FINAL DRAINAGE REPORT

FOR

CROSSROADS MIXED USE FILING NO. 1 EL PASO COUNTY, COLORADO

DECEMBER 2021

Prepared for: Crossroads Metropolitan District No. 1 Mr. Danny Mientka 90 South Cascade Avenue, Suite 1500 Colorado Springs, Colorado Springs 80903

Prepared by:



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Project #18-003A PCD Filing No.: SF 21-029

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DRAINAGE PLAN STATEMENTS

ENGINEERS STATEMENT

The attached drainage plan and report was prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the County for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.

the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.
Virgil A. Sanchez, P.E. #37160 For and on Behalf of M&S Civil Consultants, Inc
DEVELOPER'S STATEMENT
I, the developer have read and will comply with all the requirements specified in this drainage report and plan.
BY:
BY: Danny Mientka –Owner
DATE:
ADDRESS: The Equity Group LLC 90 South Cascade Avenue, Suite 1500 Colorado Springs, CO 80903
EL PASO COUNTY'S STATEMENT
Filed in accordance with the requirements of El Paso County Land Development Code, Drainage Criteria Manual Volumes 1 and 2, and the Engineering Manual, as amended.
BY: DATE: Jennifer Irvine, P.E. County Engineer / ECM Administrator

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FINAL DRAINAGE REPORT FOR CROSSROADS MIXED USE FILING NO. 1

Purpose

This Final Drainage Report for Crossroads Mixed Use is in support of the Final Plat, Preliminary Plan, and Construction Drawings of the subject site. This report functions to identify the existing and proposed runoff patterns and recommend proposed drainage improvements which are intended to safely convey runoff through the proposed development, while minimizing impacts to downstream facilities and adjacent properties.

The Final Plat and Construction Drawings for this site will be submitted concurrently with this report. Individual drainage letters and/or reports shall be required with the development of each lot not otherwise clearly analyzed by this report for Crossroads Mixed Use Filing No. 1. This report is subject to changes dependent upon future lot development. In such case, an updated report and accompanying drawings shall be submitted.

Project Location and Description

The subject site is located at 0 Meadowbrook Parkway in the southwestern quarter of Section 8, Township 14 South, Range 65 West of the 6th P.M. in El Paso County, Colorado. The 29.049 Acre site is currently undeveloped. The site is bound to the west by undeveloped Softball West Subdivision Filing No.2, to the north by Meadowbrook Crossing Subdivision, south by Highway 24, and to the east by Newt Drive.

Revise to 10

The proposed site is will be developed into ten (1) commercial tract, one (1) multifamily residential lot, and three (3) tracts for detention and roadway use. The development will extend Meadowbrook Parkway to the west and will include a single lane roundabout to be constructed at the intersection of the Meadowbrook Parkway and Newt Drive. The property is within the commercial aviation district overlay. A rezone application has been approved to rezone 12.703 acres from CR to the RM-30 Zone.

The majority of the existing site is covered with native grasses with fair to good cover, the exception being portions of the future Meadowbrook Parkway corridor where exposed soils are present. Known earthwork operations for "borrow material" have occurred over a small area of the eastern portion of the site in early to mid 2019, but have since stabilized. A few dirt paths/trails are present along the far west end of the site, likely from recreational vehicles. Generally, the site slopes from east to west slightly greater than 1% with some localized depressions and general terrain undulations near the west boundary that have slopes ranging from 1-20%. Some of these may be the results of previous earthwork activities. The site lies within the Sand Creek Drainage Basin. No existing drainage facilities or improvements are onsite. No known irrigation systems or wells are present.

Soils

Soils in the project area have been determined to be Blakeland Loamy Sand (8) and Blendon Sandy Loam (10), which are characterized to be part of Hydrologic Soil Types "A" & "B" as determined from the United States Department of Agriculture (USDA) Natural Resources Conservation Service (NRCS) "Web Soils Survey". A soils map illustrating the site location and soil types is provided in the appendix of this report.

Floodplain Statement

According to the Federal Emergency Management Agency (FEMA) Flood Insurance Rate Map (FIRM) Nos. 08041C0754 G & 08041C0752 G, effective date December 7th, 2018, none of the site lies within a designated floodplain. A copy of these annotated maps can be found in the appendix. The Sand Creek East Fork Channel is located to the northwest of the adjacent Meadowbrook Crossing subdivision.

Previous Studies

The area which encompasses Crossroads Mixed Use has been previously studied. Below is a short outline of the assumptions regarding the lands of the subject site and those based upon the previously assembled and approved drainage reports and how the assumptions within them impact the subject site.

"Sand Creek Drainage Basin Planning Study, Preliminary Design Report", prepared by Kiowa Engineering Corporation, dated January 1993, revised March 1996.

- Establishes that the subject site falls within the East Fork Sand Creek Drainage Basin, a portion of the larger Sand Creek Watershed
- Establishes that there are no requirements for major infrastructure improvements and subsequently no drainage-improvement related reimbursements with the development of this parcel
- Drainage fees shall be required to plat the subdivision

"Claremont Business Park Filing No.2 prepared by Matrix Design Group, revised November 2006

- Establishes the drainage patterns of offsite Basins 0S-4 and E2 which are to be conveyed within the Meadowbrook Rights of Way
- Established up-gradient offsite drainage to be directed under Meadowbrook north to offsite East Fork Sand Creek Channel, and away from the subject site

"Final Drainage Report, Lot 1 24/94 Business Park Filing No.1 prepared by Core Engineering Group, dated July 14, 2016

• The development of the 24/94 Business Park FDR shows future curb inlets along the future

- Meadowbrook Parkway extension on the south and west corners of the intersection to capture runoff from up-gradient watersheds in addition to a proposed inlet which was to be located above the intersection at the northwest corner of the subject site.
- Establishes that flows from the parcel upstream of the convenience store (29/94 FDR Basin OS4) EX-B now to be collected by the extension of a 36" RCP along the south side of Meadowbrook Parkway. Runoff within the right of way/roadway separated out as Basin EX-A2.
- Continues assumption that flows from Newt Drive be conveyed north to East Fork Sand Creek.
- Evaluated pre-development drainage patterns for subject site including direct discharge flow rates to the CDOT rights of way of 1.9 and 14.5 cfs for the 5 and 100 year events, respectively. (Basin EX-E).

"Preliminary and Final Drainage Report Meadowbrook Crossing Filing No. 1 and Filing 2, El Paso County, Colorado prepared by Kiowa Engineering Corporation, dated July 25, 2017

- Proposed the installation of a future 10' Type R inlet at the southeast corner of Newt Drive and Meadowbrook Parkway with the extension of Meadowbrook Parkway to the west (along the northern boundary of the subject site). The inlet was to function to collect offsite runoff from a portion of the south half of Meadowbrook Parkway and Newt Drive north of Hwy 24. Intercepted runoff would be conveyed via a proposed 24" storm sewer to the existing storm sewer system within the Meadowbrook Crossings development.
- Proposed the installation of a 10' Type R inlet at the west end of future Meadowbrook Parkway. The inlet was to collect runoff from the north half of the future roadway. An 18" storm drain was proposed to convey collected runoff to the existing water quality pond located within the Meadowbrook Crossings Development. The report indicates a separate forebay or the modification of an existing forebay would be required.
- Shifted the location of the existing 10' Type R curb inlet to be installed upstream of the intersection of Newt Drive (as shown with the 24/94 Business Park FDR), flows in excess of the inlet capacity are to continue within the future Meadowbrook.

"Final Drainage Report for Meadowbrook Dirt Borrow Site, El Paso County Colorado, prepared by M&S Civil Consultants, November 2018.

- Evaluated onsite drainage patterns
- Excluded offsite runoff impacts from areas to the east of site.
- Allowed site to be utilized as a "borrow site" for offsite earthwork activities.

Hydrologic Calculations

Hydrologic calculations were performed using the El Paso County and City of Colorado Springs Storm Drainage Design Criteria manual and where applicable the Urban Storm Drainage Criteria Manual. The Rational Method was used to estimate stormwater runoff anticipated from design storms with 5-year and 100-year recurrence intervals.

Identify design rainfall precipitation data used.

Hydraulic Calculations

Hydraulic calculations were estimated using the Manning's Formula and the methods described in the El Paso County and City of Colorado Springs Storm Drainage Design Criteria manual. The relevant data sheets are included in the appendix of this report. Hydraulic grade line calculations shall be provided with the Final Drainage report.

Drainage Criteria

This drainage analysis has been prepared in accordance with current El Paso County Drainage Criteria Manual and, where applicable, City of Colorado Springs and Mile High Flood District Criteria Manuals. Calculations were performed to determine runoff quantities for the 5-year and

Revise statement. This is

100-year frequency storms for developed conditions using the Rational Method as required for basins having areas less than 100 acres. See Appendix for supporting calculations.

Historic (Pre-Grading) Drainage Characteristics

The historic drainage patterns discussed within this report reflect the site conditions prior to the approval of the 2018 Meadowbrook Dirt Borrow Site Grading and Erosion Control Plan. This 'historic condition' generally coincides with the existing condition analysis and mapping that accompanied that project's hydrologic analysis.

The following excerpt is from the existing Drainage Characteristics section of the Final Drainage Report for Meadowbrook Dirt Borrow Site, El Paso County, Colorado, by M&S Civil Consultants and adequately describes the general site characteristics prior to grading.

"Site vegetation is sparse, consisting primarily of native grasses and weeds. The parcel possesses a ridgeline that bisects the parcel, directing runoff to the south and west boundaries, with slopes varying from 1% to 20%. A few small depressions are located on site, near the west boundary. For the purposes of hydrologic analysis, the small depressions are not considered to detain runoff."

Given the increase in breadth and scope of this study, significant consideration of the impacts of offsite drainage from the adjacent developments will be evaluated. This includes drainage from a small portion of Hwy 24 which combines with flows within existing from portions of Newt Drive. Runoff from this offsite area combines with by-pass flows from two inlets located within existing Meadowbrook Drive, prior to entering the site at its northeast corner. Runoff from these locations ultimately combines with onsite flows within the proposed Meadowbrook Parkway corridor, prior to discharging to downstream properties.

The detailed description of the historic (pre-grading) condition is as follows. Please refer to the historic conditions drainage map which is provided within the appendix of this report.

Does not match flows shown on FDR drainage plan for Lot 1 24/94 Business Park Filing 1

Historic Conditions - Detailed Drainage Discussion

Design Point 1

Basin E2 (Claremont Business Park Filing No.2) consists of a reported 3.86 developed acres of development located along the southeastern half of existing Meadowbrook Parkway, some 1200' northeast of the subject site. Runoff produced by the offsite development (CBPF2 Lot 46) is conveyed to Meadowbrook Parkway at flow rates of Q5=15.1 and Q100=28.6 cfs in the 5 and 100-year storm events respectively. The collected flows combines with runoff from Basin EX-A2 (Lot 1 24/94 Business Park Filing No.1) (Q5=2.5, Q100=4.5 cfs) which consists of 0.59 acres of the southeastern half of Meadowbrook Parkway, and is located immediately east of existing Newt Drive. The collected flows from the two basins culminate at Design Point 1 at peak rates of Q5=14.2 and Q100=26.5 cfs. An existing 10' CDOT Type R at-grade inlet (Inlet 1) intercepts flows of Q5=8.4 and Q100=11.1 cfs, with subsequent by-pass flows of 5.8 and 15.4 cfs in the 5 and 100 year events. Surface flows continue west within the south half of existing Meadowbrook Parkway.

Design Point 2

Basin OS-A (Meadowbrook Crossing Filing 1 and 2) consists of 1.29 acres of the northern half of existing Meadowbrook Parkway located immediately east of Newt Drive. Runoff produced within this basin totals Q5=3.1 and Q100=6.0 cfs. An existing 10' CDOT Type R at grade inlet (Inlet 2) collects runoff of Q5=3.1 and Q100=5.3 cfs, with subsequent by-pass flows in only the 100 year event of 0.7 cfs. Runoff leaving the design point continuing west within the north half of existing Meadowbrook Parkway.

Design Point 3

Basin OS-1 consists of approximately 1.28 developed acres of existing Newt Drive located along the eastern boundary of the site. Runoff produced within the basin (Q5=5.8 cfs, Q100=10.5 cfs) combine with flow-by from **DP1** in the intersection at peak flow rates of 9.8 cfs, and 22.5 cfs in the 5 and 100-year storm events.

Surface runoff and by-pass flows from both **DP2** and **DP3** enter **Basin A** in the undeveloped rights of way of future Meadowbrook Parkway, at the northeast corner of the site.

Design Point 4

Basin A consists of 12.88 undeveloped acres located along the northern boundary that drains from east to west across the subject site. Runoff produced by this basin (Q5=1.9 cfs, Q100=14.2 cfs) combine with flows from **DP2 and DP3.** The cumulative runoff at **DP4** of Q5=7.4 cfs, Q100=27.7 cfs discharges onto the adjacent property (Lot 1, Softball West Subdivision 2) along the western boundary of the site, approximately 250' to south of the northern property line.

Design Point 5

Basin B consists of 13.63 undeveloped acres located along the western side of the subject site. Runoff produced by the basin generally flows from northeast to southwest, discharging onto the adjacent property (Lot 2, Softball West Subdivision 2) approximately 200' north of the southern property line. Runoff reaching the boundary at **DP5** are calculated at 8.3 cfs and 18.2 cfs in the 5 year and 100 year events respectively.

Revise to match drainage map summary table in appendix.

information in appendix.

Design Point 6

Basin C currently consists of 5.89 undeveloped acres located along the southern boundary of the site. Runoff produced within the basin travels east to west as sheet flow before eventually discharging into the existing barrow ditch which travels along the US HWY 24 CDOT right of way. Peak runoff rates reaching the subdivision boundary at **DP6** are calculated at 1.2 cfs and 8.5 cfs in the 5 year and 100 year events respectively.

Design Point 7

Include flows for Basin OS-2.

Basin OS-2 consists of 4.98 acres of a portion of the northern half of the US HWY 24 roadway and the adjoining, native, grass-lined barrow ditch. Runoff produced within the basin combines with flows from the subject site at cumulative peak runoff rates of 10.4 and 31.9 cfs in the 5 and 100 year storm events at **DP7**. A modeled hydraulic cross section of the ditch section at **DP7** calculates flow depths of 0.76 feet traveling at a velocity of approximately 3.54 feet per second. Input parameters for this analysis can be found in the Hydraulics section of the Appendix. Swale parameters do not match

Runoff from **Design Points 4 and 5** ultimately combine with the flows from **DP7** within the barrow ditch of US Hwy 24 several hundred feet downstream of the subject site. An existing 36" RCP culvert located at the interchange of HWY 24 and Peterson Road aids in conveying a portion of the runoff from the subject site and adjacent offsite areas under the roadway. Flows in excess of the culverts carrying capacity, overtop the roadway before rejoining within a subsequent drainage swale that parallels the west bound HWY 24 on-ramp. Ultimately flows discharge into the East Fork of the Sand Creek via an existing riprap rundown. Site visits conducted by M&S Civil at the time of the writing of this report, found no significant signs of erosion or deposition along the aforementioned corridor.

Provide analysis of this existing culvert to show what flow is handled by culverts and how much overtops and how deep over roadway.

A Drainageway Exhibit in the appendix of this report provides an aerial illustration of the aforementioned conveyance route to the channel, which will also serve to function as the emergency overflow path for the proposed site development.

Existing Drainage Characteristics

The subject site has been utilized as a "borrow site" to provide surplus earthwork to offsite developments in the area. This recent grading effort occurred during the spring and summer of 2019. At the request of El Paso County, an existing conditions drainage analysis has been provided to show the changes to the topography and drainage patterns as a result of this effort. As the only changes between the two conditions are onsite, the offsite drainage patterns calculations and

assumptions determined within the historical analysis will remain the same. It should be noted that the subject site was not disturbed to the full extent of the approved plan, with limited excavation primarily occurring within the eastern side of the subject site.

List basins & DP's that did not change.

In the existing condition, vegetation remains sparse, consisting primarily of native grasses and weeds with good to fair cover. Areas disturbed by grading activities were reseeded and have since stabilized. With regards to historic versus existing drainage basin delineation, the bisecting parcel ridgeline has been relocated further to the south, which results in redirecting more of the runoff to the southwestern part of the site and less to the CDOT rights of way. The few small depressions remain on site, near the west boundary. For the purposes of hydrologic analysis, these small depressions will continue to not be evaluated for their ability to detain runoff. Ultimately, all runoff from the parcel is conveyed to the west towards existing drainage facilities located under Peterson Road and ultimately the East Fork of Sand Creek as in the historic condition.

This section only discusses the changes in basin geometry and drainage pattern and provides a direct comparison of the historic versus existing conditions, utilizing the same outfall (design) points, which have remained undisturbed.

Design Point 4

Provide Basin A flows

Basin A currently consists of 11.02 acres which continues to drain from east to west eventually discharging along the western boundary of the site, approximately 250' south of the northern property line. Peak runoff, post grading, has decreased to 7.1 and 25.5 cfs as compared to the historic condition flow rates of 7.4 and 27.7 cfs in the 5-year and 100-year events respectively.

Design Point 5

Basin B currently consists of 17.31 acres that drains from northeast to southwest, eventually discharging along the western boundary of the site, approximately 200' north of the southern property line. Peak runoff rates at this location are also than lower than the historic conditions with post grading flows of 5.0 cfs and 14.5 cfs, as compared to 8.3 cfs and 18.2 cfs in the 5-year and 100-year events respectively. Despite the basin currently being larger in area than in the historic condition, a decrease in the peak flow rates occurs as a result of a longer flow path to the given design point.

Design Point 6

Basin C consists of 3.99 undeveloped acres that drains from east to west into the US HWY 24 Right of Way at the southern boundary of the site. The peak runoff at this location is less than the historic condition at an estimated 0.9 and 6.3 cfs, as compared to 1.2 and 8.5 cfs in the 5-year and 100-year events, respectively.

Design Point 7

Provide Basin OS-2 flows

Basin OS-2 consists of 4.98 acres of the northern half of the US HWY 24 roadway and adjoining native grass lined barrow ditch. Runoff produced within the basin combines with runoff from the subject site at lower cumulative peak runoff rates of 9.9 and 28.0 cfs in the 5 and 100-year storm events at **DP7** as compared to 10.4 and 31.9 cfs in the historic condition.

Four Step Process

- Step 1 Employ Runoff Reduction Practices Approx. 2.54 acres of the proposed development is being set aside for a Full Spectrum Detention (FSD) Pond. Whenever possible, runoff produced within developable area containing impervious surfaces will be routed through landscaped areas or earthen swales (grass-lined where slope exceeds 2%) to minimize direct connection of impervious surfaces. In the interim, runoff will be reduced through the use of (4) temporary sediments ponds until the ground has been stabilized with vegetation or permanently developed.
- Step 2 Stabilize Drainageways The development of this site is not anticipated to have negative effects on downstream drainage ways since flows released will be below historic rates. In the interim, the site proposes four temporary sedimentation ponds, before discharging at the southwest property corner of the site and onto an adjacent undeveloped property via riprap-lined spillways. This ensures that in this stage of the development negative effects on the downstream drainage ways will be avoided.

In the final condition, the flow is discharged to the same location offsite through an RCP pipe outfall lined with rip rap. From here it continues southwest in CDOT's man-made roadside ditch until it reaches Peterson Road. It is then conveyed to the other side of the road, into a similar earthen channel, via a 36" CMP culvert. The drainage continues southwest in the right of way, until it reaches the East Fork Sand Creek Channel. Existing rip rap barriers are lined throughout this portion of the pathway approximately every 90-100 feet within the ditch to the channel bank. The Drainageway Exhibit provided in the Drainage Maps section of the Appendix provides a visual representation of this information. Swale calculations for various storm events are provided at the project site's discharge location to ensure the facility can adequately contain and convey the flows.

- **Step 3 Provide Water Quality Capture Volume (WQCV)** The site will use a Full Spectrum Detention (FSD) Pond to control developed runoff that is discharging into an existing CDOT ROW roadside ditch and ultimately into Sand Creek. The FSD pond's outlet structure will be designed to drain the water quality event storm in 40 hours, while reducing the 100 year peak discharge to approximately 90% of the predevelopment conditions.
- Step 4 Consider Need For Selecting Industrial And Commercial BMP's The proposed development will implement a Stormwater Management Plan including property housekeeping practices, spill containment procedures, and coverage of storage/handling areas. Specialized BMP's are not required since the vertical development of the commercial areas are unknown at this time.

Proposed Drainage Characteristics

Revise to 10 lots

The proposed site is will be developed into ten (1) commercial tract, one (1) multifamily residential lot, and three (3) tracts for detention and roadway use. The proposed development will extend Meadowbrook Parkway to the west and will include a single lane roundabout to be constructed at the intersection of the Meadowbrook Parkway and Newt Drive to aid in traffic control. A proposed private looped roadway, consisting of Southern Rail Point and Pacific Rail Point will extend into the site to provide access and a utility corridor to both the commercial and residential developments. At this time, it is anticipated that the development and design of Lot 11 (by others) is planned to occur concurrently with the construction of the proposed utilities and infrastructure provided by this plan. A separate drainage letter or report will be required for that portion of the development.

The following summary generalizes the proposed drainage patterns and drainage improvements required to safely route developed runoff to downstream facilities.

A storm sewer pipe and inlet will be constructed at the southwest corner of the newly constructed roundabout to aid in collecting runoff reaching the site from offsite watersheds. These facilities will connect to the existing system located inside the existing Meadowbrook Subdivision. Bypassed flows and developed flows within the newly constructed Meadowbrook Parkway will be collected by a pair of sump inlets located at the west end of the roadway. The drainage facilities located with the rights of way will be public and all remaining onsite storm sewer and drainage improvements shall be private. A future, private, looped roadway will provide access and utility corridors for development. Private storm sewer mains, stubs, and inlets will be extended along these corridors to serve the development. The extension of these facilities beyond what is shown by this plan is likely with future development. Runoff collected by the infrastructure will be conveyed to a single full spectrum detention pond located in the southwest corner of the subdivision. The proposed outfall from the pond is planned to discharge into the existing barrow ditch located with the north half of the existing CDOT Right of Way. A drainage easement will be required from CDOT for the outfall and slope protection facilities that fall within the corridor. It should be noted that the storm outfall will be shaped into the existing hillside and any soil riprap protection will be buried. Runoff leaving the site and entering the CDOT corridor will discharge at less than historic rates. The previous discharge points along the west boundary of the subject site, which also previously contributed to the barrow ditch will be virtually eliminated, further reducing the peak flow rates to downstream facilities.

Proposed Detailed Drainage Discussion

Design Point 1

Basin E2 (Claremont Business Park Filing No.2) consists of a reported 3.86 developed acres of development located along the southeastern half of existing Meadowbrook Parkway some 1200' northeast of the subject site. Runoff produced by the offsite development (CBPF2 Lot 46) is conveyed to Meadowbrook Parkway at flow rates of Q5=15.1 and Q100=28.6 cfs in the 5 and 100-year storm events respectively. The collected flows combines with runoff from **Basin EX-A2** (Lot

it-grade

1 24/94 Business Park Filing No.1) (Q5=2.5, Q100=4.5 cfs) which consists of 0.59 acres of the southeastern half of Meadowbrook Parkway located immediately east of existing Newt Drive. The collected flows from the two basins culminate at **Design Point 1** at peak rates of Q5=14.2 and Q100=26.5 cfs. An existing 10' CDOT Type R at-grade inlet (**Inlet 1**) intercepts flows of Q5=8.4 and Q100=11.1 cfs, with subsequent by-pass flows of 5.8 and 15.4 cfs in the 5 and 100 year events. Surface flows continue west within the south half of existing Meadowbrook Parkway.

Design Point 2

Basin OS-A (Meadowbrook Crossing Filing 1 and 2) consists of 1.29 acres of the northern half of existing Meadowbrook Parkway located immediately east of Newt Drive. Runoff produced within this basin totals Q5=3.1 and Q100=6.0 cfs. An existing 10' CDOT Type R at grade inlet (**Inlet 2**) collects runoff of Q5=3.1 and Q100=5.3 cfs, with subsequent by-pass flows in only the 100 year event of 0.7 cfs. Runoff leaving the design point continuing west within the north half of existing Meadowbrook Parkway.

Design Point 3

In accordance with the assumptions outlined within the Meadowbrook Subdivision Final Drainage Report, an offsite public storm sewer pipe and inlet will be constructed at the southwest corner of the proposed roundabout to aid in collecting runoff from a portion of the offsite watershed located to the east of the site. A new manhole may be required to connect the outfall to the existing pipe located inside the existing Meadowbrook Subdivision. As this area is already paved, increases to the imperviousness of this area are not anticipated.

Basin OS-1 consists of approximately 1.40 acres of existing Newt Drive that will be retrofitted with new raised median as part of an intersection conversion to a roundabout. Runoff produced within the basin (Q5=6.4 and Q100=11.5 cfs) will combine with flow-by from **DP1** at a proposed public 10'a-grade inlet located at DP3. A proposed public 24" storm sewer (**PR1**) will convey water across the intersection to the existing 42" storm sewer with Meadowbrook Crossings in accordance with that subdivision's drainage report. A new larger manhole may be required to make the connection to the existing line. It is important to note that this connection remains feasible as the roundabout is not anticipated to significantly increase the overall imperviousness of the area above that of the existing condition. Runoff in excess of the inlet capacity (Q5=3.5 and Q100=13.5 cfs) will continue westward via the curb and gutter of Proposed Meadowbrook Parkway.

Design Point 4

Basin A consists of 1.67 acres of the north half of proposed Meadowbrook. Runoff within this basin (Q5=6.5 and Q100=11.6 cfs) combines with minor flow by from **DP2** for total flows of 6.5 and 12.4 cfs in the 5 year and 100 year events, respectively. A proposed 15' at grade inlet located at the west end of the roadway, just before the proposed temporary cul-de-sac, is anticipated to intercept all of the minor event flows, conveying them to **PR1.5**, a 24" RCP public storm sewer. 1.9 cfs of flowby in the 100 year event continues west towards **Inlet 4.5**, a **NEENAH R-6116** grated manhole lid and frame at the low point of the cul-de-sac. Supporting calculations for this non-standard inlet are provided in the Appendix. This inlet will convey the rest of the runoff (Q100=1.9 cfs) underneath the roadway via a public 24" storm sewer (**PR2**). The NEENAH inlet

Calculation seen in the Please program of th

is to be removed and replaced with a standard CDOT 5' Type R inlet when the roadway cul de sac is removed and the roadway is extended to the west with future development.

Design Point 5

Basin B consists of 1.48 acres of the south half of proposed Meadowbrook Parkway. Runoff produced within this basin (O5=5.8 and O100=10.3 cfs) combines with flow-by leaving **DP3**. A proposed public 15' sump inlet (Inlet 5) located at west end of the roadway will prevent developed flows from leaving exiting the roadway corridor. The intercepted runoff of 9.8 cfs and 25.8 cfs in the 5 and 100-year events will combine with **PR2** flows in a 36" private storm sewer system (PR3, by others). Combined flows within the proposed system are calculated to reach peak rates of 16.4 and 38.5 cfs. The storm sewer system is to be planned by others through the multi-family site (Lot 11) but ultimately will tie back into the system at **DP15**.

Design Point 6

Basin C consists of 4.61 acres of commercial lots (1-5 and portions of lot 6) located along the east side of the site. Earthen swales are proposed to convey flows along the basin edge to the proposed depression. Rip rap is proposed at the terminus and will protect the slopes of the depression. A private 30" storm sewer (PR4-PR6) is provided to collect flows of Q5=18.7 and Q100=34.5 cfs at **DP6** in the 5 and 100-year storm event, respectively. Intercepted flows are conveyed west underground within the roadway tract. Include riprap size/type

for DP 6 and DP 7.

from the proposed inlets.

match inlet spreadsheet

Design Point 7

Basin D consists of 2.22 acres of commercial lots located between Meadowbrook Parkway and the looped roadway. Basin D, which includes portions of Lots 9 and 10, will require a private 24" storm drain (PR8) to collect flows of Q5=9.3 and Q100=17.0 cfs in the 5 and 100 year storm events, respectively. Earthen swales are proposed to convey flows along the basin edge to the proposed depression. Rip rap is proposed at the terminus of the swale and will protect the slopes of the depression. Intercepted rates do not

Design Points 8 and 9

Basin E consists of 2.71 acres of commercial lots and roadway located in the central portion of the site. Two private 10' CDOT Type R at-grade inlets (Inlets 7 and 8) located on the north and south sides of the roadway will each collect flows of 5.2 and 9.5 cfs in the 5 and 100 year storm events, respectively. Runoff bypassing the inlets continues to downstream infrastructure. Flows collected from the inlets will be conveyed to a box base manhole in the middle of the planned roadway via two private 30" (PR9) and 18" (PR10) storm drains. A proposed 36" private storm sewer (PR11) will then convey flows west underground at peak flow rates of 35.0 and 60.5 cfs in the 5 and 100year events. PR12, a 42" private storm sewer, then directs the system south from another box base manhole. State what flowby rates are

Design Point 10

Area doesn't match

spreadsheet

Basin G (Q5=2.1, Q100=3.8) cfs consists of 0.77 acres of multi-family lots and roadway located in the central portion of the site. A private 10' CDOT Type R sump inlet (Inlet 8) located on the west side of the street functions to collect the runoff from Basin G. PR13, a proposed 18" private storm sewer, will direct runoff east to a box base manhole at peak flow rates of 2.1 cfs and 3.8 cfs in the minor and major storm events, respectively.

Design Point 11

List Basin G1 flow

Basin G1 consists of 0.60 acres of commercial lots and roadway located in the central portion of the site. A private 15' CDOT Type R sump inlet (**Inlet 9**), located on the east side of the street functions to collect the runoff from **Basin G1** as well as any bypass flows from Design **DP8 and 9**. **PR14**, a proposed 30" private storm sewer, will direct runoff west to an underground box base manhole at peak flow rates of 3.6 cfs and 17.3 cfs in the minor and major storm events, respectively. From the junction, flows combine at **PR15** (Q5=39.4, Q100=79.6), a 42" private storm sewer, and are directed south.

Design Point 12

Basin F consists of 2.57 acres of commercial lots (Lot 8 and portions of Lot 7) located along the southern boundary of the site. An earthen swale is proposed to convey flows to the depression. A private 24" storm drain (**PR16**) is provided to collect flows of Q5=10.8 and Q100=19.6 cfs at **DP12** in the 5 and 100 year events, respectively. Intercepted flows are conveyed west underground to the main line, **PR17**, where they combine with flows from **PR15** at the manhole junction. **PR17** and **PR18** (private 48" storm sewers) direct the collected runoff to the concrete forebay located within the east end of the proposed full spectrum detention pond at peak flow rates of Q5=49.1 and Q100=97.4 cfs.

Design Point 13

DP13 consists of a 2' bottom earthen swale that is designed to convey runoff from the proposed apartment site (Lot 11) to the northwest corner of the pond. A proposed 2' wide rip rap rundown with 2:1 side slopes will convey flows into the pond. The maximum runoff expected from the site is 2.0 and 7.5 cfs in the 5 and 100 year events, respectively. Calculations for the swale and rundown are included in the appendix of this report.

Design Point 14

DP14 represents the on-site portion of a proposed, v-shaped, earthen swale that collects flows not anticipated to be collected by storm sewer, and combines with flows from **Design Point 13**. Runoff collected within this swale (maximum Q5=2.7 cfs, Q100=9.8 cfs) is conveyed from north to south to the proposed FSD pond at **DP15**. Calculations for this swale before and after the junction are provided in the appendix of this report.

Design Point 15

(Section A-A)

Basin J consists of 3.21 acres of the p than D-D in appendix n detention pond. Runoff produced within this basin reaches peak runoff rates (Q5=2.3 and Q100=10.0 cfs) combines with flows from **DP14**, **PR18**, and **PR19** (48" RCP) in the pond. The cumulative flows at **FSD Pond 1** are Q5=99.6 and Q100=216.6 cfs. Flow exiting the pond will be routed to the existing 5' bottom earthen swale in CDOT's Right of Way at **DP16** via 18" private **PR20** (Q5=1.2 and Q100=11.4 cfs). A rip rap pad is provided as outlet protection.

List riprap size/type and note that sizing calculations are included in appendix

for swale B-B, since different

(Section D-D

flow of PR 17 & PR 21

(Section B-B)

(Section C-C)

Pond release flows at

Explain why flows are lower

Design Point 16

Basin OS-2 consists of 4.98 acres. Approximately half of this basin is comprised of the paved surface of U.S. Highway 24, while the other half is comprised of the 5 foot bottom earthen swale in CDOT's Right of Way. Runoff produced within this basin (Q5=8.7 and Q100=19.6 cfs) flows from northeast to southwest, combining with flows from DP15. This combination of runoff collects in the existing swale in the right of way. The cumulative flows at DP16 are Q5=9.9 and Q100=31.0 cfs, which are lower than the historic and existing rates. Calculations for the 5, 10, 25, 50, and 100 year events for this swale are provided in the Appendix. Flows from this design point continue to downstream infrastructure. A rip rap pad is located at the terminus of the storm sewer, as previously mentioned in DP15's discussion.

Water Quality Provisions and Maintenance

Include discussion for all sump inlets where overflow will go if inlets become clogged.

The proposed full spectrum detention (FSD) pond functions to provide detention and water quality for the proposed development. This full spectrum detention pond will function to treat approximately 32.10 acres of 78.67% impervious, tributary area by providing 0.863 acre-feet of storage for the water quality event, 3.316 acre feet of storage at the EURV storm event, and 4.619 acre-feet of storage in the 100-year event. The 33' wide emergency spillway is designed with a foot of freeboard in the 100-year event. This spillway safely conveys flows to CDOT's Right of Way in the event of outlet clogging or failure, and will be armored with permanent erosion control fabric and soil rip rap. The results show that the FSD pond remains functional in the 100-year event and the outlet structure is able to discharge flows to an existing swale and ultimately to Sand Creek. The sizing for the full spectrum detention facility has been determined using the guidelines set forth in the Urban Drainage and Flood Control District Criteria Manual. Refer to the UDFCD MHFD-Detention, Version 4.03, Excel Workbook located within the appendix of this report for calculations.

The proposed FSD pond will be privately owned and maintained by Crossroads Metropolitan District No. 1. Access to the pond shall be granted to the owner/district and El Paso County for access and maintenance of the private facility. A private maintenance agreement document shall accompany this report submittal.

Erosion Control

It is the policy of the El Paso County that M&S Civil Consultants submit a grading and erosion control plan with the drainage report. The plan includes proposed silt fence, vehicle tracking control, (4) temporary sediment basins, and straw bale barriers as proposed erosion control measures. The plan also includes provisions for stockpiling, staging, and concrete washout areas. A stormwater management plan is provided to accompany the plans.

In the report text address the increase in post-development discharge at the pond outlet, as shown on pg 44 below.

Per ECM Chap 3.2.8.B, "The proposed project or developed land use shall not change historical runoff values, cause downstream damage, or adversely impact adjacent properties." Increases from the historical flowrates is allowable without full spectrum detention if it is shown (via text and/or calcs) that the flow increase can be accommodated downstream (ie: show that there is a suitable outfall, per ECM, Chap 3.2.4). If applicable, reference the downstream facilities in a DBPS or MDDP.

Revise to exclude Tract D.

Add a note stating that Tract D drainage fee shall be paid with future platting/development of said tract.

2021 Drainage & Bridge Fees:

Drainage Fees: 29.049 x 78.67% **Bridge Fees:** 29.049 x 78.67%

Drainage fees shall be paid at the time of platting.

Construction Cost Estimate (Non-Reimbursable)

Item	Amount	Unit	Unit Cost	Total Cost	
10' CDOT Type R Inlet	4	EA	\$ 9,890.00	\$ 39,560.0	00
15' CDOT Type R Inlet	3	EA	\$ 13,002.00	\$ 39,006.0	00
Custom Grate Inlet	1	EA	\$ 5,000.00	\$ 5,000.0	00
Type I MH	8	EA	\$ 9,800.00	\$ 78,400.0	00
Type II MH	1	EA	\$ 6,000.00	\$ 6,000.0	00
Rip Rap Aprons	84.5	CY	\$ 65.00	\$ 5,492.5	50
18" SD	113	LF	\$ 45.00	\$ 5,085.0	00
24" SD	232	LF	\$ 81.00	\$ 18,792.0	00
30" SD	432	LF	\$ 100.00	\$ 35,800.0	00
36" SD	16	LF	\$ 124.00	\$ 1,984.0	00
42" SD	396	LF	\$ 166.00	\$ 65,736.0	00
48" SD	395	LF	\$ 202.00	\$ 79,790.0	00
Concrete Channel	2,416	SF	\$ 5.00	\$ 12,080.0	00
Outlet Structure	1	EA	\$ 15,000.00	\$ 15,000.0	00
Forebay	2	EA	\$ 8,000.00	\$ 16,000.0	00
Gravel (Access)	629	CY	\$ 52.00	\$ 32,708.0	00
Spillway	1	EA	\$ 20,000.00	\$ 20,000.0	00
TOTAL COST:	5			476,433.	50

M & S Civil Consultants, Inc. (M & S) cannot and does not guarantee the construction cost will not vary from these opinions of probable costs. These opinions represent our best judgment as design professionals familiar with the construction industry and this development in particular. The above is only an estimate of the facility cost and drainage basin fee amounts in 2021.

Summary:

The construction of this site is for the purposes of creating a commercial tract, detention tract, and an apartment site. The site will be graded and all disturbed areas will be seeded. Post construction runoff will be discharged to downstream property at rates that are below historic discharge rates. In the historic condition, the total flows leaving the site that reach the East Fork Sand Creek Channel are 19.0 cfs and 68.1 cfs in the 5 year and 100 year storm events, respectively. Through the strategic design and placement of storm sewer infrastructure components, the overall discharge rates are reduced to approximately 50% of the historic rates at 9.9 and 31.0 cfs in the proposed condition. Erosion control measures will be implemented to prevent sediment migration. The construction of Crossroads Mixed Use Filing No. 1 shall not

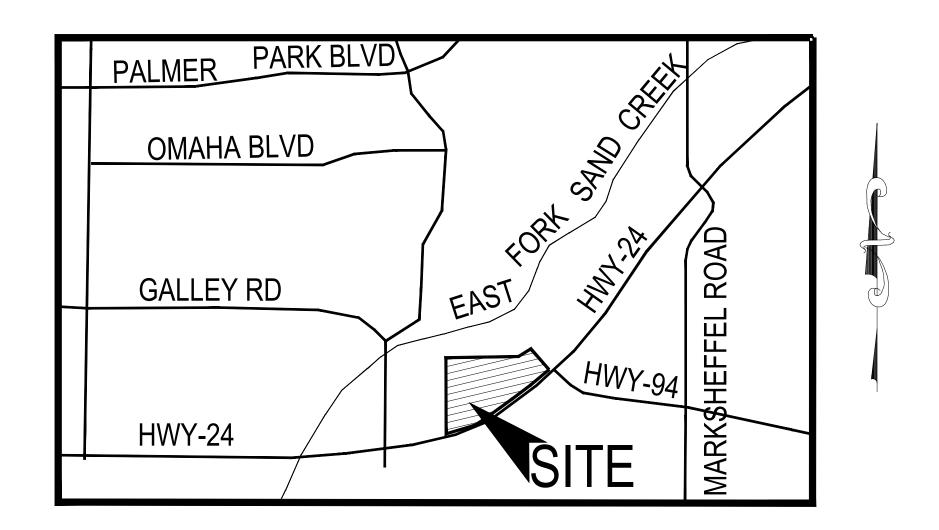
adversely affect adjacent or downstream property. Subsequent drainage reports will be required when the site is developed behind the uses defined within this report.

References

- 1.) "El Paso County and City of Colorado Springs Drainage Criteria Manual".
- 2.) "Urban Storm Drainage Criteria Manual"
- 3.) SCS Soils Map for El Paso County.
- 4.) Flood Insurance Rate Map (FIRM), Federal Emergency Management Agency, Revised date December 7th, 2018.
- 5.) "Final Drainage Report for Claremont Business Park Filing No. 2", dated November 2006, by Matrix Design Group, Inc.
- 6.) "Preliminary and Final Drainage Report Meadowbrook Crossing Filing 1 and Filing 2", dated July 25, 2017, by Kiowa Engineering Corporation.
- 7.) "Final Drainage Report Lot 1 24/94 Business Park Filing No. 1 on Platte Avenue and Meadowbrook Parkway", dated April 28, 2016 and revised July 14, 2016, by Core Engineering Group, LLC.
- 8.) "Final Drainage Report for Meadowbrook Dirt Borrow Site", dated November 2018, by M&S Civil Consultants, Inc.
- 9.) "Sand Creek Drainage Basin Planning Study", revised March 1996, by Kiowa Engineering Corporation.

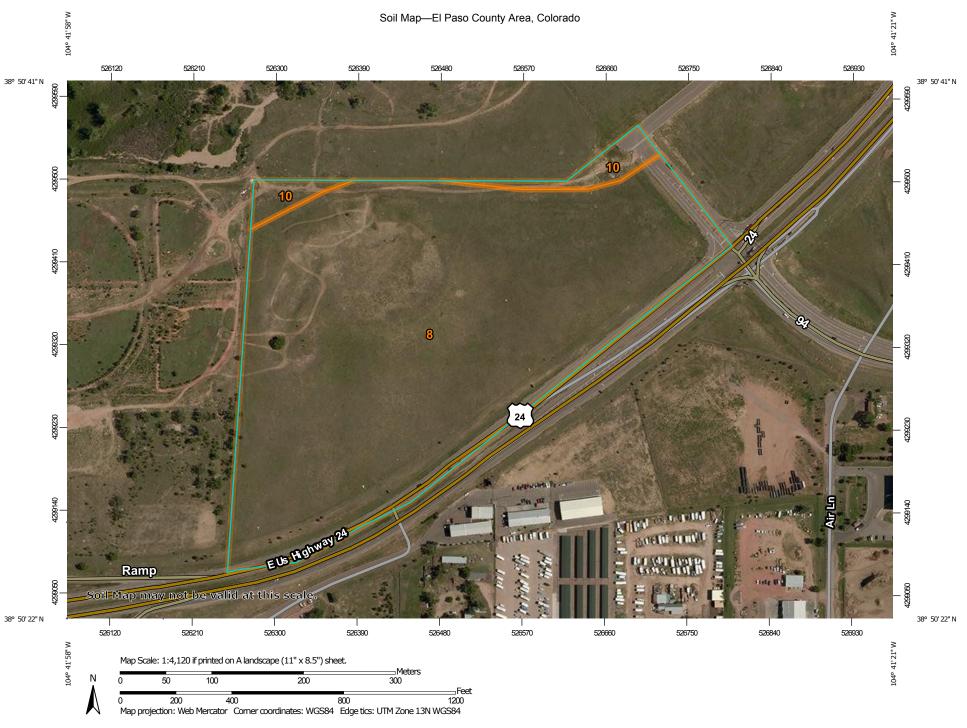
APPENDIX

VICINITY MAP



VICINITY MAP N.T.S.

SOILS MAP



MAP LEGEND

Area of Interest (AOI)

Area of Interest (AOI)

Soils

Soil Map Unit Polygons



Soil Map Unit Points

Special Point Features

Blowout

Borrow Pit

Clay Spot

Closed Depression

Gravel Pit

Gravelly Spot

Landfill

Lava Flow

Marsh or swamp

Mine or Quarry

Miscellaneous Water

Perennial Water

Rock Outcrop

Saline Spot
Sandy Spot

Severely Eroded Spot

Sinkhole

Slide or Slip

Sodic Spot

CLIND

Spoil Area

Stony Spot

Very Stony Spot

Wet Spot

△ Other

Special Line Features

Water Features

Streams and Canals

Transportation

Rails

Interstate Highways

US Routes

Major Roads

Local Roads

Background

Aerial Photography

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24.000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service Web Soil Survey URL:

Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: El Paso County Area, Colorado Survey Area Data: Version 15, Oct 10, 2017

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Jun 3, 2014—Jun 17, 2014

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
8	Blakeland loamy sand, 1 to 9 percent slopes	35.2	95.4%
10	Blendon sandy loam, 0 to 3 percent slopes	1.7	4.6%
Totals for Area of Interest		36.9	100.0%

FIRM PANELS

NOTES TO USERS

This map is for use in administering the National Flood Insurance Program. It does not necessarily identify all areas subject to flooding, particularly from local drainage sources of small size. The community map repository should be consulted for possible updated or additional flood hazard information.

To obtain more detailed information in areas where Base Flood Elevations (BFEs) and/or floodways have been determined, users are encouraged to consult the Flood Profiles and Floodway Data and/or Summary of Stillwater Elevations tables contained within the Flood Insurance Study (FIS) report that accompanies this FIRM. Users should be aware that BFEs shown on the FIRM represent rounded whole-foot elevations. These BFEs are intended for flood insurance rating purposes only and should not be used as the sole source of flood elevation information. Accordingly, flood elevation data presented in the FIS report should be utilized in conjunction with the FIRM for purposes of construction and/or floodplain management.

Coastal Base Flood Elevations shown on this map apply only landward of 0.0' North American Vertical Datum of 1988 (NAVD88). Users of this FIRM should be aware that coastal flood elevations are also provided in the Summary of Stillwater Elevations table in the Flood Insurance Study report for this jurisdiction. Elevations shown in the Summary of Stillwater Elevations table should be used for construction and/or floodplain management purposes when they are higher than the elevations shown on this FIRM.

Boundaries of the floodways were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations with regard to requirements of the National Flood Insurance Program. Floodway widths and other pertinent floodway data are provided in the Flood Insurance Study report for this jurisdiction.

Certain areas not in Special Flood Hazard Areas may be protected by flood control structures. Refer to section 2.4 "Flood Protection Measures" of the Flood Insurance Study report for information on flood control structures for this jurisdiction.

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NGS Information Services NOAA, N/NGS12 National Geodetic Survey SSMC-3, #9202 1315 East-West Highway Silver Spring, MD 20910-3282

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Base Map information shown on this FIRM was provided in digital format by El Paso County, Colorado Springs Utilities, City of Fountain, Bureau of Land Management, National Oceanic and Atmospheric Administration, United States Geological Survey, and Anderson Consulting Engineers, Inc. These data are current as of 2006.

This map reflects more detailed and up-to-date stream channel configurations and **loodplain delineations** than those shown on the previous FIRM for this jurisdiction. The floodplains and floodways that were transferred from the previous FIRM may have been adjusted to conform to these new stream channel configurations. As a result, the Flood Profiles and Floodway Data tables in the Flood Insurance Study Report (which contains authoritative hydraulic data) may reflect stream channe distances that differ from what is shown on this map. The profile baselines depicted on this map represent the hydraulic modeling baselines that match the flood profiles and Floodway Data Tables if applicable, in the FIS report. As a result, the profile paselines may deviate significantly from the new base map channel representation and may appear outside of the floodplain.

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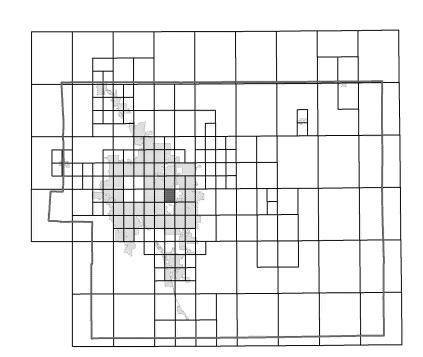
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El Paso County Vertical Datum Offset Table **Vertical Datum** Flooding Source REFER TO SECTION 3.3 OF THE EL PASO COUNTY FLOOD INSURANCE STUDY FOR STREAM BY STREAM VERTICAL DATUM CONVERSION INFORMATION

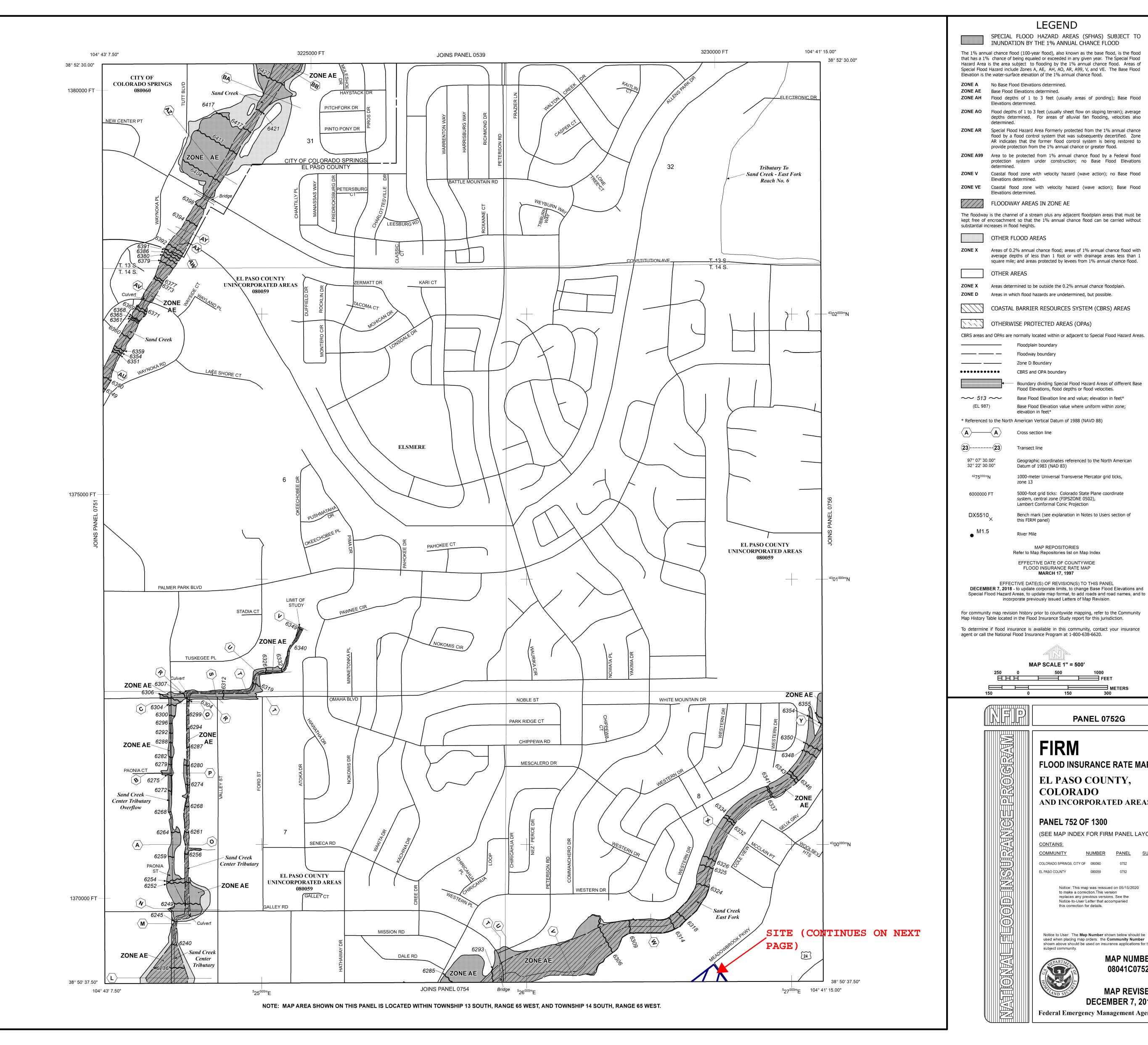
Panel Location Map



This Digital Flood Insurance Rate Map (DFIRM) was produced through a Cooperating Technical Partner (CTP) agreement between the State of Colorado Water Conservation Board (CWCB) and the Federal Emergency Management Agency (FEMA).



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LEGEND

Floodway boundary

Zone D Boundary

elevation in feet*

Cross section line

this FIRM panel)

Datum of 1983 (NAD 83)

CBRS and OPA boundary

Boundary dividing Special Flood Hazard Areas of different Base

lood Elevations, flood depths or flood velocities.

Base Flood Elevation line and value; elevation in feet*

Base Flood Elevation value where uniform within zone;

Geographic coordinates referenced to the North American

1000-meter Universal Transverse Mercator grid ticks,

5000-foot grid ticks: Colorado State Plane coordinate

Bench mark (see explanation in Notes to Users section of

system, central zone (FIPSZONE 0502).

MAP REPOSITORIES

Refer to Map Repositories list on Map Index

EFFECTIVE DATE OF COUNTYWIDE FLOOD INSURANCE RATE MAP

MARCH 17, 1997

EFFECTIVE DATE(S) OF REVISION(S) TO THIS PANEL

incorporate previously issued Letters of Map Revision.

FIRM

EL PASO COUNTY

COLORADO

PANEL 752 OF 1300

PANEL 0752G

FLOOD INSURANCE RATE MAP

AND INCORPORATED AREAS

(SEE MAP INDEX FOR FIRM PANEL LAYOUT)

Notice: This map was reissued on 05/15/2020 to make a correction. This version

replaces any previous versions. See the

Notice to User: The Map Number shown below should be used when placing map orders: the Community Number shown above should be used on insurance applications for the

Federal Emergency Management Agency

MAP NUMBER

MAP REVISED

DECEMBER 7, 2018

08041C0752G

Notice-to-User Letter that accompanied this correction for details.

EL PASO COUNTY,

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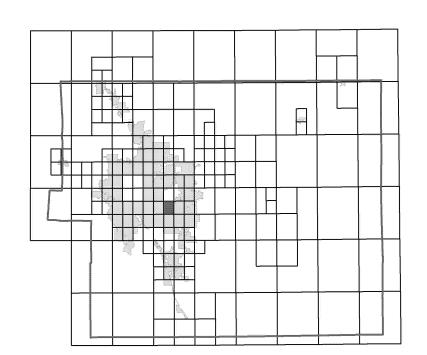
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El Paso County Vertical Datum Offset Table Vertical Datum

REFER TO SECTION 3.3 OF THE EL PASO COUNTY FLOOD INSURANCE STUDY FOR STREAM BY STREAM VERTICAL DATUM CONVERSION INFORMATION

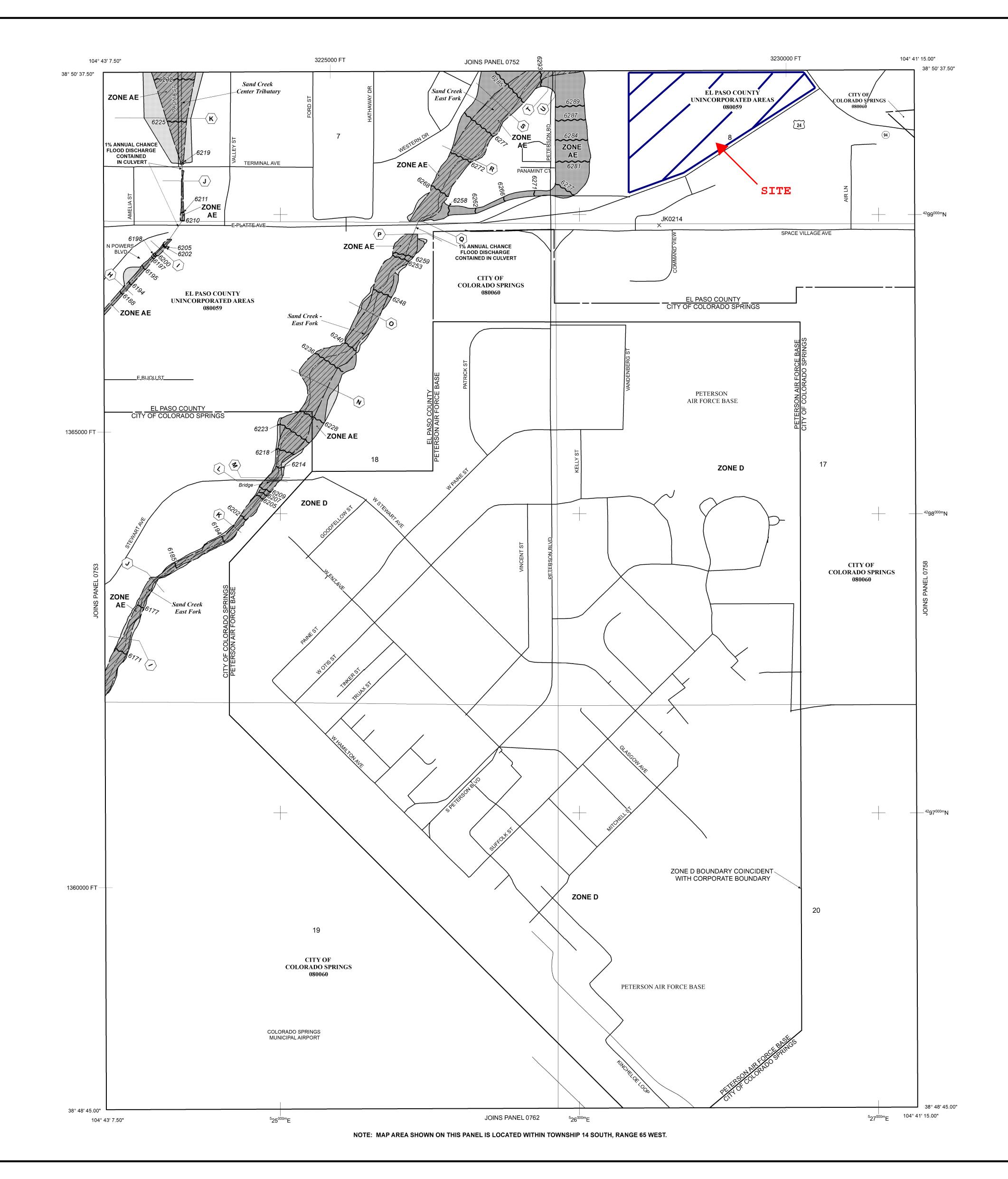
Panel Location Map



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LEGEND

SPECIAL FLOOD HAZARD AREAS (SFHAS) SUBJECT TO INUNDATION BY THE 1% ANNUAL CHANCE FLOOD

The 1% annual chance flood (100-year flood), also known as the base flood, is the flood that has a 1% chance of being equaled or exceeded in any given year. The Special Flood Hazard Area is the area subject to flooding by the 1% annual chance flood. Areas of Special Flood Hazard include Zones A, AE, AH, AO, AR, A99, V, and VE. The Base Flood Elevation is the water-surface elevation of the 1% annual chance flood.

ZONE A No Base Flood Elevations determined. Base Flood Elevations determined.

Flood depths of 1 to 3 feet (usually areas of ponding); Base Flood Elevations determined

Flood depths of 1 to 3 feet (usually sheet flow on sloping terrain); average depths determined. For areas of alluvial fan flooding, velocities also

ZONE AR Special Flood Hazard Area Formerly protected from the 1% annual chance flood by a flood control system that was subsequently decertified. Zone AR indicates that the former flood control system is being restored to provide protection from the 1% annual chance or greater flood.

ZONE A99 Area to be protected from 1% annual chance flood by a Federal flood protection system under construction; no Base Flood Elevations

Coastal flood zone with velocity hazard (wave action); no Base Flood Elevations determined

ZONE VE Coastal flood zone with velocity hazard (wave action); Base Flood

Elevations determined. FLOODWAY AREAS IN ZONE AE

The floodway is the channel of a stream plus any adjacent floodplain areas that must be kept free of encroachment so that the 1% annual chance flood can be carried without substantial increases in flood heights.

OTHER FLOOD AREAS

Areas of 0.2% annual chance flood; areas of 1% annual chance flood with average depths of less than 1 foot or with drainage areas less than 1 square mile; and areas protected by levees from 1% annual chance flood.

OTHER AREAS Areas determined to be outside the 0.2% annual chance floodplain.

Areas in which flood hazards are undetermined, but possible.

COASTAL BARRIER RESOURCES SYSTEM (CBRS) AREAS

CBRS areas and OPAs are normally located within or adjacent to Special Flood Hazard Areas.

OTHERWISE PROTECTED AREAS (OPAs)

Floodway boundary

Zone D Boundary ********** CBRS and OPA boundary

> Boundary dividing Special Flood Hazard Areas of different Base Flood Elevations, flood depths or flood velocities. Base Flood Elevation line and value; elevation in feet* Base Flood Elevation value where uniform within zone; (EL 987)

elevation in feet* * Referenced to the North American Vertical Datum of 1988 (NAVD 88)

Cross section line

6000000 FT

97° 07' 30.00" Geographic coordinates referenced to the North American 32° 22' 30.00" Datum of 1983 (NAD 83)

1000-meter Universal Transverse Mercator grid ticks, 5000-foot grid ticks: Colorado State Plane coordinate

system, central zone (FIPSZONE 0502), DX5510 Bench mark (see explanation in Notes to Users section of

this FIRM panel)

MAP REPOSITORIES Refer to Map Repositories list on Map Index EFFECTIVE DATE OF COUNTYWIDE

FLOOD INSURANCE RATE MAP MARCH 17, 1997 EFFECTIVE DATE(S) OF REVISION(S) TO THIS PANEL DECEMBER 7, 2018 - to update corporate limits, to change Base Flood Elevations and

Special Flood Hazard Areas, to update map format, to add roads and road names, and to

incorporate previously issued Letters of Map Revision.

For community map revision history prior to countywide mapping, refer to the Community Map History Table located in the Flood Insurance Study report for this jurisdiction.

To determine if flood insurance is available in this community, contact your insurance

agent or call the National Flood Insurance Program at 1-800-638-6620.

PANEL 0754G

FIRM FLOOD INSURANCE RATE MAP **EL PASO COUNTY,** COLORADO

PANEL 754 OF 1300

EL PASO COUNTY

(SEE MAP INDEX FOR FIRM PANEL LAYOUT)

AND INCORPORATED AREAS

080059

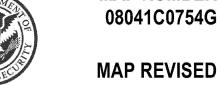
Notice: This map was reissued on 05/15/2020 to make a correction. This version replaces any previous versions. See the

this correction for details.

Notice to User: The Map Number shown below should be

Notice-to-User Letter that accompanied

used when placing map orders: the Community Number shown above should be used on insurance applications for the MAP NUMBER



MAP REVISED DECEMBER 7, 2018

Federal Emergency Management Agency

HYDROLOGIC CALCULATIONS

Crossroads Mixed Use FINAL DRAINAGE REPORT (Historic Area Runoff Coefficient Summary)

			STREE	TS / DEVE	ELOPED	OVERI	LAND / DEVI	ELOPED	WEIG	HTED
BASIN	TOTAL AREA (SF)	TOTAL AREA (Acres)	AREA (Acres)	C ₅	C ₁₀₀	AREA (Acres)	C ₅	C ₁₀₀	C_5	C ₁₀₀
C	256383.3	5.89	0.00	0.90	0.96	5.89	0.08	0.35	0.08	0.35
A	561176.6	12.88	0.00	0.90	0.96	12.88	0.08	0.35	0.08	0.35
В	593693.4	13.63	0.00	0.90	0.96	13.63	0.08	0.35	0.08	0.35
OS-1	55560.16	1.28	1.28	0.90	0.96	0.00	0.08	0.35	0.90	0.96
OS-2	216993.7	4.98	2.49	0.90	0.96	2.49	0.08	0.35	0.49	0.66
EX-A2***		0.59	0.59	0.90	0.96	0.00	0.08	0.35	0.90	0.96
OS-A**		1.29	1.29	0.62	0.72	0.00	0.08	0.35	0.62	0.72
E2*		3.86	3.86	0.80	0.90	0.00	0.08	0.35	0.80	0.90

^{*}FROM FDR FOR CLAREMONT BUSINESS PARK FILING NO. 2

^{**}FROM FDR FOR MEADOWBROOK CROSSING FILING 1 AND FILING 2

^{***}FROM FOR FOR LOT 1 24/94 BUSINESS PARK FILING NO. 1 ON PLATTE AVENUE AND MEADOWBROOK PARKWAY

Crossroads Mixed Use FINAL DRAINAGE REPORT (Historic Area Drainage Summary)

Flows do not match DP 5

Fron	n Area Runoff Coe	efficient Summar	y		OVERL A	1ND		ST	REET / CH	ANNEL FLO	OW .	Time of Trave	$l(T_t)$	INTEN	SITY ^	TOTAL	TOTAL FLOWS	
BASIN	AREA TOTAL	C ₅ C ₁₀₀		C ₅	Length	Height	$T_{\rm C}$	Length	Slope	Velocity	T _t	TOTAL	СНЕСК	I ₅	I ₁₀₀	Q_5	Q_{100}	
	(Acres)	From DCM	A Table 5-1		(ft)	(ft)	(min)	(ft)	(%)	(fps)	(min)	(min)	(min)	(in/hr)	(in/hr)	(c.f.s.)	(c.f.s.)	
С	5.89	0.08	0.35	0.08	300	9	22.2	500	2.0%	1.0	8.4	30.6	14.4	2.5	4.1	1.2	8.5	
A	12.88	0.08	0.35	0.08	300	13	19.7	1350	1.6%	0.9	25.2	44.8	19.2	1.9	3.2	1.9	14.2	
В	13.63	0.08	0.35	0.08	300	11	20.8	750	1.7%	0.9	13.7	34.5	15.8	2.3	3.8	2.5	18.2	
OS-1	1.28	0.90	0.96	0.90	100	3	2.5	490	2.2%	3.0	2.8	5.3	13.3	5.1	8.5	5.8	10.5	
OS-2	4.98	0.49	0.66	0.49	85	8	4.8	1165	1.8%	2.0	9.6	14.5	16.9	3.6	6.0	8. 7	19.6	
EX-A2***	0.59	0.90	0.96	0.90	10	0.2	0.9	916	1.9%	2.7	5.6	6.5	15.1	4.8	8.0	2.5	4.5	
OS-A**	1.29	0.62	0.72	0.62	40	0.8	4.4	1310	1.9%	2.8	7.9	12.3	17.5	3.8	6.4	3.1	6.0	
E2*	3.86	0.80	0.90	0.80	50	1	3.0	400	1.3%	2.3	2.9	6.0	12.5	4.9	8.2	15.1	28.6	

[^] Intensity equations assume a minimum travel time of 5 minutes.

Calculated by: CVW

Date: 2/23/2021

Checked by: DLM

^{*}VALUES DERIVED USING DATA FROM FDR FOR <u>CLAREMONT BUSINESS PARK FILING NO. 2</u>

^{**}VALUES DERIVED USING DATA FROM <u>FDR FOR MEADOWBROOK CROSSING FILING 1 AND FILING 2 PAGE 31</u>

^{***}VALUES DERIVED USING DATA FROM FDR FOR LOT 1 24/94 BUSINESS PARK FILING NO. 1 ON PLATTE AVENUE AND MEADOWBROOK PARKWAY

Crossroads Mixed Use FINAL DRAINAGE REPORT

(Historic Basin Routing Summary)

	From Area Runoff Coefficient Summar	y			OVI	ERLAND		PIPI	E / CHA	NNEL FLO	W	Time of Travel (T _t)	INTEN	SITY *	TOTAL	FLOWS		
DESIGN POINT	CONTRIBUTING BASINS	CA ₅	CA ₁₀₀	C ₅	Length	Height	T_{C}	Length	Slope	Velocity	T _t	TOTAL	I ₅	I ₁₀₀	Q_5	Q_{100}	COMMENTS	
			•		(ft)	(ft)	(min)	(ft)	(%)	(fps)	(min)	(min)	(in/hr)	(in/hr)	(c.f.s.)	(c.f.s.)		
1	E2	3.09	3.47				6.0	916	1.9%	2.7	5.6	11.6	3.9	6.6	14.2	26.5		
	EX-A2	0.53	0.57															
																	EXISTING 10' CDOT TYPE R AT	
		3.62	4.04		Te fe	or E2 Used											GRADE INLET	
2	OS-A	0.80	0.93									12.3	3.8	6.4	3.1	6.0		
																	EXISTING 10' CDOT TYPE R AT	
				Se	e Area Drai	inage Sheet	for Input										GRADE INLET	
3	OS-1	1.15	1.22				11.6	150	1.0%	2.0	1.3	12.8	3.8	6.3	9.8	22.5		
	FB-DP1	1.47	2.35															
		Remo	ve this	s ref	ferend	ce an	d										END OF PAVEMENT	
4							12.8	1470	1.6%	0.9	28.0	40.8	2.0	3.4	7.4	27.7		
	FB-INDP5	include	HOW	by from DP2														
	DP3	2.62	3.57															
		3.65	8.19		Tc fo	r DP3 Used	l										ADJACENT PARCEL (LOT 1)	
5	В	1.09	4.77									34.5	2.3	3.8	8.3	18.2	Flows do not ma	
																1		
				Se	e Area Drai	nage Sheet	for Input										ADJAC Basin B	
6	С	0.47	2.06									30.6	2.5	4.1	1.2	8.5		
				Se	e Area Drai	inage Sheet	for Input										DISCHARGE TO CDOT ROW	
7	OS2	2.44	3.26									14.5	3.6	6.0	10.4	31.9	, I	
	DP6	0.47	2.06														BARROW DITCH	
		2.91	5.32		Tc fo	r OS2 Used	1										SW CORNER OF SITE/CDOT ROW	

Calculated by: CVW

Date: 2/23/2021

Checked by: DLM

Crossroads Mixed Use FINAL DRAINAGE REPORT (Existing Area Runoff Coefficient Summary)

			STREE	TS / DEVE	ELOPED	OVERI	LAND / DEVI	ELOPED	WEIG	HTED
BASIN	TOTAL AREA (SF)	TOTAL AREA (Acres)	AREA (Acres)	C ₅	C ₁₀₀	AREA (Acres)	C ₅	C ₁₀₀	C ₅	C ₁₀₀
C	173960	3.99	0.00	0.90	0.96	5.89	0.08	0.35	0.08	0.35
A	480166.8	11.02	0.00	0.90	0.96	11.02	0.08	0.35	0.08	0.35
В	754121.6	17.31	0.00	0.90	0.96	17.31	0.08	0.35	0.08	0.35
OS-1	55560.16	1.28	1.28	0.90	0.96	0.00	0.08	0.35	0.90	0.96
OS-2	216993.7	4.98	2.49	0.90	0.96	2.49	0.08	0.35	0.49	0.66
EX-A2***		0.59	0.59	0.90	0.96	0.00	0.08	0.35	0.90	0.96
OS-A**		1.29	1.29	0.62	0.72	0.00	0.08	0.35	0.62	0.72
E2*		3.86	3.86	0.80	0.90	0.00	0.08	0.35	0.80	0.90

^{*}FROM FDR FOR CLAREMONT BUSINESS PARK FILING NO. 2

^{**}FROM TO FDR MEADOWBROOK CROSSING FILING 1 AND FILING 2

^{***}FROM FDR LOT 1 24/94 BUSINESS PARK FILING NO. 1 ON PLATTE AVENUE AND MEADOWBROOK PARKWAY

Crossroads Mixed Use FINAL DRAINAGE REPORT

(Existing Area Drainage Summary)

Fron	n Area Runoff Co	efficient Summar	у		OVERL A	IND		ST	REET / CH	ANNEL FLO)W	Time of Trave	$l(T_t)$	INTEN	SITY ^	TOTAL FLOWS	
BASIN	AREA TOTAL	C ₅	C ₁₀₀	C ₅	Length	Height	$T_{\rm C}$	Length	Slope	Velocity	T _t	TOTAL	СНЕСК	I ₅	I ₁₀₀	Q_5	Q_{100}
	(Acres)	From DCM	1 Table 5-1		(ft)	(ft)	(min)	(ft)	(%)	(fps)	(min)	(min)	(min)	(in/hr)	(in/hr)	(c.f.s.)	(c.f.s.)
С	3.99	0.08	0.35	0.08	120	2.8	15.3	555	1.5%	0.9	10.6	25.9	13.8	2.7	4.5	0.9	6.3
A	11.02	0.08	0.35	0.08	165	8	13.8	1730	1.3%	0.8	36.3	50.1	20.5	1.7	2.9	1.5	11.1
В	17.31	0.08	0.35	0.08	300	3	30.9	1390	1.2%	0.8	29.7	60.6	19.4	1.4	2.4	2.0	14.5
OS-1	1.28	0.90	0.96	0.90	100	3	2.5	490	2.2%	3.0	2.8	5.3	13.3	5.1	8.5	5.8	10.5
OS-2	4.98	0.49	0.66	0.49	85	8	4.8	1165	1.8%	2.0	9.6	14.5	16.9	3.6	6.0	8.7	19.6
EX-A2***	0.59	0.90	0.96	0.90	10	0.2	0.9	916	1.9%	2.7	5.6	6.5	15.1	4.8	8.0	2.5	4.5
OS-A**	1.29	0.62	0.72	0.62	40	0.8	4.4	1310	1.9%	2.8	7.9	12.3	17.5	3.8	6.4	3.1	6.0
E2*	3.86	0.80	0.90	0.80	50	1	3.0	400	1.3%	2.3	2.9	6.0	12.5	4.9	8.2	15.1	28.6

 $^{^{\}wedge}$ Intensity equations assume a minimum travel time of 5 minutes.

Calculated by: CVW

Date: 2/23/2021

Checked by: DLM

^{*}VALUES DERIVED USING DATA FROM FDR FOR <u>CLAREMONT BUSINESS PARK FILING NO. 2</u>

^{**}VALUES DERIVED USING DATA FROM <u>FDR FOR MEADOWBROOK CROSSING FILING 1 AND FILING 2 PAGE 31</u>

^{***}VALUES DERIVED USING DATA FROM FDR FOR LOT 1 24/94 BUSINESS PARK FILING NO. 1 ON PLATTE AVENUE AND MEADOWBROOK PARKWAY

Crossroads Mixed Use FINAL DRAINAGE REPORT (Existing Basin Routing Summary)

	From Area Runoff Coefficient Summary	,			OVE	ERLAND		PIPI	C / CHA	NNEL FLO)W	Time of Travel (T_t)	INTEN	SITY *	TOTAL	FLOWS	
DESIGN POINT	CONTRIBUTING BASINS	CA ₅	CA ₁₀₀	C ₅	Length	Height	T_{C}	Length	Slope	Velocity	T_t	TOTAL	I_5	I ₁₀₀	Q_5	Q_{100}	COMMENTS
					(ft)	(ft)	(min)	(ft)	(%)	(fps)	(min)	(min)	(in/hr)	(in/hr)	(c.f.s.)	(c.f.s.)	
1	E2	3.09	3.47				6.0	916	1.9%	2.7	5.6	11.6	3.9	6.6	14.2	26.5	
	EX-A2	0.53	0.57									1					
																	EXISTING 10' CDOT TYPE R AT
		3.62	4.04		Te fo	or E2 Used											GRADE INLET
2	OS-A	0.80	0.93									12.3	3.8	6.4	3.1	6.0	
																	EXISTING 10' CDOT TYPE R AT
				Se	e Area Drai	nage Sheet t	or Input										GRADE INLET
3	OS-1	1.15	1.22				11.6	150	1.0%	2.0	1.3	12.8	3.8	6.3	9.8	22.5	
	FB-DP1	1.47	2.35									1					
		2.62	3.57		Tc for	r DP1 Used											END OF PAVEMENT
4	A	0.88	3.86				12.8	1470	1.6%	0.9	28.0	40.8	2.0	3.4	7.1	25.5	
	FB-DP2	0.00	0.10														
	DP3	2.62	3.57														
		3.50	7.54		Tc for	r DP3 Used											ADJACENT PARCEL (LOT 1)
5	В	1.38	6.06									60.6	1.4	2.4	5.0	14.5	
				Se	e Area Drai	nage Sheet t	or Input										ADJACENT PARCEL (LOT 2)
6	C	0.32	1.40									25.9	2.7	4.5	0.9	6.3	
				See Area Drainage Sheet for Input											DISCHARGE TO CDOT ROW		
7	OS2	2.44	3.26									14.5	3.6	6.0	9.9	28.0	
	DP6	0.32	1.40														BARROW DITCH
		2.76	4.66		Tc fo	r OS2 Used											SW CORNER OF SITE/CDOT ROW

Calculated by: CVW
Date: 2/23/21

Checked by: DLM

CROSSROADS MIXED USE FILING NO. 1 FINAL DRAINAGE CALCULATIONS

(Area Runoff Coefficient Summary)

			STREE	TS / COM	MERC.	MULTI-FAMILY/PARKLAND			OVERLAN	OVERLAND / UNDEVELOPED			WEIGHTED	
	TOTAL	TOTAL												
BASIN	AREA	AREA	AREA	C_5	C_{100}	AREA	C_5	C_{100}	AREA	C_5	C_{100}	C_5	C_{100}	
	(Sq Ft)	(Acres)	(Acres)			(Acres)			(Acres)					
					PROPOS	ED BASINS								
<i>OS-A</i> **		1.29	1.29	0.62	0.72	0.00	0.49	0.62	0.00	0.08	0.35	0.62	0.72	
E2*		3.86	3.86	0.80	0.90	0.00	0.49	0.62	0.00	0.08	0.35	0.80	0.90	
EX-A2***		0.59	0.59	0.90	0.96	0.00	0.49	0.62	0.00	0.08	0.35	0.90	0.96	
OS-1	60793.3017	1.40	1.40	0.90	0.96	0.00	0.49	0.62	0.00	0.08	0.35	0.90	0.96	
OS-2	216993.7096	4.98	2.49	0.90	0.96	0.00	0.49	0.62	2.49	0.08	0.35	0.49	0.66	
A	72787.0873	1.67	1.67	0.90	0.96	0.00	0.49	0.62	0.00	0.08	0.35	0.90	0.96	
В	64490.3787	1.48	1.48	0.90	0.96	0.00	0.49	0.62	0.00	0.08	0.35	0.90	0.96	
С	200631.5748	4.61	4.46	0.81	0.88	0.00	0.49	0.62	0.15	0.08	0.35	0.79	0.86	
D	96773.7602	2.22	2.22	0.81	0.88	0.00	0.49	0.62	Decem	14 man a 4 a la		0.81	0.88	
E	118133.5827	2.71	Does	sn't mate	ch plan	2.23	0.81	0.88	Doesn	't match	pian , 	0.83	0.89	
F	112036.6061	2.57	4.31	U.01	0.00	0.00	0.49	0.62	0.00	0.08	0.35	0.81	0.88	
G	20057.4496	0.46	0.46	0.90	0.96	0.00	0.49	0.62	0.00	0.08	0.35	0.90	0.96	
J	139924.2472	3.21	0.00	0.90	0.96	3.21	0.16	0.41	0.00	0.08	0.35	0.16	0.41	
<i>A</i> -6****	138956.4	3.19	0.00	0.90	0.96	3.19	0.60	0.73	0.00	0.08	0.35	0.60	0.73	
2 -1***	16117.2	0.37	0.00	0.90	0.96	0.37	0.33	0.52	0.00	0.08	0.35	0.33	0.52	
B -3***	33976.8	0.78	0.00	0.90	0.96	0.78	0.62	0.75	0.00	0.08	0.35	0.62	0.75	
Z -2****	24393.6	0.56	0.00	0.90	0.96	0.56	0.60	0.73	0.00	0.08	0.35	0.28	0.49	
G1	25962.0179	0.60	0.60	0.90	0.96	0.00	0.16	0.41	0.00	0.08	935	0.90	0.96	

^{*}FROM FDR FOR CLAREMONT BUSINESS PARK FILING NO. 2

sin not found in Aura

Basin not found in Aura at Crossroads FDR

Info for basin does not match with Aura at Crossroads FDR

Calculated by: CVW

Date: 11/22/2021

^{**}FROM FDR FOR MEADOWBROOK CROSSING FILING 1 AND FILING 2

^{***}FROM FOR FOR LOT 1 24/94 BUSINESS PARK FILING NO. 1 ON PLATTE AVENUE AND MEADOWBROOK PARKWAY

^{****}FROM FDR FOR AURA AT CROSSROADS, DATED MAY 17, 2021

ind in sroads

CROSSROADS MIXED USE FILING NO. 1 FINAL DRAINAGE REPORT

(Area Drainage Summary)

From Area Run	off Coefficient S	'ummary			OVER	LAND		STRE	ET / CH	ANNEL F	LOW	Time of T	ravel (T _t)	INTEN	SITY#	TOTAL FLOWS	
BASIN	AREA TOTAL	C ₅	C ₁₀₀	C ₅	Length	Height	T_{C}	Length	Slope	Velocity	T_t	TOTAL	CHECK	I ₅	I ₁₀₀	Q ₅	Q ₁₀₀
	(Acres)	From DCM	1 Table 5-1		(ft)	(ft)	(min)	(ft)	(%)	(fps)	(min)	(min)	(min)	(in/hr)	(in/hr)	(c.f.s.)	(c.f.s.)
	Proposed Area Drainage Summary																
OS-A**	1.29	0.62	0.72	0.62	40	0.8	4.4	1310	1.9%	2.8	7.9	12.3	17.5	3.8	6.4	3.1	6.0
E2*	3.86	0.80	0.90	0.80	50	1	3.0	400	1.3%	2.3	2.9	6.0	12.5	4.9	8.2	15.1	28.6
EX-A2***	0.59	0.90	0.96	0.90	10	0.2	0.9	916	1.9%	2.7	5.6	6.5	15.1	4.8	8.0	2.5	4.5
OS-1	1.40	0.90	0.96	0.90	100	3	2.5	490	2.2%	3.0	2.7	5.2	13.3	5.1	8.6	6.4	11.5
OS-2	4.98	0.49	0.66	0.49	85	8	4.8	1165	1.8%	2.0	9.6	14.5	16.9	3.6	6.0	8.7	19.6
A	1.67	0.90	0.96	0.90	30	0.6	1.6	1325	0.7%	1.7	7.3	8.9	17.5	4.3	7.2	6.5	11.6
В	1.48	0.90	0.96	0.90	25	0.5	1.4	1335	0.7%	1.7	7.3	8.8	17.6	4.3	7.3	5.8	10.3
С	4.61	0.79	0.86	0.79	50	1	3.2	260	1.5%	2.4	1.4	5.0	11.7	5.2	8.7	18.7	34.5
D	2.22	0.81	0.88	0.81	50	1	2.9	200	1.5%	2.4	1.1	5.0	11.4	5.2	8.7	9.3	17.0
E	2.71	0.83	0.89	0.83	60	1.2	3.0	700	1.0%	2.0	3.8	6.9	14.2	4.7	7.9	10.5	19.1
F	2.57	0.81	0.88	0.81	50	0.8	3.2	300	1.3%	2.3	1.6	5.0	11.9	5.2	8.7	10.8	19.6
G	0.46	0.90	0.96	0.90	50	1	2.0	466	1.1%	2.1	2.6	5.0	12.9	5.2	8.7	2.1	3.8
J	3.21	0.16	0.41	0.16	50	2	7.6	0	0.0%	0.0	0.0	7.6	10.3	4.5	7.6	2.3	10.0
A-6****	3.19	0.60	0.73	0.60			REF	ER TO "FE	OR FOR AU	JRA AT CR	OSSROAI	DS" FOR D	ETAILS			6.77	13.85
Z-1****	0.37	0.33	0.52	0.33		REFER TO "FDR FOR AURA AT CROSSROADS" FOR DETAILS						0.47	1.27				
B-3****	0.78	0.62	0.75	0.62	REFER TO "FDR FOR AURA AT CROSSROADS" FOR DETAILS						2.08	4.20					
Z-2****	0.56	0.28	0.49	0.28	REFER TO "FDR FOR AURA AT CROSSROADS" FOR DETAILS						0.63	1.84					
<i>G1</i>	0.60	0.90	0.96	0.90	50	1	2.0	466	1.1%	2.1	2.6	5.0	12.9	5.2	8.7	2.8	5.0

[#] Intensity equations assume a minimum travel time of 5 minutes.

Calculated by: CVW

Date: 11/22/2021

Checked by: DLM

Does not match with Aura at Crossroads FDR

^{*}VALUES DERIVED USING DATA FROMFDR FOR CLAREMONT BUSINESS PARK FILING NO. 2

^{**}VALUES DERIVED USING DATA FROMFDR MEADOWBROOK CROSSING FILING 1 AND FILING 2 PAGE 31

^{***}VALUES DERIVED USING DATA FROMFDR LOT 1 24/94 BUSINESS PARK FILING NO. 1 ON PLATTE AVENUE AND MEADOWBROOK PARKWAY

^{****}FROM FDR FOR AURA AT CROSSROADS, DATED MAY 17, 2021

CROSSROADS MIXED USE FILING NO. 1 FINAL DRAINAGE REPORT (Basin Routing Summary)

				_								, , , , , , , , , , , , , , , , , , ,	_				
	From Area Runoff Coefficient Summary				OVER	RLAND		PIPE		NNEL FLO)W	Time of Travel (T_t)	INTEN	VSITY *	TOTAL	FLOWS	
DESIGN POINT	CONTRIBUTING BASINS	CA ₅	CA ₁₀₀	C ₅	Length	Height	T_{C}	Length	Slope	Velocity	T_t	TOTAL	I_5	I ₁₀₀	Q ₅	Q ₁₀₀	COMMENTS
					(ft)	(ft)	(min)	(ft)	(%)	(fps)	(min)	(min)	(in/hr)	(in/hr)	(c.f.s.)	(c.f.s.)	
			P	ROPO	SED D	RAINA	GE BA	SIN RO	UTING	G SUMM	ARY						
1	E2, EX-A2	3.62	4.04		To for	E2 Used	6.0	916	1.9%	2.7	5.6	11.6	3.9	6.6	14.2	26.5	Existing 10' CDOT Type R At-Grade Inlet (Public)
2	OS-A	0.80	0.93	See	Area Draina		or Input					12.3	3.8	6.4	3.1	6.0	Existing 10' CDOT Type R At-Grade Inlet (Public)
3	OS-1, FB-DP1	2.73	3.69			OP1 Used	11.6	150	1.0%	2.0	1.3	12.8	3.8	6.3	10.2	23.3	Proposed 10' CDOT Type R At-Grade Inlet (Public)
4	A, FB-DP2, FB-IN4	1.50	1.71			nsin A used						8.9	4.3	7.2	6.5	12.4	Proposed 15' CDOT Type R At-Grade Inlet Proposed NEENAH R-6116 MH Lid and Frame (Public)
5	B, FB-DP3, FB-IN4.5	2.28	3.56			sin B Used						8.8	4.3	7.3	9.8	25.8	Proposed 15' CDOT Type R Sump Inlet (Public)
6	С	3.62	3.98	See	Area Draina	ige Sheet fo	or Input					5.0	5.2	8.7	18.7	34.5	Proposed 30" RCP or PP Storm Sewer (Private)
7	D	1.80	1.96	See	Area Draina	ige Sheet fo	or Input					5.0	5.2	8.7	9.3	17.0	Proposed 24" RCP or PP Storm Sewer (Private)
8	1/2 E	1.12	1.21	See	Area Draina	ige Sheet fo	or Input					6.9	4.7	7.9	5.2	9.5	Proposed 10' CDOT Type R At-Grate Inlet (Private)
9	1/2 E	1.12	1.21	See	Area Draina	ige Sheet fo	or Input					6.9	4.7	7.9	5.2	9.5	Proposed 10' CDOT Type R At-Grade Inlet (Private)
10	Basin G	0.41	0.44			sin G Used						5.0	5.2	8.7	2.1	3.8	Proposed 10' CDOT Type R Sump Inlet (Private)
11	Basin G1 FB-DP8/9	0.51 0.19 0.71	1.32 0.67 1.99		Tc for Bas	sin G1 Used	1					5.0	5.2	8.7	3.6	17.3	Proposed 15' CDOT Type R Sump Inlet (Private)
12	F	2.08	2.26	See	Area Draina	ige Sheet fo	or Input					5.0	5.2	8.7	10.8	19.6	Proposed 24" RCP or PP Storm Sewer (Private)
13	Basin A-6 Basin B-3	0.05 0.48 0.53	0.78 0.42 1.20		Weighte	d Tc Used						12.8	3.8	6.3	2.0	7.5	Proposed 2' Bottom Earthen Swale, Rip Rap Rundown
14	Basin Z-2 DP 13	0.16 0.53 0.69	0.27 1.20 1.47		Tc for Bas	sin Z-2 Use	d					11.1	4.0	6.7	2.7	9.8	Proposed Earthen Swale (Private)
15	J, DP14, PR17, PR 18	20.61	^{26.69}	per	drai	nage	e pla	n				6.3	4.8	8.1	99.6	216.6	Full Spectrum Extended Detention Basin (Private)
16	POND OUTFALL OS-2		5.16		Tc for Basi							14.5	3.6	6.0	9.9	31.0	HISTORIC FLOW IN CDOT BARROW DITCH Q5= 10.4 CFS, Q100 = 31.9 CFS PER HISTORIC DRAINAGE ANALYSIS

^{*} Intensity equations assume a minimum travel time of 5 minutes.

Basin E should be 2 separate basins.

Missing Basin Z-1 in routing

| CVW |
| Date: | 11/22/2021 |
| Checked by: | DLM |

CROSSROADS MIXED USE FILING NO. 1 FINAL DRAINAGE CALCULATIONS

(Storm Sewer Routing Summary)

					Inter	ısity*	Fl	ow	PIPE SIZE
PIPE RUN	Contributing Pipes/Design Points	Equivalent CA 5	Equivalent CA 100	Maximum T _C	I_5	I 100	Q 5	Q 100	
1	INLET 3	1.78	1.55	12.8	3.8	6.3	6.7	9.8	24" SD
1.5	INLET 4	1.51	1.48	8.9	4.3	7.2	6.5	10.7	24" SD
2	PR1.5, INLET 4.5	1.51	1.74	8.9	4.3	7.2	6.5	12.6	24" SD
3	PROUNDET S	3.78	5.30	8.8	4.3	7.3	16.4	38.5	36" SD
4	DP6	3.62	3.98	5.0	5.2	8.7	18.7	34.5	30" SD
5	PR4	3.62	3.98	5.0	5.2	8.7	18.7	34.5	30" SD
6	PR5	3.62	3.98	5.0	5.2	8.7	18.7	34.5	30" SD
7	PR6	3.62	3.98	5.0	5.2	8.7	18.7	34.5	36" SD
8	DP7	1.80	1.96	5.0	5.2	8.7	9.3	17.0	24" SD
9	PR8, DP8	2.82	2.83	6.9	4.7	7.9	13.2	22.3	30" SD
10	DP9	1.02	0.88	6.9	4.7	7.9	4.8	6.9	18" SD
11	PR7, PR9, PR10	7.47	7.68	6.9	4.7	7.9	35.0	60.5	36" SD
12	PR11	7.47	7.68	6.9	4.7	7.9	35.0	60.5	42" SD
13	DP10	0.41	0.44	5.0	5.2	8.7	2.1	3.8	18" SD
14	DP11	0.51	1.99	5.0	5.2	8.7	2.7	17.3	30" SD
15	PR12, PR13, PR14	8.40	10.11	6.9	4.7	7.9	39.4	79.6	42" SD
16	DP12	2.08	2.26	5.0	5.2	8.7	10.8	19.6	24" SD
17	PR15, PR16	10.48	12.38	6.9	4.7	7.9	49.1	97.4	48" SD
18	PR17	10.48	12.38	6.9	4.7	7.9	49.1	97.4	48" SD
19*	SEE FOR FOR AURA AT CROSSROADS	8.92	11.52	15.2	3.5	5.9	31.2	67.7	48" SD
20	POND OUTFALL	PER	MHFD	WKSHT			1.2	11.4	18" SD
21*	SEE FDR FOR AURA AT CROSSROADS	0.48	0.58	8.8	4.3	7.3	2.1	4.2	30" SD
	O FOR FOR AURA AN CROSSROADS FOR			ETAILS	Ca	lculated by:			
DP -	Design Point		om Design Point	D. i	,		11/22/2021	-	=
EX -	Existing Design Point	IN 1 - Intercepted	Flow from Desig	n Point	(hecked by:	DLM	-\	_

Include flow from PR21

Use inlet labels where appropriate for easier reference to StormCAD model & Drainage plan

Doesn't match flow for DP 11

Weig	Weighted Percent Imperviousness of FSD POND 1									
Contributing Basins	Area (Acres)	C 5	Impervious % (I)	(Acres)*(I)						
A	1.67	0.90	100	167.10						
В	1.48	0.90	100	148.05						
С	4.61	0.79	93	428.35						
D	2.22	0.81	95	211.05						
E	2.71	0.83	96	260.35						
F	2.57	0.81	95	244.34						
G	0.46	0.90	100	46.05						
Residential Lot	12.67	N/A	76	962.92						
G1	0.60	0.90	75	44.70						
J	3.21	0.16	7	22.49						
Totals	32.20			2535.39						
Imperviousness of WQ Pond 1	78.7	%								

HYDRAULIC CALCULATIONS

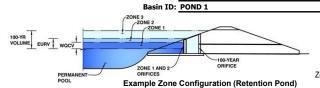
DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.03 (May 2020)

Project: Basin ID:	CROSSROAI	DS MIXED L	ISE		D-Detendon, Versio	WI 4.03 (14e	19 2020)							
ZONE 3														-
100-YR VOLUME EURY WQCV	ONE 1	1												
VOLUME EURV WaCV		Lan Maria		\geq	ı		1							
PERMANENT ORIFIC	1 AND 2	ORIFIC	E		Depth Increment =	2.00	ft Optional				Optional			
POOL Example Zone		on (Retenti	on Pond)		Stage - Storage Description	Stage (ft)	Override Stage (ft)	Length (ft)	Width (ft)	Area (ft²)	Override Area (ft ²)	Area (acre)	Volume (ft ³)	Volume (ac-ft)
Watershed Information			00.0	A 8	Top of Micropool		0.00				125	0.003	(,,,	(uc it)
Selected BMP Type =	EDB /		32.2	Ac	88		0.40				240	0.006	73	0.002
Watershed Area =	32.10	acres			90		2.40				16,471	0.378	16,784	0.385
Watershed Length = Watershed Length to Centroid =	1,725 1,000	ft			92		4.40 6.40		-		39,263 47,710	0.901 1.095	72,518 159,490	1.665 3.661
Watershed Slope =	0.006	ft/ft	Fro	m rei	oort, soil		8.40				60,034	1.378	267,234	6.135
Watershed Imperviousness =	78.67%	percent												
Percentage Hydrologic Soil Group A = Percentage Hydrologic Soil Group B =	100.0%	percent percent	IS T	ype <i>P</i>	and B.									
Percentage Hydrologic Soil Groups C/D =	0.0%	percent												
Target WQCV Drain Time =	40.0	hours												
Location for 1-hr Rainfall Depths =														
After providing required inputs above inc depths, click 'Run CUHP' to generate rund														
the embedded Colorado Urban Hydro			Optional Use	r Overrides										
Water Quality Capture Volume (WQCV) =	0.857	acre-feet		acre-feet										
Excess Urban Runoff Volume (EURV) = 2-yr Runoff Volume (P1 = 1.19 in.) =	3.306 2.394	acre-feet acre-feet	1.19	acre-feet inches										
5-yr Runoff Volume (P1 = 1.5 in.) =	3.107	acre-feet	1.50	inches										
10-yr Runoff Volume (P1 = 1.75 in.) =	3.679	acre-feet	1.75	inches										
25-yr Runoff Volume (P1 = 2 in.) =	4.353	acre-feet	2.00	inches										
50-yr Runoff Volume (P1 = 2.25 in.) = 100-yr Runoff Volume (P1 = 2.52 in.) =	5.011 5.779	acre-feet acre-feet	2.25	inches										
500-yr Runoff Volume (P1 = 3.14 in.) =	7.477	acre-feet		inches										
Approximate 2-yr Detention Volume =	2.169	acre-feet												
Approximate 5-yr Detention Volume = Approximate 10-yr Detention Volume =	2.821 3.370	acre-feet acre-feet												
Approximate 10-yr Deterition Volume =	4.007	acre-feet												
Approximate 50-yr Detention Volume =	4.381	acre-feet												
Approximate 100-yr Detention Volume =	4.729	acre-feet												
Define Zones and Basin Geometry														
Zone 1 Volume (WQCV) =	0.857	acre-feet												
Zone 2 Volume (EURV - Zone 1) =	2.449	acre-feet												
Zone 3 Volume (100-year - Zones 1 & 2) = Total Detention Basin Volume =	1.424 4.729	acre-feet acre-feet												
Initial Surcharge Volume (ISV) =	user	ft 3												
Initial Surcharge Depth (ISD) =	user	ft												
Total Available Detention Depth $(H_{total}) =$	user	ft												
Depth of Trickle Channel (H_{TC}) = Slope of Trickle Channel (S_{TC}) =	user	ft ft/ft												
Slopes of Main Basin Sides (S _{main}) =	user	H:V						-	-					
Basin Length-to-Width Ratio ($R_{L/W}$) =	user													
Initial Curchage Area (A) -		٦٠												
Initial Surcharge Area (A_{ISV}) = Surcharge Volume Length (L_{ISV}) =	user	ft ²												
Surcharge Volume Width (W _{ISV}) =	user	ft												
Depth of Basin Floor (H _{FLOOR}) =	user	ft												
Length of Basin Floor (L_{FLOOR}) = Width of Basin Floor (W_{FLOOR}) =	user	ft fr												
Area of Basin Floor (A_{FLOOR}) =	user	ft ²												
Volume of Basin Floor $(V_{FLOOR}) =$	user	ft ³												
Depth of Main Basin (H_{MAIN}) = Length of Main Basin (L_{MAIN}) =	user	ft fr												
Width of Main Basin (W _{MAIN}) =	user	ft.												
Area of Main Basin (A _{MAIN}) =	user	ft ²												
Volume of Main Basin (V _{MAIN}) =	user	ft ³												
Calculated Total Basin Volume (V_{total}) =	user	acre-feet												
										1 1				
														7
									=					
						-			=					

Pond Sizing - FINAL, Basin 10/11/2021, 4:02 PM

DETENTION BASIN OUTLET STRUCTURE DESIGN



	Estimated Stage (ft)	Estimated Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	3.35	0.857	Orifice Plate
Zone 2 (EURV)	6.08	2.449	Orifice Plate
Zone 3 (100-year)	7.33	1.424	Weir&Pipe (Restrict)
•	Total (all zones)	4,729	

<u>User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)</u>

Underdrain Orifice Invert Depth = ft (distance below the filtration media surface) N/A Underdrain Orifice Diameter = N/A inches

Project: CROSSROADS MIXED USE

	Calculated Parameters for Underdr					
Underdrain Orifice Area =	N/A	ft²				
Underdrain Orifice Centroid =	N/A	feet				

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP) Invert of Lowest Orifice = ft (relative to basin bottom at Stage = 0 ft) 0.00

Depth at top of Zone using Orifice Plate = 6.08 ft (relative to basin bottom at Stage = 0 ft) Orifice Plate: Orifice Vertical Spacing = N/A inches Orifice Plate: Orifice Area per Row = N/A linches

BMP)	Calculated Parame	ters for Plate
NQ Orifice Area per Row =	N/A	ft ²
Elliptical Half-Width =	N/A	feet
Elliptical Slot Centroid =	N/A	feet
Elliptical Slot Area =	N/A	ft ²

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	and rotal rated of Edit of the Andribered from torrest to highest									
	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)		
Stage of Orifice Centroid (ft)	0.00	2.03	4.05							
Orifice Area (sq. inches)	3.77	6.25	12.60							

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

	Not Selected	Not Selected
Invert of Vertical Orifice =	N/A	N/A
Depth at top of Zone using Vertical Orifice =	N/A	N/A
Vertical Orifice Diameter =	N/A	N/A

ft (relative to basin bottom at Stage = 0 ft) ft (relative to basin bottom at Stage = 0 ft) inches

Vertical Orifice Area Vertical Orifice Centroid

	Calculated Parame	ters for Vertical Or	ifice
	Not Selected	Not Selected	
=	N/A	N/A	ft ²
=	N/A	N/A	feet

User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe

Input. Overnow wen (Droppox with hat o	i Siopeu Grate ariu	Outlet Fipe OK Ket	<u>ctarigular/ rrapezoluar vveli (ariu ivo Out</u>	et ripe)
	Zone 3 Weir	Not Selected		
Overflow Weir Front Edge Height, Ho =	6.09	N/A	ft (relative to basin bottom at Stage = 0 ft)	Height of Grate Upper Edge, H_t =
Overflow Weir Front Edge Length =	5.70	N/A	feet	Overflow Weir Slope Length =
Overflow Weir Grate Slope =	0.00	N/A	H:V Gra	te Open Area / 100-yr Orifice Area =
Horiz. Length of Weir Sides =	2.91	N/A	feet Ove	rflow Grate Open Area w/o Debris =
Overflow Grate Open Area % =	70%	N/A	%, grate open area/total area Ov	erflow Grate Open Area w/ Debris =
Debris Clogging % =	50%	N/A	%	

	Calculated Paramet	ters for Overflow V	Veir
	Zone 3 Weir	Not Selected	
t =	6.09	N/A	feet
1 =	2.91	N/A	feet
1 =	13.14	N/A	
5 =	11.61	N/A	ft ²
; =	5.81	N/A	ft ²
			•

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

	Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	0.33	N/A	f
Outlet Pipe Diameter =	18.00	N/A	i
Restrictor Plate Height Above Pipe Invert =	9.00		i

ft (distance below basin bottom at Stage = 0 ft) inches inches

Outlet Orifice Area = Outlet Orifice Centroid = Half-Central Angle of Restrictor Plate on Pipe =

	Zone 3 Restrictor	Not Selected	
=	0.88	N/A	ft ²
=	0.43	N/A	feet
=	1.57	N/A	radians
_	1.5/	IN/A	laulaii

100 Year

5.779

13.5

0.42

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate

50 Year

5.011

8.1

0.25

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage=	7.30	ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length =	33.00	feet
Spillway End Slopes =	3.00	H:V
Freeboard above Max Water Surface =	1.00	feet

Calculated Parameters for Spillway

Spillway Design Flow Depth=	0.85	feet
Stage at Top of Freeboard =	9.15	feet
Basin Area at Top of Freeboard =	1.38	acres
Basin Volume at Top of Freeboard =	6.13	acre-ft
		•

25 Year

2.00

4.353

4.0

0.13

Design Storm Return Period One-Hour Rainfall Depth (in) CLIUD Dunoff Valuma (a. OPTIONA Pred

Routed Hydrograph Results

COTIF RUITOTI VOIUTTE (acte-it) -
Inflow Hydrograph Volume (acre-ft) =
CUHP Predevelopment Peak Q (cfs) =
IAL Override Predevelopment Peak Q (cfs) =
edevelopment Unit Peak Flow, q (cfs/acre) =
Peak Inflow Q (cfs) =
Peak Outflow Q (cfs) =
Ratio Peak Outflow to Predevelopment Q =
Structure Controlling Flow =
Max Velocity through Grate 1 (fps) =
Max Velocity through Grate 2 (fps) =
ne to Drain 97% of Inflow Volume (hours) =
ne to Drain 99% of Inflow Volume (hours) =
Maximum Ponding Depth (ft) =
Area at Maximum Ponding Depth (acres) =

Maximum Volume Stored (acre-ft) =

i =	WQCV	EURV	2 Year	5 Year	Ī
) =[N/A	N/A	1.19	1.50	_
) =	0.857	3.306	2.394	3.107	_
) =	N/A	N/A	2.394	3.107	
) =	N/A	N/A	0.2	0.3	
) =	N/A	N/A			
) =	N/A	N/A	0.00	0.01	Ξ
) =	N/A	N/A	33.0	42.4	
) =	0.5	1.3	1.1	1.2	
) =	N/A	N/A	N/A	3.9	
<i>i</i> =	Plate	Plate	Plate /	Plate	
) =	N/A	N/A	N/A	N/A	
) =	N/A	N/A	N/A /	N/A	
) =	38	67	61 /	66	
) =	40	72	65	72	
۱ ـ ا	3 32	6.08	5 01	5.60	_

70.9 107.3 49.3 82.7 61.1 Overflow Weir 1 Overflow Weir 1 Outlet Plate Outlet Plate Spillway 0.1 0.6 0.8 0.9 N/A N/A N/A N/A N/A 76 75 74 75 6.18 7.24 7.71 1.28 5.218 1.10 3.694 Unresolved from Review #1: These need to be <1.0

10 Year

3.679

3.679 0.4

0.01

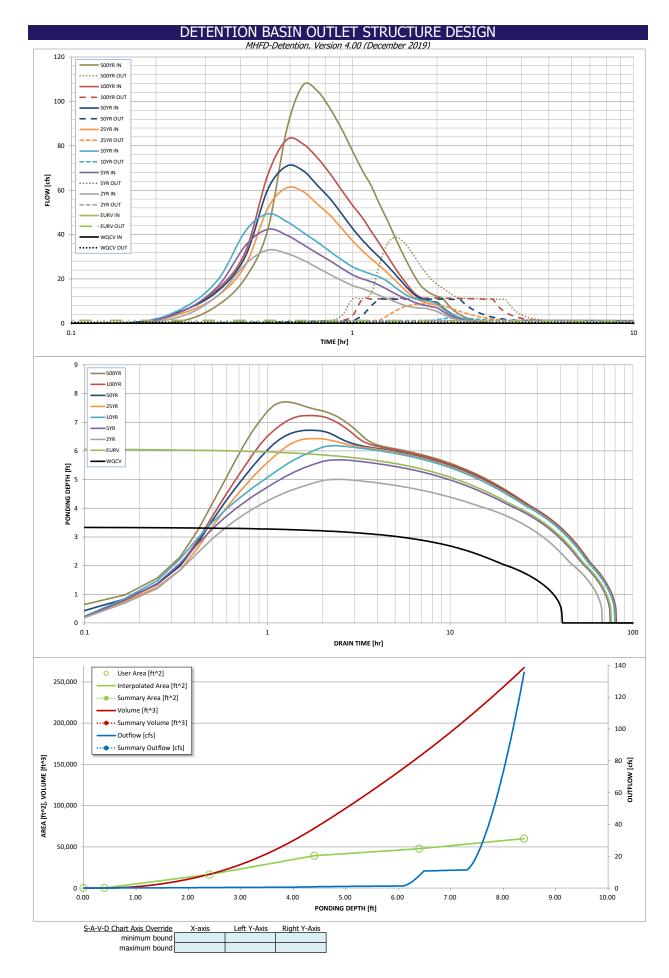
unless it is shown in report text about that there is a suitable outfall downstream with capacity to handle the additional flows.

500 Year

3.14 7.477

24.8

0.77



Pond Sizing - FINAL, Outlet Structure 10/11/2021, 4:50 PM

CROSSROADS MIXED USE FILING NO. 1

EMERGENCY SPILLWAY CALCULATIONS PRIVATE FSD POND (POND 1)

Horizontal Broad-Crested Weir (Eqn 12-20 UDFCD)						CD)
	Variable				Solve For	
С	3.00			L (ft)	H (ft)	Q (cfs)
L	33.00	ft		0.0	0.0	79.0
Н	0.86	ft	· ·		-	
Q		cfs				

	Sloping	g Broad-Cre	sted Weir	· (Eqn 12-2	1 UDFCD,)
	Variabl	e				
С	3.00			Z (ft)	H (ft)	Q (cfs)
Z	3.00	ft		0.0	0.0	2.5
Н	0.86	ft	1			-
Q		cfs				

Equation 12-20

 $Q = C_{BCW} L H^{1.5}$

Equation 12-21

$$Q = \left(\frac{2}{5}\right) C_{BCW} Z H^{2.5}$$

Where:

Q = discharge (cfs)

 C_{BCW} = broad-crested weir coefficient (This ranges from 2.6 to 3.0. A value of 3.0 is often used in practice.) See Hydraulic Engineering Circular No. 22 for additional information.

L =broad-crested weir length (ft)

H = head above weir crest (ft)

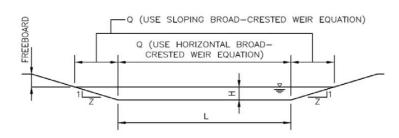


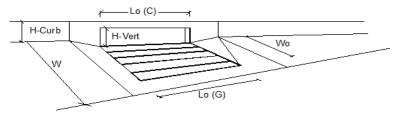
Figure 12-20. Sloping broad-crest weir



ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) Project: **Crossroads Mixed Use Existing Inlets** Inlet ID: INLET 1 CRONN Gutter Geometry (Enter data in the blue cells) T_{BACK} Maximum Allowable Width for Spread Behind Curb 14.0 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) S_{BACK} : 0.020 ft/ft Manning's Roughness Behind Curb (typically between 0.012 and 0.020) 0.020 Height of Curb at Gutter Flow Line H_{CURB} 6.00 Distance from Curb Face to Street Crown 26.0 T_{CROWN} Gutter Width w: 2.00 Street Transverse Slope S_X : 0.020 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) S_w : 0.083 ft/ft S_o : Street Longitudinal Slope - Enter 0 for sump condition 0.010 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) n_{STREET} : 0.016 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm 20.0 26.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm 6.0 12.0 Allow Flow Depth at Street Crown (leave blank for no) check = yes MINOR STORM Allowable Capacity is based on Depth Criterion Minor Storm Major Storm MAJOR STORM Allowable Capacity is based on Spread Criterion 13.8 32.7 WARNING: MINOR STORM max. allowable capacity is less than the design flow given on sheet 'Inlet Management' lajor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management

Existing Inlet Calcs-DLM.xlsm, INLET 1 2/24/2021, 6:57 AM

Version 4.06 Released August 2018



Design Information (Input)		MINOR	MAJOR	
Type of Inlet CDOT Type R Curb Opening ▼	Type =	CDOT Type F	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	10.00	10.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: WARNING: Q > ALLOWABLE Q FOR MINOR STORM		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	8.4	11.1	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	5.8	15.4	cfs
Capture Percentage = Q _a /Q _o =	C% =	59	42	%

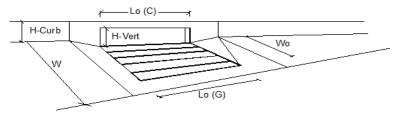
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ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) Project: **Crossroads Mixed Use Existing Inlets** Inlet ID: INLET 2 CRONN Gutter Geometry (Enter data in the blue cells) T_{BACK} Maximum Allowable Width for Spread Behind Curb 14.0 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) $\mathsf{S}_{\mathsf{BACK}}$ 0.020 ft/ft Manning's Roughness Behind Curb (typically between 0.012 and 0.020) 0.020 Height of Curb at Gutter Flow Line H_{CURB} 6.00 Distance from Curb Face to Street Crown 26.0 T_{CROWN} Gutter Width w: 2.00 Street Transverse Slope S_X : 0.020 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) S_w : 0.083 ft/ft S_o : Street Longitudinal Slope - Enter 0 for sump condition 0.010 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) n_{STREET} : 0.016 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm 20.0 26.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm 6.0 12.0 Allow Flow Depth at Street Crown (leave blank for no) check = yes MINOR STORM Allowable Capacity is based on Depth Criterion Minor Storm Major Storm MAJOR STORM Allowable Capacity is based on Spread Criterion 13.8 32.7 linor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Manage lajor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Manager

Existing Inlet Calcs-DLM.xlsm, INLET 2 2/24/2021, 6:57 AM

Version 4.06 Released August 2018



Design Information (Input) CDOT Type R Curb Opening		MINO	R MAJOR	
Type of Inlet	Тур	e = CDOT	Type R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCA}	L = 3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	N	o = 1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L	o = 10.00	10.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W	o = N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _r (9 = N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _r -(0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity		MINO	R MAJOR	
Total Inlet Interception Capacity	(Q = 3.1	5.3	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q	_b = 0.0	0.7	cfs
Capture Percentage = Q _a /Q _o =	C%	6 = 100	88	%

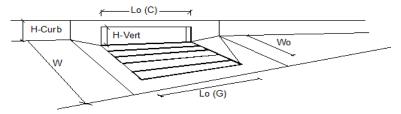
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ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) Project: Crossroads Mixed Use Inlet ID: Inlet 3 CRONN Gutter Geometry (Enter data in the blue cells) T_{BACK} Maximum Allowable Width for Spread Behind Curb 7.5 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) S_{BACK} : 0.020 ft/ft Manning's Roughness Behind Curb (typically between 0.012 and 0.020) 0.020 Height of Curb at Gutter Flow Line H_{CURB} 6.00 Distance from Curb Face to Street Crown T_{CROWN} 27.0 Gutter Width w: 1.00 Street Transverse Slope S_X : 0.020 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) S_w : 0.083 ft/ft S_o : Street Longitudinal Slope - Enter 0 for sump condition 0.005 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) n_{STREET} : 0.016 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm 22.8 27.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm 6.0 12.0 Allow Flow Depth at Street Crown (leave blank for no) check = yes MINOR STORM Allowable Capacity is based on Depth Criterion Minor Storm Major Storm MAJOR STORM Allowable Capacity is based on Spread Criterion 13.8 24.4 Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Manage lajor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Manager

Proposed Inlet Calcs.xlsm, Inlet 3

Version 4.06 Released August 2018



Design Information (Input) CDOT Type R Curb Opening ▼		MINOR	MAJOR	
Type of Inlet CDOT Type R Curb Opening	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	10.00	10.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	6.7	9.8	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	3.5	13.5	cfs
Capture Percentage = Q _a /Q _o =	C% =	65	42	%

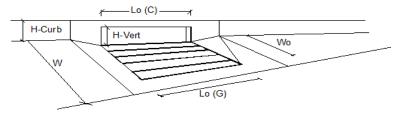
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ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) Project: Crossroads Mixed Use Inlet ID: Inlet 4 - AT-GRADE STREET Gutter Geometry (Enter data in the blue cells) T_{BACK} Maximum Allowable Width for Spread Behind Curb 7.5 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) 0.020 ft/ft Manning's Roughness Behind Curb (typically between 0.012 and 0.020) 0.020 Height of Curb at Gutter Flow Line H_{CURB} 6.00 Distance from Curb Face to Street Crown 26.0 T_{CROWN} Gutter Width W = 2.00 Street Transverse Slope S_X : 0.020 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) S_w : 0.083 ft/ft S_o : Street Longitudinal Slope - Enter 0 for sump condition 0.010 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) n_{STREET} : 0.016 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm 20.8 26.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm 6.0 12.0 Allow Flow Depth at Street Crown (leave blank for no) check = yes MINOR STORM Allowable Capacity is based on Depth Criterion Minor Storm Major Storm MAJOR STORM Allowable Capacity is based on Spread Criterion 13.8 32.7

Ainor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Manager Aajor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Manager

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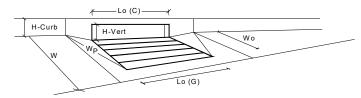
Design Information (Input) CDOT Type R Curb Opening		MINOR	MAJOR	_
Type of Inlet	Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	15.00	15.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'	_	MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	6.6	10.7	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	-0.1	1.7	cfs
Capture Percentage = Q _a /Q _o =	C% =	102	86	%

Version 4.06 Released August 2018 ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) Crossroads Mixed Use Project: Inlet ID: STREET Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb 7.5 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) 0.020 ft/ft Manning's Roughness Behind Curb (typically between 0.012 and 0.020) Height of Curb at Gutter Flow Line H_{CURB} : 6.00 Distance from Curb Face to Street Crown 26.0 Gutter Width W= 2.00 Street Transverse Slope S_X = Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) S_{W} 0.083 t/ft Street Longitudinal Slope - Enter 0 for sump condition s_{o} Manning's Roughness for Street Section (typically between 0.012 and 0.020) Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm 20.8 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm 6.0 12.0 Check boxes are not applicable in SUMP conditions MINOR STORM Allowable Capacity is based on Depth Criterion Minor Storm Major Storm SUMP MAJOR STORM Allowable Capacity is based on Depth Criterion

Proposed Inlet Calcs.xlsm, Inlet 5 6/18/2021, 4:56 PM

INLET IN A SUMP OR SAG LOCATION

Version 4.06 Released August 2018



Design Information (Input)	CDOT Type R Curb Opening ▼	_	MINOR	MAJOR	_
Type of Inlet		Type =		Curb Opening	
Local Depression (additional to co	ontinuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or C	urb Opening)	No =	1	1	
Water Depth at Flowline (outside	of local depression)	Ponding Depth =	6.0	12.0	inches
Grate Information			MINOR	MAJOR	Override Depths
Length of a Unit Grate		L _o (G) =	N/A	N/A	feet
Width of a Unit Grate		W _o =	N/A	N/A	feet
Area Opening Ratio for a Grate (t	vpical values 0.15-0.90)	A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grat		C _f (G) =	N/A	N/A	-
Grate Weir Coefficient (typical va	,	C _w (G) =	N/A	N/A	-
					-
Grate Orifice Coefficient (typical v	/alue 0.60 - 0.80)	C _o (G) =	N/A	N/A	
Curb Opening Information			MINOR	MAJOR	٦
Length of a Unit Curb Opening		L _o (C) =	15.00	15.00	feet
Height of Vertical Curb Opening in		H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Ir	nches	H _{throat} =	6.00	6.00	inches
Angle of Throat (see USDCM Fig	ure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (ty	ypically the gutter width of 2 feet)	W _p =	2.00	2.00	feet
Clogging Factor for a Single Curb	Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (ty	/pical value 2.3-3.7)	C _w (C) =	3.60	3.60	7
Curb Opening Orifice Coefficient		C _o (C) =	0.67	0.67	7
Grate Flow Analysis (Calculated		-01-7	MINOR	MAJOR	
Clogging Coefficient for Multiple I		Coef =	N/A	N/A	7
Clogging Coemcient for Multiple Units		Clog =	N/A	N/A	-
Grate Capacity as a Weir (base		Clog -	MINOR	MAJOR	_
	1 on Modified REC22 Method)	o -F	N/A		٦.,.
Interception without Clogging		Q _{wi} =		N/A	cfs
Interception with Clogging		Q _{wa} =	N/A	N/A	cfs
	sed on Modified HEC22 Method)	_	MINOR	MAJOR	_
Interception without Clogging		Q _{oi} =	N/A	N/A	cfs
Interception with Clogging		Q _{oa} =	N/A	N/A	cfs
Grate Capacity as Mixed Flow		_	MINOR	MAJOR	
Interception without Clogging		Q _{mi} =	N/A	N/A	cfs
Interception with Clogging		Q _{ma} =	N/A	N/A	cfs
Resulting Grate Capacity (assu	mes cloaged condition)	Q _{Grate} =	N/A	N/A	cfs
Curb Opening Flow Analysis (C	,	*****	MINOR	MAJOR	
Clogging Coefficient for Multiple I		Coef =	1.31	1.31	7
Clogging Factor for Multiple Units		Clog =	0.04	0.04	┥
Curb Opening as a Weir (based		City	MINOR	MAJOR	_
Interception without Clogging	on mounted ricozz methody	Q _{wi} =	10.4	51.0	cfs
		Q _{wa} =	9.9	48.8	cfs
Interception with Clogging		Q _{wa} –			cis
	sed on Modified HEC22 Method)		MINOR	MAJOR	٦,
Interception without Clogging		Q _{oi} =	29.4	40.9	cfs
Interception with Clogging		Q _{oa} =	28.1	39.1	cfs
Curb Opening Capacity as Mixe	ed Flow	_	MINOR	MAJOR	_
Interception without Clogging		Q _{mi} =	16.2	42.5	cfs
Interception with Clogging		Q _{ma} =	15.5	40.6	cfs
Resulting Curb Opening Capac	ity (assumes clogged condition)	Q _{Curb} =	9.9	39.1	cfs
Resultant Street Conditions	·		MINOR	MAJOR	
Total Inlet Length		L=	15.00	15.00	feet
	sed on street geometry from above)	T =	18.9	43.7	ft.>T-Crown
Resultant Flow Depth at Street Cr		d _{CROWN} =	0.0	4.2	inches
		CROWN			-
_ow Head Performance Reduct	ion (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	,	d _{Grate} =	N/A	N/A	ft
Depth for Curb Opening Weir Equ	ation	d _{Grate} =	0.34	0.83	
				1.00	- "
Combination Inlet Performance R		RF _{Combination} =	0.57	1.00	-1
Control Destaurance Destaurance		RF _{Curb} =			
		RF _{Grate} =	N/A	N/A	⊣
	ion Factor for Long Inlets	-			
	ion Factor for Long Inlets	_			
Grated Inlet Performance Reduct		_	MINOR	MAJOR	_
Curb Opening Performance Reduct Grated Inlet Performance Reduct Fotal Inlet Interception Ca	on Factor for Long Inlets pacity (assumes clogged condition)	Q _a =	MINOR 9.9	MAJOR 39.1	cfs

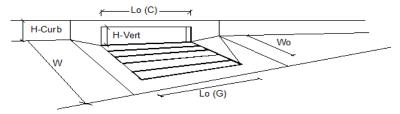
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ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) Project: Crossroads Mixed Use Inlet ID: Inlet 6 CRONN Gutter Geometry (Enter data in the blue cells) T_{BACK} Maximum Allowable Width for Spread Behind Curb 7.5 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) S_{BACK} : 0.020 ft/ft Manning's Roughness Behind Curb (typically between 0.012 and 0.020) 0.020 Height of Curb at Gutter Flow Line H_{CURB} 6.00 Distance from Curb Face to Street Crown T_{CROWN} 14.5 Gutter Width w: 2.00 Street Transverse Slope S_X : 0.020 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) S_w : 0.083 ft/ft S_o : Street Longitudinal Slope - Enter 0 for sump condition 0.020 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) n_{STREET} : 0.016 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm 14.0 14.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm 4.4 12.0 Allow Flow Depth at Street Crown (leave blank for no) check = yes MINOR STORM Allowable Capacity is based on Depth Criterion Minor Storm Major Storm MAJOR STORM Allowable Capacity is based on Spread Criterion 9.6 linor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Manage lajor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Manager

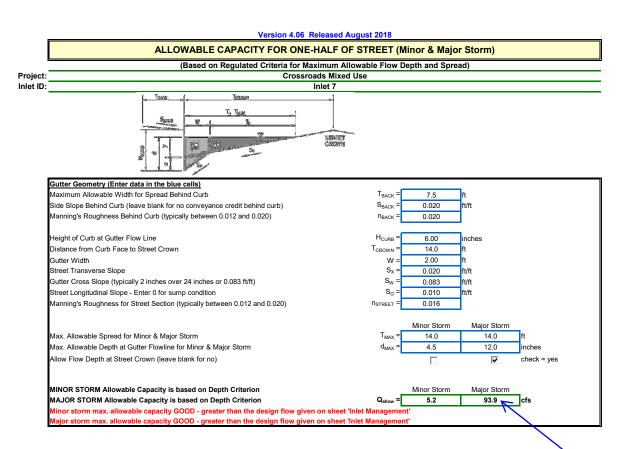
Proposed Inlet Calcs.xlsm, Inlet 6 2/24/2021, 6:56 AM

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Design Information (Input)		MINOR	MAJOR	
Type of Inlet CDOT Type R Curb Opening	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	10.00	10.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	4.8	6.9	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.4	2.6	cfs
Capture Percentage = Q _a /Q _o =	C% =	93	73	%

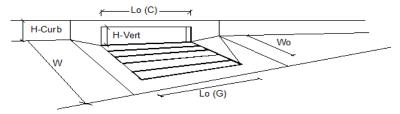
Proposed Inlet Calcs.xlsm, Inlet 6 2/24/2021, 6:56 AM



Why is this half of the road carrying so much more than the other half? See previous inlet 6 sheet.

Proposed Inlet Calcs.xlsm, Inlet 7 2/25/2021, 9:39 AM

Version 4.06 Released August 2018



Design Information (Input)		MINOR	MAJOR	
Type of Inlet CDOT Type R Curb Opening ▼	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	10.00	10.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	•
Total Inlet Interception Capacity	Q =	4.8	6.9	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.4	2.6	cfs
Capture Percentage = Q _a /Q _o =	C% =	92	72	%

Proposed Inlet Calcs.xlsm, Inlet 7 2/25/2021, 9:39 AM

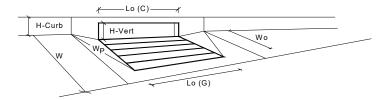


ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) Project: Crossroads Mixed Use Inlet ID: Inlet 8 STREET Gutter Geometry (Enter data in the blue cells) T_{BACK} Maximum Allowable Width for Spread Behind Curb 7.5 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) $\mathsf{S}_{\mathsf{BACK}}$ 0.020 ft/ft Manning's Roughness Behind Curb (typically between 0.012 and 0.020) 0.020 Height of Curb at Gutter Flow Line H_{CURB} 6.00 Distance from Curb Face to Street Crown T_{CROWN} 14.0 Gutter Width W = 2.00 Street Transverse Slope S_X : 0.020 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) S_w : 0.083 ft/ft Street Longitudinal Slope - Enter 0 for sump condition S_o : 0.000 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) n_{STREET} : 0.016 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm 14.0 14.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm 4.4 12.0 Check boxes are not applicable in SUMP conditions MINOR STORM Allowable Capacity is based on Depth Criterion Minor Storm Major Storm MAJOR STORM Allowable Capacity is based on Depth Criterion SUMP SUMP

Proposed Inlet Calcs.xlsm, Inlet 8 6/18/2021, 4:57 PM

INLET IN A SUMP OR SAG LOCATION

Version 4.06 Released August 2018



Design Information (Input) CDOT Type R Curb Opening ▼	_	MINOR	MAJOR	_
Type of Inlet	Type =	CDOT Type F	Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	4.4	8.0	inches
Grate Information	_	MINOR	MAJOR	Override Depths
Length of a Unit Grate	L ₀ (G) =	N/A	N/A	feet
Width of a Unit Grate	W _o =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	C _f (G) =	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C _w (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	C _o (G) =	N/A	N/A	
Curb Opening Information	_	MINOR	MAJOR	_
Length of a Unit Curb Opening	L ₀ (C) =	10.00	10.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H _{throat} =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W _p =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	C _w (C) =	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	C _o (C) =	0.67	0.67]
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d _{Curb} =	0.20	0.50	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	0.41	0.75	
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	0.82	1.00	
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A	
		MINOR	MAJOR	_
Total Inlet Interception Capacity (assumes clogged condition)	Q _a =	3.3	16.3	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q _{PEAK REQUIRED} =	2.1	3.8	cfs

Proposed Inlet Calcs.xlsm, Inlet 8 6/18/2021, 4:57 PM

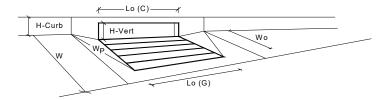


ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) Project: Crossroads Mixed Use Inlet ID: Inlet 9 STREET Gutter Geometry (Enter data in the blue cells) T_{BACK} Maximum Allowable Width for Spread Behind Curb 7.5 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) $\mathsf{S}_{\mathsf{BACK}}$ 0.020 ft/ft Manning's Roughness Behind Curb (typically between 0.012 and 0.020) 0.020 Height of Curb at Gutter Flow Line H_{CURB} 6.00 Distance from Curb Face to Street Crown T_{CROWN} 14.0 Gutter Width W = 2.00 Street Transverse Slope S_X : 0.020 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) S_w : 0.083 ft/ft Street Longitudinal Slope - Enter 0 for sump condition S_o : 0.000 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) n_{STREET} : 0.016 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm 14.0 14.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm 4.4 12.0 Check boxes are not applicable in SUMP conditions MINOR STORM Allowable Capacity is based on Depth Criterion Minor Storm Major Storm MAJOR STORM Allowable Capacity is based on Depth Criterion SUMP SUMP

Proposed Inlet Calcs.xlsm, Inlet 9 6/18/2021, 4:58 PM

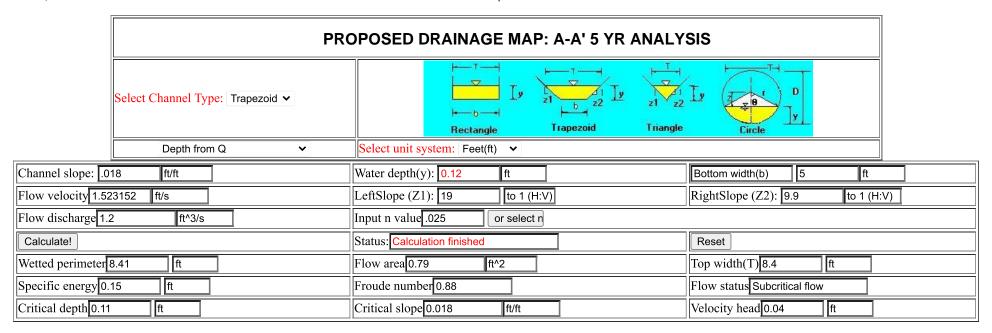
INLET IN A SUMP OR SAG LOCATION

Version 4.06 Released August 2018

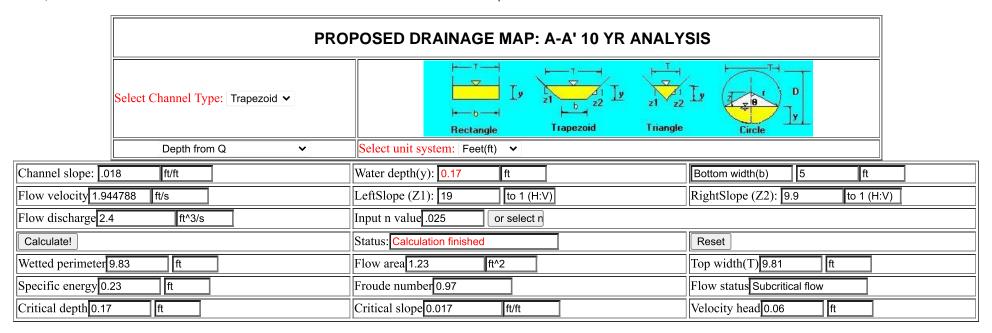


Design Information (Input) CDOT Type R Curb Opening ▼	_	MINOR	MAJOR	_
Type of Inlet	Type =	CDOT Type F	Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	4.4	8.0	inches
Grate Information	_	MINOR	MAJOR	Override Depths
Length of a Unit Grate	L ₀ (G) =	N/A	N/A	feet
Width of a Unit Grate	W _o =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	C _f (G) =	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C _w (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	C _o (G) =	N/A	N/A	
Curb Opening Information	_	MINOR	MAJOR	_
Length of a Unit Curb Opening	L _o (C) =	15.00	15.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H _{throat} =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W _p =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_f(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	C _w (C) =	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	C _o (C) =	0.67	0.67]
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d _{Curb} =	0.20	0.50	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	0.41	0.75	
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	0.67	0.89	
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A	
		MINOR	MAJOR	_
Total Inlet Interception Capacity (assumes clogged condition)	Q _a =	3.7	20.3	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q _{PEAK REQUIRED} =	3.6	17.3	cfs

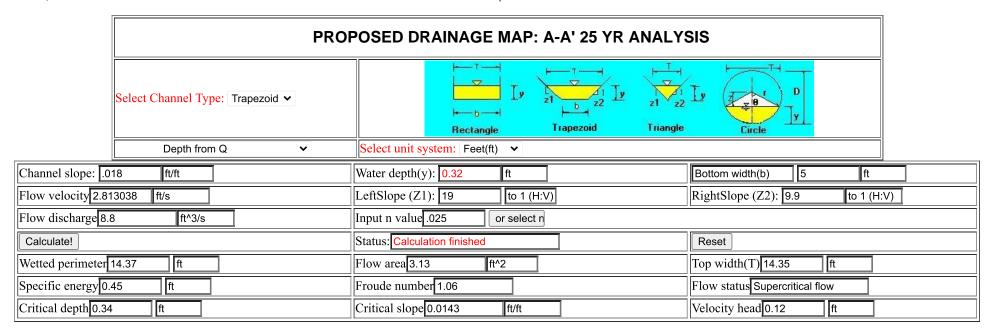
Proposed Inlet Calcs.xlsm, Inlet 9 6/18/2021, 4:58 PM



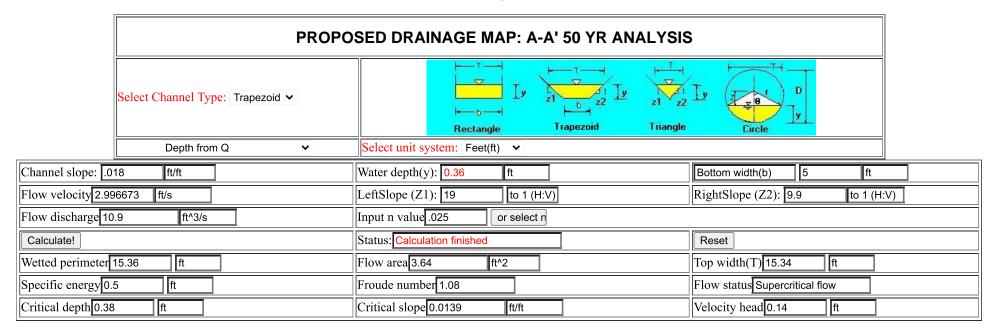
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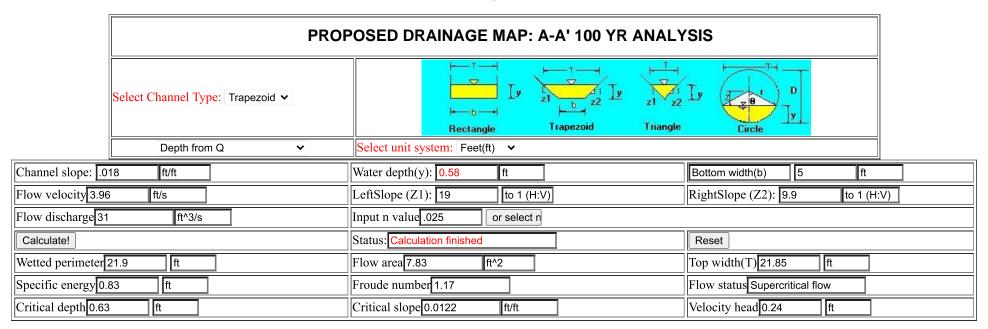
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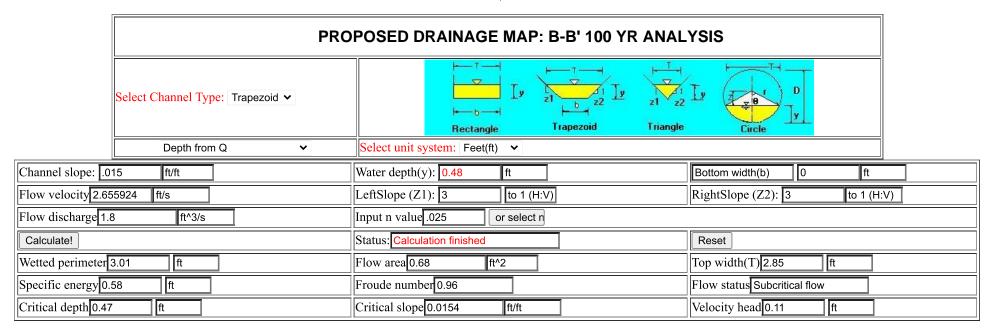
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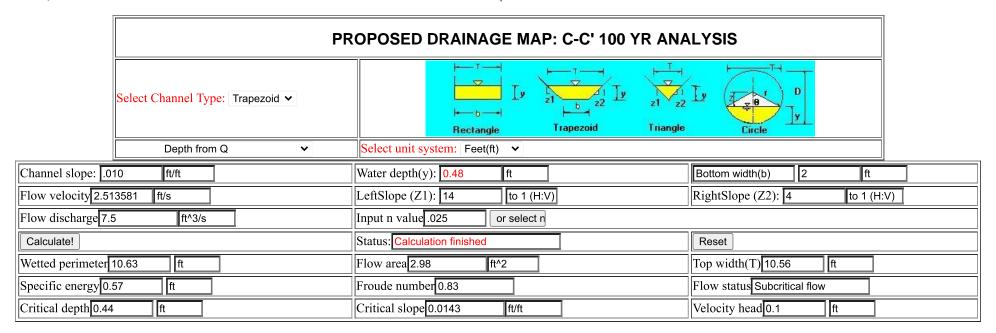
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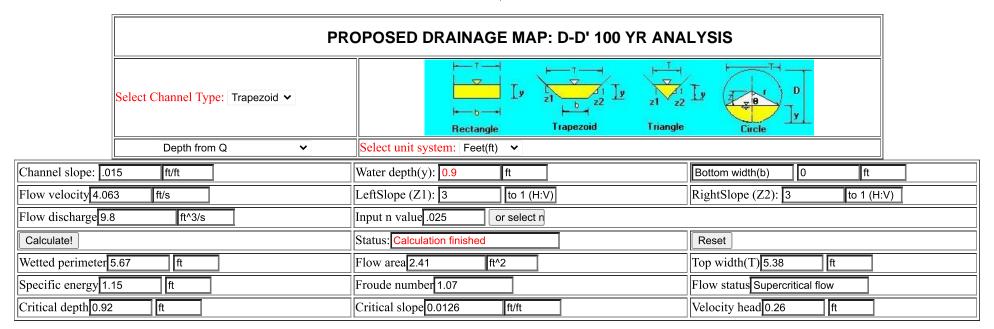
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Project: CROSSROADS MIXED USE FIL. NO. 1: POND STRUCTURES

Date: 10/11/2021

Minimum Forebay (olime. 3% of WOCV = (0.03)(0.857ac.ft)(43560ft) = 1/19.93ft3 = 560ft / Forebay (design)	!5
(301ft²)(25ft depth) = 602ft (Actual) > 560ft (Design)	W 44. HOLD
Forebuy Belease and Configuration Belease 296 of 100-yr Reale Discharge **A	/
(0.07)(82.7cfs) = 1.65 cfs (design) < 2.13 cfs (actual) **See attached Bectongular Contracted Webs Sheet "for actual flow determination	Mar Julya . 2 P
Micropool Stelng 32.10 acres @ 78.7% imperviousness	
Tributary Imperious Area = (32.10 acres) (78.745) = 25.3 acres Trom Fig. I - Micropool Surface Area (5A) determination whart provided by Othy of Colorado Springs, - 7	
See Attached 1.) See attached Open Channel Flow Calc- ulator sheet for Low-Flow channel capacity	Hy

Irrigation in the Pacific Northwest

Rectangular Contracted Weir

level right as it leaves the weir). Learn more about the units used on this page.

Washington State University Extension

This calculates the water flow rate over a rectangular contracted weir. This weir has a rectangular opening where the

sides are straight up and down. A contracted weir means that the ditch or canal leading up to the weir is wider than

the weir opening itself. The water before the weir should be held in a relatively calm and smooth pool. There should

be air (not trapped) underneath the water leaving the weir. The Length is the bottom width of the weir. The height is

measured from the bottom of the weir opening to the top of the water level ponded behind the weir (not the water

Oregon State University Extension University of Idaho Extension

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Cipolletti

(Trapezoidal) Weir

90° Triangular Notch Weir

Parshall Flume

Rectangular Contracted Weir

Rectangular Submerged

Orifices Trapezoidal Flume

Vertical Pipes

Chemigation

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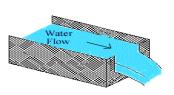
Calculators

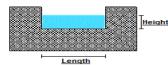
3 in 🗸 Height: Calculate

Flow Rate:

Length:

2.13 cfs 🗸





* Note: 1 point = 1/100 ft.

The Equation

The Equation used to determine the flow rate (Q) of a Rectangular Contracted Weir is:

$$Q = 3.247 \cdot L \cdot H^{1.48} - \frac{0.566 L^{1.9}}{1 + 2 \cdot L^{1.87}} \cdot H^{1.9}$$

Where:

Q = Flow Rate in cfs.

L= Bottom width of the weir in feet.

H = Height of the upstream water above the weir crest in feet.

WSU Prosser - IAREC, 24106 N Bunn Rd, Prosser WA 99350-8694, 509-786-2226. Contact Us

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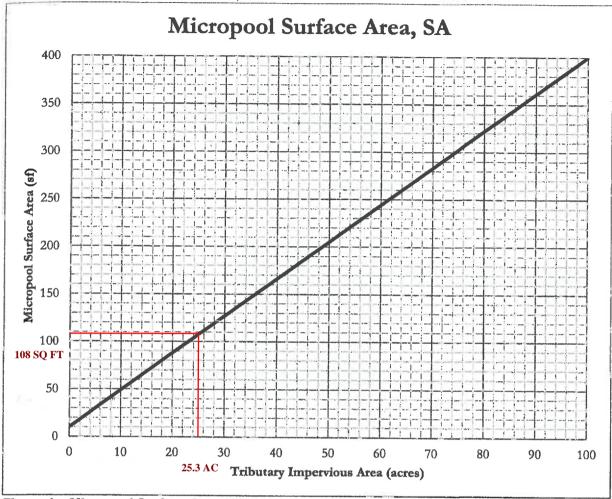


Figure 1 - Micropool Surface Area (SA) Determination Chart

The tributary impervious area is the effective number of impervious acres that will be treated by the extended detention basin (EDB). It is calculated by multiplying the tributary area to be treated by the impervious fraction of that area.

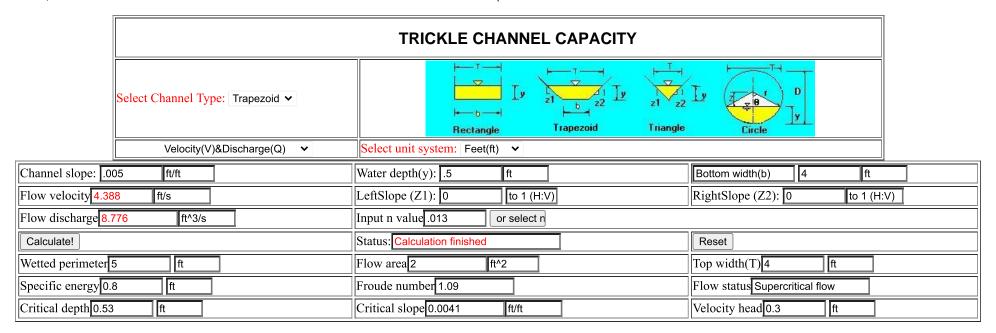
$$TIA = I \times A$$

TIA = Tributary impervious area (acres)

I = Imperviousness (fraction)

= Tributary catchment area upstream (acres)

For EDBs with tributary impervious areas greater than 100 acres, the micropool surface area is 400 sf. The initial surcharge depth (ISD) is defined as the depth of the initial surcharge volume (ISV). The surface area determined using Figure 1 assumes an ISD of 4 inches. The initial surcharge volume is thus calculated by multiplying the micropool surface area by 4 inches.



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Chapter 8 Open Channels

SOIL RIPRAP NOTES:

 ELEVATION TOLERANCES FOR THE SOIL RIPRAP SHALL BE 0.10 FEET. THICKNESS OF SOIL RIPRAP SHALL BE NO LESS THAN THICKNESS SHOWN AND NO MORE THAN 2-INCHES GREATER THAN THE THICKNESS SHOWN.

- 2. WHERE "SOIL RIPRAP" IS DESIGNATED ON THE CONTRACT DRAWINGS, RIPRAP VOIDS ARE TO BE FILLED WITH NATIVE SOIL. THE RIPRAP SHALL BE PRE-MIXED WITH THE NATIVE SOIL AT THE FOLLOWING PROPORTIONS BY VOLUME: 65PERCENT RIPRAP AND 35 PERCENT SOIL. THE SOIL USED FOR MIXING SHALL BE NATIVE TOPSOIL AND SHALL HAVE A MINIMUM FINES CONTENT OF 15 PERCENT. THE SOIL RIPRAP SHALL BE INSTALLED IN A MANNER THAT RESULTS IN A DENSE, INTERLOCKED LAYER OF RIPRAP WITH RIPRAP VOIDS FILLED COMPLETELY WITH SOIL. SEGREGATION OF MATERIALS SHALL BE AVOIDED AND IN NO CASE SHALL THE COMBINED MATERIAL CONSIST PRIMARILY OF SOIL; THE DENSITY AND INTERLOCKING NATURE OF RIPRAP IN THE MIXED MATERIAL SHALL ESSENTIALLY BE THE SAME AS IF THE RIPRAP WAS PLACED WITHOUT SOIL.
- 3. WHERE SPECIFIED (TYPICALLY AS "BURIED SOIL RIPRAP"), A SURFACE LAYER OF TOPSOIL SHALL BE PLACED OVER THE SOIL RIPRAP ACCORDING TO THE THICKNESS SPECIFIED ON THE CONTRACT DRAWINGS. THE TOPSOIL SURFACE LAYER SHALL BE COMPACTED TO APPROXIMATELY 85% OF MAXIMUM DENSITY AND WITHIN TWO PERCENTAGE POINTS OF OPTIMUM MOISTURE IN ACCORDANCE WITH ASTM D698. TOPSOIL SHALL BE ADDED TO ANY AREAS THAT SETTLE.
- 4. ALL SOIL RIPRAP THAT IS BURIED WITH TOPSOIL SHALL BE REVIEWED AND APPROVED BY THE ENGINEER PRIOR TO ANY TOPSOIL PLACEMENT.

	GRADATION FOR GRANULAR BEDDING											
	PERCENT PASSING BY WEIGHT											
U.S. STANDARD SIEVE SIZE	TYPE I CDOT SECT. 703.01	TYPE II CDOT SECT. 703.09 CLASS A										
3 INCHES	-	90 — 100										
1½ INCHES	_	_										
¾ INCHES	_	20 — 90										
¾ INCHES	100	_										
#4	95 — 100	0 - 20										
#16	45 - 80	-										
#50	10 - 30	-										
#100	2 - 10	_										
#200	0 - 2	0 - 3										

RIPRAP BEDDING

Figure 8-34. Riprap and soil riprap placement and gradation (part 2 of 3)

Open Channels Chapter 8

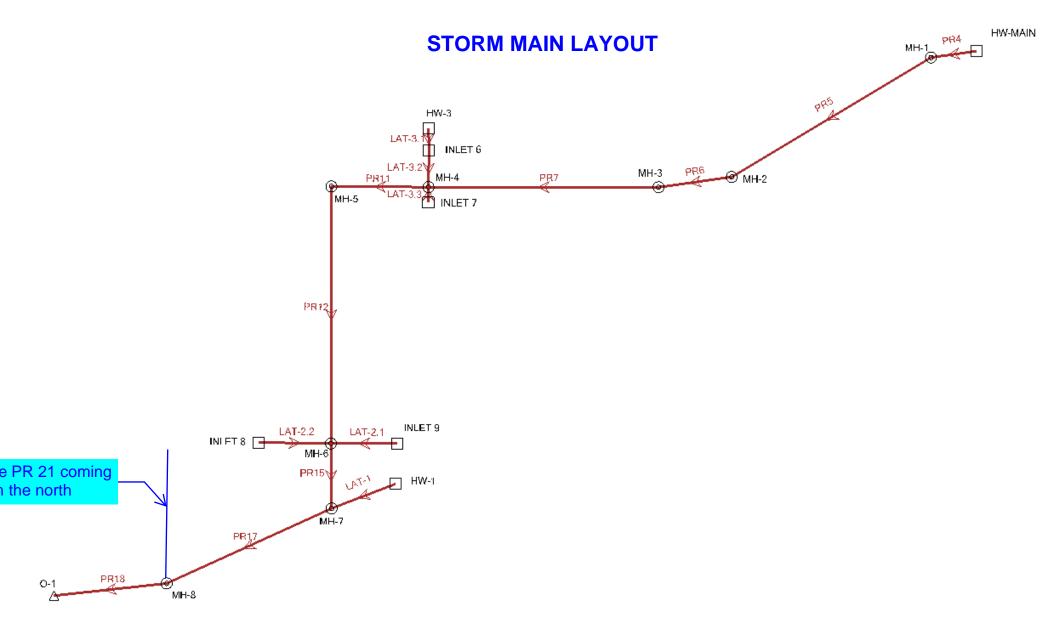
THICKNESS REQUIREMENTS FOR GRANULAR BEDDING											
	MINIMUM BEDDING THICKNESS (INCHES)										
RIPRAP DESIGNATION	FINE-GRAIN	COARSE-GRAINED SOILS 2									
	TYPE I (LOWER LAYER)	TYPE II (UPPER LAYER)	TYPE II								
$VL (D_{50} = 6 IN)$	4	4	6								
$L (D_{50} = 9 IN)$	4	4	6								
$M (D_{50} = 12 IN)$	4	4	6								
$H (D_{50} = 18 IN)$	4	6	8								
VH ($D_{50} = 24 \text{ IN}$)	4	6	8								

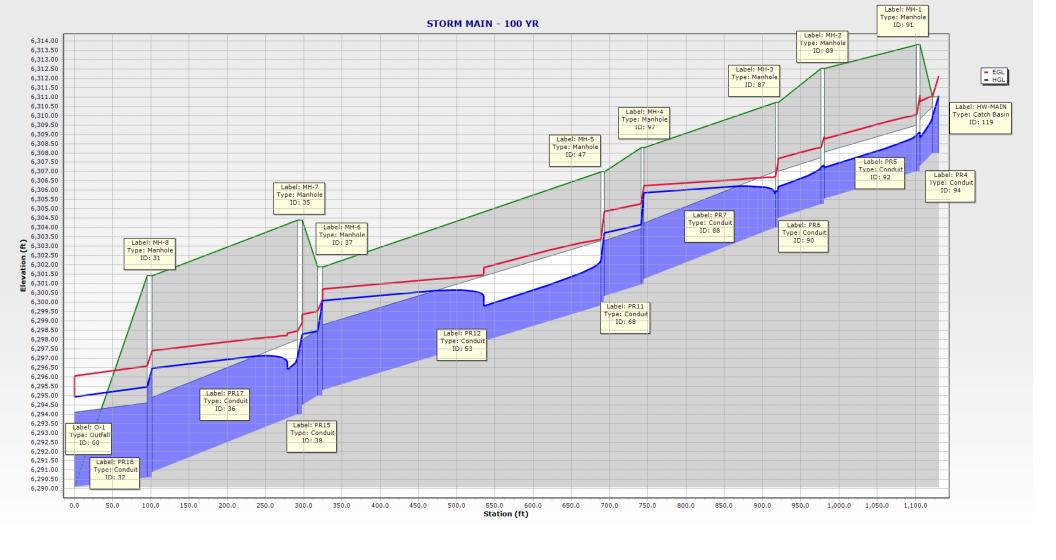
NOTES:

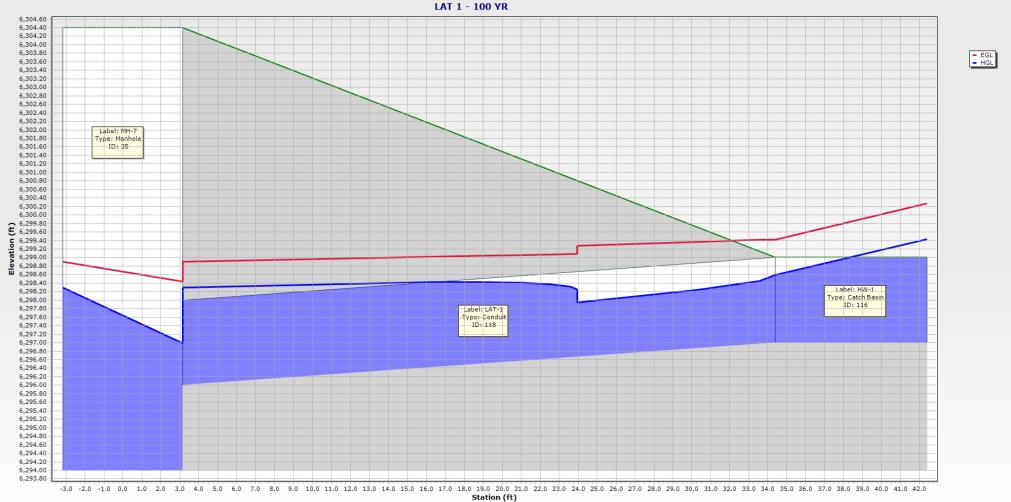
1. MAY SUBSTITUTE ONE 12-INCH LAYER OF TYPE II BEDDING. THE SUBSTITUTION OF ONE LAYER OF TYPE II BEDDING SHALL NOT BE PERMITTED AT DROP STRUCTURES. THE USE OF A COMBINATION OF FILTER FABRIC AND TYPE II BEDDING AT DROP STRUCTURES IS ACCEPTABLE.

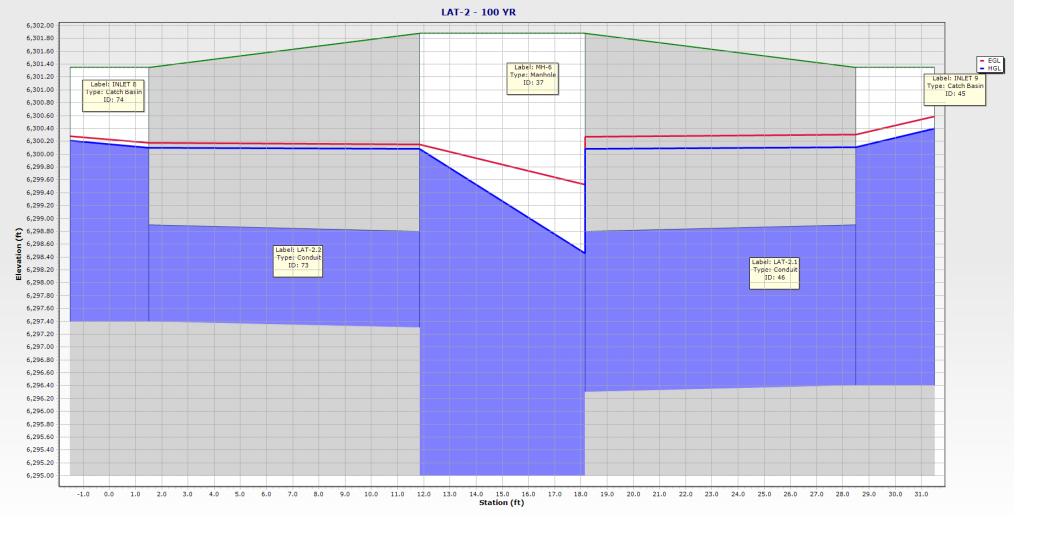
2. FIFTY PERCENT OR MORE BY WEIGHT RETAINED ON THE #40 SIEVE.

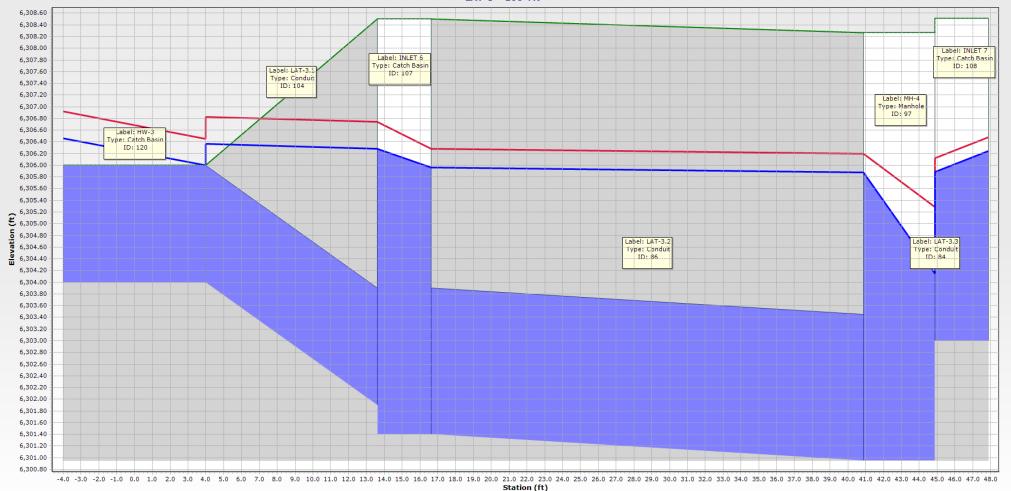
Figure 8-34. Riprap and soil riprap placement and gradation (part 3 of 3)











STORM MAIN - FLEXTABLE

FlexTable: Conduit Table

	FlexTable: Conduit Table													
Label	ID	Upstream Structure	Flow (cfs)	Flow / Capacity (Design) (%)	Length (Unified) (ft)	Velocity (ft/s)	Froude Number (Normal)	Depth (Normal) (ft)	Depth (Critical) (ft)	Energy Grade Line (In) (ft)	Energy Grade Line (Out) (ft)	Hydraulic Grade Line (In) (ft)	Hydraulic Grade Line (Out) (ft)	Headloss (ft)
PR18	32	MH-8	106.60	104.0	98.2	8.48	0.800	3.45	3.12	6,296.40	6,295.86	6,295.28	6,294.74	0.54
PR17	36	MH-7	97.40	54.0	196.4	14.64	1.999	2.09	2.99	6,298.44	6,297.22	6,296.99	6,296.29	0.70
PR15	38	MH-6	79.60	57.6	26.5	14.86	2.114	1.91	2.79	6,299.53	6,299.36	6,298.46	6,298.30	0.16
LAT-2.1	46	INLET 9	17.30	51.7	15.0	3.52	1.209	1.27	1.41	6,300.30	6,300.27	6,300.11	6,300.08	0.03
PR12	53	MH-5	60.50	54.4	369.6	11.80	1.717	1.84	2.44	6,303.36	6,300.70	6,302.25	6,300.08	2.17
PR11	68	MH-4	60.50	82.0	52.3	8.56	1.502	2.07	2.51	6,305.28	6,304.85	6,304.15	6,303.71	0.43
LAT-2.2	73	INLET 8	3.80	44.3	15.0	2.15	1.130	0.70	0.75	6,300.17	6,300.15	6,300.10	6,300.08	0.02
LAT-3.3	84	INLET 7	6.90	19.7	2.3	3.90	2.064	0.70	1.02	6,306.12	6,306.11	6,305.89	6,305.88	0.01
LAT-3.2	86	INLET 6	22.30	42.7	27.8	4.54	1.925	1.14	1.61	6,306.28	6,306.20	6,305.96	6,305.88	0.08
PR7	88	MH-3	34.50	41.3	175.7	11.24	1.955	1.34	1.91	6,306.73	6,306.25	6,305.91	6,305.88	0.03
PR6	90	MH-2	34.50	75.3	60.1	10.25	1.522	1.62	2.00	6,308.29	6,307.69	6,307.25	6,306.18	1.07
PR5	92	MH-1	34.50	78.2	125.3	9.95	1.446	1.66	2.00	6,310.04	6,308.74	6,309.00	6,307.22	1.77
PR4	94	HW-MAIN	34.50	47.7	22.5	14.56	2.635	1.22	2.00	6,311.04	6,310.76	6,310.00	6,308.80	1.20
LAT-3.1	104	HW-3	17.00	20.2	15.1	5.41	5.583	0.61	1.49	6,306.82	6,306.74	6,306.37	6,306.28	0.09
LAT-1	118	HW-1	19.60	53.7	38.4	11.83	2.290	1.04	1.59	6,299.42	6,298.90	6,298.59	6,298.30	0.29
Upstream Structure Hydraulic Grade Line (In) (ft)	Upstream Structure Velocity (In- Governing) (ft/s)	Upstream Structure Headloss Coefficient	Upstream Structure Headloss (ft)	Elevation Ground (Start) (ft)	Elevation Ground (Stop) (ft)	Invert (Start) (ft)	Invert (Stop) (ft)	Conduit Description						
6,296.29	7.75	0.900	1.01	6,290.10	6,301.41	6,290.10	6,290.60	Circle - 48.0 in						
6,298.30	6.24	0.900	1.31	6,301.41	6,304.40	6,290.90	6,294.00	Circle - 48.0 in						
6,300.08	2.15	1.520	1.62	6,304.40	6,301.88	6,294.50	6,295.00	Circle - 42.0 in						
6,300.40	3.52	1.500	0.29	6,301.88	6,301.35	6,296.30	6,296.40	Circle - 30.0 in						
6,303.71	8.56	1.320	1.47	6,306.98	6,301.88	6,299.81	6,295.30	Circle - 42.0 in						

6,300.95 | Circle - 36.0 in

6,297.40 Circle - 18.0 in

6,303.00 Circle - 18.0 in

6,301.40 Circle - 30.0 in

6,304.00 Circle - 36.0 in

6,305.25 | Circle - 30.0 in

6,307.00 Circle - 30.0 in

6,308.00 Circle - 30.0 in 6,304.00 Circle - 24.0 in

6,297.00 Circle - 24.0 in

6,305.88

6,300.21

6,306.24

6,306.28

6,305.99

6,307.35

6,309.10

6,311.06

6,306.46

6,299.44

1.520

1.500

1.500

1.020

0.100

0.100

0.100

1.020

1.020

1.020

4.54

2.15

3.90

5.41

9.85

9.89

11.25

8.21

5.41

7.31

1.73

0.11

0.36

0.33

0.08

0.10

0.10

1.07

0.46

0.85

6,306.98

6,301.88

6,308.27

6,308.27

6,308.27

6,310.70

6,312.53

6,313.79

6,308.50

6,304.40

6,308.27

6,301.35

6,308.51

6,308.50

6,310.70

6,312.53

6,313.79

6,311.00

6,304.00

6,297.00

6,300.31

6,297.30

6,302.75

6,300.95

6,301.25

6,304.50

6,305.55

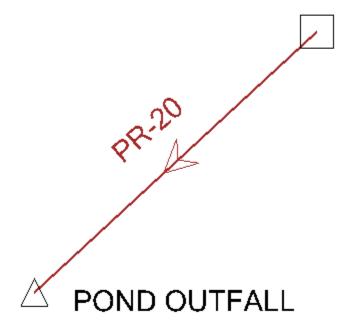
6,307.30

6,301.90

6,296.00

STORM 1 LAYOUT

OUTLET STRUCTURE



55.0 60.0 **Station (ft)**

65.0

70.0

75.0

80.0

85.0

90.0

95.0

100.0

105.0

110.0

115.0

40.0

45.0

50.0

0.0

10.0

5.0

15.0

20.0

25.0

30.0

35.0

STORM 1 - FLEXTABLE

FlexTable: Conduit Table

Label	ID	Upstream Structure	Flow (cfs)	Flow / Capacity (Design) (%)	Length (Unified) (ft)	Velocity (ft/s)	Froude Number (Normal)	Depth (Normal) (ft)	Depth (Critical) (ft)	Energy Grade Line (In) (ft)	Energy Grade Line (Out) (ft)	Hydraulic Grade Line (In) (ft)
PR-20	40	OUTLET STRUCTURE	11.40	102.0	112.2	7.20	1.059	1.26	1.29	6,289.33	6,288.06	6,288.56
Upstream Structure Hydraulic Grade Line (In) (ft)	Upstream Structure Velocity (In- Governing) (ft/s)	Upstream Structure Headloss Coefficient	Upstream Structure Headloss (ft)	Elevation Ground (Start) (ft)	Elevation Ground (Stop) (ft)	Invert (Start) (ft)	Invert (Stop) (ft)	Conduit Description				
6,289.72	7.06	1.500	1.16	6,287.50	6,293.77	6,286.00	6,287.27	Circle - 18.0 in				

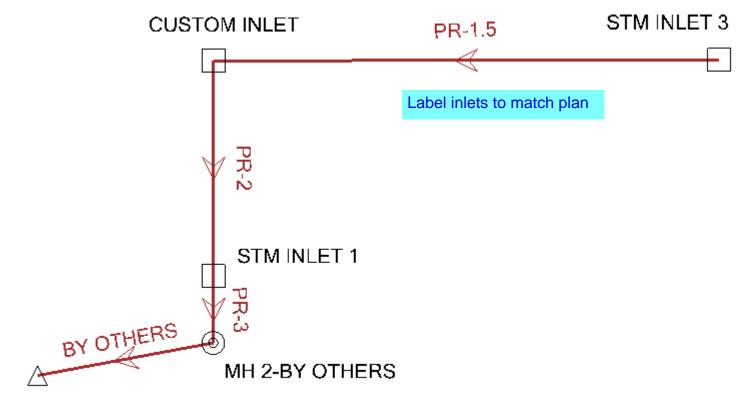
Hydraulic Grade Line (Out) (ft)

6,287.26

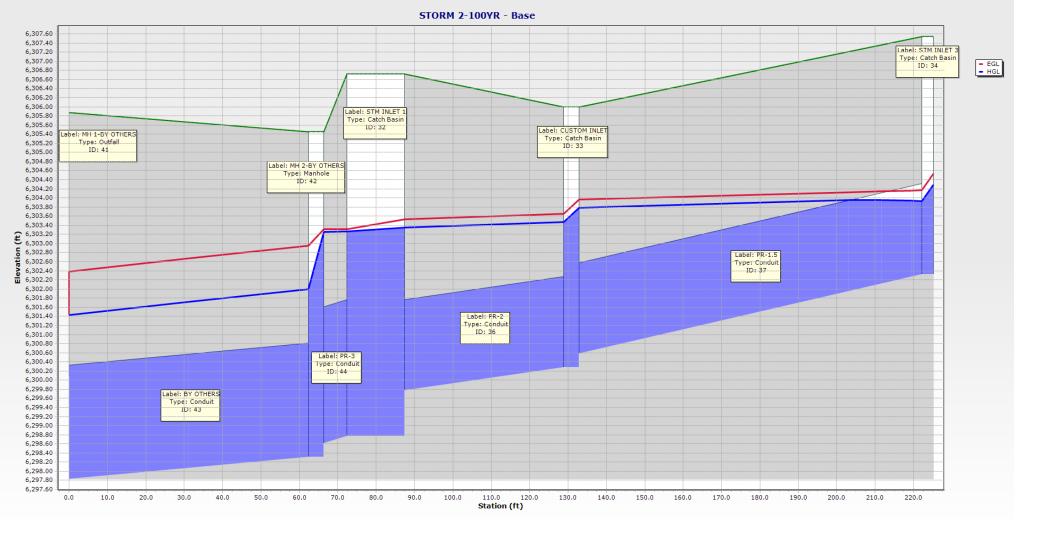
Headloss (ft)

1.30

STORM 2 LAYOUT



MH 1-BY OTHERS



STORM 2 - FLEXTABLE

FlexTable: Conduit Table

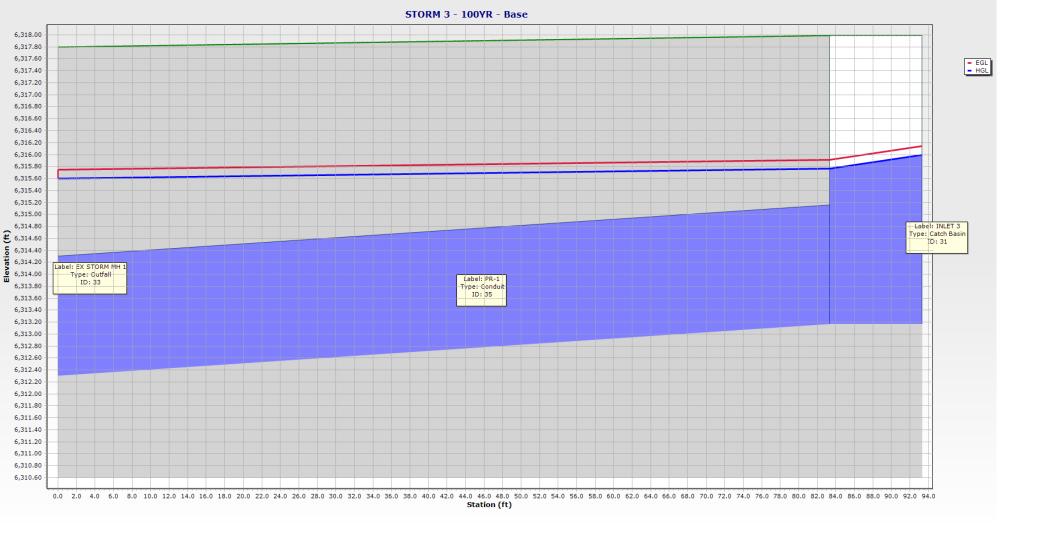
Label	ID	Upstream Structure	Flow (cfs)	Flow / Capacity (Design) (%)	Length (Unified) (ft)	Velocity (ft/s)	Froude Number (Normal)	Depth (Normal) (ft)	Depth (Critical) (ft)	Energy Grade Line (In) (ft)	Energy Grade Line (Out) (ft)	Hydraulic Grade Line (In) (ft)	Hydraulic Grade Line (Out) (ft)	Headloss (ft)
PR-2	36	CUSTOM INLET	10.70	47.3	51.0	3.41	1.442	0.97	1.17	6,303.65	6,303.53	6,303.47	6,303.35	0.11
PR-1.5	37	STM INLET 3	10.70	34.5	92.8	8.95	2.024	0.81	1.17	6,304.17	6,303.96	6,303.93	6,303.78	0.14
BY OTHERS	43	MH 2-BY OTHERS	38.50	108.6	64.3	7.84	0.875	(N/A)	2.10	6,302.95	6,302.39	6,302.00	6,301.43	0.57
PR-3	44	STM INLET 1	12.60	18.7	15.6	1.78	1.623	0.88	1.13	6,303.31	6,303.31	6,303.26	6,303.26	0.01
Upstream Structure Hydraulic Grade Line (In) (ft)	Upstream Structure Velocity (In- Governing) (ft/s)	Upstream Structure Headloss Coefficient	Upstream Structure Headloss (ft)	Elevation Ground (Start) (ft)	Elevation Ground (Stop) (ft)	Invert (Start) (ft)	Invert (Stop) (ft)	Conduit Description	26" DC	CD on CDia			^	
6,303.78	3.41	1.770	0.32	6,306.72	6,306.00	6,299.77	· ·	Circle - 24.0 in		36" RCP on CD's.			HGL set at tie	
6,304.29	3.96	1.500	0.36	6,306.00	6,307.54	6,300.58	l '	Circle - 24.0 in	Please	Revise		location?	Can the future	system
6,303.26	1.78	1.320	1.26	6,305.87	6,305.45	6,297.83	l '	Circle - 30.0 in				be added	in to ensure w	hole
6,303.35	3.41	1.770	0.09	6,305.45	6,306.72	6,298.61	6,298.77	Circle - 36.0 in				system ful	nctions prope	ly?

STORM 3 LAYOUT

EX STORM MH 1



INLET 3



STORM 3 - FLEXTABLE

FlexTable: Conduit Table

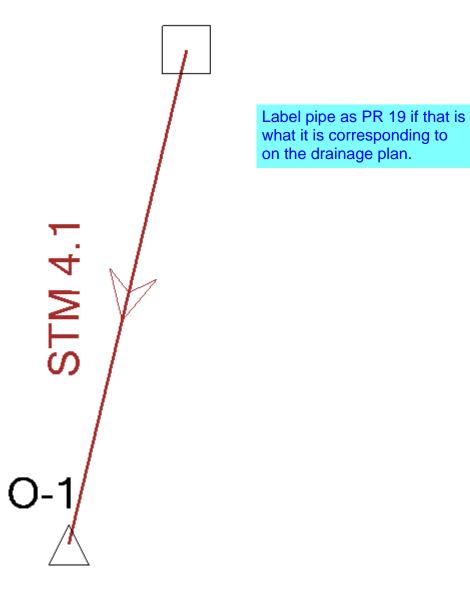
Label	ID	Upstream Structure	Flow (cfs)	Flow / Capacity (Design) (%)	Length (Unified) (ft)	Velocity (ft/s)	Froude Number (Normal)	Depth (Normal) (ft)	Depth (Critical) (ft)	Energy Grade Line (In) (ft)	Energy Grade Line (Out) (ft)	Hydraulic Grade Line (In) (ft)	Hydraulic Grade Line (Out) (ft)	Headloss (ft)
PR-1	35	INLET 3	9.80	43.9	88.3	3.12	1.434	0.93	1.12	6,315.92	6,315.75	6,315.77	6,315.60	0.17
Upstream Structure Hydraulic Grade Line (In) (ft)	Upstream Structure Velocity (In- Governing) (ft/s)	Upstream Structure Headloss Coefficient	Upstream Structure Headloss (ft)	Elevation Ground (Start) (ft)	Elevation Ground (Stop) (ft)	Invert (Start) (ft)	Invert (Stop) (ft)	Conduit Description						
6,315.99	3.12	1.500	0.23	6,317.99	6,317.80	6,313.16	6,312.30	Circle - 24.0 in			C	come from? If	L at existing m from previous	report,
													copy of this, o system in ana	

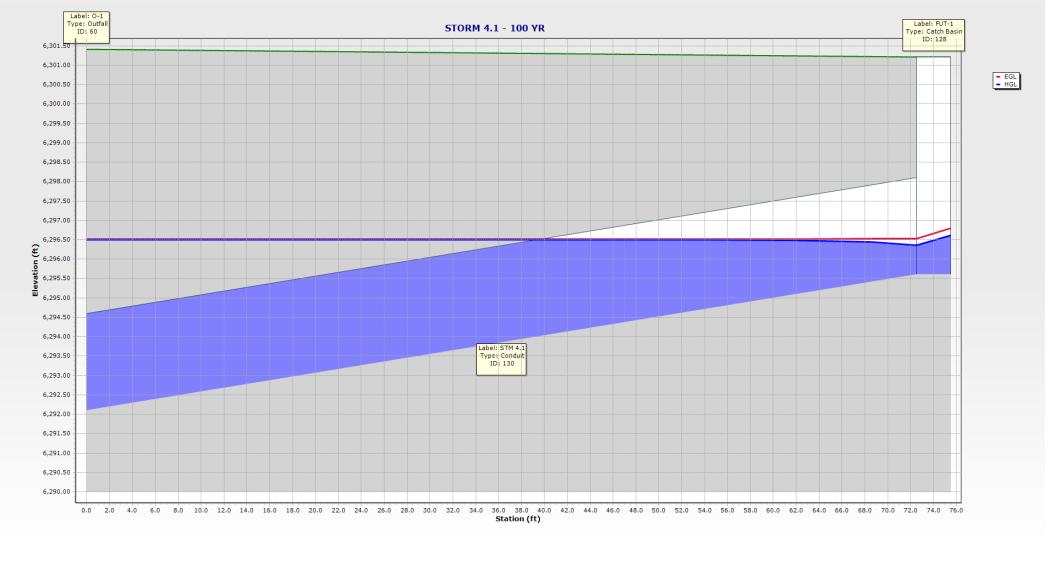
ensure whole system functions

adequately.

STORM 4.1 LAYOUT







STORM 4.1 FLEXTABLE

FlexTable: Conduit Table

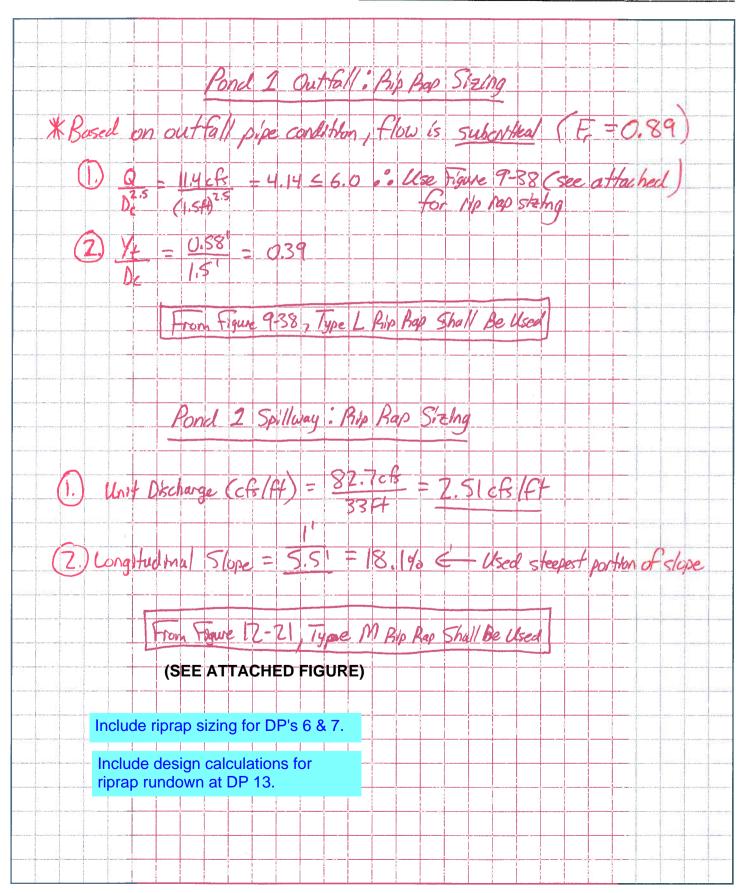
Label	ID	Upstream Structure	Flow (cfs)	Flow / Capacity (Design) (%)	Length (Unified) (ft)	Velocity (ft/s)	Froude Number (Normal)	Depth (Normal) (ft)	Depth (Critical) (ft)	Energy Grade Line (In) (ft)	Energy Grade Line (Out) (ft)	Hydraulic Grade Line (In) (ft)	Hydraulic Grade Line (Out) (ft)	Headloss (ft)
STM 4.1	130	FUT-1	4.20	4.7	74.0	9.30	3.251	0.37	0.67	6,296.53	6,296.51	6,296.35	6,296.50	-0.15
Upstream Structure Hydraulic Grade Line (In) (ft)	Upstream Structure Velocity (In- Governing) (ft/s)	Upstream Structure Headloss Coefficient	Upstream Structure Headloss (ft)	Elevation Ground (Start) (ft)	Elevation Ground (Stop) (ft)	Invert (Start) (ft)	Invert (Stop) (ft)	Conduit Description						
6,296.62	3.37	1.500	0.27	6,301.41	6,301.21	6,292.10	6,295.60	Circle - 30.0 in)	and this HOL			HGL out show match 100 yearsurface of po	ar water
									Where/How w storm? If used include copy of into model to functions prop	d from anothe or add design ensure whole	r report, pleas of that system	se		



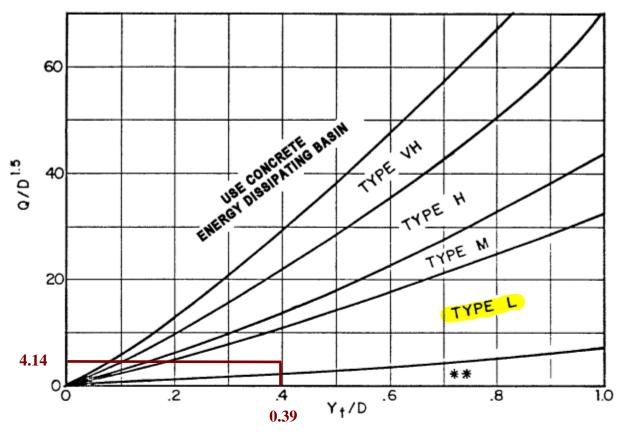


Project: CROSSROADS MIXED USE FIL. NO. 1: RIP RAP SIZING

Date: 10/15/2021



POND 1 OUTFALL: RIP RAP SIZING

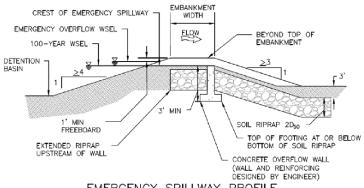


Use D_{α} instead of D whenever flow is supercritical in the barrel. **Use Type L for a distance of 3D downstream.

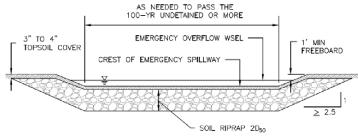
Figure 9-38. Riprap erosion protection at circular conduit outlet (valid for Q/D2.5 ≤ 6.0)

Urban Drainage and Flood Control District Urban Storm Drainage Criteria Manual Volume 2 September 2017

Chapter 12 Storage



EMERGENCY SPILLWAY PROFILE



EMERGENCY SPILLWAY SECTION AND SPILLWAY CHANNEL

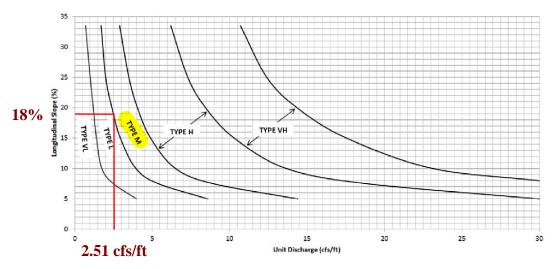
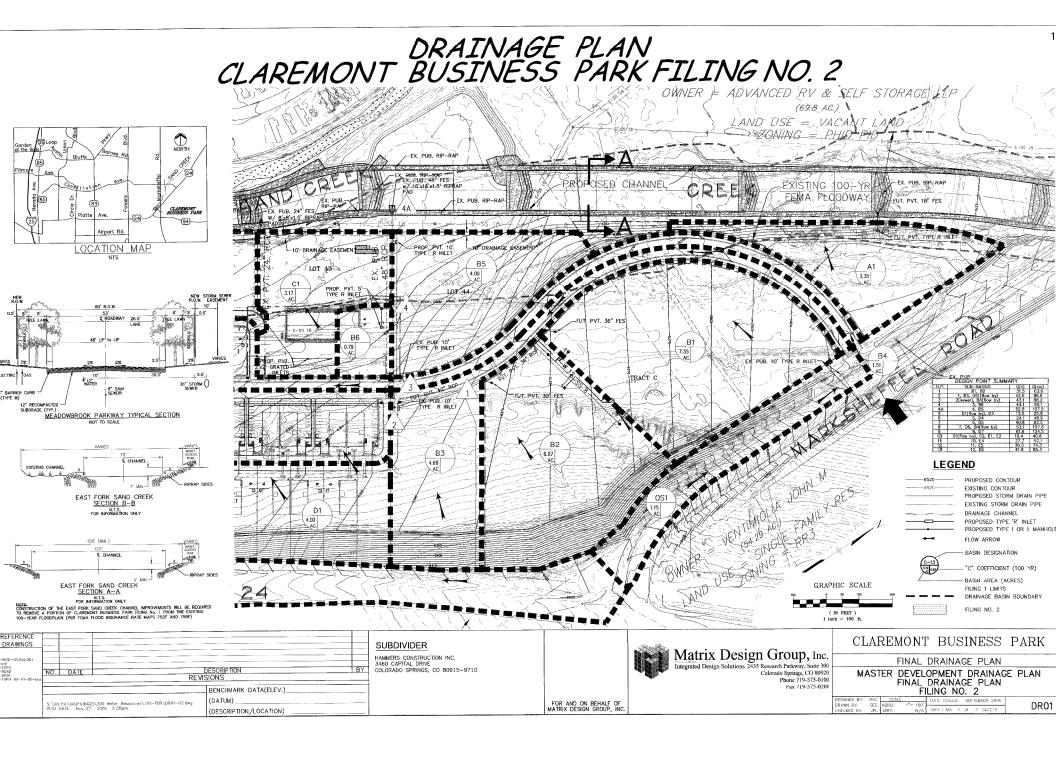
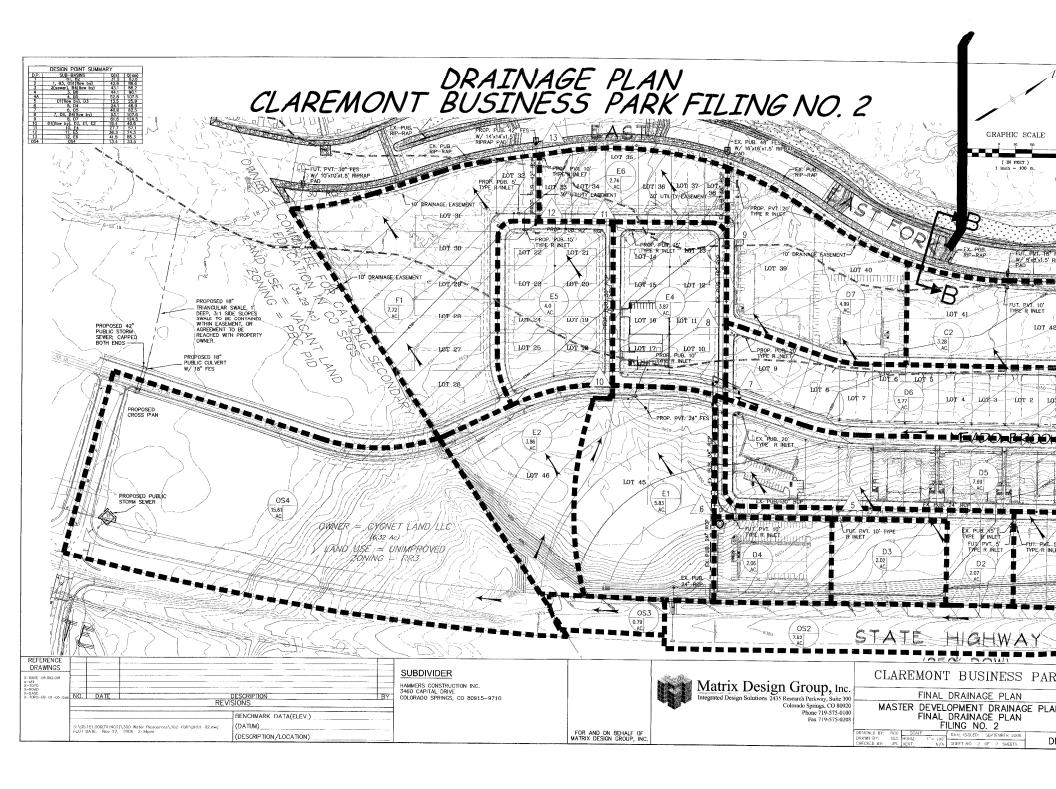


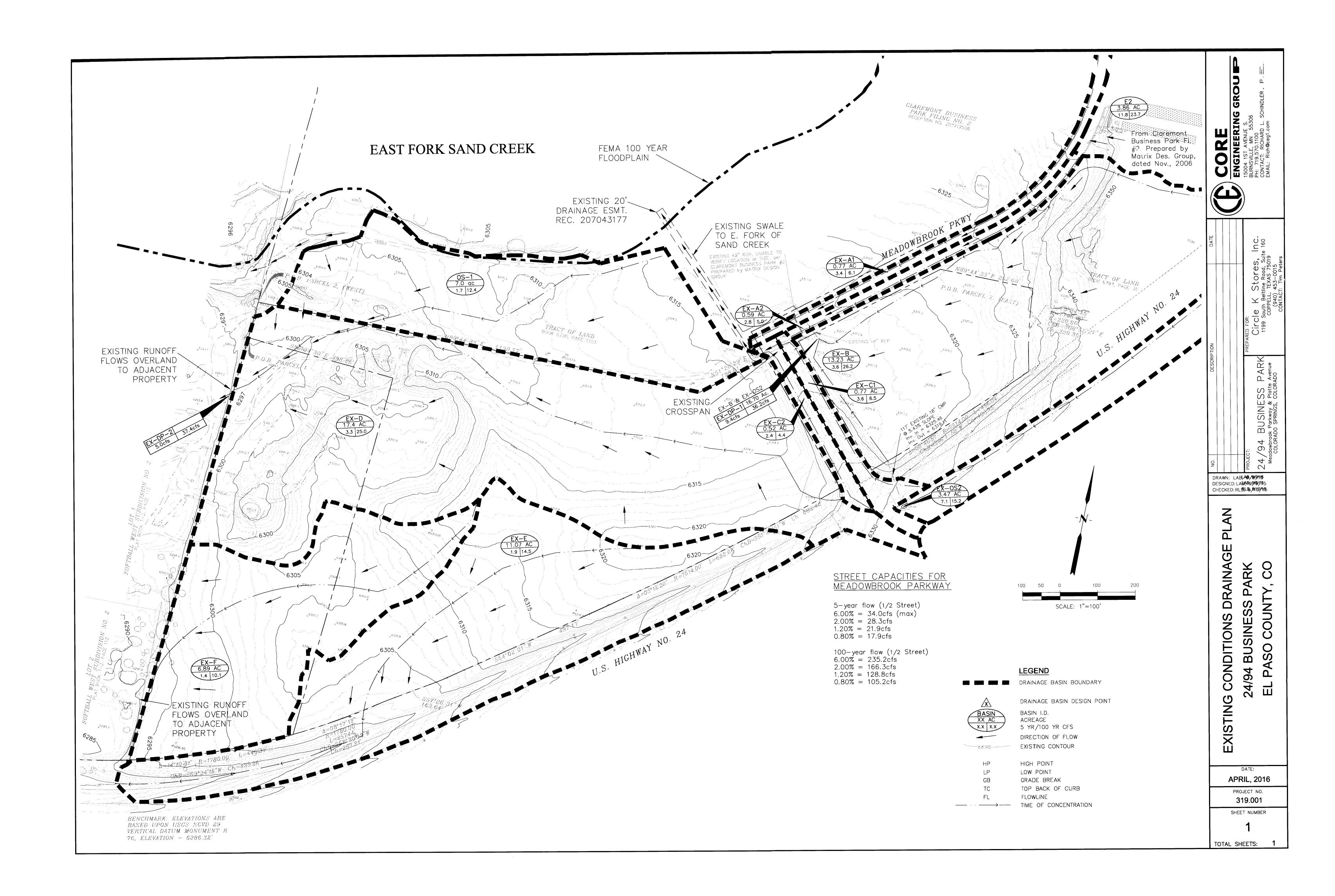
Figure 12-21. Embankment protection details and rock sizing chart (adapted from Arapahoe County)

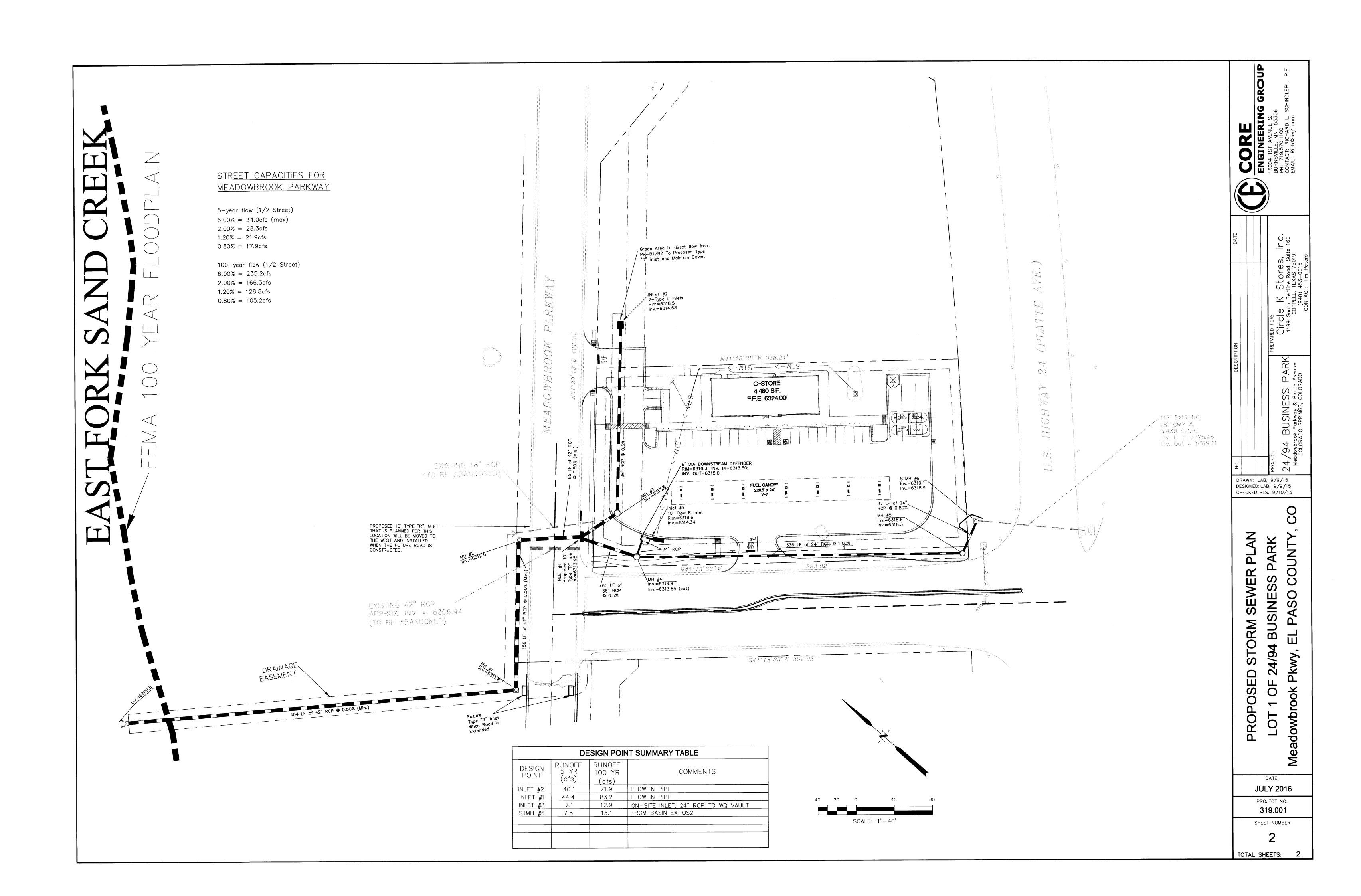
BACKGROUND

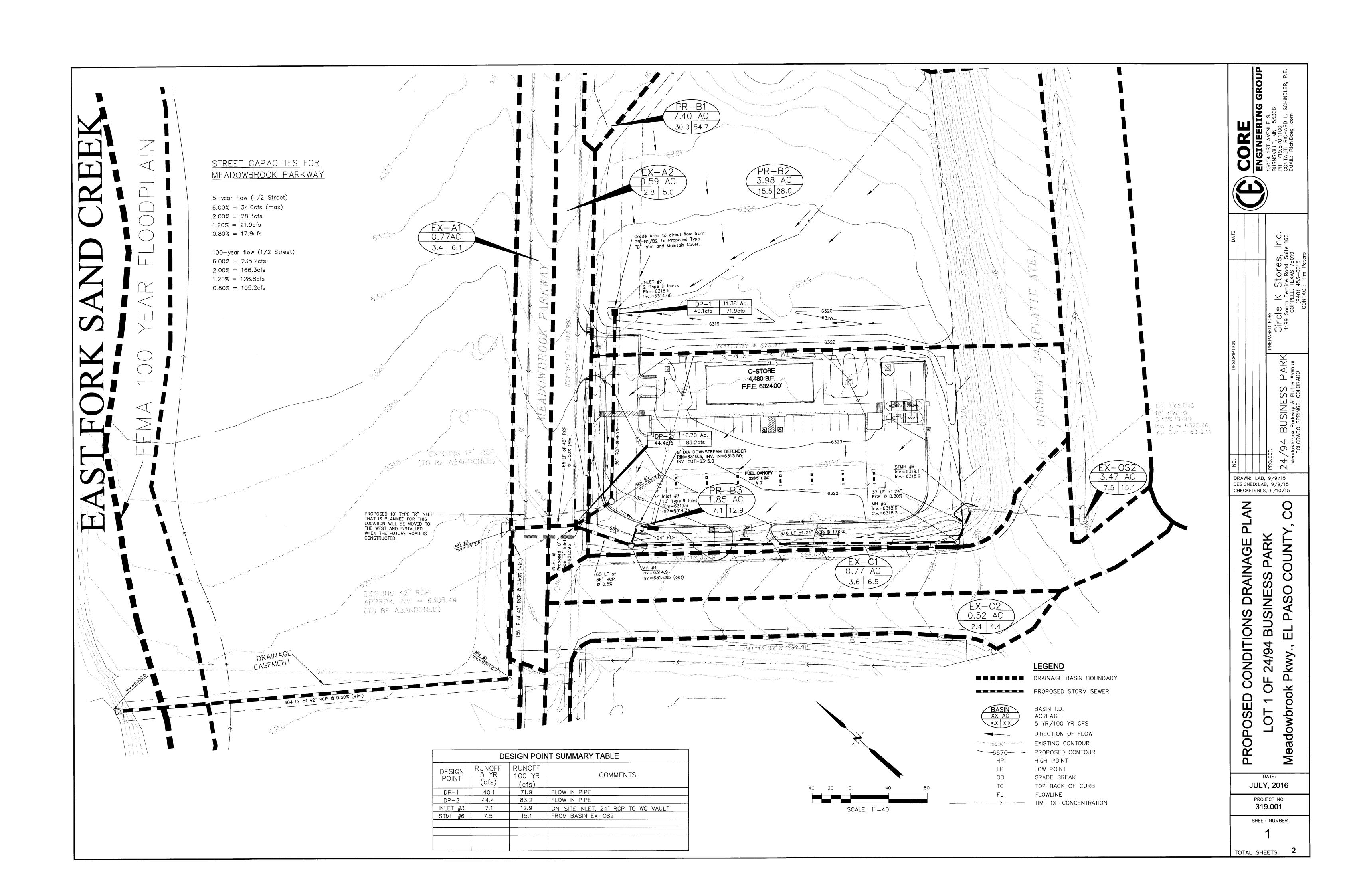
Include copy of drainage map from FDR for Aura at Crossroads, as referenced in rational spreadsheet.

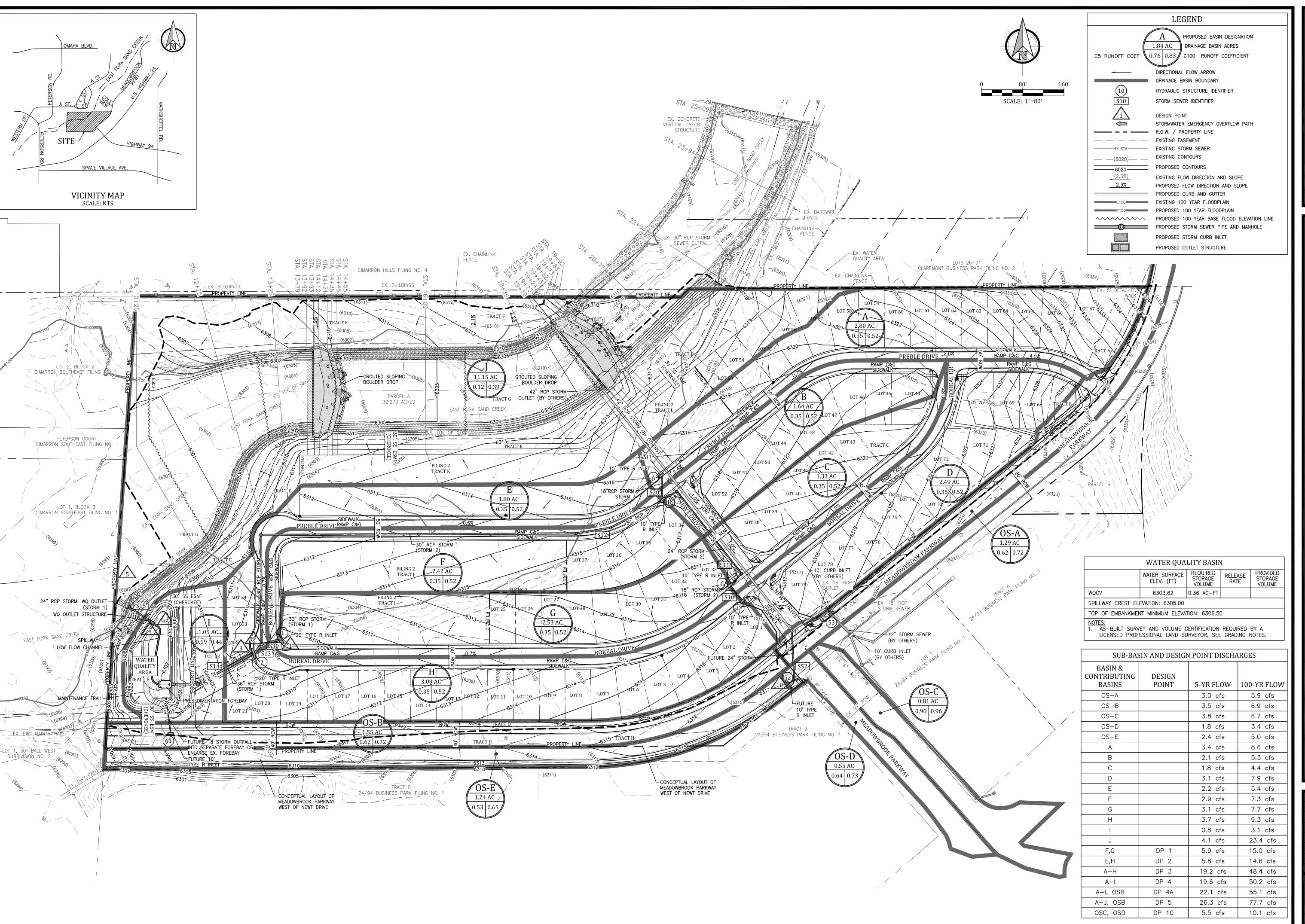


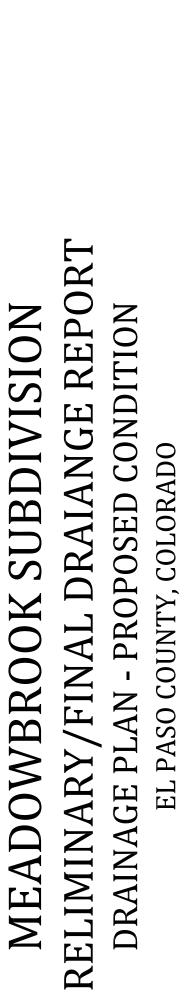












Project No.: 16039

Date: July 25, 2017

Design: ELS

Drawn: ELS

Check: MWE

Revisions:

В

DRAINAGE MAPS

