PCD-ENGINEERING REVIEW COMMENTS IN BLUE BOXES WITH BLUE TEXT



PRELIMINARY DRAINAGE REPORT

GRANDVIEW RESERVE

El Paso County, Colorado

PREPARED FOR: D.R. Horton 9555 S. Kingston Court Englewood, CO

PREPARED BY:

Galloway & Company, Inc. 1155 Kelly Johnson Blvd., Suite 305 Colorado Springs, CO 80920

DATE:

August 11, 2021

Add text: PCD Filing No.: PUDSP2110

Engineering Review

EPC Planning & Community Development Department

Cursory comments - see comment letter also.



ENGINEER'S STATEMENT

to the best of n established by plan of the drai	Irainage plan and report were prepared by knowledge and belief. Said drainage the County for drainage reports and sai inage basin. I accept responsibility for a my part in preparing this report.	report has been prepared accordi d report is in conformity with the a	ing to the criteria applicable master
	am, PE #36727	 Date	_
For and on ber	nalf of Galloway & Company, Inc.		
DEVELOPER'	S CERTIFICATION		
I, The develope and plan.	er, have read and will comply with all of	the requirements specified in this	drainage report
Ву:			_
Address:	D.R. Horton 9555 S. Kingston Court Englewood, CO	Date	
EL PASO COL	JNTY CERTIFICATION		
	ance with the requirements of the Drain ering Criteria Manual and Land Develop	-	nd 2, El Paso
Jennifer Irvine, County Engine	P.E. er/ECM Administrator	 Date	_

Conditions:

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I. Purpose

The purpose of this Preliminary Drainage Report is to identify on and offsite drainage patterns, locate and identify tributary or downstream drainage features and facilities that impact the site, and to identify which types of drainage facilities will be needed and where they will be located. This report will remain in general compliance with the approved MDDP prepared by HR Green, dated November 2020.

II. General Description

the proposed extension of

The project is a single-family residential development located in the Falcon area of El Paso County, Colorado. The site is located in a portion of the South half of Section 21, the North half of Section 28, Township 12 South, Range 64 West of the 6th Principal Meridian, County of El Paso, State of Colorado. The subject property is bounded by Eastonville Road to the west, Rex Road to the north, undeveloped land proposed as future development to the east, and undeveloped land to the south. A Vicinity Map is included in **Appendix A**.

development)

This preliminary drainage report was the basis for the drainage facility design contained within the previously approved MDDP for the site prepared by HR Green. The site consists of approximately 182.61 acres and includes 568 dwelling units.

this is confusing

The existing soil types within the proposed site as determined by the NRCS Web Soil Survey for El Paso County Area consist of Columbine gravelly sandy loam (hydrologic soil group A) and Stapleton sandy loam (hydrologic soil group B). See the soils map included in **Appendix A**.

189.5?

III. Drainage Criteria

Hydrology calculations were performed using the City of Colorado Springs/El Paso County Drainage Criteria Manual, as revised in November 1991 and October 1994 with County adopted Chapter 6 and Section 3.2.1 of Chapter 13 of the City of Colorado Springs/El Paso County Drainage Criteria Manual as revised in May 2014.

The drainage calculations were based on the criteria manual Figure 6-5 and IDF equations to determine the intensity and are listed in Table 1 below.

Table 1 - Precipitation Data

Return Period	One Hour Depth (in).	Intensity (in/hr)
5-year	1.50	5.17
100-year	2.52	8.68

The rational method was used to calculate peak flows as the tributary areas are less than 100 acres. The rational method has been proven to be accurate for basins of this size and is based on the following formula:

Q = CIA

Where:

Q = Peak Discharge (cfs)

C = Runoff Coefficient

I = Runoff intensity (inches/hour)

A = Drainage area (acres)

The runoff coefficients are calculated based on land use, percent imperviousness, and design storm for each basin, as shown in the drainage criteria manual (Table 6-6). Composite percent impervious and C values were calculated using the residential, streets, roofs, and lawns coefficients found in Table 6-6 of the manual.

The 100-year event was used as the major storm event. The 5-year event was used as the minor event. The UD-Inlets v5.01 spreadsheet was utilized for the sizing of the proposed sump inlets.

The UD-Detention v4.04 spreadsheet was utilized for the design of the proposed on-site water quality ponds, Ponds A, B, C, D, E.

IV. Existing Drainage Conditions

Address the additional culvert

The site is contained fully within one major drainage basin; the Gieck Ranch Drainage Basin and is tributary to Black Squirrel Creek. The site generally drains from north to south with an average slope of 2% outside of the channel. The rational method was used to analyze the individual basins within the site because their size permits it.

There are two (2) major drainage ways the currently convey existing on & off-site flows through the site – these are the Main Stem (MS) and Main Stem Tributary Number 2 (MST). Both drainageways generally flow to the southeast to Highway 24, before crossing via existing drainage structures. Currently, these channels receive flows from two off-site basins, one from the west and the other from the north and are routed under Eastonville Road via existing pipe culverts.

An existing basin map has been prepared for this site to analyze the existing basins as well as the offsite basins contributing to the site. The existing map is included in **Appendix F** and basins are described below.

Basin EX-1 (105.72 AC, Q5 = 22.3 cfs, Q100 = 159.1 cfs): Located on the southwest portion of the site, this basin consists of un-developed land. Runoff from this basin will sheet flow to the southeast before channelizing and eventually out falling into Main Stem channel **(DP 1)**.

Basin EX-2 (57.68 AC, Q5 = 13.1 cfs, Q100 = 93.4 cfs): Located on the northeast portion of the site, this basin consists of un-developed land. Runoff from this basin will sheet flow to the southeast before channelizing and eventually out falling into Main Stem Tributary #2 channel (**DP 2**).

Basin EX-3 (23.35 AC, Q5 = 6.8 cfs, Q100 = 48.4 cfs): Located on the southeast portion of the site, this basin consists of un-developed land. Runoff from this basin will sheet flow to the southeast before channelizing and eventually out falling into Main Stem Tributary #2 channel (**DP 3**).

Based on the MDDP there should be at least 7 onsite and offsite existing basins

V. **Four Step Process**

The Four Step Process is used to minimize the adverse impacts of urbanization and is a vital component of developing a balanced, sustainable project. Below identifies the approach to the four-step process:

Employ Runoff Reduction Practices

This step uses low impact development (LID) practices to reduce runoff at the source. Generally, rather than creating point discharges that are directly connected to impervious areas runoff is routed through pervious areas to promote infiltration. The Impervious Reduction Factor (IRF) method was used and calculations can be found in Appendix E.

2. Stabilize Channels

This step implements stabilization to channels to accommodate developed flows while protecting infrastructure and controlling sediment loading from erosion in the drainageways. Erosion protection in the form of riprap pads at all outfall points to the channel to prevent scouring of the channel from point discharges. The existing channel analysis and design is to be completed by others and a separate report for the major channels will be submitted for review. provide when

3. Provide Water Quality Capture Volume (WQCV)

This step utilizes formalized water quality capture volume to slow the release of runoff from the site. The EURV volume will release in 72 hours, while the WQCV will release in no less than 40 hours. Onsite water quality control volume detention ponds will provide water quality treatment for all of the developed areas, prior to the runoff being released into either of the major drainage ways. Refer to WQCV Plan in Appendix F.

Consider Need for Industrial and Commercial BMPs 4.

As this project is all residential development and no commercial or industrial development is proposed, there will be no need for any specialized BMPs which would be associated with an industrial or commercial site.

VI. **Proposed Drainage Conditions**

MDDP? (There is

available

The proposed development lies completely within the Gieck Drainage Basin and consists of six (6) basins. Site runoff will be collected via inlets & pipes and diverted to one of the five proposed full spectrum detention ponds. All necessary calculations can be found within the appendices of the report.

According to the DBP sthere are two major channels that run through the site. As was discussed within the Existing Conditions portion of the report both the Main Stem (MS) and Main Stem Tributary Number 2 (MST) run through the site. There are no proposed major channel improvements for MS -however, MST is proposed to be re-routed. The analysis for both channels and design of MST were done by others and a separate report will be submitted for review for all channel improvements.

The site will provide five (5) WQCV Detention Ponds, Pond A, B, C, D, & E, to provide water quality treatment prior to discharging the runoff directly into either the MS or MST Channel.

As has been mentioned previously, the site is proposed to be single family residential. The site will consist primarily of 1/8 Acre lots, with some 1/4 Acre and 1/3 Acre lots, public roadways, along with dedicated Tracts for amenity and/or institutional uses.

> address the flow from the additional culvert in both existing and proposed conditions

Grandview Reserve PDR

Please state that (per your drainage map) that this basin is excluded from WQ per ECM App I.7.1.B.7. And that WQ will be addressed with the future development of the institutional site.

needs to be treated when constructed

The proposed institutional use area flows have not been included in this analysis. It is anticipated that the lot will not be developed until after construction of the proposed site. This area will need to submit a separate drainage report prior to development. Installation of a separate storm sewer system for the tract may be required. The development is responsible for ensuring the site drainage, once constructed, will not negatively impact any adjacent development. Water quality for this area will need to be included in the future site drainage design for the area.

Provide preliminary design with assumptions.

Basin-1 (1.40 AC, Q5 = 4.8 cfs, Q100 = 9.7 cfs): Located on the northwest border of the site, Basin-1 contains the proposed Phase 1 improvements to Rex Rd. This drainage basin consists entirely of off-site areas tributary to the project site. Runoff from this basin will sheet flow to the proposed curb & gutter along Rex Rd. The flows will then be routed to the east where they will discharge directly into main stem tributary #2 channel. It is anticipated that these flows will be captured and treated further downstream when the next segment of Rex Rd. is constructed.

Rex Road is part of the site

Basin A-1 (11.23 AC, Q5 = 3.9 cfs, Q100 = 27.5 cfs): Located on the northwest corner of the site, East of Eastonville Rd. & south of Rex Rd. This drainage basin is proposed future development to include an institutional site. Runoff from this basin will sheet flow from the northwest to the southeast, to a proposed CDOT Type 'C' inlet on the west side of Road V (DP 1). Flows will then be routed under Road V, via 24" RCP, to the updated Main Stem Tributary 2 channel.

provide developed design assumptions and preliminary pond sizing and location Basin A-2 (6.94 AC, Q5 = 13.2 cfs, Q100 = 29.7 cfs): Located on the north portion of the site, this basin

Basin A-2 (6.94 AC, Q5 = 13.2 cfs, Q100 = 29.7 cfs): Located on the north portion of the site, this basin consists of residential lots, Road G, Road V, and a portion of the north half of Road F. Runoff from this basin will sheet flow from the lots to the adjacent road. Flows will then be routed, via curb & gutter, to a proposed (public) CDOT Type 'R' inlet in sump conditions, located on the northeast side of the intersection of Road V and Road F (**DP 2**).

Basin A-3 (0.34 AC, Q5 = 1.6 cfs, Q100 = 3.0 cfs): Located on the north portion of the site, this basin consists of a portion of the south half of Road F. Flows will be routed, via curb & gutter, to a proposed (public) CDOT Type 'R' inlet in sump conditions, located on the southeast side of the intersection of Road V and Road F (**DP 3**).

Basin A-4 (10.15 AC, Q5 = 19.8 cfs, Q100 = 45.1 cfs): Located on the north portion of the site, this basin consists of residential lots, Road H, Road I, and a portion of the west half of Road F. Runoff from this basin will sheet flow from the lots to the adjacent road. Flows will then be routed, via curb & gutter, to a proposed (public) CDOT Type 'R' inlet in sump conditions, located on the west side of Road F (DP 4), between Road H and Road I. Address where overflows will go

Basin A-5 (0.34 AC, Q5 = 1.6 cfs, Q100 = 3.0 cfs): Located on the north portion of the site, this basin consists of a portion of the east half of Road F. Flows will be routed, via curb & gutter, to a proposed (public) CDOT Type 'R' inlet in sump conditions, located on the east side of Road F (**DP 5**), Just north of the intersection of Road M and Road F.

Basin A-6 (2.67 AC, Q5 = 4.7 cfs, Q100 = 11.5 cfs): Located centrally on the site, this basin consists of residential lots, Road N, and a portion of the south half of Road M. Runoff from this basin will sheet flow from the lots to the adjacent road. Flows will then be routed, via curb & gutter, to a proposed (public) CDOT Type 'R' inlet in sump conditions, located on the south side of Road M (**DP 6**), Just southeast of the intersection of Road N & Road M.

Basin A-7 (2.91 AC, Q5 = 2.3 cfs, Q100 = 8.4 cfs): Located centrally on the site, this basin consists of residential lots and a portion of the north half of Road M. Runoff from this basin will sheet flow from the lots to the adjacent road. Flows will then be routed, via curb & gutter, to a proposed (public) CDOT Type 'R' inlet in sump conditions, located on the north side of Road M (**DP 7**), Just northeast of the intersection of Road N & Road M.

Address where overflows will go

Basin A-8 (6.31 AC, Q5 = 1.9 cfs, Q100 = 13.5 cfs): Located on the eastern limits of the site, adjacent to the proposed Main Stem Tributary #2 drainageway. This basin consists of a portion of an open area amenity and the proposed (private) Full Spectrum Detention Pond A. Runoff from this basin will sheet flow directly to the northwest corner of Pond A. Flows will then be routed to the outlet structure (DP 8), via a concrete trickle channel, where it will eventually discharge, at a controlled rate, into the adjacent Main Stem Tributary #2 channel.

Address overflow spillway size and location

Basin B-1 (4.02 AC, Q5 = 6.6 cfs, Q100 = 16.0 cfs): Located on the western limits of the site, adjacent to Eastonville Road. This basin consists of residential lots and the southwest portion of Road J. Runoff from this basin will sheet flow from the lots to the adjacent road. Flows will then be routed, via curb & gutter, to a proposed (public) CDOT Type 'R' inlet in sump conditions, located at the end of the Cul-De-Sac of Road J (**DP 9**).

Basin B-2 (7.58 AC, Q5 = 13.1 cfs, Q100 = 29.3 cfs): Located on the western limits of the site, partially adjacent to Eastonville Road. This basin consists of residential lots, the northwest portion of Road J, the southwestern portion of Road F, and western portion of Road K. Runoff from this basin will sheet flow from the lots to the adjacent road. Flows will then be routed, via curb & gutter, to a proposed (public) CDOT Type 'R' inlet in sump conditions, located south of Road K on the northwest side of Road F (**DP 10**).

Basin B-3 (0.76 AC, Q5 = 3.1 cfs, Q100 = 6.0 cfs): Located on the western portion of the site, this basin consists of the south & east half portions of Road F. Flows will be routed, via curb & gutter, to a proposed (public) CDOT Type 'R' inlet in sump conditions, located on the north side of Road O (DP 11), between Road K & Road I.

Basin B-4 (9.17 AC, Q5 = 16.0 cfs, Q100 = 35.5 cfs): Located centrally on the site. This basin consists of residential lots, the northwest portion of Road J, western portion of Road K, and north half of a portion of road I & south half of Road O. Runoff from this basin will sheet flow from the lots to the adjacent road. Flows will then be routed, via curb & gutter, to a proposed (public) CDOT Type 'R' inlet in sump conditions, located east of Road P on the northwest side of Road L **(DP 12)**.

Basin B-5 (2.57 AC, Q5 = 4.7 cfs, Q100 = 10.4 cfs): Located centrally on the site, adjacent to the north side of Main Stem channel. This basin consists of residential lots and the south portion of Road L. Runoff from this basin will sheet flow from the lots to the adjacent road. Flows will then be routed, via curb & gutter, to a proposed (public) CDOT Type 'R' inlet in sump conditions, located on the south side of Road L **(DP 13)**, southeast of Road P.

Basin B-6 (2.06 AC, Q5 = 3.9 cfs, Q100 = 8.8 cfs): Located centrally on the site. This basin consists of residential lots and the northwest portion of Road P. Runoff from this basin will sheet flow from the lots to the adjacent road. Flows will then be routed, via curb & gutter, to a proposed (public) CDOT Type 'R' inlet in sump conditions, located on the northwest side of Road P (**DP 14**).

Address overflow route

This basin needs to be split up with more design points

Basin B-7 (0.99 AC, Q5 = 2.4 cfs, Q100 = 5.3 cfs): Located centrally on the site. This basin consists of residential lots and the southeast portion of Road P. Runoff from this basin will sheet flow from the lots to the adjacent road. Flows will then be routed, via curb & gutter, to a proposed (public) CDOT Type 'R' inlet in sump conditions, located on the southeast side of Road P (**DP 15**).

Basin B-8 (0.87 AC, Q5 = 0.4 cfs, Q100 = 2.6 cfs): Located centrally on the site, adjacent to the Main Stem channel. This basin consists of the proposed (private) Full Spectrum Detention Pond B. Runoff from this basin will sheet flow directly to Pond B. Flows will then be routed to the outlet structure **(DP 16)**, via a concrete trickle channel, where it will eventually discharge, at a controlled rate, into the adjacent Main Stem channel.

Basin C-1 (34.69 AC, Q5 = 40.3 cfs, Q100 = 89.9 cfs): Located on the east portion of the site, this basin consists of residential lots, Road S, Road T, Road R and portions of Roads; J, O, M, & Q. Runoff from this basin will sheet flow from the lots to the adjacent road. Flows will then be routed, via curb & gutter, to a proposed (public) CDOT Type 'R' inlet in sump conditions, located on the northeast side of Road Q (**DP** 17), northeast from Road U and Road Q intersection.

Basin C-2 (9.90 AC, Q5 = 12.9 cfs, Q100 = 29.8 cfs): Located centrally on the site, this basin consists of residential lots and portions of Roads L & Q. Runoff from this basin will sheet flow from the lots to the adjacent road. Flows will then be routed, via curb & gutter, to a proposed (public) CDOT Type 'R' inlet in sump conditions, located on the southeast side of Road Q (**DP 18**), north from Road U and Road Q intersection.

Address overflow

Basin C-3 (0.50 AC, Q5 = 0.9 cfs, Q100 = 2.5 cfs): Located on the southeast portion of the site, this basin consists of landscape and half of Road U. Runoff from this basin will sheet flow to the adjacent road. Flows will then be routed, via curb & gutter, to a proposed (public) CDOT Type 'R' in let in sump conditions, located on the west side of Road U (**DP 19**).

Basin C-4 (1.61 AC, Q5 = 3.0 cfs, Q100 = 6.8 cfs): Located on the southeast portion of the site, this basin consists of residential lots and the south half of Road U. Runoff from this basin will sheet flow to the adjacent road. Flows will then be routed, via curb & gutter, to a proposed (public) CDOT Type 'R' inlet in sump conditions, located on the east side of Road U (**DP 20**).

Basin C-5 (3.99 AC, Q5 = 1.3 cfs, Q100 = 9.4 cfs): Located on the southeast corner of the site, adjacent to the Main Stem channel. This basin consists of the proposed (private) Full Spectrum Detention Pond C. Runoff from this basin will sheet flow directly to Pond C. Flows will then be routed to the outlet structure (DP 21), via a concrete trickle channel, where it will eventually discharge, at a controlled rate, into the adjacent Main Stem channel.

Expand on the description - most of the area drains into a channel?

Basin D-1 (2.46 AC, Q5 = 5.0 cfs, Q100 = 12.3 cfs): Located on the southwest portion of the site, adjacent to Eastonville Road. This basin consists of residential lots, a portion Road B, and the north half of Road A. Runoff from this basin will sheet flow to the adjacent road. Flows will then be routed, via curb & gutter, to a proposed (public) CDOT Type 'R' inlet in sump conditions, located on the west side of Road B (**DP 22**), just north of the intersection of Road B & Road C.

Basin D-2 (0.75 AC, Q5 = 2.4 cfs, Q100 = 4.9 cfs): Located on the southwest portion of the site, this basin consists of residential lots and a portion of Road B. Runoff from this basin will sheet flow to the adjacent road. Flows will then be routed, via curb & gutter, to a proposed (public) CDOT Type, 'R' inlet in

sump conditions, located on the east side of Road B (**DP 23**), just north of the intersection of Road B & Road C.

Basin D-3 (4.76 AC, Q5 = 9.1 cfs, Q100 = 21.5 cfs): Located on the south west portion of the site, this basin consists of residential lots and a portion of Road B & Road C. Runoff from this basin will sheet flow to the adjacent road. Flows will then be routed, via curb & gutter, to a proposed (public) CDOT Type 'R' inlet in sump conditions, located on the west side of Road C (DP 24)

Basin D-4 (4.74 AC, Q5 = 9.2 cfs, Q100 = 21.1 cfs): Located on the southwest portion of the site, this basin consists of residential lots and the east half of Road C. Runoff from this basin will sheet flow to the adjacent road. Flows will then be routed, via curb & gutter, to a proposed (public) CDOT Type 'R' inlet in sump conditions, located on the east side of Road C (**DP 25**).

Basin D-5 (1.71 AC, Q5 = 0.7 cfs, Q100 = 4.8 cfs): Located on the southwest portion of the site, adjacent to the Main Stem channel. This basin consists of the proposed (private) Full Spectrum Detention Pond D. Runoff from this basin will sheet flow directly to Pond D. Flows will then be routed to the outlet structure (DP 26), via a concrete trickle channel, where it will eventually discharge, at a controlled rate, into the adjacent Main Stem channel.

Needs to be broken up

Basin E-1 (6.86 AC, Q5 = 8.0 cfs, Q100 = 21.0 cfs): Located on the southern portion of the site, this basin consists of residential lots and a portion of Road D. Runoff from this basin will sheet flow to the adjacent road. Flows will then be routed, via curb & gutter, to a proposed (public) CDOT Type 'R' inlet in sump conditions, located on the east side of Road D (**DP 27**), just north of the cul-de-sac.

Basin E-2 (11.66 AC, Q5 = 15.4 cfs, Q100 = 38.2 cfs): Located on the southern portion of the site, this basin consists of residential lots, all of Road E, the south half of Road A, and a portion of Roads; B, D & E. Runoff from this basin will sheet flow to the adjacent road. Flows will then be routed, via curb & gutter, to a proposed (public) CDOT Type 'R' inlet in sump conditions, located on the west side of Road D (**DP** 28), just north of the Cul-De-Sac.

Basin E-3 (1.74 AC, Q5 = 0.6 cfs, Q100 = 4.6 cfs): Located on the southern portion of the site, adjacent to the south side of the Main Stem channel. This basin consists of the proposed (private) Full Spectrum Detention Pond E. Runoff from this basin will sheet flow directly to Pond E. Flows will then be routed to the outlet structure **(DP 29)**, via a concrete trickle channel, where it will eventually discharge, at a controlled rate, into the adjacent Main Stem channel.

VII. Storm Sewer System

All development is anticipated to be urban and will include storm sewer & street inlets. Storm sewers collect storm water runoff and convey the water to the water quality facilities prior to discharging. Storm sewer systems will be designed to the 100-year storm and checked with the 5-year storm. Inlets will be placed at sump areas and intersections where street flow is larger than street capacity. UDFCD Inlet spreadsheet has been used to determine the size of all sump inlets.

There will be a minimum of 5 proposed storm systems within the site. Each of the five storm sewer systems will discharge storm water into its correlated WQCV pond. Each system will consist of reinforced concrete pipe (RCP), CDOT Type 'R' inlets, and storm sewer manholes.

The Final drainage report will include details concerning at-grade inlet locations, street capacity, storm sewer sizing, outlet protection and location. Preliminary sump inlets have been sized and the calculations can be found in **Appendix D**. As mentioned, these sump inlets sizes are preliminary and are currently oversized. It is anticipated that the inlets will reduce in size with the addition of at-grade inlets at the time of the Final Drainage Report.

VIII. Proposed Water Quality Detention Ponds

Five (5) Water Quality Capture Volume Detention Ponds will be provided for the proposed site. All of the proposed ponds are private and will be maintained by the HOA, once established. These detention ponds are proposed to be full spectrum and will provide water quality and detention. The WQCV and EURV release will be controlled with an orifice plate. The release rates for the WQCV and EURV will be 40-hours and 72-hours, respectively. The 100-year volume will be controlled by orifice and/or restrictor plate and will be designed to release at or below the pre-development flow rate. Outlet structures, forebays, trickle channels, etc. will be designed with the final drainage report during final plat. The required FSD pond volumes are as described below:

Pond A: Located to the north of the site, just west of the newly routed Main Stem Tributary #2 channel. This pond will discharge into the Main Stem Tributary #2, ultimately merging with Main Stem to the south, off-site. The required volume WQCV and EURV are 0.49 Ac-Ft & 1.090 Ac-Ft, respectively. The total required detention basin volume is 2.55 Ac-Ft.

Pond B: Located centrally on the site, just east of the Main Stem drainage way. This pond will discharge into the Main Stem channel. The required volume WQCV and EURV are 0.52 Ac-Ft & 1.47 Ac-Ft, respectively. The total required detention basin volume is 2.95 Ac-Ft.

Pond C: Located on the southeast portion of the site, between the Main Stem & Main Stem Tributary #2 channels. This pond will discharge into the Main Stem channel. The required volume WQCV and EURV are 0.26 Ac-Ft & 0.57 Ac-Ft, respectively. The total required detention basin volume is 1.35 Ac-Ft.

Pond D: Located centrally on the site, just west of the Main Stem channel. This pond will discharge into the Main Stem channel. The required volume WQCV and EURV are 0.22 Ac-Ft & 0.55 Ac-Ft, respectively. The total required detention basin volume is 1.23 Ac-Ft.

Pond E: Located on the south side of the site, just west of the Main Stem channel. This pond will discharge into the Main Stem channel. The required volume WQCV and EURV are 0.22 Ac-Ft & 0.48 Ac-Ft, respectively. The total required detention basin volume is 1.17 Ac-Ft.

IX. Proposed Channel Improvements Provide Pond F for basin A-1

According to the DBPS, there are two major drainage ways that run through the site. As was discussed within the Existing Conditions portion of the report, both the Main Stem channel (MS) and Main Stem Tributary #2 channel (MST) run through the site. There are no proposed major channel improvements for MS -however, MST is proposed to be rerouted. The analysis for both drainage ways and design of MST were done by others and a separate report will be submitted for review.

— MDDP?

Address the additional culvert and basin

Provide discussion and analysis of existing and proposed downstream drainage facilities and their ability to convey developed runoff from the proposed development.

Page **11** of **18**

Address channel maintenance by the district.

Address wetland maintenance by the district

X. Maintenance

After completion of construction and upon the Board of County Commissioners acceptance, it is anticipated all drainage facilities within the public Right-of-Way are to be owned and maintained by El Paso County.

All private detention ponds are to be owned and maintained by the HOA, once established, unless an agreement is reached stating otherwise.

Address maintenance access roads for the ponds and channels

XI. Wetlands Mitigation

There are two existing wetlands on site associated with the two major channels, MS and MST. The wetlands are both contained within the existing channels with the wetland in MS being classified as jurisdictional and the wetland in MST classified as non-jurisdictional. The wetlands will be analyzed with the channel report by others.

XII. Floodplain Statement

provide final USACE determination

A portion of the project sit lies with Zone A Special Flood Hazard Area as defined by the FIRM Map number 08041C0552G effective December 7, 2018. A copy of the FIRM Panel is included in **Appendix A**.

and556G

XIII. Drainage Fees & Maintenance

Gieck Ranch Basin is not listed as part of the El Paso County drainage basin fee program. Unless otherwise instructed, no drainage fees will be assessed. If it is found drainage basin fees are required, these will be included in the Final Drainage Report.

XIV. Conclusion

The Grandview Reserve residential subdivision lies within the Gieck Ranch Drainage Basin. Water quality for the site is provided in five on-site Full Spectrum Detention Ponds; Ponds A, B, C, D, & E. All drainage facilities within this report were sized according to the El Paso County Drainage Criteria Manuals. There are two major channels passing through the site Main Stem and Main Stem Tributary #2, which will be addressed by others in a channel improvement report. The five (5) WQCV ponds will be maintained by a newly established HOA. A Final Drainage Report will be submitted along with the final plat and construction drawings.

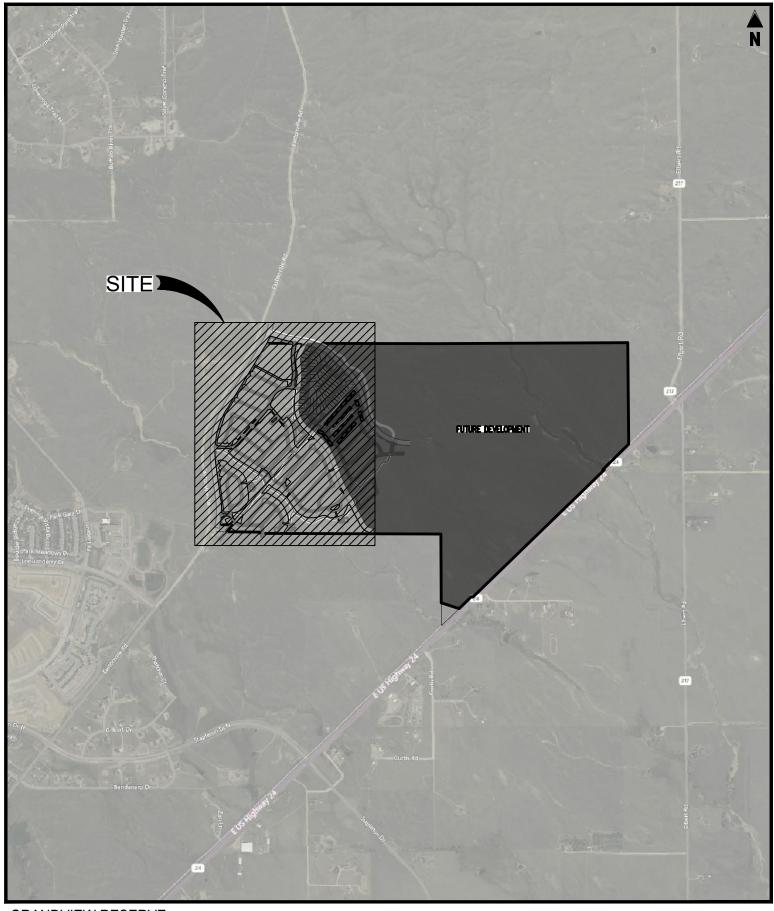
XV. References

1990 ____ 2002

- 1. El Paso County Drainage Criteria Manual, 2014.
- 2. Drainage Criteria Manual, Volume 2, City of Colorado Springs, May 2014.
- 3. *Urban Storm Drainage Criteria Manual*, Urban Drainage and Flood Control District, January 2016 (with current revisions).
- 4. Gieck Ranch Drainage Basin Study (DBPS), Drexel Barrell, October 2010 (Not adopted by County).
- 5. Grandview Reserve Master Development Drainage Plan (MDDP), HR Green, November 2020.

Add EPC DCM Update (2015) and ECM (2020)

APPENDIX A Exhibits and Figures



GRANDVIEW RESERVE

-

EASTONVILLE RD SCALE: 1"=2,000' VICINITY MAP

Project No:	HRG1.20
Drawn By:	JDP
Checked By:	RGD
Date:	07/26/2021



1155 Kelly Johnson Blvd., Suite 305 Colorado Springs, CO 80920 719.900.7220 • GallowayUS.com

In obtain more detailed information in areas where Base Flood Elevations (BFEs) and/or floodways have been determined, users are encouraged to consult the Flood Profites and Floodway Data and/or Summay of Stilware Elevations tables confaring within the Flood Insurance Study (FIS) report that accompanies this FIRM. Users should be aware that BFEs shown on the FIRM represent rounded whole-flood elevations. These BFEs are intended for flood insurance rating purposes only and should not be used as the sole source of flood elevation information. Accordingly, if flood elevation and are presented in the FIS report should be fullitled in conjunction with the FIRM for purposes of construction and/or flood-ware reconstruction and/or flood-ware reconstruction with an exercise.

ZONE A No Base Flood Elevations determined.

ZONE AE Base Flood Elevations determined.

ZONE AH Flood depths of 1.0 3 feet (usually areas of ponding); Base Flood Elevations determined.

depths of 1 to 3 feet (usually sheet flow on sloping terrain); average s determined. For areas of alluvial fan flooding, velocities also

Ite 1's animal charles tool (Universit moot), as so known as the Seas Indo.), as the flood that has 1's chance of being qualed or exceeded in any given year. The Special Product Hazard Area is the area subject, to flooding by the 1's animal chance flood. Areas of Special Rooting by We 1's animal chance flood. Areas of Special Rooting Land Inchine Zones A, AE, AA, AA, A, A9, V, and VE. The Base Rood Elevation is the water-surface betwator of the 1's animal chance flood.

Coastal Base Flood Evertaines shown on this map apply only landward or North American Vertical Datum of 1988 (NAVD98). Users of this FFRM show aware that coastal flood elevations are also provided in the Summary of Still Berainors table in the Frood instruction. Ever shown in the Summary of Still restriction for sport of the Summary of Still restriction. Ever shown in the Summary of Still restriction is shown in the Summary of Still restriction. Ever shown in the Summary of Still restriction is shown in the Summary of Still restriction. Ever and the Summary of Still restriction is shown in the Summary of Still restriction.

Boundaries of the **floodways** were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations with regard to requirements of the National Flood insurance Program. Floodway widths and other petrinent floodway data are provided in the Flood Insurance Study report for this jurisdiction.

Certain areas not in Special Flood Hazard Areas may be protected by flood contro structures. Refer to section 2.4 Flood Protection Measures" of the Flood Insuranc Sudy report for information on flood control structures for this jurisdiction.

The projection used in the preparation of this map was Universal Transver Maccaro (UM) 2004 13. GASBO spheromore according to a production of RIAMs. GASBO spheromore in datum, spheroid, projection or UTM zones zones used in production of RIAMs for adjacent jurisdictions may result in slight position differences in map features across jurisdiction boundaries. These differences do affect the accusery of this FIRM.

Flood elevations on this map are referenced to the North American Vertical Datum of 1988 (NAVD88). These flood elevations related adum. For information regarding opcured elevations referenced to the same vertical adum. For information regarding conversion between the National Geodetic Vertical Datum of 1929 and the North American Vertical Datum of 1988, visit the National Geodetic Survey website at http://www.ngs.noaa.gov/ or contact the National Geodetic Survey at the following address.

NGS Information Services NOAA, NINGS12 National Geodetic Survey SSMC-3, #2002 1315 East-West Highway Silver Spring, MD 20910-3282

To obtain current elevation, description, and/or location information for bench marks ashown on this map, please contact the Information Services Branch of the National studenties Library at (301) 715-324 or visit its website at http://www.ngs.naaa.govi.

Base Map information shown on this FIRM was provided in digital format by EI Pasc County, Colorado Sprinces, and Anderson Consulting Engineers, Inc. These data are current as of 2008.

This map reflects more detailed and up-to-date stream channel configurations and floodplain definiteations than those shown on the previous FIRM for this jurisdiction. The floodplains and floodways that were transferred from the previous FIRM may have been adjusted to conform to these enew stream channel configurations. As a result, the Flood Profless and Floodway Data tables in the Flood insurance Study Report (which contains authoritative hydraulic data) may reflect stream channel distances that differ from what is shown on this map. The profile beasilines depicted on this map represent the hydraulic modeling baselines that match the flood profiles and Floodway Data Tables if applicable, in the FIS report. As a result, the profile baselines may deviate significantly from the new base map channel representation and may appear outside of the floodplain.

Please refer to the separately printed Map Index for an overview map of the county showing the layout of map parels; community map repositions; and a Listing of Communities table containing National Flood Insurance Program dates for each community as well as a listing of the panels on which each community is

Contact FEMA Map Service Center (MSC) via the FEMA Map Information eXchange (FMIX) 1477-338-287-27 or information on available products associated with this FIRM. Available products may include previously issued Letters of Map Change, a Flood Insurance Study Report, and/or digital versions of this map. The MSC may also, be reached by Fax at 1-800-358-9620 and its website at http://www.msc.ferna.gov/.

you have questions about this map or questions concerning the National Flood surance Program in general, please call 1-877-FEMA MAP (1-877-336-2627) or

REFER TO SECTION 3.3 OF THE EL PASO COUNTY FLOOD INSURANCE STUDY FOR STREAM BY STREAM VERTICAL DATUM CONVERSION INFORMATION

Panel Location Map

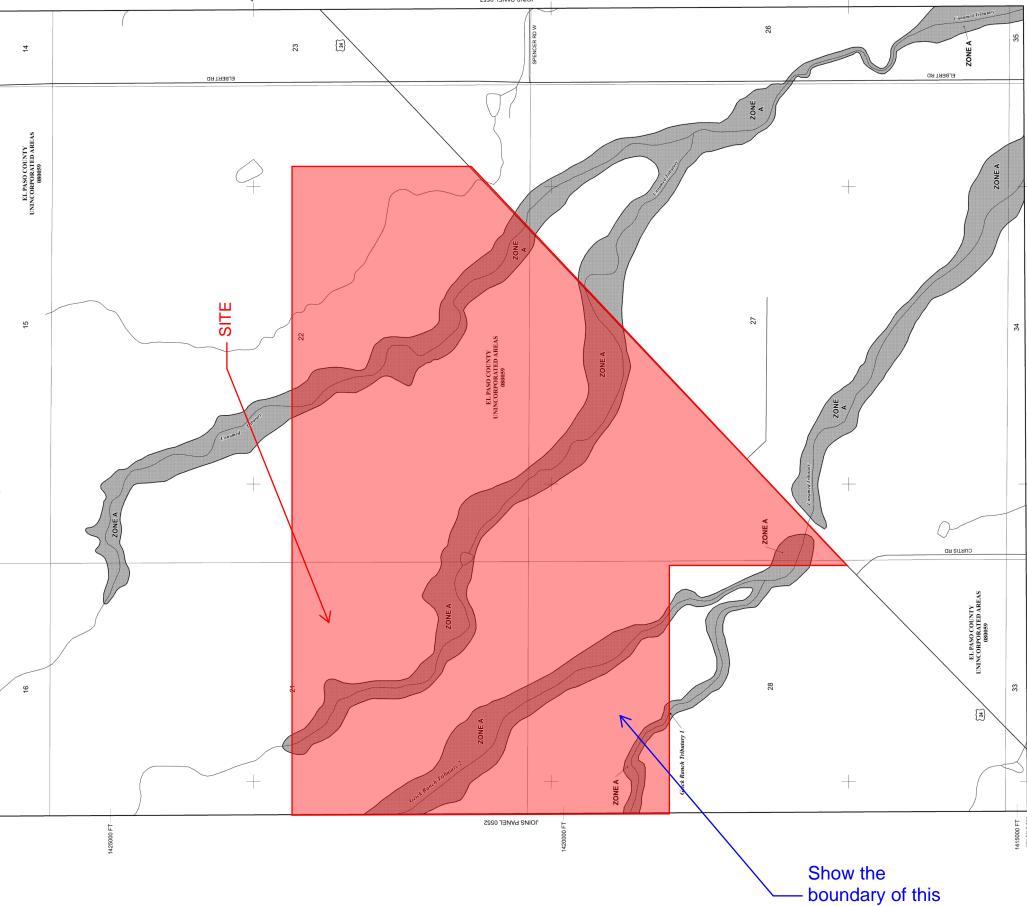
PUDSP

This Digital Flood Insurance Rate Map (DFIRM) was produced through a Opporating Technical Partner (CTP) agreement between the State of Colorado Water Conservation Board (CWCB) and the Federal Emergency Management Agency (FEMA).

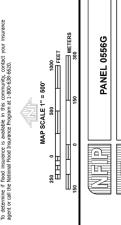








EFFECTIVE DATE(S) OF REVISION(S) TO THIS PANEL DECEMBER 7, 2014. Subject and concrose limits, to change Base Flood Elevations and Special Flood Hazard Areas, to update map format, to add roads and road names, and to incorporate previously issuade Letters of Map Revision. floodway is the channel of a stream plus any adjacent floodplain areas that must be the of encoordinent to that the 1% annual chance flood can be carried without at the lain increases in flood heights. Areas of 0.2% annual chance flood; areas of 1% annual chance flood with average depths of less than 1 foot or with drainage areas less than 1 square mile; and areas protected by levees from 1% annual chance flood. Coastal flood zone with velocity hazard (wave action); Base Floo Elevations determined. COASTAL BARRIER RESOURCES SYSTEM (CBRS) AREAS Boundary dividing Special Flood Hazard Areas of different Flood Elevations, flood depths or flood velocities. i to be protected from 1% annual chance flood by a Federa ection system under construction; no Base Flood Ele mined. For community map revision history prior to countywide mapping, refer to the Con Map History Table located in the Flood Insurance Study report for this jurisdiction. Areas determined to be outside the 0.2% annual chance floodplair Areas in which flood hazards are undetermined, but possible. Geographic coordinates referenced to the North Am Datum of 1983 (NAD 83) To determine if flood insurance is available in this community, contact your agent or call the National Flood Insurance Program at 1-800-638-6620. CBRS areas and OPAs are normally located within or adjacent to Special 5000-foot grid ticks: Colorado State Plane system, central zone (FIPSZONE 0502), Lambert Conformal Conic Projection MAP REPOSITORIES Refer to Map Repositories list on Map Index EFFECTIVE DATE OF COUNTYWIDE FLOOD INSURANCE RATE MAP MARCH 17, 1997 OTHERWISE PROTECTED AREAS (OPAs) MAP SCALE 1" = 500' Bench mark (see explanation this FIRM panel) FLOODWAY AREAS IN ZONE AE 250 0 500 HHH H Floodplain boundary Floodway boundary Zone D Boundary OTHER FLOOD AREAS OTHER AREAS * Referenced to the 97° 07' 30.00" 32° 22' 30.00" ~~ 513 ~~ (EL 987) DX5510_× • M1.5





FLOOD INSURANCE RATE MAP FIRM

EL PASO COUNTY, COLORADO AND INCORPORATED AREAS

PANEL 556 OF 1300

CONTAINS:

(SEE MAP INDEX FOR FIRM PANEL LAYOUT)

Notice to User: The Map Number shown below should be used when plasting map orders: the Community Number shown above should be used on insurance applications for the

MAP NUMBER 08041C0556G

IAD DEVISED

To obtain more detailed information in areas where Base Flood Elevations (BFEs) and/or floodways have been determined, users are encouraged to consult the Flood Profiles and Floodway Data and/or Summary of Sillwater Elevations tables contained within the Flood Insurance Study (FIS) report that accompanies this FIRM. Users should be aware that BEs shown on the FIRM represent curded winde-tool elevations. These BFEs are the remove of flood development rating purposes only and should not be used as the sole source of flood development manipul conjunction with the FIRM for purposes of construction and/or flood be utilized in conjunction with the FIRM for purposes of construction and/or floodplain management.

Coastal Base Flood Elevations shown on this map apply only landward of Dr North American Vertical Datum of 1988 (NAV.D89). Users of this FIRM should be alware that coastal flood elevations are also provided in the Summary of Sillware Elevation table in the Flood instance Study report for this shadisdrion. Elevations shown in the Summary of Sillware Elevations is shown in the Summary of Sillware Elevations and Summary of Sillware Elevations and the Summary of Sillware Elevation in the Summary of Sillware Elevations and the Sillware Sillwa

Boundaries of the **floodways** were computed at cross sections and interpolated between cross sections. The floodways were based on hydratalic considerations with regard to requirements of the National Flood Insurance Program. Floodway widths and other pertinent floodway data are provided in the Flood Insurance Study report for this jurisdiction.

Certain areas not in Special Flood Hazard Areas may be protected by flood contro structures. Refet to section 2.4 Flood Protection Measures" of the Flood Insurance Study report for information on flood control structures for this jurisdiction.

The projection used in the preparation of this map was Universal Transve Michacian (UM) 2004 5. The horizontal datum was NDAGS, GRS90 spher Differences in datum, spheroid, projection of UTM zones zones used in production of FRMs for adjacent jurisdictions may result in slight position differences in map features across jurisdiction boundaries. These differences deficiences of affect the accuracy of this FRM.

Flood elevations on this map are referenced to the **North American Vertical Datum** of 1988 (NAVD88). These flood elevations must be compared to structure and ground elevations reterenced to the same vertical adhum. For information regarding conversion between the National Geodetic Vertical Datum of 1929 and the North American Vertical Datum of 1988 visit the National Geodetic Survey website at https://www.ngs.noaa.gov/ or contact the National Geodetic Survey at the following address.

NGS Information Services NOAA, IN/NGS12 National Geodetic Survey SSMC-3, #8202 1315 East-West Highway Silver Spring, MD 20910-3282

To obtain current elevation, description, and/or location information for bench marks intown on this map, please contact the information Services Branch of the National Geodetic Survey at (301) 713-5242 or visit its website at http://www.ngs.noaa.gov/

Base Map information shown on this FIRM was provided in digital format by El Paso County, Colorado Springs Utilities, City of Foundain, Bureau of Lam Management, National Oceanic and Amrospheric Administration, United States Geological Survey, and Anderson Consulting Engineers, inc. These data are current as of 2006.

This map reflects more detailed and up-to-date stream channel configurations and floodplain delineations than those shown on the previous FINA the this jurisdiction. The floodplain sand floodways that were transferred from the previous FINA maps have been adjusted to confirm to these new stream channel configurations. As a result, the Flood Profiles and Floodway Data tables in the Flood insurance Study Report (which contains authoritative bydraulic data) may reflect stream channel distances that differ from what is shown on this map. The potile baselines depicted on this map represent the hydraulic modeling baselines that match the flood profiles and Floodway Data This map represent the hydraulic modeling baselines that match the flood profiles and Floodway Data Tables if applicable, in the FIS report. As a result, the profile asselines may devide significantly irom the new base map channel representation.

Corporate limits shown on this map are based on the best data available at the time of publication. Reseauce changes due to annexations or de-annexations may have cocurred after this map was published, map users should contact appropriate community officials to verify current corporate limit locations.

Please refer to the separately printed **Map Index** for an overview map of the coun whowing the leyout of map panels, community map repositorly addresses; and Listing of Communities table containing National Flood Insurance Program dates it, each community as well as a listing of the panels on which each community is

Contact FEMA Map Service Center (MSC) via the FEMA Map Information eXchange (FMIX) — 1477-358-2572 for information on available products associated with this FIRM. Available products may include previously issued Letters of Map Change, a Flood Insurance Study Report, and/or digital versions of this map. The MSC may also, bee reached by Fax at 1-800-358-9620 and its website at http://www.msc.lema.gov/i.

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REFER TO SECTION 3.3 OF THE EL PASO COUNTY FLOOD INSURANCE STOY FOR STREAM BY STREAM VERTICAL DATUM CONVERSION INFORMATION

Panel Location Map

This Digital Flood Insurance Rate Map (DFIRM) was produced through a Moderating Technical Partner (CTP) agreement between the State of Colorado Water-Coperating Deard (CWCB) and the Federal Emergency Management Agency (FEMA).



Additional Flood Hazard information and resources are available from local communities and the Colorado Water Conservation Board.

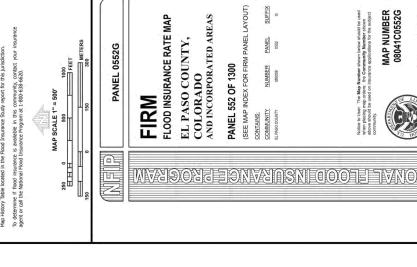
1415000 FT 38° 58' 7.50"

ZONE A 28 21 Haegler Ranch Tributary 2 ZONEA 1% ANNUAL CHANCE FLOOD DISCHARGE CONTAINED IN CULVERT Site Haegler Ranch Tributary Ia **ZONE A** 1% ANNUAL CHANCE FLOOD DISCHARGE CONTAINED IN CULVERY 1% ANNUAL CHANCE FLOOD DISCHARGE CONTAINED IN CULVERT ZONE AE (EL 7060) Haegler Ranch Tributary 2 EL PASO COUNTY UNINCORPORATED AREAS 080059 EL PASO COUNTY UNINCORPORATED AREAS 080059 30 10INS PANEL 0551 1420000 FT

EFFECTIVE DATE(s) OF REVISION(s) TO THIS PANEL.
DECEMBER 7. 2018 to update made copyrate imits, to change Base Flood Elevations and Special Flood Hazard Areas, to update map format, to add coads and road names, and to incorporate previously issued Letters of Map Revision. ZONE A No Base Flood Bleations determined.

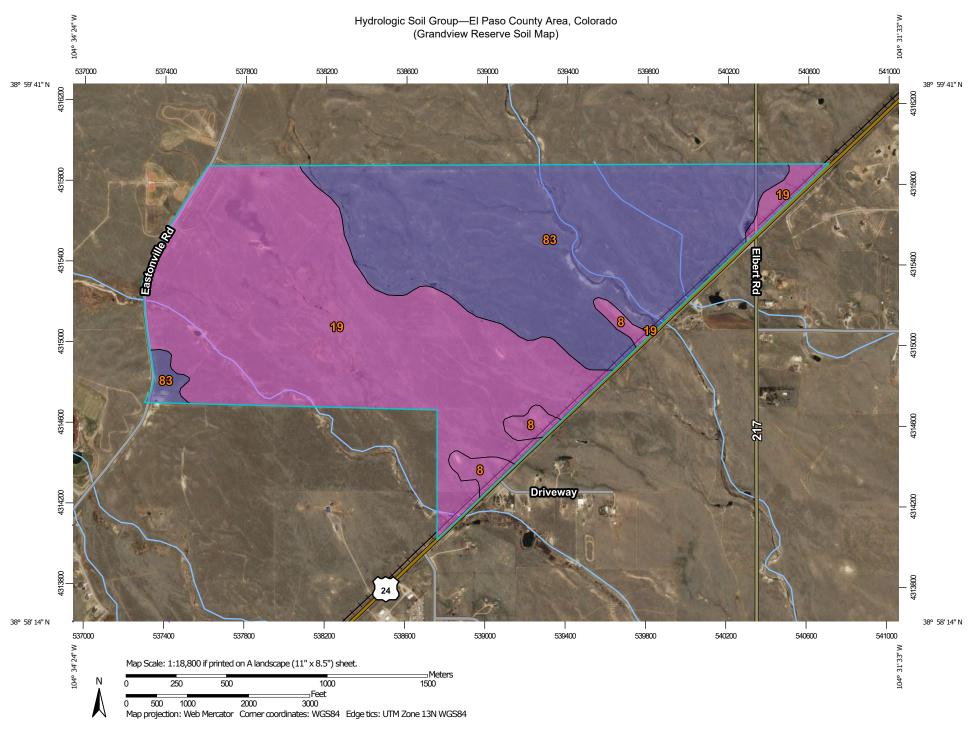
ZONE AR Base Flood deaphins determined.

ZONE AH Flood deaphis of 1 to 3 feet (usually areas of pording); Base Flood Elevations determined. Inte 1's aminand another look (Liny-Petro Taoo), as so known as the asser look, is not noot that has a 1% chance of being aquated or exceeded in any given year. The Special Rhood Assert Assert Assert of the form of the 1% aminal chance froot. Areas of Special Rhood Assert of those Zones A, & AH, AO, AR, AS, AS, V, and VE. The Base Flood Elevation is the water surface elevation of the 1% aminal chance flood. The floodway is the channel of a stream plus any adjacent floodplain areas that must be kept free of enroadchments so that the 1% annual chance flood can be carried without assignatie increases in flood heights. Areas of 0.2% annual chance flood; areas of 1% annual chance flood with average depths of less than 1 foot or with drainage areas less than 1 square mile; and areas protected by lewees from 1% annual chance flood. Flood depths of 1 to 3 feet (usually sheet flow on sloping terrain); average depths determined. For areas of alluvial fan flooding, velocities also Coastal flood zone with velocity hazard (wave action); no Base Floor Elevations determined. Coastal flood zone with velocity hazard (wave action); Base Floo Elevations determined. Special Flood Hazard Area Formerly protected from the 1% annual cha flood they at flood control system that was subsequently decertified. Zone inicideates that the former flood control system is being restored to proprotection from the 1% annual chance or greater flood. COASTAL BARRIER RESOURCES SYSTEM (CBRS) AREAS Area to be protected from 1% annual chance flood by a Federal protection system under construction; no Base Flood Elevialemental Geographic coordinates referenced to the North Amer Datum of 1983 (NAD 83) For community map revision history prior to countywide mapping, refer to the Co Map History Table located in the Flood Insurance Study report for this jurisdiction. Areas determined to be outside the 0.2% annual chance floodplain Areas in which flood hazards are undetermined, but possible. To determine if flood insurance is available in this community, contact your agent or call the National Flood Insurance Program at 1-800-638-6620. Boundary dividing Special Flood Hazard Areas of Flood Elevations, flood depths or flood velocities. CBRS areas and OPAs are normally located within or adjacent to Special Floo 5000-foot grid ticks: Colorado State Plar system, central zone (FIPSZONE 0502), ambert Conformal Conic Projection MAP REPOSITORIES Refer to Map Repositories list on Map Inde EFFECTIVE DATE OF COUNTYWIDE FLOOD INSURANCE RATE MAP MARCH 17, 1997 OTHERWISE PROTECTED AREAS (OPAs) MAP SCALE 1" = 500' FLOODWAY AREAS IN ZONE AE Floodplain boundary
Floodway boundary
Zone D Boundary
CBRS and OPA boundary Bench mark (see explan this FIRM panel) OTHER FLOOD AREAS OTHER AREAS 250 0 HHH ~~ 513 ~~ (EL 987) * Referenced to the 97° 07' 30.00" 32° 22' 30.00" DX5510_× 60000000 FT • M1.5



MAP NUMBER 08041C0552G

Notice to User: The Map Number shown below should be used when placing map orders: the Community Number shown above should be used on insurance applications for the subject



MAP LEGEND MAP INFORMATION The soil surveys that comprise your AOI were mapped at Area of Interest (AOI) С 1:24.000. Area of Interest (AOI) C/D Please rely on the bar scale on each map sheet for map Soils D measurements. Soil Rating Polygons Not rated or not available Α Source of Map: Natural Resources Conservation Service Web Soil Survey URL: **Water Features** A/D Coordinate System: Web Mercator (EPSG:3857) Streams and Canals В Maps from the Web Soil Survey are based on the Web Mercator Transportation projection, which preserves direction and shape but distorts B/D Rails --distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more Interstate Highways accurate calculations of distance or area are required. C/D **US Routes** This product is generated from the USDA-NRCS certified data as D Major Roads of the version date(s) listed below. Not rated or not available -Local Roads Soil Survey Area: El Paso County Area, Colorado Soil Rating Lines Survey Area Data: Version 17, Sep 13, 2019 Background Aerial Photography Soil map units are labeled (as space allows) for map scales 1:50.000 or larger. A/D Date(s) aerial images were photographed: Sep 8, 2018—May 26, 2019 B/D The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor C/D shifting of map unit boundaries may be evident. D Not rated or not available **Soil Rating Points** A/D B/D

Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
8	Blakeland loamy sand, 1 to 9 percent slopes	A	22.4	2.6%
19	Columbine gravelly sandy loam, 0 to 3 percent slopes	A	450.7	52.5%
83	Stapleton sandy loam, 3 to 8 percent slopes	В	385.4	44.9%
Totals for Area of Inter	rest		858.5	100.0%

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

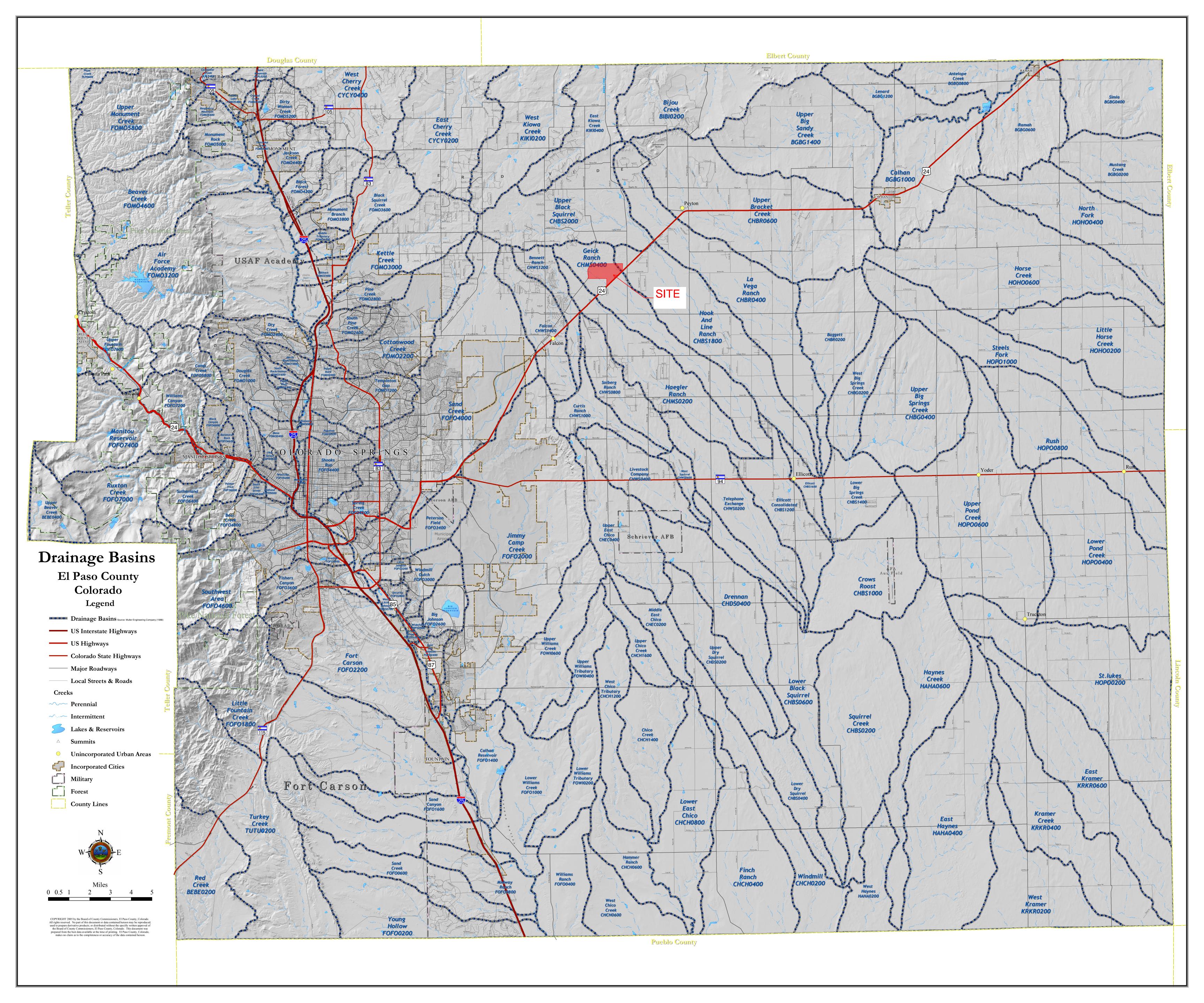
If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

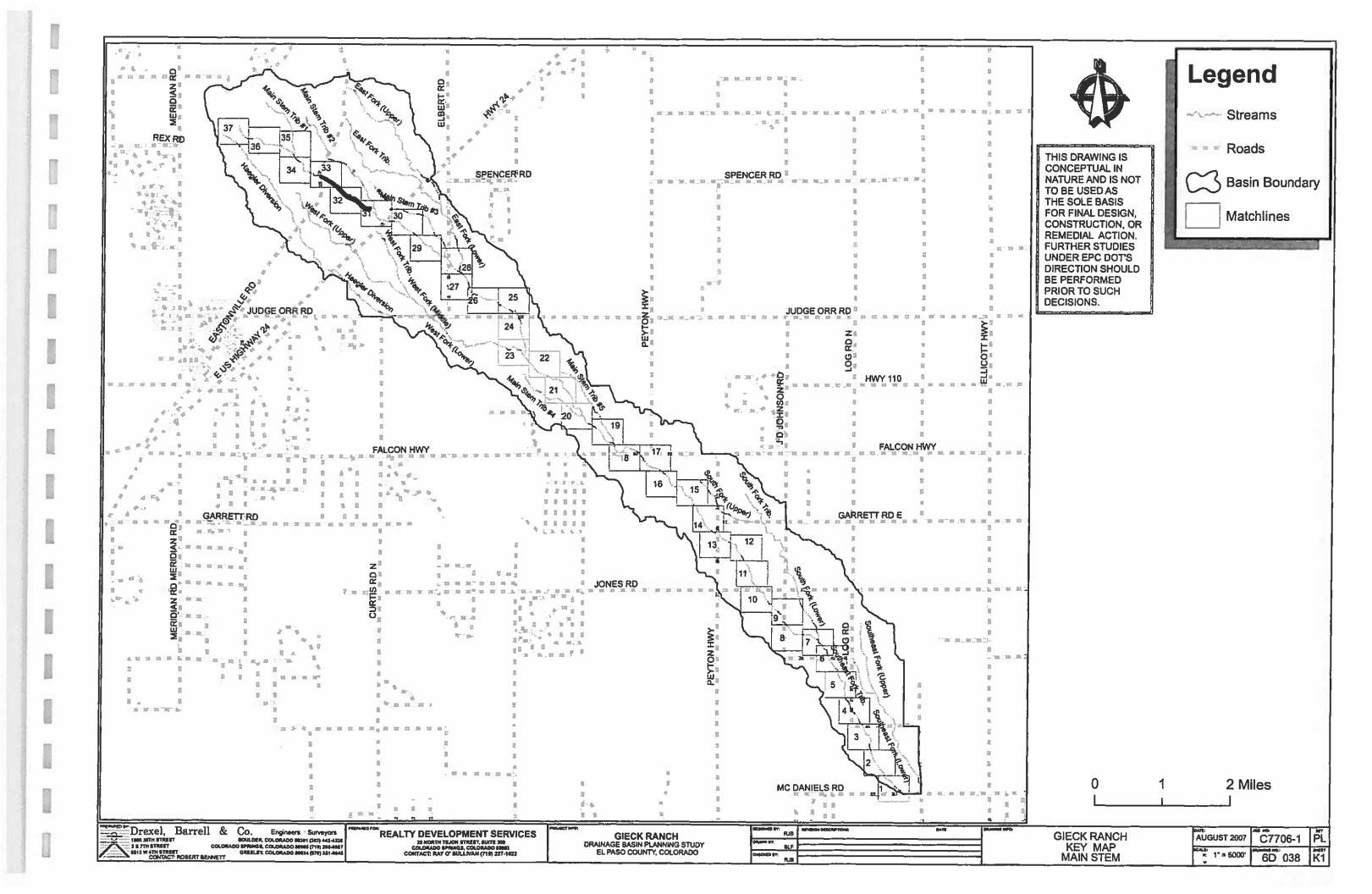
Rating Options

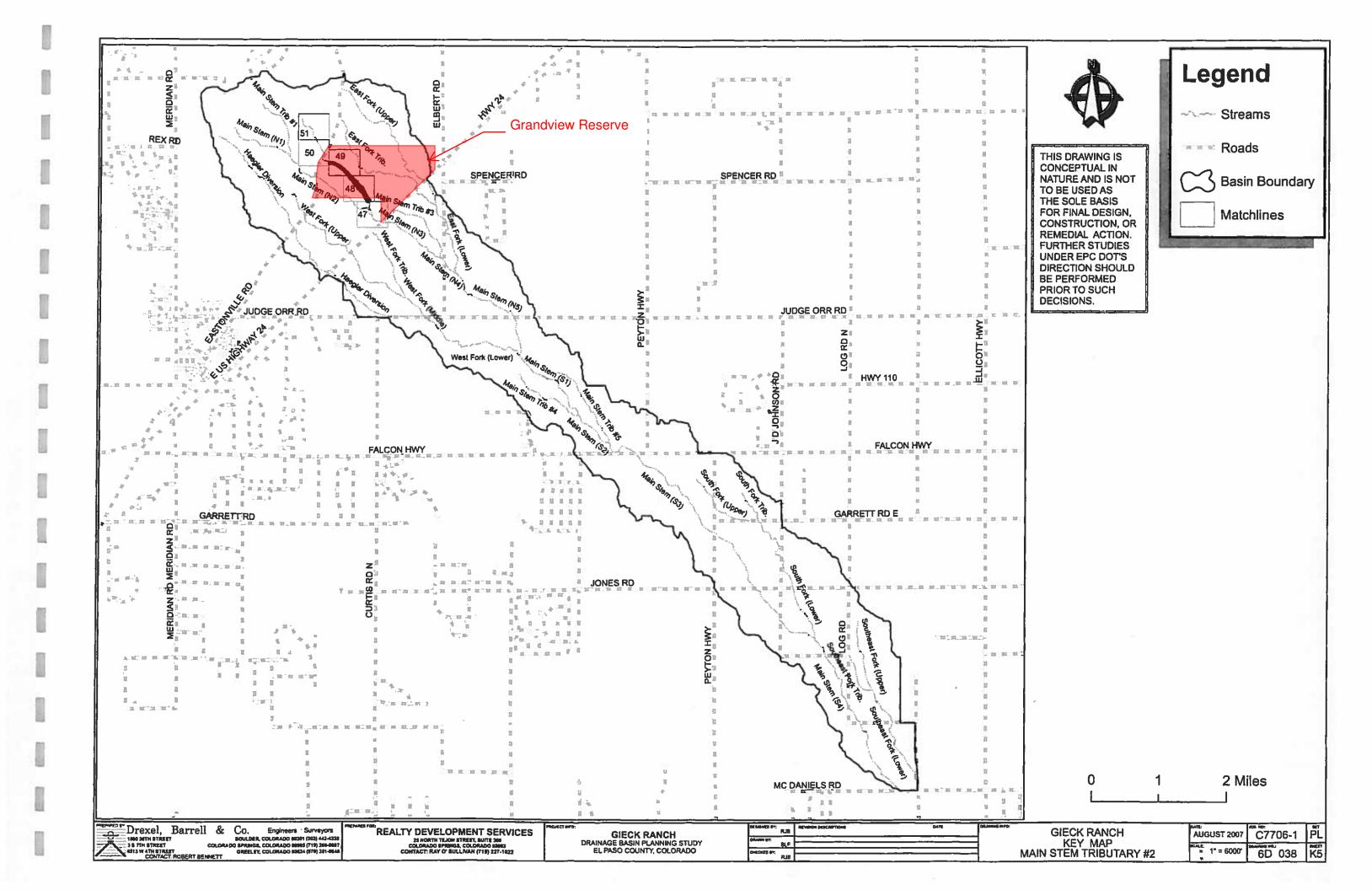
Aggregation Method: Dominant Condition
Component Percent Cutoff: None Specified

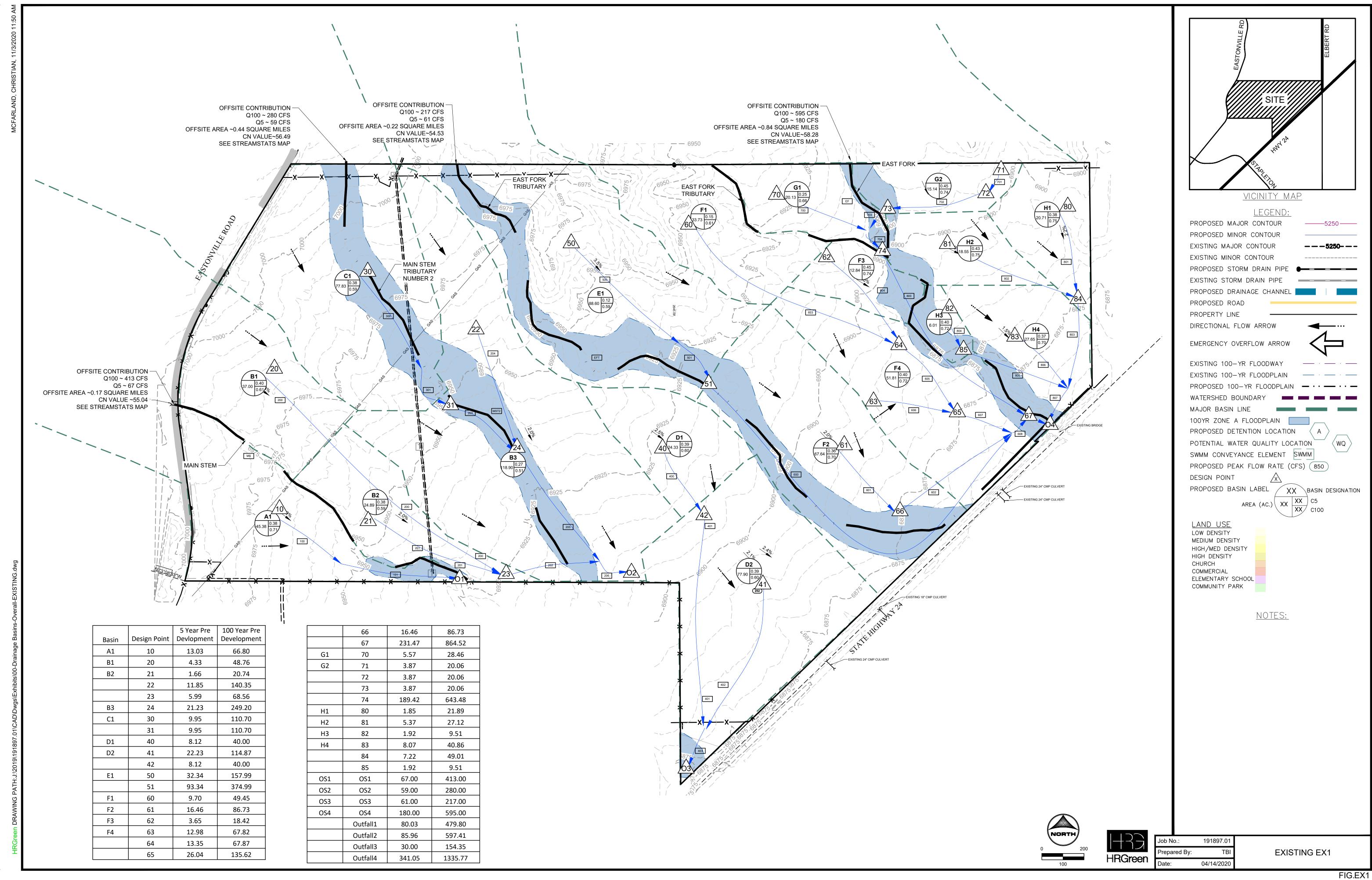
Tie-break Rule: Higher

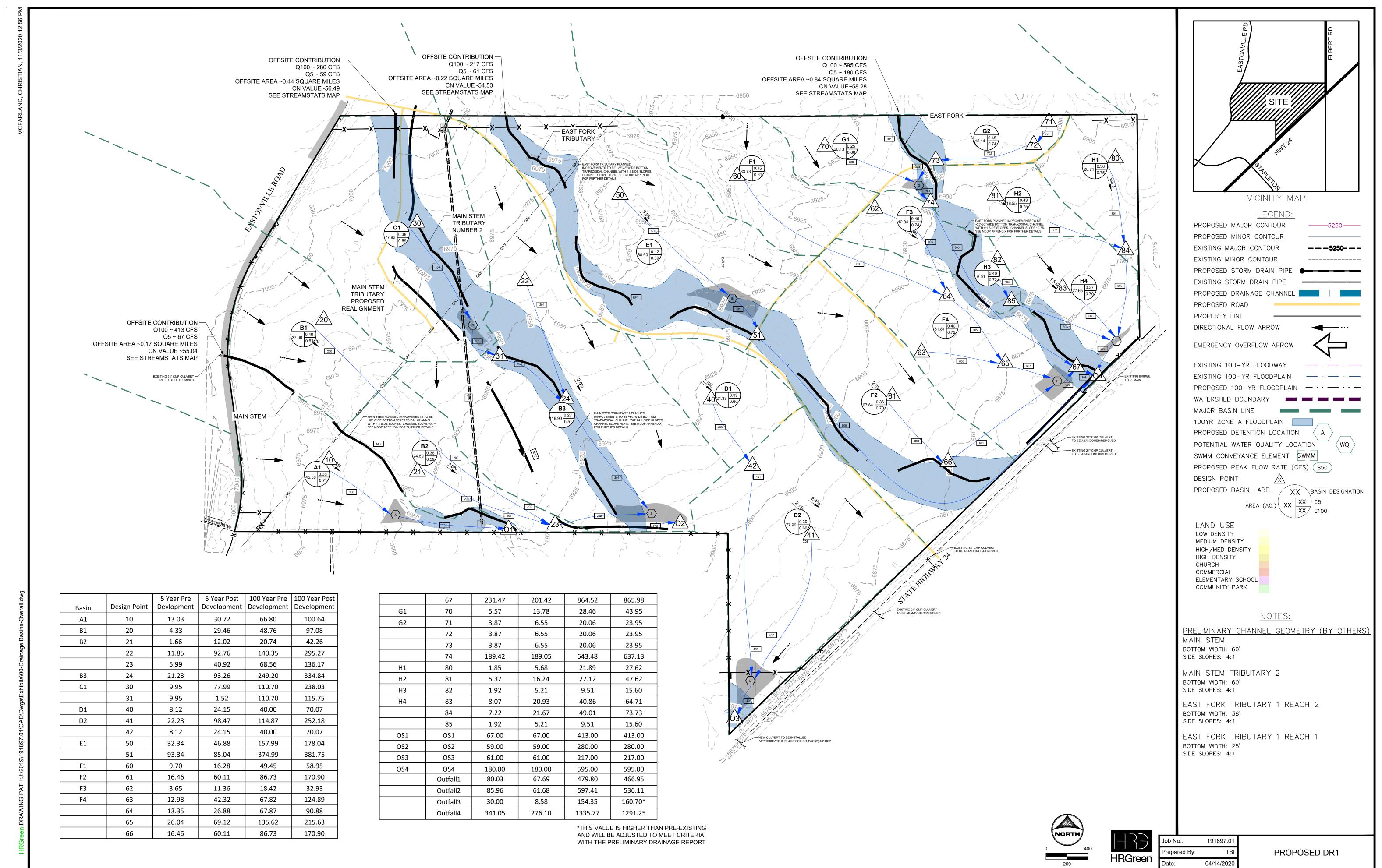
APPENDIX B MDDP & DBPS Sheet References











APPENDIX C Hydrologic Computations

COMPOSITE % IMPERVIOUS CALCULATIONS: EXISTING & PROPOSED

Subdivision: Grandview Reserve
Location: CO, El Paso County

There should be – more than 3

Project Name: Grandview Subdivision PDR
Project No.: HRG01

Calculated By: NJA
Checked By: CMD
Date: 8/11/21

1	2	3	existin	ng basin	S 6	7	8	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27
		Pa	ved/Gravel Ro	oads	La	wns/Undevelo	ped	Res	idential - 1/8	Acre	Res	sidential - 1/4	Acre	Res	sidential - 1/3	Acre	Res	idential - 1/2 A	Acre	Res	sidential - 1 A	cre	Basins Total
Basin ID	Total Area (ac)	% Imp.	Area (ac)	Weighted % Imp.	% Imp.	Area (ac)	Weighted % Imp.	% Imp.	Area (ac)	Weighted % Imp.	% Imp.	Area (ac)	Weighted % Imp.	% Imp.	Area (ac)	Weighted % Imp.	% Imp.	Area (ac)	Weighted % Imp.	% Imp.	Area (ac)	Weighted % Imp.	Weighted % Imp.
EXISTING				•		•	-					•			•	-			-			-	•
EX-1	105.72	100	0	0	2	105.72	2	65	0	0	40	0	0	30	0	0	25	0	0	20	0	0	2
EX-2	57.68	100	0	0	2	57.68	2	65	0	0	40	0	0	30	0	0	25	0	0	20	0	0	2
EX-3	23.35	100	0	0	2	23.35	2	65	0	0	40	0	0	30	0	0	25	0	0	20	0	0	2
PROPOSED						•						•			•								
Basin-1	1.4	100	1.13	80.5	2	0.27	0.4	65.0	0.00	0.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	80.9
A-1	11.23	100	0.00	0.0	2	11.23	2.0	65.0	0.00	0.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	2.0
A-2	6.94	100	2.47	35.6	2	1.37	0.4	65.0	2.88	27.0	40	0.22	1.3	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	64.3
A-3	0.34	100	0.34	100.0	2	0.00	0.0	65.0	0.00	0.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	100.0
A-4	10.15	100	1.85	18.2	2	0.77	0.2	65.0	7.44	47.6	40	0.09	0.4	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	66.4
A-5	0.34	100	0.34	100.0	2	0.00	0.0	65.0	0.00	0.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	100.0
A-6	2.67	100	0.72	27.0	2	0.67	0.5	65.0	0.45	11.0	40	0.73	10.9	30	0.10	1.1	25	0.00	0.0	20	0.00	0.0	50.5
A-7	2.91	100	0.28	9.6	2	2.23	1.5	65.0	0.40	8.9	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	20.0
A-8	6.31	100	0.00	0.0	2	6.31	2.0	65.0	0.00	0.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	2.0
B-1	4.02	100	0.74	18.4	2	1.09	0.5	65.0	2.19	35.4	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	54.3
B-2	7.58	100	1.57	20.7	2	0.74	0.2	65.0	5.14	44.1	40	0.13	0.7	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	65.7
B-3	0.76	100	0.76	100.0	2	0.00	0.0	65.0	0.00	0.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	100.0
B-4	9.17	100	2.03	22.1	2	0.73	0.2	65.0	6.41	45.4	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	67.7
B-5	2.57	100	0.51	19.8	2	0.13	0.1	65.0	1.93	48.8	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	68.7
B-6	2.06	100	0.27	13.1	2	0.00	0.0	65.0	1.79	56.5	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	69.6
B-7	0.99	100	0.27	27.3	2	0.00	0.0	65.0	0.72	47.3	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	74.6
B-8	0.87	100	0.00	0.0	2	0.87	2.0	65.0	0.00	0.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	2.0
C-1	34.69	100	6.81	19.6	2	2.05	0.1	65.0	24.10	45.2	40	1.51	1.7	30	0.22	0.2	25	0.00	0.0	20	0.00	0.0	66.8
C-2	9.90	100	1.59	16.1	2	1.34	0.3	65.0	6.58	43.2	40	0.00	0.0	30	0.39	1.2	25	0.00	0.0	20	0.00	0.0	60.8
C-3	0.50	100	0.19	38.0	2	0.31	1.2	65.0	0.00	0.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	39.2
C-4	1.61	100	0.23	14.3	2	0.11	0.1	65.0	1.27	51.3	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	65.7
C-5	3.99	100	0.00	0.0	2	3.99	2.0	65.0	0.00	0.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	2.0
D-1	2.46	100	0.43	17.5	2	0.59	0.5	65.0	1.44	38.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	56.0
D-2	0.75	100	0.36	48.0	2	0.00	0.0	65.0	0.39	33.8	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	81.8
D-3	4.76	100	0.91	19.1	2	0.61	0.3	65.0	3.01	41.1	40	0.23	1.9	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	62.4
D-4	4.74	100	0.67	14.1	2	0.34	0.1	65.0	3.73	51.1	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	65.3
D-5	1.71	100	0.00	0.0	2	1.71	2.0	65.0	0.00	0.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	2.0
E-1	6.86	100	0.87	12.7	2	1.63	0.5	65.0	2.32	22.0	40	2.04	11.9	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	47.1
E-2	11.66	100	2.42	20.8	2	1.85	0.3	65.0	3.40	19.0	40	3.99	13.7	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	53.8
E-3	1.71	100	0.00	0.0	2	1.71	2.0	65.0	0.00	0.0	40	0.00	0.0	30	0.00	0.0	25	0.00	0.0	20	0.00	0.0	2.0

Lot Type Identification:										
Lot Size (SF)	Lot Size (Acre)									
0 - 8,167	1/8 Acre									
8,168 - 12,704	1/4 Acre									
12,705 - 18,149	1/3 Acre									
18,150 - 32,670	1/2 Acre									
32,671 - 43,560	1 Acre									

% Impervious values are taken directly from Table 6-6 in the Colorado Springs DCM Vol. 1. CH. 6 (Referencing UDFCD 2001)

Page 1 of 1 8/11/2021 HRG01_Pr. Drainage Calcs Update.xlsm

COMPOSITE RUNOFF COEFFICIENT CALCULATIONS: EXISTING & PROPOSED

Subdivision: Grandview Reserve

Location: CO, El Paso County

Project Name: Grandview Subdivision PDR

Project No.: HRG01
Calculated By: NJA

Checked By: CMD

Date: 8/11/21

		Pa	ved/Gravel R	Roads	La	wns/Undevel	oped		Roofs		Res	sidential - 1/8	Acre	Res	sidential - 1/4	Acre	Residential - 1/3 Acre			Resi	dential - 1/2	Acre	Residential - 1 Acre				Composite
Basin ID	Total Area (ac)	C_5	C ₁₀₀	Area (ac)	C_5	C_{100}	Area (ac)	C_5	C ₁₀₀	Area (ac)	C_5	C ₁₀₀	Area (ac)	C_5	C ₁₀₀	Area (ac)	C_5	C ₁₀₀	Area (ac)	C_5	C_{100}	Area (ac)	C_5	C ₁₀₀	Area (ac)	Composite C ₅	C ₁₀₀
EXISTING			•			<u>'</u>								-		•	_		<u>'</u>						•		
EX-1	105.72	0.90	0.96	0.00	0.09	0.36	105.72	0.73	0.81	0.00	0.45	0.59	0.00	0.30	0.50	0.00	0.25	0.47	0.00	0.22	0.46	0.00	0.20	0.44	0.00	0.09	0.36
EX-2	57.68	0.90	0.96	0.00	0.09	0.36	57.68	0.73	0.81	0.00	0.45	0.59	0.00	0.30	0.50	0.00	0.25	0.47	0.00	0.22	0.46	0.00	0.20	0.44	0.00	0.09	0.36
EX-3	23.35	0.90	0.96	0.00	0.09	0.36	23.35	0.73	0.81	0.00	0.45	0.59	0.00	0.30	0.50	0.00	0.25	0.47	0.00	0.22	0.46	0.00	0.20	0.44	0.00	0.09	0.36
PROPOSED	_				-									_			_									_	
Basin-1	1.40	0.90	0.96	1.13	0.09	0.36	0.27	0.73	0.81	0.00	0.45	0.59	0.00	0.30	0.50	0.00	0.25	0.47	0.00	0.22	0.46	0.00	0.20	0.44	0.00	0.74	0.84
A-1	11.23	0.90	0.96	0.00	0.09	0.36	11.23	0.73	0.81	0.00	0.45	0.59	0.00	0.30	0.50	0.00	0.25	0.47	0.00	0.22	0.46	0.00	0.20	0.44	0.00	0.09	0.36
A-2	6.94	0.90	0.96	2.47	0.09	0.36	1.37	0.73	0.81	0.00	0.45	0.59	2.88	0.30	0.50	0.22	0.25	0.47	0.00	0.22	0.46	0.00	0.20	0.44	0.00	0.53	0.67
A-3	0.34	0.90	0.96	0.34	0.09	0.36	0.00	0.73	0.81	0.00	0.45	0.59	0.00	0.30	0.50	0.00	0.25	0.47	0.00	0.22	0.46	0.00	0.20	0.44	0.00	0.90	0.96
A-4	10.15	0.90	0.96	1.85	0.09	0.36	0.77	0.73	0.81	0.00	0.45	0.59	7.44	0.30	0.50	0.09	0.25	0.47	0.00	0.22	0.46	0.00	0.20	0.44	0.00	0.50	0.64
A-5	0.34	0.90	0.96	0.34	0.09	0.36	0.00	0.73	0.81	0.00	0.45	0.59	0.00	0.30	0.50	0.00	0.25	0.47	0.00	0.22	0.46	0.00	0.20	0.44	0.00	0.90	0.96
A-6	2.67	0.90	0.96	0.72	0.09	0.36	0.67	0.73	0.81	0.00	0.45	0.59	0.45	0.30	0.50	0.73	0.25	0.47	0.10	0.22	0.46	0.00	0.20	0.44	0.00	0.43	0.60
A-7	2.91	0.90	0.96	0.28	0.09	0.36	2.23	0.73	0.81	0.00	0.45	0.59	0.40	0.30	0.50	0.00	0.25	0.47	0.00	0.22	0.46	0.00	0.20	0.44	0.00	0.22	0.45
A-8	6.31	0.90	0.96	0.00	0.09	0.36	6.31	0.73	0.81	0.00	0.45	0.59	0.00	0.30	0.50	0.00	0.25	0.47	0.00	0.22	0.46	0.00	0.20	0.44	0.00	0.09	0.36
B-1	4.02	0.90	0.96	0.74	0.09	0.36	1.09	0.73	0.81	0.00	0.45	0.59	2.19	0.30	0.50	0.00	0.25	0.47	0.00	0.22	0.46	0.00	0.20	0.44	0.00	0.44	0.60
B-2	7.58	0.90	0.96	1.57	0.09	0.36	0.74	0.73	0.81	0.00	0.45	0.59	5.14	0.30	0.50	0.13	0.25	0.47	0.00	0.22	0.46	0.00	0.20	0.44	0.00	0.51	0.64
B-3	0.76	0.90	0.96	0.76	0.09	0.36	0.00	0.73	0.81	0.00	0.45	0.59	0.00	0.30	0.50	0.00	0.25	0.47	0.00	0.22	0.46	0.00	0.20	0.44	0.00	0.90	0.96
B-4	9.17	0.90	0.96	2.03	0.09	0.36	0.73	0.73	0.81	0.00	0.45	0.59	6.41	0.30	0.50	0.00	0.25	0.47	0.00	0.22	0.46	0.00	0.20	0.44	0.00	0.52	0.65
B-5	2.57	0.90	0.96	0.51	0.09	0.36	0.13	0.73	0.81	0.00	0.45	0.59	1.93	0.30	0.50	0.00	0.25	0.47	0.00	0.22	0.46	0.00	0.20	0.44	0.00	0.52	0.65
B-6	2.06	0.90	0.96	0.27	0.09	0.36	0.00	0.73	0.81	0.00	0.45	0.59	1.79	0.30	0.50	0.00	0.25	0.47	0.00	0.22	0.46	0.00	0.20	0.44	0.00	0.51	0.64

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Lot Type Ide	entification:
Lot Size (SF)	Lot Size (Acre)
0 - 8,167	= 1/8 Acre</td
8,168 - 12,704	1/4 Acre
12,705 - 18,149	1/3 Acre
18,150 - 32,670	1/2 Acre
32 671 - 43 560	1 Acre

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C values are taken directly from Table 6-6 in the Colorado Springs DCM Vol. 1. CH. 6 (Referencing UDFCD 2001)

Coeffficients use HSG A&B soils - Refer to "Appendix A: Exhibits and Figures" for soil map

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STANDARD FORM SF-2: EXISTING & PROPOSED TIME OF CONCENTRATION

not urbanized for existing?

Subdivision:	Grandview Reserve
Location	CO. El Paco County

Project Name: Grandview Subdivision PDR
Project No.: HRG01
Calculated By: NJA
Checked By: CMD

9.8

442.0

12.5

									Date: 8/11/21										
				_		_													
1	2	3	4	5	6	7	8 * (OVED)	9	10	11	12	13	14	15	16 Tc CHECK	17	18		
		SUB-BA				INITIA	L/OVER	LAND		TR	AVEL TI	ME		(III)	F-14.4				
		DAT					(T _i)				(T _t)			(UR	FINAL				
BASIN	D.A.		Impervious	C_5	C_{100}	L	S	T_i	L	S	Cv	VEL.	T_t	COMP. T _c		Urbanized T _c	T _c		
ID	(AC)	Soils Group	(%)			(FT)	(%)	(MIN)	(FT)	(%)		(FPS)	(MIN)	(MIN)	LENGTH(FT)	(MIN)	(MIN)		
EXISTING					,										1				
EX-1	105.72	A	2.0	0.09	0.36	300	2.2	24.6	3603	2.2	15	2.2	26.9	51.5		31.7	¥ 31.7		
EX-2	57.68	A	2.0	0.09	0.36	300	1.7	27.1	2906	2.2	15	2.2	21.8	48.8		27.8	27.8		
EX-3	23.35	A	2.0	0.09	0.36	300	3.4	21.3	1029	2.2	15	2.2	7.7	29.0	1329.0	17.4	17.4		
PROPOSEI			_									I			1				
Basin-1	1.40	A	80.9	0.74	0.84	46	2.0	3.5	556	1.8	20	2.7	3.5	7.0		13.3	7.0		
A-1	11.23	A	2.0	0.09	0.36	100	10.0	8.6	907	5.0	20	4.5	3.4	12.0	1007.0	15.6	12.0		
A-2	6.94	A	64.3	0.53	0.67	160	5.0	7.7	1143	2.4	20	3.1	6.1	13.9	1303.0	17.2	13.9		
A-3	0.34	A	100.0	0.90	0.96	18	2.0	1.2	560	1.9	20	2.8	3.4	4.6		13.2	5.0		
A-4	10.15	A	66.4	0.50	0.64	90	5.0	6.1	920	2.1	20	2.9	5.3	11.4	1010.0	15.6	11.4		
A-5	0.34	A	100.0	0.90	0.96	18	2.0	1.2	332	1.4	20	2.4	2.3	3.6		11.9	5.0		
A-6	2.67	A	50.5	0.43	0.60	207	10.0	8.2	340	1.7	20	2.6	2.2	10.4	547.0	13.0	10.4		
A-7	2.91	A	20.0	0.22	0.45	327	5.0	17.0	351	3.3	20	3.6	1.6	18.7	678.0	13.8	13.8		
A-8	6.31	A	2.0	0.09	0.36	250	5.0	17.1	857	5.0	20	4.5	3.2	20.3	1107.0	16.2	16.2		
B-1	4.02	A	54.3	0.44	0.60	147	5.0	8.6	648	1.7	20	2.6	4.1	12.7	795.0	14.4	12.7		
B-2	7.58	A	65.7	0.51	0.64	228	5.0	9.5	930	1.6	20	2.5	6.1	15.7	1158.0	16.4	15.7		
B-3	0.76	A	100.0	0.90	0.96	18	2.0	1.2	721	1.0	20	2.0	6.0	7.2	739.0	14.1	7.2		
B-4	9.17	A	67.7	0.52	0.65	72	2.0	7.2	1364	1.6	20	2.5	9.0	16.1	1436.0	18.0	16.1		
B-5	2.57	A	68.7	0.52	0.65	124	2.0	9.4	899	2.1	20	2.9	5.2	14.6	1023.0	15.7	14.6		
B-6	2.06	A	69.6	0.51	0.64	179	2.0	11.5	287	2.0	20	2.8	1.7	13.2	466.0	12.6	12.6		
B-7	0.99	A	74.6	0.57	0.69	79	2.0	6.8	292	2.0	20	2.8	1.7	8.6	371.0	12.1	8.6		
B-8	0.87	A	2.0	0.09	0.36	66	25.0	5.1	187	1.0	20	2.0	1.6	6.7	253.0	11.4	6.7		
C-1	34.69	A	66.8	0.51	0.64	233	2.0	13.1	3978	1.3	20	2.3	29.1	42.2	4211.0	33.4	33.4		
C-2	9.90	A	60.8	0.47	0.61	289	2.0	15.6	2124	1.5	20	2.4	14.5	30.0	2413.0	23.4	23.4		
C-3	0.50	A	39.2	0.40	0.59	24	2.0	5.0		1.2	20	2.2	1.9	6.9	277.0	11.5	6.9		
C-4	1.61	A	65.7	0.49	0.63	132	2.0	10.2	272	0.9	20	1.9	2.4	12.6	404.0	12.2	12.2		
C-5	3.99	A	2.0	0.09	0.36	225	15.0	11.3	352	1.0	20	2.0	2.9	14.2	577.0	13.2	13.2		
D-1	2.46	A	56.0	0.44	0.60	32	4.6	4.1	446	1.7	20	2.6	2.9	7.0	478.0	12.7	7.0		
D-2	0.75	A	81.8	0.67	0.77	66	2.7	4.6	291	1.8	20	2.7	1.8	6.4	357.0	12.0	6.4		
D-3	4.76	A	62.4	0.48	0.63	69	4.8	5.6	802	1.8	20	2.7	5.0	10.6	871.0	14.8	10.6		
D-4	4.74	A	65.3	0.49	0.63	69	4.8	5.5	841	1.7	20	2.6	5.4	10.9	910.0	15.1	10.9		
D-5	1.71	A	2.0	0.09	0.36	110	25.0	6.6	201	1.0	20	2.0	1.7	8.3	311.0	11.7	8.3		
E-1	6.86	A	47.1	0.38	0.56	370	5.0	14.8	1283	1.3	20	2.3	9.4	24.2	1653.0	19.2	19.2		
E-2	11.66	A	53.8	0.43	0.60	309	5.0	12.6	1364	1.9	20	2.8	8.2	20.9	1673.0	19.3	19.3		

E-3 NOTES:

 $T_i = (0.395*(1.1 - C_5)*(L)^0.5)/((S)^0.33)$, S in ft/ft

T_t=L/60V (Velocity From Fig. 501)

1.71

Velocity V=Cv*S^0.5, S in ft/ft

 $T_c Check = 10 + L/180$

For Urbanized basins a minimum $T_{\rm c}$ of 5.0 minutes is required.

For non-urbanized basins a minimum T_c of 10.0 minutes is required

0.09

0.36

127

25.0

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315

STANDARD FORM SF-3: EXISTING & PROPOSED STORM DRAINAGE SYSTEM DESIGN

(RATIONAL METHOD PROCEDURE)

Not checked on first review

Subdivision: Grandview Reserve
Location: CO, El Paso County
Design Storm: 5-Year

 Project Name:
 Grandview Subdivision PDR

 Project No.:
 HRG01

 Calculated By:
 NJA

 Checked By:
 CMD

 Date:
 8/11/21

				DIRI	ECT RUI	NOFF				TOTAL	RUNOF	F	STR	REET		PIPE T			VEL T	IME	
STREET	Design Point	Basin ID	Area (Ac)	Runoff Coeff.	Tc (min)	C*A (Ac)	I (in/hr)	Q (cfs)	Tc (min)	C*A (Ac)	I (in/hr)	Q (cfs)	Slope (%)	Street Flow (cfs)	Design Flow (cfs)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	Tt (min)	REMARKS
EXISTING		EX-1	105.72	0.09	31.7	9.51	2.35	22.3	Г	ı	l	l	T	ı		1	Π	ı	ı	1	Sheet flow to Main Stem Tributary #2 Channel
	1											89.3									Total Flow - Incl. Offsite flow of Q(5)=67 cfs (from MDDP)
	2	EX-2	57.68	0.09	27.8	5.19	2.53	13.1				72.1									Sheet flow to Main Stem Channel Total Flow - Incl. Offsite flow of Q(5)=59 cfs (from MDDP)
	3	EX-3	23.35	0.09	17.4	2.10	3.23	6.8													Sheet flow offiste - outfalls to Main Stem Tributary #2 Channel
PROPOSED		<u> </u>			<u> </u>					<u> </u>			l			l					
	<u> </u>	Basin-1	1.40	0.74	7.0	1.04	4.64	4.8	<u> </u>				T	l l		Ι		Ι	l I		
	1	A-1	11.23	0.09	12.0	1.01	3.82	3.9													
	2	A-2	6.94	0.53	13.9	3.68	3.59	13.2													
	3	A-3	0.34	0.90	5.0	0.31	5.10	1.6													
	4	A-4	10.15	0.50	11.4	5.08	3.90	19.8													
	5	A-5	0.34	0.90	5.0	0.31	5.10	1.6													
	6	A-6	2.67	0.43	10.4	1.15	4.05	4.7													
	7	A-7	2.91	0.22	13.8	0.64	3.60	2.3													
		A-8	6.31	0.09	16.2	0.57	3.35	1.9													
	8								16.2	11.74	3.35	39.3									Total of flows to Pond A
	9	B-1	4.02	0.44	12.7	1.77	3.72	6.6													
	10	B-2	7.58	0.51	15.7	3.87	3.39	13.1													
	11	B-3	0.76	0.90	7.2	0.68	4.59	3.1													
	12	B-4	9.17	0.52	16.1	4.77	3.35	16.0													
	13	B-5	2.57	0.52	14.6	1.34	3.51	4.7													
	14	B-6	2.06	0.51	12.6	1.05	3.74	3.9													
	15	B-7	0.99	0.57	8.6	0.56	4.34	2.4													
	13																				
	16	B-8	0.87	0.09	6.7	0.08	4.70	0.4	16.1	14.12	3.35	47.3									Total of flows to Pond B
	17	C-1	34.69	0.51	33.4	17.69	2.28	40.3													
	18	C-2	9.90	0.47	23.4	4.65	2.78	12.9													
	19	C-3	0.50	0.40	6.9	0.20	4.66	0.9													
	20	C-4	1.61	0.49	12.2	0.79	3.78	3.0													
		C-5	3.99	0.09	13.2	0.36	3.66	1.3							<u> </u>						
	21 22	D-1	2.46	0.44	7.0	1.08	4.65	5.0	33.4	23.69	2.28	54.0	-	-	-	-	-		-		Total of flows to Pond C
										ļ											
	23	D-2	0.75	0.67	6.4	0.50	4.77	2.4													
	24	D-3	4.76	0.48	10.6	2.28	4.01	9.1													
MDCOLD D. C. C. L. V. L.													•——								D 1 52 0/10/001

STANDARD FORM SF-3: EXISTING & PROPOSED

STORM DRAINAGE SYSTEM DESIGN

(RATIONAL METHOD PROCEDURE)

	Project Name: Grandview Subdivision PDR
Subdivision: Grandview Reserve	Project No.: HRG01
Location: CO, El Paso County	Calculated By: NJA
Design Storm: 5-Year	Checked By: CMD
	Date: 8/11/21

		DIRECT RUNOFF								TOTAL :	RUNOF	STF	STREET PIPE					VEL T	IME		
STREET	Design Point	Basin ID	Area (Ac)	Runoff Coeff.	Tc (min)	C*A (Ac)	I (in/hr)	Q (cfs)	Tc (min)	C*A (Ac)	I (in/hr)	Q (cfs)	Slope (%)	Street Flow (cfs)	Design Flow (cfs)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	Tt (min)	REMARKS
	25	D-4	4.74	0.49	10.9	2.32	3.97	9.2													
	26	D-5	1.71	0.09	8.3	0.15	4.39	0.7	10.9	6.33	3.97	25.1									Total of flows to Pond D
	27	E-1	6.86	0.38	19.2	2.61	3.08	8.0													
	28	E-2	11.66	0.43	19.3	5.01	3.07	15.4													
	29	E-3	1.71	0.09	9.8	0.15	4.14	0.6	19.3	7.77	3.07	23.9									Total of flows to Pond E

HRG01_Pr. Drainage Cales Update.xlsm

STANDARD FORM SF-3: EXISTING & PROPOSED

STORM DRAINAGE SYSTEM DESIGN

(RATIONAL METHOD PROCEDURE)

Subdivision: Grandview Reserve

Location: CO, El Paso County

Design Storm: 100-Year

 Project Name:
 Grandview Subdivision PDR

 Project No.:
 HRG01

 Calculated By:
 NJA

 Checked By:
 CMD

Date: 8/11/21

		DIRECT RUNOFF							TOTAL RUNOFF					REET		PIPE		TRAVEL TI			
STREET	Design Point	Basin ID	Area (Ac)	Runoff Coeff.	Tc (min)	C*A (Ac)	I (in/hr)	Q (cfs)	Tc (min)	C*A (Ac)	I (in/hr)	Q (cfs)	Slope (%)	Street Flow (cfs)	Design Flow (cfs)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	Tt (min)	REMARKS
EXISTING		EX-1	105.72	0.36	31.7	38.06	4.18	159.1	ı	1					ı						Sheet flow to Main Stem Tributary #2 Channel
	1	EX-2	57.68	0.36	27.8	20.76	4.50	93.4				572.1									Total Flow - Incl. Offsite flow of Q(100)=413 cfs (from MDDP) Sheet flow to Main Stem Channel
	2 3	EX-3	23.35	0.36	17.4	8.41	5.75	48.4				373.4									Total Flow - Incl. Offsite flow of Q(100)=280 cfs (from MDDP) Sheet flow offiste - outfalls to Main Stem Tributary #2 Channel
	3	EA-3	23.33	0.36	17.4	8.41	3.73	40.4													Sheet flow offiste - outlans to Main Stem Tributary #2 Channel
PROPOSED																					
		Basin-1	1.40	0.84	7.0	1.18	8.26	9.7													
	1	A-1	11.23	0.36	12.0	4.04	6.80	27.5													
	2	A-2	6.94	0.67	13.9	4.65	6.38	29.7													
	3	A-3	0.34	0.96	5.0	0.33	9.09	3.0													
	4	A-4	10.15	0.64	11.4	6.50	6.94	45.1													
	5	A-5	0.34	0.96	5.0	0.33	9.09	3.0													
	6	A-6	2.67	0.60	10.4	1.60	7.20	11.5													
	7	A-7	2.91	0.45	13.8	1.31	6.40	8.4													
		A-8	6.31	0.36	16.2	2.27	5.96	13.5													
	8	B-1	4.02	0.60	12.7	2.41	6.63	16.0	16.2	16.99	5.96	101.3									Total of flows to Pond A
	9																				
	10	B-2	7.58	0.64	15.7	4.85	6.04	29.3													
	11	B-3	0.76	0.96	7.2	0.73	8.17	6.0													
	12	B-4	9.17	0.65	16.1	5.96	5.96	35.5													
	13	B-5	2.57	0.65	14.6	1.67	6.25	10.4													
	14	B-6	2.06	0.64	12.6	1.32	6.66	8.8													
	15	B-7	0.99	0.69	8.6	0.68	7.73	5.3													
	16	B-8	0.87	0.36	6.7	0.31	8.37	2.6	16.1	17.93	5.96	106.9									Total Co., and D. ID.
	17	C-1	34.69	0.64	33.4	22.20	4.05	89.9	16.1	17.93	3.96	106.9									Total of flows to Pond B
	18	C-2	9.90	0.61	23.4	6.04	4.94	29.8													
	19	C-3	0.50	0.59	6.9	0.30	8.30	2.5													
	20	C-4	1.61	0.63	12.2	1.01	6.73	6.8	-												
		C-5	3.99	0.36	13.2	1.44	6.52	9.4													
	21 22	D-1	2.46	0.60	7.0	1.48	8.28	12.3	33.4	30.99	4.05	125.5									Total of flows to Pond C
	23	D-2	0.75	0.77	6.4	0.58	8.49	4.9													
	24	D-3	4.76	0.63	10.6	3.00	7.15	21.5													

STANDARD FORM SF-3: EXISTING & PROPOSED

STORM DRAINAGE SYSTEM DESIGN

(RATIONAL METHOD PROCEDURE)

 Subdivision: Grandview Reserve
 Project Name: Grandview Subdivision PDR

 Location: CO, El Paso County
 Froject No.: HRG01

 Design Storm: 100-Year
 Calculated By: NJA

 Checked By: OMD
 Checked By: NJA

 Judical County
 Budical County

	DIRECT RUNOFF							1	TOTAL:	RUNOF	F	ST	REET	PIPE			TRAY	VEL T	IME		
STREET	Design Point	Basin ID	Area (Ac)	Runoff Coeff.	Tc (min)	C*A (Ac)	I (in/hr)	Q (cfs)	Tc (min)	C*A (Ac)	I (in/hr)	Q (cfs)	Slope (%)	Street Flow (cfs)	Design Flow (cfs)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	Tt (min)	REMARKS
	25	D-4	4.74	0.63	10.9	2.99	7.07	21.1													
	26	D-5	1.71	0.36	8.3	0.62	7.81	4.8	10.9	8.67	7.07	61.3									Total of flows to Pond D
	27	E-1	6.86	0.56	19.2	3.84	5.48	21.0													
	28	E-2	11.66	0.60	19.3	7.00	5.46	38.2													
	29	E-3	1.71	0.36	9.8	0.62	7.37	4.6	19.3	11.46	5.46	62.6									Total of flows to Pond E

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APPENDIX D Hydraulic Computations

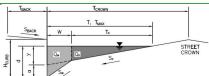
Inlets not checked with first review.

MHFD-Inlet, Version 5.01 (April 2021)

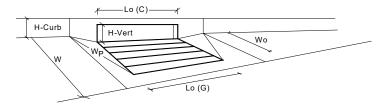
ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: Grandview Reserve
Inlet ID: Inlet 1 (DP 2)



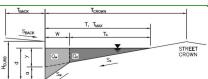
Gutter Geometry: Maximum Allowable Width for Spread Behind Curb 7.5 Side Slope Behind Curb (leave blank for no conveyance credit behind curb)
Manning's Roughness Behind Curb (typically between 0.012 and 0.020) ft/ft $S_{BACK} =$ 0.020 $n_{BACK} =$ 0.012 Height of Curb at Gutter Flow Line H_{CURB} = 6.00 inches T_{CROWN} = Distance from Curb Face to Street Crown 14.0 Gutter Width 2.00 Street Transverse Slope S_X = 0.024 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) 0.083 ft/ft Street Longitudinal Slope - Enter 0 for sump condition S_0 0.000 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) n_{STREET} = Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm 14.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm linches 6.0 12.0 Check boxes are not applicable in SUMP conditions MINOR STORM Allowable Capacity is based on Depth Criterion Minor Storm Major Storm MAJOR STORM Allowable Capacity is based on Depth Criterion SUMP SUMP



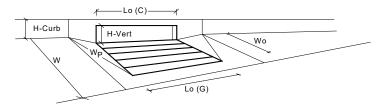
Design Information (Input)		MINOR	MAJOR	
Type of Inlet CDOT Type R Curb Opening	Type =		Curb Opening	1
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	3	3	1
Water Depth at Flowline (outside of local depression)	Ponding Depth =	6.0	12.0	inches
Grate Information		MINOR	MAJOR	✓ Override Depths
Length of a Unit Grate	L₀ (G) =	N/A	N/A	feet
Width of a Unit Grate	W _o =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	1
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_f(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C _w (G) =	N/A	N/A	1
Grate Orifice Coefficient (typical value 0.60 - 0.80)	$C_o(G) =$	N/A	N/A	
<u>Curb Opening Information</u>		MINOR	MAJOR	
Length of a Unit Curb Opening	$L_o(C) =$	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	$H_{vert} =$	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	$H_{throat} =$	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	$W_p = L$	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) = $	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_o(C) = $	0.67	0.67	
 Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A]ft
Depth for Curb Opening Weir Equation	d _{Curb} =	0.33	0.83	T ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	0.57	1.00	1
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	0.79	1.00	1
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A]
		MINOR	MAJOR	
Total Inlet Interception Capacity (assumes clogged condition)	0 _a = [13.5	39.1	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	13.2	29.7	cfs

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: Grandview Reserve
Inlet ID: Inlet 2 (DP 3)



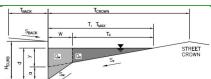
Gutter Geometry: Maximum Allowable Width for Spread Behind Curb 7.5 Side Slope Behind Curb (leave blank for no conveyance credit behind curb)
Manning's Roughness Behind Curb (typically between 0.012 and 0.020) ft/ft $S_{BACK} =$ 0.020 $n_{BACK} =$ 0.012 Height of Curb at Gutter Flow Line H_{CURB} = 6.00 inches T_{CROWN} = Distance from Curb Face to Street Crown 14.0 Gutter Width 2.00 Street Transverse Slope S_X = 0.019 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) S_{W} 0.083 ft/ft Street Longitudinal Slope - Enter 0 for sump condition Manning's Roughness for Street Section (typically between 0.012 and 0.020) S_{0} 0.000 ft/ft n_{STREET} = 0.012 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm T_{MAX} = 7.0 14.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm linches 6.0 12.0 Check boxes are not applicable in SUMP conditions Major Storm MINOR STORM Allowable Capacity is based on Depth Criterion Minor Storm MAJOR STORM Allowable Capacity is based on Depth Criterion SUMP SUMP



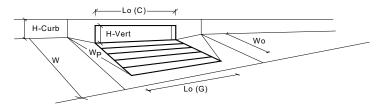
Design Information (Input)		MINOR	MAJOR	
Type of Inlet CDOT Type R Curb Opening	Type =		Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	7
Water Depth at Flowline (outside of local depression)	Ponding Depth =	6.0	12.0	inches
Grate Information		MINOR	MAJOR	Override Depths
Length of a Unit Grate	L, (G) =	N/A	N/A	feet
Width of a Unit Grate	W ₀ =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	7
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	C _f (G) =	N/A	N/A	1
Grate Weir Coefficient (typical value 2.15 - 3.60)	C _w (G) =	N/A	N/A	7
Grate Orifice Coefficient (typical value 0.60 - 0.80)	C ₀ (G) =	N/A	N/A	7
Curb Opening Information	-	MINOR	MAJOR	-
Length of a Unit Curb Opening	$L_o(C) = [$	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	$H_{throat} = $	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	$W_p = [$	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$	3.60	3.60	_
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_o(C) = $	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	Πft
Depth for Curb Opening Weir Equation	d _{Curb} =	0.33	0.83	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	0.77	1.00	7
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	1.00	1.00	7
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A	
		MATHOD		
Tabal Talah Tahanan dian Canasib (0 -	MINOR	MAJOR	٦
Total Inlet Interception Capacity (assumes clogged condition)	Q _a =	5.4 1.6	12.3 3.0	cfs cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	1.0] 3.0	Jus

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: Grandview Reserve
Inlet ID: Inlet 3 (DP4)



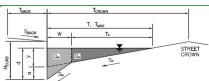
Gutter Geometry: Maximum Allowable Width for Spread Behind Curb 7.5 Side Slope Behind Curb (leave blank for no conveyance credit behind curb)
Manning's Roughness Behind Curb (typically between 0.012 and 0.020) ft/ft $S_{BACK} =$ 0.020 $n_{BACK} =$ 0.012 Height of Curb at Gutter Flow Line H_{CURB} = 6.00 inches T_{CROWN} = Distance from Curb Face to Street Crown 14.0 Gutter Width 2.00 Street Transverse Slope S_X = 0.021 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) S_{W} 0.083 ft/ft Street Longitudinal Slope - Enter 0 for sump condition Manning's Roughness for Street Section (typically between 0.012 and 0.020) S_{0} 0.000 ft/ft n_{STREET} = 0.012 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm T_{MAX} = 7.0 14.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm linches 6.0 12.0 Check boxes are not applicable in SUMP conditions Major Storm MINOR STORM Allowable Capacity is based on Depth Criterion Minor Storm MAJOR STORM Allowable Capacity is based on Depth Criterion SUMP SUMP



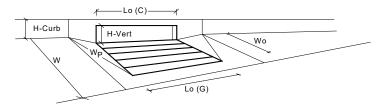
Design Information (Innut)		MINOR	MAJOR	
Design Information (Input) CDOT Type R Curb Opening	Type =		Curb Opening	1
Local Depression (additional to continuous gutter depression 'a' from above)	,, I	3.00	3.00	inches
	a _{local} =		5.00	linches
Number of Unit Inlets (Grate or Curb Opening)	No =	5)	in also a
Water Depth at Flowline (outside of local depression)	Ponding Depth =	6.0	12.0	inches
Grate Information	. (6)	MINOR	MAJOR	Override Depths
Length of a Unit Grate	L ₀ (G) =	N/A	N/A	feet
Width of a Unit Grate	$W_0 =$	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	_
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_f(G) =$	N/A	N/A	4
Grate Weir Coefficient (typical value 2.15 - 3.60)	C _w (G) =	N/A	N/A	_
Grate Orifice Coefficient (typical value 0.60 - 0.80)	$C_o(G) = [$	N/A	N/A	
<u>Curb Opening Information</u>	1	MINOR	MAJOR	٦.
Length of a Unit Curb Opening	$L_{o}(C) =$	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	$H_{throat} =$	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	$W_p = [$	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_o(C) = $	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	Tft .
Depth for Curb Opening Weir Equation	d _{Curb} =	0.33	0.83	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	0.57	1.00	1
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	0.79	1.00	1
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A	1
				_
L		MINOR	MAJOR	٦.
Total Inlet Interception Capacity (assumes clogged condition)	Q _a =	22.9	66.3	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	19.8	45.1	cfs

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: Grandview Reserve
Inlet ID: Inlet 4 (DP 5)



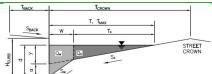
Gutter Geometry: Maximum Allowable Width for Spread Behind Curb 7.5 Side Slope Behind Curb (leave blank for no conveyance credit behind curb)
Manning's Roughness Behind Curb (typically between 0.012 and 0.020) ft/ft $S_{BACK} =$ 0.020 $n_{BACK} =$ 0.012 Height of Curb at Gutter Flow Line H_{CURB} = 6.00 inches T_{CROWN} = Distance from Curb Face to Street Crown 14.0 Gutter Width 2.00 Street Transverse Slope S_X = 0.014 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) S_{W} 0.083 ft/ft Street Longitudinal Slope - Enter 0 for sump condition Manning's Roughness for Street Section (typically between 0.012 and 0.020) S_{0} 0.000 ft/ft n_{STREET} = 0.012 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm T_{MAX} = 7.0 14.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm linches 6.0 12.0 Check boxes are not applicable in SUMP conditions Major Storm MINOR STORM Allowable Capacity is based on Depth Criterion Minor Storm MAJOR STORM Allowable Capacity is based on Depth Criterion SUMP SUMP



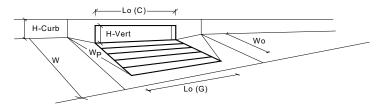
Design Information (Input)		MINOR	MAJOR	
Type of Inlet CDOT Type R Curb Opening	Type =		Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	7
Water Depth at Flowline (outside of local depression)	Ponding Depth =	6.0	12.0	inches
Grate Information		MINOR	MAJOR	Override Depths
Length of a Unit Grate	L, (G) =	N/A	N/A	feet
Width of a Unit Grate	W ₀ =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	7
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	C _f (G) =	N/A	N/A	1
Grate Weir Coefficient (typical value 2.15 - 3.60)	C _w (G) =	N/A	N/A	7
Grate Orifice Coefficient (typical value 0.60 - 0.80)	C ₀ (G) =	N/A	N/A	7
Curb Opening Information	-	MINOR	MAJOR	-
Length of a Unit Curb Opening	$L_o(C) = [$	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	$H_{throat} = $	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	$W_p = [$	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_o(C) = $	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	Πft
Depth for Curb Opening Weir Equation	d _{Curb} =	0.33	0.83	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	0.77	1.00	7
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	1.00	1.00	7
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A	
		MATHOD		
Tabal Talah Tahanan dian Canasib (0 -	MINOR	MAJOR	٦
Total Inlet Interception Capacity (assumes clogged condition)	Q _a =	5.4 1.6	12.3 3.0	cfs cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	1.0] 3.0	Jus

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: Grandview Reserve
Inlet ID: Inlet 5 (DP 6)



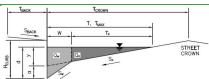
Gutter Geometry: Maximum Allowable Width for Spread Behind Curb 7.5 Side Slope Behind Curb (leave blank for no conveyance credit behind curb)
Manning's Roughness Behind Curb (typically between 0.012 and 0.020) ft/ft $S_{BACK} =$ 0.020 $n_{BACK} =$ 0.012 Height of Curb at Gutter Flow Line H_{CURB} = 6.00 inches T_{CROWN} = Distance from Curb Face to Street Crown 14.0 Gutter Width 2.00 Street Transverse Slope S_X = 0.017 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) S_{W} 0.083 ft/ft Street Longitudinal Slope - Enter 0 for sump condition Manning's Roughness for Street Section (typically between 0.012 and 0.020) S_{0} 0.000 ft/ft n_{STREET} = 0.012 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm T_{MAX} = 7.0 14.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm linches 6.0 12.0 Check boxes are not applicable in SUMP conditions Major Storm MINOR STORM Allowable Capacity is based on Depth Criterion Minor Storm MAJOR STORM Allowable Capacity is based on Depth Criterion SUMP SUMP



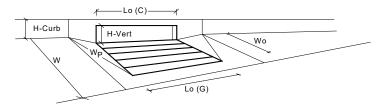
Design Information (Input) CDOT Type R Curb Opening	-	MINOR	MAJOR	_
Type of Inlet	Type =	CDOT Type R		1
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	_
Water Depth at Flowline (outside of local depression)	Ponding Depth =	6.0	12.0	inches
Grate Information	_	MINOR	MAJOR	Override Depths
Length of a Unit Grate	L₀ (G) =	N/A	N/A	feet
Width of a Unit Grate	$W_o = $	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	$A_{ratio} =$	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_f(G) = [$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	$C_w(G) = $	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	C₀ (G) =	N/A	N/A	
Curb Opening Information	-	MINOR	MAJOR	-
Length of a Unit Curb Opening	$L_o(C) = $	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H _{throat} =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	$W_p = $	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	C _w (C) =	3.60	3.60]
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_o(C) =$	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	Π _{ft}
Depth for Curb Opening Weir Equation	d _{Curb} =	0.33	0.83	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	0.77	1.00	1"
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	1.00	1.00	†
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A	1
	· · · Grace	,	7	_
	_	MINOR	MAJOR	_
Total Inlet Interception Capacity (assumes clogged condition)	$Q_a =$	5.4	12.3	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	4.7	11.5	cfs

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: Grandview Reserve
Inlet ID: Inlet 6 (DP 7)



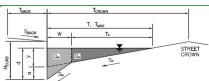
Gutter Geometry: Maximum Allowable Width for Spread Behind Curb 7.5 Side Slope Behind Curb (leave blank for no conveyance credit behind curb)
Manning's Roughness Behind Curb (typically between 0.012 and 0.020) ft/ft $S_{BACK} =$ 0.020 $n_{BACK} =$ 0.012 Height of Curb at Gutter Flow Line H_{CURB} = 6.00 inches T_{CROWN} = Distance from Curb Face to Street Crown 14.0 Gutter Width 2.00 Street Transverse Slope S_X = 0.033 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) S_{W} 0.083 ft/ft Street Longitudinal Slope - Enter 0 for sump condition Manning's Roughness for Street Section (typically between 0.012 and 0.020) S_{0} 0.000 ft/ft n_{STREET} = 0.012 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm T_{MAX} = 7.0 14.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm linches 6.0 12.0 Check boxes are not applicable in SUMP conditions Major Storm MINOR STORM Allowable Capacity is based on Depth Criterion Minor Storm MAJOR STORM Allowable Capacity is based on Depth Criterion SUMP SUMP



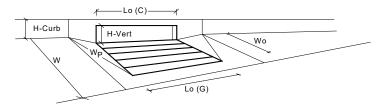
Design Information (Input)		MINOR	MAJOR	
Type of Inlet CDOT Type R Curb Opening	Type =		Curb Opening	1
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	1
Water Depth at Flowline (outside of local depression)	Ponding Depth =	6.0	12.0	inches
Grate Information		MINOR	MAJOR	✓ Override Depths
Length of a Unit Grate	L, (G) =	N/A	N/A	feet
Width of a Unit Grate	W _o =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	1
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_f(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C _w (G) =	N/A	N/A	1
Grate Orifice Coefficient (typical value 0.60 - 0.80)	$C_o(G) = $	N/A	N/A	
Curb Opening Information	-	MINOR	MAJOR	-
Length of a Unit Curb Opening	$L_o(C) = [$	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	$H_{throat} =$	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	$W_p = $	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_o(C) = $	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	∃ft
Depth for Curb Opening Weir Equation	d _{Curb} =	0.33	0.83	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	0.77	1.00	1
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	1.00	1.00	1
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A	
		MATERIAL		
Tabal Talah Tahanan dian Canasib (0 -	MINOR	MAJOR 12.3	7.4.
Total Inlet Interception Capacity (assumes clogged condition)	Q _a =	5.4 2.3	8.4	cfs cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	2.3	0.4	lrin

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: Grandview Reserve
Inlet ID: Inlet 7 (DP 9)



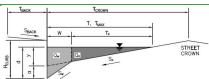
Gutter Geometry: Maximum Allowable Width for Spread Behind Curb 7.5 Side Slope Behind Curb (leave blank for no conveyance credit behind curb)
Manning's Roughness Behind Curb (typically between 0.012 and 0.020) ft/ft $S_{BACK} =$ 0.020 $n_{BACK} =$ 0.012 Height of Curb at Gutter Flow Line H_{CURB} = 6.00 inches T_{CROWN} = Distance from Curb Face to Street Crown 14.0 Gutter Width 2.00 Street Transverse Slope S_X = 0.017 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) S_{W} 0.083 ft/ft Street Longitudinal Slope - Enter 0 for sump condition Manning's Roughness for Street Section (typically between 0.012 and 0.020) S_{0} 0.000 ft/ft n_{STREET} = 0.012 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm T_{MAX} = 7.0 14.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm linches 6.0 12.0 Check boxes are not applicable in SUMP conditions Major Storm MINOR STORM Allowable Capacity is based on Depth Criterion Minor Storm MAJOR STORM Allowable Capacity is based on Depth Criterion SUMP SUMP



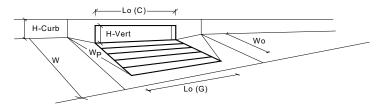
Design Information (Innut)		MINOR	MAJOR	
Design Information (Input) CDOT Type R Curb Opening	T.ma _ [Curb Opening	1
70	Type =	3.00		inches
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	0.00	3.00	Inches
Number of Unit Inlets (Grate or Curb Opening)	No =	2	2	- l. ,
Water Depth at Flowline (outside of local depression)	Ponding Depth =	6.0	12.0	inches
Grate Information	. (6) [MINOR	MAJOR	Override Depths
Length of a Unit Grate	L ₀ (G) =	N/A	N/A	feet
Width of a Unit Grate	$W_o =$	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	C _f (G) =	N/A	N/A	_
Grate Weir Coefficient (typical value 2.15 - 3.60)	C _w (G) =	N/A	N/A	_
Grate Orifice Coefficient (typical value 0.60 - 0.80)	$C_o(G) = [$	N/A	N/A	_
<u>Curb Opening Information</u>		MINOR	MAJOR	٦.
Length of a Unit Curb Opening	$L_o(C) =$	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	$H_{throat} =$	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	$W_p = [$	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_o(C) = $	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	Π _{ft}
Depth for Curb Opening Weir Equation	d _{Curb} =	0.33	0.83	fft
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	0.57	1.00	1"
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	0.93	1.00	†
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A	†
States Affect Growniance readeds actor for Early Infect	ro Grate — [.4/1	_
	_	MINOR	MAJOR	_
Total Inlet Interception Capacity (assumes clogged condition)	Q _a =	10.5	25.5	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	6.6	16.0	cfs

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: Grandview Reserve
Inlet ID: Inlet 8 (DP 10)



Gutter Geometry: Maximum Allowable Width for Spread Behind Curb 7.5 Side Slope Behind Curb (leave blank for no conveyance credit behind curb)
Manning's Roughness Behind Curb (typically between 0.012 and 0.020) ft/ft $S_{BACK} =$ 0.020 $n_{BACK} =$ 0.012 Height of Curb at Gutter Flow Line H_{CURB} = 6.00 inches T_{CROWN} = Distance from Curb Face to Street Crown 14.0 Gutter Width 2.00 Street Transverse Slope S_X = 0.016 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) S_{W} 0.083 ft/ft Street Longitudinal Slope - Enter 0 for sump condition Manning's Roughness for Street Section (typically between 0.012 and 0.020) S_{0} 0.000 ft/ft n_{STREET} = 0.012 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm T_{MAX} = 7.0 14.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm linches 6.0 12.0 Check boxes are not applicable in SUMP conditions Major Storm MINOR STORM Allowable Capacity is based on Depth Criterion Minor Storm MAJOR STORM Allowable Capacity is based on Depth Criterion SUMP SUMP

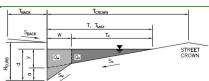


Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	13.1	29.3	cfs
Total Inlet Interception Capacity (assumes clogged condition)	Q _a =	13.5	39.1	cfs
	_	MINOR	MAJOR	_
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} = [N/A	N/A	_
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =			4
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	0.57	1.00	4
Depth for Curb Opening Weir Equation	d _{Curb} =	0.33		- '`
Depth for Grate Midwidth	d _{Grate} =	N/A 0.33	N/A 0.83	_ft ft
Low Head Performance Reduction (Calculated)	٦ .	MINOR	MAJOR	٦4
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_{o}(C) = [$	0.67	0.67	_
Curb Opening Weir Coefficient (typical value 2.3-3.7)	C _w (C) =	3.60	3.60	4
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	4
Side Width for Depression Pan (typically the gutter width of 2 feet)	$W_p = $	2.00	2.00	feet
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Height of Curb Orifice Throat in Inches	$H_{throat} =$	6.00	6.00	inches
Height of Vertical Curb Opening in Inches	$H_{vert} =$	6.00	6.00	inches
Length of a Unit Curb Opening	$L_o(C) =$	5.00	5.00	feet
Curb Opening Information		MINOR	MAJOR	_
Grate Orifice Coefficient (typical value 0.60 - 0.80)	$C_o(G) = $	N/A	N/A	_
Grate Weir Coefficient (typical value 2.15 - 3.60)	C_w (G) =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_f(G) =$	N/A	N/A	
Area Opening Ratio for a Grate (typical values 0.15-0.90)	$A_{ratio} =$	N/A	N/A	
Width of a Unit Grate	$W_o = $	N/A	N/A	feet
Length of a Unit Grate	L₀ (G) =	N/A	N/A	feet
Grate Information	L	MINOR	MAJOR	Override Depths
Water Depth at Flowline (outside of local depression)	Ponding Depth =	6.0	12.0	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	3	3	1
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Type of Inlet CDOT Type R Curb Opening	Type =	CDOT Type R	Curb Opening	
Design Information (Input)		MINOR	MAJOR	

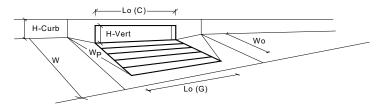
(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: Grandview Reserve
Inlet ID: Inlet 9 (DP 11)

nlet 9 (DP 11)



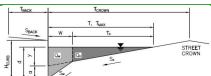
Gutter Geometry: Maximum Allowable Width for Spread Behind Curb 7.5 Side Slope Behind Curb (leave blank for no conveyance credit behind curb)
Manning's Roughness Behind Curb (typically between 0.012 and 0.020) ft/ft $S_{BACK} =$ 0.020 $n_{BACK} =$ 0.012 Height of Curb at Gutter Flow Line H_{CURB} = 6.00 inches T_{CROWN} = Distance from Curb Face to Street Crown 14.0 Gutter Width 2.00 Street Transverse Slope S_X = 0.010 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) S_{W} 0.083 ft/ft Street Longitudinal Slope - Enter 0 for sump condition Manning's Roughness for Street Section (typically between 0.012 and 0.020) S_{0} 0.000 ft/ft n_{STREET} = 0.012 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm T_{MAX} = 7.0 14.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm linches 6.0 12.0 Check boxes are not applicable in SUMP conditions Major Storm MINOR STORM Allowable Capacity is based on Depth Criterion Minor Storm MAJOR STORM Allowable Capacity is based on Depth Criterion SUMP SUMP



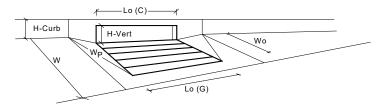
Design Information (Input)		MINOR	MAJOR	
Type of Inlet CDOT Type R Curb Opening	Type =		Curb Opening	1
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	6.0	12.0	inches
Grate Information	_	MINOR	MAJOR	Override Depths
Length of a Unit Grate	$L_o(G) = $	N/A	N/A	feet
Width of a Unit Grate	$W_o =$	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	$A_{ratio} =$	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_f(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C_w (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	C₀ (G) =	N/A	N/A	
<u>Curb Opening Information</u>		MINOR	MAJOR	_
Length of a Unit Curb Opening	$L_{o}(C) = L$	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	$H_{throat} =$	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	$W_p = $	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_o(C) = $	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	Tft .
Depth for Curb Opening Weir Equation	d _{Curb} =	0.33	0.83	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	0.77	1.00	1
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	1.00	1.00	1
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A]
		MINOR	MAJOR	
Total Inlet Interception Capacity (assumes clogged condition)	Q _a = [5.4	12.3	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	3.1	6.0	cfs

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: Grandview Reserve
Inlet ID: Inlet 10 (DP 12)



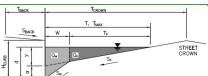
Gutter Geometry: Maximum Allowable Width for Spread Behind Curb 7.5 Side Slope Behind Curb (leave blank for no conveyance credit behind curb)
Manning's Roughness Behind Curb (typically between 0.012 and 0.020) ft/ft $S_{BACK} =$ 0.020 $n_{BACK} =$ 0.012 Height of Curb at Gutter Flow Line H_{CURB} = 6.00 inches T_{CROWN} = Distance from Curb Face to Street Crown 14.0 Gutter Width 2.00 Street Transverse Slope S_X = 0.017 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) S_{W} 0.083 ft/ft Street Longitudinal Slope - Enter 0 for sump condition Manning's Roughness for Street Section (typically between 0.012 and 0.020) S_{0} 0.000 ft/ft n_{STREET} = 0.012 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm T_{MAX} = 7.0 14.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm linches 6.0 12.0 Check boxes are not applicable in SUMP conditions Major Storm MINOR STORM Allowable Capacity is based on Depth Criterion Minor Storm MAJOR STORM Allowable Capacity is based on Depth Criterion SUMP SUMP



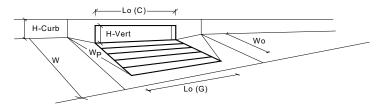
Design Information (Input)		MINOR	MAJOR	
Type of Inlet CDOT Type R Curb Opening	Type =		Curb Opening	1
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	4	4	7
Water Depth at Flowline (outside of local depression)	Ponding Depth =	6.0	12.0	inches
Grate Information	_	MINOR	MAJOR	Override Depths
Length of a Unit Grate	$L_{o}(G) = $	N/A	N/A	feet
Width of a Unit Grate	$W_o =$	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	$A_{ratio} =$	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_f(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C_w (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	$C_o(G) =$	N/A	N/A	
Curb Opening Information		MINOR	MAJOR	_
Length of a Unit Curb Opening	$L_o(C) = $	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	$H_{throat} =$	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	$W_p = $	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_o(C) = $	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	∃ft
Depth for Curb Opening Weir Equation	d _{Curb} =	0.33	0.83	⊤ ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	0.57	1.00	7
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	0.79	1.00	7
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A]
		MINOR	MAJOR	
Total Inlet Interception Capacity (assumes clogged condition)	Q _a = [18.2	52.7	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	16.0	35.5	cfs

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: Grandview Reserve
Inlet ID: Inlet 11 (DP 13)



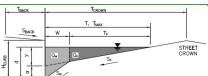
Gutter Geometry: Maximum Allowable Width for Spread Behind Curb 7.5 Side Slope Behind Curb (leave blank for no conveyance credit behind curb)
Manning's Roughness Behind Curb (typically between 0.012 and 0.020) ft/ft $S_{BACK} =$ 0.020 $n_{BACK} =$ 0.012 Height of Curb at Gutter Flow Line H_{CURB} = 6.00 inches T_{CROWN} = Distance from Curb Face to Street Crown 14.0 Gutter Width 2.00 Street Transverse Slope S_X = 0.021 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) S_{W} 0.083 ft/ft Street Longitudinal Slope - Enter 0 for sump condition Manning's Roughness for Street Section (typically between 0.012 and 0.020) S_{0} 0.000 ft/ft n_{STREET} = 0.012 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm T_{MAX} = 7.0 14.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm linches 6.0 12.0 Check boxes are not applicable in SUMP conditions Major Storm MINOR STORM Allowable Capacity is based on Depth Criterion Minor Storm MAJOR STORM Allowable Capacity is based on Depth Criterion SUMP SUMP



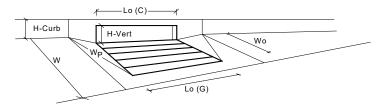
Design Information (Input) CDOT Type R Curb Opening		MINOR	MAJOR	
Type of Inlet	Type =		Curb Opening	٠
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	_
Water Depth at Flowline (outside of local depression)	Ponding Depth =	6.0	12.0	inches
Grate Information	-	MINOR	MAJOR	Override Depths
Length of a Unit Grate	$L_{o}(G) =$	N/A	N/A	feet
Width of a Unit Grate	$W_o = $	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	$A_{ratio} = $	N/A	N/A	_
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_f(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C_w (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	$C_o(G) = L$	N/A	N/A	╛
<u>Curb Opening Information</u>	_	MINOR	MAJOR	_
Length of a Unit Curb Opening	$L_{o}(C) = L$	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	$H_{vert} = L$	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	$H_{throat} =$	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	$W_p = L$	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_o(C) = $	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	Πft
Depth for Curb Opening Weir Equation	d _{Curb} =	0.33	0.83	⊤ ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	0.77	1.00	7
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	1.00	1.00	7
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A	
		MINOR	MAJOR	
Total Inlet Interception Capacity (assumes cloqged condition)	Q _a = [5.4	12.3	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	4.7	10.4	cfs

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: Grandview Reserve
Inlet ID: Inlet 12 (DP 14)



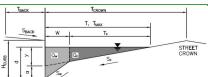
Gutter Geometry: Maximum Allowable Width for Spread Behind Curb 7.5 Side Slope Behind Curb (leave blank for no conveyance credit behind curb)
Manning's Roughness Behind Curb (typically between 0.012 and 0.020) ft/ft $S_{BACK} =$ 0.020 $n_{BACK} =$ 0.012 Height of Curb at Gutter Flow Line H_{CURB} = 6.00 inches T_{CROWN} = Distance from Curb Face to Street Crown 14.0 Gutter Width 2.00 Street Transverse Slope S_X = 0.020 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) S_{W} 0.083 ft/ft Street Longitudinal Slope - Enter 0 for sump condition Manning's Roughness for Street Section (typically between 0.012 and 0.020) S_{0} 0.000 ft/ft n_{STREET} = 0.012 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm T_{MAX} = 7.0 14.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm inches 6.0 12.0 Check boxes are not applicable in SUMP conditions Major Storm MINOR STORM Allowable Capacity is based on Depth Criterion Minor Storm MAJOR STORM Allowable Capacity is based on Depth Criterion SUMP SUMP



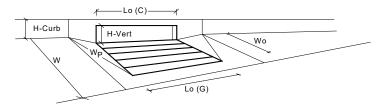
Design Information (Input)		MINOR	MAJOR	
Type of Inlet CDOT Type R Curb Opening	Type =		Curb Opening	1
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	1
Water Depth at Flowline (outside of local depression)	Ponding Depth =	6.0	12.0	inches
Grate Information		MINOR	MAJOR	✓ Override Depths
Length of a Unit Grate	L, (G) =	N/A	N/A	feet
Width of a Unit Grate	W _o =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	1
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_f(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C _w (G) =	N/A	N/A	1
Grate Orifice Coefficient (typical value 0.60 - 0.80)	C ₀ (G) =	N/A	N/A	1
Curb Opening Information	-	MINOR	MAJOR	-
Length of a Unit Curb Opening	$L_o(C) = [$	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	$H_{throat} = $	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	$W_p = [$	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) = $	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_o(C) = $	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	∃ft
Depth for Curb Opening Weir Equation	d _{Curb} =	0.33	0.83	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	0.77	1.00	1
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	1.00	1.00	1
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A	
		MINOR	MAJOR	
Total Inlet Interception Canacity (accumes closued condition)	Q _a = [MINOR 5.4	MAJOR 12.3	cfs
Total Inlet Interception Capacity (assumes clogged condition)	$Q_a = Q_a = Q_a$ $Q_{PEAK REQUIRED} = Q_a$	3.9	8.8	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	✓ PEAK REQUIRED —	J.7	1 0.0	Lus

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: Grandview Reserve
Inlet ID: Inlet 13 (DP 15)



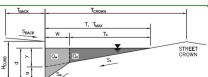
Gutter Geometry: Maximum Allowable Width for Spread Behind Curb 7.5 Side Slope Behind Curb (leave blank for no conveyance credit behind curb)
Manning's Roughness Behind Curb (typically between 0.012 and 0.020) ft/ft $S_{BACK} =$ 0.020 $n_{BACK} =$ 0.012 Height of Curb at Gutter Flow Line H_{CURB} = 6.00 inches T_{CROWN} = Distance from Curb Face to Street Crown 14.0 Gutter Width 2.00 Street Transverse Slope S_X = 0.020 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) S_{W} 0.083 ft/ft Street Longitudinal Slope - Enter 0 for sump condition Manning's Roughness for Street Section (typically between 0.012 and 0.020) S_{0} 0.000 ft/ft n_{STREET} = 0.012 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm T_{MAX} = 7.0 14.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm inches 6.0 12.0 Check boxes are not applicable in SUMP conditions Major Storm MINOR STORM Allowable Capacity is based on Depth Criterion Minor Storm MAJOR STORM Allowable Capacity is based on Depth Criterion SUMP SUMP



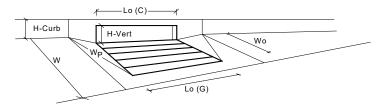
Design Information (Input)		MINOR	MAJOR	
Type of Inlet CDOT Type R Curb Opening	Type =	CDOT Type R Curb Opening		
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	1
Water Depth at Flowline (outside of local depression)	Ponding Depth =	6.0	12.0	inches
Grate Information	_	MINOR	MAJOR	Override Depths
Length of a Unit Grate	$L_{o}(G) = $	N/A	N/A	feet
Width of a Unit Grate	$W_o =$	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_f(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C_w (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	C₀ (G) =	N/A	N/A	
<u>Curb Opening Information</u>		MINOR	MAJOR	_
Length of a Unit Curb Opening	$L_{o}(C) = L$	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	$H_{throat} =$	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	$W_p = L$	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_o(C) = $	0.67	0.67	
 Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A]ft
Depth for Curb Opening Weir Equation	d _{Curb} =	0.33	0.83	f ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	0.77	1.00	1
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	1.00	1.00	1
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A]
		MINOR	MAJOR	
Total Inlet Interception Capacity (assumes clogged condition)	0 _a = [5.4	12.3	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	2.4	5.3	cfs

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: Grandview Reserve
Inlet ID: Inlet 14 (DP 17)



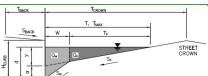
Gutter Geometry: Maximum Allowable Width for Spread Behind Curb 7.5 Side Slope Behind Curb (leave blank for no conveyance credit behind curb)
Manning's Roughness Behind Curb (typically between 0.012 and 0.020) ft/ft $S_{BACK} =$ 0.020 $n_{BACK} =$ 0.012 Height of Curb at Gutter Flow Line H_{CURB} = 6.00 inches T_{CROWN} = Distance from Curb Face to Street Crown 14.0 Gutter Width 2.00 Street Transverse Slope S_X = 0.013 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) S_{W} 0.083 ft/ft Street Longitudinal Slope - Enter 0 for sump condition Manning's Roughness for Street Section (typically between 0.012 and 0.020) S_{0} 0.000 ft/ft n_{STREET} = 0.012 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm T_{MAX} = 7.0 14.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm inches 6.0 12.0 Check boxes are not applicable in SUMP conditions Major Storm MINOR STORM Allowable Capacity is based on Depth Criterion Minor Storm MAJOR STORM Allowable Capacity is based on Depth Criterion SUMP SUMP



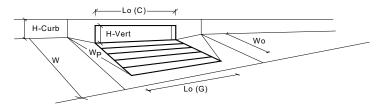
Design Information (Input)		MINOR	MAJOR	
Type of Inlet CDOT Type R Curb Opening	Type =		Curb Opening	1
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	9	9	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	6.0	12.0	inches
Grate Information	ronang papar [MINOR	MAJOR	✓ Override Depths
Length of a Unit Grate	L ₀ (G) =	N/A	N/A	Ifeet
Width of a Unit Grate	W ₀ =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	1
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	C _f (G) =	N/A	N/A	1
Grate Weir Coefficient (typical value 2.15 - 3.60)	C _w (G) =	N/A	N/A	7
Grate Orifice Coefficient (typical value 0.60 - 0.80)	C _o (G) =	N/A	N/A	7
Curb Opening Information		MINOR	MAJOR	-
Length of a Unit Curb Opening	$L_o(C) = [$	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	$H_{throat} =$	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	$W_p = $	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$	3.60	3.60	_
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_o(C) = $	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	∃ft
Depth for Curb Opening Weir Equation	d _{Curb} =	0.33	0.83	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	0.57	1.00	1
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	0.79	1.00	7
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A	
L	a 1	MINOR	MAJOR	٦.
Total Inlet Interception Capacity (assumes clogged condition)	Q _a =	41.7	120.8	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	40.3	89.9	cfs

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: Grandview Reserve
Inlet ID: Inlet 15 (DP 18)



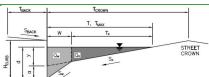
Gutter Geometry: Maximum Allowable Width for Spread Behind Curb 7.5 Side Slope Behind Curb (leave blank for no conveyance credit behind curb)
Manning's Roughness Behind Curb (typically between 0.012 and 0.020) ft/ft $S_{BACK} =$ 0.020 $n_{BACK} =$ 0.012 Height of Curb at Gutter Flow Line H_{CURB} = 6.00 inches T_{CROWN} = Distance from Curb Face to Street Crown 14.0 Gutter Width 2.00 Street Transverse Slope S_X = 0.015 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) S_{W} 0.083 ft/ft Street Longitudinal Slope - Enter 0 for sump condition Manning's Roughness for Street Section (typically between 0.012 and 0.020) S_{0} 0.000 ft/ft n_{STREET} = 0.012 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm T_{MAX} = 7.0 14.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm inches 6.0 12.0 Check boxes are not applicable in SUMP conditions Major Storm MINOR STORM Allowable Capacity is based on Depth Criterion Minor Storm MAJOR STORM Allowable Capacity is based on Depth Criterion SUMP SUMP



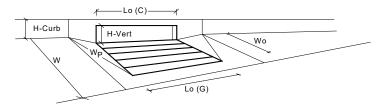
Design Information (Input)		MINOR	MAJOR	
Type of Inlet CDOT Type R Curb Opening	Type =	CDOT Type R Curb Opening		1
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	3	3	1
Water Depth at Flowline (outside of local depression)	Ponding Depth =	6.0	12.0	inches
Grate Information	, <u>.</u>	MINOR	MAJOR	✓ Override Depths
Length of a Unit Grate	L₀ (G) =	N/A	N/A	feet
Width of a Unit Grate	$W_o =$	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	1
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_f(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C_w (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	C₀ (G) =	N/A	N/A	
<u>Curb Opening Information</u>		MINOR	MAJOR	_
Length of a Unit Curb Opening	$L_{o}(C) = L$	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	$H_{vert} =$	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	$H_{throat} =$	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	$W_p = $	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$	3.60	3.60	_
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_o(C) = $	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	Tft .
Depth for Curb Opening Weir Equation	d _{Curb} =	0.33	0.83	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	0.57	1.00	1
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	0.79	1.00	1
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A	
		MINOR	MAJOR	
Total Inlet Interception Capacity (assumes clogged condition)	0 _a = [13.5	39.1	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	12.9	29.8	cfs

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: Grandview Reserve
Inlet ID: Inlet 16 (DP 19)



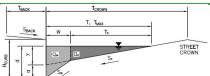
Gutter Geometry: Maximum Allowable Width for Spread Behind Curb 7.5 Side Slope Behind Curb (leave blank for no conveyance credit behind curb)
Manning's Roughness Behind Curb (typically between 0.012 and 0.020) ft/ft $S_{BACK} =$ 0.020 $n_{BACK} =$ 0.012 Height of Curb at Gutter Flow Line H_{CURB} = 6.00 inches T_{CROWN} = Distance from Curb Face to Street Crown 14.0 Gutter Width 2.00 Street Transverse Slope S_X = 0.012 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) S_{W} 0.083 ft/ft Street Longitudinal Slope - Enter 0 for sump condition Manning's Roughness for Street Section (typically between 0.012 and 0.020) S_{0} 0.000 ft/ft n_{STREET} = 0.012 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm T_{MAX} = 7.0 14.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm inches 6.0 12.0 Check boxes are not applicable in SUMP conditions Major Storm MINOR STORM Allowable Capacity is based on Depth Criterion Minor Storm MAJOR STORM Allowable Capacity is based on Depth Criterion SUMP SUMP



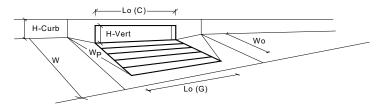
D: I-f (I		MINOR	144300	
Design Information (Input) CDOT Type R Curb Opening	- 1	MINOR	MAJOR	1
Type of Inlet	Type =		Curb Opening	ļ. ,
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	6.0	12.0	inches
<u>Grate Information</u>	,	MINOR	MAJOR	Override Depths
Length of a Unit Grate	L₀ (G) =	N/A	N/A	feet
Width of a Unit Grate	$W_o = [$	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_f(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C_w (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	C₀ (G) =	N/A	N/A	
<u>Curb Opening Information</u>		MINOR	MAJOR	
Length of a Unit Curb Opening	$L_{o}(C) = [$	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	$H_{vert} = $	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	$H_{throat} = [$	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	$W_p = [$	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) = $	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_o(C) = $	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	∃ft
Depth for Curb Opening Weir Equation		0.33	0.83	ft
Combination Inlet Performance Reduction Factor for Long Inlets	d _{Curb} =	0.33	1.00	- ''
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Combination} =	1.00	1.00	-
	RF _{Curb} =			-
Grated Inlet Performance Reduction Factor for Long Inlets	$RF_{Grate} = [$	N/A	N/A	_
		MINOR	MAJOR	
Total Inlet Interception Capacity (assumes clogged condition)	Q _a =	5.4	12.3	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	0.9	2.5	cfs

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: Grandview Reserve
Inlet ID: Inlet 17 (DP 20)



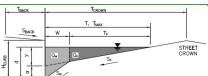
Gutter Geometry: Maximum Allowable Width for Spread Behind Curb 7.5 Side Slope Behind Curb (leave blank for no conveyance credit behind curb)
Manning's Roughness Behind Curb (typically between 0.012 and 0.020) ft/ft $S_{BACK} =$ 0.020 $n_{BACK} =$ 0.012 Height of Curb at Gutter Flow Line H_{CURB} = 6.00 inches T_{CROWN} = Distance from Curb Face to Street Crown 14.0 Gutter Width 2.00 Street Transverse Slope S_X = 0.009 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) S_{W} 0.083 ft/ft Street Longitudinal Slope - Enter 0 for sump condition Manning's Roughness for Street Section (typically between 0.012 and 0.020) S_{0} 0.000 ft/ft n_{STREET} = 0.012 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm T_{MAX} = 7.0 14.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm inches 6.0 12.0 Check boxes are not applicable in SUMP conditions Major Storm MINOR STORM Allowable Capacity is based on Depth Criterion Minor Storm MAJOR STORM Allowable Capacity is based on Depth Criterion SUMP SUMP



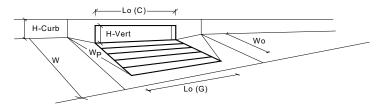
Design Information (Input) CDOT Type R Curb Opening		MINOR	MAJOR	_
Type of Inlet	Type =		Curb Opening	<u> </u>
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	<u> </u>
Water Depth at Flowline (outside of local depression)	Ponding Depth =	6.0	12.0	inches
Grate Information	_	MINOR	MAJOR	Override Depths
Length of a Unit Grate	L₀ (G) =	N/A	N/A	feet
Width of a Unit Grate	$W_o = $	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	$A_{ratio} =$	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_f(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C_w (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	$C_o(G) = [$	N/A	N/A	
Curb Opening Information		MINOR	MAJOR	
Length of a Unit Curb Opening	$L_o(C) = $	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	$H_{throat} = $	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	$W_p = [$	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) = [$	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_o(C) = $	0.67	0.67]
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	٦ _{ft} I
Depth for Curb Opening Weir Equation	d _{Curb} =	0.33	0.83	dft l
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	0.77	1.00	1
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	1.00	1.00	†
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A]
		MINOR	MATOR	
Tatal Julet Interception Conneits (consumer elegand condition)	0 -	MINOR 5.4	MAJOR 12.3	cfs
Total Inlet Interception Capacity (assumes clogged condition)	Q _a = Q	3.0	6.8	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	✓ PEAK REQUIRED —	5.0	0.0	LIS

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: Grandview Reserve
Inlet ID: Inlet 18 (DP 22)



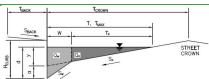
Gutter Geometry: Maximum Allowable Width for Spread Behind Curb 7.5 Side Slope Behind Curb (leave blank for no conveyance credit behind curb)
Manning's Roughness Behind Curb (typically between 0.012 and 0.020) ft/ft $S_{BACK} =$ 0.020 $n_{BACK} =$ 0.012 Height of Curb at Gutter Flow Line H_{CURB} = 6.00 inches T_{CROWN} = Distance from Curb Face to Street Crown 14.0 Gutter Width 2.00 Street Transverse Slope S_X = 0.017 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) S_{W} 0.083 ft/ft Street Longitudinal Slope - Enter 0 for sump condition Manning's Roughness for Street Section (typically between 0.012 and 0.020) S_{0} 0.000 ft/ft n_{STREET} = 0.012 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm T_{MAX} = 7.0 14.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm inches 6.0 12.0 Check boxes are not applicable in SUMP conditions Major Storm MINOR STORM Allowable Capacity is based on Depth Criterion Minor Storm MAJOR STORM Allowable Capacity is based on Depth Criterion SUMP SUMP



Design Information (Input)		MINOR	MAJOR	
Design Information (Input) CDOT Type R Curb Opening	Type =		Curb Opening	1
Local Depression (additional to continuous gutter depression 'a' from above)	,, I	3.00	3.00	inches
	a _{local} =		3.00	Inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	12.0	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	6.0	12.0	inches
Grate Information	. (6)	MINOR	MAJOR	Override Depths
Length of a Unit Grate	L ₀ (G) =	N/A	N/A	feet
Width of a Unit Grate	$W_0 =$	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	_
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_f(G) =$	N/A	N/A	4
Grate Weir Coefficient (typical value 2.15 - 3.60)	C _w (G) =	N/A	N/A	_
Grate Orifice Coefficient (typical value 0.60 - 0.80)	$C_o(G) = [$	N/A	N/A	_
<u>Curb Opening Information</u>	1	MINOR	MAJOR	٦.
Length of a Unit Curb Opening	$L_{o}(C) =$	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	$H_{throat} =$	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	$W_p = [$	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_o(C) = [$	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	l ft
Depth for Curb Opening Weir Equation	d _{Curb} =	0.33	0.83	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	0.77	1.00	1
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	1.00	1.00	1
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A	1
States Allect Stromands reduction actor for Long Thick	ro Grate — [, / 1		_
	_	MINOR	MAJOR	_
Total Inlet Interception Capacity (assumes clogged condition)	Q _a =	5.4	12.3	cfs
WARNING: Inlet Capacity less than Q Peak for Major Storm	Q PEAK REQUIRED =	5.1	12.3	cfs

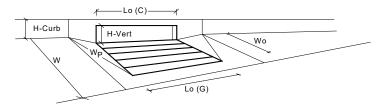
(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: Grandview Reserve
Inlet ID: Inlet 19 (DP 23)



Gutter Geometry: Maximum Allowable Width for Spread Behind Curb 7.5 Side Slope Behind Curb (leave blank for no conveyance credit behind curb)
Manning's Roughness Behind Curb (typically between 0.012 and 0.020) ft/ft $S_{BACK} =$ 0.020 $n_{BACK} =$ 0.012 Height of Curb at Gutter Flow Line H_{CURB} = 6.00 inches T_{CROWN} = Distance from Curb Face to Street Crown 14.0 Gutter Width 2.00 Street Transverse Slope S_X = 0.018 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) S_{W} 0.083 ft/ft Street Longitudinal Slope - Enter 0 for sump condition Manning's Roughness for Street Section (typically between 0.012 and 0.020) S_{0} 0.000 ft/ft n_{STREET} = 0.012 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm T_{MAX} = 7.0 14.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm inches 6.0 12.0 Check boxes are not applicable in SUMP conditions Major Storm MINOR STORM Allowable Capacity is based on Depth Criterion Minor Storm MAJOR STORM Allowable Capacity is based on Depth Criterion SUMP SUMP

INLET IN A SUMP OR SAG LOCATION MHFD-Inlet, Version 5.01 (April 2021)

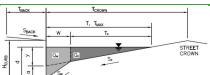


Design Information (Input)		MINOR	MAJOR	
Type of Inlet CDOT Type R Curb Opening	Type =		Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	1
Water Depth at Flowline (outside of local depression)	Ponding Depth =	6.0	12.0	inches
Grate Information		MINOR	MAJOR	✓ Override Depths
Length of a Unit Grate	L, (G) =	N/A	N/A	feet
Width of a Unit Grate	W _o =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	7
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_f(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C _w (G) =	N/A	N/A	7
Grate Orifice Coefficient (typical value 0.60 - 0.80)	C ₀ (G) =	N/A	N/A	7
Curb Opening Information	-	MINOR	MAJOR	-
Length of a Unit Curb Opening	$L_o(C) = [$	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	$H_{throat} = [$	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	$W_p = [$	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_o(C) = $	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	Πft
Depth for Curb Opening Weir Equation	d _{Curb} =	0.33	0.83	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	0.77	1.00	7
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	1.00	1.00	7
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A	
		MINOR	MAJOR	
Total Inlet Interception Canacity (accumes closued condition)	Q _a = [MINOR 5.4	MAJOR 12.3	cfs
Total Inlet Interception Capacity (assumes clogged condition)	$Q_a = Q_a = Q_a$ $Q_{PEAK REQUIRED} = Q_a$	2.4	4.9	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Y PEAK REQUIRED -	4.4	1 7.3	lrio

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

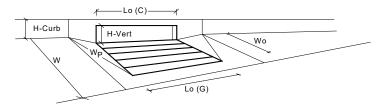
(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: Grandview Reserve
Inlet ID: Inlet 20 (DP 24)



Gutter Geometry: Maximum Allowable Width for Spread Behind Curb 7.5 Side Slope Behind Curb (leave blank for no conveyance credit behind curb)
Manning's Roughness Behind Curb (typically between 0.012 and 0.020) ft/ft $S_{BACK} =$ 0.020 $n_{BACK} =$ 0.012 Height of Curb at Gutter Flow Line H_{CURB} = 6.00 inches T_{CROWN} = Distance from Curb Face to Street Crown 14.0 Gutter Width 2.00 Street Transverse Slope S_X = 0.018 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) S_{W} 0.083 ft/ft Street Longitudinal Slope - Enter 0 for sump condition Manning's Roughness for Street Section (typically between 0.012 and 0.020) S_{0} 0.000 ft/ft n_{STREET} = 0.012 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm T_{MAX} = 7.0 14.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm inches 6.0 12.0 Check boxes are not applicable in SUMP conditions Major Storm MINOR STORM Allowable Capacity is based on Depth Criterion Minor Storm MAJOR STORM Allowable Capacity is based on Depth Criterion SUMP SUMP

INLET IN A SUMP OR SAG LOCATION MHFD-Inlet, Version 5.01 (April 2021)

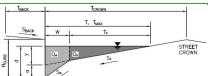


Design Information (Input)		MINOR	MAJOR	
Type of Inlet CDOT Type R Curb Opening	Type =		Curb Opening	1
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	2	2	1
Water Depth at Flowline (outside of local depression)	Ponding Depth =	6.0	12.0	inches
Grate Information	_	MINOR	MAJOR	Override Depths
Length of a Unit Grate	$L_{o}(G) = $	N/A	N/A	feet
Width of a Unit Grate	$W_o =$	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	$A_{ratio} =$	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_f(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C_w (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	$C_o(G) =$	N/A	N/A	
Curb Opening Information		MINOR	MAJOR	_
Length of a Unit Curb Opening	$L_o(C) = $	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	$H_{vert} =$	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	$H_{throat} =$	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	$W_p = L$	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_o(C) = $	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	קft −
Depth for Curb Opening Weir Equation	$d_{Curb} =$	0.33	0.83	f t
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	0.57	1.00	1
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	0.93	1.00	1
Grated Inlet Performance Reduction Factor for Long Inlets	$RF_{Grate} =$	N/A	N/A	
		MINOR	MAJOR	
Total Inlet Interception Capacity (assumes clogged condition)	Q _a = [10.5	25.5	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	9.1	21.5	cfs

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

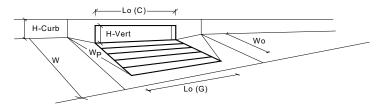
(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: Grandview Reserve
Inlet ID: Inlet 21 (DP 25)



Gutter Geometry: Maximum Allowable Width for Spread Behind Curb 7.5 Side Slope Behind Curb (leave blank for no conveyance credit behind curb)
Manning's Roughness Behind Curb (typically between 0.012 and 0.020) ft/ft $S_{BACK} =$ 0.020 $n_{BACK} =$ 0.012 Height of Curb at Gutter Flow Line H_{CURB} = 6.00 inches T_{CROWN} = Distance from Curb Face to Street Crown 14.0 Gutter Width 2.00 Street Transverse Slope S_X = 0.017 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) S_{W} 0.083 ft/ft Street Longitudinal Slope - Enter 0 for sump condition Manning's Roughness for Street Section (typically between 0.012 and 0.020) S_{0} 0.000 ft/ft n_{STREET} = 0.012 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm T_{MAX} = 7.0 14.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm inches 6.0 12.0 Check boxes are not applicable in SUMP conditions Major Storm MINOR STORM Allowable Capacity is based on Depth Criterion Minor Storm MAJOR STORM Allowable Capacity is based on Depth Criterion SUMP SUMP

INLET IN A SUMP OR SAG LOCATION MHFD-Inlet, Version 5.01 (April 2021)

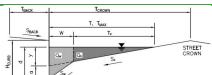


Design Information (Input)		MINOR	MAJOR	
Type of Inlet CDOT Type R Curb Opening	Type =		Curb Opening	1
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	2	2	1
Water Depth at Flowline (outside of local depression)	Ponding Depth =	6.0	12.0	inches
Grate Information	_	MINOR	MAJOR	Override Depths
Length of a Unit Grate	$L_{o}(G) = $	N/A	N/A	feet
Width of a Unit Grate	$W_o =$	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_f(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C_w (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	$C_o(G) =$	N/A	N/A	
<u>Curb Opening Information</u>		MINOR	MAJOR	_
Length of a Unit Curb Opening	$L_{o}(C) = L$	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	$H_{vert} = $	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	$H_{throat} =$	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	$W_p = L$	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) = $	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_o(C) = $	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	קft −
Depth for Curb Opening Weir Equation	d _{Curb} =	0.33	0.83	f t
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	0.57	1.00	1
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	0.93	1.00	1
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A	
		MINOR	MAJOR	
Total Inlet Interception Capacity (assumes clogged condition)	0 _a = [10.5	25.5	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	9.2	21.1	cfs

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

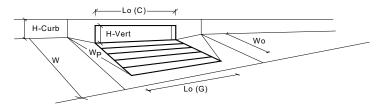
(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: Grandview Reserve
Inlet ID: Inlet 22 (DP 27)



Gutter Geometry: Maximum Allowable Width for Spread Behind Curb 7.5 Side Slope Behind Curb (leave blank for no conveyance credit behind curb)
Manning's Roughness Behind Curb (typically between 0.012 and 0.020) ft/ft $S_{BACK} =$ 0.020 $n_{BACK} =$ 0.012 Height of Curb at Gutter Flow Line H_{CURB} = 6.00 inches T_{CROWN} = Distance from Curb Face to Street Crown 14.0 Gutter Width 2.00 Street Transverse Slope S_X = 0.013 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) S_{W} 0.083 ft/ft Street Longitudinal Slope - Enter 0 for sump condition Manning's Roughness for Street Section (typically between 0.012 and 0.020) S_{0} 0.000 ft/ft n_{STREET} = 0.012 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm T_{MAX} = 7.0 14.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm inches 6.0 12.0 Check boxes are not applicable in SUMP conditions Major Storm MINOR STORM Allowable Capacity is based on Depth Criterion Minor Storm MAJOR STORM Allowable Capacity is based on Depth Criterion SUMP SUMP

INLET IN A SUMP OR SAG LOCATION MHFD-Inlet, Version 5.01 (April 2021)

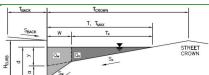


Desire Information (Insurt)		MINOR	144300	
Design Information (Input) CDOT Type R Curb Opening	[MINOR CDOT Type R	MAJOR Curb Opening	7
Type of Inlet	Type =			in also a
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	2	2	<u>.</u> .
Water Depth at Flowline (outside of local depression)	Ponding Depth =	6.0	12.0	inches
Grate Information		MINOR	MAJOR	Override Depths
Length of a Unit Grate	L ₀ (G) =	N/A	N/A	feet
Width of a Unit Grate	W _o =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	$A_{ratio} =$	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_f(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C_w (G) =	N/A	N/A	_
Grate Orifice Coefficient (typical value 0.60 - 0.80)	$C_o(G) = [$	N/A	N/A	
<u>Curb Opening Information</u>		MINOR	MAJOR	_
Length of a Unit Curb Opening	$L_o(C) =$	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	$H_{throat} =$	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	$W_p = [$	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_o(C) = [$	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	Π _{ft}
Depth for Curb Opening Weir Equation	d _{Curb} =	0.33	0.83	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	0.57	1.00	1 '
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	0.93	1.00	†
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A	1
	· · · · · · · ·	,	, ,,,	_
	_	MINOR	MAJOR	_
Total Inlet Interception Capacity (assumes clogged condition)	$Q_a = [$	10.5	25.5	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	8.0	21.0	cfs

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

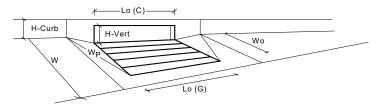
(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: Grandview Reserve
Inlet ID: Inlet 23 (DP 28)



Gutter Geometry: Maximum Allowable Width for Spread Behind Curb 7.5 Side Slope Behind Curb (leave blank for no conveyance credit behind curb)
Manning's Roughness Behind Curb (typically between 0.012 and 0.020) ft/ft $S_{BACK} =$ 0.020 $n_{BACK} =$ 0.012 Height of Curb at Gutter Flow Line H_{CURB} = 6.00 inches T_{CROWN} = Distance from Curb Face to Street Crown 14.0 Gutter Width 2.00 Street Transverse Slope S_X = 0.019 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) S_{W} 0.083 ft/ft Street Longitudinal Slope - Enter 0 for sump condition Manning's Roughness for Street Section (typically between 0.012 and 0.020) S_{0} 0.000 ft/ft n_{STREET} = 0.012 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm T_{MAX} = 7.0 14.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm inches 6.0 12.0 Check boxes are not applicable in SUMP conditions Major Storm MINOR STORM Allowable Capacity is based on Depth Criterion Minor Storm MAJOR STORM Allowable Capacity is based on Depth Criterion SUMP SUMP

INLET IN A SUMP OR SAG LOCATION MHFD-Inlet, Version 5.01 (April 2021)



Design Information (Input)		MINOR	MAJOR	
Type of Inlet CDOT Type R Curb Opening	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	4	4	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	6.0	12.0	inches
Grate Information		MINOR	MAJOR	Override Depths
Length of a Unit Grate	$L_{o}(G) = [$	N/A	N/A	feet
Width of a Unit Grate	$W_o = $	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	$A_{ratio} =$	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_f(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C _w (G) =	N/A	N/A	1
Grate Orifice Coefficient (typical value 0.60 - 0.80)	C₀ (G) =	N/A	N/A	
Curb Opening Information	_	MINOR	MAJOR	_
Length of a Unit Curb Opening	$L_{o}(C) = $	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H _{throat} =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	$W_p = $	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$	3.60	3.60	1
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_o(C) = $	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A]ft
Depth for Curb Opening Weir Equation	d _{Curb} =	0.33	0.83	T _{ft}
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	0.57	1.00	1
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	0.79	1.00	1
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A]
		MINOR	MAJOR	
Total Inlet Interception Capacity (assumes cloqged condition)	Q _a = [18.2	52.7	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q _{PEAK REQUIRED} =	15.4	38.2	cfs

Provide box culvert and channel calculations.

APPENDIX E Water Quality Computations

Detention Pond Tributary Areas

Subdivision: Grandview Reserve Project Name: Grandview Reserve

Location: CO, El Paso County
Project No.: HRG01
Calculated By: NJA
Checked By: CMD

Date: 8/11/21

Pond A

Basin	Area	% Imp
A-2	6.94	64.3
A-3	0.34	100
A-4	10.15	66.4
A-5	0.34	100
A-6	2.67	50.5
A-7	2.91	20
A-8	6.31	2
Total	29.66	47.0

Pond B

Basin	Area	% Imp
B-1	4.02	54.3
B-2	7.58	65.7
B-3	0.76	100
B-4	9.17	67.7
B-5	2.57	68.7
B-6	2.06	69.6
B-7	0.99	74.6
B-8	0.87	2
Total	24,00	66.3

Pond C 28? —

Basin	Area	% Imp
C-1	34.69	66.8
C-2	9.90	60.8
C-3	0.50	39.2
C-4	1.61	65.7
C-5	3.99	2
Total	16.00	46.0

50.69? ______ 60?

Pond D

Basin	Area	% Imp
D-1	2.46	56
D-2	0.75	81.8
D-3	4.76	62.4
D-4	4.74	65.3
D-5	1.71	2
Total	11.96	56.1

Pond E

I ond E		
Basin	Area	% Imp
E-1	6.86	47.1
E-2	11.66	53.8
E-3	1.71	2
Total	13,37	47.2

20.23?

Site-Level Low Impact Development (LID) Design Effective Impervious Calculator LID Credit by Impervious Reduction Factor (IRF) Method UD-BMP (Version 3.06, November 2016) User Input Calculated cells Designer: TJE Company: Galloway & Co. ***Design Storm: 1-Hour Rain Depth WQCV Event 0.60 August 12, 2021 Date: inches ***Minor Storm: 1-Hour Rain Depth 1.50 inches Project: Grandviewe Reserve ***Major Storm: 1-Hour Rain Depth 100-Year Event 2.52 inches Location: Pond A Optional User Defined Storm (CUHP) NOAA 1 Hour Rainfall Depth and Frequency 100-Year Event for User Defined Storm Max Intensity for Optional User Defined Storm SITE INFORMATION (USER-INPUT) A-2 A-3 A-4 A-5 A-6 A-7 A-8 Sub-basin Identifier Receiving Pervious Area Soil Type Sandy Loar andy Loam Total Area (ac., Sum of DCIA, UIA, RPA, & SPA) 0.340 10.150 0.340 2.670 2.910 6.310 6.940 4.462 0.340 6.740 0.340 1.348 0.582 0.126 Directly Connected Impervious Area (DCIA, acres) Unconnected Impervious Area (UIA, acres) 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 Receiving Pervious Area (RPA, acres) 2.478 0.000 3.410 0.000 1.322 2.328 6.184 Separate Pervious Area (SPA, acres) RPA Treatment Type: Conveyance (C) С С C С C С С Volume (V), or Permeable Pavement (PP) CALCULATED RESULTS (OUTPUT) Total Calculated Area (ac, check against input) 6.940 0.340 10.150 0.340 2.670 2.910 6.310 64.3% 100.0% 100.0% 50.5% 20.0% 2.0% 66.4% Directly Connected Impervious Area (DCIA, %) 0.0% 0.0% 0.0% 0.0% 0.0% 0.0% Unconnected Impervious Area (UIA, %) 0.0% Receiving Pervious Area (RPA, %) 0.0% 0.0% 0.0% 0.0% 0.0% 0.0% 0.0% Separate Pervious Area (SPA, %) 35.7% 0.0% 33.6% 0.0% 49.5% 80.0% 98.0% A_R (RPA / UIA) 0.000 0.000 0.000 0.000 0.000 0.000 0.000 I, Check 1 000 1 000 1 000 1 000 1 000 1 000 1 000 f / I for WQCV Event 1.7 1.7 1.7 1.7 1.7 1.7 1.7 f / I for 5-Year Event 0.5 0.5 0.5 0.5 0.5 0.5 0.5 f / I for 100-Year Event 0.3 0.3 0.3 0.3 0.3 0.3 0.3 f / I for Optional User Defined Storm CUHP: IRF for WQCV Event 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 IRF for 5-Year Event 1.00 1.00 IRF for 100-Year Event 1.00 1.00 1.00 1.00 1.00 1.00 1.00 Total Site Imperviousness: I.... 64.3% 100.0% 66.4% 100.0% 50.5% 20.0% 2.0% Effective Imperviousness for WQCV Event 64.3% 100.0% 66.4% 100.0% 50.5% 20.0% 2.0% Effective Imperviousness for 5-Year Event: 64.3% 100.0% 66.4% 100.0% 50.5% 20.0% 2.0% 100.0% 2.0% Effective Imperviousness for 100-Year Event. 64.3% 66.4% 100.0% 50.5% 20.0% Effective Imperviousness for Optional User Defined Storm CUHP LID / EFFECTIVE IMPERVIOUSNESS CREDITS WOCV Event CREDIT: Reduce Detention By: 0.0% 0.0% N/A 0.0% 0.0% 0.0% 0.0% 0.0% N/A N/A N/A N/A N/A N/A This line only for 10-Year Event N/A 100-Year Event CREDIT**: Reduce Detention By: N/A 0.0% 0.1% 0.0% 0.1% 0.0% 0.0% -63.5% N/A N/A N/A N/A N/A N/A User Defined CUHP CREDIT: Reduce Detention By: Total Site Imperviousness: 47.0% 47.0% Total Site Effective Imperviousness for WQCV Event: * Use Green-Ampt average infiltration rate values from Table 3-3. Total Site Effective Imperviousness for 5-Year Event: 47.0% ** Flood control detention volume credits based on empirical equations from Storage Chapter of USDCM. Total Site Effective Imperviousness for 100-Year Event: *** Method assumes that 1-hour rainfall depth is equivalent to 1-hour intensity for calculation purposed Total Site Effective Imperviousness for Optional User Defined Storm CUHP

HRG01_IRF Calcs Pond A.xlsm, IRF

Site-Level Low Impact Development (LID) Design Effective Impervious Calculator LID Credit by Impervious Reduction Factor (IRF) Method UD-BMP (Version 3.06, November 2016) User Input Calculated cells Designer: Company: Galloway & Co. July 29, 2021 0.60 ***Design Storm: 1-Hour Rain Depth WOCV Event inches Date: 5-Year Event 1.50 inches Project: **Grandview Reserve** ***Minor Storm: 1-Hour Rain Depth ***Major Storm: 1-Hour Rain Depth 100-Year Event 2.52 inches Location: Pond B CUHP Optional User Defined Storm (CUHP) NOAA 1 Hour Rainfall Depth and Frequency for User Defined Storm Max Intensity for Optional User Defined Storm SITE INFORMATION (USER-INPUT) Sub-basin Identifier B-1 B-2 B-3 B-4 B-5 B-6 B-7 B-8 Receiving Pervious Area Soil Type Sandy Loar Sandy Loan Sandy Loa andy Loar Sandy Loan Sandy Loar andy Loai Sandy Loar Total Area (ac., Sum of DCIA, UIA, RPA, & SPA) 4.020 7.580 0.760 9.170 2.570 2.060 0.990 0.870 4.980 6.208 1.434 0.017 Directly Connected Impervious Area (DCIA, acres) 2.183 0.760 1.766 0.739 Unconnected Impervious Area (UIA, acres) 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 Receiving Pervious Area (RPA, acres) 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 Separate Pervious Area (SPA, acres) 1 837 2 600 0.000 2 962 0.804 0.626 0.251 0.853 RPA Treatment Type: Conveyance (C). Volume (V), or Permeable Pavement (PP) CALCULATED RESULTS (OUTPUT) Total Calculated Area (ac, check against input) 4.020 7.580 0.760 9.170 2.570 2.060 0.990 0.870 Directly Connected Impervious Area (DCIA, %) 65.7% 100.0% 67.7% 68.7% 69.6% 74.6% 2.0% Unconnected Impervious Area (UIA, %) 0.0% 0.0% 0.0% 0.0% 0.0% 0.0% 0.0% 0.0% 0.0% 0.0% 0.0% 0.0% Receiving Pervious Area (RPA. %) 0.0% 0.0% 0.0% 0.0% Separate Pervious Area (SPA, %) 45.7% 34.3% 0.0% 32.3% 31.3% 30.4% 25.4% 98.0% A_R (RPA / UIA) 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 I. Check f / I for WQCV Event 1.7 1.7 1.7 1.7 1.7 1.7 1.7 1.7 f / I for 5-Year Event: 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5 f / I for 100-Year Event: 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 f / I for Optional User Defined Storm CUHP: IRF for WQCV Event: 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 IRF for 5-Year Event: 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 IRF for 100-Year Event: 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 IRF for Optional User Defined Storm CUHP: 74.6% Effective Imperviousness for WQCV Event: 54.3% 65.7% 100.0% 67.7% 68.7% 69.6% 74.6% 2.0% 100.0% 67.7% 68.7% 69.6% 74.6% Effective Imperviousness for 5-Year Event: 54.3% 65.7% 2.0% Effective Imperviousness for 100-Year Event: 65.7% 100.0% 69.6% 54.3% 67.7% 68.7% 74.6% 2.0% Effective Imperviousness for Optional User Defined Storm CUHP LID / EFFECTIVE IMPERVIOUSNESS CREDITS WQCV Event CREDIT: Reduce Detention By: 0.0% 0.0% 0.0% 0.0% 0.0% 0.0% 0.0% 0.0% N/A N/A N/A N/A N/A This line only for 10-Year Event N/A N/A N/A N/A N/A N/A N/A N/A N/A 100-Year Event CREDIT**: Reduce Detention By: 0.0% 0.0% 0.0% 0.0% 0.0% -460.7% N/A N/A N/A N/A 0.0% 0.0% N/A N/A Total Site Imperviousness 64.5% Total Site Effective Imperviousness for WQCV Event: 64.5% * Use Green-Ampt average infiltration rate values from Table 3-3. Total Site Effective Imperviousness for 5-Year Event: 64.5% ** Flood control detention volume credits based on empirical equations from Storage Chapter of USDCM.

HRG01_IRF Calcs Pond B.xism, IRF

*** Method assumes that 1-hour rainfall depth is equivalent to 1-hour intensity for calculation purposed

Total Site Effective Imperviousness for 100-Year Event:

Total Site Effective Imperviousness for Optional User Defined Storm CUHP

Site-Level Low Impact Development (LID) Design Effective Impervious Calculator LID Credit by Impervious Reduction Factor (IRF) Method UD-BMP (Version 3.06, November 2016) User Input Calculated cells Designer: Company: Galloway & Co. July 29, 2021 0.60 ***Design Storm: 1-Hour Rain Depth WQCV Event inches Date: ***Minor Storm: 1-Hour Rain Depth 5-Year Event 1.50 inches Project: **Grandview Reserve** ***Major Storm: 1-Hour Rain Depth 100-Year Event 2.52 inches Location: Pond C CUHP Optional User Defined Storm (CUHP) NOAA 1 Hour Rainfall Depth and Frequency for User Defined Storm Max Intensity for Optional User Defined Storm SITE INFORMATION (USER-INPUT) Sub-basin Identifier C-1 C-2 C-3 C-4 C-5 Receiving Pervious Area Soil Type Sandy Loan Sandy Loar Sandy Loan Sandy Loa andy Loar Total Area (ac., Sum of DCIA, UIA, RPA, & SPA) 34.690 9.900 0.500 1.610 3.990 23.173 6.019 0.196 1.058 0.080 Directly Connected Impervious Area (DCIA, acres) 0.000 0.000 Unconnected Impervious Area (UIA, acres) 0.000 0.000 0.000 Receiving Pervious Area (RPA, acres) 0.000 0.000 0.000 0.000 0.000 Separate Pervious Area (SPA, acres) 11.517 3.881 0.304 0.552 3 910 RPA Treatment Type: Conveyance (C), С Volume (V), or Permeable Pavement (PP) CALCULATED RESULTS (OUTPUT) Total Calculated Area (ac, check against input) 34.690 9.900 0.500 1.610 3.990 Directly Connected Impervious Area (DCIA, %) 66.8% 60.8% 39.2% 65.7% 2.0% 0.0% 0.0% Unconnected Impervious Area (UIA, %) 0.0% 0.0% 0.0% 0.0% 0.0% 0.0% Receiving Pervious Area (RPA. %) 0.0% 0.0% Separate Pervious Area (SPA, %) 33.2% 39.2% 60.8% 34.3% 98.0% A_R (RPA / UIA) 0.000 0.000 0.000 0.000 0.000 1.000 1.000 I. Check 1.000 1.000 1.000 f / I for WQCV Event: 1.7 1.7 1.7 1.7 1.7 f / I for 5-Year Event: 0.5 0.5 0.5 0.5 0.5 f / I for 100-Year Event: 0.3 0.3 0.3 0.3 0.3 f / I for Optional User Defined Storm CUHP: IRF for WQCV Event: 1.00 1.00 1.00 1.00 1.00 IRF for 5-Year Event: 1.00 1.00 1.00 1.00 1.00 IRF for 100-Year Event: 1.00 1.00 1.00 1.00 1.00 IRF for Optional User Defined Storm CUHP: 60.8% Effective Imperviousness for WQCV Event: 66.8% 60.8% 39.2% 65.7% 2.0% 60.8% 39.2% 65.7% 2.0% Effective Imperviousness for 5-Year Event: 66.8% Effective Imperviousness for 100-Year Event: 60.8% 39.2% 66.8% 65.7% 2.0% Effective Imperviousness for Optional User Defined Storm CUHP LID / EFFECTIVE IMPERVIOUSNESS CREDITS WQCV Event CREDIT: Reduce Detention By: 0.0% 0.0% 0.0% 0.0% 0.0% N/A N/A N/A N/A N/A N/A This line only for 10-Year Event N/A 100-Year Event CREDIT**: Reduce Detention By: 0.0% 0.0% 0.1% 0.0% -100.5% N/A N/A N/A N/A N/A N/A N/A N/A N/A Total Site Imperviousness 60.2% Total Site Effective Imperviousness for WQCV Event: 60.2% * Use Green-Ampt average infiltration rate values from Table 3-3. Total Site Effective Imperviousness for 5-Year Event: 60.2% ** Flood control detention volume credits based on empirical equations from Storage Chapter of USDCM. Total Site Effective Imperviousness for 100-Year Event: *** Method assumes that 1-hour rainfall depth is equivalent to 1-hour intensity for calculation purposed Total Site Effective Imperviousness for Optional User Defined Storm CUHP

HRG01_IRF Calcs Pond C.xism, IRF

Site-Level Low Impact Development (LID) Design Effective Impervious Calculator LID Credit by Impervious Reduction Factor (IRF) Method UD-BMP (Version 3.06, November 2016) User Input Calculated cells Designer: Company: Galloway & Co. July 29, 2021 0.60 ***Design Storm: 1-Hour Rain Depth WQCV Event inches Date: ***Minor Storm: 1-Hour Rain Depth 5-Year Event 1.50 inches Project: **Grandview Reserve** ***Major Storm: 1-Hour Rain Depth 100-Year Event 2.52 inches Location: Pond D CUHP Optional User Defined Storm (CUHP) NOAA 1 Hour Rainfall Depth and Frequency for User Defined Storm Max Intensity for Optional User Defined Storm SITE INFORMATION (USER-INPUT) Sub-basin Identifier D-1 D-2 D-3 D-4 D-5 Receiving Pervious Area Soil Type Sandy Loan Sandy Loar Sandy Loan Sandy Loa andy Loar Total Area (ac., Sum of DCIA, UIA, RPA, & SPA) 2.460 0.750 4.760 4.740 1.710 1.378 0.614 2.970 3.095 0.034 Directly Connected Impervious Area (DCIA, acres) 0.000 0.000 0.000 Unconnected Impervious Area (UIA, acres) 0.000 0.000 Receiving Pervious Area (RPA, acres) 0.000 0.000 0.000 0.000 0.000 Separate Pervious Area (SPA, acres) 1.082 0.137 1.790 1 645 1 676 RPA Treatment Type: Conveyance (C), С Volume (V), or Permeable Pavement (PP) CALCULATED RESULTS (OUTPUT) Total Calculated Area (ac, check against input) 2.460 0.750 4.760 4.740 1.710 Directly Connected Impervious Area (DCIA, %) 81.8% 62.4% 65.3% 2.0% 0.0% 0.0% Unconnected Impervious Area (UIA, %) 0.0% 0.0% 0.0% 0.0% 0.0% 0.0% Receiving Pervious Area (RPA. %) 0.0% 0.0% Separate Pervious Area (SPA, %) 44.0% 18.2% 37.6% 34.7% 98.0% A_R (RPA / UIA) 0.000 0.000 0.000 0.000 0.000 1.000 1.000 I. Check 1.000 1.000 1.000 f / I for WQCV Event: 1.7 1.7 1.7 1.7 1.7 f / I for 5-Year Event: 0.5 0.5 0.5 0.5 0.5 f / I for 100-Year Event: 0.3 0.3 0.3 0.3 0.3 f / I for Optional User Defined Storm CUHP: IRF for WQCV Event: 1.00 1.00 1.00 1.00 1.00 IRF for 5-Year Event: 1.00 1.00 1.00 1.00 1.00 IRF for 100-Year Event: 1.00 1.00 1.00 1.00 1.00 IRF for Optional User Defined Storm CUHP: Effective Imperviousness for WQCV Event: 56.0% 81.8% 62.4% 65.3% 2.0% 81.8% 62.4% 65.3% 2.0% Effective Imperviousness for 5-Year Event: 56.0% Effective Imperviousness for 100-Year Event: 81.8% 56.0% 65.3% 2.0% Effective Imperviousness for Optional User Defined Storm CUHP LID / EFFECTIVE IMPERVIOUSNESS CREDITS WQCV Event CREDIT: Reduce Detention By: 0.0% 0.0% 0.0% 0.0% 0.0% N/A N/A N/A N/A N/A N/A This line only for 10-Year Event N/A 100-Year Event CREDIT**: Reduce Detention By: 0.0% 0.0% 0.0% 0.0% -234.4% N/A N/A N/A N/A N/A N/A N/A N/A Total Site Imperviousness 56.1% Total Site Effective Imperviousness for WQCV Event: 56.1% * Use Green-Ampt average infiltration rate values from Table 3-3. Total Site Effective Imperviousness for 5-Year Event: 56.1% ** Flood control detention volume credits based on empirical equations from Storage Chapter of USDCM. Total Site Effective Imperviousness for 100-Year Event: *** Method assumes that 1-hour rainfall depth is equivalent to 1-hour intensity for calculation purposed Total Site Effective Imperviousness for Optional User Defined Storm CUHP

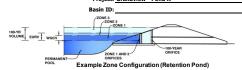
HRG01_IRF Calcs Pond D.xism, IRF

Site-Level Low Impact Development (LID) Design Effective Impervious Calculator LID Credit by Impervious Reduction Factor (IRF) Method UD-BMP (Version 3.06, November 2016) User Input Calculated cells Designer: Company: Galloway & Co. July 29, 2021 0.60 ***Design Storm: 1-Hour Rain Depth WQCV Event inches Date: ***Minor Storm: 1-Hour Rain Depth 5-Year Event 1.50 inches Project: **Grandview Reserve** ***Major Storm: 1-Hour Rain Depth 100-Year Event 2.52 inches Location: Pond F CUHP Optional User Defined Storm (CUHP) NOAA 1 Hour Rainfall Depth and Frequency for User Defined Storm Max Intensity for Optional User Defined Storm SITE INFORMATION (USER-INPUT) Sub-basin Identifier E-E-2 E-3 Receiving Pervious Area Soil Type Sandy Loar Sandy Loan Sandy Loa Total Area (ac., Sum of DCIA, UIA, RPA, & SPA) 6.860 11.660 1.710 3.231 0.034 Directly Connected Impervious Area (DCIA, acres) 6.273 0.000 0.000 Unconnected Impervious Area (UIA, acres) 0.000 Receiving Pervious Area (RPA, acres) 0.000 0.000 0.000 1.676 Separate Pervious Area (SPA, acres) 3.629 5.387 RPA Treatment Type: Conveyance (C), С Volume (V), or Permeable Pavement (PP) CALCULATED RESULTS (OUTPUT) Total Calculated Area (ac, check against input) 6.860 11.660 1.710 Directly Connected Impervious Area (DCIA, %) 47.1% 53.8% 2.0% Unconnected Impervious Area (UIA, %) 0.0% 0.0% 0.0% Receiving Pervious Area (RPA, %) 0.0% 0.0% 0.0% Separate Pervious Area (SPA, %) 52.9% 46.2% 98.0% A_R (RPA / UIA) 0.000 0.000 0.000 1.000 1.000 1.000 I. Check f / I for WQCV Event: 1.7 1.7 1.7 f / I for 5-Year Event: 0.5 0.5 0.5 f / I for 100-Year Event: 0.3 0.3 0.3 f / I for Optional User Defined Storm CUHP: IRF for WQCV Event: 1.00 1.00 1.00 IRF for 5-Year Event: 1.00 1.00 1.00 IRF for 100-Year Event: 1.00 1.00 1.00 IRF for Optional User Defined Storm CUHP: 2.0% Effective Imperviousness for WQCV Event: 47.1% 53.8% 2.0% 2.0% 47.1% 53.8% Effective Imperviousness for 5-Year Event: Effective Imperviousness for 100-Year Event: 53.8% 2.0% Effective Imperviousness for Optional User Defined Storm CUHP LID / EFFECTIVE IMPERVIOUSNESS CREDITS WQCV Event CREDIT: Reduce Detention By: 0.0% 0.0% 0.0% N/A N/A N/A N/A N/A N/A N/A This line only for 10-Year Event N/A 100-Year Event CREDIT**: Reduce Detention By: 0.0% 0.0% -234.4% N/A Total Site Imperviousness 47.1% Total Site Effective Imperviousness for WQCV Event: 47.1% * Use Green-Ampt average infiltration rate values from Table 3-3. Total Site Effective Imperviousness for 5-Year Event: 47.1% ** Flood control detention volume credits based on empirical equations from Storage Chapter of USDCM. Total Site Effective Imperviousness for 100-Year Event: *** Method assumes that 1-hour rainfall depth is equivalent to 1-hour intensity for calculation purposed Total Site Effective Imperviousness for Optional User Defined Storm CUHP

HRG01_IRF Calcs Pond E.xism, IRF

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.04 (February 2021)



Watershed Information

ershed Information		
Selected BMP Type =	EDB	
Watershed Area =	29.66	acres
Watershed Length =	2,360	ft
Watershed Length to Centroid =	1,180	ft
Watershed Slope =	0.020	ft/ft
Watershed Imperviousness =	47.00%	percent
Percentage Hydrologic Soil Group A =	100.0%	percent
Percentage Hydrologic Soil Group B =	0.0%	percent
Percentage Hydrologic Soil Groups C/D =	0.0%	percent
Target WQCV Drain Time =	40.0	hours
Location for 1-hr Rainfall Depths =	User Input	

After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

the embedded Colorado Urban Hydrograph Procedure.			
Water Quality Capture Volume (WQCV) =	0.490	acre-feet	
Excess Urban Runoff Volume (EURV) =	1.580	acre-feet	
2-yr Runoff Volume (P1 = 1.19 in.) =	1.193	acre-feet	
5-yr Runoff Volume (P1 = 1.5 in.) =	1.591	acre-feet	
10-yr Runoff Volume (P1 = 1.75 in.) =	1.908	acre-feet	
25-yr Runoff Volume (P1 = 2 in.) =	2.435	acre-feet	
50-yr Runoff Volume (P1 = 2.25 in.) =	2.948	acre-feet	
100-yr Runoff Volume (P1 = 2.52 in.) =	3.606	acre-feet	
500-yr Runoff Volume (P1 = 3.68 in.) =	6.350	acre-feet	
Approximate 2-yr Detention Volume =	1.013	acre-feet	
Approximate 5-yr Detention Volume =	1.336	acre-feet	
Approximate 10-yr Detention Volume =	1.635	acre-feet	
Approximate 25-yr Detention Volume =	2.008	acre-feet	
Approximate 50-yr Detention Volume =	2.249	acre-feet	
Approximate 100-yr Detention Volume =	2.554	acre-feet	
		-	

C	Optional User Overrides					
		acre-feet				
		acre-feet				
	1.19	inches				
	1.50	inches				
	1.75	inches				
	2.00	inches				
	2.25	inches				
	2.52	inches				
	3.68	inches				

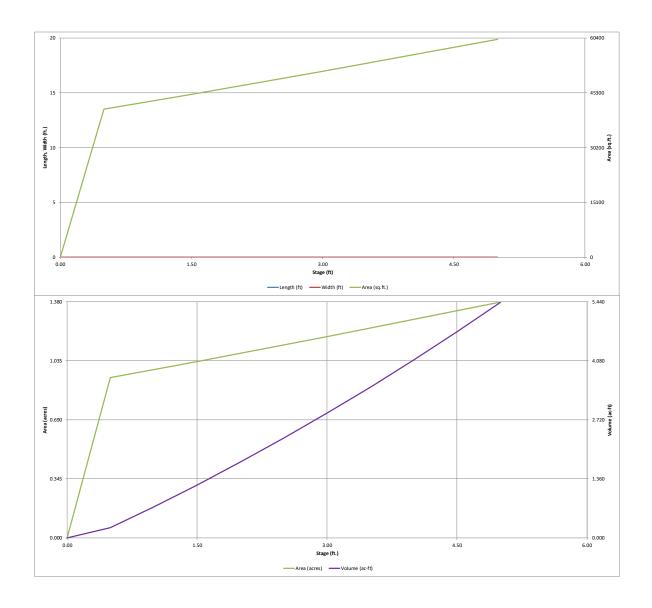
Define Zones and Basin Geometry

		enne zones and basin deomedy
acre-fee	0.490	Zone 1 Volume (WQCV) =
acre-fee	1.090	Zone 2 Volume (EURV - Zone 1) =
acre-fee	0.974	Zone 3 Volume (100-year - Zones 1 & 2) =
acre-fee	2.554	Total Detention Basin Volume =
ft 3	user	Initial Surcharge Volume (ISV) =
ft	user	Initial Surcharge Depth (ISD) =
ft	user	Total Available Detention Depth (H _{total}) =
ft	user	Depth of Trickle Channel (H _{TC}) =
ft/ft	user	Slope of Trickle Channel $(S_{TC}) =$
H:V	user	Slopes of Main Basin Sides (Smain) =
1	user	Basin Length-to-Width Ratio (R _{L/W}) =

Initial Surcharge Area $(A_{ISV}) =$	user	ft ²
Surcharge Volume Length $(L_{ISV}) =$	user	ft
Surcharge Volume Width $(W_{ISV}) =$	user	ft
Depth of Basin Floor $(H_{FLOOR}) =$	user	ft
Length of Basin Floor (L_{FLOOR}) =	user	ft
Width of Basin Floor $(W_{FLOOR}) =$	user	ft
Area of Basin Floor $(A_{FLOOR}) =$		ft²
Volume of Basin Floor $(V_{FLOOR}) =$	user	ft ³
Depth of Main Basin $(H_{MAIN}) =$	user	ft
Length of Main Basin $(L_{MAIN}) =$	user	ft
Width of Main Basin $(W_{MAIN}) =$	user	ft
Area of Main Basin $(A_{MAIN}) =$	user	ft²
Volume of Main Basin $(V_{MAIN}) =$	user	ft ³
Calculated Total Basin Volume (V_{total}) =	user	acre-feet

		1.							
Depth Increment =	0.50	ft Optional				Optional			
Stage - Storage Description	Stage	Override Stage (ft)	Length (ft)	Width (ft)	Area (ft²)	Override Area (ft ²)	Area (acre)	Volume (ft 3)	Volume (ac-ft)
Top of Micropool	(ft) 	0.00				35	0.001	(10)	(aC-IL)
		0.50	-		-	40,768	0.936	10,198	0.234
		1.00	-		_	42,811	0.983	31,093	0.714
	-	1.50	ı		1	44,876	1.030	53,015	1.217
		2.00	-		-	46,970	1.078	75,976	1.744
		2.50	-		-	49,084	1.127	99,990	2.295
		3.00	-		-	51,229 53,393	1.176 1.226	125,068 151,224	2.871 3.472
	-	4.00	_		_	55,589	1.276	178,470	4.097
		4.50	-		-	57,803	1.327	206,818	4.748
	-	5.00	-		-	60,050	1.379	236,281	5.424
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MHFD-Detention_v4.04 - Pond A./smr, Basin 8/11/2021, 3.29 PM

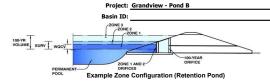


Provide the outlet design sheets for each pond

MHFD-Detention_v4.04 - Pond Axism, Basin 8/11/2021, 3:29 PM

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.04 (February 2021)



Watershed Information

28?

Optional User Overrides
acre-feet
acre-feet

inches

1.19 inches

1.50

1.75 inches

2.00 inches 2.25 inches 2.52 inches 3.68 inches

CISICO IIIOIIIIOOII	_	
Selected BMP Type =	EDB	
Watershed Area =	24.00	acres
Watershed Length =	1,700	ft
Watershed Length to Centroid =	850	ft
Watershed Slope =	0.020	ft/ft
Watershed Imperviousness =	66.30%	percent
Percentage Hydrologic Soil Group A =	100.0%	percent
Percentage Hydrologic Soil Group B =	0.0%	percent
Percentage Hydrologic Soil Groups C/D =	0.0%	percent
Target WQCV Drain Time =	40.0	hours
Location for 1-br Painfall Denths -	User Innut	

After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

the embedded Colorado Urban Hydro	igraph Procedu	ire.
Water Quality Capture Volume (WQCV) =	0.519	acre-feet
Excess Urban Runoff Volume (EURV) =	1.986	acre-feet
2-yr Runoff Volume (P1 = 1.19 in.) =	1.457	acre-feet
5-yr Runoff Volume (P1 = 1.5 in.) =	1.909	acre-feet
10-yr Runoff Volume (P1 = 1.75 in.) =	2.271	acre-feet
25-yr Runoff Volume (P1 = 2 in.) =	2.739	acre-feet
50-yr Runoff Volume (P1 = 2.25 in.) =	3.199	acre-feet
100-yr Runoff Volume (P1 = 2.52 in.) =	3.755	acre-feet
500-yr Runoff Volume (P1 = 3.68 in.) =	6.074	acre-feet
Approximate 2-yr Detention Volume =	1.293	acre-feet
Approximate 5-yr Detention Volume =	1.689	acre-feet
Approximate 10-yr Detention Volume =	2.034	acre-feet
Approximate 25-yr Detention Volume =	2.445	acre-feet
Approximate 50-yr Detention Volume =	2.692	acre-feet
Approximate 100-yr Detention Volume =	2.946	acre-feet
	•	

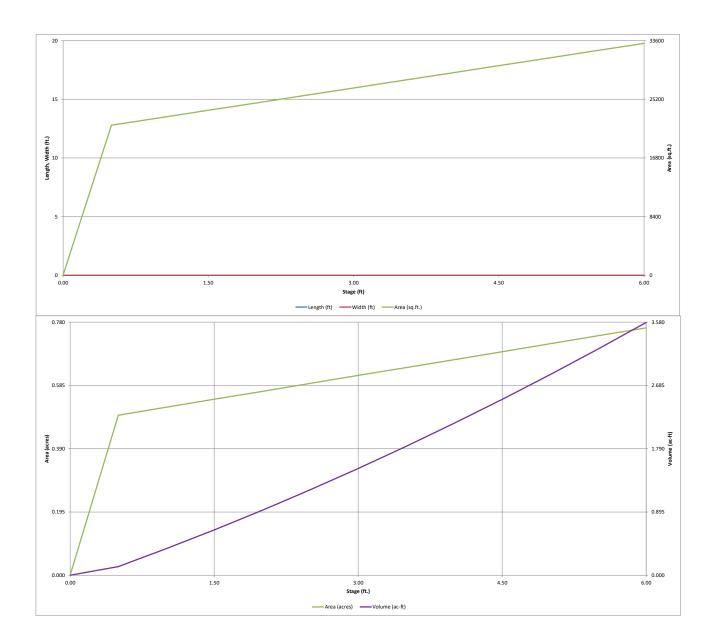
Define Zones and Basin Geometry	Define	Zones	and	Basin	Geometry
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Zone 1 Volume (WQCV) =	0.519	acre-feet
Zone 2 Volume (EURV - Zone 1) =	1.467	acre-feet
Zone 3 Volume (100-year - Zones 1 & 2) =	0.960	acre-feet
Total Detention Basin Volume =	2.946	acre-feet
Initial Surcharge Volume (ISV) =	user	ft ³
Initial Surcharge Depth (ISD) =	user	ft
Total Available Detention Depth (H _{total}) =	user	ft
Depth of Trickle Channel $(H_{TC}) =$	user	ft
Slope of Trickle Channel $(S_{TC}) =$	user	ft/ft
Slopes of Main Basin Sides (S _{main}) =	user	H:V
Basin Length-to-Width Ratio ($R_{L/W}$) =	user	

Initial Surcharge Area $(A_{ISV}) =$	user	ft ²
Surcharge Volume Length $(L_{ISV}) =$	user	ft
Surcharge Volume Width $(W_{ISV}) =$	user	ft
Depth of Basin Floor (H_{FLOOR}) =	user	ft
Length of Basin Floor (L_{FLOOR}) =	user	ft
Width of Basin Floor (W_{FLOOR}) =	user	ft
Area of Basin Floor (A_{FLOOR}) =	user	ft ²
Volume of Basin Floor (V _{FLOOR}) =	user	ft ³
Depth of Main Basin (H _{MAIN}) =	user	ft
Length of Main Basin $(L_{MAIN}) =$	user	ft
Width of Main Basin (W_{MAIN}) =	user	ft
Area of Main Basin $(A_{MAIN}) =$	user	ft ²
Volume of Main Basin (V_{MAIN}) =	user	ft ³
Calculated Total Basin Volume (V_{total}) =	user	acre-feet

		,							
Depth Increment =	0.50	ft				Outland			
Stage - Storage	Stage	Optional Override	Length	Width	Area	Optional Override	Area	Volume	Volume
Description	(ft)	Stage (ft)	(ft)	(ft)	(ft 2)	Area (ft 2)	(acre)	(ft 3)	(ac-ft)
Top of Micropool		0.00	-			35	0.001		
		0.50				21,497	0.493	5,382	0.124
		1.00				22,562	0.518	16,396	0.376
		1.50				23,626	0.542	27,943	0.641
		2.00				24,691	0.567	40,023	0.919
		2.50				25,756	0.591	52,635	1.208
		3.00				26,822	0.616	65,779	1.510
		3.50				27,887	0.640	79,456	1.824
		4.00				28,952	0.665	93,666	2.150
		4.50				30,018	0.689	108,409	2.489
		5.00				31,084	0.714	123,684	2.839
		5.50				32,150	0.738	139,492	3.202
		6.00				33,216	0.763	155,834	3.577
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MHFD-Detention_v4.04 - Pond B.xlsm, Basin 7/29/2021, 11:40 AM



MHFD-Detention_v4.04 - Pond B.xlsm, Basin 7/29/2021, 11:40 AM

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.04 (February 2021)

acre-feet acre-feet

inches

inches

inches

inches inches 2.25 2.52

inches

inches

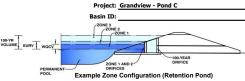
1.19

1.50

1.75

2.00

3.68



49.7? Watershed Information 16.00 Note: L / W Ratio > 8 Selected BMP Type = L / W Ratio = 11.25 Watershed Area = Watershed Length = 2,800 Watershed Length to Centroid = 1,400 60? Watershed Slope = 0.020 Watershed Imperviousness = 46.00% percent Percentage Hydrologic Soil Group A = Percentage Hydrologic Soil Group B = 0.0% Percentage Hydrologic Soil Groups C/D = 0.0% Target WQCV Drain Time = 40.0

Location for 1-hr Rainfall Depths = User Input hours

After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

Water Quality Capture Volume (WQCV) =	0.261	acre-feet
Excess Urban Runoff Volume (EURV) =	0.829	acre-feet
2-yr Runoff Volume (P1 = 1.19 in.) =	0.628	acre-feet
5-yr Runoff Volume (P1 = 1.5 in.) =	0.838	acre-feet
10-yr Runoff Volume (P1 = 1.75 in.) =	1.006	acre-feet
25-yr Runoff Volume (P1 = 2 in.) =	1.289	acre-feet
50-yr Runoff Volume (P1 = 2.25 in.) =	1.565	acre-feet
100-yr Runoff Volume (P1 = 2.52 in.) =	1.920	acre-feet
500-yr Runoff Volume (P1 = 3.68 in.) =	3.400	acre-feet
Approximate 2-yr Detention Volume =	0.531	acre-feet
Approximate 5-yr Detention Volume =	0.701	acre-feet
Approximate 10-yr Detention Volume =	0.859	acre-feet
Approximate 25-yr Detention Volume =	1.056	acre-feet
Approximate 50-yr Detention Volume =	1.184	acre-feet
Approximate 100-yr Detention Volume =	1.348	acre-feet

Define Zones and Basin Geometry

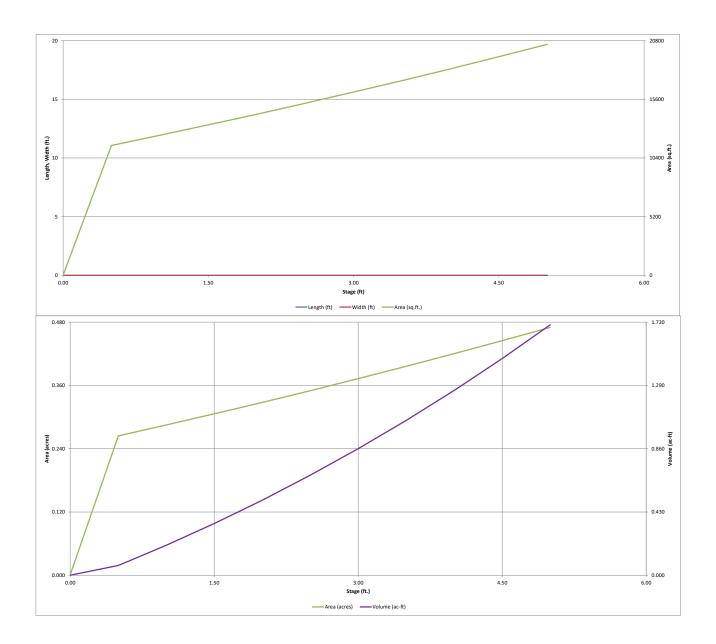
Zone 1 Volume (WQCV) =	0.261	acre-feet
Zone 2 Volume (EURV - Zone 1) =	0.568	acre-feet
Zone 3 Volume (100-year - Zones 1 & 2) =	0.519	acre-feet
Total Detention Basin Volume =	1.348	acre-feet
Initial Surcharge Volume (ISV) =	user	ft ³
Initial Surcharge Depth (ISD) =	user	ft
Total Available Detention Depth (H _{total}) =	user	ft
Depth of Trickle Channel $(H_{TC}) =$	user	ft
Slope of Trickle Channel (S_{TC}) =	user	ft/ft
Slopes of Main Basin Sides (Smain) =	user	H:V
Basin Length-to-Width Ratio (R _{L/W}) =	user	

Initial Surcharge Area $(A_{ISV}) =$	user	ft²
Surcharge Volume Length $(L_{ISV}) =$	user	ft
Surcharge Volume Width $(W_{ISV}) =$	user	ft
Depth of Basin Floor (H_{FLOOR}) =	user	ft
Length of Basin Floor (L_{FLOOR}) =	user	ft
Width of Basin Floor $(W_{FLOOR}) =$	user	ft
Area of Basin Floor $(A_{FLOOR}) =$	user	ft ²
Volume of Basin Floor (V _{FLOOR}) =	user	ft ³
Depth of Main Basin $(H_{MAIN}) =$	user	ft
Length of Main Basin $(L_{MAIN}) =$	user	ft
Width of Main Basin (W _{MAIN}) =	user	ft
Area of Main Basin $(A_{MAIN}) =$	user	ft ²
Volume of Main Basin $(V_{MAIN}) =$	user	ft ³
Calculated Total Basin Volume (V_{total}) =	user	acre-feet

Stage - Storage Description	Stage (ft)	Optional Override Stage (ft)	Length (ft)	Width (ft)	Area (ft ²)	Optional Override Area (ft ²)	Area (acre)	Volume (ft ³)	Volume (ac-ft)
Top of Micropool		0.00				35	0.001	(10)	(uc it)
.,		0.50				11,520	0.264	2,888	0.066
		1.00				12,417	0.285	8,873	0.204
		1.50				13,333	0.306	15,310	0.351
		2.00				14,281	0.328	22,214	0.510
		2.50				15,247	0.350	29,596	0.679
		3.00				16,245	0.373	37,469	0.860
		3.50				17,261	0.396	45,845	1.052
		4.00				18,310	0.420	54,738	1.257
		4.50				19,376	0.445	64,159	1.473
		5.00				20,475	0.470	74,122	1.702
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7/29/2021, 11:48 AM

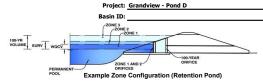
MHFD-Detention_v4.04 - Pond C.xlsm, Basin



MHFD-Detention_v4.04 - Pond C.xlsm, Basin 7/29/2021, 11:48 AM

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.04 (February 2021)



Watershed Information >14.5?

Selected BMP Type =	EDB /	
Watershed Area =	11.96	acres
Watershed Length =	1,200	ft
Watershed Length to Centroid =	600	ft
Watershed Slope =	0.020	ft/ft
Watershed Imperviousness =	56.10%	percent
Percentage Hydrologic Soil Group A =	100.0%	percent
Percentage Hydrologic Soil Group B =	0.0%	percent
Percentage Hydrologic Soil Groups C/D =	0.0%	percent
Target WQCV Drain Time =	40.0	hours
Location for 1-hr Rainfall Depths =	User Input	

After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

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Water Quality Capture Volume (WQCV) =	0.223	acre-feet
Excess Urban Runoff Volume (EURV) =	0.799	acre-feet
2-yr Runoff Volume (P1 = 1.19 in.) =	0.000	acre-feet
5-yr Runoff Volume (P1 = 1.5 in.) =	0.000	acre-feet
10-yr Runoff Volume (P1 = 1.75 in.) =	0.000	acre-feet
25-yr Runoff Volume (P1 = 2 in.) =	0.000	acre-feet
50-yr Runoff Volume (P1 = 2.25 in.) =	0.000	acre-feet
100-yr Runoff Volume (P1 = 2.52 in.) =	0.000	acre-feet
500-yr Runoff Volume (P1 = 3.68 in.) =	0.000	acre-feet
Approximate 2-yr Detention Volume =	0.516	acre-feet
Approximate 5-yr Detention Volume =	0.678	acre-feet
Approximate 10-yr Detention Volume =	0.823	acre-feet
Approximate 25-yr Detention Volume =	0.999	acre-feet
Approximate 50-yr Detention Volume =	1.108	acre-feet
Approximate 100-yr Detention Volume =	1.233	acre-feet

Optional	User	Overrides
		acro-foot

	acre-feet
	acre-feet
1.19	inches
1.50	inches
1.75	inches
2.00	inches
2.25	inches
2.52	inches
3.68	inches
	,

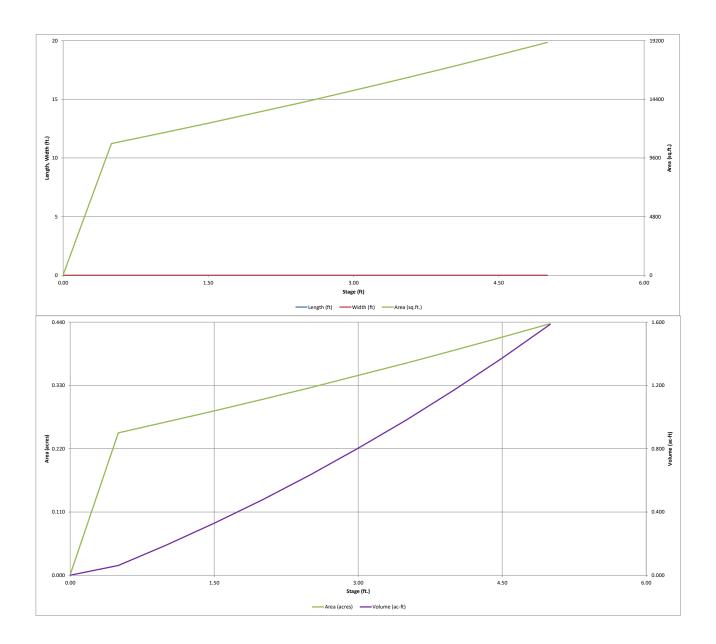
Define Zones and Basin Geometry

erine Zones and Basin Geometry		
Zone 1 Volume (WQCV) =	0.223	acre-feet
Zone 2 Volume (EURV - Zone 1) =	0.576	acre-feet
Zone 3 Volume (100-year - Zones 1 & 2) =	0.434	acre-feet
Total Detention Basin Volume =	1.233	acre-feet
Initial Surcharge Volume (ISV) =	user	ft ³
Initial Surcharge Depth (ISD) =	user	ft
Total Available Detention Depth $(H_{total}) =$	user	ft
Depth of Trickle Channel $(H_{TC}) =$	user	ft
Slope of Trickle Channel $(S_{TC}) =$	user	ft/ft
Slopes of Main Basin Sides (S _{main}) =	user	H:V
Basin Length-to-Width Ratio (R _{L/W}) =	user	

Initial Surcharge Area (A _{ISV}) =	user	ft 2
Surcharge Volume Length $(L_{ISV}) =$	user	ft
Surcharge Volume Width $(W_{ISV}) =$	user	ft
Depth of Basin Floor $(H_{FLOOR}) =$	user	ft
Length of Basin Floor (L_{FLOOR}) =	user	ft
Width of Basin Floor $(W_{FLOOR}) =$	user	ft
Area of Basin Floor (A _{FLOOR}) =	user	ft ²
Volume of Basin Floor (V _{FLOOR}) =	user	ft ³
Depth of Main Basin (H _{MAIN}) =	user	ft
Length of Main Basin $(L_{MAIN}) =$	user	ft
Width of Main Basin (W _{MAIN}) =	user	ft
Area of Main Basin (A _{MAIN}) =	user	ft 2
Volume of Main Basin (V _{MAIN}) =	user	ft ³
Calculated Total Basin Volume (Vtotal) =	user	acre-fe

Donth Incoment	0.50	٦,							
Depth Increment = Stage - Storage	Stage	ft Optional Override	Length	Width	Area	Optional Override	Area	Volume	Volume
Description	(ft)	Stage (ft)	(ft)	(ft)	(ft ²)	Area (ft ²)	(acre)	(ft 3)	(ac-ft)
Top of Micropool		0.00				35	0.001		
		0.50				10,786	0.248	2,705	0.062
	-	1.00				11,607	0.266	8,303	0.191
		1.50 2.00				12,446 13,318	0.286	14,316 20,758	0.329
		2.50				14,207	0.326	27,639	0.635
		3.00				15,130	0.347	34,973	0.803
		3.50				16,069	0.369	42,773	0.982
		4.00				17,042	0.391	51,051	1.172
		4.50				18,031	0.414	59,819	1.373
		5.00				19,055	0.437	69,090	1.586
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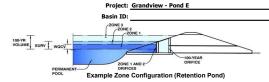
MHFD-Detention_v4.04 - Pond D.xlsm, Basin 7/29/2021, 11:55 AM



MHFD-Detention_v4.04 - Pond D.xlsm, Basin 7/29/2021, 11:55 AM

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.04 (February 2021)



Watershed Information

- 20.23?

tersned Information		_
Selected BMP Type =	EDB	
Watershed Area =	13.37	acres
Watershed Length =	1,800	ft
Watershed Length to Centroid =	900	ft
Watershed Slope =	0.020	ft/ft
Watershed Imperviousness =	47.20%	percent
Percentage Hydrologic Soil Group A =	90.0%	percent
Percentage Hydrologic Soil Group B =	10.0%	percent
Percentage Hydrologic Soil Groups C/D =	0.0%	percent
Target WQCV Drain Time =	40.0	hours
Location for 1-br Rainfall Denths =	User Innut	

After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

the embedded colorado orban riyuro	graph Frocedo	ii e.
Water Quality Capture Volume (WQCV) =	0.221	acre-feet
Excess Urban Runoff Volume (EURV) =	0.712	acre-feet
2-yr Runoff Volume (P1 = 1.19 in.) =	0.548	acre-feet
5-yr Runoff Volume (P1 = 1.5 in.) =	0.728	acre-feet
10-yr Runoff Volume (P1 = 1.75 in.) =	0.873	acre-feet
25-yr Runoff Volume (P1 = 2 in.) =	1.157	acre-feet
50-yr Runoff Volume (P1 = 2.25 in.) =	1.391	acre-feet
100-yr Runoff Volume (P1 = 2.52 in.) =	1.704	acre-feet
500-yr Runoff Volume (P1 = 3.68 in.) =	2.971	acre-feet
Approximate 2-yr Detention Volume =	0.464	acre-feet
Approximate 5-yr Detention Volume =	0.614	acre-feet
Approximate 10-yr Detention Volume =	0.760	acre-feet
Approximate 25-yr Detention Volume =	0.921	acre-feet
Approximate 50-yr Detention Volume =	1.023	acre-feet
Approximate 100-yr Detention Volume =	1.160	acre-feet

Optional	User	Overrides
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	acre-feet
	acre-feet
1.19	inches
1.50	inches
1.75	inches
2.00	inches
2.25	inches
2.52	inches
3.68	inches

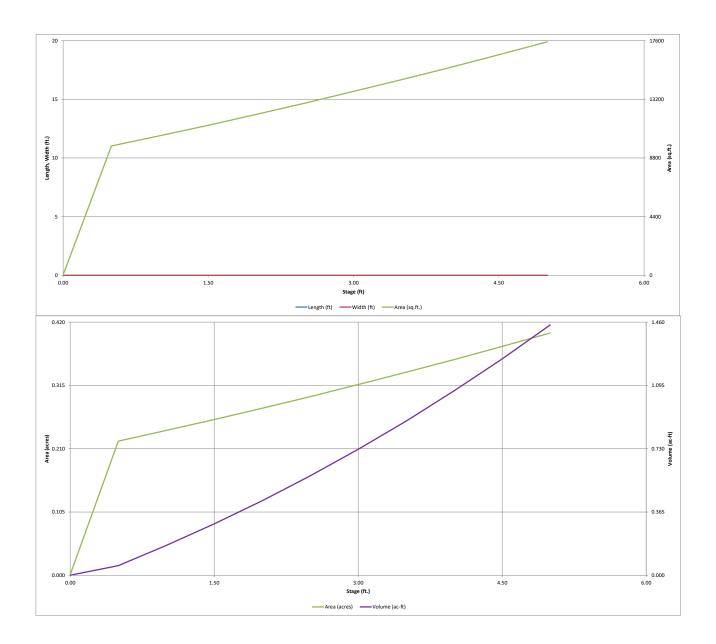
Define Zones and Basin Geometry

enne zones and basin deomedy		
Zone 1 Volume (WQCV) =	0.221	acre-feet
Zone 2 Volume (EURV - Zone 1) =	0.490	acre-feet
Zone 3 Volume (100-year - Zones 1 & 2) =	0.449	acre-feet
Total Detention Basin Volume =	1.160	acre-feet
Initial Surcharge Volume (ISV) =	user	ft ³
Initial Surcharge Depth (ISD) =	user	ft
Total Available Detention Depth (H _{total}) =	user	ft
Depth of Trickle Channel (H _{TC}) =	user	ft
Slope of Trickle Channel (S_{TC}) =	user	ft/ft
Slopes of Main Basin Sides (S _{main}) =	user	H:V
Basin Length-to-Width Ratio (R _{L/W}) =	user	

Initial Surcharge Area $(A_{ISV}) =$	user	ft 2
Surcharge Volume Length $(L_{ISV}) =$	user	ft
Surcharge Volume Width $(W_{ISV}) =$	user	ft
Depth of Basin Floor $(H_{FLOOR}) =$	user	ft
Length of Basin Floor (L_{FLOOR}) =	user	ft
Width of Basin Floor (WFLOOR) =	user	ft
Area of Basin Floor $(A_{FLOOR}) =$	user	ft 2
Volume of Basin Floor (V _{FLOOR}) =	user	ft ³
Depth of Main Basin (H _{MAIN}) =	user	ft
Length of Main Basin $(L_{MAIN}) =$	user	ft
Width of Main Basin (W _{MAIN}) =	user	ft
Area of Main Basin (A _{MAIN}) =	user	ft 2
Volume of Main Basin (V _{MAIN}) =	user	ft ³
Calculated Total Basin Volume (Vtotal) =	user	acre-fe

Depth Increment = Stage - Storage	0.50 Stage	Optional Override Stage (ft)	Length	Width	Area (ft ²)	Optional Override Area (ft ²)	Area (acre)	Volume (ft ³)	Volume (ac-ft)
Description Top of Micropool	(ft) 	Stage (ft) 0.00	(ft) 	(ft) 		35	(acre) 0.001	(IL*)	(dC-IL)
тор от містороог								2.422	0.056
		0.50				9,697	0.223	2,433	0.056
		1.00				10,467	0.240	7,474	0.172
		1.50				11,257	0.258	12,905	0.296
		2.00				12,077	0.277	18,738	0.430
		2.50				12,917	0.297	24,987	0.574
		3.00				13,788	0.317	31,663	0.727
		3.50				14,677	0.337	38,779	0.890
		4.00				15,599	0.358	46,348	1.064
		4.50				16,538	0.380	54,383	1.248
		5.00				17,511	0.402	62,895	1.444
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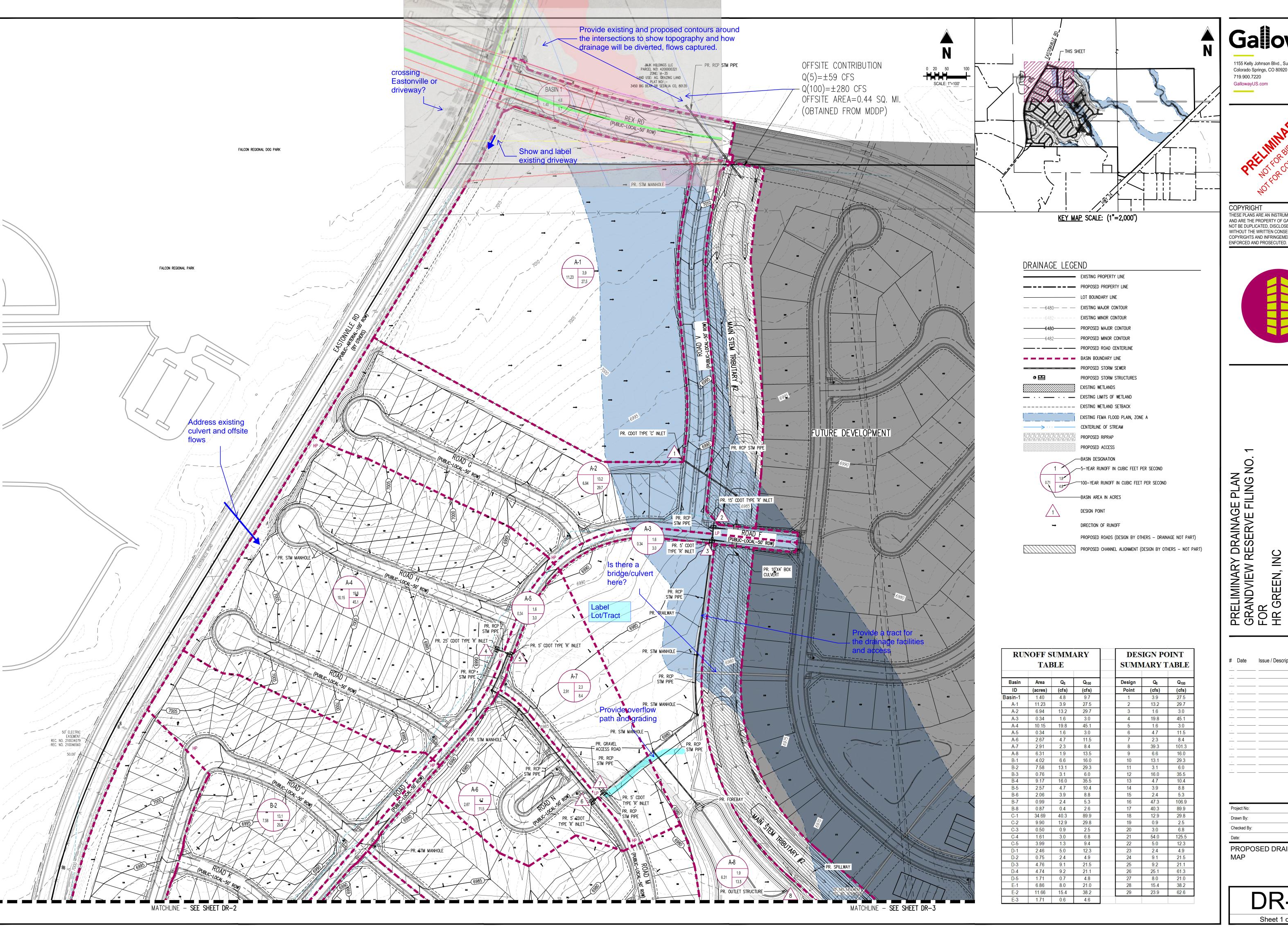
MHFD-Detention_v4.04 - Pond E.xlsm, Basin 7/29/2021, 12:04 PM



MHFD-Detention_v4.04 - Pond E.xlsm, Basin 7/29/2021, 12:04 PM

APPENDIX F Drainage Maps

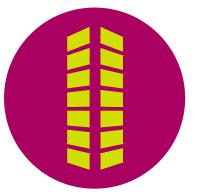
Provide detailed existing conditions plan(s) for the PUDSP area.



1155 Kelly Johnson Blvd., Suite 305 Colorado Springs, CO 80920 GallowayUS.com



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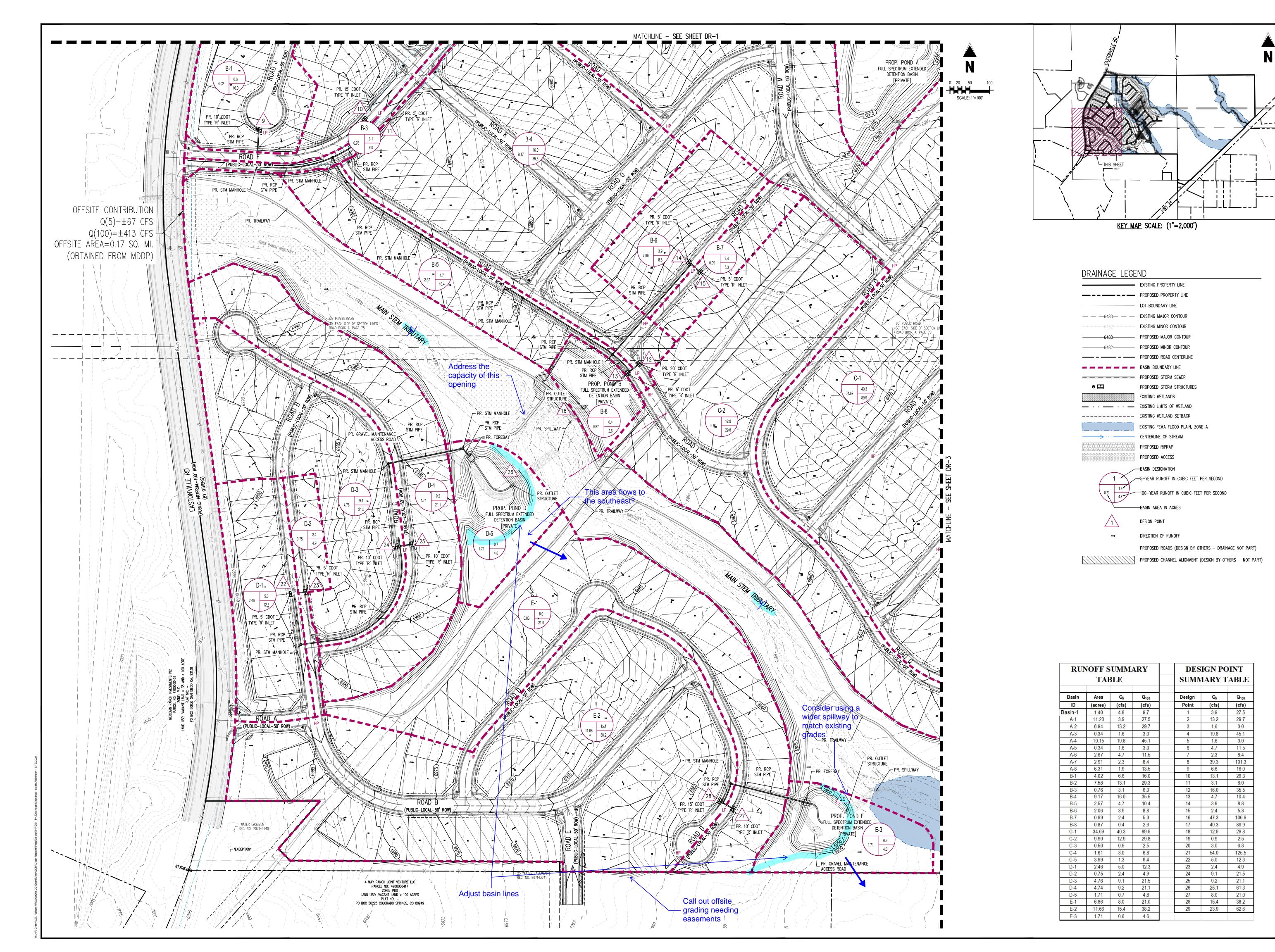


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Project No:	HRG 1.20	
Drawn By:	TJE	
Checked By:	GRD	
Date:	8/13/2021	
DPODOSED DPAINAGE		

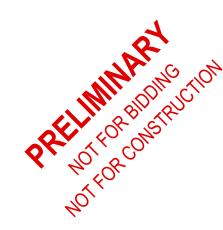
PROPOSED DRAINAGE

Sheet 1 of 3



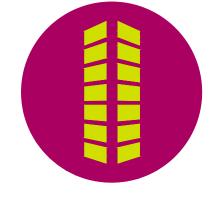


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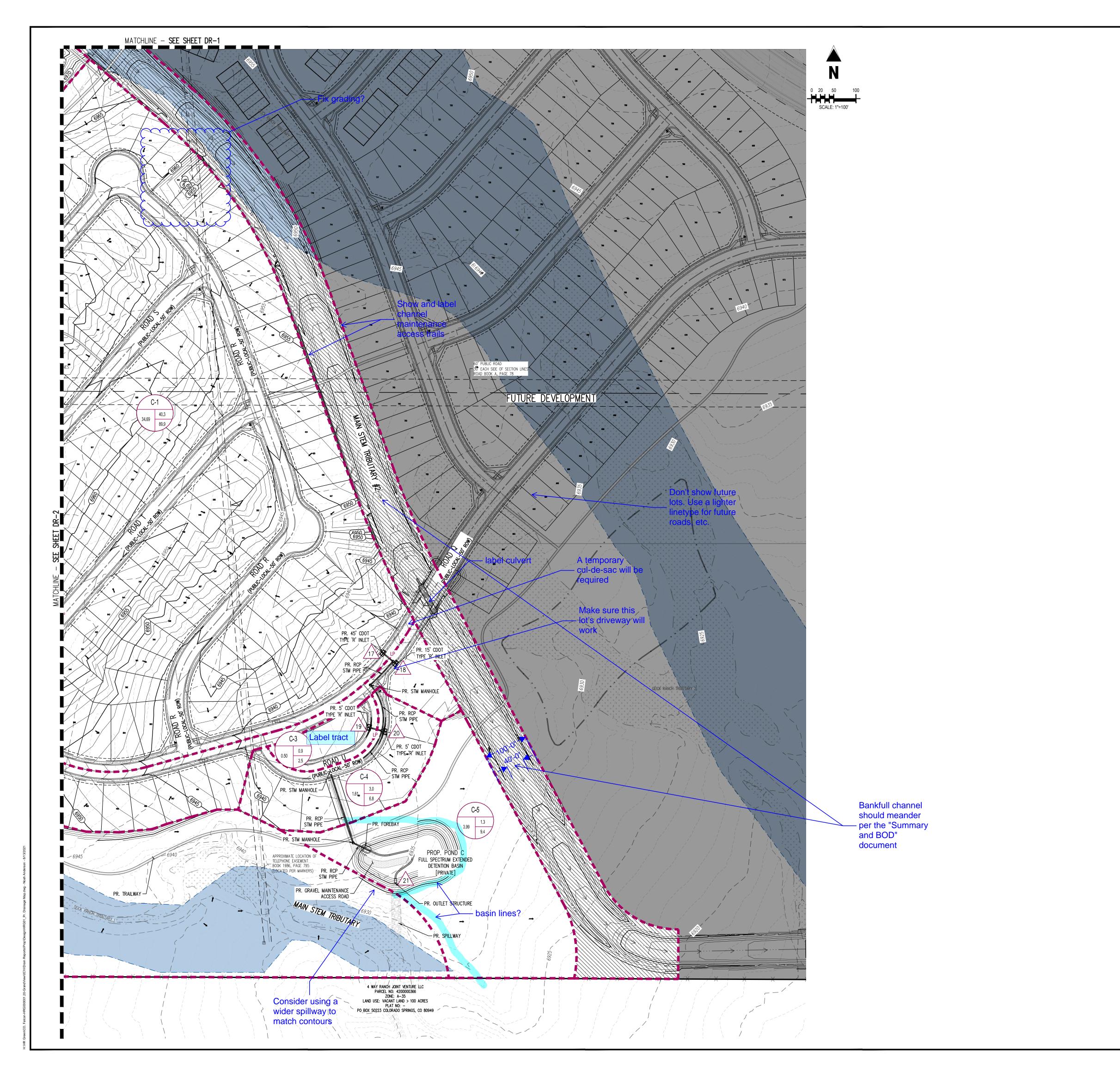


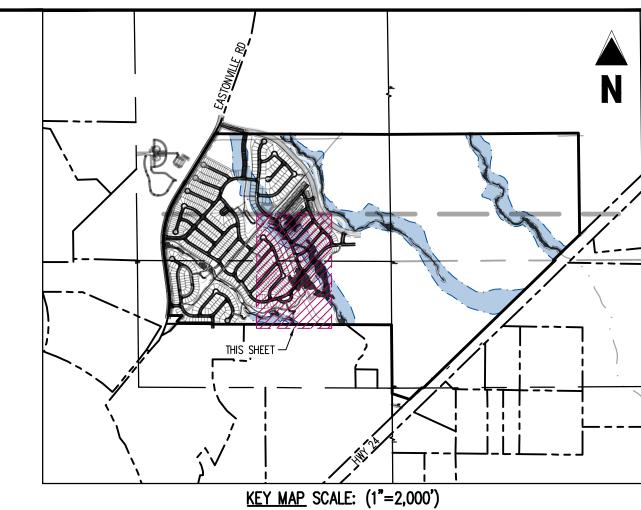
PRELIMINARY DRAINAGE PLANGRANDVIEW RESERVE FILING FOR HR GREEN, INC

HRG 1.20 TJE GRD 8/13/2021

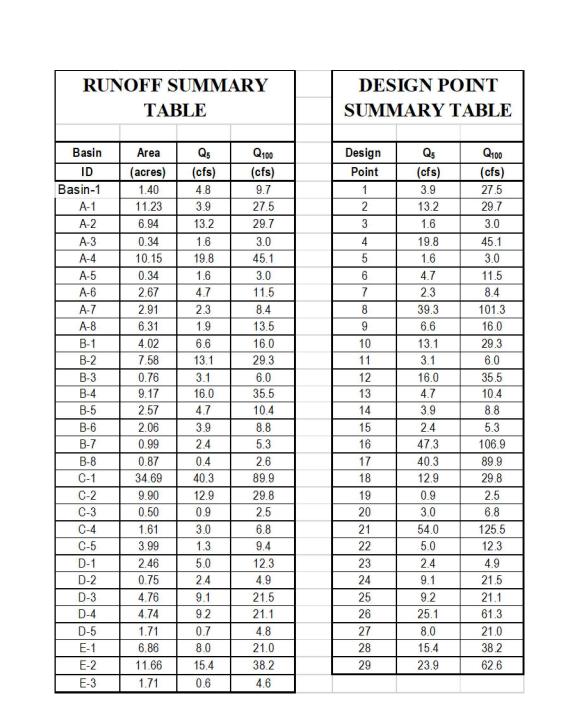
PROPOSED DRAINAGE

Sheet 2 of 3





ENFORCED AND PROSECUTED. DRAINAGE LEGEND EXISTING PROPERTY LINE PROPOSED PROPERTY LINE _____ LOT BOUNDARY LINE EXISTING MINOR CONTOUR 6480———— PROPOSED MAJOR CONTOUR BASIN BOUNDARY LINE PROPOSED STORM SEWER PROPOSED STORM STRUCTURES EXISTING WETLANDS — · · — EXISTING LIMITS OF WETLAND ---- EXISTING WETLAND SETBACK EXISTING FEMA FLOOD PLAIN, ZONE A PROPOSED RIPRAP



PROPOSED ACCESS

—BASIN DESIGNATION

0.71 | 100-YEAR RUNOFF IN CUBIC FEET PER SECOND

—BASIN AREA IN ACRES

DIRECTION OF RUNOFF

DESIGN POINT

____5_YEAR RUNOFF IN CUBIC FEET PER SECOND

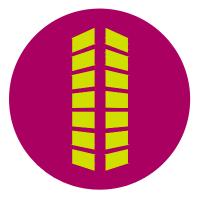
PROPOSED ROADS (DESIGN BY OTHERS - DRAINAGE NOT PART)

PROPOSED CHANNEL ALIGNMENT (DESIGN BY OTHERS - NOT PART)

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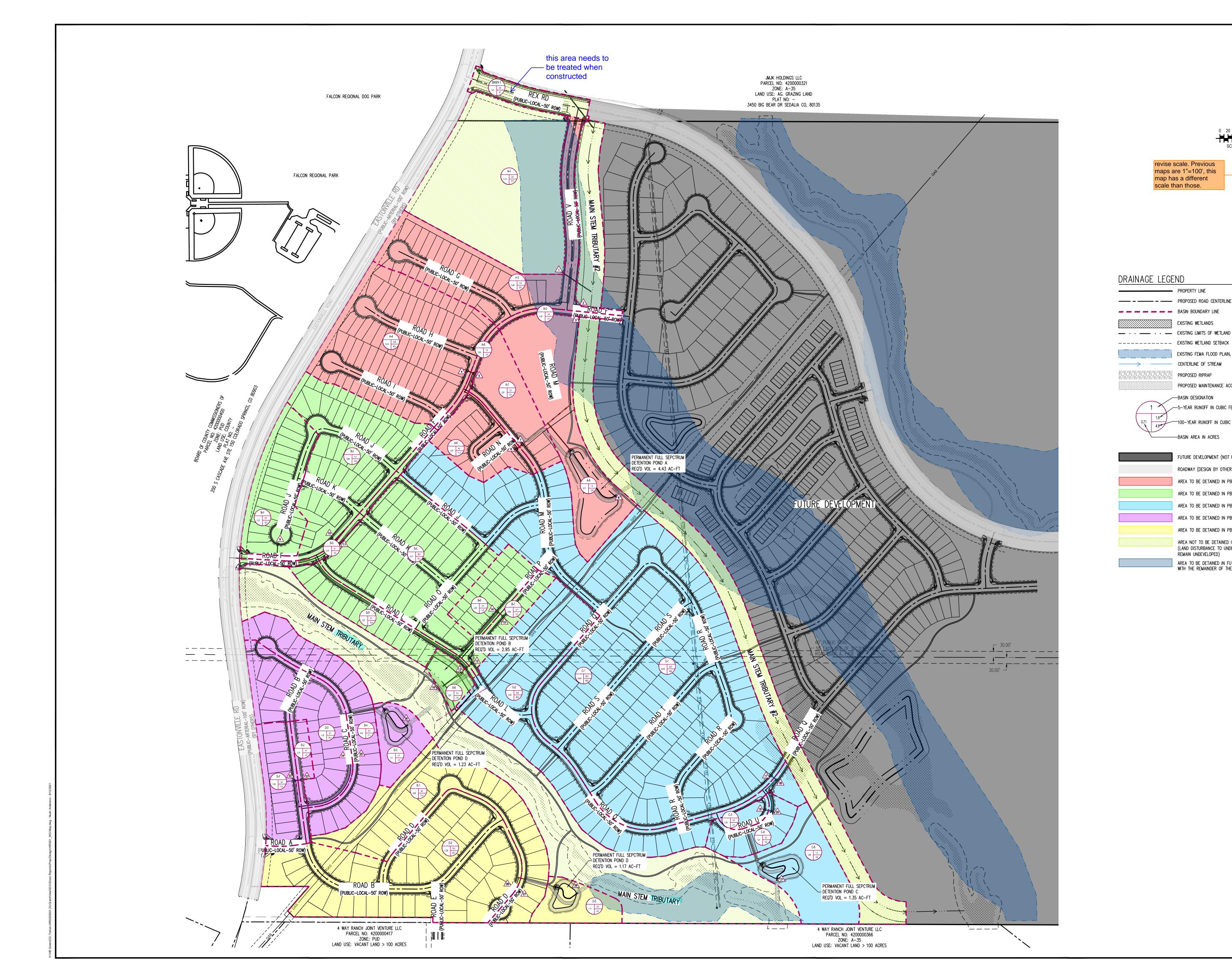
AN IG NO PRELIMINARY DRAINAGE PLANGRANDVIEW RESERVE FILING FOR HR GREEN, INC

Date Issue / Description

Date:	8/13/2021	
Checked By:	GRD	
orawn By:	TJE	
Project No:	HRG 1.20	

PROPOSED DRAINAGE

Sheet 3 of 3



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revise scale. Previous maps are 1"=100', this

map has a different scale than those.

PROPERTY LINE

EXISTING WETLANDS

—BASIN DESIGNATION

----BASIN AREA IN ACRES

EXISTING FEMA FLOOD PLAIN, ZONE A

PROPOSED MAINTENANCE ACCESS

100-YEAR RUNOFF IN CUBIC FEET PER SECOND

FUTURE DEVELOPMENT (NOT PART)

ROADWAY (DESIGN BY OTHERS - NOT PART)

AREA TO BE DETAINED IN PBMP (POND A)

AREA TO BE DETAINED IN PBMP (POND B)

AREA TO BE DETAINED IN PBMP (POND C)

AREA TO BE DETAINED IN PBMP (POND D)

AREA TO BE DETAINED IN PBMP (POND E)

REMAIN UNDEVELOPED)

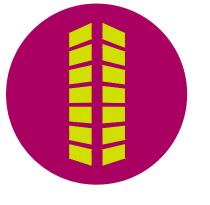
AREA NOT TO BE DETAINED IN PBMP PER SECTION I.7.1.B.7 (LAND DISTURBANCE TO UNDEVELOPED LAND THAT WILL

AREA TO BE DETAINED IN FUTURE PBMP WITH THE REMAINDER OF THE REX RD DEVELOPMENT

____5_YEAR RUNOFF IN CUBIC FEET PER SECOND



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PRELIMINARY DRAINAGE PLANGRANDVIEW RESERVE FILINGFOR HR GREEN, INC

Date	Issue / Description	Init.

Project No:	HRG 1.20
Drawn By:	NJA
Checked By:	GRD
Date:	8/12/2021
WQ MAP	