FINAL DRAINAGE REPORT FOR DWIRE STORAGE YARD FILING NO. 1

EL PASO COUNTY, COLORADO

JANUARY 2021

Prepared for: **DWIRE Earthmoving, Inc.** 6799 Bismark Road, Suite C Colorado Springs, CO 80922 (719)-574-7123

Prepared by:



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Project #43-117

PCD Project No. MS-20-002

FINAL DRAINAGE REPORT FOR DWIRE STORAGE YARD FILING NO. 1

DRAINAGE PLAN STATEMENTS

ENGINEERS STATEMENT

The attached drainage plan and report was prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the County for drainage reports and said report is in conformity with the applicable master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omission on my part in preparing this report.



Virgil A. Sanchez, P.E. #37160 For and on Behalf of M&S Civil Consultants, Inc

DEVELOPER'S STATEMENT

I, the developer have read and will comply with all the requirements specified in this drainage report and plan.

BY:

TITLE:Jeff Dwire, OwnerDATE:2-1-21

ADDRESS: Dwire Earthmoving, Inc. 6799 Bismark Road, Suite C Colorado Springs, CO 80922

EL PASO COUNTY'S STATEMENT

Filed in accordance with the requirements of El Paso County Land Development Code, Drainage Criteria Manual Volumes 1 and 2, and the Engineering Manual, as amended.

BY:

DATE:_____

Jennifer Irvine, P.E. County Engineer

CONDITIONS:

FINAL DRAINAGE REPORT FOR DWIRE STORAGE YARD FILING NO. 1

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FINAL DRAINAGE REPORT FOR DWIRE STORAGE YARD FILING NO. 1

PURPOSE

This document is intended to serve as the Final Drainage Report for the DWIRE Storage Yard Filing No. 1. The purpose of this document is to identify and analyze the on and offsite drainage patterns and to ensure that post development runoff is routed through the site safely and in a manner that satisfies the requirements set forth by the El Paso County Drainage Criteria Manual. The development plan for Lot 1 will consist of a gravel storage yard with office/warehouse buildings, asphalt, curb, lighting, and Tract B Full Spectrum Detention Pond and landscaping. Tract A will include areas within the 100 year floodplain and is identified as "No Build Area and No Disturbance" and Tract C is proposed as a gravel storage yard and can be replatted in the future, upon which an updated drainage letter shall be required for review and approval. The parcel is zoned "I-3" and the proposed use is permissible within the Industrial zoning criteria.

GENERAL LOCATION AND DESCRIPTION

DWIRE Storage Yard Filing No. 1 is located in the southeast quarter of the southwest quarter of Section 28, Township 13 South, Range 65 West of the 6th P.M. in El Paso County, Colorado. The parcel is bound to the north by an existing and abandoned railroad embankment approximately 100 feet from the northern boundary and the East Fork Sand Creek Sub-tributary, to the west by Transit Mix property and East Fork Sand Creek Sub-tributary, to the south by Lot 7 of the Marksheffel Industrial Park, Capitol Drive, and to the east by Timberline Storage Yard. As shown on the enclosed FIRM panel, a channel known as the East Fork of Sand Creek Sub-tributary flows from north to south approximately 85 feet from the western boundary of the site. The site is located within the greater Sand Creek Drainage Basin and is tributary to the Sand Creek Channel via the East Fork Sand Creek Sub-Tributary. A vicinity map showing the location of the proposed development has been provided in the appendix of this report.

The proposed storage yard development and improvements will be constructed on approximately 8.356 acres of the 19.362 acre parcel. The site is currently zoned "I-3" which is associated with industrial development. In the existing condition, both the parcel and offsite contributing watershed lands are sparsely vegetated, with ground cover consisting primarily of native grasses ranging in density from fair to good. The proposed development will consist of a gravel storage yard with two office/warehouse buildings, gravel and asphalt parking areas, lighting, landscaping, and an access road. Slopes across the development typically range between 2% to 5%. Offsite flows reaching development are contributed in part from areas of Timberline Storage Yard along the eastern boundary and from small portions of unplatted property to the north. Flows produced within the development will be collected by proposed storm sewer improvements, swales, riprap rundowns, and will be routed to a proposed full spectrum detention (FSD) pond located at the southern boundary of the development.

SOILS

Soils for this project are delineated by the map in the appendix as Blendon Sandy Loam (10) which is characterized as Hydrologic Soil Types "B". Soils in the study area are shown as mapped by Soil Conservation Service in the "Soils Survey of El Paso County Area".

HYDROLOGIC CALCULATIONS

Hydrologic calculations were performed using the El Paso County and City of Colorado Springs Storm Drainage Design Criteria manual and where applicable the Urban Storm Drainage Criteria Manual. The Rational Method was used to estimate stormwater runoff anticipated from design storms with 5-year and 100-year recurrence intervals.

HYDRAULIC CALCULATIONS

Hydraulic calculations were estimated using the Manning's Formula and the methods described in the El Paso County and City of Colorado Springs Storm Drainage Design Criteria manual. The relevant data sheets are included in the appendix of this report.

FLOODPLAIN STATEMENT

A portion of the site lies within the 100 year floodplain according to the Federal Emergency Management Agency (FEMA) Flood Insurance Rate Map (FIRM) Panel No. 08041C0543 F, effective date March 17, 1997 and the more recent FIRM Panel No. 08041C0543 G, effective date December 7, 2018. Base Flood Elevation (BFE) lines from FIRM Panel No. 08041C0543 F (NGVD29) are used for hydraulic calculations, drainage maps, and a discussion within this report. No development is anticipated to occur within the floodplain located at the northwest corner of the site. See Proposed Drainage Map and the FIRM Panels located in the appendix of this report for details. Tract A is provided on the plat for the portion of the lot encumbered by the floodplain. The Floodplain application and Floodplain permit are included in this report, in the Floodplain Map section in the appendix. No portions of the local floodplain administrator in accordance with FEMA policy.

DRAINAGE CRITERIA

This drainage analysis has been prepared in accordance with the current El Paso County Drainage Criteria Manual and where applicable the City of Colorado Springs DCM Volume 1 dated May 2014 effective January 2015. Hydrologic calculations were performed to determine runoff quantities for the 5-year and 100-year frequency storms for developed conditions using the Rational Method as required for basins having areas less than 130 acres (in accordance with Chapter 6 of the City of Colorado Springs DCM Volume 1). Full spectrum detention facilities have been designed in accordance with Section 3.2.1. of Chapter 13 of the City of Colorado Springs DCM Volume 1, dated May 2014, effective January 31, 2015 and Urban Drainage and Flood Control District Manuals dated January 2016.

FOUR STEP PROCESS

- Step 1: Employ Runoff Reduction Practices. Approx. 1.469 acres of the proposed development 19.362 acres is being set aside for a Full Spectrum Detention (FSD) Pond. Whenever possible, runoff produced within developable area containing impervious surfaces will be routed through landscaped areas or earthen swales (grass-lined where slope exceeds 2%) to minimize direct connection of impervious surfaces.
- **Step 2: Stabilize drainage ways** –The DWIRE Storage Yard site proposes a Full Spectrum Detention (FSD) Pond to control developed runoff that is discharging to the East Fork Sand Creek Sub-Tributary located approximately 85-170 feet from the northern and western boundaries of the subject site. The FSD outlet structure has been designed to drain the water quality event storm in 40 hours, while reducing the 100 year peak discharge to approximately 90% of the predevelopment conditions. The development of this site is not anticipated to have negative effects on downstream drainageways. The existing channel embankment has been stabilized at the FSD pond's emergency spillway and where the outlet pipe from the pond enters the channel. Per the DBPS the existing channel is to remain, and no improvements are necessary for this reach of the channel (See "Referenced Reports" in the Appendix, Sheets EF-27 & EF-28).
- **Step 3: Provide water quality capture volume.** A Full Spectrum Detention Pond is proposed to reduce peak discharge rates and provide water quality treatment. The WQCV will be released over a 40 hour period while larger event storms will be released in periods of times between 64-80 hours.
- **Step 4: Consider Need for Industrial and Commercial BMP's** This submittal provides a final grading and erosion control plans with BMPs in place. The proposed project will use silt fence, inlet protection, straw bales, a vehicle tracking control pad, and concrete washout area, mulching and reseeding to mitigate the potential for erosion across the site. DL Holdings, LLC shall be responsible for existing and potentially necessary the BMPs for the site including staging, storage and stockpile areas as determined by the contractor. Individual lot owners will be responsible for additional permanent BMPs if necessary because of site uses.

EXISTING DRAINAGE CONDITIONS

The DWIRE Storage Yard Filing No. 1site consists of 19.362 acres situated south and east of the East Fork Sub-tributary of Sand Creek. There are no existing structures within the site. In accordance with the Engineering Criteria Manual (ECM) and Drainage Criteria Manual (DCM) an existing conditions hydrologic analysis was performed to determine existing flow quantities entering and exiting the subject site so a comparison to post development discharge rates could be made. As shown on the enclosed Existing Drainage Map (located in the appendix of this report) the existing site terrain within the parcel generally slopes from north to south at grades that vary between 2% to 5%. An existing and abandoned railroad embankment lies approximately 100 feet from the northern boundary of the site and protects the site from the East Fork Sand Creek Sub-tributary and offsite runoff. The East Fork Sand Creek Sub-tributary continues from north to south approximately 85 feet from the western boundary of the site. A site visit was made and it was observed that existing channel banks appear to be stable with established vegetation and minimal scour. Per the DBPS the existing channel is to remain, and no improvements are necessary for this reach of the channel (See "Reference Reports" in the Appendix, Sheets EF-27 & EF-28).

An overlay of the 100 yr floodplain (Zone AE) is shown on the Existing Drainage Map and the Floodplain Map, of which 0.28 acres overlaps the northwest corner of the site. Refer to the enclosed Existing Drainage Map for specific flow rates associated with Existing Basins and Design Points.

Design Point 1 consists of native grass covered un-platted land located along the east parcel property boundary. Runoff produced by **Basins OS1, OS2 and A**, has been calculated to be 0.8 cfs in the 5-year storm event and 5.10 cfs in the 100-year storm event. Runoff from these basins is conveyed as sheet flow and earthen swale to the east towards **Design Point 1**. These flows will combine with flows from the Timberline storage yard and be routed via a swale to and be treated by the Timberline Storage Yard Full Spectrum Detention Pond 1. The "Amendment No.1 to the Final Drainage Report for Timberline Storage Yard", dated March 2020, by M&S Civil Consultants, Inc. accounts for these flows and the Full Spectrum Detention Pond 1 was designed with consideration to this tributary area (See Timberline Storage Yard Proposed Drainage Map, Basins OS2).

Design Point 2 consists of grass covered un-platted land and a portion of Timberline Storage Yard (Basin OS3). Runoff produced by **Basins A1 and OS3**, has been calculated to be 3.6 cfs in the 5-year storm event and 7.5 cfs in the 100-year storm event. Runoff from these basins is conveyed as sheet flow to the east towards **Design Point 2**. Runoff from Basin OS3 and A1 continues south on existing Capital Drive.

Design Point 3 consists of native grass covered un-platted land located central portion of the property and along the south and west property boundary. Runoff produced by **Basins OS4, OS5 and B**, has been calculated to be 2.6 cfs in the 5-year storm event and 17.2 cfs in the 100-year storm event. Runoff from these basins is conveyed as sheet flow to the south and is captured by an existing swale on the southern property boundary and routed west towards **Design Point 3**. This runoff outfalls into the East Fork Sand Creek Sub-tributary.

Design Point 4 consists of native grass covered un-platted land located at the northwest portion of the property boundary. Runoff produced by **Basins OS6 and C**, has been calculated to be 0.4 cfs in the 5-year storm event and 2.4 cfs in the 100-year storm event. Runoff from these basins is conveyed as sheet flow to the northwest towards **Design Point 4**. This runoff outfalls into the East Fork Sand Creek Sub-tributary.

Design Point 5 consists of native grass covered un-platted land located at the west portion of the property boundary. Runoff produced by **Basins OS7, D, Design Point 3 and Design Point 4,** has been calculated to be 4.5 cfs in the 5-year storm event and 29.3 cfs in the 100-year storm event. Runoff from these basins is conveyed as sheet flow to the southwest towards **Design Point 5.** This runoff outfalls into the East Fork Sand Creek Sub-tributary. The cumulative runoff values are from the onsite flows and do not include the East Fork Sand Creek Sub-tributary upstream flows. The values provided by FEMA for Sand Creek East Fork Subtributary at confluence with Sand Creek East Fork are 1970 cfs for the 100 year event.

PROPOSED DRAINAGE CHARACTERISTICS

General Proposed Conditions Drainage Discussion

The proposed storage yard development and improvements will be constructed on approximately 8.356 acres of the 19.362 acre parcel. The majority of the site has been accounted for as a storage yard and the remaining northern portion identified as Tract C being considered as pastureland/undeveloped is shown on the Proposed Drainage Map. Refer to the Proposed Drainage Map for weighted runoff coefficients for the

site. Proposed drainage patterns generally remain consistent with those in the existing condition with surface runoff traveling north to south. A swale is proposed on the western boundary of the site to capture and route runoff south to the Full Spectrum Detention (FSD) pond. The combined onsite runoff, offsite runoff from Timberline Storage Yard, and adjacent Basins OS3 & OS4 are conveyed to the proposed FSD pond. The runoff reaching the pond will be detained and discharged via a staged outlet structure and proposed 24" RCP storm system to the East Fork Sand Creek Sub-Tributary below historic rates. The outfall into the East Fork Sand Creek Sub-Tributary channel is armored with a proposed riprap pad and is grading away from main flows within the channel. Type M riprap protection is also proposed to stabilize the emergency spillway bank and all proposed grading around the outfall. Refer to the Proposed Drainage Map in the appendix for an illustration of the proposed site drainage patterns. A detailed description of the proposed drainage characteristics follows:

Proposed Conditions Detailed Drainage Discussion

Design Point 1, 2.59 acres, consists of offsite **Basins OS1** and onsite **Basin A**. Surface runoff, from these contributing areas, generally flows from north to south and exits the site at **Design Point 1**, where it combines with flows from neighboring Timberline Storage Yard and ultimately enters the Full Spectrum Detention Pond 1 on the Timberline Storage Yard site. The Proposed Drainage Map overlays Timberline Basin OS2 boundary in a gray dashed line type. Any discrepancy is minor, and within tolerance, with no significant drainage affects and changes to runoff values. The "Amendment No.1 for the Final Drainage Report for Timberline Storage Yard", dated March 2020, by M&S Civil Consultants, Inc. accounts for these flows and the Full Spectrum Detention Pond 1 was designed with consideration to this undeveloped tributary area (See Timberline Storage Yard Proposed Drainage Map, Basin OS2, referenced in the appendix). Onsite Basin A is to remain undeveloped at this time and runoff values are Q5=4.1 cfs and Q100=9.3 cfs have been calculated for **DP1**. The Timberline pond has been built.

Design Point 2, 2.89 acres, consists of offsite **Basin OS2** and onsite **Basin B**. Developed runoff of Q5=8.6 cfs and Q100=16.7 cfs has been calculated for **DP2**. Runoff from the existing neighboring Timberline Storage Yard improvements (parking lot, gravel lot, building) within offsite Basin OS2 travels as sheet flow west to onsite Basin B. All tributary runoff will be routed via a 6' wide pan, curb and gutter and collected by a 10' CDOT Type R sump inlet located at a low point at **DP2**. Captured flows are routed to the east forebay of the FSD pond and are treated before being discharged to the East Fork Sand Creek Sub-Tributary.

Design Point 3, 2.74 acres, consists of onsite **Basin B1**. Developed runoff of Q5=6.1 cfs and Q100=12.1 cfs has been calculated for **DP3**. Existing and proposed grading conveys runoff south (to **DP3**) where a localized swale captures all sheet and concentrated flows conveying them south into the FSD pond via a 3' wide trapezoidal riprap rundown. Energy associated with the runoff is dissipated by the trapezoidal rundown and outfalls into a concrete forebay located at the bottom of the rundown. All runoff tributary to **DP3** is treated within the FSD pond prior to being discharged to the East Fork Sand Creek Sub-Tributary.

Design Point 4, 10.67 acres, consists of onsite **Basins B2** and **Basin D**. Developed runoff of Q5=20.4 cfs and Q100=40.5 cfs has been calculated for **DP4**. A proposed swale along the western property boundary prevents any runoff produced within **Basin D** from traveling offsite. A proposed swale located along the north side of the larger proposed building routes runoff west where it combines with flows in the aforementioned swale prior to reaching **DP4**. At **DP4**, a 3' wide trapezoidal riprap rundown conveys concentrated flows south into the FSD pond. Energy associated with the runoff is dissipated by the

trapezoidal rundown and outfalls into a concrete forebay located at the bottom of the rundown. All runoff tributary to DP4 is treated within the FSD pond prior to being discharged to the East Fork Sand Creek Sub-Tributary.

Design Point 5, 1.34 acres, consists of Basin OS4 and Basin B3. Developed runoff from Design Points DP2, DP3, DP4, offsite Basins OS4 and Basin B3 contribute to the proposed FSD pond at DP5 at a peak flow rate of Q5=32.8 cfs, Q100=66.3 cfs. The proposed full spectrum detention pond was sized utilizing the UDFCD MFHD-Detention Worksheet, Ver 4.03. Based upon the contributing watershed acreage, characteristics, and imperviousness of the site, the pond requires a minimum of 2.352 acre feet of storage in the 100-year event and was limited to a peak discharge of 17.5 cfs. A proposed outlet structure with a 24" RCP storm pipe and restrictor plate is recommended to meet the allowable discharge rate. All treated discharge from the FSD pond is released to the East Fork Sand Creek Sub-Tributary via a flared end section and riprap pad to dissipate energy and maintain integrity of the outfall. The low tailwater basin, $D_{50}=12$ ", riprap and flared end section have been graded into the channel bank away from higher velocity main channel flows. In the case that the outlet structure were to become clogged, 100 year flows will be released through a 25.5' wide emergency spillway and rundown armored with Type M riprap, $D_{50}=12$ ". The emergency spillway is designed with a foot of freeboard in the 100-year event and has a crest elevation of 6533.15. This crest elevation is 5' above the 100-year FEMA water surface elevation of 6528.0. A hydraulic analysis for the FSD pond outlet structure and 24" RCP was performed in StormCAD and is enclosed in the appendix. The FEMA 100-year water surface elevation of 6528.0 was used as the starting hydraulic grade line (HGL) elevation. The results show that the FSD pond remains functional in the 100year event and the outlet structure is able to discharge flows to the East Fork Sand Creek Sub-Tributary.

Design Point 6, 1.44 acres, consists of offsite **Basin OS5** and **Basin C**. Developed runoff of Q5=0.5 cfs and Q100=3.2 cfs has been calculated for **DP6**. As shown on the Proposed Drainage Map, runoff from **DP6** enters the East Fork Sand Creek Sub-Tributary channel and continues south. The FEMA 100 yr floodplain, Zone AE, has been overlayed on the Proposed Drainage Map and crosses the northwest corner of the site within Basin C. Tract A within the plat has been dedicated to this area and no development is anticipated to occur within the floodplain, per plat restriction.

Design Point 7, 4.64 acres, consists of **Basin OS6.** Developed runoff from Design Point **DP6** and Pipe Run **PR2** contribute to the existing East Fork Sand Creek Sub-tributary at **DP7** at a peak flow rate of Q5=2.3 cfs, Q100=29.7 cfs. The flows released do not exceed the flows calculated in the historic condition. The cumulative runoff values are from the onsite flows and do not include the East Fork Sand Creek Sub-tributary upstream flows. The FEMA 100 yr floodplain, Zone AE, has been overlayed on the Proposed Drainage Map along with the associated cross section IDs and water surface elevation markers. No grading is proposed within the floodplain with the exception of the emergency spillway from the proposed FSD pond and some cut around the FSD pond outfall to grade in the 24" RCP flared end section and riprap pad. Riprap is proposed in these areas to protect the FSD pond and all storm improvements discharging from the FSD pond to the East Fork Sand Creek Sub-Tributary channel. A floodplain development permit is included in the appendix on this report.

Basin OS3, 0.46 acres, consists of 4:1 vegetated slope with runoff of Q5=0.2 cfs and Q100=1.1 cfs has been calculated for **Basin OS3**. As shown on the Proposed Drainage Map, runoff from **Basin OS3** is released as sheet flow.

WATER QUALITY PROVISIONS AND MAINTENANCE

The proposed full spectrum detention (FSD) pond functions to provide detention and water quality for the proposed development. This full spectrum detention pond will function to treat approximately 19.362 acres of tributary area by providing 0.453 acre-feet of storage for the water quality event, 1.519 acre feet of storage at the EURV event storm and 2.352 acre-feet of storage in the 100-year event. The 25.5' wide emergency spillway is designed with a foot of freeboard in the 100-year event and has a crest elevation of 6533.15. This crest elevation is 5' above the 100-year FEMA water surface elevation of 6528.0. A hydraulic analysis for the FSD pond outlet structure and 24" RCP was performed and is enclosed in the appendix (Storm Cad). The FEMA 100-year water surface elevation of 6528.0 was used as the starting hydraulic grade line (HGL) elevation. The results show that the FSD pond remains functional in the 100-year event and the outlet structure is able to discharge flows to the East Fork Sand Creek Sub-Tributary. The sizing for the full spectrum detention facility has been determined using the guidelines set forth in the Urban Drainage and Flood Control District Criteria Manual. Refer to the UDFCD MHFD-Detention, Version 4.03, Excel Workbook located within the appendix of this report for calculations.

The proposed FSD pond will be private and shall be maintained by the property owner. Access shall be granted to the owner and El Paso County for access and maintenance of the private WQCV facility. A private maintenance agreement document shall accompany this report submittal.

EROSION CONTROL

It is the policy of the El Paso County that we submit a grading and erosion control plan with the drainage report. Proposed silt fence, vehicle traffic control, and concrete washout area are proposed as erosion control measures. The costs for these measures have been provided on the Grading and Erosion Control plan.

CONSTRUCTION COST OPINION

Item	Description	Qua	ntity	Unit Co	ost		Cost
1.	18" RCP	22	LF	\$40	/LF		\$880.00
2.	24" RCP	42	LF	\$50	/LF		\$2,100.00
3.	18" RCP FES	1	EA	\$800	/EA		\$800.00
4.	24" RCP FES	1	EA	\$900	/EA		\$900.00
5.	10' CDOT Type R Inlet	1	EA	\$5,000	/EA		\$5,000.00
6.	Type M riprap, 2' deep	255	CY	\$65	/CY		\$16,575.00
7.	FSD Pond (Inlcuding Outlet Struct, Access Road, Trickle Channel, Forebays)	1	EA	\$23,000	/EA		\$23,000.00
	• '					Total \$	\$49,255.00

Private Drainage Facilities (NON-Reimbursable):

M & S Civil Consultants, Inc. (M & S) cannot and does not guarantee the construction cost will not vary from these opinions of probable costs. These opinions represent our best judgment as design professionals familiar with the construction industry and this development in particular. The above and below is only an estimate of the facility cost and drainage basin fee amounts in 2020.

DRAINAGE & BRIDGE FEES – DWIRE STOREAGE YARD

This site is within the Sand Creek Drainage Basin. The 2020 (Resolution 19-441) Drainage and Bridge Fees per El Paso County for the DWIRE Storage Yard Filing No. 1 site are as follows:

Per DWIRE Storage Tract A (No build pe				oodp	,	al Area	19.362 <u>-0.432</u> 18.93	Acres
DWIRE STORAGE	E YARD F	ILIN	G NO. 1	FEES	S:			
Drainage Fees:	18.93	х	72.2%	\$	19,698.00	=		\$ 269,221.63
Bridge Fees:	18.93	х	72.2%	\$	8,057.00	=	75 ()	<u>\$ 110,118.73</u>
							Total	\$ 379,340.36

SUMMARY

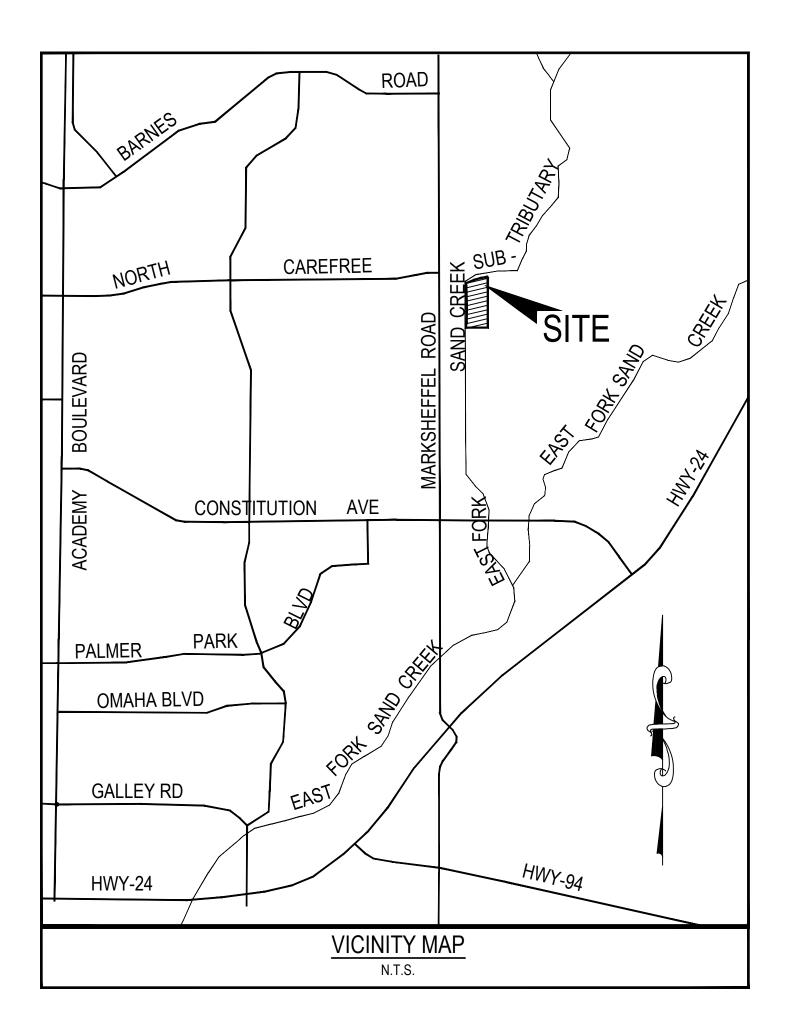
Per this final drainage report, the proposed drainage facilities recommended within this report will adequately convey, detain and route runoff from the planned development to the East Fork Sand Creek Sub-Tributary drainage way at peak flow rates which are below existing with no negative impacts on surrounding developments. All drainage facilities described herein and shown on the included Proposed Drainage Map (See Appendix), this final Drainage Report and site construction documents are simultaneous review. Tract C shall be identified on "No Build Area"(gravel-surfaced storage only) and Tract C can be replated in the future, upon which an updated drainage letter shall be required for review and approval. Care will be taken to accommodate overland emergency flow routes on site and temporary drainage conditions. The development of the DWIRE Storage Yard Filing No.1 site will not adversely affect adjacent or downstream properties.

REFERENCES

- 1.) "El Paso County and City of Colorado Springs Drainage Criteria Manuals".
- 2.) "Urban Storm Drainage Criteria Manual"
- 3.) SCS Soils Map for El Paso County.
- 4.) Flood Insurance Rate Map (FIRM), Federal Emergency Management Agency (Map No. 08041C0543F), Effective date March 17, 1997.
- 5.) Flood Insurance Rate Map (FIRM), Federal Emergency Management Agency (Map No. 08041C0543G), Effective date December 7, 2018.
- 6.) "Amendment No.1 to the Final Drainage Report for Timberline Storage Yard", dated March 2020, by M&S Civil Consultants, Inc.
- 7.) "Sand Creek Drainage Basin Planning Study, Preliminary Design Report", Revised March 1996, by Kiowa Engineering Corporation.

APPENDIX

VICINITY MAP



SOILS MAP



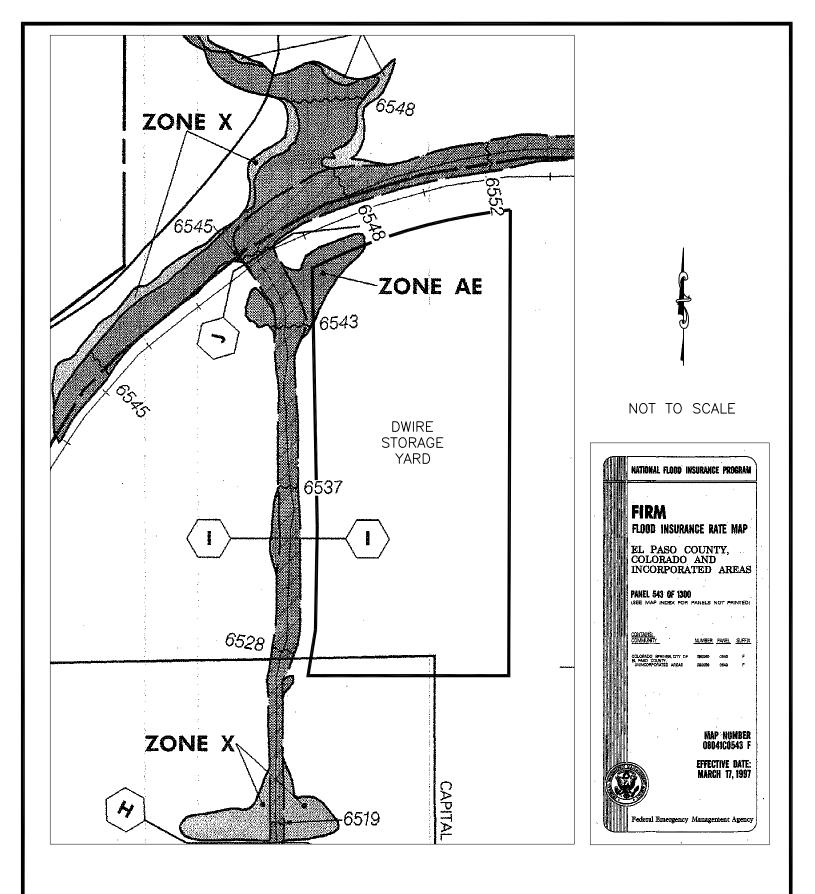
NOT TO SCALE



	Summary by Map Unit — El Paso County A	Area, Colorado (CO625)
Summary by Map Unit — E	l Paso County Area, Colorado (CO625)	
Map unit symbol	Map unit name	Rating
10	Blendon sandy loam, 0 to 3 percent slopes	В

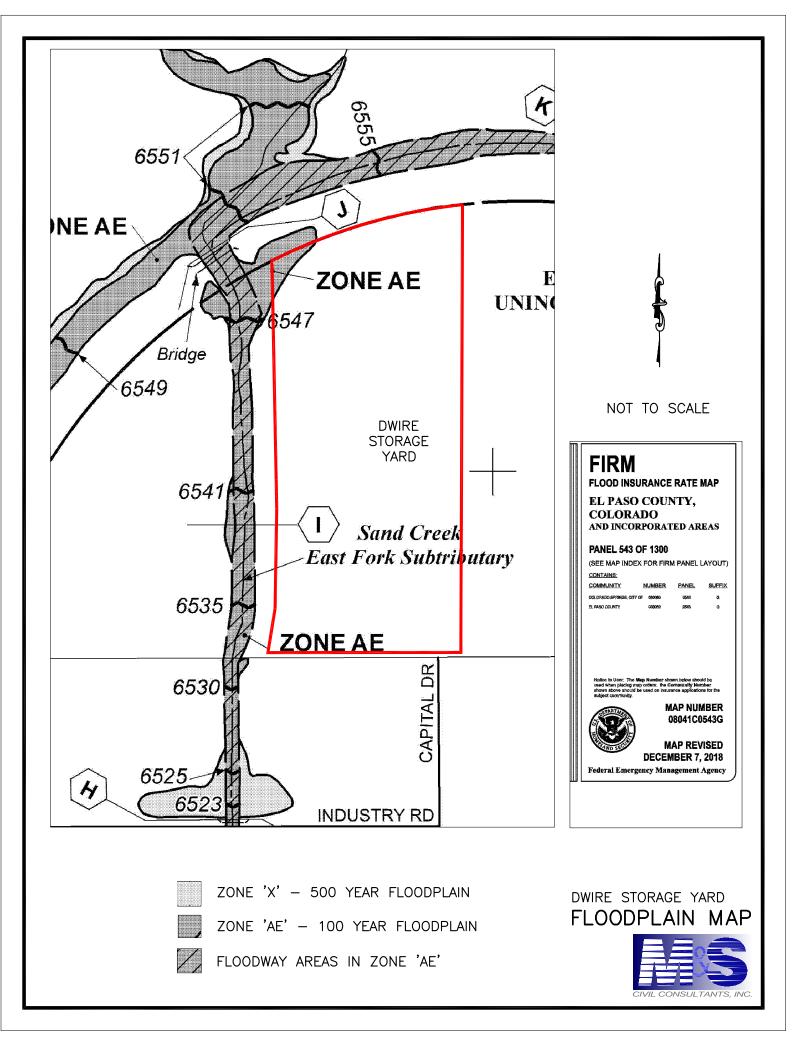


FIRM PANEL



ZONE 'X' – 500 YEAR FLOODPLAIN ZONE 'AE' – 100 YEAR FLOODPLAIN FLOODWAY AREAS IN ZONE 'AE'







January 31, 2020

Tim Emick 8110 Opportunity View Colorado Springs, CO 80939

Via Email temick@timberlinelandscaping.com

When replying, please refer to: DWIRE Storage Yard DAM Non-Jurisdictional Water Division 2 Water District 10

SUBJECT: Signed Notice of Intent to Construct a Non-Jurisdictional Water Impoundment Structure

Dear Mr. Emick:

Our office is in receipt of a Notice of Intent (NOI) to Construct a Non-Jurisdictional Water Impoundment Structure for the subject dam. The impoundments are to be located adjacent to East Fork of Sand Creek tributary to Fountain Creek, with the filling source to be Stormwater for Temporary Detention.

In accordance with Rule 11.1 of the Colorado Rules and Regulations for Dam Safety and Dam Construction, the hazard of this dam has been assessed as Low based on the construction drawing plans submitted with the NOI. A copy of the signed NOI is attached. An electronic copy will be maintained with the Division of Water Resources.

Please note the following:

- Location information has been corrected on your submission.
- This structure must be designed and constructed to standards outlined in 37-92-602(8) for stormwater detention facilities.
- Because this structure is located on a tributary to Fountain Creek, the structure can only operate pursuant a Colorado Discharge Permit System Municipal, Separate Storm Sewer System Permit issued by the Department of Public Health and Environment Pursuant to Article 8 of Title 25, C.R.S.
- In the event groundwater is encountered during construction of the pond, the pond must be backfilled so as not to expose groundwater until such time as: 1) a well permit has been obtained for the groundwater pond pursuant to CRS §37-90-137, or 2) the pond is lined in accordance with the document, <u>"State Engineer Guidelines for Lining Criteria for Gravel Pits,"</u> dated August 1999.

310 East Abriendo Avenue, Suite B, Pueblo, CO 81004 P 719.542.3368 F 719.544.0800 www.colorado.gov/waterJared S. Polis, Governor| Dan Gibbs, Executive Director| Kevin G. Rein, State Engineer/Director



The requirements and recommendations provided herein are based on our review of the safety and water administration aspects of the proposed dam and the information provided in the submitted NOI. These requirements and recommendations create no liability for the State of Colorado should the dam fail for any reason. Please be aware that it is in the owner's best interest to construct, operate, and maintain the structure in a safe manner, as he or she may be held liable in civil court for any downstream damages resulting from failure of the dam. A copy of Specifications for Construction of Non-Jurisdictional Dams is provided to assist you in the construction of a sound structure.

Finally, please be aware of any other permitting or regulatory requirements associated with the construction of a water impoundment structure, including but not limited to county and/or municipal regulations and wetland permitting through the U.S. Army Corps of Engineers (see www.usace.army.mil for regional contact information).

The plans reviewed in this determination are submitted as part of the Developmental Approval process. Prior to the operation of this structure, please provide notice of completion of construction and asconstructed plans in PDF form including as constructed Stormwater Detention and Infiltration Data Sheet. Additionally, prior to the operation of this structure, notice must be provided pursuant to 37-92-602(8)(d) to the substitute water supply plan notification list maintained by the state engineer pursuant to section 37-92-308 (6) for the water division in which the facility is located.

If you have any questions regarding this approval, please contact Water Commissioner, Doug Hollister, at (719) 227-5291 or via email to <u>doug.hollister@state.co.us</u>, or Dam Safety Engineer, John Hunyadi, at (719)-227-5294, or via email to <u>john.hunyadi@state.co.us</u>,

Sincerely,

Bill W. Jyner

Bill W. Tyner, P.E. Division Engineer, Division 2

Enc:

Signed Notice of Intent to Construct a Non-Jurisdictional Water Impoundment Structure Specifications for Construction of Non-Jurisdictional Dams Completion of Construction Form

ec: John Hunyadi, P.E., Dam Safety Engineer Doug Hollister, District 10 Water Commissioner

Laserfiche File



COMPLETION OF CONSTRUCTION

DAM ID. 100541

Upon the completion of the <u>DWIRE Storage Yard DAM</u>, Subject of the Notice of Intent to Construct a Non-Jurisdictional Dam under the Receipt above, location in Sec. <u>28</u> ______Twp. <u>13 S</u> Rng. <u>65 W</u>; UTM NAD83, Northing 4304006, Easting 527860.

Indicate in the blank at the bottom of this form, the date of completion of construction and return to:

Colorado Division of Water Resources Division 2 310 East Abriendo Ave, Suite B Pueblo, CO 81004

Date of Completion: _____

Signature of Owner

Date





NON-JURISDICTIONAL WATER IMPOUNDMENT STRUCTURE¹

This notice is required per Section 37-87-125, C.R.S. (1998) and

must be submitted to the Division Engineer's Office a minimum of 45 days prior to construction.

OWNER INFORMATION

Name: <u>Tim Emick</u> Telephone	e/E-Mais: (19)111	TATLY TEMIL	r e i imiderline made
Address: 8110 OPORTUNITY VIEW Co			
Street / P.O. Box/ Rural Route Cit	ty	State	Zip Code
Responsible Person: Tam Emack Te	lephone/E-Mail: () SAME !	
Address: Street / P.O. Box/ Rural Route Cit		State	7 in Code
	•		Zip Code
Contractor: <u>SANE</u> Telephon	ne/E-Mail: ()	/	
STRUCTURE INFORMATION			
Name of Dam: DWIRE STOLAGE YARD	Water Divisio	on: <u> </u>	/ater District: <u>CS</u>
Location: (Provide Section, Township, Range, and GPS Po	int taken at crest of d	am above stream	line/outlet)
- Section: 28_, Township: /3 South, Range: 65 Most			
- Northing 527860meters, Easting 430400		ers (Datum should	l be UTM, NAD 83)
Dam Dimensions:	1.00	4.1	
- Vertical Height ² : <u>5,08</u> ft., Length: <u>85</u> ft., Crest Wi	dth: <u>17</u> _ft., Slope	es: U/S: <u>7.: 1 (</u> H:	:1V), D/S <u> </u>
Reservoir:			
- Surface Area ¹ : <u>0.7</u> acres, Capacity ¹ : <u>1.6(9</u> *(If drainage area is unknown leave blank and a spillway s	acre-feet, Drai: ize will be assigned):	nage Area*:9	. <u>362</u> acros
Emergency Spillway: (See Table 1, Spillway Sizing Guidelin	nes)	#	
- Bottom Width: ft., Side Slopes:4; \	_H:1V, Freeboard ³ :_	0.95 ft	
Outlet Conduit Type:, Siz	ze: <u>24 ^{//} inches, L</u> o	ocation: WEST	SIDE
Stream Name or Water Source4: SAND CREEL E. TRI	8 Proposed Wate	er Use: 51	ornwater
Water Court Case or WDID :		2	$\sum I I$
(Water District Identification Number)			1/1/20'
ii a	Signature of O	HEDOF	Deta
office Use Only			Date
DIVISION ENGINEER'S REQUIREMENTS:			
	Billu	1. Jyner	January 31, 2020
		V	
100541 Dam I.D	Signature of Div		Date

³ Freeboard" is the vertical distance from the bottom of spillway to the crest of the dam. Minimum Freeboard is 3 feet.

⁴ If construction in reservoir intercepts groundwater, a well permit is required. (Well permit applications can be found at <u>www.water.state.co.us</u>)

HYDROLOGIC CALCULATIONS

DWIRE STORAGE YARD FINAL DRAINAGE REPORT DRAINAGE CALCULATIONS (Existing Conditions Area Runoff Coefficient Summary)

			P	AVEMEN	T		ROOF		STORAG	E YARD (C	GRAVEL)	LANDSCA	PED/PAST	URELAND	WEIG	HTED
BASIN	TOTAL AREA (Sq Ft)	TOTAL AREA (Acres)	AREA (Acres)	C ₅	C ₁₀₀	C ₅	C ₁₀₀									
OS1	39125.8	0.90	0.00	0.90	0.96	0.00	0.73	0.81	0.00	0.30	0.50	0.90	0.09	0.35	0.09	0.35
OS2	6346.6	0.15	0.00	0.90	0.96	0.00	0.73	0.81	0.00	0.30	0.50	0.15	0.09	0.35	0.09	0.35
OS3	55083.7	1.26	0.54	0.90	0.96	0.28	0.73	0.81	0.45	0.30	0.50	0.00	0.09	0.35	0.65	0.76
OS4	7008.0	0.16	0.00	0.90	0.96	0.00	0.73	0.81	0.00	0.30	0.50	0.16	0.09	0.35	0.09	0.35
OS5	15582.7	0.36	0.00	0.90	0.96	0.00	0.73	0.81	0.00	0.30	0.50	0.36	0.09	0.35	0.09	0.35
OS6	64655.6	0.78	0.00	0.90	0.96	0.00	0.73	0.81	0.00	0.30	0.50	0.78	0.09	0.35	0.09	0.35
OS7	198141.1	4.55	0.00	0.90	0.96	0.00	0.73	0.81	0.00	0.30	0.50	4.55	0.09	0.35	0.09	0.35
A	107676.5	2.47	0.00	0.90	0.96	0.00	0.73	0.81	0.00	0.30	0.50	2.47	0.09	0.35	0.09	0.35
A1	13107.4	0.30	0.00	0.90	0.96	0.00	0.73	0.81	0.00	0.30	0.50	0.30	0.09	0.35	0.09	0.35
В	550809.9	12.64	0.00	0.90	0.96	0.00	0.73	0.81	0.00	0.30	0.50	12.64	0.09	0.35	0.09	0.35
С	28780.7	0.66	0.00	0.90	0.96	0.00	0.73	0.81	0.00	0.30	0.50	0.66	0.09	0.35	0.09	0.35
D	139029.7	3.19	0.00	0.90	0.96	0.00	0.73	0.81	0.00	0.30	0.50	3.19	0.09	0.35	0.09	0.35

Calculated by: DLM Date: 11/19/2018 Checked by: VAS

DWIRE STORAGE YARD FINAL DRAINAGE REPORT DRAINAGE CALCULATIONS (Existing Conditions - Area Drainage Summary)

From Area Runoff Coef	ficient Summar	у			OVER	LAND		STRE	ET / CH	ANNEL F	LOW	Time o	f Travel	INTENS	SITY *	TOTAL FLOWS	
BASIN	AREA TOTAL	C ₅	C ₁₀₀	C ₅	Length	Height	T _C	Length	Slope	Velocity	T _t	TOTAL	CHECK	I ₅	I ₁₀₀	Q5	Q ₁₀₀
	(Acres)	From DCM	M Table 6-6		(ft)	(ft)	(min)	(ft)	(%)	(fps)	(min)	(min)	(min)	(in/hr)	(in/hr)	(c.f.s.)	(c.f.s.)
OS1	0.90	0.09	0.35	0.09	150	4	17.1	300	1.0%	1.0	5.0	22.1	12.5	2.9	4.9	0.2	1.6
OS2	0.15	0.09	0.35	0.09	100	3	13.4	350	1.4%	1.2	4.9	18.3	12.5	3.2	5.4	0.0	0.3
OS3	1.26	0.65	0.76	0.65	50	3	5.1	540	1.0%	2.0	4.5	9.6	13.3	4.2	7.0	3.4	6.8
OS4	0.16	0.09	0.35	0.09	50	1	10.9	300	0.7%	0.8	6.1	17.0	11.9	3.3	5.6	0.0	0.3
OS5	0.36	0.09	0.35	0.09	100	1	19.3	325	3.7%	1.9	2.8	22.1	12.4	2.9	4.9	0.1	0.6
OS6	0.78	0.09	0.35	0.09	100	1	19.3	480	4.8%	2.2	3.7	23.0	13.2	2.9	4.8	0.2	1.3
OS7	4.55	0.09	0.35	0.09	100	1.5	16.9	1200	1.2%	1.1	18.5	35.4	17.2	2.2	3.7	0.9	6.0
A	2.47	0.09	0.35	0.09	150	5	15.9	885	1.1%	1.1	13.9	29.8	15.8	2.5	4.2	0.6	3.6
A1	0.30	0.09	0.35	0.09	50	1.5	9.5	460	3.7%	2.9	2.7	12.2	12.8	3.8	6.4	0.1	0.7
В	12.64	0.09	0.35	0.09	180	6	17.4	1450	1.8%	1.3	18.0	35.5	19.1	2.2	3.7	2.5	16.6
С	0.66	0.09	0.35	0.09	50	1	10.9	60	10.0%	3.2	0.3	11.2	10.6	4.0	6.7	0.2	1.5
D	3.19	0.09	0.35	0.09	150	1.5	23.7	750	1.6%	1.3	9.9	33.5	15.0	2.3	3.9	0.7	4.3

Calculated by: DLM Date: 11/19/2018 Checked by: VAS

'ARD					
AGE CALC	ULATION	S			
uting Sumn	narv)				
INNEL FLOW	Time of Travel (T ,)	INTENSITY	* TOTAL	. FLOWS	
ope Velocity T _t	TOTAL	I ₅ I ₁	-	Q ₁₀₀	COMMENTS
%) (fps) (min)	(min)	(in/hr) (in/		<100 (c.f.s.)	CONNENTS
NG SUMMARY	(min)	(<i>m/nr</i>) (<i>m/</i>	ur) (c.j.s.)	(C.J.S.)	4
					1
From Basin A	29.8	2.5 4.	2 0.8	5.1	
rom Basin OS3	9.6	4.2 7.	0 3.6	7.5	4
Totili Basili 035	9.0	4.2 /.	0 3.0	7.5	
From Basin B	35.5	2.2 3.	7 2.6	17.2	
					1
From Basin OS6	23.0	2.9 4.	8 0.4	2.4	
From Basin OS7	35.4	2.2 3.	7 4.5	29.3	1
Tc I	Tc From Basin OS7	Tc From Basin OS7 35.4		Te From Basin OS7 35.4 2.2 3.7 4.5 Calculated by: DLM	

Calculated by: DLM

Date: 11/19/2018 Checked by: VAS

DWIRE STORAGE YARD FINAL DRAINAGE REPORT DRAINAGE CALCULATIONS (Proposed Conditions Area Runoff Coefficient Summary)

			PAVI	EMENT/C	ONC		ROOF		STO	ORAGE YAI	RD	PASTURE	LAND/UNDI	EVELOPED	WEIG	HTED
BASIN	TOTAL AREA (Sq Ft)	TOTAL AREA (Acres)	AREA (Acres)	C ₅	C ₁₀₀	C ₅	C ₁₀₀									
OS1	6346.6	0.15	0.00	0.90	0.96	0.00	0.73	0.81	0.00	0.30	0.50	0.15	0.09	0.36	0.09	0.36
OS2	65383.0	1.50	0.85	0.90	0.96	0.00	0.73	0.81	0.55	0.30	0.50	0.10	0.09	0.36	0.63	0.75
OS3	19864.6	0.46	0.00	0.90	0.96	0.00	0.73	0.81	0.00	0.30	0.50	0.46	0.09	0.36	0.09	0.36
OS4	5124.1	0.12	0.00	0.90	0.96	0.00	0.73	0.81	0.00	0.30	0.50	0.12	0.09	0.36	0.09	0.36
OS5	64655.6	0.78	0.00	0.90	0.96	0.00	0.73	0.81	0.00	0.30	0.50	0.78	0.09	0.36	0.09	0.36
OS6	202148.8	4.64	0.00	0.90	0.96	0.00	0.73	0.81	0.00	0.30	0.50	4.64	0.09	0.36	0.09	0.36
A	106469.9	2.44	0.00	0.90	0.96	0.00	0.73	0.81	1.90	0.59	0.70	0.54	0.09	0.36	0.48	0.62
В	60512.9	1.39	0.66	0.90	0.96	0.00	0.73	0.81	0.73	0.59	0.70	0.00	0.09	0.36	0.74	0.82
B1	119490.8	2.74	0.16	0.90	0.96	0.23	0.73	0.81	2.35	0.59	0.70	0.00	0.09	0.36	0.62	0.72
B2	325993.3	7.48	0.14	0.90	0.96	0.11	0.73	0.81	7.23	0.59	0.70	0.00	0.09	0.36	0.60	0.71
B3	53002.6	1.22	0.00	0.90	0.96	0.00	0.73	0.81	0.00	0.59	0.70	1.22	0.16	0.41	0.16	0.41
С	28780.7	0.66	0.00	0.90	0.96	0.00	0.73	0.81	0.00	0.59	0.70	0.66	0.09	0.36	0.09	0.36
D	139029.7	3.19	0.00	0.90	0.96	0.00	0.73	0.81	3.19	0.59	0.70	0.00	0.09	0.36	0.59	0.70

Calculated by: GT Date: 11/12/2020 Checked by: VAS

DWIRE STORAGE YARD FINAL DRAINAGE REPORT DRAINAGE CALCULATIONS (Proposed Conditions - Area Drainage Summary)

From Area Runoff Coeff	ficient Summa	ry			OVER	LAND		STRE	ET / CH	ANNEL F	LOW	Time o	f Travel	INTENS	SITY *	TOTAL FLOWS	
BASIN	AREA TOTAL	C ₅	C ₁₀₀	C ₅	Length	Height	T _C	Length	Slope	Velocity	T _t	TOTAL	CHECK	I ₅	I ₁₀₀	Q5	Q ₁₀₀
	(Acres)	From DCM	M Table 6-6		(ft)	(ft)	(min)	(ft)	(%)	(fps)	(min)	(min)	(min)	(in/hr)	(in/hr)	(c.f.s.)	(c.f.s.)
OS1	0.15	0.09	0.36	0.09	100	4	11.5	44	4.5%	2.1	0.3	11.9	10.8	4.0	6.7	0.1	0.4
OS2	1.50	0.63	0.75	0.63	50	1	4.8	47	4.0%	4.0	0.2	5.0	10.5	5.2	8.7	4.9	9.8
OS3	0.46	0.09	0.36	0.09	50	1	10.3	0	0.0%	0.0	0.0	10.3	10.3	4.1	6.9	0.2	1.1
OS4	0.12	0.09	0.36	0.09	100	1	18.2	200	2.5%	1.6	2.1	20.3	11.7	3.9	6.5	0.0	0.3
OS5	0.78	0.09	0.36	0.09	100	1	18.2	480	4.8%	2.2	3.7	21.9	13.2	3.7	6.2	0.3	1.7
OS6	4.64	0.09	0.36	0.09	100	1.5	16.0	1200	1.2%	1.1	18.5	34.5	17.2	3.3	5.6	1.4	9.3
A	2.44	0.48	0.62	0.48	100	7	5.9	830	2.0%	1.4	9.7	15.6	15.2	3.5	5.9	4.1	9.0
В	1.39	0.74	0.82	0.74	100	3	4.6	440	1.6%	1.9	3.9	8.4	13.0	4.4	7.4	4.5	8.4
B1	2.74	0.62	0.72	0.62	100	1	8.7	636	1.8%	1.3	7.9	16.6	14.1	3.6	6.1	6.1	12.1
B2	7.48	0.60	0.71	0.60	100	6	5.0	1435	1.9%	2.1	11.6	16.6	18.5	3.2	5.4	14.3	28.4
B3	1.22	0.16	0.41	0.16	30	6	3.5	447	0.5%	1.4	5.3	8.7	12.7	4.3	7.3	0.8	3.6
С	0.66	0.09	0.36	0.09	53	2	8.6	54	25.0%	5.0	0.2	8.7	10.6	4.3	7.3	0.3	1.7
D	3.19	0.59	0.70	0.59	100	5	5.4	905	1.7%	1.3	11.7	17.1	15.6	3.5	5.8	6.5	13.0

Calculated by: GT Date: 11/12/2020 Checked by: VAS

			MAR	RKS	HE	FFE	L &	<i>CO</i> Λ	STI	TUT	ION	T					
	FINAL	DR.	1 <i>INA</i>	GF	E RE	POR	T D		VAG	EE CA	4LC	ULATION	S				
												nary)	~				
F	rom Area Runoff Coefficient Summary					RLAND				NNEL FLO		Time of Travel (T_t)	INTEN	SITY *	TOTAL	FLOWS	
DESIGN POINT	CONTRIBUTING BASINS	CA ₅	CA100	C5	Length	Height	T _C	Length	Slope	Velocity	Tt	TOTAL	I,	I ₁₀₀	Q5	Q ₁₀₀	COMMENTS
		- 3	- 100	- 3	(ft)	(ft)	(min)	(ft)	(%)	(fps)	(min)	(min)	(in/hr)	(in/hr)	(c.f.s.)	(c.f.s.)	
			PRO)POS			. ,			SUMM	(()	(()	(0,0)	(0.9.04)	
1	OS1	0.01	0.05	105				n v no c									
	A	1.17	1.53														
		1.18	1.58						Tc From	n Basin A		15.2	3.5	5.9	4.1	9.3	
2	OS2	0.94	1.13														
	В	1.02	1.14														
		1.96	2.27						Tc Fron	n Basin B		8.4	4.4	7.4	8.6	16.7	
3	B1	1.70	1.99														
		1.70	1.99						Tc From	n Basin B1	-	14.1	3.6	6.1	6.1	12.1	
4	B2	4.47	5.29														
	D	1.88	2.23														
		6.36	7.52						Tc From	n Basin B2		18.5	3.2	5.4	20.4	40.5	
5	DP2	1.96	2.27 1.99														
	DP3 DP4	1.70 6.36	7.52														
	OS4	0.30	0.04														
	B3	0.19	0.50														
		10.23	12.32						Tc From	Basin DP4		18.5	3.2	5.4	32.8	66.3	FSD Pond
6	OS5	0.07	0.28														
	С	0.06	0.24														
		0.13	0.52						Tc From	Basin OS5		13.2	3.7	6.2	0.5	3.2	
7	DP6	0.13	0.52														
	OS6	0.42	1.67 2.19						Te From	Basin OS6		17.2	3.3	5.6	1.8	12.2	
	PR2	0.55	2.19						re riom	Dasili O30		17.2	5.5	3.0	1.8 0.5	12.2	
	1 1\2												Т	otal	2.3	29.7	

Calculated by: GT Date: 11/12/2020

Checked by: VAS

DWIRE STORAGE YARD FINAL DRAINAGE REPORT DRAINAGE CALCULATIONS (Storm Sewer Routing Summary)

					Inten	sity*	Fl	ow	PIPE SIZE		
PIPE RUN	Contributing Pipes/Design Points	Equivalent CA 5	Equivalent CA ₁₀₀	Maximum T _C	I_5	I 100	Q 5	Q 100			
1	DP2	1.96	2.27	8.4	4.4	7.4	8.6	16.7	18" RCP		
2	FSD Outlet Structure	UD-D	etention, V 3.07,	Routed Hydrogr	aph Results		0.5	17.5	24" RCP		
* Intensity	equations assume a minimum travel time of 5	minutes. Calculated by						y: GT			

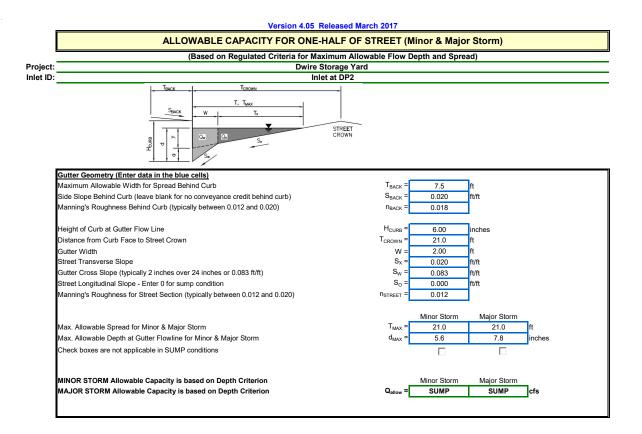
DP - Design Point

EX - Existing Design Point

FB- Flow By from Design Point INT- Intercepted Flow from Design Point Date: 11/12/2020Checked by: VAS

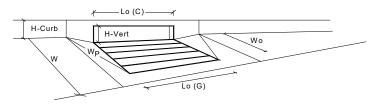
FDR Prop Drainage Calcs.xls

HYDRAULIC CALCULATIONS / FSD POND CALCULATIONS



INLET IN A SUMP OR SAG LOCATION

Version 4.05 Released March 2017



Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R Curb Opening		
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	2	2	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	5.6	7.8	inches
Grate Information		MINOR	MAJOR	Override Depths
Length of a Unit Grate	L _o (G) =	N/A	N/A	feet
Width of a Unit Grate	W _o =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	C _f (G) =	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C _w (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	C _o (G) =	N/A	N/A	
Curb Opening Information	_	MINOR	MAJOR	
Length of a Unit Curb Opening	L _o (C) =	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H _{throat} =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W _p =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	C _f (C) =	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	C _w (C) =	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	C _o (C) =	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d _{Curb} =	0.30	0.48	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	0.53	0.74	
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	0.91	1.00	
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A]
	_	MINOR	MAJOR	_
Total Inlet Interception Capacity (assumes clogged condition)	Q _a =	8.7	18.7	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	8.6	16.7	cfs

18'' RCP INDEX MAP



Conduit FlexTable: 18inch Outfall 100-YR

Label	ID	Upstream Structure	Flow (cfs)	Flow / Capacity (Design) (%)	Length (Unified) (ft)	Velocity (ft/s)	Froude Number (Normal)	Depth (Normal) (ft)	Depth (Critical) (ft)	Energy Grade Line (In) (ft)	Energy Grade Line (Out) (ft)	Hydraulic Grade Line (In) (ft)	Hydraulic Grade Line (Out) (ft)	Headloss (ft)
PR1, Prop. 18" RCP	88	CDOT Type R Sump Inlet	16.70	78.2	27.8	9.45	2.511	1.00	1.44	6,535.22	6,534.52	6,533.83	6,533.13	0.70
Upstream Structure Hydraulic Grade Line (In) (ft)	Upstream Structure Velocity (In- Governing) (ft/s)	Upstream Structure Headloss Coefficient	Upstream Structure Headloss (ft)	Elevation Ground (Start) (ft)	Elevation Ground (Stop) (ft)	Invert (Start) (ft)	Invert (Stop) (ft)	Conduit Description	Manning's n	Friction Slope (ft/ft)				
6,535.92	9.45	1.500	2.08	6,536.58	6,530.10	6,532.00	6,530.85	Circle - 18.0 in	0.013	0.025				

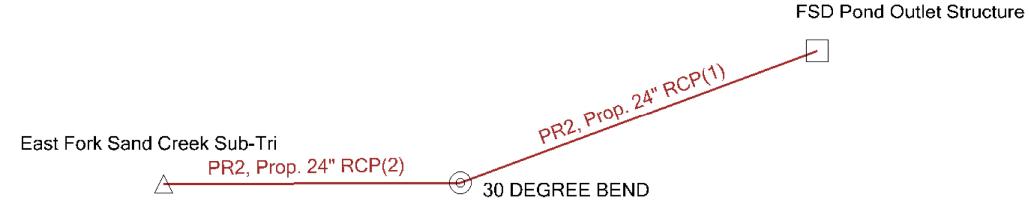
Bentley StormCAD CONNECT Edition [10.01.01.04] Page 1 of 1



Pipe Run 1, 18" RCP - 100 yr Event

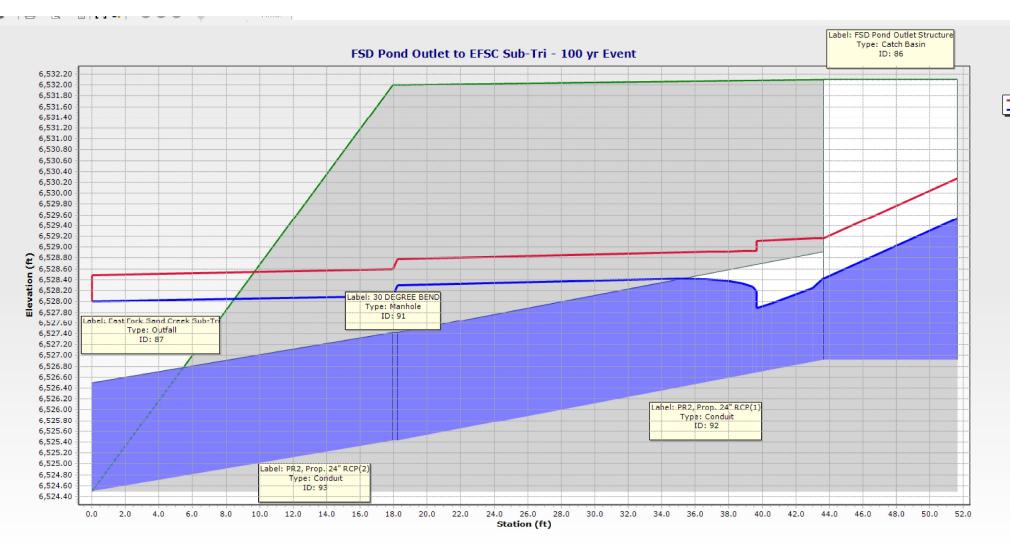
= EGL = HGL

24" RCP INDEX MAP



Conduit FlexTable: POND 1- 24inch OUTFALL 100-YR

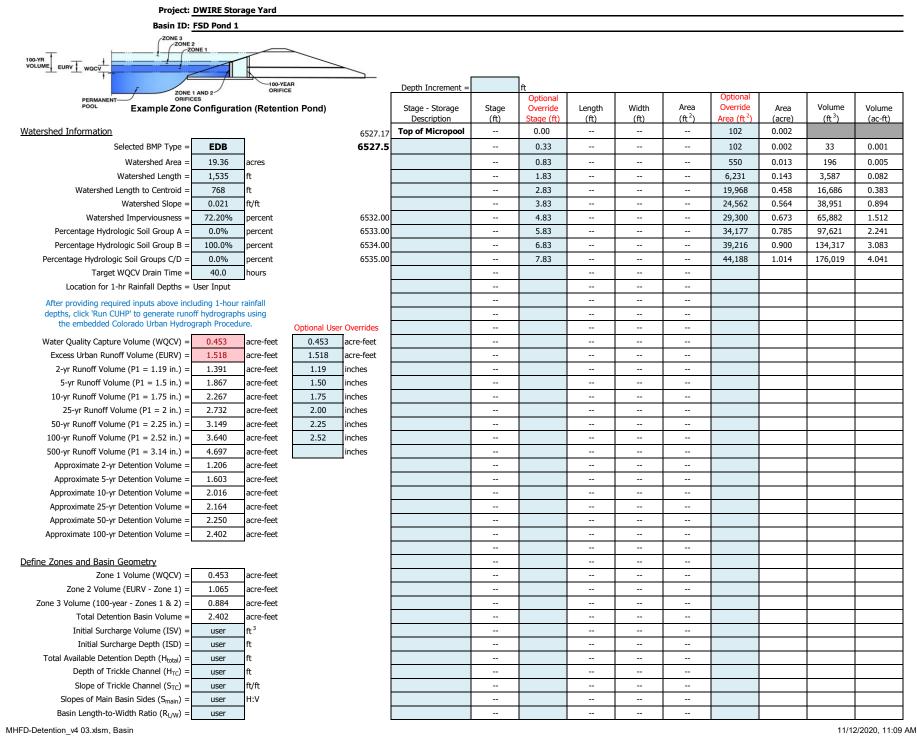
Label	ID	Upstream Structure	Flow (cfs)	Flow / Capacity (Design) (%)	Length (Unified) (ft)	Velocity (ft/s)	Froude Number (Normal)	Depth (Normal) (ft)	Depth (Critical) (ft)	Energy Grade Line (In) (ft)	Energy Grade Line (Out) (ft)	Hydraulic Grade Line (In) (ft)	Hydraulic Grade Line (Out) (ft)	Headloss (ft)	Upstream Structure Hydraulic Grade Line (In) (ft)
PR2, Prop. 24" RCP(1)	92	FSD Pond Outlet Structure	17.50	34.3	29.5	14.71	3.332	0.81	1.51	6,529.17	6,528.78	6,528.43	6,528.30	0.13	6,529.53
PR2, Prop. 24" RCP(2)	93	30 DEGREE BEND	17.50	34.3	18.1	5.57	3.335	0.81	1.51	6,528.59	6,528.48	6,528.11	6,528.00	0.11	6,528.30
Upstream Structure Velocity (In- Governing) (ft/s)	Upstream Structure Headloss Coefficient	Upstream Structure Headloss (ft)	Elevation Ground (Start) (ft)	Elevation Ground (Stop) (ft)	Invert (Start) (ft)	Invert (Stop) (ft)	Conduit Description								
6.89 5.57	1.500 0.400		6,532.10 6,532.00	6,532.00 6,524.50	6,526.92 6,525.42		Circle - 24.0 in Circle - 24.0 in								



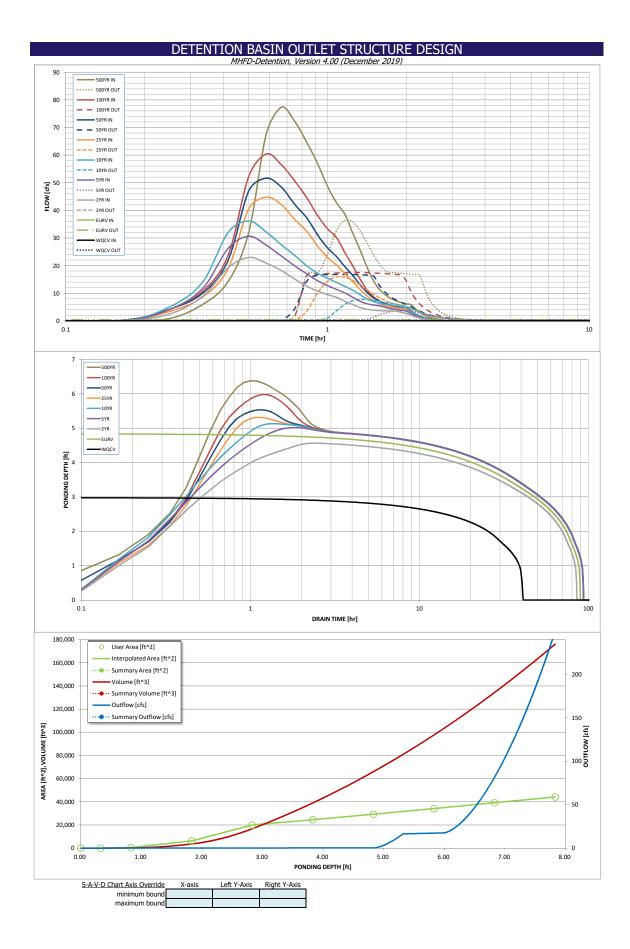
Weighted P	Percent Impe	rviousness a	of Dwire Storage Y	ard Site
Contributing Onsite Basins	Area (Acres)	<i>C</i> 5	Impervious % (I)	(Acres)*(I)
A	2.44	0.48	69	168.65
В	1.39	0.74	91	126.42
<i>B1</i>	2.74	0.62	82	224.94
<i>B2</i>	7.48	0.60	81	606.19
<i>B3</i>	1.22	0.16	13	15.82
С	0.66	0.09	2	1.32
D	3.19	0.59	80	255.33
Totals	19.36			1398.66
Imperviousness of Site %	72.2			

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.03 (May 2020)



		DE	TENTION				SIGN			
Structure	Project:		М							
Signed Protocols Signed Protocols Signed Protocols Signed Protocols Signed Protocols Signed Protocols Signed Proto			ra							
Signed Protocols Signed Protocols Signed Protocols Signed Protocols Signed Protocols Signed Protocols Signed Proto	ZONE 3				Estimated	Estimated				
					Stage (ft)	Volume (ac-ft)	Outlet Type			
				Zone 1 (WQCV)	2.98	0.453	Orifice Plate]		
Description Description Description Description Description Control and Contro And Contre And Control and Control and Control and Control and C				Zone 2 (EURV)	4.84	1.065	Orifice Plate			
Term Date 200 Comparison pressure register Term (2) dest (2) d	PERMANENT ORIFICES			Zone 3 (100-year)	6.04	0.884	Weir&Pipe (Restrict)			
Understand Online Data Index Data	POOL Example Zone	Configuration (Re	tention Pond)		Total (all zones)	2.402		1		
Under dan Onflike Diesender meding Under dan Onflike Cardinal = medi Stati Institution Conflike Arrange in Station of Station in Station Location and Station = 0.0000 Novel And Station Station of Station in Station Location and Station = 0.0000 Novel And Station of Station								Calculated Parame		
Instruct. Conclusion for reactions of Theorem Optice Tables of Control Version 44.44 () () () () () () () () () () () () () (-	the filtration media	surface)					
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Inter of Jose Config Example 10 (b) WQ Daffe Area yr Rev Example 20 (b) WQ Daffe Area yr Rev WQ	User Tracity Orifice Dista with ano or more orific		the therein the second		the FUDV in a codi	materian PMD)		Columbiate d Doromoi	the fee Dista	
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Online Peter: Online Area or Rev = 191 np. inches (dameter = 1-9/16 inches) Pippicol Six Area = N/A R* User Input: Stage and Total Area of Each Diffice Boar (personnel Rev 2 (spterard) Rev 1 (spterard) Rev 2 (spterard) Rev 1 (spterard)			-	Docton: at c	010					
User Input: Stage and Total Area of Each Online Rook (quantum from 1 (quantum from 1 2 (quantum from 1 2 (quantum from 1 2 (quantum from 1 2 (quantum from 1 1 (quantum from 1 (quantum from 1 1 (quantum from from 1 (quantum				er = 1-9/16 inches))					
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Stage of drive cheres (H) Nov 1 (optional) Nov 4 (optional) Nov 4 (optional) Nov 4 (optional) Nov 1 (o										
Stage of Ontice Correct (th) 0.00 1.61 3.22 1.61 <	User Input: Stage and Total Area of Each Orifice		-							
Ondire Area (op. Introl) 1.91 1		,			Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)	
Number Rev 12 (getown) Rev 11 (getown) Rev 11 (getown) Rev 11 (getown) Rev 12 (getown) Rev 14 (getown) Rev 15 (getown) Stage of Orlice Centrol (No) Image: Centrol (No) I										
Stage of Ordic Certrols (f) Image: Stage of Ordic Certrol (f) Image: Stage of Ordice Certrol (f) Image: Stage of Ordi (f) <td>Orifice Area (sq. inches)</td> <td>1.91</td> <td>1.91</td> <td>1.91</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>	Orifice Area (sq. inches)	1.91	1.91	1.91						
Stage of Ordic Certrols (f) Image: Stage of Ordic Certrol (f) Image: Stage of Ordice Certrol (f) Image: Stage of Ordi (f) <td></td> <td></td> <td></td> <td>T</td> <td>1</td> <td></td> <td></td> <td></td> <td></td> <td>ı</td>				T	1					ı
Ontice Area (qu, nches) Collabel Parameters for Vertical Office User Input: Vertical Office Clanar e. Rectangular) Collabel Parameters for Vertical Office Depth a top of zero using vertical Office N/A N/A N/A User Input: Vertical Office Dameter N/A N/A N/A N/A User Input: Overflow Wer for togs high, here N/A N/A N/A N/A Overflow Wer for togs high, here Collabel Parameters for Overflow Wer N/A N/A N/A Overflow Wer for togs high, here Collabel Parameters for Overflow Wer Collabel Parameters for Overflow Wer Collabel Parameters for Overflow Wer Overflow Wer for togs high, here Collabel Parameters for Overflow Wer Collabel Parameters for Overflow Wer Collabel Parameters for Overflow Wer Overflow Wer for togs high, here Collabel Parameters for Overflow Wer Collabel Parameters for Overflow Wer Collabel Parameters for Overflow Wer Overflow Wer for togs high, here Collabel Parameters for Overflow Wer Collabel Parameters for Overflow Wer Collabel Parameters for Overflow Wer Overflow Wer for togs high, here Collabel Parameters for Overflow Wer Collabel Parameters for Overflow Wer Collabel Parameters for Overflow	Charac of Orifica Controld (#)	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)	
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Invert of Vertical Orifice = Inversion of Vertical Orifice Orifi	Office Area (Sq. incres)									1
Invert of Vertical Orifice = Inversion of Vertical Orifice Orifi	User Input: Vertical Orifice (Circular or Rectange	ular)						Calculated Parame	ter <u>s for Vertical Ori</u>	fice
Liver of Vertical Orifice N/A N/A f(relative to basin bottom at Stage = 0 f) Vertical Orifice Centrol = N/A N/A N/A Depth at top of zone using Vertical Orifice Dameter = N/A N			Not Selected	1			I			1
Vertical Onfice Dameter = N/A N/A nches User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Floe OR Rectangular/Trapecodal Weir (and No Dutlet Floe). Calculated Parameters for Overflow Weir Overflow Weir Front Edge Height, He = 48.00 N/A Het 43.50 N/A Overflow Weir Front Edge Height, He = 48.00 N/A Het 43.50 N/A Overflow Weir Grate Stope = 0.00 N/A Het Grate Open Area / 100-yr Onfice Area = 12.60 N/A Hortz, Length of Weir Sdae = 3.50 N/A Het Overflow Grate Open Area / 100-yr Onfice Area = 12.60 N/A Het Overflow Grate Open Area / 100-yr Onfice Area = 12.60 N/A Het Area / 100-yr Onfice Area = 12.60 N/A Het Overflow Grate Open Area / 100-yr Onfice Area = 12.60 N/A Het Area / Area	Invert of Vertical Orifice =			ft (relative to basin	1 bottom at Stage =	0 ft) Ver	tical Orifice Area =	N/A		ft ²
Jase Input: Overflow Weir (Drophox with Hat or Slope Grife and Outlet Pipe OR Restrangular/Trapszoldal Weir (and No Dutlet Pipe). Calculated Parameters for Overflow Weir Toolt Sign Langth = Overflow Weir Front Edge Height, Ho Overflow Weir Toolt Sign Langth = 20nc 3 Weir Not Solected = 4.85 N/A feet Overflow Weir Front Edge Height, Ho Overflow Weir Stope Langth = 3.00 N/A feet 4.85 N/A feet Overflow Weir Stoles = 3.00 N/A feet Overflow Grate Open Area Wo Debris = 13.60 N/A feet Overflow Grate Open Area Wo Debris = 3.60 N/A %, grate open area/total area Overflow Grate Open Area Wo Debris = 13.60 N/A feet Overflow Grate Open Area Wo Debris = 0.80 N/A %, grate open area/total area Overflow Grate Open Area Wo Debris = 13.60 N/A fc ² Debris Cooging % = 50% N/A fc (distance below besin bottom at Stage = 0 ft) Calculated Parameters for Outlet Pipe W. Flow Restricton Pite For Starter No Solected Debrits Cooging % = 0.25 N/A fc (distance below besin bottom at Stage = 0 ft) Spillway Cooffiee Area = 1.53 N/A <td>Depth at top of Zone using Vertical Orifice =</td> <td>N/A</td> <td>N/A</td> <td>ft (relative to basin</td> <td>1 bottom at Stage =</td> <td>0 ft) Vertical</td> <td> Orifice Centroid =</td> <td>N/A</td> <td>N/A</td> <td>feet</td>	Depth at top of Zone using Vertical Orifice =	N/A	N/A	ft (relative to basin	1 bottom at Stage =	0 ft) Vertical	Orifice Centroid =	N/A	N/A	feet
Zone 3 Weir Not Selected Height of Grate Upper Edge, H, e Zone 3 Weir Net Selected Overflow Weir Front Edge Langth = 8.00 N/A freet Overflow Weir Slope Length = 3.50 N/A feet Overflow Weir Grate Upper Area % = 0.00 N/A feet Overflow Grate Open Area % 0 Debris = 10.50 N/A feet Overflow Grate Open Area % = 70% N/A %, grate open area/total area Overflow Grate Open Area % 0 Debris = 9.80 N/A ft* User Input: Outlet Pipe w/ Flow Restriction Plate Circular Orifice, Restrictor Plate, or Restangular Orifice) Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate Zone 3 Restrictor Not Selected Outlet Pipe Dameter = 11.75 Inches Half-Central Angle of Restrictor Plate on Pipe = 15.5 N/A ft* Splitway Invert Stage 50.00 ft ft ft ft ft 78 50 N/A ft Splitway Invert Stage 50.00 ft	Vertical Orifice Diameter =	N/A	N/A	inches					•	
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$										
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$										
Overflow Weir Front Edge Height, Ho 4.85 N/A freet Overflow Weir Front Edge Length 8.00 N/A feet Overflow Weir Stope Length 3.50 N/A Overflow Weir Stope Length 0.00 N/A feet Overflow Weir Stope Length 3.50 N/A Overflow Grate Dgen Area % 3.50 N/A feet Overflow Grate Dgen Area % 10.92 N/A feet Overflow Grate Dgen Area % 50% N/A feet Overflow Grate Dgen Area w/ Debris 19.60 N/A ft ² Debris Clogging % 50% N/A % strate Overflow Grate Dgen Area w/ Debris 9.80 N/A ft ² User Input: Outlet Pipe w/ Flow Restriction Plate Cance 1 Restrictor Not Selected Cance 3 Restrictor Not Selected 1.53 N/A ft ² Depth to Invert of Outlet Pipe Coult Mpc Diameter 24.00 N/A fteet 1.53 N/A fteet Splitway Invert Stage 6.00 ft (relative to basin bottom at Stage = 0 ft) Splitway Invert Stage 0.78 ftee		1. A A A						1		
Overflow Weir Front Edge Length + Overflow Weir Grate Stope - Horiz. Length of Weir Sides + Overflow Weir Grate Stope - Stope Length + Debris Coging % - Debris Coging %	User Input: Overflow Weir (Dropbox with Flat or			tangular/Trapezoida	I Weir (and No Out	let Pipe)				/eir
Overflow Weir Gare Sope + Horiz, Length of Weir Sides - Overflow Grate Open Area Vio Debris - Debris Clogging % - Out of the Area * 20% Overflow Grate Open Area Vio Debris - Debris Clogging % - Image: Clogeing % - Image: Clogging % - <thima< td=""><td></td><td>Zone 3 Weir</td><td>Not Selected</td><td></td><td></td><td></td><td></td><td>Zone 3 Weir</td><td>Not Selected</td><td></td></thima<>		Zone 3 Weir	Not Selected					Zone 3 Weir	Not Selected	
Hord. Length of Weir Sides = Debris Clogging % = Edited Clorular Orifice, Restrictor Plate, or Rectangular Orifice) Debris Clogging % = Edited Clorular Orifice, Restrictor Plate, or Rectangular Orifice) Clorular Of Outlet Pipe w/ Flow Restriction Plate (Clorular Orifice, Restrictor Plate, or Rectangular Orifice) Debris Clogging % = Edited Depth to Invert of Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe and the Clorular Orifice, Restrictor Plate, or Rectangular Orifice) Depth to Invert of Outlet Pipe and the Clorular Orifice, Restrictor Plate, or Rectangular Orifice) Depth to Invert of Outlet Pipe and the Clorular Orifice, Restrictor Plate, or Rectangular Orifice) Outlet Orifice Area at 0 0 United Orifice Area at 0 0 0 Oriented Pipe at 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Overflow Weir Front Edge Height, Ho =	Zone 3 Weir 4.85	Not Selected N/A	ft (relative to basin b		ft) Height of Grate	e Upper Edge, H _t =	Zone 3 Weir 4.85	Not Selected N/A	feet
Overflow Grate Open Area % - Debris Clogging % = 70% N/A %, grate open area/total area Overflow Grate Open Area w/ Debris = 9.80 N/A R² User Input: Outlet Pipe w/ Flow Restriction Plate, Or Rectangular Onfice) Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate Zone 3 Restrictor Not Selected 0.35 N/A R² Depth to Invert of Outlet Pipe w/ Flow Restriction Plate, or Rectangular Onfice) Calculated Parameters for Outlet Onfice Area a 0.05 N/A R² Outlet Pipe w/ Flow Restriction Plate 0.035 N/A R² Restrictor Not Selected 0.05 N/A R² Outlet Plate Height Above Pipe Invert a 24.00 N/A nches Outlet Onfice Area a 0.05 N/A r² Spillway (Rectangular or Trapezoidal) Inches Half-Central Angle of Restrictor Plate on Pipe a 7.78 feet 7.78 feet Spillway (Restangular or Trapezoidal) Exercice and above Max Water Surface a 0.06 feet 7.78 feet 7.78 feet 7.78 feet 7.78 feet 7.78 feet 7.78 feet	Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length =	Zone 3 Weir 4.85 8.00	Not Selected N/A N/A	ft (relative to basin t feet	bottom at Stage = 0 f	ft) Height of Grate Overflow W	e Upper Edge, H _t = /eir Slope Length =	Zone 3 Weir 4.85 3.50	Not Selected N/A N/A	feet
Debris Clogging % = 50% N/A % User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice) Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe Cance 3 Restrictor Not Selected R Outlet Pipe Diameter 0.25 N/A R ² Outlet Pipe Diameter 11.75 inches Outlet Orifice Centrol = 0.56 N/A Ret User Input: Emergency Spillway (Rectangular or Tapezolda) inches Half-Central Angle of Restrictor Plate end presenter 0.56 N/A Ret Spillway Invert Stage 6.00 fret inches Half-Central Angle of Restrictor Plate or Pipe 0.78 fret Spillway Invert Stage 6.00 fret Stage at Top of Freeboard = 0.78 freet Spillway Invert Stage 1.00 freet Basin Volume at Top of Freeboard = 0.39 acres Cuted Hydrograph Result The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF). 2.25 2.52 3.14 3.640 4.697	Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope =	Zone 3 Weir 4.85 8.00 0.00	Not Selected N/A N/A N/A	ft (relative to basin t feet H:V	bottom at Stage = 0 f Gr	ft) Height of Grate Overflow W rate Open Area / 10	e Upper Edge, H _t = /eir Slope Length =)0-yr Orifice Area =	Zone 3 Weir 4.85 3.50 12.82	Not Selected N/A N/A N/A	feet feet
User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate Pipe w/ Edw Restriction Plate (Circular Orifice) Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice) Cone 3 Restrictor Not Selected Outlet Pipe Jonarder = 0.25 N/A ft (distance below basin bottom at Stage = 0 ft) Outlet Orifice Area = 1.53 N/A fte Outlet Pipe w/ Flow Restrictor Plate or Plate Information 11.75 inches Half-Central Angle of Restrictor Plate on Pipe 1.55 N/A fte User Input: Emergency Spillway Invert Stages 6.00 ft (relative to basin bottom at Stage = 0 ft) Spillway Despin Flow Depth 0.78 feet 7.78	Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides =	Zone 3 Weir 4.85 8.00 0.00 3.50	Not Selected N/A N/A N/A N/A	ft (relative to basin t feet H:V feet	bottom at Stage = 0 f Gr ດາ	ft) Height of Grate Overflow W rate Open Area / 10 verflow Grate Open	e Upper Edge, H _t = /eir Slope Length =)0-yr Orifice Area = Area w/o Debris =	Zone 3 Weir 4.85 3.50 12.82 19.60	Not Selected N/A N/A N/A N/A	feet feet ft ²
Zone 3 Restrictor Not Selected Case N/A ft (distance below basin bottom at Stage = 0 ft) Outlet Orifice Centrol = Zone 3 Restrictor Not Selected Outlet Pipe Diametre = 24.00 N/A ft (distance below basin bottom at Stage = 0 ft) Outlet Orifice Centrol = 1.33 N/A ft ² Restrictor Plate Height Above Pipe Invert = 11.75 inches Half-Central Angle of Restrictor Plate on Pipe = 1.55 N/A radians User Input: Emergency Spillway Invert Stage 6.00 ft (relative to basin bottom at Stage = 0 ft) Spillway Design Flow Depth 0.78 feet Spillway Crest Length 25.00 feet Spillway Crest Length 0.78 feet 3.99 acres Spillway End Slopes = 4.00 H:V Basin Area at Top of Freeboard = 1.01 acres 3.99 acres CUHP Runoff Volume (are-ft) Cule CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrograph Stable (Columns W through AF). Nota 4.697 N/A N/A 1.19 1.50 1.75 2.00 2.25 2.52 3.14 Outed Preselored metheedeporent Pea	Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Open Area % =	Zone 3 Weir 4.85 8.00 0.00 3.50 70%	Not Selected N/A N/A N/A N/A N/A	ft (relative to basin t feet H:V feet %, grate open area	bottom at Stage = 0 f Gr ດາ	ft) Height of Grate Overflow W rate Open Area / 10 verflow Grate Open	e Upper Edge, H _t = /eir Slope Length =)0-yr Orifice Area = Area w/o Debris =	Zone 3 Weir 4.85 3.50 12.82 19.60	Not Selected N/A N/A N/A N/A	feet feet ft ²
Depth to Invert of Outlet Pipe 0.25 N/A ft (distance below basin bottom at Stage = 0 ft) Outlet Orifice Arrea = 1.53 N/A ft ² Outlet Pipe Diameter = 24.00 N/A inches Outlet Orifice Arrea = 0.55 N/A feet Restrictor Plate Height Above Pipe Invert = 11.75 inches Half-Central Angle of Restrictor Plate on Pipe 0.55 N/A feet Spillway Invert Stage = 6.00 ft (relative to basin bottom at Stage = 0 ft) Spillway Design Flow Depth= 0.78 feet Spillway Invert Stage = 4.00 H:V Basin Area at Top of Freeboard = 1.01 acres Spillway End Slopes = 1.00 feet Basin Volume at Top of Freeboard = 1.01 acres Routed Hydrograph Results The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrograph stable (Columns W through AF). 50 Year 50 Year 50 Year 100 Year 50 Yea	Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Open Area % =	Zone 3 Weir 4.85 8.00 0.00 3.50 70%	Not Selected N/A N/A N/A N/A N/A	ft (relative to basin t feet H:V feet %, grate open area	bottom at Stage = 0 f Gr ດາ	ft) Height of Grate Overflow W rate Open Area / 10 verflow Grate Open	e Upper Edge, H _t = /eir Slope Length =)0-yr Orifice Area = Area w/o Debris =	Zone 3 Weir 4.85 3.50 12.82 19.60	Not Selected N/A N/A N/A N/A	feet feet ft ²
Outlet Pipe Diameter = 24.00 N/A Inches Outlet Orifice Centroid = 0.56 N/A feet Restrictor Plate Height Above Pipe Invert = 11.75 inches Half-Central Angle of Restrictor Plate on Pipe = 1.55 N/A radians User Input: Emergency Spillway (Rectangular or Trapezoidal) Calculated Parameters for Spillway Calculated Parameters for Spillway Feet Spillway Crest Length 25.00 feet 510 7.78 feet Spillway Crest Length 25.00 feet 510 7.78 feet Spillway Crest Length 4.00 H:V Basin Area at Top of Freeboard = 7.78 feet Spillway Starge Table Starge Tabl	Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Open Area % = Debris Clogging % =	Zone 3 Weir 4.85 8.00 0.00 3.50 70% 50%	Not Selected N/A N/A N/A N/A N/A N/A estrictor Plate, or R	ft (relative to basin t feet H:V feet %, grate open area %	bottom at Stage = 0 f Gr ດາ	ft) Height of Grate Overflow W rate Open Area / 10 verflow Grate Open Overflow Grate Open	te Upper Edge, H_t = /eir Slope Length =)0-yr Orifice Area = Area w/o Debris = n Area w/ Debris =	Zone 3 Weir 4.85 3.50 12.82 19.60 9.80	Not Selected N/A N/A N/A N/A N/A Elow Restriction Pl	feet feet ft ² ft ²
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Area at Maximum Ponding Depth (acres) = 0.47 0.67 0.64 0.69 0.71 0.73 0.75 0.80 0.85	Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Open Area % = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length = Spillway Crest Length = Spillway Crest Length = Spillway Ed Slopes = Freeboard above Max Water Surface = CUHP Runoff Volume (acre-ft) = Inflow Hydrograph Nolume (acre-ft) = CUHP Predevelopment Peak Q (cfs) = OPTIONAL Override Predevelopment Peak Q (cfs) = Peak Inflow Q (cfs) = Peak fundow Q (cfs) = Ratio Peak Outflow to Predevelopment Q acre ft) = Ratio Peak Outflow to Predevelopment Peak Q (cfs) = Peak Inflow Q (cfs) = Peak Inflow Q (cfs) = Max Velocity through Grate 1 (fps) = Max Velocity through Grate 1 (fps) =	Zone 3 Weir 4.85 8.00 0.00 3.50 70% 50% (Circular Orifice, Re Zone 3 Restrictor 0.25 24.00 11.75 Trapezoidal) 6.00 25.00 4.00 1.00 The user can overr WQCV N/A N/A N/A N/A N/A N/A N/A N/A	Not Selected N/A N/A N/A N/A N/A N/A N/A N/A Setrictor Plate, or R Not Selected N/A N/A N/A ft (relative to basin feet H:V feet ide the default CUH EURV N/A 1.518 N/A	ft (relative to basin the feet H:V feet %, grate open area %, grate open area %, grate open area %, ft (distance below base inches inches inches %) ft (distance below base inch	bottom at Stage = 0 f Gr a/total area C asin bottom at Stage Half-Cent = 0 ft) 1.867 1.867 1.867 1.867 1.867 0.27 30.6 3.7 0.27 30.7 0.27 30.6 3.7 0.7 0.7 0.7 0.7 0.7 0.7	 Height of Gratt Overflow W rate Open Area / 10 verflow Grate Open Dverflow Grate Open Dverflow Grate Open Dverflow Grate Open Called	e Upper Edge, H _t = Veir Slope Length = 00-yr Orifice Area = Area w/o Debris = n Area w/o Debris = alculated Parameters utlet Orifice Area = t Orifice Centroid = t Orifice Cent	Zone 3 Weir 4.85 3.50 12.82 19.60 9.80 s for Outlet Pipe w/ Zone 3 Restrictor 1.53 0.56 1.55 Calculated Parame ^c 0.78 7.78 1.01 3.99 SO Year 2.25 3.149 3.149 1.7.7 0.91 51.6 1.6.8 1.0 Outlet Plate 1 0.8 N/A	Not Selected N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A	feet feet ft ² ft ² ft ² feet radians 500 Year 3.14 4.697 4.697 3.1.6 3.1.6 7.7.4 3.1.6 3.1.6 3.1.6 3.7.4 3.6.4 1.2 Spillway 0.9 N/A
	Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Open Area % = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Reuted Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Punoff Volume (arce-ft) = Inflow Hydrograph Volume (arce-ft) = CUHP Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, q (cfs/arce) = Peak Inflow Q (cfs) = Ratio Peak Outflow Q (cfs) = Ratio Peak Outflow to Predevelopment Q = Max Velocity through Grate 1 (fps) = Max Velocity through Grate 1 (fps) = Time to Drain 97% of Inflow Volume (hours) = Time to Drain 97% of Inflow Volume (hours)	Zone 3 Weir 4.85 8.00 0.00 3.50 70% 50% (Circular Orifice, Re Zone 3 Restrictor 0.25 24.00 11.75 Trapezoidal) 6.00 25.00 4.00 1.00 The user can overr WQCV N/A 0.453 N/A N/A N/A N/A N/A N/A N/A N/A	Not Selected N/A N/A N/A N/A N/A N/A N/A Setrictor Plate, or R Not Selected N/A N/A ft (relative to basin feet H:V feet ide the default CUI EURV N/A 1.518 N/A 1.518 N/A	ft (relative to basin the feet H:V feet %, grate open area % feet %, grate open area % ft (distance below be inches inches inches hottom at Stage = 4/P hydrographs and 2 Year 1.19 1.391 1.8 1.391 1.8 1.391 1.8 1.391 1.8 1.391 1.8 1.391 1.8 1.391 1.8 1.391 1.8 1.391 1.8 1.391 1.8 1.391 1.8 1.391 1.8 1.391	bottom at Stage = 0 f Gr Op a/total area O asin bottom at Stage Half-Cent tain bottom at Stage tain bottom at Stagettain tain bottom at Stagettai	 Height of Gratt Overflow Wir rate Open Area / 10 verflow Grate Open Overflow Grate Open Dverflow Grate Open Dverflow Grate Open Outlet Tral Angle of Restrict Spillway D Stage at T Basin Area at T Basin Volume at T Basin Volume at T In Year 1.75 2.267 2.267 2.267 2.267 2.267 2.267 2.267 2.267 36.1 7.8 0.40 36.1 7.8 1.0 Overflow Weir 1 0.4 N/A 82 89 	e Upper Edge, H _t = Veir Slope Length = 00-yr Orifice Area = Area w/O Debris = n Area w/O Debris = n Area w/Debris = n Area w/Debris = alculated Parameters utlet Orifice Area = t Orifice Centroid = tor Plate on Pipe = Cop of Freeboard = Top of Freeboard = Cop	Zone 3 Weir 4.85 3.50 12.82 19.60 9.80 20ne 3 Restrictor 1.53 0.56 1.55 <u>Calculated Parame</u> 0.78 7.78 1.01 3.99 <i>trographs table (Col</i> 50 Year 2.25 3.149 3.149 3.149 1.77 0.91 51.6 16.8 1.0 Outlet Plate 1 0.8 N/A 80 88	Not Selected N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A	feet feet feet ft ² ft ² feet radians 500 Year 3.14 4.697 3.14 4.697 3.16 7.7.4 3.6.4 1.6 3.6.4 1.2 Spillway 0.9 N/A 76 86
Maximum Volume Stored (acre-ft) = 0.453 1.519 1.335 1.635 1.719 1.848 2.011 2.352 2.682	Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Open Area % = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = CUHP Runoff Volume (acre-ft) = Inflow Hydrograph Nesults OPTIONAL Override Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, q (cfs/acre) = Peak Inflow Q (cfs) = Peak Inflow Q (cfs) = Peak Inflow Q (cfs) = Max Velocity through Grate 1 (fps) = Max Velocity through Grate 1 (fps) = Maximun Ponding Depth (ft) = Maximun Ponding Depth (ft) =	Zone 3 Weir 4.85 8.00 0.00 3.50 70% 50% (Circular Orifice, Re Zone 3 Restrictor 0.25 24.00 11.75 Trapezoidal) 6.00 25.00 4.00 1.00 The user can overr WQCV N/A N/A N/A N/A N/A N/A N/A N/A	Not Selected N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A	ft (relative to basin the feet H:V feet H:V feet 9%, grate open area 9% feet open area 9% ft (distance below be inches inches inches inches 1.19 1.391 1.391 1.391 1.391 1.391 1.391 1.391 1.8 0.10 22.9 0.3 N/A Plate N/A Plate N/A N/A 78 83 4.56	bottom at Stage = 0 f Gr Da/total area C asin bottom at Stage Half-Cent asin bottom at Stage Half-Cent tage Half-Cent s 0 ft) 1.867 1.867 1.867 5.1 0.27 30.6 3.7 0.27 0.27 0.2 N/A 84 90 5.02	 Height of Gratt Overflow Wrate Open Area / 10 verflow Grate Open Dverflow Grate Open Dverflow Grate Open Dverflow Grate Open Called Comparison Stage at 7 Basin Volume at 7 Basin Volume at 7 Basin Volume at 7 Called Comparison Spillway D Stage at 7 Basin Volume at 7 Basin Volume at 7 Called Comparison Spillway D Stage at 7 Basin Volume at 7 Called Comparison Spillway D Stage at 7 Basin Volume at 7 Called Comparison Spillway D Stage at 7 Called Comparison Spillway D Spillway D Spillway	e Upper Edge, H _t = Veir Slope Length = 00-yr Orifice Area = Area w/o Debris = n Area w/o Debris = n Area w/ Debris = alculated Parameters utlet Orifice Area = t Orifice Centroid = t Orifice Centro	Zone 3 Weir 4.85 3.50 12.82 19.60 9.80 S for Outlet Pipe w/ Zone 3 Restrictor 1.53 0.56 1.55 Calculated Parame ^o 0.78 7.78 1.01 3.99 S Year 2.25 3.149 3.149 1.7.7 0.91 51.6 16.8 1.0 Outlet Plate 1 0.8 N/A 80 88 5.54	Not Selected N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A	feet feet feet ft ² ft ² feet radians 500 Year 3.14 4.697 3.14 4.697 3.16 1.63 7.7.4 3.16 1.63 7.7.4 3.16 1.63 7.7.4 3.16 1.63 7.7.4 3.16 1.63 7.7.4 3.16 1.63 7.7.4 3.16 1.63 7.7.4 1.2 5pillway 0.9 N/A 7.6 8.6 6.38



Stormwater Detention and Infiltration Design Data Sheet

Norkbook Protected

Worksheet Protected

User Defined User Defined User Defined User Defined

Stormwater Facility Name: Dwire Storage Yard

Facility Location & Jurisdiction: 38.88423 Latitude, -104.67879 Longitude, El Paso County

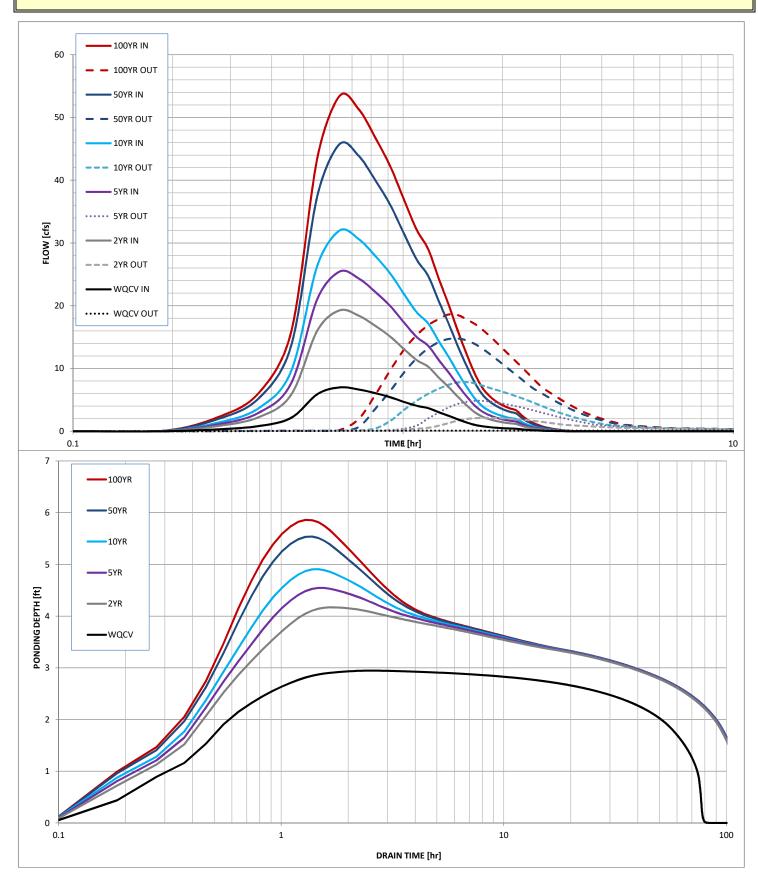
User Input: Watershed Characteristics Watershed Slope = 0.021 ft/ft Watershed Length = 1535 ft 19.36 Watershed Area = acres 72.2% Watershed Imperviousness = percent 0.0% Percentage Hydrologic Soil Group A = percent Percentage Hydrologic Soil Group B = 100.0% percent Percentage Hydrologic Soil Groups C/D = 0.0% percent Location for 1-hr Rainfall Depths (use dropdown): User Input

WQCV Treatment Method = Extended Detention

	User Defined	User Defined	User Defined	User Defined
	Stage [ft]	Area [ft^2]	Stage [ft]	Discharge [cfs]
ſ	0.00	102	0.00	0.00
I	0.33	102	0.33	0.01
ſ	0.50	220	0.50	0.02
ſ	0.83	550	0.83	0.03
ſ	1.00	1,682	1.00	0.04
ſ	1.40	3,841	1.40	0.05
ſ	1.83	6,231	1.83	0.06
	2.00	9,035	2.00	0.07
	2.40	14,248	2.40	0.08
	2.83	19,968	2.83	0.09
	3.00	21,616	3.00	0.10
	3.35	23,672	3.35	0.12
	3.83	24,562	3.83	0.50
	4.00	26,058	4.00	1.00
	4.30	27,609	4.30	3.00
	4.83	29,200	4.83	7.00
	5.83	34,177	5.83	18.00
	6.83	39,216	6.83	40.00
ſ				
Į				

After completing and printing this worksheet to a pdf, go to: https://maperture.digitaldataservices.com/gvh/?viewer=cswdif create a new stormwater facility, and attach the pdf of this worksheet to that record.

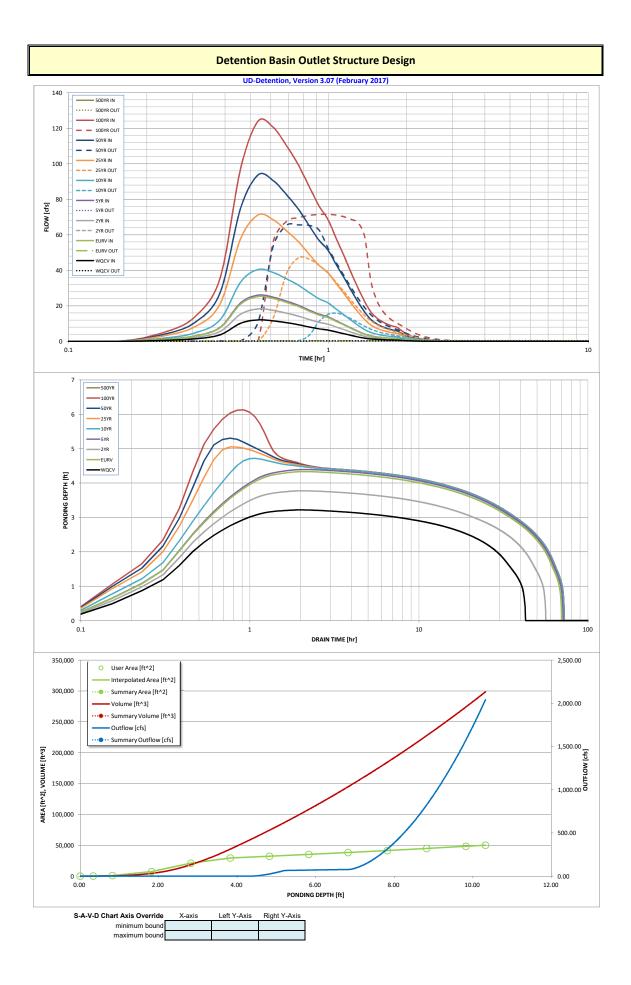
Routed Hydrograph Results											
Design Storm Return Period =	WQCV	2 Year	5 Year	10 Year	50 Year	100 Year					
One-Hour Rainfall Depth =	0.53	1.19	1.50	1.75	2.25	2.52	in				
Calculated Runoff Volume =	0.460	1.287	1.706	2.151	3.092	3.621	acre-ft				
OPTIONAL Override Runoff Volume =							acre-ft				
Inflow Hydrograph Volume =	0.460	1.286	1.705	2.150	3.092	3.620	acre-ft				
Time to Drain 97% of Inflow Volume =	72.5	103.5	101.3	98.9	93.4	90.7	hours				
Time to Drain 99% of Inflow Volume =	75.4	110.1	109.7	108.8	106.9	105.8	hours				
Maximum Ponding Depth =	2.95	4.17	4.55	4.91	5.54	5.86	ft				
Maximum Ponded Area =	0.48	0.62	0.65	0.68	0.75	0.79	acres				
Maximum Volume Stored =	0.441	1.117	1.354	1.593	2.047	2.294	acre-ft				



Stormwater Detention and Infiltration Design Data Sheet

DETENTION BASIN STAGE-STORAGE TABLE BUILDER														
UD-Detention, Version 3.07 (February 2017)														
Project: Ti	imberline St	torage (Ame	nded)											
Basin ID: FS	SD Pond 1													
ZONE 3														
ZON	IE 1													
		100-YE	AR		Depth Increment =									
PERMANENT ORIFICES	AND 2	ORIFIC	E		Deptit Increment -		Optional				Optional			
POOL Example Zone C	Configurati	on (Retent	ion Pond)		Stage - Storage Description	Stage (ft)	Override Stage (ft)	Length (ft)	Width (ft)	Area (ft^2)	Override Area (ft ²)	Area (acre)	Volume (ft^3)	Volume (ac-ft)
Required Volume Calculation				30.18	Top of Micropool	(11)	0.00			(11.2)	0	(acre) 0.000	(11.3)	(ac-it)
Selected BMP Type =	EDB	1		30.18	30.51		0.33				147	0.003	23	0.001
Watershed Area =	63.84	acres			31 32		0.82				853	0.020	261	0.006
Watershed Length =	1,880 0.014	π ft/ft			32		1.82 2.82				7,247 20,867	0.166	4,247 18,376	0.097
Watershed Slope = Watershed Imperviousness =	22.50%	π/π percent			33		3.82	-			20,867	0.479	18,376 43,470	0.422
Percentage Hydrologic Soil Group A =	30.0%	percent			35		4.82			-	32,162	0.738	74,212	1.704
Percentage Hydrologic Soil Group R =	70.0%	percent			36		5.82			-	35,142	0.807	107.864	2.476
Percentage Hydrologic Soil Groups C/D =	0.0%	percent			37		6.82			-	38,215	0.877	144,542	3.318
Desired WQCV Drain Time =	40.0	hours			38		7.82				41,392	0.950	184,346	4.232
Location for 1-hr Rainfall Depths = Us		lingaro			39		8.82				44,738	1.027	227,411	5.221
Water Quality Capture Volume (WQCV) =	0.668	acre-feet	Optional Use		40		9.82				48,283	1.108	273,921	6.288
Excess Urban Runoff Volume (EURV) =	1.406	acre-feet	1-hr Precipita		40.5		10.32				50.043	1.149	298,503	6.853
2-yr Runoff Volume (P1 = 1.19 in.) =	1.016	acre-feet	1.19	inches									,	
5-yr Runoff Volume (P1 = 1.5 in.) =	1.450	acre-feet	1.50	inches										
10-yr Runoff Volume (P1 = 1.75 in.) =	2.269	acre-feet	1.75	inches										
25-yr Runoff Volume (P1 = 2 in.) =	4.027	acre-feet	2.00	inches										
50-yr Runoff Volume (P1 = 2.25 in.) =	5.340	acre-feet	2.25	inches										
100-yr Runoff Volume (P1 = 2.52 in.) =	7.102	acre-feet	2.52	inches						-				
500-yr Runoff Volume (P1 = 0 in.) =	0.000	acre-feet		inches										
Approximate 2-yr Detention Volume =	0.947	acre-feet	-	-										
Approximate 5-yr Detention Volume =	1.358	acre-feet								-				
Approximate 10-yr Detention Volume =	2.026	acre-feet								-				
Approximate 25-yr Detention Volume =	2.489	acre-feet								-				
Approximate 50-yr Detention Volume =	2.700	acre-feet												
Approximate 100-yr Detention Volume =	3.333	acre-feet												
Stage-Storage Calculation		-												
Zone 1 Volume (WQCV) =	0.668	acre-feet												
Zone 2 Volume (EURV - Zone 1) =	0.737	acre-feet												
Zone 3 Volume (100-year - Zones 1 & 2) =	1.928	acre-feet												
Total Detention Basin Volume =	3.333	acre-feet												
Initial Surcharge Volume (ISV) =	user	ft^3												
Initial Surcharge Depth (ISD) =	user	ft												┥───┤
Total Available Detention Depth (H _{total}) =	user	ft												┝───┤
Depth of Trickle Channel (H_{TC}) = Slope of Trickle Channel (S_{TC}) =	user	n 												├── ┤
Slope of Trickle Channel $(S_{TC}) =$ Slopes of Main Basin Sides $(S_{main}) =$	user	ft/ft												├ ───┤
Basin Length-to-Width Ratio $(R_{I/W}) =$	user	H:V								-				<u> </u>
Dasin Lengur-to-Width Mallo (RL/W) -	usei	J												┝───┤
														<u> </u>

	Detention Basin Outlet Structure Design									
UD-Detention, Version 3.07 (February 2017)										
	: Timberline Storage : FSD Pond 1	e (Amended)								
(ZONE 3 (ZONE 2										
				Stage (ft)	Zone Volume (ac-ft)	Outlet Type				
			Zone 1 (WQCV)	3.29	0.668	Orifice Plate				
	100-YEA ORIFICE	R	Zone 2 (EURV)	4.41	0.737	Orifice Plate				
PERMANDA POOL Example Zone			'one 3 (100-year)	6.84	1.928	Weir&Pipe (Restrict)				
Example Zone	e Configuration (Re	etention Pond)	-		3.333	Total				
User Input: Orifice at Underdrain Outlet (typically u		-	6 1				ed Parameters for Un			
Underdrain Orifice Invert Depth = Underdrain Orifice Diameter =		ft (distance below th	ne filtration media surf	face)		rdrain Orifice Area = ain Orifice Centroid =	N/A N/A	ft ² feet		
	N/A	inches			onderuna	in onne centroid -	N/A	leet		
User Input: Orifice Plate with one or more orifices of	or Elliptical Slot Weir	(typically used to dra	ain WQCV and/or EUR	V in a sedimentation	n BMP)	Calcu	lated Parameters for	Plate		
Invert of Lowest Orifice =			pottom at Stage = 0 ft)			rifice Area per Row =		ft²		
Depth at top of Zone using Orifice Plate =	4.41		bottom at Stage = 0 ft)			lliptical Half-Width =	N/A	feet		
Orifice Plate: Orifice Vertical Spacing = Orifice Plate: Orifice Area per Row =	= 19.60 = N/A	inches inches			Elli	ptical Slot Centroid = Elliptical Slot Area =	N/A N/A	feet ft ²		
office Plate. Office Area per Now -	N/A	inches				Emptical Slot Area -	N/A	In		
User Input: Stage and Total Area of Each Orifice	· · · · ·	-	1					1	1	
	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)		
Stage of Orifice Centroid (ft) Orifice Area (sq. inches)		1.47 2.30	2.94 1.50							
Office Area (sq. Inches)	2.01	2.30	1.00						1	
	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)		
Stage of Orifice Centroid (ft)										
Orifice Area (sq. inches))								J	
User Input: Vertical Orifice (Cir	cular or Rectangular)					Calculated	Parameters for Vert	tical Orifice		
oser input. Vertical office (eith	Not Selected	Not Selected	1			Calculated	Not Selected	Not Selected	1	
Invert of Vertical Orifice =	N/A	N/A	ft (relative to basin b	ottom at Stage = 0 ft)	i v	ertical Orifice Area =	N/A	N/A	ft ²	
Depth at top of Zone using Vertical Orifice =	N/A	N/A	ft (relative to basin b	ottom at Stage = 0 ft)	Verti	cal Orifice Centroid =	N/A	N/A	feet	
Vertical Orifice Diameter =	N/A	N/A	inches							
User Input: Overflow Weir (Dropbox) and G	Grate (Flat or Sloped)					Calculated	Parameters for Ove	rflow Weir		
	Zone 3 Weir	Not Selected					Zone 3 Weir	Not Selected		
Overflow Weir Front Edge Height, Ho =	4.41	N/A	ft (relative to basin bot	ttom at Stage = 0 ft)	Height of Gr	ate Upper Edge, H _t =	4.41			
Overflow Weir Front Edge Length = Overflow Weir Slope =	17.00				0.00			N/A	feet	
		N/A N/A	feet H:V (enter zero for fla	at grate)		Weir Slope Length =	4.00	N/A	feet	
Horiz. Length of Weir Sides =	= 0.00	N/A N/A N/A	feet H:V (enter zero for fla feet	at grate)	Grate Open Area /					
	0.00	N/A	H:V (enter zero for fla		Grate Open Area / Overflow Grate Op	Weir Slope Length = 100-yr Orifice Area =	4.00 7.24	N/A N/A	feet should be <u>></u> 4	
Horiz. Length of Weir Sides =	= 0.00 = 4.00	N/A N/A	H:V (enter zero for fla feet		Grate Open Area / Overflow Grate Op	Weir Slope Length = 100-yr Orifice Area = en Area w/o Debris =	4.00 7.24 47.60	N/A N/A N/A	feet should be <u>></u> 4 ft ²	
Horiz. Length of Weir Sides = Overflow Grate Open Area % = Debris Clogging % =	= 0.00 = 4.00 = 70% = 50%	N/A N/A N/A N/A	H:V (enter zero for fla feet %, grate open area/to %		Grate Open Area / Overflow Grate Op Overflow Grate O	Weir Slope Length = 100-yr Orifice Area = en Area w/o Debris = ben Area w/ Debris =	4.00 7.24 47.60 23.80	N/A N/A N/A N/A	feet should be ≥ 4 ft ² ft ²	
Horiz. Length of Weir Sides = Overflow Grate Open Area % =	= 0.00 = 4.00 = 70% = 50%	N/A N/A N/A N/A	H:V (enter zero for fla feet %, grate open area/to %		Grate Open Area / Overflow Grate Op Overflow Grate O	Weir Slope Length = 100-yr Orifice Area = en Area w/o Debris =	4.00 7.24 47.60 23.80	N/A N/A N/A N/A	feet should be ≥ 4 ft ² ft ²	
Horiz. Length of Weir Sides = Overflow Grate Open Area % = Debris Clogging % =	= 0.00 = 4.00 = 70% = 50%	N/A N/A N/A N/A ctor Plate, or Rectang	H:V (enter zero for fla feet %, grate open area/to %	otal area	Grate Open Area / Overflow Grate Op Overflow Grate O	Weir Slope Length = 100-yr Orifice Area = en Area w/o Debris = ben Area w/ Debris =	4.00 7.24 47.60 23.80	N/A N/A N/A N/A	feet should be≥4 ft ² ft ²	
Horiz. Length of Weir Sides = Overflow Grate Open Area % = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate (Ci	= 0.00 = 4.00 = 70% = 50% ircular Orifice, Restric Zone 3 Restrictor = 0.25 = 42.00	N/A N/A N/A N/A ctor Plate, or Rectang Not Selected	H:V (enter zero for fla feet %, grate open area/to % gular Orifice)	otal area n bottom at Stage = 0 f	Grate Open Area / Overflow Grate Op Overflow Grate Op (t) Out	Weir Slope Length = 100-yr Orifice Area = en Area w/o Debris = ben Area w/ Debris = Calculated Parameter Outlet Orifice Area = let Orifice Centroid =	4.00 7.24 47.60 23.80 s for Outlet Pipe w/ Zone 3 Restrictor 6.58 1.28	N/A N/A N/A N/A Flow Restriction Plat Not Selected N/A N/A	feet should be \geq 4 ft ² ft ² ft ² ft ² feet	
Horiz. Length of Weir Sides = Overflow Grate Open Area % = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate (Ci Depth to Invert of Outlet Pipe =	= 0.00 = 4.00 = 70% = 50% ircular Orifice, Restric Zone 3 Restrictor = 0.25 = 42.00	N/A N/A N/A ctor Plate, or Rectang Not Selected N/A	H:V (enter zero for fla feet %, grate open area/to % gular Orifice) ft (distance below basi	otal area n bottom at Stage = 0 f	Grate Open Area / Overflow Grate Op Overflow Grate O Overflow Grate O	Weir Slope Length = 100-yr Orifice Area = en Area w/o Debris = ben Area w/ Debris = Calculated Parameter Outlet Orifice Area = let Orifice Centroid =	4.00 7.24 47.60 23.80 *s for Outlet Pipe w/ Zone 3 Restrictor 6.58	N/A N/A N/A Flow Restriction Plat Not Selected N/A	feet should be \geq 4 ft ² ft ² ft ² ft ²	
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Horiz. Length of Weir Sides = Overflow Grate Open Area % = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate (Cr Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectan Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Routed Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = Calculated Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = Predevelopment Deak Flow, q (cfs/acre) = Predevelopment Peak Q (cfs) = Peak Inflow Q (cfs) = Ratio Peak Outflow to Predevelopment Q = Structure Controlling Flow = Max Velocity through Grate 1 (fps) = Max Velocity through Grate 1 (fps) =	= 0.00 = 4.00 = 70% 50% ircular Orifice, Restrict Zone 3 Restrictor = 0.25 = 42.00 = 27.15 sular or Trapezoidal) = 6.85 = 72.50 = 10.00 = 0.67 = 0.668 = 0.00 = 0.668 = 0.00 = 12.1 = 0.3 = N/A = N/A = N/A	N/A N/A N/A N/A N/A N/A N/A Ctor Plate, or Rectang Not Selected N/A N/A ft (relative to basin I feet H:V feet EURV 1.07 1.406 0.00 0.0 25.2 0.4 N/A Plate N/A N/A	H:V (enter zero for fli feet %, grate open area/t % gular Orifice) ft (distance below basi inches inches bottom at Stage = 0 ft) 2 Year 1.19 1.016 0.01 0.6 18.3 0.3 N/A Plate N/A N/A	5 Year 1.50 1.450 1.451 0.02 1.2 26.0 0.4 0.3 Plate N/A N/A	Grate Open Area / Overflow Grate Op Overflow Grate Op Overflow Grate O Overflow Grate O Out Central Angle of Rest Spillway Stage a Basin Area a Basin Area a 2.270 0.16 10.5 40.4 15.9 1.5 Overflow Grate 1 0.3 N/A	Weir Slope Length = 100-yr Orifice Area = en Area w/o Debris = ben Area w/o Debris = Calculated Parameter Outlet Orifice Area = let Orifice Centroid = rictor Plate on Pipe = Calcula Design Flow Depth= t Top of Freeboard = t Top of Freeboard = 25 Year 2.00 4.027 4.030 0.53 33.6 71.2 4.7.0 1.4 Overflow Grate 1 1.0 N/A	4.00 7.24 47.60 23.80 s for Outlet Pipe w/ Zone 3 Restrictor 6.58 1.28 1.87 ted Parameters for S 0.65 8.17 0.98 5.65 8.17 0.98 5.340 5.336 0.78 49.9 9.3.7 65.5 1.3 Outlet Plate 1 1.4 N/A	N/A N/A N/A N/A N/A Flow Restriction Plat Not Selected N/A N/A N/A N/A N/A Spillway feet feet acres 100 Year 2.52 7.102 71.5 1.23.9 71.5 1.0 Outlet Plate 1 1.5 N/A	feet should be ≥ 4 ft ² ft ² fe ft ² feet radians #N/A 0.00 0.00 0.00 0.00 0.00 0.00 mN/A #N/A #N/A #N/A #N/A	
Horiz. Length of Weir Sides = Overflow Grate Open Area % = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate (Cr Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectan Spillway Invert Stage= Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Routed Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = Calculated Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = Predevelopment Unit Peak Flow, g (cfs/acre) Peak Inflow Q (cfs) = Peak Outflow to Predevelopment Q = Structure Controlling Flow = Max Velocity through Grate 1 (fps) = Max Velocity through Grate 2 (fps) = Time to Drain 97% of Inflow Volume (hours)	= 0.00 = 4.00 = 70% = 50% ircular Orifice, Restrict Zone 3 Restrictor = 0.25 = 42.00 = 27.15 = 42.00 = 0.75 = 0.685 = 72.50 = 10.00 = 0.668 = 0.668 = 0.668 = 0.668 = 0.668 = 0.668 = 0.668 = 0.668 = 0.668 = 0.3 = 0.668 = 0.71 = 0.3 = 0.468 = 0.71 = 0.3 = 0.468 = 0.71 = 0.73 = 0.73 = 0.75 = 0	N/A N/A N/A N/A N/A Stor Plate, or Rectang Not Selected N/A N/A N/A ft (relative to basin lifeet H:V feet H:V feet U.07 1.406 0.00 0.0 25.2 0.4 N/A Plate N/A 64	H:V (enter zero for fli feet %, grate open area/t % gular Orifice) ft (distance below basi inches inches bottom at Stage = 0 ft) 2 Year 1.19 1.016 0.01 0.6 18.3 0.3 0.3 N/A Plate N/A N/A 52	5 Year 1.50 1.450 1.450 1.451 0.02 1.2 26.0 0.4 0.3 Plate N/A 65	Grate Open Area / Overflow Grate Op Overflow Grate Op Overflow Grate Op () (t) Central Angle of Rest Spillway Stage a Basin Area a Basin Area a 2.270 0.16 10.5 40.4 15.9 1.5 Overflow Grate 1 0.3 N/A 64	Weir Slope Length = 100-yr Orifice Area = en Area w/o Debris = been Area w/o Debris = Calculated Parameter Outlet Orifice Centroid = rictor Plate on Pipe = Calcula Design Flow Depth= t Top of Freeboard = t Top of Freeboard = t Top of Freeboard = 25 Year 2.00 4.027 4.030 0.53 33.6 7.1.2 47.0 1.4 Overflow Grate 1 1.0 N/A 60	4.00 7.24 47.60 23.80 s for Outlet Pipe w/ Zone 3 Restrictor 6.58 1.28 1.28 1.28 1.87 ted Parameters for S 0.65 8.17 0.98 50 Year 2.25 5.340 5.336 0.78 4.9.9 93.7 65.5 1.3 Outlet Plate 1 1.4 N/A 57	N/A N/A N/A N/A N/A Flow Restriction Plate Not Selected N/A N/A N/A N/A N/A N/A N/A Spillway feet feet acres 100 Year 2.52 7.108 1.12 71.5 123.9 71.5 1.0 Outlet Plate 1 1.5 N/A 54	feet should be ≥ 4 ft ² ft ² ft ² feet radians	
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Horiz. Length of Weir Sides = Overflow Grate Open Area % = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate (Cr Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectan Spillway Invert Stage= Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Routed Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = Calculated Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = Predevelopment Unit Peak Flow, g (cfs/acre) Peak Inflow Q (cfs) = Peak Outflow to Predevelopment Q (cfs) Peak Outflow to Predevelopment Q (cfs) Structure Controlling Flow = Max Velocity through Grate 1 (fps) = Max Velocity through Grate 2 (fps) = Time to Drain 97% of Inflow Volume (hours)	= 0.00 = 4.00 = 70% = 50% ircular Orifice, Restrict Zone 3 Restrictor = 0.25 = 42.00 = 27.15 = 42.00 = 0.75 = 0.685 = 72.50 = 10.00 = 0.668 = 0.668 = 0.668 = 0.668 = 0.668 = 0.668 = 0.668 = 0.668 = 0.668 = 0.3 = 0.668 = 0.71 = 0.3 = 0.468 = 0.71 = 0.3 = 0.468 = 0.71 = 0.73 = 0.73 = 0.75 = 0	N/A N/A N/A N/A N/A Stor Plate, or Rectang Not Selected N/A N/A N/A ft (relative to basin lifeet H:V feet H:V feet 0.07 1.406 0.00 0.0 25.2 0.4 N/A Plate N/A 64	H:V (enter zero for fla feet %, grate open area/td % gular Orifice) ft (distance below basi inches inches bottom at Stage = 0 ft) 2 Year 1.19 1.016 0.01 0.6 18.3 0.3 N/A Plate N/A N/A N/A N/A S2 55	5 Year Half-4 1.50 1.450 1.450 1.450 1.2 26.0 0.4 0.3 Plate N/A N/A N/A N/A 65 69	Grate Open Area / Overflow Grate Op Overflow Grate Op Overflow Grate O (t) Out Central Angle of Rest Spillway Stage a Basin Area a 10 Year 1.75 2.269 2.270 0.16 10.5 40.4 15.9 1.5 Overflow Grate 1 0.3 N/A 64 69	Weir Slope Length = 100-yr Orifice Area = en Area w/o Debris = ben Area w/o Debris = calculated Parameter Outlet Orifice Area = let Orifice Centroid = rictor Plate on Pipe = Calcula Design Flow Depth= t Top of Freeboard = t Top of Freeboard = t Top of Freeboard = 25 Year 2.00 4.027 4.030 0.53 3.3.6 71.2 4.7.0 1.4 Overflow Grate 1 1.0 N/A 60 67	4.00 7.24 47.60 23.80 s for Outlet Pipe w/ Zone 3 Restrictor 6.58 1.28 1.87 ted Parameters for S 0.65 8.17 0.98 5.817 0.98 5.340 5.340 5.336 0.78 49.9 93.7 65.5 1.3 0Utlet Plate 1 1.4 N/A N/A 57 65	N/A N/A N/A N/A N/A Flow Restriction Plate Not Selected N/A N/A N/A N/A N/A N/A N/A Spillway feet feet acres 100 Year 2.52 7.108 1.12 71.5 123.9 71.5 1.0 Outlet Plate 1 1.5 N/A 54	feet should be ≥ 4 ft ² ft ² feet radians	



Detention Basin Outlet Structure Design

Outflow Hydrograph Workbook Filename: 0:\43095A\Tim Emick\Documents\Reports\Drainage\Excel\2019 UPDATE

	Storm Inflow H			ention, Versio			iranhs develone	d in a separate p	rogram	
	SOURCE	WORKBOOK	WORKBOOK	WORKBOOK	WORKBOOK	WORKBOOK	WORKBOOK	WORKBOOK	WORKBOOK	#N/A
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
4.59 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
4.00 mm	0:04:35	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
Hydrograph	0:09:11	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
Constant	0:13:46	0.53	1.09	0.80	1.13	1.73	2.96	3.79	4.83	#N/A
1.090	0:18:22	1.44	2.98	2.17	3.07	4.74	8.22	10.67	13.83	#N/A
	0:22:57	3.70	7.65	5.57	7.88	12.17	21.10	27.39	35.52	#N/A
	0:27:32	10.17	20.99	15.30	21.64	33.40	57.87	75.04	97.23	#N/A
	0:32:08	12.08 11.53	25.21 24.11	18.28 17.47	25.99 24.87	40.44 38.75	71.18 68.46	93.68 90.53	123.90 120.54	#N/A #N/A
	0:41:19	10.50	21.95	15.90	22.64	35.27	62.33	82.61	110.29	#N/A
	0:45:54	9.38	19.68	14.23	20.30	31.68	56.15	74.46	99.46	#N/A
	0:50:29	8.10	17.07	12.32	17.61	27.58	49.11	65.25	87.35	#N/A
	0:55:05	7.05	14.84	10.72	15.30	23.98	42.87	57.03	76.42	#N/A
	0:59:40 1:04:16	6.39	13.45	9.72	13.88	21.73	38.70	51.38	68.69	#N/A
	1:04:10	5.28 4.31	11.19 9.20	8.06	11.54 9.49	18.13 14.97	32.43 26.87	43.19 35.83	57.97 48.16	#N/A #N/A
	1:13:26	3.32	7.17	5.12	7.41	11.76	21.28	28.50	38.48	#N/A
	1:18:02	2.48	5.43	3.85	5.61	8.98	16.43	22.09	29.94	#N/A
	1:22:37	1.79	3.96	2.79	4.10	6.63	12.26	16.57	22.56	#N/A
	1:27:13	1.39	3.03	2.14	3.13	5.02	9.20	12.38	16.77	#N/A
	1:31:48 1:36:23	1.14	2.47	1.76	2.56	4.07	7.40	9.91	13.37 11.22	#N/A #N/A
	1:40:59	0.97	2.09	1.49	2.16 1.89	3.44 3.00	6.23 5.42	8.33	9.73	#N/A #N/A
	1:45:34	0.85	1.64	1.18	1.89	2.69	4.85	6.47	8.68	#N/A #N/A
	1:50:10	0.71	1.51	1.08	1.56	2.47	4.44	5.92	7.93	#N/A
	1:54:45	0.52	1.11	0.79	1.15	1.82	3.31	4.44	6.01	#N/A
	1:59:20	0.38	0.81	0.58	0.84	1.33	2.40	3.21	4.34	#N/A
	2:03:56 2:08:31	0.28	0.60	0.43	0.62	0.98	1.77	2.38	3.22	#N/A
	2:08:31	0.21 0.15	0.44	0.32	0.46	0.73	1.32 0.96	1.77	2.39	#N/A #N/A
	2:17:42	0.10	0.23	0.16	0.23	0.38	0.69	0.93	1.27	#N/A
	2:22:17	0.07	0.16	0.12	0.17	0.27	0.50	0.68	0.92	#N/A
	2:26:53	0.05	0.11	0.08	0.11	0.19	0.35	0.48	0.65	#N/A
	2:31:28	0.03	0.07	0.05	0.07	0.12	0.23	0.31	0.43	#N/A
	2:36:04	0.01	0.04	0.02	0.04	0.06	0.13	0.18	0.25	#N/A
	2:40:39 2:45:14	0.00	0.01	0.01	0.01	0.03	0.06	0.08	0.12	#N/A #N/A
	2:49:50	0.00	0.00	0.00	0.00	0.00	0.02	0.02	0.04	#N/A
	2:54:25	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	2:59:01	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	3:03:36	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	3:08:11 3:12:47	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	3:12:47	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A #N/A
	3:21:58	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A #N/A
	3:26:33	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	3:31:08	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	3:35:44	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	3:40:19	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	3:44:55 3:49:30	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A #N/A
	3:54:05	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	3:58:41	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	4:03:16	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	4:07:52 4:12:27	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A #N/A
	4:17:02	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	4:21:38	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	4:26:13 4:30:49	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A #N/A
	4:35:24	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A #N/A
	4:39:59	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	4:44:35 4:49:10	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A #N/A
	4:53:46	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A #N/A
	4:58:21	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	5:02:56	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	5:07:32 5:12:07	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A #N/A
	5:16:43	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A #N/A
	5:21:18	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	5:25:53	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	5:30:29	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A

Stormwater Detention and Infiltration Design Data Sheet

User Defined

Stage [ft]

0.00

User Defined

Area [ft^2]

0

Workbook Protected

Worksheet Protected

User Defined

Stage [ft]

0.00

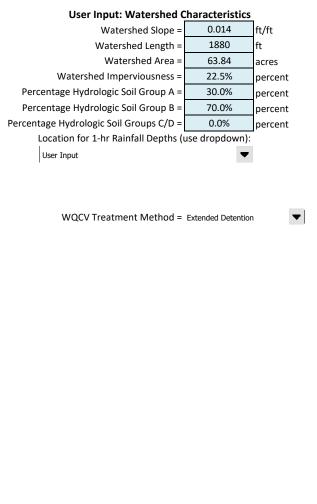
User Defined

Discharge [cfs]

0.00

Stormwater Facility Name: Pond 1

Facility Location & Jurisdiction: Timberline Storage Yard, El Paso County / El Paso County

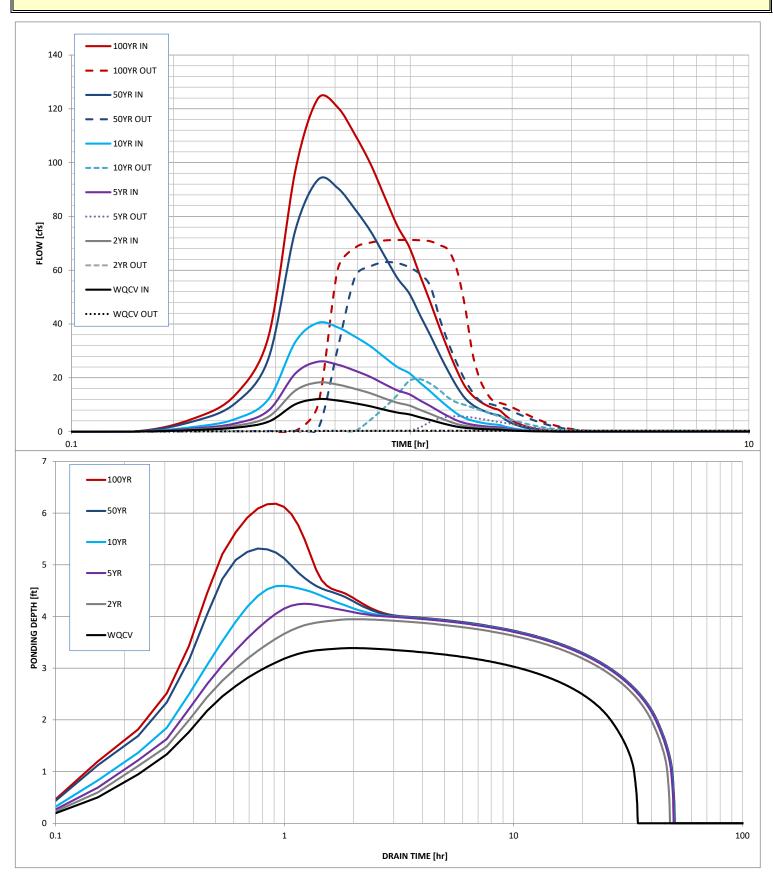


0.33 147 0.30 0.06 1.00 843 1.00 0.10 2.00 7,247 2.00 0.20 3.00 20,867 3.00 0.28 3.50 25,252 0.30 3.50 4.00 29,321 4.00 0.33 4.50 30,747 4.50 11.20 5.00 32,162 5.00 55.50 5.50 33,655 5.50 67.53 35,142 70.91 6.00 6.00 6.31 36,692 6.31 71.50

After completing and printing this worksheet to a pdf, go to: <u>https://maperture.digitaldataservices.com/gvh/?viewer=cswdif</u> create a new stormwater facility, and

attach the pdf of this worksheet to that record.

Routed Hydrograph Results											
Design Storm Return Period =	WQCV	2 Year	5 Year	10 Year	50 Year	100 Year					
One-Hour Rainfall Depth =	0.53	1.19	1.50	1.75	2.25	2.52	in				
Calculated Runoff Volume =	0.668	1.016	1.450	2.269	5.340	7.102	acre-ft				
OPTIONAL Override Runoff Volume =							acre-ft				
Inflow Hydrograph Volume =	0.668	1.015	1.449	2.268	5.331	7.101	acre-ft				
Time to Drain 97% of Inflow Volume =	32.5	44.9	45.7	44.1	38.9	36.2	hours				
Time to Drain 99% of Inflow Volume =	33.9	46.9	48.1	47.6	45.4	44.3	hours				
Maximum Ponding Depth =	3.39	3.95	4.25	4.59	5.31	6.18	ft				
Maximum Ponded Area =	0.56	0.66	0.69	0.71	0.76	0.83	acres				
Maximum Volume Stored =	0.622	0.964	1.165	1.410	1.936	2.625	acre-ft				



Stormwater Detention and Infiltration Design Data Sheet

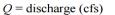
DWIRE YARD EMERGENCY SPILLWAY CALCULATIONS FSD POND

Ha	Horizontal Broad-Crested Weir (Eqn 12-20 UDFCD)										
	Variable			Solve For							
С	3.00			L (ft)	H (ft)	Q (cfs)					
L	25.50	ft		0.0	0.0	60.0					
Н	0.85	ft									
Q		cfs									



Equation 12-20 $Q = C_{BCW} L H^{1.5}$

Where:



 C_{BCW} = broad-crested weir coefficient (This ranges from 2.6 to 3.0. A value of 3.0 is often used in practice.) See Hydraulic Engineering Circular No. 22 for additional information.

L = broad-crested weir length (ft)

H = head above weir crest (ft)

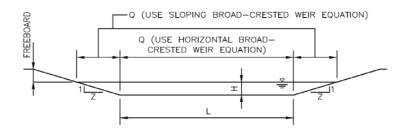
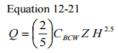


Figure 12-20. Sloping broad-crest weir

Å	Sloping Broad-Crested Weir (Eqn 12-21 UDFCD)										
	Variable				Solve For						
С	3.00			Z (ft)	H (ft)	Q (cfs)					
Ζ	4.00	ft		0.0	0.0	3.2					
H	0.85	ft									
Q		cfs									



20 BOULDER CRESCENT, STE 110 COLORADO SPRINGS, CO 80903 (719) 955-5485 PROJECT: DWIRE STURAGE YARD CIVIL CONSULTANTS, INC. DATE: DUTTFALL REDZAP APRON Q= 17.5 ess $\frac{1}{12} = \frac{1}{12} \left(\frac{1}{12} - \frac{1}{12} \right) = \frac{1}{12} \left(\frac{1}{12} + \frac{1}$ D = 125 = 3.0926.0 At 17.5.55 = 1.19212 0=tan 1 (2 (Expression Francisco) = tan 1 (2 (6.6)) = 4,33 degrees 3(D) = 3(2) = 6 ft $b_{p} = \left(\frac{1}{2L_{p}}\right) \left(\frac{2.0}{0.0} - 2\right) = 3.3 \angle 6 ft$ Use bft minimum FIGURE 9-38 QfD15 = 17.5285/28t1.5= 6.19 FROM FRO. 9-38 REP PAR TYPE"L"= Doo-9" UPGRODE TO TYPE "M" = DOO-12" Tittek NESS 2050 = 2 (12") = 24" THECK Lp= 6ft -T= 2 (10 ban (4.33)) +2 = 2.90 DESTEN = 6x29 x 2' REPEAR ACTUAL 12 X18' X 2' REPRAP BASEN



20 BOULDER CRESCENT. STE 110 COLORADO SPRINGS, CO 80903 (719) 955-5485

PROJECT: DEVILE STORAGE YAR

DATE:

FORE BAY VOLUMES FSD POND SIZE OF CONTRIBUTZNG ANEA = 19.36 AEPES MEN FOR VOLUME = 3% WQCV (MHFD V. 4,03) WOCV = D. 453 AC-FT TOTAL VOL REQ = 0.03 (0.453 Ac-A+) (43560 Ft3) = /591 CF Quo = DESTEND PORNOT Z = 16.7 cts } 16. Quo TOTAL = 266.3 cts } 16.3 = 24 10 EAST FLEESHY RIVER = DESCENDENT 3 = Kilcfs 3 12 18% NORTH FUE RAY RUDTOTAL = 66.3 cfs 3 1003 Que = Poston Point +1 = 405 cts 3 40 4010 WEST FORT BAY Brus TOTAL = 66.3 cts 3 66.3 REQ VOLUME ACTUAL VOLUME (391 CF) (0,24) = 141 CF (1265F) (1.25 dt) = 158 CF (591 CF) (0.10) = 106 CF (98 SF) (1.14) = 108 CF (591 CF) (0.60) = 354.CF (2575F) (1.482) = 360CF



20 BOULDER CRESCENT, STE 110 COLORADO SPRINGS, CO 80903 (719) 955-5485

PROJECT: DWIRE STORAGE AND

DATE:

SIZE FOREBA1 Notelles WITHE FON. 240 of CONTREEBUTTON 1004P. FLOW Q = CLH1.5 EAST Q100 = 16.7cts x 0.02 = 0.334 cts H=1.25 st 4 = CH 1.5 NORTH DIDD = 12.1 cfs x 0.02 = 0.242 cfs H=1.1 St WEST Q100 = 40.5 cts x 0.02 = 0.81 cts H=1484 EAST L = 0.334 3.0 (1.25) 15 = (0.08) (12in) = 0.96" USE 3" WZDE REP DOM MANNAL NORTH L = 0.24284 $3.0(1.1)^{15} = (0.07)(\frac{1210}{184}) = 0.83'' USE 3' w 10E$ PER Den mannalWEST <math>L = 0.81 $3.0(1.4)^{15} = (0.16)(\frac{12''}{184}) = 1.95'' USE 3' w 10E$ $3.0(1.4)^{15} = (0.16)(\frac{12''}{184}) = 1.95''' USE 3' w 10E$ PER DOM MANUAL

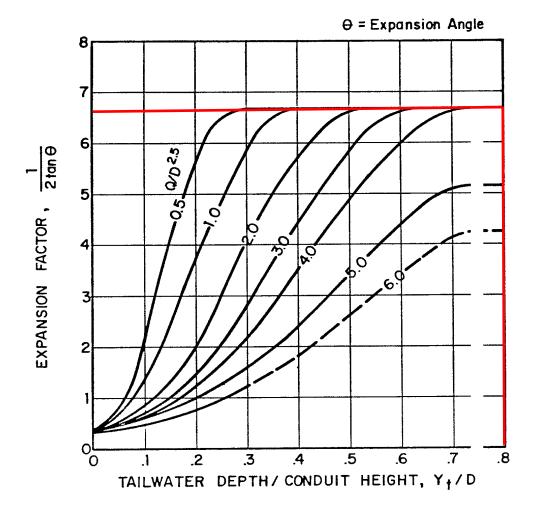


Figure 9-35. Expansion factor for circular conduits

Equation 9-19

$$H_a = \frac{\left(H + Y_n\right)}{2}$$

Where the maximum value of H_a shall not exceed H, and:

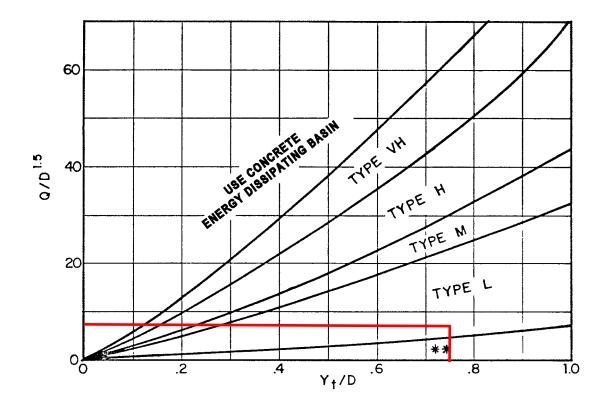
 D_a = parameter to use in place of D in Figure 9-38 when flow is supercritical (ft)

 D_c = diameter of circular culvert (ft)

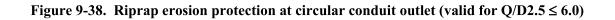
 H_a = parameter to use in place of H in Figure 9-39 when flow is supercritical (ft)

H = height of rectangular culvert (ft)

 Y_n = normal depth of supercritical flow in the culvert (ft)



Use D_a instead of D whenever flow is supercritical in the barrel. **Use Type L for a distance of 3D downstream.





Specification Sheet – VMax[®] SC250[®] Turf Reinforcement Mat

DESCRIPTION

The composite turf reinforcement mat (C-TRM) shall be a machine-produced mat of 70% straw and 30% coconut fiber matrix incorporated into permanent three-dimensional turf reinforcement matting. The matrix shall be evenly distributed across the entire width of the matting and stitch bonded between a heavy duty UV stabilized nettings with 0.50 x 0.50 inch (1.27 x 1.27 cm) openings, an ultra heavy UV stabilized, dramatically corrugated (crimped) intermediate netting with 0.5 x 0.5 inch (1.27 x 1.27 cm) openings, and covered by an heavy duty UV stabilized nettings with 0.50×0.50 inch (1.27 x 1.27 cm) openings. The middle corrugated netting shall form prominent closely spaced ridges across the entire width of the mat. The three nettings shall be stitched together on 1.50 inch (3.81cm) centers with UV stabilized polypropylene thread to form permanent three-dimensional turf reinforcement matting. All mats shall be manufactured with a colored thread stitched along both outer edges as an overlap guide for adjacent mats.

The SC250 shall meet Type 5A, 5B, and 5C specification requirements established by the Erosion Control Technology Council (ECTC) and Federal Highway Administration's (FHWA) FP-03 Section 713.18

Material Content				
Matrix	70% Straw Fiber	0.35 lb/sq yd (0.19 kg/sm)		
MatilX	30% Coconut Fiber	0.15 lbs/sq yd (0.08 kg/sm)		
	Top and Bottom, UV-Stabilized Polypropylene	5 lb/1000 sq ft (2.44 kg/100 sm)		
Netting	Middle, Corrugated UV-Stabilized Polypropylene	24 lb/1000 sf (11.7 kg/100 sm)		
Thread	Polypropylene, UV Stable			

Standard Roll Sizes					
Width	6.5 ft (2.0 m)	8 ft (2.44m)			
Length	55.5 ft (16.9 m)	90 ft (27.4 m)			
Weight ± 10%	34 lbs (15.42 kg)	70 lbs (31.8 kg)			
Area	40 sq yd (33.4 sm)	80 sq. yd. (66.8 sm)			

Index Property	Test Method	Typical
Thickness	ASTM D6525	0.62 in. (15.75 mm)
Resiliency	ASTM 6524	95.2%
Density	ASTM D792	0.891 g/cm ³
Mass/Unit Area	ASTM 6566	16.13 oz/sy (548 g/sm)
UV Stability	ASTM D4355/ 1000 HR	100%
Porosity	ECTC Guidelines	99%
Stiffness	ASTM D1388	222.65 oz-in.
Light Penetration	ASTM D6567	4.1%
Tensile Strength – MD	ASTM D6818	709 lbs/ft (10.51 kN/m)
Elongation - MD	ASTM D6818	23.9%
Tensile Strength – TD	ASTM D6818	712 lbs/ft (10.56 kN/m)
Elongation - TD	ASTM D6818	36.9%
Biomass Improvement	ASTM D7322	441%

Design Permissible Shear Stress						
	Short Duration	Long Duration				
Phase 1: Unvegetated	3.0 psf (144 Pa)	2.5 psf (120 Pa)				
Phase 2: Partially Veg.	8.0 psf (383 Pa)	8.0 psf (383 Pa)				
Phase 3: Fully Veg.	10.0 psf (480 Pa) 8.0 psf (383 Pa)					
Unvegetated Velocity	9.5 fps (2.9 m/s)					
Vegetated Velocity	15 fps (4.6 m/s)					

Slope Design Data: C Factors						
	Slope Gradients (S)					
Slope Length (L)	≤ 3:1	3:1 - 2.1	≥ 2:1			
≤ 20 ft (6 m)	0.0010	0.0209	0.0507			
20-50 ft	0.0081	0.0266	0.0574			
≥ 50 ft (15.2 m)	0.0455	0.0555	0.081			

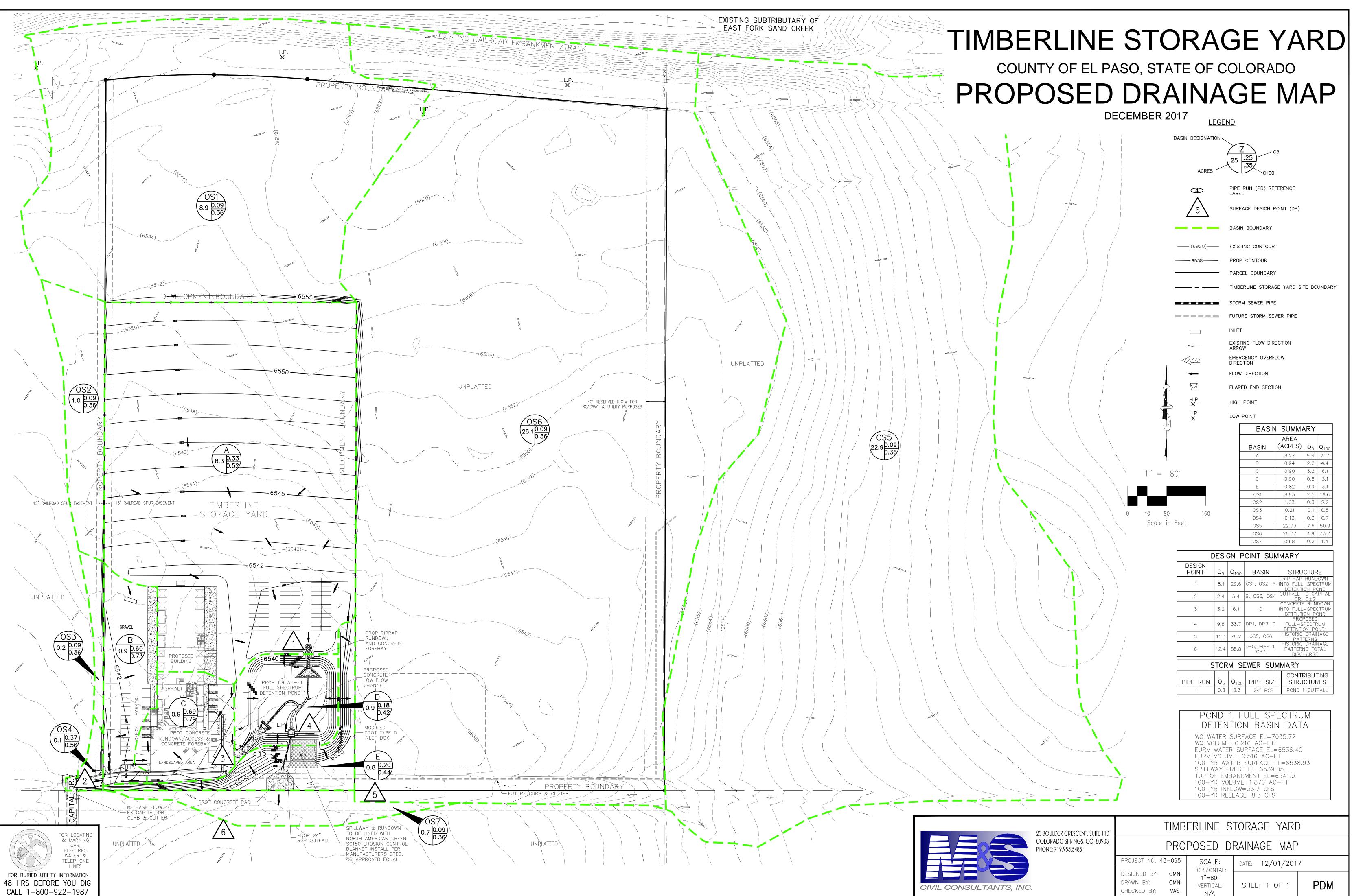
Roughness Coefficients – Unveg.				
Flow Depth	Manning's n			
≤ 0.50 ft (0.15 m)	0.040			
0.50 – 2.0 ft	0.040-0.012			
≥ 2.0 ft (0.60 m)	0.011			



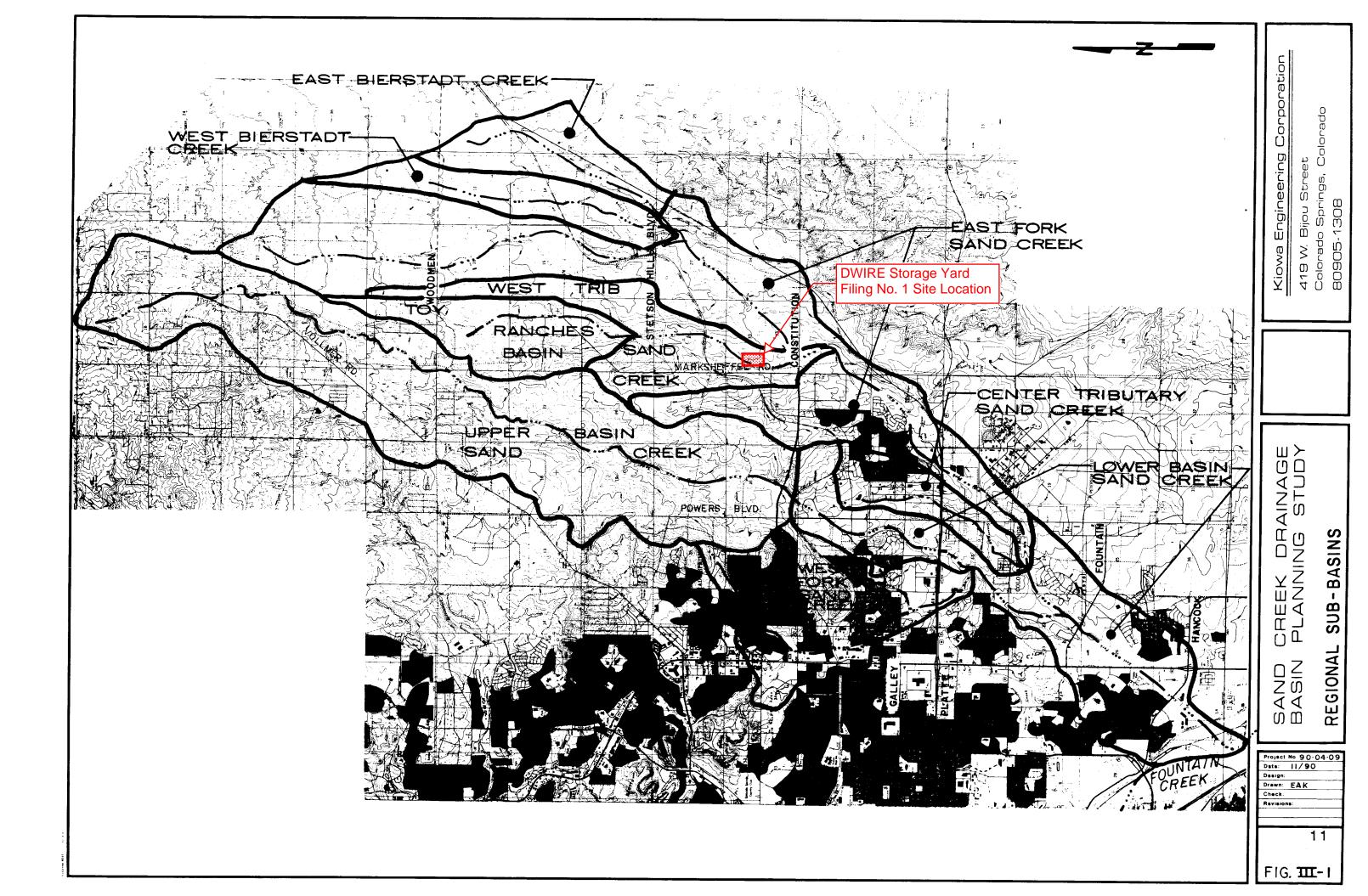
North American Green 5401 St. Wendel-Cynthiana Road Poseyville, Indiana 47633

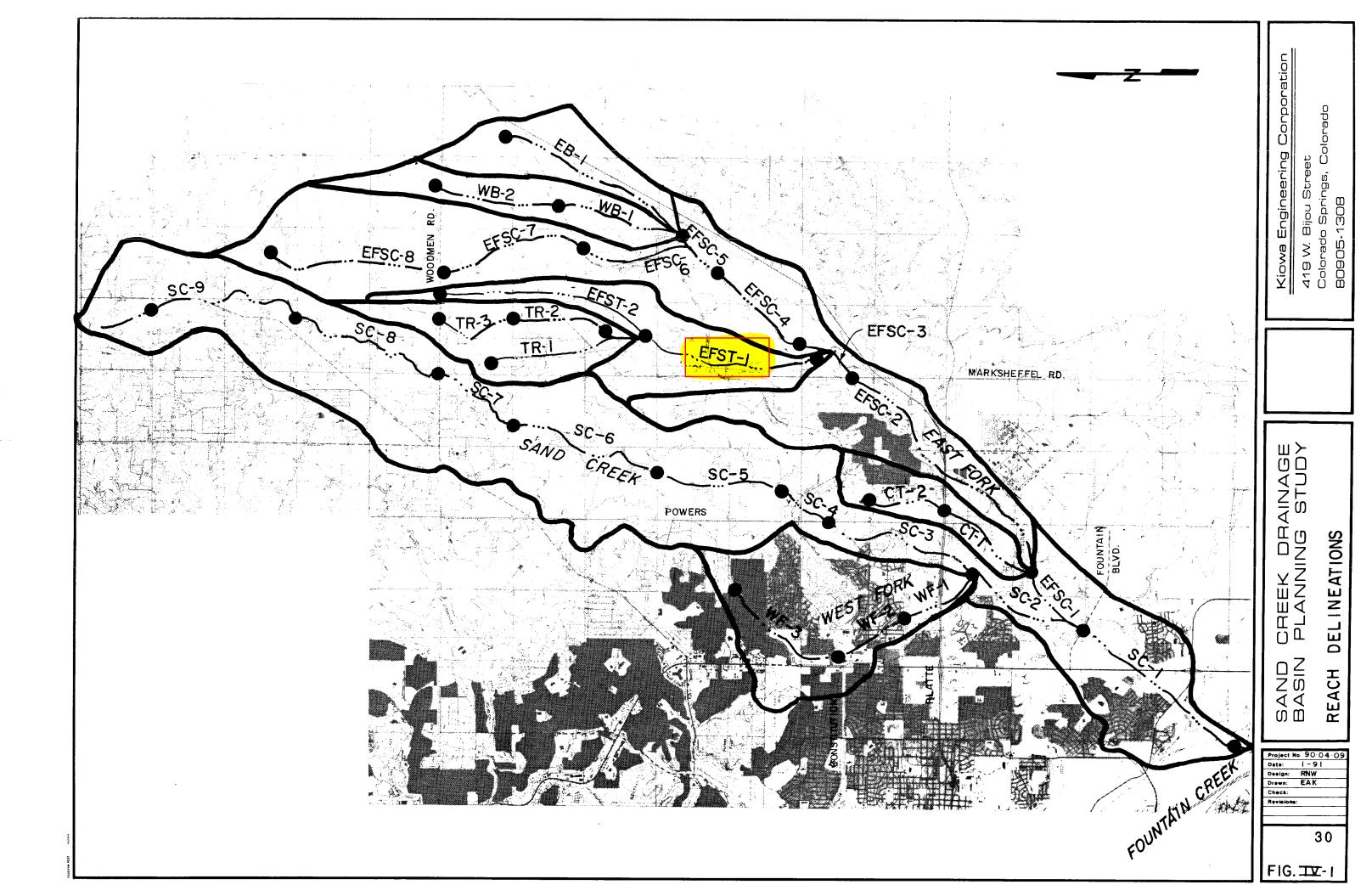
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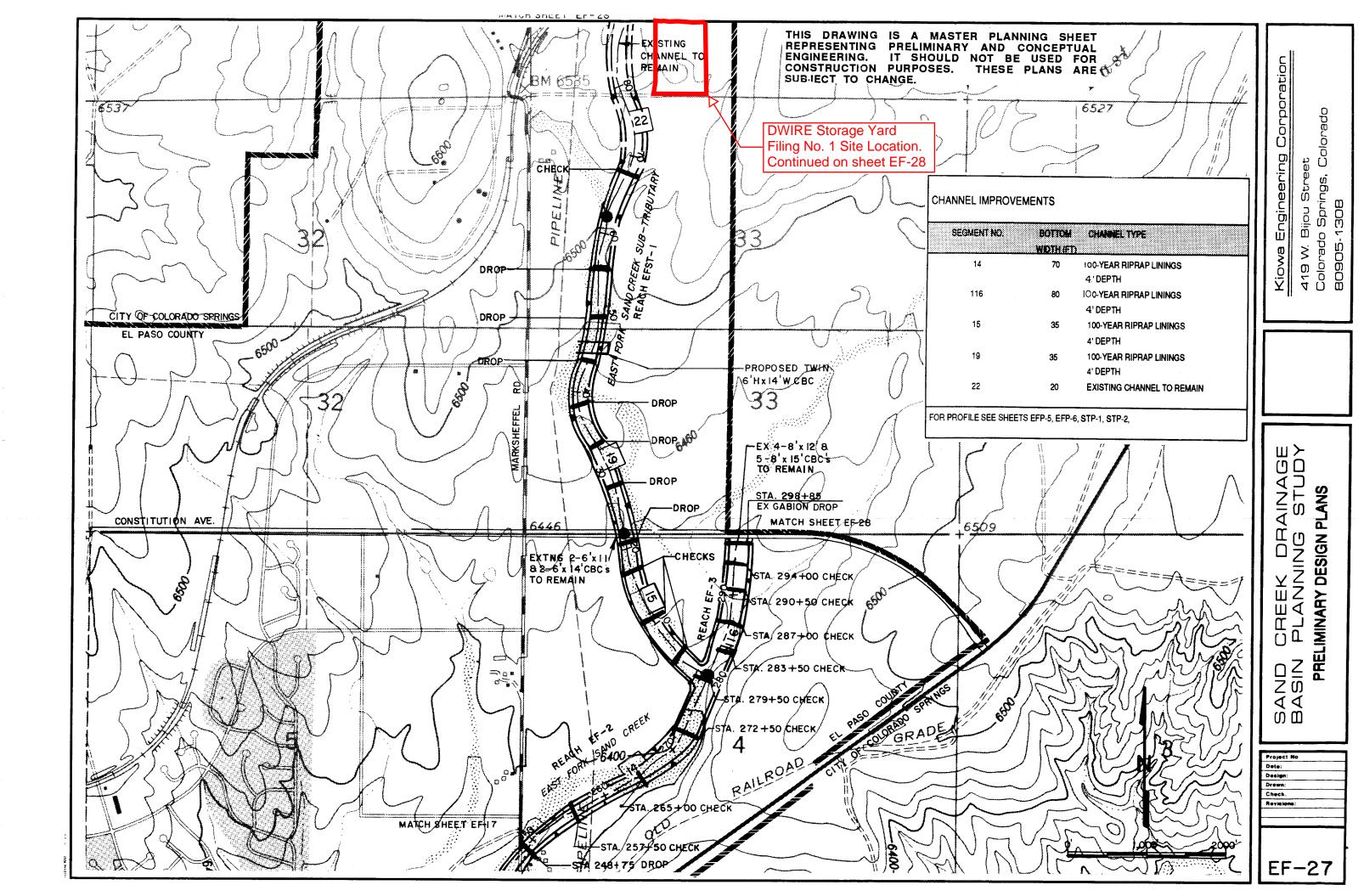
REFERENCED REPORTS

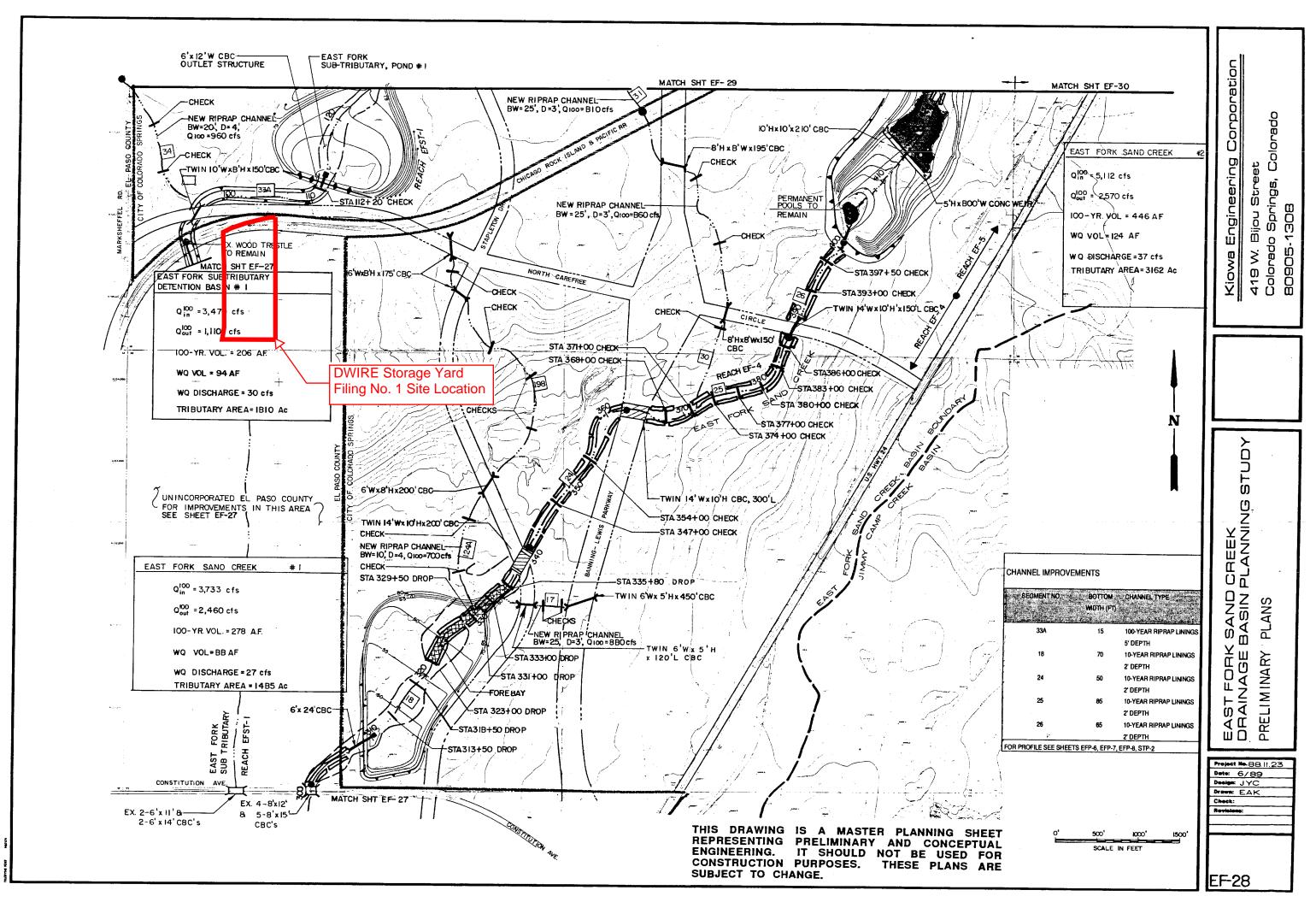


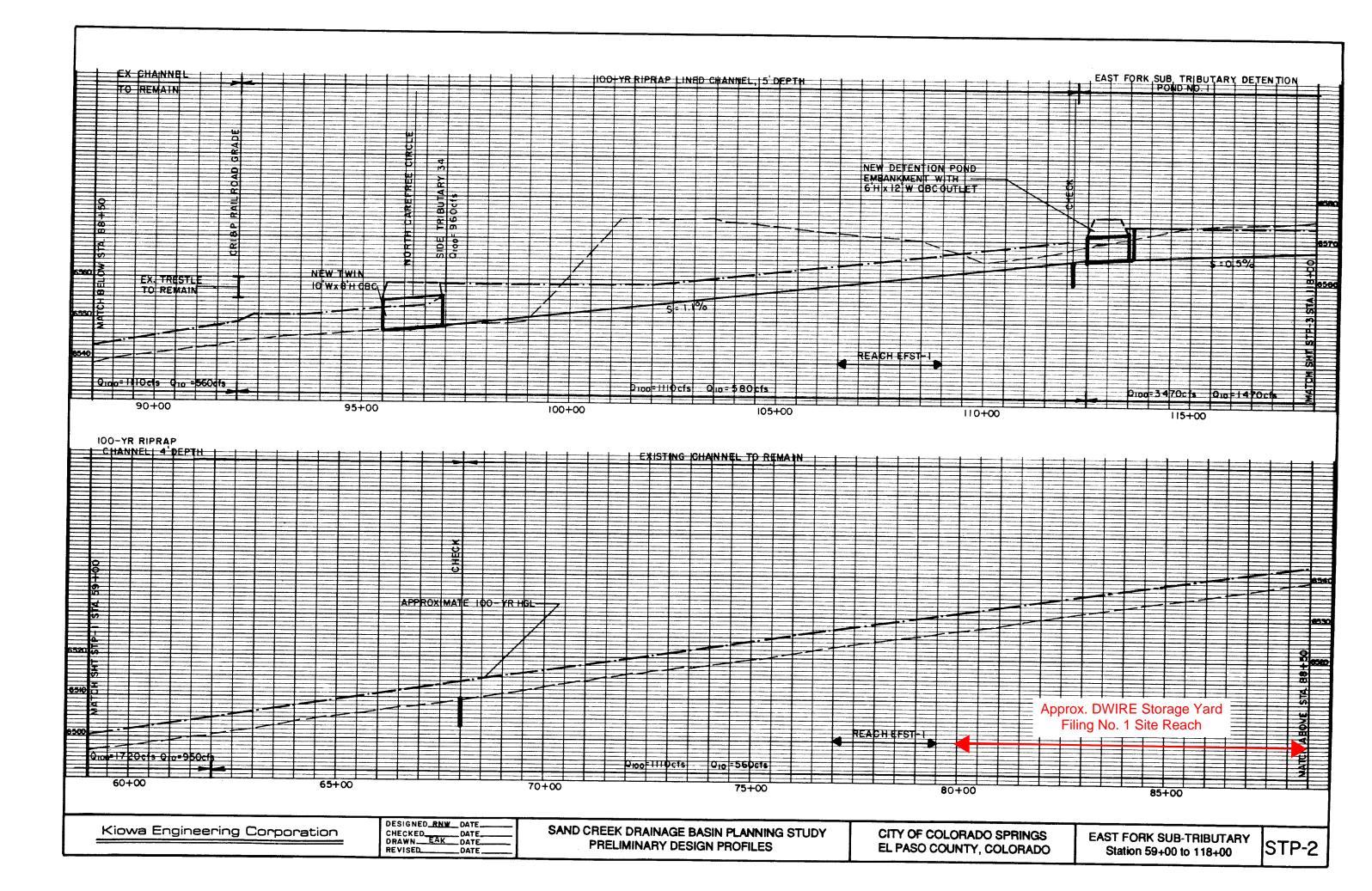
0903	PROPOSED DRAINAGE MAP					
	PROJECT NO. 4	3–095	SCALE: HORIZONTAL:	DATE: 12/01/20	17	
	DESIGNED BY: DRAWN BY: CHECKED BY:	CMN CMN VAS	1"=80' VERTICAL: N/A	SHEET 1 OF 1	PDM	







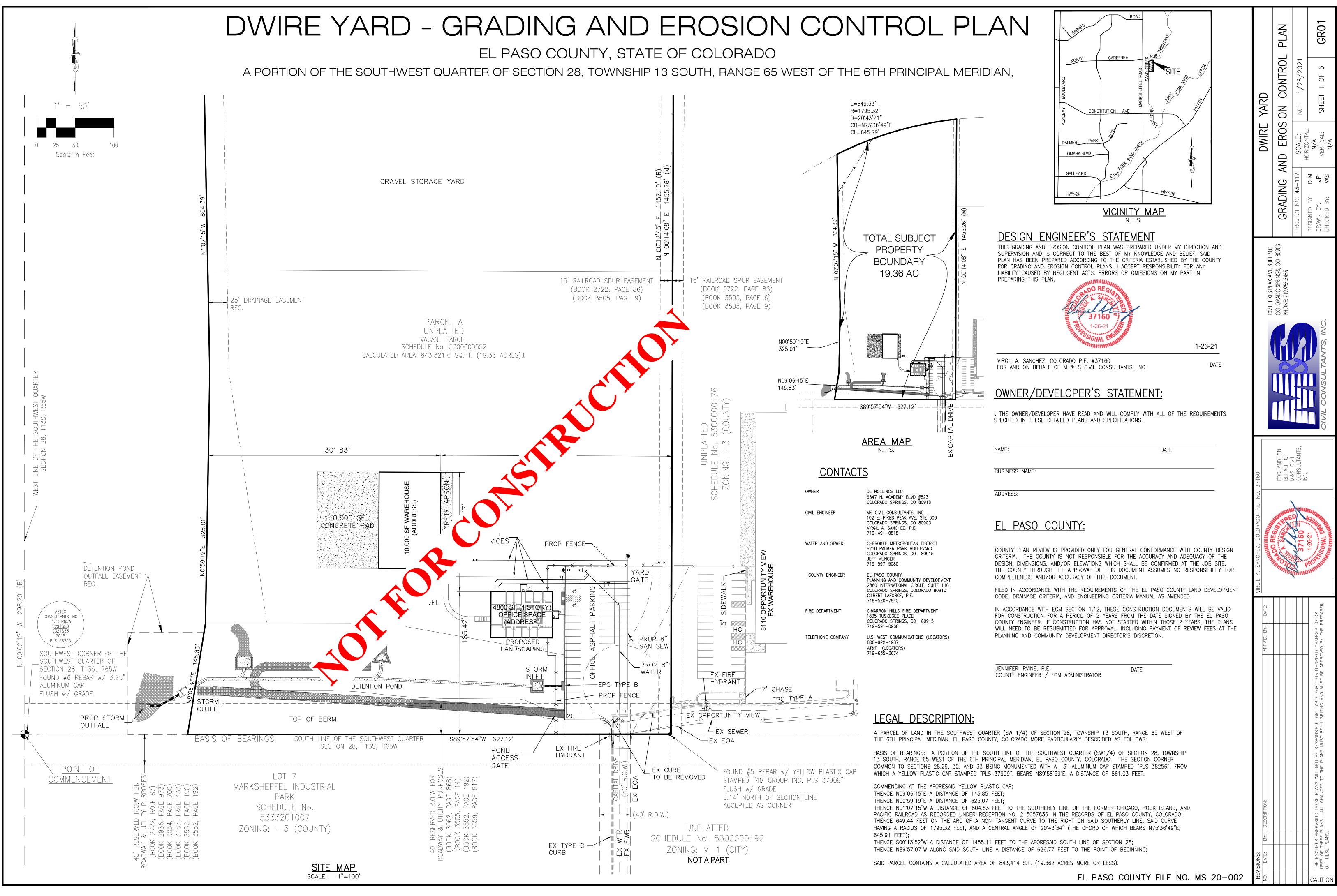




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GRADING AND EROSION CONTROL PLAN



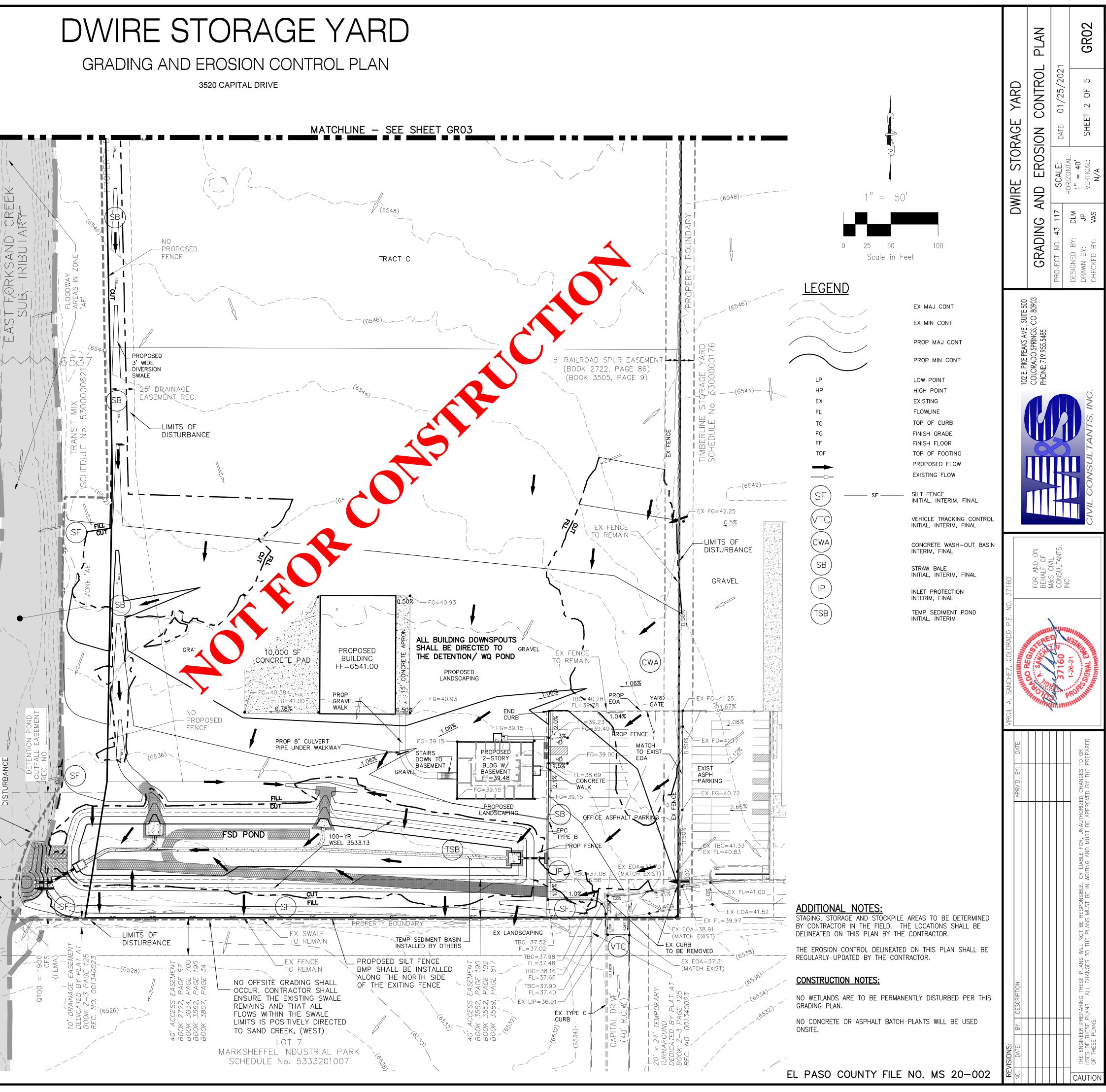
GRADING AND EROSION CONTROL NOTES:

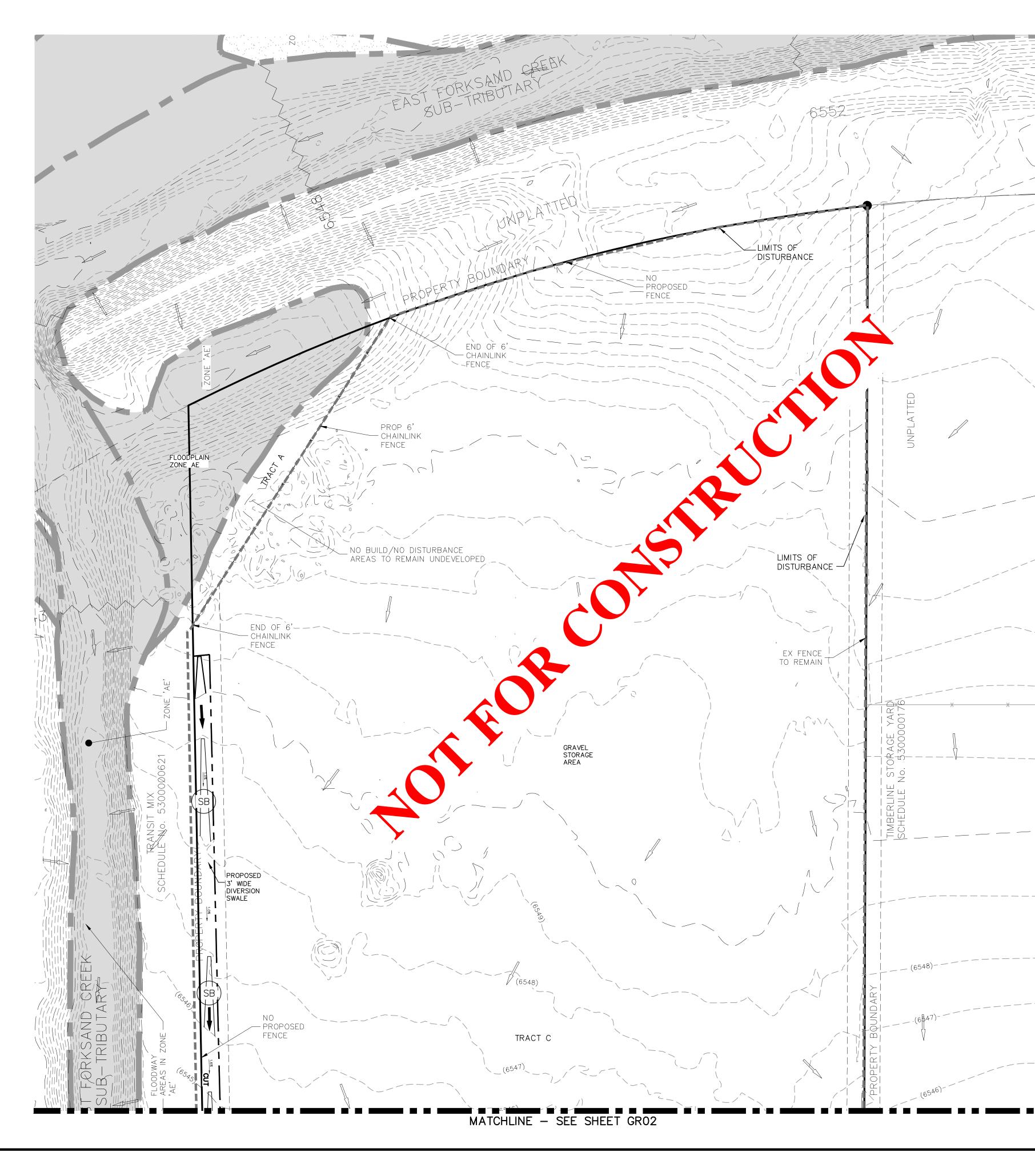
- STORMWATER DISCHARGES FROM CONSTRUCTION SITES SHALL NOT CAUSE OR THREATEN TO CAUSE POLLUTION. CONTAMINATION. OR DEGRADATION OF STATE WATERS. ALL WORK AND EARTH DISTURBANCE SHALL BE DONE IN A MANNER THAT MINIMIZES POLLUTION OF ANY ON-SITE OR OFF-SITE WATERS. INCLUDING WETLANDS.
- NOTWITHSTANDING ANYTHING DEPICTED IN THESE PLANS IN WORDS OR GRAPHIC REPRESENTATION. ALL DESIGN AND CONSTRUCTION RELATED TO ROADS. STORM DRAINAGE AND EROSION CONTROL SHALL CONFORM TO THE STANDARDS AND REQUIREMENTS OF THE MOST RECENT VERSION OF THE RELEVANT ADOPTED EL PASO COUNTY STANDARDS, INCLUDING THE LAND DEVELOPMENT CODE, THE ENGINEERING CRITERIA MANUAL, THE DRAINAGE CRITERIA MANUAL, AND THE DRAINAGE CRITERIA MANUAL VOLUME 2. ANY DEVIATIONS FROM REGULATIONS AND STANDARDS MUST BE REQUESTED, AND APPROVED, IN WRITING.
- A SEPARATE STORMWATER MANAGEMENT PLAN (SMWP) FOR THIS PROJECT SHALL BE COMPLETED AND AN EROSION AND STORMWATER QUALITY CONTROL PERMIT (ESQCP) ISSUED PRIOR TO COMMENCING CONSTRUCTION. MANAGEMENT OF THE SWMP DURING CONSTRUCTION IS THE RESPONSIBILITY OF THE DESIGNATED QUALIFIED STORMWATER MANAGER OR CERTIFIED EROSION CONTROL INSPECTOR. THE SWMP SHALL BE LOCATED ON SITE AT ALL TIMES DURING CONSTRUCTION AND SHALL BE KEPT UP TO DATE WITH WORK PROGRESS AND CHANGES IN THE FIELD.
- ONCE THE ESQCP IS APPROVED AND A "NOTICE TO PROCEED" HAS BEEN ISSUED, THE CONTRACTOR MAY INSTALL THE INITIAL STAGE EROSION AND SEDIMENT CONTROL MEASURES AS INDICATED ON THE APPROVED GEC. A PRECONSTRUCTION MEETING BETWEEN THE CONTRACTOR, ENGINEER, AND EL PASO COUNTY WILL BE HELD PRIOR TO ANY CONSTRUCTION. IT IS THE RESPONSIBILITY OF THE APPLICANT TO COORDINATE THE MEETING TIME AND PLACE WITH COUNTY STAFF
- CONTROL MEASURES MUST BE INSTALLED PRIOR TO COMMENCEMENT OF ACTIVITIES THAT COULD CONTRIBUTE POLLUTANTS TO STORMWATER. CONTROL MEASURES FOR ALL SLOPES, CHANNELS, DITCHES, AND DISTURBED LAND AREAS SHALL BE INSTALLED IMMEDIATELY UPON COMPLETION OF THE DISTURBANCE
- ALL TEMPORARY SEDIMENT AND EROSION CONTROL MEASURES SHALL BE MAINTAINED AND REMAIN IN EFFECTIVE OPERATING CONDITION UNTIL PERMANENT SOIL EROSION CONTROL MEASURES ARE IMPLEMENTED AND FINAL STABILIZATION IS ESTABLISHED. ALL PERSONS ENGAGED IN LAND DISTURBANCE ACTIVITIES SHALL ASSESS THE ADEQUACY OF CONTROL MEASURES AT THE SITE AND IDENTIFY IF CHANGES TO THOSE CONTROL MEASURES ARE NEEDED TO ENSURE THE CONTINUED EFFECTIVE PERFORMANCE OF THE CONTROL MEASURES. ALL CHANGES TO TEMPORARY SEDIMENT AND EROSION CONTROL MEASURES MUST BE INCORPORATED INTO THE STORMWATER MANAGEMENT PLAN.
- TEMPORARY STABILIZATION SHALL BE IMPLEMENTED ON DISTURBED AREAS AND STOCKPILES WHERE GROUND DISTURBING CONSTRUCTION ACTIVITY HAS PERMANENTLY CEASED OR TEMPORARILY CEASED FOR LONGER THAN 14 DAYS.
- FINAL STABILIZATION MUST BE IMPLEMENTED AT ALL APPLICABLE CONSTRUCTION SITES. FINAL STABILIZATION IS ACHIEVED WHEN ALL GROUND DISTURBING ACTIVITIES ARE COMPLETE AND ALL DISTURBED AREAS EITHER HAVE A UNIFORM VEGETATIVE COVER WITH INDIVIDUAL PLANT DENSITY OF 70 PERCENT OF PRE-DISTURBANCE LEVELS ESTABLISHED OR EQUIVALENT PERMANENT ALTERNATIVE STABILIZATION METHOD IS IMPLEMENTED. ALL TEMPORARY SEDIMENT AND EROSION CONTROL MEASURES SHALL BE REMOVED UPON FINAL STABILIZATION AND BEFORE PERMIT CLOSURE.
- ALL PERMANENT STORMWATER MANAGEMENT FACILITIES SHALL BE INSTALLED AS DESIGNED IN THE APPROVED PLANS. ANY PROPOSED CHANGES THAT EFFECT THE DESIGN OR FUNCTION OF PERMANENT STORMWATER MANAGEMENT STRUCTURES MUST BE APPROVED BY THE ECM ADMINISTRATOR PRIOR TO IMPLEMENTATION.
- 10. EARTH DISTURBANCES SHALL BE CONDUCTED IN SUCH A MANNER SO AS TO EFFECTIVELY MINIMIZE ACCELERATED SOIL EROSION AND RESULTING SEDIMENTATION. ALL DISTURBANCES SHALL BE DESIGNED, CONSTRUCTED, AND COMPLETED SO THAT THE EXPOSED AREA OF ANY DISTURBED LAND SHALL BE LIMITED TO THE SHORTEST PRACTICAL PERIOD OF TIME. PRE-EXISTING VEGETATION SHALL BE PROTECTED AND MAINTAINED WITHIN 50 HORIZONTAL FEET OF A WATERS OF THE STATE UNLESS SHOWN TO BE INFEASIBLE AND SPECIFICALLY REQUESTED AND APPROVED
- COMPACTION OF SOIL MUST BE PREVENTED IN AREAS DESIGNATED FOR INFILTRATION CONTROL MEASURES OR WHERE FINAL STABILIZATION WILL BE ACHIEVED BY VEGETATIVE COVER. AREAS DESIGNATED FOR INFILTRATION CONTROL MEASURES SHALL ALSO BE PROTECTED FROM SEDIMENTATION DURING CONSTRUCTION UNTIL FINAL STABILIZATION IS ACHIEVED. IF COMPACTION PREVENTION IS NOT FEASIBLE DUE TO SITE CONSTRAINTS, ALL AREAS DESIGNATED FOR INFILTRATION AND VEGETATION CONTROL MEASURES MUST BE LOOSENED PRIOR TO INSTALLATION OF THE CONTROL MEASURE(S)
- ANY TEMPORARY OR PERMANENT FACILITY DESIGNED AND CONSTRUCTED FOR THE CONVEYANCE OF STORMWATER AROUND, 12. THROUGH, OR FROM THE EARTH DISTURBANCE AREA SHALL BE A STABILIZED CONVEYANCE DESIGNED TO MINIMIZE EROSION AND THE DISCHARGE OF SEDIMENT OFF SITE.
- CONCRETE WASH WATER SHALL BE CONTAINED AND DISPOSED OF IN ACCORDANCE WITH THE SWMP. NO WASH WATER SHALL BE 13. DISCHARGED TO OR ALLOWED TO ENTER STATE WATERS, INCLUDING ANY SURFACE OR SUBSURFACE STORM DRAINAGE SYSTEM OR FACILITIES. CONCRETE WASHOUTS SHALL NOT BE LOCATED IN AN AREA WHERE SHALLOW GROUNDWATER MAY BE PRESENT, OR WITHIN 50 FEET OF A SURFACE WATER BODY, CREEK OR STREAM.
- DURING DEWATERING OPERATIONS OF UNCONTAMINATED GROUND WATER MAY BE DISCHARGED ON SITE, BUT SHALL NOT LEAVE 14. THE SITE IN THE FORM OF SURFACE RUNOFF UNLESS AN APPROVED STATE DEWATERING PERMIT IS IN PLACE.
- 15. EROSION CONTROL BLANKETING OR OTHER PROTECTIVE COVERING SHALL BE USED ON SLOPES STEEPER THAN 3:1.
- CONTRACTOR SHALL BE RESPONSIBLE FOR THE REMOVAL OF ALL WASTES FROM THE CONSTRUCTION SITE FOR DISPOSAL IN 16. ACCORDANCE WITH LOCAL AND STATE REGULATORY REQUIREMENTS. NO CONSTRUCTION DEBRIS, TREE SLASH, BUILDING MATERIAL WASTES OR UNUSED BUILDING MATERIALS SHALL BE BURIED, DUMPED, OR DISCHARGED AT THE SITE.
- WASTE MATERIALS SHALL NOT BE TEMPORARILY PLACED OR STORED IN THE STREET, ALLEY, OR OTHER PUBLIC WAY, UNLESS IN 17. ACCORDANCE WITH AN APPROVED TRAFFIC CONTROL PLAN. CONTROL MEASURES MAY BE REQUIRED BY EL PASO COUNTY ENGINEERING IF DEEMED NECESSARY, BASED ON SPECIFIC CONDITIONS AND CIRCUMSTANCES.
- TRACKING OF SOILS AND CONSTRUCTION DEBRIS OFF-SITE SHALL BE MINIMIZED. MATERIALS TRACKED OFF-SITE SHALL BE 18 CLEANED UP AND PROPERLY DISPOSED OF IMMEDIATELY.
- THE OWNER/DEVELOPER SHALL BE RESPONSIBLE FOR THE REMOVAL OF ALL CONSTRUCTION DEBRIS. DIRT. TRASH. ROCK. 19. SEDIMENT, SOIL, AND SAND THAT MAY ACCUMULATE IN ROADS, STORM DRAINS AND OTHER DRAINAGE CONVEYANCE SYSTEMS AND STORMWATER APPURTENANCES AS A RESULT OF SITE DEVELOPMENT.
- 20. THE QUANTITY OF MATERIALS STORED ON THE PROJECT SITE SHALL BE LIMITED, AS MUCH AS PRACTICAL, TO THAT QUANTITY REQUIRED TO PERFORM THE WORK IN AN ORDERLY SEQUENCE. ALL MATERIALS STORED ON-SITE SHALL BE STORED IN A NEAT, ORDERLY MANNER, IN THEIR ORIGINAL CONTAINERS, WITH ORIGINAL MANUFACTURER'S LABELS.
- 21. NO CHEMICAL(S) HAVING THE POTENTIAL TO BE RELEASED IN STORMWATER ARE TO BE STORED OR USED ONSITE UNLESS PERMISSION FOR THE USE OF SUCH CHEMICAL(S) IS GRANTED IN WRITING BY THE ECM ADMINISTRATOR. IN GRANTING APPROVAL FOR THE USE OF SUCH CHEMICAL(S), SPECIAL CONDITIONS AND MONITORING MAY BE REQUIRED.
- 22. BULK STORAGE OF ALLOWED PETROLEUM PRODUCTS OR OTHER ALLOWED LIQUID CHEMICALS IN EXCESS OF 55 GALLONS SHALL REQUIRE ADEQUATE SECONDARY CONTAINMENT PROTECTION TO CONTAIN ALL SPILLS ONSITE AND TO PREVENT ANY SPILLED MATERIALS FROM ENTERING STATE WATERS, ANY SURFACE OR SUBSURFACE STORM DRAINAGE SYSTEM OR OTHER FACILITIES.
- NO PERSON SHALL CAUSE THE IMPEDIMENT OF STORMWATER FLOW IN THE CURB AND GUTTER OR DITCH EXCEPT WITH APPROVED 23. SEDIMENT CONTROL MEASURES.
- 24. OWNER/DEVELOPER AND THEIR AGENTS SHALL COMPLY WITH THE "COLORADO WATER QUALITY CONTROL ACT" (TITLE 25, ARTICLE 8, CRS), AND THE "CLEAN WATER ACT" (33 USC 1344), IN ADDITION TO THE REQUIREMENTS OF THE LAND DEVELOPMENT CODE, DCM VOLUME II AND THE ECM APPENDIX I. ALL APPROPRIATE PERMITS MUST BE OBTAINED BY THE CONTRACTOR PRIOR TO CONSTRUCTION (1041, NPDES, FLOODPLAIN, 404, FUGITIVE DUST, ETC.). IN THE EVENT OF CONFLICTS BETWEEN THESE REQUIREMENTS AND OTHER LAWS, RULES, OR REGULATIONS OF OTHER FEDERAL, STATE, LOCAL, OR COUNTY AGENCIES, THE MOST RESTRICTIVE LAWS, RULES, OR REGULATIONS SHALL APPLY.
- 25. ALL CONSTRUCTION TRAFFIC MUST ENTER/EXIT THE SITE ONLY AT APPROVED CONSTRUCTION ACCESS POINTS.
- 26. PRIOR TO CONSTRUCTION THE PERMITTEE SHALL VERIFY THE LOCATION OF EXISTING UTILITIES.
- A WATER SOURCE SHALL BE AVAILABLE ON SITE DURING EARTHWORK OPERATIONS AND SHALL BE UTILIZED AS REQUIRED TO MINIMIZE DUST FROM EARTHWORK EQUIPMENT AND WIND.
- THE SOILS REPORT FOR THIS SITE HAS BEEN PREPARED BY RMG ENGINEERS, DATED MAY 3RD, 2019 AND SHALL BE CONSIDERED 28. A PART OF THESE PLANS.
- 29. AT LEAST TEN (10) DAYS PRIOR TO THE ANTICIPATED START OF CONSTRUCTION, FOR PROJECTS THAT WILL DISTURB ONE (1) ACRE OR MORE, THE OWNER OR OPERATOR OF CONSTRUCTION ACTIVITY SHALL SUBMIT A PERMIT APPLICATION FOR STORMWATER DISCHARGE TO THE COLORADO DEPARTMENT OF PUBLIC HEALTH AND ENVIRONMENT, WATER QUALITY DIVISION. THE APPLICATION CONTAINS CERTIFICATION OF COMPLETION OF A STORMWATER MANAGEMENT PLAN (SWMP), OF WHICH THIS GRADING AND EROSION CONTROL PLAN MAY BE A PART. FOR INFORMATION OR APPLICATION MATERIALS CONTACT:

COLORADO DEPARTMENT OF PUBLIC HEALTH AND ENVIRONMENT

WATER QUALITY CONTROL DIVISION WQCD - PERMITS 4300 CHERRY CREEK DRIVE SOUTH DENVER, CO 80246-1530

ATTN: PERMITS UNIT

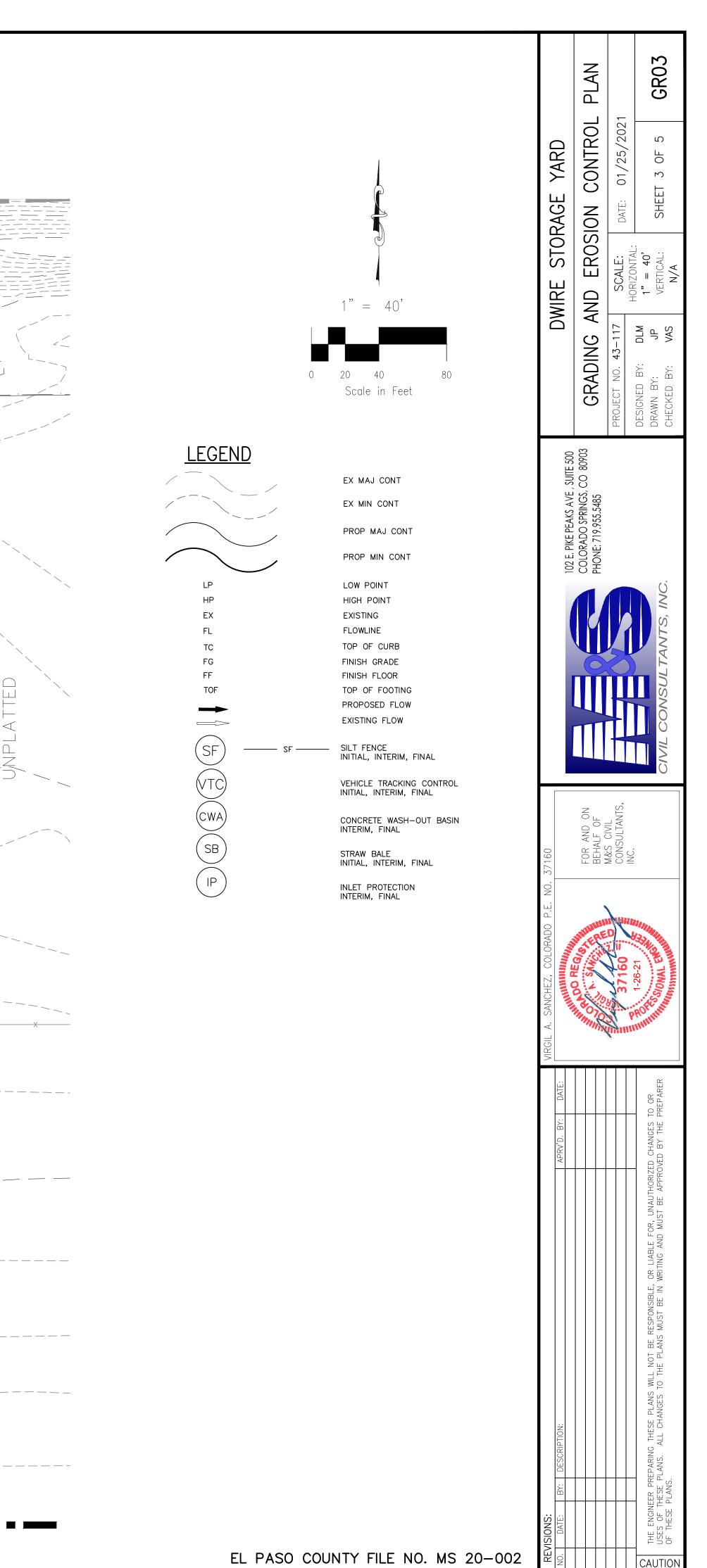


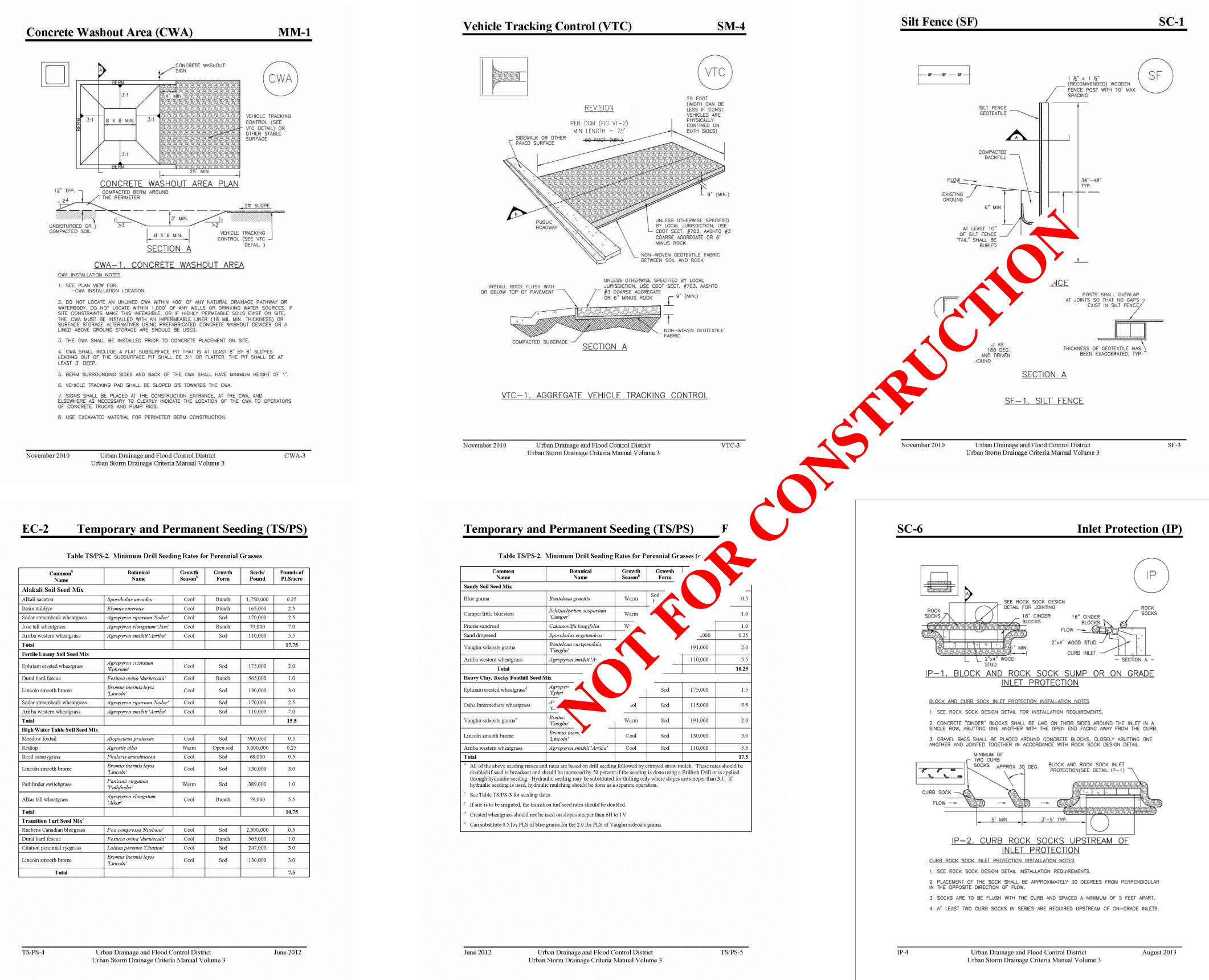


DWIRE STORAGE YARD

GRADING AND EROSION CONTROL PLAN

3520 CAPITAL DRIVE



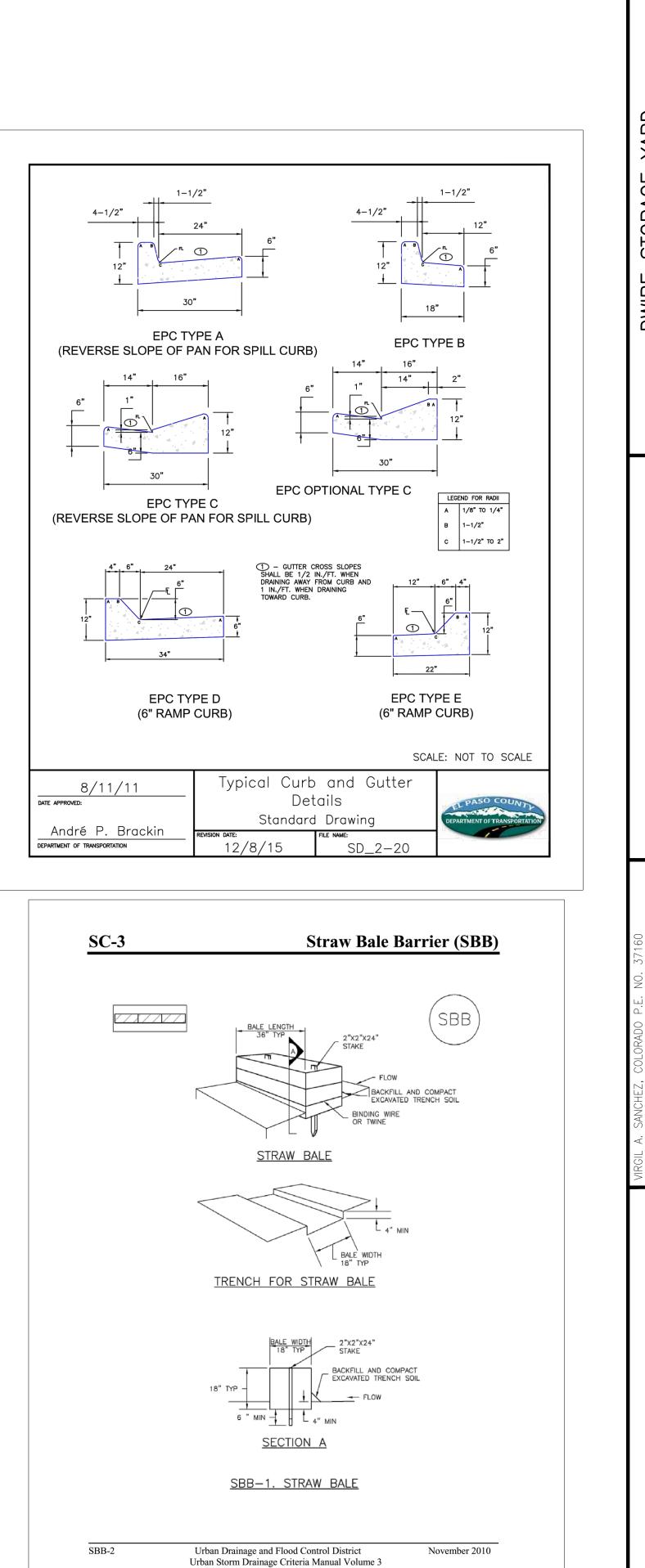


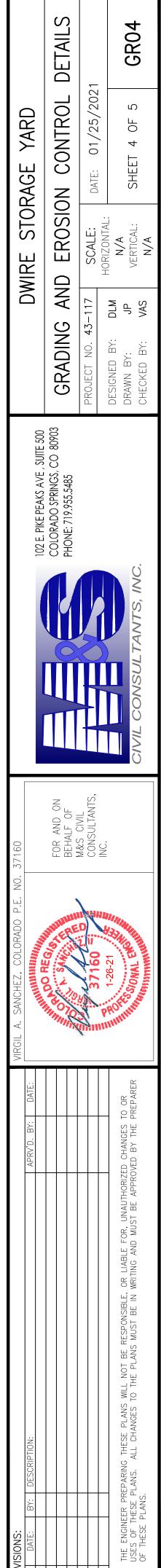
Common ^a Name	Botanical Name	Growth Season ^b	Growth Form	Seeds/ Pound	Pounds of PLS/acre
Alakali Soil Seed Mix					
Alkali sacaton	Sporobolus airoides	Cool	Bunch	1,750,000	0.25
Basin wildrye	Elymus cinereus	Cool	Bunch	165,000	2.5
Sodar streambank wheatgrass	Agropyron riparium 'Sodar'	Cool	Sod	170,000	2.5
Jose tall wheatgrass	Agropyron elongatum 'Jose'	Cool	Bunch	79,000	7.0
Arriba western wheatgrass	Agropyron smithii 'Arriba'	Cool	Sod	110,000	5.5
Total					17.75
Fertile Loamy Soil Seed Mix					
Ephriam crested wheatgrass	Agropyron cristatum 'Ephriam'	Cool	Sod	175,000	2.0
Dural hard fescue	Festuca ovina 'duriuscula'	Cool	Bunch	565,000	1.0
Lincoln smooth brome	Bromus inermis leyss 'Lincoln'	Cool	Sod	130,000	3.0
Sodar streambank wheatgrass	Agropyron riparium 'Sodar'	Cool	Sod	170,000	2.5
Arriba western wheatgrass	Agropyron smithii 'Arriba'	Cool	Sod	110,000	7.0
Total					15.5
High Water Table Soil Seed Miz	τ.				
Meadow foxtail	Alopecurus pratensis	Cool	Sod	900,000	0.5
Redtop	Agrostis alba	Warm	Open sod	5,000,000	0.25
Reed canarygrass	Phalaris arundinacea	Cool	Sod	68,000	0.5
Lincoln smooth brome Bromus inermis leyss Lincoln'		Cool	Sod	130,000	3.0
Pathfinder switchgrass	Panicum virgatum 'Pathfinder'	Warm	Sod	389,000	1.0
Alkar tall wheatgrass	Agropyron elongatum 'Alkar'	Cool	Bunch	79,000	5.5
Total					10.75
Transition Turf Seed Mix ^c					
Ruebens Canadian bluegrass	Poa compressa 'Ruebens'	Cool	Sod	2,500,000	0.5
Dural hard fescue	Festuca ovina 'duriuscula'	Cool	Bunch	565,000	1.0
Citation perennial ryegrass	Lolium perenne 'Citation'	Cool	Sod	247,000	3.0
Lincoln smooth brome	Bromus inermis leyss 'Lincoln'	Cool	Sod	130,000	3.0
Total					7.5

	Table TS/PS-2	2. Min
	Common Name	
Sai	ndy Soil Seed Mix	
Blı	ne grama	Boi
Ca	mper little bluestern	Scł 'Ca
Pra	irie sandreed	Ca
Sat	nd dropseed	Spo
Va	ughn sideoats grama	Boi 'Va
An	iba western wheatgrass	Agr
	Total	
He	avy Clay, Rocky Foothill See	d Mix
Epl	hriam crested wheatgrass ^d	Agr 'Ep
Oa	he Intermediate wheatgrass	Аr 'С.
Va	ughn sideoats grama ^e	Bot 'Va
Lir	coln smooth brome	Bro 'Lit
Arı	iba western wheatgrass	Ag
To	tal	
ہ 1	All of the above seeding mixes doubled if seed is broadcast and through hydraulic seeding. Hy hydraulic seeding is used, hydr	d should draulic s
b	See Table TS/PS-3 for seeding	dates.
c :	If site is to be irrigated, the tran	nsition tu
d (Crested wheatgrass should not	be used
e	Can substitute 0.5 lbs PLS of b	lue oran

DWIRE STORAGE YARD

GRADING AND EROSION CONTROL PLAN





CAUTION

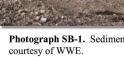
EL PASO COUNTY FILE NO. MS 20-002

Sediment Basin (SB)

Description

A sediment basin is a temporary pond built on a construction site to capture eroded or disturbed soil transported in storm runoff prior to discharge from the site. Sediment basins are designed to capture site runoff and slowly release it to allow time for settling of sediment prior to discharge. Sediment basins are often constructed in locations that will later be modified to serve as post-construction stormwater basins.





Most large construction sites (typically greater than 2 acres) will require one or more sediment basins for effective

controls should also be implemented upstream.

impractical; instead, sediment traps or other combinations of BMPs may be more appropriate. Sediment basins should not be used as stand-alone sediment controls. Erosion and other sediment

When feasible, the sediment basin should be installed in the same location where a permanent postconstruction detention pond will be located.

Design and Installation

- The design procedure for a sediment basin includes these steps: Basin Storage Volume: Provide a storage volume of at least 3,600 cubic feet per acre of drainage area. To the extent practical, undisturbed and/or off-site areas should be diverted around sediment basins to prevent "clean" runoff from mixing with runoff from disturbed areas. For undisturbed areas (both on-site and off-site) that cannot be diverted around the sediment basin, provide a minimum of 500 ft³/acre of storage for undeveloped (but stable) off-site areas in addition to the 3,600 ft³/acre for disturbed areas. For stable, developed areas that cannot be diverted around the sediment basin, storage volume requirements are summarized in Table SB-1.
- Basin Geometry: Design basin with a minimum length-to-width ratio of 2:1 (L:W). If this cannot be achieved because of site space constraints, baffling may be required to extend the effective distance between the inflow point(s) and the outlet to minimize short-circuiting.
- **Dam Embankment**: It is recommended that embankment slopes be 4:1 (H:V) or flatter and no steeper Erosion Control than 3:1 (H:V) in any location.

Urban Drainage and Flood Control District Urban Storm Drainage Criteria Manual Volume 3

SC-7

August 2013

Maintenance and Removal

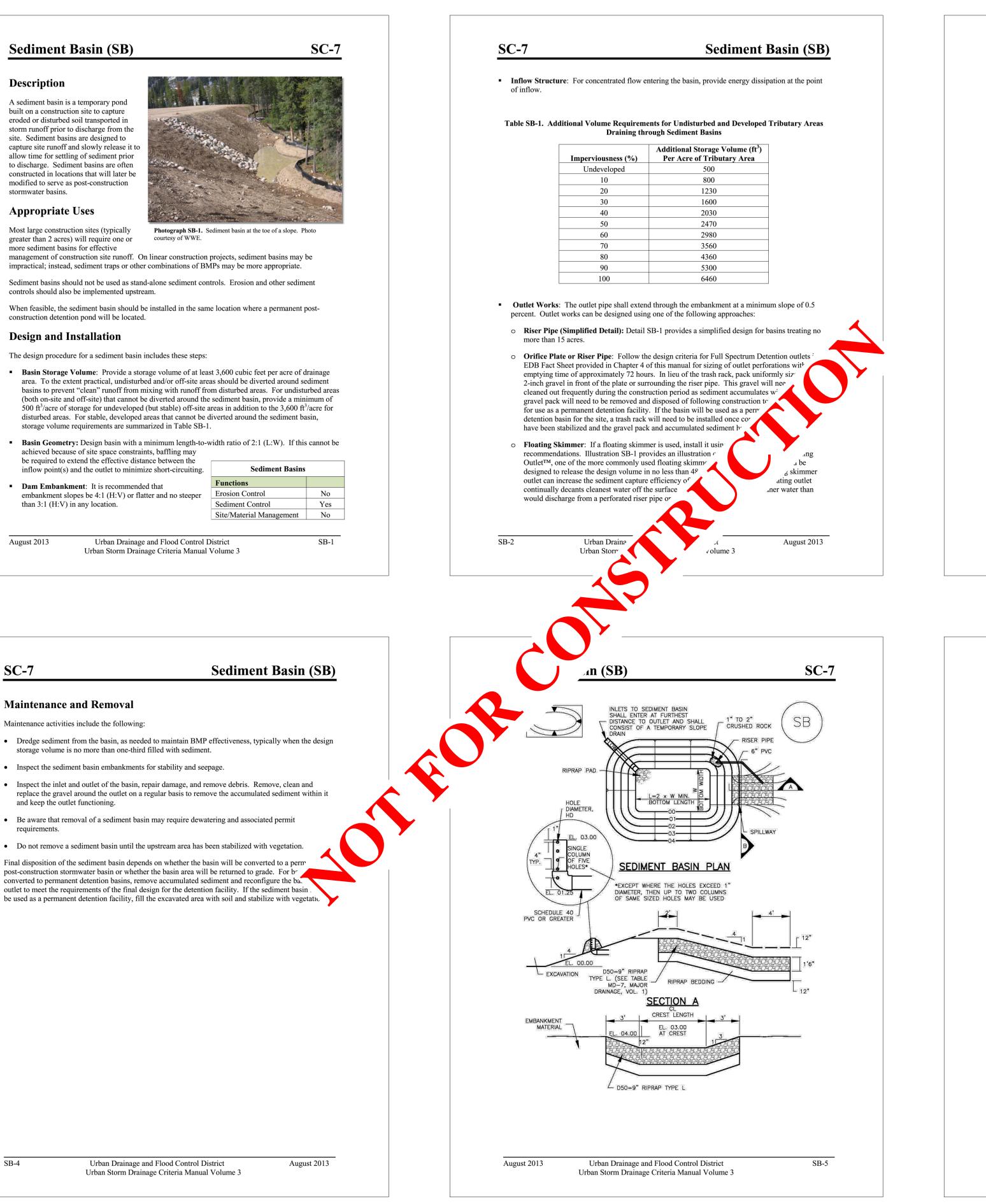
- Maintenance activities include the following: • Dredge sediment from the basin, as needed to maintain BMP effectiveness, typically when the design storage volume is no more than one-third filled with sediment.
- Inspect the sediment basin embankments for stability and seepage.
- Inspect the inlet and outlet of the basin, repair damage, and remove debris. Remove, clean and replace the gravel around the outlet on a regular basis to remove the accumulated sediment within it and keep the outlet functioning.
- Be aware that removal of a sediment basin may require dewatering and associated permit requirements.

• Do not remove a sediment basin until the upstream area has been stabilized with vegetation. Final disposition of the sediment basin depends on whether the basin will be converted to a perm post-construction stormwater basin or whether the basin area will be returned to grade. For br converted to permanent detention basins, remove accumulated sediment and reconfigure the ba outlet to meet the requirements of the final design for the detention facility. If the sediment basin .

SB-4

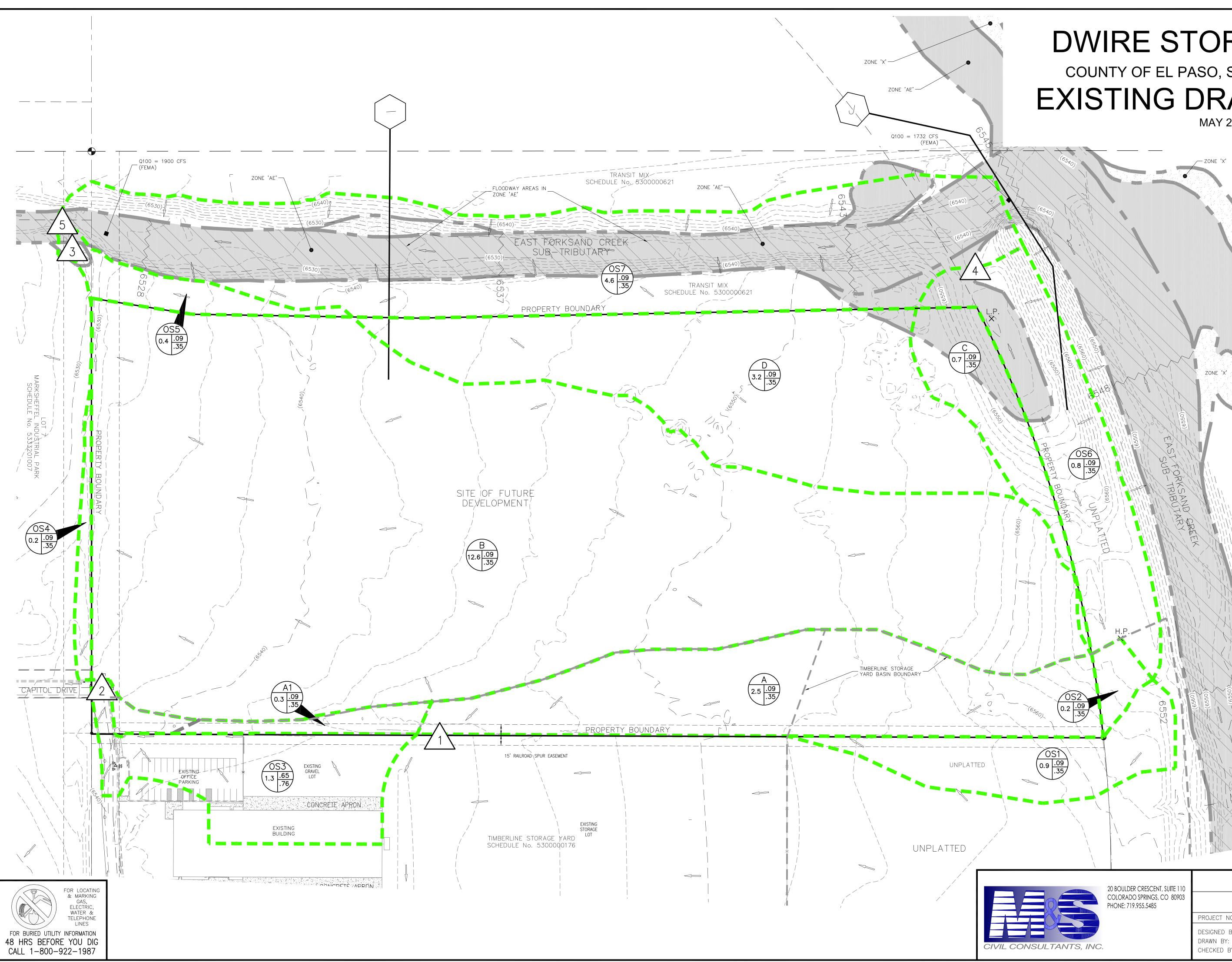
DWIRE STORAGE YARD

GRADING AND EROSION CONTROL PLAN



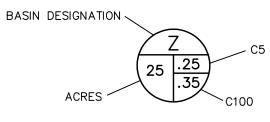
		1	
		DETAILS	GR05
	YARD	CONTROL	01/25/2021 - 5 OF 5
Sediment Basin (SB) SC-7	STORAGE		DATE: (SHEET
		EROSION	SCALE: Horizontal: N/A Vertical: N/A
	DWIRE	AND E	
			. 43–117 .: DLM JP : VAS
Illustration SB-1. Outlet structure for a temporary sediment basin - Faircloth Skimmer Floating Outlet. Illustration courtesy		GRADING	PROJECT NO. DESIGNED BY: DRAWN BY: CHECKED BY:
of J. W. Faircloth & Sons, Inc., FairclothSkimmer.com.	00		DE DR CH
 Outlet Protection and Spillway: Consider all flow paths for runoff leaving the basin, including protection at the typical point of discharge as well as overtopping. Outlet Protection: Outlet protection should be provided where the velocity of flow will exceed 	AVE SUITE 5	VGS, CO 80903 485	
 the maximum permissible velocity of the material of the waterway into which discharge occurs. This may require the use of a riprap apron at the outlet location and/or other measures to keep the waterway from eroding. Emergency Spillway: Provide a stabilized emergency overflow spillway for rainstorms that 	102 F PIKF PFAKS AVF	COLORADO SPRINGS, PHONE: 719.955.5485	
exceed the capacity of the sediment basin volume and its outlet. Protect basin embankments from erosion and overtopping. If the sediment basin will be converted to a permanent detention basin, design and construct the emergency spillway(s) as required for the permanent facility. If the sediment basin will not become a permanent detention basin, it may be possible to substitute a	100 F	COLC	Ú.
heavy polyvinyl membrane or properly bedded rock cover to line the spillway and downstream embankment, depending on the height, slope, and width of the embankments.			VTS, IN
			UL TAN
			CONS
August 2013 Urban Drainage and Flood Control District SB-3			CIVIL
Urban Storm Drainage Criteria Manual Volume 3		0 ON	ANTS,
	7160	Z L d	M&S CIVIL CONSULTANI INC.
SC-7 Sediment Basin (SB)	P.E. NO. 3		
See 7 Seument Busin (SD)	ORADO	STERE STERE	
TABLE SB-1. SIZING INFORMATION FOR STANDARD SEDIMENT BASIN Upstream Drainage Area (rounded to Basin Bottom Width Spillway Crest Hole Diameter		119 A 119	37160 37160 1-26-21
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$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	VII DATE:		ARER
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	D. BY:		NGES TO OR
SEDIMENT BASIN INSTALLATION NOTES	APRV'		UNAUTHORIZED CHANGES
-LOCATION OF SEDIMENT BASIN. -TYPE OF BASIN (STANDARD BASIN OR NONSTANDARD BASIN). -FOR STANDARD BASIN, BOTTOM WIDTH W, CREST LENGTH CL, AND HOLE DIAMETER, HD. -FOR NONSTANDARD BASIN, SEE CONSTRUCTION DRAWINGS FOR DESIGN OF BASIN INCLUDING RISER HEIGHT H, NUMBER OF COLUMNS N, HOLE DIAMETER HD AND PIPE DIAMETER D.			DR, UNAUTH MUST BE A
2. FOR STANDARD BASIN, BOTTOM DIMENSION MAY BE MODIFIED AS LONG AS BOTTOM AREA IS NOT REDUCED. 3. SEDIMENT BASINS SHALL BE INSTALLED PRIOR TO ANY OTHER LAND-DISTURBING ACTIVITY THAT RELIES ON ON BASINS AS AS A STORMWATER CONTROL.			OR LIABLE FOR, UN WRITING AND MUST
 4. EMBANKMENT MATERIAL SHALL CONSIST OF SOIL FREE OF DEBRIS, ORGANIC MATERIAL, AND ROCKS OR CONCRETE GREATER THAN 3 INCHES AND SHALL HAVE A MINIMUM OF 15 PERCENT BY WEIGHT PASSING THE NO. 200 SIEVE. 5. EMBANKMENT MATERIAL SHALL BE COMPACTED TO AT LEAST 95 PERCENT OF MAXIMUM DENSITY IN ACCORDANCE WITH ASTM D698. 			
6. PIPE SCH 40 OR GREATER SHALL BE USED. 7. THE DETAILS SHOWN ON THESE SHEETS PERTAIN TO STANDARD SEDIMENT BASIN(S) FOR DRAINAGE AREAS LESS THAN 15 ACRES. SEE CONSTRUCTION DRAWINGS FOR EMBANKMENT, STORAGE VOLUME, SPILLWAY, OUTLET, AND OUTLET PROTECTION DETAILS FOR			WILL NOT BE RESPONSIBLE, TO THE PLANS MUST BE IN
ANY SEDIMENT BASIN(S) THAT HAVE BEEN INDIVIDUALLY DESIGNED FOR DRAINAGE AREAS LARGER THAN 15 ACRES.			LANS WILL UGES TO TH
	DESCRIPTION:		NG THESE PLANS ALL CHANGES T
B-6 Urban Drainage and Flood Control District August 2013 Urban Storm Drainage Criteria Manual Volume 3	BY: DESC		THE ENGINEER PREPARING USES OF THESE PLANS. /
	REVISIONS: IO. DATE:		THE ENGINEL JSES OF TH OF THESE P
EL PASO COUNTY FILE NO. MS 20-002	REV NO.		CAUTION

EXISTING AND PROPOSED DRAINAGE MAPS



DWIRE STORAGE YARD COUNTY OF EL PASO, STATE OF COLORADO EXISTING DRAINAGE MAP MAY 2020

<u>LEGEND</u>





- -- (6920) -- -

6920

BASIN BOUNDARY

TIMBERLINE STORAGE YARD BASIN BOUNDARY

EXISTING INDEX CONTOUR (10') EXISTING NOMINAL CONTOUR (2')

FEMA BASE FLOOD EL. (NGVD29)

STORAGE YARD SITE BOUNDARY

EXISTING FLOW DIRECTION ARROW

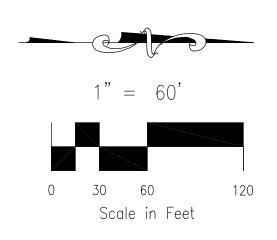
HIGH POINT

LOW POINT

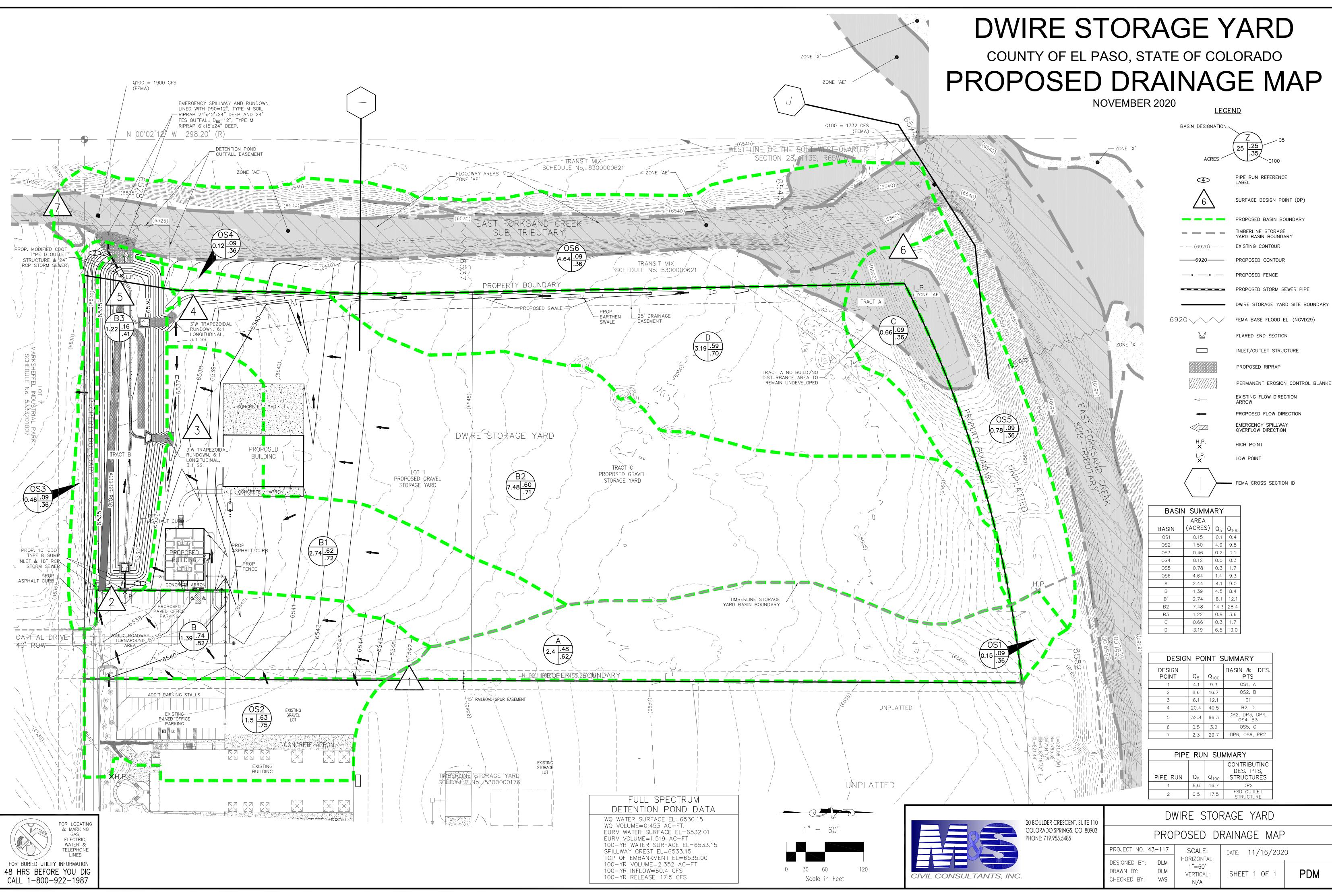
FEMA CROSS SECTION ID

BASIN SUMMARY					
BASIN	AREA (ACRES)	Q ₅	Q ₁₀₀		
OS1	0.90	0.2	1.6		
0S2	0.15	0.0	0.3		
OS3	1.26	3.4	6.8		
OS4	0.16	0.0	0.3		
0S5	0.36	0.1	0.6		
OS6	0.78	0.2	1.3		
0S7	4.55	0.9	6.0		
A	2.47	0.6	3.6		
A1	0.30	0.1	0.7		
В	12.64	2.5	16.6		
С	0.66	0.2	1.5		
D	3.19	0.7	4.3		

DESIGN POINT SUMMARY						
DESIGN POINT	Q_5	Q 100	BASIN & DES. PTS			
1	0.8	5.1	0S1,0S2,A			
2	3.6	7.5	A1,0S3			
3	2.6	17.2	0S4,0S5,B			
4	0.4	2.4	0S6,C			
5	4.5	29.3	DP3,DP4,OS7,D			



CONSULTANTS, INC.	20 BOULDER CRESCENT, SUITE 110 COLORADO SPRINGS, CO 80903 PHONE: 719.955.5485	DWIRE STORAGE YARD			
		EXISTING DRAINAGE MAP			
		PROJECT NO. 43-117	SCALE: HORIZONTAL: 1"=60' VERTICAL: N/A	DATE: 05/21/202	0
		DESIGNED BY: DLM DRAWN BY: DLM CHECKED BY: VAS		SHEET 1 OF 1	EDM



CONSUL	TANTS,	INC.

PROJECT NO. 43-117		SCALE:	DATE: 11/16/2020		
DESIGNED BY:	DLM	HORIZONTAL: 1"=60'			
DRAWN BY: CHECKED BY:	DLM VAS	VERTICAL: N/A	SHEE	T 1 OF 1	