

**FINAL DRAINAGE REPORT FOR
TRACT IN NE4NW4 SEC 18-14-65
2601 EAST PLATTE AVENUE
COLORADO SPRINGS, COLORADO 80916**

JULY, 2021

Prepared For:

T-BONE CONSTRUCTION, INC.
1310 Ford Street
Colorado Springs, CO 80915

Prepared By:

TERRA NOVA ENGINEERING, INC.
721 S. 23RD STREET
Colorado Springs, CO 80904
(719) 635-6422

Job No. 1895.00

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DRAINAGE REPORT STATEMENT

Design Engineer's Statement

This attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the County for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.

L DUCETT, P.E. 32339

Seal

Developers Statement

I, _____ the developer have read and will comply with all of the requirements specified in this drainage report and plan.

Business Name

By: _____

Title: _____

Address: _____

El Paso County Approval:

Filed in accordance with the requirements of the Drainage Criteria Manual, Volumes 1 & 2, El Paso County Engineering Criteria Manual and Land Development Code as amended.

Jennifer Irvine,

Date

County Engineer / ECM Administrator

Conditions:

Purpose

The purpose of this Final Drainage Report is to identify and analyze the existing and proposed drainage patterns, determine proposed runoff quantities, size drainage structures to safely convey the developed runoff, and present solutions to drainage impacts on-site and off-site resulting from this development.

General Description

This Final Drainage Report is an analysis of the development of TRACT IN NE4NW4 SEC 18-14-65 owned by HCD Properties, LLC. The site is located at 2601 East Platte Avenue, Colorado Springs, CO 80916 in Section 18, Township 14S, Range 65 West of the 6th Principal Meridian in El Paso County. The site is bounded on the west by a landscaping supply business, on the north by E Platte Avenue Frontage Road, on the east by an RV and boat storage business, and on the south by a vacant lot owned by the City of Colorado Springs. The site is currently unplatted.

The site is currently used primarily for the parking and storage of vehicles and heavy equipment with some areas of soil excavation and storage at the southern end.

The proposed development is the addition of a 22,479 square foot building near the centroid of the lot but this project also makes preparations for a future building to be placed near the front of the lot with all of the associated drives, utilities, grading, and stormwater features. The proposed building will be used to house a drilling company and includes a front office building with an asphalt parking lot and an attached industrial building with a surrounding gravel lot. The use of the future building will be established at a later time. The access will be from E Platte Avenue Frontage Road via two paved entrances.

The site lies within the Sand Creek Drainage Basin.

Soils Condition

The soil for this project is composed completely of Blakeland Loamy Sand per the “Soils Survey of El Paso County Area, which is in Hydrologic Soil Group A.

Drainage Criteria

Hydrologic and Hydraulic calculations were performed using the El Paso County Storm Drainage Design Criteria Manual Volumes 1 & 2, latest editions. The Rational Method was used to estimate storm water runoff and the design of the FSEDB was performed using UD-Detention v3.07.

Existing (Historic) Drainage Conditions

No previous drainage reports or studies could be found for this site. A drainage map for the existing conditions is included in the Appendix of this report. The site lies within the Sand Creek Basin. The existing topography has a relatively consistent 3% slope from the northeast to

the southwest but drops off more steeply at the western property line. The surface cover is composed of gravel lots and areas of disturbed ground with minimal vegetation.

Drainage ways for this site are poorly defined and runoff primarily sheet flows from the east/northeast to the west/southwest and leaves the site at three locations which are designated as Design Points (DP) for analysis. At the northwest property corner (DP X-1), runoff exits into the public drainage way along E Platte Avenue Frontage Road. At the west property line, about 250 feet south of the northwest property corner (DP X-2), runoff drains into a shallow swale and onto adjacent private property. Along the south side of the proposed development (DP X-3), runoff flows onto the same adjacent private property at a location approximately 500 feet south of DP X-2. At the southeast property line (DP X-4 & DP X-5), very small areas of runoff sheet flow onto Basin EX-C.

Basin EX-A contributes to DP X-1 and has an area of 1.10 acres consisting of gravel lots and areas of disturbed soil, generating runoff amounts of $Q_5 = 1.83$ cfs and $Q_{100} = 4.62$ cfs.

Basin EX-B contributes to DP X-2 and has an area of 2.10 acres consisting of gravel lots and areas of disturbed soil, generating runoff amounts of $Q_5 = 2.20$ cfs and $Q_{100} = 7.14$ cfs.

Basin EX-C contributes to DP X-3 and has an area of 0.30 acres consisting of areas of disturbed soil, generating runoff amounts of $Q_5 = 0.16$ cfs and $Q_{100} = 0.88$ cfs.

Basin OS-1 contributes to DP X-4 and has an area of 0.05 acres consisting of undeveloped land, generating runoff amounts of $Q_5 = 0.02$ cfs and $Q_{100} = 0.14$ cfs.

Basin OS-2 contributes to DP X-5 and has an area of 0.10 acres consisting of undeveloped land, generating runoff amounts of $Q_5 = 0.03$ cfs and $Q_{100} = 0.25$ cfs.

Developed Drainage Conditions

A drainage map for the proposed condition is included in the appendix of this report.

A Full Spectrum Extended Detention Basin (FSEDB) will be provided for the proposed and future development with a watershed area of 6.05 acres.

The proposed facility is comprised of asphalt parking lots, gravel lots, buildings, and landscaping. The drainage pattern for the site remains generally the same; however, the runoff of the proposed developed/impervious areas are routed to the FSEDB.

Runoff continues to exit into the public drainage way along E Platte Avenue Frontage Road at the northwest corner (DP 11). The area draining to this location is significantly reduced as compared to existing conditions.

Runoff is no longer discharged at design point X2 as it had been in the existing conditions.

The outlet of the FSEDB (DP 9) is the location at which runoff from the proposed development is discharged after treatment.

Basin A contributes to DP 1 and has an area of 1.36 acres consisting primarily of proposed paved and future building area with a small portion of landscaped area, generating runoff amounts of $Q_5 = 5.26$ cfs and $Q_{100} = 10.67$ cfs. Minor runoff is conveyed under the entrances at E Platte Avenue Frontage Road via 2 ft wide concrete trench drains just to the north of this basin. The

runoff is collected by a 8' D-10-R inlet at design point 1 and conveyed to the FSEDB via storm pipe.

Basin B contributes to DP 2 and has an area of 0.71 acres consisting mostly of paved areas and much smaller areas of lawn/landscaping, generating runoff amounts of $Q_5 = 2.58$ cfs and $Q_{100} = 5.35$ cfs. The runoff is collected by a type C inlet at design point 2 and conveyed to the FSEDB via storm pipe.

Basin C contributes to DP 3 and has an area of 0.54 acres consisting of paved area, building, gravel lot, and lawn/landscaping, generating runoff amounts of $Q_5 = 1.59$ cfs and $Q_{100} = 3.47$ cfs. The runoff sheet flows and travels by a 2' concrete pan to a type C inlet at design point 3 and then conveyed to the FSEDB via storm pipe.

Basin D contributes to DP 4 and has an area of 0.26 acres consisting of building, paved area, gravel lot, and lawn/landscaping, generating runoff amounts of $Q_5 = 0.82$ cfs and $Q_{100} = 1.74$ cfs. The runoff is collected by an inlet at design point 4 and conveyed to the FSEDB via storm pipe.

Basin E contributes to DP 5 and has an area of 0.35 acres consisting of building, paved area, and gravel lot, generating runoff amounts of $Q_5 = 1.20$ cfs and $Q_{100} = 2.48$ cfs. The runoff is collected by an inlet at design point 5 and conveyed to the FSEDB via storm pipe.

Basin F contributes to DP 6 and has an area of 0.29 acres consisting of building, paved area, and gravel lot, generating runoff amounts of $Q_5 = 1.03$ cfs and $Q_{100} = 2.10$ cfs. The runoff is collected by an inlet at design point 6 and conveyed to the FSEDB via storm pipe.

Basin G contributes to DP 7 and has an area of 0.35 acres consisting of building, paved area, and gravel lot, generating runoff amounts of $Q_5 = 1.20$ cfs and $Q_{100} = 2.48$ cfs. The runoff is collected by an inlet at design point 7 and conveyed to the FSEDB via storm pipe.

Basin H contributes to DP 8 and has an area of 0.20 acres consisting of building, paved area, and gravel lot, generating runoff amounts of $Q_5 = 0.71$ cfs and $Q_{100} = 1.46$ cfs. The runoff is collected by an inlet at design point 8 and conveyed to the FSEDB via storm pipe.

Basin I contributes to DP 9 and has an area of 0.96 acres consisting of grading needed for the construction of the FSEDB and other landscaped area generating runoff amounts of $Q_5 = 0.26$ cfs and $Q_{100} = 1.95$ cfs. No new impervious area is being added and the ground cover will be improved from gravel and disturbed soil to maintained landscaping; therefore, the area does not require treatment in the FSEDB. The runoff sheet flows to onto adjacent property at design point 9 as in existing conditions.

Basin J contributes to DP 10 and has an area of 1.82 acres consisting of the FSEDB, some paved area, gravel lot, and landscaped area, generating runoff amounts of $Q_5 = 1.81$ cfs and $Q_{100} = 5.37$ cfs. The runoff sheet flows towards the FSEDB located at design point 10.

Basin K is the small area that continues to exit into the public drainage way along E Platte Avenue Frontage Road at the northwest corner (DP 11) as it had previously. The area and runoff of this basin is significantly reduced as compared to existing conditions. It generates runoff amounts of $Q_5 = 0.09$ cfs and $Q_{100} = 0.45$.

Basin L contributes to DP 12 and has an area of 0.06 acres consisting of building, paved area, and gravel lot, generating runoff amounts of $Q_5 = 0.23$ cfs and $Q_{100} = 0.47$ cfs. The runoff is collected by an inlet at design point 12 and conveyed to the FSEDB via storm pipe.

Basin M contributes to DP 13 and has an area of 0.06 acres consisting of building, paved area, and gravel lot, generating runoff amounts of $Q_5 = 0.19$ cfs and $Q_{100} = 0.41$ cfs. The runoff is collected by an inlet at design point 13 and conveyed to the FSEDB via storm pipe.

Basins OS-1 & OS-2 remain as they had previously.

FSEDB

In an effort to protect receiving water and as part of the “four step process to minimize adverse impacts of urbanization” this site was analyzed in the following manner:

1. Reduce Runoff – the nature of the development precludes reducing runoff as most of the site is used for buildings, asphalt lots, and gravel lots.
2. Treat Slowly Release WQCV – the FSEDB is designed to capture and treat the runoff from the proposed development in the appropriate manner.
3. Stabilize Stream Channels – there are no existing streams associated with this site.
4. Source Controls – given that the site will be used to house a drilling company, the presence of fuel and other contaminants are likely; therefore, spill kits should be kept on site and any outdoor storage of industrial materials should include the appropriate safeguards.

The runoff from Basins A, B, C, D, E, F, G, H, J, L, M, & OS-1 of the proposed development are routed to the proposed 2.235 ac-ft private FSEDB located at the southern portion of the property at DP 10. The FSEDB treats runoff from a combined watershed area of 6.05 acres with an imperviousness of 65.3%. The elevation of the bottom of the pond is 6243.00 and the top of the berm is at 6252.00. The pond design has a WQCV storage volume of 0.129 ac-ft at a water surface elevation of 6245.20. The EURV storage volume is 0.362 ac-ft at a water surface elevation of 6246.82. The 100-year storage volume of 0.240 ac-ft corresponds to a water surface of 6247.71. The WQCV discharge is less than 0.1 cfs and will be fully released in 40 hours. The EURV discharge is 0.2 cfs and will fully released in 72 hours. The 100 year outflow is 3.5 cfs and is fully released in 73 hours.

The forebay exceeds the size requirement of 2% of the WQCV volume of 0.129 ac-ft. A Trickle channel 2 ft wide and 0.5 ft deep at 0.54% slope runs from the forebay to the micropool at the FSEDB outlet structure. The outlet structure is a 2.0 ft by 2.0 ft riser box with the inlet invert set at 6243.00 and the top of grate set at elevation 6246.82. A metal orifice plate on the front of the structure regulates the WQCV and EURV via three orifices with 0.7 square inches, 0.7 square inches, and 4 square inches spaced 1.27 ft apart. The invert of 18” outlet pipe is at elevation 6242.75 with a restrictor plate set 4.5 inches higher. The outlet pipe is 82 ft long at a slope of 1.12% with a metal end section at the outlet end with type L riprap protection ($D_{50} = 12$ in).

An emergency spillway is set at elevation 6249.00. The spillway has a bottom width of 8 ft with 4:1 side slopes and is protected by type VL riprap ($D_{50} = 12$ in). The 100 year HWL is 1.29 feet below the spillway. In an emergency overflow situation, the runoff will flow onto the property south of the site.

Floodplain Statement

According to FEMA's FIRM No. 08041CO754G (eff. 12/7/2018), the proposed development is within an area designated as Zone X, having minimal flood hazard.

Construction Cost Opinion

Private Drainage Facilities Improvements (Non-Reimbursable)

Description	Quantity	Unit Price	Cost
4 ft Concrete Drain Pan	735 LF	\$42	\$30,870
2 ft Conc. Trench Drain	56 LF	\$230	\$12,880
Total			\$43,750

Private Permanent BMP (Non-Reimbursable) – 1 FSEDB

Description	Quantity	Unit Price	Cost
Earthwork	3607 Cu Yd	\$12	\$43284
Forebays	1 EA	\$1500	\$1500
Trickle Channel	92 LF	\$32	\$2944
Outlet Structure (box riser, micropool, pipe, headwall, and riprap)	1 EA	\$5000	\$5000
Emergency Spillway	1 EA	\$1500	\$1500
Maintenance Access Rd	1 EA	\$500	\$500
Stabilization	1 EA	\$5000	\$5000
<i>Subtotal</i>			<i>\$59,728</i>
<i>10% Contingency</i>			<i>\$5973</i>
Total			\$65,701

Drainage And Bridge Fees

This currently unplatted site is in the Sand Creek Drainage Basin. The site is 7.13 acres. The combined Drainage Fees (2021) are due prior to final plat recordation.

Fee Type	% Imp.	Parcel Area (acre)	Imp. Area (acre)	Fee per Imp Acre	Mod %	Fee Cost
Drainage	65.3	7.13	4.66	\$18,940	100	\$88,260
Bridge	65.3	7.13	4.66	\$5,559	100	\$25,905
				Total		\$114,165

Maintenance

The proposed FSEDB will be privately maintained and is accessible via a 12' wide aggregate base maintenance access road. The proposed entrance trench drains and proposed concrete drain pans will be privately maintained.

Summary

This Final Drainage Report analyzed the development of TRACT IN NE4NW4 SEC 18-14-65 owned by HCD Properties, LLC, located at 2601 East Platte Avenue, Colorado Springs, CO 80916. Runoff from the development will not adversely affect the surrounding or downstream developments. Proposed flows, as detailed in this report, will follow existing drainage patterns and will be safely routed downstream. Water quality and detention are provided on-site using a FSEDB. No public storm drainage modifications or design changes are necessary as a result of the development.

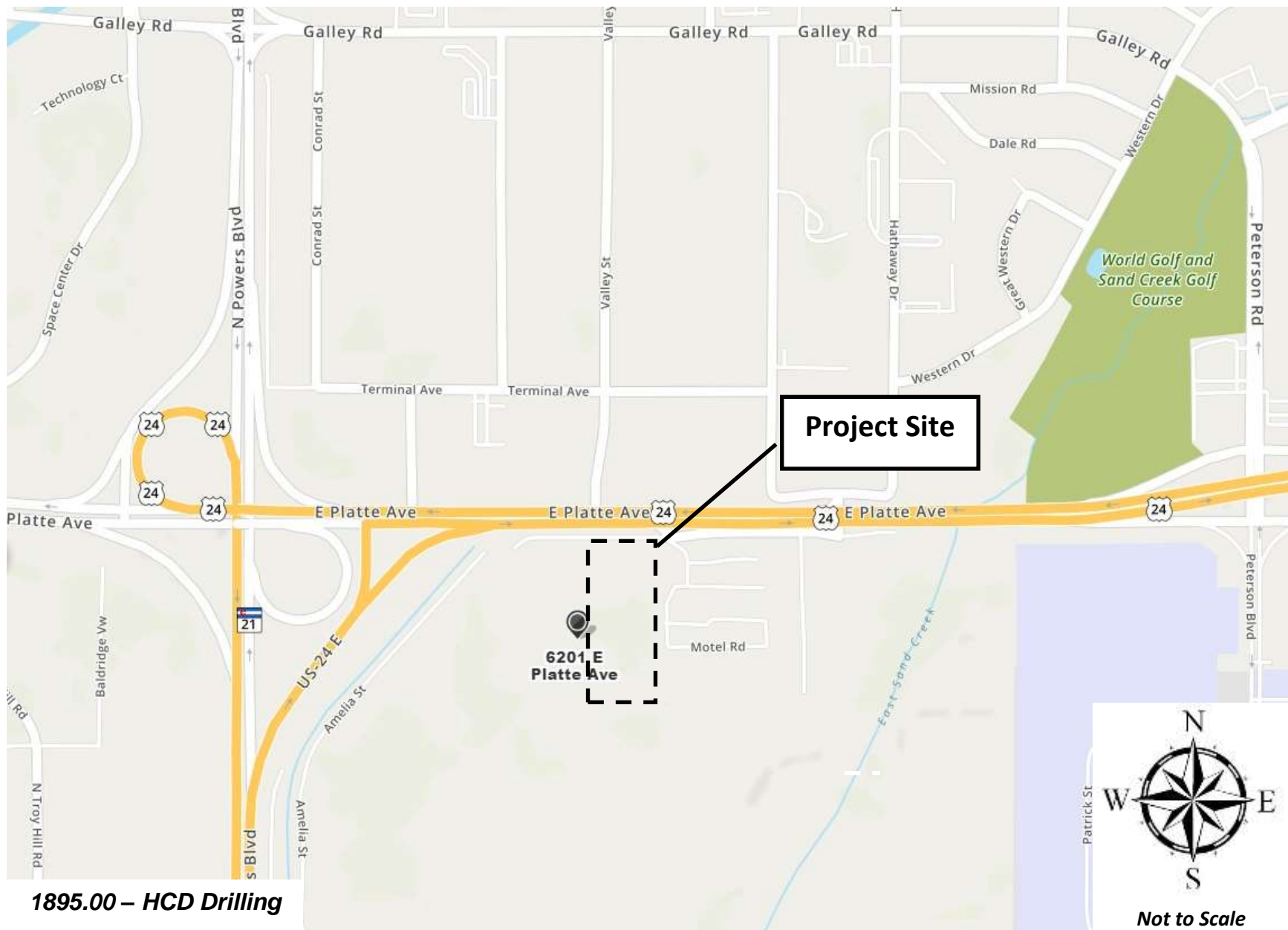
An Erosion Control Plan will be submitted separately.

References

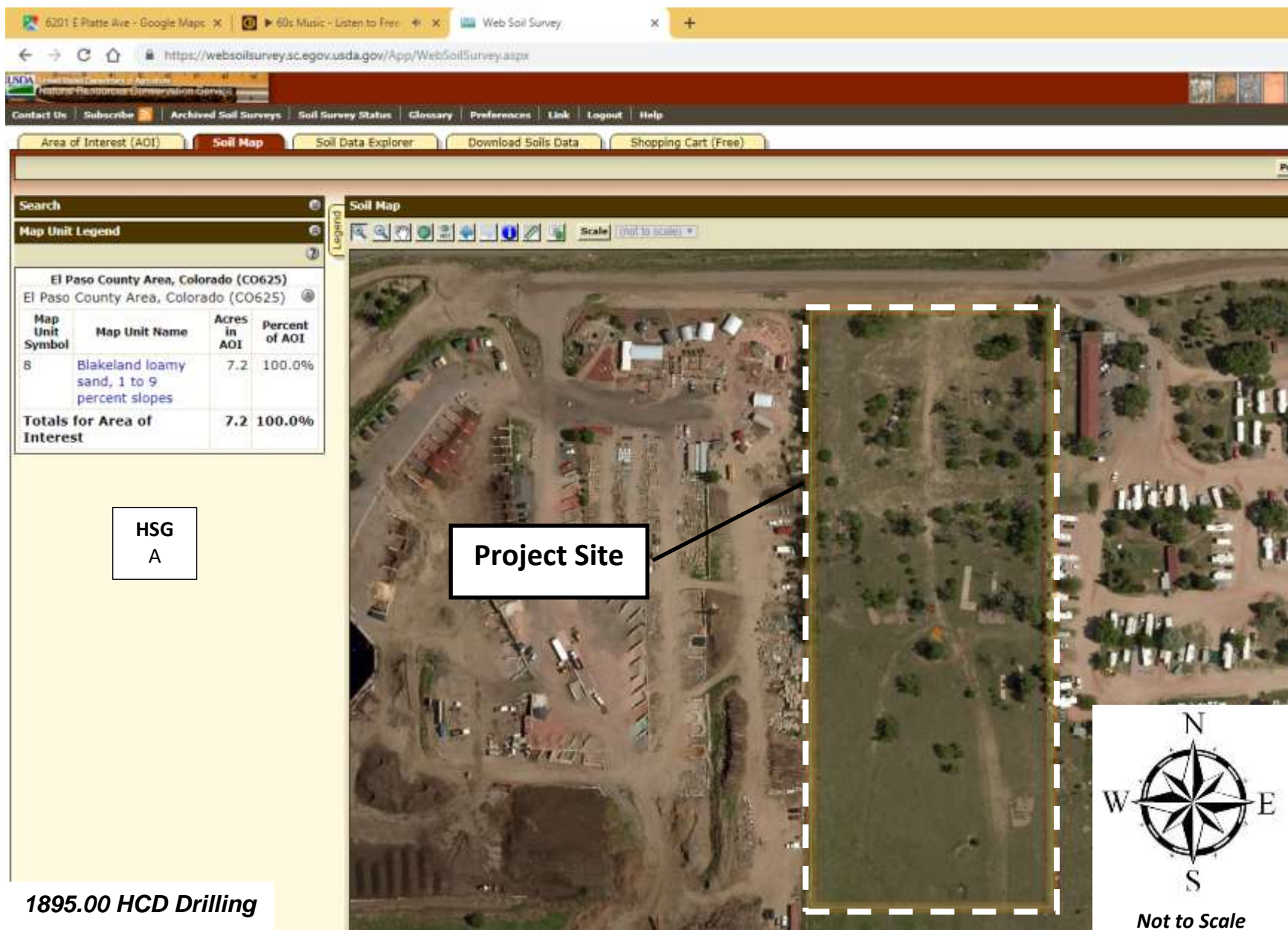
- 1) *City of Colorado Springs/County of El Paso Drainage Criteria Manual*, dated May 2014.
- 2) *Soil survey of El Paso County Area, Colorado, Prepared by United States Department of Agriculture Soil Conservation Service*, dated June 1981.
- 3) *Federal Emergency Management Agency (FEMA) Flood Insurance Rate Map Number 08041C0754G*.

APPENDICES

VICINITY MAP



SOILS MAP



FEMA FLOODPLAIN MAP

National Flood Hazard Layer FIRMette



38°50'29.58"N



0 250 500 1,000 1,500 2,000 Feet

1:6,000

38°50'1.56"N

Legend

SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT

SPECIAL FLOOD HAZARD AREAS		Without Base Flood Elevation (BFE) Zone A, V, A99
		With BFE or Depth Zone AE, AO, AH, VE, AR
		Regulatory Floodway
OTHER AREAS OF FLOOD HAZARD		0.2% Annual Chance Flood Hazard, Areas of 1% annual chance flood with average depth less than one foot or with drainage areas of less than one square mile Zone X
		Future Conditions 1% Annual Chance Flood Hazard Zone X
		Area with Reduced Flood Risk due to Levee. See Notes. Zone X
		Area with Flood Risk due to Levee Zone D
OTHER AREAS		NO SCREEN Area of Minimal Flood Hazard Zone X
		Effective LOMRs
GENERAL STRUCTURES		Area of Undetermined Flood Hazard Zone D
		Channel, Culvert, or Storm Sewer
		Levee, Dike, or Floodwall
OTHER FEATURES		20.2 Cross Sections with 1% Annual Chance Water Surface Elevation
		17.5 Cross Sections with 1% Annual Chance Water Surface Elevation
		Coastal Transect
		Base Flood Elevation Line (BFE)
		Limit of Study
		Jurisdiction Boundary
MAP PANELS		Coastal Transect Baseline
		Profile Baseline
		Hydrographic Feature
		Digital Data Available
		No Digital Data Available
		Unmapped



The pin displayed on the map is an approximate point selected by the user and does not represent an authoritative property location.

This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The basemap shown complies with FEMA's basemap accuracy standards

The flood hazard information is derived directly from the authoritative NFHL web services provided by FEMA. This map was exported on 7/24/2019 at 5:22:04 PM and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or become superseded by new data over time.

This map image is void if the one or more of the following map elements do not appear: basemap imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for unmapped and unmodernized areas cannot be used for regulatory purposes.



104°42'29.72"W

USGS The National Map: Orthoimagery. Data refreshed April, 2019.

HYDROLOGIC CALCULATIONS

1895.00 HCD DRILLING

Area Runoff Coefficient (C) Summary

HSG - A

EXISTING

		GRAVEL LOT			DISTURBED AREA			LAWN/LANDSCAPING			WEIGHTED		WEIGHTED CA	
BASIN	TOTAL AREA	AREA	C5	C100	AREA	C5	C100	AREA	C5	C100	C5	C100	CA5	CA100
	(Acres)	(Acres)			(Acres)			(Acres)						
EX-A	1.1	0.7	0.59	0.70	0.4	0.15	0.50	0.0	0.08	0.35	0.43	0.63	0.47	0.69
EX-B	2.1	0.7	0.59	0.70	1.4	0.15	0.50	0.0	0.08	0.35	0.30	0.57	0.62	1.19
EX-C	0.3	0.0	0.59	0.70	0.3	0.15	0.50	0.0	0.08	0.35	0.15	0.50	0.05	0.15
OS-1	0.1	0.0	0.59	0.70	0.0	0.15	0.50	0.1	0.08	0.35	0.08	0.35	0.00	0.02
OS-2	0.1	0.0	0.59	0.70	0.0	0.15	0.50	0.1	0.08	0.35	0.08	0.35	0.01	0.04

3.7

DEVELOPED

		GRAVEL LOT			PAVEMENT/ROOF			LAWN/LANDSCAPING			WEIGHTED		WEIGHTED CA	
BASIN	TOTAL AREA	AREA	C5	C100	AREA	C5	C100	AREA	C5	C100	C5	C100	CA5	CA100
	(Acres)	(Acres)			(Acres)			(Acres)						
A	1.36	0.00	0.59	0.70	1.15	0.90	0.96	0.21	0.08	0.35	0.77	0.87	1.05	1.18
B	0.76	0.00	0.59	0.70	0.60	0.90	0.96	0.16	0.08	0.35	0.73	0.83	0.55	0.63
C	0.61	0.12	0.59	0.70	0.33	0.90	0.96	0.16	0.08	0.35	0.62	0.75	0.38	0.46
D	0.26	0.15	0.59	0.70	0.08	0.90	0.96	0.03	0.08	0.35	0.63	0.74	0.16	0.19
E	0.35	0.24	0.59	0.70	0.11	0.90	0.96	0.00	0.08	0.35	0.69	0.78	0.24	0.27
F	0.29	0.18	0.59	0.70	0.11	0.90	0.96	0.00	0.08	0.35	0.71	0.80	0.21	0.23
G	0.35	0.24	0.59	0.70	0.11	0.90	0.96	0.00	0.08	0.35	0.69	0.78	0.24	0.27
H	0.20	0.12	0.59	0.70	0.08	0.90	0.96	0.00	0.08	0.35	0.71	0.80	0.14	0.16
I	0.96	0.00	0.59	0.70	0.00	0.90	0.96	0.96	0.08	0.35	0.08	0.35	0.08	0.34
J	1.82	0.62	0.59	0.70	0.06	0.90	0.96	1.14	0.08	0.35	0.28	0.49	0.51	0.89
K	0.16	0.00	0.59	0.70	0.01	0.90	0.96	0.15	0.08	0.35	0.13	0.39	0.02	0.06
OS-1	0.05	0.00	0.59	0.70	0.00	0.90	0.96	0.05	0.08	0.35	0.08	0.35	0.00	0.02
OS-2	0.10	0.00	0.59	0.70	0.00	0.90	0.96	0.10	0.08	0.35	0.08	0.35	0.01	0.04

7.27

Calculated by: JF

Date: 7/20/2021 Checked by: _____

1895.00 HCD DRILLING Runoff Summary

EXISTING

		WEIGHTED		OVERLAND				SHALLOW CONCENTRATED FLOW				T _c	INTENSITY		TOTAL FLOWS	
BASIN	AREA TOTAL (Acres)	C ₅	C ₁₀₀	C ₅	Length (ft)	Slope (ft/ft)	T _i (min)	Length (ft)	Slope (%)	Velocity (fps)	T _i (min)	TOTAL (min)	I ₅ (in/hr)	I ₁₀₀ (in/hr)	Q ₅ (c.f.s.)	Q ₁₀₀ (c.f.s.)
		* For Calcs See Runoff Summary														
EX-A	1.10	0.43	0.63	0.43	150	0.029	10.4	180	4.4%	3.2	0.9	11.4	3.9	6.7	1.83	4.62
EX-B	2.10	0.30	0.57	0.30	150	0.027	12.8	276	3.6%	2.8	1.6	14.4	3.5	6.0	2.20	7.14
EX-C	0.30	0.15	0.50	0.15	150	0.033	14.2	176	3.5%	2.8	1.0	15.2	3.4	5.9	0.16	0.88
OS-1	0.05	0.08	0.35	0.08	35	0.029	7.7	0	3.5%	2.8	0.0	7.7	4.4	7.9	0.02	0.14
OS-2	0.10	0.08	0.35	0.08	75	0.040	10.1	0	3.5%	2.8	0.0	10.1	4.1	7.0	0.03	0.25

DEVELOPED

		WEIGHTED		OVERLAND				SHALLOW CONCENTRATED FLOW				T _c	INTENSITY		TOTAL FLOWS	
BASIN	AREA TOTAL (Acres)	C ₅	C ₁₀₀	C ₅	Length (ft)	Slope (ft/ft)	T _t (min)	Length (ft)	Slope (%)	Velocity (fps)	T _t (min)	TOTAL (min)	I ₅ (in/hr)	I ₁₀₀ (in/hr)	Q ₅ (c.f.s.)	Q ₁₀₀ (c.f.s.)
		* For Calcs See Runoff Summary														
A	1.36	0.77	0.87	0.77	55	0.02	3.4	255	3.0%	3.5	1.2	5.0	5.0	9.1	5.26	10.67
B	0.76	0.73	0.83	0.73	0	0.04	0.0	260	1.3%	2.2	2.0	5.0	5.0	9.1	2.77	5.73
C	0.61	0.62	0.75	0.62	45	0.02	4.6	95	1.0%	2.0	0.8	5.4	4.9	8.9	1.87	4.05
D	0.26	0.63	0.74	0.63	0	0.04	0.0	160	2.5%	3.2	0.8	5.0	5.0	9.1	0.82	1.74
E	0.35	0.69	0.78	0.69	0	0.33	0.0	180	4.0%	2.0	1.5	5.0	5.0	9.1	1.20	2.48
F	0.29	0.71	0.80	0.71	0	0.10	0.0	160	4.0%	2.0	1.3	5.0	5.0	9.1	1.03	2.10
G	0.35	0.69	0.78	0.69	0	0.10	0.0	180	4.0%	2.0	1.5	5.0	5.0	9.1	1.20	2.48
H	0.20	0.71	0.80	0.71	0	0.10	0.0	160	4.0%	2.0	1.3	5.0	5.0	9.1	0.71	1.46
I	0.96	0.08	0.35	0.08	100	0.03	12.8	310	4.0%	2.0	2.6	15.4	3.4	5.8	0.26	1.95
J	1.82	0.28	0.49	0.28	100	0.03	10.3	240	4.2%	1.0	4.0	14.3	3.5	6.0	1.81	5.37
K	0.16	0.13	0.39	0.13	100	0.07	9.4	0	1.0%	1.0	0.0	9.4	4.1	7.2	0.09	0.45
OS-1	0.05	0.08	0.35	0.08	40	0.03	8.6	0	1.0%	1.0	0.0	8.6	4.3	7.5	0.02	0.13
OS-2	0.10	0.08	0.35	0.08	70	0.04	9.6	0	1.0%	1.0	0.0	9.6	4.1	7.2	0.03	0.25

1895.00 HCD DRILLING

Surface Routing

EXISTING CONDITIONS									
Design Point(s)	Contributing Basins	Area (Acres)	Equivalent CA_5	Equivalent CA_{100}	Maximum T_C	Intensity		Flow	
						I_5	I_{100}	Q_5	Q_{100}
X1	EX-A	1.10	0.47	0.69	11.4	3.9	6.7	1.83	4.62
X2	EX-B	2.10	0.62	1.19	14.4	3.5	6.0	2.20	7.14
X3	EX-C, OS-1, OS-2	4.07	0.05	0.15	15.2	3.4	5.9	0.21	1.27
X4	OS-1	0.05	0.00	0.02	7.7	4.4	7.9	0.02	0.14
X5	OS-2	0.10	0.01	0.04	10.1	4.1	7.0	0.03	0.25

PROPOSED CONDITIONS									
Design Point(s)	Contributing Basins	Area (Acres)	Equivalent CA_5	Equivalent CA_{100}	Maximum T_C	Intensity		Flow	
						I_5	I_{100}	Q_5	Q_{100}
1	A	1.36	1.05	1.18	5.0	5.0	9.1	5.26	10.67
2	B	0.76	0.52	0.59	5.0	5.0	9.1	2.58	5.35
3	C	0.54	0.33	0.40	5.6	4.9	8.8	1.59	3.47
4	D	0.26	0.16	0.19	5.0	5.0	9.1	0.82	1.74
5	E	0.35	0.24	0.27	5.0	5.0	9.1	1.20	2.48
6	F	0.29	0.21	0.23	5.0	5.0	9.1	1.03	2.10
7	G	0.35	0.24	0.27	5.0	5.0	9.1	1.20	2.48
8	H	0.20	0.14	0.16	5.0	5.0	9.1	0.71	1.46
9	I, OS-2	1.06	0.08	0.37	27.2	2.6	4.3	0.22	1.59
10	J, OS-1	1.87	0.52	0.91	24.7	2.7	4.5	1.42	4.12
11	K	0.16	0.02	0.06	9.4	4.1	7.2	0.09	0.45
12	L	0.06	0.05	0.05	5.0	5.0	9.1	0.23	0.47
13	M	0.06	0.04	0.05	5.0	5.0	9.1	0.19	0.41
14	OS-1	0.05	0.00	0.02	10.4	4.0	7.0	0.02	0.12
15	OS-2	0.10	0.01	0.04	11.8	3.8	6.6	0.03	0.23

DEVELOPED CONDITIONS

<i>Pipe Run(s)</i>	<i>Contributing Design Points/Pipe Runs</i>	<i>Area (Acres)</i>	<i>Equivalent CA₅</i>	<i>Equivalent CA₁₀₀</i>	<i>Maximum T_c</i>	<i>Intensity</i>		<i>Flow</i>	
						<i>I₅</i>	<i>I₁₀₀</i>	<i>Q₅</i>	<i>Q₁₀₀</i>
1	DP 1	1.36	1.05	1.18	5.0	5.0	9.1	5.3	10.7
2	DP 12	0.06	0.05	0.05	5.0	5.0	9.1	0.2	0.5
3	DP 13, PR 2	0.12	0.08	0.10	5.0	5.0	9.1	0.4	0.9
4	DP 3, PR 3, PR 1	2.02	1.46	1.67	5.0	5.0	9.1	7.3	15.1
5	DP 5, PR 4	2.37	1.70	1.94	5.0	5.0	9.1	8.5	17.6
6	DP 7, PR 5	2.72	1.94	2.22	5.0	5.0	9.1	9.7	20.1
7	DP 2	0.71	0.52	0.59	5.0	5.0	9.1	2.6	5.3
8	DP 4, PR 7	0.97	0.68	0.78	5.0	5.0	9.1	3.4	7.1
9	DP 6, PR 8	1.26	0.88	1.01	5.0	5.0	9.1	4.4	9.2
10	DP 8, PR 9	1.46	1.03	1.17	5.0	5.0	9.1	5.1	10.6
11	POND OUTLET							0.2	3.5

Calculated by: JF

Date: 7/21/2021

Checked by: _____

HYDRAULIC CALCULATIONS

Manning Formula Uniform Pipe Flow at Given Slope and Depth

Check out our spreadsheet version of this calculator [Download Spreadsheet](#) [Open Google Sheets version](#) [View All Spreadsheets](#)

Pipe Run 1

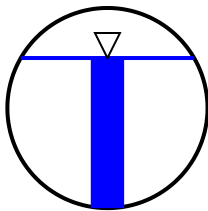
24" RCP

Inputs

Pipe diameter, d_0	24	in
Manning roughness, n	0.013	
Pressure slope (possibly ? equal to pipe slope), S_0	0.01	rise/run
Percent of (or ratio to) full depth (100% or 1 if flowing full)	.75	fraction

Results

Flow, Q (See notes)	20.6269	cfs
Velocity, v	2.4877	m/s
Velocity head, h_v	0.3155	m H2O
Flow area	0.2348	m^2
Wetted perimeter	1.2767	m
Hydraulic radius	0.1839	m
Top width, T	0.5279	m
Froude number, F	1.19	
Shear stress (tractive force), τ	18.0341	N/m^2



Notes:

This is the flow and depth *inside* the pipe.
Getting the flow into the pipe may require significantly higher headwater depth. Add at least 1.5 times the velocity head to get the headwater depth or [see my 2-minute tutorial](#) for standard culvert headwater calculations using HY-8.

Manning Formula Uniform Pipe Flow at Given Slope and Depth

Check out our spreadsheet version of this calculator [Download Spreadsheet](#) [Open Google Sheets version](#) [View All Spreadsheets](#)

Pipe Run 2

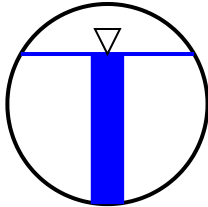
12" HDPE

Inputs

Pipe diameter, d_0	12	in
Manning roughness, n	0.013	
Pressure slope (possibly ? equal to pipe slope), S_0	0.01	rise/run
Percent of (or ratio to) full depth (100% or 1 if flowing full)	.75	fraction

Results

Flow, Q (See notes)	3.2485	cfs
Velocity, v	1.5671	m/s
Velocity head, h_v	0.1252	m H2O
Flow area	0.0587	m^2
Wetted perimeter	0.6384	m
Hydraulic radius	0.0920	m
Top width, T	0.2640	m
Froude number, F	1.06	
Shear stress (tractive force), τ	9.0170	N/m^2



Notes:

This is the flow and depth *inside* the pipe.
Getting the flow into the pipe may require significantly higher headwater depth. Add at least 1.5 times the velocity head to get the headwater depth or [see my 2-minute tutorial](#) for standard culvert headwater calculations using HY-8.

Manning Formula Uniform Pipe Flow at Given Slope and Depth

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Pipe Run 3

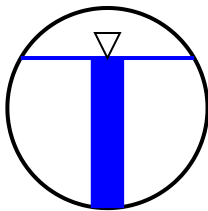
12" HDPE

Inputs

Pipe diameter, d_0	12	in
Manning roughness, n	0.013	
Pressure slope (possibly ? equal to pipe slope), S_0	0.01	rise/run
Percent of (or ratio to) full depth (100% or 1 if flowing full)	.75	fraction

Results

Flow, Q (See notes)	3.2485	cfs
Velocity, v	1.5671	m/s
Velocity head, h_v	0.1252	m H2O
Flow area	0.0587	m^2
Wetted perimeter	0.6384	m
Hydraulic radius	0.0920	m
Top width, T	0.2640	m
Froude number, F	1.06	
Shear stress (tractive force), τ	9.0170	N/m^2



Notes:

This is the flow and depth *inside* the pipe.
Getting the flow into the pipe may require significantly higher headwater depth. Add at least 1.5 times the velocity head to get the headwater depth or [see my 2-minute tutorial](#) for standard culvert headwater calculations using HY-8.

Manning Formula Uniform Pipe Flow at Given Slope and Depth

Check out our spreadsheet version of this calculator [Download Spreadsheet](#) [Open Google Sheets version](#) [View All Spreadsheets](#)

Pipe Run 4

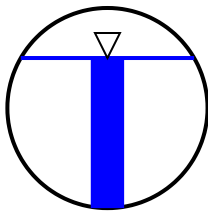
24" RCP

Inputs

Pipe diameter, d_0	24	in
Manning roughness, n	0.013	
Pressure slope (possibly ? equal to pipe slope), S_0	0.01	rise/run
Percent of (or ratio to) full depth (100% or 1 if flowing full)	.75	fraction

Results

Flow, Q (See notes)	20.6269	cfs
Velocity, v	2.4877	m/s
Velocity head, h_v	0.3155	m H2O
Flow area	0.2348	m^2
Wetted perimeter	1.2767	m
Hydraulic radius	0.1839	m
Top width, T	0.5279	m
Froude number, F	1.19	
Shear stress (tractive force), τ	18.0341	N/m^2



Notes:

This is the flow and depth *inside* the pipe.
Getting the flow into the pipe may require significantly higher headwater depth. Add at least 1.5 times the velocity head to get the headwater depth or [see my 2-minute tutorial](#) for standard culvert headwater calculations using HY-8.

Manning Formula Uniform Pipe Flow at Given Slope and Depth

Check out our spreadsheet version of this calculator [Download Spreadsheet](#) [Open Google Sheets version](#) [View All Spreadsheets](#)

Pipe Run 5

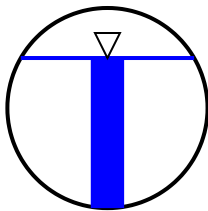
24" RCP

Inputs

Pipe diameter, d_0	24	in
Manning roughness, n	0.013	
Pressure slope (possibly ? equal to pipe slope), S_0	0.01	rise/run
Percent of (or ratio to) full depth (100% or 1 if flowing full)	.75	fraction

Results

Flow, Q (See notes)	20.6269	cfs
Velocity, v	2.4877	m/s
Velocity head, h_v	0.3155	m H2O
Flow area	0.2348	m^2
Wetted perimeter	1.2767	m
Hydraulic radius	0.1839	m
Top width, T	0.5279	m
Froude number, F	1.19	
Shear stress (tractive force), τ	18.0341	N/m^2



Notes:

This is the flow and depth *inside* the pipe.
Getting the flow into the pipe may require significantly higher headwater depth. Add at least 1.5 times the velocity head to get the headwater depth or [see my 2-minute tutorial](#) for standard culvert headwater calculations using HY-8.

Manning Formula Uniform Pipe Flow at Given Slope and Depth

Check out our spreadsheet version of this calculator [Download Spreadsheet](#) [Open Google Sheets version](#) [View All Spreadsheets](#)

Pipe Run 6

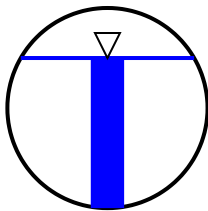
24" RCP

Inputs

Pipe diameter, d_0	24	in
Manning roughness, n	0.013	
Pressure slope (possibly ? equal to pipe slope), S_0	0.01	rise/run
Percent of (or ratio to) full depth (100% or 1 if flowing full)	.75	fraction

Results

Flow, Q (See notes)	20.6269	cfs
Velocity, v	2.4877	m/s
Velocity head, h_v	0.3155	m H2O
Flow area	0.2348	m^2
Wetted perimeter	1.2767	m
Hydraulic radius	0.1839	m
Top width, T	0.5279	m
Froude number, F	1.19	
Shear stress (tractive force), τ	18.0341	N/m^2



Notes:

This is the flow and depth *inside* the pipe.
Getting the flow into the pipe may require significantly higher headwater depth. Add at least 1.5 times the velocity head to get the headwater depth or [see my 2-minute tutorial](#) for standard culvert headwater calculations using HY-8.

Manning Formula Uniform Pipe Flow at Given Slope and Depth

Check out our spreadsheet version of this calculator [Download Spreadsheet](#) [Open Google Sheets version](#) [View All Spreadsheets](#)

Pipe Run 7

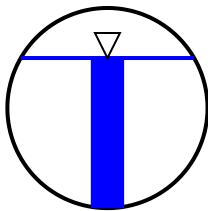
15" HDPE

Inputs

Pipe diameter, d_0	15	in
Manning roughness, n	0.013	
Pressure slope (possibly ? equal to pipe slope), S_0	0.01	rise/run
Percent of (or ratio to) full depth (100% or 1 if flowing full)	.75	fraction

Results

Flow, Q (See notes)	5.8900	cfs
Velocity, v	1.8185	m/s
Velocity head, h_v	0.1686	m H2O
Flow area	0.0917	m^2
Wetted perimeter	0.7980	m
Hydraulic radius	0.1149	m
Top width, T	0.3300	m
Froude number, F	1.10	
Shear stress (tractive force), τ	11.2713	N/m^2



Notes:

This is the flow and depth *inside* the pipe.
Getting the flow into the pipe may require significantly higher headwater depth. Add at least 1.5 times the velocity head to get the headwater depth or [see my 2-minute tutorial](#) for standard culvert headwater calculations using HY-8.

Manning Formula Uniform Pipe Flow at Given Slope and Depth

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Pipe Run 8

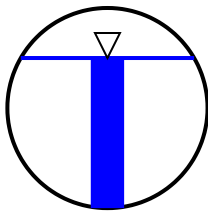
18" RCP

Inputs

Pipe diameter, d_0	18	in
Manning roughness, n	0.013	
Pressure slope (possibly ? equal to pipe slope), S_0	0.01	rise/run
Percent of (or ratio to) full depth (100% or 1 if flowing full)	.75	fraction

Results

Flow, Q (See notes)	9.5777	cfs
Velocity, v	2.0535	m/s
Velocity head, h_v	0.2150	m H2O
Flow area	0.1321	m^2
Wetted perimeter	0.9576	m
Hydraulic radius	0.1379	m
Top width, T	0.3959	m
Froude number, F	1.14	
Shear stress (tractive force), τ	13.5256	N/m^2



Notes:

This is the flow and depth *inside* the pipe.
Getting the flow into the pipe may require significantly higher headwater depth. Add at least 1.5 times the velocity head to get the headwater depth or [see my 2-minute tutorial](#) for standard culvert headwater calculations using HY-8.

Manning Formula Uniform Pipe Flow at Given Slope and Depth

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Pipe Run 9

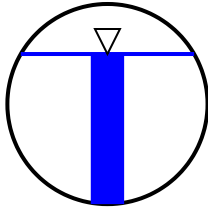
18" RCP

Inputs

Pipe diameter, d_0	18	in
Manning roughness, n	0.013	
Pressure slope (possibly ? equal to pipe slope), S_0	0.01	rise/run
Percent of (or ratio to) full depth (100% or 1 if flowing full)	.75	fraction

Results

Flow, Q (See notes)	9.5777	cfs
Velocity, v	2.0535	m/s
Velocity head, h_v	0.2150	m H2O
Flow area	0.1321	m^2
Wetted perimeter	0.9576	m
Hydraulic radius	0.1379	m
Top width, T	0.3959	m
Froude number, F	1.14	
Shear stress (tractive force), τ	13.5256	N/m^2



Notes:

This is the flow and depth *inside* the pipe.
Getting the flow into the pipe may require significantly higher headwater depth. Add at least 1.5 times the velocity head to get the headwater depth or [see my 2-minute tutorial](#) for standard culvert headwater calculations using HY-8.

Manning Formula Uniform Pipe Flow at Given Slope and Depth

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Pipe Run 10

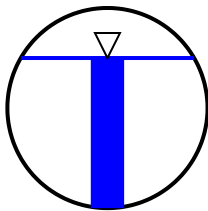
24" RCP

Inputs

Pipe diameter, d_0	24	in
Manning roughness, n	0.013	
Pressure slope (possibly ? equal to pipe slope), S_0	0.01	rise/run
Percent of (or ratio to) full depth (100% or 1 if flowing full)	.75	fraction

Results

Flow, Q (See notes)	20.6269	cfs
Velocity, v	2.4877	m/s
Velocity head, h_v	0.3155	m H2O
Flow area	0.2348	m^2
Wetted perimeter	1.2767	m
Hydraulic radius	0.1839	m
Top width, T	0.5279	m
Froude number, F	1.19	
Shear stress (tractive force), τ	18.0341	N/m^2



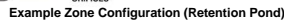
Notes:

This is the flow and depth *inside* the pipe.
Getting the flow into the pipe may require significantly higher headwater depth. Add at least 1.5 times the velocity head to get the headwater depth or [see my 2-minute tutorial](#) for standard culvert headwater calculations using HY-8.

FSEDB CALCULATIONS

MHFD-Detention, Version 4.04 (February 2021)

Basin ID:

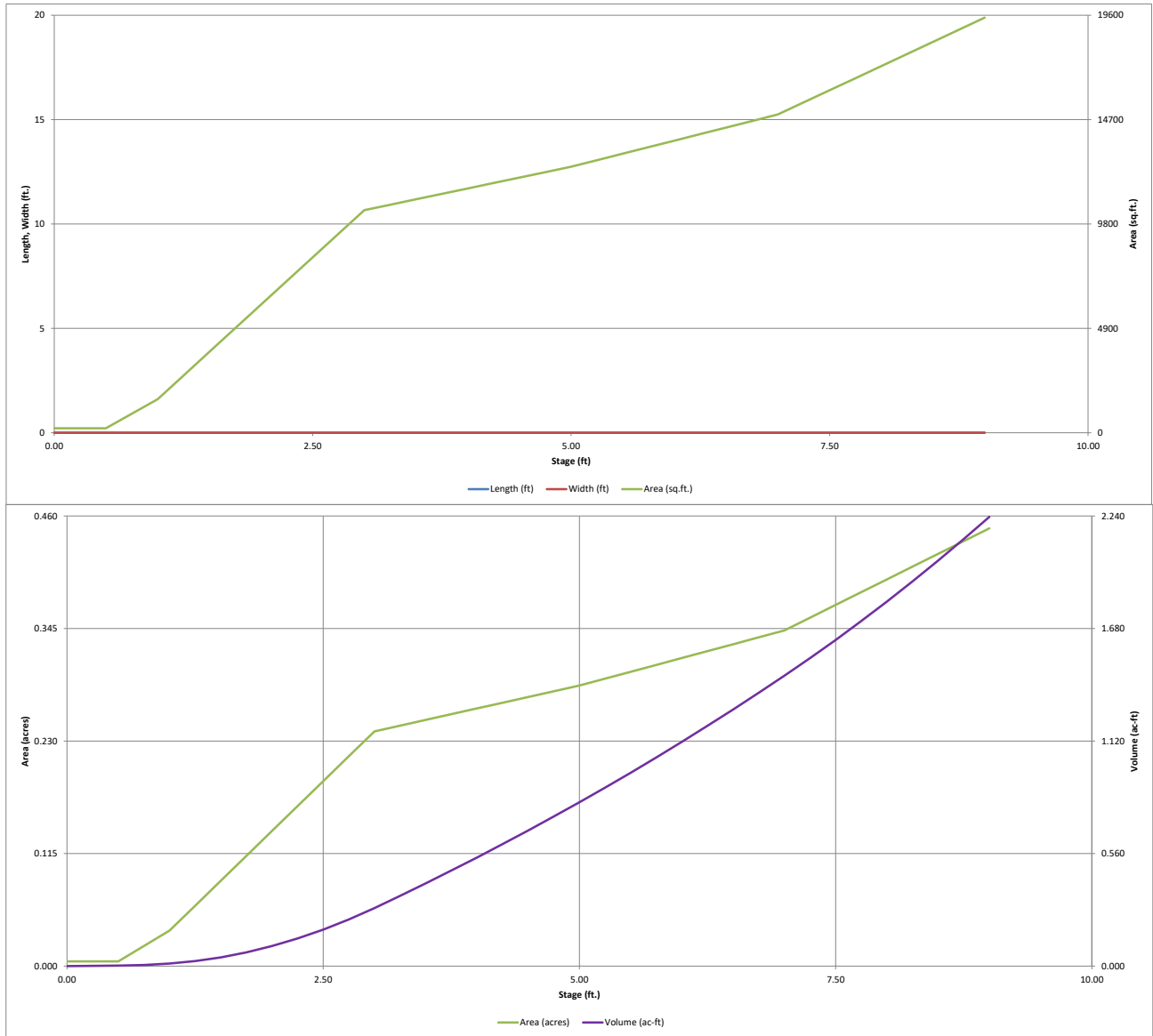


Optional User Overrides

7/21/2021, 7:00 PM

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.04 (February 2021)

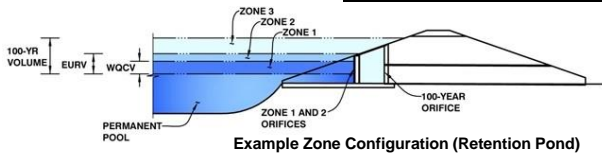


DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.04 (February 2021)

Project: _____

Basin ID: _____



	Estimated Stage (ft)	Estimated Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	2.20	0.129	Orifice Plate
Zone 2 (EURV)	3.82	0.362	Orifice Plate
Zone 3 (100-year)	4.71	0.240	Weir&Pipe (Restrict)
Total (all zones)		0.731	

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth = ft (distance below the filtration media surface)
Underdrain Orifice Diameter = inches

Calculated Parameters for Underdrain
Underdrain Orifice Area = ft²
Underdrain Orifice Centroid = feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice = ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Orifice Plate = ft (relative to basin bottom at Stage = 0 ft)
Orifice Plate: Orifice Vertical Spacing = inches
Orifice Plate: Orifice Area per Row = inches

Calculated Parameters for Plate
WQ Orifice Area per Row = ft²
Elliptical Half-Width = feet
Elliptical Slot Centroid = feet
Elliptical Slot Area = ft²

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	1.27	2.55					
Orifice Area (sq. inches)	0.70	0.70	4.00					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

Invert of Vertical Orifice = ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Vertical Orifice = ft (relative to basin bottom at Stage = 0 ft)
Vertical Orifice Diameter = inches

Calculated Parameters for Vertical Orifice
Vertical Orifice Area = ft²
Vertical Orifice Centroid = feet

User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe))

Overflow Weir Front Edge Height, H_o = ft (relative to basin bottom at Stage = 0 ft)
Overflow Weir Front Edge Length = feet
Overflow Weir Grate Slope = H:V
Horiz. Length of Weir Sides = feet
Overflow Grate Type =
Debris Clogging % = %

Calculated Parameters for Overflow Weir
Height of Grate Upper Edge, H_u = feet
Overflow Weir Slope Length = feet
Grate Open Area / 100-yr Orifice Area =
Overflow Grate Open Area w/o Debris = ft²
Overflow Grate Open Area w/ Debris = ft²

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

Depth to Invert of Outlet Pipe = ft (distance below basin bottom at Stage = 0 ft)
Outlet Pipe Diameter = inches
Restrictor Plate Height Above Pipe Invert = inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate
Outlet Orifice Area = ft²
Outlet Orifice Centroid = feet
Half-Central Angle of Restrictor Plate on Pipe = radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage = ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length = feet
Spillway End Slopes = H:V
Freeboard above Max Water Surface = feet

Calculated Parameters for Spillway
Spillway Design Flow Depth = feet
Stage at Top of Freeboard = feet
Basin Area at Top of Freeboard = acres
Basin Volume at Top of Freeboard = acre-ft

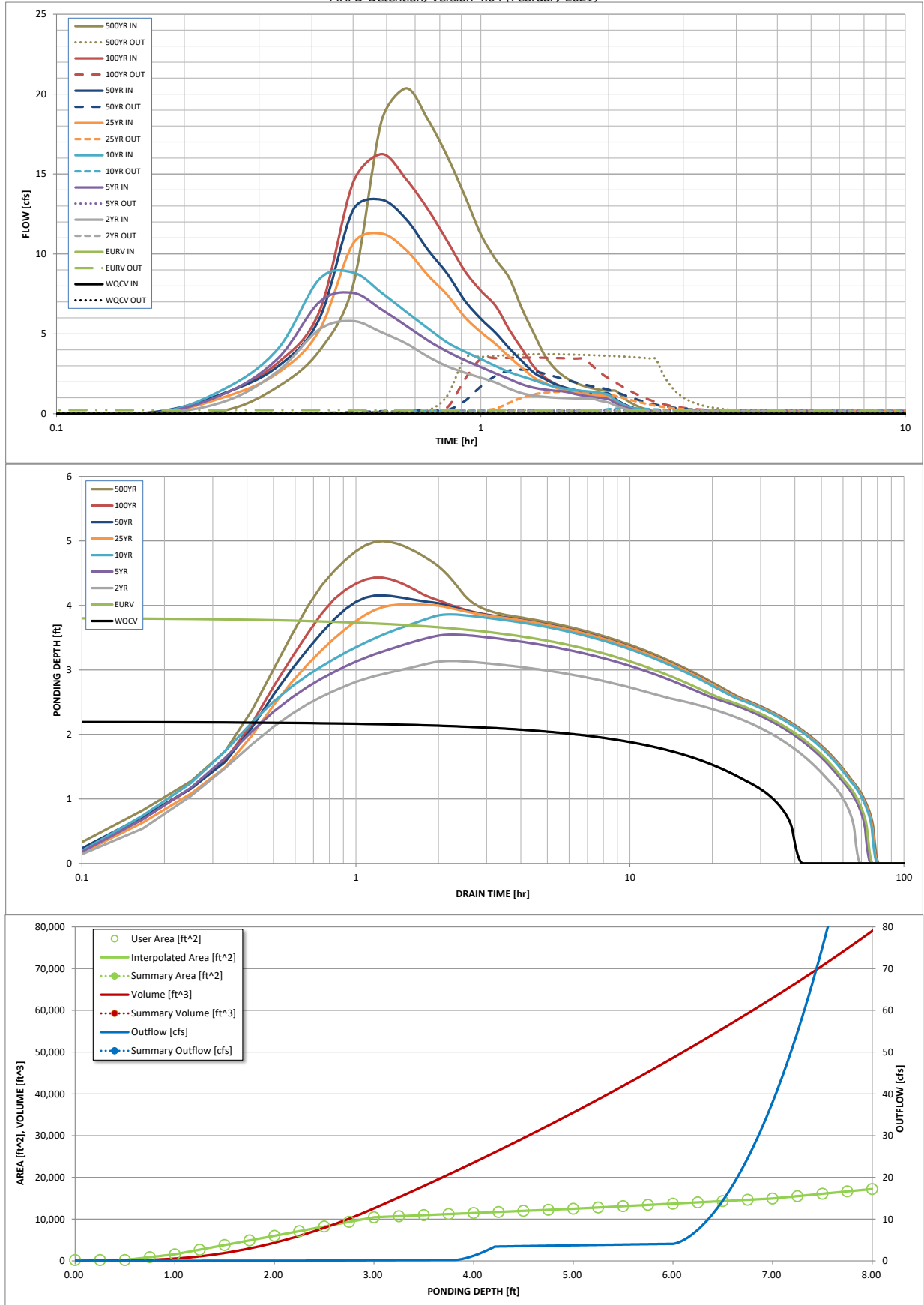
Routed Hydrograph Results

The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).

	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52	3.00
One-Hour Rainfall Depth (in) =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52	3.00
CUHP Runoff Volume (acre-ft) =	0.129	0.491	0.346	0.454	0.540	0.653	0.763	0.898	1.123
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	0.346	0.454	0.540	0.653	0.763	0.898	1.123
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A	0.0	0.1	0.1	1.1	2.3	3.7	6.0
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A							
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.01	0.02	0.02	0.19	0.38	0.62	0.99
Peak Inflow Q (cfs) =	N/A	N/A	5.8	7.6	8.8	11.3	13.4	16.2	20.4
Peak Outflow Q (cfs) =	0.1	0.2	0.2	0.2	0.3	1.4	2.8	3.5	3.7
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	2.3	2.7	1.2	1.2	0.9	0.6
Structure Controlling Flow =	Plate	Overflow Weir 1	Plate	Plate	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Outlet Plate 1	Outlet Plate 1
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	N/A	0.0	0.4	0.9	1.2	1.2
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	38	67	61	66	69	68	66	64	62
Time to Drain 99% of Inflow Volume (hours) =	40	72	65	71	75	75	74	73	73
Maximum Ponding Depth (ft) =	2.20	3.82	3.14	3.55	3.86	4.02	4.16	4.43	5.00
Area at Maximum Ponding Depth (acres) =	0.16	0.26	0.24	0.25	0.26	0.26	0.27	0.27	0.29
Maximum Volume Stored (acre-ft) =	0.129	0.493	0.320	0.422	0.501	0.543	0.580	0.656	0.813

DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.04 (February 2021)



S-A-V-D Chart Axis Override	X-axis	Left Y-Axis	Right Y-Axis
minimum bound			
maximum bound			

DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename:

Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.09	0.01	0.22
	0:15:00	0.00	0.00	0.79	1.28	1.59	1.07	1.32	1.30	1.71
	0:20:00	0.00	0.00	2.69	3.50	4.10	2.58	2.99	3.22	3.95
	0:25:00	0.00	0.00	5.29	7.00	8.43	5.24	5.96	6.42	8.05
	0:30:00	0.00	0.00	5.80	7.56	8.84	10.65	12.75	14.46	18.31
	0:35:00	0.00	0.00	5.10	6.53	7.58	11.27	13.39	16.25	20.36
	0:40:00	0.00	0.00	4.40	5.51	6.38	10.25	12.18	14.68	18.41
	0:45:00	0.00	0.00	3.58	4.59	5.35	8.67	10.26	12.80	16.11
	0:50:00	0.00	0.00	2.97	3.90	4.46	7.44	8.76	10.81	13.64
	0:55:00	0.00	0.00	2.57	3.35	3.89	6.05	7.08	8.93	11.23
	1:00:00	0.00	0.00	2.26	2.92	3.43	5.11	5.94	7.70	9.67
	1:05:00	0.00	0.00	1.96	2.52	2.99	4.37	5.06	6.75	8.49
	1:10:00	0.00	0.00	1.57	2.17	2.61	3.56	4.10	5.26	6.57
	1:15:00	0.00	0.00	1.28	1.84	2.34	2.88	3.30	4.05	5.02
	1:20:00	0.00	0.00	1.13	1.63	2.11	2.27	2.57	2.94	3.62
	1:25:00	0.00	0.00	1.06	1.52	1.86	1.92	2.17	2.27	2.78
	1:30:00	0.00	0.00	1.01	1.44	1.69	1.64	1.84	1.87	2.27
	1:35:00	0.00	0.00	0.98	1.39	1.57	1.45	1.63	1.62	1.95
	1:40:00	0.00	0.00	0.96	1.24	1.48	1.32	1.49	1.45	1.74
	1:45:00	0.00	0.00	0.95	1.13	1.42	1.24	1.40	1.33	1.59
	1:50:00	0.00	0.00	0.94	1.05	1.38	1.18	1.33	1.25	1.49
	1:55:00	0.00	0.00	0.80	0.99	1.31	1.15	1.29	1.21	1.44
	2:00:00	0.00	0.00	0.70	0.92	1.18	1.12	1.26	1.19	1.42
	2:05:00	0.00	0.00	0.50	0.65	0.83	0.80	0.89	0.85	1.01
	2:10:00	0.00	0.00	0.35	0.46	0.58	0.56	0.63	0.60	0.71
	2:15:00	0.00	0.00	0.24	0.31	0.40	0.39	0.44	0.42	0.50
	2:20:00	0.00	0.00	0.16	0.21	0.27	0.26	0.29	0.28	0.33
	2:25:00	0.00	0.00	0.10	0.13	0.18	0.17	0.19	0.19	0.22
	2:30:00	0.00	0.00	0.06	0.09	0.11	0.11	0.13	0.12	0.14
	2:35:00	0.00	0.00	0.03	0.05	0.06	0.07	0.07	0.07	0.08
	2:40:00	0.00	0.00	0.01	0.02	0.03	0.03	0.04	0.03	0.04
	2:45:00	0.00	0.00	0.00	0.01	0.01	0.01	0.01	0.01	0.01
	2:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

FORBAY VOLUMES

FORBAY VOLUME

<i>ELEV</i>	<i>AREA</i>	<i>AREA AVG.</i>	<i>DELTA ELEV.</i>	<i>VOLUME</i>	<i>VOLUME TOTAL</i>
6244.00	200	200	1.5	300	
6245.50	200				300

End Area Method: 300 C.F.
0.007 A.F.

Required Forbay Volume = 3% of WQCV

WQCV = 0.129 ac-ft

WQCV = 5,619 cu-ft

3% of WQCV = 168.58 cu-ft

MANNING'S EQUATION for OPEN CHANNEL FLOW

Project: **Templeton Gap Townhomes**

Location: **EDB Forebay Notch - Q=16.2 cfs * 3% = 0.49 cfs**

By: **John Fornander**

Date: **7/21/2021**

Chk By:

Date:

version 12-2004

Mannings Formula

$$Q = (1.486/n)AR_h^{2/3}S^{1/2}$$

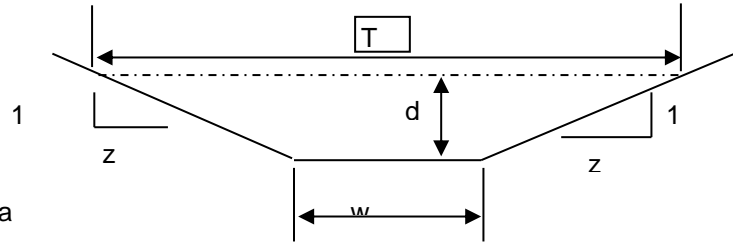
$$R = A/P$$

A = cross sectional area

P = wetted perimeter

S = slope of channel

n = Manning's roughness coefficient



$$V = (1.49/n)R_h^{2/3}S^{1/2}$$

$$Q = V \times A$$

INPUT

z (sideslope)= 0
z (sideslope)= 0
b (btm width, ft)= 0.25
d (depth, ft)= 1.5
S (slope, ft/ft) 0.005
n low = 0.013
n high = 0.013

Clear Data
Entry Cells

				Low N		High N			
Depth, ft	Area, sf	Wetted Perimeter, ft	Hydraulic Radius, ft	Velocity,		Velocity,		T =	
				fps	Flow, cfs	fps	Flow, cfs		
1.5	0.38	3.25	0.12	1.91555431	0.71833	1.915554	0.71833		0.25
								Dm =	1.500
				Sc low =	0.0657	Sc high =	0.0657		
s _c = critical slope ft / ft									
T = top width of the stream				.7 Sc	1.3 Sc	.7 Sc	1.3 Sc		
d _m = a/T = mean depth of flow				0.0460	0.0854	0.0460	0.0854		

s_c = critical slope ft / ft

T = top width of the stream

$d_m = a/T$ = mean depth of flow

Created by: Mike O'Shea

MANNING'S EQUATION for OPEN CHANNEL FLOW

Project: **Templeton Gap Townhomes**

Location: **EDB Trickle Channels (need Q= 0.49 cfs)**

By: **John Fornander**

Date: **7/21/2021**

Chk By:

Date:

version 12-2004

Mannings Formula

$$Q = (1.486/n)AR_h^{2/3}S^{1/2}$$

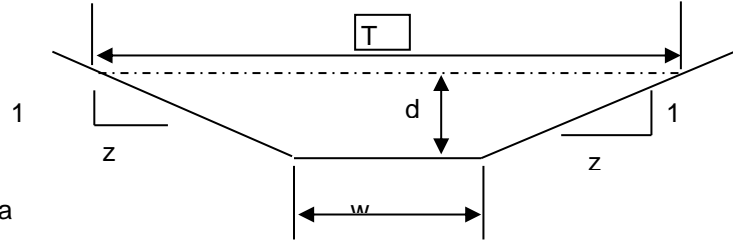
$$R = A/P$$

A = cross sectional area

P= wetted perimeter

S = slope of channel

n = Manning's roughness coefficient



$$V = (1.49/n)R_h^{2/3}S^{1/2}$$

$$Q = V \times A$$

INPUT

z (sideslope)= 0
z (sideslope)= 0
b (btm width, ft)= 1
d (depth, ft)= 0.5
S (slope, ft/ft) 0.0054
n low = 0.013
n high = 0.013

Clear Data
Entry Cells

				Low N		High N			
Depth, ft	Area, sf	Wetted Perimeter, ft	Hydraulic Radius, ft	Velocity,				T =	Dm =
				Velocity, fps	Flow, cfs	fps	Flow, cfs		
0.5	0.50	2.00	0.25	3.33333483	1.66667	3.333335	1.66667	1	0.500
				Sc low =	0.0078	Sc high =	0.0078		
s _c = critical slope ft / ft									
T = top width of the stream				.7 Sc	1.3 Sc	.7 Sc	1.3 Sc		
d _m = a/T = mean depth of flow				0.0055	0.0102	0.0055	0.0102		

s_c = critical slope ft / ft

T = top width of the stream

$d_m = a/T$ = mean depth of flow

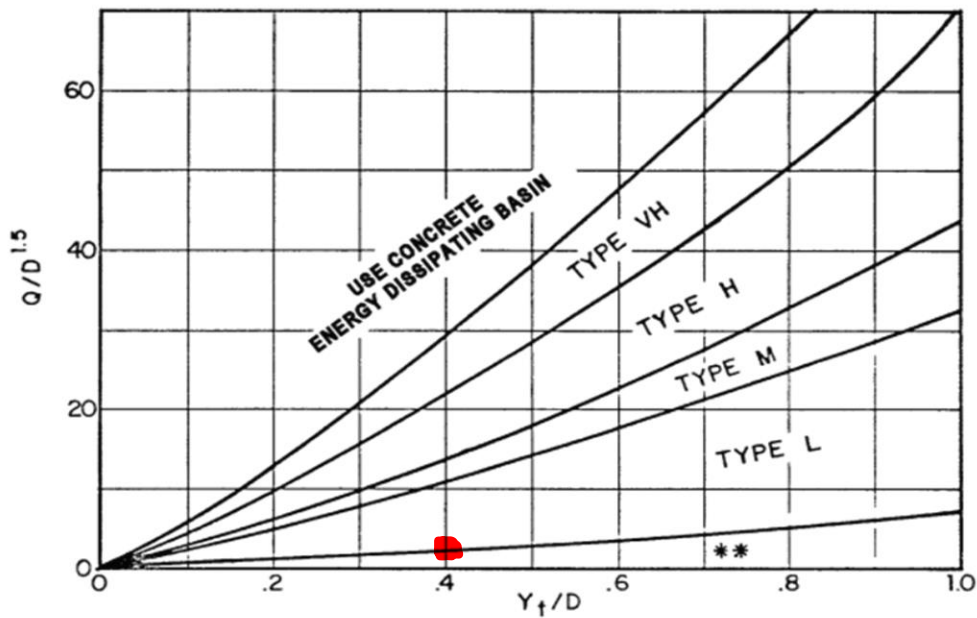
Created by: Mike O'Shea

1895.00 HCD Drilling

Riprap Protection for FSEDB Outlet Pipe¹

Q100=	3.5	cfs	$Q/D^{2.5} =$	1.27
D=	1.5	ft	$Q/D^{1.5} =$	1.91
Yt=	0.25	ft	$Yt/D =$	0.4

Minimum Riprap d_{50} Required = $d_{50} = 9$ in \implies use $d_{50} = 12$ in



Use D_d instead of D whenever flow is supercritical in the barrel.
** Use Type L for a distance of $3D$ downstream.

Figure 9-38. Riprap erosion protection at circular conduit outlet (valid for $Q/D^{2.5} \leq 6.0$)

¹ see USDCM Chapter 9 Section 3.2.3

Figure 13-12c. Emergency Spillway Protection

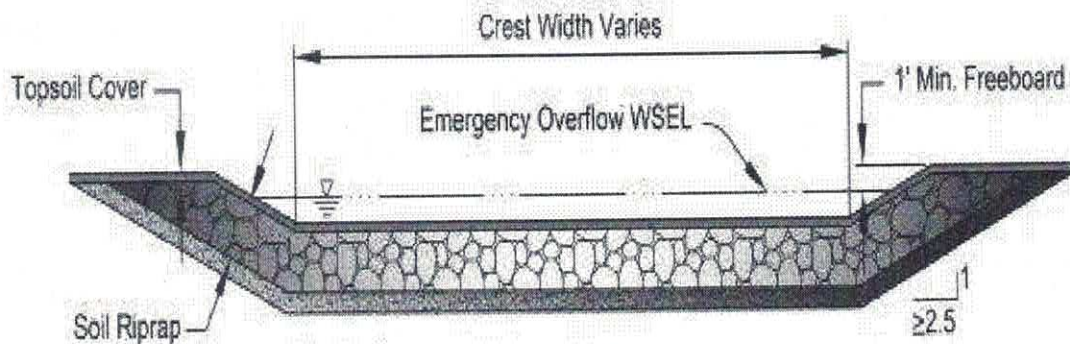
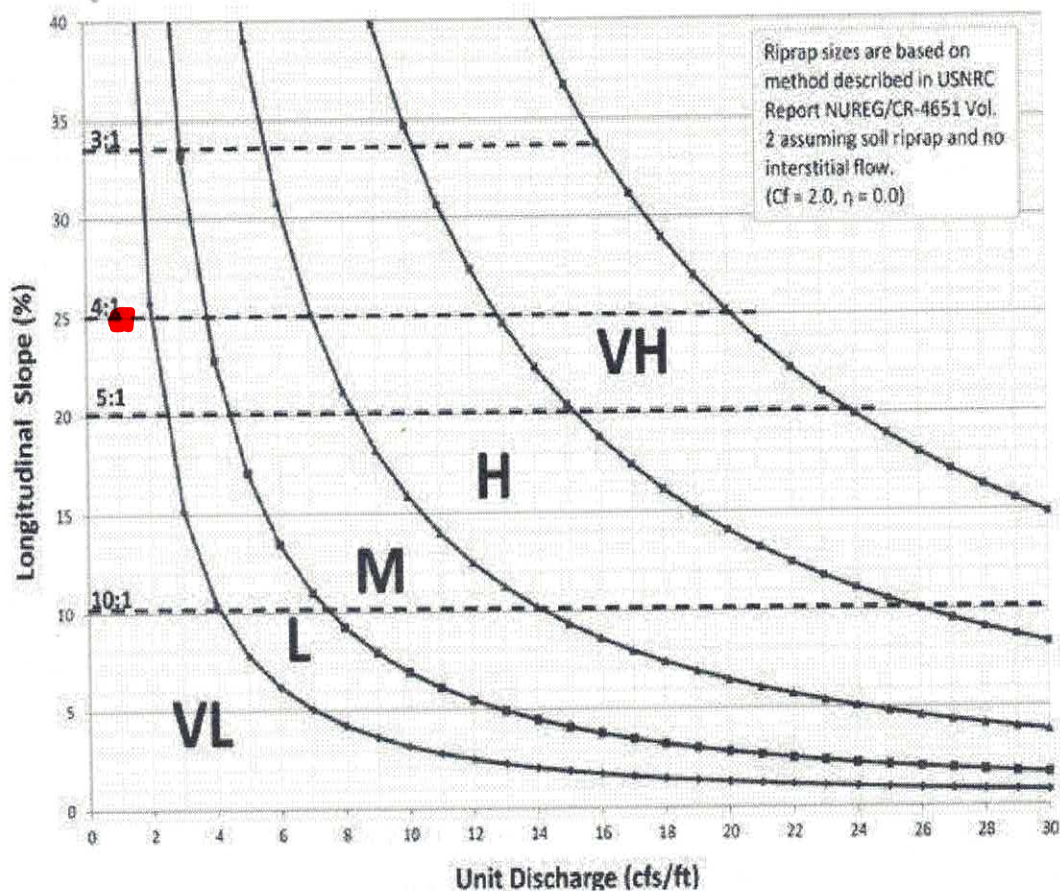


Figure 13-12d. Riprap Types for Emergency Spillway Protection

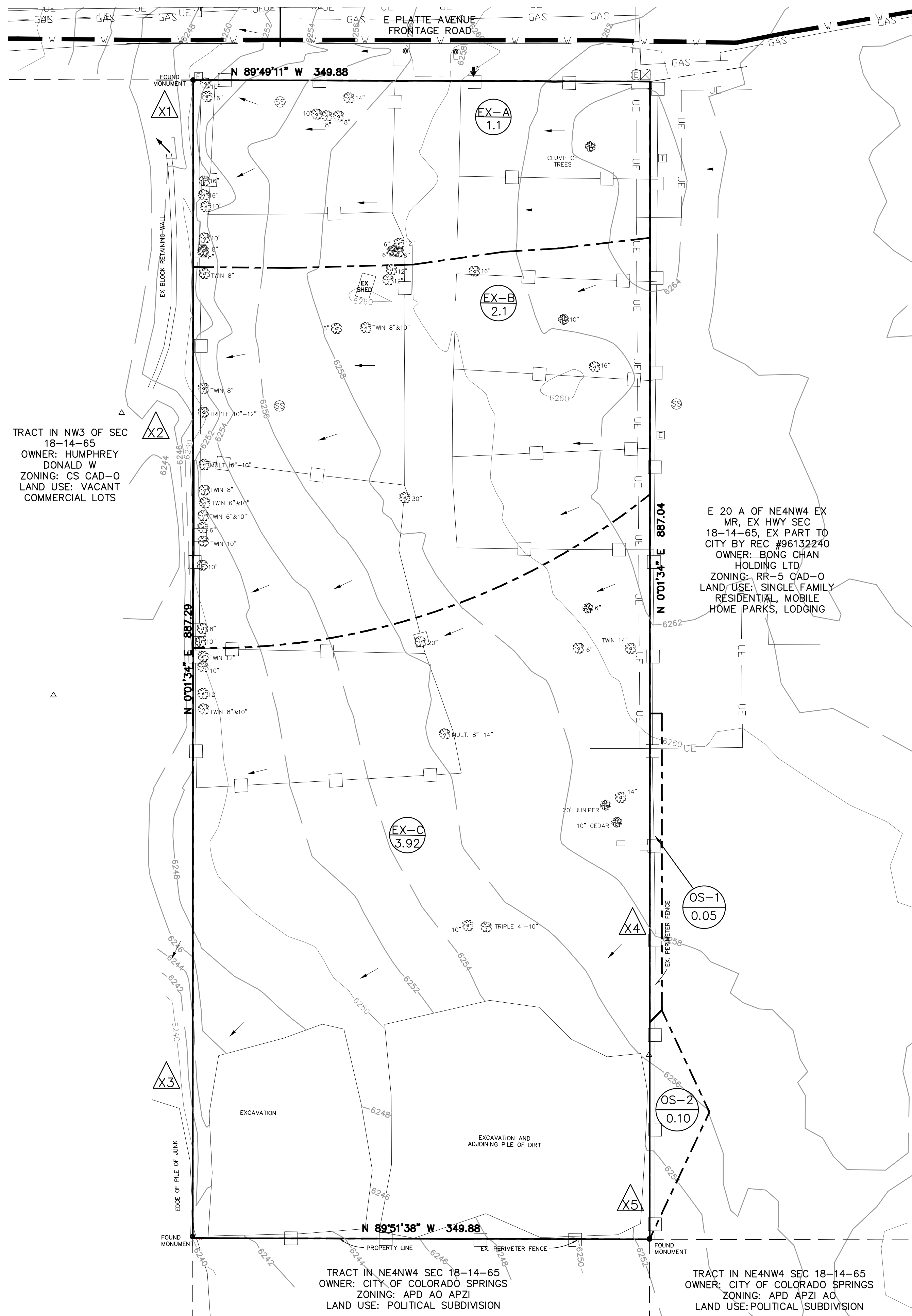


DRAINAGE MAPS

HCD PROPERTIES MINOR SUBDIVISION

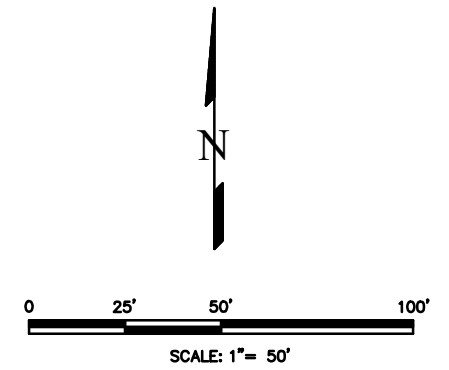
6201 EAST PLATTE AVE

EXISTING DRAINAGE MAP



DRAINAGE SUMMARY			
BASIN NAME	AREA (ACRES)	FLOW	
		5 YR (cfs)	100 YR (cfs)
EX-A	1.10	1.83	4.62
EX-B	2.10	2.20	7.14
EX-C	3.92	0.16	0.88
OS-1	0.05	0.02	0.14
OS-2	0.10	0.03	0.25
TOTAL		7.27	

DESIGN POINT SUMMARY				
DP	CONTRIBUTING BASINS	AREA AC.	Q5 CFS	Q100 CFS
X1	EX-A	1.10	1.83	4.62
X2	EX-B	2.10	2.20	7.14
X3	EX-C, OS-1, OS-2	4.07	0.21	1.27
X4	OS-1	0.05	0.02	0.14
X5	OS-2	0.10	0.03	0.25



- LEGEND**
- EX-B 12.22 BASIN DESIGNATION
 - 1 AREA IN BASIN (AC)
 - 1 PIPE RUN
 - 2 DESIGN POINT
 - BASIN BOUNDARY
 - 6132 EXISTING MINOR CONTOUR
 - 6130 EXISTING MAJOR CONTOUR
 - GROUND SURFACE FLOW DIRECTION

REVISIONS

NO.	DESCRIPTION	DATE

UNTIL SUCH TIME AS THESE DRAWINGS ARE APPROVED BY THE APPROPRIATE REVIEWING AGENCIES, THIS DRAWING IS NOT TO BE USED FOR THE PURPOSES DESIGNATED BY WRITTEN AUTHORIZATION.

PREPARED FOR:
T-BONE CONSTRUCTION
ATTN:
1310 FORD STREET
COLORADO SPRINGS, CO 80915
(719) 570-1456

Terra Nova
Engineering, Inc.
Creative Civil Engineering

721 S. 23RD ST.
COLORADO SPRINGS, CO 80904
OFFICE: 719-635-6422
FAX: 719-635-6426
www.tnec.com

HCD PROPERTIES MINOR SUBDIVISION
6201 E PLATTE AVE.

EXISTING DRAINAGE MAP

DESIGNED BY JF
DRAWN BY JF
CHECKED BY LD

H-SCALE AS NOTED
V-SCALE N/A

JOB NO. 1895.00
DATE ISSUED 7/20/21
SHEET NO. 1 OF 2

N:\job\1895\00\Drawings\189500 DRAINAGE MAPS.dwg, 7/21/2021 3:40:11 PM, DWG To PDF.p3

HCD PROPERTIES MINOR SUBDIVISION

6201 EAST PLATTE AVE

PROPOSED DRAINAGE MAP

DRAINAGE SUMMARY

BASIN NAME	AREA (ACRES)	FLOW	
		5 YR (cfs)	100 YR (cfs)
A	1.36	5.26	10.67
B	0.71	2.58	5.35
C	0.54	1.59	3.47
D	0.26	0.82	1.74
E	0.35	1.20	2.48
F	0.29	1.03	2.10
G	0.35	1.20	2.48
H	0.20	0.71	1.46
I	0.96	0.26	1.95
J	1.82	1.81	5.37
K	0.16	0.09	0.45
L	0.06	0.23	0.47
M	0.06	0.19	0.41
OS-1	0.05	0.02	0.12
OS-2	0.10	0.03	0.23

1895.00 HCD DRILLING

Surface Routing

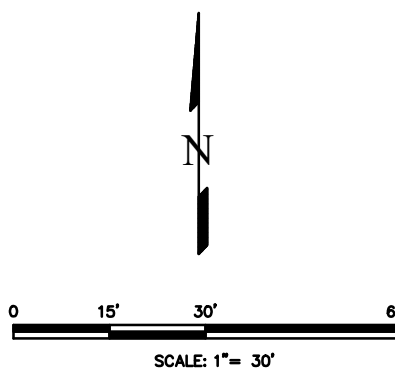
EXISTING CONDITIONS									
Design Point(s)	Contributing Basins	Area (Acres)	Equivalent CA ₅	Equivalent CA ₁₀₀	Maximum T _c	Intensity I ₅	Intensity I ₁₀₀	Flow Q ₅	Flow Q ₁₀₀
X1	EX-A	1.10	0.47	0.69	11.4	3.9	6.7	1.83	4.62
X2	EX-B	2.10	0.62	1.19	14.4	3.5	6.0	2.20	7.14
X3	EX-C, OS-1, OS-2	4.07	0.05	0.15	15.2	3.4	5.9	0.21	1.27
X4	OS-1	0.05	0.00	0.02	7.7	4.4	7.9	0.02	0.14
X5	OS-2	0.10	0.01	0.04	10.1	4.1	7.0	0.03	0.25

PROPOSED CONDITIONS									
Design Point(s)	Contributing Basins	Area (Acres)	Equivalent CA ₅	Equivalent CA ₁₀₀	Maximum T _c	Intensity I ₅	Intensity I ₁₀₀	Flow Q ₅	Flow Q ₁₀₀
1	A	1.36	1.05	1.18	5.0	5.0	9.1	5.26	10.67
2	B	0.76	0.52	0.59	5.0	5.0	9.1	2.58	5.35
3	C	0.54	0.33	0.40	5.6	4.9	8.8	1.59	3.47
4	D	0.26	0.16	0.19	5.0	5.0	9.1	0.82	1.74
5	E	0.35	0.24	0.27	5.0	5.0	9.1	1.20	2.48
6	F	0.29	0.21	0.23	5.0	5.0	9.1	1.03	2.10
7	G	0.35	0.24	0.27	5.0	5.0	9.1	1.20	2.48
8	H	0.20	0.14	0.16	5.0	5.0	9.1	0.71	1.46
9	I, OS-2	1.06	0.08	0.37	27.2	2.6	4.3	0.22	1.59
10	J, OS-1	1.87	0.52	0.91	24.7	2.7	4.5	1.42	4.12
11	K	0.16	0.02	0.06	9.4	4.1	7.2	0.09	0.45
12	L	0.06	0.05	0.05	5.0	5.0	9.1	0.23	0.47
13	M	0.06	0.04	0.05	5.0	5.0	9.1	0.19	0.41
14	OS-1	0.05	0.00	0.02	10.4	4.0	7.0	0.02	0.12
15	OS-2	0.10	0.01	0.04	11.8	3.8	6.6	0.03	0.23

DEVELOPED CONDITIONS

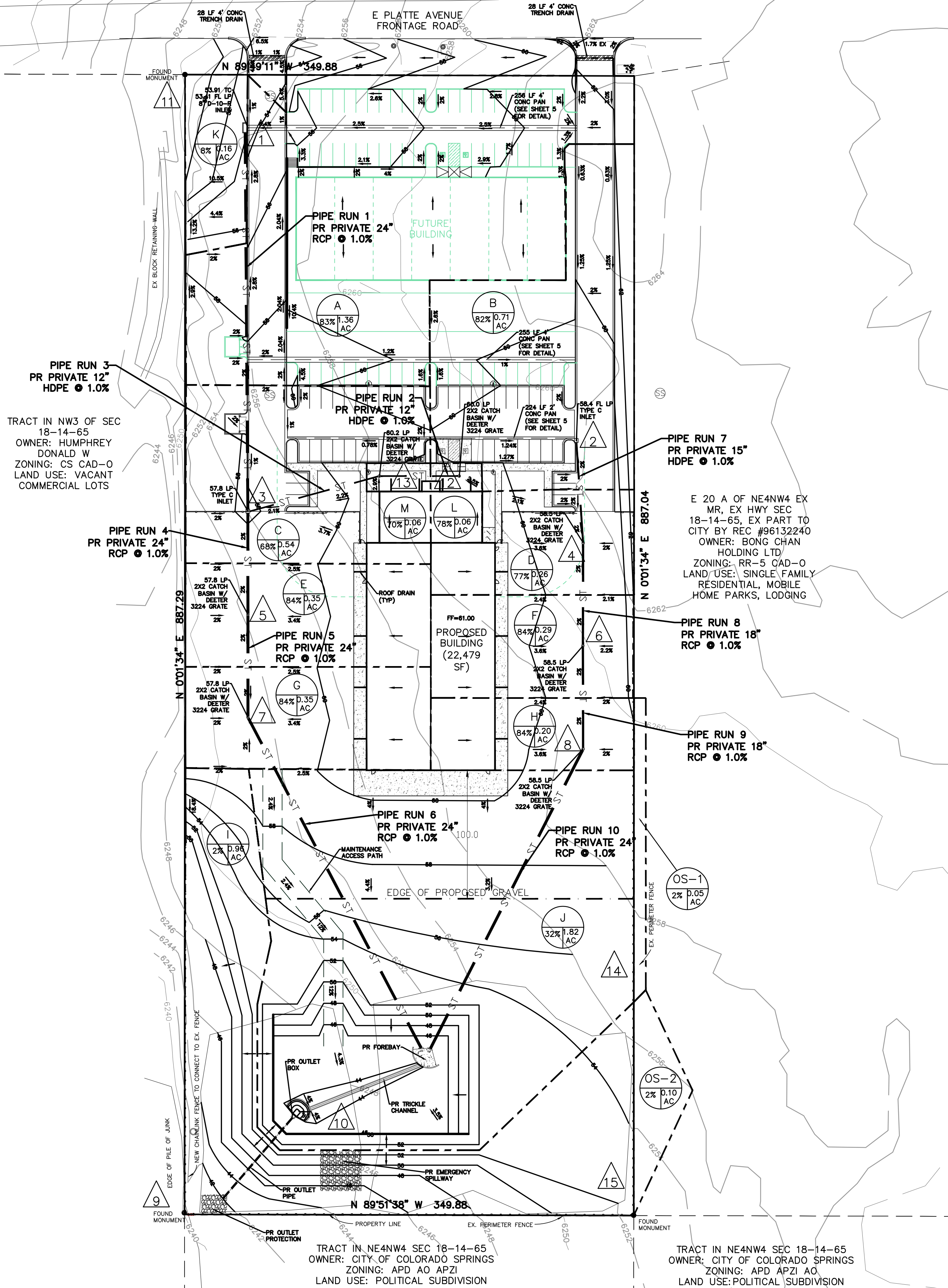
Pipe Run(s)	Contributing Design Points/Pipe Runs	Area (Acres)	Equivalent CA ₅	Equivalent CA ₁₀₀	Maximum T _c	Intensity		Flow		
						I ₅	I ₁₀₀	Q ₅	Q ₁₀₀	
1	DP 1	1.36	1.05	1.18	5.0	5.0	9.1	5.3	10.7	24" RCP PRIVATE
2	DP 12	0.06	0.05	0.05	5.0	5.0	9.1	0.2	0.5	12" HDPE PRIVATE
3	DP 13, PR 2	0.12	0.08	0.10	5.0	5.0	9.1	0.4	0.9	12" HDPE PRIVATE
4	DP 3, PR 3, PR 1	2.02	1.46	1.67	5.0	5.0	9.1	7.3	15.1	24" RCP PRIVATE
5	DP 5, PR 4	2.37	1.70	1.94	5.0	5.0	9.1	8.5	17.6	24" RCP PRIVATE
6	DP 7, PR 5	2.72	1.94	2.22	5.0	5.0	9.1	9.7	20.1	24" RCP PRIVATE
7	DP 2	0.71	0.52	0.59	5.0	5.0	9.1	2.6	5.3	15" HDPE PRIVATE
8	DP 4, PR 7	0.97	0.68	0.78	5.0	5.0	9.1	3.4	7.1	18" RCP PRIVATE
9	DP 6, PR 8	1.26	0.88	1.01	5.0	5.0	9.1	4.4	9.2	18" RCP PRIVATE
10	DP 8, PR 9	1.46	1.03	1.17	5.0	5.0	9.1	5.1	10.6	24" RCP PRIVATE
11	POND OUTLET							0.2	3.5	18" RCP PRIVATE

NOTE: All drainage structures are PRIVATE unless otherwise labeled.



LEGEND

- OS-2 2% 0.10 AC BASIN DESIGNATION
- PERCENT IMPERVIOUSNESS
- 1 PIPE RUN
- 2 DESIGN POINT
- BASIN BOUNDARY
- 6132 EXISTING MINOR CONTOUR
- 6130 EXISTING MAJOR CONTOUR
- GROUND SURFACE FLOW DIRECTION



REVISIONS

NO.	DESCRIPTION	DATE

UNTIL SUCH TIME AS THESE DRAWINGS ARE APPROVED BY THE APPROPRIATE REVIEWING AGENCIES, THIS DRAWING IS NOT TO BE USED FOR ANY PURPOSES DESIGNATED BY WRITTEN AUTHORIZATION.

PREPARED FOR:
T-BONE CONSTRUCTION
ATTN:
1310 FORD STREET
COLORADO SPRINGS, CO 80915

Terra Nova
Engineering, Inc.
Creative Civil Engineers

721 S. 23RD ST.
COLORADO SPRINGS, CO 80904
OFFICE: 719-635-6422
FAX: 719-635-6426
www.terrano.com

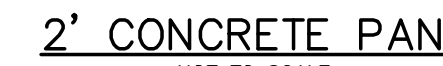
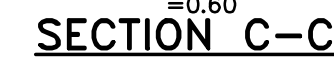
HCD PROPERTIES MINOR SUBDIVISION
6201 E PLATTE AVE.

PROPOSED DRAINAGE MAP

DESIGNED BY JF
DRAWN BY JF
CHECKED BY LD

H-SCALE AS NOTED
V-SCALE N/A

JOB NO. 1895.00
DATE ISSUED 7/21/21
SHEET NO. 2 OF 2



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721 S. 23RD ST
COLORADO SPRINGS, CO 80904

OFFICE: 719-635-6422
FAX: 719-635-6426
www.tnesinc.com

6201 E PLATIE AVE.

DETAIL SHEET

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DRAWN BY JF
CHECKED BY LD
- SCALE
- SCALE
DOB NO. 1895.00
DATE ISSUED 7/19/21
SHEET NO. 5 OF 8