



The Cottages at Mesa Ridge Preliminary Drainage Report

December 2021

HR Green Project No: 200541
PCD File No. PUDSP2111

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The Cottages at Mesa Ridge Preliminary Drainage Report Project No.: 200541



▷ ENGINEER'S STATEMENT

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by El Paso County for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by negligent acts, errors, or omission on my part in preparing this report.

	Ken Huhn, PE	Date		
	Registered Professional	Engineer State of Cold	orado No	
	For and on behalf of HR	Green Development, I	LC	
D	DEVELOPER'S STATEME	NT		
	I, the developer, have re	ad and will comply with	n all of the requirements specified in this dra	ainage report and plan.
	Name of Developer		Authorized Signature	Date
	Printed Name	Title	Address	
	· ····································		/ (d. 1.000	
D	EL PASO COUNTY			
			e El Paso County Land Development Code	e, Drainage Criteria
	Manual, Volumes 1 and	2 and Engineering Crit	eria Manual, as amended.	
	Jennifer Irvine, P.E.			
	County Engineer/ECM A	dministrator		



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I. General Purpose, Location and Description

a. Purpose

The purpose of this Preliminary Drainage Report (PDR) is to describe the onsite and offsite drainage patterns, existing and proposed storm infrastructure, and the planned stormwater management for The Cottages at Mesa Ridge. This report will support the development plan that is currently in review with El Paso County.

b. Location

The Cottages at Mesa Ridge, referred to as 'the site' herein, is in a portion of the northeast quarter of section 29, the southeast quarter of section 20, the southwest quarter of section 21, and the northwest quarter of section 28, township 15 south, range 65 west of the 6th P.M., County of El Paso, Colorado. The site is bound by S. Powers Boulevard to the east, multi-family residential development to the south, single-family residential development to the west and undeveloped land to the north. Surrounding platted developments include Mesa Ridge Filing 8 and 9 to the south, Sunrise Ridge to the west and the Glen at Widefield to the east. A vicinity map is presented in Appendix A.

c. Description of Property

The site is approximately 10.22 acres of undeveloped land with existing vegetation consisting of native grasses. Once developed, the site will include 122 dwelling units, a club house and open space tracts. The site will be platted as a single lot. In general, the site slopes south towards the Fountain Mutual Irrigation Co canal. Onsite elevations range from 5750' - 5795' with slopes ranging 1 - 33%. Per a NRCS soil survey, the site is made up of Type B Stoneham sandy loam and Type B Nelson-Tassel fine sand loams. The NRCS soil survey is presented in Appendix A.

There are no major drainageways or irrigation facilities that traverse the site nor does the site fall within the Streamside Overlay Zone. Onsite, existing utilities include water, sewer, fiberoptic, underground gas and underground electric/telecommunication. An existing drainage map is presented in Appendix F.

d. Floodplain Statement

Based on FEMA Firm map 08041C0956G dated December 8, 2018, the site is Zone X, which are areas determined to be outside the 0.2% annual chance flood.

II. Drainage Basins and Subbasins

a. Major Basin Description

The site is located within West Fork Jimmy Camp Creek Drainage Basin. The site's drainage characteristics were previously studied in the following reports:

- 1. "West Fork Jimmy Camp Creek Drainage Basin Planning Study" prepared by Kiowa Engineering Corporation, October 2003, revised. .
- 2. "Master Development Drainage Plan Mesa Ridge Development" prepared by Kiowa Engineering Corporation, December 17, 2006. (2006 MDDP)
- 3. "Mesa Ridge Development Master Development Drainage Plan Update" prepared by Kiowa Engineering Corporation, January 15, 2013. (2013 MDDP)

In the 2006 MDDP, the site was identified as Basin 1040 and Basin 1030. Basin 1040 was planned to be routed to Detention Basin D (located within Mesa Ridge Subdivision Filing 8) while Basin 1030 was routed to



Detention Basin 1031 (located on the east side of S. Powers Boulevard adjacent to the site). The 2013 MDDP did not alter the planned detention scenario for the site.

b. Existing Subbasin Description

The site's existing drainage is split into five basins. An existing drainage map is presented in Appendix B. See below for existing basin descriptions:

Basin EX1 is 5.69 acres of undeveloped area and existing single family residential lots. Existing stormwater from this basin ($Q_5 = 2.5$ cfs $Q_{100} = 13.7$ cfs) is conveyed onsite to DP1.

Basin EX2 is 3.12 acres of undeveloped area and a portion of S. Powers Boulevard. Existing stormwater from this basin ($Q_5 = 4.2$ cfs $Q_{100} = 12.4$ cfs) follows historic drainage patterns to an existing roadside swale to DP2. The flow is captured in an existing area inlet at DP2 and conveyed underneath S. Powers Boulevard in a 24" RCP culvert to an existing, temporary sediment basin.

Basin EX3 is 1.46 acres of undeveloped area. Existing stormwater from this basin ($Q_5 = 1.6$ cfs $Q_{100} = 5.1$ cfs) is conveyed to the existing irrigation canal to DP3.

Basin EX4 is 0.28 acres of undeveloped area. Existing stormwater from this basin ($Q_5 = 0.1$ cfs $Q_{100} = 0.8$ cfs) is conveyed in an existing roadside swale to DP4.

Basin EX5 is 3.38 acres of undeveloped area and existing single family residential lots. Existing stormwater from this basin ($Q_5 = 2.8$ cfs $Q_{100} = 11.9$ cfs) flows offsite along the site's southern boundary at DP5.

c. Proposed Subbasin Description

The proposed site has been divided into 9 subbasins for analysis. All storm sewer and appurtenances are private. A drainage map has been presented in Appendix F. See below for basin descriptions:

Basin 1 is 3.56 acres of single-family residential lots, duplex homes, roadway and landscaping. Stormwater from this basin ($Q_5 = 7.6$ cfs $Q_{100} = 16.1$ cfs) is conveyed in curb and gutter to a 15' Type R on-grade inlet at DP1. Basin 1 stormwater is piped in proposed storm sewer along the north side of Landover Lane. From there, the flow is piped in an existing 48" culvert to the existing full spectrum detention pond (Basin D) for water quality and detention.

Basin 2 is 4.93 acres of single-family residential lots, duplex homes, roadway and landscaping. Stormwater from this basin ($Q_5 = 9.5$ cfs $Q_{100} = 20.3$ cfs) is conveyed in curb and gutter to a 15' Type R on-grade inlet at DP2. Basin 2 stormwater is piped in proposed storm sewer along the north side of Landover Lane. From there, the flow is piped in an existing 48" culvert to the existing full spectrum detention pond (Basin D) for water quality and detention.

Basin 3 is 3.03 acres of existing roadway (S. Powers Boulevard), a compacted breeze trail and undeveloped area. Stormwater from this basin ($Q_5 = 3.4$ cfs $Q_{100} = 9.7$ cfs) follows historic drainage patterns in an existing roadside swale to an existing Type C inlet at DP3. An existing 24" RCP culvert conveys to flow to an existing, temporary sediment basin. Per Section I.7.1.B.7 and I.7.1.B.9 of the EPCDCM Appendix I – Stormwater Quality Polic. Basin y and Procedures, Basin 3 will not be routed to a permanent stormwater control measure. The trail improvements associated with Basin 3 will not increase existing stormwater flows.

Basin 4 is 0.52 acres of landscaping and undeveloped area. Stormwater from this basin ($Q_5 = 0.4$ cfs $Q_{100} = 1.8$ cfs) follows historic drainage patterns towards the Fountain Irrigation Ditch at DP4. From there, flow is conveyed under S. Powers Blvd in an existing box culvert (size unknown) to an existing, temporary sediment



basin. Per Section I.7.1.B.7 and I.7.1.B.9 of the El Paso County Appendix I – Stormwater Quality Policy and Procedures, Basin 4 will not be routed to a permanent stormwater control measure. The basin will remain mostly undeveloped with a proposed trail and retaining wall. The trail and retaining wall improvements associated with Basin 4 will not increase existing stormwater flows.

Basin 5 is 1.50 acres of landscaping and a fire access road. Stormwater from this basin ($Q_5 = 2.1$ cfs $Q_{100} = 5.7$ cfs) is captured in a grass-lined swale and captured in a Type C inlet. Basin 5 stormwater is piped in proposed storm sewer along the north side of Landover Lane. From there, the flow is piped in an existing 48" culvert to the existing full spectrum detention pond (Basin D) for water quality and detention.

Basin 6 is 0.63 acres of undeveloped area. Stormwater from this basin ($Q_5 = 0.2$ cfs $Q_{100} = 1.2$ cfs) follows historic drainage patterns in an existing roadside swale along S. Powers Boulevard at DP6 and continues south along S. Powers. Per Section I.7.1.B.7 of the EPCDCM Appendix I – Stormwater Quality Policy and Procedures, Basin 6 will not be routed to a permanent stormwater control measure. The land disturbance associated with Basin 6 will not increase existing stormwater flows.

Basin 7 is 0.56 acres of landscaping and existing single family residential. Stormwater from this basin ($Q_5 = 0.4 \text{ cfs } Q_{100} = 1.8 \text{ cfs}$) follows historic drainage patterns towards DP7. From there, the flow continues into Mesa Ridge Subdivision Filing 8 where it is captured and detained in Basin D. See Basin 1040 from the Mesa Ridge Filing No. 8 FDR for additional detail.

Basin 8 is 0.24 acres of roadway. Stormwater from this basin ($Q_5 = 1.1$ cfs $Q_{100} = 2.0$ cfs) is conveyed in curb and gutter down Landover Lane to a 10' Type R inlet at DP8. Basin 8 stormwater is piped in proposed storm

sewer along the north side of Landover Lane. From there, the flow is piped in an expectate delete the stated date.

existing full spectrum detention pond (Basin D) for water quality and detention.

Basin 9 is 0.14 acres of roadway. Stormwater from this basin ($Q_5 = 0.7$ cfs $Q_{100} = 1$ adopted version" if you'd like and gutter down Landover Lane to a 10' Type R inlet at DP9. Basin 9 stormwater is but it is not necessary. There sewer along the north side of Landover Lane. From there, the flow is piped in an existing full spectrum detention pond (Basin D) for water quality and detention.

you may state "current adopted version" if you'd like but it is not necessary. There were no formal changes to the criteria on the date listed (10/31/18). This date listed on the Municode homepage is not reflective of an adopted change to the criteria and may

III. Drainage Design Criteria

a. Development Criteria Reference

Storm drainage analysis and design criteria for the project were taken from the "Di have been some formating EL Paso County, Colorado" Volumes 1 and 2 (EPCDCM), dated October 31, 2018 Changes of and Section 3.2.1 of Chapter 13 of the "Colorado Springs Drainage Criteria Manual" (CCSDCM), dated May 2014, as adopted by El Paso County, as well as the July 2019 El Paso County Engineering Criteria Manual update.

b. Hydrologic Criteria

Hydrologic data was obtained from the "City of Colorado Springs Drainage Criteria Manual – Chapter 6 Hydrology". Onsite drainage improvements are designed for the 5-year storm (minor event) and 100-year storm (major event) using rainfall values from CCSDCM Table 6-2 below. Runoff was calculated per CCSDCM Section 6.3.0 - Rational Method. Full spectrum pond design was completed using the latest version of Mile High Flood District's (MHFD) UD-Detention per CCSDCM Section 13.3.2.1 – Full Spectrum Detention in addition to CUHP v.2.0.1 and EPA-SWMM v.5.1. Detention pond allowable release rate will be limited to less than or equal to those noted in the 2013 Mesa Ridge MDDP.



Table 6-2: Rainfall Depths for Colorado Springs						
Return Period (yr)	5	100				
1-hr Rainfall Depth (in)	1.50	2.52				

IV. Drainage Facility Design

a. General Concept

Onsite stormwater will be conveyed via Type 5 curb and gutter to Type R inlets. Captured stormwater will be piped to and detained in an existing, full spectrum detention pond located in Mesa Ridge Filing 9 south of the site. The full spectrum detention pond will outfall at less than historic values to the east side of S. Powers Boulevard and to the site's historic outfall. See below section regarding the existing detention basin analysis and retrofit. The ultimate outfall for the site is Jimmy Camp Creek, south of Hale Reservoir.

b. Water Quality & Detention

The Cottages at Mesa Ridge will utilize the existing regional Full Spectrum Detention Basin D for water quality and detention. Detailed analysis performed with this Report indicates that in its existing condition, there is adequate 100-year volume in the Detention Basin D for development of The Cottages at Mesa Ridge site. However, there are some concerns regarding the detention pond drain times. See discussion below for details on the analysis completed on Detention Basin D.

This pond was included originally as flood control in the 2006 MDDP and was updated to provide Full Spectrum detention with the 2013 MDDP. In addition, the record drawings for the retrofit of the pond confirmed the use of an orifice plate to control the full spectrum volume. Record documents are titled: *Mesa Ridge Filings 8 & 9, Detention Basin 'D', Full Spectrum Detention Modifications, Final Design Drawings*, by Kiowa Engineering Corporation, dated October 2011. Both MDDPs show Basin 1040 routed to Full Spectrum Detention Basin D. However, the basin characteristics provided with the most recent MDDP included The Cottages at Mesa Ridge site as historic.

In order to confirm that the existing Full Spectrum Detention Basin D has capacity for development of The Cottages at Mesa Ridge, updated modeling with proposed basin 1040 characteristics is necessary.

Hydrology and hydraulics included with the previous MDDPs utilized HEC-1 software to determine peak runoff quantities at specific design points and routing elements. These HEC-1 models were not available for use, so an effort was made to update them to the more current HEC-HMS program. However, there were too many unknown variables with the program to get it to provide reliable results.

Current CCSDCM V.1 CH.6 1.4 Selecting Methods for Estimating Design Flows notes in part that:

- For more complex drainage basins and routing requirements, the HEC-HMS model or the EPA SWMM
 method is better suited but requires more experience and expertise to properly apply. The EPA SWMM
 method also provides hydrographs, reservoir routing, and the ability to evaluate runoff reduction practices
 in detail.
- If detention facilities are to be sized based on hydrograph routing, or if hydrograph information is desired for any other reason, the EPA SWMM or the NRCS method must be used.





Therefore, CUHP and EPA SWMM methodology were selected as appropriate modeling programs to confirm volumes and release rates for Full Spectrum Detention Basin D are in line with the intent of the previous MDDPs and current CCSDCM criteria.

CUHP

A new CUHP model was prepared streamlined with only the MDDP basins being updated at this time and major basins tributary to Full Spectrum Detention Basin D. This includes Basin 1040, 6001, 6005, 6010, 6011 and 6020. Basin parameters included in the CUHP as follows:

- Basin parameters for Basin 1040 were updated based on the most current design information available and correspond to the Rational Method calculations noted elsewhere in this report. The area to Basin 1040 increased from what was accounted for in the previous MDDPs.
- Basins 6001, 6005, 6010, 6011 and 6020 used area and length parameters taken directly from the HEC-1 noted above.
- Basins 6001, 6005, 6010, 6011 and 6020 utilized percent impervious estimated from existing asconstructed land uses.
- All basins used the standard depression storage and infiltration parameters for Hydrologic Soil Type B.

Rainfall data was taken from NOAA Atlas 14 Point Precipitation for a 60-minute (1-hour) recurrence interval depth, 100=2.74 in. The 1-hour point precipitation was chosen in part because the MHFD-Detention worksheet uses the 1-hour depth as an input parameter to run the CUHP program in the background. This allows a more accurate review of the existing pond by using consistent storms across both the CUHP and MHFD-Detention software.

Input parameters and results for the 100-year event are included with Appendix D.

EPA SWMM

Similar to the CUHP modeling, a simplified hydraulic routing model was prepared. In this case, the U.S. Environmental Protection Agency Stormwater Management Model (EPA SWMM) software was used for the proposed conditions with the development of The Cottages at Mesa Ridge.

The model includes a stage-storage curve for Pond D extracted directly from the pond grading shown on the 2011 Full Spectrum Detention Modifications Plan noted above. The proposed Pond D stage-release curve was developed through an iterative process, described more in depth below.

The other separate existing pond (Detention Basin 6002) which is tributary to Pond D provides storage for Basin 6001. Parameters for modeling Detention Basin 6002 were taken directly from the 2013 MDDP HEC-1. Additionally, EPA SWMM element routing parameters such as channel length and size were taken directly from the previous HEC-1 model with the exception of elevations (not used in HEC-1). For this a reasonable starting (downstream) elevation was used from the Pond D plans, and slope/length parameters from HEC-1 used to set all other upstream elevations. A back-check was completed to ensure resultant upstream elevations seem reasonable given rough elevations on 2013 MDDP Exhibit.

Input parameters and results for the 100-year event are included with Appendix D.



Full Spectrum Detention Basin D

MHFD-Detention worksheets were set up using updated total watershed area and percent imperviousness for several reasons, they include:

- To confirm the updated full spectrum volume required within Pond D. Note, because an inflow hydrograph will be used for the 100-year event only the resultant full spectrum volumes are relevant from this data.
- To review how the existing pond is functioning under the proposed condition by incorporating the as-built stage-storage and stage-release data into the workbook. Note, the release structure was surveyed to provide accurate structure parameters.
- To route the 100-year hydrograph developed in the CUHP and EPA SWMM through the provided pond volume and as-built release structure.

MHFD-Detention (as-built) results from routing the proposed 100-year hydrograph through the as-built pond volume and release structure indicate that there is adequate 100-year volume in the existing pond for development of The Cottages at Mesa Ridge site. However, results also indicate that the existing pond is exceeding drain time limitations noted in current MHFD criteria and Colorado Revised Statute 37-92-602(8).

To rectify the drain times discrepancy a separate MHFD-Detention (proposed) worksheet was set up matching the previously noted stage-storage curve and input hydrograph but altering the release structure (and corresponding stage-release curve). The drain times were revised by enlarging the orifice areas and updating the detention stages to correlate with the new Full Spectrum volume. Once the 100-year peak release rate was confirmed to be at or below the threshold established with the 2013 MDDP (223 cfs) the resultant stage-release curve was transferred back to the prepared SWMM and re-run to confirm the same results as found with the MHFD-Detention (proposed) analysis.

Key pond parameters from the 2011 Full Spectrum Detention Modifications Plan along with the values determined with this Preliminary Drainage Report are summarized below.

Full Spectrum Detention Basin D Summary								
	2011 Full Spectrum Modifications	As-Built Pond D without Modifications	As-Built Pond D with Proposed Modifications					
Tributary Area (acres)	not provided	98.8	98.8					
% Impervious (%)	not provided	48.8	48.8					
Full Spectrum Volume (acre-ft)	4.2	5.1	5.1					
Full Spectrum WSEL (ft)	5686.8	5687.2	5687.2					
Full Spectrum Drain Time (hrs)	not provided	> 120	73					
100-yr volume (acre-ft)	8.3	11.6	12.5					
Release Rate (cfs)	219	252	232					
100-yr WSEL (ft)	5690.2	5691.2	5691.7					
100-yr Drain Time (hrs)	not provided	> 120	70					



Conclusions from the analysis presented with this Report are that Full Spectrum Detention Basin D will function as intended in the proposed conditions taking into consideration the Basin 1040 changes (including increase in basin area) that will occur with development of The Cottages at Mesa Ridge. No modifications to the as-built volume are anticipated at this time. Minor modifications are expected to the release structure to bring the existing pond in conformance with current drain time and stage-storage requirements. The detailed extent of modifications to the existing structure will be provided with the Final Drainage Report as the project design progresses.

c. Inspection and Maintenance

An Inspection and maintenance manual will be provided with the Final Drainage Report. The manual will specify maintenance intervals and required actions to maintain the function of the extended detention basin and appurtenances.

d. Grading and Erosion Control Plan

Due to the project disturbance area, a separate Grading and Erosion Control plan will be required. The Grading and Erosion Control Plan will be submitted in conjunction with the Final Drainage Report and Construction Drawings.

e. Four Step Method to Minimize Adverse Impacts of Urbanization

Step 1 – Reducing Runoff Volumes: Roof drains will route across landscape areas and grass lined swales are used for stormwater conveyance, whenever possible to promote infiltration.

Step 2 – Treat and slowly release the WQCV: An existing, regional full spectrum detention pond provides water quality for the site. The WQCV is released over a period of 44 hours.

Step 3 – Stabilize stream channels: Drainage swales will be lined with non-erosive soils and permanently seeded to provide stabilization. If required due to erosive velocities, additional protection will be provided in the form of riprap lining and drop structures to reduce stormwater velocities and provide stabilization.

Step 4 – Consider the need for source controls: No industrial or commercial uses are proposed within this development and therefore no source controls are proposed.

f. Drainage and Bridge Fees

Cottages at Mesa Ridge is located within the West Fork Jimmy Camp Creek drainage basin. See below for drainage fees associated with The Cottages at Mesa Ridge development. Fees are due at time of platting.

2021 Drainage & Bridge Fees								
Impervious Acreage	Drainage Fee							
5.48	\$13,524	\$74,069						

g. Opinion of Probable Cost

We respectfully request that the engineer's opinion of probably cost be postponed until the Final Drainage Report.

Please also provide the bridge fee. The 2021 bridge fee for West Fork Jimmy Camp Creek is \$4001 per impervious acre.



V. Summary

The Cottages at Mesa Ridge development remains consistent with pre-development drainage conditions with the construction of the recommended drainage improvements. The proposed development will not adversely affect downstream stormwater infrastructure or surrounding developments. This report meets the latest El Paso County Drainage criteria and is in accordance with the Mesa Ridge MDDP.

VI. Drawings

Please refer to the appendices for vicinity and drainage basin maps.

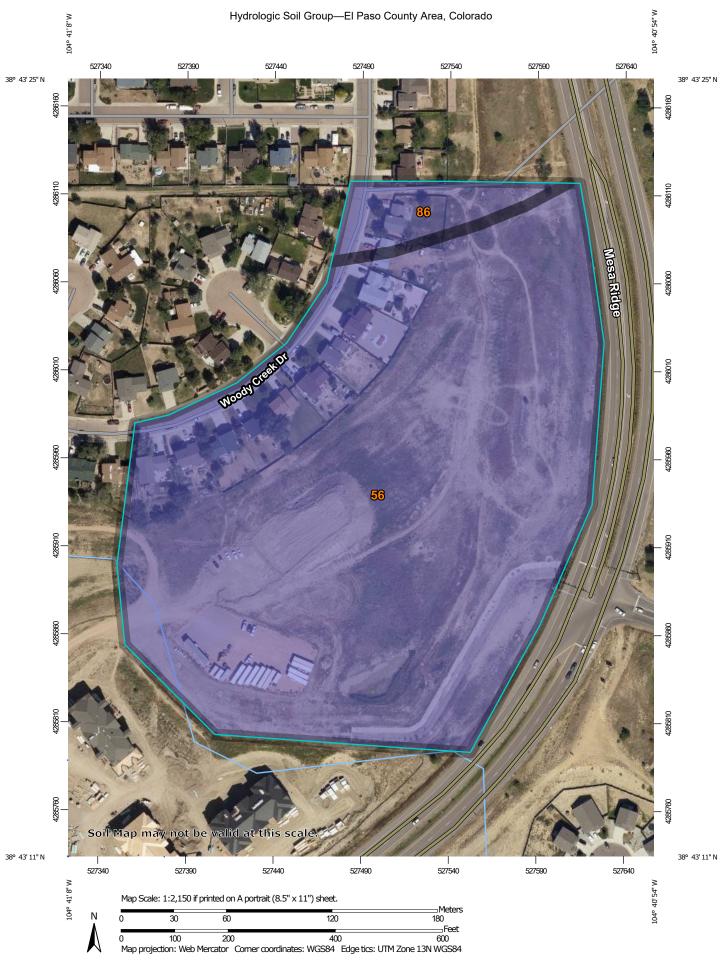
VII. References

- 1. City of Colorado Springs Drainage Criteria Manual, May 2014, Revised January 2021.
- 2. Urban Storm Drainage Criteria Manual, Mile High Flood District, January 2018.
- 3. *Master Development Drainage Plan Mesa Ridge Development*, Kiowa Engineering Corporation, December 17, 2006.
- 4. *Mesa Ridge Development Master Development Drainage Plan Update*, Kiowa Engineering Corporation, January 15, 2013.
- 5. *Mesa Ridge Filings* 8 & 9, *Detention Basin 'D'*, *Full Spectrum Detention Modifications, Final Design Drawings*, by Kiowa Engineering Corporation, October 2011.
- 6. Colorado Unit Hydrograph Procedure (CUHP), Version 2.0.1, October 2019.
- 7. Environmental Protection Agency Stormwater Management Model (EPA SWMM), Version 5.1, 2020.
- 8. Mile High Flood District Detention Basin Design Workbook (MHFD-Detention), Version 4.04, February 2021.





APPENDIX A - VICINITY MAP, SOIL MAP, FEMA MAP



MAP LEGEND MAP INFORMATION The soil surveys that comprise your AOI were mapped at Area of Interest (AOI) С 1:24.000. Area of Interest (AOI) C/D Soils Warning: Soil Map may not be valid at this scale. D Soil Rating Polygons Enlargement of maps beyond the scale of mapping can cause Not rated or not available Α misunderstanding of the detail of mapping and accuracy of soil **Water Features** line placement. The maps do not show the small areas of A/D Streams and Canals contrasting soils that could have been shown at a more detailed Transportation B/D Rails ---Please rely on the bar scale on each map sheet for map measurements. Interstate Highways C/D Source of Map: Natural Resources Conservation Service **US Routes** Web Soil Survey URL: D Major Roads Coordinate System: Web Mercator (EPSG:3857) Not rated or not available -Local Roads Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts Soil Rating Lines Background distance and area. A projection that preserves area, such as the Aerial Photography Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required. This product is generated from the USDA-NRCS certified data as of the version date(s) listed below. B/D Soil Survey Area: El Paso County Area, Colorado Survey Area Data: Version 17, Sep 13, 2019 Soil map units are labeled (as space allows) for map scales 1:50.000 or larger. Not rated or not available Date(s) aerial images were photographed: Aug 14, 2018—Sep 23. 2018 **Soil Rating Points** The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background A/D imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident. B/D

Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
56	Nelson-Tassel fine sandy loams, 3 to 18 percent slopes	В	15.6	94.7%
86	Stoneham sandy loam, 3 to 8 percent slopes	В	0.9	5.3%
Totals for Area of Intere	est	•	16.5	100.0%

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

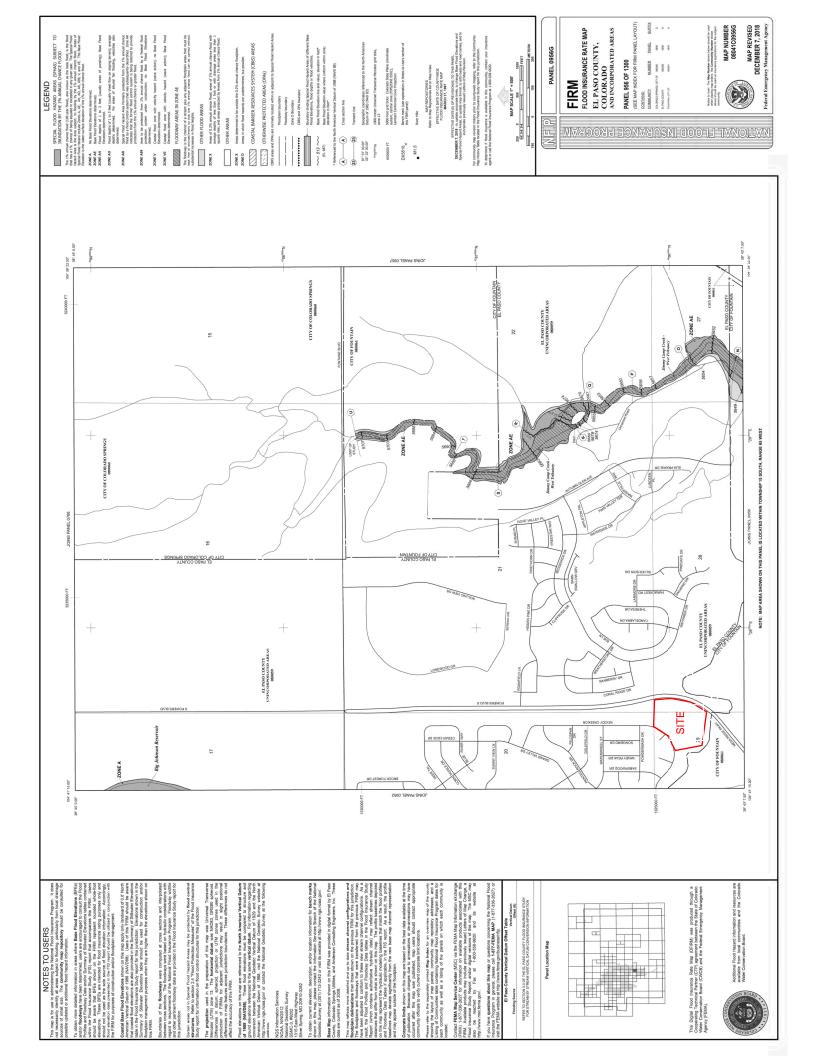
Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.







APPENDIX B - HYDROLOGIC CALCULATIONS

1433	COTTAGES AT MESA RIDGE	Calc'd by:		
	EXISTING CONDITIONS	Checked by:		
HRGreen	LOCATION: COLORADO SPRINGS, COLORADO	Date:	12/6/2021	

SUMMARY RUNOFF TABLE									
BASIN	AREA (ac)	Q ₅ (cfs)	Q ₁₀₀ (cfs)						
EX1	5.69	7	2.5	13.4					
EX2	3.12	28	3.5	10.0					
EX3	1.46	24	1.4	4.1					
EX4	0.28	2	0.1	0.5					
EX5	3.38	15	2.1	8.7					

DESIGN POINT SUMMARY TABLE									
DESIGN POINT	UPSTREAM BASIN	ΣQ ₅ (cfs)	ΣQ ₁₀₀ (cfs)						
1	EX1	2.5	13.4						
2	EX2	3.5	10.0						
3	3 EX3		4.1						
4	EX4	0.1	0.5						
5	EX5	2.1	8.7						



	COTTAGES AT MESA RIDGE	ИQJ	Calc'd by:
	EXISTING CONDITIONS		Checked by:
7	LOCATION: COLORADO SPRINGS, COLORADO	12/6/2021	Date:

	COMPOSITE 'C' FACTORS																	
BASIN	UNDEVELOPED	PAVED	SINGLE FAMILY LOT	TOTAL	SOIL	VDF					PAVE	D	SINC	SLE FA LOT	MILY	CO IMPERV	MPOSI IOUSNE	
		ACRI	ES		ITPE			%I	C ₅	C ₁₀₀	%I	C ₅	C ₁₀₀	%I	C ₅	C ₁₀₀		
EX1	5.25	0.00	0.44	5.69	В	2	0.09	0.36	100	0.90	0.96	65	0.45	0.59	7	0.12	0.38	
EX2	2.28	0.84	0.00	3.12	В	2	0.09	0.36	100	0.90	0.96	65	0.45	0.59	28	0.31	0.52	
EX3	1.13	0.33	0.00	1.46	В	2	0.09	0.36	100	0.90	0.96	65	0.45	0.59	24	0.27	0.50	
EX4	0.28	0.00	0.00	0.28	В	2	0.09	0.36	100	0.90	0.96	65	0.45	0.59	2	0.09	0.36	
EX5	2.70	0.00	0.68	3.38	В	2	0.09	0.36	100	0.90	0.96	65	0.45	0.59	15	0.16	0.41	
Total				13.93											15.30			



COTTAGES AT MESA RIDGE	Calc'd by:	NQJ
EXISTING CONDITIONS	Checked by:	
LOCATION: COLORADO SPRINGS, COLORADO	Date:	12/6/2021

TIME OF CONCENTRATION												
BAS	IN DATA		OVER	LAND TIM		TOTAL						
DESIGNATION	C ₅	AREA (ac)	LENGTH (ft)	SLOPE %	t _i (min)	C _V	LENGTH (ft)	SLOPE %	V (ft/s)	t _t (min)	t _c (min)	
EX1	0.12	5.69	100	25.0	6.2	10	750	3.2	1.8	7.0	13.1	
EX2	0.31	3.12	158	7.1	9.5	10	620	6.5	2.5	4.1	13.5	
EX3	0.27	1.46	25	25.0	2.6	20	520	0.1	0.6	13.7	16.3	
EX4	0.09	0.28	75	1.0	16.0	10	305	5.4	2.3	2.2	18.2	
EX5	0.16	3.38	42	1.8	9.2	10	440	4.2	2.0	3.6	12.7	



COTTAGES AT MESA RIDGE	Calc'd by:	NQJ
EXISTING CONDITIONS	Checked by:	
DESIGN STORM: 5-YEAR	Date:	12/6/2021

	101				DIR	ECT R		T	OTAL	RUNG	OFF	S	TREE	т		PIF	PΕ		TR	AVEL	TIME	REMARKS		
STREET	FNICO NO	DESIGN POINT	BASIN ID	AREA (ac)	C ₅	t _c (min)	C ₅ *A (ac)	/ (in./ hr.)	Q (cfs)	t _c (min)	C ₅ *A (ac)	/ (in./ hr.)	Q (cfs)	Q _{street} (cfs)	C ₅ *A (ac)	SLOPE %	Q _{PIPE} (cfs)	C ₅ *A (ac)	% alone	PIPE SIZE (in)	LENGTH (FT)	VEL. (FPS)	TRAVEL TIME (mir	
		1	EX1	5.69	0.12	13.1	0.67	3.72	2.5															
		_	->																					
	2	2	EX2	3.12	0.31	13.5	0.96	3.67	3.5															
		3	EX3	1.46	0.27	16.3	0.40	2.40	1 1															
		3	EV9	1.40	0.27	10.3	0.40	3.40	1.4															
	4	4	EX4	0.28	0.09	18.2	0.03	3.23	0.1															
		1					,,,,,																	
	Ę	5	EX5	3.38	0.16	12.7	0.55	3.77	2.1															
																					·			

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COTTAGES AT MESA RIDGE	Calc'd by:	ИQJ
PROPOSED CONDITIONS	Checked by	<u>.</u>
LOCATION: COLORADO SPRINGS, COLORADO	Date:	8/11/2021

SUMMARY RUNOFF TABLE												
BASIN	AREA (ac)	% IMPERVIOUS	Q ₅ (cfs)	Q ₁₀₀ (cfs)								
1	3.56	63	7.6	16.1								
2	4.93	59	9.5	20.3								
3	3.03	29	3.4	9.7								
4	0.52	8	0.4	1.8								
5	1.50	32	2.1	5.7								
6	0.63	2	0.2	1.2								
7	0.56	26	0.5	1.6								
8	0.24	100	1.1	2.0								
9	0.14	100	0.7	1.2								

DESIGN POINT SUMMARY TABLE													
DESIGN POINT	UPSTREAM BASIN	ΣQ ₅ (cfs)	ΣQ ₁₀₀ (cfs)										
1	1	7.6	16.1										
2	2	9.5	20.3										
2.1	3	15.6	29.9										
3	4	3.4	9.7										
4	5	0.4	1.8										
5	5	2.1	5.7										
6	6	0.2	1.2										
7	7	0.5	1.6										
8	8	1.1	2.0										
9	9	1.1	1.2										
9.1	8&9	17.1	39.6										



COTTAGES AT MESA RIDGE

PROPOSED CONDITIONS

HRGreen LOCATION: COLORADO SPRINGS, COLORADO

Calc'd by:
Checked by:

Date:

	COMPOSITE 'C' FACTORS																				
BASIN	LANDSCAPING	PAVED	ROOFS	SINGLE FAMILY	TOTAL	SOIL	LAN	DSCA	PING	I	PAVED			ROOF	S	SIN	IGLE FAM	IILY	IMPERV	MPOSI IOUSNE	
			ACRES			ITPE	% I	C ₅	C ₁₀₀	% I	C ₅	C ₁₀₀	%I	C ₅	C ₁₀₀	%I	C ₅	C ₁₀₀	%I	C ₅	C ₁₀₀
1	0.86	1.38	0.66	0.66	3.56	В	2	0.09	0.36	100	0.90	0.96	90	0.73	0.81	40	0.30	0.50	63	0.56	0.70
2	1.76	1.69	1.21	0.27	4.93	В	2	0.09	0.36	100	0.90	0.96	90	0.73	0.81	40	0.30	0.50	59	0.54	0.68
3	2.19	0.84	0.00	0.00	3.03	В	2	0.09	0.36	100	0.90	0.96	90	0.73	0.81	40	0.30	0.50	29	0.31	0.53
4	0.49	0.03	0.00	0.00	0.52	В	2	0.09	0.36	100	0.90	0.96	90	0.73	0.81	40	0.30	0.50	8	0.14	0.39
5	1.04	0.46	0.00	0.00	1.50	В	2	0.09	0.36	100	0.90	0.96	90	0.73	0.81	40	0.30	0.50	32	0.34	0.54
6	0.63	0.00	0.00	0.00	0.63	В	2	0.09	0.36	100	0.90	0.96	90	0.73	0.81	40	0.30	0.50	2	0.09	0.36
7	0.21	0.00	0.00	0.35	0.56	В	2	0.09	0.36	100	0.90	0.96	90	0.73	0.81	40	0.30	0.50	26	0.22	0.45
8	0.00	0.24	0.00	0.00	0.24	В	2	0.09	0.36	100	0.90	0.96	90	0.73	0.81	40	0.30	0.50	100	0.90	0.96
9	0.00	0.14	0.00	0.00	0.14	В	2	0.09	0.36	100	0.90	0.96	90	0.73	0.81	40	0.30	0.50	100	0.90	0.96
Pond					11.56														54		
Total					15.11																



COTTAGES AT MESA RIDGE	Calc'd by:	NQJ
PROPOSED CONDITIONS	Checked by:	
LOCATION: COLORADO SPRINGS, COLORADO	Date:	8/10/2021

TIME OF CONCENTRATION OVERLAND TIME (T_i) **BASIN DATA** TRAVEL TIME (T_t) **TOTAL** AREA (ac) LENGTH (ft) SLOPE % t_i (min) LENGTH (ft) SLOPE % V (ft/s) t_c (min) DESIGNATION C_5 C_V t_t (min) 0.56 3.56 100 2.0 7.8 20 900 2.9 3.4 4.4 12.2 4.93 100 20 3.2 2 0.54 2.0 8.2 1160 2.5 6.1 14.3 9.2 3 0.31 3.03 65 2.0 10 715 6.0 2.4 4.9 14.1 0.14 0.52 22 25.0 2.8 20 92 9.0 6.0 0.3 5.0 4 5 0.34 1.50 54 25.0 3.5 10 260 0.5 0.7 6.1 9.6 0.63 70 15.5 380 5.5 2.3 18.2 6 0.09 1.0 10 2.7 0.22 0.56 58 2.0 9.7 10 260 3.0 1.7 2.5 12.2 7 8 0.90 0.24 16 2.0 1.2 20 270 9.0 6.0 0.8 5.0 1.2 6.0 5.0 9 0.90 0.14 16 2.0 20 270 9.0 8.0



COTTAGES AT MESA RIDGE	Calc'd by:	NQJ
PROPOSED CONDITIONS	Checked by:	
DESIGN STORM: 5-YEAR	Date:	8/10/2021

ПК	<u> </u>	en																					
				DIR	ECT F	RUNOF	F		TO	TAL	RUNO	FF	S	TREE	ΞT		PIF	PE		TI	RAVEL	. TIME	REMARKS
STREET	DESIGN POINT	BASIN ID	AREA (ac)	Cs	t _c (min)	C ₅ *A (ac)	/ (in./ hr.)	Q (cfs)	t _c (min)	C ₅ *A (ac)	/ (in./ hr.)	Q (cfs)	Q _{street} (cfs)	C ₅ *A (ac)	SLOPE %	Q _{PIPE} (cfs)	C ₅ *A (ac)	% HODE %	PIPE SIZE (in)	LENGTH (FT)	VEL. (FPS)	TRAVEL TIME (min)	
																7.4	1.93	9.0	18.0	16	21.6	0.01	BASIN 1 FLOW CAPTURED IN 15' TYPE R INLET (ON GRADE)
	1	1	3.56	0.56	12.2	2.00	3.83	7.6					0.2	0.07	2.0					280		1.65	DP1 FLOW BY, C&G FLOW TO DP8
																8.7	2.42	9.0	18.0	16	21.6	0.01	BASIN 2 FLOW CAPTURED IN 15' TYPE R INLET (ON GRADE)
	2	2	4.93	0.54	14.3	2.64	3.59	9.5					0.8	0.22	2.0					280	2.8	1.65	DP2 FLOW BY, C&G FLOW TO DP9
	3	3	3.03	0.31	14.1	0.95	3.62	3.4															BASIN 3 FLOW, SWALE FLOW TO EX TYPE C INLET @ DP3
	4	4	0.52	0.14	5.0	0.07	5.17	0.4															BASIN 4 FLOW, FOLLOW HISTORIC DRAINAGE PATTERNS TO DP4
	5	5	1.5	0.34	9.6	0.51	4.18	2.1								2.1	0.51	0.5	18.0	536	5.1	1.75	BASIN 5 FLOW @ DP5, CAPTURED IN TYPE C INLET, PIPE TO DP2.1
	2.1			0.01	0.0	0.01			14.3	4.36	3.59	15.6				15.6	4.36	9.0	18.0	280	21.6	0.22	COMBINED DP1 & DP2 FLOW, PIPE TO DP9.1
	6	6	0.63	0.09	18.2	0.06	3.23	0.2															BASIN 6 FLOW @ DP6, FOLLOWS HISTORIC DRAINAGE PATTERNS
	7	7	0.56	0.22	12.2	0.12	3.83	0.5															BASIN 7 FLOW @ DP7, FOLLOWS HISTORIC DRAINAGE PATTERNS
	8	8	0.24	0.90	5.0	0.22			13.9	0.28	3 64	1.0				1.0	0.28	2.0	18.0	16	10.2	0.03	BASIN 8 AND DP1 FLOW BY, CAPTURED IN 10' TYPE R INLET (ON GRADE) DP8 FLOW BY, C&G FLOW TO LANDOVER LANE
	9	9	0.14	0.90	5.0					0.35		1.2				1.2	0.35	2.0	18.0	16	10.2	0.03	BASIN 9 AND DP2 FLOW BY, CAPTURED IN 10' TYPE R INLET (ON GRADE) DP9 FLOW BY, C&G FLOW TO LANDOVER LANE
	9	Э	0.14	0.90	5.0	0.13	5.17	0.7	10.0	0.35	3.43	1.2								l	1		DF9 FLOW B1, CAG FLOW TO LANDOVER LANE
	9.1								16.0	4.98	3.42	17.1											COMBINED DP2.1, DP8 DP9 FLOW, PIPE TO EX DETENTION POND D



COTTAGES AT MESA RIDGE	Calc'd by:	NQJ
PROPOSED CONDITIONS	Checked by:	
DESIGN STORM: 100-YEAR	Date:	8/10/2021

				DII	RECT	RUNOI	F		TO	TAL F	RUNO	FF	S	TREE	ΞT		PII	PE		TRAVEL TIME			REMARKS		
STREET	DESIGN POINT	BASIN ID	AREA (ac)	C ₁₀₀	t _c (min)	C ₁₀₀ *A (ac)	/ (in./ hr.)	Q (cfs)	t_c (min)	C ₁₀₀ *A (ac)	/ (in./ hr.)	Q (cfs)	Q _{street} (cfs)	C ₁₀₀ *A (ac)	SLOPE %	Q _{PIPE} (cfs)	C ₁₀₀ *A (ac)	% SCOPE %	PIPE SIZE (ft)	LENGTH (ft)	VEL. (ft/s)	TRAVEL TIME (min)			
																12.1	1.88		18.0		10.2	0.03	BASIN 1 FLOW CAPTURED IN 15' TYPE R INLET (ON GRADE)		
	1	1	3.56	0.70	12.2	2.50	6.42	16.1					4.0	0.62	9.0					280	6.0	0.78	DP1 FLOW BY, C&G FLOW TO DP8		
																	2.26	2.0	18.0		10.2	0.03	BASIN 2 FLOW CAPTURED IN 15' TYPE R INLET (ON GRADE)		
	2	2	4.93	0.68	14.3	3.37	6.03	20.3					6.7	1.11	9.0					280	6.0	0.78	DP2 FLOW BY, C&G FLOW TO DP9		
	3	3	3.03	0.53	14.1	1.59	6.07	9.7															BASIN 3 FLOW, SWALE FLOW TO EX TYPE C INLET @ DP3		
	4	4	0.52	0.39	5.0	0.21	8.68	1.8															BASIN 4 FLOW, FOLLOW HISTORIC DRAINAGE PATTERNS TO DP4		
																5.7	0.82	0.5	18.0	536	5.1	1.75	BASIN 5 FLOW @ DP5, CAPTURED IN TYPE C INLET, PIPE TO DP2.1		
	5	5	1.5	0.54	9.6	0.82	7.03	5.7																	
	2.1								14.3	4.96	6.02	29.9				29.9	4.96	9.0	18.0	280	21.6	0.22	COMBINED DP1 & DP2 FLOW, PIPE TO DP9.1		
	2.1								14.5	4.30	0.02	23.3													
	6	6	0.63	0.36	18.2	0.23	5.42	1.2															BASIN 6 FLOW @ DP6, FOLLOWS HISTORIC DRAINAGE PATTERNS		
	7	7	0.56	0.45	12.2	0.25	6.42	1.6															BASIN 7 FLOW @ DP7, FOLLOWS HISTORIC DRAINAGE PATTERNS		
																	0.77	9.0	18.0	16	21.6	0.01	BASIN 8 AND DP1 FLOW BY, CAPTURED IN 10' TYPE R INLET (ON GRADE)		
	8	8	0.24	0.96	5.0	0.23	8.68	2.0	13.0	0.85	6.27	5.3	0.5	0.08	9.0								DP8 FLOW BY, C&G FLOW TO LANDOVER LANE		
																	1.00	9.0	18.0	16	21.6	0.01	BASIN 9 AND DP2 FLOW BY, CAPTURED IN 10' TYPE R INLET (ON GRADE)		
	9	9	0.14	0.96	5.0	0.13	8.68	1.2	15.1	1.25	5.89	7.4	1.5	0.25	9.0						ļ		DP9 FLOW BY, C&G FLOW TO LANDOVER LANE		
	9.1								15.1	6.72	5.89	39.6											COMBINED DP2.1, DP8 DP9 FLOW, PIPE TO EX DETENTION POND D		
							1																		
							l																		





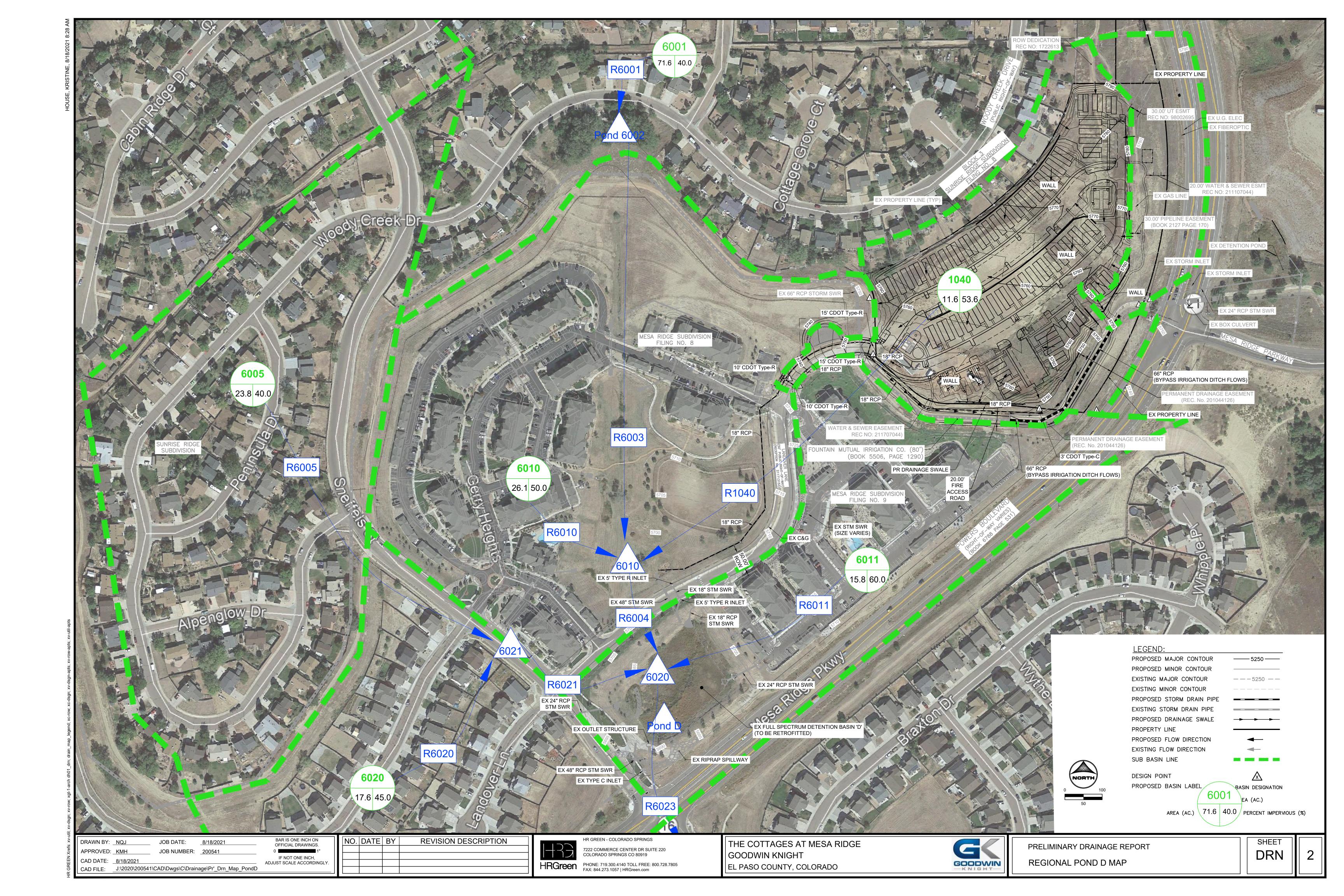
APPENDIX C - HYDRAULIC CALCULATIONS*

* HYDRAULIC CALCULATIONS INCLUDING INLET, STREET CAPACITY AND HYDRAULIC MODELING WILL BE INCLUDED WITH THE FINAL DRAINAGE REPORT.





APPENDIX D - WATER QUALITY & DETENTION



Columns with this color heading are for required user-input Columns with this color heading are for optional override values Columns with this color heading are for program-calculated value

								(Watershe	ed inches)	Parameters			DCIA	
Subcatchment	EPA SWMM		Area	Length to	Length		Percent			Initial Rate	Coefficient	Rate	Level 0, 1, or	
Name	Target Node	Raingage	(mi²)	Centroid (mi)	(mi)	Slope (ft/ft)	Imperviousness	Pervious	Impervious	(in/hr)	(1/seconds)	(in/hr)	2	Comment
6001	E6001	100-YR	0.1120	0.2178	0.4356	0.0120	40.0	0.35	0.1	4.5	0.0018	0.6	0	
6005	E6005	100-YR	0.0362	0.0786	0.2235	0.0300	40.0	0.35	0.1	4.5	0.0018	0.6	0	
6010	E6010	100-YR	0.0433	0.1009	0.2216	0.0490	50.0	0.35	0.1	4.5	0.0018	0.6	0	Updated imperviousness to include open space
6011	E6011	100-YR	0.0267	0.1621	0.3136	0.0362	60.0	0.35	0.1	4.5	0.0018	0.6	0	
6020	E6020	100-YR	0.0300	0.1345	0.2083	0.0504	45.0	0.35	0.1	4.5	0.0018	0.6	0	Updated to single-family imperviousness
1040	E1040	100-YR	0.0181	0.0758	0.1894	0.0220	53.6	0.35	0.1	4.5	0.0018	0.6	0	Updated for new size and imperviousness

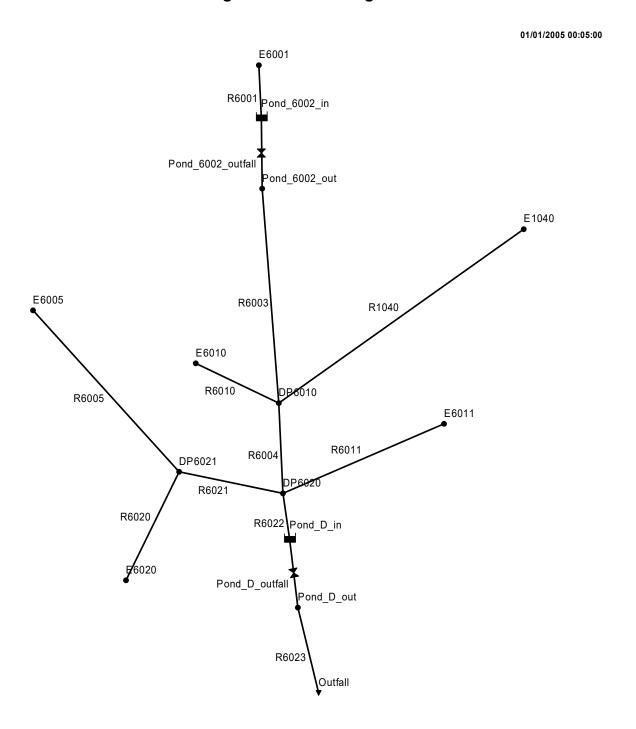
Maximum Depression Storage

Horton's Infiltration

Summary of Unit Hydrograph Parameters Used By Program and Calculated Results (Version 2.0.1)

				Uni	it Hydrogra _l	ph Paramet	ers and Res	ults			Excess Precip.		Storm Hydrograph			
Catchment Name/ID	User Comment for Catchment	СТ	Ср	W50 (min.)	W50 Before Peak	W75 (min.)	W75 Before Peak	Time to Peak (min.)	Peak (cfs)	Volume (c.f)	Excess (inches)	Excess (c.f.)	Time to Peak (min.)	Peak Flow (cfs)	Total Volume (c.f.)	Runoff per Unit Area (cfs/acre)
6,001		0.094	0.178	23.1	3.45	12.0	2.44	5.7	146	260,198	2.09	542,819	40.0	173	542,806	2.41
6,005		0.094	0.107	13.7	1.42	7.1	1.01	2.4	79	84,100	2.09	175,447	36.0	77	175,455	3.32
6,010	Updated imperviousness to include open space	0.089	0.131	10.5	1.36	5.5	0.96	2.3	123	100,595	2.22	223,481	35.0	110	223,473	3.96
6,011		0.084	0.115	18.3	1.91	9.5	1.35	3.2	44	62,029	2.36	146,231	37.0	51	146,214	2.99
6,020	Updated to single-family imperviousness	0.091	0.105	15.0	1.51	7.8	1.07	2.5	60	69,696	2.15	150,108	36.0	62	150,075	3.21
1,040	Updated for new size and imperviousness	0.087	0.092	14.5	1.32	7.5	0.93	2.2	37	42,050	2.27	95,468	36.0	39	95,489	3.36

The Cottages at Mesa Ridge



SWMM 5.1 Page 1

EPA STORM WATER MANAGEMENT MODEL - VERSION 5.1 (Build 5.1.012) _____

WARNING 04: minimum elevation drop used for Conduit R6022

************** ${\tt NOTE:}$ The summary statistics displayed in this report are based on results found at every computational time step,

not just on results from each reporting time step.

Analysis Options

Flow Units CFS Process Models: Rainfall/Runoff NO RDII NO Snowmelt NO Groundwater NO

Flow Routing YES Ponding Allowed NO Water Quality NO

Flow Routing Method KINWAVE

Starting Date 01/01/2005 00:00:00 Ending Date 01/01/2005 12:00:00

Antecedent Dry Days 0.0 Report Time Step 00:05:00 Routing Time Step 60.00 sec

*******	Volume	Volume
Flow Routing Continuity	acre-feet	10^6 gal

Dry Weather Inflow	0.000	0.000
Wet Weather Inflow	0.000	0.000
Groundwater Inflow	0.000	0.000
RDII Inflow	0.000	0.000
External Inflow	30.612	9.975
External Outflow	25.293	8.242
Flooding Loss	0.000	0.000
Evaporation Loss	0.000	0.000
Exfiltration Loss	0.000	0.000
Initial Stored Volume	0.000	0.000
Final Stored Volume	5.306	1.729
Continuity Error (%)	0.042	

Highest Flow Instability Indexes

All links are stable.

****** Routing Time Step Summary *******

Minimum Time Step : 60.00 sec
Average Time Step : 60.00 sec
Maximum Time Step : 60.00 sec
Percent in Steady State : 0.00
Average Iterations per Step : 1.13
Percent Not Converging : 0.00

****** Node Depth Summary

Node	Туре	Average Depth Feet	Maximum Depth Feet	Maximum HGL Feet	Occu	of Max rrence hr:min	Reported Max Depth Feet
E6005	JUNCTION	0.14	1.79	5715.48	0	00:37	1.76
E6010	JUNCTION	0.00	0.00	5693.19	0	00:00	0.00
E6001	JUNCTION	0.00	0.00	5750.46	0	00:00	0.00
E1040	JUNCTION	0.04	0.53	5732.80	0	00:37	0.53
E6011	JUNCTION	0.00	0.00	5688.69	0	00:00	0.00
E6020	JUNCTION	0.00	0.00	5691.39	0	00:00	0.00

DP6010	JUNCTION	0.48	3.14	5691.33	0	00:42	3.08
DP6021	JUNCTION	0.18	2.13	5693.32	0	00:37	2.09
DP6020	JUNCTION	0.48	3.14	5686.83	0	00:42	3.06
Pond D out	JUNCTION	0.18	1.06	5683.65	0	01:13	1.06
Pond 6002 out	JUNCTION	0.18	1.25	5749.71	0	00:59	1.24
Outfall	OUTFALL	0.18	1.06	5673.90	0	01:13	1.06
Pond 6002 in	STORAGE	4.90	9.61	5759.07	0	00:59	9.61
Pond D in	STORAGE	5.06	9.34	5693.03	0	01:13	9.32

Node Inflow Summary

		Maximum	Maximum			Lateral	Total	Flow
		Lateral	Total	Time	of Max	Inflow	Inflow	Balance
		Inflow	Inflow	0ccu	rrence	Volume	Volume	Error
Node	Type	CFS	CFS	davs	hr:min	10^6 gal	10^6 gal	Percent
E6005	JUNCTION	76.91	76.91	0	00:37	1.31	1.31	0.000
E6010	JUNCTION	109.76	109.76	0	00:36	1.67	1.67	0.000
E6001	JUNCTION	172.95	172.95	0	00:41	4.06	4.06	0.000
E1040	JUNCTION	38.88	38.88	0	00:37	0.714	0.714	-0.000
E6011	JUNCTION	51.06	51.06	0	00:38	1.09	1.09	0.000
E6020	JUNCTION	61.62	61.62	0	00:37	1.12	1.12	0.000
DP6010	JUNCTION	0.00	231.62	0	00:42	0	6.26	0.000
DP6021	JUNCTION	0.00	138.54	0	00:37	0	2.43	0.000
DP6020	JUNCTION	0.00	412.18	0	00:41	0	9.79	0.000
Pond D out	JUNCTION	0.00	233.78	0	01:13	0	8.24	0.000
Pond 6002 out	JUNCTION	0.00	136.68	0	00:59	0	3.87	0.000
Outfall	OUTFALL	0.00	233.77	0	01:13	0	8.24	0.000
Pond 6002 in	STORAGE	0.00	172.95	0	00:41	0	4.06	0.152
Pond_D_in	STORAGE	0.00	412.18	0	00:41	0	9.79	0.048

No nodes were flooded.

Storage Unit	Average Volume 1000 ft3	Avg Pcnt Full	Pcnt	Exfil Pcnt Loss	Maximum Volume 1000 ft3	Max Pcnt Full	Time of Max Occurrence days hr:min	Maximum Outflow CFS
Pond_6002_in Pond D in	45.849 246.767	16 32	0	0	126.976 548.176	45 70	0 00:59 0 01:13	136.68 233.78

	Flow	Avg Flow	Max Flow	Total Volume								
	Freq											
Outfall Node	Pcnt	CFS	CFS	10^6 gal								
Outfall	97.92	26.05	233.77	8.242								
System	97.92	26.05	233.77	8.242								

****** Link Flow Summary **********

Link	Туре	Maximum Flow CFS	Occu	of Max errence hr:min	Maximum Veloc ft/sec	Max/ Full Flow	Max/ Full Depth
R1040	CONDUIT	38.58	0	00:38	6.04	0.01	0.11
R6003	CONDUIT	136.55	0	01:01	8.00	0.06	0.25
R6004	CONDUIT	231.40	0	00:42	19.56	0.83	0.70
R6005	CONDUIT	76.92	0	00:37	17.52	0.67	0.60
R6011	DUMMY	51.06	0	00:38			
R6010	DUMMY	109.76	0	00:36			
R6021	CONDUIT	138.54	0	00:37	20.33	0.56	0.53
R6020	DUMMY	61.62	0	00:37			
R6001	DUMMY	172.95	0	00:41			
R6022	DUMMY	412.18	0	00:41			
R6023	CONDUIT	233.77	0	01:13	18.44	0.10	0.18
Pond 6002 outfall	DUMMY	136.68	0	00:59			
Pond_D_outfall	DUMMY	233.78	0	01:13			

****** Conduit Surcharge Summary

No conduits were surcharged.

Analysis begun on: Tue Aug 17 14:10:59 2021 Analysis ended on: Tue Aug 17 14:10:59 2021 Total elapsed time: < 1 sec

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.04 (February 2021)

pond bottom

5682.4

Optional User Overrides acre-feet acre-feet

inches

inches

inches

inches

inches

inches

inches

1.00

1.28

1.55

1.97

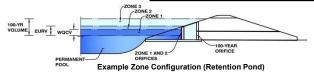
2.34

2.74

3.84

Project: Mesa Ridge Cottages

Basin ID: Existing Pond D Sizing Confirmation



Watershed Information

Selected BMP Type =	EDB	
Watershed Area =	98.80	acres
Watershed Length =	4,090	ft
Watershed Length to Centroid =	2,000	ft
Watershed Slope =	0.035	ft/ft
Watershed Imperviousness =	48.80%	percent
Percentage Hydrologic Soil Group A =	0.0%	percent
Percentage Hydrologic Soil Group B =	100.0%	percent
Percentage Hydrologic Soil Groups C/D =	0.0%	percent
Target WQCV Drain Time =	40.0	hours
Location for 1-hr Rainfall Depths =	User Input	

After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

the embedded Colorado Urban Hydrograph Procedure.								
1.671	acre-feet							
5.144	acre-feet							
3.741	acre-feet							
5.462	acre-feet							
7.357	acre-feet							
11.295	acre-feet							
14.367	acre-feet							
18.116	acre-feet							
27.672	acre-feet							
3.247	acre-feet							
4.538	acre-feet							
6.263	acre-feet							
7.639	acre-feet							
8.436	acre-feet							
9.873	acre-feet							
	1.671 5.144 3.741 5.462 7.357 11.295 14.367 18.116 27.672 3.247 4.538 6.263 7.639 8.436							

Define Zones and Basin Geometry

Zone 1 Volume (User Defined) =	5.14	acre-feet
Zone 2 Volume (User Defined - Zone 1) =	0.32	acre-feet
Zone 3 Volume (User Defined - Zones 1 & 2) =	6.10	acre-feet
Total Detention Basin Volume =	11.57	acre-feet

				5-Yr	5687.40	5.00	5.46	
Depth Increment =		ft		100-YR	5691.16	8.76	11.57	
		Optional				Optional		T
Stage - Storage	Stage (ft)	Override Stage (ft)	Length (ft)	Width (ft)	Area (ft 2)	Override Area (ft ²)	Area (acre)	

Elevation

EURV (FSV) 5687.18

Stage

4.78

Volume

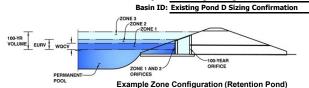
5.14

Depth Increment =		ft		100-YR	5691.16	8.76	11.57		
		Optional				Optional			
Stage - Storage	Stage	Override	Length	Width	Area	Override	Area	Volume	Volume
Description	(ft)	Stage (ft)	(ft)	(ft)	(ft ²)	Area (ft 2)	(acre)	(ft ³)	(ac-ft)
Top of Micropool		0.00				0	0.000		
5684.00		1.60				50,745	1.165	40,595	0.932
5685.00		2.60				55,231	1.268	93,583	2.148
5686.00		3.60				58,662	1.347	150,529	3.456
5687.00		4.60				64,191	1.474	211,956	4.866
5688.00		5.60				67,213	1.543	277,658	6.374
5689.00		6.60				70,292	1.614	346,410	7.952
5690.00		7.60				73,458	1.686	418,285	9.603
5691.00		8.60				73,831	1.695	491,930	11.293
5692.00		9.60				80,094	1.839	568,892	13.060
5693.00		10.60				83,415	1.915	650,647	14.937
5694.00		11.60				87,173	2.001	735,941	16.895
		-						-	

DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.04 (February 2021)

Project: Mesa Ridge Cottages



	Estimated	Estimated	
	Stage (ft)	Volume (ac-ft)	Outlet Type
Zone 1 (User)	4.79	5.144	Orifice Plate
Zone 2 (User)	5.01	0.318	Orifice Plate
Zone 3 (User)	8.76	6.104	Weir&Pipe (Rect.)
•	Total (all zones)	11.566	

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth = ft (distance below the filtration media surface) Underdrain Orifice Diameter = inches

	Calculated Parameters for Underdrain				
Underdrain Orifice Area =		ft ²			
Underdrain Orifice Centroid =		feet			

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice = ft (relative to basin bottom at Stage = 0 ft) 0.00 Depth at top of Zone using Orifice Plate = 4.46 ft (relative to basin bottom at Stage = 0 ft) Orifice Plate: Orifice Vertical Spacing = N/A inches Orifice Plate: Orifice Area per Row = N/A inches

Calculated Parame	ters for Plate
N/A	ft ²
N/A	feet
N/A	feet
N/A	ft ²
	N/A N/A

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.85	1.19	1.52	1.85	2.19	2.52	2.85	3.19
Orifice Area (sq. inches)	3.93	3.93	3.93	3.93	3.93	3.93	3.93	3.93

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)		0.00	0.00	0.00	0.00	0.00	0.00	0.00
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

	Not Selected	Not Selected
Invert of Vertical Orifice =	N/A	N/A
Depth at top of Zone using Vertical Orifice =	N/A	N/A
Vertical Orifice Diameter =	N/A	N/A

Not Selected ft (relative to basin bottom at Stage = 0 ft) Vertical Orifice Area N/A ft (relative to basin bottom at Stage = 0 ft) Vertical Orifice Centroid = inches

User Input: Overflow Weir (Dropbox with Flat o	Calculated Parameters for Overflow Weir					
	Zone 3 Weir	Not Selected		Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	4.46	N/A	ft (relative to basin bottom at Stage = 0 ft) Height of Grate Upper Edge, H_t =	6.46	N/A	feet
Overflow Weir Front Edge Length =	12.00	N/A	feet Overflow Weir Slope Length =	6.32	N/A	feet
Overflow Weir Grate Slope =	3.00	N/A	H:V Grate Open Area / 100-yr Orifice Area =	3.34	N/A	
Horiz. Length of Weir Sides =	6.00	N/A	feet Overflow Grate Open Area w/o Debris =	60.03	N/A	ft ²
Overflow Grate Type =	Close Mesh Grate	N/A	Overflow Grate Open Area w/ Debris =	60.03	N/A	ft ²
Debris Clogging % =	0%	N/A	%			-

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

Outlet Pipe w/ Flow Restriction Plate	e (Circular Orifice, R	Restrictor Plate, or	Rectangular Orifice)	Calculated Parameter	s for Outlet Pipe w/ Flow Restriction Plate				
	Zone 3 Rectangulai	Not Selected			Zone 3 Rectangular	Not Selected			
Depth to Invert of Outlet Pipe =	1.21	N/A	ft (distance below basin bottom at Stage = 0 ft)	Outlet Orifice Area =	18.00	N/A	ft ²		
Rectangular Orifice Width =	72.00	N/A	inches	Outlet Orifice Centroid =	1.50	N/A	feet		
Rectangular Orifice Height =	36.00		inches Half-Central Angle o	f Restrictor Plate on Pipe =	N/A	N/A	radians		

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage=	11.00	ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length =	185.00	feet
Spillway End Slopes =	4.00	H:V
Freeboard above Max Water Surface =	0.40	feet

Calculated Parameters for Spillway

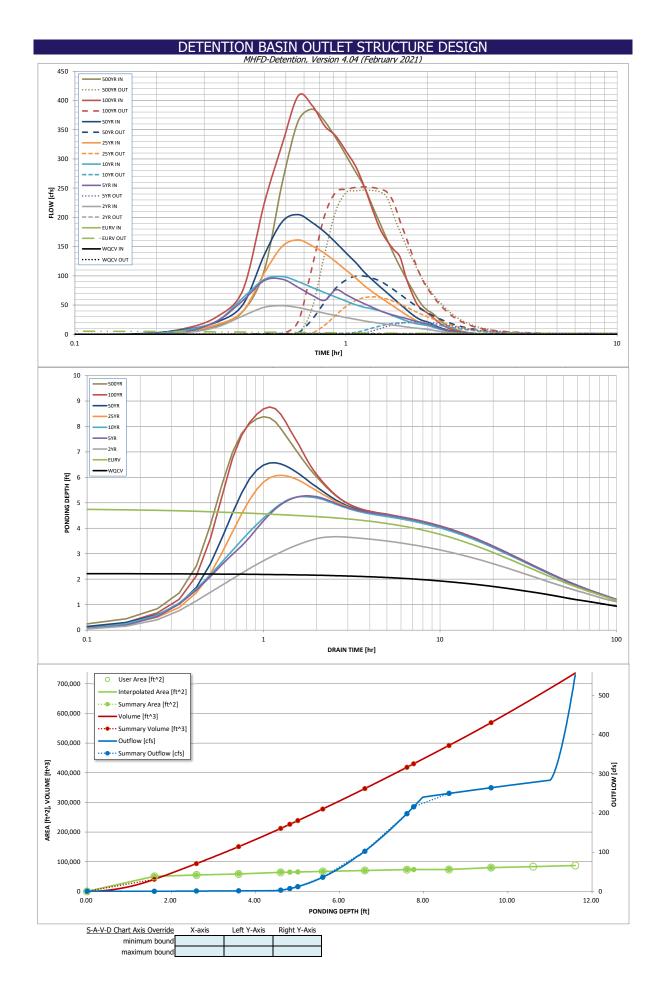
Calculated Parameters for Vertical Orifice

Not Selected

N/A

Spillway Design Flow Depth= 0.59 feet Stage at Top of Freeboard = 11.99 feet Basin Area at Top of Freeboard 2.00 acres Basin Volume at Top of Freeboard = 16.89 acre-ft

Routed Hydrograph Results	The user can over	rride the default CUI	HP hydrographs an	nd runoff volumes b	y entering new valt	ues in the Inflow H	ydrographs table (C	Columns W through	AF).
Design Storm Return Period =	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
One-Hour Rainfall Depth (in) =	N/A	N/A	1.00	1.28	1.55	1.97	2.34	2.74	3.84
CUHP Runoff Volume (acre-ft) =	1.671	5.144	3.741	5.462	7.357	11.295	14.367	18.116	27.672
User Override Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	3.741	7.663	7.357	11.295	14.367	29.508	27.672
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A	1.1	11.3	25.6	67.8	94.1	127.9	209.2
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A							
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.01	0.11	0.26	0.69	0.95	1.29	2.12
Peak Inflow Q (cfs) =	N/A	N/A	48.9	94.1	98.7	161.4	204.6	407.9	385.0
Peak Outflow Q (cfs) =	0.5	6.0	1.3	21.3	20.1	64.1	99.5	252.3	246.5
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	1.9	0.8	0.9	1.1	2.0	1.2
Structure Controlling Flow =	Plate	Overflow Weir 1	Plate	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Outlet Plate 1	Outlet Plate 1
Max Velocity through Grate 1 (fps) =	N/A	0.08	N/A	0.3	0.3	1.0	1.6	4.2	4.1
Max Velocity through Grate 2 (fps) =		N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	>120	>120	>120	>120	>120	>120	116	71	74
Time to Drain 99% of Inflow Volume (hours) =	>120	>120	>120	>120	>120	>120	>120	>120	>120
Maximum Ponding Depth (ft) =	2.22	4.79	3.66	5.27	5.24	6.08	6.57	8.76	8.38
Area at Maximum Ponding Depth (acres) =	1.23	1.49	1.35	1.52	1.52	1.58	1.61	1.72	1.69
Maximum Volume Stored (acre-ft) =	1.674	5.147	3.537	5.869	5.823	7.107	7.888	11.566	10.904
Equivalent Elevation (ft) =		5687.19	5686.06	5687.67	5687.64	5688.48	5688.97	5691.16	
Pond Bottom (ft) =	5682.400								



DETENTION BASIN OUTLET STRUCTURE DESIGN Outflow Hydrograph Workbook Filename:

Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

Time Name Time		SOURCE	CUHP	CUHP	CUHP	USER	CUHP	CUHP	CUHP	USER	CUHP
Dispose	Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
0.1000	5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.1500		0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.2000		0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.70	0.00	3.09
0.2500 0.00 0.00 1.05 1.51 57.69 66.27 38.54 59.87 77.2 190.66 0.0500 0.00 0.00 0.00 46.16 91.81 93.76 190.65 180.67 77.2 190.66 0.05500 0.00 0.00 0.00 48.87 94.12 98.66 150.73 193.05 326.49 355.14 0.4000 0.00 0.00 46.87 94.12 98.66 150.73 193.05 326.49 355.14 0.4000 0.00 0.00 45.61 90.25 90.11 10.13 20.464 407.23 385.04 0.4500 0.00 0.00 0.00 45.61 90.25 90.11 10.13 20.464 407.23 385.04 0.4500 0.00 0.00 0.00 15.99 58.09 97.147 138.64 17.55 356.83 336.11 0.55500 0.00 0.00 0.00 32.15 76.88 58.78 124.09 157.03 392.23 356.19 1.0000 0.00 0.00 0.00 28.77 67.25 58.88 10.1079 139.37 313.47 129.15 10.00 0.00 0.00 0.00 25.79 19.43 59.09 98.45 124.07 33.23 392.21 356.19 11.000 0.00 0.00 0.00 25.79 19.43 59.09 98.45 124.27 28.888 125.27 125.20 11.000 0.00 0.00 0.00 25.79 19.43 59.09 98.45 123.27 125.20 125.2											
0.330-00 0.00 0.00 46.616 91.81 93.76 105.05 136.02 224.60 226.08											
0.35900 0.00 0.00 48.87 94.12 98.66 139.75 133.05 328.69 365.14 0.45000 0.00 0.00 0.00 46.51 80.25 90.11 161.36 1246.4 497.3 385.04 0.45000 0.00 0.00 40.59 66.76 80.26 151.30 191.18 391.67 348.60 0.55000 0.00 0.00 0.00 32.15 76.88 63.78 124.09 157.03 339.23 308.19 10.00 0.00 0.00 0.00 32.15 76.88 63.78 124.09 157.03 339.23 308.19 110000 0.00 0.00 0.00 22.75 76.88 63.78 124.09 157.03 339.23 308.19 110000 0.00 0.00 0.00 25.79 99.43 50.69 96.85 123.27 228.08 228.35 110000 0.00 0.00 0.00 25.79 159.04 50.00 159.04 159.0											
0.4000	ŀ										
0.55000 0.00 0.00 35.99 \$8.00 71.47 138.64 175.05 35.63 330.31 30.59 0.5500 0.00 0.00 0.00 20.75 21.55 76.08 63.73 124.09 175.03 392.33 306.19 1.0000 0.00 0.00 0.00 20.77 67.02 58.86 109.79 139.37 131.47 27.00 1.000 0.00 0.00 0.00 28.77 67.02 58.86 109.79 139.37 131.47 27.00 11.000 0.00 0.00 0.00 28.79 93.43 59.69 96.55 122.22 28.08 82 22.38 11.100 0.00 0.00 0.00 21.01 52.79 94.33 59.69 96.55 122.22 28.08 82 22.38 11.100 0.00 0.00 0.00 21.01 52.70 44.30 81.54 106.61 27.154 222.11 11.100 0.00 0.00 0.00 21.04 43.05 44.10 81.54 106.61 27.154 222.11 11.100 0.00 0.00 0.00 18.86 405.2 44.10 65.1 81.64 100.99 11.25.2 12.250 0.00 0.00 0.00 11.22 36.01 58.76 55.2 17.12 100.14 12.23 11.2500 0.00 0.00 15.66 32.055 31.27 47.24 60.92 100.14 11.23 11.3500 0.00 0.00 11.64.2 29.66 27.15 27.26 44.25 11.25 11.25 11.25 11.35 10 0.00 0.00 0.00 11.64.2 29.66 13.25 11.27 47.24 60.92 100.14 11.53 11.35 11.35 10 0.00 0.00 0.00 11.12.62 27.15 23.26 33.64 42.25 59.66 87.70 11.45 10 0.00 0.00 0.00 11.00 10.00 10.00 10.00 10.00 10.00 11.30 10.40 21.55 11.25 22.22 27.27 55.89 46.38 11.55 10 0.00 0.00 0.00 10.0		0:40:00									
0.55.00											
1,90,00 0,00 0,00 26,77 67.82 56,86 190,79 139,37 313,47 278,30 105,500 1,000 0,00 25,79 59,43 50,66 68,85 123,327 286,08 252,85 11,1000 0,00 0,00 20,74 46,55 48,30 83,54 106,61 253,54 221,13 11,1500 0,00 0,00 18,86 40,52 44,10 63,61 61,64 180,99 162,32 12,500 0,00 0,00 17,22 36,61 35,76 55,52 71,12 160,14 177,22 13,000 0,00 0,00 17,22 36,61 35,76 55,52 71,12 160,14 177,22 13,500 0,00 0,00 14,12 29,66 27,06 40,42 51,33 132,08 57,55 140,00 0,00 14,12 29,66 27,06 40,42 51,33 132,08 57,55 140,00 0,00 14,45 20,45 31,65 47,55 34,55 70,46 61,83 15,500 0,00 0,00 11,30 24,16 19,99 27,25 34,55 70,46 61,83 15,500 0,00 0,00 10,40 21,51 17,80 22,22 27,75 50,89 48,98 15,500 0,00 0,00 3,38 17,41 15,00 16,30 13,33 17,36 26,63 33,64 20,99 36,08 33,98 20,500 0,00 0,00 0,00 3,38 17,41 15,00 16,40 13,48 20,99 36,08 33,98 20,500 0,00 0,00 3,50 70,00 62,00 63,81 17,41 15,90 63,45 63,4	ļ										
1.05:00											
1:10:00											
1:20:00											
1:25:00			0.00	0.00	20.74	46.35	43.41	72.79	93.34	214.87	190.34
1:30:00											
1:35:00 0.00	ŀ										
1:40:00	ŀ										
1.55:00											
1.55.00											
2.005:00	[
2:05:00 0.00 0.00 7.01 14.97 12.69 13.93 17.36 29.63 29.33 2:10:00 0.00 0.00 5.61 11.89 10.11 11.084 13.48 22.74 22.26 2:20:00 0.00 0.00 0.00 3.50 7.02 6.20 6.43 7.94 12.61 12.36 2:25:00 0.00 0.00 2.75 5.27 4.81 4.94 6.07 9.30 9.21 2:30:00 0.00 0.00 0.00 1.67 3.12 2.286 3.48 4.99 5.26 2:40:00 0.00 0.00 1.67 3.12 2.286 3.48 4.99 5.26 2:40:00 0.00 0.00 1.67 3.12 2.286 3.48 4.99 5.26 2:40:00 0.00 0.00 0.98 1.78 1.61 1.65 2.00 2.77 3.10 2:50:00 0.00 0.00 0.51											
2:10:00 0.00 0.00 5.61 11.89 10.11 10.84 13.48 22.74 22.26 2:15:00 0.00 0.00 0.00 4.44 9.04 7.93 8.34 10.34 16.69 16.62 2:20:00 0.00 0.00 2.75 5.27 4.81 4.94 6.07 9.30 9.21 2:30:00 0.00 0.00 1.67 3.12 2.78 2.86 3.48 4.99 5.26 2:40:00 0.00 0.00 1.67 3.12 2.78 2.86 3.48 4.99 5.26 2:40:00 0.00 0.00 0.00 1.88 2.39 2.10 2.16 2.62 3.71 4.01 2:45:00 0.00 0.00 0.98 1.78 1.61 1.65 2.00 2.77 3.10 2:50:00 0.00 0.00 0.00 0.72 1.41 1.20 1.25 1.51 2.08 2.33 2:50:00											
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DETENTION BASIN OUTLET STRUCTURE DESIGN MHFD-Detention, Version 4.04 (February 2021)

Summary Stage-Area-Volume-Discharge Relationships
The user can create a summary S-A-V-D by entering the desired stage increments and the remainder of the table will populate automatically.
The user should graphically compare the summary S-A-V-D table to the full S-A-V-D table in the chart to confirm it captures all key transition points.

Stage - Storage Description	Stage [ft]	Area [ft ²]	Area [acres]	Volume [ft ³]	Volume [ac-ft]	Total Outflow [cfs]	
				0			
	0.00	0	0.000		0.000	0.00	For best results, include the stages of all grade slope
	1.60	50,745	1.165	40,595	0.932	0.24	changes (e.g. ISV and Floor)
	2.60	55,231 58,662	1.268 1.347	93,583 150,529	2.148 3.456	0.70 1.28	from the S-A-V table on
	3.60 4.60	64,191	1.474	211,956	4.866	2.89	Sheet 'Basin'.
EURV (FS)	4.82	64,856	1.489	226,151	5.192	7.01	Also include the inverts of all
5-Year	5.01	65,430	1.502	238,528	5.476	12.09	outlets (e.g. vertical orifice,
5 1001	5.60	67,213	1.543	277,658	6.374	35.96	overflow grate, and spillway,
	6.60	70,292	1.614	346,410	7.952	102.27	where applicable).
	7.60	73,458	1.686	418,285	9.603	198.34	
100-Year	7.76	73,518	1.688	430,043	9.872	215.81	
	8.60	73,831	1.695	491,930	11.293	249.84	
	9.60	80,094	1.839	568,892	13.060	264.45	
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DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.04 (February 2021)

Project: Mesa Ridge Cottages

Basin ID: Existing Pond D Sizing Confirmation - with Structure Modifications

acre-feet

inches

inches

inches

inches

inches

inches

1.00

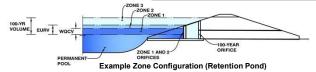
1.28

1.55

1.97

2.34

3.84



Watershed Information

Selected BMP Type =	EDB	
Watershed Area =	98.80	acres
Watershed Length =	4,090	ft
Watershed Length to Centroid =	2,000	ft
Watershed Slope =	0.035	ft/ft
Watershed Imperviousness =	48.80%	percent
Percentage Hydrologic Soil Group A =	0.0%	percent
Percentage Hydrologic Soil Group B =	100.0%	percent
Percentage Hydrologic Soil Groups C/D =	0.0%	percent
Target WQCV Drain Time =	40.0	hours
Location for 1-br Painfall Denths -	Hear Innut	

After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

the embedded Colorado Urban Hydro	graph Procedu	re.
Water Quality Capture Volume (WQCV) =	1.671	acre-feet
Excess Urban Runoff Volume (EURV) =	5.144	acre-feet
2-yr Runoff Volume (P1 = 1 in.) =	3.741	acre-feet
5-yr Runoff Volume (P1 = 1.28 in.) =	5.462	acre-feet
10-yr Runoff Volume (P1 = 1.55 in.) =	7.357	acre-feet
25-yr Runoff Volume (P1 = 1.97 in.) =	11.295	acre-feet
50-yr Runoff Volume (P1 = 2.34 in.) =	14.367	acre-feet
100-yr Runoff Volume (P1 = 2.74 in.) =	18.116	acre-feet
500-yr Runoff Volume (P1 = 3.84 in.) =	27.672	acre-feet
Approximate 2-yr Detention Volume =	3.247	acre-feet
Approximate 5-yr Detention Volume =	4.538	acre-feet
Approximate 10-yr Detention Volume =	6.263	acre-feet
Approximate 25-yr Detention Volume =	7.639	acre-feet
Approximate 50-yr Detention Volume =	8.436	acre-feet
Approximate 100-yr Detention Volume =	9.873	acre-feet

Define Zones and Basin Geometry

Zone 1 Volume (User Defined) =	5.14	acre-feet
Zone 2 Volume (User Defined - Zone 1) =	0.32	acre-feet
Zone 3 Volume (User Defined - Zones 1 & 2) =	7.04	acre-feet
Total Detention Basin Volume =	12.50	acre-feet

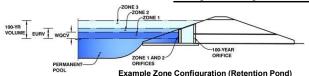
				Lievation	Stage	Volume	
5682.4	pond botto	m	EURV (FSV)	5687.18	4.78	5.14	
			5-Yr	5687.40	5.00	5.46	
Depth Increment =		ft	100-YR	5691.71	9.31	12.50	
		0-6			Ontional		т

Depth Increment =		ft		100-YR	5691.71	9.31	12.50		
		Optional			_	Optional			
Stage - Storage	Stage	Override	Length	Width	Area (ft ²)	Override Area (ft ²)	Area	Volume (ft 3)	Volume
Description Top of Micropool	(ft) 	Stage (ft) 0.00	(ft)	(ft) 	(Tt) 	Area (π)	(acre) 0.000	(π')	(ac-ft)
						-			
5684.00		1.60				50,745	1.165	40,595	0.932
5685.00		2.60				55,231	1.268	93,583	2.148
5686.00		3.60				58,662	1.347	150,529	3.456
5687.00		4.60				64,191	1.474	211,956	4.866
5688.00		5.60				67,213	1.543	277,658	6.374
5689.00		6.60				70,292	1.614	346,410	7.952
5690.00		7.60	-			73,458	1.686	418,285	9.603
5691.00		8.60				73,831	1.695	491,930	11.293
5692.00		9.60	-			80,094	1.839	568,892	13.060
5693.00		10.60				83,415	1.915	650,647	14.937
5694.00		11.60				87,173	2.001	735,941	16.895
			-						
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			-						
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MHFD-Detention, Version 4.04 (February 2021)

Project: Mesa Ridge Cottages

Basin ID: Existing Pond D Sizing Confirmation - with Structure Modifications



	Estimated Stage (ft)	Estimated Volume (ac-ft)	Outlet Type
Zone 1 (User)	4.79	5.144	Orifice Plate
Zone 2 (User)	5.01	0.318	Rectangular Orifice
Zone 3 (User)	9.30	7.035	Weir&Pipe (Rect.)
,	Total (all zones)	12.497	

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth = N/A ft (distance below the filtration media surface) Underdrain Orifice Diameter =

Underdrain Orifice Area Underdrain Orifice Centroid

N/A ft2 N/A

Calculated Parameters for Underdrain

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice = 0.00 ft (relative to basin bottom at Stage = 0 ft) Depth at top of Zone using Orifice Plate = 4.79 ft (relative to basin bottom at Stage = 0 ft) Orifice Plate: Orifice Vertical Spacing = 19.20 inches Orifice Plate: Orifice Area per Row = 11.10 sq. inches (use rectangular openings)

Calculated Parameters for Plate WQ Orifice Area per Row = 7.708E-02 ft² Fllintical Half-Width = N/A feet Elliptical Slot Centroid = N/A feet ft² Elliptical Slot Area N/A

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	1.60	3.19					
Orifice Area (sq. inches)	11.10	11.10	11.10					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

	Zone 2 Rectangulai	Not Selected	
Invert of Vertical Orifice =	4.79	N/A	ft (
Depth at top of Zone using Vertical Orifice =	5.01	N/A	ft (
Vertical Orifice Height =	2.00	N/A	inc
Vortical Orifice Width -	72.00		inc

Calculated Parameters for Vertical Orifice Zone 2 Rectangula Not Selected (relative to basin bottom at Stage = 0 ft) Vertical Orifice Area : 1.00 N/A (relative to basin bottom at Stage = 0 ft) Vertical Orifice Centroid = 0.08 N/A

Grate Open Area / 100-yr Orifice Area =

Overflow Grate Open Area w/o Debris

Half-Central Angle of Restrictor Plate on Pipe =

Overflow Grate Open Area w/ Debris =

inches Vertical Orifice Width = 72.00

User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe) Zone 3 Weir Not Selected

pe)_	Calculated Parame	ters for Overflow V	/eir
	Zone 3 Weir	Not Selected	
eight of Grate Upper Edge, H_t =	7.01	N/A	feet
Overflow Weir Slope Length =	6.32	N/A	feet

N/A

N/A

N/A

N/A

feet

radians

o basin bottom at Stage = 0 ft) Height of Grate Upper Edge	f	N/A	5.01	Overflow Weir Front Edge Height, Ho =
Overflow Weir Slope Ler	f	N/A	12.00	Overflow Weir Front Edge Length =
Grate Open Area / 100-yr Orifice A	H	N/A	3.00	Overflow Weir Grate Slope =
Overflow Grate Open Area w/o De	f	N/A	6.00	Horiz. Length of Weir Sides =
Overflow Grate Open Area w/ De		N/A	Close Mesh Grate	Overflow Grate Type =
	9	N/A	0%	Debris Clogging % =

72.00

32.00

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice) Zone 3 Rectangular Not Selected Depth to Invert of Outlet Pipe = 1.21 N/A

N/A

linches

inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate Zone 3 Rectangular Not Selected Outlet Orifice Area 16.00 N/A Outlet Orifice Centroid : 1.33 N/A feet

N/A

3.75

60.03

60.03

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Fı

Rectangular Orifice Width =

Rectangular Orifice Height =

Spillway Invert Stage=	11.00	ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length =	185.00	feet
Spillway End Slopes =	4.00	H:V
reeboard above Max Water Surface =	0.40	feet

Calculated Parameters for Spillway Spillway Design Flow Depth= 0.59 feet

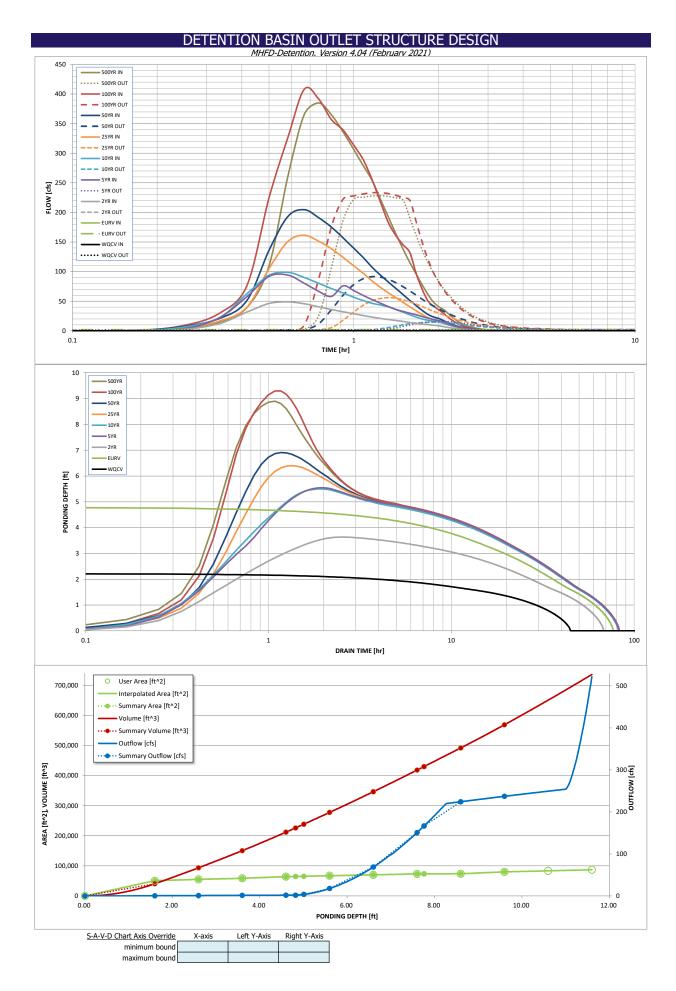
Stage at Top of Freeboard = 11.99 feet Basin Area at Top of Freeboard = 2.00 acres Basin Volume at Top of Freeboard = 16.89 acre-ft

Routed Hydrograph Results	The user can over	ride the default CUF	HP hydrographs and	d runoff volumes by	entering new value	es in the Inflow Hyd	drographs table (Co	lumns W through	AF).
Design Storm Return Period =	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
One-Hour Rainfall Depth (in) =	N/A	N/A	1.00	1.28	1.55	1.97	2.34	2.74	3.84
CUHP Runoff Volume (acre-ft) =	1.671	5.144	3.741	5.462	7.357	11.295	14.367	18.116	27.672
User Override Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	3.741	7.663	7.357	11.295	14.367	29.508	27.672
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A	1.1	11.3	25.6	67.8	94.1	127.9	209.2
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A							
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.01	0.11	0.26	0.69	0.95	1.29	2.12
Peak Inflow Q (cfs) =	N/A	N/A	48.9	94.1	98.7	161.4	204.6	407.9	385.0
Peak Outflow Q (cfs) =	0.8	1.9	1.5	16.0	14.5	55.9	91.5	233.4	228.2
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	1.4	0.6	0.8	1.0	1.8	1.1
Structure Controlling Flow =	Plate	Vertical Orifice 1	Plate	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Outlet Plate 1	Outlet Plate 1
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	0.2	0.1	0.8	1.4	3.7	3.6
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A /	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	41	69	62 /	72	71	67	64	52	53
Time to Drain 99% of Inflow Volume (hours) =	43	73	65 /	78	77	76	75	70	70
Maximum Ponding Depth (ft) =	2.22	4.79	3.68	5.54	5.50	6.40	6.91	9.30	8.90
Area at Maximum Ponding Depth (acres) =	1.23	1.49	1⁄.35	1.54	1.54	1.60	1.64	1.79	1.74
Maximum Volume Stored (acre-ft) =	1.674	5.147	/ 3.496	6.282	6.205	7.615	8.440	12.497	11.791
Equivalent Elevation (ft) =		5687.19	5686.03	5687.94	5687.90	5688.80	5689.31	5691.70	
Pond Bottom (ft) =	5682.400								

ft (distance below basin bottom at Stage = 0 ft)

Ratio should be less than or equal to 1.

will require a guard rail or adjust velocity



DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename:

Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

								l in a separate pr		
	SOURCE	CUHP	CUHP	CUHP	USER	CUHP	CUHP	CUHP	USER	CUHP
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.70	0.00	3.09
	0:15:00	0.00	0.00	2.43	3.68	6.53	5.30	7.67	9.15	14.49
	0:20:00	0.00	0.00	12.29	22.29	22.28	16.37	20.88	29.83	38.98
	0:25:00	0.00	0.00	31.51	57.69	62.37	39.54	50.87	75.72	109.68
	0:30:00	0.00	0.00	46.16	91.81	93.76	105.05	136.02	224.60	260.83
	0:35:00	0.00	0.00	48.87	94.12	98.66	150.75	193.05	326.49	365.14
	0:40:00	0.00	0.00	45.61	80.25	90.11	161.36	204.64	407.93	385.04
	0:45:00	0.00	0.00	40.59	66.76	80.26	151.30	191.18	391.67	364.86
	0:50:00	0.00	0.00	35.99	58.09	71.47	138.64	175.05	356.83	336.13
	0:55:00	0.00	0.00	32.15	76.08	63.78	124.09	157.03	339.23	306.19
	1:00:00	0.00	0.00	28.77	67.82	56.86	109.79	139.37	313.47	278.30
	1:05:00	0.00	0.00	25.79	59.43	50.69	96.85	123.27	288.08	252.85
	1:10:00	0.00	0.00	23.01	52.50	46.30	83.54	106.61	253.54	220.13
	1:15:00	0.00	0.00	20.74	46.35	43.41	72.79	93.34	214.87	190.34
	1:20:00	0.00	0.00	18.86	40.52	40.10	63.61	81.64	180.99	162.52
	1:25:00 1:30:00	0.00	0.00	17.22	36.01	35.76	55.52	71.12	160.14	137.32
	1:35:00	0.00	0.00	15.66 14.12	32.65 29.66	31.27 27.06	47.74 40.42	60.92 51.35	145.01 132.08	115.32 95.75
	1:40:00	0.00	0.00	14.12	29.66	27.06	33.66	42.55	96.68	95.75 77.90
	1:45:00	0.00	0.00	11.30	24.16	19.99	27.50	34.55	70.46	61.83
	1:50:00	0.00	0.00	10.40	21.51	17.80	22.22	27.75	50.89	48.98
	1:55:00	0.00	0.00	9.39	19.21	16.39	18.85	23.57	42.17	41.05
	2:00:00	0.00	0.00	8.38	17.41	15.05	16.81	20.99	36.08	35.98
	2:05:00	0.00	0.00	7.01	14.97	12.69	13.93	17.36	29.63	29.23
	2:10:00	0.00	0.00	5.61	11.89	10.11	10.84	13.48	22.74	22.26
	2:15:00	0.00	0.00	4.44	9.04	7.93	8.34	10.34	16.89	16.62
	2:20:00	0.00	0.00	3.50	7.02	6.20	6.43	7.94	12.61	12.36
	2:25:00	0.00	0.00	2.75	5.27	4.81	4.94	6.07	9.30	9.21
	2:30:00	0.00	0.00	2.14	4.09	3.67	3.78	4.62	6.83	6.99
	2:35:00	0.00	0.00	1.67	3.12	2.78	2.86	3.48	4.99	5.26
	2:40:00	0.00	0.00	1.28	2.39	2.10	2.16	2.62	3.71	4.01
	2:45:00	0.00	0.00	0.98	1.78	1.61	1.65	2.00	2.77	3.10
	2:50:00	0.00	0.00	0.72	1.41	1.20	1.25	1.51	2.08	2.33
	2:55:00 3:00:00	0.00	0.00	0.51	1.22	0.86	0.90	1.09	1.53	1.67
	3:05:00	0.00	0.00	0.34	1.11	0.58	0.61	0.74	1.24	1.12
	3:10:00	0.00	0.00	0.20 0.10	1.06	0.35 0.18	0.38 0.20	0.45 0.24	1.11	0.67 0.34
	3:15:00	0.00	0.00	0.10	1.03	0.18	0.20	0.24	1.03	0.12
	3:20:00	0.00	0.00	0.01	1.02	0.01	0.01	0.01	1.02	0.00
	3:25:00	0.00	0.00	0.00	1.01	0.00	0.00	0.00	1.02	0.00
	3:30:00	0.00	0.00	0.00	1.01	0.00	0.00	0.00	1.01	0.00
	3:35:00	0.00	0.00	0.00	1.01	0.00	0.00	0.00	1.01	0.00
	3:40:00	0.00	0.00	0.00	1.01	0.00	0.00	0.00	1.01	0.00
	3:45:00	0.00	0.00	0.00	1.01	0.00	0.00	0.00	1.01	0.00
	3:50:00	0.00	0.00	0.00	1.01	0.00	0.00	0.00	1.01	0.00
	3:55:00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
	4:00:00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
	4:05:00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
	4:10:00 4:15:00	0.00	0.00	0.00	1.00 1.00	0.00	0.00	0.00	1.00 1.00	0.00
	4:20:00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
	4:25:00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
	4:30:00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
	4:35:00 4:40:00	0.00	0.00	0.00	1.00 1.00	0.00	0.00	0.00	1.00 1.00	0.00
	4:45:00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
	4:50:00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
	4:55:00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
	5:00:00 5:05:00	0.00	0.00	0.00	1.00 0.00	0.00	0.00	0.00	1.00 0.00	0.00
	5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:25:00 5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:50:00 5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.04 (February 2021)

Summary Stage-Area-Volume-Discharge Relationships

The user can create a summary S-A-V-D by entering the desired stage increments and the remainder of the table will populate automatically. The user should graphically compare the summary S-A-V-D table to the full S-A-V-D table in the chart to confirm it captures all key transition points.

							_
	Stane	Area	Area	Volume	Volume	Total	
Stage - Storage	Stage	Aita	Aita	Tolaine	Volume	Outflow	
Description	[ft]	[ft²]	[acres]	[ft ³]	[ac-ft]	[cfs]	
	[.e]	[it]	[ucres]	[ic]	[uc ic]	[6.5]	
	0.00	0	0.000	0	0.000	0.00	F
	0.00	_	0.000		0.000	0.00	
	1.60	50,745	1.165	40,595	0.932	0.47	5
							-
	2.60	55,231	1.268	93,583	2.148	0.97	(f
		E0 663	1.347	150 520	3.456	1.47	
	3.60	58,662	1.34/	150,529	3.430	1.4/	4
	4.60	64,191	1.474	211,956	4.866	1.88	- 1
							┨.
EURV (FS)	4.82	64,856	1.489	226,151	5.192	2.02	_ /
5-Year	5.01	65,430	1.502	238,528	5.476	3.80	
J-16ai	3.01						-1`
	5.60	67,213	1.543	277,658	6.374	17.82	7
		70,292	1.614	346,410	7.952	68.87	٦,
	6.60						_
	7.60	73,458	1.686	418,285	9.603	150.83	
100 1/			1.000		0.073		\neg
100-Year	7.76	73,518	1.688	430,043	9.872	166.59	_
	8.60	73,831	1.695	491,930	11.293	224.30	
							\dashv
	9.60	80,094	1.839	568,892	13.060	237.16	
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For best results, include the stages of all grade slope changes (e.g. ISV and Floor) from the S-A-V table on Sheet 'Basin'.

Also include the inverts of all outlets (e.g. vertical orifice, overflow grate, and spillway, where applicable).





APPENDIX E - REFERENCE MATERIAL

Mesa Ridge Development Master Development Drainage Plan Update

Fountain, Colorado

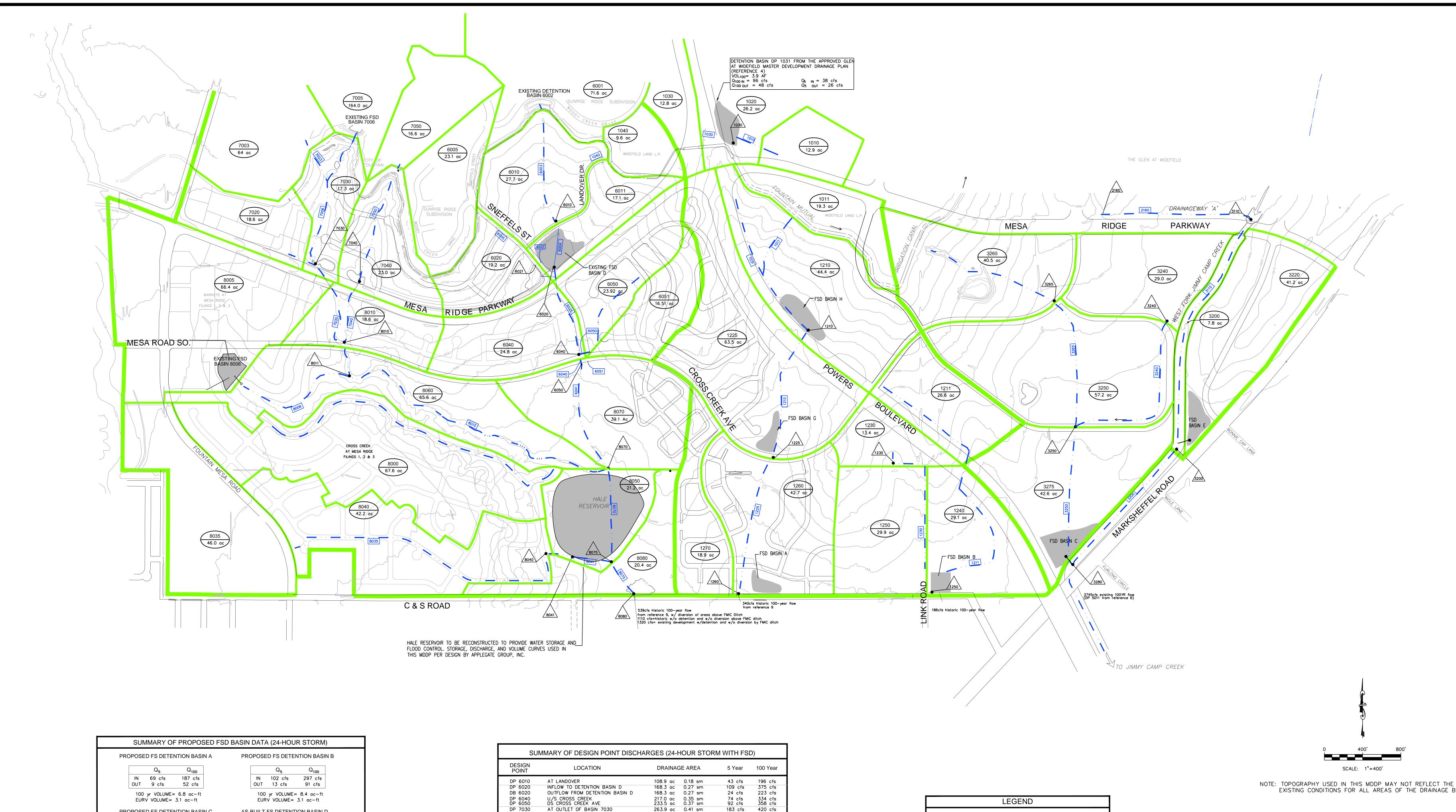
Prepared for:
Nor'wood Development
111 South Tejon Suite 222
Colorado Springs, Colorado 80903

Prepared by:



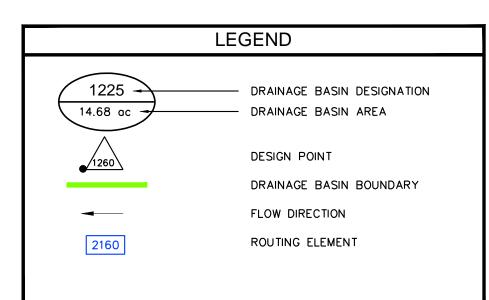
1604 South 21st Street Colorado Springs, Colorado 80904 (719) 630-7342

Kiowa Project No. 11045 January 15, 2013



SUMMARY OF PROPOSED FS	D BASIN DATA (24-HOUR STORM)
PROPOSED FS DETENTION BASIN A	PROPOSED FS DETENTION BASIN B
Q ₅ Q ₁₀₀ IN 69 cfs 187 cfs OUT 9 cfs 52 cfs	Q5 Q100 IN 102 cfs 297 cfs OUT 13 cfs 91 cfs
100 yr VOLUME= 6.8 ac-ft EURV VOLUME= 3.1 ac-ft	100 yr VOLUME= 8.4 ac-ft EURV VOLUME= 3.1 ac-ft
PROPOSED FS DETENTION BASIN C	AS-BUILT FS DETENTION BASIN D
Q ₅ Q ₁₀₀	Q ₅ Q ₁₀₀
IN 158 cfs 490 cfs OUT 9 cfs 145 cfs	IN 109 cfs 375 cfs OUT 24 cfs 233 cfs
100 yr VOLUME= 14.8 ac-ft EURV VOLUME= 8.3 ac-ft	100 yr VOLUME= 8.0 ac-ft 5 yr VOLUME= 4.1 ac-ft
PROPOSED FS DETENTION BASIN E	RECONSTRUCTED DAM & RESERVOIR BASIN 'F
Q ₅ Q ₁₀₀	Q ₅ Q ₁₀₀
IN 41 cfs 120 cfs OUT 5 cfs 24 cfs	IN 540 cfs 1540 cfs OUT 7 cfs 255 cfs
100 yr VOLUME= 3.9 ac-ft EURV VOLUME= 1.3 ac-ft	100 yr VOLUME= 95.9 ac-ft 5 yr VOLUME= 50.0 ac-ft
PROPOSED FS DETENTION BASIN G	PROPOSED FS DETENTION BASIN H
Q ₅ Q ₁₀₀	Q ₅ Q ₁₀₀
IN 74 cfs 216 cfs OUT 10 cfs 51 cfs	IN 161 cfs 323 cfs OUT 23 cfs 56 cfs
100 yr VOLUME= 6.6 ac-ft EURV VOLUME= 2.2 ac-ft	100 yr VOLUME= 13.2 ac-ft EURV VOLUME= 2.5 ac-ft

SU	MMARY OF DESIGN POINT DISCH	ARGES (24-l	HOUR STOR	RM WITH FS	D)
DESIGN POINT	LOCATION	DRAINAC	GE AREA	5 Year	100 Year
DP 6010	AT LANDOVER	108.9 ac	0.18 sm	43 cfs	196 cfs
DP 6020	INFLOW TO DETENTION BASIN D	168.3 ac	0.27 sm	109 cfs	375 cfs
DB 6020	OUTFLOW FROM DETENTION BASIN D	168.3 ac	0.27 sm	24 cfs	223 cfs
DP 6040	U/S CROSS CREEK DS CROSS CREEK AVE	217.0 ac	0.35 sm	74 cfs	334 cfs
DP 6050 DP 7030	AT OUTLET OF BASIN 7030	233.5 ac 263.9 ac	0.37 sm 0.41 sm	92 cfs 183 cfs	358 cfs 420 cfs
DP 7030 DP 7040	AT OUTLET OF BASIN 7030 AT OUTLET OF BASIN 7040	263.9 dc 39.6 ac	0.41 sm	30 cfs	110 cfs
DP 8010	AT OUTLET OF BASIN 8010	322.1 ac	0.50 sm	241 cfs	603 cfs
DP 8070	U/S OF HALE RESERVOIR	726.7 ac	1.15 sm	446 cfs	1259 cfs
DP 8075	INFLOW TO HALE RESERVOIR	908.8 ac	1.42 sm	540 cfs	1540 cfs
DB 8075	OUTFLOW FROM HALE RESERVOIR	908.8 ac	1.42 sm	7 cfs	255 cfs
DP 8080	C&S ROAD	928 ac	1.45 sm	13 cfs	257 cfs
DP 1031	D/S POWERS BOULEVARD	51.0 ac	0.08 sm	28 cfs	55 cfs
DP 1211	INFLOW TO DET. BASIN H	108.8 ac	0.17 sm	161 cfs	323 cfs
DB 1210	OUTLOW FROM DET. BASIN H	108.8 ac	0.17 sm	23 cfs	36 cfs
SB 1225	INFLOW TO DETENTION BASIN G	70.4 ac	0.11 sm	74 cfs	216 cfs
DP 1225	AT CROSS CREEK AVENUE	185.6 ac	0.29 sm	33 cfs	104 cfs
DP 1250	INFLOW TO DETENTION BASIN B	96.0 ac	0.15 sm	102 cfs	297 cfs
DB 1250	OUTFLOW FROM DETENTION BASIN B	96.0 ac	0.15 sm	13 cfs	91 cfs
DP 1265	INFLOW TO DETENTION BASIN A	64 ac	0.10 sm	69 cfs	187 cfs
DP 1260	AT C & S ROAD	243 ac	0.38 sm	41 cfs	156 cfs
DP 2160	DESIGN POINT 2160	448 ac	0.70 sm	188 cfs	640 cfs
DP 3110	AT MESA RIDGE PARKWAY	2163.2 ac	3.38 sm	766 cfs	3095 cfs
DP 3200	DESIGN POINT 3200	2208 ac	3.44 sm	764 cfs	3089 cfs
DP 3250	AT COLLECTOR ROAD	126.7 ac	0.20 sm	130 cfs	380 cfs
DP 3265	AT OUTLET OF BASIN 3265	40.5 ac	0.06 sm	52 cfs	135 cfs
DP 3275	INFLOW TO DET. BASIN C	172.8 ac	0.27 sm	158 cfs	490 cfs
DB 3280	OUTFLOW FROM DETENTION BASIN C	172.8 ac	0.27 sm	9 cfs	145 cfs
DP 3280	AT MARKSHEFFEL ROAD	2381.0 ac	3.72 sm	772 cfs	3215 cfs



	SUMMARY OF HISTORIC	DISCHARGES	
DESIGN POINT	LOCATION	5 Year	100 Year
3280	WF JIMMY CAMP CREEK MARKSHEFFEL ROAD	992 cfs	3745 cfs
1250	@ C & S ROAD	35 cfs	186 cfs
1260	@ C & S ROAD	48 cfs	340 cfs
8080 (1)	@ C & S ROAD	152 cfs	1110 cfs

(1) AREA ABOVE FOUNTAIN MUTUAL IRRIGATION CANAL ASSUMED TRIBUTARY TO THIS DESIGN POINT. FMIC CANAL ASSUMED TO CONVEY IRRIGATION FLOW ONLY.

EXISTING CONDITIONS FOR ALL AREAS OF THE DRAINAGE BASINS.

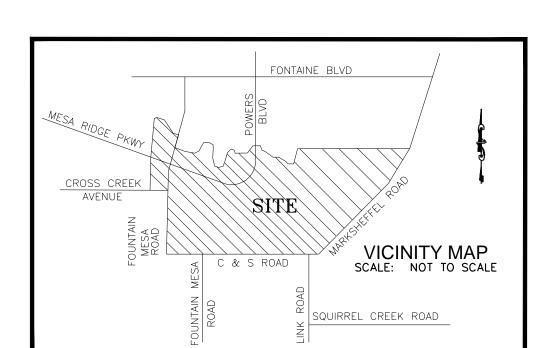
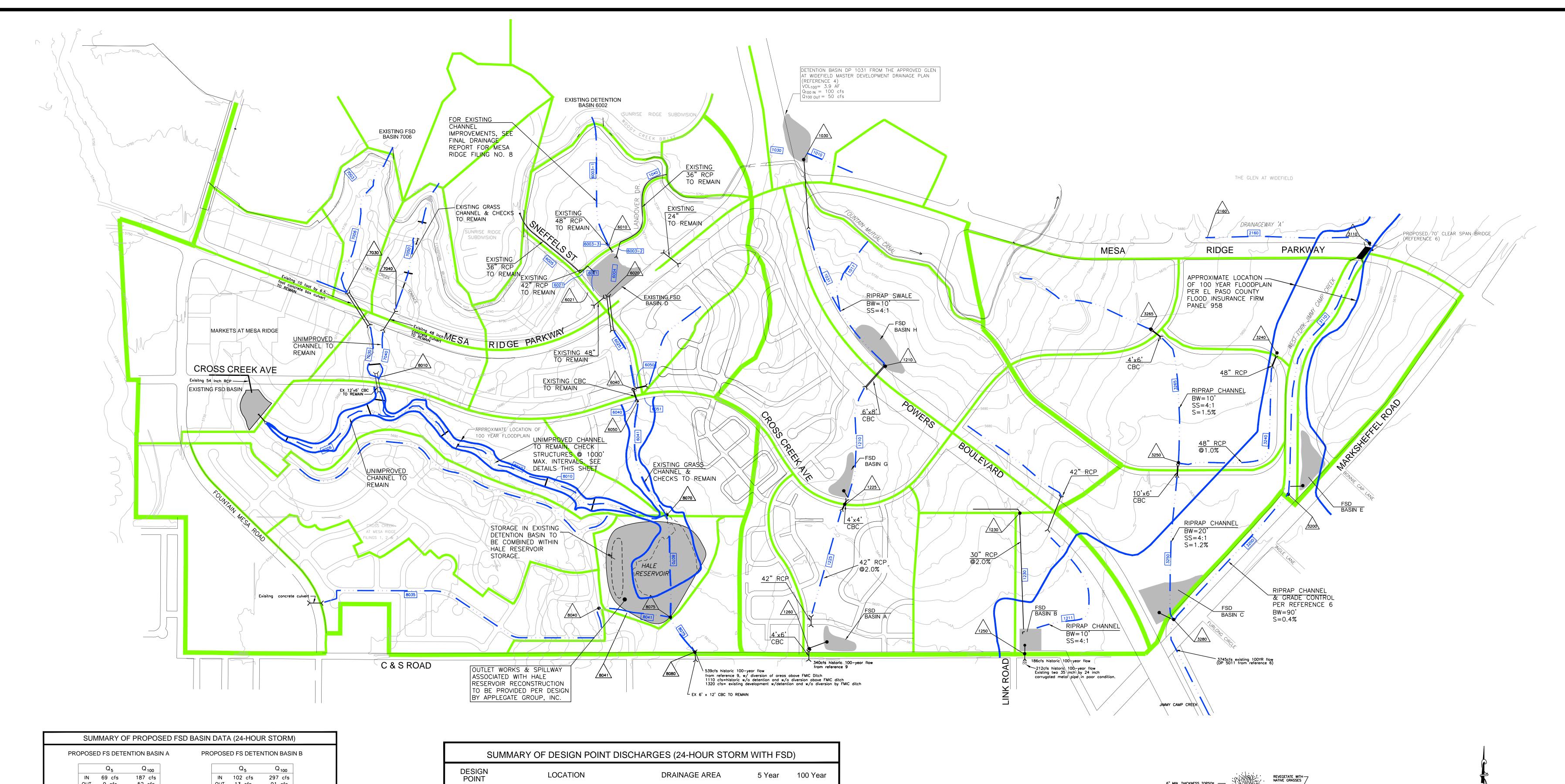


EXHIBIT 1 MESA RIDGE DEVELOPMENT MASTER DEVELOPMENT DRAINAGE PLAN UPDATE HYDROLOGIC SUB-BASIN MAP DEVELOPED WITH EXISTING & PROPOSED DETENTION FOUNTAIN, COLORADO

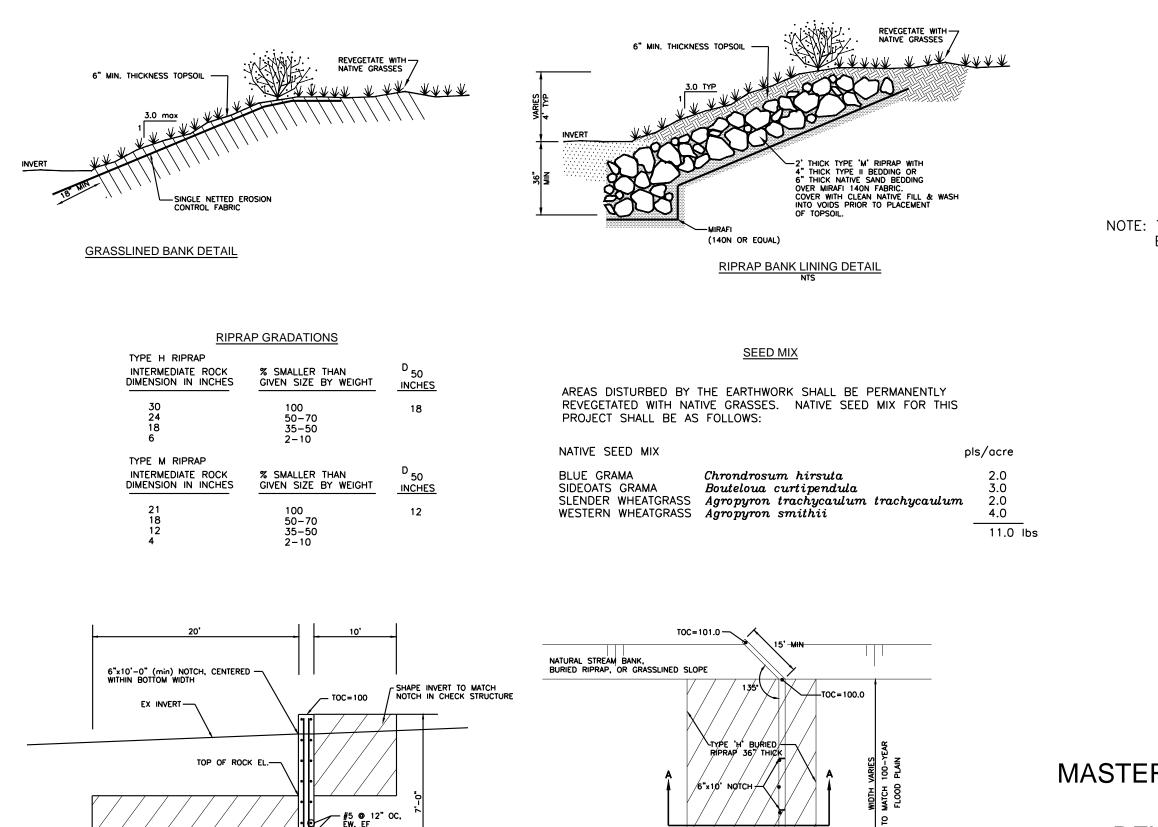
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PROPOSED FS DETENTION BASIN A	PROPOSED FS DETENTION BASIN B
Q ₅ Q ₁₀₀	Q ₅ Q ₁₀₀
IN 69 cfs 187 cfs OUT 9 cfs 52 cfs	IN 102 cfs 297 cfs OUT 13 cfs 91 cfs
100 yr VOLUME= 6.8 ac-ft EURV VOLUME= 3.1 ac-ft	100 yr VOLUME= 8.4 ac-ft EURV VOLUME= 3.1 ac-ft
PROPOSED FS DETENTION BASIN C	AS-BUILT FS DETENTION BASIN D
Q ₅ Q ₁₀₀	Q ₅ Q ₁₀₀
IN 158 cfs 490 cfs OUT 9 cfs 145 cfs	IN 109 cfs 375 cfs OUT 24 cfs 233 cfs
100 yr VOLUME= 14.8 ac-ft EURV VOLUME= 8.3 ac-ft	100 yr VOLUME= 8.0 ac-ft 5 yr VOLUME= 4.1 ac-ft
PROPOSED FS DETENTION BASIN E	RECONSTRUCTED DAM & RESERVOIR BAS
Q ₅ Q ₁₀₀	Q ₅ Q ₁₀₀
IN 41 cfs 120 cfs OUT 5 cfs 24 cfs	IN 540 cfs 1540 cfs OUT 7 cfs 255 cfs
100 yr VOLUME= 3.9 ac-ft EURV VOLUME= 1.3 ac-ft	100 yr VOLUME= 95.9 ac-ft 5 yr VOLUME= 50.0 ac-ft
PROPOSED FS DETENTION BASIN G	PROPOSED FS DETENTION BASIN H
Q ₅ Q ₁₀₀	Q ₅ Q ₁₀₀
IN 74 cfs 216 cfs	IN 161 cfs 323 cfs OUT 23 cfs 56 cfs

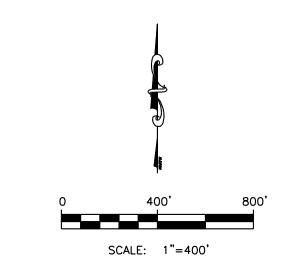
	LECEND
	LEGEND
	100-YEAR FLOODPLAIN
1250	DESIGN POINT
	MAJOR DRAINAGE BASIN BOUNDARY
-	FLOW DIRECTION
· · · · ·	DRAINAGEWAY & CHECK/DROP STRUCTURE

	JMMARY OF DESIGN POINT DISCH				<i>)</i>
DESIGN POINT	LOCATION	DRAINAC	GE AREA	5 Year	100 Year
DP 6010	AT LANDOVER	108.9 ac	0.18 sm	43 cfs	196 cfs
DP 6020	INFLOW TO DETENTION BASIN D	168.3 ac	0.27 sm	109 cfs	375 cfs
DB 6020	OUTFLOW FROM DETENTION BASIN D	168.3 ac	0.27 sm	24 cfs	223 cfs
DP 6040 DP 6050	U/S CROSS CREEK DS CROSS CREEK AVE	217.0 ac 233.5 ac	0.35 sm 0.37 sm	74 cfs 92 cfs	334 cfs 358 cfs
DP 7030	AT OUTLET OF BASIN 7030	263.9 ac	0.41 sm	183 cfs	420 cfs
DP 7040	AT OUTLET OF BASIN 7040	39.6 ac	0.06 sm	30 cfs	110 cfs
DP 8010	AT OUTLET OF BASIN 8010	322.1 ac	0.50 sm	241 cfs	603 cfs
DP 8070	U/S OF HALE RESERVOIR	726.7 ac	1.15 sm	446 cfs	1259 cfs
DP 8075	INFLOW TO HALE RESERVOIR	908.8 ac	1.42 sm	540 cfs	1540 cfs
DB 8075	OUTFLOW FROM HALE RESERVOIR	908.8 ac	1.42 sm	7 cfs	255 cfs
DP 8080	C&S ROAD	928 ac	1.45 sm	13 cfs	257 cfs
DP 1031	D/S POWERS BOULEVARD	51.0 ac	0.08 sm	28 cfs	55 cfs
DP 1211	INFLOW TO DET. BASIN H 1210, POWERS	BLVD 108.8 ac	0.17 sm	161 cfs	323 cfs
DP 1210	OUTLOW FROM DET. BASIN H	108.8 ac	0.17 sm	23 cfs	36 cfs
SB 1225	INFLOW TO DETENTION BASIN G	70.4 ac	0.11 sm	74 cfs	216 cfs
DP 1225	AT CROSS CREEK AVENUE	185.6 ac	0.29 sm	33 cfs	104 cfs
DP 1250	INFLOW TO DETENTION BASIN B	96.0 ac	0.15 sm	102 cfs	297 cfs
DB 1250	OUTFLOW FROM DETENTION BASIN B	96.0 ac	0.15 sm	13 cfs	91 cfs
DP 1265	INFLOW TO DETENTION BASIN A	64 ac	0.10 sm	69 cfs	187 cfs
DP 1260	AT C & S ROAD	243 ac	0.38 sm	41 cfs	156 cfs
DP 2160	DESIGN POINT 2160	448 ac	0.70 sm	188 cfs	640 cfs
DP 3110	AT MESA RIDGE PARKWAY	2163.2 ac	3.38 sm	766 cfs	3095 cfs
DP 3200	DESIGN POINT 3200	2208 ac	3.44 sm	764 cfs	3089 cfs
DP 3250	AT COLLECTOR ROAD	126.7 ac	0.20 sm	130 cfs	380 cfs
DP 3265	AT OUTLET OF BASIN 3265	40.5 ac	0.06 sm	52 cfs	135 cfs
DP 3281	INFLOW TO DET. BASIN C	172.8 ac	0.27 sm	158 cfs	490 cfs
DB 3281	OUTFLOW FROM DETENTION BASIN C	172.8 ac	0.27 sm	9 cfs	145 cfs
DP 3280	AT MARKSHEFFEL ROAD	2381.0 ac	3.72 sm	772 cfs	3215 cfs



TYPICAL CHECK STRUCTURE PLAN
NO SCALE

SECTION A-A



NOTE: TOPOGRAPHY USED IN THIS MDDP MAY NOT REFLECT THE EXISTING CONDITIONS FOR ALL AREAS OF THE DRAINAGE BASINS.

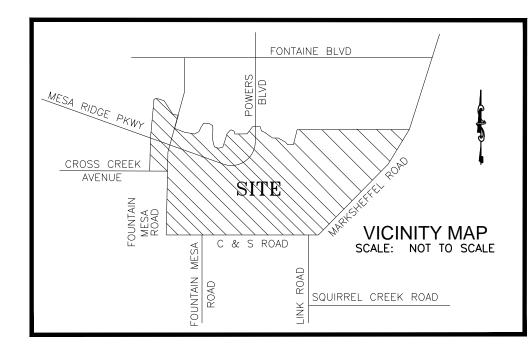


EXHIBIT 2
MESA RIDGE DEVELOPMENT
MASTER DEVELOPMENT DRAINAGE PLAN UPDATE
PROPOSED FACILITIES PLAN
DEVELOPED WITH REGIONAL DETENTION
FOUNTAIN, COLORADO

Kiowa Engineering Corporation

1604 South 21st Street
Colorado Springs, Colorado
80904 - 4208
(719) 630-7342



Master Development Drainage Plan Mesa Ridge Development

City of Fountain, Colorado

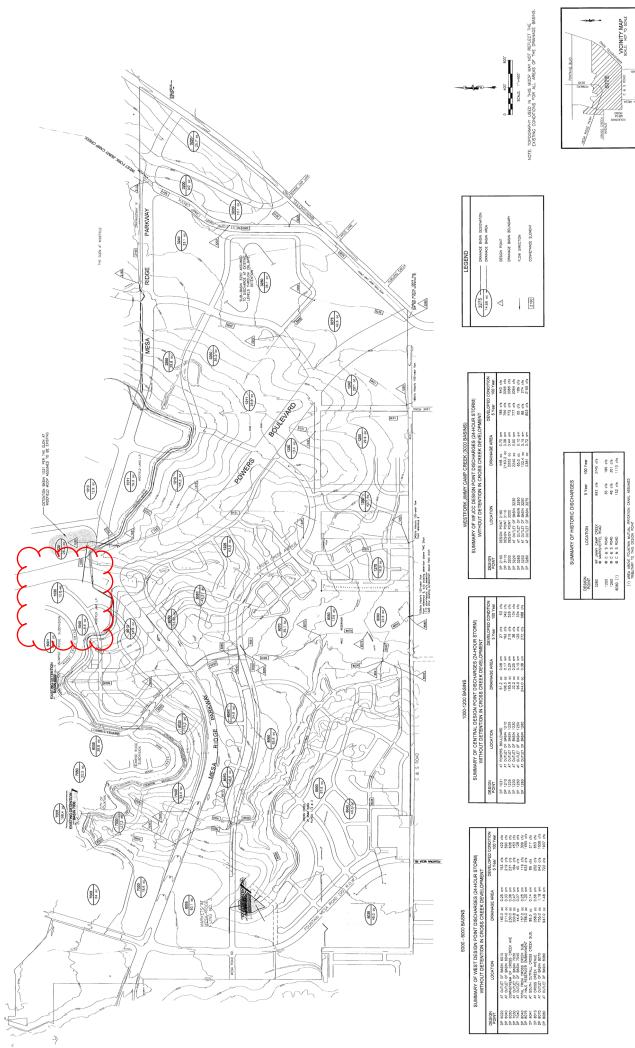
Prepared For:

Norwood Development 111 South Tejon #222 Colorado Springs, CO 80903

Prepared By:

Kiowa Engineering Corporation 1604 South 21st Street Colorado Springs, Colorado 80904

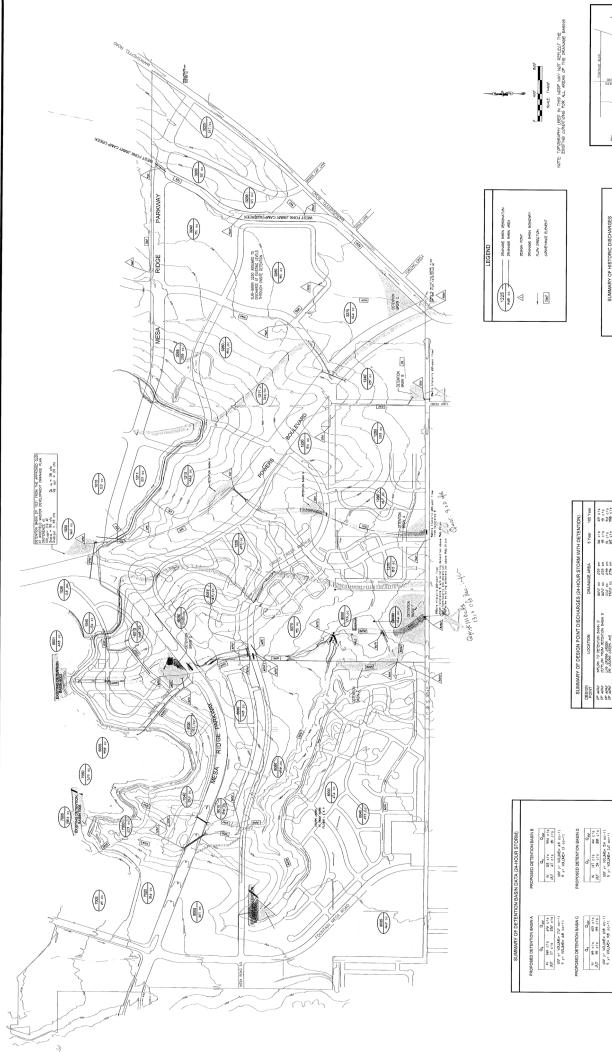
Project Number 05011 December 17, 2006





MESA RIDGE DEVELOPMENT
MASTER DEVELOPMENT DRAINAGE PLAN UPDATE
HYDROLOGIC SUB-BASIN MAP
DEVELOPED WITHOUT REGIONAL DETENTION
& DRAINAGEWAY IMPROVEMENTS
FOUNTAIN, COLORADO **EXHIBIT 1**

Kiowa Engineering Corporation 1604 South 21st Street Correct Springs, Colorado 80904 - 4208 (719) 80-7342





0, 0,000 0,0 ROPOSED DETENTION BASIN G

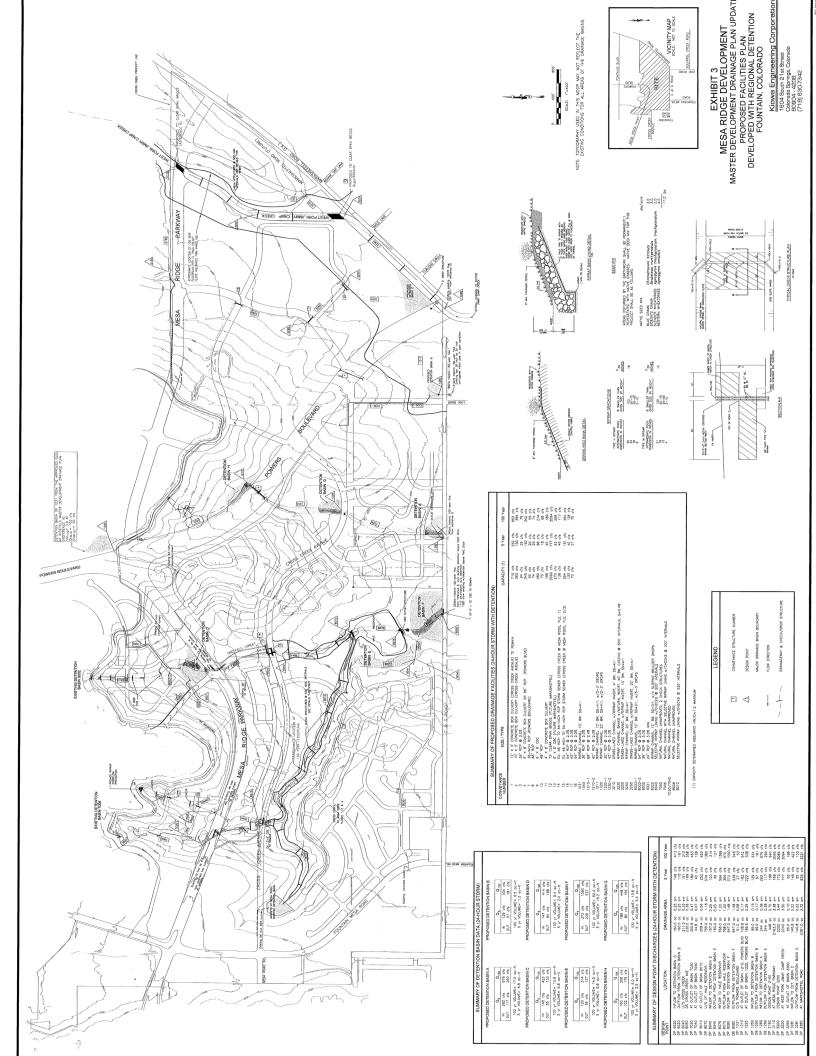
)EC	LEGEND			
225	PRANVEE PASH PESSAUTION PRANVEE PASH AREA	×.		
	PESIGN PONT			
	PRAINGE BASIN BOURDARY	·		
1	PLOW DRECTON			
2100	CONEYNICE ELEMENT			
			NOTE: TOPOGRAPI EXISTING C	A. 0
			L	- 1
SUMMARY OF HISTORIC DISCHARGES	ORIC DISCHARGES		<u></u>	3/
LOCATION	5 Year	100 Year	-	
WF JAMY CAMP CREEK & MARKSPETFEL ROAD	992 ofs	\$145 cis	0	5
8 C & 5 ROND	St ofs	Se ots		
8 0 2 5 RONO 8 0 2 5 RONO	Albors 192 of s	Mo ets Illo ets		
E PONTAN MITHE IRRIGATION CANAL ASSUMED	MILDN CANAL ASSUMED			

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NOTE: TOPOGRAPH		DISCHARGES	5 Year 100 Year	992 of a 9745 of a	75 of a 154 of a 154 of a 155	I CAVAL, MESUAED	

VICINITY MAP

MESA RIDGE DEVELOPMENT
MASTER DEVELOPMENT DRAINAGE PLAN UPDAT
HYDROLOGIC SUB-BASIN MAP
DEVELOPED WITH DETERTION
FOUNTAIN, COLORADO

Kiowa Engineering Corporation 1604 South 21st Street Colorado Springs, Colorado 80904 - 4208 (719) 630-7342



GENERAL NOTES

- 1. ALL WORK REQUIRED OF THESE PLANS SHALL BE COMPLETED IN ACCORDANCE WITH CITY OF COLORADO SPRINGS, ENGINEERING DIVISION, STANDARD SPECIFICATIONS, AND WITH THE APPLICABLE SECTIONS OF THE COLORADO DEPARTMENT OF TRANSPORTATION. STANDARD SPECIFICATIONS FOR ROAD AND BRIDGE CONSTRUCTION.
- 2. THE CONTRACTOR IS RESPONSIBLE FOR THE FIELD VERIFICATION OF ALL PUBLIC AND PRIVATE UTILITIES PRIOR TO THE COMMENCEMENT OF WORK. THE UTILITIES SHOWN ON THESE PLANS HAVE BEEN LOCATED USING THE BEST AVAILABLE INFORMATION. SHOULD A UTILITY BE DAMAGED AS A RESULT OF THIS CONSTRUCTION, IT SHALL BE REPAIRED IMMEDIATELY BY EITHER THE CONTRACTOR OR THE AFFECTED UTILITY OWNER. THE FULL COST OF SUCH A REPAIR SHALL BE THE RESPONSIBILITY OF THE
- 3. SURFACE AND GROUNDWATER AT THE SITE MAY CREATE A NEED FOR DEWATERING DURING THE CONSTRUCTION OF THE DRAINAGEWAY FACILITIES. CONTRACTOR SHALL BE RESPONSIBLE FOR THE MAINTENANCE OF TEMPORARY DEWATERING STRUCTURES, AND PROVIDE FOR THE SAFE AND STABLE DISCHARGE OF WATER FROM THE CONSTRUCTION SITE. THE COST OF DEWATERING IS CONSIDERED INCIDENTAL TO THE CONSTRUCTION AND WILL NOT BE PAID FOR UNDER A SPECIFIC ITEM IN THE BID DOCUMENTS.
- 4. CLASS III RCP SHALL BE USED FOR ALL STORM SEWERS UNLESS OTHERWISE SPECIFIED.
- 5. THE CONTRACTOR SHALL NOTIFY THE CITY OF FOUNTAIN DEPARTMENT OF PUBLIC WORKS 48 HOURS PRIOR TO THE START OF CONSTRUCTION TO OUTLINE METHODS OF CONSTRUCTION, SCHEDULING, AND ISSUING OF INSPECTION PERMITS.

STRUCTURAL CONCRETE NOTES

- 1. ALL CONSTRUCTION INVOLVING THE PLACEMENT OF STRUCTURAL CONCRETE SHALL BE COMPLETED IN ACCORDANCE WITH SECTION 600 OF THE CITY OF COLORADO SPRINGS ENGINEERING DIVISION STANDARD SPECIFICATIONS.
- 2. STEEL REINFORCING SHALL BE GRADE 60 FOR ALL REINFORCING STEEL GREATER THAN #4. A TABLE SPECIFYING MINIMUM SPLICE LENGTHS HAS BEEN PROVIDED ON THE STRUCTURAL DETAIL SHEETS. ALL REINFORCING SHALL HAVE A 2-INCH MINIMUM COVER UNLESS OTHERWISE SPECIFIED. REBAR SHOP DRAWINGS SHALL BE SUBMITTED TO THE ENGINEER FOR REVIEW
- 3. CAST-IN-PLACE CONCRETE SHALL HAVE A MINIMUM COMPRESSIVE STRENGTH (F'C) OF 4,000 PSI AT 28 DAYS. ALL CONCRETE PLACED AGAINST SOIL SHALL BE TYPE II/V PORTLAND CEMENT. ALL EXPOSED CORNERS SHALL BE FORMED WITH A 3/4" CHAMFER UNLESS OTHERWISE SPECIFIED.
- 4. EXPANSION JOINT MATERIAL SHALL MEET AASHTO SPECIFICATION M-213.
- 5. BACKFILL AGAINST STRUCTURES SHALL NOT COMMENCE UNTIL ALL SUPPORTING DIAPHRAGMS ARE IN PLACE AND CONCRETE HAS OBTAINED ITS FULL SEVEN DAY STRENGTH. BACKFILL SHALL BE PLACED EQUALLY ON EACH SIDE OF CHECK STRUCTURES AND CUTOFF WALLS UNTIL THE FINAL GRADE IS REACHED.
- 6. FOOTING EXCAVATIONS SHALL BE EXAMINED BY THE GEOTECHNICAL ENGINEER PRIOR TO THE FORMING AND PLACING OF CONCRETE.
- 7. CONTRACTOR IS RESPONSIBLE FOR PROVIDING THE ENGINEER AND GEOTECHNICAL ENGINEER WITH A 24-HOUR MINIMUM NOTIFICATION FOR REBAR OBSERVATION, SOIL AND/OR CONCRETE TESTING. PLACEMENT OF CONCRETE IN THE ABSENCE OF TESTING SHALL BE COMPLETED AT THE SOLE RISK OF THE CONTRACTOR.

- A. NO ADMIXTURES PERMITTED WITHOUT THE REVIEW OF ENGINEER. SUBMIT DESIGN MIX FOR ENGINEER APPROVAL.
- B. CONTRACTOR IS RESPONSIBLE FOR THE ADEQUACY OF FORMS AND SHORING AND FOR SAFE PRACTICE IN THEIR USE AND REMOVAL. C. COMPRESSIVE STRENGTH SHALL BE 4,000 psi, MIN.

9. REINFORCING STEEL:

- A. TO BE BILLET STEEL CONFORMING TO THE LATEST A.S.T.M/ A615 GRADE 60 SPECIFICATION, FABRICATED IN ACCORDANCE WITH MANUAL OF STANDARD PRACTICE OF THE C.R.S.I. AND PLACED IN ACCORDANCE WITH A.C.I. 315 AND A.C.I. MANUAL OF PRACTICE.
- B. MINIMUM OF CONCRETE COVER UNLESS OTHERWISE DETAILED ON DRAWINGS: FOOTINGS 3 INCHES, WALLS 3 INCHES, SLABS EXPOSED TO WEATHER 1-1/12 INCHES, SLABS ON GRADE 1-1/2 INCHES MEASURED FROM TOP OF SLAB.
- C. SLAB REINFORCEMENT: LAPPED 36 BAR DIAMETER OR MINIMUM 18 INCHES. BOTTOM BARS SPLICED ONLY AT SUPPORTS, TOP BARS SPLICED ONLY AT MID-SPAN. ALL TOP BARS HOOKED AT NON-CONTINUOUS EDGES (U.O.N.) ALL HOOKS TO BE STANDARD 90 DEGREE OR 180 DEGREE HOOKS AS REQUIRED (U.O.N.), DOWELS IN FOUNDATION TO MATCH REINFORCING ABOVE.
- D. SUBMIT SHOP DRAWINGS FOR REINFORCING PRIOR TO FABRICATION.

10. FOUNDATIONS:

- A. STRUCTURES SHALL BEAR ON SOIL HAVING A MINIMUM BEARING CAPACITY OF 2,000 P.S.F. COMPACTION FOR SUBGRADE PREPARATION SHALL BE IN ACCORDANCE WITH REQUIREMENTS OF THE SOILS REPORT. SUBGRADE PREPARATION SHALL BE MONITORED BY THE SOILS ENGINEER.
- .11. BACKFILL AND STABILIZATION MATERIAL
- A. BACKFILL MATERIAL CONSISTING OF SELECT, GRANULAR, NON-SWELLING MATERIAL TO BE PLACED ALONG THE SIDES OF THE VAULTS EXTENDING 3 FEET OUTSIDE THE VAULT WALLS.
- B. 3/4-INCH ROCK, 12-INCHES DEEP, TO BE PLACED UNDER ALL VAULTS. C. 2-INCH TO 4-INCH STABILIZATION MATERIAL SHALL BE PLACED UNDER THE 3/4" ROCK IF SUBGRADE STABILIZATION IS REQUIRED.

12. ABBREVIATIONS

E.C -- EPOXY COATED O.F. -- OUTSIDE FACE E.F. -- EACH FACE I.F. -- INSIDE FACE N.F. -- NEAR FACE T.O.C. -- TOP OF CONCRETE B.O.C. -- BOTTOM OF CONCRETE CONT. -- CONTINUOUS

INDEX OF SHEETS

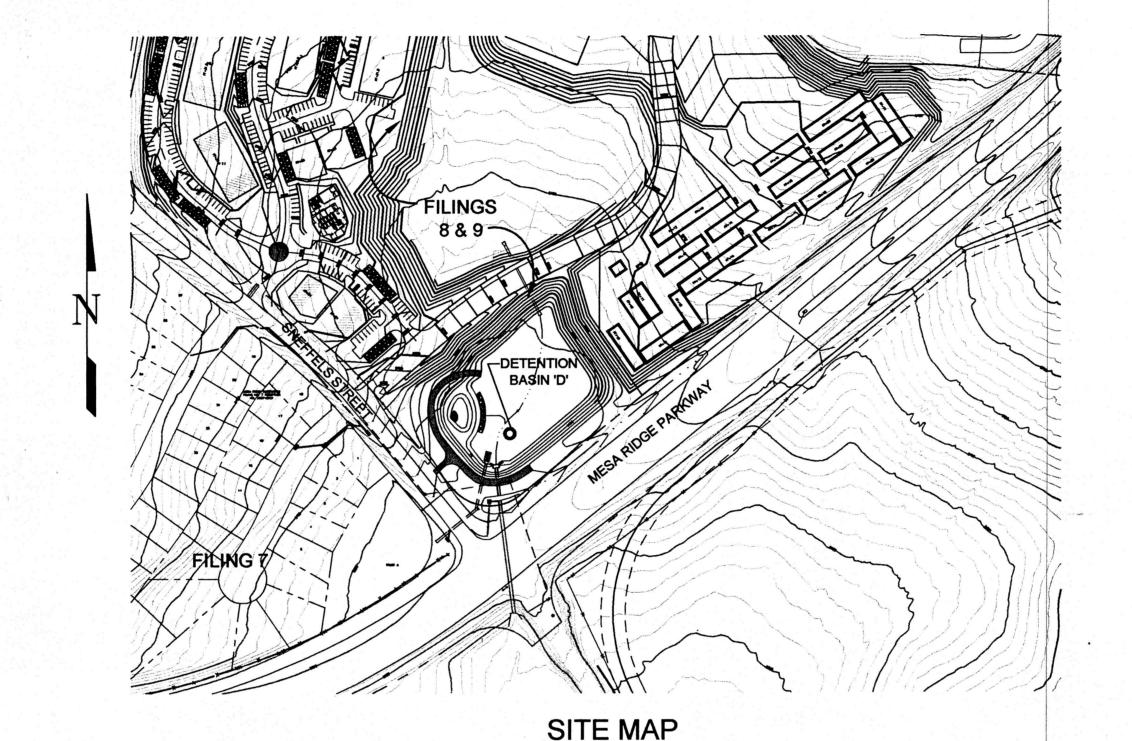
- COVER SHEET
- 2 GRADING AND EROSION CONTROL PLAN & STORM PROFILE
- 3 OUTLET STRUCTURE DETAILS

ABBREVIATIONS PVC = POINT OF VERTICAL CURVATURE ASSY = ASSEMBLYHORIZ.= HORIZONTAL PVI = POINT OF VERTICAL INTERSECTION BNDY = BOUNDARY HYD = HYDRANTPVT = POINT OF VERTICAL TANGENCY B.O.P. = BOTTOM OF PIPEI.D. = INSIDE DIAMETER RCB = REINFORCED CONCRETE BOX = LEFT CL = CENTERLINE RCP = REINFORCED CONCRETE PIPE CRA = CONCRETE REVERSE ANCHOR LF = LINEAR FEET ROW = RIGHT OF WAY LP = LOW POINT CTRB = CONCRETE THRUST BLOCK RT = RIGHT CR = POINT OF CURB RETURN MAX. = MAXIMUM SHT = SHEET DIP = DUCTILE IRON PIPE M.H. = MANHOLE SS = SANITARY SEWER MIN. = MINIMUM EL = ELEVATION STA. = STATION ESMT = EASEMENTNTS = NOT TO SCALE O.D. = OUTSIDE DIAMETER STD. = STANDARD EX. = EXISTING T.O.P. = TOP OF PIPE FC = FACE OF CURB PC = POINT OF HORIZONTAL CURVATURE PCHC = POINT OF CURVATURE ON HORIZ. CURVE TYP. = TYPICAL FES = FLARED END SECTION VC = VERTICAL CURVE FLG = FLANGE PT = POINT OF HORIZONTAL TANGENCY VERT. = VERTICAL FL = FLOWLINE PTHC = POINT OF TANGENCY ON HORIZ. CURVE GB = GRADE BREAK HP = HIGH POINT PVC = POLY VINYL CHLORIDE PIPE

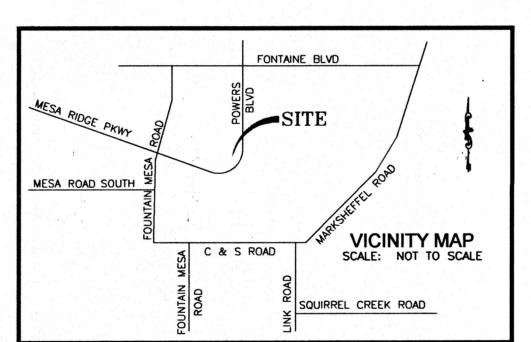
MESA RIDGE FILINGS 8 & 9

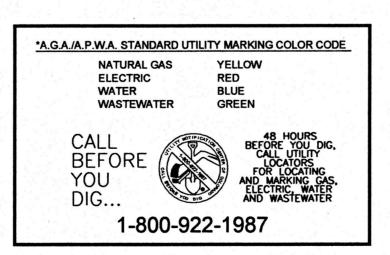
DETENTION BASIN 'D' FULL SPECTRUM DETENTION MODIFICATIONS FINAL DESIGN DRAWINGS

FOUNTAIN, COLORADO



SCALE: 1"=200'





DUANE GREENWOOD, PUBLIC WORKS DIR./CITY ENGINEER DETAILED DRAINAGE CONSTRUCTION PLANS & SPECIFICATIONS **ENGINEER'S STATEMENT:** THESE DETAILED PLANS AND SPECIFICATIONS WERE PREPARED UNDER MY DIRECTION AND SUPERVISION. SAID DETAILED PLANS AND SPECIFICATIONS HAVE BEEN PREPARED ACCORDING TO THE CRITERIA ESTABLISHED BY THE CITY FOR DETAILED DRAINAGE PLANS AND SPECIFICATIONS SAID DETAILED DRAINAGE PLANS AND SPECIFICATIONS MEET THE PURPOSES FOR WHICH THE PARTICULAR DRAINAGE FACILITY(S) IS DESIGNED. I ACCEPT RESPONSIBILITY FOR LIABILITY CAUSED BY NEGLIGENT ACTS, ERRORS OR OMISSIONS ON MY PART IN PREPARATION OF THE DETAILED DRAINAGE PLANS AND SPECIFICATIONS. RICHARD N. WRAY P.E. #19310 DEVELOPER \ NOR'WOOD DEVELOPMENT PLAZA OF THE ROCKIES 11 S. TEJON STREET, SUITE 222 COLORADO SPRINGS, COLORADO 80903

CITY OF FOUNTAIN ACCEPTANCE:

STATEMENTS

THE PLANS OR REPORT SUBMITTED APPEAR TO BE IN CONFORMANCE WITH THE CITY OF

PRACTICES APPEAR TO HAVE BEEN FOLLOWED. THE PROFESSIONAL ENGINEER SUBMITTING

AND SEALING THE PLANS OR REPORT IS SOLELY RESPONSIBLE FOR THEIR ACCURACY AND

DATE

FOUNTAIN SUBMITTAL REQUIREMENTS AND STANDARD ENGINEERING PRINCIPALS AND

VALIDITY. THIS REVIEW IS ONLY VALID FOR ONE (1) YEAR FROM THE DATE BELOW.

Kiowa Project No. 09061 October 25, 2011

PROJECT SPECIFIC GRADING AND EROSION CONTROL NOTES

- 1. All earthwork required of this construction shall be completed in accordance with all applicable sections of the Project
- Specifications and Soil Investigation Report (Geotechnical Report). 2. Rubbish including timber, concrete rubble, trees, brush, and asphalt shall not be backfilled adjacent to any of the structures or be in the placement of any unclassified fill. The Contractor shall be responsible for the removal and hauling of such materials to a suitable spoil area. Costs associated with the removal of such materials shall be paid for as documented in the Project
- 3. Excess excavation shall become the property of the Contractor and shall be disposed of at the Contractor's expense. The cost of
- haulage and spoiling of excess excavated materials shall be paid for as documented in the Project Specifications. 4. Water shall be used as a dust palliative as required and shall be included in the cost for earthwork item(s). No separate payment will be made for dust control associated with the site construction.
- 5. The road grades shall be cleared of vegetation and the topsoil stockpiled for later use.
- 6. All grading shall be in conformance with the Geotechnical Report for the area. . Placement of fill for roadway embankments shall be completed in conformance with the Geotechnical Report.
- 8. Grading contours shown on this plan are to final grade.
- 9. Compaction under filled areas, including roadway and detention basin embankments, shall be 95 percent of the maximum
- Standard Proctor Density (ASTM D698) at two (2) percent of optimum moisture content. 10. No rubble or debris shall be placed in the backfill under any of the proposed buildings, streets, curb & gutter, sidewalk and drainage structures or within five (5) feet of a building footprint. Properly graded rubble may be used in some locations as
- specified and verified by the Geotechnical Engineer. 11. Contractor is responsible for reviewing the site prior to bidding to verify site conditions.
- 12. Contractor is responsible for providing erosion control measures as approved by the City of Fountain Dept. of Public Works
- Division and as may be required by the El Paso County Inspector. 13. All slopes equal to or greater than 3:1 shall require erosion control blanket, single netted fabric, American Excelsior or equal.
- 14. The Developer is responsible for maintaining erosion control measures until a mature stage of vegetation is established.
- 15. All soils used for fill must be approved by a representative of the Geotechnical Engineer.
- 16. All natural ground to receive fill must be properly scarified, watered and compacted prior to placing fill.
- 17. The Contractor is solely responsible for the design, maintenance and operation of any required dewatering system. The Contractor shall perform such independent investigation as he deems necessary to satisfy himself as to the subsurface groundwater conditions and unstable soil conditions to be encountered throughout the construction.
- 18. No fill shall be placed, spread or rolled while it is frozen, thawing or during unfavorable weather conditions. When the work is interrupted by heavy rain, fill operations shall not be resumed until a representative of the Geotechnical Engineer indicates that the moisture content and density of the previously placed fill are as specified. Fill surfaces may be scarified and recompacted after rainfall if necessary, to obtain proper moisture density relation.
- 19. Additional erosion control structures and/or grading may be required at the time of construction.
- 20. Sediment removal for erosion control facilities shall be performed continuously for proper function.
- 21. Base mapping was provided by Rockwell Consulting. The date of the survey was January 2008. 22. Proposed Construction Schedule:
- Begin Construction: 60-TO GER 25, 2011 End Construction: FEBRUARY 28, 2017
- Total Site Area = 3.6 Acres 23. Area to be disturbed = 3.6 Acres (est.) Existing 100-year runoff coefficient = 0.40 Proposed 100-year runoff coefficient = 0.40

DAMAGE TO ADJACENT PROPERTY.

- Existing Hydrological Soil Groups: B & C
- 24. Site is currently undeveloped and covered with native grasses on mild slopes (2%-7%). 25. Site is located in the Jimmy Camp Creek Drainage Basin.
- 26. All grading and erosion control shall be completed in accordance with the City of Fountain Municipal Code Sections 12.04.160

GRADING AND EROSION CONTROL NOTES

- 1. ALL GRADING AND EROSION CONTROL SHALL BE COMPLETED IN ACCORDANCE WITH THE CITY OF FOUNTAIN
- MUNICIPAL CODE SECTIONS 12.04.160 AND 12.10.
- 2. ALL FILL AREAS SHALL BE COMPACTED IN ACCORDANCE WITH THE GEOTECHNICAL ENGINEER'S RECOMMENDATIONS.
- SOIL EROSION CONTROL MEASURES FOR ALL SLOPES, CHANNELS, DITCHES, OR ANY DISTURBED LAND AREA SHALL BE COMPLETED WITHIN TWENTY ONE (21) CALENDAR DAYS AFTER FINAL GRADING, OR FINAL EARTH DISTURBANCE HAS BEEN COMPLETED. AN AREA THAT IS GOING TO REMAIN IN AN INTERIM STATE FOR MORE THAN 60 DAYS SHALL ALSO BE SEEDED. ALL TEMPORARY SOIL EROSION CONTROL MEASURES AND BMPS SHALL BE MAINTAINED UNTIL PERMANENT SOIL EROSION CONTROL MEASURES ARE IMPLEMENTED.
- 4. EROSION CONTROL SHALL CONSIST OF SILT FENCES AND HAY BALES AS SHOWN ON THE DRAWING, AND TOPSOIL WITH GRASS SEED WHICH WILL BE WATERED UNTIL VEGETATION HAS BEEN REESTABLISHED.
- 5. EROSION CONTROL BALES OR SILT FENCE SHALL BE PLACED AT THE TOE AND DRAINAGE OUTFALL POINTS OF ALL SLOPES 4:1 OR STEEPER TO PREVENT SILTATION ON STREETS. REFER TO STORM WATER MANAGEMENT PLAN FOR DETAIL AND LOCATION OF EROSION CONTROL MEASURES.
- 6. CONTRACTOR SHALL COMPLY WITH ALL LOCAL, COUNTY AND STATE REGULATIONS PERTAINING TO GRADING, DUST
- NATURAL VEGETATION SHALL BE RETAINED AND PROTECTED WHEREVER POSSIBLE. EXPOSURE OF SOIL TO EROSION BY REMOVAL OR DISTURBANCE OF VEGETATION SHALL BE LIMITED TO THE AREA REQUIRED FOR
- IMMEDIATE CONSTRUCTION OPERATIONS AND FOR THE SHORTEST PRACTICAL PERIOD OF TIME. 8. TOPSOIL SHALL BE STOCKPILED TO THE EXTENT PRACTICABLE ON THE SITE FOR USE ON AREAS TO BE
- REVEGETATED. ANY AND ALL STOCKPILES SHALL BE LOCATED AND PROTECTED FROM EROSIVE ELEMENTS. AT ALL TIMES, THE PROPERTY SHALL BE MAINTAINED AND/OR WATERED TO PREVENT WIND-CAUSED EROSION. EARTHWORK OPERATIONS SHALL BE DISCONTINUED WHEN FUGITIVE DUST SIGNIFICANTLY IMPACTS ADJACENT PROPERTY. IF EARTHWORK IS COMPLETE OR DISCONTINUED AND DUST FROM THE SITE CONTINUES TO CREATE PROBLEMS, THE OWNER/DEVELOPER SHALL IMMEDIATELY INSTITUTE MITIGATIVE MEASURES AND SHALL CORRECT
- 10. ALL PERSONS ENGAGED IN EARTH DISTURBANCE SHALL IMPLEMENT AND MAINTAIN ACCEPTABLE SOIL EROSION AND SEDIMENT CONTROL MEASURES INCLUDING BMPS IN CONFORMANCE WITH THE EROSION CONTROL TECHNICAL STANDARDS OF THE MANUAL AND IN ACCORDANCE WITH THE EROSION AND STORMWATER QUALITY CONTROL PLAN APPROVED BY THE CITY OF FOUNTAIN, IF REQUIRED.
- 11. ALL EARTH DISTURBANCE SHALL BE CONDUCTED IN SUCH A MANNER SO AS TO EFFECTIVELY REDUCE
- ACCELERATED SOIL EROSION. 12. ALL EARTH DISTURBANCE SHALL BE DESIGNED, CONSTRUCTED, AND COMPLETED IN SUCH A MANNER SO THAT THE
- EXPOSED AREA OF ANY DISTURBED LAND SHALL BE LIMITED TO THE SHORTEST PRACTICAL PERIOD OF TIME. 13. ALL EARTH DISTURBANCE SHALL BE DONE IN A MANNER THAT MINIMIZES POLLUTION OF ANY ON-SITE OR OFF-SITE
- 14. SUSPENDED SEDIMENT CAUSED BY ACCELERATED SOIL EROSION SHALL BE MINIMIZED IN RUNOFF WATER BEFORE
- 15. TEMPORARY SOIL EROSION CONTROL FACILITIES SHALL BE REMOVED AND EARTH DISTURBANCE AREAS GRADED AND STABILIZED WITH PERMANENT SOIL EROSION CONTROL MEASURES PURSUANT TO THE STANDARDS AND SPECIFICATIONS PRESCRIBED IN THE MANUAL, AND IN ACCORDANCE WITH THE PERMANENT EROSION CONTROL FEATURES SHOWN ON THE EROSION AND STORMWATER CONTROL PLANS APPROVED BY THE CITY OF FOUNTAIN, IF
- ANY STREET OR DRAINAGE FACILITY WHICH HAS HAD EROSION SEDIMENT DEPOSITED IN IT DUE TO CONSTRUCTION, GRADING, OR OTHER DEVELOPMENT ACTIVITY, MUST BE CLEANED IMMEDIATELY AT THE EXPENSE OF THE CONTRACTOR, DEVELOPER, HOMEBUILDER, OR WHOEVER IS RESPONSIBLE FOR THE CONSTRUCTION, GRADING, OR LAND DEVELOPMENT ACTIVITY. IF THE FACILITY IS NOT CLEANED IMMEDIATELY OR WITHIN A RESPONSIBLE PERIOD OF TIME AFTER NOTIFICATION BY THE CITY, THE CITY MAY PERFORM THE WORK OR HAVE THE WORK DONE AND
- BILL THE RESPONSIBLE PARTY. 17. IT IS THE RESPONSIBILITY OF THE OWNER TO ENSURE THAT VEHICLE TRACKING CONTROL IS IN PLACE,
- FUNCTIONAL, AND MAINTAINED THROUGHOUT THE CONSTRUCTION PHASE OF THIS PROJECT. 18. INDIVIDUALS SHALL COMPLY WITH THE "COLORADO WATER QUALITY CONTROL ACT" (TITLE 25, ARTICLE 8, CRS), AND THE "CLEAN WATER ACT" (33USC 1344), REGULATIONS PROMULGATED, CERTIFICATIONS OR PERMITS ISSUED, IN ADDITION TO CITY OF FOUNTAIN REQUIREMENTS. IN THE EVENT OF CONFLICTS BETWEEN THESE REQUIREMENTS, THE MORE RESTRICTIVE LAWS, RULES, OR REGULATIONS SHALL APPLY.

PREPARED BY:

DEVELOPER:

NOR'WOOD DEVELOPMENT

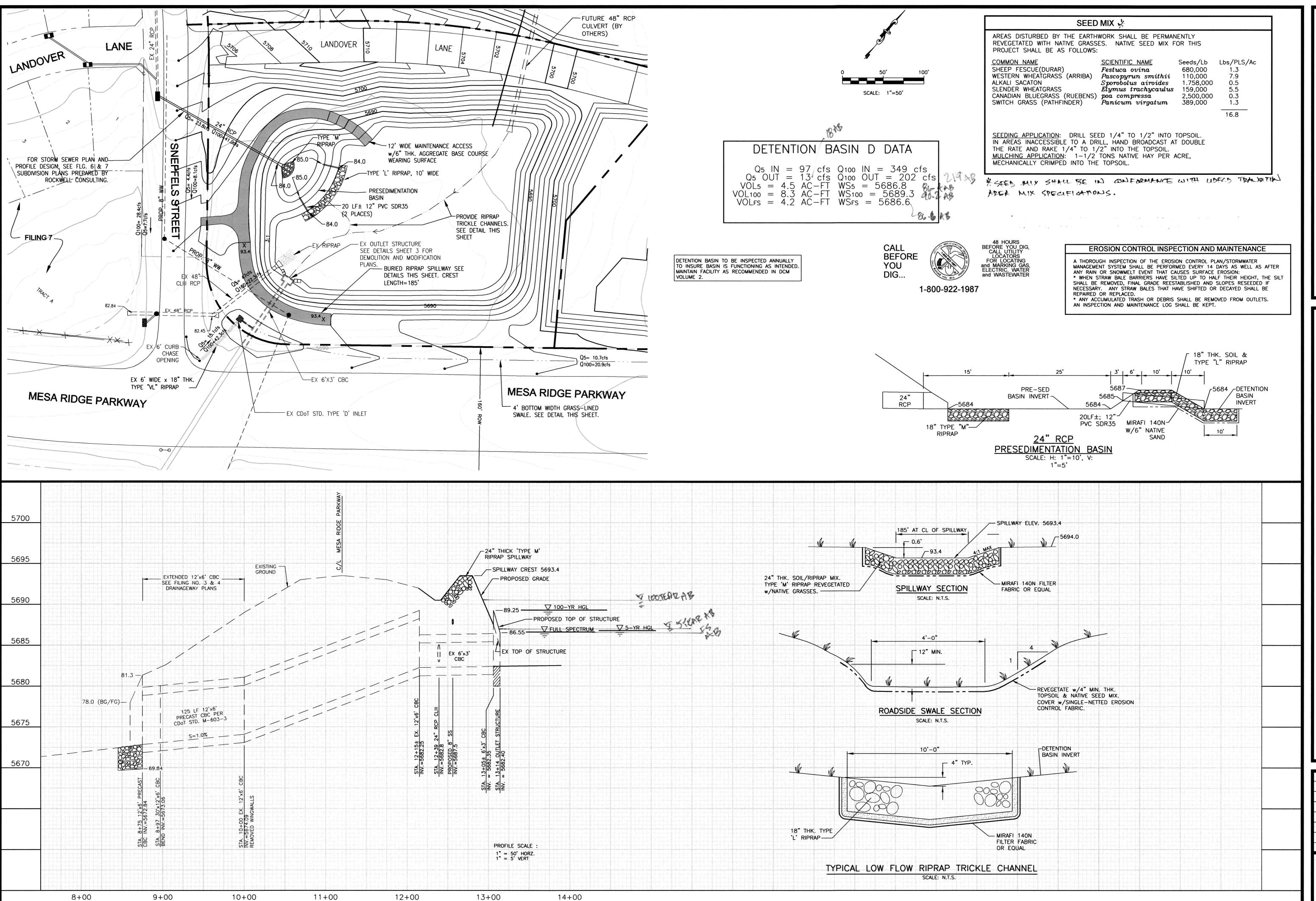
PLAZA OF THE ROCKIES

11 S. TEJON STREET, SUITE 222

COLORADO SPRINGS, COLORADO 80903

Kiowa Engineering Corporation

1604 South 21st Street Colorado Springs, Colorado 80904-4208 [719] 630-7342



9 - DETENTION BASIN 'D'
TION MODIFICATIONS
OL PLAN AND STORM PROFILE

Kiowa Engineerin
1604 South 21st Street
Colorado Springs, Colorad
719] 630-7342

ESA RIDGE FILINGS 8 & 9 - DETENTION BASIN FULL SPECTRUM DETENTION MODIFICATIONS RADING AND EROSION CONTROL PLAN AND STORM PROF FOUNTAIN, COLORADO

Project No.: 09061

Date: October 17, 2011

Design: RNW

Drawn: JGD

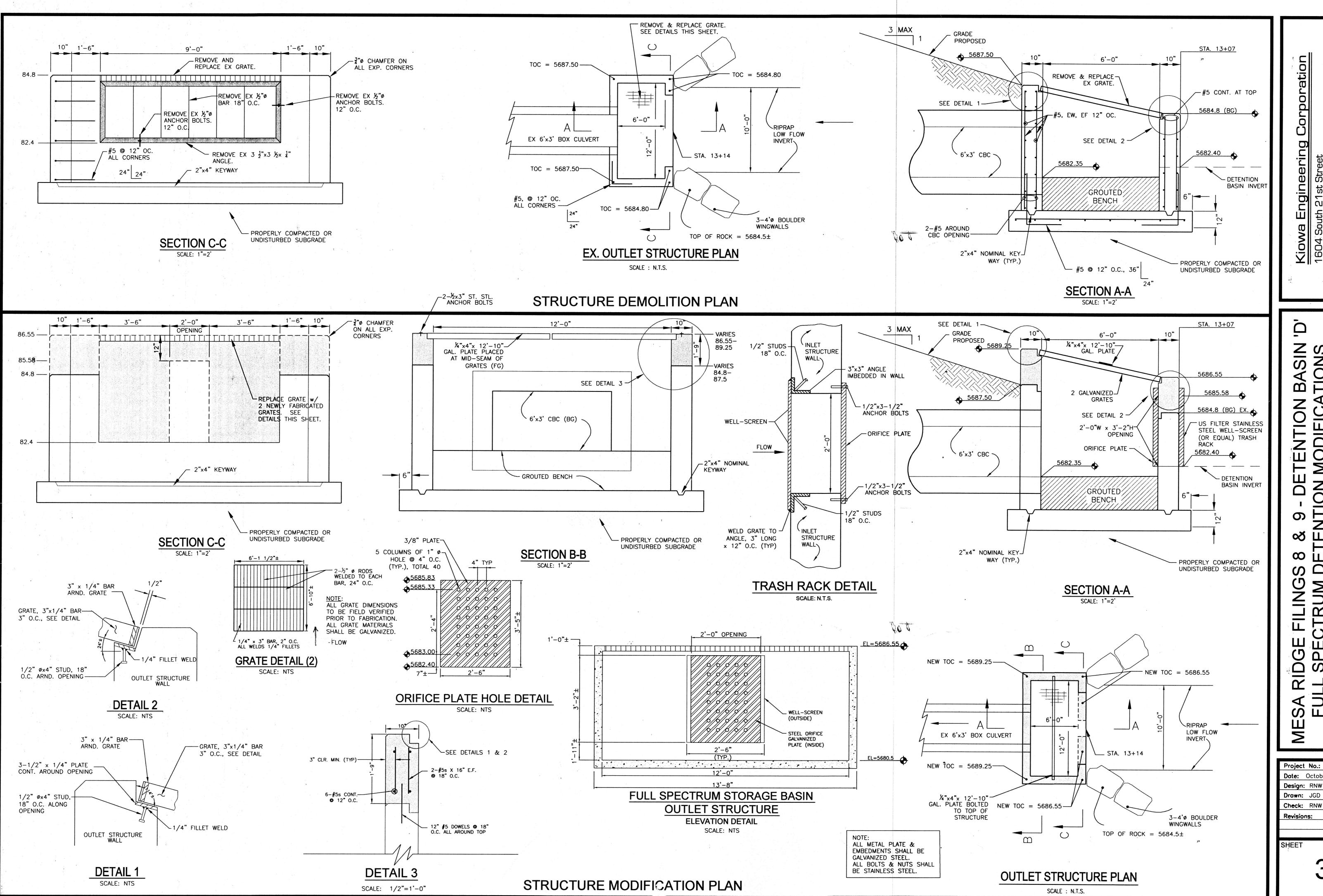
Check: RNW

Revisions:

SHEET

OF 3 SHEETS

0906102PP.dwg/Oct 24, 20



1604 South 21st S Colorado Springs, (80904-4208 (719) 630-7342 FILING RIDGE LL SPE(

Project No.: 09061 Date: October 24, 2011 Design: RNW Drawn: JGD Check: RNW Revisions: SHEET

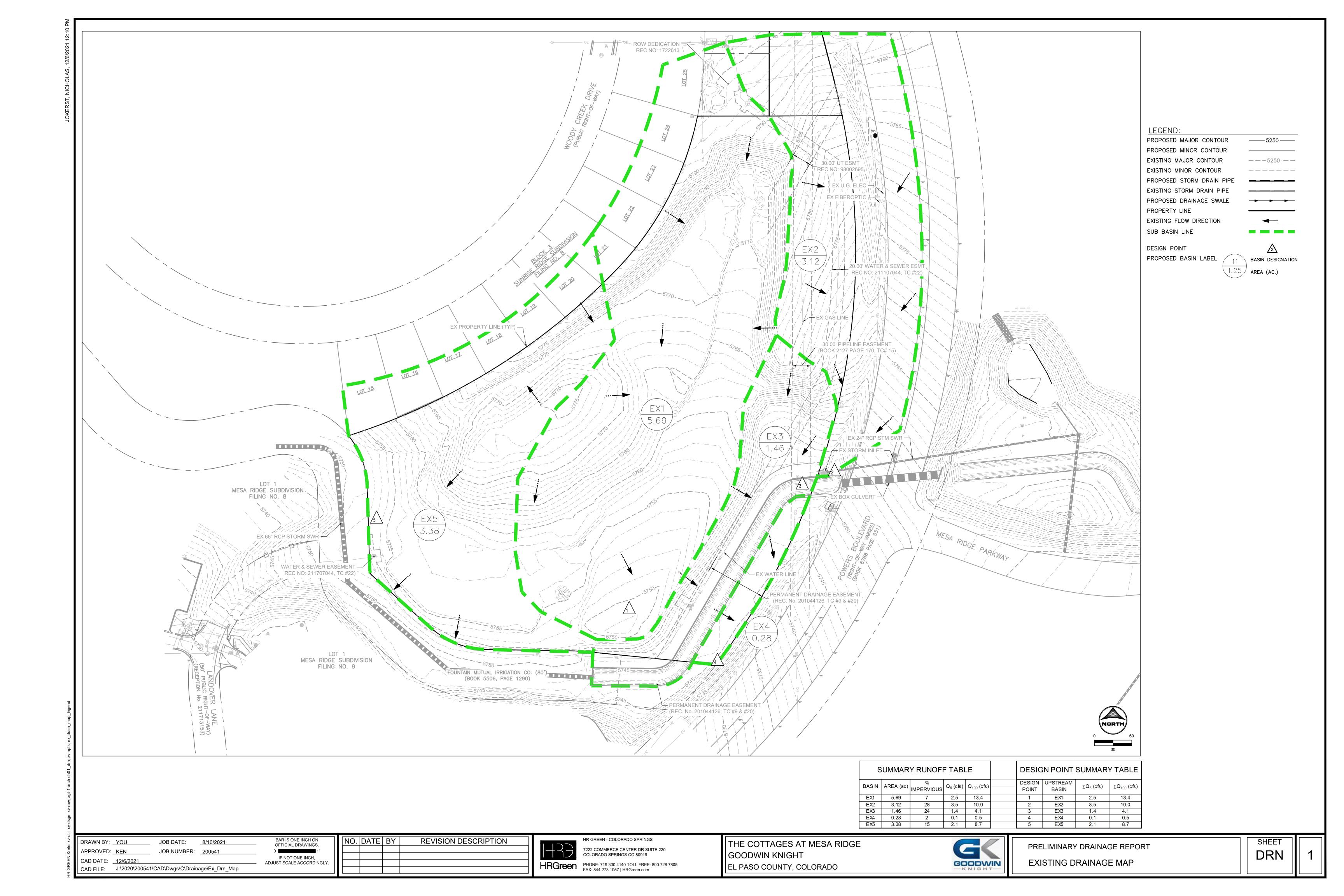
OF 3 SHEETS

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APPENDIX F - DRAINAGE MAPS





LEGEND: PROPOSED MAJOR CONTOUR PROPOSED MINOR CONTOUR EXISTING MAJOR CONTOUR EXISTING MINOR CONTOUR PROPOSED STORM DRAIN PIPE EXISTING STORM DRAIN PIPE PROPOSED DRAINAGE SWALE PROPERTY LINE PROPOSED FLOW DIRECTION EXISTING FLOW DIRECTION SUB BASIN LINE DESIGN POINT 11 BASIN DESIGNATION PROPOSED BASIN LABEL 1.25 AREA (AC.)

BASIN	AREA (ac)	% IMPERVIOUS	Q ₅ (cfs)	Q ₁₀₀ (cfs)
1	3.56	63	7.6	16.1
2	4.93	59	9.5	20.3
3	3.03	29	3.4	9.7
4	0.52	8	0.4	1.8
5	1.50	32	2.1	5.7
6	0.63	2	0.2	1.2
7	0.56	26	0.5	1.6
8	0.24	100	1.1	2.0
9	0.14	100	0.7	1.2

DESIG	SN POINT	SUMMAR'	Y TABLE

DESIGN POINT	UPSTREAM BASIN	ΣQ_5 (cfs)	∑Q ₁₀₀ (cfs)
1	1	7.6	16.1
2	2	9.5	20.3
2.1	3	15.6	29.9
3	4	3.4	9.7
4	5	0.4	1.8
5	5	2.1	5.7
6	6	0.2	1.2
7	7	0.5	1.6
8	8	1.1	2.0
9	9	1.1	1.2
9.1	8&9	17.1	39.6

 DRAWN BY:
 NQJ
 JOB DATE:
 12/6/2021
 BAR IS ONE INCH ON OFFICIAL DRAWINGS.

 APPROVED:
 KMH
 JOB NUMBER:
 200541
 0
 IF NOT ONE INCH, ADJUST SCALE ACCORDINGLY.

 CAD DATE:
 12/17/2021
 J:\2020\200541\CAD\Dwgs\C\Drainage\Pr'_Drn_Map
 ADJUST SCALE ACCORDINGLY.

NO. DATE BY REVISION DESCRIPTION

HR GREEN - COLORADO SPRINGS

7222 COMMERCE CENTER DR SUITE 220
COLORADO SPRINGS CO 80919

HRGreen

PHONE: 719.300.4140 TOLL FREE: 800.728.7805
FAX: 844.273.1057 | HRGreen.com

THE COTTAGES AT MESA RIDGE
GOODWIN KNIGHT
EL PASO COUNTY, COLORADO



PRELIMINARY DRAINAGE REPORT
PROPOSED DRAINAGE MAP

SHEET

Draiange Report _V2.pdf Markup Summary 2-14-2022

Daniel Torres (4)



Subject: Callout Page Label: 6

Author: Daniel Torres Date: 2/14/2022 12:56:45 PM

Status: Color: Layer: Space:

Please delete the stated date. you may state "current adopted version" if you'd like but it is not necessary. There were no formal changes to the criteria on the date listed (10/31/18). This date listed on the Municode homepage is not reflective of an adopted change to the criteria and may have

been some formating changes.

ect were ta Subject: Pen Page Label: 6

1), dated (Author: Daniel Torres Date: 2/14/2022 9:18:30 AM

rainana Cr Status:

oject were taken from the "*Drainage* CM), dated October 31, 2018, and (*Drainage Criteria Manual*" (CCSDC 19 El Paso County Engineering Cri

Color: Layer: Space:

Subject: Pen Page Label: 6

Author: Daniel Torres Date: 2/14/2022 9:18:33 AM

Status: Color: Layer: Space:

Subject: Cloud+ Page Label: 10 Author: Daniel Torres Date: 2/14/2022 9:01:51 AM

Status: Color: Layer: Space:

Please also provide the bridge fee. The 2021 bridge fee for West Fork Jimmy Camp Creek is

\$4001 per impervious acre.

dotprete (2)



Subject: Engineer Page Label: 39 Author: dotprete

Date: 2/10/2022 3:22:48 PM

Status: Color: Layer: Space:

will require a guard rail or adjust velocity

Subject: Engineer Page Label: 39 Author: dotprete

Date: 2/10/2022 3:23:36 PM

Status: Color: Layer: Space:

Ratio should be less than or equal to 1.