

MONUMENT STEEL STRUCTURES FINAL DRAINAGE STUDY

JUNE 2019

For: Steel Structures America Inc. 3635 E. Covington Ave. Post Falls, ID 83854

By: Terra Forma Solutions 9994 Quintero Street Commerce City, CO 80022 Todd Johnson, P.E. 303.257.7653

PCD File No. PPR1919

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ENGINEER'S CERTIFICATION:

The attached drainage plan and report were prepared unbest of my knowledge and belief. Said drainage report by the County for drainage reports and said report is in cobasin. I accept responsibility for any liability caused by preparing this report.	t has been prepared according to the criteria established conformity with the applicable master plan of the drainage
Todd Johnson, P.E. #37660	Date
Owner/Developer's Statement:	
I, the owner/developer have read and will comply with and plan.	all of the requirements specified in this drainage repor
Justin Sternberg Steel Structures America Inc. 3635 E. Covington Ave. Post Falls, ID 83854	Date
El Paso County:	
Filed in accordance with the requirements of the Drain Engineering Criteria Manual and Land Development Co	
Jennifer Irvine, P.E. County Engineer / ECM Administrator	Date
Conditions:	

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SCOPE

The purpose of this report is to present the drainage plan for the proposed Monument Steel Structures development. The following includes final analysis and design information for the proposed drainage systems in general conformance with the standards and specifications established by El Paso County, Colorado Springs and the Urban Drainage and Flood Control District (UDFCD).

I. GENERAL LOCATION AND DESCRIPTION

A. <u>Site Location</u>

- The Monument Steel Structures development is located at 18910 Base Camp Road in Section 11, Township 11 South, Range 67 West of the 6th Principal Meridian in El Paso County, State of Colorado.
- Approximate geodetic coordinates for the site are: 39°6'21"N, 104°51'48"W
- The site is bordered to the north by the Greater Europe Missions, to the east by Base Camp Road, to the west by Monument Hill Road and to the south by Deer Creek Road.
- See Site Location Map below for overall site location: (See Vicinity Map in the Appendices)



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B. Description of Property

- The site is approximately 4.0 acres in size. The site is currently vacant and is covered by native grasses and weeds. Topography generally slopes from northeast to southwest towards a roadside ditch along Monument Hill Road with grades generally varying from 1% to 10%.
- The site is not located within a flooplain as shown on the FEMA FIRM Map No. 08041C0276G dated December 7, 2018.
- The site lies within Zone X which is described as follows: Areas of 0.2% annual chance flood; areas of 1% annual chance of a flood with average depths of less than 1 foot or with drainage areas less than 1 square mile; and areas protected by levees from 1% annual chance flood. See Appendix D for a FEMA Firm panel exhibit.
- The proposed Monument Steel Structures development is proposing a sales office with display structures and Mini Warehouse and RV Boat Storage.
- Soil types on site as identified by the Natural Resources Conservation Service (NRCS) are as follows:

Hydrologic Soil Group											
Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI							
92	Tomah – Crowfoot Loamy sands, 3 to 8 percent slopes	В	4.7	80.6%							
93	Tomah – Crowfoot complex, 8 to 15 percent slopes	В	1.1	19.4%							

- See Appendix D for soils map.
- There are no known irrigation canals or ditches within the project boundaries.

II. DRAINAGE BASINS AND SUB-BASINS

A. Major Drainage Basins

- The site is tributary to the Crystal Creek basin within Monument Creek watershed. There
 are no major drainageways crossing or adjacent to the site. Runoff from the proposed
 site will release from the on-site extended detention basin at the southwest corner of the
 site and will enter the recently constructed 30" FES (constructed with the Monument Hill
 Widening Project), matching existing drainage patterns.
- Off-site flow patterns will not be influenced by the development of this site.

B. Historic Drainage Basins

Basin E-1: Consists of the West half of Base Camp Road from the Greater Europe
Missions southern access to the Deer Creek Road intersection, native grasses and
weeds between the Base Camp Road and the eastern property boundary and native
grasses and weeds from the Greater Europe Missions parking lot to the northern property
boundary.

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- Historically, runoff from this basin flows onto the site and sheet flows across the subject property to the southwest corner of the site where it releases through the recently constructed 30" FES (constructed with the Monument Hill Widening Project).
- Basin E-2: Encompasses the property boundary and consists of vacant land covered by native grasses and weeds.
 - Historically, runoff from this basin sheet flows to the southwest corner of the site
 where it releases through the recently constructed 30" FES (constructed with the
 Monument Hill Widening Project).

C. Minor Drainage Basins

- Basin OS-1: Consists of vacant land in between the north boundary of the site and the southern parking lot of the Greater Europe Missions property.
 - Runoff generated in this basin will sheet flow overland from north to south entering the site along the northern property boundary and combine flows with Basin A-4 (See Below)
- Basin OS-2: Consists of vacant land in between the north boundary of the site and the southern parking lot of the Greater Europe Missions property.
 - Runoff generated in this basin will sheet flow overland from north to south entering the site along the northern property boundary and combine flows with Basin A-3.
- Basin OS-3: Consists of vacant land between the north boundary of the site and the southern parking lot of the Greater Europe Missions property. This basin also consists of the western half of Base Camp Road from the middle of the eastern property boundary north to the southern access of Greater Europe Missions property.
 - Runoff generated in this basin will sheet flow overland from north to south and east to west entering the site along the northern and eastern property boundary and combine flows with Basin A-2
- Basin OS-4: Consists of the western half of Base Camp Road and landscaping from the middle of the eastern property boundary south to the intersection of Base Camp Road and Deer Creek Road.
 - Runoff generated in this basin will sheet flow overland from east to west entering the site along the eastern property boundary and combine flows with Basin A-1.
- Basin OS-5: Consists of vacant land in between the north boundary of the site and the southern parking lot of the Greater Europe Missions property.
 - Runoff generated in this basin will sheet flow overland from the north to the south entering the site along the northern boundary and be directed west to the Monument Hill Road roadside via a drainage swale.
- Basin OS-6: Consists of rooftops and landscaping at the western portion of the site.
 - Runoff generated within this boundary will be released from the rooftops via downspouts and be directed west to the Monument Hill Road roadside ditch.
 Low Impact Development is being achieved within this basin as impervious and

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pervious areas are being disconnected along with implementing infiltration as the flows run along the earth lined roadside ditch. The 100-year allowable release for the EDB has been reduced by the derived 100-yr runoff of this basin.

A Deviation for this basin has been included in Appendix F.

- Basin OS-7: Consists of the Monument Hill roadside ditch and landscaping behind the proposed buildings along the western boundary recently constructed with the Monument Hill Widening Project.
 - Runoff generated in this basin will combine with the flows entering the basin from the Monument Hill roadside ditch to the north and the flows from Basin OS-5 and OS-6 described above. The combined flows will travel south along the earth lined roadside ditch to the recently constructed 30" FES transporting the flows under Deer Creek Road and off site.
 - A Deviation for this basin has been included in Appendix F.

Basin A-1; Consist of rooftops, pavement and landscaping at the southeastern corner of

the site.

Runoff generated in this basin will combine with the flows entering the site from the east (Basin OS-4) and the flows entering the site from the south (Basin OS-5). The flows will travel along the southern curb and gutter from the northeast to the southwest being captured by the proposed on-grade 10' Type R inlet (IN-1) at Design Point 1 where it will combine with flows from Basin A-2. This inlet has been sized to capture the 5-year flows and most of the 100-yr flows

- Captured flows will be transported to the proposed EDB via concrete pipe.
- Bypassing flows will travel west to Design Point 3 and be captured by a proposed Double Type 13 Combo inlet (IN-2) before entering the proposed EDB via concrete pipe.
- Basin A-2: Consists of rooftops, pavement and landscaping stretching from the northern boundary to the southern boundary encompassing the eastern-middle portion of the site.
 - Runoff generated in this basin will combine with the flows entering the site from the north (Basin OS-3). The flows will be directed towards and transported south via a 4-foot drainage pan being captured by the proposed on-grade 10' Type R inlet (IN-1) at Design Point 1 where it will combine with flows from Basin A-1 (See basin description above).
- Basin A-3: Consists of rooftops, pavement, and landscaping stretching from the northern boundary to the southern boundary encompassing the middle portion of the site.
 - Runoff generated in this basin will combine with the flows entering the site from the north (Basin OS-2). The flows will be directed towards and transported south vie a modified 2-foot curb and gutter running along the east side of the 48-foot storage building.

Remove the deviation request. The ECM has recently been updated to incorporate the exclusions from the MS4 permit. See the exclusion provision of the ECM. Verify if Appendix I Section I.7.1.C.1.a would be applicable. Update the narrative accordingly by discussing the applicable exclusion.

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- The said curb is proposed to be modified by having a 1-foot vertical height instead of the typical 0.5-foot vertical height for added capacity and building protection.
- The flows will flow from the 2-curb and gutter to a 4-foot drainage pan at the south end of the 48-foot storage building directing flows south to Design Point 3. Here the flows will be combined with any bypass flows bypassing the on-grade IN-1 and be captured by a proposed Double Type 13 Combo inlet (IN-2) in sump and be transported to the EDB via concrete pipe.
- Basin A-4: Consists of rooftops, pavement, sidewalk and landscaping stretching from the northern boundary to the southern boundary encompassing the western-middle portion of the site.
 - Runoff generated in this basin will combine with the flows entering the site from the north (Basin OS-1). The flows will be directed towards and transported south via a 4-foot drainage pan towards Design Point 4 being captured by a proposed Triple Type 13 Combo inlet (IN-3) in sump and be transported to the EDB via concrete pipe.
- Basin A-5: Consists of the onsite EDB.
 - Runoff generated in this basin will combine with all flows tributary to the EDB and will be captured and released by a controlled outlet structure.

III. DRAINAGE DESIGN CRITERIA

A. <u>Regulations</u>

• The site has been designed in accordance with the El Paso County Drainage Design Criteria Manual, adopted portions of the City of Colorado Springs Drainage Criteria Manual Volume 1, dated May 2014, and the Urban Storm Drainage Criteria Manual, Volumes 1, 2, and 3 (UDFCD), Urban Drainage and Flood Control District, latest revisions. The portions of the City of Colorado Springs Drainage Criteria Manual adopted by the County are Chapter 6 (Hydrology) and Chapter 13 Section 3.2.1 (Full Spectrum Detention).

B. Drainage Studies, Outfall Systems Plans, Site Constraints

The site is included within the limits of the Dirty Woman Creek and Crystal Creek
Drainage Basin Planning Study prepared by Kiowa Engineering in September of 1993.
There are no drainage way facilities proposed in the study that are located within the
limits of the site.

C. Hydrology

- Peak storm runoff was determined using the Rational Formula: Q=CIA
- Design storm recurrence intervals are the 5-year storm for the minor event and the 100year storm for the major event.
- Rainfall intensities were determined per Table 6-2, in accordance with the City of Colorado Springs Drainage Criteria Manual Volume 1, dated May 2014.

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- Runoff coefficients have been determined per Table 6-6, in accordance with the City of Colorado Springs Drainage Criteria Manual Volume 1, dated May 2014.
- Time of Concentration has been calculated per Section 3-2, in accordance with the City of Colorado Springs Drainage Criteria Manual Volume 1, dated May 2014.
- See Appendix A for all hydrologic calculations.

D. <u>Hydraulics</u>

- The calculation methods for private improvements are based upon the Manning's Equation and the City of Colorado Springs Drainage Criteria Manual Volumes 1 and 2, dated May 2014.
- On-Site storm drainage improvements are designed for the 5-year and 100-year events.
- See Appendix B for all hydraulic calculations.

IV. STORMWATER MANAGEMENT FACILITY DESIGN

A. Existing Stormwater Drainage

- The existing stormwater runoff for the proposed site flows overland from the northeast corner of the site towards the southwest corner with a fairly uniform grade of 3.5%.
- Historically the runoff from the vacant land between the north boundary of the site and
 the southern parking lot of the Greater Europe Missions property flows onto the site along
 the northern boundary of the site.
- Historically the runoff from the western half of Base Camp Road flows onto the site along the eastern boundary of the site.
- The eastern half of the proposed site flows into the Monument Hill roadside ditch north of Deer Creek Road and flows to the southwest corner of the site where it will be captured by the recently constructed 30" RCP flared end section (constructed with the Monument Hill Widening Project). As the proposed site will be release at or below historic levels the recently constructed 30" RCP crossing under Deer Creek Road is suitable outfall for the proposed development.
- The western half of the proposed site flows into the reconstructed roadside ditch east of Monument Hill Road (reconstructed with the Monument Hill widening project) and flows to the southwest corner of the site where it will be captured by the recently constructed 30" RCP flared end section (constructed with the Monument Hill Widening Project).

B. Proposed Stormwater Conveyance Facilities

- The proposed drainage patterns will follow historic flow patterns as closely as possible.
- The general concept for the site drainage will be for storm runoff to surface flow from the
 building roofs and pavement generally flowing from the north side of the site to the south
 side of the site via 4-foot v-channel drainage pans and curb and gutter. Runoff will be
 captured by a series of inlets south of the on-site drive isles and piped to the proposed
 Extended Detention Basin designed in accordance with City of Colorado Springs criteria.
- The proposed Extended Detention Basin will drain through a modified CDOT Type C outlet structure. The outlet structures released flow will be piped to the roadside ditch

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east of Monument Hill Road and be captured by the 30" RCP flared end section (which was constructed with the Monument Hill widening project.)

- The on-site storm sewers and EDB will be private and will be maintained by the property owner.
- Conveyance of off-site runoff is generated from Basin OS-6. Low Impact Development is being achieved within this basin as impervious and pervious areas are being disconnected along with implementing infiltration as the flows run along the earth lined roadside ditch. The 100-year allowable release for the EDB has been reduced by the derived 100-yr runoff of this basin.

Remove.

A Deviation for this basin has been included in Appendix F.

C. <u>Proposed Stormwater Storage Facilities</u>

- An Extended Detention Basin is proposed at the southwest corner of the site to treat storm runoff and attenuate peak flows in accordance with the City of Colorado Springs criteria and UDFCD.
- The Extended Detention Basin and outlet structure have been sized and designed with the UDFCD UD-Detention v3.07 spreadsheet to control the Water Quality Capture Volume (WQCV) and 100-year detention volume.
- The pond will include a trickle channel for low flow conditions, an outlet structure including a 2.5-ft deep micropool, and an emergency spillway with riprap erosion protection.
- See Appendix C for Detention and Water Quality Calculations

D. Water Quality Enhancement Best Management Practices

- El Paso County requires the Four Step Process be followed for the selection and siting of structural BMPs for new development to provide water quality for stormwater runoff being discharged into State Waters. The Four Steps are; employ runoff reduction practices, stabilize drainageways, provide water quality capture volume (WQCV) and consider need for industrial and commercial BMP's.
 - The design of the site has followed this process as much as possible. Pavement has been minimized to meet only the parking spaces as required by the county and landscaped areas are included to assist in reducing runoff. There are no major drainageways on site. The drainageways adjacent to the site are being improved with riprap protection where concentrated flows may cause erosion. The WQCV is being provided in the permanent BMP which is an Extended Detention Basin designed in accordance with county regulations
- Discharge will be controlled by a standard outlet structure with a flow control plate designed to release the WQCV over 40 hours and release 97% of the 5-year storm in less than 72 hours.
- The 100-year discharge will be limited to be at or below 2.95 cfs (0.85 cfs/acre for Type B soils minus the 100-yr peak runoff from Basin OS-7 which will bypass the EDB) and will be controlled by a circular orifice plate located at the discharge side of the outlet structure prior to the flow entering an 18" RCP flowing to the proposed drainage swale adjacent to

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Monument Hill Road. This swale flows to the south and will be captured by the 30" FES to be constructed as part of the Monument Hill Road widening Improvements. In the event the outlet structure should become clogged with debris, and emergency overflow weir and swale will be constructed along the west side of the EDB. The emergency overflow swale will be a notched 15' wide by 1' deep cavity in the proposed EDB upper wall. Overflow will go to the proposed drainage swale along Monument Hill Road flowing to the south to the existing 30" FES and will be routed off site.

E. Floodplain Modification

 A floodplain modification is not anticipated for the construction of the Monument Steel Structures development.

F. Additional Permitting Requirements

 No additional permitting is anticipated for the construction of the Monument Steel Structures development.

V. CONCLUSIONS

A. Compliance with Standards

- The drainage design for the Monument Steel Structures site detailed within this report is in general compliance with the El Paso County, Colorado Springs and UDFCD criteria.
- Per Note 9 of the Greater Europe Mission Subdivision Filing Number 1 Plat:
 - DRAINAGE FEES FOR LOT 2 SHALL BE PAID PRIOR TO THE ISSUANCE OF A BUILDING PERMIT AND THOSE FEES ARE TO BE CALCULATED ON THE BASIS OF THE FEE STRUCTURE IN EFFECT AT THE TIME OF BUILDING PERMIT APPLICATION.
- Per the 2019 Drainage Basin Fees Drainage Basin FOMO5300
 - Drainage Basin Fee = \$18,350 / Impervious Acre
 - Bridge Fee = \$1,004 / Impervious Acre

2019 DRAINAGE BASIN FEES - LOT 2											
Fee	\$ / Imp Acre	Imp Acres	Fee								
Drainage Basin Fee	\$18,350	2.98	\$54,629.39								
Bridge Fee	\$1,004	2.98	\$2,988.99								

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B. Variances / Deviations 4

Deviation request does not appear to be required anymore with the recently updated ECM.

Remove or update to discuss the applicable exclusion. See comment on page 6 of 12.

- We request the Deviation from Appendix I Section 1.7.1B—Providing Water Quality for Entire Development for proposed basins OS-6 and OS-7.
 - Approximately 0.56 acres (14.0%) of 4.0 acres of the area inside the development boundary will not reach a proposed on-site water quality facility. Of the area inside the development boundary that will not reach a facility, 0.14 acres is proposed roofs and 0.42 acres is the existing Monument Hill Roadside ditch and landscape areas behind the proposed buildings.
 - The site is however receiving and treating 1.23 acres of untreated areas outside of the development boundary including 0.16 acres of pavement from Base Camp Road.
 - In Summary, 0.14 acres of impervious area (rooftops) is leaving our site untreated but 0.16 acres of impervious area is entering our site and being treated by the proposed treatment facility. Therefore, we have a net +0.02 impervious area being treated overall.

C. <u>Drainage Concept</u>

- The proposed drainage patterns will follow historic flow patterns as closely as possible.
 The majority of the site will sheet flow to the southwest into the proposed Extended Detention Basin.
- With the development of the proposed site; there should be no adverse impact to downstream facilities, adjacent properties, channel depths, velocities, or erosion rates, due to release flows being below historic rates.

VI. LIST OF REFERENCES

- El Paso County's Engineering Criteria Manual, Revised 07/29/2015 Revision 5.
- City of Colorado Springs Drainage Criteria Manual Volumes 1 and 2, dated May 2014.
- Urban Storm Drainage Criteria Manual, Volumes 1, 2, and 3, Urban Drainage and Flood Control District, latest editions.
- Federal Emergency Management Agency Flood Insurance Rate Map Panel Number 08041C0276G, effective December 7, 2018.
- Dirty Woman Creek and Crystal Creek Drainage Basin Planning Study prepared by Kiowa Engineering Dated September, 1993.

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APPENDICES

VICINITY MAP

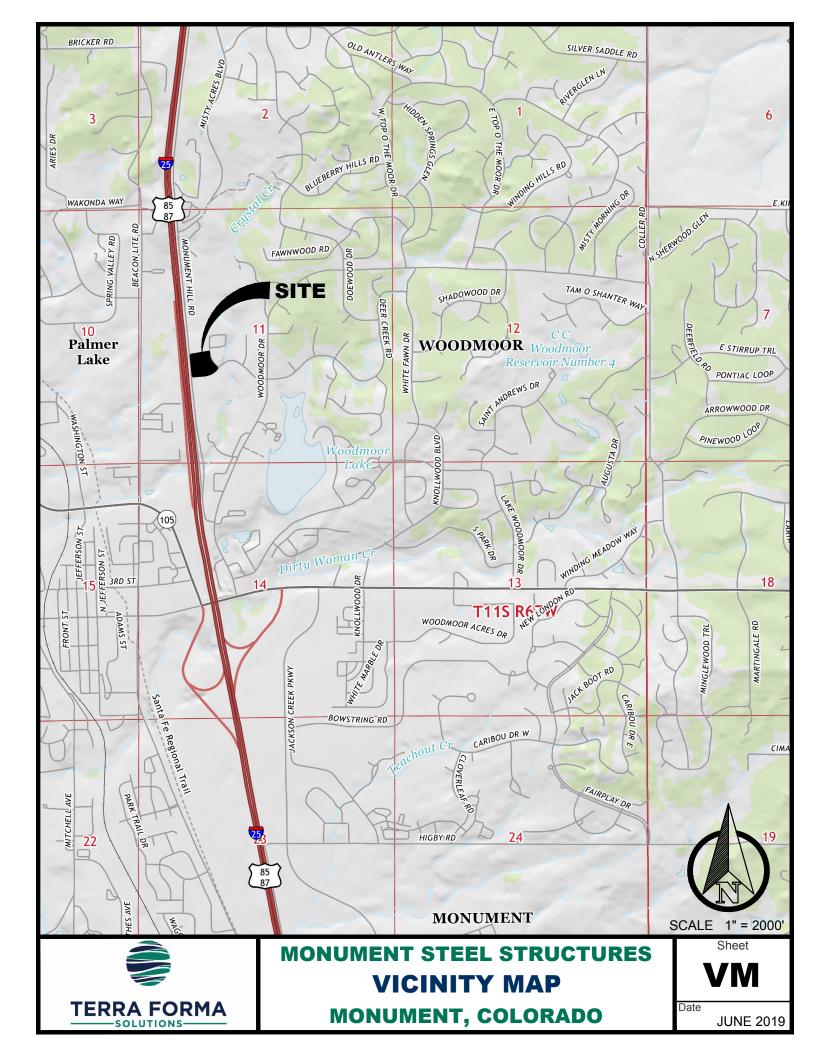
APPENDIX A – Hydrologic Computations

APPENDIX B – Hydraulic Computations

APPENDIX C – Detention/Water Quality Enhancement BMPs

APPENDIX D – Referenced Information

APPENDIX E – Drainage Maps



APPENDIX A - HYDROLOGIC COMPUTATIONS



Project: Monument Steel Structures

Location: Monument, CO

Designer: TAJ
Date: 4/7/2019
Latest Revision: 6/15/2019

 1 From Table 6-6 in Colorado Springs DCM, Volume 1

²From Table 6-6 in Colorado Springs DCM, Volume 1

IMPERVIOUSNESS AND RUNOFF COEFFICIENT CALCULATIONS

				Roofs	Lawn	Pavement	Sidewalk	Pond HWL	Misc						
			Impervious %1	90%	0%	100%	100%	100%	0%						
Davis Davis satism	NRCS Hydrologic	Total Area	Total Area	Roofs	Lawn	Pavement	C:-l - (-f)	Pond HWL	Misc	Percent	Impervious		Runoff Coeff	ficients, C ²	
Basin Designation	Soil Group	(ac)	(sf)	(sf)	(sf)	(sf)	Sidewalk (sf)	(sf)	(sf)	Impervious	Area (ac)	C ₂	C ₅	C ₁₀	C ₁₀₀
E-1	В	1.35	58,906		52,085	6,821				11.58%	0.16	0.12	0.17	0.24	0.42
E-2	В	4.00	174,280		174,280					0.00%	0.00	0.02	0.08	0.15	0.35
OS-1	В	0.45	19,479		19,479			0	0	0.00%	0.00	0.02	0.08	0.15	0.35
OS-2	В	0.22	9,459		9,459			0	0	0.00%	0.00	0.02	0.08	0.15	0.35
OS-3	В	0.42	18,281		13,642	4,639		0	0	25.38%	0.11	0.24	0.29	0.35	0.50
OS-4	В	0.15	6,407		4,225	2,182		0	0	34.06%	0.05	0.32	0.36	0.41	0.56
OS-5	В	0.12	5,280		5,280			0	0	0.00%	0.00	0.02	0.08	0.15	0.35
OS-6	В	0.16	7,031	6,636	395			0	0	84.94%	0.14	0.67	0.69	0.72	0.78
OS-7	В	0.40	17,418		17,418			0	0	0.00%	0.00	0.02	0.08	0.15	0.35
A-1	В	0.43	18,530	3,272	4,867	10,392		0	0	71.97%	0.31	0.63	0.65	0.69	0.77
A-2	В	0.90	39,189	9,409	6,191	23,589		0	0	81.80%	0.74	0.71	0.73	0.76	0.83
A-3	В	0.79	34,223	10,340	819	23,064				94.59%	0.74	0.81	0.83	0.85	0.90
A-4	В	1.10	48,025	20,538	825	25,847	815	0	0	94.01%	1.04	0.80	0.81	0.83	0.89
A-5	В	0.23	9,864		9,064	800		0	0	8.11%	0.02	0.09	0.15	0.21	0.40
								0	0						
Area Treated by EDB	В	4.67	203,457	Basins (OS	S-1, OS-2 OS-	3, OS-4, A-1, A-	2, A-3, A-4, A-5)	0	0	64.16%	3.00				
Area Not Treated by EDB	В	0.68	29,729		Basins (0	OS-5, OS-6, OS-	7)	0	0	20.09%	0.14				
								0	0						
Overall		5.35	233,186					0	0	58.54%	3.13				



Project: Monument Steel Structures

Location: Monument, CO Designer: TAJ Date: 4/7/2019 Latest Revision: 6/15/2019

NRCS Conveyance Factors, K² Type of Land Surface Κ Heavy Meadow 2.5 Tillage/Field 5 Short Pasture/Lawns 7 Nearly Bare Ground 10 Grassed Waterway 15

¹Max 100 ft in Urban areas and 300 ft in rural areas ²From Table 6-7 - Coloardo Springs DCM

TIME OF CONCENTRATION CALCULATIONS

20

			Initial/	Overland Flo	w Time, T _i		Channelize	d Flow/Trave	l Time, T _t		Time o			
Basin Designation	Imperviousness (%)	C₅	Length (ft) ¹	Slope (%)	T _i (min)	Land Surface	Length (ft)	Slope (%)	Velocity (ft/sec)	T _t (min)	Computed T _c (min)	First Design Point T _c (min)	Minimum T _c (min)	Selected T _c (min)
E-1	11.58%	0.17	25	3.00	5.81	Paved Areas	140	3.40	3.69	0.63	6.44	10.92	10.00	10.00
E-2	0.00%	0.08	100	3.40	12.30	Short Pasture/Lawns	445	4.65	1.51	4.91	17.21	13.03	10.00	13.03
OS-1	0.00%	0.08	25	5.00	5.41	Short Pasture/Lawns	175	5.00	1.57	1.86	7.28	11.11	5.00	7.28
OS-2	0.00%	0.08	25	5.00	5.41	Short Pasture/Lawns	110	5.00	1.57	1.17	6.59	10.75	5.00	6.59
OS-3	25.38%	0.29	25	2.00	5.83	Short Pasture/Lawns	130	5.00	1.57	1.38	7.22	10.86	5.00	7.22
OS-4	34.06%	0.36	15	2.00	4.12	Short Pasture/Lawns	20	16.00	2.80	0.12	4.24	10.19	5.00	5.00
OS-5	0.00%	0.08	25	5.00	5.41	Short Pasture/Lawns	163	5.00	1.57	1.74	7.15	11.04	5.00	7.15
OS-6	84.94%	0.69	10	2.00	1.85	Grassed Waterway	25	2.00	2.12	0.20	2.04	10.19	5.00	5.00
OS-7	0.00%	0.08	25	25.00	3.18	Grassed Waterway	392	2.80	2.51	2.60	5.79	12.32	5.00	5.79
A-1	71.97%	0.65	45	3.05	3.73	Paved Areas	292	1.37	2.34	2.08	5.81	11.87	5.00	5.81
A-2	81.80%	0.73	45	4.80	2.67	Paved Areas	412	2.18	2.96	2.32	5.00	12.54	5.00	5.00
A-3	94.59%	0.83	45	2.50	2.43	Paved Areas	433	1.73	2.63	2.74	5.17	12.66	5.00	5.17
A-4	94.01%	0.81	65	1.65	3.54	Paved Areas	365	2.19	2.96	2.05	5.59	12.39	5.00	5.59
A-5	8.11%	0.15	25	10.00	4.03	Paved Areas	140	0.50	1.41	1.65	5.68	10.92	5.00	5.68

3.2.1 Overland (Initial) Flow Time

The overland flow time, t_i , may be calculated using Equation 6-8.

$$t_i = \frac{0.395(1.1 - C_5)\sqrt{L}}{5^{0.33}}$$
 (Eq. 6-8)

Where

- t_i = overland (initial) flow time (min)
- C_5 = runoff coefficient for 5-year frequency (see Table 6-6) L = length of overland flow (300 ft maximum for non-urban land uses, 100 ft maximum for
- S = average basin slope (ft/ft)

3.2.2 Travel Time

For catchments with overland and channelized flow, the time of concentration needs to be considered in combination with the travel time, t_t, which is calculated using the hydraulic properties of the swale, ditch, or channel. For preliminary work, the overland travel time, t_t, can be estimated with the help of Figure 6-25 or Equation 6-9 (Guo 1999).

$$V = C_v S_w^{0.5}$$
 (Eq. 6-9)

Where:

Paved Areas

V = velocity (ft/s)

 C_v = conveyance coefficient (from Table 6-7)

 S_{w} = watercourse slope (ft/ft)

 $t_c = t_i + t_r$ (Eq. 6-7)

Where:

 t_c = time of concentration (min)

 t_i = overland (initial) flow time (min)

 t_i = travel time in the ditch, channel, gutter, storm sewer, etc. (min)

3.2.3 First Design Point Time of Concentration in Urban Catchments

Using this procedure, the time of concentration at the first design point (typically the first inlet in the system) in an urbanized eatchment should not exceed the time of concentration calculated using Equation 6-10. The first design point is defined as the point where runoff first enters the storm sewer system.

$$t_c = \frac{L}{180} + 10 \tag{Eq. 6-10}$$

Where:

 t_c = maximum time of concentration at the first design point in an urban watershed (min)

L = waterway length (ft)

Equation 6-10 was developed using the rainfall-runoff data collected in the Denver region and, in essence, represents regional "calibration" of the Rational Method. Normally, Equation 6-10 will result in a lesser

3.2.4 Minimum Time of Concentration

If the calculations result in a t_c of less than 10 minutes for undeveloped conditions, it is recommended that a minimum value of 10 minutes be used. The minimum t_c for urbanized areas is 5 minutes.



Location: Monument, CO

Designer: TAJ

Date: 4/7/2019

Latest Revision: 6/15/2019

Design Storm: 5-Yr 1-hr Design Point Rainfall (in): 1.50

5-YEAR PEAK RUNOFF CALCULATIONS

Basin Designation	Design Point	Basin Outfall	Area (ac)	C ₅	CXA	T _c (min)	Intensity (in/hr)	Peak Flow, Q (cfs)
E-1	1	Basin E-1	1.35	0.17	0.24	10.00	4.06	0.96
E-2	2	Ex 30" RCP	4.00	0.08	0.32	13.03	3.63	1.16
OS-1	4	Basin A-4	0.45	0.08	0.04	7.28	4.55	0.16
OS-2	3	Basin A-3	0.22	0.08	0.02	6.59	4.70	0.08
OS-3	2	Basin A-2	0.42	0.29	0.12	7.22	4.57	0.55
OS-4	1	Basin A-1	0.15	0.36	0.05	5.00	5.09	0.27
OS-5		Basin OS-7	0.12	0.08	0.01	7.15	4.58	0.04
OS-6		Basin OS-7	0.16	0.69	0.11	5.00	5.09	0.57
OS-7		Ex 30" RCP	0.40	0.08	0.03	5.79	4.89	0.16
A-1	1	IN-1 (10' Type R)	0.43	0.65	0.28	5.81	4.88	1.36
A-2	2	IN-1 (10' Type R)	0.90	0.73	0.66	5.00	5.09	3.34
A-3	3	IN-2 (Double Type 13)	0.79	0.83	0.65	5.17	5.04	3.28
A-4	4	IN-3 (Triple Type 13)	1.10	0.81	0.90	5.59	4.94	4.42
A-5	5	EDB Outlet Structure	0.23	0.15	0.03	5.68	4.91	0.16



Project: Monument Steel Structures

Location: Monument, CO

Designer: TAJ

Date: 4/7/2019

Latest Revision: 6/15/2019

Design Storm:	100-Yr
1-hr Design Point Rainfall (in):	2.52

100-YEAR PEAK RUNOFF CALCULATIONS

Basin Designation	Design Point	Basin Outfall	Area (ac)	C ₁₀₀	CXA	T _c (min)	Intensity (in/hr)	Peak Flow, Q (cfs)
E-1	1	Basin E-1	1.35	0.42	0.57	10.00	6.82	3.88
E-2	2	Ex 30" RCP	4.00	0.35	1.40	13.03	6.10	8.55
OS-1	4	Basin A-4	0.45	0.35	0.16	7.28	7.65	1.20
OS-2	3	Basin A-3	0.22	0.35	0.08	6.59	7.90	0.60
OS-3	2	Basin A-2	0.42	0.50	0.21	7.22	7.67	1.62
OS-4	1	Basin A-1	0.15	0.56	0.08	5.00	8.55	0.70
OS-5		Basin OS-7	0.12	0.35	0.04	7.15	7.69	0.33
OS-6		Basin OS-7	0.16	0.78	0.13	5.00	8.55	1.08
OS-7		Ex 30" RCP	0.40	0.35	0.14	5.79	8.21	1.15
A-1	1	IN-1 (10' Type R)	0.43	0.77	0.33	5.81	8.20	2.70
A-2	2	IN-1 (10' Type R)	0.90	0.83	0.74	5.00	8.55	6.36
A-3	3	IN-2 (Double Type 13)	0.79	0.90	0.71	5.17	8.47	5.99
A-4	4	IN-3 (Triple Type 13)	1.10	0.89	0.98	5.59	8.29	8.09
A-5	5	EDB Outlet Structure	0.23	0.40	0.09	5.68	8.26	0.75



Project: Monument Steel Structures

Location: Monument, CO

Designer: TAJ

Date: 4/7/2019

Revision: 6/15/2019

Design Storm: 5-Yr 1-hr Design Point Rainfall (in): 1.50

MINOR STORM ROUTING CALCULATIONS

						Direct F	lunoff					Runoff		Str	eet		Travel	Time		
Design Point	Contributing Basins	Basin Outfall	Basin Designation	Area (ac)	C ₅	CXA	T _c (min)	Intensity (in/hr)	Peak Flow, Q (cfs)	T _c (min)	Sum Area (C X A)	Intensity (in/hr)	Q (cfs)	Slope (%)	Street Q (cfs)	Length (ft)	Velocity (ft/sec)	T _t (min)	Carry Over CA	Remarks
			OS-4	0.15	0.36	0.05	5.00	5.09	0.27											
			A-1	0.43	0.65	0.28	5.81	4.88	1.36											
1	A-1, OS-4	C&G to IN-1								5.81	0.33	4.88	1.62							Used to check Gutter Capacity
			OS-3	0.42	0.29	0.12	7.22	4.57	0.55					1.80%	0.55	422	2.68	2.62	0.12	Flows from OS-3 to DP 2
			A-2	0.90	0.73	0.66	5.00	5.09	3.34											
2	A-2, OS-3	Drainage Pan to IN-1								9.84	0.78	4.08	3.17							Used to Check Drainage Pan Capacity
	A-1, A-2, OS-3, OS-4	IN-1								9.84	1.11	4.08	4.53							Inlet Overflows to DP 3
			OS-2	0.22	0.08	0.02	6.59	4.70	0.08					2.00%	0.08	415	2.83	2.45	0.02	Flows from OS-2 to DP 3
			A-3	0.79	0.83	0.65	5.17	5.04	3.28											
3	A-3, OS-2	IN-2								9.03	0.67	4.22	2.82							Inlet Overflows to DP 5 (EDB)
			OS-1	0.45	0.08	0.04	7.28	4.55	0.16					2.00%	0.16	358	2.83	2.11	0.04	
			A-4	1.10	0.81	0.90	5.59	4.94	4.42											
4	A-4, OS-1	IN-3								9.39	0.93	4.16	3.88							Inlet Overflows to DP 5 (EDB)
5	A-1 - A-4, OS-1 Through OS-4	EDB								9.84	2.71	4.08	11.07							
			OS-5	0.12	0.08	0.01	7.15	4.58	0.04											Used to check swale capacity
			OS-6	0.16	0.69	0.11	5.00	5.09	0.57											
			OS-7	0.40	0.08	0.03	5.79	4.89	0.16											



Project: Monument Steel Structures
Location: Monument, CO
Designer: TAJ
Date: 4/7/2019

t Revision: 6/15/2019

Design Storm: 100-Yr 1-hr Design Point Rainfall (in): 2.52

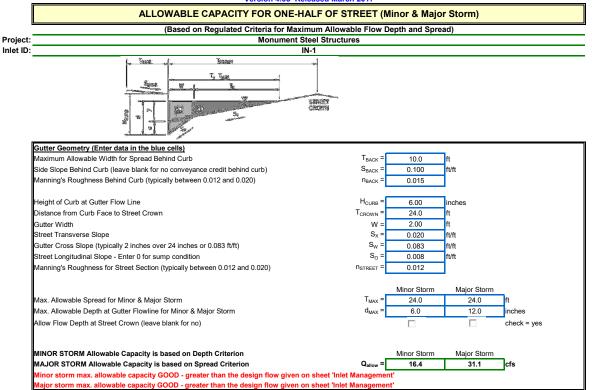
MAJOR STORM ROUTING CALCULATIONS

					Di	rect Runoff						Runoff		Str	eet	Travel Time				
Design Point	Contributing Basins	Basin Oufall	Basin Designation	Area (ac)	C ₁₀₀	CXA	T _c (min)	Intensity (in/hr)	Peak Flow, Q (cfs)	T _c (min)	Sum Area (C X A)	Intensity (in/hr)	Q (cfs)	Slope (%)	Street Q (cfs)	Length (ft)	Velocity (ft/sec)	T _t (min)	Carry Over CA	Remarks
			OS-4	0.15	0.56	0.08	5.00	8.55	0.70											
			A-1	0.43	0.77	0.33	5.81	8.20	2.70											
1	A-1, OS-4	C&G to IN-1								5.81	0.41	8.20	3.37							Used to check Gutter Capacity
			OS-3	0.42	0.50	0.21	7.22	7.67	1.62					1.80%	1.62	422	2.68	2.62	0.21	Flows from OS-3 to DP 2
			A-2	0.90	0.83	0.74	5.00	8.55	6.36											
2	A-2, OS-3	Drainage Pan to IN-1								9.84	0.96	6.86	6.56							Used to Check Drainage Pan Capacity
	A-1, A-2, OS-3, OS-4	IN-1								9.84	1.37	6.86	9.38							Inlet Overflows to DP 3
			OS-2	0.22	0.35	0.08	6.59	7.90	0.60					2.00%	0.60	415	2.83	2.45	0.08	Flows from OS-2 to DP 3
			A-3	0.79	0.90	0.71	5.17	8.47	5.99											
3	A-3, OS-2	IN-2								9.03	0.78	7.09	5.55							Inlet Overflows to DP 5 (EDB)
			OS-1	0.45	0.35	0.16	7.28	7.65	1.20					2.00%	1.20	358	2.83	2.11	0.16	
			A-4	1.10	0.89	0.98	5.59	8.29	8.09											
4	A-4, OS-1	IN-3								9.39	1.13	6.99	7.91							Inlet Overflows to DP 5 (EDB)
5	A-1 - A-4, OS-1 Through OS-4	EDB								9.84	3.28	6.86	22.53							
			OS-5	0.12	0.35	0.04	7.15	7.69	0.33											
			OS-6	0.16	0.78	0.13	5.00	8.55	1.08											
			OS-7	0.40	0.35	0.14	5.79	8.21	1.15											

APPENDIX B - HYDRAULIC COMPUTATIONS

2ft Catch Curb and 24' Drive Isle Capacity

Version 4.05 Released March 2017



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Channel Report

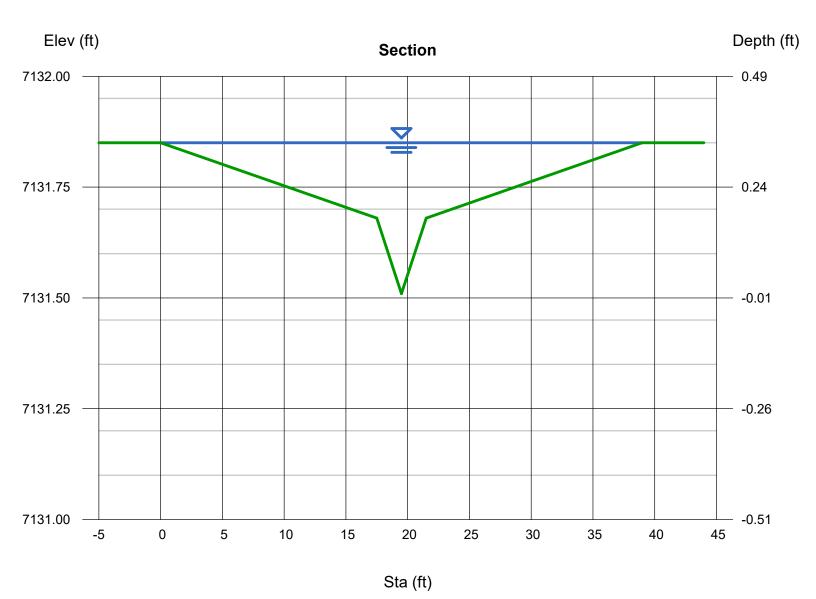
Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Monday, Apr 8 2019

40 Foot Drainage Pan Capacity

User-defined		Highlighted	
Invert Elev (ft)	= 7131.51	Depth (ft)	= 0.34
Slope (%)	= 1.80	Q (cfs)	= 14.54
N-Value ´	= Composite	Area (sqft)	= 3.99
	·	Velocity (ft/s)	= 3.64
Calculations		Wetted Perim (ft)	= 39.00
Compute by:	Q vs Depth	Crit Depth, Yc (ft)	= 0.34
No. Increments	= 10	Top Width (ft)	= 38.98
		EGL (ft)	= 0.55

(Sta, EI, n)-(Sta, EI, n)... (0.00, 7131.85)-(17.50, 7131.68, 0.012)-(19.50, 7131.51, 0.012)-(21.50, 7131.68, 0.012)-(38.98, 7131.85, 0.012)



Channel Report

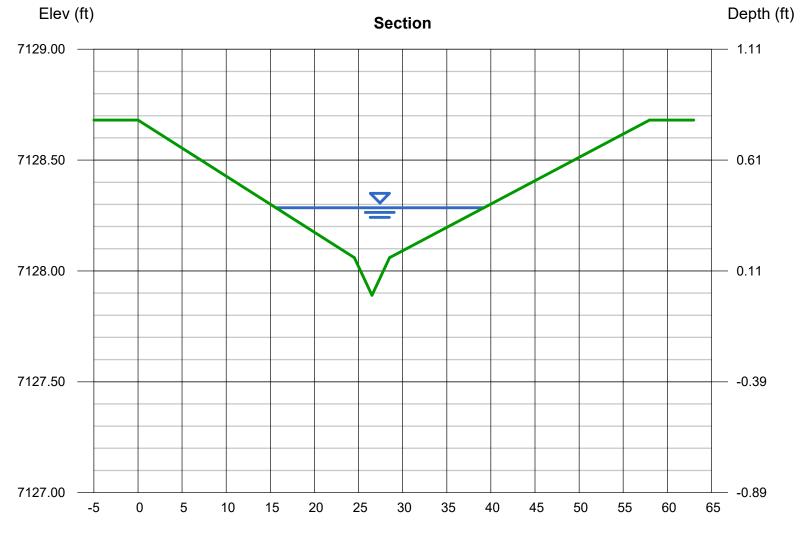
Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Monday, Apr 8 2019

60 Foot Drainage Pan Capacity

User-defined Invert Elev (ft)	= 7127.89	Highlighted Depth (ft)	= 0.40
Slope (%)	= 2.00	Q (cfs)	= 16.75
N-Value	= Composite	Area (sqft)	= 3.45
	•	Velocity (ft/s)	= 4.86
Calculations		Wetted Perim (ft)	= 23.61
Compute by:	Q vs Depth	Crit Depth, Yc (ft)	= 0.51
No. Increments	= 10	Top Width (ft)	= 23.59
		EĠL (ft)	= 0.76

(Sta, EI, n)-(Sta, EI, n)... (0.00, 7128.68)-(24.52, 7128.06, 0.012)-(26.52, 7127.89, 0.012)-(28.52, 7128.06, 0.012)-(57.98, 7128.68, 0.012)



Channel Report

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Monday, Apr 8 2019

= 0.50

= 18.14

12 IN Vertical Curb Alley Capacity

User-defined
Invert Elev (ft) = 7131.32
Slope (%) = 2.00
N-Value = Composite

Calculations

Compute by: Q vs Depth No. Increments = 10

Area (sqft) = 3.08
Velocity (ft/s) = 5.89
Wetted Perim (ft) = 15.87
Crit Depth, Yc (ft) = 0.66
Top Width (ft) = 15.54
EGL (ft) = 1.04

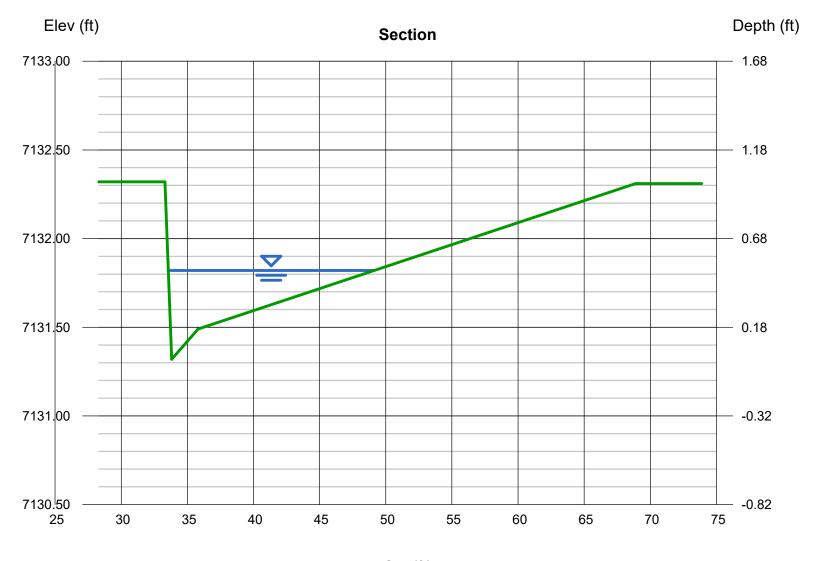
Highlighted

Depth (ft)

Q (cfs)

(Sta, El, n)-(Sta, El, n)...

(33.31, 7132.32)-(33.81, 7131.32, 0.012)-(35.81, 7131.49, 0.012)-(68.88, 7132.31, 0.012)



Sta (ft)



Version 4.05 Released March 2017

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) Project: Monument Steel Structures Inlet ID: IN-1 STREET Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb T_{BACK} : 10.0 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) S_{BACK} 0.100 ft/ft Manning's Roughness Behind Curb (typically between 0.012 and 0.020) 0.015 Height of Curb at Gutter Flow Line H_{CURB} : 6.00 inches Distance from Curb Face to Street Crown T_{CROWN} 24.0 Gutter Width W = 2.00 Street Transverse Slope S_X = ft/ft 0.020 Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) S_W : 0.083 ft/ft Street Longitudinal Slope - Enter 0 for sump condition So 0.008 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) n_{STREET} : 0.012 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm 24.0 24.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm 6.0 12.0 inches Allow Flow Depth at Street Crown (leave blank for no) check = yes MINOR STORM Allowable Capacity is based on Depth Criterion Minor Storm Major Storm MAJOR STORM Allowable Capacity is based on Spread Criterion

linor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Manag lajor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Manag

16.4

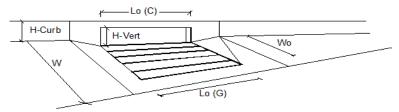
31.1

cfs

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INLET ON A CONTINUOUS GRADE

Version 4.05 Released March 2017



Design Information (Input)		MINOR	MAJOR	_
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a') a _{LOCAL} =			3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	2	2	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	5.00	5.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C_f - $G =$	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C_f - $C =$	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	4.2	6.5	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.3	2.9	cfs
Capture Percentage = Q _a /Q _o =	C% =	93	69	%

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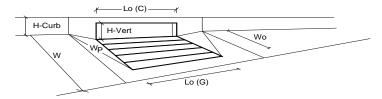
Version 4.05 Released March 2017

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) Project: Monument Steel Structures Inlet ID: IN-2 STREET Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb T_{BACK} : 5.0 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) S_{BACK} 0.020 ft/ft Manning's Roughness Behind Curb (typically between 0.012 and 0.020) 0.015 Height of Curb at Gutter Flow Line H_{CURB} : 6.00 inches Distance from Curb Face to Street Crown T_{CROWN} 24.0 Gutter Width W = 2.00 S_X = Street Transverse Slope 0.020 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) S_W : 0.083 ft/ft Street Longitudinal Slope - Enter 0 for sump condition So 0.000 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) n_{STREET} : 0.012 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm 24.0 24.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm 6.0 8.0 Check boxes are not applicable in SUMP conditions MINOR STORM Allowable Capacity is based on Depth Criterion Minor Storm Major Storm SUMP MAJOR STORM Allowable Capacity is based on Depth Criterion SUMP cfs

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INLET IN A SUMP OR SAG LOCATION

Version 4.05 Released March 2017



Design Information (Input)			MINOR	MAJOR	
Type of Inlet	CDOT/Denver 13 Combination	Type =	CDOT/Denver	13 Combination	7
Local Depression (additional to cor	a _{local} =	2.00	2.00	inches	
Number of Unit Inlets (Grate or Cu	No =	2	2]	
Water Depth at Flowline (outside o	of local depression)	Ponding Depth =	6.0	7.3	inches
Grate Information			MINOR	MAJOR	Override Depths
Length of a Unit Grate		L ₀ (G) =	3.00	3.00	feet
Width of a Unit Grate		$W_o =$	1.73	1.73	feet
Area Opening Ratio for a Grate (ty	pical values 0.15-0.90)	A _{ratio} =	0.43	0.43]
Clogging Factor for a Single Grate	(typical value 0.50 - 0.70)	$C_f(G) =$	0.50	0.50	
Grate Weir Coefficient (typical value	ue 2.15 - 3.60)	C _w (G) =	3.30	3.30	
Grate Orifice Coefficient (typical va	alue 0.60 - 0.80)	C _o (G) =	0.60	0.60	1
Curb Opening Information			MINOR	MAJOR	_
Length of a Unit Curb Opening		L _o (C) =	3.00	3.00	feet
Height of Vertical Curb Opening in	Inches	H _{vert} =	6.50	6.50	inches
Height of Curb Orifice Throat in Inc	ches	H _{throat} =	5.25	5.25	inches
Angle of Throat (see USDCM Figu	re ST-5)	Theta =	0.00	0.00	degrees
Side Width for Depression Pan (ty	pically the gutter width of 2 feet)	$W_p =$	2.00	2.00	feet
Clogging Factor for a Single Curb	Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	1
Curb Opening Weir Coefficient (ty	pical value 2.3-3.7)	$C_w(C) =$	3.70	3.70	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	C _o (C) =	0.66	0.66]
Low Head Performance Reducti	on (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth		d _{Grate} =	0.523	0.629	ft
Depth for Curb Opening Weir Equ	ation	d _{Curb} =	0.33	0.44	ft
Combination Inlet Performance Re	eduction Factor for Long Inlets	RF _{Combination} =	0.71	0.86]
Curb Opening Performance Reduc	e e e e e e e e e e e e e e e e e e e	RF _{Curb} =	1.00	1.00	1
Grated Inlet Performance Reduction	on Factor for Long Inlets	RF _{Grate} =	0.71	0.86	I
		_	MINOR	MAJOR	_
Total Inlet Interception Ca	pacity (assumes clogged condition)	$Q_a =$	5.3	9.0	cfs
Inlet Capacity IS GOOD for Mino	r and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	3.1	8.5	cfs

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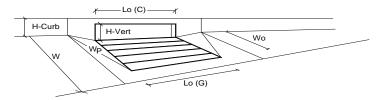
Version 4.05 Released March 2017

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) Project: Monument Steel Structures Inlet ID: IN-3 STREET Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb T_{BACK} : 5.0 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) S_{BACK} 0.020 ft/ft Manning's Roughness Behind Curb (typically between 0.012 and 0.020) 0.015 Height of Curb at Gutter Flow Line H_{CURB} : 6.00 inches Distance from Curb Face to Street Crown T_{CROWN} 24.0 Gutter Width W = 2.00 S_X = Street Transverse Slope 0.020 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) S_W : 0.083 ft/ft Street Longitudinal Slope - Enter 0 for sump condition So 0.000 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) n_{STREET} : 0.012 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm 24.0 24.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm 6.0 8.0 Check boxes are not applicable in SUMP conditions MINOR STORM Allowable Capacity is based on Depth Criterion Minor Storm Major Storm SUMP MAJOR STORM Allowable Capacity is based on Depth Criterion SUMP cfs

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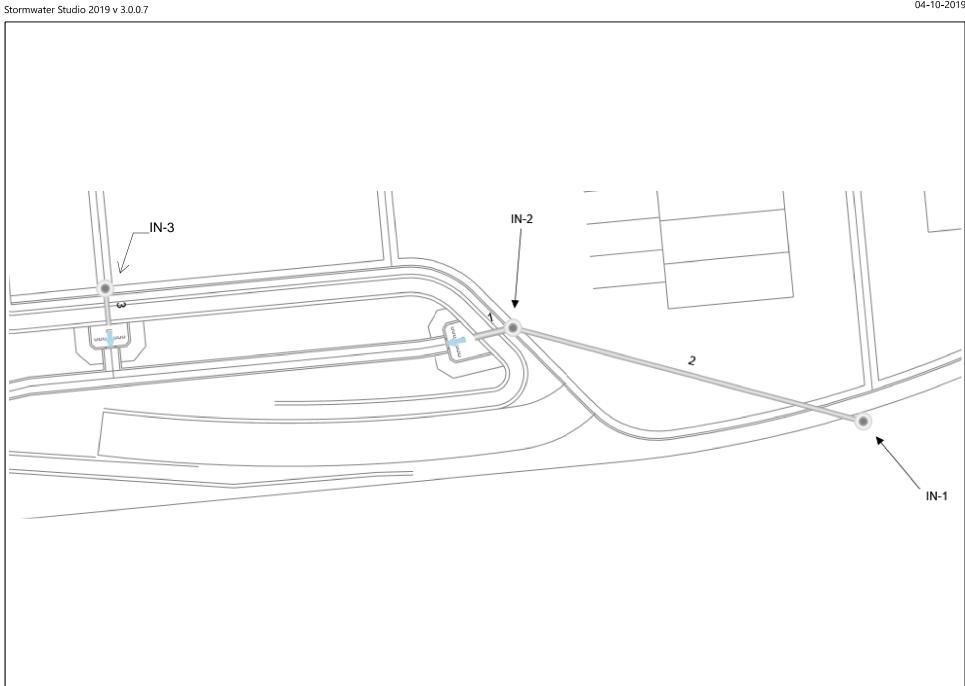
INLET IN A SUMP OR SAG LOCATION

Version 4.05 Released March 2017



Design Information (Input)	CDOT/Denver 13 Combination			MINOR	MAJOR	
Type of Inlet		Type =	CDOT/Denver	13 Combination	T	
Local Depression (additional to continuous gutter depression 'a' from above)			a _{local} =	2.00	2.00	inches
Number of Unit Inlets (Grate or Curb Opening)			No =	3	3]
Water Depth at Flowline (outside of	local depression)		Ponding Depth =	6.0	7.3	inches
Grate Information				MINOR	MAJOR	Override Depths
Length of a Unit Grate			$L_o(G) =$	3.00	3.00	feet
Width of a Unit Grate			$W_o =$	1.73	1.73	feet
Area Opening Ratio for a Grate (typi	ical values 0.15-0.90)		$A_{ratio} =$	0.43	0.43	1
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)		$C_f(G) =$	0.50	0.50	
Grate Weir Coefficient (typical value	2.15 - 3.60)		C_w (G) =	3.30	3.30	
Grate Orifice Coefficient (typical value	ue 0.60 - 0.80)		C _o (G) =	0.60	0.60	1
Curb Opening Information				MINOR	MAJOR	
Length of a Unit Curb Opening			$L_o(C) =$	3.00	3.00	feet
Height of Vertical Curb Opening in I	nches		H _{vert} =	6.50	6.50	inches
Height of Curb Orifice Throat in Inch	ies		$H_{throat} =$	5.25	5.25	inches
Angle of Throat (see USDCM Figure ST-5)			Theta =	0.00	0.00	degrees
Side Width for Depression Pan (typi	cally the gutter width of 2 feet)		$W_p =$	2.00	2.00	feet
Clogging Factor for a Single Curb O	pening (typical value 0.10)		$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typi		$C_w(C) =$	3.70	3.70		
Curb Opening Orifice Coefficient (ty		C _o (C) =	0.66	0.66		
Low Head Performance Reduction	n (Calculated)			MINOR	MAJOR	
Depth for Grate Midwidth			d _{Grate} =	0.523	0.629	ft
Depth for Curb Opening Weir Equation			d _{Curb} =	0.33	0.44	ft
Combination Inlet Performance Reduction Factor for Long Inlets			RF _{Combination} =	0.57	0.69	
Curb Opening Performance Reduction Factor for Long Inlets			RF _{Curb} =	0.97	1.00]
Grated Inlet Performance Reduction Factor for Long Inlets			RF _{Grate} =	0.57	0.69	
			_	MINOR	MAJOR	_
Total Inlet Interception Cap	acity (assumes clogged condition))	$Q_a =$	6.4	11.0	cfs
Inlet Capacity IS GOOD for Minor	and Major Storms(>Q PEAK)		Q _{PEAK REQUIRED} =	3.9	7.9	cfs

SSA - Inlet Calcs.xlsm, IN-3 6/20/2019, 2:02 AM



Project Name: 10StormDesign

06-22-2019

Energy Grade Line Calculations Stormwater Studio 2019 v 1.0.0.0

	Enrgy	(#)	0.08	0.00	00.00	A - 5 yr.sws
Junction	EGLa Elev	(ft)	7121.17	7125.64	7120.60	Project File: Monument SSA - 5 yr.sws
7	HGLa Elev	(#)	7120.79	7125.32	7120.30	roject File: M
Pipe	Enrgy Loss	(#)	0.052	0.561	0.054	
	n Value		0.013	0.013	0.013	
	EGL Elev	(#)	7121.09	7125.64	7120.60	
	Vel Head	(#)	0.38	0.32	0.30	
	Vel	(ft/s)	4.92	4.51	4.39	
Upstream	HGL Elev	(#)	7120.71	7125.32	7120.30	
ר 	Area	(sqft)	1.48	0.93	68.0	
	Depth	(ft)	96.0	0.78²	0.75²	
	Invert Elev	(#)	7119.76	7124.54	7119.55	
կյճւ	ΙΘΊ	(#)	10.71	100.98	26.6	
	EGL Elev	(#)	7120.55	7122.35	7120.10	
	Vel Head	(ft)	0.74	96.0	0.064	
E	Vel	(ft/s)	6.88	7.85	6.42	
Downstream	HGL Elev	Œ	7119.96	7121.77	7119.61	itical.
Do	Area	(sdft)	1.06	0.53	0.0	Supercr
	Depth	(#)	0.74	0.51	0.56‡	epth. ‡
	Invert Elev	(#)	7119.22	7121.26	7119.05	² Critical depth. ‡ Supercritical.
	<u>م</u>	(cfs)	7.30	4.20	3.90	
Line	Size	(in)	24	18	8-	Notes: Return Period = 5-yrs.
Line	<u>و</u>		1	7	m	Notes: R

Project Name: 10StormDesign

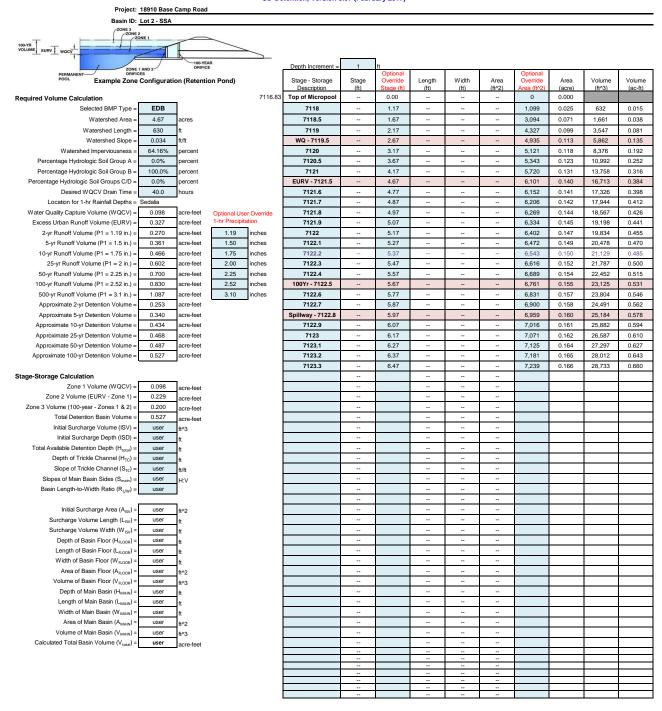
06-22-2019

Energy Grade Line Calculations Stormwater Studio 2019 v 1.0.0.0

APPENDIX C - DETENTION/WATER QUALITY ENHANCEMENT BMPs

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

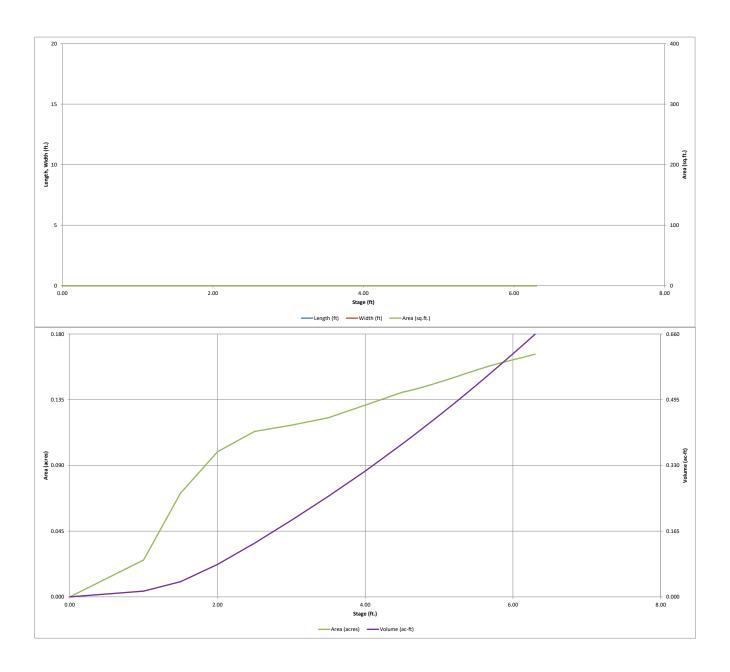
UD-Detention, Version 3.07 (February 2017)



Lot 2 - UD-Detention_v3.07.xlsm, Basin 6/20/2019, 6:57 PM

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

UD-Detention, Version 3.07 (February 2017)



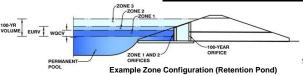
Lot 2 - UD-Detention_v3.07.xlsm, Basin 6/20/2019, 6:57 PM

Detention Basin Outlet Structure Design

UD-Detention, Version 3.07 (February 2017)

Project: Monument Steel Structures - PCD File No. PPR1919

Basin ID: 18910 Base Camp Road - El Paso County



	Stage (ft)	Zone Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	2.33	0.098	Orifice Plate
Zone 2 (EURV)	4.26	0.229	Orifice Plate
'one 3 (100-year)	5.65	0.200	Weir&Pipe (Circular)
'•		0.537	Tatal

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth = N/A ft (distance below the filtration media surface)
Underdrain Orifice Diameter = N/A inches

Calculated Parameters for Underdrain

Underdrain Orifice Area = N/A ft²

Underdrain Orifice Centroid = N/A feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice = 0.00 ft (relative to basin bottom at Stage = 0 ft)

Depth at top of Zone using Orifice Plate = 4.55 ft (relative to basin bottom at Stage = 0 ft)

Orifice Plate: Orifice Area per Row = N/A inches

Calcu	iateu Parailleters ioi	riate
WQ Orifice Area per Row =	N/A	ft ²
Elliptical Half-Width =	N/A	feet
Elliptical Slot Centroid =	N/A	feet
Elliptical Slot Area =	N/A	ft ²

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	2.17	2.42					
Orifice Area (sq. inches)	0.69	0.89	0.52					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

Not Selected	Not Selected	
N/A	N/A	ft (rela
N/A	N/A	ft (rela
N/A	N/A	inches
	N/A N/A	N/A N/A N/A

ft (relative to basin bottom at Stage = 0 ft)

 Calculated Parameters for Vertical Orifice

 Not Selected
 Not Selected

 Vertical Orifice Area =
 N/A
 N/A
 ft²

 Vertical Orifice Centroid =
 N/A
 N/A
 fee

User Input: Overflow Weir (Dropbox) and Grate (Flat or Sloped)

	Zone 3 Weir	Not Selected							
Overflow Weir Front Edge Height, Ho =	4.55	N/A	ft (relative to basin bottom at Stage = 0 ft)						
Overflow Weir Front Edge Length =	2.50	N/A	feet						
Overflow Weir Slope =	4.00	N/A	H:V (enter zero for flat grate)						
Horiz. Length of Weir Sides =	2.92	N/A	feet						
Overflow Grate Open Area % =	70%	N/A	%, grate open area/total area						
Debris Clogging % =	50%	N/A	%						

Calculated	_		
	Zone 3 Weir	Not Selected	
Height of Grate Upper Edge, H_t =	5.28	N/A	feet
Over Flow Weir Slope Length =	3.01	N/A	feet
Grate Open Area / 100-yr Orifice Area =	11.91	N/A	should be ≥ 4
Overflow Grate Open Area w/o Debris =	5.26	N/A	ft ²
Overflow Grate Open Area w/ Debris =	2.63	N/A	ft ²

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

	Zone 3 Circular	Not Selected	
Depth to Invert of Outlet Pipe =	0.33	N/A	ft (distance below basin bottom at Stage = 0 ft)
Circular Orifice Diameter =	9.00	N/A	inches

	Calculated Parameters	for Outlet Pipe w/ I	Flow Restriction Pla	ate
		Zone 3 Circular	Not Selected	
age = 0 ft)	Outlet Orifice Area =	0.44	N/A	ft^2
	Outlet Orifice Centroid =	0.38	N/A	feet
Half-Central An	gle of Restrictor Plate on Pipe =	N/A	N/A	radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

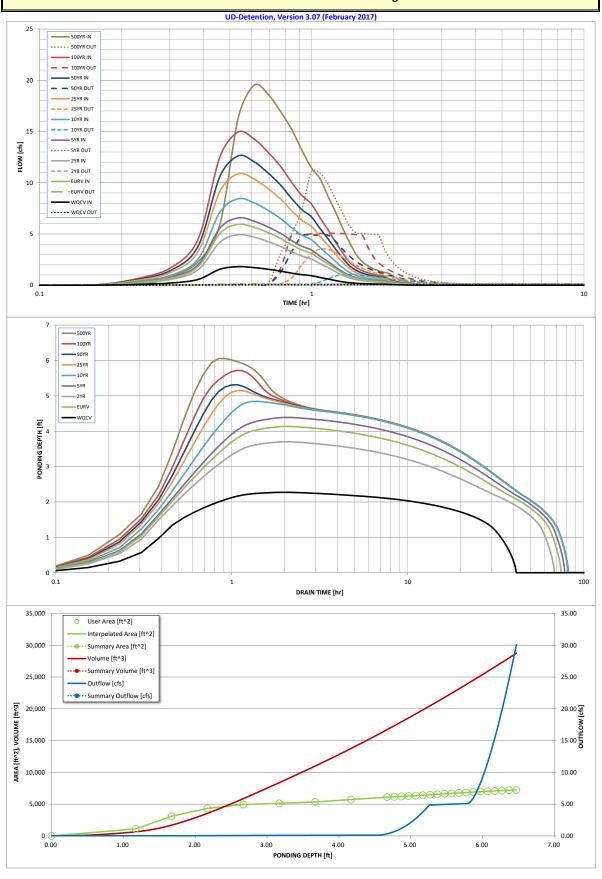
Freeboard ab

8 , , (
Spillway Invert Stage=	5.80	ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length =	15.00	feet
Spillway End Slopes =	0.00	H:V
oove Max Water Surface =	1.00	feet

Calcula	ted Parameters for S	pillway
Spillway Design Flow Depth=	0.47	feet
Stage at Top of Freeboard =	7.27	feet
asin Area at Top of Freeboard =	0.17	acres

Routed Hydrograph Results									
Design Storm Return Period =	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
One-Hour Rainfall Depth (in) =	0.53	1.07	1.19	1.50	1.75	2.00	2.25	2.52	3.10
Calculated Runoff Volume (acre-ft) =	0.098	0.327	0.270	0.361	0.466	0.602	0.700	0.830	1.087
OPTIONAL Override Runoff Volume (acre-ft) =									
Inflow Hydrograph Volume (acre-ft) =	0.098	0.326	0.270	0.361	0.465	0.602	0.700	0.831	1.088
Predevelopment Unit Peak Flow, q (cfs/acre) =	0.00	0.00	0.01	0.02	0.23	0.73	1.01	1.36	1.98
Predevelopment Peak Q (cfs) =	0.0	0.0	0.1	0.1	1.1	3.4	4.7	6.4	9.3
Peak Inflow Q (cfs) =	1.8	5.9	4.9	6.6	8.4	10.9	12.6	15.0	19.5
Peak Outflow Q (cfs) =	0.0	0.1	0.1	0.1	1.0	3.5	4.9	5.1	11.1
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	1.1	1.0	1.0	1.0	0.8	1.2
Structure Controlling Flow =	Plate	Plate	Plate	Plate	Overflow Grate 1	Overflow Grate 1	Outlet Plate 1	Outlet Plate 1	Spillway
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	N/A	0.2	0.6	0.9	0.9	1.0
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	39	68	62	71	72	71	69	68	65
Time to Drain 99% of Inflow Volume (hours) =	40	72	66	75	78	77	76	76	74
Maximum Ponding Depth (ft) =	2.27	4.13	3.70	4.39	4.84	5.15	5.31	5.72	6.06
Area at Maximum Ponding Depth (acres) =	0.10	0.13	0.12	0.13	0.14	0.15	0.15	0.16	0.16
Maximum Volume Stored (acre-ft) =	0.091	0.311	0.256	0.344	0.408	0.451	0.476	0.537	0.591

Detention Basin Outlet Structure Design



Forebay Design

	Tributary Area (ac)	Imp. Tributary Area (ac)	% Imp.	WQCV (in)	WQCV (ac-ft)	Forebay Vol (cf)	
North Forebay	1.55	1.04	66.9%	0.27	0.035	30.11	2% of WQCV
East Forebay	2.89	1.94	67.1%	0.27	0.065	56.42	2% of WQCV

 $WQCV = a(0.91I^3 - 1.19I^2 + 0.78I)$

Equation 3-1

Where:

WQCV = Water Quality Capture Volume (watershed inches)

a = Coefficient corresponding to WQCV drain time (Table 3-2)

I = Imperviousness (%/100) (see Figures 3-3 through 3-5 [single family land use] and /or the Runoff chapter of Volume 1[other typical land uses])

Table 3-2. Drain Time Coefficients for WQCV Calculations

Drain Time (hrs)	Coefficient, a
12 hours	0.8
24 hours	0.9
40 hours	1.0

Once the WQCV in watershed inches is found from Figure 3-2 or using Equation 3-1 and/or 3-2, the required BMP storage volume in acre-feet can be calculated as follows:

$$V = \left(\frac{\text{WQCV}}{12}\right)A$$
 Equation 3-3

Table EDB-4. EDB component criteria

	On-Site EDBs for Watersheds up to 1 Impervious Acre ¹	EDBs with Watersheds between 1 and 2 Impervious Acres ¹	EDBs with Watersheds up to 5 Impervious Acres	EDBs with Watersheds over 5 Impervious Acres	EDBs with Watersheds over 20 Impervious Acres
Forebay Release and Configuration		Release 2% of the undetained 100-year peak discharge by way of a wall/notch configuration	Release 2% of the undetained 100-year peak discharge by way of a wall/notch configuration	Release 2% of the undetained 100-year peak discharge by way of a wall/notch configuration	Release 2% of the undetained 100-year peak discharge by way of a wall/notch or berm/pipe ² configuration
Minimum Forebay Volume	EDBs should not be used for watersheds	1% of the WQCV	2% of the WQCV	3% of the WQCV	3% of the WQCV
Maximum Forebay Depth	with less than 1 impervious	12 inches	18 inches	18 inches	30 inches
Trickle Channel Capacity	acre.	≥ the maximum possible forebay outlet capacity	≥ the maximum possible forebay outlet capacity	≥ the maximum possible forebay outlet capacity	≥ the maximum possible forebay outlet capacity
Micropool		Area ≥ 10 ft ²			
Initial Surcharge Volume		Depth ≥ 4 inches	Depth ≥ 4 inches	Depth ≥ 4 in. Volume ≥ 0.3% WQCV	Depth ≥ 4 in. Volume ≥ 0.3% WQCV

¹ EDBs are not recommended for sites with less than 2 impervious acres. Consider a sand filter or rain

² Round up to the first standard pipe size (minimum 8 inches).

APPENDIX D - REFERENCED INFORMATION

NOTES TO USERS

This map is for use in administering the National Flood Insurance Program. It does not necessarily identify all areas subject to flooding, particularly from local drainage sources of small size. The community map repository should be consulted for possible updated or additional flood hazard information.

To obtain more detailed information in areas where Base Flood Elevations (BFEs) and/or floodways have been determined, users are encouraged to consult the Flood Profiles and Floodway Data and/or Summary of Stillwater Elevations tables contained within the Flood Insurance Study (FIS) report that accompanies this FIRM. Users should be aware that BFEs shown on the FIRM represent rounded whole-foot elevations. These BFEs are intended for flood insurance rating purposes only and should not be used as the sole source of flood elevation information. Accordingly, flood elevation data presented in the FIS report should be utilized in conjunction with the FIRM for purposes of construction and/or floodplain management.

Coastal Base Flood Elevations shown on this map apply only landward of 0.0' North American Vertical Datum of 1988 (NAVD88). Users of this FIRM should be aware that coastal flood elevations are also provided in the Summary of Stillwater Elevations table in the Flood Insurance Study report for this jurisdiction. Elevations shown in the Summary of Stillwater Elevations table should be used for construction and/or floodplain management purposes when they are higher than the elevations shown on

Boundaries of the floodways were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations with regard to requirements of the National Flood Insurance Program. Floodway widths and other pertinent floodway data are provided in the Flood Insurance Study report for this jurisdiction.

Certain areas not in Special Flood Hazard Areas may be protected by flood control structures. Refer to section 2.4 "Flood Protection Measures" of the Flood Insurance Study report for information on flood control structures for this jurisdiction.

The projection used in the preparation of this map was Universal Transverse Mercator (UTM) zone 13. The horizontal datum was NAD83, GRS80 spheroid. Differences in datum, spheroid, projection or UTM zones zones used in the production of FIRMs for adjacent jurisdictions may result in slight positional differences in map features across jurisdiction boundaries. These differences do not affect the accuracy of this FIRM.

Flood elevations on this map are referenced to the North American Vertical Datum of 1988 (NAVD88). These flood elevations must be compared to structure and ground elevations referenced to the same vertical datum. For information regarding conversion between the National Geodetic Vertical Datum of 1929 and the North American Vertical Datum of 1988, visit the National Geodetic Survey website at http://www.ngs.noaa.gov/ or contact the National Geodetic Survey at the following

NGS Information Services NOAA, N/NGS12 National Geodetic Survey SSMC-3, #9202 1315 East-West Highway Silver Spring, MD 20910-3282

To obtain current elevation, description, and/or location information for bench marks shown on this map, please contact the Information Services Branch of the National Geodetic Survey at (301) 713-3242 or visit its website at http://www.ngs.noaa.gov/.

Base Map information shown on this FIRM was provided in digital format by El Paso County, Colorado Springs Utilities, City of Fountain, Bureau of Land Management, National Oceanic and Atmospheric Administration, United States Geological Survey, and Anderson Consulting Engineers, Inc. These data are current as of 2006.

This map reflects more detailed and up-to-date stream channel configurations and floodplain delineations than those shown on the previous FIRM for this jurisdiction. The floodplains and floodways that were transferred from the previous FIRM may have been adjusted to conform to these new stream channel configurations. As a result, the Flood Profiles and Floodway Data tables in the Flood Insurance Study Report (which contains authoritative hydraulic data) may reflect stream channel distances that differ from what is shown on this map. The profile baselines depicted on this map represent the hydraulic modeling baselines that match the flood profiles and Floodway Data Tables if applicable, in the FIS report. As a result, the profile baselines may deviate significantly from the new base map channel representation and may appear outside of the floodplain.

Corporate limits shown on this map are based on the best data available at the time of publication. Because changes due to annexations or de-annexations may have occurred after this map was published, map users should contact appropriate community officials to verify current corporate limit locations.

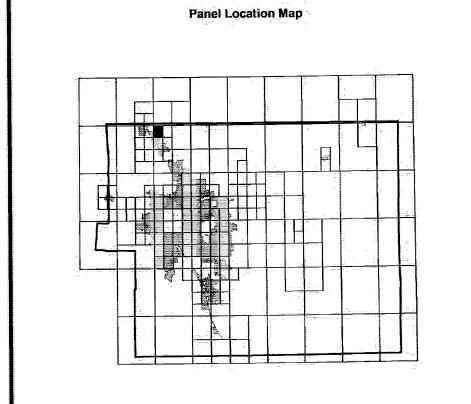
Please refer to the separately printed Map Index for an overview map of the county showing the layout of map panels; community map repository addresses; and a Listing of Communities table containing National Flood Insurance Program dates for each community as well as a listing of the panels on which each community is

Contact FEMA Map Service Center (MSC) via the FEMA Map Information eXchange (FMIX) 1-877-336-2627 for information on available products associated with this FIRM. Available products may include previously issued Letters of Map Change, a Flood Insurance Study Report, and/or digital versions of this map. The MSC may also be reached by Fax at 1-800-358-9620 and its website at http://www.msc.fema.gov/.

f you have questions about this map or questions concerning the National Flood Insurance Program in general, please call 1-877-FEMA MAP (1-877-336-2627) or risit the FEMA website at http://www.fema.gov/business/nfip. El Paso County Vertical Datum Offset Table

Vertical Datum

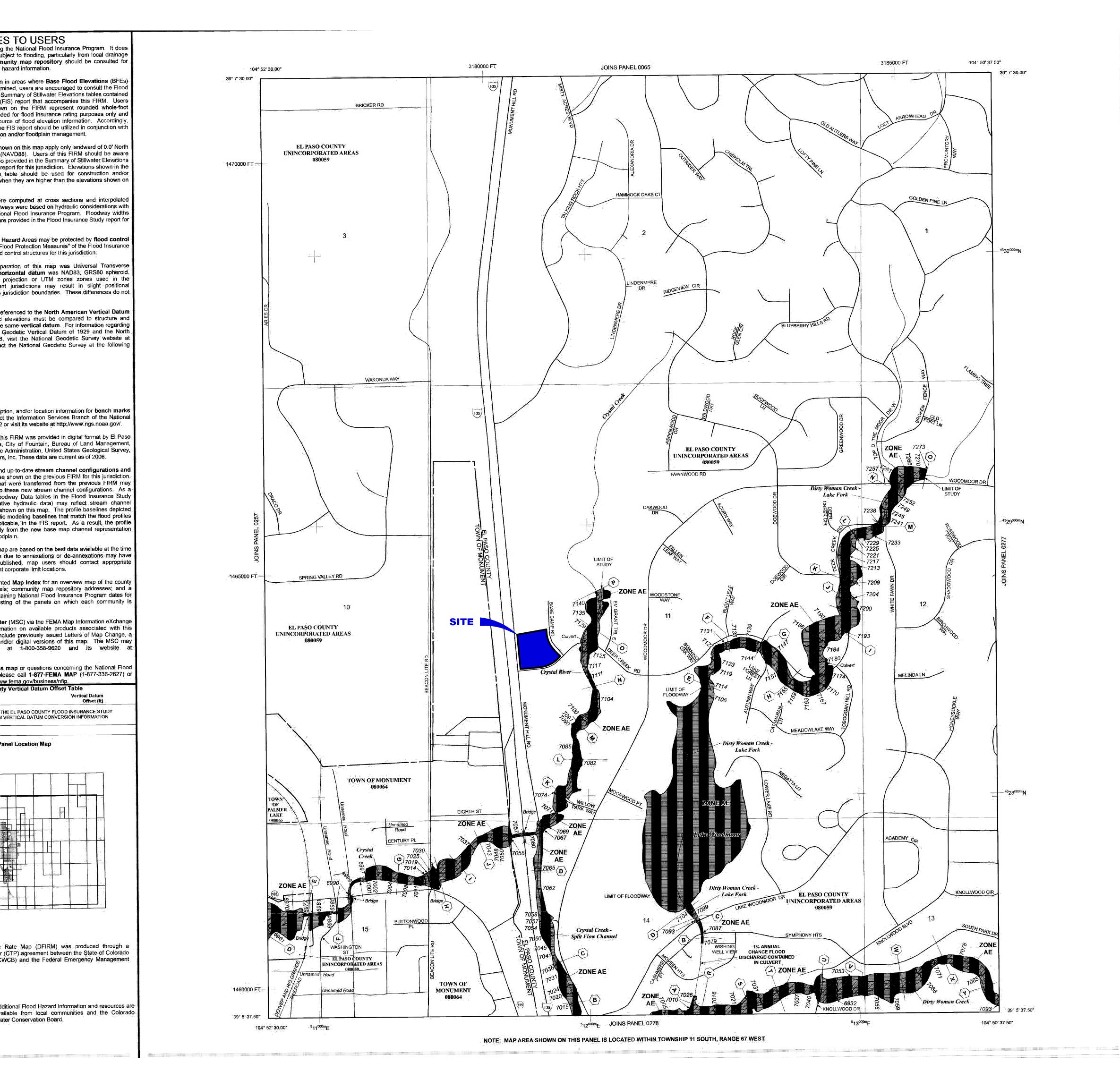
REFER TO SECTION 3.3 OF THE EL PASO COUNTY FLOOD INSURANCE STUDY FOR STREAM BY STREAM VERTICAL DATUM CONVERSION INFORMATION



This Digital Flood Insurance Rate Map (DFIRM) was produced through a Cooperating Technical Partner (CTP) agreement between the State of Colorado Water Conservation Board (CWCB) and the Federal Emergency Management Agency (FEMA).



Additional Flood Hazard information and resources are available from local communities and the Colorado Water Conservation Board.



LEGEND

SPECIAL FLOOD HAZARD AREAS (SFHAS) SUBJECT TO INUNDATION BY THE 1% ANNUAL CHANCE FLOOD

The 1% annual chance flood (100-year flood), also known as the base flood, is the flood that has a 1% chance of being equaled or exceeded in any given year. The Special Flood Hazard Area is the area subject to flooding by the 1% annual chance flood. Areas of Special Flood Hazard include Zones A, AE, AH, AO, AR, A99, V, and VE. The Base Flood

Elevation is the water-surface elevation of the 1% annual chance flood.

ZONE A No Base Flood Elevations determined. ZONE AE Base Flood Elevations determined.

ZONE AH Flood depths of 1 to 3 feet (usually areas of ponding); Base Flood

ZONE AO Flood depths of 1 to 3 feet (usually sheet flow on sloping terrain); average depths determined. For areas of alluvial fan flooding, velocities also

ZONE AR Special Flood Hazard Area Formerly protected from the 1% annual chance flood by a flood control system that was subsequently decertified. Zone AR indicates that the former flood control system is being restored to provide protection from the 1% annual chance or greater flood

ZONE A99 Area to be protected from 1% annual chance flood by a Federal flood protection system under construction; no Base Flood Elevations

Coastal flood zone with velocity hazard (wave action); no Base Flood Elevations determined.

Coastal flood zone with velocity hazard (wave action); Base Flood

FLOODWAY AREAS IN ZONE AE

The floodway is the channel of a stream plus any adjacent floodplain areas that must be kept free of encroachment so that the 1% annual chance flood can be carried without substantial increases in flood heights.

OTHER FLOOD AREAS

Areas of 0.2% annual chance flood; areas of 1% annual chance flood with average depths of less than 1 foot or with drainage areas less than 1 square mile; and areas protected by levees from 1% annual chance flood.

OTHER AREAS

Areas determined to be outside the 0.2% annual chance floodplain. Areas in which flood hazards are undetermined, but possible.

COASTAL BARRIER RESOURCES SYSTEM (CBRS) AREAS

OTHERWISE PROTECTED AREAS (OPAs)

CBRS areas and OPAs are normally located within or adjacent to Special Flood Hazard Areas.

Floodplain boundary Floodway boundary Zone D Boundary

********* CBRS and OPA boundary

Boundary dividing Special Flood Hazard Areas of different Base Flood Elevations, flood depths or flood velocities. Base Flood Elevation line and value; elevation in feet* ~~ 513 ~~

Base Flood Elevation value where uniform within zone;

elevation in feet* * Referenced to the North American Vertical Datum of 1988 (NAVD 88)

(EL 987)

Geographic coordinates referenced to the North American 32° 22' 30.00" Datum of 1983 (NAD 83) 1000-meter Universal Transverse Mercator grid ticks, 4275000mN

5000-foot grid ticks: Colorado State Plane coordinate

system, central zone (FIPSZONE 0502), Lambert Conformal Conic Projection

Bench mark (see explanation in Notes to Users section of DX5510

River Mile

Refer to Map Repositories list on Map Index

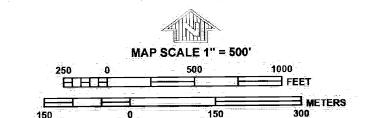
EFFECTIVE DATE OF COUNTYWIDE FLOOD INSURANCE RATE MAP MARCH 17, 1997

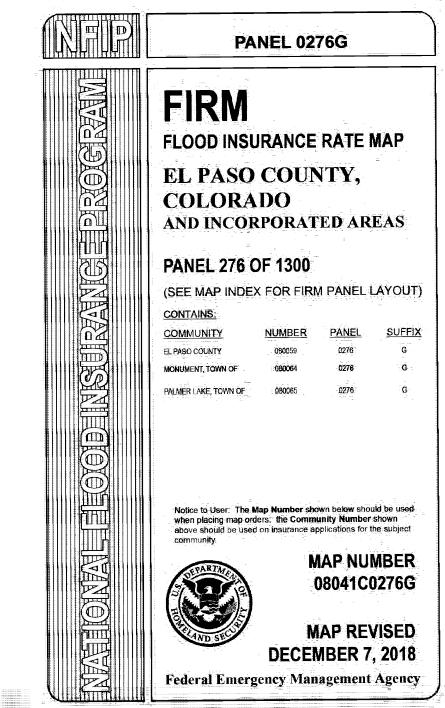
EFFECTIVE DATE(S) OF REVISION(S) TO THIS PANEL DECEMBER 7, 2018 - to update corporate limits, to change Base Flood Elevations and Special Flood Hazard Areas, to update map format, to add roads and road names, and to incorporate previously issued Letters of Map Revision.

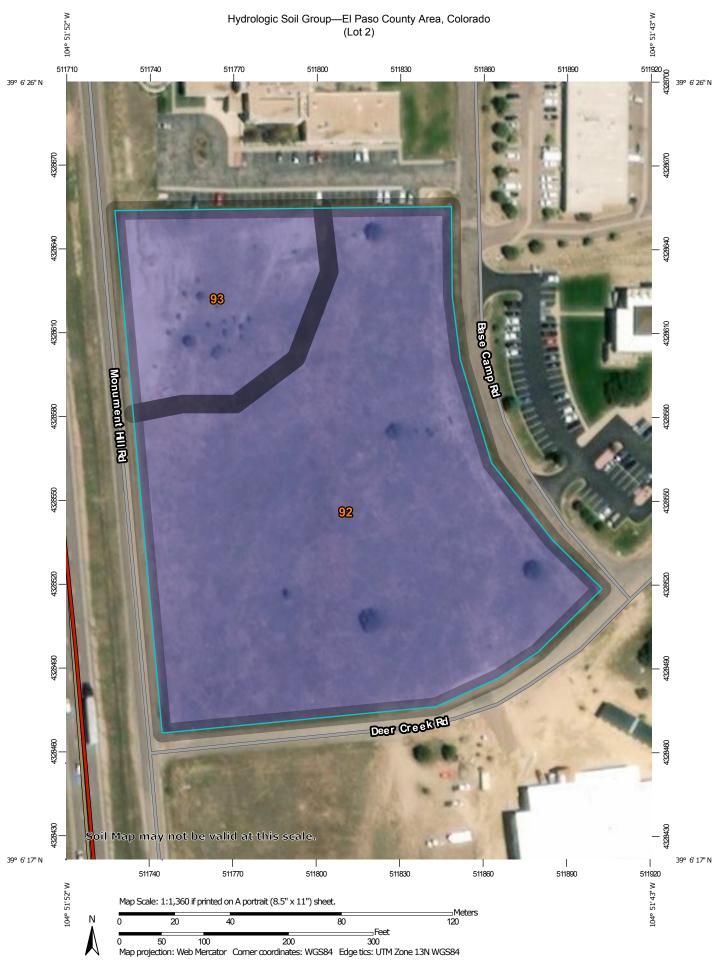
For community map revision history prior to countywide mapping, refer to the Community

Map History Table located in the Flood Insurance Study report for this jurisdiction.

To determine if flood insurance is available in this community, contact your insurance agent or call the National Flood Insurance Program at 1-800-638-6620.







MAP LEGEND MAP INFORMATION The soil surveys that comprise your AOI were mapped at Area of Interest (AOI) С 1:24.000. Area of Interest (AOI) C/D Soils Warning: Soil Map may not be valid at this scale. D **Soil Rating Polygons** Enlargement of maps beyond the scale of mapping can cause Not rated or not available Α misunderstanding of the detail of mapping and accuracy of soil **Water Features** line placement. The maps do not show the small areas of A/D Streams and Canals contrasting soils that could have been shown at a more detailed В Transportation B/D Rails ---Please rely on the bar scale on each map sheet for map measurements. Interstate Highways C/D Source of Map: Natural Resources Conservation Service **US Routes** Web Soil Survey URL: D Major Roads Coordinate System: Web Mercator (EPSG:3857) Not rated or not available -Local Roads Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts Soil Rating Lines Background distance and area. A projection that preserves area, such as the Aerial Photography Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required. This product is generated from the USDA-NRCS certified data as of the version date(s) listed below. B/D Soil Survey Area: El Paso County Area, Colorado Survey Area Data: Version 16, Sep 10, 2018 C/D Soil map units are labeled (as space allows) for map scales 1:50,000 or larger. D Not rated or not available Date(s) aerial images were photographed: Jul 4, 2010—Oct 16, 2017 **Soil Rating Points** The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background A/D imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident. B/D

Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
92	Tomah-Crowfoot loamy sands, 3 to 8 percent slopes	В	4.7	80.6%
93	Tomah-Crowfoot complex, 8 to 15 percent slopes	В	1.1	19.4%
Totals for Area of Interest			5.9	100.0%

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

Rating Options

Aggregation Method: Dominant Condition
Component Percent Cutoff: None Specified

Tie-break Rule: Higher

El Paso County Drainage Basin Fees Resolution No. 18-470

Basin Number	Receiving Waters	Year Studied	Drainage Basin Name	2019 Drainage Fee (per Impervious Acre)	2019 Bridge Fee (per Impervious Acre)
Drainage Basins wit	Mark Control	Studied		(per limpervious Acre)	(per impervious zere)
		0040	Manalan Danah	E10 224	£1 624
CHMS0200	Chico Creek	2013	Haegler Ranch	\$10,324 \$11,559	\$1,524 \$4,433
CHWS1200	Chico Creek	2001	Bennett Ranch	\$11,558 \$29,622	\$4,069
CHWS1400	Chico Creek	2013	Falcon	\$12,564	\$3,717
OFO2000	Fountain Creek	2001 1991*	West Fork Jimmy Camp Creek Big Johnson / Crews Gulch	\$18,350	\$2,370
OFO2600	Fountain Creek Fountain Creek	1988*	Widefield	\$18,350	\$0
FOFO2800 FOFO2900	Fountain Creek	1988*	Security	\$18,350	\$0
FOFO3000	Fountain Creek	1991*	Windmill Gulch	\$18,350	\$275
FOFO3100 / FOFO3200		1988*	Carson Street / Little Johnson	\$11,192	\$0
FOFO3400	Fountain Creek	1984*	Peterson Field	\$13,235	\$1,004
FOFO3600	Fountain Creek	1991*	Fisher's Canyon	\$18,350	\$0
FOFO4000	Fountain Creek	1996	Sand Creek	\$18,940	\$5,559
FOFO4200	Fountain Creek	1977	Spring Creek	\$9,517	\$0
FOFO4600	Fountain Creek	1984*	Southwest Area	\$18,350	\$0
FOFO4800	Fountain Creek	1991	Bear Creek	\$18,350	\$1,004
FOFO5400	Fountain Creek	1977	21st Street	\$5,521	\$0
FOFO5600	Fountain Creek	1964	19th Street	\$3,611	\$0
FOFO5800	Fountain Creek	1964	Camp Creek	\$2,033	\$0
FOMO0400	Monument Creek	1986*	Mesa	\$9,598	\$0
FOMO1000	Monument Creek	1981	Douglas Creek	\$11,540	\$255
FOMO1200	Monument Creek	1977	Templeton Gap	\$11,847	\$275
FOMO1400	Monument Creek	1976	Pope's Bluff	\$3,676	\$627
FOMO1600	Monument Creek	1976	South Rockrimmon	\$4,314	\$0
FOMO1800	Monument Creek	1973	North Rockrimmon	\$5,521	\$0
OMO2000	Monument Creek	1971	Pulpit Rock	\$6,085	\$0
FOMO2200	Monument Creek	1994	Cottonwood Creek / S. Pine	\$18,350	\$1,004
OMO2400	Monument Creek	1966	Dry Creek	\$14,486	\$524
FOMO3600	Monument Creek	1989*	Black Squirrel Creek	\$8,331	\$524
FOMO3700	Monument Creek	1987*	Middle Tributary	\$15,312	\$0
FOMO3800	Monument Creek	1987*	Monument Branch	\$18,350	\$0
FOMO4000	Monument Creek	1996	Smith Creek	\$7,481	\$1,004
FOMO4200	Monument Creek	1989*	Black Forest	\$18,350	\$500
FOMO5200 FOMO5300	Monument Creek Fountain Creek	1993* 1993*	Dirty Woman Creek Crystal Creek	\$18,350 \$18,350	\$1,004 \$1,004
		1993	Crystal Creek	ψ10,550	\$ 1,00 T
Miscellaneous Drair					
CHBS0800	Chico Creek		Book Ranch	\$17,217	\$2,492
CHEC0400	Chico Creek		Upper East Chico	\$9,380	\$272
CHWS0200	Chico Creek		Telephone Exchange	\$10,306	\$241
CHWS0400	Chico Creek		Livestock Company	\$16,976	\$202
CHWS0600	Chico Creek		West Squirrel	\$8,849	\$3,672
CHWS0800	Chico Creek		Solberg Ranch	\$18,350	\$0 \$0
FOFO1200	Fountain Creek		Crooked Canyon	\$5,540	\$0 \$270
FOFO1400	Fountain Creek		Calhan Reservoir	\$4,625 \$3,343	\$270 \$0
FOFO1600	Fountain Creek		Sand Canyon	\$3,342	
FOFO2000	Fountain Creek		Jimmy Camp Creek ^J	\$18,350	\$858
FOFO2200	Fountain Creek		Fort Carson	\$14,486	\$524
FOFO2700	Fountain Creek		West Little Johnson	\$1,209	\$0
	Fountain Creek		Stratton	\$8,801	\$394
FOFO5000	Fountain Creek		Midland	\$14,486	\$524
FOFO5000 FOFO6000	Fountain Creek Fountain Creek		Palmer Trail	\$14,486	\$524
FOFO5000 FOFO6000 FOFO6800	Fountain Creek Fountain Creek Fountain Creek		Palmer Trail Black Canyon	\$14,486 \$14,486	\$524 \$524
FOFO5000 FOFO6000 FOFO6800 FOMO4600	Fountain Creek Fountain Creek Fountain Creek Monument Creek		Palmer Trail Black Canyon Beaver Creek	\$14,486 \$14,486 \$10,970	\$524 \$524 \$0
FOFO5000 FOFO6000 FOFO6800 FOMO4600 FOMO3000	Fountain Creek Fountain Creek Fountain Creek Monument Creek Monument Creek		Palmer Trail Black Canyon Beaver Creek Kettle Creek	\$14,486 \$14,486 \$10,970 \$9,909	\$524 \$524 \$0 \$0
FOFO5000 FOFO6000 FOFO6800 FOMO4600 FOMO3000 FOMO3400	Fountain Creek Fountain Creek Fountain Creek Monument Creek Monument Creek Monument Creek		Palmer Trail Black Canyon Beaver Creek Kettle Creek Eikhom	\$14,486 \$14,486 \$10,970 \$9,909 \$1,665	\$524 \$524 \$0 \$0 \$0
FOFO5000 FOFO6000 FOFO6800 FOMO4600 FOMO3400 FOMO3400 FOMO5000	Fountain Creek Fountain Creek Fountain Creek Monument Creek Monument Creek Monument Creek Monument Creek		Palmer Trail Black Canyon Beaver Creek Kettle Creek Elkhorn Monument Rock	\$14,486 \$14,486 \$10,970 \$9,909 \$1,665 \$7,953	\$524 \$524 \$0 \$0 \$0 \$0
FOFO5000 FOFO6000 FOFO6800 FOMO3000 FOMO3000 FOMO5000 FOMO5000	Fountain Creek Fountain Creek Fountain Creek Monument Creek Monument Creek Monument Creek Monument Creek Monument Creek		Palmer Trail Black Canyon Beaver Creek Kettle Creek Elkhorn Monument Rock Palmer Lake	\$14,486 \$14,486 \$10,970 \$9,909 \$1,665 \$7,953 \$12,717	\$524 \$524 \$0 \$0 \$0 \$0 \$0
FOFO5000 FOFO6000 FOFO6800 FOMO3000 FOMO3400 FOMO5400 FOMO5400 FOMO5600	Fountain Creek Fountain Creek Fountain Creek Monument Creek Monument Creek Monument Creek Monument Creek Monument Creek Monument Creek		Palmer Trail Black Canyon Beaver Creek Kettle Creek Elkhom Monument Rock Palmer Lake Raspberry Mountain	\$14,486 \$14,486 \$10,970 \$9,909 \$1,665 \$7,953 \$12,717 \$4,278	\$524 \$524 \$0 \$0 \$0 \$0 \$0 \$0
FOFO5000 FOFO6000 FOFO6800 FOMO3000 FOMO3400 FOMO5000 FOMO5400 FOMO5600 PLPL0200	Fountain Creek Fountain Creek Fountain Creek Monument Creek Monument Creek Monument Creek Monument Creek Monument Creek Monument Creek Monument Creek		Palmer Trail Black Canyon Beaver Creek Kettle Creek Elkhorn Monument Rock Palmer Lake	\$14,486 \$14,486 \$10,970 \$9,909 \$1,665 \$7,953 \$12,717	\$524 \$524 \$0 \$0 \$0 \$0 \$0
FOFO5000 FOFO6000 FOFO6800 FOMO3000 FOMO3000 FOMO5000 FOMO5400 FOMO5600 PLPL0200	Fountain Creek Fountain Creek Monument Creek		Palmer Trail Black Canyon Beaver Creek Kettle Creek Eikhorn Monument Rock Palmer Lake Raspberry Mountain Bald Mountain	\$14,486 \$14,486 \$10,970 \$9,909 \$1,665 \$7,953 \$12,717 \$4,278 \$9,116	\$524 \$524 \$0 \$0 \$0 \$0 \$0 \$0
FOFO3800 FOFO3800 FOFO6000 FOFO6800 FOMO4600 FOMO3000 FOMO5400 FOMO5400 FOMO5600 PLPL0200 Interim Drainage Ba FOFO1800 FOMO4400	Fountain Creek Fountain Creek Fountain Creek Monument Creek Monument Creek Monument Creek Monument Creek Monument Creek Monument Creek Monument Creek		Palmer Trail Black Canyon Beaver Creek Kettle Creek Elkhom Monument Rock Palmer Lake Raspberry Mountain	\$14,486 \$14,486 \$10,970 \$9,909 \$1,665 \$7,953 \$12,717 \$4,278	\$524 \$524 \$0 \$0 \$0 \$0 \$0 \$0

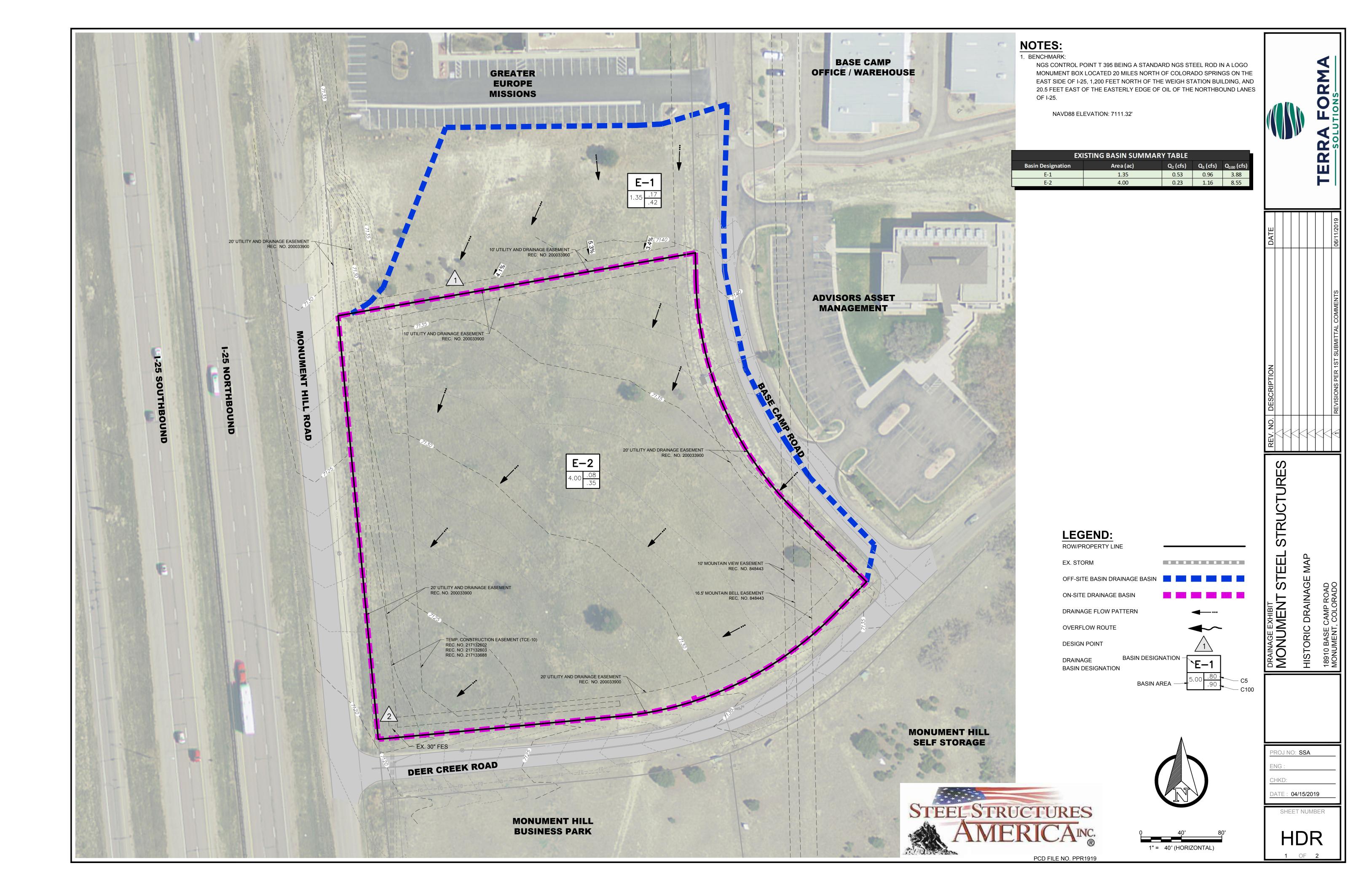
^{1.} The miscellaneous drainage fee previous to September 1999 resolution was the average of all drainage fees for basins with Basin Planning Studies perform

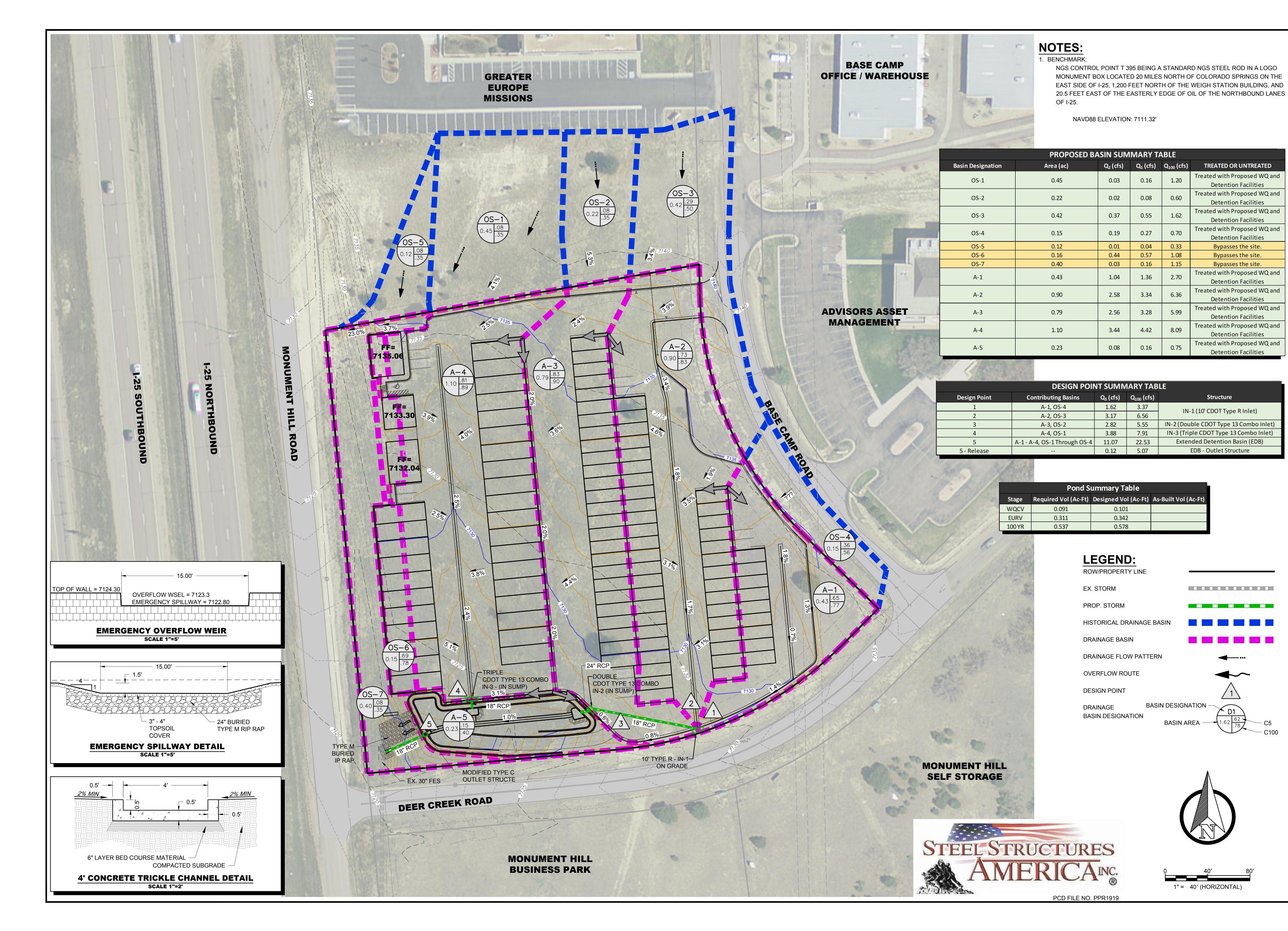
EPC Stormwater Management	Jennifer Irvine, P.E.	

^{2.} Interim Drainage Fees are based upon draft Drainage Basin Planning Studies or the Drainage Basin Identification and Fee Estimation Report. (Best available

^{3.} This is an interim fee and will be adjusted when a DBPS is completed. In addition to the Drainage Fee a surety in the amount of \$7,285 per impervious acre shifted DBPS results in a fee greater than the current fee. Fees paid in excess of the future revised fee will be reimbursed. See Resolution 06-326 (9/14/06) and Resolution 06-326 (9/14/06) an

APPENDIX E - DRAINAGE MAPS







TERRA FORM,

REVISIONS PER 1ST SUBMITTAL COMMENTS 06

MENT STEEL STRUCTUR

MONUMENT ST
PROPOSED DRAINAG

PROJ NO: SSA ENG:

CHKD: DATE: **04/15/2019**

SHEET NUMBER

PDR 2 OF 2

Drainage Report_v2-redline.pdf Markup Summary

dsdlaforce (3)



Subject: Callout Page Label: 7 Lock: Unlocked Author: dsdlaforce Date: 7/8/2019 10:09:08 AM

Status: Color: Layer: Space:

Remove the deviation request. The ECM has recently been updated to incorporate the exclusions from the MS4 permit. See the exclusion provision of the ECM. Verify if Appendix I Section I.7.1.C.1.a would be applicable. Update the narrative accordingly by discussing the

applicable exclusion.

Remove.

Proposed Stormwat An Extended Detention storm runoff and attenu criteria and UDFCD.

Subject: Callout Page Label: 10 Lock: Unlocked Author: dsdlaforce

Date: 7/8/2019 10:12:25 AM

Status: Color: Layer: Space:

The Extended Detention

Subject: Callout Page Label: 12

Status: Color: Layer: Space:

Lock: Unlocked Author: dsdlaforce

Date: 7/8/2019 10:17:44 AM

Deviation request does not appear to be required anymore with the recently updated ECM.

Remove or update to discuss the applicable exclusion. See comment on

page 6 of 12.