FINAL DRAINAGE LETTER for CROSSROADS MIXED USE FILING NO. 1 UNDERGROUND DETENTION

EL PASO COUNTY, COLORADO

FEBRUARY 2023

Prepared for:

Crossroads Metropolitan District No. 1 Mr. Danny Mientka 90 South Cascade Avenue, Suite 1500 Colorado Springs, Colorado Springs 80903

Prepared by:



CIVIL CONSULTANTS, INC.

212 N. Wahsatch Avenue, Suite 305 Colorado Springs, CO 80903 (719) 955-5485

> Project #18-003 PCD File No. CDR232

FINAL DRAINAGE LETTER FOR CROSSROADS MIXED USE FILING NO.1 UNDERGROUND DETENTION EL PASO COUNTY COLORADO

DRAINAGE PLAN STATEMENTS

ENGINEERS STATEMENT

The attached drainage plan and report was prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the County for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.

Virgil A. Sanchez, P.E. #37160 For and on Behalf of M&S Civil Consultants, Inc

DEVELOPER'S STATEMENT

I, the developer have read and will comply with all the requirements specified in this drainage report and plan.

BY:

Danny Mientka – Owner

DATE:_____

ADDRESS: Crossroads Metropolitan District No. 1 90 South Cascade Avenue, Suite 1500 Colorado Springs, Colorado Springs 80903

EL PASO COUNTY'S STATEMENT

Filed in accordance with the requirements of El Paso County Land Development Code, Drainage Criteria Manual Volumes 1 and 2, and the Engineering Manual, as amended.

BY:

DATE: _____

Joshua Palmer, P.E. County Engineer / ECM Administrator

CONDITIONS:



February 11, 2023

El Paso County Planning & Community Development 2880 International Circle Suite 110 Colorado Springs, Colorado 80910 Attn: Joshua Palmer, P.E./County Engineer

RE: Drainage Letter for Crossroads Mixed Use Filing No.1 Underground Detention

Dear Mr. Palmer,

The following is the Drainage Letter for Crossroads Mixed Use Filing No.1 Underground Detention. The purpose of this letter is to show general conformance with the drainage patterns established by the **Final Drainage Report for Crossroads Mixed Use Filing No.1** (herein referenced as **FDR-CMU**) and to revise drainage patterns within the pond site to accommodate the underground detention (**Pond 1in Tract A**). **Pond 1**contains 3.120 acres and is located at 0 Meadowbrook Parkway in the southwestern quarter of Section 8, Township 14 South, Range 65 West of the 6th P.M. in El Paso County, Colorado.

Soils in the project area have been determined to be Blakeland Loamy Sand (8), which are characterized to be part of Hydrologic Soil Types "A" as determined from the United States Department of Agriculture (USDA) Natural Resources Conservation Service (NRCS) "Web Soils Survey". A soils map illustrating the site location and soil types is provided in the appendix of this report. The Underground Detention (UGD) may be supported on shallow foundations of compacted native soil or imported compacted structural fill prepared in accordance with the "Soil and Geology Study for Crossroads Commercial" prepared by RMG, revised date August 20, 2021 PCD File No. SP2011. Recommendations by ADS and RMG have been reflected on the construction drawings for the UGD. Groundwater was not encountered in the test boring performed by this report or subsequent reports.

According to the Federal Emergency Management Agency (FEMA) Flood Insurance Rate Map (FIRM) Nos. 08041C0754 G, effective date December 7th, 2018, none of the site lies within a designated floodplain. A copy of these annotated maps can be found in the appendix. The Sand Creek East Fork Channel is located to the northwest of the adjacent Meadowbrook Crossing subdivision.

Four Step Process

Step 1 Employ Runoff Reduction Practices – Approx. 3.120 acres of the proposed development is being set aside for an Underground Detention (UGD)-Full Spectrum Detention (FSD) Pond 1. Runoff produced within the site will be routed over landscaped park area to 2-2'x3' area inlets. The developed parking area will be routed to 2-5' Type R inlets. Runoff reduction shall also be provided in the development of the upstream commercial pads that are conveyed in this system.

Step 2 Stabilize Drainageways – The development of this site is not anticipated to have negative effects on downstream drainage ways since flows released will be below historic rates. In the interim, the

site proposes a temporary sedimentation pond, before discharging at the southwest property corner of the site and onto an adjacent undeveloped property. This ensures that in this stage of the development negative effects on the downstream drainage ways will be avoided.

In the proposed condition, the flow is discharged to the same location offsite through an RCP pipe outfall lined with rip rap. From here it continues southwest in CDOT's man-made roadside ditch until it reaches Peterson Road. It is then conveyed to the other side of the road, into a similar earthen channel, via a 36" CMP culvert. The drainage continues southwest in the right of way, until it reaches the East Fork Sand Creek Channel. Existing rip rap barriers are lined throughout this portion of the pathway approximately every 90-100 feet within the ditch to the channel bank. The Drainageway Exhibit provided in the Drainage Maps section of the Appendix provides a visual representation of this information. Roadside ditch calculations for various storm events are provided for the selected suitable downstream outfall (project site's discharge location) to ensure the facility can adequately contain and convey the flows.

Step 3 Provide Water Quality Capture Volume (WQCV)– The site will use an Underground Detention-Full Spectrum Detention (FSD) **Pond 1** to control developed runoff that is discharging into an existing CDOT ROW roadside ditch and ultimately into Sand Creek. The UGD pond outlet structure will be designed to drain the water quality event storm in 40 hours, while reducing the 100 year peak discharge to approximately 90% of the predevelopment conditions. This outlet design is very similar to a standard full spectrum detention pond. The Baysavers upstream of the UGD are designed to remove 80% of the TSS on an annual aggregate removal basis.

Step 4 Consider Need For Selecting Industrial And Commercial BMP's – This submittal provides a Preliminary Grading and Erosion Control plan. The proposed project will use silt fence, a vehicle tracking control pad, a concrete washout area, mulching and reseeding to mitigate the potential for erosion across the site.

The **Final Drainage Report for Crossroads Mixed Use Filing No.1 (FDR-CMU),** prepared by M&S Civil Consultants, Inc. and approved 06/09/2022. **Tract A** is identified as **Basin J** and consists of the proposed EDB pond. The majority of the surface flow (**Basin J**) was routed into the pond and will now be routed as surface flow, over the underground detention facility, to two proposed 5' sump inlets and 2-2' x 3'area inlets. The commercial and multi-family development surrounding the site will still route flows to the underground detention specified by the **FDR-CMU** and the **Final Drainage Report for Aura at Crossroads** (herein referenced as **FDR-AC**), prepared by Harris Kocher Smith, approved 06/23/2022. Due to the extension of the parking lot within Tract A and with some additional surface runoff from the commercial site to the North, surface runoff has increased slightly. There has been no significant change in flows from what was analyzed for the above ground detention pond. The additional flows are accounted for in the inlet and storm sewer summary and in the Underground Detention.

Design Point 1 (Q5=1.2 cfs, Q100=4.7 cfs) total runoff generated by **Basin A** and adjacent planned Lot 11 runoff. **Basin A** (Q5=0.6 cfs, Q100=3.4cfs) contains 1.32 acres of park/playground area and access road and adjacent planned landscaped area of Lot 1 DP16 (FDR-AC, Q5=0.57 cfs, Q100=1.43cfs). The combined surface runoff sheet flows to **Design Point 1** (Q5=1.2 cfs, Q100=4.7 cfs) and will captured by a proposed 2'x3' ADS area inlet. The captured flow shall be routed via a proposed 24" RCP storm pipe **PR25** (Q5=1.2 cfs, Q100=4.7 cfs). These flows are routed to a proposed Type 1 manhole. See proposed drainage map in the appendix.

Design Point 2 (Q5=0.4 cfs, Q100=2.3cfs) total runoff generated by **Basin B**. **Basin B** (Q5=0.3 cfs, Q100=1.7cfs) contains 0.88 acres of park/playground area and access road. The surface runoff sheet flows to **Design Point 2** (Q5=0.4 cfs, Q100=2.3 cfs) and will captured by a proposed 2'x3' ADS area inlet. The captured flow shall be routed via a proposed 24" RCP storm pipe **PR26** (Q5=0.4 cfs, Q100=2.3 cfs). These flows are routed to a proposed Type 1 manhole. The cumulative flows from **PR26**, **PR25** and **PR19** (48" RCP **FDR-AC**, Q5=35.4 cfs, Q100=65.5 cfs) are routed via a proposed 48" RCP **PR27** (Q5=36.8 cfs, Q100=71.9 cfs) to an XK Baysaver north vault which is part of the underground detention infrastructure. See proposed drainage map and underground detention details in the appendix. The Baysaver system removes greater than 80% pollution relying on density differences and gravity to remove suspended solids and floatables (hydrocarbons, floating debris, etc.) from stormwater runoff. The Baysaver is a concrete structure that routes the stormwater between two different bays for optimal removal efficiency. Pollutants are trapped inside the precast structure until they are removed by routine maintenance. Sizing shall be determined by ADS per our design flows, annual aggregate removal and local design regulations.

Design Point 3 (Q5=1.6 cfs, Q100=3.6 cfs) total runoff generated by **Basin C** and adjacent planned **Lot 11** runoff. **Basin C** (Q5=1.0 cfs, Q100=1.9 cfs) contains 0.25 acres of parking lot and adjacent planned landscaped area of **Lot 1 DP15** (**FDR-AC**, Q5=0.47 cfs, Q100=1.27cfs). The combined surface runoff sheet flows to **Design Point 3** (Q5=1.6 cfs, Q100=3.6 cfs) and will captured by a proposed 5' CDOT Type R sump inlet. The captured flow shall be routed via a proposed 18" RCP storm pipe **PR23.1** (Q5=1.6 cfs, Q100=3.6 cfs). These flows are routed through a proposed 4' diameter Type II manhole and then routed to **Design Point 4**. Simultaneous construction of UGD and parking lot to be anticipated. In the event construction of parking lot is delayed flows will be routed to Design Point 2. The 2'x3' area inlet and storm sewer have been sized to accept additional flow.

Design Point 4 (Q5=2.2 cfs, Q100=4.3 cfs) total runoff generated by **Basin D**. **Basin D** (Q5=2.2 cfs, Q100=4.3 cfs) contains 0.64 acres of parking lot and landscaped areas. The surface runoff flows to **Design Point 4** (Q5=2.2 cfs, Q100=4.3 cfs) and will captured by a proposed 5' CDOT Type R sump inlet. The flows from **PR23.1** shall combine with the flow captured flows from **DP4** be routed via a proposed 24" RCP storm pipe **PR23.2** (Q5=1.7 cfs, Q100=4.2 cfs). These flows are routed to a proposed Type 1 manhole. The cumulative flows from **PR15** (48" RCP **FDR-CMU**, Q5=48.0 cfs, Q100=93.7 cfs) and **PR16** (24" RCP **FDR-CMU**, Q5=10.8 cfs, Q100=19.6 cfs) are routed via a proposed 48" RCP **PR17** (Q5=55.6 cfs, Q100=107.4 cfs) to a Type 1 manhole. The cumulative flows from **Lot 1 DP14 PR21** (30" RCP **FDR-AC**, Q5=2.1 cfs, Q100=4.2 cfs) and **PR17** are routed via a proposed 54" RCP **PR22** (Q5=56.5 cfs, Q100=109.4 cfs) to a Type 1 manhole. The cumulative flows from **PR23.2** and **PR22** are routed via a proposed 54" RCP **PR24** (Q5=57.8 cfs, Q100=112.6 cfs) to an XK Baysaver east vault which is part of the underground detention infrastructure. See proposed drainage map and underground detention details in the appendix. See discussion of Baysaver in Design Point 2 paragraph. Simultaneous construction of UGD and parking lot to be anticipated. In the event construction of parking lot is delayed flows will be routed to Design Point 2. The 2'x3' area inlet and storm sewer have been sized to accept additional flow.

<u>Design Point 5</u> (Q5=0.1 cfs, Q100=0.7 cfs) total runoff generated by **Basin E** contains 0.20 acres of seeded embankment and landscaped area. The surface runoff sheet flows to **Design Point 5** (Q5=0.1 cfs, Q100=0.7 cfs) and will follow historic drainage patterns. The flows are significantly less than the historic flows (**FDR-CMU**, Q5=0.1 cfs, Q100=0.7 cfs) that were released along this section of property boundary, therefore no negative impacts are anticipated to the downstream improvements or facilities with the approval of this drainage letter.

Proposed FSD Pond 1 shall be replaced with proposed UGD Pond 1 improvements and shall be installed per the Crossroads Mixed Use Filing No.1 Storm Underground Detention construction plans. The proposed **UGD** has a design volume of 206,903 cubic feet. The proposed UGD Pond 1 will release 14.5 cfs in the 100-year event. No additional storm sewer improvements are proposed for this site. This drainage letter

includes the previously approved Proposed Drainage Map for Drainage Report for Crossroads Mixed Use Filing No.1 (FDR-CMU) and Final Drainage Report for Aura at Crossroads (FDR-AC).

This final drainage letter for Pond 1 Tract A and underground detention is in compliance with the design as proposed within the Final Drainage Report for Crossroads Mixed Use Filing No.1 (FDR-CMU); therefore no negative impacts are anticipated to the downstream improvements or facilities with the approval of this drainage letter. ADS will accommodate a preconstruction meeting to discuss installation and inspection requirements for the UGD as outlined in the Operation and Maintenance (O&M) Manual accompanying this submittal. Contractor will comply with ADS requirements and submit lab results that are in compliance with requirements. As a condition of deviation request DEV221, this UGD will follow the post-construction requirements of the Pilot Program outlined by EPC on a separate document.

clarify where stage=0ft. Is it at "floor" of arch ADS Sizing 🗲

system? Or at the bottom of the stone layer?

Stormtech underground detention systems are designed to meet the minimum detention volume requirement. The volume is held within the chambers and stone. The stone surrounding the chambers consists of the foundation stone below the chambers and embedment stone surrounding the chambers. The stone is an important component of the structural system and provides open void space for stormwater storage (40% porosity). A Cumulative Stage Storage spreadsheet is provided to show the cumulative storage volumes and stage area data.

The stage area date is utilized within the MHFD Detention spreadsheet for outlet structure design.

Sediment Loading /Maintenance Interval Calculation

The Mass Load Interval Calculation is provided for the two isolator rows for this project (given the area, curve number, and # of Isolator Row chambers). Based on the provided specification, a minimum requirement for sediment removal maintenance from the system to be done every 7-8 years, which are met by setting the maintenance interval to be after 3" of sediment accumulation. Since the BaySeparator is directly upstream of the Isolator Rows, the two items will be acting in series. We anticipate the BaySeparators will pro long the maintenance interval of the Isolator Rows. Without knowing exactly what the BaySeparator is capturing in terms of particle size and % captured in real time, we cannot say for certain the added length of maintenance interval the Isolator Row will have.

Outline of inspection requirements during construction as follows;

-Set-up a pre-con with manufacturer/vendor and EPC staff.

-EPC-DPW Stormwater staff need to be onsite to perform QC/testing for the following milestones. Contractor to alert EPC prior to commencing any of these items.

-Installation of fabric.

-Placement of underground structures (line ADS arch chambers, BaySeperator, Outlet structure,etc.).

-Placement of stone.

-Provide EPC staff with lab results, spec sheets, and delivery receipts;

-Subgrade compaction per ADS requirements.

- -Stone (size, washed type, etc.)
- -Fabric.

As a condition of deviation request DEV221, this system will follow the post-construction requirements of the Pilot Program outlined by EPC on a separate document.

This site is in the Sand Creek Drainage Basin. Drainage fees were paid at the time of platting as Tract A of Crossroads Mixed Use Filing No. 1 (Reception No. 222714975), therefore no additional Drainage Bridge and/or Pond fees are not required. See Appendix of the "Crossroads Mixed Use Filing No.1", approved June 22, 2022, by MS Civil Consultants, Inc, for previously paid drainage and bridge fees.

Unresolved comment from Review 1: Discuss how much extra capacity above the 100-yr storm has been provided in the UGD system.

Review 2 update: At a minimum just discuss the freeboard provided. Private Drainage Facilities (NON-Reimbursable) Underground Detention Pond 1. Additional storm not accounted for in **FDR-CMU**:

CONSTRUCTION COST OPINION

Item	Description	Quar	ntity	Unit	Cost		Cost
1.	18" RCP	375	LF	\$78	/LF		\$29,250.00
2.	24" RCP	166	LF	\$104	/LF		\$17,264.00
3.	4' Type II Manhole	1	EA	\$4,500	/EA		\$4,500.00
4.	2'x3'Nyloplast Area Inlet	2	EA	\$4,028	/EA		\$8,056.00
5.	5' CDOT Type R Sump Inlet	2	EA	\$5,700	/EA		\$11,400.00
6.	Underground Detention Pond 1	1	LS	\$TBD	/LS		\$TBD
						Total	\$TBD

TBD - The costs for the ADS components of the UGD system are currently being requested. The engineer does not have access to previous cost data on the Baysavers, or the MC 7200 Chambers.

Respectfully,

Virgil A Sanchez

Virgil A. Sanchez, P.E. M&S Civil Consultants, Inc.

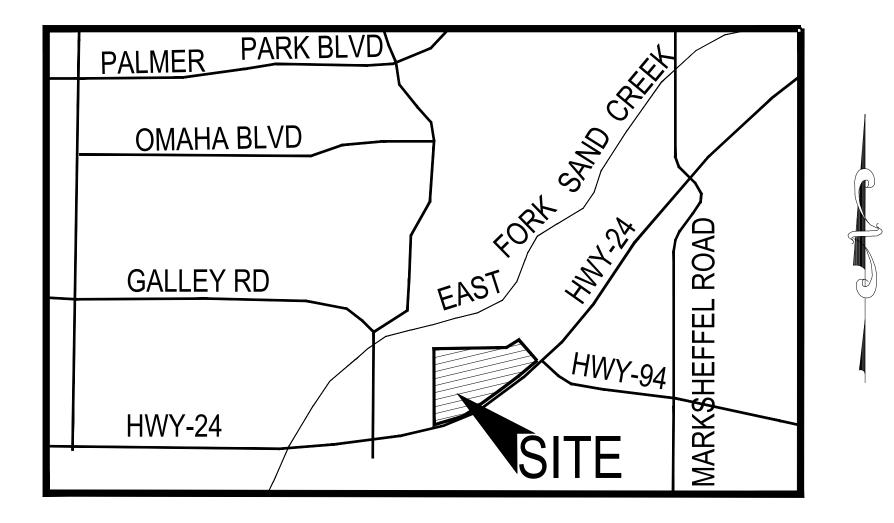
REFERENCES

- 1.) "El Paso County and City of Colorado Springs Drainage Criteria Manual".
- 2.) "Mile High Flood District Storm Drainage Criteria Manual"
- 3.) SCS Soils Map for El Paso County.
- Flood Insurance Rate Map (FIRM), Federal Emergency Management Agency, Revised date December 7th, 2018.
- 5.) "Final Drainage Report for Crossroads Mixed Use Filing No.1", prepared by M&S Civil Consultants, Inc. and approved 06/09/2022Final Drainage Report for Claremont Business Park 2 Filing No.1", dated December, 2020, by M&S Civil Consultants, Inc.
- 6.) "Final Drainage Report for Aura at Crossroads", prepared by Harris Kocher Smith, approved 06/23/2022
- Soil and Geology Study for Crossroads Commercial" prepared by RMG, revised date August 20, 2021 PCD File No. SP2011.

ATTACHMENTS:

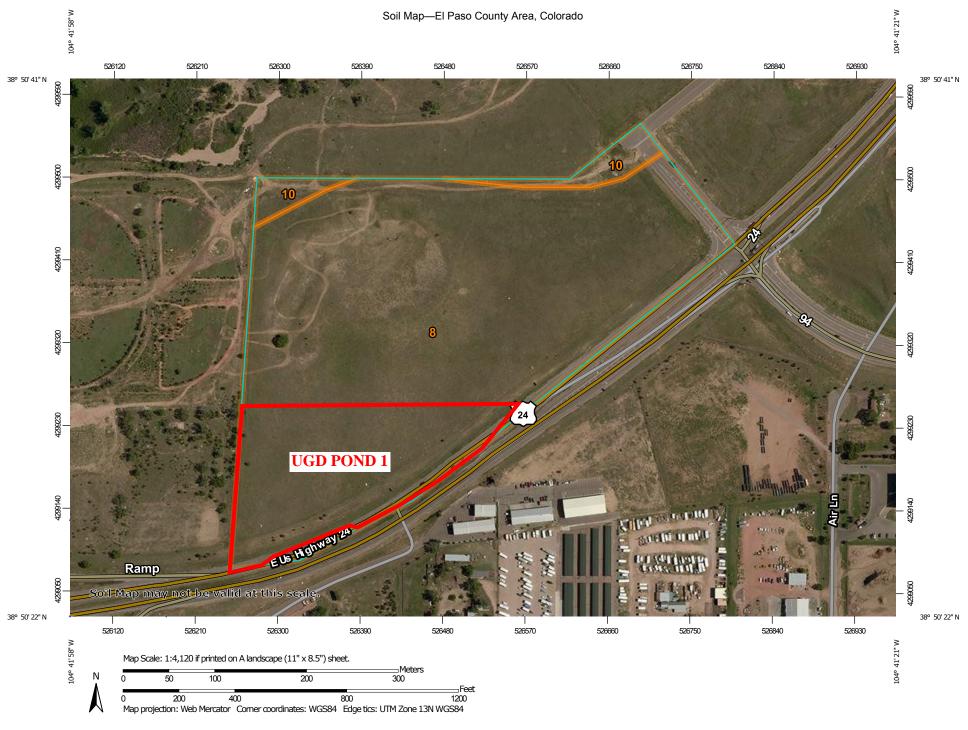
Vicinity map Final Drainage Report for Crossroads Mixed Use Filing No.1- Proposed Drainage Map Final Drainage Report for Aura at Crossroads - Proposed Drainage Map Hydrologic and Hydraulic Calculations Underground Detention Details Final Drainage Letter Crossroads Mixed Use Filing No.1 Underground Detention – Proposed Drainage Map ATTACHMENTS

VICINITY MAP



VICINITY MAP N.T.S.

SOILS MAP



USDA Natural Resources Conservation Service Web Soil Survey National Cooperative Soil Survey

MAP	LEGEND	MAP INFORMATION
Area of Interest (AOI)	 Spoil Area Stony Spot Very Stony Spot 	MAP INFORMATION The soil surveys that comprise your AOI were mapped at 1:24,000. Warning: Soil Map may not be valid at this scale. Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale. Please rely on the bar scale on each map sheet for map measurements. Source of Map: Natural Resources Conservation Service Web Soil Survey URL: Coordinate System: Web Mercator (EPSG:3857)
Sinkhole Sodic Spot	 US Routes Major Roads Local Roads Background Aerial Photography	 Maps from the Web Soil Survey are based on the Web Mercato projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as th Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required. This product is generated from the USDA-NRCS certified data a of the version date(s) listed below. Soil Survey Area: El Paso County Area, Colorado Survey Area Data: Version 15, Oct 10, 2017 Soil map units are labeled (as space allows) for map scales 1:50,000 or larger. Date(s) aerial images were photographed: Jun 3, 2014—Jun 2014 The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.



Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI			
8	Blakeland loamy sand, 1 to 9 percent slopes	35.2	95.4%			
10	Blendon sandy loam, 0 to 3 percent slopes	1.7	4.6%			
Totals for Area of Interest		36.9	100.0%			



FIRM PANELS

NOTES TO USERS

This map is for use in administering the National Flood Insurance Program. It does not necessarily identify all areas subject to flooding, particularly from local drainage sources of small size. The community map repository should be consulted for possible updated or additional flood hazard information.

To obtain more detailed information in areas where Base Flood Elevations (BFEs) and/or floodways have been determined, users are encouraged to consult the Flood Profiles and Floodway Data and/or Summary of Stillwater Elevations tables contained within the Flood Insurance Study (FIS) report that accompanies this FIRM. Users should be aware that BFEs shown on the FIRM represent rounded whole-foot elevations. These BFEs are intended for flood insurance rating purposes only and should not be used as the sole source of flood elevation information. Accordingly, flood elevation data presented in the FIS report should be utilized in conjunction with the FIRM for purposes of construction and/or floodplain management.

Coastal Base Flood Elevations shown on this map apply only landward of 0.0' North American Vertical Datum of 1988 (NAVD88). Users of this FIRM should be aware that coastal flood elevations are also provided in the Summary of Stillwater Elevations table in the Flood Insurance Study report for this jurisdiction. Elevations shown in the Summary of Stillwater Elevations table should be used for construction and/or floodplain management purposes when they are higher than the elevations shown on this FIRM.

Boundaries of the floodways were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations with regard to requirements of the National Flood Insurance Program. Floodway widths and other pertinent floodway data are provided in the Flood Insurance Study report for this jurisdiction.

Certain areas not in Special Flood Hazard Areas may be protected by flood control structures. Refer to section 2.4 "Flood Protection Measures" of the Flood Insurance Study report for information on flood control structures for this jurisdiction.

The projection used in the preparation of this map was Universal Transverse Mercator (UTM) zone 13. The horizontal datum was NAD83, GRS80 spheroid. Differences in datum, spheroid, projection or UTM zones zones used in the production of FIRMs for adjacent jurisdictions may result in slight positional differences in map features across jurisdiction boundaries. These differences do not affect the accuracy of this FIRM.

Flood elevations on this map are referenced to the North American Vertical Datum of 1988 (NAVD88). These flood elevations must be compared to structure and ground elevations referenced to the same vertical datum. For information regarding conversion between the National Geodetic Vertical Datum of 1929 and the North American Vertical Datum of 1988, visit the National Geodetic Survey website a http://www.ngs.noaa.gov/ or contact the National Geodetic Survey at the following address:

NGS Information Services NOAA, N/NGS12

National Geodetic Survey SSMC-3, #9202 1315 East-West Highway

Silver Spring, MD 20910-3282

To obtain current elevation, description, and/or location information for bench marks shown on this map, please contact the Information Services Branch of the National Geodetic Survey at (301) 713-3242 or visit its website at http://www.ngs.noaa.gov/.

Base Map information shown on this FIRM was provided in digital format by EI Paso County, Colorado Springs Utilities, and Anderson Consulting Engineers, Inc. These data are current as of 2008.

This map reflects more detailed and up-to-date stream channel configurations and floodplain delineations than those shown on the previous FIRM for this jurisdiction. The floodplains and floodways that were transferred from the previous FIRM may have been adjusted to conform to these new stream channel configurations. As a result, the Flood Profiles and Floodway Data tables in the Flood Insurance Study Report (which contains authoritative hydraulic data) may reflect stream channel distances that differ from what is shown on this map. The profile baselines depicted on this map represent the hydraulic modeling baselines that match the flood profiles and Floodway Data Tables if applicable, in the FIS report. As a result, the profile baselines may deviate significantly from the new base map channel representation and may appear outside of the floodplain.

Corporate limits shown on this map are based on the best data available at the time of publication. Because changes due to annexations or de-annexations may have occurred after this map was published, map users should contact appropriate community officials to verify current corporate limit locations.

Please refer to the separately printed Map Index for an overview map of the county showing the layout of map panels; community map repository addresses; and a Listing of Communities table containing National Flood Insurance Program dates for each community as well as a listing of the panels on which each community is located.

Contact FEMA Map Service Center (MSC) via the FEMA Map Information eXchange (FMIX) 1-877-336-2627 for information on available products associated with this FIRM. Available products may include previously issued Letters of Map Change, a Flood Insurance Study Report, and/or digital versions of this map. The MSC may also be reached by Fax at 1-800-358-9620 and its website at http://www.msc.fema.gov/.

f you have questions about this map or questions concerning the National Flood Insurance Program in general, please call 1-877-FEMA MAP (1-877-336-2627) or visit the FEMA website at http://www.fema.gov/business/nfip.

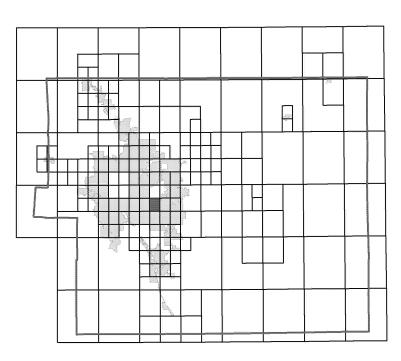
> El Paso County Vertical Datum Offset Table Vertical Datum

Offset (ft)

REFER TO SECTION 3.3 OF THE EL PASO COUNTY FLOOD INSURANCE STUDY FOR STREAM BY STREAM VERTICAL DATUM CONVERSION INFORMATION

Flooding Source

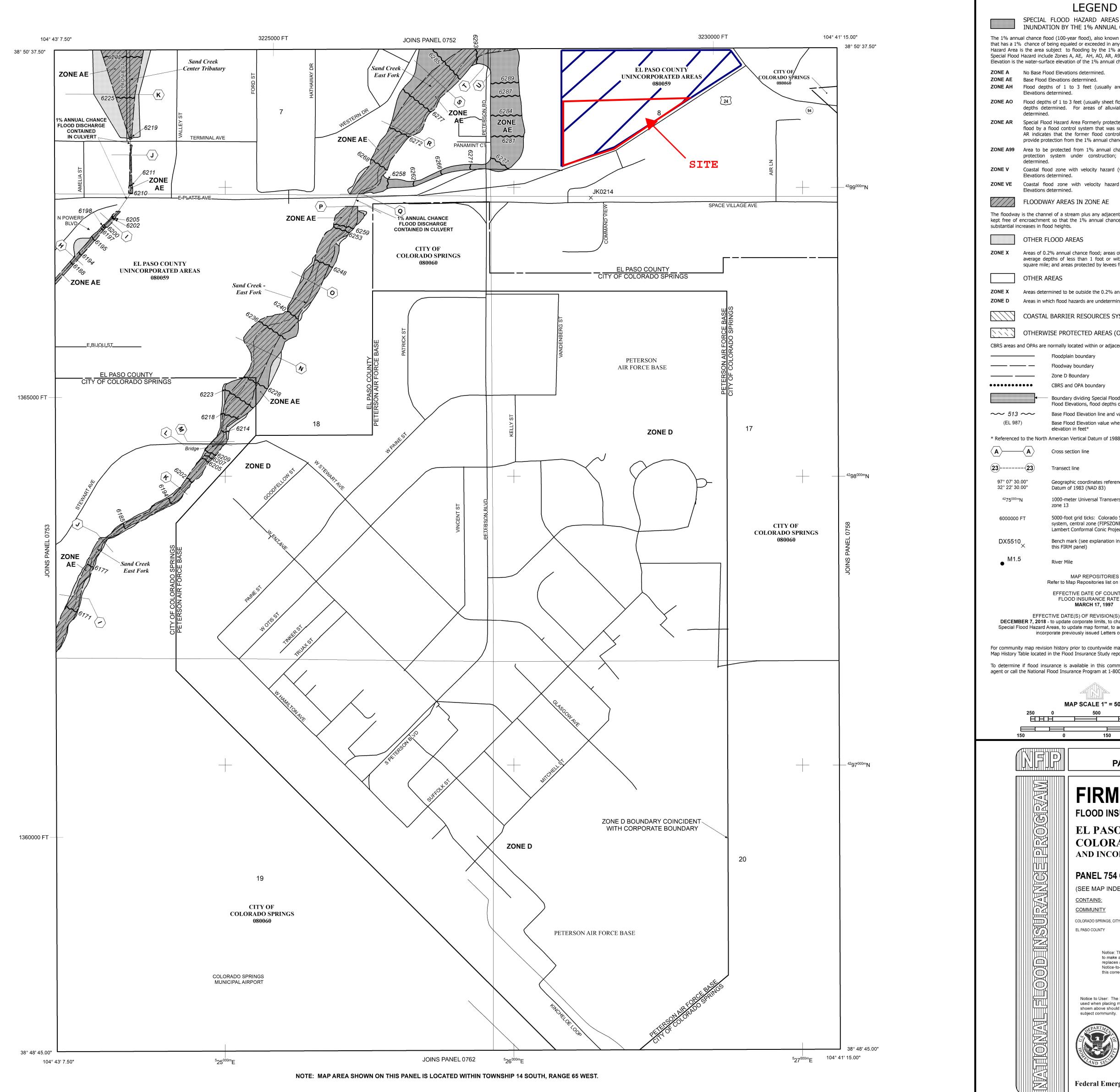
Panel Location Map



This Digital Flood Insurance Rate Map (DFIRM) was produced through a Cooperating Technical Partner (CTP) agreement between the State of Colorado Water Conservation Board (CWCB) and the Federal Emergency Management Agency (FEMA).

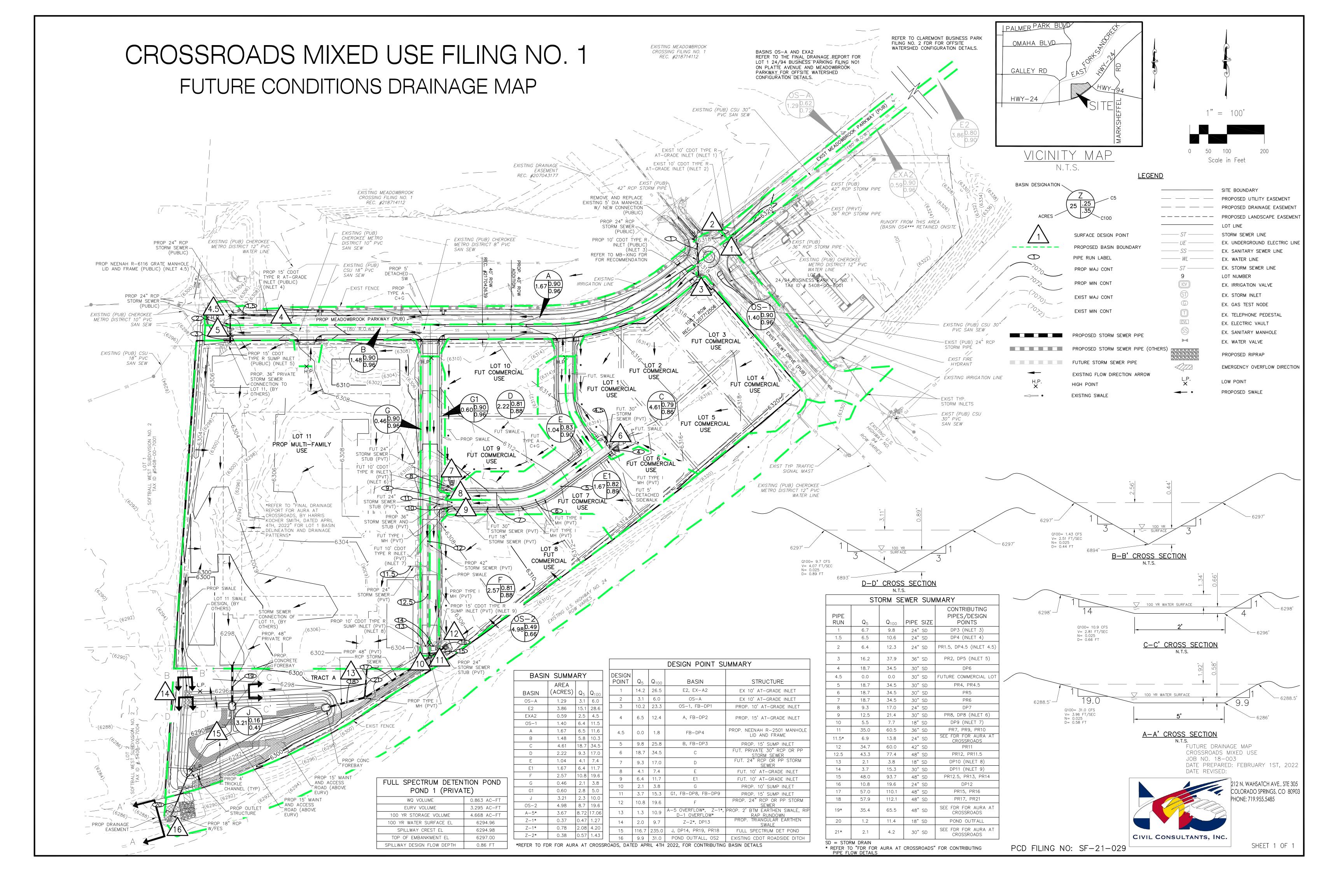


Additional Flood Hazard information and resources are available from local communities and the Colorado Water Conservation Board.

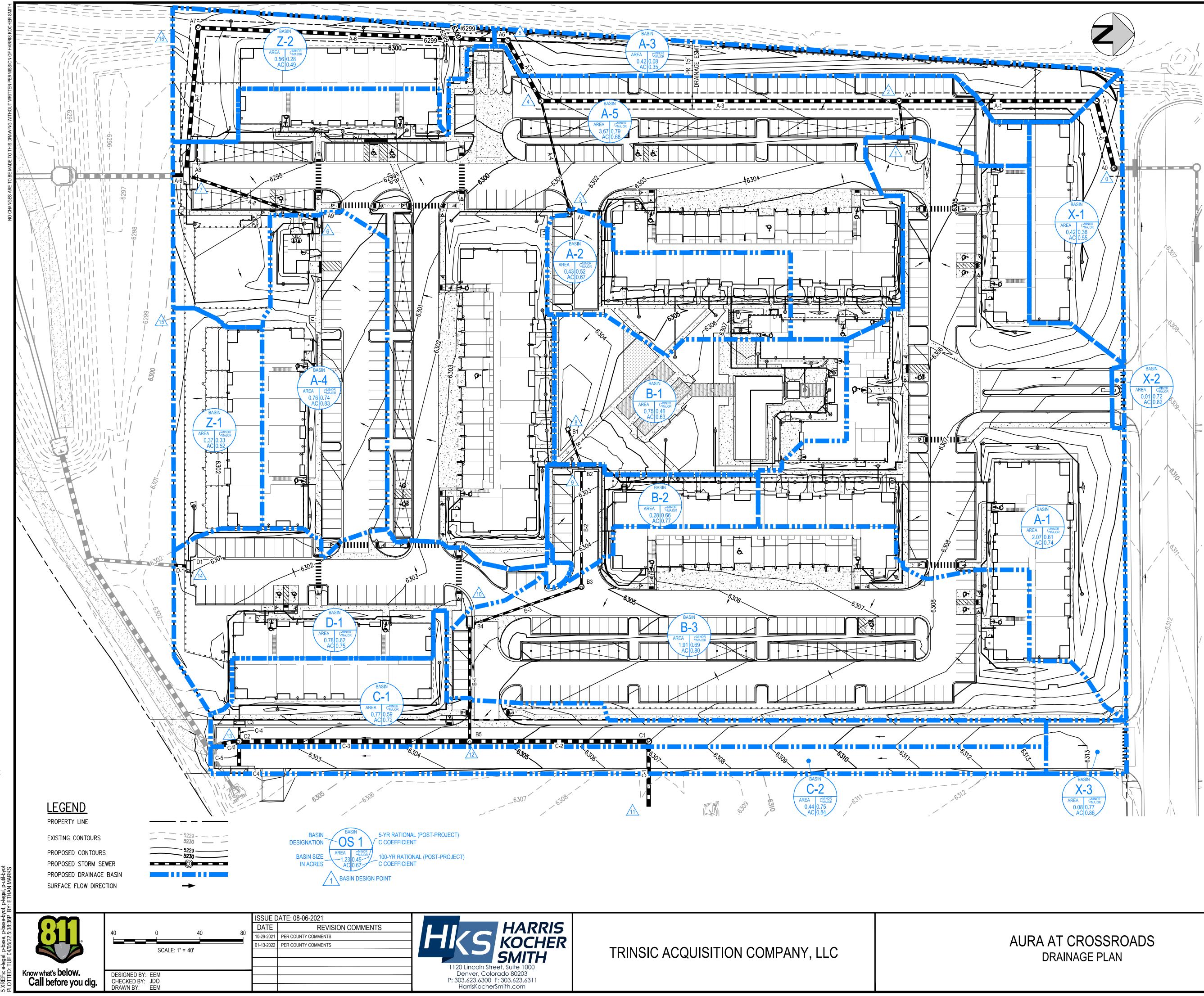


	INUNDATION	DD HAZARD AREAS (SFHAS) SUBJECT TO BY THE 1% ANNUAL CHANCE FLOOD
that has a 1% Hazard Area	 chance of being e is the area subject 	0-year flood), also known as the base flood, is the flood qualed or exceeded in any given year. The Special Flood to flooding by the 1% annual chance flood. Areas of es A, AE, AH, AO, AR, A99, V, and VE. The Base Flood
ZONE A	No Base Flood Ele	vation of the 1% annual chance flood. vations determined.
ZONE AE ZONE AH	Base Flood Elevati Flood depths of Elevations determ	1 to 3 feet (usually areas of ponding); Base Flood
ZONE AO		to 3 feet (usually sheet flow on sloping terrain); average d. For areas of alluvial fan flooding, velocities also
ZONE AR	flood by a flood of AR indicates that	ard Area Formerly protected from the 1% annual chance control system that was subsequently decertified. Zone the former flood control system is being restored to from the 1% annual chance or greater flood.
ZONE A99		cted from 1% annual chance flood by a Federal flood n under construction; no Base Flood Elevations
ZONE V	Elevations determ	
	Elevations determ	ne with velocity hazard (wave action); Base Flood ined. REAS IN ZONE AE
	is the channel of a	stream plus any adjacent floodplain areas that must be nat the 1% annual chance flood can be carried without
	OTHER FLOOD	jhts.
ZONE X	Areas of 0.2% an	nual chance flood; areas of 1% annual chance flood with f less than 1 foot or with drainage areas less than 1
		areas protected by levees from 1% annual chance flood.
	Areas determined	to be outside the 0.2% annual chance floodplain.
		od hazards are undetermined, but possible. RIER RESOURCES SYSTEM (CBRS) AREAS
		ROTECTED AREAS (OPAs)
CBRS areas a		ly located within or adjacent to Special Flood Hazard Areas. Iplain boundary
	— — Flood	lway boundary
••••••		D Boundary 5 and OPA boundary
~~ 513	Floor	dary dividing Special Flood Hazard Areas of different Base I Elevations, flood depths or flood velocities. Flood Elevation line and value; elevation in feet*
(EL 987) Base	Flood Elevation where uniform within zone; tion in feet*
* Referenced		can Vertical Datum of 1988 (NAVD 88)
(23)		sect line
97° 07' 30. 32° 22' 30.	3	raphic coordinates referenced to the North American m of 1983 (NAD 83)
⁴² 75 ^{000m}	N 1000 zone	-meter Universal Transverse Mercator grid ticks, 13
6000000	syste	-foot grid ticks: Colorado State Plane coordinate m, central zone (FIPSZONE 0502), pert Conformal Conic Projection
DX5510		h mark (see explanation in Notes to Users section of TRM panel)
● M1.5	River	Mile
	Refer t	MAP REPOSITORIES o Map Repositories list on Map Index
	Refer t EFF Fl	MAP REPOSITORIES o Map Repositories list on Map Index ECTIVE DATE OF COUNTYWIDE OOD INSURANCE RATE MAP MARCH 17, 1997
	Refer t EFF FI EFFECTIVE I BER 7, 2018 - to up ood Hazard Areas,	MAP REPOSITORIES o Map Repositories list on Map Index ECTIVE DATE OF COUNTYWIDE LOOD INSURANCE RATE MAP
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FINAL DRAINAGE REPORT CROSSROAD MIXED USE FILING NO. 1 - PROPOSED DRAINAGE MAP



FINAL DRAINAGE REPORT FOR AURA AT CROSSROADS - PROPOSED DRAINAGE MAP



STRUC	TURE TABLE							
STRUCTURE ID	DESCRIPTION							
A0	TYPE I MANHOLE							
A1	TYPE I MANHOLE							
A2	TYPE I MANHOLE							
A3	INLET TYPE R 10'							
A4	INLET TYPE R 5'							
A5	TYPE I MANHOLE							
A6	TYPE I MANHOLE							
A7	TYPE I MANHOLE							
A8	INLET TYPE R 15' MOD							
A9	INLET TYPE R 10'							
B1	INLET TYPE C							

STRUCTURE TABLE										
STRUCTURE ID	DESCRIPTION									
B2	INLET TYPE R 5'									
B3	TYPE II MANHOLE									
B4	INLET TYPE R 10'									
B5	TYPE I MANHOLE									
C1	TYPE I MANHOLE									
C2	TYPE I MANHOLE									
C3	INLET TYPE R 10'									
C4	INLET TYPE R 15'									
D1	INLET TYPE R 10'									

	PIPE TABLE												
NAME	UPSTREAM STRUCTURE	DOWNSTREAM STRUCTURE	SIZE	LENGTH	SLOPE	MATERIAL							
A-0	A0	A1	36"	64.26'	0.50%	RCP							
A-1	A1	A2	36"	182.49'	0.50%	RCP							
A-2	A3	A2	18"	36.82'	4.50%	RCP							
A-3	A2	A5	36"	331.29'	0.50%	RCP							
A-4	A4	A5	15"	102.94'	1.50%	RCP							
A-5	A5	A6	36"	64.06'	2.03%	RCP							
A-6	A6	A7	36"	286.28'	0.58%	RCP							
A-7	A7	A8	36"	130.14'	0.50%	RCP							
A-8	A9	A8	24"	125.80'	1.00%	RCP							
A-9	A8		48"	10.05'	0.50%	RCP							
B-1	B1		15"	35.69'	0.50%	RCP							
B-2	B2	B3	18"	109.40'	0.50%	RCP							
B-3	В3	B4	18"	107.86'	0.50%	RCP							
B-4	B4	B5	24"	110.33'	0.50%	RCP							
C-1		C1	36"	60.28'	2.00%	RCP							
C-2	C1	B5	42"	165.64'	1.30%	RCP							
C-3	B5	C2	48"	213.24'	0.60%	RCP							
C-4	C3	C2	18"	15.67'	5.00%	RCP							
C-5	C4	C2	30"	25.67'	5.00%	RCP							
C-6	C2		48"	16.52'	0.60%	RCP							

DESIG	N POINT SUM	MARY				
DESIGN POINT	Q5 (CFS)	Q100 (CFS)				
0	16.48	38.58				
1	4.61	9.36				
2	19.17	43.45				
3	0.88	1.90				
4	19.60	44.42				
5	19.55	45.20				
6	2.76	5.24				
7	30.16	65.43				
8	1.38	3.17				
9	2.06	4.57				
10	6.85	13.80				
11	35.00	60.50				
12	41.65	73.75				
13	44.47	79.25				
14	2.08	4.20				
15	0.47	1.27				
16	0.57	1.43				

r												
	DIRECT RUNOFF SUMMARY											
SUBBASIN	AREA (AC)	Q5 (CFS)	Q100 (CFS)									
X-1	0.42	0.58	1.50									
X-2	0.01	0.05	0.10									
X-3	0.08	0.26	0.50									
A-1	2.07	4.61	9.36									
A-2	0.43	0.88	1.90									
A-3	0.42	0.13	0.94									
A-4	0.76	2.76	5.24									
A-5	3.67	8.72	17.06									
B-1	0.75	1.38	3.17									
B-2	0.28	0.74	1.45									
B-3	1.91	4.89	9.52									
C-1	0.77	1.86	3.84									
C-2	0.44	1.39	2.64									
D-1	0.78	2.08	4.20									
Z-1	0.37	0.47 1.2										
Z-2	0.38	0.57	1.43									

PROJECT #: 200823 SHEET NUMBER HYDROLIC AND HYDRALIC CALCULATIONS

CROSSROADS MIXED USE FIL. NO.1 FOR UNDERGROUND DETENTION PRELIMINARY/FINAL DRAINAGE CALCULATIONS (Area Runoff Coefficient Summary)

			STREE	TS / COM	MERC.	MULTI	-FAMILY/	PARKS	OVERLAN	D / UNDE	WEIGHTED		
BASIN	BASIN TOTAL TOTAL AREA AREA AREA C ₅ C ₁₀₀					AREA (Acres)	C ₅	C ₁₀₀	AREA C ₅ C ₁₀₀			C ₅	C ₁₀₀
					PROPOS	ED BASINS							
A	57624	1.32	0.00	0.90	0.96	1.32	0.12	0.39	0.00	0.08	0.35	0.12	0.39
В	38411	0.88	0.00	0.90	0.96	0.88	0.12	0.39	0.00	0.08	0.35	0.12	0.39
С	10729	0.25	0.21	0.90	0.96	0.03	0.12	0.39	0.00	0.08	0.35	0.79	0.88
D	27815	0.64	0.46	0.90	0.96	0.18	0.12	0.39	0.00	0.08	0.35	0.68	0.80
E	8718	0.20	0.00	0.90	0.96	0.20	0.20 0.12 0.39			0.08	0.35	0.12	0.39

Calculated by: GT Date: 2/1/2023 Checked by: DLM

CROSSROADS MIXED USE FIL. NO.1 FOR UNDERGROUND DETENTION PRELIMINARY/FINAL DRAINAGE CALCULATIONS

(Area Drainage Summary)

From Area Ru	noff Coefficient S	lummary			OVER	LAND		STRE	ET / CH	ANNEL F	FLOW	Time of T	ravel (T _t)	INTENSITY #		TOTAL FLOWS	
BASIN	AREA TOTAL	C ₅	C ₁₀₀	C ₅	Length	Height	T _C	Length	Slope	Velocity	T _t	TOTAL	CHECK	I ₅	I ₁₀₀	Q5	Q ₁₀₀
	(Acres) From DCM Table 5-1				(ft)	(ft)	(min)	(ft)	(%)	(fps)	(min)	(min)	(min)	(in/hr)	(in/hr)	(c.f.s.)	(c.f.s.)
	Proposed Area Drainage Summary																
A	1.32	0.12	0.39	0.12	60	0.3	17.2	261	0.5%	0.5	8.8	26.0	11.8	3.9	6.5	0.6	3.4
В	0.88	0.12	0.39	0.12	60	0.3	17.2	134	0.5%	0.5	4.5	21.7	11.1	4.0	6.7	0.4	2.3
С	0.25	0.79	0.88	0.79	35	0.5	2.9	75	1.4%	2.4	0.5	5.0	10.6	5.2	8.7	1.0	1.9
D	0.64	0.68	0.80	0.68	25	0.5	3.0	266	1.5%	1.9	2.4	5.4	11.6	5.1	8.5	2.2	4.3
E	0.20	0.12	0.39	0.12	25	4	3.5	0	0.0%	0.0	0.0	5.0	10.1	5.2	8.7	0.1	0.7

Intensity equations assume a minimum travel time of 5 minutes.

Calculated by: GT Date: 2/1/2023 Checked by: DLM

MS CIVIL, INC. Proposed Drainage Calcs revised parking 12-1-23.xls

CROSSROADS MIXED USE FIL. NO.1 FOR UNDERGROUND DETENTION PRELIMINARY/FINAL DRAINAGE CALCULATIONS

	T KLEIMINAK I/FINAL DRAINAGE CALCULATIONS																
	(Basin Routing Summary) From Area Rumoff Coefficient Summary OVERLAND PIPE / CHANNEL FLOW Time of Travel (T,) INTENSITY* TOTAL FLOWS																
		OVERLAND			PIP	E / CHA	NNEL FLO	OW	Time of Travel (T_t)	Time of Travel (T_t) INTENSITY *		TOTAL FLOWS					
DESIGN POINT	CONTRIBUTING BASINS	CA5	CA100	C ₅	Length	Height	T _C	Length	Slope	Velocity	Tt	TOTAL	I5	I ₁₀₀	Q5	Q100	COMMENTS
					(ft)	(ft)	(min)	(ft)	(%)	(fps)	(min)	(min)	(in/hr)	(in/hr)	(c.f.s.)	(c.f.s.)	
	PROPOSED DRAINAGE BASIN ROUTING SUMMARY																
1	Α	0.16	0.52									11.8	3.9	6.5	1.2	4.7	Prop 2' x 3' Area Inlet
	Offsite DP16*	0.14	0.21														
		0.30	0.73		Tc for	A Used											
2	В	0.11	0.34									11.1	4.0	6.7	0.4	2.3	Prop 2' x 3' Area Inlet
	<u> </u>	0.11	0.34		Te for B	asin B used											
3	С	0.20	0.22									5.0	5.2	8.7	1.6	3.6	Proposed 10' CDOT Type R Sump Inlet
	Offsite DP15*	0.12	0.20														
		0.32	0.42		Te for B	asin C used											
4	D	0.43	0.51									5.4	5.1	8.5	2.2	4.3	Proposed 5' CDOT Type R Sump Inlet
		0.43	0.51		Tc for	D Used											
5	Е	0.02	0.08									5.0	5.2	8.7	0.1	0.7	Sheet flow offsite
		0.02	0.08		Tc for	E Used											

Intensity equations assume a minimum travel time of 5 minutes.

*FDR for AURA at Crossroads, prepared by HKS, dated April 4, 2022

**FDR for Crossroads Mixed Use Filing No.1, prepared by MS Civil Consultants, Inc., dated April 2022

GT Date: 2/1/2023 Checked by: DLM

CROSSROADS MIXED USE FIL. NO.1 FOR UNDERGROUND DETENTION PRELIMINARY/FINAL DRAINAGE CALCULATIONS

					Inter	ısity*	Fl	ow	PIPE SIZE
PIPE RUN	Contributing Pipes/Design Points	Equivalent CA 5	Equivalent CA 100	Maximum T _C	Ι,	I 100	Q 5	Q 100	
15**	PR12.5, PR13, PR14	10.52	12.24	7.5	4.6	7.7	48.0	93. 7	48" RCP
16**	DP12	2.08	2.26	5.0	5.2	8.7	10.8	19.6	24" RCP
17	PR15**, PR16**	12.60	14.50	8.3	4.4	7.4	55.6	107.4	48" RCP
19*	SEE FDR FOR AURA AT CROSSROADS	10.05	11.09	15.0	3.5	5.9	35.4	65.5	48" RCP
21*	SEE FDR FOR AURA AT CROSSROADS	0.48	0.58	9.0	4.3	7.2	2.1	4.2	30" RCP
22	PR17, PR21*	13.08	15.08	8.8	4.3	7.3	56.5	109.4	54" RCP
23.1	DP3	0.32	0.42	5.0	5.2	8.7	1.6	3.6	18" RCP
23.2	DP4, PR23.1	0.34	0.50	5.6	5.0	8.4	1.7	4.2	24" RCP
24	PR22, PR23.2	13.42	15.58	8.9	4.3	7.2	57.8	112.6	54" RCP
25	DP1	0.30	0.73	11.8	3.9	6.5	1.2	4.7	24" RCP
26	DP2	0.11	0.34	11.1	4.0	6.7	0.4	2.3	24" RCP
27	PR19*,PR25,PR26	10.45	12.16	15.0	3.5	5.9	36.8	71.9	48" RCP
20	POND OUTFALL	PER	MHFD	WKSHT			4.4	14.5	18" RCP
DR for AURA at Cros	ssroads, prepared by HKS, dated April 4, 2022				Са	lculated by:	GT		_

(Storm Sewer Routing Summary)

**FDR for Crossroads Mixed Use Filing No.1, prepared by MS Civil Consultants, Inc., dated April 2022 DP - Design Point FB- Flow By from D EX - Existing Design Point INT- Intercepted Flow

FB- Flow By from Design Point INT- Intercepted Flow from Design Point

Checked by: DLM

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.06 (July 2022)

Volume (ac-ft) 0.035 0.074 0.109 0.144 0.184 0.219 0.254 0.293 0.328 0.384 0.469 0.545 0.620 0.705 0.780 0.856 0.940 1.015 1.089 1.173 1.247 1.321 1.404 1.477 1.550 1.632 1.705 1.777 1.858 1.929 2.001 2.081 2.151 2.221 2.300 2.369 2.438 2.515 2.583 2.651 2.726 2.793 2.859 2.932 2.997 3.061 3.133 3.196 3.258 3.327 3.388 3.448 3.515 3.573 3.631 3.694 3.749 3.804 3.864 3.915 3.966 4.021

4.067 4.111 4.157 4.196 4.234 4.276 4.313 4.348 4.387 4.422 4.457

4.497 4.532 4.567

4.606 4.641 4.676 4.716

197,405 198,930

200,647

202,172 203,697

205,414

206,939 4.751 2/14/2023 3:47 PM

0.438 0.438 0.438

19,068 19,068 19,068

19,068 0.438 19,068 0.438

19,068 0.438 19,068 0.438

6.25 6.33 6.42

6.50

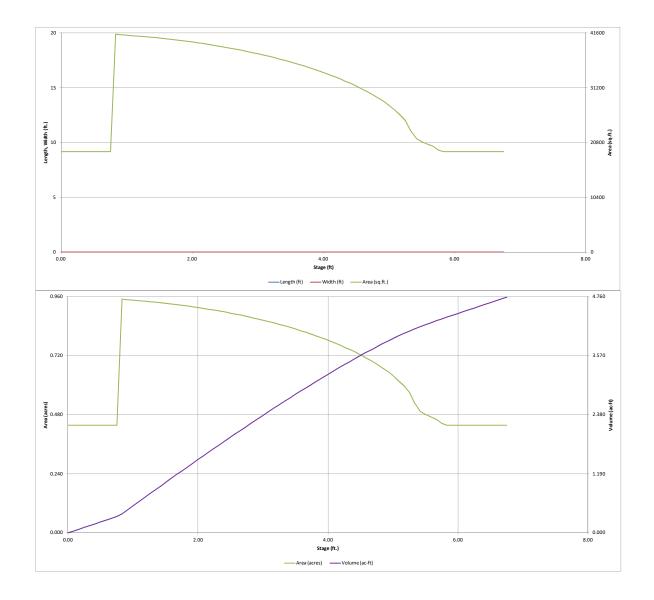
6.67

6.75

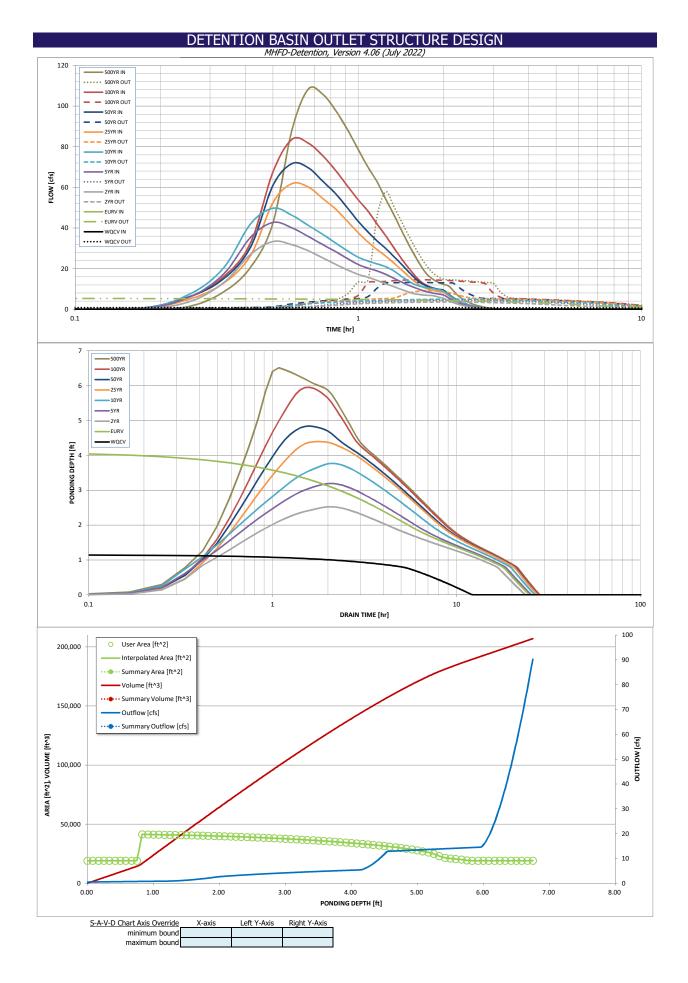
Project:	CROSSROAD	DS MIXED U	ISE											_
	POND 1 UND	DERGROUN	D DETENTION	N										_
	2 ONE 1		_											
		T												
±	= 1	100-YE	AB				1.							
PERMANENT ORIFI	1 AND 2	ORIFIC	E		Depth Increment =	0.50	ft Optional				Optional		T	Т
POOL Example Zone	Configurati	on (Retent	ion Pond)		Stage - Storage	Stage	Override	Length	Width	Area	Override Area (ft ²)	Area	Volume	
Watershed Information				6287.4	7 Media Surface	(ft) 	Stage (ft) 0.00	(ft) 	(ft) 	(ft²) 	19,068	(acre) 0.438	(ft 3)	t
Selected BMP Type =	SF	1		0207.4	/		0.08				19,068	0.438	1,525	Ť
Watershed Area =	32.20	acres					0.17				19,068	0.438	3,242	t
Watershed Length =	1,725	ft									19,068	0.438	4,767	t
Watershed Length to Centroid =	1,000	ft			Update e	either	the				19,068	0.438	6,292	t
Watershed Slope =	0.006	ft/ft			narrative			or			19,068	0.438	8,009	Ī
Watershed Imperviousness =	78.67%	percent						<u> </u>			19,068	0.438	9,534	
Percentage Hydrologic Soil Group A =	95.4%	percent			the calcu	lation	tor				19,068	0.438	11,059	+
Percentage Hydrologic Soil Group B =	4.6%	percent			consister	ncv.					19,068 19,068	0.438	12,776	┿
Percentage Hydrologic Soil Groups C/D = Target WQCV Drain Time =	12.0	percent nours					0.83	·			41,371	0.438	14,301 16,718	$\frac{1}{2}$
Location for 1-hr Rainfall Depths =		nours		:	Step 3 Provide Water Qu	ality Capture Vol	lume (WQCV)– T	he site will use an	Underground		41,255	0.947	20,436	t
After providing required inputs above inc		rainfall			Detention-Full Spectrum Detention existing CDOT ROW roadside di	tch and ultimately	into Sand Creek. 7	The UGD pond out	let structure will		41,182	0.945	23,733	t
depths, click 'Run CUHP' to generate rund	off hydrograph	is using		1	e designed to drain the water qua o approximately 90% of the pred	evelopment condit	ions. This outlet de	sign is very similar	r to a standard		41,104	0.944	27,025	I
the embedded Colorado Urban Hydro	graph Procedu	ure.	Optional Use	r Overrides	ull spectrum detention pond. The ISS on an annual aggregate remo	e Baysavers upstrea wal basis.	im of the UGD are	designed to remov	e 80% of the		41,017	0.942	30,720	
Water Quality Capture Volume (WQCV) =	0.687	acre-feet		acre-feet		ł					40,930	0.940	33,998	ļ
Excess Urban Runoff Volume (EURV) =	3.293	acre-feet	1.10	acre-feet			1.33				40,842	0.938	37,269	ł
2-yr Runoff Volume (P1 = 1.19 in.) = 5-yr Runoff Volume (P1 = 1.5 in.) =	2.407 3.122	acre-feet acre-feet	1.19	inches inches			1.42				40,744 40,640	0.935 0.933	40,940 44,196	t
10-yr Runoff Volume (P1 = 1.75 in.) =	3.696	acre-feet	1.75	inches			1.58				40,531	0.930	47,443	t
25-yr Runoff Volume (P1 = 2 in.) =	4.394	acre-feet	2.00	inches			1.67				40,415	0.928	51,085	t
50-yr Runoff Volume (P1 = 2.25 in.) =	5.058	acre-feet	2.25	inches			1.75				40,293	0.925	54,314	Ī
100-yr Runoff Volume (P1 = 2.52 in.) =	5.833	acre-feet	2.52	inches			1.83				40,166	0.922	57,532	I
500-yr Runoff Volume (P1 = 3.14 in.) =	7.551	acre-feet		inches			1.92				40,026	0.919	61,141	_
Approximate 2-yr Detention Volume =	2.178	acre-feet					2.00				39,892	0.916	64,337	ł
Approximate 5-yr Detention Volume =	2.835	acre-feet					2.08				39,744	0.912	67,523	╞
Approximate 10-yr Detention Volume = Approximate 25-yr Detention Volume =	3.393 4.014	acre-feet acre-feet					2.17				39,591 39,430	0.909	71,093 74,254	t
Approximate 50-yr Detention Volume =	4.379	acre-feet					2.33				39,260	0.901	77,401	t
Approximate 100-yr Detention Volume =	4.723	acre-feet					2.42				39,089	0.897	80,927	Ť
		-					2.50				38,907	0.893	84,047	Ī
Define Zones and Basin Geometry		-					2.58				38,718	0.889	87,152	
Zone 1 Volume (WQCV) =	0.687	acre-feet					2.67				38,517	0.884	90,627	∔
Zone 2 Volume (EURV - Zone 1) =	2.605	acre-feet acre-feet					2.75				38,315 38,103	0.880	93,701	ł
Zone 3 Volume (100-year - Zones 1 & 2) = Total Detention Basin Volume =	4.723	acre-feet					2.83				37,882	0.875	96,757 100,177	╉
Initial Surcharge Volume (ISV) =	N/A	ft ³					3.00				37,653	0.864	103,198	t
Initial Surcharge Depth (ISD) =	N/A	ft					3.08				37,416	0.859	106,201	Ť
Total Available Detention Depth $(H_{total}) =$	user	ft					3.17				37,169	0.853	109,557	I
Depth of Trickle Channel (H_{TC}) =	N/A	ft					3.25				36,912	0.847	112,520	
Slope of Trickle Channel $(S_{TC}) =$	N/A	ft/ft					3.33			-	36,646	0.841	115,463	+
Slopes of Main Basin Sides (S_{main}) = Basin Length-to-Width Ratio ($R_{L/W}$) =	user	H:V					3.42 3.50				36,369 36,081	0.835	118,748 121,646	╉
basin Lengur-to-Width Ratio (RL/W) =	usei						3.58				35,779	0.821	121,040	t
Initial Surcharge Area (A _{ISV}) =	user	ft ²					3.67				35,472	0.814	127,727	t
Surcharge Volume Length $(L_{ISV}) =$	user	ft					3.75				35,150	0.807	130,552	T
Surcharge Volume Width (W_{ISV}) =	user	ft					3.83				34,814	0.799	133,350	
Depth of Basin Floor $(H_{FLOOR}) =$	user	ft					3.92				34,466	0.791	136,468	ļ
Length of Basin Floor (L_{FLOOR}) = Width of Basin Floor (W_{FLOOR}) =	user	ft A					4.00				34,101	0.783	139,211	╀
Area of Basin Floor (M_{FLOOR}) =	user	ft ft ²					4.08 4.17				33,720 33,322	0.774 0.765	141,924 144,940	t
Volume of Basin Floor (V _{FLOOR}) =	user	ft ³					4.17				32,904	0.755	147,590	t
Depth of Main Basin (H _{MAIN}) =	user	ft					4.33				32,466	0.745	150,204	Ť
Length of Main Basin (L_{MAIN}) =	user	ft					4.42				32,005	0.735	153,106	Ī
Width of Main Basin (W_{MAIN}) =	user	ft					4.50				31,522	0.724	155,647	
Area of Main Basin $(A_{MAIN}) =$	user	ft ²					4.58				31,010	0.712	158,148	ļ
Volume of Main Basin (V _{MAIN}) =	user	ft ³					4.67				30,463	0.699	160,914	┿
Calculated Total Basin Volume (V_{total}) =	user	acre-feet					4.75 4.83				29,887 29,259	0.686	163,328 165,694	t
							4.92				28,588	0.656	168,297	ţ
							5.00 5.08				27,845 27,013	0.639	170,554 172,749	t
							5.17				26,058	0.598	175,137	ļ
							5.25 5.33				24,880 23,005	0.571 0.528	177,175 179,090	t
							5.42 5.50				21,507 20,969	0.494 0.481	181,093 182,792	t
							5.58				20,533	0.471	184,452	t
							5.67 5.75				20,080 19,385	0.461 0.445	186,280 187,858	ł
							5.83				19,068	0.438	189,396	ţ
							5.92 6.00				19,068 19,068	0.438	191,113 192,638	t
							6.08 6.17				19,068 19,068	0.438	194,163 195,880	Į
							6.25				19,068	0.438	195,880	ţ

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.06 (July 2022)



DETENTION BASIN OUTLET STRUCTURE DESIGN MHFD-Detention, Version 4.06 (July 2022) Project: CROSSROADS MIXED USE Basin ID: POND 1 UNDERGROUND DETENTION Estimated Estimated Stage (ft) Volume (ac-ft) Outlet Type EURV WQCV Zone 1 (WQCV) 1.16 0.687 Filtration Media Zone 2 (EURV) 4.13 2.605 Circular Orifice 100-YEAR ZONE 1 AND 2 Zone 3 (100-year) 6.69 1.430 Weir&Pipe (Restrict) PERM. POOL Example Zone Configuration (Retention Pond) Total (all zones) 4.723 User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP) Calculated Parameters for Underdrain ft (distance below the filtration media surface) Underdrain Orifice Area ft² Underdrain Orifice Invert Depth : 0.75 0.1 Underdrain Orifice Centroid Underdrain Orifice Diameter = feet 4.93 inches 0.21 User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP) Calculated Parameters for Plate Centroid of Lowest Orifice = N/A ft (relative to basin bottom at Stage = 0 ft) WQ Orifice Area per Row N/A ft² Depth at top of Zone using Orifice Plate ft (relative to basin bottom at Stage = 0 ft) Elliptical Half-Width N/A feet N/A Orifice Plate: Orifice Vertical Spacing N/A inches Elliptical Slot Centroid N/A feet ft² Orifice Plate: Orifice Area per Row : N/A sa. inches Elliptical Slot Area N/A User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest) Row 1 (optional) Row 2 (optional) Row 3 (optional) Row 4 (optional) Row 5 (optional) Row 6 (optional) Row 7 (optional) Row 8 (optional) Stage of Orifice Centroid (ft N/A N/A N/A N/A N/A N/A N/A N/A Orifice Area (sq. inches) N/A N/A N/A N/A N/A N/A N/A N/A Row 9 (optional) Row 10 (optional) Row 11 (optional) Row 12 (optional) Row 13 (optional) Row 14 (optional) Row 15 (optional) Row 16 (optional) Stage of Orifice Centroid (ft N/A N/A N/A N/A N/A N/A N/A N/A Orifice Area (sg. inches N/A N/A N/A N/A N/A N/A N/A N/A User Input: Vertical Orifice (Circular or Rectangular) Calculated Parameters for Vertical Ori Zone 2 Circular Not Selected Zone 2 Circular Not Selected Invert of Vertical Orifice ft (relative to basin bottom at Stage = 0 ft) Vertical Orifice Area 1.17 N/A 0.52 N/A Depth at top of Zone using Vertical Orifice : ft (relative to basin bottom at Stage = 0 ft) Vertical Orifice Centroid 4.13 N/A 0.41 N/A Vertical Orifice Diameter 9.76 N/A inches User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir and No Outlet Pipe) Calculated Parameters for Overflow W Zone 3 Weir Not Selected Zone 3 Weir Not Selected ft (relati<mark>5.5ftsionttSht SF05.ft)Revise of C</mark>rate Upper Edge, H_t Overflow Weir Front Edge Height, Ho 4.14 N/A 4.14 N/A low Weir Slope Length Overflow Weir Front Edge Length 5.70 N/A to remove discrepanciesArea / 100-yr Orifice Area 2.90 N/A feet Overflow Weir Grate Slope 0.00 N/A H:V 9.65 N/A Horiz. Length of Weir Sides 2.90 N/A feet Overflow Grate Open Area w/o Debris 11.50 N/A Overflow Grate Type 8in on Sht ST05, Reviserto Open Area w/ Debris = 5.75 Type C Grate N/A N/A Debris Clogging % = 50% N/A remove discrepancies. User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice) Calculated Parameters for Outlet Pipe w/ Flow Restriction Pla Zone 3 Restrictor Not Selected Zone 3 Restrictor Not Selected Depth to Invert of Outlet Pipe Outlet Orifice Area 1.00 N/A ft (distance below basin bottom at Stage = 0 ft) 1.19 N/A 18.00 Outlet Orifice Centroid = 0.54 Outlet Pipe Diameter N/A inches N/A Restrictor Plate Height Above Pipe Invert = Half-Cen Is this shown on plans somewhere? I don't see it in plan or detail. 11.50 inches Does the spreadsheet allow you to input "N/A" for spillway values? User Input: Emergency Spillway (Rectangular or Trapezoidal) alculated Parameters for Spillway Spillway Design Flow Depth= ft (relative to basin bottom at Stage = 0 ft) Spillway Invert Stage= 5.96 0.84 feet Spillway Crest Length 33.00 feet The release is greater than the Fil 1 Spillway End Slopes H:V 4.00 Freeboard above Max Water Surface = 1.00 feet FDR analysis. Revise to match or provide an explanation/justification Routed Hydrograph Results The user can override the defau off volume i Al similar to what was given on the Fil 1 Design Storm Return Period WOCV FURV 5 Year One-Hour Rainfall Depth (in) N/A N/A 1.50 report. 3.293 3.122 CUHP Runoff Volume (acre-ft) 0.687 Inflow Hydrograph Volume (acre-ft) N/A N/A 3.12 0.5 9.2 14.8 CUHP Predevelopment Peak Q (cfs) N/A N/A 0.3 OPTIONAL Override Predevelopment Peak Q (cfs) N/A N/A Predevelopment Unit Peak Flow, q (cfs/acre) N/A N/A 0.01 0.01 0.29 0.46 0.16 Peak Inflow Q (cfs) N/A N/A 33.3 42.7 71.7 83.5 49. 61.8 Peak Outflow Q (cfs) 0.8 3.6 4.4 5.0 13.2 14.5 5.4 9.7 Ratio Peak Outflow to Predevelopment O N/A N/A N/A 13.1 1.0 1 8 Structure Controlling Flow Filtration Media Outlet Plate Vertical Orifice rflow Weir Outlet Plate tical Orifice Vertical Orifice 1 Vertical Orifice Max Velocity through Grate 1 (fps) N/A N/A N/A 0.7 N/A N/A 0.3 0.6 N/A 22 N/A 24 N/A 24 Max Velocity through Grate 2 (fps) N/A N/A N/A N/A N/A 23 23 25 24 Time to Drain 97% of Inflow Volume (hours) 12 27 Time to Drain 99% of Inflow Volume (hours) 12 24 23 25 26 27 27 Maximum Ponding Depth (ft) 2.52 3.19 5.95 4.13 3.77 4.39 4.84 1.16 Area at Maximum Ponding Depth (acres) 0.89 0.85 0.94 0.81 0.74 0.44 0.67 0.77 Maximum Volume Stored (acre-ft) 0.696 3 297 1 947 3.00! 3 493 3.804 4.400



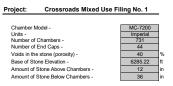
DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename:

Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

								in a separate pro	1	
	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.39	0.04	1.25
	0:15:00	0.00	0.00	3.46	5.62	6.96	4.67	5.89	5.69	8.36
	0:20:00	0.00	0.00	12.83	16.99	20.01	12.66	14.80	15.76	20.62
	0:25:00	0.00	0.00	26.94	35.34	41.95	26.44	30.57	32.65	42.44
	0:30:00	0.00	0.00	33.30	42.69	49.70	52.46	60.93	67.51	88.01
	0:35:00	0.00	0.00	31.75	40.04	46.24	61.83	71.65	83.54	108.32
	0:40:00	0.00	0.00	28.76	35.78	41.26	60.15	69.62	81.73	105.76
	0:45:00	0.00	0.00	25.24	31.76	36.81	54.48	62.96	75.48	97.70
	0:50:00	0.00	0.00	22.08	28.32	32.53	49.25	56.81	68.18	88.41
	0:55:00 1:00:00	0.00	0.00	19.37	24.91 22.01	28.73 25.61	43.27 37.64	49.85 43.31	60.62 53.86	78.63 69.88
	1:05:00	0.00	0.00	17.17 15.76	22.01	23.73	37.04	38.03	48.24	62.68
	1:10:00	0.00	0.00	14.15	18.82	22.31	29.32	33.64	41.85	54.29
	1:15:00	0.00	0.00	12.58	17.18	20.93	26.15	29.93	36.21	46.84
	1:20:00	0.00	0.00	11.18	15.31	18.94	22.83	26.07	30.49	39.31
	1:25:00	0.00	0.00	9.82	13.47	16.35	19.64	22.38	25.23	32.44
	1:30:00	0.00	0.00	8.59	11.88	14.02	16.49	18.74	20.67	26.49
	1:35:00	0.00	0.00	7.63	10.64	12.22	13.63	15.45	16.69	21.29
	1:40:00	0.00	0.00	7.11	9.47	11.22	11.37	12.85	13.51	17.17
	1:45:00	0.00	0.00	6.88	8.60	10.60	10.09	11.39	11.68	14.80
	1:50:00	0.00	0.00	6.73	7.98	10.16	9.28	10.46	10.53	13.28
	1:55:00	0.00	0.00	6.06	7.51	9.68	8.74	9.85	9.74	12.24
	2:00:00	0.00	0.00	5.38	7.00	8.94	8.35	9.41	9.17	11.49
	2:05:00	0.00	0.00	4.29	5.61	7.16	6.74	7.58	7.28	9.11
	2:10:00	0.00	0.00	3.29	4.28	5.47	5.12	5.76	5.45	6.80
	2:15:00	0.00	0.00	2.52	3.28	4.17	3.90	4.38	4.10	5.11
	2:20:00 2:25:00	0.00	0.00	1.92 1.45	2.49 1.87	3.15 2.35	2.95 2.21	3.32 2.49	3.11 2.35	3.88 2.92
	2:30:00	0.00	0.00	1.43	1.37	1.74	1.63	1.84	1.75	2.32
	2:35:00	0.00	0.00	0.79	0.99	1.74	1.05	1.34	1.75	1.60
	2:40:00	0.00	0.00	0.57	0.72	0.95	0.90	1.01	0.96	1.20
	2:45:00	0.00	0.00	0.39	0.50	0.66	0.64	0.72	0.69	0.85
	2:50:00	0.00	0.00	0.24	0.33	0.43	0.43	0.48	0.46	0.57
	2:55:00	0.00	0.00	0.13	0.20	0.25	0.26	0.29	0.27	0.34
	3:00:00	0.00	0.00	0.06	0.10	0.12	0.13	0.14	0.14	0.17
	3:05:00	0.00	0.00	0.02	0.03	0.04	0.04	0.05	0.04	0.05
	3:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:30:00 3:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:15:00 4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:40:00 4:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:05:00 5:10:00	0.00 0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:30:00 5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:55:00 6:00:00	0.00 0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0.00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00



Area of system -



✓ Include Perimeter Stone in Calculations
Click for Stage Area Data
Click to Invert Stage Area Data
Click Here for Metric

36 47670 sf Min. Area - 45260 sf min. area

40 6285.22 in

StormTe	ch MC-7200 (Cumulative S	torage Vo	lumes					
Height of System	Incremental Single Chamber	Incremental Single End Cap	Incremental Chambers	Incremental End Cap	Incremental Stone	Incremental Ch, EC and Stone	Cumulative System	Elevation	
(inches) 108	(cubic feet) 0.00	(cubic feet) 0.00	(cubic feet) 0.00	(cubic feet) 0.00	(cubic feet) 1589.00	(feet) 1589.00	(cubic feet) 249806.58	(feet) 6294.22	
107	0.00	0.00	0.00	0.00	1589.00	1589.00	248217.58	6294.14	
106 105	0.00	0.00	0.00	0.00	1589.00 1589.00	1589.00 1589.00	246628.58 245039.58	6294.05 6293.97	
104 103	0.00	0.00	0.00	0.00	1589.00 1589.00	1589.00 1589.00	243450.58 241861.58	6293.89 6293.80	
102	0.00	0.00	0.00	0.00	1589.00	1589.00	240272.58	6293.72	
101 100	0.00	0.00	0.00	0.00	1589.00 1589.00	1589.00 1589.00	238683.58 237094.58	6293.64 6293.55	100-yr
99 98	0.00	0.00	0.00	0.00	1589.00 1589.00	1589.00 1589.00	235505.58 233916.58	6293.47 6293.39	
97	0.00	0.00	0.00	0.00	1589.00	1589.00	232327.58	6293.30	191,664 cu ft
96 95	0.06 0.19	0.01 0.03	43.40 139.02	0.57 1.49	1571.41 1532.79	1615.39 1673.31	230738.58 229123.20	6293.22 6293.14	
94 93	0.28	0.05	201.16 261.15	2.28 2.90	1507.63 1483.38	1711.06 1747.43	227449.89 225738.83	6293.05 6292.97	
92	0.46	0.08	335.09	3.66	1453.50	1792.25	223991.40	6292.89	
91 90	0.74 1.10	0.11 0.13	542.14 801.45	4.63 5.83	1370.29 1266.09	1917.06 2073.36	222199.15 220282.09	6292.80 6292.72	
89 88	1.32 1.50	0.16 0.19	963.81 1095.21	7.08 8.30	1200.64 1147.60	2171.54 2251.11	218208.72 216037.19	6292.64 6292.55	
87	1.65	0.22	1209.43	9.62	1101.38	2320.43	213786.08	6292.47	
86 85	1.79 1.92	0.25 0.28	1311.39 1403.27	10.87 12.11	1060.10 1022.85	2382.35 2438.23	211465.65 209083.30	6292.39 6292.30	
84 83	2.04 2.15	0.30	1489.37 1568.23	13.28 14.41	987.94 955.94	2490.59 2538.59	206645.07 204154.48	6292.22 6292.14	
82	2.25	0.35	1643.07	15.60	925.53	2584.20	201615.90	6292.05	
81 80	2.34 2.43	0.38 0.41	1712.84 1778.85	16.88 18.00	897.11 870.26	2626.83 2667.11	199031.70 196404.86	6291.97 6291.89	
79 78	2.52 2.60	0.44 0.47	1841.43 1901.02	19.40 20.63	844.67 820.34	2705.50 2741.99	193737.75 191032.25	6291.80 6291.72	
77	2.68	0.50	1957.92	21.79	797.12	2776.83	188290.27	6291.64	EURV
76 75	2.75 2.82	0.52 0.54	2012.13 2063.93	22.91 23.96	774.98 753.84	2810.02 2841.73	185513.44 182703.42	6291.55 6291.47	143,617 cu ft
74 73	2.89 2.96	0.57	2113.62 2161.10	24.94 25.89	733.58 714.20	2872.14 2901.20	179861.68 176989.55	6291.39 6291.30	
72	3.02	0.61	2206.72	26.84	695.57	2929.14	174088.35	6291.22	
71 70	3.08 3.14	0.63 0.64	2250.48 2292.62	27.81 28.30	677.68 660.63	2955.98 2981.55	171159.21 168203.24	6291.14 6291.05	
69 68	3.19 3.25	0.68 0.70	2333.18 2372.11	29.80 30.79	643.81 627.84	3006.79 3030.74	165221.69 162214.89	6290.97 6290.89	
67	3.30	0.72	2409.61	31.79	612.44	3053.84	159184.15	6290.80	5-yr
66 65	3.35 3.39	0.74	2445.65 2480.36	32.72 33.64	597.65 583.40	3076.02 3097.40	156130.32 153054.30	6290.72 6290.64	110 204 8
64 63	3.44 3.48	0.79	2513.80 2545.99	34.56 35.32	569.65 556.48	3118.02 3137.78	149956.90 146838.88	6290.55 6290.47	110,294 cu ft
62 61	3.53 3.57	0.82	2577.04 2606.87	36.08 36.89	543.75 531.49	3156.87 3175.26	143701.10 140544.23	6290.39 6290.30	
60	3.61	0.85	2635.68	37.46	519.75	3192.88	137368.97	6290.22	
59 58	3.64 3.68	0.86 0.89	2663.38 2690.04	37.82 39.14	508.52 497.33	3209.72 3226.50	134176.09 130966.36	6290.14 6290.05	
57 56	3.71 3.75	0.90	2715.66 2740.29	39.79 40.36	486.82 476.74	3242.27 3257.39	127739.86 124497.59	6289.97 6289.89	
55 54	3.78 3.81	0.92	2763.91 2786.61	40.47 41.51	467.25 457.75	3271.63 3285.87	121240.20 117968.57	6289.80 6289.72	
53	3.84	0.96	2808.28	42.08	448.86	3299.21	114682.70	6289.64	
52 51	3.87 3.90	0.97 0.98	2829.09 2849.00	42.62 43.18	440.32 432.13	3312.03 3324.31	111383.49 108071.46	6289.55 6289.47	
50 49	3.92 3.95	0.97 1.00	2868.04 2886.19	42.73 44.14	424.69 416.87	3335.46 3347.20	104747.15 101411.69	6289.39 6289.30	
48	3.97	1.01	2903.49	44.49	409.81	3357.79	98064.49	6289.22 6289.14	
46	3.99 4.02	1.02 1.03	2920.00 2935.64	44.90 45.33	403.04 396.61	3367.94 3377.59	94706.70 91338.76	6289.05	
45 44	4.04 4.06	1.04 1.05	2950.47 2964.52	45.70 46.04	390.53 384.78	3386.70 3395.33	87961.18 84574.47	6288.97 6288.89	
43 42	4.07 4.09	1.05 1.05	2977.77 2990.16	46.38 46.22	379.34 374.45	3403.49 3410.83	81179.14 77775.65	6288.80 6288.72	WOCV
41 40	4.11	1.06	3001.99	46.49	369.61	3418.09	74364.83	6288.64 6288.55	WQCV
39	4.14	1.08 1.08	3023.81	47.64	364.77 360.42	3431.87	67521.39	6288.47	30,318 cu ft
38 37	4.15 4.17	1.09 1.11	3033.63 3049.01	47.88 48.68	356.40 349.92	3437.90 3447.62	64089.52 60651.62	6288.39 6288.30	R
36	0.00	0.00	0.00	0.00	1589.00 1589.00	1589.00	57204.00 55615.00	6288.22	
35 34	0.00	0.00	0.00	0.00	1589.00	1589.00	54026.00	6288.14 6288.05	·
33 32	0.00	0.00	0.00	0.00	1589.00 1589.00	1589.00 1589.00	52437.00 50848.00	6287.97 6287.89	
31 30	0.00	0.00	0.00	0.00	1589.00 1589.00	1589.00 1589.00	49259.00 47670.00	6287.80 6287.72	·
29	0.00	0.00	0.00	0.00	1589.00	1589.00	46081.00	6287.64	<u> </u>
28 27	0.00	0.00	0.00	0.00	1589.00 1589.00	1589.00 1589.00	44492.00 42903.00	6287.55 6287.47	
26 25	0.00	0.00	0.00	0.00	1589.00 1589.00	1589.00 1589.00	41314.00 39725.00	6287.39 6287.30	
24	0.00	0.00	0.00	0.00	1589.00	1589.00	38136.00	6287.22	
23 22	0.00	0.00	0.00	0.00	1589.00 1589.00	1589.00 1589.00	36547.00 34958.00	6287.14 6287.05	
21 20	0.00	0.00	0.00	0.00	1589.00 1589.00	1589.00 1589.00	33369.00 31780.00	6286.97 6286.89	
19	0.00	0.00	0.00	0.00	1589.00	1589.00	30191.00	6286.80	
18 17	0.00	0.00	0.00	0.00	1589.00 1589.00	1589.00 1589.00	28602.00 27013.00	6286.72 6286.64	
16 15	0.00	0.00	0.00	0.00	1589.00 1589.00	1589.00 1589.00	25424.00 23835.00	6286.55 6286.47	
14 13	0.00	0.00	0.00	0.00	1589.00 1589.00	1589.00 1589.00	22246.00 20657.00	6286.39 6286.30	
12	0.00	0.00	0.00	0.00	1589.00	1589.00	19068.00	6286.22	
11 10	0.00	0.00	0.00	0.00	1589.00 1589.00	1589.00 1589.00	17479.00 15890.00	6286.14 6286.05	
9 8	0.00	0.00	0.00	0.00	1589.00 1589.00	1589.00 1589.00	14301.00 12712.00	6285.97 6285.89	
7	0.00	0.00	0.00	0.00	1589.00	1589.00	11123.00	6285.80	
6 5	0.00	0.00	0.00	0.00	1589.00 1589.00	1589.00 1589.00	9534.00 7945.00	6285.72 6285.64	
4 3	0.00	0.00	0.00	0.00	1589.00 1589.00	1589.00 1589.00	6356.00 4767.00	6285.55 6285.47	
2	0.00	0.00	0.00	0.00	1589.00 1589.00	1589.00 1589.00	3178.00 1589.00	6285.39 6285.30	
	0.00	0.00	0.00	0.00		1000.00	1000.00	0200.00	

206904cf above elevation 6287.47

Provide calcs that show that the 294.38ft (196.62 + 97.75) of isolator rows provided meets this calculated WQCV.

Also look at providing the UD-BMP spreadsheet that shows the origin of how the WQCV is calculated (ie: what inputs were used for impervious % and soil types).

Version 4.06 Released August 2018

INLET MANAGEMENT

Worksheet Protected

INLET NAME	DP3	DP4
Site Type (Urban or Rural)	URBAN	URBAN
Inlet Application (Street or Area)	STREET	STREET
Hydraulic Condition	In Sump	In Sump
Inlet Type	CDOT Type R Curb Opening	CDOT Type R Curb Opening

USER-DEFINED INPUT

User-Defined Design Flows		
Minor Q _{Known} (cfs)	1.6	2.2
Major Q _{Known} (cfs)	3.5	4.3

Bypass (Carry-Over) Flow from Upstream

Receive Bypass Flow from:	No Bypass Flow Received	No Bypass Flow Received
Minor Bypass Flow Received, Q _b (cfs)	0.0	0.0
Major Bypass Flow Received, Q _b (cfs)	0.0	0.0

Watershed Characteristics

Subcatchment Area (acres)	
Percent Impervious	
NRCS Soil Type	

Watershed Profile

Overland Slope (ft/ft)	
Overland Length (ft)	
Channel Slope (ft/ft)	
Channel Length (ft)	

Minor Storm Rainfall Input

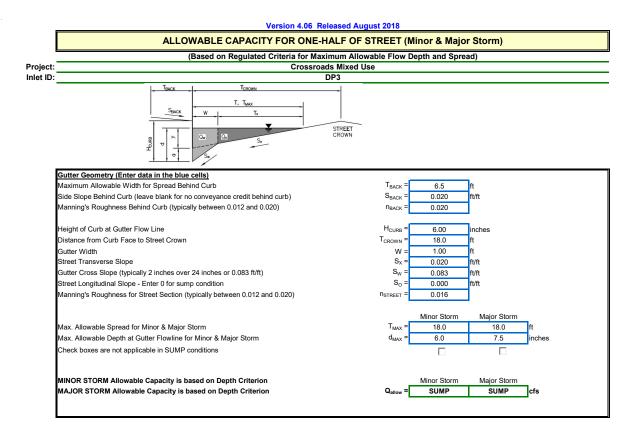
Design Storm Return Period, T _r (years)	
One-Hour Precipitation, P ₁ (inches)	

Major Storm Rainfall Input

Design Storm Return Period, T _r (years)	
One-Hour Precipitation, P ₁ (inches)	

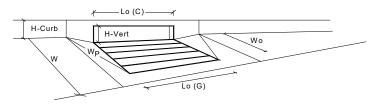
CALCULATED OUTPUT

Minor Total Design Peak Flow, Q (cfs)	1.6	2.2
Major Total Design Peak Flow, Q (cfs)	3.5	4.3
Minor Flow Bypassed Downstream, Q _b (cfs)	N/A	N/A
Major Flow Bypassed Downstream, Q _b (cfs)	N/A	N/A

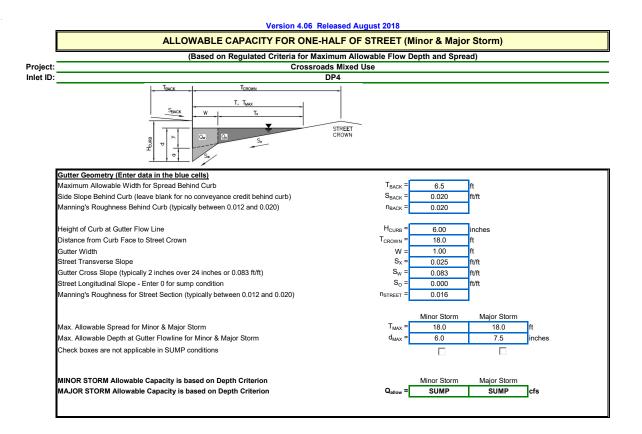


INLET IN A SUMP OR SAG LOCATION

Version 4.06 Released August 2018

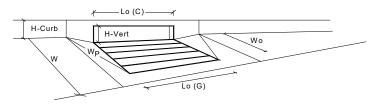


Design Information (Input) CDOT Type R Curb Opening		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R Curb Opening		
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	5.1	5.1	inches
Grate Information		MINOR	MAJOR	Override Depths
ength of a Unit Grate	L _o (G) =	N/A	N/A	feet
Width of a Unit Grate	W _o =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	C _f (G) =	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C _w (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	C _o (G) =	N/A	N/A	
Curb Opening Information		MINOR	MAJOR	-4
Length of a Unit Curb Opening	L _o (C) =	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H _{throat} =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W _p =	1.00	1.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	C _f (C) =	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	C _w (C) =	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	C _o (C) =	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d _{Curb} =	0.34	0.34	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	0.65	0.65	
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	1.00	1.00	
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A]
		MINOR	MAJOR	
Total Inlet Interception Capacity (assumes clogged condition)	Q _a =	4.4	4.4	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	1.6	3.5	cfs



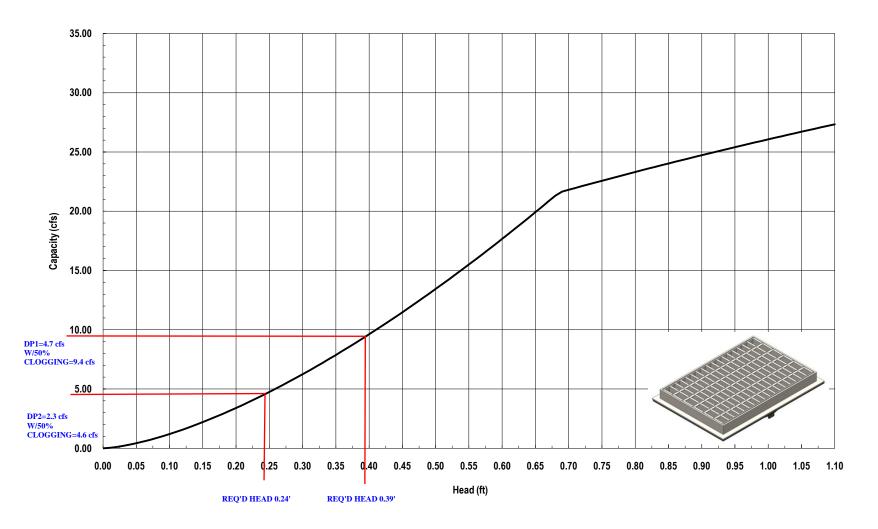
INLET IN A SUMP OR SAG LOCATION

Version 4.06 Released August 2018



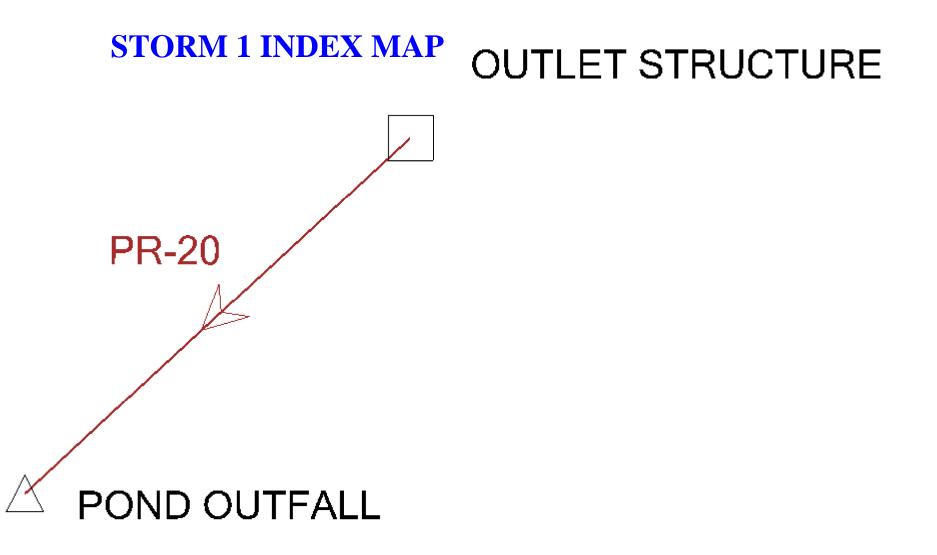
Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	6.0	6.1	inches
Grate Information		MINOR	MAJOR	Override Depths
Length of a Unit Grate	L _o (G) =	N/A	N/A	feet
Width of a Unit Grate	W _o =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	C _f (G) =	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C _w (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	C _o (G) =	N/A	N/A	
Curb Opening Information		MINOR	MAJOR	
Length of a Unit Curb Opening	L ₀ (C) =	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H _{throat} =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W _p =	1.00	1.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	C _f (C) =	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	C _w (C) =	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	C _o (C) =	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d _{Curb} =	0.42	0.43	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	0.77	0.78	
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	1.00	1.00	
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A]
	_	MINOR	MAJOR	_
Total Inlet Interception Capacity (assumes clogged condition)	Q _a =	5.9	6.1	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	2.2	4.3	cfs

Nyloplast 2' x 3' Steel Bar / MAG Grate Inlet Capacity Chart





3130 Verona Avenue • Buford, GA 30518 (866) 888-8479 / (770) 932-2443 • Fax: (770) 932-2490 © Nyloplast Inlet Capacity Charts June 2012

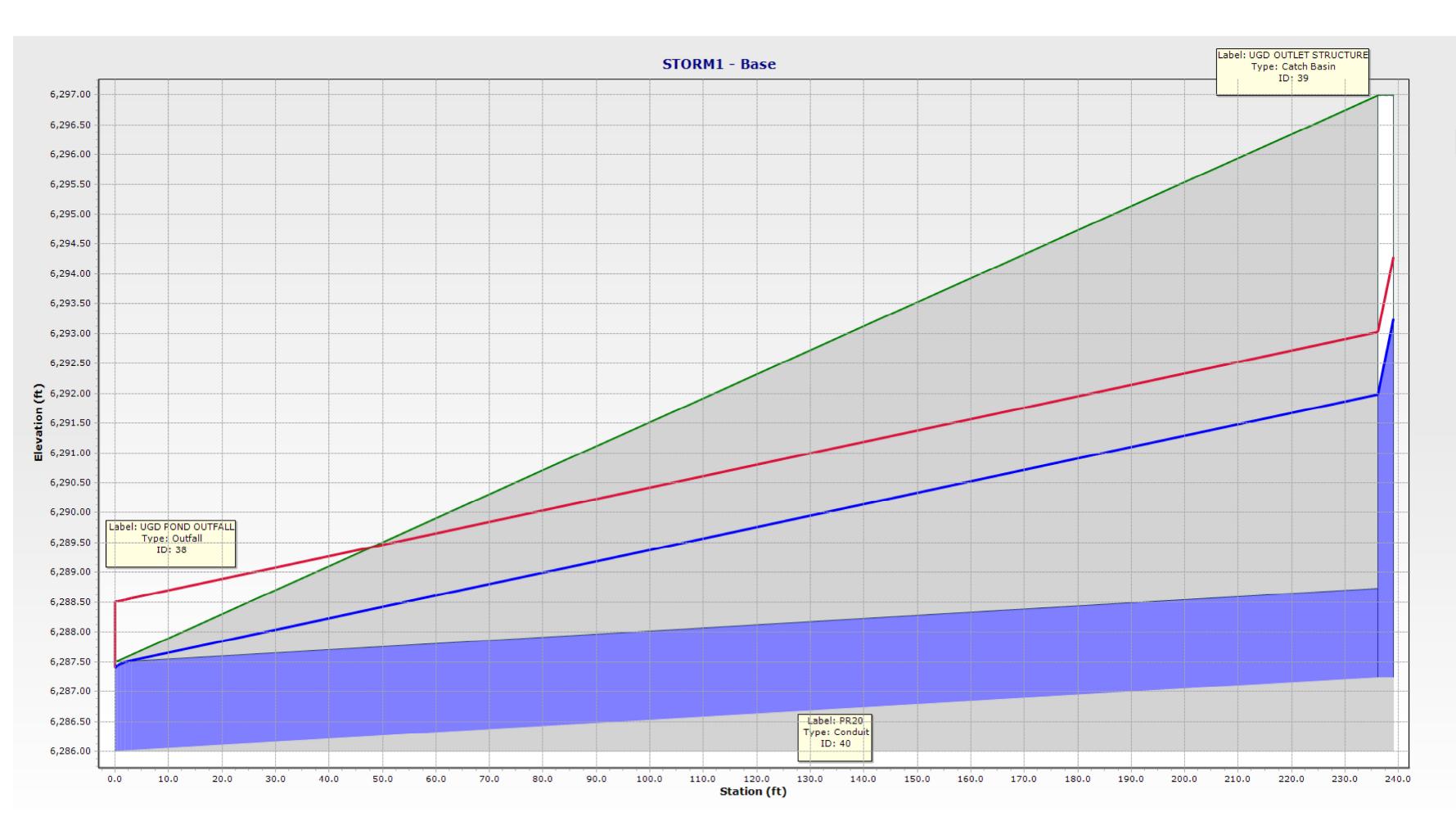


Label	ID	Upstream Structure	Flow (cfs)	Flow / Capacity (Design) (%)	Length (Unified) (ft)	Velocity (ft/s)	Depth (Normal) (ft)	Depth (Critical) (ft)
PR-20	40	OUTLET STRUCTURE	14.50	129.8	112.2	8.21	(N/A)	1.39
Energy Grade Line (In) (ft)	Energy Grade Line (Out) (ft)	Hydraulic Grade Line (In) (ft)	Hydraulic Grade Line (Out) (ft)	Headloss (ft)	Upstream Structure Hydraulic Grade Line (In) (ft)	Upstream Structure Velocity (In- Governing) (ft/s)	Upstream Structure Headloss Coefficient	Upstream Structure Headloss (ft)
6,290.64	6,288.51	6,289.59	6,287.39	2.20	6,291.16	8.21	1.500	1.57
Elevation Ground (Start) (ft)	Elevation Ground (Stop) (ft)	Invert (Start) (ft)	Invert (Stop) (ft)	Conduit Description	Manning's n	Friction Slope (ft/ft)	Slope (Calculated) (ft/ft)	
6,287.50	6,293.77	6,286.00	6,287.27	Circle - 18.0 in	0.013	0.019	-0.011	

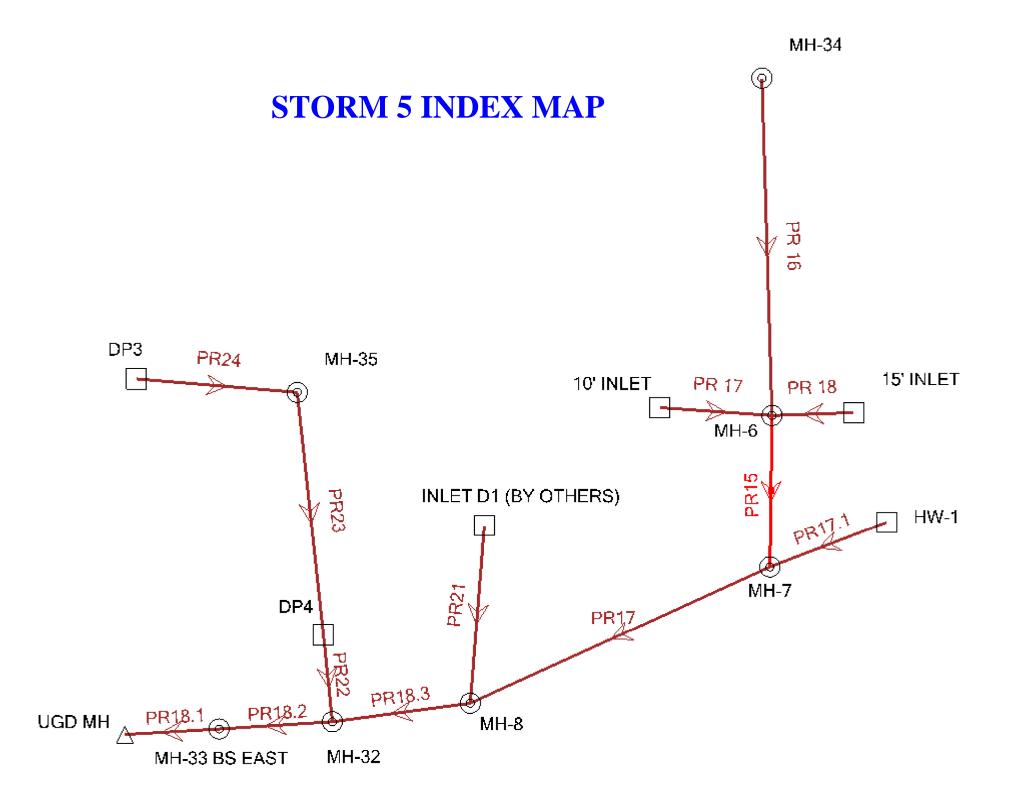
Conduit FlexTable: STRM1 100 YR

Storm 1-100YR.stsw 3/2/2023

Bentley Systems, Inc. Haestad Methods Solution Center 76 Watertown Road, Suite 2D Thomaston, CT 06787 USA +1-203-755-1666 StormCAD [10.03.04.53] Page 1 of 1



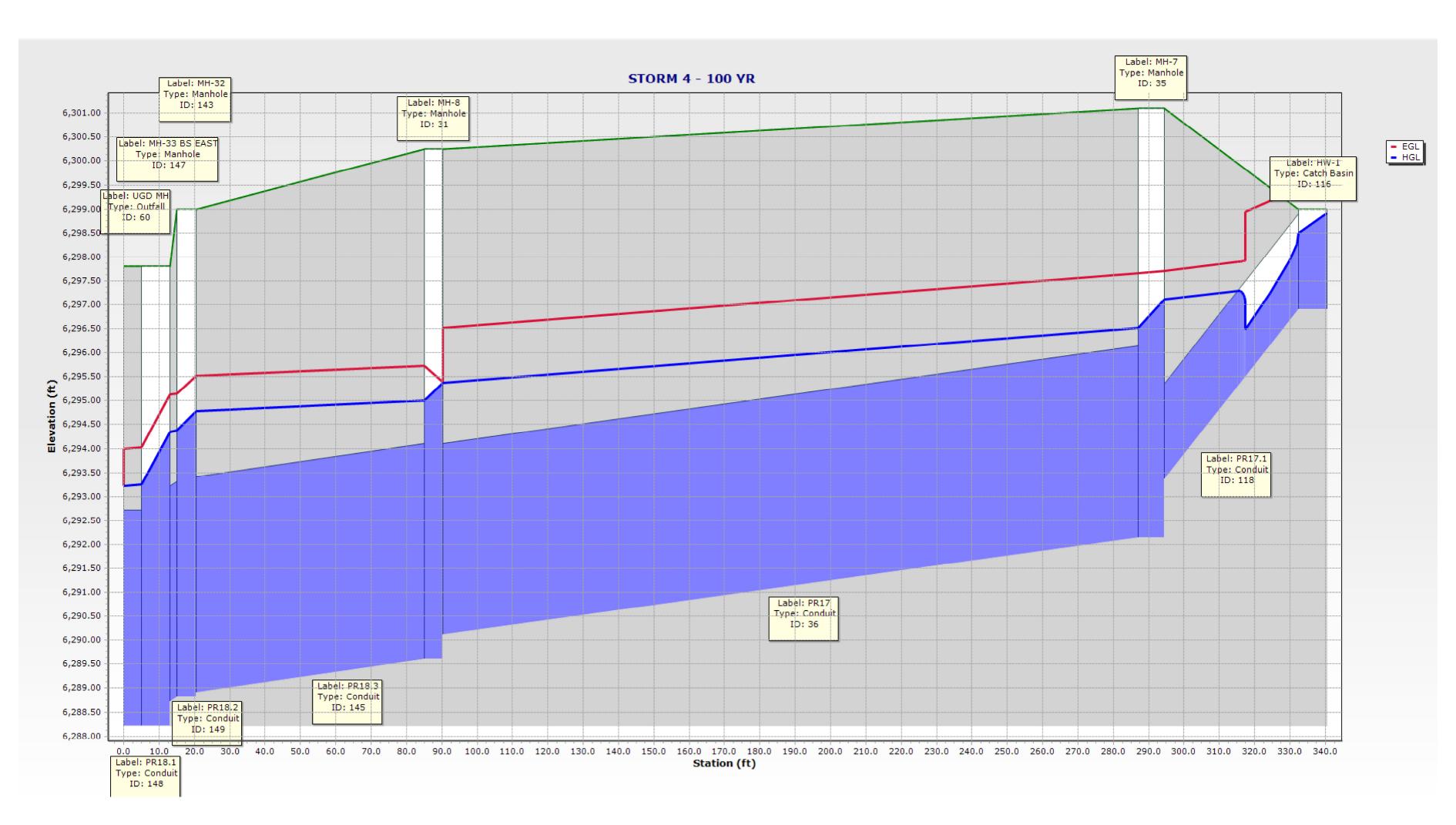


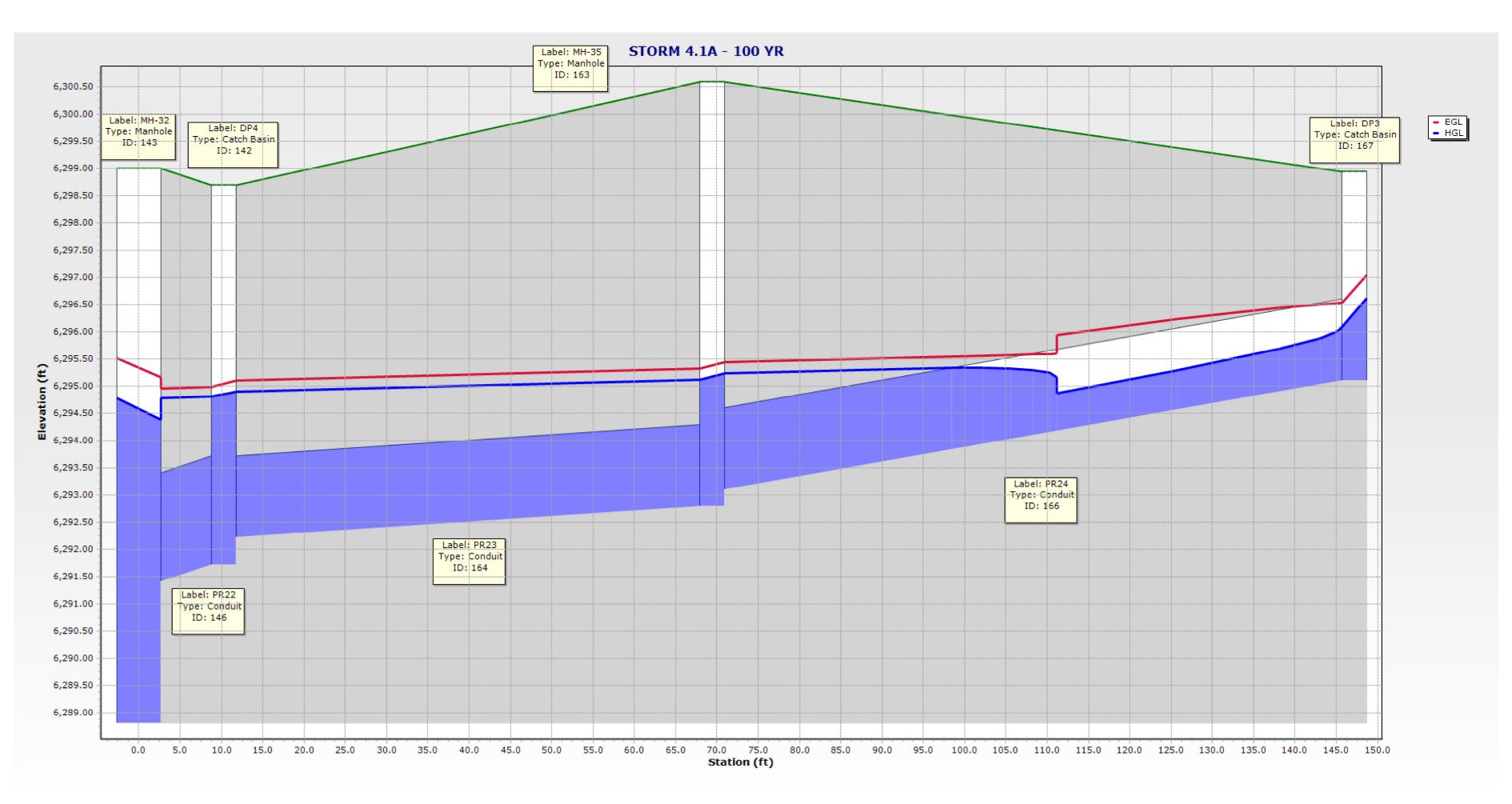


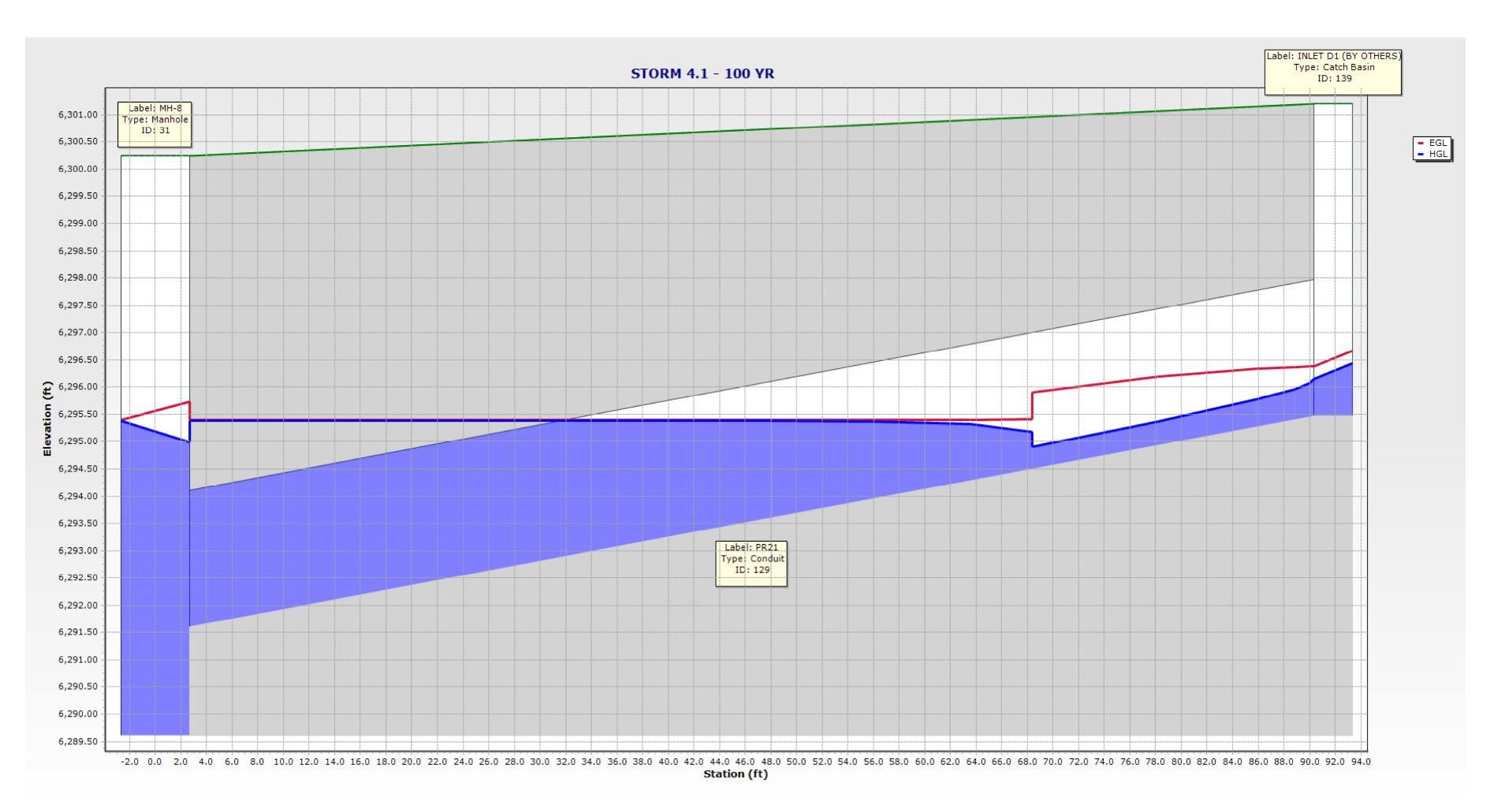
Conduit FlexTable: STRM4 100 YR

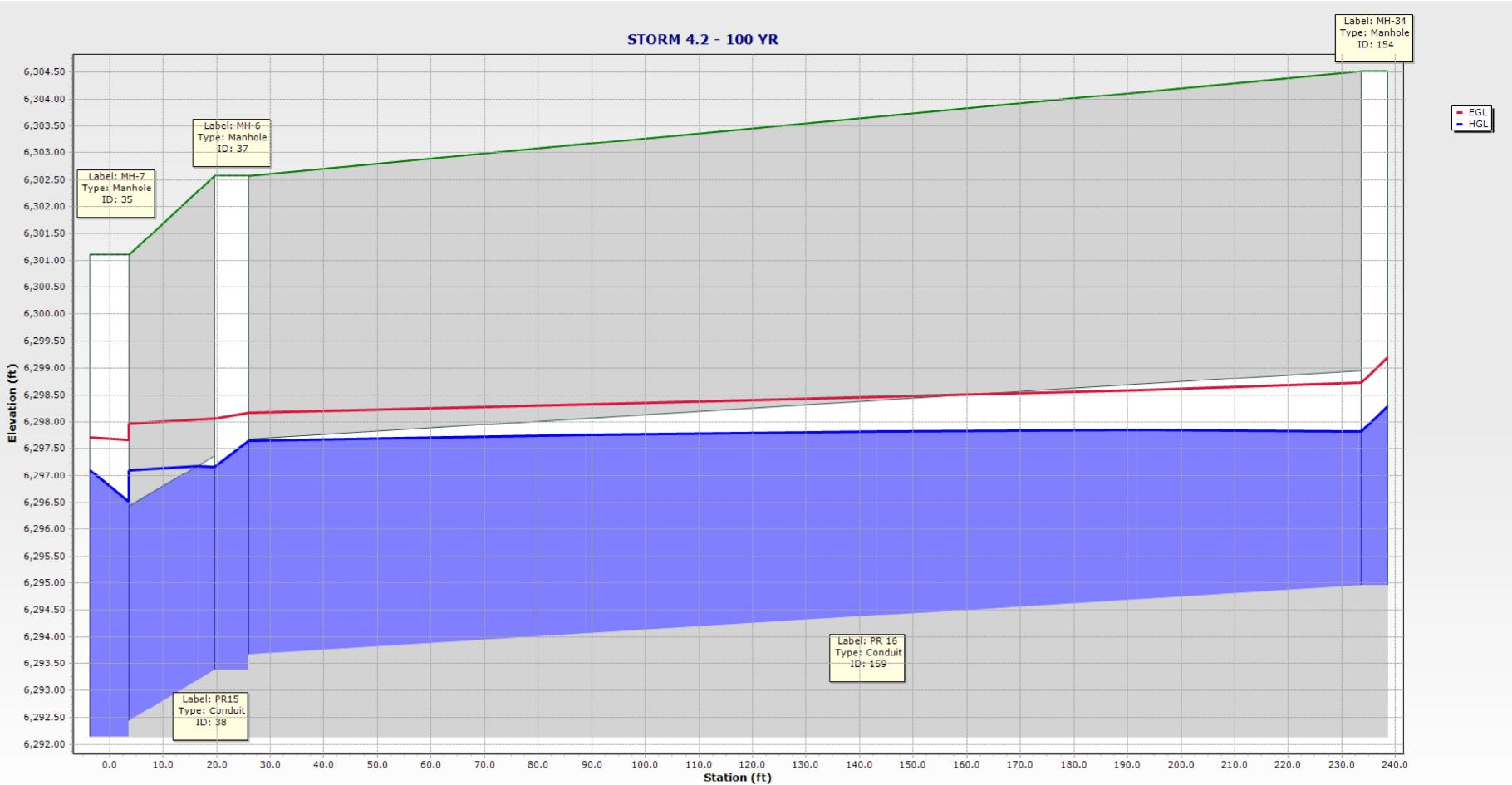
Label	ID	Upstream Structure	Flow (cfs)	Flow / Capacity (Design) (%)	Length (Unified) (ft)	Velocity (ft/s)	Depth (Normal) (ft)	Depth (Critical) (ft)	Energy Grade Line (In) (ft)	Energy Grade Line (Out) (ft)	Hydraulic Grade Line (In) (ft)	Hydraulic Grade Line (Out) (ft)	Headloss (ft)	Upstream Structure Hydraulic Grade Line (In) (ft)
PR17		MH-7	107.40	74.8	203.0	8.55	2.58	3.14	6,297.65	6,296.52	6,296.52	6,295.38	1.13	6,297.11
PR15		MH-6	93.70	32.3	22.8	20.59	1.56	2.93	6,298.07	6,297.97	6,297.17	6,297.11	0.06	6,297.64
PR17.1	118	HW-1	19.60	31.2	45.8	17.68	0.77	1.59	6,299.32	6,297.71	6,298.49	6,297.11	1.38	6,298.91
PR21	129	INLET D1 (BY OTHERS)	4.20	5.0	91.9	8.92	0.38	0.67	6,296.38	6,295.39	6,296.14	6,295.38	0.76	6,296.43
PR18.3		MH-8	109.40	55.6	69.9	6.88	2.40	3.08	6,295.73	6,295.52	6,295.00	6,294.78	0.22	6,295.38
PR22	146	DP4	4.20	10.7	10.3	1.34	0.44	0.72	6,294.81	6,294.81	6,294.79	6,294.78	0.00	6,294.80
PR18.1		MH-33 BS EAST	112.60	5,726.2	9.0	7.08	(N/A)	3.12	6,294.03	6,294.00	6,293.25	6,293.22	0.03	6,294.35
PR18.2	149	MH-32	112.60	56.6	8.8	7.08	2.42	3.12	6,295.16	6,295.13	6,294.38	6,294.35	0.03	6,294.78
PR 18		15' INLET	17.30	21.0	24.4	13.27	0.78	1.41	6,298.13	6,297.83	6,297.56	6,297.64	-0.08	6,298.25
PR 17	158	10' INLET	3.84	20.9	15.7	8.22	0.47	0.75	6,297.74	6,297.71	6,297.55	6,297.64	-0.09	6,297.77
PR 16		MH-34	73.75	66.3	213.2	9.47	2.38	2.60	6,298.73	6,298.17	6,297.82	6,297.64	0.18	6,298.29
PR23	164	MH-35	3.60	34.6	59.2	2.04	0.61	0.72	6,294.93	6,294.87	6,294.87	6,294.80	0.07	6,294.90
PR24	166	DP3	3.60	21.3	77.8	7.60	0.47	0.72	6,296.12	6,294.97	6,295.83	6,294.90	0.93	6,296.17
Upstream Structure Velocity (In- Governing) (ft/s)	Upstream Structure Headloss Coefficient	Upstream Structure Headloss (ft)	Elevation Ground (Start) (ft)	Elevation Ground (Stop) (ft)	Invert (Start) (ft)	Invert (Stop) (ft)	Conduit Description	Manning's n	Friction Slope (ft/ft)	Slope (Calculated) (ft/ft)				
6.24	0.520	0.59	6,300.25	6,301.10	6,290.11	6,292.14	Circle - 48.0 in	0.013	0.006	-0.010				
5.88	0.520	0.47	6,301.10	6,302.57	6,292.44		Circle - 48.0 in	0.013	0.004	-0.041				
7.31	0.500	0.42	6,301.10	6,299.00	6,293.36		Circle - 24.0 in	0.013	0.035	-0.077				
3.93	1.200	0.29	6,300.25	6,301.20	6,291.61	•	Circle - 30.0 in	0.013	0.011	-0.042				
0.86	0.520	0.38	6,299.00	6,300.25	6,288.91		Circle - 54.0 in	0.013	0.003	-0.010				
2.04	0.500	0.01	6,298.70	6,299.00	6,291.72	•	Circle - 24.0 in	0.013	0.000	0.030				
7.08	1.000	1.10	6,297.80	6,297.80	6,288.22		Circle - 54.0 in	0.013	0.003	0.000				
6.88	0.520	0.41	6,297.80	6,299.00	6,288.72	•	Circle - 54.0 in	0.013	0.003	-0.010				
6.08	1.200	0.69	6,302.57	6,302.27	6,295.17		Circle - 30.0 in	0.013	0.012	-0.040				
3.48	1.200	0.23	6,302.57	6,302.23	6,296.17		Circle - 18.0 in	0.013	0.002	-0.031				
7.64	0.520	0.47	6,302.57	6,304.52	6,293.67	•	Circle - 48.0 in	0.013	0.003	-0.006				
2.04	0.520	0.03	6,298.70	6,300.59	6,292.22		Circle - 18.0 in	0.013	0.001	-0.010				
4.26	1.200	0.34	6,300.59	6,298.94	6,293.10	6,295.11	Circle - 18.0 in	0.013	0.015	-0.026				

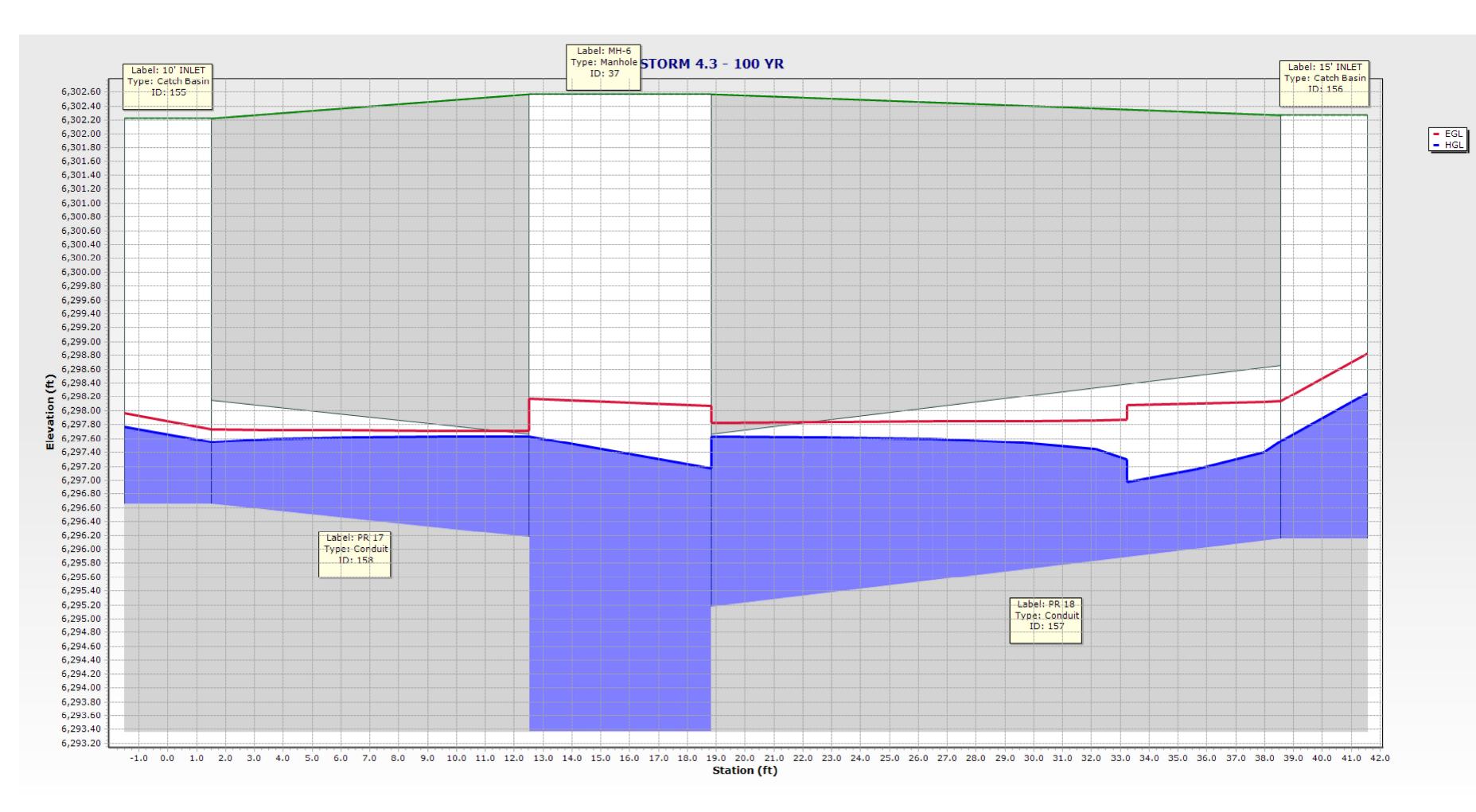
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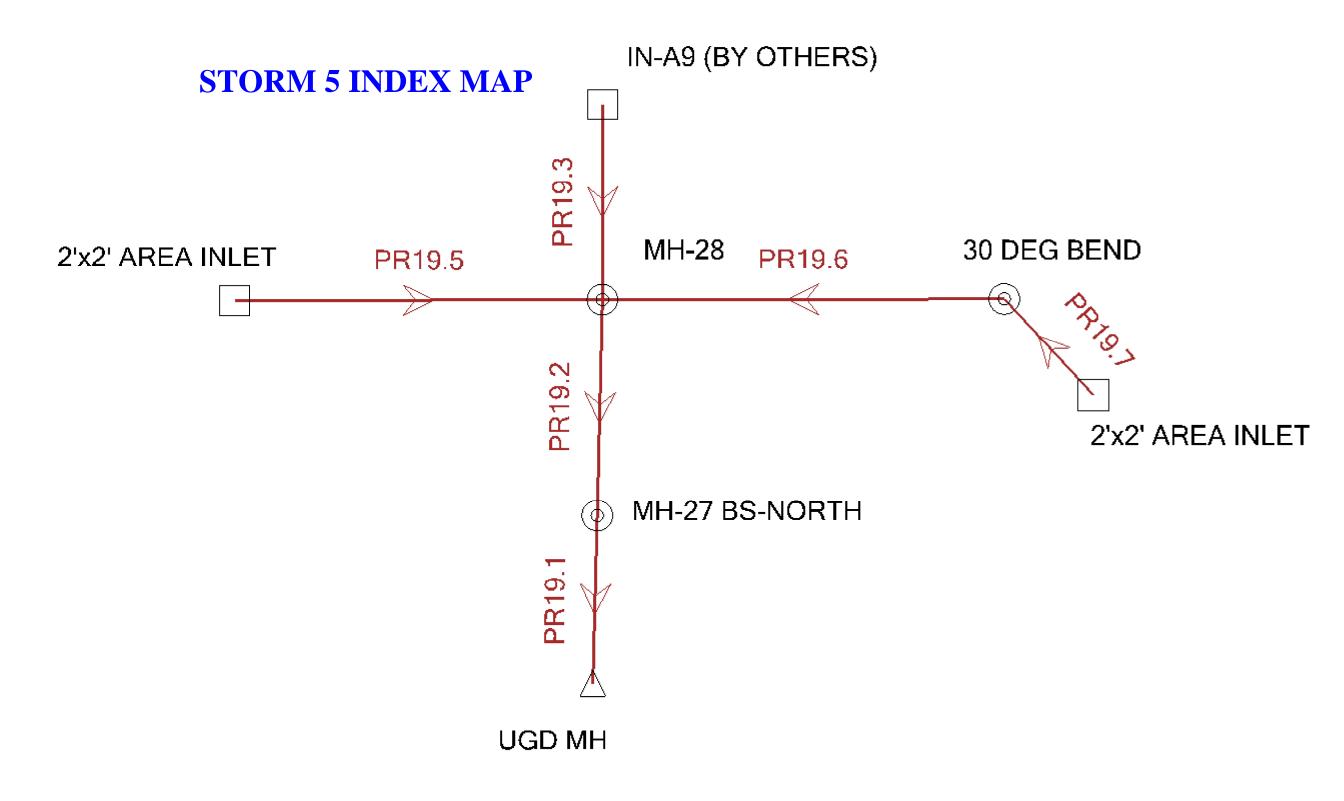








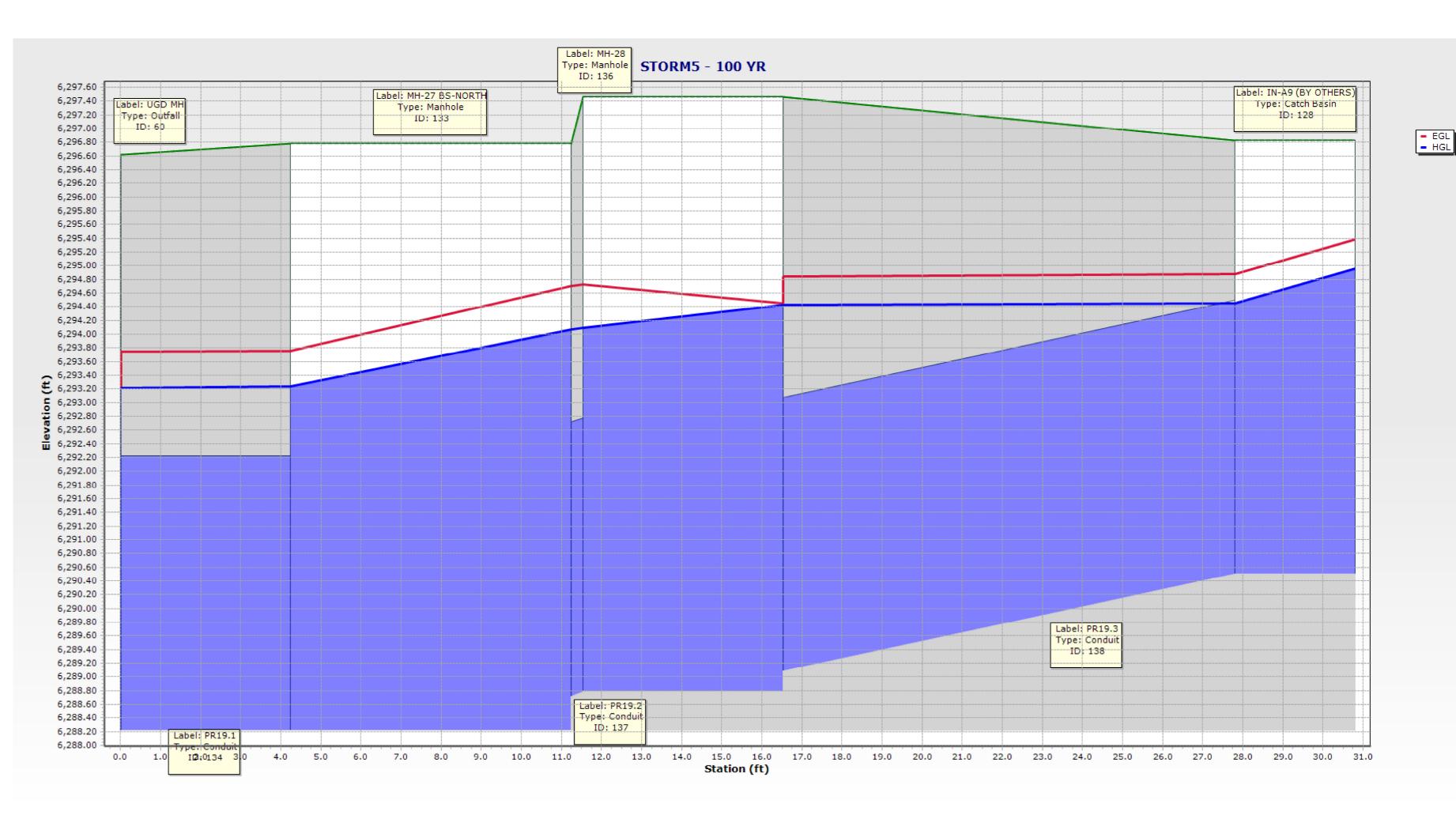


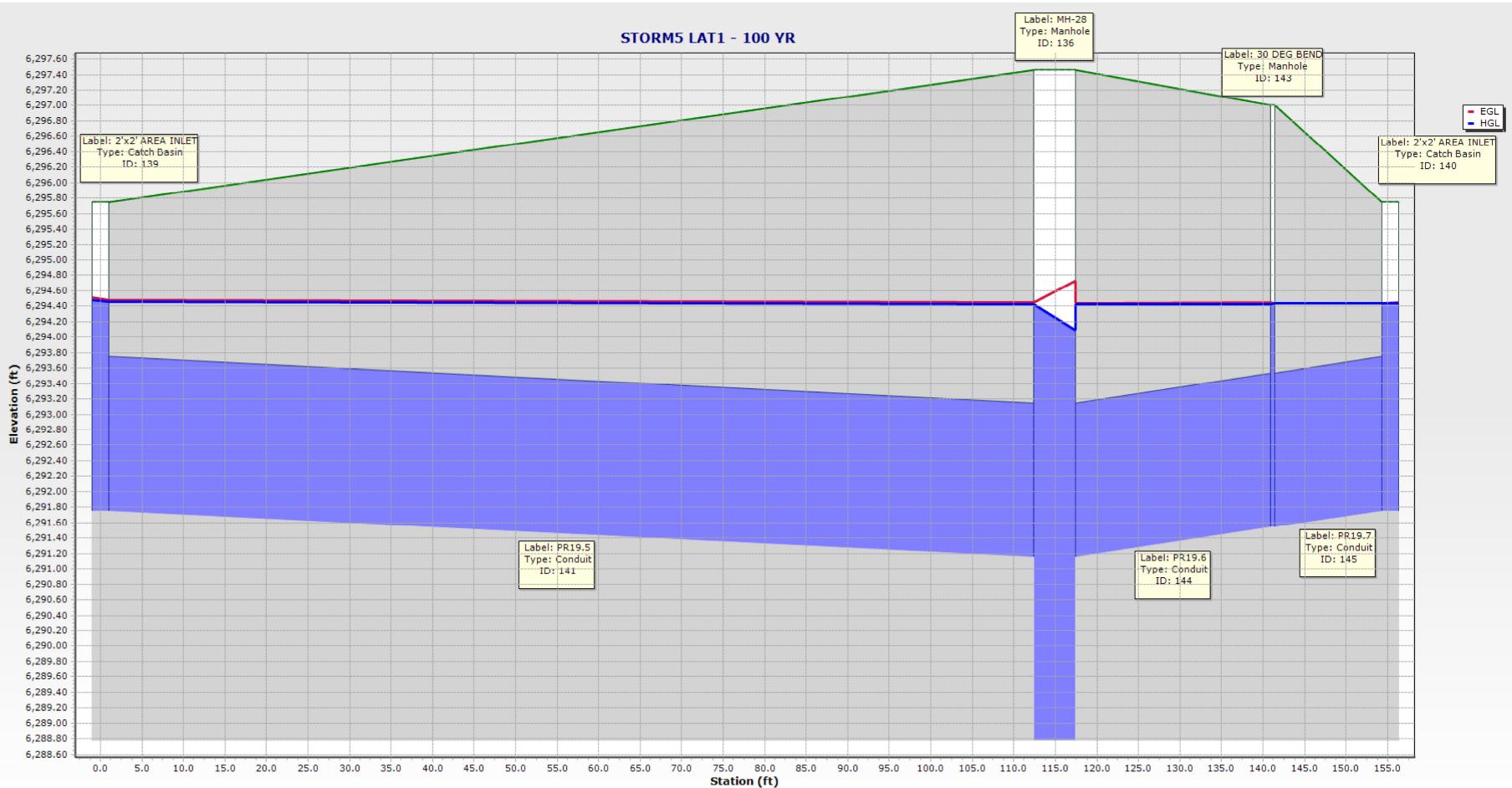


Conduit FlexTable: STRM5 100 YR

ID	Upstream Structure	Flow (cfs)	Flow / Capacity (Design) (%)	Length (Unified) (ft)	Velocity (ft/s)	Depth (Normal) (ft)	Depth (Critical) (ft)	Energy Grade Line (In) (ft)	Energy Grade Line (Out) (ft)	Hydraulic Grade Line (In) (ft)	Hydraulic Grade Line (Out) (ft)	Headloss (ft)	Upstream Structure Hydraulic Grade Line (In) (ft)
134	MH-27 BS- NORTH	71.90	5,005.7	7.7	5.72	(N/A)	2.56	6,293.75	6,293.73	6,293.24	6,293.22	0.02	6,294.07
137	MH-28	71.90	51.3	6.3	5.72	2.03	2.56	6,294.59	6,294.58	6,294.08	6,294.07	0.02	6,294.35
138	IN-A9 (BY OTHERS)	65.50	14.9	15.3	25.06	1.05	2.44	6,294.80	6,294.77	6,294.37	6,294.35	0.02	6,294.89
141	2'x2' AREA INLET	4.70	28.7	114.9	1.50	0.73	0.76	6,294.43	6,294.38	6,294.40	6,294.35	0.05	6,294.44
144	30 DEG BEND	2.30	8.3	26.3	0.73	0.39	0.53	6,294.36	6,294.36	6,294.35	6,294.35	0.00	6,294.36
145	2'x2' AREA INLET	2.30	8.4	14.2	0.73	0.39	0.53	6,294.37	6,294.36	6,294.36	6,294.36	0.00	6,294.37
Upstream Structure Headloss Coefficient	Upstream Structure Headloss (ft)	Elevation Ground (Start) (ft)	Elevation Ground (Stop) (ft)	Invert (Start) (ft)	Invert (Stop) (ft)	Conduit Description	Manning's n	Friction Slope (ft/ft)	Slope (Calculated) (ft/ft)				
1.000	0.83	6,296.62	6,296.78	6,288.22	6,288.22	Circle - 48.0 in	0.013	0.003	0.000				
0.520	0.26	6,296.78	6,297.46	6,288.72			0.013	0.003					
					,								
			-										
	134 137 138 141 144 145 Upstream Structure Headloss Coefficient	Structure134MH-27 BS- NORTH137MH-28138IN-A9 (BY OTHERS)1382'x2' AREA INLET14130 DEG BEND2'x2' AREA INLET2'x2' AREA INLET1452'x2' AREA (Rt)Upstream Structure Headloss CoefficientUpstream Structure Headloss (ft)1.0000.830.5200.261.2000.040.4000.00	Structure (cfs) 134 MH-27 BS- NORTH 71.90 137 MH-28 71.90 138 IN-A9 (BY OTHERS) 65.50 141 2'x2' AREA INLET 4.70 144 30 DEG BEND 2.30 2'x2' AREA INLET 2.30 145 2'x2' AREA INLET 2.30 Upstream Structure Headloss Coefficient Upstream Structure Headloss (ft) Elevation Ground (Start) (ft) 1.000 0.833 6,296.62 0.520 0.26 6,296.78 1.200 0.04 6,297.46 1.200 0.04 6,297.46 0.400 0.00 6,297.46	Structure(cfs)(Design) (%)134MH-27 BS- NORTH71.905,005.7137MH-2871.905,005.7138IN-A9 (BY OTHERS)65.5014.91412'x2' AREA INLET4.7028.714430 DEG BEND2.308.32'x2' AREA INLET2.308.31452'x2' AREA INLET2.308.4Upstream Structure Headloss CoefficientUpstream (ft)Elevation Ground (Start) (ft)Elevation Ground (Start) (ft)1.0000.836,296.626,296.780.5200.266,296.786,297.461.2000.526,297.466,297.461.2000.046,297.466,295.750.4000.006,297.466,297.46	Structure (cfs) (Design) (%) (ft) 134 MH-27 BS- NORTH 71.90 5,005.7 7.7 137 MH-28 71.90 51.3 6.3 138 IN-A9 (BY OTHERS) 65.50 14.9 15.3 141 2'x2' AREA INLET 4.70 28.7 114.9 144 30 DEG BEND 2.30 8.3 26.3 2'x2' AREA INLET 2.30 8.4 14.2 Upstream Structure Headloss Coefficient Upstream Structure Headloss (ft) Elevation Ground (Start) (ft) Invert (Start) (ft) Invert (Start) (ft) 1.000 0.83 6,296.62 6,296.78 6,288.22 0.520 0.26 6,296.78 6,288.72 1.200 0.52 6,297.46 6,296.83 6,289.08 1.200 0.04 6,297.46 6,295.75 6,291.15 0.400 0.00 6,297.46 6,297.00 6,291.15	Structure (cfs) (Design) (%) (ft) (ft/s) 134 MH-27 BS- NORTH 71.90 5,005.7 7.7 5.72 137 MH-28 71.90 5,005.7 7.7 5.72 138 IN-A9 (BY OTHERS) 65.50 14.9 15.3 6.3 5.72 138 IN-A9 (BY OTHERS) 65.50 14.9 15.3 25.06 141 2'x2' AREA INLET 4.70 28.7 114.9 1.50 144 30 DEG BEND 2.30 8.3 26.3 0.73 2'x2' AREA INLET 2.30 8.4 14.2 0.73 Upstream Structure Headloss Coefficient Upstream Structure Headloss (ft) Elevation Ground (Start) (ft) Invert (Start) (ft) Invert (Stop) (ft) Invert (Stop) (ft) 1.000 0.83 6,296.78 6,297.46 6,288.72 6,288.72 0.520 0.26 6,297.46 6,297.46 6,289.08 6,290.50 1.200 0.04 6,297.46 6,297.50 6,291.15 6,291.75 </td <td>Structure Structure (cfs) (Design) (%) (ft) (ft/s) (ft/s) (ft) 134 MH-27 BS- NORTH 71.90 5,005.7 7.7 5.72 (N/A) 137 MH-28 71.90 5,005.7 7.7 5.72 (N/A) 138 IN-A9 (BY OTHERS) 65.50 14.9 15.3 25.06 1.05 2'x2' AREA INLET 4.70 28.7 114.9 1.50 0.73 144 30 DEG BEND 2.30 8.3 26.3 0.73 0.39 144 30 DEG BEND 2.30 8.4 14.2 0.73 0.39 145 INLET 2.30 8.4 14.2 0.73 0.39 145 Structure Kitucture Structure Conduit Description 0.39 145 INLET 6.296.78 6.296.78 6.288.22 6.288.22 6.288.12 1.000 0.83 6.296.62 6.296.78 6.288.72 6.288.72 6.288.78 <</td> <td>Structure Structure (cfs) (Design) (%) (ft) (ft/s) (ft) (ft)</td> <td>Structure Structure (cfs) (Design) (%) (ft) (ft/s) (ft) (ft) (ft) Line (In) (ft) 134 MH-27 BS- NORTH 71.90 5,005.7 7.7 5.72 (N/A) 2.56 6.293.75 137 MH-28 71.90 51.3 6.3 5.72 2.03 2.56 6.294.59 138 IN-A9 (BY OTHERS) 65.50 14.9 15.3 25.06 1.05 2.44 6.294.43 141 2'X2' AREA INLET 4.70 28.7 114.9 1.50 0.73 0.76 6.294.43 144 30 DEG BEND 2.30 8.3 26.3 0.73 0.39 0.53 6.294.43 145 ZX2' AREA INLET 2.30 8.4 14.2 0.73 0.39 0.53 6.294.35 Structure Upstream Structure Upstream Upstream (ft) Invert (Start) (ft) Invert (Start) Description Manning's n Friction Slope (ft/ft) 1.000 0.83 6.296</td> <td>Structure Structure (cfs) (Design) (ft) (ft) (ft) (ft) (ft) (ft) Line (n) Line (Out) 134 MH-27 BS- NORTH 71.90 5,005.7 7.7 5.72 (N)A 2.56 6,293.75 6,293.73 137 MH-28 71.90 5,005.7 7.7 5.72 2.03 2.56 6,294.59 6,294.58 138 MH-28 71.90 55.00 14.9 15.3 25.66 1.05 2.44 6,294.80 6,294.77 141 722' AREA 4.70 2.83 114.9 1.50 0.73 0.76 6,294.43 6,294.38 144 30 DEG BEND 2.30 8.3 26.3 0.73 0.39 0.53 6,294.36 6,294.36 1145 722' AREA 2.30 8.4 14.2 0.73 0.39 0.53 6,294.36 6,294.36 1145 NUET Headloss (ft) (ft) Invert (Stor) (ft) Description</td> <td>Structure Structure (cfs) (cbesign) cff) (ff/s) (ff) (ff</td> <td>Structure Structure (cfs) (besign) (ft) (ft) (ft) (ft) (ft) Line (n) Line (n)</td> <td>Structure Headloss Coefficient C(fs) HI-2 (fs) (%) (ft) (%) (ft) (ft) (ft)</td>	Structure Structure (cfs) (Design) (%) (ft) (ft/s) (ft/s) (ft) 134 MH-27 BS- NORTH 71.90 5,005.7 7.7 5.72 (N/A) 137 MH-28 71.90 5,005.7 7.7 5.72 (N/A) 138 IN-A9 (BY OTHERS) 65.50 14.9 15.3 25.06 1.05 2'x2' AREA INLET 4.70 28.7 114.9 1.50 0.73 144 30 DEG BEND 2.30 8.3 26.3 0.73 0.39 144 30 DEG BEND 2.30 8.4 14.2 0.73 0.39 145 INLET 2.30 8.4 14.2 0.73 0.39 145 Structure Kitucture Structure Conduit Description 0.39 145 INLET 6.296.78 6.296.78 6.288.22 6.288.22 6.288.12 1.000 0.83 6.296.62 6.296.78 6.288.72 6.288.72 6.288.78 <	Structure Structure (cfs) (Design) (%) (ft) (ft/s) (ft) (ft)	Structure Structure (cfs) (Design) (%) (ft) (ft/s) (ft) (ft) (ft) Line (In) (ft) 134 MH-27 BS- NORTH 71.90 5,005.7 7.7 5.72 (N/A) 2.56 6.293.75 137 MH-28 71.90 51.3 6.3 5.72 2.03 2.56 6.294.59 138 IN-A9 (BY OTHERS) 65.50 14.9 15.3 25.06 1.05 2.44 6.294.43 141 2'X2' AREA INLET 4.70 28.7 114.9 1.50 0.73 0.76 6.294.43 144 30 DEG BEND 2.30 8.3 26.3 0.73 0.39 0.53 6.294.43 145 ZX2' AREA INLET 2.30 8.4 14.2 0.73 0.39 0.53 6.294.35 Structure Upstream Structure Upstream Upstream (ft) Invert (Start) (ft) Invert (Start) Description Manning's n Friction Slope (ft/ft) 1.000 0.83 6.296	Structure Structure (cfs) (Design) (ft) (ft) (ft) (ft) (ft) (ft) Line (n) Line (Out) 134 MH-27 BS- NORTH 71.90 5,005.7 7.7 5.72 (N)A 2.56 6,293.75 6,293.73 137 MH-28 71.90 5,005.7 7.7 5.72 2.03 2.56 6,294.59 6,294.58 138 MH-28 71.90 55.00 14.9 15.3 25.66 1.05 2.44 6,294.80 6,294.77 141 722' AREA 4.70 2.83 114.9 1.50 0.73 0.76 6,294.43 6,294.38 144 30 DEG BEND 2.30 8.3 26.3 0.73 0.39 0.53 6,294.36 6,294.36 1145 722' AREA 2.30 8.4 14.2 0.73 0.39 0.53 6,294.36 6,294.36 1145 NUET Headloss (ft) (ft) Invert (Stor) (ft) Description	Structure Structure (cfs) (cbesign) cff) (ff/s) (ff) (ff	Structure Structure (cfs) (besign) (ft) (ft) (ft) (ft) (ft) Line (n) Line (n)	Structure Headloss Coefficient C(fs) HI-2 (fs) (%) (ft) (%) (ft) (ft) (ft)

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UNDERGROUND DETENTION DETAILS

PROJECT INFORMATION

-	
ENGINEERED	JEROME MAGSINO
PRODUCT	303-349-7555
MANAGER:	JEROME.MAGSINO@ADSPIPE.COM
	AARON ZEE
ADS SALES REP:	
	AARON.ZEE@ADSPIPE.COM
PROJECT NO:	S295850



CROSSROADS MIXED USE FILING NO. 1 COLORADO SPRINGS, CO

MC-7200 STORMTECH CHAMBER SPECIFICATIONS

- CHAMBERS SHALL BE STORMTECH MC-7200. 1.
- 2. CHAMBERS SHALL BE ARCH-SHAPED AND SHALL BE MANUFACTURED FROM VIRGIN, IMPACT-MODIFIED POLYPROPYLENE COPOLYMERS
- CHAMBERS SHALL MEET THE REQUIREMENTS OF ASTM F2418, "STANDARD SPECIFICATION FOR POLYPROPYLENE (PP) CORRUGATED 3. WALL STORMWATER COLLECTION CHAMBERS" CHAMBER CLASSIFICATION 60x101.
- CHAMBER ROWS SHALL PROVIDE CONTINUOUS, UNOBSTRUCTED INTERNAL SPACE WITH NO INTERNAL SUPPORTS THAT WOULD 4 IMPEDE FLOW OR LIMIT ACCESS FOR INSPECTION.
- THE STRUCTURAL DESIGN OF THE CHAMBERS, THE STRUCTURAL BACKFILL, AND THE INSTALLATION REQUIREMENTS SHALL ENSURE 5. THAT THE LOAD FACTORS SPECIFIED IN THE AASHTO LRFD BRIDGE DESIGN SPECIFICATIONS, SECTION 12.12, ARE MET FOR: 1) LONG-DURATION DEAD LOADS AND 2) SHORT-DURATION LIVE LOADS. BASED ON THE AASHTO DESIGN TRUCK WITH CONSIDERATION FOR IMPACT AND MULTIPLE VEHICLE PRESENCES.
- CHAMBERS SHALL BE DESIGNED, TESTED AND ALLOWABLE LOAD CONFIGURATIONS DETERMINED IN ACCORDANCE WITH ASTM F2787, 6. "STANDARD PRACTICE FOR STRUCTURAL DESIGN OF THERMOPLASTIC CORRUGATED WALL STORMWATER COLLECTION CHAMBERS". LOAD CONFIGURATIONS SHALL INCLUDE: 1) INSTANTANEOUS (<1 MIN) AASHTO DESIGN TRUCK LIVE LOAD ON MINIMUM COVER 2) MAXIMUM PERMANENT (75-YR) COVER LOAD AND 3) ALLOWABLE COVER WITH PARKED (1-WEEK) AASHTO DESIGN TRUCK
- REQUIREMENTS FOR HANDLING AND INSTALLATION: 7.
 - TO MAINTAIN THE WIDTH OF CHAMBERS DURING SHIPPING AND HANDLING, CHAMBERS SHALL HAVE INTEGRAL, INTERLOCKING STACKING LUGS.
 - TO ENSURE A SECURE JOINT DURING INSTALLATION AND BACKFILL. THE HEIGHT OF THE CHAMBER JOINT SHALL NOT BE LESS THAN 3"
 - TO ENSURE THE INTEGRITY OF THE ARCH SHAPE DURING INSTALLATION, a) THE ARCH STIFFNESS CONSTANT SHALL BE GREATER THAN OR EQUAL TO 450 LBS/FT/%. THE ASC IS DEFINED IN SECTION 6.2.8 OF ASTM F2418. AND b) TO RESIST CHAMBER DEFORMATION DURING INSTALLATION AT ELEVATED TEMPERATURES (ABOVE 73° F / 23° C), CHAMBERS SHALL BE PRODUCED FROM REFLECTIVE GOLD OR YELLOW COLORS
- ONLY CHAMBERS THAT ARE APPROVED BY THE SITE DESIGN ENGINEER WILL BE ALLOWED. UPON REQUEST BY THE SITE DESIGN 8. ENGINEER OR OWNER, THE CHAMBER MANUFACTURER SHALL SUBMIT A STRUCTURAL EVALUATION FOR APPROVAL BEFORE DELIVERING CHAMBERS TO THE PROJECT SITE AS FOLLOWS:
 - THE STRUCTURAL EVALUATION SHALL BE SEALED BY A REGISTERED PROFESSIONAL ENGINEER. ٠
 - THE STRUCTURAL EVALUATION SHALL DEMONSTRATE THAT THE SAFETY FACTORS ARE GREATER THAN OR EQUAL TO 1.95 FOR DEAD LOAD AND 1.75 FOR LIVE LOAD, THE MINIMUM REQUIRED BY ASTM F2787 AND BY SECTIONS 3 AND 12.12 OF THE AASHTO LRFD BRIDGE DESIGN SPECIFICATIONS FOR THERMOPLASTIC PIPE.
 - THE TEST DERIVED CREEP MODULUS AS SPECIFIED IN ASTM F2418 SHALL BE USED FOR PERMANENT DEAD LOAD DESIGN EXCEPT THAT IT SHALL BE THE 75-YEAR MODULUS USED FOR DESIGN.
- CHAMBERS AND END CAPS SHALL BE PRODUCED AT AN ISO 9001 CERTIFIED MANUFACTURING FACILITY. 9

IMPORTANT - THIS PROJECT REQUIRES COMPACTION OF EMBEDMENT STONE AND REQUIREMENTS FOR STONE HARDNESS AND SHAPE WHICH ARE NOT SPECIFIED IN OTHER STORMTECH DOCUMENTS. CONTRACTORS MUST FOLLOW THE SPECIAL PROVISIONS IN THIS PLAN SET.

IMPORTANT - NOTES FOR THE BIDDING AND INSTALLATION OF MC-7200 CHAMBER SYSTEM

- STORMTECH MC-7200 CHAMBERS SHALL NOT BE INSTALLED UNTIL THE MANUFACTURER'S REPRESENTATIVE HAS COMPLETED A PRE-CONSTRUCTION MEETING WITH THE INSTALLERS.
- 2 STORMTECH MC-7200 CHAMBERS SHALL BE INSTALLED IN ACCORDANCE WITH THE "STORMTECH MC-7200 CONSTRUCTION GUIDE".
- CHAMBERS ARE NOT TO BE BACKFILLED WITH A DOZER OR EXCAVATOR SITUATED OVER THE CHAMBERS. 3. STORMTECH RECOMMENDS 3 BACKFILL METHODS:
 - STONESHOOTER LOCATED OFF THE CHAMBER BED.
 - BACKFILL AS ROWS ARE BUILT USING AN EXCAVATOR ON THE FOUNDATION STONE OR SUBGRADE. BACKFILL FROM OUTSIDE THE EXCAVATION USING A LONG BOOM HOE OR EXCAVATOR.
- THE FOUNDATION STONE SHALL BE LEVELED AND COMPACTED PRIOR TO PLACING CHAMBERS. 4.
- JOINTS BETWEEN CHAMBERS SHALL BE PROPERLY SEATED PRIOR TO PLACING STONE. 5.
- MAINTAIN MINIMUM 9" (230 mm) SPACING BETWEEN THE CHAMBER ROWS. 6.
- INLET AND OUTLET MANIFOLDS MUST BE INSERTED A MINIMUM OF 12" (300 mm) INTO CHAMBER END CAPS. 7.
- 8. OR #4.
- 9. STONE SHALL BE BROUGHT UP EVENLY AROUND CHAMBERS SO AS NOT TO DISTORT THE CHAMBER SHAPE. STONE DEPTHS SHOULD NEVER DIFFER BY MORE THAN 12" (300 mm) BETWEEN ADJACENT CHAMBER ROWS.
- STONE MUST BE PLACED ON THE TOP CENTER OF THE CHAMBER TO ANCHOR THE CHAMBERS IN PLACE AND PRESERVE ROW SPACING. 10
- 11. THE CONTRACTOR MUST REPORT ANY DISCREPANCIES WITH CHAMBER FOUNDATION MATERIAL BEARING CAPACITIES TO THE SITE DESIGN ENGINEER.
- ADS RECOMMENDS THE USE OF "FLEXSTORM CATCH IT" INSERTS DURING CONSTRUCTION FOR ALL INLETS TO PROTECT THE SUBSURFACE 12. STORMWATER MANAGEMENT SYSTEM FROM CONSTRUCTION SITE RUNOFF.

NOTES FOR CONSTRUCTION EQUIPMENT

- 1 STORMTECH MC-7200 CHAMBERS SHALL BE INSTALLED IN ACCORDANCE WITH THE "STORMTECH MC-7200 CONSTRUCTION GUIDE"
- THE USE OF EQUIPMENT OVER MC-7200 CHAMBERS IS LIMITED: 2.
 - NO EQUIPMENT IS ALLOWED ON BARE CHAMBERS.
 - WITH THE "STORMTECH MC-7200 CONSTRUCTION GUIDE"
 - WEIGHT LIMITS FOR CONSTRUCTION EQUIPMENT CAN BE FOUND IN THE "STORMTECH MC-7200 CONSTRUCTION GUIDE"
- 3. FULL 36" (900 mm) OF STABILIZED COVER MATERIALS OVER THE CHAMBERS IS REQUIRED FOR DUMP TRUCK TRAVEL OR DUMPING.

USE OF A DOZER TO PUSH EMBEDMENT STONE BETWEEN THE ROWS OF CHAMBERS MAY CAUSE DAMAGE TO CHAMBERS AND IS NOT AN ACCEPTABLE BACKFILL METHOD. ANY CHAMBERS DAMAGED BY USING THE "DUMP AND PUSH" METHOD ARE NOT COVERED UNDER THE STORMTECH STANDARD WARRANTY

CONTACT STORMTECH AT 1-888-892-2694 WITH ANY QUESTIONS ON INSTALLATION REQUIREMENTS OR WEIGHT LIMITS FOR CONSTRUCTION EQUIPMENT.

2022 ADS INC





EMBEDMENT STONE SURROUNDING CHAMBERS MUST BE A CLEAN, CRUSHED, ANGULAR STONE MEETING THE AASHTO M43 DESIGNATION OF #3

NO RUBBER TIRED LOADER, DUMP TRUCK, OR EXCAVATORS ARE ALLOWED UNTIL PROPER FILL DEPTHS ARE REACHED IN ACCORDANCE

CONCEPTUAL LAYOUT

731	STORMTECH MC-7200 CHAMBERS
44	STORMTECH MC-7200 END CAPS
12	STONE ABOVE (in)
36	STONE BELOW (in)
40	% STONE VOID
206,903	INSTALLED SYSTEM VOLUME (CF) ABOVE ELEVATION 6287.47 (PERIMETER STONE INCLUDED)
47670	SYSTEM AREA (ft ²)
1006	SYSTEM PERIMETER (ft)

CONCEPTUAL ELEVATIONS

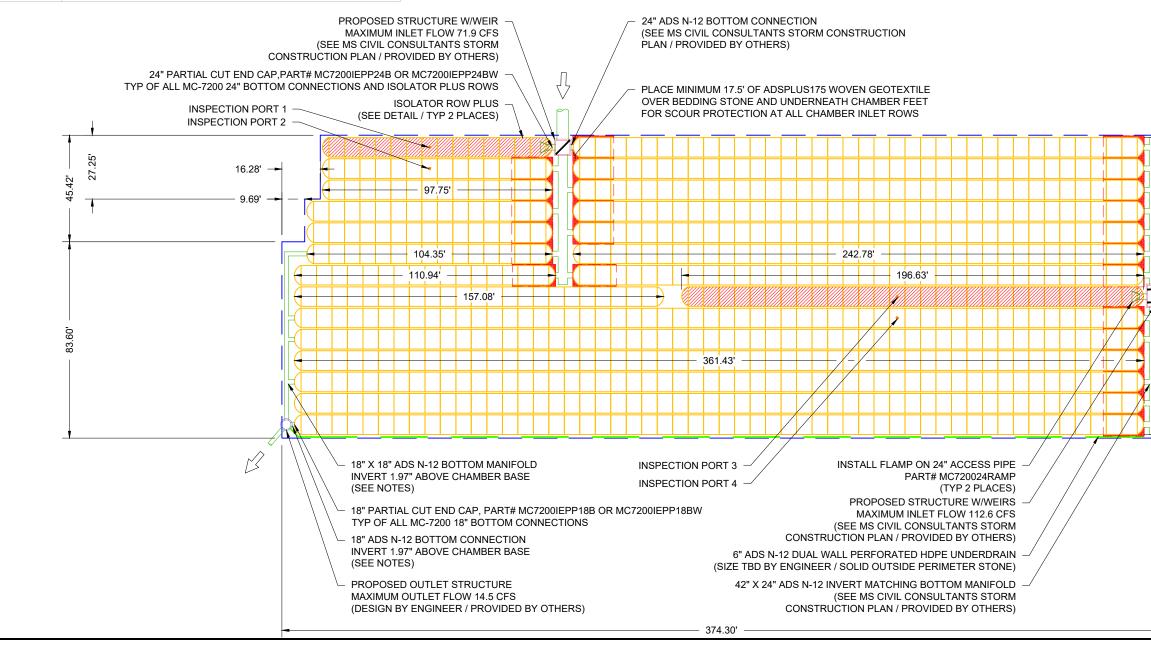
6300.52±	MAXIMUM GRADE PER ENGINEER'S PLAN
6297.72	MINIMUM ALLOWABLE GRADE (UNPAVED WITH TRAFFIC)
6297.22	MINIMUM ALLOWABLE GRADE (UNPAVED NO TRAFFIC)
6297.22	MINIMUM ALLOWABLE GRADE (BASE OF FLEXIBLE PAVEMENT)
6297.22	MINIMUM ALLOWABLE GRADE (TOP OF RIGID PAVEMENT)
6296.22	TOP OF STONE
6295.22	TOP OF MC-7200 CHAMBER
6290.41	42" X 24" MANIFOLD INVERT
6290.41	24" ISOLATOR ROW PLUS CONNECTION INVERT
6290.41	24" BOTTOM CONNECTION
6290.38	18" BOTTOM MANIFOLD / CONNECTION INVERT
6290.22	BOTTOM OF MC-7200 CHAMBER
6289.47	UNDERDRAIN INVERT
6287.22	BOTTOM OF STONE

NOTES

- MANIFOLD SIZE TO BE DETERMINED BY SITE DESIGN ENGINEER. SEE TECHNICAL NOTE 6.32 FOR MANIFOLD SIZING GUIDANCE.
- DUE TO THE ADAPTATION OF THIS CHAMBER SYSTEM TO SPECIFIC SITE AND DESIGN CONSTRAINTS, IT MAY BE NECESSARY TO CUT AND CO MANIFOLD COMPONENTS IN THE FIELD.
- THE SITE DESIGN ENGINEER MUST REVIEW ELEVATIONS AND IF NECESSARY ADJUST GRADING TO ENSURE THE CHAMBER COVER REQUIRE
 THIS CHAMBER SYSTEM WAS DESIGNED WITHOUT SITE-SPECIFIC INFORMATION ON SOIL CONDITIONS OR BEARING CAPACITY. THE SITE DE DETERMINING THE SUITABILITY OF THE SOIL AND PROVIDING THE BEARING CAPACITY OF THE INSITU SOILS. THE BASE STONE DEPTH MAY IT THIS INFORMATION IS PROVIDED.
- NOT FOR CONSTRUCTION: THIS LAYOUT IS FOR DIMENSIONAL PURPOSES ONLY TO PROVE CONCEPT & THE REQUIRED STORA

TIER 1 DEEP COVER SPECIAL PROVISIONS

- INSTALLATION REQUIREMENTS SHALL BE AS SPECIFIED IN THE STORMTECH DESIGN MANUALS AND CONSTRUCTION GUIDES EXCEPT AS MC
 ATTENTION IS CALLED TO "TABLE 1 ACCEPTABLE FILL MATERIALS" IN THE STORMTECH CONSTRUCTION GUIDE AND ALL OTHER APPEARAN MATERIALS TABLE. FOR AREAS OF THE SYSTEM WITH COVER ABOVE 7 FEET (2.1 m) FOR THE MC-4500/MC-7200 AND ABOVE 8 FEET (2.4 m) FO SHALL BE COMPACTED WITH 1-3 PASSES OF A WALK BEHIND VIBRATORY PLATE COMPACTOR OR JUMPING JACK IN 12-18" (300-450 mm) LIFTS
- STONE SHALL BE CLEAN, CRUSHED, AND ANGULAR AND SHALL CONFORM TO THE SPECIFICATIONS DESIGNATED IN THE ACCEPTABLE FILL
 STONE SHALL BE HARD AND DURABLE. IT IS THE ENGINEER'S OR CONTRACTOR'S RESPONSIBILITY TO SELECT HARD AND DURABLE STONE.
 - ABRASION VALUE OF LESS THAN OR EQUAL TO 30 TO BE HARD STONE.
- 5. FOUNDATION STONE SHALL BE MECHANICALLY COMPACTED WITH A VIBRATORY ROLLER OR VIBRATORY PLATE IN 6" (152 mm) LIFTS.
- EMBEDMENT STONE MUST BE DUMPED IN PLACE BY A STONE SHOOTER OR CONVEYOR OR EXCAVATOR.
 INSPECTION DURING THE INSTALLATION BY THE ENGINEER. OWNER OR OTHER REPRESENTATIVE IS REC
- INSPECTION DURING THE INSTALLATION BY THE ENGINEER, OWNER OR OTHER REPRESENTATIVE IS RECOMMENDED. THE INSPECTION SHA CHAMBER SYMMETRY DURING BACKFILLING TO ENSURE THE CONTRACTOR'S METHODS ARE NOT CAUSING UNACCEPTABLE DISTORTION OF
- AN ADS FIELD TECHNICIAN WILL CONDUCT A PRE-CONSTRUCTION MEETING TO TRAIN REPRESENTATIVES INSTALLING THE CHAMBERS AND INSTALLATION INSPECTIONS.



-			128.01				IALL INCLUDE OBSERVATIONS OF THE OF THE CHAMBERS. D THOSE WHO MAY BE PERFORMING	MODIFIED IN THESE SPECIAL PROVISIONS. INCES OF THE "ACCEPTABLE FILL FOR THE MC-3500, EMBEDMENT STONE TS. MATERIALS TABLE. E. STORMTECH CONSIDERS AN LA	ESIGN ENGINEER IS RESPONSIBLE FOR ' BE INCREASED OR DECREASED ONCE	COUPLE ADDITIONAL PIPE TO STANDARD	
								CROSSROADS MIXED USE	S MIXE	D USE	
2	4640 TRUE	4640 TRUEMAN BLVD	e I I I I I I I I I I I I I I I I I I I					FILINC	FILING NO. 1		
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O			Chamber Svetem	-	IKI						
	0 40'	80'			JAL IPR	UPDATED ELEVATIONS FI EVATION AND I AYOUT ADJUISTMENTS		DATE: 05-05-22	DRAWN:	TSG	
			888-892-2694 WWW.STORMTECH.COM		CHKD	DESCRIPTION		PROJECT #: S295850	CHECKED:	D: CTS	
5	THIS DRAWING HAS BEEN PREPARED BASED ON INFORMATION PROVIDED TO ADS UNDER THE DIRECTION O RESPONSIBILITY OF THE SITE DESIGN ENGINEER TO ENSURE THAT THE PRODUCT(S) DEPICTED AND ALL ASS	INFORMATION PROV	THIS DRAWING HAS BEEN PREPARED BASED ON INFORMATION PROVIDED TO ADS UNDER THE DIRECTION OF THE SITE DESIGN ENGIN RESPONSIBILITY OF THE SITE DESIGN ENGINEER TO ENSURE THAT THE PRODUCT(S) DEPICTED AND ALL ASSOCIATED DETAILS MEET ALL APPLICABLE LAWS, REGULATIONS, AND PROJECT REQUIREMENTS	R OR OTHER - APPLICABLE	PROJECT REPRE LAWS, REGULAT	SENTATIVE. THE SITE DESIGN E IONS, AND PROJECT REQUIREMI	ENGINEER SHALL ENTS.	F THE SITE DESIGN ENGINEER OR OTHER PROJECT REPRESENTATIVE. THE SITE DESIGN ENGINEER SHALL REVIEW THIS DRAWING PRIOR TO CONSTRUCTION. IT IS THE ULTIMAT SOCIATED DETAILS MEET ALL APPLICABLE LAWS, REGULATIONS, AND PROJECT REQUIREMENTS.	CONSTRUCTIO	N. IT IS THE UL	ILTIMATE

ACCEPTABLE FILL MATERIALS: STORMTECH MC-7200 CHAMBER SYSTEMS

	MATERIAL LOCATION	DESCRIPTION	AASHTO MATERIAL CLASSIFICATIONS	COMPAC
D	FINAL FILL: FILL MATERIAL FOR LAYER 'D' STARTS FROM THE TOP OF THE 'C' LAYER TO THE BOTTOM OF FLEXIBLE PAVEMENT OR UNPAVED FINISHED GRADE ABOVE. NOTE THAT PAVEMENT SUBBASE MAY BE PART OF THE 'D' LAYER	ANY SOIL/ROCK MATERIALS, NATIVE SOILS, OR PER ENGINEER'S PLANS. CHECK PLANS FOR PAVEMENT SUBGRADE REQUIREMENTS.	N/A	PREPARE F INSTALLAT
С	INITIAL FILL: FILL MATERIAL FOR LAYER 'C' STARTS FROM THE TOP OF THE EMBEDMENT STONE ('B' LAYER) TO 24" (600 mm) ABOVE THE TOP OF THE CHAMBER. NOTE THAT PAVEMENT SUBBASE MAY BE A PART OF THE 'C' LAYER.	GRANULAR WELL-GRADED SOIL/AGGREGATE MIXTURES, <35% FINES OR PROCESSED AGGREGATE. MOST PAVEMENT SUBBASE MATERIALS CAN BE USED IN LIEU OF THIS LAYER.	AASHTO M145 ¹ A-1, A-2-4, A-3 OR AASHTO M43 ¹ 3, 357, 4, 467, 5, 56, 57, 6, 67, 68, 7, 78, 8, 89, 9, 10	BEGIN COMPA THE CHAMBER 12" (300 mm) M WELL GRADE PR
В	EMBEDMENT STONE: FILL SURROUNDING THE CHAMBERS FROM THE FOUNDATION STONE ('A' LAYER) TO THE 'C' LAYER ABOVE.	CLEAN, CRUSHED, ANGULAR STONE	AASHTO M431 3, 4	COMPACTION
А	FOUNDATION STONE: FILL BELOW CHAMBERS FROM THE SUBGRADE UP TO THE FOOT (BOTTOM) OF THE CHAMBER.	CLEAN, CRUSHED, ANGULAR STONE	AASHTO M431 3, 4	PLATE COMP

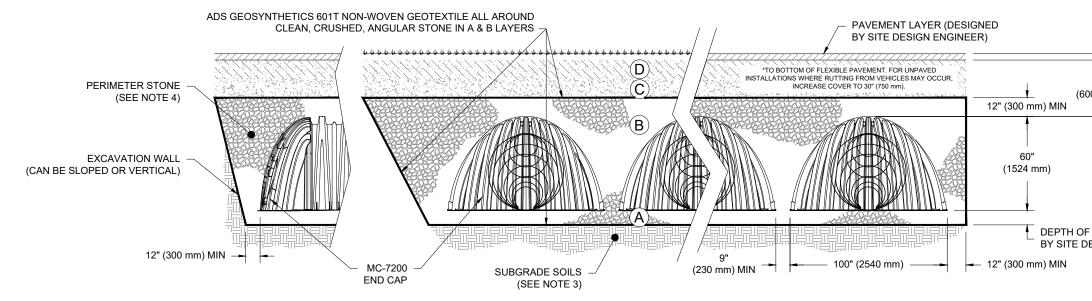
PLEASE NOTE:

THE LISTED AASHTO DESIGNATIONS ARE FOR GRADATIONS ONLY. THE STONE MUST ALSO BE CLEAN, CRUSHED, ANGULAR. FOR EXAMPLE, A SPECIFICATION FOR #4 STONE WOULD STATE: "CLEAN, CRUSHED, ANGULAR NO. 4 (AASHTO M43) STONE".

STORMTECH COMPACTION REQUIREMENTS ARE MET FOR 'A' LOCATION MATERIALS WHEN PLACED AND COMPACTED IN 9" (230 mm) (MAX) LIFTS USING TWO FULL COVERAGES WITH A VIBRATORY COMPACTOR. 2.

WHERE INFILTRATION SURFACES MAY BE COMPROMISED BY COMPACTION, FOR STANDARD DESIGN LOAD CONDITIONS, A FLAT SURFACE MAY BE ACHIEVED BY RAKING OR DRAGGING WITHOUT COMPACTION EQUIPMENT. FOR SPECIAL LOAD DESIGNS, CONTACT STORMTECH FOR COMPACTION REQUIREMENTS

4. ONCE LAYER 'C' IS PLACED, ANY SOIL/MATERIAL CAN BE PLACED IN LAYER 'D' UP TO THE FINISHED GRADE. MOST PAVEMENT SUBBASE SOILS CAN BE USED TO REPLACE THE MATERIAL REQUIREMENTS OF LAYER 'C' OR 'D' AT THE SITE DESIGN ENGINEER'S DISCRETION.



CROSSROADS MIXED USE FILING NO. 1 SPECIFIC CROSS SECTION

NOTES:

- 1. CHAMBERS SHALL MEET THE REQUIREMENTS OF ASTM F2418, "STANDARD SPECIFICATION FOR POLYPROPYLENE (PP) CORRUGATED WALL STORMWATER COLLECTION CHAMBERS" CHAMBER CLASSIFICATION 60x101
- 2. MC-7200 CHAMBERS SHALL BE DESIGNED IN ACCORDANCE WITH ASTM F2787 "STANDARD PRACTICE FOR STRUCTURAL DESIGN OF THERMOPLASTIC CORRUGATED WALL STORMWATER COLLECTION CHAMBERS".
- 3. THE SITE DESIGN ENGINEER IS RESPONSIBLE FOR ASSESSING THE BEARING RESISTANCE (ALLOWABLE BEARING CAPACITY) OF THE SUBGRADE SOILS AND THE DEPTH OF FOUNDATION STONE WITH CONSIDERATION FOR THE RANGE OF EXPECTED SOIL MOISTURE CONDITIONS.
- PERIMETER STONE MUST BE EXTENDED HORIZONTALLY TO THE EXCAVATION WALL FOR BOTH VERTICAL AND SLOPED EXCAVATION WALLS.
- 5. REQUIREMENTS FOR HANDLING AND INSTALLATION:
 - TO MAINTAIN THE WIDTH OF CHAMBERS DURING SHIPPING AND HANDLING, CHAMBERS SHALL HAVE INTEGRAL, INTERLOCKING STACKING LUGS.
 - TO ENSURE A SECURE JOINT DURING INSTALLATION AND BACKFILL, THE HEIGHT OF THE CHAMBER JOINT SHALL NOT BE LESS THAN 3".
 - TO ENSURE THE INTEGRITY OF THE ARCH SHAPE DURING INSTALLATION, a) THE ARCH STIFFNESS CONSTANT AS DEFINED IN SECTION 6.2.8 OF ASTM F2418 SHALL BE GREATER THAN OR EQUAL TO 500 LBS/FT/%. • AND b) TO RESIST CHAMBER DEFORMATION DURING INSTALLATION AT ELEVATED TEMPERATURES (ABOVE 73° F / 23° C), CHAMBERS SHALL BE PRODUCED FROM REFLECTIVE GOLD OR YELLOW COLORS.

CTION / DENSITY REQUIREMENT

E PER SITE DESIGN ENGINEER'S PLANS. PAVED ATIONS MAY HAVE STRINGENT MATERIAL AND PREPARATION REQUIREMENTS.

PACTIONS AFTER 24" (600 mm) OF MATERIAL OVER RS IS REACHED. COMPACT ADDITIONAL LAYERS IN MAX LIFTS TO A MIN. 95% PROCTOR DENSITY FOR DED MATERIAL AND 95% RELATIVE DENSITY FOR PROCESSED AGGREGATE MATERIALS.

ON REQUIRED. SEE SPECIAL REQUIREMENTS ON LAYOUT PAGE.

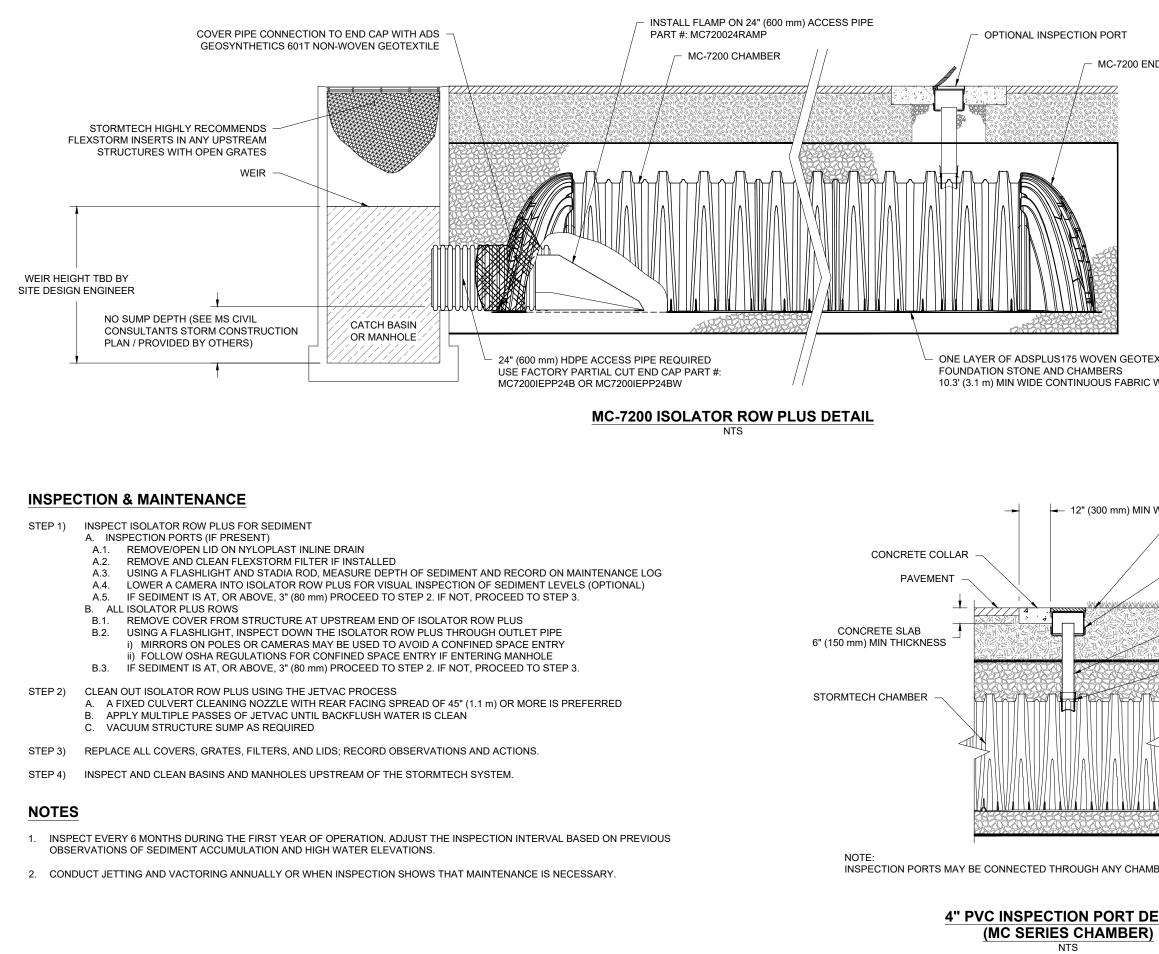
MPACT OR ROLL TO ACHIEVE A FLAT SURFACE.^{2,3}

	+
⊺ 24" 0 mm) MIN*	6300.52± MAXIMUM GRADE PER ENGINEER'S PLAN
	!

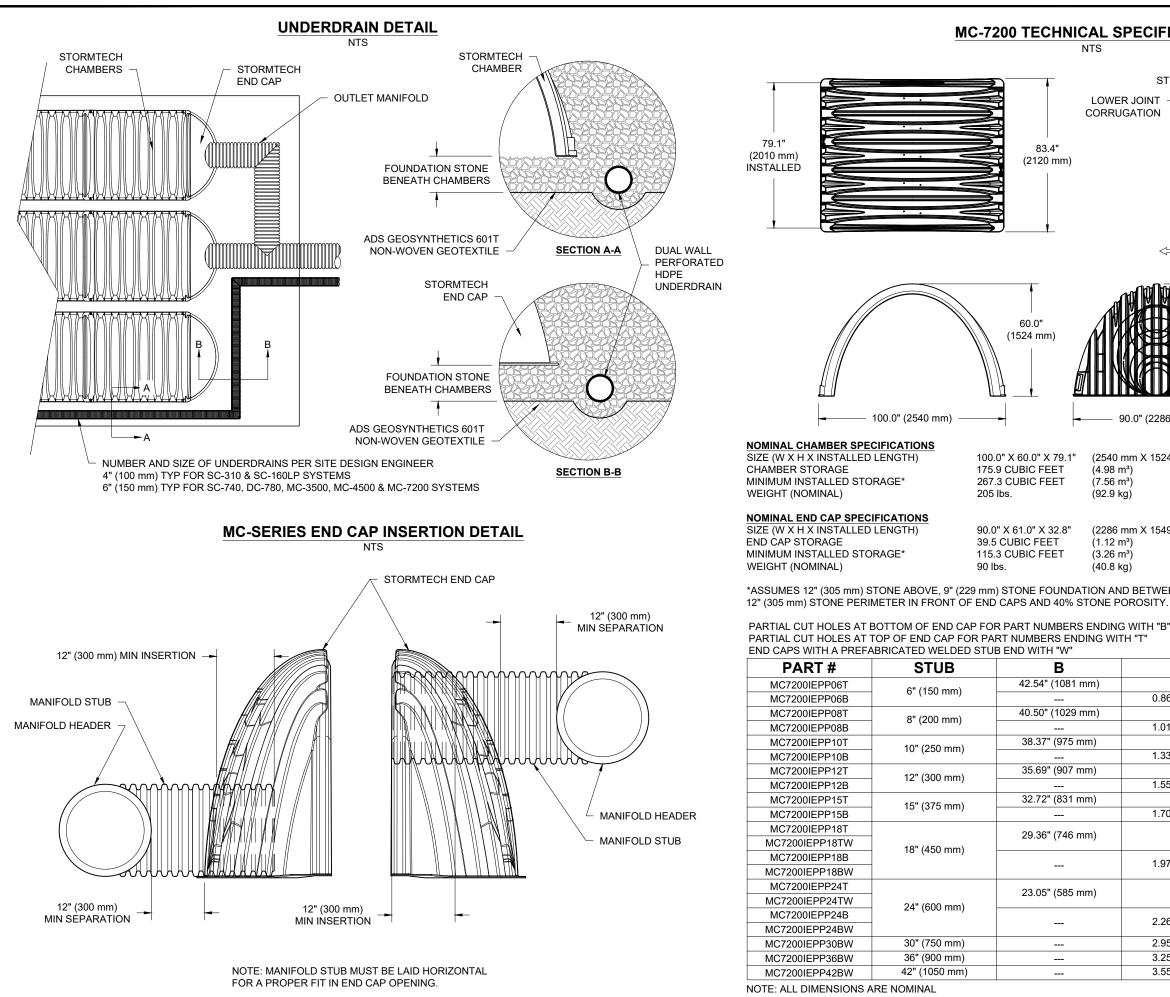
**THIS CROSS SECTION DETAIL REPRESENTS MINIMUM REQUIREMENTS FOR INSTALLATION. PLEASE SEE THE LAYOUT SHEET(S) FOR PROJECT SPECIFIC REQUIREMENTS.

DEPTH OF STONE TO BE DETERMINED BY SITE DESIGN ENGINEER 9" (230 mm) MIN 12" OF STONE UNDERNEATH THE CHAMBERS WITH ONE LAYER OF **TENSAR NX 850 GEOGRID BELOW** THE STONE THE SUBGRADE WILL STILL NEED TO BE PREPARED IN ACCORDANCES WITH THE **RECOMMENDATIONS OF THE** PROJECTS GEOTECHNICAL REPORT

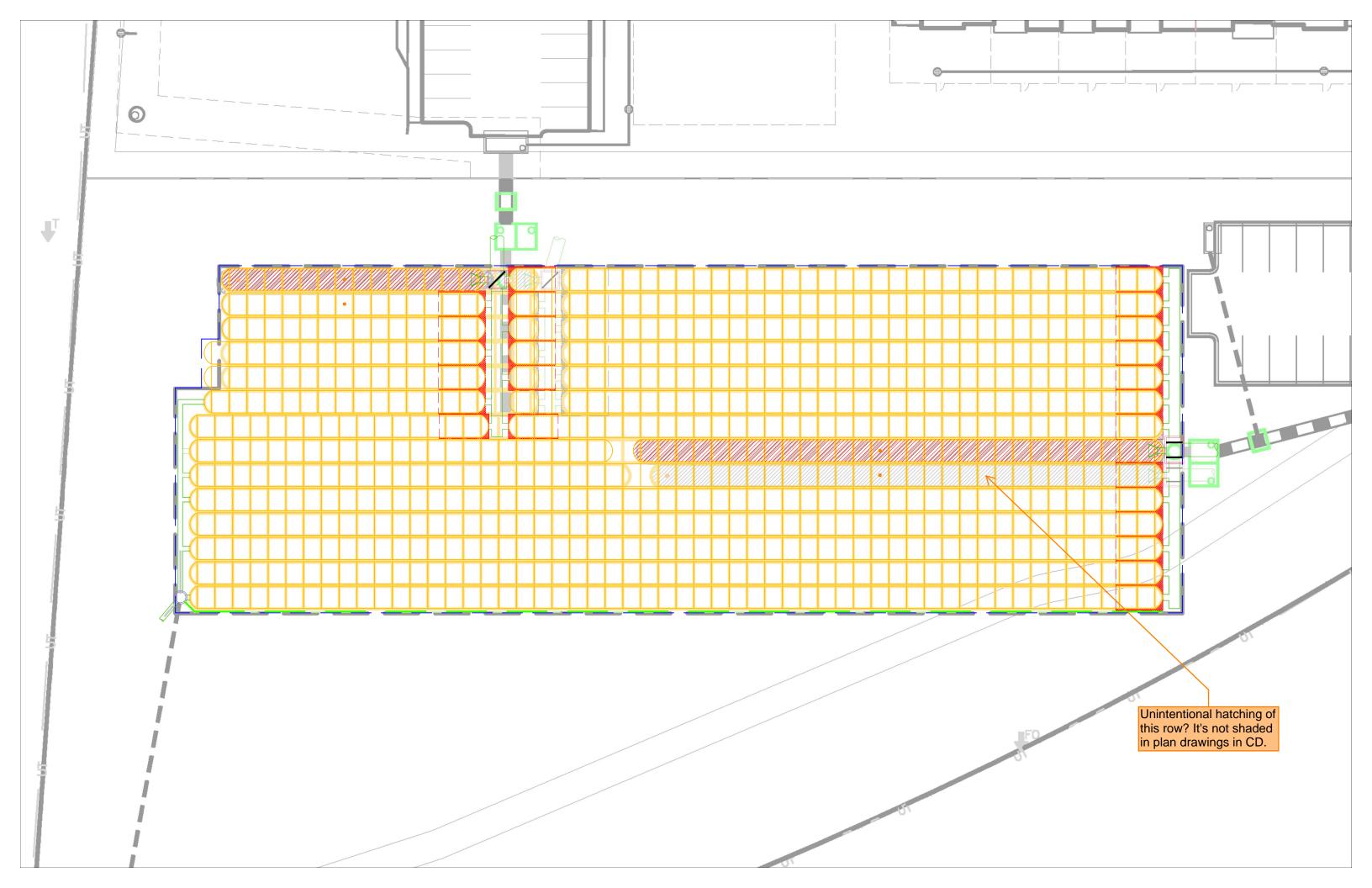
							CROSSROADS MIXED USF
3		4640 TRUEMAN BLVD					
•	R	HILLIARD, OH 43026	StormTach®				FILING NO. 1
	E			03/17/23 M	WH MWH REVISED	MWH MWH REVISED PER COMMENTS, TIER 1	COLORADO SPRINGS, CO
			Chamber System	12-18-22 RI	RKC JKL UPDATED ELEVATIONS		
				12/13/22 Bh	1W JPR ELEVATIO	12/13/22 BMW JPR ELEVATION AND LAYOUT ADJUSTMENTS	
			888-892-2694 WWW.STORMTECH.COM	DATE DRWN CHKD	WN CHKD		PROJECT #: S295850 CHECKED: CTS
5	THIS DRAWING HAS BEEN PRI RESPONSIBILITY OF THE SITE	EPARED BASED ON INFORMATION PROV DESIGN ENGINEER TO ENSURE THAT TI	THIS DRAWING HAS BEEN PREPARED BASED ON INFORMATION PROVIDED TO ADS UNDER THE DIRECTION OF THE SITE DESIGN ENGINEER OR OTHER PROJECT REPRESENTATIVE. THE SITE DESIGN ENGINE RESPONSIBILITY OF THE SITE DESIGN ENGINEER TO ENSURE THAT THE PRODUCT(S) DEPICTED AND ALL ASSOCIATED DETAILS MEET ALL APPLICABLE LAWS, REGULATIONS, AND PROJECT REQUIREMENTS.	ER OR OTHER F	ROJECT REPRESEN AWS, REGULATIONS	ITATIVE. THE SITE DESIGN ENGINEER SHALL 3, AND PROJECT REQUIREMENTS.	THIS DRAWING HAS BEEN PREPARED BASED ON INFORMATION PROVIDED TO ADS UNDER THE DIRECTION OF THE SITE DESIGN ENGINEER OR OTHER PROJECT REPRESENTATIVE. THE SITE DESIGN ENGINEER TO ENSTRUCTION. IT IS THE ULTIMATE RESPONSIBILITY OF THE SITE DESIGN ENGINEER TO ENSURE THAT THE PRODUCT(S) DEPICIED AND ALL ASSOCIATED DETALLS MEET ALL APPLICABLE LAWS, REGULATIONS, AND PROJECT REQUIREMENTS.



							E
ID CAP	CROSSROADS MIXED USE	FILING NO. 1	COLORADO SPRINGS, CO	DATE: 05-05-22 DRAWN: TSG		PROJECT #: S295850 CHECKED: CTS	VLL REVIEW THIS DRAWING PRIOR TO CONSTRUCTION. IT IS THE ULTIM
XTILE BETWEEN WITHOUT SEAMS			03/17/23 MWH MWH REVISED PER COMMENTS, TIER 1	12-18-22 RKC JKL UPDATED ELEVATIONS	12/13/22 BMW JPR ELEVATION AND LAYOUT ADJUSTMENTS	DATE DRWN CHKD DESCRIPTION	HE SITE DESIGN ENGINEER OR OTHER PROJECT REPRESENTATIVE. THE SITE DESIGN ENGINEER SHALL REVIEW THIS DRAWING PRIOR TO CONSTRUCTION. IT IS THE ULTIMATI MATED DETAILS MEET ALL APPLICABLE LAWS, REGULATIONS, AND PROJECT REQUIREMENTS.
WIDTH CONCRETE COLLAR NOT REQUIRED FOR UNPAVED APPLICATIONS 8" NYLOPLAST INSPECTION PORT BODY (PART# 2708AG4IPKIT) OR TRAFFIC RATED BOX W/SOLID LOCKING COVER 4" (100 mm) SDR 35 PIPE 4" (100 mm) INSERTA TEE TO BE CENTERED ON CORRUGATION VALLEY		Ctorm Toch®		Chamber System		888-892-2694 WWW.STORMTECH.COM	
BER CORRUGATION VALLEY.		464U I KUEMAN BLVD HILLIARD. OH 43026					THIS DRAWING HAS BEEN PREPARED BASED ON INFORMATION PROVIDED TO ADS UNDER THE DIRECTION OF TI RESPONSIBILITY OF THE SITE DESIGN ENGINEER TO ENSURE THAT THE PRODUCITES DEPICTED AND ALL ASSOC
	4	1					<u>⊧</u> ≞ 5



CATION VALLEY CREST FFENING RIB WEB	S MIXED USE NO. 1 SPRINGS, CO DRAWN: TSG CHECKED: CTS
CORRUGATION CREST STIFFENING RIB BUILD ROW IN THIS DIRECTION	CROSSROADS MIXED USE FILING NO. 1 COLORADO SPRINGS, CO DATE: 05-05-22 DRAWN: TSG PROJECT #: S295850 CHECKED: CTS
61.0" (833 mm) (1549 mm) INSTALLED	REVISED PER COMMENTS, TIER 1 UPDATED ELEVATIONS ELEVATION AND LAYOUT ADJUSTMENTS DESCRIPTION
nm) nm X 2010 mm) 38.0"	03/17/23 MWH MWH REV 12/18-22 RKC JKL UP 12/18-22 BMW JPR ELE DATE DRWN CHKO
mm X 833 mm) (965 mm) (965 mm) (965 mm) (965 mm)	StormTech [®] Chamber System 888-892-2694 WWW.STORMTECH.COM
 (34 mm) (39 mm) 	4640 TRUEMAN BLVD HILLIARD, OH 43026
(43 mm) CUSTOM PREFABRICATED INVERTS ARE AVAILABLE UPON REQUEST. INVENTORIED MANIFOLDS INCLUDE 12-24" (300-600 mm) SIZE ON SIZE AND 15-48" (375-1200 mm) ECCENTRIC MANIFOLDS. CUSTOM INVERT LOCATIONS ON THE MC-7200 END CAP CUT IN THE FIELD ARE NOT RECOMMENDED FOR PIPE SIZES GREATER THAN 10" (250 mm). THE INVERT LOCATION IN COLUMN 'B'	46 HI



PRO	JECT INFORMATION
ENGINEERED PRODUCT MANAGER:	JEROME MAGSINO 303-349-7555 JEROME.MAGSINO@ADSPIPE.COM
ADS SALES REP:	AARON ZEE AARON.ZEE@ADSPIPE.COM
PROJECT NO:	S295850



CROSSROADS MIXED USE FILING NO. 1 COLORADO SPRINGS, CO

BAYSAVER BAYSEPARATOR SPECIFICATIONS

MATERIALS AND DESIGN

- CONCRETE STRUCTURES SHALL BE DESIGNED FOR H-20 TRAFFIC LOADING AND APPLICABLE SOIL LOADS OR AS OTHERWISE DETERMINED BY A LICENSED PROFESSIONAL ENGINEER. THE MATERIALS AND STRUCTURAL DESIGN OF THE DEVICES SHALL BE PER ASTM C857 AND ASTM C858.
 - THE MINIMUM COMPRESSIVE STRENGTH OF THE CONCRETE IN THE MANHOLE BASE, RISER, AND TOP SECTIONS SHALL BE 4000 PSI.
- 2. THE MINIMUM WALL THICKNESS SHALL BE ONE TWELFTH OF THE INTERNAL DIAMETER OF THE RISER OF LARGEST CONE DIAMETER.
- CEMENT SHALL CONFORM TO THE REQUIREMENTS FOR PORTLAND CEMENT OF SPECIFICATION C150. 3.
- AGGREGATES SHALL CONFORM TO SPECIFICATION C33, EXCEPT THAT THE REQUIREMENT FOR GRADATION SHALL NOT APPLY.
- REINFORCEMENT SHALL CONSIST OF WIRE CONFORMING TO SPECIFICATION A82 OR SPECIFICATION A496, OF WIRE FABRIC CONFORMING 5 TO SPECIFICATION A185 OR SPECIFICATION A497, OR OF BARS OF GRADE 40 STEEL CONFORMING TO SPECIFICATION A615/A615M. THE ACCESS COVER SHALL BE DESIGNED FOR HS20-44 TRAFFIC LOADING AND SHALL PROVIDE A MINIMUM 30 INCH CLEAR OPENING.
- 6.
- ALL JOINTS SHALL BE WATERPROOF WITH WRAPPED GASKETS OR SEALED WITH A MASTIC TREATMENT. 8 ANY GROUT USED WITHIN THE SYSTEM SHALL MEET THE ASTM C 1107 "STANDARD SPECIFICATION FOR PACKAGED DRY.
- HYDRAULIC-CEMENT GROUT (NON-SHRINK)". GRADES A, B AND C AT A POURABLE AND PLASTIC CONSISTENCY AT 70°F. CRD C 621 "CORPS OF ENGINEERS SPECIFICATION FOR NON-SHRINK GROUT."
- STORAGE MANHOLE CONNECTOR PIPES SHALL BE EQUIPPED WITH A SEAL GASKET THAT MEETS OR EXCEEDS MATERIAL SPECIFICATIONS 9 OF ASTM C-923 OR OTHER LOCALLY APPROVED METHODS.
- THE SEPARATOR STRUCTURE SHALL BE SUBSTANTIALLY CONSTRUCTED OF HDPE OR EQUIVALENT CORROSION RESISTANT MATERIAL MEETING R ASTM D330, ASTM F412, AND ASTM C-425.
- PIPES WITHIN THE UNIT, (I.E., TEE PIPES, CONNECTOR PIPES AND DOWN PIPES) SHALL BE CONSTRUCTED OF AT LEAST SDR 32.5 HDPE PIPE OF C STANDARD ASTM F412
- PIPE AND FITTING MATERIAL SHALL BE HIGH DENSITY POLYETHYLENE MEETING ASTM D330 MINIMUM CELL CLASSIFICATION 335400C FOR 24-INCH D THROUGH 60-INCH DIAMETERS. THE 24- THROUGH 60-INCH PIPE MATERIAL SHALL BE SLOW CRACK RESISTANT HDPE MATERIAL, EVALUATED USING THE SINGLE POINT NOTCHED CONSTANT TENSILE LOAD (SP-NCTL) TEST.

PERFORMANCE

- THE STORMWATER TREATMENT UNIT SHALL BE AN ONLINE UNIT CAPABLE OF CONVEYING 100% OF THE DESIGN PEAK FLOW. Α
- THE BAYSEPARATOR UNIT SHALL BE DESIGNED TO REMOVE AT LEAST 80% OF THE SUSPENDED SOLIDS LOAD ON AN ANNUAL AGGREGATE B. REMOVAL BASIS. SAID REMOVAL SHALL BE BASED ON FULL-SCALE THIRD PARTY TESTING USING F-95 MEDIA GRADATION (MANUFACTURED BY US SILICA) OR EQUIVALENT. SAID FULL SCALE TESTING SHALL HAVE INCLUDED SEDIMENT CAPTURE BASED ON ACTUAL TOTAL MASS COLLECTED BY THE STORMWATER TREATMENT UNIT(S).
- THE STORMWATER TREATMENT UNIT SHALL CONSIST OF ONE (1) PREFABRICATED SEPARATOR STRUCTURE, ONE (1) ONLINE COARSE SEDIMENT С CAPTURE STRUCTURE, AND ONE (1) OFFLINE SEDIMENT AND FLOATABLE CAPTURE STRUCTURE. THE SEPARATOR STRUCTURE SHALL BE SUBSTANTIALLY CONSTRUCTED OF HDPE OR EQUIVALENT CORROSION RESISTANT MATERIAL. THE OFFLINE SEDIMENT STORAGE STRUCTURE MUST PROVIDE FOR OFFLINE SEDIMENT STORAGE OF SEDIMENTS AND FLOATABLES THAT ARE ISOLATED FROM HIGH INTENSITY STORMS.
- D THE STORMWATER TREATMENT UNIT(S) HEAD LOSS AT THE PEAK DESIGN FLOW RATE SHALL NOT EXCEED THE HEAD LOSS SPECIFIED BY THE ENGINEER.
- THE UNIT SHALL BE DESIGNED TO REMOVE SEDIMENT PARTICLES AS WELL AS FLOATING OILS AND DEBRIS F

MANUFACTURER

- THE STORMWATER TREATMENT UNIT(S) SHALL BE OF A BASIC DESIGN THAT HAS BEEN INSTALLED AND USED SUCCESSFULLY FOR A MINIMUM OF 5 Α. YFARS
- EACH STORMWATER TREATMENT SYSTEM SHALL BE A BAYSEPARATOR SYSTEM AS MANUFACTURED BY BAYSAVER. LLC. 1030 DEER HOLLOW DR.. в MOUNT AIRY, MD 21771, PHONE (301) 829-6470, FAX (301-829-3747, TOLL FREE 1-800-229-7283 (1-800-BAYSAVER), EMAIL INFO@BAYSAVER.COM PROTECTED UNDER US PATENT NUMBER 5746911

BAYSEPARATOR MAINTENANCE

BAYSEPARATOR SYSTEMS MUST BE INSPECTED AND MAINTAINED PERIODICALLY. INSPECTION IS MADE BY CHECKING THE DEPTH OF SEDIMENT IN EACH MANHOLE WITH A GRADE STICK OR SIMILAR DEVICE. MAINTENANCE IS REQUIRED WHEN THE SEDIMENT DEPTH IN EITHER MANHOLE EXCEEDS 2 FEET. MINIMUM INSPECTION IS RECOMMENDED TWICE A YEAR TO MAINTAIN OPERATION AND FUNCTION OF BAYSAVER.

MAINTENANCE CONSISTS OF THE FOLLOWING:

A. STORAGE MANHOLE

- REMOVE THE ENTIRE VOLUME OF THE CONTAMINATED WATER BY VACUUM TRUCK.
- 2 VACUUM TRUCK. MAKE CERTAIN MANHOLE IS CLEAN.

B. PRIMARY MANHOLE

- MANHOLE UNTIL THE WATER LEVEL FALLS TO 1 FOOT ABOVE THE SEDIMENT LAYER. REMOVE THE SETTLED SEDIMENT AND REMAINING WATER BY VACUUM TRUCK.
- 3 VACUUM TRUCK. MAKE CERTAIN MANHOLE IS CLEAN.
- Λ OF THE VACUUM TRUCK.

BAYSEPARATOR INSTALLATION NOTES

- EXCAVATION MUST PROVIDE ADEQUATE SPACE TO CONNECT INLET AND OUTLET PIPES TO STORAGE MANHOLE AND BAYSEPARATOR 1 UNIT. INSTALL PRECAST DROP STRUCTURES ON SOLID GROUND AS VERIFIED BY A GEOTECHNICAL ENGINEER.
- 2 3.
- 4 ENGINEER
- 5 REDUCER/ADAPTER. CUT EXCESS LENGTH OFF CONNECTING PIPES INSIDE STORAGE MANHOLE.
- 6 #7, OR PEA GRAVEL
- INSTALL AND SET MANHOLE COVER GRADE ADJUSTMENT RINGS AS NECESSARY. 7
- INSTALL AND SET MANHOLE FRAME AND COVER UNITS.

INSTALL BAYSEPARATOR UNIT AND CONNECTING PIPES. SEAL ALL CONNECTING JOINTS AND INSTALL SEPARATOR HDPE BACKFILL SEPARATOR UNIT AND MANHOLES. AREAS NOT ACCESSIBLE TO COMPACTION EQUIPMENT MUST BE BACKFILLED WITH #57,

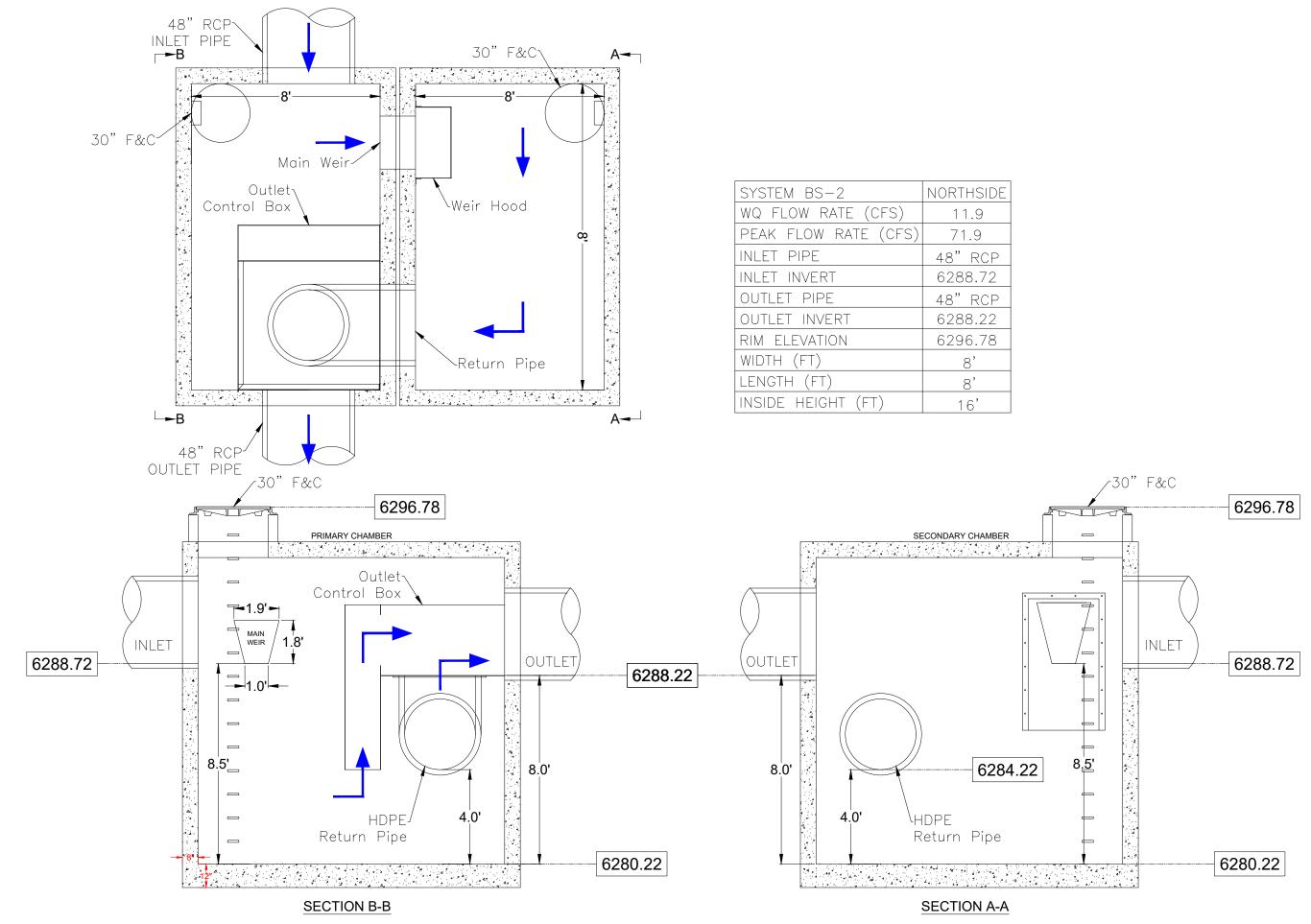
VERIFY THE SUBGRADE ELEVATION AGAINST THE MANHOLE DIMENSIONS AND CONNECTING STORM DRAIN INVERTS MAKING SURE THE BASES ARE LEVEL AND THE STORAGE MANHOLE OPENINGS ARE ALIGNED WITH THE SEPARATOR UNIT, INSTALL PRIMARY AND STORAGE MANHOLES. INSTALL WATERTIGHT GASKETS ON BASE UNITS AND COAT WITH LUBRICATING GREASE (IF REQUIRED). INSTALL ADDITIONAL MANHOLE SECTIONS AS REQUIRED. SEAL LIFT HOLES WITH NON-SHRINK GROUT. BACKFILL BASE SECTIONS OF MANHOLES TO INVERT OF STORAGE MANHOLE CONNECTING PIPES. USING APPROVED BACKFILL MATERIAL, BACKFILL AND COMPACT IN 8 INCH LIFTS. BACKFILL AND COMPACTION SHOULD BE MONITORED BY A GEOTECHNICAL

CONTAMINATED MATERIAL REMOVED FROM THE MANHOLES MUST BE DISPOSED OF RESPONSIBLY AND LEGALLY BY THE OPERATOR

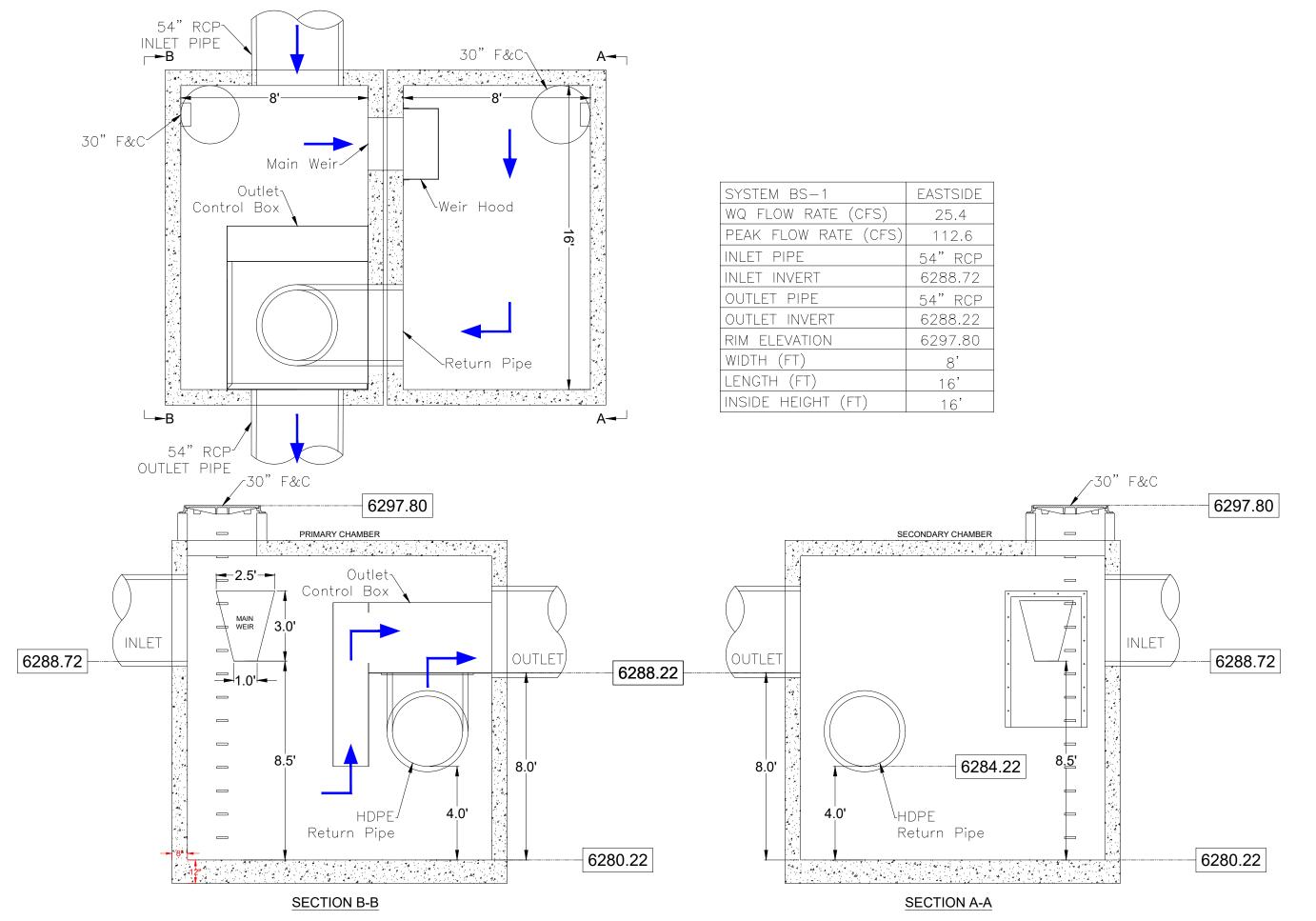
CLEAN THE MANHOLE WALLS AND FLUSH OUT THE MANHOLE USING A HIGH PRESSURE HOSE AND REMOVE FLUSHING WATER BY

USING A SUBMERSIBLE PUMP. PUMP THE CLEAN WATER FROM THE CENTER OF THE MANHOLE DIRECTLY INTO THE EMPTY STORAGE

CLEAN THE MANHOLE WALLS AND FLUSH OUT THE MANHOLE USING A HIGH PRESSURE HOSE AND REMOVE FLUSHING WATER BY

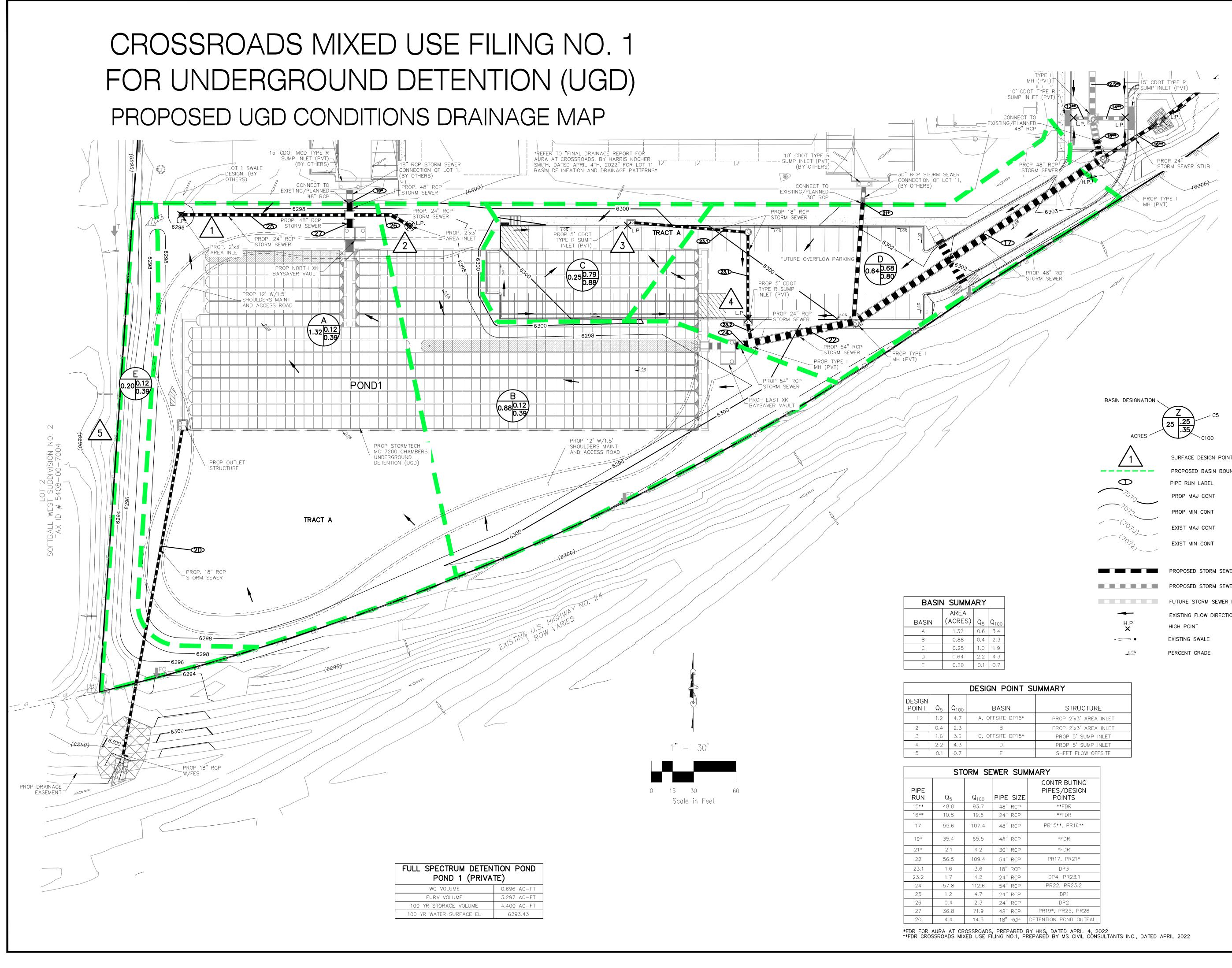


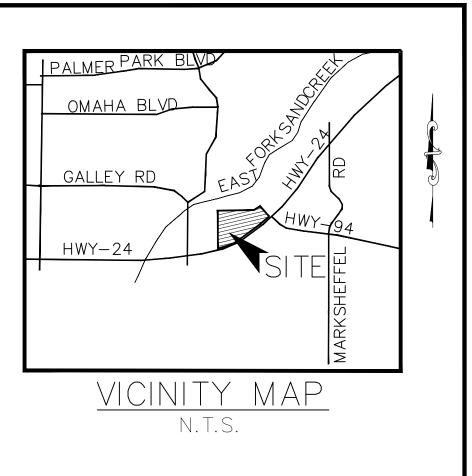
MMMS 4640 TRUEMAN BLVD HILLIARD, OH 43026 A640 TRUEMAN BLVD CROSSROADS MIXED USE FILING NO. 1 MMMS Affaired of the construction of the constructing of the construction of the construction of the constr		00.12	96.78				
Stormwater Treatment System 23/17/23 PR PR CITYS COMMENTS. DEFENDING PREVISED FLOW RATES AND ADDED DETAILS PER 14/23 PR REVISED SIZING, PIPE SIZES & ELEVATIONS. PACUEC DATE DATE DATE DEVISED SIZING, PIPE SIZES & ELEVATIONS. PROJEC		RUEMAN BLVD 3D, OH 43026	BavSeparator			CROSSROADS MIXI	ED USE FILING NO.
TIAI23 PR PR REVISED SIZING, PIPE SIZES & ELEVATIONS. UALLE: 12/21/22 Date Drawn CHKD DESCRIPTION PROJECT #: S295850			Stormwater Treatment System	R	D FLOW RATES AND ADDED DETAILS PER		SPRINGS, CO
DATE DRWN CHKD DESCRIPTION PROJECT #: S295850	NOT TO SC	AI F		РК) SIZING, PIPE SIZES & ELEVATIONS.		UKAWN:
]		RWN CHKD	DESCRIPTION	PROJECT #: \$295850	CHECKED: PR



3				CROSSROADS MIXED USE FILING NO. 1
sн С		BaySeparator		COLORADO SPRINGS, CO
EET		stormwater I reatment System	03/17/23 PR PR REVISED FLOW RATES AND ADDED DETAILS PEK 1/4/23 PR PR REVISED STZNG PIPE SIZES & FLEVATIONS	DATE: 12/21/22 DRAWN: PR
			DRWN CHKD	PROJECT #: S295850 CHECKED: PR
3	THIS DRAWING HAS BEEN PREPARED BASED ON INFORMATION PROVIDED TO ADS UNDER THE DIRECTION OF ULTIMATE RESPONSIBILITY OF THE SITE DESIGN ENGINEER TO ENSURE THAT THE PRODUCT(S) DEPICTED AN	VIDED TO ADS UNDER THE DIRECTION OF THE SITE DESIGN ENGIN. JRE THAT THE PRODUCT(S) DEPICTED AND ALL ASSOCIATED DETA.	THIS DRAWING HAS BEEN PREPARED BASED ON INFORMATION PROVIDED TO ADS UNDER THE DIRECTION OF THE SITE DESIGN ENGINEER OR OTHER PROJECT REPRESENTATIVE. THE SITE DESIGN ENGINEER 20 NO INFORMATION PROVIDED TO ADS UNDER THAT THE PRODUCT(S) DEPICTED AND ALL APPLICABLE LAWS, REGULATIONS, AND PROJECT REQUIREMENTS.	LL REVIEW THIS DRAWING PRIOR TO CONSTRUCTION. IT IS THE 'S'

FINAL DRAINAGE REPORT CROSSROADS MIXED USE FILING NO. 1 UNDERGROUND DETENTION – PROPOSED DRAINAGE MAP





SITE BOUNDARY

STORM SEWER LINE

EX. WATER LINE

LOT NUMBER

EX. SANITARY SEWER LINE

EX. STORM SEWER LINE

EX. IRRIGATION VALVE

EX. TELEPHONE PEDESTAL

EX. ELECTRIC VAULT EX. SANITARY MANHOLE

EX. WATER VALVE

PROPOSED RIPRAP

PROPOSED SWALE

LOW POINT

EMERGENCY OVERFLOW DIRECTION

EX. STORM INLET EX. GAS TEST NODE

_OT LINE

PROPOSED UTILITY EASEMENT PROPOSED DRAINAGE EASEMEN

PROPOSED LANDSCAPE EASEMENT

EX. UNDERGROUND ELECTRIC LINE

<u>LEGEND</u>

PROPOSED BASIN BOUNDARY	UE SS
	WL
PROP MAJ CONT	ST
PROP MIN CONT	9 (ICV)
EXIST MAJ CONT	ST
EXIST MIN CONT	G
	EVL
PROPOSED STORM SEWER PIPE	(SS)
PROPOSED STORM SEWER PIPE (OTHERS)	7505050505050505 7505050505050505
FUTURE STORM SEWER PIPE	
EXISTING FLOW DIRECTION ARROW	L.P.
HIGH POINT	×
EXISTING SWALE	~ ••

STRUCTURE
prop 2'x3' area inlet
PROP 2'x3' AREA INLET
PROP 5' SUMP INLET
PROP 5' SUMP INLET
SUFET ELOW AFESITE

V	IMARY
	PIPES/DESIGN POINTS
	**FDR
	**FDR
	PR15**, PR16**
	*FDR
	*FDR
	PR17, PR21*
	DP3
	DP4, PR23.1
	PR22, PR23.2
	DP1
	DP2
	PR19*, PR25, PR26
	DETENTION POND OUTFALL

PROPOSED DRAINAGE MAP CROSSROADS MIXED USE FILING NO.1 FOR UGD JOB NO. 18-003 DATE PREPARED: FEBRUARY 14, 2022

212 N. WAHSATCH AVE., STE 305 COLORADO SPRINGS, CO 80903 PHONE: 719.955.5485

PCD FILING NO: CDR232

DATE REVISED:

SHEET 1 OF 1