# Kimley»)Horn 

April 18, 2024

Mr. Louis Ferrante
UDON Holdings, LLC
5801 N. Union Boulevard
Suite 100
Colorado Springs, CO 80918
Re: UDON Rezone Traffic Study
El Paso County, Colorado
Dear Mr. Ferrante:
This traffic study has been prepared for a proposed UDON Rezoning project to be located at 12150 State Highway 94-(SH-94) on the north side of SH-94 and 12265 SH-94 on the south side of SH-94 in El Paso County, Colorado. The existing property contains one residence at $12150 \mathrm{SH}-94$ and one residence at $12265 \mathrm{SH}-94$. Of note, the northern portion of this project at $12150 \mathrm{SH}-94$ is proposed to rezone the existing 15.74 -acre property from Residential Rural (RR5) to Commercial Service (CS). For purposes of this study, it was assumed that the area on the south side of SH-94 would be developed first as phase one with 860 spaces for vehicle, boat, and RV storage. The north side of the development was studied with two alternatives for the full buildout scenario; the proposed use which includes 1,000 storage units and the highest use which includes a 16 fueling position gas station and approximately 150,000 square feet of retail.

A vicinity map illustrating the location of the property is attached as Figure 1. The surrounding area primarily consists of rural residences, vacant and agricultural land, industrial uses, and Aztec Family Raceway. There are auto salvage yards located to the east of the site.

This traffic study identifies the amount of traffic associated with this proposed project and the expected trip distribution and traffic assignment along with an operational analysis for the project access intersection along State Highway 94 (SH-94). The project access to the site is proposed to be located approximately 200 feet west of the existing west access at the 12265 SH-94 site. The existing east access will be closed with development of the project. It is expected that project construction of the development area south of SH-94 will be completed within the next couple years; therefore, analysis was performed for the 2026 Phase 1 horizon. The development area to the north of SH-94 is expected to follow phase 1 by a couple years and was evaluated as a full buildout horizon in 2028. Lastly, a 2045 long-term twenty-year horizon was also evaluated.

## EXISTING ROADWAY NETWORK AND TRAFFIC COUNTS

Regional access to the UDON Rezoning project is provided by SH-94. Direct access to the development will be provided by an access driveway along the south side of SH-94 for the Phase 1 development and an access driveway along the north side of SH-94 to align with the Phase 1 access for the buildout scenario. SH-94 extends primarily east-west with one through lane in each direction with a speed limit of 65 miles per hour eastbound and 60 miles per hour westbound. SH-94 provides a double yellow striped centerline within the project limits. Both Table 4: 2045 Roadway Improvement Projects of the 2016 El Paso County Major Transportation Corridor Plan (MTCP) and the State Highway 94 Access Management Plan show that SH-94 will be widened from two lanes to four lanes within the project limits sometime in the future.


#### Abstract

Existing daily and peak hour bi-directional count data was obtained from CDOT traffic information along SH-94 to the east of Space Village Avenue, which is in nearby vicinity of the existing UDON Rezoning property project access. These counts were collected on Thursday, July 11, 2019 and were conducted in one-hour intervals for 24 hours. These counts were adjusted by the annual growth rate (described in the next section) to calculate existing 2024 volumes. Of note, more recent count data along SH-94 reports less traffic volumes compared to the 2019 traffic counts; therefore, the 2019 count data grown to 2024 was utilized to provide a conservative analysis. The daily counts from the Colorado Department of Transportation (CDOT) Online Transportation Information System (OTIS) were used as a basis for providing a directional split of project traffic. Existing lane configuration, and the existing peak hour counts are shown in attached Figure 2, with count information attached as well.


## UNSPECIFIED DEVELOPMENT TRAFFIC GROWTH

Based on information provided on the website for the Colorado Department of Transportation, the 20year growth factor along SH-94 adjacent to the study area is 1.21 which equates to an annual growth rate of approximately one (1) percent per year. Traffic information from the CDOT Online Transportation Information System (OTIS) is attached. Based on this, a one (1) percent annual growth rate was used to calculate future background traffic volumes at the study area access intersection. This annual growth rate was used to estimate 2026 Phase 1, 2028 Buildout, and long term 2045 background traffic volumes at the key intersection.

## TRIP GENERATION

Site-generated traffic estimates are determined through a process known as trip generation. Rates and equations are applied to the proposed land use to estimate traffic generated by the development during a specific time interval. The acknowledged source for trip generation rates is the Trip Generation Manual ${ }^{1}$ published by the Institute of Transportation Engineers (ITE). ITE has established trip rates in nationwide studies of similar land uses. For this study, Kimley-Horn used the ITE Trip Generation Report average rates for Mini-Warehouse (ITE Code 151) for phase 1 and the proposed buildout, and Shopping Center (ITE Code 820) and Convenience Store/Gas Station (ITE Code 945) for the north development area under the highest use buildout scenario.

Since the highest use buildout scenario is a commercial development, pass-by trips are expected. These pass-by trips are vehicles already on the street network that will be attracted to the project site in route to a final destination.

The UDON Rezoning Phase 1 is expected to generate approximately 156 daily weekday driveway trips, with 10 of these trips occurring during the morning peak hour and 14 trips occurring during the afternoon peak hour. The proposed buildout is expected to generate 336 daily weekday driveway trips, with 23 of these trips occurring during the morning peak hour and 32 trips occurring during the afternoon peak hour.

The UDON Rezoning Highest Use Buildout scenario is expected to generate approximately 9,666 daily weekday driveway trips to the north driveway, with 559 of these trips occurring during the morning peak hour and 874 trips occurring during the afternoon peak hour. Accounting for pass-by, expected net new (non pass-by) trips to the surrounding street network results in approximately 4,970 weekday daily trips, of which 193 trips and 454 trips are anticipated during the weekday morning and afternoon peak hours, respectively. Table 1 summarizes the estimated trip generation for the UDON Rezoning project. The trip generation worksheets are attached.

[^0]Table 1 - UDON Rezoning Project Weekday Traffic Generation

| Land Use and Size | Daily Vehicle Trips | Weekday Vehicle Trips |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | AM Peak Hour |  |  | PM Peak Hour |  |  |
|  |  | In | Out | Total | In | Out | Total |
| Phase 1 - South Development |  |  |  |  |  |  |  |
| Mini-Warehouse (ITE 151) 860 Units | 156 | 5 | 5 | 10 | 7 | 7 | 14 |
| Buildout - Proposed Use (North and South Development) |  |  |  |  |  |  |  |
| Mini-Warehouse (ITE 151) 1,860 Units | 336 | 12 | 11 | 23 | 16 | 16 | 32 |
| Buildout - Highest Use (North Development) |  |  |  |  |  |  |  |
| Shopping Center (ITE 820) 150,000 Square Feet | 5,552 | 78 | 48 | 126 | 245 | 265 | 510 |
| Convenience Store/Gas Station (ITE 945) 16 Fueling Positions | 4,114 | 216 | 217 | 433 | 182 | 182 | 364 |
| Total Project Trips - Highest Use | 9,666 | 294 | 265 | 559 | 427 | 447 | 874 |
| Total Project Trips after Pass-By Highest Use | 4,970 | 107 | 86 | 193 | 220 | 234 | 454 |

## DISTRIBUTION, ASSIGNMENT, AND TOTAL TRAFFIC

Distribution of site traffic was based on the area street system characteristics, existing traffic patterns and volumes, and the proposed access system for the project. As mentioned previously, the traffic volumes from CDOT OTIS were used as a basis for providing a directional split of project traffic. The distribution of traffic is a means to quantify the percentage of site-generated traffic that approaches the site from a given direction and departs the site back to the original source. Project traffic originating from either direction can access the site. As identified from the counts from CDOT OTIS, approximately 63 percent of the UDON Rezone trips arrive from and depart to the west and 37 percent of trips arrive and depart from the east. Figure 3 illustrates the expected non pass-by trip distribution for Phase 1 (South Development), Figure 4 shows the expected non pass-by trip distribution for the proposed buildout (North and South Development), and Figure 5 illustrates the expected non pass-by trip distribution for the highest use buildout (North Development).

Since the highest use buildout scenario is a commercial development, a certain amount of traffic attracted to the site will already be passing by the site. This pass-by distribution is a means to quantify the amount of traffic arriving to the site from a given direction and then leaving the site in the same original direction of travel, continuing the driver's trip. The expected weekday morning and afternoon peak hour pass-by trip distributions were calculated based on existing traffic volumes along SH-94 in the site vicinity. Directional differences in the morning and afternoon peak hours were accounted for in the pass-by distributions as shown in Figures 6 and 7, respectively.

Project traffic assignment was obtained by applying the project trip distribution to the estimated project traffic generation of the development scenarios shown in the trip generation table. The non pass-by traffic assignment is shown in Figure 8 for Phase 1 (South Development), Figure 9 for the proposed buildout (North and South Development), and Figure 10 for the highest use buildout (North Development). The pass-by traffic assignment is shown in Figure 11 for the highest use buildout scenario (North Development).

Site traffic volumes were added to the 2026, 2028, and 2045 background volumes to represent estimated Phase 1, build-out year, and long-term traffic conditions. These total traffic volumes are shown for 2026 Phase 1 in Figure 12, 2028 Proposed Buildout in Figure 13, 2028 Highest Use

Scenario in Figure 14, 2045 Proposed Buildout in Figure 15, and 2045 Highest Use Scenario in Figure 16.

## TRAFFIC OPERATIONS ANALYSIS

Kimley-Horn's analysis of traffic operations in the site vicinity was conducted to determine potential capacity deficiencies at the project key intersections for the 2026 Phase 1, 2028 Buildout, and 2045 long term horizons. The acknowledged source for determining overall capacity is the Highway Capacity Manual.

Capacity analysis results are listed in terms of Level of Service (LOS). LOS is a qualitative term describing operating conditions a driver will experience while traveling on a particular street or highway during a specific time interval. It ranges from A (very little delay) to F (long delays and congestion). For intersections and roadways in this study area, typical traffic study practice identifies overall intersection LOS D and movement or approach LOS E as the minimum thresholds for acceptable operations. The following Table 2 shows the definition of level of service for signalized and unsignalized intersections.

Table 2 - Level of Service Definitions

| Level of <br> Service | Signalized Intersection <br> Average Total Delay <br> (sec/veh) | Unsignalized Intersection <br> Average Total Delay <br> (sec/veh) |
| :---: | :---: | :---: |
| A | $\leq 10$ | $\leq 10$ |
| B | $>10$ and $\leq 20$ | $>10$ and $\leq 15$ |
| C | $>20$ and $\leq 35$ | $>15$ and $\leq 25$ |
| D | $>35$ and $\leq 55$ | $>25$ and $\leq 35$ |
| E | $>55$ and $\leq 80$ | $>35$ and $\leq 50$ |
| F | $>80$ | $>50$ |

## SH-94 Project Access Intersection

With the initial phase, the proposed project access along SH-94 will be a T-intersection with a south leg and will operate with stop control along the northbound exiting approach. With completion of Phase 1 of the rezone project, it is recommended that the northbound access approach be designated with one lane for all movements and be stop-controlled with installation of a R1-1 "STOP" sign. With the proposed buildout by 2028 on the north side of SH-94, it is recommended that the southbound access be designated with one lane for all movements and be stop-controlled with installation of a R1-1 "STOP" sign.

With the highest use scenario, it is anticipated that an eastbound left turn lane, a westbound right turn lane, and a southbound to westbound right turn acceleration will be needed based on CDOT standards. With these improvements, the northbound and southbound approaches are anticipated to operate poorly at LOS F under stop control during both the morning and afternoon peak hours in 2028. A signal warrant analysis was completed for this intersection, and it was found that a signal is warrant by 2028 for this highest use scenario. Therefore, it is recommended that this intersection be signalized if the highest use scenario is the future development program. Signal warrant analysis worksheets are attached. If this intersection is signalized, it is recommended that left turn lanes be designated on all four approaches. With these improvements this intersection is anticipated to operate acceptably throughout 2028.

[^1]
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Both Table 4: 2045 Roadway Improvement Projects of the 2016 El Paso County Major Transportation Corridor Plan (MTCP) and the State Highway 94 Access Management Plan show that SH-94 will be widened from two lanes to four lanes within the project limits sometime in the future. Therefore, this intersection was analyzed with two eastbound and westbound through lanes for the 2045 horizon in both scenarios. With the recommended improvements and the addition of project traffic, all movements at the proposed access intersection are expected to operate acceptably the 2045 horizon for both buildout scenarios. Table 3 provides the results of the level of service analysis for this intersection with LOS worksheets attached.

Table 3 - SH-94 and Project Access Intersection LOS Results

| Scenario | AM Peak Hour |  | PM Peak Hour |  |
| :---: | :---: | :---: | :---: | :---: |
|  | $\begin{aligned} & \text { Delay } \\ & \text { (sec/veh) } \end{aligned}$ | LOS | Delay (sec/veh) | LOS |
| Phase 1 - South Development |  |  |  |  |
| 2026 Background Plus Project |  |  |  |  |
| Northbound Approach | 27.3 | D | 22.9 | C |
| Westbound Left | 10.3 | B | 8.2 | A |
| Buildout - Proposed Use |  |  |  |  |
| 2028 Background Plus Project |  |  |  |  |
| Northbound Approach | 35.9 | E | 30.8 | D |
| Eastbound Left | 8.4 | A | 10.5 | B |
| Westbound Left | 10.4 | B | 8.3 | A |
| Southbound Approach | 23.3 | C | 27.3 | D |
| 2045 Background Plus Project \# |  |  |  |  |
| Northbound Approach | 38.5 | E | 21.9 | C |
| Eastbound Left | 8.7 | A | 11.5 | B |
| Westbound Left | 11.4 | B | 8.5 | A |
| Southbound Approach | 17.9 | C | 26.8 | D |
| Buildout - Highest Use |  |  |  |  |
| 2028 Background Plus Project \#\# |  |  |  |  |
| Northbound Approach | 56.0 | F | 60.8 | F |
| Eastbound Left | 9.4 | A | 14.0 | B |
| Westbound Left | 9.8 | A | 8.1 | A |
| Southbound Approach | >300 | F | >300 | F |
| 2028 Background Plus Project \#\#\# | 25.0 | C | 27.9 | C |
| 2045 Background Plus Project \#\#\#\# | 43.8 | D | 51.9 | D |

\# = Two eastbound and westbound through lanes
\#\# = Eastbound left, westbound left and right, northbound and southbound approaches with left turn lane and shared through/right turn lane, southbound to westbound right turn acceleration lane \#\#\# = \#\# + Signalized
\#\#\#\# = \#\#\# + Two eastbound and westbound through lanes

## CDOT ACCESS PERMIT AND TURN LANE EVALUATION

The need or threshold for requiring an access permit along CDOT roadways occurs when a new access is proposed or if project traffic is anticipated to increase existing access traffic volumes by more than 20 percent. Therefore, it is believed that an access permit will be needed for both the north and south accesses along $\mathrm{SH}-94$ for both development scenarios.

Since SH-94 is a state owned and maintained facility, it is recommended that auxiliary turn lanes along SH-94 be constructed in accordance with the current CDOT State Highway Access Code (SHAC). CDOT categorizes the segment of SH-94 adjacent to the property as NR-A: Non-Rural

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Principal Highway. SH-94 has a posted speed limit of 65 miles per hour (mph) eastbound and 60 miles per hour westbound within the project limits. According to the State Highway Access Code for category NR-A roadways, the following thresholds apply:

- A left turn deceleration lane is required for any access with a projected average peak hour left turn ingress volume greater than 10 vehicles per hour (vph).
- A right turn deceleration lane is required for any access with a projected peak hour right turning volume greater than 25 vph.
- A right turn acceleration lane is required for any access with a projected peak hour right turning volume greater than 50 vph when the posted speed on the highway is greater than 40 mph.

Based on traffic projections and the above thresholds, auxiliary turn lane requirements were calculated for the SH-94 full movement access to the property. As such, turn lane requirements at the study area intersection along SH-94 are as follows:

## Proposed Buildout:

- An eastbound right turn deceleration lane is not warranted based on projected 2028 background plus project traffic being four (4) right turns during the peak hour and the threshold being 25 vehicles per hour.
- An eastbound left turn deceleration lane is not warranted based on projected 2028 background plus project traffic being six (6) left turns during the peak hour and the threshold being 10 vehicles per hour.
- A westbound right turn deceleration lane is not warranted based on projected 2028 background plus project traffic being three (3) right turns during the peak hour and the threshold being 25 vehicles per hour.
- A westbound left turn deceleration lane is not warranted based on projected 2028 background plus project traffic being three (3) left turns during the peak hour and the threshold being 10 vehicles per hour.
- An eastbound acceleration lane along SH-94 from the project access northbound right turn is not warranted based on projected 2028 background plus project traffic being three (3) right turns during the peak hour and the threshold being 50 vehicles per hour.
- A westbound acceleration lane along SH-94 from the project access southbound right turn is not warranted based on projected 2028 background plus project traffic being six (6) right turns during the peak hour and the threshold being 50 vehicles per hour.


## Highest Use:

- An eastbound right turn deceleration lane is not warranted based on projected 2028 background plus project traffic being four (4) right turns during the peak hour and the threshold being 25 vehicles per hour.
- An eastbound left turn deceleration lane is warranted based on projected 2028 background plus project traffic being 201 left turns during the peak hour. Since SH-94 has a category of NR-A, the left turn lane requirement is deceleration and storage lengths. Based on the 65-mile per hour speed limit, the deceleration lane length is 800 feet plus 200 feet of storage for a total length of 1,000 feet (which includes the 300-foot taper). Therefore, it is recommended that this lane be constructed to 700 feet plus 300-foot taper by 2028.
- A westbound right turn deceleration lane is warranted based on projected 2028 background plus project traffic being 226 right turns during the peak hour. Since $\mathrm{SH}-94$ has a category of NR-A the right turn lane requirement is deceleration length. Based on the 60-mile per hour speed limit, the deceleration lane length is 700 feet. Therefore, it is recommended that this lane be constructed to 700 feet (which includes the 300-foot taper) by 2028.
- A westbound left turn deceleration lane is not warranted based on projected 2028 background plus project traffic being three (3) right turns during the peak hour and the threshold being 25
vehicles per hour. However, if an eastbound left turn lane is constructed at this access intersection, a substandard westbound left turn lane could be implemented within the shadow of the widening needed in association with the eastbound left turn lane.
- An eastbound acceleration lane along SH-94 from the project access northbound right turn is not warranted based on projected 2028 background plus project traffic being three (3) right turns during the peak hour and the threshold being 50 vehicles per hour.
- A westbound acceleration lane along SH-94 from the project access southbound right turn is warranted based on projected 2028 background plus project traffic being 296 right turns during the peak hour. Since SH-94 has a category of NR-A the right turn lane requirement is deceleration length. Based on the 60-mile per hour speed limit, the acceleration lane length is 1,170 feet. Therefore, it is recommended that this lane be constructed to 1,170 feet (which includes the 300-foot taper) by 2028 .


## SIGHT DISTANCE EVALUATION

Access for this project will be approximately 625 feet from the westernmost property line. It is believed that this access is appropriate at this location to provide the necessary sight distance needed. It is recommended that appropriate sight distance triangles be provided at all site access points to give drivers exiting the development areas a clear view of oncoming traffic. Landscaping and objects within sight triangles must not obstruct drivers' views of the adjacent travel lanes. Intersection sight distances for left turn from stop and right turn from stop were analyzed for the proposed project accesses along SH-94.

With AASHTO standards and a design speed of 65 miles per hour eastbound along SH-94, the intersection sight distance for a vehicle turning left from stop is 720 feet, while the sight distance for a vehicle turning right from stop is 625 feet. Therefore, all obstructions for left turning vehicles from stop should be clear to the right within the triangle created with a vertex point located 14.5 feet from the edge of the major road traveled way (typical position of the minor road driver's eye when stopped) and a line of sight distance of 720 feet located in the middle of the eastbound through lane along SH94. Likewise, all obstructions for right turning vehicles from stop should be clear to the left within the triangle created with a vertex point located 14.5 feet from the edge of the major road traveled way and a line of sight distance of 625 feet located in the middle of the westbound through lane along SH 94.

With AASHTO standards and a design speed of 60 miles per hour westbound along $\mathrm{SH}-94$, the intersection sight distance for a vehicle turning left from stop is 665 feet, while the sight distance for a vehicle turning right from stop is 575 feet. Therefore, all obstructions for left turning vehicles from stop should be clear to the right within the triangle created with a vertex point located 14.5 feet from the edge of the major road traveled way (typical position of the minor road driver's eye when stopped) and a line of sight distance of 665 feet located in the middle of the westbound through lane along SH94. Likewise, all obstructions for right turning vehicles from stop should be clear to the left within the triangle created with a vertex point located 14.5 feet from the edge of the major road traveled way and a line of sight distance of 575 feet located in the middle of the eastbound through lane along SH94.

## BICYCLE AND PEDESTRIAN ACCESS

Bicycle and pedestrian access evaluations were conducted for the UDON Rezone project. This focused on the areas of SH-94 adjacent to the site development areas. The following provides a description of the assessment.

Adjacent to the site, there are no bicycle lanes or sidewalks along SH-94. Although there are no bicycle lanes or sidewalks that exist within the study area there are very few destinations along SH-
94. By 2045, the MTCP states that the secondary regional trail is proposed along SH-94 within the project limits.

## CONCLUSIONS AND RECOMMENDATIONS

In summary, this traffic study provides project traffic generation estimates to identify potential project traffic related impacts on the local street system with the proposed UDON Rezoning project for the proposed buildout and highest use scenarios. Kimley-Horn believes the proposed UDON Rezoning project will be successfully incorporated into the existing and future roadway network.

Based on the results of this study and the proposed use scenario, it is recommended that the access intersection along SH-94 be stop controlled with a R1-1 "STOP" sign installed on the northbound and southbound exiting approaches. Of note, this access will initially be a T-intersection with only the south area developing in Phase 1. The recommended intersection lane configurations and control for the project development are illustrated in Figure 17 for the 2026 horizon and Figure 18 for the 2028 horizon.

If the alternative highest use scenario develops, it is recommended that the access intersection along SH-94 be signalized with 700 -foot plus 300 -foot taper eastbound left turn lane, a 150 -foot westbound left turn lane, a 400 -foot plus 300 -foot taper westbound right turn lane, a 870 -foot with 300 -foot taper westbound acceleration lane from the southbound right turn, and a left turn lane on the northbound and southbound approaches exiting the site. The recommended intersection lane configurations and control for the project development under the highest use scenario are illustrated in Figure 19 for the 2028.

By 2045, it is anticipated that SH-94 will be reconstructed with two through lanes in each direction. The recommended 2045 intersection lane configurations and control for the project development are illustrated in Figure $\mathbf{2 0}$ for the proposed buildout and Figure $\mathbf{2 1}$ for the highest use scenario. If you have any questions or require anything further, please feel free to call me at (720) 943-9962.

Sincerely,
KIMLEY-HORN AND ASSOCIATES, INC.


Jeffrey R. Planck, P.E.
Project Traffic Engineer


## Kimley»Horn

## Traffic Engineer's Statement

The attached traffic report and supporting information were prepared under my responsible charge and they comport with the standard of care. So far as is consistent with the standard of care, said report was prepared in general conformance with the criteria established by the County for traffic reports.

Jeffrey R. Planck, P.E., PE \#53006
April 18, 2024

Developer's Statement
I, the Developer, have read and will comply with all commitments made on my behalf within this report.

Mr. Louis Ferrante Date
UDON Holdings, LLC
5801 N. Union Boulevard
Suite 100
Colorado Springs, CO 80918

Figures


FIGURE 1
UDON REZONE
EL PASO COUNTY, COLORADO
VICINITY MAP
Kimley"Horn

## 



FIGURE 2
UDON REZONE
EL PASO COUNTY, COLORADO
2024 EXISTING LANE CONFIGURATIONS AND TRAFFIC VOLUMES

## LEGEND

$X X X(X X X)$

## $X X, X 00$

Estimated Daily Traffic Volume
Study Area Key Intersection
Weekday AM (PM)
Peak Hour Traffic Volumes


Roadway Speed Limit

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## Kimley Horm



FIGURE 5
UDON REZONE
EL PASO COUNTY, COLORADO
NON PASS-BY PROJECT TRIP
DISTRIBUTION - NORTH AREA HIGHEST USE

## LEGEND

(X) Study Area Key Intersection
$\xrightarrow{\text { XX\% External Trip Distribution Percentage }}$
Entering[Exiting]
Trip Distribution Percentage

## $\widehat{N}$



FIGURE 6
UDON REZONE
EL PASO COUNTY, COLORADO
AM PASS-BY PROJECT TRIP
DISTRIBUTION - NORTH AREA HIGHEST USE

## LEGEND

(X) Study Area Key Intersection
$\xrightarrow{\text { XX\% External Trip Distribution Percentage }}$
Entering[Exiting]
Trip Distribution Percentage

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FIGURE 7
UDON REZONE
EL PASO COUNTY, COLORADO
PM PASS-BY PROJECT TRIP
DISTRIBUTION - NORTH AREA HIGHEST USE

## LEGEND

(X) Study Area Key Intersection
$\xrightarrow{\text { XX\% External Trip Distribution Percentage }}$
Entering[Exiting]
Trip Distribution Percentage

## Kimley Horm



FIGURE 8
UDON REZONE
EL PASO COUNTY, COLORADO
NON PASS-BY PROJECT TRAFFIC ASSIGNMENT - SOUTH AREA

## LEGEND

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FIGURE 9
UDON REZONE
EL PASO COUNTY, COLORADO
NON PASS-BY PROJECT TRAFFIC
ASSIGNMENT - PROPOSED BUILDOUT

## LEGEND

XXX(XXX)
Weekday AM (PM)
Peak Hour Traffic Volumes

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FIGURE 10
UDON REZONE
EL PASO COUNTY, COLORADO
NON PASS-BY PROJECT TRAFFIC ASSIGNMENT - NORTH AREA HIGHEST USE

## LEGEND

(X) Study Area Key Intersection
$X X X(X X X)$
Weekday AM (PM)
Peak Hour Traffic Volumes
$X X, X 00$ Estimated Daily Traffic Volume

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| :---: | :---: |
| $\begin{array}{r} 125(62) \\ -125(-62) \end{array} \rightarrow$ |  |
| SH-94 | ACCESS |

FIGURE 11
UDON REZONE
EL PASO COUNTY, COLORADO
PASS-BY PROJECT TRAFFIC
ASSIGNMENT - NORTH AREA HIGHEST USE

## LEGEND

## 



FIGURE 12
UDON REZONE
EL PASO COUNTY, COLORADO
2026 TOTAL TRAFFIC VOLUMES PHASE 1

## LEGEND

(X) Study Area Key Intersection
$X X X(X X X)$
Weekday AM (PM)
Peak Hour Traffic Volumes
XX,X00 Estimated Daily Traffic Volume

## 



## LEGEND

FIGURE 13
UDON REZONE
EL PASO COUNTY, COLORADO
2028 TOTAL TRAFFIC VOLUMES PROPOSED BUILDOUT

## 



FIGURE 14
UDON REZONE
EL PASO COUNTY, COLORADO
2028 TOTAL TRAFFIC VOLUMES HIGHEST USE

## LEGEND

(X) Study Area Key Intersection
$X X X(X X X)$
Weekday AM (PM)
Peak Hour Traffic Volumes
XX,X00 Estimated Daily Traffic Volume

## 



## LEGEND

FIGURE 15
UDON REZONE
EL PASO COUNTY, COLORADO
2045 TOTAL TRAFFIC VOLUMES PROPOSED BUILDOUT

## 



FIGURE 16
UDON REZONE
EL PASO COUNTY, COLORADO
2045 TOTAL TRAFFIC VOLUMES HIGHEST USE

## LEGEND

(X) Study Area Key Intersection
$X X X(X X X)$
Weekday AM (PM)
Peak Hour Traffic Volumes
XX,X00 Estimated Daily Traffic Volume

## 



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FIGURE 18
UDON REZONE
EL PASO COUNTY, COLORADO
2028 RECOMMENDED GEOMETRY \&

## Improvement

-100' Turn Lane Length (feet)

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## Intersection Count Sheets

2019 CDOT Traffic Volume Data
Thursday, July 11, 2019
On SH-94 E/O Space Village Ave CR 2804


## Traffic Projections

CDOT OTIS TRAFFCPROJECTIONS: UDON REZONE

| ROUTE | REFPT | ENDREFPT | ENGGTH | AADT | AADTYR | YR2OFACTOR | GROWTH RATE | LOCATION |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


| $094 A$ | 1 | 8.085 | 7.077 | 11000 | 2022 | 1.21 | $1.0 \%$ |
| :--- | :--- | ---: | ---: | ---: | ---: | ---: | ---: |

## Trip Generation Worksheets

| Project | UDON Rezone (South - Proposed) |  |  |
| :--- | :--- | :--- | :--- |
| Subject | Trip Generation for Mini Warehouse |  |  |
| Designed by | TES | Date $\quad$ March 14, 2024 | Job No. |
| Checked by | Date__ | Sheet No. |  |

## TRIP GENERATION MANUAL TECHNIQUES

ITE Trip Generation Manual 11th Edition, Average Rate Equations
Land Use Code - Mini-W arehouse (151)

Independent Variable - 100 Storage Units (X)
Storage Units =
X $=8.6$
T $=$ Average Vehicle Trip Ends

Peak Hour of Adjacent Street Traffic, One Hour Between 7 and 9 a.m. (Page 120)


## Peak Hour of Adjacent Street Traffic, One Hour Between 4 and 6 p.m. (Page 121)

| Weekday Average |  |
| :--- | ---: |
| $\mathrm{T}=1.68(\mathrm{X})$ |  |
| $\mathrm{T}=1.68{ }^{*}$ | 8.6 |

AM Peak Hour of Generator (Page 122)

| Weekday Average |  |
| :--- | ---: |
| $\mathrm{T}=2.04(\mathrm{X})$ |  |
| $\mathrm{T}=2.04^{*}$ | 8.60 |

$$
\begin{aligned}
& \text { Directional Distribution: } \\
& \begin{array}{l}
\mathrm{T}= \\
= \\
10
\end{array} \begin{array}{l}
\text { entering } \\
\text { Average Vehicle Trip Ends }
\end{array} \\
& \begin{array}{l}
8 \\
\text { exiting }
\end{array} \\
& 10+8=18
\end{aligned}
$$

PM Peak Hour of Generator (Page 123)

| Weekday Average |  | Directional Distribution: |  |  | 48\% ent. 52\% |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{T}=2.07$ (X) |  | T = | 17 | Averag | Vehicle |
| T = 2.07* | 8.6 | 8 | entering |  | 9 ex |
|  |  | 8 | + 9 | $=$ | 17 |

## Weekday (Page 119)

Weekday Average

| $\mathrm{T}=17.96(X)$ |  |
| :--- | :--- |
| $\mathrm{T}=17.96^{*}$ | 8.6 |

Directional Distribution: $50 \%$ entering, $50 \%$ exiting
$\mathrm{T}=156 \quad$ Average Vehicle Trip Ends
$\mathrm{T}=156 \quad$ Average Vehicle Trip Ends
78 entering 78 exiting

$$
78+78=156
$$

## Saturday (Page 124)

|  |  |
| :--- | :--- | :--- |
| $T=16.29(X)$ |  |
| $T=16.29^{*}$ | 8.6 |

 71 entering 71 exiting

$$
71+71=142
$$

Saturday Peak Hour of Generator (Page 125)

|  |  |
| :--- | :--- |
| $\mathrm{T}=2.67(\mathrm{X})$ |  |
| $\mathrm{T}=2.67^{*}$ |  |

Directional Distribution: $56 \%$ entering, $44 \%$ exiting

$\mathrm{T}=$| 24 | Average Vehicle Trip Ends |  |
| :---: | :---: | :---: |
| 13 | entering | 11 |
| exiting |  |  |

$13+11$

| Project | UDON Rezone (North/South - Proposed) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Subject | Trip Generation for Mini Warehouse |  |  |  |  |
| Designed by | TES | Date | March 14, 2024 | Job No. | 196020000 |
| Checked by |  | Date |  | Sheet No. | of |

## TRIP GENERATION MANUAL TECHNIQUES

ITE Trip Generation Manual 11th Edition, Average Rate Equations

```
Land Use Code - Mini-Warehouse (151)
Independent Variable - 100 Storage Units (X)
    Storage Units = 1,860
    X = 18.6
    T = Average Vehicle Trip Ends
```

Peak Hour of Adjacent Street Traffic, One Hour Between 7 and 9 a.m. (Page 120)

(*) TRIP END WAS CHANGED BY 1 TO SATISFY THE TOTAL

## Peak Hour of Adjacent Street Traffic, One Hour Between 4 and 6 p.m. (Page 121)

Weekday Average
$\mathrm{T}=1.68$ (X)
$\mathrm{T}=1.68$ * 18.6

AM Peak Hour of Generator (Page 122)

| Weekday Average |  |
| :--- | ---: |
| $\mathrm{T}=2.04(\mathrm{X})$ |  |
| $\mathrm{T}=2.04{ }^{\text {* }}$ | 18.60 |

PM Peak Hour of Generator (Page 123)


Weekday (Page 119)
Weekday Average
$\mathrm{T}=17.96$ (X)
$\mathrm{T}=17.96$ * 18.6
Directional Distribution: $50 \%$ entering, $50 \%$ exiting
$\mathrm{T}=336 \quad$ Average Vehicle Trip Ends
168 entering 168 exiting
$168+168=336$
Saturday (Page 124)

|  |  |
| :--- | :--- |
| $\mathrm{T}=16.29(X)$ |  |
| $\mathrm{T}=16.29^{*}$ | 18.6 |

$$
\begin{aligned}
& \text { Directional Distribution: } 50 \% \text { entering, } 50 \% \text { exiting } \\
& \mathrm{T}= \\
& \begin{array}{ll}
304 & \text { Average Vehicle Trip Ends } \\
152 & \text { entering } \\
152 & \text { exiting }
\end{array} \\
& 152+152=304
\end{aligned}
$$

Saturday Peak Hour of Generator (Page 125)

|  |  |
| :--- | :--- |
| $T=2.67(X)$ |  |
| $T=2.67^{*}$ | 18.6 |



| Weekday Trip Generation <br> Trips Based on Average Rates/Equations |  |  | Project Name <br> Project Number | UDON Rezone - North - Highest Use |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ITE <br> Code | Internal Capture Land |  | Independent Variable | Setting/Location | No. of Units | Avg <br> Rate <br> or Eq | Rates |  |  | Total Trips |  |  |  |  |  |  | Net Trips after Pass-By |  |  |  |  |  |  |
|  |  |  | Daily Rate |  |  |  | $\begin{gathered} \text { AM } \\ \text { Rate } \end{gathered}$ | $\begin{gathered} \text { PM } \\ \text { Rate } \end{gathered}$ | Daily Trips | $\begin{gathered} \text { AM } \\ \text { Trips } \end{gathered}$ | $\begin{gathered} \text { PM } \\ \text { Trips } \end{gathered}$ | $\begin{gathered} \text { AM } \\ \text { Trips } \\ \text { In } \end{gathered}$ | $\begin{gathered} \text { AM } \\ \text { Trips } \\ \text { Out } \end{gathered}$ | $\begin{gathered} \text { PM } \\ \text { Trips } \\ \text { In } \end{gathered}$ | $\begin{gathered} \text { PM } \\ \text { Trips } \\ \text { Out } \end{gathered}$ | $\begin{array}{\|l} \text { Daily } \\ \text { Trips } \\ \hline \end{array}$ | $\begin{gathered} \text { AM } \\ \text { Trips } \end{gathered}$ | $\begin{gathered} \text { PM } \\ \text { Trips } \end{gathered}$ | $\begin{gathered} \text { AM } \\ \text { Trips } \\ \text { In } \end{gathered}$ | $\begin{gathered} \text { AM } \\ \text { Trips } \\ \text { Out } \end{gathered}$ | $\begin{gathered} \text { PM } \\ \text { Trips } \\ \text { In } \end{gathered}$ | $\begin{aligned} & \text { PM } \\ & \text { Trips } \\ & \text { Out } \end{aligned}$ |
| 820 | Select Use | Shopping Center ( $>150 \mathrm{k}$ ) |  | 1,000 Sq Ft GLA | General Urban/Suburban | 150 | Avg | 37.01 | 0.84 | 3.40 | 5,552 | 126 | 510 | 78 | 48 | 245 | 265 | 3,942 | 89 | 362 | 55 | 34 | 174 | 188 |
| 945 | Select Use | Convenience Store/Gas Station | Fueling Position(s) | General Urban/Suburban | 16 | Avg | 257.13 | 27.04 | 22.76 | 4,114 | 433 | 364 | 216 | 217 | 182 | 182 | 1,028 | 104 | 92 | 52 | 52 | 46 | 46 |

Kimley»Horn


## TRIP GENERATION MANUAL TECHNIQUES

ITE Trip Generation Manual 11th Edition, Average Rate Equations
Land Use Code - Shopping Center (>150k) (820)
Independent Variable - 1000 Square Feet Gross Leasable Area (X)

```
Gross Leasable Area = 150,000 Square Feet
X = 150.000
T = Average Vehicle Trip Ends
```

Peak Hour of Adjacent Street Traffic, One Hour Between 7 and 9 a.m. ( 800 Series Page 178)


Peak Hour of Adjacent Street Traffic, One Hour Between 4 and 6 p.m. ( 800 Series page 179)


Weekday ( 800 Series page 177)
Average Weekday Directional Distribution: 50\% entering, 50\% exiting
$\mathrm{T}=37.01^{*}$ (X)
$T=37.01^{*} \quad 150$
T = $5552 \quad$ Average Vehicle Trip Ends 2776 entering 2776 exiting $2776+2776=5552$

Non Pass-By Trip Volumes (Between 150 and 300k) (Per ITE Trip Generation Manual, 11th Edition)
AM Peak Hour $=71 \% \quad$ Non-Pass By $\quad$ PM Peak Hour $=71 \%$ Non-Pass By

|  | IN | Out | Total |  |
| :--- | :---: | :---: | :---: | :--- |
| AM Peak | 55 | 34 | 89 | PM Peak Hour Rate Applied to AM Peak Hour |
| PM Peak | 174 | 188 | 363 |  |
| Daily | 1971 | 1971 | 3942 | PM Peak Hour Rate Applied to Daily |

Pass-By Trip Volumes (Between 150 and 300k) (Per ITE Trip Generation Manual, 11th Edition)
AM Peak Hour $=29 \%$ Pass By $\quad$ PM Peak Hour $=29 \%$ Pass By

|  | IN | Out | Total |  |
| :--- | :---: | :---: | :---: | :---: |
| AM Peak | 23 | 14 | 37 | PM Peak Hour Rate Applied to AM Peak Hour |
| PM Peak | 71 | 77 | 148 |  |
| Daily | 805 | 805 | 1610 | PM Peak Hour Rate Applied to Daily |


| AM Peak Hour = |  | 81\% Non-Pass By |  | PM Peak Hour = | 81\% Non-Pass By |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | IN | Out | Total |  |  |  |
| AM Peak | 63 | 39 | 102 | PM Peak Hour Rate Applied to AM Peak Hour |  |  |
| PM Peak | 198 | 215 | 414 |  |  |  |  |  |
| Daily | 2249 | 2249 | 4498 | PM Peak Hour R | Appli | d to Daily |

Pass-By Trip Volumes (Between 300 and 900k) (Per ITE Trip Generation Manual, 11th Edition)
AM Peak Hour $=19 \%$ Pass By $\quad$ PM Peak Hour $=19 \%$ Pass By

|  | IN | Out | Total |  |
| :--- | :---: | :---: | :---: | :---: |
| AM Peak | 15 | 9 | 24 | PM Peak Hour Rate Applied to AM Peak Hour |
| PM Peak | 47 | 50 | 97 |  |

Daily $527 \quad 527 \quad 1054 \quad$ PM Peak Hour Rate Applied to Daily

## Kimley»)Horn

| Project | UDON Rezone (North - Highest Use) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Subject | Trip Generation for Gasoline/Service Station with Convenience Market |  |  |  |  |
| Designed by | TES | Date | March 14, 2024 | Job No. | 196020000 |
| Checked by |  | Date |  | Sheet No. | of |

## TRIP GENERATION MANUAL TECHNIQUES

ITE Trip Generation Manual 11th Edition, Average Rate Equations
Land Use Code - Convenience Store/Gas Station - GFA (4-5.5K) (945)
Independent Variable - Vehicle Fueling Positions (X)
Vehicle Fueling Positions $=16$ Positions
$X=16$
T = Average Vehicle Trip Ends

## Peak Hour of Adjacent Street Traffic, One Hour Between 7 and 9 a.m. (Page 873)



## Peak Hour of Adjacent Street Traffic, One Hour Between 4 and 6 p.m. (Page 874)

Average Weekday
$\begin{array}{ll}\mathrm{T}=22.76(\mathrm{X}) & \\ \mathrm{T}=22.76 \text { * } & 16.000\end{array}$
Directional Distribution: 50\% ent. 50\% exit.
$\mathrm{T}=364 \quad$ Average Vehicle Trip Ends 182 entering 182 exiting $182+182=364$

## Weekday (Page 872)

Average Weekday
T = 257.13 (X)
$\mathrm{T}=257.13$ * $\quad 16.000$ Directional Distribution: 50\% entering, 50\% exiting $\mathrm{T}=4114 \quad$ Average Vehicle Trip Ends 2057 entering 2057 exiting
$2057+2057=4114$

Non Pass-By Trip Volumes (Per ITE Trip Generation Manual, 11th Edition)

| PM Peak Hour $=$ | IN | Out | Non-Pass By | AM Peak Hour $=$ | $24 \%$ | Non-Pass By |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
|  | On |  |  |  |  |  |
| AM Peak | 52 | 52 | 104 |  |  |  |
| PM Peak | 46 | 46 | 91 |  |  |  |
| Daily | 514 | 514 | 1028 | PM Peak Hour Rate Applied to Daily |  |  |

Pass-By Trip Volumes (Per ITE Trip Generation Manual, 11th Edition)

| PM Peak Hour $=$ | $75 \%$ |  | Pass By | AM Peak Hour $=$ | $76 \%$ | Pass By |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Out | Total |  |  |  |  |
| AM Peak | 164 | 165 | 329 |  |  |  |
| PM Peak | 137 | 137 | 273 |  |  |  |
| Daily | 1543 | 1543 | 3086 | PM Peak Hour Rate Applied to Daily |  |  |

## Intersection Capacity Analysis Outputs

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.1 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | $\uparrow$ |  |  | - | Tr |  |
| Traffic Vol, veh/h | 933 | 3 | 2 | 459 | 3 | 2 |
| Future Vol, veh/h | 933 | 3 | 2 | 459 | 3 | 2 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 1014 | 3 | 2 | 499 | 3 | 2 |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.1 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | $\uparrow$ |  |  | - | ric |  |
| Traffic Vol, veh/h | 404 | 4 | 3 | 937 | 4 | 3 |
| Future Vol, veh/h | 404 | 4 | 3 | 937 | 4 | 3 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 439 | 4 | 3 | 1018 | 4 | 3 |











|  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\frac{\text { Intersection }}{\text { Int Delay, s/veh }} 99.2$ |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{1}$ | F |  |  | $\uparrow$ | 「 |  | $\ddagger$ |  | ${ }^{7}$ | $\uparrow$ |  |
| Traffic Vol, veh/h | 192 | 827 | 3 | 2 | 406 | 102 | 3 | 0 | 2 | 152 | 0 | 113 |
| Future Vol, veh/h | 192 | 827 | 3 | 2 | 406 | 102 | 3 | 0 | 2 | 152 | 0 | 113 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | Free |
| Storage Length | 600 | - | - | - | - | 400 | - | - | - | 0 | - | - |
| Veh in Median Storage, | \# | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 209 | 899 | 3 | 2 | 441 | 111 | 3 | 0 | 2 | 165 | 0 | 123 |



| Approach | EB | WB | NB | SB |
| :--- | ---: | ---: | ---: | ---: |
| HCM Control Delay, s | 1.8 | 0 | 56 | $\$ 1088.7$ |
| HCM LOS |  | $F$ | $F$ |  |


| Minor Lane/Major Mvmt | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR SBLn1 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Capacity (veh/h) | 76 | 1018 | - | - | 754 | - | 54 | - |  |
| HCM Lane V/C Ratio | 0.072 | 0.205 | - |  | 0.003 | - | 3.06 | - |  |
| HCM Control Delay (s) | 56 | 9.4 | - |  | 9.8 | 0 | \$1088.7 | 0 |  |
| HCM Lane LOS | F | A | - | - | A | A | F | A |  |
| HCM 95th \%tile Q(veh) | 0.2 | 0.8 | - | - | 0 | - | 17.5 | - |  |
| Notes |  |  |  |  |  |  |  |  |  |
| $\sim$ : Volume exceeds capacity | \$: Delay | Day exc | eeds 3 | 30s | +: Com | putatio | Not Defined | *: A | All major volume in platoon |




| Approach | EB | WB | NB | SB |
| :--- | ---: | ---: | ---: | ---: |
| HCM Control Delay, s | 5.1 | 0 | 60.8 | $\$ 1137.1$ |
| HCM LOS |  |  | F | F |


| Minor Lane/Major Mvmt | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR SBLn1 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Capacity (veh/h) | 72 | 619 | - | - | 1174 | - | 52 | - |  |
| HCM Lane V/C Ratio | 0.106 | 0.353 | - |  | 0.003 | - | 3.156 | - |  |
| HCM Control Delay (s) | 60.8 | 14 | - |  | 8.1 | 0 | \$1137.1 | 0 |  |
| HCM Lane LOS | F | B | - | - | A | A | F | A |  |
| HCM 95th \%tile Q(veh) | 0.3 | 1.6 | - | - | 0 | - | 17.5 | - |  |
| Notes |  |  |  |  |  |  |  |  |  |
| $\sim$ : Volume exceeds capacity | \$: Delay | Day exc | eeds 3 |  | +: Com | putatio | Not Defined | *: A | All major volume in platoon |


|  | 4 |  |  |  |  | 4 | 4 | $\checkmark$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | WBL | WBT | WBR | NBL | NBT | SBL | SBT |
| Lane Configurations | \% | ¢ | \% | 4 | 「 | \% | $\uparrow$ | \% | $\uparrow$ |
| Traffic Volume (vph) | 192 | 827 | 2 | 406 | 102 |  | 0 | 152 | 0 |
| Future Volume (vph) | 192 | 827 | 2 | 406 | 102 | 3 | 0 | 152 | 0 |
| Turn Type | pm+pt | NA | pm+pt | NA | Perm | Perm | NA | Perm | NA |
| Protected Phases | 7 | 4 | 3 | 8 |  |  | 2 |  | 6 |
| Permitted Phases | 4 |  | 8 |  | 8 | 2 |  | 6 |  |
| Detector Phase | 7 | 4 | 3 | 8 | 8 | 2 | 2 | 6 | 6 |
| Switch Phase |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Minimum Split (s) | 9.5 | 22.5 | 9.5 | 22.5 | 22.5 | 22.5 | 22.5 | 22.5 | 22.5 |
| Total Split (s) | 13.6 | 48.0 | 9.5 | 43.9 | 43.9 | 22.5 | 22.5 | 22.5 | 22.5 |
| Total Split (\%) | 17.0\% | 60.0\% | 11.9\% | 54.9\% | 54.9\% | 28.1\% | 28.1\% | 28.1\% | 28.1\% |
| Yellow Time (s) | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 |
| All-Red Time (s) | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 |
| Lead/Lag | Lead | Lag | Lead | Lag | Lag |  |  |  |  |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes |  |  |  |  |
| Recall Mode | None | None | None | None | None | C-Max | C-Max | Max | Max |
| Act Effct Green (s) | 45.2 | 43.3 | 36.9 | 31.9 | 31.9 | 25.8 | 25.8 | 25.8 | 25.8 |
| Actuated g/C Ratio | 0.56 | 0.54 | 0.46 | 0.40 | 0.40 | 0.32 | 0.32 | 0.32 | 0.32 |
| v/c Ratio | 0.45 | 0.89 | 0.01 | 0.59 | 0.16 | 0.01 | 0.00 | 0.36 | 0.15 |
| Control Delay | 10.8 | 29.3 | 6.0 | 21.8 | 3.1 | 22.7 | 0.0 | 26.0 | 0.4 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 10.8 | 29.3 | 6.0 | 21.8 | 3.1 | 22.7 | 0.0 | 26.0 | 0.4 |
| LOS | B | C | A | C | A | C | A | C | A |
| Approach Delay |  | 25.8 |  | 18.0 |  |  | 13.6 |  | 15.1 |
| Approach LOS |  | C |  | B |  |  | B |  | B |
| Intersection Summary |  |  |  |  |  |  |  |  |  |
| Cycle Length: 80 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 80 |  |  |  |  |  |  |  |  |  |
| Offset: $0(0 \%)$, Referenced to phase 2:NBTL, Start of Green |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 80 |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.89 |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 22.0 |  |  |  |  | Intersection LOS: C |  |  |  |  |
| Intersection Capacity Utilization 74.2\% |  |  |  |  | ICU Level of Service D |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |

Splits and Phases: 1: Access \& SH-94


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{1}$ | ¢ |  | * | $\uparrow$ | 「 | \% | F |  | \% | F |  |
| Traffic Volume (veh/h) | 192 | 827 | 3 | , | 406 | 102 | 3 | 0 | 2 | 152 | 0 | 113 |
| Future Volume (veh/h) | 192 | 827 | 3 | 2 | 406 | 102 | 3 | 0 | 2 | 152 | 0 | 113 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow, veh/h/ln | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate, veh/h | 209 | 899 | 3 | 2 | 441 | 111 | 3 | 0 | 2 | 165 | 0 | 0 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 462 | 958 | 3 | 133 | 805 | 682 | 535 | 0 | 498 | 533 | 588 |  |
| Arrive On Green | 0.09 | 0.51 | 0.51 | 0.00 | 0.43 | 0.43 | 0.31 | 0.00 | 0.31 | 0.31 | 0.00 | 0.00 |
| Sat Flow, veh/h | 1781 | 1863 | , | 1781 | 1870 | 1585 | 1418 | 0 | 1585 | 1415 | 1870 | 0 |
| Grp Volume(v), veh/h | 209 | 0 | 902 | 2 | 441 | 111 | 3 | 0 | 2 | 165 | 0 | 0 |
| Grp Sat Flow(s),veh/h/ln | 1781 | 0 | 1869 | 1781 | 1870 | 1585 | 1418 | 0 | 1585 | 1415 | 1870 | 0 |
| Q Serve(g_s), s | 4.9 | 0.0 | 36.2 | 0.1 | 14.1 | 3.4 | 0.1 | 0.0 | 0.1 | 7.3 | 0.0 | 0.0 |
| Cycle Q Clear(g_c), s | 4.9 | 0.0 | 36.2 | 0.1 | 14.1 | 3.4 | 0.1 | 0.0 | 0.1 | 7.3 | 0.0 | 0.0 |
| Prop In Lane | 1.00 |  | 0.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 0.00 |
| Lane Grp Cap(c), veh/h | 462 | 0 | 961 | 133 | 805 | 682 | 535 | 0 | 498 | 533 | 588 |  |
| V/C Ratio(X) | 0.45 | 0.00 | 0.94 | 0.02 | 0.55 | 0.16 | 0.01 | 0.00 | 0.00 | 0.31 | 0.00 |  |
| Avail Cap(c_a), veh/h | 511 | 0 | 1016 | 239 | 921 | 781 | 535 | 0 | 498 | 533 | 588 |  |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(1) | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 0.00 |
| Uniform Delay (d), s/veh | 11.6 | 0.0 | 18.2 | 18.3 | 17.0 | 14.0 | 18.9 | 0.0 | 18.8 | 21.3 | 0.0 | 0.0 |
| Incr Delay (d2), s/veh | 0.7 | 0.0 | 15.2 | 0.0 | 0.6 | 0.1 | 0.0 | 0.0 | 0.0 | 1.5 | 0.0 | 0.0 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 1.8 | 0.0 | 17.8 | 0.0 | 5.8 | 1.2 | 0.0 | 0.0 | 0.0 | 2.5 | 0.0 | 0.0 |

Unsig. Movement Delay, s/veh

| LnGrp Delay(d), S/veh | 12.3 | 0.0 | 33.4 | 18.4 | 17.6 | 14.1 | 18.9 | 0.0 | 18.9 | 22.9 | 0.0 | 0.0 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| LnGrp LOS | B | A | C | B | B | B | B | A | B | C | A |  |
| Approach Vol, veh/h |  | 1111 |  |  | 554 |  |  | 5 |  | 165 |  |  |
| Approach Delay, s/veh |  | 29.4 |  |  | 16.9 |  |  | 18.9 |  | 22.9 |  |  |
| Approach LOS | C |  |  | B |  |  | B |  | C |  |  |  |


| Timer - Assigned Phs | 2 | 3 | 4 | 6 | 7 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Phs Duration $(\mathrm{G}+\mathrm{Y}+\mathrm{Rc})$, s | 29.6 | 4.7 | 45.6 | 29.6 | 11.4 | 38.9 |
| Change Period $(\mathrm{Y}+\mathrm{Rc}$ ), s | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 |
| Max Green Setting (Gmax), s | 18.0 | 5.0 | 43.5 | 18.0 | 9.1 | 39.4 |
| Max Q Clear Time (g_c+1), s | 2.1 | 2.1 | 38.2 | 9.3 | 6.9 | 16.1 |
| Green Ext Time (p_c), s | 0.0 | 0.0 | 2.9 | 0.3 | 0.1 | 3.2 |

## Intersection Summary

| HCM 6th Ctrl Delay | 25.0 |
| :--- | ---: |
| HCM 6th LOS | C |

## Notes

Unsignalized Delay for [SBR] is excluded from calculations of the approach delay and intersection delay.

|  | 4 | $\rightarrow$ | 7 |  | 4 | 4 | $\dagger$ | , | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | WBL | WBT | WBR | NBL | NBT | SBL | SBT |
| Lane Configurations | ${ }^{*}$ | $\uparrow$ | ${ }^{*}$ | 4 | 「 | ${ }^{1}$ | $\uparrow$ | ${ }^{*}$ | $\uparrow$ |
| Traffic Volume (vph) | 201 | 350 | 3 | 811 | 226 | 4 | 0 | 151 | 0 |
| Future Volume (vph) | 201 | 350 | 3 | 811 | 226 | 4 | 0 | 151 | 0 |
| Turn Type | pm+pt | NA | pm+pt | NA | Perm | Perm | NA | Perm | NA |
| Protected Phases | 7 | 4 | 3 | 8 |  |  | 2 |  | 6 |
| Permitted Phases | 4 |  | 8 |  | 8 | 2 |  | 6 |  |
| Detector Phase | 7 | 4 | 3 | 8 | 8 | 2 | 2 | 6 | 6 |
| Switch Phase |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Minimum Split (s) | 9.5 | 22.5 | 9.5 | 22.5 | 22.5 | 22.5 | 22.5 | 22.5 | 22.5 |
| Total Split (s) | 11.6 | 47.1 | 9.5 | 45.0 | 45.0 | 23.4 | 23.4 | 23.4 | 23.4 |
| Total Split (\%) | 14.5\% | 58.9\% | 11.9\% | 56.3\% | 56.3\% | 29.3\% | 29.3\% | 29.3\% | 29.3\% |
| Yellow Time (s) | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 |
| All-Red Time (s) | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 |
| Lead/Lag | Lead | Lag | Lead | Lag | Lag |  |  |  |  |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes |  |  |  |  |
| Recall Mode | None | None | None | None | None | C-Max | C-Max | Max | Max |
| Act Effct Green (s) | 51.0 | 49.6 | 44.9 | 39.9 | 39.9 | 19.5 | 19.5 | 19.5 | 19.5 |
| Actuated g/C Ratio | 0.64 | 0.62 | 0.56 | 0.50 | 0.50 | 0.24 | 0.24 | 0.24 | 0.24 |
| v/c Ratio | 0.87 | 0.33 | 0.00 | 0.95 | 0.27 | 0.04 | 0.00 | 0.48 | 0.59 |
| Control Delay | 49.5 | 8.8 | 5.0 | 40.3 | 2.4 | 24.8 | 0.0 | 31.8 | 14.2 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 49.5 | 8.8 | 5.0 | 40.3 | 2.4 | 24.8 | 0.0 | 31.8 | 14.2 |
| LOS | D | A | A | D | A | C | A | C | B |
| Approach Delay |  | 23.5 |  | 32.0 |  |  | 14.1 |  | 20.1 |
| Approach LOS |  | C |  | C |  |  | B |  | C |
| Intersection Summary |  |  |  |  |  |  |  |  |  |
| Cycle Length: 80 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 80 |  |  |  |  |  |  |  |  |  |
| Offset: $0(0 \%)$, Referenced to phase 2:NBTL, Start of Green |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 90 |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.95 |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 27.0 |  |  |  |  | Intersection LOS: C |  |  |  |  |
| Intersection Capacity Utilization 83.4\% |  |  |  |  | ICU Level of Service E |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |

Splits and Phases: 1: Access \& SH-94


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{1}$ | ¢ |  | \% | $\uparrow$ | F' | * | F |  | \% | F |  |
| Traffic Volume (veh/h) | 201 | 350 | 4 | 3 | 811 | 226 | 4 | 0 | 3 | 151 | 0 | 296 |
| Future Volume (veh/h) | 201 | 350 | 4 | 3 | 811 | 226 | 4 | 0 | 3 | 151 | 0 | 296 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow, veh/h/ln | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate, veh/h | 218 | 380 | 4 | 3 | 882 | 246 | 4 | 0 | 3 | 164 | 0 | 0 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 257 | 1058 | 11 | 559 | 927 | 786 | 451 | 0 | 404 | 448 | 476 |  |
| Arrive On Green | 0.08 | 0.57 | 0.57 | 0.00 | 0.50 | 0.50 | 0.25 | 0.00 | 0.25 | 0.25 | 0.00 | 0.00 |
| Sat Flow, veh/h | 1781 | 1847 | 19 | 1781 | 1870 | 1585 | 1418 | 0 | 1585 | 1414 | 1870 | 0 |
| Grp Volume(v), veh/h | 218 | 0 | 384 | 3 | 882 | 246 | 4 | 0 | 3 | 164 | 0 | 0 |
| Grp Sat Flow(s),veh/h/ln | 1781 | 0 | 1867 | 1781 | 1870 | 1585 | 1418 | 0 | 1585 | 1414 | 1870 | 0 |
| Q Serve(g_s), s | 4.5 | 0.0 | 8.9 | 0.1 | 36.0 | 7.4 | 0.2 | 0.0 | 0.1 | 7.8 | 0.0 | 0.0 |
| Cycle Q Clear(g_c), s | 4.5 | 0.0 | 8.9 | 0.1 | 36.0 | 7.4 | 0.2 | 0.0 | 0.1 | 8.0 | 0.0 | 0.0 |
| Prop In Lane | 1.00 |  | 0.01 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 0.00 |
| Lane Grp Cap(c), veh/h | 257 | 0 | 1069 | 559 | 927 | 786 | 451 | 0 | 404 | 448 | 476 |  |
| V/C Ratio(X) | 0.85 | 0.00 | 0.36 | 0.01 | 0.95 | 0.31 | 0.01 | 0.00 | 0.01 | 0.37 | 0.00 |  |
| Avail Cap(c_a), veh/h | 271 | 0 | 1069 | 663 | 947 | 802 | 451 | 0 | 404 | 448 | 476 |  |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 0.00 |
| Uniform Delay (d), s/veh | 18.0 | 0.0 | 9.2 | 10.1 | 19.3 | 12.0 | 22.3 | 0.0 | 22.3 | 25.2 | 0.0 | 0.0 |
| Incr Delay (d2), s/veh | 20.9 | 0.0 | 0.2 | 0.0 | 18.4 | 0.2 | 0.0 | 0.0 | 0.0 | 2.3 | 0.0 | 0.0 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 3.4 | 0.0 | 3.2 | 0.0 | 18.6 | 2.5 | 0.1 | 0.0 | 0.0 | 2.8 | 0.0 | 0.0 |

Unsig. Movement Delay, s/veh

| LnGrp Delay(d), s/veh | 38.9 | 0.0 | 9.4 | 10.1 | 37.7 | 12.3 | 22.3 | 0.0 | 22.3 | 27.5 | 0.0 | 0.0 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| LnGrp LOS | D | A | A | B | D | B | C | A | C | C | A |  |
| Approach Vol, veh/h |  | 602 |  |  | 1131 |  |  | 2 |  | 164 |  |  |
| Approach Delay, s/veh |  | 20.1 |  |  | 32.1 |  |  | 22.3 |  | 27.5 |  |  |
| Approach LOS | C |  |  | C |  |  | C |  |  | C |  |  |


| Timer - Assigned Phs | 2 | 3 | 4 | 6 | 7 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Phs Duration $(G+Y+R c)$, s | 24.9 | 4.8 | 50.3 | 24.9 | 11.0 | 44.2 |
| Change Period $(\mathrm{Y}+\mathrm{Rc}), \mathrm{s}$ | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 |
| Max Green Setting (Gmax), s | 18.9 | 5.0 | 42.6 | 18.9 | 7.1 | 40.5 |
| Max Q Clear Time (g_c+11), s | 2.2 | 2.1 | 10.9 | 10.0 | 6.5 | 38.0 |
| Green Ext Time (p_C), s | 0.0 | 0.0 | 2.5 | 0.3 | 0.0 | 1.6 |

## Intersection Summary

HCM 6th Ctrl Delay 27.9
HCM 6th LOS
C

## Notes

Unsignalized Delay for [SBR] is excluded from calculations of the approach delay and intersection delay.

|  | 4 | $\rightarrow$ | 7 |  | 4 | 4 | $\dagger$ | , | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | WBL | WBT | WBR | NBL | NBT | SBL | SBT |
| Lane Configurations | ${ }^{7}$ | $\uparrow$ | ${ }^{*}$ | 4 | 「 | ${ }^{1}$ | $\uparrow$ | ${ }^{7}$ | $\uparrow$ |
| Traffic Volume (vph) | 192 | 1003 | 2 | 493 | 102 | 3 | 0 | 152 | 0 |
| Future Volume (vph) | 192 | 1003 | 2 | 493 | 102 | 3 | 0 | 152 | 0 |
| Turn Type | pm+pt | NA | pm+pt | NA | Perm | Perm | NA | Perm | NA |
| Protected Phases | 7 | 4 | 3 | 8 |  |  | 2 |  | 6 |
| Permitted Phases | 4 |  | 8 |  | 8 | 2 |  | 6 |  |
| Detector Phase | 7 | 4 | 3 | 8 | 8 | 2 | 2 | 6 | 6 |
| Switch Phase |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Minimum Split (s) | 9.5 | 22.5 | 9.5 | 22.5 | 22.5 | 22.5 | 22.5 | 22.5 | 22.5 |
| Total Split (s) | 14.2 | 48.0 | 9.5 | 43.3 | 43.3 | 22.5 | 22.5 | 22.5 | 22.5 |
| Total Split (\%) | 17.8\% | 60.0\% | 11.9\% | 54.1\% | 54.1\% | 28.1\% | 28.1\% | 28.1\% | 28.1\% |
| Yellow Time (s) | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 |
| All-Red Time (s) | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 |
| Lead/Lag | Lead | Lag | Lead | Lag | Lag |  |  |  |  |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes |  |  |  |  |
| Recall Mode | None | None | None | None | None | C-Max | C-Max | Max | Max |
| Act Effct Green (s) | 53.0 | 51.1 | 44.8 | 39.8 | 39.8 | 18.0 | 18.0 | 18.0 | 18.0 |
| Actuated g/C Ratio | 0.66 | 0.64 | 0.56 | 0.50 | 0.50 | 0.22 | 0.22 | 0.22 | 0.22 |
| v/c Ratio | 0.41 | 0.92 | 0.01 | 0.58 | 0.13 | 0.01 | 0.00 | 0.52 | 0.19 |
| Control Delay | 7.6 | 28.0 | 5.0 | 17.6 | 1.6 | 24.3 | 0.0 | 34.0 | 0.7 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 7.6 | 28.0 | 5.0 | 17.6 | 1.6 | 24.3 | 0.0 | 34.0 | 0.7 |
| LOS | A | C | A | B | A | C | A | C | A |
| Approach Delay |  | 24.8 |  | 14.8 |  |  | 14.6 |  | 19.8 |
| Approach LOS |  | C |  | B |  |  | B |  | B |
| Intersection Summary |  |  |  |  |  |  |  |  |  |
| Cycle Length: 80 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 80 |  |  |  |  |  |  |  |  |  |
| Offset: $0(0 \%)$, Referenced to phase 2:NBTL, Start of Green |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 90 |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.92 |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 21.2 |  |  |  |  | Intersection LOS: C |  |  |  |  |
| Intersection Capacity Utilization 83.5\% |  |  |  |  | ICU Level of Service E |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |

Splits and Phases: 1: Access \& SH-94


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{1}$ | ¢ |  | * | $\uparrow$ | 「 | \% | F |  | \% | F |  |
| Traffic Volume (veh/h) | 192 | 1003 | 3 | , | 493 | 102 | 3 | 0 | 2 | 152 | 0 | 113 |
| Future Volume (veh/h) | 192 | 1003 | 3 | 2 | 493 | 102 | 3 | 0 | 2 | 152 | 0 | 113 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow, veh/h/ln | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate, veh/h | 209 | 1090 | 3 | 2 | 536 | 111 | 3 | 0 | 2 | 165 | 0 | 0 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 432 | 1014 | 3 | 95 | 866 | 734 | 494 | 0 | 451 | 492 | 533 |  |
| Arrive On Green | 0.08 | 0.54 | 0.54 | 0.00 | 0.46 | 0.46 | 0.28 | 0.00 | 0.28 | 0.28 | 0.00 | 0.00 |
| Sat Flow, veh/h | 1781 | 1864 | 5 | 1781 | 1870 | 1585 | 1418 | 0 | 1585 | 1415 | 1870 | 0 |
| Grp Volume(v), veh/h | 209 | 0 | 1093 | 2 | 536 | 111 | 3 | 0 | 2 | 165 | 0 | 0 |
| Grp Sat Flow(s),veh/h/ln | 1781 | 0 | 1869 | 1781 | 1870 | 1585 | 1418 | 0 | 1585 | 1415 | 1870 | 0 |
| Q Serve(g_s), s | 4.6 | 0.0 | 43.5 | 0.0 | 17.3 | 3.2 | 0.1 | 0.0 | 0.1 | 7.6 | 0.0 | 0.0 |
| Cycle Q Clear(g_c), s | 4.6 | 0.0 | 43.5 | 0.0 | 17.3 | 3.2 | 0.1 | 0.0 | 0.1 | 7.6 | 0.0 | 0.0 |
| Prop In Lane | 1.00 |  | 0.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 0.00 |
| Lane Grp Cap(c), veh/h | 432 | 0 | 1017 | 95 | 866 | 734 | 494 | 0 | 451 | 492 | 533 |  |
| V/C Ratio(X) | 0.48 | 0.00 | 1.08 | 0.02 | 0.62 | 0.15 | 0.01 | 0.00 | 0.00 | 0.34 | 0.00 |  |
| Avail Cap(c_a), veh/h | 500 | 0 | 1017 | 201 | 907 | 769 | 494 | 0 | 451 | 492 | 533 |  |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(1) | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 0.00 |
| Uniform Delay (d), s/veh | 11.5 | 0.0 | 18.3 | 20.0 | 16.2 | 12.4 | 20.5 | 0.0 | 20.5 | 23.2 | 0.0 | 0.0 |
| Incr Delay (d2), s/veh | 0.8 | 0.0 | 50.7 | 0.1 | 1.2 | 0.1 | 0.0 | 0.0 | 0.0 | 1.8 | 0.0 | 0.0 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 1.7 | 0.0 | 30.5 | 0.0 | 7.1 | 1.1 | 0.0 | 0.0 | 0.0 | 2.7 | 0.0 | 0.0 |

Unsig. Movement Delay, s/veh

| LnGrp Delay(d), s/veh | 12.3 | 0.0 | 69.0 | 20.1 | 17.4 | 12.5 | 20.5 | 0.0 | 20.5 | 25.1 | 0.0 | 0.0 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| LnGrp LOS | B | A | F | C | B | B | C | A | C | C | A |  |
| Approach Vol, veh/h |  | 1302 |  |  | 649 |  |  | 5 |  | 165 |  |  |
| Approach Delay, s/veh |  | 59.9 |  |  | 16.5 |  |  | 20.5 |  | 25.1 |  |  |
| Approach LOS | E |  |  | B |  |  | C |  | C |  |  |  |


| Timer - Assigned Phs | 2 | 3 | 4 | 6 | 7 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Phs Duration $(G+Y+R c)$, s | 27.3 | 4.7 | 48.0 | 27.3 | 11.2 | 41.6 |
| Change Period $(Y+R c)$, s | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 |
| Max Green Setting (Gmax), s | 18.0 | 5.0 | 43.5 | 18.0 | 9.7 | 38.8 |
| Max Q Clear Time (g_c+11), s | 2.1 | 2.0 | 45.5 | 9.6 | 6.6 | 19.3 |
| Green Ext Time (p_C), s | 0.0 | 0.0 | 0.0 | 0.3 | 0.2 | 3.8 |

## Intersection Summary

HCM 6th Ctrl Delay 43.8
HCM 6th LOS D

## Notes

Unsignalized Delay for [SBR] is excluded from calculations of the approach delay and intersection delay.

|  | 4 | $\rightarrow$ | 7 |  | 4 | 4 | $\dagger$ | , | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | WBL | WBT | WBR | NBL | NBT | SBL | SBT |
| Lane Configurations | ${ }^{1}$ | $\uparrow$ | ${ }^{*}$ | 4 | 「 | ${ }^{1}$ | $\uparrow$ | ${ }^{*}$ | $\uparrow$ |
| Traffic Volume (vph) | 201 | 426 | 3 | 988 | 226 | 4 | 0 | 151 | 0 |
| Future Volume (vph) | 201 | 426 | 3 | 988 | 226 | 4 | 0 | 151 | 0 |
| Turn Type | pm+pt | NA | pm+pt | NA | Perm | Perm | NA | Perm | NA |
| Protected Phases | 7 | 4 | 3 | 8 |  |  | 2 |  | 6 |
| Permitted Phases | 4 |  | 8 |  | 8 | 2 |  | 6 |  |
| Detector Phase | 7 | 4 | 3 | 8 | 8 | 2 | 2 | 6 | 6 |
| Switch Phase |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Minimum Split (s) | 9.5 | 22.5 | 9.5 | 22.5 | 22.5 | 22.5 | 22.5 | 22.5 | 22.5 |
| Total Split (s) | 10.2 | 47.2 | 9.5 | 46.5 | 46.5 | 23.3 | 23.3 | 23.3 | 23.3 |
| Total Split (\%) | 12.8\% | 59.0\% | 11.9\% | 58.1\% | 58.1\% | 29.1\% | 29.1\% | 29.1\% | 29.1\% |
| Yellow Time (s) | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 |
| All-Red Time (s) | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 |
| Lead/Lag | Lead | Lag | Lead | Lag | Lag |  |  |  |  |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes |  |  |  |  |
| Recall Mode | None | None | None | None | None | C-Max | C-Max | Max | Max |
| Act Effct Green (s) | 51.4 | 50.3 | 47.0 | 42.0 | 42.0 | 18.8 | 18.8 | 18.8 | 18.8 |
| Actuated g/C Ratio | 0.64 | 0.63 | 0.59 | 0.52 | 0.52 | 0.24 | 0.24 | 0.24 | 0.24 |
| v/c Ratio | 1.03 | 0.40 | 0.01 | 1.10 | 0.26 | 0.03 | 0.00 | 0.50 | 0.63 |
| Control Delay | 92.8 | 9.3 | 5.0 | 81.0 | 2.2 | 24.8 | 0.0 | 32.6 | 18.3 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 92.8 | 9.3 | 5.0 | 81.0 | 2.2 | 24.8 | 0.0 | 32.6 | 18.3 |
| LOS | F | A | A | F | A | C | A | C | B |
| Approach Delay |  | 35.9 |  | 66.2 |  |  | 14.1 |  | 23.1 |
| Approach LOS |  | D |  | E |  |  | B |  | C |
| Intersection Summary |  |  |  |  |  |  |  |  |  |
| Cycle Length: 80 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 80 |  |  |  |  |  |  |  |  |  |
| Offset: $0(0 \%)$, Referenced to phase 2:NBTL, Start of Green |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 90 |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 1.10 |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 49.4 |  |  |  |  | Intersection LOS: D |  |  |  |  |
| Intersection Capacity Utilization 92.7\% |  |  |  |  | ICU Level of Service F |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |

Splits and Phases: 1: Access \& SH-94


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \% | ¢ |  | \% | $\uparrow$ | F' | * | ¢ |  | \% | F |  |
| Traffic Volume (veh/h) | 201 | 426 | 4 | , | 988 | 226 | 4 | 0 | 3 | 151 | 0 | 296 |
| Future Volume (veh/h) | 201 | 426 | 4 | 3 | 988 | 226 | 4 | 0 | 3 | 151 | 0 | 296 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow, veh/h/ln | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate, veh/h | 218 | 463 | 4 | 3 | 1074 | 246 | 4 | 0 | 3 | 164 | 0 | 0 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 217 | 1096 | 9 | 520 | 982 | 832 | 423 | 0 | 372 | 420 | 440 |  |
| Arrive On Green | 0.07 | 0.59 | 0.59 | 0.00 | 0.52 | 0.52 | 0.23 | 0.00 | 0.23 | 0.23 | 0.00 | 0.00 |
| Sat Flow, veh/h | 1781 | 1851 | 16 | 1781 | 1870 | 1585 | 1418 | 0 | 1585 | 1414 | 1870 | 0 |
| Grp Volume(v), veh/h | 218 | 0 | 467 | 3 | 1074 | 246 | 4 | 0 | 3 | 164 | 0 | 0 |
| Grp Sat Flow(s),veh/h/ln | 1781 | 0 | 1867 | 1781 | 1870 | 1585 | 1418 | 0 | 1585 | 1414 | 1870 | 0 |
| Q Serve(g_s), s | 5.7 | 0.0 | 10.9 | 0.1 | 42.0 | 7.0 | 0.2 | 0.0 | 0.1 | 8.0 | 0.0 | 0.0 |
| Cycle Q Clear(g_c), s | 5.7 | 0.0 | 10.9 | 0.1 | 42.0 | 7.0 | 0.2 | 0.0 | 0.1 | 8.2 | 0.0 | 0.0 |
| Prop In Lane | 1.00 |  | 0.01 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 0.00 |
| Lane Grp Cap(c), veh/h | 217 | 0 | 1106 | 520 | 982 | 832 | 423 | 0 | 372 | 420 | 440 |  |
| V/C Ratio(X) | 1.00 | 0.00 | 0.42 | 0.01 | 1.09 | 0.30 | 0.01 | 0.00 | 0.01 | 0.39 | 0.00 |  |
| Avail Cap(c_a), veh/h | 217 | 0 | 1106 | 624 | 982 | 832 | 423 | 0 | 372 | 420 | 440 |  |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(1) | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 0.00 |
| Uniform Delay (d), s/veh | 23.4 | 0.0 | 8.9 | 9.1 | 19.0 | 10.7 | 23.5 | 0.0 | 23.5 | 26.6 | 0.0 | 0.0 |
| Incr Delay (d2), s/veh | 62.4 | 0.0 | 0.3 | 0.0 | 57.8 | 0.2 | 0.0 | 0.0 | 0.0 | 2.7 | 0.0 | 0.0 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 5.8 | 0.0 | 3.9 | 0.0 | 31.6 | 2.3 | 0.1 | 0.0 | 0.0 | 2.9 | 0.0 | 0.0 |

Unsig. Movement Delay, s/veh

| LnGrp Delay(d), S/veh | 85.8 | 0.0 | 9.1 | 9.1 | 76.8 | 10.9 | 23.5 | 0.0 | 23.5 | 29.3 | 0.0 | 0.0 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| LnGrp LOS | F | A | A | A | F | B | C | A | C | C | A |  |
| Approach Vol, veh/h |  | 685 |  |  | 1323 |  |  | 7 |  | 164 |  |  |
| Approach Delay, s/veh |  | 33.5 |  |  | 64.4 |  |  | 23.5 |  | 29.3 |  |  |
| Approach LOS | C |  |  | E |  |  | C |  | C |  |  |  |


| Timer - Assigned Phs | 2 | 3 | 4 | 6 | 7 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Phs Duration $(G+Y+R c)$, s | 23.3 | 4.8 | 51.9 | 23.3 | 10.2 | 46.5 |
| Change Period $(\mathrm{Y}+\mathrm{Rc}), \mathrm{s}$ | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 |
| Max Green Setting (Gmax), s | 18.8 | 5.0 | 42.7 | 18.8 | 5.7 | 42.0 |
| Max Q Clear Time (g_c+11), s | 2.2 | 2.1 | 12.9 | 10.2 | 7.7 | 44.0 |
| Green Ext Time (p_C), s | 0.0 | 0.0 | 3.2 | 0.3 | 0.0 | 0.0 |

## Intersection Summary

| HCM 6th Ctrl Delay | 51.9 |
| :--- | ---: |
| HCM 6th LOS | D |

## Notes

Unsignalized Delay for [SBR] is excluded from calculations of the approach delay and intersection delay.

Signal Warrant Analysis Worksheet

WARRANT 2 - FOUR HOUR VEHICULAR VOLUME (70\% FACTOR) (COMMUNITY LESS THAN 10,000 POPULATION OR ABOVE $70 \mathrm{~km} / \mathrm{h}$ ( 40 mph ) ON MAJOR STREET)


* NOTE: 80 VPH APPLIES AS THE LOWER THRESHOLD VOLUME FOR A MINOR STREET

SH-94 ACCESS APPROACH WITH TWO OR MORE LANES AND 60 VPH APPLIES AS THE LOWER

SIGNAL WARRANT ANALYSIS
FOUR HOUR VOLUME WARRANT 2028 TOTAL TRAFFIC DATA POINT WITH PROJECT - HIGHEST USE

Source: Manual of Uniform Traffic Control Devices 2009

## Queue Analysis Worksheets

|  | 4 | $\rightarrow$ | 7 | 4 | 4 | 4 | $\dagger$ |  | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | WBL | WBT | WBR | NBL | NBT | SBL | SBT |
| Lane Group Flow (vph) | 209 | 902 | 2 | 441 | 111 | 3 | 2 | 165 | 123 |
| v/c Ratio | 0.45 | 0.89 | 0.01 | 0.59 | 0.16 | 0.01 | 0.00 | 0.36 | 0.15 |
| Control Delay | 10.8 | 29.3 | 6.0 | 21.8 | 3.1 | 22.7 | 0.0 | 26.0 | 0.4 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 10.8 | 29.3 | 6.0 | 21.8 | 3.1 | 22.7 | 0.0 | 26.0 | 0.4 |
| Queue Length 50th (ft) | 50 | 366 | 0 | 175 | 0 | 1 | 0 | 61 | 0 |
| Queue Length 95th (ft) | 60 | \#637 | 2 | 216 | 24 | 8 | 0 | 134 | 0 |
| Internal Link Dist (tt) |  | 1750 |  | 1759 |  |  | 261 |  | 205 |
| Turn Bay Length (tt) | 600 |  |  |  | 400 |  |  |  |  |
| Base Capacity (vph) | 473 | 1039 | 194 | 917 | 835 | 406 | 666 | 454 | 798 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.44 | 0.87 | 0.01 | 0.48 | 0.13 | 0.01 | 0.00 | 0.36 | 0.15 |

## Intersection Summary

\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.

|  | $\stackrel{ }{ }$ | $\rightarrow$ | 7 | $\leftarrow$ | 4 | 4 | $\dagger$ |  | $\ddagger$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | WBL | WBT | WBR | NBL | NBT | SBL | SBT |
| Lane Group Flow (vph) | 218 | 384 | 3 | 882 | 246 | 4 | 3 | 164 | 322 |
| v/c Ratio | 0.87 | 0.33 | 0.00 | 0.95 | 0.27 | 0.04 | 0.00 | 0.48 | 0.59 |
| Control Delay | 49.5 | 8.8 | 5.0 | 40.3 | 2.4 | 24.8 | 0.0 | 31.8 | 14.2 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 49.5 | 8.8 | 5.0 | 40.3 | 2.4 | 24.8 | 0.0 | 31.8 | 14.2 |
| Queue Length 50th (ft) | 55 | 74 | 1 | 390 | 0 | 2 | 0 | 71 | 43 |
| Queue Length 95th (ft) | \#184 | 166 | 3 | \#652 | 33 | 9 | 0 | 131 | 124 |
| Internal Link Dist (tt) |  | 1750 |  | 1759 |  |  | 261 |  | 205 |
| Turn Bay Length (tt) | 600 |  |  |  | 400 |  |  |  |  |
| Base Capacity (vph) | 250 | 1153 | 607 | 943 | 922 | 114 | 769 | 343 | 549 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.87 | 0.33 | 0.00 | 0.94 | 0.27 | 0.04 | 0.00 | 0.48 | 0.59 |

## Intersection Summary

\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.

|  | 4 | $\rightarrow$ | 7 | 4 | 4 | 4 | $\uparrow$ |  | $\ddagger$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | WBL | WBT | WBR | NBL | NBT | SBL | SBT |
| Lane Group Flow (vph) | 209 | 1093 | 2 | 536 | 111 | 3 | 2 | 165 | 123 |
| v/c Ratio | 0.41 | 0.92 | 0.01 | 0.58 | 0.13 | 0.01 | 0.00 | 0.52 | 0.19 |
| Control Delay | 7.6 | 28.0 | 5.0 | 17.6 | 1.6 | 24.3 | 0.0 | 34.0 | 0.7 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 7.6 | 28.0 | 5.0 | 17.6 | 1.6 | 24.3 | 0.0 | 34.0 | 0.7 |
| Queue Length 50th (ft) | 35 | 387 | 0 | 181 | 0 | 1 | 0 | 73 | 0 |
| Queue Length 95th (ft) | 60 | \#851 | 2 | 282 | 16 | 8 | 0 | 134 | 0 |
| Internal Link Dist (tt) |  | 1750 |  | 1759 |  |  | 261 |  | 205 |
| Turn Bay Length (t) | 600 |  |  |  | 400 |  |  |  |  |
| Base Capacity (vph) | 531 | 1190 | 195 | 927 | 859 | 277 | 504 | 317 | 632 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.39 | 0.92 | 0.01 | 0.58 | 0.13 | 0.01 | 0.00 | 0.52 | 0.19 |

## Intersection Summary

\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.

|  | $\rangle$ |  | 7 |  |  | 4 | $\dagger$ |  | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | WBL | WBT | WBR | NBL | NBT | SBL | SBT |
| Lane Group Flow (vph) | 218 | 467 | 3 | 1074 | 246 | 4 | 3 | 164 | 322 |
| v/c Ratio | 1.03 | 0.40 | 0.01 | 1.10 | 0.26 | 0.03 | 0.00 | 0.50 | 0.63 |
| Control Delay | 92.8 | 9.3 | 5.0 | 81.0 | 2.2 | 24.8 | 0.0 | 32.6 | 18.3 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 92.8 | 9.3 | 5.0 | 81.0 | 2.2 | 24.8 | 0.0 | 32.6 | 18.3 |
| Queue Length 50th (tt) | -66 | 94 | 1 | -618 | 0 | 2 | 0 | 71 | 60 |
| Queue Length 95th (ft) | \#213 | 209 | 3 | \#848 | 32 | 9 | 0 | 131 | 146 |
| Internal Link Dist (t) |  | 1750 |  | 1759 |  |  | 261 |  | 205 |
| Turn Bay Length (ft) | 600 |  |  |  | 400 |  |  |  |  |
| Base Capacity (vph) | 211 | 1170 | 582 | 978 | 947 | 115 | 703 | 330 | 509 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 1.03 | 0.40 | 0.01 | 1.10 | 0.26 | 0.03 | 0.00 | 0.50 | 0.63 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |
| ~ Volume exceeds capacity, queue is theoretically infinite. |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer. |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |

## Conceptual Site Plan





[^0]:    ${ }^{1}$ Institute of Transportation Engineers, Trip Generation Manual, Eleventh Edition, Washington DC, 2021.

[^1]:    2 Transportation Research Board, Highway Capacity Manual, Sixth Edition, Washington DC, 2016.

