## PRELIMINARY DRAINAGE REPORT

## **FOR**

# CROSSROADS MIXED USE EL PASO COUNTY, COLORADO

#### FEBRUARY 2021

# Prepared for: Crossroads Metropolitan District No. 2 Mr. Danny Mientka 90 South Cascade Avenue, Suite 1500 Colorado Springs, Colorado Springs 80903

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# Prepared by:



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> Project #18-003A PCD Filing No.: SP-20-011

#### **PRELIMINARY DRAINAGE REPORT FOR CROSSROADS MIXED USE**

#### **DRAINAGE PLAN STATEMENTS**

#### **ENGINEERS STATEMENT**

The attached drainage plan and report was prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according

to the criteria established by the County for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.
Virgil A. Sanchez, P.E. #37160 For and on Behalf of M&S Civil Consultants, Inc
DEVELOPER'S STATEMENT
I, the developer have read and will comply with all the requirements specified in this drainage report and plan.
BY:
BY: Danny Mientka –Owner
DATE:
ADDRESS: The Equity Group, LLC 90 South Cascade Avenue, Suite 1500 Colorado Springs, CO 80903
EL PASO COUNTY'S STATEMENT
Filed in accordance with the requirements of El Paso County Land Development Code, Drainag Criteria Manual Volumes 1 and 2, and the Engineering Manual, as amended.
BY: DATE:  Jennifer Irvine, P.E.  County Engineer / ECM Administrator
<u>CONDITIONS:</u>

#### PRELIMINARY DRAINAGE REPORT

#### **FOR**

#### **CROSSROADS MIXED USE**

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#### PRELIMINARY DRAINAGE REPORT FOR CROSSROADS MIXED USE

#### Purpose

This preliminary drainage report for Crossroads Mixed Use is in support of a Preliminary Plan and Rezone of the subject site. This report functions to identify the existing and proposed runoff patterns and recommend proposed drainage improvements which are intended to safely convey runoff through the proposed development, while minimizing impacts to downstream facilities and adjacent properties.

A Final Drainage Report for this site and Construction Drawings will be submitted concurrently with the Final Plat. Individual drainage letters and/or reports shall be required with the development of each lot not otherwise clearly analyzed by the aforementioned by this Final Drainage Report for Crossroads Mixed Use.

#### **Project Location and Description**

The subject site is located at 0 Meadowbrook Parkway in the southwestern quarter of Section 8, Township 14 South, Range 65 West of the 6<sup>th</sup> P.M. in El Paso County, Colorado. The 29.04 Acre site is currently undeveloped. The site is bound to the west by undeveloped Softball West Subdivision Filing No.2, to the north by Meadowbrook Crossing Subdivision and south by Highway 24 and to the east by Newt Drive.

The proposed site is will be developed into ten (10) commercial lots, one (1) multifamily residential and three tracts. The development will extend Meadowbrook Parkway to the west and will include a single lane roundabout to be constructed at the intersection of the Meadowbrook Parkway and Newt Drive. The property is within the commercial aviation district overlay. A concurrent rezone application has been submitted to rezone 12.695 acres from CR to the RM-30 Zone.

The majority of the existing site is covered with native grasses with fair to good cover, the exception being portions of the future Meadowbrook Parkway corridor where exposed soils are present. Known earthwork operations to "borrow material" have occurred over a small segment of the eastern portion of the site in early and mid 2019, but have since stabilized. A few dirt paths/trails are present along the far west end of the site, likely from recreational vehicles. Generally the site slopes from east to west at slightly greater than 1% with some localized depressions and general terrain undulations near the west boundary that have slopes ranging from 1-20%. Some of these may be the results of previous earthwork activities. The site lies within the Sand Creek Drainage Basin. No existing drainage facilities or improvements exist onsite. No known irrigation or wells are present.

#### Soils

Soils in the project area have been determined to be Blakeland Loamy Sand (8) and Blendon Sandy Loam (10) which are characterized to be part of Hydrologic Soil Types "A" & "B" as determined from the United States Department of Agriculture (USDA) Natural Resources Conservation Service (NRCS) "Web Soils Survey". A soils map illustrating the site location and soil types is provided in the appendix of this report.

#### Floodplain Statement

According to the Federal Emergency Management Agency (FEMA) Flood Insurance Rate Map (FIRM) Nos. 08041C0754 G & 08041C0752 G, effective date December 7<sup>th</sup>, 2018; none of the site lies within a designated floodplain. A copy of these annotated maps can be found in the appendix. The Sand Creek East Fork Channel is located to the northwest of the adjacent Meadowbrook Crossing subdivision.

#### **Previous Studies**

The area which encompasses Crossroads Mixed Use has been previously studied. Below is a short outline of the assumptions regarding the lands of the subject site and those based upon the previously assembled and approved drainage reports and how the assumptions within them impact the subject site.

Sand Creek Drainage Basin Planning Study, Preliminary Design Report", prepared by Kiowa Engineering Corporation, dated January 1993, revised March 1996.

- Establishes that the subject site falls within the East Fork Sand Creek Drainage Basin a portion of the larger Sand Creek Watershed
- Establishes that there are no requirements for major infrastructure improvements and subsequently no drainage improvement related reimbursements with the development of this parcel
- Drainage fees shall be required to plat

"Claremont Business Park Filing No.2 prepared by Matrix Design Group, revised November 2006

- Establishes the drainage patterns of offsite Basins 0S4 and E2 which are to be conveyed within the Meadowbrook Rights of Way
- Established up-gradient offsite drainage to be directed under Meadowbrook north to offsite East Fork Sand Creek Channel, and away from the subject site

"Final Drainage Report, Lot 1 24/94 Business Park Filing No.1 prepared by Core Engineering Group, dated July 14, 2016

• The development of the 24/94 Business Park FDR shows future curb inlets along the future

- Meadowbrook Parkway extension on the south and west corners of the intersection to capture runoff from up-gradient watersheds in addition to a proposed inlet which was to be located above the intersection at the northwest corner of the subject site.
- Establishes that flows from the parcel upstream of the convenience store (29/94 FDR Basin OS4) EX-B now to be collected by the extension of a 36" RCP along the south side of Meadowbrook Parkway. Runoff within the right of way/roadway separated out as Basin EXA2.
- Continues assumption that flows from Newt Drive be conveyed north to East Fork Sand Creek.
- Evaluated predevelopment drainage patterns for subject site. Including direct discharge flow rates to the CDOT rights of way of 1.9 and 14.5 cfs for the 5 and 100 year events respectively. (Basin EX-E).

"Preliminary and Final Drainage Report Meadowbrook Crossing Filing No. 1 and Filing 2, El Paso County, Colorado prepared by Kiowa Engineering Corporation, dated July 25, 2017

- Proposed the installation of a future 10' Type R inlet at the southeast corner of Newt Drive and Meadowbrook Parkway with the extension of Meadowbrook Parkway to the west (along the northern boundary of the subject site). The inlet was to function to collect offsite runoff from a portion of the south half of Meadowbrook Parkway and Newt Drive north of Hwy 24. Intercepted runoff would be conveyed via a proposed 24" storm sewer to the existing storm sewer system within the Meadowbrook Crossings development.
- Proposed the installation of a 10' Type R inlet at the west end of future Meadowbrook Parkway. The inlet was to collect runoff from the north half of the future roadway. An 18" storm drain was proposed to convey collected runoff to the existing water quality pond located within the Meadowbrook Crossings Development. The report indicates a separate forebay or the modification of an existing forebay would be required.
- Shifted the location of the existing 10'ft Type R curb inlet to be installed upstream of the intersection of Newt Drive (as shown with the 24/94 Business Park FDR), flows in excess of the inlet capacity are to continue within the future Meadowbrook.

"Final Drainage Report for Meadowbrook Dirt Borrow Site, El Paso County Colorado, prepared by M&S Civil Consultants, November 2018.

- Evaluated onsite drainage patterns
- Excluded offsite runoff impacts from areas to the east of site.
- Allowed site to be utilized as a "borrow site" for offsite earthwork activities.

#### **Hydrologic Calculations**

Hydrologic calculations were performed using the El Paso County and City of Colorado Springs Storm Drainage Design Criteria manual and where applicable the Urban Storm Drainage Criteria Manual. The Rational Method was used to estimate stormwater runoff anticipated from design storms with 5-year and 100-year recurrence intervals.

#### **Hydraulic Calculations**

Hydraulic calculations were estimated using the Manning's Formula and the methods described in the El Paso County and City of Colorado Springs Storm Drainage Design Criteria manual. The relevant data sheets are included in the appendix of this report. Hydraulic grade line calculations shall be provided with the Final Drainage report.

#### **Drainage Criteria**

This drainage analysis has been prepared in accordance with current El Paso County Drainage Criteria Manual and where applicable the City of Colorado Springs and Mile High Flood District Criteria Manuals. Calculations were performed to determine runoff quantities for the 5-year and 100-year frequency storms for developed conditions using the Rational Method as required for basins having areas less than 100 acres. See Appendix for supporting calculations.

#### **Historic (Pre-Grading) Drainage Characteristics**

The historic drainage patterns discussed within this report reflect the site conditions prior to the approval of the 2018 Meadowbrook Dirt Borrow Site Grading and Erosion Control Plan. This 'historic condition' generally coincides with the existing condition analysis and mapping that accompanied that project's hydrologic analysis.

The following excerpt is from the existing Drainage Characteristics section of the Final Drainage Report for Meadowbrook Dirt Borrow Site, El Paso County, Colorado, by M&S Civil Consultants and adequately describes the general site characteristics prior to grading.

"Site vegetation is sparse, consisting primarily of native grasses and weeds. The parcel possesses a ridgeline that bisects the parcel, directing runoff to the south and west boundaries, with slopes varying from 1% to 20%. A few small depressions are located on site, near the west boundary. For the purposes of hydrologic analysis, the small depressions are not considered to detain runoff."

Given the increase in breath and scope of this study, significant consideration of the impacts of offsite drainage from the adjacent developments will evaluated. This includes drainage from a small portion of Hwy 24 which combines with flows within existing from portions of Newt Drive. Runoff from this offsite area combines with by-pass flows from two inlets located within existing Meadowbrook Drive, prior to entering the site at its northeast corner. Runoff from these locations ultimately combines with onsite flows within the proposed Meadowbrook Parkway corridor, before discharging to downstream properties.

The detailed description of the historic (pre-grading) condition is as follows. Please refer to the historic conditions drainage map which is provided within the appendix of this report.

#### **Historic Conditions - Detailed Drainage Discussion**

#### **Design Point 1**

Basin E2 (Claremont Business Park Filing No.2) consists of a reported 3.86 developed acres of Development located along the southeastern half of existing Meadowbrook Parkway some 1200' northeast of the subject site. Runoff produced by the offsite development (CBPF2 Lot 46) is conveyed to Meadowbrook Parkway at flow rates of Q5=15.1, Q100=28.6 cfs in the 5 and 100-year storm events respectively. The collected flows combines with runoff from Basin EX-A2 (Lot 1 24/94 Business Park Filing No.1) (Q5=2.5, Q100=4.5 cfs) which consist of 0.59 acres of the southeastern half of Meadowbrook Parkway located immediately east of existing Newt Drive. The collected flows from the two basins culminate at Design Point 1 at peak rates of Q5=14.2 and Q100=26.5 cfs. An existing 10' CDOT Type R at-grade inlet (Inlet 1) intercepts flows of Q5=8.4 and Q100=11.1 cfs, with subsequent by-pass flows of 5.8 and 15.4 cfs in the 5 and 100 year events. Surface flows continue west within the south half of existing Meadowbrook Parkway.

#### **Design Point 2**

**Basin OS-A (Meadowbrook Crossing Filing 1 and 2)** consists of 1.29 acres of the northern half of existing Meadowbrook Parkway located immediately east of Newt Drive. Runoff produced within this basin totals Q5=3.1 and Q100=6.0 cfs. An existing 10' CDOT Type R at grade inlet (Inlet 2) collects runoff of Q5=3.1 and Q100=5.3 cfs, with subsequent by-pass flows in only the 100 year event of 0.7 cfs. Runoff leaving the design point continuing west within the north half of existing Meadowbrook Parkway.

#### **Design Point 3**

**Basin OS-1** consists of approximately 1.28 developed acres of existing Newt Drive located along the eastern boundary of the site. Runoff produced within the basin (Q5=5.8 cfs, Q100=10.5 cfs) combine with flow-by from **DP1** in the intersection at peak flow rates of 9.8 cfs, and 22.5 cfs in the 5 and 100-year storm events.

Surface runoff and by-pass flows from both **DP2** and **DP3** entering **Basin A**, and the undeveloped rights of way of future Meadowbrook Parkway, at the northeast corner of the site.

#### **Design Point 4**

**Basin A** consists of 12.88 undeveloped acres located along the northern boundary that drain from east to west across the subject site. Runoff produced by this basin (Q5=1.9 cfs, Q100=14.2 cfs) combine with flows from **DP2 and DP3.** The cumulative runoff at **DP4** of Q5=7.4 cfs, Q100=27.7 cfs discharges onto the adjacent property (Lot 1, Softball West Subdivision 2) along the western boundary of the site, approximately 250' to south of the northern property line.

#### **Design Point 5**

**Basin B** consists of 13.63 undeveloped acres located along the western side of the subject site. Runoff produced by the basin generally flows from northeast to southwest discharging onto the adjacent property (Lot 2, Softball West Subdivision 2) approximately 200' north of the southern property line. Runoff reaching the boundary at **DP5**, is estimated at 8.3 cfs and 18.2 cfs in the 5 year and 100 year events respectively.

#### **Design Point 6**

**Basin** C currently consists of 5.89 undeveloped acres located along the southern boundary of the site. Runoff produced within the basin travels east to west as sheet flow before eventually discharging into the existing barrow ditch which travels along the US HWY 24 CDOT right of way. Peak runoff rates reaching the subdivision boundary at this location are calculated at 1.2 cfs and 8.5 cfs in the 5 year and 100 year events respectively.

#### **Design Point 7**

**Basin OS-2** consists of 4.98 acres of a portion of the northern half of the US HWY 24 roadway and adjoining native grass lined barrow ditch. Runoff produced within the basin combines with runoff from the subject site (**DP6**) at cumulative peak runoff rates of 10.4. and 31.9 cfs in the 5 and 100 year storm events at **DP7**. A modeled hydraulic cross section of the ditch section at **DP7** calculates flow depths of 0.76 feet traveling at a velocity of approximately 3.54 feet per second. Input parameters for this analysis can be found in the Hydraulics section of the Appendix below.

Runoff from **Design Points 4 and 5** ultimately combine with the flows from **DP7** within the barrow ditch of US Hwy 24 several hundred feet downstream of the subject site. An existing 36" RCP culvert located at the interchange of HWY 24 and Peterson Road aids in conveying a portion of the runoff from the subject site and adjacent offsite areas under the roadway. Flows in excess of the culverts carrying capacity, overtop the roadway before rejoining within a subsequent drainage swale that parallels the west bound HWY 24 on-ramp. Ultimately flows discharge into the East Fork of the Sand Creek via an existing riprap rundown. Site visits conducted by M&S Civil at the time of the writing of this report, found no significant signs of erosion or deposition along the aforementioned corridor.

A Drainageway Exhibit in the appendix of this report provides and aerial illustration the aforementioned conveyance route to the channel, which will also serve to function as the emergency overflow path for the proposed site development.

#### **Existing Drainage Characteristics**

The subject site has been utilized as a "borrow site" to provide surplus earthwork to offsite developments in the area. This recent grading effort occurred during the spring and summer of 2019. At the request of El Paso County, an existing condition drainage analysis has been provided to show the changes to the topography and drainage pattern as a result of this effort. As the only changes between the two conditions are onsite, the offsite drainage patterns calculations and assumptions determined with the historical analysis will remain the same. It should be noted that

the subject site was not disturbed to the full extent of the approved plan, with limited excavation primarily occurring within the eastern side of the subject site.

In the existing condition, vegetation remains sparse, consisting primarily of native grasses and weeds with good to fair cover. Areas disturbed by grading activities were reseeded and have since stabilized. In regarding to historic versus existing drainage basin delineation, the bisecting parcel ridgeline has been relocated further to the south, which results in redirectingmore of the runoff to the southwestern part of the site and less to the CDOT rights of way. The few small depressions remain on site, near the west boundary. For the purposes of hydrologic analysis, these small depressions will continue to not be evaluated for their ability to detain runoff. Ultimately, all runoff from the parcel is conveyed to the west toward to existing drainage facilities located under Peterson Road and ultimately the East Fork of Sand Creek as in the historic condition.

This section only discusses the changes in basin geometry and drainage pattern and provides a direct comparison the historic versus existing conditions utilizing the same outfall (design) points, which have remained undisturbed.

#### **Design Point 4**

**Basin A** currently consists of 11.02 acres which continues to drain from east to west eventually discharging along the western boundary of the site, approximately 250' south of the northern property line. Peak runoff, post grading, is lower at an estimated 7.1 cfs and 25.5 cfs (**Design Point 2**) as compared to the historic condition flow rates of 7.4 cfs and 27.7 cfs in the 5-year and 100-year events respectively

#### **Design Point 5**

**Basin** C currently consists of 7.84 acres that drain from northeast to southwest eventually discharging along the western boundary of the site, approximately 200' north of the southern property line. Peak runoff rates at this location, are also than lower than the historic conditions with post grading flows of 5.0 cfs and 14.5 cfs at **Design Point 3** as compared to 8.3 cfs and 18.2 cfs in the 5-year and 100-year events respectively. Despite the basin currently being larger in area than in the historic condition, a decrease occurs in the peak flow rates as a result of a longer flow path to the given design point.

#### **Design Point 6**

**Basin A** consists of 3.99 undeveloped acres that drains from east to west into the US HWY 24 Right of Way at the southern boundary of the site. Peak runoff at this location is lower than the historic condition at an estimated 0.9 cfs and 6.3 cfs (**DP 6**), as compared to 1.2 cfs and 8.5 cf in the 5-year and 100-year events respectively.

#### **Design Point 7**

**Basin OS-2** consists of 4.98 acres of the northern half of the US HWY 24 roadway and adjoining native grass lined barrow ditch. Runoff produced within the basin combines with runoff from the subject site (**DP6**) at a lower cumulative peak runoff rates of 9.9 and 28.0 cfs in the 5 and 100-year storm events at **DP7**.

#### **Four Step Process**

- **Step 1** Employ Runoff Reduction Practices Approx. 2.54 acres of the proposed development is being set aside for a Full Spectrum Detention (FSD) Pond. Whenever possible, runoff produced within developable area containing impervious surfaces will be routed through landscaped areas or earthen swales (grass-lined where slope exceeds 2%) to minimize direct connection of impervious surfaces. In the interim, runoff will be reduced through the use of (4) temporary sediments ponds until the ground has been stabilized with vegetation or permanently developed.
- **Step 2 Provide Water Quality Capture Volume** A Full Spectrum Detention Pond is proposed to reduce peak discharge rates and provide water quality treatment. In the interim stage, four (4) temporary Sedimentation Ponds are provided to collect sediment for the disturbed area this will function to maintain existing water quality levels during construction, and prior to permanent development.
- Stabilize Drainageways The site will use a Full Spectrum Detention (FSD) Pond to control developed runoff that is discharging into an existing CDOT ROW roadside ditch and ultimately into Sand Creek. The FSD outlet structure will be designed to drain the water quality event storm in 40 hours, while reducing the 100 year peak discharge to approximately 90% of the predevelopment conditions. As the flow is discharged offsite, it continues southwest in CDOT's manmade roadside ditch until it reaches Peterson Road. From here, it is conveyed to the other side of the road, into a similar earthen channel, via a 36" CMP culvert. The drainage continues southwest in the right of way, until it reaches the East Fork Sand Creek Channel. Rip Rap barriers are lined throughout this portion of the pathway approximately every 90-100 feet to the channel. The Drainageway Exhibit provided in the Drainage Maps section of the Appendix provides a better visual representation of this information.

The development of this site is not anticipated to have negative effects on downstream drainage ways since flows released will be below historic rates. In the interim, the site proposes four temporary sedimentation ponds, before discharging at the southwest property corner of the site and onto an adjacent undeveloped property via riprap-lined spillways. This ensures that in this stage of the development negative effects on the downstream drainage ways will be avoided.

**Step 4 Consider Need for Industrial and Commercial BMP's** – The proposed development will implement a Stormwater Management Plan including property housekeeping practices and spill containment procedures.

#### **Proposed Drainage Characteristics**

The proposed site is will be developed into ten (10) commercial lots, one (1) multifamily residential and three tracts. The proposed development will extend Meadowbrook Parkway to the west and will include a single lane roundabout to be constructed at the intersection of the Meadowbrook Parkway and Newt Drive to aid in traffic control. A proposed private looped roadway, Crossroad Heights, will extend into the site to provide access and a utility corridor to both the commercial and

residential developments. At this time, it is anticipated that the development and design of Lot 11 (by others) is planned to occur concurrently with the construction of the proposed utilities and infrastructure provided by this plan. Coordination is ongoing, as such; the routing of storm sewer main line thru the site and the planned outfall locations will be formalized with the Final Drainage Report. A separate drainage letter or report will be required for that portion of the development.

The following summary generalizes the proposed drainage patterns and drainage improvements required to safely route developed runoff to downstream facilities.

A storm sewer pipe and inlet will be constructed at the southwest corner of the newly constructed roundabout to aid in collecting runoff reaching the site from offsite watersheds. These facilities will connect to the existing system located inside the existing Meadowbrook Subdivision. Bypassed flows and developed flows within the newly constructed Meadowbrook Parkway will be collected by a pair of sump inlets located at the west end of the roadway. The drainage facilities located with the rights of way will be public all remaining onsite storm sewer and drainage improvements shall be private. A private looped roadway will provide access and utility corridors for development. Private storm sewer mains, stubs, and inlets will be extended along these corridors to serve the development. The extension of these facilities beyond what is shown by this plan is likely with future development. Runoff collected by the infrastructure will be conveyed to a single full spectrum detention pond located in the southwest corner of the subdivision. The proposed outfall from the pond is planned to discharge to the existing barrow ditch located with the north half of the existing CDOT Right of Way. A drainage easement will be required from CDOT for the outfall and slope protection facilities that fall within the corridor. It should be noted that the storm outfall will be shaped into the existing hillside and any soil riprap protection will be buried. Runoff leaving the site and entering the CDOT corridor will discharge at less than historic rates. The previous discharge points along the west boundary of the subject site which also previously contributed to the barrow ditch will be virtually eliminated, further reducing the peak flow rates to downstream facilities.

#### **Proposed Detailed Drainage Discussion**

#### **Design Point 1**

Basin E2 (Claremont Business Park Filing No.2) consists of a reported 3.86 developed acres of Development located along the southeastern half of existing Meadowbrook Parkway some 1200' northeast of the subject site. Runoff produced by the offsite development (CBPF2 Lot 46) is conveyed to Meadowbrook Parkway at flow rates of Q5=15.1, Q100=28.6 cfs in the 5 and 100-year storm events respectively. The collected flows combines with runoff from Basin EX-A2 (Lot 1 24/94 Business Park Filing No.1) (Q5=2.5, Q100=4.5 cfs) which consist of 0.59 acres of the southeastern half of Meadowbrook Parkway located immediately east of existing Newt Drive. The collected flows from the two basins culminate at Design Point 1 at peak rates of Q5=14.2 and Q100=26.5. An existing 10' CDOT Type R at-grade inlet (Inlet 1) intercepts flows of Q5=8.4 and Q100=11.1, with subsequent by-pass flows of 5.8 and 15.4 cfs in the 5 and 100 year events. Surface flows continue west within the south half of existing Meadowbrook Parkway.

#### **Design Point 2**

**Basin OS-A (Meadowbrook Crossing Filing 1 and 2)** consists of 1.29 acres of the northern half of existing Meadowbrook Parkway located immediately east of Newt Drive. Runoff produced within this basin totals Q5=3.1 and Q100=6.0 cfs. An existing 10' CDOT Type R at grade inlet (**Inlet 2**) collects runoff of Q5=3.1 and Q100=5.3 cfs, with subsequent by-pass flows in only the 100 year event of 0.7 cfs. Runoff leaving the design point continuing west within the north half of existing Meadowbrook Parkway.

#### **Design Point 3**

**Basin OS-1** consists of approximately 1.40 acres of existing Newt Drive that will be retrofitted with new raised median as part of an intersection conversion to a roundabout. Runoff produced within the basin (Q5=6.5, Q100=11.6 cfs) will combine with flow-by from **DP1** at a proposed public 10'a-grade inlet located at DP3. A proposed public 24 storm sewer (**PR1**) will convey water across the intersection to the existing 42" storm sewer with Meadowbrook Crossings in accordance with that subdivisions drainage report. A new larger manhole may be required to make the connection to the existing line. It is important to note that this connection remains feasible as the roundabout is not anticipated to significantly increase the overall imperviousness of the area above that of the existing condition. Runoff in excess of the inlet capacity (Q5=3.5 and Q100=13.5 cfs) will continue westward via the curb and gutter of Proposed Meadowbrook Parkway.

#### **Design Point 4**

**Basin A** consists of 1.68 acres of the north half of proposed Meadowbrook. Runoff within this basin (Q5=6.5, Q100=11.6 cfs) combines with minor flow by from **DP2**. A proposed 10' sump inlet located at west end of the roadway will prevent developed flows from leaving the roadway corridor. The inlet will convey intercept runoff of 6.5 and 19.1 (split 100 yr flows with DP5) underneath the roadway via a public 24" RCP (**PR2**).

flow rate.

#### **Design Point 5**

**Basin B** consists of 1.49 acres of the south half of proposed Meadowbrook Parkway. Runoff produced within this basin (Q5=5.8, Q100=10.4 cfs) combines with flow-by leaving **DP3**. A proposed public 10' sump inlet located at west end of the roadway will prevent developed flows from leaving exiting the roadway corridor. The intercepted runoff of 9.9 cfs and 19.1 cfs in the 5 and 100 year events respectively will combine with **PR2** flows in a 36" Private storm sewer system (**PR3**). Combined flows within the proposed system are calculated to peak at 16.4 and 38.2 cfs.

#### **Design Point 6**

**Basin** C consists of 4.61 acres of commercial lots (1-5 and portions of lot 6) located along the east side of the site. A private 36" storm drain (**PR4-PR6**) is provided to collect flows of Q5=5.8 and Q100=10.4 cfs at **DP6** in the 5 and 100 years respectively. Intercepted flows are conveyed west underground within a public access and utility easement.

#### **Design Point 7**

**Basin D** consists of 2.22 acres of commercial lots located between Meadowbrook Parkway and the looped roadway. **Basin D** which includes portions of lot 9 and 10 will require a private 24" storm drain (**PR7**) to collect flows of Q5=9.3 and Q100=17.0 cfs in the 5 and 100 year storm event.

#### **Design Points 8 and 9**

**Basin E** consists of 2.71 acres of commercial lots and roadway located in the central portion of the site. Two private 10' CDOT Type R at-grade inlets (**Inlets 7 and 8**) located on the north and south will each collect flows approximately 4.8 and 6.9 cfs in the minor and major storm events. Runoff collected from the inlets will be conveyed to the south side of the planned roadway via private 24" (**PR8**) and 30" (**PR9**) storm drains. A proposed 36" storm sewer (**PR10**) will convey flows to the west underground a peak flow rates of 35.0 and 60.5 cfs in the 5 and 100 year events. A drainage easement storm sewer easement may need to be provided along this portion of the alignment depending upon the building setback requirements.

#### **Design Point 10 and 11**

**Basin** G consists of 0.94 acres of commercial lots and roadway located in the central portion of the site. Two private 10' CDOT Type R sump inlets (Inlets 7 and 8) located on the east and west side of the street function to collect the runoff from basin G as well as any by pass flows from Design DP8 and 9. Pipe Run 14 a 42" private storm sewer will direct runoff south underground at peak flow rates of 39.9 cfs and 78.1 cfs in the minor and major storm event.

#### **Design Point 12**

**Basin F** consists of 2.57 acres of commercial lots (lot 8 and portions of lot 7) located along the southern boundary of the site. A private 24" storm drain (**PR15**) is provided to collect flows of Q5=10.8 and Q100=19.6 cfs at **DP12** in the 5 and 100 years respectively. Intercepted flows are conveyed west underground to the main line. **Pipe Runs 16** and **17** (private 42" storm sewer) direct the collected runoff to the concrete forebay located within the east end of a proposed full spectrum detention pond at peak flow rates of 05-40.7 and 0100-05.0 cfs

#### Design Point 12

**Basin F** consists of 2.57 acres of commercial lots (lot 8 and portions of lot 7) located along the southern boundary of the site. A private 24" storm drain (**PR15**) is provided to collect flows of Q5=10.8 and Q100=19.6 cfs at **DP12** in the 5 and 100 years respectively. Intercepted flows are conveyed west underground to the main line. **Pipe Runs 16** and **17** (private 42" storm sewer) direct the collected runoff to the concrete forebay located within the east end of a proposed full spectrum detention pond at peak flow rates of Q5=49.7 and Q100=96.0 cfs

#### **Design Points 13**

**Basin H** consists of 11.07 acres of proposed apartment site (Lot 11). Runoff produced within this basin (Q5=26.2, Q100=53.8 cfs) flows from northeast to southwest until it reaches the proposed public 42" RCP storm sewer at the design point. The cumulative flows at **Design Point 13** are Q5=26.2 and Q100=53.8 cfs and will be routed to the full spectrum detention pond at **Design** 

CONNECTION OF

TRÀCT A

POTENTIAL STORM SEWER OUTFALL

**Point 15** via **Pipe Run 18** (Q5=42.1, Q100=91.1)

include a narrative regarding the following notes on the drainage map.

Include a narrative regarding the swale and lot 11 site plan



#### **Design Points 14**

**Basin I** consists of 1.60 acres of proposed apartment site (Lot 11). Runoff produced within this basin (Q5=3.8, Q100=7.8 cfs) flows from north to south and collects in the proposed, grass-lined swale. The cumulative flows at **Design Point 14** are Q5=3.8 and Q100=7.8 cfs and will be routed to the full spectrum detention pond at **Design Point 15**.

#### **Design Points 15**

**Basin J** consists of 3.21 acres of the proposed full spectrum detention pond. Runoff produced within this basin (Q5=2.3, Q100=10.0 cfs) flows from northeast to southwest, combining with flows from **Design Point 14**, **Pipe Run 17**, and **Pipe Run 18**. This combination of runoff collects in the proposed outlet structure of the pond. The cumulative flows at **Design Point 14** are Q5=95.3 and Q100=199.8 cfs, and will be routed to the existing 5' bottom earthen swale in CDOT's Right of Way at **Design Point 16** via **Pipe Run 19** (Q5=1.9, Q100=8.2).

#### **Design Points 16**

**Basin OS-2** consists of 4.98 acres. Approximately half of this basin is comprised of the paved surface of U.S. Highway 24, while the other half is comprised of the 5 foot bottom earthen swale in CDOT's Right of Way. Runoff produced within this basin (Q5=8.7, Q100=19.6 cfs) flows from northeast to southwest, combining with flows from **Design Point 15**. This combination of runoff collects in the existing swale in the right of way. The cumulative flows at **Design Point 16** are Q5=9.9 and Q100=27.7 cfs, which are lower than the historic rates. Flows from this design point continue to downstream infrastructure. A rip rap pad is located at the terminus of the storm sewer. This should be under DP3

In accordance with the assumptions outlined within the Meadowbrook Subdivision Final Drainage Report an offsite public storm sewer pipe and inlet will be constructed at the southwest corner of the newly constructed roundabout to aid in collecting runoff from the a portion of the offsite watersheds located to the east of the site. A new manhole may be required to connect the outfall to the existing pipe located inside the existing Meadowbrook Subdivision. As the area is already paved increases to the imperviousness of this area are not anticipated and thus should not intiate the need for

#### **Water Quality Provisions and Maintenance**

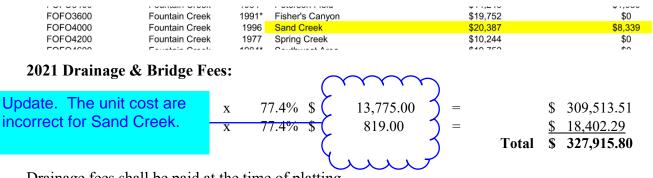
The proposed full spectrum detention (FSD) pond functions to provide detention and water quality for the proposed development. This full spectrum detention pond will function to treat approximately 32.10 acres of tributary area by providing 0.857 acre-feet of storage for the water quality event, 3306 acre feet of storage at the EURV storm event, and 4.729 acre-feet of storage in the 100-year event. The 25' wide emergency spillway is designed with a foot of freeboard in the 100-year event. This spillway safely conveys flows to CDOT's Right of Way in the event of outlet clogging or failure, and will be armored with permanent erosion control fabric. The results show that the FSD pond remains functional in the 100-year event and the outlet structure is able to

discharge flows to the to an existing swale and ultimately to Sand Creek. The sizing for the full spectrum detention facility has been determined using the guidelines set forth in the Urban Drainage and Flood Control District Criteria Manual. Refer to the UDFCD MHFD-Detention, Version 4.03, Excel Workbook located within the appendix of this report for calculations.

The proposed FSD pond will be privately owned and maintained by the property owner or the metropolitan district. Access to the pond shall be granted to the owner/district and El Paso County for access and maintenance of the private facility. A private maintenance agreement document shall accompany this report submittal.

#### **Erosion Control**

It is the policy of the El Paso County that M&S Civil Consultants submit a grading and erosion control plan with the drainage report since pre-development grading is being requested. The plan includes proposed silt fence, vehicle traffic control and (4) temporary sediment basins as proposed as erosion control measures. The plan also includes provisions for stockpiling and staging. A stormwater management plan is provided to accompany the plans.



Drainage fees shall be paid at the time of platting.

<b>Construction Cost Estim</b>	mate (Noi	mbursable)							
Item	Amount	Unit	U	nit Cost		Total Cost			
10' CDOT Type R Inlet	5	EA	\$	9,890.00	\$	49,450.00			
15' CDOT Type R Inlet	2	EA	\$ 1	3,002.00	\$	26,004.00			
Type II MH	8	EA	\$	6,000.00	\$	48,000.00			
18" RCP	181	LF	\$	69.00	\$	12,489.00			
24" RCP	184	LF	\$	107.00	\$	19,688.00			
30" RCP	33	LF	\$	170.00	\$	5,610.00			
42" RCP	746	LF	\$	306.00	\$	228,276.00			
Tot	al Cost:				\$	389,517.00			

M & S Civil Consultants, Inc. (M & S) cannot and does not guarantee the construction cost will not vary from these opinions of probable costs. These opinions represent our best judgment as design professionals familiar with the construction industry and this development in particular. The above is only an estimate of the facility cost and drainage basin fee amounts in 2020.

revise to 2021

#### **Summary:**

The construction of this site is for the purposes of creating commercial lots and an apartment site. Currently, no impervious surfaces are being constructed. The site will be graded and all disturbed areas will be seeded and mulched. Post construction runoff will be discharged to downstream property at rates that are below historic discharge rates. In the historic condition, the total flows leaving the site that reach the East Fork Sand Creek Channel are 19.0 cfs and 68.1 cfs in the 5 year and 100 year storm events, respectively. Through the strategic design and placement of storm sewer infrastructure components, this overall rate is reduced to approximately 50% of historic rates at 9.9 and 27.7 cfs in the proposed condition. Erosion control measures will be implemented to prevent sediment migration. The construction of Crossroads Mixed Use shall not adversely affect adjacent or downstream property. Subsequent drainage reports will be required if and when the site is developed behind the uses defined within this report.

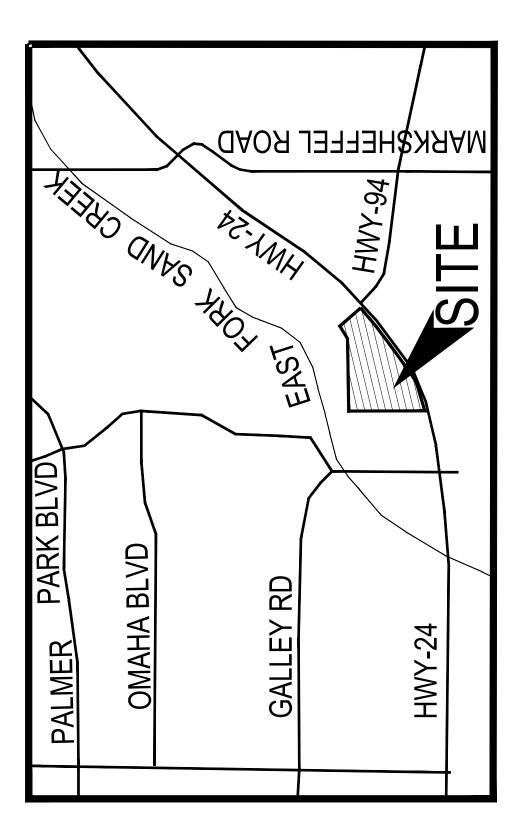
#### **References:**

- 1.) "El Paso County and City of Colorado Springs Drainage Criteria Manual".
- 2.) "Urban Storm Drainage Criteria Manual"
- 3.) SCS Soils Map for El Paso County.
- 4.) Flood Insurance Rate Map (FIRM), Federal Emergency Management Agency, Revised date December 7<sup>th</sup>, 2018.
- 5.) "Final Drainage Report for Claremont Business Park Filing No. 2", dated November 2006, by Matrix Design Group, Inc.
- 6.) "Preliminary and Final Drainage Report Meadowbrook Crossing Filing 1 and Filing 2", dated July 25, 2017, by Kiowa Engineering Corporation.
- 7.) "Final Drainage Report Lot 1 24/94 Business Park Filing No. 1 on Platte Avenue and Meadowbrook Parkway", dated April 28, 2016 and revised July 14, 2016, by Core Engineering Group, LLC.
- 8.) "Final Drainage Report for Meadowbrook Dirt Borrow Site", dated November 2018, by M&S Civil Consultants, Inc.
- 9.) "Sand Creek Drainage Basin Planning Study", revised March 1996, by Kiowa Engineering Corporation.

APPENDIX

VICINITY MAP

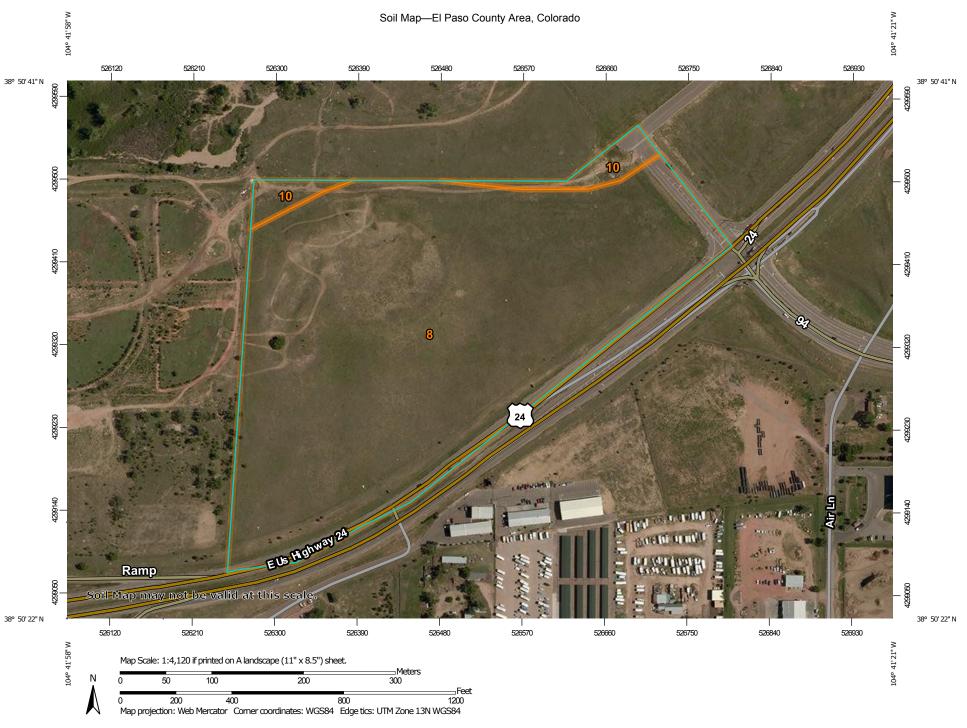




# VICINITY MAP

NTS

**SOILS MAP** 



#### MAP LEGEND

#### Area of Interest (AOI)

Area of Interest (AOI)

#### Soils

Soil Map Unit Polygons



Soil Map Unit Points

#### Special Point Features

Blowout

Borrow Pit

Clay Spot

Closed Depression

Gravel Pit

Gravelly Spot

Landfill

Lava Flow

Marsh or swamp

Mine or Quarry

Miscellaneous Water

Perennial Water

Rock Outcrop

Saline Spot
Sandy Spot

Severely Eroded Spot

Sinkhole

Slide or Slip

Sodic Spot

#### CLIND

Spoil Area

Stony Spot

Very Stony Spot

Wet Spot

△ Other

Special Line Features

#### Water Features

Streams and Canals

#### Transportation

Rails

Interstate Highways

US Routes

Major Roads

Local Roads

#### Background

Aerial Photography

#### MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24.000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service Web Soil Survey URL:

Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: El Paso County Area, Colorado Survey Area Data: Version 15, Oct 10, 2017

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Jun 3, 2014—Jun 17, 2014

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

# **Map Unit Legend**

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
8	Blakeland loamy sand, 1 to 9 percent slopes	35.2	95.4%
10	Blendon sandy loam, 0 to 3 percent slopes	1.7	4.6%
Totals for Area of Interest		36.9	100.0%

FIRM PANELS

## NOTES TO USERS

This map is for use in administering the National Flood Insurance Program. It does not necessarily identify all areas subject to flooding, particularly from local drainage sources of small size. The community map repository should be consulted for possible updated or additional flood hazard information.

To obtain more detailed information in areas where Base Flood Elevations (BFEs) and/or floodways have been determined, users are encouraged to consult the Flood Profiles and Floodway Data and/or Summary of Stillwater Elevations tables contained within the Flood Insurance Study (FIS) report that accompanies this FIRM. Users should be aware that BFEs shown on the FIRM represent rounded whole-foot elevations. These BFEs are intended for flood insurance rating purposes only and should not be used as the sole source of flood elevation information. Accordingly, flood elevation data presented in the FIS report should be utilized in conjunction with the FIRM for purposes of construction and/or floodplain management.

Coastal Base Flood Elevations shown on this map apply only landward of 0.0' North American Vertical Datum of 1988 (NAVD88). Users of this FIRM should be aware that coastal flood elevations are also provided in the Summary of Stillwater Elevations table in the Flood Insurance Study report for this jurisdiction. Elevations shown in the Summary of Stillwater Elevations table should be used for construction and/or floodplain management purposes when they are higher than the elevations shown on this FIRM.

Boundaries of the floodways were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations with regard to requirements of the National Flood Insurance Program. Floodway widths and other pertinent floodway data are provided in the Flood Insurance Study report for this jurisdiction.

Certain areas not in Special Flood Hazard Areas may be protected by flood control structures. Refer to section 2.4 "Flood Protection Measures" of the Flood Insurance Study report for information on flood control structures for this jurisdiction.

The projection used in the preparation of this map was Universal Transverse Mercator (UTM) zone 13. The horizontal datum was NAD83, GRS80 spheroid. Differences in datum, spheroid, projection or UTM zones zones used in the production of FIRMs for adjacent jurisdictions may result in slight positional differences in map features across jurisdiction boundaries. These differences do not affect the accuracy of this FIRM.

Flood elevations on this map are referenced to the North American Vertical Datum of 1988 (NAVD88). These flood elevations must be compared to structure and ground elevations referenced to the same **vertical datum**. For information regarding conversion between the National Geodetic Vertical Datum of 1929 and the North American Vertical Datum of 1988, visit the National Geodetic Survey website a http://www.ngs.noaa.gov/ or contact the National Geodetic Survey at the following

NGS Information Services NOAA, N/NGS12 National Geodetic Survey SSMC-3, #9202 1315 East-West Highway Silver Spring, MD 20910-3282

To obtain current elevation, description, and/or location information for bench marks shown on this map, please contact the Information Services Branch of the National Geodetic Survey at (301) 713-3242 or visit its website at http://www.ngs.noaa.gov/.

Base Map information shown on this FIRM was provided in digital format by El Paso County, Colorado Springs Utilities, City of Fountain, Bureau of Land Management, National Oceanic and Atmospheric Administration, United States Geological Survey, and Anderson Consulting Engineers, Inc. These data are current as of 2006.

This map reflects more detailed and up-to-date stream channel configurations and **loodplain delineations** than those shown on the previous FIRM for this jurisdiction. The floodplains and floodways that were transferred from the previous FIRM may have been adjusted to conform to these new stream channel configurations. As a result, the Flood Profiles and Floodway Data tables in the Flood Insurance Study Report (which contains authoritative hydraulic data) may reflect stream channe distances that differ from what is shown on this map. The profile baselines depicted on this map represent the hydraulic modeling baselines that match the flood profiles and Floodway Data Tables if applicable, in the FIS report. As a result, the profile paselines may deviate significantly from the new base map channel representation and may appear outside of the floodplain.

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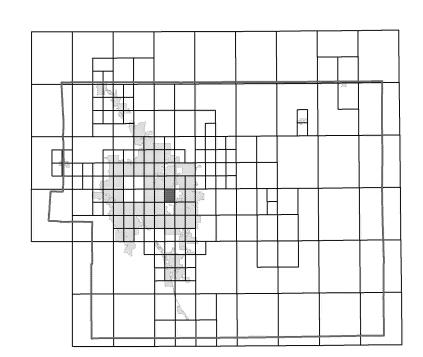
Please refer to the separately printed Map Index for an overview map of the county showing the layout of map panels; community map repository addresses; and a Listing of Communities table containing National Flood Insurance Program dates for each community as well as a listing of the panels on which each community is

Contact FEMA Map Service Center (MSC) via the FEMA Map Information eXchange (FMIX) 1-877-336-2627 for information on available products associated with this FIRM. Available products may include previously issued Letters of Map Change, a Flood Insurance Study Report, and/or digital versions of this map. The MSC may also be reached by Fax at 1-800-358-9620 and its website a http://www.msc.fema.gov/.

f you have questions about this map or questions concerning the National Flood Insurance Program in general, please call 1-877-FEMA MAP (1-877-336-2627) or visit the FEMA website at http://www.fema.gov/business/nfip.

El Paso County Vertical Datum Offset Table **Vertical Datum** Flooding Source REFER TO SECTION 3.3 OF THE EL PASO COUNTY FLOOD INSURANCE STUDY FOR STREAM BY STREAM VERTICAL DATUM CONVERSION INFORMATION

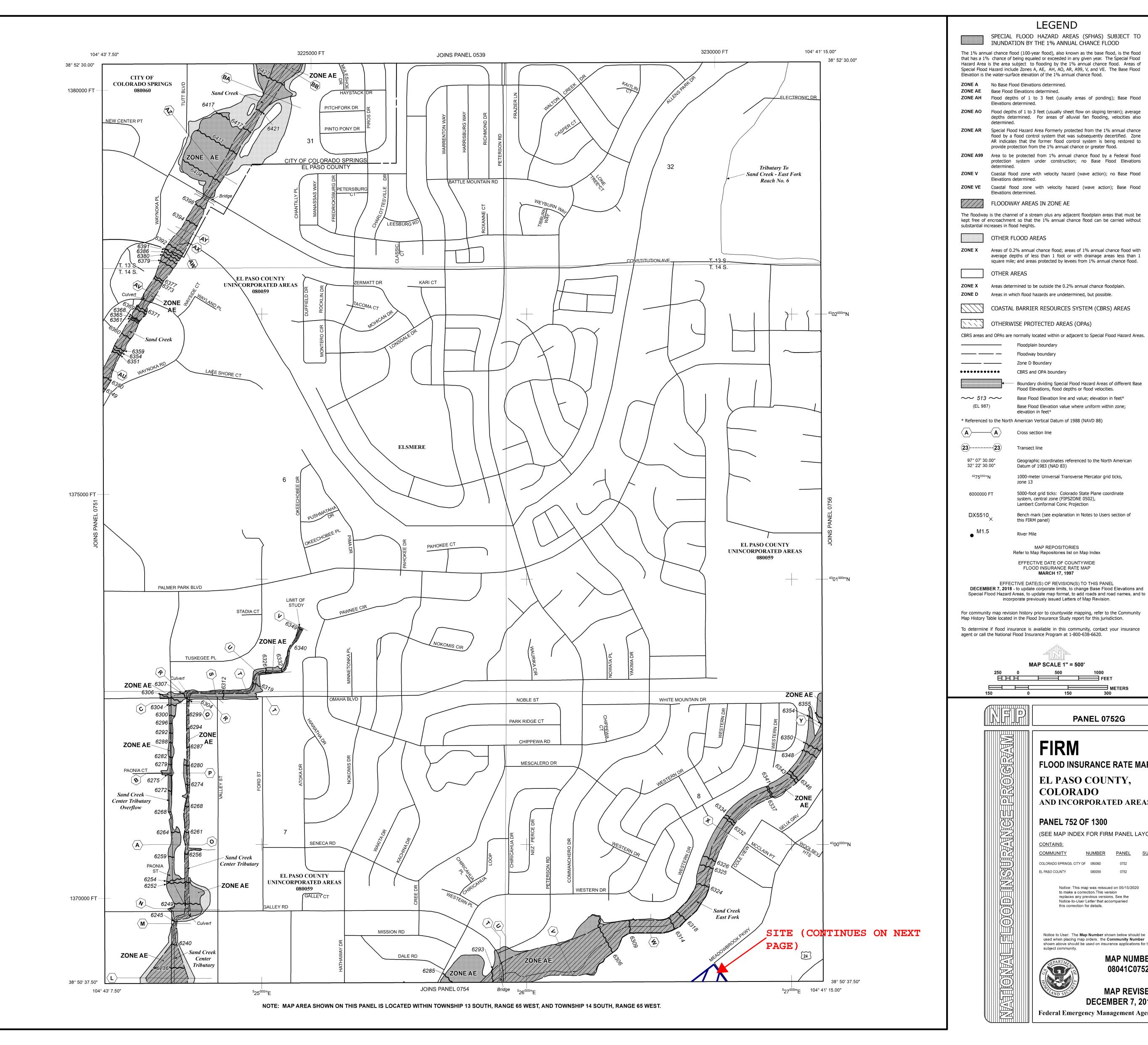
# Panel Location Map



This Digital Flood Insurance Rate Map (DFIRM) was produced through a Cooperating Technical Partner (CTP) agreement between the State of Colorado Water Conservation Board (CWCB) and the Federal Emergency Management Agency (FEMA).



Additional Flood Hazard information and resources are available from local communities and the Colorado Water Conservation Board.



**LEGEND** 

Floodway boundary

Zone D Boundary

elevation in feet\*

Cross section line

this FIRM panel)

Datum of 1983 (NAD 83)

CBRS and OPA boundary

Boundary dividing Special Flood Hazard Areas of different Base

lood Elevations, flood depths or flood velocities.

Base Flood Elevation line and value; elevation in feet\*

Base Flood Elevation value where uniform within zone;

Geographic coordinates referenced to the North American

1000-meter Universal Transverse Mercator grid ticks,

5000-foot grid ticks: Colorado State Plane coordinate

Bench mark (see explanation in Notes to Users section of

system, central zone (FIPSZONE 0502).

MAP REPOSITORIES

Refer to Map Repositories list on Map Index

EFFECTIVE DATE OF COUNTYWIDE FLOOD INSURANCE RATE MAP

MARCH 17, 1997

EFFECTIVE DATE(S) OF REVISION(S) TO THIS PANEL

incorporate previously issued Letters of Map Revision.

**FIRM** 

EL PASO COUNTY

**COLORADO** 

PANEL 752 OF 1300

**PANEL 0752G** 

FLOOD INSURANCE RATE MAP

AND INCORPORATED AREAS

(SEE MAP INDEX FOR FIRM PANEL LAYOUT)

Notice: This map was reissued on 05/15/2020 to make a correction. This version

replaces any previous versions. See the

Notice to User: The Map Number shown below should be used when placing map orders: the Community Number shown above should be used on insurance applications for the

Federal Emergency Management Agency

MAP NUMBER

**MAP REVISED** 

**DECEMBER 7, 2018** 

08041C0752G

Notice-to-User Letter that accompanied this correction for details.

**EL PASO COUNTY,** 

## NOTES TO USERS

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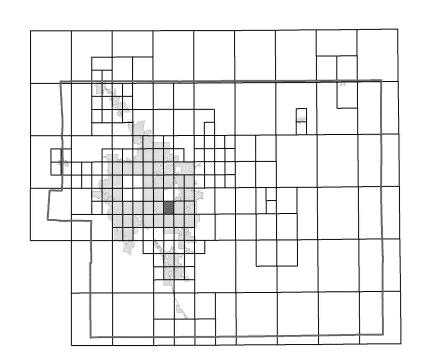
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## El Paso County Vertical Datum Offset Table Vertical Datum

REFER TO SECTION 3.3 OF THE EL PASO COUNTY FLOOD INSURANCE STUDY FOR STREAM BY STREAM VERTICAL DATUM CONVERSION INFORMATION

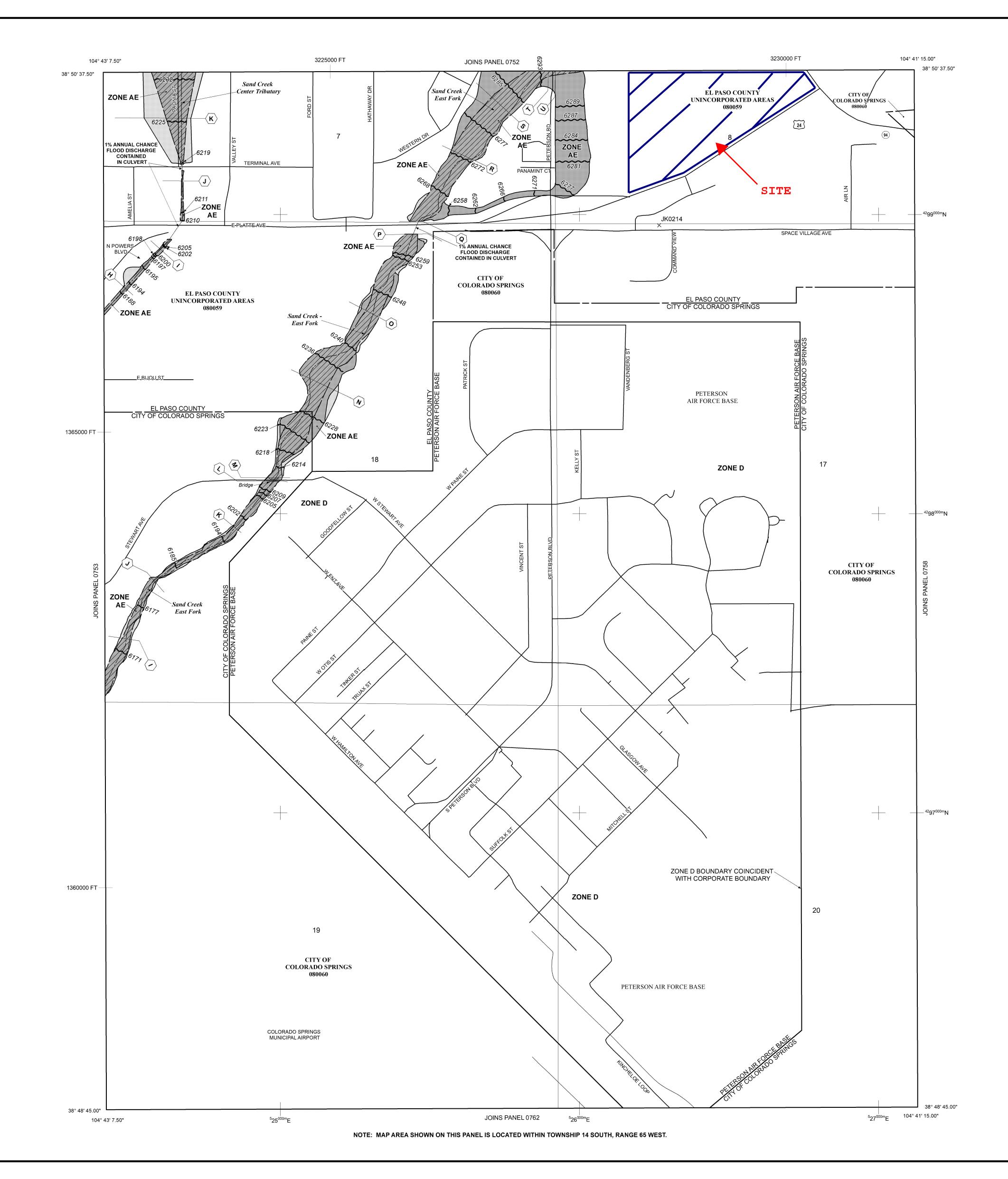
# Panel Location Map



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Additional Flood Hazard information and resources are available from local communities and the Colorado Water Conservation Board.



## **LEGEND**

SPECIAL FLOOD HAZARD AREAS (SFHAS) SUBJECT TO INUNDATION BY THE 1% ANNUAL CHANCE FLOOD

The 1% annual chance flood (100-year flood), also known as the base flood, is the flood that has a 1% chance of being equaled or exceeded in any given year. The Special Flood Hazard Area is the area subject to flooding by the 1% annual chance flood. Areas of Special Flood Hazard include Zones A, AE, AH, AO, AR, A99, V, and VE. The Base Flood Elevation is the water-surface elevation of the 1% annual chance flood.

**ZONE A** No Base Flood Elevations determined. Base Flood Elevations determined.

Flood depths of 1 to 3 feet (usually areas of ponding); Base Flood Elevations determined

Flood depths of 1 to 3 feet (usually sheet flow on sloping terrain); average depths determined. For areas of alluvial fan flooding, velocities also

**ZONE AR** Special Flood Hazard Area Formerly protected from the 1% annual chance flood by a flood control system that was subsequently decertified. Zone AR indicates that the former flood control system is being restored to provide protection from the 1% annual chance or greater flood.

**ZONE A99** Area to be protected from 1% annual chance flood by a Federal flood protection system under construction; no Base Flood Elevations

Coastal flood zone with velocity hazard (wave action); no Base Flood Elevations determined

ZONE VE Coastal flood zone with velocity hazard (wave action); Base Flood

Elevations determined. FLOODWAY AREAS IN ZONE AE

The floodway is the channel of a stream plus any adjacent floodplain areas that must be kept free of encroachment so that the 1% annual chance flood can be carried without substantial increases in flood heights.

OTHER FLOOD AREAS

Areas of 0.2% annual chance flood; areas of 1% annual chance flood with average depths of less than 1 foot or with drainage areas less than 1 square mile; and areas protected by levees from 1% annual chance flood.

OTHER AREAS Areas determined to be outside the 0.2% annual chance floodplain.

Areas in which flood hazards are undetermined, but possible.

COASTAL BARRIER RESOURCES SYSTEM (CBRS) AREAS

CBRS areas and OPAs are normally located within or adjacent to Special Flood Hazard Areas.

OTHERWISE PROTECTED AREAS (OPAs)

Floodway boundary

Zone D Boundary \*\*\*\*\*\*\*\*\*\* CBRS and OPA boundary

> Boundary dividing Special Flood Hazard Areas of different Base Flood Elevations, flood depths or flood velocities. Base Flood Elevation line and value; elevation in feet\* Base Flood Elevation value where uniform within zone; (EL 987)

elevation in feet\* \* Referenced to the North American Vertical Datum of 1988 (NAVD 88)

Cross section line

6000000 FT

97° 07' 30.00" Geographic coordinates referenced to the North American 32° 22' 30.00" Datum of 1983 (NAD 83)

1000-meter Universal Transverse Mercator grid ticks, 5000-foot grid ticks: Colorado State Plane coordinate

system, central zone (FIPSZONE 0502), DX5510 Bench mark (see explanation in Notes to Users section of

this FIRM panel)

MAP REPOSITORIES Refer to Map Repositories list on Map Index EFFECTIVE DATE OF COUNTYWIDE

FLOOD INSURANCE RATE MAP MARCH 17, 1997 EFFECTIVE DATE(S) OF REVISION(S) TO THIS PANEL DECEMBER 7, 2018 - to update corporate limits, to change Base Flood Elevations and

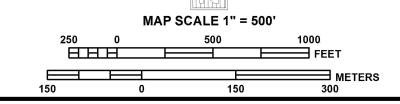
Special Flood Hazard Areas, to update map format, to add roads and road names, and to

incorporate previously issued Letters of Map Revision.

For community map revision history prior to countywide mapping, refer to the Community

Map History Table located in the Flood Insurance Study report for this jurisdiction. To determine if flood insurance is available in this community, contact your insurance

agent or call the National Flood Insurance Program at 1-800-638-6620.





**FIRM** FLOOD INSURANCE RATE MAP **EL PASO COUNTY,** 

COLORADO

EL PASO COUNTY

**PANEL 754 OF 1300** (SEE MAP INDEX FOR FIRM PANEL LAYOUT)

AND INCORPORATED AREAS

080059

Notice: This map was reissued on 05/15/2020 to make a correction. This version replaces any previous versions. See the

this correction for details.

Notice to User: The Map Number shown below should be used when placing map orders: the Community Number

shown above should be used on insurance applications for the

Notice-to-User Letter that accompanied



**MAP REVISED DECEMBER 7, 2018** 

Federal Emergency Management Agency

HYDROLOGIC CALCULATIONS

# Crossroads Mixed Use PRELIMINARY DRAINAGE REPORT (Historic Area Runoff Coefficient Summary)

			STREE	TS / DEVE	ELOPED	OVERI	LAND / DEVI	ELOPED	WEIGHTED			
BASIN	TOTAL AREA (SF)	TOTAL AREA (Acres)	AREA (Acres)	C <sub>5</sub>	C <sub>100</sub>	AREA (Acres)	C <sub>5</sub>	C <sub>100</sub>	C <sub>5</sub>	C <sub>100</sub>		
C	256383.3	5.89	0.00	0.90	0.96	5.89	0.08	0.35	0.08	0.35		
A	561176.6	12.88	0.00	0.90	0.96	12.88	0.08	0.35	0.08	0.35		
В	593693.4	13.63	0.00	0.90	0.96	13.63	0.08	0.35	0.08	0.35		
OS-1	55560.16	1.28	1.28	0.90	0.96	0.00	0.08	0.35	0.90	0.96		
OS-2	216993.7	4.98	2.49	0.90	0.96	2.49	0.08	0.35	0.49	0.66		
EX-A2***		0.59	0.59	0.90	0.96	0.00	0.08	0.35	0.90	0.96		
OS-A**		1.29	1.29	0.62	0.72	0.00	0.08	0.35	0.62	0.72		
E2*		3.86	3.86	0.80	0.90	0.00	0.08	0.35	0.80	0.90		

<sup>\*</sup>FROM FDR FOR CLAREMONT BUSINESS PARK FILING NO. 2

<sup>\*\*</sup>FROM FDR FOR MEADOWBROOK CROSSING FILING 1 AND FILING 2

<sup>\*\*\*</sup>FROM FOR FOR LOT 1 24/94 BUSINESS PARK FILING NO. 1 ON PLATTE AVENUE AND MEADOWBROOK PARKWAY

# Crossroads Mixed Use PRELIMINARY DRAINAGE REPORT

# (Historic Area Drainage Summary)

Fron	n Area Runoff Cod	efficient Summar	y		OVERLA.	1ND		ST	REET / CH	ANNEL FLO	)W	Time of Trave	$l(T_t)$	INTEN	SITY ^	TOTAL FLOWS	
BASIN	AREA TOTAL	C <sub>5</sub>	C <sub>100</sub>	C <sub>5</sub>	Length	Height	$T_{C}$	Length	Slope	Velocity	T <sub>t</sub>	TOTAL	СНЕСК	I <sub>5</sub>	I <sub>100</sub>	$Q_5$	Q <sub>100</sub>
	(Acres)	From DCM	M Table 5-1		(ft)	(ft)	(min)	(ft)	(%)	(fps)	(min)	(min)	(min)	(in/hr)	(in/hr)	(c.f.s.)	(c.f.s.)
С	5.89	0.08	0.35	0.08	300	9	22.2	500	2.0%	1.0	8.4	30.6	14.4	2.5	4.1	1.2	8.5
A	12.88	0.08	0.35	0.08	300	13	19.7	1350	1.6%	0.9	25.2	44.8	19.2	1.9	3.2	1.9	14.2
В	13.63	0.08	0.35	0.08	300	11	20.8	750	1.7%	0.9	13.7	34.5	15.8	2.3	3.8	2.5	18.2
OS-1	1.28	0.90	0.96	0.90	100	3	2.5	490	2.2%	3.0	2.8	5.3	13.3	5.1	8.5	5.8	10.5
OS-2	4.98	0.49	0.66	0.49	85	8	4.8	1165	1.8%	2.0	9.6	14.5	16.9	3.6	6.0	8.7	19.6
EX-A2***	0.59	0.90	0.96	0.90	10	0.2	0.9	916	1.9%	2.7	5.6	6.5	15.1	4.8	8.0	2.5	4.5
OS-A**	1.29	0.62	0.72	0.62	40	0.8	4.4	1310	1.9%	2.8	7.9	12.3	17.5	3.8	6.4	3.1	6.0
E2*	3.86	0.80	0.90	0.80	50	1	3.0	400	1.3%	2.3	2.9	6.0	12.5	4.9	8.2	15.1	28.6

<sup>^</sup> Intensity equations assume a minimum travel time of 5 minutes.

Calculated by: CVW

Date: 2/23/2021
Checked by: DLM

<sup>\*</sup>VALUES DERIVED USING DATA FROM FDR FOR CLAREMONT BUSINESS PARK FILING NO. 2

<sup>\*\*</sup>VALUES DERIVED USING DATA FROM FDR FOR MEADOWBROOK CROSSING FILING 1 AND FILING 2 PAGE 31

<sup>\*\*\*</sup>VALUES DERIVED USING DATA FROM FDR FOR LOT 1 24/94 BUSINESS PARK FILING NO. 1 ON PLATTE AVENUE AND MEADOWBROOK PARKWAY

# Crossroads Mixed Use PRELIMINARY DRAINAGE REPORT (Historic Basin Routing Summary)

	From Area Runoff Coefficient Summary	,			OVE	ERLAND		PIPI	E / CHA	NNEL FLO	)W	Time of Travel $(T_t)$	INTE	SITY *	TOTAL	FLOWS	
DESIGN POINT	CONTRIBUTING BASINS	CA <sub>5</sub>	CA <sub>100</sub>	C <sub>5</sub>	Length	Height	T <sub>C</sub>	Length	Slope	Velocity	T <sub>t</sub>	TOTAL	$I_5$	I <sub>100</sub>	$Q_5$	$Q_{100}$	COMMENTS
			•		(ft)	(ft)	(min)	(ft)	(%)	(fps)	(min)	(min)	(in/hr)	(in/hr)	(c.f.s.)	(c.f.s.)	
1	E2	3.09	3.47				6.0	916	1.9%	2.7	5.6	11.6	3.9	6.6	14.2	26.5	
	EX-A2	0.53	0.57									1					
																	EXISTING 10' CDOT TYPE R AT
		3.62	4.04		Tc fo	or E2 Used											GRADE INLET
2	OS-A	0.80	0.93									12.3	3.8	6.4	3.1	6.0	
																	EXISTING 10' CDOT TYPE R AT
				Se	e Area Drai	nage Sheet t	or Input										GRADE INLET
3	OS-1	1.15	1.22				11.6	150	1.0%	2.0	1.3	12.8	3.8	6.3	9.8	22.5	
	FB-DP1	1.47	2.35														
		2.62	3.57		Te fo	r DP1 Used											END OF PAVEMENT
4	A	1.03	4.51				12.8	1470	1.6%	0.9	28.0	40.8	2.0	3.4	7.4	27.7	
	FB-INDP5	0.00	0.10														
	DP3	2.62	3.57														
		3.65	8.19		Tc for	r DP3 Used											ADJACENT PARCEL (LOT 1)
5	В	1.09	4.77									34.5	2.3	3.8	8.3	18.2	
				Se	e Area Drai	nage Sheet t	or Input										ADJACENT PARCEL (LOT 2)
6	C	0.47	2.06									30.6	2.5	4.1	1.2	8.5	
				Se	e Area Drai	nage Sheet t	or Input										DISCHARGE TO CDOT ROW
7	OS2	2.44	3.26									14.5	3.6	6.0	10.4	31.9	
	DP6	0.47	2.06					]									BARROW DITCH
		2.91	5.32		Tc for	r OS2 Used											SW CORNER OF SITE/CDOT ROW

Calculated by: CVW

Date: 2/23/2021

Checked by: DLM

# Crossroads Mixed Use PRELIMINARY DRAINAGE REPORT (Existing Area Runoff Coefficient Summary)

			STREE	TS / DEVE	ELOPED	OVERI	LAND / DEVI	ELOPED	WEIGHTED			
BASIN	TOTAL AREA (SF)	TOTAL AREA (Acres)	AREA (Acres)	C <sub>5</sub>	C <sub>100</sub>	AREA (Acres)	C <sub>5</sub>	C <sub>100</sub>	C <sub>5</sub>	C <sub>100</sub>		
C	173960	3.99	0.00	0.90	0.96	5.89	0.08	0.35	0.08	0.35		
A	480166.8	11.02	0.00	0.90	0.96	11.02	0.08	0.35	0.08	0.35		
В	754121.6	17.31	0.00	0.90	0.96	17.31	0.08	0.35	0.08	0.35		
OS-1	55560.16	1.28	1.28	0.90	0.96	0.00	0.08	0.35	0.90	0.96		
OS-2	216993.7	4.98	2.49	0.90	0.96	2.49	0.08	0.35	0.49	0.66		
EX-A2***		0.59	0.59	0.90	0.96	0.00	0.08	0.35	0.90	0.96		
OS-A**		1.29	1.29	0.62	0.72	0.00	0.08	0.35	0.62	0.72		
E2*		3.86	3.86	0.80	0.90	0.00	0.08	0.35	0.80	0.90		

<sup>\*</sup>FROM FDR FOR CLAREMONT BUSINESS PARK FILING NO. 2

<sup>\*\*</sup>FROM TO FDR MEADOWBROOK CROSSING FILING 1 AND FILING 2

<sup>\*\*\*</sup>FROM FDR LOT 1 24/94 BUSINESS PARK FILING NO. 1 ON PLATTE AVENUE AND MEADOWBROOK PARKWAY

# Crossroads Mixed Use PRELIMINARY DRAINAGE REPORT

# (Existing Area Drainage Summary)

Fron	n Area Runoff Co	efficient Summar	y		<b>OVERL</b> A	IND		ST	REET / CH	ANNEL FLO	)W	Time of Trave	$l(T_t)$	INTEN	SITY ^	TOTAL FLOWS	
BASIN	AREA TOTAL	C <sub>5</sub>	C <sub>100</sub>	C <sub>5</sub>	Length	Height	$T_{\rm C}$	Length	Slope	Velocity	T <sub>t</sub>	TOTAL	СНЕСК	I <sub>5</sub>	I <sub>100</sub>	$Q_5$	$Q_{100}$
	(Acres)	From DCM	1 Table 5-1		(ft)	(ft)	(min)	(ft)	(%)	(fps)	(min)	(min)	(min)	(in/hr)	(in/hr)	(c.f.s.)	(c.f.s.)
С	3.99	0.08	0.35	0.08	120	2.8	15.3	555	1.5%	0.9	10.6	25.9	13.8	2.7	4.5	0.9	6.3
A	11.02	0.08	0.35	0.08	165	8	13.8	1730	1.3%	0.8	36.3	50.1	20.5	1.7	2.9	1.5	11.1
В	17.31	0.08	0.35	0.08	300	3	30.9	1390	1.2%	0.8	29.7	60.6	19.4	1.4	2.4	2.0	14.5
OS-1	1.28	0.90	0.96	0.90	100	3	2.5	490	2.2%	3.0	2.8	5.3	13.3	5.1	8.5	5.8	10.5
OS-2	4.98	0.49	0.66	0.49	85	8	4.8	1165	1.8%	2.0	9.6	14.5	16.9	3.6	6.0	8.7	19.6
EX-A2***	0.59	0.90	0.96	0.90	10	0.2	0.9	916	1.9%	2.7	5.6	6.5	15.1	4.8	8.0	2.5	4.5
OS-A**	1.29	0.62	0.72	0.62	40	0.8	4.4	1310	1.9%	2.8	7.9	12.3	17.5	3.8	6.4	3.1	6.0
E2*	3.86	0.80	0.90	0.80	50	1	3.0	400	1.3%	2.3	2.9	6.0	12.5	4.9	8.2	15.1	28.6

<sup>^</sup> Intensity equations assume a minimum travel time of 5 minutes.

Calculated by: CVW

Date: 2/23/2021

Checked by: DLM

<sup>\*</sup>VALUES DERIVED USING DATA FROM FDR FOR <u>CLAREMONT BUSINESS PARK FILING NO. 2</u>

<sup>\*\*</sup>VALUES DERIVED USING DATA FROM <u>FDR FOR MEADOWBROOK CROSSING FILING 1 AND FILING 2 PAGE 31</u>

<sup>\*\*\*</sup>VALUES DERIVED USING DATA FROM FDR FOR LOT 1 24/94 BUSINESS PARK FILING NO. 1 ON PLATTE AVENUE AND MEADOWBROOK PARKWAY

# Crossroads Mixed Use PRELIMINARY DRAINAGE REPORT (Existing Basin Routing Summary)

	From Area Runoff Coefficient Summary	,			OVE	ERLAND		PIPI	C / CHA	NNEL FLO	)W	Time of Travel $(T_t)$	INTE	SITY *	TOTAL	FLOWS	
DESIGN POINT	CONTRIBUTING BASINS	CA <sub>5</sub>	CA <sub>100</sub>	C <sub>5</sub>	Length	Height	$T_{C}$	Length	Slope	Velocity	$T_t$	TOTAL	$I_5$	I <sub>100</sub>	$Q_5$	$Q_{100}$	COMMENTS
					(ft)	(ft)	(min)	(ft)	(%)	(fps)	(min)	(min)	(in/hr)	(in/hr)	(c.f.s.)	(c.f.s.)	
1	E2	3.09	3.47				6.0	916	1.9%	2.7	5.6	11.6	3.9	6.6	14.2	26.5	
	EX-A2	0.53	0.57									1					
																	EXISTING 10' CDOT TYPE R AT
		3.62	4.04		Te fe	or E2 Used											GRADE INLET
2	OS-A	0.80	0.93									12.3	3.8	6.4	3.1	6.0	
																	EXISTING 10' CDOT TYPE R AT
				Se	e Area Drai	nage Sheet t	or Input										GRADE INLET
3	OS-1	1.15	1.22				11.6	150	1.0%	2.0	1.3	12.8	3.8	6.3	9.8	22.5	
	FB-DP1	1.47	2.35									1					
		2.62	3.57		Tc for	r DP1 Used											END OF PAVEMENT
4	A	0.88	3.86				12.8	1470	1.6%	0.9	28.0	40.8	2.0	3.4	7.1	25.5	
	FB-DP2	0.00	0.10														
	DP3	2.62	3.57														
		3.50	7.54		Tc for	r DP3 Used											ADJACENT PARCEL (LOT 1)
5	В	1.38	6.06									60.6	1.4	2.4	5.0	14.5	
				Se	e Area Drai	nage Sheet t	or Input										ADJACENT PARCEL (LOT 2)
6	C	0.32	1.40									25.9	2.7	4.5	0.9	6.3	
				Se	e Area Drai	nage Sheet t	or Input										DISCHARGE TO CDOT ROW
7	OS2	2.44	3.26									14.5	3.6	6.0	9.9	28.0	
	DP6	0.32	1.40														BARROW DITCH
		2.76	4.66		Tc fo	r OS2 Used											SW CORNER OF SITE/CDOT ROW

Calculated by: CVW

Date: #######

Checked by: DLM

# CROSSROADS MIXED USE PRELIMINARY DRAINAGE CALCULATIONS

# (Area Runoff Coefficient Summary)

			STREE	TS / COM	MERC.	MULTI-F2	AMILY/PA	RKLAND	<b>OVERL</b> AN	D / UNDE	WEIGHTED		
BASIN	TOTAL AREA (Sq Ft)	TOTAL AREA (Acres)	AREA (Acres)	C <sub>5</sub>	C <sub>100</sub>	AREA (Acres)	C <sub>5</sub>	C <sub>100</sub>	AREA (Acres)	C <sub>5</sub>	C <sub>100</sub>	C <sub>5</sub>	C <sub>100</sub>
					PROPOS	ED BASINS							
OS-A**		1.29	1.29	0.62	0.72	0.00	0.49	0.62	0.00	0.08	0.35	0.62	0.72
E2*		3.86	3.86	0.80	0.90	0.00	0.49	0.62	0.00	0.08	0.35	0.80	0.90
EX-A2***		0.59	0.59	0.90	0.96	0.00	0.49	0.62	0.00	0.08	0.35	0.90	0.96
OS-1	60793.3017	1.40	1.40	0.90	0.96	0.00	0.49	0.62	0.00	0.08	0.35	0.90	0.96
OS-2	216993.7096	4.98	2.49	0.90	0.96	0.00	0.49	0.62	2.49	0.08	0.35	0.49	0.66
A	72967.0787	1.68	1.68	0.90	0.96	0.00	0.49	0.62	0.00	0.08	0.35	0.90	0.96
В	65021.9778	1.49	1.49	0.90	0.96	0.00	0.49	0.62	0.00	0.08	0.35	0.90	0.96
С	200631.5748	4.61	4.46	0.81	0.88	0.00	0.49	0.62	0.15	0.08	0.35	0.79	0.86
D	96773.7602	2.22	2.22	0.81	0.88	0.00	0.49	0.62	0.00	0.08	0.35	0.81	0.88
E	118133.5827	2.71	0.48	0.90	0.96	2.23	0.81	0.88	0.00	0.08	0.35	0.83	0.89
F	112036.6061	2.57	2.57	0.81	0.88	0.00	0.49	0.62	0.00	0.08	0.35	0.81	0.88
G	40937.4999	0.94	0.94	0.90	0.96	0.00	0.49	0.62	0.00	0.08	0.35	0.90	0.96
Н	482081.5171	11.07	0.00	0.90	0.96	11.07	0.54	0.66	0.00	0.08	0.35	0.54	0.66
I	69600.2016	1.60	0.00	0.90	0.96	1.60	0.54	0.66	0.00	0.08	0.35	0.54	0.66
J	139924.2472	3.21	0.00	0.90	0.96	3.21	0.16	0.41	0.00	0.08	0.35	0.16	0.41

# CROSSROADS MIXED USE PRELIMINARY DRAINAGE REPORT

# (Area Drainage Summary)

From Area Rui	From Area Runoff Coefficient Summary				OVERLAND			STREET / CHANNEL FLOW			Time of Travel $(T_t)$		INTENSITY#		TOTAL FLOWS		
BASIN	AREA TOTAL	C <sub>5</sub>	C <sub>100</sub>	C <sub>5</sub>	Length	Height	$T_{C}$	Length	Slope	Velocity	T <sub>t</sub>	TOTAL	CHECK	I <sub>5</sub>	I <sub>100</sub>	$Q_5$	Q <sub>100</sub>
	(Acres)	From DCM	1 Table 5-1		(ft)	(ft)	(min)	(ft)	(%)	(fps)	(min)	(min)	(min)	(in/hr)	(in/hr)	(c.f.s.)	(c.f.s.)
	Proposed Area Drainage Summary																
<i>OS-A**</i>	1.29	0.62	0.72	0.62	40	0.8	4.4	1310	1.9%	2.8	7.9	12.3	17.5	3.8	6.4	3.1	6.0
E2*	3.86	0.80	0.90	0.80	50	1	3.0	400	1.3%	2.3	2.9	6.0	12.5	4.9	8.2	15.1	28.6
EX-A2***	0.59	0.90	0.96	0.90	10	0.2	0.9	916	1.9%	2.7	5.6	6.5	15.1	4.8	8.0	2.5	4.5
OS-1	1.40	0.90	0.96	0.90	100	3	2.5	490	2.2%	3.0	2.7	5.2	13.3	5.1	8.6	6.4	11.5
OS-2	4.98	0.49	0.66	0.49	85	8	4.8	1165	1.8%	2.0	9.6	14.5	16.9	3.6	6.0	<b>8.</b> 7	19.6
A	1.68	0.90	0.96	0.90	30	0.6	1.6	1325	0.7%	1.7	7.3	8.9	17.5	4.3	7.2	6.5	11.6
В	1.49	0.90	0.96	0.90	25	0.5	1.4	1335	0.7%	1.7	7.3	8.8	17.6	4.3	7.3	5.8	10.4
C	4.61	0.79	0.86	0.79	50	1	3.2	260	1.5%	2.4	1.4	5.0	11.7	5.2	8.7	18.7	34.5
D	2.22	0.81	0.88	0.81	50	1	2.9	200	1.5%	2.4	1.1	5.0	11.4	5.2	8.7	9.3	17.0
E	2.71	0.83	0.89	0.83	60	1.2	3.0	700	1.0%	2.0	3.8	6.9	14.2	4.7	7.9	10.5	19.1
F	2.57	0.81	0.88	0.81	50	0.8	3.2	300	1.3%	2.3	1.6	5.0	11.9	5.2	8.7	10.8	19.6
G	0.94	0.90	0.96	0.90	50	1	2.0	500	1.0%	2.0	2.7	5.0	13.1	5.2	8.7	4.4	7.8
Н	11.07	0.54	0.66	0.54	50	1	5.7	500	1.5%	2.4	2.7	8.4	13.1	4.4	7.4	26.2	53.8
I	1.60	0.54	0.66	0.54	50	1	5.7	500	1.5%	2.4	2.7	8.4	13.1	4.4	7.4	3.8	7.8
J	3.21	0.16	0.41	0.16	50	2	7.6	0	0.0%	0.0	0.0	7.6	10.3	4.5	7.6	2.3	10.0

<sup>#</sup> Intensity equations assume a minimum travel time of 5 minutes.

Calculated by: DLM

Date: 2/21/2021 Checked by: VAS

<sup>\*</sup>VALUES DERIVED USING DATA FROM  $\underline{\mathsf{FDR}}$  FOR CLAREMONT BUSINESS PARK FILING NO. 2

<sup>\*\*</sup>VALUES DERIVED USING DATA FROM  $\underline{FDR}$  MEADOWBROOK CROSSING FILING 1 AND FILING 2 PAGE 31

<sup>\*\*\*</sup>VALUES DERIVED USING DATA FROM FDR LOT 1 24/94 BUSINESS PARK FILING NO. 1 ON PLATTE AVENUE AND MEADOWBROOK PARKWAY

# CROSSROADS MIXED USE PRELIMINARY DRAINAGE REPORT (Basin Routing Summary)

	From Area Runoff Coefficient Summar			1		RLAND				NNEL FLO		Time of Travel (T <sub>1</sub> )	INTEN	VSITY *	TOTAL	FLOWS	1
DESIGN POINT	CONTRIBUTING BASINS	CA <sub>5</sub>	CA <sub>100</sub>	C <sub>5</sub>	Length	Height	T <sub>C</sub>	Length	Slope	Velocity	T <sub>t</sub>	TOTAL	INTER I <sub>5</sub>	I <sub>100</sub>	Q <sub>5</sub>	Q <sub>100</sub>	COMMENTS
DESIGNTOIN	CONTRIBUTING BASINS	CA5	CA100	C5	(ft)	(ft)	(min)	(ft)	(%)	(fps)	(min)	(min)	(in/hr)		(c.f.s.)	(c.f.s.)	COMMENTS
1				PRO						ING SUN			/	(	(-99	(-37	
1	E2, EX-A2	3.62	4.04				6.0	916	1.9%	2.7	5.6	11.6	3.9	6.6	14.2	26.5	Existing 10' CDOT Type R At-Grade Inlet
																	(Public)
_					Tc for	E2 Used											
2	OS-A	0.80	0.93									12.3	3.8	6.4	3.1	6.0	Existing 10' CDOT Type R At-Grade Inlet (Public)
				See	Area Draina	ige Sheet fo	r Input										(Public)
3	OS-1, FB-DP1	2.73	3.69				11.6	150	1.0%	2.0	1.3	12.8	3.8	6.3	10.2	23.3	Proposed 10' CDOT Type R At-Grade Inlet
																	(Public)
	. En no				Tc for I	DP1 Used										10.1	
4	A, FB-DP2	1.51	1.71 3.57									8.9	4.3	7.2	6.5	19.1	Proposed 10' CDOT Type R Sump Inlet (Public)
	(100 YR SPLIT FLOWS)		2.64		Tc for Ba	asin A used											(rubile)
5	B, FB-DP3	2.29	3.57									8.9	4.3	7.2	9.9	19.1	Proposed 10' CDOT Type R Sump Inlet
			1.71														(Public)
	(100YR SPLIT FLOWS)		2.64		Tc for Ba	sin A Used								0.5	10.7	24.5	
6	С	3.62	3.98									5.0	5.2	8.7	18.7	34.5	Proposed 30" RCP or PP Storm Sewer (Private)
				See .	Area Draina	ige Sheet fo	r Input										(Hivate)
7	D	1.80	1.96									5.0	5.2	8.7	9.3	17.0	Proposed 24" RCP or PP Storm Sewer
																	(Private)
	1/2 E	1.10	1.01	See .	Area Draina	ige Sheet fo	r Input					60	4.7	7.0		0.5	
8	1/2 E	1.12	1.21									6.9	4.7	7.9	5.2	9.5	Proposed 10' CDOT Type R At-Grate Inlet (Private)
				See .	Area Draina	ige Sheet fo	r Input										(Tivale)
9	1/2 E	1.12	1.21									6.9	4.7	7.9	5.2	9.5	Proposed 10' CDOT Type R At-Grade Inlet
																	(Private)
10	1/2 G	0.42	0.45	See .	Area Draina	ige Sheet fo	r Input					6.9	4.7	7.9	2.0	8.8	D. HOLODOTT D.C. VI.
10	1/2 G	0.42	0.43									6.9	4.7	7.9	2.0	0.0	Proposed 10' CDOT Type R Sump Inlet (Private)
	(100 YR SPLIT FLOWS)		1.12		Tc for Ba	sin E Used											(Tivac)
11	1/2 G FB-DP8/9	0.61	0.45									6.9	4.7	7.9	2.9	8.8	Proposed 10' CDOT Type R Sump Inlet
			0.67														(Private)
12	(100 YR SPLIT FLOWS) F	2.08	1.12 2.26		Tc for Ba	sin E Used						5.0	5.2	8.7	10.8	19.6	Proposed 30" RCP or PP Storm Sewer
12	Г	2.06	2.20									3.0	3.2	0.7	10.0	19.0	(Private)
				See .	Area Draina	ige Sheet fo	r Input										<u> </u>
13	Н	5.98	7.30					_				8.4	4.4	7.4	26.2	53.8	Proposed 36" RCP or PP Storm Sewer
				C	Area Draina	as Chast C	n Immust										(Private)
14	I	0.86	1.05	See .	Area Draina	ige Sneet to	1 input					8.4	4.4	7.4	3.8	7.8	Proposed Grasslined Swale
17	*	0.00	1.05									0.4	7.7	7.4	5.0	7.0	(Private)
	<u> </u>				Tc for Ba	sin E Used											
15	J, DP14, PR17,	21.74	27.15					_				8.4	4.4	7.4	95.3	199.8	Full Spectrum Extended Detention Basin
	PR 18				To for D	ısin H Used											(Private)
16	POND OUTFALL	2.78	4.61		1 c for Ba	ISHI H USCO						14.5	3.6	6.0	9.9	27,7	HISTORIC FLOW IN CDOT BARROW DITCH
10	OS-2	2.70											3.0	0.0	/./	27.7	Q5= 10.4 CFS, Q100 = 31.9 CFS
					Tc for Basi	in OS-2 Use	ed										PER HISTORIC DRAINAGE ANALYSIS

<sup>#</sup> Intensity equations assume a minimum travel time of 5 minutes.

Calculated by: DLM

Date: 2/24/2021

Checked by: VAS

# CROSSROADS MIXED USE PRELIMINARY DRAINAGE CALCULATIONS

(Storm Sewer Routing Summary)

					Inter	ısity*	El	ow	PIPE SIZE
					Inter	isity"	Fl	ow I	PIPE SIZE
PIPE RUN	Contributing Pipes/Design Points	Equivalent CA 5	Equivalent CA <sub>100</sub>	Maximum T <sub>C</sub>	$I_5$	I 100	<b>Q</b> 5	Q 100	
1	INLET 3	1.78	1.55	12.8	3.8	6.3	6.7	9.8	18" SD
2	INLET 4	1.51	2.64	8.9	4.3	7.2	6.5	19.1	24" SD
3	PR2, INLET 5	3.79	5.28	8.9	4.3	7.2	16.4	38.2	36" SD
4	DP6	3.62	3.98	5.0	5.2	8.7	<b>18.</b> 7	34.5	36" SD
5	PR4	3.62	3.98	5.0	5.2	8.7	<b>18.</b> 7	34.5	36" SD
6	PR5	3.62	3.98	5.0	5.2	8.7	<b>18.</b> 7	34.5	36" SD
7	DP7	1.80	1.96	5.0	5.2	8.7	9.3	17.0	24" SD
8	PR7, INLET 6	2.82	2.83	6.9	4.7	7.9	13.2	22.3	24" SD
9	PR8, INLET 7	3.85	3.71	6.9	4.7	7.9	18.0	29.2	30" SD
10	PR6, PR9	7.47	7.68	6.9	4.7	7.9	35.0	60.5	36" SD
11	PR10	7.47	7.68	6.9	4.7	7.9	35.0	60.5	36" SD
12	INLET 8	0.42	1.12	6.9	4.7	7.9	2.0	8.8	18" SD
13	INLET 9	0.61	1.12	6.9	4.7	7.9	2.9	8.8	18" SD
14	PR11, PR12, PR13	8.51	9.93	6.9	4.7	7.9	39.9	78.1	42" SD
15	DP12	2.08	2.26	5.0	5.2	8.7	10.8	19.6	24" SD
16	PR14, PR15	10.59	12.19	6.9	4.7	7.9	<b>49.</b> 7	96.0	42" SD
17	PR16	10.59	12.19	6.9	4.7	7.9	49.7	96.0	42" SD
18	PR3, DP13	9.77	12.58	8.9	4.3	7.2	42.1	91.1	42" SD
19	POND OUTFALL	PER	MHFD	WKSHT			1.2	8.2	18" SD

\* Intensity equations assume a minimum travel time of 5 minutes.

DP - Design Point FB-FI

EX - Existing Design Point

FB- Flow By from Design Point INT- Intercepted Flow from Design Point Calculated by: DLM
Date: 2/24/2021
Checked by: VAS

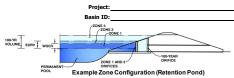
Weig	hted Perce	nt Impervioi	ısness of WQ Pond	1
Contributing Basins	Area (Acres)	C 5	Impervious % (I)	(Acres)*(I)
A	1.68	0.90	100	167.51
В	1.49	0.90	100	149.27
С	4.61	0.79	93	428.35
D	2.22	0.81	95	211.05
E	2.71	0.83	96	260.35
F	2.57	0.81	95	244.34
G	0.94	0.90	100	93.98
H	11.07	0.54	75	830.03
I	1.60	0.54	75	119.84
J	3.21	0.16	7	22.49
Totals	32.10			2527.20
Imperviousness of WQ Pond 1	78.7	%		

# **HYDRAULIC CALCULATIONS**

NOTICE: Staff is only providing cursory review of the hydraulic calculations with the preliminary plan. Detailed review will be conducted with the Final Drainage Report.

### DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.03 (May 2020)



Watershed Information

SHEU IIIIOIIIIauoii						
Selected BMP Type =	EDB					
Watershed Area =	32.10	acres				
Watershed Length =	1,725	ft				
Watershed Length to Centroid =	1,000	ft				
Watershed Slope =	0.006	ft/ft				
Watershed Imperviousness =	78.67%	percent				
Percentage Hydrologic Soil Group A =	100.0%	percent				
Percentage Hydrologic Soil Group B =	0.0%	percent				
ercentage Hydrologic Soil Groups C/D =	0.0%	percent				
Target WQCV Drain Time =	40.0	hours				
Location for 1-hr Rainfall Depths = User Input						

After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

the embedded Colorado Urban Hydrograph Procedure.								
Water Quality Capture Volume (WQCV) =	0.857	acre-feet						
Excess Urban Runoff Volume (EURV) =	3.306	acre-feet						
2-yr Runoff Volume (P1 = 1.19 in.) =	2.394	acre-feet						
5-yr Runoff Volume (P1 = 1.5 in.) =	3.107	acre-feet						
10-yr Runoff Volume (P1 = 1.75 in.) =	3.679	acre-feet						
25-yr Runoff Volume (P1 = 2 in.) =	4.353	acre-feet						
50-yr Runoff Volume (P1 = 2.25 in.) =	5.011	acre-feet						
100-yr Runoff Volume (P1 = 2.52 in.) =	5.779	acre-feet						
500-yr Runoff Volume (P1 = 3.14 in.) =	7.477	acre-feet						
Approximate 2-yr Detention Volume =	2.169	acre-feet						
Approximate 5-yr Detention Volume =	2.821	acre-feet						
Approximate 10-yr Detention Volume =	3.370	acre-feet						
Approximate 25-yr Detention Volume =	4.007	acre-feet						
Approximate 50-yr Detention Volume =	4.381	acre-feet						
Approximate 100-yr Detention Volume =	4.729	acre-feet						

acre-feet	
acre-feet	
1.19 inches	
1.50 inches	
1.75 inches	
2.00 inches	
2.25 inches	
2.52 inches	
inches	

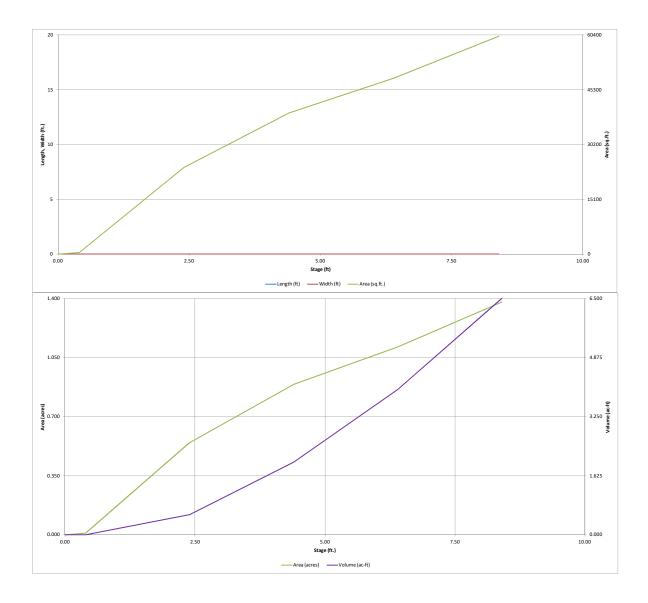
Define Zones and Basin Geometry

		Define Zones and Dasin Geometry
acre-	0.857	Zone 1 Volume (WQCV) =
acre-	2.449	Zone 2 Volume (EURV - Zone 1) =
acre-	1.424	Zone 3 Volume (100-year - Zones 1 & 2) =
acre-	4.729	Total Detention Basin Volume =
ft 3	user	Initial Surcharge Volume (ISV) =
ft	user	Initial Surcharge Depth (ISD) =
ft	user	Total Available Detention Depth (H <sub>total</sub> ) =
ft	user	Depth of Trickle Channel $(H_{TC}) =$
ft/ft	user	Slope of Trickle Channel (S <sub>TC</sub> ) =
H:V	user	Slopes of Main Basin Sides (Smain) =
1	user	Basin Length-to-Width Ratio (R <sub>L/W</sub> ) =

Initial Surcharge Area $(A_{ISV}) =$	user	ft²
Surcharge Volume Length $(L_{ISV}) =$	user	ft
Surcharge Volume Width $(W_{ISV}) =$	user	ft
Depth of Basin Floor $(H_{FLOOR}) =$	user	ft
Length of Basin Floor $(L_{FLOOR}) =$	user	ft
Width of Basin Floor $(W_{FLOOR}) =$	user	ft
Area of Basin Floor $(A_{FLOOR}) =$	user	ft²
Volume of Basin Floor $(V_{FLOOR}) =$	user	ft <sup>3</sup>
Depth of Main Basin $(H_{MAIN}) =$	user	ft
Length of Main Basin $(L_{MAIN}) =$	user	ft
Width of Main Basin $(W_{MAIN}) =$	user	ft
Area of Main Basin $(A_{MAIN}) =$	user	ft²
Volume of Main Basin (V <sub>MAIN</sub> ) =	user	ft <sup>3</sup>
Calculated Total Basin Volume $(V_{total}) =$	user	acre-fe

_	Depth Increment =		ft							
	Stage - Storage Description	Stage (ft)	Optional Override Stage (ft)	Length (ft)	Width (ft)	Area (ft²)	Optional Override Area (ft <sup>2</sup> )	Area (acre)	Volume (ft 3)	Volume (ac-ft)
6287.6			0.00				10	0.000	(10)	(dc 1c)
0207.0			0.40	-	-	-	414	0.010	85	0.002
			2.40	-	-	-	23,852	0.548	24,351	0.559
			4.40				38,877	0.892	87,080	1.999
			6.40	-	-		48,493	1.113	174,450	4.005
			8.40	-	-		60,123	1.380	283,066	6.498
				-	-	-				
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re-feet				1	1					
re-feet				-	-	-				
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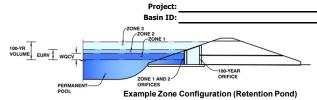
MHFD Prelim Pond Sizing -DLM.xism, Basin 2/24/2021, 7:02 AM



MHFD Prelim Pond Sizing - DLM.xlsm, Basin 2/24/2021, 7.02 AM

### DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.03 (May 2020)



	Estimated	Estimated	
_	Stage (ft)	Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	2.91	0.857	Orifice Plate
Zone 2 (EURV)	5.76	2.449	Orifice Plate
Zone 3 (100-year)	7.03	1.424	Weir&Pipe (Restrict)
•	Total (all zones)	4,729	

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth = N/A ft (distance below the filtration media surface) Underdrain Orifice Diameter = inches N/A

	Calculated Parame	ters for Underdrain
Underdrain Orifice Area =	N/A	ft <sup>2</sup>
Underdrain Orifice Centroid =	N/A	feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice = 0.00 ft (relative to basin bottom at Stage = 0 ft) Depth at top of Zone using Orifice Plate : 5.76 ft (relative to basin bottom at Stage = 0 ft) Orifice Plate: Orifice Vertical Spacing 23.00 inches Orifice Plate: Orifice Area per Row = N/A inches

MP <u>)</u>	Calculated Paramet	ters for Plate
NQ Orifice Area per Row =	N/A	ft <sup>2</sup>
Elliptical Half-Width =	N/A	feet
Elliptical Slot Centroid =	N/A	feet
Elliptical Slot Area =	N/A	ft <sup>2</sup>
P		1

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	1.92	3.84					
Orifice Area (sq. inches)	4.66	4.66	12.20					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

	Not Selected	Not Selected	
Invert of Vertical Orifice =	N/A	N/A	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Vertical Orifice =	N/A	N/A	ft (relative to basin bottom at Stage = 0 ft)
Vertical Orifice Diameter -	NI/A	N/A	inches

	Calculated Paramet	ters for Vertical Orif	ice
	Not Selected	Not Selected	
Vertical Orifice Area =	N/A	N/A	ft²
ertical Orifice Centroid =	N/A	N/A	fee

Zone 3 Weir

6.87

3.07

13.51

8.59

4.29

Calculated Parameters for Overflow Weir

Not Selected

N/A

N/A

N/A

N/A

N/A

feet

feet

ft<sup>2</sup> ft<sup>2</sup>

User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe)

	Zone 3 Weir	Not Selected		
Overflow Weir Front Edge Height, Ho =	5.90	N/A	ft (relative to basin bottom at Stage = 0 ft) Height of Grate Uppe	er Edge, H <sub>t</sub> =
Overflow Weir Front Edge Length =	4.00	N/A	feet Overflow Weir Sk	pe Length =
Overflow Weir Grate Slope =	3.00	N/A	H:V Grate Open Area / 100-yr C	Orifice Area =
Horiz. Length of Weir Sides =	2.91	N/A	feet Overflow Grate Open Area	w/o Debris =
Overflow Grate Open Area % =	70%	N/A	%, grate open area/total area Overflow Grate Open Area	w/ Debris =
Debris Clogging % =	50%	N/A	%	_

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

ser Input: Outlet Pipe w/ Flow Restriction Plate	(Circular Orifice, Re	estrictor Plate, or R	ectangular Orifice)	s for Outlet Pipe w/ Flow Restriction Plate			
	Zone 3 Restrictor	Not Selected			Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	0.25	N/A	ft (distance below basin bottom at Stage = 0 ft)	Outlet Orifice Area =	0.64	N/A	ft <sup>2</sup>
Outlet Pipe Diameter =	18.00	N/A	inches	Outlet Orifice Centroid =	0.34	N/A	feet
Restrictor Plate Height Above Pipe Invert =	7.00	•	inches Half-Central Angle of	Restrictor Plate on Pipe =	1.35	N/A	radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage=	7.25	ft (relative to basin bottom at Stage = $0 \text{ ft}$ )
Spillway Crest Length =	25.00	feet
Spillway End Slopes =	4.00	H:V
Freehoard above May Water Surface -	1.00	feet

	Calculated Paramet	ters for Spillway
Spillway Design Flow Depth=	0.98	feet
Stage at Top of Freeboard =	9.23	feet
Basin Area at Top of Freeboard =	1.38	acres
cin Volume at Top of Freehoard -	6.50	acro-ft

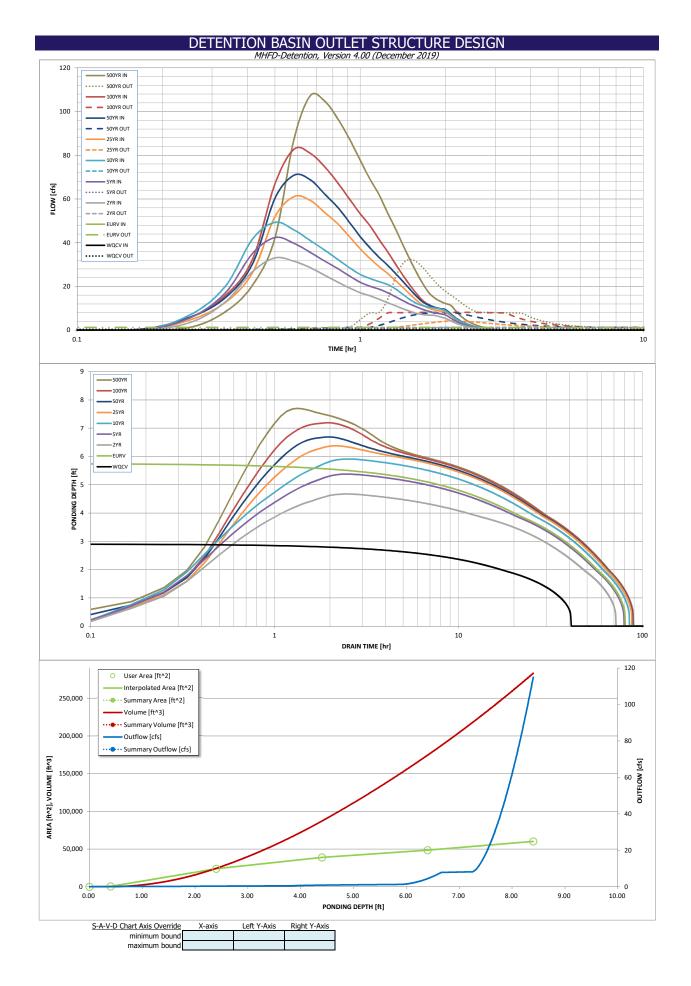
Routed Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = OPTIONAL Ove Predevelo

CUHP Runoff Volume (acre-ft) =
Inflow Hydrograph Volume (acre-ft) =
CUHP Predevelopment Peak Q (cfs) =
FIONAL Override Predevelopment Peak Q (cfs) =
Predevelopment Unit Peak Flow, q (cfs/acre) =
Peak Inflow Q (cfs) =
Peak Outflow Q (cfs) =
Ratio Peak Outflow to Predevelopment Q =
Structure Controlling Flow =
Max Velocity through Grate 1 (fps) =
Max Velocity through Grate 2 (fps) =
Time to Drain 97% of Inflow Volume (hours) =
Time to Drain 99% of Inflow Volume (hours) =
Maximum Ponding Denth (ft) =

Area at Maximum Ponding Depth (acres) =

ograph Results	The user can overi	ide the default CUF	HP hydrographs and	d runoff volumes by	entering new value	es in the Inflow Hya	lrographs table (Col	lumns W through A	F).
Design Storm Return Period =	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
One-Hour Rainfall Depth (in) =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52	3.14
CUHP Runoff Volume (acre-ft) =	0.857	3.306	2.394	3.107	3.679	4.353	5.011	5.779	7.477
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	2.394	3.107	3.679	4.353	5.011	5.779	7.477
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A	0.2	0.3	0.4	4.0	8.1	13.5	24.8
verride Predevelopment Peak Q (cfs) =	N/A	N/A							
lopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.00	0.01	0.01	0.13	0.25	0.42	0.77
Peak Inflow Q (cfs) =	N/A	N/A	33.0	12/	19.3	61.1	70.9	82.7	107.3
Peak Outflow Q (cfs) =	0.4	1.2	1.0	1.2	1.3	4.2	7.9	8.2	32.3
Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	3.7	2.9	1.0	1.0	0.6	1.3
Structure Controlling Flow =	Plate	Plate	Plate	Plate	Overflow Weir 1	Overflow Weir 1	Outlet Plate 1	Outlet Plate 1	Spillway
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	N/A	9.99	0.3	0.7	0.8	0.8
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Drain 97% of Inflow Volume (hours) =	38	72	66	72	76	77	77	76	73
Drain 99% of Inflow Volume (hours) =	40	77	69	77	81	84	84	84	83
Maximum Ponding Depth (ft) =	2.91	5.76	4.67	5.38	5.91	6.38	6.69	7.19	7.70
a at Maximum Ponding Depth (acres) =	0.64	1.04	0.92	1.00	1.06	1.11	1.15	1.22	1.29
Maximum Volume Stored (acre-ft) =	0.861	3.315	2.244	2.917	3.462	3.971	4.322	4.914	5.552

Revise. Must be at or below predevelopment. Unresolved.



# DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename:

Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

Time   Interval	i								in a separate pro		
Section   Control   Cont		SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
0.055.00	Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
0:10:00	5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
C15:00		0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
C-20-00									0.39		
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G.35500         0.00         0.00         3150         39,75         48,90         61,06         70,86         82,89         107,72           G.4500         0.00         0.00         25,08         31,57         36,99         53,77         62,23         74,62         96,89           G.5500         0.00         0.00         12,95         22,17         32,38         48,83         56,17         67,37         67,48           G.5500         0.00         0.00         11,799         22,192         25,30         37,24         40,94         43,26         69,04           1.19500         0.00         0.00         15,89         20,09         23,63         32,73         37,62         47,72         41,41         53,02           1.19500         0.00         0.00         11,49         18,74         22,22         29,04         33,31         14,14         53,02           1.12500         0.00         0.00         11,15         15,26         18,99         22,66         25,93         28,66         35,88         46,81           1.22500         0.00         0.00         11,35         15,66         18,99         22,26         22,87         22,28         23,09         22,2											
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1:00:00		0:50:00	0.00	0.00	21.95	28.17	32.36	48.63	56.17	67.37	87.45
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1:40:00         0.00         0.00         7:10         9:45         11:20         11:35         12:81         13:45         17:04           1:50:00         0.00         0.00         6:71         7:96         10:14         9:25         10:42         10:49         13:20           1:55:00         0.00         0.00         6:04         7:49         9:66         8:72         9:82         9:70         12:18           2:00:00         0.00         0.00         6:04         7:49         9:66         8:72         9:82         9:70         12:18           2:05:00         0.00         0.00         0.00         4:28         5:60         7:14         6:72         7:56         7:26         9:07           2:15:00         0.00         0.00         2:52         3:28         4:28         5:46         5:11         5:75         5:44         6:72           2:10:00         0.00         0.00         2:52         3:28         4:17         3:89         4:37         4:10         5:10           2:10:00         0.00         0.00         1:43         1:87         2:35         2:22         2:49         2:34         2:91           2:30:00         0.00 <th></th>											
1:45:00         0.00         0.00         6.86         8.58         10.98         10.07         11.35         11.63         14.70           1:50:00         0.00         0.00         6.71         7.96         10.14         9.25         10.42         10.49         13.20           1:55:00         0.00         0.00         6.04         7.49         9.66         8.72         9.82         9.70         12.18           2:00:00         0.00         0.00         5.37         6.98         8.92         8.33         9.38         9.14         11.44           2:00:00         0.00         0.00         3.28         4.28         5.46         5.11         5.75         5.44         6.78           2:15:00         0.00         0.00         1.92         2.49         3.15         2.95         3.31         3.11         3.87           2:25:00         0.00         0.00         1.98         1.37         1.74         1.84         1.75         2.91           2:30:00         0.00         0.00         1.48         1.87         2.35         2.22         2.49         2.34         2.91           2:30:00         0.00         0.00         0.79         0.99 <th></th> <th></th> <th>0.00</th> <th>0.00</th> <th>7.62</th> <th>10.63</th> <th>12.22</th> <th>13.58</th> <th>15.38</th> <th>16.61</th> <th>21.13</th>			0.00	0.00	7.62	10.63	12.22	13.58	15.38	16.61	21.13
1:50:00         0.00         0.00         6.71         7.96         10.14         9.25         10.42         10.49         13.20           1:55:00         0.00         0.00         6.04         7.49         9.66         8.72         9.82         9.70         12.18           2:00:00         0.00         0.00         0.00         5.37         6.98         8.92         8.33         9.38         9.14         11.44           2:00:00         0.00         0.00         4.28         5.60         7.14         6.72         7.56         7.26         9.07           2:15:00         0.00         0.00         2.52         3.28         4.28         5.46         5.11         5.75         5.44         6.78           2:15:00         0.00         0.00         1.43         1.87         2.95         3.31         3.11         3.87           2:25:00         0.00         0.00         1.48         1.87         2.35         2.22         2.49         2.34         2.91           2:39:00         0.00         0.00         1.08         1.37         1.74         1.64         1.84         1.75         2.17           2:35:00         0.00         0.00											
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2:05:00         0.00         0.00         4.28         5.60         7.14         6.72         7.56         7.26         9.07           2:10:00         0.00         0.00         3.28         4.28         5.46         5.11         5.75         5.44         6.78           2:15:00         0.00         0.00         0.00         1.92         2.49         3.15         2.95         3.31         3.11         3.87           2:25:00         0.00         0.00         1.45         1.87         2.35         2.22         2.49         2.24         2.21           2:35:00         0.00         0.00         1.48         1.87         2.35         2.22         2.49         2.24         2.91           2:35:00         0.00         0.00         0.00         0.79         0.99         1.28         1.20         1.34         1.29         1.60           2:35:00         0.00         0.00         0.00         0.77         0.72         0.95         0.90         1.01         0.96         0.85           2:46:00         0.00         0.00         0.00         0.33         0.50         0.67         0.64         0.72         0.69         0.85 <td< th=""><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th></td<>											
2:10:00         0.00         0.00         3.28         4.28         5.46         5.11         5.75         5.44         6.78           2:15:00         0.00         0.00         2.52         3.28         4.17         3.89         4.37         4.10         5.10           2:20:00         0.00         0.00         1.92         2.49         3.15         2.95         3.31         3.11         3.87           2:25:00         0.00         0.00         1.65         1.87         2.35         2.22         2.49         2.34         2.91           2:30:00         0.00         0.00         0.00         1.08         1.37         1.74         1.64         1.84         1.29         1.60           2:40:00         0.00         0.00         0.07         9.99         1.28         1.20         1.34         1.29         1.60           2:45:00         0.00         0.00         0.07         0.59         0.67         0.64         0.72         0.69         0.88           2:50:00         0.00         0.00         0.02         2.4         0.33         0.43         0.43         0.48         0.46         0.57           2:55:00         0.00         <											
2:15:00         0.00         0.00         2.52         3.28         4.17         3.89         4.37         4.10         5.10           2:20:00         0.00         0.00         1.92         2.49         3.15         2.95         3.31         3.11         3.87           2:25:00         0.00         0.00         0.00         1.08         1.37         1.74         1.64         1.84         1.75         2.17           2:35:00         0.00         0.00         0.07         0.99         1.28         1.20         1.34         1.29         1.60           2:40:00         0.00         0.00         0.57         0.72         0.95         0.59         1.01         0.96         1.20           2:45:00         0.00         0.00         0.03         0.50         0.67         0.64         0.72         0.69         0.85           2:55:00         0.00         0.00         0.02         0.33         0.43         0.43         0.48         0.46         0.57           2:55:00         0.00         0.00         0.13         0.20         0.25         0.26         0.29         0.28         0.34           3:00:00         0.00         0.00											
2:25:00         0.00         0.00         1.45         1.87         2.35         2.22         2.49         2.34         2.91           2:30:00         0.00         0.00         1.08         1.37         1.74         1.64         1.84         1.75         2.17           2:35:00         0.00         0.00         0.00         0.09         9.99         1.20         1.34         1.29         1.60           2:40:00         0.00         0.00         0.57         0.72         0.95         0.90         1.01         0.96         1.20           2:45:00         0.00         0.00         0.00         0.39         0.50         0.67         0.64         0.72         0.69         0.85           2:55:00         0.00         0.00         0.00         0.33         0.43         0.43         0.48         0.46         0.57           2:55:00         0.00         0.00         0.00         0.01         0.12         1.13         0.14         0.14         0.11           3:05:00         0.00         0.00         0.02         0.03         0.04         0.04         0.05         0.05         0.06           3:15:00         0.00         0.00											
2:30:00         0.00         0.00         1.08         1.37         1.74         1.64         1.84         1.75         2.17           2:35:00         0.00         0.00         0.09         0.99         1.28         1.20         1.34         1.29         1.60           2:46:00         0.00         0.00         0.05         0.95         0.90         1.01         0.96         1.20           2:45:00         0.00         0.00         0.39         0.50         0.67         0.64         0.72         0.69         0.85           2:50:00         0.00         0.00         0.00         0.24         0.33         0.43         0.43         0.48         0.46         0.57           2:55:00         0.00         0.00         0.00         0.06         0.10         0.12         0.13         0.26         0.29         0.28         0.34           3:00:00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00		2:20:00	0.00	0.00	1.92	2.49	3.15	2.95	3.31	3.11	3.87
2:35:00			0.00	0.00	1.45	1.87	2.35	2.22	2.49	2.34	2.91
2:40:00         0.00         0.00         0.57         0.72         0.95         0.90         1.01         0.96         1.20           2:45:00         0.00         0.00         0.00         0.39         0.50         0.67         0.64         0.72         0.69         0.85           2:50:00         0.00         0.00         0.00         0.13         0.20         0.25         0.26         0.29         0.28         0.34           3:00:00         0.00         0.00         0.06         0.10         0.12         0.13         0.14         0.14         0.14         0.14         0.14         0.14         0.14         0.14         0.14         0.14         0.07         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00											
2:45:00         0.00         0.00         0.39         0.50         0.67         0.64         0.72         0.69         0.85           2:55:00         0.00         0.00         0.24         0.33         0.43         0.48         0.46         0.57           2:55:00         0.00         0.00         0.00         0.01         1.02         0.25         0.26         0.29         0.28         0.34           3:00:00         0.00         0.00         0.06         0.10         0.12         0.13         0.14         0.14         0.14         0.14         0.14         0.14         0.14         0.14         0.14         0.14         0.14         0.14         0.14         0.14         0.14         0.14         0.14         0.14         0.14         0.14         0.14         0.14         0.14         0.14         0.05         0.05         0.05         0.05         0.05         0.05         0.06         3.35         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00											
2:50:00         0.00         0.00         0.24         0.33         0.43         0.43         0.48         0.46         0.57           2:55:00         0.00         0.00         0.00         0.13         0.20         0.25         0.26         0.29         0.28         0.34           3:00:00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00											
2:55:00         0.00         0.00         0.13         0.20         0.25         0.26         0.29         0.28         0.34           3:00:00         0.00         0.00         0.06         0.10         0.12         0.13         0.14         0.14         0.17           3:05:00         0.00         0.00         0.00         0.00         0.00         0.00         0.00           3:10:00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00           3:15:00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00											
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3:10:00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00		3:00:00	0.00	0.00					0.14		
3:15:00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00			0.00	0.00	0.02	0.03	0.04	0.04	0.05	0.05	0.06
3:20:00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00									0.00		
3:25:00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00											
$\begin{array}{c} 3:30:00 \\ 3:35:00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.0$											
3:35:00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00											
3:40:00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00											
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3:55:00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00		3:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
4:00:00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00											
4:05:00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00											
4:10:00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00											
4:15:00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00											
4:25:00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00		4:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
4:30:00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00											
4:35:00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00											
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# DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.03 (May 2020)

Summary Stage-Area-Volume-Discharge Relationships
The user can create a summary S-A-V-D by entering the desired stage increments and the remainder of the table will populate automatically.
The user should graphically compare the summary S-A-V-D table to the full S-A-V-D table in the chart to confirm it captures all key transition points.

Stage - Storage Description	Stage [ft]	Area [ft²]	Area [acres]	Volume [ft <sup>3</sup> ]	Volume [ac-ft]	Total Outflow [cfs]	
							For best results, include the
							stages of all grade slope changes (e.g. ISV and Floor)
							from the S-A-V table on Sheet 'Basin'.
							Also include the inverts of all
							outlets (e.g. vertical orifice, overflow grate, and spillway,
							where applicable).
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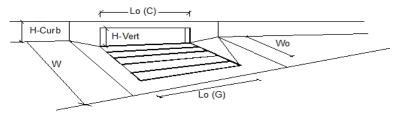


#### ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) Project: **Crossroads Mixed Use Existing Inlets** Inlet ID: INLET 1 CRONN Gutter Geometry (Enter data in the blue cells) T<sub>BACK</sub> Maximum Allowable Width for Spread Behind Curb 14.0 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) S<sub>BACK</sub> : 0.020 ft/ft Manning's Roughness Behind Curb (typically between 0.012 and 0.020) 0.020 Height of Curb at Gutter Flow Line $H_{\text{CURB}}$ 6.00 Distance from Curb Face to Street Crown 26.0 $T_{CROWN}$ Gutter Width w: 2.00 Street Transverse Slope S<sub>X</sub> : 0.020 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) S<sub>w</sub> : 0.083 ft/ft S<sub>o</sub> : Street Longitudinal Slope - Enter 0 for sump condition 0.010 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) n<sub>STREET</sub> : 0.016 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm 20.0 26.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm 6.0 12.0 Allow Flow Depth at Street Crown (leave blank for no) check = yes MINOR STORM Allowable Capacity is based on Depth Criterion Minor Storm Major Storm MAJOR STORM Allowable Capacity is based on Spread Criterion 13.8 32.7 WARNING: MINOR STORM max. allowable capacity is less than the design flow given on sheet 'Inlet Management' lajor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management

Existing Inlet Calcs-DLM.xlsm, INLET 1 2/24/2021, 6:57 AM

# INLET ON A CONTINUOUS GRADE

Version 4.06 Released August 2018



Design Information (Input)		MINOR	MAJOR	
Type of Inlet CDOT Type R Curb Opening   ▼	Type =	CDOT Type F	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a <sub>LOCAL</sub> =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L <sub>o</sub> =	10.00	10.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W <sub>o</sub> =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C <sub>f</sub> -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C <sub>f</sub> -C =	0.10	0.10	
Street Hydraulics: WARNING: Q > ALLOWABLE Q FOR MINOR STORM		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	8.4	11.1	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	<b>Q</b> <sub>b</sub> =	5.8	15.4	cfs
Capture Percentage = Q <sub>a</sub> /Q <sub>o</sub> =	C% =	59	42	%

Existing Inlet Calcs-DLM.xlsm, INLET 1 2/24/2021, 6:57 AM

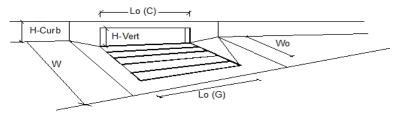


#### ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) Project: **Crossroads Mixed Use Existing Inlets** Inlet ID: INLET 2 CRONN Gutter Geometry (Enter data in the blue cells) T<sub>BACK</sub> Maximum Allowable Width for Spread Behind Curb 14.0 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) $\mathsf{S}_{\mathsf{BACK}}$ 0.020 ft/ft Manning's Roughness Behind Curb (typically between 0.012 and 0.020) 0.020 Height of Curb at Gutter Flow Line $H_{\text{CURB}}$ 6.00 Distance from Curb Face to Street Crown 26.0 $T_{CROWN}$ Gutter Width w: 2.00 Street Transverse Slope S<sub>X</sub> : 0.020 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) S<sub>w</sub> : 0.083 ft/ft S<sub>o</sub> : Street Longitudinal Slope - Enter 0 for sump condition 0.010 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) n<sub>STREET</sub> : 0.016 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm 20.0 26.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm 6.0 12.0 Allow Flow Depth at Street Crown (leave blank for no) check = yes MINOR STORM Allowable Capacity is based on Depth Criterion Minor Storm Major Storm MAJOR STORM Allowable Capacity is based on Spread Criterion 13.8 32.7 linor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Manage lajor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Manager

Existing Inlet Calcs-DLM.xlsm, INLET 2 2/24/2021, 6:57 AM

# INLET ON A CONTINUOUS GRADE

Version 4.06 Released August 2018



Design Information (Input)  CDOT Type R Curb Opening		MINO	R MAJOR	
Type of Inlet	Тур	e = CDOT	Type R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a <sub>LOCA</sub>	L = 3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	N	o = 1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L	o = 10.00	10.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W	o = N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C <sub>r</sub> (	9 = N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C <sub>r</sub> -(	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity		MINO	R MAJOR	
Total Inlet Interception Capacity	(	Q = 3.1	5.3	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q	<sub>b</sub> = 0.0	0.7	cfs
Capture Percentage = Q <sub>a</sub> /Q <sub>o</sub> =	C%	6 = 100	88	%

Existing Inlet Calcs-DLM.xlsm, INLET 2 2/24/2021, 6:57 AM

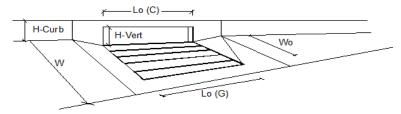


#### ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) Project: Crossroads Mixed Use Inlet ID: Inlet 3 CRONN Gutter Geometry (Enter data in the blue cells) T<sub>BACK</sub> Maximum Allowable Width for Spread Behind Curb 7.5 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) S<sub>BACK</sub> : 0.020 ft/ft Manning's Roughness Behind Curb (typically between 0.012 and 0.020) 0.020 Height of Curb at Gutter Flow Line $H_{\text{CURB}}$ 6.00 Distance from Curb Face to Street Crown T<sub>CROWN</sub> 27.0 Gutter Width w: 1.00 Street Transverse Slope S<sub>X</sub> : 0.020 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) S<sub>w</sub> : 0.083 ft/ft S<sub>o</sub> : Street Longitudinal Slope - Enter 0 for sump condition 0.005 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) n<sub>STREET</sub> : 0.016 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm 22.8 27.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm 6.0 12.0 Allow Flow Depth at Street Crown (leave blank for no) check = yes MINOR STORM Allowable Capacity is based on Depth Criterion Minor Storm Major Storm MAJOR STORM Allowable Capacity is based on Spread Criterion 13.8 24.4 Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Manage lajor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Manager

Proposed Inlet Calcs.xlsm, Inlet 3 2/24/2021, 6:54 AM

# INLET ON A CONTINUOUS GRADE

Version 4.06 Released August 2018



Design Information (Input)  CDOT Type R Curb Opening  ▼		MINOR	MAJOR	
Type of Inlet CDOT Type R Curb Opening	Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a <sub>LOCAL</sub> =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L <sub>o</sub> =	10.00	10.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W <sub>o</sub> =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C <sub>f</sub> -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C <sub>f</sub> -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	6.7	9.8	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	<b>Q</b> <sub>b</sub> =	3.5	13.5	cfs
Capture Percentage = Q <sub>a</sub> /Q <sub>o</sub> =	C% =	65	42	%

Proposed Inlet Calcs.xlsm, Inlet 3 2/24/2021, 6:54 AM

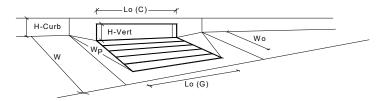


#### ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) Project: Crossroads Mixed Use Inlet ID: Inlet 4 CRONN Gutter Geometry (Enter data in the blue cells) T<sub>BACK</sub> Maximum Allowable Width for Spread Behind Curb 7.5 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) $\mathsf{S}_{\mathsf{BACK}}$ 0.020 ft/ft Manning's Roughness Behind Curb (typically between 0.012 and 0.020) 0.020 Height of Curb at Gutter Flow Line $H_{\text{CURB}}$ 6.00 Distance from Curb Face to Street Crown T<sub>CROWN</sub> 26.0 Gutter Width W = 2.00 Street Transverse Slope S<sub>X</sub> : 0.020 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) S<sub>w</sub> : 0.083 ft/ft Street Longitudinal Slope - Enter 0 for sump condition S<sub>o</sub> : 0.000 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) n<sub>STREET</sub> : 0.016 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm 20.8 26.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm 6.0 12.0 Check boxes are not applicable in SUMP conditions MINOR STORM Allowable Capacity is based on Depth Criterion Minor Storm Major Storm MAJOR STORM Allowable Capacity is based on Depth Criterion SUMP SUMP

Proposed Inlet Calcs.xlsm, Inlet 4 2/24/2021, 6:55 AM

# **INLET IN A SUMP OR SAG LOCATION**

Version 4.06 Released August 2018



Design Information (Input)		MINOR	MAJOR	
Type of Inlet CDOT Type R Curb Opening   ▼	Type =	CDOT Type R	Curb Opening	1
Local Depression (additional to continuous gutter depression 'a' from above)	a <sub>local</sub> =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	6.0	12.0	inches
Grate Information		MINOR	MAJOR	Override Depths
ength of a Unit Grate	L <sub>0</sub> (G) =	N/A	N/A	feet
Width of a Unit Grate	W <sub>o</sub> =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A <sub>ratio</sub> =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_f(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C <sub>w</sub> (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	C <sub>o</sub> (G) =	N/A	N/A	
Curb Opening Information	_	MINOR	MAJOR	_
Length of a Unit Curb Opening	L <sub>o</sub> (C) =	15.00	15.00	feet
Height of Vertical Curb Opening in Inches	H <sub>vert</sub> =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H <sub>throat</sub> =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W <sub>p</sub> =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	C <sub>w</sub> (C) =	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	C <sub>o</sub> (C) =	0.67	0.67	]
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d <sub>Grate</sub> =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d <sub>Curb</sub> =	0.33	0.83	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF <sub>Combination</sub> =	0.57	1.00	
Curb Opening Performance Reduction Factor for Long Inlets	RF <sub>Curb</sub> =	0.79	1.00	
Grated Inlet Performance Reduction Factor for Long Inlets	RF <sub>Grate</sub> =	N/A	N/A	
		MINOR	MAJOR	_
Total Inlet Interception Capacity (assumes clogged condition)	$Q_a =$	9.7	39.1	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	6.5	19.1	cfs

Proposed Inlet Calcs.xlsm, Inlet 4 2/24/2021, 6:55 AM

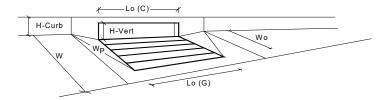


#### ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) Project: Crossroads Mixed Use Inlet ID: Inlet 5 CRONN Gutter Geometry (Enter data in the blue cells) T<sub>BACK</sub> Maximum Allowable Width for Spread Behind Curb 7.5 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) $\mathsf{S}_{\mathsf{BACK}}$ 0.020 ft/ft Manning's Roughness Behind Curb (typically between 0.012 and 0.020) 0.020 Height of Curb at Gutter Flow Line $H_{\text{CURB}}$ 6.00 Distance from Curb Face to Street Crown T<sub>CROWN</sub> 26.0 Gutter Width W = 2.00 Street Transverse Slope S<sub>X</sub> : 0.020 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) S<sub>w</sub> : 0.083 ft/ft Street Longitudinal Slope - Enter 0 for sump condition S<sub>o</sub> : 0.000 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) n<sub>STREET</sub> : 0.016 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm 20.8 26.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm 6.0 12.0 Check boxes are not applicable in SUMP conditions MINOR STORM Allowable Capacity is based on Depth Criterion Minor Storm Major Storm MAJOR STORM Allowable Capacity is based on Depth Criterion SUMP SUMP

Proposed Inlet Calcs.xlsm, Inlet 5 2/24/2021, 6:55 AM

# **INLET IN A SUMP OR SAG LOCATION**

Version 4.06 Released August 2018



Design Information (Input)		MINOR	MAJOR	
Type of Inlet CDOT Type R Curb Opening   ▼	Type =	CDOT Type R	Curb Opening	1
Local Depression (additional to continuous gutter depression 'a' from above)	a <sub>local</sub> =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	6.0	12.0	inches
Grate Information		MINOR	MAJOR	Override Depths
ength of a Unit Grate	L <sub>o</sub> (G) =	N/A	N/A	feet
Width of a Unit Grate	W <sub>o</sub> =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A <sub>ratio</sub> =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_f(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C <sub>w</sub> (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	C <sub>o</sub> (G) =	N/A	N/A	
Curb Opening Information	_	MINOR	MAJOR	_
Length of a Unit Curb Opening	L <sub>o</sub> (C) =	15.00	15.00	feet
Height of Vertical Curb Opening in Inches	H <sub>vert</sub> =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H <sub>throat</sub> =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W <sub>p</sub> =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	C <sub>w</sub> (C) =	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	C <sub>o</sub> (C) =	0.67	0.67	]
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d <sub>Grate</sub> =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d <sub>Curb</sub> =	0.34	0.83	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF <sub>Combination</sub> =	0.57	1.00	
Curb Opening Performance Reduction Factor for Long Inlets	RF <sub>Curb</sub> =	0.79	1.00	
Grated Inlet Performance Reduction Factor for Long Inlets	RF <sub>Grate</sub> =	N/A	N/A	]
		MINOR	MAJOR	_
Total Inlet Interception Capacity (assumes clogged condition)	$Q_a =$	9.9	39.1	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	9.9	19.1	cfs

Proposed Inlet Calcs.xlsm, Inlet 5 2/24/2021, 6:55 AM

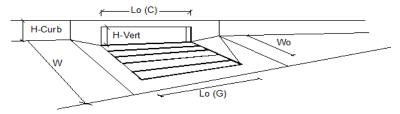


#### ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) Project: Crossroads Mixed Use Inlet ID: Inlet 6 CRONN Gutter Geometry (Enter data in the blue cells) T<sub>BACK</sub> Maximum Allowable Width for Spread Behind Curb 7.5 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) S<sub>BACK</sub> : 0.020 ft/ft Manning's Roughness Behind Curb (typically between 0.012 and 0.020) 0.020 Height of Curb at Gutter Flow Line $H_{\text{CURB}}$ 6.00 Distance from Curb Face to Street Crown T<sub>CROWN</sub> 14.5 Gutter Width w: 2.00 Street Transverse Slope S<sub>X</sub> : 0.020 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) S<sub>w</sub> : 0.083 ft/ft S<sub>o</sub> : Street Longitudinal Slope - Enter 0 for sump condition 0.020 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) n<sub>STREET</sub> : 0.016 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm 14.0 14.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm 4.4 12.0 Allow Flow Depth at Street Crown (leave blank for no) check = yes MINOR STORM Allowable Capacity is based on Depth Criterion Minor Storm Major Storm MAJOR STORM Allowable Capacity is based on Spread Criterion 9.6 linor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Manage lajor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Manager

Proposed Inlet Calcs.xlsm, Inlet 6 2/24/2021, 6:56 AM

# INLET ON A CONTINUOUS GRADE

Version 4.06 Released August 2018



Design Information (Input)		MINOR	MAJOR	
Type of Inlet CDOT Type R Curb Opening	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a <sub>LOCAL</sub> =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L <sub>o</sub> =	10.00	10.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W <sub>o</sub> =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C <sub>f</sub> -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C <sub>f</sub> -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	4.8	6.9	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	<b>Q</b> <sub>b</sub> =	0.4	2.6	cfs
Capture Percentage = Q <sub>a</sub> /Q <sub>o</sub> =	C% =	93	73	%

Proposed Inlet Calcs.xlsm, Inlet 6 2/24/2021, 6:56 AM

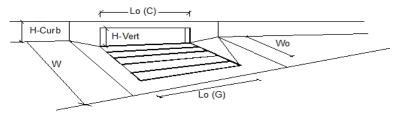


#### ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) Project: Crossroads Mixed Use Inlet ID: Inlet 7 CRONN Gutter Geometry (Enter data in the blue cells) T<sub>BACK</sub> Maximum Allowable Width for Spread Behind Curb 7.5 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) S<sub>BACK</sub> : 0.020 ft/ft Manning's Roughness Behind Curb (typically between 0.012 and 0.020) 0.020 Height of Curb at Gutter Flow Line $H_{\text{CURB}}$ 6.00 Distance from Curb Face to Street Crown T<sub>CROWN</sub> 14.0 Gutter Width w: 2.00 Street Transverse Slope S<sub>X</sub> : 0.020 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) S<sub>w</sub> : 0.083 ft/ft S<sub>o</sub> : Street Longitudinal Slope - Enter 0 for sump condition 0.010 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) n<sub>STREET</sub> : 0.016 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm 14.0 14.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm 4.4 12.0 Allow Flow Depth at Street Crown (leave blank for no) check = yes MINOR STORM Allowable Capacity is based on Depth Criterion Minor Storm Major Storm MAJOR STORM Allowable Capacity is based on Spread Criterion WARNING: MINOR STORM max. allowable capacity is less than the design flow given on sheet 'Inlet Management' ARNING: MAJOR STORM max. allowable capacity is less than the design flow given on sheet 'Inlet Management

Proposed Inlet Calcs.xlsm, Inlet 7 2/24/2021, 6:56 AM

# INLET ON A CONTINUOUS GRADE

Version 4.06 Released August 2018



Design Information (Input)  CDOT Type R Curb Opening  ▼	_	MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a <sub>LOCAL</sub> =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L <sub>o</sub> =	10.00	10.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W <sub>o</sub> =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C <sub>f</sub> -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C <sub>f</sub> -C =	0.10	0.10	
Street Hydraulics: WARNING: Q > ALLOWABLE Q FOR MINOR & MAJOR STORM		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	4.8	6.9	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	<b>Q</b> <sub>b</sub> =	0.4	2.6	cfs
Capture Percentage = Q <sub>a</sub> /Q <sub>o</sub> =	C% =	92	72	%

Proposed Inlet Calcs.xlsm, Inlet 7 2/24/2021, 6:56 AM

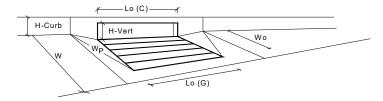


#### ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) Project: Crossroads Mixed Use Inlet ID: Inlet 8 CRONN Gutter Geometry (Enter data in the blue cells) T<sub>BACK</sub> Maximum Allowable Width for Spread Behind Curb 7.5 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) $\mathsf{S}_{\mathsf{BACK}}$ 0.020 ft/ft Manning's Roughness Behind Curb (typically between 0.012 and 0.020) 0.020 Height of Curb at Gutter Flow Line $H_{\text{CURB}}$ 6.00 Distance from Curb Face to Street Crown T<sub>CROWN</sub> 14.0 Gutter Width W = 2.00 Street Transverse Slope S<sub>X</sub> : 0.020 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) S<sub>w</sub> : 0.083 ft/ft Street Longitudinal Slope - Enter 0 for sump condition S<sub>o</sub> : 0.000 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) n<sub>STREET</sub> : 0.016 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm 14.0 14.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm 4.4 12.0 Check boxes are not applicable in SUMP conditions MINOR STORM Allowable Capacity is based on Depth Criterion Minor Storm Major Storm MAJOR STORM Allowable Capacity is based on Depth Criterion SUMP SUMP

Proposed Inlet Calcs.xlsm, Inlet 8 2/24/2021, 6:56 AM

# **INLET IN A SUMP OR SAG LOCATION**

Version 4.06 Released August 2018



Design Information (Input) CDOT Type R Curb Opening   ▼		MINOR	MAJOR	_
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a <sub>local</sub> =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	4.4	8.0	inches
Grate Information		MINOR	MAJOR	Override Depths
Length of a Unit Grate	L <sub>0</sub> (G) =	N/A	N/A	feet
Width of a Unit Grate	W <sub>o</sub> =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A <sub>ratio</sub> =	N/A	N/A	1
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	C <sub>f</sub> (G) =	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C <sub>w</sub> (G) =	N/A	N/A	1
Grate Orifice Coefficient (typical value 0.60 - 0.80)	C <sub>o</sub> (G) =	N/A	N/A	7
Curb Opening Information	_	MINOR	MAJOR	
Length of a Unit Curb Opening	L <sub>0</sub> (C) =	10.00	10.00	feet
Height of Vertical Curb Opening in Inches	H <sub>vert</sub> =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H <sub>throat</sub> =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W <sub>p</sub> =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	C <sub>w</sub> (C) =	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	C <sub>o</sub> (C) =	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d <sub>Grate</sub> =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d <sub>Curb</sub> =	0.20	0.50	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF <sub>Combination</sub> =	0.41	0.75	
Curb Opening Performance Reduction Factor for Long Inlets	RF <sub>Curb</sub> =	0.82	1.00	
Grated Inlet Performance Reduction Factor for Long Inlets	RF <sub>Grate</sub> =	N/A	N/A	
		MINOR	MAJOR	
Total Inlet Interception Capacity (assumes clogged condition)	$Q_a =$	3.3	16.3	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	2.0	8.8	cfs

Proposed Inlet Calcs.xlsm, Inlet 8 2/24/2021, 6:56 AM

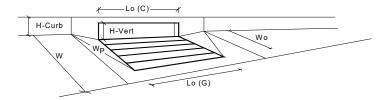


#### ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) Project: Crossroads Mixed Use Inlet ID: Inlet 9 CRONN Gutter Geometry (Enter data in the blue cells) T<sub>BACK</sub> Maximum Allowable Width for Spread Behind Curb 7.5 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) $\mathsf{S}_{\mathsf{BACK}}$ 0.020 ft/ft Manning's Roughness Behind Curb (typically between 0.012 and 0.020) 0.020 Height of Curb at Gutter Flow Line $H_{\text{CURB}}$ 6.00 Distance from Curb Face to Street Crown T<sub>CROWN</sub> 14.0 Gutter Width W = 2.00 Street Transverse Slope S<sub>X</sub> : 0.020 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) S<sub>w</sub> : 0.083 ft/ft Street Longitudinal Slope - Enter 0 for sump condition S<sub>o</sub> : 0.000 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) n<sub>STREET</sub> : 0.016 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm 14.0 14.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm 4.4 12.0 Check boxes are not applicable in SUMP conditions MINOR STORM Allowable Capacity is based on Depth Criterion Minor Storm Major Storm MAJOR STORM Allowable Capacity is based on Depth Criterion SUMP SUMP

Proposed Inlet Calcs.xlsm, Inlet 9 2/24/2021, 6:57 AM

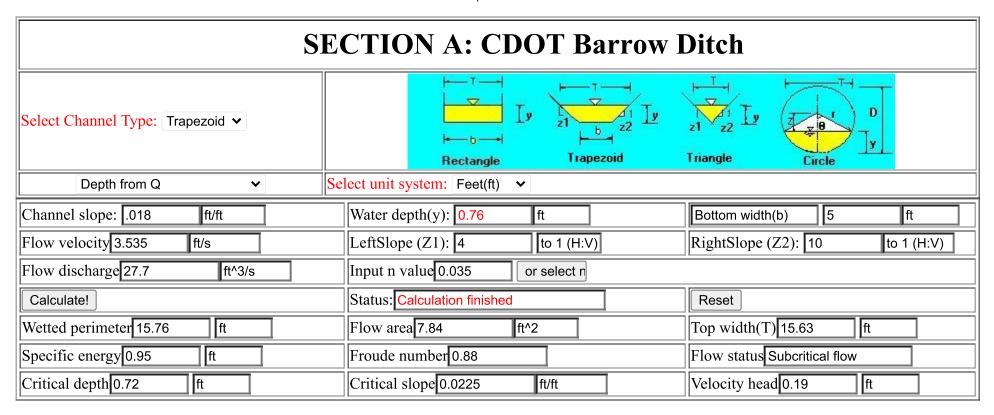
# **INLET IN A SUMP OR SAG LOCATION**

Version 4.06 Released August 2018



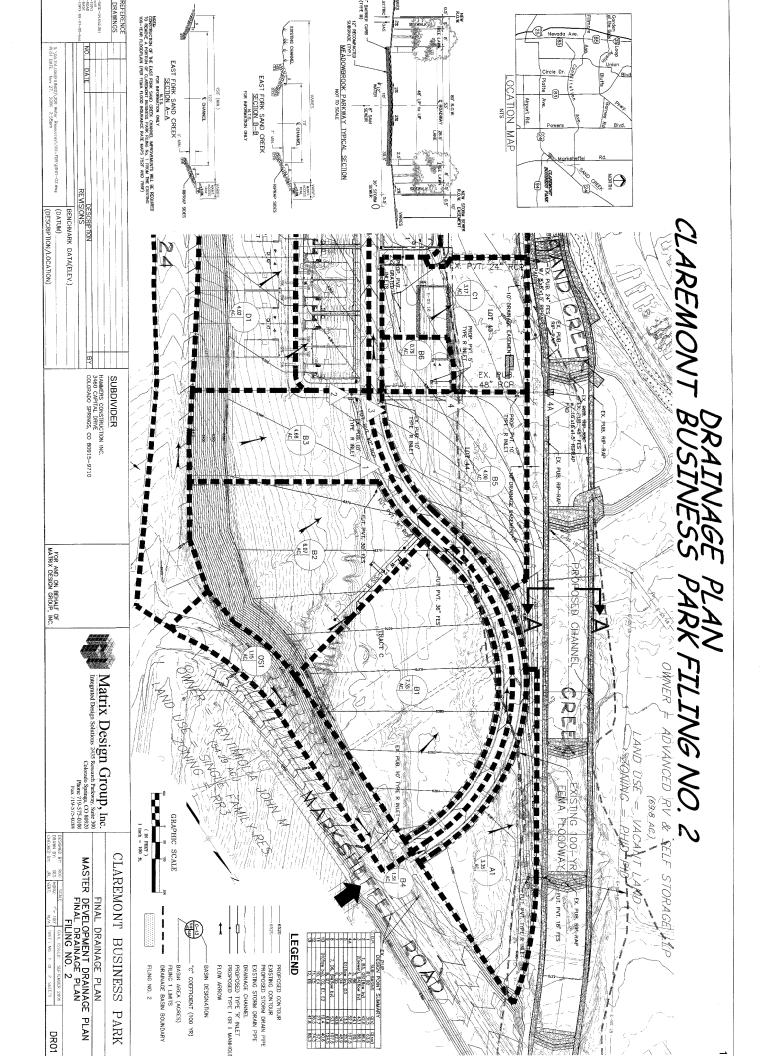
Design Information (Input) CDOT Type R Curb Opening		MINOR	MAJOR	_
Type of Inlet	Type =	CDOT Type F	Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a <sub>local</sub> =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	4.4	8.0	inches
Grate Information		MINOR	MAJOR	Override Depths
Length of a Unit Grate	L <sub>0</sub> (G) =	N/A	N/A	feet
Width of a Unit Grate	W <sub>o</sub> =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A <sub>ratio</sub> =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_f(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C <sub>w</sub> (G) =	N/A	N/A	1
Grate Orifice Coefficient (typical value 0.60 - 0.80)	C <sub>o</sub> (G) =	N/A	N/A	
Curb Opening Information	_	MINOR	MAJOR	
Length of a Unit Curb Opening	L <sub>0</sub> (C) =	10.00	10.00	feet
Height of Vertical Curb Opening in Inches	H <sub>vert</sub> =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H <sub>throat</sub> =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W <sub>p</sub> =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	C <sub>w</sub> (C) =	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	C <sub>o</sub> (C) =	0.67	0.67	]
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d <sub>Grate</sub> =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d <sub>Curb</sub> =	0.20	0.50	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF <sub>Combination</sub> =	0.41	0.75	
Curb Opening Performance Reduction Factor for Long Inlets	RF <sub>Curb</sub> =	0.82	1.00	
Grated Inlet Performance Reduction Factor for Long Inlets	RF <sub>Grate</sub> =	N/A	N/A	
		MINOR	MAJOR	_
Total Inlet Interception Capacity (assumes clogged condition)	Q <sub>a</sub> =	3.3	16.3	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q <sub>PEAK REQUIRED</sub> =	2.9	8.8	cfs

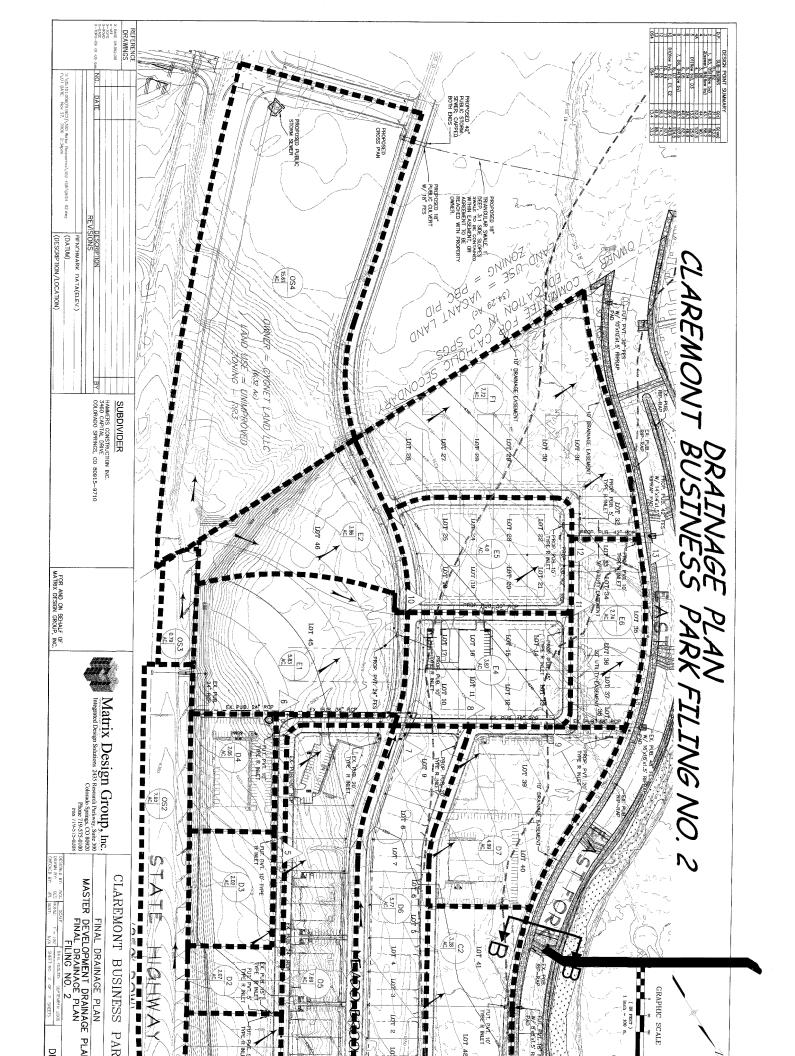
Proposed Inlet Calcs.xlsm, Inlet 9 2/24/2021, 6:57 AM

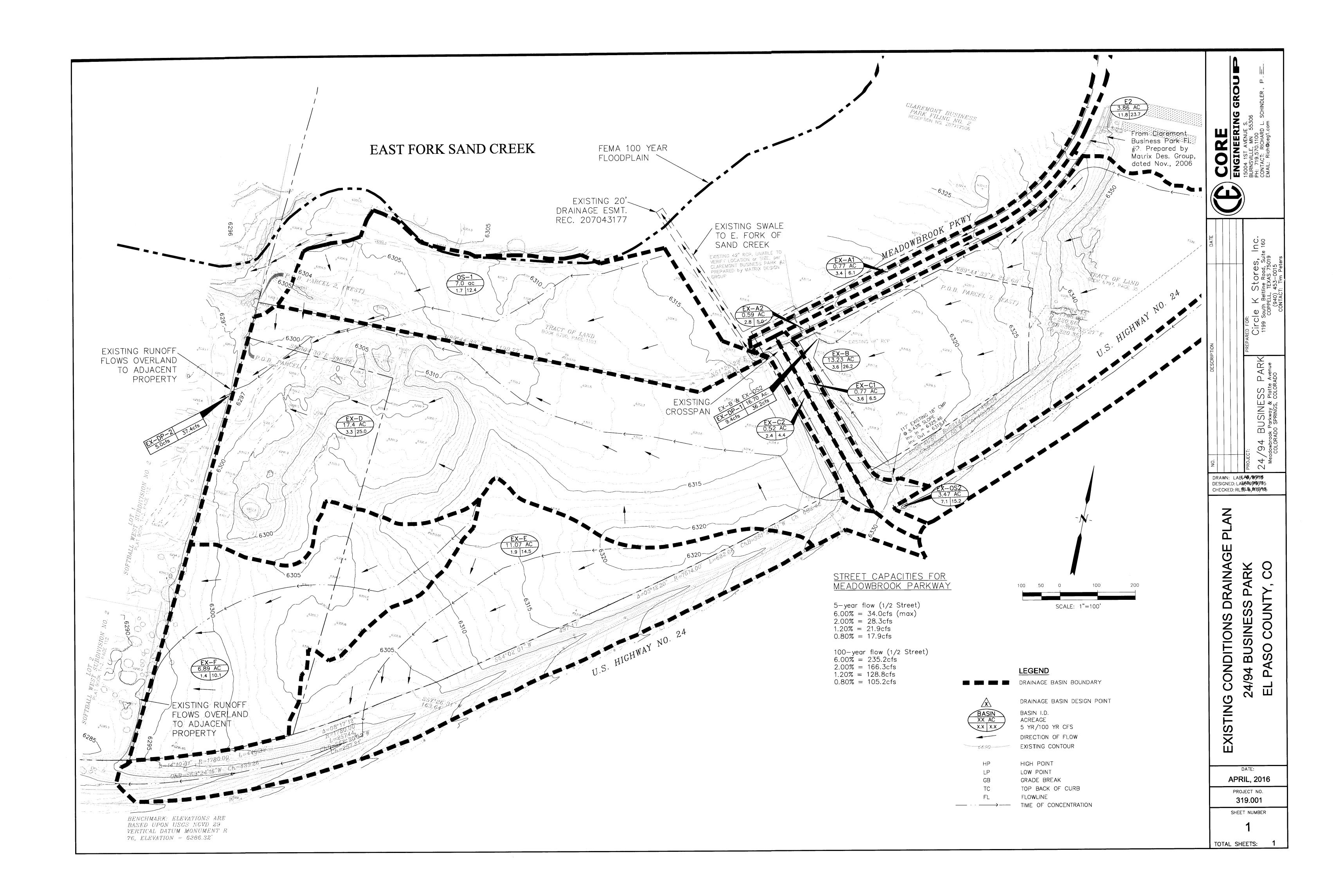


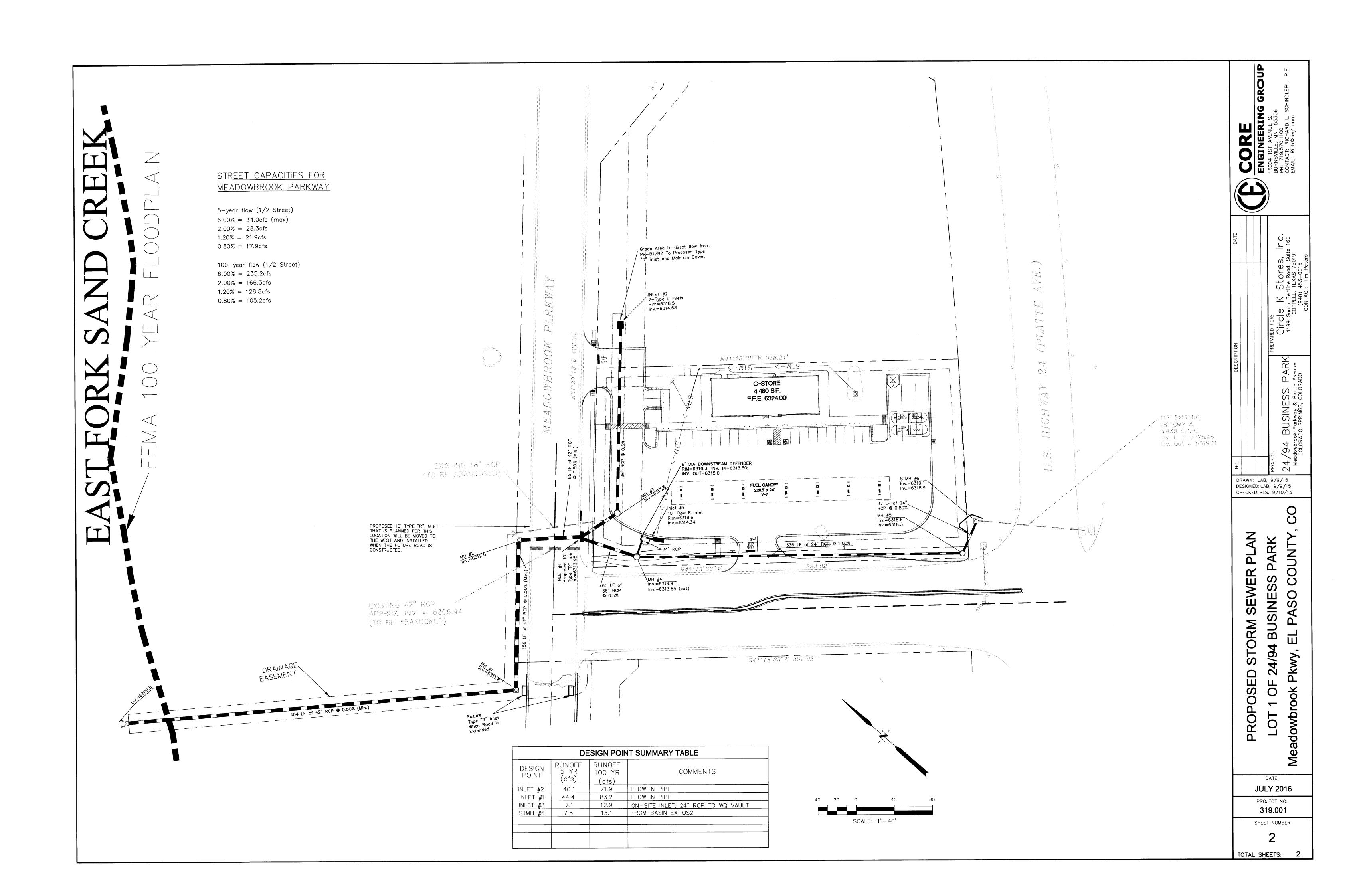
Copyright 2000 Dr. Xing Fang, Department of Civil Engineering, Lamar University.

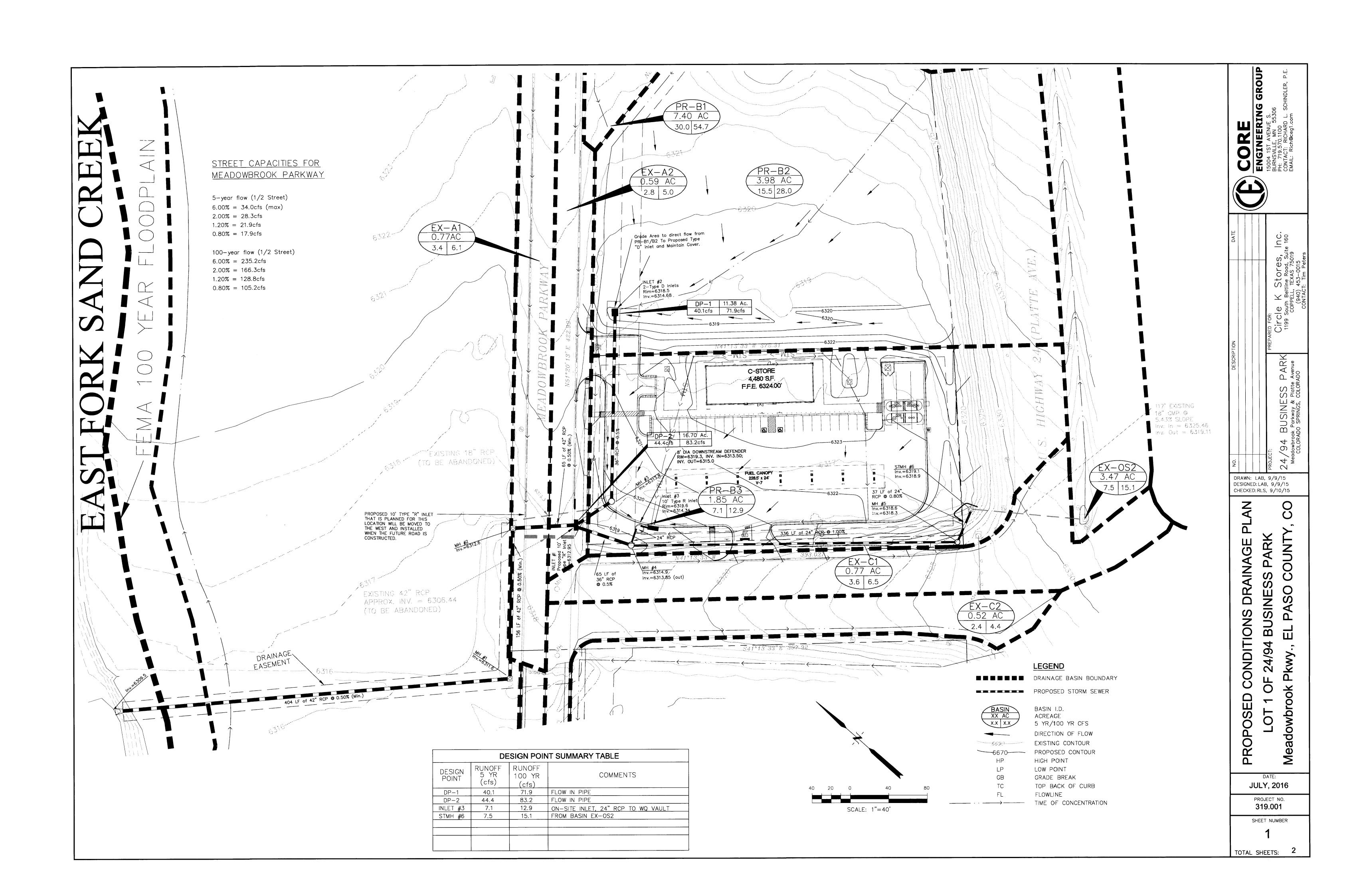
**BACKGROUND** 

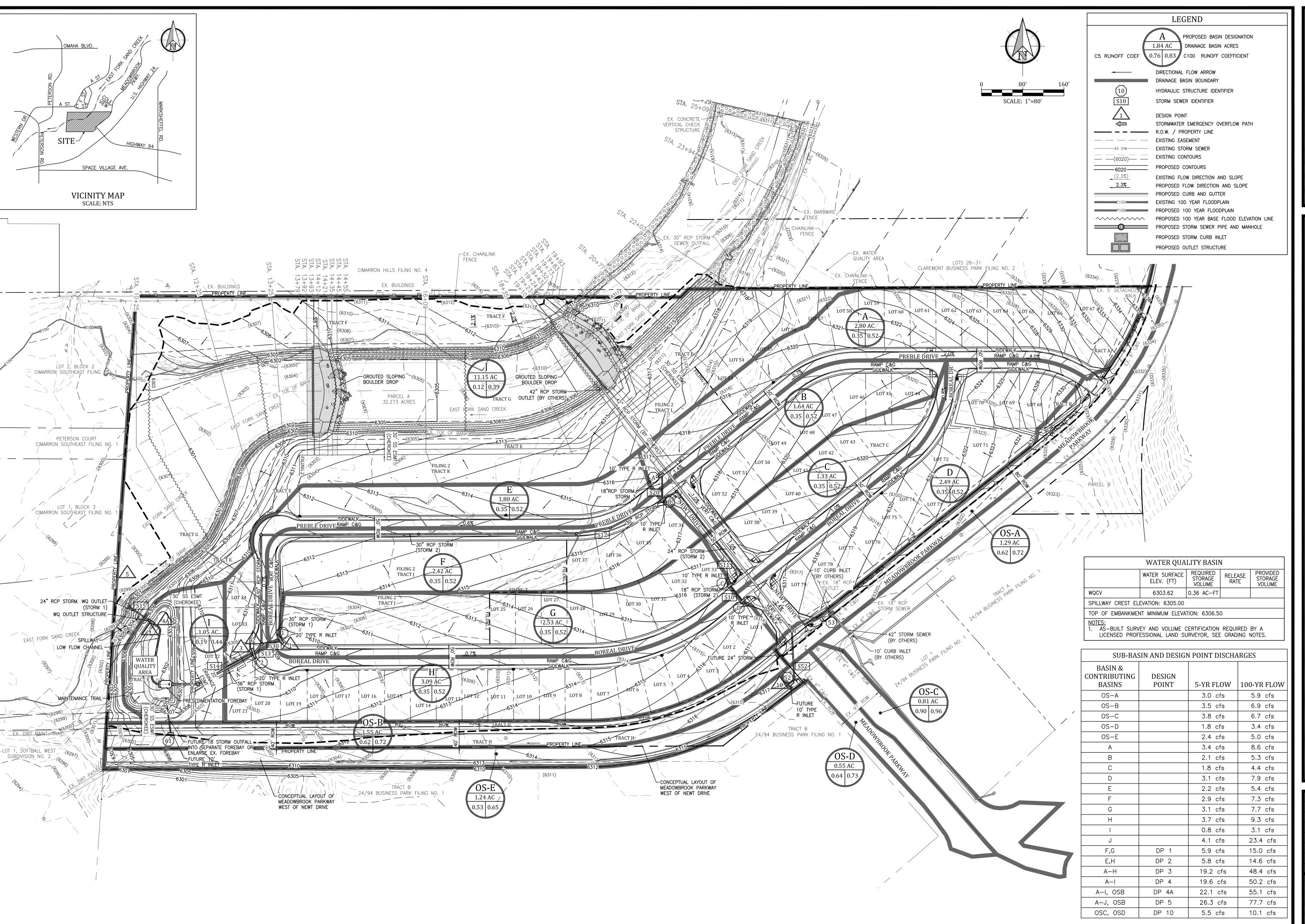


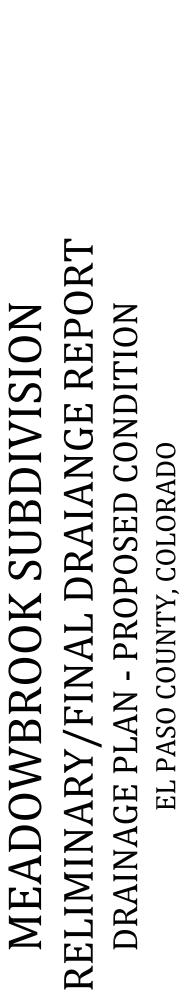












Project No.: 16039

Date: July 25, 2017

Design: ELS

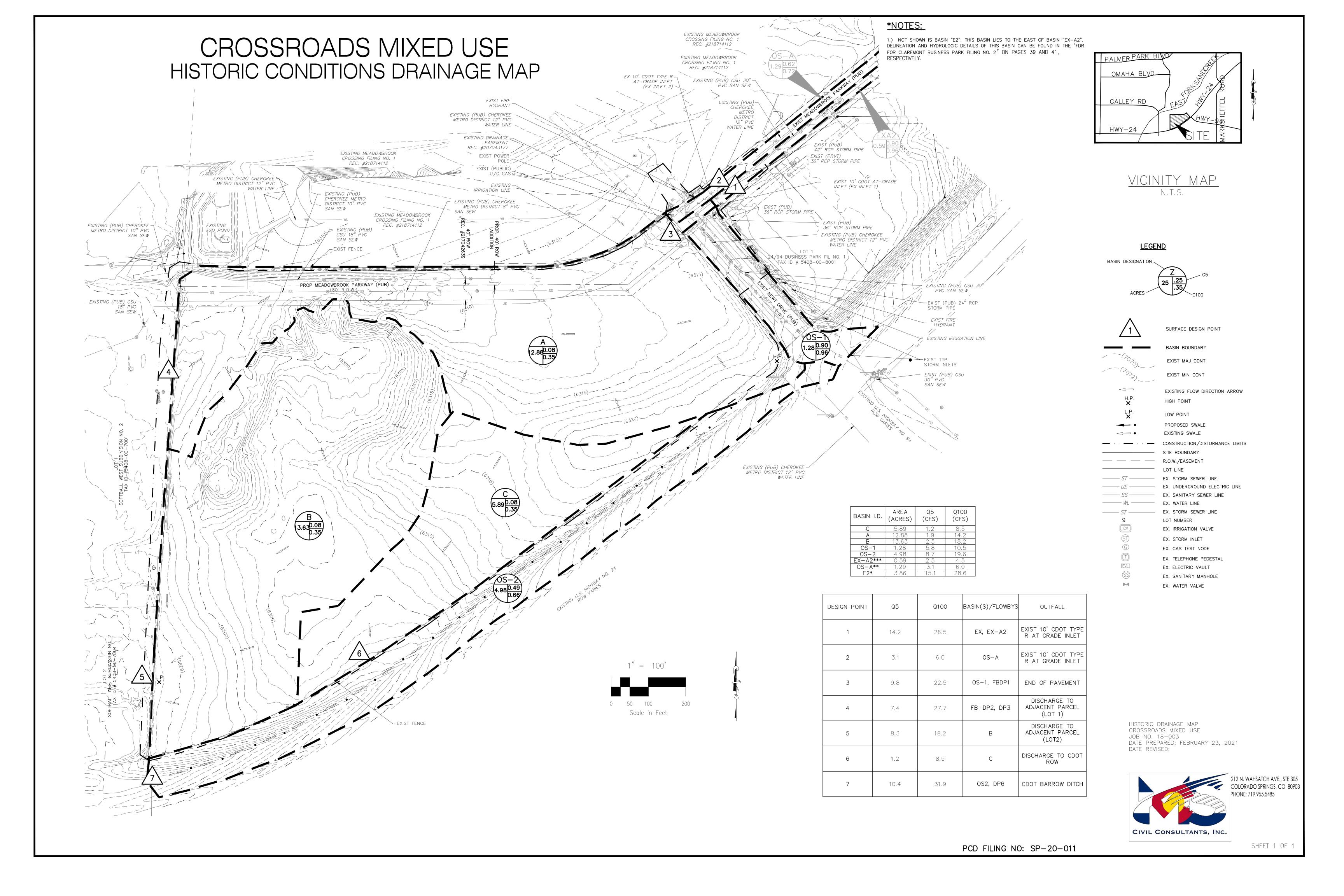
Drawn: ELS

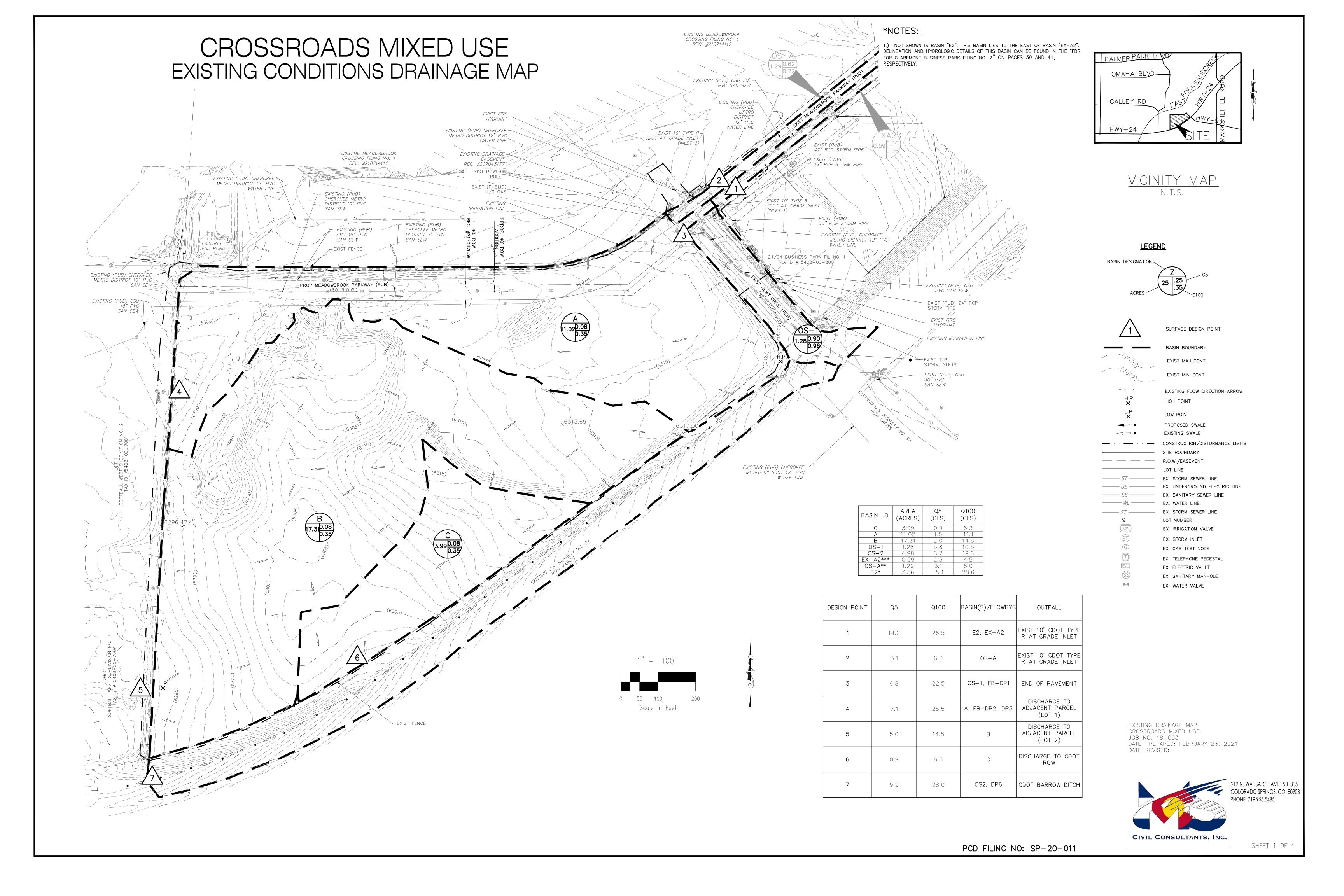
Check: MWE

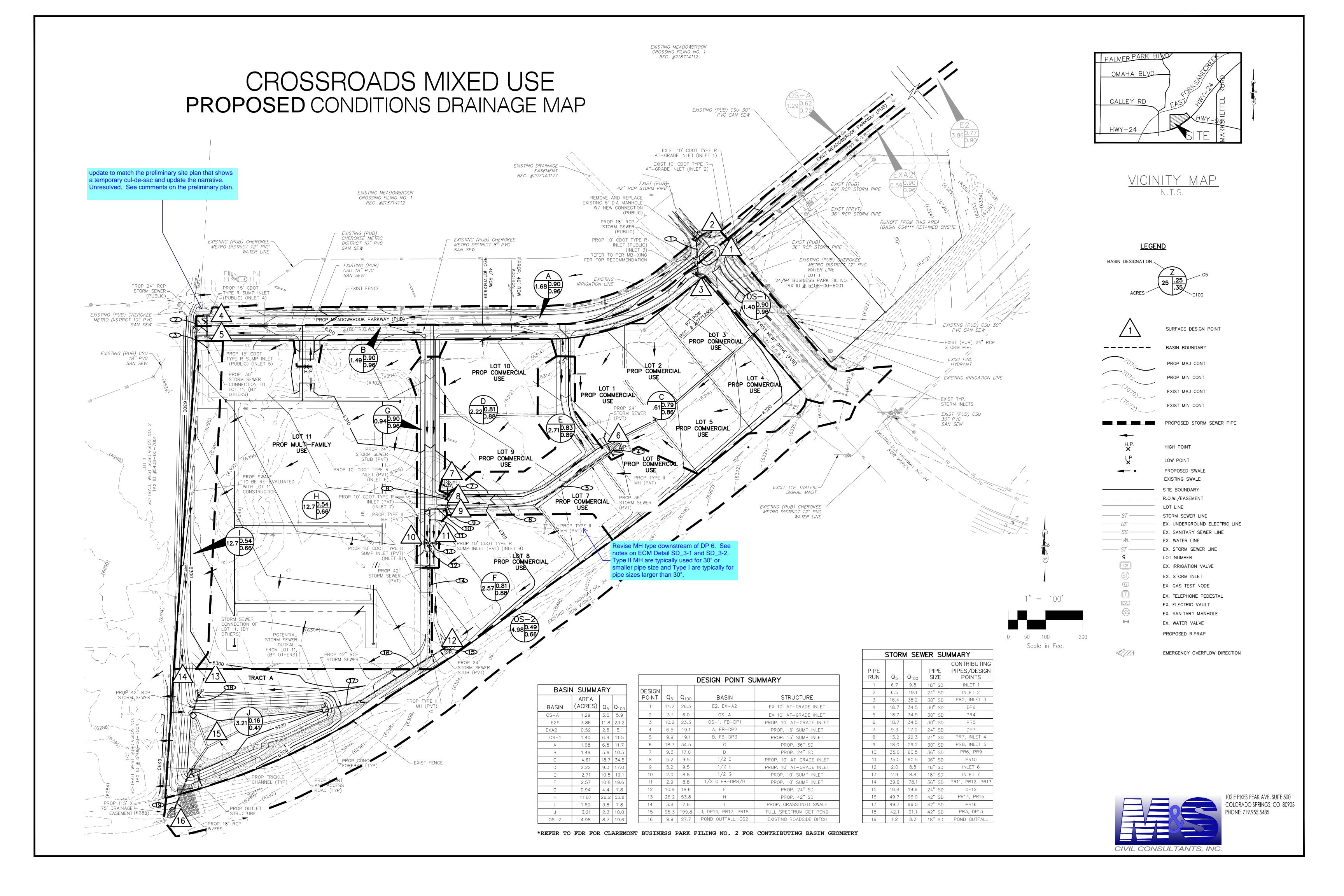
Revisions:

В

**DRAINAGE MAPS** 







# drainage V\_2 engr comments.pdf Markup Summary

## dsdlaforce (17)

Subject: Callout Page Label: 13 Author: dsdlaforce

Date: 4/14/2021 10:34:13 AM

Status: Color: Layer: Space:

identify the flow-by flow rate.



Subject: Callout Page Label: [1] DM Author: dsdlaforce

Date: 4/14/2021 10:46:32 AM

Status: Color: Layer: Space:

Revise MH type downstream of DP 6. See notes on ECM Detail SD\_3-1 and SD\_3-2. Type II MH are typically used for 30" or smaller pipe size and Type I are typically for pipe sizes larger than 30".



Subject: Line Page Label: 14 Author: dsdlaforce

Date: 4/14/2021 10:47:30 AM

Status: Color: Layer: Space:



Subject: Line Page Label: 14 Author: dsdlaforce

Date: 4/14/2021 10:47:40 AM

Status: Color: Layer: Space:

Subject: Callout Page Label: 14 Author: dsdlaforce

Date: 4/14/2021 10:47:52 AM

Status: Color: Layer: Space:

Delete duplicate



Subject: Callout Page Label: 15 Author: dsdlaforce

Date: 4/14/2021 10:51:39 AM

Status: Color: Layer: Space:

Include a narrative regarding the swale and lot 11

site plan



Subject: Image Page Label: 15 Author: dsdlaforce

Date: 4/14/2021 10:52:00 AM

Status: Color: Layer: Space:



ated to the full spectrum detention p Subject: Image Page Label: 14 Author: dsdlaforce

Date: 4/14/2021 10:53:16 AM

Status: Color: Layer: Space:

Subject: Callout Page Label: 14 Author: dsdlaforce

Date: 4/14/2021 10:53:25 AM

Status: Color: Layer: Space:

include a narrative regarding the following notes on the drainage map.



Subject: Cloud+ Page Label: 15

Author: dsdlaforce

Date: 4/14/2021 11:28:32 AM

Status: Color: Layer: Space:

This should be under DP3

Subject: Callout Page Label: 15 Author: dsdlaforce

Date: 4/14/2021 11:34:10 AM

Status: Color: Layer: Space:

update. Missing decimal point.

Subject: Image Page Label: 17 Author: dsdlaforce

Date: 4/14/2021 11:47:49 AM

Layer: Space:

Status: Color:

Subject: Callout Page Label: 17 Author: dsdlaforce

Date: 4/14/2021 11:48:52 AM

Status: Color: Layer: Space:

Subject: Text Box Page Label: 41 Author: dsdlaforce

Date: 4/14/2021 11:57:02 AM

Status: Color: Layer: Space:

NOTICE: Staff is only providing cursory review of the hydraulic calculations with the preliminary plan. Detailed review will be conducted with the Final

Drainage Report.

revise to 2021



Subject: Cloud+ Page Label: 44 Author: dsdlaforce

Date: 4/14/2021 12:49:39 PM

Status: Color: Revise. Must be at or below predevelopment. Unresolved.

Layer: Space:



Subject: Callout Page Label: [1] DM Author: dsdlaforce

Date: 4/14/2021 12:52:56 PM

Status: Color: Layer: Space:

update to match the preliminary site plan that shows a temporary cul-de-sac and update the narrative.

Unresolved. See comments on the preliminary

plan.



Subject: Cloud+ Page Label: 17 Author: dsdlaforce

Date: 4/14/2021 12:55:36 PM

Status: Color: Layer: Space:

Update. The unit cost are incorrect for Sand

Creek.