## FINAL DRAINAGE REPORT FOR URBAN COLLECTION AT PALMER VILLAGE

**Prepared For:** 

MDC Holdings – Richmond American Homes 4350 South Monaco Street Denver, CO 80237 720-977-3827

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Prepared By: JR Engineering, LLC 5475 Tech Center Drive, Suite 235 Colorado Springs, CO 80919 719-593-2593



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#### **ENGINEER'S STATEMENT:**

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by El Paso County for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors, or omissions on my part in preparing this report.

Glenn D. Ellis, Colorado P.E. 38861 For and On Behalf of JR Engineering, LLC



#### **DEVELOPER'S STATEMENT:**

I, the developer, have read and will comply with all of the requirements specified in this drainage report and plan.

**Business Name:** 

MDC Holdings – Richmond American Homes

By:

Title: Address: <u>VP • Fleure Acquisition + Entitlements</u> <u>4350 South Monaco Street</u> Denver, CO 80237

#### **El Paso County:**

Filed in accordance with the requirements of the El Paso County Land Development Code, Drainage Criteria Manual, Volumes 1 and 2 and Engineering Criteria Manual, as amended.

	Approved	
Jennifer Irvine, P.E.	by Jeff Rice El Paso County Planning and Community Development on behalf of Elizabeth Nijkamp, Engineering Review Manager	
County Engineer/ ECM Administrator	09/07/2021 10:32:14 AM	1

Conditions:



April 2021

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# **Table of Contents**

Purpose	1
General Site Description	1
General Location	1
Description of Property	1
Floodplain statement	2
Existing Drainage Conditions	2
Major Basin Descriptions	2
Existing Sub-basin Drainage	3
Proposed Drainage Conditions	4
Proposed Sub-basin Drainage	4
Drainage Design Criteria	10
Development Criteria Reference	10
Hydrologic Criteria	10
Hydraulic Criteria	10
Drainage Facility Design	11
Four Step Process to Minimize Adverse Impacts of Urbanization	11
Water Quality	11
Erosion Control Plan	12
Operation & Maintenance	12
Drainage and Bridge Fees	13
Summary	13
References	14

#### APPENDIX

- Appendix A Vicinity Map, Soil Descriptions, FEMA Floodplain Map
- Appendix B Hydrologic Calculations
- Appendix C Hydraulic Calculations
- Appendix D Water Quality & Detention
- Appendix E Reference Material
- Appendix F Drainage Maps



# PURPOSE

This document is the Final Drainage Report for Urban Collection at Palmer Village. The purpose of this report is to identify on-site and off-site drainage patterns, storm sewer, culvert and inlet locations, areas tributary to the site, and to safely route developed storm water to adequate outfall facilities.

# **GENERAL SITE DESCRIPTION**

## **GENERAL LOCATION**

Urban Collection at Palmer Village is a proposed development within the Urban Collection at Palmer Village subdivision with a total area of 23.1 acres. The site is located in the northeast quarter of Section 5, Township 14 South, Range 65 West of the Sixth Principal Meridian in the County of El Paso, State of Colorado. The site is located immediately south of Constitution Avenue on the west and east side of Hannah Ridge Drive, extending to the east to Marksheffel Road. The site is bounded by Constitution Avenue to the north, Marksheffel Road to the east, Jessica Heights Filing No. 1 to the south, and the Cherokee Park Townhomes to the west. Refer to the vicinity map in Appendix A.

#### **DESCRIPTION OF PROPERTY**

A 100-unit residential development is proposed on lots 1 through 100 and Tracts A through L within the subdivision (hereby referred to as the "site") per the corresponding approved Final Plat. The area of the site totals 10.83 acres. The two tracts (M and N) along Constitution Avenue, east to Marksheffel Road will not be developed at this time. They are referenced in this report only in the context of being included in the plat of the proposed development. Any development of these two tracts shall require separate drainage analysis and drainage reports. The site is currently undeveloped other than a sanitary sewer easement that follows the eastern border of the site on the east side of Hannah Ridge Drive. The proposed development site is comprised of variable sloping grasslands that generally slope east at approximately 3% on the east side of Hannah Ridge Drive. On the west side of Hannah Ridge Drive the land slopes at about 1% to the east, draining into the curb and gutter in Hannah Ridge Drive.

Soil characteristics are comprised of Blakeland loamy sand. NRCS rates this soil designation as Hydrologic Group A. Group A soils exhibit a high infiltration rate when thoroughly wet and consist chiefly of deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a high rate of water transmission. Refer to the soil survey mapping in Appendix A.

There are no major drainageways on the proposed development site, although a tributary to the East Fork Sand Creek is immediately to the east of the site, within the undeveloped tracts.



There are no known irrigation facilities located on the project site. A 12" PVC sanitary sewer runs along the eastern side of the site within an easement.

#### **FLOODPLAIN STATEMENT**

Based on the FEMA Firm Map Number 08041C0752G, revised December 7, 2018, the entire development is located within Zone X, or areas area outside the Special Flood Hazard Area (SFHA) and higher than the elevation of the 0.2-percent-annual-chance (or 500-year) flood. The FEMA map containing the site has been presented in Appendix A.

## **EXISTING DRAINAGE CONDITIONS**

#### MAJOR BASIN DESCRIPTIONS

The site lies within the Sand Creek Drainage Basin based on the "Sand Creek Drainage Basin Planning Study" completed by Kiowa Engineering Corporation in January 1993. The Sand Creek Drainage Basin covers approximately 54 square miles and is divided into five major sub-basins: Sand Creek Mainstem, East Fork Sand Creek, Central Tributary to East Fork, West Fork, and East Fork Subtributary. The site is within the East Fork Sand Creek sub-basin, as shown in Appendix E. The Sand Creek Basin discharges into Fountain Creek approximately 1.5 miles upstream of Academy Boulevard Bridge over Fountain Creek.

As development occurred within the basin, the site was analyzed with the "Jessica Heights Filing No. 1 Final Drainage Report" completed by M.V.E. Inc. in April 2005. The portion of the site west of Hannah Ridge Drive was identified as Basin C1 and the portion of the site east of Hannah Ridge Drive was identified as Basin C1 contributes existing flows of  $Q_5 = 2.8$  cfs and  $Q_{100} = 6.8$  cfs. Basin A2 contributes existing flows of  $Q_5 = 3.2$  cfs and  $Q_{100} = 7.6$  cfs. Runoff from both basins flows east. Basin C1 is captured in Hannah Ridge Drive curb and gutter and is conveyed to Constitution Avenue, while Basin A2 sheet flows off site to the adjacent parcel to the east.

Most recently, the site was analyzed within the "Hannah Ridge at Feathergrass Master Drainage Development Plan" completed by M.V.E. Inc in November 2007. The site was identified as Basin OSA14 with existing flows of  $Q_5=14$  and  $Q_{100}=27$  cfs flowing easterly to Tributary to Sand Creek – East Fork Reach No. 6.

As previously stated, there are no known irrigation facilities within the site that would impact drainage. An existing 12" PVC sanitary sewer runs along the eastern boundary of the site and is contained within a dedicated easement.



## **EXISTING SUB-BASIN DRAINAGE**

The site is bisected by Hannah Ridge Drive, dividing the site into east and west parcels. The east side drains directly into a tributary to the East Fork Sand Creek (Tributary to Sand Creek – East Fork Reach No. 6). Runoff from the west site sheet flows across the site and is collected in Hannah Ridge Drive curb and gutter and is conveyed either north to Constitution Avenue or south to the Jessica Heights Subdivision. The west site is comprised of existing Basins EX3 and EX4. The east site is comprised of Basin EX6. Basins EX1 and EX2 are offsite basins that sheet flow onto Basins EX3 and EX4, respectively. Basin EX5 flows offsite to Constitution Avenue. The basins shown in the "Jessica Heights Filing No. 1 Final Drainage Report" created by M.V.E., Inc. in April, 2005 correspond to the existing basins in this report in the following manner: OSA = EX1, OSB = EX2, C1 = EX3 and EX4, A4 = EX5, A2 = EX6.

Existing Basin EX1 is approximately 0.15 acres and is consistent with the Jessica Heights Filing No. 1 Final Drainage Report Basin OSA. Flow from this basin sheet flows onto the site to Basin EX3 at Design Point (DP) 1 ( $Q_5=0.04$  cfs,  $Q_{100}=0.4$  cfs), eventually reaching DP3, a local depression.

Existing Basin EX2 is approximately 0.46 acres and is consistent with the Jessica Heights Filing No. 1 Final Drainage Report Basin OSB. Flow from this basin ( $Q_5=0.2$  cfs,  $Q_{100}=1.2$  cfs) sheet flows onto the site to Basin EX4 at DP2, eventually reaching Hannah Ridge Drive at DP4.

Existing Basin EX3 is approximately 4.27 acres and consists of prairie grasses. Flow from this basin  $(Q_5 = 1.2 \text{ cfs}, Q_{100} = 9.0 \text{ cfs})$  sheet flows to the local depression at DP3. According to the available contour data, once the local depression has filled, the overtopping flow travels to the northeast. The flow then is conveyed to the curb and gutter along the south side of Constitution Avenue, where it is conveyed to an existing Type R inlet approximately 670 feet east of Hannah Ridge Drive. The flow that enters the existing inlet is routed into the existing double 10' x 6' concrete box culvert that conveys the tributary to the East Fork Sand Creek under Constitution Avenue.

Existing Basin EX4 is approximately 1.62 acres and consists of prairie grasses and a portion of Hannah Ridge Drive. Flow from this basin ( $Q_5$ =1.1 cfs,  $Q_{100}$  =4.0 cfs) sheet flows to the curb and gutter in Hannah Ridge Drive at DP4. The flow then is conveyed south via the Jessica Heights Subdivision storm sewer system, eventually discharging into a tributary to the East Fork Sand Creek.

Existing Basin EX5 is approximately 0.37 acres and consists of a portion of Hannah Ridge Drive and prairie grasses. Flow from this basin ( $Q_5=1.4$  cfs,  $Q_{100}=2.7$  cfs) flows north along the Hannah Ridge Drive curb and gutter until it reaches the curb and gutter on the south side of Constitution Avenue at DP5. From there, the flow follows the same path as the flow that overtops the local depression in Basin EX3.



#### FINAL DRAINAGE REPORT FOR URBAN COLLECTION AT PALMER VILLAGE

Existing Basin EX6 is approximately 5.25 acres and consists of prairie grasses. Flow from this basin ( $Q_5=1.5$  cfs,  $Q_{100}=11.1$  cfs) sheet flows to the eastern property line at DP6 and enters a tributary to the East Fork Sand Creek.

As stated previously, the undeveloped tracts east of the site have not been analyzed in their existing conditions as part of this report. Future development of these tracts will require a separate drainage report.

# **PROPOSED DRAINAGE CONDITIONS**

## **PROPOSED SUB-BASIN DRAINAGE**

The site was broken into two major proposed basins: Basin A (west parcel) and Basin B (east parcel). The proposed basin (and sub-basin) delineation is shown on the drainage basin map and is described as follows:

Basin EX1 is approximately 0.15 acres and is consistent with the Jessica Heights Filing No. 1 Final Drainage Report Basin OSA. Flow from this basin sheet flows onto the site to Basin A1 at Design Point (DP) EX1 ( $Q_5=0.04$  cfs,  $Q_{100}=0.4$  cfs). The flow is combined with runoff from Basin A1 at DP1.

Basin A1 consists of approximately 0.78 acres and includes walks, drives, roofs and landscape areas. Flow from this basin ( $Q_5=2.6$  cfs and  $Q_{100}=5.1$  cfs) will be collected and conveyed in the centerline of Vanhoutte View to DP1. At DP1 ( $Q_5=2.3$  cfs and  $Q_{100}=4.9$  cfs), flow combines with runoff from Basin EX1 and enters EPC Type A curb and gutter. The curb and gutter conveys the flow east to a sump Double Denver Type 16 Combination Inlet (Double Type 16 inlet) at DP3, where it combines with Basin A2 flow.

Basin A2 consists of approximately 0.22 acres and includes walks, drives, and landscape areas. Flow from this basin ( $Q_5=0.6$  cfs and  $Q_{1oo}=1.3$  cfs) will be collected and conveyed in EPC Type A curb and gutter on the north side of Wayfaring Tree Heights to a sump Double Type 16 inlet at DP3, where it combines with the flow from DP1.

Total flows at DP3 are  $Q_5=3.0$  cfs and  $Q_{100}=6.2$  cfs. The sump Double Type 16 inlet captures all flow in the 5-year and 100-year events. DP3 flow combine with DP4 flow at DP4.1. In the event that the inlet becomes clogged, the flow will follow the curb flowline to the east to the on-grade Double Type 16 inlet at DP5.

Basin A3 consists of approximately 0.11 acres and includes walks, drives, and landscape areas. Flow from this basin ( $Q_5=0.3$  cfs and  $Q_{100}=0.7$  cfs) will be collected and conveyed in EPC Type A curb



and gutter on the south side of Wayfaring Tree Heights to an on-grade Double Type 16 inlet at DP4, where it combines with Basin A4 flow.

Basin A4 consists of approximately 0.62 acres and includes walks, drives, roofs and landscape areas. Flow from this basin ( $Q_5=2.0$  cfs and  $Q_{100}=4.0$  cfs) will be collected and conveyed in the centerline of Vanhoutte View to DP2. At DP2, flow enters EPC Type A curb and gutter and is conveyed east to an on-grade Double Type 16 inlet at DP4, where it combines with Basin A3 flow.

Total flows at DP4 are  $Q_5=2.4$  cfs and  $Q_{100}=5.7$  cfs. The on-grade Double Type 16 inlet captures 1.9 cfs in the 5-year and 3.4 cfs in the 100-year event. DP4 flow-by of  $Q_5=0.5$  cfs and  $Q_{100}=2.3$  cfs continues east via curb and gutter to DP6 where it combines with Basin A7 flow. DP4 captured flow is piped in 18" RCP to DP4.1, where it combines with flow from DP3.

Total flows at DP4.1 are  $Q_5=4.8$  cfs and  $Q_{100}=9.4$  cfs. The flow is conveyed via 18" and 24" RCP to DP5.1, where it combines with flow from DP5.

Basin A5 consists of approximately 0.83 acres and includes walks, drives, roofs and landscape areas. Flow from this basin ( $Q_5=2.0$  cfs and  $Q_{100}=4.2$  cfs) will be collected and conveyed in the centerline of Serviceberry Grove and the EPC Type A curb and gutter on the north side of Wayfaring Tree Heights to an on-grade Double Type 16 inlet at DP5. The on-grade Double Type 16 inlet captures 1.6 cfs in the 5-year and 2.7 cfs in the 100-year event. DP5 flow-by of  $Q_5=0.4$  cfs and  $Q_{100}=1.5$  cfs continues east via curb and gutter to DP8 where it combines with Basin A6 and DP7 flow. DP5 captured flow combines with DP4.1 flow at DP5.1.

Total flows at DP5.1 are  $Q_5=6.7$  cfs and  $Q_{100}=13.5$  cfs. The flow is conveyed via 30" RCP to DP8.1, where it combines with flow from DP8.

Basin A6 consists of approximately 0.18 acres and includes walks, drives, and landscape areas. Flow from this basin ( $Q_5=0.6$  cfs and  $Q_{1oo}=1.1$  cfs) will be collected and conveyed in EPC Type A curb and gutter in Wayfaring Tree Heights to a sump Triple Type 16 inlet at DP8, where it combines with flow from DP7 and DP5 flow-by.

Basin A7 consists of approximately 0.46 acres and includes walks, drives, roofs and landscape areas. Flow from this basin ( $Q_5=1.3$  cfs and  $Q_{100}=2.7$  cfs) will be collected and conveyed in the centerline of Serviceberry Grove to DP6. At DP6, flow enters EPC Type A curb and gutter and combines with DP4 flow-by. The combined flow is conveyed to a sump Triple Type 16 inlet at DP9, where it combines with Basin A9 flow.

Total flows at DP6 are  $Q_5=1.8$  cfs and  $Q_{100}=4.8$  cfs. The flow is conveyed east via curb and gutter to DP9, where it combines with flow from Basin A9 and DP8 flow-by.



#### FINAL DRAINAGE REPORT FOR URBAN COLLECTION AT PALMER VILLAGE

Basin A8 consists of approximately 0.75 acres and includes walks, drives, roofs and landscape areas. Flow from this basin ( $Q_5=1.5$  cfs and  $Q_{100}=3.5$  cfs) will be collected and conveyed in the centerline of Fountain Grass Grove to DP7. At DP7, flow enters EPC Type A curb and gutter and is conveyed west to a sump Triple Type 16 inlet at DP8 where it combines with DP5 flow-by and Basin A6 flow.

Total flows at DP8 are  $Q_5=2.4$  cfs and  $Q_{100}=5.9$  cfs. The sump Triple Type 16 inlet captures all flows in the 5-year and 4.3 cfs in the 100-year event. DP8 flow-by of  $Q_{100}=1.6$  cfs overtops the centerline crown of the road south to DP9 where it combines with Basin A9 and DP6 flow. DP8 captured flow combines with DP5.1 flow at DP8.1.

Total flows at DP8.1 are  $Q_5=8.8$  cfs and  $Q_{100}=15.0$  cfs. All flow at DP8.1 is conveyed via 30" RCP to DP9.1, where it combines with flow from DP9.

Basin A9 consists of approximately 0.57 acres and includes walks, drives, roofs and landscape areas. Flow from this basin ( $Q_5=1.8$  cfs and  $Q_{100}=3.5$  cfs) will be collected and conveyed in EPC Type A curb and gutter on the west side of Fountain Grass Grove to a sump Triple Type 16 inlet at DP9, where it combines with flow from DP6 and DP8 flow-by.

The total combined flow at DP9 from DP6, DP8 flow-by, and Basin A9 is  $Q_5=3.4$  cfs and  $Q_{100}=9.2$  cfs. All flow at DP9 is captured and combines with flow from DP8.1 at DP9.1. If the sump inlet at DP9 were to become clogged, flow would overtop the curb to the south and discharge directly into Pond A.

Total flows at DP9.1 are  $Q_5=11.8$  cfs and  $Q_{100}=23.9$  cfs. All flow at DP9.1 is conveyed via 30" RCP to Pond A at DP10, where it combines with flow from Basin A10.

Basin A10 consists of approximately 0.78 acres of sidewalk, landscaped areas, and contains Full Spectrum Water Quality and Detention Pond A. Flow from this basin ( $Q_5=0.4$  cfs and  $Q_{1oo}=2.1$  cfs) is captured in a grass-lined swale that discharges directly into Pond A where it combines with flow from DP9.1. A detailed discussion of Full-Spectrum Water Quality and Detention Pond A is presented in the Water Quality section later in this report.

Total flows at DP10 are  $Q_5=12.1$  cfs and  $Q_{100}=25.7$  cfs. All flow at DP10 is routed through the Pond A outlet structure and proposed RCP (various sizes) before discharging into the existing double 10'x6' concrete box culvert that conveys a tributary to the East Fork Sand Creek.

Basin A11 consists of approximately 0.16 acres and includes walks, drives, and landscape areas. Due to topographical constraints, Basin A11 ( $Q_5=0.3$  cfs and  $Q_{1oo}=0.6$  cfs) flow drains overland to the existing curb and gutter on the south side of Constitution Avenue, which conveys it east to an existing Type R inlet at DP11.



Basin A12 consists of approximately 0.13 acres and includes landscaped area and sidewalk. Due to topographical constraints, Basin A12 ( $Q_5=0.2$  cfs and  $Q_{1oo}=0.6$  cfs) flow drains overland to the existing curb and gutter on the south side of Constitution Avenue, which conveys it east to the existing Hannah Ridge Drive cross pan at DP12.

Basin B1 consists of approximately 0.61 acres and includes walks, drives, roofs and landscape areas. Flow from this basin ( $Q_5=1.4$  cfs and  $Q_{1oo}=3.2$  cfs) will be collected and conveyed in the centerline of Fountain Grass Grove to DP15. At DP15, flow enters EPC Type A curb and gutter and is conveyed east to an on-grade Double Type 16 inlet at DP17, where it combines with Basin B2 flow.

Basin B2 consists of approximately 0.08 acres and includes walks and drives. Flow from this basin  $(Q_5=0.4 \text{ cfs} \text{ and } Q_{100}=0.6 \text{ cfs})$  will be collected and conveyed in EPC Type A curb and gutter in Blue Avena View to an on-grade Double Type 16 inlet at DP17, where it combines with flow from DP15.

Total flows at DP17 are  $Q_5=1.7$  cfs and  $Q_{100}=3.6$  cfs. The on-grade Double Type 16 inlet captures 1.4 cfs in the 5-year event and 2.3 cfs in the 100-year event. DP17 flow-by of  $Q_5=0.3$  cfs and  $Q_{100}=1.3$  cfs continues east in curb and gutter to an on-grade Single Type 16 inlet at DP19 where it combines with Basin B5 flow. DP17 captured flows are piped in 18" RCP to DP18.1, where it combines with flow from DP18.

Basin B3 consists of approximately 0.12 acres and includes walks, drives, and landscape areas. Flow from this basin ( $Q_5=0.5$  cfs and  $Q_{100}=0.9$  cfs) will be collected and conveyed in EPC Type A curb and gutter in Blue Avena View to an on-grade Double Type 16 inlet at DP18, where it combines with flow from DP16.

Basin B4 consists of approximately 0.76 acres and includes walks, drives, roofs and landscape areas. Flow from this basin ( $Q_5=2.5$  cfs and  $Q_{100}=4.9$  cfs) will be collected and conveyed in the centerline of Fountain Grass Grove to DP16. At DP16, flow enters EPC Type A curb and gutter and is conveyed east to a sump Double Type 16 inlet at DP18, where it combines with Basin B3 flow.

Total flows at DP18 from DP16 and Basin B3 are  $Q_5=2.8$  cfs and  $Q_{100}=5.4$  cfs. The sump Double Type 16 inlet captures all flow in the 5-year and 100-year events. DP18 flow combines with DP17 flow at DP18.1. In the event that the inlet at DP18 becomes clogged, flow will follow the flowline east to the sump Double Type 16 inlet at DP23.

Total flows at DP18.1 are  $Q_5=4.2$  cfs and  $Q_{100}=7.8$  cfs. The flow is conveyed via 18" RCP to DP23.1, where it combines with flow from DP23.

Basin B5 consists of approximately 0.66 acres and includes walks, drives, roofs and landscape areas. Flow from this basin ( $Q_5=1.6$  cfs and  $Q_{100}=3.5$  cfs) will be collected and conveyed in the centerline



of Purple Fountain Point to an on-grade Single Type 16 inlet at DP19, where it combines with DP17 flow-by.

Total flows at DP19 from Basin B5 and DP17 flow-by are  $Q_5=1.9$  cfs and  $Q_{100}=4.8$  cfs. The on-grade Single Type 16 inlet captures 1.2 cfs in the 5-year and 2.1 cfs in the 100-year event. DP19 flow-by of  $Q_5=0.7$  cfs and  $Q_{100}=2.7$  cfs continues east via curb and gutter to a sump Triple Type 16 inlet at DP24 where it combines with Basin B6 flow. DP19 captured flow is conveyed via 18" RCP to DP24.1, where it combines with DP24 flow.

Basin B6 consists of approximately 0.08 acres and includes walks, drives and landscape areas. Flow from this basin ( $Q_5=0.3$  cfs and  $Q_{100}=0.6$  cfs) will be collected and conveyed in EPC Type A curb and gutter in Blue Avena View to a sump Triple Type 16 inlet at DP24, where it combines with DP19 flow-by.

Total flows at DP24 from DP19 flow-by and Basin B6 are  $Q_5=1.0$  cfs and  $Q_{100}=3.2$  cfs. All flow at DP24 is captured by a sump Triple Type 16 inlet and combines with flow from DP19 and DP23.1 at DP24.1. In the event that the inlet at DP24 becomes clogged, flow will overtop the curb to the north and enter Pond B.

Basin B7 consists of approximately 0.13 acres and includes walks, drives, and landscape areas. Flow from this basin ( $Q_5=0.5$  cfs and  $Q_{100}=1.0$  cfs) will be collected and conveyed in EPC Type A curb and gutter in Blue Avena View to a sump Double Type 16 inlet at DP23, where it combines with flow from DP20 and DP22 flow-by.

Basin B8 consists of approximately 0.72 acres and includes walks, drives, roofs and landscape areas. Flow from this basin ( $Q_5=2.2$  cfs and  $Q_{1oo}=4.4$  cfs) will be collected and conveyed in the centerline of Purple Fountain Point to DP20. The flow is conveyed east to a sump Double Type 16 inlet at DP23, where it combines with Basin B7 flow and DP22 flow-by.

Basin B9 consists of approximately 0.31 acres of landscaped areas and sidewalk. Flow from this basin ( $Q_5=0.1$  cfs and  $Q_{100}=0.9$  cfs) is conveyed in a grass-lined swale to a sump Type C Inlet at DP21. All Basin B9 flow is captured at DP21 and is piped via 18" RCP to DP22.1, where it combines with flows from DP22. In the event that the inlet at DP21 becomes clogged, the flow will overtop the one-foot depression and continue to flow east to DP30 via a grass-lined swale.

Basin B10 consists of approximately 0.55 acres and includes walks, drives, roofs and landscape areas. Flow from this basin ( $Q_5=1.6$  cfs and  $Q_{100}=3.2$  cfs) will be collected and conveyed in EPC Type A curb and gutter on the west side of Foerster Grass View to a sump Double Type 16 inlet at DP22. All captured flow at DP22 ( $Q_5=1.4$  cfs and  $Q_{100}=2.6$  cfs) is piped via 18" RCP to DP22.1, where it combines with flow from DP21. DP22 flow-by ( $Q_{100}=0.6$  cfs) will follow the curb flowline



north to the sump Double Type 16 inlet at DP23. In the event that the inlet at DP22 becomes clogged, the flow would follow the curb flowline north to the sump Double Type 16 inlet at DP23.

The total combined flow at DP23 from Basin B7, DP20, and DP22 flow-by is  $Q_5=2.6$  cfs and  $Q_{100}=5.6$  cfs. All flow at DP23 is captured and combines with flow from DP18.1 at DP23.1. In the event the inlet at DP23 becomes clogged, the flow will overtop the road crown to the north and enter the sump Triple Type 16 inlet at DP24.

Total flows at DP22.1 are  $Q_5=1.7$  cfs and  $Q_{100}=3.5$  cfs. The flow is conveyed via 18" RCP to DP23.1, where it combines with flow from DP23.

Total flows at DP23.1 from DP18.1, DP22.1, and DP23 are  $Q_5=8.2$  cfs and  $Q_{100}=16.5$  cfs. The flow is conveyed via 24" RCP to DP24.1, where it combines with flow from DP19 and DP24.

Total flows at DP24.1 are  $Q_5=10.2$  cfs and  $Q_{100}=21.5$  cfs. The flow is conveyed via 30" RCP to Pond B at DP25, where it combines with flow from Basin B11.

Basin B11 consists of approximately 0.55 acres of walks and landscaped areas and contains Full-Spectrum Water Quality and Detention Pond B. Flow from this basin ( $Q_5=0.3$  cfs and  $Q_{100}=1.7$  cfs) sheet flows directly into Pond B where it combines with flow from DP24.1 at DP25. A detailed discussion of Full-Spectrum Water Quality and Detention Pond B is presented in the Water Quality section later in this report.

Total flows at DP25 are  $Q_5=10.4$  cfs and  $Q_{100}=22.9$  cfs. All flow at DP25 is routed through the Pond B outlet structure and proposed RCP (various sizes) before discharging into the existing double 10'x6' concrete box culvert that conveys a tributary to the East Fork Sand Creek.

Basin B12 consists of approximately 0.06 acres of landscaped areas and sidewalk. Due to topographical constraints, flow from this basin ( $Q_5=0.1$  cfs and  $Q_{100}=0.3$  cfs) will discharge directly into Constitution Avenue curb and gutter at DP26, which conveys the flow east to an existing Type R inlet about 670 feet east of Hannah Ridge Drive.

Basin B13 consists of approximately 0.18 acres of landscaped areas and sidewalk. Due to topographical constraints, flow from this basin ( $Q_5=0.3$  cfs and  $Q_{100}=0.9$  cfs) will discharge directly into Constitution Avenue curb and gutter at DP27, and will follow the same flow path as Basin B12.

Basin B14 consists of approximately 0.17 acres of landscaped areas and contains approximately 1,870 square feet of asphalt roadway. Flow from this basin ( $Q_5=0.2$  cfs and  $Q_{1oo}=0.7$  cfs) follows historic drainage patterns and sheet flows offsite at DP28, along the eastern site boundary, eventually flowing directly into the Tributary to Sand Creek – East Fork Reach No. 6.



Basin B15 consists of approximately 0.17 acres of walks and landscaped areas. Flow from this basin ( $Q_5=0.2$  cfs and  $Q_{1oo}=0.6$  cfs) follows historic drainage patterns and sheet flows easterly offsite at DP29 to Tributary to Sand Creek – East Fork Reach No. 6.

Basin B16 consists of approximately 0.11 acres of landscaped areas and will remain undeveloped. Flow from this basin ( $Q_5=0.1$  cfs and  $Q_{1oo}=0.3$  cfs) is conveyed in a grass-lined swale onsite before discharging to the east property line at DP30. From here, the flow follows historic drainage patterns to the Tributary to Sand Creek – East Fork Reach No. 6.

# **DRAINAGE DESIGN CRITERIA**

## **DEVELOPMENT CRITERIA REFERENCE**

Storm drainage analysis and design criteria for this project were taken from the "*City of Colorado Springs/El Paso County Drainage Criteria Manual*" Volumes 1 and 2 (EPCDCM), dated October 12, 1994, the "*Urban Storm Drainage Criteria Manual*" Volumes 1 to 3 (USDCM) and Chapter 6 and Section 3.2.1 of Chapter 13 of the "*Colorado Springs Drainage Criteria Manual*" (CSDCM), dated May 2014, as adopted by El Paso County.

## HYDROLOGIC CRITERIA

All hydrologic data was obtained from the "*El Paso Drainage Criteria Manual*" Volumes 1 and 2, and the "*Urban Drainage and Flood Control District Urban Storm Drainage Criteria Manual*" Volumes 1, 2, and 3. Onsite drainage improvements were designed based on the 5-year (minor) storm event and the 100-year (major) storm event. Runoff was calculated using the Rational Method, and rainfall intensities for the 5-year and the 100-year storm return frequencies were obtained from Table 6-2 of the CSDCM. One hour point rainfall data for the storm events is identified in the chart below. Runoff coefficients were determined based on proposed land use and from data in Table 6-6 from the CSDCM. Time of concentrations were developed using equations from CSDCM. All runoff calculations and applicable charts and graphs are included in the Appendices.

Table 2 - 1-m Tollit Kalifali Data				
Storm	Rainfall (in.)			
5-year	1.50			
100-year	2.52			

## HYDRAULIC CRITERIA

The Rational Method and USDCM's SF-2 and SF-3 forms were used to determine the runoff from the minor and major storms on the site, and the UDFCD UD-Detention v4.04 spreadsheet was utilized for evaluating proposed detention and water quality pond. Sump and on-grade inlets were sized using UDFCD UD-Inlet v4.05. Manning's equation was used to size the proposed pipes in this report and StormCAD was used to model the proposed storm sewer system and to analyze the



proposed HGL calculations for the Construction Drawings. See Appendix C for the HGL calculations.

# **DRAINAGE FACILITY DESIGN**

#### FOUR STEP PROCESS TO MINIMIZE ADVERSE IMPACTS OF URBANIZATION

In accordance with the El Paso County Drainage Criteria Manual Volume 2, this site has implemented the four step process to minimize adverse impacts of urbanization. The four step process includes reducing runoff volumes, treating the water quality capture volume (WQCV), stabilizing drainage ways, and implementing long-term source controls.

Step 1 – Reducing Runoff Volumes: The Urban Collection at Palmer Village development project consists of 50 duplex structures with open spaces and lawn areas interspersed within the development which helps disconnect impervious areas and reduce runoff volumes. Roof drains from the structures will discharge to lawn areas, where feasible, to allow for infiltration and runoff volume reduction.

Step 2 – Stabilize Drainageways: The site lies within the Sand Creek Drainage Basin. Basin and bridge fees will be paid at time of platting. These funds will be used on future projects within the basin to stabilize drainageways. The site does not discharge directly into the open drainageway of Sand Creek, therefore no downstream stabilization will be accomplished with this project.

Step 3 – Treat the WQCV: Water Quality treatment for this site is provided in two proposed fullspectrum water quality detention ponds: Pond A and Pond B. The runoff from this site will be collected within inlets and conveyed to the proposed ponds via storm sewer. Upon entrance to the ponds, flows will be captured in a forebay designed to promote settlement of suspended solids. A trickle channel is also incorporated into the ponds to minimize the amount of standing water. The outlet structure has been designed to detain the water quality capture volume (WQCV) for 40 hours, and the extended urban runoff volume (EURV) for 72 hours. All flows released from the ponds will be reduced to less than historic rates.

Step 4 – Consider Need for Industrial and Commercial BMPs: Step 4 does not apply to this project since the site is not an industrial or commercial site.

## WATER QUALITY

The site is split by Hannah Ridge Drive, therefore, a full-spectrum water quality and detention pond is provided on both sides. Basins EX1, EX2, and A1-A10, located west of Hannah Ridge Drive, will discharge to Pond A. Basins B1-B11, located east of Hannah Ridge Drive, will discharge to Pond B. Both ponds have been designed per Section 13.3.2.1 of Resolution 15-042 of the El Paso County Drainage Criteria Manual.



#### FINAL DRAINAGE REPORT FOR URBAN COLLECTION AT PALMER VILLAGE

Full-Spectrum Water Quality and Detention Pond A is designed for a total contributing acreage of 5.92 acres at 50.5% impervious from Basins EX1, EX2, and A1-A10. The total WQCV is 0.102 acft, the excess urban runoff volume (EURV) is 0.346 ac-ft, and the total required detention volume is 0.548 ac-ft. The WQCV is released over 41 hours, the EURV is released over 72 hours, and the 100year volume is released over 80 hours. The 100-year discharge of 2.4 cfs is less than 90% of predevelopment rates. An emergency inlet is provided that conveys the full undetained, peak 100year flow of 25.7 cfs with a 1.0' freeboard.

Pond A's outlet structure outfalls into a 30" RCP that flows along the site's southern property line before discharging into the existing double 10'x6' RCBC located in the adjacent parcel, east of the eastern parcel. A drainage easement is provided for both the onsite and offsite portions of this pond outfall. The ultimate discharge of the double 10'x6' RCBC is the "Tributary to Sand Creek – East Fork Reach No. 6". A drainage map including Pond A and its outfall has been presented in Appendix F. Due to the fact that there are no upstream regional detention facilities, an "emergency conditions" scenario was not analyzed for Pond A.

Pond B is designed for a total contributing acreage of 4.57 acres at 54.3% impervious from Basins B1-B11. The total WQCV is 0.083 ac-ft, the excess urban runoff volume (EURV) is 0.293 ac-ft and the total required detention volume is 0.456 ac-ft. The WQCV is released over 42 hours, the EURV is released over 72 hours and the 100-year volume is released over 78 hours. The 100-year discharge of 1.8 cfs is less than 90% of predevelopment rates. A riprap spillway is provided that conveys the full undetained, peak 100-year flow of 22.9 cfs with a 1.0' freeboard. The spillway has a crest length of 20' and a total depth of 1.50'. Additionally, emergency overflow inlets are included to capture emergency flows.

The pond outfalls into a 30" RCP that flows east and south, connecting to the Pond A outfall. A drainage easement will be provided for both the onsite and offsite portions of this pond outfall. The ultimate discharge of the double 10' x 6' RCBC is the" Tributary to Sand Creek – East Fork Reach No. 6". A drainage map including Pond B and it's outfall has been presented in Appendix F. Due to the fact that there are no upstream regional detention facilities, an "emergency conditions" scenario was not analyzed for Pond B.

## **EROSION CONTROL PLAN**

The Erosion Control Plan and Cost Estimate have been submitted for review in conjunction with the grading and erosion control plan and construction assurances will be posted prior to issuance of a building permit.

## **OPERATION & MAINTENANCE**

In order to ensure the function and effectiveness of the stormwater infrastructure, maintenance activities such as inspection, routine maintenance, restorative maintenance, rehabilitation and repair, are required. The property owner shall be responsible for the inspection, maintenance, rehabilitation



and repair of stormwater and erosion control facilities located on the property unless another party accepts such responsibility in writing and responsibility is properly assigned through legal documentation. Access is provided from onsite facilities and easements for proposed infrastructure located offsite. We respectfully request that the Operation & Maintenance Manual be submitted in conjunction with the construction documents, prior to obtaining a grading permit.

## **DRAINAGE AND BRIDGE FEES**

The site lies within the Sand Creek Drainage Basin. Anticipated drainage and bridge fees are presented below, based on Resolution No. 19-441, and will be paid at time of platting. Fees could change, and are dependent on the timing of the plat.

2020 DRAIN	IAGE AND BRIDGI	E FEES - URBAN C	OLLECTION AT PAL	MER VILLAGE
Impervious Acres	Drainage Fee (Per Imp. Acre)	Bridge Fee (Per Imp. Acre)	Urban Collection at Palmer Village Drainage Fee	Urban Collection at Palmer Village Bridge Fee
5.67	\$19,698	\$8,057	\$111,688	\$45,683

# SUMMARY

The proposed Urban Collection at Palmer Village development drainage improvements, including storm sewer and two full-spectrum water quality and detention ponds were designed to meet or exceed the El Paso County Drainage Criteria. The proposed development will not adversely affect the offsite drainageways or surrounding development. This report is in conformance and meets the latest El Paso County Storm Drainage Criteria requirements for this site.



# REFERENCES

- <u>City of Colorado Springs Drainage Criteria Manual</u> (Volumes I & II), City of Colorado Springs, Colorado, Updated May, 2014.
- 2. <u>Urban Storm Drainage Criteria Manual</u> (Volumes 1, 2, and 3), Urban Drainage and Flood Control District, June 2001.
- 3. <u>Sand Creek Drainage Basin Planning Study</u>, prepared Kiowa Engineering Corporation, January, 1993.
- 4. Jessica Heights Filing No. 1 Final Drainage Report, prepared by M.V.E., Inc, April, 2005.
- 5. <u>Hannah Ridge at Feathergrass Master Drainage Development Plan</u>, prepared by M.V.E., Inc., November 15, 2007.
- 6. <u>Preliminary Drainage Report for Urban Collection at Palmer Village</u>, prepared by JR Engineering, LLC, July, 2020.



Appendix A Vicinity Map, Soil Descriptions, FEMA Floodplain Map





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#### NOTES TO USERS

is map is for use in administering the National Flood Insurance Program. It does t necessarily identify all areas subject to flooding, particularly from local drainage urces of small size. The **community map repository** should be consulted for ssible updated or additional flood hazard information.

To obtain more detailed information in areas where Base Flood Elevations (BFEs) and/or floodways have been determined, users are encouraged to consult the Flood Profiles and Floodway Data and/or Summary of Sillwaret Elevations tables contained within the Flood insurance Study (FIS) report that accompanies this FIRM. Users should be aware that BFEs shown on the FIRM represent rounded whole-to-elevations. These BFEs are intended for flood insurance rating purposes only and node elevations are presented in the FIS report handle builtized in conjunction with the FIRM for purposes of construction and/or floodplain management.

Costal Base Flood Elevations shown on this map apply only landward of 0.0' Not American Vertical Datum of 1988 (NAVD8). Users of this FIRM should be awar that coastal flood elevations are also provided in the Summary of Sulfivater Elevations table in the Flood Insurance Study report for this jurisdiction. Elevations shown in th Summary of Sulfivater Elevations table should be used for construction and/ floodplain management purposes when they are higher than the elevations shown or be FIRM. his FIRM.

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Certain areas not in Special Flood Hazard Areas may be protected by **flood contro** structures. Refer to section 2.4 "Flood Protection Measures" of the Flood Insurano Study report for information on flood control structures for this jurisdiction.

The projection used in the proparation of this may was whiteveal Transvers Mercator (UTM) zona 13. The horizontal datum was NADB3, GRS30 spheroic Difference in datum, spheroit projection of urUM zonas zones used in the production of FIRMs for adjacent juridictions may result in slight positions differences in may feature across juridiction boundaries. These differences do no affect the accuracy of this FIRM.

Pood elevations on this map are referenced to the **North American Vartical Datum f 1988** (**NAVD88**). These flood elevations must be compared to structure and round elevations referenced to the same **vertical datum**. For information regarding conversion between the National Geodetic Vartical Datum of 1929 and the North Merician Vertical Datum of 1988, visit the National Geodetic Survey vebsite at thtp://www.ngs.nosa.gov/ or contact the National Geodetic Survey at the following dotress:

NGS Information Services NOAA, N/NGS12 National Geodetic Survey SSMC-3, #9202 1315 East-West Highway Silver Spring, MD 20910-3282

To obtain current elevation, description, and/or location information for **bench marks** shown on this map, please contact the Information Services Branch of the Nationa Seodetic Survey at (301) 713-3242 or visit its website at http://www.ngs.noaa.gov/.

Base Map information shown on this FIRM was provided in digital format by EI Pasc County, Colorado Springs Utilities, City of Fountain, Bureau of Land Management National Oceanic and Armospheric Administration, United States Geological Survey and Anderson Consulting Engineers, Inc. These data are current as of 2006.

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Panel Locati	on Map	

available from local communities and the Colora-Water Conservation Board.

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Elevations determi ZONE AO Flood depths of 1	to 3 feet (usually sheet flow on sloping terrain); average
depths determined determined. ZONE AR Special Flood Hazz	d. For areas of alluvial fan flooding, velocities also rd Area Formerly protected from the 1% annual chance
flood by a flood co indicates that the protection from the	ntrol system that was subsequently decertified. Zone AR former flood control system is being restored to provide e 1% annual chance or greater flood.
ZONE A99 Area to be protection system	ted from 1% annual chance flood by a Federal flood n under construction; no Base Flood Elevations
ZONE V Coastal flood zon Elevations determined.	e with velocity hazard (wave action); no Base Flood ned.
ZONE VE Coastal flood zo Elevations determi	ne with velocity hazard (wave action); Base Flood ned.
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OTHER AREAS	to be outside the 0.2% annual chance floodplain.
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To determine if flood insurance agent or call the National Flood In	is available in this community, contact your insurance isurance Program at 1-800-638-6620.
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This Digital Flood Insurance Rate Map (DFIRM) was produced through a Cooperating Technical Partner (CTP) agreement between the State of Colorado Water Conservation Board (CWCB) and the Federal Emergency Management Agency (FEMA).

155

Additional Flood Hazard information and resource available from local communities and the Colorad Water Conservation Board.



NOTE: MAP AREA SHOWN ON THIS PANEL IS LOCATED WITHIN TOWNSHIP 13 SOUTH, RANGE 65 WEST, AND TOWNSHIP 14 SOUTH, RANGE 65 WEST.

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	ZONE AO	Flood depths of	1 to 3 feet (usually sheet flow on sloping terrain); average
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USDA Natural Resources Conservation Service Web Soil Survey National Cooperative Soil Survey



# Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
8	Blakeland loamy sand, 1 to 9 percent slopes	A	11.3	100.0%
Totals for Area of Intere	st		11.3	100.0%

## Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

# **Rating Options**

Aggregation Method: Dominant Condition Component Percent Cutoff: None Specified

USDA

Tie-break Rule: Higher

# Appendix B Hydrologic Calculations



## PALMER VILLAGE - EXISTING DRAINAGE SUMMARY

EXISTING BASIN SUMMARY TABLE								
Tributary	Area	Percent			t <sub>c</sub>	Q <sub>5</sub>	Q <sub>100</sub>	
Sub-basin	(acres)	Impervious	$C_5$	C <sub>100</sub>	(min)	(cfs)	(cfs)	
EX1	0.15	2%	0.08	0.35	7.9	0.04	0.4	
EX2	0.46	2%	0.08	0.35	8.1	0.2	1.2	
EX3	4.27	2%	0.08	0.35	14.2	1.2	9.0	
EX4	1.62	19%	0.22	0.45	17.9	1.1	4.0	
EX5	0.37	82%	0.75	0.85	5.0	1.4	2.7	
EX6	5.25	2%	0.08	0.35	14.4	1.5	11.1	

EXISTING	EXISTING DESIGN POINT												
SUMMARY TABLE													
DP Q <sub>5</sub> Q <sub>100</sub>													
1	0.04	0.4											
2	0.2	1.2											
3	1.3	9.3											
4	1.3	4.9											
5 1.4 2.7													
6	1.5	11.1											

#### 6 IMPERVIOUS & COMPOSITE RUNOFF COEFFICIENT C,

# Subdivision: PALMER VILLAGE PALMER VILLAGE Location: Colorado Springs 2000-5149.01 RPD NQJ 1/30/20

	Total	P	AVED STR	REETS	UNDEV	ELOPED I	MEADOW	Basins Total
Basin ID	Area (ac)	% Imp.	Area (ac)	Weighted % Imp.	% Imp.	Area (ac)	Weighted % Imp.	Weighted % Imp.
EX1	0.15	100%	0.00	0.0%	2%	0.15	2.0%	2.0%
EX2	0.46	100%	0.00	0.0%	2%	0.46	2.0%	2.0%
EX3	4.27	100%	0.00	0.0%	2%	4.27	2.0%	2.0%
EX4	1.62	100%	0.27	17.0%	2%	1.35	1.7%	18.6%
EX5	0.37	100%	0.30	81.8%	2%	0.07	0.4%	82.1%
EX6	5.25	100%	0.00	0.0%	2%	5.25	2.0%	2.0%
TOTAL	12.12							6.7%

#### Table 6-6. Runoff Coefficients for Rational Method

(Source: UDFCD 2001)

in the second second							Runoff Co	efficients	1				
Characteristics	Impervious	2-y	ear	5-y	ear	10-1	year	25-1	/ear	50-1	year	100-	year
		HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D
Business													
Commercial Areas	95	0.79	0.80	0.81	0.82	0.83	0.84	0.85	0.87	0.87	0.88	0.88	0.89
Neighborhood Areas	70	0.45	0.49	0.49	0.53	0.53	0.57	0.58	0.62	0.60	0.65	0.62	0.68
Residential													
1/8 Acre or less	65	0.41	0.45	0.45	0.49	0.49	0.54	0.54	0.59	0.57	0.62	0.59	0.65
1/4 Acre	40	0.23	0.28	0.30	0.35	0.36	0.42	0.42	0.50	0.46	0.54	0.50	0.58
1/3 Acre	30	0.18	0.22	0.25	0.30	0.32	0.38	0.39	0.47	0.43	0.52	0.47	0.57
1/2 Acre	25	0.15	0.20	0.22	0.28	0.30	0.36	0.37	0.46	0.41	0.51	0.46	0.56
1 Acre	20	0.12	0.17	0.20	0.26	0.27	0.34	0.35	0.44	0.40	0.50	0.44	0.55
Industrial										-			
Light Areas	80	0.57	0.60	0.59	0.63	0.63	0.66	0.66	0.70	0.68	0.72	0.70	0.74
Heavy Areas	90	0.71	0.73	0.73	0.75	0.75	0.77	0.78	0.80	0.80	0.82	0.81	0.83
Parks and Cemeteries	7	0.05	0.09	0.12	0.19	0.20	0.29	0.30	0.40	0.34	0.46	0.39	0.52
Playgrounds	13	0.07	0.13	0.16	0.23	0.24	0.31	0.32	0.42	0.37	0.48	0.41	0.54
Railroad Yard Areas	40	0.23	0.28	0.30	0.35	0.36	0.42	0.42	0.50	0.46	0.54	0.50	0.58
Undeveloped Areas													
Historic Flow Analysis Greenhelts, Agriculture	2	0.03	0.05	0.09	0.16	0.17	0.26	0.26	0.38	0.31	0.45	0.36	0.51
Pasture/Meadow	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50
Forest	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50
Exposed Rock	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Offsite Flow Analysis (when	45	0.00	0.24		0.07	0.00				0.40	0.55	0.51	0.50
landuse is undefined)		0.26	0.31	0.32	0.37	0.38	0.44	0.44	0.51	0.48	0.55	0.51	0.59
Streets													
Paved	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Gravel	80	0.57	0.60	0.59	0.63	0.63	0.66	0.66	0.70	0.68	0.72	0.70	0.74
Drive and Walke	100	0.90	0.90	0.90	0.90	0.92	0.92	0.94	0.04	0.05	0.05	0.96	0.95
Roofs	90	0.05	0.03	0.50	0.50	0.52	0.72	0.78	0.80	0.95	0.95	0.90	0.90
Lawns	30	0.02	0.73	0.08	0.15	0.15	0.25	0.78	0.80	0.30	0.62	0.35	0.65

#### COMPOSITE RUNOFF COEFFICIENT CALCULATIONS

#### Subdivision: PALMER VILLAGE Location: Colorado Springs

#### Project Name: PALMER VILLAGE

Project No.: 2000-5149.01

Calculated By: RPD

Checked By: NQJ

Date: 1/30/20

		Basins Total	Hydr	ologic Soil (	Group	Lar	nd Use	Mino	r Coefficients	Majo	r Coefficients		
Basin ID	Total Area (ac)	Weighted % Imp.	Area A (ac)	Area B (ac)	Area C/D (ac)	Area Paved Streets (ac)	Area Undeveloped Meadow (ac)	C <sub>5,A,PAVED STREETS</sub>	C <sub>5,A</sub> , undeveloped meadow	C <sub>100,A,PAVED STREETS</sub>	C <sub>100,A</sub> , undeveloped meadow	Basins Total Weighted C <sub>5</sub>	Basins Total Weighted C <sub>100</sub>
EX1	0.15	2.0%	0.15	0.00	0.00	0.00	0.15	0.90	0.08	0.96	0.35	0.08	0.35
EX2	0.46	2.0%	0.46	0.00	0.00	0.00	0.46	0.90	0.08	0.96	0.35	0.08	0.35
EX3	4.27	2.0%	4.27	0.00	0.00	0.00	4.27	0.90	0.08	0.96	0.35	0.08	0.35
EX4	1.62	18.6%	1.62	0.00	0.00	0.27	1.35	0.90	0.08	0.96	0.35	0.22	0.45
EX5	0.37	82.1%	0.37	0.00	0.00	0.30	0.07	0.90	0.08	0.96	0.35	0.75	0.85
EX6	5.25	2.0%	5.25	0.00	0.00	0.00	5.25	0.90	0.08	0.96	0.35	0.08	0.35
TOTAL	12.12	6.7%	12.12	0.00	0.00	5%	95%					0.12	0.38

Table 6-6. Runoff Coefficients for Rational Method

(Source: UDFCD 2001)

Land Use or Surface	0						Runoff Co	efficients					-
Characteristics	Impervious	2.9	rear	5-1	rear	10-	year	25-	year	50-	year	100	year
		HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D
Business		10000000000							1.1.1.1.1.1.1.1.1				
Commercial Areas	95	0.79	0.80	0.81	0.82	0.83	0.84	0.85	0.87	0.87	0.88	0.88	0.89
Neighborhood Areas	70	0.45	0.49	0.49	0.53	0.53	0.57	0.58	0.62	0.60	0.65	0.62	0.68
Residential					-		-					<u> </u>	
1/8 Acre or less	65	0.41	0.45	0.45	0.49	0.49	0.54	0.54	0.59	0.57	0.62	0.59	0.65
1/4 Acre	40	0.23	0.28	0.30	0.35	0.36	0.42	0.42	0.50	0.46	0.54	0.50	0.58
1/3 Acre	30	0.18	0.22	0.25	0.30	0.32	0.38	0.39	0.47	0.43	0.52	0.47	0.57
1/2 Acre	25	0.15	0.20	0.22	0.28	0.30	0.36	0.37	0.46	0.41	0.51	0.46	0.56
1 Acre	20	0.12	0.17	0.20	0.26	0.27	0.34	0.35	0.44	0.40	0.50	0.44	0.55
Industrial													
Light Areas	80	0.57	0.60	0.59	0.63	0.63	0.66	0.66	0.70	0.68	0.72	0.70	0.74
Heavy Areas	90	0.71	0.73	0.73	0.75	0.75	0.77	0.78	0.80	0.80	0.82	0.81	0.83
Parks and Cemeteries	7	0.05	0.09	0.12	0.19	0.20	0.29	0.30	0.40	0.34	0.46	0.39	0.52
Playgrounds	13	0.07	0.13	0.16	0.23	0.24	0.31	0.32	0.42	0.37	0.48	0.41	0.54
Railroad Yard Areas	40	0.23	0.28	0.30	0.35	0.36	0.42	0.42	0.50	0.46	0.54	0.50	0.58
Undeveloped Areas												-	
Historic Flow Analysis	2		0.07		0.16	0.17	0.75	0.25	0.30		0.45		
Greenberts, Agriculture	0	0.03	0.05	0.09	0.16	0.17	0.26	0.26	0.38	0.31	0.45	0.30	0.51
Fascule/Weadow	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50
Exported Bock	100	0.02	0.04	0.00	0.90	0.02	0.02	0.23	0.9/	0.30	0.95	0.95	0.96
Offsite Flow Analysis (when	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
landuse is undefined)	45	0.26	0.31	0.32	0.37	0.38	0.44	0.44	0.51	0.48	0.55	0.51	0.59
Streets				<u> </u>				-			<u> </u>	<u> </u>	
Paved	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Gravel	80	0.57	0.60	0.59	0.63	0.63	0.66	0.66	0.70	0.68	0.72	0.70	0.74
Drive and Walks	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Roofs	90	0.71	0.73	0.73	0.75	0.75	0.77	0.78	0.80	0.80	0.82	0.81	0.83
Lawns	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50

#### STANDARD FORM SF-2 TIME OF CONCENTRATION

Subdivision: PALMER VILLAGE

Location: Colorado Springs

# Project Name: PALMER VILLAGE Project No.: 2000-5149.01

,	
Calculated By:	RPD
Checked By:	NQJ
Date:	1/30/20

		SUB-	BASIN			INIT	IAL/OVER	LAND			TRAVEL TI	ME			tc CHECK		
		D/	ATA				(T <sub>i</sub> )				(T <sub>t</sub> )			(L	JRBANIZED BA	(SINS)	FINAL
BASIN	D.A.	Hydrologic	Impervious	C <sub>5</sub>	C <sub>100</sub>	L	S <sub>o</sub>	t i	L <sub>t</sub>	S <sub>t</sub>	K	VEL.	t <sub>t</sub>	COMP. tc	TOTAL	Urbanized t <sub>c</sub>	t <sub>c</sub>
ID	(ac)	Soils Group	(%)			(ft)	(%)	(min)	(ft)	(%)		(ft/s)	(min)	(min)	LENGTH (ft)	(min)	(min)
EX1	0.15	А	2%	0.08	0.35	50	5.0%	7.7	26	5.0%	10.0	2.2	0.2	7.9	76.0	25.9	7.9
EX2	0.46	А	2%	0.08	0.35	50	5.0%	7.7	56	5.0%	10.0	2.2	0.4	8.1	106.0	26.1	8.1
EX3	4.27	А	2%	0.08	0.35	50	7.8%	6.6	471	1.1%	10.0	1.0	7.6	14.2	521.0	33.9	14.2
EX4	1.62	А	19%	0.22	0.45	50	7.8%	5.7	643	0.8%	10.0	0.9	12.2	17.9	693.0	33.3	17.9
EX5	0.37	А	82%	0.75	0.85	0	N/A	N/A	189	0.5%	20.0	1.4	2.3	2.3	189.0	14.3	5.0
EX6	5.25	А	2%	0.08	0.35	50	3.0%	9.1	550	3.0%	10.0	1.7	5.3	14.4	600.0	31.4	14.4

NOTES:

1 - 1 + 1	_	$0.395(1.1-C_5)\sqrt{L_i}$	Envire (2	Table 6-2. NRCS Conve	eyance factors, K
$i_c - i_i + i_t$	Equation	$b_{i}^{-1} = \frac{S_{0}^{033}}{S_{0}^{033}}$	Equation 0-3	Type of Land Surface	Conveyance Factor, K
Where:				Heavy meadow	2.5
t = computed time of concentration (minutes)		Where:		Tillage/field	5
$i_e$ = computed time of concentration (initiates)		$t_i$ = overland (initial) flow time (minutes)		Short pasture and lawns	7
$t_i$ = overland (initial) flow time (minutes)		$C_5 =$ runoff coefficient for 5-year frequency (from Table 6-4) $L_1 =$ length of overland flow (ft)		Nearly bare ground	10
$t_t$ = channelized flow time (minutes).		$S_o =$ average slope along the overland flow path (ft/ft).		Grassed waterway	15
L. L.		L	101 TA 1020	Paved areas and shallow paved swales	20
$t_t = \frac{-t}{60K\sqrt{S_o}} = \frac{-t}{60V_t}$	Equation 6-4	$t_c = (26 - 17i) + \frac{-t}{60(14i + 9)\sqrt{S_r}}$	Equation 6-5		
Where:		Where:			
$r_r = \text{channelized flow time (travel time, min)}$ $L_r = \text{waterway length (ft)}$ $S_o = \text{waterway alope (ft)ft)}$ $V_r = \text{travel time velocity (ft)esc) = K \sqrt{S_o}$ K = NRCS conveyance factor (see Table 6-2).		$t_c = \mininum time of concentration for first design point when less than L_t = \text{length of channelized flow path (ft)}t = imperviousness (expressed as a decimal) S_t = \text{slope of the channelized flow path (ft/ft)}.$	te from Equation 6-1.		

Use a minimum te value of 5 minutes for urbanized areas and a minimum te value of 10 minutes for areas

that are not considered urban. Use minimum values even when calculations result in a lesser time of concentration.

#### STANDARD FORM SF-3

## STORM DRAINAGE SYSTEM DESIGN (RATIONAL METHOD PROCEDURE)

												(	INA IIC			JUIN	OULD	UKL)						
Subdivision: Location: Design Storm:	PALM Colora 5-Year	ER VILI ado Spr r	LAGE													Pro I Cal C	ject N Projec culate hecke	ame: t No.: d By: d By: Date:	PALN 2000 RPD NQJ 1/30/	1ER VII -5149. /20	LLAG	E		Figure 6-5. Colorado Springs Rainfall Inten
				DIRE	CT RUI	NOFF			T	OTAL I	RUNO	FF	0\	/ERLA	ND		P	IPE		TRAV	'EL TI	ME		0.0
STREET	Design Point	Basin ID	Area (Ac)	Runoff Coeff.	t <sub>c</sub> (min)	C*A (Ac)	l (in/hr)	Q (cfs)	tc (min)	C*A (ac)	l (in/hr)	Q (cfs)	Q <sub>overland</sub> (cfs)	C*A (ac)	Slope (%)	Q <sub>pipe</sub> (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	t <sub>t</sub> (min)	REMARKS	10 III Tenerally, 1 (Diff)
	1	EX1	0.15	0.08	7.9	0.01	4.49	0.04					0.04	0.01	1.90					468	1.4	5.7	BASIN EX1 FLOW AT DP1, OVERLAND FLOW TO DP3	Rainfa
	2	EX2	0.46	0.08	8.1	0.04	4.45	0.2					0.2	0.04	1.61					626	1.3	8.2	BASIN EX2 FLOW AT DP2, OVERLAND FLOW TO DP4	2.0 Deta Source: NOAA Atlas
		EX3	4.27	0.08	14.2	0.34	3.60	1.2															BASIN EX3 FLOW AT DP3 (LOCAL DEPRESSION)	1.0 Elevation = 6,840ft
	3								14.2	0.35	3.60	1.3											COMBINED DP1 AND EX3 FLOW AT DP3 (LOCAL DEPRESSION)	0 5 10 15 20 25 30 35 Duration, D (min
		EX4	1.62	0.22	17.9	0.35	3.26	1.1															BASIN EX4 FLOW AT DP4, FLOWS SOUTH ALONG C&G	IDF Equations
	4								17.9	0.39	3.26	1.3											COMBINED DP2 AND EX4 FLOW AT DP4	$I_{100} = -2.52 \ln(n\underline{D}) + 1$ $I_{50} = -2.25 \ln(n\underline{D}) + 11$
	5	EX5	0.37	0.75	5.0	0.28	5.17	1.4															BASIN EX5 FLOW AT DP5, FLOWS EAST ALONG C&G	$I_{15} = -2.00 \ln(n\underline{D}) + 10$
	6	EX6	5.25	0.08	14.4	0.42	3.59	1.5															BASIN EX6 FLOW AT DP6	$I_{50} = -1.75 \text{ m}(\underline{a}\underline{D}) + 0.3$ $I_5 = -1.50 \text{ m}(\underline{a}\underline{D}) + 7.50$
																								$I_2 = -1.19 \ln(\underline{aD}) + 6.0$ None: Values calculated by
																								equations may not precisely duplicate values read from t
																								1
																								]

Notes: Street and Pipe C\*A values are determined by Q/i using the catchment's intensity value.

sity Duration Frequency





#### STANDARD FORM SF-3 STORM DRAINAGE SYSTEM DESIGN (RATIONAL METHOD PROCEDURE)

Project Name: PALMER VILLAGE Project No.: 2000-5149. Calculated By: RPD

Design Storm:	Direct RUNOFF TOTAL RUNOFF OVERLAND PIPE														d By: Date:	NQJ 1/30/	/20						
				DIR	ECT RI	JNOFF			T(	OTAL F	RUNO	FF	0\	/ERLA	ND		PI	PE		TRAV	'EL TIN	ЛE	
Description	Design Point	Basin ID	Area (ac)	Runoff Coeff.	$t_c$ (min)	C*A (ac)	l (in/hr)	Q (cfs)	tc (min)	C*A (ac)	l (in/hr)	Q (cfs)	Q <sub>overland</sub> (cfs)	C*A (ac)	Slope (%)	Q <sub>pipe</sub> (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	$\mathbf{t}_{\mathrm{t}}$ (min)	REMARKS
	1	EX1	0.15	0.35	7.9	0.05	7.54	0.4					0.4	0.05	1.90					468	1.4	5.7	BASIN EX1 FLOW AT DP1, OVERLAND FLOW TO DP3
	2	EX2	0.46	0.35	8.1	0.16	7.47	1.2					1.2	0.16	1.61					626	1.3	8.2	BASIN EX2 FLOW AT DP2, OVERLAND FLOW TO DP4
		EX3	4.27	0.35	14.2	1.49	6.04	9.0															BASIN EX3 FLOW AT DP3 (LOCAL DEPRESSION)
	3								14.2	1.54	6.04	9.3											COMBINED DP1 AND EX3 FLOW AT DP3 (LOCAL DEPRESSION)
		EX4	1.62	0.45	17.9	0.73	5.47	4.0															BASIN EX4 FLOW AT DP4, FLOWS SOUTH ALONG C&G
	4								17.9	0.89	5.47	4.9											COMBINED DP2 AND EX4 FLOW AT DP4
	5	EX5	0.37	0.85	5.0	0.31	8.68	2.7															BASIN EX5 FLOW AT DP5, FLOWS EAST ALONG C&G
	6	EX6	5.25	0.35	14.4	1.84	6.02	11.1															BASIN EX6 FLOW AT DP6
									I														

Notes:

Street and Pipe C\*A values are determined by Q/i using the catchment's intensity value.

Subdivision: PALMER VILLAGE Location: Colorado Springs

#### PALRMER VILLAGE - PROPOSED DRAINAGE SUMMARY

		BASIN '	A' SUM	MARY T	ABLE		
Tributary	Area	Percent			t <sub>c</sub>	Q <sub>5</sub>	Q <sub>100</sub>
Sub-basin	(acres)	Impervious	C <sub>5</sub>	C <sub>100</sub>	(min)	(cfs)	(cfs)
EX1	0.15	0%	0.08	0.35	7.9	0.0	0.2
EX2	0.46	0%	0.08	0.35	8.1	0.2	0.7
A1	0.78	75%	0.65	0.77	5.5	2.6	5.1
A2	0.22	67%	0.63	0.76	7.8	0.6	1.3
A3	0.11	63%	0.60	0.74	6.2	0.3	0.7
A4	0.62	75%	0.65	0.76	5.2	2.0	4.0
A5	0.83	55%	0.50	0.65	7.0	2.0	4.2
A6	0.18	84%	0.74	0.84	7.9	0.6	1.1
A7	0.46	67%	0.60	0.73	5.8	1.3	2.7
A8	0.75	48%	0.44	0.61	7.8	1.5	3.5
A9	0.57	72%	0.66	0.77	6.9	1.8	3.5
A10	0.78	5%	0.12	0.38	9.4	0.4	2.1
A11	0.16	40%	0.41	0.60	9.8	0.3	0.6
A12	0.13	39%	0.40	0.59	7.8	0.2	0.6

	BASIN 'B' SUMMARY TABLE														
Tributary	Area	Percent			t <sub>c</sub>	Q <sub>5</sub>	Q <sub>100</sub>								
Sub-basin	(acres)	Impervious	C <sub>5</sub>	C <sub>100</sub>	(min)	(cfs)	(cfs)								
B1	0.61	55%	0.50	0.65	6.3	1.4	3.2								
B2	0.08	100%	0.90	0.96	5.0	0.4	0.6								
B3	0.12	87%	0.79	0.88	5.0	0.5	0.9								
B4	0.76	75%	0.66	0.77	5.9	2.5	4.9								
B5	0.66	53%	0.49	0.64	6.2	1.6	3.5								
B6	0.08	84%	0.77	0.87	5.0	0.3	0.6								
B7	0.13	88%	0.80	0.89	5.0	0.5	1.0								
B8	0.72	68%	0.60	0.72	5.5	2.2	4.4								
B9	0.31	2%	0.10	0.36	5.6	0.1	0.9								
B10	0.55	65%	0.59	0.72	6.4	1.6	3.2								
B11	0.55	3%	0.10	0.37	5.6	0.3	1.7								
B12	0.06	36%	0.37	0.57	5.0	0.1	0.3								
B13	0.18	39%	0.40	0.59	7.0	0.3	0.9								
B14	0.17	21%	0.25	0.48	5.6	0.2	0.7								
B15	0.17	11%	0.17	0.42	5.0	0.2	0.6								
B16	0.11	0%	0.08	0.35	5.0	0.1	0.3								

DESIGN	DESIGN POINT SUMMARY										
	TABLE										
Design Point	Q <sub>5</sub> (cfs)	Q <sub>100</sub> (cfs)									
EX1	0.04	0.2									
EX2	0.2	0.7									
1	2.3	4.9									
2	2.0	4.7									
3	3.0	6.2									
4	2.4	5.7									
4.1	4.8	9.4									
5	2.0	4.2 13.5 4.8 3.5									
5.1	6.7										
6	1.8										
7	1.5										
8	2.4	5.9									
8.1	8.8	15.0									
9	3.4	9.2									
9.1	11.9	23.9									
10	12.1	25.7									
11	0.3	0.6									
12	0.2	0.6									

DESIGN POINT SUMMARY TABLE										
Design Point	Q <sub>5</sub> (cfs)	Q <sub>100</sub> (cfs)								
15	1.4	3.2								
16	2.5	4.9								
17	1.7	3.6								
18	2.8	5.4								
18.1	4.2	7.8								
19	1.9	4.8								
20	2.2	4.4								
21	0.1	0.9								
22	1.6	3.2								
22.1	1.7	3.5								
23	2.6	5.6								
23.1	8.2	16.5								
24	1.0	3.2								
24.1	10.2	21.5								
25	10.4	22.9								
26	0.3	1.7								
27	0.1	0.3								
28	0.3	0.9								
29	0.2	0.7								
30	0.1	0.3								

2020 DRAINAGE AND BRIDGE FEES - PALMER VILLAGE												
Impervious	Drainage Fee Bridge Fee Feathergrass Feathergrass											
Acres (ac)	s (ac) (Per Imp. Acre) (Per Imp. Acre) Drainage Fee Bridge Fee											
5.67	\$19,698	\$8,057	\$111,688	\$45,683								

#### COMPOSITE % IMPERVIOUS CALCULATIONS

Subdivision: PALMER VILLAGE Location: Colorado Springs Project Name: PALMER VILLAGE

Project No.:	2514901
Calculated By:	RPD
Checked By:	
Date:	1/27/21

			Drives/Wal	ks		Roofs			Basins Total			
Basin ID	Total Area (ac)	% Imp.	Area (ac)	Weighted %	% Imp.	Area (ac)	Weighted	% Imp.	Area (ac)	Weighted %	Weighted %	
		1000		Imp.			% Imp.			Imp.	Imp.	
EX1	0.15	100%	0.00	0.0%	90%	0.00	0.0%	0%	0.15	0.0%	0.0%	
EX2	0.46	100%	0.00	0.0%	90%	0.00	0.0%	0%	0.46	0.0%	0.0%	
A1	0.78	100%	0.28	36.2%	90%	0.33	38.3%	0%	0.17	0.0%	/4.5%	
A2	0.22	100%	0.15	67.3%	90%	0.00	0.0%	0%	0.07	0.0%	67.3%	
A3	0.11	100%	0.07	63.3%	90%	0.00	0.0%	0%	0.04	0.0%	63.3%	
A4	0.62	100%	0.16	26.6%	90%	0.33	48.3%	0%	0.12	0.0%	74.8%	
A5	0.83	100%	0.21	24.8%	90%	0.28	29.9%	0%	0.35	0.0%	54.7%	
A6	0.18	100%	0.11	59.4%	90%	0.05	24.5%	0%	0.02	0.0%	83.9%	
A7	0.46	100%	0.16	34.5%	90%	0.17	32.7%	0%	0.13	0.0%	67.1%	
A8	0.75	100%	0.16	20.9%	90%	0.22	26.6%	0%	0.37	0.0%	47.5%	
A9	0.57	100%	0.32	54.9%	90%	0.11	17.4%	0%	0.15	0.0%	72.3%	
A10	0.78	100%	0.04	5.2%	90%	0.00	0.0%	0%	0.74	0.0%	5.2%	
A11	0.16	100%	0.06	40.5%	90%	0.00	0.0%	0%	0.09	0.0%	40.5%	
A12	0.13	100%	0.05	38.9%	90%	0.00	0.0%	0%	0.08	0.0%	38.9%	
B1	0.61	100%	0.13	21.6%	90%	0.22	33.0%	0%	0.25	0.0%	54.6%	
B2	0.08	100%	0.08	100.0%	90%	0.00	0.0%	0%	0.00	0.0%	100.0%	
B3	0.12	100%	0.10	87.0%	90%	0.00	0.0%	0%	0.02	0.0%	87.0%	
B4	0.76	100%	0.27	35.8%	90%	0.33	39.2%	0%	0.16	0.0%	75.0%	
B5	0.66	100%	0.15	23.0%	90%	0.22	30.0%	0%	0.29	0.0%	53.0%	
B6	0.08	100%	0.07	84.4%	90%	0.00	0.0%	0%	0.01	0.0%	84.4%	
B7	0.13	100%	0.11	87.9%	90%	0.00	0.0%	0%	0.02	0.0%	87.9%	
B8	0.72	100%	0.19	26.4%	90%	0.33	41.6%	0%	0.20	0.0%	68.0%	
B9	0.31	100%	0.01	2.2%	90%	0.00	0.0%	0%	0.30	0.0%	2.2%	
B10	0.55	100%	0.21	38.0%	90%	0.17	27.0%	0%	0.18	0.0%	65.0%	
B11	0.55	100%	0.02	2.8%	90%	0.00	0.0%	0%	0.54	0.0%	2.8%	
B12	0.06	100%	0.02	36.0%	90%	0.00	0.0%	0%	0.04	0.0%	36.0%	
B13	0.18	100%	0.07	39.3%	90%	0.00	0.0%	0%	0.11	0.0%	39.3%	
B14	0.17	100%	0.04	20.7%	90%	0.00	0.0%	0%	0.14	0.0%	20.7%	
B15	0.17	100%	0.02	11.0%	90%	0.00	0.0%	0%	0.15	0.0%	11.0%	
B16	0.11	100%	0.00	0.0%	90%	0.00	0.0%	0%	0.11	0.0%	0.0%	
SITE TOTAL	11.46									SITE	50.0%	
WEST POND	5.92									WEST POND	50.5%	
EAST POND	4.57									EAST POND	54.3%	

#### COMPOSITE RUNOFF COEFFICIENT CALCULATIONS

Subdivision: PALMER VILLAGE Location: Colorado Springs

Project Name: PALMER VILLAGE Project No.: 2514901 Calculated By: RPD Checked By:

Date: 1/27/21

			Hydr	ologic Soil	Group		Land Use		Minor	Coefficient	S	Major Coefficients				
Basin ID	Total Area (ac)	Basins Total Weighted % Imp.	Area A (ac)	Area B (ac)	Area C/D (ac)	Area Walks & Drives (ac)	Area Roofs (ac)	Area Lawns (ac)	C <sub>5,A,WALKS &amp; DRIVES</sub>	C <sub>5,A,ROOFS</sub>	$C_{5,A,LAWNS}$	C <sub>100,A,WALKS &amp; DRIVES</sub>	C <sub>100,A,ROOFS</sub>	C <sub>100,A,LAWNS</sub>	Basins Total Weighted C₅	Basins Total Weighted C <sub>100</sub>
EX1	0.15	0%	0.15	0.00	0.00	0.00	0.00	0.15	0.90	0.73	0.08	0.96	0.81	0.35	0.08	0.35
EX2	0.46	0%	0.46	0.00	0.00	0.00	0.00	0.46	0.90	0.73	0.08	0.96	0.81	0.35	0.08	0.35
A1	0.78	75%	0.78	0.00	0.00	0.28	0.33	0.17	0.90	0.73	0.08	0.96	0.81	0.35	0.65	0.77
A2	0.22	67%	0.22	0.00	0.00	0.15	0.00	0.07	0.90	0.73	0.08	0.96	0.81	0.35	0.63	0.76
A3	0.11	63%	0.11	0.00	0.00	0.07	0.00	0.04	0.90	0.73	0.08	0.96	0.81	0.35	0.60	0.74
A4	0.62	75%	0.62	0.00	0.00	0.16	0.33	0.12	0.90	0.73	0.08	0.96	0.81	0.35	0.65	0.76
A5	0.83	55%	0.83	0.00	0.00	0.21	0.28	0.35	0.90	0.73	0.08	0.96	0.81	0.35	0.50	0.65
A6	0.18	84%	0.18	0.00	0.00	0.11	0.05	0.02	0.90	0.73	0.08	0.96	0.81	0.35	0.74	0.84
A7	0.46	67%	0.46	0.00	0.00	0.16	0.17	0.13	0.90	0.73	0.08	0.96	0.81	0.35	0.60	0.73
A8	0.75	48%	0.75	0.00	0.00	0.16	0.22	0.37	0.90	0.73	0.08	0.96	0.81	0.35	0.44	0.61
A9	0.57	72%	0.57	0.00	0.00	0.32	0.11	0.15	0.90	0.73	0.08	0.96	0.81	0.35	0.66	0.77
A10	0.78	5%	0.78	0.00	0.00	0.04	0.00	0.74	0.90	0.73	0.08	0.96	0.81	0.35	0.12	0.38
A11	0.16	40%	0.16	0.00	0.00	0.06	0.00	0.09	0.90	0.73	0.08	0.96	0.81	0.35	0.41	0.60
A12	0.13	39%	0.13	0.00	0.00	0.05	0.00	0.08	0.90	0.73	0.08	0.96	0.81	0.35	0.40	0.59
B1	0.61	55%	0.61	0.00	0.00	0.13	0.22	0.25	0.90	0.73	0.08	0.96	0.81	0.35	0.50	0.65
B2	0.08	100%	0.08	0.00	0.00	0.08	0.00	0.00	0.90	0.73	0.08	0.96	0.81	0.35	0.90	0.96
B3	0.12	87%	0.12	0.00	0.00	0.10	0.00	0.02	0.90	0.73	0.08	0.96	0.81	0.35	0.79	0.88
B4	0.76	75%	0.76	0.00	0.00	0.27	0.33	0.16	0.90	0.73	0.08	0.96	0.81	0.35	0.66	0.77
B5	0.66	53%	0.66	0.00	0.00	0.15	0.22	0.29	0.90	0.73	0.08	0.96	0.81	0.35	0.49	0.64
B6	0.08	84%	0.08	0.00	0.00	0.07	0.00	0.01	0.90	0.73	0.08	0.96	0.81	0.35	0.77	0.87
B7	0.13	88%	0.13	0.00	0.00	0.11	0.00	0.02	0.90	0.73	0.08	0.96	0.81	0.35	0.80	0.89
B8	0.72	68%	0.72	0.00	0.00	0.19	0.33	0.20	0.90	0.73	0.08	0.96	0.81	0.35	0.60	0.72
B9	0.31	2%	0.31	0.00	0.00	0.01	0.00	0.30	0.90	0.73	0.08	0.96	0.81	0.35	0.10	0.36
B10	0.55	65%	0.55	0.00	0.00	0.21	0.17	0.18	0.90	0.73	0.08	0.96	0.81	0.35	0.59	0.72
B11	0.55	3%	0.55	0.00	0.00	0.02	0.00	0.54	0.90	0.73	0.08	0.96	0.81	0.35	0.10	0.37
B12	0.06	36%	0.06	0.00	0.00	0.02	0.00	0.04	0.90	0.73	0.08	0.96	0.81	0.35	0.37	0.57
B13	0.18	39%	0.18	0.00	0.00	0.07	0.00	0.11	0.90	0.73	0.08	0.96	0.81	0.35	0.40	0.59
B14	0.17	21%	0.17	0.00	0.00	0.04	0.00	0.14	0.90	0.73	0.08	0.96	0.81	0.35	0.25	0.48
B15	0.17	11%	0.17	0.00	0.00	0.02	0.00	0.15	0.90	0.73	0.08	0.96	0.81	0.35	0.17	0.42
B16	0.11	0%	0.11	0.00	0.00	0.00	0.00	0.11	0.90	0.73	0.08	0.96	0.81	0.35	0.08	0.35
				L												
TOTAL	11.46	50.0%	11.46	0.00	0.00	3.24	2.76	5.45							0.47	0.63
### STANDARD FORM SF-2 TIME OF CONCENTRATION

Subdivision: PALMER VILLAGE Location: Colorado Springs

Project Name:	PALMER VILLAGE
Project No.:	2514901
Calculated By:	RPD
Checked By:	
Date:	1/27/21

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		SUB-	BASIN			INIT	IAL/OVER	LAND			TRAVEL TIM	ЛЕ					
		DA	ATA				(T <sub>i</sub> )				(T <sub>t</sub> )			(L	JRBANIZED BA	(SINS)	FINAL
BASIN	D.A.	Hydrologic	Impervious	C <sub>5</sub>	C <sub>100</sub>	L	S <sub>o</sub>	t <sub>i</sub>	L <sub>t</sub>	S <sub>t</sub>	K	VEL.	t <sub>t</sub>	COMP. t <sub>c</sub>	TOTAL	Urbanized $t_c$	t <sub>c</sub>
ID	(ac)	Soils Group	(%)			(ft)	(%)	(min)	(ft)	(%)		(ft/s)	(min)	(min)	LENGTH (ft)	(min)	(min)
EX1	0.15	A	0%	0.08	0.35	50	5.0%	7.7	26	5.0%	10.0	2.2	0.2	7.9	76.0	26.2	7.9
EX2	0.46	A	0%	0.08	0.35	50	5.0%	7.7	56	5.0%	10.0	2.2	0.4	8.1	106.0	26.5	8.1
A1	0.78	A	75%	0.65	0.77	87	5.0%	4.4	155	1.4%	20.0	2.4	1.1	5.5	242.0	14.4	5.5
A2	0.22	A	67%	0.63	0.76	87	2.0%	6.3	180	1.0%	20.0	2.0	1.5	7.8	267.0	16.2	7.8
A3	0.11	A	63%	0.60	0.74	87	6.0%	4.7	180	1.0%	20.0	2.0	1.5	6.2	267.0	16.9	6.2
A4	0.62	A	75%	0.65	0.76	87	6.0%	4.2	150	1.6%	20.0	2.5	1.0	5.2	237.0	14.3	5.2
A5	0.83	A	55%	0.50	0.65	87	5.0%	5.9	150	1.6%	20.0	2.5	1.0	7.0	237.0	17.9	7.0
A6	0.18	A	84%	0.74	0.84	99	1.0%	6.4	178	1.0%	20.0	2.0	1.5	7.9	277.0	13.2	7.9
A7	0.46	A	67%	0.60	0.73	87	5.5%	4.8	153	1.6%	20.0	2.5	1.0	5.8	240.0	15.7	5.8
A8	0.75	A	48%	0.44	0.61	90	4.5%	6.8	115	1.1%	20.0	2.1	0.9	7.8	205.0	19.1	7.8
A9	0.57	A	72%	0.66	0.77	87	3.0%	5.2	200	1.0%	20.0	2.0	1.7	6.9	287.0	15.5	6.9
A10	0.78	A	5%	0.12	0.38	50	15.0%	5.1	325	0.7%	15.0	1.3	4.3	9.4	375.0	31.8	9.4
A11	0.16	A	40%	0.41	0.60	90	2.0%	9.4	55	1.0%	20.0	2.0	0.5	9.8	145.0	19.7	9.8
A12	0.13	A	39%	0.40	0.59	20	2.0%	4.5	280	0.5%	20.0	1.4	3.3	7.8	300.0	24.0	7.8
B1	0.61	А	55%	0.50	0.65	97	8.0%	5.4	105	1.0%	20.0	2.0	0.9	6.3	202.0	17.8	6.3
B2	0.08	А	100%	0.90	0.96	12	2.0%	1.0	182	2.3%	20.0	3.1	1.0	2.0	194.0	9.9	5.0
B3	0.12	А	87%	0.79	0.88	12	2.0%	1.5	190	2.3%	20.0	3.0	1.0	2.6	202.0	12.2	5.0
B4	0.76	А	75%	0.66	0.77	120	6.0%	4.9	183	2.0%	20.0	2.8	1.1	5.9	303.0	14.4	5.9
B5	0.66	А	53%	0.49	0.64	97	8.0%	5.5	103	1.6%	20.0	2.5	0.7	6.2	200.0	17.8	6.2
B6	0.08	А	84%	0.77	0.87	12	2.0%	1.6	160	2.5%	20.0	3.2	0.8	2.5	172.0	12.5	5.0
B7	0.13	А	88%	0.80	0.89	12	2.0%	1.5	170	2.5%	20.0	3.2	0.9	2.4	182.0	11.9	5.0
B8	0.72	А	68%	0.60	0.72	97	9.0%	4.3	145	1.0%	20.0	2.0	1.2	5.5	242.0	15.7	5.5
B9	0.31	А	2%	0.10	0.36	15	10.0%	3.3	365	3.0%	15.0	2.6	2.3	5.6	380.0	29.4	5.6
B10	0.55	А	65%	0.59	0.72	87	5.0%	5.1	155	1.0%	20.0	2.0	1.3	6.4	242.0	16.4	6.4
B11	0.55	А	3%	0.10	0.37	15	2.0%	5.5	40	33.0%	15.0	8.6	0.1	5.6	55.0	25.6	5.6
B12	0.06	А	36%	0.37	0.57	20	2.0%	4.7	19	2.5%	20.0	3.2	0.1	4.8	39.0	20.0	5.0
B13	0.18	A	39%	0.40	0.59	20	2.0%	4.5	450	2.2%	20.0	3.0	2.5	7.0	470.0	22.8	7.0
B14	0.17	А	21%	0.25	0.48	20	2.0%	5.5	20	2.0%	20.0	2.8	0.1	5.6	40.0	22.7	5.6
B15	0.17	А	11%	0.17	0.42	20	25.0%	2.6	35	25.0%	15.0	7.5	0.1	2.7	55.0	24.2	5.0
B16	0.11	А	0%	0.08	0.35	15	10.0%	3.3	150	1.5%	15.0	1.9	1.3	4.7	165.0	28.2	5.0

bdivision:	PALM	ER VILL	AGE													Proj F	ect N Projec	ame: t No.:	PALM 2514	IER VILI 90 <u>1</u>	LAGE		
Location:	Colora 5-Year	ido Spr	ings													Calc	ulate	d By: d By:	RPD				
gii 0.01	0.02																10000	Date:	1/27/	21			
<b></b>				DIREC	T RUI	NOFF			TC	DTAL F	RUNO	FF	S	STREET	ſ		PI	PE		TRAVE	LTIM	E	
																			es)				
STREET	Design Point	Basin ID	Area (Ac)	Runoff Coeff.	t <sub>c</sub> (min)	C*A (Ac)	l (in/hr)	Q (cfs)	tc (min)	C*A (ac)	l (in/hr)	Q (cfs)	Ostreet (cfs)	C*A (ac)	Slope (%)	Opipe (cfs)	C* A (ac)	Slope (%)	Pipe Size (inche	Length (ft)	Velocity (fps)	t <sub>t</sub> (min)	REMARKS
	EX1	EX1	0.15	0.08	7.9	0.01	4.49	0.0															OFFSITE BASIN EX1 FLOW @ DPEX1, FLOW INTO BASIN A1 (ROUTED IN SF2)
	EX2	EX2	0.46	0.08	8.1	0.04	4.45	0.2															BASIN EX2 FLOW @ DPEX2, FLOW INTO BASIN A2 (ROUTED IN SF2)
	1	A1	0.78	0.65	5.5	0.51	5.03	2.6	7.9	0.52	4.49	2.3	2.3	0.52	1.13					170	2.1	1.3	BASIN A1 & DPEX1 FLOW @ DP1, C&G FLOW TO DP3
		A2	0.22	0.63	7.8	0.14	4.51	0.6															BASIN A2 FLOW @ DP3 (ROUTED IN SF2)
		A3	0.11	0.60	6.2	0.07	4.85	0.3							BASIN A3 FLOW @ DP4 (ROUTED IN SF2)								
	2	A4	0.62	0.65	5.2	0.40	5.10	2.0	8.1	0.44	4.45	2.0	2.0	0.44	1.13					170	2.1	1.3	BASIN A4 & DPEX2 FLOW @ DP2, C&G TO DP4
	3			_			_		7.8	0.66	4.51	3.0				3.0	0.66	1.0	18	5	5.1	0.0	DP1 & BASIN A2 FLOW CAPTURED IN DBL. DENVER TYPE 16 COMBO INLET (SUMP), PIPE TO DP4.1
	4								6.6	0.51	4.76	2.4	0.5	0.11	1.13	1.9	0.40	1.0	18	60 31	2.1 4.4	0.5 0.1	DP4 FLOW-BY, C&G FLOW TO DP6 BASIN A3 & DP2 FLOW CAPTURED IN DBL. DENVER TYPE 16 COMBO INLET (ON-GRADE), PIPE TO DP4.1
	4.1								7.8	1.06	4.50	4.8				4.8	4.50	0.8	24	110	5.2	0.4	COMBINED DP3&DP4 CAPTURED FLOW, PIPE FLOW TO DP5.1
	5	A5	0.83	0.50	7.0	0.42	4.67	2.0	7.0	0.42	4.67	2.0	0.4	0.08	0.66	1.6	0.34	0.8	24	115 5	1.6 3.9	1.2 0.0	DP5 FLOW-BY, C&G FLOW TO DP8 BASIN AS FLOW @ DP5, CAPTURED IN DBL DENVER TYPE 16 COMBO INLET (ON-GRADE), PIPE TO 5.1
	5.1								7.8	1.48	4.50	6.7				6.7	1.48	0.8	30	50	5.6	0.1	DP4.1 & DP5 FLOW @ DP5.1, PIPE FLOW TO DP8.1
		A6	0.18	0.74	7.9	0.14	4.49	0.6															BASIN A6 FLOW @ DP8 (ROUTED IN SF2)
	6	A7	0.46	0.60	5.8	0.27	4.94	1.3	7.0	0.38	4.66	1.8	1.8	0.38	1.13					130	2.1	1.0	BASIN A7 FLOW & DP4 FLOW-BY @ DP6, C&G FLOW TO DP9
	7	A8	0.75	0.44	7.8	0.33	4.51	1.5	7.8	0.33	4.50	1.5	1.5	0.33	1.00					100	2.0	0.8	BASIN A8 FLOW @ DP7, C&G FLOW TO DP8
	8								8.6	0.55	4.36	2.4				2.4	0.55	0.5	30	5	3.5	0.0	BASIN A6, DP5 & DP7 FLOW @ DP8, CAPTURED BY TRP DENVER TYPE 16 COMBO INLET (SUMP), PIPE FLOW TO DP8.1
	8.1								8.6	2.03	4.35	8.8				8.8	2.03	0.5	30	50	2.0	0.4	DP5.1 & DP8 FLOW @ DP8.1, PIPE FLOW TO DP9.1
	9	A9	0.57	0.66	6.9	0.38	4.69	1.8	8.1	0.76	4.45	3.4				3.4	0.76	1.3	30	5	5.5	0.0	DP6, DP8 FLOW-BY & BASIN A9 FLOW @ DP9, CAPTURED BY TRP. DENVER TYPE 16 COMBO INLET (SUMP), PIPE FLOW TO DP9.1
	9.1						_		9.0	2.79	4.28	11.9				11.9	2.79	1.3	30	18	7.9	0.0	DP8.1 & DP9 FLOW @ DP9.1, PIPE FLOW TO DP10 (POND A)
	10	A10	0.78	0.12	9.4	0.09	4.22	0.4	9.4	2.88	4.22	12.1											BASIN A1-10 FLOW @ DP10, TOTAL FLOW ENTERING POND A
	11	A11	0.16	0.41	9.8	0.07	4.15	0.3															BASIN A11 FLOW, FOLLOWS HISTORIC DRAINAGE PATTERNS TO CONSTITUTION AVENUE @ DP11
	12	A12	0.13	0.40	7.8	0.05	4.50	0.2															BASIN A12 FLOW, FOLLOWS HISTORIC DRAINAGE PATTERNS TO CONSTITUTION AVENUE @ DP12

odivision:	n: PALMER VILLAGE												Proj P	ect Na roject	me: No.:	PALM 25149	ER VILI 901	AGE									
Location: gn Storm:	Colora 5-Year	ido Spr	ings													Calc Ch	ulateo neckeo	d By: d By:	RPD								
-																	C	ate:	1/27/.	21							
				DIREC	CT RUN	NOFF			TC	DTAL R	UNOF	F	S	TREET			PI	PE		TRAVE	L TIM	E					
STREET	Design Point	Basin ID	Area (Ac)	Runoff Coeff.	t <sub>c</sub> (min)	C*A (Ac)	l (in/hr)	Q (cfs)	tc (min)	C*A (ac)	l (in/hr)	Q (cfs)	Ostreet (cfs)	C*A (ac)	Slope (%)	Q <sub>pipe</sub> (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	t <sub>t</sub> (min)	REMARKS				
	15	B1	0.61	0.50	6.3	0.30	4.83	1.4	6.3	0.30	4.83	1.4	1.4	0.30	2.85					160	3.4	0.	BASIN B1 FLOW @ DP15, C&G FLOW TO DP17				
	17	B2	0.08	0.90	5.0	0.07	5.17	0.4	7.1	0.37	4.65	1.7	0.3	0.07	2.85	1.4	0.30	1.0	18	70 32	3.4 4.1	0. 0.	DP17 FLOW-BY, C&G FLOW TO DP19 BASIN B2 AND DP15 FLOW @ DP17, CAPTURED IN DBL: DENVER TYPE 16 COMBO INLET (ON-GRADE), PIPE TO DP18.1				
		B3	0.12	0.79	5.0	0.09	5.17	0.5														BASIN B3 FLOW @ DP18 (ROUTED IN SF2)					
	16	B4	0.76	0.66	5.9	0.50	4.91	2.5	5.9	0.50	4.91	2.5	2.5	0.50	2.85					185	3.4 0.9 BASIN B4 FLOW @ DP16, C&G FLOW TO DP18						
	18								6.8	0.59	4.70	2.8				2.8	0.59	1.4	18	5	5.5	0.	BASIN B3 & DP16 FLOW @ DP18, CAPTURED BY DBL. DENVER TYPE 16 COMBO INLET (SUMP), PIPE TO DP18.1				
	18.1								6.9	0.89	4.69	4.2				4.2	0.89	1.4	18	165	6.2	0.	DP17 & DP18 CAPTURED FLOW, PIPE FLOW TO DP22.1				
	19	B5	0.66	0.49	6.2	0.32	4.85	1.6	6.2	0.39	4.85	1.9	0.7	0.14	2.85	1.2	0.25	0.9	18	92 92	3.4 3.7	0. 0.	DP19 FLOW-BY, C&G FLOW TO DP24 BASIN B5 & DP17 FLOW-BY @ DP19, CAPTURED IN SINGLE DENVER TYPE 16 COMBO INLET (ON-GRADE), PIPE TO DP24.1				
		B6	0.08	0.77	5.0	0.06	5.17	0.3															BASIN B6 FLOW AT DP24 (ROUTED IN SF2)				
		B7	0.13	0.80	5.0	0.10	5.17	0.5														_	BASIN B7 FLOW AT DP23 (ROUTED IN SF2)				
	20	B8	0.72	0.60	5.5	0.43	5.02	2.2	5.5	0.43	5.02	2.2	2.2	0.43	2.85					125	3.4	0.	BASIN 88 FLOW @ DP20, C&G FLOW TO DP23				
	21	B9	0.31	0.10	5.6	0.03	4.99	0.1	5.6	0.03	4.99	0.1				0.1	0.03	0.5	18	147	1.6	1.	BASIN B9 FLOW @ DP21, CAPTURED IN TYPE C INLET (SUMP), PIPED TO DP22.1				
	22	B10	0.55	0.59	6.4	0.33	4.80	1.6	6.4	0.33	4.80	1.6				1.6	0.33	1.0	18	20	4.2	0.	BASIN B10 FLOW @ DP22, CAPTURED BY DBL DENVER TYPE 16 COMBO INLET (SUMP), PIPE TO DP22.1				
	22.1								7.1	0.36	4.64	1.7				1.7	0.36	0.5	18	25	3.3	0.	COMBINED DP21 & DP22 CAPTURED FLOW, PIPE TO DP23.1				
	23								6.2	0.53	4.86	2.6				2.6	0.53	0.5	18	5	3.8	0.	BASIN B7 & DP20 FLOW @ DP23, CAPTURED IN DBL. DENVER TYPE 16 COMBO INLET (SUMP), PIPE TO DP23.1				
	23.1								7.3	1.78	4.60	8.2				8.2	1.78	0.5	24	32	5.1	0.	DP23 CAPTURED FLOW & DP22.1 FLOW, PIPE TO DP24.1				
	24								6.6	0.20	4.74	1.0				1.0	0.20	0.5	24	5	2.7	0.	BASIN B6 & DP19 FLOW-BY @ DP24, CAPTURED IN TRIPLE DENVER TYPE 16 COMBO INLET (SUMP), PIPE TO DP24.1				
	24.1								7.4	2.23	4.58	10.2				10.2	2.23	0.5	30	47	5.4	0.	COMBINED DP23.1 & DP24 FLOW, PIPE TO DP25				
	25	B11	0.55	0.10	5.6	0.06	4.99	0.3	7.6	2.29	4.55	10.4											DP24.1 AND BASIN B11 FLOW, TOTAL FLOW @ DP25 (POND B)				
	26	B12	0.06	0.37	5.0	0.02	5.17	0.1															BASIN B12 FLOW, FOLLOWS EX PATTERNS & FLOWS NORTH TO CONSTITUTION AVENUE @ DP26				
	27	B13	0.18	0.40	7.0	0.07	4.66	0.3															BASIN B13 FLOW, FOLLOWS EX PATTERNS & FLOWS NORTH TO CONSTITUTION AVENUE @ DP27				
	28	B14	0.17	0.25	5.6	0.04	5.00	0.2			_	_											BASIN B14 FLOW, FOLLOWS EX PATTERNS & FLOWS EAST OFF SITE @ DP28				
	29	B15	0.17	0.17	5.0	0.03	5.17	0.2			_												BASIN B15 FLOW, FOLLOWS EX PATTERNS & FLOWS EAST OFF SITE @ DP29				
	30	B16	0.11	0.08	5.0	0.01	5.17	0.1															BASIN B16 FLOW, SWALE CONVEYS FLOW OFFSITE EAST (FOLLLOWS HISTORIC PATTERNS) @ DP30				

Notes: Street and Pipe C\*A values are determined by Q/i using the catchment's intensity value.

sion: tion: orm:	PALM Colora 100-Y	ER VILL ado Spr ear	_AGE rings									-				Proj F Calc Cł	ect Na Project ulateo neckeo E	ime: No.: I By: I By: I By: Date:	PALM 25149 RPD 1/27/	IER VIL 201 21	LAGE						
				DIRE	CT RUN	IOFF			T	OTAL	RUNC	)FF	5	TREE	Г		PIF	ΡE		TRAVE	EL TIM	E					
TREE	Design Point	Basin ID	Area (ac)	Runoff Coeff.	t <sub>c</sub> (min)	C *A (ac)	l (in/hr)	Q (cfs)	tc (min)	C*A (ac)	l (in/hr)	Q (cfs)	Q <sub>street</sub> (cfs)	C*A (ac)	Slope (%)	Q <sub>pipe</sub> (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	t <sub>t</sub> (min)	REMARKS				
	EX1	EX1	0.15	0.35	7.9	0.05	4.49	0.2															OFFSITE BASIN EX1 FLOW @ DPEX1, FLOW INTO BASIN A1 (ROUTED IN SF2)				
	EX2	EX2	0.46	0.35	8.1	0.16	4.45	0.7															BASIN EX2 FLOW @ DPEX2, FLOW INTO BASIN A2 (ROUTED IN SF2)				
	1	A1	0.78	0.77	5.5	0.60	8.44	5.1	7.9	0.65	7.54	4.9	4.9	0.65	1.13					170	2.1	1.3	BASIN A1 & DPEX1 FLOW @ DP1, C&G FLOW TO DP3				
		A2	0.22	0.76	7.8	0.17	7.57	1.3															BASIN A2 FLOW @ DP3 (ROUTED IN SF2)				
		A3	0.11	0.74	6.2	0.08	8.15	0.7															BASIN A3 FLOW @ DP4 (ROUTED IN SF2)				
	2	A4	0.62	0.76	5.2	0.47	8.56	4.0	8.1	0.63	7.47	4.7	4.7	0.63 1.13 170 2.1 1.3 BASIN A4 & DPEX2 FLOW @ DP2, C&G TO DP4							BASIN A4 & DPEX2 FLOW @ DP2, C&G TO DP4						
	3								7.8	0.82	7.57	6.2				6.2	0.82	1.0	18	5	6.2	0.0	0.0 DP1 & BASIN A2 FLOW CAPTURED IN DB1_DENVER TYPE 16 COMBO INFT (SUMP)_PIPE TO DP4 1				
	4								6.6	0.71	7.99	5.7	2.3	0.28	1.13	3.4	0.43	1.0	18	60 31	2.1 5.3	0.5	DP4 FLOW-BY, C&G FLOW TO DP6 BASIN A3 & DP2 FLOW CAPTURED IN DBL DENVER TYPE 16 COMBO INLET (ON-GRADE), PIPE TO DP4.1				
	4.1								7.8	1.25	7.56	9.4				9.4	7.56	0.8	24	110	6.2	0.3	COMBINED DP3&DP4 CAPTURED FLOW, PIPE FLOW TO DP5.1				
	5	A5	0.83	0.65	7.0	0.54	7.85	4.2	7.0	0.54	7.85	4.2	1.5	0.20	0.66	2.7	0.34	0.8	24	115 5	1.6 4.4	1.2 0.0	DP5 FLOW-BY, C&G FLOW TO DP8 BASIN A5 FLOW @ DP5, CAPTURED IN DBL DENVER TYPE 16 COMBO INLET (ON-GRADE), PIPE TO 5.1				
	5.1								7.8	1.79	7.56	13.5				13.5	1.79	0.8	30	50	6.9	0.1	DP4.1 & DP5 FLOW @ DP5.1, PIPE FLOW TO DP8.1				
		A6	0.18	0.84	7.9	0.15	7.53	1.1															BASIN A6 FLOW @ DP8 (ROUTED IN SF2)				
	6	A7	0.46	0.73	5.8	0.33	8.29	2.7	7.0	0.61	7.82	4.8	4.8	0.61	1.13					130	2.1	1.0	BASIN A7 FLOW & DP4 FLOW-BY @ DP6, C&G FLOW TO DP9				
	7	A8	0.75	0.61	7.8	0.46	7.57	3.5	7.8	0.46	7.56	3.5	3.5	0.46	1.00					100	2.0	0.8	BASIN A8 FLOW @ DP7, C&G FLOW TO DP8				
	8								8.6	0.81	7.32	5.9	1.6	0.22	2.00	4.3	0.59	0.5	30	60 5	2.8 4.2	0.4	DP8 FLOW-BY, OVERTOPS CROWN TO DP9 BASIN A6, DP5 & DP7 FLOW @ DP8, CAPTURED BY TRP DENVER TYPE 16 COMBO INLET (SUMP), PIPE FLOW TO DP8.1				
	8.1								8.6	2.05	7.31	15.0				15.0	2.05	0.5	30	50	2.0	0.4	DP5.1 & DP8 FLOW @ DP8.1, PIPE FLOW TO DP9.1				
	9	A9	0.57	0.77	6.9	0.44	7.88	3.5	8.9	1.27	7.22	9.2				9.2	1.27	1.3	30	5	7.3	0.0	DP6, DP8 FLOW-BY & BASIN A9 FLOW @ DP9, CAPTURED BY TRP. DENVER TYPE 16 COMBO INLET (SUMP), PIPE FLOW TO DP9.1				
	9.1								9.0	3.32	7.19	23.9				23.9	3.32	1.3	30	18	9.6 0.0 DP8.1 & DP9 FLOW @ DP9.1, PIPE FLOW TO DP10 (POND A)						
	10	A10	0.78	0.38	9.4	0.30	7.08	2.1	9.4	3.62	7.08	25.7										BASIN A1-10 FLOW @ DP10, TOTAL FLOW ENTERING POND A					
	11	A11	0.16	0.60	9.8	0.09	6.97	0.6														BASIN A11 FLOW, FOLLOWS HISTORIC DRAINAGE PATTERNS TO CONSTITUTION AVENUE @ DP11					
	12	A12	0.13	0.59	7.8	0.08	7.56	0.6															BASIN A12 FLOW, FOLLOWS HISTORIC DRAINAGE PATTERNS TO CONSTITUTION AVENUE @ DP12				

in	PALM	IER VILLAGE Project Name: PALM Project No.: 2514														Proj	ect Na Project	ame:	25149	ER VIL	LAGE			
tio	: Color	ado Spi	rings									-				Calc	ulated	d By:	RPD					
orn	100-Y	ear										-				CI	neckeo r	d By:	1/27/	21				
_																		ate.						
				DIREC	CT RUN	IOFF			T	OTAL	RUNC	FF	S	TREET	Γ		PI	PE		TRAV	EL TIN	IE		
TRI	m Design Point	Basin ID	Area (ac)	Runoff Coeff.	t <sub>c</sub> (min)	C*A (ac)	l (in/hr)	Q (cfs)	tc (min)	C*A (ac)	l (in/hr)	Q (cfs)	O <sub>street</sub> (cfs)	C*A (ac)	Slope (%)	O <sub>pipe</sub> (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	t <sub>t</sub> (min)	REMARKS	
	15	B1	0.61	0.65	63	0.39	8 10	3.2	63	0.39	8 10	3.2	3.2	0.39	2.85					160	3.4	0.8	BASIN B1 FLOW @ DP15, C&G FLOW TO DP17	
	17	B2	0.08	0.96	5.0	0.07	8.68	0.6	7.1	0.46	7.80	3.6	1.3	0.17	2.85	23	0.29	1.0	18	70 32	3.4	0.3	DP17 FLOW-BY, C&G FLOW TO DP19 RASIN 82 AND DP15 FLOW @ DP17 CAPTURED IN DRI. DERIVER TYPE 16 COMBO INLET (ON-GRADE). PIPE TO DP18 1	
		D2	0.12	0.00	5.0	0.10	0 6 0	0.0								2.0								
_		53	0.12	0.00	5.0	0.10	0.00	0.7		0.50	0.05		4.9	0.59	2.85					185	3.4	0.9	BASIN BAFLOW @ DP16, C&G FLOW TO DP18	
	10	В4	0.76	0.77	5.9	0.59	8.25	4.9	5.9	0.59	8.25	4.9								_			0	
-	18								6.8	0.69	7.89	5.4				5.4	0.69	1.4	18	5	6.7	0.0	BASIN B3 & DP16 FLOW @ DP18, CAPTURED BY DBL. DENVER TYPE 16 COMBO INLET (SUMP), PIPE TO DP18.1	
-	18.1								6.9	0.98	7.88	7.8	2.7	0.34	2.85	7.8	0.98	1.4	18	165 92	7.3	0.4	DP17 & DP18 CAPTURED FLOW, PIPE FLOW TO DP22.1 DP19 FLOW-BY, C&G FLOW TO DP24	
_	19	B5	0.66	0.64	6.2	0.43	8.14	3.5	6.2	0.60	8.14	4.8				2.1 0.26 0.9 18 92 4.3 0.4 BASIN 55 & DP17 FLOW-BI, CAST LOW TO DP24 2.1 0.26 0.9 18 92 4.3 0.4 BASIN 55 & DP17 FLOW-BI @ DP19, CAPTURED IN SINGLE DENVER TYPE 16 COMBO INLET (ON-GRADE), PIPE TO DP24.1							BASIN B5 & DP17 FLOW-BY @ DP19, CAPTURED IN SINGLE DENVER TYPE 16 COMBO INLET (ON-GRADE), PIPE TO DP24.1	
_		B6	0.08	0.87	5.0	0.07	8.68	0.6															BASIN B6 FLOW AT DP24 (ROUTED IN SF2)	
		B7	0.13	0.89	5.0	0.11	8.68	1.0						0.50	0.05					405			BASIN B7 FLOW AT DP23 (ROUTED IN SF2)	
	20	B8	0.72	0.72	5.5	0.52	8.42	4.4	5.5	0.52	8.42	4.4	4.4	0.52	2.85					125	3.4	0.6	BASIN B8 FLOW @ DP20, L&G FLOW TO DP23	
	21	B9	0.31	0.36	5.6	0.11	8.38	0.9	5.6	0.11	8.38	0.9				0.9	0.11	0.5	18	147	2.8	0.9	BASIN B9 FLOW @ DP21, CAPTURED IN TYPE C INLET (SUMP), PIPED TO DP22.1	
	22	B10	0.55	0.72	6.4	0.40	8.07	3.2	6.4	0.40	8.07	3.2	0.6	0.08	1.00	2.6	0.32	1.0	18	65 20	2.0 4.9	0.5 0.1	DP22 FLOW-BY, C&G FLOW TO DP23 BASIN B10 FLOW @ DP22, CAPTURED BY DBL DENVER TYPE 16 COMBO INLET (SUMP), PIPE TO DP22.1	
	22.1								6.5	0.43	8.02	3.5				3.5	0.43	0.5	18	25	4.1	0.1	COMBINED DP21 & DP22 CAPTURED FLOW, PIPE TO DP23.1	
	23								6.9	0.71	7.86	5.6				5.6	0.71	0.5	18	5	4.6	0.0	BASIN B7, DP20 FLOW & DP22 FLOW-BY@ DP23, CAPTURED IN DBL. DENVER TYPE 16 COMBO INLET (SUMP), PIPE TO DP23.1	
	23.1								7.2	2.12	7.75	16.5				16.5	2.12	0.5	24	32	5.8	0.1	DP23 CAPTURED FLOW & DP22.1 FLOW, PIPE TO DP24.1	
	24								6.6	0.41	7.96	3.2				3.2	0.41	0.5	24	5	3.9	0.0	BASIN B6 & DP19 FLOW-BY @ DP24, CAPTURED IN TRIPLE DENVER TYPE 16 COMBO INLET (SUMP), PIPE TO DP24.1	
	24.1								7.3	2.79	7.71	21.5				21.5	2.79	0.5	30	47	6.4	0.1	COMBINED DP23.1 & DP24 FLOW, PIPE TO DP25	
	25	B11	0.55	0.37	5.6	0.20	8.38	1.7	7.5	2.99	7.67	22.9											DP24.1 AND BASIN B11 FLOW, TOTAL FLOW @ DP25 (POND B)	
	26	B12	0.06	0.57	5.0	0.03	8.68	0.3															BASIN B12 FLOW, FOLLOWS EX PATTERNS & FLOWS NORTH TO CONSTITUTION AVENUE @ DP26	
	27	B13	0.18	0.59	7.0	0.11	7.83	0.9															BASIN B13 FLOW, FOLLOWS EX PATTERNS & FLOWS NORTH TO CONSTITUTION AVENUE @ DP27	
	28	B14	0.17	0.48	5.6	0.08	8.40	0.7													BASIN B14 FLOW, FOLLOWS EX PATTERNS & FLOWS EAST OFF SITE @ DP28			
	29	B15	0.17	0.42	5.0	0.07	8.68	0.6										BASIN B15 FLOW, FOLLOWS EX PATTERNS & FLOWS EAST OFF SITE @ DP29						
	30	B16	0.11	0.35	5.0	0.04	8.68	0.3															BASIN B16 FLOW, SWALE CONVEYS FLOW OFFSITE EAST (FOLLLOWS HISTORIC PATTERNS) @ DP30	

Street and Pipe C\*A values are determined by Q/i using the catchment's intensity value.

# Appendix C Hydraulic Calculations



# **Channel Report**

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

# Alley Street Capacity - 1% CL - Allowable Spread - Edge of Pavement

User-defined		Highlighted	
Invert Elev (ft)	= 0.36	Depth (ft)	= 0.24
Slope (%)	= 1.00	Q (cfs)	= 6.000
N-Value	= 0.016	Area (sqft)	= 2.88
		Velocity (ft/s)	= 2.08
Calculations		Wetted Perim (ft)	= 24.00
Compute by:	Known Q	Crit Depth, Yc (ft)	= 0.25
Known Q (cfs)	= 6.00	Top Width (ft)	= 24.00
		EGL (ft)	= 0.31

(Sta, El, n)-(Sta, El, n)... ( 0.00, 1.00)-(8.00, 0.60, 0.016)-(20.00, 0.36, 0.016)-(32.00, 0.60, 0.016)-(40.00, 1.00, 0.016)



# **Channel Report**

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

# Alley Street Capacity - 1.55% CL - Allowable Spread - Edge of Pavement

User-defined		Highlighted	
Invert Elev (ft)	= 0.36	Depth (ft)	= 0.24
Slope (%)	= 1.55	Q (cfs)	= 8.000
N-Value	= 0.016	Area (sqft)	= 2.88
		Velocity (ft/s)	= 2.78
Calculations		Wetted Perim (ft)	= 24.00
Compute by:	Known Q	Crit Depth, Yc (ft)	= 0.28
Known Q (cfs)	= 8.00	Top Width (ft)	= 24.00
		EGL (ft)	= 0.36

(Sta, El, n)-(Sta, El, n)... ( 0.00, 1.00)-(8.00, 0.60, 0.016)-(20.00, 0.36, 0.016)-(32.00, 0.60, 0.016)-(40.00, 1.00, 0.016)



#### INLET MANAGEMENT

Worksheet Protected

INLET NAME	DP3	DP4	STREET CAPACITY @ DP4	DP8	DP9	DP24
Site Type (Urban or Rural)	URBAN	URBAN	URBAN	URBAN	URBAN	URBAN
Inlet Application (Street or Area)	STREET	STREET	STREET	STREET	STREET	STREET
Hydraulic Condition	In Sump	On Grade	On Grade	In Sump	In Sump	In Sump
Inlet Type	Denver No. 16 Combination	Denver No. 16 Combination		Denver No. 16 Combination	Denver No. 16 Combination	Denver No. 16 Combination
SER-DEFINED INPUT						
User-Defined Design Flows						
Minor Q <sub>Known</sub> (cfs)	3.0	2.4	2.4	2.4	3.4	1.0
Major Q <sub>Known</sub> (cts)	6.2	5.7	5.7	5.9	9.2	3.2
Bypass (Carry-Over) Flow from Upstream						
Receive Bypass Flow from:	No Bypass Flow Received	No Bypass Flow Received	No Bypass Flow Received	No Bypass Flow Received	No Bypass Flow Received	No Bypass Flow Received
Minor Bypass Flow Received, Q <sub>b</sub> (cfs)	0.0	0.0	0.0	0.0	0.0	0.0
Major Bypass Flow Received, Q <sub>b</sub> (cfs)	0.0	0.0	0.0	0.0	0.0	0.0
Watershed Characteristics						
Subcatchment Area (acres)						
Percent Impervious						
NRCS Soil Type						
Watershed Profile						
Overland Slope (ft/ft)						
Overland Length (ft)						
Channel Slope (ft/ft)						
Channel Length (ft)						
<b>v</b> 、/				•	•	•
Minor Storm Rainfall Input						
Design Storm Return Period, T <sub>r</sub> (years)						
One-Hour Precipitation, P1 (inches)						
Major Storm Rainfall Input						
Design Storm Return Period, 1, (years)						
One-nour Precipitation, P <sub>1</sub> (Inches)						
I CULATED OUTPUT						

Minor Total Design Peak Flow, Q (cfs)	3.0	2.4	2.4	2.4	3.4	1.0
Major Total Design Peak Flow, Q (cfs)	6.2	5.7	5.7	5.9	9.2	3.2
Minor Flow Bypassed Downstream, Q <sub>b</sub> (cfs)	N/A	0.5		N/A	N/A	N/A
Major Flow Bypassed Downstream, Qb (cfs)	N/A	2.3		N/A	N/A	N/A
Minor Storm (Calculated) Analysis of Flow	<u>Fime</u>					
C	N/A	N/A	N/A	N/A	N/A	N/A
C <sub>5</sub>	N/A	N/A	N/A	N/A	N/A	N/A
Overland Flow Velocity, Vi	N/A	N/A	N/A	N/A	N/A	N/A
Channel Flow Velocity, Vt	N/A	N/A	N/A	N/A	N/A	N/A
Overland Flow Time, Ti	N/A	N/A	N/A	N/A	N/A	N/A
Channel Travel Time, Tt	N/A	N/A	N/A	N/A	N/A	N/A
Calculated Time of Concentration, T <sub>c</sub>	N/A	N/A	N/A	N/A	N/A	N/A
Regional T <sub>c</sub>	N/A	N/A	N/A	N/A	N/A	N/A
Recommended T <sub>c</sub>	N/A	N/A	N/A	N/A	N/A	N/A
T <sub>c</sub> selected by User	N/A	N/A	N/A	N/A	N/A	N/A
Design Rainfall Intensity, I	N/A	N/A	N/A	N/A	N/A	N/A
Calculated Local Peak Flow, Qp	N/A	N/A	N/A	N/A	N/A	N/A
			•			
Major Storm (Calculated) Analysis of Flow 1	Time					
С	N/A	N/A	N/A	N/A	N/A	N/A
C <sub>5</sub>	N/A	N/A	N/A	N/A	N/A	N/A
Overland Flow Velocity, Vi	N/A	N/A	N/A	N/A	N/A	N/A
Channel Flow Velocity, Vt	N/A	N/A	N/A	N/A	N/A	N/A
Overland Flow Time, Ti	N/A	N/A	N/A	N/A	N/A	N/A
Channel Travel Time, Tt	N/A	N/A	N/A	N/A	N/A	N/A
Calculated Time of Concentration, T <sub>c</sub>	N/A	N/A	N/A	N/A	N/A	N/A
Regional T <sub>c</sub>	N/A	N/A	N/A	N/A	N/A	N/A
Recommended T <sub>c</sub>	N/A	N/A	N/A	N/A	N/A	N/A
T <sub>c</sub> selected by User	N/A	N/A	N/A	N/A	N/A	N/A
Design Rainfall Intensity, I	N/A	N/A	N/A	N/A	N/A	N/A
Calculated Local Peak Flow, Qp	N/A	N/A	N/A	N/A	N/A	N/A

#### INLET MANAGEMENT

Worksheet Protected

INI FT NAME	DP23	DP17	DP18	DP22	DP19	DP21
Site Type (Urban or Rural)	URBAN	LIRBAN	LIRBAN	LIRBAN	LIBBAN	RURAI
Inlet Application (Street or Area)	STREET	STREET	STREET	STREET	STREET	AREA
Hydraulic Condition	In Sump	On Grade		In Sump	On Grade	Swale
Inlet Type	Denver No. 16 Combination	Denver No. 16 Combination	CDOT Type C			
/·						
ISER-DEFINED INPUT						
User-Defined Design Flows						
Minor Q <sub>Known</sub> (cfs)	2.6	1.7	2.8	1.6	1.9	0.1
Major Q <sub>Known</sub> (cfs)	5.6	3.6	5.4	3.2	4.8	0.9
Bypass (Carry-Over) Flow from Upstream				No Description Description		
Minor Bypass Flow Irom:	No Bypass Flow Received	No Bypass Flow Received	No Bypass Flow Received			
Major Durgess Flow Received, Q <sub>b</sub> (cls)	0.0	0.0	0.0	0.0	0.0	0.0
Major Bypass Flow Received, Qb (cis)	0.0	0.0	0.0	0.0	0.0	0.0
Watershed Characteristics						
Subcatchment Area (acres)						
Percent Impervious						
NRCS Soil Type						
						•
Watershed Profile						
Overland Slope (ft/ft)						
Overland Length (ft)						
Channel Slope (ft/ft)						
Channel Length (ft)						
Minor Storm Rainfall Input						
Design Storm Return Period, 1, (years)						
One-Hour Precipitation, P1 (Inches)						
Major Storm Bainfall Input						
Design Storm Return Period T (years)						
One-Hour Precipitation P. (inches)						
one near recipitation, r (meneo)						
ALCULATED OUTPUT						
Minor Total Design Peak Flow, Q (cfs)	2.6	1.7	2.8	1.6	1.9	0.1
Major Total Design Peak Flow, Q (cfs)	5.6	3.6	5.4	3.2	4.8	0.9
Minor Elow Bypassed Downstream () (cfs)						
winter new bypassed bownstream, Qb (crs)	N/A	0.3	N/A	N/A	0.6	0.0

#### Minor Storm (Calculated) Analysis of Flow T

C	N/A	N/A	N/A	N/A	N/A	N/A
C <sub>5</sub>	N/A	N/A	N/A	N/A	N/A	N/A
Overland Flow Velocity, Vi	N/A	N/A	N/A	N/A	N/A	N/A
Channel Flow Velocity, Vt	N/A	N/A	N/A	N/A	N/A	N/A
Overland Flow Time, Ti	N/A	N/A	N/A	N/A	N/A	N/A
Channel Travel Time, Tt	N/A	N/A	N/A	N/A	N/A	N/A
Calculated Time of Concentration, T <sub>c</sub>	N/A	N/A	N/A	N/A	N/A	N/A
Regional T <sub>c</sub>	N/A	N/A	N/A	N/A	N/A	N/A
Recommended T <sub>c</sub>	N/A	N/A	N/A	N/A	N/A	N/A
T <sub>c</sub> selected by User	N/A	N/A	N/A	N/A	N/A	N/A
Design Rainfall Intensity, I	N/A	N/A	N/A	N/A	N/A	N/A
Calculated Local Peak Flow, Qp	N/A	N/A	N/A	N/A	N/A	N/A

#### Major Storm (Calculated) Analysis of Flow T

С	N/A	N/A	N/A	N/A	N/A	N/A
C <sub>5</sub>	N/A	N/A	N/A	N/A	N/A	N/A
Overland Flow Velocity, Vi	N/A	N/A	N/A	N/A	N/A	N/A
Channel Flow Velocity, Vt	N/A	N/A	N/A	N/A	N/A	N/A
Overland Flow Time, Ti	N/A	N/A	N/A	N/A	N/A	N/A
Channel Travel Time, Tt	N/A	N/A	N/A	N/A	N/A	N/A
Calculated Time of Concentration, T <sub>c</sub>	N/A	N/A	N/A	N/A	N/A	N/A
Regional T <sub>c</sub>	N/A	N/A	N/A	N/A	N/A	N/A
Recommended T <sub>c</sub>	N/A	N/A	N/A	N/A	N/A	N/A
T <sub>c</sub> selected by User	N/A	N/A	N/A	N/A	N/A	N/A
Design Rainfall Intensity, I	N/A	N/A	N/A	N/A	N/A	N/A
Calculated Local Peak Flow, Qp	N/A	N/A	N/A	N/A	N/A	N/A

#### INLET MANAGEMENT

Worksheet Protected

INLET NAME	DP5
Site Type (Urban or Rural)	URBAN
Inlet Application (Street or Area)	STREET
Hydraulic Condition	On Grade
Inlet Type	Denver No. 16 Combination

#### USER-DEFINED INPUT

User-Defined Design Flows	
Minor Q <sub>Known</sub> (cfs)	2.0
Major Q <sub>Known</sub> (cfs)	4.2
Bypass (Carry-Over) Flow from Upstream	
Receive Bypass Flow from:	No Bypass Flow Received
Minor Bypass Flow Received, Q <sub>b</sub> (cfs)	0.0
Major Bypass Flow Received, Q <sub>b</sub> (cfs)	0.0
Watershed Characteristics	
Subcatchment Area (acres)	
Percent Impervious	
NRCS Soil Type	
Watershed Profile	
Overland Slope (ft/ft)	
Overland Length (ft)	
Channel Slope (ft/ft)	
Channel Length (ft)	
Minor Storm Rainfall Input	
Design Storm Return Period, T <sub>r</sub> (years)	
One-Hour Precipitation, P1 (inches)	
Major Storm Rainfall Input	
Design Storm Return Period, T <sub>r</sub> (years)	
One Hour Presinitation B (inches)	

#### CALCULATED OUTPUT

Minor Total Design Peak Flow, Q (cfs)	2.0
Major Total Design Peak Flow, Q (cfs)	4.2
Minor Flow Bypassed Downstream, Q <sub>b</sub> (cfs)	0.4
Major Flow Bypassed Downstream, Q <sub>b</sub> (cfs)	1.5
Minor Storm (Calculated) Analysis of Flow T	
С	N/A
C <sub>5</sub>	N/A
Overland Flow Velocity, Vi	N/A
Channel Flow Velocity, Vt	N/A
Overland Flow Time, Ti	N/A
Channel Travel Time, Tt	N/A
Calculated Time of Concentration, T <sub>c</sub>	N/A
Regional T <sub>c</sub>	N/A
Recommended T <sub>c</sub>	N/A
T <sub>c</sub> selected by User	N/A
Design Rainfall Intensity, I	N/A
Calculated Local Peak Flow, Qp	N/A
Major Storm (Calculated) Analysis of Flow T	
C	N/A
C <sub>5</sub>	N/A
Overland Flow Velocity, Vi	N/A
Channel Flow Velocity, Vt	N/A
Overland Flow Time, Ti	N/A
Channel Travel Time, Tt	N/A
Calculated Time of Concentration, T <sub>c</sub>	N/A
Regional T <sub>c</sub>	N/A
Recommended T <sub>c</sub>	N/A
T <sub>c</sub> selected by User	N/A
Design Rainfall Intensity, I	N/A
Calculated Local Peak Flow, Qp	N/A





Design Information (Input)			MINOR	MAJOR	
Type of Inlet	Denver No. 16 Combination	Type =	Denver No. 1	6 Combination	7
Local Depression (additional to co	ntinuous gutter depression 'a' from above)	a <sub>local</sub> =	2.00	2.00	inches
Number of Unit Inlets (Grate or Cu	rb Opening)	No =	2	2	1
Water Depth at Flowline (outside of	of local depression)	Ponding Depth =	6.0	6.6	inches
Grate Information			MINOR	MAJOR	Override Depths
Length of a Unit Grate		L <sub>o</sub> (G) =	3.00	3.00	feet
Width of a Unit Grate		W <sub>o</sub> =	1.73	1.73	feet
Area Opening Ratio for a Grate (ty	pical values 0.15-0.90)	A <sub>ratio</sub> =	0.31	0.31	
Clogging Factor for a Single Grate	e (typical value 0.50 - 0.70)	C <sub>f</sub> (G) =	0.50	0.50	
Grate Weir Coefficient (typical value	ue 2.15 - 3.60)	C <sub>w</sub> (G) =	3.60	3.60	
Grate Orifice Coefficient (typical va	alue 0.60 - 0.80)	C <sub>0</sub> (G) =	0.60	0.60	1
Curb Opening Information			MINOR	MAJOR	-
Length of a Unit Curb Opening		L <sub>o</sub> (C) =	3.00	3.00	feet
Height of Vertical Curb Opening in	Inches	H <sub>vert</sub> =	6.50	6.50	inches
Height of Curb Orifice Throat in In-	ches	H <sub>throat</sub> =	5.25	5.25	inches
Angle of Throat (see USDCM Figu	ire ST-5)	Theta =	0.00	0.00	degrees
Side Width for Depression Pan (ty	pically the gutter width of 2 feet)	W <sub>p</sub> =	2.00	2.00	feet
Clogging Factor for a Single Curb	Opening (typical value 0.10)	$C_{f}(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (ty	pical value 2.3-3.7)	C <sub>w</sub> (C) =	3.70	3.70	
Curb Opening Orifice Coefficient (	typical value 0.60 - 0.70)	C <sub>0</sub> (C) =	0.66	0.66	
Low Head Performance Reducti	on (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth		d <sub>Grate</sub> =	0.523	0.569	ft
Depth for Curb Opening Weir Equ	ation	d <sub>Curb</sub> =	0.33	0.38	ft
Combination Inlet Performance Re	eduction Factor for Long Inlets	RF <sub>Combination</sub> =	0.71	0.77	1
Curb Opening Performance Redu	ction Factor for Long Inlets	RF <sub>Curb</sub> =	1.00	1.00	1
Grated Inlet Performance Reduction	on Factor for Long Inlets	RF <sub>Grate</sub> =	0.71	0.77	
			MINOR	MAJOR	
Total Inlet Interception Ca	nacity (assumes clogged condition)	0. =	6.2	7.9	cfs
		• • • • • • • • • • • • • • • • • • •	0.2	1.3	
iniet Capacity IS GOOD for Mind	or and major Storms(>Q PEAK)	Q PEAK REQUIRED =	3.0	6.2	CIS



# INLET ON A CONTINUOUS GRADE





Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	Denver No. 1	6 Combination	
Local Depression (additional to continuous gutter depression 'a')	a <sub>LOCAL</sub> =	2.0	2.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	2	2	
Length of a Single Unit Inlet (Grate or Curb Opening)	L <sub>o</sub> =	3.00	3.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W <sub>o</sub> =	1.73	1.73	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C <sub>f</sub> -G =	0.50	0.50	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C <sub>f</sub> -C =	0.10	0.10	
Street Hydraulics: WARNING: Q > ALLOWABLE Q FOR MAJOR STORM		MINOR	MAJOR	_
Total Inlet Interception Capacity	Q =	1.9	3.4	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q <sub>b</sub> =	0.5	2.3	cfs
Capture Percentage = Q <sub>a</sub> /Q <sub>o</sub> =	C% =	80	60	%



# INLET ON A CONTINUOUS GRADE





Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	Denver No. 16	6 Combination	
Local Depression (additional to continuous gutter depression 'a')	a <sub>LOCAL</sub> =	2.0	2.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	2	2	
Length of a Single Unit Inlet (Grate or Curb Opening)	L <sub>o</sub> =	3.00	3.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W <sub>o</sub> =	1.73	1.73	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C <sub>f</sub> -G =	0.50	0.50	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	$C_{f}-C =$	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'	_	MINOR	MAJOR	_
Total Inlet Interception Capacity	Q =	1.6	2.7	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q <sub>b</sub> =	0.4	1.5	cfs
Capture Percentage = Q <sub>a</sub> /Q <sub>o</sub> =	C% =	82	64	%





Design Information (Input)	r		MINOR	MAIOR	
Type of Inlet	Denver No. 16 Combination	Type -	Denver No. 1	16 Combination	
Local Depression (additional to co	ontinuous gutter depression 'a' from above)	a <sub>local</sub> =	2.00	2.00	inches
Number of Unit Inlets (Grate or C	urb Opening)	No =	3	3	
Water Depth at Flowline (outside	of local depression)	Ponding Depth =	4.9	4.9	inches
Grate Information			MINOR	MAJOR	Override Depths
Length of a Unit Grate		L <sub>o</sub> (G) =	3.00	3.00	feet
Width of a Unit Grate		W <sub>o</sub> =	1.73	1.73	feet
Area Opening Ratio for a Grate (t	ypical values 0.15-0.90)	A <sub>ratio</sub> =	0.31	0.31	
Clogging Factor for a Single Grate	e (typical value 0.50 - 0.70)	$C_{f}(G) =$	0.50	0.50	
Grate Weir Coefficient (typical val	lue 2.15 - 3.60)	C <sub>w</sub> (G) =	3.60	3.60	1
Grate Orifice Coefficient (typical v	value 0.60 - 0.80)	C <sub>o</sub> (G) =	0.60	0.60	1
Curb Opening Information			MINOR	MAJOR	-
Length of a Unit Curb Opening		$L_{o}(C) =$	3.00	3.00	feet
Height of Vertical Curb Opening in	n Inches	H <sub>vert</sub> =	6.50	6.50	inches
Height of Curb Orifice Throat in In	nches	H <sub>throat</sub> =	5.25	5.25	inches
Angle of Throat (see USDCM Fig	ure ST-5)	Theta =	0.00	0.00	degrees
Side Width for Depression Pan (ty	pically the gutter width of 2 feet)	W <sub>p</sub> =	2.00	2.00	feet
Clogging Factor for a Single Curb	Opening (typical value 0.10)	$C_{f}(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (ty	vpical value 2.3-3.7)	$C_w(C) =$	3.70	3.70	
Curb Opening Orifice Coefficient	(typical value 0.60 - 0.70)	C <sub>o</sub> (C) =	0.66	0.66	
Low Head Performance Reduct	ion (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth		d <sub>Grate</sub> =	0.432	0.432	ft
Depth for Curb Opening Weir Equ	uation	d <sub>Curb</sub> =	0.24	0.24	ft
Combination Inlet Performance R	eduction Factor for Long Inlets	RF <sub>Combination</sub> =	0.46	0.46	
Curb Opening Performance Redu	ction Factor for Long Inlets	RF <sub>Curb</sub> =	0.90	0.90	
Grated Inlet Performance Reducti	ion Factor for Long Inlets	RF <sub>Grate</sub> =	0.46	0.46	
			MINOR	MAJOR	
Total Inlet Interception Ca	apacity (assumes clogged condition)	Q <sub>a</sub> =	4.3	4.3	cfs
WARNING: Inlet Capacity less t	han Q Peak for Major Storm	Q PEAK REQUIRED =	2.4	5.9	cfs





Design Information (Innut)			MINOD	MALOD	
Design information (input)	Denver No. 16 Combination	Turne -	Denver No. 1	INAJUR I6 Combination	<b>-</b>
Local Depression (additional to co	ntinuous autter depression 'a' from above)	alogal =	2.00	2.00	inches
Number of Unit Inlets (Grate or Cu	Infinited as galler appression a norm above)	No -	3	3	indites
Water Depth at Flowline (outside of	of local depression)	Ponding Depth =	6.0	6.6	inches
Grate Information	, , , , , , , , , , , , , , , , , , , ,		MINOR	MAJOR	Override Depths
Length of a Unit Grate		L <sub>o</sub> (G) =	3.00	3.00	feet
Width of a Unit Grate		W <sub>o</sub> =	1.73	1.73	feet
Area Opening Ratio for a Grate (ty	pical values 0.15-0.90)	A <sub>ratio</sub> =	0.31	0.31	
Clogging Factor for a Single Grate	e (typical value 0.50 - 0.70)	C <sub>f</sub> (G) =	0.50	0.50	
Grate Weir Coefficient (typical val	ue 2.15 - 3.60)	C <sub>w</sub> (G) =	3.60	3.60	
Grate Orifice Coefficient (typical va	alue 0.60 - 0.80)	C <sub>0</sub> (G) =	0.60	0.60	
Curb Opening Information			MINOR	MAJOR	-
Length of a Unit Curb Opening		L <sub>o</sub> (C) =	3.00	3.00	feet
Height of Vertical Curb Opening in	Inches	H <sub>vert</sub> =	6.50	6.50	inches
Height of Curb Orifice Throat in In	ches	H <sub>throat</sub> =	5.25	5.25	inches
Angle of Throat (see USDCM Figu	ire ST-5)	Theta =	0.00	0.00	degrees
Side Width for Depression Pan (ty	pically the gutter width of 2 feet)	W <sub>p</sub> =	2.00	2.00	feet
Clogging Factor for a Single Curb	Opening (typical value 0.10)	$C_{f}(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (ty	pical value 2.3-3.7)	C <sub>w</sub> (C) =	3.70	3.70	
Curb Opening Orifice Coefficient (	typical value 0.60 - 0.70)	C <sub>o</sub> (C) =	0.66	0.66	
Low Head Performance Reducti	on (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth		d <sub>Grate</sub> =	0.523	0.569	ft
Depth for Curb Opening Weir Equ	ation	d <sub>Curb</sub> =	0.33	0.38	ft
Combination Inlet Performance Re	eduction Factor for Long Inlets	RF <sub>Combination</sub> =	0.57	0.62	
Curb Opening Performance Redu	ction Factor for Long Inlets	RF <sub>Curb</sub> =	0.97	1.00	
Grated Inlet Performance Reduction	on Factor for Long Inlets	RF <sub>Grate</sub> =	0.57	0.62	
		_	MINOR	MAJOR	
Total Inlet Interception Ca	pacity (assumes clogged condition)	Q <sub>a</sub> =	7.6	9.6	cfs
Inlet Capacity IS GOOD for Mind	or and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	3.4	9.2	cfs



# INLET ON A CONTINUOUS GRADE





Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	Denver No. 16	6 Combination	
Local Depression (additional to continuous gutter depression 'a')	a <sub>LOCAL</sub> =	2.0	2.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	2	2	
Length of a Single Unit Inlet (Grate or Curb Opening)	L <sub>o</sub> =	3.00	3.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W <sub>o</sub> =	1.73	1.73	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C <sub>f</sub> -G =	0.50	0.50	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	$C_{f}-C =$	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'	_	MINOR	MAJOR	_
Total Inlet Interception Capacity	Q =	1.4	2.3	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q <sub>b</sub> =	0.3	1.3	cfs
Capture Percentage = Q <sub>a</sub> /Q <sub>o</sub> =	C% =	82	64	%





Design Information (Input)	ſ		MINOR	MAJOR	
Type of Inlet	Denver No. 16 Combination	Type =	Denver No. 1	6 Combination	
Local Depression (additional to co	ntinuous gutter depression 'a' from above)	a <sub>local</sub> =	2.00	2.00	inches
Number of Unit Inlets (Grate or Cu	urb Opening)	No =	2	2	1
Water Depth at Flowline (outside	of local depression)	Ponding Depth =	6.0	6.6	inches
Grate Information			MINOR	MAJOR	Override Depths
Length of a Unit Grate		L <sub>o</sub> (G) =	3.00	3.00	feet
Width of a Unit Grate		W <sub>o</sub> =	1.73	1.73	feet
Area Opening Ratio for a Grate (ty	pical values 0.15-0.90)	A <sub>ratio</sub> =	0.31	0.31	
Clogging Factor for a Single Grate	e (typical value 0.50 - 0.70)	C <sub>f</sub> (G) =	0.50	0.50	
Grate Weir Coefficient (typical val	ue 2.15 - 3.60)	C <sub>w</sub> (G) =	3.60	3.60	
Grate Orifice Coefficient (typical v	alue 0.60 - 0.80)	C <sub>o</sub> (G) =	0.60	0.60	1
Curb Opening Information			MINOR	MAJOR	-
Length of a Unit Curb Opening		L <sub>o</sub> (C) =	3.00	3.00	feet
Height of Vertical Curb Opening in	Inches	H <sub>vert</sub> =	6.50	6.50	inches
Height of Curb Orifice Throat in In	ches	H <sub>throat</sub> =	5.25	5.25	inches
Angle of Throat (see USDCM Figu	ire ST-5)	Theta =	0.00	0.00	degrees
Side Width for Depression Pan (ty	pically the gutter width of 2 feet)	W <sub>p</sub> =	2.00	2.00	feet
Clogging Factor for a Single Curb	Opening (typical value 0.10)	C <sub>f</sub> (C) =	0.10	0.10	
Curb Opening Weir Coefficient (ty	pical value 2.3-3.7)	C <sub>w</sub> (C) =	3.70	3.70	
Curb Opening Orifice Coefficient (	typical value 0.60 - 0.70)	C <sub>0</sub> (C) =	0.66	0.66	
Low Head Performance Reducti	on (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth		d <sub>Grate</sub> =	0.523	0.569	ft
Depth for Curb Opening Weir Equ	ation	d <sub>Curb</sub> =	0.33	0.38	ft
Combination Inlet Performance Re	eduction Factor for Long Inlets	RF <sub>Combination</sub> =	0.71	0.77	1
Curb Opening Performance Redu	ction Factor for Long Inlets	RF <sub>Curb</sub> =	1.00	1.00	
Grated Inlet Performance Reduction	on Factor for Long Inlets	RF <sub>Grate</sub> =	0.71	0.77	
			MINOR	MAJOR	
Total Inlet Interception Ca	pacity (assumes clogged condition)	Q <sub>a</sub> =	6.2	7.9	cfs
Inlet Capacity IS GOOD for Mind	or and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	2.8	5.4	cfs



# INLET ON A CONTINUOUS GRADE





Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	Denver No. 16	6 Combination	
Local Depression (additional to continuous gutter depression 'a')	a <sub>LOCAL</sub> =	2.0	2.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L <sub>o</sub> =	3.00	3.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W <sub>o</sub> =	1.73	1.73	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C <sub>f</sub> -G =	0.50	0.50	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	$C_{f}-C =$	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	1.3	2.2	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q <sub>b</sub> =	0.6	2.6	cfs
Capture Percentage = Q <sub>a</sub> /Q <sub>o</sub> =	C% =	68	45	%

### AREA INLET IN A SWALE



### AREA INLET IN A SWALE







Design Information (Input)		-	MINOR	MAJOR	
Type of Inlet	Denver No. 16 Combination	Type =	Denver No. 16 Combination		
Local Depression (additional to continuous gutter depression 'a' from above)		a <sub>local</sub> =	2.00	2.00	inches
Number of Unit Inlets (Grate or Cu	Number of Unit Inlets (Grate or Curb Opening)		2	2	
Water Depth at Flowline (outside	of local depression)	Ponding Depth =	4.4	4.4	inches
Grate Information			MINOR	MAJOR	Override Depths
Length of a Unit Grate		L <sub>o</sub> (G) =	3.00	3.00	feet
Width of a Unit Grate		W <sub>o</sub> =	1.73	1.73	feet
Area Opening Ratio for a Grate (ty	A <sub>ratio</sub> =	0.31	0.31		
Clogging Factor for a Single Grate	e (typical value 0.50 - 0.70)	C <sub>f</sub> (G) =	0.50	0.50	
Grate Weir Coefficient (typical val	ue 2.15 - 3.60)	C <sub>w</sub> (G) =	3.60	3.60	
Grate Orifice Coefficient (typical v	alue 0.60 - 0.80)	C <sub>0</sub> (G) =	0.60	0.60	
Curb Opening Information			MINOR	MAJOR	-
Length of a Unit Curb Opening		L <sub>o</sub> (C) =	3.00	3.00	feet
Height of Vertical Curb Opening in	Inches	H <sub>vert</sub> =	6.50	6.50	inches
Height of Curb Orifice Throat in In	ches	H <sub>throat</sub> =	5.25	5.25	inches
Angle of Throat (see USDCM Figu	ure ST-5)	Theta =	0.00	0.00	degrees
Side Width for Depression Pan (ty	W <sub>p</sub> =	2.00	2.00	feet	
Clogging Factor for a Single Curb	$C_{f}(C) =$	0.10	0.10		
Curb Opening Weir Coefficient (ty	rpical value 2.3-3.7)	C <sub>w</sub> (C) =	3.70	3.70	
Curb Opening Orifice Coefficient (	(typical value 0.60 - 0.70)	C <sub>0</sub> (C) =	0.66	0.66	
Low Head Performance Reducti	ion (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth		d <sub>Grate</sub> =	0.389	0.389	ft
Depth for Curb Opening Weir Equ	lation	d <sub>Curb</sub> =	0.20	0.20	ft
Combination Inlet Performance Re	eduction Factor for Long Inlets	RF <sub>Combination</sub> =	0.52	0.52	
Curb Opening Performance Redu	ction Factor for Long Inlets	RF <sub>Curb</sub> =	1.00	1.00	
Grated Inlet Performance Reduction	on Factor for Long Inlets	RF <sub>Grate</sub> =	0.52	0.52	
			MINOR	MAJOR	
Total Inlet Interception Ca	pacity (assumes clogged condition)	Q <sub>a</sub> =	2.6	2.6	cfs
WARNING: Inlet Capacity less the second se	han Q Peak for Major Storm	Q PEAK REQUIRED =	1.6	3.2	cfs





Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	Denver No. 16 Combination		
Local Depression (additional to continuous gutter depression 'a' from	above) alocal =	2.00	2.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	2	2	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	6.0	6.6	inches
Grate Information		MINOR	MAJOR	Override Depths
Length of a Unit Grate	L <sub>o</sub> (G) =	3.00	3.00	feet
Width of a Unit Grate	W <sub>o</sub> =	1.73	1.73	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A <sub>ratio</sub> =	0.31	0.31	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_{f}(G) =$	0.50	0.50	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C <sub>w</sub> (G) =	3.60	3.60	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	C <sub>o</sub> (G) =	0.60	0.60	
Curb Opening Information		MINOR	MAJOR	-
Length of a Unit Curb Opening	$L_{o}(C) =$	3.00	3.00	feet
Height of Vertical Curb Opening in Inches	H <sub>vert</sub> =	6.50	6.50	inches
Height of Curb Orifice Throat in Inches	H <sub>throat</sub> =	5.25	5.25	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	0.00	0.00	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W <sub>p</sub> =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_{f}(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$	3.70	3.70	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	C <sub>o</sub> (C) =	0.66	0.66	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d <sub>Grate</sub> =	0.523	0.569	ft
Depth for Curb Opening Weir Equation	d <sub>Curb</sub> =	0.33	0.38	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF <sub>Combination</sub> =	0.71	0.77	
Curb Opening Performance Reduction Factor for Long Inlets	RF <sub>Curb</sub> =	1.00	1.00	
Grated Inlet Performance Reduction Factor for Long Inlets	RF <sub>Grate</sub> =	0.71	0.77	
		MINOR	MAJOR	
Total Inlet Interception Capacity (assumes clogged o	condition) Q <sub>a</sub> =	6.2	7.9	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	2.6	5.6	cfs





Design Information (Input)			MINOR	MAIOP	
Type of Inlet	Denver No. 16 Combination	Type =	Denver No. 1	16 Combination	ר ר
Local Depression (additional to continuous outter depression 'a' from above)		a <sub>local</sub> =	2.00	2.00	inches
Number of Unit Inlets (Grate or Curb Opening)		No =	3	3	
Water Depth at Flowline (outside o	of local depression)	Ponding Depth =	4.4	4.4	inches
Grate Information			MINOR	MAJOR	Override Depths
Length of a Unit Grate		L <sub>o</sub> (G) =	3.00	3.00	feet
Width of a Unit Grate		W <sub>o</sub> =	1.73	1.73	feet
Area Opening Ratio for a Grate (ty	rpical values 0.15-0.90)	A <sub>ratio</sub> =	0.31	0.31	1
Clogging Factor for a Single Grate	e (typical value 0.50 - 0.70)	C <sub>f</sub> (G) =	0.50	0.50	
Grate Weir Coefficient (typical value	ue 2.15 - 3.60)	C <sub>w</sub> (G) =	3.60	3.60	1
Grate Orifice Coefficient (typical va	alue 0.60 - 0.80)	C <sub>o</sub> (G) =	0.60	0.60	
Curb Opening Information			MINOR	MAJOR	-
Length of a Unit Curb Opening		$L_{o}(C) =$	3.00	3.00	feet
Height of Vertical Curb Opening in	Inches	H <sub>vert</sub> =	6.50	6.50	inches
Height of Curb Orifice Throat in In	ches	H <sub>throat</sub> =	5.25	5.25	inches
Angle of Throat (see USDCM Figu	ire ST-5)	Theta =	0.00	0.00	degrees
Side Width for Depression Pan (ty	pically the gutter width of 2 feet)	W <sub>p</sub> =	2.00	2.00	feet
Clogging Factor for a Single Curb	$C_{f}(C) =$	0.10	0.10		
Curb Opening Weir Coefficient (ty	Curb Opening Weir Coefficient (typical value 2.3-3.7)			3.70	
Curb Opening Orifice Coefficient (	typical value 0.60 - 0.70)	C <sub>o</sub> (C) =	0.66	0.66	
Low Head Performance Reducti	on (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	<u> </u>	d <sub>Grate</sub> =	0.389	0.389	ft
Depth for Curb Opening Weir Equ	Depth for Curb Opening Weir Equation			0.20	ft
Combination Inlet Performance Re	eduction Factor for Long Inlets	RF <sub>Combination</sub> =	0.41	0.41	1
Curb Opening Performance Redu	ction Factor for Long Inlets	RF <sub>Curb</sub> =	0.86	0.86	
Grated Inlet Performance Reduction	on Factor for Long Inlets	RF <sub>Grate</sub> =	0.41	0.41	
			MINOR	MAIOR	
Total Inlat Intercontian Ca	nonity (nonuman alonged or without)	ا_ <b>م</b>	2.2		lofo
Total Inlet Interception Ca	Q <sub>a</sub> =	3.2	3.2		
WARNING: Inlet Capacity less the	nan Q Peak for Major Storm	Q PEAK REQUIRED =	1.0	3.2	cfs

# **Channel Report**

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Friday, Jan 15 2021

# SWALE A

Triangular		Highlighted			
Side Slopes (z:1)	= 3.00, 3.0	DO Depth (ft)	=	0.23	
Total Depth (ft)	= 0.33	Q (cfs)	=	0.380	
,		Area (sqft)	=	0.16	
Invert Elev (ft)	= 1.00	Velocity (ft/s)	=	2.39	
Slope (%)	= 1.00	Wetted Perim (ft)	=	1.45	
N-Value	= 0.013	Crit Depth, Yc (ft)	=	0.26	
		Top Width (ft)	=	1.38	
Calculations		EGL (ft)	=	0.32	
Compute by:	Known Q				
Known Q (cfs)	= 0.38				
× ,		100-year Flow Calculation:			
		Area drainage to swale: 0.14 ac			
		Basin A10 area: 0.78 ac			
		Percentage of Basin A10 draining to swale: 18%			
		Basin A10 Q100: 2.1 cfs			
		Q100 in swale: 0.38 cfs (2.1 cfs * 18%)			


Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Friday, Jan 15 2021

## SWALE B

Triangular		Highlighted		
Side Slopes (z:1)	= 5.00, 3	.00 Depth (ft)	=	0.28
Total Depth (ft)	= 1.50	Q (cfs)	=	0.520
,		Area (sqft)	=	0.31
Invert Elev (ft)	= 1.00	Velocity (ft/s)	=	1.66
Slope (%)	= 3.06	Wetted Perim (ft)	=	2.31
N-Value	= 0.040	Crit Depth, Yc (ft)	=	0.26
		Top Width (ft)	=	2.24
Calculations		EGL (ft)	=	0.32
Compute by:	Known Q			
Known Q (cfs)	= 0.52			
		Area draining to Swale B: 0.18 ac	1	
		Basin B9 area: 0,31 ac		
		Percentage of Basin B9 draining to Swale B: 58%		
		Basin B9 Q100: 0.9 cfs		
		Q100 in Swale B: 0.52 cfs (0.9 cfs * 58%)		



Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Friday, Jan 15 2021

0.25

0.520 0.34 1.51

### SWALE B'

### Triangular

Side Slopes (z:1)	= 8.00, 3.00
Total Depth (ft)	= 1.50
Invert Elev (ft)	= 1.00
Slope (%)	= 3.06
N-Value	= 0.040
Calculations Compute by:	Known Q

### Compute by:

	1 (110 111)
Known Q (cfs)	= 0.52

See 100-year flow calculation on Swale B Channel Report.

Highlighted	
Depth (ft)	=
Q (cfs)	=
Area (sqft)	=
Velocity (ft/s)	=
Wetted Perim (ft)	=
Crit Depth, Yc (ft)	=
Top Width (ft)	=

=	2.81
=	0.23
=	2.75
=	0.29
	= = =



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Friday, Jan 15 2021

## SWALE C

Triangular		Highlighted	
Side Slopes (z:1)	= 25.00, 4.00	Depth (ft)	= 0.12
Total Depth (ft)	= 0.50	Q (cfs)	= 0.300
		Area (sqft)	= 0.21
Invert Elev (ft)	= 1.00	Velocity (ft/s)	= 1.44
Slope (%)	= 4.80	Wetted Perim (ft)	= 3.50
N-Value	= 0.030	Crit Depth, Yc (ft)	= 0.13
		Top Width (ft)	= 3.48
Calculations		EGL (ft)	= 0.15
Compute by:	Known Q		
Known Q (cfs)	= 0.30		



Reach (ft)

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Friday, Jan 15 2021

### SWALE C'

Triangular		Highlighted	
Side Slopes (z:1)	= 50.00, 3.00	Depth (ft)	= 0.12
Total Depth (ft)	= 0.12	Q (cfs)	= 0.300
		Area (sqft)	= 0.38
Invert Elev (ft)	= 1.00	Velocity (ft/s)	= 0.79
Slope (%)	= 1.50	Wetted Perim (ft)	= 6.38
N-Value	= 0.030	Crit Depth, Yc (ft)	= 0.10
		Top Width (ft)	= 6.36
Calculations		EGL (ft)	= 0.13
Compute by:	Known Q		
Known Q (cfs)	= 0.30		



## URBAN COLLECTION AT BRIARGATE SQUARE

StormCAD Map 1





## URBAN COLLECTION AT BRIARGATE SQUARE



StormCAD Map 2

URBAN COLLECTION AT BRIARGATE SQUARE																	
StormCAD Pipe and Node Report - 5-Year																	
Unstream Structure	Label	Flow (cfs)	Velocity (ft/s)	Diameter (in)	Slope (ft/ft)	Invert (Start)	Invert (Stop)	Elevation Ground	Elevation Ground	HGL (Up)	HGL (Down)	EGL (In)	EGL (Out)	Upstream Structure	Length	Capacity (Full	Manning's
opstream structure	Label	FIOW (CIS)	velocity (it/s)	Diameter (III)	Slope (TI/TI)	(ft)	(ft)	(Start) (ft)	(Stop) (ft)	(ft)	(ft)	(ft)	(ft)	Headloss Coefficient	(ft)	Flow) (cfs)	n
DP4.1_Dbl Type 16	DP4.1_Pipe	4.8	4.47	18	0.005	6,446.91	6,446.87	6,450.77	6,451.83	6,447.79	6,447.71	6,448.10	6,448.05	0.05	9	7.43	0.013
DP4.1-2_Type II MH	DP4.1_Pipe 2	4.8	5.22	24	0.008	6,446.37	6,445.51	6,451.83	6,449.55	6,447.14	6,446.44	6,447.43	6,446.62	1.32	110.2	19.93	0.013
DP4_Dbl Type 16	DP4_Pipe	2.4	4.81	18	0.01	6,447.33	6,447.01	6,450.95	6,450.77	6,447.91	6,447.80	6,448.13	6,447.90	0	31.5	10.5	0.013
DP5_Dbl Type 16	DP5.1_Pipe	6.6	5.65	30	0.008	6,445.01	6,444.61	6,449.55	6,449.27	6,446.44	6,446.45	6,446.52	6,446.49	0.05	50.4	36.58	0.013
DP8_Trpl Type 16	DP8.1_Pipe	8.7	5.16	30	0.005	6,444.61	6,444.36	6,449.27	6,449.11	6,446.33	6,446.32	6,446.42	6,446.39	1.32	49.5	29	0.013
DP9_Trpl Type 16	DP9.1_Pipe	11.8	8.07	30	0.014	6,444.26	6,444.01	6,449.11	6,446.80	6,446.31	6,446.32	6,446.43	6,446.42	0.05	18	47.87	0.013
DP10+25_Type II MH	DP10+25_Pipe	0.4	2.04	36	0.005	6,426.88	6,426.20	6,434.67	6,429.54	6,427.08	6,426.40	6,427.14	6,426.46	1.02	136.1	47.16	0.013
DP10_Pond A OS	DP10_Pipe1	0.2	2.35	30	0.013	6,441.24	6,440.73	6,444.03	6,452.20	6,441.39	6,440.84	6,441.44	6,440.93	0	40.2	46.54	0.013
DP10_Type II MH1	DP10_Pipe2	0.2	2.9	30	0.024	6,440.62	6,436.77	6,452.20	6,452.64	6,440.77	6,436.88	6,440.82	6,437.01	0.4	163.4	62.96	0.013
DP10_Type II MH2	DP10_Pipe3	0.2	1.69	30	0.005	6,435.77	6,435.34	6,452.64	6,452.54	6,435.92	6,435.48	6,435.97	6,435.53	0.05	86.6	29	0.013
DP10_Type II MH3	DP10_Pipe4	0.2	1.7	30	0.005	6,435.24	6,433.94	6,452.54	6,442.89	6,435.39	6,434.09	6,435.44	6,434.14	0.05	257.9	29.11	0.013
DP10_Type II MH4	DP10_Pipe5	0.2	2.64	30	0.018	6,433.84	6,433.34	6,442.89	6,442.41	6,433.99	6,433.45	6,434.04	6,433.56	0.1	27.8	55.12	0.013
DP10_Type II MH5	DP10_Pipe6	0.2	2.57	30	0.016	6,433.24	6,430.70	6,442.41	6,437.77	6,433.39	6,430.81	6,433.44	6,430.92	0.1	154.2	52.64	0.013
DP10_Type II MH6	DP10_Pipe7	0.2	2.48	30	0.015	6,430.61	6,430.16	6,437.77	6,437.81	6,430.75	6,430.28	6,430.80	6,430.37	0.1	29.6	50.23	0.013
DP10_Type II MH7	DP10_Pipe8	0.2	2.48	30	0.015	6,430.07	6,427.88	6,437.81	6,434.67	6,430.21	6,428.00	6,430.26	6,428.09	0.1	145.6	50.23	0.013
DP19_Type 16	DP16_Pipe	1.2	3.75	18	0.009	6,435.37	6,434.57	6,439.82	6,438.25	6,435.78	6,435.03	6,435.92	6,435.14	0	92.2	9.75	0.013
DP17_Dbl Type 16	DP17_Pipe	1.4	4.13	18	0.01	6,437.63	6,437.31	6,441.89	6,441.71	6,438.18	6,438.21	6,438.27	6,438.24	0	31.5	10.5	0.013
DP18_Dbl Type 16	DP18.1_Pipe	4.2	6.32	18	0.014	6,437.01	6,434.73	6,441.71	6,438.07	6,437.80	6,435.65	6,438.11	6,435.86	1.32	165	12.35	0.013
DP21_Type C Inlet	DP21_Pipe	0.1	1.48	18	0.005	6,435.67	6,434.96	6,437.98	6,439.33	6,435.79	6,435.69	6,435.82	6,435.69	0	140.9	7.43	0.013
DP22.1_Type II MH	DP22.1_Pipe	1.5	3.29	18	0.005	6,434.86	6,434.73	6,439.33	6,438.07	6,435.65	6,435.65	6,435.69	6,435.68	1.02	25.4	7.42	0.013
DP22_Dbl Type 16	DP22_Pipe	1.4	4.13	18	0.01	6,435.05	6,434.84	6,438.42	6,439.33	6,435.68	6,435.69	6,435.74	6,435.72	0	20.3	10.5	0.013
DP23_Dbl Type 16	DP23.1_Pipe	8.1	5.11	24	0.005	6,434.23	6,434.07	6,438.07	6,438.25	6,435.24	6,435.08	6,435.64	6,435.49	1.02	31.5	16	0.013
DP24_Trpl Type 16	DP24.1_Pipe	10	5.41	30	0.005	6,433.57	6,433.41	6,438.25	6,438.48	6,434.63	6,434.59	6,435.03	6,434.89	1.02	30.7	29.34	0.013
DP24.1_Type II MH	DP24.1_Pipe2	10	5.97	30	0.007	6,433.11	6,433.00	6,438.48	6,435.79	6,434.51	6,434.52	6,434.70	6,434.68	0.4	16.6	33.58	0.013
DP25_Pond B OS	DP25_Pipe	0.2	1.72	30	0.005	6,430.84	6,430.77	6,433.63	6,438.04	6,430.99	6,430.91	6,431.04	6,430.96	0	14.8	29.53	0.013
DP25_Type II MH1	DP25_Pipe2	0.2	1.69	30	0.005	6,430.56	6,430.25	6,438.04	6,436.82	6,430.71	6,430.40	6,430.76	6,430.45	0.4	61.8	29	0.013
DP25_Type II MH2	DP25_Pipe3	0.2	2.25	30	0.011	6,429.95	6,427.38	6,436.82	6,434.67	6,430.10	6,427.51	6,430.15	6,427.58	1.32	228.4	43.5	0.013

URBAN COLLECTION AT BRIARGATE SQUARE																	
StormCAD Pipe and Node Report - 100-Year																	
Unstream Structure	Label	Flow (cfs)	Velocity (ft/s)	Diameter (in)	Slope (ft/ft)	Invert (Start)	Invert (Stop)	Elevation Ground	Elevation Ground	HGL (Up)	HGL (Down)	EGL (In)	EGL (Out)	Upstream Structure	Length	Capacity (Full	Manning's
opstream structure	Laber	FIOW (CIS)	velocity (173)	Diameter (III)	Slope (TI/TI)	(ft)	(ft)	(Start) (ft)	(Stop) (ft)	(ft)	(ft)	(ft)	(ft)	Headloss Coefficient	(ft)	Flow) (cfs)	n
DP4.1_Dbl Type 16	DP4.1_Pipe	9.3	5.26	18	0.005	6,446.91	6,446.87	6,450.77	6,451.83	6,448.76	6,448.69	6,449.19	6,449.12	0.05	9	7.43	0.013
DP4.1-2_Type II MH	DP4.1_Pipe 2	9.3	2.96	24	0.008	6,446.37	6,445.51	6,451.83	6,449.55	6,448.51	6,448.32	6,448.65	6,448.46	1.32	110.2	19.93	0.013
DP4_Dbl Type 16	DP4_Pipe	3.4	5.3	18	0.01	6,447.33	6,447.01	6,450.95	6,450.77	6,448.81	6,448.78	6,448.87	6,448.84	0	31.5	10.5	0.013
DP5_Dbl Type 16	DP5.1_Pipe	13.4	2.73	30	0.008	6,445.01	6,444.61	6,449.55	6,449.27	6,448.32	6,448.26	6,448.43	6,448.38	0.05	50.4	36.58	0.013
DP8_Trpl Type 16	DP8.1_Pipe	14.9	3.04	30	0.005	6,444.61	6,444.36	6,449.27	6,449.11	6,448.07	6,448.01	6,448.22	6,448.15	1.32	49.5	29	0.013
DP9_Trpl Type 16	DP9.1_Pipe	23.8	4.85	30	0.014	6,444.26	6,444.01	6,449.11	6,447.93	6,447.99	6,447.93	6,448.36	6,448.30	0.05	18	47.87	0.013
DP10+25_Type II MH	DP10+25_Pipe	48.2	7.6	36	0.005	6,426.88	6,426.20	6,434.67	6,429.54	6,429.38	6,428.46	6,430.29	6,429.57	1.02	136.1	47.16	0.013
DP10_Pond A OS	DP10_Pipe1	25.6	9.71	30	0.013	6,441.24	6,440.73	6,444.03	6,452.20	6,442.97	6,442.66	6,443.75	6,443.27	0	40.2	46.54	0.013
DP10_Type II MH1	DP10_Pipe2	25.6	12.16	30	0.024	6,440.62	6,436.77	6,452.20	6,452.64	6,442.35	6,437.88	6,443.13	6,440.18	0.4	163.4	62.96	0.013
DP10_Type II MH2	DP10_Pipe3	25.6	6.67	30	0.005	6,435.77	6,435.34	6,452.64	6,452.54	6,437.60	6,437.10	6,438.29	6,437.85	0.05	86.6	29	0.013
DP10_Type II MH3	DP10_Pipe4	25.6	6.69	30	0.005	6,435.24	6,433.94	6,452.54	6,442.89	6,437.06	6,435.67	6,437.76	6,436.45	0.05	257.9	29.11	0.013
DP10_Type II MH4	DP10_Pipe5	25.6	11.02	30	0.018	6,433.84	6,433.34	6,442.89	6,442.41	6,435.57	6,434.70	6,436.35	6,436.08	0.1	27.8	55.12	0.013
DP10_Type II MH5	DP10_Pipe6	25.6	10.65	30	0.016	6,433.24	6,430.70	6,442.41	6,437.77	6,434.97	6,431.93	6,435.75	6,433.69	0.1	154.2	52.64	0.013
DP10_Type II MH6	DP10_Pipe7	25.6	10.28	30	0.015	6,430.61	6,430.16	6,437.77	6,437.81	6,432.33	6,431.56	6,433.11	6,432.84	0.1	29.6	50.23	0.013
DP10_Type II MH7	DP10_Pipe8	25.6	10.28	30	0.015	6,430.07	6,427.88	6,437.81	6,434.67	6,431.79	6,430.31	6,432.57	6,430.74	0.1	145.6	50.23	0.013
DP19_Type 16	DP16_Pipe	2.1	4.4	18	0.009	6,435.37	6,434.57	6,439.82	6,438.25	6,436.39	6,436.37	6,436.43	6,436.40	0	92.2	9.75	0.013
DP17_Dbl Type 16	DP17_Pipe	2.3	4.76	18	0.01	6,437.63	6,437.31	6,441.89	6,441.71	6,438.77	6,438.76	6,438.81	6,438.79	0	31.5	10.5	0.013
DP18_Dbl Type 16	DP18.1_Pipe	7.8	7.39	18	0.014	6,437.01	6,434.73	6,441.71	6,438.07	6,438.10	6,436.96	6,438.60	6,437.27	1.32	165	12.35	0.013
DP21_Type C Inlet	DP21_Pipe	0.9	2.84	18	0.005	6,435.67	6,434.96	6,437.98	6,439.33	6,437.06	6,437.05	6,437.07	6,437.06	0	140.9	7.43	0.013
DP22.1_Type II MH	DP22.1_Pipe	3.5	1.98	18	0.005	6,434.86	6,434.73	6,439.33	6,438.07	6,436.99	6,436.96	6,437.05	6,437.02	1.02	25.4	7.42	0.013
DP22_Dbl Type 16	DP22_Pipe	2.6	1.47	18	0.01	6,435.05	6,434.84	6,438.42	6,439.33	6,437.07	6,437.05	6,437.10	6,437.09	0	20.3	10.5	0.013
DP23_Dbl Type 16	DP23.1_Pipe	16.3	5.19	24	0.005	6,434.23	6,434.07	6,438.07	6,438.25	6,436.54	6,436.37	6,436.96	6,436.79	1.02	31.5	16	0.013
DP24_Trpl Type 16	DP24.1_Pipe	21.1	4.3	30	0.005	6,433.57	6,433.41	6,438.25	6,438.48	6,436.08	6,436.00	6,436.37	6,436.29	1.02	30.7	29.34	0.013
DP24.1_Type II MH	DP24.1_Pipe2	21.1	4.3	30	0.007	6,433.11	6,433.00	6,438.48	6,435.84	6,435.88	6,435.84	6,436.17	6,436.13	0.4	16.6	33.58	0.013
DP25_Pond B OS	DP25_Pipe	22.6	6.63	30	0.005	6,430.84	6,430.77	6,433.63	6,438.04	6,432.81	6,432.79	6,433.27	6,433.23	0	14.8	29.53	0.013
DP25_Type II MH1	DP25_Pipe2	22.6	6.53	30	0.005	6,430.56	6,430.25	6,438.04	6,436.82	6,432.61	6,432.50	6,433.04	6,432.87	0.4	61.8	29	0.013
DP25_Type II MH2	DP25_Pipe3	22.6	8.95	30	0.011	6,429.95	6,427.38	6,436.82	6,434.67	6,431.57	6,430.31	6,432.27	6,430.64	1.32	228.4	43.5	0.013





























# Appendix D Water Quality & Detention



Project: Palmer Village
Basin ID: Pond A (West Parcel)
ZONE 3 ZONE 2 ZONE 1

ORIFICE ZONE 1 AND 2 ORIFICE Example Zone Configuration (Retention Pond)

#### Watershed Information

PERMA

Selected BMP Type =	EDB	[			
Watershed Area =	5.92	acres			
Watershed Length =	700	ft			
Watershed Length to Centroid =	152	ft			
Watershed Slope =	0.012	ft/ft			
Watershed Imperviousness =	50.50%	percent			
Percentage Hydrologic Soil Group A =	100.0%	percent			
Percentage Hydrologic Soil Group B =	0.0%	percent			
Percentage Hydrologic Soil Groups C/D =	0.0%	percent			
Target WQCV Drain Time =	40.0	hours			
Location for 1-hr Rainfall Depths = User Input					

## After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

	3	
Water Quality Capture Volume (WQCV) =	0.102	acre-feet
Excess Urban Runoff Volume (EURV) =	0.346	acre-feet
2-yr Runoff Volume (P1 = 1.19 in.) =	0.245	acre-feet
5-yr Runoff Volume (P1 = 1.5 in.) =	0.326	acre-feet
10-yr Runoff Volume (P1 = 1.75 in.) =	0.390	acre-feet
25-yr Runoff Volume (P1 = 2 in.) =	0.491	acre-feet
50-yr Runoff Volume (P1 = 2.25 in.) =	0.590	acre-feet
100-yr Runoff Volume (P1 = 2.52 in.) =	0.715	acre-feet
500-yr Runoff Volume (P1 = 3 in.) =	0.922	acre-feet
Approximate 2-yr Detention Volume =	0.222	acre-feet
Approximate 5-yr Detention Volume =	0.293	acre-feet
Approximate 10-yr Detention Volume =	0.357	acre-feet
Approximate 25-yr Detention Volume =	0.436	acre-feet
Approximate 50-yr Detention Volume =	0.487	acre-feet
Approximate 100-yr Detention Volume =	0.548	acre-feet

Define	70000	and	Deele	Coometre	
Denne	ZOHES	anu	DOPILI	Geometry	y

efine Zones and Basin Geometry		
Zone 1 Volume (WQCV) =	0.102	acre-feet
Zone 2 Volume (EURV - Zone 1) =	0.243	acre-feet
Zone 3 Volume (100-year - Zones 1 & 2) =	0.202	acre-feet
Total Detention Basin Volume =	0.548	acre-feet
Initial Surcharge Volume (ISV) =	user	ft <sup>3</sup>
Initial Surcharge Depth (ISD) =	user	ft
Total Available Detention Depth (H <sub>total</sub> ) =	user	ft
Depth of Trickle Channel $(H_{TC}) =$	user	ft
Slope of Trickle Channel (S <sub>TC</sub> ) =	user	ft/ft
Slopes of Main Basin Sides (Smain) =	user	H:V
Basin Length-to-Width Ratio (R <sub>L/W</sub> ) =	user	

ft 2	user	Initial Surcharge Area (A <sub>ISV</sub> ) =
ft	user	Surcharge Volume Length ( $L_{ISV}$ ) =
ft	user	Surcharge Volume Width ( $W_{ISV}$ ) =
ft	user	Depth of Basin Floor $(H_{FLOOR}) =$
ft	user	Length of Basin Floor $(L_{FLOOR}) =$
ft	user	Width of Basin Floor ( $W_{FLOOR}$ ) =
ft 2	user	Area of Basin Floor (A <sub>FLOOR</sub> ) =
ft <sup>3</sup>	user	Volume of Basin Floor ( $V_{FLOOR}$ ) =
ft	user	Depth of Main Basin (H <sub>MAIN</sub> ) =
ft	user	Length of Main Basin (L <sub>MAIN</sub> ) =
ft	user	Width of Main Basin ( $W_{MAIN}$ ) =
ft 2	user	Area of Main Basin (A <sub>MAIN</sub> ) =
ft 3	user	Volume of Main Basin (VMAIN) =

Calculated Total Basin Volume (Vtotal) = user acre-feet

		Depth Increment =		ft							
				Optional				Optional			
on Pond)		Stage - Storage	Stage	Override	Length	Width	Area	Override	Area	Volume	Volume
,		Description	(ft)	Stage (ft)	(ft)	(ft)	(ft <sup>2</sup> )	Area (ft 2)	(acre)	(ft <sup>3</sup> )	(ac-ft)
	6442	Top of Micropool		0.00				0	0.000		
	0112	(442		1.00				200	0.007	144	0.000
		0443		1.00				288	0.007	144	0.003
		6444		2.00				2,350	0.054	1,463	0.034
		6445		3.00				4 702	0.108	4 989	0.115
		(44)		1.00				4,702	0.140	10.007	0.000
		6446		4.00				6,115	0.140	10,397	0.239
		6447		5.00				7,661	0.176	17,285	0.397
		6448		6.00				9.399	0.216	25.815	0.593
		( 440		7.00				11 474	0.2/2	24,252	0.000
		6449		7.00				11,474	0.263	36,252	0.832
		6449.6		7.60				13,146	0.302	43,638	1.002
0											
optional use	T										
	acre-feet										
	acre-feet										
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1 50	inchos										
1.50	inches										
1.75	inches										
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MHFD-Detention, Version 4.04 (February 2021)



MHFD-Detention, Version 4.04 (February 2021)

Project:	Palmer Village	10111	D-Detention, Vers	1011 4.04 (1 ebi uai	1 y 2021)				
Basin ID:	Pond A (West Pare	cel)							
ZONE 3 ZONE 2 ZONE 1				Estimated	Estimated				
				Stage (ft)	Volume (ac-ft)	Outlet Type	-		
VOLUME EURV WOCV			Zone 1 (WQCV)	2.89	0.102	Orifice Plate			
I TONE LANDA	100-YEAR ORIFICE		Zone 2 (EURV)	4.71	0.243	Orifice Plate			
PERMANENT ORIFICES			Zone 3 (100-year)	5.79	0.202	Weir&Pipe (Restrict)			
Example Zone	Configuration (R	etention Pond)		Total (all zones)	0.548		-		
User Input: Orifice at Underdrain Outlet (typical	ly used to drain WO	DCV in a Filtration E	<u>3MP)</u>			-	Calculated Parame	ters for Underdrain	<u>1</u>
Underdrain Orifice Invert Depth =	N/A	ft (distance below	the filtration media	surface)	Underd	rain Orifice Area =	N/A	ft <sup>2</sup>	
Underdrain Orifice Diameter =	N/A	inches			Underdrain	Orifice Centroid =	N/A	feet	
User Input: Orifice Plate with one or more orific	ces or Elliptical Slot	Weir (typically use	ed to drain WQCV ar	nd/or EURV in a se	dimentation BMP)	an Area nor Dour	Calculated Parame	ters for Plate	
Dopth at top of Zopo using Orifico Plate -	0.00	ft (relative to basin	n bottom at Stage =	= 0 IL) - 0 ft)		ce Area per Row =	2.708E-03	TI foot	
Orifice Plate: Orifice Vertical Spacing -	4.07 N/A	inches	i bottom at Stage -	- 01()	Ellipti	cal Slot Centroid -	N/A	feet	
Orifice Plate: Orifice Area per Row =	0.39	sa inches (diamet	rer = 11/16 inch)		F	llintical Slot Area =	N/A N/A	ft <sup>2</sup>	
	0.07	oq: monos (alamot			2	inplical clot fired		In	
User Input: Stage and Total Area of Each Orific	e Row (numbered	from lowest to high	nest)						
	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)	
Stage of Orifice Centroid (ft)	0.00	1.25	2.50						
Orifice Area (sq. inches)	0.39	0.39	0.39						J
								<del></del>	1
	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)	
Stage of Orifice Centroid (ft)									
Orifice Area (sq. inches)									1
User Input: Vertical Orifice (Circular or Rectand	ular)						Calculated Parame	ters for Vertical Or	ifice
	Not Selected	Not Selected	1				Not Selected	Not Selected	1
Invert of Vertical Orifice =	3.60	N/A	ft (relative to basin	bottom at Stage =	= 0 ft) Ver	tical Orifice Area =	0.03	N/A	ft <sup>2</sup>
Depth at top of Zone using Vertical Orifice =	4.69	N/A	ft (relative to basir	bottom at Stage =	= 0 ft) Vertical	Orifice Centroid =	0.08	N/A	feet
Vertical Orifice Diameter or Height =	2.00	N/A	inches					<u>.</u>	•
Vertical Orifice Width =	2.00		inches						
User Input: Overflow Weir (Dropbox with Flat of	or Sloped Grate and	Outlet Pipe OR Re	ectangular/Trapezoi	dal Weir (and No C	Dutlet Pipe)		Calculated Parame	ters for Overflow V	Veir
	Zone 3 Weir	Not Selected					Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	5.60	N/A	ft (relative to basin b	bottom at Stage = 0	ft) Height of Grate	e Upper Edge, Ht =	5.60	N/A	feet
Overflow Weir Front Edge Length =	3.00	N/A	feet	0	Overflow W	eir Slope Length =	3.00	N/A	feet
Uvernow weir Grate Slope =	0.00	N/A	H:V	Gra	ate Open Area / 10	U-yr Urifice Area =	36.77	N/A	cu2
Horiz. Length of Well Sides =	3.00 Cloco Moch Croto	N/A	leet	00	verflow Grate Open	Area w/o Debris =	7.12	N/A	TL 6+2
Debris Clogging % =	50%	N/A	%	0	vernow drate oper	TAICA W/ DEDITS -	3.50	IN/A	III
bobilo dioggilig ve	0070		,						
User Input: Outlet Pipe w/ Flow Restriction Plate	e (Circular Orifice, !	Restrictor Plate, or	Rectangular Orifice	)	Ca	lculated Parameter	s for Outlet Pipe w/	Flow Restriction P	late
	Zone 3 Restrictor	Not Selected					Zone 3 Restrictor	Not Selected	1
Depth to Invert of Outlet Pipe =	0.67	N/A	ft (distance below ba	asin bottom at Stage	= 0 ft) Ou	utlet Orifice Area =	0.19	N/A	ft <sup>2</sup>
Outlet Pipe Diameter =	18.00	N/A	inches		Outlet	Orifice Centroid =	0.15	N/A	feet
Restrictor Plate Height Above Pipe Invert =	3.00		inches	Half-Centr	ral Angle of Restric	tor Plate on Pipe =	0.84	N/A	radians
User Input: Emergency Spillway (Rectangular or	Irapezoidal)			2.5	- ··· -		Calculated Parame	ters for Spillway	
Spillway Invert Stage=		ft (relative to basin	n bottom at Stage =	= 0 ft)	Spillway D	esign Flow Depth=		feet	
Spillway Crest Length =		reet			Stage at I	op of Freeboard =		reet	
Splilway End Slopes =		H:V foot			Basin Area at T	op of Freeboard =		acre ft	
Fleeboard above max water surface =		leet			basin volume at i	op of Freeboard =		acre-n	
Routed Hydrograph Results	The user can over	ride the default CU	HP hydrographs an	d runoff volumes b	y entering new val	ues in the Inflow H	ydrographs table (0	Columns W through	n AF).
Design Storm Return Period =	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	2 00
CUHP Runoff Volume (acre-ft) =	0.102	0.346	0.245	0.326	0.390	0.491	0.590	0.715	0.922
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	0.245	0.326	0.390	0.491	0.590	0.715	0.922
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A	0.1	0.1	0.2	1.4	2.8	4.5	7.2
OPTIONAL Override Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow a (ofc/core)	N/A N/A	N/A	0.01	0.02	0.03	0.24	0.47	0.77	1 22
Peak Inflow O (cfs) =	N/A	N/A	4.4	5.9	7.0	9.4	11.6	14.6	18.9
Peak Outflow Q (cfs) =	0.0	0.2	0.1	0.2	0.2	0.3	0.8	2.4	2.5
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	1.6	1.3	0.2	0.3	0.5	0.3
Structure Controlling Flow = Max Velocity through Croto 1 (fee)	Plate N/A	vertical Orifice 1	vertical Orifice 1	vertical Orifice 1	vertical Orifice 1	vertical Orifice 1	Overflow Weir 1	Outlet Plate 1	Outlet Plate 1
Max Velocity through Grate 1 (fps) = Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	0.3 N/A
Time to Drain 97% of Inflow Volume (hours) =	39	67	63	67	69	72	74	72	70
Time to Drain 99% of Inflow Volume (hours) =	41	72	67	72	75	79	81	80	79
Maximum Ponding Depth (ft) =	2.89	4.71	3.94	4.43	4.80	5.33	5.69	5.91	6.55
Maximum Volume Stored (acre-ft) =	0.103	0.347	0.230	0.302	0.361	0.457	0.528	0.571	0.24



# DETENTION BASIN OUTLET STRUCTURE DESIGN Outflow Hydrograph Workbook Filename:

Inflow Hydrographs

The upor con calculated inflow bydrographs from this workbook with inflow bydrographs develo d in a c ato pre

<b>T</b>	SUURCE				CUMP			COMP		
Time Interval	LIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.07	0.01	0.17
	0:15:00	0.00	0.00	0.61	0.99	1.23	0.83	1.03	1.01	1.33
	0:20:00	0.00	0.00	2.06	2.67	3.13	1.97	2.29	2.47	3.03
	0:25:00	0.00	0.00	4.00	5.50	6.75	3.98	4.61	5.02	6.44
	0:30:00	0.00	0.00	4.41	5.87	6.95	8.87	11.08	12.92	16.98
	0:35:00	0.00	0.00	3.75	4.88	5.72	9.42	11.59	14.61	18.86
	0:40:00	0.00	0.00	3.15	4.01	4.68	8.30	10.23	12.78	16.55
	0:45:00	0.00	0.00	2.50	3.25	3.80	6.//	8.28	10.76	14.00
	0.50.00	0.00	0.00	2.00	2.74	3.15	5.60	0.// E 2E	6.00	0.00
	1.00.00	0.00	0.00	1.75	1.02	2.07	3.64	4.33	5.95	7.61
	1:05:00	0.00	0.00	1.40	1.73	1.92	2.04	3 54	4 94	6.45
	1:10:00	0.00	0.00	0.98	1.38	1.67	2.30	2.68	3.58	4.60
	1:15:00	0.00	0.00	0.84	1.23	1.58	1.81	2.08	2.60	3.31
	1:20:00	0.00	0.00	0.77	1.11	1.45	1.47	1.67	1.89	2.39
	1:25:00	0.00	0.00	0.72	1.04	1.27	1.27	1.44	1.48	1.83
	1:30:00	0.00	0.00	0.70	0.99	1.16	1.09	1.23	1.23	1.51
	1:35:00	0.00	0.00	0.68	0.96	1.07	0.97	1.09	1.07	1.29
	1:40:00	0.00	0.00	0.67	0.85	1.02	0.90	1.01	0.96	1.16
	1:45:00	0.00	0.00	0.66	0.77	0.98	0.84	0.95	0.89	1.06
	1:50:00	0.00	0.00	0.66	0.72	0.95	0.81	0.91	0.85	1.01
	1:55:00	0.00	0.00	0.55	0.68	0.90	0.79	0.89	0.84	1.00
	2:00:00	0.00	0.00	0.48	0.63	0.81	0.78	0.88	0.83	0.99
	2:10:00	0.00	0.00	0.33	0.43	0.33	0.35	0.40	0.38	0.45
	2:15:00	0.00	0.00	0.15	0.19	0.25	0.24	0.27	0.25	0.30
	2:20:00	0.00	0.00	0.09	0.12	0.16	0.15	0.17	0.16	0.19
	2:25:00	0.00	0.00	0.05	0.08	0.10	0.10	0.11	0.10	0.12
	2:30:00	0.00	0.00	0.03	0.04	0.06	0.06	0.06	0.06	0.07
	2:35:00	0.00	0.00	0.01	0.02	0.02	0.03	0.03	0.03	0.03
	2:40:00	0.00	0.00	0.00	0.01	0.01	0.01	0.01	0.01	0.01
	2:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2.00.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:55:00	0,00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

MHFD-Detention, Version 4.04 (February 2021)

Summary Stage-Area-Volume-Discharge Relationships The user can create a summary S-A-V-D by entering the desired stage increments and the remainder of the table will populate automatically. The user should graphically compare the summary S-A-V-D table to the full S-A-V-D table in the chart to confirm it captures all key transition points.

Stage - Storage	Stage	Area	Агеа	Volume	Volume	Total Outflow	
Description	[ft]	[ft 2]	[acres]	[ft 3]	[ac-ft]	[cfs]	
6442	0.00	0	0.000	0	0.000	0.00	For best results, include the
6443	1.00	288	0.007	144	0.003	0.01	stages of all grade slope
6444	2.00	2,350	0.054	1,463	0.034	0.03	changes (e.g. ISV and Floor)
6445	3.00	4,702	0.108	4,989	0.115	0.05	from the S-A-V table on Sheet 'Basin'
6446	4.00	6,115	0.140	10,397	0.239	0.14	Sheet Basin.
6447	5.00	7,661	0.176	17,285	0.397	0.23	Also include the inverts of all
6448	6.00	9,399	0.216	25,815	0.593	2.38	outlets (e.g. vertical orifice,
6449	7.00	11,474	0.263	36,252	0.832	2.56	overflow grate, and spillway,
6449.60	7.60	13,146	0.302	43,638	1.002	2.66	where applicable).
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	Project: Palmer Village
	Basin ID: Pond B (East Parcel)
100-YR EURY WOCY	ZONE 2 ZONE 2 ZONE 1

> -ORIFICE ZONE 1 AND 2 ORIFICES Example Zone Configuration (Retention Pond)

#### Watershed Information

PERM

Selected BMP Type =	EDB	
Watershed Area =	4.57	acres
Watershed Length =	700	ft
Watershed Length to Centroid =	227	ft
Watershed Slope =	0.028	ft/ft
Watershed Imperviousness =	54.30%	percent
Percentage Hydrologic Soil Group A =	100.0%	percent
Percentage Hydrologic Soil Group B =	0.0%	percent
Percentage Hydrologic Soil Groups C/D =	0.0%	percent
Target WQCV Drain Time =	40.0	hours
Location for 1-hr Rainfall Depths =	User Input	

## After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

Water Quality Capture Volume (WQCV) =	0.083	acre-feet
Excess Urban Runoff Volume (EURV) =	0.293	acre-feet
2-yr Runoff Volume (P1 = 1.19 in.) =	0.207	acre-feet
5-yr Runoff Volume (P1 = 1.5 in.) =	0.274	acre-feet
10-yr Runoff Volume (P1 = 1.75 in.) =	0.328	acre-feet
25-yr Runoff Volume (P1 = 2 in.) =	0.408	acre-feet
50-yr Runoff Volume (P1 = 2.25 in.) =	0.485	acre-feet
100-yr Runoff Volume (P1 = 2.52 in.) =	0.583	acre-feet
500-yr Runoff Volume (P1 = 3 in.) =	0.745	acre-feet
Approximate 2-yr Detention Volume =	0.189	acre-feet
Approximate 5-yr Detention Volume =	0.248	acre-feet
Approximate 10-yr Detention Volume =	0.302	acre-feet
Approximate 25-yr Detention Volume =	0.367	acre-feet
Approximate 50-yr Detention Volume =	0.408	acre-feet
Approximate 100-yr Detention Volume =	0.456	acre-feet

#### Define Zones and Basin Geometry

efine Zones and Basin Geometry		
Zone 1 Volume (WQCV) =	0.083	acre-feet
Zone 2 Volume (EURV - Zone 1) =	0.210	acre-feet
Zone 3 Volume (100-year - Zones 1 & 2) =	0.163	acre-feet
Total Detention Basin Volume =	0.456	acre-feet
Initial Surcharge Volume (ISV) =	user	ft <sup>3</sup>
Initial Surcharge Depth (ISD) =	user	ft
Total Available Detention Depth (H <sub>total</sub> ) =	user	ft
Depth of Trickle Channel $(H_{TC}) =$	user	ft
Slope of Trickle Channel (S <sub>TC</sub> ) =	user	ft/ft
Slopes of Main Basin Sides (Smain) =	user	H:V
Basin Length-to-Width Ratio (Rive) =	user	

Initial Surcharge Area (A <sub>ISV</sub> ) =	user	ft <sup>2</sup>
Surcharge Volume Length ( $L_{ISV}$ ) =	user	ft
Surcharge Volume Width ( $W_{ISV}$ ) =	user	ft
Depth of Basin Floor (H <sub>FLOOR</sub> ) =	user	ft
Length of Basin Floor $(L_{FLOOR}) =$	user	ft
Width of Basin Floor ( $W_{FLOOR}$ ) =	user	ft
Area of Basin Floor (A <sub>FLOOR</sub> ) =	user	ft <sup>2</sup>
Volume of Basin Floor ( $V_{FLOOR}$ ) =	user	ft <sup>3</sup>
Depth of Main Basin (H <sub>MAIN</sub> ) =	user	ft
Length of Main Basin $(L_{MAIN}) =$	user	ft
Width of Main Basin ( $W_{MAIN}$ ) =	user	ft
Area of Main Basin (A <sub>MAIN</sub> ) =	user	ft <sup>2</sup>
Volume of Main Basin (V <sub>MAIN</sub> ) =	user	ft <sup>3</sup>

H:V user

Calculated Total Basin Volume (Vtotal) = user acre-feet

		-									
		Depth Increment =		ft							
				Optional				Optional			
on Pond)		Stage - Storage	Stage	Override	Length	Width	Area	Override	Area	Volume	Volume
,		Description	(ft)	Stage (ft)	(ft)	(ft)	(ft 2)	Area (ft 2)	(acre)	(ft 3)	(ac-ft)
	6421	Top of Micropool		0.00				0	0.000	_	_
	0431	6422		1.00				447	0.010	222	0.005
		0432		1.00				44/	0.010	225	0.005
		6433		2.00				3,633	0.083	2,263	0.052
		6434		3.00				5.896	0.135	7.028	0 161
		6425		4.00				7 270	0.140	12 441	0.214
		0435		4.00				7,370	0.109	13,001	0.314
		6436		5.00				9,044	0.208	21,868	0.502
		6437		6.00				10,876	0.250	31,828	0.731
		4420		7.00				12.042	0.200	42 707	1.005
		0438		7.00				13,042	0.299	43,787	1.005
Optional Use	r Overrides										
	acre-feet										
	acre-feet										
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MHFD-Detention, Version 4.04 (February 2021)



110,000	Palmer Village													
Basin ID:	Pond B (East Parc	el)												
ZONE 3				Ectimated	Estimated									
ZONE 2 ZONE 1				Stage (ft)	Volumo (ac ft)	Outlot Typo								
			7	Stage (II)			1							
T			Zone I (WQCV)	2.34	0.083	Orifice Plate								
T ZONE 1 AND 2	0RIFICE		Zone 2 (EURV)	3.88	0.210	Orifice Plate								
PERMANENT ORIFICES			Zone 3 (100-year)	4.78	0.163	Weir&Pipe (Restrict)								
Example Zone	Configuration (Re	tention Pond)		Total (all zones)	0.456									
User Input: Orifice at Underdrain Outlet (typical	used to drain WQ	CV in a Filtration BM	AP)			4	Calculated Parame	ters for Underdrain	<u>1</u>					
Underdrain Orifice Invert Depth =	N/A	ft (distance below	the filtration media	surface)	Underg	rain Orifice Area =	N/A	ft <sup>2</sup>	-					
Underdrain Orifice Diameter =	N/A	inches		,	Underdrair	Orifice Centroid =	N/A	feet						
								1						
User Input: Orifice Plate with one or more orific	es or Elliptical Slot '	Weir (typically used	to drain WQCV and	d/or EURV in a sedi	mentation BMP)		Calculated Parame	ters for Plate						
Invert of Lowest Orifice =	0.00	ft (relative to basir	bottom at Stage =	= 0 ft)	WQ Orifi	ce Area per Row =	2.361E-03	ft <sup>2</sup>						
Depth at top of Zone using Orifice Plate =	3.90 ft (relative to basin bottom at Stage = 0 ft) Elliptical Half-Width = N/A feet							feet						
Orifice Plate: Orifice Vertical Spacing =	N/A	N/A linches Filintical Slat Centroid - N/A feet												
Orifice Plate: Orifice Area per Row =	0.34	sa. inches (diamete	er = 5/8 inch)		E	Iliptical Slot Area =	N/A	ft <sup>2</sup>						
		-4						1						
User Input: Stage and Total Area of Each Orific	Row (numbered f	rom lowest to high	et)											
User input. Stage and Total Area of Each Onlice	Pow 1 (required)	Row 2 (ontional)	Row 3 (optional)	Pow 4 (optional)	Pow 5 (optional)	Pow 6 (optional)	Pow 7 (optional)	Pow 8 (ontional)	1					
Stage of Orifice Controld (ft)	0.00	1.00	2.00	Row 4 (optional)	Row 5 (optional)	now o (optional)	Row / (optional)	Row o (optional)						
	0.00	0.24	2.00						-					
Office Area (sq. Inches)	0.34	0.34	0.34						1					
	Davis Q (antilanal)	Dave 10 (antianal)	David 11 (anti-mal)	David 2 (antianal)	David 2 (anti-mal)	David A (antilanal)	David 5 (antianal)	David ( (antional)	1					
	Row 9 (optional)	Row TO (optional)	Row IT (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)						
Stage of Orifice Centroid (ft)									-					
Orifice Area (sq. inches)									1					
Lleas Janut, Mastical Onifica (Circular on Dectors	(lan)						Coloulated Decema	tere for Vertical Or	fine .					
User input. Vertical Office (circular of Rectarig	IIdi )	Nat Calentari	1				Net Celested	Net Selected	<u>ince</u>					
Invent of Vention Orifice	Not Selected	Not Selected	ft (nalative ta hacin	hatten at Class	0.61)	tiaal Orifiaa Area	Not Selected	Not Selected						
Invertion Vertical Onlice =	2.85	N/A	It (relative to basin	i bollom al Slage =	= UTL) Ver	tical Onlice Area =	0.03	N/A	ft <sup>-</sup>					
Depth at top of Zone using vertical Orlifice =	3.84	N/A	It (relative to basin	bottom at Stage =	= 0 ft) Vertica	I Orifice Centrold =	0.08	N/A	reet					
Vertical Orifice Diameter or Height =	2.00	N/A	inches											
Vertical Orifice Width =	2.00		inches											
User Input: Overflow Weir (Dropbox with Flat o	Sloped Grate and	Outlet Pipe OR Rec	tangular/Trapezoid	al Weir (and No Ou	itlet Pipe)		Calculated Parame	ters for Overflow V	Veir					
	Zone 3 Weir	Not Selected					Zone 3 Weir	Not Selected	l					
Overflow Weir Front Edge Height, Ho =	4.55	N/A	ft (relative to basin I	bottom at Stage = 0 f	ft) Height of Grat	e Upper Edge, Ht =	4.55	N/A	feet					
Overflow Weir Front Edge Length =	3.00	N/A	feet		Overflow W	/eir Slope Length =	3.00	N/A	feet					
Overflow Weir Grate Slope =	0.00	N/A	H:V	Gra	ate Open Area / 10	0-yr Orifice Area =	40.63	N/A						
Horiz. Length of Weir Sides =	3.00	N/A	feet	Ov	erflow Grate Open	Area w/o Debris =	7.12	N/A	ft <sup>2</sup>					
Overflow Grate Type =	Close Mesh Grate	N/A		0	verflow Grate Ope	n Area w/ Debris =	3.56	N/A						
Debris Clogging % =	50%	N/A	%			Debris Clogging % = 50% N/A %								
User Input: Outlet Pipe w/ Flow Restriction Plate	(Circular Orifice R								ft²					
		estrictor Plate, or R	ectangular Orifice)		Ca	Iculated Parameters	s for Outlet Pipe w/	<sup>r</sup> Flow Restriction Pl	ft <sup>2</sup>					
	Zone 3 Restrictor	estrictor Plate, or R Not Selected	ectangular Orifice)		<u>Ca</u>	Iculated Parameters	s for Outlet Pipe w/ Zone 3 Restrictor	<u>' Flow Restriction Pl</u> Not Selected	ft <sup>2</sup>					
Depth to Invert of Outlet Pipe =	Zone 3 Restrictor 0.00	estrictor Plate, or R Not Selected N/A	ectangular Orifice) ft (distance below b	asin bottom at Stage	<u>Ca</u> = 0 ft) O	lculated Parameter: utlet Orifice Area =	s for Outlet Pipe w/ Zone 3 Restrictor 0.18	<sup>′</sup> Flow Restriction Pl Not Selected N/A	ft <sup>2</sup>					
Depth to Invert of Outlet Pipe = Outlet Pipe Diameter =	Zone 3 Restrictor 0.00 18.00	estrictor Plate, or R Not Selected N/A N/A	ectangular Orifice) ft (distance below b inches	asin bottom at Stage	<u>Ca</u> = 0 ft) O Outle	lculated Parameters utlet Orifice Area = t Orifice Centroid =	s for Outlet Pipe w/ Zone 3 Restrictor 0.18 0.14	/ Flow Restriction Pl Not Selected N/A N/A	ft <sup>2</sup>					
Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert =	Zone 3 Restrictor 0.00 18.00 2.80	estrictor Plate, or R Not Selected N/A N/A	ectangular Orifice) ft (distance below b inches inches	asin bottom at Stage Half-Cent	Ca = 0 ft) O Outle ral Angle of Restric	lculated Parameter; utlet Orifice Area = t Orifice Centroid = tor Plate on Pipe =	s for Outlet Pipe w/ Zone 3 Restrictor 0.18 0.14 0.81	/ Flow Restriction Pl Not Selected N/A N/A N/A	ft <sup>2</sup> ft <sup>2</sup> feet radians					
Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert =	Zone 3 Restrictor 0.00 18.00 2.80	estrictor Plate, or R Not Selected N/A N/A	ectangular Orifice) ft (distance below b inches inches	asin bottom at Stage Half-Cent	<u>Ca</u> = 0 ft) O Outle ral Angle of Restric	lculated Parameter: utlet Orifice Area = t Orifice Centroid = tor Plate on Pipe =	s for Outlet Pipe w/ Zone 3 Restrictor 0.18 0.14 0.81	/ Flow Restriction Pl Not Selected N/A N/A N/A	ft <sup>2</sup> <u>ate</u> ft <sup>2</sup> feet radians					
Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or	Zone 3 Restrictor 0.00 18.00 2.80 <u>Trapezoidal)</u>	estrictor Plate, or R Not Selected N/A N/A	ectangular Orifice) ft (distance below b inches inches	asin bottom at Stage Half-Cent	<u>Ca</u> = 0 ft) O Outle ral Angle of Restric	Iculated Parameter: utlet Orifice Area = t Orifice Centroid = tor Plate on Pipe =	s for Outlet Pipe w/ Zone 3 Restrictor 0.18 0.14 0.81 <u>Calculated Parame</u>	/ Flow Restriction Pl Not Selected N/A N/A N/A ters for Spillway	ft <sup>2</sup> ate ft <sup>2</sup> feet radians					
Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = <u>User Input: Emergency Spillway (Rectangular or</u> Spillway Invert Stage=	Zone 3 Restrictor 0.00 18.00 2.80 <u>Trapezoidal)</u> 5.00	Not Selected N/A N/A N/A ft (relative to basin	ectangular Orifice) ft (distance below b inches inches bottom at Stage =	asin bottom at Stage Half-Cent = 0 ft)	<u>Ca</u> = 0 ft) O Outle ral Angle of Restric Spillway D	Iculated Parameter: utlet Orifice Area = t Orifice Centroid = tor Plate on Pipe = vesign Flow Depth=	s for Outlet Pipe w/ Zone 3 Restrictor 0.18 0.14 0.81 <u>Calculated Parame</u> 0.31	/ Flow Restriction Pl Not Selected N/A N/A N/A ters for Spillway feet	ft <sup>2</sup> ate ft <sup>2</sup> feet radians					
Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = <u>User Input: Emergency Spillway (Rectangular or</u> Spillway Invert Stage = Spillway Crest Length =	Zone 3 Restrictor       0.00       18.00       2.80       Trapezoidal)       5.00       20.00	Not Selected N/A N/A N/A ft (relative to basin feet	ectangular Orifice) ft (distance below b inches inches bottom at Stage =	asin bottom at Stage Half-Cent = 0 ft)	<u>Ca</u> = 0 ft) O Outle ral Angle of Restric Spillway D Stage at T	Iculated Parameter: utlet Orifice Area = t Orifice Centroid = tor Plate on Pipe = esign Flow Depth= Fop of Freeboard =	s for Outlet Pipe w/ Zone 3 Restrictor 0.18 0.14 0.81 <u>Calculated Parame</u> 0.31 6.31	/ Flow Restriction Pl Not Selected N/A N/A N/A ters for Spillway feet feet	ft <sup>2</sup> ate ft <sup>2</sup> feet radians					
Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = <u>User Input: Emergency Spillway (Rectangular or</u> Spillway Invert Stage= Spillway Crest Length = Spillway End Slopes =	Zone 3 Restrictor       0.00       18.00       2.80       Trapezoidal)       5.00       20.00       4.00	Restrictor Plate, or R Not Selected N/A N/A N/A ft (relative to basin feet H:V	ectangular Orifice) ft (distance below b inches inches bottom at Stage =	asin bottom at Stage Half-Cent = 0 ft)	<u>Ca</u> = 0 ft) O Outle ral Angle of Restric Spillway D Stage at 1 Basin Area at 1	Iculated Parameter: utlet Orifice Area = t Orifice Centroid = tor Plate on Pipe = Design Flow Depth= Fop of Freeboard = Fop of Freeboard =	s for Outlet Pipe w/ Zone 3 Restrictor 0.18 0.14 0.81 <u>Calculated Parame</u> 0.31 6.31 0.27	/ Flow Restriction Pl Not Selected N/A N/A N/A ters for Spillway feet feet acres	ft <sup>2</sup> ate ft <sup>2</sup> feet radians					
Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = <u>User Input: Emergency Spillway (Rectangular or</u> Spillway Invert Stage= Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface =	Zone 3 Restrictor       0.00       18.00       2.80       Trapezoidal)       5.00       20.00       4.00       1.00	Restrictor Plate, or R Not Selected N/A N/A ft (relative to basin feet H:V feet	ectangular Orifice) ft (distance below b inches inches h bottom at Stage =	asin bottom at Stage Half-Cent - 0 ft)	<u>Ca</u> = 0 ft) O Outle ral Angle of Restric Spillway E Stage at T Basin Area at T Basin Volume at T	Iculated Parameter: utlet Orifice Area = t Orifice Centroid = tor Plate on Pipe = Design Flow Depth= Top of Freeboard = Top of Freeboard =	s for Outlet Pipe w/ Zone 3 Restrictor 0.18 0.14 0.81 Calculated Parame 0.31 6.31 0.27 0.81	/ Flow Restriction Pl Not Selected N/A N/A N/A ters for Spillway feet feet acres acres acre-ft	ft <sup>2</sup> ate ft <sup>2</sup> feet radians					
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# DETENTION BASIN OUTLET STRUCTURE DESIGN Outflow Hydrograph Workbook Filename:

Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.06	0.01	0.14
	0:15:00	0.00	0.00	0.50	0.81	1.00	0.67	0.83	0.82	1.08
	0:25:00	0.00	0.00	3.28	2.18	2.56	3.25	3.73	2.01	2.47
	0:30:00	0.00	0.00	3.59	4.77	5.63	7.03	8.68	10.03	13.05
	0:35:00	0.00	0.00	3.11	4.03	4.71	7.49	9.13	11.37	14.56
	0:40:00	0.00	0.00	2.65	3.36	3.92	6.68	8.15	10.07	12.93
	0:45:00	0.00	0.00	2.13	2.76	3.24	5.55	6.73	8.62	11.12
	0:55:00	0.00	0.00	1.76	2.34	2.69	4.67	5.62	5.79	7.45
	1:00:00	0.00	0.00	1.31	1.70	2.00	3.11	3.68	4.90	6.31
	1:05:00	0.00	0.00	1.12	1.44	1.71	2.61	3.06	4.21	5.43
	1:10:00	0.00	0.00	0.88	1.24	1.48	2.06	2.39	3.15	4.02
	1:15:00	0.00	0.00	0.74	1.07	1.36	1.63	1.86	2.32	2.92
	1:25:00	0.00	0.00	0.66	0.96	1.24	1.30	1.47	1.68	2.10
	1:30:00	0.00	0.00	0.60	0.85	0.99	0.95	1.07	1.08	1.32
	1:35:00	0.00	0.00	0.58	0.82	0.92	0.84	0.95	0.93	1.13
	1:40:00	0.00	0.00	0.57	0.73	0.87	0.77	0.87	0.84	1.01
	1:45:00	0.00	0.00	0.56	0.66	0.84	0.73	0.82	0.77	0.92
	1:55:00	0.00	0.00	0.30	0.58	0.81	0.70	0.76	0.73	0.87
	2:00:00	0.00	0.00	0.41	0.54	0.69	0.66	0.75	0.71	0.84
	2:05:00	0.00	0.00	0.29	0.38	0.48	0.46	0.52	0.49	0.59
	2:10:00	0.00	0.00	0.20	0.26	0.33	0.32	0.36	0.34	0.40
	2:15:00	0.00	0.00	0.13	0.17	0.23	0.22	0.24	0.23	0.27
	2:25:00	0.00	0.00	0.09	0.07	0.15	0.14	0.10	0.10	0.18
	2:30:00	0.00	0.00	0.03	0.05	0.06	0.06	0.06	0.06	0.07
	2:35:00	0.00	0.00	0.02	0.02	0.03	0.03	0.03	0.03	0.04
	2:40:00	0.00	0.00	0.01	0.01	0.01	0.01	0.01	0.01	0.01
	2:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:25:00 5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	6.00.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

MHFD-Detention, Version 4.04 (February 2021)

Summary Stage-Area-Volume-Discharge Relationships The user can create a summary S-A-V-D by entering the desired stage increments and the remainder of the table will populate automatically. The user should graphically compare the summary S-A-V-D table to the full S-A-V-D table in the chart to confirm it captures all key transition points.

0.1		1 A A A A A A A A A A A A A A A A A A A					2
Stage - Storage	Stage	Area	Area	Volume	Volume	Total Outflow	
Description	[ft]	[ft <sup>2</sup> ]	[acres]	[ft <sup>3</sup> ]	[ac-ft]	[cfs]	
6431	0.00	0	0.000	0	0.000	0.00	For best results, include the
6432	1.00	447	0.010	223	0.005	0.01	stages of all grade slope
6433	2.00	3,633	0.083	2,263	0.052	0.03	from the S-A-V table on
6434	3.00	5,896	0.135	7,028	0.161	0.08	Sheet 'Basin'.
6435	4.00	9.044	0.169	21.868	0.314	0.20	Also include the inverts of all
6436	6.00	10.876	0.250	31,828	0.731	71.64	outlets (e.g. vertical orifice,
6538	7.00	13,042	0.299	43,787	1.005	226.22	overflow grate, and spillway,
							where applicable).
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Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

## POND A FOREBAY NOTCH

	Highlighted	
= Sharp	Depth (ft)	= 0.72
= 0.25	Q (cfs)	= 0.510
= 1.25	Area (sqft)	= 0.18
	Velocity (ft/s)	= 2.83
	Top Width (ft)	= 0.25
= 3.33		
Known Q		
= 0.51		
	= Sharp = 0.25 = 1.25 = 3.33 Known Q = 0.51	Highlighted= SharpDepth (ft)= 0.25Q (cfs)= 1.25Area (sqft) Velocity (ft/s) Top Width (ft)= 3.33Known Q= 0.51


Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

## POND B FOREBAY NOTCH

Rectangular Weir		Highlighted	
Crest	= Sharp	Depth (ft)	= 0.66
Bottom Length (ft)	= 0.25	Q (cfs)	= 0.450
Total Depth (ft)	= 1.25	Area (sqft)	= 0.17
		Velocity (ft/s)	= 2.71
Calculations		Top Width (ft)	= 0.25
Weir Coeff. Cw	= 3.33		
Compute by:	Known Q		
Known Q (cfs)	= 0.45		
Bottom Length (ft) Total Depth (ft) Calculations Weir Coeff. Cw Compute by: Known Q (cfs)	= 0.25 = 1.25 = 3.33 Known Q = 0.45	Q (cfs) Area (sqft) Velocity (ft/s) Top Width (ft)	= 0.4 = 0.7 = 2.7 = 0.7





Nyloplast 3' x 3' Road & Highway Inlet Capacity Chart

3130 Verona Avenue • Buford, GA 30518 (866) 888-8479 / (770) 932-2443 • Fax: (770) 932-2490 © Nyloplast Inlet Capacity Charts June 2012

Nyloplast

100-year peak flow to pond (SF-3): Pond A: 25.6 cfs Pond B: 22.6 cfs Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

## POND B SPILLWAY (Q100 = 22.6 CFS PER SF-3 MAJOR (RATIONAL CALCULATIONS))

Trapezoidal Weir		Highlighted	
Crest	= Sharp	Depth (ft)	= 0.49
Bottom Length (ft)	= 20.00	Q (cfs)	= 22.60
Total Depth (ft)	= 1.50	Area (sqft)	= 10.76
Side Slope (z:1)	= 4.00	Velocity (ft/s)	= 2.10
		Top Width (ft)	= 23.92
Calculations			
Weir Coeff. Cw	= 3.10		
Compute by:	Known Q		
Known Q (cfs)	= 22.60		

## Depth (ft)POND B SPILLWAY (Q100 = 22.6 CFS PER SF-3 MAJOR (RATIONAL CALCULATIONS))Depth (ft)



April 2021

## Appendix E Reference Material



## El Paso County Drainage Basin Fees

Resolution No. 19-441

Basin	Receiving	Year	Drainage Basin Name	2020 Drainage Fee	2020 Bridge Fee
Number	Waters	Studied		(per Impervious Acre)	(per Impervious Acre)
Drainage Basins with	<u>n DBPS's:</u>				
CHMS0200	Chico Creek	2013	Haegler Ranch	\$10,737	\$1,585
CHWS1200	Chico Creek	2001	Bennett Ranch	\$12,020	\$4,611
CHWS1400	Chico Creek	2013	Falcon	\$30,807	\$4,232
FOFO2000	Fountain Creek	2001	West Fork Jimmy Camp Creek	\$13,066	\$3,866
FOFO2600	Fountain Creek	1991*	Big Johnson / Crews Gulch	\$19,084	\$2,464
FOFO2800	Fountain Creek	1988*		\$19,084	\$0
	Fountain Creek	1988"	Security Windmill Culob	\$19,084	\$U \$296
FOF03000 FOF03100 / FOF03200	Fountain Creek	1088*	Carson Street / Little Johnson	\$19,004	\$200 ¢0
FOF03400	Fountain Creek	1984*	Peterson Field	\$13,764	\$0 \$1 044
FOFO3600	Fountain Creek	1991*	Fisher's Canvon	\$19,084	\$0
FOFO4000	Fountain Creek	1996	Sand Creek	\$19,698	\$8,057
FOFO4200	Fountain Creek	1977	Spring Creek	\$9,897	\$0
FOFO4600	Fountain Creek	1984*	Southwest Area	\$19,084	\$0
FOFO4800	Fountain Creek	1991	Bear Creek	\$19,084	\$1,044
FOFO5400	Fountain Creek	1977	21st Street	\$5,742	\$0
FOFO5600	Fountain Creek	1964	19th Street	\$3,756	\$0
FOFO5800	Fountain Creek	1964	Camp Creek	\$2,115	\$0 \$0
	Monument Creek	1986*	Mesa	\$9,982	\$U #205
FOMO1000	Monument Creek	1981	Douglas Creek	\$12,001	\$205 ¢286
	Monument Creek	1977	Pope's Bluff	\$12,320 \$3,823	\$200 \$652
FOMO1600	Monument Creek	1970	South Rockrimmon	\$3,823 \$4,486	\$052 \$0
FOMO1800	Monument Creek	1973	North Rockrimmon	\$5 742	\$0
FOMO2000	Monument Creek	1971	Pulpit Rock	\$6.328	\$0
FOMO2200	Monument Creek	1994	, Cottonwood Creek / S. Pine	\$19,084	\$1,044
FOMO2400	Monument Creek	1966	Dry Creek	\$15,065	\$545
FOMO3600	Monument Creek	1989*	Black Squirrel Creek	\$8,664	\$545
FOMO3700	Monument Creek	1987*	Middle Tributary	\$15,925	\$0
FOMO3800	Monument Creek	1987*	Monument Branch	\$19,084	\$0
FOMO4000	Monument Creek	1996	Smith Creek	\$7,780	\$1,044
FOMO4200	Monument Creek	1989*	Black Forest	\$19,084	\$520
FOMO5200	Monument Creek	1993*	Dirty Woman Creek	\$19,084	\$1,044
FOMO5300	Fountain Creek	1993"	Crystal Creek	\$19,084	\$1,044
Miscellaneous Draina	age Basins: 1				
CHBS0800	Chico Creek		Book Ranch	\$17,906	\$2,592
CHEC0400	Chico Creek		Upper East Chico	\$9,755	\$283
CHWS0200	Chico Creek		Telephone Exchange	\$10,718	\$251
CHWS0400	Chico Creek		Livestock Company	\$17,655	\$210
CHWS0600	Chico Creek		West Squirrel	\$9,203	\$3,819
CHWS0800	Chico Creek		Solberg Ranch	\$19,084	\$U \$0
F0F01200	Fountain Creek		Crooked Canyon	\$0,701 \$4,810	\$U €290
FOFO1400	Fountain Creek		Sand Canvon	\$3,475	\$280 \$0
	Fountain Crock		limmy Comp Crock <sup>3</sup>	¢0,+70	¢0
	Fountain Creek		Fort Carson	\$19,084 \$15,065	\$893 \$545
FOFO2700	Fountain Creek		West Little Johnson	\$13,000	\$045 \$0
FOF03800	Fountain Creek		Stratton	\$9 154	\$409
FOFO5000	Fountain Creek		Midland	\$15.065	\$545
FOFO6000	Fountain Creek		Palmer Trail	\$15,065	\$545
FOFO6800	Fountain Creek		Black Canyon	\$15,065	\$545
FOMO4600	Monument Creek		Beaver Creek	\$11,409	\$0
FOMO3000	Monument Creek		Kettle Creek	\$10,305	\$0
FOMO3400	Monument Creek		Elkhorn	\$1,731	\$0
FOMO5000	Monument Creek		Monument Rock	\$8,272	\$0
FOMO5400	Monument Creek		Palmer Lake	\$13,226	\$0 \$2
	wonument Creek		Raspberry Mountain	\$4,449	\$U \$C
PLPLU200	wonument Creek			\$9,481	\$U
Interim Drainage Bas	sins: 2				
FOF01800	Fountain Creek		Little Fountain Creek	\$2,440	\$0 \$0
FOMO4400 FOMO4800	Monument Creek		Teachout Creek	φ1,004 \$5,245	⊅∪ \$788
				Ψ <b>0</b> , <b>2τ0</b>	φ, σσ

1. The miscellaneous drainage fee previous to September 1999 resolution was the average of all drainage fees for basins with Basin Planning Studies performed within the last 14 years.

2. Interim Drainage Fees are based upon draft Drainage Basin Planning Studies or the Drainage Basin Identification and Fee Estimation Report. (Best available information suitable for setting a fee.)

3. This is an interim fee and will be adjusted when a DBPS is completed. In addition to the Drainage Fee a surety in the amount of \$7,285 per impervious acre shall be provided to secure payment of additional fees in the event that the DBPS results in a fee greater than the current fee. Fees paid in excess of the future revised fee will be reimbursed. See Resolution 06-326 (9/14/06) and Resolution 16-320 (9/07/16).

## SAND CREEK DRAINAGE BASIN PLANNING STUDY

# PRELIMINARY DESIGN REPORT

# CITY OF COLORADO SPRINGS, EL PASO COUNTY, COLORADO



PREPARED FOR:

City of Colorado Springs Department of Comprehensive Planning, Development and Finance Engineering Division 30 S. Nevada Colorado Springs, Colorado 80903

## PREPARED BY:

Kiowa Engineering Corporation 1011 North Weber Colorado Springs, CO 80903

#### **STUDY AREA DESCRIPTION** II.

The Sand Creek drainage basin is a left-bank tributary to the Fountain Creek lying in the west-central portions of El Paso County. Sand Creek's drainage area at Fountain Creek is approximately 54 square miles of which approximately 18.8 square miles are inside the City of Colorado Springs corporate limits. The basin is divided into five major sub-basins, the Sand Creek mainstem, the East Fork Sand Creek, the Central Tributary to East Fork, the West Fork, and the East Fork Subtributary. Figure II-1 shows the location of the Sand Creek basin.

## **Basin Description**

The Sand Creek basin covers a total of 54 square miles in unincorporated El Paso County and Colorado Springs, Colorado. Of this total, approximately 28 square miles is encompassed by the Sand Creek basin, and 26 square miles for the East Fork Sand Creek basin. The basin trends in generally a south to southwesterly direction, entering the Fountain Creek approximately two miles upstream of the Academy Boulevard bridge over Fountain Creek. Two main tributaries drain the basin, those being the mainstem of Sand Creek and East Fork Sand Creek. Development presence in most evident along the mainstream. At this time, approximately 25 percent of the basin is developed. This alternative evaluation focuses upon the Sand Creek basin only.

The maximum basin elevation is approximately 7,620 feet above mean sea level, and falls to approximately 5,790 feet at the confluence with Fountain Creek. The headwaters of the basin originate in the conifer covered areas of The Black Forest. The middle eastern portions of the basin are typified by rolling range land with fair to good vegetative cover associated with semi-arid climates.

#### Climate

This area of El Paso County can be described, in general as high plains, with total precipitation amounts typical of a semi-arid region. Winters are generally cold and dry. Precipitation ranges from 14 to 16 inches per year, with the majority of this precipitation occurring in spring and summer in the form of rainfall. Thunderstorms are common during the summer months, and are typified by quick-moving low pressure cells which draw moisture from the Gulf of Mexico into the region. Average temperatures range from about 30°F in the winter to 75° in the summer. The relative humidity ranges from about 25 percent in the summer to 45 percent in the winter.

## Soils and Geology

Soils within the Sand Creek basin vary between soil types A through D, as identified by the U.S. Department of Agriculture, Soil Conservation Service. The predominant soil groupings are in the Truckton and Bresser soil associations. The soils consist of deep, well drained soils that formed in alluvium and residium, derived from sedimentary rock. The soils have high to moderate infiltration rates, and are extremely susceptible to wind and water erosion where poor vegetation cover exists. In undeveloped areas, the predominance of Type A and B soils give this basin a lower runoff per unit area as compared to basins with soils dominated by Types C and D. Presented on Figure II-2 is the Hydrologic Soil distribution map for the Sand Creek basin.

## Property Ownership and Impervious Land Densities

Property ownership along the major drainageway within the Sand Creek basin vary from public to private. Along the developed reaches, drainage right-of-ways and greenbelts have been dedicated during the development of the adjacent residential and commercial land. Where development has not occurred, the drainageways remain under private ownership with no delineated drainage right-of-way or easements. There are several public parks which abut the mainstem of Sand Creek. Roadway and utility easements abutting or crossing the major drainageways occur most frequently in the developed portions of the basin.

Land use information for the existing and future conditions were reviewed as part of the planning effort. This information is used in the hydrologic analysis to predict runoff rates and volumes for the purposes of facility evaluation. The identification of land uses abutting the drainageways is also useful in the identification of feasible plans for stabilization and aesthetic treatment of the creek. Presented on Figure II-3 is the proposed land use map used in the evaluation of impervious land densities discussed in the hydrologic section of this report. Figure II-3 is not intended to reflect the future zoning or land use policies of the City or the County.

The land use information within the Banning-Lewis Ranch property was obtained from Aries Properties during the time the draft East Fork Sand Creek Drainage Basin Planning Study was being prepared. The land use information was again reviewed with the City of Colorado Springs Department of Planning and was found to be appropriate for use in the estimation of hydrology for the East Fork Basin. The location of future arterial streets and roadways within







Mar. 20, 702

EPC DEVELOPMENT SERVICES

## HANNAH RIDGE AT FEATHERGRASS MASTER DRAINAGE DEVELOPMENT PLAN

November 15, 2007 Project No. 60754

## **PREPARED FOR:**

FEATHERGRASS INVESTMENTS, LLC 4715 North Chestnut Street Colorado Springs, CO 80907 (719) 593-8367

Kenneth P. Driscoll, Manager

## **PREPARED BY:**

M.V.E., Inc. 1903 Lelaray Street, Suite 200 Colorado Springs, CO 80909 (719) 635-5736

discharges of  $Q_5 = 2$  cfs and  $Q_{100} = 5$  cfs. Basin OSA8, on the east side of Akers Drive, drains south onto the eastern section of the property with peak discharges of  $Q_5 = 30$  cfs and  $Q_{100} = 60$  cfs. Flows from Basin OSA3 and a portion of Basin OSA8 enters Akers Drive. The existing Akers Drive and Akers drainage improvements were designed by M.V.E., Inc. and approved by El Paso County D.O.T. in September 2006. The system was designed to capture and convey developed flows in Akers Drive. One 10 ft Type R inlet and one 15 ft Type R inlet, connected by an 18" RCP are installed on the east side of Akers, just north of the Constitution intersection. A 10 ft Type R inlet is located on the west side of Akers. The flows collected by the inlets are discharged at the CBC opening, just to the west, with a 24" RCP. The inlets and connecting pipes are adequate to collect and route developed 100 year flows of 20.9 cfs to the creek. In the 100-year event, bypass flows of 5.1 cfs reaches Constitution and travels west to the sump inlet at the CBC crossing. Off-site basins OSA11, OSA12, and OSA13 contain portions of Constitution Avenue. These basins drain to the existing double 12' x 6' CBC under Constitution Avenue. Runoff from Basin OSA14 drains easterly onto the southern portion of the proposed project located on the south side of Constitution Avenue with flows of  $Q_5 = 14$  cfs and  $Q_{100} = 27$  cfs. Basin OSA14 is currently undeveloped commercial property, just north of the Jessica Heights Filing Nol. 1 residential subdivision. A storm drain pipe from Jessica Heights delivers an additional  $Q_5 = 9.8$  cfs and  $Q_{100} = 18.5$  cfs to the Tributary 6 channel. These flow enter the property and then travel to the creek flowing to the south.

#### IV. ON-SITE DRAINAGE BASINS

The existing site drains southerly and easterly from the old Rock Island Railroad that bounds the property on the north and west. Tributary 6 to the East Fork of Sand Creek runs north to south through the property to Constitution Avenue. Offsite storm discharges from the Tributary enter onsite Basin A4 at Design Point 1 (the existing 7'x7' CBC). The existing channel area from the railroad culvert to existing Electronic Drive will be maintained in nearly existing condition. Basin A4 will contain single family residential development with open space components and produce runoff quantities of  $Q_5 = 41$  cfs and  $Q_{100} = 83$  cfs. Flows from Basin A4, along with the Tributary flows will drain to Design Point 2 at proposed Under Saddle Street. A new CBC beneath the street will allow runoff into Basin A9, where flows will enter a park area by way of an improved channel from the DP 2 culvert. Basin A9 contains single family residential development and open space. Developed runoff discharges of  $Q_5 = 51$  cfs and  $Q_{100} = 109$  cfs are generated by the basin. A storm



## JESSICA HEIGHTS FILING NO. 1 FINAL DRAINAGE REPORT

April 27, 2005 Project No. 60742

## **PREPARED FOR:**

Sand Creek Investments South, LLC % Equity Investments 90 South Cascade, Suite 1500 Colorado Springs, CO 80903

## **PREPARED BY:**

M.V.E., Inc. 1903 Lelaray Street, Suite 200 Colorado Springs, CO 80909 (719) 635-5736

60742Final Drainage Report.wpd-05

roads will be paved county streets within 50 to 80 foot of right-of-ways. Curb & gutter will be constructed on the streets and route storm water flows to storm water inlets. Grading operations will be done in order to improve drainage conditions and to direct runoff to a desired location. Overlot grading will be necessary for subdivision development.

The included **Drainage Map - Developed Condition** shows the proposed road scheme, lot layout, and developed drainage basins with basin designations. The basin sizes and estimated peak storm runoff flows are shown in the table below and on the included map.

	Table 3.1 - Developed	l Condition Hydrolo	gic Data	
	Design Point or Basin	Cumulative Drainage Area (Ac)	5-yr Discharge (cfs)	100-yr Discharge (cfs)
	OSA	0.15	0.6	1.1
	OSB	0.46	1.8	3.3
	OSC	0.88	3.3	6.0
	Al	0.96	2.0	4.0
	A2	5.25	3.2	7.6
	A3	0.51	1.4	2.8
	A4	O.32	1.3	2.3
	B1	2.27	4.1	8.2
DP 2	B2	0.70	2.0	3.8
DP 3a	B3a	0.77	1.7	3.4
DP 3b	B3b	2.53	4.8	9.6
	B3c	1.35	3.2	6.6
DP3	B3+3b+3c	4.65	8.4	16.9
	B4	0.51	1.4	2.7
	B5	1.06	2.5	5.0
DP5	B6	0.53	1.4	2.6
DP6	B8	1.98	3.9	7.8

	Table 3.1 - Developed	Condition Hydrolog	gic Data	
	Design Point or Basin	Cumulative Drainage Area (Ac)	5-yr Discharge (cfs)	100-yr Discharge (cfs)
DP7	В9	1.29	3.3	6.3
DP8	B10	1.75	3.7	7.6
	B11	1.88	3.9	7.9
DP10	B12	2.48	4.9	9.8
DP11	B13	2.30	5.1	10.2
	B14	0.98	2.4	4.9
	B15	0.24	1.1	2.1
	C1	5.99	2.8	6.8
	OSA+OSB+C1	6.19	3.6	8.1
DP1	OSC+B1	3.15	6.6	12.8
	OSC1+B1+B2+B4	4.36	8.7	17.1
DP4	OSC1+B1+B2+B4+B5	5.42	10.3	20.3
	OSC1+B1+B2+B4+B5+B8	7.40	14.0	27.6
	OSC1+B1+B2+B4+B5+B8+B9	8.69	15.2	30.5
DP9	B10+B11	3.63	7.5	15.2
	A1+A2	6.21	4.6	10.6
	B10+B11+B13+B15+A3	6.68	13.8	27.9

The future lot owners in Jessica Heights Filing No. 1 will adhere to proper construction technics and erosion control. The recommendations within this report need to be followed by the new lot owners. We also recommend that the existing down gradient lot owners not construct their homes in existing drainage swales or flow paths.

The developed conditions will route storm water flows over the site in sheet flow and shallow concentrated flow, depending on the topography and the contributing flow areas. These flows will be routed to the streets. The five and one hundred year frequency storm water flows will be collected and routed to the offsite earthen channel.

The nature of this development dictates that some lots will contribute storm flows onto other lots. This cross-lot drainage cannot be avoided. It is the responsibility of the individual lot owners and the building contractors to locate new structures on each lot so that the structures do not interfere with the proposed drainage pathways. The individual lot owners and contractors should provide positive drainage away from all structures. Individual lot owners are also responsible for maintaining their properties in such a manner that does not allow soil movement from one lot to another.

## 3.2 <u>Offsite</u>

The offsite pipe flow will continue to drain easterly. The pipe will be extended easterly and shall, in addition to the offsite flow, carry the proposed pipe flows from Jessica Heights. The small strip of land adjacent to the west boundary of the site shall continue to drain onto the site as defined by Basin OSC to the north and Basin OSB to the south. Basin C1, which is not being developed at this time, will continue to drain to the east. A berm and swale will direct runoff to the northeast where the flow will enter Hannah Ridge Drive and flow north. When Basin C1 is developed, all flows will be collected and piped to the east. Basin A2 is also not to be developed at this time. Basin A2 will continue to drain to the east.

## 3.3 <u>Onsite</u>

Basin OSC overland storm water flows enter the subdivision along the western boundary of Basin B1 and travel easterly overland to Great Sky Road. These flows then travel southerly in the street section of said Great Sky Road to a 10' inlet at Design Point No.1. The inlet intercepts  $Q_5 =$ 4.5 cfs /  $Q_{100}$ = 6.5 cfs of the calculated storm water runoff.

Basin B2 overland storm water flows enter Great Sky Road from the adjacent lots and travel southerly in the street section of said Great Sky Road to a 5' inlet at Design Point No. 2. The inlet intercepts  $Q_5 = 1.4 \text{ cfs} / Q_{100} = 1.9 \text{ cfs}$  of the calculated storm water runoff. This collected inlet runoff flows via a 15" reinforced concrete pipe (RC Pipe) to the 10' inlet at Design Point No. 1. The combined collected flows of Design Point No's 1 & 2 then flow in a 24" RC Pipe which connects to a Type I Manhole along with the extended existing 42" corrugated metal pipe in Palmer Park Boulevard. A 42" RC Pipe continues east in Palmer Park Boulevard.

Basins B3a, B3b and B3c overland storm water flows enter Buffalo Plains Court, Majestic plains Court, and Talus Ridge Drive. These flows travel via street section easterly, westerly, and



PROJECT:

April 2021

## Appendix F Drainage Maps





TributaryAreaPercentImpervious $C_5$ $C_{100}$ $t_c$ $Q_5$ $Q_{100}$ Sub-basin(acres)Impervious $C_5$ $C_{100}$ (min)(cfs)(cfs)EX10.152%0.080.357.90.040.4EX20.462%0.080.358.10.21.2EX34.272%0.080.3514.21.29.0EX41.6219%0.220.455.01.42.7EX65.252%0.080.3514.41.511.1		EXISTING BASIN SUMMARY TABLE						
Sub-basin         (acres)         Impervious         C5         C100         (min)         (cfs)         (cfs)           EX1         0.15         2%         0.08         0.35         7.9         0.04         0.4           EX2         0.46         2%         0.08         0.35         8.1         0.2         1.2           EX3         4.27         2%         0.08         0.35         14.2         1.2         9.0           EX4         1.62         19%         0.22         0.45         17.9         1.1         4.0           EX5         0.37         82%         0.75         0.85         5.0         1.4         2.7           EX6         5.25         2%         0.08         0.35         14.4         1.5         11.1	Tributary	Area	Percent			t <sub>c</sub>	Q₅	<b>Q</b> 100
EX10.152%0.080.357.90.040.4EX20.462%0.080.358.10.21.2EX34.272%0.080.3514.21.29.0EX41.6219%0.220.4517.91.14.0EX50.3782%0.750.855.01.42.7EX65.252%0.080.3514.41.511.1	Sub-basin	(acres)	Impervious	C <sub>5</sub>	C <sub>100</sub>	(min)	(cfs)	(cfs)
EX10.152%0.080.357.90.040.4EX20.462%0.080.358.10.21.2EX34.272%0.080.3514.21.29.0EX41.6219%0.220.4517.91.14.0EX50.3782%0.750.855.01.42.7EX65.252%0.080.3514.41.511.1								
EX20.462%0.080.358.10.21.2EX34.272%0.080.3514.21.29.0EX41.6219%0.220.4517.91.14.0EX50.3782%0.750.855.01.42.7EX65.252%0.080.3514.41.511.1	EX1	0.15	2%	0.08	0.35	7.9	0.04	0.4
EX34.272%0.080.3514.21.29.0EX41.6219%0.220.4517.91.14.0EX50.3782%0.750.855.01.42.7EX65.252%0.080.3514.41.511.1	EX2	0.46	2%	0.08	0.35	8.1	0.2	1.2
EX41.6219%0.220.4517.91.14.0EX50.3782%0.750.855.01.42.7EX65.252%0.080.3514.41.511.1	EX3	4.27	2%	0.08	0.35	14.2	1.2	9.0
EX50.3782%0.750.855.01.42.7EX65.252%0.080.3514.41.511.1	EX4	1.62	19%	0.22	0.45	17.9	1.1	4.0
EX6 5.25 2% 0.08 0.35 14.4 1.5 11.1	EX5	0.37	82%	0.75	0.85	5.0	1.4	2.7
	EX6	5.25	2%	0.08	0.35	14.4	1.5	11.1



# **URBAN COLLECTION AT PALMER VILLAGE EXISTING DRAINAGE MAP**

XISTING DESIGN POINT					
SUMI	MARY T	ABLE			
DP	Q₅	<b>Q</b> <sub>100</sub>			
1	0.04	0.4			
2	0.2	1.2			
3	1.3	9.3			
4	1.3	4.9			
5	1.4	2.7			
6	1.5	11.1			

LEGEND

A B C	I.D.: BASIN A: BASIN B: MINOR C: MAJOR
$\sum_{X}$	DESIGN P
	BASIN DE
6100	EXISTING
6101	EXISTING

 $\Rightarrow$ 





	Tributary         Sub-basin         EX1         EX2         A1         A2         A3         A4         A5         A6         A7         A8         A9         A10         A11	Area (acres) 0.15 0.46 0.78 0.22 0.11 0.62 0.83 0.18 0.46 0.75 0.57 0.57 0.78 0.16	Percent         Impervious         0%         0%         67%         63%         75%         63%         75%         48%         72%         5%         40%	A' SUM C₅ 0.08 0.08 0.65 0.63 0.60 0.65 0.50 0.74 0.60 0.74 0.60 0.44 0.66 0.12 0.41	<b>MARY 1</b> <b>C</b> <sub>100</sub> 0.35 0.35 0.77 0.76 0.74 0.76 0.65 0.84 0.73 0.61 0.77 0.38 0.60	tc         (min)         7.9         8.1         5.5         7.8         6.2         5.2         7.0         7.9         5.8         7.8         6.9         9.4         9.8	Q₅ (cfs) 0.0 0.2 2.6 0.6 0.3 2.0 2.0 0.6 1.3 1.5 1.8 0.4 0.3	Q100 (cfs) 0.2 0.7 5.1 1.3 0.7 4.0 4.2 1.1 2.7 3.5 3.5 3.5 2.1 0.6	PREPARED FOR UNTIL SUCH TIME AS UND AMERICAN HOMES APPROVED BY THE APPROVED BY THE	2. MULACU JINELI APPROPRIATE REVIEMING ENVER, CO 80237 AGENCIES, JR ENGINEERING 720) 977-3827 APPROVES THEIR USE ONLY FOR THE PURPOSES	DN.POCK@MDCH.COM DESIGNATED BY WRITTEN AUTHORIZATION.
	A12	0.13	39% DESK Desig Poin EX1 EX2 1 2 3 4 4 4.1 5 5 5.1 6 7 8	0.40 GN POINT TAB gn Q₅ (cl 0.00 0.2 0.2 0.2 0.2 0.2 0.2 0.	0.59 <b>SUMMAI</b> <b>LE</b> <b>fs) Q</b> <sub>100</sub> (c 4 0.2 4 0.2 5 0.7 3 4.9 0 4.7 0 6.2 4 0.2 5.7 3 4.9 0 4.7 0 5.7 3 9.4 0 4.8 5 5.9 4 5.9 4 5.9	7.8	0.2	0.6	J.R ENGINEERING	A Westrian Company DE	ennial 303–740–9393 • Colorado Springs 719–593–2593 Collins 970–491–9888 • www.jrengineering.com
HWWWH- -6454 -74544 -74544 -74544 -74544 -74544 -74544 -74544 -74544	LEGEN I.D. A C X	BAS I.D. A:E B:C C:C DES	8.1 9 9.1 10 11 12 SIN DESIGN BASIN IDE BASIN AREA 5 100 SIGN POINT	A TION	3 15.0 4 9.2 9 23.9 1 25.7 3 0.6 2 0.6	) )			ВҮ DATE 		Center Ce
30.00' GRAINAGE CASEMENT W	6100 6100 6100- 	EXI EXI PRO PRO PRO PRO EXI PRO	STING INDE STING INTE OPOSED INE OPOSED IN OPOSED SA OPOSED ST OPOSED WA STING FLOV	X CONTO RMEDIATI DEX CON TERMEDIA NITARY ORM SEV ATER LIN V DIRECT	DURS E CONTO TOURS ATE CONT SEWER WER E ION CTION	URS TOURS			H-SCALE 1"=30' No. REVISION V-SCALE N/A	DESIGNED BY RPD	DRAWN BY RPD CHECKED BY
$W = \frac{1}{1}$	30 15 ORIG PREPARED ENGINEERIN	0 INAL SO EER'S UNDER G	30 CALE: 1" = S STA MY DIRECT	30' TEME		Know wh Call	Thats being the second	JR	URBAN COLLECTION AT PALMER VILLAGE	WEST DRAINAGE MAP	









SWALE SECTION NOTES
1. ALL SWALE SECTIONS ARE FACING UPSTREAM (WEST).
2. SEE LANDSCAPE PLANS BY OTHERS FOR PROPOSED SURFACE MATERIAL.

PROPERTY BOUNDARY 14.46' 10.00'	PREPARED FORRICHMOND AMERICAN HOMES4350 S. MONACO STREET4350 S. MONACO STREET4350 S. MONACO STREET4750 S. MONACO STREET500 S. MONACO STREET720) 977-3827JASON.POCK@MDCH.COMADTOCK@MDCH.COMADTOR
B' SWALE B'-B' SECTION SCALE: 1"=2' (HOR), 1"=1' (VERT)	TE  <b>J-R ENGINEERING</b> A westrian Company Centennial 303–740–9393 • Colorado Springs 719–593–2593 Fort Collins 970–491–9888 • wwwjrengineering.com
	1"=2'     No.     REVISION     BY     DA'       1"=1'           01/27/21           Y     RPD
ENGINEER'S STATEMENT PREPARED UNDER MY DIRECT SUPERVISION AND ON BEHALF OF JR ENGINEERING	URBAN COLLECTION AT     H-SCALE       PALMER VILLAGE     V-SCALE       SWALE CROSS SECTIONS     Date       Date     Date



	BASIN BOUNDARY
6100	EXISTING INDEX CONTOURS
	EXISTING INTERMEDIATE CONTOURS
6100	PROPOSED INDEX CONTOURS
	PROPOSED INTERMEDIATE CONTOURS
	AREA TRIBUTARY TO PBMP (9.87 AC)
	OFFSITE AREA TRIBUTARY TO PBMP (0.
	AREA NOT TRIBUTARY TO PBMP (0.97