



**MVE, INC.**  
ENGINEERS SURVEYORS

1903 lelaray street, suite 200  
colorado springs, co 80909  
719.635.5736

# Final Drainage Report

## **The Townhomes at Bradley Crossroads**

**Project No. 61093**

**February 14, 2019**

PCD File No. PPR1846

# Final Drainage Report

for

**The Townhomes at Bradley Crossroads**  
Multifamily Residential Community

**Project No. 61093**

**February 14, 2019**

prepared for

**J. Elliott Homes, Inc.**  
12218 Crystal Downs Road  
Peyton, CO 80931  
719.499.8214

prepared by

**MVE, Inc.**  
1903 Lelaray Street, Suite 200  
Colorado Springs, CO 80909  
719.635.5736

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61093-FDR-TH at Bradley Crossing.odt

# Statements and Acknowledgments

## Engineer's Statement

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the County for drainage reports and said report is in conformity with the applicable master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.

  
David R. Gorman, P.E. Colorado No. 31672  
For and on Behalf of MVI, Inc.



2/14/2019  
Date

## Developer's Statement

I, the owner/developer have read and will comply with all of the requirements specified in this drainage report and plan.

  
Printed Name: Jordan Guinane  
Title: President  
J. Elliott Homes, Inc.  
12218 Crystal Downs Road  
Peyton, CO 80931

2/14/2017  
Date

## El Paso County

Filed in accordance with the requirements of the Drainage Criteria Manual, Volumes 1 and 2, El Paso County Engineering Criteria Manual and Land Development Code as amended.

Approved  
by Elizabeth Nijkamp  
El Paso County Planning and Community Development  
on behalf of Jennifer Irvine, County Engineer, ECM Administrator

05/30/2019 6:20:19 PM

Jennifer Irvine, P.E.,  
County Engineer / ECM Administrator

Date

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# Final Drainage Report

The purpose of this Final Drainage Report is to identify drainage patterns and quantities within and affecting the proposed The Townhomes at Bradley Crossroads project located in Lot 1A, Bradley Crossroads Filing No. 1B. This project is the development of the existing platted lot having an area of approximately 5.24± Acres with a multi-family use. The report will “identify specific solutions to problems on-site and off-site resulting from the proposed project.”<sup>1</sup> The report and included maps present results of hydrologic and drainage facilities analyses. The report will discuss the recommended drainage improvements to the site and identify drainage requirements relative to the proposed project. This report has been prepared and submitted in accordance with the requirements of the El Paso County land development approval process. An Appendix is included with this report with pertinent calculations and graphs used in the drainage analyses and design.

## 1 General Location and Description

### 1.1 Location

The proposed The Townhomes at Bradley Crossroads site is located within the southeast one-quarter of Section 2, Township 15 South, Range 66 west of the 6th principal meridian in El Paso County, Colorado. The 5.24± acre site is situated south of Bradley Road and west of Main Street (Hancock Expressway) in the Security-Widefield area. The proposed site is platted as Lot 1A, Bradley Crossroad, Filing No. 1B. A **Vicinity Map** is included in the **Appendix**.

Lincoln Commons Townhomes, zoned PUD CAD-O (Planned Unit Development, Commercial Airport Development District), is adjacent to the property to the west and contains a developed townhome community. Undeveloped Lots 2A, 3A, 4A, 5A, Bradley Crossroads Filing No. 1A, zoned CC CAD-O (Commercial Community, Commercial Airport Development District), are adjacent to the site along the north and east sides. Lot 7A, Bradley Crossroads Filing No. 1A, zoned CC CAD-O (Commercial Community, Commercial Airport Development District), containing a car wash, adjoins the site on the southeast edge. Gladiator Drive is adjacent along the south side of the site. The north and east sides of the site have existing paved private roadways that are shared by the adjoining developed and undeveloped lots.

### 1.2 Description of Property

The The Townhomes at Bradley Crossroads project contains 5.24± acres and is zoned RM-30 (Residential Multi-Dwelling). The property contains no structures, but has a paved private roadways along the north and east sides for access. Utilities also exist around the perimeter of the site, which are available for extension as part of the development of the site.

The site is covered with native prairie grasses and weeds in fair to good condition. There are also small trees and brush scattered throughout the site. The existing site topography exhibits only a moderate amount of relief, but slopes to the south at grades ranging from 0.5% to 1%. There are areas of small mounds and depressions throughout the site. The south edge of the site is encumbered by utility and drainage easements and contains existing storm drain and water mains.

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<sup>1</sup> DCM

There are no major drainageways in the The Townhomes at Bradley Crossroads site. All storm runoff flows south and then west to the southwest corner of the site. These flows are captured in existing storm drain inlets and are conveyed by pipe to the existing storm drain detention pond located at the southwest corner of adjacent Lincoln Commons Townhomes. This pond was designed and constructed to accommodate flows from this site.

The site is located in the Little Johnson Basin and is part of the Little Johnson/Security Creek Basin Planning Study by Kiowa Engineering Corporation dated April 1988.

According to the National Resource Conservation Service, the dominant soil in the immediate area of the The Townhomes at Bradley Crossroads site is Blakeland loamy sand (map unit 8). The Blakeland loamy sand is typically deep and somewhat excessively drained. Permeability is rapid, surface runoff is slow, and the hazard of erosion is moderate. Blakeland loamy sand is classified as being part of Hydrologic Soil Group A. A portion of the **Soil Map** and data tables from the National Cooperative Soil Survey and relevant **Official Soil Series Descriptions (OSD)** are included in the **Appendix**.<sup>2 3</sup>

The current Flood Insurance Study of the region includes Flood Insurance Rate Maps (FIRMs), effective December 7, 2018.<sup>4 5</sup> The project site is included in Community Panel Number 08041C0763 G of the FIRMs for El Paso County, Colorado. No portion of the site lies within FEMA designated Special Flood Hazard Areas (SFHAs). An excerpt of the current **FEMA Flood Insurance Rate Maps** with the site delineated is included in the **Appendix**.

A new multi-family residential development will be constructed on the site. The proposed buildings will be accessed by paved drives and walkways. The southern portion of the site will remain open space to preserve the existing utility and drainage easements. The development will include a new buildings, paved parking, paved drives, landscaping and recreational open area. The site will drain to the southwest corner of the site, as in existing conditions, and the flows will enter the existing detention pond in the adjacent Lincoln Commons Townhomes site.

## 2 Drainage Basins and Sub-Basins

### 2.1 Major Basin Descriptions

The Townhomes at Bradley Crossroads site is located in the Little Johnson Drainage Basin (FOFO3200) in the Security/Widefield area of El Paso County, which contains properties in both City of Colorado Springs and unincorporated El Paso County jurisdictions. The basin is a studied basin with an approved and operative Drainage Basin Planning Study (DBPS). The Basin stretches for approximately 17 miles on the east side of Colorado Springs and drains from northeast to southwest into Fountain Creek at a point just north of the crossing of Interstate 25 and US Highway 85-87. The site is located in the southeastern portion of the Little Johnson Drainage Basin, in the East Fork sub-area and eventually drains into the East Fork of Sand Creek. A copy of a portion of the **“Drainage Area Identification Study” map**, showing the site location within the Basin is included in the **Appendix**.<sup>6</sup>

The Drainage Basin Planning Study for the Little Johnson Drainage Basin was completed in 1988 by Kiowa Engineering Corporation.<sup>7</sup> The site is contained within sub-basin 24, located just upstream of Design Point No. 11, as indicated in the 1988 report. There are not drainage improvements noted in the DBPS for the site.

Other previously prepared and approved drainage reports were reviewed in this drainage study and are referenced in this report including:

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2 WSS  
3 OSD  
4 FIS  
5 FIRM, Map No. 08041C0763 G  
6 Drain. Area Ident. Study  
7 1988 DBPS

- Final Drainage Report and Plan for Lincoln Plaza Subdivision Filing No. 2 by Leigh Whitehead and Associates, Inc., dated March 2001.<sup>8</sup> This report studied existing conditions for the proposed site and the Lincoln Commons to the west. This report is referenced by later reports for the site by Westworks Engineering and Terra Nova Engineering.
- Preliminary/Final Drainage Report for Lincoln Plaza Subdivision No. 2 by WestWorks Engineering, dated August 2004.<sup>9</sup> This report studied the area of this current site together with the Lincoln Commons area to the west. The site was considered in commercial developed characteristics and to drain to a pond in the Lincoln Commons property.
- Final Drainage Report for Lincoln Commons by WestWorks Engineering revised July 25, 2007. This report included this subject site and adjacent property as an offsite contributing basin in the fully developed condition, generating  $Q_5=34$  cfs and  $Q_{100}=68$  cfs which drains to the Lincoln Common Townhomes water quality and storm detention pond.<sup>10</sup> Construction plans for Lincoln Commons Townhomes were approved and the project was constructed with the pond in 2016-2018.
- Final Drainage Report for Lots1 Thru 6, Bradley Crossroads, El Paso County, Colorado by Terra Nova Engineering, Inc. revised November 2008.<sup>11</sup> This report includes this subject site as mini-storage in a 100% paved condition. Developed flows are shown draining to the southwest corner of the site and entering the existing Stormwater pond in adjacent Lincoln Commons Townhomes.<sup>12</sup>

## 2.2 Sub-Basin Description

### 2.2.1 General Existing Conditions

The site and existing sub-basin historically drains from northeast to southwest with slopes of 1% to 2%. The site was studied by Terra Nova Engineering Inc. in previous drainage reports noted above. Historic conditions are documented in those prior reports and incorporated by reference in this analysis.

### 2.2.2 Existing Drainage Patterns (Off-Site)

Off-site drainage flows enter the north edge of the The Townhomes at Bradley Crossroads property from two off-site drainage basins located north of the site. These are both part of the Bradley Crossroads Filing No. 1A subdivision and both undeveloped at this time. These basins drain into the existing paved private drive located along the north boundary of the site. These flows drain through the site to the southwest corner. An additional offsite basin is located on the east edge of the site and consists of a portion the existing paved drive which currently drains west into the site.

### 2.2.3 Existing Drainage Patterns (On-Site)

The existing site is undeveloped, except for the existing paved access drives on the north and east edges. The site drains to the southwest corner and the flows are collected and directed to the existing detention pond in Lincoln Commons.

## 3 Drainage Design Criteria

### 3.1 Development Criteria Reference

This Final Drainage Report for The Townhomes at Bradley Crossroads has been prepared according to the report guidelines presented in the latest edition of *El Paso County Drainage Criteria Manual (DCM)*<sup>13</sup>. The County has also adopted portions of the City of Colorado Springs Drainage Criteria Manual Volumes 1 and 2, especially concerning the calculation of rainfall runoff flow rates.<sup>14 15</sup> The

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<sup>8</sup> LP FDR

<sup>9</sup> LP2 FDR

<sup>10</sup> LC FDR

<sup>11</sup> BC FDR

<sup>12</sup> BC FDR

<sup>13</sup> DCM Section 4.3 and Section 4.4

<sup>14</sup> CS DCM Vol 1

<sup>15</sup> CS DCM Vol 2

hydrologic analysis is based on a collection of data from the DCM, the NRCS Web Soil Survey<sup>16</sup>, Existing topographic data and proposed site plan by Land Development Consultants, Inc.

### 3.2 Hydrologic Criteria

For this Final Drainage Report, the Rational Method as described in the *Drainage Criteria Manual* has been used for all Storm Runoff calculations, as the development and all sub-basins are less than 130 acres in area. "Colorado Springs Rainfall Intensity Duration Frequency" curves, Figure 6-5 in the DCM, was used to obtain the design rainfall values; a copy is included in the **Appendix**. The "Overland (Initial) Flow Equation" (Eq. 6-8) in the DCM, and Manning's equation with estimated depths were used in time of concentration calculations. "Runoff Coefficients for Rational Method", Table 6-6 in the DCM, was utilized as a guide in estimating runoff coefficient and Percent Impervious values; a copy is included in the **Appendix**. Peak runoff discharges were calculated for each drainage sub-basin for both the 5-year storm event and the 100-year storm event with the Rational Method formula, (Eq. 6-5) in the DCM.<sup>17</sup>

## 4 Drainage Facility Design

### 4.1 General Concept

The intent of the drainage concept presented in this Final Drainage Report is to maintain the existing drainage patterns on the site which delivers the site flows to the existing detention pond in adjacent Lincoln Commons Townhomes site as determined in the previous drainage reports considering this site and the adjacent properties. Major and minor storm flows will continue to be safely conveyed through the site and downstream. The runoff from all developed areas will drain to the existing Extended Detention Basin (EDB). The existing and proposed private on-site storm drain system will collect the flow from the various developed on-site sub-basins and convey them to the existing EDB. The developed flows will be detained and released to the downstream drainage system at the historic flow rates.

The proposed drainage hydrologic conditions are described in more detail below. Input data and results for all calculations are included in the **Appendix**. A Drainage Maps for the hydrology are also included in the **Appendix**.

### 4.2 Specific Details

#### 4.2.1 Proposed Hydrologic Conditions

**Design Point 0 (DP0).** The off-site drainage basin, OS-1 (0.19 acres), will drain to a low point on the east edge of the site. This flow formerly entered the existing site and continued west into the site. However, in the developed condition, a new grated Type C inlet will collect the flows which will enter the existing 24 inch RC Pipe located in the drive. The developed discharges from sub-basin OS-1 are  $Q_5 = 0.8$  cfs and  $Q_{100} = 1.4$  cfs.

**Design Point 1 (DP1).** DP1 is the combination of sub-basins OS-1, OS-2, A1 and A2 at the northwest corner of the site where the combined runoff enters the west drain swale from the existing paved north driveway.

Offsite sub-basin OS-2 (1.02 acres) is located adjacent to the northeast corner of the site and drains to the existing paved drive along the north edge of the site. The basin is assumed to be developed in accordance with the commercial zoning. The peak flow rates generated by sub-basin OS-2 are  $Q_5 = 3.6$  cfs and  $Q_{100} = 6.9$  cfs. These flows will travel west in the drive and join additional flows from sub-basin OS-3.

Offsite sub-basin basin OS-3 (0.81 acres) is located adjacent to the northwest edge of the site and will contain offsite commercial development in accordance with the existing zoning. The sub-basin drains to the southwest and flows enter the existing paved drive with peak runoff rates of  $Q_5 = 3.2$  cfs

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<sup>16</sup> WSS  
<sup>17</sup> DCM

and  $Q_{100} = 6.0$  cfs. These flows join the runoff from sub-basin OS-2 in the existing paved drive and are directed to a drainage swale located on the west edge of the subject property by way of an existing concrete run-down at Design Point 1 (DP1).

Proposed sub-basin A1 (0.21 acres) consists of half of a proposed townhome building along with sidewalks and landscaping that drains north to the existing paved drive. Sub-basin A1 will produce runoff at peak flow rates of  $Q_5 = 0.5$  cfs and  $Q_{100} = 1.2$  cfs which joins the flows from sub-basin OS-2 and flows west in the drive into sub-basin OS-3.

Proposed sub-basin A2 (0.20 acres) is comprised of building, sidewalk and landscaping area at the northwest edge of the site. The flows of sub-basin A2 are  $Q_5 = 0.5$  cfs and  $Q_{100} = 1.1$  cfs which drain north into the existing paved drive, joining flows from sub-basins OS-2, OS-3 and A1 at DP1. The combined discharges at **DP 1** are  $Q_5 = 7.3$  cfs and  $Q_{100} = 14.1$  cfs. The flows enter a drain swale located along the west edge of the site and continue south through sub-basin A3.

**Design Point 2 (DP2).** DP2 is the combination of sub-basins A4 and A5 at the west edge of the site where the combined runoff enters the west drain swale in sub-basin A3 from a curb opening in the proposed paved driveway.

Proposed sub-basin A4 (0.34 acres) is comprised of building, drive and landscape area located on the east side of the site, just to the south of A1. The discharges from sub-basin A4 are  $Q_5 = 1.3$  cfs and  $Q_{100} = 2.5$  cfs which drain west into sub-basin A5.

Proposed sub-basin A5 (0.28 acres) consists of building, drive and landscape area located on the east side of the site, just west of A4. The sub-basin generates storm runoff peak discharges of  $Q_5 = 1.1$  cfs and  $Q_{100} = 2.0$  cfs. The sub-basin also accepts the flows from sub-basin A4 and the combined discharges of  $Q_5 = 2.2$  cfs and  $Q_{100} = 4.2$  cfs enter the west drain swale at **DP2** by way of a 2' curb opening.

**Design Point 3 (DP3).** DP3 is the combination of sub-basins OS-2, OS-3, A3, A4 and A5 at the access road leading to adjacent Lincoln Commons Townhomes to the west in the drain swale at the west edge of the site.

Proposed sub-basin A3 (0.20 acres) will consist of the open channel swale on the west edge of the property. The sub-basin generates peak discharges of  $Q_5 = 0.1$  cfs and  $Q_{100} = 0.6$  cfs, which drain south in the swale to DP3. Sub-basin A3 also collects flows from sub-basins OS-2, OS-3, A4 and A5 with combined discharges of  $Q_5 = 9.1$  cfs and  $Q_{100} = 17.9$  cfs at **DP3**. 5-yr flows cross beneath the access road in 3 private 12" RC Pipes. Overflows greater than the 5-year runoff crosses over the access in a depressed concrete pan and continue south in the drain swale.

**Design Point 4 (DP4).** DP4 is the combination of sub-basins A6 and A7 at the west edge of the site where the combined runoff enters the west drain swale in sub-basin A12 from the depressed concrete pan in the proposed paved access driveway.

Proposed sub-basin A6 (0.50 acres) is comprised of building, drive and landscape area located on the east side of the site, just to the south of A4. The discharges from sub-basin A6 are  $Q_5 = 1.9$  cfs and  $Q_{100} = 3.6$  cfs which drain west into sub-basin A7.

Proposed sub-basin A7 (0.52 acres) consists of building, drive and landscape area located on the east side of the site, just west of A6. The sub-basin generates storm runoff peak discharges of  $Q_5 = 1.9$  cfs and  $Q_{100} = 3.7$  cfs. The sub-basin also accepts the flows from sub-basin A6 and the combined discharges of  $Q_5 = 3.6$  cfs and  $Q_{100} = 6.9$  cfs enter the west drain swale at **DP4** by way of the depressed concrete pan at the Lincoln Commons Townhomes access.

**Design Point 5 (DP5).** DP5 is the combination of sub-basins A8 and A9 at the west edge of the site where the combined runoff enters the west drain swale in sub-basin A12 from a curb opening in the proposed paved driveway.

Proposed sub-basin A8 (0.33 acres) is comprised of building, drive and landscape area located on the east side of the site, just to the south of A6. The discharges from sub-basin A8 are  $Q_5 = 1.3$  cfs and  $Q_{100} = 2.4$  cfs which drain west into sub-basin A9.

Proposed sub-basin A9 (0.28 acres) consists of building, drive and landscape area located on the east side of the site, just west of A8. The sub-basin generates storm runoff peak discharges of  $Q_5 = 1.1$  cfs and  $Q_{100} = 2.0$  cfs. The sub-basin also accepts the flows from sub-basin A8 and the combined discharges of  $Q_5 = 2.2$  cfs and  $Q_{100} = 4.2$  cfs enter the west drain swale in sub-basin A12 at **DP5** by way of a 2' curb opening.

**Design Point 6 (DP6).** DP6 is the combination of sub-basins A10 and A11 at the west edge of the site where the combined runoff enters the west drain swale in sub-basin A12 from a curb opening in the proposed paved driveway.

Proposed sub-basin A10 (0.49 acres) is comprised of building, drive and landscape area located on the east side of the site, just to the south of A8. The discharges from sub-basin A10 are  $Q_5 = 1.9$  cfs and  $Q_{100} = 3.6$  cfs which drain west into sub-basin A11.

Proposed sub-basin A11 (0.38 acres) consists of building, drive and landscape area located on the east side of the site, just west of A10. The sub-basin generates storm runoff peak discharges of  $Q_5 = 1.5$  cfs and  $Q_{100} = 2.8$  cfs. The sub-basin also accepts the flows from sub-basin A10 and the combined discharges of  $Q_5 = 3.2$  cfs and  $Q_{100} = 6.1$  cfs enter the west drain swale in sub-basin A12 at **DP6** by way of a 2' curb opening.

**Design Point 7 (DP7).** DP7 is the combination of sub-basins OS-1, OS-2, A1, A2, A3, A4, A5, A6, A7, A8, A9, A10, A11 and A12 near the southwest corner of the site where the combined runoff enters an existing 24" RC Pipe at the downstream end the west drain swale.

Proposed sub-basin A12 (0.11 acres) will consist of the open channel swale on the west edge of the property. The sub-basin generates peak discharges of  $Q_5 = 0.1$  cfs and  $Q_{100} = 0.6$  cfs, which drains south in the swale to DP7. Sub-basin A3 also collects flows from the upstream sub-basins OS-2, OS-3 and A1 – A11 (DP1-DP6) with combined discharges of  $Q_5 = 16.4$  cfs and  $Q_{100} = 32.0$  cfs at **DP7**. 5-year flows enter the existing 24" RC Pipe. Overflows greater than the 5-year continue south to an existing D-9 grated inlet at DP8 in sub-basin A13. All these flows are collected in the storm drain system and continue west in the existing 36" RC Pipe which drains into the existing Lincoln Commons Townhomes EDB.

**Design Point 8 (DP8).** DP8 consists of sub-basin A13, which drains by surface flow to the west and is captured in the existing D-9 inlet at the west property boundary. These flows are combined with the flows from DP7 and are conveyed to the west. Proposed sub-basin A13 (0.15 acres) is comprised of building and a significantly sized open landscape area located along the south side of the just to the south of A10 and A11. The discharges from sub-basin A13 are  $Q_5 = 1.0$  cfs and  $Q_{100} = 3.2$  cfs. The combined discharges at **DP8** are  $Q_5 = 17.4$  cfs and  $Q_{100} = 35.3$  cfs.

#### **Existing Extended Detention Basin (EDB).**

The development of Lincoln Commons and the construction of Lincoln Commons Townhomes provided for the detention and water quality treatment of the entire Lincoln Commons and Bradley Crossroads developments. The Final Drainage Report for Lincoln Commons by WestWorks Engineering, revised July 25, 2007 calculated the offsite flows from Bradley Crossroads Filing No. 1, Lots 1-6 to have developed flows of  $Q_5 = 34$  cfs and  $Q_{100} = 68$  cfs. Those flows combine with the Lincoln Commons Townhome development, were used to size the detention and water quality basin. The Final Drainage Report for Bradley Crossroads Filing No. 1 Lots 1 – 6 by Terra Nova Engineering, revised November 2008 recalculated the offsite flows going to the EDB to have peak flow rates of  $Q_5 = 34.2$  cfs and  $Q_{100} = 61.3$  cfs, which is less than the overall capacity of the existing facility. This report considers a portion of the Bradley Crossroads site, and revised the developed flows from the Terra Nova report and determines offsite developed flows entering the EDB to be  $Q_5 = 31.9$  cfs and  $Q_{100} = 62.3$  cfs. These revised flows are also lower than the original design flows used to size the existing EDB. The existing EDB will provide adequate storm detention and water quality capacity for the Townhomes at Bradley Crossroads site. Existing EDB is in new condition, recently verified by M.V.E, Inc. to be constructed in accordance with the approved construction plans and recently released by El Paso County inspections.

#### **4.2.2 Proposed Drainage Facilities**

The proposed on-site storm drain system will be owned and maintained by The Townhomes at Bradley Crossroads. The pipe system will be 6", 12" and 18" HDPE material. The proposed inlets will be Type 16 combination inlets with concrete boxes and adjustable steel grate and curb openings. The area inlet will be PVC and non-traffic bearing located in landscaped areas. The proposed pipe system discharges into the Full Spectrum Sand Filter Basin, which is designed to detain the WQCV, EURV and 100-year developed runoff volumes. The proposed FS Sand Filter Basin has storage volume of 0.281 acre-feet. The facility is located in Type A soils and will be full-infiltration type. The EURV and 100-year flows will be regulated by a concrete outlet box with steel orifice plate and outlet pipe. The facility will have an emergency spillway with 6' bottom width discharging to Western Drive and protected by riprap lining.

#### **4.3 Erosion Control**

During future construction, best management practices (BMP's) for erosion control will be employed based on the previously referenced City of Colorado Springs Drainage Criteria Manual Volume 2 and the Erosion Control Plan to minimize erosion from the site. The BMP's will remain in place until the site is stabilized with the new hard surfacing or landscape seeding, planting and cover materials. Also, BMP's will be utilized as deemed necessary by the contractor, engineer, owner, or County inspector and are not limited to the measures described on the Erosion Control Plan.

#### **4.4 Water Quality Enhancement Best Management Practices**

This development will utilize the existing Extended Detention Basin (EDB) west of the site in Lincoln Commons Townhomes. This existing EDB was designed and constructed for this purpose as indicated in the referenced previous drainage reports. The pond adequately sized for this purpose. Other drainage facilities in this project consist of rip rap drainage swale on the west side of the site and minor modifications to the existing surrounding storm drain system. These facilities will be private and will be maintained by the development's homeowners association. A Grading and Erosion Control Plan for the construction of the site has been prepared in accordance with the provisions of the County's Engineering Criteria Manual. Placement of construction stormwater BMP's will as required by the plan will limit soil erosion and deposition by stormwater flowing over the site.

The El Paso County Engineering Criteria Manual (Appendix I, Section I.7.2 ) requires the consideration of a "Four Step Process for receiving water protection that focuses on reducing runoff volumes, treating the water quality capture volume (WQCV), stabilizing drainageways, and implementing long term source controls". The Four Step Process is incorporated in this project and the elements are discussed below.

- 1) Runoff Reduction Practices are employed in this project. Impervious surfaces have been reduced as much as practically possible. The parking lot contains landscape islands and a significant portion of the south side of the site will remain as pervious landscaped open space.
- 2) All drainage paths on the site are stabilized with pavement or appropriate landscape treatment. The existing EDB will intercept flows from developed areas. Additionally, all inflow points will be stabilized with rip-rap or concrete protection.
- 3) The project contains no potentially hazardous uses. All developed areas drain into a proposed a WQCV BMP.
- 4) The site is residential in nature and contains no storage of potentially harmful substances or use of potentially harmful substances. No Site Specific or Other Source Control BMP's are required.

## 5 Opinion of Probable Cost for Drainage Facilities

There are no public drainage improvements associated with this project. Costs for the private non-reimbursable drainage improvements for this project are listed in the table below:

<b>The Townhomes at Bradley Crossroads Private Drainage Costs (Non-Reimbursable)</b>				
<b>Item</b>	<b>Quantity</b>	<b>Unit</b>	<b>Unit Cost</b>	<b>Cost</b>
Storm Sewer Manhole, Box Base	1	EA	\$8,592	\$8,592
Reinforced Concrete Pipe - 12"	156	LF	\$48	\$7,488
Reinforced Concrete Pipe – 36"	4	LF	\$124	\$496
Flared End Section - 24"	1	EA	\$325	\$325
Grated Inlet (Type C)	1	EA	\$3,270	\$3,270
<b>GRAND TOTAL</b>				<b>\$20,171.00</b>

## 6 Drainage and Bridge Fees

The site is already platted and replatted. No additional Drainage or Bridge Fees are due for this project.

## 7 Conclusion

This Final Drainage Report presents existing and proposed drainage conditions for the proposed The Townhomes at Bradley Crossroads project. The development will have negligible and inconsequential effects on the existing site drainage and drainage conditions downstream. Full Spectrum Detention and Water Quality treatment will be provided. The proposed project will not, with respect to stormwater runoff, negatively impact the adjacent properties and downstream properties.

is being provided in the adjacent site, Lincoln Commons Townhomes, EPC file # SF 7-012

## References

*City of Colorado Springs/El Paso County Drainage Criteria Manual.* City of Colorado Springs, Department of Public Works, Engineering Division; HDR Infrastructure, Inc.; El Paso County, Department of Public Works, Engineering Division (Colorado Springs: City of Colorado Springs, Revised November 1991).

*NRCS Official Soil Series Descriptions.* United States Department of Agriculture, Natural Resources Conservation Service ("http://soils.usda.gov/technical/classification/osd/index.html", accessed Accessed September 2018).

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*Flood Insurance Rate Map.* Federal Emergency Management Agency, National Flood Insurance Program (Washington D.C.: FEMA, December 7, 2018).

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*Final Drainage Report and Plan for Lincoln Plaza Filing No. 2.* Leigh Whitehead & Associates, Inc. (El Paso County, Colorado: , March, 2001).

*Preliminary/Final Drainage Report for Lincoln Plaza Subdivision No. 2.* WestWorks Engineering (El Paso County, Colorado: , August, 2004).

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*Final Drainage Report for Lots 1 Thru 6, Bradley Crossroads.* Terra Nova Engineering, Inc. (Revised November 2008: , El Paso County, Colorado).

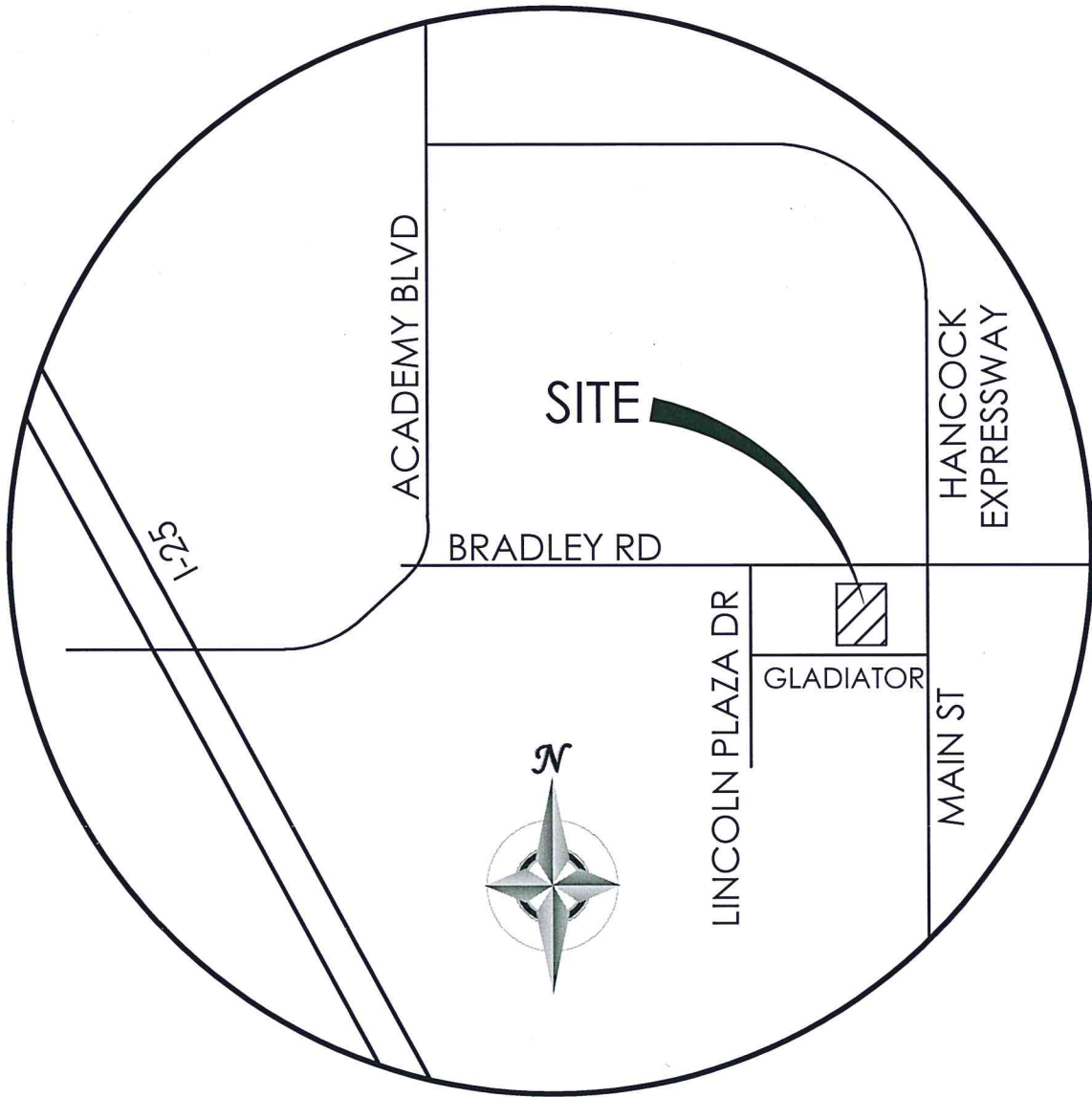
*Drainage Criteria Manual Volume 2, Stormwater Policies, Procedures and Best Management Practices (BMPs).* City of Colorado Springs Engineering Division (Colorado Springs, Colorado: , May 2014).

*City of Colorado Springs Drainage Criteria Manual Volume 1.* City of Colorado Springs Engineering Division with Matrix Design Group and Wright Water Engineers (Colorado Springs, Colorado: , May 2014).

# | Appendices

## **1 General Maps and Supporting Data**

- Vicinity Map
- Portion of Flood Insurance Rate Map (FIRMette)
- Portion of Drainage Area Identification Study Map
- Portion of DBPS Map
- NRCS Soil Map and Tables
- SCS Soil Type Descriptions
- Hydrologic Soil Group Map and Tables



VICINITY MAP  
N.T.S.

# National Flood Hazard Layer FIRMette



38°46'22.98"N

104°44'52.53"W



USGS The National Map: Orthoimagery. Data refreshed October, 2017.  
38°45'54.93"N  
104°44'15.07"W



## Legend

SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT

### SPECIAL FLOOD HAZARD AREAS



### OTHER AREAS OF FLOOD HAZARD



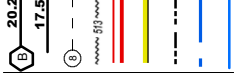
### OTHER AREAS



### GENERAL STRUCTURES



### OTHER FEATURES



### MAP PANELS



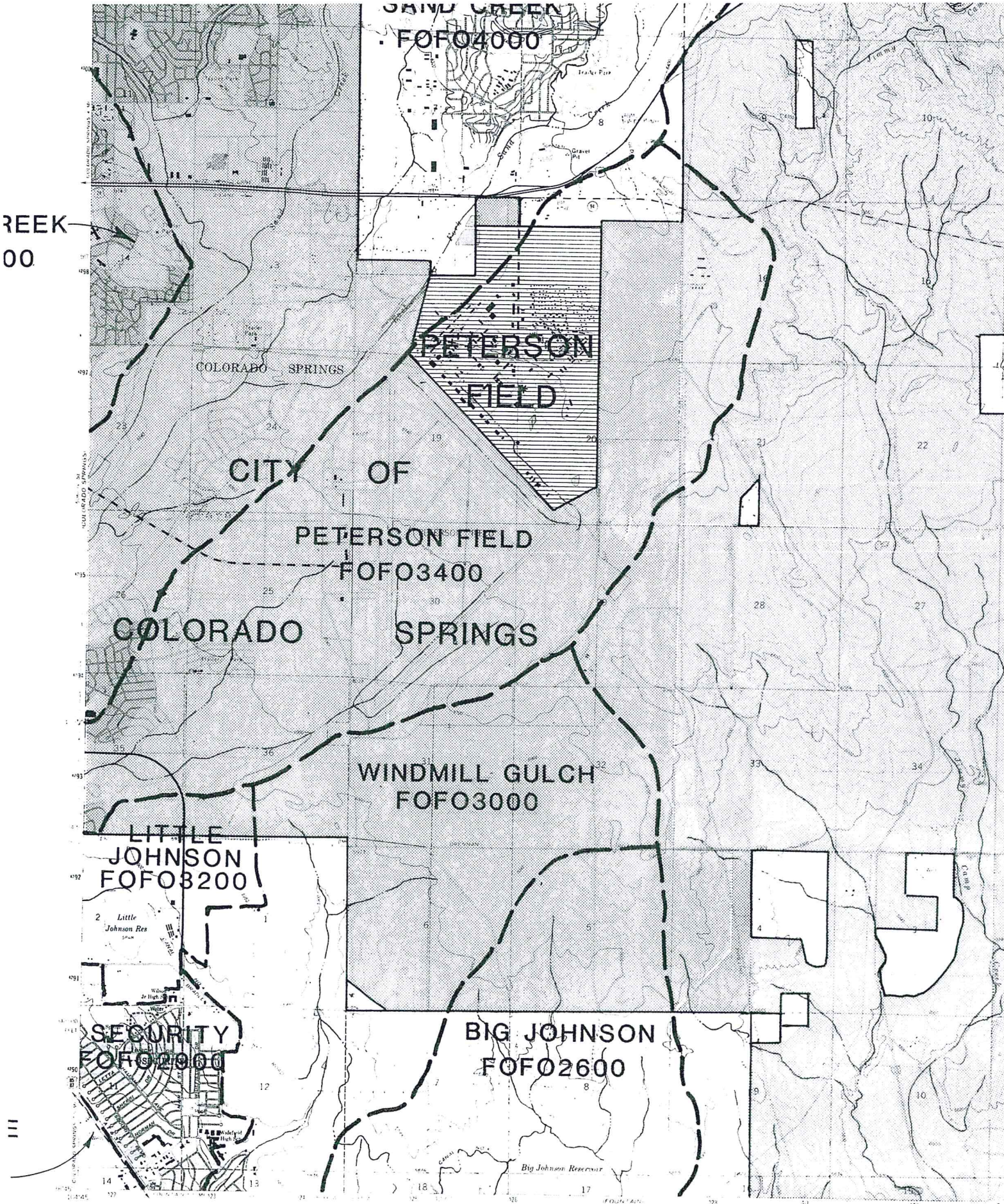
The pin displayed on the map is an approximate point selected by the user and does not represent an authoritative property location.

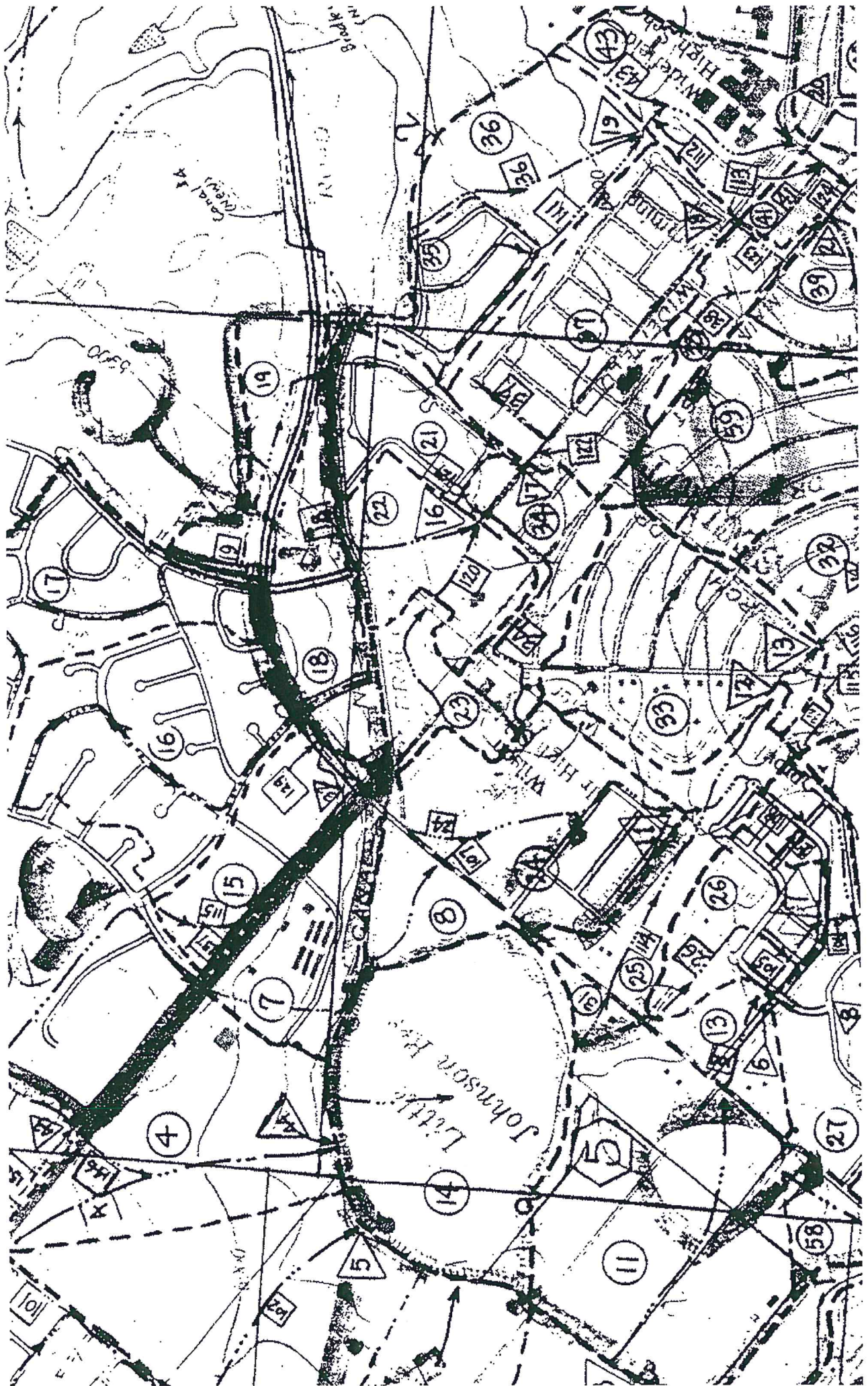
This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The basemap shown complies with FEMA's basemap accuracy standards.

The flood hazard information is derived directly from the authoritative NFHL web services provided by FEMA. This map was exported on 2/14/2019 at 12:54:18 PM and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or become superseded by new data over time.

This map image is void if the one or more of the following map elements do not appear: basemap imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for unmapped and unmodernized areas cannot be used for regulatory purposes.

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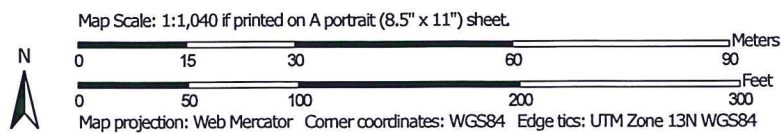




# Soil Map—El Paso County Area, Colorado



Soil Map may not be valid at this scale.



Natural Resources  
Conservation Service

Web Soil Survey  
National Cooperative Soil Survey

9/11/2018  
Page 1 of 3

## Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
8	Blakeland loamy sand, 1 to 9 percent slopes	4.9	100.0%
Totals for Area of Interest		4.9	100.0%

is severely eroded and blowouts have developed, the new seeding should be fertilized.

Windbreaks and environmental plantings are generally suited to this soil. Soil blowing is the main limitation for the establishment of trees and shrubs. This limitation can be overcome by cultivating only in the tree rows and leaving a strip of vegetation between the rows. Supplemental irrigation may be necessary when planting and during dry periods. Trees that are best suited and have good survival are Rocky Mountain juniper, eastern redcedar, ponderosa pine, Siberian elm, Russian-olive, and hackberry. Shrubs that are best suited are skunkbush sumac, lilac, and Siberian peashrub.

This soil is suited to wildlife habitat. It is best suited to habitat for openland and rangeland wildlife. In cropland areas, habitat favorable for ring-necked pheasant, mourning dove, and many nongame species can be developed by establishing areas for nesting and escape cover. For pheasant, the provision of undisturbed nesting cover is vital and should be included in plans for habitat development. Rangeland wildlife, such as pronghorn antelope, can be encouraged by developing livestock watering facilities, properly managing livestock grazing, and reseeding range where needed.

This soil has good potential for use as homesites. Shallow excavation is severely limited because cut banks cave in. This sandy soil requires special management practices to reduce water erosion and soil blowing. Capability subclasses IIIe, irrigated, and IVe, nonirrigated.

**7—Bijou sandy loam, 3 to 8 percent slopes.** This deep, well drained soil is on flood plains, terraces, and uplands. It formed in sandy alluvium and eolian material derived from arkose deposits. Elevation ranges from 5,400 to 6,200 feet. The average annual precipitation is about 13 inches, the average annual air temperature is about 49 degrees F, and the average frost-free period is about 145 days.

Typically, the surface layer is brown sandy loam about 4 inches thick. The subsoil is brown or grayish brown sandy loam about 24 inches thick. The substratum is pale brown loamy coarse sand.

Included with this soil in mapping are small areas of Olney sandy loam, 3 to 5 percent slopes; Valent sand, 1 to 9 percent slopes; Vona sandy loam, 3 to 9 percent slopes; and Wigton loamy sand, 1 to 8 percent slopes.

Permeability of this Bijou soil is rapid. Effective rooting depth is 60 inches or more. Available water capacity is moderate. Organic matter content of the surface layer is low. Surface runoff is slow, and the hazards of erosion and soil blowing are moderate.

Almost all areas of this soil are used for range.

This soil is suited to the production of native vegetation suitable for grazing. Because of the hazards of water erosion and soil blowing, the soil is not suited to nonirrigated crops.

Native vegetation is dominantly blue grama, sand dropseed, needleandthread, side-oats grama, and buckwheat.

Seeding is a suitable practice if the range has deteriorated. Seeding the native grasses is a good practice. If the range is severely eroded and blowouts have developed, the new seeding should be fertilized. Brush control and grazing management may be needed to improve the depleted range. Grazing should be managed so that enough forage is left standing to protect the soil from blowing, to increase infiltration of water, and to catch and hold snow.

Windbreaks and environmental plantings are generally suited to this soil. Soil blowing is the main limitation for the establishment of trees and shrubs. This limitation can be overcome by cultivating only in the tree rows and leaving a strip of vegetation between the rows. Supplemental irrigation may be needed when planting and during dry periods. Trees that are best suited and have good survival are Rocky Mountain juniper, eastern redcedar, ponderosa pine, Siberian elm, Russian-olive, and hackberry. Shrubs that are best suited are skunkbush sumac, lilac, and Siberian peashrub.

This soil is suited to wildlife habitat. It is best suited to habitat for openland and rangeland wildlife. Rangeland wildlife, such as pronghorn antelope, can be encouraged by developing livestock watering facilities, by properly managing livestock grazing, and by reseeding range where needed.

This soil has good potential for use as homesites. Shallow excavation is severely limited because cut banks cave in. This soil requires special management practices to reduce water erosion and soil blowing. Capability subclass VIe.

**8—Blakeland loamy sand, 1 to 9 percent slopes.** This deep, somewhat excessively drained soil formed in alluvial and eolian material derived from arkosic sedimentary rock on uplands. The average annual precipitation is about 15 inches, the average annual air temperature is about 47 degrees F, and the average frost-free period is about 135 days.

Typically, the surface layer is dark grayish brown loamy sand about 11 inches thick. The substratum, to a depth of 27 inches, is brown loamy sand; it grades to pale brown sand that extends to a depth of 60 inches.

Included with this soil in mapping are small areas of Bresser sandy loam, 0 to 3 percent slopes; Bresser sandy loam, 3 to 5 percent slopes; Truckton sandy loam, 0 to 3 percent slopes; Truckton sandy loam, 3 to 9 percent slopes; and Stapleton sandy loam, 3 to 8 percent slopes. In some areas, mainly north of Colorado Springs in the Cottonwood Creek area, arkosic beds of sandstone and shale are at a depth of 0 to 40 inches.

Permeability of this Blakeland soil is rapid. Effective rooting depth is 60 inches or more. Available water capacity is low to moderate. Organic matter content of the surface layer is medium. Surface runoff is slow, the hazard of erosion is moderate, and the hazard of soil blowing is severe.

Most areas of this soil are used for range, homesites, and wildlife habitat.

Native vegetation is dominantly western wheatgrass, side-oats grama, and needleandthread. This soil is best suited to deep-rooted grasses.

Proper range management is necessary to prevent excessive removal of plant cover from the soil. Interseeding improves the existing vegetation. Deferment of grazing in spring increases plant vigor and soil stability. Proper location of livestock watering facilities helps to control grazing.

Windbreaks and environmental plantings are fairly well suited to this soil. Blowing sand and low available water capacity are the main limitations for the establishment of trees and shrubs. The soil is so loose that trees need to be planted in shallow furrows and plant cover needs to be maintained between the rows. Supplemental irrigation may be needed to insure survival. Trees that are best suited and have good survival are Rocky Mountain juniper, eastern redcedar, ponderosa pine, and Siberian elm. Shrubs that are best suited are skunkbush sumac, lilac, and Siberian peashrub.

This soil is suited to wildlife habitat. It is best suited to habitat for openland and rangeland wildlife. Rangeland wildlife, such as pronghorn antelope, can be encouraged by developing livestock watering facilities, properly managing livestock grazing, and reseeding range where needed.

This soil has good potential for urban development. Soil blowing is a hazard if protective vegetation is removed. Special erosion control practices must be provided to minimize soil losses. Capability subclass VIe.

**9—Blakeland complex, 1 to 9 percent slopes.** This complex is on uplands, mostly in the Falcon area. The average annual precipitation is about 15 inches, the average annual air temperature is about 47 degrees F, and the frost-free period is about 135 days.

This complex is about 60 percent Blakeland loamy sand, about 30 percent Fluvaquentic Haplaquolls, and 10 percent other soils.

Included with these soils in mapping are areas of Columbine gravelly sandy loam, 0 to 3 percent slopes, Ellicott loamy coarse sand, 0 to 5 percent slopes, and Ustic Torrifluvents, loamy.

The Blakeland soil is in the more sloping areas. It is deep and somewhat excessively drained. It formed in sandy alluvium and eolian material derived from arkosic sedimentary rock. Typically, the surface layer is dark grayish brown loamy sand about 11 inches thick. The substratum, to a depth of 27 inches, is brown loamy sand; it grades to pale brown sand that extends to a depth of 60 inches or more.

Permeability of the Blakeland soil is rapid. The effective rooting depth is more than 60 inches. The available water capacity is moderate to low. Surface runoff is slow, and the hazard of erosion is moderate.

The Fluvaquentic Haplaquolls are in swale areas. They are deep, poorly drained soils. They formed in alluvium derived from arkosic sedimentary rock. Typically, the surface layer is brown. The texture is variable throughout. The water table is at a depth of 0 to 3 feet.

The Blakeland soil is well suited to deep-rooted grasses. Native vegetation is dominantly western wheatgrass, side-oats grama, and needleandthread. Rangeland vegetation on the Fluvaquentic Haplaquolls is dominantly tall grasses, including sand bluestem, switchgrass, prairie cordgrass, little bluestem, and sand reedgrass. Cattails and bulrushes are common in the swampy areas.

Proper range management is needed to prevent excess removal of plant cover from these soils. It is also needed to maintain the productive grasses. Interseeding improves the existing vegetation. Deferment of grazing during the growing season increases plant vigor and soil stability, and it helps to maintain and improve range condition. Proper location of livestock watering facilities helps to control grazing of animals.

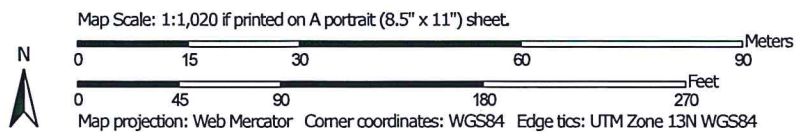
Windbreaks and environmental plantings are fairly well suited to these soils. Blowing sand and low available water capacity are the main limitations to the establishment of trees and shrubs. The soils are so loose that trees need to be planted in shallow furrows and plant cover needs to be maintained between the rows. Supplemental irrigation may be needed to insure survival. Trees that are best suited and have good survival are Rocky Mountain juniper, eastern redcedar, ponderosa pine, and Siberian elm. Shrubs that are best suited are skunkbush sumac, lilac, and Siberian peashrub.

The Blakeland soil is well suited to wildlife habitat. It is best suited to habitat for openland and rangeland wildlife. Rangeland wildlife, such as pronghorn antelope, can be encouraged by developing livestock watering facilities, properly managing livestock grazing, and reseeding range where needed. Wetland wildlife can be attracted to the Fluvaquentic Haplaquolls and the wetland habitat can be enhanced by several means. Shallow water developments can be created by digging or by blasting potholes to create open-water areas. Fencing to control livestock grazing is beneficial, and it allows wetland plants such as cattails, reed canarygrass, and rushes to grow. Control of unplanned burning and prevention of drainage that would remove water from the wetlands are good practices. Openland wildlife use the vegetation on these soils for nesting and escape cover. These shallow marsh areas are especially important for winter cover if natural vegetation is allowed to grow.

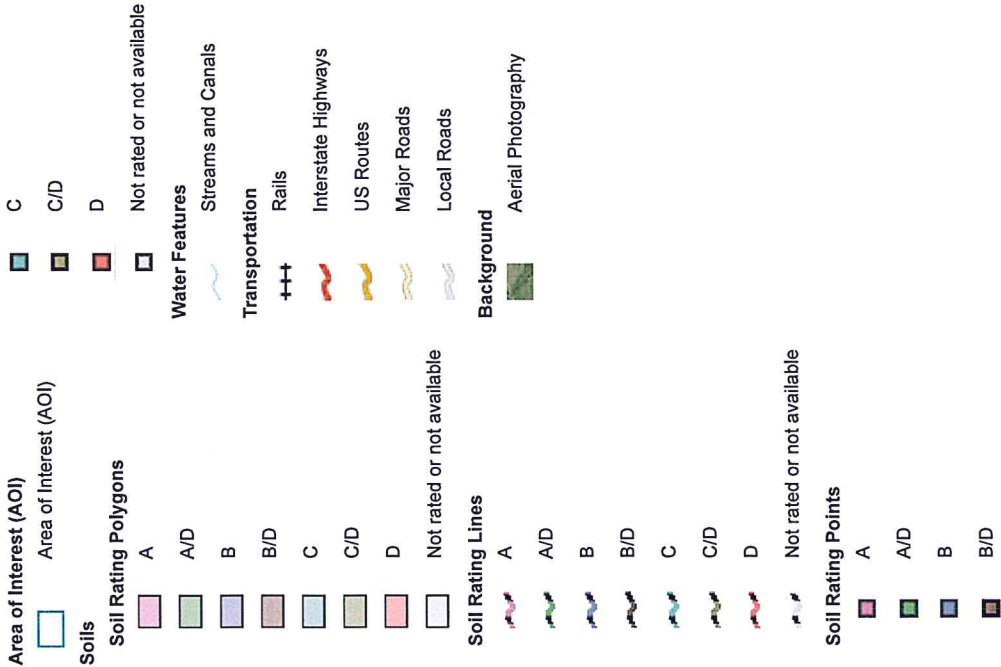
The Blakeland soil has good potential for homesites, roads, and streets. It needs to be protected from erosion when vegetation has been removed from building sites. The Fluvaquentic Haplaquolls have poor potential for homesites. Their main limitations for this use are the high water table and the hazard of flooding. Capability subclass VIe.

**10—Blendon sandy loam, 0 to 3 percent slopes.** This deep, well drained soil formed in sandy arkosic alluvium on alluvial fans and terraces. The average annual precipitation is about 15 inches, the mean annual air temperature is about 47 degrees F, and the average frost-free period is about 135 days.

# Hydrologic Soil Group—El Paso County Area, Colorado



## MAP LEGEND



## MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24,000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service  
Web Soil Survey URL:  
Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: El Paso County Area, Colorado  
Survey Area Data: Version 15, Oct 10, 2017

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Jun 3, 2014—Jun 17, 2014

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

## Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
8	Blakeland loamy sand, 1 to 9 percent slopes	A	4.8	100.0%
Totals for Area of Interest			4.8	100.0%

## Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

## Rating Options

*Aggregation Method:* Dominant Condition

*Component Percent Cutoff:* None Specified

## 2 Hydrologic Calculations

Runoff Coefficients and Percent Imperviousness Table 6-6

Colorado Springs Rainfall Intensity Duration Frequency Table 6-5

Hydrologic Calculations Summary Form SF-1 for Existing & Developed Conditions

Hydrologic Calculations Summary 5-yr Form SF-2 for Existing & Developed Conditions

Hydrologic Calculations Summary 100-yr Form SF-2 for Existing & Developed Conditions

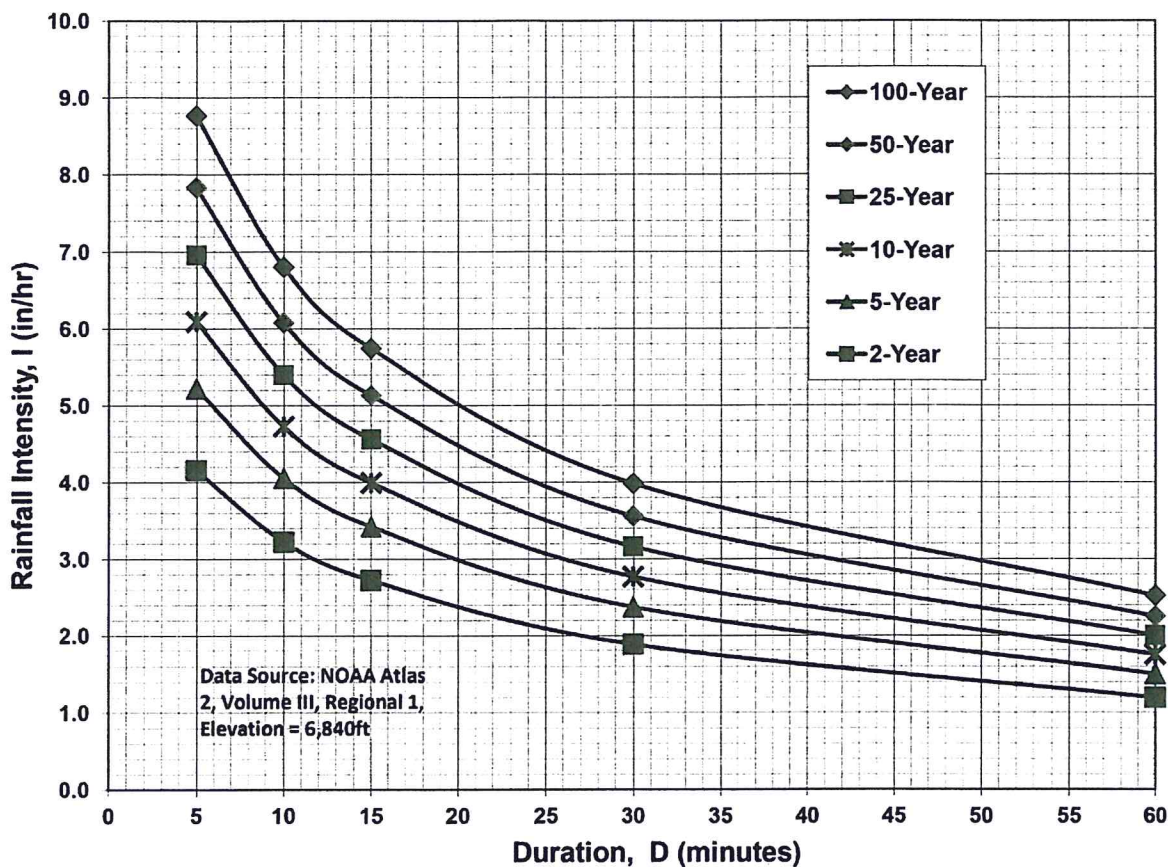
Sub-Basin and Design Point Hydrologic Calculations

**Table 6-6. Runoff Coefficients for Rational Method**  
(Source: UDFCD 2001)

Land Use or Surface Characteristics	Percent Impervious	Runoff Coefficients											
		2-year		5-year		10-year		25-year		50-year		100-year	
		HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D
Business													
Commercial Areas	95	0.79	0.80	0.81	0.82	0.83	0.84	0.85	0.87	0.87	0.88	0.88	0.89
Neighborhood Areas	70	0.45	0.49	0.49	0.53	0.53	0.57	0.58	0.62	0.60	0.65	0.62	0.68
Residential													
1/8 Acre or less	65	0.41	0.45	0.45	0.49	0.49	0.54	0.54	0.59	0.57	0.62	0.59	0.65
1/4 Acre	40	0.23	0.28	0.30	0.35	0.36	0.42	0.42	0.50	0.46	0.54	0.50	0.58
1/3 Acre	30	0.18	0.22	0.25	0.30	0.32	0.38	0.39	0.47	0.43	0.52	0.47	0.57
1/2 Acre	25	0.15	0.20	0.22	0.28	0.30	0.36	0.37	0.46	0.41	0.51	0.46	0.56
1 Acre	20	0.12	0.17	0.20	0.26	0.27	0.34	0.35	0.44	0.40	0.50	0.44	0.55
Industrial													
Light Areas	80	0.57	0.60	0.59	0.63	0.63	0.66	0.66	0.70	0.68	0.72	0.70	0.74
Heavy Areas	90	0.71	0.73	0.73	0.75	0.75	0.77	0.78	0.80	0.80	0.82	0.81	0.83
Parks and Cemeteries	7	0.05	0.09	0.12	0.19	0.20	0.29	0.30	0.40	0.34	0.46	0.39	0.52
Playgrounds	13	0.07	0.13	0.16	0.23	0.24	0.31	0.32	0.42	0.37	0.48	0.41	0.54
Railroad Yard Areas	40	0.23	0.28	0.30	0.35	0.36	0.42	0.42	0.50	0.46	0.54	0.50	0.58
Undeveloped Areas													
Historic Flow Analysis--													
Greenbelts, Agriculture	2	0.03	0.05	0.09	0.16	0.17	0.26	0.26	0.38	0.31	0.45	0.36	0.51
Pasture/Meadow	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50
Forest	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50
Exposed Rock	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Offsite Flow Analysis (when landuse is undefined)	45	0.26	0.31	0.32	0.37	0.38	0.44	0.44	0.51	0.48	0.55	0.51	0.59
Streets													
Paved	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Gravel	80	0.57	0.60	0.59	0.63	0.63	0.66	0.66	0.70	0.68	0.72	0.70	0.74
Drive and Walks	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Roofs	90	0.71	0.73	0.73	0.75	0.75	0.77	0.78	0.80	0.80	0.82	0.81	0.83
Lawns	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50



Figure 6-5. Colorado Springs Rainfall Intensity Duration Frequency

**IDF Equations**

$$I_{100} = -2.52 \ln(D) + 12.735$$

$$I_{50} = -2.25 \ln(D) + 11.375$$

$$I_{25} = -2.00 \ln(D) + 10.111$$

$$I_{10} = -1.75 \ln(D) + 8.847$$

$$I_5 = -1.50 \ln(D) + 7.583$$

$$I_2 = -1.19 \ln(D) + 6.035$$

Note: Values calculated by equations may not precisely duplicate values read from figure.

Sub-Basin	Sub-Basin Data				Overland			Shallow Channel				Channelized				t <sub>c</sub> Check		
	Area (Acres)	C <sub>5</sub>	C <sub>100</sub> /CN	% Imp.	L <sub>0</sub> (ft)	S <sub>0</sub> (%)	t <sub>i</sub> (min)	L <sub>0t</sub> (ft)	S <sub>0t</sub> (ft/ft)	V <sub>osc</sub> (ft/s)	t <sub>t</sub> (min)	L <sub>0c</sub> (ft)	S <sub>0c</sub> (ft/ft)	V <sub>oc</sub> (ft/s)	t <sub>c</sub> (min)	L (min)	t <sub>c,alt</sub> (min)	t <sub>c</sub> (min)
A1	0.21	0.49	0.65	55%	23	1%	5.3	25	0.060	4.9	0.1	0	0.000	0.0	0.0	48	10.3	5.4
A2	0.20	0.50	0.65	56%	23	1%	5.2	25	0.060	4.9	0.1	0	0.000	0.0	0.0	48	10.3	5.3
A3	0.20	0.13	0.39	6%	39	8%	5.6	0	0.000	0.0	0.0	135	0.010	0.6	3.6	174	11.0	9.2
A4	0.34	0.75	0.84	87%	23	1%	3.0	95	0.010	2.0	0.8	130	0.010	1.5	1.4	248	11.4	5.2
A5	0.28	0.77	0.84	91%	23	1%	2.9	95	0.010	2.0	0.8	88	0.010	1.4	1.0	206	11.1	5.0
A6	0.50	0.74	0.84	85%	23	1%	3.1	140	0.014	2.4	1.0	98	0.015	1.9	0.8	261	11.5	5.0
A7	0.52	0.71	0.81	80%	23	1%	3.4	118	0.019	2.8	0.7	80	0.009	1.6	0.9	221	11.2	5.0
A8	0.33	0.77	0.85	90%	23	1%	2.8	115	0.011	2.1	0.9	106	0.009	1.5	1.2	244	11.4	5.0
A9	0.28	0.77	0.84	91%	23	1%	2.9	98	0.014	2.4	0.7	79	0.009	1.4	1.0	200	11.1	5.0
A10	0.49	0.76	0.85	87%	23	1%	3.0	138	0.013	2.3	1.0	102	0.012	1.8	1.0	263	11.5	5.0
A11	0.38	0.76	0.85	88%	23	1%	2.9	118	0.015	2.5	0.8	83	0.014	1.8	0.8	224	11.2	5.0
A12	0.21	0.09	0.36	2%	20	15%	3.3	0	0.000	0.0	0.0	230	0.007	0.7	5.7	250	11.4	9.0
A13	1.09	0.24	0.46	21%	100	1%	17.6	113	0.014	0.8	2.3	201	0.015	2.4	1.4	414	12.3	12.3
OS-1	0.19	0.77	0.86	84%	24	2%	2.3	0	0.000	0.0	0.0	196	0.031	2.9	1.1	220	11.2	5.0
OS-2	1.02	0.72	0.82	78%	45	2%	3.7	137	0.011	2.1	1.1	238	0.011	2.8	1.4	420	12.3	6.2
OS-3	0.81	0.78	0.87	85%	48	1%	4.1	49	0.031	3.5	0.2	146	0.010	2.6	0.9	243	11.4	5.2

DP	Sub-Basin	Area (Acres)	C5	Direct Runoff				Combined Runoff				Streetflow			Pipe Flow				Travel Time		
				t <sub>c</sub> (min)	CA (Acres)	I5 (in/hr)	Q5 (cfs)	t <sub>c</sub> (min)	CA (Acres)	I5 (in/hr)	Q5 (cfs)	Slope (%)	Length (ft)	Q (cfs)	Slope (%)	Mnngs n	Length (ft)	D <sub>Pipe</sub> (in)	Length (ft)	V <sub>ave</sub> (ft/s)	t <sub>t</sub> (min)
DP1	OS-1	0.19	0.77	5.0	0.15	5.17	0.8														
	OS-2	1.02	0.72	6.2	0.73	4.85	3.6														
	OS-3	0.81	0.78	5.2	0.63	5.11	3.2														
	A1	0.21	0.49	5.4	0.10	5.06	0.5														
	A2	0.20	0.50	5.3	0.10	5.09	0.5	7.1	1.57	4.64	7.3										
DP2	OS-2,OS-3,A1,A2	2.25	0.70																		
	A3	0.20	0.13	9.2	0.03	4.26	0.1														
	A4	0.34	0.75	5.2	0.26	5.10	1.3														
	A5	0.28	0.77	5.0	0.21	5.17	1.1	6.4	0.47	4.80	2.2										
		0.62	0.76					8.2	2.06	4.43	9.1										
DP3	A6	0.50	0.67	5.0	0.37	5.17	1.9														
	A7	0.52	0.71	5.0	0.37	5.17	1.9	6.1	0.74	4.88	3.6										
DP4	A8	1.02	0.73	5.0	0.25	5.17	1.3														
	A9	0.28	0.77	5.0	0.21	5.17	1.1	6.2	0.46	4.84	2.2										
DP5	A10	0.60	0.77	5.0	0.37	5.17	1.9														
	A11	0.49	0.76	5.0	0.29	5.17	1.5	6.1	0.67	4.88	3.2										
DP6	A12	0.38	0.76	9.0	0.02	4.29	0.1	9.8	3.95	4.15	16.4										
		0.21	0.09																		
DP7		5.78	0.68																		
	A13	1.09	0.24	12.3	0.26	3.82	1.0	9.9	4.21	4.14	17.4										
DP8		6.87	0.61																		

DCM: I = C1 \* ln(tc) + C2  
C1: 1.5  
C1: 7.583

DP	Sub-Basin	Area (Acres)	C100	Direct Runoff				Combined Runoff				Streetflow			Pipe Flow				Travel Time	
				t <sub>c</sub> (min)	CA (Acres)	I100 (in/hr)	Q100 (cfs)	t <sub>c</sub> (min)	CA (Acres)	I100 (in/hr)	Q100 (cfs)	Slope (%)	Length (ft)	Q (cfs)	Slope (%)	Mnngs n	Length (ft)	D <sub>Pipe</sub> (in)	Length (ft)	V <sub>0.05</sub> (ft/s)
DP1	OS-1	0.19	0.86	5.0	0.17	8.68	1.4	7.1	1.81	7.78	14.1									
	OS-2	1.02	0.82	6.2	0.84	8.15	6.9													
	OS-3	0.81	0.87	5.2	0.70	8.58	6.0													
	A1	0.21	0.65	5.4	0.14	8.50	1.2													
	A2	0.20	0.65	5.3	0.13	8.54	1.1													
DP2	OS-2,OS-3,A1,A2	2.25	0.81	9.2	0.08	7.15	0.6	6.4	0.52	8.06	4.2									
	A3	0.20	0.39	5.2	0.29	8.57	2.5													
	A4	0.34	0.84	5.0	0.23	8.68	2.0													
	A5	0.28	0.84	5.0	0.23	8.68	2.0													
	A6	0.62	0.84	5.0	0.42	8.68	3.6													
DP3	A7	3.07	0.79	5.0	0.42	8.68	3.7	6.1	0.84	8.19	6.9									
	A8	0.50	0.84	5.0	0.42	8.68	3.7													
DP4	A9	0.52	0.81	5.0	0.42	8.68	3.7	6.2	0.51	8.13	4.2									
	A10	1.02	0.82	5.0	0.28	8.68	2.4													
DP5	A11	0.33	0.85	5.0	0.23	8.68	2.0	6.1	0.74	8.19	6.1									
	A12	0.60	0.85	5.0	0.42	8.68	3.6													
DP6	A13	0.49	0.85	5.0	0.42	8.68	3.6	9.8	4.58	6.97	32.0									
	A14	0.38	0.85	5.0	0.33	8.68	2.8													
DP7	A15	0.88	0.85	9.0	0.08	7.20	0.6	9.9	5.09	6.95	35.3									
	A16	0.21	0.36	9.0	0.08	7.20	0.6													
DP8	A17	5.78	0.79	12.3	0.50	6.41	3.2	9.9	5.09	6.95	35.3									
	A18	1.09	0.46	12.3	0.50	6.41	3.2													
	A19	6.87	0.74	12.3	0.50	6.41	3.2	9.9	5.09	6.95	35.3									
	A20	6.87	0.74	12.3	0.50	6.41	3.2													

DCM: I = C1 \* ln (tc) + C2  
C1: 2.52  
C2: 12.735

## Sub-Basin OS-1 Runoff Calculations

Job No.: **61093**

Date: **10/19/18 3:06**

Project: **Townhomes at Bradley Crossroads**

Calcs by: **TJW**

Checked by: \_\_\_\_\_

Jurisdiction **DCM**

Soil Type **B**

Runoff Coefficient **Surface Type**

Urbanization **Urban**

### Basin Land Use Characteristics

Surface	Area		Runoff Coefficient						% Imperv.
	(SF)	(Acres)	C2	C5	C10	C25	C50	C100	
Roofs			0.71	0.73	0.75	0.78	0.8	0.81	90%
Driveways & Walks	6,973	0.16	0.89	0.9	0.92	0.94	0.95	0.96	100%
Landscaping	1,376	0.03	0.03	0.09	0.17	0.26	0.31	0.36	2%
<b>Combined</b>	<b>8,349</b>	<b>0.19</b>	<b>0.75</b>	<b>0.77</b>	<b>0.80</b>	<b>0.83</b>	<b>0.84</b>	<b>0.86</b>	<b>83.8%</b>

8349

### Basin Travel Time

	Shallow Channel Ground Cover		Paved areas/shallow paved swales				
	$L_{max, Overland}$	100 ft			$C_v$	20	
	L (ft)	$\Delta Z_o$ (ft)	$S_o$ (ft/ft)	$v$ (ft/s)	t (min)	$t_{Alt}$ (min)	
Total	220	6	-	-	-	-	
Initial Time	24	0	0.020	-	2.3	11.2	DCM Eq. 6-8
Shallow Channel			0.000	0.0	0.0	-	DCM Eq. 6-9
Channelized	196	6	0.031	2.9	1.1	-	C&G
				$t_c$	5.0 min.		

### Rainfall Intensity & Runoff

	2-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr
Intensity (in/hr)	4.12	5.17	6.03	6.89	7.75	8.68
Runoff (cfs)	0.6	0.8	0.9	1.1	1.3	1.4
Release Rates (cfs/ac)	-	-	-	-	-	-
Allowed Release (cfs)	0.6	0.8	0.9	1.1	1.3	1.4

$$DCM: I = C1 * \ln(tc) + C2$$

C1 1.19 1.5 1.75 2 2.25 2.52

C2 6.035 7.583 8.847 10.111 11.375 12.735

### Notes

## Sub-Basin OS-2 Runoff Calculations

Job No.: **61093**

Date: **10/19/18 3:06**

Project: **Townhomes at Bradley Crossroads**

Calcs by: **TJW**

Jurisdiction **DCM**  
Runoff Coefficient **Surface Type**

Checked by:

Soil Type **B**  
Urbanization **Urban**

### Basin Land Use Characteristics

Surface	Area		Runoff Coefficient						% Imperv.
	(SF)	(Acres)	C2	C5	C10	C25	C50	C100	
Roofs			0.71	0.73	0.75	0.78	0.8	0.81	90%
Driveways & Walks	34,551	0.79	0.89	0.9	0.92	0.94	0.95	0.96	100%
Landscaping	10,072	0.23	0.03	0.09	0.17	0.26	0.31	0.36	2%
<b>Combined</b>	<b>44,623</b>	<b>1.02</b>	<b>0.70</b>	<b>0.72</b>	<b>0.75</b>	<b>0.79</b>	<b>0.81</b>	<b>0.82</b>	<b>77.9%</b>

44623

### Basin Travel Time

Shallow Channel Ground Cover		Paved areas/shallow paved swales					
$L_{max, Overland}$		100 ft	$C_v$		20		
	$L$ (ft)	$\Delta Z_0$ (ft)	$S_0$ (ft/ft)	$v$ (ft/s)	$t$ (min)	$t_{Alt}$ (min)	
Total	420	5	-	-	-	-	
Initial Time	45	1	0.020	-	3.7	12.3	DCM Eq. 6-8
Shallow Channel	137	2	0.011	2.1	1.1	-	DCM Eq. 6-9
Channelized	238	3	0.011	2.8	1.4	-	C&G
$t_c$					6.2 min.		

### Rainfall Intensity & Runoff

	2-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr
Intensity (in/hr)	3.87	4.85	5.66	6.47	7.28	8.15
Runoff (cfs)	2.8	3.6	4.4	5.2	6.0	6.9
Release Rates (cfs/ac)	-	-	-	-	-	-
Allowed Release (cfs)	2.8	3.6	4.4	5.2	6.0	6.9

DCM:  $I = C1 * \ln(tc) + C2$

C1 1.19 1.5 1.75 2 2.25 2.52  
C2 6.035 7.583 8.847 10.111 11.375 12.735

### Notes

## Sub-Basin OS-3 Runoff Calculations

Job No.: **61093**

Date: **10/19/18 3:06**

Project: **Townhomes at Bradley Crossroads**

Calcs by: **TJW**

Jurisdiction **DCM**  
Runoff Coefficient **Surface Type**

Checked by:

Soil Type **B**  
Urbanization **Urban**

### Basin Land Use Characteristics

Surface	Area		Runoff Coefficient						% Imperv.
	(SF)	(Acres)	C2	C5	C10	C25	C50	C100	
Roofs			0.71	0.73	0.75	0.78	0.8	0.81	90%
Driveways & Walks	29,931	0.69	0.89	0.9	0.92	0.94	0.95	0.96	100%
Landscaping	5,399	0.12	0.03	0.09	0.17	0.26	0.31	0.36	2%
<b>Combined</b>	<b>35,330</b>	<b>0.81</b>	<b>0.76</b>	<b>0.78</b>	<b>0.81</b>	<b>0.84</b>	<b>0.85</b>	<b>0.87</b>	<b>85.0%</b>

35330

### Basin Travel Time

Shallow Channel Ground Cover		Paved areas/shallow paved swales					
$L_{max, Overland}$	100 ft	$C_v$	20				
$L$ (ft)	$\Delta Z_0$ (ft)	$S_0$ (ft/ft)	$v$ (ft/s)	$t$ (min)	$t_{Alt}$ (min)		
Total	243	3	-	-	-		
Initial Time	48	0	0.010	-	4.1	11.4	DCM Eq. 6-8
Shallow Channel	49	2	0.031	3.5	0.2	-	DCM Eq. 6-9
Channelized	146	1	0.010	2.6	0.9	-	C&G
				$t_c$	5.2 min.		

### Rainfall Intensity & Runoff

	2-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr
Intensity (in/hr)	4.07	5.11	5.96	6.81	7.66	8.58
Runoff (cfs)	2.5	3.2	3.9	4.6	5.3	6.0
Release Rates (cfs/ac)	-	-	-	-	-	-
Allowed Release (cfs)	2.5	3.2	3.9	4.6	5.3	6.0

$$DCM: I = C1 * \ln(tc) + C2$$

C1	1.19	1.5	1.75	2	2.25	2.52
C2	6.035	7.583	8.847	10.111	11.375	12.735

### Notes

## Sub-Basin A1 Runoff Calculations

Job No.: **61093**  
 Project: **Townhomes at Bradley Crossroads**  
 Jurisdiction: **DCM**  
 Runoff Coefficient: **Surface Type**

Date: **10/19/18 3:06**  
 Calcs by: **TJW**  
 Checked by: \_\_\_\_\_  
 Soil Type: **B**  
 Urbanization: **Urban**

### Basin Land Use Characteristics

Surface	Area		Runoff Coefficient						% Imperv.
	(SF)	(Acres)	C2	C5	C10	C25	C50	C100	
Roofs	3,864	0.09	0.71	0.73	0.75	0.78	0.8	0.81	90%
Driveways & Walks	1,458	0.03	0.89	0.9	0.92	0.94	0.95	0.96	100%
Landscaping	3,807	0.09	0.03	0.09	0.17	0.26	0.31	0.36	2%
<b>Combined</b>	<b>9,129</b>	<b>0.21</b>	<b>0.46</b>	<b>0.49</b>	<b>0.54</b>	<b>0.59</b>	<b>0.62</b>	<b>0.65</b>	<b>54.9%</b>

9129

### Basin Travel Time

Shallow Channel Ground Cover		Paved areas/shallow paved swales					
$L_{max, Overland}$		100 ft	$C_v$		20		
	$L$ (ft)	$\Delta Z_0$ (ft)	$S_0$ (ft/ft)	$v$ (ft/s)	$t$ (min)	$t_{Alt}$ (min)	
Total	48	2	-	-	-	-	
Initial Time	23	0	0.010	-	5.3	10.3	DCM Eq. 6-8
Shallow Channel	25	2	0.060	4.9	0.1	-	DCM Eq. 6-9
Channelized			0.000	0.0	0.0	-	V-Ditch
$t_c$					5.4 min.		

### Rainfall Intensity & Runoff

	2-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr
Intensity (in/hr)	4.04	5.06	5.91	6.75	7.60	8.50
Runoff (cfs)	0.4	0.5	0.7	0.8	1.0	1.2
Release Rates (cfs/ac)	-	-	-	-	-	-
Allowed Release (cfs)	0.4	0.5	0.7	0.8	1.0	1.2

DCM:  $I = C1 * \ln(tc) + C2$

C1	1.19	1.5	1.75	2	2.25	2.52
C2	6.035	7.583	8.847	10.111	11.375	12.735

### Notes

## Sub-Basin A2 Runoff Calculations

Job No.: **61093**  
 Project: **Townhomes at Bradley Crossroads**  
 Jurisdiction: **DCM**  
 Runoff Coefficient: **Surface Type**

Date: **10/19/18 3:06**  
 Calcs by: **TJW**  
 Checked by: \_\_\_\_\_  
 Soil Type: **B**  
 Urbanization: **Urban**

### Basin Land Use Characteristics

Surface	Area		Runoff Coefficient						% Imperv.
	(SF)	(Acres)	C2	C5	C10	C25	C50	C100	
Roofs	3,864	0.09	0.71	0.73	0.75	0.78	0.8	0.81	90%
Driveways & Walks	1,352	0.03	0.89	0.9	0.92	0.94	0.95	0.96	100%
Landscaping	3,497	0.08	0.03	0.09	0.17	0.26	0.31	0.36	2%
<b>Combined</b>	<b>8,713</b>	<b>0.20</b>	<b>0.47</b>	<b>0.50</b>	<b>0.54</b>	<b>0.60</b>	<b>0.63</b>	<b>0.65</b>	<b>56.2%</b>

8713

### Basin Travel Time

Shallow Channel Ground Cover		Paved areas/shallow paved swales					
$L_{max, Overland}$	100 ft	$C_v$	20				
$L$ (ft)	$\Delta Z_o$ (ft)	$S_o$ (ft/ft)	$v$ (ft/s)	$t$ (min)	$t_{Alt}$ (min)		
Total	48	2	-	-	-		
Initial Time	23	0	0.010	-	5.2	10.3	DCM Eq. 6-8
Shallow Channel	25	2	0.060	4.9	0.1	-	DCM Eq. 6-9
Channelized			0.000	0.0	0.0	-	V-Ditch
				$t_c$	5.3 min.		

### Rainfall Intensity & Runoff

	2-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr
Intensity (in/hr)	4.05	5.09	5.93	6.78	7.63	8.54
Runoff (cfs)	0.4	0.5	0.6	0.8	1.0	1.1
Release Rates (cfs/ac)	-	-	-	-	-	-
Allowed Release (cfs)	0.4	0.5	0.6	0.8	1.0	1.1

DCM:  $I = C1 * \ln(tc) + C2$

C1	1.19	1.5	1.75	2	2.25	2.52
C2	6.035	7.583	8.847	10.111	11.375	12.735

### Notes

## Sub-Basin A3 Runoff Calculations

Job No.: **61093**  
 Project: **Townhomes at Bradley Crossroads**  
 Jurisdiction: **DCM**  
 Runoff Coefficient: **Surface Type**

Date: **10/19/18 3:06**  
 Calcs by: **TJW**  
 Checked by: \_\_\_\_\_  
 Soil Type: **B**  
 Urbanization: **Urban**

### Basin Land Use Characteristics

Surface	Area		Runoff Coefficient						% Imperv.
	(SF)	(Acres)	C2	C5	C10	C25	C50	C100	
Roofs	-	0.00	0.71	0.73	0.75	0.78	0.8	0.81	90%
Driveways & Walks	393	0.01	0.89	0.9	0.92	0.94	0.95	0.96	100%
Landscaping	8,514	0.20	0.03	0.09	0.17	0.26	0.31	0.36	2%
<b>Combined</b>	<b>8,907</b>	<b>0.20</b>	<b>0.07</b>	<b>0.13</b>	<b>0.20</b>	<b>0.29</b>	<b>0.34</b>	<b>0.39</b>	<b>6.3%</b>

8907

### Basin Travel Time

Shallow Channel Ground Cover		Paved areas/shallow paved swales					
$L_{max, Overland}$		100 ft	$C_v$		20		
	$L$ (ft)	$\Delta Z_0$ (ft)	$S_0$ (ft/ft)	$v$ (ft/s)	$t$ (min)	$t_{Alt}$ (min)	
Total	174	4	-	-	-	-	
Initial Time	39	3	0.077	-	5.6	11.0	DCM Eq. 6-8
Shallow Channel			0.000	0.0	0.0	-	DCM Eq. 6-9
Channelized	135	1	0.010	0.6	3.6	-	Trap Ditch
$t_c$					9.2 min.		

### Rainfall Intensity & Runoff

	2-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr
Intensity (in/hr)	3.40	4.26	4.97	5.68	6.39	7.15
Runoff (cfs)	0.0	0.1	0.2	0.3	0.4	0.6
Release Rates (cfs/ac)	-	-	-	-	-	-
Allowed Release (cfs)	0.0	0.1	0.2	0.3	0.4	0.6

DCM:  $I = C1 * \ln(tc) + C2$

C1	1.19	1.5	1.75	2	2.25	2.52
C2	6.035	7.583	8.847	10.111	11.375	12.735

Notes

## Sub-Basin A4 Runoff Calculations

Job No.: **61093**  
 Project: **Townhomes at Bradley Crossroads**  
 Jurisdiction: **DCM**  
 Runoff Coefficient: **Surface Type**

Date: **10/19/18 3:06**  
 Calcs by: **TJW**  
 Checked by: \_\_\_\_\_  
 Soil Type: **B**  
 Urbanization: **Urban**

### Basin Land Use Characteristics

Surface	Area		Runoff Coefficient						% Imperv.
	(SF)	(Acres)	C2	C5	C10	C25	C50	C100	
Roofs	6,762	0.16	0.71	0.73	0.75	0.78	0.8	0.81	90%
Driveways & Walks	6,817	0.16	0.89	0.9	0.92	0.94	0.95	0.96	100%
Landscaping	1,269	0.03	0.03	0.09	0.17	0.26	0.31	0.36	2%
<b>Combined</b>	<b>14,848</b>	<b>0.34</b>	<b>0.73</b>	<b>0.75</b>	<b>0.78</b>	<b>0.81</b>	<b>0.83</b>	<b>0.84</b>	<b>87.1%</b>

14848

### Basin Travel Time

	Shallow Channel Ground Cover		Paved areas/shallow paved swales				
	$L_{max, Overland}$	100 ft		$C_v$	20		
	$L$ (ft)	$\Delta Z_0$ (ft)	$S_0$ (ft/ft)	$v$ (ft/s)	$t$ (min)	$t_{Alt}$ (min)	
Total	248	2	-	-	-	-	
Initial Time	23	0	0.010	-	3.0	11.4	DCM Eq. 6-8
Shallow Channel	95	1	0.010	2.0	0.8	-	DCM Eq. 6-9
Channelized	130	1	0.010	1.5	1.4	-	V-Ditch
				$t_c$	5.2 min.		

### Rainfall Intensity & Runoff

	2-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr
Intensity (in/hr)	4.07	5.10	5.95	6.80	7.66	8.57
Runoff (cfs)	1.0	1.3	1.6	1.9	2.2	2.5
Release Rates (cfs/ac)	-	-	-	-	-	-
Allowed Release (cfs)	1.0	1.3	1.6	1.9	2.2	2.5

DCM:  $I = C1 * \ln(tc) + C2$

C1	1.19	1.5	1.75	2	2.25	2.52
C2	6.035	7.583	8.847	10.111	11.375	12.735

### Notes

## Sub-Basin A5 Runoff Calculations

Job No.: **61093**  
 Project: **Townhomes at Bradley Crossroads**

Date: **10/19/18 3:06**

Calcs by: **TJW**

Checked by: \_\_\_\_\_

Jurisdiction **DCM**  
 Runoff Coefficient **Surface Type**

Soil Type **B**  
 Urbanization **Urban**

### Basin Land Use Characteristics

Surface	Area		Runoff Coefficient						% Imperv.
	(SF)	(Acres)	C2	C5	C10	C25	C50	C100	
Roofs	7,728	0.18	0.71	0.73	0.75	0.78	0.8	0.81	90%
Driveways & Walks	3,884	0.09	0.89	0.9	0.92	0.94	0.95	0.96	100%
Landscaping	368	0.01	0.03	0.09	0.17	0.26	0.31	0.36	2%
<b>Combined</b>	<b>11,980</b>	<b>0.28</b>	<b>0.75</b>	<b>0.77</b>	<b>0.79</b>	<b>0.82</b>	<b>0.83</b>	<b>0.84</b>	<b>90.5%</b>

11980

### Basin Travel Time

	Shallow Channel Ground Cover		Paved areas/shallow paved swales				
	$L_{max, Overland}$	100 ft			$C_v$	20	
	$L$ (ft)	$\Delta Z_0$ (ft)	$S_0$ (ft/ft)	$v$ (ft/s)	$t$ (min)	$t_{Alt}$ (min)	
Total	206	2	-	-	-	-	
Initial Time	23	0	0.010	-	2.9	11.1	DCM Eq. 6-8
Shallow Channel	95	1	0.010	2.0	0.8	-	DCM Eq. 6-9
Channelized	88	1	0.010	1.4	1.0	-	V-Ditch
				$t_c$	5.0 min.		

### Rainfall Intensity & Runoff

	2-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr
Intensity (in/hr)	4.12	5.17	6.03	6.89	7.75	8.68
Runoff (cfs)	0.8	1.1	1.3	1.5	1.8	2.0
Release Rates (cfs/ac)	-	-	-	-	-	-
Allowed Release (cfs)	0.8	1.1	1.3	1.5	1.8	2.0

DCM:  $I = C1 * \ln(tc) + C2$

C1      1.19      1.5      1.75      2      2.25      2.52  
 C2      6.035      7.583      8.847      10.111      11.375      12.735

### Notes

## Sub-Basin A6 Runoff Calculations

Job No.: 61093  
 Project: Townhomes at Bradley Crossroads  
 Jurisdiction: DCM  
 Runoff Coefficient: Surface Type

Date: 10/19/18 3:06  
 Calcs by: TJW  
 Checked by: \_\_\_\_\_  
 Soil Type: B  
 Urbanization: Urban

### Basin Land Use Characteristics

Surface	Area		Runoff Coefficient						% Imperv.
	(SF)	(Acres)	C2	C5	C10	C25	C50	C100	
Roofs	6,762	0.16	0.71	0.73	0.75	0.78	0.8	0.81	90%
Driveways & Walks	12,186	0.28	0.89	0.9	0.92	0.94	0.95	0.96	100%
Landscaping	2,729	0.06	0.03	0.09	0.17	0.26	0.31	0.36	2%
<b>Combined</b>	<b>21,677</b>	<b>0.50</b>	<b>0.73</b>	<b>0.74</b>	<b>0.77</b>	<b>0.80</b>	<b>0.82</b>	<b>0.84</b>	<b>84.5%</b>

21677

### Basin Travel Time

Shallow Channel Ground Cover		Paved areas/shallow paved swales					
$L_{max, Overland}$		100 ft	$C_v$		20		
	$L$ (ft)	$\Delta Z_o$ (ft)	$S_o$ (ft/ft)	$v$ (ft/s)	$t$ (min)	$t_{Alt}$ (min)	
Total	261	4	-	-	-	-	
Initial Time	23	0	0.010	-	3.1	11.5	DCM Eq. 6-8
Shallow Channel	140	2	0.014	2.4	1.0	-	DCM Eq. 6-9
Channelized	98	2	0.015	1.9	0.8	-	V-Ditch
					$t_c$	5.0 min.	

### Rainfall Intensity & Runoff

	2-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr
Intensity (in/hr)	4.12	5.17	6.03	6.89	7.75	8.68
Runoff (cfs)	1.5	1.9	2.3	2.8	3.2	3.6
Release Rates (cfs/ac)	-	-	-	-	-	-
Allowed Release (cfs)	1.5	1.9	2.3	2.8	3.2	3.6

$$DCM: I = C1 * \ln(tc) + C2$$

C1	1.19	1.5	1.75	2	2.25	2.52
C2	6.035	7.583	8.847	10.111	11.375	12.735

### Notes

## Sub-Basin A7 Runoff Calculations

Job No.: 61093  
 Project: Townhomes at Bradley Crossroads  
 Jurisdiction: DCM  
 Runoff Coefficient: Surface Type

Date: 10/19/18 3:06  
 Calcs by: TJW  
 Checked by: \_\_\_\_\_  
 Soil Type: B  
 Urbanization: Urban

### Basin Land Use Characteristics

Surface	Area		Runoff Coefficient						% Imperv.
	(SF)	(Acres)	C2	C5	C10	C25	C50	C100	
Roofs	7,728	0.18	0.71	0.73	0.75	0.78	0.8	0.81	90%
Driveways & Walks	11,300	0.26	0.89	0.9	0.92	0.94	0.95	0.96	100%
Landscaping	3,749	0.09	0.03	0.09	0.17	0.26	0.31	0.36	2%
<b>Combined</b>	<b>22,777</b>	<b>0.52</b>	<b>0.69</b>	<b>0.71</b>	<b>0.74</b>	<b>0.77</b>	<b>0.79</b>	<b>0.81</b>	<b>80.5%</b>

22777

### Basin Travel Time

Shallow Channel Ground Cover		Paved areas/shallow paved swales					
$L_{max, Overland}$		100 ft	$C_v$		20		
	$L$ (ft)	$\Delta Z_0$ (ft)	$S_0$ (ft/ft)	$v$ (ft/s)	$t$ (min)	$t_{Alt}$ (min)	
Total	221	3	-	-	-	-	
Initial Time	23	0	0.010	-	3.4	11.2	DCM Eq. 6-8
Shallow Channel	118	2	0.019	2.8	0.7	-	DCM Eq. 6-9
Channelized	80	1	0.009	1.6	0.9	-	V-Ditch
					$t_c$	5.0 min.	

### Rainfall Intensity & Runoff

	2-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr
Intensity (in/hr)	4.12	5.17	6.03	6.89	7.75	8.68
Runoff (cfs)	1.5	1.9	2.3	2.8	3.2	3.7
Release Rates (cfs/ac)	-	-	-	-	-	-
Allowed Release (cfs)	1.5	1.9	2.3	2.8	3.2	3.7

DCM:  $I = C1 * \ln(tc) + C2$

C1	1.19	1.5	1.75	2	2.25	2.52
C2	6.035	7.583	8.847	10.111	11.375	12.735

### Notes

## Sub-Basin A8 Runoff Calculations

Job No.: **61093**  
 Project: **Townhomes at Bradley Crossroads**  
 Jurisdiction: **DCM**  
 Runoff Coefficient: **Surface Type**

Date: **10/19/18 3:06**  
 Calcs by: **TJW**  
 Checked by: \_\_\_\_\_  
 Soil Type: **B**  
 Urbanization: **Urban**

### Basin Land Use Characteristics

Surface	Area		Runoff Coefficient						% Imperv.
	(SF)	(Acres)	C2	C5	C10	C25	C50	C100	
Roofs	7,728	0.18	0.71	0.73	0.75	0.78	0.8	0.81	90%
Driveways & Walks	5,922	0.14	0.89	0.9	0.92	0.94	0.95	0.96	100%
Landscaping	640	0.01	0.03	0.09	0.17	0.26	0.31	0.36	2%
<b>Combined</b>	<b>14,290</b>	<b>0.33</b>	<b>0.75</b>	<b>0.77</b>	<b>0.79</b>	<b>0.82</b>	<b>0.84</b>	<b>0.85</b>	<b>90.2%</b>

14290

### Basin Travel Time

	Shallow Channel Ground Cover		Paved areas/shallow paved swales				
	$L_{max, Overland}$	100 ft			$C_v$	20	
	$L$ (ft)	$\Delta Z_0$ (ft)	$S_0$ (ft/ft)	$v$ (ft/s)	$t$ (min)	$t_{Alt}$ (min)	
Total	244	3	-	-	-	-	
Initial Time	23	0	0.010	-	2.8	11.4	DCM Eq. 6-8
Shallow Channel	115	1	0.011	2.1	0.9	-	DCM Eq. 6-9
Channelized	106	1	0.009	1.5	1.2	-	V-Ditch
				$t_c$	5.0 min.		

### Rainfall Intensity & Runoff

	2-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr
Intensity (in/hr)	4.12	5.17	6.03	6.89	7.75	8.68
Runoff (cfs)	1.0	1.3	1.6	1.9	2.1	2.4
Release Rates (cfs/ac)	-	-	-	-	-	-
Allowed Release (cfs)	1.0	1.3	1.6	1.9	2.1	2.4

$$DCM: I = C1 * \ln(tc) + C2$$

C1	1.19	1.5	1.75	2	2.25	2.52
C2	6.035	7.583	8.847	10.111	11.375	12.735

### Notes

## Sub-Basin A9 Runoff Calculations

Job No.: **61093**  
 Project: **Townhomes at Bradley Crossroads**

Date: **10/19/18 3:06**

Calcs by: **TJW**

Checked by: \_\_\_\_\_

Jurisdiction **DCM**  
 Runoff Coefficient **Surface Type**

Soil Type **B**  
 Urbanization **Urban**

### Basin Land Use Characteristics

Surface	Area		Runoff Coefficient						% Imperv.
	(SF)	(Acres)	C2	C5	C10	C25	C50	C100	
Roofs	7,728	0.18	0.71	0.73	0.75	0.78	0.8	0.81	90%
Driveways & Walks	3,884	0.09	0.89	0.9	0.92	0.94	0.95	0.96	100%
Landscaping	368	0.01	0.03	0.09	0.17	0.26	0.31	0.36	2%
<b>Combined</b>	<b>11,980</b>	<b>0.28</b>	<b>0.75</b>	<b>0.77</b>	<b>0.79</b>	<b>0.82</b>	<b>0.83</b>	<b>0.84</b>	<b>90.5%</b>

11980

### Basin Travel Time

	Shallow Channel Ground Cover		Paved areas/shallow paved swales				
	$L_{max, Overland}$	100 ft			$C_v$	20	
	$L$ (ft)	$\Delta Z_o$ (ft)	$S_o$ (ft/ft)	$v$ (ft/s)	$t$ (min)	$t_{Alt}$ (min)	
Total	200	2	-	-	-	-	
Initial Time	23	0	0.010	-	2.9	11.1	DCM Eq. 6-8
Shallow Channel	98	1	0.014	2.4	0.7	-	DCM Eq. 6-9
Channelized	79	1	0.009	1.4	1.0	-	V-Ditch
				$t_c$	5.0 min.		

### Rainfall Intensity & Runoff

	2-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr
Intensity (in/hr)	4.12	5.17	6.03	6.89	7.75	8.68
Runoff (cfs)	0.8	1.1	1.3	1.5	1.8	2.0
Release Rates (cfs/ac)	-	-	-	-	-	-
Allowed Release (cfs)	0.8	1.1	1.3	1.5	1.8	2.0

$$DCM: I = C1 * \ln(tc) + C2$$

C1 1.19 1.5 1.75 2 2.25 2.52

C2 6.035 7.583 8.847 10.111 11.375 12.735

### Notes

## Sub-Basin A10 Runoff Calculations

Job No.: 61093  
 Project: Townhomes at Bradley Crossroads

Date: 10/19/18 3:06

Calcs by: TJW

Checked by: \_\_\_\_\_

Jurisdiction DCM  
 Runoff Coefficient Surface Type

Soil Type B  
 Urbanization Urban

### Basin Land Use Characteristics

Surface	Area		Runoff Coefficient						% Imperv.
	(SF)	(Acres)	C2	C5	C10	C25	C50	C100	
Roofs	7,728	0.18	0.71	0.73	0.75	0.78	0.8	0.81	90%
Driveways & Walks	11,558	0.27	0.89	0.9	0.92	0.94	0.95	0.96	100%
Landscaping	2,127	0.05	0.03	0.09	0.17	0.26	0.31	0.36	2%
<b>Combined</b>	<b>21,413</b>	<b>0.49</b>	<b>0.74</b>	<b>0.76</b>	<b>0.78</b>	<b>0.81</b>	<b>0.83</b>	<b>0.85</b>	<b>86.7%</b>

21413

### Basin Travel Time

	Shallow Channel Ground Cover		Paved areas/shallow paved swales				
	$L_{max, Overland}$	100 ft			$C_v$	20	
	$L$ (ft)	$\Delta Z_0$ (ft)	$S_0$ (ft/ft)	$v$ (ft/s)	$t$ (min)	$t_{Alt}$ (min)	
Total	263	3	-	-	-	-	
Initial Time	23	0	0.010	-	3.0	11.5	DCM Eq. 6-8
Shallow Channel	138	2	0.013	2.3	1.0	-	DCM Eq. 6-9
Channelized	102	1	0.012	1.8	1.0	-	V-Ditch
				$t_c$	5.0 min.		

### Rainfall Intensity & Runoff

	2-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr
Intensity (in/hr)	4.12	5.17	6.03	6.89	7.75	8.68
Runoff (cfs)	1.5	1.9	2.3	2.8	3.2	3.6
Release Rates (cfs/ac)	-	-	-	-	-	-
Allowed Release (cfs)	1.5	1.9	2.3	2.8	3.2	3.6

$$DCM: I = C1 * \ln(tc) + C2$$

C1 1.19 1.5 1.75 2 2.25 2.52

C2 6.035 7.583 8.847 10.111 11.375 12.735

### Notes

## Sub-Basin A11 Runoff Calculations

Job No.: **61093**  
 Project: **Townhomes at Bradley Crossroads**  
 Jurisdiction: **DCM**  
 Runoff Coefficient: **Surface Type**

Date: **10/19/18 3:06**  
 Calcs by: **TJW**  
 Checked by: \_\_\_\_\_  
 Soil Type: **B**  
 Urbanization: **Urban**

### Basin Land Use Characteristics

Surface	Area		Runoff Coefficient						% Imperv.
	(SF)	(Acres)	C2	C5	C10	C25	C50	C100	
Roofs	7,728	0.18	0.71	0.73	0.75	0.78	0.8	0.81	90%
Driveways & Walks	7,780	0.18	0.89	0.9	0.92	0.94	0.95	0.96	100%
Landscaping	1,232	0.03	0.03	0.09	0.17	0.26	0.31	0.36	2%
<b>Combined</b>	<b>16,740</b>	<b>0.38</b>	<b>0.74</b>	<b>0.76</b>	<b>0.79</b>	<b>0.82</b>	<b>0.83</b>	<b>0.85</b>	<b>88.2%</b>

16740

### Basin Travel Time

Shallow Channel Ground Cover			Paved areas/shallow paved swales				
$L_{max, Overland}$	100	ft	$C_v$	20			
$L$ (ft)	$\Delta Z_0$ (ft)	$S_0$ (ft/ft)	$v$ (ft/s)	$t$ (min)	$t_{Alt}$ (min)		
Total	224	3	-	-	-		
Initial Time	23	0	0.010	-	2.9	11.2	DCM Eq. 6-8
Shallow Channel	118	2	0.015	2.5	0.8	-	DCM Eq. 6-9
Channelized	83	1	0.014	1.8	0.8	-	V-Ditch
			$t_c$	5.0	min.		

### Rainfall Intensity & Runoff

	2-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr
Intensity (in/hr)	4.12	5.17	6.03	6.89	7.75	8.68
Runoff (cfs)	1.2	1.5	1.8	2.2	2.5	2.8
Release Rates (cfs/ac)	-	-	-	-	-	-
Allowed Release (cfs)	1.2	1.5	1.8	2.2	2.5	2.8

$$DCM: I = C1 * \ln(tc) + C2$$

C1	1.19	1.5	1.75	2	2.25	2.52
C2	6.035	7.583	8.847	10.111	11.375	12.735

### Notes

## Sub-Basin A12 Runoff Calculations

Job No.: **61093**

Date: **10/19/18 3:06**

Project: **Townhomes at Bradley Crossroads**

Calcs by: **TJW**

Jurisdiction **DCM**  
Runoff Coefficient **Surface Type**

Checked by:

Soil Type **B**  
Urbanization **Urban**

### Basin Land Use Characteristics

Surface	Area		Runoff Coefficient						% Imperv.
	(SF)	(Acres)	C2	C5	C10	C25	C50	C100	
Roofs			0.71	0.73	0.75	0.78	0.8	0.81	90%
Driveways & Walks			0.89	0.9	0.92	0.94	0.95	0.96	100%
Landscaping	9,251	0.21	0.03	0.09	0.17	0.26	0.31	0.36	2%
<b>Combined</b>	<b>9,251</b>	<b>0.21</b>	<b>0.03</b>	<b>0.09</b>	<b>0.17</b>	<b>0.26</b>	<b>0.31</b>	<b>0.36</b>	<b>2.0%</b>

9251

### Basin Travel Time

Shallow Channel Ground Cover		Short Pasture/Lawns					
$L_{max, Overland}$		100 ft	$C_v$		7		
	$L$ (ft)	$\Delta Z_0$ (ft)	$S_0$ (ft/ft)	$v$ (ft/s)	$t$ (min)	$t_{Alt}$ (min)	
Total	250	5	-	-	-	-	
Initial Time	20	3	0.150	-	3.3	11.4	DCM Eq. 6-8
Shallow Channel			0.000	0.0	0.0	-	DCM Eq. 6-9
Channelized	230	2	0.007	0.7	5.7	-	Trap Ditch
					$t_c$	9.0 min.	

### Rainfall Intensity & Runoff

	2-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr
Intensity (in/hr)	3.42	4.29	5.00	5.72	6.43	7.20
Runoff (cfs)	0.0	0.1	0.2	0.3	0.4	0.6
Release Rates (cfs/ac)	-	-	-	-	-	-
Allowed Release (cfs)	0.0	0.1	0.2	0.3	0.4	0.6

$$DCM: I = C1 * \ln(tc) + C2$$

C1	1.19	1.5	1.75	2	2.25	2.52
C2	6.035	7.583	8.847	10.111	11.375	12.735

### Notes

## Sub-Basin A13 Runoff Calculations

Job No.: **61093**  
 Project: **Townhomes at Bradley Crossroads**  
 Jurisdiction: **DCM**  
 Runoff Coefficient: **Surface Type**

Date: **10/19/18 3:06**  
 Calcs by: **TJW**  
 Checked by: \_\_\_\_\_  
 Soil Type: **B**  
 Urbanization: **Urban**

### Basin Land Use Characteristics

Surface	Area		Runoff Coefficient						% Imperv.
	(SF)	(Acres)	C2	C5	C10	C25	C50	C100	
Roofs	7,728	0.18	0.71	0.73	0.75	0.78	0.8	0.81	90%
Driveways & Walks	2,409	0.06	0.89	0.9	0.92	0.94	0.95	0.96	100%
Landscaping	37,250	0.86	0.03	0.09	0.17	0.26	0.31	0.36	2%
<b>Combined</b>	<b>47,387</b>	<b>1.09</b>	<b>0.18</b>	<b>0.24</b>	<b>0.30</b>	<b>0.38</b>	<b>0.42</b>	<b>0.46</b>	<b>21.3%</b>

47387

### Basin Travel Time

	Shallow Channel Ground Cover		Short Pasture/Lawns				
	$L_{max, Overland}$	100 ft			$C_v$	7	
	$L$ (ft)	$\Delta Z_o$ (ft)	$S_o$ (ft/ft)	$v$ (ft/s)	$t$ (min)	$t_{Alt}$ (min)	
Total	414	5	-	-	-	-	
Initial Time	100	1	0.007	-	17.6	12.3	DCM Eq. 6-8
Shallow Channel	113	2	0.014	0.8	2.3	-	DCM Eq. 6-9
Channelized	201	3	0.015	2.4	1.4	-	V-Ditch
				$t_c$	12.3 min.		

### Rainfall Intensity & Runoff

	2-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr
Intensity (in/hr)	3.05	3.82	4.46	5.09	5.73	6.41
Runoff (cfs)	0.6	1.0	1.5	2.1	2.6	3.2
Release Rates (cfs/ac)	-	-	-	-	-	-
Allowed Release (cfs)	0.6	1.0	1.5	2.1	2.6	3.2

$$DCM: I = C1 * \ln(tc) + C2$$

C1	1.19	1.5	1.75	2	2.25	2.52
C2	6.035	7.583	8.847	10.111	11.375	12.735

### Notes

## Combined Sub-Basin Runoff Calculations (DP1)

Includes Basins A1 A2 OS-2 OS-3

Job No.: **61093**

Date: **10/19/18 3:26**

Project: **Townhomes at Bradley Crossroads**

Calcs by: **TJW**

Jurisdiction: **DCM**

Checked by:

Runoff Coefficient: **Surface Type**

Soil Type: **B**

Urbanization: **Urban**

### Basin Land Use Characteristics

Surface	Area		Runoff Coefficient						% Imperv.
	(SF)	(Acres)	C2	C5	C10	C25	C50	C100	
Roofs	7,728	0.18	0.71	0.73	0.75	0.78	0.8	0.81	90%
Driveways & Walks	67,292	1.54	0.89	0.9	0.92	0.94	0.95	0.96	100%
Landscaping	22,775	0.52	0.03	0.09	0.17	0.26	0.31	0.36	2%
<b>Combined</b>	<b>97,795</b>	<b>2.25</b>	<b>0.68</b>	<b>0.70</b>	<b>0.73</b>	<b>0.77</b>	<b>0.79</b>	<b>0.81</b>	<b>76.4%</b>

### Basin Travel Time

	Sub-basin or Channel Type	Material Type	L (ft)	Elev. $\Delta Z_0$ (ft)	$Q_i$ (cfs)	Base or Dia (ft)	Sides z:1 (ft/ft)	v (ft/s)	t (min)
Furthest Reach	OS-2	-	420	5	-	-	-	-	6.2
Channelized-1	C&G	Concrete	154	1	7	0	0	2.7	1.0
Channelized-2									
Channelized-3									
Total			574	6					
								$t_c$ (min)	7.1

### Contributing Offsite Flows (Added to Runoff and Allowed Release, below.)

Contributing Basins/Areas

$Q_{Minor}$  (cfs) - 5-year Storm  
 $Q_{Major}$  (cfs) - 100-year Storm

### Rainfall Intensity & Runoff

	2-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr
Intensity (in/hr)	3.70	4.64	5.41	6.18	6.95	7.78
Site Runoff (cfs)	5.61	7.26	8.89	10.67	12.32	14.12
OffSite Runoff (cfs)	-	0.00	-	-	-	0.00
Release Rates (cfs/ac)	-	-	-	-	-	-
Allowed Release (cfs)	-	7.3	-	-	-	14.1

DCM:  $I = C1 * \ln(tc) + C2$

C1 1.19 1.5 1.75 2 2.25 2.52

C2 6.035 7.583 8.847 10.111 11.375 12.735

### Notes

Runoff from Offsite basins have been assumed constant, despite additional times of concentration.

## Combined Sub-Basin Runoff Calculations (DP2)

Includes Basins A4 A5

Job No.: **61093**

Date: **10/19/18 3:26**

Project: **Townhomes at Bradley Crossroads**

Calcs by: **TJW**

Jurisdiction: **DCM**

Checked by: \_\_\_\_\_

Runoff Coefficient: **Surface Type**

Soil Type: **B**

Urbanization: **Urban**

### Basin Land Use Characteristics

Surface	Area		Runoff Coefficient						% Imperv.
	(SF)	(Acres)	C2	C5	C10	C25	C50	C100	
Roofs	14,490	0.33	0.71	0.73	0.75	0.78	0.8	0.81	90%
Driveways & Walks	10,701	0.25	0.89	0.9	0.92	0.94	0.95	0.96	100%
Landscaping	1,637	0.04	0.03	0.09	0.17	0.26	0.31	0.36	2%
<b>Combined</b>	<b>26,828</b>	<b>0.62</b>	<b>0.74</b>	<b>0.76</b>	<b>0.78</b>	<b>0.81</b>	<b>0.83</b>	<b>0.84</b>	<b>88.6%</b>

### Basin Travel Time

	Sub-basin or Channel Type	Material Type	L (ft)	Elev. $\Delta Z_0$ (ft)	$Q_i$ (cfs)	Base or Dia (ft)	Sides z:1 (ft/ft)	v (ft/s)	t (min)
Furthest Reach	A4	-	248	2	-	-	-	-	5.2
Channelized-1	V-Ditch	1	180	2	2	0	2	2.5	1.2
Channelized-2									
Channelized-3									
<b>Total</b>			<b>428</b>	<b>4</b>					

1 = Man-made, Smooth, Straight

**$t_c$  (min) 6.4**

### Contributing Offsite Flows (Added to Runoff and Allowed Release, below.)

Contributing Basins/Areas

$Q_{Minor}$  (cfs) - 5-year Storm  
 $Q_{Major}$  (cfs) - 100-year Storm

### Rainfall Intensity & Runoff

	2-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr
<b>Intensity (in/hr)</b>	3.83	4.80	5.60	6.40	7.20	8.06
<b>Site Runoff (cfs)</b>	1.74	2.24	2.70	3.20	3.68	4.18
<b>OffSite Runoff (cfs)</b>	-	0.00	-	-	-	0.00
<b>Release Rates (cfs/ac)</b>	-	-	-	-	-	-
<b>Allowed Release (cfs)</b>	-	2.2	-	-	-	4.2

DCM:  $I = C1 * \ln(tc) + C2$

C1 1.19 1.5 1.75 2 2.25 2.52  
C2 6.035 7.583 8.847 10.111 11.375 12.735

### Notes

Runoff from Offsite basins have been assumed constant, despite additional times of concentration.

## Combined Sub-Basin Runoff Calculations (DP3)

Includes Basins DP1 DP2 A3

Job No.: **61093**

Date: **10/19/18 3:26**

Project: **Townhomes at Bradley Crossroads**

Calcs by: **TJW**

Jurisdiction: **DCM**

Checked by:

Runoff Coefficient: **Surface Type**

Soil Type: **B**

Urbanization: **Urban**

### Basin Land Use Characteristics

Surface	Area		Runoff Coefficient						% Imperv.
	(SF)	(Acres)	C2	C5	C10	C25	C50	C100	
Roofs	22,218	0.51	0.71	0.73	0.75	0.78	0.8	0.81	90%
Driveways & Walks	78,386	1.80	0.89	0.9	0.92	0.94	0.95	0.96	100%
Landscaping	32,926	0.76	0.03	0.09	0.17	0.26	0.31	0.36	2%
<b>Combined</b>	<b>133,530</b>	<b>3.07</b>	<b>0.65</b>	<b>0.67</b>	<b>0.71</b>	<b>0.75</b>	<b>0.77</b>	<b>0.79</b>	<b>74.2%</b>

### Basin Travel Time

	Sub-basin or Channel Type	Material Type	L (ft)	Elev. $\Delta Z_0$ (ft)	$Q_i$ (cfs)	Base or Dia (ft)	Sides z:1 (ft/ft)	v (ft/s)	t (min)
Furthest Reach	DP1	-	574	6	-	-	-	-	7.1
Channelized-1	Trap Ditch	4	172	1	14	2	2	2.7	1.1
Channelized-2									
Channelized-3									
Total			746	8					
	4 = Riprap							$t_c$ (min)	8.2

### Contributing Offsite Flows (Added to Runoff and Allowed Release, below.)

Contributing Basins/Areas

$Q_{Minor}$  (cfs) - 5-year Storm  
 $Q_{Major}$  (cfs) - 100-year Storm

### Rainfall Intensity & Runoff

	2-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr
Intensity (in/hr)	3.53	4.43	5.17	5.91	6.64	7.44
Site Runoff (cfs)	7.02	9.12	11.20	13.50	15.63	17.94
OffSite Runoff (cfs)	-	0.00	-	-	-	0.00
Release Rates (cfs/ac)	-	-	-	-	-	-
Allowed Release (cfs)	-	9.1	-	-	-	17.9

$$DCM: I = C1 * \ln(tc) + C2$$

C1: 1.19 1.5 1.75 2 2.25 2.52

C2: 6.035 7.583 8.847 10.111 11.375 12.735

### Notes

Runoff from Offsite basins have been assumed constant, despite additional times of concentration.

## Combined Sub-Basin Runoff Calculations (DP4)

Includes Basins A6 A7

Job No.: **61093**

Date: **10/19/18 3:26**

Project: **Townhomes at Bradley Crossroads**

Calcs by: **TJW**

Jurisdiction: **DCM**

Checked by: \_\_\_\_\_

Runoff Coefficient: **Surface Type**

Soil Type: **B**

Urbanization: **Urban**

### Basin Land Use Characteristics

Surface	Area		Runoff Coefficient						%
	(SF)	(Acres)	C2	C5	C10	C25	C50	C100	Imperv.
Roofs	14,490	0.33	0.71	0.73	0.75	0.78	0.8	0.81	90%
Driveways & Walks	23,486	0.54	0.89	0.9	0.92	0.94	0.95	0.96	100%
Landscaping	6,478	0.15	0.03	0.09	0.17	0.26	0.31	0.36	2%
Combined	44,454	1.02	0.71	0.73	0.76	0.79	0.81	0.82	82.5%

### Basin Travel Time

	Sub-basin or Channel Type	Material Type	L (ft)	Elev. $\Delta Z_0$ (ft)	$Q_i$ (cfs)	Base or Dia (ft)	Sides z:1 (ft/ft)	v (ft/s)	t (min)
Furthest Reach	A6	-	261	4	-	-	-	-	5.0
Channelized-1	V-Ditch	1	180	2	4	0	2	2.8	1.1
Channelized-2									
Channelized-3									
Total			441	6					
1 = Man-made, Smooth, Straight									
									$t_c$ (min) <b>6.1</b>

### Contributing Offsite Flows (Added to Runoff and Allowed Release, below.)

Contributing Basins/Areas

$Q_{Minor}$  (cfs) - 5-year Storm  
 $Q_{Major}$  (cfs) - 100-year Storm

### Rainfall Intensity & Runoff

	2-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr
Intensity (in/hr)	3.89	4.88	5.69	6.50	7.32	8.19
Site Runoff (cfs)	2.80	3.62	4.39	5.23	6.03	6.88
OffSite Runoff (cfs)	-	0.00	-	-	-	0.00
Release Rates (cfs/ac)	-	-	-	-	-	-
Allowed Release (cfs)	-	3.6	-	-	-	6.9

DCM:  $I = C1 * \ln(tc) + C2$

C1 1.19 1.5 1.75 2 2.25 2.52  
C2 6.035 7.583 8.847 10.111 11.375 12.735

### Notes

Runoff from Offsite basins have been assumed constant, despite additional times of concentration.

## Combined Sub-Basin Runoff Calculations (DP5)

Includes Basins A8 A9

Job No.: **61093**

Date: **10/19/18 3:26**

Project: **Townhomes at Bradley Crossroads**

Calcs by: **TJW**

Jurisdiction: **DCM**

Checked by:

Runoff Coefficient: **Surface Type**

Soil Type: **B**

Urbanization: **Urban**

### Basin Land Use Characteristics

Surface	Area		Runoff Coefficient						% Imperv.
	(SF)	(Acres)	C2	C5	C10	C25	C50	C100	
Roofs	15,456	0.35	0.71	0.73	0.75	0.78	0.8	0.81	90%
Driveways & Walks	9,806	0.23	0.89	0.9	0.92	0.94	0.95	0.96	100%
Landscaping	1,008	0.02	0.03	0.09	0.17	0.26	0.31	0.36	2%
<b>Combined</b>	<b>26,270</b>	<b>0.60</b>	<b>0.75</b>	<b>0.77</b>	<b>0.79</b>	<b>0.82</b>	<b>0.84</b>	<b>0.85</b>	<b>90.4%</b>

### Basin Travel Time

	Sub-basin or Channel Type	Material Type	L (ft)	Elev. $\Delta Z_0$ (ft)	$Q_i$ (cfs)	Base or Dia (ft)	Sides z:1 (ft/ft)	v (ft/s)	t (min)
Furthest Reach	A8	-	244	3	-	-	-	-	5.0
Channelized-1	V-Ditch	1	180	2	2	0	2	2.5	1.2
Channelized-2									
Channelized-3									
<b>Total</b>			<b>424</b>	<b>4</b>					

1 = Man-made, Smooth, Straight

$t_c$  (min) **6.2**

### Contributing Offsite Flows (Added to Runoff and Allowed Release, below.)

Contributing Basins/Areas

$Q_{Minor}$  (cfs) - 5-year Storm  
 $Q_{Major}$  (cfs) - 100-year Storm

### Rainfall Intensity & Runoff

	2-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr
<b>Intensity (in/hr)</b>	3.86	4.84	5.65	6.46	7.27	8.13
<b>Site Runoff (cfs)</b>	1.75	2.25	2.70	3.19	3.67	4.16
<b>OffSite Runoff (cfs)</b>	-	0.00	-	-	-	0.00
<b>Release Rates (cfs/ac)</b>	-	-	-	-	-	-
<b>Allowed Release (cfs)</b>	-	2.2	-	-	-	4.2

$$DCM: I = C1 * \ln(tc) + C2$$

C1 1.19 1.5 1.75 2 2.25 2.52

C2 6.035 7.583 8.847 10.111 11.375 12.735

### Notes

Runoff from Offsite basins have been assumed constant, despite additional times of concentration.

## Combined Sub-Basin Runoff Calculations (DP6)

Includes Basins A10 A11

Job No.: **61093**

Date: **10/19/18 3:26**

Project: **Townhomes at Bradley Crossroads**

Calcs by: **TJW**

Jurisdiction **DCM**  
Runoff Coefficient **Surface Type**

Checked by: \_\_\_\_\_

Soil Type **B**  
Urbanization **Urban**

### Basin Land Use Characteristics

Surface	Area		Runoff Coefficient						% Imperv.
	(SF)	(Acres)	C2	C5	C10	C25	C50	C100	
Roofs	15,456	0.35	0.71	0.73	0.75	0.78	0.8	0.81	90%
Driveways & Walks	19,338	0.44	0.89	0.9	0.92	0.94	0.95	0.96	100%
Landscaping	3,359	0.08	0.03	0.09	0.17	0.26	0.31	0.36	2%
<b>Combined</b>	<b>38,153</b>	<b>0.88</b>	<b>0.74</b>	<b>0.76</b>	<b>0.79</b>	<b>0.82</b>	<b>0.83</b>	<b>0.85</b>	<b>87.3%</b>

### Basin Travel Time

	Sub-basin or Channel Type	Material Type	L (ft)	Elev. $\Delta Z_0$ (ft)	$Q_i$ (cfs)	Base or Dia (ft)	Sides z:1 (ft/ft)	v (ft/s)	t (min)
Furthest Reach	A10	-	263	3	-	-	-	-	5.0
Channelized-1	V-Ditch	1	185	2	4	0	2	2.9	1.1
Channelized-2									
Channelized-3									
Total			448	5					

1 = Man-made, Smooth, Straight

$t_c$  (min) **6.1**

### Contributing Offsite Flows (Added to Runoff and Allowed Release, below.)

Contributing Basins/Areas	
$Q_{Minor}$	(cfs) - 5-year Storm
$Q_{Major}$	(cfs) - 100-year Storm

### Rainfall Intensity & Runoff

	2-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr
Intensity (in/hr)	3.89	4.88	5.69	6.50	7.32	8.19
Site Runoff (cfs)	2.53	3.25	3.91	4.64	5.34	6.07
OffSite Runoff (cfs)	-	0.00	-	-	-	0.00
Release Rates (cfs/ac)	-	-	-	-	-	-
Allowed Release (cfs)	-	3.2	-	-	-	6.1

DCM:  $I = C1 * \ln(tc) + C2$

C1	1.19	1.5	1.75	2	2.25	2.52
C2	6.035	7.583	8.847	10.111	11.375	12.735

### Notes

Runoff from Offsite basins have been assumed constant, despite additional times of concentration.

## Combined Sub-Basin Runoff Calculations (DP7)

Includes Basins DP3 DP4 DP5 DP6 A12

Job No.: **61093**

Date: **10/19/18 3:26**

Project: **Townhomes at Bradley Crossroads**

Calcs by: **TJW**

Jurisdiction: **DCM**

Checked by: \_\_\_\_\_

Runoff Coefficient: **Surface Type**

Soil Type: **B**

Urbanization: **Urban**

### Basin Land Use Characteristics

Surface	Area		Runoff Coefficient						%
	(SF)	(Acres)	C2	C5	C10	C25	C50	C100	Imperv.
Roofs	67,620	1.55	0.71	0.73	0.75	0.78	0.8	0.81	90%
Driveways & Walks	131,016	3.01	0.89	0.9	0.92	0.94	0.95	0.96	100%
Landscaping	53,022	1.22	0.03	0.09	0.17	0.26	0.31	0.36	2%
Combined	251,658	5.78	0.66	0.68	0.72	0.75	0.77	0.79	76.7%

### Basin Travel Time

	Sub-basin or Channel Type	Material Type	L (ft)	Elev. $\Delta Z_0$ (ft)	$Q_i$ (cfs)	Base or Dia (ft)	Sides z:1 (ft/ft)	v (ft/s)	t (min)
Furthest Reach	DP3	-	746	8	-	-	-	-	8.2
Channelized-1	Trap Ditch	4	265	3	18	5	3	2.7	1.6
Channelized-2									
Channelized-3									
Total			1,011	11					
	4 = Riprap							$t_c$ (min)	9.8

### Contributing Offsite Flows (Added to Runoff and Allowed Release, below.)

Contributing Basins/Areas

$Q_{Minor}$  (cfs) - 5-year Storm  
 $Q_{Major}$  (cfs) - 100-year Storm

### Rainfall Intensity & Runoff

	2-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr
Intensity (in/hr)	3.31	4.15	4.85	5.54	6.23	6.97
Site Runoff (cfs)	12.65	16.41	20.06	24.12	27.90	31.97
OffSite Runoff (cfs)	-	0.00	-	-	-	0.00
Release Rates (cfs/ac)	-	-	-	-	-	-
Allowed Release (cfs)	-	16.4	-	-	-	32.0

DCM:  $I = C1 * \ln(tc) + C2$

C1 1.19 1.5 1.75 2 2.25 2.52  
C2 6.035 7.583 8.847 10.111 11.375 12.735

### Notes

Runoff from Offsite basins have been assumed constant, despite additional times of concentration.

## Combined Sub-Basin Runoff Calculations (DP8)

Includes Basins A13

Job No.: **61093**

Date: **10/19/18 3:26**

Project: **Townhomes at Bradley Crossroads**

Calcs by: **TJW**

Jurisdiction: **DCM**

Checked by:

Runoff Coefficient: **Surface Type**

Soil Type: **B**

Urbanization: **Urban**

### Basin Land Use Characteristics

Surface	Area		Runoff Coefficient						% Imperv.
	(SF)	(Acres)	C2	C5	C10	C25	C50	C100	
Roofs	7,728	0.18	0.71	0.73	0.75	0.78	0.8	0.81	90%
Driveways & Walks	2,409	0.06	0.89	0.9	0.92	0.94	0.95	0.96	100%
Landscaping	37,250	0.86	0.03	0.09	0.17	0.26	0.31	0.36	2%
<b>Combined</b>	<b>47,387</b>	<b>1.09</b>	<b>0.18</b>	<b>0.24</b>	<b>0.30</b>	<b>0.38</b>	<b>0.42</b>	<b>0.46</b>	<b>21.3%</b>

### Basin Travel Time

	Sub-basin or Channel Type	Material Type	L (ft)	Elev. $\Delta Z_0$ (ft)	$Q_i$ (cfs)	Base or Dia (ft)	Sides z:1 (ft/ft)	v (ft/s)	t (min)
Furthest Reach	A13	-	414	5	-	-	-	-	12.3
Channelized-1									
Channelized-2									
Channelized-3									
Total			414	5					
								$t_c$ (min)	12.3

### Contributing Offsite Flows (Added to Runoff and Allowed Release, below.)

Contributing Basins/Areas

$Q_{Minor}$  (cfs) - 5-year Storm  
 $Q_{Major}$  (cfs) - 100-year Storm

### Rainfall Intensity & Runoff

	2-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr
Intensity (in/hr)	3.05	3.82	4.46	5.09	5.73	6.41
Site Runoff (cfs)	0.61	0.98	1.47	2.10	2.63	3.24
OffSite Runoff (cfs)	-	0.00	-	-	-	0.00
Release Rates (cfs/ac)	-	-	-	-	-	-
Allowed Release (cfs)	-	1.0	-	-	-	3.2

$$DCM: I = C1 * \ln(tc) + C2$$

C1: 1.19      1.5      1.75      2      2.25      2.52

C2: 6.035      7.583      8.847      10.111      11.375      12.735

### Notes

Runoff from Offsite basins have been assumed constant, despite additional times of concentration.

## Combined Sub-Basin Runoff Calculations (DP8)

Includes Basins DP7 A13

Job No.: **61093**

Date: **10/19/18 13:45**

Project: **Townhomes at Bradley Crossroads**

Calcs by: **TJW**

Jurisdiction: **DCM**

Checked by:

Runoff Coefficient: **Surface Type**

Soil Type: **B**

Urbanization: **Urban**

### Basin Land Use Characteristics

Surface	Area		Runoff Coefficient						% Imperv.
	(SF)	(Acres)	C2	C5	C10	C25	C50	C100	
Roofs	75,348	1.73	0.71	0.73	0.75	0.78	0.8	0.81	90%
Driveways & Walks	133,425	3.06	0.89	0.9	0.92	0.94	0.95	0.96	100%
Landscaping	90,272	2.07	0.03	0.09	0.17	0.26	0.31	0.36	2%
<b>Combined</b>	<b>299,045</b>	<b>6.87</b>	<b>0.59</b>	<b>0.61</b>	<b>0.65</b>	<b>0.69</b>	<b>0.72</b>	<b>0.74</b>	<b>67.9%</b>

### Basin Travel Time

	Sub-basin or Channel Type	Material Type	L (ft)	Elev. $\Delta Z_0$ (ft)	$Q_i$ (cfs)	Base or Dia (ft)	Sides z:1 (ft/ft)	v (ft/s)	t (min)
Furthest Reach	DP7	-	1,011	11	-	-	-	-	9.8
Channelized-1	Pipe	RCP	55	1	32	2	0	8.4	0.1
Channelized-2									
Channelized-3									
Total			1,066	12					
								$t_c$ (min)	9.9

### Contributing Offsite Flows (Added to Runoff and Allowed Release, below.)

Contributing Basins/Areas

$Q_{Minor}$  (cfs) - 5-year Storm  
 $Q_{Major}$  (cfs) - 100-year Storm

### Rainfall Intensity & Runoff

	2-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr
Intensity (in/hr)	3.30	4.14	4.83	5.52	6.21	6.95
Site Runoff (cfs)	13.26	17.40	21.57	26.30	30.64	35.34
OffSite Runoff (cfs)	-	0.00	-	-	-	0.00
Release Rates (cfs/ac)	-	-	-	-	-	-
Allowed Release (cfs)	-	17.4	-	-	-	35.3

$$DCM: I = C1 * \ln(tc) + C2$$

C1: 1.19      1.5      1.75      2      2.25      2.52

C2: 6.035      7.583      8.847      10.111      11.375      12.735

### Notes

Runoff from Offsite basins have been assumed constant, despite additional times of concentration.

### **3 Hydraulic Calculations**

Inlet Calculations

Storm Drain Pipe and Culvert Calculations

Channel Calculations

# ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

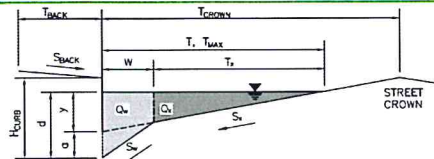
(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project:

61093 - The Townhomes at Bradley Crossroads

Inlet ID:

OS-1

**Gutter Geometry (Enter data in the blue cells)**

Maximum Allowable Width for Spread Behind Curb

Side Slope Behind Curb (leave blank for no conveyance credit behind curb)

Manning's Roughness Behind Curb (typically between 0.012 and 0.020)

Height of Curb at Gutter Flow Line

Distance from Curb Face to Street Crown

Gutter Width

Street Transverse Slope

Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)

Street Longitudinal Slope - Enter 0 for sump condition

Manning's Roughness for Street Section (typically between 0.012 and 0.020)

Max. Allowable Spread for Minor &amp; Major Storm

Max. Allowable Depth at Gutter Flowline for Minor &amp; Major Storm

Check boxes are not applicable in SUMP conditions

MINOR STORM Allowable Capacity is based on Depth Criterion

MAJOR STORM Allowable Capacity is based on Depth Criterion

$T_{BACK} = 10.0$  ft  
 $S_{BACK} = 0.020$  ft/ft  
 $n_{BACK} = 0.020$

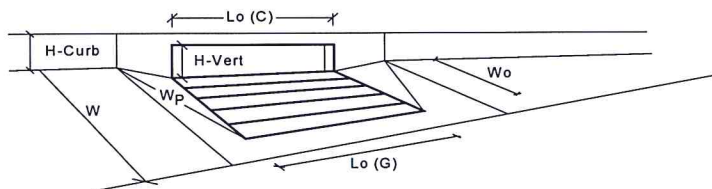
$H_{CURB} = 6.00$  inches  
 $T_{CROWN} = 14.0$  ft  
 $W = 4.00$  ft  
 $S_x = 0.040$  ft/ft  
 $S_w = 0.083$  ft/ft  
 $S_o = 0.000$  ft/ft  
 $n_{STREET} = 0.013$

	Minor Storm	Major Storm	
$T_{MAX} =$	6.0	14.0	ft
$d_{MAX} =$	6.0	6.0	inches

	Minor Storm	Major Storm	
$Q_{allow} =$	SUMP	SUMP	cfs

# INLET IN A SUMP OR SAG LOCATION

Version 4.05 Released March 2017



Design Information (Input)		CDOT Type C Grate	
Type of Inlet		CDOT Type C Grate	
Local Depression (additional to continuous gutter depression 'a' from above)			
Number of Unit Inlets (Grate or Curb Opening)			
Water Depth at Flowline (outside of local depression)			
<b>Grate Information</b>			
Length of a Unit Grate			
Width of a Unit Grate			
Area Opening Ratio for a Grate (typical values 0.15-0.90)			
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)			
Grate Weir Coefficient (typical value 2.15 - 3.60)			
Grate Orifice Coefficient (typical value 0.60 - 0.80)			
<b>Curb Opening Information</b>			
Length of a Unit Curb Opening			
Height of Vertical Curb Opening in Inches			
Height of Curb Orifice Throat in Inches			
Angle of Throat (see USDCM Figure ST-5)			
Side Width for Depression Pan (typically the gutter width of 2 feet)			
Clogging Factor for a Single Curb Opening (typical value 0.10)			
Curb Opening Weir Coefficient (typical value 2.3-3.7)			
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)			
<b>Low Head Performance Reduction (Calculated)</b>			
Depth for Grate Midwidth			
Depth for Curb Opening Weir Equation			
Combination Inlet Performance Reduction Factor for Long Inlets			
Curb Opening Performance Reduction Factor for Long Inlets			
Grated Inlet Performance Reduction Factor for Long Inlets			
<b>Total Inlet Interception Capacity (assumes clogged condition)</b>			
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)			

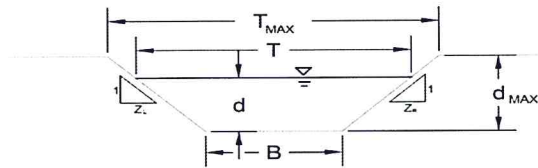
  

	MINOR	MAJOR	
Type =	CDOT Type C Grate		
$\theta_{local}$ =	0.00	0.00	inches
No =	1	1	
Ponding Depth =	4.9	6.0	inches
	MINOR	MAJOR	Override Depths
$L_o$ (G) =	2.92	2.92	feet
$W_o$ =	2.92	2.92	feet
$A_{ratio}$ =	0.70	0.70	
$C_r$ (G) =	0.50	0.50	
$C_w$ (G) =	2.41	2.41	
$C_o$ (G) =	0.67	0.67	
	MINOR	MAJOR	
$L_o$ (C) =	N/A	N/A	feet
$H_{vert}$ =	N/A	N/A	inches
$H_{throat}$ =	N/A	N/A	inches
Theta =	N/A	N/A	degrees
$W_p$ =	N/A	N/A	feet
$C_r$ (C) =	N/A	N/A	
$C_w$ (C) =	N/A	N/A	
$C_o$ (C) =	N/A	N/A	
	MINOR	MAJOR	
$d_{Grate}$ =	0.291	0.379	ft
$d_{Curb}$ =	N/A	N/A	ft
RF <sub>Combination</sub> =	N/A	N/A	
RF <sub>Curb</sub> =	N/A	N/A	
RF <sub>Grate</sub> =	0.78	0.95	
	MINOR	MAJOR	
$Q_a$ =	1.1	2.0	cfs
Q PEAK REQUIRED =	0.8	1.4	cfs

## AREA INLET IN A SWALE

61093 - The Townhomes at Bradley Crossroads

DP8 Area Inlet



This worksheet uses the NRCS  
vegetal retardance method to  
determine Manning's n.

For more information see  
Section 7.2.3 of the USDCM.

## Analysis of Trapezoidal Grass-Lined Channel Using SCS Method

NRCS Vegetal Retardance (A, B, C, D, or E)

Manning's n (Leave cell D16 blank to manually enter an n value)

Channel Invert Slope

Bottom Width

Left Side Slope

Right Side Slope

Check one of the following soil types:

Soil Type	Max. Velocity ( $V_{MAX}$ )	Max Froude No. ( $F_{MAX}$ )
Non-Cohesive	5.0 fps	0.60
Cohesive	7.0 fps	0.80
Paved	N/A	N/A

Max. Allowable Top Width of Channel for Minor &amp; Major Storm

Max. Allowable Water Depth in Channel for Minor &amp; Major Storm

A, B, C, D or E

C
n = see details below
$S_o = 0.0200$ ft/ft
B = 10.00 ft
Z1 = 50.00 ft/ft
Z2 = 4.00 ft/ft

Choose One:

☒ Non-Cohesive☐ Cohesive☐ Paved

	Minor Storm	Major Storm	
$T_{MAX} =$	40.00	50.00	feet
$d_{MAX} =$	0.50	1.00	feet

## Allowable Channel Capacity Based On Channel Geometry

MINOR STORM Allowable Capacity is based on Depth Criterion

MAJOR STORM Allowable Capacity is based on Top Width Criterion

	Minor Storm	Major Storm	
$Q_{allow} =$	2.7	12.7	cfs
$d_{allow} =$	0.50	0.74	ft

## Water Depth in Channel Based On Design Peak Flow

Design Peak Flow

Water Depth

	Minor Storm	Major Storm	
$Q_o =$	1.0	3.2	cfs
d =	0.31	0.54	feet

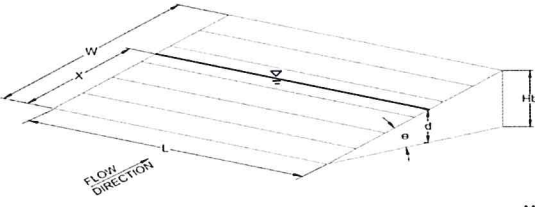
Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

## AREA INLET IN A SWALE

61093 - The Townhomes at Bradley Crossroads

DP8 Area Inlet

Inlet Design Information (Input)							
Type of Inlet	User-Defined						
Inlet Type =	User-Defined						
Angle of Inclined Grate (must be <= 30 degrees)	$\theta = 0.00$ degrees						
Width of Grate	$W = 3.00$ feet						
Length of Grate	$L = 10.00$ feet						
Open Area Ratio	$A_{\text{RATIO}} = 0.70$						
Height of Inclined Grate	$H_B = 0.00$ feet						
Clogging Factor	$C_f = 0.50$						
Grate Discharge Coefficient	$C_d = \text{N/A}$						
Orifice Coefficient	$C_o = 0.64$						
Weir Coefficient	$C_w = 2.05$						
							
Water Depth at Inlet (for depressed inlets, 1 foot is added for depression)	<table border="1"> <thead> <tr> <th></th> <th>MINOR</th> <th>MAJOR</th> </tr> </thead> <tbody> <tr> <td><math>d =</math></td> <td>0.31</td> <td>0.54</td> </tr> </tbody> </table>		MINOR	MAJOR	$d =$	0.31	0.54
	MINOR	MAJOR					
$d =$	0.31	0.54					
Total Inlet Interception Capacity (assumes clogged condition)	<table border="1"> <thead> <tr> <th></th> <th>MINOR</th> <th>MAJOR</th> </tr> </thead> <tbody> <tr> <td><math>Q_a =</math></td> <td>7.5</td> <td>17.4</td> </tr> </tbody> </table>		MINOR	MAJOR	$Q_a =$	7.5	17.4
	MINOR	MAJOR					
$Q_a =$	7.5	17.4					
Bypassed Flow, $Q_b =$	<table border="1"> <thead> <tr> <th></th> <th>MINOR</th> <th>MAJOR</th> </tr> </thead> <tbody> <tr> <td>0.0</td> <td>0.0</td> <td>0.0</td> </tr> </tbody> </table>		MINOR	MAJOR	0.0	0.0	0.0
	MINOR	MAJOR					
0.0	0.0	0.0					
Capture Percentage = $Q_a/Q_o = C\%$	<table border="1"> <thead> <tr> <th></th> <th>MINOR</th> <th>MAJOR</th> </tr> </thead> <tbody> <tr> <td>100</td> <td>100</td> <td>100</td> </tr> </tbody> </table>		MINOR	MAJOR	100	100	100
	MINOR	MAJOR					
100	100	100					

# Channel Report

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Friday, Oct 19 2018

## North Curb flowing to DP1 (14.1 cfs)

### Gutter

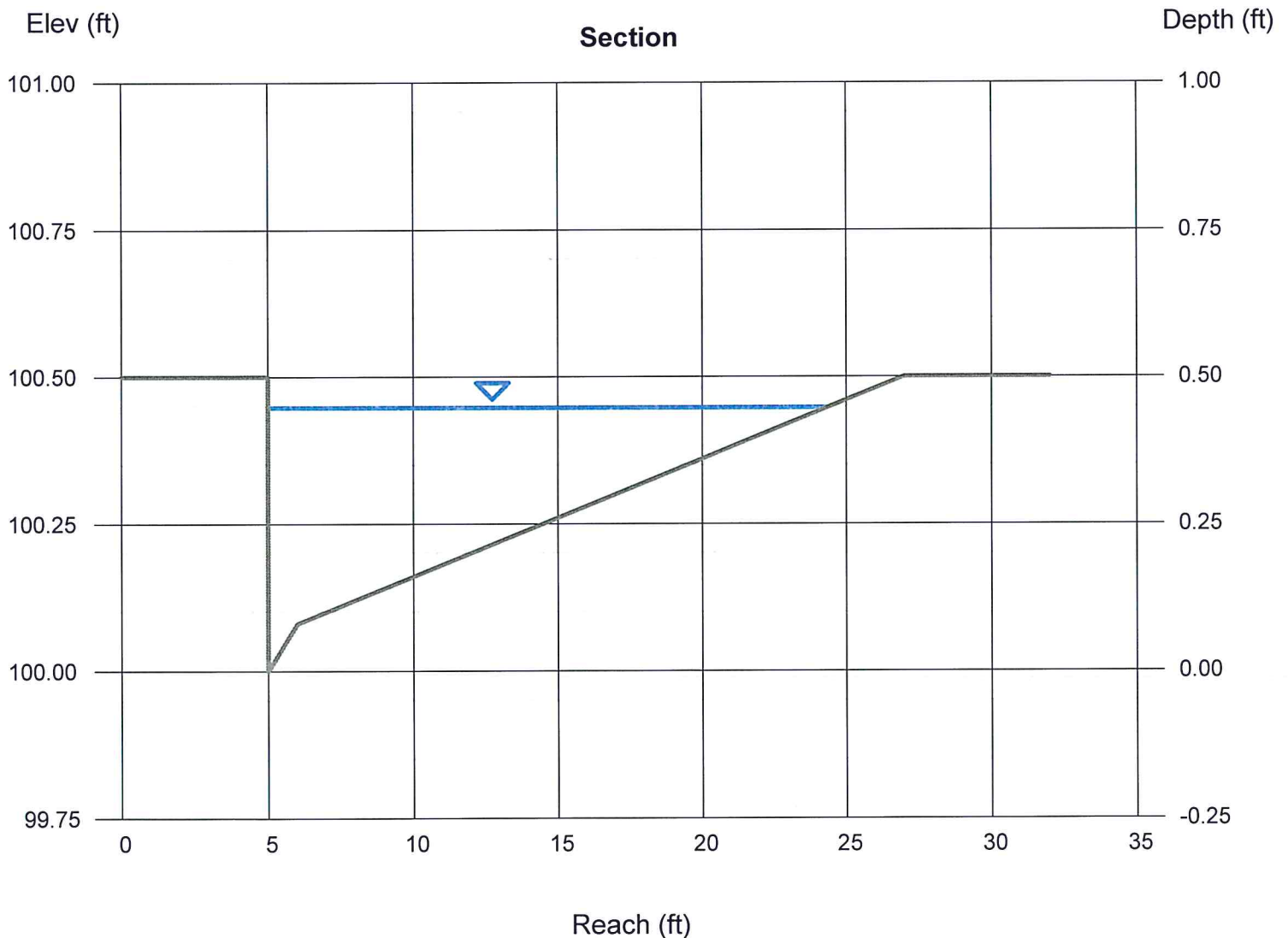
Cross Sl, Sx (ft/ft) = 0.020  
Cross Sl, Sw (ft/ft) = 0.080  
Gutter Width (ft) = 1.00  
Invert Elev (ft) = 100.00  
Slope (%) = 1.00  
N-Value = 0.016

### Calculations

Compute by: Known Q  
Known Q (cfs) = 14.10

### Highlighted

Depth (ft) = 0.45  
Q (cfs) = 14.10  
Area (sqft) = 3.77  
Velocity (ft/s) = 3.74  
Wetted Perim (ft) = 19.80  
Crit Depth, Yc (ft) = 0.52  
Spread Width (ft) = 19.35  
EGL (ft) = 0.66



# Channel Report

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Friday, Oct 19 2018

## DP1 - Concrete Pan 100 YR Flow (17.9 cfs)

### Trapezoidal

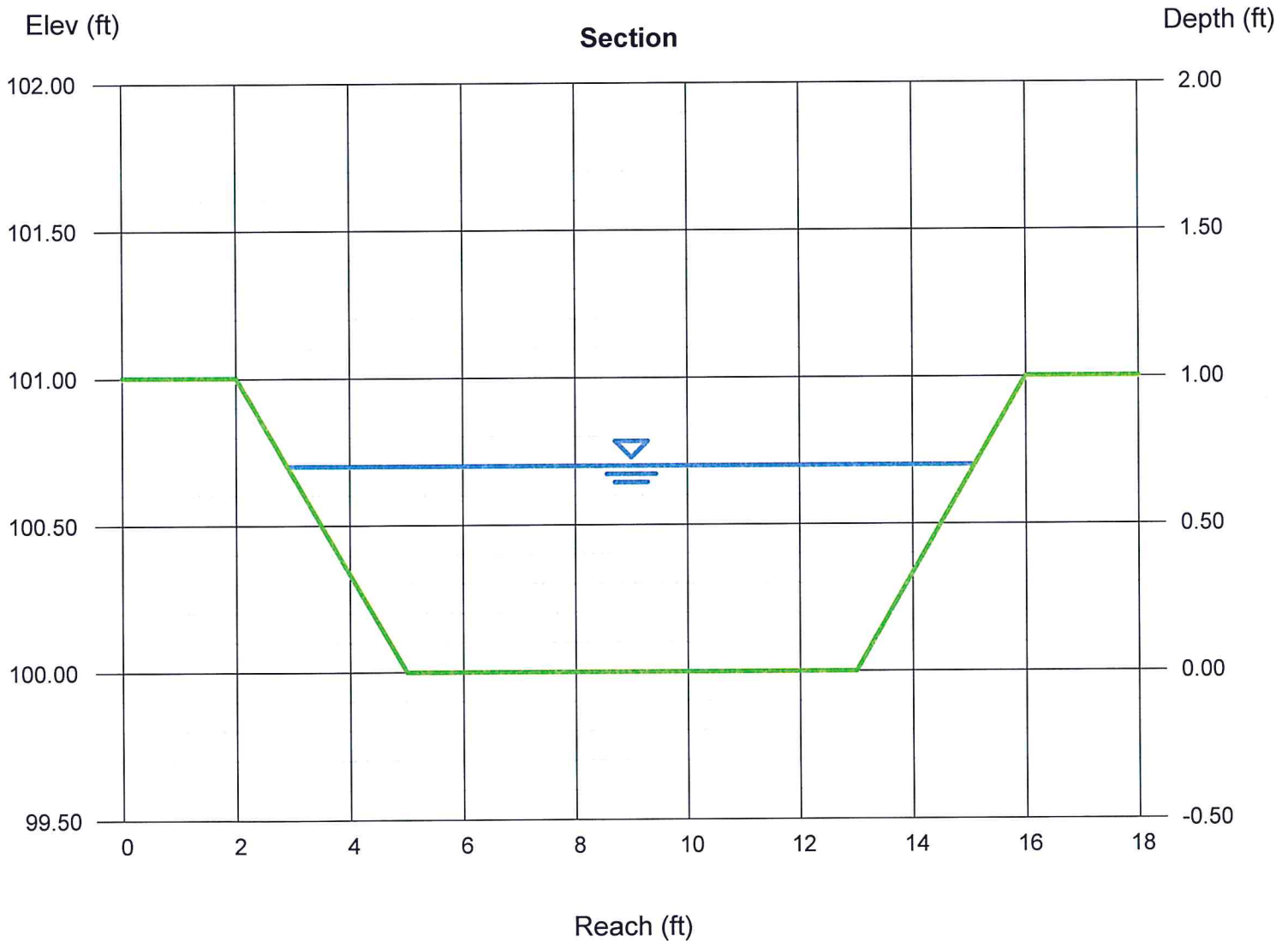
Bottom Width (ft) = 8.00  
Side Slopes (z:1) = 3.00, 3.00  
Total Depth (ft) = 1.00  
Invert Elev (ft) = 100.00  
Slope (%) = 1.00  
N-Value = 0.040

### Calculations

Compute by: Known Q  
Known Q (cfs) = 17.90

### Highlighted

Depth (ft) = 0.70  
Q (cfs) = 17.90  
Area (sqft) = 7.07  
Velocity (ft/s) = 2.53  
Wetted Perim (ft) = 12.43  
Crit Depth, Yc (ft) = 0.51  
Top Width (ft) = 12.20  
EGL (ft) = 0.80



# Channel Report

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Thursday, Feb 14 2019

## DP2 Alley V-Channel 100 YR Flow (4.2 cfs)

### Triangular

Side Slopes (z:1) = 20.00, 20.00  
Total Depth (ft) = 0.50

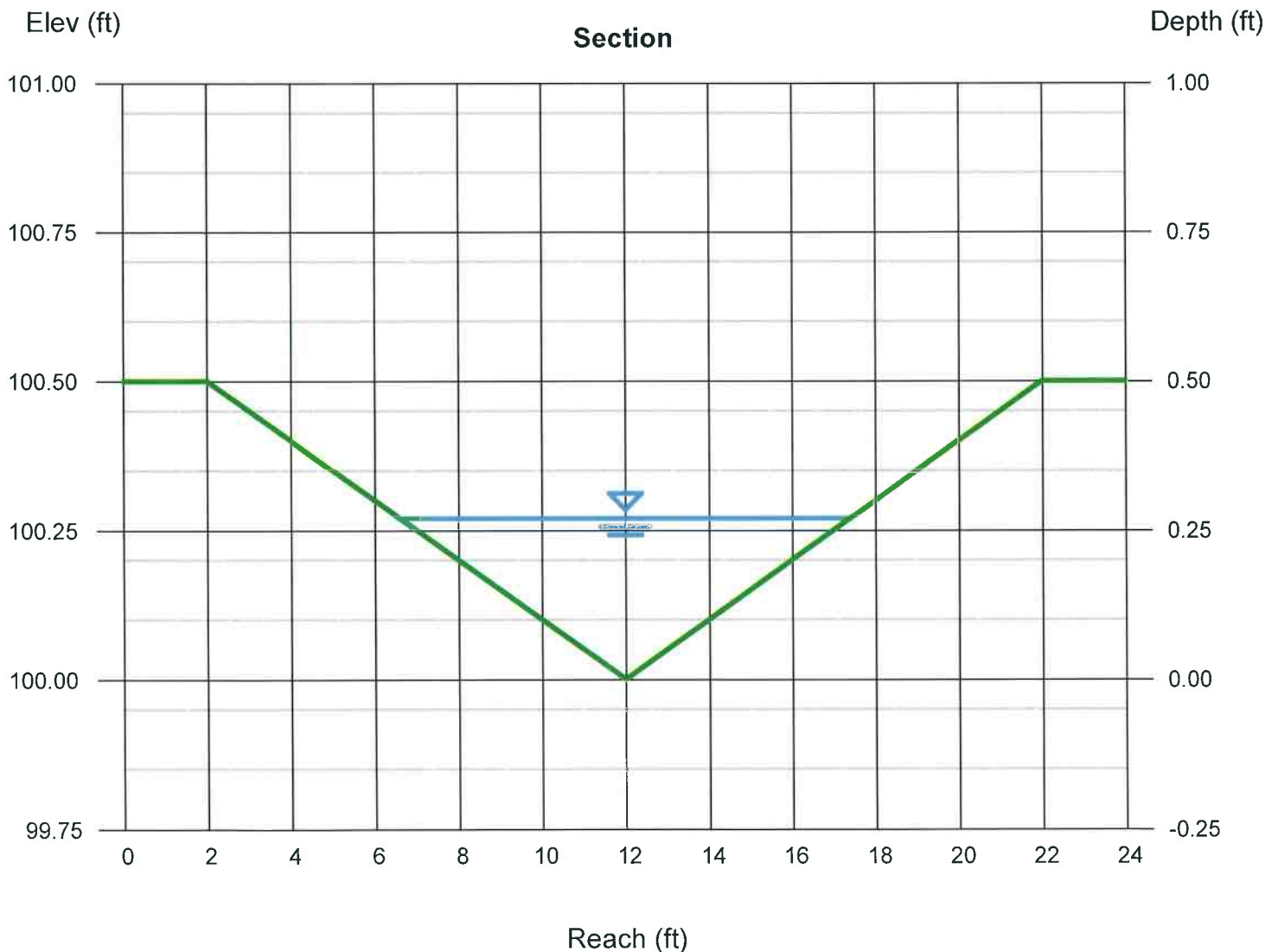
Invert Elev (ft) = 100.00  
Slope (%) = 0.80  
N-Value = 0.011

### Calculations

Compute by: Known Q  
Known Q (cfs) = 4.20

### Highlighted

Depth (ft) = 0.27  
Q (cfs) = 4.200  
Area (sqft) = 1.46  
Velocity (ft/s) = 2.88  
Wetted Perim (ft) = 10.81  
Crit Depth, Yc (ft) = 0.31  
Top Width (ft) = 10.80  
EGL (ft) = 0.40



# Channel Report

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Friday, Oct 19 2018

## DP2 Alley Curb Opening 100 YR Flow (4.2 cfs)

### Trapezoidal

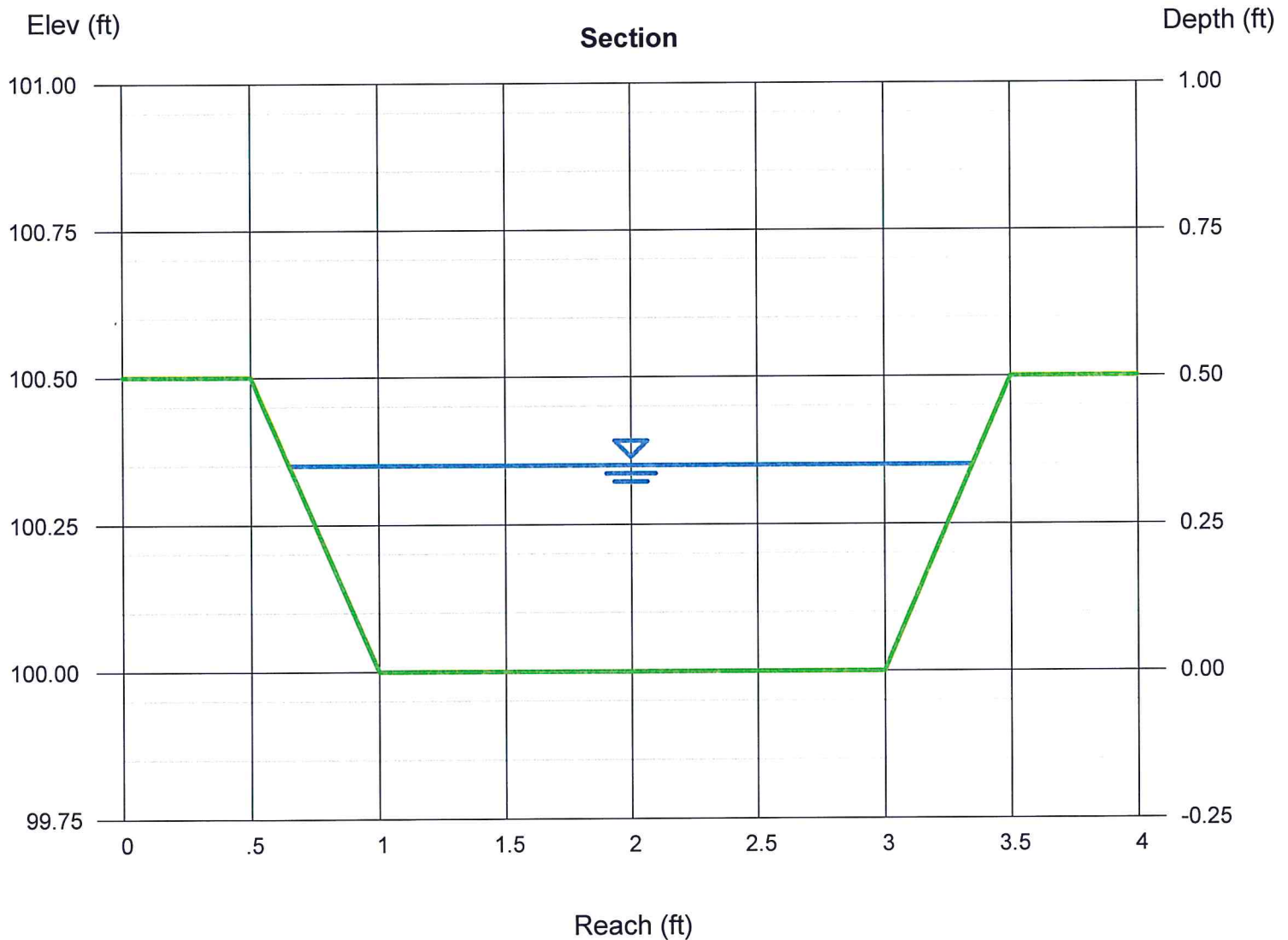
Bottom Width (ft) = 2.00  
Side Slopes (z:1) = 1.00, 1.00  
Total Depth (ft) = 0.50  
Invert Elev (ft) = 100.00  
Slope (%) = 0.80  
N-Value = 0.011

### Calculations

Compute by: Known Q  
Known Q (cfs) = 4.20

### Highlighted

Depth (ft) = 0.35  
Q (cfs) = 4.200  
Area (sqft) = 0.82  
Velocity (ft/s) = 5.11  
Wetted Perim (ft) = 2.99  
Crit Depth, Yc (ft) = 0.48  
Top Width (ft) = 2.70  
EGL (ft) = 0.76



# Channel Report

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Friday, Oct 19 2018

## Basin A3 Trapezoidal Ditch 100 YR Flow (17.9 cfs)

### Trapezoidal

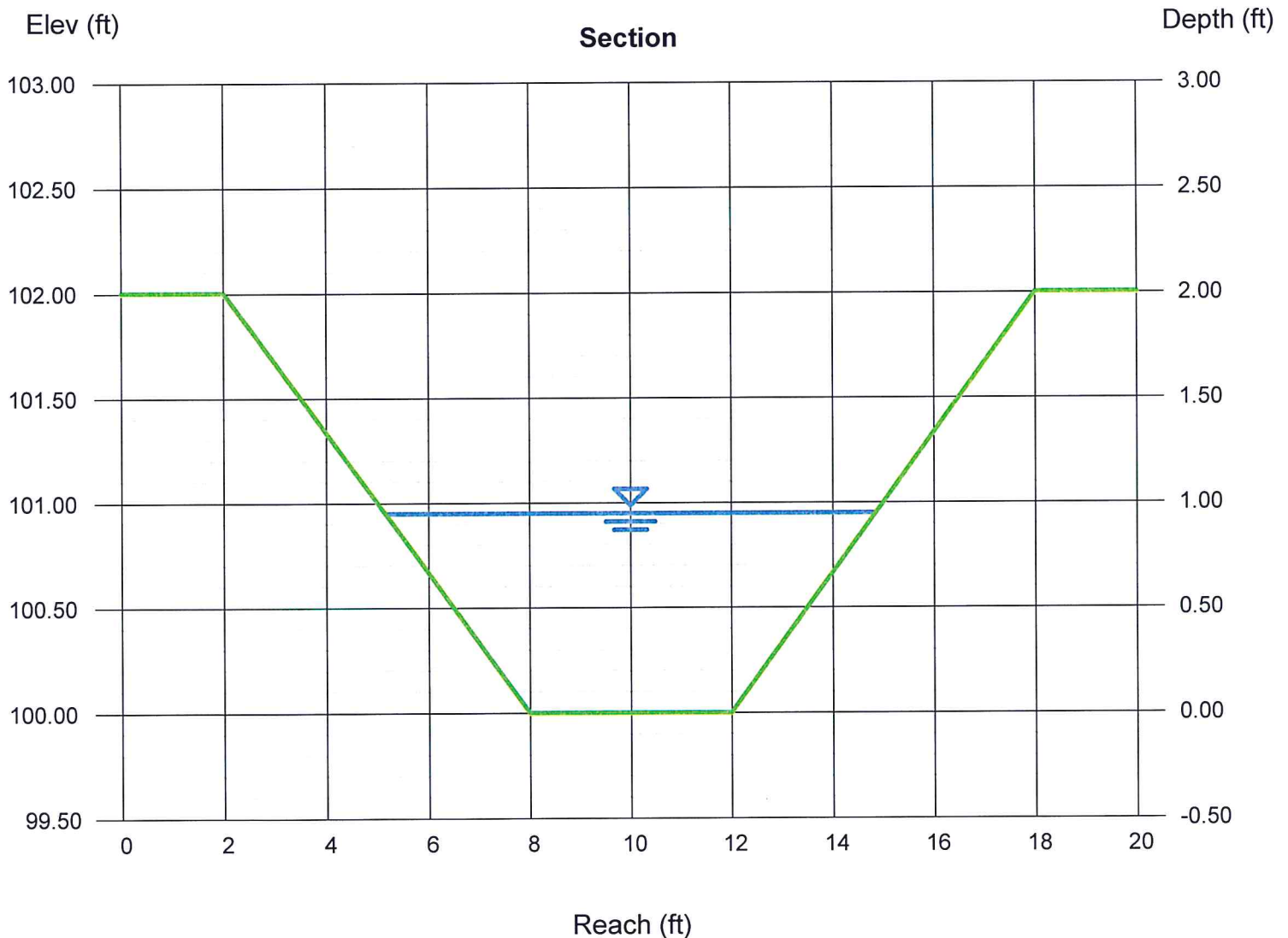
Bottom Width (ft) = 4.00  
Side Slopes (z:1) = 3.00, 3.00  
Total Depth (ft) = 2.00  
Invert Elev (ft) = 100.00  
Slope (%) = 1.00  
N-Value = 0.040

### Highlighted

Depth (ft) = 0.95  
Q (cfs) = 17.90  
Area (sqft) = 6.51  
Velocity (ft/s) = 2.75  
Wetted Perim (ft) = 10.01  
Crit Depth, Yc (ft) = 0.71  
Top Width (ft) = 9.70  
EGL (ft) = 1.07

### Calculations

Compute by: Known Q  
Known Q (cfs) = 17.90



# Channel Report

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Thursday, Feb 14 2019

## DP4 Cold Harbor V-Channel 100 YR Flow (6.9 cfs)

### Triangular

Side Slopes (z:1) = 28.00, 28.00

Total Depth (ft) = 0.80

Invert Elev (ft) = 100.00

Slope (%) = 0.80

N-Value = 0.011

### Calculations

Compute by: Known Q

Known Q (cfs) = 6.90

### Highlighted

Depth (ft) = 0.28

Q (cfs) = 6.900

Area (sqft) = 2.20

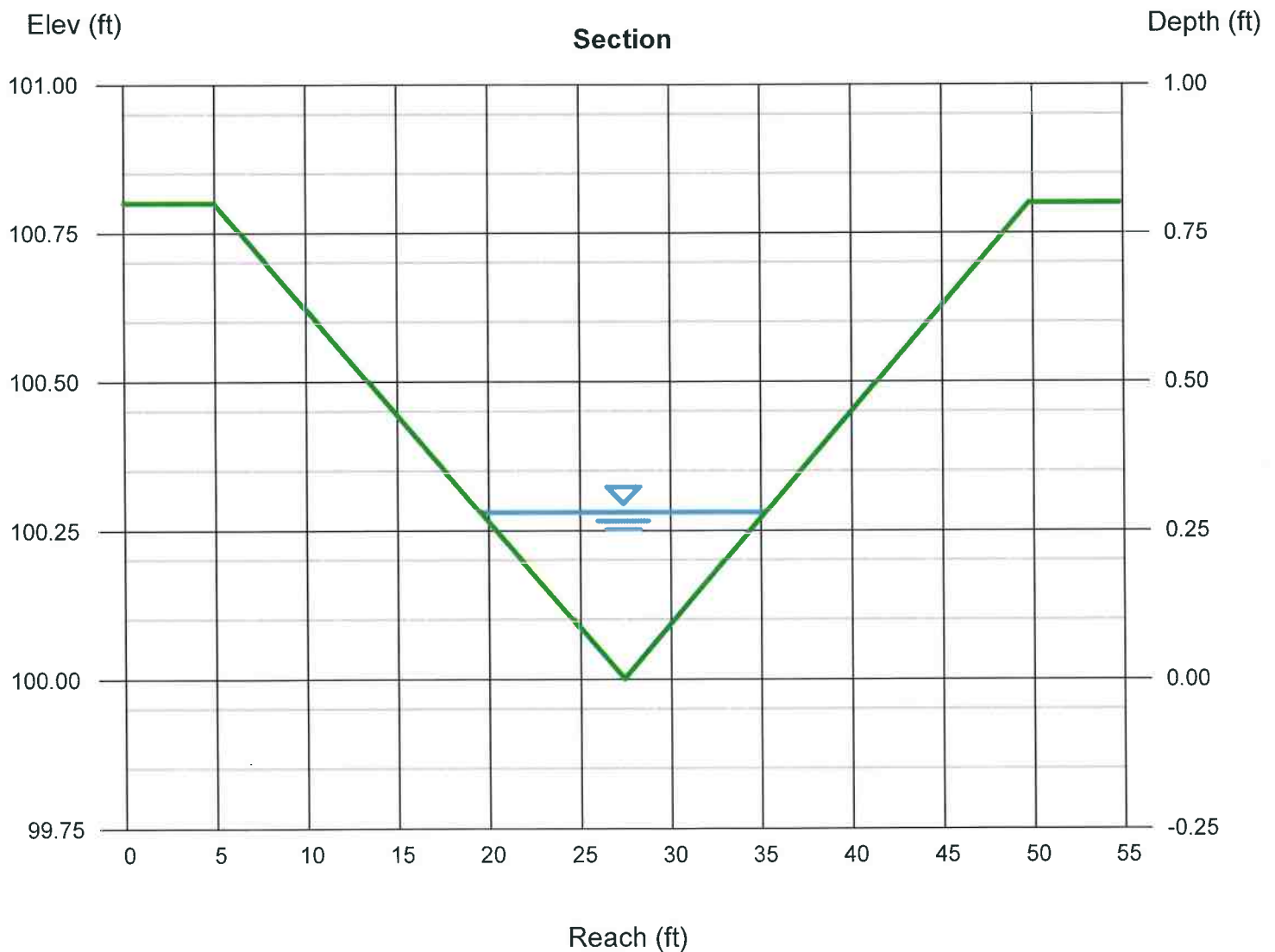
Velocity (ft/s) = 3.14

Wetted Perim (ft) = 15.69

Crit Depth, Yc (ft) = 0.33

Top Width (ft) = 15.68

EGL (ft) = 0.43



# Channel Report

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Friday, Oct 19 2018

## DP3 - Texas Crossing 100 YR Flow (17.9 cfs)

### Trapezoidal

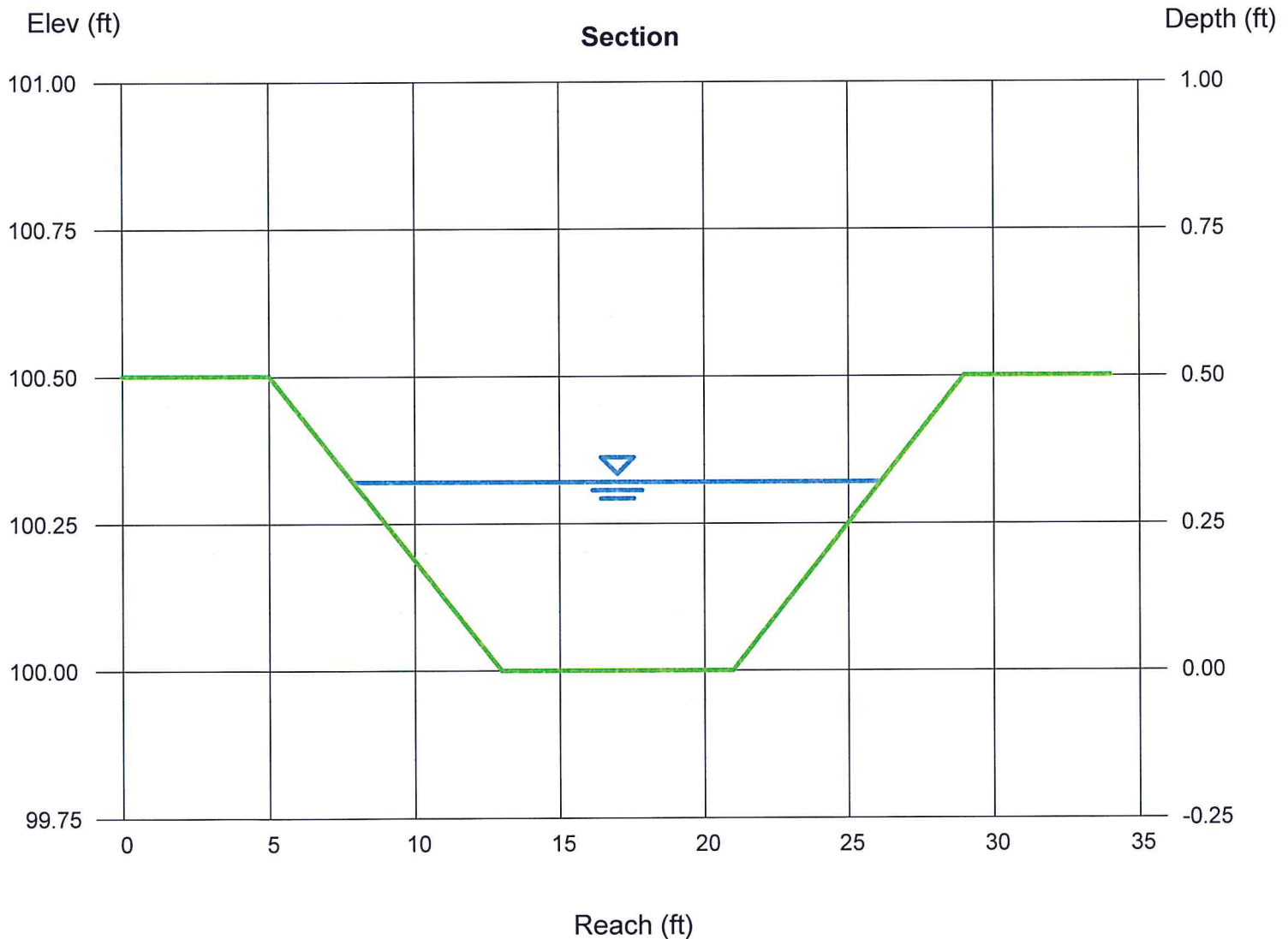
Bottom Width (ft) = 8.00  
Side Slopes (z:1) = 16.00, 16.00  
Total Depth (ft) = 0.50  
Invert Elev (ft) = 100.00  
Slope (%) = 1.00  
N-Value = 0.013

### Calculations

Compute by: Known Q  
Known Q (cfs) = 17.90

### Highlighted

Depth (ft) = 0.32  
Q (cfs) = 17.90  
Area (sqft) = 4.20  
Velocity (ft/s) = 4.26  
Wetted Perim (ft) = 18.26  
Crit Depth, Yc (ft) = 0.41  
Top Width (ft) = 18.24  
EGL (ft) = 0.60



# Culvert Report

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Friday, Oct 19 2018

## DP3 culvert entrance

Invert Elev Dn (ft)	=	39.13
Pipe Length (ft)	=	45.00
Slope (%)	=	1.02
Invert Elev Up (ft)	=	39.59
Rise (in)	=	12.0
Shape	=	Circular
Span (in)	=	12.0
No. Barrels	=	3
n-Value	=	0.013
Culvert Type	=	Circular Concrete
Culvert Entrance	=	Square edge w/headwall (C)
Coeff. K,M,c,Y,k	=	0.0098, 2, 0.0398, 0.67, 0.5

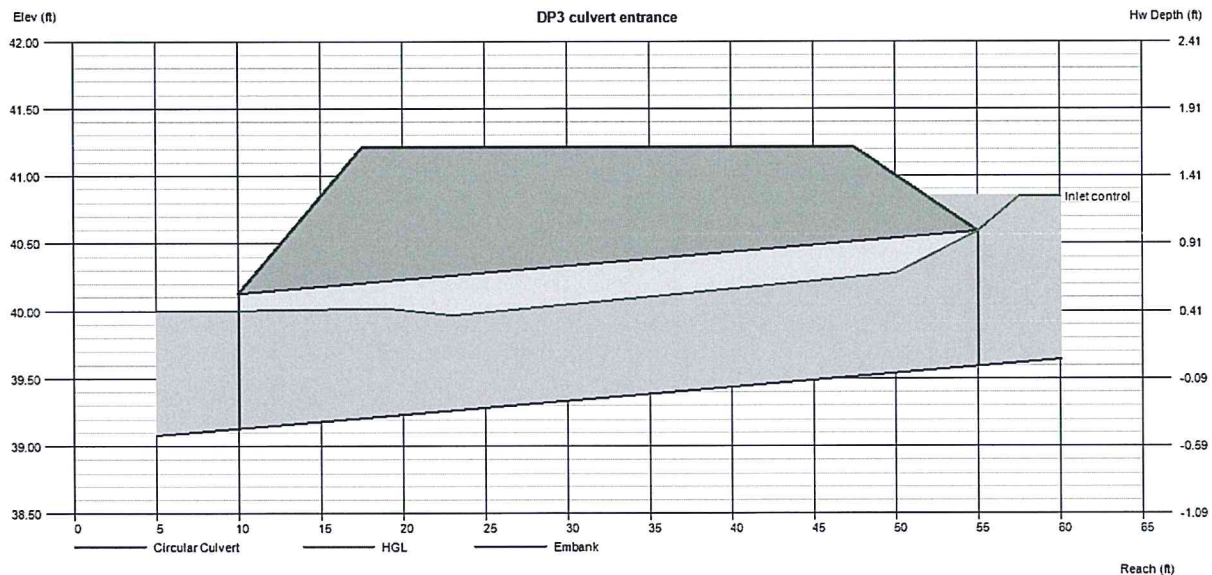
<b>Embankment</b>	
Top Elevation (ft)	= 41.21
Top Width (ft)	= 30.00
Crest Width (ft)	= 30.00

### Calculations

Qmin (cfs)	=	9.10
Qmax (cfs)	=	18.10
Tailwater Elev (ft)	=	(dc+D)/2

### Highlighted

Qtotal (cfs)	=	9.10
Qpipe (cfs)	=	9.10
Qovertop (cfs)	=	0.00
Veloc Dn (ft/s)	=	4.17
Veloc Up (ft/s)	=	4.83
HGL Dn (ft)	=	40.00
HGL Up (ft)	=	40.34
Hw Elev (ft)	=	40.85
Hw/D (ft)	=	1.26
Flow Regime	=	Inlet Control



# Channel Report

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Thursday, Feb 14 2019

## DP5 Alley V-Channel 100 YR Flow (4.2 cfs)

### Triangular

Side Slopes (z:1) = 20.00, 20.00

Total Depth (ft) = 0.50

Invert Elev (ft) = 100.00

Slope (%) = 0.80

N-Value = 0.011

### Calculations

Compute by: Known Q

Known Q (cfs) = 4.20

### Highlighted

Depth (ft) = 0.27

Q (cfs) = 4.200

Area (sqft) = 1.46

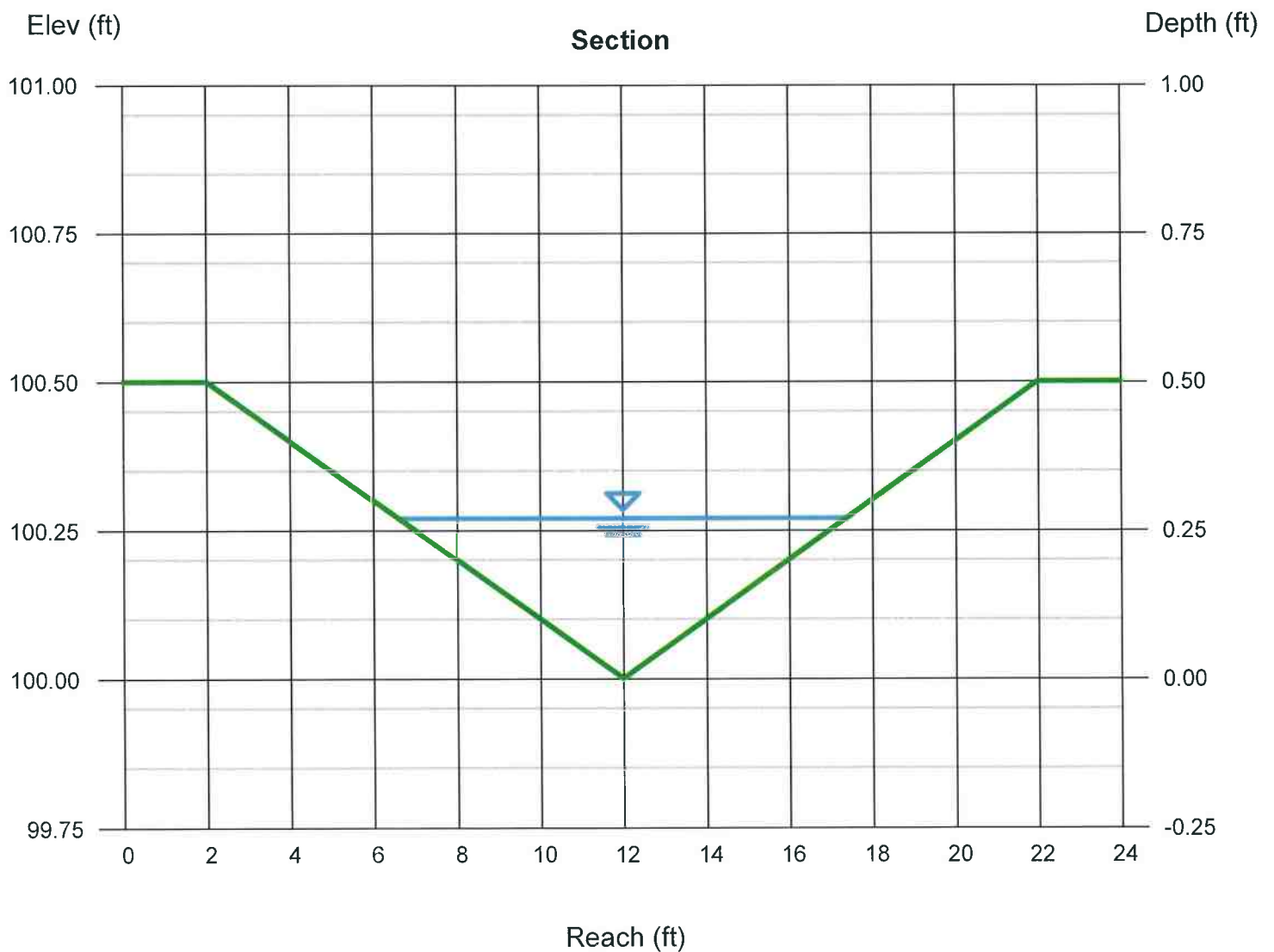
Velocity (ft/s) = 2.88

Wetted Perim (ft) = 10.81

Crit Depth, Yc (ft) = 0.31

Top Width (ft) = 10.80

EGL (ft) = 0.40



# Channel Report

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Friday, Oct 19 2018

## DP5 Alley Curb Opening 100 YR Flow (4.2 cfs)

### Trapezoidal

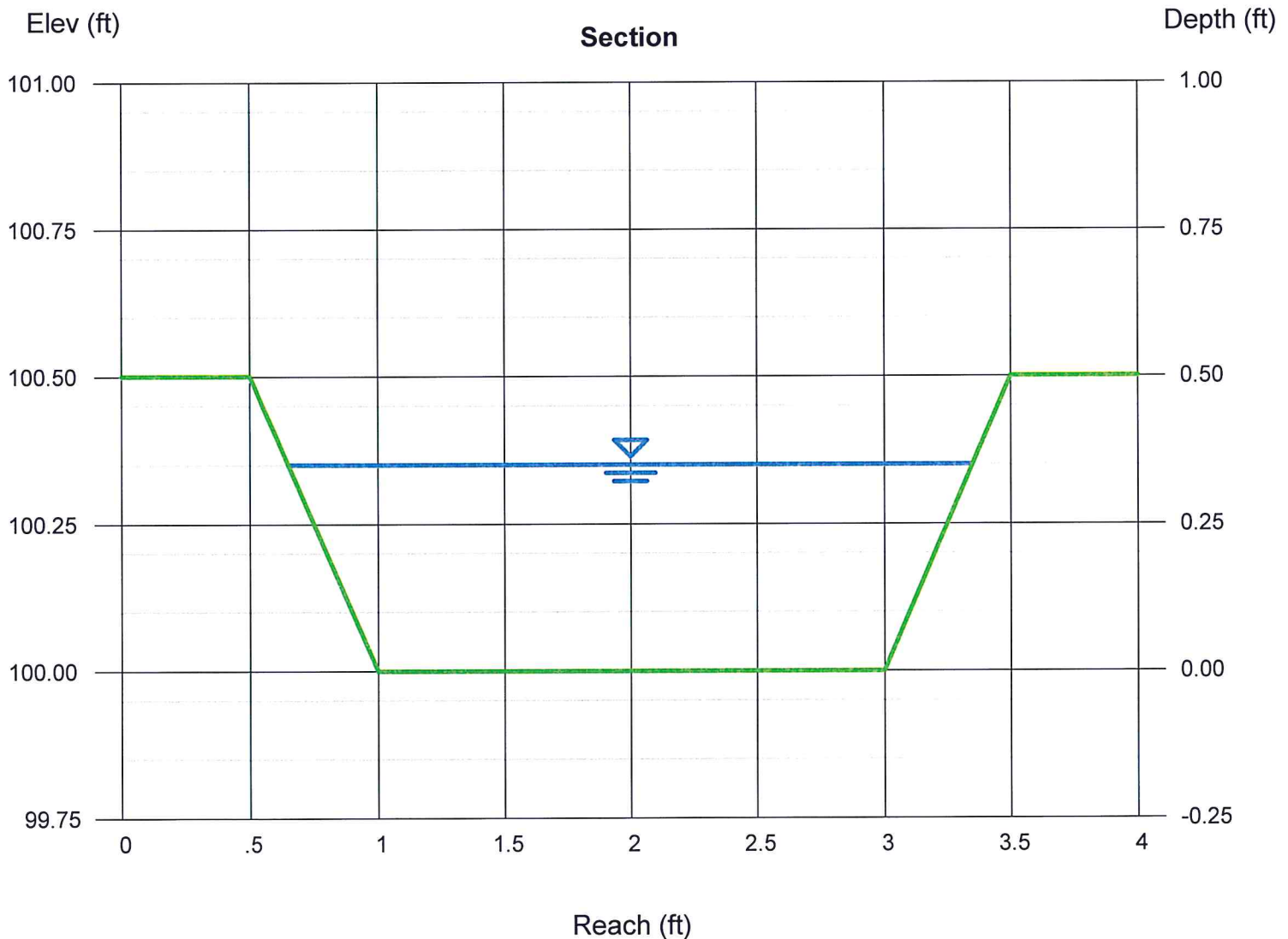
Bottom Width (ft) = 2.00  
Side Slopes (z:1) = 1.00, 1.00  
Total Depth (ft) = 0.50  
Invert Elev (ft) = 100.00  
Slope (%) = 0.80  
N-Value = 0.011

### Calculations

Compute by: Known Q  
Known Q (cfs) = 4.20

### Highlighted

Depth (ft) = 0.35  
Q (cfs) = 4.200  
Area (sqft) = 0.82  
Velocity (ft/s) = 5.11  
Wetted Perim (ft) = 2.99  
Crit Depth, Yc (ft) = 0.48  
Top Width (ft) = 2.70  
EGL (ft) = 0.76



# Channel Report

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Thursday, Feb 14 2019

## DP6 Alley V-Channel 100 YR Flow (6.1 cfs)

### Triangular

Side Slopes (z:1) = 20.00, 20.00

Total Depth (ft) = 0.50

Invert Elev (ft) = 100.00

Slope (%) = 0.80

N-Value = 0.011

### Calculations

Compute by: Known Q

Known Q (cfs) = 6.10

### Highlighted

Depth (ft) = 0.30

Q (cfs) = 6.100

Area (sqft) = 1.80

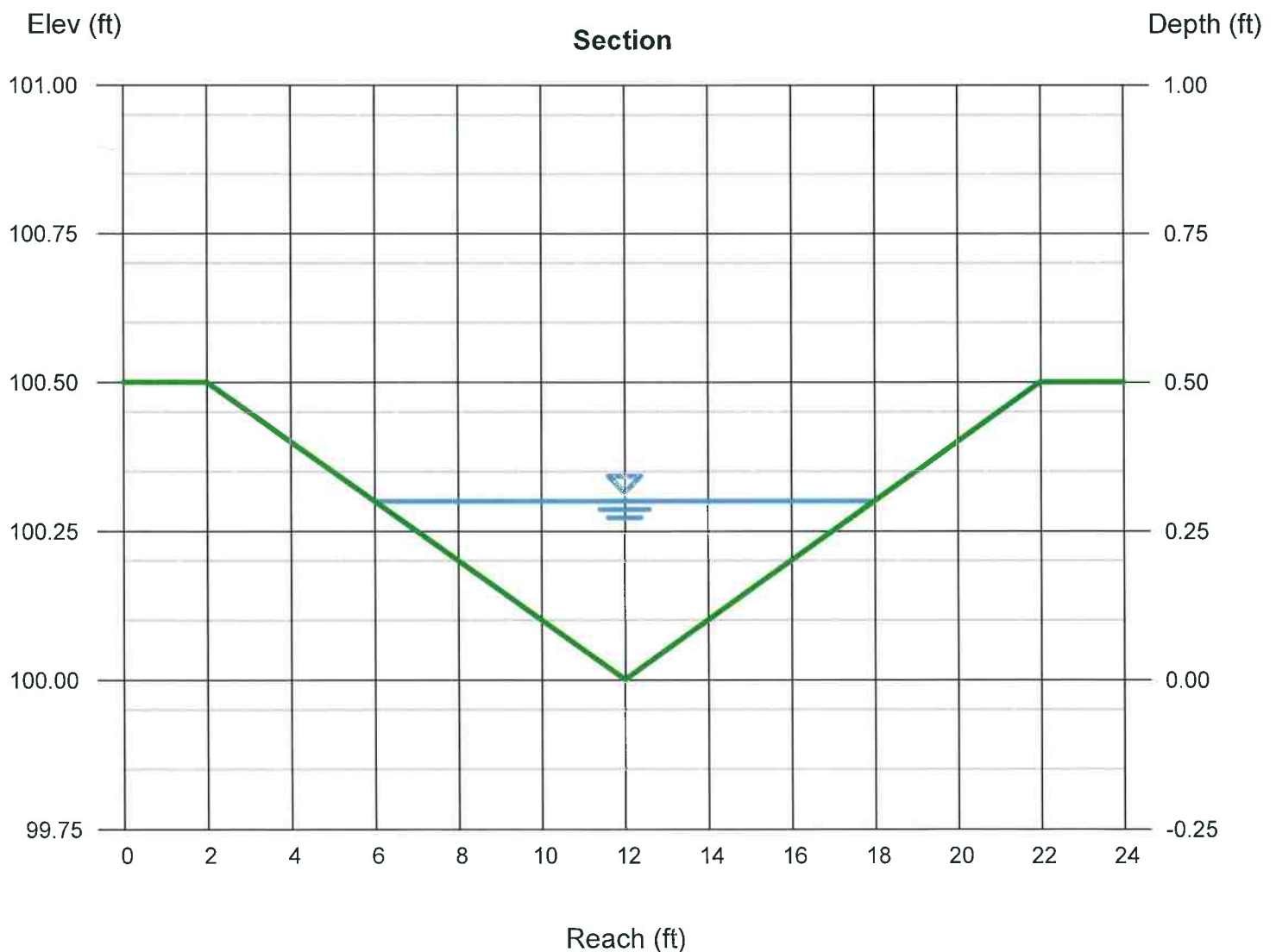
Velocity (ft/s) = 3.39

Wetted Perim (ft) = 12.01

Crit Depth, Yc (ft) = 0.36

Top Width (ft) = 12.00

EGL (ft) = 0.48



# Channel Report

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Friday, Oct 19 2018

## DP6 Alley Curb Opening 100 YR Flow (4.2 cfs)

### Trapezoidal

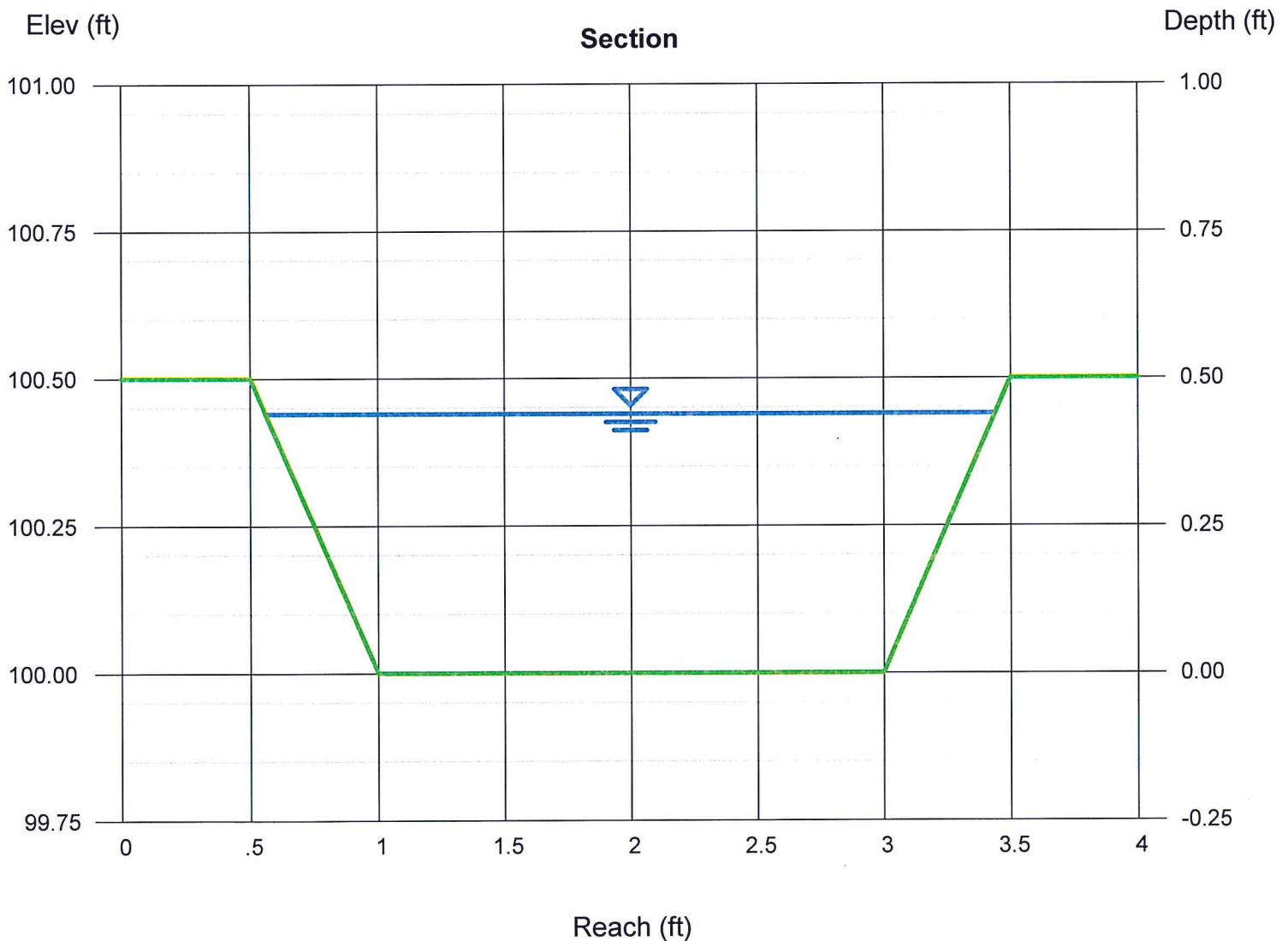
Bottom Width (ft) = 2.00  
Side Slopes (z:1) = 1.00, 1.00  
Total Depth (ft) = 0.50  
Invert Elev (ft) = 100.00  
Slope (%) = 0.80  
N-Value = 0.011

### Highlighted

Depth (ft) = 0.44  
Q (cfs) = 6.100  
Area (sqft) = 1.07  
Velocity (ft/s) = 5.68  
Wetted Perim (ft) = 3.24  
Crit Depth, Yc (ft) = 0.50  
Top Width (ft) = 2.88  
EGL (ft) = 0.94

### Calculations

Compute by: Known Q  
Known Q (cfs) = 6.10



# Channel Report

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Friday, Oct 19 2018

## DP7 Trapazoidal Ditch 100 YR Flow (32.0 cfs)

### Trapezoidal

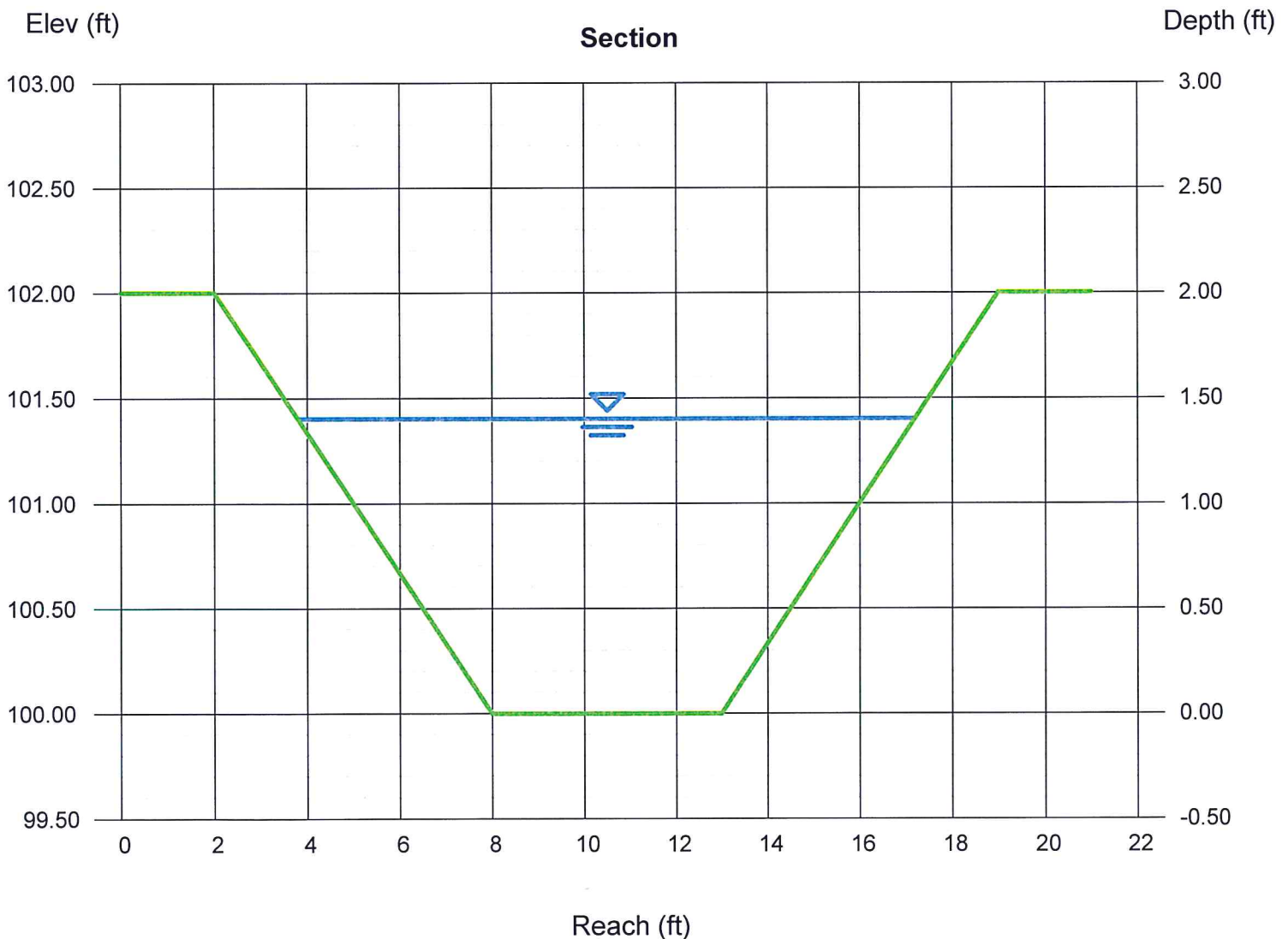
Bottom Width (ft) = 5.00  
Side Slopes (z:1) = 3.00, 3.00  
Total Depth (ft) = 2.00  
Invert Elev (ft) = 100.00  
Slope (%) = 0.50  
N-Value = 0.040

### Highlighted

Depth (ft) = 1.40  
Q (cfs) = 32.00  
Area (sqft) = 12.88  
Velocity (ft/s) = 2.48  
Wetted Perim (ft) = 13.85  
Crit Depth, Yc (ft) = 0.90  
Top Width (ft) = 13.40  
EGL (ft) = 1.50

### Calculations

Compute by: Known Q  
Known Q (cfs) = 32.00



# Channel Report

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Friday, Oct 19 2018

## DP7 24in RCP Pipe 5 YR Flow (16.4 cfs)

### Circular

Diameter (ft) = 2.00

Invert Elev (ft) = 100.00

Slope (%) = 0.82

N-Value = 0.013

### Calculations

Compute by: Known Q

Known Q (cfs) = 16.40

### Highlighted

Depth (ft) = 1.36

Q (cfs) = 16.40

Area (sqft) = 2.28

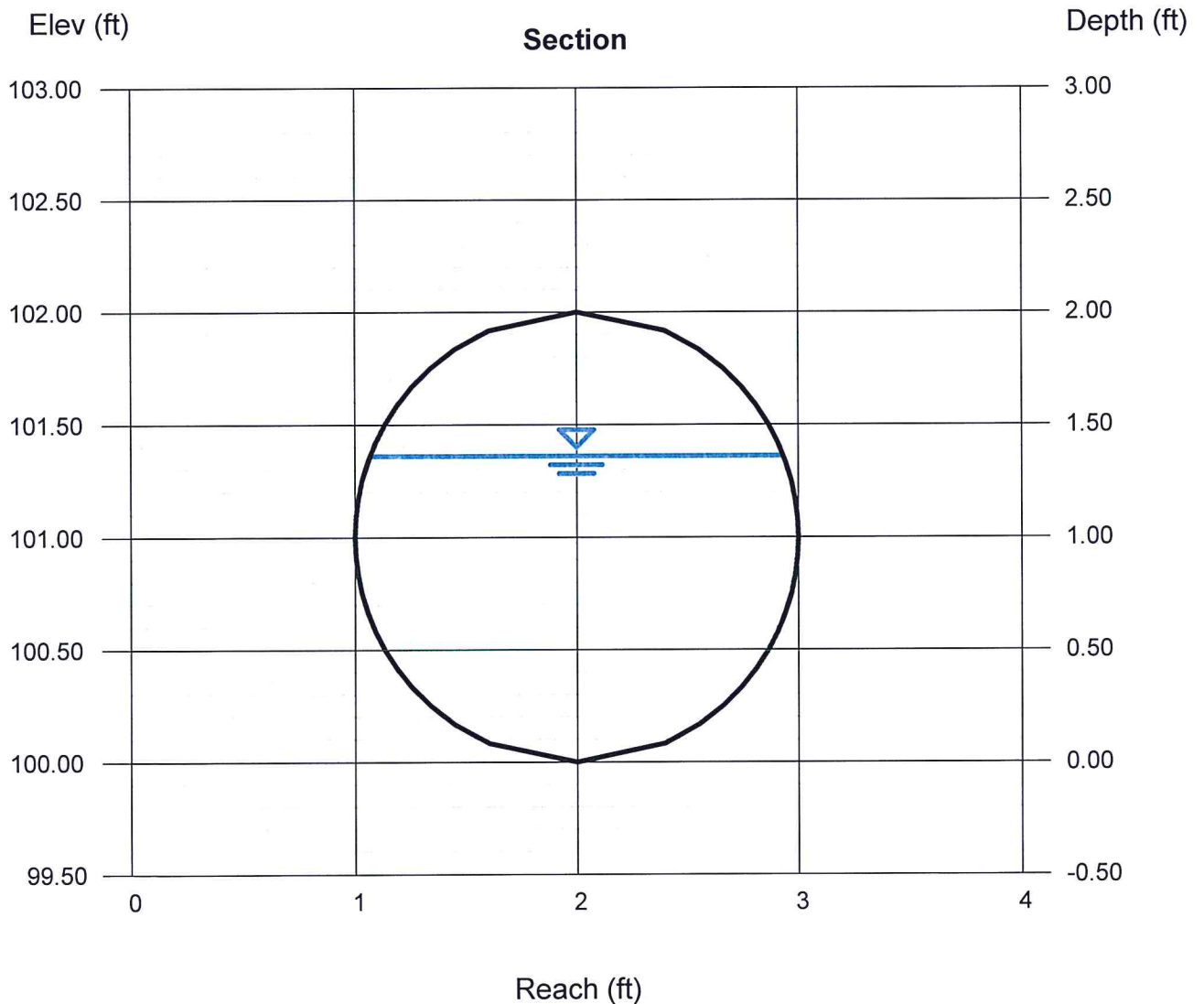
Velocity (ft/s) = 7.20

Wetted Perim (ft) = 3.88

Crit Depth, Yc (ft) = 1.46

Top Width (ft) = 1.87

EGL (ft) = 2.17



# Culvert Report

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Friday, Oct 19 2018

## DP7 culvert entrance

Invert Elev Dn (ft)	=	37.14
Pipe Length (ft)	=	47.00
Slope (%)	=	1.81
Invert Elev Up (ft)	=	37.99
Rise (in)	=	24.0
Shape	=	Circular
Span (in)	=	24.0
No. Barrels	=	1
n-Value	=	0.013
Culvert Type	=	Circular Concrete
Culvert Entrance	=	Square edge w/headwall (C)
Coeff. K,M,c,Y,k	=	0.0098, 2, 0.0398, 0.67, 0.5

### Embankment

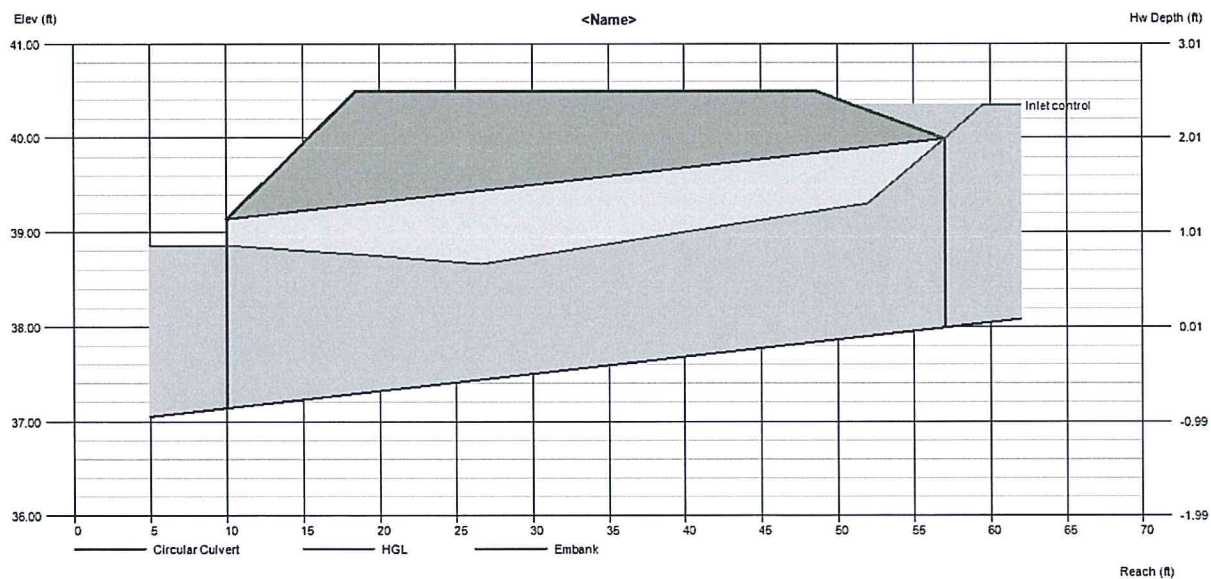
Top Elevation (ft)	=	40.50
Top Width (ft)	=	30.00
Crest Width (ft)	=	30.00

### Calculations

Qmin (cfs)	=	16.20
Qmax (cfs)	=	32.20
Tailwater Elev (ft)	=	(dc+D)/2

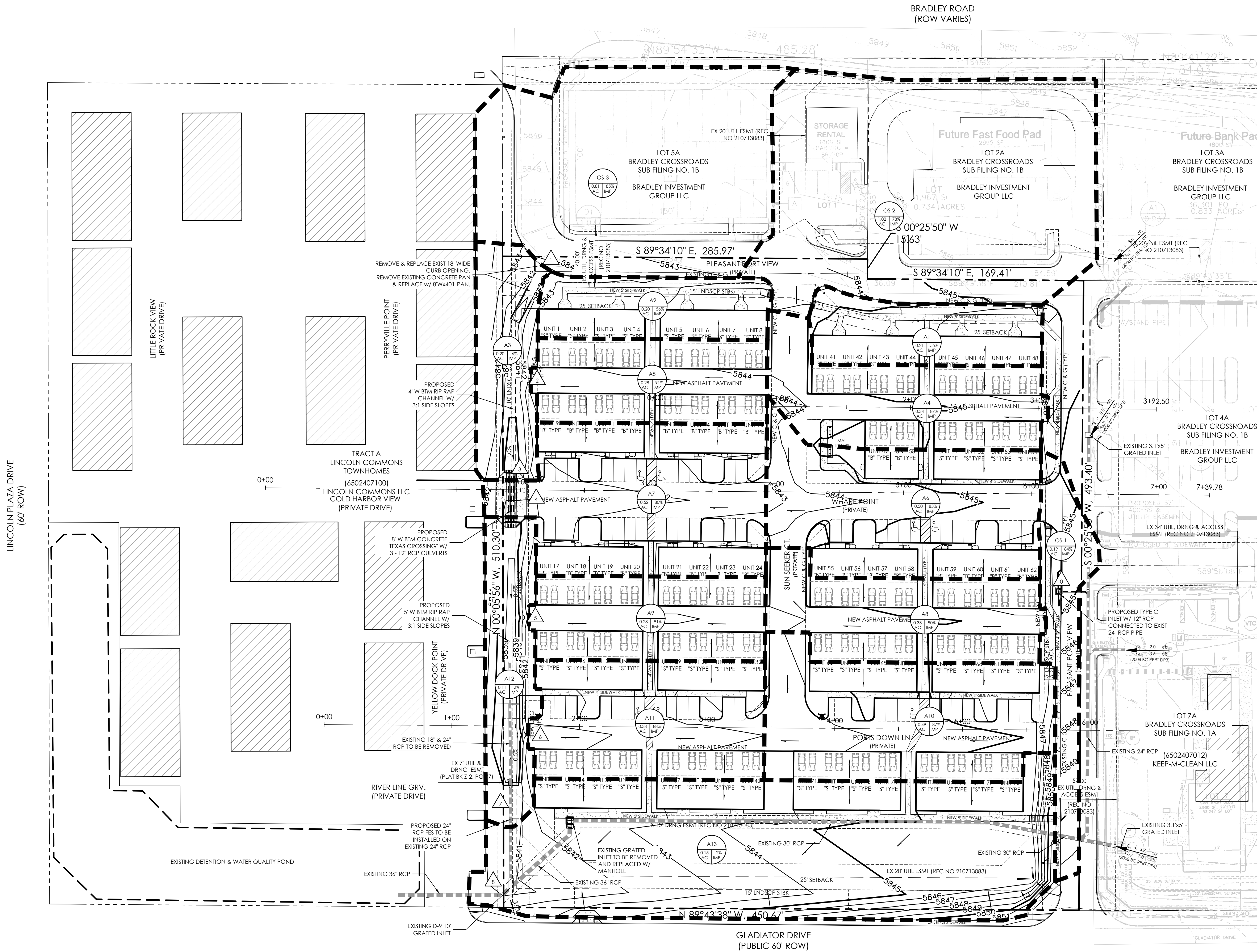
### Highlighted

Qtotal (cfs)	=	16.20
Qpipe (cfs)	=	16.20
Qovertop (cfs)	=	0.00
Veloc Dn (ft/s)	=	5.62
Veloc Up (ft/s)	=	6.64
HGL Dn (ft)	=	38.86
HGL Up (ft)	=	39.44
Hw Elev (ft)	=	40.37
Hw/D (ft)	=	1.19
Flow Regime	=	Inlet Control



## **4 Report Maps**

Proposed Condition Drainage Map (Map Pocket)



**LEGEND**

PROPERTY LINE  
EASEMENT LINE  
LOT LINE

**EXISTING**

INDEX CONTOUR  
INTERMEDIATE CONTOUR

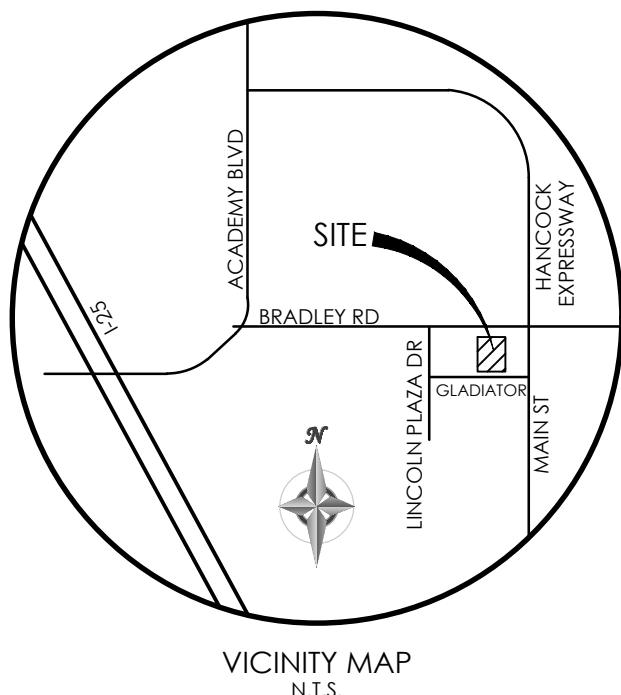
**PROPOSED**

INDEX CONTOUR  
INTERMEDIATE CONTOUR

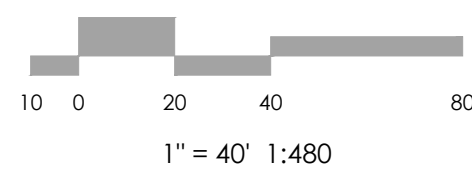
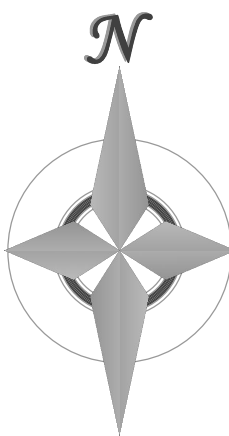
BASIN BOUNDARY  
GENERAL FLOW/DIRECTION  
SLOPE DIRECTION AND GRADE  
BASIN LABEL  
AREA IN ACRES  
PERCENT IMPERVIOUS  
POINT OF INTEREST

**FLOODPLAIN STATEMENT:**

NO PORTION OF THE SUBJECT PROPERTY IS NOT LOCATED WITHIN A FEMA DESIGNATED SPECIAL FLOOD HAZARD AREA (SFHA) AS INDICATED ON THE FLOOD INSURANCE RATE MAP (FIRM) FOR EL PASO COUNTY, COLORADO AND INCORPORATED AREAS - MAP NUMBER 08041C0763 G, EFFECTIVE DECEMBER 7, 2018.



BENCHMARK



DEVELOPED DRAINAGE SUMMARY TABLE				
POINT OF INTEREST/ BASIN(S)	AREA (AC)	Tc (MIN.)	RUNOFF	
			Q5 (CFS)	Q100 (CFS)
OS-1	0.19	5.0	0.8	1.4
OS-2	1.02	6.2	3.6	6.9
OS-3	0.81	5.2	3.2	6.0
A1	0.21	5.4	0.5	1.2
A2	0.20	5.3	0.5	1.1
DP1 (A1, A2, OS-2, OS-3)	2.25	7.1	7.3	14.1
A3	0.20	9.2	0.1	0.6
A4	0.34	5.2	1.3	2.5
A5	0.28	5.0	1.1	2.0
DP2 (A4, A5)	0.62	6.4	2.2	4.2
DP3 (DP1, DP2, A3)	3.07	8.2	9.1	17.9
A6	0.50	5.0	1.9	3.6
A7	0.52	5.0	1.9	3.7
DP4 (A6, A7)	1.02	6.1	3.6	6.9
A8	0.33	5.0	1.3	2.4
A9	0.28	5.0	1.1	2.0
DP5 (A8, A9)	0.60	6.2	2.2	4.2
A10	0.49	5.0	1.9	3.6
A11	0.38	5.0	1.5	2.8
DP6 (A10, A11)	0.88	6.1	3.2	6.1
A12	0.21	9.0	0.1	0.6
DP7 (DP1-6, A12)	5.78	9.8	16.4	32.0
A13	1.09	12.3	1.0	3.2
DP8 (DP1-7, A13)	6.87	9.9	17.4	35.3

**MVE, INC.**  
ENGINEERS & SURVEYORS

1903 Library Street, Suite 200 Colorado Springs, CO 80909 719.635.5736

REVISIONS

DESIGNED BY  
DRAWN BY  
CHECKED BY  
AS-BUILT BY  
CHECKED BY

**THE TOWNHOMES AT  
BRADLEY CROSSROADS**

**Drainage Map  
Developed  
Condition**

MVE PROJECT 61093  
MVE DRAWING -DRAIN-PP

APRIL 26, 2019  
SHEET 1 OF 1