Please refer to comments provided on the drainage report for PPR2322 and revise accordingly.

DRAINAGE LETTER REPORT

for

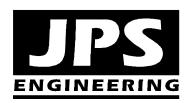
SHOPS AT MERIDIAN RANCH CONVENIENCE STORE 11810 STAPLETON DRIVE LOT 2, THE SHOPS FILING NO. 1A AT MERIDIAN RANCH

Prepared for:

Hunjan Gas Stations LLC 12599 Mt. Lindsey Drive Peyton, CO 80831

March 31, 2023

Prepared by:



19 E. Willamette Ave. Colorado Springs, CO 80903 (719)-477-9429 www.jpsengr.com

JPS Project No. 092202 PCD Filing No. PPR____

Please add "VR2314 & PPR2322"

SHOPS AT MERIDIAN RANCH CONVENIENCE STORE DRAINAGE LETTER REPORT <u>TABLE OF CONTENTS</u>

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DRAINAGE STATEMENT

Engineer's Statement:

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the County for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for liability caused by negligent acts, errors or omissions on my part in preparing this report.

John P. Schwab, P.E. #29891

Developer's Statement:

I, the developer have read and will comply with all of the requirements specified in this drainage report and plan.

By:

Date

Hunjan Gas Stations LLC 12599 Mt. Lindsey Drive, Peyton, CO 80831

El Paso County's Statement

Filed in accordance with the requirements of the El Paso County Land Development Code, Drainage Criteria Manual, Volumes 1 and 2, and Engineering Criteria Manual as amended.

Joshua Palmer, P.E. County Engineer / ECM Administrator Date

Conditions:

I. INTRODUCTION

A. Property Location and Description

Hunjan Gas Stations LLC (Owner) is planning to construct a new Convenience Store on the vacant 1.46-acre property in the Shops at Meridian Ranch commercial area northeast of Stapleton Drive and Meridian Road in the Falcon area of El Paso County, Colorado. The property is currently described as part of Lot 2, The Shops Filing No. 1 at Meridian Ranch (El Paso County Assessor's Parcel Number 42303-19-056).

The project consists of a new 12,000 square-foot, single-story Convenience Store and Gas Station with associated parking and site improvements. The property adjoins Stapleton Drive on the south side, which is a fully improved, asphalt-paved arterial public street. The property is bounded by an existing shared private driveway along the north and east sides. The west boundary of the site adjoins a vacant 1.0-acre commercial tract currently described as the balance of Lot 2, The Shops Filing No. 1 at Meridian Ranch (El Paso County Assessor's Parcel Number 42303-19-055).

The property is zoned Commercial Regional District (CR), and the proposed site development is fully consistent with the existing zoning of the site. Access to the site will be provided by new connections to the existing shared private driveways adjoining the north and east boundaries of the site.

The site is located in the Bennett Ranch Drainage Basin, and surface drainage from this site sheet flows southeasterly to an existing private storm sewer system draining easterly across the property, ultimately flowing to the existing Bennett Regional Detention Pond.

This report is intended to meet the requirements of a site-specific "Letter Type" drainage report in accordance with El Paso County subdivision drainage criteria.

B. Drainage Analysis Methods and Criteria

ITEM	DESCRIPTION	REFERENCE
Design Storm (initial/major)	5-year/100-year	CS/EPC DCM
Storm Runoff	Rational Method (Area<100acres)	CS/EPC DCM
Major Drainage Basin	Bennett Ranch	
Floodplain Impacts	Parcel is located outside any delineated	FIRM
	FEMA floodplains	
Existing Downstream	Existing storm sewer system flowing to	
Facilities	Bennett Regional Detention Pond	

CS/EPC DCM = City of Colorado Springs & El Paso County Drainage Criteria Manual

C. References

Olsson Associates, "Drainage Letter – Lot 3, The Shops at Meridian Ranch Filing 4B," May 7, 2015 (approved by El Paso County 8/20/15).

1

Tech Contractors, "Preliminary / Final Drainage Report for Meridian Ranch Filing 4B, The Shops at Meridian Ranch Filing 1," April 2014 (approved by El Paso County 9/9/14).

Tech Contractors Engineering Group, "Drainage Conformance Letter, Building E, Lot 4, the Shops Filing 1 at Meridian Ranch," April 1, 2022 (approved by El Paso County 4/7/22).

Tech Contractors Engineering Group, "Drainage Conformance Letter, Lot 4, the Shops Filing 1 at Meridian Ranch," May 3, 2019 (approved by El Paso County 6/5/19).

II. EXISTING / PROPOSED DRAINAGE CONDITIONS

The site slopes downward to the southeast, with average grades of 1-4 percent. Soils within the proposed Convenience Store site are classified by SCS as type 19, "Columbine gravelly sandy loam" soils. These soils have high infiltration rates, rapid permeability, and low runoff potential. The soils are classified as hydrologic soils group A.

Subdivision Drainage Report

Drainage planning for this site was previously studied in several approved drainage reports for the Meridian Ranch Subdivision, the most comprehensive of which is the "Drainage Letter – Lot 3, The Shops at Meridian Ranch Filing 4B" by Olsson Associates (OA), dated May 7, 2015. As shown on the enclosed OA Drainage Plan (Appendix A), the proposed Convenience Store site lies entirely within Basin C as delineated in the previously approved drainage plans. The previously approved drainage reports for The Shops at Meridian Ranch assumed full commercial development for this basin, which is consistent with the proposed site development.

Developed drainage from this commercial site will sheet flow southeasterly to the existing storm sewer system which flows east across The Shops at Meridian Ranch commercial area, ultimately flowing to the existing downstream Bennett Regional Detention Pond. The existing detention pond was sized to account for fully developed flows from this commercial area.

The previously approved subdivision drainage planning assumed full commercial development within all of Basin C1, with runoff coefficients of $C_5 = 0.78$ and $C_{100} = 0.89$ (equivalent to impervious areas of approximately 90 percent). According to the Rational Method calculations in the original subdivision drainage report, developed peak flows from Basin C (Design Point #3) were calculated as $Q_5 = 8.2$ cfs and $Q_{100} = 15.5$ cfs.

Developed Drainage Plan

Developed drainage flows have been calculated based on the impervious areas associated with the proposed building and parking improvements. Surface drainage swales and a private storm sewer system will convey flows to the existing private storm sewer system that has been designed to convey developed flows from this site to the existing downstream Bennett Regional Detention Pond.

Site grades will slope to storm inlets and curb openings at selected locations, collecting surface drainage and conveying stormwater to the existing storm sewer system. The proposed building pad will be graded with protective slopes to provide positive drainage away from the building, and the curb, gutter, drainage swales, and private storm sewer improvements will convey developed flows to the existing storm sewer system at the southeast corner of the site.

For consistency with the previously approved subdivision drainage report, the site drainage basins have been delineated as Basins C1.1-C1.3. The proposed Convenience Store site on Lot 2 has been delineated as Basin C1.2, which drains by sheet flow and curb and gutter to the proposed Storm Inlet C1.2 (Private Type C Inlet) at the southeast corner of the property. Water quality and runoff reduction will be provided by routing the majority of developed flows from the site to the proposed landscaped Water Quality Swale C1.2 along the south edge of the property. Developed peak flows from Basin C1.2 are calculated as $Q_5 = 4.3$ cfs and $Q_{100} = 8.0$ cfs. In the event of clogging, overflows from Inlet C1.2 would sheet flow easterly into the existing 20' Type R Inlet #3.

Private Storm Sewer C1.2 (12" HDPE) will convey the flow from Inlet C1.2 into the back side of the existing private Storm Inlet #3 located at the northwest corner of Stapleton Drive and the shared private access drive along the east side of the property.

The future commercial site development lot to the west of this site has been delineated as Basin C1.1, which will drain southeasterly, contributing to DP-C1. Assuming developed runoff coefficients consistent with the previous subdivision drainage reports, developed peak flows from Basin C1.1 are calculated as $Q_5 = 3.6$ cfs and $Q_{100} = 6.6$ cfs.

Development of the proposed Lot 2 Convenience Store will include construction of the shared access drive between Lots 1 and 2, and the proposed private Storm Inlet C1.1 (10' Type R) will be installed along the east side of Basin C1.1 to accept future developed flows. Proposed Private Storm Sewer SD-C1.1 (12" RCP) will convey the flow from Inlet C1.1 into the existing Storm Manhole (MH-3), connecting to the existing 30" RCP private storm sewer flowing easterly across the site.

Depending on the future site grading scheme for Lot 1, additional private storm sewer improvements may be constructed within Basin C1.1 if necessary.

Developed flows from Basins C1.1 and C1.2 combine at Design Point #C1, with peak flows calculated as $Q_5 = 7.2$ cfs and $Q_{100} = 13.4$ cfs. Proposed Inlet C1.2 and Storm

Sewer C1.2 have been sized to accept the full developed flow from Design Point #C1 (combined Basins C1.1 and C1.2).

The existing shared private access drive along the north and east sides of the site has been delineated as Basin C1.3, which drains by curb and gutter to the existing Private Storm Inlet #3 at the northwest corner of Stapleton Drive and the shared driveway. Developed peak flows from Basin C1.3 are calculated as $Q_5 = 1.4$ cfs and $Q_{100} = 2.5$ cfs.

Developed flows from Basins C1.1-C1.3 combine at Design Point #3, with peak flows calculated as $Q_5 = 8.4$ cfs and $Q_{100} = 15.7$ cfs. The calculated flows in this report are fully consistent with the previously approved drainage report by Olsson Associates ($Q_5 = 8.2$ cfs and $Q_{100} = 15.5$ cfs at DP #3). The OA report identifies the combined flow at DP #3 being conveyed easterly through "PIPE-10" (24" RCP) and continuing downstream in the existing 24"-42" RCP storm sewer system flowing to the Bennett Regional Detention Pond.

The landscaped area along the south boundary of the site has been delineated as Basin OS-1.1, consistent with the previously approved subdivision drainage report. Basin OS-1.1 sheet flows southeasterly into the existing curb and gutter along the north side of Stapleton Drive, flowing to existing downstream storm sewer facilities. Developed peak flows from Basin OS-1.1 are calculated as $Q_5 = 0.05$ cfs and $Q_{100} = 0.3$ cfs.

Hydrologic and hydraulic calculations for the site are detailed in the appendices (Appendix B and C), and peak flows are identified on Figure D1 (Appendix D).

III. DRAINAGE PLANNING FOUR STEP PROCESS

El Paso County Drainage Criteria require drainage planning to include a Four Step Process for receiving water protection that focuses on reducing runoff volumes, treating the water quality capture volume (WQCV), stabilizing drainageways, and implementing long-term source controls.

As stated in ECM Appendix I.7., the Four Step Process is applicable to all new and redevelopment projects with construction activities that disturb 1 acre or greater or that disturb less than 1 acre but are part of a larger common plan of development. The Four Step Process has been implemented as follows in the planning of this project:

Step 1: Employ Runoff Reduction Practices

- Minimize Directly Connected Impervious Areas (MDCIA): A landscaped drainage swale has been designed along the downstream edge of the parking area, providing for disconnection of the impervious area of the south parking lot from the downstream storm sewer system (see "Sh. RR-1: Runoff Reduction Exhibit" in Appendix D).
- Landscaped Swale: A landscaped water quality swale has been designed to serve as a Receiving Pervious Areas (RPA) to mitigate impacts of the on-site impervious areas.

- Runoff Reduction Calculations: Runoff reduction has been calculated using the MHFD "UD-BMP v3.07" software package as detailed in Appendix C.
- Runoff Reduction calculations are summarized as follows:

Basin	Impervious Area (SF)	RPA Area (SF)	Volume Reduction (%)
C1.2	39,172	720	20%

• DCM Volume 2, Chapter 1, Section 4.0, specifies a minimum volume reduction of 10% for the WQCV event. As tabulated above, the proposed RPA area exceeds the specified minimum runoff reduction.

Step 2: Stabilize Drainageways

- There are no drainageways directly adjacent to this project site. The on-site private drainage improvements will convey developed flows to the existing downstream storm sewer system and regional detention basin, which has been designed to minimize downstream drainage impacts.
- Drainage basin fees were previously paid during recording of the subdivision plat, and these fees provided the applicable cost contribution towards regional drainage improvements.

Step 3: Provide Water Quality Capture Volume (WQCV)

• EDB: Developed flows from this site will be conveyed to the existing downstream Bennett Regional Detention Pond. The extended detention basin which will capture and slowly release the WQCV over an extended release period.

Step 4: Consider Need for Industrial and Commercial BMPs

- No industrial uses are proposed for this site.
- The commercial property owner will implement a Stormwater Management Plan including proper housekeeping practices and spill containment procedures.

IV. FLOODPLAIN IMPACTS

According to the FEMA floodplain map for this area, El Paso County FIRM Panel No. 08041C0551G, dated December 7, 2018, the site is located beyond the limits of any delineated 100-year floodplains.

V. STORMWATER DETENTION AND WATER QUALITY

Stormwater detention for this site is provided in the existing Bennett Ranch Regional Detention Pond.

According to the previously approved OA drainage report, the "Bennett Regional Pond has been adequately sized such that 100 YR developed flows will be detained and released at (or below) the pre-developed flow rate."

As detailed in Appendix B, the calculated runoff coefficients for this site ($C_{100} = 0.89$ at DP3) are fully consistent with the impervious area assumptions in the previously approved subdivision drainage reports.

An on-site Water Quality Swale will be constructed to meet stormwater quality improvements in accordance with current El Paso County drainage criteria. As stated in previously approved drainage letter reports for this subdivision, water quality is provided by applying the "20%/10% Rule" described in Section I.7.1.C.5. of the El Paso County Engineering Criteria Manual for "Applicable Development Site Draining to a Regional WQCV Facility." This rule specifies that "at least 20 percent of the applicable development site must be disconnected from the storm drainage system and drain through a receiving pervious area control measure comprising a footprint of at least 10 percent of the upstream disconnected impervious area."

The drainage design for Basin C1.2 meets or exceeds the requirements listed above by routing the south and west parking areas through the landscaped drainage swale along the south edge of the site. The "Unconnected Impervious Area" (UIA) of the parking areas is 25,847 square feet, which is 66.0 percent of the total basin impervious area. The total landscaped swale area along the south edge of the site is 4,375 square feet, which is 16.9 percent of the disconnected impervious area of the project site.

As detailed in the Runoff Reduction calculations in Appendix C, the proposed landscaped swale provides adequate runoff reduction to mitigate the water quality impacts of the proposed convenience store development.

In addition to the on-site water quality swale, previously approved drainage reports identify the existing downstream "SNOUT" stormwater quality facility as being sufficient to meet stormwater quality requirements for Meridian Ranch Filing 4B, including this commercial area.

VI. PUBLIC IMPROVEMENTS / DRAINAGE BASIN FEES

No public drainage improvements are required or proposed for this project.

The site lies completely within the Bennett Ranch Drainage Basin. Applicable drainage basin fees were paid at the time of original platting, so no drainage basin fees or bridge fees are applicable at this time.

VII. SUMMARY

The developed drainage patterns for the proposed Convenience Store site development on Lot 2, The Shops Filing No. 1 at Meridian Ranch will remain consistent with the established drainage plan for this subdivision. The grading and drainage plan for the proposed convenience store development fully conforms to the approved drainage plan for this subdivision.

Developed flows from the site will drain through a private storm sewer system at the southeast corner of the property, connecting to the existing downstream public drainage system. Stormwater detention is provided by the existing Bennett Regional Detention Pond, which was designed to accept fully developed flows from the commercial area encompassing this site (including all of The Shops Filing No. 1 at Meridian Ranch Subdivision). Stormwater quality is provided in the proposed landscaped swale along the south edge of the property.

Construction and proper maintenance of the on-site drainage facilities, in conjunction with proper erosion control practices, will ensure that this developed site has no significant adverse drainage impact on downstream or surrounding areas.

APPENDIX A EXCERPTS FROM SUBDIVISION DRAINAGE REPORT



NEW DOC

May 7, 2015

Brandy Williams El Paso County 2880 International Circle Colorado Springs, CO 80910

RE: Drainage Letter – Lot 3, The Shops at Meridian Ranch Filing 4B

Ms. Williams:

This letter is to serve as a statement of compliance with the *Preliminary/Final Drainage Report for Meridian Ranch Filing 4B, The Shops at Meridian Ranch* (the REPORT) prepared by Tech Contractors, dated April 2014, and approved on September 9, 2014. The REPORT provides hydrologic and hydraulic analysis for the development located at the northeast corner of Meridian Road and Stapleton Drive in El Paso County, Colorado.

The first phase of commercial construction within Filing 4B will occur within Lot 3, which will include construction of the main roadway through the commercial portion of Filing 4B. While this letter proposes to demonstrate Lot 3's compliance with the REPORT, we are also including conceptual layout/development of Lots 1, 2 & 4 Filing 4B in this analysis for posterity. Development of Lots 1, 2 or 4 Filing 4B must be preceded by a separate drainage letter demonstrating compliance with the REPORT.

The REPORT anticipated runoff from the commercial areas, collectively referred to as The Shops (Lots 1-4, Filing 4B), to be discharged to the previously-constructed storm sewer system within Tract F, Filing 4. Said storm sewer system will ultimately discharge developed flows from Filing 4B, including The Shops, to the Bennett Regional Pond. The Bennett Regional Pond has been adequately sized such that 100 YR developed flows from Filing 4B will be detained and released at (or below) the predeveloped flow rate for the same event.

Anticipated developed flows from The Shops were accounted for in two basins within the REPORT; basin 4 and basin 9. The flows from basin 4 were expected to discharge directly into the previously-constructed Filing 4 storm sewer system via pipe (Design Point X01). The flows from basin 9 were expected to be discharged into the Filing 4 storm sewer system via a 15' Type R inlet located near the intersection of Meridian Ranch Boulevard & Stapleton Drive (Inlet El03). Anticipated developed flows from the REPORT are summarized in Table 1. Drainage basin maps from the REPORT have also been included with this letter for reference.

Table 1: Anticipated Developed Flows from the REPORT

Basin Description	5 YR Flow (cfs)	100 YR Flow (cfs)
Basin 4 (X01)	38.4	71.0
Basin 9 (El03)	11.9	25.4

Based upon a detailed analysis of The Shops along with portions of the adjacent roadways, we have determined that 34.7 cfs during the 5 YR event and 68.1 cfs during the 100 YR event will be discharged to the pipe connection at design point X01, while 11.4 cfs during the 5 YR event and 25.4 cfs during the 100 YR event will be conveyed to the inlet at design point El03. The flows to be collected at design point El03 are comprised of the direct runoff from Basin OS-1 as well as flows bypassing inlets in the proposed commercial subdivision. The calculated developed flows are summarized in Table 2.

Table 2: Calculated Developed Flows

DP Description	5 YR Flow (cfs)	100 YR Flow (cfs)
Storm Sewer (X01)	34.7	68.1
Inlet (El03)	11.4	25.4

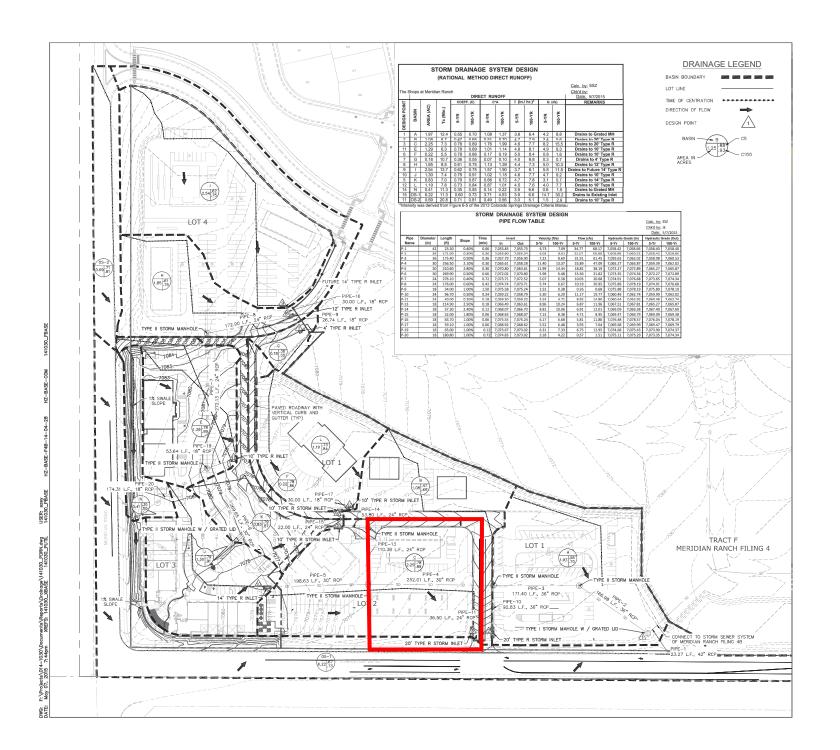
The Shops proposes inlets whose bypass flows will result in additional flow to Stapleton Drive. The routed flows from this bypass are 0.00 cfs during the minor event and 3.76 cfs during the major event. This results in a cumulative expected street flow of approximately 7.2 cfs during the minor event and 18.5 cfs during the major event on Stapleton Drive. Based upon Figure 7-3 of the 2013 Colorado Springs Drainage Criteria Manual the minor storm street capacity for an arterial road is 16 cfs during the minor event and 36 cfs during major event. In both the minor and major event the expected flows are less than the road capacity.

Development of Lot 3 will not adversely impact downstream facilities, as those facilities were designed to convey developed flows from all areas within The Shops. Upon full build-out of The Shops (according to the planned layout of Lot 3 & the conceptual layout of Lots 1, 2 & 4 as presented in the attached Developed Drainage Basin map), the resulting developed flows will be less than the REPORT's expected flows at Design Point X01 and inlet El03.

Drainage and Bridge Fees:

The 4.11± acre site is the Bennett Drainage Basin. Drainage & Bridge Fees for this basin will be paid to the County at the time of platting. Based on the County's drainage basin maps, the 2015 Drainage & Bridge fees are as follows:

Bennett Drainage Basin Drainage Fee: 4.11 ac*\$9,447/Ac* .867 Imp Area = \$33,663.16 Bennett Drainage Basin Bridge Fee: 4.11 ac*\$3,624/Ac* 0.867 Imp Area = \$12,913.65



Tech Contractors ENGINEERING GROUP

April 1, 2022

Ed Schoenheit El Paso County Planning and Community Development 2880 International Cir Colorado Springs, CO 80910

RE:

Drainage Conformance Letter
Building E, Lot 4, the Shops Filing 1 at Meridian Ranch
PCD File No. PPR-223

Dear Mr. Schoenheit

The attached short form drainage report is to serve as a statement of compliance for the development of Building E, Lot 4 of the Shops Filing 1 at Meridian Ranch commercial property with the *Drainage Conformance Letter for Lot 4*, the Shops Filing 1 at Meridian Ranch (the LETTER) prepared by Tech Contractors, dated May 3, 2019, and approved on June 5, 2019, and the *Preliminary/Final Drainage Report for Meridian Ranch Filing 4B, The Shops at Meridian Ranch* (the REPORT) prepared by Tech Contractors, dated April 2014, and approved on September 9, 2014. The REPORT provides hydrologic and hydraulic analysis for the commercial development located at the northeast corner of Meridian Road and Stapleton Drive in El Paso County, Colorado.

Sincerely

Thomas A. Kerby, PE

Tech Contractors

Telephone No.: 719.495.7444

11910 Tourmaline Drive, Suite 130

Falcon, CO 80831

719.495.7444

PCD File No. PPR-223

CERTIFICATIONS

Design Engineer's Statement:

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the County for drainage reports and said report is in conformity with the applicable master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.

Thomas A. Kerby, P.E. #31429

Owner/Developer's Statement:

I, the owner/developer have read and will comply with all of the requirements specified in this drainage report and plan.

Raul Guzinan, Vice President

The Shops at Meridian Ranch LLC

P.O. Box 80036 San Diego, CA 92138 April 1, 2022

Date

El Paso County:

Filed in accordance with the requirements of the Drainage Criteria Manual, Volumes 1 & 2, El Paso County Engineering Criteria Manual and Land Development Code as amended.

Jennifer Irvine, P.E.
County Engineer / ECM Administrator

APPROVED Engineering Department

04/07/2022 2:02:38 PM dsdnijkamp

EPC Planning & Community Development Department

Introduction

This short report was prepared for the Commercial Building E of Lot 4 of the Shops Filing 1 at Meridian Ranch. The report shows the storm drainage associated with the construction of Building E is in substantial conformance with the updated calculations of the *Drainage Comformance Letter for Lot 4, the Shops Filing 1 at Meridian Ranch* (the LETTER) prepared by Tech Contractors, dated May 3, 2019, and approved on June 5, 2019, and original calculations established with the *Preliminary/Final Drainage Report for Meridian Ranch Filing 4B, The Shops at Meridian Ranch* (the REPORT) prepared by Tech Contractors, dated April 2014, and approved on September 9, 2014. The LETTER and REPORT provides hydrologic and hydraulic analysis for the development located at the northeast corner of Meridian Road and Stapleton Drive in El Paso County, Colorado.

Background

Building E is proposed to be built on Lot 4 and is located near the southeast corner of Tourmaline Dr. and Meridian Rd. The pad site for Building E was graded with Development Plan associated with Lot 4 of the Shops Filing 1 at Meridian Ranch approved on June 6 2019. At that time Building D and the parking lot for the entire Lot 4 development was completed. The building pad for Building E generally slopes in a southerly direction toward Fleece Flower Way and the main roadway for the Shops development. A drainage letter (LETTER) showing Lot 4's compliance with the REPORT was approved by the County on June 5 2019.

The initial phase of commercial construction included the utility and private storm drain system and the construction of the main roadway through the commercial center and the development of Lot 3 of The Shops Filing 1 at Meridian Ranch. A drainage letter showing Lot 3's compliance with the REPORT was approved by the County on August 20, 2015.

The REPORT anticipated runoff from the commercial areas, collectively referred to as The Shops (Lots 1-4, The Shops Filing 1 at Meridian Ranch), to be discharged to the storm drain system constructed as a part of Meridian Ranch Filing 4B. Said storm sewer system will ultimately discharge developed flows from Filing 4B, including The Shops, to the main stem of the Bennett Ranch Channel then convey the flow downstream to the Bennett Regional Detention Pond. The Bennett Regional Detention Pond was designed and constructed as a regional facility providing detention and water quality for all areas within the Bennett Ranch Drainage Basin within the Woodmen Hills Filings 10 & 11 and Meridian Ranch including the flows from The Shops Filing 1 at Meridian Ranch. The Bennett Pond has been adequately sized such that 100 YR developed will be detained and released at (or below) the predeveloped flow rate for the same event.

Water Quality

When regional water quality capture volume facilities are present, BMPs are still required onsite to address water quality and channel stability for the reach of the drainageway upstream of the regional facility. In accordance with MS4 permits and regulations, BMPs must be implemented prior to discharges to a State Water from areas of "New Development and Significant Redevelopment." Therefore, if a regional BMP is utilized downstream of a discharge from a development into a State Water, additional BMPs are required to protect the State Water between the development site and the regional facility. However, these BMPs may not have to be as extensive as would normally be required, as long as they are adequate to protect the State Water upstream of the regional BMP.

Additional water quality for the entirety of Lot 4 was approved by the LETTER by applying the 'Applicable Development Site Draining to a Regional WQCV Facility' rule (20%/10% Rule) found in Part I.E.4.a.iv.E, Control Measure Requirements of the El Paso County MS4 Program. The regional WQCV facility is designed to accept drainage from the applicable development site. Stormwater from the site may discharge to a water of the state before being discharged to the regional WQCV facility. Before discharging to a water of the state, 20 percent of the total impervious surface of the applicable development site must first drain to a control measure covering an area equal to 10 percent of the total impervious surface of the applicable development site. The control measure must be designed in accordance with a design manual identified by the permittee. In addition, the stream channel between the discharge point of the applicable development site and the regional WQCV facility must be stabilized.

The project site meets or exceeds the requirements listed above in that the roof top areas (including Building E) discharge to grass lined swales prior to entering into the storm drain system. The storm drainage system is then routed through Meridian Ranch Filing 4b and is discharged into a stabilized stream channel prior to entering the downstream WQCV facility located within the Bennett Ranch Regional Detention Pond.

The total roof top area of the two buildings is 28,820 SQ. FT or 22.2% of the total impervious surface area of the project site. The two buildings discharge the storm runoff to grass lined swales via the roof drains. The total grass lined swale area is 16,735 SQ. FT. or 12.9% of the total impervious surface area of the project site. Please see the Water Quality Exhibit A of the LETTER for a graphic representation of the site.

By applying the 20%/10% Rule for regional WQCV facilities, this project meets or exceeds the requirements for water quality.

Drainage Analysis

The anticipated developed flows from The Shops remain unchanged from the LETTER and the REPORT, therefore the drainage patterns and flow values are in substantial conformance with the previously approved documents and will not adversely impact downstream facilities.

The analysis completed for the initial phase of the Shops, Lot 3 found in the REPORT along with portions of the adjacent roadways, showed 35 cfs during the 5 YR event and 68 cfs for the 100 YR event for the on-site flows discharged to the pipe connection at design point X01.

The storm drainage analysis for this phase of the Shops Filing 1 at Meridian Ranch found in the LETTER yields a 5 YR event flow of 29 cfs and 58 cfs for the 100 YR at the pipe connection at design point X01 entering Meridian Ranch Filing 4B. A comparison of the different flow rates from the various drainage studies can be found in the table below.

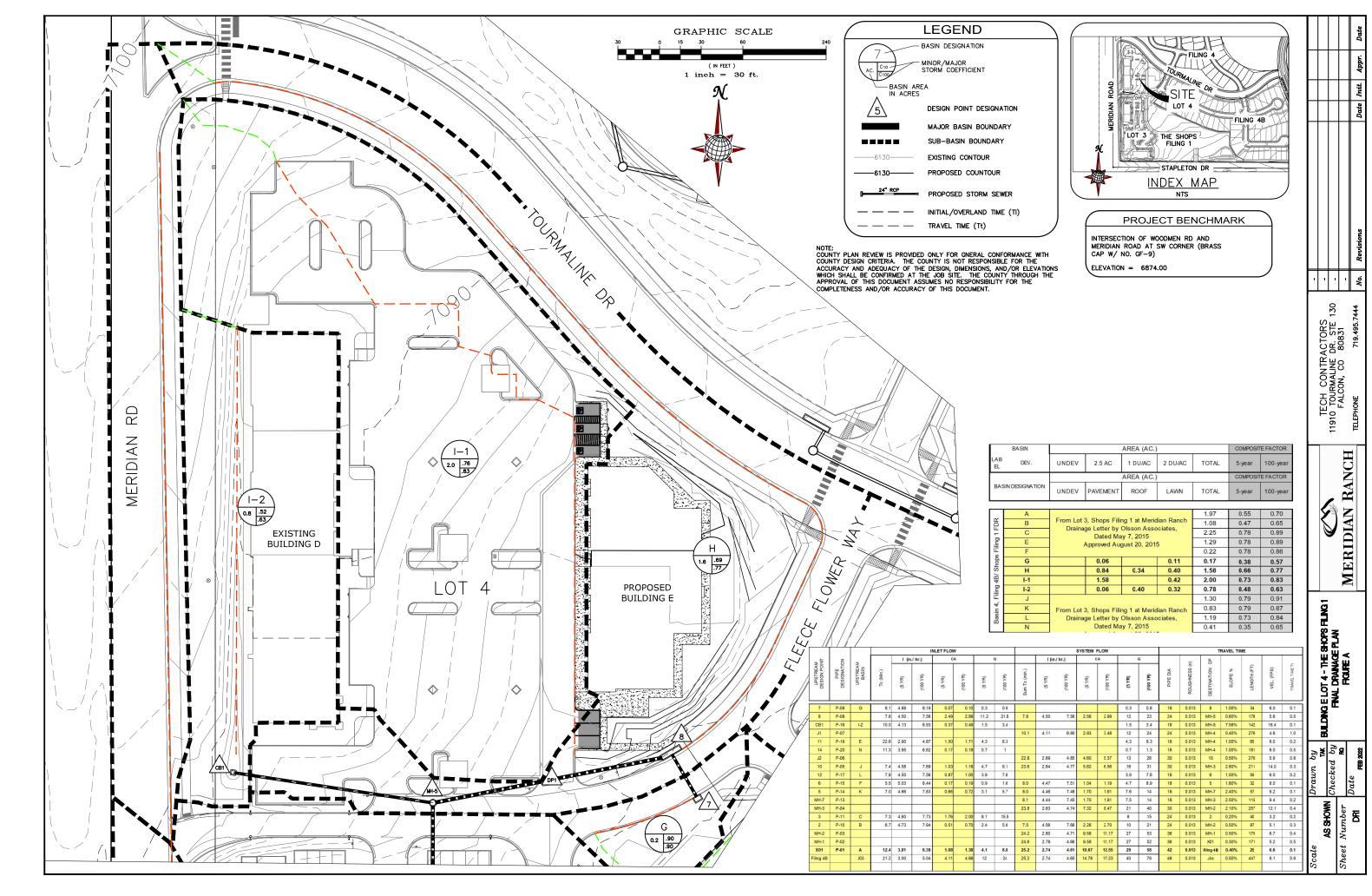
Table 1 Design Flow Rates for Design Point X01

	Minor Storm (5-yr/10-yr)	Major Storm (100-yr)
Filing 4B/The Shops - FDR, 2014	38	70
The Shops, Lot 3 - Drainage Letter, 2015	35	68
The Shops, Lot 4 - Drainage Letter, 2018	29	58

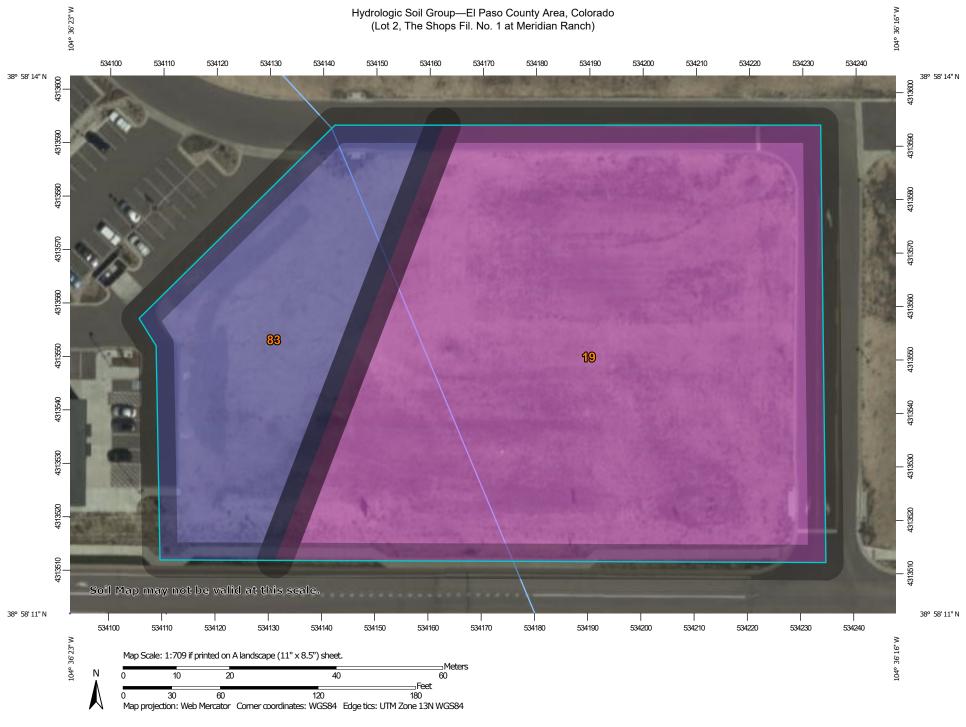
Drainage and Bridge Fees

There are no Drainage and Bridge Fees with this project as the fees were paid at the time of the recordation of the Shops Filing 1 at Meridian Ranch on August 12, 2015.

Dra	Drainage Calculations from the LETTER												
			COM	POSITE	'C' FAC	TORS							
	PROJECT:	Lot 4, S	hops Fi	ling 1				1/2/2019					
	BASIN			AREA (AC.))		COMPOSI	Percent					
LAB EL	DEV.	UNDEV	2.5 AC	1 DU/AC	2 DU/AC	TOTAL	5-year	100-year	Impervious				
				COMPOSI	TE FACTOR	Doroont							
BAS	SIN DESIGNATION	UNDEV	PAVEMENT	ROOF	LAWN	TOTAL	5-year	100-year	Percent Impervious				
						-							
l ~	A	From Lot	3, Shops Filir	ng 1 at Meric	lian Ranch	1.97	0.55	0.70					
FDR	В		ge Letter by	0	1.08	0.47	0.65						
_	С			y 7, 2015	2.25	0.78	0.89						
Filing	E		Approved Aug	gust 20, 201	1.29	0.78	0.89						
S F	F					0.22	0.78	0.86					
Shops	G		0.06		0.11	0.17	0.38	0.57					
S/	Н		0.84	0.34	0.40	1.58	0.66	0.77					
4B	I-1		1.58		0.42	2.00	0.73	0.83					
Filing 4B/	I-2		0.06	0.40	0.32	0.78	0.48	0.63					
	J					1.30	0.79	0.91					
asin 4,	K	From Lot	3, Shops Filir	ng 1 at Merio	lian Ranch	0.83	0.79	0.87					
Bas	L	Draina	ge Letter by	Olsson Asso	ociates,	1.19	0.73	0.84					
	N			y 7, 2015		0.41	0.35	0.65					
	OS-1	,	Approved Aug	gust 20, 201	5	6.22	0.60	0.73					
	OS-2					0.69	0.71	0.81					
	TOTAL		2.54	0.74	1.25	15.8	0.67	0.80	90.0%				



APPENDIX B HYDROLOGIC CALCULATIONS



MAP LEGEND MAP INFORMATION The soil surveys that comprise your AOI were mapped at Area of Interest (AOI) С 1:24.000. Area of Interest (AOI) C/D Soils Warning: Soil Map may not be valid at this scale. D Soil Rating Polygons Enlargement of maps beyond the scale of mapping can cause Not rated or not available Α misunderstanding of the detail of mapping and accuracy of soil **Water Features** line placement. The maps do not show the small areas of A/D Streams and Canals contrasting soils that could have been shown at a more detailed В Transportation B/D Rails ---Please rely on the bar scale on each map sheet for map measurements. Interstate Highways C/D Source of Map: Natural Resources Conservation Service **US Routes** Web Soil Survey URL: D Major Roads Coordinate System: Web Mercator (EPSG:3857) Not rated or not available -Local Roads Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts Soil Rating Lines Background distance and area. A projection that preserves area, such as the Aerial Photography Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required. This product is generated from the USDA-NRCS certified data as of the version date(s) listed below. B/D Soil Survey Area: El Paso County Area, Colorado Survey Area Data: Version 20, Sep 2, 2022 Soil map units are labeled (as space allows) for map scales 1:50.000 or larger. Not rated or not available Date(s) aerial images were photographed: Sep 11, 2018—Oct 20. 2018 **Soil Rating Points** The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background A/D imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident. B/D

Hydrologic Soil Group

	,			
Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
19	Columbine gravelly sandy loam, 0 to 3 percent slopes	A	1.8	73.7%
83	Stapleton sandy loam, 3 to 8 percent slopes	В	0.6	26.3%
Totals for Area of Intere	est		2.4	100.0%

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

Rating Options

Aggregation Method: Dominant Condition
Component Percent Cutoff: None Specified

Tie-break Rule: Higher

Chapter 6 Hydrology

Table 6-6. Runoff Coefficients for Rational Method

(Source: UDFCD 2001)

Land Harris Confess	B	Runoff Coefficients											
Land Use or Surface Characteristics	Percent Impervious	2-у	ear	5-у	ear	10-1	year	25-	/ear	50-1	year	100-	year
		HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D
Business													
Commercial Areas	95	0.79	0.80	0.81	0.82	0.83	0.84	0.85	0.87	0.87	0.88	0.88	0.89
Neighborhood Areas	70	0.45	0.49	0.49	0.53	0.53	0.57	0.58	0.62	0.60	0.65	0.62	0.68
Residential													
1/8 Acre or less	65	0.41	0.45	0.45	0.49	0.49	0.54	0.54	0.59	0.57	0.62	0.59	0.65
1/4 Acre	40	0.23	0.28	0.30	0.35	0.36	0.42	0.42	0.50	0.46	0.54	0.50	0.58
1/3 Acre	30	0.18	0.22	0.25	0.30	0.32	0.38	0.39	0.47	0.43	0.52	0.47	0.57
1/2 Acre	25	0.15	0.20	0.22	0.28	0.30	0.36	0.37	0.46	0.41	0.51	0.46	0.56
1 Acre	20	0.12	0.17	0.20	0.26	0.27	0.34	0.35	0.44	0.40	0.50	0.44	0.55
Industrial													
Light Areas	80	0.57	0.60	0.59	0.63	0.63	0.66	0.66	0.70	0.68	0.72	0.70	0.74
Heavy Areas	90	0.71	0.73	0.73	0.75	0.75	0.77	0.78	0.80	0.80	0.82	0.81	0.83
Parks and Cemeteries	7	0.05	0.09	0.12	0.19	0.20	0.29	0.30	0.40	0.34	0.46	0.39	0.52
Playgrounds	13	0.07	0.13	0.16	0.23	0.24	0.31	0.32	0.42	0.37	0.48	0.41	0.54
Railroad Yard Areas	40	0.23	0.28	0.30	0.35	0.36	0.42	0.42	0.50	0.46	0.54	0.50	0.58
Undeveloped Areas													
Historic Flow Analysis Greenbelts, Agriculture	2	0.03	0.05	0.09	0.16	0.17	0.26	0.26	0.38	0.31	0.45	0.36	0.51
Pasture/Meadow	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50
Forest	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50
Exposed Rock	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Offsite Flow Analysis (when landuse is undefined)	45	0.26	0.31	0.32	0.37	0.38	0.44	0.44	0.51	0.48	0.55	0.51	0.59
Streets													
Paved	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Gravel	80	0.57	0.60	0.59	0.63	0.63	0.66	0.66	0.70	0.68	0.72	0.70	0.74
Drive and Walks	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Roofs	90	0.71	0.73	0.73	0.75	0.75	0.77	0.78	0.80	0.80	0.82	0.81	0.83
Lawns	0	0.71	0.73	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.82	0.35	0.50

3.2 Time of Concentration

One of the basic assumptions underlying the Rational Method is that runoff is a function of the average rainfall rate during the time required for water to flow from the hydraulically most remote part of the drainage area under consideration to the design point. However, in practice, the time of concentration can be an empirical value that results in reasonable and acceptable peak flow calculations.

For urban areas, the time of concentration (t_c) consists of an initial time or overland flow time (t_i) plus the travel time (t_t) in the storm sewer, paved gutter, roadside drainage ditch, or drainage channel. For non-urban areas, the time of concentration consists of an overland flow time (t_i) plus the time of travel in a concentrated form, such as a swale or drainageway. The travel portion (t_i) of the time of concentration can be estimated from the hydraulic properties of the storm sewer, gutter, swale, ditch, or drainageway. Initial time, on the other hand, will vary with surface slope, depression storage, surface cover, antecedent rainfall, and infiltration capacity of the soil, as well as distance of surface flow. The time of concentration is represented by Equation 6-7 for both urban and non-urban areas.

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$$t_c = t_i + t_t \tag{Eq. 6-7}$$

Where:

 t_c = time of concentration (min)

 t_i = overland (initial) flow time (min)

 t_t = travel time in the ditch, channel, gutter, storm sewer, etc. (min)

3.2.1 Overland (Initial) Flow Time

The overland flow time, t_i , may be calculated using Equation 6-8.

$$t_i = \frac{0.395(1.1 - C_5)\sqrt{L}}{S^{0.33}}$$
 (Eq. 6-8)

Where:

 t_i = overland (initial) flow time (min)

 C_5 = runoff coefficient for 5-year frequency (see Table 6-6)

L = length of overland flow (300 ft <u>maximum</u> for non-urban land uses, 100 ft <u>maximum</u> for urban land uses)

S = average basin slope (ft/ft)

Note that in some urban watersheds, the overland flow time may be very small because flows quickly concentrate and channelize.

3.2.2 Travel Time

For catchments with overland and channelized flow, the time of concentration needs to be considered in combination with the travel time, t_t , which is calculated using the hydraulic properties of the swale, ditch, or channel. For preliminary work, the overland travel time, t_t , can be estimated with the help of Figure 6-25 or Equation 6-9 (Guo 1999).

$$V = C_v S_w^{-0.5}$$
 (Eq. 6-9)

Where:

V = velocity (ft/s)

 C_v = conveyance coefficient (from Table 6-7)

 S_w = watercourse slope (ft/ft)

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Type of Land Surface	C_{v}
Heavy meadow	2.5
Tillage/field	5
Riprap (not buried)*	6.5
Short pasture and lawns	7
Nearly bare ground	10
Grassed waterway	15
Paved areas and shallow paved swales	20

Table 6-7. Conveyance Coefficient, C_{ν}

The travel time is calculated by dividing the flow distance (in feet) by the velocity calculated using Equation 6-9 and converting units to minutes.

The time of concentration (t_c) is then the sum of the overland flow time (t_i) and the travel time (t_t) per Equation 6-7.

3.2.3 First Design Point Time of Concentration in Urban Catchments

Using this procedure, the time of concentration at the first design point (typically the first inlet in the system) in an urbanized catchment should not exceed the time of concentration calculated using Equation 6-10. The first design point is defined as the point where runoff first enters the storm sewer system.

$$t_c = \frac{L}{180} + 10 \tag{Eq. 6-10}$$

Where:

 t_c = maximum time of concentration at the first design point in an urban watershed (min)

L = waterway length (ft)

Equation 6-10 was developed using the rainfall-runoff data collected in the Denver region and, in essence, represents regional "calibration" of the Rational Method. Normally, Equation 6-10 will result in a lesser time of concentration at the first design point and will govern in an urbanized watershed. For subsequent design points, the time of concentration is calculated by accumulating the travel times in downstream drainageway reaches.

3.2.4 Minimum Time of Concentration

If the calculations result in a t_c of less than 10 minutes for undeveloped conditions, it is recommended that a minimum value of 10 minutes be used. The minimum t_c for urbanized areas is 5 minutes.

3.2.5 Post-Development Time of Concentration

As Equation 6-8 indicates, the time of concentration is a function of the 5-year runoff coefficient for a drainage basin. Typically, higher levels of imperviousness (higher 5-year runoff coefficients) correspond to shorter times of concentration, and lower levels of imperviousness correspond to longer times of

^{*}For buried riprap, select C_v value based on type of vegetative cover.

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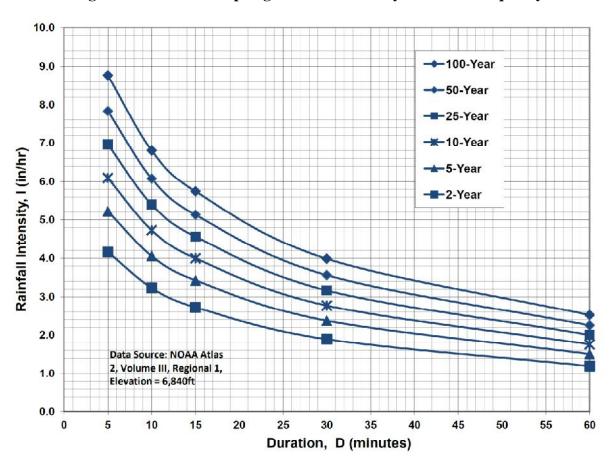


Figure 6-5. Colorado Springs Rainfall Intensity Duration Frequency

IDF Equations

$$I_{100} = -2.52 \ln(D) + 12.735$$

$$I_{50} = -2.25 \ln(D) + 11.375$$

$$I_{25} = -2.00 \ln(D) + 10.111$$

$$I_{10} = -1.75 \ln(D) + 8.847$$

$$I_5 = -1.50 \ln(D) + 7.583$$

$$I_2 = -1.19 \ln(D) + 6.035$$

Note: Values calculated by equations may not precisely duplicate values read from figure.

SHOPS AT MERIDIAN RANCH CONVENIENCE STORE COMPOSITE RUNOFF COEFFICIENTS

	ES										
	TOTAL		SUB-AREA 1			SUB-AREA 2			SUB-AREA 3		
	AREA		DEVELOPMENT/		AREA	DEVELOPMENT/			DEVELOPMENT/		WEIGHTED
BASIN	(AC)	(AC)	COVER	С	(AC)	COVER	С	(AC)	COVER	С	C VALUE
C1.1	0.9	0.80	PAVED/IMPERVIOUS	0.9	0.10	LANDSCAPED	0.08				0.809
1.2	1.08	0.90	PAVED/IMPERVIOUS	0.9	0.18	LANDSCAPED	0.08				0.763
C1.1,C1.2	1.98										0.784
1.3	0.3	0.30	PAVED/IMPERVIOUS	0.9							0.900
C1.1-C1.3	2.28										0.799
100-YEAR C VAL	.UES		I								
	TOTAL		SUB-AREA 1			SUB-AREA 2			SUB-AREA 3		
	AREA		DEVELOPMENT/		AREA	DEVELOPMENT/			DEVELOPMENT/	1	WEIGHTED
BASIN	(AC)	(AC)	COVER	С	(AC)	COVER	С	(AC)	COVER	С	C VALUE
C1.1	0.9	0.80	PAVED/IMPERVIOUS	0.96	0.10	LANDSCAPED	0.35				0.892
C1.2	1.08	0.90	PAVED/IMPERVIOUS	0.96	0.18	LANDSCAPED	0.35				0.858
C1.1,C1.2	1.98										0.874
C1.3	0.3	0.30	PAVED/IMPERVIOUS	0.96							0.960
	0.00										0.885
C1.1-C1.3	2.28										
SHOPS AT MERI COMPOSITE IMP	DIAN RANCH PERVIOUS AR		CE STORE								
SHOPS AT MERI	DIAN RANCH PERVIOUS AR					SUB-AREA 2			SUB-ARFA 3		
SHOPS AT MERI COMPOSITE IMP	DIAN RANCH PERVIOUS AR REAS		SUB-AREA 1	PERCENT	ARFA	SUB-AREA 2	PERCENT		SUB-AREA 3	PERCENT	WEIGHTED
SHOPS AT MERI COMPOSITE IMP	DIAN RANCH PERVIOUS AR			PERCENT IMPERVIOUS	AREA (AC)	SUB-AREA 2 DEVELOPMENT/ COVER	PERCENT IMPERVIOUS	(AC)	SUB-AREA 3 DEVELOPMENT/ COVER	PERCENT IMPERVIOUS	WEIGHTED % IMP
SHOPS AT MERICOMPOSITE IMP MPERVIOUS AR BASIN	REAS TOTAL AREA (AC) 0.9	(AC)	SUB-AREA 1 DEVELOPMENT/ COVER PAVED/IMPERVIOUS			DEVELOPMENT/ COVER LANDSCAPED		(AC)	DEVELOPMENT/		
SHOPS AT MERICOMPOSITE IMP MPERVIOUS AR BASIN C1.1 C1.2	DIAN RANCH PERVIOUS AR REAS TOTAL AREA (AC) 0.9 1.08	(AC)	SUB-AREA 1 DEVELOPMENT/ COVER	IMPERVIOUS	(AC)	DEVELOPMENT/ COVER	IMPERVIOUS	(AC)	DEVELOPMENT/		% IMP 88.889 83.333
SHOPS AT MERICOMPOSITE IMP MPERVIOUS AR BASIN C1.1 C1.2	REAS TOTAL AREA (AC) 0.9	(AC)	SUB-AREA 1 DEVELOPMENT/ COVER PAVED/IMPERVIOUS	IMPERVIOUS 100	(AC)	DEVELOPMENT/ COVER LANDSCAPED	IMPERVIOUS 0	(AC)	DEVELOPMENT/		% IMP 88.889
SHOPS AT MERI COMPOSITE IMP MPERVIOUS AR BASIN	DIAN RANCH PERVIOUS AR REAS TOTAL AREA (AC) 0.9 1.08	(AC)	SUB-AREA 1 DEVELOPMENT/ COVER PAVED/IMPERVIOUS	IMPERVIOUS 100	(AC)	DEVELOPMENT/ COVER LANDSCAPED	IMPERVIOUS 0	(AC)	DEVELOPMENT/		% IMP 88.889 83.333

RATL.SHOPS-0323

SHOPS AT MERIDIAN RANCH CONVENIENCE STORE RATIONAL METHOD

DEVELOPED CONDITIONS

					0	verland Flo	w		Cha	annel flow			1					
			(С			CHANNEL CONVEYANCE			SCS (2)		TOTAL TOTAL		INTENSITY (5)		PEAK FLOW		
BASIN	DESIGN POINT	AREA (AC)	5-YEAR	100-YEAR	LENGTH (FT)	SLOPE (FT/FT)	Tco ⁽¹⁾ (MIN)	LENGTH (FT)	COEFFICIENT C	SLOPE (FT/FT)	VELOCITY (FT/S)	Tt ⁽³⁾ (MIN)	Tc ⁽⁴⁾ (MIN)	Tc ⁽⁴⁾ (MIN)	5-YR (IN/HR)	100-YR (IN/HR)	Q5 ⁽⁶⁾ (CFS)	Q100 ⁽⁶⁾ (CFS)
C1.1	C1.1	0.90	0.809	0.892	100	0.020	4.2	275	20	0.018	2.68	1.7	5.9	5.9	4.91	8.25	3.58	6.62
C1.2	C1.2	1.08	0.763	0.858	70	0.036	3.4	285	20	0.030	3.46	1.4	4.7	5.0	5.17	8.68	4.26	8.04
Tt C1.1-C1.2								260	20	0.029	3.41	1.3						
C1.1,C1.2	C1	1.98	0.784	0.874									7.2	7.2	4.62	7.76	7.17	13.42
C1.3	C1.3	0.30	0.900	0.960	45	0.020	1.9	415	20	0.019	2.76	2.5	4.5	5.0	5.17	8.68	1.40	2.50
C1.1-C1.3	3	2.28	0.799	0.885									7.2	7.2	4.62	7.76	8.42	15.65
OS-1.1	OS-1.1	0.12	0.080	0.350	40	0.160	4.7	350	20	0.02	2.83	2.1	6.8	6.8	4.72	7.92	0.05	0.33

- 1) OVERLAND FLOW Tco = (0.395*(1.1-RUNOFF COEFFICIENT)*(OVERLAND FLOW LENGTH^(0.5)/(SLOPE^(0.333))
- 2) SCS VELOCITY = C * ((SLOPE(FT/FT)^0.5)
 - C = 2.5 FOR HEAVY MEADOW
 - C = 5 FOR TILLAGE/FIELD
 - C = 7 FOR SHORT PASTURE AND LAWNS
 - C = 10 FOR NEARLY BARE GROUND
 - C = 15 FOR GRASSED WATERWAY
 - C = 20 FOR PAVED AREAS AND SHALLOW PAVED SWALES
- 3) MANNING'S CHANNEL TRAVEL TIME = L/V (WHEN CHANNEL VELOCITY IS KNOWN)
- 4) Tc = Tco + Tt
- *** IF TOTAL TIME OF CONCENTRATION IS LESS THAN 5 MINUTES, THEN 5 MINUTES IS USED
- 5) INTENSITY BASED ON I-D-F EQUATIONS IN CITY OF COLORADO SPRINGS DRAINAGE CRITERIA MANUAL
 - $I_5 = -1.5 * In(Tc) + 7.583$
 - $I_{100} = -2.52 * In(Tc) + 12.735$
- 6) Q = CiA

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APPENDIX C HYDRAULIC CALCULATIONS

			Desig	gn Procedu	re Form: I	Runoff Red	luction					
UD-BMP (Version 3.07, March 2018)										Sheet 1 of 1		
Designer:	JPS											
Company:	JPS									=		
Date:	April 1, 2023									_		
Project:	Shops at Meridian Ranch Convenience Store									_		
Location:	ocation: Basin C1.2 (Lot 2)											
SITE INFORMATION (User Input in Blue Cells)												
	WQCV F	VQCV Rainfall Depth 0.60 inches										
Depth of Average Runoff Producing Storm, d ₆ = 0.43 inches (for Watersheds Outside of the Denver Region, Figure 3-1 in USDCM Vol. 3)												
Area Type	UIA:RPA	DCIA	SPA									
Area ID	C1.2a	C1.2b	C1.2c									
Downstream Design Point ID	C1.2	C1.2	C1.2									1
Downstream BMP Type	EDB	EDB	EDB									
DCIA (ft²)		13,325										
UIA (ft²)	25,847		-									
RPA (ft²)	720											
SPA (ft²)			7,153									
HSG A (%)	100%		100%									
HSG B (%)	0%		0%									
HSG C/D (%)	0%		0%									<u> </u>
Average Slope of RPA (ft/ft) UIA:RPA Interface Width (ft)	0.020 4.00											+
OIA.N A Interlace Width (it)	4.00								l		l .	
CALCULATED RUNOFF	RESULTS											
Area ID	C1.2a	C1.2b	C1.2c									
UIA:RPA Area (ft²)	26,567											
L / W Ratio	16.00											
UIA / Area	0.9729		0.00									
Runoff (in) Runoff (ft ³)	0.34 754	0.50 555	0.00									+
Runoff Reduction (ft ³)	323	0	358									
runon reduction (it)	020		000	1					<u>l</u>	<u>l</u>	l.	
CALCULATED WQCV RI	ESULTS											
Area ID	C1.2a	C1.2b	C1.2c									
WQCV (ft ³)	1077	555	0									
WQCV Reduction (ft ³)	323	0	0									
WQCV Reduction (%)	30%	0%	0%									
Untreated WQCV (ft ³)	754	555	0									
CALCULATED DESIGN	POINT RESU	LTS (sums re	sults from	all columns v	vith the same	Downstream	n Desian Po	int ID)				
Downstream Design Point ID												
DCIA (ft²)	13,325											
UIA (ft²)	25,847											
RPA (ft²)	720											
SPA (ft²)	7,153											
Total Area (ft²)	47,045											
Total Impervious Area (ft²)	39,172											<u> </u>
WQCV (ft ³)	1,632											+
WQCV Reduction (ft ³) WQCV Reduction (%)	323 20%											
Untreated WQCV (ft ³)												
Unitediated WQCV (it.) 1,300 1,500												
CALCULATED SITE RES	SULTS (sums	results from	all column	s in workshe	et)							
Total Area (ft²)	47,045											
Total Impervious Area (ft²)	39,172											
WQCV (ft ³)	1,632											
WQCV Reduction (ft ³)	323											
WQCV Reduction (%)	20%											
Untreated WQCV (ft ³)	1,309	j										

LOT 2, THE SHOPS FIL. NO. 1A AT MERIDIAN RANCH **CHANNEL CALCULATION SUMMARY - SITE DRAINAGE SWALES**

PROPOSED CHANNEL / SWALE	SLOPE (%)	SIDE SLOPE (Z)	BOT. WIDTH (FT)	CHANNEL DEPTH (FT)	FRICTION FACTOR (n)	BASIN	Q100 BASIN FLOW (CFS)	CHANNEL FLOW % OF BASIN	Q100 CHANNEL FLOW (CFS)	Q100 DEPTH (FT)	Q100 VELOCITY (FT/S)	TOP WIDTH (FT)	CHANNEL LINING
SWALE C1.2	2.0	4:1	4	1.0	0.030	C1.2	8.0	100	8.0	0.4	3.3	7.4	GRASS
				-									

ASSUMPTIONS:

- 1) Channel flow calculations based on Manning's Equation
 2) Channel depth includes 1' minimum freeboard
 3) n = 0.03 for grass-lined non-irrigated channels (minimum)

- 4) n = 0.035 for riprap-lined channels
 5) Vmax = 5.0 fps for 100-year flows w/ grass-lined channels
 6) Vmax = 8.0 fps for 100-year flows w/ Erosion Control Blankets (Tensar Eronet SC150 or equal)
 7) Vmax = 10.0 fps for 100-year flows w/ Erosion Control Blankets (Tensar Eronet C125 or equal)

Hydraulic Analysis Report

Project Data

Project Title: Project - Lot 2, The Shops Fil. No. 1A at Meridian Ranch

Designer: JPS

Project Date: Thursday, March 16, 2023 Project Units: U.S. Customary Units

Notes:

Channel Analysis: Channel Analysis-Swale C1.2

Notes:

Input Parameters

Channel Type: Trapezoidal Side Slope 1 (Z1): 4.0000 ft/ft Side Slope 2 (Z2): 4.0000 ft/ft Channel Width: 4.0000 ft

Longitudinal Slope: 0.0200 ft/ft

Manning's n: 0.0300 Flow: 8.0000 cfs

Result Parameters

Depth: 0.4254 ft

Area of Flow: 2.4258 ft^2 Wetted Perimeter: 7.5083 ft Hydraulic Radius: 0.3231 ft Average Velocity: 3.2979 ft/s

Top Width: 7.4036 ft
Froude Number: 1.0153
Critical Depth: 0.4292 ft
Critical Velocity: 3.2601 ft/s
Critical Slope: 0.0193 ft/ft
Critical Top Width: 7.43 ft

Calculated Max Shear Stress: 0.5310 lb/ft^2 Calculated Avg Shear Stress: 0.4032 lb/ft^2

JPS ENGINEERING

SHOPS AT MERIDIAN RANCH CONVENIENCE STORE STORM INLET SIZING SUMMARY

	BASIN F	LOW		INLET FLOW						
INLET	DP	Q5 FLOW (CFS)	Q100 FLOW (CFS)	INLET FLOW % OF BASIN	Q5 FLOW (CFS)	Q100 FLOW (CFS)		INLET CONDITION / TYPE	INLET SIZE (FT)	INLET CAPACITY (CFS)
		,	, ,		` '	Ì			Ì	,
C1.1	C1.1	3.6	6.2	100	3.6	6.6		TYPE R (GRADE)	10'	5.3
C1.2	C1.2	4.2	7.8	100	4.3	8.0		TYPE C (SUMP)	SGL	17.2

STORM-INLET-SHOPS-0323 4/1/2023

MHFD-Inlet, Version 5.01 (April 2021)

INLET MANAGEMENT

Worksheet Protected

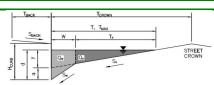
INLET NAME	Inlet C1.1	Inlet C1.2		
Site Type (Urban or Rural)	URBAN	URBAN		
Inlet Application (Street or Area)	STREET	AREA		
Hydraulic Condition	On Grade	Swale		
Inlet Type	CDOT Type R Curb Opening	CDOT Type C (Depressed)		

User-Defined Design Flows				
Minor Q _{Known} (cfs)	3.6	4.3		
Major Q _{Known} (cfs)	6.6	8.0		
Bypass (Carry-Over) Flow from Upstream	1			
Receive Bypass Flow from:	No Bypass Flow Received	User-Defined		
Minor Bypass Flow Received, Q _b (cfs)	0.0	0.1		
Major Bypass Flow Received, Q _b (cfs)	0.0	1.3		
Watershed Characteristics				
Subcatchment Area (acres)				
Percent Impervious				
NRCS Soil Type				
Trices son Type				
Watershed Profile				
•				
Watershed Profile Overland Slope (ft/ft)				
Watershed Profile Overland Slope (ft/ft) Overland Length (ft)				
Watershed Profile Overland Slope (ft/ft) Overland Length (ft) Channel Slope (ft/ft) Channel Length (ft)				
Watershed Profile Overland Slope (ft/ft) Overland Length (ft) Channel Slope (ft/ft) Channel Length (ft) Minor Storm Rainfall Input				
Watershed Profile Overland Slope (ft/ft) Overland Length (ft) Channel Slope (ft/ft) Channel Length (ft) Minor Storm Rainfall Input Design Storm Return Period, T _r (years)				
Watershed Profile Overland Slope (ft/ft) Overland Length (ft) Channel Slope (ft/ft) Channel Length (ft) Minor Storm Rainfall Input				
Watershed Profile Overland Slope (ft/ft) Overland Length (ft) Channel Slope (ft/ft) Channel Length (ft) Minor Storm Rainfall Input Design Storm Return Period, T _r (years) One-Hour Precipitation, P ₁ (inches) Major Storm Rainfall Input				
Watershed Profile Overland Slope (ft/ft) Overland Length (ft) Channel Slope (ft/ft) Channel Length (ft) Minor Storm Rainfall Input Design Storm Return Period, T _r (years) One-Hour Precipitation, P ₁ (inches)				

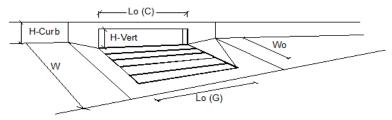
CALCULATED OUTPUT

Minor Total Design Peak Flow, Q (cfs)	3.6	4.4
Major Total Design Peak Flow, Q (cfs)	6.6	9.3
Minor Flow Bypassed Downstream, Q _b (cfs)	0.1	0.0
Major Flow Bypassed Downstream, Q _b (cfs)	1.3	0.0

MHFD-Inlet, Version 5.01 (April 2021) ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) Project: Shops at Meridian Ranch Convenience Store Inlet ID: Inlet C1.1



INLET ON A CONTINUOUS GRADE MHFD-Inlet, Version 5.01 (April 2021)



Design Information (Input) CDOT Type R Curb Opening	1 -	MINOR	MAJOR	
Type of Inlet	Type =		Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	10.00	10.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	$W_o =$	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity	_	MINOR	Major	
Total Inlet Interception Capacity	Q =	3.5	5.3	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	$Q_b =$	0.1	1.3	cfs
Capture Percentage = Q_a/Q_o =	C% =	98	80	%

1

AREA INLET IN A SWALE

A, B, C, D, or E =

n =

S₀ =

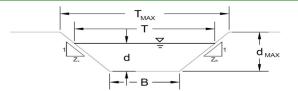
Z1 =

Z2 =

Q_o =

d =

Shops at Meridian Ranch Convenience Store Inlet C1.2



This worksheet uses the NRCS vegetal retardance method to determine Manning's n.

ft/ft

ft/ft

ft/ft

Major Storm **42.3**

1.00

9.3

0.46

cfs

ft

cfs

ft

For more information see Section 7.2.3 of the USDCM.

Analysis of Trapezoidal Grass-Lined Channel Using SCS Method

NRCS Vegetal Retardance (A, B, C, D, or E) Manning's n (Leave cell D16 blank to manually enter an n value) Channel Invert Slope

Bottom Width

Left Side Slope

Right Side Sloe

Check one of the following soil types:

Soil Type:	Max. Velocity (V_{MAX})	Max Froude No. (F_{MAX})
Non-Cohesive	5.0 fps	0.60
Cohesive	7.0 fps	0.80
Paved	N/A	N/A

Maximum Allowable Top Width of Channel for Minor & Major Storm Maximum Allowable Water Depth in Channel for Minor & Major Storm

Paved Minor Storm Major Storm T_{MAX} = 12.00 12.00 0.50 1.00 d_{MAX} = ft

10.8

0.50

4.4

0.31

0.030

0.0200 4.00

4.00

4.00

Non-Cohesive Cohesive

Choose One:

Allowable Channel Capacity Based On Channel Geometry

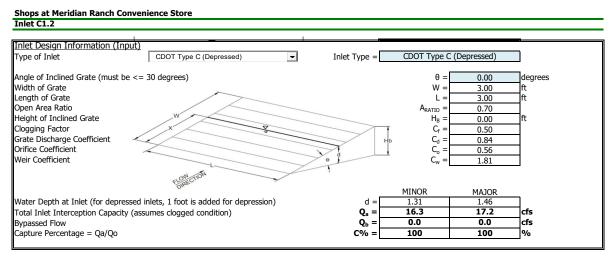
MINOR STORM Allowable Capacity is based on Depth Criterion MAJOR STORM Allowable Capacity is based on Depth Criterion

Water Depth in Channel Based On Design Peak Flow Design Peak Flow

Water Depth

Minor storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management' Major storm max. allowable capacity GOOD - greater than the design flow given on sheet 'Inlet Management'

AREA INLET IN A SWALE



Warning 04: Froude No. exceeds USDCM Volume I recommendation.

SHOPS AT MERIDIAN RANCH CONVENIENCE STORE STORM SEWER SIZING SUMMARY

	PIPE FLOW			F	PIPE CAPACITY		
PIPE	DESIGN POINT	Q5 FLOW (CFS)	Q100 FLOW (CFS)		PIPE SIZE	MIN. PIPE SLOPE	PIPE CAPACITY (CFS)
04.4	04.4	0.5	F.0		40	0.00/	5.0
C1.1	C1.1	3.5	5.3	H	12	2.2%	5.3
C1.2	C1.2	4.3	8.0		12	5.1%	8.0

ASSUMPTIONS:

1. STORM DRAIN PIPE ASSUMED TO BE RCP OR HDPE

STORM-INLET-SHOPS-0323 4/1/2023

Hydraulic Analysis Report

Project Data

Project Title: Project - Shops at Meridian Ranch C-Store

Designer: JPS

Project Date: Tuesday, February 7, 2023 Project Units: U.S. Customary Units

Notes:

Channel Analysis: SD-C1.1

Notes:

Input Parameters

Channel Type: Circular Pipe Diameter: 1.0000 ft

Longitudinal Slope: 0.0220 ft/ft

Manning's n: 0.0130 Depth: 1.0000 ft

Result Parameters

Flow: 5.2845 cfs

Area of Flow: 0.7854 ft^2 Wetted Perimeter: 3.1416 ft Hydraulic Radius: 0.2500 ft Average Velocity: 6.7284 ft/s

Top Width: 0.0000 ft
Froude Number: 0.0000
Critical Depth: 0.9302 ft
Critical Velocity: 6.9412 ft/s
Critical Slope: 0.0190 ft/ft
Critical Top Width: 0.51 ft

Calculated Max Shear Stress: 1.3728 lb/ft^2 Calculated Avg Shear Stress: 0.3432 lb/ft^2

Channel Analysis: SD-C1.2

Notes:

Input Parameters

Channel Type: Circular Pipe Diameter: 1.0000 ft

Longitudinal Slope: 0.0510 ft/ft

Manning's n: 0.0130 Depth: 1.0000 ft

Result Parameters

Flow: 8.0459 cfs

Area of Flow: 0.7854 ft^2 Wetted Perimeter: 3.1416 ft Hydraulic Radius: 0.2500 ft Average Velocity: 10.2444 ft/s

Top Width: 0.0000 ft

Froude Number: 0.0000
Critical Depth: 0.9855 ft
Critical Velocity: 10.2748 ft/s
Critical Slope: 0.0463 ft/ft
Critical Top Width: 0.24 ft

Calculated Max Shear Stress: 3.1824 lb/ft^2 Calculated Avg Shear Stress: 0.7956 lb/ft^2

APPENDIX D FIGURES

National Flood Hazard Layer FIRMette

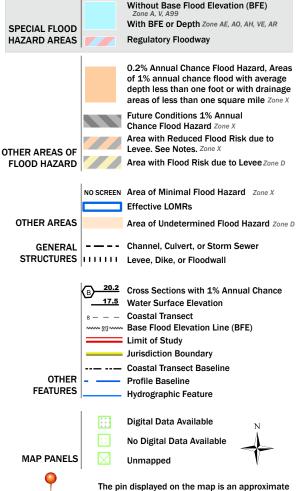


Basemap: USGS National Map: Orthoimagery: Data refreshed October, 2020



Legend

SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT



This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The basemap shown complies with FEMA's basemap accuracy standards

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