Preliminary/Final Drainage Report

Meadowbrook Park El Paso County, Colorado

PCD File No.: PUDSP208

Prepared for:

Danny Mientka Meadowbrook Development, LLC. 90 South Cascade Avenue Suite 1500 Colorado Springs, Colorado 80903

Prepared by: Kimley-Horn and Associates, Inc. 2 North Nevada Ave Suite 300 Colorado Springs, CO 80903 (719) 284-7272 Contact: John Heiberger, P.E.

Project #: 096956009

Prepared: March 18, 2021

# Kimley **»Horn**



#### CERTIFICATION

#### ENGINEERS STATEMENT

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the City/County for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.

SIGNATURE (Affix Seal):

Colorado P.E. No. 50096

Date

#### DEVELOPER'S STATEMENT

I, the developer, have read and will comply with all of the requirements specified in this drainage report and plan.

**Business Name** 

By:

Title:

Address:

#### EL PASO COUNTY STATEMENT

Filed in accordance with the requirements of the Drainage Criteria Manual, Volumes 1 and 2, El Paso County Engineering Criteria Manual and Land Development Code, as amended.

Jennifer Irving, County Engine	P.E. Date er/ECM Administrator	
Conditions:	Approval is only for the PUDSP; The report will need to be verified with the final plat and CDs. If the report needs revisions, the whole report will need to the approved again.	Kimley <b>»Horn</b>

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#### **GENERAL LOCATION AND DESCRIPTION**

#### PURPOSE AND SCOPE OF STUDY

The purpose of this Preliminary/Final Drainage Report (FDR) is to provide the hydrologic and hydraulic calculations and to document and finalize the drainage design methodology in support of the proposed Meadowbrook Park development ("the Project") for Meadowbrook Development LLC. The Project is located within the jurisdictional limits of El Paso County ("the County"). Thus, the guidelines for the hydrologic and hydraulic design components were based on the criteria outlined by the County.

#### LOCATION

The Project is located northwest of the Meadowbrook Parkway and US Highway 24 intersection in El Paso County, Colorado. More specifically, the Project is made up of Tract A 94/24 Business Park Filing No. 1, Tract I Meadowbrook Crossing Filing No. 1, and a Tract within the Claremont Business park Filing No. 2 (parcel number 5408000053) plat within the southeast quarter of Section 8, Township 14 South, Range 65 West of the 6<sup>th</sup> Principal Meridian, County of El Paso, State of Colorado. The site is bounded by Meadowbrook Parkway and the Meadowbrook Crossing Filings No. 1 and No. 2 to the west, Lot 46A Claremont Business Park Filing No. 2A, a commercial storage development to the north, US Highway 24 (CDOT Right of Way) to the east, and Lot 1 24/94 Business Park Filing No. 1, a commercial gas station to the south. A vicinity map has been provided in the Appendix of this report.



#### VICINITY MAP

Kimley **»Horn** 

#### **DESCTIPTION OF PROPERTY**

The Project is located on approximately 8.01 acres of undeveloped land with limited vegetation and grass cover. The site currently does not provide stormwater quality or detention and there are no known major drainage ways or irrigation facilities on the site. The site generally drains from the east to west with slopes ranging from 2% to 25% with the steeper slopes along the east side of the site adjacent to US Highway 24 and Lot 46A Claremont Business Park Filing No. 2A, the commercial storage facility to the north. There is an existing 30" CMP CDOT culvert that outfalls onto the site, conveying flow from the median of Hwy 24. This runoff flows across the Site to an existing storm area inlet located in the southwest corner of the Site. The Project is not adjacent to any major drainageways and does not outfall directly to any major drainageways.

NRCS soil data is available for the Site (See Appendix) and the onsite soils are USCS Hydrologic Soil Group A. Group A soils have higher infiltration rates compared to other soil groups and are generally made up of well drained, cohesive sands or gravelly sands. A Soils and Geology Study has also been prepared for the site by Rocky Mountain Group dated August 26, 2020 and is attached in the Appendix of this report for reference.

#### **PROJECT CHARACTERISTICS**

The Project is a proposed single family development that will include 67 lots. The project will include the construction of private streets, sidewalks, driveways, hardscape/landscape, and associated utility infrastructure required to serve each lot. Water quaility and detention is required for the site improvements and will be accomplished with the construction of a Full Spectrum Extended Detention Basin located in the southeast corner of the site and a water quaility Rain Garden located in the southwest corner of the Site. As part of the utility infrastructure improvements, a proposed storm sewer system will be constructed to collect runoff. Stormwater will be conveyed via overland flow across the lots, within the curb and gutter of the proposed streets before being captured in proposed storm inlets. The storm sewer system will then convey runoff into the Full Spectrum Extended Detention Basin before being discharged offsite. A small portion of the Site drains to curb chase that outfalls into the Rain Garden for water quality treatment, only. The Full Spectrum Extended Detention Basin will overdetain to inlcude the area flowing to the Rain Garden to provide detention volume.

#### DRAINAGE BASINS AND SUB-BASINS

#### MAJOR BASIN DESCRIPTIONS

The site is located within the Sand Creek Drainage Basin Study (DBPS). It is not directly adjacent to East Fork Sand Creek, but East Fork Sand Creek is the ultimate receiving water for the discharge from this Site. The Sand Creek DBPS calls for bank stabilization improvements and two drop structures which were constructed with the Meadowbrook Crossing Filings No. 1 and No. 2 developments. No additional creek improvements are included with the development of this Project.

The Site is also located outside the 100-year floodplain and within Zone X (an area of minimal flood hazard) as noted on the FEMA FIRM Map No. 08041C0752G revised on December 7, 2018 (See Appendix).

There are no identified nearby irrigation facilities or other obstructions which could influence the local drainage, other than the CDOT off-site flow from the 30" CMP culvert previously mentioned.

#### SUB-BASIN DESCRIPTION

#### **Historic Drainage Patterns**

The existing runoff onsite generally drains from east to west and is collected by an existing storm area inlet located in the southwest corner of the site. The runoff is then conveyed via storm sewer through the neighboring site to the southwest before discharging into the County storm sewer system within Meadowbrook Parkway. Runoff from offsite enters to the east of the site from US Highway 24 and drains to the same inlet as the onsite runoff in the southeast corner.

The existing drainage is divided into three sub-basins, Basin EX-A, EX-B, and EX-C. Sub-Basin EX-A is approximately 8.18 acres on consists of most of the on-site area within the property line. Runoff generated from this Sub-Basin drains overland from east to west towards the existing storm area inlet. The weighted imperviousness for Sub-Basin EX-A with existing conditions is 2% and the runoff for the 5-year and 100-year storm events are 2.49 cfs and 16.70 cfs respectively.

#### **Off-Site Drainage Flow Patterns**

Sub-Basin EX-B is approximately 1.34 acres and consists of the area within the CDOT Right of Way, downstream of the existing 30" CMP culvert and area inlet within the median. It comprises of the west portion of US Highway 24 (US-24) travel lanes, shoulder and existing 4:1 slope down to Site. The flows generated from the east portion of US-24 and within the median flow south to another area inlet and culvert away from the project area. The weighted imperviousness for Sub-Basin EX-A with existing conditions is 51.1% and the runoff for the 5-year and 100-year storm events are 3.01 cfs and 6.73 cfs respectively.

Sub-Basin EX-C is approximately 3.87 acres and consists of the area within the CDOT Right of Way upstream of the existing 30" CMP culvert and area inlet within the median. It comprises of runoff generated from all four travel lanes on US-24 and runoff generated within the existing median. Runoff is either conveyed overland onto the Site or through an existing area inlet within the median and then into a 30" CMP culvert. The culvert outfalls onto the Site and flows overland to the southwest corner to the existing storm area inlet. The weighted imperviousness for Sub-Basin EX-C with existing conditions is 54.0%% and the runoff for the 5-year and 100-year storm events are 7.71 cfs and 16.89 cfs respectively.

#### DRAINAGE DESIGN CRITERIA

#### DEVELOPMENT CRITERIA REFERENCE

The proposed storm facilities follow the El Paso County Drainage Criteria Manual (the

"CRITERIA"), El Paso Engineering Criteria Manual (the "ECM"), and the Mile High Flood District Urban Storm Drainage Criteria Manual (the "MANUAL"). Site drainage is not significantly impacted by such constraints as utilities or existing development. Further detail regarding onsite drainage patterns is provided in the Proposed Drainage Conditions Section.

There are previous drainage studies that include portions of the Project Site limits:

24/94 Business Park Final Drainage Report- This report completed by Core Engineering Group, LLC dated, July 14, 2016 details the existing 2- Type D inlets in the southwest corner of the Site. It also shows the storm alignment from the existing Type D inlet, across Meadowbrook Parkway and to the outfall in East Fork Sand Creek. This alignment will be the ultimate outfall for the discharge from this project. Proposed flows from the Site are less than the historic flows through the existing infrastructure shown in this drainage report.

Claremont Business Park Filing No. 2 Final Drainage Report- This report completed by Matrix Design Group, Inc. dated, November 2006. This report shows that the runoff from Lot 46A Claremont Business Park Filing No. 2A is maintained on the lot as does not generate runoff onto the Site that would be classified as off-site drainage for this Project.

Meadowbrook Crossing Filings No. 1 and No. 2 Preliminary and Final Drainage Report- This report completed by Kiowa Engineering Corporation dated, July 25, 2017 does not specifically include area on Site on the Drainage Map, but provides details about the improvements made to East Fork Sand Creek for stabilization and documents the extension of Meadowbrook Parkway f

#### HYDROLOGIC CRITERIA

The 5-year and 100-year design storm events were used in determining rainfall and runoff for the proposed drainage system per chapter 6 of the CRITERIA. Table 6-2 of the CRITERIA is the source for rainfall data for the 5-year and 100-year design storm events. Design runoff was calculated using the Rational Method for developed conditions as established in the CRITERIA and MANUAL. Runoff coefficients for the proposed development were determined using Table 6-6 of the CRITERIA by calculating weighted impervious values for each specific site basin. The detention storage requirement was calculated using Full Spectrum Detention methods as specified in the CRITERIA and MANUAL. The Full Spectrum Extended Detention Basin's outlet structure was designed to release the Water Quality Capture Volume (WQCV) in 40 hours. The Rain Garden was designed to release the WQCV in 12 hours. Based upon this approach, we feel that the drainage design provided for the Site is conservative and in keeping with the historic drainage patterns for the Site.

The proposed drainage facilities are designed in accordance with the CRITERIA and MANUAL. Floodplain identification was determined using FIRM panels by FEMA and information provided in the CRITERIA. Hydraulic calculations were computed using StormCAD for the proposed storm sewer system. Results of the hydraulic calculations are summarized in the Appendix.

#### DRAINAGE FACILITY DESIGN

#### <u>GENERAL CONCEPT</u>

#### **COMPLIANCE WITH OFF-SITE RUNOFF**

The runoff generated from US-24 currently outfalls onto the Site through an existing 30" CMP culvert. The off-site drainage basins were analyzed and found to include parts of the travel lanes, median and Right of Way. Currently, there is not a CDOT stormwater quality and detention facility that captures and treats this area. For that reason, each off-site Sub-Basin is collected in a swale parallel to US-24 roadway and within the CDOT Right of Way and conveyed to the southeast property corner of the Site. Off-site flows will be captured from the proposed swale by a proposed private CDOT Type D inlet (depressed and in series) and by-pass the property in a proposed 36" RCP storm pipe. This storm pipe runs along the southern property line within a proposed 15' private drainage easement and will connect to the existing 36" RCP storm pipe with a proposed manhole. Hydrologic and hydraulic analysis was completed to verify the capacity of the downstream facilities to handle the by-passed flows. All generated from the off-site Sub-Basins will be by-passed through the Site.

#### PROPOSED DRAINAGE PATTERNS

The developed runoff from the Project will generally be collected by means of a private storm sewer system with inlets located in the private streets (Nova View, Tenebris Point, Spatium View, Solum Grove and Lux Point) within each delineated sub-basin area. The runoff collected form each Sub-Basin A, C-J will be captured by storm inlets and conveyed through storm pipes to a Full Spectrum Extended Detention Basin located in the southeast corner of the site. The controlled stormwater will be treated, detained, and released from an outlet structure which will convey stormwater through a proposed storm pipe that runs along the southern property line with a 15' private drainage easement. Eventually the outfall pipe connects to the existing private storm sewer in the southwest corner. A portion of the site Sub-Basin B, surface drains to the southwest corner, entering a proposed rain garden through a concrete chase. The WQCV in the rain garden will be treated and released through an outlet structure and conveyed through a storm pipe to a connection in the existing private 36" RCP pipe.

The existing 36" extends long the northern property line of Lot 1 24/94 Business Park Filing No. 1, a commercial gas station to the north east corner of the lot and stubbed into an existing public 10' Type R Inlet. The inlet is used as a junction structure and runoff is conveyed through an existing public 42" RCP storm pipe across Meadowbrook Parkway and long Newt Drive until it ultimately outfalls into the East Fork Sand Creek. This is depicted in the proposed drainage map as part of the Meadowbrook Crossing Filings No. 1 and No. 2 Preliminary and Final Drainage Report

#### SPECIFIC DETAILS

The property has been divided into fourteen sub-basins, A through J and OS-A- OS-C. Subbasins A through J make up the Project on-site area and Sub-Basins OS-A -OS-C are the offsite basins consisting of runoff from US Highway 24.

The weighted imperviousness of the Site area (Sub-basins A through J) with proposed conditions is 43.3%. Cumulative runoff for the 5-year and 100-year storm events are 15.15 cfs and 34.11 cfs, respectively. The weighted imperviousness of the offsite area (Sub-basin OS-A-

OS-C) with Sub-Bains A through J on site is 46.8%. Cumulative runoff for the 5-year and 100-year storm events are 25.84 cfs and 59.19 cfs, respectively.

#### Sub-Basin A

Sub-basin A consists of approximately 2.47 acres and is the area along the eastern property line, north of the Extended Detention Basin, and captures the runoff from the back of lots on the east side of Nova View. The runoff is collected in swales along the back of the lots and is conveyed directly into a grass lined swale that conveys runoff to the Extended Detention Basin down a riprap rundown/ rock chute into a forebay (Design Point 1). Additionally, this area comprises of the areas uphill of the proposed big block retaining walls. Runoff not captured from the off-stie Sub-Basins is captured in a swale on top of the retaining walls and is conveyed towards the Extended Detention Basin down a riprap rundown/ rock chute into a forebay. Developed runoff during the 5-year and 100-year events are 2.08 cfs and 7.19 cfs respectively.

#### Sub-Basin B

#### — not shown on plans?

Sub-basin B consists of approximately 1.85 acres and is made up of a majority of the Solum Grove runoff and the lots adjacent to Solum Grove. The lots on the south side of Tenebris Point are also included within this sub-basin. This Sub-Basin is the only Sub-Basin contributing to the Rain Garden in The runoff from the lots drains into the Solum Grove and is conveyed in the curb and gutter to a curb chase (Design Point 2) in the southwest corner of the Site and it conveyed into the proposed Rain Garden. Developed runoff during the 5-year and 100-year events are 4.04 cfs and 8.86 cfs respectively.

#### Sub-Basin C

Sub-basin C consists of approximately 0.20 acres and consists of driveway runoff from six lots and the west portion of Nova View between Spatium View and Tenebris Point. The runoff from the lots drains into the Celeste Heights and is conveyed in the curb and gutter before being collected a private 5-foot curb Type R inlet (Design Point 3). Developed runoff during the 5-year and 100-year events are 0.82 cfs and 1.53 cfs respectively.

#### Sub-Basin D

Sub-basin D consists of approximately 0.87 acres and consists of Tenebris Point runoff and the lots adjacent to Tenebris Point and the tract behind the associated lots. To prevent the runoff from the Tract to drain out towards Meadowbrook Parkway, a swale will collect runoff along the west property line and convey to a small area inlet. This area inlet will connect to the 5' Type R inlet at the end of Tenebris Point (Design Point 4). The runoff from the lots drains into the Tenebris Point and is conveyed in the curb and gutter before being collected by a 5-foot curb Type R inlet at the end of the road (Design Point 4). Developed runoff during the 5-year and 100-year events are 1.43 cfs and 3.43 cfs respectively.

#### Sub-Basin E

Sub-basin E consists of approximately 0.42 acres and consists of the eastern half of the Nova View from Tenebris Point to Lux Point and the adjacent driveway sections. The runoff flows along Nova View and is conveyed in the curb and gutter before being collected by a 5-foot Type R inlet (Design Point 5). Developed runoff during the 5-year and 100-year events are 1.38 cfs and 2.70 cfs respectively.



#### Sub-Basin F

Sub-basin F consists of approximately 0.10 acres and consists of the southern half of Spatium View. The runoff from Spatium View and is conveyed in the curb and gutter before being collected by a 5-foot curb Type R inlet (Design Point 6). Developed runoff during the 5-year and 100-year events are 0.44 cfs and 0.80 cfs respectively.

#### Sub-Basin G

Sub-basin G consists of approximately 0.92 acres and consists of the northern half of Spatium View, the adjacent tract, and the western half of Nova View from Spatium View to Lux Point. The runoff from the lots and driveways drain into Spatium View and Nova View and is conveyed in the curb and gutter before being collected by a 5-foot curb Type R inlet (Design Point 7). To prevent the runoff from the Tract to drain out towards Meadowbrook Parkway, a swale will collect runoff along the west property line and convey to a small area inlet. This area inlet will connect to the 5' Type R inlet withing Spatium View (Design Point 7). Developed runoff during the 5-year and 100-year events are 1.72 cfs and 4.02 cfs respectively.

#### Sub-Basin H

Sub-basin H consists of approximately 0.83 acres and consists of Lux Point and the adjacent driveways to the west and entire lots to the east. The runoff from the lots drains into Lux Point and is conveyed in the curb and gutter before being collected by a 5-foot curb Type R inlet (Design Point 8). Developed runoff during the 5-year and 100-year events are 1.66 cfs and 3.85 cfs respectively.

#### Sub-Basin I

Sub-basin I consists of approximately 0.28 acres and consists of the western half of Nova view north of Lux Point. It also included the driveways directly adjacent to the west. The runoff from the driveways drains into Nova View and is conveyed in the curb and gutter and collected by a 5-foot curb Type R inlet (Design Point 9). Developed runoff during the 5-year and 100-year events are 0.82 cfs and 1.73 cfs respectively.

#### Sub-Basin J

Sub-basin J consists of approximately 0.23 acres and consists of the eastern half of Nova View north of Lux Point. It also included the driveways directly adjacent to the east. The runoff from the driveways drains into Nova View and is conveyed in the curb and gutter and is collected by a 5-foot curb Type R inlet (Design Point 10). Developed runoff during the 5-year and 100-year events are 0.77 cfs and 1.54 cfs respectively.

#### Sub-Basin OS-A

Sub-basin OS-A consists of approximately 1.77 acres and consists of the eastern half of US 24 (both travel lanes, shoulder and Right of Way) upstream and north of the existing CDOT 30" CMP culvert. Runoff from this Sub-Basin is conveyed in an already existing roadside ditch that converges with the outfall of the CMP culvert at Design Point 11. From Design Point 11 the flows will be routed through a proposed swale on CDOT Right of Way parallel to the property line and will eventually be captured into a Type D inlet and by-passed through the Site in a 36"



RCP storm pipe. Developed runoff during the 5-year and 100-year events are 3.76 cfs and 8.14 cfs respectively.

#### Sub-Basin OS-B

Sub-basin OS-B consists of approximately 1.34 acres and consists of the eastern half of US 24 (both travel lanes, shoulder and Right of Way) downstream and south of the existing CDOT 30" CMP culvert. Runoff from this Sub-Basin be captured and routed through a proposed swale on CDOT Right of Way parallel to the property line and will eventually be captured into a Type D inlet and by-passed through the Site in a 36" RCP storm pipe. Developed runoff during the 5-year and 100-year events are 3.01 cfs and 6.73 cfs respectively.

#### Sub-Basin OS-C

Sub-basin OS-C consists of approximately 2.10 acres and consists of the western half of US 24 (both travel lanes and vegetated median) upstream and north of the existing CDOT 30" CMP culvert. Runoff from this Sub-Basin is collected in the already existing swale within the roadway median and is conveyed through the 30" CMP culvert to Design Point 11. From Design Point 11 the flows will be routed through a proposed swale on CDOT Right of Way parallel to the property line and will eventually be captured into a Type D inlet and by-passed through the Site in a 36" RCP storm pipe. Developed runoff during the 5-year and 100-year events are 3.92 cfs and 8.67 cfs respectively.

#### EMERGENCY OVERFLOW ROUTING

Emergency overflow routing consists of flows following the proposed drainage pattern of northeast to southwest along the proposed roadways. Once the flows reach the southwest portion of the site, they will flow through the access driveway to Meadowbrook Parkway for Lot 1 24/94 Business Park Filing No. 1.

#### **DETENTION AND WATER QUALITY**

The WQCV and 100-year detention is required for this Project. This is accomplished through the proposed private Full Spectrum Extended Detention Basin on the southeast corner of the Site and a private Rain Garden on the southwest corner of the Site. The Extended Detention Basin was sized to provide detention for the entire Site (Sub-Basins A-J) per UDFCD criteria. WQCV will be provided in the Extended Detention Basin for Sub-Basins A, C-J only. WQCV for Sub-Basin B will be provided by the Rain Garden. The water quality and detention calculations are provided in the Appendix of this report. The proposed Extended Detention Basin and Rain Garden will be maintained by the Owner

- (Meadowbrook Park HOA)

#### Four-Step Process

The four-step process per the MANUAL provides guidance and requirements for the selection of siting of structural Construction Control Measures (CCMs) for new development and significant redevelopment.

#### Step 1: Employ Runoff Reduction Practices

Currently the site is vacant undeveloped land with surrounding development. Development of the site will increase current runoff conditions due to increased imperviousness values. However, implementation the of landscaping throughout the site, the proposed storm sewer



infrastructure, and the proposed Extended Detention Basin will help slow runoff and encourage infiltration.

#### Step 2: Provide Water Quality Capture Volume (WQCV)

The water quality capture volume will be detained using Full Spectrum Extended Detention Basin on the southeast corner of the Site and a Rain Garden on the southwest corner of the Site. The outfall pipes from the water quality outlet structures will control the release of stormwater to less than historic rates.

#### Step 3: Stabilize Drainageways

There are no current drainageways conveyed through this property. No improvements to stabilize drainageways are a part of this Project.

#### Step 4: Consider need for Industrial and Commercial BMPs

Erosion control features for the final stages of the Project will be designed to reduce contamination. Source control BMPs will include the use of, inlet protection, silt fences, concrete washout areas, stockpile management, and stabilized staging areas. The Grading and Erosion Control Plans will be submitted as a separate construction document set.

#### **Detention and Water Quality Design**

The proposed private Full Spectrum Extended Detention Basin is designed with an outlet structure that is fitted with an orifice plat and restrictor plate to release the WQCV in a 40-hour time period per the MANUAL. The proposed private Rain Garden is designed with an outlet structure that is fitted with a restrictor plate to release the WQCV in a 12-hour time period per the MANUAL.

Calculations included in the Appendix provide details regarding the private water quality and detention basins design. The calculations include determination of the storage volumes required for full spectrum detention for the WQCV and 100 year detention and allowable release rates.

Overall, 0.101 acre-feet of WQCV is required for Sub-Basins A, C-J, and 0.648 acre-feet of detention volume is required for the proposed Extended Detention Basin (Sub-Basins A-J). The total area contributing to the Extended Detention Basin consists of 8.17 acres (43.3% imperviousness). The outlet structure and orifice releases approximately 0.1 cfs in the 5-year event and 5.5 cfs in the 100-year event. This is less than the historic flows of 2.49 cfs in the 5-year event and 16.70 cfs in the 100-year event.

The WQCV requirement for Sub-Basin B (1.85 acres and 54.5% imperiousness), is 1,176 cubic feet and is provided by a Rain Garden with this a 1,215 Square Foot bottom and 12" WQCV depth. See the Appendix for calculations.

#### **Outlet Requirements**

The water quality standards established by the CRITERIA are met by the proposed Full Spectrum Extended Detention Basin and Rain Garden. The water quality outlet structures were designed per the specifications in the CRITERIA. The outlet structure for the Extended Detention Basin meets the micro-pool requirement that it be integrated into the design of the structure with an additional initial surcharge volume. The orifice plates of the structures were designed based on the CRITERIA. The orifice plates will allow the WQCV to be drained from the structure in 40 hours for the Extended Detention Basin and 12 hours for the Rain Garden. The calculations for the design of the outlet structures are presented in the Appendix.



#### Channel Design and Soil Erodibility

A proposed concrete lined trickle channel within the basin was designed per the MANUAL. A forebay structure is located at both upstream entrances to the Extended Detention Base. The forebay structures were designed per the MANUAL. The surrounding protection is designed as Type L riprap. Calculations detailing the design and dimensions of the trickle channel and forebay structure are included in the Appendix. Additionally, a riprap rundown or rock chute is provided to stabilize the flows coming from swales and entering the Extended Detention Basin. Calculations for the rock chute are included in the Appendix.

#### **Emergency Spillway Path**

The emergency overflow from the Extended Detention Basin is designed to spill over the sidewalk and curb and gutter into Solum Grove and run west towards the access to Lot 1 24/94 Business Park Filing No. 1. Calculations are provided in the Appendix, showing that the flow from the emergency spillway will not overtop the curb in the 500-year event.

#### COST OF PROPOSED DRAINAGE FACILITIES

An Opinion of Probable Construction Cost (OPCC) is provided in the Appendix of the report. There are no public drainage facilities. All improvements with this Project will be private.

#### DRAINAGE AND BRIDGE FEES

All portions of the Site were previously platted and no drainage or bridge fees are due with this project.

#### OTHER GOVERNMENT AGENCY REQUIREMENTS

Approval from other agencies such as the FEMA, the Army Corps of Engineers, Colorado State Engineer, Colorado Water Conservation Board, and others are not needed with this Project.

#### SUMMARY

#### **COMPLIANCE WITH STANDARDS**

The drainage design presented within this report for Meadowbrook Park, conforms to the El Paso County Drainage Criteria Manual and the Mile High Flood District Urban Storm Drainage Criteria Manual. Additionally, the Site runoff and storm drain facilities will not adversely affect the downstream and surrounding developments. The proposed developed flows entering the Extended Detention Basin and are greater than the existing ultimate outfall of the site due to the greater imperviousness of the site, however the implementation of the drainage basins will disperse the flow of an extended period of time therefore releasing at equal to or less than the historic rate.

Replace the "Erosion Control Plan" and "Maintenance and Operations" sections. Mention the O&M manual that will be required. This is not the case. If part of the site has been platted (Plat #14112) and fees deferred, the proportionate fee amount can remain deferred if credits have been finalized. Verify and provide in report.

Sondaux Pre-Credits No Cash | Drainace Free Diving ainage Fee: \$154,143,00 Pre-Credit School Fee: Bridge Fee: \$ 44,694.00 Theachaid Urban Park Fi Regional Park Fee: Area 2 5 32, 15300

PCD File No. SF-17-002

#### REFERENCES

- 1. City of Colorado Springs Drainage Criteria Manual, May 2014.
- 2. El Paso County Drainage Criteria Manual, Vol. 1 and 2, October 1994.
- 3. Urban Drainage and Flood Control District Drainage Criteria Manual (UDFCDCM), Vol. 1, prepared by Wright-McLaughlin Engineers, June 2001, with latest revisions.
- 4. Flood Insurance Rate Map, El Paso County, Colorado and Incorporated Areas, Map Number 08041C0459G, Effective Date December 7, 2018, prepared by the Federal Emergency Management Agency (FEMA).

### APPENDIX

SOILS MAP AND FEMA FIRM PANEL

#### NOTES TO USERS

This map is for use in administering the National Flood Insurance Program. It does not necessarily identify all areas subject to flooding, particularly from local drainage sources of small size. The community map repository should be consulted fo possible updated or additional flood hazard information.

To obtain more detailed information in areas where **Base Flood Elevations** (BFEs) and/or **floodways** have been determined, users are encouraged to consult the Flood Profiles and Poodway Data and/or Summary of Silliwater Elevations tables contained within the Flood Insurance Study (FIS) report that accompanies this FIRM. Users should be aware that BFEs are intended for flood insurance rating purposes only and should not used as the solver of flood elevation information. Accordingly, flood devation data presented in the FIS report should be utilized in conjunction with the FIRM for purposes of construction and/or floodplain management.

Coastal Base Flood Elevations shown on this map apply only landward of 0.0' North American Vertical Datum of 1988 (NAVD88). Users of this FIRM should be aware that coastal food elevations are also provided in the Summary of Stillweter Elevations table in the Flood Insurance Study report for this jurisdiction. Elevations shown in the Summary of Stillwater Elevations table should be used for construction and/or floodplain management purposes when they are higher than the elevations shown on this FIRM.

Boundaries of the **floodways** were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations with regard to requirements of the National Flood Insurance Program. Floodway widths and other pertinent floodway data are provided in the Flood Insurance Study report for this jurisdiction.

Certain areas not in Special Flood Hazard Areas may be protected by **flood control** structures. Refer to section 2.4 "Flood Protection Measures" of the Flood Insurance Study report for information on flood control structures for this jurisdiction.

The projection used in the preparation of this map was Universal Transverse Mercator (UTM) zone 13. The horizontal datum was NADB3, GRS60 spheroid. Differences in datum, spheroid, projection or UTM zones zones used in the production of FIRMs for adjacent jurisdictions may result in slight positional differences in map features across jurisdiction boundaries. These differences do not affect the accuracy of this FIRM.

Flood elevations on this map are referenced to the North American Vertical Datum of 1988 (NAVD88). These flood elevations must be compared to structure and ground elevations referenced to the same vertical datum. For information regarding conversion between the National Geodetic Vertical Datum of 1929 and the North American Vertical Datum of 1988, visit the National Geodetic Survey website at http://www.ngs.noaa.gov/ or contact the National Geodetic Survey at the following address:

NGS Information Services NOAA, N/NGS12 National Geodetic Survey SSMC-3, #9202 1315 East-West Highway Silver Spring, MD 20910-3282

To obtain current elevation, description, and/or location information for **bench marks** shown on this map, please contact the Information Services Branch of the National Geodetic Survey at (301) 713-3242 or visit its website at http://www.ngs.noaa.gov/.

Base Map information shown on this FIRM was provided in digital format by EI Paso County, Colorado Springs Utilities, City of Fountain, Bureau of Land Management, National Oceanic and Atmospheric Administration, United States Geological Survey, and Anderson Consulting Engineers, Inc. These data are current as of 2006.

This map reflects more detailed and up-to-date stream channel configurations and floodplain delineations than those shown on the previous FRM for this jurisdiction. The floodplain additional floodways that were transferred from the previous FRM may have been adjusted to conform to these new stream channel configurations. As a result, the Flood Profiles and Floodway Data tables in the Flood Insurance Study Report (which contains authoritative hydraulic data) may reflect stream channel distances that differ from what is shown on this map. The profile baselines depicted on this map represent the hydraulic modeling baselines that match the flood profiles and Floodway Data Tables if applicable, in the FIS report. As a result, the profile baselines may deviate significantly from the new base map channel representation and may appear outside of the floodplain.

Corporate limits shown on this map are based on the best data available at the time of publication. Because changes due to annexations or de-annexations may have occurred after this map was published, map users should contact appropriate community officials to verify current corporate limit locations.

Please refer to the separately printed **Map Index** for an overview map of the county showing the layout of map panels; community map repository addresses; and a Listing of Communities table containing National Flood Insurance Program dates for each community as well as a listing of the panels on which each community is located.

Contact FEMA Map Service Center (MSC) via the FEMA Map Information eXchange (FMX) 1-877-336-2627 for information on available products associated with this FIRM. Available products may include previously issued Letters of Map Change, a Flood Insurance Study Report, and/or digital versions of this map. The MSC may also be reached by Fax at 1-800-356-9620 and its website at http://www.msc.fema.gov/.

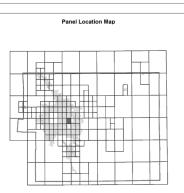
If you have **questions about this map** or questions concerning the National Flooc Insurance Program in general, please call **1-877-FEMA MAP** (1-877-336-2627) or visit the FEMA website at http://www.fema.gov/business/inflp.

El Paso County Vertical Datum Offset Table Vertical Datum ding Source Offset (ft)

 
 Vertical Datum

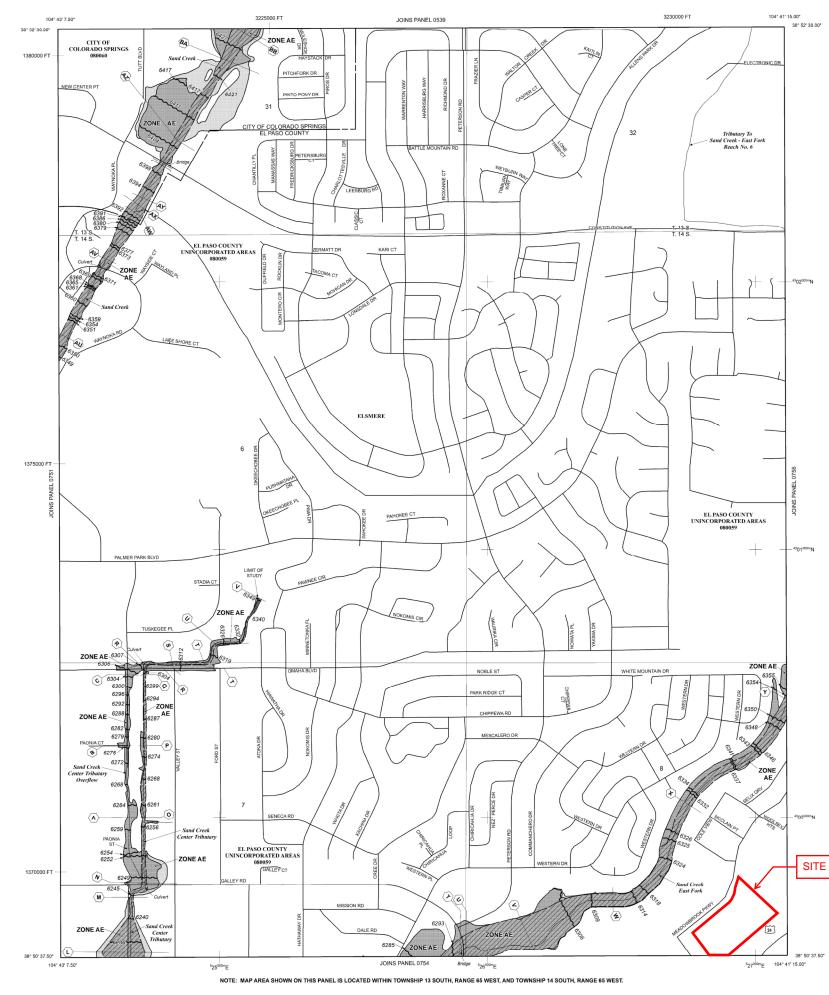
 Flooding Source
 Offset (ft)

 REFER TO SECTION 3.3 OF THE EL PASO COUNTY FLOOD INSURANCE STUDY FOR STREAM BY STREAM VERTICAL DATUM CONVERSION INFORMATION



This Digital Flood Insurance Rate Map (DFIRM) was produced through a Cooperating Technical Partner (CTP) agreement between the State of Colorado Water Conservation Board (CWCB) and the Federal Emergency Management Agency (FEMA).

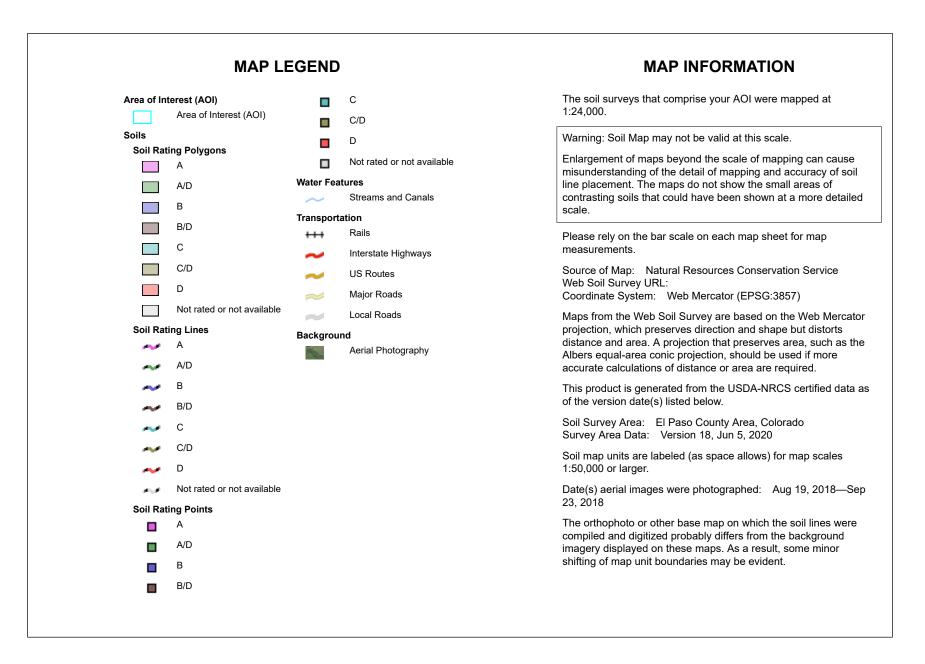
Additional Flood Hazard information and resources are available from local communities and the Colorado Water Conservation Board.



				LEGEND
		SPECIAL FL	LOOD	HAZARD AREAS (SFHAS) SUBJECT TO THE 1% ANNUAL CHANCE FLOOD
	The 1% annual	I chance flood	(100-ye	ar flood), also known as the base flood, is the flood ed or exceeded in any given year. The Special Flood
	Hazard Area is Special Flood H	the area subjection and include a	ject to Zones A	flooding by the 1% annual chance flood. Areas of A.E. AH, AO, AR, A99, V, and VE. The Base Flood
	Elevation is the	water-surface No Base Flood	elevatio	n of the 1% annual chance flood.
	ZONE AE	Base Flood Elev	vations	
		Elevations dete	ermined.	feet (usually sheet flow on sloping terrain); average
		depths determ determined.	nined.	For areas of alluvial fan flooding, velocities also
		flood by a floo	od contr	area Formerly protected from the 1% annual chance of system that was subsequently decertified. Zone former flood control system is being restored to
	ZONE A99	provide protect Area to be pro	tion from rotected	n the 1% annual chance or greater flood. from 1% annual chance flood by a Federal flood
		protection sys determined.	stem u	inder construction; no Base Flood Elevations
		Elevations dete	ermined.	ith velocity hazard (wave action); no Base Flood with velocity hazard (wave action); Base Flood
		Elevations dete	ermined.	
				S IN ZONE AE
	kept free of er substantial incr	ncroachment so	o that t	am plus any adjacent floodplain areas that must be ne 1% annual chance flood can be carried without
		OTHER FLO	IOD AR	EAS
	ZONE X	Areas of 0.2% average depth	annual	chance flood; areas of 1% annual chance flood with s than 1 foot or with drainage areas less than 1
				s than 1 foot or with drainage areas less than 1 protected by levees from 1% annual chance flood.
		OTHER ARE		
				e outside the 0.2% annual chance floodplain. izards are undetermined, but possible.
				R RESOURCES SYSTEM (CBRS) AREAS
				ECTED AREAS (OPAs)
	<u> </u>			cated within or adjacent to Special Flood Hazard Areas.
				boundary
			one D B	
	•••••			OPA boundary
		BC Fli	loundary lood Elev	dividing Special Flood Hazard Areas of different Base rations, flood depths or flood velocities.
	513 - (EL 987)	Ba	ase Floo	d Elevation line and value; elevation in feet* d Elevation value where uniform within zone;
		el	levation	
	_	$\frown$	ross sec	
	23	_	ransect	ine
	97° 07' 30.0 32° 22' 30.0	10" Ge	ieograph	ic coordinates referenced to the North American
	32° 22' 30.0 4275 <sup>000</sup> "N	10	000-met	1983 (NAD 83) er Universal Transverse Mercator grid ticks,
		20	one 13	
	6000000 F	i 50 sy La	ouu-foot ystem, c ambert (	grid ticks: Colorado State Plane coordinate entral zone (FIPSZONE 0502), Conformal Conic Projection
	DX5510	Be		rk (see explanation in Notes to Users section of
	M1.5	- u	iver Mile	
	•	N		IAP REPOSITORIES
			fer to Ma	p Repositories list on Map Index
		E	FLOO	VE DATE OF COUNTYWIDE DINSURANCE RATE MAP MARCH 17, 1997
	DECEMBE	EFFECTIV ER 7, 2018 - to	VE DATE	(S) OF REVISION(S) TO THIS PANEL corporate limits, to change Base Flood Elevations and date map format, to add roads and road names, and to
	Special Flor	od Hazard Area incorpora	as, to up ate previ	date map format, to add roads and road names, and to ously issued Letters of Map Revision.
	For community Map History Tal	map revision h ble located in ti	history p the Floor	rior to countywide mapping, refer to the Community Insurance Study report for this jurisdiction.
	To determine i	if flood insuran	nce is a	vailable in this community, contact your insurance
	agent or call th	e maulonal Floo	JU INSUR	ince Program at 1-800-638-6620.
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USDA Natural Resources Conservation Service Web Soil Survey National Cooperative Soil Survey



## Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
8	Blakeland loamy sand, 1 to 9 percent slopes	A	7.4	100.0%
Totals for Area of Intere	st		7.4	100.0%

## Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

## **Rating Options**

Aggregation Method: Dominant Condition Component Percent Cutoff: None Specified

USDA

Tie-break Rule: Higher

**EXISTING HYDROLOGIC CALCULATIONS** 

Meadowbrook Drainage Report El Paso County, CO

**IDF Equations:** 

I <sub>100</sub> = -2.52In(D) + 12.735
I₅₀ = -2.25In(D) + 11.375
I <sub>25</sub> -2.00In(D) + 10.111
I₁₀ -1.75In(D) + 8.847
l₅ -1.50ln(D) + 7.583
l₂ -1.19In(D) + 6.035

#### Where:

I = Rainfall Intensity (in/hr)

D= Duration (minutes)

	<u>2-yr</u>	<u>5-yr</u>	<u>10-yr</u>	<u>100-yr</u>
P1 =	1.19	1.5	1.75	2.52

Time Intensity Frequency Tabulation

			7 1	,		
Time	2 YR	5 YR	10 YR	25 YR	50 YR	100 YR
5	4.12	5.17	6.03	6.89	7.75	8.68
10	3.29	4.13	4.82	5.51	6.19	6.93
15	2.81	3.52	4.11	4.69	5.28	5.91
30	1.99	2.48	2.89	3.31	3.72	4.16
60	1.16	1.44	1.68	1.92	2.16	2.42
120	0.34	0.40	0.47	0.54	0.60	0.67

\*The Design Point Rainfall Values and Time Intensity Frequency Tabulation are found in Table 6-2 and Figure 6-5 respectively, of the Colorado Springs Drainage Criteria Manual, Volume 1

Meadowbrook Park Drainage Report El Paso County, CO

## Weighted Imperviousness Calculations (Existing Conditions)

SU	B-	AREA	AREA	ROOF	ROOF		RO	OF		LANDSCAPE	LANDSCAPE		LAND	SCAPE		PAVEMENT	PAVEMENT		PAVE	MENT		WEIGHTED		WEIGHTED	OCOEFFICIEN	ITS
BAS	IN	(SF)	(Acres)	AREA	IMPERVIOUSNESS	C2	C5	C10	C100	AREA	IMPERVIOUSNESS	C2	C5	C10	C100	AREA	IMPERVIOUSNESS	C2	C5	C10	C100	IMPERVIOUSNESS	C2	C5	C10	C100
EX	Α	356,327	8.18	0	90%	0.71	0.73	0.75	0.81	356,327	2%	0.03	0.09	0.17	0.36	0	100%	0.89	0.90	0.92	0.96	2.0%	0.03	0.09	0.17	0.36
EX	·B	58,532	1.34	0	90%	0.71	0.73	0.75	0.81	29,227	2%	0.03	0.09	0.17	0.36	29,305	100%	0.89	0.90	0.92	0.96	51.1%	0.46	0.50	0.55	0.66
EX	-C	168,766	3.87	0	<del>9</del> 0%	0.71	0.73	0.75	0.81	79,173	2%	0.03	0.09	0.17	0.36	89,593	100%	0.89	0.90	0.92	0.96	54.0%	0.49	0.52	0.57	0.68
TOT	AL	583,625	13.40	0	90%	0.71	0.73	0.75	0.81	385,554	2%	0.03	0.09	0.17	0.36	29,305	100%	0.89	0.90	0.92	0.96	6.3%	0.06	0.10	0.16	0.29

Meadow	brook Park	- Drainage	Report							Watercou	rse Coeffic	ient				
Existing F	Runoff Calcu	ilations			Forest	& Meadow	2.50	Short G	ass Pastur	e & Lawns	7.00			Grasse	d Waterway	15.00
Time of C	Concentratio	ON Fallow or Cultivation 5.00 Nearly Bare Ground 10.00 Paved Area & Shallow Gu								allow Gutter	20.0					
		SUB-BASIN			INIT	IAL / OVERL	AND	T	RAVEL TIM	E				T(c) CHECK		FINAL
	DATA					TIME			T(t)				(URE	BANIZED BA	SINS)	T(c)
DESIGN	DRAIN	AREA	AREA	C(5)	Length	Slope	T(i)	Length	Slope	Coeff.	Velocity	T(t)	COMP.	TOTAL	L/180+10	
POINT	BASIN	sq. ft.	ac.		ft.	%	min	ft.	%		fps	min.	T(c)	LENGTH		min.
1	EX-A	356,327	8.18	0.09	300	11.5%	14.2	867	2.0%	15.00	2.1	6.8	21.0	1167	16.5	16.5
2	EX-B	58,532	1.34	0.50	65	4.5%	5.4	405	3.8%	15.00	2.9	2.3	7.7	470	12.6	7.7
3	EX-C	168,766	3.87	0.52	65	4.5%	5.2	1000	2.5%	15.00	2.4	7.0	12.2	1065	15.9	12.2

Existing Ru	ook Park - Dra noff Calculatio hod Procedure)		eport		Desi	gn Storm	5 Year					
DESIGN	ASIN INFORMATIC DRAIN	AREA	RUNOFF	T(c)	DIRECT C x A	RUNOFF	Q	T(c)	UMULATI C x A	I	Q	NOTES
POINT	BASIN	ac.	COEFF	min	0.74	in/hr	cfs	min		in/hr	cfs	
1	EX-A	8.18	0.09	16.5	0.74	3.38	2.49					Existing On-Site Property (Vacant Undeveloped Land
2	EX-B	1.34	0.50	7.7	0.67	4.52	3.01					Flows from CDOT ROW, sheet flowing onto property
3	EX-C	3.87	0.52	12.2	2.01	3.83	7.71					Flows from CDOT ROW at the culvert outlet design point

Existing	vbrook Park - Dra Runoff Calculatic Method Procedure)		Report		Des	ign Storm	100 Year					
	BASIN INFORMATION	4		DIF	RECT RUN	OFF		CUMULATI	VE RUNOF	F		
DESIGN POINT	DRAIN BASIN	AREA ac.	RUNOFF COEFF	T(c) min	СхА	l in/hr	Q cfs	T(c) min	СхА	l in/hr	Q cfs	NOTES
1	EX-A	8.18	0.36	16.5	2.94	5.67	16.70					Existing On-Site Property (Vacant Undeveloped Land
2	EX-B	1.34	0.66	7.7	0.89	7.59	6.73					Flows from CDOT ROW, sheet flowing onto property
3	EX-C	3.87	0.68	12.2	2.63	6.43	16.89					Flows from CDOT ROW at the culvert outlet design point

	SUMMARY - EXISTING RUNOFF TABLE												
DESIGN POINT	BASIN DESIGNATION	BASIN AREA (ACRES)	DIRECT 5-YR RUNOFF (CFS)	DIRECT 100-YR RUNOFF (CFS)	CUMULATIVE 5-YR RUNOFF (CFS)	CUMULATIVE 100- YR RUNOFF (CFS)							
1	EX-A	8.18	2.49	16.70									
2	EX-B	1.34	3.01	6.73									
3	EX-C	3.87	7.71	16.89									
TOTAL		13.40	13.21	40.32									

PROPOSED HYDROLOGIC CALCULATIONS

Meadowbrook Drainage Report El Paso County, CO

**IDF Equations:** 

I <sub>100</sub> = -2.52In(D) + 12.735
I₅₀ = -2.25In(D) + 11.375
I <sub>25</sub> -2.00In(D) + 10.111
I₁₀ -1.75In(D) + 8.847
l₅ -1.50ln(D) + 7.583
l <sub>2</sub> -1.19ln(D) + 6.035

#### Where:

I = Rainfall Intensity (in/hr)

D= Duration (minutes)

	<u>2-yr</u>	<u>5-yr</u>	<u>10-yr</u>	<u>100-yr</u>
P1 =	1.19	1.5	1.75	2.52

Time Intensity Frequency Tabulation

			7 1	,		
Time	2 YR	5 YR	10 YR	25 YR	50 YR	100 YR
5	4.12	5.17	6.03	6.89	7.75	8.68
10	3.29	4.13	4.82	5.51	6.19	6.93
15	2.81	3.52	4.11	4.69	5.28	5.91
30	1.99	2.48	2.89	3.31	3.72	4.16
60	1.16	1.44	1.68	1.92	2.16	2.42
120	0.34	0.40	0.47	0.54	0.60	0.67

\*The Design Point Rainfall Values and Time Intensity Frequency Tabulation are found in Table 6-2 and Figure 6-5 respectively, of the Colorado Springs Drainage Criteria Manual, Volume 1

Meadowbrook Drainage Report El Paso County, CO

## Weighted Imperviousness Calculations

	AREA	AREA	ROOF	ROOF		RO	OF		LANDSCAPE	LANDSCAPE		LAND	SCAPE		PAVEMENT	PAVEMENT		PAVE	MENT		WEIGHTED		WEIGHTED	COEFFICIEN	ITS
SUB-BASIN	(SF)	(Acres)	AREA	IMPERVIOUSNESS	C2	C5	C10	C100	AREA	IMPERVIOUSNESS	C2	C5	C10	C100	AREA	IMPERVIOUSNESS	C2	C5	C10	C100	IMPERVIOUSNESS	C2	C5	C10	C100
А	107,496	2.47	21,654	90%	0.71	0.73	0.75	0.81	85,842	0%	0.03	0.09	0.17	0.36	0	100%	0.89	0.90	0.92	0.96	18.1%	0.17	0.22	0.29	0.45
В	80,559	1.85	22,073	90%	0.71	0.73	0.75	0.81	34,457	0%	0.03	0.09	0.17	0.36	24,029	100%	0.89	0.90	0.92	0.96	54.5%	0.47	0.51	0.55	0.66
С	8,878	0.20	0	90%	0.71	0.73	0.75	0.81	1,377	0%	0.03	0.09	0.17	0.36	7,501	100%	0.89	0.90	0.92	0.96	84.5%	0.76	0.77	0.80	0.87
D	38,113	0.87	10,260	90%	0.71	0.73	0.75	0.81	20,629	0%	0.03	0.09	0.17	0.36	7,224	100%	0.89	0.90	0.92	0.96	43.2%	0.38	0.42	0.47	0.59
E	18,246	0.42	0	90%	0.71	0.73	0.75	0.81	4,546	0%	0.03	0.09	0.17	0.36	13,700	100%	0.89	0.90	0.92	0.96	75.1%	0.68	0.70	0.73	0.81
F	4,229	0.10	0	90%	0.71	0.73	0.75	0.81	79	0%	0.03	0.09	0.17	0.36	4,150	100%	0.89	0.90	0.92	0.96	98.1%	0.87	0.88	0.91	0.95
G	40,228	0.92	8,808	90%	0.71	0.73	0.75	0.81	20,973	0%	0.03	0.09	0.17	0.36	10,447	100%	0.89	0.90	0.92	0.96	45.7%	0.40	0.44	0.49	0.61
Н	35, <b>9</b> 48	0.83	6,289	90%	0.71	0.73	0.75	0.81	18,616	0%	0.03	0.09	0.17	0.36	11,043	100%	0.89	0.90	0.92	0.96	46.5%	0.41	0.45	0.50	0.62
I	12,368	0.28	0	90%	0.71	0.73	0.75	0.81	5,168	0%	0.03	0.09	0.17	0.36	7,200	100%	0.89	0.90	0.92	0.96	58.2%	0.53	0.56	0.61	0.71
J	9,994	0.23	0	90%	0.71	0.73	0.75	0.81	3,127	0%	0.03	0.09	0.17	0.36	6,867	100%	0.89	0.90	0.92	0.96	68.7%	0.62	0.65	0.69	0.77
OS-A	77,099	1.77	0	90%	0.71	0.73	0.75	0.81	34,833	2%	0.03	0.09	0.17	0.36	42,266	100%	0.89	0.90	0.92	0.96	55.7%	0.50	0.53	0.58	0.69
OS-B	58,532	1.34	0	90%	0.71	0.73	0.75	0.81	29,227	2%	0.03	0.09	0.17	0.36	29,305	100%	0.89	0.90	0.92	0.96	51.1%	0.46	0.50	0.55	0.66
OS-C	91,667	2.10	0	90%	0.71	0.73	0.75	0.81	44,340	2%	0.03	0.09	0.17	0.36	47,327	100%	0.89	0.90	0.92	0.96	52.6%	0.47	0.51	0.56	0.67
TOTAL (A-J)	356,059	8.17	69,084	90%	0.71	0.73	0.75	0.81	194,814	0%	0.03	0.09	0.17	0.36	92,161	100%	0.89	0.90	0.92	0.96	43.3%	0.38	0.42	0.48	0.60
TOTAL	583,357	13.39	69084	90%	0.71	0.73	0.75	0.81	303,214	0%	0.03	0.09	0.17	0.36	211,059	100%	0.89	0.90	0.92	0.96	46.8%	0.42	0.46	0.51	0.63

Meadow	brook Park	- Drainage	Report							Watercou	irse Coeffic	ient				
Proposed	Runoff Cal	culations			Forest	& Meadow	2.50	Short G	rass Pastur	e & Lawns	7.00			Grasse	d Waterway	15.00
Time of C	Concentratio	n			Fallow or	Cultivation	5.00		Nearly Bare Ground 10.00				Paved Area & Shallow Gutter			20.00
SUB-BASIN DATA					INIT	IAL / OVERL TIME		ſ	RAVEL TIM T(t)	IE			(URI	T(c) CHECK BANIZED BA		FINAL T(c)
DESIGN POINT	DRAIN BASIN	AREA sq. ft.	AREA ac.	C(5)	Length ft.	Slope %	T(i) min	Length ft.	Slope %	Coeff.	Velocity fps	T(t) min.	COMP. T(c)	TOTAL LENGTH	L/180+10	min.
1	Α	107,496	2.47	0.22	100	15.0%	6.5	745	2.3%	15.00	2.3	5.5	12.0	845	14.7	12.0
2	В	80,559	1.85	0.51	90	2.9%	7.2	200	1.0%	20.00	2.0	1.7	8.9	290	11.6	8.9
3	С	8,878	0.20	0.77	30	1.3%	3.0	225	3.0%	20.00	3.5	1.1	5.0	255	11.4	5.0
4	D	38,113	0.87	0.42	100	3.0%	8.7	235	0.5%	20.00	1.4	2.8	11.5	335	11.9	11.5
5	E	18,246	0.42	0.70	70	2.8%	4.4	420	2.3%	20.00	3.0	2.3	6.7	490	12.7	6.7
6	F	4,229	0.10	0.88	6	2.0%	0.8	150	2.0%	20.00	2.8	0.9	5.0	156	10.9	5.0
7	G	40,228	0.92	0.44	100	3.0%	8.4	170	2.0%	20.00	2.8	1.0	9.4	270	11.5	9.4
8	Н	35,948	0.83	0.45	100	8.5%	5.8	190	0.5%	20.00	1.4	2.2	8.0	290	11.6	8.0
9	1	12,368	0.28	0.56	100	10.0%	4.6	109	2.7%	20.00	3.3	0.6	5.2	209	11.2	5.2
10	J	9,994	0.23	0.65	70	5.5%	3.9	160	2.8%	20.00	3.3	0.8	5.0	230	11.3	5.0
11	OS-A	77,099	1.77	0.53	100	4.3%	6.4	665	2.5%	15.00	2.4	4.7	11.1	765	14.3	11.1
12	OS-B	58,532	1.34	0.50	65	4.5%	5.4	405	3.8%	15.00	2.9	2.3	7.7	470	12.6	7.7
13	OS-C	91,667	2.10	0.51	65	4.5%	5.3	1035	1.9%	15.00	2.1	8.3	13.6	1100	16.1	13.6

	ook Park - Dra unoff Calculat		eport		Desi	an Storm	5 Year					
	hod Procedure)					-						
BA	SIN INFORMATIO	ON			DIRECT	RUNOFF		С	UMULATI	VE RUNO	FF	
DESIGN POINT	DRAIN BASIN	AREA ac.	RUNOFF COEFF	T(c) min	СхА	l in/hr	Q cfs	T(c) min	СхА	l in/hr	Q cfs	NOTES
1	A	2.47	0.22	12.0	0.54	3.85	2.08					
2	В	1.85	0.51	8.9	0.94	4.31	4.04					
3	С	0.20	0.77	5.0	0.16	5.17	0.82					
4	D	0.87	0.42	11.5	0.36	3.92	1.43					
5	E	0.42	0.70	6.7	0.29	4.73	1.38					
6	F	0.10	0.88	5.0	0.09	5.17	0.44					
7	G	0.92	0.44	9.4	0.41	4.22	1.72					
8	Н	0.83	0.45	8.0	0.37	4.46	1.66					
9	I	0.28	0.56	5.2	0.16	5.12	0.82					
10	J	0.23	0.65	5.0	0.15	5.17	0.77					
11	OS-A	1.77	0.53	11.1	0.95	3.98	3.76					
12	OS-B	1.34	0.50	7.7	0.67	4.52	3.01					
13	OS-C	2.10	0.51	13.6	1.07	3.66	3.92					

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Proposed	brook Park - Dr Runoff Calcula Jethod Procedure)		Report		Design Storm 100 Year												
BA	ASIN INFORMATIO	N		DIF	RECT RUN	OFF			CUMULATI	VE RUNOF	F						
DESIGN POINT	DRAIN BASIN	AREA ac.	RUNOFF COEFF	T(c) min	СхА	l in/hr	Q cfs	T(c) min	СхА	l in/hr	Q cfs	NOTES					
1	А	2.47	0.45	12.0	1.11	6.47	7.19										
2	В	1.85	0.66	8.9	1.22	7.24	8.86										
3	С	0.20	0.87	5.0	0.18	8.68	1.53										
4	D	0.87	0.59	11.5	0.52	6.59	3.43										
5	E	0.42	0.81	6.7	0.34	7.94	2.70										
6	F	0.10	0.95	5.0	0.09	8.68	0.80										
7	G	0.92	0.61	9.4	0.57	7.09	4.02										
8	Н	0.83	0.62	8.0	0.51	7.48	3.85										
9	I	0.28	0.71	5.2	0.20	8.60	1.73										
10	J	0.23	0.77	5.0	0.18	8.68	1.54										
11	OS-A	1.77	0.69	11.1	1.22	6.68	8.14										
12	OS-B	1.34	0.66	7.7	0.89	7.59	6.73										
13	OS-C	2.10	0.67	13.6	1.41	6.15	8.67										

	SUMMARY - PROPOSED RUNOFF TABLE													
DESIGN POINT	BASIN DESIGNATION	BASIN AREA (ACRES)	DIRECT 5-YR RUNOFF (CFS)	DIRECT 100-YR RUNOFF (CFS)	CUMULATIVE 5-YR RUNOFF (CFS)	CUMULATIVE 100- YR RUNOFF (CFS)								
1	А	2.47	2.08	7.19										
2	В	1.85	4.04	8.86										
3	С	0.20	0.82	1.53										
4	D	0.87	1.43	3.43										
5	E	0.42	1.38	2.70										
6	F	0.10	0.44	0.80										
7	G	0.92	1.72	4.02										
8	Н	0.83	1.66	3.85										
9	I	0.28	0.82	1.73										
10	J	0.23	0.77	1.54										
11	OS-A	1.77	3.76	8.14										
12	OS-B	1.34	3.01	6.73										
13	OS-C	2.10	3.92	8.67										
14	POND OUTFALL		0.10	5.50										
TOTAL		13.39	25.84	59.19										

HYDRAULIC CALCULATIONS

#### DETENTION BASIN STAGE-STORAGE TABLE BUILDER

Project: Meadowb	prook Park	
Basin ID:		
ZONE 3 ZONE 2 ZONE 1 ZONE 1 AND 2	100-YEAR ORIFICE	2
	ration (Retention Pond)	
ORIFICES	ORIFICE	2

#### Watershed Information

ator shou mitor mation		
Selected BMP Type =	EDB	
Watershed Area =	8.17	acres
Watershed Length =	1,090	ft
Watershed Length to Centroid =	350	ft
Watershed Slope =	0.040	ft/ft
Watershed Imperviousness =	43.30%	percent
Percentage Hydrologic Soil Group A =	100.0%	percent
Percentage Hydrologic Soil Group B =	0.0%	percent
Percentage Hydrologic Soil Groups C/D =	0.0%	percent
Target WQCV Drain Time =	40.0	hours
Location for 1-hr Rainfall Depths =	User Input	

# After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

the embedded colorado orban nyard	graphinoceuu	10.
Water Quality Capture Volume (WQCV) =	0.101	acre-feet
Excess Urban Runoff Volume (EURV) =	0.392	acre-feet
2-yr Runoff Volume (P1 = 1.19 in.) =	0.288	acre-feet
5-yr Runoff Volume (P1 = 1.5 in.) =	0.386	acre-feet
10-yr Runoff Volume (P1 = 1.75 in.) =	0.463	acre-feet
25-yr Runoff Volume (P1 = 2 in.) =	0.600	acre-feet
50-yr Runoff Volume (P1 = 2.25 in.) =	0.734	acre-feet
100-yr Runoff Volume (P1 = 2.52 in.) =	0.908	acre-feet
500-yr Runoff Volume (P1 = 3.14 in.) =	1.282	acre-feet
Approximate 2-yr Detention Volume =	0.250	acre-feet
Approximate 5-yr Detention Volume =	0.331	acre-feet
Approximate 10-yr Detention Volume =	0.406	acre-feet
Approximate 25-yr Detention Volume =	0.502	acre-feet
Approximate 50-yr Detention Volume =	0.565	acre-feet
Approximate 100-yr Detention Volume =	0.648	acre-feet

Define	Zones	and	Basin	Geometry

Define Zones and Basin Geometry		
Zone 1 Volume (WQCV) =	0.101	acre-feet
Zone 2 Volume (EURV - Zone 1) =	0.291	acre-feet
Zone 3 Volume (100-year - Zones 1 & 2) =	0.256	acre-feet
Total Detention Basin Volume =	0.648	acre-feet
Initial Surcharge Volume (ISV) =	user	ft <sup>3</sup>
Initial Surcharge Depth (ISD) =	user	ft
Total Available Detention Depth (H <sub>total</sub> ) =	user	ft
Depth of Trickle Channel (H <sub>TC</sub> ) =	user	ft
Slope of Trickle Channel (S <sub>TC</sub> ) =	user	ft/ft
Slopes of Main Basin Sides (Smain) =	user	H:V
Basin Length-to-Width Ratio (R <sub>L/W</sub> ) =	user	

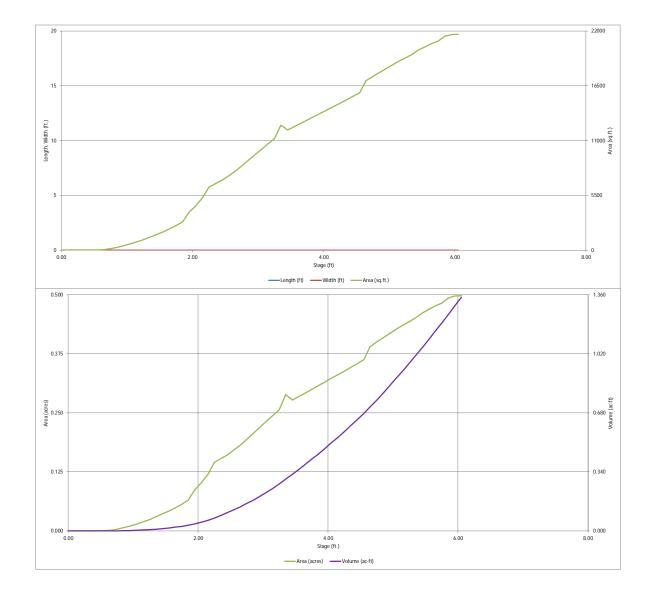
Initial Surcharge Area (A <sub>ISV</sub> ) =	user	ft <sup>2</sup>
Surcharge Volume Length ( $L_{ISV}$ ) =	user	ft
Surcharge Volume Width ( $W_{ISV}$ ) =	user	ft
Depth of Basin Floor (H <sub>FLOOR</sub> ) =	user	ft
Length of Basin Floor $(L_{FLOOR}) =$	user	ft
Width of Basin Floor ( $W_{FLOOR}$ ) =	user	ft
Area of Basin Floor $(A_{FLOOR}) =$		ft <sup>2</sup>
Volume of Basin Floor (V <sub>FLOOR</sub> ) =	user	ft <sup>3</sup>
Depth of Main Basin (H <sub>MAIN</sub> ) =	user	ft
Length of Main Basin $(L_{MAIN}) =$	user	ft
Width of Main Basin ( $W_{MAIN}$ ) =	user	ft
Area of Main Basin $(A_{MAIN}) =$		ft <sup>2</sup>
Volume of Main Basin (V <sub>MAIN</sub> ) =	user	ft <sup>3</sup>

Calculated Total Basin Volume (V<sub>total</sub>) = user acre-feet

	_		_							
EAR	Depth Increment =		ft							
			Optional				Optional			
ntion Pond)	Stage - Storage	Stage	Override	Length	Width	Area	Override Area (ft <sup>2</sup> )	Area	Volume	Volume
	Description	(ft)	Stage (ft)	(ft)	(ft)	(ft <sup>2</sup> )		(acre)	(ft 3)	(ac-ft)
	Top of Micropool		0.00				16	0.000		
	Top of ISV		0.55				22	0.001	10	0.000
			0.65				57	0.001	14	0.000
			0.75				147	0.003	25	0.001
			0.85				278	0.006	46	0.001
			0.95				434	0.010	81	0.002
			1.05				615	0.014	134	0.002
			1.15				814	0.019	205	0.005
			1.25				1,026	0.024	297	0.007
			1.35				1,287	0.030	413	0.009
			1.45				1,556	0.036	555	0.013
			1.55				1,823	0.042	724	0.017
			1.65				2,124	0.049	921	0.021
			1.75				2,458	0.056	1,151	0.026
Optional User Overrides			1.85				2,846	0.065	1,416	0.033
0.101 acre-feet			1.95				3,816	0.088	1,749	0.040
acre-feet			2.05				4,437	0.102	2,161	0.050
1.19 inches			2.15				5,224	0.120	2,644	0.061
1.50 inches			2.25				6,307	0.145	3,221	0.074
1.75 inches			2.35				6,666	0.153	3,870	0.089
2.00 inches			2.45				7,002	0.161	4,553	0.105
			2.55							
2.25 inches 2.52 inches			2.55				7,449 7,916	0.171 0.182	5,276 6,044	0.121 0.139
inches			2.75				8,441	0.194	6,862	0.158
			2.85				9,005	0.207	7,734	0.178
			2.95				9,556	0.219	8,662	0.199
			3.05				10,096	0.232	9,645	0.221
			3.15				10,634	0.244	10,681	0.245
			3.25	-	-		11,191	0.257	11,772	0.270
			3.35				12,559	0.288	12,960	0.298
			3.45				12,056	0.277	14,191	0.326
			3.55				12,386	0.284	15,413	0.354
			3.65				12,718	0.292	16,668	0.383
			3.75				13,050	0.300	17,956	0.412
			3.85				13,384	0.307	19,278	0.443
			3.85							
							13,720	0.315	20,633	0.474
			4.05				14,057	0.323	22,022	0.506
			4.15				14,395	0.330	23,445	0.538
			4.25				14,734	0.338	24,901	0.572
			4.35				15,080	0.346	26,392	0.606
			4.45				15,434	0.354	27,918	0.641
			4.55				15,793	0.363	29,479	0.677
			4.65				17,002	0.390	31,119	0.714
			4.75				17,444	0.400	32,841	0.754
			4.85				17,833	0.409	34,605	0.794
			4.95				18,199	0.418	36,406	0.836
			5.05							
							18,586	0.427	38,246	0.878
			5.15				18,965	0.435	40,123	0.921
			5.25				19,308	0.443	42,037	0.965
			5.35				19,656	0.451	43,985	1.010
			5.45				20,089	0.461	45,972	1.055
			5.55				20,410	0.469	47,997	1.102
			5.65				20,747	0.476	50,055	1.149
			5.75				21,001	0.482	52,143	1.197
			5.85				21,480	0.493	54,267	1.246
			5.95				21,646	0.497	56,423	1.295
			6.05				21,700	0.498	58,590	1.345
				-						
			-							
			-	-						
			-							
			1				1			1

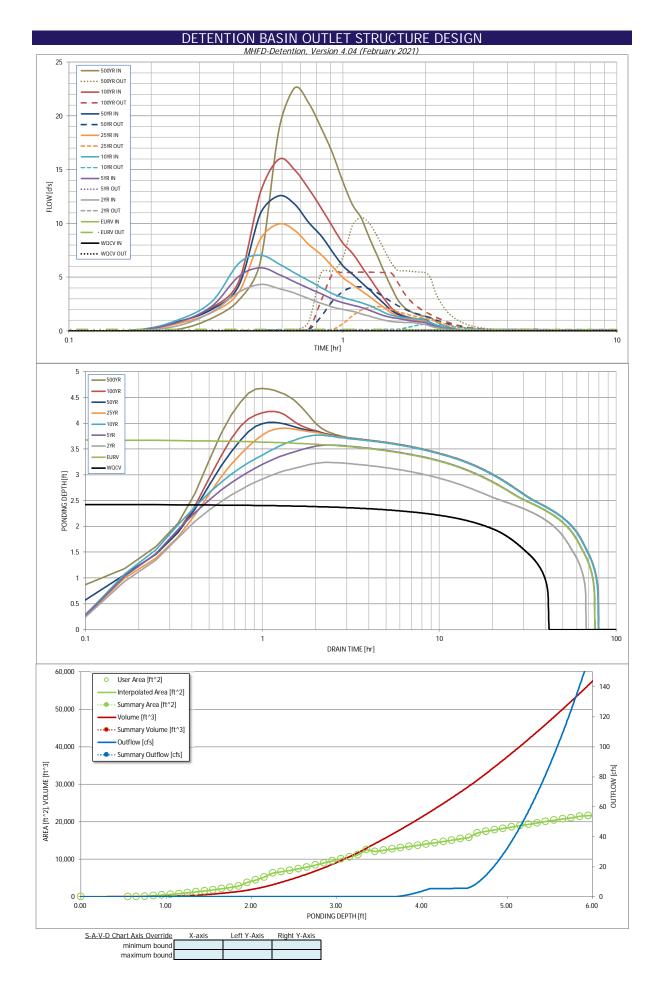
#### DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.04 (February 2021)



#### DETENTION BASIN OUTLET STRUCTURE DESIGN

Project: Basin ID:	MHFD-Detention, Version 4.04 (February 2021)								
	Meadowbrook Par	k							
ZONE 3									
ZONE 2	$\sim$			Estimated	Estimated				
				Stage (ft)	Volume (ac-ft)	Outlet Type	l		
			Zone 1 (WQCV)	2.43	0.101	Orifice Plate			
1	-100-YEAR ORIFICE		Zone 2 (EURV)	3.69	0.291	Circular Orifice			
PERMANENT ORIFICES			Zone 3 (100-year)	4.48	0.256	Weir&Pipe (Restrict)			
POOL Example Zone	Configuration (Re	tention Pond)		Total (all zones)	0.648				
User Input: Orifice at Underdrain Outlet (typical	y used to drain WQ	CV in a Filtration BM	<u>//P)</u>			1	Calculated Parame	ters for Underdrain	
Underdrain Orifice Invert Depth =	N/A		the filtration media	surface)	Underd	Irain Orifice Area =	N/A	ft <sup>2</sup>	
Underdrain Orifice Diameter =	N/A	inches			Underdrain	Orifice Centroid =	N/A	feet	
User Input: Orifice Plate with one or more orific	es or Elliptical Slot	Weir (typically used	to drain WQCV and	d/or EURV in a sedi	mentation BMP)		Calculated Parame	ters for Plate	
Invert of Lowest Orifice =	0.00	ft (relative to basir	n bottom at Stage =	0 ft)	WQ Orifi	ce Area per Row =	3.264E-03	ft <sup>2</sup>	
Depth at top of Zone using Orifice Plate =	3.69	ft (relative to basir	n bottom at Stage =	0 ft)	Elli	ptical Half-Width =	N/A	feet	
Orifice Plate: Orifice Vertical Spacing =	N/A	inches			Ellipt	ical Slot Centroid =	N/A	feet	
Orifice Plate: Orifice Area per Row =	0.47	sq. inches (diamet	er = 3/4 inch)		E	Iliptical Slot Area =	N/A	ft <sup>2</sup>	
User Input: Stage and Total Area of Each Orific	e Row (numbered f	rom lowest to highe	est)						
	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)	1
Stage of Orifice Centroid (ft)	· · · · · · · · · · · · · · · · · · ·	1.50							1
Orifice Area (sq. inches)	0.47	0.47							
									-
	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)	1
Stage of Orifice Centroid (ft)									
Orifice Area (sq. inches)									1
(-q. monos)									•
User Input: Vertical Orifice (Circular or Rectang	ular)						Calculated Parame	ters for Vertical Ori	fice
	Zone 2 Circular	Not Selected					Zone 2 Circular	Not Selected	
Invert of Vertical Orifice =	2.43	N/A	ft (relative to basir	bottom at Stage =	0 ft) Ver	tical Orifice Area =	0.02	N/A	ft <sup>2</sup>
Depth at top of Zone using Vertical Orifice =	3.69	N/A		bottom at Stage =		I Orifice Centroid =	0.08	N/A	feet
Vertical Orifice Diameter =	1.88	N/A	inches	9	,				1
User Input: Overflow Weir (Dropbox with Flat o	r Sloped Grate and	Outlet Pipe OR Red	tangular/Trapezoid	al Weir (and No Ou	tlet Pipe)		Calculated Parame	ters for Overflow W	/eir
	Zone 3 Weir	Not Selected					Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	3.69	N/A	ft (relative to basin	oottom at Stage = 0 1	t) Height of Grate	e Upper Edge, Ht =	3.69	N/A	feet
Overflow Weir Front Edge Length =	3.67	N/A	feet	5		/eir Slope Length =	2.79		
Overflow Weir Grate Slope =	0.00					rel = 30000  Lenger =		N/A	feet
		N/A	H:V	Gra					feet
Horiz, Lenath of Weir Sides =		N/A N/A	H:V feet		ate Open Area / 10	0-yr Orifice Area =	13.24	N/A	
Horiz. Length of Weir Sides = Overflow Grate Type =	2.79	N/A	H:V feet	Ov	ate Open Area / 10 erflow Grate Open	0-yr Orifice Area = Area w/o Debris =	13.24 7.12	N/A N/A	ft²
Overflow Grate Type =	2.79 Type C Grate	N/A N/A	feet	Ov	ate Open Area / 10	0-yr Orifice Area = Area w/o Debris =	13.24	N/A	
	2.79	N/A		Ov	ate Open Area / 10 erflow Grate Open	0-yr Orifice Area = Area w/o Debris =	13.24 7.12	N/A N/A	ft <sup>2</sup>
Overflow Grate Type = Debris Clogging % =	2.79 Type C Grate 50%	N/A N/A N/A	feet %	Ov	ate Open Area / 10 rerflow Grate Open rverflow Grate Open	0-yr Orifice Area = Area w/o Debris = n Area w/ Debris =	13.24 7.12 3.56	N/A N/A N/A	ft <sup>2</sup> ft <sup>2</sup>
Overflow Grate Type =	2.79 Type C Grate 50%	N/A N/A N/A estrictor Plate, or R	feet %	Ov	ate Open Area / 10 rerflow Grate Open rverflow Grate Open	0-yr Orifice Area = Area w/o Debris = n Area w/ Debris =	13.24 7.12 3.56	N/A N/A N/A Flow Restriction Pl	ft <sup>2</sup> ft <sup>2</sup>
Overflow Grate Type = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate	2.79 Type C Grate 50% (Circular Orifice, R Zone 3 Restrictor	N/A N/A N/A estrictor Plate, or R Not Selected	feet % <u>ectangular Orifice)</u>	Ov C	ate Open Area / 10 rerflow Grate Open werflow Grate Open <u>Ca</u>	0-yr Orifice Area = Area w/o Debris = n Area w/ Debris = lculated Parameter:	13.24 7.12 3.56 s for Outlet Pipe w/ Zone 3 Restrictor	N/A N/A N/A Flow Restriction Pli Not Selected	ft <sup>2</sup> ft <sup>2</sup>
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Overflow Grate Type = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage = Spillway Invert Stage = Spillway Crest Length = Spillway End Slopes = Spillway End Slopes = Freeboard above Max Water Surface = Routed Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = CUHP Rendevlopment Peak Q (cfs) = Predevelopment Unit Peak Flow, q (cfs/acre) = Peak Inflow Q (cfs) = Ratio Peak Outflow to Predevelopment Q = Max Velocity through Grate 1 (fps) = Max Velocity through Grate 1 (fps) = Time to Drain 97% of Inflow Volume (hours) = Time to Drain 99% of Inflow Volume (hours) = Time to Drain 99% of Inflow Volume (hours) =	2.79 Type C Grate 50% 20ne 3 Restrictor 0.50 30.00 5.00 Trapezoidal) 4.52 25.00 4.00 1.00 The user can over WQCV N/A 0.101 N/A N/A N/A N/A N/A N/A N/A N/A	N/A N/A N/A N/A N/A estrictor Plate, or R Not Selected N/A N/A ft (relative to basin feet H:V feet ride the default CU/I EURV N/A 0.392 N/A N/A N/A N/A N/A N/A N/A N/A O.2 N/A O.2 N/A O.2 N/A N/A O.2 O.2 N/A O.2 N/A O.2 N/A O.2 O.2 N/A O.2 N/A O.2 O.2 N/A O.2 O.2 N/A O.2 O.2 N/A O.2	feet % ectangular Orifice) ft (distance below b inches inches h bottom at Stage = <i>HP hydrographs and</i> 2 Year 1.19 0.288 0.288 0.1 0.288 0.1 0.288 0.1 Vertical Orifice 1 N/A N/A 65 3.24	Ov Casin bottom at Stage Half-Cent - 0 ft) - 0 ft) - 1.50 - 0.386 - 0.386 - 0.1 - 0.2 - 5.9 - 0.1 - 1.1 - Vertical Orifice 1 - N/A - N/A - 67 - 73 - 3.58	ate Open Area / 10 rerflow Grate Open verflow Grate Open verflow Grate Open verflow Grate Open ( at a open ( at a ngle of Restric Spillway D Stage at T Basin Area at T Basin Area at T Basin Area at T Basin Volume at T ( entering new value 1.75 0.463 0.463 0.2 ( 0.02 7.1 0.7 3.5 Overflow Weir 1 0.1 N/A 69 76 3.77	0-yr Orifice Area = Area w/o Debris = n Area w/ Debris = n Area w/ Debris = utlet Orifice Area = t Orifice Centroid = tor Plate on Pipe = op of Freeboard = cop of Freeboard = <u>op of Freeboard =</u> <u>op of Freeboard =</u> <u>op of Freeboard =</u> <u>op of Freeboard =</u> <u>op of Freeboard =</u> <u>0 0.600</u> <u>0.600</u> <u>1.7</u> <u>0.21</u> <u>10.0</u> <u>2.3</u> <u>1.3</u> <u>0verflow Weir 1</u> <u>0.3</u> <u>N/A</u> <u>67</u> <u>75</u> <u>3.91</u>	13.24           7.12           3.56           5 for Outlet Pipe w/           Zone 3 Restrictor           0.54           0.25           0.84           Calculated Parame           0.35           5.87           0.49           1.25           trographs table (Co           S0 Year           2.25           0.734           3.4           0.42           12.6           4.1           1.2           Overflow Weir 1           0.6           N/A           65           74           4.02	N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A	<i>F).</i> <i>500 Year</i> <i>3.14</i> <i>1.282</i> <i>1.282</i> <i>9.9</i> <i>1.22</i> <i>22.6</i> <i>10.6</i> <i>1.1</i> <i>Spillway</i> <i>0.8</i> <i>N/A</i> <i>59</i> <i>70</i> <i>4.68</i>
Overflow Grate Type = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage = Spillway Crest Length = Spillway Crest Length = Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Reuted Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = CUHP Redevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, q (cfs/acre) = Peak Inflow Q (cfs) = Peak Inflow Q (cfs) = Peak Nutflow Q (cfs) = Ratio Peak Outflow to Predevelopment 2 (fps) = Max Velocity through Grate 1 (fps) = Max Velocity through Grate 1 (fps) = Max Velocity through Grate 1 (fps) = Time to Drain 97% of Inflow Volume (hours) =	2.79 Type C Grate 50% 2006 2 Restrictor 0.50 30.00 5.00 Trapezoidal) 4.52 25.00 4.00 1.00 7 MOCV N/A N/A N/A N/A N/A N/A N/A N/A	N/A N/A N/A N/A N/A N/A estrictor Plate, or R Not Selected N/A N/A ft (relative to basir feet H:V feet EURV N/A 0.392 N/A	feet % ectangular Orifice) ft (distance below b inches inches h bottom at Stage = HP hydrographs and 2 Year 1.19 0.288 0.288 0.1 0.01 4.3 0.1 N/A Vertical Orifice 1 N/A Vertical Orifice 1 N/A	Ov Casin bottom at Stage Half-Cent to ft) Control to the stage Half-Cent to ft) Control to the stage Control to th	ate Open Area / 10 erflow Grate Open verflow Grate Open verflow Grate Open (Ca = 0 ft) Or Outlet ral Angle of Restric Spillway D Stage at T Basin Area at T Basin Volume at T entering new value 10 Year 1.75 0.463 0.463 0.2 	0-yr Orifice Area = Area w/o Debris = n Area w/ Debris = n Area w/ Debris = lculated Parameter: utlet Orifice Area = t Orifice Centroid = tor Plate on Pipe = op of Freeboard = con of Freeboard = op of Freeboard = on of Freeboard = con of Freeboar	13.24           7.12           3.56           s for Outlet Pipe w/           Zone 3 Restrictor           0.54           0.25           0.84           Calculated Parame           0.35           5.87           0.49           1.25           drographs table (Co           50 Year           2.25           0.734           3.4           0.42           12.6           4.1           1.2           Overflow Weir 1           0.6           N/A           65           74	N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A	<i>F).</i> 500 Year 3.14 1.282 9.9 1.22 22.6 10.6 1.1 Spillway 0.8 N/A 59 70



# DETENTION BASIN OUTLET STRUCTURE DESIGN Outflow Hydrograph Workbook Filename:

Inflow Hydrographs

the calculated inflow hydrographs from this workbook with inflow hydrographs de ed in a separate program The user can

	The user can o	verride the calcu	ulated inflow hyd	drographs from	this workbook w	ith inflow hydro	graphs develop	ed in a separate	program.	
	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.06	0.01	0.19
	0:15:00	0.00	0.00	0.51	0.83	1.04	0.70	0.88	0.86	1.23
	0:20:00	0.00	0.00	1.81	2.36	2.78	1.76	2.05	2.21	2.88
	0:25:00	0.00	0.00	3.63	5.09	6.31	3.63	4.24	4.65	6.44
	0:30:00	0.00	0.00	4.33	5.88	7.06	8.53	10.91	12.87	18.68
	0:35:00	0.00	0.00	3.97	5.27	6.26	9.98	12.58	15.98	22.60
	0:40:00	0.00	0.00	3.53	4.58	5.41	9.37	11.81	15.00	21.21
	0:50:00	0.00	0.00	3.02 2.59	3.98 3.47	4.71 4.04	8.06 7.11	10.11 8.85	13.23 11.45	18.88 16.50
	0:55:00	0.00	0.00	2.24	2.98	3.47	5.97	7.35	9.69	13.89
	1:00:00	0.00	0.00	2.01	2.65	3.13	4.98	6.08	8.19	11.76
	1:05:00	0.00	0.00	1.84	2.42	2.88	4.34	5.28	7.24	10.49
	1:10:00	0.00	0.00	1.61	2.21	2.63	3.75	4.52	6.03	8.64
	1:15:00	0.00	0.00	1.39	1.94	2.39	3.23	3.86	4.98	7.04
	1:20:00	0.00	0.00	1.18	1.66	2.06	2.66	3.15	3.91	5.47
	1:25:00	0.00	0.00	1.01	1.42	1.71	2.17	2.53	2.98	4.10
	1:30:00 1:35:00	0.00	0.00	0.90	1.27	1.48	1.69	1.94	2.19	2.94
	1:35:00	0.00	0.00	0.84	1.19	1.36 1.27	1.38 1.21	1.57	1.69 1.43	2.26
	1:45:00	0.00	0.00	0.80	0.98	1.27	1.21	1.37	1.43	1.64
	1:50:00	0.00	0.00	0.79	0.98	1.17	1.03	1.25	1.16	1.04
	1:55:00	0.00	0.00	0.69	0.86	1.12	0.99	1.11	1.08	1.36
	2:00:00	0.00	0.00	0.61	0.80	1.02	0.95	1.07	1.02	1.28
	2:05:00	0.00	0.00	0.47	0.61	0.77	0.73	0.81	0.76	0.95
	2:10:00	0.00	0.00	0.35	0.45	0.57	0.54	0.60	0.56	0.70
	2:15:00	0.00	0.00	0.26	0.34	0.42	0.40	0.44	0.42	0.52
	2:20:00 2:25:00	0.00	0.00	0.19	0.25	0.31	0.29	0.33	0.31	0.38
	2:23:00	0.00	0.00	0.14	0.18	0.23	0.21	0.23	0.22	0.27
	2:35:00	0.00	0.00	0.10	0.13	0.18	0.15	0.17	0.18	0.19
	2:40:00	0.00	0.00	0.05	0.06	0.08	0.07	0.08	0.08	0.09
	2:45:00	0.00	0.00	0.03	0.04	0.05	0.05	0.05	0.05	0.06
	2:50:00	0.00	0.00	0.01	0.02	0.02	0.03	0.03	0.02	0.03
	2:55:00	0.00	0.00	0.01	0.01	0.01	0.01	0.01	0.01	0.01
	3:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:10:00 3:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:55:00 4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:25:00 4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:45:00 4:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:05:00 5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:30:00 5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:55:00 6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0.00.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

#### DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.04 (February 2021)

Summary Stage-Area-Volume-Discharge Relationships The user can create a summary S-A-V-D by entering the desired stage increments and the remainder of the table will populate automatically. The user should graphically compare the summary S-A-V-D table to the full S-A-V-D table in the chart to confirm it captures all key transition points.

Stage - Storage Description	Stage [ft]	Area [ft²]	Area [acres]	Volume [ft <sup>3</sup> ]	Volume [ac-ft]	Total Outflow [cfs]	
							For best results, include the
							stages of all grade slope changes (e.g. ISV and Floor)
							from the S-A-V table on
							Sheet 'Basin'.
							Also include the inverts of al
							outlets (e.g. vertical orifice.
							overflow grate, and spillway where applicable).
							where applicable).
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	Design Procedure	e Form: Rain Garden (RG)						
	UD-BMP	(Version 3.07, March 2018)	Sheet 1 of 2					
Designer:	KRK							
Company:	Kimley-Horn and Associates							
Date:	March 12, 2021							
Project:	Meadowbrook Park							
Location:	RG SWC of Site							
1. Basin Sto	rage Volume							
	$^{\rm ve}$ Imperviousness of Tributary Area, ${\rm I_a}$ if all paved and roofed areas upstream of rain garden)	l <sub>a</sub> = 54.5 %						
B) Tributa	ary Area's Imperviousness Ratio (i = I <sub>a</sub> /100)	i = 0.545						
	Quality Capture Volume (WQCV) for a 12-hour Drain Time CV= 0.8 * (0.91* $i^3$ - 1.19 * $i^2$ + 0.78 * i)	WQCV = 0.18 watershe	ed inches					
D) Contri	buting Watershed Area (including rain garden area)	Area = <u>80,559</u> sq ft						
	Quality Capture Volume (WQCV) Design Volume (WQCV / 12) * Area	V <sub>WQCV</sub> =cu ft						
	atersheds Outside of the Denver Region, Depth of ge Runoff Producing Storm	d <sub>6</sub> = 0.43 in						
	'atersheds Outside of the Denver Region, · Quality Capture Volume (WQCV) Design Volume	V <sub>WQCV OTHER</sub> = 1,176 cu ft						
	nput of Water Quality Capture Volume (WQCV) Design Volume f a different WQCV Design Volume is desired)	V <sub>WQCV USER</sub> =cu ft						
2. Basin Geo	ometry							
A) WQCV	Depth (12-inch maximum)	D <sub>WQCV</sub> = <u>12</u> in						
	arden Side Slopes (Z = 4 min., horiz. dist per unit vertical) 0" if rain garden has vertical walls)	Z = 0.00 ft / ft						
C) Mimim	um Flat Surface Area	A <sub>Min</sub> = 878 sq ft						
D) Actual	Flat Surface Area	A <sub>Actual</sub> = <u>1215</u> sq ft						
E) Area a	t Design Depth (Top Surface Area)	A <sub>Top</sub> = <u>1215</u> sq ft						
	arden Total Volume A <sub>Top</sub> + A <sub>Actual</sub> ) / 2) * Depth)	V <sub>T</sub> = <u>1,215</u> cu ft						
3. Growing N	<i>l</i> ledia	Choose One ① 18" Rain Garden Gro 〇 Other (Explain):	wing Media					
4 11 1 1								
4. Underdrai	n System	Choose One						
A) Are un	derdrains provided?	YES						
B) Underg	drain system orifice diameter for 12 hour drain time	◯ NO						
,	i) Distance From Lowest Elevation of the Storage Volume to the Center of the Orifice	y= <u>0.3</u> ft						
	ii) Volume to Drain in 12 Hours	Vol <sub>12</sub> = 1,176 cu ft						
	iii) Orifice Diameter, 3/8" Minimum	$D_0 = 1 3/16$ in						

	Design Proced	ure Form: Rain Garden (RG)
Designer:	KRK	Sheet 2 of
Company:	Kimley-Horn and Associates	
Date:	March 12, 2021	
Project:	Meadowbrook Park	
Location:	RG SWC of Site	
A) Is an	able Geomembrane Liner and Geotextile Separator Fabric impermeable liner provided due to proximity uctures or groundwater contamination?	Choose One VES NO PROVIDE A 30 MIL (MIN) PVC LINER WITH CDOT CLASS B GEOTEXTILE ABOVE IT. USE THE SAME GEOTEXTILE BELOW THE LINER IF THE SUBGRADE IS ANGULAR
6. Inlet / Ou A) Inlet (		Choose One Sheet Flow- No Energy Dissipation Required Concentrated Flow- Energy Dissipation Provided
7. Vegetatic	n	Choose One Seed (Plan for frequent weed control) Plantings Sand Grown or Other High Infiltration Sod
8. Irrigation A) Will th	ne rain garden be irrigated?	Choose One
Notes:		

## Kimley »Horn

Forebay Sizing Calculations- Detention Basin Forebay Contributing Sub-Basins: C-J

Checked By Forebay A Flow:  $Q_{100} = (cfs)$ Required Release Rate Release 2% of the undetained Forebay Release 100-year peak discharge by way and Configuration 19.60 0.39 of a wall/notch or berm/pipe configuration Required (CF) Provided (CF) Minimum Forebay 40hr drain time a = 1 Volume Required I = 0.641 2% of the WQCV 70.07 84.00 A = 3.85 AC Maximum Forebay Required Provided Depth 18" Max 18" Concrete Forebay Structure Forebay Notch Calculations  $Q = C_o A_o (2gH_o)$ 0.39 cfs Qa 2% of Peak 100 YR Discharge for contributing Sub-Basins 0.6 0.5 ft H, 32.2 ft/s<sup>2</sup> 0.12 ft<sup>2</sup> 0.08 ft 0.92 in 3" Minimum per Criteria

 $WQCV = a(0.91l^3 - 1.19l^2 + 0.78l)$ 

Equation 3-1

2/22/2021

KRK

JRH

Date

Prepared By

Where:

WQCV = Water Quality Capture Volume (watershed inches)

а = Coefficient corresponding to WQCV drain time (Table 3-2)

= Imperviousness (%/100) (see Figures 3-3 through 3-5 [single family land use] and /or the *Runoff* chapter of Volume 1[other typical land uses]) I

Table 3-2. Drain Time Coefficients for WQCV Calculations

Drain Time (hrs)	Coefficient, a
12 hours	0.8
24 hours	0.9
40 hours	1.0

## Kimley **»Horn**

Forebay Sizing Calculations- Detention Basin Forebay Contributing Sub-Basins: A

3					
		Foreb	ay B		
	Required	Flow: Q <sub>100</sub> = (cfs)	Release Rate		
Forebay Release and Configuration	Release 2% of the undetained 100-year peak discharge by way of a wall/notch or berm/pipe configuration	7.19	0.14		
Minimum Forebay		40hr drain time a = 1	Required (CF)	Provided (CF)	
Volume Required	2% of the WQCV	I = 0.197 A = 2.47 AC	20.52	154.00	
Maximum Foreboy			1		
Maximum Forebay Depth	<u>Required</u> 12" Max	Provided 12"	Concrete Berm		
Forebay Notch Calc	ulations		]		
$Q = C_o A_o (2gH_o)^{0.5}$	5				
Q <sub>a</sub>	0.14	cfs	2% of Peak 100 YR D	ischarge for contrib	uting Sub-Ba
C <sub>o</sub>	0.6				
H <sub>o</sub>	0.5		-		
g		ft/s <sup>2</sup>			
		61 <sup>2</sup>			
A <sub>a</sub>	0.04	π	4		
La	0.03	ft	1		
3	0.34		3" Minimum per Cri	toria	

 $WQCV = a(0.91I^3 - 1.19I^2 + 0.78I)$ 

Equation 3-1

2/22/2021

KRK

JRH

Date

Prepared By

Checked By

Where:

WQCV = Water Quality Capture Volume (watershed inches)

*a* = Coefficient corresponding to WQCV drain time (Table 3-2)

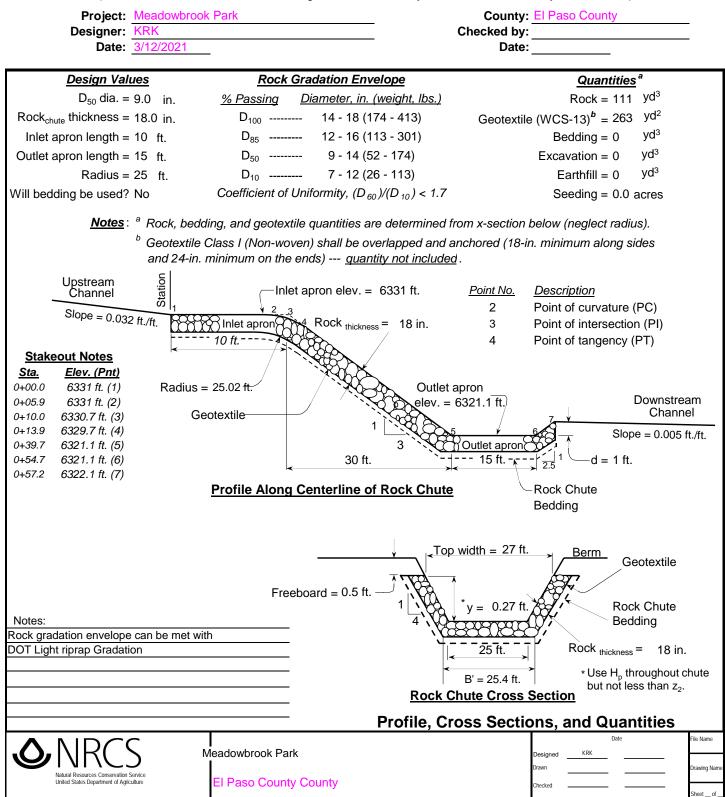
I = Imperviousness (%/100) (see Figures 3-3 through 3-5 [single family land use] and /or the Runoff chapter of Volume 1[other typical land uses])

#### Table 3-2. Drain Time Coefficients for WQCV Calculations

Drain Time (hrs)	Coefficient, a
12 hours	0.8
24 hours	0.9
40 hours	1.0

## **Rock Chute Design - Cut/Paste Plan**

(Version WI-Nov. 2017, Based on Design of Rock Chutes by Robinson, Rice, Kadavy, ASAE, 1998)



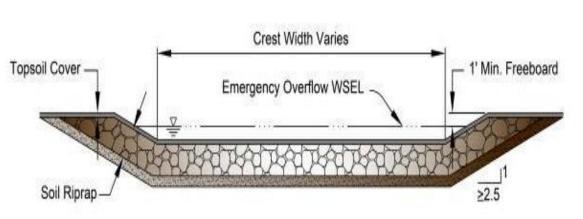
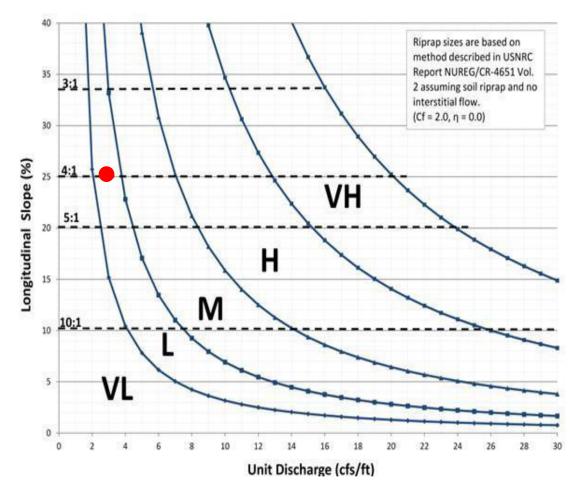
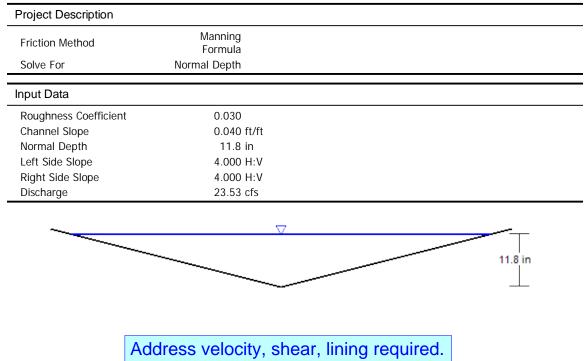


Figure 13-12c. Emergency Spillway Protection

Figure 13-12d. Riprap Types for Emergency Spillway Protection





#### Cross Section for CDOT By Pass Ditch

V: 1 📐 H: 1

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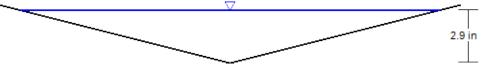
Project Description					
Friction Method	Manning Formula				
Solve For	Normal Depth				
Input Data					
Channel Slope	0.011 ft/ft				
Normal Depth	5.2 in				
Discharge	11.20 cfs				
		22	0.5 SS		
	0.20				
	0.00				
	-0.20	1			
	0.40	1			
	0.40	4		_	
	-0.80	~	V		
	-1.00		~		
	-1.20			Y	
	-1.40				
	0+00	0+10	0+20 Station	0+30	

## Cross Section for Emergency Overflow Spillway

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Friction Method	Manning Formula
Solve For	Normal Depth
Input Data	
Roughness Coefficient	0.030
Channel Slope	0.010 ft/ft
Normal Depth	2.9 in
Left Side Slope	4.000 H:V
Right Side Slope	4.000 H:V
Discharge	0.27 cfs

#### Cross Section for Meadowbrook Ditch North

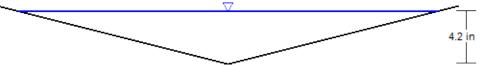


V:1 L H:1

Ditch Sizes.fm8 3/12/2021 Bentley Systems, Inc. Haestad Methods Solution Center 27 Siemon Company Drive Suite 200 W Watertown, CT 06795 USA +1-203-755-1666

Friction Method	Manning Formula
Solve For	Normal Depth
Input Data	
Roughness Coefficient	0.030
Channel Slope	0.010 ft/ft
Normal Depth	4.2 in
Left Side Slope	4.000 H:V
Right Side Slope	4.000 H:V
Discharge	0.73 cfs



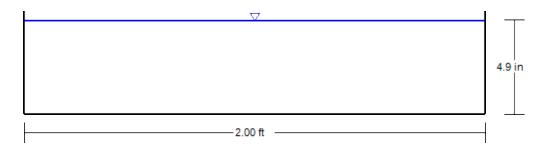


V: 1 L H: 1

Ditch Sizes.fm8 3/12/2021 Bentley Systems, Inc. Haestad Methods Solution Center 27 Siemon Company Drive Suite 200 W Watertown, CT 06795 USA +1-203-755-1666

Project Description									
Friction Method	Manning Formula								
Solve For	Normal Depth								
Input Data									
Roughness Coefficient	0.013								
Channel Slope	0.010 ft/ft								
Normal Depth	4.9 in								
Bottom Width	2.00 ft								
Discharge	4.04 cfs								

#### Cross Section for Rain Garden- Curb Chase

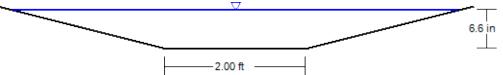


V:1 📐 H:1

Ditch Sizes.fm8 3/12/2021 Bentley Systems, Inc. Haestad Methods Solution Center 27 Siemon Company Drive Suite 200 W Watertown, CT 06795 USA +1-203-755-1666

Friction Method	Manning Formula	
Solve For	Normal Depth	
nput Data		
Roughness Coefficient	0.030	
Channel Slope	0.016 ft/ft	
Normal Depth	6.6 in	
Left Side Slope	4.000 H:V	
Right Side Slope	4.000 H:V	
Bottom Width	2.00 ft	
Discharge	7.19 cfs	





V:1 L H:1

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Start Node	Stop Node	Invert (Start) (ft)	Invert (Stop) (ft)	Length (User Defined) (ft)	Slope (Calculated) (ft/ft)	Diameter (in)	Manning's n	Flow (cfs)	Velocity (ft/s)	Capacity (Full Flow) (cfs)	Hydraulic Grade Line (In) (ft)	Hydraulic Grade Line (Out) (ft)	Flow / Capacity (Design) (%)
MH A7	MH A6	6,328.09	6,327.34	55.4	0.014	18.0	0.013	2.48	5.42	12.22	6,328.69	6,328.03	20.3
MH A6	MH A5	6,327.14	6,326.74	29.9	0.013	18.0	0.013	2.48	5.40	12.15	6,327.74	6,327.50	20.4
INLET G1	MH A5	6,326.78	6,326.74	4.5	0.009	18.0	0.013	0.77	3.33	9.90	6,327.50	6,327.50	7.8
INLET H1	MH A7	6,328.34	6,328.29	4.7	0.011	18.0	0.013	0.82	3.62	10.87	6,328.91	6,328.91	7.5
MH A5	MH A4	6,326.54	6,323.95	191.1	0.014	18.0	0.013	3.25	5.85	12.23	6,327.23	6,324.48	26.6
INLET A8	MH A7	6,330.70	6,328.29	177.6	0.014	18.0	0.013	1.66	4.84	12.24	6,331.18	6,328.91	13.6
MH E1	MH A4	6,325.66	6,323.68	196.6	0.010	18.0	0.013	2.16	4.69	10.54	6,326.21	6,324.59	20.5
MH A4	MH A3	6,323.45	6,321.67	148.3	0.012	24.0	0.013	5.41	6.31	24.78	6,324.27	6,322.30	21.8
INLET F1	MH E1	6,326.00	6,325.86	25.0	0.006	18.0	0.013	0.44	2.39	7.82	6,326.53	6,326.53	5.6
INLET F2	MH E1	6,325.99	6,325.94	9.0	0.006	18.0	0.013	1.72	3.55	7.83	6,326.52	6,326.53	22.0
MH A3	MH A2	6,321.47	6,320.19	106.8	0.012	24.0	0.013	5.41	6.31	24.77	6,322.29	6,321.44	21.8
MH A2	Outfall A1	6,319.99	6,319.85	46.0	0.003	36.0	0.013	9.04	4.31	36.79	6,321.00	6,320.80	24.6
MH C1	MH A2	6,320.30	6,320.19	56.3	0.002	18.0	0.013	2.25	2.61	4.64	6,321.46	6,321.44	48.5
MH B1	MH A2	6,320.34	6,320.19	31.0	0.005	18.0	0.013	1.38	3.18	7.31	6,321.44	6,321.44	18.9
INLET B2	MH B1	6,320.57	6,320.54	4.5	0.007	18.0	0.013	1.38	3.56	8.58	6,321.46	6,321.46	16.1
MH C1	INLET D1	6,320.50	6,320.55	5.4	-0.009	18.0	0.013	0.82	3.45	10.14	6,321.50	6,321.50	8.1
INLET C2	MH C1	6,320.78	6,320.50	137.6	0.002	18.0	0.013	1.43	2.35	4.74	6,321.55	6,321.50	30.2
MH J3	INLET K1	6,317.16	6,317.25	18.0	-0.005	30.0	0.013	0.10	1.37	29.00	6,318.69	6,318.69	0.3
MH J3	MH J2	6,317.16	6,315.21	270.6	0.007	30.0	0.013	10.79	6.26	34.82	6,318.26	6,317.25	31.0
MH J3	INLET J4	6,317.16	6,318.31	43.2	-0.027	30.0	0.013	10.69	9.99	66.94	6,319.40	6,318.69	16.0
MH J2	MH J1	6,315.01	6,314.62	43.2	0.009	30.0	0.013	10.79	6.79	38.96	6,317.25	6,317.23	27.7
0-2	MH J1	6,314.18	6,314.40	53.8	-0.004	36.0	0.013	10.82	5.04	42.65	6,317.19	6,317.18	25.4
INLET 11	MH J1	6,315.40	6,314.62	162.5	0.005	18.0	0.013	0.03	0.02	7.28	6,317.23	6,317.23	0.4

#### 5 Year FlexTable: Conduit Table

Meadowbrook Park.stsw 3/13/2021

Label	Elevation (Rim) (ft)	Elevation (Invert) (ft)	Hydraulic Grade Line (In) (ft)	Hydraulic Grade Line (Out) (ft)	Flow (Total Out) (cfs)	Headloss Coefficient (Standard)
INLET A8	6,334.79	6,330.70	6,331.19	6,331.18	1.66	0.050
INLET B2	6,324.98	6,320.57	6,321.46	6,321.46	1.38	0.050
INLET C2	6,324.27	6,320.78	6,321.55	6,321.55	1.43	0.050
INLET D1	6,324.79	6,320.55	6,321.50	6,321.50	0.82	0.050
INLET F1	6,329.50	6,325.99	6,326.53	6,326.53	0.44	0.050
INLET F2	6,329.50	6,325.99	6,326.52	6,326.52	1.72	0.050
INLET G1	6,336.35	6,326.78	6,327.50	6,327.50	0.77	0.050
INLET H1	6,336.24	6,328.34	6,328.91	6,328.91	0.82	0.050
INLET 11	6,318.36	6,315.40	6,317.23	6,317.23	0.03	0.050
INLET J4	6,323.01	6,318.31	6,319.42	6,319.40	10.69	0.050
INLET K1	6,320.21	6,317.25	6,318.69	6,318.69	0.10	0.050

## 5 Year FlexTable: Catch Basin Table

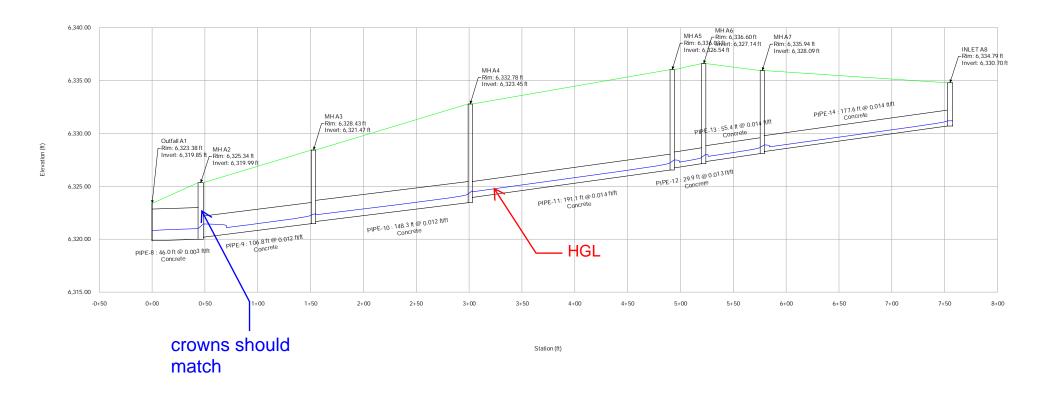
Meadowbrook Park.stsw 3/13/2021

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Label	Elevation (Rim) (ft)	Flow (Total Out) (cfs)	Hydraulic Grade Line (In) (ft)	Hydraulic Grade Line (Out) (ft)	Headloss Coefficient (Standard)	Headloss (ft)
MH A6	6,336.60	2.48	6,328.03	6,327.74	1.320	0.29
MH A5	6,336.03	3.25	6,327.50	6,327.23	1.020	0.27
MH A7	6,335.94	2.48	6,328.91	6,328.69	1.020	0.23
MH A4	6,332.78	5.41	6,324.59	6,324.27	1.020	0.31
MH E1	6,329.29	2.16	6,326.53	6,326.21	1.520	0.31
MH A3	6,328.43	5.41	6,322.41	6,322.29	0.400	0.12
MH A2	6,325.34	9.04	6,321.44	6,321.00	1.520	0.44
MH B1	6,324.51	1.38	6,321.46	6,321.44	1.320	0.02
MH C1	6,324.51	2.25	6,321.50	6,321.46	1.020	0.04
MH J3	6,323.40	10.79	6,318.69	6,318.26	1.020	0.43
MH J2	6,321.76	10.79	6,317.25	6,317.25	0.040	0.00
MH J1	6,320.86	10.82	6,317.23	6,317.19	1.020	0.04

## 5 Year FlexTable: Manhole Table

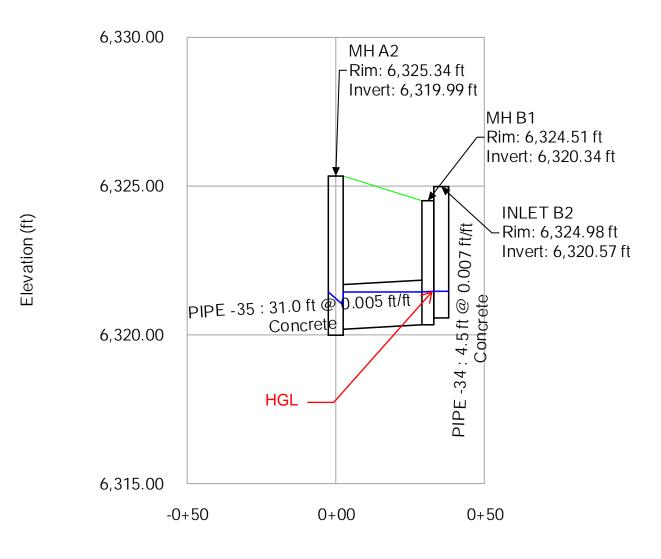
Profile Report **5 Year** Engineering Profile - STRM LINE A (Meadowbrook Park.stsw)



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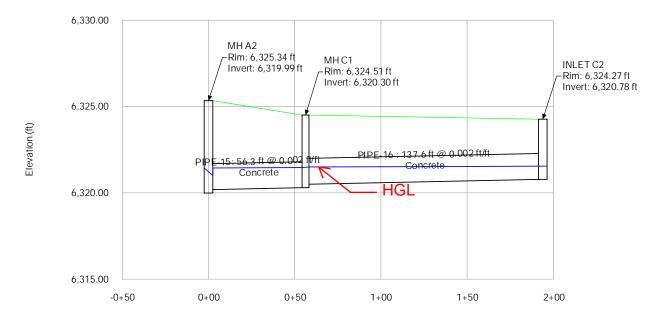
Profile Report 5 Year Engineering Profile - STRM LINE B (Meadowbrook Park.stsw)



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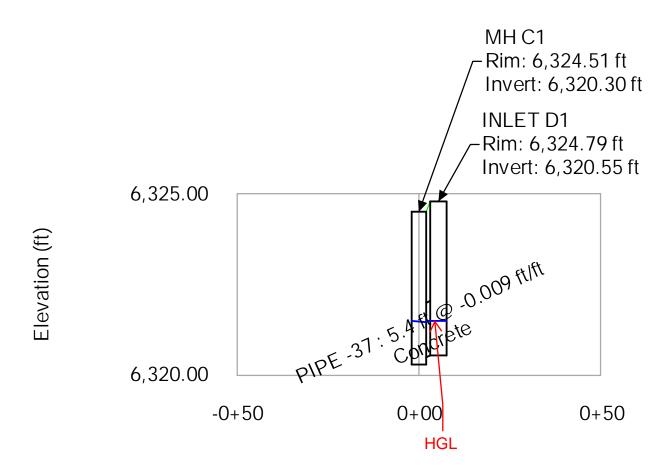
Profile Report 5 Year Engineering Profile - STRM LINE C (Meadowbrook Park.stsw)



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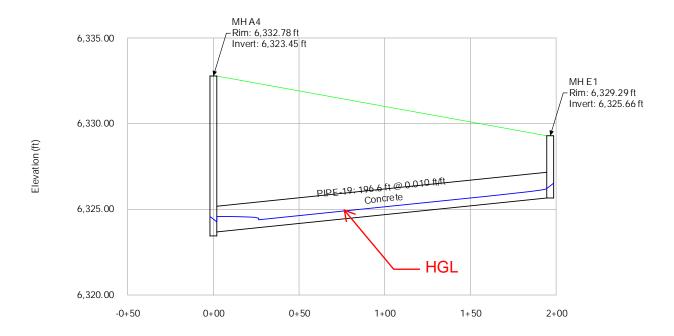
Profile Report 5 Year Engineering Profile - STRM LINE D (Meadowbrook Park.stsw)



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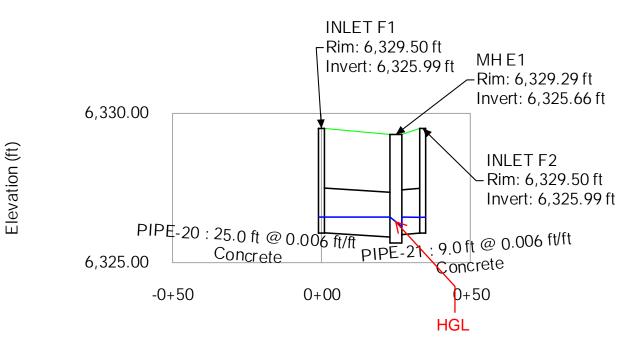
Profile Report 5 Year Engineering Profile - STRM LINE E (Meadowbrook Park.stsw)



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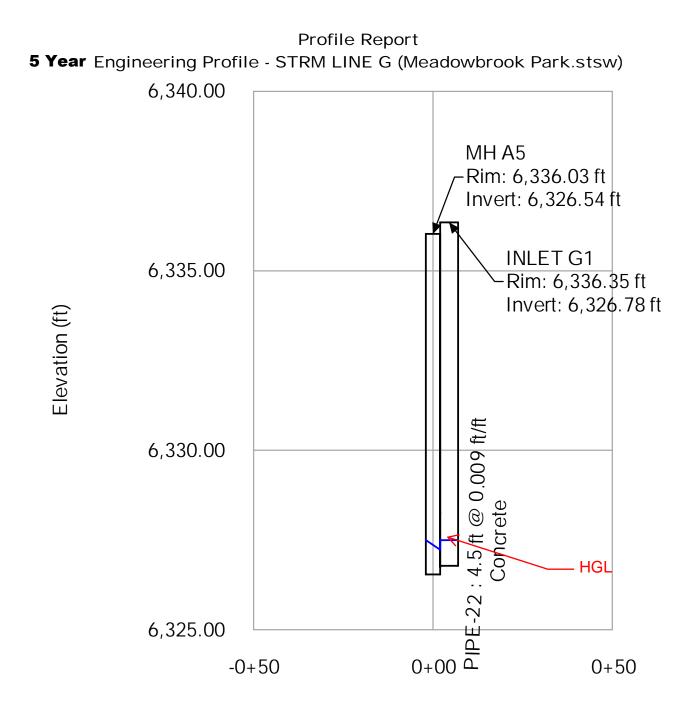
Profile Report 5 Year Engineering Profile - STRM LINE F (Meadowbrook Park.stsw)





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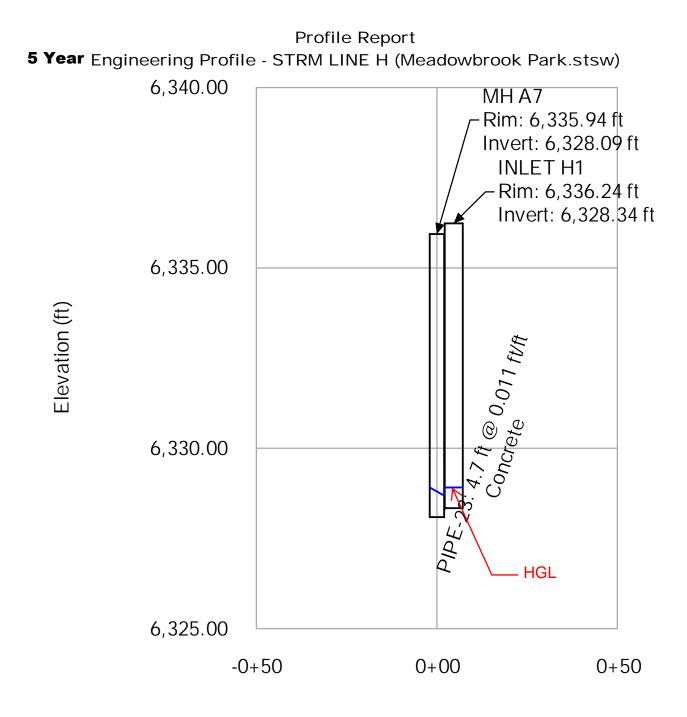
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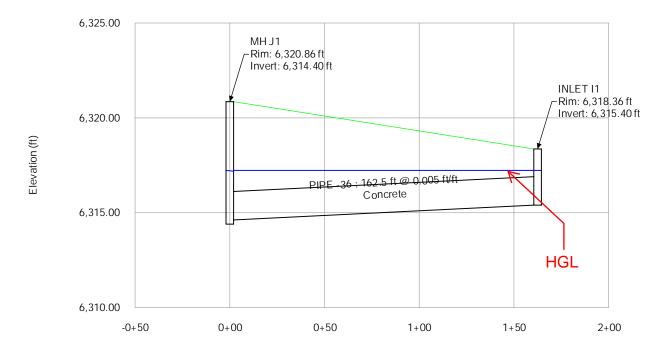
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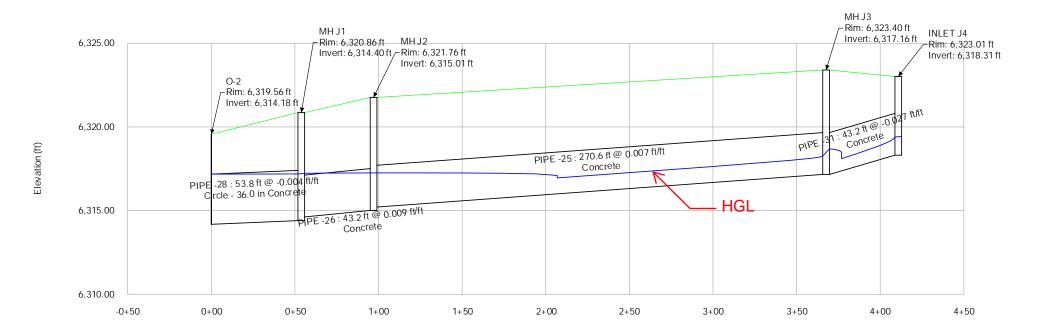
Profile Report 5 Year Engineering Profile - STRM LINE I (Meadowbrook Park.stsw)



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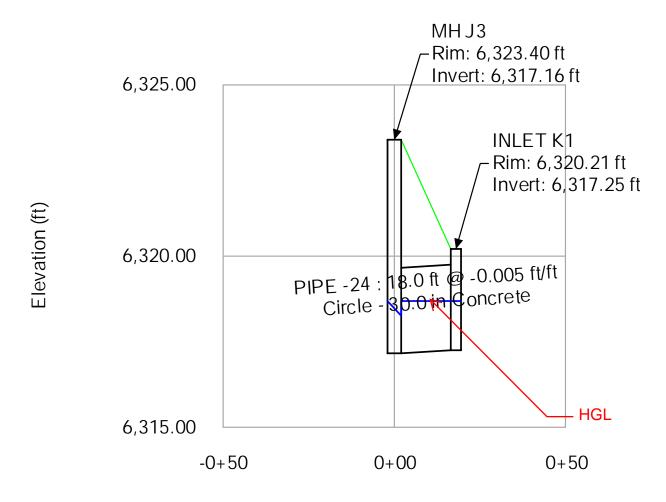
Profile Report **5 Year** Engineering Profile - STRM LINE J (Meadowbrook Park.stsw)



Meadowbrook Park.stsw 3/13/2021

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Profile Report 5 Year Engineering Profile - STRM LINE K (Meadowbrook Park.stsw)



Meadowbrook Park.stsw 3/13/2021

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100 Year FlexTable: Conduit Table

Start Node	Stop Node	Invert (Start) (ft)	Invert (Stop) (ft)	Length (User Defined) (ft)	Slope (Calculated) (ft/ft)	Diameter (in)	Manning's n	Flow (cfs)	Velocity (ft/s)	Capacity (Full Flow) (cfs)	Hydraulic Grade Line (In) (ft)	Hydraulic Grade Line (Out) (ft)	Flow / Capacity (Design) (%)
MH A7	MH A6	6,328.09	6,327.34	55.4	0.014	18.0	0.013	5.57	6.76	12.22	6,329.00	6,328.56	45.6
MH A6	MH A5	6,327.14	6,326.74	29.9	0.013	18.0	0.013	5.57	6.73	12.15	6,328.05	6,328.05	45.8
INLET G1	MH A5	6,326.78	6,326.74	4.5	0.009	18.0	0.013	1.53	4.07	9.90	6,328.05	6,328.05	15.5
INLET H1	MH A7	6,328.34	6,328.29	4.7	0.011	18.0	0.013	1.72	4.49	10.87	6,329.39	6,329.39	15.8
MH A5	MH A4	6,326.54	6,323.95	191.1	0.014	18.0	0.013	7.10	7.18	12.23	6,327.57	6,325.23	58.1
INLET A8	MH A7	6,330.70	6,328.29	177.6	0.014	18.0	0.013	3.85	6.13	12.24	6,331.45	6,329.39	31.5
MH E1	MH A4	6,325.66	6,323.68	196.6	0.010	18.0	0.013	4.82	5.83	10.54	6,326.50	6,325.23	45.7
MH A4	MH A3	6,323.45	6,321.67	148.3	0.012	24.0	0.013	11.92	7.81	24.78	6,324.69	6,322.92	48.1
INLET F1	MH E1	6,326.00	6,325.86	25.0	0.006	18.0	0.013	0.80	2.85	7.82	6,327.03	6,327.03	10.2
INLET F2	MH E1	6,325.99	6,325.94	9.0	0.006	18.0	0.013	4.02	4.46	7.83	6,327.03	6,327.03	51.3
MH A3	MH A2	6,321.47	6,320.19	106.8	0.012	24.0	0.013	11.92	7.81	24.77	6,322.71	6,322.21	48.1
MH A2	Outfall A1	6,319.99	6,319.85	46.0	0.003	36.0	0.013	19.57	5.29	36.79	6,321.53	6,321.27	53.2
MH C1	MH A2	6,320.30	6,320.19	56.3	0.002	18.0	0.013	4.95	2.80	4.64	6,322.33	6,322.21	106.6
MH B1	MH A2	6,320.34	6,320.19	31.0	0.005	18.0	0.013	2.70	1.53	7.31	6,322.23	6,322.21	37.0
INLET B2	MH B1	6,320.57	6,320.54	4.5	0.007	18.0	0.013	2.70	1.53	8.58	6,322.28	6,322.28	31.5
MH C1	INLET D1	6,320.50	6,320.55	5.4	-0.009	18.0	0.013	1.52	0.86	10.14	6,322.46	6,322.46	15.0
INLET C2	MH C1	6,320.78	6,320.50	137.6	0.002	18.0	0.013	3.43	1.94	4.74	6,322.60	6,322.46	72.4
MH J3	INLET K1	6,317.16	6,317.25	18.0	-0.005	30.0	0.013	5.10	1.04	29.00	6,319.87	6,319.87	17.6
MH J3	MH J2	6,317.16	6,315.21	270.6	0.007	30.0	0.013	28.64	7.92	34.82	6,318.98	6,317.77	82.3
MH J3	INLET J4	6,317.16	6,318.31	43.2	-0.027	30.0	0.013	23.54	12.45	66.94	6,319.96	6,319.87	35.2
MH J2	MH J1	6,315.01	6,314.62	43.2	0.009	30.0	0.013	28.64	5.83	38.96	6,317.74	6,317.53	73.5
0-2	MH J1	6,314.18	6,314.40	53.8	-0.004	36.0	0.013	28.67	6.47	42.65	6,317.26	6,317.18	67.2
INLET 11	MH J1	6,315.40	6,314.62	162.5	0.005	18.0	0.013	0.03	0.02	7.28	6,317.53	6,317.53	0.4



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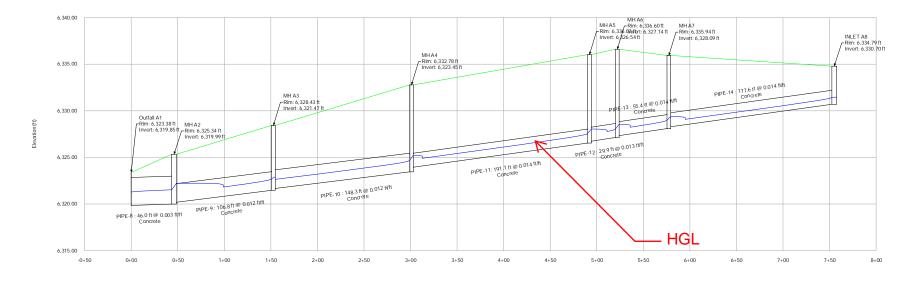
Label	Elevation (Rim) (ft)	Elevation (Invert) (ft)	Hydraulic Grade Line (In) (ft)	Hydraulic Grade Line (Out) (ft)	Flow (Total Out) (cfs)	Headloss Coefficient (Standard)
INLET A8	6,334.79	6,330.70	6,331.47	6,331.45	3.85	0.050
INLET B2	6,324.98	6,320.57	6,322.28	6,322.28	2.70	0.050
INLET C2	6,324.27	6,320.78	6,322.61	6,322.60	3.43	0.050
INLET D1	6,324.79	6,320.55	6,322.46	6,322.46	1.52	0.050
INLET F1	6,329.50	6,325.99	6,327.03	6,327.03	0.80	0.050
INLET F2	6,329.50	6,325.99	6,327.04	6,327.03	4.02	0.050
INLET G1	6,336.35	6,326.78	6,328.05	6,328.05	1.53	0.050
INLET H1	6,336.24	6,328.34	6,329.39	6,329.39	1.72	0.050
INLET 11	6,318.36	6,315.40	6,317.53	6,317.53	0.03	0.050
INLET J4	6,323.01	6,318.31	6,320.00	6,319.96	23.54	0.050
INLET K1	6,320.21	6,317.25	6,319.87	6,319.87	5.10	0.050

## 100 Year FlexTable: Catch Basin Table

Label	Elevation (Rim) (ft)	Flow (Total Out) (cfs)	Hydraulic Grade Line (In) (ft)	Hydraulic Grade Line (Out) (ft)	Headloss Coefficient (Standard)	Headloss (ft)
MH A6	6,336.60	5.57	6,328.56	6,328.05	1.320	0.51
MH A5	6,336.03	7.10	6,328.05	6,327.57	1.020	0.48
MH A7	6,335.94	5.57	6,329.39	6,329.00	1.020	0.39
MH A4	6,332.78	11.92	6,325.23	6,324.69	1.020	0.54
MH E1	6,329.29	4.82	6,327.03	6,326.50	1.520	0.52
MH A3	6,328.43	11.92	6,322.92	6,322.71	0.400	0.21
MH A2	6,325.34	19.57	6,322.21	6,321.53	1.520	0.68
MH B1	6,324.51	2.70	6,322.28	6,322.23	1.320	0.05
MH C1	6,324.51	4.95	6,322.46	6,322.33	1.020	0.12
MH J3	6,323.40	28.64	6,319.87	6,318.98	1.020	0.88
MH J2	6,321.76	28.64	6,317.77	6,317.74	0.040	0.02
MH J1	6,320.86	28.67	6,317.53	6,317.26	1.020	0.27

#### 100 Year FlexTable: Manhole Table

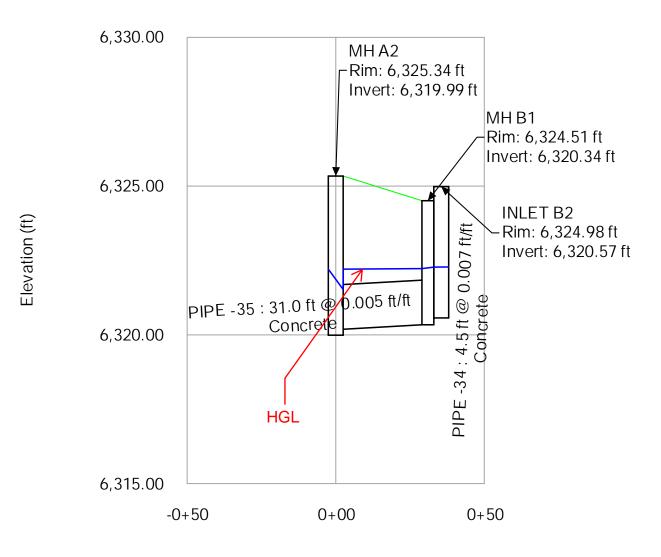
Profile Report **100 Year** Engineering Profile - STRM LINE A (Meadowbrook Park.stsw)



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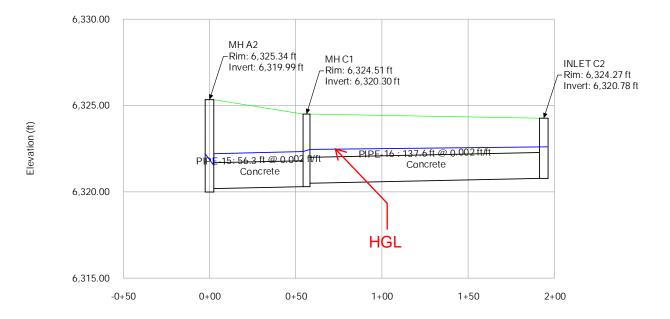
Profile Report **100 Year** Engineering Profile - STRM LINE B (Meadowbrook Park.stsw)



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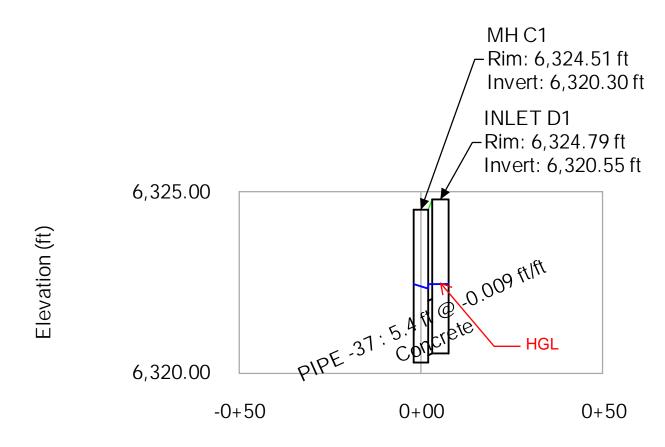
Profile Report **100 Year** Engineering Profile - STRM LINE C (Meadowbrook Park.stsw)



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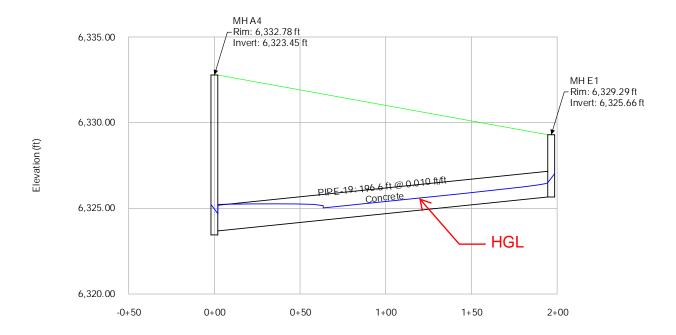
Profile Report **100 Year** Engineering Profile - STRM LINE D (Meadowbrook Park.stsw)



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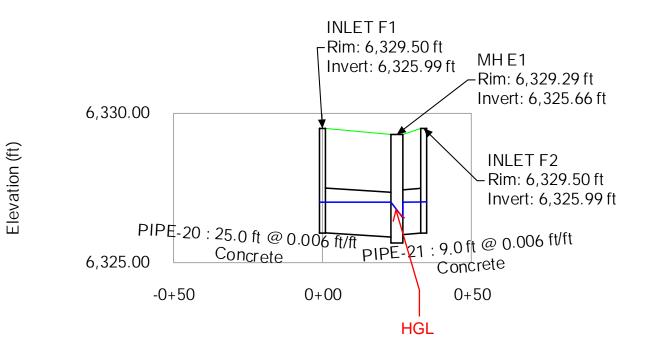
Profile Report **100 Year** Engineering Profile - STRM LINE E (Meadowbrook Park.stsw)



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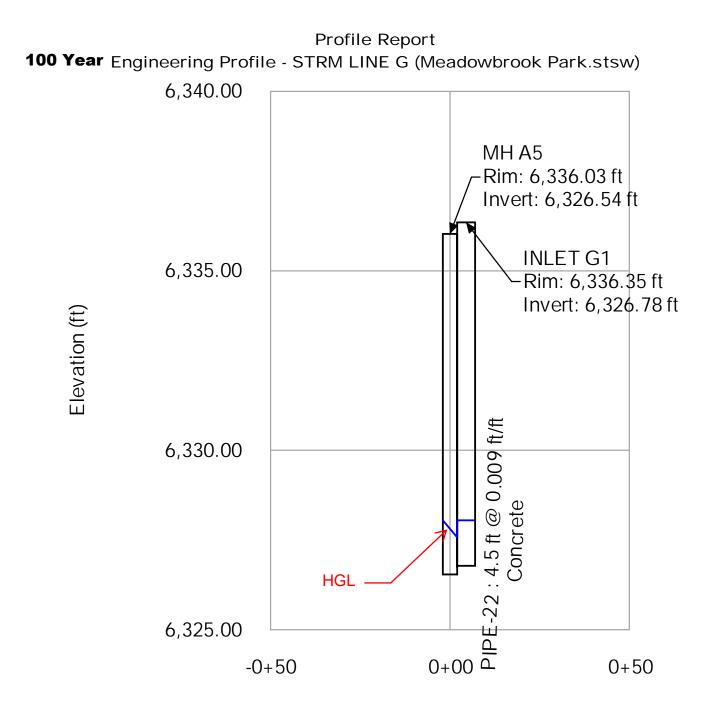
Profile Report **100 Year** Engineering Profile - STRM LINE F (Meadowbrook Park.stsw)



Station (ft)

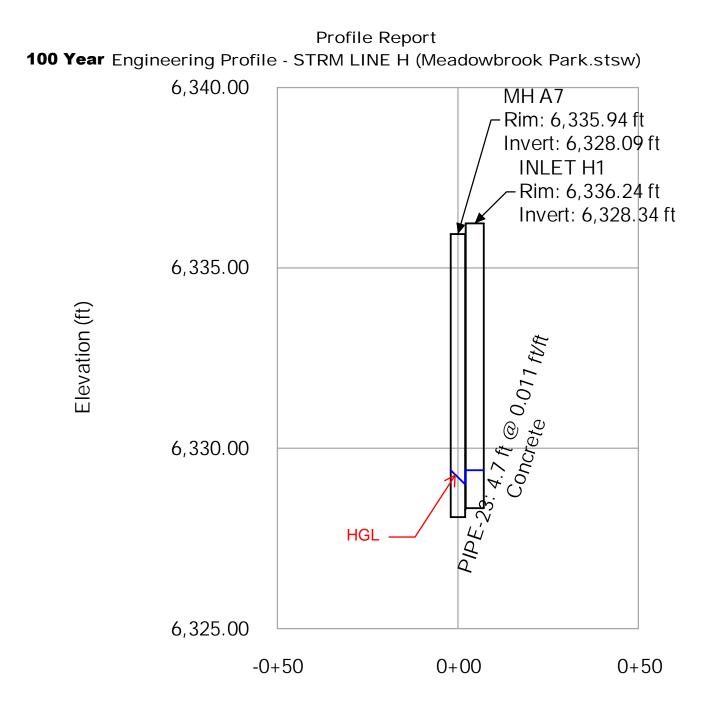
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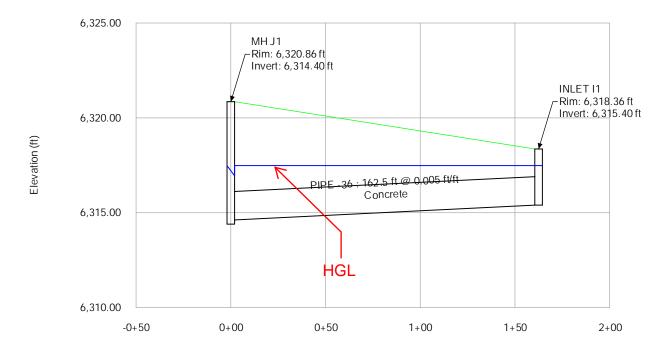
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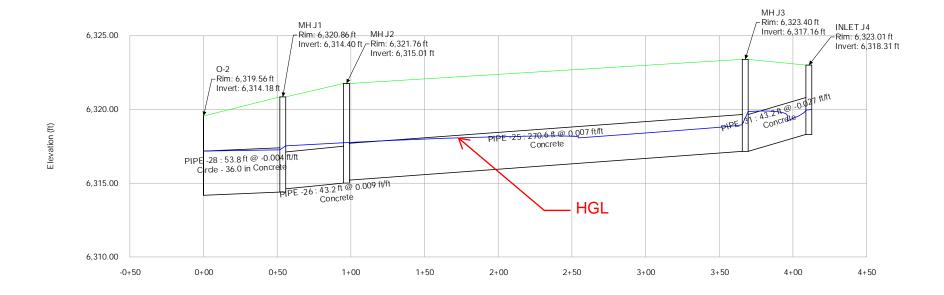
Profile Report **100 Year** Engineering Profile - STRM LINE I (Meadowbrook Park.stsw)



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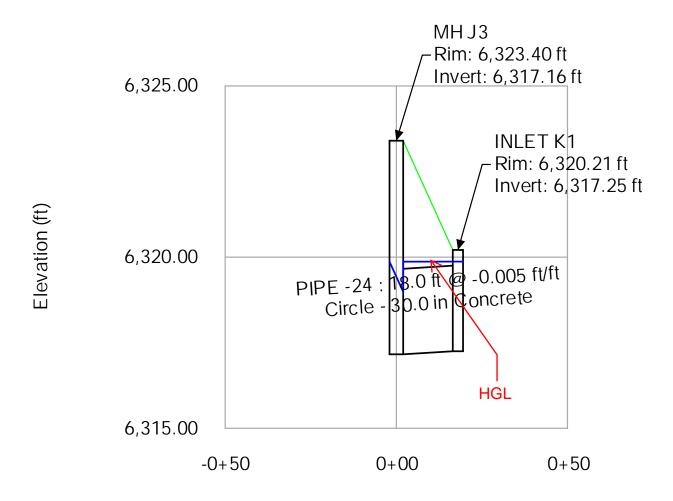
Profile Report **100 Year** Engineering Profile - STRM LINE J (Meadowbrook Park.stsw)



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Profile Report **100 Year** Engineering Profile - STRM LINE K (Meadowbrook Park.stsw)



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#### Version 4.06 Released August 2018

#### INLET MANAGEMENT

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LET NAME	Design Point 3	Design Point 4	Design Point 5	Design Point 6	Design Point 7	Design Point 8
e Type (Urban or Rural)						
et Application (Street or Area)	STREET	STREET	STREET	STREET	STREET	STREET
draulic Condition	On Grade	In Sump	On Grade	In Sump	In Sump	In Sump
ет Туре	CDOT Type R Curb Opening					
-DEFINED INPUT						
er-Defined Design Flows						
nor Q <sub>Known</sub> (cfs)	0.8	1.4	1.4	0.4	1.7	1.7
ajor Q <sub>Known</sub> (cfs)	1.5	3.4	2.7	0.8	4.0	3.9
pass (Carry-Over) Flow from Upstream eceive Bypass Flow from:	No Bypass Flow Received	User-Defined	User-Defined	No Bypass Flow Received	No Bypass Flow Received	User-Defined
nor Bypass Flow Received, Q <sub>h</sub> (cfs)	0.0	0.0	0.0	0.0	0.0	0.0
ajor Bypass Flow Received, Q <sub>b</sub> (cfs)	0.0	0.0	0.0	0.0	0.0	0.0
ijor Bypass Flow Received, Qb (CIS)	0.0	0.1	0.1	0.0	0.0	0.2
tershed Characteristics						
bcatchment Area (acres)						
ercent Impervious						
RCS Soil Type						
atershed Profile						
verland Slope (ft/ft)						
verland Length (ft)						
nannel Slope (ft/ft)						
nannel Length (ft)						
inor Storm Rainfall Input						
esign Storm Return Period, Tr (years)						
ne-Hour Precipitation, P1 (inches)						
ajor Storm Rainfall Input						
esign Storm Return Period, T <sub>r</sub> (years)						
ne-Hour Precipitation, P1 (inches)				l		
CULATED OUTPUT						
nor Total Design Peak Flow, Q (cfs)	0.8	1.4	1.4	0.4	1.7	1.7
ajor Total Design Peak Flow, Q (cfs)	1.5	3.5	2.8	0.8	4.0	4.1
nor Flow Bypassed Downstream, Q <sub>b</sub> (cfs)	0.0	N/A	0.0	N/A	N/A	N/A
ajor Flow Bypassed Downstream, Qb (cfs)	0.1	N/A	0.7	N/A	N/A	N/A
nor Storm (Calculated) Analysis of Flow Ti	me					
ne. eterm (ouloulded) Analysis of Flow T	N/A	N/A	N/A	N/A	N/A	N/A
	N/A	N/A	N/A	N/A	N/A	N/A
erland Flow Velocity, Vi	N/A N/A	N/A	N/A	N/A	N/A	N/A
annel Flow Velocity, Vt	N/A	N/A	N/A	N/A	N/A	N/A
rerland Flow Time. Ti	N/A N/A	N/A	N/A	N/A	N/A	N/A
annel Travel Time, Tt	N/A N/A	N/A	N/A N/A	N/A N/A	N/A N/A	N/A N/A
culated Time of Concentration, $T_c$	N/A N/A	N/A	N/A N/A	N/A N/A	N/A N/A	N/A N/A
gional T <sub>c</sub>	N/A N/A	N/A N/A	N/A N/A	N/A N/A	N/A N/A	N/A N/A
ecommended T <sub>c</sub>	N/A N/A	N/A N/A	N/A N/A	N/A N/A	N/A N/A	N/A N/A
selected by User	N/A N/A	N/A N/A	N/A N/A	N/A N/A	N/A N/A	N/A N/A
	N/A N/A	N/A N/A	N/A N/A	N/A N/A	N/A N/A	
esign Rainfall Intensity, I Ilculated Local Peak Flow, Q <sub>p</sub>				N/A N/A		N/A N/A
iculated Local Peak Flow, Qp	N/A	N/A	N/A	N/A	N/A	N/A
lajor Storm (Calculated) Analysis of Flow Ti	N/A	N/A	N/A	N/A	N/A	N/A

υ U	N/A	N/A	N/A	N/A	N/A	N/A
C <sub>5</sub>	N/A	N/A	N/A	N/A	N/A	N/A
Overland Flow Velocity, Vi	N/A	N/A	N/A	N/A	N/A	N/A
Channel Flow Velocity, Vt	N/A	N/A	N/A	N/A	N/A	N/A
Overland Flow Time, Ti	N/A	N/A	N/A	N/A	N/A	N/A
Channel Travel Time, Tt Calculated Time of Concentration, T <sub>c</sub>	N/A	N/A	N/A	N/A	N/A	N/A
	N/A	N/A	N/A	N/A	N/A	N/A
Regional T <sub>c</sub>	N/A	N/A	N/A	N/A	N/A	N/A
Recommended T <sub>c</sub>	N/A	N/A	N/A	N/A	N/A	N/A
T <sub>c</sub> selected by User	N/A	N/A	N/A	N/A	N/A	N/A
Design Rainfall Intensity, I	N/A	N/A	N/A	N/A	N/A	N/A
Calculated Local Peak Flow, Qp	N/A	N/A	N/A	N/A	N/A	N/A

#### Version 4.06 Released August 2018

#### INLET MANAGEMENT

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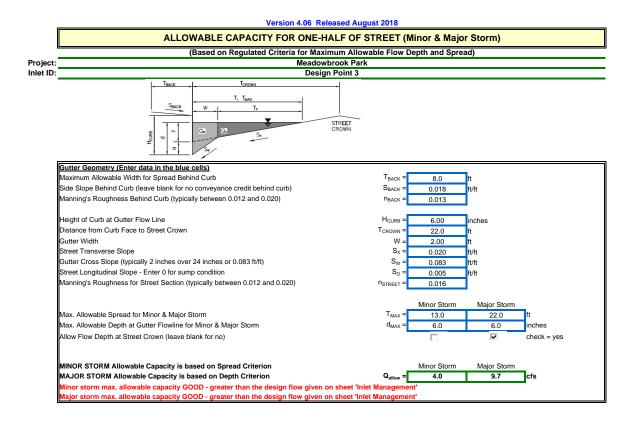
INLET NAME	Design Point 9		Design Point 11
Site Type (Urban or Rural)			RURAL
Inlet Application (Street or Area)	STREET	STREET	AREA
Hydraulic Condition	On Grade	On Grade	Swale
Inlet Type	CDOT Type R Curb Opening	CDOT Type R Curb Opening	CDOT Type D (In Series & Depressed)

#### USER-DEFINED INPUT

Vinor Q <sub>Known</sub> (cfs)	0.8	0.8	10.7
Major Q <sub>Known</sub> (cfs)	1.7	1.5	23.5
		110	2010
Bypass (Carry-Over) Flow from Upstream			
Receive Bypass Flow from:	No Bypass Flow Received	No Bypass Flow Received	No Bypass Flow Received
Minor Bypass Flow Received, Qb (cfs)	0.0	0.0	0.0
Major Bypass Flow Received, Qb (cfs)	0.0	0.0	0.0
Watershed Characteristics			
Subcatchment Area (acres)			
Percent Impervious			
NRCS Soil Type			
Watershed Profile			
Watershed Profile Overland Slope (ft/ft)			
Overland Slope (ft/ft)			
Overland Slope (ft/ft) Overland Length (ft)			
Overland Slope (ft/ft) Overland Length (ft) Channel Slope (ft/ft)			
Overland Slope (ft/ft) Overland Length (ft) Channel Slope (ft/ft)			
Overland Slope (ft/ft) Overland Length (ft) Channel Slope (ft/ft) Channel Length (ft)			
Overland Slope (ft/ft) Overland Length (ft) Channel Slope (ft/ft) Channel Length (ft) Minor Storm Rainfall Input			
Overland Slope (ft/ft) Overland Length (ft) Channel Slope (ft/ft) Channel Length (ft) Minor Storm Rainfall Input Design Storm Return Period, T <sub>r</sub> (years)			
Overland Slope (ft/ft) Overland Length (ft) Channel Slope (ft/ft) Channel Length (ft) Minor Storm Rainfall Input Design Storm Return Period, T <sub>r</sub> (years)			
Overland Slope (ft/ft) Overland Length (ft) Channel Slope (ft/ft) Channel Length (ft) Minor Storm Rainfall Input Design Storm Return Period, T <sub>r</sub> (years) One-Hour Precipitation, P <sub>1</sub> (inches)			

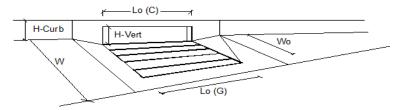
#### CALCULATED OUTPUT

Minor Total Design Peak Flow, Q (cfs)	0.8	0.8	10.7
lajor Total Design Peak Flow, Q (cfs)	1.7	1.5	23.5
linor Flow Bypassed Downstream, Q <sub>b</sub> (cfs)	0.0	0.0	0.0
Major Flow Bypassed Downstream, Qb (cfs)	0.2	0.1	0.0
Minor Storm (Calculated) Analysis of Flow T			
	N/A	N/A	N/A
5	N/A	N/A	N/A
Overland Flow Velocity, Vi	N/A	N/A	N/A
Channel Flow Velocity, Vt	N/A	N/A	N/A
verland Flow Time, Ti	N/A	N/A	N/A
hannel Travel Time, Tt	N/A	N/A	N/A
alculated Time of Concentration, T <sub>c</sub>	N/A	N/A	N/A
egional T <sub>c</sub>	N/A	N/A	N/A
ecommended T <sub>c</sub>	N/A	N/A	N/A
c selected by User	N/A	N/A	N/A
Design Rainfall Intensity, I	N/A	N/A	N/A
Calculated Local Peak Flow, Qp	N/A	N/A	N/A
Major Storm (Calculated) Analysis of Flow T			
	N/A	N/A	N/A
25	N/A	N/A	N/A
overland Flow Velocity, Vi	N/A	N/A	N/A
Channel Flow Velocity, Vt	N/A	N/A	N/A
Overland Flow Time, Ti	N/A	N/A	N/A
hannel Travel Time, Tt	N/A	N/A	N/A
Calculated Time of Concentration, T <sub>c</sub>	N/A	N/A	N/A
Regional T <sub>c</sub>	N/A	N/A	N/A
Recommended T <sub>c</sub>	N/A	N/A	N/A
c selected by User	N/A	N/A	N/A
Design Rainfall Intensity, I	N/A	N/A	N/A
Calculated Local Peak Flow, Qn	N/A	N/A	N/A

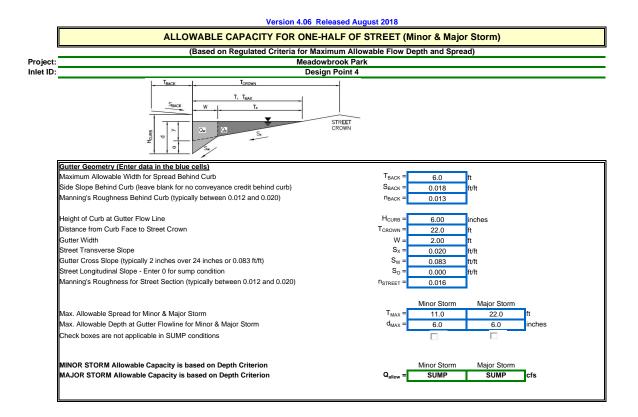


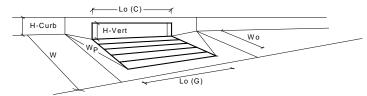
## INLET ON A CONTINUOUS GRADE

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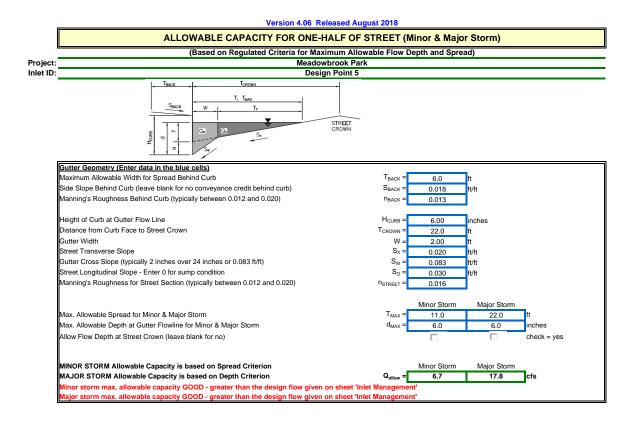


Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a <sub>LOCAL</sub> =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L <sub>o</sub> =	5.00	5.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W <sub>o</sub> =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C <sub>f</sub> -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C <sub>f</sub> -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'	_	MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	0.8	1.4	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q <sub>b</sub> =	0.0	0.1	cfs
Capture Percentage = Q <sub>a</sub> /Q <sub>o</sub> =	C% =	100	94	%



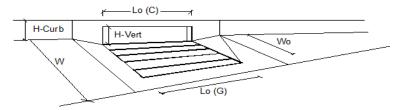


Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a <sub>local</sub> =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	4.2	6.0	inches
Grate Information		MINOR	MAJOR	Override Depths
Length of a Unit Grate	L <sub>o</sub> (G) =	N/A	N/A	feet
Width of a Unit Grate	W <sub>o</sub> =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A <sub>ratio</sub> =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	C <sub>f</sub> (G) =	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C <sub>w</sub> (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	C <sub>0</sub> (G) =	N/A	N/A	
Curb Opening Information		MINOR	MAJOR	
Length of a Unit Curb Opening	$L_{o}(C) =$	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H <sub>vert</sub> =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H <sub>throat</sub> =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W <sub>p</sub> =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_{f}(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	C <sub>w</sub> (C) =	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_{o}(C) =$	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d <sub>Grate</sub> =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d <sub>Curb</sub> =	0.18	0.33	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF <sub>Combination</sub> =	0.53	0.77	
Curb Opening Performance Reduction Factor for Long Inlets	RF <sub>Curb</sub> =	1.00	1.00	
Grated Inlet Performance Reduction Factor for Long Inlets	RF <sub>Grate</sub> =	N/A	N/A	
		MINOR	MAJOR	
Total Inlet Interception Capacity (assumes clogged condition)	<b>Q</b> <sub>a</sub> =	2.1	5.4	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	1.4	3.5	cfs

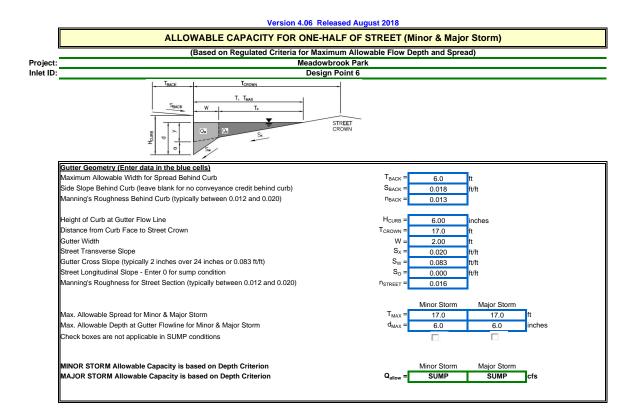


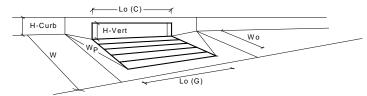
## INLET ON A CONTINUOUS GRADE

Version 4.06 Released August 2018

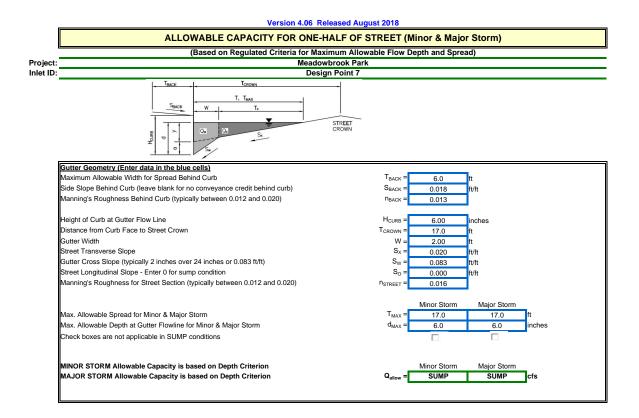


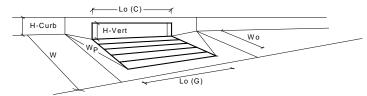
Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type F	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a <sub>LOCAL</sub> =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L <sub>o</sub> =	5.00	5.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W <sub>o</sub> =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C <sub>f</sub> -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C <sub>f</sub> -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'	_	MINOR	MAJOR	_
Total Inlet Interception Capacity	Q =	1.3	2.1	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q <sub>b</sub> =	0.0	0.7	cfs
Capture Percentage = Q <sub>a</sub> /Q <sub>o</sub> =	C% =	97	76	%



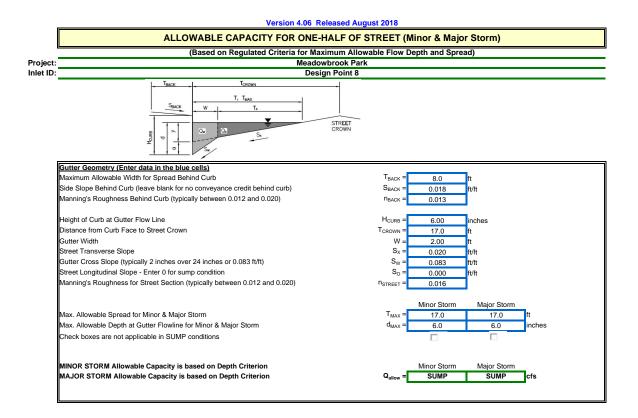


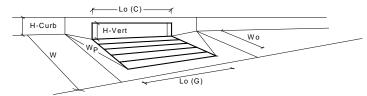
Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a <sub>local</sub> =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	5.6	5.6	inches
Grate Information		MINOR	MAJOR	Override Depths
Length of a Unit Grate	$L_{o}(G) =$	N/A	N/A	feet
Width of a Unit Grate	W <sub>o</sub> =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A <sub>ratio</sub> =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_{f}(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C <sub>w</sub> (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	$C_o(G) =$	N/A	N/A	
Curb Opening Information		MINOR	MAJOR	
Length of a Unit Curb Opening	$L_{o}(C) =$	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H <sub>vert</sub> =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H <sub>throat</sub> =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W <sub>p</sub> =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_{f}(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	C <sub>w</sub> (C) =	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_{o}(C) =$	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d <sub>Grate</sub> =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d <sub>Curb</sub> =	0.30	0.30	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF <sub>Combination</sub> =	0.72	0.72	
Curb Opening Performance Reduction Factor for Long Inlets	RF <sub>Curb</sub> =	1.00	1.00	
Grated Inlet Performance Reduction Factor for Long Inlets	RF <sub>Grate</sub> =	N/A	N/A	]
		MINOR	MAJOR	
Total Inlet Interception Capacity (assumes clogged condition)	<b>Q</b> <sub>a</sub> =	4.6	4.6	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	0.4	0.8	cfs



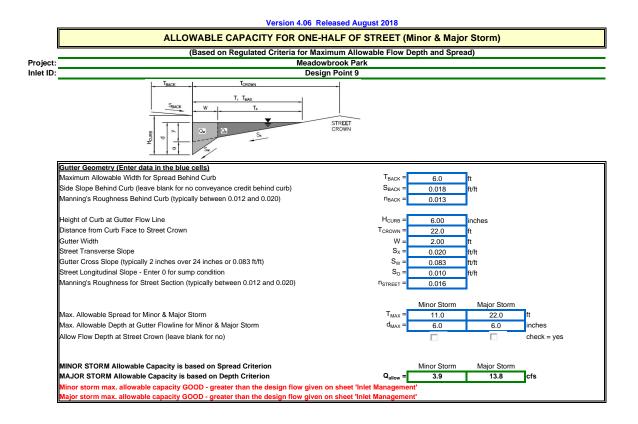


Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a <sub>local</sub> =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	5.6	5.6	inches
Grate Information		MINOR	MAJOR	Override Depths
Length of a Unit Grate	L <sub>o</sub> (G) =	N/A	N/A	feet
Width of a Unit Grate	W <sub>o</sub> =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A <sub>ratio</sub> =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	C <sub>f</sub> (G) =	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C <sub>w</sub> (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	C <sub>o</sub> (G) =	N/A	N/A	
Curb Opening Information		MINOR	MAJOR	
Length of a Unit Curb Opening	$L_{o}(C) =$	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H <sub>vert</sub> =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H <sub>throat</sub> =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W <sub>p</sub> =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_{f}(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	C <sub>w</sub> (C) =	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_{o}(C) =$	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d <sub>Grate</sub> =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d <sub>Curb</sub> =	0.30	0.30	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF <sub>Combination</sub> =	0.72	0.72	
Curb Opening Performance Reduction Factor for Long Inlets	RF <sub>Curb</sub> =	1.00	1.00	
Grated Inlet Performance Reduction Factor for Long Inlets	RF <sub>Grate</sub> =	N/A	N/A	
		MINOR	MAJOR	
Total Inlet Interception Capacity (assumes clogged condition)	Q <sub>a</sub> =	4.6	4.6	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	1.7	4.0	cfs



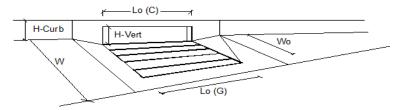


Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a <sub>local</sub> =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	5.6	5.6	inches
Grate Information		MINOR	MAJOR	Override Depths
Length of a Unit Grate	$L_{o}(G) =$	N/A	N/A	feet
Width of a Unit Grate	W <sub>o</sub> =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A <sub>ratio</sub> =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_{f}(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C <sub>w</sub> (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	$C_o(G) =$	N/A	N/A	
Curb Opening Information		MINOR	MAJOR	
Length of a Unit Curb Opening	$L_{o}(C) =$	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H <sub>vert</sub> =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H <sub>throat</sub> =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W <sub>p</sub> =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_{f}(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	C <sub>w</sub> (C) =	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_{o}(C) =$	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d <sub>Grate</sub> =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d <sub>Curb</sub> =	0.30	0.30	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF <sub>Combination</sub> =	0.72	0.72	
Curb Opening Performance Reduction Factor for Long Inlets	RF <sub>Curb</sub> =	1.00	1.00	
Grated Inlet Performance Reduction Factor for Long Inlets	RF <sub>Grate</sub> =	N/A	N/A	
		MINOR	MAJOR	
Total Inlet Interception Capacity (assumes clogged condition)	Q <sub>a</sub> =	4.6	4.6	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	1.7	4.1	cfs

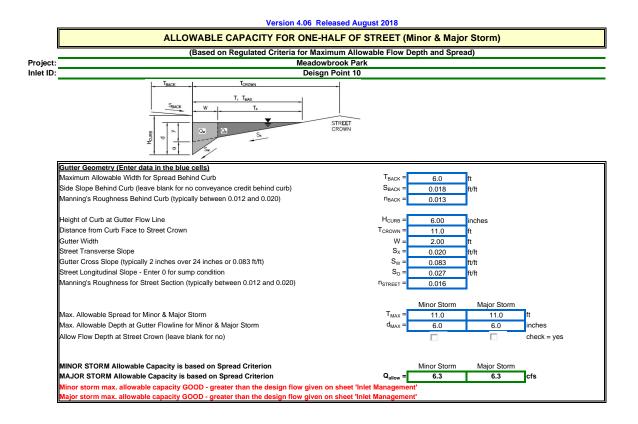


## INLET ON A CONTINUOUS GRADE

Version 4.06 Released August 2018

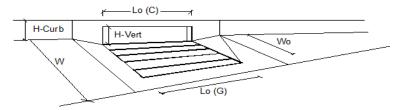


Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type F	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a <sub>LOCAL</sub> =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L <sub>o</sub> =	5.00	5.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W <sub>o</sub> =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C <sub>f</sub> -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C <sub>f</sub> -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'	_	MINOR	MAJOR	_
Total Inlet Interception Capacity	Q =	0.8	1.6	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q <sub>b</sub> =	0.0	0.2	cfs
Capture Percentage = Q <sub>a</sub> /Q <sub>o</sub> =	C% =	100	91	%



## INLET ON A CONTINUOUS GRADE

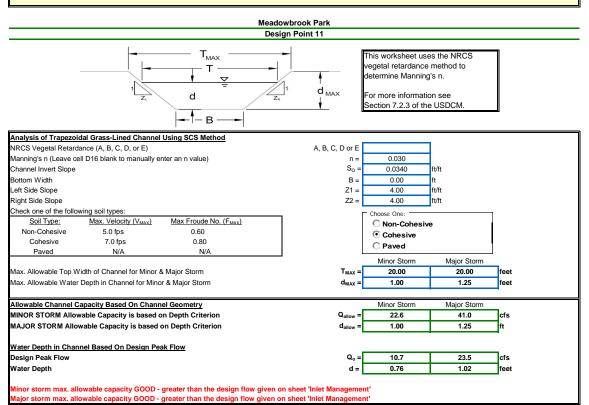
Version 4.06 Released August 2018



Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type F	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a <sub>LOCAL</sub> =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L <sub>o</sub> =	5.00	5.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W <sub>o</sub> =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C <sub>f</sub> -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C <sub>f</sub> -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'	_	MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	0.7	1.5	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q <sub>b</sub> =	0.0	0.1	cfs
Capture Percentage = Q <sub>a</sub> /Q <sub>o</sub> =	C% =	100	95	%

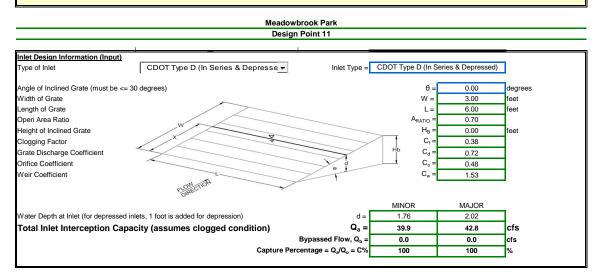
#### Version 4.06 Released August 2018

#### AREA INLET IN A SWALE



Version 4.06 Released August 2018

#### AREA INLET IN A SWALE



Warning 04: Froude No. exceeds USDCM Volume I recommendation.

**OPINION OF PROBABLE CONSTRUCTION COST** 

# Kimley **»Horn**

## Kimley-Horn & Associates, Inc.

## **Opinion of Probable Construction Cost**

Client:	Meadowbrook Development, LLC	Date:		3/12/2021
Project:	Meadowbrook Park	Prepared By:		KRK
KHA No.	: 096956009	Checked By:		EJG
		Sheet:	1 of 1	

This OPC is not intended for basing financial decisions, or securing funding. Review all notes and assumptions. Since Kimley-Horn & Associates, Inc. has no control over the cost of labor, materials, equipment, or services furnished by others, or over methods of determining price, or over competitive bidding or market conditions, any and all opinions as to the cost herein, including but not limited to opinions as to the costs of construction materials, shall be made on the basis of experience and best available data. Kimley-Horn & Associates, Inc. cannot and does not guarantee that proposals, bids, or actual costs will not vary from the opinions on costs shown herein. The total costs and other numbers in this Opinion of Probable Cost have been rounded.

Item No.	Item Description	Quantity	Unit	Unit Price	Item Cost
	Private Storm Sewer - Non-Reimbur	sable			
1	18" RCP	1,092	LF	\$65.00	\$70,980
2	24" RCP	254	LF	\$78.00	\$19,812
3	30" RCP	375	LF	\$97.00	\$36,375
4	36" RCP	46	LF	\$120.00	\$960
5	5' Type R Inlet	8	EA	\$5,736.00	\$45,888
6	CDOT Type D Inlet	2	EA	\$5,932.00	\$11,864
7	CDOT Type C Inlet	1	EA	\$4,802.00	\$4,802
8	Modifed Type C Inlet	1	EA	\$10,000.00	\$10,000
9	8" Area Drain	2	EA	\$500.00	\$1,000
10	4' Type II Manhole	8	EA	\$6,619.00	\$52,952
11	5' Type II Manhole	4	EA	\$12,034.00	\$48,136
12	Concrete Forebay	2	EA	\$7,500.00	\$15,000
13	Concrete Trickle Channel	330	LF	\$10.00	\$3,300
14	Maintenance Road Material (CDOT Class 6 Base)	36	CY	\$85.00	\$3,060
15	Emergency Overflow (Type L Riprap)	20	Ton	\$83.00	\$1,660
16	Rock Chute (Type L Riprap)	110	Ton	\$83.00	\$9,130
		Subtotal:			\$334,919
		Contingency	/ (%,+/-)	10%	\$33,492
		Project Tota	al:		\$368,411

#### **Basis for Cost Projection:**

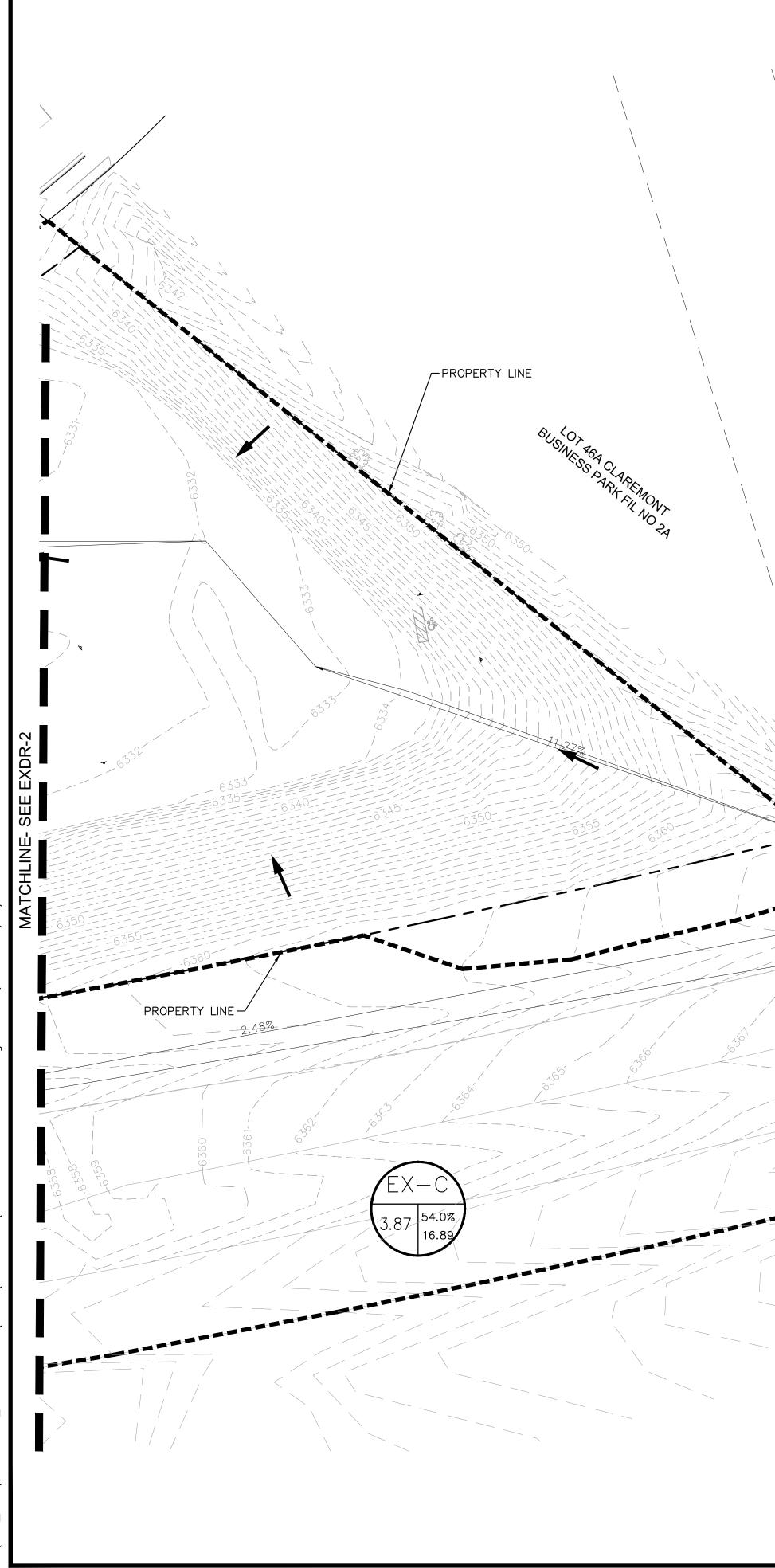
No Design Completed

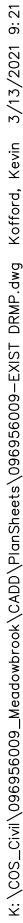
Preliminary Design

✓ Final Design

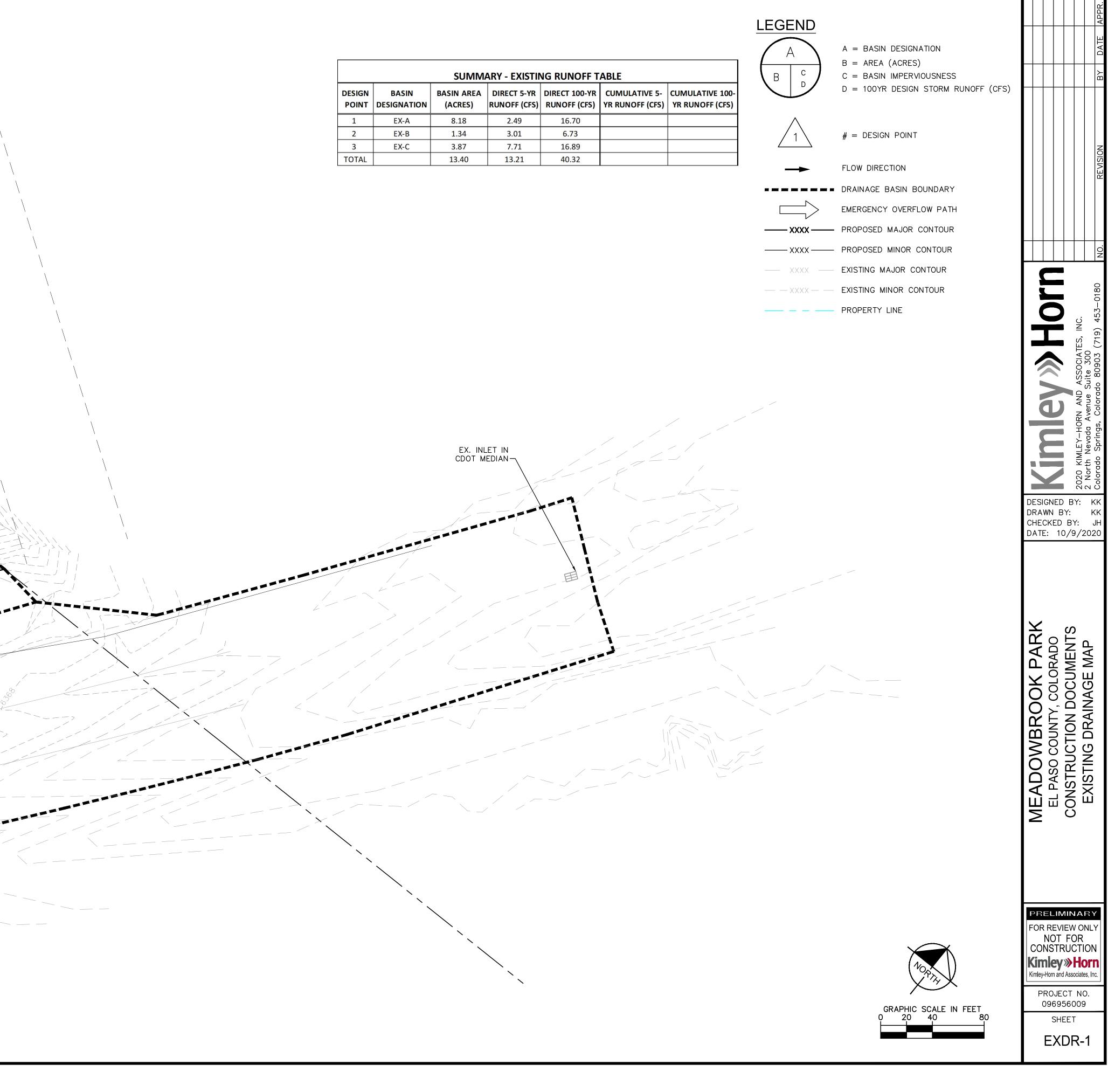
Design Engineer:

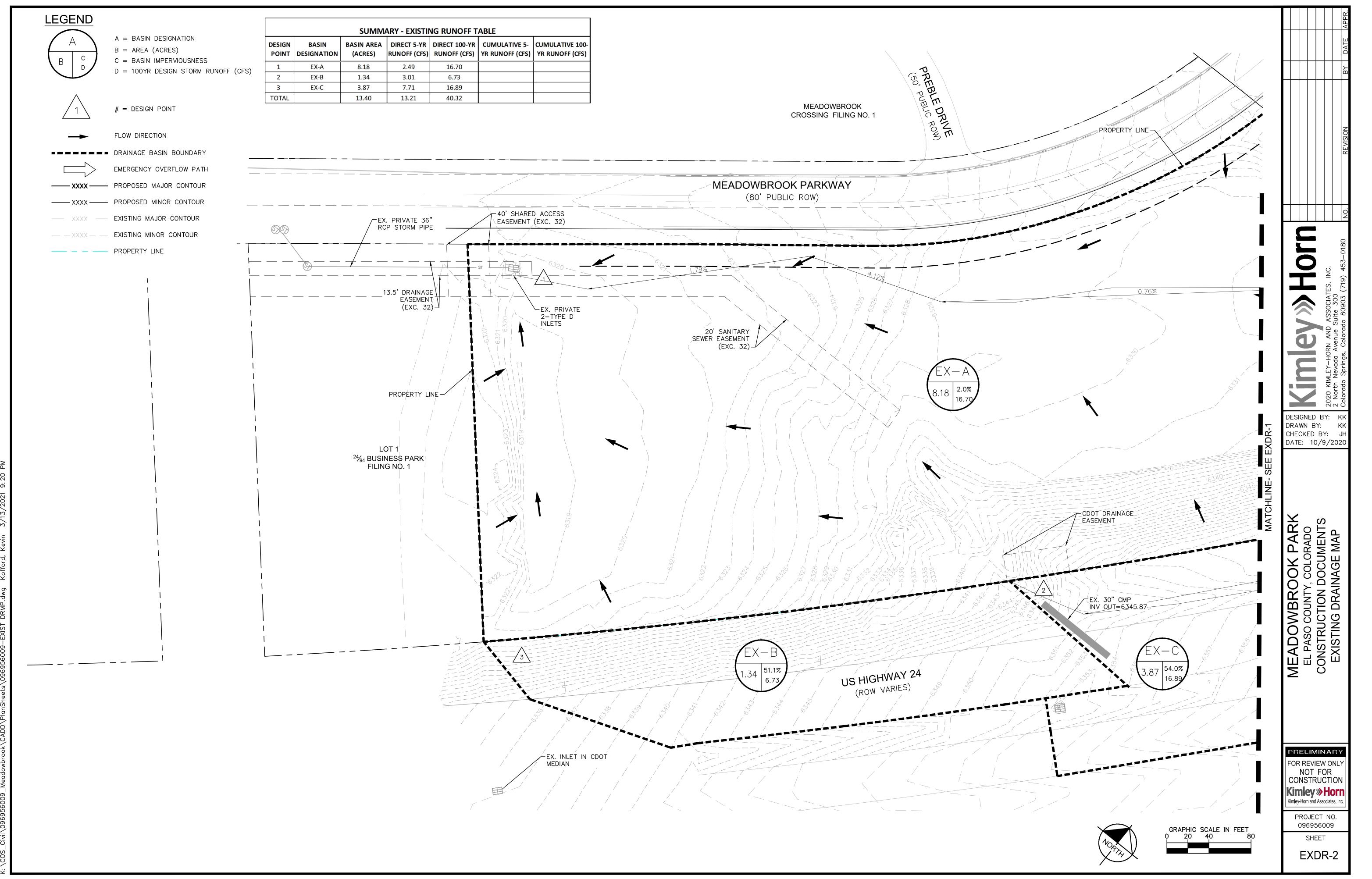
EXISTING AND PROPOSED DRAINAGE MAP

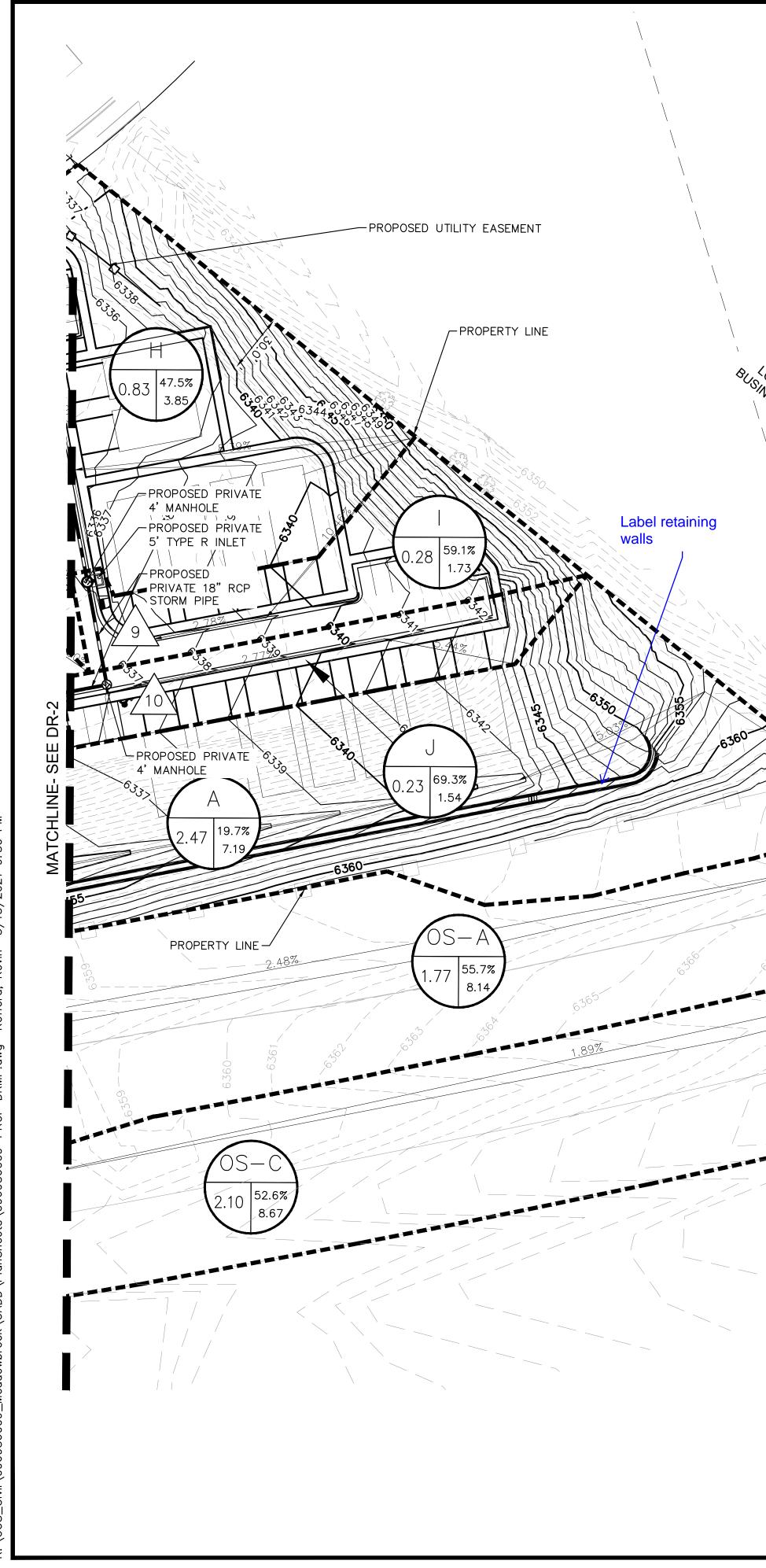




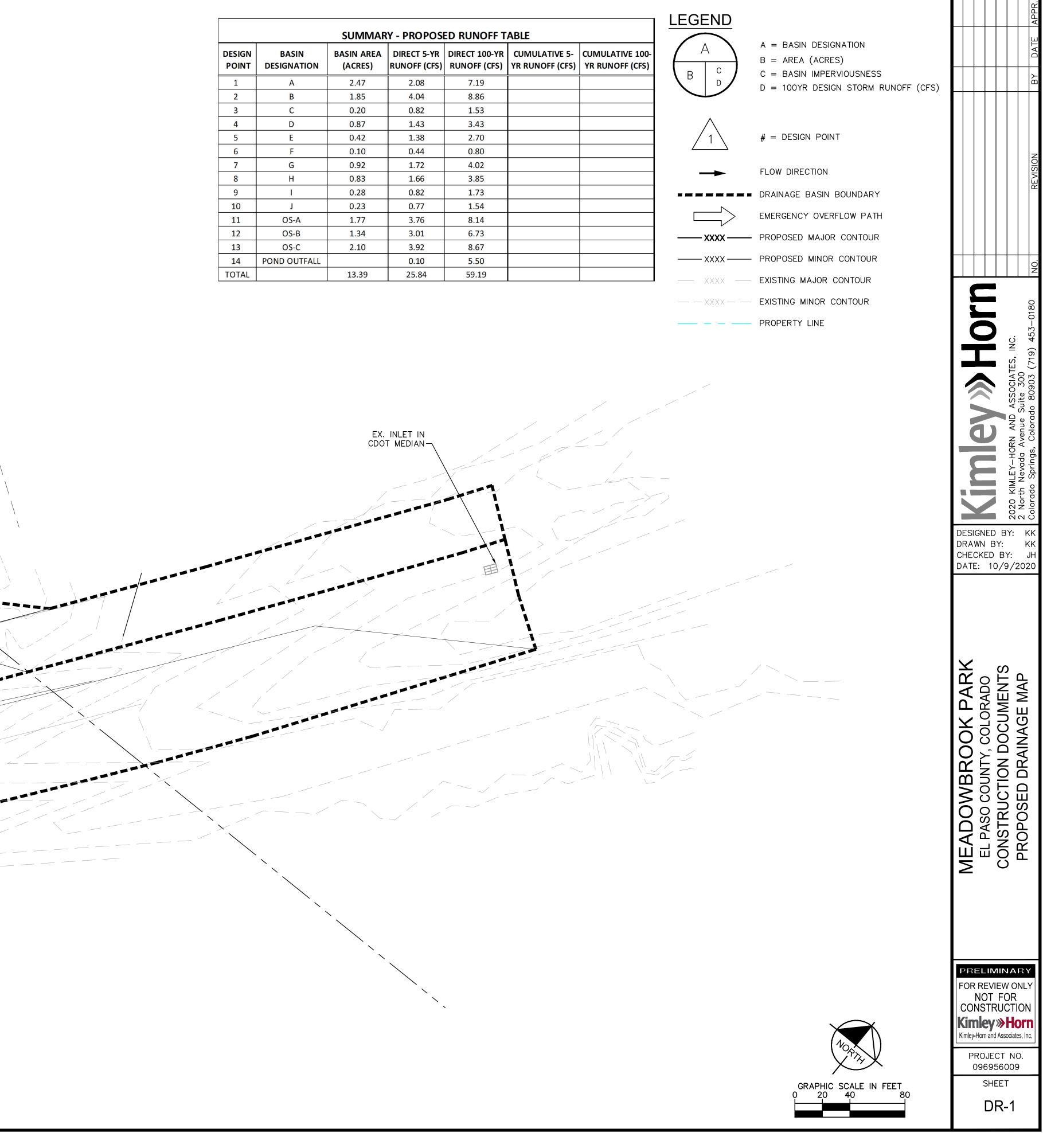
SUMMARY - EXISTING RUNOFF TABLE						
DESIGN POINT	BASIN DESIGNATION	BASIN AREA (ACRES)	DIRECT 5-YR RUNOFF (CFS)	DIRECT 100-YR RUNOFF (CFS)	CUMU YR RUI	
1	EX-A	8.18	2.49	16.70		
2	EX-B	1.34	3.01	6.73		
3	EX-C	3.87	7.71	16.89		
TOTAL		13.40	13.21	40.32		

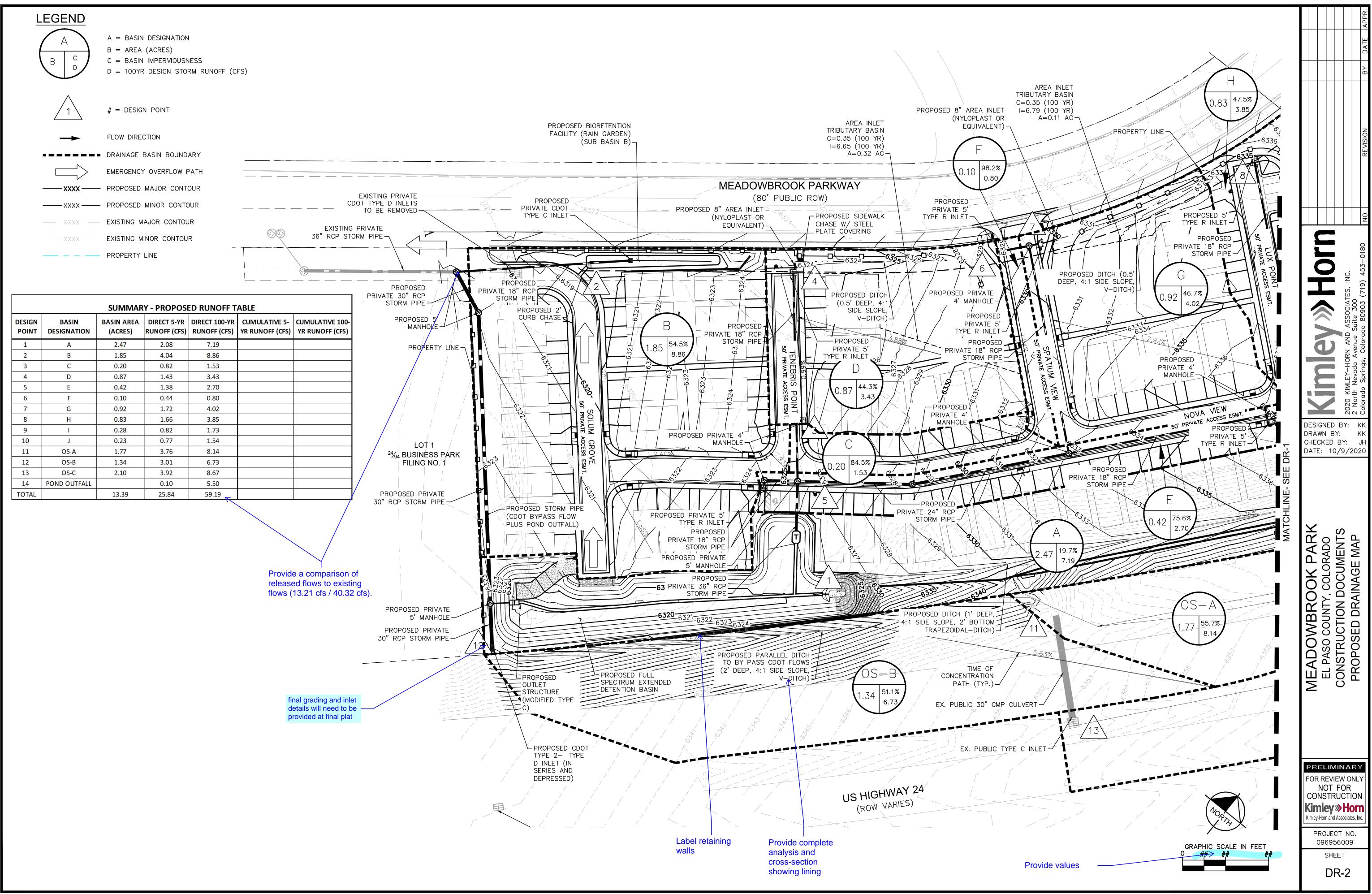




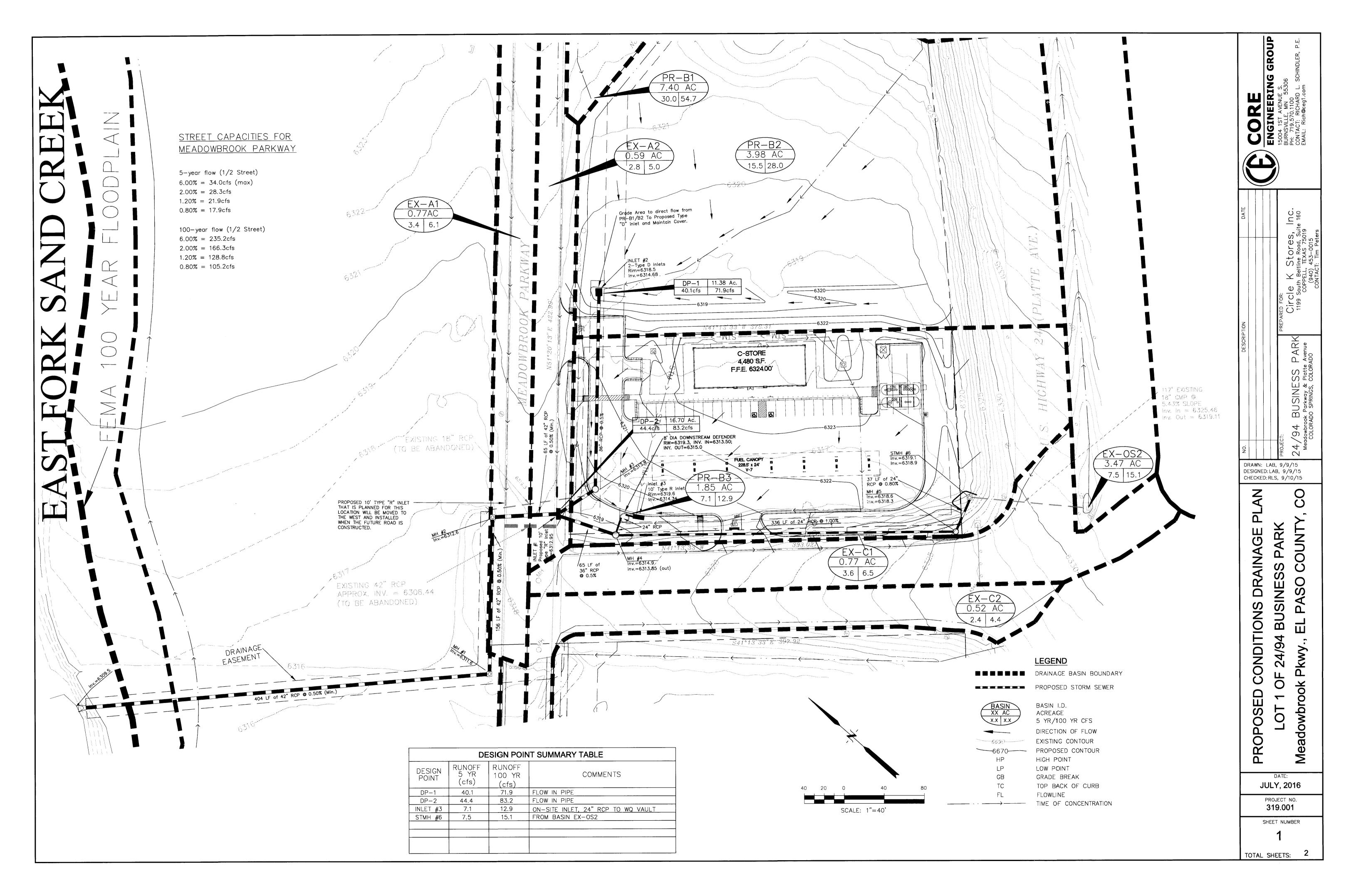


SUMMARY - PROPOSED RUNOFF TABLE							
DESIGN POINT	BASIN DESIGNATION	BASIN AREA (ACRES)	DIRECT 5-YR RUNOFF (CFS)	DIRECT 100-YR RUNOFF (CFS)	CUN YR R		
1	A	2.47	2.08	7.19			
2	В	1.85	4.04	8.86			
3	С	0.20	0.82	1.53			
4	D	0.87	1.43	3.43			
5	E	0.42	1.38	2.70			
6	F	0.10	0.44	0.80			
7	G	0.92	1.72	4.02			
8	Н	0.83	1.66	3.85			
9	I	0.28	0.82	1.73			
10	J	0.23	0.77	1.54			
11	OS-A	1.77	3.76	8.14			
12	OS-B	1.34	3.01	6.73			
13	OS-C	2.10	3.92	8.67			
14	POND OUTFALL		0.10	5.50			
TOTAL		13.39	25.84	59.19			





PRIVATE - STO	SUMMARY - PROPOSED RUNOFF TABLE						
P		CUMULATIVE 5- YR RUNOFF (CFS)	DIRECT 100-YR RUNOFF (CFS)	DIRECT 5-YR RUNOFF (CFS)	BASIN AREA (ACRES)	BASIN DESIGNATION	DESIGN POINT
			7.19	2.08	2.47	А	1
			8.86	4.04	1.85	В	2
			1.53	0.82	0.20	С	3
			3.43	1.43	0.87	D	4
			2.70	1.38	0.42	E	5
,			0.80	0.44	0.10	F	6
/			4.02	1.72	0.92	G	7
			3.85	1.66	0.83	Н	8
			1.73	0.82	0.28	I	9
			1.54	0.77	0.23	J	10
24/9.			8.14	3.76	1.77	OS-A	11
/9/			6.73	3.01	1.34	OS-B	12
			8.67	3.92	2.10	OS-C	13
/			5.50	0.10		POND OUTFALL	14
PROP			59.19	25.84	13.39		TOTAL
30" RCI	/		'				



x