	0.5	30.0	0 10	13.2	0.01	BASIN FT.S FLOW, CAFTORED IN AX INLET @ DFS.S, FIFE TO FOID B
		P1.6A	2.72	0.35	13.4	0.95	6.19	5.9)							11.0	4.04	0.5	20.0	175	40.0	0.00	BASIN P1.6A FLOW, CAPTURED IN 5' TYPE R SUMP INLET @ DP3.6, PIPE FLOW TO DP3.8
	3.6	P1.6B	0.73	0.90	5.0	0.66	8.68	5.7	5.0	1.61	8.68	11.6				11.6	1.61	0.5	30.0	175	13.2	0.22	BASIN P1.6B FLOW, CAPTURED IN 5' TYPE R SUMP INLET @ DP3.6, PIPE FLOW TO DP3.8
			4 70		10.0											3.9	0.60	0.5	24.0	0 10	10.2	0.02	
		P1.7A	1.72	0.35	12.3	0.60	6.41	3.9)							8.4	1.13	0.5	24.0) 450	10.2	0.74	BASIN P1.7A FLOW, CAPTURED IN 5' TYPE R SUMP INLET @ DP3.7, PIPE FLOW TO DP3.9
	3.7	P1.7B	0.59	0.89	5.0	0.52	8.68	4.6	5.0	1.13	8.68	8.4											BASIN P1.7B FLOW, CAPTURED IN 5' TYPE R SUMP INLET @ DP3.7, PIPE FLOW TO DP3.9
	3.8	P1.9	0.2	0,96	5.0	0,19	8.68	1.7	11.8	1.80	6.51	17.6				17.6	1.80	0.5	30.0	38	13.2	0.05	BASIN P1.9 FLOW, CAPTURED IN 5' TYPE R SUMP INLET @ DP3.8. PIPE FLOW TO DP3.9
	0.0															28.8	2.93	0.5	36.0	0 193	16.3	0.20	
	3.9								11.9	2.93	6.50	28.8	$\left \right $			57	0.73	0.5	18 () 228	73	0.52	DP3.9 FLOW, PIPE TO DP3.11
	3.1	P1.8	0.76	0.96	7.2	0.73	7.77	5.7								5.7	0.75	0.0	10.0	, 220	7.5	0.52	BASIN P1.8 FLOW, CAPTURED IN 5' TYPE R SUMP INLET @ DP3.10, PIPE FLOW TO DP3.11
	3 11								12.1	3.66	6 /6	22 E				23.6	3.66	0.5	36.0	24	16.3	0.02	
	5.11								12.1	5.00	0.40	23.0								1			
	3.12	P1.10	2.41	0.62	5.2	1.49	8.59	12.8	12.1	8.35	6.45	53.9								1			BASIN P1.10 SHEET FLOW TO DP3.12, POND B TOTAL FLOW

	1
HRGreen	

4-WAY COMMERCIAL	<u>Calc'd by:</u>
PR. ULTIMATE GRADING CONDITIONS	Checked by:
EL PASO COUNTY, CO	<u>Date:</u>

	SUMM	ARY RUNOF	TABLE	
BASIN	AREA (ac)	% IMPERVIOUS	Q ₅ (cfs)	Q ₁₀₀ (cfs)
TSA	11.46	0	3.1	13.5
PNT1	0.13	0	0.0	0.3
PNT2	0.87	0	0.2	1.7
PNT3	0.56	0	0.2	1.4
PD	14.99	0	3.8	27.8
PE	2.56	0	0.7	4.8
PF	2.73	12	1.7	6.9
P1.1	0.78	100	3.1	5.6
P1.2	0.26	100	1.1	2.0
P1.3	0.59	68	1.9	3.9
P1.4	1.23	98	5.5	9.9
P1.5	0.64	100	3.0	5.3
P1.6A	2.72	95	10.2	17.1
P1.6B	0.73	96	3.1	5.7
P1.7A	1.72	95	6.3	10.6
P1.7B	0.59	95	2.5	4.6
P1.8	0.76	100	3.2	5.7
P1.9	0.20	100	0.9	1.7
P1.10	2.41	46	5.5	12.8

DES	SIGN POINT SU	MMARY T	ABLE
DESIGN POINT	CONTRIBUTING BASINS	ΣQ_5 (cfs)	ΣQ_{100} (cfs)
1	PD,PE	4.3	31.4
2	PNT1,PNT2	0.2	1.7
3.1	P1.3	3.1	5.6
3.2	P1.2,DP3.1	4.2	7.5
3.3	P1.3,DP3.2	5.8	10.8
3.4	P1.4,DP3.3	10.4	19.3
3.5	P1.5,DP1.4	8.4	15.2
3.6	P1.6A,P1.6B	21.4	21.7
3.7	P1.7A,P1.7B	14.0	14.3
3.8	P1.9,DP3.6	3.4	23.1
3.9	DP3.7,DP3.8	21.0	36.9
3.10	P1.8	3.1	5.6
3.11	DP3.9,DP3.10	23.6	41.9
3.12	DP3.5,DP3.11	39.8	74.6
4	TSA	3.1	13.5

SPC

СМ

10/12/2023

ULTIMATE CONDITION CALCULATIONS ACCOUNT FOR SUBBASINS P1.6A & P1.7A AS BEING FUTURE COMMERCIAL DEVELOPMENT AND DRAIN TO THE PROVIDED 30" & 24" HDPE STUBS.

Pr_Drainage_Calcs_Ultimate

RBM 10/12/2023 4:30 PM

	4-WAY COMME	ERCIAL	-										<u>Calc'</u>	d by:	SPC						
	PR. ULTIMA	TE GR	RADING	CONDITION	15								<u>Chec</u>	ked by:	СМ						
HRGreen	EL PASO COUNT	Y, CO											Date:		10/12/2023						
						СОМ	POS	TE '	C' FAC	CTORS	;	1	<u></u>	_				.			
	UNDEVELOPED/L	Peofe		Commercial	τοται	5011	UND	EVEL	OPED/L		Boofc			D/		Со	mme	rcial	CO	MPOSIT	ſE
BASIN	AWNS	RUUIS	PAVED	Area	IUIAL	TVDE		AWN	S		KUUIS	-					Area	a	IMPERV	OUSNE	SS & C
						IIFE	%	C ₅	C ₁₀₀	%I	C 5	C ₁₀₀	%I	C ₅	C ₁₀₀	%	C ₅	C ₁₀₀	%I	C ₅	C ₁₀₀
TSA	11.46	0.00	0.00	0.00	11.46	A/B	0	0.08	0.35	90	0.73	0.81	100	0.90	0.96	95	0.81	0.88	0	0.08	0.35
PNT1	0.13	0.00	0.00	0.00	0.13	A/B	0	0.08	0.35	90	0.73	0.81	100	0.90	0.96	95	0.81	0.88	0	0.08	0.35
PNT2	0.87	0.00	0.00	0.00	0.87	A/B	0	0.08	0.35	90	0.73	0.81	100	0.90	0.96	95	0.81	0.88	0	0.08	0.35
PNT3	0.56	0.00	0.00	0.00	0.56	A/B	0	0.08	0.35	90	0.73	0.81	100	0.90	0.96	95	0.81	0.88	0	0.08	0.35
P1.1	0.00	0.00	0.78	0.00	0.78	A/B	0	0.08	0.35	90	0.73	0.81	100	0.90	0.96	95	0.81	0.88	100	0.90	0.96
P1.2	0.00	0.00	0.26	0.00	0.26	A/B	0	0.08	0.35	90	0.73	0.81	100	0.90	0.96	95	0.81	0.88	100	0.90	0.96
P1.3	0.19	0.00	0.40	0.00	0.59	A/B	0	0.08	0.35	90	0.73	0.81	100	0.90	0.96	95	0.81	0.88	68	0.64	0.76
P1.4	0.00	0.28	0.95	0.00	1.23	A/B	0	0.08	0.35	90	0.73	0.81	100	0.90	0.96	95	0.81	0.88	98	0.86	0.93
P1.5	0.00	0.00	0.64	0.00	0.64	A/B	0	0.08	0.35	90	0.73	0.81	100	0.90	0.96	95	0.81	0.88	100	0.90	0.96
P1.6A	0.00	0.00	0.00	2.72	2.72	A/B	0	0.08	0.35	90	0.73	0.81	100	0.90	0.96	95	0.81	0.88	95	0.88	0.88
P1.6B	0.00	0.28	0.45	0.00	0.73	A/B	0	0.08	0.35	90	0.73	0.81	100	0.90	0.96	95	0.81	0.88	96	0.83	0.90
P1.7A	0.00	0.00	0.00	1.72	1.72	A/B	0	0.08	0.35	90	0.73	0.81	100	0.90	0.96	95	0.81	0.88	95	0.88	0.88
P1.7B	0.00	0.28	0.31	0.00	0.59	A/B	0	0.08	0.35	90	0.73	0.81	100	0.90	0.96	95	0.81	0.88	95	0.82	0.89
P1.8	0.00	0.00	0.76	0.00	0.76	A/B	0	0.08	0.35	90	0.73	0.81	100	0.90	0.96	95	0.81	0.88	100	0.90	0.96
P1.9	0.00	0.00	0.20	0.00	0.20	A/B	0	0.08	0.35	90	0.73	0.81	100	0.90	0.96	95	0.81	0.88	100	0.90	0.96
P1.10	1.28	0.28	0.85	0.00	2.41	A/B	0	0.08	0.35	90	0.73	0.81	100	0.90	0.96	95	0.81	0.88	46	0.44	0.62
PD	14.99	0.00	0.00	0.00	14.99	A/B	0	0.08	0.35	90	0.73	0.81	100	0.90	0.96	95	0.81	0.88	0	0.08	0.35
PE	2.56	0.00	0.00	0.00	2.56	A/B	0	0.08	0.35	90	0.73	0.81	100	0.90	0.96	95	0.81	0.88	0	0.08	0.35
PF	2.41	0.00	0.32	0.00	2.73	A/B	0	0.08	0.35	90	0.73	0.81	100	0.90	0.96	95	0.81	0.88	12	0.18	0.42
Total					14.19																

ULTIMATE CONDITION CALCULATIONS ACCOUNT FOR SUBBASINS P1.6A & P1.7A AS BEING FUTURE COMMERCIAL DEVELOPMENT AND DRAIN TO THE PROVIDED 30" & 24" HDPE STUBS.

	4-WA `	у соми	MERCIAI	_				Calc'd b	y:	5	6PC		
	PR. U	LTIMA	re grad	DING CO	ONDITI	ONS		Checked	by:		СМ		
HRGreen	EL PAS	O COUNT	r y, co					Date:		10/1	2/2023		
				TIME O	F CONCE	NTRATI	ON						
BAS	SIN DATA		OVER		E (T _i)		TRAV	EL TIME ((T _t)		TOTAL	tc=(L/180)+10	Design tc
DESIGNATION	C ₅	AREA (ac)	LENGTH (ft)	SLOPE %	t _i (min)	Cv	LENGTH (ft)	SLOPE %	V (ft/s)	t _t (min)	t _c (min)	tc max	tc design (min)
TSA	0.08	11.46	100	1.5	16.3	10	1106	2.0	1.4	12.9	29.2	16.7	16.7
PNT1	0.08	0.13	100	4.2	11.6	10	0	0.0	0.0	0.0	11.6	10.6	10.6
PNT2	0.08	0.87	100	2.3	14.1	10	1175	2.2	1.5	13.1	27.2	17.1	17.1
PNT3	0.08	0.56	58	5.0	8.3	10	0	0.0	0.0	0.0	8.3	10.3	8.3
P1.1	0.90	0.78	75	3.0	2.2	20	694	1.0	2.0	5.8	8.0	14.3	8.0
P1.2	0.90	0.26	15	2.0	1.1	20	625	1.0	2.0	5.2	6.3	13.6	6.3
P1.3	0.64	0.59	15	2.0	2.6	20	155	1.0	2.0	1.3	5.0	10.9	5.0
P1.4	0.86	1.23	81	18.5	1.5	20	217	0.5	1.4	2.6	5.0	11.7	5.0
P1.5	0.90	0.64	100	1.0	3.7	20	171	1.0	2.0	1.4	5.1	11.5	5.1
P1.6A	0.88	2.72	300	2.0	5.5	20	315	0.5	1.4	3.7	9.3	13.4	9.3
P1.6B	0.83	0.73	81	18.5	1.7	20	225	1.6	2.5	1.5	5.0	11.7	5.0
P1.7A	0.88	1.72	300	0.5	8.8	20	115	1.1	2.1	0.9	9.7	12.3	9.7
P1.7B	0.82	0.59	81	18.5	1.8	20	87	1.7	2.6	0.6	5.0	10.9	5.0
P1.8	0.90	0.76	89	1.5	3.0	20	351	0.5	1.4	4.1	7.2	12.4	7.2
P1.9	0.90	0.20	28	1.0	1.9	20	161	0.5	1.4	1.9	5.0	11.1	5.0
P1.10	0.44	2.41	81	18.5	4.1	20	233	3.2	3.6	1.1	5.2	11.7	5.2
PD	0.08	14.99	200	1.5	23.1	10	1430	2.2	1.5	16.1	39.2	19.1	19.1
PE	0.08	2.56	200	2.0	21.0	10	1300	1.8	1.3	16.1	37.1	18.3	18.3
PF	0.18	2.73	200	2.5	17.7	10	585	4.4	2.1	4.6	22.3	14.4	14.4
FORMULAS:		-											

$$t_i = \frac{0.395(1.1 - C_5)\sqrt{L}}{S^{0.33}}$$

Table 6-7. Conveyance Coefficient,
$$C_{\nu}$$

Type of Land Surface	C_{ν}
Heavy meadow	2.5
Tillage/field	5
Riprap (not buried)*	6.5
Short pasture and lawns	7
Nearly bare ground	10
Grassed waterway	15
Paved areas and shallow paved swales	20

^{*} For buried riprap, select C_v value based on type of vegetative cover.

ULTIMATE CONDITION CALCULATIONS ACCOUNT FOR SUBBASINS P1.6A & P1.7A AS BEING FUTURE COMMERCIAL DEVELOPMENT AND DRAIN TO THE PROVIDED 30" & 24" HDPE STUBS.

 $V = C_v S_w^{0.5}$



1 1									4-WA	Y CO	MME	RCIA	L								Calc	c'd by:	SPC
	$\neg \neg \neg$						PR.	ULT	ΙΜΑΤΕ	GR	ADING	; CO	NDI	τιο	NS						Chec	ked by:	СМ
		1							DESIG		DRM: 5	-YEA	R								D	ate:	10/12/2023
HR	Gree	n																					
				DIR	ECT R	UNOF	F		т	OTAL	RUNOFF		รเ	JRFA	CE		PI	PE		TR	AVEL	TIME	REMARKS
STREET	DESIGN POINT	BASIN ID	AREA (ac)	C ₅	t _e (min)	C₅*A (ac)	/ (in./ hr.)	Q (cfs)	<i>t_e (</i> min)	C ₅ *A (ac)	/ (in./ hr.)	Q (cfs)	Q _{street} (cfs)	C ₅ *A (ac)	SLOPE %	Q _{PIPE} (cfs)	C ₅ *A (ac)	SLOPE %	PIPE SIZE (in)	LENGTH (FT)	VEL. (FPS)	TRAVEL TIME (min	
	5 ā																						
		PNT1 PNT2	0.13	0.08	10.6 17 1	0.01	4.05	0.0					0.3	0.05	1.1 19.4	739.0 460.0				739 460	1.0 4 4	11.85 1 74	
	2	(PNT1, PNT2)	0.07	0.00	17.1	0.07	0.020	0.2	22.4	0.08	2.92	0.2	2	0.01	10.4	400.0				400		1.74	Total flow to DP2 (DBPS 5 Per the MDDP Ammendment/Preliminary/Final Drainage report for Stapleton Drive From Bandero DR to US HWY 24
		PNT3	0.56	0.08	83	0.04	4 40	0.2															
			0.00	0.00	0.0	0.01		0.2															
		PD PE	14.99	0.08	19.1	1.20	3.16	3.8					3.8	1.20	2.0					125	1.4	1.47	
	1	(PD PF)	2.00	0.00	10.5	0.20	5.22	0.7	20.5	1 40	3 05	4.3											Total flow to D1 (DBPS 4 Per the MDDP Ammendment/Preliminary/Final Drainage report for
		(1 2,1 2)							20.0	1.10	0.00	1.0											Stapleton Drive From Bandero DR to US HWY 24
		PF	2.73	0.18	14.4	0.48	3.59	1.7															
																3.1	0.70	0.5	15.0	60	5.9	0.17	
	3.1	P1.1	0.78	0.90	8.0	0.70	4.47	3.1															BASIN P1.1 FLOW, CAPTURED IN 5' TYPE C SUMP INLET @ DP3.1, PIPE FLOW TO DP3.2
																4.2	0.94	0.5	18.0	34	7.3	0.08	
	3.2	P1.2	0.26	0.90	6.3	0.23	4.81	1.1	8.2	0.94	4.44	4.2											BASIN P1.2 FLOW, CAPTURED IN 5' TYPE R SUMP INLET @ DP3.2, PIPE FLOW TO DP3.3
		D4 a	0.50	0.04	5.0		- 17				4.40					5.8	1.31	0.5	18.0	100	7.3	0.23	
	3.3	P1.3	0.59	0.64	5.0	0.38	5.17	1.9	8.2	1.31	4.42	5.8				40.4	0.07	0.5	04.0	005	40.0	0.07	BASIN P1.3 FLOW, CAPTURED IN 5° TYPE R SUMP INLET @ DP3.3, PIPE FLOW TO DP3.7
	2.4	D1 4	1 00	0.96	5.0	1.00	E 17	E E	0 5	0.07	4.00	10.4				10.4	2.37	0.5	24.0	225	10.2	0.37	
	3.4	P1.4	1.23	0.86	5.0	1.06	5.17	5.5	6.5	2.37	4.38	10.4	·			0.4	2.05	0.5	24.0	24	10.2	0.05	BASIN PT.4 FLOW, CAPTURED IN 5 TYPE C INLET @ DP3.4, PIPE FLOW TO DP3.5
	3.5	P1.5	0.64	0.90	5.1	0.58	5.14	3.0	5.4	2.95	5.06	8.4				0.4	2.90	0.5	24.0	31	10.2	0.05	BASIN P1.5 FLOW, CAPTURED IN XX' INLET @ DP3.5, PIPE TO POND B
																10.2	2.39	0.5	30.0	10	13.2	0.01	
		P1.6A	2.72	0.88	9.3	2.39	4.24	10.2															BASIN P1.6A FLOW, CAPTURED IN 5' TYPE R SUMP INLET @ DP3.6, PIPE FLOW TO DP3.8
																21.4	3.00	0.5	30.0	175	13.2	0.22	
	3.6	P1.6B	0.73	0.83	5.0	0.61	5.17	3.1	9.3	3.00	7.12	21.4											BASIN P1.6B FLOW, CAPTURED IN 5' TYPE R SUMP INLET @ DP3.6, PIPE FLOW TO DP3.8
																6.3	1.51	0.5	24.0	10	10.2	0.02	
		P1.7A	1.72	0.88	9.7	1.51	4.17	6.3															BASIN P1.7A FLOW, CAPTURED IN 5' TYPE R SUMP INLET @ DP3.7, PIPE FLOW TO DP3.9
																14.0	2.00	0.5	24.0	450	10.2	0.74	
	3.7	P1.7B	0.59	0.82	5.0	0.48	5.17	2.5	9.7	2.00	7.00	14.0					0.40					0.05	BASIN P1.7B FLOW, CAPTURED IN 5' TYPE R SUMP INLET @ DP3.7, PIPE FLOW TO DP3.9
	3.8	P1.9	0.2	0.90	5.0	0.18	5.17	0.9	9.5	3.18	4.21	3.4				3.4	3.18	0.5	30.0	38	13.2	0.05	BASIN P1.9 FLOW, CAPTURED IN 5' TYPE R SUMP INLET @ DP3.8, PIPE FLOW TO DP3.9
	30								10 5	5 19	1.00	21.0				21.0	5.18	0.5	36.0	193	16.3	0.20	
	3.9								10.5	5.16	4.00	21.0				3.2	0.68	0.5	18.0	228	7.3	0.52	
	3.10	P1.8	0.76	0.90	7.2	0.68	4.63	3.2															BASIN P1.8 FLOW, CAPTURED IN 5' TYPE R SUMP INLET @ DP3.10, PIPE FLOW TO DP3.11
	3 1 1								10.7	5.86	1 03	22.6				23.6	5.86	0.5	36.0	24	16.3	0.02	
	0.11								10.7	0.00	+.03	20.0											
	3.12	P1.10	2.41	0.44	5.2	1.07	5.12	5.5	10.7	9.88	4.03	39.8											BASIN P1.10 SHEET FLOW TO DP3.12, POND B TOTAL FLOW

ULTIMATE CONDITION CALCULATIONS ACCOUNT FOR SUBBASINS P1.6A & P1.7A AS BEING FUTURE COMMERCIAL DEVELOPMENT AND DRAIN TO THE PROVIDED 30" & 24" HDPE STUBS.

J:\2022\2202654\Design\Calc\Drainage\Appendix B - Hydrologic\Pr_Drainage_Calcs_Ultimate



									4-W/	AY C	OMME		AL								SPC		
	$\neg \neg$	х 7					PR.	. UL1	ΓΙΜΑΤ	E G R	RADIN	G CC)ND	ΙΤΙΟΙ	NS						Chec	cked by	<u>у:</u> СМ
		1							DESIG	N STO	DRM: 1	00-YI	EAR								D	ate:	10/12/2023
HR	Gree	n																					
													1										
		1		D	IRECT	RUNG	DFF	1	٦	OTAL	RUNOFI	F	S	URFAC	E		PI	PE		TR	AVEL	TIME	REMARKS
STREET	DESIGN POINT	BASIN ID	AREA (ac)	C ₁₀₀	t _e (min)	C ₁₀₀ *A (ac)	/ (in./ hr.)	Q (cfs)	f _c (min)	C ₁₀₀ *A (ac)	/ (in./ hr.)	Q (cfs)	Q _{street} (cfs)	C ₁₀₀ *A (ac)	SLOPE %	Q _{PIPE} (cfs)	C ₁₀₀ *A (ac)	SLOPE %	PIPE SIZE (in)	LENGTH (FT)	VEL. (FPS)	TRAVEL TIME (mi	
	4	тел	11 46	0.25	16.7	1.01	2.26	125															
	4	154	11.40	0.35	10.7	4.01	3.30	13.5	,														
		PNT1	0.13	0.35	10.6	0.05	6.80	0.3	8				0.3	0.05	1.1					739	1.0	11.85	
		PNT2	0.87	0.35	17.1	0.30	5.58298	1.7	, 				1.7	0.30	19.4					460	4.4	1.74	
	2	(PNT1, PNT2)							22.4	0.35	4.90) 1.7											Total flow to DP2 (DBPS 5 Per the MDDP Ammendment/Preliminary/Final Drainage report for Stapleton Drive From Bandero DR to US HWY 24
		,																					
		PNT3	0.56	0.35	8.3	0.20	7.39	1.4										_					
		PD	14,99	0.35	19.1	5.25	5.31	27.8	3				27.8	5.25	2.0					125	1.4	1.47	
		PE	2.56	0.35	18.3	0.90	5.40502	4.8	3				21.0	0.20	2.0					.20			
	1	(PD,PE)							20.5	6.14	5.12	31.4											Total flow to D1 (DBPS 4 Per the MDDP Ammendment/Preliminary/Final Drainage report for Stapleton Drive From Bandero
		PF	2.73	0.42	14.4	1.15	6.02	6.9)														
																5.6	0.75	5 0.5	5 15.0	15.0) 5.9	0.04	
	3.1	P1.1	0.78	0.96	8.0	0.75	7.50	5.6	5							75	1.00	0.5	5 18 0	18 () 73	0.04	BASIN P1.1 FLOW, CAPTURED IN 5' TYPE C SUMP INLET @ DP3.1, PIPE FLOW TO DP3.2
	3.2	P1.2	0.26	0.96	6.3	0.25	8.08	2.0	8.0	1.00	7.49	7.5				7.5	1.00	0.0	10.0	, 10.0	, 7.5	0.04	BASIN P1.2 FLOW, CAPTURED IN 5' TYPE R SUMP INLET @ DP3.2, PIPE FLOW TO DP3.3
																10.8	1.45	5 0.5	5 18.0	18.0	7.3	0.04	
	3.3	P1.3	0.59	0.76	5.0	0.45	8.68	3.9	8.1	1.45	7.47	7 10.8				40.0	0.50		04.0	04.0	10.0	0.04	BASIN P1.3 FLOW, CAPTURED IN 5' TYPE R SUMP INLET @ DP3.3, PIPE FLOW TO DP3.7
	34	P1 4	1 23	0.93	5.0	1 1 4	8 68	99	8 1	2 59	7 46	19.3				19.3	2.5	9 0.5	24.0	24.0	10.2	0.04	BASIN P1 4 FLOW, CAPTURED IN 5' TYPE C INLET @ DP3 4 PIPE FLOW TO DP3 5
	0.1		1.20	0.00	0.0		0.00	0.0	0.1	2.00		, 10.0				15.2	3.20	0.5	5 24.0	24.0	0 10.2	0.04	
	3.5	P1.5	0.64	0.96	5.1	0.61	8.63	5.3	5.1	3.20	8.63	3 15.2											BASIN P1.5 FLOW, CAPTURED IN XX' INLET @ DP3.5, PIPE TO POND B
		P1 64	2 72	0.88	03	2 30	7 13	171								17.1	2.39	9 0.5	5 30.0	30.0) 13.2	0.04	
		F 1.0A	2.12	0.00	9.0	2.00	7.13	17.1								21.7	3.05	5 0.5	5 30.0	30.0) 13.2	0.04	BASIN FT.OATLOW, CAFTORED IN 3 TIFE R SOME INLET @ DF3.0, FIFE FLOW TO DF3.0
	3.6	P1.6B	0.73	0.90	5.0	0.66	8.68	5.7	9.3	3.05	7.12	2 21.7											BASIN P1.6B FLOW, CAPTURED IN 5' TYPE R SUMP INLET @ DP3.6, PIPE FLOW TO DP3.8
			1 70	0.00	0.7	1 5 1	7.01	10.0								10.6	1.5	1 0.5	5 24.0	24.0	0 10.2	0.04	
		P1.7A	1.72	0.88	9.7	1.51	7.01	10.6								14.3	2.04	4 0.5	5 24.0	24.0) 10.2	0.04	BASIN PT.7A FLOW, CAPTURED IN 5 TYPE R SOMPTINLET @ DP3.7, PIPE FLOW TO DP3.9
	3.7	P1.7B	0.59	0.89	5.0	0.52	8.68	4.6	9.8	3 2.04	6.99	14.3											BASIN P1.7B FLOW, CAPTURED IN 5' TYPE R SUMP INLET @ DP3.7, PIPE FLOW TO DP3.9
		54.0			- 0											23.1	3.24	4 0.5	5 30.0	30.0) 13.2	0.04	
	3.8	P1.9	0.2	0.96	5.0	0.19	8.68	1.7	9.3	3.24	7.11	23.1				36.0	5.29	3 0 5	5 36 0	36.0) 16 3	0.04	BASIN P1.9 FLOW, CAP I URED IN 5' TYPE R SUMP INLET @ DP3.8, PIPE FLOW TO DP3.9
	3.9								9.8	5.28	6.98	36.9				50.9	0.20	0.0			, 10.0	0.04	DP3.9 FLOW, PIPE TO DP3.11
							_									5.7	0.73	3 0.5	5 18.0	18.0	7.3	0.04	
	3.1	P1.8	0.76	0.96	7.2	0.73	7.77	5.7							├ -	/1 0	6.04	1 0 5	36.0	26.0	16.2	0.04	BASIN P1.8 FLOW, CAPTURED IN 5' TYPE R SUMP INLET @ DP3.10, PIPE FLOW TO DP3.11
	3.11								9.8	6.01	6.98	41.9				41.9	0.0	0.5	30.0	30.0	10.3	0.04	DP3.9 FLOW, PIPE TO POND B
	3.12	P1.10	2.41	0.62	5.2	1.49	8.59	12.8	9.9	10.70	6.97	74.6							1	1	1	1	BASIN P1.10 SHEET FLOW TO DP3.12, POND B TOTAL FLOW

ULTIMATE CONDITION CALCULATIONS ACCOUNT FOR SUBBASINS P1.6A & P1.7A AS BEING FUTURE COMMERCIAL DEVELOPMENT AND DRAIN TO THE PROVIDED 30" & 24" HDPE STUBS.





Notes:

1. The standard inlet parameters must apply to use these charts.



Figure 8-11. Inlet Capacity Chart Sump Conditions, Curb Opening (Type R) Inlet

DP3.2 DIRECT RUNOFF Q100 = 2.0 CFS -> 5' TYPE R SUMP INLET DP3.3 DIRECT RUNOFF Q100 = 3.9 CFS -> 5' TYPE R SUMP INLET DP3.5 DIRECT RUNOFF Q100 = 5.3 CFS -> 5' TYPE R SUMP INLET DP3.6 DIRECT RUNOFF Q100 = 5.7 CFS -> 5' TYPE R SUMP INLET DP3.7 DIRECT RUNOFF Q100 = 4.6 CFS -> 5' TYPE R SUMP INLET DP3.8 DIRECT RUNOFF Q100 = 1.7 CFS -> 5' TYPE R SUMP INLET DP3.10 DIRECT RUNOFF Q100 = 5.7 CFS -> 5' TYPE R SUMP INLET

Notes:

1. The standard inlet parameters must apply to use this chart.



4-Way Commercial Early Grading Drainage Report Project No: 2202654

APPENDIX D – WQ & DETENTION

Why are the following pond calcs provided (presumably for Pond B) when no detail drawings were provided to compare the calcs to? If the pond design is to come under a different EDARP submittal (like an SF, for example) than just remove the calcs from this drainage report to avoid confusion.

DETENTION BASIN STAGE-STORAGE TABLE BUILDER



		 			ļ	
		 		10/12/	2023, 5 [.] 01 P	V

ft	user	Initial Surcharge Depth (ISD) =
ft	user	Total Available Detention Depth $(H_{total}) =$
ft	user	Depth of Trickle Channel (H_{TC}) =
ft/ft	user	Slope of Trickle Channel (S_{TC}) =
H:V	user	Slopes of Main Basin Sides (S_{main}) =
	user	Basin Length-to-Width Ratio $(R_{L/W}) =$
-		
<u>4</u> 2	ucor	Initial Surcharge Area (A) -

Initial Surcharge Area (A_{ISV}) =	user	ft ²
Surcharge Volume Length (L_{ISV}) =	user	ft
Surcharge Volume Width (W_{ISV}) =	user	ft
Depth of Basin Floor $(H_{FLOOR}) =$	user	ft
Length of Basin Floor $(L_{FLOOR}) =$	user	ft
Width of Basin Floor (W_{FLOOR}) =	user	ft
Area of Basin Floor (A_{FLOOR}) =	user	ft ²
Volume of Basin Floor (V_{FLOOR}) =	user	ft ³
Depth of Main Basin $(H_{MAIN}) =$	user	ft
Length of Main Basin $(L_{MAIN}) =$	user	ft
Width of Main Basin (W_{MAIN}) =	user	ft
Area of Main Basin $(A_{MAIN}) =$	user	ft ²
Volume of Main Basin (V_{MAIN}) =	user	ft ³
Calculated Total Basin Volume (V_{total}) =	user	acre-feet

DETENTION BASIN OUTLET STRUCTURE DESIGN

		Λ	MHFD-Detention, Vo	ersion 4.06 (July 2	2022)				
Project:	4-Way Commercia	I							
Basin ID:	Southern Parcel (I	nterim Condition -	Pre development of	f future commercia	al area tributary to	pond)			
ZONE 3 ZONE 2				Estimated	Estimated				
				Stage (ft)	Volume (ac-ft)	Outlet Type			
VOLUME EURV WOCV			Zone 1 (WQCV)	1.29	0.214	Orifice Plate			
	100-YEAR		Zone 2 (EURV)	2.17	0.504	Circular Orifice			
PERMANENT ORIFICES	ORIFICE		Zone 3 (100-year)	2.74	0.423	Weir&Pipe (Restrict)			
POOL Example Zone	Configuration (Re	tention Pond)		Total (all zones)	1.141		1		
User Input: Orifice at Underdrain Outlet (typically	used to drain WOC	V in a Filtration BMI	P)			1	Calculated Parame	ters for Underdrain	n
Underdrain Orifice Invert Depth =	N/A	ft (distance below		surface)	Under	drain Orifice Area =	N/A	ft ²	-
Underdrain Orifice Diameter =	N/A	inches		,	Underdrai	n Orifice Centroid =	N/A	feet	
		1						_	
User Input: Orifice Plate with one or more orifice	s or Elliptical Slot W	eir (typically used t	o drain WQCV and/o	r EURV in a sedime	ntation BMP)		Calculated Parame	ters for Plate	
Centroid of Lowest Orifice =	0.00	ft (relative to basir	n bottom at Stage =	0 ft)	WQ Orif	fice Area per Row =	N/A	ft ²	
Depth at top of Zone using Orifice Plate =	2.17	ft (relative to basir	n bottom at Stage =	0 ft)	El	liptical Half-Width =	N/A	feet	
Orifice Plate: Orifice Vertical Spacing =	N/A	inches			Ellip	tical Slot Centroid =	N/A	feet	
Orifice Plate: Orifice Area per Row =	N/A	sq. inches			I	Elliptical Slot Area =	N/A	ft ²	
		-						_	
User Input: Stage and Total Area of Each Orifice	Row (numbered fro	m lowest to highes	<u>t)</u>						
	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)	
Stage of Orifice Centroid (ft)	0.00	0.50	1.00						
Orifice Area (sq. inches)	1.45	1.45	1.45						
	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)	
Stage of Orifice Centroid (ft)									
Orifice Area (sq. inches)									
User Input: Vertical Orifice (Circular or Rectangu	lar)		-				Calculated Parame	ters for Vertical Ori	<u>ifice</u>
	Zone 2 Circular	Not Selected					Zone 2 Circular	Not Selected	
Invert of Vertical Orifice =	1.30	N/A	ft (relative to basin	bottom at Stage =	0 ft) Ve	rtical Orifice Area =	0.01	N/A	ft ²
Depth at top of Zone using Vertical Orifice =	2.17	N/A	ft (relative to basin	bottom at Stage =	0 ft) Vertica	al Orifice Centroid =	0.04	N/A	feet
Vertical Orifice Diameter =	1.00	N/A	inches						
User Input: Overflow Weir (Dropbox with Flat or	Sloped Grate and O	utlet Pipe OR Recta	angular/Trapezoidal \ ¬	Neir and No Outlet	<u>Pipe)</u>		Calculated Parame	ters for Overflow W	<u>Veir</u>
	Zone 3 Weir	Not Selected	_				Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	3.07	N/A	ft (relative to basin b	oottom at Stage = 0 f	ft) Height of Grat	e Upper Edge, $H_t =$	3.07	N/A	feet
Overflow Weir Front Edge Length =	5.67	N/A	feet		Overflow V	Veir Slope Length =	2.92	N/A	feet
Overflow Weir Grate Slope =	0.00	N/A	H:V	G	Frate Open Area / 1	00-yr Orifice Area =		N/A	
Horiz. Length of Weir Sides =	2.92	N/A	feet	C	Overflow Grate Oper	n Area w/o Debris =	11.52	N/A	ft^2
Overflow Grate Type =	Type C Grate	N/A	_		Overflow Grate Ope	en Area w/ Debris =	5.76	N/A	ft ²
Debris Clogging % =	50%	N/A	_%						

Oser input. Outlet i pe w/ now Restriction i late	Circular Office, Res				<u></u>				
	Zone 3 Restrictor	Not Selected					Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =		N/A	ft (distance below ba	asin bottom at Stage	= 0 ft) O	utlet Orifice Area =		N/A	ft ²
Outlet Pipe Diameter =		N/A	inches		Outle	t Orifice Centroid =		N/A	feet
Restrictor Plate Height Above Pipe Invert =			inches	Half-Cer	ntral Angle of Restric	tor Plate on Pipe =		N/A	radians
					-				1
User Input: Emergency Spillway (Rectangular or T	<u>rapezoidal)</u>						Calculated Paramet	ers for Spillway	
Spillway Invert Stage=	4.00	ft (relative to basin	bottom at Stage =	0 ft)	Spillway D	esign Flow Depth=	0.50	feet	
Spillway Crest Length =	33.00	feet	5	,	Stage at	Top of Freeboard =	6.50	feet	
Spillway End Slopes =	4.00	H:V			Basin Area at ⁻	Top of Freeboard =	1.08	acres	
Freeboard above Max Water Surface =	2.00	feet			Basin Volume at	Top of Freeboard =	4 65	acre-ft	
	2.00				Dusin volume at		1.05		
Routed Hydrograph Results	The user can overn	ide the default CUH	P hydrographs and	runoff volumes by e	entering new values	in the Inflow Hydro	graphs table (Colum	ns W through AF).	
Design Storm Return Period =	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
One-Hour Rainfall Depth (in) =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52	3.14
CUHP Runoff Volume (acre-ft) =	0.214	0.718	0.535	0.711	0.851	1.074	1.291	1.566	2.163
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	0.535	0.711	0.851	1.074	1.291	1.566	2.163
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A	0.1	0.1	0.2	1.8	3.7	6.0	11.1
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A							
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.01	0.01	0.02	0.15	0.30	0.49	0.89
Peak Inflow Q (cfs) =	N/A	N/A	6.6	8.9	10.6	14.4	17.8	22.0	30.5
Peak Outflow Q (cfs) =	0.1	0.2	0.2	0.2	0.2	0.2	0.3	1.1	7.0
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	1.4	1.1	0.1	0.1	0.2	0.6
Structure Controlling Flow =	Plate	Vertical Orifice 1	Vertical Orifice 1	Vertical Orifice 1	Vertical Orifice 1	Vertical Orifice 1	Vertical Orifice 1	Overflow Weir 1	Dverflow Weir
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	0.0	0.0
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	38	66	58	66	73	82	91	98	95
Time to Drain 99% of Inflow Volume (hours) =	40	72	63	73	80	90	100	108	106
Maximum Ponding Depth (ft) =	1.29	2.17	1.85	2.10	2.29	2.59	2.87	3.16	3.46
Area at Maximum Ponding Depth (acres) =	0.38	0.72	0.63	0.71	0.73	0.76	0.78	0.81	0.84

0.720

0.215

0.499

this is too high revise as appropriate

0.807

1.023

0.670

see comment on Table Builder sheet. These flows should - approximate the total calculated flows entering the pond. (These values are less than half)

1.239

1.478

1.725

Area at Maximum Ponding Depth (acres) = Maximum Volume Stored (acre-ft) =

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.06 (July 2022)



DETENTION BASIN OUTLET STRUCTURE DESIGN

maximum bound

DETENTION BASIN OUTLET STRUCTURE DESIGN Outflow Hydrograph Workbook Filename:

Inflow Hydrographs

The user can	override the cal	culated inflow h	nydrographs f	from this workboo	k with inflow	hydrographs	developed in a	a separate program.
			, , ,			/ 2 /	•	

	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0100 11	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:15:00	0.00	0.00	0.72	1.17	1.46	0.98	1.24	1.21	1.75
	0:20:00	0.00	0.00	2.61	3.43	4.05	2.57	3.00	3.21	4.22
	0:25:00	0.00	0.00	5.37	7.36	9.02	5.35	6.22	6.76	9.22
	0:30:00	0.00	0.00	6.61	8.87	10.59	11.95	14.85	17.20	24.26
	0:35:00	0.00	0.00	6.37	8.38	9.90	14.40	17.78	21.99	30.51
	0:40:00	0.00	0.00	5.92	7.66	9.01	14.16	17.47	21.66	30.05
	0:45:00	0.00	0.00	5.31	6.93	8.17	12.94	15.89	20.18	28.14
	0:50:00	0.00	0.00	4.80	6.35	7.42	11.83	14.44	18.25	25.58
	0:55:00	0.00	0.00	4.36	5.75	6.73	10.55	12.81	16.37	22.91
	1:00:00	0.00	0.00	3.94	5.18	6.09	9.39	11.35	14.77	20.67
	1:05:00	0.00	0.00	3.59	4.68	5.53	8.37	10.06	13.32	18.68
	1:10:00	0.00	0.00	3.22	4.35	5.18	7.29	8.70	11.33	15.79
	1:15:00	0.00	0.00	2.94	4.04	4.93	6.52	7.75	9.83	13.63
	1:20:00	0.00	0.00	2.70	3.72	4.58	5.81	6.89	8.50	11.73
	1.25.00	0.00	0.00	2.49	3.42	4.13	5.20	6.14	7.34	10.07
	1:35:00	0.00	0.00	2.28	2.13	3.70	3.06	2.30	5.33	0.02
	1:40:00	0.00	0.00	1.87	2.05	2 92	3.90	3 95	4 50	6.02
	1:45:00	0.00	0.00	1.70	2.10	2.61	2,90	3,33	3,70	4.87
	1:50:00	0.00	0.00	1.58	1.91	2.39	2.46	2.79	3.01	3.91
	1:55:00	0.00	0.00	1.40	1.76	2.24	2.17	2.45	2.56	3.30
	2:00:00	0.00	0.00	1.25	1.64	2.06	2.00	2.25	2.30	2.95
	2:05:00	0.00	0.00	1.02	1.34	1.69	1.61	1.81	1.82	2.32
	2:10:00	0.00	0.00	0.82	1.07	1.35	1.27	1.43	1.41	1.78
	2:15:00	0.00	0.00	0.66	0.85	1.08	1.01	1.13	1.10	1.37
	2:20:00	0.00	0.00	0.52	0.68	0.86	0.79	0.89	0.84	1.05
	2:25:00	0.00	0.00	0.41	0.54	0.67	0.62	0.70	0.65	0.80
	2:30:00	0.00	0.00	0.32	0.42	0.52	0.48	0.54	0.50	0.62
	2:35:00	0.00	0.00	0.25	0.32	0.40	0.37	0.41	0.38	0.47
	2:40:00	0.00	0.00	0.19	0.25	0.31	0.28	0.31	0.29	0.36
	2:45:00	0.00	0.00	0.15	0.19	0.24	0.22	0.24	0.23	0.28
	2:50:00	0.00	0.00	0.11	0.14	0.18	0.17	0.18	0.18	0.21
	2:55:00	0.00	0.00	0.08	0.10	0.13	0.12	0.13	0.13	0.15
	3:00:00	0.00	0.00	0.05	0.07	0.09	0.08	0.09	0.09	0.10
	3.10.00	0.00	0.00	0.03	0.04	0.05	0.05	0.08	0.03	0.08
	3:15:00	0.00	0.00	0.02	0.02	0.03	0.03	0.03	0.03	0.03
	3:20:00	0.00	0.00	0.01	0.01	0.01	0.01	0.01	0.01	0.01
	3:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:10:00 4:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:25:00 5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

DETENTION BASIN OUTLET STRUCTURE DESIGN MHFD-Detention, Version 4.06 (July 2022)

Summary Stage-Area-Volume-Discharge Relationships

The user can create a summary S-A-V-D by entering the desired stage increments and the remainder of the table will populate automatically. The user should graphically compare the summary S-A-V-D table to the full S-A-V-D table in the chart to confirm it captures all key transition points.

Stage - Storage	Stage	Area	Area	Volume	Volume	Total Outflow	
Description	[ft]	[ft ²]	[acres]	[ft ³]	[ac-ft]	[cfs]	
	0.00	0	0.000	0	0.000	0.00	For best results, include the
	0.20	2,163	0.050	216	0.005	0.02	stages of all grade slope
	0.40	4,325	0.099	865	0.020	0.03	changes (e.g. ISV and Floor)
	0.60	6,488	0.149	1,946	0.045	0.05	from the S-A-V table on Sheet 'Basin'
	0.80	8,650	0.199	3,460	0.079	0.07	
	1.00	10,813	0.248	5,406	0.124	0.08	Also include the inverts of all
	1.29	16,548	0.380	9,373	0.215	0.12	outlets (e.g. vertical orifice, overflow grate, and spillway.
	1.40	18,723	0.430	11,313	0.260	0.14	where applicable).
	1.60	22,079	0.521	20.385	0.355	0.16	
	2.00	30,589	0.702	26,303	0.599	0.20	-
	2.20	31,420	0.721	32,308	0.742	0.21	
	2.40	32,251	0.740	38,675	0.888	0.23	
	2.60	33,082	0.759	45,208	1.038	0.24	
	2.80	33,913	0.779	51,908	1.192	0.25	
	3.06	34,959	0.803	60,865	1.397	0.27	
	3.20	35,462	0.814	65,794	1.510	1.57	4
	3.40	36,179	0.831	72,958	1.675	5.53	-
	3.60	30,89/	0.84/	80,266	1.843 2.014	10.9/	4
	3.80	38,296	0.879	94,928	2.014	24 74	1
	4.20	39,072	0.897	103.052	2.366	39.60	1
	4.40	39,812	0.914	110,940	2.547	62.07	1
	4.60	40,553	0.931	118,977	2.731	89.41]
	4.80	41,293	0.948	127,161	2.919	119.63	
	5.00	42,033	0.965	135,494	3.111	154.31	
	5.20	42,796	0.982	143,977	3.305	193.30	
	5.40	43,559	1.000	152,612	3.503	236.47	
	5.60	44,321	1.01/	161,400	3.705	283.76	-
	5.80	45 847	1.055	170,341	4 119	390.60	4
	6.20	46,331	1.064	188,652	4.331	450.13	-
	6.40	46,816	1.075	197,967	4.545	513.74	
	6.50	47,058	1.080	202,660	4.652	547.08	
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DETENTION BASIN STAGE-STORAGE TABLE BUILDER

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DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.06 (July 2022)

	D	ETENTION	BASIN OUT	LET STRU	CTURE DES	SIGN			
		۸	MHFD-Detention, V	ersion 4.06 (July 2	2022)				
Project:	4-Way Commercia								
ZONE 3	Southern Parcel								
ZONE 2	\frown			Estimated	Estimated				
				Stage (ft)	volume (ac-rt)	Outlet Type	1		
			Zone 1 (WQCV)	1.63	0.368	Orifice Plate			
T ZONE 1 AND 2	100-YEAR ORIFICE		Zone 2 (EURV)	3.06	1.026	Circular Orifice			
PERMANENT ORIFICES			Zone 3 (100-year)	3.75	0.575	Weir&Pipe (Restrict)			
Example Zone	Configuration (Re	tention Pond)		Total (all zones)	1.969				
ser Input: Orifice at Underdrain Outlet (typically	used to drain WQC	V in a Filtration BMI	<u>)</u>				Calculated Paramet	ters for Underdrain	
Underdrain Orifice Invert Depth =	N/A	ft (distance below	the filtration media s	surface)	Under	drain Orifice Area =	N/A	ft²	
Underdrain Orifice Diameter =	N/A	inches			Underdrai	n Orifice Centroid =	N/A	feet	
Iser Input: Orifice Plate with one or more orifices	or Elliptical Slot W	eir (typically used to	o drain WQCV and/o	r EURV in a sedimer	ntation BMP)		Calculated Paramet	ters for Plate	
Centroid of Lowest Orifice =	0.00	ft (relative to basin	bottom at Stage =	0 ft)	WQ Orif	fice Area per Row =	1.319E-02	ft ²	
Depth at top of Zone using Orifice Plate =	1.63	If (relative to basin	bottom at Stage =	0 ft)	El	liptical Half-Width =	N/A	feet	
Orifice Plate: Orifice Vertical Spacing =	N/A	Inches	1.0/10 :		Ellip	tical Slot Centroid =	N/A	reet	
Orifice Plate: Orifice Area per Row =	1.90	sq. inches (diamete	er = 1-9/16 incres)		I	Elliptical Slot Area =	IN/A	jft ²	
ser Input: Stage and Total Area of Each Orifice	Pow (numbered fro	m lowest to highest	+)						
	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)	1
Stage of Orifice Centroid (ft)	0.00	0.50	1.00						
Orifice Area (sq. inches)	1.90	1.90	1.90						1
		•				•		•	-
	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)]
Stage of Orifice Centroid (ft)									
Orifice Area (sq. inches)									
ser Input: Vertical Orifice (Circular or Rectangula	<u>ar)</u>		-				Calculated Paramet	ters for Vertical Orif	<u>ice</u>
	Zone 2 Circular	Not Selected					Zone 2 Circular	Not Selected	
Invert of Vertical Orifice =	1.64	N/A	ft (relative to basin	bottom at Stage =	0 ft) Ve	rtical Orifice Area =	0.03	N/A	ft ²
Depth at top of Zone using Vertical Orifice =	3.06	N/A	ft (relative to basin	bottom at Stage =	0 ft) Vertica	al Orifice Centroid =	0.10	N/A	feet
Vertical Orifice Diameter =	2.33	N/A	inches						

User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir and No Outlet Pipe)

 User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir and No Outlet Pipe)
 Calculated Parameters for Overflow Weir

 Zone 3 Weir
 Not Selected
 Zone 3 Weir
 Not Selected

 Overflow Weir Front Edge Height He =
 3 07
 N/A
 ft (relative to basin bettern at Stage = 0.ft)

Overflow Weir Front Edge Height, Ho =	3.07	N/A	ft (relative to basin bottom at Stage = 0 ft) Height of Grate Upper Edge, $H_t =$	3.07	N/A	feet
Overflow Weir Front Edge Length =	5.67	N/A	feet Overflow Weir Slope Length =	2.92	N/A	feet
Overflow Weir Grate Slope =	0.00	N/A	H:V Grate Open Area / 100-yr Orifice Area =	17.14	N/A	
Horiz. Length of Weir Sides =	2.92	N/A	feet Overflow Grate Open Area w/o Debris =	11.52	N/A	ft ²
Overflow Grate Type =	Type C Grate	N/A	Overflow Grate Open Area w/ Debris =	5.76	N/A	ft ²
Debris Clogging % =	50%	N/A	%			_

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Res	trictor Plate, or Re	<u>ctangular Orifice)</u>	Calculated Parameter	Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate		
	Zone 3 Restrictor	Not Selected			Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	0.25	N/A	ft (distance below basin bottom at Stage =	= 0 ft) Outlet Orifice Area =	0.67	N/A	ft ²
Outlet Pipe Diameter =	18.00	N/A	inches	Outlet Orifice Centroid =	0.35	N/A	feet
Restrictor Plate Height Above Pipe Invert =	7.30		inches Half-Cent	tral Angle of Restrictor Plate on Pipe =	1.38	N/A	radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage=	4.00	ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length =	33.00	feet
Spillway End Slopes =	4.00	H:V
Freeboard above Max Water Surface =	2.00	feet

Calculated Parameters for Spillway

Spillway Design Flow Depth=	0.50	feet
Stage at Top of Freeboard =	6.50	feet
Basin Area at Top of Freeboard =	1.08	acres
Basin Volume at Top of Freeboard =	4.65	acre-ft

Routed Hydrograph Results	The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).								
Design Storm Return Period =	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
One-Hour Rainfall Depth (in) =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52	3.14
CUHP Runoff Volume (acre-ft) =	0.368	1.394	0.989	1.279	1.512	1.776	2.035	2.331	2.990
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	0.989	1.279	1.512	1.776	2.035	2.331	2.990
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A	0.1	0.1	0.2	1.8	3.7	6.0	11.1
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A							
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.01	0.01	0.02	0.15	0.30	0.49	0.89
Peak Inflow Q (cfs) =	N/A	N/A	15.7	19.9	22.9	28.0	32.1	37.6	48.2
Peak Outflow Q (cfs) =	0.2	0.5	0.4	0.4	0.6	2.9	5.0	6.0	9.6
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	3.1	3.2	1.6	1.4	1.0	0.9
Structure Controlling Flow =	Plate	Vertical Orifice 1	Vertical Orifice 1	Vertical Orifice 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Outlet Plate 1	Spillway
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	N/A	0.0	0.2	0.4	0.5	0.5
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	37	65	57	63	68	67	66	65	64
Time to Drain 99% of Inflow Volume (hours) =	40	72	63	70	75	75	75	74	73
Maximum Ponding Depth (ft) =	1.63	3.06	2.46	2.82	3.10	3.26	3.37	3.59	4.10
Area at Maximum Ponding Depth (acres) =	0.53	0.80	0.75	0.78	0.81	0.82	0.83	0.85	0.89
Maximum Volume Stored (acre-ft) =	0.371	1.397	0.925	1.207	1.429	1.559	1.642	1.826	2.268

Revise grading to include only historic tributary area or acquire downstream drainage easements and address stable conveyance the highlighted cells are too high revise as appropriate

DETENTION BASIN OUTLET STRUCTURE DESIGN

DETENTION BASIN OUTLET STRUCTURE DESIGN Outflow Hydrograph Workbook Filename:

Inflow Hydrographs

	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.22	0.02	0.70
	0:15:00	0.00	0.00	1.95	3.17	3.92	2.63	3.27	3.20	4.55
	0:20:00	0.00	0.00	6.82	8.91	10.44	6.57	7.63	8.18	10.61
	0:25:00	0.00	0.00	13.74	17.90	21.16	13.46	15.52	16.54	21.33
	0:30:00	0.00	0.00	15.67	19.86	22.93	25.94	29.91	33.12	42.70
	0:35:00	0.00	0.00	14.11	17.63	20.26	27.96	32.14	37.61	48.23
	0:40:00	0.00	0.00	12.35	15.18	17.42	26.04	29.92	34.98	44.82
	0:45:00	0.00	0.00	10.35	12.99	15.03	22.64	25.98	31.21	40.04
	0:50:00	0.00	0.00	8.71	11.21	12.79	20.01	22.93	27.39	35.17
	0:55:00	0.00	0.00	7.54	9.69	11.17	16.80	19.21	23.45	30.07
	1.00.00	0.00	0.00	6.74	8.64	10.09	14.38	16.44	20.53	26.31
	1:10:00	0.00	0.00	5.00	6.92	9.10	12.09	14.49	15.32	19 59
	1:15:00	0.00	0.00	4.25	5.93	7.39	9.19	10.45	12.53	15.99
	1:20:00	0.00	0.00	3.57	5.03	6.39	7.47	8.47	9,68	12.31
	1:25:00	0.00	0.00	3.17	4.49	5.50	6.11	6.90	7.39	9.37
	1:30:00	0.00	0.00	2.96	4.21	4.95	5.06	5.71	5.91	7.47
	1:35:00	0.00	0.00	2.85	4.03	4.59	4.40	4.96	5.02	6.33
	1:40:00	0.00	0.00	2.78	3.62	4.32	3.97	4.48	4.44	5.58
	1:45:00	0.00	0.00	2.73	3.31	4.13	3.68	4.14	4.05	5.07
	1:50:00	0.00	0.00	2.70	3.08	4.00	3.48	3.92	3.77	4.72
	1:55:00	0.00	0.00	2.35	2.90	3.80	3.35	3.77	3.58	4.46
	2:00:00	0.00	0.00	2.06	2.69	3.45	3.25	3.66	3.45	4.30
	2:05:00	0.00	0.00	1.53	2.00	2.55	2.42	2.73	2.57	3.20
	2.10.00	0.00	0.00	1.12	1.45	1.84	1.75	1.97	1.86	2.31
	2.13.00	0.00	0.00	0.80	0.73	0.04	0.00	1.42	1.35	1.00
	2:25:00	0.00	0.00	0.39	0.75	0.66	0.90	0.70	0.68	0.84
	2:30:00	0.00	0.00	0.27	0.34	0.45	0.44	0.49	0.47	0.58
	2:35:00	0.00	0.00	0.17	0.23	0.30	0.30	0.33	0.32	0.39
	2:40:00	0.00	0.00	0.10	0.14	0.18	0.18	0.21	0.20	0.24
	2:45:00	0.00	0.00	0.05	0.07	0.09	0.10	0.11	0.10	0.13
	2:50:00	0.00	0.00	0.02	0.03	0.03	0.04	0.04	0.04	0.05
	2:55:00	0.00	0.00	0.00	0.00	0.01	0.01	0.01	0.01	0.01
	3:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3.13.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:15:00 5:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

DETENTION BASIN OUTLET STRUCTURE DESIGN MHFD-Detention, Version 4.06 (July 2022)

Summary Stage-Area-Volume-Discharge Relationships

The user can create a summary S-A-V-D by entering the desired stage increments and the remainder of the table will populate automatically. The user should graphically compare the summary S-A-V-D table to the full S-A-V-D table in the chart to confirm it captures all key transition points.

Stage - Storage	Stage	Area	Area	Volume	Volume	Total Outflow	
Description	[ft]	[ft ²]	[acres]	[ft ³]	[ac-ft]	[cfs]	
	0.00	0	0.000	0	0.000	0.00	
	0.00	0	0.000	216	0.000	0.00	For best results, include the
	0.20	2,163	0.050	216	0.005	0.03	stages of all grade slope
	0.40	4,325	0.099	865	0.020	0.04	from the S-A-V table on
	0.60	6,488	0.149	1,946	0.045	0.07	Sheet 'Basin'.
	0.80	8,650	0.199	3,460	0.079	0.09	
	1.00	10,813	0.248	5,406	0.124	0.11	Also include the inverts of all
	1.20	14,768	0.339	7,964	0.183	0.15	outlets (e.g. vertical orifice,
	1.40	18,723	0.430	11,313	0.260	0.18	where applicable).
	1.60	22,679	0.521	15,454	0.355	0.20	
	1.80	26,634	0.611	20,385	0.468	0.25	-
	2.00	30,589	0.702	26,107	0.599	0.30	-
	2.20	31,420	0.721	32,308	0.742	0.34	-
	2.40	32,251	0.740	38,675	0.888	0.38	-
	2.60	33,082	0.759	45,208	1.038	0.41	-
	2.80	33,913	0.779	51,908	1.192	0.43	-
	3.00	34,744	0.798	58,774	1.349	0.46	-
	3.20	35,462	0.814	65,794	1.510	1.78	-
	3.40	36,179	0.831	72,958	1.675	5.75	-
	3.60	36,897	0.847	80,266	1.843	6.05	-
	3.80	37,614	0.864	87,717	2.014	6.22	-
	4.00	38,332	0.880	95,312	2.188	6.39	-
	4.20	39,072	0.897	103,052	2.366	15.58	-
	4.40	39,812	0.914	110,940	2.547	32.73	-
	4.60	40,553	0.931	118,977	2.731	55.55	-
	4.80	41,293	0.948	127,161	2.919	83.35	-
	5.00	42,033	0.965	135,494	3.111	115.76	-
	5.20	42,796	0.982	143,977	3.305	152.59	-
	5.40	43,559	1.000	152,612	3.503	193.71	-
	5.60	44,321	1.017	161,400	3.705	239.04	-
	5.80	45,084	1.035	170,341	3.910	288.54	-
	6.00	45,847	1.053	179,434	4.119	342.18	-
	6.20	46,331	1.064	188,652	4.331	399.96	-
	6.40	46,816	1.075	197,967	4.545	461.88	-
	6.50	47,058	1.080	202,660	4.652	494.39	
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4-Way Commercial Preliminary Drainage Report Project No: 2202654

Provide all calculations and analyses for culverts, swales, offsite conveyances, TSB spillways, etc.

APPENDIX E – REFERENCE MATERIAL

MDDP AMMENDMENT/PRELIMINARY/FINAL DRAINAGE REPORT FOR STAPLETON DRIVE FROM BANDANERO DR TO US HWY 24 EL PASO COUNTY, COLORADO

November 2009 Revised May 2010

Prepared For:

935 Development, Inc. PO Box 50223 Colorado Springs CO 80949 (719) 447-8773

Prepared By:

JR ENGINEERING 7200 S Alton Way, Suite C100 Centennial, CO 80112 (303) 740-9393

Job No. 29931.25

4-Way Commercial Preliminary Drainage Report Project No: 2202654

APPENDIX F – DRAINAGE MAPS

EFN Xrefs: xv-Ititil-2564: xv-dson-2564: xv-row-2564: drain map legend: xqt-1-dhf

