



## Flying Horse North Master Development Drainage Plan

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HR Green Project No: 211030.01

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## Engineer's Statement

This report and plan for the drainage design of the development, Flying Horse North, was prepared by me (or under my direct supervision) and is correct to the best of my knowledge and belief. Said report and plan has been prepared in accordance with the *El Paso County Drainage Criteria* Manual and is in conformity with the master plan of the drainage basin. I understand that El Paso County does not and will not assume liability for drainage facilities designed by others. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.

9/20/2022

Gregory Panza, PE

Date

State of Colorado No. 37081

For and on behalf of HR Green Development, LLC

## Developer's Statement

I, the developer, have read and will comply with all of the requirements specified in this drainage report and plan.

Flying Horse Development, LLC

By: \_\_\_\_\_

Title: \_\_\_\_\_

Address: \_\_\_\_\_

\_\_\_\_\_

## El Paso County:

Filed in accordance with the requirements of the El Paso County Land Development Code, Drainage Criteria Manual, Volumes 1 and 2 and the Engineering Criteria Manual, as amended.

\_\_\_\_\_  
Jennifer Irvine, P.E.

\_\_\_\_\_  
Date

County Engineer/ECM Administrator

# Master Development Drainage Plan – Flying Horse North

## I. General Purpose, Location and Description

### a. Purpose and Scope

The Purpose of this Master Development Drainage Plan (MDDP) is to describe the onsite and offsite drainage patterns, existing and proposed storm infrastructure as it relates to preliminary water quality and stormwater detention, areas tributary to the site and the planned storm water management for the Flying Horse North development for Filings No. 2, 3 and remaining filings. Flying Horse North Filing No. 1 combined Preliminary Drainage Report (PDR) and Final Drainage Report (FDR) was previously written by Classic Engineering and included in Appendix F. The items discussed in this report are preliminary in nature and final drainage calculations and design will be required as development proceeds. This report provides a general drainage concept and guidance for future development of Flying Horse North.

### b. DBPS Investigations

Flying Horse North is split by the Arkansas River Basin and South Platte Basin. Within each of those river basins, the site stretches across the Black Squirrel Basin and East Cherry Creek Drainage Basins.

The Black Squirrel Drainage Basin Planning Study (DBPS) Preliminary Design Report prepared by URS Corporation was reviewed to determine existing plans and constraints that would influence the design of the Flying Horse North Development. The proposed plans for Flying Horse North are in general conformance with the DBPS.

Currently Flying Horse North Filing 1 is located within a major portion of the Black Squirrel Creek Drainage Basin of the development. A Preliminary Drainage Report and Final Drainage Report for this area was prepared in June 2018 by Classic Consulting and it is the intent of this MDDP to follow the general drainage approach for this area where densities for the development will remain similar to the report.

For the portion of Flying Horse North which lies within the East Cherry Creek Drainage Basin, a DBPS does not currently exist and the MDDP will comply with standard El Paso County regulations regarding drainage within this corridor.

### c. Stakeholder Process

There are no amendments to the current DBPS.

### d. Agency Jurisdictions

Listed below are the jurisdictions that this project will conform to:

El Paso County

Federal Emergency Management Agency

### e. General Project Description

Flying Horse North is in El Paso County. The development is bordered by Highway 83 to the west, Black Forest Road to the east, Cathedral Pines to the south, and High Forest Ranch to the north. The area contains approximately 1,459 acres within the whole Section 36, Township 11 South, Range 66 West of

the Sixth Principal Meridian, and a portion of Section 30 and 31, Township 11 South, and Range 65 West of the Sixth Principal Meridian.

This MDDP will cover approximately 912.5 acres of 973 residential units, which is shown in the figure below. This development will include estate lots, low through high density residential lots, commercial development, an 18-acre hotel site, open space and park areas, fitness center and a clubhouse.

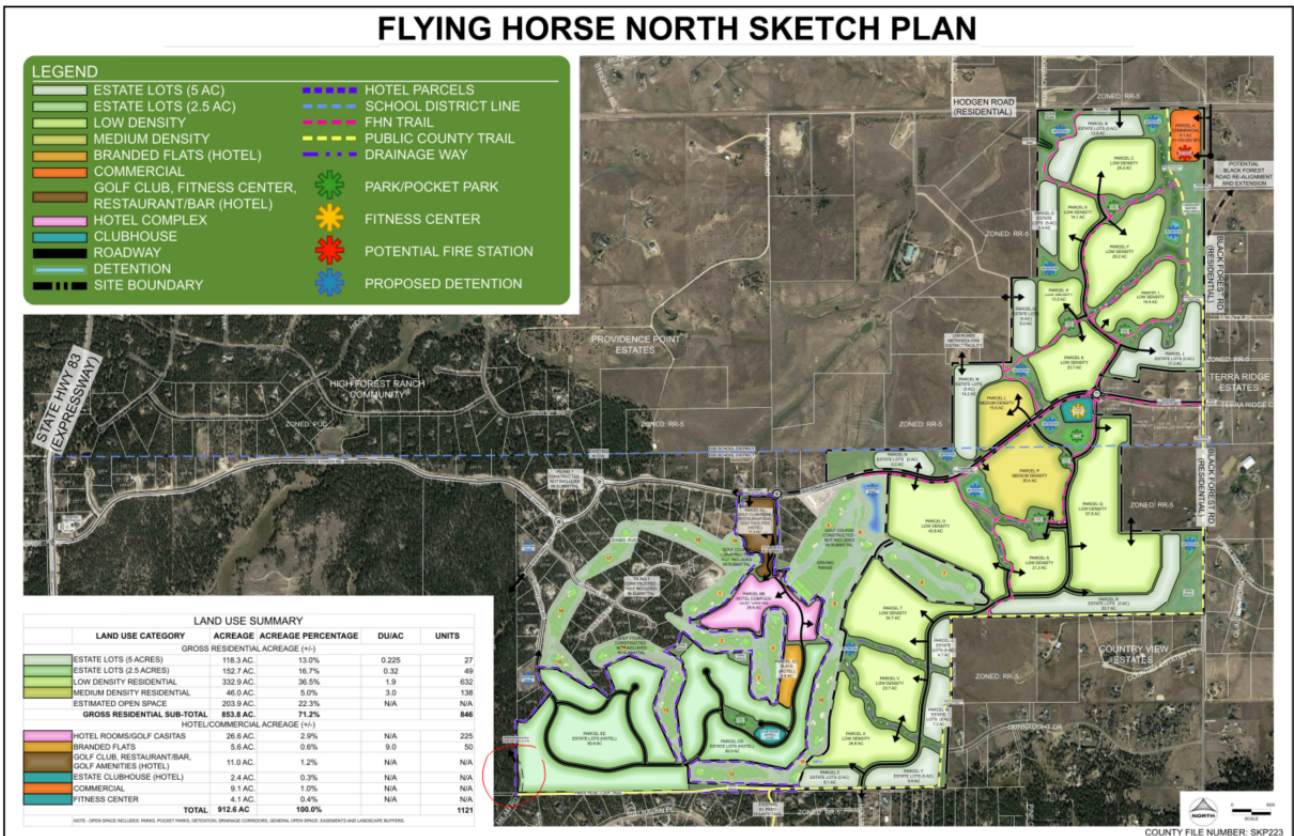


Figure 1 - Site Map

## f. Data Sources

Listed Below are the technical resources reviewed in the preparation of this MDDP:

El Paso County Drainage Criteria Manual (DCM)

Mile High Flood District

NOAA Atlas 14

NRCS Soil Survey for El Paso County Area, Colorado

FEMA FIRM 08041C0305G and FIRM 08041C0315G (eff. 12/7/2018)

El Paso County Assessor Property Records

Preliminary Drainage Report for Flying Horse North Preliminary Plan and Final Drainage Report for Flying Horse North Filing No. 1 – June 2018

Flying Horse North Irrigation Reservoir Embankment Design Report – August 2018

## g. Applicable Criteria and Standards

Per the DBPS and El Paso County Criteria Manual, flows from the proposed site will be limited to historic flows to maintain the stability of the existing channels within the drainage basins. The master plan follows the Drainage Criteria Manual for El Paso County which refers to the City of Colorado Springs Drainage Criteria Manuals as amended.

# II. Project Characteristics

## a. Location in Drainage Basin, Offsite Flows, Size

Flying Horse North is located within both the Black Squirrel Drainage Basin and East Cherry Creek Basin. Predominantly, the existing Filing No.1 and part of the proposed Filing No. 2 is located within the Black Squirrel Drainage Basin. This drainage basin encompasses 10.9 square miles of mostly forested area and generally slopes from east to west and outfalls into Monument Creek. Black Squirrel is a sub-basin of the Arkansas River. The remaining filings and part of Filing No. 2 is located within the East Cherry Creek Basin. There is not a current planning study of the drainage basin, but generally it slopes from southwest to northeast. The basin eventually flows into the South Platte River.

As the site generally lies at the top of each of the respective basins, minimal offsite flows are conveyed onto the site. The Black Squirrel Creek Drainage basin has no offsite flow come onto the site sans those flows generated as part of Filing 1 of Flying Horse North. The development which is within the Black Squirrel Creek Drainage Basin is unchanged from the FDR shown in Filing 1.

For the East Cherry Creek basin, 4 drainage basins are conveyed onto the site on the southwestern portion of the basin. These basins are labeled A, C, F and Q. The respective contributing flows from these basins is shown in the table below:

| Basin Name | Acreage | 5 Year Flow (cfs) | 100 Year Flow (cfs) |
|------------|---------|-------------------|---------------------|
| A          | 18.99   | 20.84             | 43.83               |
| C          | 36.39   | 33.36             | 71.27               |
| F          | 25.25   | 24.27             | 51.63               |
| Q          | 72.29   | 64.68             | 137.80              |

These four basins are generally conveyed through the development via natural drainage ways. The proposed ponds discussed later within this report have been sized to pass through the offsite flows.

## b. Compliance with DBPS

This MDDP is in general conformance with the guidelines outlined in the Black Squirrel DBPS and current drainage flows of the East Cherry Creek Basin. Flying Horse North will construct multiple full spectrum detention facilities to limit the effects of development and mimic natural flow patterns.

Existing downstream infrastructure is currently limited to the historic drainage channels and minimal downstream improvements exist. As such, the site follows the DBPS and restricts offsite flow rates to not exceed historic flow rates. The sites ultimate outfalls will generally be along the same historic tributaries. Although outfall rates will be at or below historic, the cumulative volume of runoff will increase and therefore downstream facilities may see an increase in the duration of flows. This may provide a net benefit to the downstream facilities by providing more water to assist with the sustenance of vegetation however it should be noted that increased volume may expedite potential erosion or channel movement.

### c. Site Characteristics

Per the NRCS web soil survey, the site is made up entirely of Type B soils. The ridge line between the Arkansas River and South Platte River Basins creates different soil environments for each. The portion of site that is within the Black Squirrel Drainage Basin, which includes Flying Horse North Filing No. 2 and No. 3, are predominately Elbeth sandy loam. The remaining filings are within the East Cherry Creek Basin which consists of Peyton sandy loam and Peyton-Pring complex. See Appendix A for the NRCS soil map.

Current ground cover varies between the two basins as well. Filings No. 2 and 3 are predominantly covered by Ponderosa Pine trees as a part of Black Forest and pasture. The remaining filings are short-to mid-grass prairie grasslands and former farmland which consists of non-native weeds and grasses. This portion of the site has very few, if any, trees and a minimal number of shrubs are found on the site.

### d. Major Drainage Ways and Structures

No major drainage ways exist within the development; however, small tertiary tributaries are within the site currently and function to convey flows to unnamed tributaries of the East Cherry Creek and Black Squirrel Creek. Additionally, as part of the Flying Horse North Filing 1 development, a large irrigation pond was built for water storage and flood control. This drains to the north and to the aforementioned unnamed tributary.

Existing minor drainage channels within the site are planned to be maintained to the maximum extent possible within parkways and greenways with the development. These will continue to be used for conveyance of storm drainage flows.

The Franktown Parker Dam (080130) is located near the northwest corner of site. The dam is designated as a jurisdictional dam and has a low hazard class. It is located along East Cherry Creek. See Appendix A for characteristics and location of dam.

### e. Existing and proposed land uses

The existing site is open rangeland on the eastern portion of the site and the western site is single family homes on large (~2.5 acre) home site within a heavily forested area. As part of Filing 1, a road was constructed along with facilities to support a golf course. Structures, outside of the homes are scattered throughout the overall development which will either be removed as part of the project or were built as part of Filing 1. The proposed development will consist of estate, low and medium lots, along with a future hotel site and multiple green spaces and small parks. The current land plan assumes approximately 897 dwelling units will be constructed on the site, not including an approximate 225 provided the proposed hotel.

| Land Use                | MAX DU/AC |
|-------------------------|-----------|
| Estate Lots (2.5 Acres) | 0.32      |
| Estate Lots (5 Acres)   | 0.2       |
| Low                     | 1.9       |
| Medium                  | 3.0       |



### III. Hydrologic Analysis

#### a. Major Basins and subbasins

##### Major Basin Description

- Previous basin study: Black Squirrel Drainage Basin Planning Study
- Per FEMA FIRM 08041C0305G and 08041C0315G (eff. 12/7/2018), Flying Horse North has the East Cherry Creek run through the northwest portion of the site. Currently, FEMA shows a LOMR effective April 4<sup>th</sup>, 2019 Base Flood Elevations and Zone A. Per the El Paso County Land Development Code Chapter 8 Section 8.4.2.B.1.e.i, the base flood elevations for Zone A will be determined once the platted lots are solidified and are confirmed within 300-ft of the current floodplain designation. Certification of the flood elevations will be via the FEMA CLOMR/LOMR process or Floodplain Certification Letter.
- There is a large irrigation pond that accounts for water storage and water control on the east side of the site.

The site has been divided into several major drainage basins per where each basin is tributary to a full spectrum detention pond facility. These basins and associated sub basins are described in more detail in the next section of this report.

##### Existing Subbasin Description

The site's flows are split by the major ridgeline of the Arkansas River Basin and South Platte Basin. Within the South Platte Basin, flow is generally carried northeast throughout the site. On the other side of the ridgeline, the Arkansas River Basin flows in a southwest direction. Subbasin IDs with single letters are part of the South Platte Basin and Subbasin IDs with double letters are part of the Arkansas River Basin.

- Subbasin A is located off site and on the southeast corner. The basin drains towards the northwest and towards Subbasin B1. The basin is 18.99 acres, with a composite impervious value of 2.00% and runoff rates for the 5 and 100 year of 20.84 cfs and 43.83 cfs respectively.
- Subbasin B is located north of Subbasin A. The basin drains towards the northwest into a natural drainageway that flows directly to an existing irrigation pond. The basin is 59.74 acres, with a composite impervious value of 2.00% and runoff rates for the 5 and 100 year of 103.48 cfs and 221.28 cfs respectively.
- Subbasin C is located off site and on the southeast corner. The basin drains towards the northwest and towards Subbasin B2. The basin is 36.39 acres, with a composite impervious value of 2.00% and runoff rates for the 5 and 100 year of 33.36 cfs and 71.27 cfs respectively.
- Subbasin D is located north of Subbasin B. The basin drains towards the northwest and towards the existing irrigation pond. The basin is 38.84 acres, with a composite impervious value of 2.00% and runoff rates for the 5 and 100 year of 31.56 cfs and 67.84 cfs respectively.
- Subbasin E is in a central location of the site and includes the existing irrigation pond. The basin drains towards the north and towards existing irrigation pond. The basin is 106.53 acres, with a composite impervious value of 2.00% and runoff rates for the 5 and 100 year of 223.69 cfs and 483.10 cfs respectively.

- Subbasin F is located off site and on the southeast corner. The basin drains towards the northwest and towards Subbasin G. The basin is 25.25 acres, with a composite impervious value of 2.00% and runoff rates for the 5 and 100 year of 24.27 cfs and 51.63 cfs respectively.
- Subbasin G is directly north of Subbasin D and east of Subbasin E. The basin drains towards the northwest and towards Subbasin E with the irrigation pond. The basins consist of the existing golf course. The basin is 52.19 acres, with a composite impervious value of 2.00% and runoff rates for the 5 and 100 year of 79.17 cfs and 166.51 cfs respectively.
- Subbasin H is located directly downstream of Subbasin E and on the north side of Stagecoach Rd. The basin drains towards the north through a natural drainageway. There are existing lots on the west side of the basin. The basin is 20.63 acres, with a composite impervious value of 2.00% and runoff rates for the 5 and 100 year of 18.59 cfs and 39.78 cfs respectively.
- Subbasin I is located west of Subbasin E and northeast of the major ridgeline between basins. The basin drains towards the northwest and towards an existing culvert. There are existing lots on the west side of the basin. The basin is 31.93 acres, with a composite impervious value of 2.00% and runoff rates for the 5 and 100 year of 34.58 cfs and 72.63 cfs respectively.
- Subbasin J is located downstream of Subbasin I. The basin drains towards the northeast to an unnamed tributary of the East Cherry Creek. The basin is 28.47 acres, with a composite impervious value of 2.00% and runoff rates for the 5 and 100 year of 56.31 cfs and 120.46 cfs respectively.
- Subbasin K is located south of proposed section of Stagecoach Rd. The basin drains towards the northwest and into an existing 48" culvert. The basin is 93.15 acres, with a composite impervious value of 2.00% and runoff rates for the 5 and 100 year of 92.05 cfs and 195.43 cfs respectively.
- Subbasin L is downstream of Subbasin K and is located on the north side of the proposed section of Stagecoach Rd. The basin drains towards the northwest to a natural drainageway of East Cherry Creek. The basin is 16.39 acres, with a composite impervious value of 2.00% and runoff rates for the 5 and 100 year of 107.58 cfs and 228.73 cfs respectively.
- Subbasin M is located on the east side of the site and between Subbasin N and V1. The basin drains towards the northwest and into an existing 30" culvert. The basin is 13.85 acres, with a composite impervious value of 2.00% and runoff rates for the 5 and 100 year of 11.48 cfs and 24.61 cfs respectively.
- Subbasin N is located south of Subbasin O and north of proposed Stagecoach Rd. The basin drains towards the northwest to a nearby unnamed tributary and eventually East Cherry Creek. The basin is 49.00 acres, with a composite impervious value of 2.00% and runoff rates for the 5 and 100 year of 64.68 cfs and 143.11 cfs respectively.
- Subbasin O is located south of Subbasin P. The basin drains towards the northwest and towards the north. The basin is 24.76 acres, with a composite impervious value of 2.00% and runoff rates for the 5 and 100 year of 22.69 cfs and 48.54 cfs respectively.
- Subbasin P is in the northeast corner of the site and downstream of Subbasin O. The basin drains towards the northeast to an unnamed tributary of East Cherry Creek. The basin is 43.80 acres, with a composite impervious value of 2.00% and runoff rates for the 5 and 100 year of 38.52 cfs and 82.17 cfs respectively.



- Subbasin Q is located off site and on the southeast corner. The basin drains towards the northeast and towards Subbasin R. The basin is 72.29 acres, with a composite impervious value of 2.00% and runoff rates for the 5 and 100 year of 64.68 cfs and 137.80 cfs respectively.
- Subbasin R is located on the east side of site adjacent to Black Forest Rd. The basin drains towards the northeast. The basin is 54.98 acres, with a composite impervious value of 2.00% and runoff rates for the 5 and 100 year of 108.65 cfs and 232.13 cfs respectively.
- Subbasin S is located north of Subbasin Q. The basin drains towards the southeast and overland towards Subbasin R. The basin is 24.36 acres, with a composite impervious value of 2.00% and runoff rates for the 5 and 100 year of 25.99 cfs and 54.65 cfs respectively.
- Subbasin T is located off site and on the southeast corner. The basin drains towards the southeast and towards Black Forest Rd. The basin is 5.24 acres, with a composite impervious value of 2.00% and runoff rates for the 5 and 100 year of 4.04 cfs and 8.68 cfs respectively.
- Subbasin U is located east of subbasin V and is composed of existing 2.5 acre lots. The basin drains offsite towards the southeast and follows historic drainage patterns. The basin is 5.86 acres, with a composite impervious value of 10.00% and runoff rates for the 5 and 100 year of 4.15 cfs and 8.95 cfs respectively.
- Subbasin V is located on the east side of the site in between Subbasin M and U. The basin drains towards the north and towards Subbasin X via culvert. The basin is 38.57 acres, with a composite impervious value of 2.00% and runoff rates for the 5 and 100 year of 29.63 cfs and 63.92 cfs respectively.
- Subbasin W is located north of Subbasin U on the site. The basin drains offsite through an existing 24" CMP culvert. The basin is 3.96 acres, with a composite impervious value of 2.00% and runoff rates for the 5 and 100 year of 3.45 cfs and 7.33 cfs respectively.
- Subbasin X is located on the northeastern corner of the site. The basin drains north towards an unnamed tributary of East Cherry Creek. The basin is 190.88 acres, with a composite impervious value of 2.00% and runoff rates for the 5 and 100 year of 167.76 cfs and 361.56 cfs respectively.
- Subbasins AA and CC are located on the west side of the site along the major ridgeline. Both basins were developed in Filing No. 1 and are included in the analysis to provide a better understanding for the flows draining towards Black Squirrel Creek. The basins drain towards the southwest. The basins are 33.8 acres and 37.15 acres, with a composite impervious value of 10% and 10% and runoff rates for the 5 and 100 year of 38.76 cfs and 80.22 cfs and 6.53 cfs and 13.57 cfs respectively.
- Subbasin BB is located downstream of Subbasin AA. The basin drains towards the southwest and towards Subbasin GG. A section of the area of the basin was developed in Filing No. 1 and consists of 2.5-acre lots. The basin is 37.15 acres, with a composite impervious value of 10.00% and runoff rates for the 5 and 100 year of 40.62 cfs and 84.15 cfs respectively.
- Subbasin DD is located west and downstream of Subbasin EE. The basin drains towards the west. A portion developed in Filing No. 1 consists of the Flying Horse North Golf Course and 2.5-acre lots. The basin is 70.07 acres, with a composite impervious value of 10.00% and runoff rates for the 5 and 100 year of 58.42 cfs and 123.69 cfs respectively.

- Subbasin EE is upstream of subbasin DD. The basin drains towards the west. A portion of the area was developed in Filing No. 1 consists of the Flying Horse North Golf Course and 2.5-acre lots. The basin is 69.47 acres, with a composite impervious value of 10.00% and runoff rates for the 5 and 100 year of 81.16 cfs and 167.45 cfs respectively.
- Subbasin FF is located downstream of Subbasins DD and EE. The basin drains towards the southwest. The north half consists of 2.5-acre lots and part of the Flying Horse North Golf Course constructed during Filing No. 1. The basin is 17.62 acres, with a composite impervious value of 10.00% and runoff rates for the 5 and 100 year of 162.77 cfs and 340.42 cfs respectively.
- Subbasin GG located downstream of Subbasin FF. The basin drains towards the southwest and towards an existing detention pond developed in Filing No. 1. The basin is 16.35 acres, with a composite impervious value of 10.00% and runoff rates for the 5 and 100 year of 14.93 cfs and 31.99 cfs respectively.
- Subbasin HH is located on the west side of the site. The basin drains towards the west and an unnamed tributary of Black Squirrel Creek. The basin is 12.61 acres, with a composite impervious value of 10.00% and runoff rates for the 5 and 100 year of 13.01 cfs and 27.42 cfs respectively.
- Subbasin II is located in the southwest corner of site. The basin drains towards the west and to an unnamed tributary of Black Squirrel. The basin is 97.53 acres, with a composite impervious value of 10.00% and runoff rates for the 5 and 100 year of 81.77 cfs and 175.60 cfs respectively.
- Subbasin JJ is in the southcentral part of the site. The basin drains towards the south and to an unnamed tributary of Black Squirrel Creek. The basin is 8.9 acres, with a composite impervious value of 2.00% and runoff rates for the 5 and 100 year of 9.74 cfs and 20.50 cfs respectively.
- Subbasin KK is in the southcentral part of the site. The basin drains towards the south and to an unnamed tributary of Black Squirrel Creek. A portion of the area is occupied by the existing Flying Horse Golf Course. The basin is 8.12 acres, with a composite impervious value of 2.00% and runoff rates for the 5 and 100 year of 7.51 cfs and 15.99 cfs respectively.
- Subbasin LL is in the southcentral part of the site. The basin drains towards the south and to an unnamed tributary of Black Squirrel Creek. The basin is 6.1 acres, with a composite impervious value of 2.00% and runoff rates for the 5 and 100 year of 6.88 cfs and 14.48 cfs respectively.

## Proposed Subbasin Description

- Subbasin A is located off site and on the southeast corner. The basin drains towards the northwest and towards Subbasin B1. The basin is 18.99 acres, with a composite impervious value of 2.00% and runoff rates for the 5 and 100 year of 20.84 cfs and 43.83 cfs respectively.
- Subbasin B1 is located north of Subbasin A. The basin drains towards the northwest and towards proposed Detention Pond 11. Current planning documents call for low density dwelling units. The basin is 59.74 acres, with a composite impervious value of 29.83% and runoff rates for the 5 and 100 year of 66.93 cfs and 133.69 cfs respectively.
- Subbasin B2 is located northeast of Subbasin B1. The basin drains towards the northwest and towards the proposed Detention Pond 11. Current planning documents call for low density dwelling units. The basin is 19.99 acres, with a composite impervious value of 24.55% and runoff rates for the 5 and 100 year of 17.99 cfs and 37.14 cfs respectively.
- Subbasin C is located off site and on the southeast corner. The basin drains towards the northwest and towards Subbasin B2. The basin is 36.39 acres, with a composite impervious value of 2.00% and runoff rates for the 5 and 100 year of 35.31 cfs and 75.28 cfs respectively.
- Subbasin D is located north of north of Subbasins B1 and B2. The basin drains towards the northwest and towards Detention Pond 15. Current planning documents call for low density dwelling units. The basin is 40.87 acres, with a composite impervious value of 37.20% and runoff rates for the 5 and 100 year of 61.12 cfs and 117.38 cfs respectively.
- Subbasin E is in a central location of the site and includes the existing irrigation pond. The basin drains towards the north and towards existing irrigation pond. Current planning documents call for two small parking lots. The basin is 106.53 acres, with a composite impervious value of 14.35% and runoff rates for the 5 and 100 year of 74.68 cfs and 157.91 cfs respectively.
- Subbasin F is located off site and on the southeast corner. The basin drains towards the northwest and towards Subbasin G. The basin is 25.25 acres, with a composite impervious value of 2.00% and runoff rates for the 5 and 100 year of 24.27 cfs and 51.63 cfs respectively.
- Subbasin G is directly north of Subbasin D and east of Subbasin E. The basin drains towards the northwest and towards Subbasin E. Current planning documents call for a small amount of low density dwelling units, where most of the basin consist of the existing golf course. The basin is 31.45 acres, with a composite impervious value of 12.48% and runoff rates for the 5 and 100 year of 27.18 cfs and 57.12 cfs respectively.
- Subbasin H is located located directly downstream of Subbasin E and on the north side of Stagecoach Rd. The basin drains towards the north and towards Detention Pond 10. Current planning documents call for medium density dwelling units. There are existing lots on the west side of the basin. The basin is 21.96 acres, with a composite impervious value of 10.00% and runoff rates for the 5 and 100 year of 17.86 cfs and 37.8 cfs respectively.
- Subbasin I is located west of Subbasin E and northeast of the major ridgeline between basins. The basin drains towards the northwest and towards proposed Detention Pond 16. There are existing lots on the west side of the basin. Current planning documents call for a commercial golf club. The basin is 28.99 acres, with a composite impervious value of 34.66% and runoff rates for the 5 and 100 year of 40.37 cfs and 78.06 cfs respectively

- Subbasin J is located downstream of Subbasin I. The basin drains towards the northeast to an unnamed tributary of the East Cherry Creek. Current planning documents do not call for any changes to this basin. The basin is 28.07 acres, with a composite impervious value of 10% and runoff rates for the 5 and 100 year of 24.25 cfs and 51.19 cfs respectively.
- Subbasin K is located south of proposed section of Stagecoach Rd. The basin drains towards the northwest and towards proposed Detention Pond 7. Current planning documents call for high, medium, and low density dwelling units and a few pocket parks. The basin is 114.73 acres, with a composite impervious value of 38.08% and runoff rates for the 5 and 100 year of 200.94 cfs and 382.3 cfs respectively
- Subbasin L is downstream of Subbasin K and is located on the north side of the proposed section of Stagecoach Rd. The basin drains towards the northwest into proposed Detention Pond 8. Current planning documents call for medium density dwelling units. The basin is 15.89 acres, with a composite impervious value of 24.82% and runoff rates for the 5 and 100 year of 15.97 cfs and 32.4 cfs respectively. The pond will discharge at predevelopment rates into an unnamed tributary of the East Cherry Creek via the ponds outlet structure.
- Subbasin M is located on the east side of the site and between Subbasin N and V1. The basin drains towards the northwest and towards proposed Detention Pond 6. Detention Pond 6 outlets into a culvert under proposed Stagecoach Rd. and eventually to Subbasin N. Current planning documents call for medium density dwelling units, potential fitness center, and a park. The basin is 26.83 acres, with a composite impervious value of 33.19% and runoff rates for the 5 and 100 year of 46.54 cfs and 89.08 cfs respectively.
- Subbasin N is located south of Subbasin O and North of proposed Stagecoach Rd. The basin drains towards the northwest towards proposed Detention Pond 5. Detention Pond 5 outlets to a nearby unnamed tributary and eventually East Cherry Creek. Current planning documents call for medium density dwelling units along with a pocket park. The basin is 41.57 acres, with a composite impervious value of 29.60% and runoff rates for the 5 and 100 year of 73.48 cfs and 141.24 cfs respectively.
- Subbasin O is located south of Subbasin P. The basin drains towards the northwest and towards Detention Pond 3. Current planning documents call for medium density dwelling units. The basin is 52.52 acres, with a composite impervious value of 30.10% and runoff rates for the 5 and 100 year of 63.86 cfs and 127.4 cfs respectively. The pond will discharge at predevelopment rates and into Pond 1 via a swale.
- Subbasin P is in the northeast corner of the site and downstream of Subbasin O. The basin drains towards the northeast to proposed Detention Pond 1. Current planning documents call for low density dwelling units. The basin is 43.71 acres, with a composite impervious value of 20.71% and runoff rates for the 5 and 100 year of 40 cfs and 82.83 cfs respectively. The pond will discharge at predevelopment rates into an unnamed tributary of the East Cherry Creek via the ponds outlet structure.
- Subbasin Q is located off site and on the southeast corner. The basin drains towards the northeast and towards Subbasin R. The basin is 72.29 acres, with a composite impervious value of 2.00% and runoff rates for the 5 and 100 year of 64.68 cfs and 137.8 cfs respectively.

- Subbasin R is located on the east side of site adjacent to Black Forest Rd. The basin drains towards the northeast and towards Detention Pond 9. Current planning documents call for low density and 1-acre lots. The basin is 76.38 acres, with a composite impervious value of 21.81% and runoff rates for the 5 and 100 year of 56.59 cfs and 116.06 cfs respectively. The pond will discharge at predevelopment rates into an unnamed tributary of the East Cherry Creek via the ponds outlet structure.
- Subbasin S is located north of Subbasin Q. The basin drains towards the southeast and overland towards Subbasin R. Current planning documents call for low density dwelling units. The basin is 21.67 acres, with a composite impervious value of 40.88% and runoff rates for the 5 and 100 year of 30.83 cfs and 58.96 cfs respectively.
- Subbasin T is located off site and on the southeast corner. The basin drains towards the southeast and towards Black Forest Rd. The basin is 5.24 acres, with a composite impervious value of 2.00% and runoff rates for the 5 and 100 year of 4.04 cfs and 8.68 cfs respectively.
- Subbasin U is located east of subbasin V2 and is composed of existing 2.5 acre lots. The basin drains offsite towards the southeast and follows historic drainage patterns. The basin is 5.86 acres, with a composite impervious value of 2% and runoff rates for the 5 and 100 year of 4.96 cfs and 10.51 cfs respectively.
- Subbasin V1 is located on the east side of the site in between Subbasin M and V2. The basin drains towards the north and towards Subbasin X3 via culvert. Current planning documents call for low density dwelling units. The basin is 11.57 acres, with a composite impervious value of 38.62% and runoff rates for the 5 and 100 year of 13.99 cfs and 27.67 cfs respectively.
- Subbasin V2 is located south of subbasin X3 and proposed Stagecoach Rd. The basin drains towards the north and towards subbasin X3. The flows are directed through a culvert and eventually to Detention Pond 4. There are no proposed dwelling unit for the area, as there are existing 2.5 acre lots that cover the basin. The basin is 15.34 acres, with a composite impervious value of 15.00% and runoff rates for the 5 and 100 year of 16.15 cfs and 33.25 cfs respectively.
- Subbasin W is located on the north side of subbasin U. The basin drains offsite to the southeast. The basin is 3.76 acres, with a composite impervious value of 10.00% and runoff rates for the 5 and 100 year of 3.58 cfs and 7.46 cfs respectively.
- Subbasin X1 is located on the northeastern corner of the site. The basin drains north towards proposed Detention Pond 2. Current planning documents call for low density dwelling units, potential fire station and a pocket park. The basin is 76.38 acres, with a composite impervious value of 29.50% and runoff rates for the 5 and 100 year of 80.91 cfs and 163.27 cfs respectively. The pond will discharge at predevelopment rates into an unnamed tributary of the East Cherry Creek via the ponds outlet structure.
- Subbasin X2 is located south of Subbasin X1 The basin drains towards the northeast towards proposed Detention Pond 4. Current planning documents call for low density dwelling units along with a pocket park. The basin is 36.33 acres, with a composite impervious value of 33.33% and runoff rates for the 5 and 100 year of 41.46 cfs and 82.46 cfs respectively.
- Subbasin X3 is located south of Subbasin X2. The basin drains towards the north and towards Detention Pond 4. Current planning documents call for low density dwelling units and a pocket

- park. The basin is 65.75 acres, with a composite impervious value of 13.53% and runoff rates for the 5 and 100 year of 47.59 cfs and 100.73 cfs respectively.
- Subbasins AA and CC are located on the west side of the site along the major ridgeline. Both basins were developed in Filing No. 1 and are included in the analysis to provide a better understanding for the flows draining towards Black Squirrel Creek. The basins drain towards the southwest. The basins are 33.8 acres and 37.15 acres, with a composite impervious value of 10% and 10% and runoff rates for the 5 and 100 year of 39.23 cfs and 81.18 cfs and 6.53 cfs and 13.57 cfs respectively.
  - Subbasin BB is located downstream of Subbasin AA. The basin drains towards the southwest and towards Subbasin GG. Current planning documents call for a small portion of 2.5-acre estate lots. The remaining area of the basin was developed in Filing No. 1 and consists of 2.5-acre lots. The basin is 37.15 acres, with a composite impervious value of 10.00% and runoff rates for the 5 and 100 year of 40.62 cfs and 84.15 cfs respectively.
  - Subbasin DD is located west and downstream of Subbasin EE1. The basin drains towards the west. Current planning documents call for 2.5-acre estate lots and a 2.4-acre clubhouse. The portion that was developed in Filing No. 1 consists of the Flying Horse North Golf Course and 2.5-acre lots. The basin is 69.5 acres, with a composite impervious value of 10.00% and runoff rates for the 5 and 100 year of 57.78 cfs and 122.41 cfs respectively.
  - Subbasin EE1 is located west of Subbasins EE2 and EE3. The basin drains towards the west. Current planning documents call for a small section of 2.5-acre estate lots. The remaining portion consists of the Flying Horse North Golf Course constructed in Filing No. 1. The portion that was developed in Filing No. 1 consists of the Flying Horse North Golf Course and 2.5-acre lots. The basin is 50.87 acres, with a composite impervious value of 10.00% and runoff rates for the 5 and 100 year of 53.25 cfs and 110.3 cfs respectively.
  - Subbasin EE2 is located along the west side of the major ridgeline. The basin drains towards the southeast and entirely towards proposed Detention Pond 13. Current planning documents call for a hotel complex/golf casitas. The basin is 16.36 acres, with a composite impervious value of 75.00% and runoff rates for the 5 and 100 year of 35.71 cfs and 63.62 cfs respectively. The pond will discharge at predevelopment rates into a swale via the ponds outlet structure.
  - Subbasin EE3 is located south of Subbasin EE2. The basin drains towards the west and Subbasin EE2. Current planning documents call for high density dwelling units. The basin is 16.36 acres, with a composite impervious value of 55.00% and runoff rates for the 5 and 100 year of 10.38 cfs and 19.33 cfs respectively.
  - Subbasin FF is located downstream of Subbasins DD and EE. The basin drains towards the southwest. Current planning documents call for 2.5-acre estate lots on the south side of the basin. The north half consists of 2.5-acre lots and part of the Flying Horse North Golf Course constructed during Filing No. 1. The basin is 18.1 acres, with a composite impervious value of 10.00% and runoff rates for the 5 and 100 year of 20.78 cfs and 43.07 cfs respectively.
  - Subbasin GG located downstream of Subbasin FF. The basin drains towards the southwest and towards an existing detention pond developed in Filing No. 1. Current planning documents call for



- 2.5-acre estate lots. The basin is 16.35 acres, with a composite impervious value of 10.00% and runoff rates for the 5 and 100 year of 15.49 cfs and 32.48 cfs respectively.
- Subbasin HH is located on the west side of the site. The basin drains towards the west and to an unnamed tributary of Black Squirrel Creek. Current planning documents call for 2.5-acre estate lots. The basin is 12.7 acres, with a composite impervious value of 10.00% and runoff rates for the 5 and 100 year of 13.56 cfs and 28.16 cfs respectively. Per El Paso County Engineering Criteria Manual – Appendix I Section 1.7.1.B, large lot single family sites greater than or equal to 2.5 acres in size and that have a maximum imperviousness of less than 20% are excluded from water quality capture volume (WQCV).
  - Subbasin II1 is located in the southwest corner of site. The basin drains towards the west and to proposed Detention Pond 14. Current planning documents call for 2.5-acre estate lots. The basin is 50.43 acres, with a composite impervious value of 10.00% and runoff rates for the 5 and 100 year of 34.94 cfs and 74.39 cfs respectively. The pond will discharge at predevelopment rates into an unnamed tributary of Black Squirrel Creek via the ponds outlet structure
  - Subbasin II2 is located north of Subbasin II1 and downstream of Subbasin II3 in the southwest corner of site. The basin drains towards the west and to Subbasin II1 via a proposed culvert. Current planning documents call for 2.5-acre estate lots. The basin is 23.13 acres, with a composite impervious value of 10.00% and runoff rates for the 5 and 100 year of 28.04 cfs and 57.88 cfs respectively.
  - Subbasin II3 is located north of Subbasin II1. The basin drains towards the west and to Subbasin II2 via a proposed culvert. Current planning documents call for 2.5-acre estate lots. The basin is 23.97 acres, with a composite impervious value of 10.00% and runoff rates for the 5 and 100 year of 28.32 cfs and 58.65 cfs respectively.
  - Subbasin JJ is in the southcentral part of the site. The basin drains towards the south and to an unnamed tributary of Black Squirrel Creek. Current planning documents call for low density and 1-acre dwelling units. The basin is 8.9 acres, with a composite impervious value of 20.70% and runoff rates for the 5 and 100 year of 11.49 cfs and 22.8 cfs respectively.
  - Subbasin LL is in the southcentral part of the site. The basin drains towards the south and to an unnamed tributary of Black Squirrel Creek. Current planning documents call for low density and 1-acre dwelling units. The basin is 6.2 acres, with a composite impervious value of 12.09% and runoff rates for the 5 and 100 year of 7.36 cfs and 15.07 cfs respectively.
  - Subbasin KK is in the southcentral part of the site. The basin drains towards the south and to an unnamed tributary of Black Squirrel Creek. Current planning documents call for 2.5 acre lots. The rest of the area is occupied by the existing Flying Horse Golf Course. The basin is 8.4 acres, with a composite impervious value of 10.00% and runoff rates for the 5 and 100 year of 8.14 cfs and 16.95 cfs respectively.

The above-mentioned basins are large planning area basins and as drainage reports are developed for the individual developed parcels additional drainage reports and calculations will be required. It is expected that storm drainage infrastructure consisting of inlets, storm sewer and open drainage channels will be constructed as the property develops.

- Although mentioned above, offsite basins include basins A, C, F, and Q. Flow contributing to the site from these basins will be routed through the proposed detention ponds. Flow rates are shown below.

| Offsite Flow Summary |                       |                 |                          |                          |                            |
|----------------------|-----------------------|-----------------|--------------------------|--------------------------|----------------------------|
| Basin Description    | Ultimate Design Point | Basin Area (ac) | Receiving Detention Pond | 5 Year Peak Runoff (cfs) | 100 Year Peak Runoff (cfs) |
| A                    | A                     | 18.99           | Pond 11                  | 20.84                    | 43.83                      |
| C                    | C                     | 36.39           | Pond 11                  | 33.36                    | 71.27                      |
| F                    | F                     | 25.25           | Irr. Pond                | 24.27                    | 51.63                      |
| Q                    | Q                     | 72.29           | Pond 9                   | 64.68                    | 137.80                     |

## b. Methodology

Design rainfall was determined utilizing Table 6-2 from the City of Colorado Springs Drainage Criteria Manual to determine the 5-year and 100-year rainfall values for the 1-hour events. The 1-hour rainfall depths are 1.5 and 2.52 in/hr respectively.

Composite percent impervious calculations were completed for each subbasin based on the density of lots and can be found in Appendix B. The El Paso County Drainage Criteria Manual Table 5-1 was used for reference when correlating land use to percent impervious values and located in Appendix F. Impervious values for 5-Acre Lots, 2.5-Acre Lots, Medium Density, Low Density, and Commercial Lots had impervious values of 10%, 15%, 45%, 55% and 75% respectively. The rainfall and percent impervious values were then used as inputs into the Colorado Urban Hydrograph Procedure (CUHP) spreadsheets to determine runoff values for both pre-development and post-development site.

CUHP is an evolution of the Snyder unit hydrograph and is calibrated for use along the Colorado Front Range. 1 Hour rainfall amounts are input into the program to produce a storm hyetograph that is then used to calculate a storm hydrograph for each basin depending on the subbasins properties including slope, length, shape, impervious area, pervious depression storage area, and various infiltration rates. Tabular hydrographs are then computed and can be used in EPA SWMM. The CUHP results are included within Appendix B.

EPA SWMM was used to determine flow routing via the kinematic wave method. Subbasins were routed to their respective design points and detention ponds for both the developed and predeveloped condition to determine peak runoff amounts for the 5-year and 100-year storm events. Information from these models along with information and calculations performed in the Mile High Flood District BMP spreadsheets was used to determine pond sizing calculations and release rates.



### c. Basin Hydrology

A summary of the flows for both the predeveloped and developed cases for each basin, subbasin and Pond are found on next page along with the full computation found in Appendix B.

| Existing SWMM Basin Summary |                 |              |                          |                            |
|-----------------------------|-----------------|--------------|--------------------------|----------------------------|
| Basin Description           | Basin Area (ac) | % Impervious | 5 Year Peak Runoff (cfs) | 100 Year Peak Runoff (cfs) |
| A                           | 18.99           | 2.00         | 20.84                    | 43.83                      |
| B                           | 59.74           | 2.00         | 103.48                   | 221.48                     |
| C                           | 34.87           | 2.00         | 33.36                    | 71.27                      |
| D                           | 38.84           | 2.00         | 31.56                    | 67.84                      |
| E                           | 127.86          | 2.00         | 223.69                   | 483.10                     |
| F                           | 25.25           | 2.00         | 24.27                    | 51.63                      |
| G                           | 52.19           | 2.00         | 79.17                    | 166.51                     |
| H                           | 20.63           | 2.00         | 18.59                    | 39.78                      |
| I                           | 31.93           | 2.00         | 34.58                    | 72.63                      |
| J                           | 28.47           | 2.00         | 56.31                    | 120.46                     |
| K                           | 93.14           | 2.00         | 92.05                    | 195.43                     |
| L                           | 16.39           | 2.00         | 107.58                   | 228.73                     |
| M                           | 13.87           | 2.00         | 11.48                    | 24.61                      |
| N                           | 49.00           | 2.00         | 68.16                    | 143.11                     |
| O                           | 24.76           | 2.00         | 22.69                    | 48.54                      |
| P                           | 43.80           | 2.00         | 38.52                    | 82.17                      |
| Q                           | 72.29           | 2.00         | 64.68                    | 137.80                     |
| R                           | 54.98           | 2.00         | 108.65                   | 232.13                     |
| S                           | 24.36           | 2.00         | 25.99                    | 48.54                      |
| T                           | 5.24            | 2.00         | 4.04                     | 8.68                       |
| U                           | 5.48            | 2.00         | 4.15                     | 8.95                       |
| V                           | 38.47           | 2.00         | 29.63                    | 63.92                      |
| W                           | 3.76            | 2.00         | 3.45                     | 7.33                       |
| X                           | 190.88          | 2.00         | 167.76                   | 361.56                     |
| AA                          | 33.49           | 10.00        | 38.76                    | 80.22                      |
| BB                          | 37.15           | 10.00        | 40.62                    | 84.15                      |
| CC                          | 6.33            | 10.00        | 6.53                     | 13.57                      |
| DD                          | 70.06           | 10.00        | 58.42                    | 123.69                     |
| EE                          | 69.47           | 10.00        | 81.16                    | 167.45                     |
| FF                          | 17.62           | 2.00         | 162.77                   | 340.42                     |
| GG                          | 16.35           | 2.00         | 14.93                    | 31.99                      |
| HH                          | 12.61           | 2.00         | 13.01                    | 27.42                      |
| II                          | 97.53           | 2.00         | 81.77                    | 175.59                     |
| JJ                          | 8.72            | 2.00         | 9.74                     | 20.50                      |
| KK                          | 8.12            | 2.00         | 7.51                     | 15.99                      |
| LL                          | 6.10            | 2.00         | 6.88                     | 14.48                      |

| Proposed SWMM Basin and Pond Summary |                 |              |                          |                            |                            |                              |
|--------------------------------------|-----------------|--------------|--------------------------|----------------------------|----------------------------|------------------------------|
| Basin Description                    | Basin Area (ac) | % Impervious | 5 Year Peak Runoff (cfs) | 100 Year Peak Runoff (cfs) | 5 Year Pond Volume (ac-ft) | 100 Year Pond Volume (ac-ft) |
| P                                    | 43.71           | 20.71%       | 40.00                    | 82.83                      |                            |                              |
| Pond 1                               |                 |              |                          |                            | 1.03                       | 1.97                         |
| X1                                   | 76.38           | 29.50%       | 80.91                    | 163.27                     |                            |                              |
| Pond 2                               |                 |              |                          |                            | 6.56                       | 8.80                         |
| O                                    | 52.52           | 30.10%       | 63.86                    | 127.40                     |                            |                              |
| Pond 3                               |                 |              |                          |                            | 3.79                       | 6.37                         |
| X2                                   | 36.33           | 33.33%       | 41.46                    | 82.46                      |                            |                              |
| X3                                   | 61.99           | 13.53%       | 47.59                    | 100.73                     |                            |                              |
| V2                                   | 15.34           | 15.00%       | 16.15                    | 33.25                      |                            |                              |
| V1                                   | 11.57           | 38.62%       | 13.99                    | 27.67                      |                            |                              |
| Pond 4                               |                 |              |                          |                            | 7.21                       | 7.35                         |
| N                                    | 41.57           | 29.60%       | 73.48                    | 141.24                     |                            |                              |
| Pond 5                               |                 |              |                          |                            | 1.86                       | 2.55                         |
| M                                    | 26.83           | 33.19%       | 46.54                    | 89.09                      |                            |                              |
| Pond 6                               |                 |              |                          |                            | 0.84                       | 0.94                         |
| K                                    | 114.73          | 38.03%       | 200.94                   | 382.30                     |                            |                              |
| Pond 7                               |                 |              |                          |                            | 8.38                       | 12.59                        |
| L                                    | 15.89           | 24.82%       | 15.97                    | 32.40                      |                            |                              |
| Pond 8                               |                 |              |                          |                            | 1.05                       | 1.09                         |
| S                                    | 21.67           | 40.88%       | 30.83                    | 58.96                      |                            |                              |
| R                                    | 56.16           | 21.81%       | 56.59                    | 116.06                     |                            |                              |
| Q                                    | 72.29           | 2.00%        | 64.68                    | 137.80                     |                            |                              |
| Pond 9                               |                 |              |                          |                            | 6.28                       | 10.31                        |
| H                                    | 21.96           | 10.00%       | 17.86                    | 37.80                      |                            |                              |
| Pond 10                              |                 |              |                          |                            | 0.66                       | 0.94                         |
| B2                                   | 19.99           | 24.55%       | 17.99                    | 37.14                      |                            |                              |
| B1                                   | 59.74           | 29.83%       | 66.93                    | 133.69                     |                            |                              |
| A                                    | 18.99           | 2.00%        | 20.84                    | 43.83                      |                            |                              |
| C                                    | 36.39           | 2.00%        | 35.31                    | 75.28                      |                            |                              |
| Pond 11                              |                 |              |                          |                            | 1.94                       | 3.23                         |
| J                                    | 28.07           | 10.00%       | 24.25                    | 51.19                      |                            |                              |
| Existing Pond 12                     |                 |              |                          |                            |                            |                              |
| EE2                                  | 16.36           | 75.00%       | 35.71                    | 63.62                      |                            |                              |
| EE3                                  | 6.67            | 55.00%       | 10.38                    | 19.93                      |                            |                              |
| Pond 13                              |                 |              |                          |                            | 1.33                       | 1.61                         |
| II3                                  | 23.97           | 10.0%        | 28.32                    | 58.65                      |                            |                              |
| II2                                  | 23.13           | 10.0%        | 28.04                    | 116.62                     |                            |                              |
| II1                                  | 50.43           | 10.0%        | 34.94                    | 74.39                      |                            |                              |
| Pond 14                              |                 |              |                          |                            | 1.06                       | 3.99                         |
| D                                    | 40.87           | 37.20%       | 61.12                    | 117.38                     |                            |                              |
| Pond 15                              |                 |              |                          |                            | 1.94                       | 3.23                         |
| E                                    | 106.53          | 14.35%       | 74.68                    | 157.91                     |                            |                              |

|   |       |        |        |        |      |      |
|---|-------|--------|--------|--------|------|------|
| I   | 26.99 | 34.66% | 40.37  | 78.06  |      |      |
| <b>Pond 16</b>                                      |       |        |        |        | 1.40 | 1.79 |
| JJ  | 8.9   | 20.70% | 11.49  | 22.8   |      |      |
| KK  | 8.4   | 12.09% | 8.14   | 16.95  |      |      |
| LL  | 6.2   | 10.00% | 7.36   | 15.07  |      |      |
| <b>Pond 17</b>                                      |       |        |        |        | 1.09 | 1.23 |
| G   | 31.45 | 12.48% | 37.69  | 107.75 |      |      |
| <b>Irrigation Pond</b>                              |       |        |        |        |      |      |
| JJ  | 8.90  | 20.70% | 11.06  | 28.04  |      |      |
| LL  | 6.2   | 12.09% | 5.85   | 15.68  |      |      |
| KK  | 8.4   | 10.00% | 5.9    | 16.72  |      |      |
| <b>Natural Drainage Way</b>                         |       |        |        |        |      |      |
| DD  | 69.5  | 10.0%  | 42.26  | 120.76 |      |      |
| EE1   | 50.87 | 10.0%  | 42.6   | 154.16 |      |      |
| <b>Existing Flying Horse North Detention Pond 6</b> |       |        |        |        |      |      |
| CC  | 6.33  | 10.0%  | 4.74   | 13.39  |      |      |
| FF  | 18.1  | 10.0%  | 100.02 | 325.29 |      |      |
| <b>Existing Flying Horse North Detention Pond 7</b> |       |        |        |        |      |      |
| GG  | 16.35 | 10.0%  | 11.25  | 32.04  |      |      |
| AA  | 33.8  | 10.0%  | 28.57  | 80.08  |      |      |
| BB  | 37.15 | 10.0%  | 29.52  | 83.01  |      |      |
| <b>Existing Flying Horse North Detention Pond 8</b> |       |        |        |        |      |      |
| HH  | 12.7  | 10.0%  | 9.86   | 27.77  |      |      |
| <b>Natural Drainage Way</b>                         |       |        |        |        |      |      |
| T   | 5.24  | 2.00%  | 2.92   | 8.56   |      |      |
| U   | 5.86  | 10.0%  | 3.63   | 10.37  |      |      |
| W   | 3.76  | 10.0%  | 2.6    | 7.36   |      |      |
| <b>Natural Drainage Way</b>                         |       |        |        |        |      |      |

## IV. Hydraulic Analysis

### a. Major Drainageways

There are no major drainage ways exist within the development; however, small tertiary tributaries are within the site currently and function to convey flows to unnamed tributaries of the East Cherry Creek and Black Squirrel Creek.

## V. Environmental Evaluations

### a. Significant Existing or Potential Wetland and Riparian Areas Impacts

As part of this work, the developer has engaged Bristlecone Ecology, LLC to perform environmental studies of the site that will be submitted with the planning documents. Major information in the report concerning wetlands concludes that there is a wetland associated with Black Squirrel Creek. Black Squirrel Creek is known to be a jurisdictional stream.

At this time, there are no improvements proposed for Black Squirrel Creek. The minimal impact to the stream will keep the natural habitat intact and the natural function of the Creek as it is to maintain the wetland habitat.

## **b. Stormwater Quality Considerations and Proposed Practices**

As part of the development, full spectrum detention facilities will be installed to provide water quality for the development. The facilities will be designed using El Paso County criteria and provide stormwater quality by slowing the release of stormwater captured by the ponds and allowing solids to settle out. Additionally, when possible, the existing natural drainage ways will be used to convey stormwater to more closely mimic the natural hydrologic and hydraulic cycle. Some of the drainage ways will be used to convey water to the ponds and others will receive water from the ponds and in both scenarios will provide additional water quality benefits.

On site practices for the homes, schools, churches, and other buildings should use means such that impervious areas drain across pervious area to allow for infiltration during the minor events. This would include discharge of the gutters onto landscape areas vs. directly connecting to storm sewer and as discussed above as well using natural ditches and swales where it is logical and makes sense to convey stormwater in lieu of storm sewer piping.

## **c. Permitting Requirements**

When work infringes upon the wetlands or floodplain a 404 Permit will be required. If the work within the waterways is minimal, it will likely be covered under a nationwide 404 permit; it is however possible that an individual permits will be required.

The Colorado Department of Public Health and Environment will require permits for any disturbance that exceed 1 acre of land. Should groundwater be encountered, a dewatering permit will also be required.

El Paso County will require an Erosion and Stormwater Quality Control Permit and any other construction permits required to complete the construction of the site.

Should development occur which effects the floodplain, FEMA will require a permit for work within the floodplain prior to the commencement of any construction or development within any special flood hazard area (SFHA). If the infrastructure is to be installed within the channel the designer shall route the design through the proper FEMA channels whether that be with a no rise certification or via the CLOMR/LOMR process should a more major improvement within the floodplain be proposed. At this time the project does not propose any direct development within the floodplain however storm infrastructure will discharge into the existing FEMA channel.

## **d. 4-Step Process**

In accordance with the Engineering Criteria Manual I.7.2.A and DCM V2, this site has implemented the four-step process to minimize adverse impacts of urbanization. The four-step process includes reducing runoff volumes, stabilizing drainageways, treating the water quality capture volume, and considering the need for Industrial Commercial BMPs.

**Step 1 – Reducing Runoff Volumes:** The development of the project site includes a variety of land uses including open and vegetated areas interspersed to help disconnect impervious areas and reduce runoff volumes.

Step 2 – Stabilize Drainageways: Altered drainage ways will be designed in a manner that provides water quality benefits through infiltration and the removal of pollutants via phytoremediation. Vegetation will also be selected to stabilize the drainage ways by reducing the velocity of flows and decreasing any scour. Should the final drainage ways require, grade control structures may be implemented to further reduce flow velocities and protect against erosion. These improvements will help stabilize drainageways.

Step 3 – Provide WQCV: Runoff from this development is treated through capture and slow release of the WQCV via detention ponds that are designed per current El Paso County DCM V2.

Step 4 – Consider the need for Industrial and Commercial BMP's: A site specific storm water quality and erosion control plan and narrative will be prepared with subsequent land use approvals prepared in conjunction with the report prior to any construction. Site specific temporary source control BMPs as well as permanent BMPs are detailed in this plan and narrative. Guidelines detailed in the El Paso DCM V2 4.2 pertaining to the covering and storage handline and spill containment and control shall be followed as necessary.

## VI. Alternatives Evaluation

The current selected plan for drainage follows the DPBS for the Black Squirrel Basin and will not require an evaluation of alternatives.

## VII. Selected Plan

### a. Plan Hydrology

This MDDP schematically addressed on-site and off-site drainage patterns using the existing topography and proposed land use plan for the overall drainage design. Individual preliminary and final drainage reports will better define the planning areas as the site is developed.

The overall site is divided into several separate major basins. Basin sizes range from 35 acres to 181 acres in size. Basins A through V2 drain and eventually discharge into an unnamed tributary of the Arkansas River. Basins AA through LL drain towards unnamed tributaries of Black Squirrel Creek.

The sub-basins are described in additional detail above.

### b. System Improvements

The site plans propose the construction of 15 separate full spectrum detention facilities and utilize the capacity of 2 existing full spectrum detention facilities. The ponds are preliminarily sized to ensure that the 5-year and 100-year release rates are equal to or less than the historic rates. For the PDR and FDR, the consultant will need to use a routing software to accurately model the routed hydrographs for ponds upstream of the irrigation pond. The irrigation pond has a 12 hr drain time for WQCV. All drains times must be within 72 hours for the 5-year storm or within 120 hours for storm events greater than the 5-year storm per Senate Bill 15-212.

- Pond 1 is located in the northwest corner of the site and discharges into an unnamed tributary of East Cherry Creek. The pond is planned to store a maximum of 1.97 ac-ft during the 100-year event and have a peak outflow of 81.7 cfs which is slightly below the predevelopment peak outflow of 81.0 cfs. The 5-year storage volume is 1.03 ac-ft with a peak outflow of 24.9 cfs.

- Pond 2 is located to the east of Pond 1 and discharges into another unnamed tributary of East Cherry Creek. The pond is planned to store a maximum of 8.8 ac-ft during the 100-year event and have a peak outflow of 74.6 cfs which is slightly below the predevelopment peak outflow of 81.0 cfs. The 5-year storage volume is 6.56 ac-ft with a peak outflow of 27.8 cfs.
- Pond 3 is located on the eastern portion of the site and south of Pond 1. The pond discharges into an unnamed tributary of East Cherry Creek. The pond is planned to store a maximum of 6.37 ac-ft during the 100-year event and have a peak outflow of 46.1 cfs which is slightly below the predevelopment peak outflow of 48.5 cfs. The 5-year storage volume is 3.79 ac-ft with a peak outflow of 22.7 cfs.
- Pond 4 is located near the eastern portion of the site adjacent to Black Forest Rd. The pond discharges into a natural drainage way, which outlets into an unnamed tributary of East Cherry Creek. The pond is planned to store a maximum of 7.35 ac-ft during the 100-year event and have a peak outflow of 198.8 cfs which is slightly below the predevelopment peak flow rate of 231.6 cfs. The 5-year storage volume is 7.12 ac-ft with a peak outflow of 70.6 cfs.
- Pond 5 is located in the northwest portion of the site. The pond discharges natural drainageway, which outlets into an unnamed tributary of East Cherry Creek. The pond is planned to store a maximum of 2.5 ac-ft during the 100-year event and have a peak outflow of 103.1 cfs which is greater than the predevelopment peak outflow of 116.9 cfs. The 5-year storage volume is 1.86 ac-ft with a peak outflow of 39.4 cfs.
- Pond 6 is located near the northwest corner of the site and upstream of Pond 5. The pond discharges into a natural drainageway which outlets into an unnamed tributary of East Cherry Creek. The pond is planned to store a maximum of 2.93 ac-ft during the 100-year event and have a peak outflow of 48.2 cfs which is greater than the predevelopment peak outflow of 47.5 cfs. The 5-year storage volume is 1.77 ac-ft with a peak outflow of 12.2 cfs.
- Pond 7 is located in the central portion of site. The pond discharges into a natural drainageway that eventually outlets to an unnamed tributary of East Cherry Creek. The pond is planned to store a maximum of 12.59 ac-ft during the 100-year event and have a peak outflow of 172.2 cfs which is slightly lower than the predevelopment peak outflow of 191.6 cfs. The 5-year storage volume is 8.38 ac-ft with a peak outflow of 65.4 cfs.
- Pond 8 is located near the central portion of the site and downstream of Pond 7. The pond discharges into an unnamed tributary of East Cherry Creek. The pond is planned to store a maximum of 0.94 ac-ft during the 100-year event and have a peak outflow of 28.9 cfs which lower than the predevelopment peak outflow of 32.7. The 5-year storage volume is 0.84 ac-ft with a peak outflow of 11.4 cfs.
- Pond 9 is located near the southeast corner of the site just and adjacent to Black Forest Road. The pond discharges into a natural drainageway and flows under Black Forest Rd. via culvert. The natural drainageway is southeast of the existing property and eventually drains northeast to East Cherry Creek. The pond is planned to store a maximum of 10.31 ac-ft during the 100-year

event and have a peak outflow of 220.7 cfs which is lower than the predevelopment peak outflow of 282.3 cfs. The 5-year storage volume is 6.28 ac-ft with a peak outflow of 94.8 cfs.

- Pond 10 is located on the north central portion of the site and north of Stagecoach Road. The pond discharges into an unnamed tributary of East Cherry Creek. The pond is planned to store a maximum of 0.94 ac-ft during the 100-year event and have a peak outflow of 33.9 cfs which is lower than the predevelopment peak outflow of 39.2 cfs. The 5-year storage volume is 0.68 ac-ft with a peak outflow of 13.6 cfs.
- Pond 11 is located near the central portion of the site. The pond discharges into a natural drainageway which eventually discharges into the Irrigation Pond. The pond is planned to store a maximum of 6.83 ac-ft during the 100-year event and have a peak outflow of 230.0 cfs which is above than the predevelopment peak outflow of 221.3 cfs. The 5-year storage volume is 3.66 ac-ft with a peak outflow of 98.4 cfs.
- Existing Pond 12 is designed in the Classic Homes Filing No. 1 FDR and located near the northwest corner of the site and north of Stagecoach Road. The pond discharges into an unnamed tributary of East Cherry Creek. The pond is planned to have a peak outflow of 45.0 cfs.
- Pond 13 is located central portion of the site and just west of the major ridgeline between the two basins. The pond discharges into a natural drainageway to an existing pond of Filing No. 1, which ultimately outlets to Black Squirrel Creek. The pond is planned to store a maximum of 1.8 ac-ft during the 100-year event and have a peak outflow of 54.2 cfs which lower than the predevelopment peak outflow of 55.0. The 5-year storage volume is 1.3 ac-ft with a peak outflow of 17.2 cfs.
- Pond 14 is located near the southwest corner of the site just east of the Black Squirrel Creek. The pond discharges into a natural drainageway of Black Squirrel Creek. The pond is planned to store a maximum of 3.99 ac-ft during the 100-year event and have a peak outflow of 152.3 cfs which is slightly lower than the predevelopment peak outflow of 173.0 cfs. The 5-year storage volume is 1.06 ac-ft with a peak outflow of 59.0 cfs.
- Pond 15 is near the central portion of the site. The pond discharges into a natural drainageway which eventually discharges into the existing Irrigation Pond. The pond is planned to store a maximum of 3.23 ac-ft during the 100- year event and have a peak outflow of 68.4 cfs which is slightly above the predevelopment peak of 67.8 cfs. The 5-year storage volume is 1.94 ac-ft with a peak outflow of 30.9 cfs.
- Pond 16 is near the central portion of the site. The pond discharges into a culvert and goes under Stagecoach Road, which eventually discharges into an existing drainageway of East Cherry Creek. The pond is planned to store a maximum of 5.40 ac-ft during the 100-year event and have a peak outflow of 63.8 cfs which is slightly below the predevelopment peak of 71.2 cfs. The 5 year storage volume is 4.66 ac-ft with a peak outflow of 24.3 cfs.

- Pond 17 is near the central portion of the site. The pond discharges into a natural drainageway which eventually discharges into an existing drainageway of Black Squirrel Creek. The pond is planned to store a maximum of 1.23 ac-ft during the 100 year event and have a peak outflow of 49.6 cfs which is slightly below the predevelopment peak of 49.9 cfs. The 5 year storage volume is 1.09 ac-ft with a peak outflow of 16.8 cfs..
- The existing Irrigation Pond is in the central portion of site and just south of existing Stagecoach Road. The pond discharges towards an unnamed tributary of East Cherry Creek. The irrigation pond was design and subsequently built as part of the Filing 1 project. Storage Volumes for the pond assumed different upstream development conditions and therefore the pond will receive a higher volume of water during the storm events however the rate into the pond will be reduced. The irrigation pond will store 35.92 ac-ft during the 100-year event with a peak outflow of 274.73 cfs and the 5 year storage volume is 19.67 ac-ft with a peak outflow of 114.0 cfs.

The site plans propose the construction of 2 culverts in the southwest corner of site that navigates flow under roads to proposed Detention Pond 14. Analyses were completed by flow master and calculations can be found in Appendix E.

- Culvert 1 carries flow from Subbasin II3 to Subbasin II2 in the southwest corner of site. Each of the basins consist of the Flying Horse Golf Course and 2.5-acre estate lots. The culvert is 36" RCP at a 1% slope and designed for the 100-year event. The culvert will have a peak outflow of 58.65 cfs, where the pipe is 72% full.
- Culvert 2 carries flow from Subbasin II2 to Subbasin II1 in the southwest corner of site. Each of the basins consist of the Flying Horse Golf Course and 2.5-acre estate lots. The culvert is 42" RCP at a 2% slope and designed for the 100-year event. The culvert will have a peak outflow of 116.62 cfs, where the pipe is 68% full.

The culverts sizes should be refined in the PDR and FDR. Energy dissipation calcs can also be performed later within the design.

Overall runoff from the site will by and large match or be less than predevelopment peak flows sans those for outfall 5 which is slightly greater than predevelopment flows. The volume of water will increase however as the drainage channels are designs, continuous simulation models will be done to see the effects of prolonged runoff rates. Predevelopment and post development flows for the 5-year and 100-year events are summarized in the following table for the 5 site outfalls.

| OUTFALL | Predevelopment |          | Postdevelopment* |          |
|---------|----------------|----------|------------------|----------|
|         | 5 year         | 100 year | 5 year           | 100 year |
| 1       | 320.31         | 725.59   | 183.76           | 705.93   |
| 2       | 145.46         | 311.00   | 80.36            | 242.18   |
| 3       | 167.76         | 361.56   | 70.06            | 271.49   |
| 4       | 346.26         | 733.92   | 230.07           | 646.46   |
| 5       | 24.12          | 50.88    | 16.85            | 45.91    |

\*Values to be refined with Preliminary and Final Drainage Reports for each filing



## VIII. Drawings

Please refer to the appendices for vicinity maps and drainage basin maps.

## IX. Summary

Flying Horse North is a large master planned community consisting of various densities of dwelling units to include single family homes, multifamily homes, parks, institutional sites, and commercial areas. Due to development increased runoff will occur. To mitigate downstream impacts, 16 large full spectrum detention facilities will be built to reduce the runoff rate to near historic levels. These detention facilities will provide water quality enhancements to account for the increased urbanization of the upstream catchment areas. The ponds are preliminarily sized to ensure that the 5-year and 100-year release rates are equal to or less than the historic rates. For the PDR and FDR, the consultant will need to use a routing software to accurately model the routed hydrographs for ponds upstream of the irrigation pond. The irrigation pond has a 12 hour drain time for WQCV. All drains times must be within 72 hours for the 5-year storm or within 120 hours for storm events greater than the 5-year storm per Senate Bill 15-212.

Additional analysis will be required and completed to review the hydraulics of the proposed major drainage channels and be included in future submittals. The proposed design, as described in this report, is not anticipated to cause any adverse impact to downstream properties however as noted previously due to the increased volume of water, downstream tributaries will see increases in the volume of flow. It is advised that low impact design be considered when designing and developing each filing. This shall include those items listed in the four-step process above and any additional measures that are within reason to disconnect impervious areas and increase infiltration. This will alleviate the additional volume of water due to development. Although the rate will remain at or below historic levels, the amount of time the channels will see water will increase which may cause more channel movement than historic. Downstream planning efforts should allow for the natural migration and movement of the channel by continuing to provide large floodplain areas to allow movement of the channel.

## X. References

El Paso County – Drainage Criteria Manual, 2014

City of Colorado Springs – Drainage Criteria Manual, May 2014

Urban Storm Drainage Criteria Manual, Urban Drainage Flood Control District, January 2018

Preliminary Drainage Report for Flying Horse North Preliminary Plan and Final Drainage Report for Flying Horse North Filing No. 1, Classic Consulting Engineers and Surveyors, November 2017

Flying Horse North Irrigation Reservoir Embankment Design Report, Classic Consulting Engineers and Surveyors, August 2018

Black Squirrel Drainage Basin Planning Study (DBPS), URS Consultants, January 1989

## Appendix A





Douglas County

Elbert County

Elbert County

Lincoln County

Pueblo County

Teller County

Teller County

Fremont County

## Drainage Basins

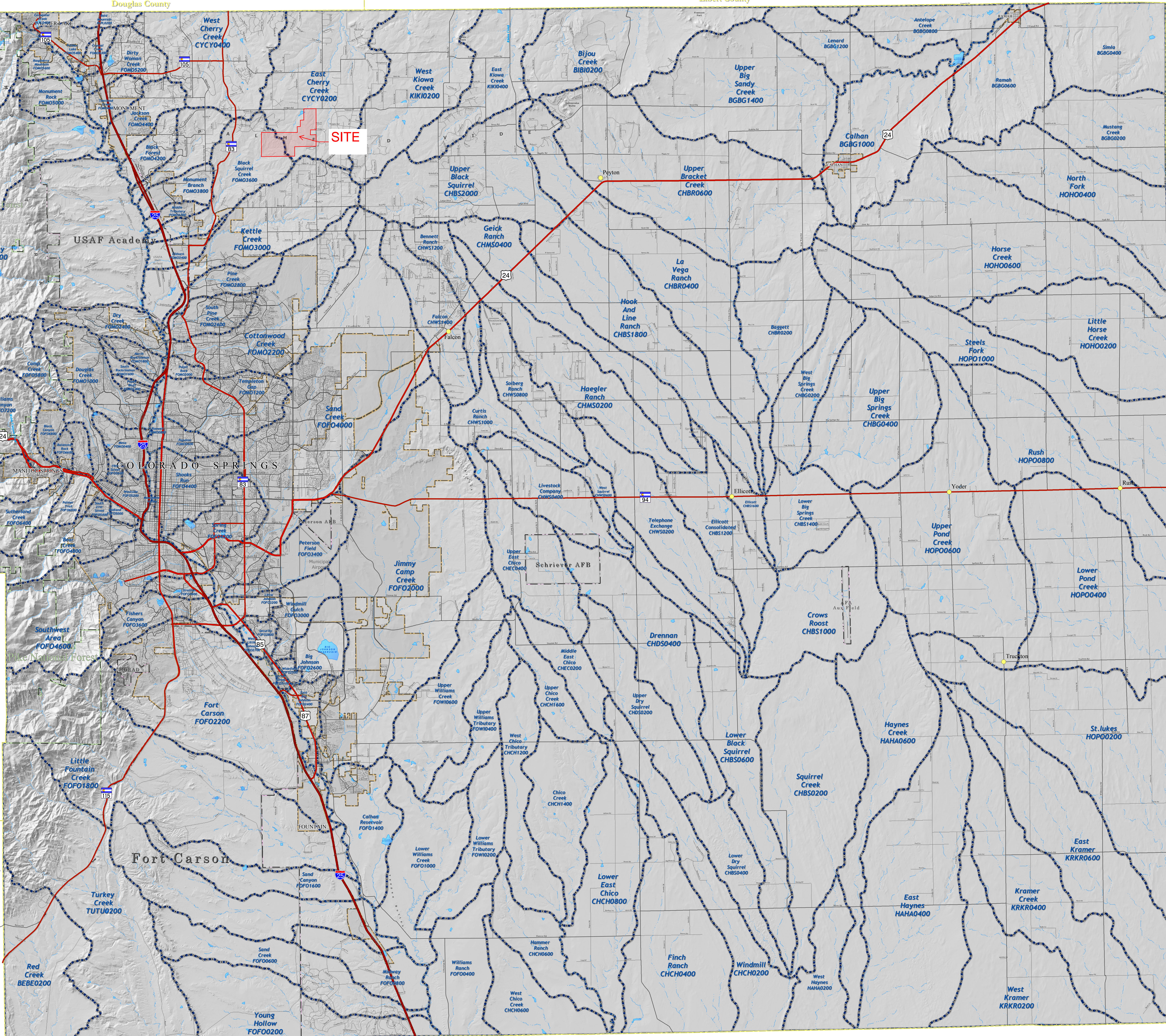
### El Paso County Colorado Legend

- Drainage Basins (Source: Muter Engineering Company 1988)
- US Interstate Highways
- US Highways
- Colorado State Highways
- Major Roadways
- Local Streets & Roads
- Creeks
  - Perennial
  - Intermittent
- Lakes & Reservoirs
- Summits
- Unincorporated Urban Areas
- Incorporated Cities
- Military
- Forest
- County Lines



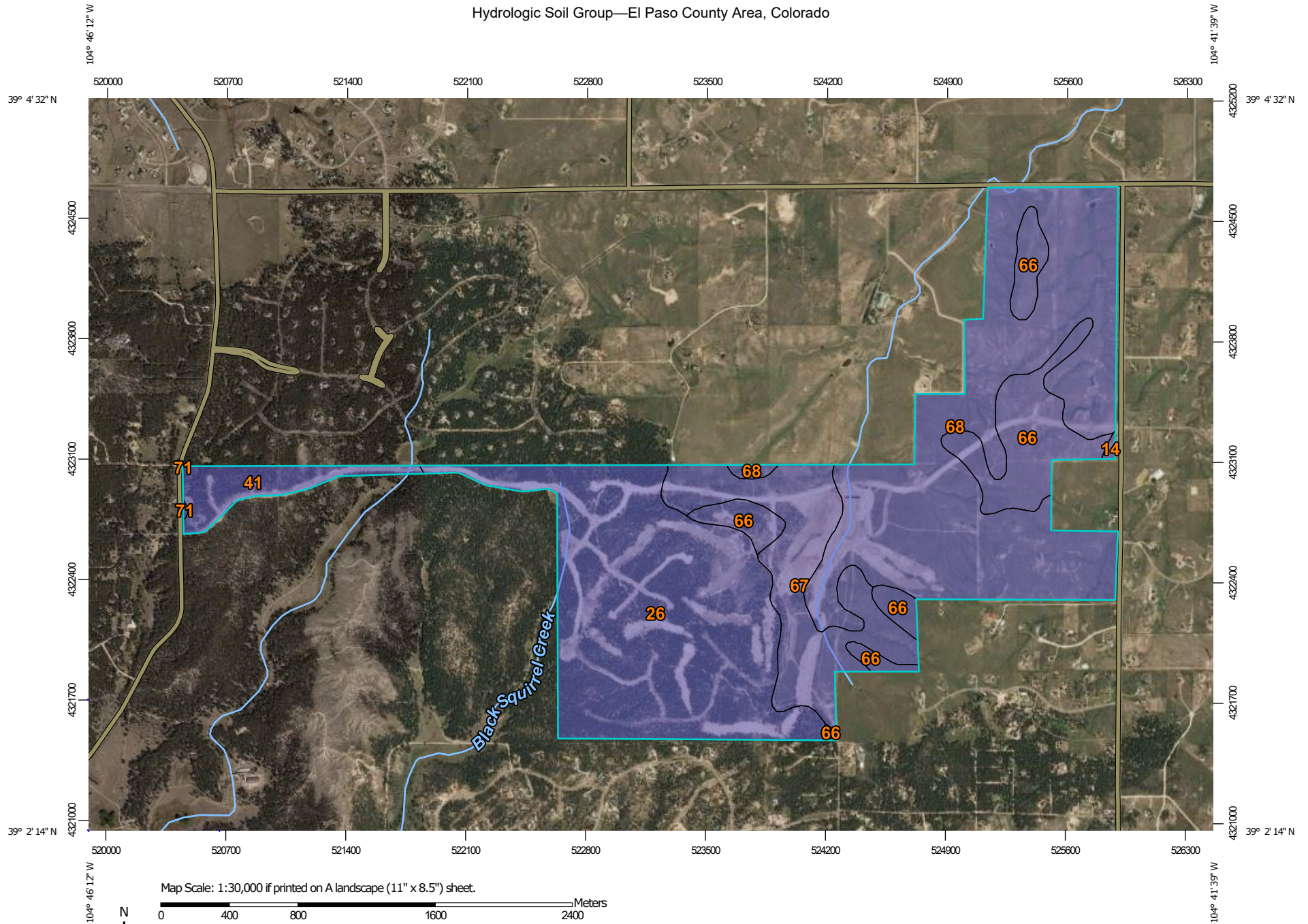
0 0.5 1 2 3 4 5  
Miles

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# Hydrologic Soil Group—El Paso County Area, Colorado



Map Scale: 1:30,000 if printed on A landscape (11" x 8.5") sheet.

0 400 800 1600 2400 Meters

0 1000 2000 4000 6000 Feet

Map projection: Web Mercator Corner coordinates: WGS84 Edge tics: UTM Zone 13N WGS84



**Natural Resources  
Conservation Service**

Web Soil Survey  
National Cooperative Soil Survey

1/27/2022  
Page 1 of 4

## MAP LEGEND

### Area of Interest (AOI)









 Area of Interest (AOI)

### Soils

#### Soil Rating Polygons

 A  
 A/D  
 B  
 B/D  
 C  
 C/D  
 D  
 Not rated or not available

#### Soil Rating Lines

 A  
 A/D  
 B  
 B/D  
 C  
 C/D  
 D  
 Not rated or not available

#### Soil Rating Points

 A  
 A/D  
 B  
 B/D

 C  
 C/D  
 D  
 Not rated or not available

### Water Features

 Streams and Canals

### Transportation

 Rails  
 Interstate Highways  
 US Routes  
 Major Roads  
 Local Roads

### Background

 Aerial Photography

## MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24,000.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service

Web Soil Survey URL:

Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: El Paso County Area, Colorado

Survey Area Data: Version 19, Aug 31, 2021

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Aug 19, 2018—May 26, 2019

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

## Hydrologic Soil Group

| Map unit symbol                    | Map unit name                                      | Rating | Acres in AOI   | Percent of AOI |
|------------------------------------|--|--------|----------------|----------------|
| 14                                 | Brussett loam, 1 to 3 percent slopes               | B      | 1.9            | 0.1%           |
| 26                                 | Elbeth sandy loam, 8 to 15 percent slopes          | B      | 474.2          | 33.7%          |
| 41                                 | Kettle gravelly loamy sand, 8 to 40 percent slopes | B      | 53.4           | 3.8%           |
| 66                                 | Peyton sandy loam, 1 to 5 percent slopes           | B      | 160.9          | 11.4%          |
| 67                                 | Peyton sandy loam, 5 to 9 percent slopes           | B      | 182.8          | 13.0%          |
| 68                                 | Peyton-Pring complex, 3 to 8 percent slopes        | B      | 533.4          | 37.9%          |
| 71                                 | Pring coarse sandy loam, 3 to 8 percent slopes     | B      | 0.6            | 0.0%           |
| <b>Totals for Area of Interest</b> |  |        | <b>1,407.3</b> | <b>100.0%</b>  |

## Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

## Rating Options

*Aggregation Method:* Dominant Condition

*Component Percent Cutoff:* None Specified

*Tie-break Rule:* Higher



## NOTES TO USERS

This map is for use in administering the National Flood Insurance Program. It does not necessarily identify all areas subject to flooding, particularly from local drainage sources of small size. The community map repository should be consulted for possible updated or additional flood hazard information.

To obtain more detailed information in areas where **Base Flood Elevations (BFEs)** and/or **Floodway Data** are provided, users are encouraged to consult the Flood Profiles and Floodway Data and/or Summary of Stillwater Elevations tables contained within the Flood Insurance Study (FIS) report that accompanies this FIRM. Users should be aware that BFEs shown on the FIRM represent rounded whole-foot elevations. These BFEs are intended for flood insurance rating purposes only and should not be used as the sole source of flood elevation information. Accordingly, flood elevation data presented in the FIS report should be utilized in conjunction with the FIRM for purposes of construction and/or floodplain management.

**Coastal Base Flood Elevations** shown on this map apply only to landward of 0.0' North American Vertical Datum of 1988 (NAVD88). Users of this FIRM should be aware that coastal flood elevations are also provided in the Summary of Stillwater Elevations tables in the Flood Insurance Study report for this jurisdiction. Elevations shown in the Summary of Stillwater Elevations table should be used for construction and/or floodplain management purposes when they are higher than the elevations shown on this FIRM.

Boundaries of the floodways were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations with regard to requirements of the National Flood Insurance Program. Floodway widths and other pertinent floodway data are provided in the Flood Insurance Study report for this jurisdiction.

Certain areas not in Special Flood Hazard Areas may be protected by **flood control structures**. Refer to section 2.4 "Flood Protection Measures" of the Flood Insurance Study report for information on flood control structures for this jurisdiction.

The **projection** used in the preparation of this map was Universal Transverse Mercator (UTM) zone 13. The **horizontal datum** was NAD83, GRS80 spheroid. Differences in datum, projection or UTM zone zones used in the production of FIRMs for adjacent jurisdictions may result in slight positional differences in map features across jurisdiction boundaries. These differences do not affect the accuracy of this FIRM.

Flood elevations on this map are referenced to the **North American Vertical Datum of 1988 (NAVD88)**. These flood elevations must be compared to structure and ground elevations referenced to the same vertical datum. For information regarding conversion between the National Geodetic Vertical Datum of 1929 and the North American Vertical Datum of 1988, visit the National Geodetic Survey website at <http://www.ngs.noaa.gov/> or contact the National Geodetic Survey at the following address:

NGS Information Services  
NOAA, NNGS12  
National Geodetic Survey  
SSMC-3, #9002  
1315 East-West Highway  
Silver Spring, MD 20910-3282

To obtain current elevation, description, and/or location information for **bench marks** shown on this map, please contact the Information Services Branch of the National Geodetic Survey at (201) 713-3242 or visit its website at <http://www.ngs.noaa.gov/>.

**Base Map** information shown on this FIRM was provided in digital format by El Paso County, Colorado Springs Utilities, City of Fountain, Bureau of Land Management, National Oceanic and Atmospheric Administration, United States Geological Survey, and Anderson Consulting Engineers, Inc. These data are current as of 2006.

This map reflects more detailed and up-to-date **stream channel configurations and floodplain delineations** than those shown on the previous FIRM for this jurisdiction. The floodplains and floodways that were transferred from the previous FIRM may have been adjusted to conform to these new stream channel configurations. As a result, the Flood Profiles and Floodway Data tables in the Flood Insurance Study Report (which contains authoritative hydraulic data) may reflect stream channel distances that differ from what is shown on this map. The profile baselines depicted on this map represent the hydraulic modeling baselines that match the flood profiles and Floodway Data tables if applicable, in the FIS report. As a result, the profile baselines may deviate significantly from the new base map channel representation and may appear outside of the floodplain.

**Corporate limits** shown on this map are based on the best data available at the time of publication. Because changes due to annexations or de-annexations may have occurred after this map was published, map users should contact appropriate community officials to verify current corporate limit locations.

Please refer to the separately printed **Map Index** for an overview map of the county showing the layout of map panels, community map repository addresses, and a Listing of Communities table containing National Flood Insurance Program dates for each community as well as a listing of the panels on which each community is located.

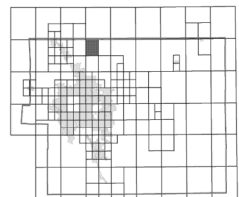
Contact **FEMA Map Service Center (MSC)** via the FEMA Map Information eXchange (FMIX) 1-877-336-3627 for information on available products associated with this FIRM. Available products may include previously issued Letters of Map Change, a Flood Insurance Study Report, and/or digital versions of this map. The MSC may also be reached by Fax at 1-800-336-9620 and its website at <http://www.msc.fema.gov/>.

If you have **questions about this map** or questions concerning the National Flood Insurance Program in general, please call 1-877-FEMA MAP (1-877-336-2627) or use the FEMA website at <http://www.fema.gov/business/fis/>.

### El Paso County Vertical Datum Offset Table

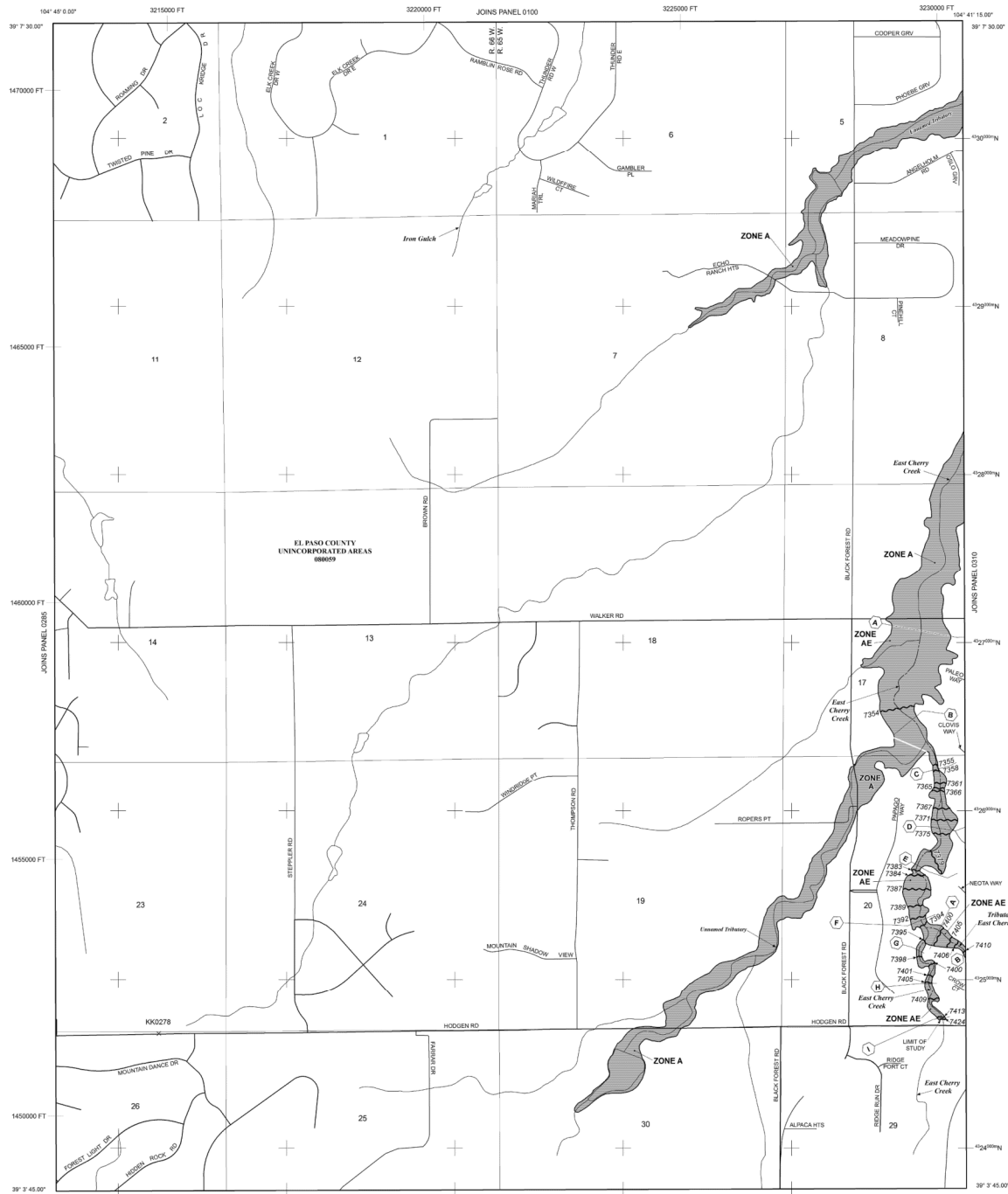
| Flooding Source   | Vertical Datum Offset (ft) |
|---|----------------------------|
| REFER TO SECTION 3.3 OF THE EL PASO COUNTY FLOOD INSURANCE STUDY FOR STREAM BY STREAM VERTICAL DATUM CONVERSION INFORMATION |                            |

### Panel Location Map



This Digital Flood Insurance Rate Map (DFIRM) was produced through a Cooperating Technical Partner (CTP) agreement between the State of Colorado Water Conservation Board (CWCB) and the Federal Emergency Management Agency (FEMA).

Additional Flood Hazard information and resources are available from local communities and the Colorado Water Conservation Board.



NOTE: MAP AREA SHOWN ON THIS PANEL IS LOCATED WITHIN TOWNSHIP 11 SOUTH, RANGE 65 WEST, AND TOWNSHIP 11 SOUTH, RANGE 66 WEST.

## LEGEND

**SPECIAL FLOOD HAZARD AREAS (SFHAS) SUBJECT TO INUNDATION BY THE 1% ANNUAL CHANCE FLOOD**

The 1% annual chance flood (100-year flood), also known as the base flood, is the flood that has a 1% chance of being equaled or exceeded in any given year. The Special Flood Hazard Area is the area subject to flooding by the 1% annual chance flood. Areas of Special Flood Hazard include Zones A, AE, AH, AO, ASB, V, and VE. The base Flood Elevation is the water-surface elevation of the 1% annual chance flood.

- ZONE A:** No Base Flood Elevations determined.
- ZONE AE:** Base Flood Elevations determined.
- ZONE AH:** Flood depths of 1 to 3 feet (usually areas of ponding); Base Flood Elevations determined.
- ZONE AO:** Flood depths of 1 to 3 feet (usually sheet flow on sloping terrain); average depths determined. For areas of alluvial fan flooding, vehicles also determined.
- ZONE AR:** Special Flood Hazard Area formerly protected from the 1% annual chance flood by a flood control system (FIS) that is no longer maintained. Zone AR indicates that the former flood control system is being restored to provide protection from the 1% annual chance or greater flood.
- ZONE ASB:** Areas to be protected from 1% annual chance flood by a Federal Flood protection system under construction; no Base Flood Elevations determined.
- ZONE V:** Coastal flood zone with velocity hazard (wave action); no Base Flood Elevations determined.
- ZONE VE:** Coastal flood zone with velocity hazard (wave action); no Base Flood Elevations determined.

**FLOODWAY AREAS IN ZONE AE**

The floodway is the channel of a stream plus any adjacent floodplain areas that must be kept free of encroachment so that the 1% annual chance flood can be carried without substantial increases in flood heights.

**OTHER FLOOD AREAS**

**ZONE X:** Areas of 0.2% annual chance flood; areas of 1% annual chance flood with average depth of less than 1 foot or with velocity hazard; areas less than 1 square mile; and areas protected by levees from 1% annual chance flood.

**OTHER AREAS**

**ZONE X:** Areas determined to be outside the 0.2% annual chance floodplain. Areas in which flood hazards are undetermined, but possible.

**ZONE D:** Areas in which flood hazards are undetermined, but possible.

**COASTAL BARRIER RESOURCES SYSTEM (CBRS) AREAS**

**OTHERWISE PROTECTED AREAS (OPAs)**

CBRS areas and OPAs are normally located within or adjacent to Special Flood Hazard Areas.

**Floodplain boundary:** Solid line.  
**Floodway boundary:** Dashed line.  
**Zone D boundary:** Dotted line.  
**CBRS and OPA boundary:** Dashed line.

**Boundary dividing Special Flood Hazard Areas of different base Flood Elevations, flood depths or flood velocities:** Solid line with dots.  
**Base Flood Elevation line and value, elevation in feet:** Solid line with dots.  
**Base Flood Elevation value where uniform within zone; elevation in feet:** Solid line with dots.

\* Referenced to the North American Vertical Datum of 1988 (NAVD 88)

**Cross section line:** Solid line with dots.

**Traverse line:** Solid line with dots.

**Geographic coordinates referenced to the North American Datum of 1983 (NAD 83):** Solid line with dots.

**1000-meter Universal Transverse Mercator grid lines, zone 13:** Solid line with dots.

**1000-foot grid lines:** Dashed line with dots.

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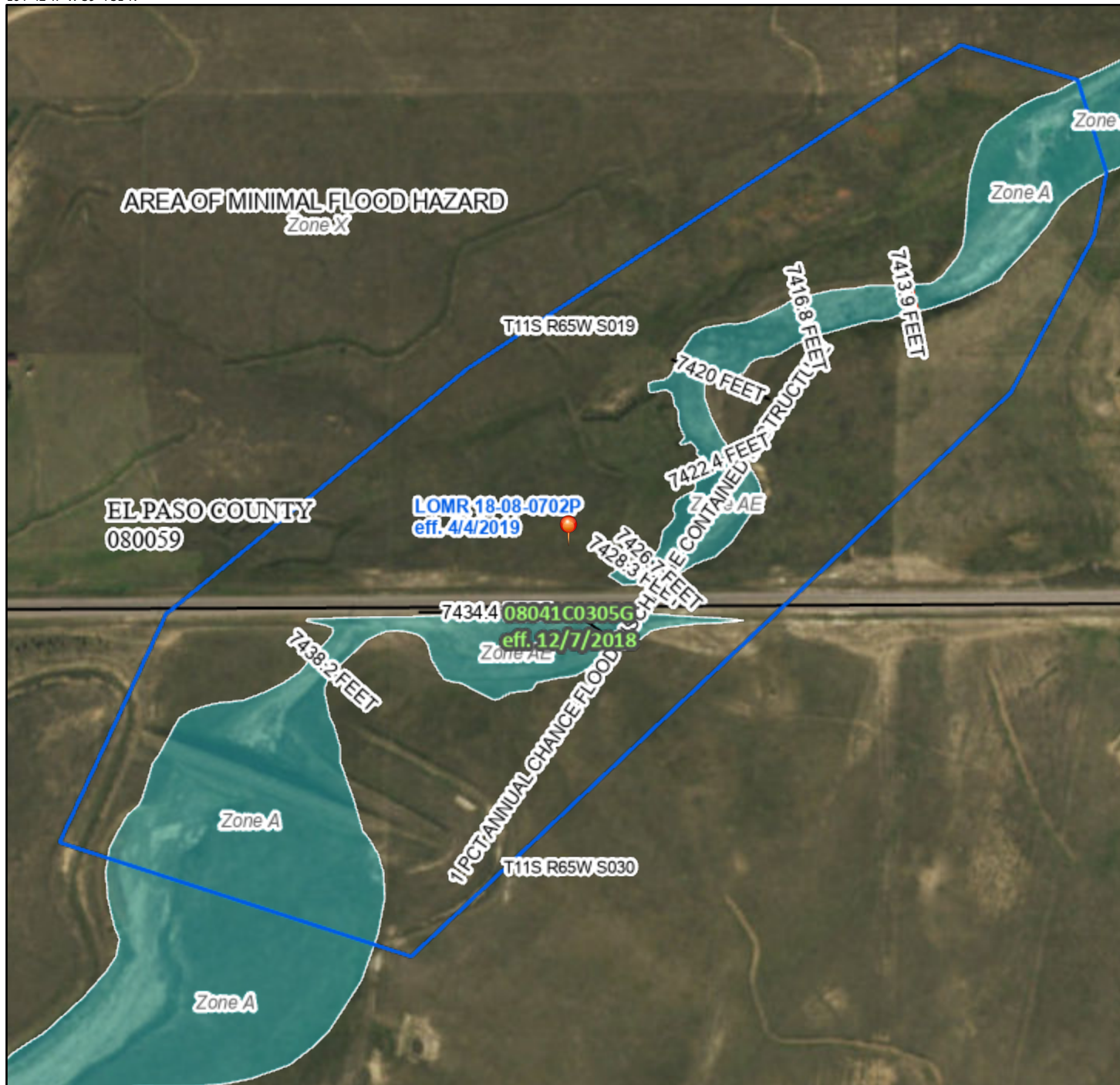
**1000-foot grid lines:** Dashed line with dots.



# National Flood Hazard Layer FIRMMette



104°42'47"W 39°4'31"N



0 250 500 1,000 1,500 2,000 Feet

1:6,000

104°42'9"W 39°4'4"N

Basemap: USGS National Map: Orthoimagery: Data refreshed October, 2020

## Legend

SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT

|                             |  |   |
|-----------------------------|--|---|
| SPECIAL FLOOD HAZARD AREAS  |  | Without Base Flood Elevation (BFE)<br>Zone A, V, A99  |
|                             |  | With BFE or Depth Zone AE, AO, AH, VE, AR   |
|                             |  | Regulatory Floodway   |
| OTHER AREAS OF FLOOD HAZARD |  | 0.2% Annual Chance Flood Hazard, Areas of 1% annual chance flood with average depth less than one foot or with drainage areas of less than one square mile Zone X |
|                             |  | Future Conditions 1% Annual Chance Flood Hazard Zone X  |
|                             |  | Area with Reduced Flood Risk due to Levee. See Notes. Zone X  |
|                             |  | Area with Flood Risk due to Levee Zone D  |
| OTHER AREAS                 |  | NO SCREEN Area of Minimal Flood Hazard Zone X   |
|                             |  | Effective LOMRs   |
| GENERAL STRUCTURES          |  | Channel, Culvert, or Storm Sewer  |
|                             |  | Levee, Dike, or Floodwall   |
| OTHER FEATURES              |  | 20.2 Cross Sections with 1% Annual Chance Water Surface Elevation   |
|                             |  | 17.5 Cross Sections with 1% Annual Chance Water Surface Elevation   |
|                             |  | Coastal Transect  |
|                             |  | Base Flood Elevation Line (BFE)   |
|                             |  | Limit of Study  |
|                             |  | Jurisdiction Boundary   |
| MAP PANELS                  |  | Coastal Transect Baseline   |
|                             |  | Profile Baseline  |
|                             |  | Hydrographic Feature  |
|                             |  | Digital Data Available  |
|                             |  | No Digital Data Available   |
|                             |  | Unmapped  |



The pin displayed on the map is an approximate point selected by the user and does not represent an authoritative property location.

This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The basemap shown complies with FEMA's basemap accuracy standards

The flood hazard information is derived directly from the authoritative NFHL web services provided by FEMA. This map was exported on 9/9/2022 at 3:00 PM and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or become superseded by new data over time.

This map image is void if the one or more of the following map elements do not appear: basemap imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for unmapped and unmodernized areas cannot be used for regulatory purposes.

Dam Overview

Dam Name

Administration Type

NID ID

WDID

Physical Status

Hazard Class

Stream

Last Inspection Result

FRANKTOWN PARKER FPE-2 (080130)

Jurisdictional Dam

CO00274

Active

Low

EAST CHERRY CR

Conditionally Satisfactory (04/11/2018)

▼ Location

Division

Water District

County

Downstream Town

Town Distance


1

8

EL PASO

FRANKTOWN

25



| Q40 | Q160 | Section | Township | Range  | PM | UTM X    | UTM Y     | Latitude  | Longitude   | Location Accuracy |
|-----|------|---------|----------|--------|----|----------|-----------|-----------|-------------|-------------------|
| NE  | NW   | 30      | 11.0 S   | 65.0 W | S  | 524990.8 | 4324584.3 | 39.070004 | -104.711118 | GPS               |

▼ Dam Details

Primary Name

EAP

EAP Date

Primary Contact

EAP Inundation Map

Inundation Map Date

EL PASO COUNTY

Not Required

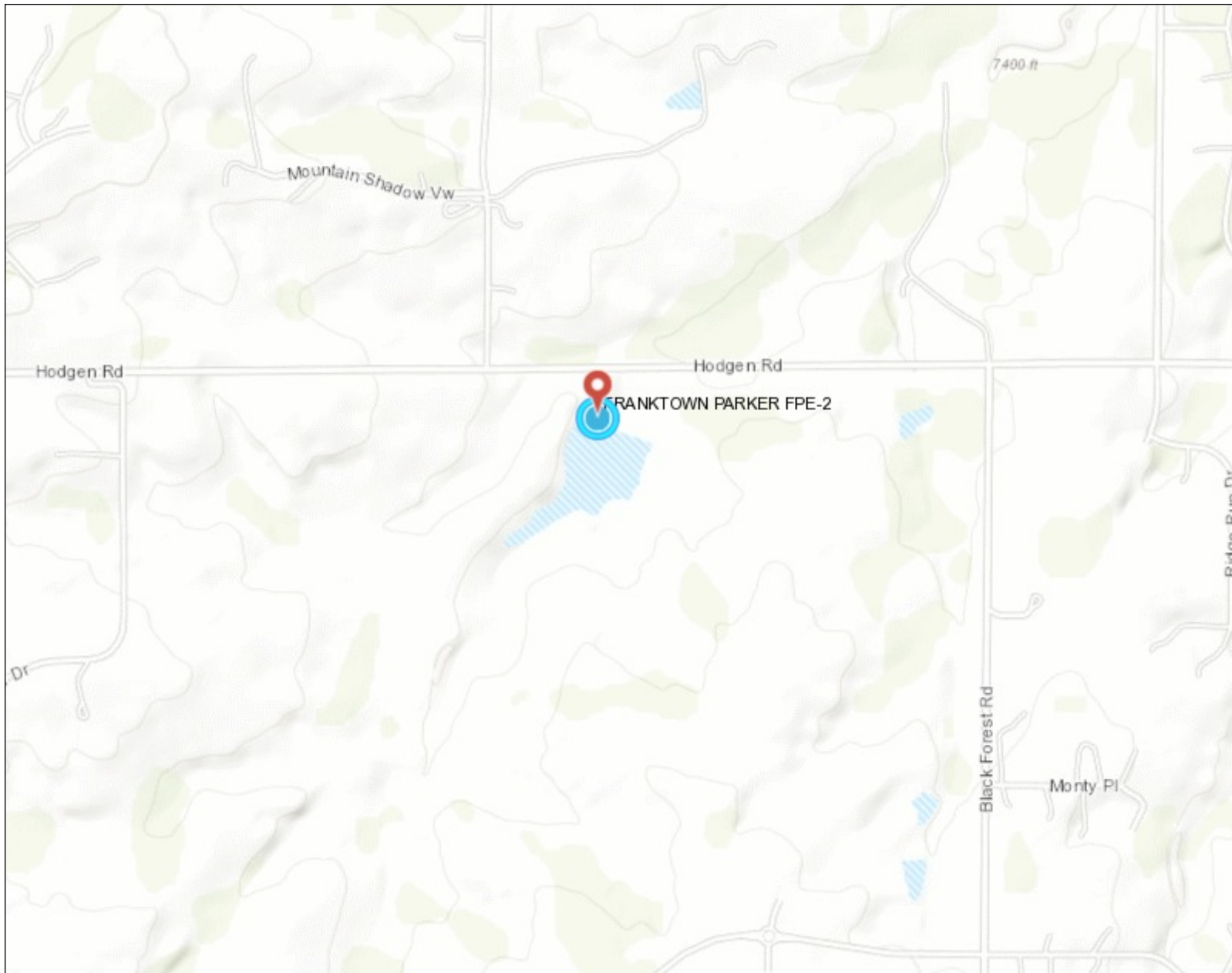
STEVE JACOBSEN

No





## Map Viewer



### Legend

#### Jurisdictional Dam

- High
- Significant
- Low
- NPH

■ Non Jurisdictional Dam

□ County

### Location



### Notes

2,339 0 1,169 2,339 Feet

1: 14,032



*This product is for informational purposes and may not have been prepared for, or be suitable for legal, engineering, or surveying purposes. Users of this information should review or consult the primary data and information sources to ascertain the usability of the information.*

Date Prepared: 9/22/2021 11:42:36 AM

## Appendix B

| Basin Description     | Park/Open Space | 5 Acre | 2.5 Acre | Low Density | Med Density | Commercial              | Total Impervious | Total Acreage | Composite Percent Impervious | Predominant Soil Group | 5 Year C Factor | 100 Year C Factor |
|-----------------------|-----------------|--------|----------|-------------|-------------|-------------------------|------------------|---------------|------------------------------|------------------------|-----------------|-------------------|
| Impervious Percentage | 10%             | 10%    | 15%      | 45%         | 55%         | 75%                     |                  |               |                              |                        |                 |                   |
| P                     | 15.55           | 14.78  | 0.00     | 13.38       | 0.00        | 0.00                    | 9.05             | 43.71         | 20.71%                       | B                      | 0.15            | 0.41              |
|                       |                 |        |          |             |             | <b>Pond 1</b>           |                  | <b>43.71</b>  | <b>20.71%</b>                |                        |                 |                   |
| X1                    | 38.32           | 3.30   | 0.00     | 25.66       | 0.00        | 9.10                    | 22.53            | 76.38         | 29.50%                       | B                      | 0.24            | 0.47              |
|                       |                 |        |          |             |             | <b>Pond 2</b>           |                  | <b>76.38</b>  | <b>29.50%</b>                |                        |                 |                   |
| O                     | 13.17           | 0.00   | 10.72    | 28.63       | 0.00        | 0.00                    | 15.81            | 52.52         | 30.10%                       | B                      | 0.19            | 0.44              |
|                       |                 |        |          |             |             | <b>Pond 3</b>           |                  | <b>52.52</b>  | <b>30.10%</b>                |                        |                 |                   |
| X2                    | 12.11           | 0.00   | 0.00     | 24.22       | 0.00        | 0.00                    | 12.11            | 36.33         | 33.33%                       | B                      | 0.19            | 0.44              |
| X3                    | 38.88           | 16.85  | 0.00     | 6.26        | 0.00        | 0.00                    | 8.39             | 61.99         | 13.53%                       | B                      | 0.13            | 0.40              |
| V2                    | 0.00            | 0.00   | 15.34    | 0.00        | 0.00        | 0.00                    | 2.30             | 15.34         | 15.00%                       | B                      |                 |                   |
| V1                    | 2.11            | 0.00   | 0.00     | 9.46        | 0.00        | 0.00                    | 4.47             | 11.57         | 38.62%                       | B                      | 0.20            | 0.45              |
|                       |                 |        |          |             |             | <b>Pond 4</b>           |                  | <b>125.23</b> | <b>20.85%</b>                |                        |                 |                   |
| N                     | 10.44           | 11.52  | 0.00     | 6.77        | 12.84       | 0.00                    | 12.30            | 41.57         | 29.60%                       | B                      | 0.19            | 0.46              |
|                       |                 |        |          |             |             | <b>Pond 5</b>           |                  | <b>41.57</b>  | <b>29.60%</b>                |                        |                 |                   |
| M                     | 14.55           | 0.00   | 0.00     | 1.24        | 6.94        | 4.10                    | 8.91             | 26.83         | 33.19%                       | B                      | 0.28            | 0.52              |
|                       |                 |        |          |             |             | <b>Pond 6</b>           |                  | <b>26.83</b>  | <b>33.19%</b>                |                        |                 |                   |
| K                     | 26.45           | 2.93   | 0.00     | 61.89       | 23.46       | 0.00                    | 43.69            | 114.73        | 38.08%                       | B                      | 0.21            | 0.47              |
|                       |                 |        |          |             |             | <b>Pond 7</b>           |                  | <b>114.73</b> | <b>38.08%</b>                |                        |                 |                   |
| L                     | 6.93            | 5.54   | 0.00     | 0.00        | 2.72        | 0.00                    | 2.74             | 15.19         | 18.06%                       | B                      | 0.15            | 0.42              |
|                       |                 |        |          |             |             | <b>Pond 8</b>           |                  | <b>15.19</b>  | <b>18.06%</b>                |                        |                 |                   |
| S                     | 2.31            | 0.24   | 0.00     | 19.12       | 0           | 0.00                    | 8.86             | 21.67         | 40.88%                       | B                      | 0.21            | 0.45              |
| R                     | 26.63           | 16.11  | 0.00     | 21.77       | 0.00        | 0.00                    | 14.07            | 64.51         | 21.81%                       | B                      | 0.15            | 0.41              |
|                       |                 |        |          |             |             | <b>Pond 9</b>           |                  | <b>86.18</b>  | <b>21.81%</b>                |                        |                 |                   |
| H                     | 17.65           | 4.31   | 0.00     | 0.00        | 0.00        | 0.00                    | 2.20             | 21.96         | 10.00%                       | B                      | 0.12            | 0.39              |
|                       |                 |        |          |             |             | <b>Pond 10</b>          |                  | <b>21.96</b>  | <b>10.00%</b>                |                        |                 |                   |
| B2                    | 7.20            | 4.48   | 0.00     | 8.31        | 0.00        | 0.00                    | 4.91             | 19.99         | 24.55%                       | B                      | 0.16            | 0.42              |
| B1                    | 12.86           | 13.03  | 0.00     | 33.85       | 0.00        | 0.00                    | 17.82            | 59.74         | 29.83%                       | B                      | 0.18            | 0.43              |
|                       |                 |        |          |             |             | <b>Pond 11</b>          |                  | <b>79.73</b>  | <b>28.51%</b>                |                        |                 |                   |
| J                     | 28.07           | 0.00   | 0.00     | 0.00        | 0.00        | 0.00                    | 2.81             | 28.07         | 10.00%                       | B                      | 0.12            | 0.39              |
|                       |                 |        |          |             |             | <b>Existing Pond 12</b> |                  |               |                              |                        |                 |                   |
| I                     | 17.99           | 0.00   | 0.00     | 0.00        | 0.00        | 11.00                   | 10.05            | 28.99         | 34.66%                       | B                      | 0.38            | 0.58              |
|                       |                 |        |          |             |             | <b>Pond 16</b>          |                  | <b>57.06</b>  | <b>22.53%</b>                |                        |                 |                   |
| EE2                   | 0.00            | 0.00   | 0.00     | 0.00        | 0.00        | 16.36                   | 12.27            | 16.36         | 75.00%                       | B                      | 0.81            | 0.88              |
| EE3                   | 0.00            | 0.00   | 0.00     | 0.00        | 6.67        | 0.00                    | 3.67             | 6.67          | 55.00%                       | B                      | 0.30            | 0.58              |
|                       |                 |        |          |             |             | <b>Pond 13</b>          |                  | <b>23.03</b>  | <b>69.21%</b>                |                        |                 |                   |
| II2                   | 0.00            | 23.13  | 0.00     | 0.00        | 0.00        | 0.00                    | 2.31             | 23.13         | 10.00%                       | B                      | 0.12            | 0.39              |
| II3                   | 0.00            | 23.97  | 0.00     | 0.00        | 0.00        | 0.00                    | 2.40             | 23.97         | 10.00%                       | B                      | 0.12            | 0.39              |
| II1                   | 15.77           | 34.66  | 0.00     | 0.00        | 0.00        | 0.00                    | 5.04             | 50.43         | 10.00%                       | B                      | 0.12            | 0.39              |
|                       |                 |        |          |             |             | <b>Pond 14</b>          |                  | <b>97.53</b>  | <b>10.00%</b>                |                        |                 |                   |
| D                     | 4.41            | 4.70   | 0.00     | 31.76       | 0.00        | 0.00                    | 15.20            | 40.87         | 37.20%                       | B                      | 0.20            | 0.44              |
|                       |                 |        |          |             |             | <b>Pond 15</b>          |                  | <b>40.87</b>  | <b>37.20%</b>                |                        |                 |                   |
| E                     | 99.63           | 8.80   | 0.00     | 1.72        | 0.00        | 6.90                    | 16.79            | 117.05        | 14.35%                       | B                      | 0.16            | 0.42              |
| G                     | 25.81           | 3.41   | 0.00     | 2.23        | 0.00        | 0.00                    | 3.93             | 31.45         | 12.48%                       | B                      | 0.13            | 0.39              |
|                       |                 |        |          |             |             | <b>Irrigation Pond</b>  |                  | <b>148.50</b> | <b>13.95%</b>                |                        |                 |                   |
| JJ                    | 1.86            | 4.32   | 0.00     | 2.72        | 0.00        | 0.00                    | 1.84             | 8.90          | 20.70%                       | B                      | 0.15            | 0.41              |
| LL                    | 4.39            | 1.44   | 0.00     | 0.37        | 0.00        | 0.00                    | 0.75             | 6.20          | 12.09%                       | B                      | 0.13            | 0.39              |
|                       |                 |        |          |             |             | <b>Pond 17</b>          |                  | <b>15.10</b>  | <b>17.16%</b>                |                        |                 |                   |
| KK                    | 5.98            | 2.42   | 0.00     | 0.00        | 0.00        | 0.00                    | 0.84             | 8.40          | 10.00%                       | B                      | 0.12            | 0.39              |
| AA                    | 0.00            | 33.88  | 0.00     | 0.00        | 0.00        | 0.00                    | 3.39             | 33.88         | 10.00%                       | B                      | 0.12            | 0.39              |
| BB                    | 0.00            | 37.15  | 0.00     | 0.00        | 0.00        | 0.00                    | 3.72             | 37.15         | 10.00%                       | B                      | 0.12            | 0.39              |
| CC                    | 0.00            | 6.33   | 0.00     | 0.00        | 0.00        | 0.00                    | 0.63             | 6.33          | 10.00%                       | B                      | 0.12            | 0.39              |
| DD                    | 0.00            | 69.5   | 0.00     | 0.00        | 0.00        | 0.00                    | 6.95             | 69.50         | 10.00%                       | B                      | 0.12            | 0.39              |
| FF                    | 0.00            | 18.1   | 0.00     | 0.00        | 0.00        | 0.00                    | 1.81             | 18.10         | 10.00%                       | B                      | 0.12            | 0.39              |
| GG                    | 0.00            | 16.35  | 0.00     | 0.00        | 0.00        | 0.00                    | 1.64             | 16.35         | 10.00%                       | B                      | 0.12            | 0.39              |
| HH                    | 0.00            | 12.7   | 0.00     | 0.00        | 0.00        | 0.00                    | 1.27             | 12.70         | 10.00%                       | B                      | 0.12            | 0.39              |

\*2% imperviousness for all, and runoff coefficients are .09 and .36 for 5 and 100 yr respectively

**Summary of Unit Hydrograph Parameters Used By Program and Calculated Results (Version 2.0.1)**

| Catchment Name/ID | User Comment for Catchment | Unit Hydrograph Parameters and Results |       |               |                       |               |                       |                           |            |                 | Excess Precip.     |                  | Storm Hydrograph          |                    |                           |                                       |
|-------------------|----------------------------|--|-------|---------------|-----------------------|---------------|-----------------------|---------------------------|------------|-----------------|--------------------|------------------|---------------------------|--------------------|---------------------------|---------------------------------------|
|                   |                            | CT                                     | Cp    | W50<br>(min.) | W50<br>Before<br>Peak | W75<br>(min.) | W75<br>Before<br>Peak | Time to<br>Peak<br>(min.) | Peak (cfs) | Volume<br>(c.f) | Excess<br>(inches) | Excess<br>(c.f.) | Time to<br>Peak<br>(min.) | Peak Flow<br>(cfs) | Total<br>Volume<br>(c.f.) | Runoff per<br>Unit Area<br>(cfs/acre) |
| 1                 | P                          | 0.156                                  | 0.139 | 37.1          | 5.47                  | 19.3          | 3.87                  | 9.1                       | 55         | 158,994         | 1.36               | 215,685          | 40.0                      | 39                 | 215,259                   | 0.89                                  |
| 2                 | X                          | 0.156                                  | 0.249 | 50.8          | 11.22                 | 26.4          | 7.93                  | 18.7                      | 176        | 692,894         | 1.36               | 939,952          | 50.0                      | 139                | 939,989                   | 0.73                                  |
| 3                 | O                          | 0.156                                  | 0.108 | 34.9          | 4.39                  | 18.2          | 3.10                  | 7.3                       | 33         | 89,879          | 1.36               | 121,926          | 40.0                      | 23                 | 121,661                   | 0.92                                  |
| 4                 | N                          | 0.156                                  | 0.147 | 25.7          | 4.39                  | 13.4          | 3.10                  | 7.3                       | 89         | 177,870         | 1.36               | 241,291          | 35.0                      | 57                 | 240,676                   | 1.16                                  |
| 5                 | W                          | 0.156                                  | 0.046 | 33.7          | 2.70                  | 17.5          | 1.90                  | 4.5                       | 5          | 13,649          | 1.36               | 18,515           | 35.0                      | 3                  | 18,246                    | 0.92                                  |
| 6                 | M                          | 0.156                                  | 0.083 | 40.0          | 4.05                  | 20.8          | 2.86                  | 6.7                       | 16         | 50,348          | 1.36               | 68,300           | 40.0                      | 11                 | 68,114                    | 0.83                                  |
| 7                 | V                          | 0.156                                  | 0.132 | 45.0          | 6.05                  | 23.4          | 4.27                  | 10.1                      | 40         | 140,009         | 1.36               | 189,931          | 45.0                      | 30                 | 189,854                   | 0.77                                  |
| 8                 | U                          | 0.156                                  | 0.055 | 44.5          | 3.37                  | 23.2          | 2.38                  | 5.6                       | 6          | 19,892          | 1.36               | 26,985           | 40.0                      | 4                  | 26,889                    | 0.76                                  |
| 9                 | L                          | 0.156                                  | 0.090 | 32.6          | 3.74                  | 17.0          | 2.64                  | 6.2                       | 24         | 59,496          | 1.36               | 80,709           | 35.0                      | 16                 | 80,352                    | 0.96                                  |
| 10                | K                          | 0.156                                  | 0.196 | 32.6          | 6.40                  | 17.0          | 4.52                  | 10.7                      | 134        | 338,098         | 1.36               | 458,650          | 40.0                      | 92                 | 458,862                   | 0.99                                  |
| 11                | S                          | 0.156                                  | 0.107 | 28.6          | 3.85                  | 14.9          | 2.72                  | 6.4                       | 40         | 88,427          | 1.36               | 119,956          | 35.0                      | 26                 | 119,542                   | 1.07                                  |
| 12                | R                          | 0.156                                  | 0.154 | 42.5          | 6.54                  | 22.1          | 4.62                  | 10.9                      | 61         | 199,577         | 1.36               | 270,738          | 45.0                      | 44                 | 270,785                   | 0.80                                  |
| 13                | G                          | 0.156                                  | 0.151 | 29.3          | 4.89                  | 15.2          | 3.46                  | 8.2                       | 83         | 189,450         | 1.36               | 257,000          | 35.0                      | 55                 | 256,005                   | 1.05                                  |
| 14                | D                          | 0.156                                  | 0.132 | 41.6          | 5.71                  | 21.6          | 4.04                  | 9.5                       | 44         | 140,989         | 1.36               | 191,260          | 40.0                      | 32                 | 191,160                   | 0.81                                  |
| 15                | B                          | 0.156                                  | 0.160 | 40.3          | 6.46                  | 20.9          | 4.56                  | 10.8                      | 70         | 216,856         | 1.36               | 294,178          | 40.0                      | 50                 | 294,255                   | 0.84                                  |
| 16                | E                          | 0.156                                  | 0.221 | 50.4          | 10.04                 | 26.2          | 7.10                  | 16.7                      | 119        | 464,132         | 1.36               | 629,622          | 50.0                      | 93                 | 629,347                   | 0.73                                  |
| 17                | H                          | 0.156                                  | 0.099 | 35.7          | 4.22                  | 18.6          | 2.98                  | 7.0                       | 27         | 74,887          | 1.36               | 101,588          | 40.0                      | 19                 | 101,348                   | 0.90                                  |
| 18                | J                          | 0.156                                  | 0.115 | 42.2          | 5.22                  | 21.9          | 3.69                  | 8.7                       | 32         | 103,346         | 1.36               | 140,195          | 40.0                      | 23                 | 139,959                   | 0.80                                  |
| 19                | I                          | 0.156                                  | 0.121 | 28.1          | 4.11                  | 14.6          | 2.90                  | 6.8                       | 53         | 115,906         | 1.36               | 157,233          | 35.0                      | 35                 | 156,699                   | 1.08                                  |
| 20                | JJ                         | 0.156                                  | 0.067 | 26.0          | 2.84                  | 13.5          | 2.01                  | 4.7                       | 16         | 31,654          | 1.36               | 42,940           | 35.0                      | 10                 | 42,323                    | 1.12                                  |
| 21                | LL                         | 0.156                                  | 0.057 | 25.2          | 2.61                  | 13.1          | 1.84                  | 4.4                       | 11         | 22,143          | 1.36               | 30,038           | 35.0                      | 7                  | 29,402                    | 1.13                                  |
| 22                | KK                         | 0.156                                  | 0.065 | 33.9          | 3.20                  | 17.6          | 2.26                  | 5.3                       | 11         | 29,476          | 1.36               | 39,985           | 35.0                      | 8                  | 39,724                    | 0.92                                  |
| 23                | EE                         | 0.126                                  | 0.142 | 26.2          | 4.37                  | 13.6          | 3.09                  | 7.3                       | 124        | 252,176         | 1.37               | 346,639          | 35.0                      | 81                 | 345,618                   | 1.17                                  |
| 24                | DD                         | 0.126                                  | 0.143 | 41.4          | 6.04                  | 21.5          | 4.27                  | 10.1                      | 79         | 254,318         | 1.37               | 349,583          | 40.0                      | 58                 | 349,629                   | 0.83                                  |
| 25                | CC                         | 0.126                                  | 0.048 | 29.8          | 2.61                  | 15.5          | 1.84                  | 4.3                       | 10         | 22,978          | 1.37               | 31,585           | 35.0                      | 7                  | 31,056                    | 1.03                                  |
| 26                | AA                         | 0.126                                  | 0.102 | 26.1          | 3.55                  | 13.6          | 2.51                  | 5.9                       | 60         | 121,569         | 1.37               | 167,107          | 35.0                      | 39                 | 166,376                   | 1.16                                  |
| 27                | BB                         | 0.126                                  | 0.107 | 28.4          | 3.84                  | 14.8          | 2.72                  | 6.4                       | 61         | 134,855         | 1.37               | 185,370          | 35.0                      | 41                 | 184,724                   | 1.09                                  |
| 28                | FF                         | 0.156                                  | 0.092 | 26.9          | 3.41                  | 14.0          | 2.41                  | 5.7                       | 31         | 63,961          | 1.36               | 86,766           | 35.0                      | 20                 | 86,304                    | 1.11                                  |
| 29                | II                         | 0.156                                  | 0.200 | 40.7          | 7.75                  | 21.2          | 5.48                  | 12.9                      | 112        | 354,034         | 1.36               | 480,268          | 45.0                      | 82                 | 479,975                   | 0.84                                  |
| 30                | HH                         | 0.156                                  | 0.080 | 29.6          | 3.31                  | 15.4          | 2.34                  | 5.5                       | 20         | 45,774          | 1.36               | 62,096           | 35.0                      | 13                 | 61,731                    | 1.03                                  |
| 31                | GG                         | 0.156                                  | 0.089 | 34.8          | 3.89                  | 18.1          | 2.75                  | 6.5                       | 22         | 59,351          | 1.36               | 80,512           | 40.0                      | 15                 | 80,308                    | 0.91                                  |
| (OS1) 32          | A                          | 0.156                                  | 0.096 | 27.3          | 3.51                  | 14.2          | 2.48                  | 5.8                       | 33         | 68,934          | 1.36               | 93,513           | 35.0                      | 21                 | 93,026                    | 1.10                                  |
| (OS2) 33          | C                          | 0.156                                  | 0.126 | 32.9          | 4.68                  | 17.1          | 3.31                  | 7.8                       | 50         | 126,578         | 1.36               | 171,711          | 40.0                      | 33                 | 171,254                   | 0.96                                  |
| (OS3) 34          | F                          | 0.156                                  | 0.109 | 32.6          | 4.22                  | 17.0          | 2.98                  | 7.0                       | 36         | 91,658          | 1.36               | 124,339          | 35.0                      | 24                 | 123,917                   | 0.96                                  |
| (OS4) 35          | Q                          | 0.156                                  | 0.175 | 37.1          | 6.48                  | 19.3          | 4.58                  | 10.8                      | 91         | 262,413         | 1.36               | 355,978          | 40.0                      | 65                 | 355,849                   | 0.89                                  |
| (OS5) 36          | T                          | 0.156                                  | 0.054 | 43.6          | 3.29                  | 22.7          | 2.33                  | 5.5                       | 6          | 19,021          | 1.36               | 25,803           | 40.0                      | 4                  | 25,686                    | 0.77                                  |



Printouts for Storm Hydrographs

flow in cfs

| time in minutes | 1     | 2      | 3     | 4     | 5    | 6     | 7     | 8    | 9     | 10    | 11    | 12    | 13    | 14    | 15    | 16    | 17    | 18    | 19    | 20   | 21   | 22   | 23    | 24    | 25    | 26    | 27    | 28    | 29    | 30    | 31    | (OS) 32 | (OS) 33 | (OS) 34 | (OS) 35 | (OS) 36 |
|-----------------|-------|--------|-------|-------|------|-------|-------|------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|------|------|------|-------|-------|-------|-------|-------|-------|-------|-------|-------|---------|---------|---------|---------|---------|
| 5               | 0.00  | 0.00   | 0.00  | 0.00  | 0.00 | 0.00  | 0.00  | 0.00 | 0.00  | 0.00  | 0.00  | 0.00  | 0.00  | 0.00  | 0.00  | 0.00  | 0.00  | 0.00  | 0.00  | 0.00 | 0.00 | 0.00 | 0.00  | 0.00  | 0.00  | 0.00  | 0.00  | 0.00  | 0.00  | 0.00  | 0.00  | 0.00    | 0.00    | 0.00    | 0.00    |         |
| 10              | 0.00  | 0.00   | 0.00  | 0.00  | 0.00 | 0.00  | 0.00  | 0.00 | 0.00  | 0.00  | 0.00  | 0.00  | 0.00  | 0.00  | 0.00  | 0.00  | 0.00  | 0.00  | 0.00  | 0.00 | 0.00 | 0.00 | 0.02  | 0.01  | 0.00  | 0.01  | 0.01  | 0.00  | 0.00  | 0.00  | 0.00  | 0.00    | 0.00    | 0.00    | 0.00    |         |
| 15              | 0.00  | 0.01   | 0.00  | 0.01  | 0.00 | 0.00  | 0.00  | 0.00 | 0.00  | 0.00  | 0.01  | 0.00  | 0.00  | 0.01  | 0.00  | 0.00  | 0.00  | 0.00  | 0.00  | 0.01 | 0.00 | 0.00 | 0.00  | 0.09  | 0.14  | 0.03  | 0.16  | 0.15  | 0.00  | 0.01  | 0.00  | 0.00    | 0.00    | 0.00    | 0.01    |         |
| 20              | 2.82  | 3.48   | 2.02  | 5.45  | 0.37 | 1.04  | 1.85  | 0.40 | 1.58  | 5.79  | 2.64  | 2.56  | 4.88  | 2.14  | 2.98  | 2.78  | 1.69  | 1.68  | 3.39  | 1.11 | 0.80 | 0.79 | 10.09 | 4.91  | 0.93  | 5.44  | 5.37  | 2.13  | 3.81  | 1.40  | 1.45  | 2.24    | 2.89    | 2.27    | 3.89    |         |
| 25              | 18.80 | 27.13  | 13.04 | 35.04 | 2.31 | 6.66  | 12.64 | 2.53 | 9.97  | 40.01 | 16.73 | 17.76 | 30.60 | 14.43 | 20.61 | 21.20 | 10.87 | 11.12 | 21.63 | 6.95 | 5.00 | 4.96 | 51.39 | 26.67 | 4.61  | 27.07 | 26.92 | 13.35 | 27.49 | 8.77  | 8.19  | 14.08   | 18.75   | 14.54   | 26.98   |         |
| 30              | 32.20 | 67.65  | 20.11 | 53.34 | 3.24 | 10.00 | 22.93 | 3.63 | 14.51 | 74.95 | 24.38 | 33.73 | 49.31 | 25.32 | 38.86 | 50.45 | 16.51 | 18.62 | 32.22 | 9.54 | 6.81 | 7.00 | 76.33 | 46.83 | 6.28  | 37.57 | 38.42 | 18.76 | 57.40 | 12.34 | 13.56 | 19.93   | 29.68   | 22.02   | 50.95   |         |
| 35              | 37.59 | 103.16 | 22.47 | 56.97 | 3.45 | 11.18 | 27.54 | 4.01 | 15.71 | 89.75 | 25.99 | 41.20 | 54.90 | 29.98 | 47.20 | 73.62 | 18.37 | 21.73 | 34.58 | 9.74 | 6.88 | 7.51 | 81.16 | 55.57 | 6.53  | 38.76 | 40.62 | 19.51 | 74.33 | 13.01 | 14.88 | 20.84   | 33.29   | 24.27   | 61.71   |         |
| 40              | 38.83 | 124.37 | 22.69 | 54.61 | 3.41 | 11.48 | 29.34 | 4.15 | 15.53 | 92.05 | 25.21 | 43.97 | 53.65 | 31.56 | 50.01 | 85.68 | 18.59 | 22.78 | 33.51 | 9.35 | 6.59 | 7.45 | 77.77 | 58.42 | 6.34  | 37.09 | 39.28 | 18.79 | 80.97 | 12.66 | 14.93 | 20.11   | 33.36   | 24.13   | 64.68   |         |
| 45              | 37.82 | 134.83 | 22.01 | 51.22 | 3.31 | 11.24 | 29.63 | 4.12 | 15.02 | 88.60 | 24.01 | 44.21 | 51.36 | 31.41 | 49.79 | 91.24 | 18.06 | 22.66 | 31.84 | 8.81 | 6.19 | 7.22 | 72.99 | 58.09 | 6.07  | 34.82 | 37.29 | 17.75 | 81.77 | 12.11 | 14.48 | 19.03   | 32.21   | 23.30   | 63.33   |         |
| 50              | 36.92 | 138.66 | 21.39 | 48.22 | 3.22 | 11.07 | 29.11 | 4.08 | 14.53 | 85.11 | 22.86 | 43.25 | 49.03 | 30.77 | 48.59 | 92.81 | 17.59 | 22.25 | 30.23 | 8.36 | 5.87 | 7.02 | 68.67 | 56.74 | 5.80  | 32.88 | 35.42 | 16.82 | 79.60 | 11.60 | 14.09 | 18.08   | 31.10   | 22.51   |         |         |
| 55              | 35.74 | 137.39 | 20.54 | 45.47 | 3.08 | 10.79 | 28.60 | 4.00 | 13.83 | 81.17 | 21.71 | 42.31 | 46.51 | 30.07 | 47.34 | 91.29 | 16.94 | 21.76 | 28.69 | 7.89 | 5.53 | 6.72 | 64.77 | 55.32 | 5.52  | 31.00 | 33.58 | 15.93 | 77.56 | 11.03 | 13.52 | 17.10   | 29.67   | 21.44   |         |         |
| 60              | 34.38 | 134.37 | 19.77 | 42.83 | 2.98 | 10.46 | 28.03 | 3.92 | 13.34 | 77.66 | 20.74 | 41.24 | 44.46 | 29.23 | 45.88 | 89.61 | 16.31 | 21.20 | 27.35 | 7.45 | 5.20 | 6.49 | 61.11 | 53.67 | 5.29  | 29.23 | 32.01 | 15.13 | 75.26 | 10.57 | 13.03 | 16.27   | 28.53   | 20.65   |         |         |
| 65              | 33.42 | 132.08 | 19.22 | 40.10 | 2.90 | 10.20 | 27.40 | 3.84 | 12.93 | 74.96 | 19.77 | 40.09 | 42.52 | 28.38 | 44.42 | 88.22 | 15.87 | 20.61 | 26.02 | 6.99 | 4.85 | 6.30 | 57.32 | 52.02 | 5.07  | 27.41 | 30.44 | 14.29 | 72.80 | 10.13 | 12.67 | 15.41   | 27.63   | 19.99   |         |         |
| 70              | 32.67 | 129.88 | 18.71 | 37.41 | 2.81 | 10.01 | 26.80 | 3.77 | 12.51 | 72.41 | 18.77 | 39.24 | 40.53 | 27.84 | 43.51 | 86.72 | 15.48 | 20.23 | 24.62 | 6.54 | 4.51 | 6.12 | 53.59 | 50.94 | 4.83  | 25.62 | 28.81 | 13.44 | 71.13 | 9.67  | 12.33 | 14.52   | 26.74   | 19.34   |         |         |
| 75              | 31.65 | 127.10 | 17.97 | 35.03 | 2.68 | 9.74  | 26.26 | 3.69 | 11.89 | 69.15 | 17.47 | 38.39 | 37.93 | 27.21 | 42.48 | 84.83 | 14.90 | 19.78 | 22.87 | 6.12 | 4.25 | 5.85 | 49.74 | 4.51  | 23.92 | 26.77 | 12.49 | 69.50 | 9.04  | 11.83 | 13.46 | 25.49   | 18.39   |         |         |         |
| 80              | 30.26 | 123.94 | 17.01 | 32.95 | 2.52 | 9.38  | 25.58 | 3.59 | 11.12 | 64.89 | 16.30 | 37.25 | 35.20 | 26.33 | 41.03 | 82.83 | 14.15 | 19.16 | 21.39 | 5.76 | 4.00 | 5.50 | 46.93 | 48.09 | 4.19  | 22.48 | 24.99 | 11.74 | 67.30 | 8.39  | 11.18 | 12.65   | 23.91   | 17.21   |         |         |
| 85              | 28.72 | 121.14 | 16.00 | 31.11 | 2.36 | 8.99  | 24.82 | 3.48 | 10.38 | 60.44 | 15.46 | 35.96 | 33.28 | 25.36 | 39.37 | 80.95 | 13.35 | 18.48 | 20.30 | 5.45 | 3.78 | 5.16 | 44.35 | 46.24 | 3.97  | 21.26 | 23.69 | 11.14 | 64.70 | 7.96  | 10.51 | 12.01   | 22.31   | 16.05   |         |         |
| 90              | 27.15 | 118.36 | 15.07 | 29.45 | 2.25 | 8.59  | 24.03 | 3.36 | 9.91  | 57.34 | 14.78 | 34.60 | 31.83 | 24.34 | 37.64 | 79.04 | 12.58 | 17.77 | 19.38 | 5.18 | 3.58 | 4.90 | 42.04 | 44.32 | 3.81  | 20.16 | 22.63 | 10.60 | 61.93 | 7.63  | 9.92  | 11.45   | 21.23   | 15.32   |         |         |
| 95              | 25.76 | 115.47 | 14.48 | 27.89 | 2.17 | 8.19  | 23.21 | 3.25 | 9.57  | 55.17 | 14.17 | 33.22 | 30.55 | 23.30 | 35.88 | 77.07 | 12.06 | 17.04 | 18.54 | 4.91 | 3.38 | 4.72 | 39.89 | 42.36 | 3.66  | 19.13 | 21.66 | 10.11 | 59.10 | 7.33  | 9.55  | 10.93   | 20.47   | 14.78   |         |         |
| 100             | 24.47 | 111.99 | 13.76 | 25.59 | 2.05 | 7.68  | 22.11 | 3.07 | 9.04  | 52.49 | 13.19 | 31.42 | 28.66 | 21.96 | 33.75 | 74.65 | 11.44 | 16.07 | 17.25 | 4.50 | 3.08 | 4.47 | 36.69 | 39.91 | 3.42  | 17.53 | 20.14 | 9.32  | 55.77 | 6.85  | 9.05  | 10.11   | 19.39   | 13.98   |         |         |
| 105             | 23.25 | 107.68 | 13.03 | 23.18 | 1.94 | 7.29  | 20.84 | 2.89 | 8.52  | 49.42 | 12.22 | 29.45 | 26.63 | 20.67 | 31.92 | 71.64 | 10.86 | 15.10 | 15.93 | 4.09 | 2.78 | 4.22 | 33.37 | 37.57 | 3.18  | 15.93 | 18.62 | 8.54  | 52.60 | 6.38  | 8.58  | 9.29    | 18.28   | 13.17   |         |         |
| 110             | 22.12 | 102.88 | 12.36 | 20.87 | 1.84 | 6.96  | 19.64 | 2.74 | 8.03  | 46.45 | 11.29 | 28.01 | 24.69 | 19.70 | 30.45 | 68.33 | 10.32 | 14.39 | 14.66 | 3.70 | 2.49 | 4.00 | 30.18 | 35.79 | 2.96  | 14.41 | 17.17 | 7.80  | 50.08 | 5.93  | 8.13  | 8.51    | 17.23   | 12.40   |         |         |
| 115             | 21.09 | 97.87  | 11.73 | 18.77 | 1.74 | 6.68  | 18.78 | 2.63 | 7.57  | 43.67 | 10.42 | 26.86 | 22.88 | 18.89 | 29.15 | 64.92 | 9.81  | 13.81 | 13.48 | 3.34 | 2.23 | 3.79 | 27.10 | 34.30 | 2.75  | 13.00 | 15.81 | 7.10  | 47.91 | 5.51  | 7.72  | 7.77    | 16.25   | 11.69   |         |         |
| 120             | 20.02 | 92.74  | 11.06 | 16.98 | 1.63 | 6.37  | 18.02 | 2.52 | 7.07  | 40.83 | 9.47  | 25.73 | 20.95 | 18.08 | 27.85 | 61.47 | 9.27  | 13.22 | 12.20 | 3.00 | 2.04 | 3.55 | 24.35 | 32.80 | 2.52  | 11.64 | 14.33 | 6.36  | 45.79 | 5.05  | 7.27  | 6.99    | 15.20   | 10.92   |         |         |
| 125             | 18.19 | 87.18  | 9.84  | 14.26 | 1.43 | 5.79  | 16.80 | 2.31 | 6.15  | 36.37 | 7.85  | 23.93 | 17.76 | 16.70 | 25.74 | 57.84 | 8.28  | 12.19 | 10.28 | 2.47 | 1.68 | 3.11 | 20.41 | 30.34 | 2.11  | 9.65  | 11.84 | 5.22  | 42.65 | 4.23  | 6.44  | 5.71    | 13.37   | 9.54    |         |         |
| 130             | 16.10 | 81.27  | 8.57  | 11.64 | 1.23 | 5.20  | 15.35 | 2.11 | 5.23  | 31.03 | 6.35  | 21.72 | 14.40 | 15.09 | 23.17 | 53.82 | 7.25  | 11.04 | 8.20  | 2.02 | 1.37 | 2.69 | 16.72 | 27.41 | 1.72  | 7.90  | 9.59  | 4.27  | 38.62 | 3.44  | 5.60  | 4.67    | 11.43   | 8.12    |         |         |
| 135             | 14.09 | 75.08  | 7.37  | 9.43  | 1.04 | 4.64  | 13.95 | 1.92 | 4.38  | 25.87 | 5.19  | 19.58 | 11.69 | 13.55 | 20.67 | 49.59 | 6.28  | 9.94  | 6.71  | 1.65 | 1.11 | 2.29 | 13.59 | 24.59 | 1.39  | 6.43  | 7.85  | 3.50  | 34.54 | 2.79  | 4.81  | 3.83    | 9.59    | 6.79    |         |         |
| 140             | 12.23 | 68.95  | 6.26  | 7.64  | 0.88 | 4.11  | 12.63 | 1.74 | 3.59  | 21.12 | 4.29  | 17.55 | 9.66  | 12.10 | 18.33 | 45.49 | 5.39  | 8.91  | 5.53  | 1.34 | 0.90 | 1.92 | 11.07 | 21.94 | 1.15  | 5.24  | 6.48  | 2.87  | 30.66 | 2.30  | 4.08  | 3.15    | 7.89    | 5.57    |         |         |
| 145             | 10.54 | 63.10  | 5.24  | 6.18  | 0.72 | 3.63  | 11.41 | 1.57 | 2.92  | 17.15 | 3.54  | 15.68 | 7.99  | 10.77 | 16.17 | 41.61 | 4.56  | 7.96  | 4.55  | 1.09 | 0.73 | 1.58 | 8.98  | 19.50 | 0.96  | 4.26  | 5.35  | 2.34  | 27.08 | 1.91  | 3.41  | 2.58    | 6.38    | 4.52    |         |         |
| 150             | 8.94  | 57.66  | 4.29  | 4.97  | 0.59 | 3.19  | 10.29 | 1.42 | 2.42  | 14.19 | 2.92  | 13.96 | 6.61  | 9.54  | 14.19 | 38.02 | 3.79  | 7.08  | 3.74  | 0.88 | 0.58 | 1.29 | 7.27  | 17.24 | 0.80  | 3.44  | 4.41  | 1.91  | 23.82 | 1.59  | 2.79  | 2.11    | 5.28    | 3.75    |         |         |
| 155             | 7.45  | 52.70  | 3.52  | 3.94  | 0.49 | 2.76  | 9.24  | 1.27 | 2.03  | 11.87 | 2.39  | 12.36 | 5.44  | 8.39  | 12.32 | 34.76 | 3.08  | 6.25  | 3.05  | 0.70 | 0.46 | 1.07 | 5.80  | 15.13 | 0.66  | 2.75  | 3.60  | 1.54  | 20.77 | 1.31  | 2.29  | 1.71    | 4.43    | 3.14    |         |         |
| 160             | 6.09  | 48.12  | 2.95  | 3.08  | 0.41 | 2.37  | 8.26  | 1.13 | 1.70  | 9.93  | 1.94  | 10.85 | 4.44  | 7.30  | 10.57 | 31.71 | 2.56  | 5.48  | 2.46  | 0.55 | 0.36 | 0.90 | 4.57  | 13.14 | 0.54  | 2.16  | 2.91  | 1.22  | 17.90 | 1.07  | 1.92  | 1.36    | 3.71    | 2.63    |         |         |
| 165             | 5.05  | 43.81  | 2.48  | 2.39  | 0.35 | 1.99  | 7.34  | 1.01 | 1.41  | 8.24  | 1.55  | 9.43  | 3.58  | 6.28  | 8.92  | 28.85 | 2.16  | 4.75  | 1.96  | 0.43 | 0.28 | 0.76 | 3.56  | 11.27 | 0.44  | 1.69  | 2.33  | 0.96  | 15.20 | 0.87  | 1.62  | 1.08    | 3.09    | 2.19    |         |         |
| 170             | 4.26  | 39.79  | 2.08  | 1.87  | 0.29 | 1.63  | 6.46  | 0.88 | 1.17  | 6.78  | 1.24  | 8.08  | 2.86  | 5.30  | 7.36  | 26.17 | 1.81  | 4.05  | 1.55  | 0.34 | 0.22 | 0.63 | 2.79  | 9.47  | 0.35  | 1.32  | 1.85  | 0.76  | 12.62 | 0.70  | 1.35  | 0.85    | 2.55    | 1.80    |         |         |
| 175             | 3.59  | 36.02  | 1.73  | 1.43  | 0.24 | 1.35  | 5.62  | 0.76 | 0.96  | 5.55  | 0.99  | 6.77  | 2.29  | 4.38  | 6.07  | 23.66 | 1.52  | 3.37  | 1.23  | 0.26 | 0.16 | 0.52 | 2.17  | 7.80  | 0.28  | 1.03  | 1.48  | 0.60  | 10.32 | 0.56  | 1.13  | 0.67    | 2.10    | 1.48    |         |         |
| 180             | 3.01  | 32.46  | 1.44  | 1.06  | 0.20 | 1.14  | 4.81  | 0.65 | 0.78  | 4.52  | 0.78  | 5.56  | 1.83  | 3.61  | 5.10  | 21.27 | 1.26  | 2.76  | 0.97  | 0.20 | 0.12 | 0    |       |       |       |       |       |       |       |       |       |         |         |         |         |         |

### Printouts for Unit Hydrographs

flow in cfs

| Time in minutes | 1     | 2      | 3     | 4     | 5     | 6     | 7     | 8     | 9     | 10     | 11    | 12    | 13    | 14    | 15    | 16     | 17    | 18    | 19    | 20    | 21    | 22     | 23     | 24    | 25     | 26    | 27    | 28    | 29     | 30    | 31    | 32    | 33    | 34    | 35    | 36   |
|-----------------|-------|--------|-------|-------|-------|-------|-------|-------|-------|--------|-------|-------|-------|-------|-------|--------|-------|-------|-------|-------|-------|--------|--------|-------|--------|-------|-------|-------|--------|-------|-------|-------|-------|-------|-------|------|
| 39.76           | 49.06 | 28.60  | 76.96 | 5.22  | 14.75 | 26.15 | 5.87  | 22.26 | 81.67 | 37.29  | 36.07 | 66.04 | 30.25 | 41.99 | 39.19 | 23.94  | 23.71 | 47.89 | 15.74 | 11.33 | 11.17 | 107.22 | 51.61  | 9.97  | 58.05  | 57.18 | 30.05 | 53.69 | 19.76  | 20.44 | 31.63 | 40.75 | 32.05 | 54.93 | 5.58  |      |
| 10              | 55.25 | 123.67 | 32.97 | 87.90 | 5.06  | 16.13 | 40.17 | 5.70  | 23.14 | 133.15 | 39.11 | 60.03 | 82.91 | 43.80 | 69.03 | 92.20  | 26.85 | 31.61 | 52.30 | 14.92 | 10.63 | 10.97  | 122.04 | 79.24 | 9.54   | 58.05 | 59.91 | 29.61 | 104.26 | 19.40 | 21.75 | 31.56 | 49.33 | 35.88 | 90.59 | 5.57 |
| 15              | 53.29 | 166.57 | 31.07 | 76.87 | 4.64  | 15.40 | 39.51 | 5.47  | 21.34 | 129.81 | 34.97 | 59.77 | 76.40 | 42.74 | 68.35 | 117.24 | 25.32 | 30.70 | 46.81 | 12.61 | 8.81  | 10.12  | 107.50 | 77.64 | 8.45   | 50.00 | 53.49 | 25.72 | 111.71 | 17.35 | 20.34 | 27.62 | 46.27 | 33.34 | 89.42 | 5.33 |
| 20              | 48.43 | 175.94 | 27.34 | 62.15 | 3.94  | 14.04 | 37.47 | 5.08  | 18.11 | 115.02 | 28.83 | 56.50 | 62.48 | 39.91 | 68.38 | 10.53  | 7.41  | 8.67  | 87.14 | 72.71 | 7.11  | 41.14  | 44.08  | 21.25 | 106.50 | 14.45 | 17.76 | 22.80 | 39.96  | 28.49 | 82.36 | 4.92  |       |       |       |      |
| 25              | 41.10 | 171.04 | 23.52 | 52.03 | 3.51  | 12.12 | 34.06 | 4.51  | 15.87 | 95.79  | 24.86 | 50.76 | 54.23 | 35.31 | 56.39 | 113.46 | 19.30 | 25.33 | 32.96 | 8.84  | 6.16  | 7.64   | 73.43  | 64.46 | 6.18   | 34.61 | 37.98 | 18.04 | 95.61  | 12.56 | 15.40 | 19.43 | 34.92 | 24.71 | 70.05 | 4.34 |
| 30              | 36.83 | 159.70 | 20.83 | 43.09 | 3.08  | 11.00 | 29.73 | 4.07  | 13.84 | 83.65  | 20.88 | 44.14 | 45.98 | 31.11 | 49.29 | 104.67 | 17.17 | 22.44 | 27.54 | 7.44  | 5.22  | 6.72   | 60.70  | 56.54 | 5.26   | 28.89 | 31.84 | 15.03 | 81.93  | 10.67 | 13.63 | 16.15 | 30.02 | 21.56 | 62.04 | 3.93 |
| 35              | 32.57 | 141.91 | 18.15 | 37.24 | 2.66  | 9.87  | 27.20 | 3.72  | 11.82 | 71.50  | 18.19 | 40.04 | 39.41 | 28.12 | 44.31 | 91.79  | 15.04 | 20.33 | 24.00 | 6.44  | 4.48  | 5.80   | 52.76  | 51.07 | 4.60   | 25.06 | 27.75 | 13.14 | 73.81  | 9.27  | 11.86 | 14.17 | 25.72 | 18.42 | 54.87 | 3.58 |
| 40              | 28.51 | 126.24 | 15.94 | 31.38 | 2.39  | 8.74  | 24.66 | 3.36  | 10.61 | 62.60  | 15.86 | 35.94 | 34.63 | 25.12 | 39.33 | 83.42  | 13.17 | 18.21 | 20.83 | 5.44  | 3.73  | 5.18   | 44.82  | 45.60 | 4.05   | 21.24 | 24.17 | 11.25 | 65.70  | 8.16  | 10.47 | 12.19 | 22.83 | 16.46 | 47.71 | 3.23 |
| 45              | 23.15 | 118.80 | 14.36 | 25.53 | 2.13  | 7.82  | 22.13 | 3.01  | 9.41  | 55.65  | 13.53 | 31.85 | 29.86 | 22.12 | 34.52 | 76.41  | 11.91 | 16.10 | 17.67 | 4.44  | 2.99  | 4.64   | 36.88  | 40.14 | 3.50   | 17.41 | 20.58 | 9.36  | 57.58  | 7.04  | 9.42  | 10.21 | 20.32 | 14.61 | 42.69 | 2.87 |
| 50              | 23.06 | 105.35 | 12.78 | 19.68 | 1.88  | 7.15  | 19.80 | 2.75  | 8.22  | 48.70  | 11.20 | 28.82 | 25.08 | 20.28 | 31.63 | 69.40  | 10.66 | 14.74 | 14.50 | 3.43  | 2.26  | 4.09   | 28.94  | 36.73 | 2.95   | 13.58 | 16.99 | 7.47  | 52.30  | 5.92  | 8.37  | 8.23  | 17.81 | 12.76 | 38.56 | 2.64 |
| 55              | 20.58 | 94.91  | 11.20 | 16.53 | 1.62  | 6.48  | 18.32 | 2.54  | 7.03  | 41.75  | 8.87  | 26.43 | 20.30 | 18.52 | 28.74 | 62.39  | 9.40  | 13.49 | 11.34 | 2.91  | 2.01  | 3.55   |        |       |        |       |       |       |        |       |       |       |       |       |       |      |

Summary of Unit Hydrograph Parameters Used By Program and Calculated Results (Version 2.0.1)

| Catchment Name/ID | User Comment for Catchment | Unit Hydrograph Parameters and Results |       |               |                       |               |                       |                           |            |                  | Excess Precip.     |                  | Storm Hydrograph          |                    |                           |                                       |
|-------------------|----------------------------|--|-------|---------------|-----------------------|---------------|-----------------------|---------------------------|------------|------------------|--------------------|------------------|---------------------------|--------------------|---------------------------|---------------------------------------|
|                   |                            | CT                                     | Cp    | W50<br>(min.) | W50<br>Before<br>Peak | W75<br>(min.) | W75<br>Before<br>Peak | Time to<br>Peak<br>(min.) | Peak (cfs) | Volume<br>(c.f.) | Excess<br>(inches) | Excess<br>(c.f.) | Time to<br>Peak<br>(min.) | Peak Flow<br>(cfs) | Total<br>Volume<br>(c.f.) | Runoff per<br>Unit Area<br>(cfs/acre) |
| 1                 | P                          | 0.156                                  | 0.139 | 37.5          | 5.52                  | 19.5          | 3.90                  | 9.2                       | 55         | 158,994          | 2.54               | 403,480          | 45.0                      | 82                 | 402,649                   | 1.88                                  |
| 2                 | X                          | 0.156                                  | 0.249 | 50.8          | 11.22                 | 26.4          | 7.93                  | 18.7                      | 176        | 692,894          | 2.54               | 1,758,362        | 55.0                      | 299                | 1,758,430                 | 1.56                                  |
| 3                 | O                          | 0.156                                  | 0.108 | 34.9          | 4.39                  | 18.2          | 3.10                  | 7.3                       | 33         | 89,879           | 2.54               | 228,086          | 45.0                      | 49                 | 227,590                   | 1.96                                  |
| 4                 | N                          | 0.156                                  | 0.147 | 25.7          | 4.39                  | 13.4          | 3.10                  | 7.3                       | 89         | 177,870          | 2.54               | 451,382          | 40.0                      | 119                | 450,230                   | 2.43                                  |
| 5                 | W                          | 0.156                                  | 0.046 | 33.7          | 2.70                  | 17.5          | 1.90                  | 4.5                       | 5          | 13,649           | 2.54               | 34,637           | 45.0                      | 7                  | 34,132                    | 1.95                                  |
| 6                 | M                          | 0.156                                  | 0.083 | 40.0          | 4.05                  | 20.8          | 2.86                  | 6.7                       | 16         | 50,348           | 2.54               | 127,769          | 45.0                      | 25                 | 127,421                   | 1.77                                  |
| 7                 | V                          | 0.156                                  | 0.132 | 45.0          | 6.05                  | 23.4          | 4.27                  | 10.1                      | 40         | 140,009          | 2.54               | 355,302          | 50.0                      | 64                 | 355,159                   | 1.66                                  |
| 8                 | U                          | 0.156                                  | 0.055 | 44.5          | 3.37                  | 23.2          | 2.38                  | 5.6                       | 6          | 19,892           | 2.54               | 50,481           | 50.0                      | 9                  | 50,301                    | 1.63                                  |
| 9                 | L                          | 0.156                                  | 0.090 | 32.6          | 3.74                  | 17.0          | 2.64                  | 6.2                       | 24         | 59,496           | 2.54               | 150,983          | 45.0                      | 33                 | 150,313                   | 2.03                                  |
| 10                | K                          | 0.156                                  | 0.196 | 32.6          | 6.40                  | 17.0          | 4.52                  | 10.7                      | 134        | 338,098          | 2.54               | 857,993          | 45.0                      | 195                | 858,390                   | 2.10                                  |
| 11                | S                          | 0.156                                  | 0.107 | 28.6          | 3.85                  | 14.9          | 2.72                  | 6.4                       | 40         | 88,427           | 2.54               | 224,401          | 40.0                      | 55                 | 223,627                   | 2.24                                  |
| 12                | R                          | 0.156                                  | 0.154 | 42.5          | 6.54                  | 22.1          | 4.62                  | 10.9                      | 61         | 199,577          | 2.54               | 506,469          | 50.0                      | 95                 | 506,557                   | 1.73                                  |
| 13                | G                          | 0.156                                  | 0.151 | 29.3          | 4.89                  | 15.2          | 3.46                  | 8.2                       | 83         | 189,450          | 2.54               | 480,767          | 40.0                      | 115                | 478,906                   | 2.21                                  |
| 14                | D                          | 0.156                                  | 0.132 | 41.6          | 5.71                  | 21.6          | 4.04                  | 9.5                       | 44         | 140,989          | 2.54               | 357,789          | 50.0                      | 68                 | 357,603                   | 1.75                                  |
| 15                | B                          | 0.156                                  | 0.160 | 40.3          | 6.46                  | 20.9          | 4.56                  | 10.8                      | 70         | 216,856          | 2.54               | 550,317          | 50.0                      | 107                | 550,461                   | 1.80                                  |
| 16                | E                          | 0.156                                  | 0.221 | 50.4          | 10.04                 | 26.2          | 7.10                  | 16.7                      | 119        | 464,132          | 2.54               | 1,177,830        | 55.0                      | 200                | 1,177,315                 | 1.56                                  |
| 17                | H                          | 0.156                                  | 0.099 | 35.7          | 4.22                  | 18.6          | 2.98                  | 7.0                       | 27         | 74,887           | 2.54               | 190,041          | 45.0                      | 40                 | 189,591                   | 1.93                                  |
| 18                | J                          | 0.156                                  | 0.115 | 42.2          | 5.22                  | 21.9          | 3.69                  | 8.7                       | 32         | 103,346          | 2.54               | 262,262          | 50.0                      | 49                 | 261,821                   | 1.72                                  |
| 19                | I                          | 0.156                                  | 0.121 | 28.1          | 4.11                  | 14.6          | 2.90                  | 6.8                       | 53         | 115,906          | 2.54               | 294,135          | 40.0                      | 73                 | 293,135                   | 2.27                                  |
| 20                | JJ                         | 0.156                                  | 0.067 | 26.0          | 2.84                  | 13.5          | 2.01                  | 4.7                       | 16         | 31,654           | 2.54               | 80,327           | 40.0                      | 20                 | 79,174                    | 2.35                                  |
| 21                | LL                         | 0.156                                  | 0.057 | 25.2          | 2.61                  | 13.1          | 1.84                  | 4.4                       | 11         | 22,143           | 2.54               | 56,192           | 40.0                      | 14                 | 55,003                    | 2.37                                  |
| 22                | KK                         | 0.156                                  | 0.065 | 33.9          | 3.20                  | 17.6          | 2.26                  | 5.3                       | 11         | 29,476           | 2.54               | 74,800           | 45.0                      | 16                 | 74,311                    | 1.97                                  |
| 23                | EE                         | 0.126                                  | 0.142 | 26.2          | 4.37                  | 13.6          | 3.09                  | 7.3                       | 124        | 252,176          | 2.55               | 643,212          | 40.0                      | 167                | 641,316                   | 2.41                                  |
| 24                | DD                         | 0.126                                  | 0.143 | 41.4          | 6.04                  | 21.5          | 4.27                  | 10.1                      | 79         | 254,318          | 2.55               | 648,674          | 50.0                      | 124                | 648,759                   | 1.77                                  |
| 25                | CC                         | 0.126                                  | 0.048 | 29.8          | 2.61                  | 15.5          | 1.84                  | 4.3                       | 10         | 22,978           | 2.55               | 58,608           | 40.0                      | 14                 | 57,626                    | 2.14                                  |
| 26                | AA                         | 0.126                                  | 0.102 | 26.1          | 3.55                  | 13.6          | 2.51                  | 5.9                       | 60         | 121,569          | 2.55               | 310,079          | 40.0                      | 80                 | 308,721                   | 2.40                                  |
| 27                | BB                         | 0.126                                  | 0.107 | 28.4          | 3.84                  | 14.8          | 2.72                  | 6.4                       | 61         | 134,855          | 2.55               | 343,966          | 40.0                      | 84                 | 342,767                   | 2.27                                  |
| 28                | FF                         | 0.156                                  | 0.092 | 26.9          | 3.41                  | 14.0          | 2.41                  | 5.7                       | 31         | 63,961           | 2.54               | 162,313          | 40.0                      | 41                 | 161,448                   | 2.33                                  |
| 29                | II                         | 0.156                                  | 0.200 | 40.7          | 7.75                  | 21.2          | 5.48                  | 12.9                      | 112        | 354,034          | 2.54               | 898,434          | 50.0                      | 176                | 897,885                   | 1.80                                  |
| 30                | HH                         | 0.156                                  | 0.080 | 29.6          | 3.31                  | 15.4          | 2.34                  | 5.5                       | 20         | 45,774           | 2.54               | 116,162          | 40.0                      | 27                 | 115,480                   | 2.17                                  |
| 31                | GG                         | 0.156                                  | 0.089 | 34.8          | 3.89                  | 18.1          | 2.75                  | 6.5                       | 22         | 59,351           | 2.54               | 150,614          | 45.0                      | 32                 | 150,232                   | 1.96                                  |
| (OS1) 32          | A                          | 0.156                                  | 0.096 | 27.3          | 3.51                  | 14.2          | 2.48                  | 5.8                       | 33         | 68,934           | 2.54               | 174,933          | 40.0                      | 44                 | 174,023                   | 2.31                                  |
| (OS2) 33          | C                          | 0.156                                  | 0.126 | 32.9          | 4.68                  | 17.1          | 3.31                  | 7.8                       | 50         | 126,578          | 2.54               | 321,218          | 45.0                      | 71                 | 320,363                   | 2.04                                  |
| (OS3) 34          | F                          | 0.156                                  | 0.109 | 32.6          | 4.22                  | 17.0          | 2.98                  | 7.0                       | 36         | 91,658           | 2.54               | 232,600          | 45.0                      | 52                 | 231,811                   | 2.04                                  |
| (OS4) 35          | Q                          | 0.156                                  | 0.175 | 37.1          | 6.48                  | 19.3          | 4.58                  | 10.8                      | 91         | 262,413          | 2.54               | 665,926          | 45.0                      | 138                | 665,685                   | 1.91                                  |
| (OS5) 36          | T                          | 0.156                                  | 0.054 | 43.6          | 3.29                  | 22.7          | 2.33                  | 5.5                       | 6          | 19,021           | 2.54               | 48,270           | 45.0                      | 9                  | 48,050                    | 1.66                                  |

Printouts for Storm Hydrographs

flow in cfs

| time in minutes | 1     | 2      | 3     | 4      | 5    | 6     | 7     | 8    | 9     | 10     | 11    | 12    | 13     | 14    | 15     | 16     | 17    | 18    | 19    | 20    | 21    | 22    | 23     | 24     | 25    | 26    | 27    | 28    | 29     | 30    | 31    | (OS) 32 | (OS) 33 | (OS) 34 | (OS) 35 | (OS) 36 |
|-----------------|-------|--------|-------|--------|------|-------|-------|------|-------|--------|-------|-------|--------|-------|--------|--------|-------|-------|-------|-------|-------|-------|--------|--------|-------|-------|-------|-------|--------|-------|-------|---------|---------|---------|---------|---------|
| 5               | 0.00  | 0.00   | 0.00  | 0.00   | 0.00 | 0.00  | 0.00  | 0.00 | 0.00  | 0.00   | 0.00  | 0.00  | 0.00   | 0.00  | 0.00   | 0.00   | 0.00  | 0.00  | 0.00  | 0.00  | 0.00  | 0.00  | 0.00   | 0.00   | 0.00  | 0.00  | 0.00  | 0.00  | 0.00   | 0.00  | 0.00  | 0.00    | 0.00    | 0.00    | 0.00    |         |
| 10              | 0.00  | 0.00   | 0.00  | 0.00   | 0.00 | 0.00  | 0.00  | 0.00 | 0.00  | 0.00   | 0.00  | 0.00  | 0.00   | 0.00  | 0.00   | 0.00   | 0.00  | 0.00  | 0.00  | 0.00  | 0.00  | 0.00  | 0.05   | 0.03   | 0.00  | 0.03  | 0.03  | 0.00  | 0.00   | 0.00  | 0.00  | 0.00    | 0.00    | 0.00    | 0.00    | 0.00    |
| 15              | 0.00  | 0.01   | 0.00  | 0.01   | 0.00 | 0.00  | 0.00  | 0.00 | 0.00  | 0.00   | 0.01  | 0.00  | 0.00   | 0.01  | 0.00   | 0.01   | 0.00  | 0.00  | 0.00  | 0.01  | 0.00  | 0.00  | 0.00   | 0.30   | 0.15  | 0.03  | 0.16  | 0.16  | 0.00   | 0.01  | 0.00  | 0.00    | 0.00    | 0.00    | 0.01    | 0.00    |
| 20              | 1.89  | 2.38   | 1.38  | 3.72   | 0.25 | 0.71  | 1.27  | 0.27 | 1.08  | 3.96   | 1.80  | 1.75  | 3.19   | 1.46  | 2.03   | 0.01   | 1.16  | 1.15  | 2.32  | 0.76  | 0.55  | 0.54  | 7.65   | 3.74   | 0.71  | 4.12  | 4.06  | 1.45  | 2.60   | 0.96  | 0.99  | 1.53    | 1.97    | 1.55    | 2.66    | 0.27    |
| 25              | 16.40 | 23.27  | 11.67 | 31.36  | 2.09 | 5.97  | 11.15 | 2.27 | 8.96  | 35.21  | 15.03 | 15.61 | 27.27  | 12.78 | 18.13  | 18.26  | 9.73  | 9.88  | 19.40 | 6.27  | 4.51  | 4.47  | 46.24  | 23.73  | 4.17  | 24.47 | 24.30 | 12.02 | 23.96  | 7.90  | 8.25  | 12.67   | 16.74   | 13.02   | 23.73   | 2.23    |
| 30              | 46.39 | 82.49  | 31.11 | 83.11  | 5.29 | 15.71 | 32.52 | 5.84 | 23.19 | 104.57 | 38.93 | 46.73 | 74.46  | 36.52 | 54.05  | 62.80  | 25.75 | 27.54 | 50.82 | 15.77 | 11.30 | 11.39 | 117.59 | 65.65  | 10.19 | 60.28 | 60.63 | 30.58 | 75.91  | 20.11 | 21.51 | 32.35   | 45.26   | 34.42   | 70.80   | 5.73    |
| 35              | 69.09 | 162.29 | 43.09 | 112.51 | 6.85 | 21.45 | 50.22 | 7.76 | 30.80 | 163.84 | 51.46 | 74.27 | 105.37 | 55.21 | 85.40  | 118.83 | 35.33 | 40.44 | 68.13 | 19.89 | 14.14 | 14.83 | 157.98 | 100.15 | 12.94 | 77.20 | 79.49 | 39.31 | 129.02 | 25.98 | 28.91 | 41.83   | 63.63   | 46.99   | 111.84  | 7.58    |
| 40              | 79.29 | 228.50 | 47.69 | 119.24 | 7.31 | 23.88 | 59.12 | 8.60 | 33.21 | 190.17 | 54.65 | 88.38 | 115.21 | 64.18 | 101.04 | 161.25 | 39.04 | 46.53 | 72.63 | 20.50 | 14.48 | 15.91 | 167.45 | 116.87 | 13.57 | 80.22 | 84.15 | 41.02 | 159.97 | 27.42 | 31.57 | 43.83   | 70.43   | 51.30   | 131.63  | 8.38    |
| 45              | 82.17 | 269.90 | 48.54 | 116.29 | 7.33 | 24.61 | 63.10 | 8.94 | 33.30 | 195.43 | 53.91 | 94.33 | 114.54 | 67.65 | 107.03 | 185.35 | 39.78 | 48.88 | 71.58 | 20.00 | 14.10 | 15.99 | 163.51 | 123.33 | 13.42 | 78.17 | 82.85 | 40.16 | 173.37 | 27.13 | 31.99 | 42.98   | 71.27   | 51.63   | 137.80  | 8.68    |
| 50              | 81.25 | 291.70 | 47.63 | 110.46 | 7.19 | 24.40 | 63.92 | 8.95 | 32.51 | 190.88 | 51.86 | 95.25 | 110.85 | 67.84 | 107.33 | 197.23 | 39.11 | 48.99 | 68.72 | 19.05 | 13.40 | 15.66 | 155.55 | 123.69 | 12.96 | 74.34 | 79.58 | 38.34 | 175.60 | 26.20 | 31.38 | 41.09   | 69.62   | 50.40   | 136.63  | 8.66    |
| 55              | 79.05 | 298.70 | 45.92 | 103.36 | 6.90 | 23.83 | 62.86 | 8.79 | 31.10 | 182.94 | 48.99 | 93.36 | 105.15 | 66.39 | 104.83 | 199.80 | 37.78 | 47.99 | 64.82 | 17.87 | 12.55 | 15.04 | 145.67 | 120.92 | 12.30 | 69.64 | 75.09 | 36.02 | 171.77 | 24.83 | 30.22 | 38.64   | 66.70   | 48.22   | 132.78  | 8.50    |
| 60              | 76.42 | 295.79 | 44.16 | 97.30  | 6.64 | 23.21 | 61.68 | 8.64 | 29.77 | 174.34 | 46.62 | 91.15 | 99.88  | 64.72 | 101.85 | 196.92 | 36.40 | 46.87 | 61.58 | 16.89 | 11.83 | 14.46 | 137.37 | 117.73 | 11.75 | 65.74 | 71.38 | 34.16 | 167.01 | 23.70 | 29.07 | 36.69   | 63.80   | 46.12   | 128.07  | 8.34    |
| 65              | 73.96 | 290.36 | 42.71 | 91.72  | 6.44 | 22.60 | 60.50 | 8.47 | 28.80 | 167.42 | 44.59 | 88.91 | 95.63  | 63.02 | 98.84  | 193.71 | 35.23 | 45.71 | 58.78 | 15.97 | 11.13 | 14.01 | 129.80 | 114.52 | 11.29 | 62.13 | 68.18 | 32.47 | 162.06 | 22.77 | 28.15 | 34.94   | 61.58   | 44.56   | 123.64  | 8.17    |
| 70              | 70.19 | 283.34 | 40.17 | 82.29  | 6.01 | 21.38 | 57.96 | 8.04 | 26.84 | 157.83 | 40.73 | 84.99 | 88.34  | 60.00 | 94.15  | 188.90 | 33.18 | 43.50 | 53.61 | 14.24 | 9.85  | 13.09 | 116.95 | 109.09 | 10.34 | 55.61 | 62.18 | 29.24 | 154.87 | 20.87 | 26.41 | 31.58   | 57.69   | 41.62   | 117.58  | 7.74    |
| 75              | 66.02 | 272.60 | 37.49 | 72.93  | 5.58 | 20.23 | 54.96 | 7.65 | 24.81 | 145.94 | 36.70 | 80.47 | 80.03  | 56.82 | 89.00  | 181.26 | 31.05 | 41.23 | 48.13 | 12.66 | 8.73  | 12.16 | 103.92 | 103.23 | 9.39  | 49.45 | 55.95 | 26.09 | 146.57 | 18.94 | 24.64 | 28.21   | 53.39   | 38.46   | 110.47  | 7.36    |
| 80              | 61.15 | 258.84 | 34.27 | 64.19  | 5.06 | 18.83 | 51.86 | 7.19 | 22.34 | 132.25 | 32.32 | 75.67 | 70.77  | 53.28 | 83.31  | 171.84 | 28.47 | 38.69 | 42.31 | 11.16 | 7.71  | 11.03 | 91.36  | 96.80  | 8.31  | 43.49 | 49.24 | 22.91 | 137.53 | 16.73 | 22.47 | 24.76   | 48.29   | 34.68   | 102.36  | 6.91    |
| 85              | 56.07 | 244.43 | 31.03 | 57.10  | 4.55 | 17.44 | 48.66 | 6.74 | 19.98 | 117.95 | 28.79 | 70.59 | 62.77  | 49.58 | 77.20  | 162.34 | 25.89 | 36.06 | 37.72 | 9.96  | 6.88  | 9.94  | 81.33  | 89.99  | 7.40  | 38.78 | 43.89 | 20.47 | 127.70 | 14.89 | 20.34 | 22.13   | 43.20   | 30.98   | 93.67   | 6.47    |
| 90              | 51.21 | 230.90 | 27.97 | 51.11  | 4.10 | 16.12 | 45.60 | 6.32 | 17.94 | 105.45 | 26.03 | 65.68 | 56.63  | 46.02 | 71.30  | 153.30 | 23.42 | 33.55 | 34.07 | 8.96  | 6.17  | 8.95  | 72.93  | 83.45  | 6.71  | 34.85 | 39.67 | 18.46 | 118.03 | 13.48 | 18.34 | 19.98   | 38.74   | 27.79   | 85.33   | 6.05    |
| 95              | 46.51 | 218.06 | 25.37 | 45.94  | 3.75 | 14.82 | 42.70 | 5.92 | 16.43 | 95.87  | 23.76 | 60.99 | 51.70  | 42.59 | 65.61  | 144.76 | 21.25 | 31.13 | 31.03 | 8.08  | 5.53  | 8.17  | 65.81  | 77.15  | 6.15  | 31.43 | 36.18 | 16.75 | 108.79 | 12.35 | 16.67 | 18.16   | 35.37   | 25.43   | 77.34   | 5.64    |
| 100             | 42.49 | 206.00 | 23.45 | 41.20  | 3.48 | 13.60 | 39.86 | 5.52 | 15.23 | 88.43  | 21.73 | 56.41 | 47.40  | 39.25 | 60.11  | 136.79 | 19.60 | 28.77 | 28.31 | 7.28  | 4.95  | 7.58  | 59.27  | 71.05  | 5.66  | 28.31 | 33.06 | 15.18 | 99.82  | 11.35 | 15.42 | 16.51   | 32.72   | 23.55   | 70.60   | 5.25    |
| 105             | 39.54 | 194.57 | 21.89 | 38.78  | 3.25 | 12.57 | 37.10 | 5.13 | 14.16 | 82.02  | 19.88 | 52.00 | 43.50  | 36.19 | 55.32  | 129.13 | 18.31 | 26.54 | 25.82 | 6.53  | 4.40  | 7.07  | 53.18  | 65.47  | 5.21  | 25.40 | 30.21 | 13.74 | 91.76  | 10.45 | 14.40 | 14.99   | 30.42   | 21.89   | 65.62   | 4.86    |
| 110             | 37.14 | 183.51 | 20.51 | 32.57  | 3.04 | 11.80 | 34.42 | 4.77 | 13.20 | 76.26  | 18.14 | 48.19 | 39.87  | 33.71 | 51.72  | 121.71 | 17.18 | 24.69 | 23.47 | 5.81  | 3.87  | 6.61  | 47.39  | 60.98  | 4.80  | 22.62 | 27.51 | 12.36 | 85.40  | 9.60  | 13.49 | 13.54   | 28.36   | 20.39   | 61.56   | 4.52    |
| 115             | 35.03 | 172.69 | 19.25 | 28.63  | 2.84 | 11.17 | 32.16 | 4.48 | 12.30 | 70.94  | 16.49 | 45.38 | 36.42  | 31.81 | 48.83  | 114.41 | 16.16 | 23.30 | 21.24 | 5.13  | 3.39  | 6.19  | 41.92  | 57.52  | 4.40  | 20.01 | 24.95 | 11.05 | 80.46  | 8.80  | 12.66 | 12.16   | 26.44   | 19.00   | 57.98   | 4.26    |
| 120             | 33.10 | 162.09 | 18.08 | 25.18  | 2.66 | 10.60 | 30.46 | 4.26 | 11.45 | 65.89  | 14.92 | 43.10 | 33.15  | 30.21 | 46.31  | 107.29 | 15.21 | 22.14 | 19.12 | 4.52  | 2.98  | 5.79  | 36.87  | 54.60  | 4.02  | 17.61 | 22.53 | 9.82  | 76.26  | 8.04  | 11.89 | 10.85   | 24.63   | 17.67   | 54.71   | 4.06    |
| 125             | 30.13 | 150.76 | 16.11 | 20.40  | 2.33 | 9.64  | 28.28 | 3.90 | 9.97  | 58.65  | 12.28 | 39.99 | 28.03  | 27.86 | 42.76  | 99.67  | 13.59 | 20.39 | 15.63 | 3.57  | 2.38  | 5.08  | 29.64  | 50.43  | 3.36  | 13.99 | 18.48 | 7.82  | 70.86  | 6.71  | 10.54 | 8.69    | 21.68   | 15.45   | 50.01   | 3.71    |
| 130             | 26.78 | 138.93 | 14.06 | 16.20  | 2.01 | 8.67  | 25.84 | 3.56 | 8.50  | 50.11  | 9.71  | 36.34 | 22.47  | 25.22 | 38.56  | 91.83  | 11.94 | 18.50 | 12.29 | 2.83  | 1.89  | 4.40  | 23.52  | 45.64  | 2.72  | 11.09 | 14.59 | 6.15  | 64.23  | 5.41  | 9.19  | 6.81    | 15.56   | 13.18   | 44.39   | 3.37    |
| 135             | 23.58 | 127.73 | 12.12 | 12.81  | 1.71 | 7.75  | 23.52 | 3.24 | 7.10  | 41.73  | 7.59  | 32.83 | 17.56  | 22.70 | 34.49  | 84.33  | 10.37 | 16.69 | 9.66  | 2.26  | 1.50  | 3.74  | 18.65  | 41.04  | 2.15  | 8.82  | 11.43 | 4.88  | 57.58  | 4.25  | 7.91  | 5.40    | 15.56   | 11.00   | 38.96   | 3.06    |
| 140             | 20.61 | 117.21 | 10.30 | 10.14  | 1.43 | 6.90  | 21.35 | 2.94 | 5.80  | 33.86  | 6.06  | 29.50 | 13.92  | 20.32 | 30.66  | 77.35  | 8.91  | 14.99 | 7.72  | 1.79  | 1.19  | 3.14  | 14.82  | 36.71  | 1.69  | 7.01  | 9.12  | 3.90  | 51.26  | 3.36  | 6.71  | 4.32    | 12.76   | 8.97    | 33.88   | 2.77    |
| 145             | 17.86 | 107.39 | 8.60  | 8.04   | 1.16 | 6.12  | 19.33 | 2.67 | 4.60  | 26.82  | 4.85  | 26.43 | 11.14  | 18.15 | 27.16  | 70.84  | 7.54  | 13.43 | 6.17  | 1.42  | 0.93  | 2.56  | 11.73  | 32.74  | 1.35  | 5.55  | 7.30  | 3.10  | 45.44  | 2.69  | 5.59  | 3.44    | 10.15   | 7.11    | 29.18   | 2.50    |
| 150             | 15.24 | 98.30  | 6.97  | 6.29   | 0.92 | 5.38  | 17.49 | 2.41 | 3.61  | 21.07  | 3.89  | 23.65 | 8.94   | 16.14 | 23.90  | 64.85  | 6.22  | 12.00 | 4.94  | 1.12  | 0.73  | 2.03  | 9.27   | 29.08  | 1.09  | 4.38  | 5.85  | 2.47  | 40.11  | 2.16  | 4.52  | 2.74    | 7.95    | 5.59    | 24.73   | 2.26    |
| 155             | 12.73 | 90.01  | 5.52  | 4.88   | 0.73 | 4.67  | 15.78 | 2.17 | 2.90  | 16.90  | 3.10  | 21.00 | 7.15   | 14.23 | 20.80  | 59.40  | 4.98  | 10.63 | 3.92  | 0.87  | 0.57  | 1.60  | 7.23   | 25.59  | 0.87  | 3.42  | 4.66  | 1.94  | 35.05  | 1.73  | 3.57  | 2.16    | 6.37    | 4.49    | 20.46   | 2.02    |
| 160             | 10.34 | 82.42  | 4.37  | 3.80   | 0.59 | 3.99  | 14.16 | 1.95 | 2.34  | 13.64  | 2.44  | 18.48 | 5.68   | 12.40 | 17.82  | 54.36  | 3.92  | 9.33  | 3.08  | 0.68  | 0.44  | 1.29  | 5.61   | 22.26  | 0.70  | 2.66  | 3.67  | 1.51  | 30.20  | 1.38  | 2.83  | 1.69    | 5.14    | 3.62    | 16.42   | 1.80    |
| 165             | 8.18  | 75.36  | 3.51  | 2.97   | 0.47 | 3.33  | 12.61 | 1.73 | 1.88  | 10.95  | 1.92  | 16.06 | 4.46   | 10.65 | 14.97  | 49.68  | 3.13  | 8.08  | 2.40  | 0.53  | 0.35  | 1.04  | 4.41   | 19.05  | 0.55  | 2.09  | 2.87  | 1.18  | 25.55  | 1.09  | 2.28  | 1.32    | 4.14    | 2.91    | 12.91   | 1.58    |
| 170             | 6.47  | 68.75  | 2.83  | 2.36   | 0.38 | 2.69  | 11.12 | 1.52 | 1.50  |        |       |       |        |       |        |        |       |       |       |       |       |       |        |        |       |       |       |       |        |       |       |         |         |         |         |         |

### Printouts for Unit Hydrographs

flow in cfs

| Time in minutes | Time in minutes |        |       |       |       |       |       |       |       |        |       |       |       |       |       |        |        |       |       |       |       |        |        |       |       |       |       |       |        |       |       |       |       |       |       |      |
|-----------------|-----------------|--------|-------|-------|-------|-------|-------|-------|-------|--------|-------|-------|-------|-------|-------|--------|--------|-------|-------|-------|-------|--------|--------|-------|-------|-------|-------|-------|--------|-------|-------|-------|-------|-------|-------|------|
|                 | 1               | 2      | 3     | 4     | 5     | 6     | 7     | 8     | 9     | 10     | 11    | 12    | 13    | 14    | 15    | 16     | 17     | 18    | 19    | 20    | 21    | 22     | 23     | 24    | 25    | 26    | 27    | 28    | 29     | 30    | 31    | 32    | 33    | 34    | 35    | 36   |
| 39.06           | 49.06           | 28.60  | 76.96 | 5.22  | 14.75 | 26.15 | 5.87  | 22.26 | 81.67 | 37.29  | 36.07 | 66.04 | 30.25 | 41.99 | 39.19 | 23.94  | 23.71  | 47.89 | 15.74 | 11.33 | 11.17 | 107.22 | 51.61  | 9.97  | 58.05 | 57.18 | 30.05 | 53.69 | 19.76  | 20.44 | 31.63 | 40.75 | 32.05 | 54.93 | 5.58  |      |
| 10              | 54.67           | 123.67 | 32.97 | 87.90 | 5.06  | 16.13 | 40.17 | 5.70  | 23.14 | 133.15 | 39.11 | 60.03 | 82.91 | 43.80 | 69.03 | 92.20  | 26.85  | 31.61 | 52.30 | 14.92 | 10.63 | 10.97  | 122.04 | 79.24 | 9.54  | 58.05 | 59.91 | 29.61 | 104.26 | 19.40 | 21.75 | 31.56 | 49.33 | 35.88 | 90.59 | 5.57 |
| 15              | 52.81           | 166.57 | 31.07 | 76.87 | 4.64  | 15.40 | 39.51 | 5.47  | 21.34 | 129.81 | 34.97 | 59.79 | 76.40 | 42.74 | 68.35 | 117.24 | 25.32  | 30.70 | 46.81 | 12.61 | 8.81  | 10.12  | 107.50 | 77.64 | 8.45  | 50.00 | 53.49 | 25.72 | 111.71 | 17.35 | 20.34 | 27.62 | 46.27 | 33.34 | 89.42 | 5.33 |
| 20              | 48.16           | 175.94 | 27.34 | 62.15 | 3.94  | 14.04 | 37.47 | 5.08  | 18.11 | 115.02 | 28.83 | 56.50 | 62.48 | 39.91 | 68.38 | 118.16 | 22.40  | 28.61 | 38.38 | 10.53 | 7.41  | 8.67   | 87.14  | 72.71 | 7.11  | 41.14 | 44.08 | 21.25 | 106.50 | 14.45 | 17.76 | 22.80 | 39.96 | 28.49 | 82.36 | 4.92 |
| 25              | 40.07           | 171.04 | 23.52 | 52.03 | 3.51  | 12.12 | 34.06 | 4.51  | 15.87 | 95.79  | 24.86 | 50.76 | 54.23 | 35.31 | 56.39 | 113.46 | 19.30  | 25.33 | 32.96 | 8.84  | 6.16  | 7.64   | 73.43  | 64.46 | 6.18  | 34.61 | 37.96 | 18.04 | 95.61  | 12.56 | 15.40 | 19.43 | 34.92 | 24.71 | 70.05 | 4.34 |
| 30              | 36.70           | 159.70 | 20.83 | 43.09 | 3.08  | 11.00 | 29.73 | 4.07  | 13.84 | 83.65  | 20.88 | 44.14 | 45.98 | 31.11 | 49.29 | 104.67 | 17.17  | 22.44 | 27.54 | 7.44  | 5.22  | 6.72   | 60.70  | 56.54 | 5.26  | 28.89 | 31.84 | 15.03 | 81.93  | 10.67 | 13.63 | 16.15 | 30.02 | 21.56 | 62.04 | 3.93 |
| 35              | 32.53           | 141.91 | 18.15 | 37.24 | 2.66  | 9.87  | 27.20 | 3.72  | 11.82 | 71.50  | 18.19 | 40.04 | 39.41 | 28.12 | 44.31 | 91.79  | 15.04  | 20.33 | 24.00 | 6.44  | 4.48  | 5.80   | 52.76  | 51.07 | 4.60  | 25.06 | 27.75 | 13.14 | 73.81  | 9.27  | 11.86 | 14.17 | 25.72 | 18.42 | 54.87 | 3.58 |
| 40              | 28.36           | 126.24 | 15.94 | 31.38 | 2.39  | 8.74  | 24.66 | 3.36  | 10.61 | 62.60  | 15.86 | 35.94 | 34.63 | 25.12 | 39.33 | 83.42  | 13.17  | 18.21 | 20.83 | 5.44  | 3.73  | 5.18   | 44.82  | 45.60 | 4.05  | 21.24 | 24.17 | 11.25 | 65.70  | 8.16  | 10.47 | 12.19 | 22.83 | 16.46 | 47.71 | 3.23 |
| 45              | 25.51           | 115.80 | 14.36 | 25.53 | 2.13  | 7.82  | 22.13 | 3.01  | 9.41  | 55.65  | 13.53 | 31.85 | 29.86 | 22.12 | 34.52 | 76.41  | 11.91  | 16.10 | 17.67 | 4.44  | 2.99  | 4.64   | 36.88  | 40.14 | 3.50  | 17.41 | 20.58 | 9.36  | 57.58  | 7.04  | 9.42  | 10.21 | 20.32 | 14.61 | 42.69 | 2.87 |
| 50              | 23.07           | 105.35 | 12.78 | 19.68 | 1.88  | 7.15  | 19.80 | 2.75  | 8.22  | 48.70  | 11.20 | 28.82 | 25.08 | 20.28 | 31.63 | 69.40  | 10.66  | 14.74 | 14.50 | 3.43  | 2.26  | 4.09   | 28.94  | 36.73 | 2.95  | 13.58 | 16.99 | 7.47  | 52.30  | 5.92  | 8.37  | 8.23  | 17.81 | 12.76 | 38.56 | 2.64 |
| 55              | 20.64           | 94.91  | 11.20 | 16.53 | 1.62  | 6.48  | 18.32 | 2.54  | 7.03  | 41.75  | 8.87  | 26.43 | 20.30 | 18.52 | 28.74 | 62.39  | 9.40</ |       |       |       |       |        |        |       |       |       |       |       |        |       |       |       |       |       |       |      |

Summary of Unit Hydrograph Parameters Used By Program and Calculated Results (Version 2.0.1)

| Catchment Name/ID | User Comment for Catchment | Unit Hydrograph Parameters and Results |       |               |                       |               |                       |                           |            |                  | Excess Precip.     |                  | Storm Hydrograph          |                    |                           |                                       |
|-------------------|----------------------------|--|-------|---------------|-----------------------|---------------|-----------------------|---------------------------|------------|------------------|--------------------|------------------|---------------------------|--------------------|---------------------------|---------------------------------------|
|                   |                            | CT                                     | Cp    | W50<br>(min.) | W50<br>Before<br>Peak | W75<br>(min.) | W75<br>Before<br>Peak | Time to<br>Peak<br>(min.) | Peak (cfs) | Volume<br>(c.f.) | Excess<br>(inches) | Excess<br>(c.f.) | Time to<br>Peak<br>(min.) | Peak Flow<br>(cfs) | Total<br>Volume<br>(c.f.) | Runoff per<br>Unit Area<br>(cfs/acre) |
| C1                | P                          | 0.109                                  | 0.109 | 37.4          | 4.63                  | 19.5          | 3.27                  | 7.7                       | 55         | 158,667          | 1.40               | 221,934          | 40.0                      | 40                 | 221,363                   | 0.92                                  |
| C2                | X1                         | 0.100                                  | 0.155 | 31.9          | 5.30                  | 16.6          | 3.75                  | 8.8                       | 112        | 277,259          | 1.42               | 393,306          | 35.0                      | 81                 | 392,534                   | 1.06                                  |
| C3                | O                          | 0.099                                  | 0.133 | 26.4          | 4.19                  | 13.7          | 2.96                  | 7.0                       | 93         | 190,648          | 1.42               | 270,701          | 35.0                      | 64                 | 269,846                   | 1.22                                  |
| C4                | X2                         | 0.097                                  | 0.119 | 29.1          | 4.16                  | 15.1          | 2.94                  | 6.9                       | 59         | 131,878          | 1.43               | 188,214          | 35.0                      | 41                 | 187,567                   | 1.14                                  |
| C5                | X3                         | 0.120                                  | 0.131 | 46.9          | 6.23                  | 24.4          | 4.40                  | 10.4                      | 62         | 225,024          | 1.38               | 311,107          | 45.0                      | 48                 | 311,075                   | 0.77                                  |
| C6                | N                          | 0.100                                  | 0.118 | 15.2          | 2.87                  | 7.9           | 2.03                  | 4.8                       | 129        | 150,899          | 1.42               | 214,092          | 30.0                      | 73                 | 208,706                   | 1.77                                  |
| C7                | V2                         | 0.118                                  | 0.069 | 30.0          | 3.10                  | 15.6          | 2.19                  | 5.2                       | 24         | 55,684           | 1.39               | 77,171           | 35.0                      | 16                 | 76,523                    | 1.05                                  |
| C8                | U                          | 0.156                                  | 0.056 | 40.0          | 3.23                  | 20.8          | 2.28                  | 5.4                       | 7          | 21,272           | 1.36               | 28,856           | 40.0                      | 5                  | 28,711                    | 0.82                                  |
| C9                | M                          | 0.097                                  | 0.104 | 15.7          | 2.75                  | 8.2           | 1.94                  | 4.6                       | 80         | 97,393           | 1.43               | 138,967          | 30.0                      | 47                 | 135,178                   | 1.73                                  |
| C10               | V1                         | 0.094                                  | 0.078 | 26.5          | 3.09                  | 13.8          | 2.18                  | 5.1                       | 20         | 41,999           | 1.44               | 60,441           | 35.0                      | 14                 | 59,892                    | 1.21                                  |
| C11               | L                          | 0.105                                  | 0.069 | 32.9          | 3.24                  | 17.1          | 2.29                  | 5.4                       | 23         | 57,681           | 1.41               | 81,214           | 35.0                      | 16                 | 80,597                    | 1.01                                  |
| C12               | K                          | 0.094                                  | 0.217 | 16.6          | 4.26                  | 8.6           | 3.01                  | 7.1                       | 324        | 416,470          | 1.44               | 598,839          | 30.0                      | 201                | 596,187                   | 1.75                                  |
| C13               | R                          | 0.108                                  | 0.122 | 33.0          | 4.58                  | 17.1          | 3.23                  | 7.6                       | 80         | 203,861          | 1.40               | 285,653          | 35.0                      | 57                 | 284,875                   | 1.01                                  |
| C14               | H                          | 0.126                                  | 0.085 | 42.1          | 4.24                  | 21.9          | 3.00                  | 7.1                       | 24         | 79,715           | 1.37               | 109,575          | 40.0                      | 18                 | 109,307                   | 0.81                                  |
| C15               | J                          | 0.126                                  | 0.095 | 38.9          | 4.33                  | 20.2          | 3.06                  | 7.2                       | 34         | 101,894          | 1.37               | 140,063          | 40.0                      | 24                 | 139,728                   | 0.86                                  |
| C16               | I                          | 0.096                                  | 0.110 | 22.0          | 3.36                  | 11.4          | 2.38                  | 5.6                       | 62         | 105,234          | 1.43               | 150,503          | 30.0                      | 40                 | 149,058                   | 1.39                                  |
| C17               | E                          | 0.119                                  | 0.167 | 54.0          | 8.41                  | 28.1          | 5.95                  | 14.0                      | 92         | 386,704          | 1.38               | 535,352          | 50.0                      | 75                 | 534,977                   | 0.70                                  |
| C18               | G                          | 0.122                                  | 0.098 | 39.3          | 4.44                  | 20.4          | 3.14                  | 7.4                       | 38         | 114,164          | 1.38               | 157,567          | 40.0                      | 27                 | 157,168                   | 0.86                                  |
| C19               | D                          | 0.095                                  | 0.134 | 20.3          | 3.59                  | 10.5          | 2.54                  | 6.0                       | 94         | 148,358          | 1.44               | 213,029          | 30.0                      | 61                 | 211,555                   | 1.50                                  |
| C20               | B2                         | 0.105                                  | 0.076 | 38.3          | 3.74                  | 19.9          | 2.65                  | 6.2                       | 24         | 72,564           | 1.41               | 102,126          | 40.0                      | 18                 | 101,809                   | 0.90                                  |
| C21               | B1                         | 0.100                                  | 0.140 | 29.6          | 4.67                  | 15.4          | 3.30                  | 7.8                       | 95         | 216,856          | 1.42               | 307,783          | 35.0                      | 67                 | 306,584                   | 1.12                                  |
| C22               | W                          | 0.156                                  | 0.046 | 33.7          | 2.70                  | 17.5          | 1.90                  | 4.5                       | 5          | 13,649           | 1.36               | 18,515           | 35.0                      | 3                  | 18,246                    | 0.92                                  |
| C23               | S                          | 0.093                                  | 0.107 | 21.8          | 3.29                  | 11.3          | 2.32                  | 5.5                       | 47         | 78,662           | 1.44               | 113,604          | 30.0                      | 31                 | 112,488                   | 1.42                                  |
| B1                | JJ                         | 0.109                                  | 0.053 | 22.5          | 2.42                  | 11.7          | 1.71                  | 4.0                       | 19         | 32,307           | 1.40               | 45,188           | 30.0                      | 11                 | 43,903                    | 1.29                                  |
| B2                | LL                         | 0.122                                  | 0.047 | 24.1          | 2.37                  | 12.5          | 1.68                  | 4.0                       | 12         | 22,506           | 1.38               | 31,043           | 30.0                      | 7                  | 30,181                    | 1.19                                  |
| B3                | KK                         | 0.126                                  | 0.055 | 32.6          | 2.87                  | 16.9          | 2.03                  | 4.8                       | 12         | 30,492           | 1.37               | 41,914           | 35.0                      | 8                  | 41,402                    | 0.97                                  |
| B4                | EE1                        | 0.126                                  | 0.124 | 30.2          | 4.37                  | 15.7          | 3.09                  | 7.3                       | 79         | 184,658          | 1.37               | 253,830          | 35.0                      | 53                 | 252,727                   | 1.05                                  |
| B5                | DD                         | 0.126                                  | 0.142 | 41.6          | 6.04                  | 21.6          | 4.27                  | 10.1                      | 78         | 252,285          | 1.37               | 346,789          | 40.0                      | 58                 | 346,842                   | 0.83                                  |
| B6                | II3                        | 0.126                                  | 0.088 | 25.0          | 3.19                  | 13.0          | 2.25                  | 5.3                       | 45         | 87,011           | 1.37               | 119,605          | 35.0                      | 28                 | 118,504                   | 1.18                                  |
| B7                | II2                        | 0.126                                  | 0.087 | 23.9          | 3.09                  | 12.4          | 2.18                  | 5.1                       | 45         | 83,962           | 1.37               | 115,413          | 30.0                      | 28                 | 114,044                   | 1.21                                  |
| B8                | II1                        | 0.126                                  | 0.123 | 53.3          | 6.54                  | 27.7          | 4.62                  | 10.9                      | 44         | 183,061          | 1.37               | 251,634          | 50.0                      | 35                 | 251,692                   | 0.69                                  |
| B9                | CC                         | 0.126                                  | 0.048 | 29.8          | 2.61                  | 15.5          | 1.84                  | 4.3                       | 10         | 22,978           | 1.37               | 31,585           | 35.0                      | 7                  | 31,056                    | 1.03                                  |
| B10               | AA                         | 0.126                                  | 0.103 | 26.0          | 3.55                  | 13.5          | 2.51                  | 5.9                       | 61         | 122,694          | 1.37               | 168,654          | 35.0                      | 39                 | 167,923                   | 1.16                                  |
| B11               | BB                         | 0.126                                  | 0.107 | 28.4          | 3.84                  | 14.8          | 2.72                  | 6.4                       | 61         | 134,855          | 1.37               | 185,370          | 35.0                      | 41                 | 184,724                   | 1.09                                  |
| B12               | FF                         | 0.126                                  | 0.078 | 26.0          | 3.05                  | 13.5          | 2.15                  | 5.1                       | 33         | 65,703           | 1.37               | 90,315           | 35.0                      | 21                 | 89,406                    | 1.15                                  |
| B13               | GG                         | 0.126                                  | 0.074 | 33.9          | 3.43                  | 17.6          | 2.43                  | 5.7                       | 23         | 59,351           | 1.37               | 81,583           | 35.0                      | 15                 | 81,214                    | 0.95                                  |
| B14               | HH                         | 0.126                                  | 0.066 | 28.7          | 2.96                  | 14.9          | 2.09                  | 4.9                       | 21         | 46,101           | 1.37               | 63,370           | 35.0                      | 14                 | 62,681                    | 1.07                                  |
| B15               | EE2                        | 0.078                                  | 0.121 | 11.6          | 2.58                  | 6.0           | 1.83                  | 4.3                       | 66         | 59,387           | 1.52               | 90,334           | 30.0                      | 36                 | 86,502                    | 2.18                                  |
| B16               | EE3                        | 0.086                                  | 0.073 | 19.8          | 2.61                  | 10.3          | 1.84                  | 4.3                       | 16         | 24,212           | 1.48               | 35,738           | 30.0                      | 10                 | 34,826                    | 1.56                                  |
| OS1               | A                          | 0.156                                  | 0.096 | 27.3          | 3.51                  | 14.2          | 2.48                  | 5.8                       | 33         | 68,934           | 1.36               | 93,513           | 35.0                      | 21                 | 93,026                    | 1.10                                  |
| OS2               | C                          | 0.156                                  | 0.128 | 32.3          | 4.68                  | 16.8          | 3.31                  | 7.8                       | 53         | 132,096          | 1.36               | 179,196          | 35.0                      | 35                 | 178,684                   | 0.97                                  |
| OS3               | F                          | 0.156                                  | 0.109 | 32.6          | 4.22                  | 17.0          | 2.98                  | 7.0                       | 36         | 91,658           | 1.36               | 124,339          | 35.0                      | 24                 | 123,917                   | 0.96                                  |
| OS4               | Q                          | 0.156                                  | 0.175 | 37.1          | 6.48                  | 19.3          | 4.58                  | 10.8                      | 91         | 262,413          | 1.36               | 355,978          | 40.0                      | 65                 | 355,849                   | 0.89                                  |
| OS5               | T                          | 0.156                                  | 0.054 | 43.6          | 3.29                  | 22.7          | 2.33                  | 5.5                       | 6          | 19,021           | 1.36               | 25,803           | 40.0                      | 4                  | 25,686                    | 0.77                                  |

### Printouts for Storm Hydrographs

|   | a    | b    | c    | d    | e    | f    | g    | h    | i    | j    | k    | l    | m    | n    | o    | p    | q    | r    | s    | t    | u    | v    | w    | x    | y    | z    | aa   | ab   | ac   | ad   | ae   | af   | ag   | ah   | ai   | aj   | ak   | al   | am   | an   | ao   | ap   | aq   | ar   | as   | at   | au   | av   | aw   | ax   | ay   | az   | ba   | bb   | bc   | bd   | be   | bf   | bg   | bh   | bi   | bj   | bk   | bl   | bm   | bn   | bo   | bp   | bq   | br   | bs   | bt   | bu   | bv   | bw   | bx   | by   | bz   | ca   | cb   | cc   | cd   | ce   | cf   | cg   | ch   | ci   | cj   | ck   | cl   | cm   | cn   | co   | cp   | cq   | cr   | cs   | ct   | cu   | cv   | cw   | cx   | cy   | cz   | da   | db   | dc   | dd   | de   | df   | dg   | dh   | di   | dj   | dk   | dl   | dm   | dn   | do   | dp   | dq   | dr   | ds   | dt   | du   | dv   | dw   | dx   | dy   | dz   | ea   | eb   | ec   | ed   | ee   | ef   | eg   | eh   | ei   | ej   | ek   | el   | em   | en   | eo   | ep   | eq   | er   | es   | et   | eu   | ev   | ew   | ex   | ey   | ez   | fa   | fb   | fc   | fd   | fe   | ff   | fg   | fh   | fi   | fj   | fk   | fl   | fm   | fn   | fo   | fp   | fq   | fr   | fs   | ft   | fu   | fv   | fw   | fx   | fy   | fz   | ga   | gb   | gc   | gd   | ge   | gf   | gg   | gh   | gi   | gj   | gk   | gl   | gm   | gn   | go   | gp   | gq   | gr   | gs   | gt   | gu   | gv   | gw   | gx   | gy   | gz   | ha   | hb   | hc   | hd   | he   | hf   | hg   | hi   | hj   | hk   | hl   | hm   | hn   | ho   | hp   | hq   | hr   | hs   | ht   | hu   | hv   | hw   | hx   | hy   | hz   | ia   | ib   | ic   | id   | ie   | if   | ig   | ih   | ii   | ij   | ik   | il   | im   | in   | io   | ip   | iq   | ir   | is   | it   | iu   | iv   | iw   | ix   | iy   | iz   | ja   | jb   | jc   | jd   | je   | jf   | jj   | jh   | ji   | jk   | jl   | jm   | jn   | jo   | jp   | jq   | jr   | js   | jt   | ju   | jv   | jw   | jx   | ky   | kz   | la   | lb   | lc   | ld   | le   | lf   | lg   | lh   | li   | lj   | lk   | ll   | lm   | ln   | lo   | lp   | lq   | lr   | ls   | lt   | lu   | lv   | lw   | lx   | ly   | lz   | ma   | mb   | mc   | md   | me   | mf   | mg   | mh   | mi   | mj   | mk   | ml   | mm   | mn   | mo   | mp   | mq   | mr   | ms   | mt   | mu   | mv   | mw   | mx   | my   | mz   | na   | nb   | nc   | nd   | ne   | nf   | ng   | nh   | ni   | nj   | nk   | nl   | nm   | nn   | no   | np   | nq   | nr   | ns   | nt   | nu   | nv   | nw   | nx   | ny   | nz   | oa   | ob   | oc   | od   | oe   | of   | og   | oh   | oi   | oj   | ok   | ol   | om   | on   | oo   | op   | oq   | or   | os   | ot   | ou   | ov   | ow   | ox   | oy   | oz   | pa   | pb   | pc   | pd   | pe   | pf   | pg | ph | pi | pj | pk | pl | pm | pn | po | pp | pq | pr | ps | pt | pu | pv | pw | px | py | pz | qa | qb | qc | qd | qe | qf | qg | qh | qi | qj | qk | ql | qm | qn | qo | qp | qq | qr | qs | qt | qu | qv | qw | qx | qy | qz | ra | rb | rc | rd | re | rf | rg | rh | ri | rj | rk | rl | rm | rn | ro | rp | rq | rr | rs | rt | ru | rv | rw | rx | ry | rz | sa | sb | sc | sd | se | sf | sg | sh | si | sj | sk | sl | sm | sn | so | sp | sq | sr | ss | st | su | sv | sw | sx | sy | sz | ta | tb | tc | td | te | tf | tg | th | ti | tj | tk | tl | tm | tn | to | tp | tq | tr | ts | tt | tu | tv | tw | tx | ty | tz | ua | ub | uc | ud | ue | uf | ug | uh | ui | uj | uk | ul | um | un | uo | up | uq | ur | us | ut | uu | uv | uw | ux | uy | uz | va | vb | vc | vd | ve | vf | vg | vh | vi | vj | vk | vl | vm | vn | vo | vp | vq | vr | vs | vt | vu | vv | vw | vx | vy | vz | wa | wb | wc | wd | we | wf | wg | wh | wi | wj | wk | wl | wm | wn | wo | wp | wq | wr | ws | wt | wu | wv | ww | wx | wy | wz | xa | xb | xc | xd | xe | xf | xg | xh | xi | xj | xk | xl | xm | xn | xo | xp | xq | xr | xs | xt | xu | xv | xw | xx | xy | xz | ya | yb | yc | yd | ye | yf | yg | yh | yi | yj | yk | yl | ym | yn | yo | yp | yq | yr | ys | yt | yu | yv | yw | yx | yy | yz | za | zb | zc | zd | ze | zf | zg | zh | zi | zj | zk | zl | zm | zn | zo | zp | zq | zr | zs | zt | zu | zv | zw | zx | zy | zz |
|---|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|
| 0 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |

### Printouts for Unit Hydrographs

| Time in minutes | 1     | 2      | 3     | 4     | 5     | 6      | 7     | 8    | 9     | 10    | 11    | 12     | 13    | 14    | 15    | 16    | 17    | 18    | 19    | 20    | 21    | 22   | 23    | 24    | 25    | 26    | 27    | 28    | 29    | 30    | 31    | 32   | 33    | 34    | 35    | 36    | 37    | 38    | 39    | 40    | 41    | 42    | 43    | 44   | 45 | 46 | 47 | 48 | 49 | 50 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |    |
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| 0               | 54.34 | 82.91  | 82.65 | 52.25 | 39.08 | 128.52 | 23.97 | 6.81 | 80.02 | 20.40 | 22.48 | 284.52 | 66.66 | 21.54 | 29.37 | 67.88 | 39.45 | 32.05 | 90.88 | 21.13 | 77.75 | 5.22 | 46.13 | 18.51 | 12.02 | 12.10 | 68.24 | 51.02 | 44.80 | 45.37 | 26.45 | 9.97 | 58.83 | 57.78 | 32.68 | 22.09 | 20.71 | 65.48 | 17.79 | 31.63 | 43.36 | 38.05 | 54.93 | 5.58 |    |    |    |    |    |    |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |    |
| 5               | 45.47 | 111.91 | 92.59 | 57.68 | 61.90 | 103.08 | 23.22 | 6.76 | 64.93 | 19.54 | 22.07 | 302.67 | 79.27 | 24.30 | 33.58 | 58.21 | 81.91 | 37.34 | 88.53 | 24.18 | 93.85 | 5.06 | 43.70 | 16.90 | 11.01 | 11.73 | 78.07 | 78.07 | 42.87 | 42.87 | 43.98 | 9.54 | 58.81 | 59.31 | 31.15 | 22.14 | 19.91 | 44.42 | 14.74 | 31.56 | 52.46 | 35.08 | 50.99 | 5.57 |    |    |    |    |    |    |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |    |
| 10              | 51.97 | 105.69 | 80.26 | 52.17 | 61.19 | 74.64  | 20.77 | 6.40 | 47.60 | 16.76 | 20.25 | 215.59 | 74.24 | 23.37 | 32.06 | 45.83 | 92.45 | 35.73 | 68.11 | 22.89 | 86.21 | 4.64 | 34.34 | 13.46 | 8.99  | 10.68 | 71.58 | 76.75 | 35.84 | 34.89 | 44.04 | 8.45 | 50.57 | 53.49 | 26.44 | 20.49 | 17.54 | 29.78 | 10.86 | 27.62 | 49.05 | 33.34 | 89.42 | 5.37 |    |    |    |    |    |    |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |    |
| 15              | 46.86 | 90.99  | 65.31 | 42.92 | 58.42 | 55.89  | 17.36 | 5.80 | 35.82 | 13.93 | 17.14 | 158.26 | 64.06 | 21.58 | 29.12 | 37.74 | 90.81 | 35.56 | 54.51 | 22.80 | 70.75 | 3.94 | 28.20 | 11.16 | 7.60  | 9.01  | 59.07 | 71.92 | 29.73 | 29.09 | 42.66 | 7.11 | 41.60 | 44.08 | 21.99 | 17.62 | 14.65 | 20.12 | 8.59  | 22.80 | 42.01 | 28.49 | 82.36 | 4.97 |    |    |    |    |    |    |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |    |
| 20              | 46.77 | 77.17  | 55.15 | 37.17 | 53.70 | 41.56  | 15.11 | 5.04 | 27.23 | 11.77 | 15.15 | 124.60 | 55.11 | 18.94 | 26.06 | 30.19 | 86.81 | 27.99 | 43.59 | 17.82 | 61.53 | 3.51 | 22.58 | 9.03  | 6.22  | 7.98  | 51.60 | 63.84 | 24.63 | 23.71 | 41.62 | 6.18 | 34.95 | 37.96 | 18.45 | 15.44 | 12.65 | 12.27 | 6.98  | 18.43 | 36.14 | 26.71 | 70.05 | 4.75 |    |    |    |    |    |    |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |    |
| 25              | 36.04 | 67.19  | 45.65 | 31.41 | 47.04 | 27.23  | 12.90 | 4.58 | 18.65 | 9.86  | 13.25 | 90.94  | 48.22 | 17.04 | 22.63 | 25.47 | 80.44 | 25.31 | 35.74 | 16.05 | 52.31 | 3.08 | 19.01 | 7.67  | 5.32  | 6.96  | 44.13 | 55.98 | 20.76 | 20.14 | 36.78 | 5.26 | 29.19 | 31.84 | 15.50 | 13.59 | 10.64 | 9.05  | 5.65  | 16.15 | 31.47 | 21.56 | 62.04 | 3.93 |    |    |    |    |    |    |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |    |
| 30              | 31.91 | 57.01  | 39.75 | 27.17 | 43.02 | 21.44  | 11.21 | 4.11 | 14.03 | 8.59  | 11.34 | 62.31  | 41.33 | 15.42 | 20.21 | 20.76 | 71.71 | 22.64 | 27.90 | 14.28 | 44.86 | 2.66 | 15.43 | 6.30  | 4.45  | 5.98  | 37.83 | 50.60 | 17.77 | 16.98 | 32.81 | 4.60 | 25.29 | 27.75 | 13.42 | 11.74 | 9.34  | 5.83  | 4.32  | 14.17 | 26.80 | 18.42 | 54.87 | 3.58 |    |    |    |    |    |    |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |    |
| 35              | 27.79 | 52.72  | 33.86 | 23.81 | 39.27 | 16.66  | 9.89  | 3.44 | 11.17 | 7.31  | 10.20 | 51.69  | 36.71 | 13.81 | 17.78 | 16.05 | 65.58 | 19.96 | 20.06 | 12.51 | 39.51 | 2.39 | 11.85 | 4.94  | 3.67  | 5.37  | 33.47 | 45.21 | 14.77 | 13.81 | 30.06 | 4.05 | 21.40 | 24.17 | 11.33 | 10.46 | 8.15  | 2.61  | 3.10  | 12.19 | 23.95 | 16.46 | 47.71 | 3.23 |    |    |    |    |    |    |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |    |
| 40              | 22.77 | 44.82  | 27.86 | 20.45 | 31.52 | 11.88  | 8.57  | 3.27 | 8.31  | 6.04  | 9.07  | 39.87  | 32.68 | 12.21 | 15.99 | 12.03 | 60.71 | 17.50 | 16.67 | 11.35 | 34.15 | 2.13 | 8.97  | 3.67  | 2.85  | 4.76  | 29.10 | 39.83 | 11.78 | 10.65 | 12.11 | 3.50 | 17.50 | 20.58 | 9.25  | 9.37  | 6.96  | 0.00  | 2.66  | 10.21 | 21.18 | 14.61 | 42.69 | 2.85 |    |    |    |    |    |    |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |    |
| 45              | 22.77 | 38.93  | 22.06 | 17.08 | 31.76 | 7.11   | 7.25  | 2.99 | 5.45  | 4.76  | 7.94  | 25.65  | 28.64 | 11.25 | 14.55 | 10.46 | 55.71 | 16.31 | 14.05 | 10.30 | 28.79 | 1.88 | 7.78  | 3.21  | 2.28  | 4.15  | 24.74 | 36.41 | 8.93  | 8.55  | 25.77 | 2.95 | 13.61 | 16.99 | 7.16  | 8.27  | 5.77  |       |       |       |       |       |       |      |    |    |    |    |    |    |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | </ |



Summary of Unit Hydrograph Parameters Used By Program and Calculated Results (Version 2.0.1)

| Catchment Name/ID | User Comment for Catchment | Unit Hydrograph Parameters and Results |       |            |                 |            |                 |                     |            |              | Excess Precip.  |               | Storm Hydrograph    |                 |                     |                                 |
|-------------------|----------------------------|--|-------|------------|-----------------|------------|-----------------|---------------------|------------|--------------|-----------------|---------------|---------------------|-----------------|---------------------|---------------------------------|
|                   |                            | CT                                     | Cp    | W50 (min.) | W50 Before Peak | W75 (min.) | W75 Before Peak | Time to Peak (min.) | Peak (cfs) | Volume (c.f) | Excess (inches) | Excess (c.f.) | Time to Peak (min.) | Peak Flow (cfs) | Total Volume (c.f.) | Runoff per Unit Area (cfs/acre) |
| C1                | P                          | 0.109                                  | 0.109 | 37.4       | 4.63            | 19.5       | 3.27            | 7.7                 | 55         | 158,667      | 2.57            | 407,452       | 45.0                | 83              | 406,404             | 1.90                            |
| C2                | X1                         | 0.100                                  | 0.155 | 31.9       | 5.30            | 16.6       | 3.75            | 8.8                 | 112        | 277,259      | 2.58            | 715,935       | 45.0                | 163             | 714,529             | 2.14                            |
| C3                | O                          | 0.099                                  | 0.133 | 26.4       | 4.19            | 13.7       | 2.96            | 7.0                 | 93         | 190,648      | 2.58            | 492,472       | 40.0                | 127             | 490,916             | 2.43                            |
| C4                | X2                         | 0.097                                  | 0.119 | 29.1       | 4.16            | 15.1       | 2.94            | 6.9                 | 59         | 131,878      | 2.59            | 341,350       | 40.0                | 82              | 340,177             | 2.27                            |
| C5                | X3                         | 0.120                                  | 0.131 | 46.9       | 6.23            | 24.4       | 4.40            | 10.4                | 62         | 225,024      | 2.56            | 575,240       | 50.0                | 101             | 575,182             | 1.62                            |
| C6                | N                          | 0.100                                  | 0.118 | 15.2       | 2.87            | 7.9        | 2.03            | 4.8                 | 129        | 150,899      | 2.58            | 389,674       | 35.0                | 141             | 379,871             | 3.40                            |
| C7                | V2                         | 0.118                                  | 0.069 | 30.0       | 3.10            | 15.6       | 2.19            | 5.2                 | 24         | 55,684       | 2.56            | 142,481       | 40.0                | 33              | 141,285             | 2.17                            |
| C8                | U                          | 0.126                                  | 0.047 | 39.1       | 2.90            | 20.3       | 2.05            | 4.8                 | 7          | 21,272       | 2.55            | 54,257        | 45.0                | 11              | 53,777              | 1.79                            |
| C9                | M                          | 0.097                                  | 0.104 | 15.7       | 2.75            | 8.2        | 1.94            | 4.6                 | 80         | 97,393       | 2.59            | 252,068       | 35.0                | 89              | 245,194             | 3.32                            |
| C10               | V1                         | 0.094                                  | 0.078 | 26.5       | 3.09            | 13.8       | 2.18            | 5.1                 | 20         | 41,999       | 2.60            | 109,069       | 40.0                | 28              | 108,078             | 2.39                            |
| C11               | L                          | 0.105                                  | 0.069 | 32.9       | 3.24            | 17.1       | 2.29            | 5.4                 | 23         | 57,681       | 2.57            | 148,506       | 40.0                | 32              | 147,376             | 2.04                            |
| C12               | K                          | 0.094                                  | 0.217 | 16.6       | 4.26            | 8.6        | 3.01            | 7.1                 | 324        | 416,470      | 2.60            | 1,081,182     | 35.0                | 382             | 1,076,395           | 3.33                            |
| C13               | R                          | 0.108                                  | 0.122 | 33.0       | 4.58            | 17.1       | 3.23            | 7.6                 | 80         | 203,861      | 2.57            | 523,871       | 45.0                | 116             | 522,444             | 2.07                            |
| C14               | H                          | 0.126                                  | 0.085 | 42.1       | 4.24            | 21.9       | 3.00            | 7.1                 | 24         | 79,715       | 2.55            | 203,324       | 45.0                | 38              | 202,827             | 1.72                            |
| C15               | J                          | 0.126                                  | 0.095 | 38.9       | 4.33            | 20.2       | 3.06            | 7.2                 | 34         | 101,894      | 2.55            | 259,896       | 45.0                | 51              | 259,274             | 1.82                            |
| C16               | I                          | 0.096                                  | 0.110 | 22.0       | 3.36            | 11.4       | 2.38            | 5.6                 | 62         | 105,234      | 2.59            | 272,611       | 35.0                | 78              | 269,994             | 2.69                            |
| C17               | E                          | 0.119                                  | 0.167 | 54.0       | 8.41            | 28.1       | 5.95            | 14.0                | 92         | 386,704      | 2.56            | 989,065       | 55.0                | 158             | 988,371             | 1.48                            |
| C18               | G                          | 0.122                                  | 0.098 | 39.3       | 4.44            | 20.4       | 3.14            | 7.4                 | 38         | 114,164      | 2.55            | 291,648       | 45.0                | 57              | 290,911             | 1.82                            |
| C19               | D                          | 0.095                                  | 0.134 | 20.3       | 3.59            | 10.5       | 2.54            | 6.0                 | 94         | 148,358      | 2.59            | 384,936       | 35.0                | 117             | 382,272             | 2.87                            |
| C20               | B2                         | 0.105                                  | 0.076 | 38.3       | 3.74            | 19.9       | 2.65            | 6.2                 | 24         | 72,564       | 2.57            | 186,792       | 45.0                | 37              | 186,213             | 1.86                            |
| C21               | B1                         | 0.100                                  | 0.140 | 29.6       | 4.67            | 15.4       | 3.30            | 7.8                 | 95         | 216,856      | 2.58            | 560,078       | 40.0                | 134             | 557,898             | 2.24                            |
| C22               | W                          | 0.126                                  | 0.038 | 32.9       | 2.47            | 17.1       | 1.74            | 4.1                 | 5          | 13,649       | 2.55            | 34,813        | 40.0                | 7               | 34,153              | 1.98                            |
| C23               | S                          | 0.093                                  | 0.107 | 21.8       | 3.29            | 11.3       | 2.32            | 5.5                 | 47         | 78,662       | 2.60            | 204,568       | 35.0                | 59              | 202,558             | 2.72                            |
| B1                | JJ                         | 0.109                                  | 0.053 | 22.5       | 2.42            | 11.7       | 1.71            | 4.0                 | 19         | 32,307       | 2.57            | 82,963        | 35.0                | 23              | 80,603              | 2.56                            |
| B2                | LL                         | 0.122                                  | 0.047 | 24.1       | 2.37            | 12.5       | 1.68            | 4.0                 | 12         | 22,506       | 2.55            | 57,481        | 40.0                | 15              | 55,886              | 2.43                            |
| B3                | KK                         | 0.126                                  | 0.055 | 32.6       | 2.87            | 16.9       | 2.03            | 4.8                 | 12         | 30,492       | 2.55            | 77,774        | 40.0                | 17              | 76,823              | 2.02                            |
| B4                | EE1                        | 0.126                                  | 0.124 | 30.2       | 4.37            | 15.7       | 3.09            | 7.3                 | 79         | 184,658      | 2.55            | 470,997       | 40.0                | 110             | 468,951             | 2.17                            |
| B5                | DD                         | 0.126                                  | 0.142 | 41.6       | 6.04            | 21.6       | 4.27            | 10.1                | 78         | 252,285      | 2.55            | 643,489       | 50.0                | 122             | 643,587             | 1.76                            |
| B6                | II3                        | 0.126                                  | 0.088 | 25.0       | 3.19            | 13.0       | 2.25            | 5.3                 | 45         | 87,011       | 2.55            | 221,934       | 40.0                | 59              | 219,892             | 2.45                            |
| B7                | II2                        | 0.126                                  | 0.087 | 23.9       | 3.09            | 12.4       | 2.18            | 5.1                 | 45         | 83,962       | 2.55            | 214,157       | 40.0                | 58              | 211,616             | 2.50                            |
| B8                | II1                        | 0.126                                  | 0.123 | 53.3       | 6.54            | 27.7       | 4.62            | 10.9                | 44         | 183,061      | 2.55            | 466,923       | 50.0                | 74              | 467,031             | 1.48                            |
| B9                | CC                         | 0.126                                  | 0.048 | 29.8       | 2.61            | 15.5       | 1.84            | 4.3                 | 10         | 22,978       | 2.55            | 58,608        | 40.0                | 14              | 57,626              | 2.14                            |
| B10               | AA                         | 0.126                                  | 0.103 | 26.0       | 3.55            | 13.5       | 2.51            | 5.9                 | 61         | 122,694      | 2.55            | 312,949       | 40.0                | 81              | 311,592             | 2.40                            |
| B11               | BB                         | 0.126                                  | 0.107 | 28.4       | 3.84            | 14.8       | 2.72            | 6.4                 | 61         | 134,855      | 2.55            | 343,966       | 40.0                | 84              | 342,767             | 2.27                            |
| B12               | FF                         | 0.126                                  | 0.078 | 26.0       | 3.05            | 13.5       | 2.15            | 5.1                 | 33         | 65,703       | 2.55            | 167,585       | 40.0                | 43              | 165,899             | 2.38                            |
| B13               | GG                         | 0.126                                  | 0.074 | 33.9       | 3.43            | 17.6       | 2.43            | 5.7                 | 23         | 59,351       | 2.55            | 151,382       | 45.0                | 32              | 150,699             | 1.99                            |
| B14               | HH                         | 0.126                                  | 0.066 | 28.7       | 2.96            | 14.9       | 2.09            | 4.9                 | 21         | 46,101       | 2.55            | 117,587       | 40.0                | 28              | 116,310             | 2.22                            |
| B15               | EE2                        | 0.078                                  | 0.121 | 11.6       | 2.58            | 6.0        | 1.83            | 4.3                 | 66         | 59,387       | 2.66            | 157,718       | 35.0                | 64              | 151,027             | 3.89                            |
| B16               | EE3                        | 0.086                                  | 0.073 | 19.8       | 2.61            | 10.3       | 1.84            | 4.3                 | 16         | 24,212       | 2.62            | 63,519        | 35.0                | 19              | 61,897              | 2.90                            |
| OS1               | A                          | 0.156                                  | 0.096 | 27.3       | 3.51            | 14.2       | 2.48            | 5.8                 | 33         | 68,934       | 2.54            | 174,933       | 40.0                | 44              | 174,023             | 2.31                            |
| OS2               | C                          | 0.156                                  | 0.128 | 32.3       | 4.68            | 16.8       | 3.31            | 7.8                 | 53         | 132,096      | 2.54            | 335,220       | 45.0                | 75              | 334,263             | 2.07                            |
| OS3               | F                          | 0.156                                  | 0.109 | 32.6       | 4.22            | 17.0       | 2.98            | 7.0                 | 36         | 91,658       | 2.54            | 232,600       | 45.0                | 52              | 231,811             | 2.04                            |
| OS4               | Q                          | 0.156                                  | 0.175 | 37.1       | 6.48            | 19.3       | 4.58            | 10.8                | 91         | 262,413      | 2.54            | 665,926       | 45.0                | 138             | 665,685             | 1.91                            |
| OS5               | T                          | 0.156                                  | 0.054 | 43.6       | 3.29            | 22.7       | 2.33            | 5.5                 | 6          | 19,021       | 2.54            | 48,270        | 45.0                | 9               | 48,050              | 1.66                            |

### Printouts for Storm Hydrographs

[illegible]

Printouts for Unit Hydrographs

| flow in cfs     |       |        |       |       |       |        |       |      |       |       |       |        |       |       |       |       |       |       |       |        |       |      |       |       |       |       |       |       |       |       |       |      |       |       |       |       |       |       |       |       |       |       |       |      |     |     |     |     |     |     |  |
|-----------------|-------|--------|-------|-------|-------|--------|-------|------|-------|-------|-------|--------|-------|-------|-------|-------|-------|-------|-------|--------|-------|------|-------|-------|-------|-------|-------|-------|-------|-------|-------|------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|------|-----|-----|-----|-----|-----|-----|--|
| time in minutes | C1    | C2     | C3    | C4    | C5    | C6     | C7    | C8   | C9    | C10   | C11   | C12    | C13   | C14   | C15   | C16   | C17   | C18   | C19   | C20    | C21   | C22  | C23   | C24   | C25   | C26   | C27   | C28   | C29   | C30   | C31   | C32  | C33   | C34   | C35   | C36   | C37   | C38   | C39   | C40   | C41   | C42   | C43   | C44  | C45 | C46 | C47 | C48 | C49 | C50 |  |
| 5               | 45.34 | 82.91  | 82.65 | 52.25 | 39.08 | 128.52 | 23.97 | 7.03 | 80.02 | 20.40 | 22.44 | 284.52 | 66.66 | 21.54 | 29.37 | 60.88 | 39.45 | 32.05 | 90.88 | 23.13  | 77.75 | 5.35 | 46.13 | 18.51 | 12.02 | 12.10 | 68.24 | 51.02 | 44.80 | 45.37 | 26.45 | 9.97 | 58.83 | 57.18 | 32.68 | 22.09 | 20.71 | 65.48 | 15.79 | 31.63 | 43.36 | 32.05 | 54.93 | 5.58 |     |     |     |     |     |     |  |
| 10              | 54.47 | 111.91 | 91.29 | 57.68 | 61.90 | 103.08 | 23.22 | 6.89 | 64.93 | 19.54 | 22.07 | 302.60 | 79.27 | 24.30 | 33.58 | 58.21 | 81.91 | 37.34 | 88.53 | 24.18  | 93.85 | 5.16 | 43.70 | 16.90 | 11.11 | 11.73 | 78.07 | 78.33 | 42.87 | 42.87 | 43.98 | 9.54 | 58.81 | 59.91 | 31.15 | 22.14 | 19.91 | 44.42 | 14.04 | 31.56 | 52.46 | 35.88 | 90.59 | 5.57 |     |     |     |     |     |     |  |
| 15              | 51.97 | 105.69 | 80.26 | 52.17 | 61.19 | 74.64  | 20.77 | 6.49 | 47.60 | 16.76 | 20.25 | 215.59 | 74.24 | 23.37 | 32.06 | 45.83 | 92.45 | 35.73 | 68.11 | 22.89  | 86.21 | 4.68 | 34.34 | 13.46 | 8.99  | 10.68 | 71.58 | 76.75 | 35.84 | 34.89 | 44.04 | 8.45 | 50.57 | 53.49 | 26.44 | 20.49 | 17.54 | 29.78 | 10.86 | 27.62 | 49.05 | 33.34 | 89.42 | 5.33 |     |     |     |     |     |     |  |
| 20              | 46.86 | 90.99  | 65.31 | 42.92 | 58.42 | 55.89  | 17.36 | 5.82 | 35.82 | 13.93 | 17.14 | 158.26 | 64.06 | 21.58 | 29.12 | 37.74 | 90.81 | 32.56 | 54.51 | 20.58  | 70.75 | 3.97 | 28.20 | 11.16 | 7.60  | 9.01  | 59.07 | 71.92 | 39.73 | 29.09 | 42.66 | 7.11 | 41.60 | 44.08 | 21.99 | 17.62 | 14.65 | 20.12 | 8.59  | 22.80 | 42.03 | 28.49 | 82.36 | 4.92 |     |     |     |     |     |     |  |
| 25              | 40.16 | 77.37  | 55.15 | 37.17 | 53.70 | 41.56  | 15.13 | 5.09 | 27.23 | 11.77 | 15.15 | 124.60 | 55.11 | 18.94 | 25.06 | 30.19 | 86.81 | 27.99 | 43.59 | 17.82  | 61.53 | 3.53 | 22.58 | 9.03  | 6.22  | 7.98  | 51.60 | 63.84 | 24.63 | 23.71 | 40.24 | 6.18 | 34.95 | 37.96 | 18.45 | 15.44 | 12.65 | 12.27 | 6.98  | 19.43 | 36.14 | 24.71 | 70.05 | 4.34 |     |     |     |     |     |     |  |
| 30              | 36.04 | 67.19  | 45.65 | 31.41 | 47.04 | 27.23  | 12.90 | 4.60 | 18.65 | 9.86  | 13.25 | 90.94  | 48.22 | 17.04 | 22.63 | 25.47 | 80.44 | 25.31 | 35.74 | 16.05  | 52.31 | 3.08 | 19.01 | 7.67  | 5.32  | 6.96  | 44.13 | 55.98 | 20.76 | 20.14 | 36.78 | 5.26 | 29.19 | 31.84 | 15.50 | 13.59 | 10.64 | 9.05  | 5.65  | 16.15 | 31.47 | 21.56 | 62.04 | 3.93 |     |     |     |     |     |     |  |
| 35              | 31.91 | 57.01  | 39.75 | 27.17 | 43.02 | 21.44  | 11.21 | 4.11 | 14.03 | 8.59  | 11.34 | 62.31  | 41.33 | 15.42 | 20.21 | 20.76 | 71.71 | 22.64 | 27.90 | 14.28  | 44.86 | 2.65 | 15.43 | 6.30  | 4.49  | 5.98  | 37.83 | 50.60 | 17.77 | 16.98 | 32.81 | 4.60 | 25.29 | 27.75 | 13.42 | 11.74 | 9.34  | 5.83  | 4.32  | 14.17 | 26.80 | 18.42 | 54.87 | 3.58 |     |     |     |     |     |     |  |
| 40              | 27.79 | 50.72  | 33.86 | 23.81 | 39.27 | 16.66  | 9.89  | 3.61 | 11.17 | 7.31  | 10.20 | 51.09  | 36.71 | 13.81 | 17.78 | 16.05 | 65.58 | 19.96 | 20.06 | 12.51  | 39.51 | 2.39 | 11.85 | 4.94  | 3.67  | 5.37  | 33.47 | 45.21 | 14.77 | 13.81 | 30.46 | 4.05 | 21.40 | 24.17 | 11.33 | 10.46 | 8.15  | 2.61  | 3.10  | 12.19 | 23.91 | 16.46 | 47.71 | 3.23 |     |     |     |     |     |     |  |
| 45              | 25.19 | 44.82  | 27.96 | 20.45 | 35.52 | 11.88  | 8.57  | 3.28 | 8.31  | 6.04  | 9.07  | 39.87  | 32.68 | 12.21 | 15.99 | 12.03 | 60.64 | 17.90 | 16.67 | 11.35  | 34.15 | 2.12 | 8.97  | 3.67  | 2.85  | 4.76  | 29.10 | 39.83 | 11.78 | 10.65 | 28.11 | 3.50 | 17.50 | 20.58 | 9.25  | 9.37  | 6.96  | 0.00  | 2.66  | 10.21 | 21.18 | 14.61 | 42.69 | 2.87 |     |     |     |     |     |     |  |
| 50              | 22.77 | 38.93  | 22.06 | 17.08 | 31.76 | 7.11   | 7.25  | 2.99 | 5.45  | 4.76  | 7.94  | 28.65  | 28.64 | 11.25 | 14.55 | 10.46 | 55.71 | 16.31 | 14.05 | 10.30  | 28.79 | 1.85 | 7.78  | 3.21  | 2.28  | 4.15  | 24.74 | 36.41 | 8.93  | 8.55  | 25.77 | 2.95 | 13.61 | 16.99 | 7.16  | 8.27  | 5.77  | 2.22  | 8.23  | 18.45 | 12.76 | 38.56 | 2.64  |      |     |     |     |     |     |     |  |
| 55              | 20.34 | 33.03  | 17.80 | 13.72 | 29.25 | 2.33   | 5.93  | 2.69 | 2.59  | 3.89  | 6.80  | 17.43  | 24.61 | 10.30 | 13.11 | 8.89  | 50.78 | 14.73 | 11.44 | 9.24   | 23.44 | 1.59 | 6.59  | 2.76  | 2.01  | 3.54  | 20.37 | 33.27 | 7.93  | 7.50  | 23.42 | 2.40 | 11.36 | 13.40 | 6.05  | 7.17  | 4.58  | 1.77  | 6.43  | 15.72 | 10.91 | 34.42 | 2.43  |      |     |     |     |     |     |     |  |
| 60              | 17.91 | 27.14  | 15.84 | 11.27 | 27.05 | 0.00   | 4.74  | 2.40 | 0.00  | 3.46  | 5.67  | 6.21   | 20.58 | 9.34  | 11.68 | 7.32  | 46.02 | 13.15 | 8.82  | 8.19   | 13.62 | 1.45 | 5.40  | 2.30  | 1.73  | 2.93  | 16.01 | 30.13 | 6.93  | 6.45  | 21.53 | 1.95 | 10.06 | 11.44 | 5.36  | 6.07  | 3.89  | 1.33  | 5.77  | 12.99 | 9.06  | 30.28 | 2.22  |      |     |     |     |     |     |     |  |
| 65              | 15.49 | 22.03  | 13.87 | 10.14 | 24.85 |        | 4.29  | 2.10 |       | 3.04  | 4.54  | 0.00   | 16.54 | 8.38  | 10.24 | 5.75  | 43.15 | 11.57 | 6.21  | 7.14   | 16.86 | 1.07 | 4.20  | 1.85  | 1.46  | 2.39  | 14.41 | 26.98 | 5.93  | 5.39  | 20.15 | 1.76 | 8.76  | 10.25 | 4.66  | 4.97  | 3.50  | 0.89  | 5.11  | 10.46 | 7.24  | 26.15 | 2.00  |      |     |     |     |     |     |     |  |
| 70              | 13.06 | 20.07  | 11.90 | 9.02  | 22.65 |        | 3.85  | 1.81 |       | 2.61  | 4.15  |        | 14.82 | 7.43  | 8.81  | 4.18  | 40.28 | 9.99  | 3.60  | 6.09   | 15.07 | 0.98 | 3.01  | 1.39  | 1.19  | 2.18  | 12.96 | 23.84 | 4.94  | 4.34  | 18.77 | 1.58 | 7.46  | 9.05  | 3.97  | 4.30  | 3.10  |       | 0.44  | 4.45  | 9.55  | 6.63  | 22.01 | 1.79 |     |     |     |     |     |     |  |
| 75              | 10.84 | 18.10  | 9.94  | 7.90  | 20.45 |        | 3.41  | 1.51 |       | 2.19  | 3.78  |        | 13.47 | 6.47  | 7.37  | 2.61  | 37.41 | 8.40  | 0.98  | 5.03   | 13.29 | 0.89 | 1.82  | 0.94  | 0.91  | 1.98  | 11.50 | 20.70 | 3.94  | 3.28  | 17.39 | 1.39 | 6.16  | 7.85  | 3.27  | 3.94  | 2.71  | 0.00  | 3.79  | 8.64  | 6.01  | 18.13 | 1.58  |      |     |     |     |     |     |     |  |
| 80              | 10.04 | 16.14  | 7.97  | 6.78  | 18.24 |        | 2.97  | 1.34 |       | 1.76  | 3.40  |        | 12.13 | 5.51  | 6.49  | 1.04  | 34.55 | 7.28  | 0.00  | 4.59   | 11.50 | 0.80 | 0.62  | 0.49  | 0.64  | 1.78  | 10.05 | 17.55 | 2.94  | 2.23  | 16.00 | 1.21 | 4.86  | 6.66  | 2.57  | 3.57  | 2.31  | 0.00  | 3.13  | 7.73  | 5.39  | 16.75 | 1.37  |      |     |     |     |     |     |     |  |
| 85              | 9.23  | 14.17  | 6.01  | 5.66  | 16.04 |        | 2.53  | 1.25 |       | 1.34  | 3.02  |        | 10.78 | 4.78  | 6.01  | 0.00  | 31.68 | 6.75  |       | 4.24   | 9.72  | 0.71 | 0.00  | 0.03  | 0.36  | 1.57  | 8.59  | 15.25 | 1.94  | 1.18  | 14.62 | 1.03 | 3.56  | 5.46  | 1.88  | 3.21  | 1.91  |       | 2.47  | 6.83  | 4.78  | 15.37 | 1.16  |      |     |     |     |     |     |     |  |
| 90              | 8.42  | 12.21  | 4.04  | 4.54  | 13.84 |        | 2.09  | 1.15 |       | 0.92  | 2.64  |        | 9.44  | 4.46  | 5.53  |       | 28.81 | 6.23  |       | 3.89   | 7.93  | 0.62 |       | 0.00  | 0.09  | 1.37  | 7.14  | 14.20 | 0.94  | 0.12  | 13.24 | 0.84 | 2.26  | 4.27  | 1.18  | 2.84  | 1.52  |       | 1.81  | 5.92  | 4.16  | 13.99 | 1.07  |      |     |     |     |     |     |     |  |
| 95              | 7.61  | 10.24  | 2.07  | 3.42  | 12.15 |        | 1.65  | 1.05 |       | 0.49  | 2.27  |        | 8.09  | 4.14  | 5.05  |       | 25.94 | 5.70  |       | 3.54   | 6.15  | 0.53 |       | 0.00  | 0.17  | 5.68  | 13.15 | 0.00  | 0.00  | 11.86 | 0.66  | 0.97 | 3.07  | 0.49  | 2.47  | 1.12  |       | 1.15  | 5.01  | 3.55  | 12.61 | 1.00  |       |      |     |     |     |     |     |     |  |
| 100             | 6.80  | 8.28   | 0.11  | 2.30  | 11.42 |        | 1.21  | 0.95 |       | 0.07  | 1.89  |        | 6.75  | 3.82  | 4.57  |       | 23.08 | 5.17  |       | 3.19   | 4.36  | 0.44 |       |       |       | 0.96  | 4.23  | 12.10 |       |       | 10.48 | 0.48 | 0.00  | 1.87  | 0.00  | 2.11  | 0.72  |       | 0.49  | 4.10  | 2.93  | 11.23 | 0.93  |      |     |     |     |     |     |     |  |
| 105             | 5.99  | 6.31   | 0.00  | 1.17  | 10.88 |        | 0.77  | 0.85 |       | 0.00  | 1.51  |        | 5.40  | 3.50  | 4.09  |       | 20.21 | 4.64  |       | 2.84   | 2.58  | 0.36 |       |       |       | 0.76  | 2.77  | 11.06 |       |       | 9.09  | 0.29 | 0.68  |       | 1.74  | 0.33  | 0.00  | 0.19  | 2.31  | 9.85  | 0.85  |       |       |      |     |     |     |     |     |     |  |
| 110             | 5.18  | 4.35   |       | 0.05  | 9.95  |        | 0.33  | 0.75 |       |       | 1.14  |        | 4.06  | 3.18  | 3.62  |       | 18.11 | 4.12  |       | 2.49   | 0.79  | 0.27 |       |       |       | 0.55  | 1.32  | 10.01 |       |       | 8.49  | 0.11 |       |       | 1.38  | 0.00  |       |       | 2.28  | 1.70  | 8.48  | 0.78  |       |      |     |     |     |     |     |     |  |
| 115             | 4.37  | 2.38   |       | 0.00  | 9.21  |        | 0.00  | 0.66 |       |       | 0.76  |        | 2.71  | 2.86  | 3.14  |       | 17.16 | 3.59  |       | 2.13   | 0.00  | 0.18 |       |       |       | 0.35  | 0.00  | 8.96  |       |       |       | 8.03 | 0.00  |       |       |       | 1.01  |       | 1.37  | 1.08  | 7.10  | 0.71  |       |      |     |     |     |     |     |     |  |
| 120             | 3.56  | 0.42   |       |       | 8.48  |        |       | 0.56 |       |       | 0.38  |        | 1.37  | 2.54  | 2.66  |       | 16.20 | 3.06  |       | 1.78   | 0.09  |      |       |       |       | 0.15  |       |       |       |       |       |      |       |       |       |       | 7.57  |       | 0.65  |       | 0.46  | 0.47  | 5.72  | 0.64 |     |     |     |     |     |     |  |
| 125             | 2.76  | 0.00   |       |       | 7.75  |        |       | 0.46 |       |       | 0.00  |        | 0.02  | 2.23  | 2.18  |       | 15.25 | 2.54  |       | 1.43   | 0.00  |      |       |       |       | 0.00  |       |       |       |       |       |      |       |       |       |       |       |       | 7.11  |       | 0.28  |       | 0.44  | 0.57 |     |     |     |     |     |     |  |
| 130             | 1.95  |        |       |       | 7.01  |        |       | 0.36 |       |       | 0.00  |        | 0.00  |       |       |       | 1.91  | 1.70  |       | 1.08   |       |      |       |       |       |       |       |       |       |       |       |      |       |       |       |       |       |       |       |       | 6.65  |       | 0.26  | 0.56 |     |     |     |     |     |     |  |
| 135             | 1.14  |        |       |       | 6.28  |        |       | 0.26 |       |       |       |        |       | 1.59  | 1.22  |       | 13.33 | 1.48  |       | 0.73   |       |      |       |       |       |       |       |       |       |       |       |      |       |       |       |       |       |       |       |       | 6.18  |       | 0.43  | 0.57 |     |     |     |     |     |     |  |
| 140             | 0.33  |        |       |       | 5.55  |        |       | 0.16 |       |       |       |        |       | 1.27  | 0.75  |       | 12.38 | 0.95  |       | 0.38   |       |      |       |       |       |       |       |       |       |       |       |      |       |       |       |       |       |       |       |       | 4.77  |       | 0.20  | 0.36 |     |     |     |     |     |     |  |
| 145             | 0.00  |        |       |       | 4.81  |        |       | 0.07 |       |       |       |        |       | 0.95  | 0.27  |       | 11.42 | 0.43  |       | 0.03   |       |      |       |       |       |       |       |       |       |       |       |      |       |       |       |       |       |       |       |       | 2.68  |       | 0.20  | 0.22 |     |     |     |     |     |     |  |
| 150             |       |        |       |       | 4.08  |        |       | 0.00 |       |       |       |        |       | 0.63  | 0.00  |       | 10.47 | 0.00  |       | 0.00   |       |      |       |       |       |       |       |       |       |       |       |      |       |       |       |       |       |       |       |       | 1.63  |       | 0.00  | 0.29 |     |     |     |     |     |     |  |
| 155             |       |        |       |       | 3.34  |        |       |      |       |       |       |        |       | 0.31  |       |       | 9.51  |       |       | 0.31</ |       |      |       |       |       |       |       |       |       |       |       |      |       |       |       |       |       |       |       |       |       |       |       |      |     |     |     |     |     |     |  |

## Appendix C

EPA STORM WATER MANAGEMENT MODEL - VERSION 5.1 (Build 5.1.012)

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NOTE: The summary statistics displayed in this report are  
based on results found at every computational time step,  
not just on results from each reporting time step.  
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\*\*\*\*\*  
Analysis Options  
\*\*\*\*\*

Flow Units ..... CFS

Process Models:

Rainfall/Runoff ..... NO  
RDII ..... NO  
Snowmelt ..... NO  
Groundwater ..... NO  
Flow Routing ..... YES  
Ponding Allowed ..... NO  
Water Quality ..... NO

Flow Routing Method ..... KINWAVE

Starting Date ..... 01/01/2022 00:00:00

Ending Date ..... 01/01/2022 06:00:00

Antecedent Dry Days ..... 0.0

Report Time Step ..... 00:05:00

Routing Time Step ..... 30.00 sec

| *****                      | Volume    | Volume   |
|----------------------------|-----------|----------|
| Flow Routing Continuity    | acre-feet | 10^6 gal |
| *****                      | -----     | -----    |
| Dry Weather Inflow .....   | 0.000     | 0.000    |
| Wet Weather Inflow .....   | 0.000     | 0.000    |
| Groundwater Inflow .....   | 0.000     | 0.000    |
| RDII Inflow .....          | 0.000     | 0.000    |
| External Inflow .....      | 164.959   | 53.754   |
| External Outflow .....     | 152.095   | 49.563   |
| Flooding Loss .....        | 0.000     | 0.000    |
| Evaporation Loss .....     | 0.000     | 0.000    |
| Exfiltration Loss .....    | 0.000     | 0.000    |
| Initial Stored Volume .... | 0.000     | 0.000    |
| Final Stored Volume .....  | 12.843    | 4.185    |
| Continuity Error (%) ..... | 0.013     |          |

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Highest Flow Instability Indexes

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Link SP101 (3)  
Link SP103 (3)  
Link SP102 (2)

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#### Routing Time Step Summary

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Minimum Time Step : 30.00 sec  
Average Time Step : 30.00 sec  
Maximum Time Step : 30.00 sec  
Percent in Steady State : 0.00  
Average Iterations per Step : 1.00  
Percent Not Converging : 0.00

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#### Node Depth Summary

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| Node | Type     | Average<br>Depth<br>Feet | Maximum<br>Depth<br>Feet | Maximum<br>HGL<br>Feet | Time of Max<br>Occurrence<br>days hr:min | Reported<br>Max Depth<br>Feet |
|------|----------|--------------------------|--------------------------|------------------------|--|-------------------------------|
| A    | JUNCTION | 0.00                     | 0.00                     | 7625.00                | 0 00:00                                  | 0.00                          |
| AA   | JUNCTION | 0.00                     | 0.00                     | 7525.00                | 0 00:00                                  | 0.00                          |
| B    | JUNCTION | 0.00                     | 0.00                     | 7570.00                | 0 00:00                                  | 0.00                          |
| BB   | JUNCTION | 0.00                     | 0.00                     | 7410.00                | 0 00:00                                  | 0.00                          |
| BB1  | JUNCTION | 0.00                     | 0.00                     | 7385.00                | 0 00:00                                  | 0.00                          |
| BB2  | JUNCTION | 0.00                     | 0.00                     | 7365.00                | 0 00:00                                  | 0.00                          |
| C    | JUNCTION | 0.00                     | 0.00                     | 7635.00                | 0 00:00                                  | 0.00                          |
| CC   | JUNCTION | 0.00                     | 0.00                     | 7495.00                | 0 00:00                                  | 0.00                          |
| D    | JUNCTION | 0.00                     | 0.00                     | 7575.00                | 0 00:00                                  | 0.00                          |
| DD   | JUNCTION | 0.00                     | 0.00                     | 7500.00                | 0 00:00                                  | 0.00                          |
| E    | JUNCTION | 0.00                     | 0.00                     | 7572.00                | 0 00:00                                  | 0.00                          |
| EE   | JUNCTION | 0.00                     | 0.00                     | 7525.00                | 0 00:00                                  | 0.00                          |
| F    | JUNCTION | 0.00                     | 0.00                     | 7633.00                | 0 00:00                                  | 0.00                          |
| FF   | JUNCTION | 0.00                     | 0.00                     | 7430.00                | 0 00:00                                  | 0.00                          |
| G    | JUNCTION | 0.00                     | 0.00                     | 7565.00                | 0 00:00                                  | 0.00                          |
| GG   | JUNCTION | 0.00                     | 0.00                     | 7420.00                | 0 00:00                                  | 0.00                          |
| H1   | JUNCTION | 0.00                     | 0.00                     | 7525.00                | 0 00:00                                  | 0.00                          |
| HH   | JUNCTION | 0.00                     | 0.00                     | 7410.00                | 0 00:00                                  | 0.00                          |
| I    | JUNCTION | 0.00                     | 0.00                     | 7595.00                | 0 00:00                                  | 0.00                          |
| II   | JUNCTION | 0.00                     | 0.00                     | 7495.00                | 0 00:00                                  | 0.00                          |
| II1  | JUNCTION | 0.00                     | 0.00                     | 7375.00                | 0 00:00                                  | 0.00                          |
| BB3  | JUNCTION | 0.00                     | 0.00                     | 7330.00                | 0 00:00                                  | 0.00                          |
| J    | JUNCTION | 0.00                     | 0.00                     | 7560.00                | 0 00:00                                  | 0.00                          |
| JJ   | JUNCTION | 0.00                     | 0.00                     | 7575.00                | 0 00:00                                  | 0.00                          |

|          |          |      |      |         |   |       |      |
|----------|----------|------|------|---------|---|-------|------|
| K        | JUNCTION | 0.00 | 0.00 | 7585.00 | 0 | 00:00 | 0.00 |
| KK       | JUNCTION | 0.00 | 0.00 | 7590.00 | 0 | 00:00 | 0.00 |
| L        | JUNCTION | 0.00 | 0.00 | 7548.00 | 0 | 00:00 | 0.00 |
| LL       | JUNCTION | 0.00 | 0.00 | 7580.00 | 0 | 00:00 | 0.00 |
| LL1      | JUNCTION | 0.00 | 0.00 | 7525.00 | 0 | 00:00 | 0.00 |
| M        | JUNCTION | 0.00 | 0.00 | 7590.00 | 0 | 00:00 | 0.00 |
| N        | JUNCTION | 0.00 | 0.00 | 7535.00 | 0 | 00:00 | 0.00 |
| O        | JUNCTION | 0.00 | 0.00 | 7525.00 | 0 | 00:00 | 0.00 |
| P        | JUNCTION | 0.00 | 0.00 | 7480.00 | 0 | 00:00 | 0.00 |
| Q        | JUNCTION | 0.00 | 0.00 | 7585.00 | 0 | 00:00 | 0.00 |
| R        | JUNCTION | 0.00 | 0.00 | 7596.00 | 0 | 00:00 | 0.00 |
| S        | JUNCTION | 0.00 | 0.00 | 7598.00 | 0 | 00:00 | 0.00 |
| SP1      | JUNCTION | 0.00 | 0.00 | 7495.00 | 0 | 00:00 | 0.00 |
| SP2      | JUNCTION | 0.00 | 0.00 | 7490.00 | 0 | 00:00 | 0.00 |
| SP3      | JUNCTION | 0.00 | 0.00 | 7435.00 | 0 | 00:00 | 0.00 |
| T        | JUNCTION | 0.00 | 0.00 | 7583.00 | 0 | 00:00 | 0.00 |
| T1       | JUNCTION | 0.00 | 0.00 | 7565.00 | 0 | 00:00 | 0.00 |
| U        | JUNCTION | 0.00 | 0.00 | 7567.00 | 0 | 00:00 | 0.00 |
| T2       | JUNCTION | 0.00 | 0.00 | 7555.00 | 0 | 00:00 | 0.00 |
| V        | JUNCTION | 0.00 | 0.00 | 7577.00 | 0 | 00:00 | 0.00 |
| X        | JUNCTION | 0.00 | 0.00 | 7500.00 | 0 | 00:00 | 0.00 |
| W        | JUNCTION | 0.00 | 0.00 | 7546.00 | 0 | 00:00 | 0.00 |
| H        | JUNCTION | 0.00 | 0.00 | 7560.00 | 0 | 00:00 | 0.00 |
| OF2      | OUTFALL  | 0.00 | 0.00 | 7550.00 | 0 | 00:00 | 0.00 |
| OF1      | OUTFALL  | 0.00 | 0.00 | 7430.00 | 0 | 00:00 | 0.00 |
| OF3      | OUTFALL  | 0.00 | 0.00 | 7435.00 | 0 | 00:00 | 0.00 |
| OF5      | OUTFALL  | 0.00 | 0.00 | 7520.00 | 0 | 00:00 | 0.00 |
| OF4      | OUTFALL  | 0.00 | 0.00 | 7325.00 | 0 | 00:00 | 0.00 |
| IRR_POND | STORAGE  | 2.17 | 3.25 | 7533.25 | 0 | 02:12 | 3.25 |

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Node Inflow Summary

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|        |         |          |         |        |             |          |      |
|--------|---------|----------|---------|--------|-------------|----------|------|
| -----  |         |          |         |        |             |          |      |
| -----  |         |          |         |        |             |          |      |
| Total  |         | Flow     | Maximum |        | Maximum     | Lateral  |      |
| Inflow |         | Balance  | Lateral | Total  | Time of Max | Inflow   |      |
| Volume |         | Error    | Inflow  | Inflow | Occurrence  | Volume   |      |
| Node   |         | Type     | CFS     | CFS    | days hr:min | 10^6 gal | 10^6 |
| gal    | Percent |          |         |        |             |          |      |
| -----  |         |          |         |        |             |          |      |
| -----  |         |          |         |        |             |          |      |
| A      |         | JUNCTION | 20.84   | 20.84  | 0 00:35     | 0.696    |      |



|       |       |          |       |        |         |       |  |
|-------|-------|----------|-------|--------|---------|-------|--|
| 0.696 | 0.000 |          |       |        |         |       |  |
| AA    |       | JUNCTION | 38.76 | 38.76  | 0 00:35 | 1.24  |  |
| 1.24  | 0.000 |          |       |        |         |       |  |
| B     |       | JUNCTION | 50.01 | 103.48 | 0 00:40 | 2.2   |  |
| 4.18  | 0.000 |          |       |        |         |       |  |
| BB    |       | JUNCTION | 40.62 | 40.62  | 0 00:35 | 1.38  |  |
| 1.38  | 0.000 |          |       |        |         |       |  |
| BB1   |       | JUNCTION | 0.00  | 242.15 | 0 00:35 | 0     |  |
| 8.7   | 0.000 |          |       |        |         |       |  |
| BB2   |       | JUNCTION | 0.00  | 257.03 | 0 00:35 | 0     |  |
| 9.31  | 0.000 |          |       |        |         |       |  |
| C     |       | JUNCTION | 33.36 | 33.36  | 0 00:40 | 1.28  |  |
| 1.28  | 0.000 |          |       |        |         |       |  |
| CC    |       | JUNCTION | 6.53  | 6.53   | 0 00:35 | 0.232 |  |
| 0.232 | 0.000 |          |       |        |         |       |  |
| D     |       | JUNCTION | 31.56 | 31.56  | 0 00:40 | 1.43  |  |
| 1.43  | 0.000 |          |       |        |         |       |  |
| DD    |       | JUNCTION | 58.42 | 58.42  | 0 00:40 | 2.62  |  |
| 2.62  | 0.000 |          |       |        |         |       |  |
| E     |       | JUNCTION | 92.81 | 223.69 | 0 00:45 | 4.71  |  |
| 10.3  | 0.000 |          |       |        |         |       |  |
| EE    |       | JUNCTION | 81.16 | 81.16  | 0 00:35 | 2.59  |  |
| 2.59  | 0.000 |          |       |        |         |       |  |
| F     |       | JUNCTION | 24.27 | 24.27  | 0 00:35 | 0.927 |  |
| 0.927 | 0.000 |          |       |        |         |       |  |
| FF    |       | JUNCTION | 19.51 | 162.77 | 0 00:35 | 0.646 |  |
| 6.08  | 0.000 |          |       |        |         |       |  |
| G     |       | JUNCTION | 54.90 | 79.17  | 0 00:35 | 1.91  |  |
| 2.84  | 0.000 |          |       |        |         |       |  |
| GG    |       | JUNCTION | 14.93 | 14.93  | 0 00:40 | 0.601 |  |
| 0.601 | 0.000 |          |       |        |         |       |  |
| H1    |       | JUNCTION | 0.00  | 133.51 | 0 02:08 | 0     |  |
| 9.72  | 0.000 |          |       |        |         |       |  |
| HH    |       | JUNCTION | 13.01 | 13.01  | 0 00:35 | 0.462 |  |
| 0.462 | 0.000 |          |       |        |         |       |  |
| I     |       | JUNCTION | 34.58 | 34.58  | 0 00:35 | 1.17  |  |
| 1.17  | 0.000 |          |       |        |         |       |  |
| II    |       | JUNCTION | 81.77 | 81.77  | 0 00:45 | 3.59  |  |
| 3.59  | 0.000 |          |       |        |         |       |  |
| II1   |       | JUNCTION | 0.00  | 81.77  | 0 00:45 | 0     |  |
| 3.59  | 0.000 |          |       |        |         |       |  |
| BB3   |       | JUNCTION | 0.00  | 346.26 | 0 00:40 | 0     |  |
| 13.4  | 0.000 |          |       |        |         |       |  |
| J     |       | JUNCTION | 22.78 | 56.31  | 0 00:35 | 1.05  |  |
| 2.22  | 0.000 |          |       |        |         |       |  |
| JJ    |       | JUNCTION | 9.74  | 9.74   | 0 00:35 | 0.317 |  |
| 0.317 | 0.000 |          |       |        |         |       |  |
| K     |       | JUNCTION | 92.05 | 92.05  | 0 00:40 | 3.43  |  |
| 3.43  | 0.000 |          |       |        |         |       |  |
| KK    |       | JUNCTION | 7.51  | 7.51   | 0 00:35 | 0.297 |  |

|       |       |          |        |        |         |       |
|-------|-------|----------|--------|--------|---------|-------|
| 0.297 | 0.000 |          |        |        |         |       |
| L     |       | JUNCTION | 15.71  | 107.58 | 0 00:40 | 0.601 |
| 4.03  | 0.000 |          |        |        |         |       |
| LL    |       | JUNCTION | 6.88   | 6.88   | 0 00:35 | 0.22  |
| 0.22  | 0.000 |          |        |        |         |       |
| LL1   |       | JUNCTION | 0.00   | 24.12  | 0 00:35 | 0     |
| 0.834 | 0.000 |          |        |        |         |       |
| M     |       | JUNCTION | 11.48  | 11.48  | 0 00:40 | 0.509 |
| 0.509 | 0.000 |          |        |        |         |       |
| N     |       | JUNCTION | 56.97  | 68.16  | 0 00:35 | 1.8   |
| 2.31  | 0.000 |          |        |        |         |       |
| O     |       | JUNCTION | 22.69  | 22.69  | 0 00:40 | 0.91  |
| 0.91  | 0.000 |          |        |        |         |       |
| P     |       | JUNCTION | 38.52  | 38.52  | 0 00:40 | 1.61  |
| 1.61  | 0.000 |          |        |        |         |       |
| Q     |       | JUNCTION | 64.68  | 64.68  | 0 00:40 | 2.66  |
| 2.66  | 0.000 |          |        |        |         |       |
| R     |       | JUNCTION | 44.21  | 108.65 | 0 00:40 | 2.03  |
| 4.69  | 0.000 |          |        |        |         |       |
| S     |       | JUNCTION | 25.99  | 25.99  | 0 00:35 | 0.894 |
| 0.894 | 0.000 |          |        |        |         |       |
| SP1   |       | JUNCTION | 0.00   | 207.17 | 0 01:51 | 0     |
| 16    | 0.000 |          |        |        |         |       |
| SP2   |       | JUNCTION | 0.00   | 281.79 | 0 00:40 | 0     |
| 19.2  | 0.000 |          |        |        |         |       |
| SP3   |       | JUNCTION | 0.00   | 320.31 | 0 00:40 | 0     |
| 20.8  | 0.000 |          |        |        |         |       |
| T     |       | JUNCTION | 4.04   | 4.04   | 0 00:40 | 0.192 |
| 0.192 | 0.000 |          |        |        |         |       |
| T1    |       | JUNCTION | 0.00   | 137.90 | 0 00:40 | 0     |
| 5.77  | 0.000 |          |        |        |         |       |
| U     |       | JUNCTION | 4.15   | 4.15   | 0 00:40 | 0.201 |
| 0.201 | 0.000 |          |        |        |         |       |
| T2    |       | JUNCTION | 0.00   | 145.46 | 0 00:40 | 0     |
| 6.11  | 0.000 |          |        |        |         |       |
| V     |       | JUNCTION | 29.63  | 29.63  | 0 00:45 | 1.42  |
| 1.42  | 0.000 |          |        |        |         |       |
| X     |       | JUNCTION | 138.66 | 167.76 | 0 00:50 | 7.03  |
| 8.45  | 0.000 |          |        |        |         |       |
| W     |       | JUNCTION | 3.45   | 3.45   | 0 00:35 | 0.136 |
| 0.136 | 0.000 |          |        |        |         |       |
| H     |       | JUNCTION | 18.59  | 18.59  | 0 00:40 | 0.758 |
| 0.758 | 0.000 |          |        |        |         |       |
| OF2   |       | OUTFALL  | 0.00   | 145.46 | 0 00:40 | 0     |
| 6.11  | 0.000 |          |        |        |         |       |
| OF1   |       | OUTFALL  | 0.00   | 320.31 | 0 00:40 | 0     |
| 20.8  | 0.000 |          |        |        |         |       |
| OF3   |       | OUTFALL  | 0.00   | 167.76 | 0 00:50 | 0     |
| 8.45  | 0.000 |          |        |        |         |       |
| OF5   |       | OUTFALL  | 0.00   | 24.12  | 0 00:35 | 0     |

|          |       |         |      |        |   |       |   |
|----------|-------|---------|------|--------|---|-------|---|
| 0.834    | 0.000 |         |      |        |   |       |   |
| OF4      |       | OUTFALL | 0.00 | 346.26 | 0 | 00:40 | 0 |
| 13.4     | 0.000 |         |      |        |   |       |   |
| IRR_POND |       | STORAGE | 0.00 | 298.49 | 0 | 00:40 | 0 |
| 13.2     | 0.052 |         |      |        |   |       |   |

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#### Node Flooding Summary

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No nodes were flooded.

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#### Storage Volume Summary

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| of Max     |              | Maximum | Average  | Avg  | Evap | Exfil | Maximum  | Max  | Time |
|------------|--------------|---------|----------|------|------|-------|----------|------|------|
| Occurrence | Storage Unit | Outflow | Volume   | Pcnt | Pcnt | Pcnt  | Volume   | Pcnt |      |
| hr:min     | CFS          |         | 1000 ft3 | Full | Loss | Loss  | 1000 ft3 | Full | days |
| IRR_POND   |              |         | 718.772  | 33   | 0    | 0     | 1098.529 | 50   | 0    |
| 02:12      | 126.25       |         |          |      |      |       |          |      |      |

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#### Outfall Loading Summary

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| Outfall Node | Flow<br>Freq<br>Pcnt | Avg<br>Flow<br>CFS | Max<br>Flow<br>CFS | Total<br>Volume<br>10^6 gal |
|--------------|----------------------|--------------------|--------------------|-----------------------------|
| OF2          | 75.42                | 50.15              | 145.46             | 6.111                       |
| OF1          | 98.06                | 131.34             | 320.31             | 20.806                      |
| OF3          | 83.19                | 62.87              | 167.76             | 8.451                       |
| OF5          | 64.44                | 8.01               | 24.12              | 0.834                       |
| OF4          | 74.72                | 110.64             | 346.26             | 13.357                      |
| System       | 79.17                | 363.02             | 989.13             | 49.559                      |

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# Link Flow Summary

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| Link  | Type  | Maximum<br> Flow <br>CFS | Time of Max<br>Occurrence<br>days hr:min | Maximum<br> Veloc <br>ft/sec | Max/<br>Full<br>Flow | Max/<br>Full<br>Depth |
|-------|-------|--------------------------|--|------------------------------|----------------------|-----------------------|
| A100  | DUMMY | 20.84                    | 0 00:35                                  |                              |                      |                       |
| AA100 | DUMMY | 38.76                    | 0 00:35                                  |                              |                      |                       |
| B100  | DUMMY | 103.48                   | 0 00:40                                  |                              |                      |                       |
| BB100 | DUMMY | 40.62                    | 0 00:35                                  |                              |                      |                       |
| BB101 | DUMMY | 242.15                   | 0 00:35                                  |                              |                      |                       |
| BB102 | DUMMY | 257.03                   | 0 00:35                                  |                              |                      |                       |
| C100  | DUMMY | 33.36                    | 0 00:40                                  |                              |                      |                       |
| CC100 | DUMMY | 6.53                     | 0 00:35                                  |                              |                      |                       |
| D100  | DUMMY | 31.56                    | 0 00:40                                  |                              |                      |                       |
| DD100 | DUMMY | 58.42                    | 0 00:40                                  |                              |                      |                       |
| E100  | DUMMY | 223.69                   | 0 00:45                                  |                              |                      |                       |
| EE100 | DUMMY | 81.16                    | 0 00:35                                  |                              |                      |                       |
| EE101 | DUMMY | 162.77                   | 0 00:35                                  |                              |                      |                       |
| F100  | DUMMY | 24.27                    | 0 00:35                                  |                              |                      |                       |
| G100  | DUMMY | 79.17                    | 0 00:35                                  |                              |                      |                       |
| GG100 | DUMMY | 14.93                    | 0 00:40                                  |                              |                      |                       |
| H101  | DUMMY | 133.51                   | 0 02:08                                  |                              |                      |                       |
| HH100 | DUMMY | 13.01                    | 0 00:35                                  |                              |                      |                       |
| I100  | DUMMY | 34.58                    | 0 00:35                                  |                              |                      |                       |
| II100 | DUMMY | 81.77                    | 0 00:45                                  |                              |                      |                       |
| II101 | DUMMY | 81.77                    | 0 00:45                                  |                              |                      |                       |
| J100  | DUMMY | 56.31                    | 0 00:35                                  |                              |                      |                       |
| JJ100 | DUMMY | 9.74                     | 0 00:35                                  |                              |                      |                       |
| K100  | DUMMY | 92.05                    | 0 00:40                                  |                              |                      |                       |
| KK100 | DUMMY | 7.51                     | 0 00:35                                  |                              |                      |                       |
| L100  | DUMMY | 107.58                   | 0 00:40                                  |                              |                      |                       |
| LL100 | DUMMY | 6.88                     | 0 00:35                                  |                              |                      |                       |
| M100  | DUMMY | 11.48                    | 0 00:40                                  |                              |                      |                       |
| N100  | DUMMY | 68.16                    | 0 00:35                                  |                              |                      |                       |
| O100  | DUMMY | 22.69                    | 0 00:40                                  |                              |                      |                       |
| BB103 | DUMMY | 346.26                   | 0 00:40                                  |                              |                      |                       |
| OF5   | DUMMY | 24.12                    | 0 00:35                                  |                              |                      |                       |
| P100  | DUMMY | 38.52                    | 0 00:40                                  |                              |                      |                       |
| Q100  | DUMMY | 64.68                    | 0 00:40                                  |                              |                      |                       |
| R100  | DUMMY | 108.65                   | 0 00:40                                  |                              |                      |                       |
| S100  | DUMMY | 25.99                    | 0 00:35                                  |                              |                      |                       |
| SP101 | DUMMY | 207.17                   | 0 01:51                                  |                              |                      |                       |
| SP102 | DUMMY | 281.79                   | 0 00:40                                  |                              |                      |                       |
| SP103 | DUMMY | 320.31                   | 0 00:40                                  |                              |                      |                       |

|            |       |        |   |       |
|------------|-------|--------|---|-------|
| T100       | DUMMY | 4.04   | 0 | 00:40 |
| T101       | DUMMY | 137.90 | 0 | 00:40 |
| U100       | DUMMY | 4.15   | 0 | 00:40 |
| U101       | DUMMY | 145.46 | 0 | 00:40 |
| V100       | DUMMY | 29.63  | 0 | 00:45 |
| W100       | DUMMY | 3.45   | 0 | 00:35 |
| X100       | DUMMY | 167.76 | 0 | 00:50 |
| H100       | DUMMY | 18.59  | 0 | 00:40 |
| IRR_OUTLET | DUMMY | 126.25 | 0 | 02:12 |

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# Conduit Surcharge Summary

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No conduits were surcharged.

Analysis begun on: Mon Jul 18 10:52:15 2022  
 Analysis ended on: Mon Jul 18 10:52:15 2022  
 Total elapsed time: < 1 sec

EPA STORM WATER MANAGEMENT MODEL - VERSION 5.1 (Build 5.1.012)

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NOTE: The summary statistics displayed in this report are  
based on results found at every computational time step,  
not just on results from each reporting time step.  
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Analysis Options  
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Flow Units ..... CFS

Process Models:

Rainfall/Runoff ..... NO  
RDII ..... NO  
Snowmelt ..... NO  
Groundwater ..... NO  
Flow Routing ..... YES  
Ponding Allowed ..... NO  
Water Quality ..... NO

Flow Routing Method ..... KINWAVE

Starting Date ..... 01/01/2022 00:00:00

Ending Date ..... 01/01/2022 06:00:00

Antecedent Dry Days ..... 0.0

Report Time Step ..... 00:05:00

Routing Time Step ..... 30.00 sec

| *****                      | Volume    | Volume              |
|----------------------------|-----------|---------------------|
| Flow Routing Continuity    | acre-feet | 10 <sup>6</sup> gal |
| *****                      | -----     | -----               |
| Dry Weather Inflow .....   | 0.000     | 0.000               |
| Wet Weather Inflow .....   | 0.000     | 0.000               |
| Groundwater Inflow .....   | 0.000     | 0.000               |
| RDII Inflow .....          | 0.000     | 0.000               |
| External Inflow .....      | 308.214   | 100.436             |
| External Outflow .....     | 294.043   | 95.818              |
| Flooding Loss .....        | 0.000     | 0.000               |
| Evaporation Loss .....     | 0.000     | 0.000               |
| Exfiltration Loss .....    | 0.000     | 0.000               |
| Initial Stored Volume .... | 0.000     | 0.000               |
| Final Stored Volume .....  | 14.142    | 4.608               |
| Continuity Error (%) ..... | 0.009     |                     |

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Highest Flow Instability Indexes

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All links are stable.

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#### Routing Time Step Summary

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Minimum Time Step : 30.00 sec  
Average Time Step : 30.00 sec  
Maximum Time Step : 30.00 sec  
Percent in Steady State : 0.00  
Average Iterations per Step : 1.00  
Percent Not Converging : 0.00

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#### Node Depth Summary

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| Node | Type     | Average<br>Depth<br>Feet | Maximum<br>Depth<br>Feet | Maximum<br>HGL<br>Feet | Time of Max<br>Occurrence<br>days hr:min | Reported<br>Max Depth<br>Feet |
|------|----------|--------------------------|--------------------------|------------------------|--|-------------------------------|
| A    | JUNCTION | 0.00                     | 0.00                     | 7625.00                | 0 00:00                                  | 0.00                          |
| AA   | JUNCTION | 0.00                     | 0.00                     | 7525.00                | 0 00:00                                  | 0.00                          |
| B    | JUNCTION | 0.00                     | 0.00                     | 7570.00                | 0 00:00                                  | 0.00                          |
| BB   | JUNCTION | 0.00                     | 0.00                     | 7410.00                | 0 00:00                                  | 0.00                          |
| BB1  | JUNCTION | 0.00                     | 0.00                     | 7385.00                | 0 00:00                                  | 0.00                          |
| BB2  | JUNCTION | 0.00                     | 0.00                     | 7365.00                | 0 00:00                                  | 0.00                          |
| C    | JUNCTION | 0.00                     | 0.00                     | 7635.00                | 0 00:00                                  | 0.00                          |
| CC   | JUNCTION | 0.00                     | 0.00                     | 7495.00                | 0 00:00                                  | 0.00                          |
| D    | JUNCTION | 0.00                     | 0.00                     | 7575.00                | 0 00:00                                  | 0.00                          |
| DD   | JUNCTION | 0.00                     | 0.00                     | 7500.00                | 0 00:00                                  | 0.00                          |
| E    | JUNCTION | 0.00                     | 0.00                     | 7572.00                | 0 00:00                                  | 0.00                          |
| EE   | JUNCTION | 0.00                     | 0.00                     | 7525.00                | 0 00:00                                  | 0.00                          |
| F    | JUNCTION | 0.00                     | 0.00                     | 7633.00                | 0 00:00                                  | 0.00                          |
| FF   | JUNCTION | 0.00                     | 0.00                     | 7430.00                | 0 00:00                                  | 0.00                          |
| G    | JUNCTION | 0.00                     | 0.00                     | 7565.00                | 0 00:00                                  | 0.00                          |
| GG   | JUNCTION | 0.00                     | 0.00                     | 7420.00                | 0 00:00                                  | 0.00                          |
| H1   | JUNCTION | 0.00                     | 0.00                     | 7525.00                | 0 00:00                                  | 0.00                          |
| HH   | JUNCTION | 0.00                     | 0.00                     | 7410.00                | 0 00:00                                  | 0.00                          |
| I    | JUNCTION | 0.00                     | 0.00                     | 7595.00                | 0 00:00                                  | 0.00                          |
| II   | JUNCTION | 0.00                     | 0.00                     | 7495.00                | 0 00:00                                  | 0.00                          |
| II1  | JUNCTION | 0.00                     | 0.00                     | 7375.00                | 0 00:00                                  | 0.00                          |
| BB3  | JUNCTION | 0.00                     | 0.00                     | 7330.00                | 0 00:00                                  | 0.00                          |
| J    | JUNCTION | 0.00                     | 0.00                     | 7560.00                | 0 00:00                                  | 0.00                          |
| JJ   | JUNCTION | 0.00                     | 0.00                     | 7575.00                | 0 00:00                                  | 0.00                          |
| K    | JUNCTION | 0.00                     | 0.00                     | 7585.00                | 0 00:00                                  | 0.00                          |
| KK   | JUNCTION | 0.00                     | 0.00                     | 7590.00                | 0 00:00                                  | 0.00                          |

|          |          |      |      |         |   |       |      |
|----------|----------|------|------|---------|---|-------|------|
| L        | JUNCTION | 0.00 | 0.00 | 7548.00 | 0 | 00:00 | 0.00 |
| LL       | JUNCTION | 0.00 | 0.00 | 7580.00 | 0 | 00:00 | 0.00 |
| LL1      | JUNCTION | 0.00 | 0.00 | 7525.00 | 0 | 00:00 | 0.00 |
| M        | JUNCTION | 0.00 | 0.00 | 7590.00 | 0 | 00:00 | 0.00 |
| N        | JUNCTION | 0.00 | 0.00 | 7535.00 | 0 | 00:00 | 0.00 |
| O        | JUNCTION | 0.00 | 0.00 | 7525.00 | 0 | 00:00 | 0.00 |
| P        | JUNCTION | 0.00 | 0.00 | 7480.00 | 0 | 00:00 | 0.00 |
| Q        | JUNCTION | 0.00 | 0.00 | 7585.00 | 0 | 00:00 | 0.00 |
| R        | JUNCTION | 0.00 | 0.00 | 7596.00 | 0 | 00:00 | 0.00 |
| S        | JUNCTION | 0.00 | 0.00 | 7598.00 | 0 | 00:00 | 0.00 |
| SP1      | JUNCTION | 0.00 | 0.00 | 7495.00 | 0 | 00:00 | 0.00 |
| SP2      | JUNCTION | 0.00 | 0.00 | 7490.00 | 0 | 00:00 | 0.00 |
| SP3      | JUNCTION | 0.00 | 0.00 | 7435.00 | 0 | 00:00 | 0.00 |
| T        | JUNCTION | 0.00 | 0.00 | 7583.00 | 0 | 00:00 | 0.00 |
| T1       | JUNCTION | 0.00 | 0.00 | 7565.00 | 0 | 00:00 | 0.00 |
| U        | JUNCTION | 0.00 | 0.00 | 7567.00 | 0 | 00:00 | 0.00 |
| T2       | JUNCTION | 0.00 | 0.00 | 7555.00 | 0 | 00:00 | 0.00 |
| V        | JUNCTION | 0.00 | 0.00 | 7577.00 | 0 | 00:00 | 0.00 |
| X        | JUNCTION | 0.00 | 0.00 | 7500.00 | 0 | 00:00 | 0.00 |
| W        | JUNCTION | 0.00 | 0.00 | 7546.00 | 0 | 00:00 | 0.00 |
| H        | JUNCTION | 0.00 | 0.00 | 7560.00 | 0 | 00:00 | 0.00 |
| OF2      | OUTFALL  | 0.00 | 0.00 | 7550.00 | 0 | 00:00 | 0.00 |
| OF1      | OUTFALL  | 0.00 | 0.00 | 7430.00 | 0 | 00:00 | 0.00 |
| OF3      | OUTFALL  | 0.00 | 0.00 | 7435.00 | 0 | 00:00 | 0.00 |
| OF5      | OUTFALL  | 0.00 | 0.00 | 7520.00 | 0 | 00:00 | 0.00 |
| OF4      | OUTFALL  | 0.00 | 0.00 | 7325.00 | 0 | 00:00 | 0.00 |
| IRR_POND | STORAGE  | 2.90 | 4.82 | 7534.82 | 0 | 01:51 | 4.82 |

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Node Inflow Summary  
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| Total  |         | Flow     |       | Maximum | Maximum | Lateral     |          |
|--------|---------|----------|-------|---------|---------|-------------|----------|
| Inflow | Balance |          |       | Lateral | Total   | Time of Max | Inflow   |
| Volume | Error   |          |       | Inflow  | Inflow  | Occurrence  | Volume   |
| Node   | Percent | Type     | CFS   | CFS     | days    | hr:min      | 10^6 gal |
| gal    |         |          |       |         |         |             | 10^6     |
| A      |         | JUNCTION | 43.83 | 43.83   | 0       | 00:40       | 1.3      |
| 1.3    | 0.000   |          |       |         |         |             |          |
| AA     |         | JUNCTION | 80.22 | 80.22   | 0       | 00:40       | 2.31     |



|       |       |          |        |        |         |       |
|-------|-------|----------|--------|--------|---------|-------|
| 2.31  | 0.000 |          |        |        |         |       |
| B     |       | JUNCTION | 107.33 | 221.28 | 0 00:45 | 4.12  |
| 7.82  | 0.000 |          |        |        |         |       |
| BB    |       | JUNCTION | 84.15  | 84.15  | 0 00:40 | 2.56  |
| 2.56  | 0.000 |          |        |        |         |       |
| BB1   |       | JUNCTION | 0.00   | 503.29 | 0 00:40 | 0     |
| 16.2  | 0.000 |          |        |        |         |       |
| BB2   |       | JUNCTION | 0.00   | 534.86 | 0 00:40 | 0     |
| 17.3  | 0.000 |          |        |        |         |       |
| C     |       | JUNCTION | 71.27  | 71.27  | 0 00:45 | 2.4   |
| 2.4   | 0.000 |          |        |        |         |       |
| CC    |       | JUNCTION | 13.57  | 13.57  | 0 00:40 | 0.431 |
| 0.431 | 0.000 |          |        |        |         |       |
| D     |       | JUNCTION | 67.84  | 67.84  | 0 00:50 | 2.67  |
| 2.67  | 0.000 |          |        |        |         |       |
| DD    |       | JUNCTION | 123.69 | 123.69 | 0 00:50 | 4.85  |
| 4.85  | 0.000 |          |        |        |         |       |
| E     |       | JUNCTION | 199.80 | 483.10 | 0 00:50 | 8.81  |
| 19.3  | 0.000 |          |        |        |         |       |
| EE    |       | JUNCTION | 167.45 | 167.45 | 0 00:40 | 4.8   |
| 4.8   | 0.000 |          |        |        |         |       |
| F     |       | JUNCTION | 51.63  | 51.63  | 0 00:45 | 1.73  |
| 1.73  | 0.000 |          |        |        |         |       |
| FF    |       | JUNCTION | 41.02  | 340.42 | 0 00:45 | 1.21  |
| 11.3  | 0.000 |          |        |        |         |       |
| G     |       | JUNCTION | 115.21 | 166.51 | 0 00:40 | 3.58  |
| 5.32  | 0.000 |          |        |        |         |       |
| GG    |       | JUNCTION | 31.99  | 31.99  | 0 00:45 | 1.12  |
| 1.12  | 0.000 |          |        |        |         |       |
| H1    |       | JUNCTION | 0.00   | 323.27 | 0 01:49 | 0     |
| 21.4  | 0.000 |          |        |        |         |       |
| HH    |       | JUNCTION | 27.42  | 27.42  | 0 00:40 | 0.864 |
| 0.864 | 0.000 |          |        |        |         |       |
| I     |       | JUNCTION | 72.63  | 72.63  | 0 00:40 | 2.19  |
| 2.19  | 0.000 |          |        |        |         |       |
| II    |       | JUNCTION | 175.60 | 175.60 | 0 00:50 | 6.72  |
| 6.72  | 0.000 |          |        |        |         |       |
| II1   |       | JUNCTION | 0.00   | 175.60 | 0 00:50 | 0     |
| 6.72  | 0.000 |          |        |        |         |       |
| BB3   |       | JUNCTION | 0.00   | 733.92 | 0 00:45 | 0     |
| 24.9  | 0.000 |          |        |        |         |       |
| J     |       | JUNCTION | 48.99  | 120.46 | 0 00:45 | 1.96  |
| 4.15  | 0.000 |          |        |        |         |       |
| JJ    |       | JUNCTION | 20.50  | 20.50  | 0 00:40 | 0.592 |
| 0.592 | 0.000 |          |        |        |         |       |
| K     |       | JUNCTION | 195.43 | 195.43 | 0 00:45 | 6.42  |
| 6.42  | 0.000 |          |        |        |         |       |
| KK    |       | JUNCTION | 15.99  | 15.99  | 0 00:45 | 0.556 |
| 0.556 | 0.000 |          |        |        |         |       |
| L     |       | JUNCTION | 33.30  | 228.73 | 0 00:45 | 1.12  |

|       |       |          |        |        |   |       |       |
|-------|-------|----------|--------|--------|---|-------|-------|
| 7.55  | 0.000 |          |        |        |   |       |       |
| LL    |       | JUNCTION | 14.48  | 14.48  | 0 | 00:40 | 0.411 |
| 0.411 | 0.000 |          |        |        |   |       |       |
| LL1   |       | JUNCTION | 0.00   | 50.88  | 0 | 00:40 | 0     |
| 1.56  | 0.000 |          |        |        |   |       |       |
| M     |       | JUNCTION | 24.61  | 24.61  | 0 | 00:45 | 0.953 |
| 0.953 | 0.000 |          |        |        |   |       |       |
| N     |       | JUNCTION | 119.24 | 143.11 | 0 | 00:40 | 3.37  |
| 4.32  | 0.000 |          |        |        |   |       |       |
| O     |       | JUNCTION | 48.54  | 48.54  | 0 | 00:45 | 1.7   |
| 1.7   | 0.000 |          |        |        |   |       |       |
| P     |       | JUNCTION | 82.17  | 82.17  | 0 | 00:45 | 3.01  |
| 3.01  | 0.000 |          |        |        |   |       |       |
| Q     |       | JUNCTION | 137.80 | 137.80 | 0 | 00:45 | 4.98  |
| 4.98  | 0.000 |          |        |        |   |       |       |
| R     |       | JUNCTION | 95.25  | 232.13 | 0 | 00:45 | 3.79  |
| 8.77  | 0.000 |          |        |        |   |       |       |
| S     |       | JUNCTION | 54.65  | 54.65  | 0 | 00:40 | 1.67  |
| 1.67  | 0.000 |          |        |        |   |       |       |
| SP1   |       | JUNCTION | 0.00   | 515.49 | 0 | 01:15 | 0     |
| 33.1  | 0.000 |          |        |        |   |       |       |
| SP2   |       | JUNCTION | 0.00   | 653.32 | 0 | 01:09 | 0     |
| 39.1  | 0.000 |          |        |        |   |       |       |
| SP3   |       | JUNCTION | 0.00   | 725.59 | 0 | 01:06 | 0     |
| 42.1  | 0.000 |          |        |        |   |       |       |
| T     |       | JUNCTION | 8.68   | 8.68   | 0 | 00:45 | 0.359 |
| 0.359 | 0.000 |          |        |        |   |       |       |
| T1    |       | JUNCTION | 0.00   | 294.73 | 0 | 00:45 | 0     |
| 10.8  | 0.000 |          |        |        |   |       |       |
| U     |       | JUNCTION | 8.95   | 8.95   | 0 | 00:50 | 0.376 |
| 0.376 | 0.000 |          |        |        |   |       |       |
| T2    |       | JUNCTION | 0.00   | 311.00 | 0 | 00:45 | 0     |
| 11.4  | 0.000 |          |        |        |   |       |       |
| V     |       | JUNCTION | 63.92  | 63.92  | 0 | 00:50 | 2.66  |
| 2.66  | 0.000 |          |        |        |   |       |       |
| X     |       | JUNCTION | 298.70 | 361.56 | 0 | 00:55 | 13.2  |
| 15.8  | 0.000 |          |        |        |   |       |       |
| W     |       | JUNCTION | 7.33   | 7.33   | 0 | 00:45 | 0.255 |
| 0.255 | 0.000 |          |        |        |   |       |       |
| H     |       | JUNCTION | 39.78  | 39.78  | 0 | 00:45 | 1.42  |
| 1.42  | 0.000 |          |        |        |   |       |       |
| OF2   |       | OUTFALL  | 0.00   | 311.00 | 0 | 00:45 | 0     |
| 11.4  | 0.000 |          |        |        |   |       |       |
| OF1   |       | OUTFALL  | 0.00   | 725.59 | 0 | 01:06 | 0     |
| 42.1  | 0.000 |          |        |        |   |       |       |
| OF3   |       | OUTFALL  | 0.00   | 361.56 | 0 | 00:55 | 0     |
| 15.8  | 0.000 |          |        |        |   |       |       |
| OF5   |       | OUTFALL  | 0.00   | 50.88  | 0 | 00:40 | 0     |
| 1.56  | 0.000 |          |        |        |   |       |       |
| OF4   |       | OUTFALL  | 0.00   | 733.92 | 0 | 00:45 | 0     |

|          |       |         |      |        |   |       |   |
|----------|-------|---------|------|--------|---|-------|---|
| 24.9     | 0.000 |         |      |        |   |       |   |
| IRR_POND |       | STORAGE | 0.00 | 644.35 | 0 | 00:50 | 0 |
| 24.6     | 0.038 |         |      |        |   |       |   |

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# Node Flooding Summary

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No nodes were flooded.

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# Storage Volume Summary

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| of Max       |         | Average  | Avg  | Evap | Exfil | Maximum  | Max  | Time |
|--------------|---------|----------|------|------|-------|----------|------|------|
| Maximum      | Maximum | Volume   | Pcnt | Pcnt | Pcnt  | Volume   | Pcnt |      |
| Occurrence   | Outflow | 1000 ft3 | Full | Loss | Loss  | 1000 ft3 | Full | days |
| Storage Unit | CFS     |          |      |      |       |          |      |      |
| hr:min       |         |          |      |      |       |          |      |      |
| IRR_POND     |         | 988.180  | 45   | 0    | 0     | 1697.949 | 78   | 0    |
| 01:51        | 306.06  |          |      |      |       |          |      |      |

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# Outfall Loading Summary

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| Outfall Node | Flow<br>Freq<br>Pcnt | Avg<br>Flow<br>CFS | Max<br>Flow<br>CFS | Total<br>Volume<br>10^6 gal |
|--------------|----------------------|--------------------|--------------------|-----------------------------|
| OF2          | 76.53                | 92.46              | 311.00             | 11.432                      |
| OF1          | 98.33                | 265.29             | 725.59             | 42.145                      |
| OF3          | 83.75                | 116.84             | 361.56             | 15.810                      |
| OF5          | 64.58                | 14.95              | 50.88              | 1.559                       |
| OF4          | 74.86                | 205.58             | 733.92             | 24.865                      |
| System       | 79.61                | 695.11             | 2117.11            | 95.811                      |

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# Link Flow Summary

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| Link  | Type  | Maximum<br> Flow <br>CFS | Time of Max<br>Occurrence<br>days hr:min | Maximum<br> Veloc <br>ft/sec | Max/<br>Full<br>Flow | Max/<br>Full<br>Depth |
|-------|-------|--------------------------|--|------------------------------|----------------------|-----------------------|
| A100  | DUMMY | 43.83                    | 0 00:40                                  |                              |                      |                       |
| AA100 | DUMMY | 80.22                    | 0 00:40                                  |                              |                      |                       |
| B100  | DUMMY | 221.28                   | 0 00:45                                  |                              |                      |                       |
| BB100 | DUMMY | 84.15                    | 0 00:40                                  |                              |                      |                       |
| BB101 | DUMMY | 503.29                   | 0 00:40                                  |                              |                      |                       |
| BB102 | DUMMY | 534.86                   | 0 00:40                                  |                              |                      |                       |
| C100  | DUMMY | 71.27                    | 0 00:45                                  |                              |                      |                       |
| CC100 | DUMMY | 13.57                    | 0 00:40                                  |                              |                      |                       |
| D100  | DUMMY | 67.84                    | 0 00:50                                  |                              |                      |                       |
| DD100 | DUMMY | 123.69                   | 0 00:50                                  |                              |                      |                       |
| E100  | DUMMY | 483.10                   | 0 00:50                                  |                              |                      |                       |
| EE100 | DUMMY | 167.45                   | 0 00:40                                  |                              |                      |                       |
| EE101 | DUMMY | 340.42                   | 0 00:45                                  |                              |                      |                       |
| F100  | DUMMY | 51.63                    | 0 00:45                                  |                              |                      |                       |
| G100  | DUMMY | 166.51                   | 0 00:40                                  |                              |                      |                       |
| GG100 | DUMMY | 31.99                    | 0 00:45                                  |                              |                      |                       |
| H101  | DUMMY | 323.27                   | 0 01:49                                  |                              |                      |                       |
| HH100 | DUMMY | 27.42                    | 0 00:40                                  |                              |                      |                       |
| I100  | DUMMY | 72.63                    | 0 00:40                                  |                              |                      |                       |
| II100 | DUMMY | 175.60                   | 0 00:50                                  |                              |                      |                       |
| II101 | DUMMY | 175.60                   | 0 00:50                                  |                              |                      |                       |
| J100  | DUMMY | 120.46                   | 0 00:45                                  |                              |                      |                       |
| JJ100 | DUMMY | 20.50                    | 0 00:40                                  |                              |                      |                       |
| K100  | DUMMY | 195.43                   | 0 00:45                                  |                              |                      |                       |
| KK100 | DUMMY | 15.99                    | 0 00:45                                  |                              |                      |                       |
| L100  | DUMMY | 228.73                   | 0 00:45                                  |                              |                      |                       |
| LL100 | DUMMY | 14.48                    | 0 00:40                                  |                              |                      |                       |
| M100  | DUMMY | 24.61                    | 0 00:45                                  |                              |                      |                       |
| N100  | DUMMY | 143.11                   | 0 00:40                                  |                              |                      |                       |
| O100  | DUMMY | 48.54                    | 0 00:45                                  |                              |                      |                       |
| BB103 | DUMMY | 733.92                   | 0 00:45                                  |                              |                      |                       |
| OF5   | DUMMY | 50.88                    | 0 00:40                                  |                              |                      |                       |
| P100  | DUMMY | 82.17                    | 0 00:45                                  |                              |                      |                       |
| Q100  | DUMMY | 137.80                   | 0 00:45                                  |                              |                      |                       |
| R100  | DUMMY | 232.13                   | 0 00:45                                  |                              |                      |                       |
| S100  | DUMMY | 54.65                    | 0 00:40                                  |                              |                      |                       |
| SP101 | DUMMY | 515.49                   | 0 01:15                                  |                              |                      |                       |
| SP102 | DUMMY | 653.32                   | 0 01:09                                  |                              |                      |                       |
| SP103 | DUMMY | 725.59                   | 0 01:06                                  |                              |                      |                       |
| T100  | DUMMY | 8.68                     | 0 00:45                                  |                              |                      |                       |
| T101  | DUMMY | 294.73                   | 0 00:45                                  |                              |                      |                       |

|            |       |        |   |       |
|------------|-------|--------|---|-------|
| U100       | DUMMY | 8.95   | 0 | 00:50 |
| U101       | DUMMY | 311.00 | 0 | 00:45 |
| V100       | DUMMY | 63.92  | 0 | 00:50 |
| W100       | DUMMY | 7.33   | 0 | 00:45 |
| X100       | DUMMY | 361.56 | 0 | 00:55 |
| H100       | DUMMY | 39.78  | 0 | 00:45 |
| IRR_OUTLET | DUMMY | 306.06 | 0 | 01:51 |

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# Conduit Surcharge Summary

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No conduits were surcharged.

Analysis begun on: Mon Jul 18 10:53:23 2022

Analysis ended on: Mon Jul 18 10:53:23 2022

Total elapsed time: < 1 sec

EPA STORM WATER MANAGEMENT MODEL - VERSION 5.1 (Build 5.1.012)

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NOTE: The summary statistics displayed in this report are  
based on results found at every computational time step,  
not just on results from each reporting time step.  
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Analysis Options

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Flow Units ..... CFS

Process Models:

Rainfall/Runoff ..... NO

RDII ..... NO

Snowmelt ..... NO

Groundwater ..... NO

Flow Routing ..... YES

Ponding Allowed ..... NO

Water Quality ..... NO

Flow Routing Method ..... KINWAVE

Starting Date ..... 01/01/2005 00:00:00

Ending Date ..... 01/01/2005 06:00:00

Antecedent Dry Days ..... 0.0

Report Time Step ..... 00:05:00

Routing Time Step ..... 30.00 sec

| *****                      | Volume    | Volume              |
|----------------------------|-----------|---------------------|
| Flow Routing Continuity    | acre-feet | 10 <sup>6</sup> gal |
| *****                      | -----     | -----               |
| Dry Weather Inflow .....   | 0.000     | 0.000               |
| Wet Weather Inflow .....   | 0.000     | 0.000               |
| Groundwater Inflow .....   | 0.000     | 0.000               |
| RDII Inflow .....          | 0.000     | 0.000               |
| External Inflow .....      | 167.014   | 54.424              |
| External Outflow .....     | 135.513   | 44.159              |
| Flooding Loss .....        | 0.000     | 0.000               |
| Evaporation Loss .....     | 0.000     | 0.000               |
| Exfiltration Loss .....    | 0.000     | 0.000               |
| Initial Stored Volume .... | 0.000     | 0.000               |
| Final Stored Volume .....  | 32.666    | 10.645              |
| Continuity Error (%) ..... | -0.697    |                     |

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Highest Flow Instability Indexes

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Link J1200 (3)  
 Link J1300 (3)  
 Link SP104 (3)  
 Link SP101 (2)  
 Link 07 (2)

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#### Routing Time Step Summary

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Minimum Time Step : 30.00 sec  
 Average Time Step : 30.00 sec  
 Maximum Time Step : 30.00 sec  
 Percent in Steady State : 0.00  
 Average Iterations per Step : 1.00  
 Percent Not Converging : 0.00

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#### Node Depth Summary

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| Node | Type     | Average<br>Depth<br>Feet | Maximum<br>Depth<br>Feet | Maximum<br>HGL<br>Feet | Time of Max<br>Occurrence<br>days hr:min | Reported<br>Max Depth<br>Feet |
|------|----------|--------------------------|--------------------------|------------------------|--|-------------------------------|
| A    | JUNCTION | 0.00                     | 0.00                     | 7625.00                | 0 00:00                                  | 0.00                          |
| AA   | JUNCTION | 0.00                     | 0.00                     | 7525.00                | 0 00:00                                  | 0.00                          |
| B1   | JUNCTION | 0.53                     | 1.73                     | 7576.73                | 0 00:35                                  | 1.73                          |
| B2   | JUNCTION | 0.55                     | 1.60                     | 7576.60                | 0 00:40                                  | 1.60                          |
| BB   | JUNCTION | 0.00                     | 0.00                     | 7410.00                | 0 00:00                                  | 0.00                          |
| BB1  | JUNCTION | 0.54                     | 1.41                     | 7386.41                | 0 00:49                                  | 1.41                          |
| BB2  | JUNCTION | 0.00                     | 0.00                     | 7365.00                | 0 00:00                                  | 0.00                          |
| BB3  | JUNCTION | 0.00                     | 0.00                     | 7330.00                | 0 00:00                                  | 0.00                          |
| C    | JUNCTION | 0.00                     | 0.00                     | 7635.00                | 0 00:00                                  | 0.00                          |
| CC   | JUNCTION | 0.00                     | 0.00                     | 7495.00                | 0 00:00                                  | 0.00                          |
| D    | JUNCTION | 0.00                     | 0.00                     | 7609.00                | 0 00:00                                  | 0.00                          |
| DD   | JUNCTION | 0.00                     | 0.00                     | 7495.00                | 0 00:00                                  | 0.00                          |
| E    | JUNCTION | 0.62                     | 1.37                     | 7573.37                | 0 00:50                                  | 1.37                          |
| EE1  | JUNCTION | 0.42                     | 1.02                     | 7476.02                | 0 00:53                                  | 1.02                          |
| EE2  | JUNCTION | 0.00                     | 0.00                     | 7550.00                | 0 00:00                                  | 0.00                          |
| EE3  | JUNCTION | 0.18                     | 0.74                     | 7575.74                | 0 00:30                                  | 0.73                          |
| F    | JUNCTION | 0.00                     | 0.00                     | 7633.00                | 0 00:00                                  | 0.00                          |
| FF   | JUNCTION | 0.54                     | 1.41                     | 7431.41                | 0 00:48                                  | 1.41                          |
| G    | JUNCTION | 0.44                     | 1.26                     | 7566.26                | 0 00:40                                  | 1.26                          |
| GG   | JUNCTION | 0.00                     | 0.00                     | 7420.00                | 0 00:00                                  | 0.00                          |
| H    | JUNCTION | 0.00                     | 0.00                     | 7530.00                | 0 00:00                                  | 0.00                          |
| HH   | JUNCTION | 0.00                     | 0.00                     | 7410.00                | 0 00:00                                  | 0.00                          |
| I    | JUNCTION | 0.00                     | 0.00                     | 7595.00                | 0 00:00                                  | 0.00                          |

|       |          |      |      |         |   |       |      |
|-------|----------|------|------|---------|---|-------|------|
| II1   | JUNCTION | 0.33 | 0.75 | 7495.75 | 0 | 00:50 | 0.75 |
| II2   | JUNCTION | 0.32 | 1.13 | 7451.13 | 0 | 00:35 | 1.13 |
| II3   | JUNCTION | 0.20 | 0.71 | 7515.71 | 0 | 00:35 | 0.71 |
| IRR_J | JUNCTION | 0.00 | 0.00 | 7528.00 | 0 | 00:00 | 0.00 |
| J10   | JUNCTION | 0.00 | 0.00 | 7520.00 | 0 | 00:00 | 0.00 |
| J11   | JUNCTION | 0.00 | 0.00 | 7565.00 | 0 | 00:00 | 0.00 |
| J12   | JUNCTION | 0.08 | 0.23 | 7545.23 | 0 | 01:04 | 0.22 |
| J13   | JUNCTION | 0.31 | 0.74 | 7520.74 | 0 | 01:00 | 0.74 |
| J14   | JUNCTION | 0.00 | 0.00 | 7375.00 | 0 | 00:00 | 0.00 |
| J15   | JUNCTION | 0.00 | 0.00 | 7552.00 | 0 | 00:00 | 0.00 |
| J2    | JUNCTION | 0.55 | 1.24 | 7436.24 | 0 | 01:46 | 1.24 |
| J3    | JUNCTION | 0.82 | 1.35 | 7496.35 | 0 | 01:51 | 1.35 |
| J4    | JUNCTION | 0.55 | 1.24 | 7466.24 | 0 | 01:42 | 1.24 |
| J5    | JUNCTION | 0.30 | 0.53 | 7525.53 | 0 | 01:29 | 0.53 |
| J6    | JUNCTION | 0.30 | 0.53 | 7570.53 | 0 | 01:27 | 0.53 |
| J7    | JUNCTION | 0.40 | 1.23 | 7546.23 | 0 | 00:37 | 1.22 |
| J8    | JUNCTION | 0.40 | 1.23 | 7526.23 | 0 | 00:38 | 1.23 |
| J9    | JUNCTION | 0.00 | 0.00 | 7550.00 | 0 | 00:00 | 0.00 |
| JJ    | JUNCTION | 0.00 | 0.00 | 7575.00 | 0 | 00:00 | 0.00 |
| K     | JUNCTION | 0.32 | 1.48 | 7586.48 | 0 | 00:30 | 1.46 |
| KK    | JUNCTION | 0.00 | 0.00 | 7590.00 | 0 | 00:00 | 0.00 |
| L     | JUNCTION | 0.00 | 0.00 | 7548.00 | 0 | 00:00 | 0.00 |
| LL    | JUNCTION | 0.00 | 0.00 | 7580.00 | 0 | 00:00 | 0.00 |
| M     | JUNCTION | 0.20 | 0.96 | 7590.96 | 0 | 00:30 | 0.95 |
| N     | JUNCTION | 0.35 | 1.63 | 7536.63 | 0 | 00:30 | 1.62 |
| O     | JUNCTION | 0.00 | 0.00 | 7559.00 | 0 | 00:00 | 0.00 |
| P     | JUNCTION | 0.00 | 0.00 | 7500.37 | 0 | 00:00 | 0.00 |
| Q     | JUNCTION | 0.00 | 0.00 | 7585.00 | 0 | 00:00 | 0.00 |
| R     | JUNCTION | 0.00 | 0.00 | 7576.00 | 0 | 00:00 | 0.00 |
| S     | JUNCTION | 0.00 | 0.00 | 7598.00 | 0 | 00:00 | 0.00 |
| SP1   | JUNCTION | 0.50 | 0.82 | 7510.82 | 0 | 00:39 | 0.82 |
| SP2   | JUNCTION | 0.83 | 1.39 | 7496.39 | 0 | 00:48 | 1.38 |
| SP3   | JUNCTION | 0.87 | 1.34 | 7491.34 | 0 | 02:06 | 1.34 |
| SP4   | JUNCTION | 0.54 | 0.88 | 7420.88 | 0 | 01:06 | 0.88 |
| T     | JUNCTION | 0.00 | 0.00 | 7583.00 | 0 | 00:00 | 0.00 |
| T1    | JUNCTION | 0.00 | 0.00 | 7565.00 | 0 | 00:00 | 0.00 |
| T2    | JUNCTION | 0.00 | 0.00 | 7555.00 | 0 | 00:00 | 0.00 |
| U     | JUNCTION | 0.00 | 0.00 | 7567.00 | 0 | 00:00 | 0.00 |
| V1    | JUNCTION | 0.00 | 0.00 | 7598.00 | 0 | 00:00 | 0.00 |
| V2    | JUNCTION | 0.19 | 0.61 | 7565.61 | 0 | 00:35 | 0.61 |
| W     | JUNCTION | 0.00 | 0.00 | 7546.00 | 0 | 00:00 | 0.00 |
| X1    | JUNCTION | 0.00 | 0.00 | 7485.00 | 0 | 00:00 | 0.00 |
| X2    | JUNCTION | 0.30 | 1.00 | 7506.00 | 0 | 00:35 | 0.99 |
| X3    | JUNCTION | 0.38 | 1.01 | 7501.01 | 0 | 00:40 | 1.01 |
| I2    | JUNCTION | 0.00 | 0.00 | 7577.00 | 0 | 00:00 | 0.00 |
| P12   | JUNCTION | 0.00 | 0.00 | 7550.00 | 0 | 00:00 | 0.00 |
| LL1   | JUNCTION | 0.00 | 0.00 | 0.00    | 0 | 00:00 | 0.00 |
| OF3   | OUTFALL  | 0.00 | 0.00 | 7431.00 | 0 | 00:00 | 0.00 |
| OF1   | OUTFALL  | 0.53 | 0.88 | 7415.88 | 0 | 01:07 | 0.88 |
| OF2   | OUTFALL  | 0.00 | 0.00 | 7550.00 | 0 | 00:00 | 0.00 |



|          |         |      |      |         |   |       |      |
|----------|---------|------|------|---------|---|-------|------|
| OF4      | OUTFALL | 0.00 | 0.00 | 7325.00 | 0 | 00:00 | 0.00 |
| OF5      | OUTFALL | 0.00 | 0.00 | 7520.00 | 0 | 00:00 | 0.00 |
| IRR_POND | STORAGE | 2.04 | 3.13 | 7533.13 | 0 | 02:26 | 3.13 |
| P1       | STORAGE | 2.52 | 3.53 | 7428.53 | 0 | 01:24 | 3.53 |
| P10      | STORAGE | 3.00 | 4.85 | 7529.85 | 0 | 01:31 | 4.85 |
| P11      | STORAGE | 3.04 | 5.09 | 7575.09 | 0 | 01:18 | 5.08 |
| P13      | STORAGE | 2.85 | 3.99 | 7528.99 | 0 | 01:00 | 3.99 |
| P14      | STORAGE | 2.97 | 4.54 | 7404.54 | 0 | 01:01 | 4.54 |
| P15      | STORAGE | 2.80 | 4.26 | 7559.26 | 0 | 01:11 | 4.26 |
| P2       | STORAGE | 5.57 | 7.19 | 7443.19 | 0 | 02:07 | 7.19 |
| P3       | STORAGE | 4.48 | 6.33 | 7516.33 | 0 | 01:51 | 6.33 |
| P4       | STORAGE | 4.93 | 7.13 | 7476.13 | 0 | 01:42 | 7.12 |
| P5       | STORAGE | 3.20 | 4.68 | 7534.68 | 0 | 00:56 | 4.68 |
| P6       | STORAGE | 3.85 | 5.74 | 7579.74 | 0 | 01:27 | 5.74 |
| P7       | STORAGE | 4.50 | 7.59 | 7557.59 | 0 | 00:37 | 7.54 |
| P8       | STORAGE | 4.01 | 6.15 | 7540.15 | 0 | 02:03 | 6.15 |
| P9       | STORAGE | 3.74 | 5.58 | 7575.58 | 0 | 01:28 | 5.58 |
| P16      | STORAGE | 3.37 | 4.66 | 7604.66 | 0 | 01:04 | 4.66 |
| P17      | STORAGE | 4.41 | 5.85 | 7566.85 | 0 | 01:15 | 5.85 |

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Node Inflow Summary

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| Total Flow    |               | Type     | Maximum Lateral | Maximum Total | Time of Max |             | Lateral Inflow | 10^6 gal | 10^6 |
|---------------|---------------|----------|-----------------|---------------|-------------|-------------|----------------|----------|------|
| Inflow Volume | Balance Error |          | Inflow CFS      | Inflow CFS    | Occurrence  | days hr:min | Volume         |          |      |
| Node gal      | Percent       |          |                 |               |             |             | 10^6 gal       |          |      |
| -----         |               |          |                 |               |             |             |                |          |      |
| -----         |               |          |                 |               |             |             |                |          |      |
| A             |               | JUNCTION | 20.84           | 20.84         | 0           | 00:35       | 0.696          |          |      |
| 0.696         | 0.000         |          |                 |               |             |             |                |          |      |
| AA            |               | JUNCTION | 39.23           | 39.23         | 0           | 00:35       | 1.26           |          |      |
| 1.26          | 0.000         |          |                 |               |             |             |                |          |      |
| B1            |               | JUNCTION | 66.93           | 87.77         | 0           | 00:35       | 2.29           |          |      |
| 2.99          | 0.000         |          |                 |               |             |             |                |          |      |
| B2            |               | JUNCTION | 17.99           | 53.23         | 0           | 00:40       | 0.762          |          |      |
| 2.1           | 0.000         |          |                 |               |             |             |                |          |      |
| BB            |               | JUNCTION | 40.62           | 40.62         | 0           | 00:35       | 1.38           |          |      |
| 1.38          | 0.000         |          |                 |               |             |             |                |          |      |
| BB1           |               | JUNCTION | 0.00            | 214.28        | 0           | 00:41       | 0              |          |      |

|       |        |          |       |        |   |       |       |
|-------|--------|----------|-------|--------|---|-------|-------|
| 8.75  | 0.000  |          |       |        |   |       |       |
| BB2   |        | JUNCTION | 0.00  | 229.61 | 0 | 00:40 | 0     |
| 9.36  | 0.000  |          |       |        |   |       |       |
| BB3   |        | JUNCTION | 0.00  | 307.27 | 0 | 00:48 | 0     |
| 13.3  | 0.000  |          |       |        |   |       |       |
| C     |        | JUNCTION | 35.31 | 35.31  | 0 | 00:35 | 1.34  |
| 1.34  | 0.000  |          |       |        |   |       |       |
| CC    |        | JUNCTION | 6.53  | 6.53   | 0 | 00:35 | 0.232 |
| 0.232 | 0.000  |          |       |        |   |       |       |
| D     |        | JUNCTION | 61.12 | 61.12  | 0 | 00:30 | 1.58  |
| 1.58  | 0.000  |          |       |        |   |       |       |
| DD    |        | JUNCTION | 57.78 | 57.78  | 0 | 00:40 | 2.59  |
| 2.59  | 0.000  |          |       |        |   |       |       |
| E     |        | JUNCTION | 74.68 | 74.68  | 0 | 00:50 | 4     |
| 4     | 0.000  |          |       |        |   |       |       |
| EE1   |        | JUNCTION | 53.25 | 60.58  | 0 | 00:53 | 1.89  |
| 2.62  | 0.000  |          |       |        |   |       |       |
| EE2   |        | JUNCTION | 35.71 | 35.71  | 0 | 00:30 | 0.647 |
| 0.647 | 0.000  |          |       |        |   |       |       |
| EE3   |        | JUNCTION | 10.38 | 10.38  | 0 | 00:30 | 0.26  |
| 0.26  | 0.000  |          |       |        |   |       |       |
| F     |        | JUNCTION | 24.27 | 24.27  | 0 | 00:35 | 0.927 |
| 0.927 | 0.000  |          |       |        |   |       |       |
| FF    |        | JUNCTION | 20.78 | 139.72 | 0 | 00:48 | 0.669 |
| 6.11  | 0.000  |          |       |        |   |       |       |
| G     |        | JUNCTION | 27.18 | 51.31  | 0 | 00:40 | 1.18  |
| 2.1   | 0.000  |          |       |        |   |       |       |
| GG    |        | JUNCTION | 15.49 | 15.49  | 0 | 00:35 | 0.607 |
| 0.607 | 0.000  |          |       |        |   |       |       |
| H     |        | JUNCTION | 17.86 | 17.86  | 0 | 00:40 | 0.818 |
| 0.818 | 0.000  |          |       |        |   |       |       |
| HH    |        | JUNCTION | 13.56 | 13.56  | 0 | 00:35 | 0.469 |
| 0.469 | 0.000  |          |       |        |   |       |       |
| I     |        | JUNCTION | 40.37 | 40.37  | 0 | 00:30 | 1.11  |
| 1.11  | 0.000  |          |       |        |   |       |       |
| II1   |        | JUNCTION | 34.94 | 34.94  | 0 | 00:50 | 1.88  |
| 1.88  | 0.000  |          |       |        |   |       |       |
| II2   |        | JUNCTION | 28.04 | 56.21  | 0 | 00:35 | 0.853 |
| 1.74  | 0.000  |          |       |        |   |       |       |
| II3   |        | JUNCTION | 28.32 | 28.32  | 0 | 00:35 | 0.886 |
| 0.886 | 0.000  |          |       |        |   |       |       |
| IRR_J |        | JUNCTION | 0.00  | 114.18 | 0 | 02:26 | 0     |
| 7.97  | 0.000  |          |       |        |   |       |       |
| J10   |        | JUNCTION | 0.00  | 124.52 | 0 | 02:25 | 0     |
| 8.74  | 0.000  |          |       |        |   |       |       |
| J11   |        | JUNCTION | 0.00  | 98.74  | 0 | 01:18 | 0     |
| 4.78  | 0.000  |          |       |        |   |       |       |
| J12   |        | JUNCTION | 0.00  | 24.66  | 0 | 01:04 | 0     |
| 0.985 | -0.000 |          |       |        |   |       |       |
| J13   |        | JUNCTION | 0.00  | 17.17  | 0 | 01:00 | 0     |

|       |       |          |        |        |   |       |       |
|-------|-------|----------|--------|--------|---|-------|-------|
| 0.729 | 0.000 |          |        |        |   |       |       |
| J14   |       | JUNCTION | 0.00   | 76.43  | 0 | 01:01 | 0     |
| 3.44  | 0.000 |          |        |        |   |       |       |
| J15   |       | JUNCTION | 0.00   | 30.95  | 0 | 01:11 | 0     |
| 1.38  | 0.000 |          |        |        |   |       |       |
| J2    |       | JUNCTION | 0.00   | 95.68  | 0 | 02:04 | 0     |
| 5.46  | 0.000 |          |        |        |   |       |       |
| J3    |       | JUNCTION | 0.00   | 22.74  | 0 | 01:51 | 0     |
| 1.57  | 0.000 |          |        |        |   |       |       |
| J4    |       | JUNCTION | 0.00   | 70.77  | 0 | 01:42 | 0     |
| 3.92  | 0.000 |          |        |        |   |       |       |
| J5    |       | JUNCTION | 0.00   | 49.82  | 0 | 00:58 | 0     |
| 2.19  | 0.000 |          |        |        |   |       |       |
| J6    |       | JUNCTION | 0.00   | 12.23  | 0 | 01:27 | 0     |
| 0.847 | 0.000 |          |        |        |   |       |       |
| J7    |       | JUNCTION | 0.00   | 180.87 | 0 | 00:37 | 0     |
| 4.34  | 0.000 |          |        |        |   |       |       |
| J8    |       | JUNCTION | 0.00   | 182.92 | 0 | 00:38 | 0     |
| 4.88  | 0.000 |          |        |        |   |       |       |
| J9    |       | JUNCTION | 0.00   | 94.99  | 0 | 01:28 | 0     |
| 4.83  | 0.000 |          |        |        |   |       |       |
| JJ    |       | JUNCTION | 11.49  | 11.49  | 0 | 00:30 | 0.328 |
| 0.328 | 0.000 |          |        |        |   |       |       |
| K     |       | JUNCTION | 200.94 | 200.94 | 0 | 00:30 | 4.46  |
| 4.46  | 0.000 |          |        |        |   |       |       |
| KK    |       | JUNCTION | 8.14   | 8.14   | 0 | 00:35 | 0.31  |
| 0.31  | 0.000 |          |        |        |   |       |       |
| L     |       | JUNCTION | 15.97  | 15.97  | 0 | 00:35 | 0.603 |
| 0.603 | 0.000 |          |        |        |   |       |       |
| LL    |       | JUNCTION | 7.36   | 7.36   | 0 | 00:30 | 0.226 |
| 0.226 | 0.000 |          |        |        |   |       |       |
| M     |       | JUNCTION | 46.54  | 46.54  | 0 | 00:30 | 1.01  |
| 1.01  | 0.000 |          |        |        |   |       |       |
| N     |       | JUNCTION | 73.48  | 73.48  | 0 | 00:30 | 1.56  |
| 1.56  | 0.000 |          |        |        |   |       |       |
| O     |       | JUNCTION | 63.86  | 63.86  | 0 | 00:35 | 2.02  |
| 2.02  | 0.000 |          |        |        |   |       |       |
| P     |       | JUNCTION | 40.00  | 40.00  | 0 | 00:40 | 1.66  |
| 1.66  | 0.000 |          |        |        |   |       |       |
| Q     |       | JUNCTION | 64.68  | 64.68  | 0 | 00:40 | 2.66  |
| 2.66  | 0.000 |          |        |        |   |       |       |
| R     |       | JUNCTION | 56.59  | 120.84 | 0 | 00:40 | 2.13  |
| 4.79  | 0.000 |          |        |        |   |       |       |
| S     |       | JUNCTION | 30.83  | 30.83  | 0 | 00:30 | 0.841 |
| 0.841 | 0.000 |          |        |        |   |       |       |
| SP1   |       | JUNCTION | 0.00   | 189.85 | 0 | 00:39 | 0     |
| 14.6  | 0.000 |          |        |        |   |       |       |
| SP2   |       | JUNCTION | 0.00   | 223.43 | 0 | 00:48 | 0     |
| 16.7  | 0.000 |          |        |        |   |       |       |
| SP3   |       | JUNCTION | 0.00   | 212.45 | 0 | 01:03 | 0     |

|          |       |          |       |        |   |       |        |
|----------|-------|----------|-------|--------|---|-------|--------|
| 18.1     | 0.000 |          |       |        |   |       |        |
| SP4      |       | JUNCTION | 0.00  | 240.49 | 0 | 01:06 | 0      |
| 19.4     | 0.000 |          |       |        |   |       |        |
| T        |       | JUNCTION | 4.04  | 4.04   | 0 | 00:40 | 0.192  |
| 0.192    | 0.000 |          |       |        |   |       |        |
| T1       |       | JUNCTION | 0.00  | 98.27  | 0 | 01:27 | 0      |
| 5.02     | 0.000 |          |       |        |   |       |        |
| T2       |       | JUNCTION | 0.00  | 104.34 | 0 | 01:26 | 0      |
| 5.37     | 0.000 |          |       |        |   |       |        |
| U        |       | JUNCTION | 4.81  | 4.81   | 0 | 00:40 | 0.215  |
| 0.215    | 0.000 |          |       |        |   |       |        |
| V1       |       | JUNCTION | 13.99 | 13.99  | 0 | 00:35 | 0.448  |
| 0.448    | 0.000 |          |       |        |   |       |        |
| V2       |       | JUNCTION | 16.15 | 16.15  | 0 | 00:35 | 0.572  |
| 0.572    | 0.000 |          |       |        |   |       |        |
| W        |       | JUNCTION | 3.45  | 3.45   | 0 | 00:35 | 0.136  |
| 0.136    | 0.000 |          |       |        |   |       |        |
| X1       |       | JUNCTION | 80.91 | 80.91  | 0 | 00:35 | 2.94   |
| 2.94     | 0.000 |          |       |        |   |       |        |
| X2       |       | JUNCTION | 41.46 | 41.46  | 0 | 00:35 | 1.4    |
| 1.4      | 0.000 |          |       |        |   |       |        |
| X3       |       | JUNCTION | 47.59 | 76.22  | 0 | 00:40 | 2.33   |
| 3.35     | 0.000 |          |       |        |   |       |        |
| I2       |       | JUNCTION | 0.00  | 24.36  | 0 | 01:04 | 0      |
| 0.936    | 0.000 |          |       |        |   |       |        |
| P12      |       | JUNCTION | 0.30  | 0.30   | 0 | 00:00 | 0.0485 |
| 0.0484   | 0.000 |          |       |        |   |       |        |
| LL1      |       | JUNCTION | 0.00  | 16.85  | 0 | 01:15 | 0      |
| 0.663    | 0.000 |          |       |        |   |       |        |
| OF3      |       | OUTFALL  | 0.00  | 95.68  | 0 | 02:04 | 0      |
| 5.46     | 0.000 |          |       |        |   |       |        |
| OF1      |       | OUTFALL  | 0.00  | 240.43 | 0 | 01:07 | 0      |
| 19.4     | 0.000 |          |       |        |   |       |        |
| OF2      |       | OUTFALL  | 0.00  | 104.34 | 0 | 01:26 | 0      |
| 5.37     | 0.000 |          |       |        |   |       |        |
| OF4      |       | OUTFALL  | 0.00  | 307.27 | 0 | 00:48 | 0      |
| 13.3     | 0.000 |          |       |        |   |       |        |
| OF5      |       | OUTFALL  | 0.00  | 16.85  | 0 | 01:15 | 0      |
| 0.663    | 0.000 |          |       |        |   |       |        |
| IRR_POND |       | STORAGE  | 0.00  | 243.77 | 0 | 01:09 | 0      |
| 12.3     | 0.046 |          |       |        |   |       |        |
| P1       |       | STORAGE  | 0.00  | 40.00  | 0 | 00:40 | 0      |
| 1.66     | 0.117 |          |       |        |   |       |        |
| P10      |       | STORAGE  | 0.00  | 17.86  | 0 | 00:40 | 0      |
| 0.818    | 0.062 |          |       |        |   |       |        |
| P11      |       | STORAGE  | 0.00  | 139.15 | 0 | 00:38 | 0      |
| 5.09     | 0.072 |          |       |        |   |       |        |
| P13      |       | STORAGE  | 0.00  | 45.11  | 0 | 00:30 | 0      |
| 0.907    | 0.149 |          |       |        |   |       |        |
| P14      |       | STORAGE  | 0.00  | 87.41  | 0 | 00:41 | 0      |



|       |        |         |    |   |   |         |    |   |
|-------|--------|---------|----|---|---|---------|----|---|
| P1    |        | 32.632  | 11 | 0 | 0 | 57.543  | 19 | 0 |
| 01:24 | 29.38  |         |    |   |   |         |    |   |
| P10   |        | 13.875  | 13 | 0 | 0 | 29.668  | 27 | 0 |
| 01:31 | 13.64  |         |    |   |   |         |    |   |
| P11   |        | 69.800  | 15 | 0 | 0 | 160.007 | 35 | 0 |
| 01:18 | 98.74  |         |    |   |   |         |    |   |
| P13   |        | 33.097  | 13 | 0 | 0 | 58.073  | 23 | 0 |
| 01:00 | 17.17  |         |    |   |   |         |    |   |
| P14   |        | 31.811  | 14 | 0 | 0 | 62.216  | 28 | 0 |
| 01:01 | 76.43  |         |    |   |   |         |    |   |
| P15   |        | 41.957  | 28 | 0 | 0 | 85.004  | 57 | 0 |
| 01:11 | 30.95  |         |    |   |   |         |    |   |
| P2    |        | 202.937 | 43 | 0 | 0 | 286.797 | 61 | 0 |
| 02:06 | 27.93  |         |    |   |   |         |    |   |
| P3    |        | 99.633  | 29 | 0 | 0 | 165.333 | 49 | 0 |
| 01:50 | 22.74  |         |    |   |   |         |    |   |
| P4    |        | 136.283 | 35 | 0 | 0 | 230.559 | 59 | 0 |
| 01:42 | 70.77  |         |    |   |   |         |    |   |
| P5    |        | 44.714  | 16 | 0 | 0 | 81.028  | 30 | 0 |
| 00:56 | 39.47  |         |    |   |   |         |    |   |
| P6    |        | 42.385  | 22 | 0 | 0 | 77.410  | 40 | 0 |
| 01:27 | 12.23  |         |    |   |   |         |    |   |
| P7    |        | 26.618  | 25 | 0 | 0 | 63.403  | 60 | 0 |
| 00:37 | 180.87 |         |    |   |   |         |    |   |
| P8    |        | 22.504  | 21 | 0 | 0 | 43.356  | 41 | 0 |
| 02:02 | 6.50   |         |    |   |   |         |    |   |
| P9    |        | 152.526 | 23 | 0 | 0 | 274.350 | 42 | 0 |
| 01:27 | 94.99  |         |    |   |   |         |    |   |
| P16   |        | 37.021  | 17 | 0 | 0 | 61.293  | 29 | 0 |
| 01:03 | 24.36  |         |    |   |   |         |    |   |
| P17   |        | 31.286  | 38 | 0 | 0 | 47.674  | 58 | 0 |
| 01:14 | 16.85  |         |    |   |   |         |    |   |

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 Outfall Loading Summary  
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| Outfall Node | Flow<br>Freq<br>Pcnt | Avg<br>Flow<br>CFS | Max<br>Flow<br>CFS | Total<br>Volume<br>10^6 gal |
|--------------|----------------------|--------------------|--------------------|-----------------------------|
| OF3          | 98.06                | 34.46              | 95.68              | 5.458                       |
| OF1          | 93.61                | 128.25             | 240.43             | 19.393                      |
| OF2          | 98.33                | 33.80              | 104.34             | 5.371                       |
| OF4          | 98.47                | 83.41              | 307.27             | 13.270                      |
| OF5          | 96.39                | 4.25               | 16.85              | 0.663                       |
| System       | 96.97                | 284.18             | 707.87             | 44.155                      |

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# Link Flow Summary

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| Link     | Type    | Maximum<br> Flow <br>CFS | Time of Max<br>Occurrence<br>days hr:min | Maximum<br> Veloc <br>ft/sec | Max/<br>Full<br>Flow | Max/<br>Full<br>Depth |
|----------|---------|--------------------------|--|------------------------------|----------------------|-----------------------|
| A100     | DUMMY   | 20.84                    | 0 00:35                                  |                              |                      |                       |
| AA100    | DUMMY   | 39.23                    | 0 00:35                                  |                              |                      |                       |
| B100     | CONDUIT | 87.22                    | 0 00:37                                  | 4.63                         | 0.29                 | 0.58                  |
| B200     | CONDUIT | 53.15                    | 0 00:42                                  | 3.55                         | 0.23                 | 0.53                  |
| BB100    | DUMMY   | 40.62                    | 0 00:35                                  |                              |                      |                       |
| BB101    | DUMMY   | 214.28                   | 0 00:41                                  |                              |                      |                       |
| BB102    | DUMMY   | 229.61                   | 0 00:40                                  |                              |                      |                       |
| BB103    | DUMMY   | 307.27                   | 0 00:48                                  |                              |                      |                       |
| C100     | DUMMY   | 35.31                    | 0 00:35                                  |                              |                      |                       |
| C900     | CONDUIT | 46.22                    | 0 00:31                                  | 7.08                         | 0.08                 | 0.32                  |
| CC100    | DUMMY   | 6.53                     | 0 00:35                                  |                              |                      |                       |
| D100     | DUMMY   | 61.12                    | 0 00:30                                  |                              |                      |                       |
| DD100    | DUMMY   | 57.78                    | 0 00:40                                  |                              |                      |                       |
| E100     | CONDUIT | 74.39                    | 0 00:53                                  | 6.43                         | 0.16                 | 0.46                  |
| EE100    | CONDUIT | 60.55                    | 0 00:55                                  | 8.40                         | 0.09                 | 0.34                  |
| EE101    | CONDUIT | 139.71                   | 0 00:49                                  | 10.28                        | 0.18                 | 0.47                  |
| EE200    | DUMMY   | 35.71                    | 0 00:30                                  |                              |                      |                       |
| EE300    | CONDUIT | 10.11                    | 0 00:33                                  | 9.87                         | 0.28                 | 0.36                  |
| F100     | DUMMY   | 24.27                    | 0 00:35                                  |                              |                      |                       |
| G100     | CONDUIT | 50.38                    | 0 00:45                                  | 5.08                         | 0.13                 | 0.42                  |
| GG100    | DUMMY   | 15.49                    | 0 00:35                                  |                              |                      |                       |
| H100     | DUMMY   | 17.86                    | 0 00:40                                  |                              |                      |                       |
| H101     | DUMMY   | 124.52                   | 0 02:25                                  |                              |                      |                       |
| HH100    | DUMMY   | 13.56                    | 0 00:35                                  |                              |                      |                       |
| I100     | DUMMY   | 40.37                    | 0 00:30                                  |                              |                      |                       |
| II100    | CONDUIT | 34.92                    | 0 00:51                                  | 7.77                         | 0.12                 | 0.38                  |
| II200    | CONDUIT | 56.13                    | 0 00:37                                  | 7.64                         | 0.26                 | 0.57                  |
| II300    | CONDUIT | 28.31                    | 0 00:36                                  | 8.19                         | 0.09                 | 0.36                  |
| IRR_J100 | DUMMY   | 114.18                   | 0 02:26                                  |                              |                      |                       |
| J1100    | DUMMY   | 98.74                    | 0 01:18                                  |                              |                      |                       |
| J1200    | CONDUIT | 22.46                    | 0 01:23                                  | 2.08                         | 0.01                 | 0.05                  |
| J1300    | CONDUIT | 17.08                    | 0 01:06                                  | 4.66                         | 0.10                 | 0.37                  |
| J1400    | DUMMY   | 76.43                    | 0 01:01                                  |                              |                      |                       |
| J1500    | DUMMY   | 30.95                    | 0 01:11                                  |                              |                      |                       |
| J300     | CONDUIT | 22.56                    | 0 02:06                                  | 2.06                         | 0.16                 | 0.45                  |
| J400     | CONDUIT | 70.72                    | 0 01:46                                  | 5.83                         | 0.08                 | 0.31                  |
| J500     | DUMMY   | 49.82                    | 0 00:58                                  |                              |                      |                       |
| J600     | CONDUIT | 12.23                    | 0 01:29                                  | 5.66                         | 0.05                 | 0.26                  |
| J700     | CONDUIT | 180.84                   | 0 00:38                                  | 23.78                        | 0.02                 | 0.25                  |

|            |         |        |   |       |       |      |      |
|------------|---------|--------|---|-------|-------|------|------|
| J800       | DUMMY   | 182.92 | 0 | 00:38 |       |      |      |
| J900       | DUMMY   | 94.99  | 0 | 01:28 |       |      |      |
| JJ100      | DUMMY   | 11.49  | 0 | 00:30 |       |      |      |
| JP20       | DUMMY   | 95.68  | 0 | 02:04 |       |      |      |
| K100       | CONDUIT | 200.43 | 0 | 00:31 | 13.74 | 0.20 | 0.49 |
| L100       | DUMMY   | 15.97  | 0 | 00:35 |       |      |      |
| LL100      | DUMMY   | 7.36   | 0 | 00:30 |       |      |      |
| N100       | CONDUIT | 72.03  | 0 | 00:32 | 4.31  | 0.25 | 0.54 |
| O100       | DUMMY   | 63.86  | 0 | 00:35 |       |      |      |
| P100       | DUMMY   | 40.00  | 0 | 00:40 |       |      |      |
| Q100       | DUMMY   | 64.68  | 0 | 00:40 |       |      |      |
| R100       | DUMMY   | 120.84 | 0 | 00:40 |       |      |      |
| S100       | DUMMY   | 30.83  | 0 | 00:30 |       |      |      |
| SP101      | CONDUIT | 186.49 | 0 | 00:44 | 3.96  | 0.05 | 0.20 |
| SP102      | CONDUIT | 208.08 | 0 | 01:03 | 2.46  | 0.12 | 0.33 |
| SP103      | CONDUIT | 212.07 | 0 | 01:06 | 6.78  | 0.02 | 0.11 |
| SP104      | CONDUIT | 240.43 | 0 | 01:07 | 4.59  | 0.04 | 0.18 |
| SP206      | DUMMY   | 104.34 | 0 | 01:26 |       |      |      |
| T100       | DUMMY   | 4.04   | 0 | 00:40 |       |      |      |
| T101       | DUMMY   | 98.27  | 0 | 01:27 |       |      |      |
| U100       | DUMMY   | 4.81   | 0 | 00:40 |       |      |      |
| V100       | DUMMY   | 13.99  | 0 | 00:35 |       |      |      |
| V200       | CONDUIT | 16.01  | 0 | 00:38 | 5.98  | 0.07 | 0.30 |
| W100       | DUMMY   | 3.45   | 0 | 00:35 |       |      |      |
| X100       | DUMMY   | 80.91  | 0 | 00:35 |       |      |      |
| X200       | CONDUIT | 41.01  | 0 | 00:38 | 5.96  | 0.08 | 0.33 |
| X300       | CONDUIT | 76.15  | 0 | 00:41 | 9.36  | 0.09 | 0.34 |
| I200       | DUMMY   | 24.36  | 0 | 01:04 |       |      |      |
| O12        | DUMMY   | 0.30   | 0 | 00:00 |       |      |      |
| KK100      | DUMMY   | 8.14   | 0 | 00:35 |       |      |      |
| LL200      | DUMMY   | 16.85  | 0 | 01:15 |       |      |      |
| IRR_OUTLET | DUMMY   | 114.18 | 0 | 02:26 |       |      |      |
| O1         | DUMMY   | 29.38  | 0 | 01:24 |       |      |      |
| O10        | DUMMY   | 13.64  | 0 | 01:31 |       |      |      |
| O11        | DUMMY   | 98.74  | 0 | 01:18 |       |      |      |
| O13        | DUMMY   | 17.17  | 0 | 01:00 |       |      |      |
| O14        | DUMMY   | 76.43  | 0 | 01:01 |       |      |      |
| O2         | DUMMY   | 27.93  | 0 | 02:07 |       |      |      |
| O3         | DUMMY   | 22.74  | 0 | 01:51 |       |      |      |
| O5         | DUMMY   | 39.47  | 0 | 00:56 |       |      |      |
| O6         | DUMMY   | 12.23  | 0 | 01:27 |       |      |      |
| O7         | DUMMY   | 180.87 | 0 | 00:37 |       |      |      |
| O8         | DUMMY   | 6.50   | 0 | 02:03 |       |      |      |
| O9         | DUMMY   | 94.99  | 0 | 01:28 |       |      |      |
| O16        | DUMMY   | 24.36  | 0 | 01:04 |       |      |      |
| O15        | DUMMY   | 30.95  | 0 | 01:11 |       |      |      |
| O17        | DUMMY   | 16.85  | 0 | 01:15 |       |      |      |
| O4         | DUMMY   | 70.77  | 0 | 01:42 |       |      |      |



\*\*\*\*\*  
Conduit Surcharge Summary  
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No conduits were surcharged.

Analysis begun on: Thu Jul 28 14:53:53 2022  
Analysis ended on: Thu Jul 28 14:53:53 2022  
Total elapsed time: < 1 sec

EPA STORM WATER MANAGEMENT MODEL - VERSION 5.1 (Build 5.1.012)

\*\*\*\*\*  
NOTE: The summary statistics displayed in this report are  
based on results found at every computational time step,  
not just on results from each reporting time step.  
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Analysis Options

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Flow Units ..... CFS

Process Models:

Rainfall/Runoff ..... NO

RDII ..... NO

Snowmelt ..... NO

Groundwater ..... NO

Flow Routing ..... YES

Ponding Allowed ..... NO

Water Quality ..... NO

Flow Routing Method ..... KINWAVE

Starting Date ..... 01/01/2005 00:00:00

Ending Date ..... 01/01/2005 06:00:00

Antecedent Dry Days ..... 0.0

Report Time Step ..... 00:05:00

Routing Time Step ..... 30.00 sec

| *****                      | Volume    | Volume              |
|----------------------------|-----------|---------------------|
| Flow Routing Continuity    | acre-feet | 10 <sup>6</sup> gal |
| *****                      | -----     | -----               |
| Dry Weather Inflow .....   | 0.000     | 0.000               |
| Wet Weather Inflow .....   | 0.000     | 0.000               |
| Groundwater Inflow .....   | 0.000     | 0.000               |
| RDII Inflow .....          | 0.000     | 0.000               |
| External Inflow .....      | 328.826   | 107.153             |
| External Outflow .....     | 290.042   | 94.514              |
| Flooding Loss .....        | 2.515     | 0.820               |
| Evaporation Loss .....     | 0.000     | 0.000               |
| Exfiltration Loss .....    | 0.000     | 0.000               |
| Initial Stored Volume .... | 0.000     | 0.000               |
| Final Stored Volume .....  | 37.312    | 12.159              |
| Continuity Error (%) ..... | -0.317    |                     |

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Highest Flow Instability Indexes

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Link J700 (3)  
 Link 07 (3)  
 Link J1300 (2)  
 Link J1200 (2)  
 Link J500 (2)

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#### Routing Time Step Summary

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Minimum Time Step : 30.00 sec  
 Average Time Step : 30.00 sec  
 Maximum Time Step : 30.00 sec  
 Percent in Steady State : 0.00  
 Average Iterations per Step : 1.00  
 Percent Not Converging : 0.00

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#### Node Depth Summary

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| Node | Type     | Average<br>Depth<br>Feet | Maximum<br>Depth<br>Feet | Maximum<br>HGL<br>Feet | Time of Max<br>Occurrence<br>days hr:min | Reported<br>Max Depth<br>Feet |
|------|----------|--------------------------|--------------------------|------------------------|--|-------------------------------|
| A    | JUNCTION | 0.00                     | 0.00                     | 7625.00                | 0 00:00                                  | 0.00                          |
| AA   | JUNCTION | 0.00                     | 0.00                     | 7525.00                | 0 00:00                                  | 0.00                          |
| B1   | JUNCTION | 0.67                     | 2.37                     | 7577.37                | 0 00:40                                  | 2.37                          |
| B2   | JUNCTION | 0.71                     | 2.22                     | 7577.22                | 0 00:45                                  | 2.21                          |
| BB   | JUNCTION | 0.00                     | 0.00                     | 7410.00                | 0 00:00                                  | 0.00                          |
| BB1  | JUNCTION | 0.69                     | 2.09                     | 7387.09                | 0 00:52                                  | 2.08                          |
| BB2  | JUNCTION | 0.00                     | 0.00                     | 7365.00                | 0 00:00                                  | 0.00                          |
| BB3  | JUNCTION | 0.00                     | 0.00                     | 7330.00                | 0 00:00                                  | 0.00                          |
| C    | JUNCTION | 0.00                     | 0.00                     | 7635.00                | 0 00:00                                  | 0.00                          |
| CC   | JUNCTION | 0.00                     | 0.00                     | 7495.00                | 0 00:00                                  | 0.00                          |
| D    | JUNCTION | 0.00                     | 0.00                     | 7609.00                | 0 00:00                                  | 0.00                          |
| DD   | JUNCTION | 0.00                     | 0.00                     | 7495.00                | 0 00:00                                  | 0.00                          |
| E    | JUNCTION | 0.81                     | 1.91                     | 7573.91                | 0 00:55                                  | 1.91                          |
| EE1  | JUNCTION | 0.52                     | 1.57                     | 7476.57                | 0 00:52                                  | 1.57                          |
| EE2  | JUNCTION | 0.00                     | 0.00                     | 7550.00                | 0 00:00                                  | 0.00                          |
| EE3  | JUNCTION | 0.23                     | 1.05                     | 7576.05                | 0 00:35                                  | 1.04                          |
| F    | JUNCTION | 0.00                     | 0.00                     | 7633.00                | 0 00:00                                  | 0.00                          |
| FF   | JUNCTION | 0.69                     | 2.09                     | 7432.09                | 0 00:51                                  | 2.08                          |
| G    | JUNCTION | 0.57                     | 1.76                     | 7566.76                | 0 00:45                                  | 1.76                          |
| GG   | JUNCTION | 0.00                     | 0.00                     | 7420.00                | 0 00:00                                  | 0.00                          |
| H    | JUNCTION | 0.00                     | 0.00                     | 7530.00                | 0 00:00                                  | 0.00                          |
| HH   | JUNCTION | 0.00                     | 0.00                     | 7410.00                | 0 00:00                                  | 0.00                          |
| I    | JUNCTION | 0.00                     | 0.00                     | 7595.00                | 0 00:00                                  | 0.00                          |

|       |          |      |      |         |   |       |      |
|-------|----------|------|------|---------|---|-------|------|
| II1   | JUNCTION | 0.44 | 1.08 | 7496.08 | 0 | 00:50 | 1.08 |
| II2   | JUNCTION | 0.41 | 1.55 | 7451.55 | 0 | 00:40 | 1.55 |
| II3   | JUNCTION | 0.26 | 0.99 | 7515.99 | 0 | 00:40 | 0.99 |
| IRR_J | JUNCTION | 0.00 | 0.00 | 7528.00 | 0 | 00:00 | 0.00 |
| J10   | JUNCTION | 0.00 | 0.00 | 7520.00 | 0 | 00:00 | 0.00 |
| J11   | JUNCTION | 0.00 | 0.00 | 7565.00 | 0 | 00:00 | 0.00 |
| J12   | JUNCTION | 0.36 | 0.54 | 7545.54 | 0 | 00:55 | 0.54 |
| J13   | JUNCTION | 0.39 | 1.25 | 7521.25 | 0 | 00:51 | 1.24 |
| J14   | JUNCTION | 0.00 | 0.00 | 7375.00 | 0 | 00:00 | 0.00 |
| J15   | JUNCTION | 0.00 | 0.00 | 7552.00 | 0 | 00:00 | 0.00 |
| J2    | JUNCTION | 0.76 | 2.02 | 7437.02 | 0 | 01:15 | 2.02 |
| J3    | JUNCTION | 1.10 | 1.84 | 7496.84 | 0 | 01:39 | 1.84 |
| J4    | JUNCTION | 0.75 | 2.02 | 7467.02 | 0 | 01:12 | 2.02 |
| J5    | JUNCTION | 0.41 | 0.99 | 7525.99 | 0 | 01:07 | 0.99 |
| J6    | JUNCTION | 0.41 | 0.99 | 7570.99 | 0 | 01:05 | 0.99 |
| J7    | JUNCTION | 0.46 | 1.36 | 7546.36 | 0 | 00:31 | 1.36 |
| J8    | JUNCTION | 0.46 | 1.37 | 7526.37 | 0 | 00:32 | 1.36 |
| J9    | JUNCTION | 0.00 | 0.00 | 7550.00 | 0 | 00:00 | 0.00 |
| JJ    | JUNCTION | 0.00 | 0.00 | 7575.00 | 0 | 00:00 | 0.00 |
| K     | JUNCTION | 0.41 | 1.98 | 7586.98 | 0 | 00:35 | 1.96 |
| KK    | JUNCTION | 0.00 | 0.00 | 7590.00 | 0 | 00:00 | 0.00 |
| L     | JUNCTION | 0.00 | 0.00 | 7548.00 | 0 | 00:00 | 0.00 |
| LL    | JUNCTION | 0.00 | 0.00 | 7580.00 | 0 | 00:00 | 0.00 |
| M     | JUNCTION | 0.26 | 1.30 | 7591.30 | 0 | 00:35 | 1.29 |
| N     | JUNCTION | 0.44 | 2.18 | 7537.18 | 0 | 00:35 | 2.17 |
| O     | JUNCTION | 0.00 | 0.00 | 7559.00 | 0 | 00:00 | 0.00 |
| P     | JUNCTION | 0.00 | 0.00 | 7500.37 | 0 | 00:00 | 0.00 |
| Q     | JUNCTION | 0.00 | 0.00 | 7585.00 | 0 | 00:00 | 0.00 |
| R     | JUNCTION | 0.00 | 0.00 | 7576.00 | 0 | 00:00 | 0.00 |
| S     | JUNCTION | 0.00 | 0.00 | 7598.00 | 0 | 00:00 | 0.00 |
| SP1   | JUNCTION | 0.85 | 1.43 | 7511.43 | 0 | 01:14 | 1.43 |
| SP2   | JUNCTION | 1.37 | 2.40 | 7497.40 | 0 | 01:16 | 2.38 |
| SP3   | JUNCTION | 1.33 | 2.37 | 7492.37 | 0 | 01:20 | 2.37 |
| SP4   | JUNCTION | 0.87 | 1.61 | 7421.61 | 0 | 01:22 | 1.60 |
| T     | JUNCTION | 0.00 | 0.00 | 7583.00 | 0 | 00:00 | 0.00 |
| T1    | JUNCTION | 0.00 | 0.00 | 7565.00 | 0 | 00:00 | 0.00 |
| T2    | JUNCTION | 0.00 | 0.00 | 7555.00 | 0 | 00:00 | 0.00 |
| U     | JUNCTION | 0.00 | 0.00 | 7567.00 | 0 | 00:00 | 0.00 |
| V1    | JUNCTION | 0.00 | 0.00 | 7598.00 | 0 | 00:00 | 0.00 |
| V2    | JUNCTION | 0.24 | 0.85 | 7565.85 | 0 | 00:40 | 0.85 |
| W     | JUNCTION | 0.00 | 0.00 | 7546.00 | 0 | 00:00 | 0.00 |
| X1    | JUNCTION | 0.00 | 0.00 | 7485.00 | 0 | 00:00 | 0.00 |
| X2    | JUNCTION | 0.38 | 1.37 | 7506.37 | 0 | 00:40 | 1.36 |
| X3    | JUNCTION | 0.50 | 1.44 | 7501.44 | 0 | 00:46 | 1.43 |
| I2    | JUNCTION | 0.00 | 0.00 | 7577.00 | 0 | 00:00 | 0.00 |
| P12   | JUNCTION | 0.00 | 0.00 | 7550.00 | 0 | 00:00 | 0.00 |
| LL1   | JUNCTION | 0.00 | 0.00 | 0.00    | 0 | 00:00 | 0.00 |
| OF3   | OUTFALL  | 0.00 | 0.00 | 7431.00 | 0 | 00:00 | 0.00 |
| OF1   | OUTFALL  | 0.87 | 1.61 | 7416.61 | 0 | 01:22 | 1.60 |
| OF2   | OUTFALL  | 0.00 | 0.00 | 7550.00 | 0 | 00:00 | 0.00 |

|          |         |      |       |         |   |       |       |
|----------|---------|------|-------|---------|---|-------|-------|
| OF4      | OUTFALL | 0.00 | 0.00  | 7325.00 | 0 | 00:00 | 0.00  |
| OF5      | OUTFALL | 0.00 | 0.00  | 7520.00 | 0 | 00:00 | 0.00  |
| IRR_POND | STORAGE | 2.76 | 4.57  | 7534.57 | 0 | 02:06 | 4.57  |
| P1       | STORAGE | 2.80 | 4.52  | 7429.52 | 0 | 01:07 | 4.52  |
| P10      | STORAGE | 3.39 | 5.83  | 7530.83 | 0 | 01:09 | 5.83  |
| P11      | STORAGE | 3.68 | 7.59  | 7577.59 | 0 | 01:11 | 7.59  |
| P13      | STORAGE | 3.01 | 4.81  | 7529.81 | 0 | 00:51 | 4.80  |
| P14      | STORAGE | 3.99 | 8.57  | 7408.57 | 0 | 01:10 | 8.57  |
| P15      | STORAGE | 3.14 | 5.82  | 7560.82 | 0 | 01:09 | 5.82  |
| P2       | STORAGE | 6.20 | 8.76  | 7444.76 | 0 | 01:38 | 8.76  |
| P3       | STORAGE | 5.54 | 8.81  | 7518.81 | 0 | 01:39 | 8.81  |
| P4       | STORAGE | 5.49 | 8.80  | 7477.80 | 0 | 01:12 | 8.79  |
| P5       | STORAGE | 3.36 | 5.72  | 7535.72 | 0 | 00:52 | 5.70  |
| P6       | STORAGE | 4.75 | 7.78  | 7581.78 | 0 | 01:05 | 7.78  |
| P7       | STORAGE | 4.94 | 10.00 | 7560.00 | 0 | 00:55 | 10.00 |
| P8       | STORAGE | 4.50 | 7.09  | 7541.09 | 0 | 01:14 | 7.09  |
| P9       | STORAGE | 4.37 | 7.80  | 7577.80 | 0 | 01:17 | 7.79  |
| P16      | STORAGE | 3.53 | 5.40  | 7605.40 | 0 | 00:55 | 5.40  |
| P17      | STORAGE | 4.59 | 6.39  | 7567.39 | 0 | 00:53 | 6.39  |

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Node Inflow Summary

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| Total  |         | Flow     |  | Maximum | Maximum | Lateral     |          |
|--------|---------|----------|--|---------|---------|-------------|----------|
| Inflow | Balance |          |  | Lateral | Total   | Time of Max | Inflow   |
| Volume | Error   |          |  | Inflow  | Inflow  | Occurrence  | Volume   |
| Node   |         | Type     |  | CFS     | CFS     | days hr:min | 10^6 gal |
| gal    | Percent |          |  |         |         |             | 10^6     |
| -----  |         |          |  |         |         |             |          |
| -----  |         |          |  |         |         |             |          |
| A      |         | JUNCTION |  | 43.83   | 43.83   | 0 00:40     | 1.3      |
| 1.3    | 0.000   |          |  |         |         |             |          |
| AA     |         | JUNCTION |  | 81.18   | 81.18   | 0 00:40     | 2.33     |
| 2.33   | 0.000   |          |  |         |         |             |          |
| B1     |         | JUNCTION |  | 133.69  | 177.52  | 0 00:40     | 4.17     |
| 5.47   | 0.000   |          |  |         |         |             |          |
| B2     |         | JUNCTION |  | 37.14   | 112.42  | 0 00:45     | 1.39     |
| 3.89   | 0.000   |          |  |         |         |             |          |
| BB     |         | JUNCTION |  | 84.15   | 84.15   | 0 00:40     | 2.56     |
| 2.56   | 0.000   |          |  |         |         |             |          |
| BB1    |         | JUNCTION |  | 0.00    | 483.72  | 0 00:50     | 0        |

|       |        |          |        |        |   |       |       |
|-------|--------|----------|--------|--------|---|-------|-------|
| 16.3  | 0.000  |          |        |        |   |       |       |
| BB2   |        | JUNCTION | 0.00   | 515.49 | 0 | 00:50 | 0     |
| 17.4  | 0.000  |          |        |        |   |       |       |
| BB3   |        | JUNCTION | 0.00   | 646.46 | 0 | 00:51 | 0     |
| 24.8  | 0.000  |          |        |        |   |       |       |
| C     |        | JUNCTION | 75.28  | 75.28  | 0 | 00:45 | 2.5   |
| 2.5   | 0.000  |          |        |        |   |       |       |
| CC    |        | JUNCTION | 13.57  | 13.57  | 0 | 00:40 | 0.431 |
| 0.431 | 0.000  |          |        |        |   |       |       |
| D     |        | JUNCTION | 117.38 | 117.38 | 0 | 00:35 | 2.86  |
| 2.86  | 0.000  |          |        |        |   |       |       |
| DD    |        | JUNCTION | 122.41 | 122.41 | 0 | 00:50 | 4.81  |
| 4.81  | 0.000  |          |        |        |   |       |       |
| E     |        | JUNCTION | 157.91 | 157.91 | 0 | 00:55 | 7.39  |
| 7.39  | 0.000  |          |        |        |   |       |       |
| EE1   |        | JUNCTION | 110.30 | 156.68 | 0 | 00:52 | 3.51  |
| 4.92  | 0.000  |          |        |        |   |       |       |
| EE2   |        | JUNCTION | 63.62  | 63.62  | 0 | 00:35 | 1.13  |
| 1.13  | 0.000  |          |        |        |   |       |       |
| EE3   |        | JUNCTION | 19.33  | 19.33  | 0 | 00:35 | 0.463 |
| 0.463 | 0.000  |          |        |        |   |       |       |
| F     |        | JUNCTION | 51.63  | 51.63  | 0 | 00:45 | 1.73  |
| 1.73  | 0.000  |          |        |        |   |       |       |
| FF    |        | JUNCTION | 43.07  | 330.28 | 0 | 00:51 | 1.24  |
| 11.4  | -0.000 |          |        |        |   |       |       |
| G     |        | JUNCTION | 57.12  | 108.76 | 0 | 00:45 | 2.18  |
| 3.91  | 0.000  |          |        |        |   |       |       |
| GG    |        | JUNCTION | 32.48  | 32.48  | 0 | 00:45 | 1.13  |
| 1.13  | 0.000  |          |        |        |   |       |       |
| H     |        | JUNCTION | 37.80  | 37.80  | 0 | 00:45 | 1.52  |
| 1.52  | 0.000  |          |        |        |   |       |       |
| HH    |        | JUNCTION | 28.16  | 28.16  | 0 | 00:40 | 0.87  |
| 0.87  | 0.000  |          |        |        |   |       |       |
| I     |        | JUNCTION | 78.06  | 78.06  | 0 | 00:35 | 2.02  |
| 2.02  | 0.000  |          |        |        |   |       |       |
| II1   |        | JUNCTION | 74.39  | 74.39  | 0 | 00:50 | 3.49  |
| 3.49  | 0.000  |          |        |        |   |       |       |
| II2   |        | JUNCTION | 57.88  | 116.26 | 0 | 00:40 | 1.58  |
| 3.23  | 0.000  |          |        |        |   |       |       |
| II3   |        | JUNCTION | 58.65  | 58.65  | 0 | 00:40 | 1.64  |
| 1.64  | 0.000  |          |        |        |   |       |       |
| IRR_J |        | JUNCTION | 0.00   | 274.80 | 0 | 02:06 | 0     |
| 18.3  | 0.000  |          |        |        |   |       |       |
| J10   |        | JUNCTION | 0.00   | 292.64 | 0 | 02:03 | 0     |
| 19.7  | 0.000  |          |        |        |   |       |       |
| J11   |        | JUNCTION | 0.00   | 230.44 | 0 | 01:11 | 0     |
| 9.06  | 0.000  |          |        |        |   |       |       |
| J12   |        | JUNCTION | 0.00   | 108.72 | 0 | 00:55 | 0     |
| 9.1   | 0.000  |          |        |        |   |       |       |
| J13   |        | JUNCTION | 0.00   | 54.35  | 0 | 00:51 | 0     |

|       |       |          |        |        |   |       |       |
|-------|-------|----------|--------|--------|---|-------|-------|
| 1.41  | 0.000 |          |        |        |   |       |       |
| J14   |       | JUNCTION | 0.00   | 155.08 | 0 | 01:10 | 0     |
| 6.54  | 0.000 |          |        |        |   |       |       |
| J15   |       | JUNCTION | 0.00   | 68.43  | 0 | 01:09 | 0     |
| 2.65  | 0.000 |          |        |        |   |       |       |
| J2    |       | JUNCTION | 0.00   | 271.49 | 0 | 01:15 | 0     |
| 11.8  | 0.000 |          |        |        |   |       |       |
| J3    |       | JUNCTION | 0.00   | 46.10  | 0 | 01:39 | 0     |
| 3.15  | 0.000 |          |        |        |   |       |       |
| J4    |       | JUNCTION | 0.00   | 199.13 | 0 | 01:12 | 0     |
| 7.87  | 0.000 |          |        |        |   |       |       |
| J5    |       | JUNCTION | 0.00   | 139.06 | 0 | 01:02 | 0     |
| 4.27  | 0.000 |          |        |        |   |       |       |
| J6    |       | JUNCTION | 0.00   | 47.71  | 0 | 01:05 | 0     |
| 1.65  | 0.000 |          |        |        |   |       |       |
| J7    |       | JUNCTION | 0.00   | 234.87 | 0 | 00:31 | 0     |
| 7.11  | 0.000 |          |        |        |   |       |       |
| J8    |       | JUNCTION | 0.00   | 259.47 | 0 | 01:14 | 0     |
| 8.15  | 0.000 |          |        |        |   |       |       |
| J9    |       | JUNCTION | 0.00   | 221.14 | 0 | 01:17 | 0     |
| 9.59  | 0.000 |          |        |        |   |       |       |
| JJ    |       | JUNCTION | 22.80  | 22.80  | 0 | 00:35 | 0.603 |
| 0.603 | 0.000 |          |        |        |   |       |       |
| K     |       | JUNCTION | 382.30 | 382.30 | 0 | 00:35 | 8.05  |
| 8.05  | 0.000 |          |        |        |   |       |       |
| KK    |       | JUNCTION | 16.95  | 16.95  | 0 | 00:40 | 0.575 |
| 0.575 | 0.000 |          |        |        |   |       |       |
| L     |       | JUNCTION | 32.40  | 32.40  | 0 | 00:40 | 1.1   |
| 1.1   | 0.000 |          |        |        |   |       |       |
| LL    |       | JUNCTION | 15.07  | 15.07  | 0 | 00:40 | 0.418 |
| 0.418 | 0.000 |          |        |        |   |       |       |
| M     |       | JUNCTION | 89.08  | 89.08  | 0 | 00:35 | 1.83  |
| 1.83  | 0.000 |          |        |        |   |       |       |
| N     |       | JUNCTION | 141.24 | 141.24 | 0 | 00:35 | 2.84  |
| 2.84  | 0.000 |          |        |        |   |       |       |
| O     |       | JUNCTION | 127.40 | 127.40 | 0 | 00:40 | 3.67  |
| 3.67  | 0.000 |          |        |        |   |       |       |
| P     |       | JUNCTION | 82.83  | 82.83  | 0 | 00:45 | 3.04  |
| 3.04  | 0.000 |          |        |        |   |       |       |
| Q     |       | JUNCTION | 137.80 | 137.80 | 0 | 00:45 | 4.98  |
| 4.98  | 0.000 |          |        |        |   |       |       |
| R     |       | JUNCTION | 116.06 | 253.86 | 0 | 00:45 | 3.91  |
| 8.89  | 0.000 |          |        |        |   |       |       |
| S     |       | JUNCTION | 58.96  | 58.96  | 0 | 00:35 | 1.52  |
| 1.52  | 0.000 |          |        |        |   |       |       |
| SP1   |       | JUNCTION | 0.00   | 511.89 | 0 | 01:14 | 0     |
| 36.8  | 0.000 |          |        |        |   |       |       |
| SP2   |       | JUNCTION | 0.00   | 618.35 | 0 | 01:16 | 0     |
| 40.8  | 0.000 |          |        |        |   |       |       |
| SP3   |       | JUNCTION | 0.00   | 641.31 | 0 | 01:20 | 0     |

|          |       |          |        |        |   |       |       |
|----------|-------|----------|--------|--------|---|-------|-------|
| 43.3     | 0.000 |          |        |        |   |       |       |
| SP4      |       | JUNCTION | 0.00   | 706.05 | 0 | 01:22 | 0     |
| 46       | 0.000 |          |        |        |   |       |       |
| T        |       | JUNCTION | 8.68   | 8.68   | 0 | 00:45 | 0.359 |
| 0.359    | 0.000 |          |        |        |   |       |       |
| T1       |       | JUNCTION | 0.00   | 228.33 | 0 | 01:17 | 0     |
| 9.95     | 0.000 |          |        |        |   |       |       |
| T2       |       | JUNCTION | 0.00   | 242.18 | 0 | 01:16 | 0     |
| 10.6     | 0.000 |          |        |        |   |       |       |
| U        |       | JUNCTION | 10.51  | 10.51  | 0 | 00:45 | 0.402 |
| 0.402    | 0.000 |          |        |        |   |       |       |
| V1       |       | JUNCTION | 27.67  | 27.67  | 0 | 00:40 | 0.808 |
| 0.808    | 0.000 |          |        |        |   |       |       |
| V2       |       | JUNCTION | 33.25  | 33.25  | 0 | 00:40 | 1.06  |
| 1.06     | 0.000 |          |        |        |   |       |       |
| W        |       | JUNCTION | 7.46   | 7.46   | 0 | 00:40 | 0.255 |
| 0.255    | 0.000 |          |        |        |   |       |       |
| X1       |       | JUNCTION | 163.27 | 163.27 | 0 | 00:45 | 5.34  |
| 5.34     | 0.000 |          |        |        |   |       |       |
| X2       |       | JUNCTION | 82.46  | 82.46  | 0 | 00:40 | 2.54  |
| 2.54     | 0.000 |          |        |        |   |       |       |
| X3       |       | JUNCTION | 100.73 | 158.96 | 0 | 00:46 | 4.3   |
| 6.17     | 0.000 |          |        |        |   |       |       |
| I2       |       | JUNCTION | 0.00   | 63.72  | 0 | 00:55 | 0     |
| 1.84     | 0.000 |          |        |        |   |       |       |
| P12      |       | JUNCTION | 45.00  | 45.00  | 0 | 00:00 | 7.27  |
| 7.27     | 0.000 |          |        |        |   |       |       |
| LL1      |       | JUNCTION | 0.00   | 49.55  | 0 | 00:53 | 0     |
| 1.39     | 0.000 |          |        |        |   |       |       |
| OF3      |       | OUTFALL  | 0.00   | 271.49 | 0 | 01:15 | 0     |
| 11.8     | 0.000 |          |        |        |   |       |       |
| OF1      |       | OUTFALL  | 0.00   | 705.93 | 0 | 01:22 | 0     |
| 45.9     | 0.000 |          |        |        |   |       |       |
| OF2      |       | OUTFALL  | 0.00   | 242.18 | 0 | 01:16 | 0     |
| 10.6     | 0.000 |          |        |        |   |       |       |
| OF4      |       | OUTFALL  | 0.00   | 646.46 | 0 | 00:51 | 0     |
| 24.8     | 0.000 |          |        |        |   |       |       |
| OF5      |       | OUTFALL  | 0.00   | 49.55  | 0 | 00:53 | 0     |
| 1.39     | 0.000 |          |        |        |   |       |       |
| IRR_POND |       | STORAGE  | 0.00   | 550.27 | 0 | 01:07 | 0     |
| 23       | 0.038 |          |        |        |   |       |       |
| P1       |       | STORAGE  | 0.00   | 82.83  | 0 | 00:45 | 0     |
| 3.04     | 0.095 |          |        |        |   |       |       |
| P10      |       | STORAGE  | 0.00   | 37.80  | 0 | 00:45 | 0     |
| 1.52     | 0.076 |          |        |        |   |       |       |
| P11      |       | STORAGE  | 0.00   | 287.54 | 0 | 00:46 | 0     |
| 9.37     | 0.043 |          |        |        |   |       |       |
| P13      |       | STORAGE  | 0.00   | 81.59  | 0 | 00:35 | 0     |
| 1.59     | 0.115 |          |        |        |   |       |       |
| P14      |       | STORAGE  | 0.00   | 184.37 | 0 | 00:47 | 0     |



|      |       |         |      |        |   |       |   |
|------|-------|---------|------|--------|---|-------|---|
| 6.72 | 0.071 |         |      |        |   |       |   |
| P15  |       | STORAGE | 0.00 | 117.38 | 0 | 00:35 | 0 |
| 2.86 | 0.060 |         |      |        |   |       |   |
| P2   |       | STORAGE | 0.00 | 163.27 | 0 | 00:45 | 0 |
| 5.34 | 0.041 |         |      |        |   |       |   |
| P3   |       | STORAGE | 0.00 | 127.40 | 0 | 00:40 | 0 |
| 3.67 | 0.027 |         |      |        |   |       |   |
| P4   |       | STORAGE | 0.00 | 240.47 | 0 | 00:46 | 0 |
| 8.71 | 0.064 |         |      |        |   |       |   |
| P5   |       | STORAGE | 0.00 | 139.56 | 0 | 00:37 | 0 |
| 2.84 | 0.133 |         |      |        |   |       |   |
| P6   |       | STORAGE | 0.00 | 88.72  | 0 | 00:36 | 0 |
| 1.83 | 0.087 |         |      |        |   |       |   |
| P7   |       | STORAGE | 0.00 | 381.85 | 0 | 00:36 | 0 |
| 8.05 | 0.051 |         |      |        |   |       |   |
| P8   |       | STORAGE | 0.00 | 32.40  | 0 | 00:40 | 0 |
| 1.1  | 0.111 |         |      |        |   |       |   |
| P9   |       | STORAGE | 0.00 | 309.44 | 0 | 00:45 | 0 |
| 10.4 | 0.048 |         |      |        |   |       |   |
| P16  |       | STORAGE | 0.00 | 78.06  | 0 | 00:35 | 0 |
| 2.02 | 0.131 |         |      |        |   |       |   |
| P17  |       | STORAGE | 0.00 | 54.80  | 0 | 00:40 | 0 |
| 1.6  | 0.221 |         |      |        |   |       |   |

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#### Node Flooding Summary

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Flooding refers to all water that overflows a node, whether it ponds or not.

| Node | Hours<br>Flooded | Maximum<br>Rate<br>CFS | Time of Max<br>Occurrence<br>days hr:min | Total<br>Flood<br>Volume<br>10 <sup>6</sup> gal | Maximum<br>Ponded<br>Volume<br>1000 ft <sup>3</sup> |
|------|------------------|------------------------|--|---|---|
| P7   | 0.39             | 144.38                 | 0 00:37                                  | 0.819   | 0.000   |

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#### Storage Volume Summary

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| of Max<br>Occurrence | Maximum<br>Outflow | Average<br>Volume | Avg<br>Pcnt | Evap<br>Pcnt | Exfil<br>Pcnt | Maximum<br>Volume | Max<br>Pcnt | Time |
|----------------------|--------------------|-------------------|-------------|--------------|---------------|-------------------|-------------|------|
|----------------------|--------------------|-------------------|-------------|--------------|---------------|-------------------|-------------|------|

| Storage Unit<br>hr:min | CFS    | 1000 ft3 | Full | Loss | Loss | 1000 ft3 | Full | days |
|------------------------|--------|----------|------|------|------|----------|------|------|
| -----                  |        |          |      |      |      |          |      |      |
| IRR_POND               |        | 937.643  | 43   | 0    | 0    | 1601.097 | 73   | 0    |
| 02:06                  | 274.80 |          |      |      |      |          |      |      |
| P1                     |        | 40.419   | 13   | 0    | 0    | 86.546   | 29   | 0    |
| 01:06                  | 73.03  |          |      |      |      |          |      |      |
| P10                    |        | 17.750   | 16   | 0    | 0    | 40.965   | 37   | 0    |
| 01:09                  | 33.90  |          |      |      |      |          |      |      |
| P11                    |        | 102.795  | 23   | 0    | 0    | 298.174  | 65   | 0    |
| 01:10                  | 230.44 |          |      |      |      |          |      |      |
| P13                    |        | 36.773   | 14   | 0    | 0    | 78.989   | 31   | 0    |
| 00:51                  | 54.35  |          |      |      |      |          |      |      |
| P14                    |        | 58.001   | 26   | 0    | 0    | 174.628  | 77   | 0    |
| 01:09                  | 155.08 |          |      |      |      |          |      |      |
| P15                    |        | 53.042   | 36   | 0    | 0    | 140.809  | 95   | 0    |
| 01:09                  | 68.43  |          |      |      |      |          |      |      |
| P2                     |        | 240.111  | 51   | 0    | 0    | 385.792  | 82   | 0    |
| 01:38                  | 74.57  |          |      |      |      |          |      |      |
| P3                     |        | 143.247  | 42   | 0    | 0    | 277.490  | 82   | 0    |
| 01:39                  | 46.10  |          |      |      |      |          |      |      |
| P4                     |        | 163.739  | 42   | 0    | 0    | 320.570  | 82   | 0    |
| 01:11                  | 199.13 |          |      |      |      |          |      |      |
| P5                     |        | 49.222   | 18   | 0    | 0    | 111.726  | 41   | 0    |
| 00:52                  | 103.73 |          |      |      |      |          |      |      |
| P6                     |        | 61.785   | 32   | 0    | 0    | 127.676  | 65   | 0    |
| 01:05                  | 47.71  |          |      |      |      |          |      |      |
| P7                     |        | 33.332   | 32   | 0    | 0    | 105.140  | 100  | 0    |
| 00:36                  | 234.87 |          |      |      |      |          |      |      |
| P8                     |        | 27.994   | 26   | 0    | 0    | 56.030   | 53   | 0    |
| 01:14                  | 24.60  |          |      |      |      |          |      |      |
| P9                     |        | 198.987  | 31   | 0    | 0    | 450.202  | 69   | 0    |
| 01:17                  | 221.14 |          |      |      |      |          |      |      |
| P16                    |        | 40.266   | 19   | 0    | 0    | 77.891   | 37   | 0    |
| 00:55                  | 63.72  |          |      |      |      |          |      |      |
| P17                    |        | 33.643   | 41   | 0    | 0    | 55.496   | 68   | 0    |
| 00:52                  | 49.55  |          |      |      |      |          |      |      |

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# Outfall Loading Summary

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| -----        |                      |                    |                    |                             |
|--------------|----------------------|--------------------|--------------------|-----------------------------|
| Outfall Node | Flow<br>Freq<br>Pcnt | Avg<br>Flow<br>CFS | Max<br>Flow<br>CFS | Total<br>Volume<br>10^6 gal |
| -----        |                      |                    |                    |                             |

|        |       |        |         |        |
|--------|-------|--------|---------|--------|
| OF3    | 98.19 | 74.32  | 271.49  | 11.790 |
| OF1    | 93.47 | 303.87 | 705.93  | 45.881 |
| OF2    | 98.47 | 66.67  | 242.18  | 10.607 |
| OF4    | 98.47 | 156.12 | 646.46  | 24.839 |
| OF5    | 96.53 | 8.92   | 49.55   | 1.391  |
| -----  |       |        |         |        |
| System | 97.03 | 609.90 | 1777.26 | 94.507 |

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Link Flow Summary  
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| Link     | Type    | Maximum<br> Flow <br>CFS | Time of Max<br>Occurrence<br>days hr:min | Maximum<br> Veloc <br>ft/sec | Max/<br>Full<br>Flow | Max/<br>Full<br>Depth |
|----------|---------|--------------------------|--|------------------------------|----------------------|-----------------------|
| -----    |         |                          |  |                              |                      |                       |
| A100     | DUMMY   | 43.83                    | 0 00:40                                  |                              |                      |                       |
| AA100    | DUMMY   | 81.18                    | 0 00:40                                  |                              |                      |                       |
| B100     | CONDUIT | 176.88                   | 0 00:42                                  | 5.55                         | 0.58                 | 0.79                  |
| B200     | CONDUIT | 112.09                   | 0 00:47                                  | 4.28                         | 0.49                 | 0.74                  |
| BB100    | DUMMY   | 84.15                    | 0 00:40                                  |                              |                      |                       |
| BB101    | DUMMY   | 483.72                   | 0 00:50                                  |                              |                      |                       |
| BB102    | DUMMY   | 515.49                   | 0 00:50                                  |                              |                      |                       |
| BB103    | DUMMY   | 646.46                   | 0 00:51                                  |                              |                      |                       |
| C100     | DUMMY   | 75.28                    | 0 00:45                                  |                              |                      |                       |
| C900     | CONDUIT | 88.72                    | 0 00:36                                  | 8.38                         | 0.14                 | 0.43                  |
| CC100    | DUMMY   | 13.57                    | 0 00:40                                  |                              |                      |                       |
| D100     | DUMMY   | 117.38                   | 0 00:35                                  |                              |                      |                       |
| DD100    | DUMMY   | 122.41                   | 0 00:50                                  |                              |                      |                       |
| E100     | CONDUIT | 157.49                   | 0 00:58                                  | 7.78                         | 0.34                 | 0.64                  |
| EE100    | CONDUIT | 156.62                   | 0 00:53                                  | 10.75                        | 0.22                 | 0.52                  |
| EE101    | CONDUIT | 330.14                   | 0 00:52                                  | 12.84                        | 0.43                 | 0.70                  |
| EE200    | DUMMY   | 63.62                    | 0 00:35                                  |                              |                      |                       |
| EE300    | CONDUIT | 19.07                    | 0 00:39                                  | 11.63                        | 0.53                 | 0.52                  |
| F100     | DUMMY   | 51.63                    | 0 00:45                                  |                              |                      |                       |
| G100     | CONDUIT | 107.69                   | 0 00:51                                  | 6.18                         | 0.28                 | 0.58                  |
| GG100    | DUMMY   | 32.48                    | 0 00:45                                  |                              |                      |                       |
| H100     | DUMMY   | 37.80                    | 0 00:45                                  |                              |                      |                       |
| H101     | DUMMY   | 292.64                   | 0 02:03                                  |                              |                      |                       |
| HH100    | DUMMY   | 28.16                    | 0 00:40                                  |                              |                      |                       |
| I100     | DUMMY   | 78.06                    | 0 00:35                                  |                              |                      |                       |
| II100    | CONDUIT | 74.41                    | 0 00:56                                  | 9.49                         | 0.25                 | 0.54                  |
| II200    | CONDUIT | 116.09                   | 0 00:42                                  | 9.17                         | 0.54                 | 0.77                  |
| II300    | CONDUIT | 58.55                    | 0 00:41                                  | 9.88                         | 0.20                 | 0.50                  |
| IRR_J100 | DUMMY   | 274.80                   | 0 02:06                                  |                              |                      |                       |
| J1100    | DUMMY   | 230.44                   | 0 01:11                                  |                              |                      |                       |
| J1200    | CONDUIT | 107.12                   | 0 01:04                                  | 3.63                         | 0.03                 | 0.13                  |
| J1300    | CONDUIT | 53.90                    | 0 00:55                                  | 6.31                         | 0.33                 | 0.62                  |

|            |         |        |   |       |       |      |      |
|------------|---------|--------|---|-------|-------|------|------|
| J1400      | DUMMY   | 155.08 | 0 | 01:10 |       |      |      |
| J1500      | DUMMY   | 68.43  | 0 | 01:09 |       |      |      |
| J300       | CONDUIT | 45.89  | 0 | 01:51 | 2.49  | 0.32 | 0.61 |
| J400       | CONDUIT | 198.78 | 0 | 01:15 | 7.55  | 0.21 | 0.51 |
| J500       | DUMMY   | 139.06 | 0 | 01:02 |       |      |      |
| J600       | CONDUIT | 47.66  | 0 | 01:07 | 8.11  | 0.19 | 0.49 |
| J700       | CONDUIT | 238.60 | 0 | 00:32 | 25.63 | 0.03 | 0.27 |
| J800       | DUMMY   | 259.47 | 0 | 01:14 |       |      |      |
| J900       | DUMMY   | 221.14 | 0 | 01:17 |       |      |      |
| JJ100      | DUMMY   | 22.80  | 0 | 00:35 |       |      |      |
| JP20       | DUMMY   | 271.49 | 0 | 01:15 |       |      |      |
| K100       | CONDUIT | 381.85 | 0 | 00:36 | 16.23 | 0.38 | 0.66 |
| L100       | DUMMY   | 32.40  | 0 | 00:40 |       |      |      |
| LL100      | DUMMY   | 15.07  | 0 | 00:40 |       |      |      |
| N100       | CONDUIT | 139.56 | 0 | 00:37 | 5.09  | 0.48 | 0.72 |
| O100       | DUMMY   | 127.40 | 0 | 00:40 |       |      |      |
| P100       | DUMMY   | 82.83  | 0 | 00:45 |       |      |      |
| Q100       | DUMMY   | 137.80 | 0 | 00:45 |       |      |      |
| R100       | DUMMY   | 253.86 | 0 | 00:45 |       |      |      |
| S100       | DUMMY   | 58.96  | 0 | 00:35 |       |      |      |
| SP101      | CONDUIT | 511.87 | 0 | 01:16 | 5.57  | 0.14 | 0.35 |
| SP102      | CONDUIT | 600.43 | 0 | 01:20 | 3.41  | 0.36 | 0.59 |
| SP103      | CONDUIT | 640.21 | 0 | 01:22 | 9.89  | 0.05 | 0.21 |
| SP104      | CONDUIT | 705.93 | 0 | 01:22 | 6.50  | 0.11 | 0.32 |
| SP206      | DUMMY   | 242.18 | 0 | 01:16 |       |      |      |
| T100       | DUMMY   | 8.68   | 0 | 00:45 |       |      |      |
| T101       | DUMMY   | 228.33 | 0 | 01:17 |       |      |      |
| U100       | DUMMY   | 10.51  | 0 | 00:45 |       |      |      |
| V100       | DUMMY   | 27.67  | 0 | 00:40 |       |      |      |
| V200       | CONDUIT | 33.09  | 0 | 00:43 | 7.22  | 0.14 | 0.43 |
| W100       | DUMMY   | 7.46   | 0 | 00:40 |       |      |      |
| X100       | DUMMY   | 163.27 | 0 | 00:45 |       |      |      |
| X200       | CONDUIT | 81.91  | 0 | 00:43 | 7.13  | 0.16 | 0.45 |
| X300       | CONDUIT | 158.95 | 0 | 00:47 | 11.36 | 0.19 | 0.48 |
| I200       | DUMMY   | 63.72  | 0 | 00:55 |       |      |      |
| O12        | DUMMY   | 45.00  | 0 | 00:00 |       |      |      |
| KK100      | DUMMY   | 16.95  | 0 | 00:40 |       |      |      |
| LL200      | DUMMY   | 49.55  | 0 | 00:53 |       |      |      |
| IRR_OUTLET | DUMMY   | 274.80 | 0 | 02:06 |       |      |      |
| O1         | DUMMY   | 73.03  | 0 | 01:07 |       |      |      |
| O10        | DUMMY   | 33.90  | 0 | 01:09 |       |      |      |
| O11        | DUMMY   | 230.44 | 0 | 01:11 |       |      |      |
| O13        | DUMMY   | 54.35  | 0 | 00:51 |       |      |      |
| O14        | DUMMY   | 155.08 | 0 | 01:10 |       |      |      |
| O2         | DUMMY   | 74.57  | 0 | 01:38 |       |      |      |
| O3         | DUMMY   | 46.10  | 0 | 01:39 |       |      |      |
| O5         | DUMMY   | 103.73 | 0 | 00:52 |       |      |      |
| O6         | DUMMY   | 47.71  | 0 | 01:05 |       |      |      |
| O7         | DUMMY   | 234.87 | 0 | 00:31 |       |      |      |
| O8         | DUMMY   | 24.60  | 0 | 01:14 |       |      |      |

|     |       |        |   |       |
|-----|-------|--------|---|-------|
| 09  | DUMMY | 221.14 | 0 | 01:17 |
| 016 | DUMMY | 63.72  | 0 | 00:55 |
| 015 | DUMMY | 68.43  | 0 | 01:09 |
| 017 | DUMMY | 49.55  | 0 | 00:53 |
| 04  | DUMMY | 199.13 | 0 | 01:12 |

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#### Conduit Surcharge Summary

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No conduits were surcharged.

Analysis begun on: Thu Jul 28 14:48:24 2022

Analysis ended on: Thu Jul 28 14:48:24 2022

Total elapsed time: < 1 sec

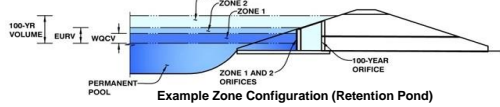
## Appendix D

# DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.04 (February 2021)

Project: **Flying Horse North Drainage Plan**

Basin ID: **Pond 1**



Example Zone Configuration (Retention Pond)

## Watershed Information

|   |            |         |
|---|------------|---------|
| Selected BMP Type =                     | <b>EDB</b> |         |
| Watershed Area =                        | 43.71      | acres   |
| Watershed Length =                      | 2,540      | ft      |
| Watershed Length to Centroid =          | 870        | ft      |
| Watershed Slope =                       | 0.046      | ft/ft   |
| Watershed Imperviousness =              | 34.30%     | percent |
| Percentage Hydrologic Soil Group A =    | 0.0%       | percent |
| Percentage Hydrologic Soil Group B =    | 100.0%     | percent |
| Percentage Hydrologic Soil Groups C/D = | 0.0%       | percent |
| Target WQCV Drain Time =                | 40.0       | hours   |
| Location for 1-hr Rainfall Depths =     | User Input |         |

After providing required inputs above including 1-hour rainfall depths, click "Run CUHP" to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

|  |       |           |
|--|-------|-----------|
| Water Quality Capture Volume (WQCV) =  | 0.598 | acre-feet |
| Excess Urban Runoff Volume (EURV) =    | 1.555 | acre-feet |
| 2-yr Runoff Volume (P1 = 0.92 in.) =   | 0.962 | acre-feet |
| 5-yr Runoff Volume (P1 = 1.2 in.) =    | 1.511 | acre-feet |
| 10-yr Runoff Volume (P1 = 1.45 in.) =  | 2.197 | acre-feet |
| 25-yr Runoff Volume (P1 = 1.69 in.) =  | 3.278 | acre-feet |
| 50-yr Runoff Volume (P1 = 2.15 in.) =  | 4.893 | acre-feet |
| 100-yr Runoff Volume (P1 = 2.49 in.) = | 6.323 | acre-feet |
| 500-yr Runoff Volume (P1 = 3.14 in.) = | 8.741 | acre-feet |
| Approximate 2-yr Detention Volume =    | 0.872 | acre-feet |
| Approximate 5-yr Detention Volume =    | 1.277 | acre-feet |
| Approximate 10-yr Detention Volume =   | 1.875 | acre-feet |
| Approximate 25-yr Detention Volume =   | 2.178 | acre-feet |
| Approximate 50-yr Detention Volume =   | 2.590 | acre-feet |
| Approximate 100-yr Detention Volume =  | 3.122 | acre-feet |

## Optional User Overrides

|  |      |           |
|--|------|-----------|
|  |      | acre-feet |
|  |      | acre-feet |
|  | 0.92 | inches    |
|  | 1.20 | inches    |
|  | 1.45 | inches    |
|  |      | inches    |
|  | 2.15 | inches    |
|  | 2.49 | inches    |
|  |      | inches    |

## Define Zones and Basin Geometry

|   |       |                 |
|---|-------|-----------------|
| Zone 1 Volume (WQCV) =                                  | 0.598 | acre-feet       |
| Zone 2 Volume (5-year - Zone 1) =                       | 0.679 | acre-feet       |
| Zone 3 Volume (100-year - Zones 1 & 2) =                | 1.845 | acre-feet       |
| Total Detention Basin Volume =                          | 3.122 | acre-feet       |
| Initial Surge Volume (ISV) =                            | 200   | ft <sup>3</sup> |
| Initial Surge Depth (ISD) =                             | 0.33  | ft              |
| Total Available Detention Depth (H <sub>total</sub> ) = | 6.00  | ft              |
| Depth of Trickle Channel (H <sub>TC</sub> ) =           | 0.50  | ft              |
| Slope of Trickle Channel (S <sub>TC</sub> ) =           | 0.004 | ft/ft           |
| Slopes of Main Basin Sides (S <sub>main</sub> ) =       | 4     | H:V             |
| Basin Length-to-Width Ratio (R <sub>LW</sub> ) =        | 2     |                 |

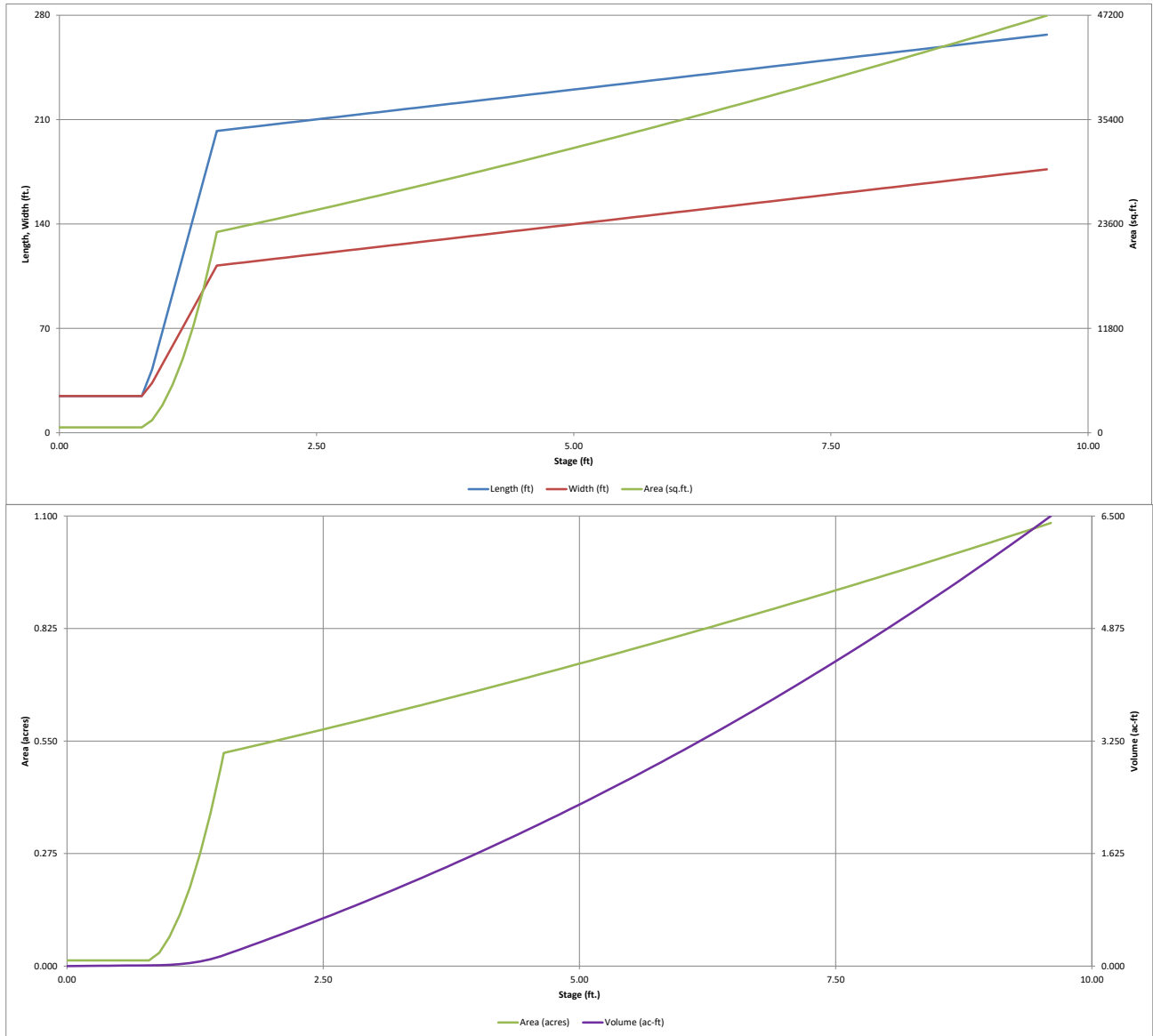
|   |              |                 |
|---|--------------|-----------------|
| Initial Surge Area (A <sub>ISV</sub> ) =              | 606          | ft <sup>2</sup> |
| Surcharge Volume Length (L <sub>ISV</sub> ) =         | 24.6         | ft              |
| Surcharge Volume Width (W <sub>ISV</sub> ) =          | 24.6         | ft              |
| Depth of Basin Floor (H <sub>FLOOR</sub> ) =          | 0.70         | ft              |
| Length of Basin Floor (L <sub>FLOOR</sub> ) =         | 202.4        | ft              |
| Width of Basin Floor (W <sub>FLOOR</sub> ) =          | 112.1        | ft              |
| Area of Basin Floor (A <sub>FLOOR</sub> ) =           | 22,695       | ft <sup>2</sup> |
| Volume of Basin Floor (V <sub>FLOOR</sub> ) =         | 6,302        | ft <sup>3</sup> |
| Depth of Main Basin (H <sub>MAIN</sub> ) =            | 4.47         | ft              |
| Length of Main Basin (L <sub>MAIN</sub> ) =           | 238.2        | ft              |
| Width of Main Basin (W <sub>MAIN</sub> ) =            | 147.9        | ft              |
| Area of Main Basin (A <sub>MAIN</sub> ) =             | 35,221       | ft <sup>2</sup> |
| Volume of Main Basin (V <sub>MAIN</sub> ) =           | 128,421      | ft <sup>3</sup> |
| Calculated Total Basin Volume (V <sub>total</sub> ) = | <b>3.104</b> | acre-feet       |

Depth Increment = 0.10 ft

| Stage - Storage Description | Stage (ft) | Optional Override Stage (ft) | Length (ft) | Width (ft) | Area (ft <sup>2</sup> ) | Optional Override Area (ft <sup>2</sup> ) | Area (acre) | Volume (ft <sup>3</sup> ) | Volume (ac-ft) |
|-----------------------------|------------|------------------------------|-------------|------------|-------------------------|---|-------------|---------------------------|----------------|
| <b>Top of Micropool</b>     | 0.00       |                              | 24.6        | 24.6       | 606                     |   | 0.014       |                           |                |
| <b>ISV</b>                  | 0.33       |                              | 24.6        | 24.6       | 606                     |   | 0.014       | 200                       | 0.005          |
|                             | 0.40       |                              | 24.6        | 24.6       | 606                     |   | 0.014       | 242                       | 0.006          |
|                             | 0.50       |                              | 24.6        | 24.6       | 606                     |   | 0.014       | 303                       | 0.007          |
|                             | 0.60       |                              | 24.6        | 24.6       | 606                     |   | 0.014       | 364                       | 0.008          |
|                             | 0.70       |                              | 24.6        | 24.6       | 606                     |   | 0.014       | 424                       | 0.010          |
|                             | 0.80       |                              | 24.6        | 24.6       | 606                     |   | 0.014       | 485                       | 0.011          |
|                             | 0.90       |                              | 42.4        | 33.4       | 1,415                   |   | 0.032       | 572                       | 0.013          |
|                             | 1.00       |                              | 67.8        | 45.9       | 3,110                   |   | 0.071       | 793                       | 0.018          |
|                             | 1.10       |                              | 93.2        | 58.4       | 5,440                   |   | 0.125       | 1,215                     | 0.028          |
|                             | 1.20       |                              | 118.6       | 70.9       | 8,405                   |   | 0.193       | 1,902                     | 0.044          |
|                             | 1.30       |                              | 144.0       | 83.4       | 12,005                  |   | 0.276       | 2,917                     | 0.067          |
|                             | 1.40       |                              | 169.4       | 95.9       | 16,240                  |   | 0.373       | 4,324                     | 0.099          |
|                             | 1.50       |                              | 194.8       | 108.4      | 21,110                  |   | 0.485       | 6,186                     | 0.142          |
| <b>Floor</b>                | 1.53       |                              | 202.4       | 112.1      | 22,695                  |   | 0.521       | 6,843                     | 0.157          |
|                             | 1.60       |                              | 203.0       | 112.7      | 22,871                  |   | 0.525       | 8,438                     | 0.194          |
|                             | 1.70       |                              | 203.8       | 113.5      | 23,124                  |   | 0.531       | 10,738                    | 0.247          |
|                             | 1.80       |                              | 204.6       | 114.3      | 23,379                  |   | 0.537       | 13,063                    | 0.300          |
|                             | 1.90       |                              | 205.4       | 115.1      | 23,635                  |   | 0.543       | 15,414                    | 0.354          |
|                             | 2.00       |                              | 206.2       | 115.9      | 23,892                  |   | 0.548       | 17,790                    | 0.408          |
|                             | 2.10       |                              | 207.0       | 116.7      | 24,150                  |   | 0.554       | 20,192                    | 0.464          |
|                             | 2.20       |                              | 207.8       | 117.5      | 24,409                  |   | 0.560       | 22,620                    | 0.519          |
|                             | 2.30       |                              | 208.6       | 118.3      | 24,670                  |   | 0.566       | 25,074                    | 0.576          |
| <b>Zone 1 (WQCV)</b>        | 2.34       |                              | 208.9       | 118.6      | 24,775                  |   | 0.569       | 26,063                    | 0.598          |
|                             | 2.40       |                              | 209.4       | 119.1      | 24,932                  |   | 0.572       | 27,554                    | 0.633          |
|                             | 2.50       |                              | 210.2       | 119.9      | 25,196                  |   | 0.578       | 30,060                    | 0.690          |
|                             | 2.60       |                              | 211.0       | 120.7      | 25,461                  |   | 0.584       | 32,593                    | 0.748          |
|                             | 2.70       |                              | 211.8       | 121.5      | 25,726                  |   | 0.591       | 35,153                    | 0.807          |
|                             | 2.80       |                              | 212.6       | 122.3      | 25,994                  |   | 0.597       | 37,739                    | 0.866          |
|                             | 2.90       |                              | 213.4       | 123.1      | 26,262                  |   | 0.603       | 40,351                    | 0.926          |
|                             | 3.00       |                              | 214.2       | 123.9      | 26,532                  |   | 0.609       | 42,991                    | 0.987          |
|                             | 3.10       |                              | 215.0       | 124.7      | 26,803                  |   | 0.615       | 45,658                    | 1.048          |
|                             | 3.20       |                              | 215.8       | 125.5      | 27,075                  |   | 0.622       | 48,352                    | 1.110          |
|                             | 3.30       |                              | 216.6       | 126.3      | 27,349                  |   | 0.628       | 51,073                    | 1.172          |
|                             | 3.40       |                              | 217.4       | 127.1      | 27,624                  |   | 0.634       | 53,822                    | 1.236          |
| <b>Zone 2 (5-year)</b>      | 3.47       |                              | 217.9       | 127.6      | 27,817                  |   | 0.639       | 55,762                    | 1.280          |
|                             | 3.50       |                              | 218.2       | 127.9      | 27,900                  |   | 0.641       | 56,598                    | 1.299          |
|                             | 3.60       |                              | 219.0       | 128.7      | 28,178                  |   | 0.647       | 59,402                    | 1.364          |
|                             | 3.70       |                              | 219.8       | 129.5      | 28,457                  |   | 0.653       | 62,233                    | 1.429          |
|                             | 3.80       |                              | 220.6       | 130.3      | 28,737                  |   | 0.660       | 65,093                    | 1.494          |
|                             | 3.90       |                              | 221.4       | 131.1      | 29,018                  |   | 0.666       | 67,981                    | 1.561          |
|                             | 4.00       |                              | 222.2       | 131.9      | 29,300                  |   | 0.673       | 70,897                    | 1.628          |
|                             | 4.10       |                              | 223.0       | 132.7      | 29,584                  |   | 0.679       | 73,841                    | 1.695          |
|                             | 4.20       |                              | 223.8       | 133.5      | 29,870                  |   | 0.686       | 76,814                    | 1.763          |
|                             | 4.30       |                              | 224.6       | 134.3      | 30,156                  |   | 0.692       | 79,815                    | 1.832          |
|                             | 4.40       |                              | 225.4       | 135.1      | 30,444                  |   | 0.699       | 82,845                    | 1.902          |
|                             | 4.50       |                              | 226.2       | 135.9      | 30,733                  |   | 0.706       | 85,904                    | 1.972          |
|                             | 4.60       |                              | 227.0       | 136.7      | 31,023                  |   | 0.712       | 88,991                    | 2.043          |
|                             | 4.70       |                              | 227.8       | 137.5      | 31,315                  |   | 0.719       | 92,108                    | 2.115          |
|                             | 4.80       |                              | 228.6       | 138.3      | 31,607                  |   | 0.726       | 95,254                    | 2.187          |
|                             | 4.90       |                              | 229.4       | 139.1      | 31,902                  |   | 0.732       | 98,430                    | 2.260          |
|                             | 5.00       |                              | 230.2       | 139.9      | 32,197                  |   | 0.739       | 101,635                   | 2.333          |
|                             | 5.10       |                              | 231.0       | 140.7      | 32,494                  |   | 0.746       | 104,869                   | 2.407          |
|                             | 5.20       |                              | 231.8       | 141.5      | 32,792                  |   | 0.753       | 108,134                   | 2.482          |
|                             | 5.30       |                              | 232.6       | 142.3      | 33,091                  |   | 0.760       | 111,428                   | 2.558          |
|                             | 5.40       |                              | 233.4       | 143.1      | 33,391                  |   | 0.767       | 114,752                   | 2.634          |
|                             | 5.50       |                              | 234.2       | 143.9      | 33,693                  |   | 0.773       | 118,106                   | 2.711          |
|                             | 5.60       |                              | 235.0       | 144.7      | 33,996                  |   | 0.780       | 121,490                   | 2.789          |
|                             | 5.70       |                              | 235.8       | 145.5      | 34,301                  |   | 0.787       | 124,905                   | 2.867          |
|                             | 5.80       |                              | 236.6       | 146.3      | 34,606                  |   | 0.794       | 128,351                   | 2.947          |
|                             | 5.90       |                              | 237.4       | 147.1      | 34,913                  |   | 0.801       | 131,827                   | 3.026          |
|                             | 6.00       |                              | 238.2       | 147.9      | 35,221                  |   | 0.809       | 135,333                   | 3.107          |
| <b>Zone 3 (100-year)</b>    | 6.02       |                              | 238.3       | 148.0      | 35,283                  |   | 0.810       | 136,038                   | 3.123          |
|                             | 6.10       |                              | 239.0       | 148.7      | 35,531                  |   | 0.816       | 138,871                   | 3.188          |
|                             | 6.20       |                              | 239.8       | 149.5      | 35,842                  |   | 0.823       | 142,440                   | 3.270          |
|                             | 6.30       |                              | 240.6       | 150.3      | 36,154                  |   | 0.830       | 146,039                   | 3.353          |
|                             | 6.40       |                              | 241.4       | 151.1      | 36,467                  |   | 0.837       | 149,670                   | 3.436          |
|                             | 6.50       |                              | 242.2       | 151.9      | 36,782                  |   | 0.844       | 153,333                   | 3.520          |
|                             | 6.60       |                              | 243.0       | 152.7      | 37,098                  |   | 0.852       | 157,027                   | 3.605          |
|                             | 6.70       |                              | 243.8       | 153.5      | 37,415                  |   | 0.859       | 160,752                   | 3.690          |
|                             | 6.80       |                              | 244.6       | 154.3      | 37,733                  |   | 0.866       | 164,510                   | 3.777          |
|                             | 6.90       |                              | 245.4       | 155.1      | 38,053                  |   | 0.874       | 168,299                   | 3.864          |
|                             | 7.00       |                              | 246.2       | 155.9      | 38,374                  |   | 0.881       | 172,120                   | 3.951          |
|                             | 7.10       |                              | 247.0       | 156.7      | 38,696                  |   | 0.888       | 175,974                   | 4.040          |
|                             | 7.20       |                              | 247.8       | 157.5      | 39,020                  |   | 0.896       | 179,860                   | 4.129          |
|                             | 7.30       |                              | 248.6       | 158.3      | 39,345                  |   | 0.903       | 183,778                   | 4.219          |
|                             | 7.40       |                              | 249.4       | 159.1      | 39,671                  |   | 0.911       | 187,728                   | 4.310          |
|                             | 7.50       |                              | 250.2       | 159.9      | 39,998                  |   | 0.918       | 191,712                   | 4.401          |
|                             | 7.60       |                              | 251.0       | 160.7      | 40,327                  |   | 0.926       | 195,728                   | 4.493          |
|                             | 7.70       |                              | 251.8       | 161.5      | 40,657                  |   | 0.933       | 199,777                   | 4.586          |
|                             | 7.80       |                              | 252.6       | 162.3      | 40,988                  |   | 0.941       | 203,860                   | 4.680          |
|                             | 7.90       |                              | 253.4       | 163.1      | 41,321                  |   | 0.949       | 207,975                   | 4.774          |
|                             | 8.00       |                              | 254.2       | 163.9      | 41,654                  |   | 0.956       | 212,124                   | 4.870          |
|                             | 8.10       |                              | 255.0       | 164.7      | 41,989                  |   | 0.964       | 216,306                   | 4.966          |
|                             | 8.20       |                              | 255.8       | 165.5      | 42,326                  |   | 0.972       | 220,522                   | 5.062          |
|                             | 8.30       |                              | 256.6       | 166.3      | 42,663                  |   | 0.979       | 224,771                   | 5.160          |
|                             | 8.40       |                              | 257.4       | 167.1      | 43,002                  |   | 0.987       | 229,054                   | 5.258          |
|                             | 8.50       |                              | 258.2       | 167.9      | 43,343                  |   | 0.995       | 233,372                   | 5.357          |
|                             | 8.60       |                              | 259.0       | 168.7      | 43,684                  |   | 1.003       | 237,723                   | 5.457          |
|                             | 8.70       |                              | 259.8       | 169.5      | 44,027                  |   | 1.011       | 242,108                   | 5.558          |
|                             | 8.80       |                              | 260.6       | 170.3      | 44,371                  |   | 1.019       | 246,528                   | 5.660          |
|                             | 8.90       |                              | 261.4       | 171.1      | 44,716                  |   | 1.027       | 250,983                   | 5.762          |
|                             | 9.00       |                              | 262.2       | 171.9      | 45,063                  |   | 1.034       | 255,472                   | 5.865          |
|                             | 9.10       |                              | 263.0       | 172.7      | 45,411                  |   | 1.042       | 259,995                   | 5.969          |
|                             | 9.20       |                              | 263.8       | 173.5      | 45,760                  |   | 1.051       | 264,554                   | 6.073          |
|                             | 9.30       |                              | 264.6       | 174.3      | 46,110                  |   | 1.059       | 269,147                   | 6.179          |
|                             | 9.40       |                              | 265.4       | 175.1      | 46,462                  |   | 1.067       | 273,776                   | 6.285          |
|                             | 9.50       |                              | 266.2       | 175.9      | 46,815                  |   | 1.075       | 278,440                   | 6.392          |
|                             | 9.60       |                              | 267.0       | 176.7      | 47,169                  |   | 1.083       | 283,139                   | 6.500          |

# DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.04 (February 2021)



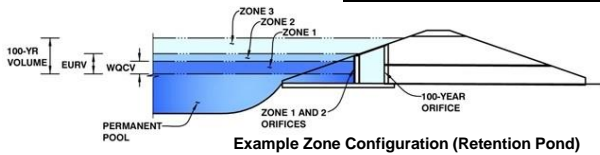


# DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-DETENTION, Version 4.04 (February 2021)

Project: Flying Horse North Drainage Plan

Basin ID: Pond 1



Example Zone Configuration (Retention Pond)

|                   | Estimated Stage (ft) | Estimated Volume (ac-ft) | Outlet Type          |
|-------------------|----------------------|--------------------------|----------------------|
| Zone 1 (WQCV)     | 2.34                 | 0.598                    | Orifice Plate        |
| Zone 2 (5-year)   | 3.47                 | 0.679                    | Weir&Pipe (Circular) |
| Zone 3 (100-year) | 6.02                 | 1.845                    | Weir&Pipe (Restrict) |
| Total (all zones) |                      | 3.122                    |                      |

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth = N/A ft (distance below the filtration media surface)  
Underdrain Orifice Diameter = N/A inches

Calculated Parameters for Underdrain  
Underdrain Orifice Area = N/A ft<sup>2</sup>  
Underdrain Orifice Centroid = N/A feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice = 0.00 ft (relative to basin bottom at Stage = 0 ft)  
Depth at top of Zone using Orifice Plate = 2.34 ft (relative to basin bottom at Stage = 0 ft)  
Orifice Plate: Orifice Vertical Spacing = 9.40 inches  
Orifice Plate: Orifice Area per Row = 2.12 sq. inches (diameter = 1-5/8 inches)

Calculated Parameters for Plate  
WQ Orifice Area per Row = 1.472E-02 ft<sup>2</sup>  
Elliptical Half-Width = N/A feet  
Elliptical Slot Centroid = N/A feet  
Elliptical Slot Area = N/A ft<sup>2</sup>

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

|                                | Row 1 (required) | Row 2 (optional) | Row 3 (optional) | Row 4 (optional) | Row 5 (optional) | Row 6 (optional) | Row 7 (optional) | Row 8 (optional) |
|--------------------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|
| Stage of Orifice Centroid (ft) | 0.00             | 0.78             | 1.56             |                  |                  |                  |                  |                  |
| Orifice Area (sq. inches)      | 2.12             | 2.12             | 2.12             |                  |                  |                  |                  |                  |

|                                | Row 9 (optional) | Row 10 (optional) | Row 11 (optional) | Row 12 (optional) | Row 13 (optional) | Row 14 (optional) | Row 15 (optional) | Row 16 (optional) |
|--------------------------------|------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| Stage of Orifice Centroid (ft) |                  |                   |                   |                   |                   |                   |                   |                   |
| Orifice Area (sq. inches)      |                  |                   |                   |                   |                   |                   |                   |                   |

User Input: Vertical Orifice (Circular or Rectangular)

|   | Not Selected | Not Selected |
|---|--------------|--------------|
| Invert of Vertical Orifice =                  | N/A          | N/A          |
| Depth at top of Zone using Vertical Orifice = | N/A          | N/A          |
| Vertical Orifice Diameter =                   | N/A          | N/A          |

ft (relative to basin bottom at Stage = 0 ft)  
ft (relative to basin bottom at Stage = 0 ft)  
inches

Calculated Parameters for Vertical Orifice  
Vertical Orifice Area = N/A ft<sup>2</sup>  
Vertical Orifice Centroid = N/A feet

User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe))

|                                       | Zone 2 Weir  | Zone 3 Weir  |
|---------------------------------------|--------------|--------------|
| Overflow Weir Front Edge Height, Ho = | 2.34         | 3.47         |
| Overflow Weir Front Edge Length =     | 6.00         | 6.00         |
| Overflow Weir Grate Slope =           | 0.00         | 0.00         |
| Horiz. Length of Weir Sides =         | 6.00         | 6.00         |
| Overflow Grate Type =                 | Type C Grate | Type C Grate |
| Debris Clogging % =                   | 50%          | 50%          |

ft (relative to basin bottom at Stage = 0 ft)  
feet  
H:V  
feet  
Type C Grate  
%

Calculated Parameters for Overflow Weir  
Height of Grate Upper Edge, H<sub>u</sub> = 2.34 feet  
Overflow Weir Slope Length = 6.00 feet  
Grate Open Area / 100-yr Orifice Area = 9.49  
Overflow Grate Open Area w/o Debris = 25.06 ft<sup>2</sup>  
Overflow Grate Open Area w/ Debris = 12.53 ft<sup>2</sup>

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

|  | Zone 2 Circular | Zone 3 Restrictor |
|--|-----------------|-------------------|
| Depth to Invert of Outlet Pipe =             | 2.50            | 2.70              |
| Circular Orifice Diameter or Pipe Diameter = | 22.00           | 36.00             |
| Restrictor Plate Height Above Pipe Invert =  |                 | 33.00             |

ft (distance below basin bottom at Stage = 0 ft)  
inches  
inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate  
Outlet Orifice Area = 2.64 ft<sup>2</sup>  
Outlet Orifice Centroid = 0.92 feet  
Half-Central Angle of Restrictor Plate on Pipe = N/A radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage = 5.00 ft (relative to basin bottom at Stage = 0 ft)  
Spillway Crest Length = 27.00 feet  
Spillway End Slopes = 4.00 H:V  
Freeboard above Max Water Surface = 1.00 feet

Calculated Parameters for Spillway  
Spillway Design Flow Depth = 0.93 feet  
Stage at Top of Freeboard = 6.93 feet  
Basin Area at Top of Freeboard = 0.88 acres  
Basin Volume at Top of Freeboard = 3.89 acre-ft

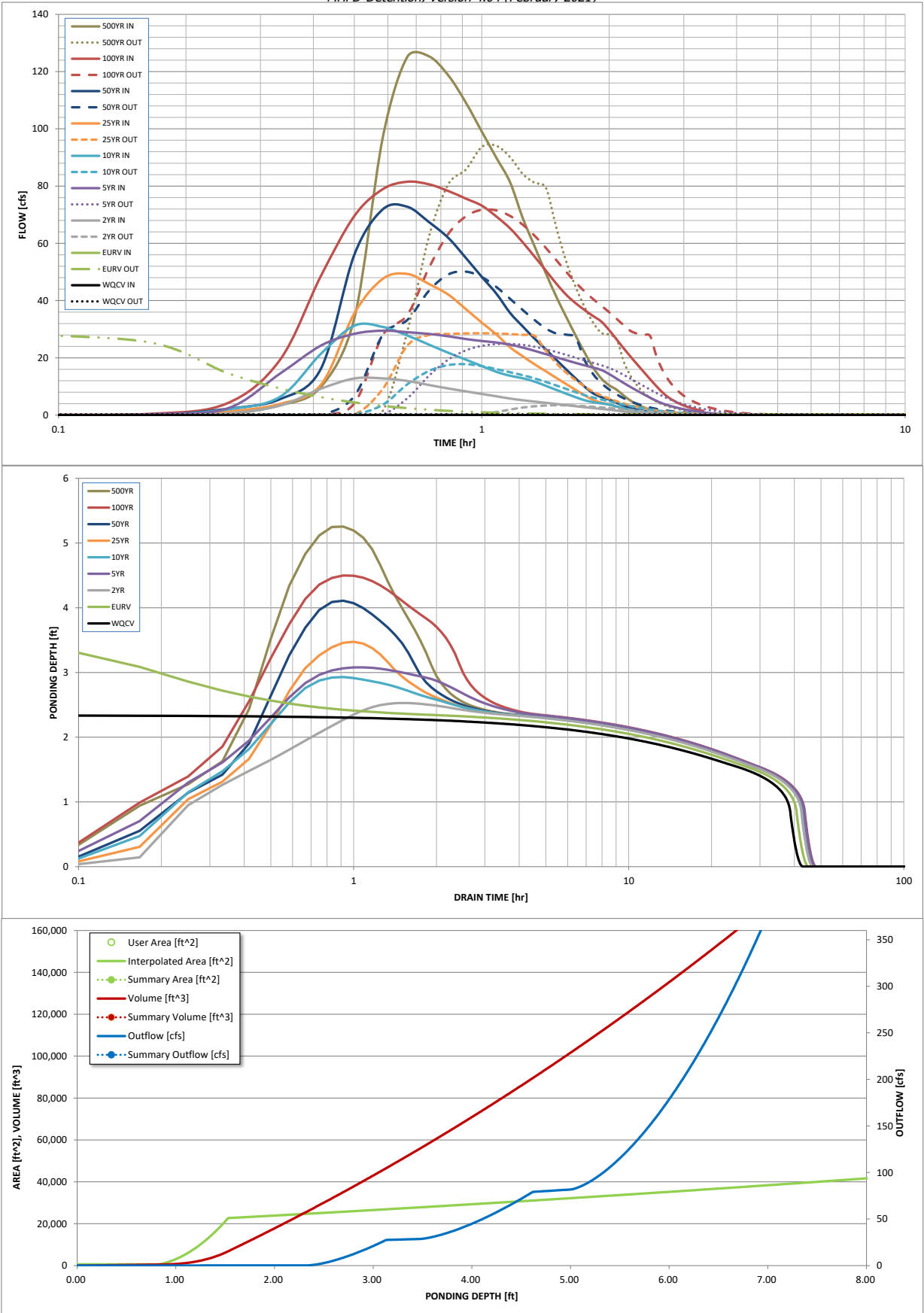
## Routed Hydrograph Results

The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).

|  | WQCV            | EURV            | 2 Year          | 5 Year          | 10 Year         | 25 Year         | 50 Year         | 100 Year        | 500 Year |
|--|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|----------|
| Design Storm Return Period =                       | N/A             | N/A             | 0.92            | 1.20            | 1.45            | 1.69            | 2.15            | 2.49            | 3.14     |
| One-Hour Rainfall Depth (in) =                     | 0.598           | 1.555           | 0.962           | 1.511           | 2.197           | 3.278           | 4.893           | 6.323           | 8.741    |
| CUHP Runoff Volume (acre-ft) =                     | N/A             | N/A             | 0.962           | 3.851           | 2.197           | 3.278           | 4.893           | 9.206           | 8.741    |
| User Override Inflow Hydrograph Volume (acre-ft) = | N/A             | N/A             | 0.5             | 3.9             | 11.5            | 26.5            | 44.5            | 60.8            | 86.2     |
| CUHP Predevelopment Peak Q (cfs) =                 | N/A             | N/A             | 0.01            | 0.64            | 0.26            | 0.61            | 1.02            | 1.85            | 1.97     |
| OPTIONAL Override Predevelopment Peak Q (cfs) =    | N/A             | N/A             | 12.8            | 29.5            | 31.3            | 49.3            | 72.8            | 81.5            | 125.3    |
| Predevelopment Unit Peak Flow, q (cfs/acre) =      | N/A             | N/A             | 3.4             | 24.9            | 17.8            | 28.6            | 50.1            | 71.7            | 94.0     |
| Peak Inflow Q (cfs) =                              | N/A             | N/A             | 0.9             | 1.6             | 1.1             | 1.1             | 1.1             | 0.9             | 1.1      |
| Peak Outflow Q (cfs) =                             | N/A             | N/A             | 0.13            | 1.0             | 0.7             | 1.1             | 1.2             | 1.2             | 1.3      |
| Ratio Peak Outflow to Predevelopment Q =           | N/A             | N/A             | N/A             | N/A             | N/A             | 0.0             | 0.8             | 1.6             | 2.0      |
| Structure Controlling Flow =                       | Overflow Weir 1 | Overflow Weir 2 | Overflow Weir 1 | Overflow Weir 1 | Overflow Weir 1 | Overflow Weir 2 | Overflow Weir 2 | Overflow Weir 2 | Spillway |
| Max Velocity through Grate 1 (fps) =               | N/A             | 1.17            | 0.44            | N/A             | N/A             | N/A             | 0.8             | 1.6             | 2.0      |
| Max Velocity through Grate 2 (fps) =               | N/A             | 0.44            | 0.41            | 0.41            | 0.41            | 0.41            | 0.41            | 0.41            | 0.41     |
| Time to Drain 97% of Inflow Volume (hours) =       | 38              | 37              | 41              | 34              | 37              | 34              | 30              | 22              | 22       |
| Time to Drain 99% of Inflow Volume (hours) =       | 40              | 41              | 43              | 41              | 42              | 40              | 39              | 36              | 35       |
| Maximum Ponding Depth (ft) =                       | 2.34            | 3.90            | 2.53            | 3.08            | 2.93            | 3.48            | 4.11            | 4.50            | 5.25     |
| Area at Maximum Ponding Depth (acres) =            | 0.57            | 0.67            | 0.58            | 0.61            | 0.60            | 0.64            | 0.68            | 0.70            | 0.76     |
| Maximum Volume Stored (acre-ft) =                  | 0.598           | 1.561           | 0.702           | 1.030           | 0.938           | 1.280           | 1.695           | 1.965           | 2.520    |

DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD- Detention, Version 4.04 (February 2021)



| S-A-V-D Chart Axis Override | X-axis | Left Y-Axis | Right Y-Axis |
|-----------------------------|--------|-------------|--------------|
| minimum bound               |        |             |              |
| maximum bound               |        |             |              |

# DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename: ...[SWM]Outflow hydrographs[Pond6 OutflowHydrograph.xlsx

## Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

|               | SOURCE  | CUHP       | CUHP       | CUHP         | USER         | CUHP          | CUHP          | CUHP          | USER           | CUHP           |
|---------------|---------|------------|------------|--------------|--------------|---------------|---------------|---------------|----------------|----------------|
| Time Interval | TIME    | WQCV [cfs] | EURV [cfs] | 2 Year [cfs] | 5 Year [cfs] | 10 Year [cfs] | 25 Year [cfs] | 50 Year [cfs] | 100 Year [cfs] | 500 Year [cfs] |
| 5.00 min      | 0:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 0:05:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.08           | 0.00           |
|               | 0:10:00 | 0.00       | 0.00       | 0.00         | 0.33         | 0.00          | 0.00          | 0.06          | 0.49           | 0.51           |
|               | 0:15:00 | 0.00       | 0.00       | 0.60         | 2.28         | 1.96          | 1.28          | 2.18          | 4.09           | 3.39           |
|               | 0:20:00 | 0.00       | 0.00       | 3.35         | 14.46        | 6.37          | 3.91          | 5.55          | 19.23          | 9.84           |
|               | 0:25:00 | 0.00       | 0.00       | 9.22         | 24.28        | 21.41         | 10.60         | 16.17         | 48.59          | 33.82          |
|               | 0:30:00 | 0.00       | 0.00       | 12.81        | 28.40        | 31.25         | 35.56         | 56.08         | 69.57          | 96.85          |
|               | 0:35:00 | 0.00       | 0.00       | 12.83        | 29.49        | 30.81         | 47.58         | 71.86         | 78.91          | 125.12         |
|               | 0:40:00 | 0.00       | 0.00       | 11.94        | 28.96        | 27.81         | 49.32         | 72.78         | 81.52          | 125.34         |
|               | 0:45:00 | 0.00       | 0.00       | 10.52        | 28.36        | 24.63         | 45.81         | 67.44         | 80.62          | 118.69         |
|               | 0:50:00 | 0.00       | 0.00       | 9.31         | 27.54        | 21.78         | 42.11         | 61.92         | 78.29          | 109.19         |
|               | 0:55:00 | 0.00       | 0.00       | 8.31         | 26.58        | 19.39         | 37.05         | 54.93         | 75.63          | 99.04          |
|               | 1:00:00 | 0.00       | 0.00       | 7.39         | 25.89        | 17.15         | 32.31         | 48.29         | 73.17          | 89.80          |
|               | 1:05:00 | 0.00       | 0.00       | 6.57         | 25.36        | 15.10         | 28.14         | 42.37         | 69.34          | 81.30          |
|               | 1:10:00 | 0.00       | 0.00       | 5.78         | 24.60        | 13.74         | 23.67         | 35.68         | 65.22          | 68.77          |
|               | 1:15:00 | 0.00       | 0.00       | 5.19         | 23.58        | 12.87         | 20.54         | 30.96         | 60.34          | 58.88          |
|               | 1:20:00 | 0.00       | 0.00       | 4.72         | 22.44        | 11.71         | 17.74         | 26.69         | 55.32          | 49.58          |
|               | 1:25:00 | 0.00       | 0.00       | 4.30         | 21.29        | 10.22         | 15.33         | 22.96         | 50.50          | 41.35          |
|               | 1:30:00 | 0.00       | 0.00       | 3.90         | 20.22        | 8.81          | 12.98         | 19.31         | 45.93          | 34.25          |
|               | 1:35:00 | 0.00       | 0.00       | 3.50         | 19.18        | 7.48          | 10.83         | 15.93         | 42.03          | 27.75          |
|               | 1:40:00 | 0.00       | 0.00       | 3.10         | 18.23        | 6.26          | 8.80          | 12.80         | 39.09          | 21.80          |
|               | 1:45:00 | 0.00       | 0.00       | 2.74         | 17.37        | 5.19          | 6.92          | 9.92          | 36.69          | 16.59          |
|               | 1:50:00 | 0.00       | 0.00       | 2.47         | 16.59        | 4.51          | 5.28          | 7.60          | 34.59          | 12.76          |
|               | 1:55:00 | 0.00       | 0.00       | 2.15         | 15.76        | 4.08          | 4.33          | 6.29          | 32.67          | 10.41          |
|               | 2:00:00 | 0.00       | 0.00       | 1.92         | 14.33        | 3.68          | 3.77          | 5.47          | 29.67          | 8.86           |
|               | 2:05:00 | 0.00       | 0.00       | 1.57         | 12.73        | 2.99          | 2.96          | 4.27          | 26.39          | 6.77           |
|               | 2:10:00 | 0.00       | 0.00       | 1.26         | 11.19        | 2.37          | 2.26          | 3.25          | 23.24          | 5.00           |
|               | 2:15:00 | 0.00       | 0.00       | 1.00         | 9.75         | 1.86          | 1.75          | 2.49          | 20.31          | 3.66           |
|               | 2:20:00 | 0.00       | 0.00       | 0.80         | 8.45         | 1.45          | 1.34          | 1.88          | 17.59          | 2.65           |
|               | 2:25:00 | 0.00       | 0.00       | 0.63         | 7.22         | 1.11          | 1.02          | 1.42          | 15.00          | 1.96           |
|               | 2:30:00 | 0.00       | 0.00       | 0.49         | 6.07         | 0.84          | 0.78          | 1.08          | 12.51          | 1.47           |
|               | 2:35:00 | 0.00       | 0.00       | 0.39         | 5.01         | 0.63          | 0.58          | 0.80          | 10.17          | 1.11           |
|               | 2:40:00 | 0.00       | 0.00       | 0.30         | 4.14         | 0.48          | 0.44          | 0.60          | 8.06           | 0.85           |
|               | 2:45:00 | 0.00       | 0.00       | 0.23         | 3.47         | 0.37          | 0.34          | 0.46          | 6.38           | 0.65           |
|               | 2:50:00 | 0.00       | 0.00       | 0.17         | 2.93         | 0.27          | 0.25          | 0.34          | 5.13           | 0.48           |
|               | 2:55:00 | 0.00       | 0.00       | 0.12         | 2.46         | 0.19          | 0.18          | 0.24          | 4.15           | 0.34           |
|               | 3:00:00 | 0.00       | 0.00       | 0.08         | 2.06         | 0.13          | 0.12          | 0.16          | 3.36           | 0.22           |
|               | 3:05:00 | 0.00       | 0.00       | 0.05         | 1.73         | 0.07          | 0.07          | 0.09          | 2.73           | 0.12           |
|               | 3:10:00 | 0.00       | 0.00       | 0.03         | 1.45         | 0.04          | 0.04          | 0.05          | 2.23           | 0.06           |
|               | 3:15:00 | 0.00       | 0.00       | 0.01         | 1.20         | 0.01          | 0.01          | 0.01          | 1.81           | 0.02           |
|               | 3:20:00 | 0.00       | 0.00       | 0.00         | 0.98         | 0.00          | 0.00          | 0.00          | 1.48           | 0.00           |
|               | 3:25:00 | 0.00       | 0.00       | 0.00         | 0.79         | 0.00          | 0.00          | 0.00          | 1.20           | 0.00           |
|               | 3:30:00 | 0.00       | 0.00       | 0.00         | 0.62         | 0.00          | 0.00          | 0.00          | 0.97           | 0.00           |
|               | 3:35:00 | 0.00       | 0.00       | 0.00         | 0.48         | 0.00          | 0.00          | 0.00          | 0.76           | 0.00           |
|               | 3:40:00 | 0.00       | 0.00       | 0.00         | 0.35         | 0.00          | 0.00          | 0.00          | 0.59           | 0.00           |
|               | 3:45:00 | 0.00       | 0.00       | 0.00         | 0.25         | 0.00          | 0.00          | 0.00          | 0.43           | 0.00           |
|               | 3:50:00 | 0.00       | 0.00       | 0.00         | 0.17         | 0.00          | 0.00          | 0.00          | 0.30           | 0.00           |
|               | 3:55:00 | 0.00       | 0.00       | 0.00         | 0.11         | 0.00          | 0.00          | 0.00          | 0.19           | 0.00           |
|               | 4:00:00 | 0.00       | 0.00       | 0.00         | 0.06         | 0.00          | 0.00          | 0.00          | 0.11           | 0.00           |
|               | 4:05:00 | 0.00       | 0.00       | 0.00         | 0.03         | 0.00          | 0.00          | 0.00          | 0.05           | 0.00           |
|               | 4:10:00 | 0.00       | 0.00       | 0.00         | 0.01         | 0.00          | 0.00          | 0.00          | 0.01           | 0.00           |
|               | 4:15:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:20:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:25:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:30:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:35:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:40:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:45:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:50:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:55:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:05:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:10:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:15:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:20:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:25:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:30:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:35:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:40:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:45:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:50:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:55:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 6:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |

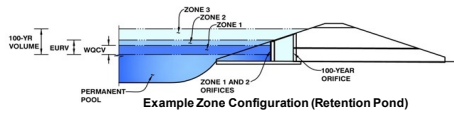
0 5:50:00 0

# DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.04 (February 2021)

Project: Flying Horse North MDDP

Basin ID: Pond 2



Example Zone Configuration (Retention Pond)

## Watershed Information

|   |                           |
|---|---------------------------|
| Selected BMP Type =                     | EDB                       |
| Watershed Area =                        | 76.38 acres               |
| Watershed Length =                      | 3,200 ft                  |
| Watershed Length to Centroid =          | 1,813 ft                  |
| Watershed Slope =                       | 0.046 ft/ft               |
| Watershed Imperviousness =              | 29.50% percent            |
| Percentage Hydrologic Soil Group A =    | 0.0% percent              |
| Percentage Hydrologic Soil Group B =    | 100.0% percent            |
| Percentage Hydrologic Soil Groups C/D = | 0.0% percent              |
| Target WQCV Drain Time =                | 40.0 hours                |
| Location for 1-hr Rainfall Depths =     | Denver - Capitol Building |

After providing required inputs above including 1-hour rainfall depths, click "Run CUHP" to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

|  |                  |
|--|------------------|
| Water Quality Capture Volume (WQCV) =  | 0.954 acre-feet  |
| Excess Urban Runoff Volume (EURV) =    | 2.309 acre-feet  |
| 2-yr Runoff Volume (P1 = 1.19 in.) =   | 2.348            |
| 5-yr Runoff Volume (P1 = 1.5 in.) =    | 3.828 acre-feet  |
| 10-yr Runoff Volume (P1 = 1.75 in.) =  | 5.193 acre-feet  |
| 25-yr Runoff Volume (P1 = 2 in.) =     | 7.260 acre-feet  |
| 50-yr Runoff Volume (P1 = 2.25 in.) =  | 8.821 acre-feet  |
| 100-yr Runoff Volume (P1 = 2.52 in.) = | 10.908 acre-feet |
| 500-yr Runoff Volume (P1 = 3.14 in.) = | 14.934 acre-feet |
| Approximate 2-yr Detention Volume =    | 1.649 acre-feet  |
| Approximate 5-yr Detention Volume =    | 2.363 acre-feet  |
| Approximate 10-yr Detention Volume =   | 3.460 acre-feet  |
| Approximate 25-yr Detention Volume =   | 4.023 acre-feet  |
| Approximate 50-yr Detention Volume =   | 4.239 acre-feet  |
| Approximate 100-yr Detention Volume =  | 5.021 acre-feet  |

## Optional User Overrides

|      |           |
|------|-----------|
|      | acre-feet |
|      | acre-feet |
| 1.19 | inches    |
| 1.50 | inches    |
| 1.75 | inches    |
| 2.00 | inches    |
| 2.25 | inches    |
| 2.52 | inches    |
|      | inches    |

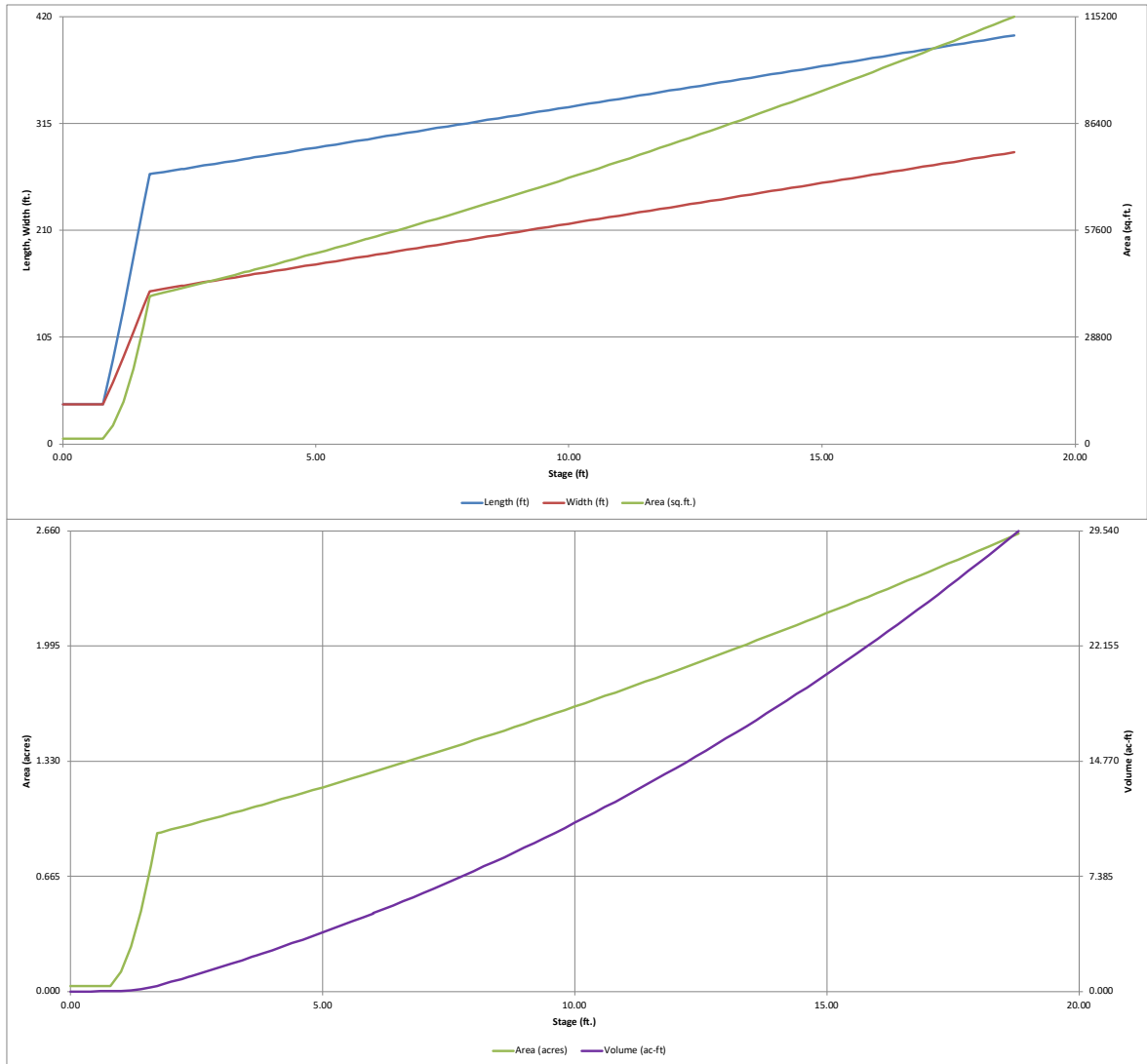
## Define Zones and Basin Geometry

|   |                         |
|---|-------------------------|
| Zone 1 Volume (WQCV) =                                  | 0.954 acre-feet         |
| Zone 2 Volume (EURV - Zone 1) =                         | 1.355 acre-feet         |
| Zone 3 Volume (100-year - Zones 1 & 2) =                | 2.712 acre-feet         |
| Total Detention Basin Volume =                          | 5.021 acre-feet         |
| Initial Surcharge Volume (ISV) =                        | 500 ft <sup>3</sup>     |
| Initial Surcharge Depth (ISD) =                         | 0.33 ft                 |
| Total Available Detention Depth (H <sub>total</sub> ) = | 6.00 ft                 |
| Depth of Trickle Channel (H <sub>tr</sub> ) =           | 0.50 ft                 |
| Slope of Trickle Channel (S <sub>tr</sub> ) =           | 0.004 ft/ft             |
| Slopes of Main Basin Sides (S <sub>main</sub> ) =       | 4 ft:H                  |
| Basin Length-to-Width Ratio (R <sub>L/W</sub> ) =       | 2                       |
| Initial Surcharge Area (A <sub>ISV</sub> ) =            | 1,515 ft <sup>2</sup>   |
| Surcharge Volume Length (L <sub>ISV</sub> ) =           | 38.9 ft                 |
| Surcharge Volume Width (W <sub>ISV</sub> ) =            | 38.9 ft                 |
| Depth of Basin Floor (H <sub>floor</sub> ) =            | 0.89 ft                 |
| Length of Basin Floor (L <sub>floor</sub> ) =           | 265.0 ft                |
| Width of Basin Floor (W <sub>floor</sub> ) =            | 150.2 ft                |
| Area of Basin Floor (A <sub>floor</sub> ) =             | 39,794 ft <sup>2</sup>  |
| Volume of Basin Floor (V <sub>floor</sub> ) =           | 14,559 ft <sup>3</sup>  |
| Depth of Main Basin (H <sub>main</sub> ) =              | 4.28 ft                 |
| Length of Main Basin (L <sub>main</sub> ) =             | 299.2 ft                |
| Width of Main Basin (W <sub>main</sub> ) =              | 184.4 ft                |
| Area of Main Basin (A <sub>main</sub> ) =               | 55,182 ft <sup>2</sup>  |
| Volume of Main Basin (V <sub>main</sub> ) =             | 202,353 ft <sup>3</sup> |
| Calculated Total Basin Volume (V <sub>total</sub> ) =   | 5,008 acre-feet         |

|                             |            |                              |             |            |                         |   |             |                           |                |
|-----------------------------|------------|------------------------------|-------------|------------|-------------------------|---|-------------|---------------------------|----------------|
| Depth Increment =           | 0.20       | ft                           |             |            |                         |   |             |                           |                |
| Stage - Storage Description | Stage (ft) | Optional Override Stage (ft) | Length (ft) | Width (ft) | Area (ft <sup>2</sup> ) | Optional Override Area (ft <sup>2</sup> ) | Area (acre) | Volume (ft <sup>3</sup> ) | Volume (ac-ft) |
| Top of Micropool            | 0.00       |                              | 38.9        | 38.9       | 1,515                   |   | 0.035       |                           |                |
| ISV                         | 0.33       |                              | 38.9        | 38.9       | 1,515                   |   | 0.035       | 500                       | 0.011          |
|                             | 0.40       |                              | 38.9        | 38.9       | 1,515                   |   | 0.035       | 606                       | 0.014          |
|                             | 0.60       |                              | 38.9        | 38.9       | 1,515                   |   | 0.035       | 909                       | 0.021          |
|                             | 0.80       |                              | 38.9        | 38.9       | 1,515                   |   | 0.035       | 1,212                     | 0.028          |
|                             | 1.00       |                              | 82.1        | 60.2       | 4,941                   |   | 0.113       | 1,780                     | 0.041          |
|                             | 1.20       |                              | 132.9       | 85.2       | 11,320                  |   | 0.260       | 3,364                     | 0.077          |
|                             | 1.40       |                              | 183.7       | 110.2      | 20,240                  |   | 0.465       | 6,478                     | 0.149          |
| Floor                       | 1.60       |                              | 234.5       | 135.2      | 31,699                  |   | 0.728       | 11,629                    | 0.267          |
|                             | 1.72       |                              | 265.0       | 150.2      | 39,794                  |   | 0.914       | 15,910                    | 0.365          |
|                             | 1.80       |                              | 265.6       | 150.8      | 40,060                  |   | 0.920       | 19,104                    | 0.439          |
|                             | 2.00       |                              | 267.2       | 152.4      | 40,729                  |   | 0.935       | 27,183                    | 0.624          |
|                             | 2.20       |                              | 268.8       | 154.0      | 41,403                  |   | 0.950       | 35,396                    | 0.813          |
| Zone 1 (WQCV)               | 2.35       |                              | 270.0       | 155.2      | 41,912                  |   | 0.962       | 41,644                    | 0.956          |
|                             | 2.40       |                              | 270.4       | 155.6      | 42,082                  |   | 0.966       | 43,744                    | 1.004          |
|                             | 2.60       |                              | 272.0       | 157.2      | 42,766                  |   | 0.982       | 52,229                    | 1.199          |
|                             | 2.80       |                              | 273.6       | 158.8      | 43,456                  |   | 0.998       | 60,851                    | 1.397          |
|                             | 3.00       |                              | 275.2       | 160.4      | 44,150                  |   | 1.014       | 69,612                    | 1.598          |
|                             | 3.20       |                              | 276.8       | 162.0      | 44,850                  |   | 1.030       | 78,512                    | 1.802          |
|                             | 3.40       |                              | 278.4       | 163.6      | 45,554                  |   | 1.046       | 87,552                    | 2.010          |
| Zone 2 (EURV)               | 3.60       |                              | 280.0       | 165.2      | 46,264                  |   | 1.062       | 96,734                    | 2.221          |
|                             | 3.69       |                              | 280.7       | 165.9      | 46,585                  |   | 1.069       | 100,912                   | 2.317          |
|                             | 3.80       |                              | 281.6       | 166.8      | 46,979                  |   | 1.078       | 106,058                   | 2.435          |
|                             | 4.00       |                              | 283.2       | 168.4      | 47,699                  |   | 1.095       | 115,526                   | 2.652          |
|                             | 4.20       |                              | 284.8       | 170.0      | 48,424                  |   | 1.112       | 125,138                   | 2.873          |
|                             | 4.40       |                              | 286.4       | 171.6      | 49,155                  |   | 1.128       | 134,896                   | 3.097          |
|                             | 4.60       |                              | 288.0       | 173.2      | 49,890                  |   | 1.145       | 144,800                   | 3.324          |
|                             | 4.80       |                              | 289.6       | 174.8      | 50,631                  |   | 1.162       | 154,852                   | 3.555          |
|                             | 5.00       |                              | 291.2       | 176.4      | 51,376                  |   | 1.179       | 165,053                   | 3.789          |
| Zone 2 (EURV)               | 5.20       |                              | 292.8       | 178.0      | 52,127                  |   | 1.197       | 175,403                   | 4.027          |
|                             | 5.40       |                              | 294.4       | 179.6      | 52,883                  |   | 1.214       | 185,904                   | 4.268          |
|                             | 5.60       |                              | 296.0       | 181.2      | 53,644                  |   | 1.232       | 196,557                   | 4.512          |
|                             | 5.80       |                              | 297.6       | 182.8      | 54,410                  |   | 1.249       | 207,362                   | 4.760          |
| Zone 3 (100-year)           | 6.00       |                              | 299.2       | 184.5      | 55,182                  |   | 1.267       | 218,321                   | 5.012          |
|                             | 6.01       |                              | 299.3       | 184.5      | 55,220                  |   | 1.268       | 218,873                   | 5.025          |
|                             | 6.20       |                              | 300.8       | 186.0      | 55,958                  |   | 1.285       | 229,435                   | 5.267          |
|                             | 6.40       |                              | 302.4       | 187.6      | 56,739                  |   | 1.303       | 240,705                   | 5.526          |
|                             | 6.60       |                              | 304.0       | 189.2      | 57,526                  |   | 1.321       | 252,131                   | 5.788          |
|                             | 6.80       |                              | 305.6       | 190.8      | 58,318                  |   | 1.339       | 263,716                   | 6.054          |
|                             | 7.00       |                              | 307.2       | 192.4      | 59,115                  |   | 1.357       | 275,459                   | 6.324          |
|                             | 7.20       |                              | 308.8       | 194.0      | 59,917                  |   | 1.375       | 287,362                   | 6.597          |
|                             | 7.40       |                              | 310.4       | 195.6      | 60,724                  |   | 1.394       | 299,426                   | 6.874          |
|                             | 7.60       |                              | 312.0       | 197.2      | 61,536                  |   | 1.413       | 311,652                   | 7.155          |
|                             | 7.80       |                              | 313.6       | 198.8      | 62,353                  |   | 1.431       | 324,041                   | 7.439          |
|                             | 8.00       |                              | 315.2       | 200.4      | 63,176                  |   | 1.450       | 336,593                   | 7.727          |
|                             | 8.20       |                              | 316.8       | 202.0      | 64,003                  |   | 1.469       | 349,311                   | 8.019          |
|                             | 8.40       |                              | 318.4       | 203.6      | 64,836                  |   | 1.488       | 362,195                   | 8.315          |
|                             | 8.60       |                              | 320.0       | 205.2      | 65,674                  |   | 1.508       | 375,246                   | 8.614          |
|                             | 8.80       |                              | 321.6       | 206.8      | 66,517                  |   | 1.527       | 388,465                   | 8.918          |
|                             | 9.00       |                              | 323.2       | 208.4      | 67,365                  |   | 1.546       | 401,853                   | 9.225          |
|                             | 9.20       |                              | 324.8       | 210.0      | 68,218                  |   | 1.566       | 415,411                   | 9.537          |
|                             | 9.40       |                              | 326.4       | 211.6      | 69,076                  |   | 1.586       | 429,141                   | 9.852          |
|                             | 9.60       |                              | 328.0       | 213.2      | 69,940                  |   | 1.606       | 443,042                   | 10.171         |
|                             | 9.80       |                              | 329.6       | 214.8      | 70,808                  |   | 1.626       | 457,117                   | 10.494         |
|                             | 10.00      |                              | 331.2       | 216.4      | 71,682                  |   | 1.646       | 471,366                   | 10.821         |
|                             | 10.20      |                              | 332.8       | 218.0      | 72,561                  |   | 1.666       | 485,790                   | 11.152         |
|                             | 10.40      |                              | 334.4       | 219.6      | 73,445                  |   | 1.686       | 500,390                   | 11.487         |
|                             | 10.60      |                              | 336.0       | 221.2      | 74,334                  |   | 1.706       | 515,168                   | 11.827         |
|                             | 10.80      |                              | 337.6       | 222.8      | 75,228                  |   | 1.727       | 530,124                   | 12.170         |
|                             | 11.00      |                              | 339.2       | 224.4      | 76,127                  |   | 1.748       | 545,260                   | 12.517         |
|                             | 11.20      |                              | 340.8       | 226.0      | 77,032                  |   | 1.768       | 560,576                   | 12.869         |
|                             | 11.40      |                              | 342.4       | 227.6      | 77,941                  |   | 1.789       | 576,073                   | 13.225         |
|                             | 11.60      |                              | 344.0       | 229.2      | 78,856                  |   | 1.810       | 591,752                   | 13.585         |
|                             | 11.80      |                              | 345.6       | 230.8      | 79,775                  |   | 1.831       | 607,615                   | 13.949         |
|                             | 12.00      |                              | 347.2       | 232.4      | 80,700                  |   | 1.853       | 623,663                   | 14.317         |
|                             | 12.20      |                              | 348.8       | 234.0      | 81,630                  |   | 1.874       | 639,896                   | 14.690         |
|                             | 12.40      |                              | 350.4       | 235.6      | 82,565                  |   | 1.895       | 656,315                   | 15.067         |
|                             | 12.60      |                              | 352.0       | 237.2      | 83,506                  |   | 1.917       | 672,922                   | 15.448         |
|                             | 12.80      |                              | 353.6       | 238.8      | 84,451                  |   | 1.939       | 689,718                   | 15.834         |
|                             | 13.00      |                              | 355.2       | 240.4      | 85,401                  |   | 1.961       | 706,703                   | 16.224         |
|                             | 13.20      |                              | 356.8       | 242.0      | 86,357                  |   | 1.982       | 723,879                   | 16.618         |
|                             | 13.40      |                              | 358.4       | 243.6      | 87,318                  |   | 2.005       | 741,246                   | 17.017         |
|                             | 13.60      |                              | 360.0       | 245.2      | 88,283                  |   | 2.027       | 758,806                   | 17.420         |
|                             | 13.80      |                              | 361.6       | 246.8      | 89,254                  |   | 2.049       | 776,560                   | 17.827         |
|                             | 14.00      |                              | 363.2       | 248.4      | 90,231                  |   | 2.071       | 794,508                   | 18.239         |
|                             | 14.20      |                              | 364.8       | 250.0      | 91,212                  |   | 2.094       | 812,652                   | 18.656         |
|                             | 14.40      |                              | 366.4       | 251.6      | 92,198                  |   | 2.117       | 830,993                   | 19.077         |
|                             | 14.60      |                              | 368.0       | 253.2      | 93,189                  |   | 2.139       | 849,532                   | 19.503         |
|                             | 14.80      |                              | 369.6       | 254.8      | 94,186                  |   | 2.162       | 868,269                   | 19.933         |
|                             | 15.00      |                              | 371.2       | 256.4      | 95,188                  |   | 2.185       | 887,207                   | 20.367         |
|                             | 15.20      |                              | 372.8       | 258.0      | 96,194                  |   | 2.208       | 906,345                   | 20.807         |
|                             | 15.40      |                              | 374.4       | 259.6      | 97,206                  |   | 2.232       | 925,685                   | 21.251         |
|                             | 15.60      |                              | 376.0       | 261.2      | 98,223                  |   | 2.255       | 945,228                   | 21.699         |
|                             | 15.80      |                              | 377.6       | 262.8      | 99,245                  |   | 2.278       | 964,974                   | 22.153         |
|                             | 16.00      |                              | 379.2       | 264.4      | 100,273                 |   | 2.302       | 984,926                   | 22.611         |
|                             | 16.20      |                              | 380.8       | 266.0      | 101,305                 |   | 2.326       | 1,005,084                 | 23.074         |
|                             | 16.40      |                              | 382.4       | 267.6      | 102,343                 |   | 2.349       | 1,025,449                 | 23.541         |
|                             | 16.60      |                              | 384.0       | 269.2      | 103,385                 |   | 2.373       | 1,046,021                 | 24.013         |
|                             | 16.80      |                              | 385.6       | 270.8      | 104,433                 |   | 2.397       | 1,066,803                 | 24.490         |
|                             | 17.00      |                              | 387.2       | 272.4      | 105,486                 |   | 2.422       | 1,087,795                 | 24.972         |
|                             | 17.20      |                              | 388.8       | 274.0      | 106,544                 |   | 2.446       | 1,108,998                 | 25.459         |
|                             | 17.40      |                              | 390.4       | 275.6      | 107,607                 |   | 2.470       | 1,130,413                 | 25.951         |
|                             | 17.60      |                              | 392.0       | 277.2      | 108,675                 |   | 2.495       | 1,152,041                 | 26.447         |
|                             | 17.80      |                              | 393.6       | 278.8      | 109,749                 |   | 2.519       | 1,173,883                 | 26.949         |
|                             | 18.00      |                              | 395.2       | 280.4      | 110,827                 |   | 2.544       | 1,195,941                 | 27.455         |
|                             | 18.20      |                              | 396.8       | 282.0      | 111,911                 |   | 2.569       | 1,218,214                 | 27.966         |
|                             | 18.40      |                              | 398.4       | 283.6      | 112,999                 |   | 2.594       | 1,240,705                 | 28.483         |
|                             | 18.60      |                              | 400.0       | 285.2      | 114,093                 |   | 2.619       | 1,263,414                 | 29.007         |
|                             | 18.80      |                              | 401.6       | 286.8      | 115,192                 |   | 2.644       | 1,286,343                 | 29.530         |

# DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.04 (February 2021)

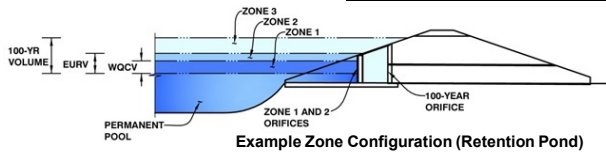


# DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-DETENTION, Version 4.04 (February 2021)

Project: Flying Horse North MDDP

Basin ID: Pond 2



Example Zone Configuration (Retention Pond)

|                   | Estimated Stage (ft) | Estimated Volume (ac-ft) | Outlet Type          |
|-------------------|----------------------|--------------------------|----------------------|
| Zone 1 (WQCV)     | 2.35                 | 0.954                    | Orifice Plate        |
| Zone 2 (EURV)     | 3.69                 | 1.355                    | Circular Orifice     |
| Zone 3 (100-year) | 6.01                 | 2.712                    | Weir&Pipe (Restrict) |
| Total (all zones) |                      | 5.021                    |                      |

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth =  ft (distance below the filtration media surface)  
Underdrain Orifice Diameter =  inches

Calculated Parameters for Underdrain  
Underdrain Orifice Area =  ft<sup>2</sup>  
Underdrain Orifice Centroid =  feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice =  ft (relative to basin bottom at Stage = 0 ft)  
Depth at top of Zone using Orifice Plate =  ft (relative to basin bottom at Stage = 0 ft)  
Orifice Plate: Orifice Vertical Spacing =  inches  
Orifice Plate: Orifice Area per Row =  sq. inches (use rectangular openings)

Calculated Parameters for Plate  
WQ Orifice Area per Row =  ft<sup>2</sup>  
Elliptical Half-Width =  feet  
Elliptical Slot Centroid =  feet  
Elliptical Slot Area =  ft<sup>2</sup>

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

|                                | Row 1 (required) | Row 2 (optional) | Row 3 (optional) | Row 4 (optional) | Row 5 (optional) | Row 6 (optional) | Row 7 (optional) | Row 8 (optional) |
|--------------------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|
| Stage of Orifice Centroid (ft) | 0.00             | 0.78             | 1.57             |                  |                  |                  |                  |                  |
| Orifice Area (sq. inches)      | 3.41             | 3.41             | 3.41             |                  |                  |                  |                  |                  |

|                                | Row 9 (optional) | Row 10 (optional) | Row 11 (optional) | Row 12 (optional) | Row 13 (optional) | Row 14 (optional) | Row 15 (optional) | Row 16 (optional) |
|--------------------------------|------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| Stage of Orifice Centroid (ft) |                  |                   |                   |                   |                   |                   |                   |                   |
| Orifice Area (sq. inches)      |                  |                   |                   |                   |                   |                   |                   |                   |

User Input: Vertical Orifice (Circular or Rectangular)

Invert of Vertical Orifice =  ft (relative to basin bottom at Stage = 0 ft)  
Depth at top of Zone using Vertical Orifice =  ft (relative to basin bottom at Stage = 0 ft)  
Vertical Orifice Diameter =  inches

Calculated Parameters for Vertical Orif  
Zone 2 Circular Not Selected  
Vertical Orifice Area =  ft<sup>2</sup>  
Vertical Orifice Centroid =  feet

User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe)

Zone 3 Weir Not Selected  
Overflow Weir Front Edge Height, H<sub>o</sub> =  ft (relative to basin bottom at Stage = 0 ft)  
Overflow Weir Front Edge Length =  feet  
Overflow Weir Grate Slope =  H:V  
Horiz. Length of Weir Sides =  feet  
Overflow Grate Type =   
Debris Clogging % =  %

Calculated Parameters for Overflow W  
Zone 3 Weir Not Selected  
Height of Grate Upper Edge, H<sub>u</sub> =  feet  
Overflow Weir Slope Length =  feet  
Grate Open Area / 100-yr Orifice Area =  N/A  
Overflow Grate Open Area w/o Debris =  N/A  
Overflow Grate Open Area w/ Debris =  N/A

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

Zone 3 Restrictor Not Selected  
Depth to Invert of Outlet Pipe =  ft (distance below basin bottom at Stage = 0 ft)  
Outlet Pipe Diameter =  inches  
Restrictor Plate Height Above Pipe Invert =  inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Pl  
Zone 3 Restrictor Not Selected  
Outlet Orifice Area =  ft<sup>2</sup>  
Outlet Orifice Centroid =  feet  
Half-Central Angle of Restrictor Plate on Pipe =  N/A

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage =  ft (relative to basin bottom at Stage = 0 ft)  
Spillway Crest Length =  feet  
Spillway End Slopes =  H:V  
Freeboard above Max Water Surface =  feet

Calculated Parameters for Spillway  
Spillway Design Flow Depth =  feet  
Stage at Top of Freeboard =  feet  
Basin Area at Top of Freeboard =  acres  
Basin Volume at Top of Freeboard =  acre-ft

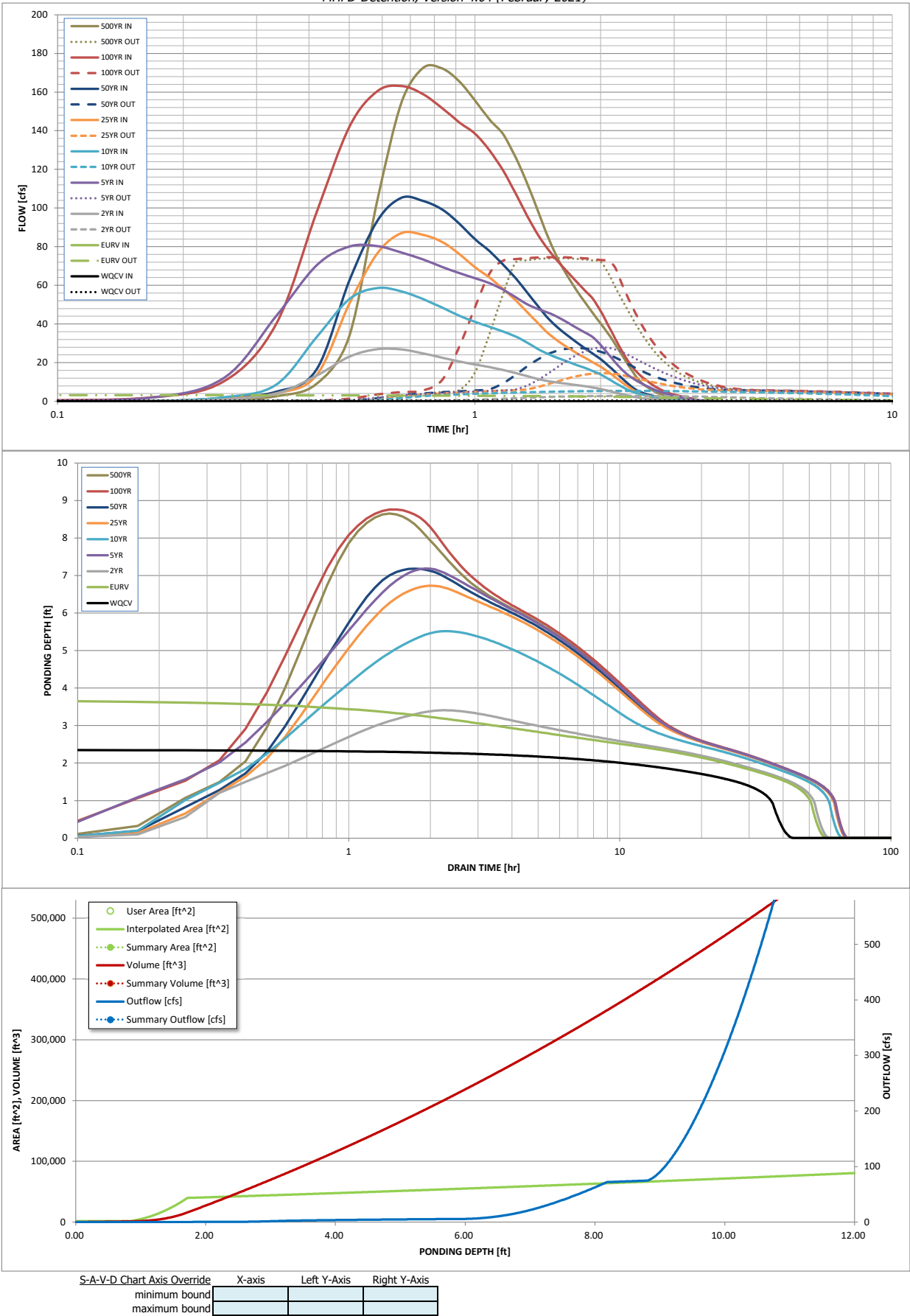
## Routed Hydrograph Results

The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AI)

|  | WQCV  | EURV               | 2 Year             | 5 Year          | 10 Year            | 25 Year         | 50 Year         | 100 Year       |
|--|-------|--------------------|--------------------|-----------------|--------------------|-----------------|-----------------|----------------|
| Design Storm Return Period =                       | N/A   | N/A                | 1.19               | 1.50            | 1.75               | 2.00            | 2.25            | 2.52           |
| One-Hour Rainfall Depth (in) =                     | N/A   | N/A                | 1.19               | 1.50            | 1.75               | 2.00            | 2.25            | 2.52           |
| CUHP Runoff Volume (acre-ft) =                     | 0.954 | 2.309              | 2.348              | 3.828           | 5.193              | 7.260           | 8.821           | 10.908         |
| User Override Inflow Hydrograph Volume (acre-ft) = | N/A   | N/A                | 2.348              | 9.011           | 5.193              | 7.260           | 8.821           | 16.404         |
| CUHP Predevelopment Peak Q (cfs) =                 | N/A   | N/A                | 7.6                | 21.4            | 32.6               | 58.3            | 73.3            | 93.7           |
| OPTIONAL Override Predevelopment Peak Q (cfs) =    | N/A   | N/A                |                    | 27.9            |                    |                 |                 | 81.0           |
| Predevelopment Unit Peak Flow, q (cfs/acre) =      | N/A   | N/A                | 0.10               | 0.37            | 0.43               | 0.76            | 0.96            | 1.06           |
| Peak Inflow Q (cfs) =                              | N/A   | N/A                | 26.9               | 80.3            | 58.6               | 87.0            | 105.2           | 163.2          |
| Peak Outflow Q (cfs) =                             | 0.4   | 3.2                | 2.8                | 27.8            | 5.4                | 14.5            | 27.5            | 74.6           |
| Ratio Peak Outflow to Predevelopment Q =           | N/A   | N/A                | N/A                | 1.0             | 0.2                | 0.2             | 0.4             | 0.9            |
| Structure Controlling Flow =                       | Plate | Vertical Orifice 1 | Vertical Orifice 1 | Overflow Weir 1 | Vertical Orifice 1 | Overflow Weir 1 | Overflow Weir 1 | Outlet Plate 1 |
| Max Velocity through Grate 1 (fps) =               | N/A   | N/A                | N/A                | 0.7             | N/A                | 0.3             | 0.7             | 2.1            |
| Max Velocity through Grate 2 (fps) =               | N/A   | N/A                | N/A                | N/A             | N/A                | N/A             | N/A             | N/A            |
| Time to Drain 97% of Inflow Volume (hours) =       | 37    | 49                 | 50                 | 49              | 52                 | 51              | 49              | 41             |
| Time to Drain 99% of Inflow Volume (hours) =       | 40    | 52                 | 54                 | 59              | 58                 | 59              | 59              | 55             |
| Maximum Ponding Depth (ft) =                       | 2.35  | 3.69               | 3.41               | 7.19            | 5.52               | 6.72            | 7.18            | 8.76           |
| Area at Maximum Ponding Depth (acres) =            | 0.96  | 1.07               | 1.05               | 1.37            | 1.22               | 1.33            | 1.37            | 1.52           |
| Maximum Volume Stored (acre-ft) =                  | 0.956 | 2.317              | 2.010              | 6.569           | 4.402              | 5.947           | 6.556           | 8.842          |

DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-DETENTION, Version 4.04 (February 2021)



# DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename: \_\_\_\_\_

## Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

|               | SOURCE  | CUHP       | CUHP       | CUHP         | USER         | CUHP          | CUHP          | CUHP          | USER           | CUHP           |
|---------------|---------|------------|------------|--------------|--------------|---------------|---------------|---------------|----------------|----------------|
| Time Interval | TIME    | WQCV [cfs] | EURV [cfs] | 2 Year [cfs] | 5 Year [cfs] | 10 Year [cfs] | 25 Year [cfs] | 50 Year [cfs] | 100 Year [cfs] | 500 Year [cfs] |
| 5.00 min      | 0:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 0:05:00 | 0.00       | 0.00       | 0.00         | 0.13         | 0.00          | 0.00          | 0.00          | 0.32           | 0.00           |
|               | 0:10:00 | 0.00       | 0.00       | 0.00         | 1.80         | 0.00          | 0.00          | 0.11          | 1.90           | 0.37           |
|               | 0:15:00 | 0.00       | 0.00       | 0.97         | 11.97        | 2.02          | 1.37          | 1.76          | 10.22          | 2.60           |
|               | 0:20:00 | 0.00       | 0.00       | 3.87         | 43.79        | 8.48          | 4.07          | 4.83          | 39.58          | 8.88           |
|               | 0:25:00 | 0.00       | 0.00       | 13.19        | 70.16        | 32.99         | 13.33         | 16.21         | 97.23          | 33.67          |
|               | 0:30:00 | 0.00       | 0.00       | 23.12        | 80.09        | 52.87         | 50.35         | 62.29         | 141.84         | 103.95         |
|               | 0:35:00 | 0.00       | 0.00       | 26.92        | 80.26        | 58.60         | 76.45         | 93.34         | 160.45         | 154.46         |
|               | 0:40:00 | 0.00       | 0.00       | 26.87        | 76.94        | 56.82         | 86.98         | 105.24        | 163.15         | 172.38         |
|               | 0:45:00 | 0.00       | 0.00       | 24.83        | 73.40        | 52.91         | 86.09         | 103.73        | 158.97         | 172.22         |
|               | 0:50:00 | 0.00       | 0.00       | 22.58        | 69.54        | 48.53         | 82.51         | 99.35         | 151.80         | 165.57         |
|               | 0:55:00 | 0.00       | 0.00       | 20.60        | 66.38        | 44.34         | 76.24         | 91.93         | 144.38         | 155.67         |
|               | 1:00:00 | 0.00       | 0.00       | 18.99        | 63.71        | 41.14         | 69.38         | 83.89         | 138.52         | 145.77         |
|               | 1:05:00 | 0.00       | 0.00       | 17.72        | 61.08        | 38.56         | 64.02         | 77.70         | 129.85         | 138.29         |
|               | 1:10:00 | 0.00       | 0.00       | 16.21        | 57.80        | 36.08         | 58.18         | 70.80         | 119.57         | 126.35         |
|               | 1:15:00 | 0.00       | 0.00       | 14.59        | 53.88        | 33.59         | 52.31         | 63.81         | 107.76         | 112.87         |
|               | 1:20:00 | 0.00       | 0.00       | 13.00        | 50.24        | 30.43         | 46.20         | 56.32         | 96.06          | 98.23          |
|               | 1:25:00 | 0.00       | 0.00       | 11.52        | 47.71        | 27.01         | 40.35         | 49.12         | 86.02          | 84.46          |
|               | 1:30:00 | 0.00       | 0.00       | 10.40        | 45.81        | 24.37         | 35.06         | 42.76         | 78.34          | 73.27          |
|               | 1:35:00 | 0.00       | 0.00       | 9.62         | 43.38        | 22.31         | 31.09         | 37.98         | 72.21          | 64.70          |
|               | 1:40:00 | 0.00       | 0.00       | 8.98         | 40.71        | 20.50         | 27.87         | 34.07         | 66.82          | 57.64          |
|               | 1:45:00 | 0.00       | 0.00       | 8.41         | 38.11        | 18.84         | 25.07         | 30.63         | 61.95          | 51.34          |
|               | 1:50:00 | 0.00       | 0.00       | 7.85         | 35.67        | 17.29         | 22.53         | 27.51         | 57.40          | 45.60          |
|               | 1:55:00 | 0.00       | 0.00       | 7.14         | 33.13        | 15.68         | 20.18         | 24.61         | 53.06          | 40.22          |
|               | 2:00:00 | 0.00       | 0.00       | 6.38         | 29.16        | 13.87         | 17.91         | 21.82         | 46.73          | 35.16          |
|               | 2:05:00 | 0.00       | 0.00       | 5.48         | 24.64        | 11.73         | 15.27         | 18.55         | 39.57          | 29.60          |
|               | 2:10:00 | 0.00       | 0.00       | 4.57         | 20.28        | 9.56          | 12.56         | 15.20         | 32.54          | 24.00          |
|               | 2:15:00 | 0.00       | 0.00       | 3.69         | 16.43        | 7.53          | 9.93          | 11.96         | 26.09          | 18.60          |
|               | 2:20:00 | 0.00       | 0.00       | 2.87         | 13.45        | 5.75          | 7.44          | 8.92          | 20.54          | 13.70          |
|               | 2:25:00 | 0.00       | 0.00       | 2.15         | 11.17        | 4.48          | 5.23          | 6.32          | 16.29          | 9.92           |
|               | 2:30:00 | 0.00       | 0.00       | 1.65         | 9.34         | 3.63          | 3.85          | 4.72          | 13.11          | 7.39           |
|               | 2:35:00 | 0.00       | 0.00       | 1.33         | 7.79         | 2.98          | 2.91          | 3.60          | 10.56          | 5.56           |
|               | 2:40:00 | 0.00       | 0.00       | 1.09         | 6.44         | 2.43          | 2.24          | 2.78          | 8.46           | 4.15           |
|               | 2:45:00 | 0.00       | 0.00       | 0.90         | 5.28         | 1.98          | 1.71          | 2.13          | 6.74           | 3.06           |
|               | 2:50:00 | 0.00       | 0.00       | 0.73         | 4.30         | 1.59          | 1.33          | 1.65          | 5.35           | 2.23           |
|               | 2:55:00 | 0.00       | 0.00       | 0.60         | 3.49         | 1.26          | 1.02          | 1.26          | 4.27           | 1.62           |
|               | 3:00:00 | 0.00       | 0.00       | 0.49         | 2.84         | 1.00          | 0.79          | 0.98          | 3.48           | 1.22           |
|               | 3:05:00 | 0.00       | 0.00       | 0.40         | 2.27         | 0.78          | 0.63          | 0.78          | 2.82           | 0.97           |
|               | 3:10:00 | 0.00       | 0.00       | 0.33         | 1.78         | 0.61          | 0.49          | 0.61          | 2.27           | 0.77           |
|               | 3:15:00 | 0.00       | 0.00       | 0.26         | 1.36         | 0.47          | 0.39          | 0.48          | 1.78           | 0.61           |
|               | 3:20:00 | 0.00       | 0.00       | 0.20         | 1.00         | 0.36          | 0.30          | 0.36          | 1.35           | 0.47           |
|               | 3:25:00 | 0.00       | 0.00       | 0.15         | 0.71         | 0.27          | 0.22          | 0.27          | 0.99           | 0.34           |
|               | 3:30:00 | 0.00       | 0.00       | 0.11         | 0.48         | 0.19          | 0.16          | 0.19          | 0.68           | 0.24           |
|               | 3:35:00 | 0.00       | 0.00       | 0.08         | 0.30         | 0.12          | 0.11          | 0.13          | 0.42           | 0.15           |
|               | 3:40:00 | 0.00       | 0.00       | 0.05         | 0.16         | 0.07          | 0.06          | 0.08          | 0.23           | 0.09           |
|               | 3:45:00 | 0.00       | 0.00       | 0.02         | 0.06         | 0.03          | 0.03          | 0.04          | 0.10           | 0.04           |
|               | 3:50:00 | 0.00       | 0.00       | 0.01         | 0.01         | 0.01          | 0.01          | 0.01          | 0.02           | 0.01           |
|               | 3:55:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:05:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:10:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:15:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:20:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:25:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:30:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:35:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:40:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:45:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:50:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:55:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:05:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:10:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:15:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:20:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:25:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:30:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:35:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:40:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:45:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:50:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:55:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 6:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |

0 5:50:00 0.72

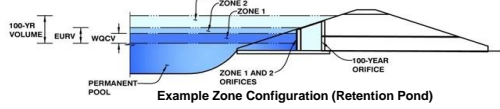


# DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.04 (February 2021)

Project: **Flying Horse North**

Basin ID: **Pond 3**



Example Zone Configuration (Retention Pond)

## Watershed Information

|   |            |         |
|---|------------|---------|
| Selected BMP Type =                     | <b>EDB</b> |         |
| Watershed Area =                        | 52.52      | acres   |
| Watershed Length =                      | 2,370      | ft      |
| Watershed Length to Centroid =          | 1,179      | ft      |
| Watershed Slope =                       | 0.033      | ft/ft   |
| Watershed Imperviousness =              | 30.10%     | percent |
| Percentage Hydrologic Soil Group A =    | 0.0%       | percent |
| Percentage Hydrologic Soil Group B =    | 100.0%     | percent |
| Percentage Hydrologic Soil Groups C/D = | 0.0%       | percent |
| Target WQCV Drain Time =                | 40.0       | hours   |
| Location for 1-hr Rainfall Depths =     | User Input |         |

After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

|  |        |           |
|--|--------|-----------|
| Water Quality Capture Volume (WQCV) =  | 0.664  | acre-feet |
| Excess Urban Runoff Volume (EURV) =    | 1.623  | acre-feet |
| 2-yr Runoff Volume (P1 = 1.19 in.) =   | 1.643  | acre-feet |
| 5-yr Runoff Volume (P1 = 1.5 in.) =    | 2.665  | acre-feet |
| 10-yr Runoff Volume (P1 = 1.75 in.) =  | 3.605  | acre-feet |
| 25-yr Runoff Volume (P1 = 2 in.) =     | 5.023  | acre-feet |
| 50-yr Runoff Volume (P1 = 2.25 in.) =  | 6.095  | acre-feet |
| 100-yr Runoff Volume (P1 = 2.52 in.) = | 7.524  | acre-feet |
| 500-yr Runoff Volume (P1 = 3.14 in.) = | 10.289 | acre-feet |
| Approximate 2-yr Detention Volume =    | 1.161  | acre-feet |
| Approximate 5-yr Detention Volume =    | 1.661  | acre-feet |
| Approximate 10-yr Detention Volume =   | 2.421  | acre-feet |
| Approximate 25-yr Detention Volume =   | 2.807  | acre-feet |
| Approximate 50-yr Detention Volume =   | 2.958  | acre-feet |
| Approximate 100-yr Detention Volume =  | 3.496  | acre-feet |

## Optional User Overrides

|  |      |           |
|--|------|-----------|
|  |      | acre-feet |
|  |      | acre-feet |
|  | 1.19 | inches    |
|  | 1.50 | inches    |
|  | 1.75 | inches    |
|  | 2.00 | inches    |
|  | 2.25 | inches    |
|  | 2.52 | inches    |
|  |      | inches    |

## Define Zones and Basin Geometry

|   |       |                 |
|---|-------|-----------------|
| Zone 1 Volume (WQCV) =                                  | 0.664 | acre-feet       |
| Zone 2 Volume (EURV - Zone 1) =                         | 0.958 | acre-feet       |
| Zone 3 Volume (100-year - Zones 1 & 2) =                | 1.873 | acre-feet       |
| Total Detention Basin Volume =                          | 3.496 | acre-feet       |
| Initial Surge Volume (ISV) =                            | 87    | ft <sup>3</sup> |
| Initial Surge Depth (ISD) =                             | 0.33  | ft              |
| Total Available Detention Depth (H <sub>total</sub> ) = | 6.00  | ft              |
| Depth of Trickle Channel (H <sub>TC</sub> ) =           | 0.50  | ft              |
| Slope of Trickle Channel (S <sub>TC</sub> ) =           | 0.004 | ft/ft           |
| Slopes of Main Basin Sides (S <sub>main</sub> ) =       | 4     | H:V             |
| Basin Length-to-Width Ratio (R <sub>L/W</sub> ) =       | 2     |                 |

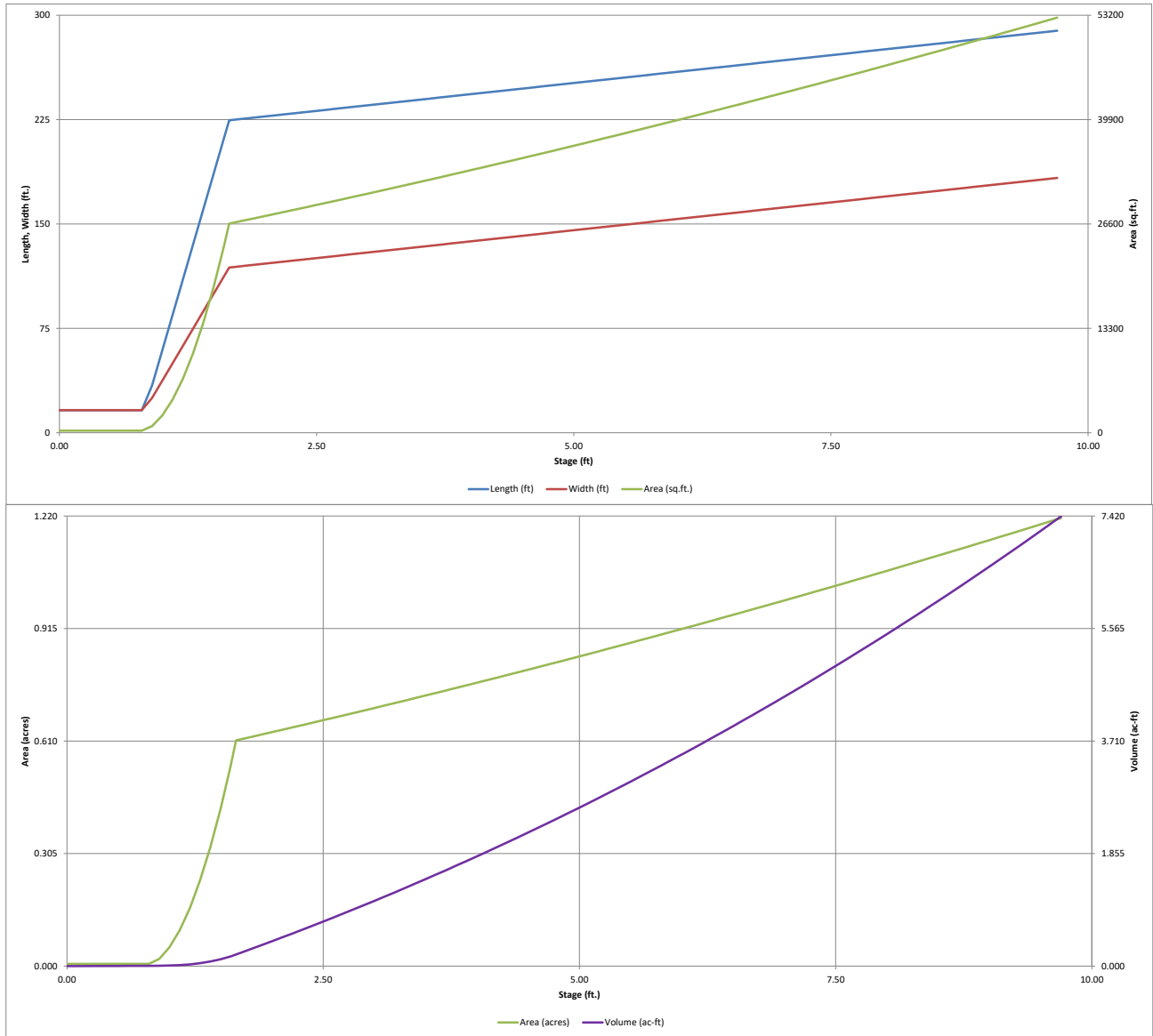
|   |              |                 |
|---|--------------|-----------------|
| Initial Surge Area (A <sub>ISV</sub> ) =              | 263          | ft <sup>2</sup> |
| Surcharge Volume Length (L <sub>ISV</sub> ) =         | 16.2         | ft              |
| Surcharge Volume Width (W <sub>ISV</sub> ) =          | 16.2         | ft              |
| Depth of Basin Floor (H <sub>FLOOR</sub> ) =          | 0.82         | ft              |
| Length of Basin Floor (L <sub>FLOOR</sub> ) =         | 224.5        | ft              |
| Width of Basin Floor (W <sub>FLOOR</sub> ) =          | 118.7        | ft              |
| Area of Basin Floor (A <sub>FLOOR</sub> ) =           | 26,652       | ft <sup>2</sup> |
| Volume of Basin Floor (V <sub>FLOOR</sub> ) =         | 8,081        | ft <sup>3</sup> |
| Depth of Main Basin (H <sub>MAIN</sub> ) =            | 4.35         | ft              |
| Length of Main Basin (L <sub>MAIN</sub> ) =           | 259.3        | ft              |
| Width of Main Basin (W <sub>MAIN</sub> ) =            | 153.5        | ft              |
| Area of Main Basin (A <sub>MAIN</sub> ) =             | 39,807       | ft <sup>2</sup> |
| Volume of Main Basin (V <sub>MAIN</sub> ) =           | 143,597      | ft <sup>3</sup> |
| Calculated Total Basin Volume (V <sub>total</sub> ) = | <b>3.487</b> | acre-feet       |

Depth Increment = 0.10 ft

| Stage - Storage Description | Stage (ft) | Optional Override Stage (ft) | Length (ft) | Width (ft) | Area (ft <sup>2</sup> ) | Optional Override Area (ft <sup>2</sup> ) | Area (acre) | Volume (ft <sup>3</sup> ) | Volume (ac-ft) |
|-----------------------------|------------|------------------------------|-------------|------------|-------------------------|---|-------------|---------------------------|----------------|
| <b>Top of Micropool</b>     | 0.00       |                              | 16.2        | 16.2       | 263                     |   | 0.006       |                           |                |
| <b>ISV</b>                  | 0.33       |                              | 16.2        | 16.2       | 263                     |   | 0.006       | 87                        | 0.002          |
|                             | 0.40       |                              | 16.2        | 16.2       | 263                     |   | 0.006       | 105                       | 0.002          |
|                             | 0.50       |                              | 16.2        | 16.2       | 263                     |   | 0.006       | 132                       | 0.003          |
|                             | 0.60       |                              | 16.2        | 16.2       | 263                     |   | 0.006       | 158                       | 0.004          |
|                             | 0.70       |                              | 16.2        | 16.2       | 263                     |   | 0.006       | 184                       | 0.004          |
|                             | 0.80       |                              | 16.2        | 16.2       | 263                     |   | 0.006       | 210                       | 0.005          |
|                             | 0.90       |                              | 34.0        | 25.0       | 849                     |   | 0.019       | 255                       | 0.006          |
|                             | 1.00       |                              | 59.4        | 37.5       | 2,226                   |   | 0.051       | 404                       | 0.009          |
|                             | 1.10       |                              | 84.8        | 50.0       | 4,237                   |   | 0.097       | 722                       | 0.017          |
|                             | 1.20       |                              | 110.2       | 62.5       | 6,884                   |   | 0.158       | 1,273                     | 0.029          |
|                             | 1.30       |                              | 135.6       | 75.0       | 10,166                  |   | 0.233       | 2,120                     | 0.049          |
|                             | 1.40       |                              | 161.0       | 87.5       | 14,082                  |   | 0.323       | 3,327                     | 0.076          |
|                             | 1.50       |                              | 186.4       | 100.0      | 18,634                  |   | 0.428       | 4,957                     | 0.114          |
|                             | 1.60       |                              | 211.8       | 112.5      | 23,821                  |   | 0.547       | 7,075                     | 0.162          |
| <b>Floor</b>                | 1.65       |                              | 224.5       | 118.7      | 26,652                  |   | 0.612       | 8,336                     | 0.191          |
|                             | 1.70       |                              | 224.9       | 119.1      | 26,790                  |   | 0.615       | 9,672                     | 0.222          |
|                             | 1.80       |                              | 225.7       | 119.9      | 27,066                  |   | 0.621       | 12,365                    | 0.284          |
|                             | 1.90       |                              | 226.5       | 120.7      | 27,343                  |   | 0.628       | 15,085                    | 0.346          |
|                             | 2.00       |                              | 227.3       | 121.5      | 27,621                  |   | 0.634       | 17,833                    | 0.409          |
|                             | 2.10       |                              | 228.1       | 122.3      | 27,901                  |   | 0.641       | 20,610                    | 0.473          |
|                             | 2.20       |                              | 228.9       | 123.1      | 28,182                  |   | 0.647       | 23,414                    | 0.538          |
|                             | 2.30       |                              | 229.7       | 123.9      | 28,464                  |   | 0.653       | 26,246                    | 0.603          |
| <b>Zone 1 (WQCV)</b>        | 2.40       |                              | 230.5       | 124.7      | 28,748                  |   | 0.660       | 29,107                    | 0.668          |
|                             | 2.50       |                              | 231.3       | 125.5      | 29,032                  |   | 0.666       | 31,996                    | 0.735          |
|                             | 2.60       |                              | 232.1       | 126.3      | 29,319                  |   | 0.673       | 34,913                    | 0.801          |
|                             | 2.70       |                              | 232.9       | 127.1      | 29,606                  |   | 0.680       | 37,859                    | 0.869          |
|                             | 2.80       |                              | 233.7       | 127.9      | 29,895                  |   | 0.686       | 40,834                    | 0.937          |
|                             | 2.90       |                              | 234.5       | 128.7      | 30,185                  |   | 0.693       | 43,838                    | 1.006          |
|                             | 3.00       |                              | 235.3       | 129.5      | 30,476                  |   | 0.700       | 46,871                    | 1.076          |
|                             | 3.10       |                              | 236.1       | 130.3      | 30,768                  |   | 0.706       | 49,933                    | 1.146          |
|                             | 3.20       |                              | 236.9       | 131.1      | 31,062                  |   | 0.713       | 53,025                    | 1.217          |
|                             | 3.30       |                              | 237.7       | 131.9      | 31,357                  |   | 0.720       | 56,146                    | 1.289          |
|                             | 3.40       |                              | 238.5       | 132.7      | 31,653                  |   | 0.727       | 59,296                    | 1.361          |
|                             | 3.50       |                              | 239.3       | 133.5      | 31,951                  |   | 0.733       | 62,477                    | 1.434          |
|                             | 3.60       |                              | 240.1       | 134.3      | 32,250                  |   | 0.740       | 65,687                    | 1.508          |
|                             | 3.70       |                              | 240.9       | 135.1      | 32,550                  |   | 0.747       | 68,927                    | 1.582          |
| <b>Zone 2 (EURV)</b>        | 3.76       |                              | 241.4       | 135.6      | 32,731                  |   | 0.751       | 70,885                    | 1.627          |
|                             | 3.80       |                              | 241.7       | 135.9      | 32,852                  |   | 0.754       | 72,197                    | 1.657          |
|                             | 3.90       |                              | 242.5       | 136.7      | 33,154                  |   | 0.761       | 75,497                    | 1.733          |
|                             | 4.00       |                              | 243.3       | 137.5      | 33,458                  |   | 0.768       | 78,828                    | 1.810          |
|                             | 4.10       |                              | 244.1       | 138.3      | 33,764                  |   | 0.775       | 82,189                    | 1.887          |
|                             | 4.20       |                              | 244.9       | 139.1      | 34,070                  |   | 0.782       | 85,580                    | 1.965          |
|                             | 4.30       |                              | 245.7       | 139.9      | 34,378                  |   | 0.789       | 89,003                    | 2.043          |
|                             | 4.40       |                              | 246.5       | 140.7      | 34,687                  |   | 0.796       | 92,456                    | 2.122          |
|                             | 4.50       |                              | 247.3       | 141.5      | 34,998                  |   | 0.803       | 95,940                    | 2.202          |
|                             | 4.60       |                              | 248.1       | 142.3      | 35,309                  |   | 0.811       | 99,456                    | 2.283          |
|                             | 4.70       |                              | 248.9       | 143.1      | 35,622                  |   | 0.818       | 103,002                   | 2.365          |
|                             | 4.80       |                              | 249.7       | 143.9      | 35,936                  |   | 0.825       | 106,580                   | 2.447          |
|                             | 4.90       |                              | 250.5       | 144.7      | 36,252                  |   | 0.832       | 110,189                   | 2.530          |
|                             | 5.00       |                              | 251.3       | 145.5      | 36,569                  |   | 0.840       | 113,830                   | 2.613          |
|                             | 5.10       |                              | 252.1       | 146.3      | 36,887                  |   | 0.847       | 117,503                   | 2.698          |
|                             | 5.20       |                              | 252.9       | 147.1      | 37,206                  |   | 0.854       | 121,208                   | 2.783          |
|                             | 5.30       |                              | 253.7       | 147.9      | 37,527                  |   | 0.862       | 124,945                   | 2.868          |
|                             | 5.40       |                              | 254.5       | 148.7      | 37,849                  |   | 0.869       | 128,713                   | 2.955          |
|                             | 5.50       |                              | 255.3       | 149.5      | 38,172                  |   | 0.876       | 132,514                   | 3.042          |
|                             | 5.60       |                              | 256.1       | 150.3      | 38,497                  |   | 0.884       | 136,348                   | 3.130          |
|                             | 5.70       |                              | 256.9       | 151.1      | 38,822                  |   | 0.891       | 140,214                   | 3.219          |
|                             | 5.80       |                              | 257.7       | 151.9      | 39,149                  |   | 0.899       | 144,112                   | 3.308          |
|                             | 5.90       |                              | 258.5       | 152.7      | 39,478                  |   | 0.906       | 148,044                   | 3.399          |
|                             | 6.00       |                              | 259.3       | 153.5      | 39,807                  |   | 0.914       | 152,008                   | 3.490          |
| <b>Zone 3 (100-year)</b>    | 6.01       |                              | 259.4       | 153.6      | 39,840                  |   | 0.915       | 152,406                   | 3.499          |
|                             | 6.10       |                              | 260.1       | 154.3      | 40,138                  |   | 0.921       | 156,005                   | 3.581          |
|                             | 6.20       |                              | 260.9       | 155.1      | 40,470                  |   | 0.929       | 160,036                   | 3.674          |
|                             | 6.30       |                              | 261.7       | 155.9      | 40,804                  |   | 0.937       | 164,099                   | 3.767          |
|                             | 6.40       |                              | 262.5       | 156.7      | 41,139                  |   | 0.944       | 168,196                   | 3.861          |
|                             | 6.50       |                              | 263.3       | 157.5      | 41,475                  |   | 0.952       | 172,327                   | 3.956          |
|                             | 6.60       |                              | 264.1       | 158.3      | 41,812                  |   | 0.960       | 176,491                   | 4.052          |
|                             | 6.70       |                              | 264.9       | 159.1      | 42,151                  |   | 0.968       | 180,690                   | 4.148          |
|                             | 6.80       |                              | 265.7       | 159.9      | 42,490                  |   | 0.975       | 184,922                   | 4.245          |
|                             | 6.90       |                              | 266.5       | 160.7      | 42,832                  |   | 0.983       | 189,188                   | 4.343          |
|                             | 7.00       |                              | 267.3       | 161.5      | 43,174                  |   | 0.991       | 193,488                   | 4.442          |
|                             | 7.10       |                              | 268.1       | 162.3      | 43,518                  |   | 0.999       | 197,823                   | 4.541          |
|                             | 7.20       |                              | 268.9       | 163.1      | 43,863                  |   | 1.007       | 202,192                   | 4.642          |
|                             | 7.30       |                              | 269.7       | 163.9      | 44,209                  |   | 1.015       | 206,595                   | 4.743          |
|                             | 7.40       |                              | 270.5       | 164.7      | 44,556                  |   | 1.023       | 211,033                   | 4.845          |
|                             | 7.50       |                              | 271.3       | 165.5      | 44,905                  |   | 1.031       | 215,506                   | 4.947          |
|                             | 7.60       |                              | 272.1       | 166.3      | 45,255                  |   | 1.039       | 220,014                   | 5.051          |
|                             | 7.70       |                              | 272.9       | 167.1      | 45,607                  |   | 1.047       | 224,557                   | 5.155          |
|                             | 7.80       |                              | 273.7       | 167.9      | 45,959                  |   | 1.055       | 229,136                   | 5.260          |
|                             | 7.90       |                              | 274.5       | 168.7      | 46,313                  |   | 1.063       | 233,749                   | 5.366          |
|                             | 8.00       |                              | 275.3       | 169.5      | 46,668                  |   | 1.071       | 238,398                   | 5.473          |
|                             | 8.10       |                              | 276.1       | 170.3      | 47,025                  |   | 1.080       | 243,083                   | 5.580          |
|                             | 8.20       |                              | 276.9       | 171.1      | 47,383                  |   | 1.088       | 247,804                   | 5.689          |
|                             | 8.30       |                              | 277.7       | 171.9      | 47,742                  |   | 1.096       | 252,560                   | 5.798          |
|                             | 8.40       |                              | 278.5       | 172.7      | 48,102                  |   | 1.104       | 257,352                   | 5.908          |
|                             | 8.50       |                              | 279.3       | 173.5      | 48,464                  |   | 1.113       | 262,180                   | 6.019          |
|                             | 8.60       |                              | 280.1       | 174.3      | 48,827                  |   | 1.121       | 267,045                   | 6.131          |
|                             | 8.70       |                              | 280.9       | 175.1      | 49,191                  |   | 1.129       | 271,946                   | 6.243          |
|                             | 8.80       |                              | 281.7       | 175.9      | 49,556                  |   | 1.138       | 276,883                   | 6.356          |
|                             | 8.90       |                              | 282.5       | 176.7      | 49,923                  |   | 1.146       | 281,857                   | 6.471          |
|                             | 9.00       |                              | 283.3       | 177.5      | 50,291                  |   | 1.155       | 286,868                   | 6.586          |
|                             | 9.10       |                              | 284.1       | 178.3      | 50,660                  |   | 1.163       | 291,915                   | 6.701          |
|                             | 9.20       |                              | 284.9       | 179.1      | 51,031                  |   | 1.172       | 297,000                   | 6.818          |
|                             | 9.30       |                              | 285.7       | 179.9      | 51,403                  |   | 1.180       | 302,121                   | 6.936          |
|                             | 9.40       |                              | 286.5       | 180.7      | 51,776                  |   | 1.189       | 307,280                   | 7.054          |
|                             | 9.50       |                              | 287.3       | 181.5      | 52,150                  |   | 1.197       | 312,477                   | 7.173          |
|                             | 9.60       |                              | 288.1       | 182.3      | 52,526                  |   | 1.206       | 317,710                   | 7.294          |
|                             | 9.70       |                              | 288.9       | 183.1      | 52,903                  |   | 1.214       | 322,982                   | 7.415          |

# DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.04 (February 2021)

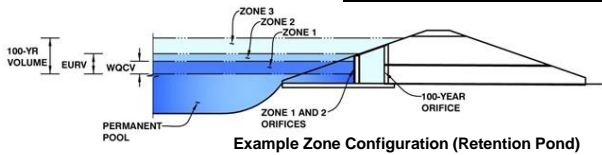


# DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.04 (February 2021)

Project: Flying Horse North

Basin ID: Pond 3



Example Zone Configuration (Retention Pond)

|                   | Estimated Stage (ft) | Estimated Volume (ac-ft) | Outlet Type          |
|-------------------|----------------------|--------------------------|----------------------|
| Zone 1 (WQCV)     | 2.40                 | 0.664                    | Orifice Plate        |
| Zone 2 (EURV)     | 3.76                 | 0.958                    | Rectangular Orifice  |
| Zone 3 (100-year) | 6.01                 | 1.873                    | Weir&Pipe (Restrict) |
| Total (all zones) |                      | 3.496                    |                      |

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth = N/A ft (distance below the filtration media surface)  
Underdrain Orifice Diameter = N/A inches

Calculated Parameters for Underdrain  
Underdrain Orifice Area = N/A ft<sup>2</sup>  
Underdrain Orifice Centroid = N/A feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice = 0.00 ft (relative to basin bottom at Stage = 0 ft)  
Depth at top of Zone using Orifice Plate = 2.36 ft (relative to basin bottom at Stage = 0 ft)  
Orifice Plate: Orifice Vertical Spacing = 9.40 inches  
Orifice Plate: Orifice Area per Row = 2.20 sq. inches (diameter = 1-11/16 inches)

Calculated Parameters for Plate  
WQ Orifice Area per Row = 1.528E-02 ft<sup>2</sup>  
Elliptical Half-Width = N/A feet  
Elliptical Slot Centroid = N/A feet  
Elliptical Slot Area = N/A ft<sup>2</sup>

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

|                                | Row 1 (required) | Row 2 (optional) | Row 3 (optional) | Row 4 (optional) | Row 5 (optional) | Row 6 (optional) | Row 7 (optional) | Row 8 (optional) |
|--------------------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|
| Stage of Orifice Centroid (ft) | 0.00             | 0.79             | 1.57             |                  |                  |                  |                  |                  |
| Orifice Area (sq. inches)      | 2.20             | 2.20             | 2.20             |                  |                  |                  |                  |                  |

|                                | Row 9 (optional) | Row 10 (optional) | Row 11 (optional) | Row 12 (optional) | Row 13 (optional) | Row 14 (optional) | Row 15 (optional) | Row 16 (optional) |
|--------------------------------|------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| Stage of Orifice Centroid (ft) |                  |                   |                   |                   |                   |                   |                   |                   |
| Orifice Area (sq. inches)      |                  |                   |                   |                   |                   |                   |                   |                   |

User Input: Vertical Orifice (Circular or Rectangular)

Invert of Vertical Orifice = 2.43 ft (relative to basin bottom at Stage = 0 ft)  
Depth at top of Zone using Vertical Orifice = 3.66 ft (relative to basin bottom at Stage = 0 ft)  
Vertical Orifice Height = 3.00 inches  
Vertical Orifice Width = 34.00 inches

Calculated Parameters for Vertical Orifice  
Zone 2 Rectangular Not Selected  
Vertical Orifice Area = 0.71 ft<sup>2</sup>  
Vertical Orifice Centroid = 0.13 feet

User Input: Overflow Weir (Dropbox with Flat or Sloped Gate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe))

Overflow Weir Front Edge Height, H<sub>o</sub> = 3.76 ft (relative to basin bottom at Stage = 0 ft)  
Overflow Weir Front Edge Length = 3.60 feet  
Overflow Weir Gate Slope = 3.00 H:V  
Horiz. Length of Weir Sides = 3.00 feet  
Overflow Gate Type = Type C Gate  
Debris Clogging % = 50%

Calculated Parameters for Overflow Weir  
Zone 3 Weir Not Selected  
Height of Gate Upper Edge, H<sub>u</sub> = 4.76 feet  
Overflow Weir Slope Length = 3.16 feet  
Gate Open Area / 100-yr Orifice Area = 2.48  
Overflow Gate Open Area w/o Debris = 7.92 ft<sup>2</sup>  
Overflow Gate Open Area w/ Debris = 3.96 ft<sup>2</sup>

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

Depth to Invert of Outlet Pipe = 1.00 ft (distance below basin bottom at Stage = 0 ft)  
Outlet Pipe Diameter = 28.00 inches  
Restrictor Plate Height Above Pipe Invert = 19.60 inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate  
Zone 3 Restrictor Not Selected  
Outlet Orifice Area = 3.20 ft<sup>2</sup>  
Outlet Orifice Centroid = 0.91 feet  
Half-Central Angle of Restrictor Plate on Pipe = 1.98 radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage = 8.80 ft (relative to basin bottom at Stage = 0 ft)  
Spillway Crest Length = 42.00 feet  
Spillway End Slopes = 4.00 H:V  
Freeboard above Max Water Surface = 1.00 feet

Calculated Parameters for Spillway  
Spillway Design Flow Depth = 0.95 feet  
Stage at Top of Freeboard = 10.75 feet  
Basin Area at Top of Freeboard = 1.31 acres  
Basin Volume at Top of Freeboard = 8.74 acre-ft

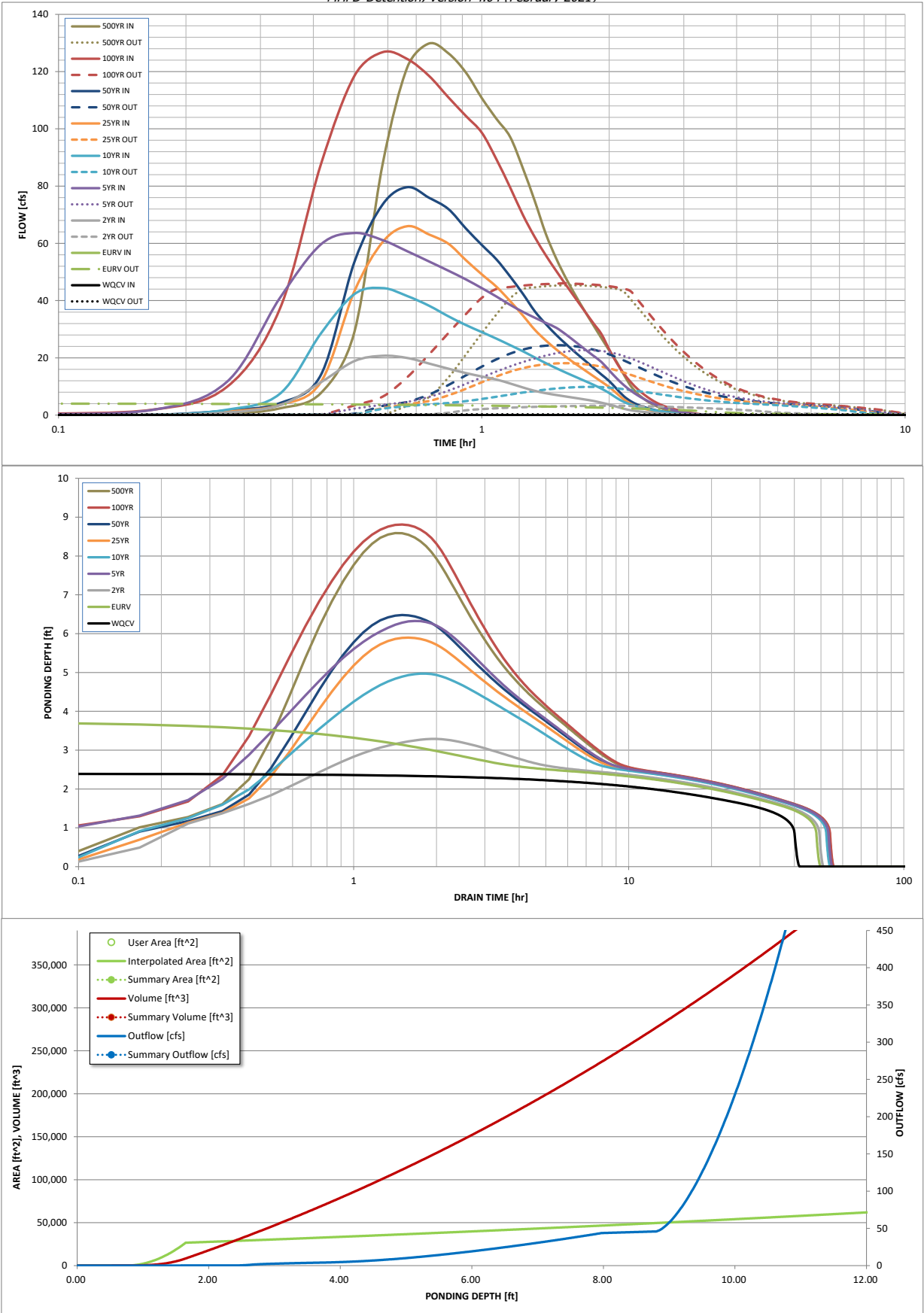
## Routed Hydrograph Results

The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).

|  | WQCV  | EURV            | 2 Year             | 5 Year          | 10 Year         | 25 Year         | 50 Year         | 100 Year | 500 Year       |
|--|-------|-----------------|--------------------|-----------------|-----------------|-----------------|-----------------|----------|----------------|
| Design Storm Return Period =                       | N/A   | N/A             | 1.19               | 1.50            | 1.75            | 2.00            | 2.25            | 2.52     | 3.14           |
| One-Hour Rainfall Depth (in) =                     | 0.664 | 1.623           | 1.643              | 2.665           | 3.605           | 5.023           | 6.095           | 7.524    | 10.289         |
| CUHP Runoff Volume (acre-ft) =                     | 0.664 | 1.623           | 1.643              | 2.665           | 3.605           | 5.023           | 6.095           | 7.524    | 10.289         |
| User Override Inflow Hydrograph Volume (acre-ft) = | N/A   | N/A             | 1.643              | 6.195           | 3.605           | 5.023           | 6.095           | 11.270   | 10.289         |
| CUHP Predevelopment Peak Q (cfs) =                 | N/A   | N/A             | 5.7                | 16.0            | 24.2            | 43.4            | 54.4            | 69.3     | 96.6           |
| OPTIONAL Override Predevelopment Peak Q (cfs) =    | N/A   | N/A             |                    | 22.7            |                 |                 |                 | 48.5     |                |
| Predevelopment Unit Peak Flow, q (cfs/acre) =      | N/A   | N/A             | 0.11               | 0.43            | 0.46            | 0.83            | 1.04            | 0.92     | 1.84           |
| Peak Inflow Q (cfs) =                              | N/A   | N/A             | 20.7               | 63.6            | 44.4            | 66.0            | 79.6            | 126.8    | 129.8          |
| Peak Outflow Q (cfs) =                             | 0.3   | 4.1             | 3.3                | 22.7            | 9.9             | 18.1            | 24.4            | 46.1     | 45.3           |
| Ratio Peak Outflow to Predevelopment Q =           | N/A   | N/A             | N/A                | 1.0             | 0.4             | 0.4             | 0.4             | 0.9      | 0.5            |
| Structure Controlling Flow =                       | Plate | Overflow Weir 1 | Vertical Orifice 1 | Overflow Weir 1 | Overflow Weir 1 | Overflow Weir 1 | Overflow Weir 1 | Spillway | Outlet Plate 1 |
| Max Velocity through Gate 1 (fps) =                | N/A   | N/A             | N/A                | 2.0             | 0.5             | 1.4             | 2.2             | 4.6      | 4.6            |
| Max Velocity through Gate 2 (fps) =                | N/A   | N/A             | N/A                | N/A             | N/A             | N/A             | N/A             | N/A      | N/A            |
| Time to Drain 97% of Inflow Volume (hours) =       | 39    | 44              | 45                 | 38              | 43              | 40              | 38              | 30       | 31             |
| Time to Drain 99% of Inflow Volume (hours) =       | 40    | 47              | 48                 | 48              | 49              | 49              | 48              | 44       | 45             |
| Maximum Ponding Depth (ft) =                       | 2.40  | 3.76            | 3.29               | 6.33            | 4.97            | 5.90            | 6.48            | 8.81     | 8.59           |
| Area at Maximum Ponding Depth (acres) =            | 0.66  | 0.75            | 0.72               | 0.94            | 0.84            | 0.91            | 0.95            | 1.14     | 1.12           |
| Maximum Volume Stored (acre-ft) =                  | 0.668 | 1.627           | 1.275              | 3.786           | 2.580           | 3.390           | 3.928           | 6.368    | 6.108          |

DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.04 (February 2021)



| S-A-V-D Chart Axis Override | X-axis | Left Y-Axis | Right Y-Axis |
|-----------------------------|--------|-------------|--------------|
| minimum bound               |        |             |              |
| maximum bound               |        |             |              |

# DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename: ...[SWM]Outflow hydrographs\Pond6 OutflowHydrograph.xlsx

## Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

|               | SOURCE  | CUHP       | CUHP       | CUHP         | USER         | CUHP          | CUHP          | CUHP          | USER           | CUHP           |
|---------------|---------|------------|------------|--------------|--------------|---------------|---------------|---------------|----------------|----------------|
| Time Interval | TIME    | WQCV [cfs] | EURV [cfs] | 2 Year [cfs] | 5 Year [cfs] | 10 Year [cfs] | 25 Year [cfs] | 50 Year [cfs] | 100 Year [cfs] | 500 Year [cfs] |
| 5.00 min      | 0:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 0:05:00 | 0.00       | 0.00       | 0.00         | 0.13         | 0.00          | 0.00          | 0.00          | 0.33           | 0.00           |
|               | 0:10:00 | 0.00       | 0.00       | 0.00         | 1.83         | 0.00          | 0.00          | 0.11          | 1.89           | 0.35           |
|               | 0:15:00 | 0.00       | 0.00       | 0.91         | 11.64        | 1.89          | 1.28          | 1.63          | 9.87           | 2.36           |
|               | 0:20:00 | 0.00       | 0.00       | 3.46         | 40.91        | 7.45          | 3.55          | 4.20          | 37.13          | 7.71           |
|               | 0:25:00 | 0.00       | 0.00       | 11.48        | 59.62        | 28.51         | 11.54         | 14.03         | 87.57          | 29.01          |
|               | 0:30:00 | 0.00       | 0.00       | 18.87        | 63.61        | 42.26         | 43.25         | 53.46         | 118.46         | 87.82          |
|               | 0:35:00 | 0.00       | 0.00       | 20.73        | 61.11        | 44.37         | 60.48         | 73.62         | 126.79         | 121.47         |
|               | 0:40:00 | 0.00       | 0.00       | 19.96        | 57.24        | 41.59         | 65.99         | 79.62         | 124.39         | 129.80         |
|               | 0:45:00 | 0.00       | 0.00       | 18.03        | 53.69        | 38.23         | 63.11         | 75.94         | 118.52         | 126.42         |
|               | 0:50:00 | 0.00       | 0.00       | 16.23        | 50.46        | 34.54         | 59.90         | 72.01         | 111.04         | 119.71         |
|               | 0:55:00 | 0.00       | 0.00       | 14.69        | 47.42        | 31.48         | 54.16         | 65.22         | 104.53         | 110.75         |
|               | 1:00:00 | 0.00       | 0.00       | 13.49        | 44.36        | 29.00         | 49.17         | 59.44         | 98.67          | 103.46         |
|               | 1:05:00 | 0.00       | 0.00       | 12.42        | 41.41        | 26.70         | 44.83         | 54.37         | 89.30          | 97.18          |
|               | 1:10:00 | 0.00       | 0.00       | 11.05        | 38.52        | 24.44         | 39.84         | 48.42         | 79.54          | 86.29          |
|               | 1:15:00 | 0.00       | 0.00       | 9.67         | 36.09        | 22.31         | 34.83         | 42.42         | 69.99          | 74.89          |
|               | 1:20:00 | 0.00       | 0.00       | 8.49         | 34.04        | 20.16         | 29.85         | 36.33         | 62.24          | 63.32          |
|               | 1:25:00 | 0.00       | 0.00       | 7.64         | 32.21        | 18.16         | 26.08         | 31.81         | 55.82          | 54.62          |
|               | 1:30:00 | 0.00       | 0.00       | 7.02         | 30.50        | 16.38         | 22.93         | 27.98         | 50.32          | 47.61          |
|               | 1:35:00 | 0.00       | 0.00       | 6.48         | 28.09        | 14.79         | 20.27         | 24.73         | 45.34          | 41.70          |
|               | 1:40:00 | 0.00       | 0.00       | 5.97         | 25.54        | 13.34         | 17.87         | 21.79         | 40.71          | 36.37          |
|               | 1:45:00 | 0.00       | 0.00       | 5.47         | 23.07        | 11.96         | 15.71         | 19.14         | 36.32          | 31.50          |
|               | 1:50:00 | 0.00       | 0.00       | 4.98         | 20.78        | 10.64         | 13.66         | 16.61         | 32.17          | 26.90          |
|               | 1:55:00 | 0.00       | 0.00       | 4.34         | 18.57        | 9.24          | 11.69         | 14.19         | 28.35          | 22.58          |
|               | 2:00:00 | 0.00       | 0.00       | 3.69         | 15.62        | 7.71          | 9.81          | 11.89         | 22.96          | 18.59          |
|               | 2:05:00 | 0.00       | 0.00       | 2.93         | 12.84        | 5.99          | 7.59          | 9.15          | 18.22          | 14.08          |
|               | 2:10:00 | 0.00       | 0.00       | 2.21         | 10.46        | 4.61          | 5.47          | 6.57          | 14.45          | 10.15          |
|               | 2:15:00 | 0.00       | 0.00       | 1.69         | 8.53         | 3.67          | 3.96          | 4.83          | 11.50          | 7.51           |
|               | 2:20:00 | 0.00       | 0.00       | 1.35         | 6.94         | 2.99          | 2.97          | 3.67          | 9.12           | 5.66           |
|               | 2:25:00 | 0.00       | 0.00       | 1.10         | 5.63         | 2.43          | 2.27          | 2.82          | 7.22           | 4.23           |
|               | 2:30:00 | 0.00       | 0.00       | 0.90         | 4.51         | 1.97          | 1.74          | 2.17          | 5.65           | 3.15           |
|               | 2:35:00 | 0.00       | 0.00       | 0.73         | 3.57         | 1.58          | 1.34          | 1.67          | 4.39           | 2.31           |
|               | 2:40:00 | 0.00       | 0.00       | 0.59         | 2.79         | 1.24          | 1.03          | 1.28          | 3.45           | 1.66           |
|               | 2:45:00 | 0.00       | 0.00       | 0.47         | 2.19         | 0.97          | 0.78          | 0.97          | 2.73           | 1.21           |
|               | 2:50:00 | 0.00       | 0.00       | 0.38         | 1.71         | 0.75          | 0.60          | 0.75          | 2.18           | 0.93           |
|               | 2:55:00 | 0.00       | 0.00       | 0.31         | 1.30         | 0.58          | 0.47          | 0.58          | 1.71           | 0.74           |
|               | 3:00:00 | 0.00       | 0.00       | 0.25         | 0.95         | 0.45          | 0.37          | 0.46          | 1.29           | 0.59           |
|               | 3:05:00 | 0.00       | 0.00       | 0.19         | 0.66         | 0.35          | 0.29          | 0.35          | 0.93           | 0.46           |
|               | 3:10:00 | 0.00       | 0.00       | 0.15         | 0.44         | 0.26          | 0.22          | 0.27          | 0.63           | 0.34           |
|               | 3:15:00 | 0.00       | 0.00       | 0.11         | 0.27         | 0.18          | 0.16          | 0.19          | 0.39           | 0.24           |
|               | 3:20:00 | 0.00       | 0.00       | 0.07         | 0.14         | 0.12          | 0.11          | 0.13          | 0.20           | 0.16           |
|               | 3:25:00 | 0.00       | 0.00       | 0.05         | 0.05         | 0.07          | 0.07          | 0.08          | 0.08           | 0.09           |
|               | 3:30:00 | 0.00       | 0.00       | 0.02         | 0.01         | 0.04          | 0.04          | 0.04          | 0.01           | 0.05           |
|               | 3:35:00 | 0.00       | 0.00       | 0.01         | 0.00         | 0.01          | 0.01          | 0.02          | 0.00           | 0.01           |
|               | 3:40:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:45:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:50:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:55:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:05:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:10:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:15:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:20:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:25:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:30:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:35:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:40:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:45:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:50:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:55:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:05:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:10:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:15:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:20:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:25:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:30:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:35:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:40:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:45:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:50:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:55:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 6:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |

0 5:50:00 0

## DETENTION BASIN OUTLET STRUCTURE DESIGN

*MHFD-Detention, Version 4.04 (February 2021)*

### Summary Stage-Area-Volume-Discharge Relationships

The user can create a summary S-A-V-D by entering the desired stage increments and the remainder of the table will populate automatically.

The user should graphically compare the summary S-A-V-D table to the full S-A-V-D table in the chart to confirm it captures all key transition points.

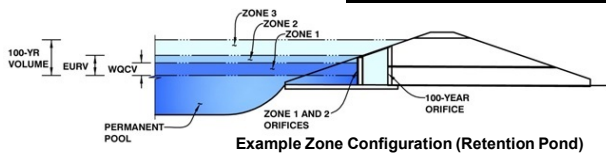
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# DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-DETENTION, Version 4.04 (February 2021)

Project: Flying Horse North MDDP

Basin ID: Pond 4



Example Zone Configuration (Retention Pond)

|                   | Estimated Stage (ft) | Estimated Volume (ac-ft) | Outlet Type          |
|-------------------|----------------------|--------------------------|----------------------|
| Zone 1 (WQCV)     | 2.90                 | 1.201                    | Orifice Plate        |
| Zone 2 (5-year)   | 4.54                 | 1.398                    | Weir&Pipe (Circular) |
| Zone 3 (100-year) | 8.10                 | 3.853                    | Weir&Pipe (Restrict) |
| Total (all zones) |                      | 6.452                    |                      |

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth =  ft (distance below the filtration media surface)  
Underdrain Orifice Diameter =  inches

Calculated Parameters for Underdrain  
Underdrain Orifice Area =  ft<sup>2</sup>  
Underdrain Orifice Centroid =  feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice =  ft (relative to basin bottom at Stage = 0 ft)  
Depth at top of Zone using Orifice Plate =  ft (relative to basin bottom at Stage = 0 ft)  
Orifice Plate: Orifice Vertical Spacing =  inches  
Orifice Plate: Orifice Area per Row =  sq. inches (use rectangular openings)

Calculated Parameters for Plate  
WQ Orifice Area per Row =  ft<sup>2</sup>  
Elliptical Half-Width =  feet  
Elliptical Slot Centroid =  feet  
Elliptical Slot Area =  ft<sup>2</sup>

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

|                                | Row 1 (required) | Row 2 (optional) | Row 3 (optional) | Row 4 (optional) | Row 5 (optional) | Row 6 (optional) | Row 7 (optional) | Row 8 (optional) |
|--------------------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|
| Stage of Orifice Centroid (ft) | 0.00             | 1.51             | 3.03             |                  |                  |                  |                  |                  |
| Orifice Area (sq. inches)      | 5.55             | 5.55             | 5.55             |                  |                  |                  |                  |                  |

|                                | Row 9 (optional) | Row 10 (optional) | Row 11 (optional) | Row 12 (optional) | Row 13 (optional) | Row 14 (optional) | Row 15 (optional) | Row 16 (optional) |
|--------------------------------|------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| Stage of Orifice Centroid (ft) |                  |                   |                   |                   |                   |                   |                   |                   |
| Orifice Area (sq. inches)      |                  |                   |                   |                   |                   |                   |                   |                   |

User Input: Vertical Orifice (Circular or Rectangular)

Invert of Vertical Orifice =  ft (relative to basin bottom at Stage = 0 ft)  
Depth at top of Zone using Vertical Orifice =  ft (relative to basin bottom at Stage = 0 ft)  
Vertical Orifice Diameter =  inches

Calculated Parameters for Vertical Orif  
Vertical Orifice Area =  ft<sup>2</sup>  
Vertical Orifice Centroid =  feet

User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe)

Overflow Weir Front Edge Height, Ho =  ft (relative to basin bottom at Stage = 0 ft)  
Overflow Weir Front Edge Length =  feet  
Overflow Weir Grate Slope =  H:V  
Horiz. Length of Weir Sides =  feet  
Overflow Grate Type =   
Debris Clogging % =  %

Calculated Parameters for Overflow W  
Height of Grate Upper Edge, H<sub>1</sub> =  ft  
Overflow Weir Slope Length =  feet  
Grate Open Area / 100-yr Orifice Area =   
Overflow Grate Open Area w/o Debris =   
Overflow Grate Open Area w/ Debris =

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

Depth to Invert of Outlet Pipe =  ft (distance below basin bottom at Stage = 0 ft)  
Circular Orifice Diameter or Pipe Diameter =  inches  
Restrictor Plate Height Above Pipe Invert =  inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Pl  
Outlet Orifice Area =  ft<sup>2</sup>  
Outlet Orifice Centroid =  feet  
Half-Central Angle of Restrictor Plate on Pipe =

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage =  ft (relative to basin bottom at Stage = 0 ft)  
Spillway Crest Length =  feet  
Spillway End Slopes =  H:V  
Freeboard above Max Water Surface =  feet

Calculated Parameters for Spillway  
Spillway Design Flow Depth =  feet  
Stage at Top of Freeboard =  feet  
Basin Area at Top of Freeboard =  acres  
Basin Volume at Top of Freeboard =  acre-ft

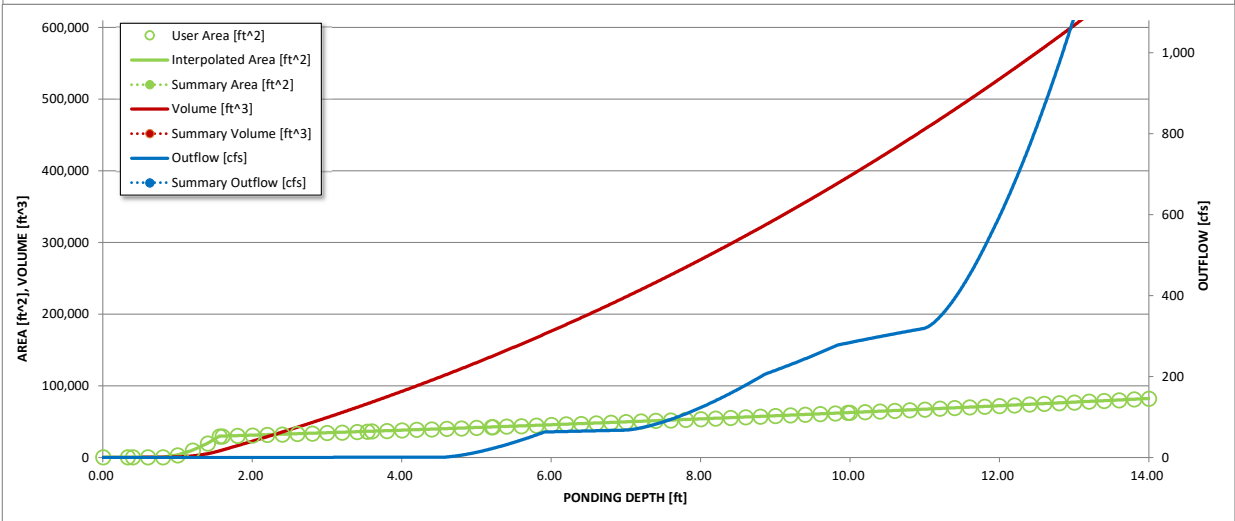
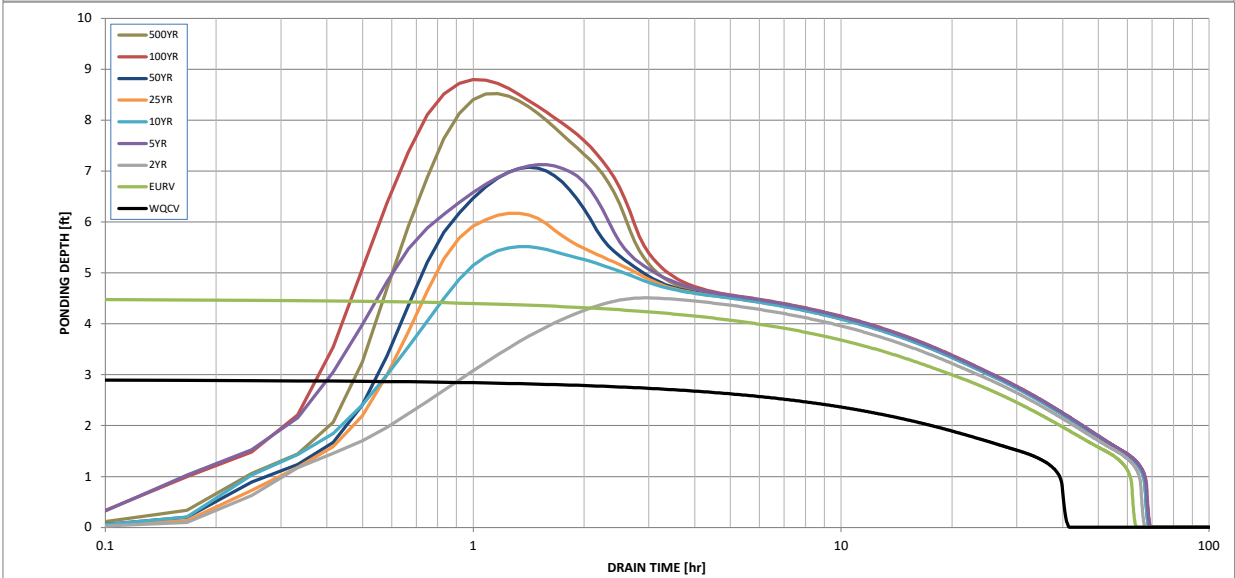
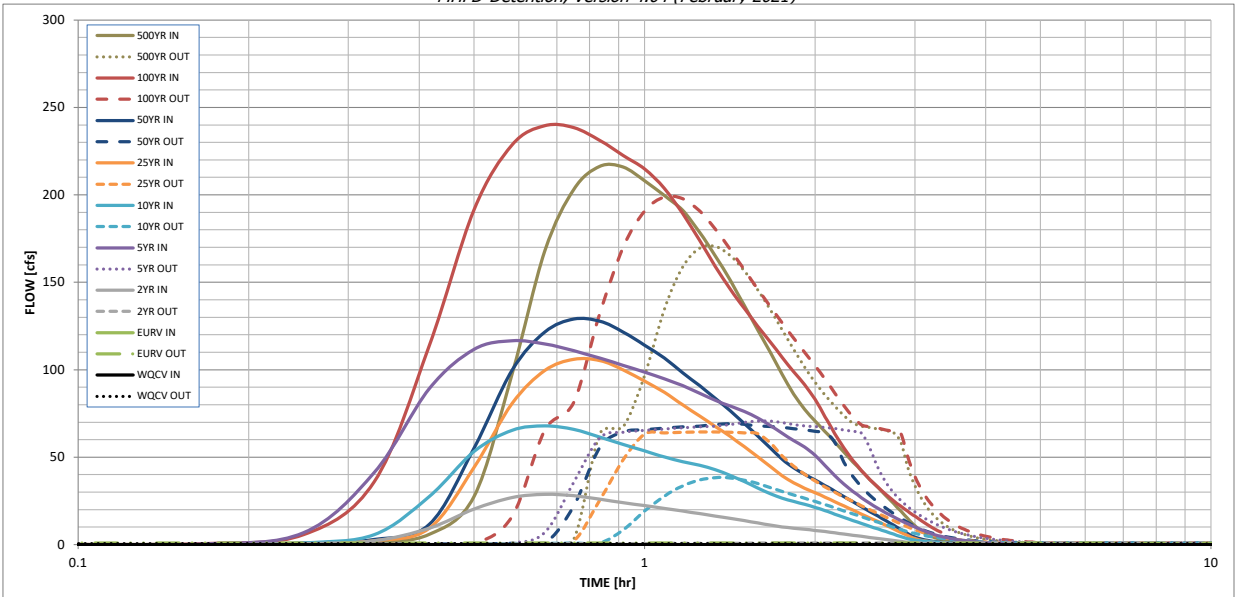
## Routed Hydrograph Results

The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AI)

|  | WQCV  | EURV  | 2 Year | 5 Year          | 10 Year         | 25 Year        | 50 Year         | 100 Year        |
|--|-------|-------|--------|-----------------|-----------------|----------------|-----------------|-----------------|
| Design Storm Return Period =                       | N/A   | N/A   | 1.19   | 1.50            | 1.75            | 2.00           | 2.25            | 2.52            |
| One-Hour Rainfall Depth (in) =                     | N/A   | N/A   | 1.19   | 1.50            | 1.75            | 2.00           | 2.25            | 2.52            |
| CUHP Runoff Volume (acre-ft) =                     | 1.201 | 2.555 | 2.764  | 4.915           | 6.951           | 10.216         | 12.579          | 15.835          |
| User Override Inflow Hydrograph Volume (acre-ft) = | N/A   | N/A   | 2.764  | 14.585          | 6.951           | 10.216         | 12.579          | 26.746          |
| CUHP Predevelopment Peak Q (cfs) =                 | N/A   | N/A   | 10.7   | 29.9            | 46.0            | 84.0           | 105.5           | 134.7           |
| OPTIONAL Override Predevelopment Peak Q (cfs) =    | N/A   | N/A   |        | 69.9            |                 |                |                 | 231.6           |
| Predevelopment Unit Peak Flow, q (cfs/acre) =      | N/A   | N/A   | 0.09   | 0.60            | 0.39            | 0.72           | 0.90            | 1.97            |
| Peak Inflow Q (cfs) =                              | N/A   | N/A   | 28.7   | 116.6           | 67.8            | 106.0          | 128.9           | 239.6           |
| Peak Outflow Q (cfs) =                             | 0.5   | 0.9   | 0.9    | 70.6            | 38.3            | 64.4           | 69.2            | 198.8           |
| Ratio Peak Outflow to Predevelopment Q =           | N/A   | N/A   | N/A    | 1.0             | 0.8             | 0.8            | 0.7             | 0.9             |
| Structure Controlling Flow =                       | Plate | Plate | Plate  | Overflow Weir 2 | Overflow Weir 1 | Outlet Plate 1 | Overflow Weir 2 | Overflow Weir 2 |
| Max Velocity through Grate 1 (fps) =               | N/A   | N/A   | N/A    | 2.7             | 1.5             | 2.5            | 2.7             | 2.9             |
| Max Velocity through Grate 2 (fps) =               | N/A   | N/A   | N/A    | 0.1             | N/A             | N/A            | 0.0             | 3.0             |
| Time to Drain 97% of Inflow Volume (hours) =       | 38    | 58    | 61     | 48              | 56              | 52             | 50              | 38              |
| Time to Drain 99% of Inflow Volume (hours) =       | 40    | 61    | 64     | 60              | 64              | 62             | 60              | 54              |
| Maximum Ponding Depth (ft) =                       | 2.90  | 4.49  | 4.51   | 7.12            | 5.52            | 6.17           | 7.07            | 8.79            |
| Area at Maximum Ponding Depth (acres) =            | 0.79  | 0.92  | 0.92   | 1.16            | 1.01            | 1.07           | 1.15            | 1.32            |
| Maximum Volume Stored (acre-ft) =                  | 1.203 | 2.560 | 2.569  | 5.284           | 3.543           | 4.228          | 5.226           | 7.349           |

DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-DETENTION, Version 4.04 (February 2021)



| S-A-V-D Chart Axis Override | X-axis | Left Y-Axis | Right Y-Axis |
|-----------------------------|--------|-------------|--------------|
| minimum bound               |        |             |              |
| maximum bound               |        |             |              |



# DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename: \_\_\_\_\_

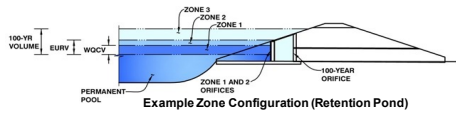
## Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

|               | SOURCE  | CUHP       | CUHP       | CUHP         | USER         | CUHP          | CUHP          | CUHP          | USER           | CUHP           |
|---------------|---------|------------|------------|--------------|--------------|---------------|---------------|---------------|----------------|----------------|
| Time Interval | TIME    | WQCV [cfs] | EURV [cfs] | 2 Year [cfs] | 5 Year [cfs] | 10 Year [cfs] | 25 Year [cfs] | 50 Year [cfs] | 100 Year [cfs] | 500 Year [cfs] |
| 5.00 min      | 0:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 0:05:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.01           | 0.00           |
|               | 0:10:00 | 0.00       | 0.00       | 0.00         | 0.36         | 0.00          | 0.00          | 0.06          | 0.49           | 0.18           |
|               | 0:15:00 | 0.00       | 0.00       | 0.48         | 6.73         | 0.99          | 0.67          | 0.88          | 5.67           | 1.32           |
|               | 0:20:00 | 0.00       | 0.00       | 2.13         | 41.21        | 5.65          | 2.26          | 2.89          | 35.90          | 5.82           |
|               | 0:25:00 | 0.00       | 0.00       | 9.38         | 89.05        | 27.50         | 9.26          | 11.47         | 113.64         | 27.45          |
|               | 0:30:00 | 0.00       | 0.00       | 20.30        | 111.59       | 53.20         | 44.07         | 55.13         | 191.47         | 97.49          |
|               | 0:35:00 | 0.00       | 0.00       | 26.92        | 116.56       | 65.38         | 80.67         | 99.67         | 228.61         | 167.89         |
|               | 0:40:00 | 0.00       | 0.00       | 28.75        | 114.74       | 67.85         | 99.55         | 121.59        | 239.57         | 203.14         |
|               | 0:45:00 | 0.00       | 0.00       | 27.97        | 110.81       | 65.87         | 105.99        | 128.94        | 238.45         | 216.31         |
|               | 0:50:00 | 0.00       | 0.00       | 25.92        | 106.63       | 61.53         | 105.24        | 127.82        | 231.20         | 215.91         |
|               | 0:55:00 | 0.00       | 0.00       | 23.93        | 102.54       | 57.32         | 99.95         | 121.53        | 222.57         | 208.11         |
|               | 1:00:00 | 0.00       | 0.00       | 22.26        | 98.67        | 53.59         | 93.45         | 114.06        | 214.84         | 199.58         |
|               | 1:05:00 | 0.00       | 0.00       | 20.71        | 94.84        | 50.07         | 87.10         | 106.71        | 203.76         | 191.23         |
|               | 1:10:00 | 0.00       | 0.00       | 19.18        | 90.87        | 47.47         | 79.98         | 98.34         | 189.33         | 178.69         |
|               | 1:15:00 | 0.00       | 0.00       | 17.72        | 86.57        | 45.43         | 73.58         | 90.88         | 174.06         | 165.11         |
|               | 1:20:00 | 0.00       | 0.00       | 16.34        | 82.55        | 42.85         | 67.61         | 83.67         | 159.11         | 151.09         |
|               | 1:25:00 | 0.00       | 0.00       | 15.00        | 79.15        | 39.55         | 61.79         | 76.45         | 146.10         | 136.67         |
|               | 1:30:00 | 0.00       | 0.00       | 13.68        | 76.09        | 36.01         | 55.97         | 69.25         | 135.00         | 122.93         |
|               | 1:35:00 | 0.00       | 0.00       | 12.39        | 72.49        | 32.45         | 50.28         | 62.20         | 125.07         | 109.91         |
|               | 1:40:00 | 0.00       | 0.00       | 11.15        | 68.09        | 29.09         | 44.69         | 55.31         | 115.83         | 97.41          |
|               | 1:45:00 | 0.00       | 0.00       | 10.11        | 63.64        | 26.50         | 39.42         | 48.83         | 107.08         | 86.08          |
|               | 1:50:00 | 0.00       | 0.00       | 9.38         | 59.52        | 24.62         | 35.39         | 43.95         | 98.86          | 77.49          |
|               | 1:55:00 | 0.00       | 0.00       | 8.76         | 55.77        | 22.98         | 32.29         | 40.17         | 91.43          | 70.60          |
|               | 2:00:00 | 0.00       | 0.00       | 8.13         | 51.08        | 21.28         | 29.70         | 36.99         | 83.00          | 64.62          |
|               | 2:05:00 | 0.00       | 0.00       | 7.45         | 45.18        | 19.40         | 27.11         | 33.76         | 73.06          | 58.71          |
|               | 2:10:00 | 0.00       | 0.00       | 6.72         | 39.50        | 17.45         | 24.54         | 30.53         | 63.57          | 52.86          |
|               | 2:15:00 | 0.00       | 0.00       | 6.01         | 34.58        | 15.56         | 22.07         | 27.42         | 55.20          | 47.30          |
|               | 2:20:00 | 0.00       | 0.00       | 5.34         | 30.40        | 13.75         | 19.69         | 24.44         | 48.18          | 42.08          |
|               | 2:25:00 | 0.00       | 0.00       | 4.70         | 26.78        | 12.05         | 17.43         | 21.62         | 42.28          | 37.24          |
|               | 2:30:00 | 0.00       | 0.00       | 4.09         | 23.59        | 10.43         | 15.25         | 18.91         | 37.20          | 32.58          |
|               | 2:35:00 | 0.00       | 0.00       | 3.50         | 20.73        | 8.90          | 13.13         | 16.27         | 32.73          | 28.03          |
|               | 2:40:00 | 0.00       | 0.00       | 2.92         | 18.16        | 7.42          | 11.04         | 13.68         | 28.74          | 23.55          |
|               | 2:45:00 | 0.00       | 0.00       | 2.35         | 15.85        | 5.98          | 8.99          | 11.15         | 25.16          | 19.13          |
|               | 2:50:00 | 0.00       | 0.00       | 1.80         | 13.75        | 4.59          | 6.98          | 8.65          | 21.91          | 14.79          |
|               | 2:55:00 | 0.00       | 0.00       | 1.28         | 11.84        | 3.38          | 5.04          | 6.26          | 18.95          | 10.72          |
|               | 3:00:00 | 0.00       | 0.00       | 0.92         | 10.10        | 2.62          | 3.40          | 4.29          | 16.20          | 7.55           |
|               | 3:05:00 | 0.00       | 0.00       | 0.72         | 8.49         | 2.13          | 2.42          | 3.11          | 13.61          | 5.49           |
|               | 3:10:00 | 0.00       | 0.00       | 0.59         | 7.01         | 1.76          | 1.78          | 2.31          | 11.16          | 4.04           |
|               | 3:15:00 | 0.00       | 0.00       | 0.49         | 5.74         | 1.45          | 1.33          | 1.75          | 8.92           | 2.96           |
|               | 3:20:00 | 0.00       | 0.00       | 0.41         | 4.74         | 1.19          | 1.01          | 1.34          | 7.06           | 2.16           |
|               | 3:25:00 | 0.00       | 0.00       | 0.33         | 3.97         | 0.96          | 0.79          | 1.03          | 5.65           | 1.55           |
|               | 3:30:00 | 0.00       | 0.00       | 0.27         | 3.35         | 0.77          | 0.60          | 0.79          | 4.58           | 1.10           |
|               | 3:35:00 | 0.00       | 0.00       | 0.22         | 2.82         | 0.60          | 0.47          | 0.61          | 3.73           | 0.82           |
|               | 3:40:00 | 0.00       | 0.00       | 0.18         | 2.36         | 0.46          | 0.37          | 0.48          | 3.04           | 0.64           |
|               | 3:45:00 | 0.00       | 0.00       | 0.15         | 1.96         | 0.35          | 0.29          | 0.37          | 2.45           | 0.50           |
|               | 3:50:00 | 0.00       | 0.00       | 0.11         | 1.61         | 0.27          | 0.22          | 0.29          | 1.98           | 0.40           |
|               | 3:55:00 | 0.00       | 0.00       | 0.09         | 1.31         | 0.20          | 0.17          | 0.22          | 1.60           | 0.31           |
|               | 4:00:00 | 0.00       | 0.00       | 0.06         | 1.06         | 0.15          | 0.13          | 0.16          | 1.30           | 0.23           |
|               | 4:05:00 | 0.00       | 0.00       | 0.04         | 0.85         | 0.10          | 0.09          | 0.11          | 1.05           | 0.16           |
|               | 4:10:00 | 0.00       | 0.00       | 0.03         | 0.67         | 0.06          | 0.06          | 0.07          | 0.85           | 0.10           |
|               | 4:15:00 | 0.00       | 0.00       | 0.01         | 0.52         | 0.03          | 0.03          | 0.04          | 0.67           | 0.06           |
|               | 4:20:00 | 0.00       | 0.00       | 0.01         | 0.39         | 0.01          | 0.02          | 0.02          | 0.51           | 0.03           |
|               | 4:25:00 | 0.00       | 0.00       | 0.00         | 0.28         | 0.00          | 0.00          | 0.01          | 0.38           | 0.01           |
|               | 4:30:00 | 0.00       | 0.00       | 0.00         | 0.20         | 0.00          | 0.00          | 0.00          | 0.27           | 0.00           |
|               | 4:35:00 | 0.00       | 0.00       | 0.00         | 0.14         | 0.00          | 0.00          | 0.00          | 0.18           | 0.00           |
|               | 4:40:00 | 0.00       | 0.00       | 0.00         | 0.09         | 0.00          | 0.00          | 0.00          | 0.12           | 0.00           |
|               | 4:45:00 | 0.00       | 0.00       | 0.00         | 0.05         | 0.00          | 0.00          | 0.00          | 0.07           | 0.00           |
|               | 4:50:00 | 0.00       | 0.00       | 0.00         | 0.03         | 0.00          | 0.00          | 0.00          | 0.04           | 0.00           |
|               | 4:55:00 | 0.00       | 0.00       | 0.00         | 0.02         | 0.00          | 0.00          | 0.00          | 0.02           | 0.00           |
|               | 5:00:00 | 0.00       | 0.00       | 0.00         | 0.01         | 0.00          | 0.00          | 0.00          | 0.01           | 0.00           |
|               | 5:05:00 | 0.00       | 0.00       | 0.00         | 0.01         | 0.00          | 0.00          | 0.00          | 0.01           | 0.00           |
|               | 5:10:00 | 0.00       | 0.00       | 0.00         | 0.01         | 0.00          | 0.00          | 0.00          | 0.01           | 0.00           |
|               | 5:15:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:20:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:25:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:30:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:35:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:40:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:45:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:50:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:55:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 6:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |

*MHFD-Detention, Version 4.04 (February 2021)*

**Basin ID: Pond 4**



### Example Zone Configuration (Retention Pond)

|   |                           |         |
|---|---------------------------|---------|
| Selected BMP Type =                     | <b>EDB</b>                |         |
| Watershed Area =                        | 117.41                    | acres   |
| Watershed Length =                      | 4,350                     | ft      |
| Watershed Length to Centroid =          | 2,200                     | ft      |
| Watershed Slope =                       | 0.036                     | ft/ft   |
| Watershed Imperviousness =              | 21.76%                    | percent |
| Percentage Hydrologic Soil Group A =    | 0.0%                      | percent |
| Percentage Hydrologic Soil Group B =    | 100.0%                    | percent |
| Percentage Hydrologic Soil Groups C/D = | 0.0%                      | percent |
| Target WQCV Drain Time =                | 40.0                      | hours   |
| Location for 1-hr Rainfall Depths =     | Denver - Capitol Building |         |

After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

|   |        |           |
|---|--------|-----------|
| Water Quality Capture Volume (WQCV) =     | 1.201  | acre-feet |
| Excess Urban Runoff Volume (EUOV) =       | 2.555  | acre-feet |
| 2-yr Runoff Volume ( $P1 = 1.19$ in.) =   | 2.764  | acre-feet |
| 5-yr Runoff Volume ( $P1 = 1.5$ in.) =    | 4.915  | acre-feet |
| 10-yr Runoff Volume ( $P1 = 1.75$ in.) =  | 6.951  | acre-feet |
| 25-yr Runoff Volume ( $P1 = 1$ in.) =     | 10.216 | acre-feet |
| 50-yr Runoff Volume ( $P1 = 2.25$ in.) =  | 12.579 | acre-feet |
| 100-yr Runoff Volume ( $P1 = 2.52$ in.) = | 15.835 | acre-feet |
| 500-yr Runoff Volume ( $P1 = 3.14$ in.) = | 21.570 | acre-feet |
| Approximate 2-yr Detention Volume =       | 1.768  | acre-feet |
| Approximate 5-yr Detention Volume =       | 2.599  | acre-feet |
| Approximate 10-yr Detention Volume =      | 4.104  | acre-feet |
| Approximate 25-yr Detention Volume =      | 5.007  | acre-feet |
| Approximate 50-yr Detention Volume =      | 5.288  | acre-feet |
| Approximate 100-yr Detention Volume =     | 6.452  | acre-feet |

|   |       |                 |
|---|-------|-----------------|
| Zone 1 Volume (WQCV) =                            | 1.201 | acre-feet       |
| Zone 2 Volume (5-year - Zone 1) =                 | 1.398 | acre-feet       |
| Zone 3 Volume (100-year - Zones 1 & 2) =          | 3.853 | acre-feet       |
| Total Detention Basin Volume =                    | 6.452 | acre-feet       |
| Initial Surge Volume (ISV) =                      | user  | ft <sup>3</sup> |
| Initial Surge Depth (ISD) =                       | user  | ft              |
| Total Available Detention Depth ( $H_{total}$ ) = | user  | ft              |
| Depth of Trickle Channel ( $H_{TC}$ ) =           | user  | ft              |
| Slope of Trickle Channel ( $S_{TC}$ ) =           | user  | ft/ft           |
| Slopes of Main Basin Sides ( $S_{main}$ ) =       | user  | H:V             |
| Basin Length-to-Width Ratio ( $R_{L/W}$ ) =       | user  |                 |

|   |   |      |                 |
|---|---|------|-----------------|
| Initial Surcharge Area ( $A_{SV}$ )         | = | user | ft <sup>2</sup> |
| Surcharge Volume Length ( $L_{SV}$ )        | = | user | ft              |
| Surcharge Volume Width ( $W_{SV}$ )         | = | user | ft              |
| Depth of Basin Floor ( $H_{LFLOOR}$ )       | = | user | ft              |
| Length of Basin Floor ( $L_{LFLOOR}$ )      | = | user | ft              |
| Width of Basin Floor ( $W_{LFLOOR}$ )       | = | user | ft              |
| Area of Basin Floor ( $A_{LFLOOR}$ )        | = | user | ft <sup>2</sup> |
| Volume of Basin Floor ( $V_{LFLOOR}$ )      | = | user | ft <sup>3</sup> |
| Depth of Main Basin ( $H_{MAIN}$ )          | = | user | ft              |
| Length of Main Basin ( $L_{MAIN}$ )         | = | user | ft              |
| Width of Main Basin ( $W_{MAIN}$ )          | = | user | ft              |
| Area of Main Basin ( $A_{MAIN}$ )           | = | user | ft <sup>2</sup> |
| Volume of Main Basin ( $V_{MAIN}$ )         | = | user | ft <sup>3</sup> |
| Calculated Total Basin Volume ( $V_{BSA}$ ) | = | user | acre-feet       |

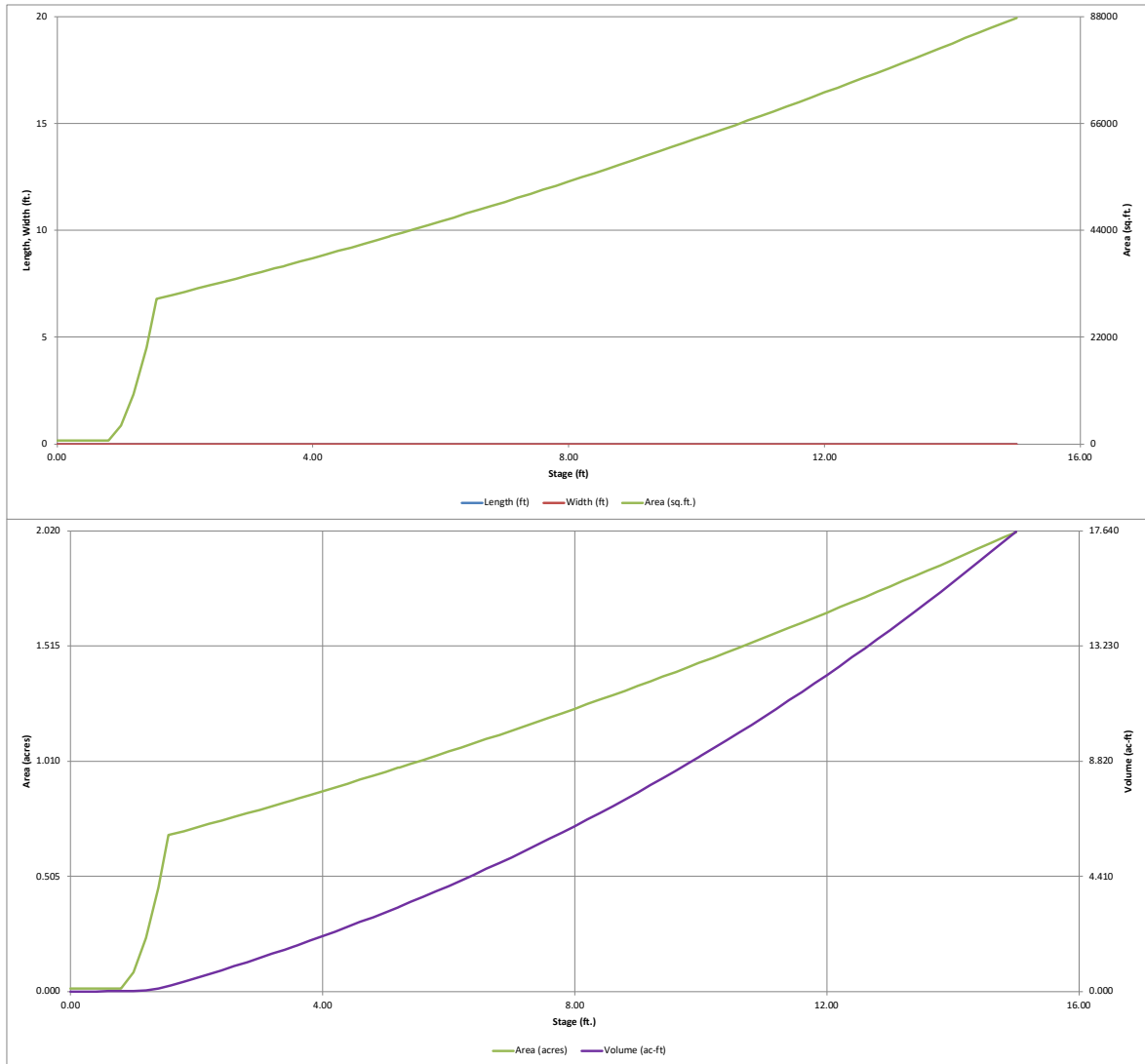
### Optional User Overrides

|      |           |
|------|-----------|
|      | acre-feet |
|      | acre-feet |
| 1.19 | inches    |
| 1.50 | inches    |
| 1.75 | inches    |
| 2.00 | inches    |
| 2.25 | inches    |
| 2.52 | inches    |
|      | inches    |

| Depth Increment =           | 0.20       |                              |             |            |                         |   |             |                           |                |
|-----------------------------|------------|------------------------------|-------------|------------|-------------------------|---|-------------|---------------------------|----------------|
| Stage - Storage Description | Stage (ft) | Optional Override Stage (ft) | Length (ft) | Width (ft) | Area (ft <sup>2</sup> ) | Optional Override Area (ft <sup>2</sup> ) | Area (acre) | Volume (ft <sup>3</sup> ) | Volume (ac-ft) |
| Top of Micropool            | --         | 0.00                         | --          | --         | --                      | 680                                       | 0.016       |                           |                |
|                             | --         | 0.33                         | --          | --         | --                      | 680                                       | 0.016       | 225                       | 0.005          |
|                             | --         | 0.40                         | --          | --         | --                      | 680                                       | 0.016       | 272                       | 0.006          |
|                             | --         | 0.60                         | --          | --         | --                      | 680                                       | 0.016       | 408                       | 0.009          |
|                             | --         | 0.80                         | --          | --         | --                      | 680                                       | 0.016       | 544                       | 0.012          |
|                             | --         | 1.00                         | --          | --         | --                      | 3,706                                     | 0.085       | 983                       | 0.023          |
|                             | --         | 1.20                         | --          | --         | --                      | 10,203                                    | 0.234       | 2,374                     | 0.054          |
|                             | --         | 1.40                         | --          | --         | --                      | 19,875                                    | 0.456       | 5,381                     | 0.124          |
|                             | --         | 1.56                         | --          | --         | --                      | 29,898                                    | 0.686       | 9,363                     | 0.215          |
|                             | --         | 1.60                         | --          | --         | --                      | 30,028                                    | 0.689       | 10,561                    | 0.242          |
|                             | --         | 1.80                         | --          | --         | --                      | 30,679                                    | 0.704       | 16,632                    | 0.382          |
|                             | --         | 2.00                         | --          | --         | --                      | 31,336                                    | 0.719       | 22,834                    | 0.524          |
|                             | --         | 2.20                         | --          | --         | --                      | 32,000                                    | 0.735       | 29,167                    | 0.670          |
|                             | --         | 2.40                         | --          | --         | --                      | 32,671                                    | 0.750       | 35,634                    | 0.818          |
|                             | --         | 2.60                         | --          | --         | --                      | 33,347                                    | 0.766       | 42,236                    | 0.970          |
|                             | --         | 2.80                         | --          | --         | --                      | 34,030                                    | 0.781       | 48,974                    | 1.124          |
|                             | --         | 3.00                         | --          | --         | --                      | 34,720                                    | 0.797       | 55,849                    | 1.282          |
|                             | --         | 3.20                         | --          | --         | --                      | 35,416                                    | 0.813       | 62,862                    | 1.443          |
|                             | --         | 3.40                         | --          | --         | --                      | 36,118                                    | 0.829       | 70,016                    | 1.607          |
|                             | --         | 3.54                         | --          | --         | --                      | 36,614                                    | 0.841       | 75,107                    | 1.724          |
|                             | --         | 3.60                         | --          | --         | --                      | 36,827                                    | 0.845       | 77,310                    | 1.775          |
|                             | --         | 3.80                         | --          | --         | --                      | 37,542                                    | 0.862       | 84,747                    | 1.946          |
|                             | --         | 4.00                         | --          | --         | --                      | 38,264                                    | 0.878       | 92,328                    | 2.120          |
|                             | --         | 4.20                         | --          | --         | --                      | 38,992                                    | 0.895       | 100,053                   | 2.297          |
|                             | --         | 4.40                         | --          | --         | --                      | 39,726                                    | 0.912       | 107,925                   | 2.478          |
|                             | --         | 4.60                         | --          | --         | --                      | 40,467                                    | 0.929       | 115,944                   | 2.662          |
|                             | --         | 4.80                         | --          | --         | --                      | 41,214                                    | 0.946       | 124,112                   | 2.849          |
|                             | --         | 5.00                         | --          | --         | --                      | 41,967                                    | 0.963       | 132,431                   | 3.040          |
|                             | --         | 5.20                         | --          | --         | --                      | 42,727                                    | 0.981       | 140,900                   | 3.235          |
|                             | --         | 5.22                         | --          | --         | --                      | 42,804                                    | 0.983       | 141,755                   | 3.254          |
|                             | --         | 5.40                         | --          | --         | --                      | 43,494                                    | 0.998       | 149,522                   | 3.433          |
|                             | --         | 5.60                         | --          | --         | --                      | 44,266                                    | 1.016       | 158,298                   | 3.634          |
|                             | --         | 5.80                         | --          | --         | --                      | 45,045                                    | 1.034       | 167,229                   | 3.839          |
|                             | --         | 6.00                         | --          | --         | --                      | 45,831                                    | 1.052       | 176,317                   | 4.048          |
|                             | --         | 6.20                         | --          | --         | --                      | 46,623                                    | 1.070       | 185,562                   | 4.260          |
|                             | --         | 6.40                         | --          | --         | --                      | 47,421                                    | 1.089       | 194,967                   | 4.476          |
|                             | --         | 6.60                         | --          | --         | --                      | 48,226                                    | 1.107       | 204,531                   | 4.695          |
|                             | --         | 6.80                         | --          | --         | --                      | 49,037                                    | 1.126       | 214,258                   | 4.919          |
|                             | --         | 7.00                         | --          | --         | --                      | 49,855                                    | 1.145       | 224,147                   | 5.146          |
|                             | --         | 7.20                         | --          | --         | --                      | 50,679                                    | 1.163       | 234,200                   | 5.376          |
|                             | --         | 7.40                         | --          | --         | --                      | 51,509                                    | 1.182       | 244,419                   | 5.611          |
|                             | --         | 7.60                         | --          | --         | --                      | 52,346                                    | 1.202       | 254,805                   | 5.850          |
|                             | --         | 7.80                         | --          | --         | --                      | 53,189                                    | 1.221       | 265,358                   | 6.092          |
|                             | --         | 8.00                         | --          | --         | --                      | 54,038                                    | 1.241       | 276,081                   | 6.338          |
|                             | --         | 8.20                         | --          | --         | --                      | 54,894                                    | 1.260       | 286,974                   | 6.588          |
|                             | --         | 8.40                         | --          | --         | --                      | 55,757                                    | 1.280       | 298,039                   | 6.842          |
|                             | --         | 8.60                         | --          | --         | --                      | 56,625                                    | 1.300       | 309,277                   | 7.100          |
|                             | --         | 8.80                         | --          | --         | --                      | 57,501                                    | 1.320       | 320,690                   | 7.362          |
|                             | --         | 9.00                         | --          | --         | --                      | 58,382                                    | 1.340       | 332,278                   | 7.628          |
|                             | --         | 9.20                         | --          | --         | --                      | 59,270                                    | 1.361       | 344,043                   | 7.89           |

# DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.04 (February 2021)

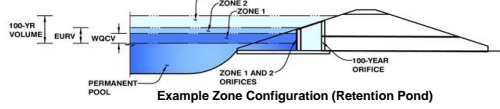


# DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.04 (February 2021)

Project: **Flying Horse North**

Basin ID: **Pond 5**



Example Zone Configuration (Retention Pond)

## Watershed Information

|   |                |                       |
|---|----------------|-----------------------|
| Selected BMP Type =                     | <b>EDB</b>     | Note: L / W Ratio < 1 |
| Watershed Area =                        | 41.57 acres    | L / W Ratio = 0.52    |
| Watershed Length =                      | 967 ft         |                       |
| Watershed Length to Centroid =          | 450 ft         |                       |
| Watershed Slope =                       | 0.045 ft/ft    |                       |
| Watershed Imperviousness =              | 29.60% percent |                       |
| Percentage Hydrologic Soil Group A =    | 0.0% percent   |                       |
| Percentage Hydrologic Soil Group B =    | 100.0% percent |                       |
| Percentage Hydrologic Soil Groups C/D = | 0.0% percent   |                       |
| Target WQCV Drain Time =                | 40.0 hours     |                       |
| Location for 1-hr Rainfall Depths =     | User Input     |                       |

After providing required inputs above including 1-hour rainfall depths, click "Run CUHP" to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

|  |                 |                         |  |
|--|-----------------|-------------------------|--|
| Water Quality Capture Volume (WQCV) =  | 0.520 acre-feet | Optional User Overrides |  |
| Excess Urban Runoff Volume (EURV) =    | 1.261 acre-feet |                         |  |
| 2-yr Runoff Volume (P1 = 1.19 in.) =   | 1.226 acre-feet | 1.19 inches             |  |
| 5-yr Runoff Volume (P1 = 1.5 in.) =    | 1.996 acre-feet | 1.50 inches             |  |
| 10-yr Runoff Volume (P1 = 1.75 in.) =  | 2.708 acre-feet | 1.75 inches             |  |
| 25-yr Runoff Volume (P1 = 2 in.) =     | 3.784 acre-feet | 2.00 inches             |  |
| 50-yr Runoff Volume (P1 = 2.25 in.) =  | 4.596 acre-feet | 2.25 inches             |  |
| 100-yr Runoff Volume (P1 = 2.52 in.) = | 5.681 acre-feet | 2.52 inches             |  |
| 500-yr Runoff Volume (P1 = 3.14 in.) = | 7.783 acre-feet |                         |  |
| Approximate 2-yr Detention Volume =    | 0.901 acre-feet |                         |  |
| Approximate 5-yr Detention Volume =    | 1.291 acre-feet |                         |  |
| Approximate 10-yr Detention Volume =   | 1.889 acre-feet |                         |  |
| Approximate 25-yr Detention Volume =   | 2.195 acre-feet |                         |  |
| Approximate 50-yr Detention Volume =   | 2.313 acre-feet |                         |  |
| Approximate 100-yr Detention Volume =  | 2.738 acre-feet |                         |  |

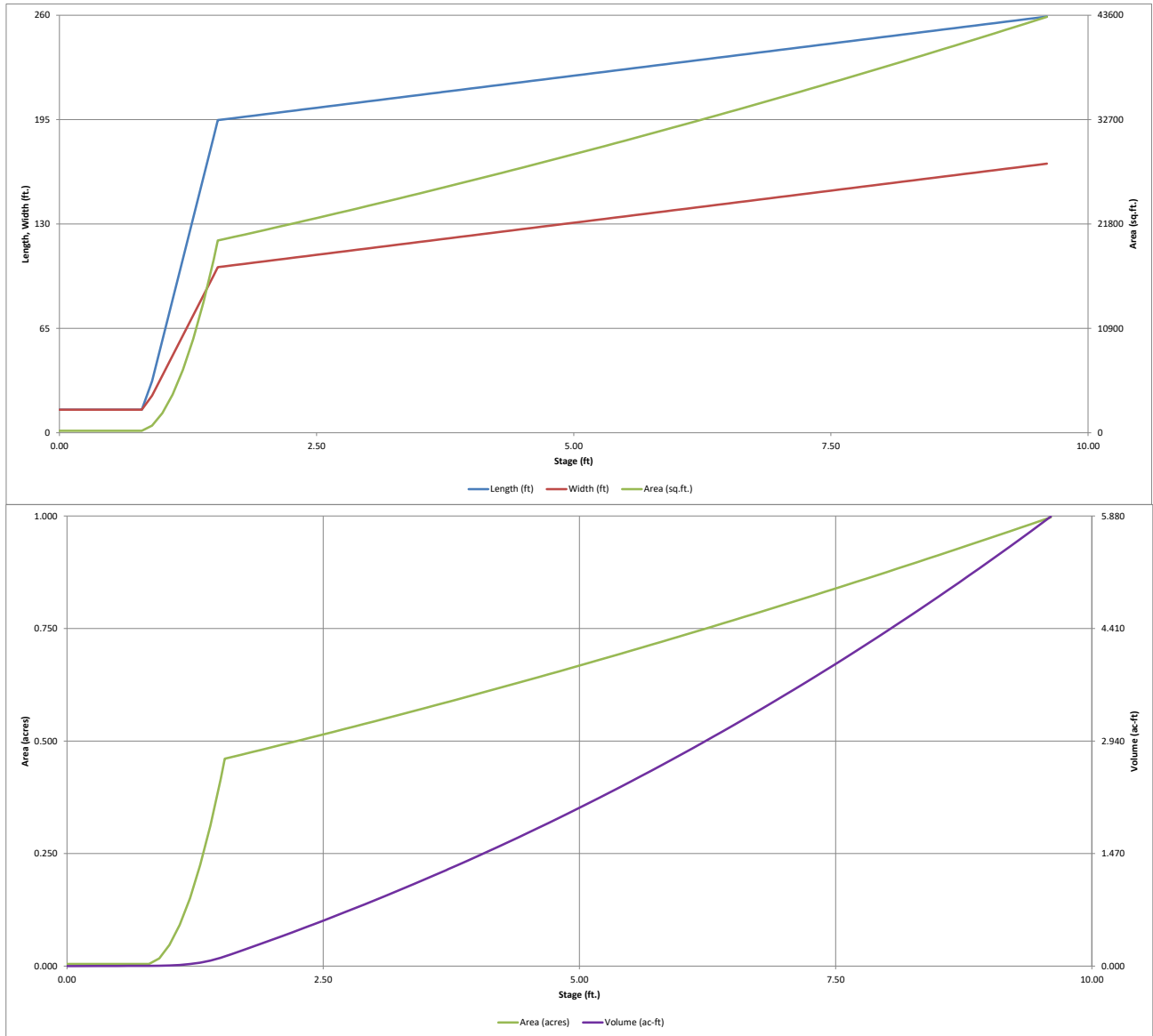
## Define Zones and Basin Geometry

|   |                         |
|---|-------------------------|
| Zone 1 Volume (WQCV) =                                  | 0.520 acre-feet         |
| Zone 2 Volume (EURV - Zone 1) =                         | 0.741 acre-feet         |
| Zone 3 Volume (100-year - Zones 1 & 2) =                | 1.477 acre-feet         |
| Total Detention Basin Volume =                          | 2.738 acre-feet         |
| Initial Surge Volume (ISV) =                            | 68 ft <sup>3</sup>      |
| Initial Surge Depth (ISD) =                             | 0.33 ft                 |
| Total Available Detention Depth (H <sub>total</sub> ) = | 6.00 ft                 |
| Depth of Trickle Channel (H <sub>TC</sub> ) =           | 0.50 ft                 |
| Slope of Trickle Channel (S <sub>TC</sub> ) =           | 0.004 ft/ft             |
| Slopes of Main Basin Sides (S <sub>main</sub> ) =       | 4 H:V                   |
| Basin Length-to-Width Ratio (R <sub>L/W</sub> ) =       | 2                       |
| Initial Surge Area (A <sub>ISV</sub> ) =                | 206 ft <sup>2</sup>     |
| Surcharge Volume Length (L <sub>ISV</sub> ) =           | 14.4 ft                 |
| Surcharge Volume Width (W <sub>ISV</sub> ) =            | 14.4 ft                 |
| Depth of Basin Floor (H <sub>FLOOR</sub> ) =            | 0.71 ft                 |
| Length of Basin Floor (L <sub>FLOOR</sub> ) =           | 194.7 ft                |
| Width of Basin Floor (W <sub>FLOOR</sub> ) =            | 103.1 ft                |
| Area of Basin Floor (A <sub>FLOOR</sub> ) =             | 20,074 ft <sup>2</sup>  |
| Volume of Basin Floor (V <sub>FLOOR</sub> ) =           | 5,281 ft <sup>3</sup>   |
| Depth of Main Basin (H <sub>MAIN</sub> ) =              | 4.46 ft                 |
| Length of Main Basin (L <sub>MAIN</sub> ) =             | 230.4 ft                |
| Width of Main Basin (W <sub>MAIN</sub> ) =              | 138.8 ft                |
| Area of Main Basin (A <sub>MAIN</sub> ) =               | 31,973 ft <sup>2</sup>  |
| Volume of Main Basin (V <sub>MAIN</sub> ) =             | 115,040 ft <sup>3</sup> |
| Calculated Total Basin Volume (V <sub>total</sub> ) =   | 2.766 acre-feet         |

|                             |            |                              |             |            |                         |   |             |                           |                |
|-----------------------------|------------|------------------------------|-------------|------------|-------------------------|---|-------------|---------------------------|----------------|
| Depth Increment =           | 0.10       | ft                           |             |            |                         |   |             |                           |                |
| Stage - Storage Description | Stage (ft) | Optional Override Stage (ft) | Length (ft) | Width (ft) | Area (ft <sup>2</sup> ) | Optional Override Area (ft <sup>2</sup> ) | Area (acre) | Volume (ft <sup>3</sup> ) | Volume (ac-ft) |
| Top of Micropool            | 0.00       |                              | 14.4        | 14.4       | 206                     |   | 0.005       |                           |                |
| ISV                         | 0.33       |                              | 14.4        | 14.4       | 206                     |   | 0.005       | 68                        | 0.002          |
|                             | 0.40       |                              | 14.4        | 14.4       | 206                     |   | 0.005       | 82                        | 0.002          |
|                             | 0.50       |                              | 14.4        | 14.4       | 206                     |   | 0.005       | 103                       | 0.002          |
|                             | 0.60       |                              | 14.4        | 14.4       | 206                     |   | 0.005       | 124                       | 0.003          |
|                             | 0.70       |                              | 14.4        | 14.4       | 206                     |   | 0.005       | 144                       | 0.003          |
|                             | 0.80       |                              | 14.4        | 14.4       | 206                     |   | 0.005       | 165                       | 0.004          |
|                             | 0.90       |                              | 32.1        | 23.1       | 742                     |   | 0.017       | 202                       | 0.005          |
|                             | 1.00       |                              | 57.5        | 35.6       | 2,049                   |   | 0.047       | 337                       | 0.008          |
|                             | 1.10       |                              | 82.9        | 48.1       | 3,990                   |   | 0.092       | 633                       | 0.015          |
|                             | 1.20       |                              | 108.3       | 60.6       | 6,566                   |   | 0.151       | 1,156                     | 0.027          |
|                             | 1.30       |                              | 133.7       | 73.1       | 9,777                   |   | 0.224       | 1,968                     | 0.045          |
|                             | 1.40       |                              | 159.1       | 85.6       | 13,623                  |   | 0.313       | 3,132                     | 0.072          |
|                             | 1.50       |                              | 184.5       | 98.1       | 18,104                  |   | 0.416       | 4,713                     | 0.108          |
| Floor                       | 1.54       |                              | 194.7       | 103.1      | 20,074                  |   | 0.461       | 5,477                     | 0.126          |
|                             | 1.60       |                              | 195.2       | 103.6      | 20,217                  |   | 0.464       | 6,685                     | 0.153          |
|                             | 1.70       |                              | 196.0       | 104.4      | 20,457                  |   | 0.470       | 8,719                     | 0.200          |
|                             | 1.80       |                              | 196.8       | 105.2      | 20,698                  |   | 0.475       | 10,777                    | 0.247          |
|                             | 1.90       |                              | 197.6       | 106.0      | 20,940                  |   | 0.481       | 12,859                    | 0.295          |
|                             | 2.00       |                              | 198.4       | 106.8      | 21,184                  |   | 0.486       | 14,965                    | 0.344          |
|                             | 2.10       |                              | 199.2       | 107.6      | 21,428                  |   | 0.492       | 17,095                    | 0.392          |
|                             | 2.20       |                              | 200.0       | 108.4      | 21,674                  |   | 0.498       | 19,250                    | 0.442          |
|                             | 2.30       |                              | 200.8       | 109.2      | 21,922                  |   | 0.503       | 21,430                    | 0.492          |
| Zone 1 (WQCV)               | 2.36       |                              | 201.3       | 109.7      | 22,071                  |   | 0.507       | 22,750                    | 0.522          |
|                             | 2.40       |                              | 201.6       | 110.0      | 22,170                  |   | 0.509       | 23,635                    | 0.543          |
|                             | 2.50       |                              | 202.4       | 110.8      | 22,420                  |   | 0.515       | 25,864                    | 0.594          |
|                             | 2.60       |                              | 203.2       | 111.6      | 22,671                  |   | 0.520       | 28,119                    | 0.646          |
|                             | 2.70       |                              | 204.0       | 112.4      | 22,924                  |   | 0.526       | 30,399                    | 0.698          |
|                             | 2.80       |                              | 204.8       | 113.2      | 23,177                  |   | 0.532       | 32,704                    | 0.751          |
|                             | 2.90       |                              | 205.6       | 114.0      | 23,433                  |   | 0.538       | 35,034                    | 0.804          |
|                             | 3.00       |                              | 206.4       | 114.8      | 23,689                  |   | 0.544       | 37,390                    | 0.858          |
|                             | 3.10       |                              | 207.2       | 115.6      | 23,946                  |   | 0.550       | 39,772                    | 0.913          |
|                             | 3.20       |                              | 208.0       | 116.4      | 24,205                  |   | 0.556       | 42,180                    | 0.968          |
|                             | 3.30       |                              | 208.8       | 117.2      | 24,465                  |   | 0.562       | 44,613                    | 1.024          |
|                             | 3.40       |                              | 209.6       | 118.0      | 24,727                  |   | 0.568       | 47,073                    | 1.081          |
|                             | 3.50       |                              | 210.4       | 118.8      | 24,989                  |   | 0.574       | 49,558                    | 1.138          |
|                             | 3.60       |                              | 211.2       | 119.6      | 25,253                  |   | 0.580       | 52,071                    | 1.195          |
|                             | 3.70       |                              | 212.0       | 120.4      | 25,519                  |   | 0.586       | 54,609                    | 1.254          |
| Zone 2 (EURV)               | 3.72       |                              | 212.1       | 120.5      | 25,572                  |   | 0.587       | 55,120                    | 1.265          |
|                             | 3.80       |                              | 212.8       | 121.2      | 25,785                  |   | 0.592       | 57,174                    | 1.313          |
|                             | 3.90       |                              | 213.6       | 122.0      | 26,053                  |   | 0.598       | 59,766                    | 1.372          |
|                             | 4.00       |                              | 214.4       | 122.8      | 26,322                  |   | 0.604       | 62,385                    | 1.432          |
|                             | 4.10       |                              | 215.2       | 123.6      | 26,592                  |   | 0.610       | 65,031                    | 1.493          |
|                             | 4.20       |                              | 216.0       | 124.4      | 26,864                  |   | 0.617       | 67,704                    | 1.554          |
|                             | 4.30       |                              | 216.8       | 125.2      | 27,137                  |   | 0.623       | 70,404                    | 1.616          |
|                             | 4.40       |                              | 217.6       | 126.0      | 27,411                  |   | 0.629       | 73,131                    | 1.679          |
|                             | 4.50       |                              | 218.4       | 126.8      | 27,687                  |   | 0.636       | 75,886                    | 1.742          |
|                             | 4.60       |                              | 219.2       | 127.6      | 27,963                  |   | 0.642       | 78,668                    | 1.806          |
|                             | 4.70       |                              | 220.0       | 128.4      | 28,242                  |   | 0.648       | 81,479                    | 1.870          |
|                             | 4.80       |                              | 220.8       | 129.2      | 28,521                  |   | 0.655       | 84,317                    | 1.936          |
|                             | 4.90       |                              | 221.6       | 130.0      | 28,801                  |   | 0.661       | 87,183                    | 2.001          |
|                             | 5.00       |                              | 222.4       | 130.8      | 29,083                  |   | 0.668       | 90,077                    | 2.068          |
|                             | 5.10       |                              | 223.2       | 131.6      | 29,367                  |   | 0.674       | 93,000                    | 2.135          |
|                             | 5.20       |                              | 224.0       | 132.4      | 29,651                  |   | 0.681       | 95,950                    | 2.203          |
|                             | 5.30       |                              | 224.8       | 133.2      | 29,937                  |   | 0.687       | 98,930                    | 2.271          |
|                             | 5.40       |                              | 225.6       | 134.0      | 30,224                  |   | 0.694       | 101,938                   | 2.340          |
|                             | 5.50       |                              | 226.4       | 134.8      | 30,512                  |   | 0.700       | 104,975                   | 2.410          |
|                             | 5.60       |                              | 227.2       | 135.6      | 30,802                  |   | 0.707       | 108,040                   | 2.480          |
|                             | 5.70       |                              | 228.0       | 136.4      | 31,092                  |   | 0.714       | 111,135                   | 2.551          |
|                             | 5.80       |                              | 228.8       | 137.2      | 31,385                  |   | 0.720       | 114,259                   | 2.623          |
| Zone 3 (100-year)           | 5.90       |                              | 229.6       | 138.0      | 31,678                  |   | 0.727       | 117,412                   | 2.695          |
|                             | 5.96       |                              | 230.1       | 138.5      | 31,855                  |   | 0.731       | 119,318                   | 2.739          |
|                             | 6.00       |                              | 230.4       | 138.8      | 31,973                  |   | 0.734       | 120,594                   | 2.768          |
|                             | 6.10       |                              | 231.2       | 139.6      | 32,269                  |   | 0.741       | 123,806                   | 2.842          |
|                             | 6.20       |                              | 232.0       | 140.4      | 32,566                  |   | 0.748       | 127,048                   | 2.917          |
|                             | 6.30       |                              | 232.8       | 141.2      | 32,864                  |   | 0.754       | 130,320                   | 2.992          |
|                             | 6.40       |                              | 233.6       | 142.0      | 33,164                  |   | 0.761       | 133,621                   | 3.068          |
|                             | 6.50       |                              | 234.4       | 142.8      | 33,465                  |   | 0.768       | 136,953                   | 3.144          |
|                             | 6.60       |                              | 235.2       | 143.6      | 33,768                  |   | 0.775       | 140,314                   | 3.221          |
|                             | 6.70       |                              | 236.0       | 144.4      | 34,071                  |   | 0.782       | 143,706                   | 3.299          |
|                             | 6.80       |                              | 236.8       | 145.2      | 34,376                  |   | 0.789       | 147,128                   | 3.378          |
|                             | 6.90       |                              | 237.6       | 146.0      | 34,682                  |   | 0.796       | 150,581                   | 3.457          |
|                             | 7.00       |                              | 238.4       | 146.8      | 34,990                  |   | 0.803       | 154,065                   | 3.537          |
|                             | 7.10       |                              | 239.2       | 147.6      | 35,299                  |   | 0.810       | 157,579                   | 3.618          |
|                             | 7.20       |                              | 240.0       | 148.4      | 35,609                  |   | 0.817       | 161,125                   | 3.699          |
|                             | 7.30       |                              | 240.8       | 149.2      | 35,920                  |   | 0.825       | 164,701                   | 3.781          |
|                             | 7.40       |                              | 241.6       | 150.0      | 36,233                  |   | 0.832       | 168,309                   | 3.864          |
|                             | 7.50       |                              | 242.4       | 150.8      | 36,547                  |   | 0.839       | 171,948                   | 3.947          |
|                             | 7.60       |                              | 243.2       | 151.6      | 36,862                  |   | 0.846       | 175,618                   | 4.032          |
|                             | 7.70       |                              | 244.0       | 152.4      | 37,178                  |   | 0.853       | 179,320                   | 4.117          |
|                             | 7.80       |                              | 244.8       | 153.2      | 37,496                  |   | 0.861       | 183,054                   | 4.202          |
|                             | 7.90       |                              | 245.6       | 154.0      | 37,815                  |   | 0.868       | 186,819                   | 4.289          |
|                             | 8.00       |                              | 246.4       | 154.8      | 38,135                  |   | 0.875       | 190,617                   | 4.376          |
|                             | 8.10       |                              | 247.2       | 155.6      | 38,457                  |   | 0.883       | 194,446                   | 4.464          |
|                             | 8.20       |                              | 248.0       | 156.4      | 38,780                  |   | 0.890       | 198,308                   | 4.553          |
|                             | 8.30       |                              | 248.8       | 157.2      | 39,104                  |   | 0.898       | 202,202                   | 4.642          |
|                             | 8.40       |                              | 249.6       | 158.0      | 39,429                  |   | 0.905       | 206,129                   | 4.732          |
|                             | 8.50       |                              | 250.4       | 158.8      | 39,756                  |   | 0.913       | 210,088                   | 4.823          |
|                             | 8.60       |                              | 251.2       | 159.6      | 40,084                  |   | 0.920       | 214,080                   | 4.915          |
|                             | 8.70       |                              | 252.0       | 160.4      | 40,413                  |   | 0.928       | 218,105                   | 5.007          |
|                             | 8.80       |                              | 252.8       | 161.2      | 40,744                  |   | 0.935       | 222,163                   | 5.100          |
|                             | 8.90       |                              | 253.6       | 162.0      | 41,075                  |   | 0.943       | 226,254                   | 5.194          |
|                             | 9.00       |                              | 254.4       | 162.8      | 41,408                  |   | 0.951       | 230,378                   | 5.289          |
|                             | 9.10       |                              | 255.2       | 163.6      | 41,743                  |   | 0.958       | 234,536                   | 5.384          |
|                             | 9.20       |                              | 256.0       | 164.4      | 42,079                  |   | 0.966       | 238,727                   | 5.480          |
|                             | 9.30       |                              | 256.8       | 165.2      | 42,415                  |   | 0.974       | 242,951                   | 5.577          |
|                             | 9.40       |                              | 257.6       | 166.0      | 42,754                  |   | 0.981       | 247,210                   | 5.675          |
|                             | 9.50       |                              | 258.4       | 166.8      | 43,093                  |   | 0.989       | 251,502                   | 5.774          |
|                             | 9.60       |                              | 259.2       | 167.6      | 43,434                  |   | 0.997       | 255,828                   | 5.873          |

# DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.04 (February 2021)

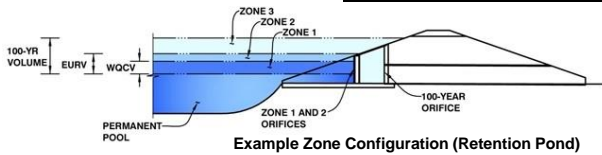


# DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.04 (February 2021)

Project: Flying Horse North

Basin ID: Pond 5



Example Zone Configuration (Retention Pond)

|                   | Estimated Stage (ft) | Estimated Volume (ac-ft) | Outlet Type          |
|-------------------|----------------------|--------------------------|----------------------|
| Zone 1 (WQCV)     | 2.36                 | 0.520                    | Orifice Plate        |
| Zone 2 (EURV)     | 3.72                 | 0.741                    | Circular Orifice     |
| Zone 3 (100-year) | 5.96                 | 1.477                    | Weir&Pipe (Restrict) |
| Total (all zones) |                      | 2.738                    |                      |

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth = N/A ft (distance below the filtration media surface)  
Underdrain Orifice Diameter = N/A inches

Calculated Parameters for Underdrain  
Underdrain Orifice Area = N/A ft<sup>2</sup>  
Underdrain Orifice Centroid = N/A feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice = 0.00 ft (relative to basin bottom at Stage = 0 ft)  
Depth at top of Zone using Orifice Plate = 2.36 ft (relative to basin bottom at Stage = 0 ft)  
Orifice Plate: Orifice Vertical Spacing = 9.40 inches  
Orifice Plate: Orifice Area per Row = 1.77 sq. inches (diameter = 1-1/2 inches)

Calculated Parameters for Plate  
WQ Orifice Area per Row = 1.229E-02 ft<sup>2</sup>  
Elliptical Half-Width = N/A feet  
Elliptical Slot Centroid = N/A feet  
Elliptical Slot Area = N/A ft<sup>2</sup>

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

|                                | Row 1 (required) | Row 2 (optional) | Row 3 (optional) | Row 4 (optional) | Row 5 (optional) | Row 6 (optional) | Row 7 (optional) | Row 8 (optional) |
|--------------------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|
| Stage of Orifice Centroid (ft) | 0.00             | 0.79             | 1.57             |                  |                  |                  |                  |                  |
| Orifice Area (sq. inches)      | 1.77             | 1.77             | 1.77             |                  |                  |                  |                  |                  |

|                                | Row 9 (optional) | Row 10 (optional) | Row 11 (optional) | Row 12 (optional) | Row 13 (optional) | Row 14 (optional) | Row 15 (optional) | Row 16 (optional) |
|--------------------------------|------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| Stage of Orifice Centroid (ft) |                  |                   |                   |                   |                   |                   |                   |                   |
| Orifice Area (sq. inches)      |                  |                   |                   |                   |                   |                   |                   |                   |

User Input: Vertical Orifice (Circular or Rectangular)

Invert of Vertical Orifice = 2.38 ft (relative to basin bottom at Stage = 0 ft)  
Depth at top of Zone using Vertical Orifice = 3.59 ft (relative to basin bottom at Stage = 0 ft)  
Vertical Orifice Diameter = 24.00 inches

Calculated Parameters for Vertical Orifice  
Zone 2 Circular Not Selected  
Vertical Orifice Area = 3.14 ft<sup>2</sup>  
Vertical Orifice Centroid = 1.00 feet

User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe))

Overflow Weir Front Edge Height, H<sub>o</sub> = 4.00 ft (relative to basin bottom at Stage = 0 ft)  
Overflow Weir Front Edge Length = 6.00 feet  
Overflow Weir Grate Slope = 0.00 H:V  
Horiz. Length of Weir Sides = 6.00 feet  
Overflow Grate Type = Type C Grate  
Debris Clogging % = 50%

Calculated Parameters for Overflow Weir  
Zone 3 Weir Not Selected  
Height of Grate Upper Edge, H<sub>u</sub> = 4.00 feet  
Overflow Weir Slope Length = 6.00 feet  
Grate Open Area / 100-yr Orifice Area = 2.41  
Overflow Grate Open Area w/o Debris = 25.06 ft<sup>2</sup>  
Overflow Grate Open Area w/ Debris = 12.53 ft<sup>2</sup>

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

Depth to Invert of Outlet Pipe = 1.00 ft (distance below basin bottom at Stage = 0 ft)  
Outlet Pipe Diameter = 48.00 inches  
Restrictor Plate Height Above Pipe Invert = 37.00 inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate  
Zone 3 Restrictor Not Selected  
Outlet Orifice Area = 10.39 ft<sup>2</sup>  
Outlet Orifice Centroid = 1.70 feet  
Half-Central Angle of Restrictor Plate on Pipe = 2.14 radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage = 7.00 ft (relative to basin bottom at Stage = 0 ft)  
Spillway Crest Length = 60.00 feet  
Spillway End Slopes = 4.00 H:V  
Freeboard above Max Water Surface = 1.00 feet

Calculated Parameters for Spillway  
Spillway Design Flow Depth = 0.80 feet  
Stage at Top of Freeboard = 8.80 feet  
Basin Area at Top of Freeboard = 0.94 acres  
Basin Volume at Top of Freeboard = 5.10 acre-ft

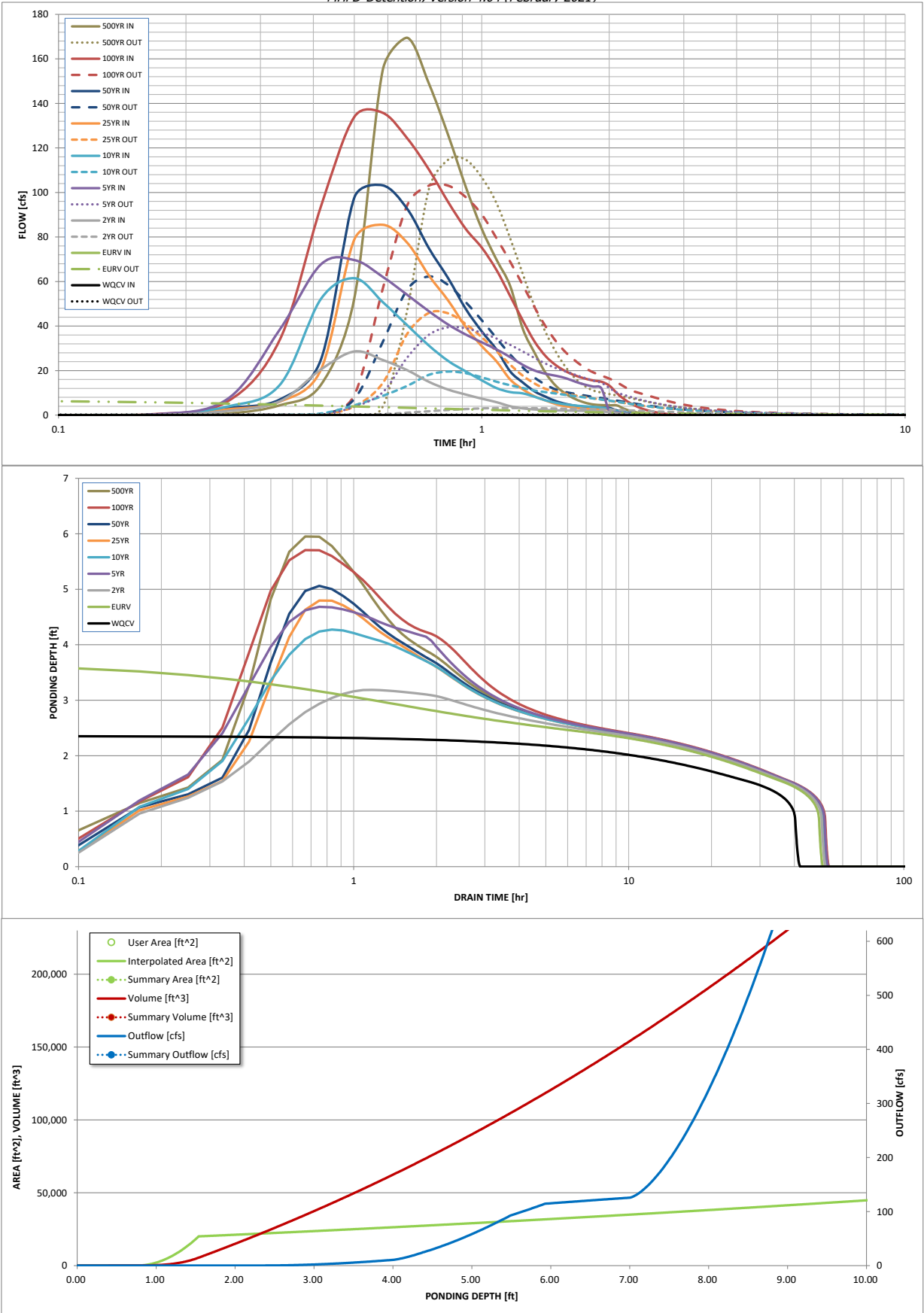
## Routed Hydrograph Results

The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).

|  | WQCV  | EURV               | 2 Year             | 5 Year          | 10 Year         | 25 Year         | 50 Year         | 100 Year        | 500 Year       |
|--|-------|--------------------|--------------------|-----------------|-----------------|-----------------|-----------------|-----------------|----------------|
| Design Storm Return Period =                       | N/A   | N/A                | 1.19               | 1.50            | 1.75            | 2.00            | 2.25            | 2.52            | 3.14           |
| One-Hour Rainfall Depth (in) =                     | 0.520 | 1.261              | 1.226              | 1.996           | 2.708           | 3.784           | 4.596           | 5.681           | 7.783          |
| CUHP Runoff Volume (acre-ft) =                     | N/A   | N/A                | 1.226              | 4.578           | 2.708           | 3.784           | 4.596           | 8.724           | 7.783          |
| User Override Inflow Hydrograph Volume (acre-ft) = | N/A   | N/A                | 9.0                | 25.3            | 37.9            | 62.0            | 78.4            | 99.1            | 137.2          |
| CUHP Predevelopment Peak Q (cfs) =                 | N/A   | N/A                | 0.22               | 0.96            | 0.91            | 1.49            | 1.89            | 2.81            | 3.30           |
| OPTIONAL Override Predevelopment Peak Q (cfs) =    | N/A   | N/A                | 28.6               | 69.6            | 61.5            | 85.5            | 103.2           | 135.8           | 169.5          |
| Predevelopment Unit Peak Flow, q (cfs/acre) =      | N/A   | N/A                | 3.2                | 39.4            | 19.6            | 45.9            | 62.2            | 103.1           | 114.7          |
| Peak Inflow Q (cfs) =                              | N/A   | N/A                | N/A                | 1.0             | 0.5             | 0.7             | 0.8             | 0.9             | 0.8            |
| Peak Outflow Q (cfs) =                             | N/A   | N/A                | N/A                | N/A             | N/A             | N/A             | N/A             | N/A             | N/A            |
| Ratio Peak Outflow to Predevelopment Q =           | Plate | Vertical Orifice 1 | Vertical Orifice 1 | Overflow Weir 1 | Overflow Weir 1 | Overflow Weir 1 | Overflow Weir 1 | Overflow Weir 1 | Outlet Plate 1 |
| Structure Controlling Flow =                       | N/A   | N/A                | N/A                | 0.9             | 0.2             | 1.1             | 1.7             | 3.2             | 3.6            |
| Max Velocity through Grate 1 (fps) =               | N/A   | N/A                | N/A                | N/A             | N/A             | N/A             | N/A             | N/A             | N/A            |
| Max Velocity through Grate 2 (fps) =               | 39    | 45                 | 46                 | 37              | 42              | 39              | 37              | 28              | 29             |
| Time to Drain 97% of Inflow Volume (hours) =       | 40    | 48                 | 49                 | 46              | 48              | 47              | 46              | 42              | 43             |
| Time to Drain 99% of Inflow Volume (hours) =       | 2.36  | 3.72               | 3.19               | 4.68            | 4.27            | 4.80            | 5.06            | 5.70            | 5.95           |
| Maximum Ponding Depth (ft) =                       | 0.51  | 0.59               | 0.55               | 0.65            | 0.62            | 0.65            | 0.67            | 0.71            | 0.73           |
| Area at Maximum Ponding Depth (acres) =            | 0.522 | 1.265              | 0.957              | 1.858           | 1.598           | 1.929           | 2.108           | 2.551           | 2.732          |
| Maximum Volume Stored (acre-ft) =                  |       |                    |                    |                 |                 |                 |                 |                 |                |

DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD- Detention, Version 4.04 (February 2021)



| S-A-V-D Chart Axis Override | X-axis | Left Y-Axis | Right Y-Axis |
|-----------------------------|--------|-------------|--------------|
| minimum bound               |        |             |              |
| maximum bound               |        |             |              |

# DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename: ...[SWM]Outflow hydrographs\Pond6 OutflowHydrograph.xlsx

## Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

|               | SOURCE  | CUHP       | CUHP       | CUHP         | USER         | CUHP          | CUHP          | CUHP          | USER           | CUHP           |
|---------------|---------|------------|------------|--------------|--------------|---------------|---------------|---------------|----------------|----------------|
| Time Interval | TIME    | WQCV [cfs] | EURV [cfs] | 2 Year [cfs] | 5 Year [cfs] | 10 Year [cfs] | 25 Year [cfs] | 50 Year [cfs] | 100 Year [cfs] | 500 Year [cfs] |
| 5.00 min      | 0:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 0:05:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 0:10:00 | 0.00       | 0.00       | 0.00         | 0.27         | 0.00          | 0.00          | 0.22          | 0.40           | 0.70           |
|               | 0:15:00 | 0.00       | 0.00       | 1.84         | 7.09         | 3.80          | 2.57          | 3.17          | 6.01           | 4.42           |
|               | 0:20:00 | 0.00       | 0.00       | 6.21         | 38.48        | 13.58         | 6.05          | 7.03          | 33.89          | 13.57          |
|               | 0:25:00 | 0.00       | 0.00       | 20.49        | 67.67        | 52.13         | 20.37         | 24.85         | 93.63          | 52.58          |
|               | 0:30:00 | 0.00       | 0.00       | 28.59        | 69.63        | 61.49         | 78.91         | 97.73         | 133.95         | 154.89         |
|               | 0:35:00 | 0.00       | 0.00       | 24.76        | 62.10        | 50.77         | 85.48         | 103.19        | 135.78         | 169.46         |
|               | 0:40:00 | 0.00       | 0.00       | 20.16        | 54.00        | 40.35         | 77.39         | 92.60         | 124.29         | 148.88         |
|               | 0:45:00 | 0.00       | 0.00       | 14.94        | 46.63        | 31.22         | 62.69         | 74.92         | 110.29         | 125.63         |
|               | 0:50:00 | 0.00       | 0.00       | 11.44        | 40.64        | 24.29         | 51.40         | 61.39         | 95.61          | 102.47         |
|               | 0:55:00 | 0.00       | 0.00       | 9.23         | 36.18        | 19.62         | 39.56         | 47.65         | 83.59          | 83.62          |
|               | 1:00:00 | 0.00       | 0.00       | 7.39         | 32.69        | 15.61         | 30.99         | 37.59         | 75.22          | 69.81          |
|               | 1:05:00 | 0.00       | 0.00       | 5.81         | 29.50        | 12.14         | 24.16         | 29.44         | 65.17          | 58.06          |
|               | 1:10:00 | 0.00       | 0.00       | 4.00         | 26.06        | 10.35         | 16.01         | 19.65         | 53.50          | 38.75          |
|               | 1:15:00 | 0.00       | 0.00       | 3.01         | 22.56        | 9.76          | 11.60         | 14.65         | 42.49          | 27.91          |
|               | 1:20:00 | 0.00       | 0.00       | 2.54         | 20.01        | 8.24          | 8.40          | 10.62         | 32.94          | 18.76          |
|               | 1:25:00 | 0.00       | 0.00       | 2.28         | 18.54        | 6.59          | 6.53          | 8.22          | 26.39          | 12.92          |
|               | 1:30:00 | 0.00       | 0.00       | 2.14         | 17.63        | 5.51          | 4.92          | 6.21          | 22.26          | 9.46           |
|               | 1:35:00 | 0.00       | 0.00       | 2.04         | 16.51        | 4.77          | 3.94          | 4.98          | 19.57          | 7.13           |
|               | 1:40:00 | 0.00       | 0.00       | 1.96         | 14.95        | 4.30          | 3.32          | 4.19          | 17.72          | 5.64           |
|               | 1:45:00 | 0.00       | 0.00       | 1.92         | 13.73        | 3.97          | 2.92          | 3.68          | 16.45          | 4.78           |
|               | 1:50:00 | 0.00       | 0.00       | 1.90         | 12.82        | 3.73          | 2.73          | 3.44          | 15.55          | 4.51           |
|               | 1:55:00 | 0.00       | 0.00       | 1.59         | 12.02        | 3.37          | 2.61          | 3.29          | 14.99          | 4.39           |
|               | 2:00:00 | 0.00       | 0.00       | 1.38         | 1.90         | 2.81          | 2.56          | 3.23          | 13.30          | 4.39           |
|               | 2:05:00 | 0.00       | 0.00       | 0.92         | 1.25         | 1.86          | 1.68          | 2.12          | 9.94           | 2.89           |
|               | 2:10:00 | 0.00       | 0.00       | 0.60         | 0.80         | 1.20          | 1.10          | 1.38          | 7.23           | 1.87           |
|               | 2:15:00 | 0.00       | 0.00       | 0.39         | 0.49         | 0.76          | 0.70          | 0.88          | 5.23           | 1.18           |
|               | 2:20:00 | 0.00       | 0.00       | 0.24         | 0.30         | 0.46          | 0.43          | 0.53          | 3.73           | 0.71           |
|               | 2:25:00 | 0.00       | 0.00       | 0.14         | 0.19         | 0.27          | 0.26          | 0.32          | 2.62           | 0.42           |
|               | 2:30:00 | 0.00       | 0.00       | 0.07         | 0.10         | 0.13          | 0.14          | 0.16          | 1.85           | 0.21           |
|               | 2:35:00 | 0.00       | 0.00       | 0.03         | 0.04         | 0.04          | 0.05          | 0.06          | 1.26           | 0.07           |
|               | 2:40:00 | 0.00       | 0.00       | 0.01         | 0.01         | 0.01          | 0.01          | 0.00          | 0.81           | 0.00           |
|               | 2:45:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.49           | 0.00           |
|               | 2:50:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.28           | 0.00           |
|               | 2:55:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.13           | 0.00           |
|               | 3:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.07           | 0.00           |
|               | 3:05:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.04           | 0.00           |
|               | 3:10:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.03           | 0.00           |
|               | 3:15:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.02           | 0.00           |
|               | 3:20:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.01           | 0.00           |
|               | 3:25:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.01           | 0.00           |
|               | 3:30:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.01           | 0.00           |
|               | 3:35:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.01           | 0.00           |
|               | 3:40:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:45:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:50:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:55:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:05:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:10:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:15:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:20:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:25:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:30:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:35:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:40:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:45:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:50:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:55:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:05:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:10:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:15:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:20:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:25:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:30:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:35:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:40:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:45:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:50:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:55:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 6:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |



## DETENTION BASIN OUTLET STRUCTURE DESIGN

*MHFD-Detention, Version 4.04 (February 2021)*

### Summary Stage-Area-Volume-Discharge Relationships

The user can create a summary S-A-V-D by entering the desired stage increments and the remainder of the table will populate automatically.

The user should graphically compare the summary S-A-V-D table to the full S-A-V-D table in the chart to confirm it captures all key transition points.

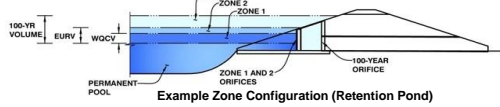
[illegible]

# DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.04 (February 2021)

Project: **Flying Horse North Master Drainage Plan**

Basin ID: **Pond 6**



Example Zone Configuration (Retention Pond)

## Watershed Information

|   |                |
|---|----------------|
| Selected BMP Type =                     | <b>EDB</b>     |
| Watershed Area =                        | 26.83 acres    |
| Watershed Length =                      | 1,140 ft       |
| Watershed Length to Centroid =          | 570 ft         |
| Watershed Slope =                       | 0.039 ft/ft    |
| Watershed Imperviousness =              | 33.19% percent |
| Percentage Hydrologic Soil Group A =    | 0.0% percent   |
| Percentage Hydrologic Soil Group B =    | 100.0% percent |
| Percentage Hydrologic Soil Groups C/D = | 0.0% percent   |
| Target WQCV Drain Time =                | 40.0 hours     |
| Location for 1-hr Rainfall Depths =     | User Input     |

After providing required inputs above including 1-hour rainfall depths, click "Run CUHP" to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

|  |                 |
|--|-----------------|
| Water Quality Capture Volume (WQCV) =  | 0.360 acre-feet |
| Excess Urban Runoff Volume (EURV) =    | 0.921 acre-feet |
| 2-yr Runoff Volume (P1 = 1.19 in.) =   | 0.903 acre-feet |
| 5-yr Runoff Volume (P1 = 1.5 in.) =    | 1.424 acre-feet |
| 10-yr Runoff Volume (P1 = 1.75 in.) =  | 1.899 acre-feet |
| 25-yr Runoff Volume (P1 = 2 in.) =     | 2.602 acre-feet |
| 50-yr Runoff Volume (P1 = 2.25 in.) =  | 3.143 acre-feet |
| 100-yr Runoff Volume (P1 = 2.52 in.) = | 3.855 acre-feet |
| 500-yr Runoff Volume (P1 = 3.14 in.) = | 5.243 acre-feet |
| Approximate 2-yr Detention Volume =    | 0.666 acre-feet |
| Approximate 5-yr Detention Volume =    | 0.945 acre-feet |
| Approximate 10-yr Detention Volume =   | 1.349 acre-feet |
| Approximate 25-yr Detention Volume =   | 1.543 acre-feet |
| Approximate 50-yr Detention Volume =   | 1.623 acre-feet |
| Approximate 100-yr Detention Volume =  | 1.899 acre-feet |

## Optional User Overrides

|      |           |
|------|-----------|
|      | acre-feet |
|      | acre-feet |
| 1.19 | inches    |
| 1.50 | inches    |
| 1.75 | inches    |
| 2.00 | inches    |
| 2.25 | inches    |
| 2.52 | inches    |
|      | inches    |

## Define Zones and Basin Geometry

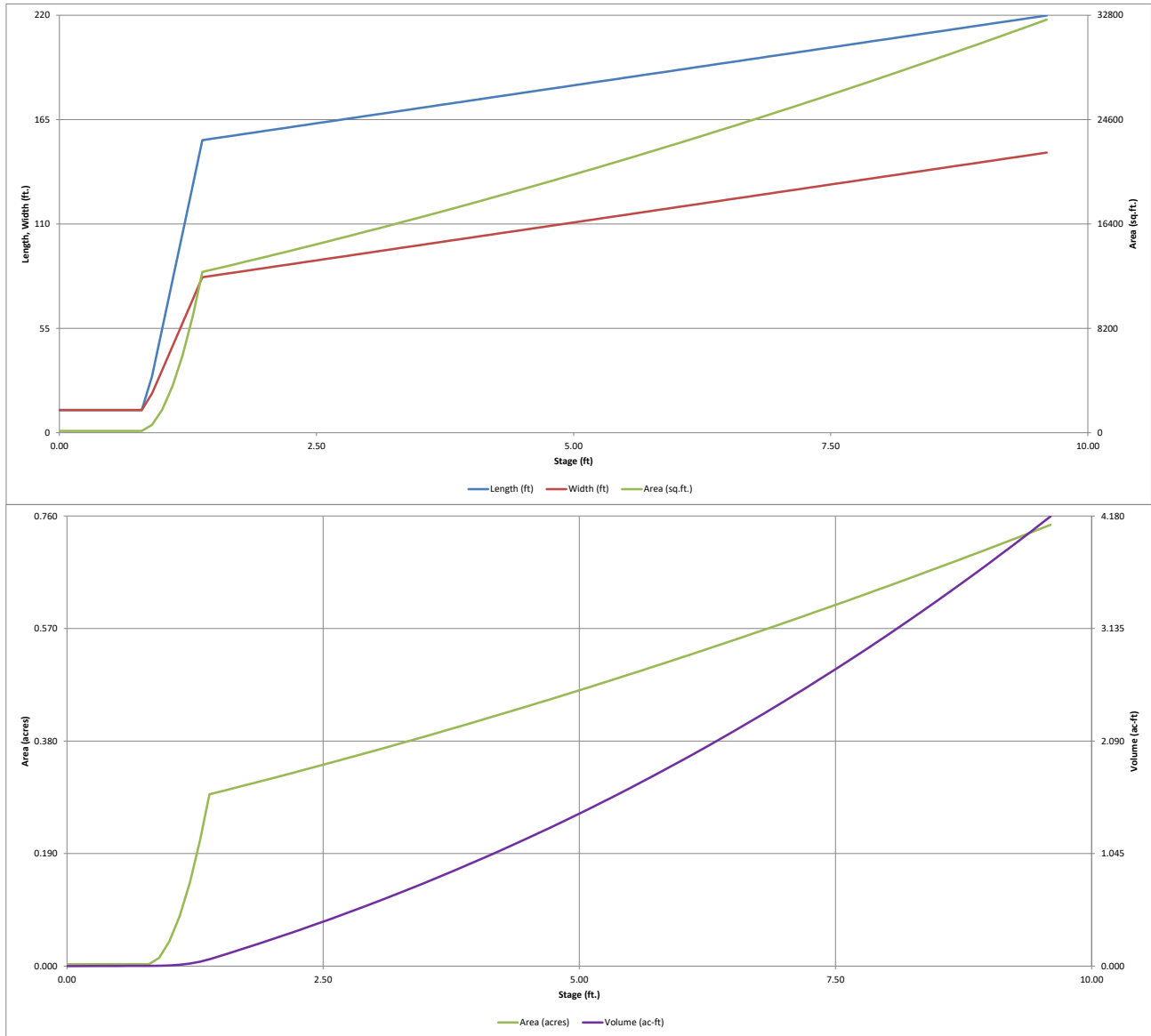
|   |                    |
|---|--------------------|
| Zone 1 Volume (WQCV) =                                  | 0.360 acre-feet    |
| Zone 2 Volume (EURV - Zone 1) =                         | 0.561 acre-feet    |
| Zone 3 Volume (100-year - Zones 1 & 2) =                | 0.978 acre-feet    |
| Total Detention Basin Volume =                          | 1.899 acre-feet    |
| Initial Surge Volume (ISV) =                            | 47 ft <sup>3</sup> |
| Initial Surge Depth (ISD) =                             | 0.33 ft            |
| Total Available Detention Depth (H <sub>total</sub> ) = | 6.00 ft            |
| Depth of Trickle Channel (H <sub>TC</sub> ) =           | 0.50 ft            |
| Slope of Trickle Channel (S <sub>TC</sub> ) =           | 0.004 ft/ft        |
| Slopes of Main Basin Sides (S <sub>main</sub> ) =       | 4 H:V              |
| Basin Length-to-Width Ratio (R <sub>L/W</sub> ) =       | 2                  |

|   |                        |
|---|------------------------|
| Initial Surge Area (A <sub>ISV</sub> ) =              | 143 ft <sup>2</sup>    |
| Surcharge Volume Length (L <sub>ISV</sub> ) =         | 11.9 ft                |
| Surcharge Volume Width (W <sub>ISV</sub> ) =          | 11.9 ft                |
| Depth of Basin Floor (H <sub>FLOOR</sub> ) =          | 0.56 ft                |
| Length of Basin Floor (L <sub>FLOOR</sub> ) =         | 154.2 ft               |
| Width of Basin Floor (W <sub>FLOOR</sub> ) =          | 81.9 ft                |
| Area of Basin Floor (A <sub>FLOOR</sub> ) =           | 12,634 ft <sup>2</sup> |
| Volume of Basin Floor (V <sub>FLOOR</sub> ) =         | 2,636 ft <sup>3</sup>  |
| Depth of Main Basin (H <sub>MAIN</sub> ) =            | 4.61 ft                |
| Length of Main Basin (L <sub>MAIN</sub> ) =           | 191.1 ft               |
| Width of Main Basin (W <sub>MAIN</sub> ) =            | 118.8 ft               |
| Area of Main Basin (A <sub>MAIN</sub> ) =             | 22,702 ft <sup>2</sup> |
| Volume of Main Basin (V <sub>MAIN</sub> ) =           | 80,325 ft <sup>3</sup> |
| Calculated Total Basin Volume (V <sub>total</sub> ) = | 1.907 acre-feet        |

| Depth Increment =           | 0.10       | ft                           |             |            |                         |   |             |                           |                |
|-----------------------------|------------|------------------------------|-------------|------------|-------------------------|---|-------------|---------------------------|----------------|
| Stage - Storage Description | Stage (ft) | Optional Override Stage (ft) | Length (ft) | Width (ft) | Area (ft <sup>2</sup> ) | Optional Override Area (ft <sup>2</sup> ) | Area (acre) | Volume (ft <sup>3</sup> ) | Volume (ac-ft) |
| Top of Micropool            | 0.00       |                              | 11.9        | 11.9       | 143                     |   | 0.003       |                           |                |
| ISV                         | 0.33       |                              | 11.9        | 11.9       | 143                     |   | 0.003       | 47                        | 0.001          |
|                             | 0.40       |                              | 11.9        | 11.9       | 143                     |   | 0.003       | 57                        | 0.001          |
|                             | 0.50       |                              | 11.9        | 11.9       | 143                     |   | 0.003       | 71                        | 0.002          |
|                             | 0.60       |                              | 11.9        | 11.9       | 143                     |   | 0.003       | 86                        | 0.002          |
|                             | 0.70       |                              | 11.9        | 11.9       | 143                     |   | 0.003       | 100                       | 0.002          |
|                             | 0.80       |                              | 11.9        | 11.9       | 143                     |   | 0.003       | 114                       | 0.003          |
|                             | 0.90       |                              | 29.7        | 20.7       | 615                     |   | 0.014       | 143                       | 0.003          |
|                             | 1.00       |                              | 55.1        | 33.2       | 1,830                   |   | 0.042       | 260                       | 0.006          |
|                             | 1.10       |                              | 80.5        | 45.7       | 3,679                   |   | 0.084       | 530                       | 0.012          |
|                             | 1.20       |                              | 105.9       | 58.2       | 6,164                   |   | 0.142       | 1,017                     | 0.023          |
|                             | 1.30       |                              | 131.3       | 70.7       | 9,283                   |   | 0.213       | 1,784                     | 0.041          |
| Floor                       | 1.39       |                              | 154.2       | 81.9       | 12,634                  |   | 0.290       | 2,766                     | 0.064          |
|                             | 1.40       |                              | 154.3       | 82.0       | 12,653                  |   | 0.290       | 2,893                     | 0.066          |
|                             | 1.50       |                              | 155.1       | 82.8       | 12,842                  |   | 0.295       | 4,168                     | 0.096          |
|                             | 1.60       |                              | 155.9       | 83.6       | 13,033                  |   | 0.299       | 5,461                     | 0.125          |
|                             | 1.70       |                              | 156.7       | 84.4       | 13,226                  |   | 0.304       | 6,774                     | 0.156          |
|                             | 1.80       |                              | 157.5       | 85.2       | 13,419                  |   | 0.308       | 8,107                     | 0.186          |
|                             | 1.90       |                              | 158.3       | 86.0       | 13,614                  |   | 0.313       | 9,458                     | 0.217          |
|                             | 2.00       |                              | 159.1       | 86.8       | 13,810                  |   | 0.317       | 10,829                    | 0.249          |
|                             | 2.10       |                              | 159.9       | 87.6       | 14,007                  |   | 0.322       | 12,220                    | 0.281          |
|                             | 2.20       |                              | 160.7       | 88.4       | 14,206                  |   | 0.326       | 13,631                    | 0.313          |
|                             | 2.30       |                              | 161.5       | 89.2       | 14,406                  |   | 0.331       | 15,062                    | 0.346          |
| Zone 1 (WQCV)               | 2.35       |                              | 161.9       | 89.6       | 14,506                  |   | 0.333       | 15,784                    | 0.362          |
|                             | 2.40       |                              | 162.3       | 90.0       | 14,607                  |   | 0.335       | 16,512                    | 0.379          |
|                             | 2.50       |                              | 163.1       | 90.8       | 14,810                  |   | 0.340       | 17,983                    | 0.413          |
|                             | 2.60       |                              | 163.9       | 91.6       | 15,013                  |   | 0.345       | 19,474                    | 0.447          |
|                             | 2.70       |                              | 164.7       | 92.4       | 15,218                  |   | 0.349       | 20,986                    | 0.482          |
|                             | 2.80       |                              | 165.5       | 93.2       | 15,425                  |   | 0.354       | 22,518                    | 0.517          |
|                             | 2.90       |                              | 166.3       | 94.0       | 15,632                  |   | 0.359       | 24,071                    | 0.553          |
|                             | 3.00       |                              | 167.1       | 94.8       | 15,841                  |   | 0.364       | 25,644                    | 0.589          |
|                             | 3.10       |                              | 167.9       | 95.6       | 16,051                  |   | 0.368       | 27,239                    | 0.625          |
|                             | 3.20       |                              | 168.7       | 96.4       | 16,263                  |   | 0.373       | 28,855                    | 0.662          |
|                             | 3.30       |                              | 169.5       | 97.2       | 16,475                  |   | 0.378       | 30,492                    | 0.700          |
|                             | 3.40       |                              | 170.3       | 98.0       | 16,689                  |   | 0.383       | 32,150                    | 0.738          |
|                             | 3.50       |                              | 171.1       | 98.8       | 16,905                  |   | 0.388       | 33,829                    | 0.777          |
|                             | 3.60       |                              | 171.9       | 99.6       | 17,121                  |   | 0.393       | 35,531                    | 0.816          |
|                             | 3.70       |                              | 172.7       | 100.4      | 17,339                  |   | 0.398       | 37,254                    | 0.855          |
|                             | 3.80       |                              | 173.5       | 101.2      | 17,558                  |   | 0.403       | 38,999                    | 0.895          |
| Zone 2 (EURV)               | 3.87       |                              | 174.0       | 101.8      | 17,712                  |   | 0.407       | 40,233                    | 0.924          |
|                             | 3.90       |                              | 174.3       | 102.0      | 17,778                  |   | 0.408       | 40,765                    | 0.936          |
|                             | 4.00       |                              | 175.1       | 102.8      | 18,000                  |   | 0.413       | 42,554                    | 0.977          |
|                             | 4.10       |                              | 175.9       | 103.6      | 18,223                  |   | 0.418       | 44,365                    | 1.018          |
|                             | 4.20       |                              | 176.7       | 104.4      | 18,447                  |   | 0.423       | 46,199                    | 1.061          |
|                             | 4.30       |                              | 177.5       | 105.2      | 18,673                  |   | 0.429       | 48,055                    | 1.103          |
|                             | 4.40       |                              | 178.3       | 106.0      | 18,900                  |   | 0.434       | 49,934                    | 1.146          |
|                             | 4.50       |                              | 179.1       | 106.8      | 19,128                  |   | 0.439       | 51,835                    | 1.190          |
|                             | 4.60       |                              | 179.9       | 107.6      | 19,357                  |   | 0.444       | 53,759                    | 1.234          |
|                             | 4.70       |                              | 180.7       | 108.4      | 19,588                  |   | 0.450       | 55,706                    | 1.279          |
|                             | 4.80       |                              | 181.5       | 109.2      | 19,820                  |   | 0.455       | 57,677                    | 1.324          |
|                             | 4.90       |                              | 182.3       | 110.0      | 20,053                  |   | 0.460       | 59,670                    | 1.370          |
|                             | 5.00       |                              | 183.1       | 110.8      | 20,287                  |   | 0.466       | 61,687                    | 1.416          |
|                             | 5.10       |                              | 183.9       | 111.6      | 20,523                  |   | 0.471       | 63,728                    | 1.463          |
|                             | 5.20       |                              | 184.7       | 112.4      | 20,760                  |   | 0.477       | 65,792                    | 1.510          |
|                             | 5.30       |                              | 185.5       | 113.2      | 20,998                  |   | 0.482       | 67,880                    | 1.558          |
|                             | 5.40       |                              | 186.3       | 114.0      | 21,238                  |   | 0.488       | 69,992                    | 1.607          |
|                             | 5.50       |                              | 187.1       | 114.8      | 21,479                  |   | 0.493       | 72,127                    | 1.656          |
|                             | 5.60       |                              | 187.9       | 115.6      | 21,721                  |   | 0.499       | 74,287                    | 1.705          |
|                             | 5.70       |                              | 188.7       | 116.4      | 21,964                  |   | 0.504       | 76,472                    | 1.756          |
|                             | 5.80       |                              | 189.5       | 117.2      | 22,209                  |   | 0.510       | 78,680                    | 1.806          |
|                             | 5.90       |                              | 190.3       | 118.0      | 22,455                  |   | 0.515       | 80,914                    | 1.858          |
| Zone 3 (100-year)           | 5.98       |                              | 190.9       | 118.7      | 22,653                  |   | 0.520       | 82,718                    | 1.899          |
|                             | 6.00       |                              | 191.1       | 118.8      | 22,702                  |   | 0.521       | 83,171                    | 1.909          |
|                             | 6.10       |                              | 191.9       | 119.6      | 22,951                  |   | 0.527       | 85,454                    | 1.962          |
|                             | 6.20       |                              | 192.7       | 120.4      | 23,201                  |   | 0.533       | 87,762                    | 2.015          |
|                             | 6.30       |                              | 193.5       | 121.2      | 23,452                  |   | 0.538       | 90,094                    | 2.068          |
|                             | 6.40       |                              | 194.3       | 122.0      | 23,704                  |   | 0.544       | 92,452                    | 2.122          |
|                             | 6.50       |                              | 195.1       | 122.8      | 23,958                  |   | 0.550       | 94,835                    | 2.177          |
|                             | 6.60       |                              | 195.9       | 123.6      | 24,213                  |   | 0.556       | 97,244                    | 2.232          |
|                             | 6.70       |                              | 196.7       | 124.4      | 24,469                  |   | 0.562       | 99,678                    | 2.288          |
|                             | 6.80       |                              | 197.5       | 125.2      | 24,727                  |   | 0.568       | 102,137                   | 2.345          |
|                             | 6.90       |                              | 198.3       | 126.0      | 24,985                  |   | 0.574       | 104,623                   | 2.402          |
|                             | 7.00       |                              | 199.1       | 126.8      | 25,245                  |   | 0.580       | 107,135                   | 2.459          |
|                             | 7.10       |                              | 199.9       | 127.6      | 25,507                  |   | 0.586       | 109,672                   | 2.518          |
|                             | 7.20       |                              | 200.7       | 128.4      | 25,769                  |   | 0.592       | 112,236                   | 2.577          |
|                             | 7.30       |                              | 201.5       | 129.2      | 26,033                  |   | 0.598       | 114,826                   | 2.636          |
|                             | 7.40       |                              | 202.3       | 130.0      | 26,298                  |   | 0.604       | 117,443                   | 2.696          |
|                             | 7.50       |                              | 203.1       | 130.8      | 26,565                  |   | 0.610       | 120,086                   | 2.757          |
|                             | 7.60       |                              | 203.9       | 131.6      | 26,833                  |   | 0.616       | 122,756                   | 2.818          |
|                             | 7.70       |                              | 204.7       | 132.4      | 27,102                  |   | 0.622       | 125,452                   | 2.880          |
|                             | 7.80       |                              | 205.5       | 133.2      | 27,372                  |   | 0.628       | 128,176                   | 2.943          |
|                             | 7.90       |                              | 206.3       | 134.0      | 27,644                  |   | 0.635       | 130,927                   | 3.006          |
|                             | 8.00       |                              | 207.1       | 134.8      | 27,916                  |   | 0.641       | 133,705                   | 3.069          |
|                             | 8.10       |                              | 207.9       | 135.6      | 28,191                  |   | 0.647       | 136,510                   | 3.134          |
|                             | 8.20       |                              | 208.7       | 136.4      | 28,466                  |   | 0.653       | 139,343                   | 3.199          |
|                             | 8.30       |                              | 209.5       | 137.2      | 28,743                  |   | 0.660       | 142,203                   | 3.265          |
|                             | 8.40       |                              | 210.3       | 138.0      | 29,021                  |   | 0.666       | 145,092                   | 3.331          |
|                             | 8.50       |                              | 211.1       | 138.8      | 29,300                  |   | 0.673       | 148,008                   | 3.398          |
|                             | 8.60       |                              | 211.9       | 139.6      | 29,581                  |   | 0.679       | 150,952                   | 3.465          |
|                             | 8.70       |                              | 212.7       | 140.4      | 29,862                  |   | 0.686       | 153,924                   | 3.534          |
|                             | 8.80       |                              | 213.5       | 141.2      | 30,145                  |   | 0.692       | 156,924                   | 3.602          |
|                             | 8.90       |                              | 214.3       | 142.0      | 30,430                  |   | 0.699       | 159,953                   | 3.672          |
|                             | 9.00       |                              | 215.1       | 142.8      | 30,715                  |   | 0.705       | 163,010                   | 3.742          |
|                             | 9.10       |                              | 215.9       | 143.6      | 31,002                  |   | 0.712       | 166,096                   | 3.813          |
|                             | 9.20       |                              | 216.7       | 144.4      | 31,291                  |   | 0.718       | 169,211                   | 3.885          |
|                             | 9.30       |                              | 217.5       | 145.2      | 31,580                  |   | 0.725       | 172,354                   | 3.957          |
|                             | 9.40       |                              | 218.3       | 146.0      | 31,871                  |   | 0.732       | 175,527                   | 4.030          |
|                             | 9.50       |                              | 219.1       | 146.8      | 32,163                  |   | 0.738       | 178,728                   | 4.103          |
|                             | 9.60       |                              | 219.9       | 147.6      | 32,456                  |   | 0.745       | 181,959                   | 4.177          |

# DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.04 (February 2021)

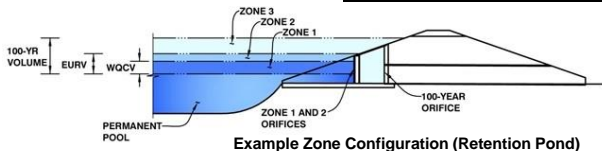


# DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.04 (February 2021)

Project: Flying Horse North Master Drainage Plan

Basin ID: Pond 6



Example Zone Configuration (Retention Pond)

|                   | Estimated Stage (ft) | Estimated Volume (ac-ft) | Outlet Type          |
|-------------------|----------------------|--------------------------|----------------------|
| Zone 1 (WQCV)     | 2.35                 | 0.360                    | Orifice Plate        |
| Zone 2 (EURV)     | 3.87                 | 0.561                    | Circular Orifice     |
| Zone 3 (100-year) | 5.98                 | 0.978                    | Weir&Pipe (Restrict) |
| Total (all zones) |                      | 1.899                    |                      |

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth =  ft (distance below the filtration media surface)  
Underdrain Orifice Diameter =  inches

Calculated Parameters for Underdrain  
Underdrain Orifice Area =  ft<sup>2</sup>  
Underdrain Orifice Centroid =  feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice =  ft (relative to basin bottom at Stage = 0 ft)  
Depth at top of Zone using Orifice Plate =  ft (relative to basin bottom at Stage = 0 ft)  
Orifice Plate: Orifice Vertical Spacing =  inches  
Orifice Plate: Orifice Area per Row =  sq. inches (diameter = 1-1/4 inches)

Calculated Parameters for Plate  
WQ Orifice Area per Row =  ft<sup>2</sup>  
Elliptical Half-Width =  feet  
Elliptical Slot Centroid =  feet  
Elliptical Slot Area =  ft<sup>2</sup>

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

|                                | Row 1 (required) | Row 2 (optional) | Row 3 (optional) | Row 4 (optional) | Row 5 (optional) | Row 6 (optional) | Row 7 (optional) | Row 8 (optional) |
|--------------------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|
| Stage of Orifice Centroid (ft) | 0.00             | 0.78             | 1.57             |                  |                  |                  |                  |                  |
| Orifice Area (sq. inches)      | 1.27             | 1.27             | 1.27             |                  |                  |                  |                  |                  |

|                                | Row 9 (optional) | Row 10 (optional) | Row 11 (optional) | Row 12 (optional) | Row 13 (optional) | Row 14 (optional) | Row 15 (optional) | Row 16 (optional) |
|--------------------------------|------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| Stage of Orifice Centroid (ft) |                  |                   |                   |                   |                   |                   |                   |                   |
| Orifice Area (sq. inches)      |                  |                   |                   |                   |                   |                   |                   |                   |

User Input: Vertical Orifice (Circular or Rectangular)

Invert of Vertical Orifice =  ft (relative to basin bottom at Stage = 0 ft)  
Depth at top of Zone using Vertical Orifice =  ft (relative to basin bottom at Stage = 0 ft)  
Vertical Orifice Diameter =  inches

Calculated Parameters for Vertical Orifice  
Zone 2 Circular Not Selected  
Vertical Orifice Area =  ft<sup>2</sup>  
Vertical Orifice Centroid =  feet

User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe)

Overflow Weir Front Edge Height, H<sub>o</sub> =  ft (relative to basin bottom at Stage = 0 ft)  
Overflow Weir Front Edge Length =  feet  
Overflow Weir Grate Slope =  H:V  
Horiz. Length of Weir Sides =  feet  
Overflow Grate Type =   
Debris Clogging % =  %

Calculated Parameters for Overflow Weir  
Zone 3 Weir Not Selected  
Height of Grate Upper Edge, H<sub>u</sub> =  feet  
Overflow Weir Slope Length =  feet  
Grate Open Area / 100-yr Orifice Area =   
Overflow Grate Open Area w/o Debris =  ft<sup>2</sup>  
Overflow Grate Open Area w/ Debris =  ft<sup>2</sup>

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

Depth to Invert of Outlet Pipe =  ft (distance below basin bottom at Stage = 0 ft)  
Outlet Pipe Diameter =  inches  
Restrictor Plate Height Above Pipe Invert =  inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate  
Zone 3 Restrictor Not Selected  
Outlet Orifice Area =  ft<sup>2</sup>  
Outlet Orifice Centroid =  feet  
Half-Central Angle of Restrictor Plate on Pipe =  radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage =  ft (relative to basin bottom at Stage = 0 ft)  
Spillway Crest Length =  feet  
Spillway End Slopes =  H:V  
Freeboard above Max Water Surface =  feet

Calculated Parameters for Spillway  
Spillway Design Flow Depth =  feet  
Stage at Top of Freeboard =  feet  
Basin Area at Top of Freeboard =  acres  
Basin Volume at Top of Freeboard =  acre-ft

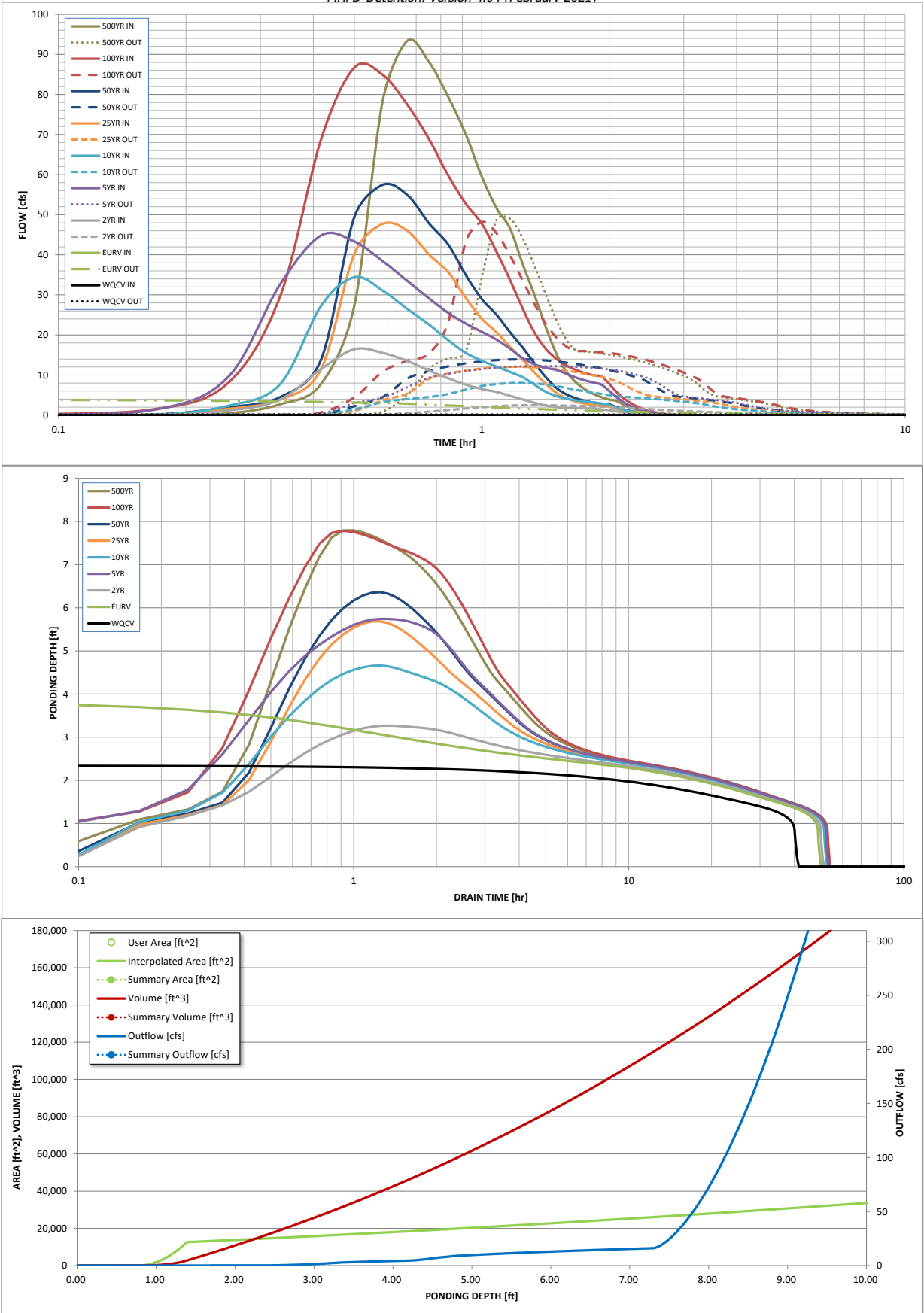
## Routed Hydrograph Results

The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).

|  | WQCV               | EURV               | 2 Year             | 5 Year          | 10 Year         | 25 Year         | 50 Year         | 100 Year | 500 Year |
|--|--------------------|--------------------|--------------------|-----------------|-----------------|-----------------|-----------------|----------|----------|
| Design Storm Return Period =                       | N/A                | N/A                | 1.19               | 1.50            | 1.75            | 2.00            | 2.25            | 2.52     | 3.14     |
| One-Hour Rainfall Depth (in) =                     | 0.360              | 0.921              | 0.903              | 1.424           | 1.899           | 2.602           | 3.143           | 3.855    | 5.243    |
| CUHP Runoff Volume (acre-ft) =                     | N/A                | N/A                | 0.903              | 3.107           | 1.899           | 2.602           | 3.143           | 5.635    | 5.243    |
| User Override Inflow Hydrograph Volume (acre-ft) = | N/A                | N/A                | 4.3                | 11.6            | 17.2            | 30.3            | 37.9            | 47.5     | 65.9     |
| CUHP Predevelopment Peak Q (cfs) =                 | N/A                | N/A                |                    |                 |                 |                 |                 |          |          |
| OPTIONAL Override Predevelopment Peak Q (cfs) =    | N/A                | N/A                |                    |                 |                 |                 |                 |          |          |
| Predevelopment Unit Peak Flow, q (cfs/acre) =      | N/A                | N/A                | 0.16               | 0.43            | 0.64            | 1.13            | 1.41            | 1.77     | 2.46     |
| Peak Inflow Q (cfs) =                              | N/A                | N/A                | 16.5               | 44.8            | 34.4            | 47.7            | 57.5            | 86.7     | 93.4     |
| Peak Outflow Q (cfs) =                             | 0.2                | 4.0                | 2.5                | 12.2            | 8.0             | 12.1            | 13.9            | 48.2     | 49.0     |
| Ratio Peak Outflow to Predevelopment Q =           | N/A                | N/A                | N/A                | 1.0             | 0.5             | 0.4             | 0.4             | 1.0      | 0.7      |
| Structure Controlling Flow =                       | Vertical Orifice 1 | Vertical Orifice 1 | Vertical Orifice 1 | Overflow Weir 1 | Overflow Weir 1 | Overflow Weir 1 | Overflow Weir 1 | Spillway | Spillway |
| Max Velocity through Grate 1 (fps) =               | N/A                | N/A                | N/A                | 3.5             | 1.7             | 3.4             | 4.2             | 5.4      | 5.4      |
| Max Velocity through Grate 2 (fps) =               | N/A                | N/A                | N/A                | N/A             | N/A             | N/A             | N/A             | N/A      | N/A      |
| Time to Drain 97% of Inflow Volume (hours) =       | 39                 | 44                 | 46                 | 38              | 43              | 40              | 38              | 30       | 31       |
| Time to Drain 99% of Inflow Volume (hours) =       | 40                 | 48                 | 49                 | 47              | 48              | 48              | 47              | 44       | 44       |
| Maximum Ponding Depth (ft) =                       | 2.35               | 3.87               | 3.27               | 5.74            | 4.66            | 5.68            | 6.36            | 7.79     | 7.79     |
| Area at Maximum Ponding Depth (acres) =            | 0.33               | 0.41               | 0.38               | 0.51            | 0.45            | 0.50            | 0.54            | 0.63     | 0.63     |
| Maximum Volume Stored (acre-ft) =                  | 0.362              | 0.924              | 0.685              | 1.776           | 1.261           | 1.745           | 2.101           | 2.930    | 2.936    |

DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.04 (February 2021)



| S-A-V-D Chart Axis Override | X-axis | Left Y-Axis | Right Y-Axis |
|-----------------------------|--------|-------------|--------------|
| minimum bound               |        |             |              |
| maximum bound               |        |             |              |

# DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename: ...[SWM]Outflow hydrographs\Pond6 OutflowHydrograph.xlsx

## Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

|               | SOURCE  | CUHP       | CUHP       | CUHP         | USER         | CUHP          | CUHP          | CUHP          | USER           | CUHP           |
|---------------|---------|------------|------------|--------------|--------------|---------------|---------------|---------------|----------------|----------------|
| Time Interval | TIME    | WQCV [cfs] | EURV [cfs] | 2 Year [cfs] | 5 Year [cfs] | 10 Year [cfs] | 25 Year [cfs] | 50 Year [cfs] | 100 Year [cfs] | 500 Year [cfs] |
| 5.00 min      | 0:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 0:05:00 | 0.00       | 0.00       | 0.00         | 0.02         | 0.00          | 0.00          | 0.00          | 0.09           | 0.00           |
|               | 0:10:00 | 0.00       | 0.00       | 0.00         | 1.28         | 0.00          | 0.00          | 0.13          | 1.42           | 0.41           |
|               | 0:15:00 | 0.00       | 0.00       | 1.10         | 9.19         | 2.27          | 1.53          | 1.91          | 7.77           | 2.68           |
|               | 0:20:00 | 0.00       | 0.00       | 3.88         | 32.51        | 7.65          | 3.83          | 4.46          | 29.44          | 7.72           |
|               | 0:25:00 | 0.00       | 0.00       | 11.46        | 44.81        | 27.18         | 11.35         | 13.73         | 68.64          | 27.37          |
|               | 0:30:00 | 0.00       | 0.00       | 16.45        | 43.32        | 34.42         | 40.25         | 49.45         | 86.70          | 78.42          |
|               | 0:35:00 | 0.00       | 0.00       | 15.52        | 38.43        | 31.05         | 47.72         | 57.47         | 84.90          | 93.38          |
|               | 0:40:00 | 0.00       | 0.00       | 13.51        | 33.50        | 26.49         | 46.00         | 54.93         | 77.48          | 88.14          |
|               | 0:45:00 | 0.00       | 0.00       | 11.12        | 29.15        | 22.63         | 40.10         | 47.88         | 68.88          | 79.41          |
|               | 0:50:00 | 0.00       | 0.00       | 9.18         | 25.51        | 18.68         | 35.67         | 42.56         | 59.79          | 70.00          |
|               | 0:55:00 | 0.00       | 0.00       | 7.60         | 22.86        | 15.52         | 29.20         | 34.93         | 52.73          | 59.52          |
|               | 1:00:00 | 0.00       | 0.00       | 6.52         | 20.78        | 13.55         | 24.05         | 28.95         | 47.77          | 51.66          |
|               | 1:05:00 | 0.00       | 0.00       | 5.79         | 18.84        | 12.11         | 20.68         | 25.05         | 40.76          | 46.51          |
|               | 1:10:00 | 0.00       | 0.00       | 4.81         | 16.55        | 10.75         | 16.99         | 20.66         | 33.68          | 37.61          |
|               | 1:15:00 | 0.00       | 0.00       | 3.90         | 14.19        | 9.44          | 13.77         | 16.83         | 26.52          | 29.85          |
|               | 1:20:00 | 0.00       | 0.00       | 3.08         | 12.64        | 7.58          | 10.57         | 12.86         | 20.51          | 21.91          |
|               | 1:25:00 | 0.00       | 0.00       | 2.40         | 11.79        | 5.80          | 7.81          | 9.45          | 16.51          | 15.33          |
|               | 1:30:00 | 0.00       | 0.00       | 2.00         | 11.26        | 4.76          | 5.55          | 6.78          | 14.04          | 10.88          |
|               | 1:35:00 | 0.00       | 0.00       | 1.82         | 10.33        | 4.13          | 4.22          | 5.21          | 12.41          | 8.22           |
|               | 1:40:00 | 0.00       | 0.00       | 1.74         | 9.38         | 3.70          | 3.41          | 4.23          | 11.29          | 6.50           |
|               | 1:45:00 | 0.00       | 0.00       | 1.68         | 8.67         | 3.39          | 2.88          | 3.58          | 10.51          | 5.31           |
|               | 1:50:00 | 0.00       | 0.00       | 1.64         | 8.14         | 3.18          | 2.53          | 3.16          | 9.96           | 4.49           |
|               | 1:55:00 | 0.00       | 0.00       | 1.43         | 7.59         | 2.90          | 2.31          | 2.88          | 9.61           | 3.90           |
|               | 2:00:00 | 0.00       | 0.00       | 1.25         | 6.09         | 2.51          | 2.16          | 2.68          | 7.83           | 3.53           |
|               | 2:05:00 | 0.00       | 0.00       | 0.94         | 4.45         | 1.84          | 1.59          | 1.97          | 5.73           | 2.57           |
|               | 2:10:00 | 0.00       | 0.00       | 0.69         | 3.20         | 1.32          | 1.15          | 1.42          | 4.16           | 1.84           |
|               | 2:15:00 | 0.00       | 0.00       | 0.51         | 2.27         | 0.94          | 0.82          | 1.02          | 3.00           | 1.33           |
|               | 2:20:00 | 0.00       | 0.00       | 0.37         | 1.57         | 0.68          | 0.59          | 0.73          | 2.12           | 0.96           |
|               | 2:25:00 | 0.00       | 0.00       | 0.26         | 1.08         | 0.48          | 0.41          | 0.51          | 1.48           | 0.67           |
|               | 2:30:00 | 0.00       | 0.00       | 0.18         | 0.73         | 0.33          | 0.29          | 0.36          | 1.02           | 0.47           |
|               | 2:35:00 | 0.00       | 0.00       | 0.12         | 0.48         | 0.22          | 0.20          | 0.25          | 0.66           | 0.32           |
|               | 2:40:00 | 0.00       | 0.00       | 0.08         | 0.28         | 0.14          | 0.13          | 0.16          | 0.39           | 0.20           |
|               | 2:45:00 | 0.00       | 0.00       | 0.04         | 0.15         | 0.07          | 0.07          | 0.09          | 0.20           | 0.11           |
|               | 2:50:00 | 0.00       | 0.00       | 0.02         | 0.07         | 0.03          | 0.03          | 0.04          | 0.09           | 0.04           |
|               | 2:55:00 | 0.00       | 0.00       | 0.01         | 0.02         | 0.01          | 0.01          | 0.01          | 0.03           | 0.01           |
|               | 3:00:00 | 0.00       | 0.00       | 0.00         | 0.01         | 0.00          | 0.00          | 0.00          | 0.01           | 0.00           |
|               | 3:05:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:10:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:15:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:20:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:25:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:30:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:35:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:40:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:45:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:50:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:55:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:05:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:10:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:15:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:20:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:25:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:30:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:35:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:40:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:45:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:50:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:55:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:05:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:10:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:15:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:20:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:25:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:30:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:35:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:40:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:45:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:50:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:55:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 6:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |

## DETENTION BASIN OUTLET STRUCTURE DESIGN

*MHFD-Detention, Version 4.04 (February 2021)*

### Summary Stage-Area-Volume-Discharge Relationships

The user can create a summary S-A-V-D by entering the desired stage increments and the remainder of the table will populate automatically.

The user should graphically compare the summary S-A-V-D table to the full S-A-V-D table in the chart to confirm it captures all key transition points.

[illegible]

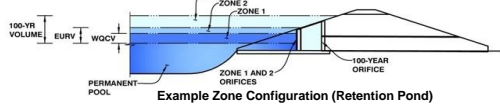


# DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.04 (February 2021)

Project: **Flying Horse North Master Drainage Plan**

Basin ID: **Pond 7**



Example Zone Configuration (Retention Pond)

## Watershed Information

|   |                |                       |
|---|----------------|-----------------------|
| Selected BMP Type =                     | <b>EDB</b>     | Note: L / W Ratio < 1 |
| Watershed Area =                        | 114.73 acres   | L / W Ratio = 0.57    |
| Watershed Length =                      | 1,683 ft       |                       |
| Watershed Length to Centroid =          | 1,362 ft       |                       |
| Watershed Slope =                       | 0.040 ft/ft    |                       |
| Watershed Imperviousness =              | 38.80% percent |                       |
| Percentage Hydrologic Soil Group A =    | 0.0% percent   |                       |
| Percentage Hydrologic Soil Group B =    | 100.0% percent |                       |
| Percentage Hydrologic Soil Groups C/D = | 0.0% percent   |                       |
| Target WQCV Drain Time =                | 40.0 hours     |                       |
| Location for 1-hr Rainfall Depths =     | User Input     |                       |

After providing required inputs above including 1-hour rainfall depths, click "Run CUHP" to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

|  |                  |             |
|--|------------------|-------------|
| Water Quality Capture Volume (WQCV) =  | 1.689 acre-feet  |             |
| Excess Urban Runoff Volume (EURV) =    | 4.663 acre-feet  |             |
| 2-yr Runoff Volume (P1 = 1.19 in.) =   | 4.575 acre-feet  | 1.19 inches |
| 5-yr Runoff Volume (P1 = 1.5 in.) =    | 6.891 acre-feet  | 1.50 inches |
| 10-yr Runoff Volume (P1 = 1.75 in.) =  | 8.978 acre-feet  | 1.75 inches |
| 25-yr Runoff Volume (P1 = 2 in.) =     | 11.989 acre-feet | 2.00 inches |
| 50-yr Runoff Volume (P1 = 2.25 in.) =  | 14.328 acre-feet | 2.25 inches |
| 100-yr Runoff Volume (P1 = 2.52 in.) = | 17.379 acre-feet | 2.52 inches |
| 500-yr Runoff Volume (P1 = 3.14 in.) = | 23.422 acre-feet |             |
| Approximate 2-yr Detention Volume =    | 3.427 acre-feet  |             |
| Approximate 5-yr Detention Volume =    | 4.799 acre-feet  |             |
| Approximate 10-yr Detention Volume =   | 6.641 acre-feet  |             |
| Approximate 25-yr Detention Volume =   | 7.450 acre-feet  |             |
| Approximate 50-yr Detention Volume =   | 7.822 acre-feet  |             |
| Approximate 100-yr Detention Volume =  | 8.992 acre-feet  |             |

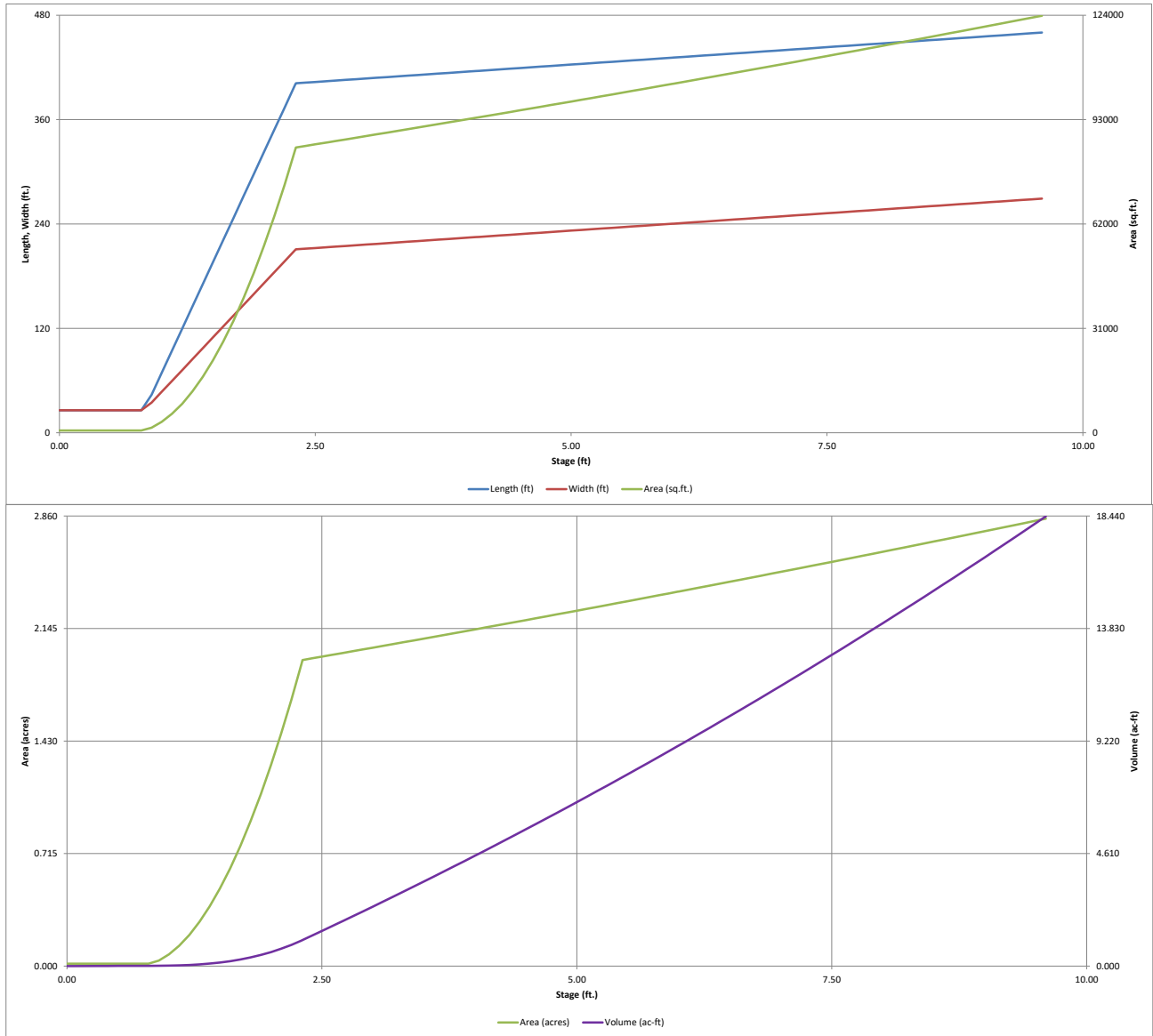
## Define Zones and Basin Geometry

|   |                         |
|---|-------------------------|
| Zone 1 Volume (WQCV) =                                  | 1.689 acre-feet         |
| Zone 2 Volume (EURV - Zone 1) =                         | 2.974 acre-feet         |
| Zone 3 Volume (100-year - Zones 1 & 2) =                | 4.329 acre-feet         |
| Total Detention Basin Volume =                          | 8.992 acre-feet         |
| Initial Surge Volume (ISV) =                            | 221 ft <sup>3</sup>     |
| Initial Surge Depth (ISD) =                             | 0.33 ft                 |
| Total Available Detention Depth (H <sub>total</sub> ) = | 6.00 ft                 |
| Depth of Trickle Channel (H <sub>TC</sub> ) =           | 0.50 ft                 |
| Slope of Trickle Channel (S <sub>TC</sub> ) =           | 0.004 ft/ft             |
| Slopes of Main Basin Sides (S <sub>main</sub> ) =       | 4 H:V                   |
| Basin Length-to-Width Ratio (L <sub>W</sub> ) =         | 2                       |
| Initial Surge Area (A <sub>ISV</sub> ) =                | 669 ft <sup>2</sup>     |
| Surcharge Volume Length (L <sub>ISV</sub> ) =           | 25.9 ft                 |
| Surcharge Volume Width (W <sub>ISV</sub> ) =            | 25.9 ft                 |
| Depth of Basin Floor (H <sub>FLOOR</sub> ) =            | 1.48 ft                 |
| Length of Basin Floor (L <sub>FLOOR</sub> ) =           | 401.8 ft                |
| Width of Basin Floor (W <sub>FLOOR</sub> ) =            | 210.9 ft                |
| Area of Basin Floor (A <sub>FLOOR</sub> ) =             | 84,720 ft <sup>2</sup>  |
| Volume of Basin Floor (V <sub>FLOOR</sub> ) =           | 45,839 ft <sup>3</sup>  |
| Depth of Main Basin (H <sub>MAIN</sub> ) =              | 3.69 ft                 |
| Length of Main Basin (L <sub>MAIN</sub> ) =             | 431.3 ft                |
| Width of Main Basin (W <sub>MAIN</sub> ) =              | 240.4 ft                |
| Area of Main Basin (A <sub>MAIN</sub> ) =               | 103,677 ft <sup>2</sup> |
| Volume of Main Basin (V <sub>MAIN</sub> ) =             | 347,004 ft <sup>3</sup> |
| Calculated Total Basin Volume (V <sub>total</sub> ) =   | <b>9.031</b> acre-feet  |

| Depth Increment =           | 0.10       | ft                           |             |            |                         |   |             |                           |                |
|-----------------------------|------------|------------------------------|-------------|------------|-------------------------|---|-------------|---------------------------|----------------|
| Stage - Storage Description | Stage (ft) | Optional Override Stage (ft) | Length (ft) | Width (ft) | Area (ft <sup>2</sup> ) | Optional Override Area (ft <sup>2</sup> ) | Area (acre) | Volume (ft <sup>3</sup> ) | Volume (ac-ft) |
| Top of Micropool            | 0.00       |                              | 25.9        | 25.9       | 669                     |   | 0.015       |                           |                |
| ISV                         | 0.33       |                              | 25.9        | 25.9       | 669                     |   | 0.015       | 221                       | 0.005          |
|                             | 0.40       |                              | 25.9        | 25.9       | 669                     |   | 0.015       | 268                       | 0.006          |
|                             | 0.50       |                              | 25.9        | 25.9       | 669                     |   | 0.015       | 334                       | 0.008          |
|                             | 0.60       |                              | 25.9        | 25.9       | 669                     |   | 0.015       | 401                       | 0.009          |
|                             | 0.70       |                              | 25.9        | 25.9       | 669                     |   | 0.015       | 468                       | 0.011          |
|                             | 0.80       |                              | 25.9        | 25.9       | 669                     |   | 0.015       | 535                       | 0.012          |
|                             | 0.90       |                              | 43.6        | 34.6       | 1,510                   |   | 0.035       | 630                       | 0.014          |
|                             | 1.00       |                              | 69.0        | 47.1       | 3,253                   |   | 0.075       | 862                       | 0.020          |
|                             | 1.10       |                              | 94.4        | 59.6       | 5,630                   |   | 0.129       | 1,301                     | 0.030          |
|                             | 1.20       |                              | 119.8       | 72.1       | 8,642                   |   | 0.198       | 2,010                     | 0.046          |
|                             | 1.30       |                              | 145.2       | 84.6       | 12,289                  |   | 0.282       | 3,051                     | 0.070          |
|                             | 1.40       |                              | 170.6       | 97.1       | 16,571                  |   | 0.380       | 4,489                     | 0.103          |
|                             | 1.50       |                              | 196.0       | 109.6      | 21,488                  |   | 0.493       | 6,386                     | 0.147          |
|                             | 1.60       |                              | 221.4       | 122.1      | 27,040                  |   | 0.621       | 8,807                     | 0.202          |
|                             | 1.70       |                              | 246.8       | 134.6      | 33,228                  |   | 0.763       | 11,815                    | 0.271          |
|                             | 1.80       |                              | 272.2       | 147.1      | 40,050                  |   | 0.919       | 15,474                    | 0.355          |
|                             | 1.90       |                              | 297.6       | 159.6      | 47,507                  |   | 1.091       | 19,847                    | 0.456          |
|                             | 2.00       |                              | 323.0       | 172.1      | 55,599                  |   | 1.276       | 24,997                    | 0.574          |
|                             | 2.10       |                              | 348.4       | 184.6      | 64,326                  |   | 1.477       | 30,988                    | 0.711          |
|                             | 2.20       |                              | 373.8       | 197.1      | 73,688                  |   | 1.692       | 37,883                    | 0.870          |
|                             | 2.30       |                              | 399.2       | 209.6      | 83,685                  |   | 1.921       | 45,746                    | 1.050          |
| Floor                       | 2.31       |                              | 401.8       | 210.9      | 84,720                  |   | 1.945       | 46,588                    | 1.070          |
|                             | 2.40       |                              | 402.5       | 211.6      | 85,162                  |   | 1.955       | 54,233                    | 1.245          |
|                             | 2.50       |                              | 403.3       | 212.4      | 85,654                  |   | 1.966       | 62,774                    | 1.441          |
|                             | 2.60       |                              | 404.1       | 213.2      | 86,147                  |   | 1.978       | 71,364                    | 1.638          |
| Zone 1 (WQCV)               | 2.63       |                              | 404.3       | 213.4      | 86,295                  |   | 1.981       | 73,950                    | 1.698          |
|                             | 2.70       |                              | 404.9       | 214.0      | 86,641                  |   | 1.989       | 80,003                    | 1.837          |
|                             | 2.80       |                              | 405.7       | 214.8      | 87,137                  |   | 2.000       | 88,692                    | 2.036          |
|                             | 2.90       |                              | 406.5       | 215.6      | 87,634                  |   | 2.012       | 97,431                    | 2.237          |
|                             | 3.00       |                              | 407.3       | 216.4      | 88,132                  |   | 2.023       | 106,219                   | 2.438          |
|                             | 3.10       |                              | 408.1       | 217.2      | 88,632                  |   | 2.035       | 115,057                   | 2.641          |
|                             | 3.20       |                              | 408.9       | 218.0      | 89,133                  |   | 2.046       | 123,945                   | 2.845          |
|                             | 3.30       |                              | 409.7       | 218.8      | 89,635                  |   | 2.058       | 132,884                   | 3.051          |
|                             | 3.40       |                              | 410.5       | 219.6      | 90,138                  |   | 2.069       | 141,872                   | 3.257          |
|                             | 3.50       |                              | 411.3       | 220.4      | 90,643                  |   | 2.081       | 150,911                   | 3.464          |
|                             | 3.60       |                              | 412.1       | 221.2      | 91,149                  |   | 2.092       | 160,001                   | 3.673          |
|                             | 3.70       |                              | 412.9       | 222.0      | 91,656                  |   | 2.104       | 169,141                   | 3.883          |
|                             | 3.80       |                              | 413.7       | 222.8      | 92,165                  |   | 2.116       | 178,332                   | 4.094          |
|                             | 3.90       |                              | 414.5       | 223.6      | 92,675                  |   | 2.128       | 187,574                   | 4.306          |
|                             | 4.00       |                              | 415.3       | 224.4      | 93,186                  |   | 2.139       | 196,867                   | 4.519          |
| Zone 2 (EURV)               | 4.07       |                              | 415.9       | 224.9      | 93,544                  |   | 2.147       | 203,403                   | 4.669          |
|                             | 4.10       |                              | 416.1       | 225.2      | 93,698                  |   | 2.151       | 206,211                   | 4.734          |
|                             | 4.20       |                              | 416.9       | 226.0      | 94,212                  |   | 2.163       | 215,607                   | 4.950          |
|                             | 4.30       |                              | 417.7       | 226.8      | 94,727                  |   | 2.175       | 225,054                   | 5.167          |
|                             | 4.40       |                              | 418.5       | 227.6      | 95,243                  |   | 2.186       | 234,552                   | 5.385          |
|                             | 4.50       |                              | 419.3       | 228.4      | 95,760                  |   | 2.198       | 244,103                   | 5.604          |
|                             | 4.60       |                              | 420.1       | 229.2      | 96,279                  |   | 2.210       | 253,705                   | 5.824          |
|                             | 4.70       |                              | 420.9       | 230.0      | 96,799                  |   | 2.222       | 263,358                   | 6.046          |
|                             | 4.80       |                              | 421.7       | 230.8      | 97,321                  |   | 2.234       | 273,064                   | 6.269          |
|                             | 4.90       |                              | 422.5       | 231.6      | 97,843                  |   | 2.246       | 282,823                   | 6.493          |
|                             | 5.00       |                              | 423.3       | 232.4      | 98,367                  |   | 2.258       | 292,633                   | 6.718          |
|                             | 5.10       |                              | 424.1       | 233.2      | 98,892                  |   | 2.270       | 302,496                   | 6.944          |
|                             | 5.20       |                              | 424.9       | 234.0      | 99,419                  |   | 2.282       | 312,412                   | 7.172          |
|                             | 5.30       |                              | 425.7       | 234.8      | 99,947                  |   | 2.294       | 322,380                   | 7.401          |
|                             | 5.40       |                              | 426.5       | 235.6      | 100,476                 |   | 2.307       | 332,401                   | 7.631          |
|                             | 5.50       |                              | 427.3       | 236.4      | 101,006                 |   | 2.319       | 342,475                   | 7.862          |
|                             | 5.60       |                              | 428.1       | 237.2      | 101,538                 |   | 2.331       | 352,602                   | 8.095          |
|                             | 5.70       |                              | 428.9       | 238.0      | 102,070                 |   | 2.343       | 362,783                   | 8.328          |
|                             | 5.80       |                              | 429.7       | 238.8      | 102,605                 |   | 2.355       | 373,016                   | 8.563          |
|                             | 5.90       |                              | 430.5       | 239.6      | 103,140                 |   | 2.368       | 383,304                   | 8.799          |
| Zone 3 (100-year)           | 5.99       |                              | 431.2       | 240.3      | 103,623                 |   | 2.379       | 392,608                   | 9.013          |
|                             | 6.00       |                              | 431.3       | 240.4      | 103,677                 |   | 2.380       | 393,644                   | 9.037          |
|                             | 6.10       |                              | 432.1       | 241.2      | 104,215                 |   | 2.392       | 404,039                   | 9.275          |
|                             | 6.20       |                              | 432.9       | 242.0      | 104,754                 |   | 2.405       | 414,487                   | 9.515          |
|                             | 6.30       |                              | 433.7       | 242.8      | 105,294                 |   | 2.417       | 424,990                   | 9.756          |
|                             | 6.40       |                              | 434.5       | 243.6      | 105,836                 |   | 2.430       | 435,546                   | 9.999          |
|                             | 6.50       |                              | 435.3       | 244.4      | 106,379                 |   | 2.442       | 446,157                   | 10.242         |
|                             | 6.60       |                              | 436.1       | 245.2      | 106,924                 |   | 2.455       | 456,822                   | 10.487         |
|                             | 6.70       |                              | 436.9       | 246.0      | 107,469                 |   | 2.467       | 467,542                   | 10.733         |
|                             | 6.80       |                              | 437.7       | 246.8      | 108,016                 |   | 2.480       | 478,316                   | 10.981         |
|                             | 6.90       |                              | 438.5       | 247.6      | 108,565                 |   | 2.492       | 489,145                   | 11.229         |
|                             | 7.00       |                              | 439.3       | 248.4      | 109,114                 |   | 2.505       | 500,029                   | 11.479         |
|                             | 7.10       |                              | 440.1       | 249.2      | 109,665                 |   | 2.518       | 510,968                   | 11.730         |
|                             | 7.20       |                              | 440.9       | 250.0      | 110,217                 |   | 2.530       | 521,962                   | 11.983         |
|                             | 7.30       |                              | 441.7       | 250.8      | 110,770                 |   | 2.543       | 533,012                   | 12.236         |
|                             | 7.40       |                              | 442.5       | 251.6      | 111,325                 |   | 2.556       | 544,116                   | 12.491         |
|                             | 7.50       |                              | 443.3       | 252.4      | 111,881                 |   | 2.568       | 555,277                   | 12.747         |
|                             | 7.60       |                              | 444.1       | 253.2      | 112,438                 |   | 2.581       | 566,493                   | 13.005         |
|                             | 7.70       |                              | 444.9       | 254.0      | 112,997                 |   | 2.594       | 577,764                   | 13.264         |
|                             | 7.80       |                              | 445.7       | 254.8      | 113,556                 |   | 2.607       | 589,092                   | 13.524         |
|                             | 7.90       |                              | 446.5       | 255.6      | 114,117                 |   | 2.620       | 600,476                   | 13.785         |
|                             | 8.00       |                              | 447.3       | 256.4      | 114,680                 |   | 2.633       | 611,915                   | 14.048         |
|                             | 8.10       |                              | 448.1       | 257.2      | 115,243                 |   | 2.646       | 623,411                   | 14.312         |
|                             | 8.20       |                              | 448.9       | 258.0      | 115,808                 |   | 2.659       | 634,964                   | 14.577         |
|                             | 8.30       |                              | 449.7       | 258.8      | 116,374                 |   | 2.672       | 646,573                   | 14.843         |
|                             | 8.40       |                              | 450.5       | 259.6      | 116,942                 |   | 2.685       | 658,239                   | 15.111         |
|                             | 8.50       |                              | 451.3       | 260.4      | 117,510                 |   | 2.698       | 669,962                   | 15.380         |
|                             | 8.60       |                              | 452.1       | 261.2      | 118,080                 |   | 2.711       | 681,741                   | 15.651         |
|                             | 8.70       |                              | 452.9       | 262.0      | 118,652                 |   | 2.724       | 693,578                   | 15.922         |
|                             | 8.80       |                              | 453.7       | 262.8      | 119,224                 |   | 2.737       | 705,471                   | 16.195         |
|                             | 8.90       |                              | 454.5       | 263.6      | 119,798                 |   | 2.750       | 717,422                   | 16.470         |
|                             | 9.00       |                              | 455.3       | 264.4      | 120,373                 |   | 2.763       | 729,431                   | 16.745         |
|                             | 9.10       |                              | 456.1       | 265.2      | 120,949                 |   | 2.777       | 741,497                   | 17.022         |
|                             | 9.20       |                              | 456.9       | 266.0      | 121,527                 |   | 2.790       | 753,621                   | 17.301         |
|                             | 9.30       |                              | 457.7       | 266.8      | 122,106                 |   | 2.803       | 765,803                   | 17.580         |
|                             | 9.40       |                              | 458.5       | 267.6      | 122,686                 |   | 2.816       | 778,042                   | 17.861         |
|                             | 9.50       |                              | 459.3       | 268.4      | 123,268                 |   | 2.830       | 790,340                   | 18.144         |
|                             | 9.60       |                              | 460.1       | 269.2      | 123,851                 |   | 2.843       | 802,696                   | 18.427         |

# DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.04 (February 2021)

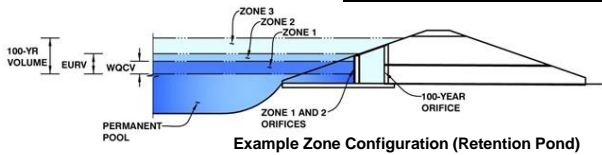


# DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.04 (February 2021)

Project: Flying Horse North Master Drainage Plan

Basin ID: Pond 7



Example Zone Configuration (Retention Pond)

|                   | Estimated Stage (ft) | Estimated Volume (ac-ft) | Outlet Type          |
|-------------------|----------------------|--------------------------|----------------------|
| Zone 1 (WQCV)     | 2.63                 | 1.689                    | Orifice Plate        |
| Zone 2 (EURV)     | 4.07                 | 2.974                    | Weir&Pipe (Circular) |
| Zone 3 (100-year) | 5.99                 | 4.329                    | Weir&Pipe (Restrict) |
| Total (all zones) |                      | 8.992                    |                      |

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth =  ft (distance below the filtration media surface)  
Underdrain Orifice Diameter =  inches

Calculated Parameters for Underdrain  
Underdrain Orifice Area =  ft<sup>2</sup>  
Underdrain Orifice Centroid =  feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice =  ft (relative to basin bottom at Stage = 0 ft)  
Depth at top of Zone using Orifice Plate =  ft (relative to basin bottom at Stage = 0 ft)  
Orifice Plate: Orifice Vertical Spacing =  inches  
Orifice Plate: Orifice Area per Row =  sq. inches (use rectangular openings)

Calculated Parameters for Plate  
WQ Orifice Area per Row =  ft<sup>2</sup>  
Elliptical Half-Width =  feet  
Elliptical Slot Centroid =  feet  
Elliptical Slot Area =  ft<sup>2</sup>

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

|                                | Row 1 (required) | Row 2 (optional) | Row 3 (optional) | Row 4 (optional) | Row 5 (optional) | Row 6 (optional) | Row 7 (optional) | Row 8 (optional) |
|--------------------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|
| Stage of Orifice Centroid (ft) | 0.00             | 0.88             | 1.77             |                  |                  |                  |                  |                  |
| Orifice Area (sq. inches)      | 5.17             | 5.17             | 5.17             |                  |                  |                  |                  |                  |

|                                | Row 9 (optional) | Row 10 (optional) | Row 11 (optional) | Row 12 (optional) | Row 13 (optional) | Row 14 (optional) | Row 15 (optional) | Row 16 (optional) |
|--------------------------------|------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| Stage of Orifice Centroid (ft) |                  |                   |                   |                   |                   |                   |                   |                   |
| Orifice Area (sq. inches)      |                  |                   |                   |                   |                   |                   |                   |                   |

User Input: Vertical Orifice (Circular or Rectangular)

Invert of Vertical Orifice =  ft (relative to basin bottom at Stage = 0 ft)  
Depth at top of Zone using Vertical Orifice =  ft (relative to basin bottom at Stage = 0 ft)  
Vertical Orifice Diameter =  inches

Calculated Parameters for Vertical Orifice  
Vertical Orifice Area =  ft<sup>2</sup>  
Vertical Orifice Centroid =  feet

User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe))

Overflow Weir Front Edge Height, H<sub>o</sub> =  ft (relative to basin bottom at Stage = 0 ft)  
Overflow Weir Front Edge Length =  feet  
Overflow Weir Grate Slope =  H:V  
Horiz. Length of Weir Sides =  feet  
Overflow Grate Type =   
Debris Clogging % =  %

Calculated Parameters for Overflow Weir  
Height of Grate Upper Edge, H<sub>u</sub> =  feet  
Overflow Weir Slope Length =  feet  
Grate Open Area / 100-yr Orifice Area =   
Overflow Grate Open Area w/o Debris =  ft<sup>2</sup>  
Overflow Grate Open Area w/ Debris =  ft<sup>2</sup>

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

Depth to Invert of Outlet Pipe =  ft (distance below basin bottom at Stage = 0 ft)  
Circular Orifice Diameter or Pipe Diameter =  inches  
Restrictor Plate Height Above Pipe Invert =  inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate  
Outlet Orifice Area =  ft<sup>2</sup>  
Outlet Orifice Centroid =  feet  
Half-Central Angle of Restrictor Plate on Pipe =  radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage =  ft (relative to basin bottom at Stage = 0 ft)  
Spillway Crest Length =  feet  
Spillway End Slopes =  H:V  
Freeboard above Max Water Surface =  feet

Calculated Parameters for Spillway  
Spillway Design Flow Depth =  feet  
Stage at Top of Freeboard =  feet  
Basin Area at Top of Freeboard =  acres  
Basin Volume at Top of Freeboard =  acre-ft

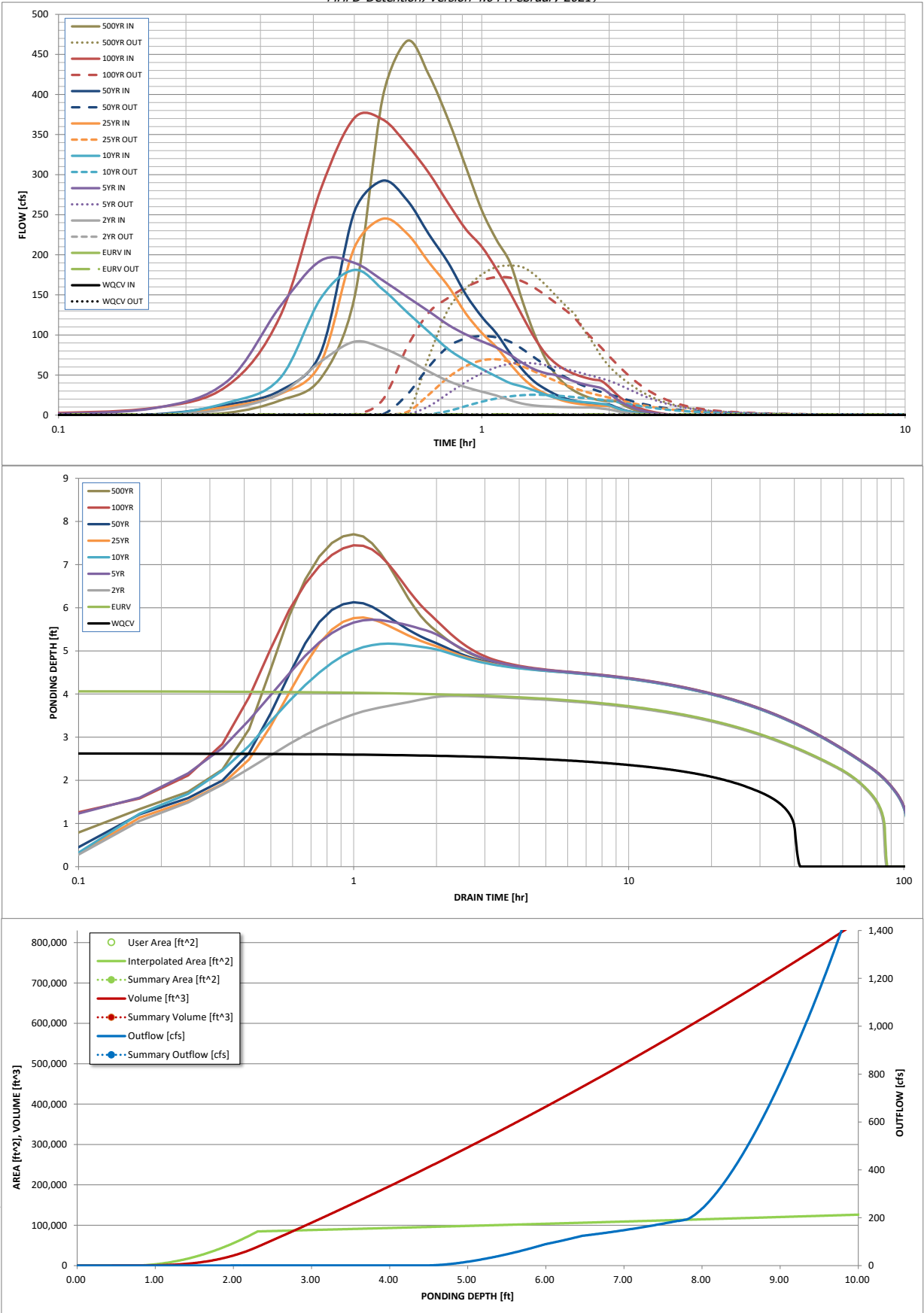
## Routed Hydrograph Results

The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).

|  | WQCV  | EURV  | 2 Year | 5 Year          | 10 Year         | 25 Year         | 50 Year         | 100 Year        | 500 Year        |
|--|-------|-------|--------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|
| Design Storm Return Period =                       | N/A   | N/A   | 1.19   | 1.50            | 1.75            | 2.00            | 2.25            | 2.52            | 3.14            |
| One-Hour Rainfall Depth (in) =                     | N/A   | N/A   | 1.19   | 1.50            | 1.75            | 2.00            | 2.25            | 2.52            | 3.14            |
| CUHP Runoff Volume (acre-ft) =                     | 1.689 | 4.663 | 4.575  | 6.891           | 8.978           | 11.989          | 14.328          | 17.379          | 23.422          |
| User Override Inflow Hydrograph Volume (acre-ft) = | N/A   | N/A   | 4.575  | 13.698          | 8.978           | 11.989          | 14.328          | 24.727          | 23.422          |
| CUHP Predevelopment Peak Q (cfs) =                 | N/A   | N/A   | 19.1   | 53.5            | 79.8            | 138.4           | 173.6           | 217.5           | 301.7           |
| OPTIONAL Override Predevelopment Peak Q (cfs) =    | N/A   | N/A   |        | 65.3            |                 |                 |                 | 191.6           |                 |
| Predevelopment Unit Peak Flow, q (cfs/acre) =      | N/A   | N/A   | 0.17   | 0.57            | 0.70            | 1.21            | 1.51            | 1.67            | 2.63            |
| Peak Inflow Q (cfs) =                              | N/A   | N/A   | 91.6   | 192.8           | 181.1           | 244.9           | 292.5           | 370.7           | 466.9           |
| Peak Outflow Q (cfs) =                             | 0.7   | 0.9   | 0.9    | 65.4            | 25.4            | 69.6            | 98.6            | 172.2           | 186.6           |
| Ratio Peak Outflow to Predevelopment Q =           | N/A   | N/A   | N/A    | 1.0             | 0.3             | 0.5             | 0.6             | 0.9             | 0.6             |
| Structure Controlling Flow =                       | Plate | Plate | Plate  | Overflow Weir 2 | Overflow Weir 2 | Overflow Weir 2 | Overflow Weir 2 | Overflow Weir 2 | Overflow Weir 2 |
| Max Velocity through Grate 1 (fps) =               | N/A   | N/A   | N/A    | 2.1             | 0.8             | 2.2             | 3.0             | 3.9             | 4.0             |
| Max Velocity through Grate 2 (fps) =               | N/A   | N/A   | N/A    | 0.1             | 0.0             | 0.1             | 0.2             | 0.9             | 1.0             |
| Time to Drain 97% of Inflow Volume (hours) =       | 38    | 80    | 80     | 90              | 94              | 91              | 89              | 82              | 83              |
| Time to Drain 99% of Inflow Volume (hours) =       | 40    | 84    | 83     | 99              | 100             | 99              | 98              | 95              | 95              |
| Maximum Ponding Depth (ft) =                       | 2.63  | 4.07  | 3.95   | 5.73            | 5.17            | 5.77            | 6.13            | 7.45            | 7.70            |
| Area at Maximum Ponding Depth (acres) =            | 1.98  | 2.15  | 2.13   | 2.35            | 2.28            | 2.35            | 2.39            | 2.56            | 2.59            |
| Maximum Volume Stored (acre-ft) =                  | 1.698 | 4.669 | 4.413  | 8.375           | 7.081           | 8.493           | 9.323           | 12.594          | 13.264          |

DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.04 (February 2021)



| S-A-V-D Chart Axis Override | X-axis | Left Y-Axis | Right Y-Axis |
|-----------------------------|--------|-------------|--------------|
| minimum bound               |        |             |              |
| maximum bound               |        |             |              |

# DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename: ...[SWMM]Outflow hydrographs\Pond6 OutflowHydrograph.xlsx

## Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

|               | SOURCE  | CUHP       | CUHP       | CUHP         | USER         | CUHP          | CUHP          | CUHP          | USER           | CUHP           |
|---------------|---------|------------|------------|--------------|--------------|---------------|---------------|---------------|----------------|----------------|
| Time Interval | TIME    | WQCV [cfs] | EURV [cfs] | 2 Year [cfs] | 5 Year [cfs] | 10 Year [cfs] | 25 Year [cfs] | 50 Year [cfs] | 100 Year [cfs] | 500 Year [cfs] |
| 5.00 min      | 0:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 0:05:00 | 0.00       | 0.00       | 0.00         | 0.35         | 0.00          | 0.00          | 0.00          | 1.15           | 0.00           |
|               | 0:10:00 | 0.00       | 0.00       | 0.00         | 8.35         | 0.00          | 0.00          | 0.87          | 8.80           | 2.79           |
|               | 0:15:00 | 0.00       | 0.00       | 7.53         | 41.96        | 15.37         | 10.35         | 12.91         | 36.23          | 18.14          |
|               | 0:20:00 | 0.00       | 0.00       | 26.66        | 135.18       | 45.76         | 26.13         | 30.39         | 122.53         | 46.04          |
|               | 0:25:00 | 0.00       | 0.00       | 66.84        | 192.81       | 145.94        | 65.52         | 78.49         | 282.20         | 146.25         |
|               | 0:30:00 | 0.00       | 0.00       | 91.59        | 189.89       | 181.09        | 208.88        | 253.77        | 370.69         | 396.24         |
|               | 0:35:00 | 0.00       | 0.00       | 83.49        | 168.08       | 156.84        | 244.93        | 292.46        | 368.77         | 466.90         |
|               | 0:40:00 | 0.00       | 0.00       | 69.51        | 147.36       | 128.13        | 226.22        | 267.84        | 337.06         | 424.31         |
|               | 0:45:00 | 0.00       | 0.00       | 54.32        | 129.31       | 103.79        | 190.55        | 225.54        | 301.99         | 368.42         |
|               | 0:50:00 | 0.00       | 0.00       | 42.53        | 112.57       | 82.17         | 160.69        | 189.97        | 264.23         | 309.75         |
|               | 0:55:00 | 0.00       | 0.00       | 34.81        | 100.65       | 68.10         | 126.75        | 150.57        | 231.91         | 255.54         |
|               | 1:00:00 | 0.00       | 0.00       | 29.24        | 91.99        | 57.54         | 102.55        | 122.63        | 210.05         | 218.61         |
|               | 1:05:00 | 0.00       | 0.00       | 24.37        | 84.30        | 48.10         | 84.65         | 101.75        | 182.04         | 189.95         |
|               | 1:10:00 | 0.00       | 0.00       | 18.53        | 75.10        | 39.94         | 63.92         | 77.12         | 152.54         | 140.96         |
|               | 1:15:00 | 0.00       | 0.00       | 14.20        | 64.91        | 35.46         | 46.28         | 56.24         | 122.62         | 100.15         |
|               | 1:20:00 | 0.00       | 0.00       | 11.95        | 56.89        | 30.57         | 33.94         | 41.44         | 96.04          | 69.57          |
|               | 1:25:00 | 0.00       | 0.00       | 10.84        | 52.28        | 25.28         | 26.43         | 32.25         | 76.32          | 49.57          |
|               | 1:30:00 | 0.00       | 0.00       | 10.26        | 49.65        | 21.53         | 20.77         | 25.24         | 63.82          | 37.19          |
|               | 1:35:00 | 0.00       | 0.00       | 9.94         | 45.63        | 19.01         | 16.94         | 20.45         | 55.99          | 29.25          |
|               | 1:40:00 | 0.00       | 0.00       | 9.68         | 41.44        | 17.27         | 14.62         | 17.52         | 50.64          | 23.93          |
|               | 1:45:00 | 0.00       | 0.00       | 9.50         | 38.27        | 16.09         | 13.10         | 15.56         | 46.97          | 20.37          |
|               | 1:50:00 | 0.00       | 0.00       | 9.40         | 35.96        | 15.24         | 12.09         | 14.28         | 44.36          | 18.18          |
|               | 1:55:00 | 0.00       | 0.00       | 8.11         | 33.53        | 13.98         | 11.56         | 13.59         | 42.55          | 17.39          |
|               | 2:00:00 | 0.00       | 0.00       | 7.01         | 27.14        | 12.28         | 11.24         | 13.17         | 34.89          | 17.03          |
|               | 2:05:00 | 0.00       | 0.00       | 5.02         | 19.98        | 8.67          | 8.06          | 9.43          | 25.68          | 12.26          |
|               | 2:10:00 | 0.00       | 0.00       | 3.38         | 14.45        | 5.83          | 5.40          | 6.30          | 18.63          | 8.24           |
|               | 2:15:00 | 0.00       | 0.00       | 2.27         | 10.39        | 3.91          | 3.64          | 4.25          | 13.59          | 5.54           |
|               | 2:20:00 | 0.00       | 0.00       | 1.48         | 7.28         | 2.54          | 2.37          | 2.76          | 9.71           | 3.59           |
|               | 2:25:00 | 0.00       | 0.00       | 0.92         | 5.00         | 1.60          | 1.52          | 1.76          | 6.81           | 2.28           |
|               | 2:30:00 | 0.00       | 0.00       | 0.53         | 3.43         | 0.95          | 0.94          | 1.09          | 4.77           | 1.39           |
|               | 2:35:00 | 0.00       | 0.00       | 0.26         | 2.28         | 0.48          | 0.50          | 0.57          | 3.20           | 0.72           |
|               | 2:40:00 | 0.00       | 0.00       | 0.10         | 1.39         | 0.18          | 0.20          | 0.22          | 1.96           | 0.26           |
|               | 2:45:00 | 0.00       | 0.00       | 0.02         | 0.74         | 0.03          | 0.03          | 0.03          | 1.04           | 0.02           |
|               | 2:50:00 | 0.00       | 0.00       | 0.00         | 0.32         | 0.00          | 0.00          | 0.00          | 0.45           | 0.00           |
|               | 2:55:00 | 0.00       | 0.00       | 0.00         | 0.11         | 0.00          | 0.00          | 0.00          | 0.15           | 0.00           |
|               | 3:00:00 | 0.00       | 0.00       | 0.00         | 0.02         | 0.00          | 0.00          | 0.00          | 0.03           | 0.00           |
|               | 3:05:00 | 0.00       | 0.00       | 0.00         | 0.01         | 0.00          | 0.00          | 0.00          | 0.01           | 0.00           |
|               | 3:10:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:15:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:20:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:25:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:30:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:35:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:40:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:45:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:50:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:55:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:05:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:10:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:15:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:20:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:25:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:30:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:35:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:40:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:45:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:50:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:55:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:05:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:10:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:15:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:20:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:25:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:30:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:35:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:40:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:45:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:50:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:55:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 6:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |

## DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.04 (February 2021)

### Summary Stage-Area-Volume-Discharge Relationships

The user can create a summary S-A-V-D by entering the desired stage increments and the remainder of the table will populate automatically.

The user should graphically compare the summary S-A-V-D table to the full S-A-V-D table in the chart to confirm it captures all key transition points.

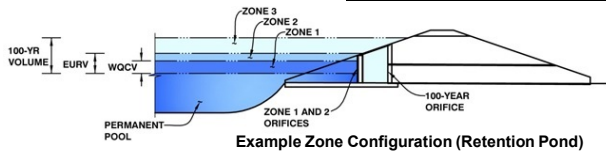
[illegible]

# DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-DETENTION, Version 4.04 (February 2021)

Project: Flying Horse North MDDP

Basin ID: Pond 8



|                   | Estimated Stage (ft) | Estimated Volume (ac-ft) | Outlet Type          |
|-------------------|----------------------|--------------------------|----------------------|
| Zone 1 (WQCV)     | 2.39                 | 0.178                    | Orifice Plate        |
| Zone 2 (EURV)     | 3.67                 | 0.221                    | Circular Orifice     |
| Zone 3 (100-year) | 5.97                 | 0.543                    | Weir&Pipe (Restrict) |
| Total (all zones) |                      | 0.942                    |                      |

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth =  ft (distance below the filtration media surface)  
Underdrain Orifice Diameter =  inches

Calculated Parameters for Underdrain  
Underdrain Orifice Area =  ft<sup>2</sup>  
Underdrain Orifice Centroid =  feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice =  ft (relative to basin bottom at Stage = 0 ft)  
Depth at top of Zone using Orifice Plate =  ft (relative to basin bottom at Stage = 0 ft)  
Orifice Plate: Orifice Vertical Spacing =  inches  
Orifice Plate: Orifice Area per Row =  sq. inches (diameter = 7/8 inch)

Calculated Parameters for Plate  
WQ Orifice Area per Row =  ft<sup>2</sup>  
Elliptical Half-Width =  feet  
Elliptical Slot Centroid =  feet  
Elliptical Slot Area =  ft<sup>2</sup>

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

|                                | Row 1 (required) | Row 2 (optional) | Row 3 (optional) | Row 4 (optional) | Row 5 (optional) | Row 6 (optional) | Row 7 (optional) | Row 8 (optional) |
|--------------------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|
| Stage of Orifice Centroid (ft) | 0.00             | 0.80             | 1.59             |                  |                  |                  |                  |                  |
| Orifice Area (sq. inches)      | 0.65             | 0.65             | 0.65             |                  |                  |                  |                  |                  |

|                                | Row 9 (optional) | Row 10 (optional) | Row 11 (optional) | Row 12 (optional) | Row 13 (optional) | Row 14 (optional) | Row 15 (optional) | Row 16 (optional) |
|--------------------------------|------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| Stage of Orifice Centroid (ft) |                  |                   |                   |                   |                   |                   |                   |                   |
| Orifice Area (sq. inches)      |                  |                   |                   |                   |                   |                   |                   |                   |

User Input: Vertical Orifice (Circular or Rectangular)

Invert of Vertical Orifice =  ft (relative to basin bottom at Stage = 0 ft)  
Depth at top of Zone using Vertical Orifice =  ft (relative to basin bottom at Stage = 0 ft)  
Vertical Orifice Diameter =  inches

Calculated Parameters for Vertical Orif  
Zone 2 Circular Not Selected  
Vertical Orifice Area =  ft<sup>2</sup>  
Vertical Orifice Centroid =  feet

User Input: Overflow Weir (Dropbox with Flat or Sloped Gate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe)

Overflow Weir Front Edge Height, H<sub>o</sub> =  ft (relative to basin bottom at Stage = 0 ft)  
Overflow Weir Front Edge Length =  feet  
Overflow Weir Gate Slope =  H:V  
Horiz. Length of Weir Sides =  feet  
Overflow Gate Type =   
Debris Clogging % =  %

Calculated Parameters for Overflow W  
Zone 3 Weir Not Selected  
Height of Gate Upper Edge, H<sub>u</sub> =  ft  
Overflow Weir Slope Length =  feet  
Gate Open Area / 100-yr Orifice Area =  ft<sup>2</sup>  
Overflow Gate Open Area w/o Debris =  ft<sup>2</sup>  
Overflow Gate Open Area w/ Debris =  ft<sup>2</sup>

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

Depth to Invert of Outlet Pipe =  ft (distance below basin bottom at Stage = 0 ft)  
Outlet Pipe Diameter =  inches  
Restrictor Plate Height Above Pipe Invert =  inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Pl  
Zone 3 Restrictor Not Selected  
Outlet Orifice Area =  ft<sup>2</sup>  
Outlet Orifice Centroid =  feet  
Half-Central Angle of Restrictor Plate on Pipe =  degrees

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage =  ft (relative to basin bottom at Stage = 0 ft)  
Spillway Crest Length =  feet  
Spillway End Slopes =  H:V  
Freeboard above Max Water Surface =  feet

Calculated Parameters for Spillway  
Spillway Design Flow Depth =  feet  
Stage at Top of Freeboard =  feet  
Basin Area at Top of Freeboard =  acres  
Basin Volume at Top of Freeboard =  acre-ft

## Routed Hydrograph Results

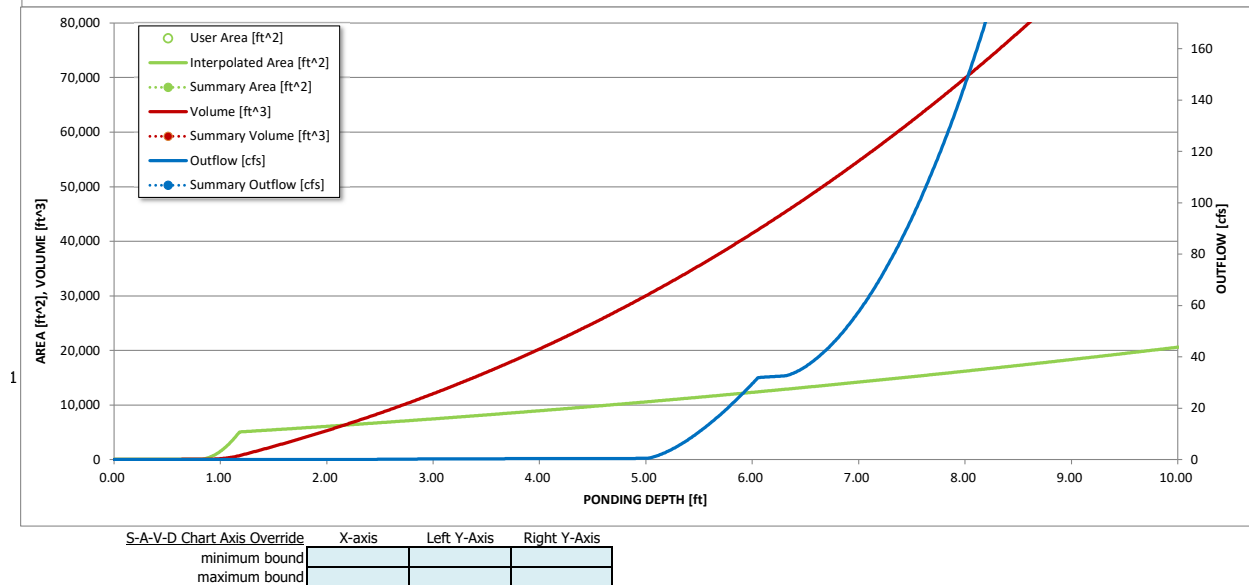
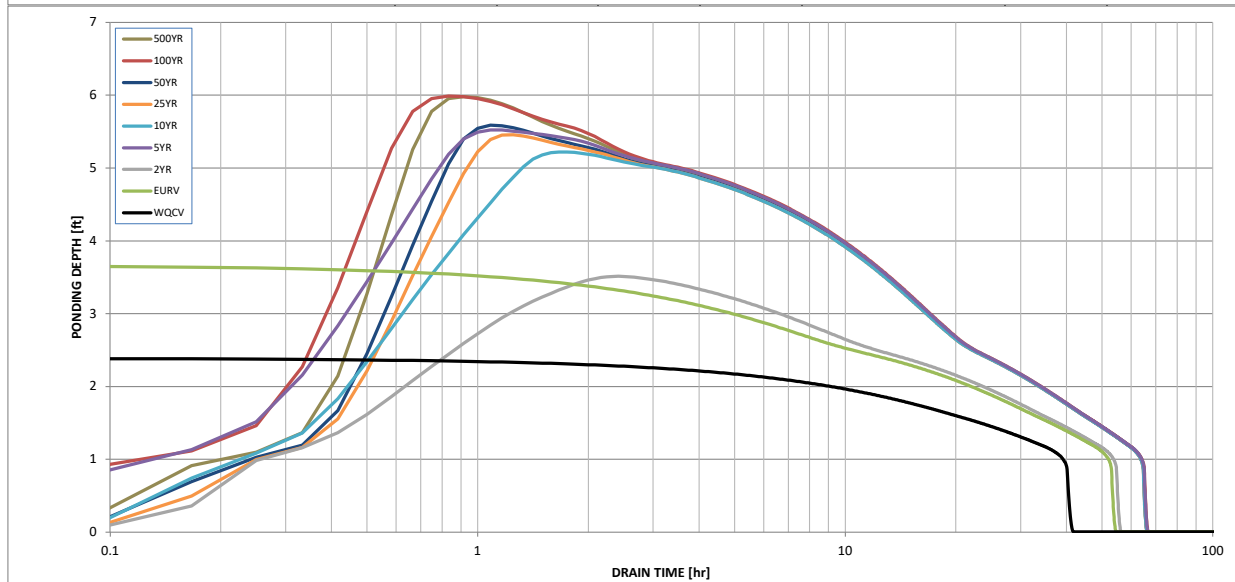
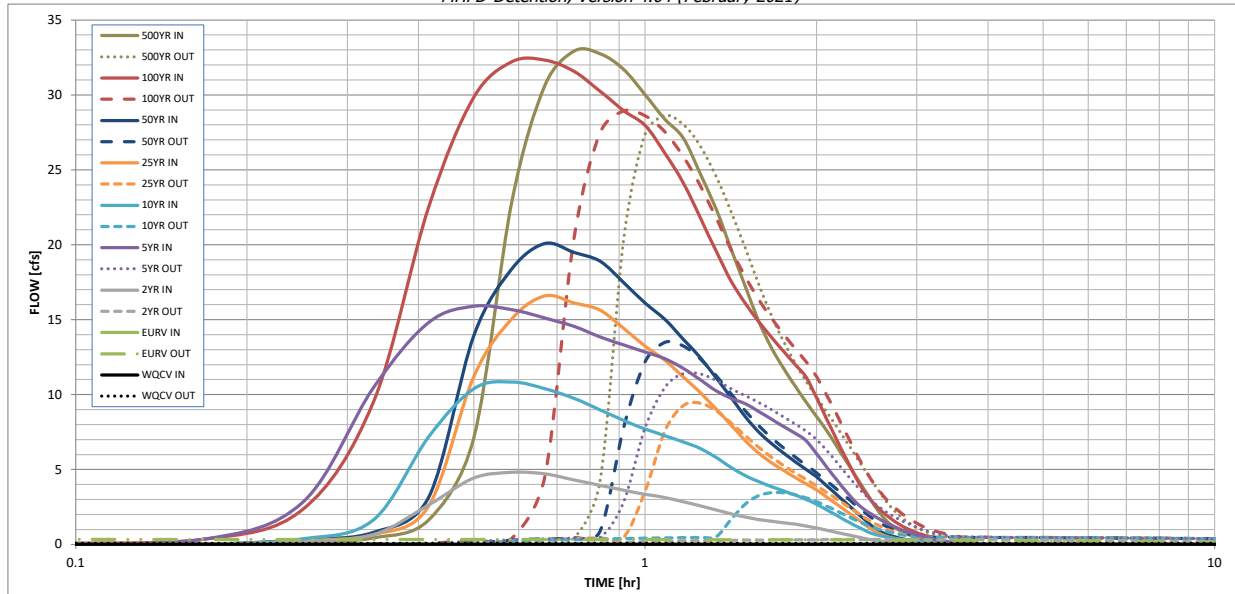
The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through A)

|  | WQCV  | EURV               | 2 Year             | 5 Year          | 10 Year         | 25 Year         | 50 Year         | 100 Year        |
|--|-------|--------------------|--------------------|-----------------|-----------------|-----------------|-----------------|-----------------|
| Design Storm Return Period =                       | N/A   | N/A                | 1.19               | 1.50            | 1.75            | 2.00            | 2.25            | 2.52            |
| One-Hour Rainfall Depth (in) =                     | N/A   | N/A                | 0.416              | 0.713           | 0.991           | 1.426           | 1.746           | 2.181           |
| CUHP Runoff Volume (acre-ft) =                     | N/A   | N/A                | 0.416              | 1.850           | 0.991           | 1.426           | 1.746           | 3.383           |
| User Override Inflow Hydrograph Volume (acre-ft) = | N/A   | N/A                | 1.6                | 4.6             | 6.9             | 12.4            | 15.5            | 19.9            |
| CUHP Predevelopment Peak Q (cfs) =                 | N/A   | N/A                | N/A                | 11.1            | N/A             | N/A             | N/A             | 32.7            |
| OPTIONAL Override Predevelopment Peak Q (cfs) =    | N/A   | N/A                | 0.10               | 0.70            | 0.44            | 0.78            | 0.98            | 2.06            |
| Predevelopment Unit Peak Flow, q (cfs/acre) =      | N/A   | N/A                | 4.8                | 15.9            | 10.8            | 16.6            | 20.1            | 32.3            |
| Peak Inflow Q (cfs) =                              | 0.1   | 0.3                | 0.3                | 11.4            | 3.5             | 9.4             | 13.5            | 28.9            |
| Peak Outflow Q (cfs) =                             | N/A   | N/A                | N/A                | 1.0             | 0.5             | 0.8             | 0.9             | 0.9             |
| Ratio Peak Outflow to Predevelopment Q =           | Plate | Vertical Orifice 1 | Vertical Orifice 1 | Overflow Weir 1 | Overflow Weir 1 | Overflow Weir 1 | Overflow Weir 1 | Overflow Weir 1 |
| Structure Controlling Flow =                       | N/A   | N/A                | N/A                | 0.8             | 0.2             | 0.6             | 0.9             | 2.1             |
| Max Velocity through Gate 1 (fps) =                | N/A   | N/A                | N/A                | N/A             | N/A             | N/A             | N/A             | N/A             |
| Max Velocity through Gate 2 (fps) =                | 39    | 49                 | 51                 | 48              | 55              | 51              | 49              | 38              |
| Time to Drain 97% of Inflow Volume (hours) =       | 40    | 52                 | 54                 | 59              | 62              | 60              | 59              | 54              |
| Time to Drain 99% of Inflow Volume (hours) =       | 2.39  | 3.67               | 3.51               | 5.52            | 5.22            | 5.46            | 5.58            | 5.99            |
| Maximum Ponding Depth (ft) =                       | 0.15  | 0.19               | 0.19               | 0.26            | 0.25            | 0.26            | 0.27            | 0.28            |
| Area at Maximum Ponding Depth (acres) =            | 0.179 | 0.399              | 0.369              | 0.821           | 0.741           | 0.802           | 0.837           | 0.946           |
| Maximum Volume Stored (acre-ft) =                  |       |                    |                    |                 |                 |                 |                 |                 |



# DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.04 (February 2021)



# DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename: \_\_\_\_\_

## Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

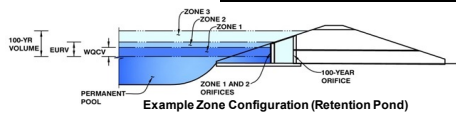
|               | SOURCE  | CUHP       | CUHP       | CUHP         | USER         | CUHP          | CUHP          | CUHP          | USER           | CUHP           |
|---------------|---------|------------|------------|--------------|--------------|---------------|---------------|---------------|----------------|----------------|
| Time Interval | TIME    | WQCV [cfs] | EURV [cfs] | 2 Year [cfs] | 5 Year [cfs] | 10 Year [cfs] | 25 Year [cfs] | 50 Year [cfs] | 100 Year [cfs] | 500 Year [cfs] |
| 5.00 min      | 0:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 0:05:00 | 0.00       | 0.00       | 0.00         | 0.02         | 0.00          | 0.00          | 0.00          | 0.06           | 0.00           |
|               | 0:10:00 | 0.00       | 0.00       | 0.00         | 0.34         | 0.00          | 0.00          | 0.02          | 0.34           | 0.07           |
|               | 0:15:00 | 0.00       | 0.00       | 0.18         | 2.78         | 0.37          | 0.25          | 0.31          | 2.31           | 0.44           |
|               | 0:20:00 | 0.00       | 0.00       | 0.66         | 10.46        | 1.64          | 0.65          | 0.80          | 9.50           | 1.64           |
|               | 0:25:00 | 0.00       | 0.00       | 2.63         | 14.81        | 7.18          | 2.58          | 3.15          | 22.52          | 7.13           |
|               | 0:30:00 | 0.00       | 0.00       | 4.43         | 15.89        | 10.39         | 11.21         | 13.94         | 29.84          | 22.90          |
|               | 0:35:00 | 0.00       | 0.00       | 4.81         | 15.66        | 10.85         | 15.07         | 18.39         | 32.21          | 30.64          |
|               | 0:40:00 | 0.00       | 0.00       | 4.71         | 15.11        | 10.40         | 16.58         | 20.07         | 32.32          | 32.92          |
|               | 0:45:00 | 0.00       | 0.00       | 4.31         | 14.56        | 9.75          | 16.12         | 19.49         | 31.57          | 32.76          |
|               | 0:50:00 | 0.00       | 0.00       | 3.95         | 13.85        | 8.98          | 15.64         | 18.90         | 30.25          | 31.70          |
|               | 0:55:00 | 0.00       | 0.00       | 3.62         | 13.31        | 8.27          | 14.42         | 17.48         | 28.95          | 30.01          |
|               | 1:00:00 | 0.00       | 0.00       | 3.35         | 12.85        | 7.71          | 13.24         | 16.11         | 27.97          | 28.37          |
|               | 1:05:00 | 0.00       | 0.00       | 3.13         | 12.39        | 7.26          | 12.28         | 15.01         | 26.11          | 27.13          |
|               | 1:10:00 | 0.00       | 0.00       | 2.85         | 11.75        | 6.83          | 11.17         | 13.71         | 24.14          | 24.72          |
|               | 1:15:00 | 0.00       | 0.00       | 2.57         | 10.98        | 6.41          | 10.13         | 12.46         | 21.80          | 22.36          |
|               | 1:20:00 | 0.00       | 0.00       | 2.30         | 10.25        | 5.80          | 9.02          | 11.10         | 19.55          | 19.70          |
|               | 1:25:00 | 0.00       | 0.00       | 2.04         | 9.75         | 5.13          | 7.96          | 9.80          | 17.56          | 17.19          |
|               | 1:30:00 | 0.00       | 0.00       | 1.82         | 9.39         | 4.59          | 6.91          | 8.50          | 16.06          | 14.90          |
|               | 1:35:00 | 0.00       | 0.00       | 1.66         | 8.88         | 4.19          | 6.09          | 7.51          | 14.87          | 13.13          |
|               | 1:40:00 | 0.00       | 0.00       | 1.55         | 8.36         | 3.86          | 5.46          | 6.74          | 13.83          | 11.76          |
|               | 1:45:00 | 0.00       | 0.00       | 1.45         | 7.87         | 3.57          | 4.94          | 6.10          | 12.89          | 10.57          |
|               | 1:50:00 | 0.00       | 0.00       | 1.35         | 7.42         | 3.30          | 4.47          | 5.53          | 12.01          | 9.51           |
|               | 1:55:00 | 0.00       | 0.00       | 1.22         | 6.93         | 3.01          | 4.05          | 5.01          | 11.18          | 8.53           |
|               | 2:00:00 | 0.00       | 0.00       | 1.10         | 6.06         | 2.68          | 3.65          | 4.51          | 9.79           | 7.61           |
|               | 2:05:00 | 0.00       | 0.00       | 0.95         | 5.17         | 2.31          | 3.17          | 3.91          | 8.39           | 6.58           |
|               | 2:10:00 | 0.00       | 0.00       | 0.81         | 4.34         | 1.94          | 2.70          | 3.34          | 7.04           | 5.61           |
|               | 2:15:00 | 0.00       | 0.00       | 0.67         | 3.57         | 1.60          | 2.25          | 2.78          | 5.79           | 4.67           |
|               | 2:20:00 | 0.00       | 0.00       | 0.53         | 2.90         | 1.28          | 1.82          | 2.25          | 4.63           | 3.76           |
|               | 2:25:00 | 0.00       | 0.00       | 0.41         | 2.39         | 0.98          | 1.40          | 1.73          | 3.63           | 2.89           |
|               | 2:30:00 | 0.00       | 0.00       | 0.30         | 2.01         | 0.74          | 1.01          | 1.25          | 2.90           | 2.09           |
|               | 2:35:00 | 0.00       | 0.00       | 0.22         | 1.68         | 0.59          | 0.70          | 0.88          | 2.34           | 1.50           |
|               | 2:40:00 | 0.00       | 0.00       | 0.18         | 1.40         | 0.48          | 0.51          | 0.65          | 1.89           | 1.11           |
|               | 2:45:00 | 0.00       | 0.00       | 0.15         | 1.16         | 0.39          | 0.38          | 0.49          | 1.51           | 0.82           |
|               | 2:50:00 | 0.00       | 0.00       | 0.12         | 0.96         | 0.32          | 0.29          | 0.37          | 1.21           | 0.60           |
|               | 2:55:00 | 0.00       | 0.00       | 0.10         | 0.78         | 0.26          | 0.22          | 0.29          | 0.97           | 0.44           |
|               | 3:00:00 | 0.00       | 0.00       | 0.08         | 0.64         | 0.21          | 0.17          | 0.22          | 0.78           | 0.32           |
|               | 3:05:00 | 0.00       | 0.00       | 0.07         | 0.52         | 0.16          | 0.13          | 0.17          | 0.64           | 0.23           |
|               | 3:10:00 | 0.00       | 0.00       | 0.05         | 0.42         | 0.13          | 0.10          | 0.13          | 0.52           | 0.17           |
|               | 3:15:00 | 0.00       | 0.00       | 0.04         | 0.32         | 0.10          | 0.08          | 0.10          | 0.42           | 0.14           |
|               | 3:20:00 | 0.00       | 0.00       | 0.03         | 0.25         | 0.08          | 0.06          | 0.08          | 0.32           | 0.11           |
|               | 3:25:00 | 0.00       | 0.00       | 0.03         | 0.18         | 0.06          | 0.05          | 0.06          | 0.24           | 0.09           |
|               | 3:30:00 | 0.00       | 0.00       | 0.02         | 0.13         | 0.04          | 0.04          | 0.05          | 0.18           | 0.06           |
|               | 3:35:00 | 0.00       | 0.00       | 0.01         | 0.08         | 0.03          | 0.03          | 0.04          | 0.12           | 0.05           |
|               | 3:40:00 | 0.00       | 0.00       | 0.01         | 0.05         | 0.02          | 0.02          | 0.02          | 0.07           | 0.03           |
|               | 3:45:00 | 0.00       | 0.00       | 0.01         | 0.03         | 0.01          | 0.01          | 0.02          | 0.04           | 0.02           |
|               | 3:50:00 | 0.00       | 0.00       | 0.00         | 0.01         | 0.01          | 0.01          | 0.01          | 0.01           | 0.01           |
|               | 3:55:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:05:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:10:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:15:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:20:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:25:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:30:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:35:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:40:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:45:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:50:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:55:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:05:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:10:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:15:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:20:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:25:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:30:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:35:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:40:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:45:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:50:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:55:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 6:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |

# DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-DETENTION, Version 4.04 (February 2021)

Project: Flying Horse North MDDP

Basin ID: Pond 8



Example Zone Configuration (Retention Pond)

## Watershed Information

|   |                |
|---|----------------|
| Selected BMP Type =                     | EDB            |
| Watershed Area =                        | 15.89 acres    |
| Watershed Length =                      | 1,507 ft       |
| Watershed Length to Centroid =          | 741 ft         |
| Watershed Slope =                       | 0.040 ft/ft    |
| Watershed Imperviousness =              | 24.82% percent |
| Percentage Hydrologic Soil Group A =    | 0.0% percent   |
| Percentage Hydrologic Soil Group B =    | 100.0% percent |
| Percentage Hydrologic Soil Groups C/D = | 0.0% percent   |
| Target WQCV Drain Time =                | 40.0 hours     |
| Location for 1-hr Rainfall Depths =     | User Input     |

After providing required inputs above including 1-hour rainfall depths, click "Run CUHP" to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

## Optional User Overrides

|  |                 |      |        |
|--|-----------------|------|--------|
| Water Quality Capture Volume (WQCV) =  | 0.178 acre-feet |      |        |
| Excess Urban Runoff Volume (EURV) =    | 0.399 acre-feet |      |        |
| 2-yr Runoff Volume (P1 = 1.19 in.) =   | 0.416 acre-feet | 1.19 | inches |
| 5-yr Runoff Volume (P1 = 1.5 in.) =    | 0.713 acre-feet | 1.50 | inches |
| 10-yr Runoff Volume (P1 = 1.75 in.) =  | 0.991 acre-feet | 1.75 | inches |
| 25-yr Runoff Volume (P1 = 2 in.) =     | 1.426 acre-feet | 2.00 | inches |
| 50-yr Runoff Volume (P1 = 2.25 in.) =  | 1.746 acre-feet | 2.25 | inches |
| 100-yr Runoff Volume (P1 = 2.52 in.) = | 2.181 acre-feet | 2.52 | inches |
| 500-yr Runoff Volume (P1 = 3.14 in.) = | 3.010 acre-feet |      |        |
| Approximate 2-yr Detention Volume =    | 0.280 acre-feet |      |        |
| Approximate 5-yr Detention Volume =    | 0.407 acre-feet |      |        |
| Approximate 10-yr Detention Volume =   | 0.620 acre-feet |      |        |
| Approximate 25-yr Detention Volume =   | 0.740 acre-feet |      |        |
| Approximate 50-yr Detention Volume =   | 0.781 acre-feet |      |        |
| Approximate 100-yr Detention Volume =  | 0.942 acre-feet |      |        |

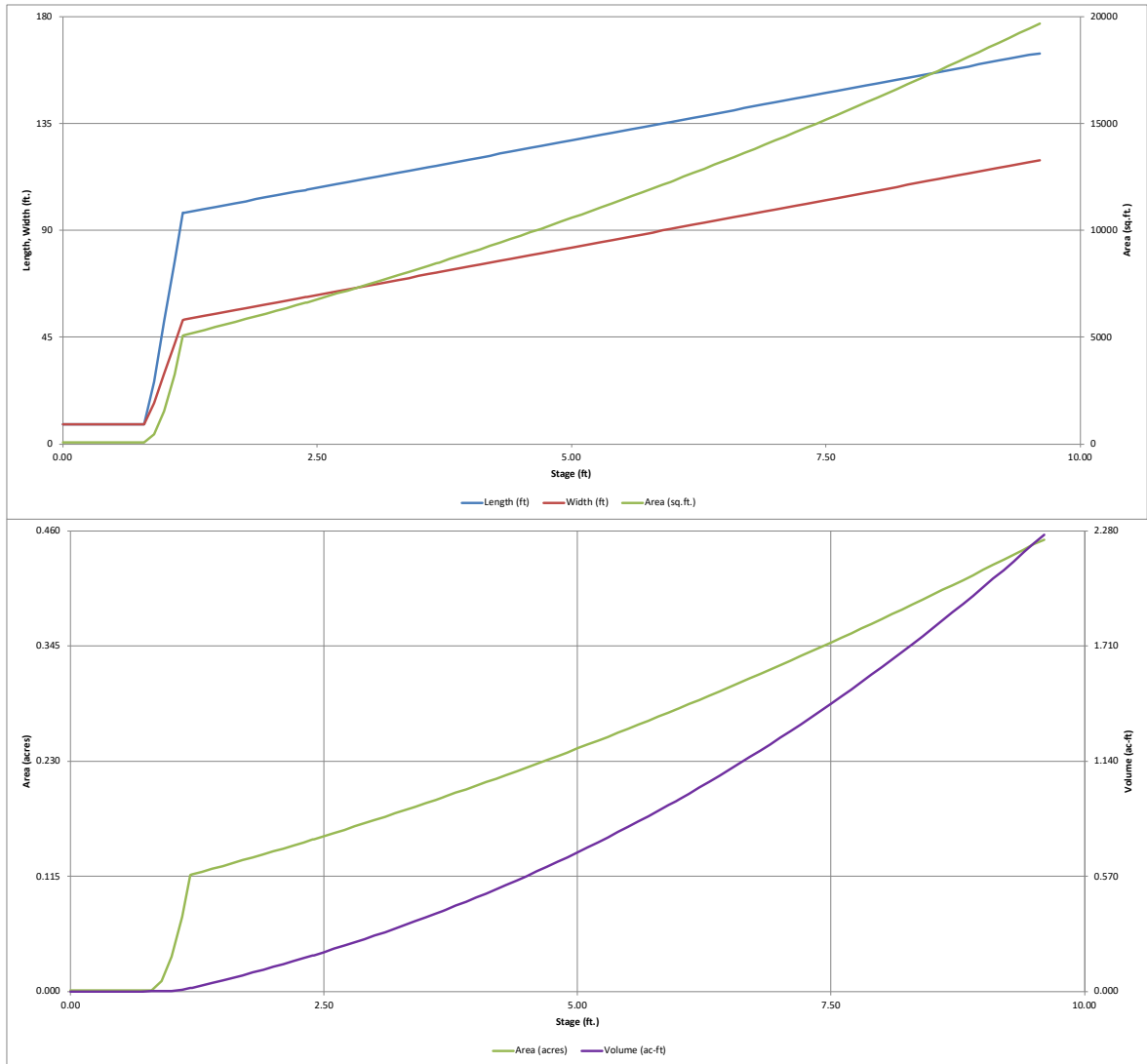
## Define Zones and Basin Geometry

|   |                        |
|---|------------------------|
| Zone 1 Volume (WQCV) =                                  | 0.178 acre-feet        |
| Zone 2 Volume (EURV - Zone 1) =                         | 0.221 acre-feet        |
| Zone 3 Volume (100-year - Zones 1 & 2) =                | 0.543 acre-feet        |
| Total Detention Basin Volume =                          | 0.942 acre-feet        |
| Initial Surge Volume (ISV) =                            | 23 ft <sup>3</sup>     |
| Initial Surge Depth (ISD) =                             | 0.33 ft                |
| Total Available Detention Depth (H <sub>total</sub> ) = | 6.00 ft                |
| Depth of Trickle Channel (H <sub>tr</sub> ) =           | 0.50 ft                |
| Slope of Trickle Channel (S <sub>tr</sub> ) =           | 0.004 ft/ft            |
| Slopes of Main Basin Sides (S <sub>main</sub> ) =       | 4 ft:H                 |
| Basin Length-to-Width Ratio (R <sub>L/W</sub> ) =       | 2                      |
| Initial Surge Area (A <sub>ISV</sub> ) =                | 70 ft <sup>2</sup>     |
| Surge Volume Length (L <sub>ISV</sub> ) =               | 8.4 ft                 |
| Surge Volume Width (W <sub>ISV</sub> ) =                | 8.4 ft                 |
| Depth of Basin Floor (H <sub>floor</sub> ) =            | 0.35 ft                |
| Length of Basin Floor (L <sub>floor</sub> ) =           | 97.3 ft                |
| Width of Basin Floor (W <sub>floor</sub> ) =            | 52.1 ft                |
| Area of Basin Floor (A <sub>floor</sub> ) =             | 5,073 ft <sup>2</sup>  |
| Volume of Basin Floor (V <sub>floor</sub> ) =           | 670 ft <sup>3</sup>    |
| Depth of Main Basin (H <sub>main</sub> ) =              | 4.82 ft                |
| Length of Main Basin (L <sub>main</sub> ) =             | 135.8 ft               |
| Width of Main Basin (W <sub>main</sub> ) =              | 90.7 ft                |
| Area of Main Basin (A <sub>main</sub> ) =               | 12,321 ft <sup>2</sup> |
| Volume of Main Basin (V <sub>main</sub> ) =             | 40,648 ft <sup>3</sup> |
| Calculated Total Basin Volume (V <sub>total</sub> ) =   | 0.950 acre-feet        |

|                             |            |                              |             |            |                         |   |             |                           |                |
|-----------------------------|------------|------------------------------|-------------|------------|-------------------------|---|-------------|---------------------------|----------------|
| Depth Increment =           | 0.10       | ft                           |             |            |                         |   |             |                           |                |
| Stage - Storage Description | Stage (ft) | Optional Override Stage (ft) | Length (ft) | Width (ft) | Area (ft <sup>2</sup> ) | Optional Override Area (ft <sup>2</sup> ) | Area (acre) | Volume (ft <sup>3</sup> ) | Volume (ac-ft) |
| Top of Micropool            | 0.00       |                              | 8.4         | 8.4        | 70                      |   | 0.002       |                           |                |
| ISV                         | 0.33       |                              | 8.4         | 8.4        | 70                      |   | 0.002       | 23                        | 0.001          |
|                             | 0.40       |                              | 8.4         | 8.4        | 70                      |   | 0.002       | 28                        | 0.001          |
|                             | 0.50       |                              | 8.4         | 8.4        | 70                      |   | 0.002       | 35                        | 0.001          |
|                             | 0.60       |                              | 8.4         | 8.4        | 70                      |   | 0.002       | 42                        | 0.001          |
|                             | 0.70       |                              | 8.4         | 8.4        | 70                      |   | 0.002       | 49                        | 0.001          |
|                             | 0.80       |                              | 8.4         | 8.4        | 70                      |   | 0.002       | 56                        | 0.001          |
|                             | 0.90       |                              | 26.2        | 17.1       | 449                     |   | 0.010       | 75                        | 0.002          |
|                             | 1.00       |                              | 51.6        | 29.6       | 1,528                   |   | 0.035       | 168                       | 0.004          |
|                             | 1.10       |                              | 77.0        | 42.1       | 3,243                   |   | 0.074       | 402                       | 0.009          |
| Floor                       | 1.18       |                              | 97.3        | 52.1       | 5,073                   |   | 0.116       | 732                       | 0.017          |
|                             | 1.20       |                              | 97.4        | 52.3       | 5,096                   |   | 0.117       | 833                       | 0.019          |
|                             | 1.30       |                              | 98.2        | 53.1       | 5,217                   |   | 0.120       | 1,349                     | 0.031          |
|                             | 1.40       |                              | 99.0        | 53.9       | 5,339                   |   | 0.123       | 1,877                     | 0.043          |
|                             | 1.50       |                              | 99.8        | 54.7       | 5,462                   |   | 0.125       | 2,417                     | 0.055          |
|                             | 1.60       |                              | 100.6       | 55.5       | 5,586                   |   | 0.128       | 2,969                     | 0.068          |
|                             | 1.70       |                              | 101.4       | 56.3       | 5,711                   |   | 0.131       | 3,534                     | 0.081          |
|                             | 1.80       |                              | 102.2       | 57.1       | 5,838                   |   | 0.134       | 4,111                     | 0.094          |
|                             | 1.90       |                              | 103.0       | 57.9       | 5,966                   |   | 0.137       | 4,702                     | 0.108          |
|                             | 2.00       |                              | 103.8       | 58.7       | 6,096                   |   | 0.140       | 5,305                     | 0.122          |
|                             | 2.10       |                              | 104.6       | 59.5       | 6,226                   |   | 0.143       | 5,921                     | 0.136          |
|                             | 2.20       |                              | 105.4       | 60.3       | 6,358                   |   | 0.146       | 6,550                     | 0.150          |
|                             | 2.30       |                              | 106.2       | 61.1       | 6,492                   |   | 0.149       | 7,192                     | 0.165          |
| Zone 1 (WQCV)               | 2.39       |                              | 107.0       | 61.8       | 6,613                   |   | 0.152       | 7,782                     | 0.179          |
|                             | 2.40       |                              | 107.0       | 61.9       | 6,626                   |   | 0.152       | 7,848                     | 0.180          |
|                             | 2.50       |                              | 107.8       | 62.7       | 6,762                   |   | 0.155       | 8,518                     | 0.196          |
|                             | 2.60       |                              | 108.6       | 63.5       | 6,899                   |   | 0.158       | 9,201                     | 0.211          |
|                             | 2.70       |                              | 109.4       | 64.3       | 7,037                   |   | 0.162       | 9,898                     | 0.227          |
|                             | 2.80       |                              | 110.2       | 65.1       | 7,177                   |   | 0.165       | 10,608                    | 0.244          |
|                             | 2.90       |                              | 111.0       | 65.9       | 7,318                   |   | 0.168       | 11,333                    | 0.260          |
|                             | 3.00       |                              | 111.8       | 66.7       | 7,460                   |   | 0.171       | 12,072                    | 0.277          |
|                             | 3.10       |                              | 112.6       | 67.5       | 7,604                   |   | 0.175       | 12,825                    | 0.294          |
|                             | 3.20       |                              | 113.4       | 68.3       | 7,748                   |   | 0.178       | 13,593                    | 0.312          |
|                             | 3.30       |                              | 114.2       | 69.1       | 7,894                   |   | 0.181       | 14,375                    | 0.330          |
|                             | 3.40       |                              | 115.0       | 69.9       | 8,042                   |   | 0.185       | 15,172                    | 0.348          |
|                             | 3.50       |                              | 115.8       | 70.7       | 8,190                   |   | 0.188       | 15,983                    | 0.367          |
|                             | 3.60       |                              | 116.6       | 71.5       | 8,340                   |   | 0.191       | 16,810                    | 0.386          |
| Zone 2 (EURV)               | 3.67       |                              | 117.2       | 72.1       | 8,446                   |   | 0.194       | 17,397                    | 0.399          |
|                             | 3.70       |                              | 117.4       | 72.3       | 8,491                   |   | 0.195       | 17,651                    | 0.405          |
|                             | 3.80       |                              | 118.2       | 73.1       | 8,644                   |   | 0.198       | 18,508                    | 0.425          |
|                             | 3.90       |                              | 119.0       | 73.9       | 8,798                   |   | 0.202       | 19,380                    | 0.445          |
|                             | 4.00       |                              | 119.8       | 74.7       | 8,953                   |   | 0.206       | 20,268                    | 0.465          |
|                             | 4.10       |                              | 120.6       | 75.5       | 9,109                   |   | 0.209       | 21,171                    | 0.486          |
|                             | 4.20       |                              | 121.4       | 76.3       | 9,266                   |   | 0.213       | 22,089                    | 0.507          |
|                             | 4.30       |                              | 122.2       | 77.1       | 9,425                   |   | 0.216       | 23,024                    | 0.529          |
|                             | 4.40       |                              | 123.0       | 77.9       | 9,585                   |   | 0.220       | 23,975                    | 0.550          |
|                             | 4.50       |                              | 123.8       | 78.7       | 9,747                   |   | 0.224       | 24,941                    | 0.573          |
|                             | 4.60       |                              | 124.6       | 79.5       | 9,909                   |   | 0.227       | 25,924                    | 0.595          |
|                             | 4.70       |                              | 125.4       | 80.3       | 10,073                  |   | 0.231       | 26,923                    | 0.618          |
|                             | 4.80       |                              | 126.2       | 81.1       | 10,239                  |   | 0.235       | 27,939                    | 0.641          |
|                             | 4.90       |                              | 127.0       | 81.9       | 10,405                  |   | 0.239       | 28,971                    | 0.665          |
|                             | 5.00       |                              | 127.8       | 82.7       | 10,573                  |   | 0.243       | 30,020                    | 0.689          |
|                             | 5.10       |                              | 128.6       | 83.5       | 10,742                  |   | 0.247       | 31,085                    | 0.714          |
|                             | 5.20       |                              | 129.4       | 84.3       | 10,912                  |   | 0.251       | 32,168                    | 0.738          |
|                             | 5.30       |                              | 130.2       | 85.1       | 11,084                  |   | 0.254       | 33,268                    | 0.764          |
|                             | 5.40       |                              | 131.0       | 85.9       | 11,257                  |   | 0.258       | 34,385                    | 0.789          |
|                             | 5.50       |                              | 131.8       | 86.7       | 11,431                  |   | 0.262       | 35,519                    | 0.815          |
|                             | 5.60       |                              | 132.6       | 87.5       | 11,607                  |   | 0.266       | 36,671                    | 0.842          |
|                             | 5.70       |                              | 133.4       | 88.3       | 11,783                  |   | 0.271       | 37,841                    | 0.869          |
|                             | 5.80       |                              | 134.2       | 89.1       | 11,961                  |   | 0.275       | 39,028                    | 0.896          |
|                             | 5.90       |                              | 135.0       | 89.9       | 12,141                  |   | 0.279       | 40,233                    | 0.924          |
| Zone 3 (100-year)           | 5.97       |                              | 135.6       | 90.5       | 12,267                  |   | 0.282       | 41,087                    | 0.943          |
|                             | 6.00       |                              | 135.8       | 90.7       | 12,321                  |   | 0.283       | 41,456                    | 0.952          |
|                             | 6.10       |                              | 136.6       | 91.5       | 12,503                  |   | 0.287       | 42,697                    | 0.980          |
|                             | 6.20       |                              | 137.4       | 92.3       | 12,686                  |   | 0.291       | 43,957                    | 1.009          |
|                             | 6.30       |                              | 138.2       | 93.1       | 12,871                  |   | 0.295       | 45,235                    | 1.038          |
|                             | 6.40       |                              | 139.0       | 93.9       | 13,057                  |   | 0.300       | 46,531                    | 1.068          |
|                             | 6.50       |                              | 139.8       | 94.7       | 13,244                  |   | 0.304       | 47,846                    | 1.098          |
|                             | 6.60       |                              | 140.6       | 95.5       | 13,432                  |   | 0.308       | 49,180                    | 1.129          |
|                             | 6.70       |                              | 141.4       | 96.3       | 13,621                  |   | 0.313       | 50,532                    | 1.160          |
|                             | 6.80       |                              | 142.2       | 97.1       | 13,812                  |   | 0.317       | 51,904                    | 1.192          |
|                             | 6.90       |                              | 143.0       | 97.9       | 14,004                  |   | 0.321       | 53,295                    | 1.223          |
|                             | 7.00       |                              | 143.8       | 98.7       | 14,198                  |   | 0.326       | 54,705                    | 1.256          |
|                             | 7.10       |                              | 144.6       | 99.5       | 14,392                  |   | 0.330       | 56,135                    | 1.289          |
|                             | 7.20       |                              | 145.4       | 100.3      | 14,588                  |   | 0.335       | 57,584                    | 1.322          |
|                             | 7.30       |                              | 146.2       | 101.1      | 14,786                  |   | 0.339       | 59,052                    | 1.356          |
|                             | 7.40       |                              | 147.0       | 101.9      | 14,984                  |   | 0.344       | 60,541                    | 1.390          |
|                             | 7.50       |                              | 147.8       | 102.7      | 15,184                  |   | 0.349       | 62,049                    | 1.424          |
|                             | 7.60       |                              | 148.6       | 103.5      | 15,385                  |   | 0.353       | 63,578                    | 1.460          |
|                             | 7.70       |                              | 149.4       | 104.3      | 15,587                  |   | 0.358       | 65,126                    | 1.495          |
|                             | 7.80       |                              | 150.2       | 105.1      | 15,791                  |   | 0.363       | 66,695                    | 1.531          |
|                             | 7.90       |                              | 151.0       | 105.9      | 15,996                  |   | 0.367       | 68,284                    | 1.568          |
|                             | 8.00       |                              | 151.8       | 106.7      | 16,202                  |   | 0.372       | 69,894                    | 1.605          |
|                             | 8.10       |                              | 152.6       | 107.5      | 16,410                  |   | 0.377       | 71,525                    | 1.642          |
|                             | 8.20       |                              | 153.4       | 108.3      | 16,618                  |   | 0.382       | 73,176                    | 1.680          |
|                             | 8.30       |                              | 154.2       | 109.1      | 16,828                  |   | 0.386       | 74,849                    | 1.718          |
| 8.40                        |            | 155.0                        | 109.9       | 17,040     |                         | 0.391                                     | 76,542      | 1.757                     |                |
| 8.50                        |            | 155.8                        | 110.7       | 17,252     |                         | 0.396                                     | 78,257      | 1.797                     |                |
| 8.60                        |            | 156.6                        | 111.5       | 17,466     |                         | 0.401                                     | 79,992      | 1.836                     |                |
| 8.70                        |            | 157.4                        | 112.3       | 17,681     |                         | 0.406                                     | 81,750      | 1.877                     |                |
| 8.80                        |            | 158.2                        | 113.1       | 17,898     |                         | 0.411                                     | 83,529      | 1.918                     |                |
| 8.90                        |            | 159.0                        | 113.9       | 18,115     |                         | 0.416                                     | 85,329      | 1.959                     |                |
| 9.00                        |            | 159.8                        | 114.7       | 18,334     |                         | 0.421                                     | 87,152      | 2.001                     |                |
| 9.10                        |            | 160.6                        | 115.5       | 18,555     |                         | 0.426                                     | 88,996      | 2.043                     |                |
| 9.20                        |            | 161.4                        | 116.3       | 18,776     |                         | 0.431                                     | 90,863      | 2.086                     |                |
| 9.30                        |            | 162.2                        | 117.1       | 18,999     |                         | 0.436                                     | 92,752      | 2.129                     |                |
| 9.40                        |            | 163.0                        | 117.9       | 19,223     |                         | 0.441                                     | 94,663      | 2.173                     |                |
| 9.50                        |            | 163.8                        | 118.7       | 19,449     |                         | 0.446                                     | 96,596      | 2.218                     |                |
| 9.60                        |            | 164.6                        | 119.5       | 19,675     |                         | 0.452                                     | 98,553      | 2.262                     |                |

# DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.04 (February 2021)

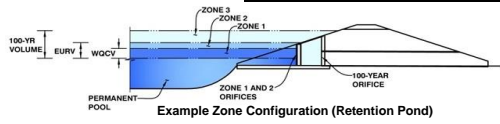


# DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.04 (February 2021)

Project: **Flying Horse North MDDP**

Basin ID: **Pond 9**



## Watershed Information

|   |                |
|---|----------------|
| Selected BMP Type =                     | <b>EDB</b>     |
| Watershed Area =                        | 86.18 acres    |
| Watershed Length =                      | 2,354 ft       |
| Watershed Length to Centroid =          | 1,434 ft       |
| Watershed Slope =                       | 0.039 ft/ft    |
| Watershed Imperviousness =              | 21.81% percent |
| Percentage Hydrologic Soil Group A =    | 0.0% percent   |
| Percentage Hydrologic Soil Group B =    | 100.0% percent |
| Percentage Hydrologic Soil Groups C/D = | 0.0% percent   |
| Target WQCV Drain Time =                | 40.0 hours     |
| Location for 1-hr Rainfall Depths =     | User Input     |

After providing required inputs above including 1-hour rainfall depths, click "Run CUHP" to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

|  |                  |
|--|------------------|
| Water Quality Capture Volume (WQCV) =  | 0.883 acre-feet  |
| Excess Urban Runoff Volume (EURV) =    | 1.880 acre-feet  |
| 2-yr Runoff Volume (P1 = 1.19 in.) =   | 2.026 acre-feet  |
| 5-yr Runoff Volume (P1 = 1.5 in.) =    | 3.599 acre-feet  |
| 10-yr Runoff Volume (P1 = 1.75 in.) =  | 5.087 acre-feet  |
| 25-yr Runoff Volume (P1 = 2 in.) =     | 7.473 acre-feet  |
| 50-yr Runoff Volume (P1 = 2.25 in.) =  | 9.201 acre-feet  |
| 100-yr Runoff Volume (P1 = 2.52 in.) = | 11.580 acre-feet |
| 500-yr Runoff Volume (P1 = 3.14 in.) = | 16.065 acre-feet |
| Approximate 2-yr Detention Volume =    | 1.301 acre-feet  |
| Approximate 5-yr Detention Volume =    | 1.913 acre-feet  |
| Approximate 10-yr Detention Volume =   | 3.018 acre-feet  |
| Approximate 25-yr Detention Volume =   | 3.681 acre-feet  |
| Approximate 50-yr Detention Volume =   | 3.888 acre-feet  |
| Approximate 100-yr Detention Volume =  | 4.742 acre-feet  |

## Optional User Overrides

|           |      |
|-----------|------|
| acre-feet |      |
| acre-feet |      |
| inches    | 1.19 |
| inches    | 1.50 |
| inches    | 1.75 |
| inches    | 2.00 |
| inches    | 2.25 |
| inches    | 2.52 |
| inches    |      |

## Define Zones and Basin Geometry

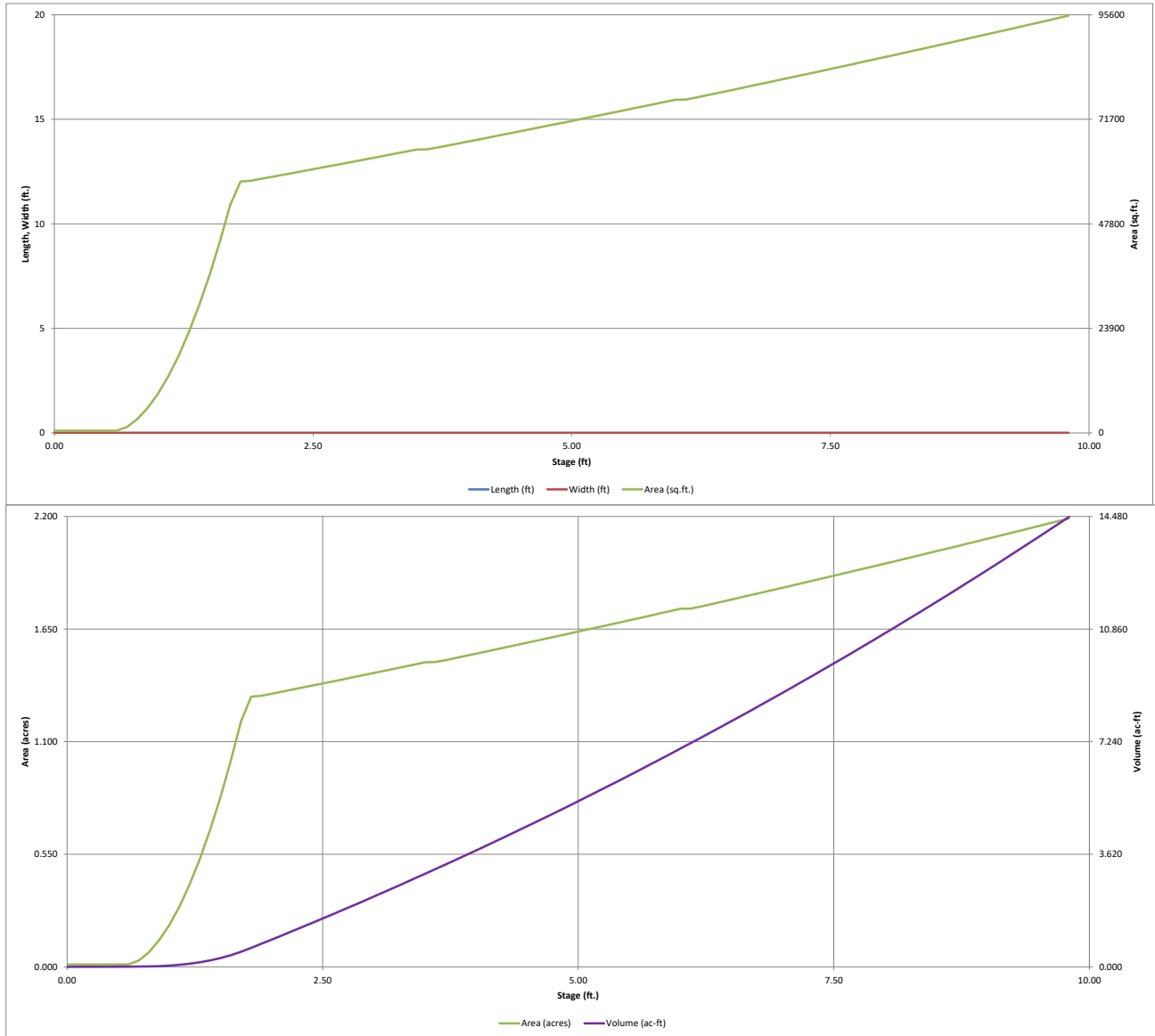
|   |                      |
|---|----------------------|
| Zone 1 Volume (WQCV) =                                  | 0.883 acre-feet      |
| Zone 2 Volume (5-year - Zone 1) =                       | 1.030 acre-feet      |
| Zone 3 Volume (100-year - Zones 1 & 2) =                | 2.829 acre-feet      |
| Total Detention Basin Volume =                          | 4.742 acre-feet      |
| Initial Surge Volume (ISV) =                            | user ft <sup>3</sup> |
| Initial Surge Depth (ISD) =                             | user ft              |
| Total Available Detention Depth (H <sub>total</sub> ) = | user ft              |
| Depth of Trickle Channel (H <sub>TC</sub> ) =           | user ft              |
| Slope of Trickle Channel (S <sub>TC</sub> ) =           | user ft/ft           |
| Slopes of Main Basin Sides (S <sub>main</sub> ) =       | user H:V             |
| Basin Length-to-Width Ratio (L <sub>W</sub> ) =         | user                 |

|   |                      |
|---|----------------------|
| Initial Surge Area (A <sub>ISV</sub> ) =              | user ft <sup>2</sup> |
| Surge Volume Length (L <sub>ISV</sub> ) =             | user ft              |
| Surge Volume Width (W <sub>ISV</sub> ) =              | user ft              |
| Depth of Basin Floor (H <sub>FLOOR</sub> ) =          | user ft              |
| Length of Basin Floor (L <sub>FLOOR</sub> ) =         | user ft              |
| Width of Basin Floor (W <sub>FLOOR</sub> ) =          | user ft              |
| Area of Basin Floor (A <sub>FLOOR</sub> ) =           | user ft <sup>2</sup> |
| Volume of Basin Floor (V <sub>FLOOR</sub> ) =         | user ft <sup>3</sup> |
| Depth of Main Basin (H <sub>MAIN</sub> ) =            | user ft              |
| Length of Main Basin (L <sub>MAIN</sub> ) =           | user ft              |
| Width of Main Basin (W <sub>MAIN</sub> ) =            | user ft              |
| Area of Main Basin (A <sub>MAIN</sub> ) =             | user ft <sup>2</sup> |
| Volume of Main Basin (V <sub>MAIN</sub> ) =           | user ft <sup>3</sup> |
| Calculated Total Basin Volume (V <sub>total</sub> ) = | user acre-feet       |

|                             |            |                              |             |            |                         |   |             |                           |                |
|-----------------------------|------------|------------------------------|-------------|------------|-------------------------|---|-------------|---------------------------|----------------|
| Depth Increment =           | 0.10       | ft                           |             |            |                         |   |             |                           |                |
| Stage - Storage Description | Stage (ft) | Optional Override Stage (ft) | Length (ft) | Width (ft) | Area (ft <sup>2</sup> ) | Optional Override Area (ft <sup>2</sup> ) | Area (acre) | Volume (ft <sup>3</sup> ) | Volume (ac-ft) |
| Top of Micropool            | --         | 0.00                         | --          | --         | --                      | 510                                       | 0.012       |                           |                |
|                             | --         | 0.10                         | --          | --         | --                      | 510                                       | 0.012       | 51                        | 0.001          |
|                             | --         | 0.20                         | --          | --         | --                      | 510                                       | 0.012       | 102                       | 0.002          |
|                             | --         | 0.30                         | --          | --         | --                      | 510                                       | 0.012       | 153                       | 0.004          |
|                             | --         | 0.40                         | --          | --         | --                      | 510                                       | 0.012       | 204                       | 0.005          |
|                             | --         | 0.50                         | --          | --         | --                      | 510                                       | 0.012       | 255                       | 0.006          |
|                             | --         | 0.60                         | --          | --         | --                      | 510                                       | 0.012       | 306                       | 0.007          |
|                             | --         | 0.70                         | --          | --         | --                      | 1,331                                     | 0.031       | 398                       | 0.009          |
|                             | --         | 0.80                         | --          | --         | --                      | 3,124                                     | 0.072       | 620                       | 0.014          |
|                             | --         | 0.90                         | --          | --         | --                      | 5,648                                     | 0.130       | 1,059                     | 0.024          |
|                             | --         | 1.00                         | --          | --         | --                      | 8,903                                     | 0.204       | 1,786                     | 0.041          |
|                             | --         | 1.10                         | --          | --         | --                      | 12,887                                    | 0.296       | 2,876                     | 0.066          |
|                             | --         | 1.20                         | --          | --         | --                      | 17,602                                    | 0.404       | 4,400                     | 0.101          |
|                             | --         | 1.30                         | --          | --         | --                      | 23,047                                    | 0.529       | 6,433                     | 0.148          |
|                             | --         | 1.40                         | --          | --         | --                      | 29,222                                    | 0.671       | 9,046                     | 0.208          |
|                             | --         | 1.50                         | --          | --         | --                      | 36,128                                    | 0.829       | 12,314                    | 0.283          |
|                             | --         | 1.60                         | --          | --         | --                      | 43,764                                    | 1.005       | 16,308                    | 0.374          |
|                             | --         | 1.70                         | --          | --         | --                      | 52,130                                    | 1.197       | 21,103                    | 0.484          |
|                             | --         | 1.80                         | --          | --         | --                      | 57,500                                    | 1.320       | 26,584                    | 0.610          |
|                             | --         | 1.90                         | --          | --         | --                      | 57,673                                    | 1.324       | 32,343                    | 0.742          |
|                             | --         | 2.00                         | --          | --         | --                      | 58,107                                    | 1.334       | 38,132                    | 0.875          |
|                             | --         | 2.10                         | --          | --         | --                      | 58,542                                    | 1.344       | 43,964                    | 1.009          |
|                             | --         | 2.20                         | --          | --         | --                      | 58,979                                    | 1.354       | 49,840                    | 1.144          |
|                             | --         | 2.30                         | --          | --         | --                      | 59,418                                    | 1.364       | 55,760                    | 1.280          |
|                             | --         | 2.40                         | --          | --         | --                      | 59,858                                    | 1.374       | 61,724                    | 1.417          |
|                             | --         | 2.50                         | --          | --         | --                      | 60,299                                    | 1.384       | 67,732                    | 1.555          |
|                             | --         | 2.60                         | --          | --         | --                      | 60,742                                    | 1.394       | 73,784                    | 1.694          |
|                             | --         | 2.70                         | --          | --         | --                      | 61,187                                    | 1.405       | 79,880                    | 1.834          |
|                             | --         | 2.80                         | --          | --         | --                      | 61,632                                    | 1.415       | 86,021                    | 1.975          |
|                             | --         | 2.90                         | --          | --         | --                      | 62,080                                    | 1.425       | 92,207                    | 2.117          |
|                             | --         | 3.00                         | --          | --         | --                      | 62,529                                    | 1.435       | 98,437                    | 2.260          |
|                             | --         | 3.10                         | --          | --         | --                      | 62,979                                    | 1.446       | 104,713                   | 2.404          |
|                             | --         | 3.20                         | --          | --         | --                      | 63,431                                    | 1.456       | 111,033                   | 2.549          |
|                             | --         | 3.30                         | --          | --         | --                      | 63,884                                    | 1.467       | 117,399                   | 2.695          |
|                             | --         | 3.40                         | --          | --         | --                      | 64,338                                    | 1.477       | 123,810                   | 2.842          |
|                             | --         | 3.50                         | --          | --         | --                      | 64,795                                    | 1.487       | 130,267                   | 2.991          |
|                             | --         | 3.60                         | --          | --         | --                      | 64,840                                    | 1.489       | 136,748                   | 3.139          |
|                             | --         | 3.70                         | --          | --         | --                      | 65,252                                    | 1.498       | 143,253                   | 3.289          |
|                             | --         | 3.80                         | --          | --         | --                      | 65,711                                    | 1.509       | 149,801                   | 3.439          |
|                             | --         | 3.90                         | --          | --         | --                      | 66,172                                    | 1.519       | 156,395                   | 3.590          |
|                             | --         | 4.00                         | --          | --         | --                      | 66,634                                    | 1.530       | 163,036                   | 3.743          |
|                             | --         | 4.10                         | --          | --         | --                      | 67,097                                    | 1.540       | 169,722                   | 3.896          |
|                             | --         | 4.20                         | --          | --         | --                      | 67,562                                    | 1.551       | 176,455                   | 4.051          |
|                             | --         | 4.30                         | --          | --         | --                      | 68,029                                    | 1.562       | 183,235                   | 4.206          |
|                             | --         | 4.40                         | --          | --         | --                      | 68,497                                    | 1.572       | 190,061                   | 4.363          |
|                             | --         | 4.50                         | --          | --         | --                      | 68,966                                    | 1.583       | 196,934                   | 4.521          |
|                             | --         | 4.60                         | --          | --         | --                      | 69,437                                    | 1.594       | 203,854                   | 4.680          |
|                             | --         | 4.70                         | --          | --         | --                      | 69,909                                    | 1.605       | 210,822                   | 4.840          |
|                             | --         | 4.80                         | --          | --         | --                      | 70,383                                    | 1.616       | 217,836                   | 5.001          |
|                             | --         | 4.90                         | --          | --         | --                      | 70,858                                    | 1.627       | 224,898                   | 5.163          |
|                             | --         | 5.00                         | --          | --         | --                      | 71,335                                    | 1.638       | 232,008                   | 5.326          |
|                             | --         | 5.10                         | --          | --         | --                      | 71,813                                    | 1.649       | 239,165                   | 5.490          |
|                             | --         | 5.20                         | --          | --         | --                      | 72,293                                    | 1.660       | 246,371                   | 5.656          |
|                             | --         | 5.30                         | --          | --         | --                      | 72,774                                    | 1.671       | 253,624                   | 5.822          |
|                             | --         | 5.40                         | --          | --         | --                      | 73,257                                    | 1.682       | 260,926                   | 5.990          |
|                             | --         | 5.50                         | --          | --         | --                      | 73,741                                    | 1.693       | 268,275                   | 6.159          |
|                             | --         | 5.60                         | --          | --         | --                      | 74,227                                    | 1.704       | 275,674                   | 6.329          |
|                             | --         | 5.70                         | --          | --         | --                      | 74,714                                    | 1.715       | 283,121                   | 6.500          |
|                             | --         | 5.80                         | --          | --         | --                      | 75,202                                    | 1.726       | 290,617                   | 6.672          |
|                             | --         | 5.90                         | --          | --         | --                      | 75,692                                    | 1.738       | 298,161                   | 6.845          |
|                             | --         | 6.00                         | --          | --         | --                      | 76,184                                    | 1.749       | 305,755                   | 7.019          |
|                             | --         | 6.10                         | --          | --         | --                      | 76,233                                    | 1.750       | 313,376                   | 7.194          |
|                             | --         | 6.20                         | --          | --         | --                      | 76,677                                    | 1.760       | 321,021                   | 7.370          |
|                             | --         | 6.30                         | --          | --         | --                      | 77,171                                    | 1.772       | 328,714                   | 7.546          |
|                             | --         | 6.40                         | --          | --         | --                      | 77,667                                    | 1.783       | 336,456                   | 7.724          |
|                             | --         | 6.50                         | --          | --         | --                      | 78,164                                    | 1.794       | 344,247                   | 7.903          |
|                             | --         | 6.60                         | --          | --         | --                      | 78,663                                    | 1.806       | 352,089                   | 8.083          |
|                             | --         | 6.70                         | --          | --         | --                      | 79,163                                    | 1.817       | 359,980                   | 8.264          |
|                             | --         | 6.80                         | --          | --         | --                      | 79,665                                    | 1.829       | 367,921                   | 8.446          |
|                             | --         | 6.90                         | --          | --         | --                      | 80,168                                    | 1.840       | 375,913                   | 8.630          |
|                             | --         | 7.00                         | --          | --         | --                      | 80,673                                    | 1.852       | 383,955                   | 8.814          |
|                             | --         | 7.10                         | --          | --         | --                      | 81,179                                    | 1.864       | 392,048                   | 9.000          |
|                             | --         | 7.20                         | --          | --         | --                      | 81,687                                    | 1.875       | 400,191                   | 9.187          |
|                             | --         | 7.30                         | --          | --         | --                      | 82,196                                    | 1.887       | 408,385                   | 9.375          |
|                             | --         | 7.40                         | --          | --         | --                      | 82,707                                    | 1.899       | 416,630                   | 9.565          |
|                             | --         | 7.50                         | --          | --         | --                      | 83,219                                    | 1.910       | 424,927                   | 9.755          |
|                             | --         | 7.60                         | --          | --         | --                      | 83,732                                    | 1.922       | 433,274                   | 9.947          |
|                             | --         | 7.70                         | --          | --         | --                      | 84,247                                    | 1.934       | 441,673                   | 10.139         |
|                             | --         | 7.80                         | --          | --         | --                      | 84,764                                    | 1.946       | 450,124                   | 10.333         |
|                             | --         | 7.90                         | --          | --         | --                      | 85,282                                    | 1.958       | 458,626                   | 10.529         |
|                             | --         | 8.00                         | --          | --         | --                      | 85,801                                    | 1.970       | 467,180                   | 10.725         |
|                             | --         | 8.10                         | --          | --         | --                      | 86,322                                    | 1.982       | 475,786                   | 10.923         |
|                             | --         | 8.20                         | --          | --         | --                      | 86,845                                    | 1.994       | 484,445                   | 11.121         |
|                             | --         | 8.30                         | --          | --         | --                      | 87,368                                    | 2.006       | 493,155                   | 11.321         |
|                             | --         | 8.40                         | --          | --         | --                      | 87,894                                    | 2.018       | 501,918                   | 11.522         |
|                             | --         | 8.50                         | --          | --         | --                      | 88,421                                    | 2.030       | 510,734                   | 11.725         |
|                             | --         | 8.60                         | --          | --         | --                      | 88,949                                    | 2.042       | 519,603                   | 11.928         |
|                             | --         | 8.70                         | --          | --         | --                      | 89,479                                    | 2.054       | 528,524                   | 12.133         |
|                             | --         | 8.80                         | --          | --         | --                      | 90,010                                    | 2.066       | 537,498                   | 12.339         |
|                             | --         | 8.90                         | --          | --         | --                      | 90,543                                    | 2.079       | 546,526                   | 12.547         |
|                             | --         | 9.00                         | --          | --         | --                      | 91,077                                    | 2.091       | 555,607                   | 12.755         |
|                             | --         | 9.10                         | --          | --         | --                      | 91,612                                    | 2.103       | 564,741                   | 12.965         |
|                             | --         | 9.20                         | --          | --         | --                      | 92,149                                    | 2.115       | 573,930                   | 13.176         |
|                             | --         | 9.30                         | --          | --         | --                      | 92,688                                    | 2.128       | 583,171                   | 13.388         |
|                             | --         | 9.40                         | --          | --         | --                      | 93,228                                    | 2.140       | 592,467                   | 13.601         |
|                             | --         | 9.50                         | --          | --         | --                      | 93,770                                    | 2.153       | 601,817                   | 13.816         |
|                             | --         | 9.60                         | --          | --         | --                      | 94,313                                    | 2.165       | 611,221                   | 14.032         |
|                             | --         | 9.70                         | --          | --         | --                      | 94,857                                    | 2.178       | 620,680                   | 14.249         |
|                             | --         | 9.80                         | --          | --         | --                      | 95,403                                    | 2.190       | 630,193                   | 14.467         |

# DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.04 (February 2021)

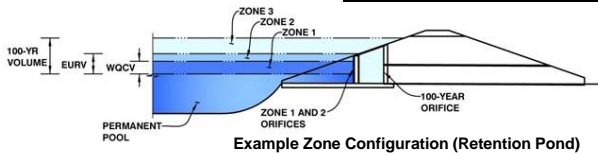


# DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.04 (February 2021)

Project: Flying Horse North MDDP

Basin ID: Pond 9



Example Zone Configuration (Retention Pond)

|                   | Estimated Stage (ft) | Estimated Volume (ac-ft) | Outlet Type          |
|-------------------|----------------------|--------------------------|----------------------|
| Zone 1 (WQCV)     | 2.01                 | 0.883                    | Orifice Plate        |
| Zone 2 (5-year)   | 2.76                 | 1.030                    | Weir&Pipe (Restrict) |
| Zone 3 (100-year) | 4.64                 | 2.829                    | Weir&Pipe (Restrict) |
| Total (all zones) |                      | 4.742                    |                      |

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth = N/A ft (distance below the filtration media surface)  
Underdrain Orifice Diameter = N/A inches

Calculated Parameters for Underdrain  
Underdrain Orifice Area = N/A ft<sup>2</sup>  
Underdrain Orifice Centroid = N/A feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice = 0.00 ft (relative to basin bottom at Stage = 0 ft)  
Depth at top of Zone using Orifice Plate = 2.36 ft (relative to basin bottom at Stage = 0 ft)  
Orifice Plate: Orifice Vertical Spacing = 9.40 inches  
Orifice Plate: Orifice Area per Row = 3.45 sq. inches (use rectangular openings)

Calculated Parameters for Plate  
WQ Orifice Area per Row = 2.396E-02 ft<sup>2</sup>  
Elliptical Half-Width = N/A feet  
Elliptical Slot Centroid = N/A feet  
Elliptical Slot Area = N/A ft<sup>2</sup>

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

|                                | Row 1 (required) | Row 2 (optional) | Row 3 (optional) | Row 4 (optional) | Row 5 (optional) | Row 6 (optional) | Row 7 (optional) | Row 8 (optional) |
|--------------------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|
| Stage of Orifice Centroid (ft) | 0.00             | 0.79             | 1.57             |                  |                  |                  |                  |                  |
| Orifice Area (sq. inches)      | 3.45             | 3.45             | 3.45             |                  |                  |                  |                  |                  |

|                                | Row 9 (optional) | Row 10 (optional) | Row 11 (optional) | Row 12 (optional) | Row 13 (optional) | Row 14 (optional) | Row 15 (optional) | Row 16 (optional) |
|--------------------------------|------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| Stage of Orifice Centroid (ft) |                  |                   |                   |                   |                   |                   |                   |                   |
| Orifice Area (sq. inches)      |                  |                   |                   |                   |                   |                   |                   |                   |

User Input: Vertical Orifice (Circular or Rectangular)

Invert of Vertical Orifice = N/A ft (relative to basin bottom at Stage = 0 ft)  
Depth at top of Zone using Vertical Orifice = N/A ft (relative to basin bottom at Stage = 0 ft)  
Vertical Orifice Diameter = N/A inches

Calculated Parameters for Vertical Orifice  
Vertical Orifice Area = N/A ft<sup>2</sup>  
Vertical Orifice Centroid = N/A feet

User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe)

Overflow Weir Front Edge Height, H<sub>o</sub> = 3.10 ft (relative to basin bottom at Stage = 0 ft)  
Overflow Weir Front Edge Length = 4.00 feet  
Overflow Weir Grate Slope = 0.00 H:V  
Horiz. Length of Weir Sides = 6.00 feet  
Overflow Grate Type = Type C Grate  
Debris Clogging % = 50%

Calculated Parameters for Overflow Weir  
Height of Grate Upper Edge, H<sub>u</sub> = 3.10 feet  
Overflow Weir Slope Length = 7.10 feet  
Grate Open Area / 100-yr Orifice Area = 1.82  
Overflow Grate Open Area w/o Debris = 16.70 ft<sup>2</sup>  
Overflow Grate Open Area w/ Debris = 34.44 ft<sup>2</sup>

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

Depth to Invert of Outlet Pipe = 2.30 ft (distance below basin bottom at Stage = 0 ft)  
Outlet Pipe Diameter = 42.00 inches  
Restrictor Plate Height Above Pipe Invert = 38.00 inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate  
Outlet Orifice Area = 9.16 ft<sup>2</sup>  
Outlet Orifice Centroid = 1.67 feet  
Half-Central Angle of Restrictor Plate on Pipe = 2.51 radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage = 7.80 ft (relative to basin bottom at Stage = 0 ft)  
Spillway Crest Length = 113.00 feet  
Spillway End Slopes = 4.00 H:V  
Freeboard above Max Water Surface = 1.00 feet

Calculated Parameters for Spillway  
Spillway Design Flow Depth = 0.98 feet  
Stage at Top of Freeboard = 9.78 feet  
Basin Area at Top of Freeboard = 2.19 acres  
Basin Volume at Top of Freeboard = 14.42 acre-ft

## Routed Hydrograph Results

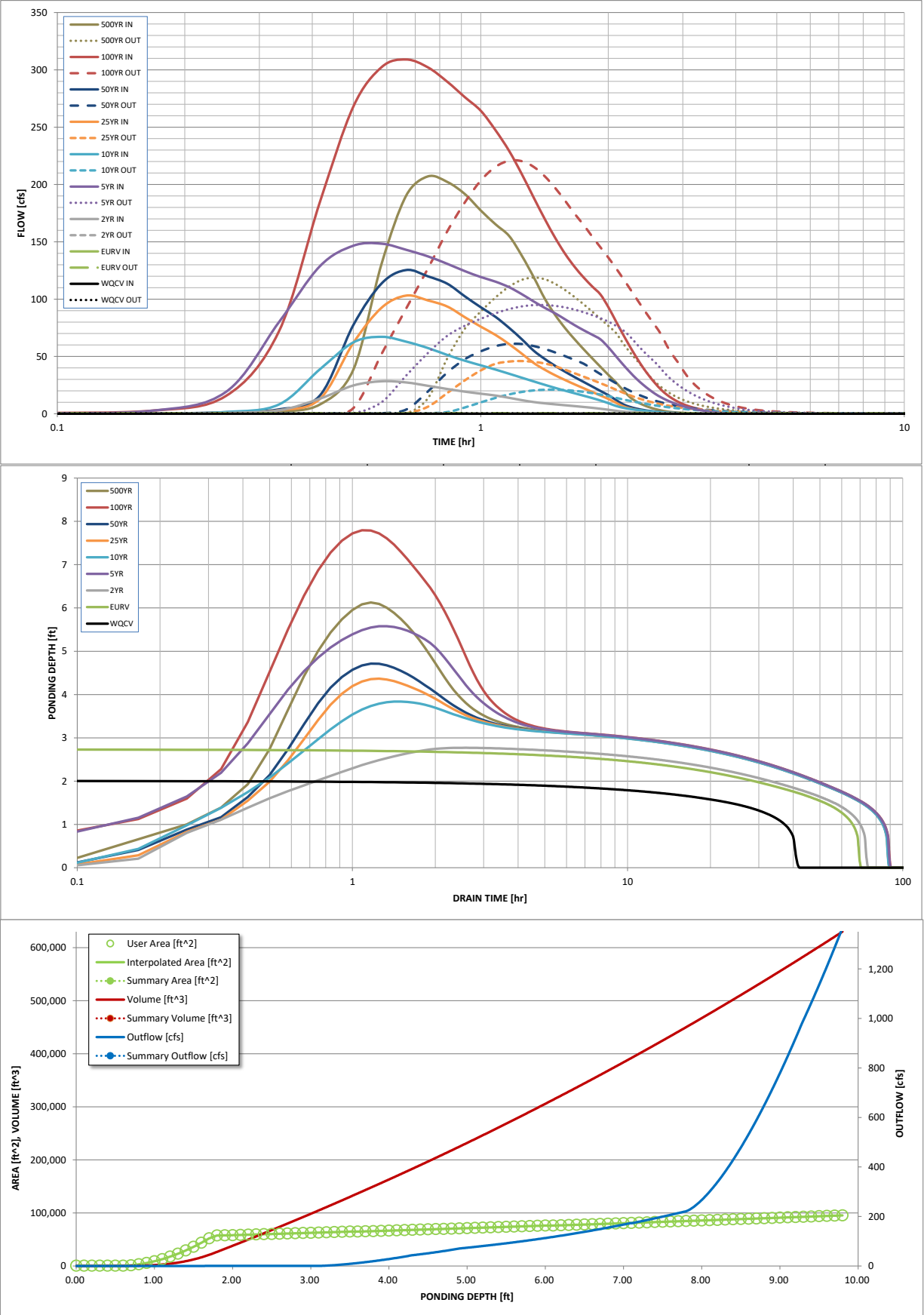
The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).

|  | WQCV  | EURV  | 2 Year | 5 Year          | 10 Year         | 25 Year         | 50 Year         | 100 Year        | 500 Year        |
|--|-------|-------|--------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|
| Design Storm Return Period =                       | N/A   | N/A   | 1.19   | 1.50            | 1.75            | 2.00            | 2.25            | 2.52            | 3.14            |
| One-Hour Rainfall Depth (in) =                     | 0.883 | 1.880 | 2.026  | 3.599           | 5.087           | 7.473           | 9.201           | 11.580          | 16.065          |
| CUHP Runoff Volume (acre-ft) =                     | 0.883 | 1.880 | 2.026  | 3.599           | 5.087           | 7.473           | 9.201           | 11.580          | 16.065          |
| User Override Inflow Hydrograph Volume (acre-ft) = | N/A   | N/A   | 2.026  | 17.291          | 5.087           | 7.473           | 9.201           | 31.926          | 16.065          |
| CUHP Predevelopment Peak Q (cfs) =                 | N/A   | N/A   | 11.0   | 30.3            | 46.1            | 81.0            | 101.4           | 129.3           | 179.9           |
| OPTIONAL Override Predevelopment Peak Q (cfs) =    | N/A   | N/A   |        | 95.0            |                 |                 |                 | 282.3           |                 |
| Predevelopment Unit Peak Flow, q (cfs/acre) =      | N/A   | N/A   | 0.13   | 1.10            | 0.53            | 0.94            | 1.18            | 3.28            | 2.09            |
| Peak Inflow Q (cfs) =                              | N/A   | N/A   | 28.4   | 148.4           | 67.1            | 103.1           | 125.4           | 309.0           | 207.1           |
| Peak Outflow Q (cfs) =                             | 0.4   | 0.5   | 0.5    | 94.8            | 21.0            | 46.0            | 61.0            | 220.7           | 118.9           |
| Ratio Peak Outflow to Predevelopment Q =           | N/A   | N/A   | N/A    | 1.0             | 0.5             | 0.6             | 0.6             | 0.8             | 0.7             |
| Structure Controlling Flow =                       | Plate | Plate | Plate  | Overflow Weir 2 | Overflow Weir 1 | Overflow Weir 2 | Overflow Weir 2 | Overflow Weir 2 | Overflow Weir 1 |
| Max Velocity through Grate 1 (fps) =               | N/A   | N/A   | N/A    | 4.5             | 1.2             | 2.7             | 3.4             | 6.1             | 4.9             |
| Max Velocity through Grate 2 (fps) =               | N/A   | N/A   | N/A    | 0.3             | N/A             | 0.0             | 0.1             | 1.7             | 0.5             |
| Time to Drain 97% of Inflow Volume (hours) =       | 38    | 65    | 69     | 61              | 78              | 74              | 71              | 46              | 62              |
| Time to Drain 99% of Inflow Volume (hours) =       | 40    | 68    | 72     | 78              | 84              | 83              | 82              | 70              | 78              |
| Maximum Ponding Depth (ft) =                       | 2.01  | 2.74  | 2.77   | 5.58            | 3.84            | 4.37            | 4.71            | 7.79            | 6.13            |
| Area at Maximum Ponding Depth (acres) =            | 1.33  | 1.41  | 1.41   | 1.70            | 1.51            | 1.57            | 1.61            | 1.94            | 1.75            |
| Maximum Volume Stored (acre-ft) =                  | 0.889 | 1.890 | 1.932  | 6.278           | 3.484           | 4.300           | 4.856           | 10.314          | 7.229           |



DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD- Detention.. Version 4.04 (February 2021)



| S-A-V-D Chart Axis Override | X-axis | Left Y-Axis | Right Y-Axis |
|-----------------------------|--------|-------------|--------------|
| minimum bound               |        |             |              |
| maximum bound               |        |             |              |

# DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename: ...[SWM]Outflow hydrographs\Pond6 OutflowHydrograph.xlsx

## Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

|               | SOURCE  | CUHP       | CUHP       | CUHP         | USER         | CUHP          | CUHP          | CUHP          | USER           | CUHP           |
|---------------|---------|------------|------------|--------------|--------------|---------------|---------------|---------------|----------------|----------------|
| Time Interval | TIME    | WQCV [cfs] | EURV [cfs] | 2 Year [cfs] | 5 Year [cfs] | 10 Year [cfs] | 25 Year [cfs] | 50 Year [cfs] | 100 Year [cfs] | 500 Year [cfs] |
| 5.00 min      | 0:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 0:05:00 | 0.00       | 0.00       | 0.00         | 0.19         | 0.00          | 0.00          | 0.00          | 0.48           | 0.00           |
|               | 0:10:00 | 0.00       | 0.00       | 0.00         | 2.62         | 0.00          | 0.00          | 0.09          | 2.67           | 0.28           |
|               | 0:15:00 | 0.00       | 0.00       | 0.76         | 19.04        | 1.55          | 1.04          | 1.33          | 15.51          | 1.92           |
|               | 0:20:00 | 0.00       | 0.00       | 2.95         | 79.68        | 8.04          | 2.99          | 3.82          | 71.52          | 8.06           |
|               | 0:25:00 | 0.00       | 0.00       | 13.17        | 128.64       | 38.75         | 12.89         | 15.88         | 184.41         | 38.44          |
|               | 0:30:00 | 0.00       | 0.00       | 24.71        | 146.60       | 62.28         | 61.82         | 77.38         | 267.93         | 131.08         |
|               | 0:35:00 | 0.00       | 0.00       | 28.36        | 148.36       | 67.13         | 92.57         | 113.75        | 302.41         | 190.37         |
|               | 0:40:00 | 0.00       | 0.00       | 27.34        | 143.02       | 62.88         | 103.09        | 125.40        | 309.03         | 207.06         |
|               | 0:45:00 | 0.00       | 0.00       | 24.41        | 137.31       | 57.36         | 98.90         | 119.90        | 302.18         | 202.23         |
|               | 0:50:00 | 0.00       | 0.00       | 21.63        | 130.82       | 51.33         | 93.57         | 113.46        | 289.65         | 191.70         |
|               | 0:55:00 | 0.00       | 0.00       | 19.31        | 124.44       | 46.31         | 84.26         | 102.47        | 276.21         | 177.33         |
|               | 1:00:00 | 0.00       | 0.00       | 17.53        | 119.29       | 42.27         | 75.99         | 92.91         | 264.30         | 165.28         |
|               | 1:05:00 | 0.00       | 0.00       | 15.91        | 115.25       | 38.56         | 68.79         | 84.53         | 247.33         | 155.08         |
|               | 1:10:00 | 0.00       | 0.00       | 13.92        | 110.41       | 34.92         | 60.71         | 74.92         | 229.27         | 137.88         |
|               | 1:15:00 | 0.00       | 0.00       | 11.89        | 104.32       | 31.47         | 52.43         | 65.01         | 209.03         | 119.21         |
|               | 1:20:00 | 0.00       | 0.00       | 10.24        | 97.99        | 28.23         | 44.33         | 55.03         | 188.58         | 100.29         |
|               | 1:25:00 | 0.00       | 0.00       | 9.11         | 92.36        | 25.24         | 38.41         | 47.78         | 169.75         | 85.97          |
|               | 1:30:00 | 0.00       | 0.00       | 8.22         | 87.52        | 22.52         | 33.51         | 41.71         | 153.19         | 74.48          |
|               | 1:35:00 | 0.00       | 0.00       | 7.43         | 82.28        | 20.08         | 29.37         | 36.58         | 139.26         | 64.85          |
|               | 1:40:00 | 0.00       | 0.00       | 6.68         | 77.25        | 17.85         | 25.63         | 31.93         | 128.04         | 56.24          |
|               | 1:45:00 | 0.00       | 0.00       | 5.94         | 72.85        | 15.74         | 22.26         | 27.74         | 118.85         | 48.37          |
|               | 1:50:00 | 0.00       | 0.00       | 5.22         | 68.94        | 13.70         | 19.04         | 23.75         | 111.03         | 40.97          |
|               | 1:55:00 | 0.00       | 0.00       | 4.38         | 64.94        | 11.58         | 15.95         | 19.92         | 104.07         | 34.02          |
|               | 2:00:00 | 0.00       | 0.00       | 3.55         | 58.11        | 9.29          | 13.00         | 16.27         | 93.16          | 27.58          |
|               | 2:05:00 | 0.00       | 0.00       | 2.64         | 50.37        | 6.91          | 9.71          | 12.19         | 80.96          | 20.65          |
|               | 2:10:00 | 0.00       | 0.00       | 1.92         | 43.04        | 5.27          | 6.60          | 8.35          | 69.34          | 14.54          |
|               | 2:15:00 | 0.00       | 0.00       | 1.47         | 36.34        | 4.21          | 4.68          | 6.04          | 58.65          | 10.55          |
|               | 2:20:00 | 0.00       | 0.00       | 1.17         | 30.41        | 3.40          | 3.43          | 4.48          | 48.94          | 7.79           |
|               | 2:25:00 | 0.00       | 0.00       | 0.94         | 25.39        | 2.74          | 2.56          | 3.37          | 40.27          | 5.71           |
|               | 2:30:00 | 0.00       | 0.00       | 0.75         | 21.07        | 2.19          | 1.91          | 2.52          | 32.86          | 4.14           |
|               | 2:35:00 | 0.00       | 0.00       | 0.60         | 17.30        | 1.72          | 1.45          | 1.92          | 26.42          | 2.94           |
|               | 2:40:00 | 0.00       | 0.00       | 0.47         | 14.29        | 1.33          | 1.08          | 1.43          | 20.94          | 2.04           |
|               | 2:45:00 | 0.00       | 0.00       | 0.37         | 11.86        | 1.02          | 0.80          | 1.06          | 16.66          | 1.43           |
|               | 2:50:00 | 0.00       | 0.00       | 0.30         | 9.83         | 0.77          | 0.62          | 0.81          | 13.31          | 1.09           |
|               | 2:55:00 | 0.00       | 0.00       | 0.24         | 8.11         | 0.59          | 0.48          | 0.63          | 10.64          | 0.85           |
|               | 3:00:00 | 0.00       | 0.00       | 0.19         | 6.68         | 0.45          | 0.37          | 0.49          | 8.52           | 0.68           |
|               | 3:05:00 | 0.00       | 0.00       | 0.14         | 5.47         | 0.34          | 0.29          | 0.37          | 6.87           | 0.53           |
|               | 3:10:00 | 0.00       | 0.00       | 0.11         | 4.47         | 0.25          | 0.21          | 0.28          | 5.54           | 0.39           |
|               | 3:15:00 | 0.00       | 0.00       | 0.07         | 3.61         | 0.17          | 0.15          | 0.20          | 4.47           | 0.28           |
|               | 3:20:00 | 0.00       | 0.00       | 0.05         | 2.87         | 0.11          | 0.10          | 0.13          | 3.60           | 0.18           |
|               | 3:25:00 | 0.00       | 0.00       | 0.03         | 2.23         | 0.06          | 0.06          | 0.08          | 2.85           | 0.11           |
|               | 3:30:00 | 0.00       | 0.00       | 0.01         | 1.69         | 0.03          | 0.03          | 0.04          | 2.21           | 0.05           |
|               | 3:35:00 | 0.00       | 0.00       | 0.00         | 1.25         | 0.01          | 0.01          | 0.01          | 1.67           | 0.02           |
|               | 3:40:00 | 0.00       | 0.00       | 0.00         | 0.88         | 0.00          | 0.00          | 0.00          | 1.20           | 0.00           |
|               | 3:45:00 | 0.00       | 0.00       | 0.00         | 0.58         | 0.00          | 0.00          | 0.00          | 0.82           | 0.00           |
|               | 3:50:00 | 0.00       | 0.00       | 0.00         | 0.36         | 0.00          | 0.00          | 0.00          | 0.52           | 0.00           |
|               | 3:55:00 | 0.00       | 0.00       | 0.00         | 0.21         | 0.00          | 0.00          | 0.00          | 0.29           | 0.00           |
|               | 4:00:00 | 0.00       | 0.00       | 0.00         | 0.11         | 0.00          | 0.00          | 0.00          | 0.16           | 0.00           |
|               | 4:05:00 | 0.00       | 0.00       | 0.00         | 0.04         | 0.00          | 0.00          | 0.00          | 0.06           | 0.00           |
|               | 4:10:00 | 0.00       | 0.00       | 0.00         | 0.01         | 0.00          | 0.00          | 0.00          | 0.01           | 0.00           |
|               | 4:15:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:20:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:25:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:30:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:35:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:40:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:45:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:50:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:55:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:05:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:10:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:15:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:20:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:25:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:30:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:35:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:40:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:45:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:50:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:55:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 6:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |

## DETENTION BASIN OUTLET STRUCTURE DESIGN

*MHFD-Detention, Version 4.04 (February 2021)*

### Summary Stage-Area-Volume-Discharge Relationships

The user can create a summary S-A-V-D by entering the desired stage increments and the remainder of the table will populate automatically.

The user should graphically compare the summary S-A-V-D table to the full S-A-V-D table in the chart to confirm it captures all key transition points.

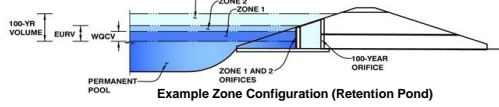
[illegible]

# DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.04 (February 2021)

Project: **Flying Horse North Master Drainage Plan**

Basin ID: **Pond 10**



Example Zone Configuration (Retention Pond)

## Watershed Information

|   |            |         |
|---|------------|---------|
| Selected BMP Type =                     | <b>EDB</b> |         |
| Watershed Area =                        | 21.96      | acres   |
| Watershed Length =                      | 1,715      | ft      |
| Watershed Length to Centroid =          | 1,346      | ft      |
| Watershed Slope =                       | 0.056      | ft/ft   |
| Watershed Imperviousness =              | 10.00%     | percent |
| Percentage Hydrologic Soil Group A =    | 0.0%       | percent |
| Percentage Hydrologic Soil Group B =    | 100.0%     | percent |
| Percentage Hydrologic Soil Groups C/D = | 0.0%       | percent |
| Target WQCV Drain Time =                | 40.0       | hours   |
| Location for 1-hr Rainfall Depths =     | User Input |         |

After providing required inputs above including 1-hour rainfall depths, click "Run CUHP" to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

|  |       |           |
|--|-------|-----------|
| Water Quality Capture Volume (WQCV) =  | 0.123 | acre-feet |
| Excess Urban Runoff Volume (EURV) =    | 0.206 | acre-feet |
| 2-yr Runoff Volume (P1 = 1.19 in.) =   | 0.293 | acre-feet |
| 5-yr Runoff Volume (P1 = 1.5 in.) =    | 0.647 | acre-feet |
| 10-yr Runoff Volume (P1 = 1.75 in.) =  | 1.000 | acre-feet |
| 25-yr Runoff Volume (P1 = 2 in.) =     | 1.630 | acre-feet |
| 50-yr Runoff Volume (P1 = 2.25 in.) =  | 2.059 | acre-feet |
| 100-yr Runoff Volume (P1 = 2.52 in.) = | 2.677 | acre-feet |
| 500-yr Runoff Volume (P1 = 3.14 in.) = | 3.804 | acre-feet |
| Approximate 2-yr Detention Volume =    | 0.132 | acre-feet |
| Approximate 5-yr Detention Volume =    | 0.207 | acre-feet |
| Approximate 10-yr Detention Volume =   | 0.429 | acre-feet |
| Approximate 25-yr Detention Volume =   | 0.599 | acre-feet |
| Approximate 50-yr Detention Volume =   | 0.627 | acre-feet |
| Approximate 100-yr Detention Volume =  | 0.810 | acre-feet |

## Optional User Overrides

|  |      |           |
|--|------|-----------|
|  |      | acre-feet |
|  |      | acre-feet |
|  | 1.19 | inches    |
|  | 1.50 | inches    |
|  | 1.75 | inches    |
|  | 2.00 | inches    |
|  | 2.25 | inches    |
|  | 2.52 | inches    |
|  |      | inches    |

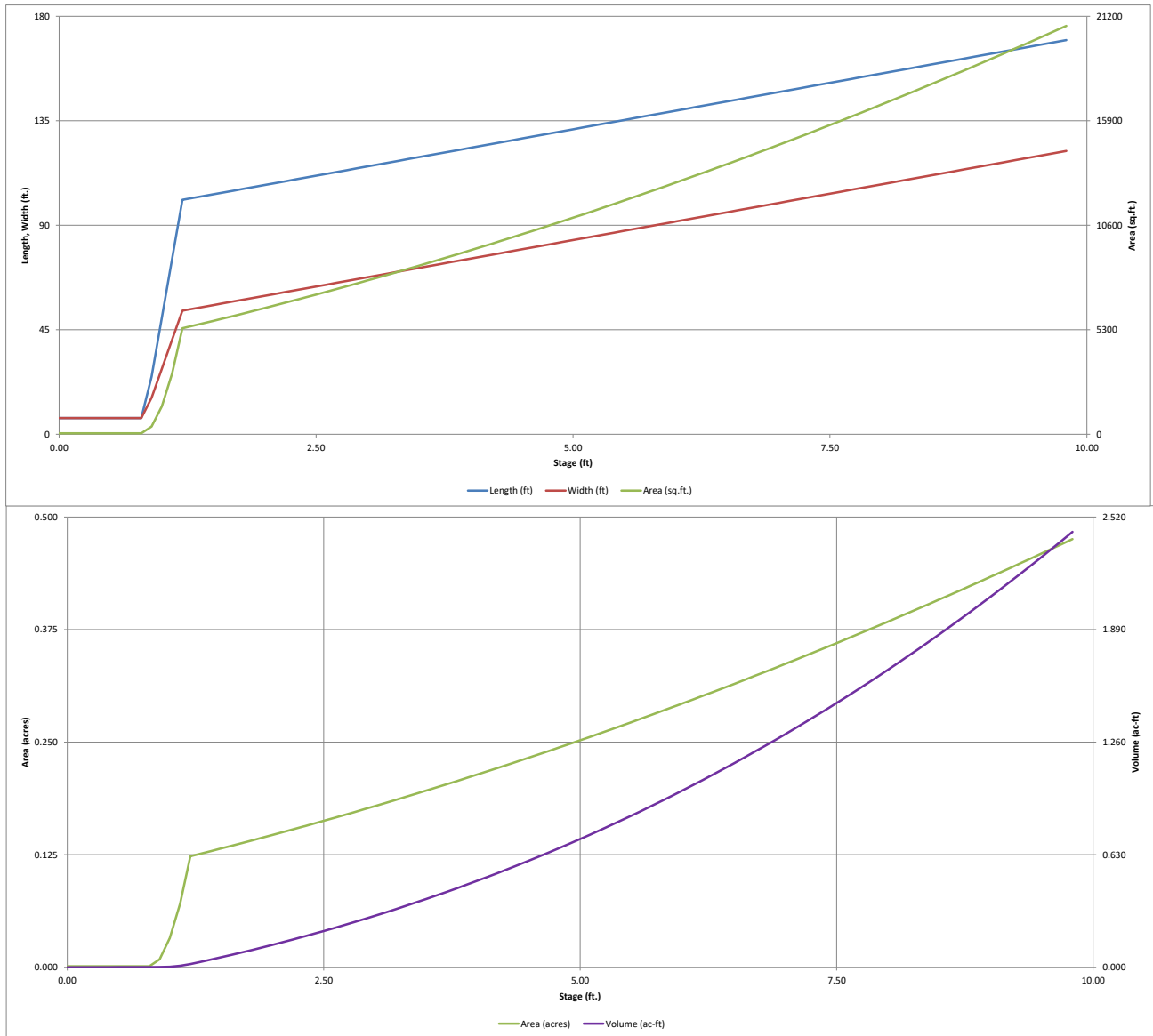
## Define Zones and Basin Geometry

|   |              |                 |
|---|--------------|-----------------|
| Zone 1 Volume (WQCV) =                                  | 0.123        | acre-feet       |
| Zone 2 Volume (5-year - Zone 1) =                       | 0.084        | acre-feet       |
| Zone 3 Volume (100-year - Zones 1 & 2) =                | 0.603        | acre-feet       |
| Total Detention Basin Volume =                          | 0.810        | acre-feet       |
| Initial Surge Volume (ISV) =                            | 16           | ft <sup>3</sup> |
| Initial Surge Depth (ISD) =                             | 0.33         | ft              |
| Total Available Detention Depth (H <sub>total</sub> ) = | 6.00         | ft              |
| Depth of Trickle Channel (H <sub>TC</sub> ) =           | 0.50         | ft              |
| Slope of Trickle Channel (S <sub>TC</sub> ) =           | 0.004        | ft/ft           |
| Slopes of Main Basin Sides (S <sub>main</sub> ) =       | 4            | H:V             |
| Basin Length-to-Width Ratio (R <sub>L/W</sub> ) =       | 2            |                 |
| Initial Surge Area (A <sub>ISV</sub> ) =                | 49           | ft <sup>2</sup> |
| Surcharge Volume Length (L <sub>ISV</sub> ) =           | 7.0          | ft              |
| Surcharge Volume Width (W <sub>ISV</sub> ) =            | 7.0          | ft              |
| Depth of Basin Floor (H <sub>FLOOR</sub> ) =            | 0.37         | ft              |
| Length of Basin Floor (L <sub>FLOOR</sub> ) =           | 100.9        | ft              |
| Width of Basin Floor (W <sub>FLOOR</sub> ) =            | 53.2         | ft              |
| Area of Basin Floor (A <sub>FLOOR</sub> ) =             | 5,372        | ft <sup>2</sup> |
| Volume of Basin Floor (V <sub>FLOOR</sub> ) =           | 732          | ft <sup>3</sup> |
| Depth of Main Basin (H <sub>MAIN</sub> ) =              | 4.80         | ft              |
| Length of Main Basin (L <sub>MAIN</sub> ) =             | 139.3        | ft              |
| Width of Main Basin (W <sub>MAIN</sub> ) =              | 91.6         | ft              |
| Area of Main Basin (A <sub>MAIN</sub> ) =               | 12,767       | ft <sup>2</sup> |
| Volume of Main Basin (V <sub>MAIN</sub> ) =             | 42,274       | ft <sup>3</sup> |
| Calculated Total Basin Volume (V <sub>total</sub> ) =   | <b>0.988</b> | acre-feet       |

| Depth Increment =           | 0.10       | ft                           |             |            |                         |   |             |                           |                |
|-----------------------------|------------|------------------------------|-------------|------------|-------------------------|---|-------------|---------------------------|----------------|
| Stage - Storage Description | Stage (ft) | Optional Override Stage (ft) | Length (ft) | Width (ft) | Area (ft <sup>2</sup> ) | Optional Override Area (ft <sup>2</sup> ) | Area (acre) | Volume (ft <sup>3</sup> ) | Volume (ac-ft) |
| Top of Micropool            | 0.00       |                              | 7.0         | 7.0        | 49                      |   | 0.001       |                           |                |
| ISV                         | 0.33       |                              | 7.0         | 7.0        | 49                      |   | 0.001       | 16                        | 0.000          |
|                             | 0.40       |                              | 7.0         | 7.0        | 49                      |   | 0.001       | 19                        | 0.000          |
|                             | 0.50       |                              | 7.0         | 7.0        | 49                      |   | 0.001       | 24                        | 0.001          |
|                             | 0.60       |                              | 7.0         | 7.0        | 49                      |   | 0.001       | 29                        | 0.001          |
|                             | 0.70       |                              | 7.0         | 7.0        | 49                      |   | 0.001       | 34                        | 0.001          |
|                             | 0.80       |                              | 7.0         | 7.0        | 49                      |   | 0.001       | 39                        | 0.001          |
|                             | 0.90       |                              | 24.7        | 15.7       | 389                     |   | 0.009       | 54                        | 0.001          |
|                             | 1.00       |                              | 50.1        | 28.2       | 1,415                   |   | 0.032       | 139                       | 0.003          |
|                             | 1.10       |                              | 75.5        | 40.7       | 3,076                   |   | 0.071       | 358                       | 0.008          |
| Floor                       | 1.20       |                              | 100.9       | 53.2       | 5,372                   |   | 0.123       | 775                       | 0.018          |
|                             | 1.30       |                              | 101.7       | 54.0       | 5,496                   |   | 0.126       | 1,319                     | 0.030          |
|                             | 1.40       |                              | 102.5       | 54.8       | 5,622                   |   | 0.129       | 1,874                     | 0.043          |
|                             | 1.50       |                              | 103.3       | 55.6       | 5,748                   |   | 0.132       | 2,443                     | 0.056          |
|                             | 1.60       |                              | 104.1       | 56.4       | 5,876                   |   | 0.135       | 3,024                     | 0.069          |
|                             | 1.70       |                              | 104.9       | 57.2       | 6,005                   |   | 0.138       | 3,618                     | 0.083          |
|                             | 1.80       |                              | 105.7       | 58.0       | 6,135                   |   | 0.141       | 4,225                     | 0.097          |
|                             | 1.90       |                              | 106.5       | 58.8       | 6,267                   |   | 0.144       | 4,845                     | 0.111          |
|                             | 2.00       |                              | 107.3       | 59.6       | 6,400                   |   | 0.147       | 5,479                     | 0.126          |
|                             | 2.10       |                              | 108.1       | 60.4       | 6,534                   |   | 0.150       | 6,125                     | 0.141          |
|                             | 2.20       |                              | 108.9       | 61.2       | 6,670                   |   | 0.153       | 6,785                     | 0.156          |
|                             | 2.30       |                              | 109.7       | 62.0       | 6,806                   |   | 0.156       | 7,459                     | 0.171          |
| Zone 1 (WQCV)               | 2.32       |                              | 109.9       | 62.2       | 6,834                   |   | 0.157       | 7,596                     | 0.174          |
|                             | 2.40       |                              | 110.5       | 62.8       | 6,945                   |   | 0.159       | 8,147                     | 0.187          |
|                             | 2.50       |                              | 111.3       | 63.6       | 7,084                   |   | 0.163       | 8,848                     | 0.203          |
|                             | 2.60       |                              | 112.1       | 64.4       | 7,224                   |   | 0.166       | 9,564                     | 0.220          |
|                             | 2.70       |                              | 112.9       | 65.2       | 7,366                   |   | 0.169       | 10,293                    | 0.236          |
|                             | 2.80       |                              | 113.7       | 66.0       | 7,510                   |   | 0.172       | 11,037                    | 0.253          |
| Zone 2 (5-year)             | 2.90       |                              | 114.5       | 66.8       | 7,654                   |   | 0.176       | 11,795                    | 0.271          |
|                             | 3.00       |                              | 115.3       | 67.6       | 7,800                   |   | 0.179       | 12,568                    | 0.289          |
|                             | 3.10       |                              | 116.1       | 68.4       | 7,947                   |   | 0.182       | 13,355                    | 0.307          |
|                             | 3.20       |                              | 116.9       | 69.2       | 8,095                   |   | 0.186       | 14,157                    | 0.325          |
|                             | 3.30       |                              | 117.7       | 70.0       | 8,245                   |   | 0.189       | 14,974                    | 0.344          |
|                             | 3.40       |                              | 118.5       | 70.8       | 8,395                   |   | 0.193       | 15,806                    | 0.363          |
|                             | 3.50       |                              | 119.3       | 71.6       | 8,548                   |   | 0.196       | 16,653                    | 0.382          |
|                             | 3.60       |                              | 120.1       | 72.4       | 8,701                   |   | 0.200       | 17,516                    | 0.402          |
|                             | 3.70       |                              | 120.9       | 73.2       | 8,856                   |   | 0.203       | 18,393                    | 0.422          |
|                             | 3.80       |                              | 121.7       | 74.0       | 9,012                   |   | 0.207       | 19,287                    | 0.443          |
|                             | 3.90       |                              | 122.5       | 74.8       | 9,169                   |   | 0.210       | 20,196                    | 0.464          |
|                             | 4.00       |                              | 123.3       | 75.6       | 9,327                   |   | 0.214       | 21,121                    | 0.485          |
|                             | 4.10       |                              | 124.1       | 76.4       | 9,487                   |   | 0.218       | 22,061                    | 0.506          |
|                             | 4.20       |                              | 124.9       | 77.2       | 9,648                   |   | 0.221       | 23,018                    | 0.528          |
|                             | 4.30       |                              | 125.7       | 78.0       | 9,811                   |   | 0.225       | 23,991                    | 0.551          |
|                             | 4.40       |                              | 126.5       | 78.8       | 9,974                   |   | 0.229       | 24,980                    | 0.573          |
|                             | 4.50       |                              | 127.3       | 79.6       | 10,139                  |   | 0.233       | 25,986                    | 0.597          |
|                             | 4.60       |                              | 128.1       | 80.4       | 10,306                  |   | 0.237       | 27,008                    | 0.620          |
|                             | 4.70       |                              | 128.9       | 81.2       | 10,473                  |   | 0.240       | 28,047                    | 0.644          |
|                             | 4.80       |                              | 129.7       | 82.0       | 10,642                  |   | 0.244       | 29,103                    | 0.668          |
|                             | 4.90       |                              | 130.5       | 82.8       | 10,812                  |   | 0.248       | 30,176                    | 0.693          |
|                             | 5.00       |                              | 131.3       | 83.6       | 10,983                  |   | 0.252       | 31,265                    | 0.718          |
|                             | 5.10       |                              | 132.1       | 84.4       | 11,156                  |   | 0.256       | 32,372                    | 0.743          |
|                             | 5.20       |                              | 132.9       | 85.2       | 11,330                  |   | 0.260       | 33,497                    | 0.769          |
|                             | 5.30       |                              | 133.7       | 86.0       | 11,505                  |   | 0.264       | 34,638                    | 0.795          |
|                             | 5.40       |                              | 134.5       | 86.8       | 11,681                  |   | 0.268       | 35,798                    | 0.822          |
|                             | 5.50       |                              | 135.3       | 87.6       | 11,859                  |   | 0.272       | 36,975                    | 0.849          |
|                             | 5.60       |                              | 136.1       | 88.4       | 12,038                  |   | 0.276       | 38,169                    | 0.876          |
|                             | 5.70       |                              | 136.9       | 89.2       | 12,218                  |   | 0.280       | 39,382                    | 0.904          |
|                             | 5.80       |                              | 137.7       | 90.0       | 12,400                  |   | 0.285       | 40,613                    | 0.932          |
| Zone 3 (100-year)           | 5.90       |                              | 138.5       | 90.8       | 12,583                  |   | 0.289       | 41,862                    | 0.961          |
|                             | 5.98       |                              | 139.2       | 91.5       | 12,730                  |   | 0.292       | 42,875                    | 0.984          |
|                             | 6.00       |                              | 139.3       | 91.6       | 12,767                  |   | 0.293       | 43,130                    | 0.990          |
|                             | 6.10       |                              | 140.1       | 92.4       | 12,952                  |   | 0.297       | 44,416                    | 1.020          |
|                             | 6.20       |                              | 140.9       | 93.2       | 13,139                  |   | 0.302       | 45,720                    | 1.050          |
|                             | 6.30       |                              | 141.7       | 94.0       | 13,327                  |   | 0.306       | 47,043                    | 1.080          |
|                             | 6.40       |                              | 142.5       | 94.8       | 13,516                  |   | 0.310       | 48,386                    | 1.111          |
|                             | 6.50       |                              | 143.3       | 95.6       | 13,707                  |   | 0.315       | 49,747                    | 1.142          |
|                             | 6.60       |                              | 144.1       | 96.4       | 13,899                  |   | 0.319       | 51,127                    | 1.174          |
|                             | 6.70       |                              | 144.9       | 97.2       | 14,092                  |   | 0.324       | 52,527                    | 1.206          |
|                             | 6.80       |                              | 145.7       | 98.0       | 14,286                  |   | 0.328       | 53,945                    | 1.238          |
|                             | 6.90       |                              | 146.5       | 98.8       | 14,482                  |   | 0.332       | 55,384                    | 1.271          |
|                             | 7.00       |                              | 147.3       | 99.6       | 14,679                  |   | 0.337       | 56,842                    | 1.305          |
|                             | 7.10       |                              | 148.1       | 100.4      | 14,877                  |   | 0.342       | 58,320                    | 1.339          |
|                             | 7.20       |                              | 148.9       | 101.2      | 15,076                  |   | 0.346       | 59,817                    | 1.373          |
|                             | 7.30       |                              | 149.7       | 102.0      | 15,277                  |   | 0.351       | 61,335                    | 1.408          |
|                             | 7.40       |                              | 150.5       | 102.8      | 15,479                  |   | 0.355       | 62,873                    | 1.443          |
|                             | 7.50       |                              | 151.3       | 103.6      | 15,683                  |   | 0.360       | 64,431                    | 1.479          |
|                             | 7.60       |                              | 152.1       | 104.4      | 15,887                  |   | 0.365       | 66,009                    | 1.515          |
|                             | 7.70       |                              | 152.9       | 105.2      | 16,093                  |   | 0.369       | 67,608                    | 1.552          |
|                             | 7.80       |                              | 153.7       | 106.0      | 16,300                  |   | 0.374       | 69,228                    | 1.589          |
|                             | 7.90       |                              | 154.5       | 106.8      | 16,509                  |   | 0.379       | 70,868                    | 1.627          |
|                             | 8.00       |                              | 155.3       | 107.6      | 16,718                  |   | 0.384       | 72,530                    | 1.665          |
|                             | 8.10       |                              | 156.1       | 108.4      | 16,929                  |   | 0.389       | 74,212                    | 1.704          |
|                             | 8.20       |                              | 156.9       | 109.2      | 17,142                  |   | 0.394       | 75,916                    | 1.743          |
|                             | 8.30       |                              | 157.7       | 110.0      | 17,355                  |   | 0.398       | 77,640                    | 1.782          |
|                             | 8.40       |                              | 158.5       | 110.8      | 17,570                  |   | 0.403       | 79,387                    | 1.822          |
|                             | 8.50       |                              | 159.3       | 111.6      | 17,786                  |   | 0.408       | 81,154                    | 1.863          |
|                             | 8.60       |                              | 160.1       | 112.4      | 18,004                  |   | 0.413       | 82,944                    | 1.904          |
|                             | 8.70       |                              | 160.9       | 113.2      | 18,222                  |   | 0.418       | 84,755                    | 1.946          |
|                             | 8.80       |                              | 161.7       | 114.0      | 18,442                  |   | 0.423       | 86,588                    | 1.988          |
|                             | 8.90       |                              | 162.5       | 114.8      | 18,664                  |   | 0.428       | 88,444                    | 2.030          |
|                             | 9.00       |                              | 163.3       | 115.6      | 18,886                  |   | 0.434       | 90,321                    | 2.073          |
|                             | 9.10       |                              | 164.1       | 116.4      | 19,110                  |   | 0.439       | 92,221                    | 2.117          |
|                             | 9.20       |                              | 164.9       | 117.2      | 19,335                  |   | 0.444       | 94,143                    | 2.161          |
|                             | 9.30       |                              | 165.7       | 118.0      | 19,561                  |   | 0.449       | 96,088                    | 2.206          |
|                             | 9.40       |                              | 166.5       | 118.8      | 19,789                  |   | 0.454       | 98,056                    | 2.251          |
|                             | 9.50       |                              | 167.3       | 119.6      | 20,018                  |   | 0.460       | 100,046                   | 2.297          |
|                             | 9.60       |                              | 168.1       | 120.4      | 20,248                  |   | 0.465       | 102,059                   | 2.343          |
|                             | 9.70       |                              | 168.9       | 121.2      | 20,480                  |   | 0.470       | 104,096                   | 2.390          |
|                             | 9.80       |                              | 169.7       | 122.0      | 20,712                  |   | 0.475       | 106,155                   | 2.437          |

# DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.04 (February 2021)

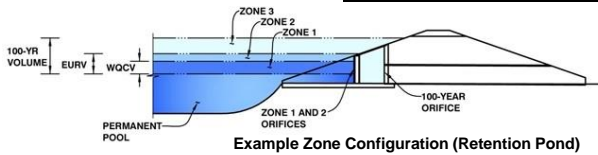


# DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.04 (February 2021)

Project: Flying Horse North Master Drainage Plan

Basin ID: Pond 10



Example Zone Configuration (Retention Pond)

|                   | Estimated Stage (ft) | Estimated Volume (ac-ft) | Outlet Type          |
|-------------------|----------------------|--------------------------|----------------------|
| Zone 1 (WQCV)     | 1.98                 | 0.123                    | Orifice Plate        |
| Zone 2 (5-year)   | 2.53                 | 0.084                    | Circular Orifice     |
| Zone 3 (100-year) | 5.36                 | 0.603                    | Weir&Pipe (Restrict) |
| Total (all zones) |                      | 0.810                    |                      |

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth = N/A ft (distance below the filtration media surface)  
Underdrain Orifice Diameter = N/A inches

Calculated Parameters for Underdrain  
Underdrain Orifice Area = N/A ft<sup>2</sup>  
Underdrain Orifice Centroid = N/A feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice = 0.00 ft (relative to basin bottom at Stage = 0 ft)  
Depth at top of Zone using Orifice Plate = 1.98 ft (relative to basin bottom at Stage = 0 ft)  
Orifice Plate: Orifice Vertical Spacing = 8.80 inches  
Orifice Plate: Orifice Area per Row = 0.45 sq. inches (diameter = 3/4 inch)

Calculated Parameters for Plate  
WQ Orifice Area per Row = 3.125E-03 ft<sup>2</sup>  
Elliptical Half-Width = N/A feet  
Elliptical Slot Centroid = N/A feet  
Elliptical Slot Area = N/A ft<sup>2</sup>

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

|                                | Row 1 (required) | Row 2 (optional) | Row 3 (optional) | Row 4 (optional) | Row 5 (optional) | Row 6 (optional) | Row 7 (optional) | Row 8 (optional) |
|--------------------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|
| Stage of Orifice Centroid (ft) | 0.00             | 0.66             | 1.32             |                  |                  |                  |                  |                  |
| Orifice Area (sq. inches)      | 0.45             | 0.45             | 0.45             |                  |                  |                  |                  |                  |

|                                | Row 9 (optional) | Row 10 (optional) | Row 11 (optional) | Row 12 (optional) | Row 13 (optional) | Row 14 (optional) | Row 15 (optional) | Row 16 (optional) |
|--------------------------------|------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| Stage of Orifice Centroid (ft) |                  |                   |                   |                   |                   |                   |                   |                   |
| Orifice Area (sq. inches)      |                  |                   |                   |                   |                   |                   |                   |                   |

User Input: Vertical Orifice (Circular or Rectangular)

Invert of Vertical Orifice = 1.98 ft (relative to basin bottom at Stage = 0 ft)  
Depth at top of Zone using Vertical Orifice = 2.53 ft (relative to basin bottom at Stage = 0 ft)  
Vertical Orifice Diameter = 18.00 inches

Calculated Parameters for Vertical Orifice  
Zone 2 Circular Not Selected  
Vertical Orifice Area = 1.77 ft<sup>2</sup>  
Vertical Orifice Centroid = 0.75 feet

User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe))

Overflow Weir Front Edge Height, H<sub>o</sub> = 4.70 ft (relative to basin bottom at Stage = 0 ft)  
Overflow Weir Front Edge Length = 3.00 feet  
Overflow Weir Grate Slope = 0.00 H:V  
Horiz. Length of Weir Sides = 3.00 feet  
Overflow Grate Type = Type C Grate  
Debris Clogging % = 50%

Calculated Parameters for Overflow Weir  
Zone 3 Weir Not Selected  
Height of Grate Upper Edge, H<sub>u</sub> = 4.70 feet  
Overflow Weir Slope Length = 3.00 feet  
Grate Open Area / 100-yr Orifice Area = 1.55  
Overflow Grate Open Area w/o Debris = 6.26 ft<sup>2</sup>  
Overflow Grate Open Area w/ Debris = 3.13 ft<sup>2</sup>

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

Depth to Invert of Outlet Pipe = 1.00 ft (distance below basin bottom at Stage = 0 ft)  
Outlet Pipe Diameter = 36.00 inches  
Restrictor Plate Height Above Pipe Invert = 20.00 inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate  
Zone 3 Restrictor Not Selected  
Outlet Orifice Area = 4.03 ft<sup>2</sup>  
Outlet Orifice Centroid = 0.95 feet  
Half-Central Angle of Restrictor Plate on Pipe = 1.68 radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage = 6.70 ft (relative to basin bottom at Stage = 0 ft)  
Spillway Crest Length = 26.00 feet  
Spillway End Slopes = 4.00 H:V  
Freeboard above Max Water Surface = 1.00 feet

Calculated Parameters for Spillway  
Spillway Design Flow Depth = 0.94 feet  
Stage at Top of Freeboard = 8.64 feet  
Basin Area at Top of Freeboard = 0.42 acres  
Basin Volume at Top of Freeboard = 1.92 acre-ft

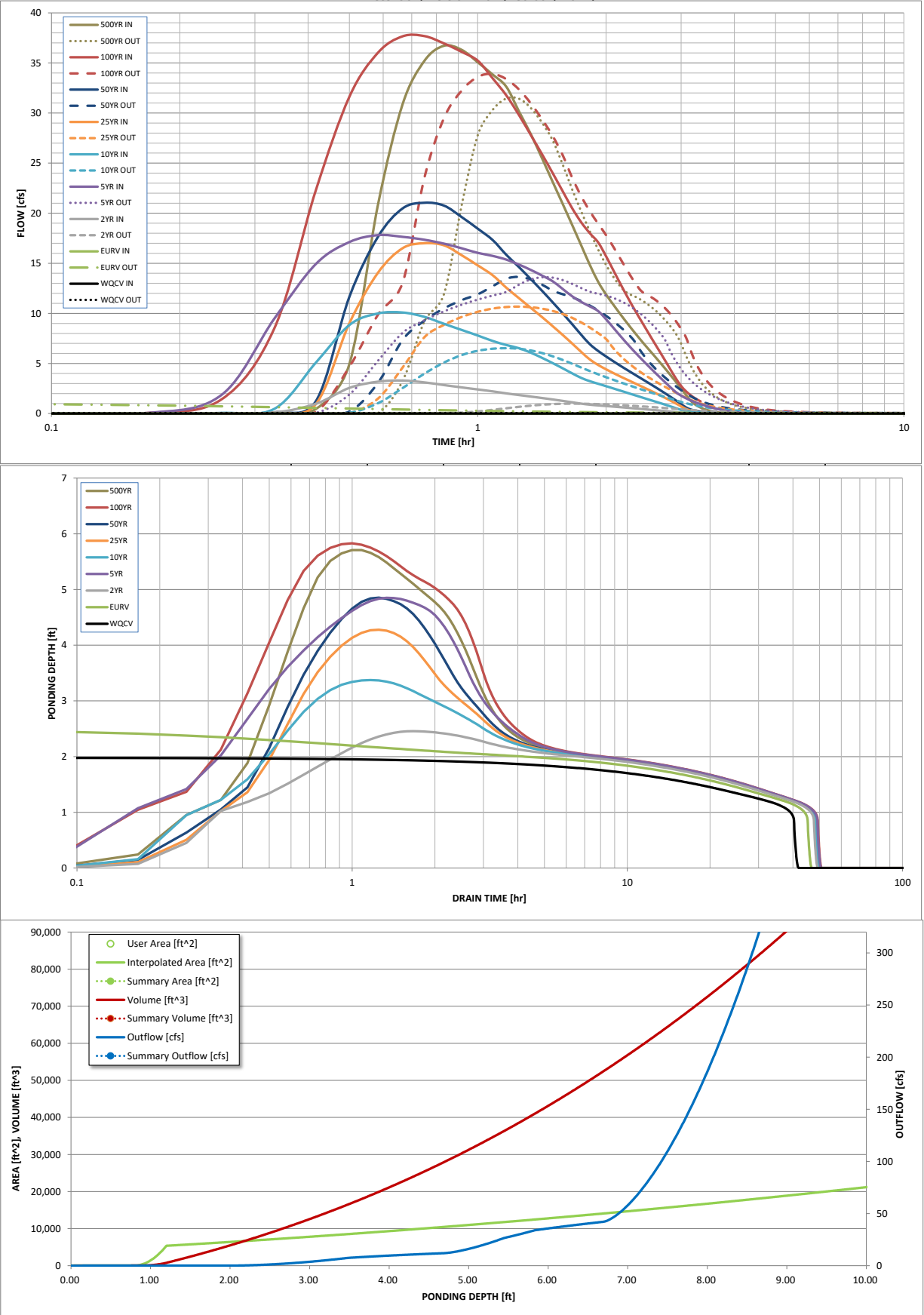
## Routed Hydrograph Results

The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).

|  | WQCV               | EURV               | 2 Year             | 5 Year          | 10 Year            | 25 Year            | 50 Year         | 100 Year        | 500 Year        |
|--|--------------------|--------------------|--------------------|-----------------|--------------------|--------------------|-----------------|-----------------|-----------------|
| Design Storm Return Period =                       | N/A                | N/A                | 1.19               | 1.50            | 1.75               | 2.00               | 2.25            | 2.52            | 3.14            |
| One-Hour Rainfall Depth (in) =                     | 0.123              | 0.206              | 0.293              | 0.647           | 1.000              | 1.630              | 2.059           | 2.677           | 3.804           |
| CUHP Runoff Volume (acre-ft) =                     | N/A                | N/A                | 0.293              | 2.509           | 1.000              | 1.630              | 2.059           | 4.656           | 3.804           |
| User Override Inflow Hydrograph Volume (acre-ft) = | N/A                | N/A                | 2.0                | 5.7             | 8.7                | 15.6               | 19.6            | 25.0            | 35.0            |
| CUHP Predevelopment Peak Q (cfs) =                 | N/A                | N/A                | 0.09               | 0.60            | 0.40               | 0.71               | 0.89            | 1.79            | 1.60            |
| OPTIONAL Override Predevelopment Peak Q (cfs) =    | N/A                | N/A                | 3.3                | 17.8            | 10.1               | 17.0               | 21.0            | 37.7            | 36.7            |
| Predevelopment Unit Peak Flow, q (cfs/acre) =      | N/A                | N/A                | 1.0                | 13.6            | 6.5                | 10.7               | 13.6            | 33.9            | 31.4            |
| Peak Inflow Q (cfs) =                              | N/A                | N/A                | N/A                | 1.0             | 0.8                | 0.7                | 0.7             | 0.9             | 0.9             |
| Peak Outflow Q (cfs) =                             | N/A                | N/A                | N/A                | N/A             | N/A                | N/A                | N/A             | N/A             | N/A             |
| Ratio Peak Outflow to Predevelopment Q =           | N/A                | N/A                | N/A                | N/A             | N/A                | N/A                | N/A             | N/A             | N/A             |
| Structure Controlling Flow =                       | Vertical Orifice 1 | Vertical Orifice 1 | Vertical Orifice 1 | Overflow Weir 1 | Vertical Orifice 1 | Vertical Orifice 1 | Overflow Weir 1 | Overflow Weir 1 | Overflow Weir 1 |
| Max Velocity through Grate 1 (fps) =               | N/A                | N/A                | N/A                | 0.2             | N/A                | N/A                | 0.2             | 3.0             | 2.7             |
| Max Velocity through Grate 2 (fps) =               | N/A                | N/A                | N/A                | N/A             | N/A                | N/A                | N/A             | N/A             | N/A             |
| Time to Drain 97% of Inflow Volume (hours) =       | 39                 | 43                 | 44                 | 21              | 35                 | 29                 | 25              | 6               | 11              |
| Time to Drain 99% of Inflow Volume (hours) =       | 40                 | 45                 | 47                 | 38              | 44                 | 41                 | 40              | 30              | 33              |
| Maximum Ponding Depth (ft) =                       | 1.99               | 2.52               | 2.46               | 4.85            | 3.37               | 4.28               | 4.85            | 5.83            | 5.71            |
| Area at Maximum Ponding Depth (acres) =            | 0.15               | 0.16               | 0.16               | 0.25            | 0.19               | 0.22               | 0.25            | 0.29            | 0.28            |
| Maximum Volume Stored (acre-ft) =                  | 0.124              | 0.206              | 0.195              | 0.680           | 0.357              | 0.544              | 0.680           | 0.938           | 0.904           |

DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.04 (February 2021)



| S-A-V-D Chart Axis Override | X-axis | Left Y-Axis | Right Y-Axis |
|-----------------------------|--------|-------------|--------------|
| minimum bound               |        |             |              |
| maximum bound               |        |             |              |



# DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename: ...[SWMM]Outflow hydrographs\Pond6 OutflowHydrograph.xlsx

## Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

|               | SOURCE  | CUHP       | CUHP       | CUHP         | USER         | CUHP          | CUHP          | CUHP          | USER           | CUHP           |
|---------------|---------|------------|------------|--------------|--------------|---------------|---------------|---------------|----------------|----------------|
| Time Interval | TIME    | WQCV [cfs] | EURV [cfs] | 2 Year [cfs] | 5 Year [cfs] | 10 Year [cfs] | 25 Year [cfs] | 50 Year [cfs] | 100 Year [cfs] | 500 Year [cfs] |
| 5.00 min      | 0:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 0:05:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.01           | 0.00           |
|               | 0:10:00 | 0.00       | 0.00       | 0.00         | 0.05         | 0.00          | 0.00          | 0.00          | 0.05           | 0.01           |
|               | 0:15:00 | 0.00       | 0.00       | 0.03         | 1.83         | 0.06          | 0.04          | 0.05          | 1.39           | 0.07           |
|               | 0:20:00 | 0.00       | 0.00       | 0.11         | 9.48         | 0.47          | 0.11          | 0.13          | 8.51           | 0.45           |
|               | 0:25:00 | 0.00       | 0.00       | 0.97         | 14.91        | 5.06          | 0.92          | 1.21          | 22.24          | 4.95           |
|               | 0:30:00 | 0.00       | 0.00       | 2.57         | 17.12        | 8.84          | 9.02          | 11.66         | 31.63          | 20.83          |
|               | 0:35:00 | 0.00       | 0.00       | 3.18         | 17.81        | 9.99          | 14.05         | 17.64         | 36.02          | 30.90          |
|               | 0:40:00 | 0.00       | 0.00       | 3.29         | 17.64        | 10.09         | 16.51         | 20.48         | 37.66          | 35.22          |
|               | 0:45:00 | 0.00       | 0.00       | 3.11         | 17.35        | 9.65          | 17.00         | 21.04         | 37.68          | 36.71          |
|               | 0:50:00 | 0.00       | 0.00       | 2.84         | 16.96        | 8.96          | 16.79         | 20.76         | 36.95          | 36.31          |
|               | 0:55:00 | 0.00       | 0.00       | 2.61         | 16.50        | 8.35          | 15.81         | 19.62         | 36.11          | 35.07          |
|               | 1:00:00 | 0.00       | 0.00       | 2.41         | 16.04        | 7.79          | 14.79         | 18.46         | 35.23          | 33.85          |
|               | 1:05:00 | 0.00       | 0.00       | 2.22         | 15.74        | 7.25          | 13.82         | 17.33         | 33.48          | 32.63          |
|               | 1:10:00 | 0.00       | 0.00       | 2.01         | 15.37        | 6.84          | 12.57         | 15.85         | 31.77          | 30.15          |
|               | 1:15:00 | 0.00       | 0.00       | 1.85         | 14.87        | 6.52          | 11.51         | 14.62         | 29.79          | 27.86          |
|               | 1:20:00 | 0.00       | 0.00       | 1.70         | 14.33        | 6.07          | 10.54         | 13.40         | 27.78          | 25.45          |
|               | 1:25:00 | 0.00       | 0.00       | 1.55         | 13.77        | 5.55          | 9.62          | 12.24         | 25.86          | 23.11          |
|               | 1:30:00 | 0.00       | 0.00       | 1.41         | 13.20        | 5.03          | 8.72          | 11.10         | 23.99          | 20.91          |
|               | 1:35:00 | 0.00       | 0.00       | 1.26         | 12.43        | 4.51          | 7.84          | 9.99          | 22.18          | 18.81          |
|               | 1:40:00 | 0.00       | 0.00       | 1.12         | 11.70        | 4.01          | 6.98          | 8.91          | 20.48          | 16.77          |
|               | 1:45:00 | 0.00       | 0.00       | 0.99         | 11.14        | 3.55          | 6.14          | 7.85          | 19.08          | 14.83          |
|               | 1:50:00 | 0.00       | 0.00       | 0.88         | 10.69        | 3.23          | 5.39          | 6.92          | 17.99          | 13.15          |
|               | 1:55:00 | 0.00       | 0.00       | 0.81         | 10.23        | 2.98          | 4.85          | 6.25          | 17.09          | 11.89          |
|               | 2:00:00 | 0.00       | 0.00       | 0.75         | 9.42         | 2.74          | 4.42          | 5.71          | 15.71          | 10.84          |
|               | 2:05:00 | 0.00       | 0.00       | 0.69         | 8.54         | 2.50          | 4.03          | 5.21          | 14.26          | 9.85           |
|               | 2:10:00 | 0.00       | 0.00       | 0.63         | 7.69         | 2.27          | 3.68          | 4.74          | 12.87          | 8.95           |
|               | 2:15:00 | 0.00       | 0.00       | 0.57         | 6.90         | 2.05          | 3.35          | 4.31          | 11.57          | 8.10           |
|               | 2:20:00 | 0.00       | 0.00       | 0.52         | 6.17         | 1.84          | 3.03          | 3.90          | 10.38          | 7.31           |
|               | 2:25:00 | 0.00       | 0.00       | 0.46         | 5.49         | 1.64          | 2.73          | 3.51          | 9.28           | 6.57           |
|               | 2:30:00 | 0.00       | 0.00       | 0.41         | 4.85         | 1.44          | 2.44          | 3.13          | 8.23           | 5.87           |
|               | 2:35:00 | 0.00       | 0.00       | 0.35         | 4.25         | 1.25          | 2.15          | 2.76          | 7.22           | 5.19           |
|               | 2:40:00 | 0.00       | 0.00       | 0.30         | 3.68         | 1.07          | 1.86          | 2.39          | 6.26           | 4.51           |
|               | 2:45:00 | 0.00       | 0.00       | 0.25         | 3.14         | 0.89          | 1.58          | 2.03          | 5.32           | 3.84           |
|               | 2:50:00 | 0.00       | 0.00       | 0.20         | 2.62         | 0.72          | 1.29          | 1.67          | 4.39           | 3.17           |
|               | 2:55:00 | 0.00       | 0.00       | 0.15         | 2.14         | 0.54          | 1.01          | 1.31          | 3.51           | 2.50           |
|               | 3:00:00 | 0.00       | 0.00       | 0.10         | 1.79         | 0.37          | 0.73          | 0.95          | 2.76           | 1.84           |
|               | 3:05:00 | 0.00       | 0.00       | 0.06         | 1.52         | 0.25          | 0.45          | 0.61          | 2.21           | 1.24           |
|               | 3:10:00 | 0.00       | 0.00       | 0.04         | 1.29         | 0.19          | 0.28          | 0.40          | 1.80           | 0.85           |
|               | 3:15:00 | 0.00       | 0.00       | 0.03         | 1.10         | 0.15          | 0.18          | 0.27          | 1.47           | 0.60           |
|               | 3:20:00 | 0.00       | 0.00       | 0.02         | 0.94         | 0.12          | 0.12          | 0.19          | 1.22           | 0.42           |
|               | 3:25:00 | 0.00       | 0.00       | 0.02         | 0.79         | 0.10          | 0.08          | 0.13          | 1.00           | 0.28           |
|               | 3:30:00 | 0.00       | 0.00       | 0.01         | 0.66         | 0.07          | 0.05          | 0.09          | 0.81           | 0.19           |
|               | 3:35:00 | 0.00       | 0.00       | 0.01         | 0.54         | 0.06          | 0.04          | 0.06          | 0.66           | 0.12           |
|               | 3:40:00 | 0.00       | 0.00       | 0.01         | 0.44         | 0.04          | 0.02          | 0.04          | 0.54           | 0.07           |
|               | 3:45:00 | 0.00       | 0.00       | 0.01         | 0.35         | 0.03          | 0.02          | 0.03          | 0.44           | 0.05           |
|               | 3:50:00 | 0.00       | 0.00       | 0.01         | 0.27         | 0.02          | 0.01          | 0.02          | 0.35           | 0.04           |
|               | 3:55:00 | 0.00       | 0.00       | 0.00         | 0.21         | 0.02          | 0.01          | 0.02          | 0.27           | 0.03           |
|               | 4:00:00 | 0.00       | 0.00       | 0.00         | 0.15         | 0.01          | 0.01          | 0.01          | 0.21           | 0.02           |
|               | 4:05:00 | 0.00       | 0.00       | 0.00         | 0.11         | 0.01          | 0.00          | 0.01          | 0.15           | 0.02           |
|               | 4:10:00 | 0.00       | 0.00       | 0.00         | 0.07         | 0.01          | 0.00          | 0.01          | 0.10           | 0.01           |
|               | 4:15:00 | 0.00       | 0.00       | 0.00         | 0.04         | 0.00          | 0.00          | 0.00          | 0.06           | 0.01           |
|               | 4:20:00 | 0.00       | 0.00       | 0.00         | 0.02         | 0.00          | 0.00          | 0.00          | 0.03           | 0.01           |
|               | 4:25:00 | 0.00       | 0.00       | 0.00         | 0.01         | 0.00          | 0.00          | 0.00          | 0.01           | 0.00           |
|               | 4:30:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:35:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:40:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:45:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:50:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:55:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:05:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:10:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:15:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:20:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:25:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:30:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:35:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:40:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:45:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:50:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:55:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 6:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |

## DETENTION BASIN OUTLET STRUCTURE DESIGN

*MHFD-Detention, Version 4.04 (February 2021)*

### Summary Stage-Area-Volume-Discharge Relationships

The user can create a summary S-A-V-D by entering the desired stage increments and the remainder of the table will populate automatically.

The user should graphically compare the summary S-A-V-D table to the full S-A-V-D table in the chart to confirm it captures all key transition points.

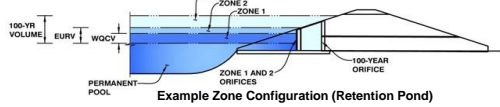
[illegible]

# DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.04 (February 2021)

Project: **Flying Horse North Master Drainage Plan**

Basin ID: **Pond 11**



Example Zone Configuration (Retention Pond)

## Watershed Information

|   |            |         |
|---|------------|---------|
| Selected BMP Type =                     | <b>EDB</b> |         |
| Watershed Area =                        | 79.73      | acres   |
| Watershed Length =                      | 2,715      | ft      |
| Watershed Length to Centroid =          | 1,530      | ft      |
| Watershed Slope =                       | 0.037      | ft/ft   |
| Watershed Imperviousness =              | 28.50%     | percent |
| Percentage Hydrologic Soil Group A =    | 0.0%       | percent |
| Percentage Hydrologic Soil Group B =    | 100.0%     | percent |
| Percentage Hydrologic Soil Groups C/D = | 0.0%       | percent |
| Target WQCV Drain Time =                | 40.0       | hours   |
| Location for 1-hr Rainfall Depths =     | User Input |         |

After providing required inputs above including 1-hour rainfall depths, click "Run CUHP" to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

|  |        |           |
|--|--------|-----------|
| Water Quality Capture Volume (WQCV) =  | 0.975  | acre-feet |
| Excess Urban Runoff Volume (EURV) =    | 2.322  | acre-feet |
| 2-yr Runoff Volume (P1 = 1.19 in.) =   | 2.370  | acre-feet |
| 5-yr Runoff Volume (P1 = 1.5 in.) =    | 3.903  | acre-feet |
| 10-yr Runoff Volume (P1 = 1.75 in.) =  | 5.321  | acre-feet |
| 25-yr Runoff Volume (P1 = 2 in.) =     | 7.486  | acre-feet |
| 50-yr Runoff Volume (P1 = 2.25 in.) =  | 9.112  | acre-feet |
| 100-yr Runoff Volume (P1 = 2.52 in.) = | 11.293 | acre-feet |
| 500-yr Runoff Volume (P1 = 3.39 in.) = | 17.208 | acre-feet |
| Approximate 2-yr Detention Volume =    | 1.653  | acre-feet |
| Approximate 5-yr Detention Volume =    | 2.375  | acre-feet |
| Approximate 10-yr Detention Volume =   | 3.504  | acre-feet |
| Approximate 25-yr Detention Volume =   | 4.095  | acre-feet |
| Approximate 50-yr Detention Volume =   | 4.317  | acre-feet |
| Approximate 100-yr Detention Volume =  | 5.132  | acre-feet |

## Optional User Overrides

|  |      |           |
|--|------|-----------|
|  |      | acre-feet |
|  |      | acre-feet |
|  | 1.19 | inches    |
|  | 1.50 | inches    |
|  | 1.75 | inches    |
|  | 2.00 | inches    |
|  | 2.25 | inches    |
|  | 2.52 | inches    |
|  | 3.39 | inches    |

## Define Zones and Basin Geometry

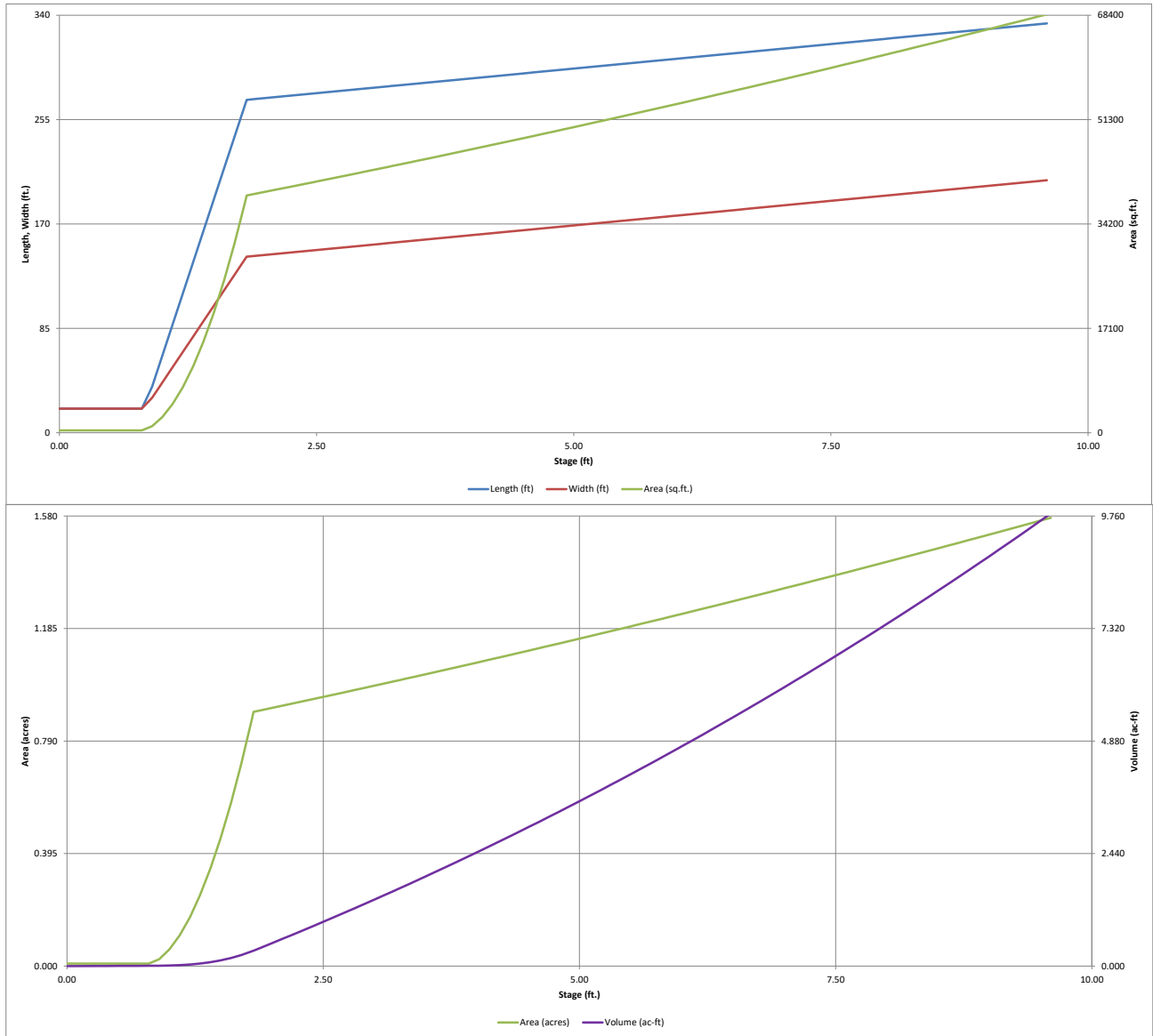
|   |       |                 |
|---|-------|-----------------|
| Zone 1 Volume (WQCV) =                                  | 0.975 | acre-feet       |
| Zone 2 Volume (5-year - Zone 1) =                       | 1.400 | acre-feet       |
| Zone 3 Volume (100-year - Zones 1 & 2) =                | 2.757 | acre-feet       |
| Total Detention Basin Volume =                          | 5.132 | acre-feet       |
| Initial Surge Volume (ISV) =                            | 127   | ft <sup>3</sup> |
| Initial Surge Depth (ISD) =                             | 0.33  | ft              |
| Total Available Detention Depth (H <sub>total</sub> ) = | 6.00  | ft              |
| Depth of Trickle Channel (H <sub>TC</sub> ) =           | 0.50  | ft              |
| Slope of Trickle Channel (S <sub>TC</sub> ) =           | 0.004 | ft/ft           |
| Slopes of Main Basin Sides (S <sub>main</sub> ) =       | 4     | H:V             |
| Basin Length-to-Width Ratio (R <sub>LW</sub> ) =        | 2     |                 |

|   |              |                 |
|---|--------------|-----------------|
| Initial Surge Area (A <sub>ISV</sub> ) =              | 386          | ft <sup>2</sup> |
| Surcharge Volume Length (L <sub>ISV</sub> ) =         | 19.6         | ft              |
| Surcharge Volume Width (W <sub>ISV</sub> ) =          | 19.6         | ft              |
| Depth of Basin Floor (H <sub>FLOOR</sub> ) =          | 0.99         | ft              |
| Length of Basin Floor (L <sub>FLOOR</sub> ) =         | 271.1        | ft              |
| Width of Basin Floor (W <sub>FLOOR</sub> ) =          | 143.4        | ft              |
| Area of Basin Floor (A <sub>FLOOR</sub> ) =           | 38,876       | ft <sup>2</sup> |
| Volume of Basin Floor (V <sub>FLOOR</sub> ) =         | 14,235       | ft <sup>3</sup> |
| Depth of Main Basin (H <sub>MAIN</sub> ) =            | 4.18         | ft              |
| Length of Main Basin (L <sub>MAIN</sub> ) =           | 304.5        | ft              |
| Width of Main Basin (W <sub>MAIN</sub> ) =            | 176.8        | ft              |
| Area of Main Basin (A <sub>MAIN</sub> ) =             | 53,855       | ft <sup>2</sup> |
| Volume of Main Basin (V <sub>MAIN</sub> ) =           | 192,959      | ft <sup>3</sup> |
| Calculated Total Basin Volume (V <sub>total</sub> ) = | <b>4.764</b> | acre-feet       |

| Depth Increment =           | 0.10       | ft                           |             |            |                         |   |             |                           |                |
|-----------------------------|------------|------------------------------|-------------|------------|-------------------------|---|-------------|---------------------------|----------------|
| Stage - Storage Description | Stage (ft) | Optional Override Stage (ft) | Length (ft) | Width (ft) | Area (ft <sup>2</sup> ) | Optional Override Area (ft <sup>2</sup> ) | Area (acre) | Volume (ft <sup>3</sup> ) | Volume (ac-ft) |
| Top of Micropool            | 0.00       |                              | 19.6        | 19.6       | 386                     |   | 0.009       |                           |                |
| ISV                         | 0.33       |                              | 19.6        | 19.6       | 386                     |   | 0.009       | 127                       | 0.003          |
|                             | 0.40       |                              | 19.6        | 19.6       | 386                     |   | 0.009       | 154                       | 0.004          |
|                             | 0.50       |                              | 19.6        | 19.6       | 386                     |   | 0.009       | 193                       | 0.004          |
|                             | 0.60       |                              | 19.6        | 19.6       | 386                     |   | 0.009       | 232                       | 0.005          |
|                             | 0.70       |                              | 19.6        | 19.6       | 386                     |   | 0.009       | 270                       | 0.006          |
|                             | 0.80       |                              | 19.6        | 19.6       | 386                     |   | 0.009       | 309                       | 0.007          |
|                             | 0.90       |                              | 37.4        | 28.4       | 1,063                   |   | 0.024       | 369                       | 0.008          |
|                             | 1.00       |                              | 62.8        | 40.9       | 2,569                   |   | 0.059       | 546                       | 0.013          |
|                             | 1.10       |                              | 88.2        | 53.4       | 4,711                   |   | 0.108       | 904                       | 0.021          |
|                             | 1.20       |                              | 113.6       | 65.9       | 7,488                   |   | 0.172       | 1,509                     | 0.035          |
| 1.30                        |            | 139.0                        | 78.4        | 10,899     |                         | 0.250                                     | 2,423       | 0.056                     |                |
| 1.40                        |            | 164.4                        | 90.9        | 14,946     |                         | 0.343                                     | 3,710       | 0.085                     |                |
| 1.50                        |            | 189.8                        | 103.4       | 19,628     |                         | 0.451                                     | 5,433       | 0.125                     |                |
| 1.60                        |            | 215.2                        | 115.9       | 24,944     |                         | 0.573                                     | 7,657       | 0.176                     |                |
| 1.70                        |            | 240.6                        | 128.4       | 30,896     |                         | 0.709                                     | 10,443      | 0.240                     |                |
| 1.80                        |            | 266.0                        | 140.9       | 37,482     |                         | 0.860                                     | 13,857      | 0.318                     |                |
| Floor                       | 1.82       |                              | 271.1       | 143.4      | 38,876                  |   | 0.892       | 14,621                    | 0.336          |
|                             | 1.90       |                              | 271.7       | 144.0      | 39,142                  |   | 0.899       | 17,741                    | 0.407          |
|                             | 2.00       |                              | 272.5       | 144.8      | 39,475                  |   | 0.906       | 21,672                    | 0.498          |
|                             | 2.10       |                              | 273.3       | 145.6      | 39,809                  |   | 0.914       | 25,636                    | 0.589          |
|                             | 2.20       |                              | 274.1       | 146.4      | 40,145                  |   | 0.922       | 29,634                    | 0.680          |
|                             | 2.30       |                              | 274.9       | 147.2      | 40,482                  |   | 0.929       | 33,665                    | 0.773          |
|                             | 2.40       |                              | 275.7       | 148.0      | 40,821                  |   | 0.937       | 37,730                    | 0.866          |
| Zone 1 (WQCV)               | 2.45       |                              | 276.1       | 148.4      | 40,990                  |   | 0.941       | 39,776                    | 0.913          |
|                             | 2.50       |                              | 276.5       | 148.8      | 41,160                  |   | 0.945       | 41,830                    | 0.960          |
|                             | 2.60       |                              | 277.3       | 149.6      | 41,501                  |   | 0.953       | 45,963                    | 1.055          |
|                             | 2.70       |                              | 278.1       | 150.4      | 41,844                  |   | 0.961       | 50,130                    | 1.151          |
| 2.80                        |            | 278.9                        | 151.2       | 42,187     |                         | 0.968                                     | 54,331      | 1.247                     |                |
| 2.90                        |            | 279.7                        | 152.0       | 42,532     |                         | 0.976                                     | 58,567      | 1.345                     |                |
| 3.00                        |            | 280.5                        | 152.8       | 42,878     |                         | 0.984                                     | 62,838      | 1.443                     |                |
| 3.10                        |            | 281.3                        | 153.6       | 43,225     |                         | 0.992                                     | 67,143      | 1.541                     |                |
| 3.20                        |            | 282.1                        | 154.4       | 43,574     |                         | 1.000                                     | 71,483      | 1.641                     |                |
| Zone 2 (5-year)             | 3.23       |                              | 282.4       | 154.7      | 43,679                  |   | 1.003       | 72,792                    | 1.671          |
|                             | 3.30       |                              | 282.9       | 155.2      | 43,924                  |   | 1.008       | 75,858                    | 1.741          |
|                             | 3.40       |                              | 283.7       | 156.0      | 44,275                  |   | 1.016       | 80,268                    | 1.843          |
|                             | 3.50       |                              | 284.5       | 156.8      | 44,627                  |   | 1.025       | 84,713                    | 1.945          |
|                             | 3.60       |                              | 285.3       | 157.6      | 44,981                  |   | 1.033       | 89,193                    | 2.048          |
|                             | 3.70       |                              | 286.1       | 158.4      | 45,336                  |   | 1.041       | 93,709                    | 2.151          |
|                             | 3.80       |                              | 286.9       | 159.2      | 45,693                  |   | 1.049       | 98,260                    | 2.256          |
|                             | 3.90       |                              | 287.7       | 160.0      | 46,050                  |   | 1.057       | 102,848                   | 2.361          |
|                             | 4.00       |                              | 288.5       | 160.8      | 46,409                  |   | 1.065       | 107,471                   | 2.467          |
|                             | 4.10       |                              | 289.3       | 161.6      | 46,769                  |   | 1.074       | 112,129                   | 2.574          |
| 4.20                        |            | 290.1                        | 162.4       | 47,131     |                         | 1.082                                     | 116,824     | 2.682                     |                |
| 4.30                        |            | 290.9                        | 163.2       | 47,493     |                         | 1.090                                     | 121,556     | 2.791                     |                |
| 4.40                        |            | 291.7                        | 164.0       | 47,857     |                         | 1.099                                     | 126,323     | 2.900                     |                |
| 4.50                        |            | 292.5                        | 164.8       | 48,223     |                         | 1.107                                     | 131,127     | 3.010                     |                |
| 4.60                        |            | 293.3                        | 165.6       | 48,589     |                         | 1.115                                     | 135,968     | 3.121                     |                |
| 4.70                        |            | 294.1                        | 166.4       | 48,957     |                         | 1.124                                     | 140,845     | 3.233                     |                |
| 4.80                        |            | 294.9                        | 167.2       | 49,326     |                         | 1.132                                     | 145,759     | 3.346                     |                |
| 4.90                        |            | 295.7                        | 168.0       | 49,696     |                         | 1.141                                     | 150,710     | 3.460                     |                |
| 5.00                        |            | 296.5                        | 168.8       | 50,068     |                         | 1.149                                     | 155,698     | 3.574                     |                |
| 5.10                        |            | 297.3                        | 169.6       | 50,441     |                         | 1.158                                     | 160,724     | 3.690                     |                |
| 5.20                        |            | 298.1                        | 170.4       | 50,815     |                         | 1.167                                     | 165,787     | 3.806                     |                |
| 5.30                        |            | 298.9                        | 171.2       | 51,191     |                         | 1.175                                     | 170,887     | 3.923                     |                |
| 5.40                        |            | 299.7                        | 172.0       | 51,568     |                         | 1.184                                     | 176,025     | 4.041                     |                |
| 5.50                        |            | 300.5                        | 172.8       | 51,946     |                         | 1.193                                     | 181,201     | 4.160                     |                |
| 5.60                        |            | 301.3                        | 173.6       | 52,325     |                         | 1.201                                     | 186,414     | 4.279                     |                |
| 5.70                        |            | 302.1                        | 174.4       | 52,706     |                         | 1.210                                     | 191,666     | 4.400                     |                |
| 5.80                        |            | 302.9                        | 175.2       | 53,087     |                         | 1.219                                     | 196,955     | 4.521                     |                |
| 5.90                        |            | 303.7                        | 176.0       | 53,471     |                         | 1.228                                     | 202,283     | 4.644                     |                |
| Zone 3 (100-year)           | 5.98       |                              | 304.4       | 176.7      | 53,778                  |   | 1.235       | 206,573                   | 4.742          |
|                             | 6.00       |                              | 304.5       | 176.8      | 53,855                  |   | 1.236       | 207,649                   | 4.767          |
|                             | 6.10       |                              | 305.3       | 177.6      | 54,241                  |   | 1.245       | 213,054                   | 4.891          |
|                             | 6.20       |                              | 306.1       | 178.4      | 54,628                  |   | 1.254       | 218,498                   | 5.016          |
|                             | 6.30       |                              | 306.9       | 179.2      | 55,016                  |   | 1.263       | 223,980                   | 5.142          |
|                             | 6.40       |                              | 307.7       | 180.0      | 55,406                  |   | 1.272       | 229,501                   | 5.269          |
|                             | 6.50       |                              | 308.5       | 180.8      | 55,797                  |   | 1.281       | 235,061                   | 5.396          |
|                             | 6.60       |                              | 309.3       | 181.6      | 56,189                  |   | 1.290       | 240,660                   | 5.525          |
|                             | 6.70       |                              | 310.1       | 182.4      | 56,582                  |   | 1.299       | 246,299                   | 5.654          |
|                             | 6.80       |                              | 310.9       | 183.2      | 56,977                  |   | 1.308       | 251,977                   | 5.785          |
|                             | 6.90       |                              | 311.7       | 184.0      | 57,373                  |   | 1.317       | 257,694                   | 5.916          |
|                             | 7.00       |                              | 312.5       | 184.8      | 57,770                  |   | 1.326       | 263,451                   | 6.048          |
|                             | 7.10       |                              | 313.3       | 185.6      | 58,169                  |   | 1.335       | 269,248                   | 6.181          |
|                             | 7.20       |                              | 314.1       | 186.4      | 58,569                  |   | 1.345       | 275,085                   | 6.315          |
|                             | 7.30       |                              | 314.9       | 187.2      | 58,970                  |   | 1.354       | 280,962                   | 6.450          |
|                             | 7.40       |                              | 315.7       | 188.0      | 59,372                  |   | 1.363       | 286,879                   | 6.586          |
|                             | 7.50       |                              | 316.5       | 188.8      | 59,776                  |   | 1.372       | 292,837                   | 6.723          |
|                             | 7.60       |                              | 317.3       | 189.6      | 60,181                  |   | 1.382       | 298,834                   | 6.860          |
|                             | 7.70       |                              | 318.1       | 190.4      | 60,587                  |   | 1.391       | 304,873                   | 6.999          |
|                             | 7.80       |                              | 318.9       | 191.2      | 60,994                  |   | 1.400       | 310,952                   | 7.138          |
| 7.90                        |            | 319.7                        | 192.0       | 61,403     |                         | 1.410                                     | 317,072     | 7.279                     |                |
| 8.00                        |            | 320.5                        | 192.8       | 61,813     |                         | 1.419                                     | 323,232     | 7.420                     |                |
| 8.10                        |            | 321.3                        | 193.6       | 62,225     |                         | 1.428                                     | 329,434     | 7.563                     |                |
| 8.20                        |            | 322.1                        | 194.4       | 62,637     |                         | 1.438                                     | 335,677     | 7.706                     |                |
| 8.30                        |            | 322.9                        | 195.2       | 63,051     |                         | 1.447                                     | 341,962     | 7.850                     |                |
| 8.40                        |            | 323.7                        | 196.0       | 63,466     |                         | 1.457                                     | 348,288     | 7.996                     |                |
| 8.50                        |            | 324.5                        | 196.8       | 63,883     |                         | 1.467                                     | 354,655     | 8.142                     |                |
| 8.60                        |            | 325.3                        | 197.6       | 64,301     |                         | 1.476                                     | 361,064     | 8.289                     |                |
| 8.70                        |            | 326.1                        | 198.4       | 64,720     |                         | 1.486                                     | 367,515     | 8.437                     |                |
| 8.80                        |            | 326.9                        | 199.2       | 65,140     |                         | 1.495                                     | 374,008     | 8.586                     |                |
| 8.90                        |            | 327.7                        | 200.0       | 65,561     |                         | 1.505                                     | 380,543     | 8.736                     |                |
| 9.00                        |            | 328.5                        | 200.8       | 65,984     |                         | 1.515                                     | 387,121     | 8.887                     |                |
| 9.10                        |            | 329.3                        | 201.6       | 66,409     |                         | 1.525                                     | 393,740     | 9.039                     |                |
| 9.20                        |            | 330.1                        | 202.4       | 66,834     |                         | 1.534                                     | 400,402     | 9.192                     |                |
| 9.30                        |            | 330.9                        | 203.2       | 67,261     |                         | 1.544                                     | 407,107     | 9.346                     |                |
| 9.40                        |            | 331.7                        | 204.0       | 67,689     |                         | 1.554                                     | 413,855     | 9.501                     |                |
| 9.50                        |            | 332.5                        | 204.8       | 68,118     |                         | 1.564                                     | 420,645     | 9.657                     |                |
| 9.60                        |            | 333.3                        | 205.6       | 68,548     |                         | 1.574                                     | 427,478     | 9.814                     |                |

# DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.04 (February 2021)

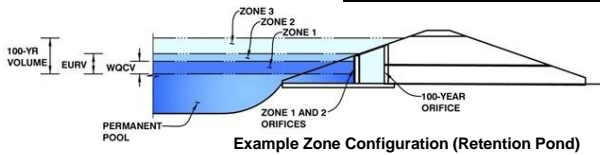


# DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-DETENTION, Version 4.04 (February 2021)

Project: Flying Horse North Master Drainage Plan

Basin ID: Pond 11



Example Zone Configuration (Retention Pond)

|                   | Estimated Stage (ft) | Estimated Volume (ac-ft) | Outlet Type          |
|-------------------|----------------------|--------------------------|----------------------|
| Zone 1 (WQCV)     | 2.52                 | 0.975                    | Orifice Plate        |
| Zone 2 (5-year)   | 3.92                 | 1.400                    | Weir&Pipe (Circular) |
| Zone 3 (100-year) | 6.30                 | 2.757                    | Weir&Pipe (Restrict) |
| Total (all zones) |                      | 5.132                    |                      |

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth = N/A ft (distance below the filtration media surface)  
Underdrain Orifice Diameter = N/A inches

Calculated Parameters for Underdrain  
Underdrain Orifice Area = N/A ft<sup>2</sup>  
Underdrain Orifice Centroid = N/A feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice = 0.00 ft (relative to basin bottom at Stage = 0 ft)  
Depth at top of Zone using Orifice Plate = 3.92 ft (relative to basin bottom at Stage = 0 ft)  
Orifice Plate: Orifice Vertical Spacing = N/A inches  
Orifice Plate: Orifice Area per Row = N/A inches

Calculated Parameters for Plate  
WQ Orifice Area per Row = N/A ft<sup>2</sup>  
Elliptical Half-Width = N/A feet  
Elliptical Slot Centroid = N/A feet  
Elliptical Slot Area = N/A ft<sup>2</sup>

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

|                                | Row 1 (required) | Row 2 (optional) | Row 3 (optional) | Row 4 (optional) | Row 5 (optional) | Row 6 (optional) | Row 7 (optional) | Row 8 (optional) |
|--------------------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|
| Stage of Orifice Centroid (ft) | 0.00             | 1.00             | 2.00             | 3.00             |                  |                  |                  |                  |
| Orifice Area (sq. inches)      | 3.57             | 3.57             | 3.57             | 10.00            |                  |                  |                  |                  |

|                                | Row 9 (optional) | Row 10 (optional) | Row 11 (optional) | Row 12 (optional) | Row 13 (optional) | Row 14 (optional) | Row 15 (optional) | Row 16 (optional) |
|--------------------------------|------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| Stage of Orifice Centroid (ft) |                  |                   |                   |                   |                   |                   |                   |                   |
| Orifice Area (sq. inches)      |                  |                   |                   |                   |                   |                   |                   |                   |

User Input: Vertical Orifice (Circular or Rectangular)

|   | Not Selected | Not Selected |
|---|--------------|--------------|
| Invert of Vertical Orifice =                  | N/A          | N/A          |
| Depth at top of Zone using Vertical Orifice = | N/A          | N/A          |
| Vertical Orifice Diameter =                   | N/A          | N/A          |

ft (relative to basin bottom at Stage = 0 ft)  
ft (relative to basin bottom at Stage = 0 ft)  
inches

Calculated Parameters for Vertical Orifice  
Vertical Orifice Area = N/A ft<sup>2</sup>  
Vertical Orifice Centroid = N/A feet

User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe))

|   | Zone 2 Weir  | Zone 3 Weir  |
|---|--------------|--------------|
| Overflow Weir Front Edge Height, H <sub>o</sub> = | 2.52         | 3.92         |
| Overflow Weir Front Edge Length =                 | 10.00        | 10.00        |
| Overflow Weir Grate Slope =                       | 0.00         | 4.00         |
| Horiz. Length of Weir Sides =                     | 10.00        | 18.00        |
| Overflow Grate Type =                             | Type C Grate | Type C Grate |
| Debris Clogging % =                               | 50%          | 50%          |

ft (relative to basin bottom at Stage = 0 ft)  
feet  
H:V  
feet  
%  
%

Calculated Parameters for Overflow Weir  
Height of Grate Upper Edge, H<sub>u</sub> = 2.52 feet  
Overflow Weir Slope Length = 10.00 feet  
Grate Open Area / 100-yr Orifice Area = 9.85  
Overflow Grate Open Area w/o Debris = 69.60 ft<sup>2</sup>  
Overflow Grate Open Area w/ Debris = 34.80 ft<sup>2</sup>

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

|  | Zone 2 Circular | Zone 3 Restrictor |
|--|-----------------|-------------------|
| Depth to Invert of Outlet Pipe =             | 2.50            | 2.80              |
| Circular Orifice Diameter or Pipe Diameter = | 36.00           | 60.00             |
| Restrictor Plate Height Above Pipe Invert =  |                 | 50.00             |

ft (distance below basin bottom at Stage = 0 ft)  
inches  
inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate  
Outlet Orifice Area = 7.07 ft<sup>2</sup>  
Outlet Orifice Centroid = 1.50 feet  
Half-Central Angle of Restrictor Plate on Pipe = N/A radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage = 15.30 ft (relative to basin bottom at Stage = 0 ft)  
Spillway Crest Length = 96.00 feet  
Spillway End Slopes = 4.00 H:V  
Freeboard above Max Water Surface = 1.00 feet

Calculated Parameters for Spillway  
Spillway Design Flow Depth = 0.97 feet  
Stage at Top of Freeboard = 17.27 feet  
Basin Area at Top of Freeboard = 2.42 acres  
Basin Volume at Top of Freeboard = 25.02 acre-ft

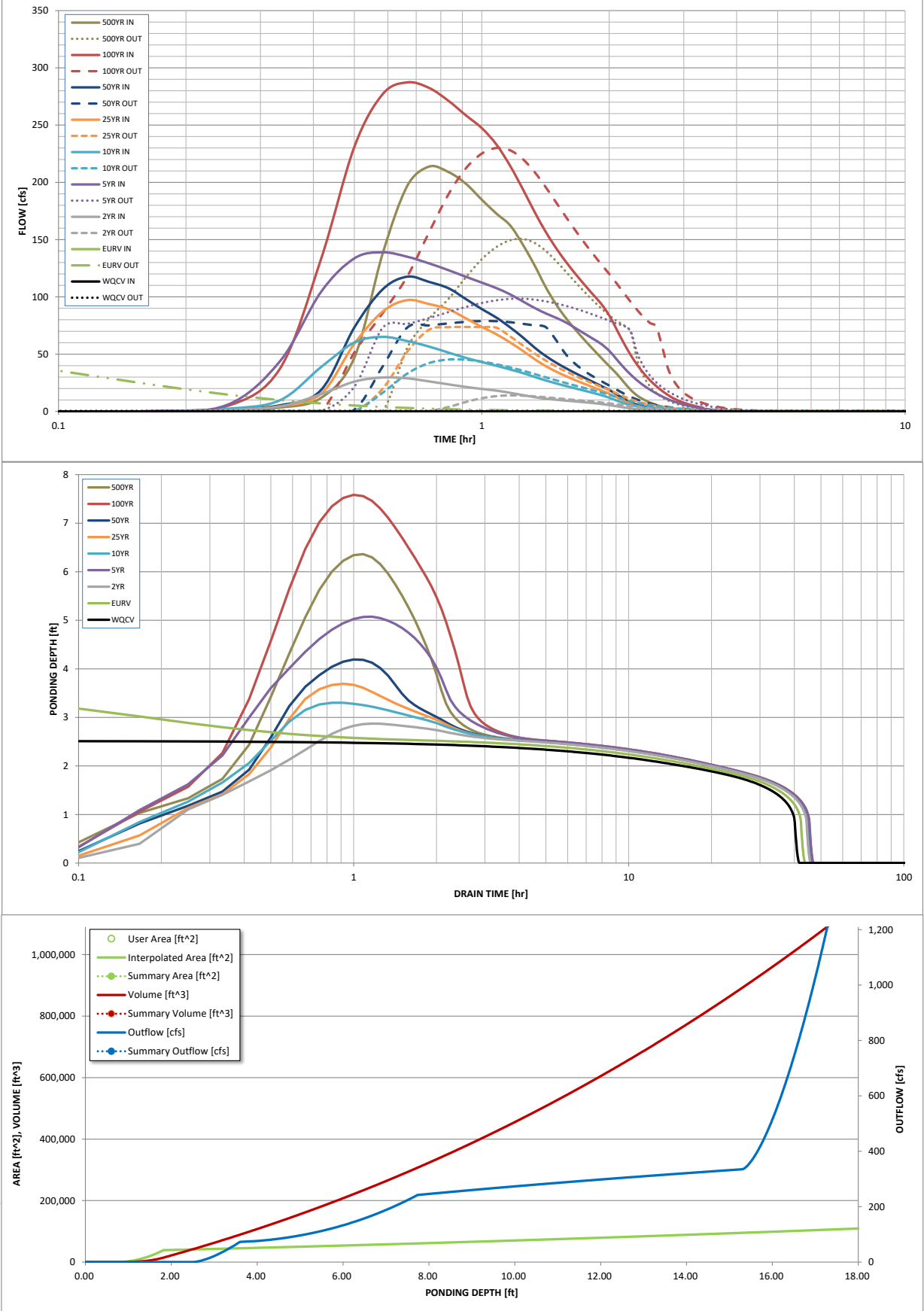
## Routed Hydrograph Results

The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).

|  | WQCV            | EURV           | 2 Year          | 5 Year          | 10 Year         | 25 Year        | 50 Year         | 100 Year        | 500 Year        |
|--|-----------------|----------------|-----------------|-----------------|-----------------|----------------|-----------------|-----------------|-----------------|
| Design Storm Return Period =                       | N/A             | N/A            | 1.19            | 1.50            | 1.75            | 2.00           | 2.25            | 2.52            | 3.39            |
| One-Hour Rainfall Depth (in) =                     | 0.975           | 2.322          | 2.370           | 3.903           | 5.321           | 7.486          | 9.112           | 11.293          | 17.208          |
| CUHP Runoff Volume (acre-ft) =                     | N/A             | N/A            | 2.370           | 15.619          | 5.321           | 7.486          | 9.112           | 28.758          | 17.208          |
| User Override Inflow Hydrograph Volume (acre-ft) = | N/A             | N/A            | 9.0             | 25.0            | 37.8            | 67.7           | 85.0            | 108.0           | 168.2           |
| CUHP Predevelopment Peak Q (cfs) =                 | N/A             | N/A            | 103.5           |                 |                 |                |                 |                 |                 |
| OPTIONAL Override Predevelopment Peak Q (cfs) =    | N/A             | N/A            | 0.11            | 1.30            | 0.47            | 0.85           | 1.07            | 2.78            | 2.11            |
| Predevelopment Unit Peak Flow, q (cfs/acre) =      | N/A             | N/A            | 29.6            | 138.9           | 65.1            | 97.2           | 117.7           | 287.3           | 213.7           |
| Peak Inflow Q (cfs) =                              | N/A             | N/A            | 14.0            | 98.4            | 45.3            | 73.7           | 78.9            | 230.0           | 150.6           |
| Peak Outflow Q (cfs) =                             | N/A             | N/A            | N/A             | 1.0             | 1.2             | 1.1            | 0.9             | 1.0             | 0.9             |
| Ratio Peak Outflow to Predevelopment Q =           | Overflow Weir 1 | Outlet Plate 1 | Overflow Weir 1 | Overflow Weir 2 | Overflow Weir 1 | Outlet Plate 1 | Overflow Weir 2 | Overflow Weir 2 | Overflow Weir 2 |
| Structure Controlling Flow =                       | N/A             | 1.07           | 0.19            | 1.2             | 0.6             | 1.0            | 1.1             | 1.4             | 1.3             |
| Max Velocity through Grate 1 (fps) =               | N/A             | N/A            | N/A             | 0.1             | N/A             | N/A            | 0.0             | 1.0             | 0.4             |
| Max Velocity through Grate 2 (fps) =               | 38              | 38             | 40              | 22              | 36              | 32             | 30              | 9               | 20              |
| Time to Drain 97% of Inflow Volume (hours) =       | 40              | 41             | 43              | 36              | 41              | 40             | 39              | 30              | 35              |
| Time to Drain 99% of Inflow Volume (hours) =       | 2.52            | 3.87           | 2.87            | 5.07            | 3.30            | 3.69           | 4.19            | 7.58            | 6.36            |
| Maximum Ponding Depth (ft) =                       | 0.95            | 1.05           | 0.97            | 1.16            | 1.01            | 1.04           | 1.08            | 1.38            | 1.27            |
| Area at Maximum Ponding Depth (acres) =            | 0.979           | 2.329          | 1.315           | 3.655           | 1.741           | 2.141          | 2.671           | 6.833           | 5.218           |
| Maximum Volume Stored (acre-ft) =                  |                 |                |                 |                 |                 |                |                 |                 |                 |

DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD- Detention, Version 4.04 (February 2021)



| S-A-V-D Chart Axis Override | X-axis | Left Y-Axis | Right Y-Axis |
|-----------------------------|--------|-------------|--------------|
| minimum bound               |        |             |              |
| maximum bound               |        |             |              |

# DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename: ...[SWM]Outflow hydrographs\Pond6 OutflowHydrograph.xlsx

## Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

|               | SOURCE  | CUHP       | CUHP       | CUHP         | USER         | CUHP          | CUHP          | CUHP          | USER           | CUHP           |
|---------------|---------|------------|------------|--------------|--------------|---------------|---------------|---------------|----------------|----------------|
| Time Interval | TIME    | WQCV [cfs] | EURV [cfs] | 2 Year [cfs] | 5 Year [cfs] | 10 Year [cfs] | 25 Year [cfs] | 50 Year [cfs] | 100 Year [cfs] | 500 Year [cfs] |
| 5.00 min      | 0:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 0:05:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 0:10:00 | 0.00       | 0.00       | 0.00         | 0.15         | 0.00          | 0.00          | 0.13          | 0.23           | 0.59           |
|               | 0:15:00 | 0.00       | 0.00       | 1.10         | 5.66         | 2.29          | 1.55          | 1.99          | 4.66           | 3.32           |
|               | 0:20:00 | 0.00       | 0.00       | 4.30         | 43.71        | 9.70          | 4.49          | 5.33          | 37.21          | 11.68          |
|               | 0:25:00 | 0.00       | 0.00       | 15.06        | 104.14       | 38.56         | 15.22         | 18.54         | 132.57         | 46.97          |
|               | 0:30:00 | 0.00       | 0.00       | 26.05        | 133.65       | 60.20         | 59.13         | 73.34         | 231.06         | 138.01         |
|               | 0:35:00 | 0.00       | 0.00       | 29.62        | 138.88       | 65.06         | 87.24         | 106.62        | 277.06         | 196.91         |
|               | 0:40:00 | 0.00       | 0.00       | 28.86        | 135.05       | 61.42         | 97.17         | 117.65        | 287.31         | 213.74         |
|               | 0:45:00 | 0.00       | 0.00       | 26.23        | 129.30       | 56.65         | 93.75         | 113.10        | 282.54         | 209.10         |
|               | 0:50:00 | 0.00       | 0.00       | 23.66        | 123.37       | 51.42         | 89.28         | 107.62        | 271.32         | 198.85         |
|               | 0:55:00 | 0.00       | 0.00       | 21.40        | 117.59       | 46.77         | 81.30         | 98.15         | 258.59         | 184.87         |
|               | 1:00:00 | 0.00       | 0.00       | 19.63        | 112.46       | 43.09         | 73.75         | 89.36         | 247.38         | 172.67         |
|               | 1:05:00 | 0.00       | 0.00       | 18.13        | 107.62       | 39.83         | 67.32         | 81.86         | 232.96         | 162.45         |
|               | 1:10:00 | 0.00       | 0.00       | 16.24        | 102.21       | 36.61         | 60.20         | 73.37         | 214.44         | 145.69         |
|               | 1:15:00 | 0.00       | 0.00       | 14.28        | 96.08        | 33.50         | 52.93         | 64.66         | 194.13         | 127.38         |
|               | 1:20:00 | 0.00       | 0.00       | 12.44        | 90.31        | 30.08         | 45.60         | 55.68         | 174.02         | 108.38         |
|               | 1:25:00 | 0.00       | 0.00       | 11.10        | 85.56        | 27.02         | 39.51         | 48.32         | 156.65         | 93.15          |
|               | 1:30:00 | 0.00       | 0.00       | 10.17        | 81.68        | 24.41         | 34.69         | 42.46         | 142.30         | 81.07          |
|               | 1:35:00 | 0.00       | 0.00       | 9.39         | 77.51        | 22.10         | 30.68         | 37.56         | 130.26         | 71.10          |
|               | 1:40:00 | 0.00       | 0.00       | 8.68         | 72.64        | 20.00         | 27.16         | 33.23         | 119.80         | 62.24          |
|               | 1:45:00 | 0.00       | 0.00       | 7.98         | 67.83        | 18.03         | 23.98         | 29.32         | 110.45         | 54.17          |
|               | 1:50:00 | 0.00       | 0.00       | 7.29         | 63.29        | 16.14         | 21.03         | 25.66         | 101.85         | 46.61          |
|               | 1:55:00 | 0.00       | 0.00       | 6.43         | 58.80        | 14.16         | 18.18         | 22.15         | 93.77          | 39.51          |
|               | 2:00:00 | 0.00       | 0.00       | 5.54         | 52.93        | 11.97         | 15.45         | 18.79         | 83.86          | 32.89          |
|               | 2:05:00 | 0.00       | 0.00       | 4.50         | 45.41        | 9.47          | 12.30         | 14.90         | 71.47          | 25.53          |
|               | 2:10:00 | 0.00       | 0.00       | 3.48         | 38.21        | 7.13          | 9.14          | 11.03         | 59.49          | 18.66          |
|               | 2:15:00 | 0.00       | 0.00       | 2.60         | 32.02        | 5.56          | 6.40          | 7.83          | 49.02          | 13.63          |
|               | 2:20:00 | 0.00       | 0.00       | 2.00         | 26.82        | 4.51          | 4.72          | 5.84          | 40.28          | 10.21          |
|               | 2:25:00 | 0.00       | 0.00       | 1.61         | 22.47        | 3.68          | 3.56          | 4.44          | 33.01          | 7.66           |
|               | 2:30:00 | 0.00       | 0.00       | 1.31         | 18.85        | 2.99          | 2.72          | 3.41          | 27.03          | 5.71           |
|               | 2:35:00 | 0.00       | 0.00       | 1.07         | 15.76        | 2.41          | 2.08          | 2.62          | 22.10          | 4.21           |
|               | 2:40:00 | 0.00       | 0.00       | 0.86         | 13.07        | 1.92          | 1.61          | 2.01          | 17.94          | 3.04           |
|               | 2:45:00 | 0.00       | 0.00       | 0.69         | 10.76        | 1.50          | 1.22          | 1.53          | 14.43          | 2.18           |
|               | 2:50:00 | 0.00       | 0.00       | 0.56         | 8.85         | 1.17          | 0.93          | 1.16          | 11.58          | 1.64           |
|               | 2:55:00 | 0.00       | 0.00       | 0.45         | 7.28         | 0.90          | 0.73          | 0.91          | 9.35           | 1.28           |
|               | 3:00:00 | 0.00       | 0.00       | 0.37         | 5.98         | 0.70          | 0.57          | 0.71          | 7.60           | 1.02           |
|               | 3:05:00 | 0.00       | 0.00       | 0.29         | 4.89         | 0.54          | 0.45          | 0.55          | 6.19           | 0.80           |
|               | 3:10:00 | 0.00       | 0.00       | 0.23         | 3.95         | 0.41          | 0.34          | 0.42          | 5.01           | 0.61           |
|               | 3:15:00 | 0.00       | 0.00       | 0.17         | 3.16         | 0.30          | 0.25          | 0.31          | 4.01           | 0.44           |
|               | 3:20:00 | 0.00       | 0.00       | 0.12         | 2.49         | 0.21          | 0.18          | 0.22          | 3.17           | 0.30           |
|               | 3:25:00 | 0.00       | 0.00       | 0.08         | 1.93         | 0.13          | 0.12          | 0.14          | 2.46           | 0.19           |
|               | 3:30:00 | 0.00       | 0.00       | 0.05         | 1.47         | 0.07          | 0.07          | 0.08          | 1.88           | 0.10           |
|               | 3:35:00 | 0.00       | 0.00       | 0.03         | 1.11         | 0.03          | 0.03          | 0.04          | 1.41           | 0.04           |
|               | 3:40:00 | 0.00       | 0.00       | 0.01         | 0.82         | 0.01          | 0.01          | 0.01          | 1.04           | 0.01           |
|               | 3:45:00 | 0.00       | 0.00       | 0.00         | 0.60         | 0.00          | 0.00          | 0.00          | 0.76           | 0.00           |
|               | 3:50:00 | 0.00       | 0.00       | 0.00         | 0.43         | 0.00          | 0.00          | 0.00          | 0.54           | 0.00           |
|               | 3:55:00 | 0.00       | 0.00       | 0.00         | 0.31         | 0.00          | 0.00          | 0.00          | 0.39           | 0.00           |
|               | 4:00:00 | 0.00       | 0.00       | 0.00         | 0.22         | 0.00          | 0.00          | 0.00          | 0.28           | 0.00           |
|               | 4:05:00 | 0.00       | 0.00       | 0.00         | 0.17         | 0.00          | 0.00          | 0.00          | 0.20           | 0.00           |
|               | 4:10:00 | 0.00       | 0.00       | 0.00         | 0.12         | 0.00          | 0.00          | 0.00          | 0.15           | 0.00           |
|               | 4:15:00 | 0.00       | 0.00       | 0.00         | 0.09         | 0.00          | 0.00          | 0.00          | 0.12           | 0.00           |
|               | 4:20:00 | 0.00       | 0.00       | 0.00         | 0.07         | 0.00          | 0.00          | 0.00          | 0.08           | 0.00           |
|               | 4:25:00 | 0.00       | 0.00       | 0.00         | 0.05         | 0.00          | 0.00          | 0.00          | 0.06           | 0.00           |
|               | 4:30:00 | 0.00       | 0.00       | 0.00         | 0.03         | 0.00          | 0.00          | 0.00          | 0.04           | 0.00           |
|               | 4:35:00 | 0.00       | 0.00       | 0.00         | 0.03         | 0.00          | 0.00          | 0.00          | 0.03           | 0.00           |
|               | 4:40:00 | 0.00       | 0.00       | 0.00         | 0.02         | 0.00          | 0.00          | 0.00          | 0.02           | 0.00           |
|               | 4:45:00 | 0.00       | 0.00       | 0.00         | 0.02         | 0.00          | 0.00          | 0.00          | 0.02           | 0.00           |
|               | 4:50:00 | 0.00       | 0.00       | 0.00         | 0.01         | 0.00          | 0.00          | 0.00          | 0.01           | 0.00           |
|               | 4:55:00 | 0.00       | 0.00       | 0.00         | 0.01         | 0.00          | 0.00          | 0.00          | 0.01           | 0.00           |
|               | 5:00:00 | 0.00       | 0.00       | 0.00         | 0.01         | 0.00          | 0.00          | 0.00          | 0.01           | 0.00           |
|               | 5:05:00 | 0.00       | 0.00       | 0.00         | 0.01         | 0.00          | 0.00          | 0.00          | 0.01           | 0.00           |
|               | 5:10:00 | 0.00       | 0.00       | 0.00         | 0.01         | 0.00          | 0.00          | 0.00          | 0.01           | 0.00           |
|               | 5:15:00 | 0.00       | 0.00       | 0.00         | 0.01         | 0.00          | 0.00          | 0.00          | 0.01           | 0.00           |
|               | 5:20:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.01           | 0.00           |
|               | 5:25:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:30:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:35:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:40:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:45:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:50:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:55:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 6:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |



## DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.04 (February 2021)

### Summary Stage-Area-Volume-Discharge Relationships

The user can create a summary S-A-V-D by entering the desired stage increments and the remainder of the table will populate automatically.

The user should graphically compare the summary S-A-V-D table to the full S-A-V-D table in the chart to confirm it captures all key transition points.

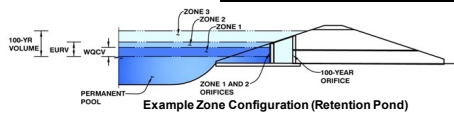
[illegible]

# DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-DETENTION, Version 4.04 (February 2021)

Project: Flying Horse North Master Drainage Plan

Basin ID: Pond 13



Example Zone Configuration (Retention Pond)

## Watershed Information

|   |            |           |
|---|------------|-----------|
| Selected BMP Type =                     | EDB        |           |
| Watershed Area =                        | 23.03      | acres     |
| Watershed Length =                      | 1,258      | ft        |
| Watershed Length to Centroid =          | 783        | ft        |
| Watershed Slope =                       | 0.050      | ft/ft     |
| Watershed Imperviousness =              | 65.00%     | percent   |
| Percentage Hydrologic Soil Group A =    | 0.0%       | percent   |
| Percentage Hydrologic Soil Group B =    | 100.0%     | percent   |
| Percentage Hydrologic Soil Groups C/D = | 0.0%       | percent   |
| Target WQCV Drain Time =                | 40.0       | hours     |
| Location for 1-hr Rainfall Depths =     | User Input |           |
| Water Quality Capture Volume (WQCV) =   | 0.488      | acre-feet |
| Excess Urban Runoff Volume (EURV) =     | 1.634      | acre-feet |
| 2-yr Runoff Volume (P1 = 1.19 in.) =    | 1.042      | acre-feet |
| 5-yr Runoff Volume (P1 = 1.5 in.) =     | 1.456      | acre-feet |
| 10-yr Runoff Volume (P1 = 1.75 in.) =   | 1.884      | acre-feet |
| 25-yr Runoff Volume (P1 = 2 in.) =      | 2.406      | acre-feet |
| 50-yr Runoff Volume (P1 = 2.25 in.) =   | 3.276      | acre-feet |
| 100-yr Runoff Volume (P1 = 2.52 in.) =  | 3.989      | acre-feet |
| 500-yr Runoff Volume (P1 = 3.14 in.) =  | 5.262      | acre-feet |
| Approximate 2-yr Detention Volume =     | 1.267      | acre-feet |
| Approximate 5-yr Detention Volume =     | 1.699      | acre-feet |
| Approximate 10-yr Detention Volume =    | 2.166      | acre-feet |
| Approximate 25-yr Detention Volume =    | 2.333      | acre-feet |
| Approximate 50-yr Detention Volume =    | 2.430      | acre-feet |
| Approximate 100-yr Detention Volume =   | 2.627      | acre-feet |

## Define Zones and Basin Geometry

|   |         |                 |
|---|---------|-----------------|
| Zone 1 Volume (WQCV) =                                  | 0.488   | acre-feet       |
| Zone 2 Volume (5-year - Zone 1) =                       | 1.211   | acre-feet       |
| Zone 3 Volume (100-year - Zones 1 & 2) =                | 0.927   | acre-feet       |
| Total Detention Basin Volume =                          | 2.627   | acre-feet       |
| Initial Surcharge Volume (ISV) =                        | 64      | ft <sup>3</sup> |
| Initial Surcharge Depth (ISD) =                         | 0.33    | ft              |
| Total Available Detention Depth (H <sub>total</sub> ) = | 6.00    | ft              |
| Depth of Trickle Channel (H <sub>tr</sub> ) =           | 0.50    | ft              |
| Slope of Trickle Channel (S <sub>tr</sub> ) =           | 0.004   | ft/ft           |
| Slopes of Main Basin Sides (S <sub>main</sub> ) =       | 4       | H:V             |
| Basin Length-to-Width Ratio (R <sub>L/W</sub> ) =       | 2       |                 |
| Initial Surcharge Area (A <sub>ISV</sub> ) =            | 193     | ft <sup>2</sup> |
| Surcharge Volume Length (L <sub>ISV</sub> ) =           | 13.9    | ft              |
| Surcharge Volume Width (W <sub>ISV</sub> ) =            | 13.9    | ft              |
| Depth of Basin Floor (H <sub>floor</sub> ) =            | 0.68    | ft              |
| Length of Basin Floor (L <sub>floor</sub> ) =           | 186.6   | ft              |
| Width of Basin Floor (W <sub>floor</sub> ) =            | 98.9    | ft              |
| Area of Basin Floor (A <sub>floor</sub> ) =             | 18,456  | ft <sup>2</sup> |
| Volume of Basin Floor (V <sub>floor</sub> ) =           | 4,655   | ft <sup>3</sup> |
| Depth of Main Basin (H <sub>main</sub> ) =              | 4.49    | ft              |
| Length of Main Basin (L <sub>main</sub> ) =             | 222.5   | ft              |
| Width of Main Basin (W <sub>main</sub> ) =              | 134.8   | ft              |
| Area of Main Basin (A <sub>main</sub> ) =               | 30,002  | ft <sup>2</sup> |
| Volume of Main Basin (V <sub>main</sub> ) =             | 107,744 | ft <sup>3</sup> |
| Calculated Total Basin Volume (V <sub>total</sub> ) =   | 2,584   | acre-feet       |

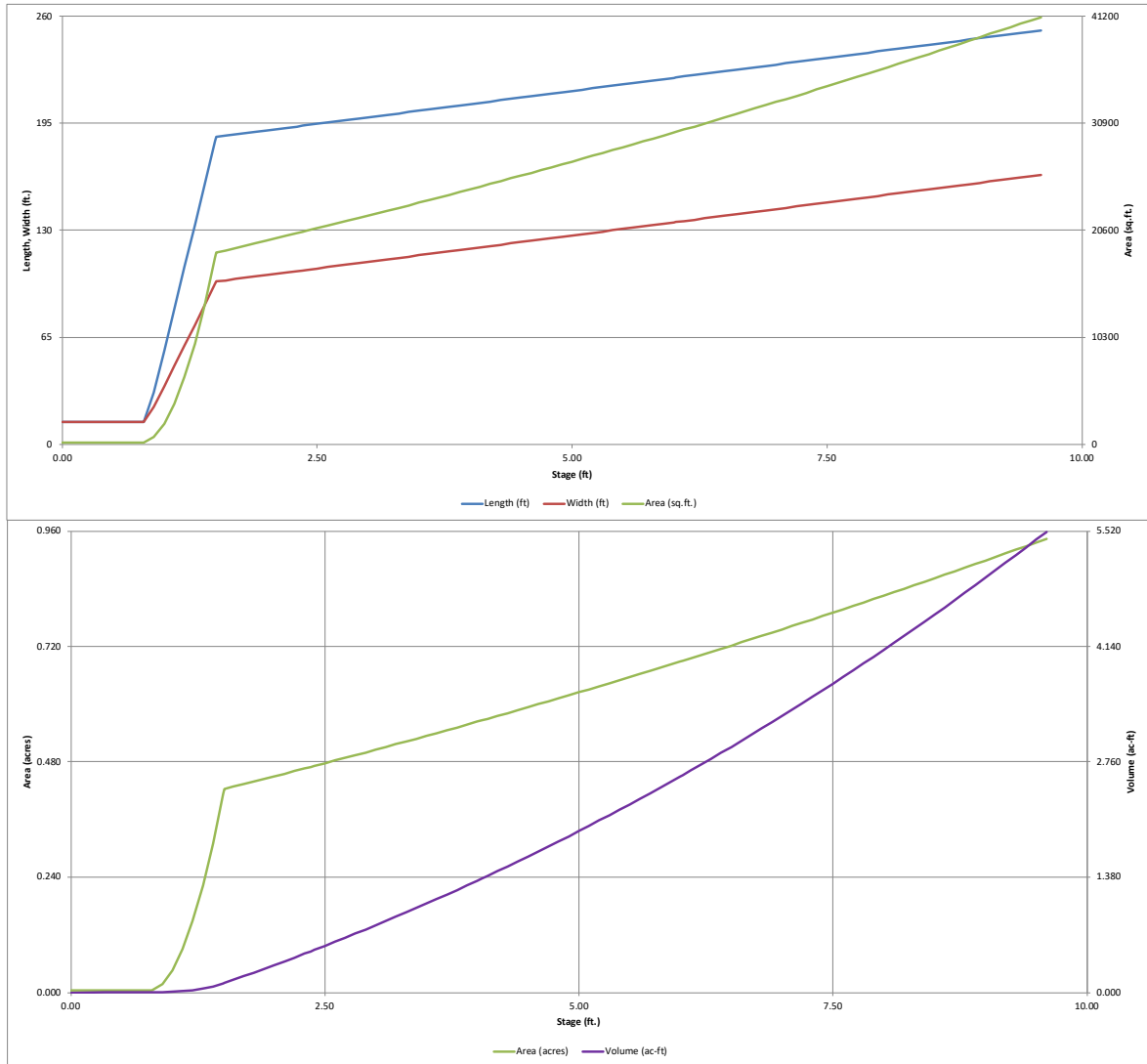
## Optional User Overrides

|      |           |
|------|-----------|
|      | acre-feet |
|      | acre-feet |
| 1.19 | inches    |
| 1.50 | inches    |
| 1.75 | inches    |
| 2.00 | inches    |
| 2.25 | inches    |
| 2.52 | inches    |
|      | inches    |

|                             |            |                              |             |            |                         |   |             |                           |                |
|-----------------------------|------------|------------------------------|-------------|------------|-------------------------|---|-------------|---------------------------|----------------|
| Depth Increment =           | 0.10       | ft                           |             |            |                         |   |             |                           |                |
| Stage - Storage Description | Stage (ft) | Optional Override Stage (ft) | Length (ft) | Width (ft) | Area (ft <sup>2</sup> ) | Optional Override Area (ft <sup>2</sup> ) | Area (acre) | Volume (ft <sup>3</sup> ) | Volume (ac-ft) |
| Top of Micropool            | 0.00       |                              | 13.9        | 13.9       | 193                     |   | 0.004       |                           |                |
| ISV                         | 0.33       |                              | 13.9        | 13.9       | 193                     |   | 0.004       | 64                        | 0.001          |
|                             | 0.40       |                              | 13.9        | 13.9       | 193                     |   | 0.004       | 77                        | 0.002          |
|                             | 0.50       |                              | 13.9        | 13.9       | 193                     |   | 0.004       | 97                        | 0.002          |
|                             | 0.60       |                              | 13.9        | 13.9       | 193                     |   | 0.004       | 116                       | 0.003          |
|                             | 0.70       |                              | 13.9        | 13.9       | 193                     |   | 0.004       | 135                       | 0.003          |
|                             | 0.80       |                              | 13.9        | 13.9       | 193                     |   | 0.004       | 155                       | 0.004          |
|                             | 0.90       |                              | 31.7        | 22.6       | 717                     |   | 0.016       | 190                       | 0.004          |
|                             | 1.00       |                              | 57.1        | 35.1       | 2,006                   |   | 0.046       | 321                       | 0.007          |
|                             | 1.10       |                              | 82.5        | 47.6       | 3,930                   |   | 0.090       | 613                       | 0.014          |
|                             | 1.20       |                              | 107.9       | 60.1       | 6,489                   |   | 0.149       | 1,128                     | 0.026          |
| Floor                       | 1.30       |                              | 133.3       | 72.6       | 9,682                   |   | 0.222       | 1,932                     | 0.044          |
|                             | 1.40       |                              | 158.7       | 85.1       | 13,511                  |   | 0.310       | 3,086                     | 0.071          |
|                             | 1.50       |                              | 184.1       | 97.6       | 17,975                  |   | 0.413       | 4,655                     | 0.107          |
|                             | 1.51       |                              | 186.6       | 98.9       | 18,456                  |   | 0.424       | 4,837                     | 0.111          |
|                             | 1.60       |                              | 187.3       | 99.6       | 18,662                  |   | 0.428       | 6,507                     | 0.149          |
|                             | 1.70       |                              | 188.1       | 100.4      | 18,892                  |   | 0.434       | 8,385                     | 0.192          |
|                             | 1.80       |                              | 188.9       | 101.2      | 19,124                  |   | 0.439       | 10,286                    | 0.236          |
|                             | 1.90       |                              | 189.7       | 102.0      | 19,357                  |   | 0.444       | 12,210                    | 0.280          |
|                             | 2.00       |                              | 190.5       | 102.8      | 19,591                  |   | 0.450       | 14,157                    | 0.325          |
|                             | 2.10       |                              | 191.3       | 103.6      | 19,826                  |   | 0.455       | 16,128                    | 0.370          |
| Zone 1 (WQCV)               | 2.20       |                              | 192.1       | 104.4      | 20,063                  |   | 0.461       | 18,123                    | 0.416          |
|                             | 2.30       |                              | 192.9       | 105.2      | 20,300                  |   | 0.466       | 20,141                    | 0.462          |
|                             | 2.36       |                              | 193.4       | 105.7      | 20,444                  |   | 0.469       | 21,363                    | 0.490          |
|                             | 2.40       |                              | 193.7       | 106.0      | 20,540                  |   | 0.472       | 22,183                    | 0.509          |
|                             | 2.50       |                              | 194.5       | 106.8      | 20,780                  |   | 0.477       | 24,249                    | 0.557          |
|                             | 2.60       |                              | 195.3       | 107.6      | 21,022                  |   | 0.483       | 26,339                    | 0.605          |
|                             | 2.70       |                              | 196.1       | 108.4      | 21,265                  |   | 0.488       | 28,453                    | 0.653          |
|                             | 2.80       |                              | 196.9       | 109.2      | 21,509                  |   | 0.494       | 30,592                    | 0.702          |
|                             | 2.90       |                              | 197.7       | 110.0      | 21,755                  |   | 0.499       | 32,755                    | 0.752          |
|                             | 3.00       |                              | 198.5       | 110.8      | 22,001                  |   | 0.505       | 34,943                    | 0.802          |
| Zone 2 (5-year)             | 3.10       |                              | 199.3       | 111.6      | 22,250                  |   | 0.511       | 37,155                    | 0.853          |
|                             | 3.20       |                              | 200.1       | 112.4      | 22,499                  |   | 0.517       | 39,393                    | 0.904          |
|                             | 3.30       |                              | 200.9       | 113.2      | 22,750                  |   | 0.522       | 41,655                    | 0.956          |
|                             | 3.40       |                              | 201.7       | 114.0      | 23,002                  |   | 0.528       | 43,943                    | 1.009          |
|                             | 3.50       |                              | 202.5       | 114.8      | 23,255                  |   | 0.534       | 46,255                    | 1.062          |
|                             | 3.60       |                              | 203.3       | 115.6      | 23,509                  |   | 0.540       | 48,594                    | 1.116          |
|                             | 3.70       |                              | 204.1       | 116.4      | 23,765                  |   | 0.546       | 50,957                    | 1.170          |
|                             | 3.80       |                              | 204.9       | 117.2      | 24,022                  |   | 0.551       | 53,347                    | 1.225          |
|                             | 3.90       |                              | 205.7       | 118.0      | 24,281                  |   | 0.557       | 55,762                    | 1.280          |
|                             | 4.00       |                              | 206.5       | 118.8      | 24,540                  |   | 0.563       | 58,203                    | 1.336          |
| Zone 2 (5-year)             | 4.05       |                              | 206.9       | 119.2      | 24,671                  |   | 0.566       | 59,433                    | 1.364          |
|                             | 4.10       |                              | 207.3       | 119.6      | 24,801                  |   | 0.569       | 60,670                    | 1.393          |
|                             | 4.20       |                              | 208.1       | 120.4      | 25,063                  |   | 0.575       | 63,163                    | 1.450          |
|                             | 4.30       |                              | 208.9       | 121.2      | 25,327                  |   | 0.581       | 65,683                    | 1.508          |
|                             | 4.40       |                              | 209.7       | 122.0      | 25,592                  |   | 0.588       | 68,228                    | 1.566          |
|                             | 4.50       |                              | 210.5       | 122.8      | 25,858                  |   | 0.594       | 70,801                    | 1.625          |
|                             | 4.60       |                              | 211.3       | 123.6      | 26,125                  |   | 0.600       | 73,400                    | 1.685          |
|                             | 4.70       |                              | 212.1       | 124.4      | 26,394                  |   | 0.606       | 76,026                    | 1.745          |
|                             | 4.80       |                              | 212.9       | 125.2      | 26,663                  |   | 0.612       | 78,679                    | 1.806          |
|                             | 4.90       |                              | 213.7       | 126.0      | 26,935                  |   | 0.618       | 81,359                    | 1.868          |
| Zone 2 (5-year)             | 5.00       |                              | 214.5       | 126.8      | 27,207                  |   | 0.625       | 84,066                    | 1.930          |
|                             | 5.10       |                              | 215.3       | 127.6      | 27,481                  |   | 0.631       | 86,800                    | 1.993          |
|                             | 5.20       |                              | 216.1       | 128.4      | 27,756                  |   | 0.637       | 89,562                    | 2.056          |
|                             | 5.30       |                              | 216.9       | 129.2      | 28,032                  |   | 0.644       | 92,351                    | 2.120          |
|                             | 5.40       |                              | 217.7       | 130.0      | 28,310                  |   | 0.650       | 95,168                    | 2.185          |
|                             | 5.50       |                              | 218.5       | 130.8      | 28,589                  |   | 0.656       | 98,013                    | 2.250          |
|                             | 5.60       |                              | 219.3       | 131.6      | 28,869                  |   | 0.663       | 100,886                   | 2.316          |
|                             | 5.70       |                              | 220.1       | 132.4      | 29,150                  |   | 0.669       | 103,787                   | 2.383          |
|                             | 5.80       |                              | 220.9       | 133.2      | 29,433                  |   | 0.676       | 106,716                   | 2.450          |
|                             | 5.90       |                              | 221.7       | 134.0      | 29,717                  |   | 0.682       | 109,674                   | 2.518          |
| Zone 3 (100-year)           | 6.00       |                              | 222.5       | 134.8      | 30,002                  |   | 0.689       | 112,660                   | 2.586          |
|                             | 6.02       |                              | 222.7       | 135.0      | 30,059                  |   | 0.690       | 113,260                   | 2.600          |
|                             | 6.10       |                              | 223.3       | 135.6      | 30,288                  |   | 0.695       | 115,674                   | 2.656          |
|                             | 6.20       |                              | 224.1       | 136.4      | 30,576                  |   | 0.702       | 118,117                   | 2.725          |
|                             | 6.30       |                              | 224.9       | 137.2      | 30,865                  |   | 0.709       | 121,789                   | 2.796          |
|                             | 6.40       |                              | 225.7       | 138.0      | 31,156                  |   | 0.715       | 124,890                   | 2.867          |
|                             | 6.50       |                              | 226.5       | 138.8      | 31,447                  |   | 0.722       | 128,021                   | 2.939          |
|                             | 6.60       |                              | 227.3       | 139.6      | 31,740                  |   | 0.729       | 131,180                   | 3.011          |
|                             | 6.70       |                              | 228.1       | 140.4      | 32,034                  |   | 0.735       | 134,369                   | 3.085          |
|                             | 6.80       |                              | 228.9       | 141.2      | 32,330                  |   | 0.742       | 137,587                   | 3.159          |
| Zone 3 (100-year)           | 6.90       |                              | 229.7       | 142.0      | 32,627                  |   | 0.749       | 140,835                   | 3.233          |
|                             | 7.00       |                              | 230.5       | 142.8      | 32,925                  |   | 0.756       | 144,112                   | 3.308          |
|                             | 7.10       |                              | 231.3       | 143.6      | 33,224                  |   | 0.763       | 147,420                   | 3.384          |
|                             | 7.20       |                              | 232.1       | 144.4      | 33,525                  |   | 0.770       | 150,757                   | 3.461          |
|                             | 7.30       |                              | 232.9       | 145.2      | 33,827                  |   | 0.777       | 154,125                   | 3.538          |
|                             | 7.40       |                              | 233.7       | 146.0      | 34,130                  |   | 0.784       | 157,523                   | 3.616          |
|                             | 7.50       |                              | 234.5       | 146.8      | 34,434                  |   | 0.791       | 160,951                   | 3.695          |
|                             | 7.60       |                              | 235.3       | 147.6      | 34,740                  |   | 0.798       | 164,409                   | 3.774          |
|                             | 7.70       |                              | 236.1       | 148.4      | 35,047                  |   | 0.805       | 167,899                   | 3.854          |
|                             | 7.80       |                              | 236.9       | 149.2      | 35,355                  |   | 0.812       | 171,419                   | 3.935          |
| Zone 3 (100-year)           | 7.90       |                              | 237.7       | 150.0      | 35,665                  |   | 0.819       | 174,970                   | 4.017          |
|                             | 8.00       |                              | 238.5       | 150.8      | 35,976                  |   | 0.826       | 178,552                   | 4.099          |
|                             | 8.10       |                              | 239.3       | 151.6      | 36,288                  |   | 0.833       | 182,165                   | 4.182          |
|                             | 8.20       |                              | 240.1       | 152.4      | 36,601                  |   | 0.840       | 185,809                   | 4.266          |
|                             | 8.30       |                              | 240.9       | 153.2      | 36,916                  |   | 0.847       | 189,485                   | 4.350          |
|                             | 8.40       |                              | 241.7       | 154.0      | 37,232                  |   | 0.855       | 193,193                   | 4.435          |
|                             | 8.50       |                              | 242.5       | 154.8      | 37,549                  |   | 0.862       | 196,932                   | 4.521          |
|                             | 8.60       |                              | 243.3       | 155.6      | 37,868                  |   | 0.869       | 200,702                   | 4.607          |
|                             | 8.70       |                              | 244.1       | 156.4      | 38,187                  |   | 0.877       | 204,505                   | 4.695          |
|                             | 8.80       |                              | 244.9       | 157.2      | 38,508                  |   | 0.884       | 208,340                   | 4.783          |
| Zone 3 (100-year)           | 8.90       |                              | 245.7       | 158.0      | 38,831                  |   | 0.891       | 212,207                   | 4.872          |
|                             | 9.00       |                              | 246.5       | 158.8      | 39,154                  |   | 0.899       | 216,106                   | 4.961          |
|                             | 9.10       |                              | 247.3       | 159.6      | 39,479                  |   | 0.906       | 220,038                   | 5.051          |
|                             | 9.20       |                              | 248.1       | 160.4      | 39,806                  |   | 0.914       | 224,002                   | 5.142          |
|                             | 9.30       |                              | 248.9       | 161.2      | 40,133                  |   | 0.921       | 227,999                   | 5.234          |
|                             | 9.40       |                              | 249.7       | 162.0      | 40,462                  |   | 0.929       | 232,029                   | 5.327          |
|                             | 9.50       |                              | 250.5       | 162.8      | 40,792                  |   | 0.936       | 236,091                   | 5.420          |
|                             | 9.60       |                              | 251.3       | 163.6      | 41,123                  |   | 0.944       | 240,187                   | 5.514          |

# DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.04 (February 2021)

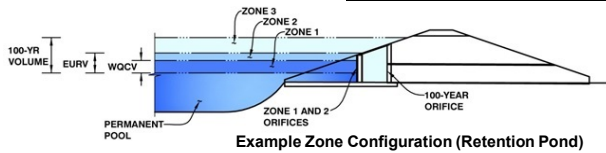


# DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-DETENTION, Version 4.04 (February 2021)

Project: Flying Horse North Master Drainage Plan

Basin ID: Pond 13



Example Zone Configuration (Retention Pond)

|                   | Estimated Stage (ft) | Estimated Volume (ac-ft) | Outlet Type          |
|-------------------|----------------------|--------------------------|----------------------|
| Zone 1 (WQCV)     | 2.36                 | 0.488                    | Orifice Plate        |
| Zone 2 (5-year)   | 4.63                 | 1.211                    | Circular Orifice     |
| Zone 3 (100-year) | 6.06                 | 0.927                    | Weir&Pipe (Restrict) |
| Total (all zones) |                      | 2.627                    |                      |

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth =  ft (distance below the filtration media surface)  
Underdrain Orifice Diameter =  inches

Calculated Parameters for Underdrain  
Underdrain Orifice Area =  ft<sup>2</sup>  
Underdrain Orifice Centroid =  feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice =  ft (relative to basin bottom at Stage = 0 ft)  
Depth at top of Zone using Orifice Plate =  ft (relative to basin bottom at Stage = 0 ft)  
Orifice Plate: Orifice Vertical Spacing =  inches  
Orifice Plate: Orifice Area per Row =  sq. inches (diameter = 1-7/16 inches)

Calculated Parameters for Plate  
WQ Orifice Area per Row =  ft<sup>2</sup>  
Elliptical Half-Width =  feet  
Elliptical Slot Centroid =  feet  
Elliptical Slot Area =  ft<sup>2</sup>

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

|                                | Row 1 (required) | Row 2 (optional) | Row 3 (optional) | Row 4 (optional) | Row 5 (optional) | Row 6 (optional) | Row 7 (optional) | Row 8 (optional) |
|--------------------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|
| Stage of Orifice Centroid (ft) | 0.00             | 0.79             | 1.57             |                  |                  |                  |                  |                  |
| Orifice Area (sq. inches)      | 1.68             | 1.68             | 1.68             |                  |                  |                  |                  |                  |

|                                | Row 9 (optional) | Row 10 (optional) | Row 11 (optional) | Row 12 (optional) | Row 13 (optional) | Row 14 (optional) | Row 15 (optional) | Row 16 (optional) |
|--------------------------------|------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| Stage of Orifice Centroid (ft) |                  |                   |                   |                   |                   |                   |                   |                   |
| Orifice Area (sq. inches)      |                  |                   |                   |                   |                   |                   |                   |                   |

User Input: Vertical Orifice (Circular or Rectangular)

Invert of Vertical Orifice =  ft (relative to basin bottom at Stage = 0 ft)  
Depth at top of Zone using Vertical Orifice =  ft (relative to basin bottom at Stage = 0 ft)  
Vertical Orifice Diameter =  inches

Calculated Parameters for Vertical Orif  
Zone 2 Circular Not Selected  
Vertical Orifice Area =  ft<sup>2</sup>  
Vertical Orifice Centroid =  feet

User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe)

Overflow Weir Front Edge Height, H<sub>o</sub> =  ft (relative to basin bottom at Stage = 0 ft)  
Overflow Weir Front Edge Length =  feet  
Overflow Weir Grate Slope =  H:V  
Horiz. Length of Weir Sides =  feet  
Overflow Grate Type =   
Debris Clogging % =  %

Calculated Parameters for Overflow W  
Zone 3 Weir Not Selected  
Height of Grate Upper Edge, H<sub>u</sub> =  ft  
Overflow Weir Slope Length =  feet  
Grate Open Area / 100-yr Orifice Area =   
Overflow Grate Open Area w/o Debris =  ft<sup>2</sup>  
Overflow Grate Open Area w/ Debris =  ft<sup>2</sup>

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

Depth to Invert of Outlet Pipe =  ft (distance below basin bottom at Stage = 0 ft)  
Outlet Pipe Diameter =  inches  
Restrictor Plate Height Above Pipe Invert =  inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Pl  
Zone 3 Restrictor Not Selected  
Outlet Orifice Area =  ft<sup>2</sup>  
Outlet Orifice Centroid =  feet  
Half-Central Angle of Restrictor Plate on Pipe =  degrees

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage =  ft (relative to basin bottom at Stage = 0 ft)  
Spillway Crest Length =  feet  
Spillway End Slopes =  H:V  
Freeboard above Max Water Surface =  feet

Calculated Parameters for Spillway  
Spillway Design Flow Depth =  feet  
Stage at Top of Freeboard =  feet  
Basin Area at Top of Freeboard =  acres  
Basin Volume at Top of Freeboard =  acre-ft

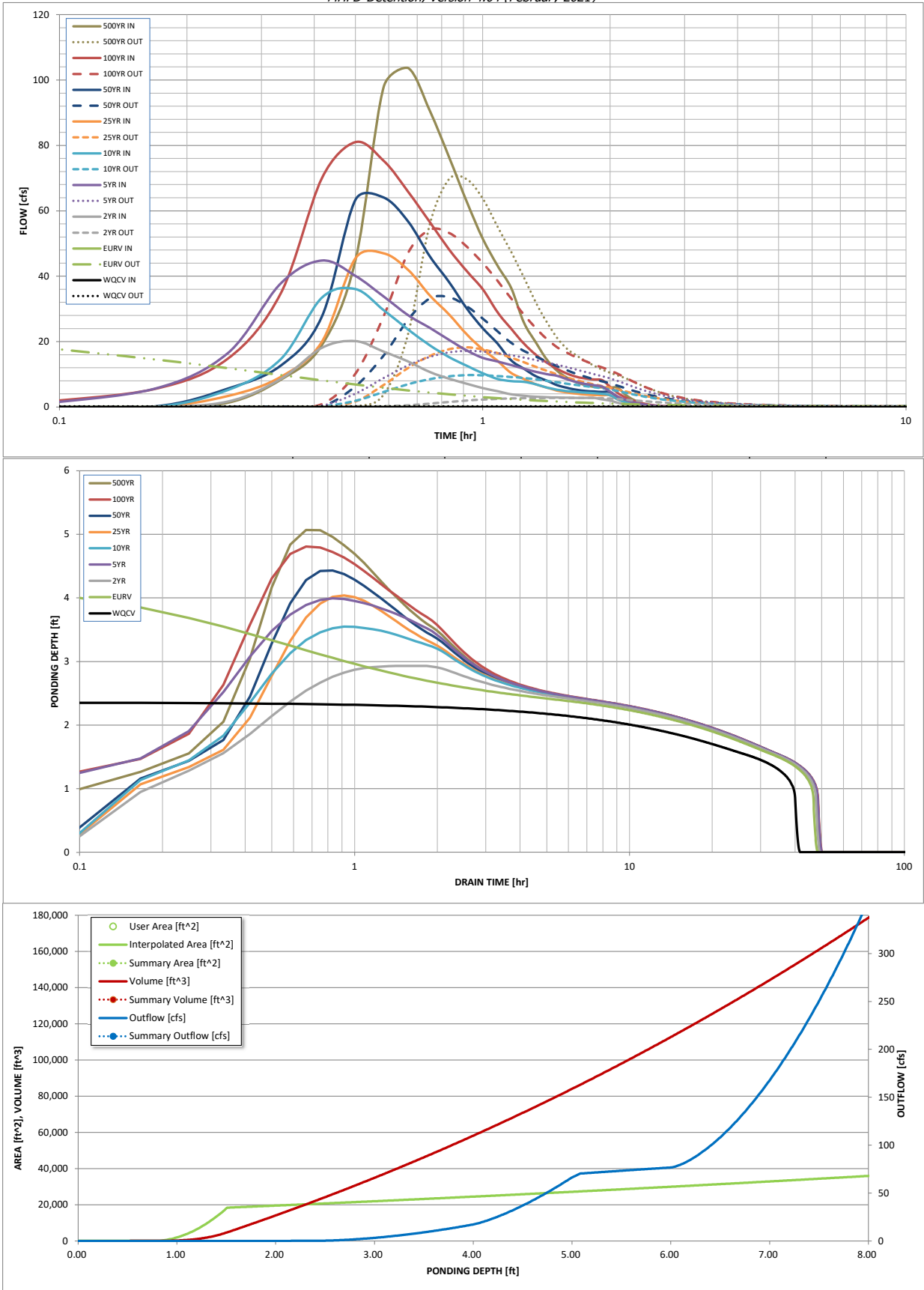
## Routed Hydrograph Results

The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through A)

|  | WQCV               | EURV            | 2 Year             | 5 Year             | 10 Year            | 25 Year         | 50 Year         | 100 Year        |
|--|--------------------|-----------------|--------------------|--------------------|--------------------|-----------------|-----------------|-----------------|
| Design Storm Return Period =                       | N/A                | N/A             | 1.19               | 1.50               | 1.75               | 2.00            | 2.25            | 2.52            |
| One-Hour Rainfall Depth (in) =                     | N/A                | N/A             | 1.19               | 1.50               | 1.75               | 2.00            | 2.25            | 2.52            |
| CUHP Runoff Volume (acre-ft) =                     | 0.488              | 1.634           | 1.042              | 1.456              | 1.884              | 2.406           | 3.276           | 3.989           |
| User Override Inflow Hydrograph Volume (acre-ft) = | N/A                | N/A             | 1.042              | 2.782              | 1.884              | 2.406           | 3.276           | 4.881           |
| CUHP Predevelopment Peak Q (cfs) =                 | N/A                | N/A             | 0.3                | 2.3                | 6.7                | 15.4            | 26.0            | 34.7            |
| OPTIONAL Override Predevelopment Peak Q (cfs) =    | N/A                | N/A             |                    | 20.0               |                    |                 |                 | 55.0            |
| Predevelopment Unit Peak Flow, q (cfs/acre) =      | N/A                | N/A             | 0.01               | 0.87               | 0.29               | 0.67            | 1.13            | 2.39            |
| Peak Inflow Q (cfs) =                              | N/A                | N/A             | 20.1               | 44.8               | 36.0               | 47.0            | 64.0            | 81.0            |
| Peak Outflow Q (cfs) =                             | 0.2                | 29.5            | 2.8                | 17.2               | 9.8                | 18.2            | 33.6            | 54.2            |
| Ratio Peak Outflow to Predevelopment Q =           | N/A                | N/A             | N/A                | 0.9                | 1.4                | 1.2             | 1.3             | 1.0             |
| Structure Controlling Flow =                       | Vertical Orifice 1 | Overflow Weir 1 | Vertical Orifice 1 | Vertical Orifice 1 | Vertical Orifice 1 | Overflow Weir 1 | Overflow Weir 1 | Overflow Weir 1 |
| Max Velocity through Grate 1 (fps) =               | N/A                | 0.87            | N/A                | N/A                | N/A                | 0.0             | 0.7             | 1.7             |
| Max Velocity through Grate 2 (fps) =               | N/A                | N/A             | N/A                | N/A                | N/A                | N/A             | N/A             | N/A             |
| Time to Drain 97% of Inflow Volume (hours) =       | 39                 | 41              | 44                 | 39                 | 42                 | 40              | 37              | 33              |
| Time to Drain 99% of Inflow Volume (hours) =       | 40                 | 45              | 47                 | 45                 | 46                 | 46              | 45              | 43              |
| Maximum Ponding Depth (ft) =                       | 2.36               | 4.52            | 2.93               | 3.99               | 3.55               | 4.04            | 4.43            | 4.81            |
| Area at Maximum Ponding Depth (acres) =            | 0.47               | 0.59            | 0.50               | 0.56               | 0.54               | 0.57            | 0.59            | 0.61            |
| Maximum Volume Stored (acre-ft) =                  | 0.490              | 1.637           | 0.767              | 1.331              | 1.083              | 1.353           | 1.584           | 1.806           |

DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-DETENTION, Version 4.04 (February 2021)



| S-A-V-D Chart Axis Override | X-axis | Left Y-Axis | Right Y-Axis |
|-----------------------------|--------|-------------|--------------|
| minimum bound               |        |             |              |
| maximum bound               |        |             |              |

# DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename: ..\SWM\Outflow hydrographs\Pond6\_OutflowHydrograph.xlsx

## Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

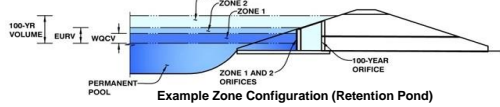
|               | SOURCE  | CUHP       | CUHP       | CUHP         | USER         | CUHP          | CUHP          | CUHP          | USER           | CUHP           |
|---------------|---------|------------|------------|--------------|--------------|---------------|---------------|---------------|----------------|----------------|
| Time Interval | TIME    | WQCV [cfs] | EURV [cfs] | 2 Year [cfs] | 5 Year [cfs] | 10 Year [cfs] | 25 Year [cfs] | 50 Year [cfs] | 100 Year [cfs] | 500 Year [cfs] |
| 5.00 min      | 0:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 0:05:00 | 0.00       | 0.00       | 0.00         | 0.41         | 0.00          | 0.00          | 0.00          | 1.01           | 0.00           |
|               | 0:10:00 | 0.00       | 0.00       | 0.00         | 5.50         | 0.00          | 0.00          | 0.16          | 5.44           | 1.32           |
|               | 0:15:00 | 0.00       | 0.00       | 1.65         | 16.52        | 5.18          | 3.36          | 5.62          | 14.77          | 8.33           |
|               | 0:20:00 | 0.00       | 0.00       | 8.60         | 37.83        | 14.67         | 9.22          | 12.68         | 34.79          | 18.87          |
|               | 0:25:00 | 0.00       | 0.00       | 18.09        | 44.78        | 33.40         | 19.95         | 27.64         | 69.96          | 44.82          |
|               | 0:30:00 | 0.00       | 0.00       | 20.15        | 40.12        | 36.04         | 45.48         | 63.36         | 81.03          | 97.91          |
|               | 0:35:00 | 0.00       | 0.00       | 16.94        | 33.76        | 29.63         | 47.00         | 64.04         | 75.29          | 103.64         |
|               | 0:40:00 | 0.00       | 0.00       | 13.89        | 28.06        | 23.69         | 41.94         | 56.72         | 65.86          | 90.52          |
|               | 0:45:00 | 0.00       | 0.00       | 10.69        | 24.15        | 18.86         | 34.08         | 46.05         | 56.52          | 76.40          |
|               | 0:50:00 | 0.00       | 0.00       | 8.62         | 20.52        | 15.26         | 28.31         | 38.19         | 48.17          | 62.76          |
|               | 0:55:00 | 0.00       | 0.00       | 7.12         | 17.27        | 12.58         | 22.18         | 30.11         | 41.54          | 51.52          |
|               | 1:00:00 | 0.00       | 0.00       | 5.79         | 15.04        | 10.31         | 17.65         | 24.11         | 36.06          | 43.26          |
|               | 1:05:00 | 0.00       | 0.00       | 4.82         | 13.92        | 8.58          | 14.12         | 19.40         | 29.01          | 36.45          |
|               | 1:10:00 | 0.00       | 0.00       | 3.89         | 12.85        | 7.88          | 10.43         | 14.27         | 23.97          | 25.86          |
|               | 1:15:00 | 0.00       | 0.00       | 3.42         | 11.72        | 7.67          | 8.59          | 11.74         | 19.45          | 19.89          |
|               | 1:20:00 | 0.00       | 0.00       | 3.15         | 10.79        | 6.93          | 6.94          | 9.44          | 16.03          | 14.49          |
|               | 1:25:00 | 0.00       | 0.00       | 3.00         | 10.06        | 5.95          | 5.95          | 8.05          | 13.55          | 11.02          |
|               | 1:30:00 | 0.00       | 0.00       | 2.90         | 9.51         | 5.30          | 5.01          | 6.68          | 11.61          | 8.96           |
|               | 1:35:00 | 0.00       | 0.00       | 2.84         | 8.46         | 4.86          | 4.43          | 5.82          | 10.19          | 7.57           |
|               | 1:40:00 | 0.00       | 0.00       | 2.79         | 7.61         | 4.57          | 4.06          | 5.27          | 9.21           | 6.69           |
|               | 1:45:00 | 0.00       | 0.00       | 2.77         | 7.03         | 4.38          | 3.81          | 4.90          | 8.72           | 6.17           |
|               | 1:50:00 | 0.00       | 0.00       | 2.77         | 6.64         | 4.25          | 3.69          | 4.72          | 8.40           | 5.99           |
|               | 1:55:00 | 0.00       | 0.00       | 2.30         | 6.20         | 4.02          | 3.61          | 4.60          | 8.20           | 5.90           |
|               | 2:00:00 | 0.00       | 0.00       | 1.98         | 4.66         | 3.60          | 3.58          | 4.55          | 6.18           | 5.90           |
|               | 2:05:00 | 0.00       | 0.00       | 1.30         | 3.24         | 2.36          | 2.35          | 2.99          | 4.29           | 3.89           |
|               | 2:10:00 | 0.00       | 0.00       | 0.82         | 2.25         | 1.52          | 1.52          | 1.93          | 3.00           | 2.50           |
|               | 2:15:00 | 0.00       | 0.00       | 0.52         | 1.57         | 0.95          | 0.96          | 1.21          | 2.06           | 1.58           |
|               | 2:20:00 | 0.00       | 0.00       | 0.30         | 1.09         | 0.56          | 0.57          | 0.73          | 1.43           | 0.94           |
|               | 2:25:00 | 0.00       | 0.00       | 0.16         | 0.74         | 0.32          | 0.34          | 0.43          | 0.96           | 0.56           |
|               | 2:30:00 | 0.00       | 0.00       | 0.07         | 0.48         | 0.15          | 0.17          | 0.21          | 0.62           | 0.28           |
|               | 2:35:00 | 0.00       | 0.00       | 0.02         | 0.32         | 0.05          | 0.06          | 0.07          | 0.41           | 0.09           |
|               | 2:40:00 | 0.00       | 0.00       | 0.00         | 0.24         | 0.00          | 0.00          | 0.00          | 0.31           | 0.00           |
|               | 2:45:00 | 0.00       | 0.00       | 0.00         | 0.18         | 0.00          | 0.00          | 0.00          | 0.24           | 0.00           |
|               | 2:50:00 | 0.00       | 0.00       | 0.00         | 0.13         | 0.00          | 0.00          | 0.00          | 0.18           | 0.00           |
|               | 2:55:00 | 0.00       | 0.00       | 0.00         | 0.09         | 0.00          | 0.00          | 0.00          | 0.12           | 0.00           |
|               | 3:00:00 | 0.00       | 0.00       | 0.00         | 0.06         | 0.00          | 0.00          | 0.00          | 0.08           | 0.00           |
|               | 3:05:00 | 0.00       | 0.00       | 0.00         | 0.04         | 0.00          | 0.00          | 0.00          | 0.06           | 0.00           |
|               | 3:10:00 | 0.00       | 0.00       | 0.00         | 0.02         | 0.00          | 0.00          | 0.00          | 0.03           | 0.00           |
|               | 3:15:00 | 0.00       | 0.00       | 0.00         | 0.01         | 0.00          | 0.00          | 0.00          | 0.02           | 0.00           |
|               | 3:20:00 | 0.00       | 0.00       | 0.00         | 0.01         | 0.00          | 0.00          | 0.00          | 0.01           | 0.00           |
|               | 3:25:00 | 0.00       | 0.00       | 0.00         | 0.01         | 0.00          | 0.00          | 0.00          | 0.01           | 0.00           |
|               | 3:30:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:35:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:40:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:45:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:50:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:55:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:05:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:10:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:15:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:20:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:25:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:30:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:35:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:40:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:45:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:50:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:55:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:05:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:10:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:15:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:20:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:25:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:30:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:35:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:40:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:45:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:50:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:55:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 6:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |

# DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.04 (February 2021)

Project: **Flying Horse North**

Basin ID: **Pond 14**



Example Zone Configuration (Retention Pond)

## Watershed Information

|   |                |
|---|----------------|
| Selected BMP Type =                     | <b>EDB</b>     |
| Watershed Area =                        | 97.53 acres    |
| Watershed Length =                      | 4,027 ft       |
| Watershed Length to Centroid =          | 2,183 ft       |
| Watershed Slope =                       | 0.059 ft/ft    |
| Watershed Imperviousness =              | 10.00% percent |
| Percentage Hydrologic Soil Group A =    | 0.0% percent   |
| Percentage Hydrologic Soil Group B =    | 100.0% percent |
| Percentage Hydrologic Soil Groups C/D = | 0.0% percent   |
| Target WQCV Drain Time =                | 40.0 hours     |
| Location for 1-hr Rainfall Depths =     | User Input     |

After providing required inputs above including 1-hour rainfall depths, click "Run CUHP" to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

|  |                  |      |        |
|--|------------------|------|--------|
| Water Quality Capture Volume (WQCV) =  | 0.545 acre-feet  |      |        |
| Excess Urban Runoff Volume (EURV) =    | 0.917 acre-feet  |      |        |
| 2-yr Runoff Volume (P1 = 0.92 in.) =   | 0.450 acre-feet  | 0.92 | inches |
| 5-yr Runoff Volume (P1 = 1.2 in.) =    | 1.153 acre-feet  | 1.20 | inches |
| 10-yr Runoff Volume (P1 = 1.45 in.) =  | 2.407 acre-feet  | 1.45 | inches |
| 25-yr Runoff Volume (P1 = 1.69 in.) =  | 4.971 acre-feet  |      |        |
| 50-yr Runoff Volume (P1 = 2.15 in.) =  | 8.392 acre-feet  | 2.15 | inches |
| 100-yr Runoff Volume (P1 = 2.49 in.) = | 11.684 acre-feet | 2.49 | inches |
| 500-yr Runoff Volume (P1 = 3.14 in.) = | 16.938 acre-feet |      |        |
| Approximate 2-yr Detention Volume =    | 0.452 acre-feet  |      |        |
| Approximate 5-yr Detention Volume =    | 0.734 acre-feet  |      |        |
| Approximate 10-yr Detention Volume =   | 1.579 acre-feet  |      |        |
| Approximate 25-yr Detention Volume =   | 2.249 acre-feet  |      |        |
| Approximate 50-yr Detention Volume =   | 2.660 acre-feet  |      |        |
| Approximate 100-yr Detention Volume =  | 3.555 acre-feet  |      |        |

## Define Zones and Basin Geometry

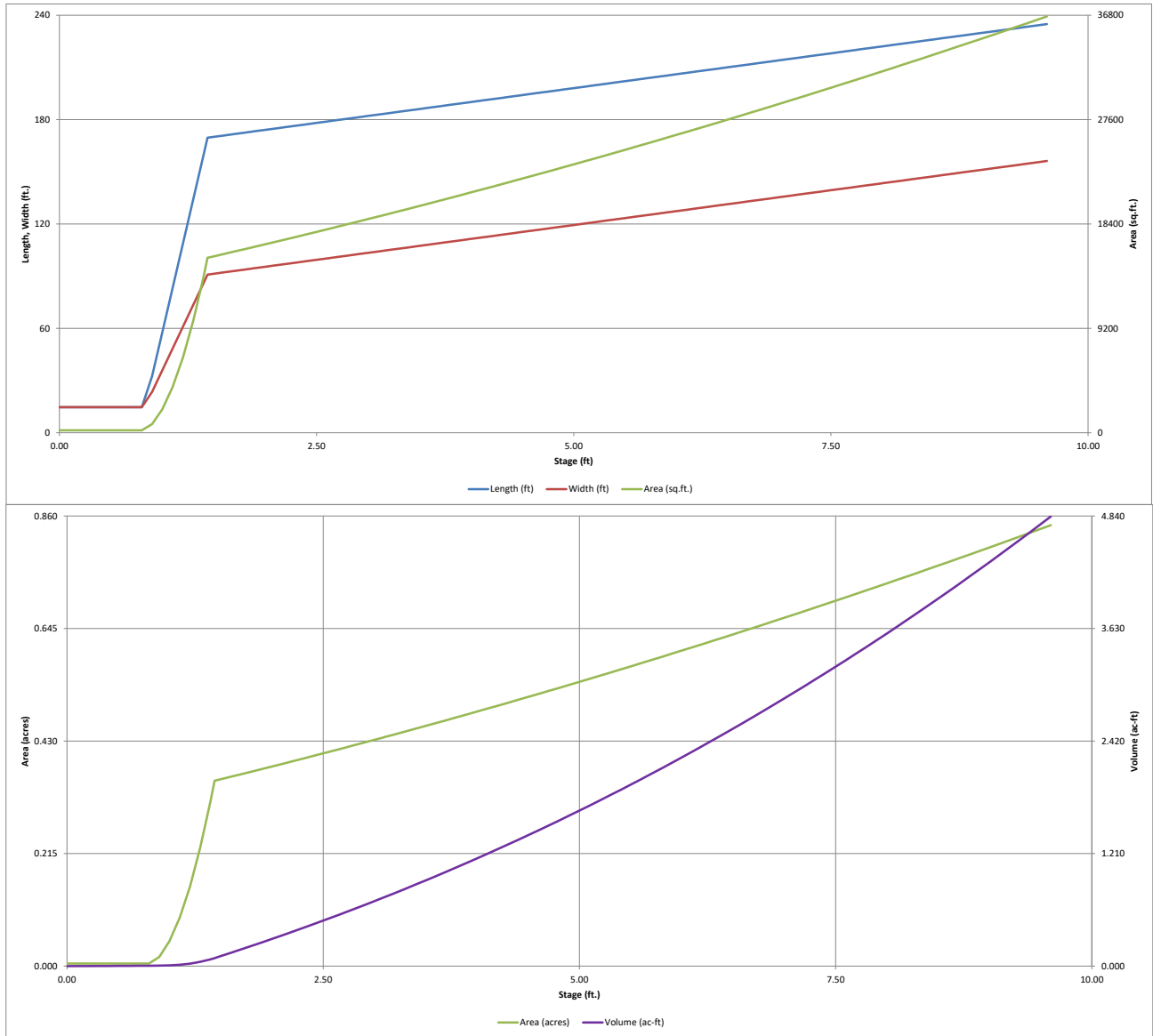
|   |                         |
|---|-------------------------|
| Zone 1 Volume (WQCV) =                                  | 0.545 acre-feet         |
| Zone 2 Volume (5-year - Zone 1) =                       | 0.190 acre-feet         |
| Zone 3 Volume (100-year - Zones 1 & 2) =                | 2.821 acre-feet         |
| Total Detention Basin Volume =                          | 3.555 acre-feet         |
| Initial Surge Volume (ISV) =                            | 71 ft <sup>3</sup>      |
| Initial Surge Depth (ISD) =                             | 0.33 ft                 |
| Total Available Detention Depth (H <sub>total</sub> ) = | 8.00 ft                 |
| Depth of Trickle Channel (H <sub>TC</sub> ) =           | 0.50 ft                 |
| Slope of Trickle Channel (S <sub>TC</sub> ) =           | 0.004 ft/ft             |
| Slopes of Main Basin Sides (S <sub>main</sub> ) =       | 4 H:V                   |
| Basin Length-to-Width Ratio (R <sub>LW</sub> ) =        | 2                       |
| Initial Surge Area (A <sub>ISV</sub> ) =                | 216 ft <sup>2</sup>     |
| Surcharge Volume Length (L <sub>ISV</sub> ) =           | 14.7 ft                 |
| Surcharge Volume Width (W <sub>ISV</sub> ) =            | 14.7 ft                 |
| Depth of Basin Floor (H <sub>FLOOR</sub> ) =            | 0.61 ft                 |
| Length of Basin Floor (L <sub>FLOOR</sub> ) =           | 169.6 ft                |
| Width of Basin Floor (W <sub>FLOOR</sub> ) =            | 90.9 ft                 |
| Area of Basin Floor (A <sub>FLOOR</sub> ) =             | 15,425 ft <sup>2</sup>  |
| Volume of Basin Floor (V <sub>FLOOR</sub> ) =           | 3,551 ft <sup>3</sup>   |
| Depth of Main Basin (H <sub>MAIN</sub> ) =              | 6.56 ft                 |
| Length of Main Basin (L <sub>MAIN</sub> ) =             | 222.1 ft                |
| Width of Main Basin (W <sub>MAIN</sub> ) =              | 143.4 ft                |
| Area of Main Basin (A <sub>MAIN</sub> ) =               | 31,853 ft <sup>2</sup>  |
| Volume of Main Basin (V <sub>MAIN</sub> ) =             | 151,852 ft <sup>3</sup> |
| Calculated Total Basin Volume (V <sub>total</sub> ) =   | <b>3.572</b> acre-feet  |

| Depth Increment =           | 0.10       | ft                           |             |            |                         |   |             |                           |                |  |
|-----------------------------|------------|------------------------------|-------------|------------|-------------------------|---|-------------|---------------------------|----------------|--|
| Stage - Storage Description | Stage (ft) | Optional Override Stage (ft) | Length (ft) | Width (ft) | Area (ft <sup>2</sup> ) | Optional Override Area (ft <sup>2</sup> ) | Area (acre) | Volume (ft <sup>3</sup> ) | Volume (ac-ft) |  |
| Top of Micropool            | 0.00       |                              | 14.7        | 14.7       | 216                     |   | 0.005       |                           |                |  |
| ISV                         | 0.33       |                              | 14.7        | 14.7       | 216                     |   | 0.005       | 71                        | 0.002          |  |
|                             | 0.40       |                              | 14.7        | 14.7       | 216                     |   | 0.005       | 86                        | 0.002          |  |
|                             | 0.50       |                              | 14.7        | 14.7       | 216                     |   | 0.005       | 108                       | 0.002          |  |
|                             | 0.60       |                              | 14.7        | 14.7       | 216                     |   | 0.005       | 129                       | 0.003          |  |
|                             | 0.70       |                              | 14.7        | 14.7       | 216                     |   | 0.005       | 151                       | 0.003          |  |
|                             | 0.80       |                              | 14.7        | 14.7       | 216                     |   | 0.005       | 173                       | 0.004          |  |
|                             | 0.90       |                              | 32.5        | 23.4       | 761                     |   | 0.017       | 211                       | 0.005          |  |
|                             | 1.00       |                              | 57.9        | 35.9       | 2,079                   |   | 0.048       | 348                       | 0.008          |  |
|                             | 1.10       |                              | 83.3        | 48.4       | 4,033                   |   | 0.093       | 648                       | 0.015          |  |
|                             | 1.20       |                              | 108.7       | 60.9       | 6,622                   |   | 0.152       | 1,176                     | 0.027          |  |
|                             | 1.30       |                              | 134.1       | 73.4       | 9,845                   |   | 0.226       | 1,994                     | 0.046          |  |
| Floor                       | 1.40       |                              | 159.5       | 85.9       | 13,704                  |   | 0.315       | 3,166                     | 0.073          |  |
|                             | 1.44       |                              | 169.6       | 90.9       | 15,425                  |   | 0.354       | 3,748                     | 0.086          |  |
|                             | 1.50       |                              | 170.1       | 91.4       | 15,550                  |   | 0.357       | 4,678                     | 0.107          |  |
|                             | 1.60       |                              | 170.9       | 92.2       | 15,760                  |   | 0.362       | 6,243                     | 0.143          |  |
|                             | 1.70       |                              | 171.7       | 93.0       | 15,971                  |   | 0.367       | 7,830                     | 0.180          |  |
|                             | 1.80       |                              | 172.5       | 93.8       | 16,184                  |   | 0.372       | 9,437                     | 0.217          |  |
|                             | 1.90       |                              | 173.3       | 94.6       | 16,397                  |   | 0.376       | 11,066                    | 0.254          |  |
|                             | 2.00       |                              | 174.1       | 95.4       | 16,612                  |   | 0.381       | 12,717                    | 0.292          |  |
|                             | 2.10       |                              | 174.9       | 96.2       | 16,829                  |   | 0.386       | 14,389                    | 0.330          |  |
|                             | 2.20       |                              | 175.7       | 97.0       | 17,046                  |   | 0.391       | 16,083                    | 0.369          |  |
|                             | 2.30       |                              | 176.5       | 97.8       | 17,265                  |   | 0.396       | 17,798                    | 0.409          |  |
|                             | 2.40       |                              | 177.3       | 98.6       | 17,485                  |   | 0.401       | 19,536                    | 0.448          |  |
|                             | 2.50       |                              | 178.1       | 99.4       | 17,707                  |   | 0.406       | 21,295                    | 0.489          |  |
|                             | 2.60       |                              | 178.9       | 100.2      | 17,929                  |   | 0.412       | 23,077                    | 0.530          |  |
| Zone 1 (WQCV)               | 2.64       |                              | 179.2       | 100.5      | 18,019                  |   | 0.414       | 23,796                    | 0.546          |  |
|                             | 2.70       |                              | 179.7       | 101.0      | 18,153                  |   | 0.417       | 24,881                    | 0.571          |  |
|                             | 2.80       |                              | 180.5       | 101.8      | 18,378                  |   | 0.422       | 26,708                    | 0.613          |  |
|                             | 2.90       |                              | 181.3       | 102.6      | 18,605                  |   | 0.427       | 28,557                    | 0.656          |  |
|                             | 3.00       |                              | 182.1       | 103.4      | 18,833                  |   | 0.432       | 30,429                    | 0.699          |  |
| Zone 2 (5-year)             | 3.09       |                              | 182.8       | 104.1      | 19,039                  |   | 0.437       | 32,133                    | 0.738          |  |
|                             | 3.10       |                              | 182.9       | 104.2      | 19,062                  |   | 0.438       | 32,323                    | 0.742          |  |
|                             | 3.20       |                              | 183.7       | 105.0      | 19,292                  |   | 0.443       | 34,241                    | 0.786          |  |
|                             | 3.30       |                              | 184.5       | 105.8      | 19,524                  |   | 0.448       | 36,182                    | 0.831          |  |
|                             | 3.40       |                              | 185.3       | 106.6      | 19,757                  |   | 0.454       | 38,146                    | 0.876          |  |
|                             | 3.50       |                              | 186.1       | 107.4      | 19,991                  |   | 0.459       | 40,133                    | 0.921          |  |
|                             | 3.60       |                              | 186.9       | 108.2      | 20,226                  |   | 0.464       | 42,144                    | 0.967          |  |
|                             | 3.70       |                              | 187.7       | 109.0      | 20,463                  |   | 0.470       | 44,179                    | 1.014          |  |
|                             | 3.80       |                              | 188.5       | 109.8      | 20,701                  |   | 0.475       | 46,237                    | 1.061          |  |
|                             | 3.90       |                              | 189.3       | 110.6      | 20,940                  |   | 0.481       | 48,319                    | 1.109          |  |
|                             | 4.00       |                              | 190.1       | 111.4      | 21,181                  |   | 0.486       | 50,425                    | 1.158          |  |
|                             | 4.10       |                              | 190.9       | 112.2      | 21,423                  |   | 0.492       | 52,555                    | 1.206          |  |
|                             | 4.20       |                              | 191.7       | 113.0      | 21,666                  |   | 0.497       | 54,709                    | 1.256          |  |
|                             | 4.30       |                              | 192.5       | 113.8      | 21,910                  |   | 0.503       | 56,888                    | 1.306          |  |
|                             | 4.40       |                              | 193.3       | 114.6      | 22,156                  |   | 0.509       | 59,091                    | 1.357          |  |
|                             | 4.50       |                              | 194.1       | 115.4      | 22,403                  |   | 0.514       | 61,319                    | 1.408          |  |
|                             | 4.60       |                              | 194.9       | 116.2      | 22,651                  |   | 0.520       | 63,572                    | 1.459          |  |
|                             | 4.70       |                              | 195.7       | 117.0      | 22,901                  |   | 0.526       | 65,850                    | 1.512          |  |
|                             | 4.80       |                              | 196.5       | 117.8      | 23,151                  |   | 0.531       | 68,152                    | 1.565          |  |
|                             | 4.90       |                              | 197.3       | 118.6      | 23,404                  |   | 0.537       | 70,480                    | 1.618          |  |
|                             | 5.00       |                              | 198.1       | 119.4      | 23,657                  |   | 0.543       | 72,833                    | 1.672          |  |
|                             | 5.10       |                              | 198.9       | 120.2      | 23,912                  |   | 0.549       | 75,211                    | 1.727          |  |
|                             | 5.20       |                              | 199.7       | 121.0      | 24,168                  |   | 0.555       | 77,615                    | 1.782          |  |
|                             | 5.30       |                              | 200.5       | 121.8      | 24,425                  |   | 0.561       | 80,045                    | 1.838          |  |
|                             | 5.40       |                              | 201.3       | 122.6      | 24,683                  |   | 0.567       | 82,500                    | 1.894          |  |
|                             | 5.50       |                              | 202.1       | 123.4      | 24,943                  |   | 0.573       | 84,982                    | 1.951          |  |
|                             | 5.60       |                              | 202.9       | 124.2      | 25,204                  |   | 0.579       | 87,489                    | 2.008          |  |
|                             | 5.70       |                              | 203.7       | 125.0      | 25,466                  |   | 0.585       | 90,023                    | 2.067          |  |
|                             | 5.80       |                              | 204.5       | 125.8      | 25,730                  |   | 0.591       | 92,582                    | 2.125          |  |
|                             | 5.90       |                              | 205.3       | 126.6      | 25,995                  |   | 0.597       | 95,169                    | 2.185          |  |
|                             | 6.00       |                              | 206.1       | 127.4      | 26,261                  |   | 0.603       | 97,781                    | 2.245          |  |
|                             | 6.10       |                              | 206.9       | 128.2      | 26,529                  |   | 0.609       | 100,421                   | 2.305          |  |
|                             | 6.20       |                              | 207.7       | 129.0      | 26,797                  |   | 0.615       | 103,087                   | 2.367          |  |
|                             | 6.30       |                              | 208.5       | 129.8      | 27,067                  |   | 0.621       | 105,780                   | 2.428          |  |
|                             | 6.40       |                              | 209.3       | 130.6      | 27,339                  |   | 0.628       | 108,501                   | 2.491          |  |
|                             | 6.50       |                              | 210.1       | 131.4      | 27,611                  |   | 0.634       | 111,248                   | 2.554          |  |
|                             | 6.60       |                              | 210.9       | 132.2      | 27,885                  |   | 0.640       | 114,023                   | 2.618          |  |
|                             | 6.70       |                              | 211.7       | 133.0      | 28,160                  |   | 0.646       | 116,825                   | 2.682          |  |
|                             | 6.80       |                              | 212.5       | 133.8      | 28,437                  |   | 0.653       | 119,655                   | 2.747          |  |
|                             | 6.90       |                              | 213.3       | 134.6      | 28,714                  |   | 0.659       | 122,513                   | 2.813          |  |
|                             | 7.00       |                              | 214.1       | 135.4      | 28,993                  |   | 0.666       | 125,398                   | 2.879          |  |
|                             | 7.10       |                              | 214.9       | 136.2      | 29,274                  |   | 0.672       | 128,311                   | 2.946          |  |
|                             | 7.20       |                              | 215.7       | 137.0      | 29,555                  |   | 0.678       | 131,253                   | 3.013          |  |
|                             | 7.30       |                              | 216.5       | 137.8      | 29,838                  |   | 0.685       | 134,222                   | 3.081          |  |
|                             | 7.40       |                              | 217.3       | 138.6      | 30,122                  |   | 0.692       | 137,220                   | 3.150          |  |
|                             | 7.50       |                              | 218.1       | 139.4      | 30,407                  |   | 0.698       | 140,247                   | 3.220          |  |
|                             | 7.60       |                              | 218.9       | 140.2      | 30,694                  |   | 0.705       | 143,302                   | 3.290          |  |
|                             | 7.70       |                              | 219.7       | 141.0      | 30,982                  |   | 0.711       | 146,386                   | 3.361          |  |
|                             | 7.80       |                              | 220.5       | 141.8      | 31,271                  |   | 0.718       | 149,498                   | 3.432          |  |
|                             | 7.90       |                              | 221.3       | 142.6      | 31,562                  |   | 0.725       | 152,640                   | 3.504          |  |
| Zone 3 (100-year)           | 7.98       |                              | 221.9       | 143.3      | 31,795                  |   | 0.730       | 155,174                   | 3.562          |  |
|                             | 8.00       |                              | 222.1       | 143.4      | 31,853                  |   | 0.731       | 155,811                   | 3.577          |  |
|                             | 8.10       |                              | 222.9       | 144.2      | 32,147                  |   | 0.738       | 159,011                   | 3.650          |  |
|                             | 8.20       |                              | 223.7       | 145.0      | 32,441                  |   | 0.745       | 162,240                   | 3.725          |  |
|                             | 8.30       |                              | 224.5       | 145.8      | 32,736                  |   | 0.752       | 165,499                   | 3.799          |  |
|                             | 8.40       |                              | 225.3       | 146.6      | 33,033                  |   | 0.758       | 168,787                   | 3.875          |  |
|                             | 8.50       |                              | 226.1       | 147.4      | 33,332                  |   | 0.765       | 172,106                   | 3.951          |  |
|                             | 8.60       |                              | 226.9       | 148.2      | 33,631                  |   | 0.772       | 175,454                   | 4.028          |  |
|                             | 8.70       |                              | 227.7       | 149.0      | 33,932                  |   | 0.779       | 178,832                   | 4.105          |  |
|                             | 8.80       |                              | 228.5       | 149.8      | 34,234                  |   | 0.786       | 182,240                   | 4.184          |  |
|                             | 8.90       |                              | 229.3       | 150.6      | 34,537                  |   | 0.793       | 185,679                   | 4.263          |  |
|                             | 9.00       |                              | 230.1       | 151.4      | 34,842                  |   | 0.800       | 189,147                   | 4.342          |  |
|                             | 9.10       |                              | 230.9       | 152.2      | 35,147                  |   | 0.807       | 192,647                   | 4.423          |  |
|                             | 9.20       |                              | 231.7       | 153.0      | 35,455                  |   | 0.814       | 196,177                   | 4.504          |  |
|                             | 9.30       |                              | 232.5       | 153.8      | 35,763                  |   | 0.821       | 199,738                   | 4.585          |  |
|                             | 9.40       |                              | 233.3       | 154.6      | 36,073                  |   | 0.828       | 203,330                   | 4.668          |  |
|                             | 9.50       |                              | 234.1       | 155.4      | 36,384                  |   | 0.835       | 206,952                   | 4.751          |  |
|                             | 9.60       |                              | 234.9       | 156.2      | 36,696                  |   | 0.842       | 210,606                   | 4.835          |  |



# DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.04 (February 2021)

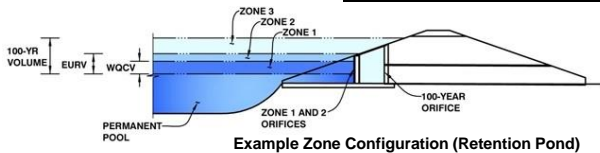


# DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.04 (February 2021)

Project: Flying Horse North

Basin ID: Pond 14



Example Zone Configuration (Retention Pond)

|                   | Estimated Stage (ft) | Estimated Volume (ac-ft) | Outlet Type          |
|-------------------|----------------------|--------------------------|----------------------|
| Zone 1 (WQCV)     | 2.64                 | 0.545                    | Orifice Plate        |
| Zone 2 (5-year)   | 3.09                 | 0.190                    | Weir&Pipe (Circular) |
| Zone 3 (100-year) | 7.98                 | 2.821                    | Weir&Pipe (Restrict) |
| Total (all zones) |                      | 3.555                    |                      |

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth = N/A ft (distance below the filtration media surface)  
Underdrain Orifice Diameter = N/A inches

Calculated Parameters for Underdrain  
Underdrain Orifice Area = N/A ft<sup>2</sup>  
Underdrain Orifice Centroid = N/A feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice = 0.00 ft (relative to basin bottom at Stage = 0 ft)  
Depth at top of Zone using Orifice Plate = 2.36 ft (relative to basin bottom at Stage = 0 ft)  
Orifice Plate: Orifice Vertical Spacing = 9.40 inches  
Orifice Plate: Orifice Area per Row = 1.77 sq. inches (diameter = 1-1/2 inches)

Calculated Parameters for Plate  
WQ Orifice Area per Row = 1.229E-02 ft<sup>2</sup>  
Elliptical Half-Width = N/A feet  
Elliptical Slot Centroid = N/A feet  
Elliptical Slot Area = N/A ft<sup>2</sup>

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

|                                | Row 1 (required) | Row 2 (optional) | Row 3 (optional) | Row 4 (optional) | Row 5 (optional) | Row 6 (optional) | Row 7 (optional) | Row 8 (optional) |
|--------------------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|
| Stage of Orifice Centroid (ft) | 0.00             | 0.79             | 1.57             |                  |                  |                  |                  |                  |
| Orifice Area (sq. inches)      | 1.77             | 1.77             | 1.77             |                  |                  |                  |                  |                  |

|                                | Row 9 (optional) | Row 10 (optional) | Row 11 (optional) | Row 12 (optional) | Row 13 (optional) | Row 14 (optional) | Row 15 (optional) | Row 16 (optional) |
|--------------------------------|------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| Stage of Orifice Centroid (ft) |                  |                   |                   |                   |                   |                   |                   |                   |
| Orifice Area (sq. inches)      |                  |                   |                   |                   |                   |                   |                   |                   |

User Input: Vertical Orifice (Circular or Rectangular)

|   | Not Selected | Not Selected |   |
|---|--------------|--------------|---|
| Invert of Vertical Orifice =                  | N/A          | N/A          | ft (relative to basin bottom at Stage = 0 ft) |
| Depth at top of Zone using Vertical Orifice = | N/A          | N/A          | ft (relative to basin bottom at Stage = 0 ft) |
| Vertical Orifice Diameter =                   | N/A          | N/A          | inches  |

Calculated Parameters for Vertical Orifice  
Vertical Orifice Area = N/A ft<sup>2</sup>  
Vertical Orifice Centroid = N/A feet

User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe)

|                                       | Zone 2 Weir  | Zone 3 Weir  |   |
|---------------------------------------|--------------|--------------|---|
| Overflow Weir Front Edge Height, Ho = | 2.64         | 3.09         | ft (relative to basin bottom at Stage = 0 ft) |
| Overflow Weir Front Edge Length =     | 8.00         | 8.00         | feet  |
| Overflow Weir Grate Slope =           | 0.00         | 4.00         | H:V   |
| Horiz. Length of Weir Sides =         | 8.00         | 16.00        | feet  |
| Overflow Grate Type =                 | Type C Grate | Type C Grate |   |
| Debris Clogging % =                   | 50%          | 50%          | %   |

Calculated Parameters for Overflow Weir  
Height of Grate Upper Edge, H<sub>u</sub> = 2.64 feet  
Overflow Weir Slope Length = 8.00 feet  
Grate Open Area / 100-yr Orifice Area = 9.07  
Overflow Grate Open Area w/o Debris = 44.54 ft<sup>2</sup>  
Overflow Grate Open Area w/ Debris = 22.27 ft<sup>2</sup>

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

|  | Zone 2 Circular | Zone 3 Restrictor |  |
|--|-----------------|-------------------|--|
| Depth to Invert of Outlet Pipe =             | 2.64            | 3.09              | ft (distance below basin bottom at Stage = 0 ft) |
| Circular Orifice Diameter or Pipe Diameter = | 30.00           | 42.00             | inches   |
| Restrictor Plate Height Above Pipe Invert =  |                 | 30.00             | inches   |

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate  
Outlet Orifice Area = 4.91 ft<sup>2</sup>  
Outlet Orifice Centroid = 1.25 feet  
Half-Central Angle of Restrictor Plate on Pipe = N/A radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

|                                     |       |   |
|-------------------------------------|-------|---|
| Spillway Invert Stage =             | 8.00  | ft (relative to basin bottom at Stage = 0 ft) |
| Spillway Crest Length =             | 30.00 | feet  |
| Spillway End Slopes =               | 4.00  | H:V   |
| Freeboard above Max Water Surface = | 1.00  | feet  |

Calculated Parameters for Spillway  
Spillway Design Flow Depth = 0.93 feet  
Stage at Top of Freeboard = 9.93 feet  
Basin Area at Top of Freeboard = 0.87 acres  
Basin Volume at Top of Freeboard = 5.12 acre-ft

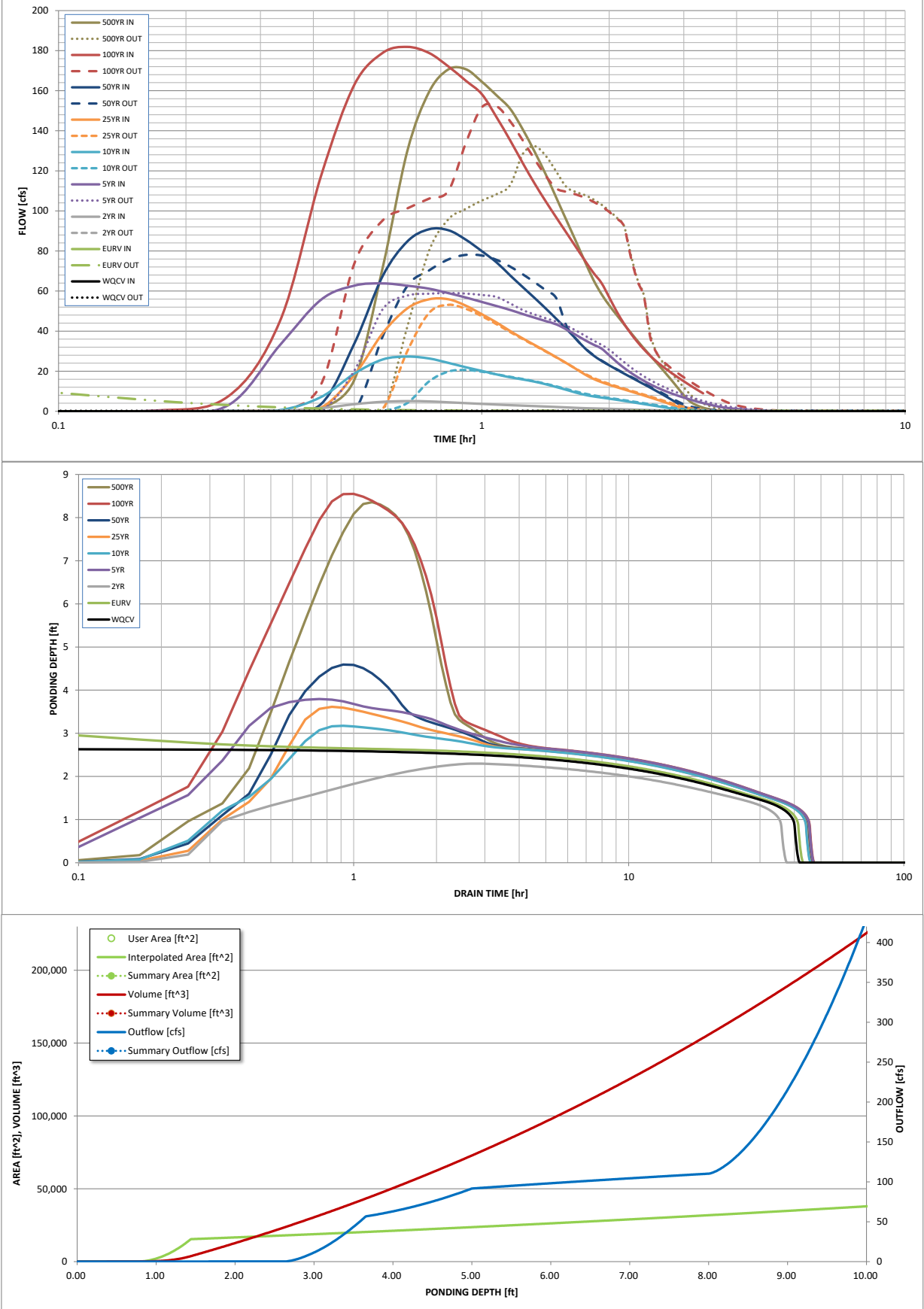
## Routed Hydrograph Results

The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).

|  | WQCV            | EURV            | 2 Year | 5 Year          | 10 Year         | 25 Year         | 50 Year         | 100 Year | 500 Year |
|--|-----------------|-----------------|--------|-----------------|-----------------|-----------------|-----------------|----------|----------|
| Design Storm Return Period =                       | N/A             | N/A             | 0.92   | 1.20            | 1.45            | 1.69            | 2.15            | 2.49     | 3.14     |
| One-Hour Rainfall Depth (in) =                     | 0.545           | 0.917           | 0.450  | 1.153           | 2.407           | 4.971           | 8.392           | 11.684   | 16.938   |
| CUHP Runoff Volume (acre-ft) =                     | N/A             | N/A             | 0.450  | 8.367           | 2.407           | 4.971           | 8.392           | 20.351   | 16.938   |
| User Override Inflow Hydrograph Volume (acre-ft) = | N/A             | N/A             | 1.0    | 7.0             | 20.9            | 50.3            | 84.7            | 115.8    | 164.5    |
| CUHP Predevelopment Peak Q (cfs) =                 | N/A             | N/A             | 0.01   | 0.61            | 0.21            | 0.52            | 0.87            | 1.77     | 1.69     |
| OPTIONAL Override Predevelopment Peak Q (cfs) =    | N/A             | N/A             | 5.1    | 63.8            | 27.3            | 55.9            | 90.8            | 181.9    | 170.7    |
| Predevelopment Unit Peak Flow, q (cfs/acre) =      | N/A             | N/A             | 0.2    | 59.0            | 20.6            | 53.1            | 78.1            | 152.3    | 132.3    |
| Peak Inflow Q (cfs) =                              | N/A             | N/A             | 1.0    | 1.0             | 1.0             | 1.1             | 0.9             | 0.9      | 0.8      |
| Peak Outflow Q (cfs) =                             | N/A             | N/A             | N/A    | N/A             | N/A             | N/A             | N/A             | N/A      | N/A      |
| Ratio Peak Outflow to Predevelopment Q =           | Overflow Weir 1 | Overflow Weir 2 | Plate  | Overflow Weir 2 | Overflow Weir 2 | Overflow Weir 2 | Overflow Weir 2 | Spillway | Spillway |
| Structure Controlling Flow =                       | N/A             | 0.92            | N/A    | 1.2             | 0.4             | 1.1             | 1.3             | 1.7      | 1.6      |
| Max Velocity through Grate 1 (fps) =               | N/A             | 0.02            | N/A    | 0.1             | 0.0             | 0.0             | 0.2             | 0.4      | 0.4      |
| Max Velocity through Grate 2 (fps) =               | 39              | 39              | 35     | 22              | 36              | 29              | 21              | 4        | 6        |
| Time to Drain 97% of Inflow Volume (hours) =       | 40              | 41              | 36     | 36              | 42              | 39              | 35              | 26       | 28       |
| Time to Drain 99% of Inflow Volume (hours) =       | 2.64            | 3.50            | 2.30   | 3.79            | 3.17            | 3.62            | 4.59            | 8.55     | 8.36     |
| Maximum Ponding Depth (ft) =                       | 0.41            | 0.46            | 0.40   | 0.47            | 0.44            | 0.46            | 0.52            | 0.77     | 0.75     |
| Area at Maximum Ponding Depth (acres) =            | 0.546           | 0.921           | 0.405  | 1.057           | 0.773           | 0.972           | 1.454           | 3.989    | 3.837    |
| Maximum Volume Stored (acre-ft) =                  |                 |                 |        |                 |                 |                 |                 |          |          |

DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-*Detention*, Version 4.04 (February 2021)



| S-A-V-D Chart Axis Override | X-axis | Left Y-Axis | Right Y-Axis |
|-----------------------------|--------|-------------|--------------|
| minimum bound               |        |             |              |
| maximum bound               |        |             |              |

# DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename: ...[SWM]Outflow hydrographs\Pond6 OutflowHydrograph.xlsx

## Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

|               | SOURCE  | CUHP       | CUHP       | CUHP         | USER         | CUHP          | CUHP          | CUHP          | USER           | CUHP           |
|---------------|---------|------------|------------|--------------|--------------|---------------|---------------|---------------|----------------|----------------|
| Time Interval | TIME    | WQCV [cfs] | EURV [cfs] | 2 Year [cfs] | 5 Year [cfs] | 10 Year [cfs] | 25 Year [cfs] | 50 Year [cfs] | 100 Year [cfs] | 500 Year [cfs] |
| 5.00 min      | 0:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 0:05:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.05           | 0.00           |
|               | 0:10:00 | 0.00       | 0.00       | 0.00         | 0.20         | 0.00          | 0.00          | 0.00          | 0.29           | 0.03           |
|               | 0:15:00 | 0.00       | 0.00       | 0.04         | 2.68         | 0.12          | 0.08          | 0.14          | 7.02           | 0.23           |
|               | 0:20:00 | 0.00       | 0.00       | 0.24         | 32.98        | 0.57          | 0.30          | 0.44          | 44.87          | 1.48           |
|               | 0:25:00 | 0.00       | 0.00       | 1.54         | 55.61        | 7.07          | 1.79          | 3.51          | 117.19         | 15.75          |
|               | 0:30:00 | 0.00       | 0.00       | 3.53         | 62.71        | 18.79         | 18.19         | 33.86         | 163.00         | 71.73          |
|               | 0:35:00 | 0.00       | 0.00       | 4.73         | 63.81        | 25.86         | 38.97         | 67.52         | 178.88         | 129.78         |
|               | 0:40:00 | 0.00       | 0.00       | 5.08         | 62.67        | 27.30         | 51.32         | 84.73         | 181.87         | 159.22         |
|               | 0:45:00 | 0.00       | 0.00       | 4.92         | 61.19        | 26.36         | 55.87         | 90.83         | 178.86         | 170.61         |
|               | 0:50:00 | 0.00       | 0.00       | 4.49         | 58.99        | 24.17         | 55.91         | 90.37         | 172.14         | 170.73         |
|               | 0:55:00 | 0.00       | 0.00       | 4.06         | 56.77        | 21.97         | 52.72         | 85.64         | 164.98         | 164.50         |
|               | 1:00:00 | 0.00       | 0.00       | 3.69         | 54.57        | 20.15         | 48.45         | 79.93         | 158.30         | 157.70         |
|               | 1:05:00 | 0.00       | 0.00       | 3.34         | 52.53        | 18.39         | 44.34         | 74.33         | 146.80         | 150.98         |
|               | 1:10:00 | 0.00       | 0.00       | 3.05         | 50.58        | 16.96         | 40.05         | 67.83         | 135.25         | 140.66         |
|               | 1:15:00 | 0.00       | 0.00       | 2.81         | 48.53        | 15.88         | 36.34         | 61.94         | 123.84         | 129.49         |
|               | 1:20:00 | 0.00       | 0.00       | 2.58         | 46.69        | 14.77         | 33.08         | 56.51         | 113.61         | 118.13         |
|               | 1:25:00 | 0.00       | 0.00       | 2.37         | 44.99        | 13.47         | 29.99         | 51.25         | 104.70         | 106.53         |
|               | 1:30:00 | 0.00       | 0.00       | 2.15         | 43.36        | 12.09         | 26.98         | 46.11         | 96.67          | 95.52          |
|               | 1:35:00 | 0.00       | 0.00       | 1.94         | 40.87        | 10.71         | 24.08         | 41.15         | 89.22          | 85.10          |
|               | 1:40:00 | 0.00       | 0.00       | 1.72         | 38.18        | 9.35          | 21.22         | 36.26         | 82.14          | 75.03          |
|               | 1:45:00 | 0.00       | 0.00       | 1.55         | 35.58        | 8.22          | 18.43         | 31.56         | 75.42          | 65.77          |
|               | 1:50:00 | 0.00       | 0.00       | 1.43         | 33.33        | 7.45          | 16.21         | 27.95         | 69.27          | 58.57          |
|               | 1:55:00 | 0.00       | 0.00       | 1.34         | 31.33        | 6.84          | 14.55         | 25.21         | 64.11          | 52.89          |
|               | 2:00:00 | 0.00       | 0.00       | 1.24         | 27.96        | 6.29          | 13.23         | 22.93         | 56.89          | 48.02          |
|               | 2:05:00 | 0.00       | 0.00       | 1.14         | 24.60        | 5.73          | 12.03         | 20.83         | 49.77          | 43.47          |
|               | 2:10:00 | 0.00       | 0.00       | 1.03         | 21.71        | 5.18          | 10.93         | 18.86         | 43.80          | 39.17          |
|               | 2:15:00 | 0.00       | 0.00       | 0.92         | 19.22        | 4.63          | 9.88          | 16.99         | 38.80          | 35.13          |
|               | 2:20:00 | 0.00       | 0.00       | 0.82         | 17.06        | 4.10          | 8.85          | 15.19         | 34.54          | 31.34          |
|               | 2:25:00 | 0.00       | 0.00       | 0.72         | 15.15        | 3.58          | 7.85          | 13.48         | 30.86          | 27.81          |
|               | 2:30:00 | 0.00       | 0.00       | 0.62         | 13.49        | 3.08          | 6.87          | 11.80         | 27.71          | 24.41          |
|               | 2:35:00 | 0.00       | 0.00       | 0.53         | 12.02        | 2.60          | 5.90          | 10.15         | 24.97          | 21.07          |
|               | 2:40:00 | 0.00       | 0.00       | 0.43         | 10.74        | 2.12          | 4.94          | 8.51          | 22.58          | 17.76          |
|               | 2:45:00 | 0.00       | 0.00       | 0.34         | 9.62         | 1.66          | 3.99          | 6.88          | 20.48          | 14.46          |
|               | 2:50:00 | 0.00       | 0.00       | 0.25         | 8.60         | 1.19          | 3.03          | 5.27          | 18.53          | 11.19          |
|               | 2:55:00 | 0.00       | 0.00       | 0.17         | 7.68         | 0.76          | 2.09          | 3.67          | 16.71          | 8.01           |
|               | 3:00:00 | 0.00       | 0.00       | 0.11         | 6.83         | 0.48          | 1.24          | 2.26          | 14.99          | 5.37           |
|               | 3:05:00 | 0.00       | 0.00       | 0.09         | 6.05         | 0.36          | 0.74          | 1.48          | 13.35          | 3.73           |
|               | 3:10:00 | 0.00       | 0.00       | 0.07         | 5.34         | 0.28          | 0.45          | 0.99          | 11.80          | 2.62           |
|               | 3:15:00 | 0.00       | 0.00       | 0.06         | 4.69         | 0.23          | 0.29          | 0.67          | 10.34          | 1.81           |
|               | 3:20:00 | 0.00       | 0.00       | 0.05         | 4.09         | 0.18          | 0.19          | 0.45          | 8.96           | 1.22           |
|               | 3:25:00 | 0.00       | 0.00       | 0.04         | 3.54         | 0.14          | 0.13          | 0.31          | 7.68           | 0.79           |
|               | 3:30:00 | 0.00       | 0.00       | 0.04         | 3.03         | 0.10          | 0.09          | 0.21          | 6.45           | 0.48           |
|               | 3:35:00 | 0.00       | 0.00       | 0.03         | 2.54         | 0.08          | 0.06          | 0.14          | 5.28           | 0.30           |
|               | 3:40:00 | 0.00       | 0.00       | 0.02         | 2.14         | 0.05          | 0.05          | 0.11          | 4.22           | 0.22           |
|               | 3:45:00 | 0.00       | 0.00       | 0.02         | 1.84         | 0.04          | 0.03          | 0.08          | 3.39           | 0.16           |
|               | 3:50:00 | 0.00       | 0.00       | 0.02         | 1.59         | 0.03          | 0.03          | 0.06          | 2.78           | 0.13           |
|               | 3:55:00 | 0.00       | 0.00       | 0.01         | 1.37         | 0.02          | 0.02          | 0.04          | 2.30           | 0.10           |
|               | 4:00:00 | 0.00       | 0.00       | 0.01         | 1.17         | 0.02          | 0.01          | 0.03          | 1.90           | 0.08           |
|               | 4:05:00 | 0.00       | 0.00       | 0.01         | 0.99         | 0.01          | 0.01          | 0.02          | 1.56           | 0.05           |
|               | 4:10:00 | 0.00       | 0.00       | 0.00         | 0.83         | 0.01          | 0.01          | 0.02          | 1.28           | 0.03           |
|               | 4:15:00 | 0.00       | 0.00       | 0.00         | 0.69         | 0.00          | 0.00          | 0.01          | 1.04           | 0.02           |
|               | 4:20:00 | 0.00       | 0.00       | 0.00         | 0.56         | 0.00          | 0.00          | 0.00          | 0.85           | 0.01           |
|               | 4:25:00 | 0.00       | 0.00       | 0.00         | 0.45         | 0.00          | 0.00          | 0.00          | 0.69           | 0.00           |
|               | 4:30:00 | 0.00       | 0.00       | 0.00         | 0.36         | 0.00          | 0.00          | 0.00          | 0.56           | 0.00           |
|               | 4:35:00 | 0.00       | 0.00       | 0.00         | 0.27         | 0.00          | 0.00          | 0.00          | 0.44           | 0.00           |
|               | 4:40:00 | 0.00       | 0.00       | 0.00         | 0.20         | 0.00          | 0.00          | 0.00          | 0.34           | 0.00           |
|               | 4:45:00 | 0.00       | 0.00       | 0.00         | 0.14         | 0.00          | 0.00          | 0.00          | 0.25           | 0.00           |
|               | 4:50:00 | 0.00       | 0.00       | 0.00         | 0.10         | 0.00          | 0.00          | 0.00          | 0.17           | 0.00           |
|               | 4:55:00 | 0.00       | 0.00       | 0.00         | 0.06         | 0.00          | 0.00          | 0.00          | 0.11           | 0.00           |
|               | 5:00:00 | 0.00       | 0.00       | 0.00         | 0.03         | 0.00          | 0.00          | 0.00          | 0.06           | 0.00           |
|               | 5:05:00 | 0.00       | 0.00       | 0.00         | 0.02         | 0.00          | 0.00          | 0.00          | 0.03           | 0.00           |
|               | 5:10:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.01           | 0.00           |
|               | 5:15:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:20:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:25:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:30:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:35:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:40:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:45:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:50:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:55:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 6:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |

0 5:50:00 0

## DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.04 (February 2021)

### Summary Stage-Area-Volume-Discharge Relationships

The user can create a summary S-A-V-D by entering the desired stage increments and the remainder of the table will populate automatically.

The user should graphically compare the summary S-A-V-D table to the full S-A-V-D table in the chart to confirm it captures all key transition points.

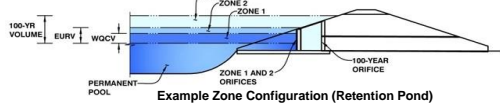
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# DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.04 (February 2021)

Project: **Flying Horse North Master Drainage Plan**

Basin ID: **Pond 15**



Example Zone Configuration (Retention Pond)

## Watershed Information

|   |            |         |
|---|------------|---------|
| Selected BMP Type =                     | <b>EDB</b> |         |
| Watershed Area =                        | 40.87      | acres   |
| Watershed Length =                      | 1,765      | ft      |
| Watershed Length to Centroid =          | 1,089      | ft      |
| Watershed Slope =                       | 0.036      | ft/ft   |
| Watershed Imperviousness =              | 37.20%     | percent |
| Percentage Hydrologic Soil Group A =    | 0.0%       | percent |
| Percentage Hydrologic Soil Group B =    | 100.0%     | percent |
| Percentage Hydrologic Soil Groups C/D = | 0.0%       | percent |
| Target WQCV Drain Time =                | 40.0       | hours   |
| Location for 1-hr Rainfall Depths =     | User Input |         |

After providing required inputs above including 1-hour rainfall depths, click "Run CUHP" to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

|  |       |           |      |        |
|--|-------|-----------|------|--------|
| Water Quality Capture Volume (WQCV) =  | 0.587 | acre-feet |      |        |
| Excess Urban Runoff Volume (EURV) =    | 1.587 | acre-feet |      |        |
| 2-yr Runoff Volume (P1 = 1.19 in.) =   | 1.565 | acre-feet | 1.19 | inches |
| 5-yr Runoff Volume (P1 = 1.5 in.) =    | 2.388 | acre-feet | 1.50 | inches |
| 10-yr Runoff Volume (P1 = 1.75 in.) =  | 3.133 | acre-feet | 1.75 | inches |
| 25-yr Runoff Volume (P1 = 2 in.) =     | 4.211 | acre-feet | 2.00 | inches |
| 50-yr Runoff Volume (P1 = 2.25 in.) =  | 5.054 | acre-feet | 2.25 | inches |
| 100-yr Runoff Volume (P1 = 2.52 in.) = | 6.152 | acre-feet | 2.52 | inches |
| 500-yr Runoff Volume (P1 = 3.39 in.) = | 9.210 | acre-feet | 3.39 | inches |
| Approximate 2-yr Detention Volume =    | 1.161 | acre-feet |      |        |
| Approximate 5-yr Detention Volume =    | 1.632 | acre-feet |      |        |
| Approximate 10-yr Detention Volume =   | 2.277 | acre-feet |      |        |
| Approximate 25-yr Detention Volume =   | 2.567 | acre-feet |      |        |
| Approximate 50-yr Detention Volume =   | 2.696 | acre-feet |      |        |
| Approximate 100-yr Detention Volume =  | 3.115 | acre-feet |      |        |

## Define Zones and Basin Geometry

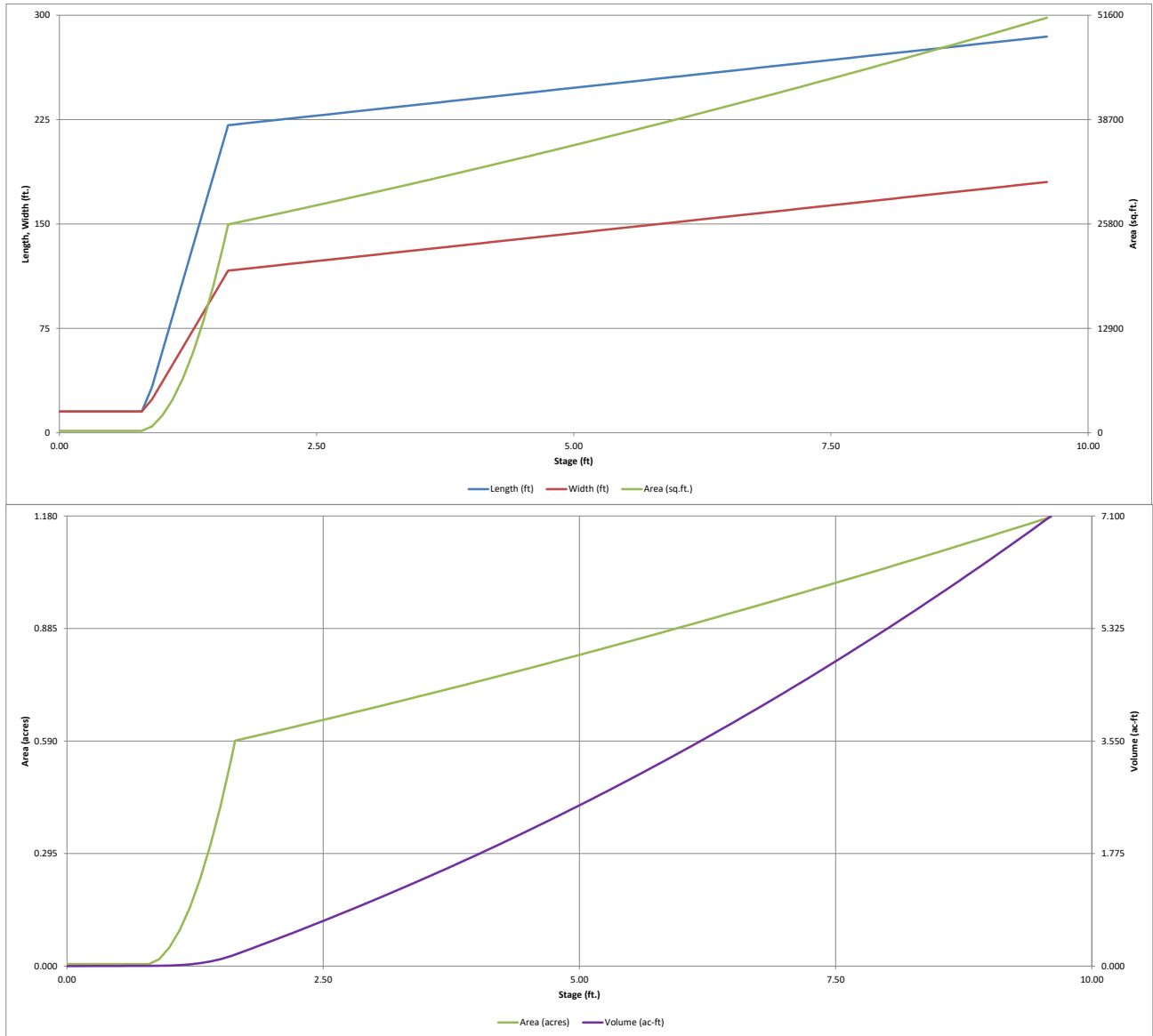
|   |       |                 |
|---|-------|-----------------|
| Zone 1 Volume (WQCV) =                                  | 0.587 | acre-feet       |
| Zone 2 Volume (EURV - Zone 1) =                         | 1.000 | acre-feet       |
| Zone 3 (100yr + 1 / 2 WQCV - Zones 1 & 2) =             | 1.821 | acre-feet       |
| Total Detention Basin Volume =                          | 3.408 | acre-feet       |
| Initial Surge Volume (ISV) =                            | 77    | ft <sup>3</sup> |
| Initial Surge Depth (ISD) =                             | 0.33  | ft              |
| Total Available Detention Depth (H <sub>total</sub> ) = | 6.00  | ft              |
| Depth of Trickle Channel (H <sub>TC</sub> ) =           | 0.50  | ft              |
| Slope of Trickle Channel (S <sub>TC</sub> ) =           | 0.004 | ft/ft           |
| Slopes of Main Basin Sides (S <sub>main</sub> ) =       | 4     | H:V             |
| Basin Length-to-Width Ratio (L <sub>W</sub> ) =         | 2     |                 |

|   |              |                 |
|---|--------------|-----------------|
| Initial Surge Area (A <sub>ISV</sub> ) =              | 232          | ft <sup>2</sup> |
| Surcharge Volume Length (L <sub>ISV</sub> ) =         | 15.2         | ft              |
| Surcharge Volume Width (W <sub>ISV</sub> ) =          | 15.2         | ft              |
| Depth of Basin Floor (H <sub>FLOOR</sub> ) =          | 0.81         | ft              |
| Length of Basin Floor (L <sub>FLOOR</sub> ) =         | 221.0        | ft              |
| Width of Basin Floor (W <sub>FLOOR</sub> ) =          | 116.5        | ft              |
| Area of Basin Floor (A <sub>FLOOR</sub> ) =           | 25,744       | ft <sup>2</sup> |
| Volume of Basin Floor (V <sub>FLOOR</sub> ) =         | 7,674        | ft <sup>3</sup> |
| Depth of Main Basin (H <sub>MAIN</sub> ) =            | 4.36         | ft              |
| Length of Main Basin (L <sub>MAIN</sub> ) =           | 255.9        | ft              |
| Width of Main Basin (W <sub>MAIN</sub> ) =            | 151.4        | ft              |
| Area of Main Basin (A <sub>MAIN</sub> ) =             | 38,732       | ft <sup>2</sup> |
| Volume of Main Basin (V <sub>MAIN</sub> ) =           | 139,596      | ft <sup>3</sup> |
| Calculated Total Basin Volume (V <sub>total</sub> ) = | <b>3.385</b> | acre-feet       |

| Depth Increment =           | 0.10       | ft                           |             |            |                         |   |             |                           |                |
|-----------------------------|------------|------------------------------|-------------|------------|-------------------------|---|-------------|---------------------------|----------------|
| Stage - Storage Description | Stage (ft) | Optional Override Stage (ft) | Length (ft) | Width (ft) | Area (ft <sup>2</sup> ) | Optional Override Area (ft <sup>2</sup> ) | Area (acre) | Volume (ft <sup>3</sup> ) | Volume (ac-ft) |
| Top of Micropool            | 0.00       |                              | 15.2        | 15.2       | 232                     |   | 0.005       |                           |                |
| ISV                         | 0.33       |                              | 15.2        | 15.2       | 232                     |   | 0.005       | 77                        | 0.002          |
|                             | 0.40       |                              | 15.2        | 15.2       | 232                     |   | 0.005       | 93                        | 0.002          |
|                             | 0.50       |                              | 15.2        | 15.2       | 232                     |   | 0.005       | 116                       | 0.003          |
|                             | 0.60       |                              | 15.2        | 15.2       | 232                     |   | 0.005       | 139                       | 0.003          |
|                             | 0.70       |                              | 15.2        | 15.2       | 232                     |   | 0.005       | 163                       | 0.004          |
|                             | 0.80       |                              | 15.2        | 15.2       | 232                     |   | 0.005       | 186                       | 0.004          |
|                             | 0.90       |                              | 33.0        | 24.0       | 792                     |   | 0.018       | 227                       | 0.005          |
|                             | 1.00       |                              | 58.4        | 36.5       | 2,132                   |   | 0.049       | 368                       | 0.008          |
|                             | 1.10       |                              | 83.8        | 49.0       | 4,107                   |   | 0.094       | 675                       | 0.015          |
|                             | 1.20       |                              | 109.2       | 61.5       | 6,717                   |   | 0.154       | 1,210                     | 0.028          |
| 1.30                        |            | 134.6                        | 74.0        | 9,962      |                         | 0.229                                     | 2,039       | 0.047                     |                |
| 1.40                        |            | 160.0                        | 86.5        | 13,841     |                         | 0.318                                     | 3,224       | 0.074                     |                |
| 1.50                        |            | 185.4                        | 99.0        | 18,356     |                         | 0.421                                     | 4,829       | 0.111                     |                |
| 1.60                        |            | 210.8                        | 111.5       | 23,506     |                         | 0.540                                     | 6,916       | 0.159                     |                |
| Floor                       | 1.64       |                              | 221.0       | 116.5      | 25,744                  |   | 0.591       | 7,901                     | 0.181          |
| 1.70                        |            | 221.5                        | 117.0       | 25,906     |                         | 0.595                                     | 9,451       | 0.217                     |                |
| 1.80                        |            | 222.3                        | 117.8       | 26,177     |                         | 0.601                                     | 12,055      | 0.277                     |                |
| 1.90                        |            | 223.1                        | 118.6       | 26,450     |                         | 0.607                                     | 14,686      | 0.337                     |                |
| 2.00                        |            | 223.9                        | 119.4       | 26,724     |                         | 0.613                                     | 17,345      | 0.398                     |                |
| 2.10                        |            | 224.7                        | 120.2       | 26,999     |                         | 0.620                                     | 20,031      | 0.460                     |                |
| 2.20                        |            | 225.5                        | 121.0       | 27,276     |                         | 0.626                                     | 22,745      | 0.522                     |                |
| 2.30                        |            | 226.3                        | 121.8       | 27,554     |                         | 0.633                                     | 25,486      | 0.585                     |                |
| Zone 1 (WQCV)               | 2.31       |                              | 226.3       | 121.9      | 27,581                  |   | 0.633       | 25,762                    | 0.591          |
|                             | 2.40       |                              | 227.1       | 122.6      | 27,833                  |   | 0.639       | 28,255                    | 0.649          |
|                             | 2.50       |                              | 227.9       | 123.4      | 28,113                  |   | 0.645       | 31,053                    | 0.713          |
|                             | 2.60       |                              | 228.7       | 124.2      | 28,395                  |   | 0.652       | 33,878                    | 0.778          |
|                             | 2.70       |                              | 229.5       | 125.0      | 28,678                  |   | 0.658       | 36,732                    | 0.843          |
|                             | 2.80       |                              | 230.3       | 125.8      | 28,962                  |   | 0.665       | 39,614                    | 0.909          |
|                             | 2.90       |                              | 231.1       | 126.6      | 29,247                  |   | 0.671       | 42,524                    | 0.976          |
|                             | 3.00       |                              | 231.9       | 127.4      | 29,534                  |   | 0.678       | 45,463                    | 1.044          |
|                             | 3.10       |                              | 232.7       | 128.2      | 29,822                  |   | 0.685       | 48,431                    | 1.112          |
|                             | 3.20       |                              | 233.5       | 129.0      | 30,111                  |   | 0.691       | 51,428                    | 1.181          |
| 3.30                        |            | 234.3                        | 129.8       | 30,402     |                         | 0.698                                     | 54,453      | 1.250                     |                |
| 3.40                        |            | 235.1                        | 130.6       | 30,694     |                         | 0.705                                     | 57,508      | 1.320                     |                |
| 3.50                        |            | 235.9                        | 131.4       | 30,987     |                         | 0.711                                     | 60,592      | 1.391                     |                |
| 3.60                        |            | 236.7                        | 132.2       | 31,281     |                         | 0.718                                     | 63,705      | 1.462                     |                |
| 3.70                        |            | 237.5                        | 133.0       | 31,577     |                         | 0.725                                     | 66,848      | 1.535                     |                |
| Zone 2 (EURV)               | 3.78       |                              | 238.1       | 133.6      | 31,815                  |   | 0.730       | 69,384                    | 1.593          |
|                             | 3.80       |                              | 238.3       | 133.8      | 31,874                  |   | 0.732       | 70,021                    | 1.607          |
|                             | 3.90       |                              | 239.1       | 134.6      | 32,172                  |   | 0.739       | 73,223                    | 1.681          |
|                             | 4.00       |                              | 239.9       | 135.4      | 32,472                  |   | 0.745       | 76,455                    | 1.755          |
|                             | 4.10       |                              | 240.7       | 136.2      | 32,773                  |   | 0.752       | 79,718                    | 1.830          |
|                             | 4.20       |                              | 241.5       | 137.0      | 33,075                  |   | 0.759       | 83,010                    | 1.906          |
|                             | 4.30       |                              | 242.3       | 137.8      | 33,378                  |   | 0.766       | 86,333                    | 1.982          |
|                             | 4.40       |                              | 243.1       | 138.6      | 33,683                  |   | 0.773       | 89,686                    | 2.059          |
|                             | 4.50       |                              | 243.9       | 139.4      | 33,989                  |   | 0.780       | 93,069                    | 2.137          |
|                             | 4.60       |                              | 244.7       | 140.2      | 34,296                  |   | 0.787       | 96,483                    | 2.215          |
| 4.70                        |            | 245.5                        | 141.0       | 34,605     |                         | 0.794                                     | 99,928      | 2.294                     |                |
| 4.80                        |            | 246.3                        | 141.8       | 34,914     |                         | 0.802                                     | 103,404     | 2.374                     |                |
| 4.90                        |            | 247.1                        | 142.6       | 35,225     |                         | 0.809                                     | 106,911     | 2.454                     |                |
| 5.00                        |            | 247.9                        | 143.4       | 35,538     |                         | 0.816                                     | 110,449     | 2.536                     |                |
| 5.10                        |            | 248.7                        | 144.2       | 35,851     |                         | 0.823                                     | 114,019     | 2.618                     |                |
| 5.20                        |            | 249.5                        | 145.0       | 36,166     |                         | 0.830                                     | 117,620     | 2.700                     |                |
| 5.30                        |            | 250.3                        | 145.8       | 36,483     |                         | 0.838                                     | 121,252     | 2.784                     |                |
| 5.40                        |            | 251.1                        | 146.6       | 36,800     |                         | 0.845                                     | 124,916     | 2.868                     |                |
| 5.50                        |            | 251.9                        | 147.4       | 37,119     |                         | 0.852                                     | 128,612     | 2.953                     |                |
| 5.60                        |            | 252.7                        | 148.2       | 37,439     |                         | 0.859                                     | 132,340     | 3.038                     |                |
| 5.70                        |            | 253.5                        | 149.0       | 37,760     |                         | 0.867                                     | 136,100     | 3.124                     |                |
| 5.80                        |            | 254.3                        | 149.8       | 38,083     |                         | 0.874                                     | 139,892     | 3.211                     |                |
| 5.90                        |            | 255.1                        | 150.6       | 38,407     |                         | 0.882                                     | 143,717     | 3.299                     |                |
| Z3 (100+1/2WQCV)            | 6.00       |                              | 255.9       | 151.4      | 38,732                  |   | 0.889       | 147,574                   | 3.388          |
|                             | 6.03       |                              | 256.1       | 151.6      | 38,830                  |   | 0.891       | 148,737                   | 3.415          |
|                             | 6.10       |                              | 256.7       | 152.2      | 39,058                  |   | 0.897       | 151,463                   | 3.477          |
|                             | 6.20       |                              | 257.5       | 153.0      | 39,386                  |   | 0.904       | 155,385                   | 3.567          |
|                             | 6.30       |                              | 258.3       | 153.8      | 39,715                  |   | 0.912       | 159,340                   | 3.658          |
|                             | 6.40       |                              | 259.1       | 154.6      | 40,045                  |   | 0.919       | 163,328                   | 3.750          |
|                             | 6.50       |                              | 259.9       | 155.4      | 40,377                  |   | 0.927       | 167,349                   | 3.842          |
|                             | 6.60       |                              | 260.7       | 156.2      | 40,710                  |   | 0.935       | 171,404                   | 3.935          |
|                             | 6.70       |                              | 261.5       | 157.0      | 41,044                  |   | 0.942       | 175,491                   | 4.029          |
|                             | 6.80       |                              | 262.3       | 157.8      | 41,379                  |   | 0.950       | 179,612                   | 4.123          |
|                             | 6.90       |                              | 263.1       | 158.6      | 41,716                  |   | 0.958       | 183,767                   | 4.219          |
|                             | 7.00       |                              | 263.9       | 159.4      | 42,054                  |   | 0.965       | 187,956                   | 4.315          |
|                             | 7.10       |                              | 264.7       | 160.2      | 42,393                  |   | 0.973       | 192,178                   | 4.412          |
|                             | 7.20       |                              | 265.5       | 161.0      | 42,733                  |   | 0.981       | 196,434                   | 4.510          |
|                             | 7.30       |                              | 266.3       | 161.8      | 43,075                  |   | 0.989       | 200,725                   | 4.608          |
|                             | 7.40       |                              | 267.1       | 162.6      | 43,418                  |   | 0.997       | 205,049                   | 4.707          |
|                             | 7.50       |                              | 267.9       | 163.4      | 43,763                  |   | 1.005       | 209,408                   | 4.807          |
|                             | 7.60       |                              | 268.7       | 164.2      | 44,108                  |   | 1.013       | 213,802                   | 4.908          |
|                             | 7.70       |                              | 269.5       | 165.0      | 44,455                  |   | 1.021       | 218,230                   | 5.010          |
|                             | 7.80       |                              | 270.3       | 165.8      | 44,803                  |   | 1.029       | 222,693                   | 5.112          |
| 7.90                        |            | 271.1                        | 166.6       | 45,153     |                         | 1.037                                     | 227,191     | 5.216                     |                |
| 8.00                        |            | 271.9                        | 167.4       | 45,504     |                         | 1.045                                     | 231,724     | 5.320                     |                |
| 8.10                        |            | 272.7                        | 168.2       | 45,856     |                         | 1.053                                     | 236,291     | 5.425                     |                |
| 8.20                        |            | 273.5                        | 169.0       | 46,209     |                         | 1.061                                     | 240,895     | 5.530                     |                |
| 8.30                        |            | 274.3                        | 169.8       | 46,564     |                         | 1.069                                     | 245,533     | 5.637                     |                |
| 8.40                        |            | 275.1                        | 170.6       | 46,919     |                         | 1.077                                     | 250,207     | 5.744                     |                |
| 8.50                        |            | 275.9                        | 171.4       | 47,277     |                         | 1.085                                     | 254,917     | 5.852                     |                |
| 8.60                        |            | 276.7                        | 172.2       | 47,635     |                         | 1.094                                     | 259,663     | 5.961                     |                |
| 8.70                        |            | 277.5                        | 173.0       | 47,995     |                         | 1.102                                     | 264,444     | 6.071                     |                |
| 8.80                        |            | 278.3                        | 173.8       | 48,356     |                         | 1.110                                     | 269,262     | 6.181                     |                |
| 8.90                        |            | 279.1                        | 174.6       | 48,718     |                         | 1.118                                     | 274,115     | 6.293                     |                |
| 9.00                        |            | 279.9                        | 175.4       | 49,081     |                         | 1.127                                     | 279,005     | 6.405                     |                |
| 9.10                        |            | 280.7                        | 176.2       | 49,446     |                         | 1.135                                     | 283,932     | 6.518                     |                |
| 9.20                        |            | 281.5                        | 177.0       | 49,812     |                         | 1.144                                     | 288,895     | 6.632                     |                |
| 9.30                        |            | 282.3                        | 177.8       | 50,180     |                         | 1.152                                     | 293,894     | 6.747                     |                |
| 9.40                        |            | 283.1                        | 178.6       | 50,549     |                         | 1.160                                     | 298,931     | 6.863                     |                |
| 9.50                        |            | 283.9                        | 179.4       | 50,918     |                         | 1.169                                     | 304,004     | 6.979                     |                |
| 9.60                        |            | 284.7                        | 180.2       | 51,290     |                         | 1.177                                     | 309,114     | 7.096                     |                |

# DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.04 (February 2021)

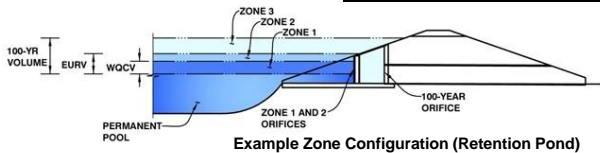


# DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD- Detention, Version 4.04 (February 2021)

Project: Flying Horse North Master Drainage Plan

Basin ID: Pond 15



Example Zone Configuration (Retention Pond)

|                      | Estimated Stage (ft) | Estimated Volume (ac-ft) | Outlet Type          |
|----------------------|----------------------|--------------------------|----------------------|
| Zone 1 (WQCV)        | 2.31                 | 0.587                    | Orifice Plate        |
| Zone 2 (EURV)        | 3.78                 | 1.000                    | Weir&Pipe (Circular) |
| Zone 3 (100+1/2WQCV) | 6.03                 | 1.821                    | Weir&Pipe (Restrict) |
| Total (all zones)    |                      | 3.408                    |                      |

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth = N/A ft (distance below the filtration media surface)  
Underdrain Orifice Diameter = N/A inches

Calculated Parameters for Underdrain  
Underdrain Orifice Area = N/A ft<sup>2</sup>  
Underdrain Orifice Centroid = N/A feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice = 0.00 ft (relative to basin bottom at Stage = 0 ft)  
Depth at top of Zone using Orifice Plate = 2.36 ft (relative to basin bottom at Stage = 0 ft)  
Orifice Plate: Orifice Vertical Spacing = 9.40 inches  
Orifice Plate: Orifice Area per Row = 1.99 sq. inches (diameter = 1-9/16 inches)

Calculated Parameters for Plate  
WQ Orifice Area per Row = 1.382E-02 ft<sup>2</sup>  
Elliptical Half-Width = N/A feet  
Elliptical Slot Centroid = N/A feet  
Elliptical Slot Area = N/A ft<sup>2</sup>

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

|                                | Row 1 (required) | Row 2 (optional) | Row 3 (optional) | Row 4 (optional) | Row 5 (optional) | Row 6 (optional) | Row 7 (optional) | Row 8 (optional) |
|--------------------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|
| Stage of Orifice Centroid (ft) | 0.00             | 0.79             | 1.57             |                  |                  |                  |                  |                  |
| Orifice Area (sq. inches)      | 1.99             | 1.99             | 1.99             |                  |                  |                  |                  |                  |

|                                | Row 9 (optional) | Row 10 (optional) | Row 11 (optional) | Row 12 (optional) | Row 13 (optional) | Row 14 (optional) | Row 15 (optional) | Row 16 (optional) |
|--------------------------------|------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| Stage of Orifice Centroid (ft) |                  |                   |                   |                   |                   |                   |                   |                   |
| Orifice Area (sq. inches)      |                  |                   |                   |                   |                   |                   |                   |                   |

User Input: Vertical Orifice (Circular or Rectangular)

Invert of Vertical Orifice = N/A ft (relative to basin bottom at Stage = 0 ft)  
Depth at top of Zone using Vertical Orifice = N/A ft (relative to basin bottom at Stage = 0 ft)  
Vertical Orifice Diameter = N/A inches

Calculated Parameters for Vertical Orifice  
Vertical Orifice Area = N/A ft<sup>2</sup>  
Vertical Orifice Centroid = N/A feet

User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe)

Overflow Weir Front Edge Height, H<sub>o</sub> = 2.39 ft (relative to basin bottom at Stage = 0 ft)  
Overflow Weir Front Edge Length = 5.00 feet  
Overflow Weir Grate Slope = 0.00 H:V  
Horiz. Length of Weir Sides = 5.00 feet  
Overflow Grate Type = Type C Grate  
Debris Clogging % = 50%

Calculated Parameters for Overflow Weir  
Height of Grate Upper Edge, H<sub>u</sub> = 2.49 feet  
Overflow Weir Slope Length = 5.00 feet  
Grate Open Area / 100-yr Orifice Area = 22.15  
Overflow Grate Open Area w/o Debris = 17.40 ft<sup>2</sup>  
Overflow Grate Open Area w/ Debris = 8.70 ft<sup>2</sup>

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

Depth to Invert of Outlet Pipe = 2.50 ft (distance below basin bottom at Stage = 0 ft)  
Circular Orifice Diameter or Pipe Diameter = 12.00 inches  
Restrictor Plate Height Above Pipe Invert = 25.00 inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate  
Outlet Orifice Area = 0.79 ft<sup>2</sup>  
Outlet Orifice Centroid = 0.50 feet  
Half-Central Angle of Restrictor Plate on Pipe = N/A radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage = 7.00 ft (relative to basin bottom at Stage = 0 ft)  
Spillway Crest Length = 31.00 feet  
Spillway End Slopes = 4.00 H:V  
Freeboard above Max Water Surface = 1.00 feet

Calculated Parameters for Spillway  
Spillway Design Flow Depth = 0.93 feet  
Stage at Top of Freeboard = 8.93 feet  
Basin Area at Top of Freeboard = 1.12 acres  
Basin Volume at Top of Freeboard = 6.33 acre-ft

Routed Hydrograph Results

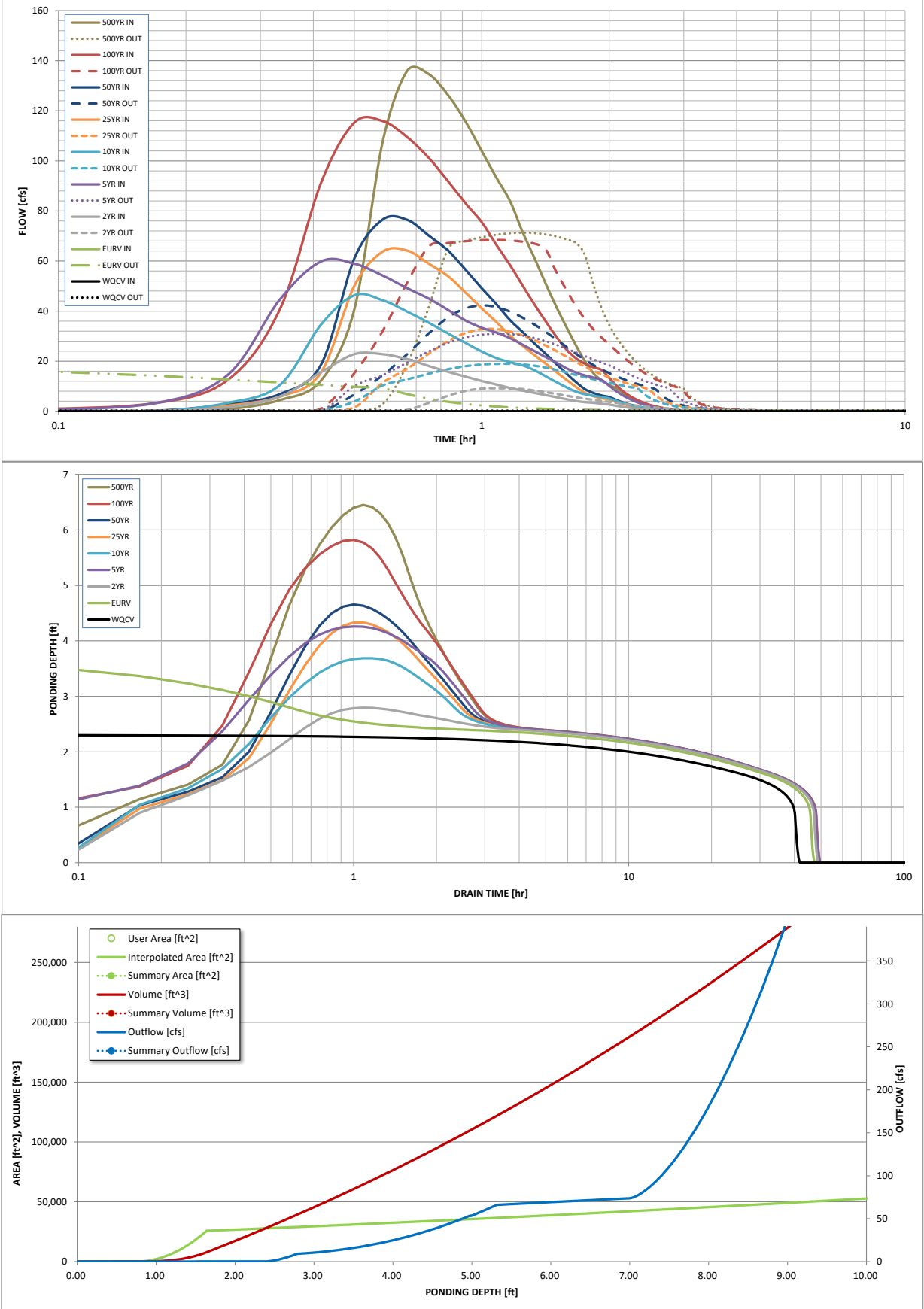
The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).

|  | WQCV  | EURV            | 2 Year          | 5 Year          | 10 Year         | 25 Year         | 50 Year         | 100 Year       | 500 Year       |
|--|-------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|----------------|----------------|
| Design Storm Return Period =                       | N/A   | N/A             | 1.19            | 1.50            | 1.75            | 2.00            | 2.25            | 2.52           | 3.39           |
| One-Hour Rainfall Depth (in) =                     | 0.587 | 1.587           | 1.565           | 2.388           | 3.133           | 4.211           | 5.054           | 6.152          | 9.210          |
| CUHP Runoff Volume (acre-ft) =                     | N/A   | N/A             | 1.565           | 4.857           | 3.133           | 4.211           | 5.054           | 8.775          | 9.210          |
| User Override Inflow Hydrograph Volume (acre-ft) = | N/A   | N/A             | 4.8             | 13.3            | 20.2            | 35.6            | 44.6            | 57.0           | 88.8           |
| CUHP Predevelopment Peak Q (cfs) =                 | N/A   | N/A             | 0.12            | 0.77            | 0.49            | 0.87            | 1.09            | 1.66           | 2.17           |
| OPTIONAL Override Predevelopment Peak Q (cfs) =    | N/A   | N/A             | 22.8            | 59.8            | 46.3            | 64.1            | 76.5            | 115.9          | 136.0          |
| Predevelopment Unit Peak Flow, q (cfs/acre) =      | N/A   | N/A             | 9.1             | 30.9            | 18.9            | 32.8            | 42.3            | 68.4           | 71.3           |
| Peak Inflow Q (cfs) =                              | N/A   | N/A             | N/A             | 1.0             | 0.9             | 0.9             | 0.9             | 1.0            | 0.8            |
| Peak Outflow Q (cfs) =                             | N/A   | N/A             | N/A             | N/A             | N/A             | N/A             | N/A             | N/A            | N/A            |
| Ratio Peak Outflow to Predevelopment Q =           | Plate | Overflow Weir 2 | Overflow Weir 2 | Overflow Weir 2 | Overflow Weir 2 | Overflow Weir 2 | Overflow Weir 2 | Outlet Plate 2 | Outlet Plate 2 |
| Structure Controlling Flow =                       | N/A   | 0.50            | 0.46            | 0.5             | 0.5             | 0.5             | 0.5             | 0.6            | 0.6            |
| Max Velocity through Grate 1 (fps) =               | N/A   | 0.32            | 0.02            | 0.6             | 0.3             | 0.6             | 0.9             | 1.6            | 1.7            |
| Max Velocity through Grate 2 (fps) =               | 39    | 41              | 43              | 34              | 39              | 36              | 34              | 26             | 25             |
| Time to Drain 97% of Inflow Volume (hours) =       | 40    | 45              | 46              | 43              | 45              | 44              | 43              | 40             | 39             |
| Time to Drain 99% of Inflow Volume (hours) =       | 2.31  | 3.78            | 2.80            | 4.26            | 3.69            | 4.33            | 4.65            | 5.82           | 6.45           |
| Maximum Ponding Depth (ft) =                       | 0.63  | 0.73            | 0.66            | 0.76            | 0.72            | 0.77            | 0.79            | 0.88           | 0.92           |
| Area at Maximum Ponding Depth (acres) =            | 0.591 | 1.593           | 0.903           | 1.944           | 1.520           | 2.005           | 2.254           | 3.229          | 3.786          |
| Maximum Volume Stored (acre-ft) =                  |       |                 |                 |                 |                 |                 |                 |                |                |



DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD- Detention, Version 4.04 (February 2021)



| S-A-V-D Chart Axis Override | X-axis | Left Y-Axis | Right Y-Axis |
|-----------------------------|--------|-------------|--------------|
| minimum bound               |        |             |              |
| maximum bound               |        |             |              |

# DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename: ...[SWM]Outflow hydrographs[Pond6 OutflowHydrograph.xlsx

## Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

|               | SOURCE  | CUHP       | CUHP       | CUHP         | USER         | CUHP          | CUHP          | CUHP          | USER           | CUHP           |
|---------------|---------|------------|------------|--------------|--------------|---------------|---------------|---------------|----------------|----------------|
| Time Interval | TIME    | WQCV [cfs] | EURV [cfs] | 2 Year [cfs] | 5 Year [cfs] | 10 Year [cfs] | 25 Year [cfs] | 50 Year [cfs] | 100 Year [cfs] | 500 Year [cfs] |
| 5.00 min      | 0:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 0:05:00 | 0.00       | 0.00       | 0.00         | 0.23         | 0.00          | 0.00          | 0.00          | 0.55           | 0.00           |
|               | 0:10:00 | 0.00       | 0.00       | 0.00         | 3.05         | 0.00          | 0.00          | 0.18          | 3.10           | 0.83           |
|               | 0:15:00 | 0.00       | 0.00       | 1.60         | 14.26        | 3.27          | 2.20          | 2.77          | 12.25          | 4.45           |
|               | 0:20:00 | 0.00       | 0.00       | 5.84         | 44.61        | 10.48         | 5.83          | 6.83          | 40.67          | 12.21          |
|               | 0:25:00 | 0.00       | 0.00       | 15.59        | 59.80        | 34.54         | 15.42         | 18.52         | 91.07          | 40.72          |
|               | 0:30:00 | 0.00       | 0.00       | 22.81        | 58.93        | 46.32         | 50.11         | 61.06         | 115.27         | 107.68         |
|               | 0:35:00 | 0.00       | 0.00       | 22.79        | 54.19        | 44.31         | 63.75         | 76.55         | 115.87         | 135.98         |
|               | 0:40:00 | 0.00       | 0.00       | 20.82        | 49.14        | 39.76         | 64.15         | 76.41         | 109.44         | 134.56         |
|               | 0:45:00 | 0.00       | 0.00       | 18.07        | 44.94        | 35.32         | 58.91         | 70.09         | 101.12         | 126.16         |
|               | 0:50:00 | 0.00       | 0.00       | 15.72        | 40.41        | 31.03         | 53.88         | 64.09         | 91.75          | 115.49         |
|               | 0:55:00 | 0.00       | 0.00       | 13.81        | 36.16        | 27.25         | 47.29         | 56.41         | 82.92          | 103.88         |
|               | 1:00:00 | 0.00       | 0.00       | 12.08        | 33.34        | 23.85         | 41.04         | 49.09         | 75.47          | 93.21          |
|               | 1:05:00 | 0.00       | 0.00       | 10.66        | 31.42        | 21.25         | 35.60         | 42.69         | 66.36          | 83.86          |
|               | 1:10:00 | 0.00       | 0.00       | 9.30         | 29.19        | 19.60         | 30.17         | 36.36         | 58.34          | 71.33          |
|               | 1:15:00 | 0.00       | 0.00       | 8.22         | 26.56        | 18.32         | 26.11         | 31.60         | 50.09          | 61.02          |
|               | 1:20:00 | 0.00       | 0.00       | 7.29         | 24.00        | 16.33         | 22.35         | 27.02         | 42.51          | 50.81          |
|               | 1:25:00 | 0.00       | 0.00       | 6.44         | 21.60        | 13.93         | 19.00         | 22.91         | 35.82          | 41.70          |
|               | 1:30:00 | 0.00       | 0.00       | 5.60         | 19.48        | 11.66         | 15.68         | 18.87         | 29.78          | 33.76          |
|               | 1:35:00 | 0.00       | 0.00       | 4.80         | 17.20        | 9.61          | 12.60         | 15.14         | 24.73          | 26.53          |
|               | 1:40:00 | 0.00       | 0.00       | 4.10         | 15.51        | 7.86          | 9.79          | 11.74         | 21.24          | 20.15          |
|               | 1:45:00 | 0.00       | 0.00       | 3.61         | 14.34        | 6.81          | 7.38          | 8.89          | 19.03          | 15.30          |
|               | 1:50:00 | 0.00       | 0.00       | 3.38         | 13.48        | 6.22          | 6.03          | 7.31          | 17.57          | 12.38          |
|               | 1:55:00 | 0.00       | 0.00       | 2.99         | 12.56        | 5.69          | 5.19          | 6.31          | 16.52          | 10.47          |
|               | 2:00:00 | 0.00       | 0.00       | 2.67         | 10.20        | 5.09          | 4.65          | 5.66          | 13.33          | 9.11           |
|               | 2:05:00 | 0.00       | 0.00       | 2.15         | 7.89         | 4.08          | 3.63          | 4.42          | 10.15          | 6.95           |
|               | 2:10:00 | 0.00       | 0.00       | 1.68         | 6.09         | 3.16          | 2.77          | 3.36          | 7.70           | 5.08           |
|               | 2:15:00 | 0.00       | 0.00       | 1.32         | 4.66         | 2.43          | 2.10          | 2.54          | 5.86           | 3.70           |
|               | 2:20:00 | 0.00       | 0.00       | 1.02         | 3.53         | 1.85          | 1.58          | 1.91          | 4.46           | 2.71           |
|               | 2:25:00 | 0.00       | 0.00       | 0.79         | 2.62         | 1.39          | 1.20          | 1.44          | 3.35           | 2.04           |
|               | 2:30:00 | 0.00       | 0.00       | 0.61         | 1.92         | 1.03          | 0.89          | 1.07          | 2.50           | 1.52           |
|               | 2:35:00 | 0.00       | 0.00       | 0.46         | 1.41         | 0.77          | 0.66          | 0.80          | 1.89           | 1.14           |
|               | 2:40:00 | 0.00       | 0.00       | 0.35         | 1.00         | 0.58          | 0.50          | 0.60          | 1.38           | 0.87           |
|               | 2:45:00 | 0.00       | 0.00       | 0.25         | 0.68         | 0.43          | 0.37          | 0.45          | 0.96           | 0.64           |
|               | 2:50:00 | 0.00       | 0.00       | 0.18         | 0.43         | 0.30          | 0.27          | 0.32          | 0.61           | 0.45           |
|               | 2:55:00 | 0.00       | 0.00       | 0.11         | 0.24         | 0.19          | 0.18          | 0.21          | 0.35           | 0.30           |
|               | 3:00:00 | 0.00       | 0.00       | 0.07         | 0.10         | 0.11          | 0.11          | 0.13          | 0.15           | 0.17           |
|               | 3:05:00 | 0.00       | 0.00       | 0.03         | 0.03         | 0.05          | 0.05          | 0.06          | 0.04           | 0.08           |
|               | 3:10:00 | 0.00       | 0.00       | 0.01         | 0.00         | 0.02          | 0.02          | 0.02          | 0.00           | 0.02           |
|               | 3:15:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:20:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:25:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:30:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:35:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:40:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:45:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:50:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:55:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:05:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:10:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:15:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:20:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:25:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:30:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:35:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:40:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:45:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:50:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:55:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:05:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:10:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:15:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:20:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:25:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:30:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:35:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:40:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:45:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:50:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:55:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 6:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |

## DETENTION BASIN OUTLET STRUCTURE DESIGN

*MHFD-Detention, Version 4.04 (February 2021)*

### Summary Stage-Area-Volume-Discharge Relationships

The user can create a summary S-A-V-D by entering the desired stage increments and the remainder of the table will populate automatically.

The user should graphically compare the summary S-A-V-D table to the full S-A-V-D table in the chart to confirm it captures all key transition points.

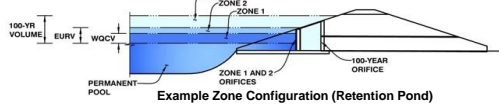
[illegible]

# DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.05 (January 2022)

Project: **Flying Horse North MDDP**

Basin ID: **Pond 16**



Example Zone Configuration (Retention Pond)

## Watershed Information

|   |                           |         |
|---|---------------------------|---------|
| Selected BMP Type =                     | <b>EDB</b>                |         |
| Watershed Area =                        | 28.99                     | acres   |
| Watershed Length =                      | 1,505                     | ft      |
| Watershed Length to Centroid =          | 954                       | ft      |
| Watershed Slope =                       | 0.035                     | ft/ft   |
| Watershed Imperviousness =              | 34.66%                    | percent |
| Percentage Hydrologic Soil Group A =    | 0.0%                      | percent |
| Percentage Hydrologic Soil Group B =    | 100.0%                    | percent |
| Percentage Hydrologic Soil Groups C/D = | 0.0%                      | percent |
| Target WQCV Drain Time =                | 40.0                      | hours   |
| Location for 1-hr Rainfall Depths =     | Denver - Capitol Building |         |

After providing required inputs above including 1-hour rainfall depths, click "Run CUHP" to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

|  |       |           |      |           |
|--|-------|-----------|------|-----------|
| Water Quality Capture Volume (WQCV) =  | 0.399 | acre-feet |      | acre-feet |
| Excess Urban Runoff Volume (EURV) =    | 1.043 | acre-feet |      | acre-feet |
| 2-yr Runoff Volume (P1 = 1.19 in.) =   | 1.034 | acre-feet | 1.19 | inches    |
| 5-yr Runoff Volume (P1 = 1.5 in.) =    | 1.610 | acre-feet | 1.50 | inches    |
| 10-yr Runoff Volume (P1 = 1.75 in.) =  | 2.133 | acre-feet | 1.75 | inches    |
| 25-yr Runoff Volume (P1 = 2 in.) =     | 2.899 | acre-feet | 2.00 | inches    |
| 50-yr Runoff Volume (P1 = 2.25 in.) =  | 3.492 | acre-feet | 2.25 | inches    |
| 100-yr Runoff Volume (P1 = 2.52 in.) = | 4.270 | acre-feet | 2.52 | inches    |
| 500-yr Runoff Volume (P1 = 3.14 in.) = | 5.793 | acre-feet |      | inches    |
| Approximate 2-yr Detention Volume =    | 0.758 | acre-feet |      |           |
| Approximate 5-yr Detention Volume =    | 1.071 | acre-feet |      |           |
| Approximate 10-yr Detention Volume =   | 1.515 | acre-feet |      |           |
| Approximate 25-yr Detention Volume =   | 1.723 | acre-feet |      |           |
| Approximate 50-yr Detention Volume =   | 1.812 | acre-feet |      |           |
| Approximate 100-yr Detention Volume =  | 2.110 | acre-feet |      |           |

## Define Zones and Basin Geometry

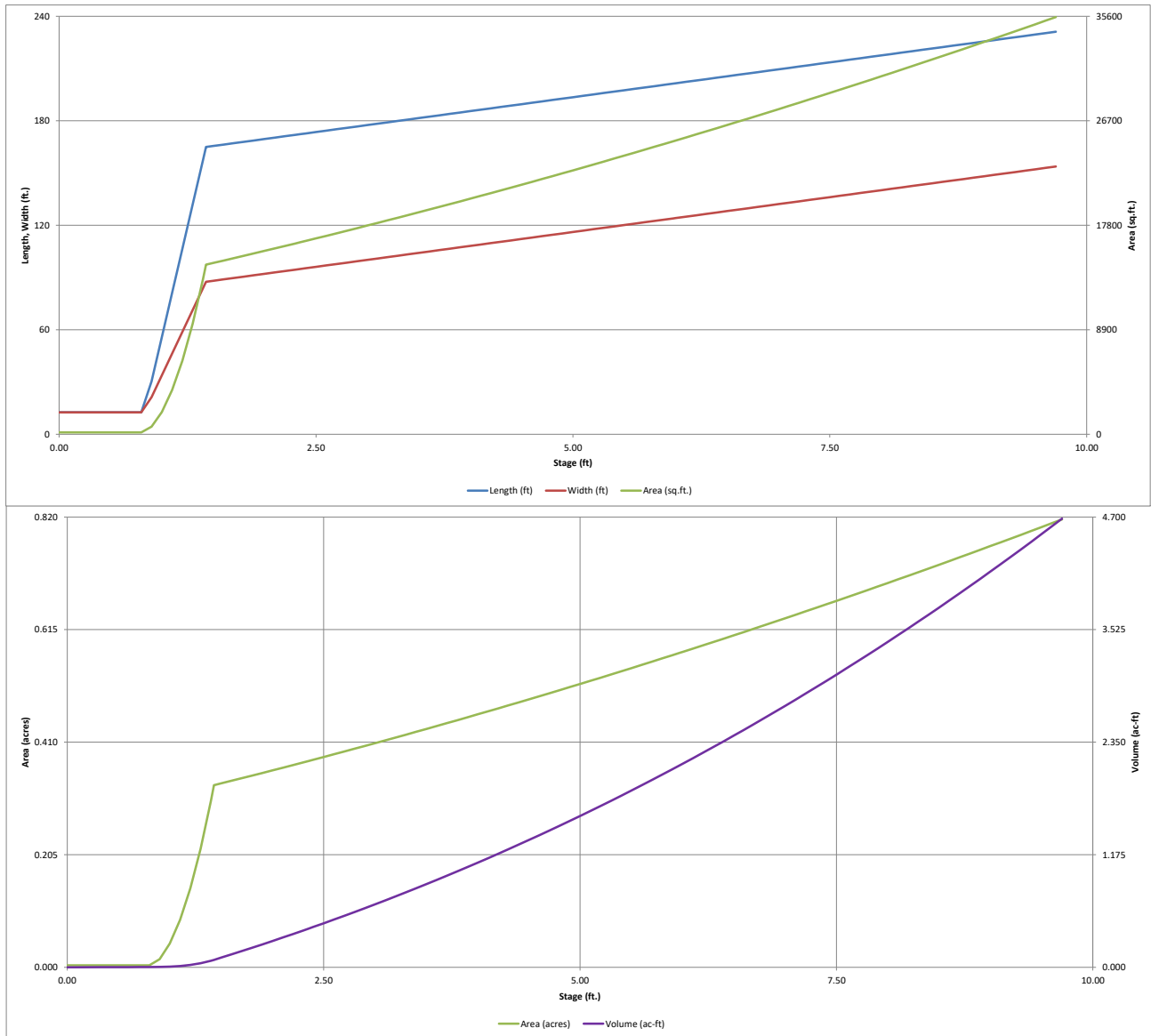
|   |       |                 |
|---|-------|-----------------|
| Zone 1 Volume (WQCV) =                                  | 0.399 | acre-feet       |
| Zone 2 Volume (EURV - Zone 1) =                         | 0.644 | acre-feet       |
| Zone 3 Volume (100-year - Zones 1 & 2) =                | 1.067 | acre-feet       |
| Total Detention Basin Volume =                          | 2.110 | acre-feet       |
| Initial Surge Volume (ISV) =                            | 52    | ft <sup>3</sup> |
| Initial Surge Depth (ISD) =                             | 0.33  | ft              |
| Total Available Detention Depth (H <sub>total</sub> ) = | 6.00  | ft              |
| Depth of Trickle Channel (H <sub>TC</sub> ) =           | 0.50  | ft              |
| Slope of Trickle Channel (S <sub>TC</sub> ) =           | 0.004 | ft/ft           |
| Slopes of Main Basin Sides (S <sub>main</sub> ) =       | 4     | H:V             |
| Basin Length-to-Width Ratio (R <sub>LW</sub> ) =        | 2     |                 |

|   |              |                 |
|---|--------------|-----------------|
| Initial Surge Area (A <sub>ISV</sub> ) =              | 158          | ft <sup>2</sup> |
| Surcharge Volume Length (L <sub>ISV</sub> ) =         | 12.6         | ft              |
| Surcharge Volume Width (W <sub>ISV</sub> ) =          | 12.6         | ft              |
| Depth of Basin Floor (H <sub>FLOOR</sub> ) =          | 0.60         | ft              |
| Length of Basin Floor (L <sub>FLOOR</sub> ) =         | 165.0        | ft              |
| Width of Basin Floor (W <sub>FLOOR</sub> ) =          | 87.6         | ft              |
| Area of Basin Floor (A <sub>FLOOR</sub> ) =           | 14,448       | ft <sup>2</sup> |
| Volume of Basin Floor (V <sub>FLOOR</sub> ) =         | 3,223        | ft <sup>3</sup> |
| Depth of Main Basin (H <sub>MAIN</sub> ) =            | 4.57         | ft              |
| Length of Main Basin (L <sub>MAIN</sub> ) =           | 201.5        | ft              |
| Width of Main Basin (W <sub>MAIN</sub> ) =            | 124.1        | ft              |
| Area of Main Basin (A <sub>MAIN</sub> ) =             | 25,017       | ft <sup>2</sup> |
| Volume of Main Basin (V <sub>MAIN</sub> ) =           | 89,079       | ft <sup>3</sup> |
| Calculated Total Basin Volume (V <sub>total</sub> ) = | <b>2.122</b> | acre-feet       |

| Depth Increment =           | 0.10       | ft                           |             |            |                         |   |             |                           |                |
|-----------------------------|------------|------------------------------|-------------|------------|-------------------------|---|-------------|---------------------------|----------------|
| Stage - Storage Description | Stage (ft) | Optional Override Stage (ft) | Length (ft) | Width (ft) | Area (ft <sup>2</sup> ) | Optional Override Area (ft <sup>2</sup> ) | Area (acre) | Volume (ft <sup>3</sup> ) | Volume (ac-ft) |
| Top of Micropool            | 0.00       |                              | 12.6        | 12.6       | 158                     |   | 0.004       |                           |                |
| ISV                         | 0.33       |                              | 12.6        | 12.6       | 158                     |   | 0.004       | 52                        | 0.001          |
|                             | 0.40       |                              | 12.6        | 12.6       | 158                     |   | 0.004       | 63                        | 0.001          |
|                             | 0.50       |                              | 12.6        | 12.6       | 158                     |   | 0.004       | 79                        | 0.002          |
|                             | 0.60       |                              | 12.6        | 12.6       | 158                     |   | 0.004       | 95                        | 0.002          |
|                             | 0.70       |                              | 12.6        | 12.6       | 158                     |   | 0.004       | 111                       | 0.003          |
|                             | 0.80       |                              | 12.6        | 12.6       | 158                     |   | 0.004       | 126                       | 0.003          |
|                             | 0.90       |                              | 30.4        | 21.3       | 647                     |   | 0.015       | 158                       | 0.004          |
|                             | 1.00       |                              | 55.8        | 33.8       | 1,886                   |   | 0.043       | 279                       | 0.006          |
|                             | 1.10       |                              | 81.2        | 46.3       | 3,759                   |   | 0.086       | 556                       | 0.013          |
|                             | 1.20       |                              | 106.6       | 58.8       | 6,268                   |   | 0.144       | 1,052                     | 0.024          |
|                             | 1.30       |                              | 132.0       | 71.3       | 9,412                   |   | 0.216       | 1,831                     | 0.042          |
| Floor                       | 1.40       |                              | 157.4       | 83.8       | 13,190                  |   | 0.303       | 2,956                     | 0.068          |
|                             | 1.43       |                              | 165.0       | 87.6       | 14,448                  |   | 0.332       | 3,370                     | 0.077          |
|                             | 1.50       |                              | 165.5       | 88.1       | 14,589                  |   | 0.335       | 4,386                     | 0.101          |
|                             | 1.60       |                              | 166.3       | 88.9       | 14,793                  |   | 0.340       | 5,855                     | 0.134          |
|                             | 1.70       |                              | 167.1       | 89.7       | 14,998                  |   | 0.344       | 7,345                     | 0.169          |
|                             | 1.80       |                              | 167.9       | 90.5       | 15,204                  |   | 0.349       | 8,855                     | 0.203          |
|                             | 1.90       |                              | 168.7       | 91.3       | 15,411                  |   | 0.354       | 10,386                    | 0.238          |
|                             | 2.00       |                              | 169.5       | 92.1       | 15,620                  |   | 0.359       | 11,937                    | 0.274          |
|                             | 2.10       |                              | 170.3       | 92.9       | 15,830                  |   | 0.363       | 13,510                    | 0.310          |
|                             | 2.20       |                              | 171.1       | 93.7       | 16,041                  |   | 0.368       | 15,103                    | 0.347          |
|                             | 2.30       |                              | 171.9       | 94.5       | 16,254                  |   | 0.373       | 16,718                    | 0.384          |
| Zone 1 (WQCV)               | 2.35       |                              | 172.3       | 94.9       | 16,361                  |   | 0.376       | 17,533                    | 0.403          |
|                             | 2.40       |                              | 172.7       | 95.3       | 16,468                  |   | 0.378       | 18,354                    | 0.421          |
|                             | 2.50       |                              | 173.5       | 96.1       | 16,683                  |   | 0.383       | 20,012                    | 0.459          |
|                             | 2.60       |                              | 174.3       | 96.9       | 16,899                  |   | 0.388       | 21,691                    | 0.498          |
|                             | 2.70       |                              | 175.1       | 97.7       | 17,117                  |   | 0.393       | 23,391                    | 0.537          |
|                             | 2.80       |                              | 175.9       | 98.5       | 17,336                  |   | 0.398       | 25,114                    | 0.577          |
|                             | 2.90       |                              | 176.7       | 99.3       | 17,556                  |   | 0.403       | 26,859                    | 0.617          |
|                             | 3.00       |                              | 177.5       | 100.1      | 17,777                  |   | 0.408       | 28,625                    | 0.657          |
|                             | 3.10       |                              | 178.3       | 100.9      | 18,000                  |   | 0.413       | 30,414                    | 0.698          |
|                             | 3.20       |                              | 179.1       | 101.7      | 18,224                  |   | 0.418       | 32,225                    | 0.740          |
|                             | 3.30       |                              | 179.9       | 102.5      | 18,450                  |   | 0.424       | 34,059                    | 0.782          |
|                             | 3.40       |                              | 180.7       | 103.3      | 18,676                  |   | 0.429       | 35,915                    | 0.825          |
|                             | 3.50       |                              | 181.5       | 104.1      | 18,904                  |   | 0.434       | 37,794                    | 0.868          |
|                             | 3.60       |                              | 182.3       | 104.9      | 19,133                  |   | 0.439       | 39,696                    | 0.911          |
|                             | 3.70       |                              | 183.1       | 105.7      | 19,364                  |   | 0.445       | 41,621                    | 0.955          |
|                             | 3.80       |                              | 183.9       | 106.5      | 19,595                  |   | 0.450       | 43,569                    | 1.000          |
| Zone 2 (EURV)               | 3.90       |                              | 184.7       | 107.3      | 19,828                  |   | 0.455       | 45,540                    | 1.045          |
|                             | 4.00       |                              | 185.5       | 108.1      | 20,063                  |   | 0.461       | 47,535                    | 1.091          |
|                             | 4.10       |                              | 186.3       | 108.9      | 20,298                  |   | 0.466       | 49,553                    | 1.138          |
|                             | 4.20       |                              | 187.1       | 109.7      | 20,535                  |   | 0.471       | 51,594                    | 1.184          |
|                             | 4.30       |                              | 187.9       | 110.5      | 20,773                  |   | 0.477       | 53,660                    | 1.232          |
|                             | 4.40       |                              | 188.7       | 111.3      | 21,013                  |   | 0.482       | 55,749                    | 1.280          |
|                             | 4.50       |                              | 189.5       | 112.1      | 21,253                  |   | 0.488       | 57,862                    | 1.328          |
|                             | 4.60       |                              | 190.3       | 112.9      | 21,495                  |   | 0.493       | 60,000                    | 1.377          |
|                             | 4.70       |                              | 191.1       | 113.7      | 21,739                  |   | 0.499       | 62,161                    | 1.427          |
|                             | 4.80       |                              | 191.9       | 114.5      | 21,983                  |   | 0.505       | 64,347                    | 1.477          |
|                             | 4.90       |                              | 192.7       | 115.3      | 22,229                  |   | 0.510       | 66,558                    | 1.528          |
|                             | 5.00       |                              | 193.5       | 116.1      | 22,476                  |   | 0.516       | 68,793                    | 1.579          |
|                             | 5.10       |                              | 194.3       | 116.9      | 22,724                  |   | 0.522       | 71,053                    | 1.631          |
|                             | 5.20       |                              | 195.1       | 117.7      | 22,974                  |   | 0.527       | 73,338                    | 1.684          |
|                             | 5.30       |                              | 195.9       | 118.5      | 23,225                  |   | 0.533       | 75,648                    | 1.737          |
|                             | 5.40       |                              | 196.7       | 119.3      | 23,477                  |   | 0.539       | 77,983                    | 1.790          |
|                             | 5.50       |                              | 197.5       | 120.1      | 23,731                  |   | 0.545       | 80,344                    | 1.844          |
|                             | 5.60       |                              | 198.3       | 120.9      | 23,986                  |   | 0.551       | 82,729                    | 1.899          |
|                             | 5.70       |                              | 199.1       | 121.7      | 24,242                  |   | 0.557       | 85,141                    | 1.955          |
|                             | 5.80       |                              | 199.9       | 122.5      | 24,499                  |   | 0.562       | 87,578                    | 2.011          |
| Zone 3 (100-year)           | 5.90       |                              | 200.7       | 123.3      | 24,758                  |   | 0.568       | 90,041                    | 2.067          |
|                             | 5.98       |                              | 201.4       | 124.0      | 24,965                  |   | 0.573       | 92,030                    | 2.113          |
|                             | 6.00       |                              | 201.5       | 124.1      | 25,017                  |   | 0.574       | 92,529                    | 2.124          |
|                             | 6.10       |                              | 202.3       | 124.9      | 25,279                  |   | 0.580       | 95,044                    | 2.182          |
|                             | 6.20       |                              | 203.1       | 125.7      | 25,541                  |   | 0.586       | 97,585                    | 2.240          |
|                             | 6.30       |                              | 203.9       | 126.5      | 25,805                  |   | 0.592       | 100,152                   | 2.299          |
|                             | 6.40       |                              | 204.7       | 127.3      | 26,070                  |   | 0.598       | 102,746                   | 2.359          |
|                             | 6.50       |                              | 205.5       | 128.1      | 26,336                  |   | 0.605       | 105,366                   | 2.419          |
|                             | 6.60       |                              | 206.3       | 128.9      | 26,604                  |   | 0.611       | 108,013                   | 2.480          |
|                             | 6.70       |                              | 207.1       | 129.7      | 26,873                  |   | 0.617       | 110,687                   | 2.541          |
|                             | 6.80       |                              | 207.9       | 130.5      | 27,143                  |   | 0.623       | 113,388                   | 2.603          |
|                             | 6.90       |                              | 208.7       | 131.3      | 27,414                  |   | 0.629       | 116,116                   | 2.666          |
|                             | 7.00       |                              | 209.5       | 132.1      | 27,687                  |   | 0.636       | 118,871                   | 2.729          |
|                             | 7.10       |                              | 210.3       | 132.9      | 27,961                  |   | 0.642       | 121,653                   | 2.793          |
|                             | 7.20       |                              | 211.1       | 133.7      | 28,236                  |   | 0.648       | 124,463                   | 2.857          |
|                             | 7.30       |                              | 211.9       | 134.5      | 28,513                  |   | 0.655       | 127,300                   | 2.922          |
|                             | 7.40       |                              | 212.7       | 135.3      | 28,790                  |   | 0.661       | 130,166                   | 2.988          |
|                             | 7.50       |                              | 213.5       | 136.1      | 29,069                  |   | 0.667       | 133,059                   | 3.055          |
|                             | 7.60       |                              | 214.3       | 136.9      | 29,350                  |   | 0.674       | 135,979                   | 3.122          |
|                             | 7.70       |                              | 215.1       | 137.7      | 29,631                  |   | 0.680       | 138,929                   | 3.189          |
|                             | 7.80       |                              | 215.9       | 138.5      | 29,914                  |   | 0.687       | 141,906                   | 3.258          |
|                             | 7.90       |                              | 216.7       | 139.3      | 30,199                  |   | 0.693       | 144,911                   | 3.327          |
|                             | 8.00       |                              | 217.5       | 140.1      | 30,484                  |   | 0.700       | 147,946                   | 3.396          |
|                             | 8.10       |                              | 218.3       | 140.9      | 30,771                  |   | 0.706       | 151,008                   | 3.467          |
|                             | 8.20       |                              | 219.1       | 141.7      | 31,059                  |   | 0.713       | 154,100                   | 3.538          |
|                             | 8.30       |                              | 219.9       | 142.5      | 31,348                  |   | 0.720       | 157,220                   | 3.609          |
|                             | 8.40       |                              | 220.7       | 143.3      | 31,639                  |   | 0.726       | 160,369                   | 3.682          |
|                             | 8.50       |                              | 221.5       | 144.1      | 31,931                  |   | 0.733       | 163,548                   | 3.755          |
|                             | 8.60       |                              | 222.3       | 144.9      | 32,224                  |   | 0.740       | 166,756                   | 3.828          |
|                             | 8.70       |                              | 223.1       | 145.7      | 32,518                  |   | 0.747       | 169,993                   | 3.902          |
|                             | 8.80       |                              | 223.9       | 146.5      | 32,814                  |   | 0.753       | 173,259                   | 3.977          |
|                             | 8.90       |                              | 224.7       | 147.3      | 33,111                  |   | 0.760       | 176,556                   | 4.053          |
|                             | 9.00       |                              | 225.5       | 148.1      | 33,409                  |   | 0.767       | 179,882                   | 4.130          |
|                             | 9.10       |                              | 226.3       | 148.9      | 33,709                  |   | 0.774       | 183,238                   | 4.207          |
|                             | 9.20       |                              | 227.1       | 149.7      | 34,010                  |   | 0.781       | 186,624                   | 4.284          |
|                             | 9.30       |                              | 227.9       | 150.5      | 34,312                  |   | 0.788       | 190,040                   | 4.363          |
|                             | 9.40       |                              | 228.7       | 151.3      | 34,615                  |   | 0.795       | 193,486                   | 4.442          |
|                             | 9.50       |                              | 229.5       | 152.1      | 34,920                  |   | 0.802       | 196,963                   | 4.522          |
|                             | 9.60       |                              | 230.3       | 152.9      | 35,226                  |   | 0.809       | 200,470                   | 4.602          |
|                             | 9.70       |                              | 231.1       | 153.7      | 35,533                  |   | 0.816       | 204,008                   | 4.683          |

# DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.05 (January 2022)

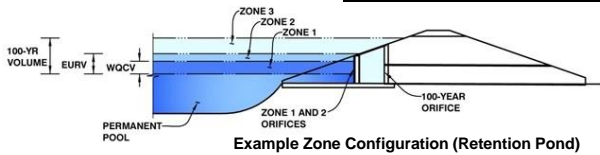


# DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-DETENTION, Version 4.05 (January 2022)

Project: Flying Horse North MDDP

Basin ID: Pond 16



Example Zone Configuration (Retention Pond)

|                   | Estimated Stage (ft) | Estimated Volume (ac-ft) | Outlet Type          |
|-------------------|----------------------|--------------------------|----------------------|
| Zone 1 (WQCV)     | 2.35                 | 0.399                    | Orifice Plate        |
| Zone 2 (EURV)     | 3.90                 | 0.644                    | Circular Orifice     |
| Zone 3 (100-year) | 5.98                 | 1.067                    | Weir&Pipe (Restrict) |
| Total (all zones) |                      | 2.110                    |                      |

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth =  ft (distance below the filtration media surface)  
Underdrain Orifice Diameter =  inches

Calculated Parameters for Underdrain  
Underdrain Orifice Area =  ft<sup>2</sup>  
Underdrain Orifice Centroid =  feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Centroid of Lowest Orifice =  ft (relative to basin bottom at Stage = 0 ft)  
Depth at top of Zone using Orifice Plate =  ft (relative to basin bottom at Stage = 0 ft)  
Orifice Plate: Orifice Vertical Spacing =  inches  
Orifice Plate: Orifice Area per Row =  sq. inches (diameter = 1-5/16 inches)

Calculated Parameters for Plate  
WQ Orifice Area per Row =  ft<sup>2</sup>  
Elliptical Half-Width =  feet  
Elliptical Slot Centroid =  feet  
Elliptical Slot Area =  ft<sup>2</sup>

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

|                                | Row 1 (required) | Row 2 (optional) | Row 3 (optional) | Row 4 (optional) | Row 5 (optional) | Row 6 (optional) | Row 7 (optional) | Row 8 (optional) |
|--------------------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|
| Stage of Orifice Centroid (ft) | 0.00             | 0.80             | 1.60             |                  |                  |                  |                  |                  |
| Orifice Area (sq. inches)      | 1.40             | 1.40             | 1.40             |                  |                  |                  |                  |                  |

|                                | Row 9 (optional) | Row 10 (optional) | Row 11 (optional) | Row 12 (optional) | Row 13 (optional) | Row 14 (optional) | Row 15 (optional) | Row 16 (optional) |
|--------------------------------|------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| Stage of Orifice Centroid (ft) |                  |                   |                   |                   |                   |                   |                   |                   |
| Orifice Area (sq. inches)      |                  |                   |                   |                   |                   |                   |                   |                   |

User Input: Vertical Orifice (Circular or Rectangular)

Invert of Vertical Orifice =  ft (relative to basin bottom at Stage = 0 ft)  
Depth at top of Zone using Vertical Orifice =  ft (relative to basin bottom at Stage = 0 ft)  
Vertical Orifice Diameter =  inches

Calculated Parameters for Vertical Orifice  
Zone 2 Circular Not Selected  
Vertical Orifice Area =  ft<sup>2</sup>  
Vertical Orifice Centroid =  feet

User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir and No Outlet Pipe)

Overflow Weir Front Edge Height, H<sub>o</sub> =  ft (relative to basin bottom at Stage = 0 ft)  
Overflow Weir Front Edge Length =  feet  
Overflow Weir Grate Slope =  H:V  
Horiz. Length of Weir Sides =  feet  
Overflow Grate Type =   
Debris Clogging % =  %

Calculated Parameters for Overflow Weir  
Zone 3 Weir Not Selected  
Height of Grate Upper Edge, H<sub>u</sub> =  feet  
Overflow Weir Slope Length =  feet  
Grate Open Area / 100-yr Orifice Area =   
Overflow Grate Open Area w/o Debris =  ft<sup>2</sup>  
Overflow Grate Open Area w/ Debris =  ft<sup>2</sup>

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

Depth to Invert of Outlet Pipe =  ft (distance below basin bottom at Stage = 0 ft)  
Outlet Pipe Diameter =  inches  
Restrictor Plate Height Above Pipe Invert =  inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate  
Zone 3 Restrictor Not Selected  
Outlet Orifice Area =  ft<sup>2</sup>  
Outlet Orifice Centroid =  feet  
Half-Central Angle of Restrictor Plate on Pipe =  radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage =  ft (relative to basin bottom at Stage = 0 ft)  
Spillway Crest Length =  feet  
Spillway End Slopes =  H:V  
Freeboard above Max Water Surface =  feet

Calculated Parameters for Spillway  
Spillway Design Flow Depth =  feet  
Stage at Top of Freeboard =  feet  
Basin Area at Top of Freeboard =  acres  
Basin Volume at Top of Freeboard =  acre-ft

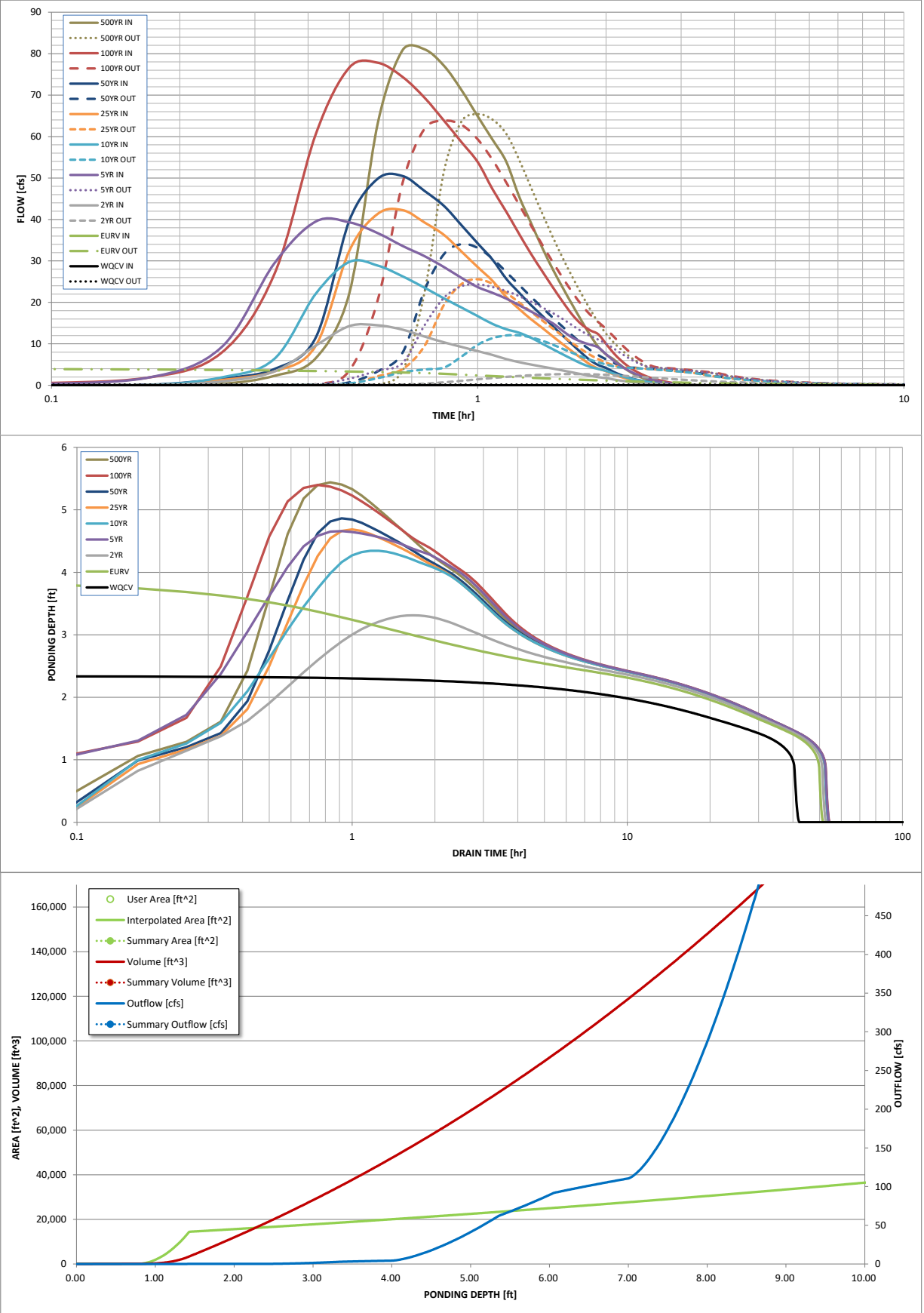
## Routed Hydrograph Results

The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).

|  | WQCV               | EURV               | 2 Year             | 5 Year          | 10 Year         | 25 Year         | 50 Year         | 100 Year        | 500 Year        |
|--|--------------------|--------------------|--------------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|
| Design Storm Return Period =                       | N/A                | N/A                | 1.19               | 1.50            | 1.75            | 2.00            | 2.25            | 2.52            | 3.14            |
| One-Hour Rainfall Depth (in) =                     | 0.399              | 1.043              | 1.034              | 1.610           | 2.133           | 2.899           | 3.492           | 4.270           | 5.793           |
| CUHP Runoff Volume (acre-ft) =                     | N/A                | N/A                | 1.034              | 3.422           | 2.133           | 2.899           | 3.492           | 6.198           | 5.793           |
| User Override Inflow Hydrograph Volume (acre-ft) = | N/A                | N/A                | 3.3                | 9.3             | 14.0            | 24.7            | 31.0            | 39.7            | 55.2            |
| CUHP Predevelopment Peak Q (cfs) =                 | N/A                | N/A                | 0.11               | 0.84            | 0.48            | 0.85            | 1.07            | 2.46            | 1.91            |
| OPTIONAL Override Predevelopment Peak Q (cfs) =    | N/A                | N/A                | 14.5               | 39.5            | 29.8            | 42.2            | 50.5            | 77.8            | 81.0            |
| Predevelopment Unit Peak Flow, q (cfs/acre) =      | N/A                | N/A                | 2.7                | 24.3            | 12.0            | 25.6            | 34.1            | 63.8            | 65.4            |
| Peak Inflow Q (cfs) =                              | N/A                | N/A                | N/A                | 1.0             | 0.9             | 1.0             | 1.1             | 0.9             | 1.2             |
| Peak Outflow Q (cfs) =                             | N/A                | N/A                | N/A                | N/A             | N/A             | N/A             | N/A             | N/A             | N/A             |
| Ratio Peak Outflow to Predevelopment Q =           | N/A                | N/A                | N/A                | N/A             | N/A             | N/A             | N/A             | N/A             | N/A             |
| Structure Controlling Flow =                       | Vertical Orifice 1 | Vertical Orifice 1 | Vertical Orifice 1 | Overflow Weir 1 | Overflow Weir 1 | Overflow Weir 1 | Overflow Weir 1 | Overflow Weir 1 | Overflow Weir 1 |
| Max Velocity through Grate 1 (fps) =               | N/A                | N/A                | N/A                | 0.9             | 0.3             | 1.0             | 1.4             | 2.8             | 2.8             |
| Max Velocity through Grate 2 (fps) =               | N/A                | N/A                | N/A                | N/A             | N/A             | N/A             | N/A             | N/A             | N/A             |
| Time to Drain 97% of Inflow Volume (hours) =       | 39                 | 46                 | 47                 | 39              | 43              | 40              | 38              | 29              | 31              |
| Time to Drain 99% of Inflow Volume (hours) =       | 40                 | 49                 | 50                 | 48              | 49              | 48              | 47              | 44              | 44              |
| Maximum Ponding Depth (ft) =                       | 2.35               | 3.90               | 3.31               | 4.66            | 4.34            | 4.69            | 4.86            | 5.40            | 5.44            |
| Area at Maximum Ponding Depth (acres) =            | 0.38               | 0.46               | 0.42               | 0.50            | 0.48            | 0.50            | 0.51            | 0.54            | 0.54            |
| Maximum Volume Stored (acre-ft) =                  | 0.403              | 1.045              | 0.786              | 1.402           | 1.251           | 1.417           | 1.508           | 1.785           | 1.806           |

DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.05 (January 2022)



| S-A-V-D Chart Axis Override | X-axis | Left Y-Axis | Right Y-Axis |
|-----------------------------|--------|-------------|--------------|
| minimum bound               |        |             |              |
| maximum bound               |        |             |              |

# DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename:

## Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

|               | SOURCE  | CUHP       | CUHP       | CUHP         | USER         | CUHP          | CUHP          | CUHP          | USER           | CUHP           |
|---------------|---------|------------|------------|--------------|--------------|---------------|---------------|---------------|----------------|----------------|
| Time Interval | TIME    | WQCV [cfs] | EURV [cfs] | 2 Year [cfs] | 5 Year [cfs] | 10 Year [cfs] | 25 Year [cfs] | 50 Year [cfs] | 100 Year [cfs] | 500 Year [cfs] |
| 5.00 min      | 0:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 0:05:00 | 0.00       | 0.00       | 0.00         | 0.13         | 0.00          | 0.00          | 0.00          | 0.32           | 0.00           |
|               | 0:10:00 | 0.00       | 0.00       | 0.00         | 1.77         | 0.00          | 0.00          | 0.11          | 1.79           | 0.34           |
|               | 0:15:00 | 0.00       | 0.00       | 0.92         | 9.10         | 1.88          | 1.27          | 1.60          | 7.77           | 2.28           |
|               | 0:20:00 | 0.00       | 0.00       | 3.34         | 29.42        | 6.38          | 3.35          | 3.92          | 26.81          | 6.51           |
|               | 0:25:00 | 0.00       | 0.00       | 9.57         | 39.49        | 22.05         | 9.51          | 11.47         | 60.50          | 22.27          |
|               | 0:30:00 | 0.00       | 0.00       | 14.29        | 39.30        | 29.77         | 32.48         | 39.77         | 76.66          | 63.40          |
|               | 0:35:00 | 0.00       | 0.00       | 14.47        | 36.68        | 28.86         | 41.39         | 49.87         | 77.79          | 80.87          |
|               | 0:40:00 | 0.00       | 0.00       | 13.41        | 33.60        | 26.27         | 42.25         | 50.47         | 74.36          | 81.05          |
|               | 0:45:00 | 0.00       | 0.00       | 11.76        | 31.16        | 23.55         | 39.28         | 46.89         | 69.39          | 77.08          |
|               | 0:50:00 | 0.00       | 0.00       | 10.37        | 28.52        | 20.96         | 36.28         | 43.27         | 63.84          | 71.17          |
|               | 0:55:00 | 0.00       | 0.00       | 9.25         | 25.89        | 18.74         | 32.24         | 38.58         | 58.62          | 64.89          |
|               | 1:00:00 | 0.00       | 0.00       | 8.24         | 23.69        | 16.69         | 28.51         | 34.22         | 53.85          | 59.25          |
|               | 1:05:00 | 0.00       | 0.00       | 7.31         | 22.30        | 14.81         | 25.19         | 30.31         | 47.30          | 53.94          |
|               | 1:10:00 | 0.00       | 0.00       | 6.32         | 20.91        | 13.52         | 21.30         | 25.69         | 41.88          | 45.60          |
|               | 1:15:00 | 0.00       | 0.00       | 5.58         | 19.32        | 12.68         | 18.43         | 22.36         | 36.55          | 39.18          |
|               | 1:20:00 | 0.00       | 0.00       | 5.01         | 17.80        | 11.48         | 15.95         | 19.36         | 31.73          | 33.21          |
|               | 1:25:00 | 0.00       | 0.00       | 4.51         | 16.35        | 10.05         | 13.86         | 16.79         | 27.53          | 28.00          |
|               | 1:30:00 | 0.00       | 0.00       | 4.04         | 14.97        | 8.71          | 11.81         | 14.28         | 23.67          | 23.53          |
|               | 1:35:00 | 0.00       | 0.00       | 3.57         | 13.11        | 7.47          | 9.92          | 11.98         | 20.13          | 19.43          |
|               | 1:40:00 | 0.00       | 0.00       | 3.12         | 11.52        | 6.31          | 8.17          | 9.85          | 17.04          | 15.66          |
|               | 1:45:00 | 0.00       | 0.00       | 2.69         | 10.50        | 5.26          | 6.52          | 7.85          | 14.74          | 12.20          |
|               | 1:50:00 | 0.00       | 0.00       | 2.33         | 9.82         | 4.48          | 5.06          | 6.09          | 13.29          | 9.32           |
|               | 1:55:00 | 0.00       | 0.00       | 1.97         | 9.15         | 3.95          | 4.02          | 4.89          | 12.33          | 7.44           |
|               | 2:00:00 | 0.00       | 0.00       | 1.73         | 7.52         | 3.49          | 3.41          | 4.18          | 10.02          | 6.27           |
|               | 2:05:00 | 0.00       | 0.00       | 1.40         | 5.94         | 2.83          | 2.64          | 3.26          | 7.78           | 4.79           |
|               | 2:10:00 | 0.00       | 0.00       | 1.13         | 4.69         | 2.25          | 2.01          | 2.49          | 6.03           | 3.57           |
|               | 2:15:00 | 0.00       | 0.00       | 0.90         | 3.67         | 1.78          | 1.55          | 1.91          | 4.63           | 2.64           |
|               | 2:20:00 | 0.00       | 0.00       | 0.71         | 2.86         | 1.39          | 1.18          | 1.46          | 3.57           | 1.92           |
|               | 2:25:00 | 0.00       | 0.00       | 0.56         | 2.19         | 1.07          | 0.90          | 1.11          | 2.74           | 1.41           |
|               | 2:30:00 | 0.00       | 0.00       | 0.44         | 1.65         | 0.82          | 0.69          | 0.84          | 2.09           | 1.05           |
|               | 2:35:00 | 0.00       | 0.00       | 0.34         | 1.24         | 0.61          | 0.52          | 0.63          | 1.60           | 0.79           |
|               | 2:40:00 | 0.00       | 0.00       | 0.27         | 0.92         | 0.46          | 0.39          | 0.48          | 1.23           | 0.61           |
|               | 2:45:00 | 0.00       | 0.00       | 0.21         | 0.67         | 0.35          | 0.30          | 0.37          | 0.91           | 0.47           |
|               | 2:50:00 | 0.00       | 0.00       | 0.16         | 0.46         | 0.27          | 0.23          | 0.28          | 0.65           | 0.36           |
|               | 2:55:00 | 0.00       | 0.00       | 0.11         | 0.30         | 0.19          | 0.17          | 0.20          | 0.42           | 0.26           |
|               | 3:00:00 | 0.00       | 0.00       | 0.08         | 0.17         | 0.13          | 0.12          | 0.14          | 0.25           | 0.18           |
|               | 3:05:00 | 0.00       | 0.00       | 0.05         | 0.08         | 0.08          | 0.07          | 0.09          | 0.12           | 0.11           |
|               | 3:10:00 | 0.00       | 0.00       | 0.02         | 0.03         | 0.04          | 0.04          | 0.05          | 0.04           | 0.06           |
|               | 3:15:00 | 0.00       | 0.00       | 0.01         | 0.00         | 0.02          | 0.02          | 0.02          | 0.00           | 0.02           |
|               | 3:20:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:25:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:30:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:35:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:40:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:45:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:50:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 3:55:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:05:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:10:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:15:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:20:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:25:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:30:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:35:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:40:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:45:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:50:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:55:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:05:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:10:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:15:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:20:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:25:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:30:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:35:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:40:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:45:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:50:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:55:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 6:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |



## DETENTION BASIN OUTLET STRUCTURE DESIGN

*MHFD-Detention, Version 4.05 (January 2022)*

### Summary Stage-Area-Volume-Discharge Relationships

The user can create a summary S-A-V-D by entering the desired stage increments and the remainder of the table will populate automatically.

The user should graphically compare the summary S-A-V-D table to the full S-A-V-D table in the chart to confirm it captures all key transition points.

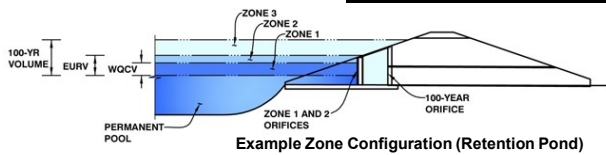
[illegible]

# DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-DETENTION, Version 4.04 (February 2021)

Project: Flying Horse North Drainage Plan

Basin ID: Pond 17



|                   | Estimated Stage (ft) | Estimated Volume (ac-ft) | Outlet Type          |
|-------------------|----------------------|--------------------------|----------------------|
| Zone 1 (WQCV)     | 2.20                 | 0.203                    | Orifice Plate        |
| Zone 2 (EURV)     | 3.19                 | 0.193                    | Circular Orifice     |
| Zone 3 (100-year) | 5.98                 | 0.739                    | Weir&Pipe (Restrict) |
| Total (all zones) |                      | 1.134                    |                      |

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth =  ft (distance below the filtration media surface)  
Underdrain Orifice Diameter =  inches

Calculated Parameters for Underdrain  
Underdrain Orifice Area =  ft<sup>2</sup>  
Underdrain Orifice Centroid =  feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice =  ft (relative to basin bottom at Stage = 0 ft)  
Depth at top of Zone using Orifice Plate =  ft (relative to basin bottom at Stage = 0 ft)  
Orifice Plate: Orifice Vertical Spacing =  inches  
Orifice Plate: Orifice Area per Row =  sq. inches (diameter = 1-1/16 inches)

Calculated Parameters for Plate  
WQ Orifice Area per Row =  ft<sup>2</sup>  
Elliptical Half-Width =  feet  
Elliptical Slot Centroid =  feet  
Elliptical Slot Area =  ft<sup>2</sup>

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

|                                | Row 1 (required) | Row 2 (optional) | Row 3 (optional) | Row 4 (optional) | Row 5 (optional) | Row 6 (optional) | Row 7 (optional) | Row 8 (optional) |
|--------------------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|
| Stage of Orifice Centroid (ft) | 0.00             | 0.73             | 1.47             |                  |                  |                  |                  |                  |
| Orifice Area (sq. inches)      | 0.86             | 0.86             | 0.86             |                  |                  |                  |                  |                  |

|                                | Row 9 (optional) | Row 10 (optional) | Row 11 (optional) | Row 12 (optional) | Row 13 (optional) | Row 14 (optional) | Row 15 (optional) | Row 16 (optional) |
|--------------------------------|------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| Stage of Orifice Centroid (ft) |                  |                   |                   |                   |                   |                   |                   |                   |
| Orifice Area (sq. inches)      |                  |                   |                   |                   |                   |                   |                   |                   |

User Input: Vertical Orifice (Circular or Rectangular)

Invert of Vertical Orifice =  ft (relative to basin bottom at Stage = 0 ft)  
Depth at top of Zone using Vertical Orifice =  ft (relative to basin bottom at Stage = 0 ft)  
Vertical Orifice Diameter =  inches

Calculated Parameters for Vertical Orif  
Zone 2 Circular Not Selected  
Vertical Orifice Area =  ft<sup>2</sup>  
Vertical Orifice Centroid =  feet

User Input: Overflow Weir (Dropbox with Flat or Sloped Gate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe)

Overflow Weir Front Edge Height, H<sub>o</sub> =  ft (relative to basin bottom at Stage = 0 ft)  
Overflow Weir Front Edge Length =  feet  
Overflow Weir Gate Slope =  H:V  
Horiz. Length of Weir Sides =  feet  
Overflow Gate Type =   
Debris Clogging % =  %

Calculated Parameters for Overflow W  
Zone 3 Weir Not Selected  
Height of Gate Upper Edge, H<sub>u</sub> =  ft  
Overflow Weir Slope Length =  feet  
Gate Open Area / 100-yr Orifice Area =  ft<sup>2</sup>  
Overflow Gate Open Area w/o Debris =  ft<sup>2</sup>  
Overflow Gate Open Area w/ Debris =  ft<sup>2</sup>

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

Depth to Invert of Outlet Pipe =  ft (distance below basin bottom at Stage = 0 ft)  
Outlet Pipe Diameter =  inches  
Restrictor Plate Height Above Pipe Invert =  inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Pl  
Zone 3 Restrictor Not Selected  
Outlet Orifice Area =  ft<sup>2</sup>  
Outlet Orifice Centroid =  feet  
Half-Central Angle of Restrictor Plate on Pipe =  degrees

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage =  ft (relative to basin bottom at Stage = 0 ft)  
Spillway Crest Length =  feet  
Spillway End Slopes =  H:V  
Freeboard above Max Water Surface =  feet

Calculated Parameters for Spillway  
Spillway Design Flow Depth =  feet  
Stage at Top of Freeboard =  feet  
Basin Area at Top of Freeboard =  acres  
Basin Volume at Top of Freeboard =  acre-ft

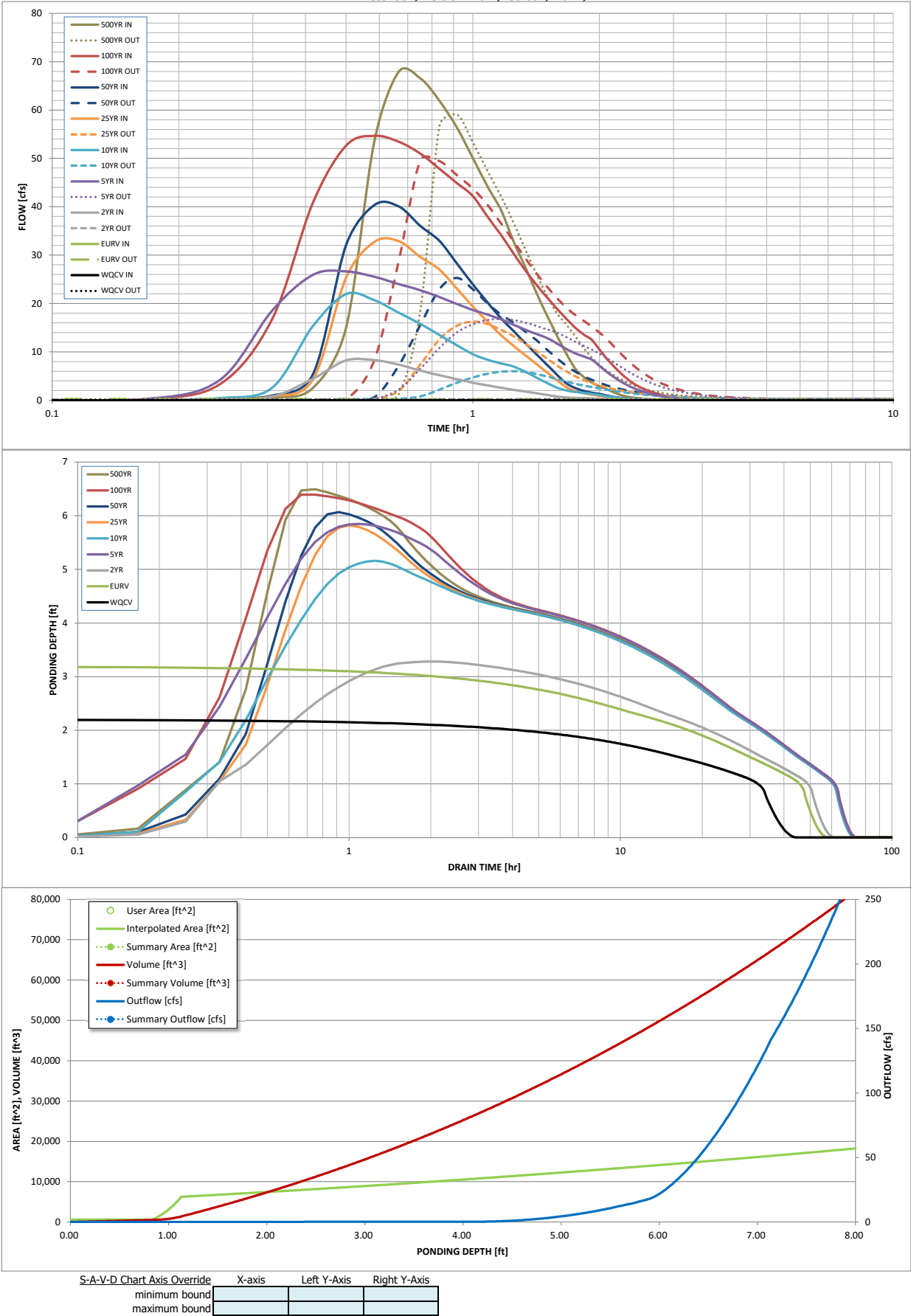
## Routed Hydrograph Results

The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through A)

|  | WQCV               | EURV               | 2 Year             | 5 Year          | 10 Year         | 25 Year         | 50 Year  | 100 Year |
|--|--------------------|--------------------|--------------------|-----------------|-----------------|-----------------|----------|----------|
| Design Storm Return Period =                       | N/A                | N/A                | 1.19               | 1.50            | 1.75            | 2.00            | 2.25     | 2.52     |
| One-Hour Rainfall Depth (in) =                     | N/A                | N/A                | 1.19               | 1.50            | 1.75            | 2.00            | 2.25     | 2.52     |
| CUHP Runoff Volume (acre-ft) =                     | 0.203              | 0.396              | 0.447              | 0.851           | 1.240           | 1.888           | 2.346    | 2.988    |
| User Override Inflow Hydrograph Volume (acre-ft) = | N/A                | N/A                | 0.447              | 2.651           | 1.240           | 1.888           | 2.346    | 4.897    |
| CUHP Predevelopment Peak Q (cfs) =                 | N/A                | N/A                | 4.1                | 11.0            | 16.6            | 28.4            | 35.5     | 44.4     |
| OPTIONAL Override Predevelopment Peak Q (cfs) =    | N/A                | N/A                |                    | 17.0            |                 |                 |          | 50.0     |
| Predevelopment Unit Peak Flow, q (cfs/acre) =      | N/A                | N/A                | 0.17               | 0.72            | 0.71            | 1.21            | 1.51     | 2.13     |
| Peak Inflow Q (cfs) =                              | N/A                | N/A                | 8.3                | 26.6            | 22.0            | 32.9            | 40.4     | 54.7     |
| Peak Outflow Q (cfs) =                             | 0.1                | 0.2                | 0.2                | 16.8            | 6.0             | 16.3            | 25.3     | 49.6     |
| Ratio Peak Outflow to Predevelopment Q =           | N/A                | N/A                | N/A                | 1.0             | 0.4             | 0.6             | 0.7      | 1.0      |
| Structure Controlling Flow =                       | Vertical Orifice 1 | Vertical Orifice 1 | Vertical Orifice 1 | Overflow Weir 1 | Overflow Weir 1 | Overflow Weir 1 | Spillway | Spillway |
| Max Velocity through Gate 1 (fps) =                | N/A                | N/A                | N/A                | 1.0             | 0.3             | 0.9             | 1.2      | 1.7      |
| Max Velocity through Gate 2 (fps) =                | N/A                | N/A                | N/A                | N/A             | N/A             | N/A             | N/A      | N/A      |
| Time to Drain 97% of Inflow Volume (hours) =       | 37                 | 48                 | 51                 | 47              | 56              | 52              | 49       | 37       |
| Time to Drain 99% of Inflow Volume (hours) =       | 40                 | 52                 | 55                 | 59              | 63              | 61              | 60       | 54       |
| Maximum Ponding Depth (ft) =                       | 2.20               | 3.20               | 3.28               | 5.85            | 5.16            | 5.82            | 6.07     | 6.39     |
| Area at Maximum Ponding Depth (acres) =            | 0.18               | 0.21               | 0.21               | 0.32            | 0.29            | 0.32            | 0.33     | 0.34     |
| Maximum Volume Stored (acre-ft) =                  | 0.203              | 0.398              | 0.415              | 1.092           | 0.883           | 1.083           | 1.163    | 1.273    |

DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD- Detention, Version 4.04 (February 2021)



# DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename: \_\_\_\_\_

## Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

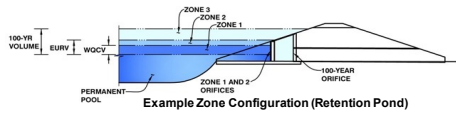
|               | SOURCE  | CUHP       | CUHP       | CUHP         | USER         | CUHP          | CUHP          | CUHP          | USER           | CUHP           |
|---------------|---------|------------|------------|--------------|--------------|---------------|---------------|---------------|----------------|----------------|
| Time Interval | TIME    | WQCV [cfs] | EURV [cfs] | 2 Year [cfs] | 5 Year [cfs] | 10 Year [cfs] | 25 Year [cfs] | 50 Year [cfs] | 100 Year [cfs] | 500 Year [cfs] |
| 5.00 min      | 0:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 0:05:00 | 0.00       | 0.00       | 0.00         | 0.02         | 0.00          | 0.00          | 0.00          | 0.05           | 0.00           |
|               | 0:10:00 | 0.00       | 0.00       | 0.00         | 0.26         | 0.00          | 0.00          | 0.02          | 0.27           | 0.08           |
|               | 0:15:00 | 0.00       | 0.00       | 0.22         | 4.18         | 0.45          | 0.30          | 0.37          | 3.29           | 0.52           |
|               | 0:20:00 | 0.00       | 0.00       | 0.79         | 18.56        | 2.61          | 0.77          | 0.98          | 16.80          | 2.53           |
|               | 0:25:00 | 0.00       | 0.00       | 4.46         | 25.92        | 15.35         | 4.29          | 5.35          | 40.82          | 15.05          |
|               | 0:30:00 | 0.00       | 0.00       | 8.26         | 26.63        | 21.95         | 25.39         | 32.12         | 52.64          | 53.58          |
|               | 0:35:00 | 0.00       | 0.00       | 8.30         | 25.54        | 20.68         | 32.77         | 40.35         | 54.68          | 67.92          |
|               | 0:40:00 | 0.00       | 0.00       | 7.36         | 24.02        | 18.10         | 32.91         | 40.08         | 53.45          | 66.58          |
|               | 0:45:00 | 0.00       | 0.00       | 6.15         | 22.77        | 15.80         | 29.61         | 36.06         | 50.98          | 61.89          |
|               | 0:50:00 | 0.00       | 0.00       | 5.18         | 21.33        | 13.47         | 27.01         | 32.92         | 47.85          | 56.39          |
|               | 0:55:00 | 0.00       | 0.00       | 4.37         | 19.93        | 11.38         | 23.07         | 28.30         | 44.90          | 50.07          |
|               | 1:00:00 | 0.00       | 0.00       | 3.63         | 18.66        | 9.55          | 19.40         | 23.96         | 42.22          | 44.24          |
|               | 1:05:00 | 0.00       | 0.00       | 3.09         | 17.72        | 8.40          | 16.26         | 20.24         | 37.98          | 39.36          |
|               | 1:10:00 | 0.00       | 0.00       | 2.60         | 16.73        | 7.64          | 13.48         | 16.97         | 34.23          | 32.88          |
|               | 1:15:00 | 0.00       | 0.00       | 2.18         | 15.62        | 6.97          | 11.29         | 14.34         | 30.38          | 27.54          |
|               | 1:20:00 | 0.00       | 0.00       | 1.81         | 14.58        | 5.89          | 9.31          | 11.82         | 26.90          | 22.25          |
|               | 1:25:00 | 0.00       | 0.00       | 1.45         | 13.70        | 4.70          | 7.53          | 9.55          | 23.90          | 17.62          |
|               | 1:30:00 | 0.00       | 0.00       | 1.11         | 12.91        | 3.60          | 5.82          | 7.39          | 21.31          | 13.49          |
|               | 1:35:00 | 0.00       | 0.00       | 0.80         | 11.76        | 2.62          | 4.19          | 5.34          | 19.01          | 9.72           |
|               | 1:40:00 | 0.00       | 0.00       | 0.58         | 10.63        | 2.04          | 2.73          | 3.53          | 16.90          | 6.62           |
|               | 1:45:00 | 0.00       | 0.00       | 0.49         | 9.74         | 1.74          | 1.93          | 2.57          | 15.06          | 4.83           |
|               | 1:50:00 | 0.00       | 0.00       | 0.44         | 9.07         | 1.53          | 1.45          | 1.97          | 13.62          | 3.68           |
|               | 1:55:00 | 0.00       | 0.00       | 0.38         | 8.43         | 1.35          | 1.16          | 1.59          | 12.53          | 2.88           |
|               | 2:00:00 | 0.00       | 0.00       | 0.33         | 7.13         | 1.12          | 0.95          | 1.33          | 10.52          | 2.30           |
|               | 2:05:00 | 0.00       | 0.00       | 0.25         | 5.87         | 0.86          | 0.71          | 0.99          | 8.61           | 1.62           |
|               | 2:10:00 | 0.00       | 0.00       | 0.19         | 4.80         | 0.64          | 0.51          | 0.71          | 6.98           | 1.08           |
|               | 2:15:00 | 0.00       | 0.00       | 0.14         | 3.88         | 0.47          | 0.36          | 0.51          | 5.58           | 0.73           |
|               | 2:20:00 | 0.00       | 0.00       | 0.11         | 3.11         | 0.34          | 0.27          | 0.37          | 4.39           | 0.53           |
|               | 2:25:00 | 0.00       | 0.00       | 0.08         | 2.50         | 0.24          | 0.20          | 0.27          | 3.43           | 0.39           |
|               | 2:30:00 | 0.00       | 0.00       | 0.06         | 2.01         | 0.17          | 0.14          | 0.20          | 2.70           | 0.29           |
|               | 2:35:00 | 0.00       | 0.00       | 0.05         | 1.61         | 0.13          | 0.10          | 0.14          | 2.14           | 0.21           |
|               | 2:40:00 | 0.00       | 0.00       | 0.03         | 1.29         | 0.09          | 0.08          | 0.11          | 1.70           | 0.16           |
|               | 2:45:00 | 0.00       | 0.00       | 0.02         | 1.02         | 0.06          | 0.06          | 0.08          | 1.34           | 0.11           |
|               | 2:50:00 | 0.00       | 0.00       | 0.01         | 0.79         | 0.04          | 0.04          | 0.05          | 1.03           | 0.08           |
|               | 2:55:00 | 0.00       | 0.00       | 0.01         | 0.61         | 0.02          | 0.02          | 0.03          | 0.79           | 0.05           |
|               | 3:00:00 | 0.00       | 0.00       | 0.00         | 0.46         | 0.01          | 0.01          | 0.02          | 0.59           | 0.02           |
|               | 3:05:00 | 0.00       | 0.00       | 0.00         | 0.34         | 0.00          | 0.00          | 0.01          | 0.44           | 0.01           |
|               | 3:10:00 | 0.00       | 0.00       | 0.00         | 0.25         | 0.00          | 0.00          | 0.00          | 0.32           | 0.00           |
|               | 3:15:00 | 0.00       | 0.00       | 0.00         | 0.18         | 0.00          | 0.00          | 0.00          | 0.23           | 0.00           |
|               | 3:20:00 | 0.00       | 0.00       | 0.00         | 0.13         | 0.00          | 0.00          | 0.00          | 0.17           | 0.00           |
|               | 3:25:00 | 0.00       | 0.00       | 0.00         | 0.09         | 0.00          | 0.00          | 0.00          | 0.12           | 0.00           |
|               | 3:30:00 | 0.00       | 0.00       | 0.00         | 0.06         | 0.00          | 0.00          | 0.00          | 0.09           | 0.00           |
|               | 3:35:00 | 0.00       | 0.00       | 0.00         | 0.04         | 0.00          | 0.00          | 0.00          | 0.06           | 0.00           |
|               | 3:40:00 | 0.00       | 0.00       | 0.00         | 0.02         | 0.00          | 0.00          | 0.00          | 0.03           | 0.00           |
|               | 3:45:00 | 0.00       | 0.00       | 0.00         | 0.01         | 0.00          | 0.00          | 0.00          | 0.02           | 0.00           |
|               | 3:50:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.01           | 0.00           |
|               | 3:55:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:05:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:10:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:15:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:20:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:25:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:30:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:35:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:40:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:45:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:50:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 4:55:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:05:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:10:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:15:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:20:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:25:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:30:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:35:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:40:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:45:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:50:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 5:55:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |
|               | 6:00:00 | 0.00       | 0.00       | 0.00         | 0.00         | 0.00          | 0.00          | 0.00          | 0.00           | 0.00           |

# DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-DETENTION, Version 4.04 (February 2021)

Project: Flying Horse North Drainage Plan

Basin ID: Pond 17



Example Zone Configuration (Retention Pond)

## Watershed Information

|   |            |         |
|---|------------|---------|
| Selected BMP Type =                     | EDB        |         |
| Watershed Area =                        | 23.50      | acres   |
| Watershed Length =                      | 1,050      | ft      |
| Watershed Length to Centroid =          | 540        | ft      |
| Watershed Slope =                       | 0.060      | ft/ft   |
| Watershed Imperviousness =              | 17.16%     | percent |
| Percentage Hydrologic Soil Group A =    | 0.0%       | percent |
| Percentage Hydrologic Soil Group B =    | 100.0%     | percent |
| Percentage Hydrologic Soil Groups C/D = | 0.0%       | percent |
| Target WQCV Drain Time =                | 40.0       | hours   |
| Location for 1-hr Rainfall Depths =     | User Input |         |

After providing required inputs above including 1-hour rainfall depths, click "Run CUHP" to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

|  |       |           |
|--|-------|-----------|
| Water Quality Capture Volume (WQCV) =  | 0.203 | acre-feet |
| Excess Urban Runoff Volume (EURV) =    | 0.396 | acre-feet |
| 2-yr Runoff Volume (P1 = 1.19 in.) =   | 0.447 | acre-feet |
| 5-yr Runoff Volume (P1 = 1.5 in.) =    | 0.851 | acre-feet |
| 10-yr Runoff Volume (P1 = 1.75 in.) =  | 1.240 | acre-feet |
| 25-yr Runoff Volume (P1 = 2 in.) =     | 1.888 | acre-feet |
| 50-yr Runoff Volume (P1 = 2.25 in.) =  | 2.346 | acre-feet |
| 100-yr Runoff Volume (P1 = 2.52 in.) = | 2.988 | acre-feet |
| 500-yr Runoff Volume (P1 = 3.14 in.) = | 4.182 | acre-feet |
| Approximate 2-yr Detention Volume =    | 0.267 | acre-feet |
| Approximate 5-yr Detention Volume =    | 0.401 | acre-feet |
| Approximate 10-yr Detention Volume =   | 0.679 | acre-feet |
| Approximate 25-yr Detention Volume =   | 0.863 | acre-feet |
| Approximate 50-yr Detention Volume =   | 0.911 | acre-feet |
| Approximate 100-yr Detention Volume =  | 1.134 | acre-feet |

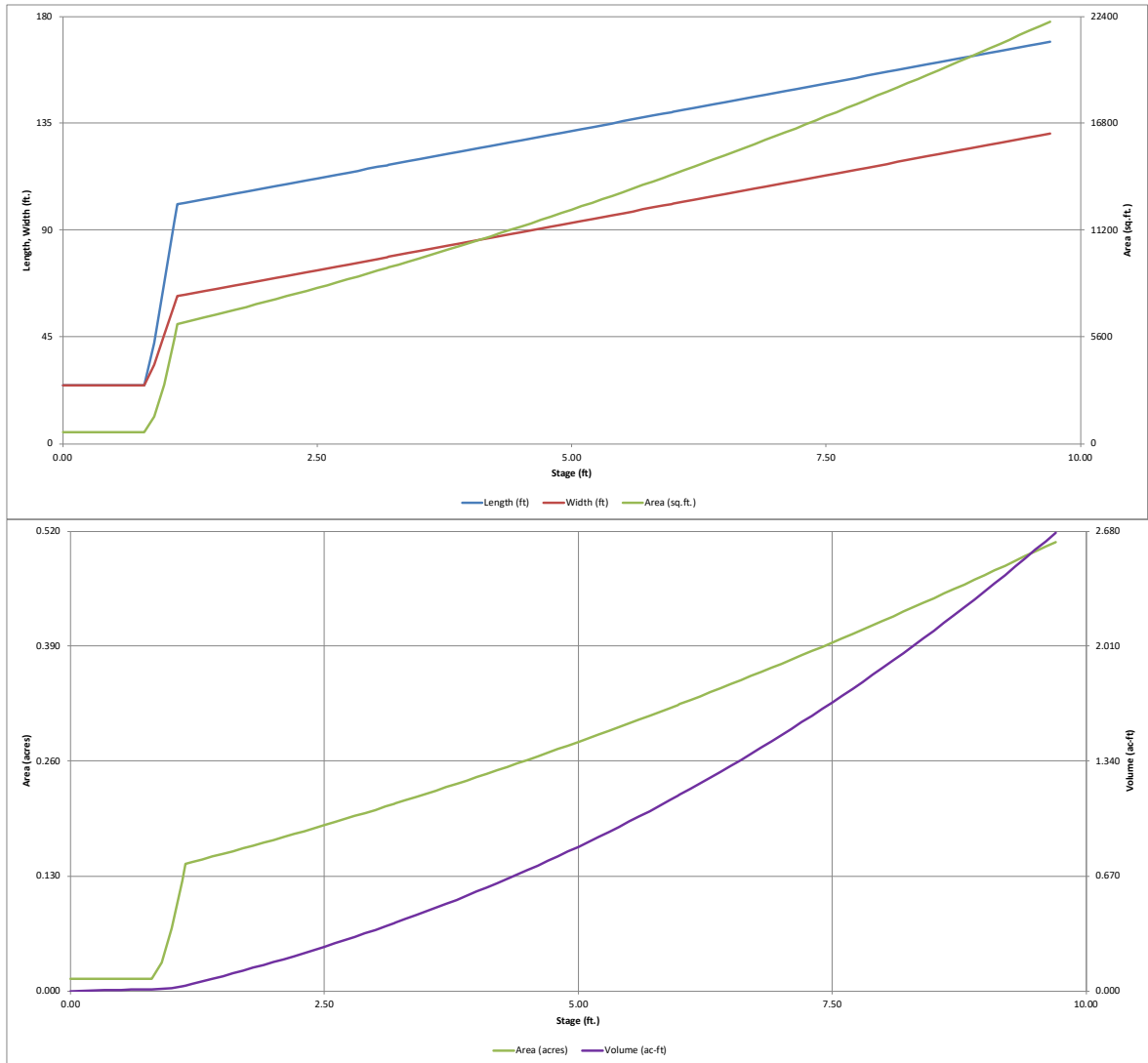
## Define Zones and Basin Geometry

|   |        |                 |
|---|--------|-----------------|
| Zone 1 Volume (WQCV) =                                  | 0.203  | acre-feet       |
| Zone 2 Volume (EURV - Zone 1) =                         | 0.193  | acre-feet       |
| Zone 3 Volume (100-year - Zones 1 & 2) =                | 0.739  | acre-feet       |
| Total Detention Basin Volume =                          | 1.134  | acre-feet       |
| Initial Surge Volume (ISV) =                            | 200    | ft <sup>3</sup> |
| Initial Surge Depth (ISD) =                             | 0.33   | ft              |
| Total Available Detention Depth (H <sub>total</sub> ) = | 6.00   | ft              |
| Depth of Trickle Channel (H <sub>TC</sub> ) =           | 0.50   | ft              |
| Slope of Trickle Channel (S <sub>TC</sub> ) =           | 4.00   | ft/ft           |
| Slopes of Main Basin Sides (S <sub>main</sub> ) =       | 4      | H:V             |
| Basin Length-to-Width Ratio (R <sub>L/W</sub> ) =       | 2      |                 |
| Initial Surge Area (A <sub>ISV</sub> ) =                | 606    | ft <sup>2</sup> |
| Surge Volume Length (L <sub>ISV</sub> ) =               | 24.6   | ft              |
| Surge Volume Width (W <sub>ISV</sub> ) =                | 24.6   | ft              |
| Depth of Basin Floor (H <sub>floor</sub> ) =            | 0.30   | ft              |
| Length of Basin Floor (L <sub>floor</sub> ) =           | 100.8  | ft              |
| Width of Basin Floor (W <sub>floor</sub> ) =            | 62.1   | ft              |
| Area of Basin Floor (A <sub>floor</sub> ) =             | 6,263  | ft <sup>2</sup> |
| Volume of Basin Floor (V <sub>floor</sub> ) =           | 882    | ft <sup>3</sup> |
| Depth of Main Basin (H <sub>main</sub> ) =              | 4.87   | ft              |
| Length of Main Basin (L <sub>main</sub> ) =             | 139.8  | ft              |
| Width of Main Basin (W <sub>main</sub> ) =              | 101.1  | ft              |
| Area of Main Basin (A <sub>main</sub> ) =               | 14,129 | ft <sup>2</sup> |
| Volume of Main Basin (V <sub>main</sub> ) =             | 48,372 | ft <sup>3</sup> |
| Calculated Total Basin Volume (V <sub>total</sub> ) =   | 1.142  | acre-feet       |

|                             |            |                              |             |            |                         |   |             |                           |                |
|-----------------------------|------------|------------------------------|-------------|------------|-------------------------|---|-------------|---------------------------|----------------|
| Depth Increment =           | 0.10       | ft                           |             |            |                         |   |             |                           |                |
| Stage - Storage Description | Stage (ft) | Optional Override Stage (ft) | Length (ft) | Width (ft) | Area (ft <sup>2</sup> ) | Optional Override Area (ft <sup>2</sup> ) | Area (acre) | Volume (ft <sup>3</sup> ) | Volume (ac-ft) |
| Top of Micropool            | 0.00       |                              | 24.6        | 24.6       | 606                     |   | 0.014       |                           |                |
| ISV                         | 0.33       |                              | 24.6        | 24.6       | 606                     |   | 0.014       | 200                       | 0.005          |
|                             | 0.40       |                              | 24.6        | 24.6       | 606                     |   | 0.014       | 242                       | 0.006          |
|                             | 0.50       |                              | 24.6        | 24.6       | 606                     |   | 0.014       | 303                       | 0.007          |
|                             | 0.60       |                              | 24.6        | 24.6       | 606                     |   | 0.014       | 364                       | 0.008          |
|                             | 0.70       |                              | 24.6        | 24.6       | 606                     |   | 0.014       | 424                       | 0.010          |
|                             | 0.80       |                              | 24.6        | 24.6       | 606                     |   | 0.014       | 485                       | 0.011          |
|                             | 0.90       |                              | 42.4        | 33.4       | 1,415                   |   | 0.032       | 572                       | 0.013          |
|                             | 1.00       |                              | 67.8        | 45.9       | 3,110                   |   | 0.071       | 793                       | 0.018          |
|                             | 1.10       |                              | 93.2        | 58.4       | 5,440                   |   | 0.125       | 1,215                     | 0.028          |
| Floor                       | 1.13       |                              | 100.8       | 62.1       | 6,263                   |   | 0.144       | 1,390                     | 0.032          |
|                             | 1.20       |                              | 101.4       | 62.7       | 6,354                   |   | 0.146       | 1,832                     | 0.042          |
|                             | 1.30       |                              | 102.2       | 63.5       | 6,486                   |   | 0.149       | 2,474                     | 0.057          |
|                             | 1.40       |                              | 103.0       | 64.3       | 6,619                   |   | 0.152       | 3,129                     | 0.072          |
|                             | 1.50       |                              | 103.8       | 65.1       | 6,754                   |   | 0.155       | 3,798                     | 0.087          |
|                             | 1.60       |                              | 104.6       | 65.9       | 6,889                   |   | 0.158       | 4,480                     | 0.103          |
|                             | 1.70       |                              | 105.4       | 66.7       | 7,026                   |   | 0.161       | 5,176                     | 0.119          |
|                             | 1.80       |                              | 106.2       | 67.5       | 7,165                   |   | 0.164       | 5,885                     | 0.135          |
|                             | 1.90       |                              | 107.0       | 68.3       | 7,304                   |   | 0.168       | 6,609                     | 0.152          |
|                             | 2.00       |                              | 107.8       | 69.1       | 7,445                   |   | 0.171       | 7,346                     | 0.169          |
|                             | 2.10       |                              | 108.6       | 69.9       | 7,587                   |   | 0.174       | 8,098                     | 0.186          |
| Zone 1 (WQCV)               | 2.20       |                              | 109.4       | 70.7       | 7,731                   |   | 0.177       | 8,864                     | 0.203          |
|                             | 2.30       |                              | 110.2       | 71.5       | 7,875                   |   | 0.181       | 9,644                     | 0.221          |
|                             | 2.40       |                              | 111.0       | 72.3       | 8,021                   |   | 0.184       | 10,439                    | 0.240          |
|                             | 2.50       |                              | 111.8       | 73.1       | 8,169                   |   | 0.188       | 11,248                    | 0.258          |
|                             | 2.60       |                              | 112.6       | 73.9       | 8,317                   |   | 0.191       | 12,073                    | 0.277          |
|                             | 2.70       |                              | 113.4       | 74.7       | 8,467                   |   | 0.194       | 12,912                    | 0.296          |
|                             | 2.80       |                              | 114.2       | 75.5       | 8,618                   |   | 0.198       | 13,766                    | 0.316          |
|                             | 2.90       |                              | 115.0       | 76.3       | 8,770                   |   | 0.201       | 14,636                    | 0.336          |
|                             | 3.00       |                              | 115.8       | 77.1       | 8,924                   |   | 0.205       | 15,520                    | 0.356          |
|                             | 3.10       |                              | 116.6       | 77.9       | 9,079                   |   | 0.208       | 16,420                    | 0.377          |
| Zone 2 (EURV)               | 3.19       |                              | 117.3       | 78.6       | 9,219                   |   | 0.212       | 17,244                    | 0.396          |
|                             | 3.20       |                              | 117.4       | 78.7       | 9,235                   |   | 0.212       | 17,336                    | 0.398          |
|                             | 3.30       |                              | 118.2       | 79.5       | 9,393                   |   | 0.216       | 18,267                    | 0.419          |
|                             | 3.40       |                              | 119.0       | 80.3       | 9,551                   |   | 0.219       | 19,215                    | 0.441          |
|                             | 3.50       |                              | 119.8       | 81.1       | 9,711                   |   | 0.223       | 20,178                    | 0.463          |
|                             | 3.60       |                              | 120.6       | 81.9       | 9,873                   |   | 0.227       | 21,157                    | 0.486          |
|                             | 3.70       |                              | 121.4       | 82.7       | 10,035                  |   | 0.230       | 22,152                    | 0.509          |
|                             | 3.80       |                              | 122.2       | 83.5       | 10,199                  |   | 0.234       | 23,164                    | 0.532          |
|                             | 3.90       |                              | 123.0       | 84.3       | 10,364                  |   | 0.238       | 24,192                    | 0.555          |
|                             | 4.00       |                              | 123.8       | 85.1       | 10,531                  |   | 0.242       | 25,237                    | 0.579          |
|                             | 4.10       |                              | 124.6       | 85.9       | 10,699                  |   | 0.246       | 26,298                    | 0.604          |
|                             | 4.20       |                              | 125.4       | 86.7       | 10,868                  |   | 0.249       | 27,377                    | 0.628          |
|                             | 4.30       |                              | 126.2       | 87.5       | 11,038                  |   | 0.253       | 28,472                    | 0.654          |
|                             | 4.40       |                              | 127.0       | 88.3       | 11,209                  |   | 0.257       | 29,584                    | 0.679          |
|                             | 4.50       |                              | 127.8       | 89.1       | 11,382                  |   | 0.261       | 30,714                    | 0.705          |
|                             | 4.60       |                              | 128.6       | 89.9       | 11,556                  |   | 0.265       | 31,861                    | 0.731          |
|                             | 4.70       |                              | 129.4       | 90.7       | 11,732                  |   | 0.269       | 33,025                    | 0.758          |
|                             | 4.80       |                              | 130.2       | 91.5       | 11,908                  |   | 0.273       | 34,207                    | 0.785          |
|                             | 4.90       |                              | 131.0       | 92.3       | 12,086                  |   | 0.277       | 35,407                    | 0.813          |
|                             | 5.00       |                              | 131.8       | 93.1       | 12,266                  |   | 0.282       | 36,625                    | 0.841          |
|                             | 5.10       |                              | 132.6       | 93.9       | 12,446                  |   | 0.286       | 37,860                    | 0.869          |
|                             | 5.20       |                              | 133.4       | 94.7       | 12,628                  |   | 0.290       | 39,114                    | 0.898          |
|                             | 5.30       |                              | 134.2       | 95.5       | 12,811                  |   | 0.294       | 40,386                    | 0.927          |
|                             | 5.40       |                              | 135.0       | 96.3       | 12,995                  |   | 0.298       | 41,676                    | 0.957          |
|                             | 5.50       |                              | 135.8       | 97.1       | 13,181                  |   | 0.303       | 42,985                    | 0.987          |
|                             | 5.60       |                              | 136.6       | 97.9       | 13,368                  |   | 0.307       | 44,312                    | 1.017          |
|                             | 5.70       |                              | 137.4       | 98.7       | 13,556                  |   | 0.311       | 45,659                    | 1.048          |
|                             | 5.80       |                              | 138.2       | 99.5       | 13,746                  |   | 0.316       | 47,024                    | 1.080          |
|                             | 5.90       |                              | 139.0       | 100.3      | 13,937                  |   | 0.320       | 48,408                    | 1.111          |
| Zone 3 (100-year)           | 5.98       |                              | 139.6       | 100.9      | 14,090                  |   | 0.323       | 49,529                    | 1.137          |
|                             | 6.00       |                              | 139.8       | 101.1      | 14,129                  |   | 0.324       | 49,811                    | 1.144          |
|                             | 6.10       |                              | 140.6       | 101.9      | 14,322                  |   | 0.329       | 51,234                    | 1.176          |
|                             | 6.20       |                              | 141.4       | 102.7      | 14,516                  |   | 0.333       | 52,675                    | 1.209          |
|                             | 6.30       |                              | 142.2       | 103.5      | 14,712                  |   | 0.338       | 54,137                    | 1.243          |
|                             | 6.40       |                              | 143.0       | 104.3      | 14,910                  |   | 0.342       | 55,618                    | 1.277          |
|                             | 6.50       |                              | 143.8       | 105.1      | 15,108                  |   | 0.347       | 57,119                    | 1.311          |
|                             | 6.60       |                              | 144.6       | 105.9      | 15,308                  |   | 0.351       | 58,640                    | 1.346          |
|                             | 6.70       |                              | 145.4       | 106.7      | 15,509                  |   | 0.356       | 60,180                    | 1.382          |
|                             | 6.80       |                              | 146.2       | 107.5      | 15,711                  |   | 0.361       | 61,741                    | 1.417          |
|                             | 6.90       |                              | 147.0       | 108.3      | 15,915                  |   | 0.365       | 63,323                    | 1.454          |
|                             | 7.00       |                              | 147.8       | 109.1      | 16,119                  |   | 0.370       | 64,924                    | 1.490          |
|                             | 7.10       |                              | 148.6       | 109.9      | 16,326                  |   | 0.375       | 66,547                    | 1.528          |
|                             | 7.20       |                              | 149.4       | 110.7      | 16,533                  |   | 0.380       | 68,190                    | 1.565          |
|                             | 7.30       |                              | 150.2       | 111.5      | 16,742                  |   | 0.384       | 69,853                    | 1.604          |
|                             | 7.40       |                              | 151.0       | 112.3      | 16,952                  |   | 0.389       | 71,538                    | 1.642          |
|                             | 7.50       |                              | 151.8       | 113.1      | 17,163                  |   | 0.394       | 73,244                    | 1.681          |
|                             | 7.60       |                              | 152.6       | 113.9      | 17,375                  |   | 0.399       | 74,970                    | 1.721          |
|                             | 7.70       |                              | 153.4       | 114.7      | 17,589                  |   | 0.404       | 76,719                    | 1.761          |
|                             | 7.80       |                              | 154.2       | 115.5      | 17,804                  |   | 0.409       | 78,488                    | 1.802          |
|                             | 7.90       |                              | 155.0       | 116.3      | 18,021                  |   | 0.414       | 80,280                    | 1.843          |
|                             | 8.00       |                              | 155.8       | 117.1      | 18,238                  |   | 0.419       | 82,093                    | 1.885          |
|                             | 8.10       |                              | 156.6       | 117.9      | 18,457                  |   | 0.424       | 83,927                    | 1.927          |
|                             | 8.20       |                              | 157.4       | 118.7      | 18,677                  |   | 0.429       | 85,784                    | 1.969          |
|                             | 8.30       |                              | 158.2       | 119.5      | 18,899                  |   | 0.434       | 87,663                    | 2.012          |
|                             | 8.40       |                              | 159.0       | 120.3      | 19,122                  |   | 0.439       | 89,564                    | 2.056          |
|                             | 8.50       |                              | 159.8       | 121.1      | 19,346                  |   | 0.444       | 91,487                    | 2.100          |
|                             | 8.60       |                              | 160.6       | 121.9      | 19,571                  |   | 0.449       | 93,433                    | 2.145          |
|                             | 8.70       |                              | 161.4       | 122.7      | 19,798                  |   | 0.454       | 95,401                    | 2.190          |
|                             | 8.80       |                              | 162.2       | 123.5      | 20,026                  |   | 0.460       | 97,393                    | 2.236          |
|                             | 8.90       |                              | 163.0       | 124.3      | 20,255                  |   | 0.465       | 99,407                    | 2.282          |
|                             | 9.00       |                              | 163.8       | 125.1      | 20,485                  |   | 0.470       | 101,444                   | 2.329          |
|                             | 9.10       |                              | 164.6       | 125.9      | 20,717                  |   | 0.476       | 103,504                   | 2.376          |
|                             | 9.20       |                              | 165.4       | 126.7      | 20,950                  |   | 0.481       | 105,587                   | 2.424          |
|                             | 9.30       |                              | 166.2       | 127.5      | 21,184                  |   | 0.486       | 107,694                   | 2.472          |
|                             | 9.40       |                              | 167.0       | 128.3      | 21,420                  |   | 0.492       | 109,824                   | 2.521          |
|                             | 9.50       |                              | 167.8       | 129.1      | 21,657                  |   | 0.497       | 111,978                   | 2.571          |
|                             | 9.60       |                              | 168.6       | 129.9      | 21,895                  |   | 0.503       | 114,155                   | 2.621          |
|                             | 9.70       |                              | 169.4       | 130.7      | 22,134                  |   | 0.508       | 116,357                   | 2.671          |

# DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.04 (February 2021)



## Appendix E

## Worksheet for Culvert 1

### Project Description

|                 |                 |
|-----------------|-----------------|
| Friction Method | Manning Formula |
| Solve For       | Normal Depth    |

### Input Data

|                       |         |                    |
|-----------------------|---------|--------------------|
| Roughness Coefficient | 0.013   |                    |
| Channel Slope         | 0.01000 | ft/ft              |
| Diameter              | 3.00    | ft                 |
| Discharge             | 58.65   | ft <sup>3</sup> /s |

### Results

|                   |               |                    |
|-------------------|---------------|--------------------|
| Normal Depth      | 2.18          | ft                 |
| Flow Area         | 5.51          | ft <sup>2</sup>    |
| Wetted Perimeter  | 6.13          | ft                 |
| Hydraulic Radius  | 0.90          | ft                 |
| Top Width         | 2.67          | ft                 |
| Critical Depth    | 2.48          | ft                 |
| Percent Full      | 72.8          | %                  |
| Critical Slope    | 0.00763       | ft/ft              |
| Velocity          | 10.65         | ft/s               |
| Velocity Head     | 1.76          | ft                 |
| Specific Energy   | 3.94          | ft                 |
| Froude Number     | 1.31          |                    |
| Maximum Discharge | 71.74         | ft <sup>3</sup> /s |
| Discharge Full    | 66.69         | ft <sup>3</sup> /s |
| Slope Full        | 0.00773       | ft/ft              |
| Flow Type         | SuperCritical |                    |

### GVF Input Data

|                  |      |    |
|------------------|------|----|
| Downstream Depth | 0.00 | ft |
| Length           | 0.00 | ft |
| Number Of Steps  | 0    |    |

### GVF Output Data

|                             |          |      |
|-----------------------------|----------|------|
| Upstream Depth              | 0.00     | ft   |
| Profile Description         |          |      |
| Profile Headloss            | 0.00     | ft   |
| Average End Depth Over Rise | 0.00     | %    |
| Normal Depth Over Rise      | 72.76    | %    |
| Downstream Velocity         | Infinity | ft/s |



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## Worksheet for Culvert 1

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### GVF Output Data

|                   |          |       |
|-------------------|----------|-------|
| Upstream Velocity | Infinity | ft/s  |
| Normal Depth      | 2.18     | ft    |
| Critical Depth    | 2.48     | ft    |
| Channel Slope     | 0.01000  | ft/ft |
| Critical Slope    | 0.00763  | ft/ft |

Cross Section for Culvert 1

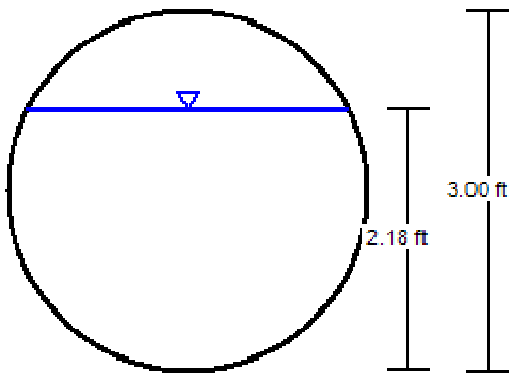
Project Description

Friction Method                      Manning Formula  
Solve For                                Normal Depth

Input Data

|                       |         |       |
|-----------------------|---------|-------|
| Roughness Coefficient | 0.013   |       |
| Channel Slope         | 0.01000 | ft/ft |
| Normal Depth          | 2.18    | ft    |
| Diameter              | 3.00    | ft    |
| Discharge             | 58.65   | ft³/s |

Cross Section Image



V: 1  
H: 1

## Worksheet for Culvert 2

### Project Description

|                 |                 |
|-----------------|-----------------|
| Friction Method | Manning Formula |
| Solve For       | Normal Depth    |

### Input Data

|                       |         |                    |
|-----------------------|---------|--------------------|
| Roughness Coefficient | 0.013   |                    |
| Channel Slope         | 0.02000 | ft/ft              |
| Diameter              | 3.50    | ft                 |
| Discharge             | 116.26  | ft <sup>3</sup> /s |

### Results

|                   |               |                    |
|-------------------|---------------|--------------------|
| Normal Depth      | 2.41          | ft                 |
| Flow Area         | 7.05          | ft <sup>2</sup>    |
| Wetted Perimeter  | 6.84          | ft                 |
| Hydraulic Radius  | 1.03          | ft                 |
| Top Width         | 3.25          | ft                 |
| Critical Depth    | 3.22          | ft                 |
| Percent Full      | 68.7          | %                  |
| Critical Slope    | 0.01159       | ft/ft              |
| Velocity          | 16.49         | ft/s               |
| Velocity Head     | 4.23          | ft                 |
| Specific Energy   | 6.63          | ft                 |
| Froude Number     | 1.97          |                    |
| Maximum Discharge | 153.05        | ft <sup>3</sup> /s |
| Discharge Full    | 142.28        | ft <sup>3</sup> /s |
| Slope Full        | 0.01335       | ft/ft              |
| Flow Type         | SuperCritical |                    |

### GVF Input Data

|                  |      |    |
|------------------|------|----|
| Downstream Depth | 0.00 | ft |
| Length           | 0.00 | ft |
| Number Of Steps  | 0    |    |

### GVF Output Data

|                             |          |      |
|-----------------------------|----------|------|
| Upstream Depth              | 0.00     | ft   |
| Profile Description         |          |      |
| Profile Headloss            | 0.00     | ft   |
| Average End Depth Over Rise | 0.00     | %    |
| Normal Depth Over Rise      | 68.73    | %    |
| Downstream Velocity         | Infinity | ft/s |

---

## Worksheet for Culvert 2

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### GVF Output Data

|                   |          |       |
|-------------------|----------|-------|
| Upstream Velocity | Infinity | ft/s  |
| Normal Depth      | 2.41     | ft    |
| Critical Depth    | 3.22     | ft    |
| Channel Slope     | 0.02000  | ft/ft |
| Critical Slope    | 0.01159  | ft/ft |

Cross Section for Culvert 2

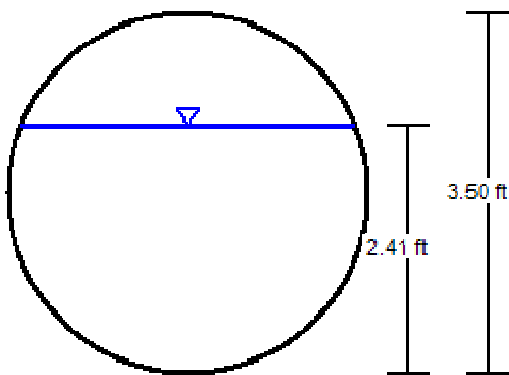
Project Description

Friction Method                      Manning Formula  
Solve For                                Normal Depth

Input Data

|                       |         |       |
|-----------------------|---------|-------|
| Roughness Coefficient | 0.013   |       |
| Channel Slope         | 0.02000 | ft/ft |
| Normal Depth          | 2.41    | ft    |
| Diameter              | 3.50    | ft    |
| Discharge             | 116.26  | ft³/s |

Cross Section Image



V: 1  
H: 1

## Appendix F

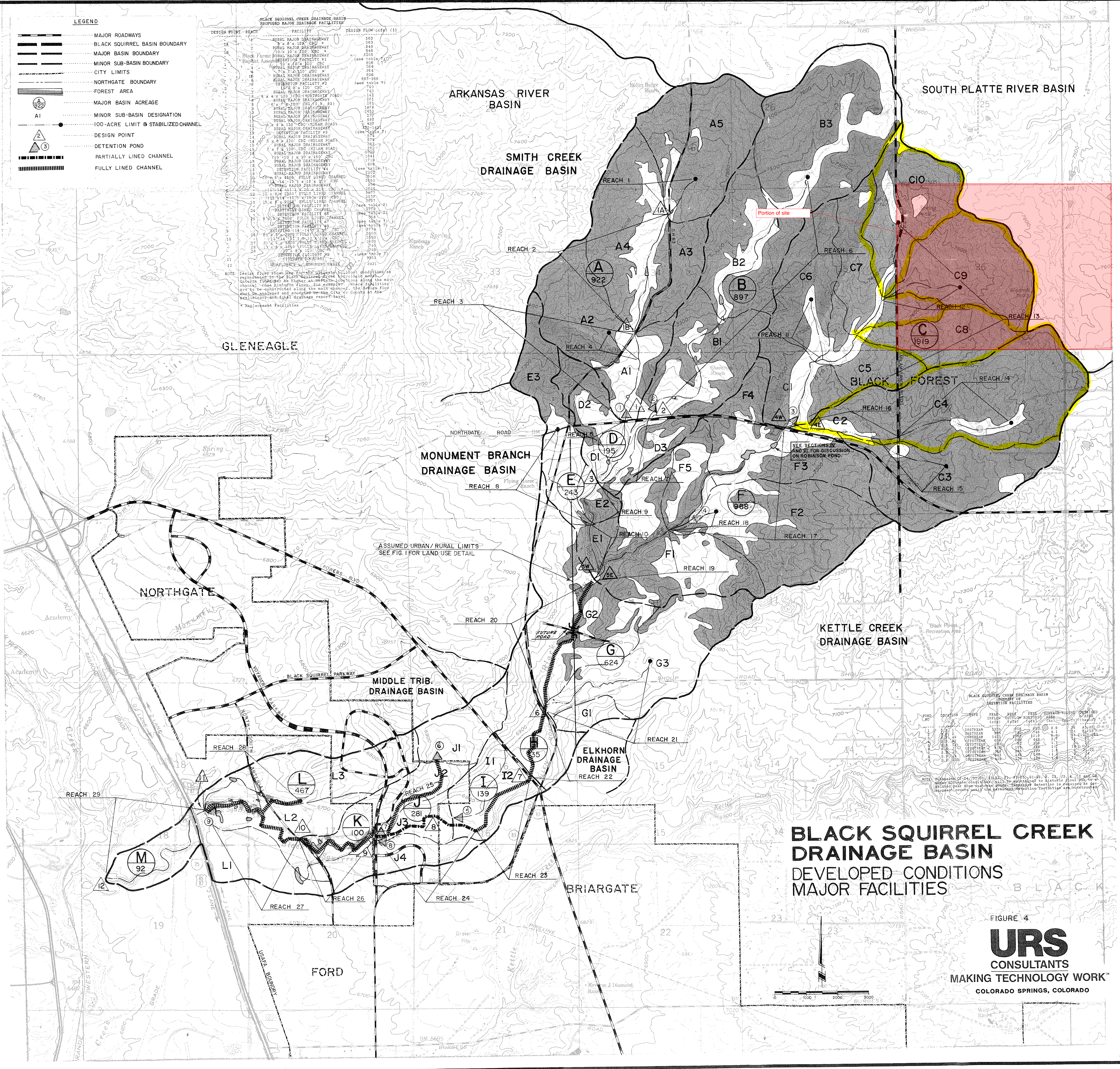


**LEGEND**

- MAJOR ROADWAYS
- BLACK SQUIRREL BASIN BOUNDARY
- MAJOR BASIN BOUNDARY
- MINOR SUB-BASIN BOUNDARY
- CITY LIMITS
- NORTHGATE BOUNDARY
- FOREST AREA
- MAJOR BASIN ACREAGE
- MINOR SUB-BASIN DESIGNATION
- 100-ACRE LIMIT & STABILIZED CHANNEL
- DESIGN POINT
- DETENTION POND
- PARTIALLY LINED CHANNEL
- FULLY LINED CHANNEL

**BLACK SQUIRREL CREEK DRAINAGE BASIN  
DEVELOPED MAJOR DRAINAGE FACILITIES**

| DESIGN POINT - REACH | FACILITY                | DESIGN FLOW (cfs) (1) |
|----------------------|-------------------------|-----------------------|
| 1A                   | RURAL MAJOR DRAINAGEWAY | 850                   |
| 2                    | RURAL MAJOR DRAINAGEWAY | 850                   |
| 3                    | RURAL MAJOR DRAINAGEWAY | 850                   |
| 4                    | RURAL MAJOR DRAINAGEWAY | 850                   |
| 5                    | RURAL MAJOR DRAINAGEWAY | 850                   |
| 6                    | RURAL MAJOR DRAINAGEWAY | 850                   |
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| 14                   | RURAL MAJOR DRAINAGEWAY | 850                   |
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| 18                   | RURAL MAJOR DRAINAGEWAY | 850                   |
| 19                   | RURAL MAJOR DRAINAGEWAY | 850                   |
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| 99                   | RURAL MAJOR DRAINAGEWAY | 850                   |
| 100                  | RURAL MAJOR DRAINAGEWAY | 850                   |



# **BLACK SQUIRREL CREEK DRAINAGE BASIN DEVELOPED CONDITIONS MAJOR FACILITIES**

FIGURE 4

**URS**  
CONSULTANTS  
MAKING TECHNOLOGY WORK™  
COLORADO SPRINGS, COLORADO





INNOVATIVE DESIGN. **CLASSIC RESULTS.**

**PRELIMINARY DRAINAGE REPORT  
FOR  
FLYING HORSE NORTH PRELIMINARY PLAN  
AND  
FINAL DRAINAGE REPORT  
FOR  
FLYING HORSE NORTH FILING NO. 1**

**NOVEMBER 2017**  
**Revised June 2018**

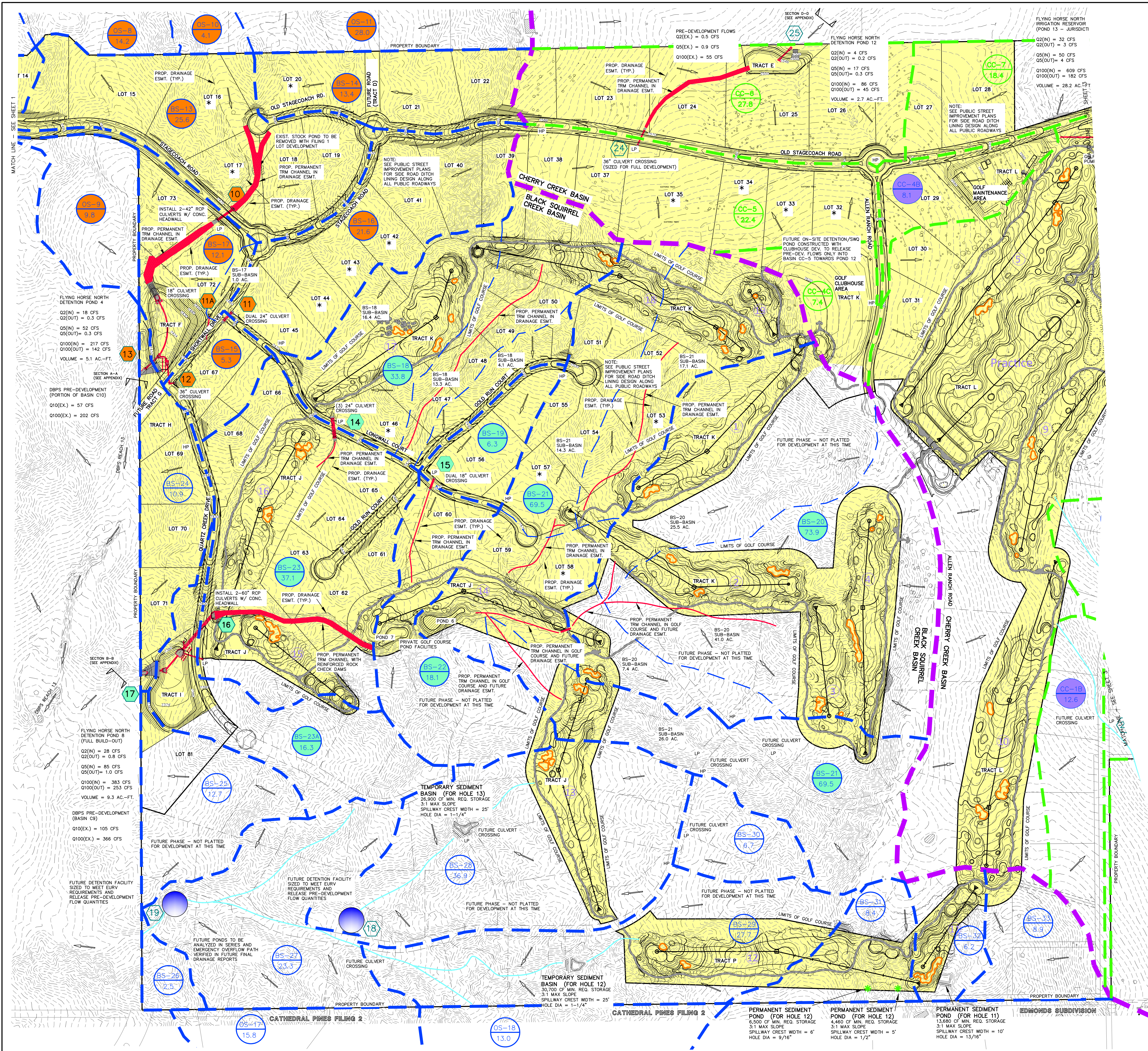
Prepared for:  
**PRI #2 LLC**  
6385 CORPORATE DRIVE SUITE 200  
COLORADO SPRINGS CO 80919  
(719) 592-9333

Prepared by:  
**CLASSIC CONSULTING ENGINEERS &  
SURVEYORS**  
619 N. CASCADE AVE SUITE 200  
COLORADO SPRINGS CO 80903  
(719) 785-0790

Job no. 1096.11  
PCD File No. SP-17-012 and SF-18-001







| BASIN SUMMARY - DEVELOPED CONDITIONS |              |              |                        |               |               |                 |               |               |                 |
|--------------------------------------|--------------|--------------|------------------------|---------------|---------------|-----------------|---------------|---------------|-----------------|
| BASIN (label)                        | AREA (acres) | COMPOSITE CN | TOTAL LAG TIME (hours) | Q 2 Yr. (cfs) | Q 5 Yr. (cfs) | Q 100 Yr. (cfs) | Q 2 Yr. (cfs) | Q 5 Yr. (cfs) | Q 100 Yr. (cfs) |
| OS-8                                 | 14.20        | 65.0         | 0.27                   | 2.1           | 6.2           | 24.7            |               |               |                 |
| OS-9                                 | 9.80         | 60.0         | 0.37                   | 0.1           | 1.0           | 9.1             |               |               |                 |
| OS-10                                | 4.10         | 65.0         | 0.17                   | 0.7           | 2.1           | 8.2             |               |               |                 |
| OS-11                                | 28.00        | 65.0         | 0.35                   | 2.4           | 8.2           | 38.7            |               |               |                 |
| OS-12                                | 68.10        | 62.7         | 0.37                   | 2.2           | 11.9          | 75.8            |               |               |                 |
| OS-13                                | 38.90        | 63.0         | 0.33                   | 1.4           | 7.4           | 45.0            |               |               |                 |
| OS-14                                | 28.40        | 62.0         | 0.31                   | 0.7           | 4.6           | 31.0            |               |               |                 |
| OS-15                                | 70.80        | 63.9         | 0.38                   | 3.3           | 14.8          | 84.2            |               |               |                 |
| OS-16                                | 4.50         | 65.0         | 0.24                   | 0.4           | 1.5           | 7.2             |               |               |                 |
| OS-17                                | 15.80        | 65.0         | 0.19                   | 1.6           | 5.9           | 27.7            |               |               |                 |
| OS-18                                | 13.00        | 65.0         | 0.20                   | 1.3           | 4.7           | 22.6            |               |               |                 |
| BS-13                                | 25.60        | 65.0         | 0.23                   | 3.7           | 10.2          | 40.7            |               |               |                 |
| BS-14                                | 13.40        | 65.0         | 0.23                   | 2.6           | 6.8           | 26.5            |               |               |                 |
| BS-15                                | 5.30         | 65.0         | 0.16                   | 1.6           | 3.7           | 12.2            |               |               |                 |
| BS-16                                | 21.50        | 65.0         | 0.34                   | 4.6           | 11.8          | 44.1            |               |               |                 |
| BS-17                                | 12.10        | 65.0         | 0.21                   | 3.1           | 7.7           | 26.7            |               |               |                 |
| BS-18                                | 33.80        | 63.6         | 0.41                   | 3.5           | 12.4          | 56.0            |               |               |                 |
| BS-19                                | 6.30         | 65.0         | 0.18                   | 2.1           | 4.6           | 15.0            |               |               |                 |
| BS-20                                | 73.90        | 63.4         | 0.31                   | 7.4           | 24.6          | 112.4           |               |               |                 |
| BS-21                                | 69.50        | 64.3         | 0.35                   | 7.8           | 23.9          | 103.0           |               |               |                 |
| BS-22                                | 18.10        | 64.4         | 0.22                   | 3.7           | 9.6           | 36.5            |               |               |                 |
| BS-23                                | 37.10        | 63.3         | 0.33                   | 4.5           | 13.6          | 58.2            |               |               |                 |
| BS-24                                | 16.30        | 64.4         | 0.29                   | 5.5           | 12.0          | 36.3            |               |               |                 |
| BS-25                                | 10.90        | 63.0         | 0.17                   | 0.6           | 3.3           | 17.6            |               |               |                 |
| EX-24 (Pre-Dev)                      | 13.20        | 60.0         | 0.17                   | 0.2           | 2.2           | 17.8            |               |               |                 |
| BS-25                                | 12.70        | 63.0         | 0.23                   | 0.4           | 2.7           | 17.3            |               |               |                 |
| BS-26                                | 2.90         | 60.0         | 0.18                   | 0.0           | 0.4           | 3.4             |               |               |                 |
| BS-27                                | 23.30        | 65.0         | 0.27                   | 2.1           | 8.0           | 38.8            |               |               |                 |
| BS-28                                | 36.90        | 64.4         | 0.32                   | 2.2           | 9.3           | 49.4            |               |               |                 |
| BS-29                                | 27.70        | 64.0         | 0.33                   | 1.4           | 6.5           | 35.9            |               |               |                 |
| BS-30                                | 6.70         | 65.0         | 0.20                   | 0.7           | 2.4           | 11.7            |               |               |                 |
| BS-31                                | 8.40         | 63.5         | 0.23                   | 0.3           | 1.9           | 11.8            |               |               |                 |
| BS-32                                | 6.20         | 62.6         | 0.20                   | 0.3           | 1.6           | 9.4             |               |               |                 |
| BS-33                                | 8.90         | 64.7         | 0.19                   | 0.8           | 3.2           | 15.3            |               |               |                 |
| CC-1A                                | 9.80         | 65.0         | 0.23                   | 0.8           | 3.3           | 16.0            |               |               |                 |
| CC-1B                                | 12.60        | 64.8         | 0.25                   | 1.0           | 4.0           | 19.4            |               |               |                 |
| CC-2A                                | 11.00        | 65.0         | 0.22                   | 1.0           | 3.8           | 18.3            |               |               |                 |
| CC-2B                                | 20.80        | 65.0         | 0.22                   | 1.9           | 7.1           | 34.6            |               |               |                 |
| CC-2C                                | 6.40         | 65.0         | 0.18                   | 0.7           | 2.5           | 11.5            |               |               |                 |
| CC-3                                 | 52.50        | 63.1         | 0.43                   | 1.8           | 8.8           | 54.5            |               |               |                 |
| CC-4A                                | 108.70       | 62.6         | 0.44                   | 15.4          | 39.0          | 156.0           |               |               |                 |
| CC-4B                                | 8.10         | 76.1         | 0.26                   | 4.0           | 7.3           | 20.6            |               |               |                 |
| CC-4C (Pre-Dev)                      | 7.40         | 61.0         | 0.13                   | 0.2           | 1.8           | 11.2            |               |               |                 |
| CC-5                                 | 22.40        | 65.0         | 0.26                   | 1.8           | 7.1           | 34.3            |               |               |                 |
| CC-6                                 | 27.80        | 65.0         | 0.25                   | 2.3           | 9.1           | 43.2            |               |               |                 |
| CC-7                                 | 18.40        | 65.0         | 0.29                   | 1.4           | 5.4           | 27.0            |               |               |                 |

DESIGN POINTS SURFACE ROUTING SUMMARY - DEVELOPED CONDITIONS

| Design Point (label)  | Contributing Basins                       | Q 2 Yr. (cfs) | Q 5 Yr. (cfs) | Q 100 Yr. (cfs) |
|---|---|---------------|---------------|-----------------|
| DP-10 DEV   | OS-8, OS-10, OS-11, BS-13, BS-14          | 10.7          | 32.0          | 143             |
| DP-11 DEV   | BS-16                                     | 4.6           | 11.8          | 36              |
| DP-12 DEV   | DP-11, 1.0 AC. Portion of BS-17 and BS-15 | 4.2           | 11.8          | 46              |
| TOTAL INFLOW TO POND 4 (UD Detention hydrograph)                      | DP-10, DP-12, BS-17, OS-9                 | 10            | 16            | 217             |
| DP-13 DEV   | Release from FHN Pond 4                   | 0.3           | 0.3           | 142             |
| DP-14 DEV   | BS-18                                     | 3.5           | 12.4          | 56              |
| DP-15 DEV   | BS-19                                     | 2.1           | 4.6           | 15              |
| DP-16 DEV   | DP-14, DP-15, BS-20, BS-21, BS-22, BS-23  | 25.0          | 78.0          | 362             |
| TOTAL INFLOW TO FHN POND 8 (Full Build-out) (UD Detention hydrograph) | DP-10, DP-12, BS-17, OS-9                 | 24            | 37            | 390             |
| DP-17 DEV (Full Build-out)  | Release from FHN Pond 8                   | 0.8           | 1.0           | 253             |
| TOTAL INFLOW TO FHN POND 8 (Filing 1 Only) (UD Detention hydrograph)  | DP-10, DP-12, BS-17, OS-9                 | 9             | 14            | 301             |
| DP-17 DEV (Filing 1 Only)   | Release from FHN Pond 8                   | 0.4           | 0.5           | 219             |
| DP-18 DEV   | BS-28, BS-29, BS-30, OS-18                | 5.0           | 21.6          | 115             |
| DP-19 DEV   | BS-27, OS-17, Release from DP-18          | 3.8           | 16.8          | 126             |
| DP-20 DEV   | CC-1A, OS-12                              | 3.2           | 14.3          | 88              |
| DP-21 DEV   | CC-2A, OS-13                              | 2.1           | 10.5          | 62              |
| DP-22 DEV   | CC-2B, Release from DP-21                 | 3.7           | 16.6          | 92              |
| DP-23 DEV   | CC-3, OS-14                               | 2.5           | 13.0          | 84              |
| DP-24 DEV   | CC-4C (Pre-Dev), CC-5                     | 1.9           | 8.4           | 45              |
| TOTAL INFLOW TO POND 12 (UD Detention hydrograph)                     | CC-4C, CC-5, CC-6                         | 6             | 9             | 85              |
| DP-25 DEV   | Release from FHN Pond 12                  | 0.2           | 0.3           | 45              |

**LEGEND**

| DESCRIPTION                         | SYMBOL  |
|-------------------------------------|---------|
| EXISTING GROUND CONTOUR             | 6910    |
| PROPOSED FINISHED CONTOUR           | 6910    |
| BASIN BOUNDARY EAST CHERRY CREEK    | ---     |
| MAJOR BASIN BOUNDARY                | ---     |
| BASIN BOUNDARY BLACK SQUIRREL       | ---     |
| DESIGN POINT                        | 3       |
| LOTS WITH NON-STANDARD CULVERT SIZE | *       |
| BASIN IDENTIFIER                    | BB 10.0 |
| EXISTING DIRECTION OF FLOW          | →       |
| PROPOSED DIRECTION OF FLOW          | →       |
| STORM SEWER                         | ---     |
| FILING NO. 1 PLAT AREA              | ---     |

200 100 0 200 400

SCALE: 1" = 200'

**CLASSIC CONSULTING ENGINEERS & SURVEYORS**

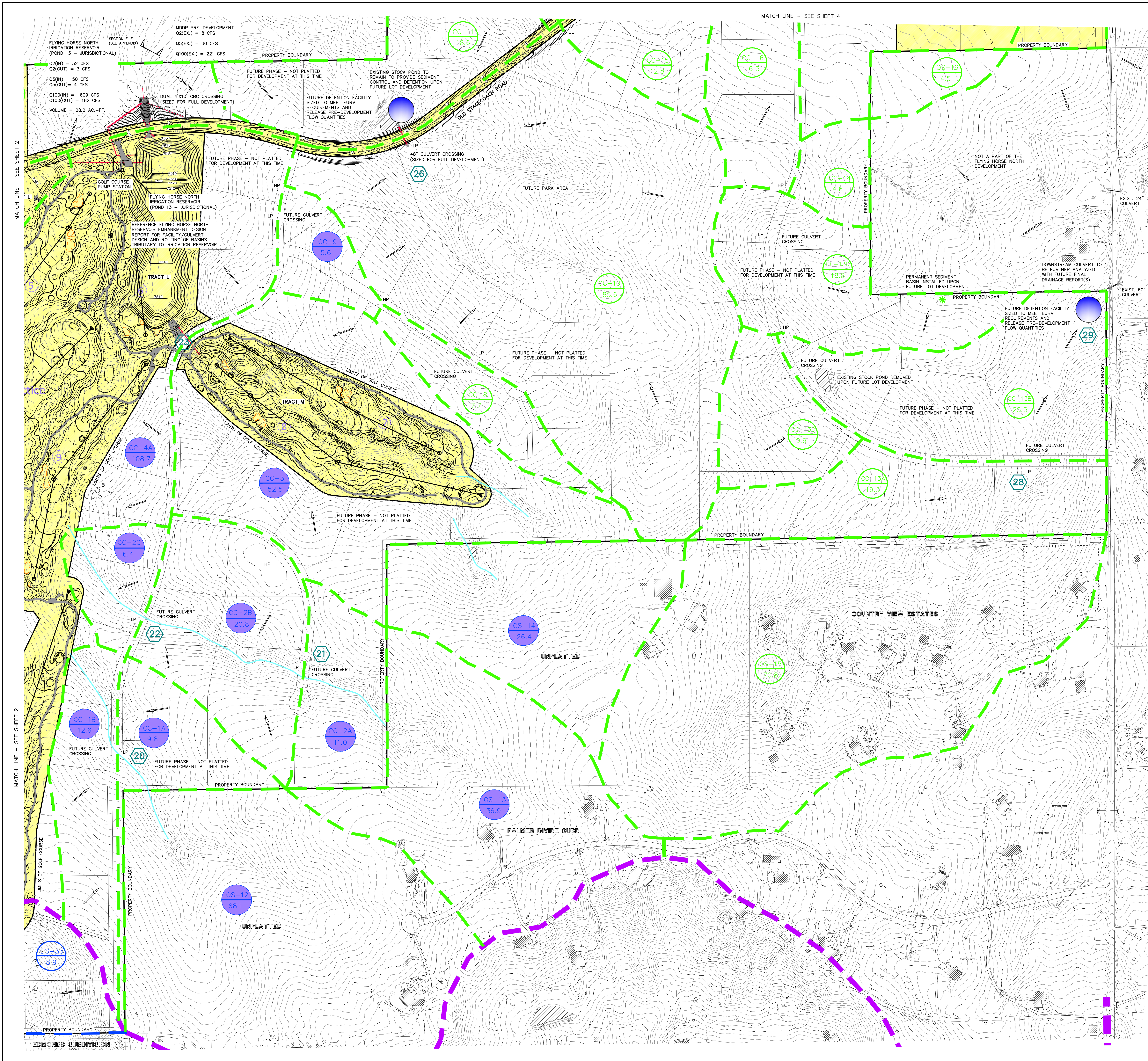
619 N. Cascade Avenue, Suite 200  
Colorado Springs, Colorado 80903

(719)785-0790  
(719)785-0799 (Fax)

FLYING HORSE NORTH  
PRELIMINARY/FINAL DRAINAGE REPORT  
FILING NO. 1 DRAINAGE MAP

|             |              |               |          |
|-------------|--------------|---------------|----------|
| DESIGNED BY | MAW          | SCALE         | DATE     |
| DRAWN BY    | MAW          | (H) 1" = 200' | 10-25-17 |
| CHECKED BY  | (V) 1" = N/A | SHEET 2 OF 4  |          |
| JOE NO.     | 1096.11      |               |          |





| BASIN SUMMARY - DEVELOPED CONDITIONS |              |              |                        |               |               |                 |                 |
|--------------------------------------|--------------|--------------|------------------------|---------------|---------------|-----------------|-----------------|
| BASIN (label)                        | AREA (acres) | COMPOSITE CN | TOTAL LAG TIME (hours) | Q 2 Yr. (cfs) | Q 5 Yr. (cfs) | Q 100 Yr. (cfs) | Q 100 Yr. (cfs) |
| OS-8                                 | 14.20        | 65.0         | 0.27                   | 2.1           | 6.2           | 24.7            |                 |
| OS-9                                 | 9.80         | 60.0         | 0.37                   | 0.1           | 1.0           | 9.1             |                 |
| OS-10                                | 4.10         | 65.0         | 0.17                   | 0.7           | 2.1           | 8.2             |                 |
| OS-11                                | 28.00        | 65.0         | 0.35                   | 2.4           | 8.2           | 38.7            |                 |
| OS-12                                | 68.10        | 62.7         | 0.37                   | 2.2           | 11.9          | 75.8            |                 |
| OS-13                                | 36.90        | 63.0         | 0.33                   | 1.4           | 7.4           | 45.0            |                 |
| OS-14                                | 26.40        | 62.0         | 0.31                   | 0.7           | 4.6           | 31.0            |                 |
| OS-15                                | 70.80        | 63.9         | 0.38                   | 3.3           | 14.8          | 84.2            |                 |
| OS-16                                | 4.50         | 65.0         | 0.24                   | 0.4           | 1.5           | 7.2             |                 |
| OS-17                                | 15.80        | 65.0         | 0.19                   | 1.6           | 5.9           | 27.7            |                 |
| OS-18                                | 13.00        | 65.0         | 0.20                   | 1.3           | 4.7           | 22.6            |                 |
|                                      |              |              |                        |               |               |                 |                 |
| CC-1A                                | 9.80         | 65.0         | 0.23                   | 0.8           | 3.3           | 16.0            |                 |
| CC-1B                                | 12.60        | 64.8         | 0.25                   | 1.0           | 4.0           | 19.4            |                 |
| CC-2A                                | 11.00        | 65.0         | 0.22                   | 1.0           | 3.8           | 18.3            |                 |
| CC-2B                                | 20.80        | 65.0         | 0.22                   | 1.9           | 7.1           | 34.6            |                 |
| CC-3C                                | 6.40         | 65.0         | 0.18                   | 0.7           | 2.5           | 11.5            |                 |
| CC-3                                 | 52.50        | 63.1         | 0.43                   | 1.8           | 8.8           | 54.5            |                 |
| CC-4A                                | 108.70       | 62.6         | 0.44                   | 15.4          | 39.0          | 156.0           |                 |
| CC-4B                                | 8.10         | 76.1         | 0.26                   | 4.0           | 7.3           | 20.6            |                 |
| CC-4C (Pre-Dev)                      | 7.40         | 61.0         | 0.13                   | 0.2           | 1.8           | 11.2            |                 |
| CC-5                                 | 22.40        | 65.0         | 0.26                   | 1.8           | 7.1           | 34.3            |                 |
| CC-6                                 | 27.80        | 65.0         | 0.25                   | 2.3           | 9.1           | 43.2            |                 |
| CC-7                                 | 18.40        | 65.0         | 0.29                   | 1.4           | 5.4           | 27.0            |                 |
| CC-8                                 | 7.70         | 65.0         | 0.25                   | 0.4           | 1.5           | 7.2             |                 |
| CC-9                                 | 5.60         | 65.0         | 0.19                   | 0.6           | 2.1           | 9.8             |                 |
| CC-10                                | 85.60        | 62.6         | 0.39                   | 2.6           | 14.1          | 91.9            |                 |
| CC-11                                | 18.60        | 63.1         | 0.21                   | 0.9           | 5.0           | 28.1            |                 |
| CC-12                                | 12.20        | 65.0         | 0.26                   | 1.0           | 3.9           | 18.7            |                 |
| CC-13A                               | 19.30        | 65.0         | 0.31                   | 1.4           | 5.4           | 27.3            |                 |
| CC-13B                               | 25.50        | 65.0         | 0.31                   | 1.8           | 7.2           | 36.1            |                 |
| CC-13C                               | 9.90         | 65.0         | 0.22                   | 0.9           | 3.4           | 16.5            |                 |
| CC-13D                               | 18.80        | 65.0         | 0.25                   | 1.5           | 6.2           | 29.2            |                 |
| CC-14                                | 4.60         | 65.0         | 0.21                   | 0.4           | 1.6           | 7.5             |                 |
| CC-15                                | 12.80        | 65.0         | 0.24                   | 1.1           | 4.3           | 20.4            |                 |
| CC-16                                | 16.30        | 65.0         | 0.30                   | 1.2           | 4.6           | 23.6            |                 |
| CC-17                                | 23.00        | 65.0         | 0.35                   | 1.7           | 6.5           | 32.8            |                 |
| CC-18                                | 6.20         | 66.5         | 0.30                   | 0.7           | 2.2           | 9.7             |                 |
| CC-19                                | 3.70         | 65.0         | 0.25                   | 0.3           | 1.2           | 5.8             |                 |
| CC-20                                | 39.30        | 65.0         | 0.25                   | 3.2           | 12.9          | 61.0            |                 |
| CC-21                                | 6.20         | 61.0         | 0.20                   | 0.1           | 1.2           | 8.5             |                 |
| CC-22                                | 13.80        | 65.0         | 0.25                   | 1.1           | 4.5           | 21.4            |                 |
| CC-23                                | 5.70         | 64.7         | 0.33                   | 0.4           | 1.5           | 7.7             |                 |
| CC-24                                | 39.60        | 65.0         | 0.25                   | 3.3           | 13.0          | 61.5            |                 |
| CC-25                                | 3.50         | 65.0         | 0.23                   | 0.3           | 1.2           | 5.7             |                 |
| CC-26                                | 10.70        | 65.0         | 0.26                   | 1.4           | 5.3           | 26.6            |                 |
| CC-27                                | 18.90        | 64.4         | 0.31                   | 1.2           | 4.9           | 25.8            |                 |
| CC-28                                | 154.80       | 64.4         | 0.63                   | 6.5           | 24.7          | 136.3           |                 |

DESIGN POINTS SURFACE ROUTING SUMMARY - DEVELOPED CONDITIONS

| Design Point (label)                              | Contributing Basins                                | Q 2 Yr. Q (cfs) | Q 5 Yr. Q (cfs) | Q 100 Yr. Q (cfs) |
|---|--|-----------------|-----------------|-------------------|
| DP-20 DEV   | CC-1A, OS-12                                       | 3.2             | 14.3            | 88                |
| DP-21 DEV   | CC-2A, OS-13                                       | 2.1             | 10.5            | 62                |
| DP-22 DEV   | CC-2B, Release from DP-21                          | 3.7             | 16.6            | 92                |
| DP-23 DEV   | CC-3, OS-14  | 2.5             | 13.0            | 84                |
| DP-24 DEV   | CC-4C (Pre-Dev), CC-5                              | 1.9             | 8.4             | 45                |
| TOTAL INFLOW TO POND 12 (UD Detention hydrograph) | CC-4C, CC-5, CC-6                                  | 6               | 9               | 85                |
| DP-25 DEV   | Release from FHN Pond 12                           | 0.2             | 0.3             | 45                |
| DP-26 DEV   | CC-8, CC-10  | 3.0             | 15.9            | 102               |
| DP-27 DEV   | CC-15, CC-20                                       | 4.3             | 17.2            | 81                |
| DP-28 DEV   | CC-13A, OS-15                                      | 4.6             | 19.8            | 110               |
| DP-29 DEV   | CC-13B, CC-13C, Release from DP-28                 | 5.8             | 26.6            | 155               |
| DP-30 DEV   | CC-18  | 0.7             | 2.2             | 10                |
| DP-31 DEV   | CC-19, Release from DP-30                          | 0.9             | 3.2             | 15                |
| DP-32 DEV   | CC-17, OS-16                                       | 2.0             | 7.8             | 40                |
| DP-33 DEV   | CC-23, CC-24                                       | 3.6             | 14.4            | 69                |
| DP-34 DEV   | CC-26, CC-27, CC-28 and Release from CC-16 & DP-32 | 6.0             | 23.5            | 168               |

LEGEND

DESCRIPTION

SYMBOL

EXISTING GROUND CONTOUR

6910

PROPOSED FINISHED CONTOUR

6910

BASIN BOUNDARY EAST CHERRY CREEK

MAJOR BASIN BOUNDARY

DESIGN POINT

3

BASIN IDENTIFIER

BB

AREA IN ACRES

10.0

EXISTING DIRECTION OF FLOW

PROPOSED DIRECTION OF FLOW

STORM SEWER

FILING NO. 1 PLAT AREA

SCALE: 1" = 200'

200 100 0 200 400

CLASSIC CONSULTING ENGINEERS & SURVEYORS

619 N. Cascade Avenue, Suite 200  
Colorado Springs, Colorado 80903

FLYING HORSE NORTH PRELIMINARY/FINAL DRAINAGE REPORT

FILING NO. 1 AND PRELIMINARY PLAN DRAINAGE MAP

DESIGNED BY

MAW

SCALE

(H) 1" = 200'

DATE

10-25-17

DRAWN BY

MAW

CHECKED BY

(V) N/A

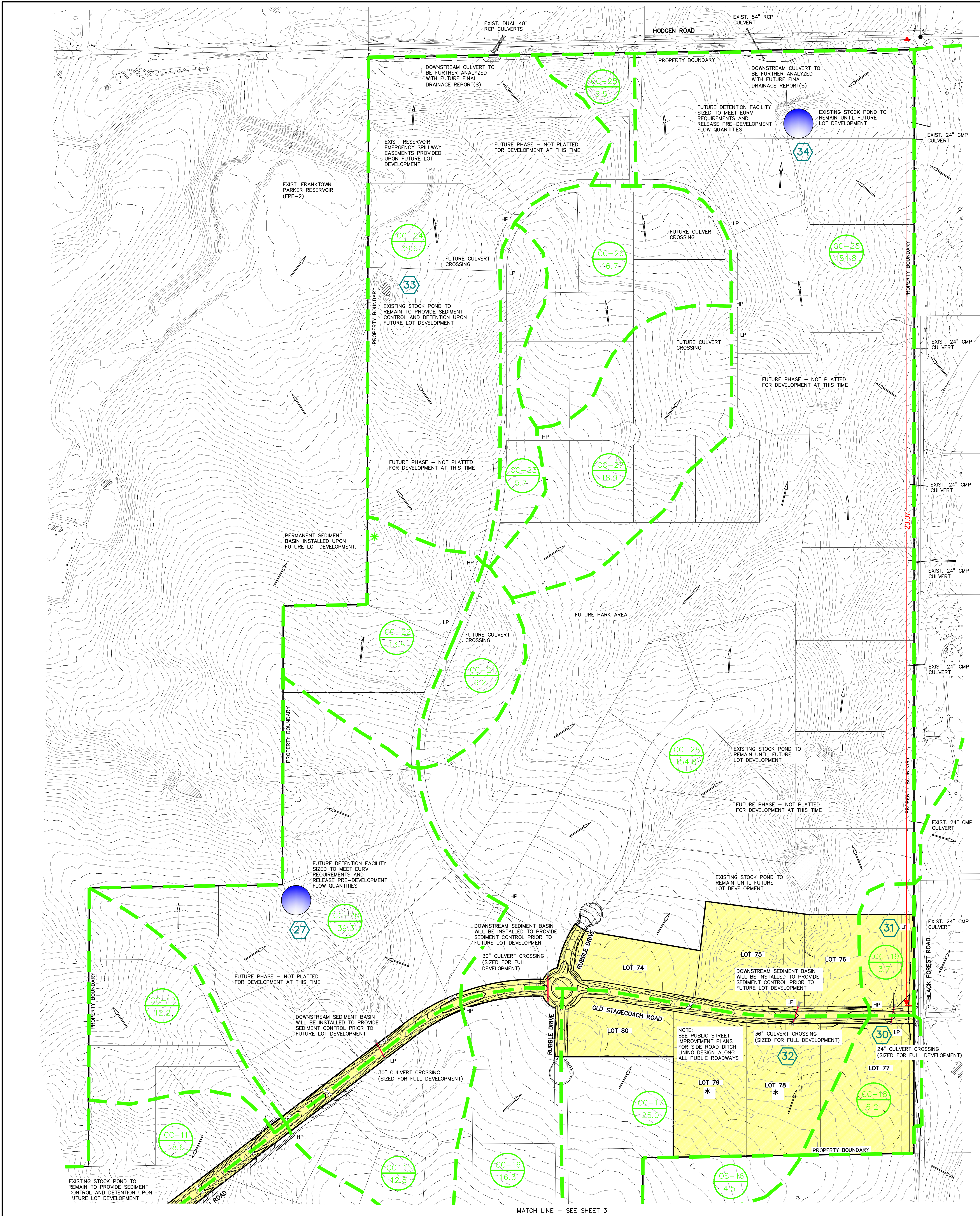
SHEET

3 OF 4

JOB NO.

1096.11



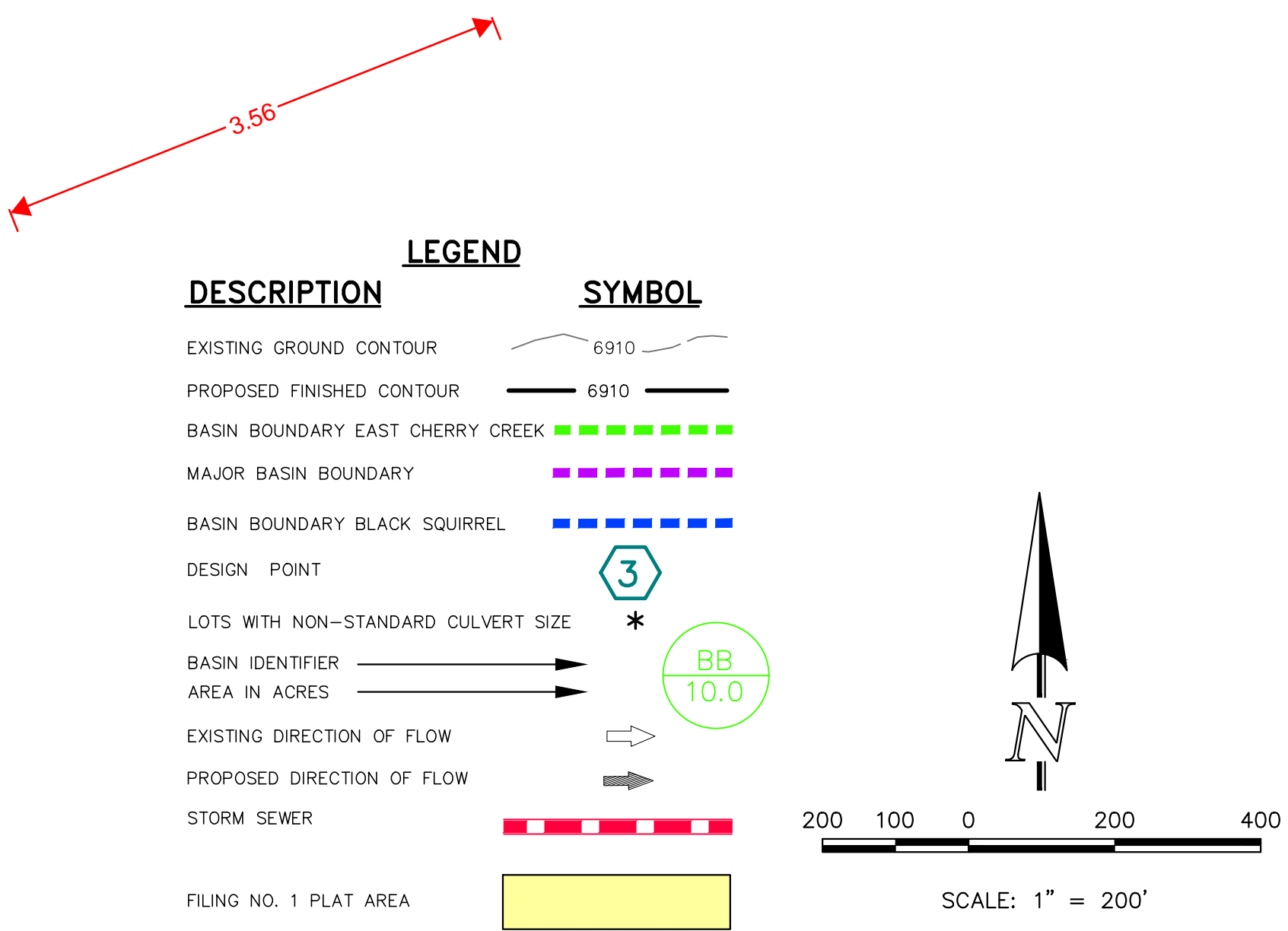


BASIN SUMMARY - DEVELOPED CONDITIONS

| BASIN (label) | AREA (acres) | COMPOSITE CN | TOTAL LAG TIME (hours) | Q 2 Yr. (cfs) | Q 5 Yr. (cfs) | Q 100 Yr. (cfs) |
|---------------|--------------|--------------|------------------------|---------------|---------------|-----------------|
| OS-16         | 4.50         | 65.0         | 0.24                   | 0.4           | 1.5           | 7.2             |
| OS-17         | 15.80        | 65.0         | 0.19                   | 1.6           | 5.9           | 27.7            |
| OS-18         | 13.00        | 65.0         | 0.20                   | 1.3           | 4.7           | 22.6            |
| CC-11         | 18.60        | 63.1         | 0.21                   | 0.9           | 5.0           | 28.1            |
| CC-12         | 12.20        | 65.0         | 0.26                   | 1.0           | 3.9           | 18.7            |
| CC-13A        | 19.30        | 65.0         | 0.31                   | 1.4           | 5.4           | 27.3            |
| CC-13B        | 25.50        | 65.0         | 0.31                   | 1.8           | 7.2           | 36.1            |
| CC-13C        | 9.90         | 65.0         | 0.22                   | 0.9           | 3.4           | 16.5            |
| CC-13D        | 18.80        | 65.0         | 0.25                   | 1.5           | 6.2           | 29.2            |
| CC-14         | 4.60         | 65.0         | 0.21                   | 0.4           | 1.6           | 7.8             |
| CC-15         | 12.80        | 65.0         | 0.24                   | 1.1           | 4.3           | 20.4            |
| CC-16         | 16.30        | 65.0         | 0.30                   | 1.2           | 4.6           | 23.6            |
| CC-17         | 25.00        | 65.0         | 0.35                   | 1.7           | 6.5           | 32.8            |
| CC-18         | 6.20         | 66.5         | 0.30                   | 0.7           | 2.2           | 9.7             |
| CC-19         | 3.70         | 65.0         | 0.25                   | 0.3           | 1.2           | 5.8             |
| CC-20         | 39.30        | 65.0         | 0.25                   | 3.2           | 12.9          | 61.0            |
| CC-21         | 6.20         | 61.0         | 0.20                   | 0.1           | 1.2           | 8.5             |
| CC-22         | 13.80        | 65.0         | 0.25                   | 1.1           | 4.5           | 21.4            |
| CC-23         | 5.70         | 64.7         | 0.33                   | 0.4           | 1.5           | 7.7             |
| CC-24         | 39.60        | 65.0         | 0.25                   | 3.3           | 13.0          | 61.5            |
| CC-25         | 3.50         | 65.0         | 0.23                   | 0.3           | 1.2           | 5.7             |
| CC-26         | 16.70        | 65.0         | 0.26                   | 1.4           | 5.3           | 25.6            |
| CC-27         | 18.90        | 64.4         | 0.31                   | 1.2           | 4.9           | 25.8            |
| CC-28         | 154.80       | 64.4         | 0.63                   | 6.5           | 24.7          | 136.3           |

DESIGN POINTS SURFACE ROUTING SUMMARY - DEVELOPED CONDITIONS

| Design Point (label) | Contributing Basins                                | Q 2 Yr. Q (cfs) | Q 5 Yr. Q (cfs) | Q 100 Yr. Q (cfs) |
|----------------------|--|-----------------|-----------------|-------------------|
| DP-27 DEV            | CC-15, CC-20                                       | 4.3             | 17.2            | 81                |
| DP-28 DEV            | CC-13A, OS-15                                      | 4.6             | 19.8            | 110               |
| DP-29 DEV            | CC-13B, CC-13C, Release from DP-28                 | 5.8             | 26.6            | 155               |
| DP-30 DEV            | CC-18  | 0.7             | 2.2             | 10                |
| DP-31 DEV            | CC-19, Release from DP-30                          | 0.9             | 3.2             | 15                |
| DP-32 DEV            | CC-17, OS-16                                       | 2.0             | 7.8             | 40                |
| DP-33 DEV            | CC-23, CC-24                                       | 3.6             | 14.4            | 69                |
| DP-34 DEV            | CC-26, CC-27, CC-28 and Release from CC-16 & DP-32 | 6.0             | 23.5            | 168               |



CLASSIC CONSULTING ENGINEERS & SURVEYORS

FLYING HORSE NORTH  
PRELIMINARY/FINAL DRAINAGE REPORT  
FILING NO. 1 AND  
PRELIMINARY PLAN DRAINAGE MAP

|             |             |              |         |          |
|-------------|-------------|--------------|---------|----------|
| DESIGNED BY | MAW         | SCALE        | DATE    | 10-17-17 |
| DRAWN BY    | MAW         | (H) 1"= 200' | SHEET   | 4 OF 4   |
| CHECKED BY  | (V) 1"= N/A | JOB NO.      | 1096.11 |          |

619 N. Cascade Avenue, Suite 200  
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INNOVATIVE DESIGN. **CLASSIC RESULTS.**

**FLYING HORSE NORTH  
IRRIGATION RESERVOIR EMBANKMENT  
DESIGN REPORT**

**DAMID: 080459  
Construction File No.: C-2085**

**AUGUST 2018**

Prepared for:  
**PRI #2 LLC**  
6385 CORPORATE DRIVE SUITE 200  
COLORADO SPRINGS CO 80919  
(719) 592-9333

Prepared by:  
**CLASSIC CONSULTING ENGINEERS &  
SURVEYORS**  
619 N. CASCADE AVE SUITE 200  
COLORADO SPRINGS CO 80903  
(719) 785-0790

Job no. 1096.11  
PCD File No. SF-18-001





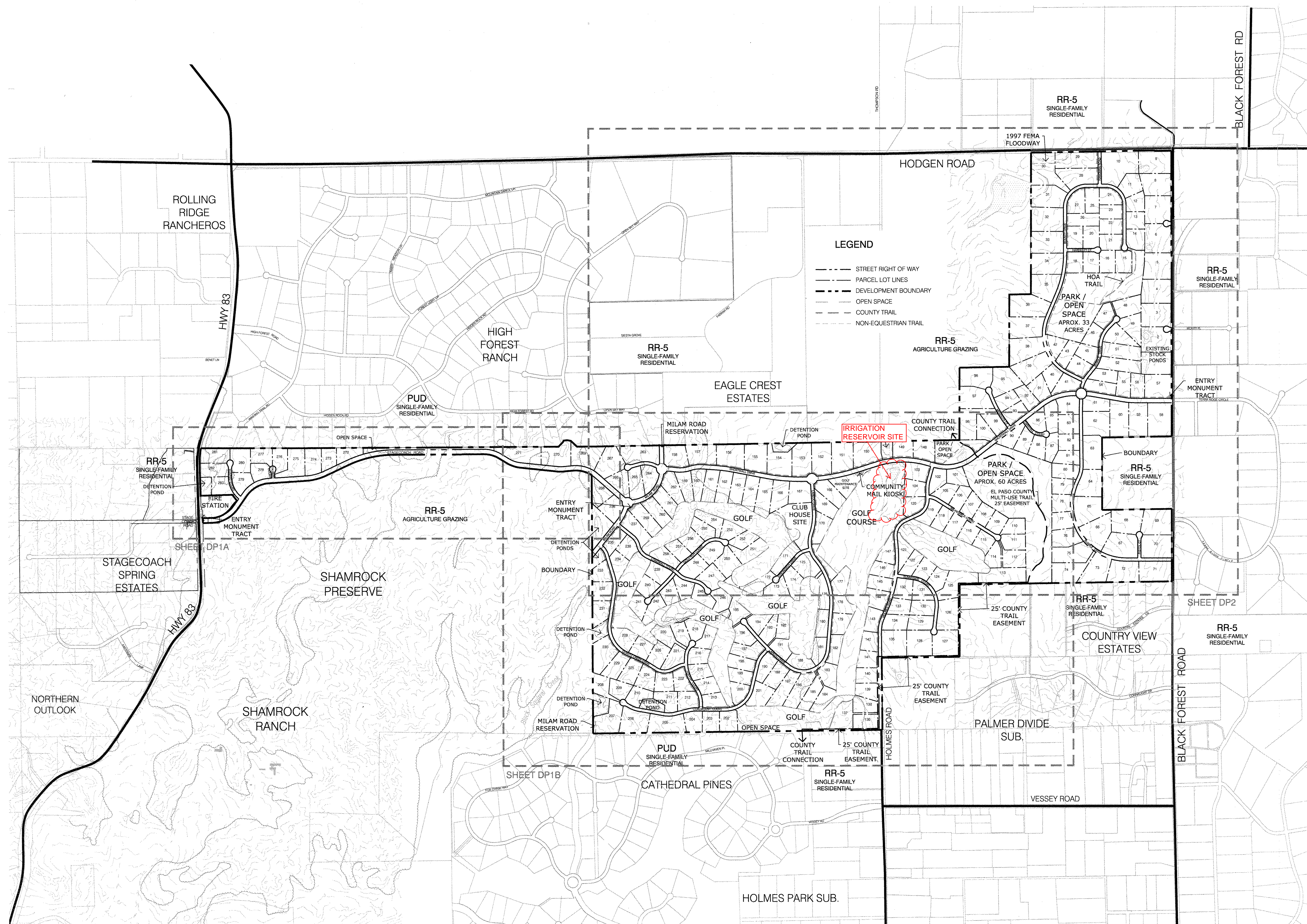
PLANNED UNIT  
DEVELOPMENT

DATE: 04-18-2011  
PROJECT MGR: J. MAYNARD  
PREPARED BY: K. MARSHALL

| DATE:    | BY: | DESCRIPTION:            |
|----------|-----|-------------------------|
| 07-25-16 | KMM | Per review comments     |
| 09-07-16 | KMM | Per 2nd review comments |
| 11-28-16 | KMM | Milam Revisions         |

DP  
2 OF 6

FIGURE 1.2







The travel time for overland flow is the estimate in time required for flow to travel from the uppermost part of a drainage basin to a defined channel or inlet of a local storm sewer system. Overland flow can be significant in small basins because a significant portion of time of concentration is due to overland flow. The velocity of overland flow can vary greatly with the surface cover and tillage characteristics. If the slope and land use of the overland flow reach are known, the travel time can be read from figure 5-2 or calculated using the following equation:

**TABLE 5-1 RECOMMENDED AVERAGE RUNOFF COEFFICIENTS AND PERCENT IMPERVIOUS**

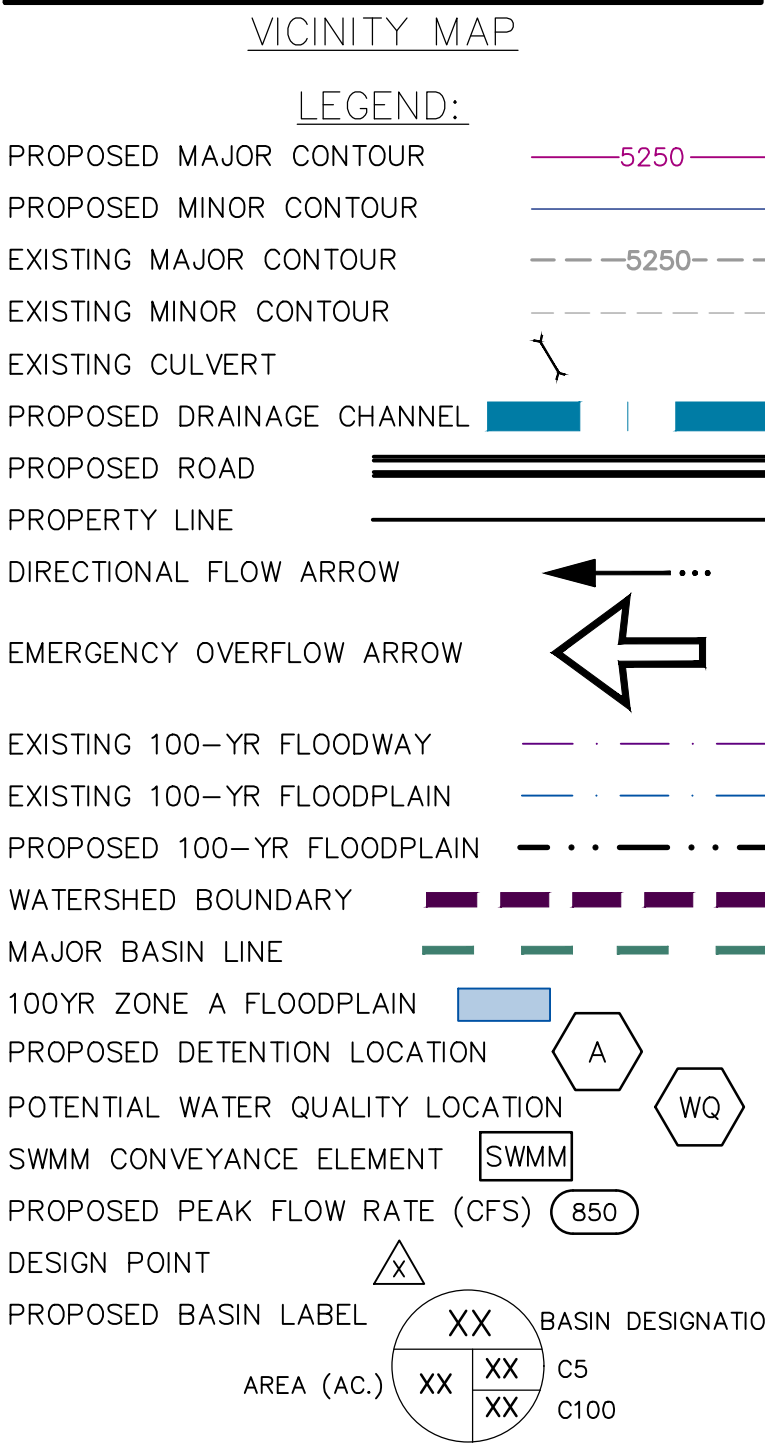
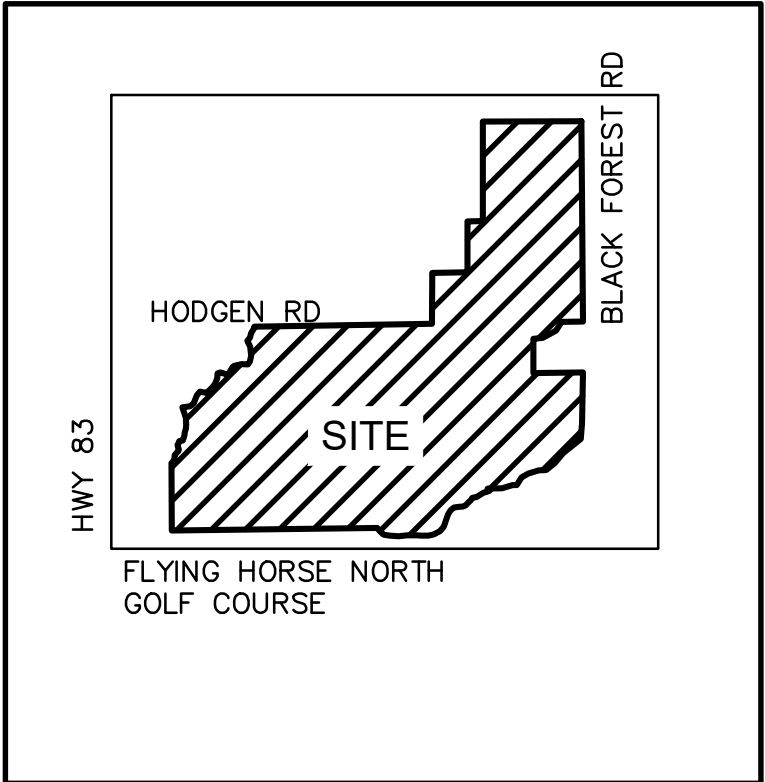
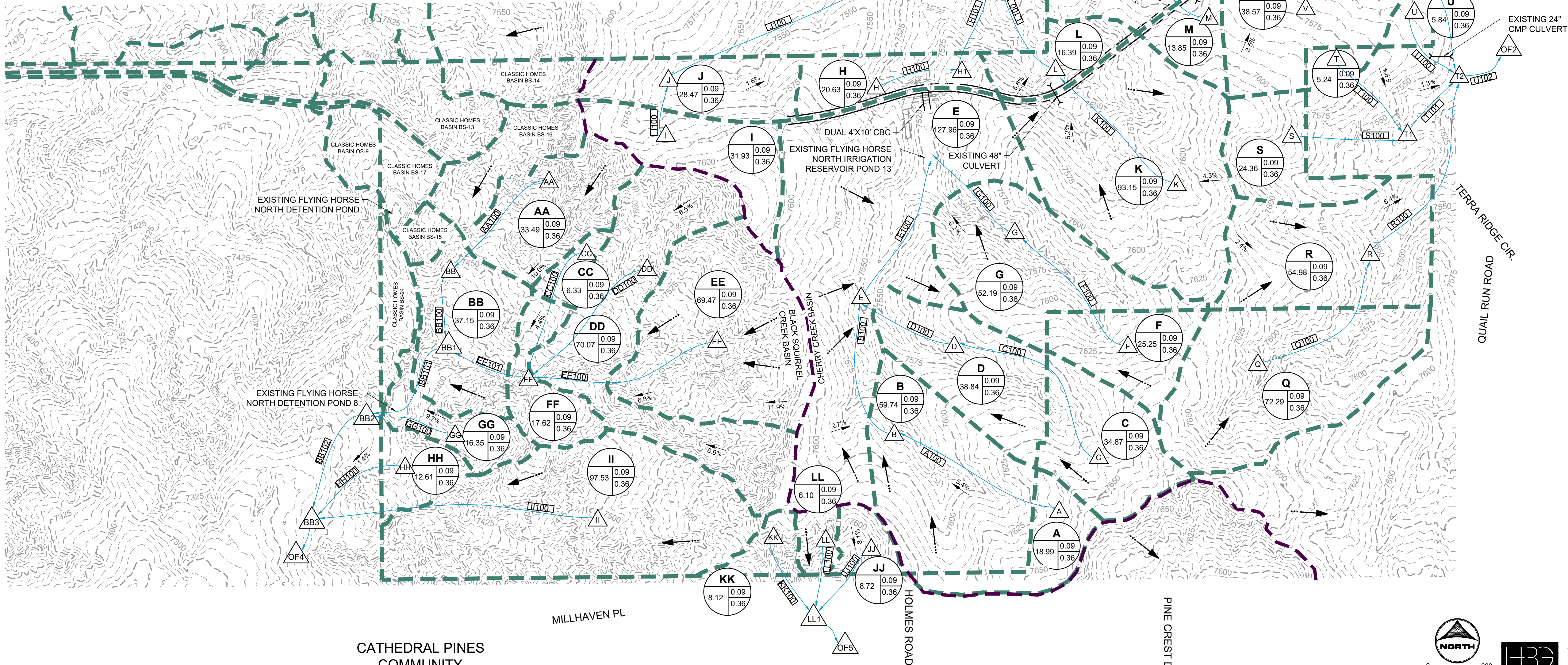
| LAND USE OR SURFACE CHARACTERISTICS               | PERCENT IMPERVIOUS | "C" FREQUENCY |      |      |      |
|---|--------------------|---------------|------|------|------|
|   |                    | 10            |      | 100  |      |
|   |                    | A&B*          | C&D* | A&B* | C&D* |
| Business  |                    |               |      |      |      |
| Commercial Areas                                  | 95                 | 0.90          | 0.90 | 0.90 | 0.90 |
| Neighborhood Areas                                | 70                 | 0.75          | 0.75 | 0.80 | 0.80 |
| Residential                                       |                    |               |      |      |      |
| ⅛ Acre or less                                    | 65                 | 0.60          | 0.70 | 0.70 | 0.80 |
| ¼ Acre  | 40                 | 0.50          | 0.60 | 0.60 | 0.70 |
| ⅓ Acre  | 30                 | 0.40          | 0.50 | 0.55 | 0.60 |
| ½ Acre  | 25                 | 0.35          | 0.45 | 0.45 | 0.55 |
| 1 Acre  | 20                 | 0.30          | 0.40 | 0.40 | 0.50 |
| Industrial  |                    |               |      |      |      |
| Light Areas                                       | 80                 | 0.70          | 0.70 | 0.80 | 0.80 |
| Heavy Areas                                       | 90                 | 0.80          | 0.80 | 0.90 | 0.90 |
| Parks and Cemeteries                              | 7                  | 0.30          | 0.35 | 0.55 | 0.60 |
| Playgrounds                                       | 13                 | 0.30          | 0.35 | 0.60 | 0.65 |
| Railroad Yard Areas                               | 40                 | 0.50          | 0.55 | 0.60 | 0.65 |
| Undeveloped Areas                                 |                    |               |      |      |      |
| Historic Flow Analysis-Greenbelts, Agricultural   | 2                  | 0.15          | 0.25 | 0.20 | 0.30 |
| Pasture/Meadow                                    | 0                  | 0.25          | 0.30 | 0.35 | 0.45 |
| Forest  | 0                  | 0.10          | 0.15 | 0.15 | 0.20 |
| Exposed Rock                                      | 100                | 0.90          | 0.90 | 0.95 | 0.95 |
| Offsite Flow Analysis (when land use not defined) | 45                 | 0.55          | 0.60 | 0.65 | 0.70 |
| Streets   |                    |               |      |      |      |
| Paved   | 100                | 0.90          | 0.90 | 0.95 | 0.95 |
| Gravel  | 80                 | 0.80          | 0.80 | 0.85 | 0.85 |
| Drive and Walks                                   | 100                | 0.90          | 0.90 | 0.95 | 0.95 |
| Roofs   | 90                 | 0.90          | 0.90 | 0.95 | 0.95 |
| Lawns   | 0                  | 0.25          | 0.30 | 0.35 | 0.45 |
| *Hydrologic Soil Group                            |                    |               |      |      |      |

## Appendix G



| Basin | Design Point | 5 Year Pre Development | 100 Year Pre Development |
|-------|--------------|------------------------|--------------------------|
| A     | A            | 20.84                  | 43.83                    |
| B     | B            | 103.48                 | 221.28                   |
| C     | C            | 33.36                  | 71.27                    |
| D     | D            | 31.56                  | 67.84                    |
| E     | E            | 223.69                 | 483.10                   |
| F     | F            | 24.27                  | 51.63                    |
| G     | G            | 79.17                  | 166.51                   |
| H     | H            | 18.59                  | 39.78                    |
| I     | I            | 34.58                  | 72.63                    |
| J     | J            | 56.31                  | 120.46                   |
| K     | K            | 92.05                  | 195.43                   |
| L     | L            | 107.58                 | 228.73                   |
| M     | M            | 11.48                  | 24.61                    |
| N     | N            | 68.16                  | 143.11                   |
| O     | O            | 22.69                  | 48.54                    |
| P     | P            | 38.52                  | 82.17                    |
| Q     | Q            | 64.68                  | 137.80                   |
| R     | R            | 108.65                 | 232.13                   |
| S     | S            | 25.99                  | 54.65                    |
| T     | T            | 4.04                   | 8.68                     |
|       | T1           | 137.90                 | 294.73                   |
|       | T2           | 145.46                 | 311.00                   |
| U     | U            | 4.15                   | 8.95                     |
| V     | V            | 29.63                  | 63.92                    |
| W     | W            | 3.45                   | 7.33                     |
| X     | X            | 167.76                 | 361.56                   |

| Basin | Design Point | 5 Year Pre Development | 100 Year Pre Development |
|-------|--------------|------------------------|--------------------------|
|       | IRR_Pond     | 298.49                 | 644.35                   |
|       | SP1          | 207.17                 | 515.49                   |
|       | SP2          | 281.79                 | 653.32                   |
|       | SP3          | 320.31                 | 725.59                   |
| AA    | AA           | 38.76                  | 80.22                    |
| BB    | BB           | 40.62                  | 84.15                    |
|       | BB1          | 242.15                 | 503.29                   |
|       | BB2          | 257.03                 | 534.86                   |
|       | BB3          | 346.26                 | 733.92                   |
| CC    | CC           | 6.53                   | 13.57                    |
| DD    | DD           | 58.42                  | 123.69                   |
| EE    | EE           | 81.16                  | 167.45                   |
| FF    | FF           | 162.77                 | 340.42                   |
| GG    | GG           | 14.93                  | 31.99                    |
| HH    | HH           | 13.01                  | 27.42                    |
| II    | II           | 81.77                  | 175.60                   |
| JJ    | JJ           | 9.74                   | 20.50                    |
| KK    | KK           | 7.51                   | 15.99                    |
| LL    | LL           | 6.88                   | 14.48                    |
|       | LL1          | 24.12                  | 50.88                    |
|       | OF1          | 320.31                 | 725.59                   |
|       | OF2          | 145.46                 | 311.00                   |
|       | OF3          | 167.76                 | 361.56                   |
|       | OF4          | 346.26                 | 733.92                   |
|       | OF5          | 24.12                  | 50.88                    |



NOTES:

Job No.: 211030.01  
Prepared By: CLB  
Date: 02/21/2022

EXISTING EX1



# FLYING HORSE NORTH SKETCH PLAN

A PORTION OF SECTIONS 34, 35 AND 36 TOWNSHIP 11 SOUTH, RANGE 66 WEST, AND A PORTION OF SECTIONS 30 AND 31, TOWNSHIP 11 SOUTH, RANGE 65 WEST OF THE SIXTH PRINCIPAL MERIDIAN, EL PASO COUNTY, COLORADO

## NOTES

### GENERAL NOTES

- A TOTAL OF 846 DWELLING UNITS ARE PROPOSED WITHIN THE FLYING HORSE NORTH SKETCH PLAN ON APPROXIMATELY 912.6 ACRES. THE SUBMITTAL ALSO, INCLUDES A LUXURY RESORT HOTEL, CASITAS AND FLATS THAT TOTAL 275 KEYS (ROOMS)/UNITS.
- CLUSTERING OF UNITS WITHIN RESIDENTIAL DISTRICTS IS PERMITTED, BUT NOT REQUIRED, SO LONG AS THE OVERALL DENSITY LIMIT IS NOT EXCEEDED. THE USE OF CLUSTERING IS ENCOURAGED TO PROMOTE COMMON OPEN SPACE, PROTECT NATURAL FEATURES, AND PROVIDE CREATIVE AND FLEXIBLE DESIGN ALTERNATIVES.
- A DENSITY TRANSFER MAY BE PERMITTED ON FLYING HORSE NORTH FOR ALL RESIDENTIAL DISTRICTS. THIS TRANSFER WOULD BE PROPOSED AT THE TIME OF REZONING AND/OR PRELIMINARY PLAN (WHERE APPROPRIATE) AND WOULD NEED TO BE REVIEWED BY STAFF TO ENSURE THAT THE OVERALL DEVELOPMENT CONCEPT IS ADHERED TO. A DENSITY TRANSFER NOT TO EXCEED TWENTY PERCENT (20%) OF THE MAXIMUM UNITS FOR EACH PARCEL IS PERMITTED. THE TRANSFERRED DENSITY SHALL MEET ALL MINIMUM REQUIREMENTS OF THE RECEIVING AREA SUCH AS LOT SIZE, SETBACKS, ETC. IN NO CASE SHALL THE OVERALL DENSITY CAP EXCEED THE TOTAL UNITS APPROVED FOR THE PROJECT.
- SPECIFIC DEVELOPMENT STANDARDS SUCH AS SETBACKS, LOT COVERAGE, BUILDING HEIGHTS AND LAND USES SHALL BE ADDRESSED WITH A SUBSEQUENT ZONING OF THE PROPERTY AT A LATER DATE. THESE STANDARDS WILL EITHER FOLLOW SPECIFIC PROPOSED PUD DEVELOPMENT PLANS OR PER COUNTY ZONING STANDARDS IF FOLLOWING "CONVENTIONAL ZONING" OF THE COUNTY.
- ALL COMMON LANDSCAPE, OPEN SPACE, PARKS, TRACTS AND DRAINAGE FACILITIES WITHIN THIS DEVELOPMENT SHALL BE OWNED AND MAINTAINED BY THE HOA (TO BE NAMED) OR FLYING HORSE NORTH METROPOLITAN DISTRICT WITH THE EXCEPTION OF THE COUNTY TRAIL AS DEPICTED ON THE SKETCH PLAN.
- ALL DETENTION PONDS AND CROSS LOT DRAINAGE DITCHES WILL BE LOCATED WITHIN DRAINAGE EASEMENTS PROVIDING ACCESS FOR MAINTENANCE TO THE FLYING HORSE NORTH METROPOLITAN DISTRICT OR HOA (TO BE NAMED).
- THERE SHALL BE NO DIRECT RESIDENTIAL LOT ACCESS TO BLACK FOREST ROAD EXCEPT FOR THE EXISTING STAGECOACH ROAD ACCESS AND POTENTIAL COMMERCIAL ACCESS.
- PARK IMPROVEMENTS PROVIDED BY THE DEVELOPER MAY BE APPLIED TO PARK LAND DEDICATION AND/OR FEES WITH REVIEW AND APPROVAL BY EL PASO COUNTY PARKS. ANY PARK IMPROVEMENTS WILL BE COORDINATED AT A LATER DATE WITH EL PASO COUNTY PARKS VIA PARK LAND AGREEMENTS.
- ALL ELECTRIC SERVICE SHALL BE PROVIDED BY MOUNTAIN VIEW ELECTRIC ASSOCIATION AND GAS TO BE PROVIDED BY BLACK HILLS ENERGY. NATURAL GAS EASEMENTS WILL BE PROVIDED AS REQUIRED.
- SITE LIGHTING, IF REQUIRED, WILL MEET THE REQUIREMENTS SET FORTH IN SECTION 6.2.3 OF EL PASO COUNTY LAND DEVELOPMENT CODE.
- THE DEVELOPER SHALL COMPLY WITH FEDERAL AND STATE LAWS, REGULATIONS, ORDINANCES, REVIEW AND PERMIT REQUIREMENTS, AN OTHER AGENCY REQUIREMENTS, IF ANY, OF APPLICABLE AGENCIES INCLUDING, BUT NOT LIMITED TO, THE COLORADO PARKS AND WILDLIFE, COLORADO DEPARTMENT OF TRANSPORTATION, U.S. ARMY CORPS OF ENGINEERS, AND THE U.S. FISH AND WILDLIFE SERVICE REGARDING THE ENDANGERED SPECIES ACT, PARTICULARLY AS IT RELATES TO ANY LISTED SPECIES.
- THE FOLLOWING DISTRICTS WILL SERVE THE PROPERTY  
LEWIS-PALMER DISTRICT 38 AND ACADEMY DISTRICT 20  
FIRE EMERGENCY - BLACK FOREST FIRE PROTECTION DISTRICT  
EMERGENCY SERVICES - BLACK FOREST FIRE PROTECTION DISTRICT  
TELECOM/FIBER - FORCE BROADBAND & COMCAST  
PIKES PEAK LIBRARY DISTRICT  
ELECTRICAL SERVICES - MVEA
- THE MAILBOX KIOSK WILL BE DETERMINED WITH EACH FINAL PLAT AND IN COORDINATION WITH THE U.S. POSTAL SERVICE.
- THE FIRE STATION LOCATED IN FILING 1 CAN BE RELOCATED ANYWHERE IN THE SKETCH PLAN AREA IF NEEDED. IF FIRE DEPARTMENT DETERMINES RELOCATION IS NOT NEEDED, THE LAND NEED NOT BE DEDICATED TO THEM.
- APPLICABLE PARK, SCHOOL, TRANSPORTATION, DRAINAGE, BRIDGE, AND TRAFFIC FEES SHALL BE PAID TO THE EL PASO COUNTY PLANNING AND COMMUNITY DEVELOPMENT DEPARTMENT AT THE TIME OF RECORDING ANY FINAL PLAT.
- ACCESS LOCATIONS AND ROADWAY CLASSIFICATIONS ARE CONCEPTUAL ONLY AND WILL BE DETERMINED AT THE TIME PRELIMINARY PLAN REVIEW. FINAL LOCATIONS AND CLASSIFICATIONS OF ROADWAYS WILL BE SUBJECT MORE DETAILED LAND DESIGN AND SUBDIVISION REVIEW.

### FLOODPLAIN NOTES:

- PORTIONS OF THIS PROPERTY ARE LOCATED WITHIN A DESIGNATED FEMA FLOODPLAIN AS DETERMINED BY THE FEMA NATIONAL FLOOD INSURANCE PROGRAM FLOOD INSURANCE MAP NUMBERS '08041C0305G' AND '08041C0315G' WITH AN EFFECTIVE DATE OF DECEMBER 7, 2018.
- THE EXISTING FLOODPLAIN BOUNDARIES ARE INTENDED TO REMAIN AND DEVELOPMENT WILL OCCUR OUTSIDE THE FLOODPLAIN LIMITS.
- NO STRUCTURES OR SOLID FENCES ARE PERMITTED WITHIN THE DESIGNATED FLOODPLAIN AREA.

### PUBLIC STREETS

- PER THE INTERGOVERNMENTAL AGREEMENT, THE CITY OF COLORADO SPRINGS WILL REQUIRE THE STREETS TO BE DESIGNED AND CONSTRUCTED TO THE CITY STANDARDS.
- SIDEWALKS OR WALKWAYS WILL BE PROVIDED ALONG ALL STREETS AND INTERIOR TO DEVELOPMENT PARCELS, PARKS AND TRAIL SYSTEMS.
- PUBLIC STREETS WITHIN THIS DEVELOPMENT SHALL PROVIDE FOR LEVELS OF VEHICULAR CIRCULATION REQUIRED BY THE TRAFFIC STUDY AND SHALL BE PAVED.
- UNTIL APPROVED BY THE COUNTY ENGINEER ALL ACCESS POINTS SHOWN ON THIS PLAN ARE CONCEPTUAL AND NON-BINDING UPON THE COUNTY APPROVAL OF THIS SKETCH PLAN AMENDMENT SHALL NOT BE INTERPRETED TO INCLUDE APPROVAL OF ANY ACCESS TO ANY PUBLIC ROADS. THE COUNTY ENGINEER SHALL APPROVE ALL ACCESSES IN ACCORDANCE WITH THE REQUIREMENTS AND PROCEDURES OF THE ENGINEERING CRITERIA MANUAL AT THE TIME OF PUD DEVELOPMENT PLAN AND/OR SUBDIVISION SUBMITTAL AND REVIEW.

### PRIVATE STREETS

- ANY FUTURE PRIVATE STREETS, IF PROPOSED, WILL BE PRIVATELY OWNED AND MAINTAINED BY THE FLYING HORSE NORTH METROPOLITAN DISTRICT NO. 1 OR HOA (HOMEOWNERS ASSOCIATION-TO BE NAMED).

### PHASING PLAN:

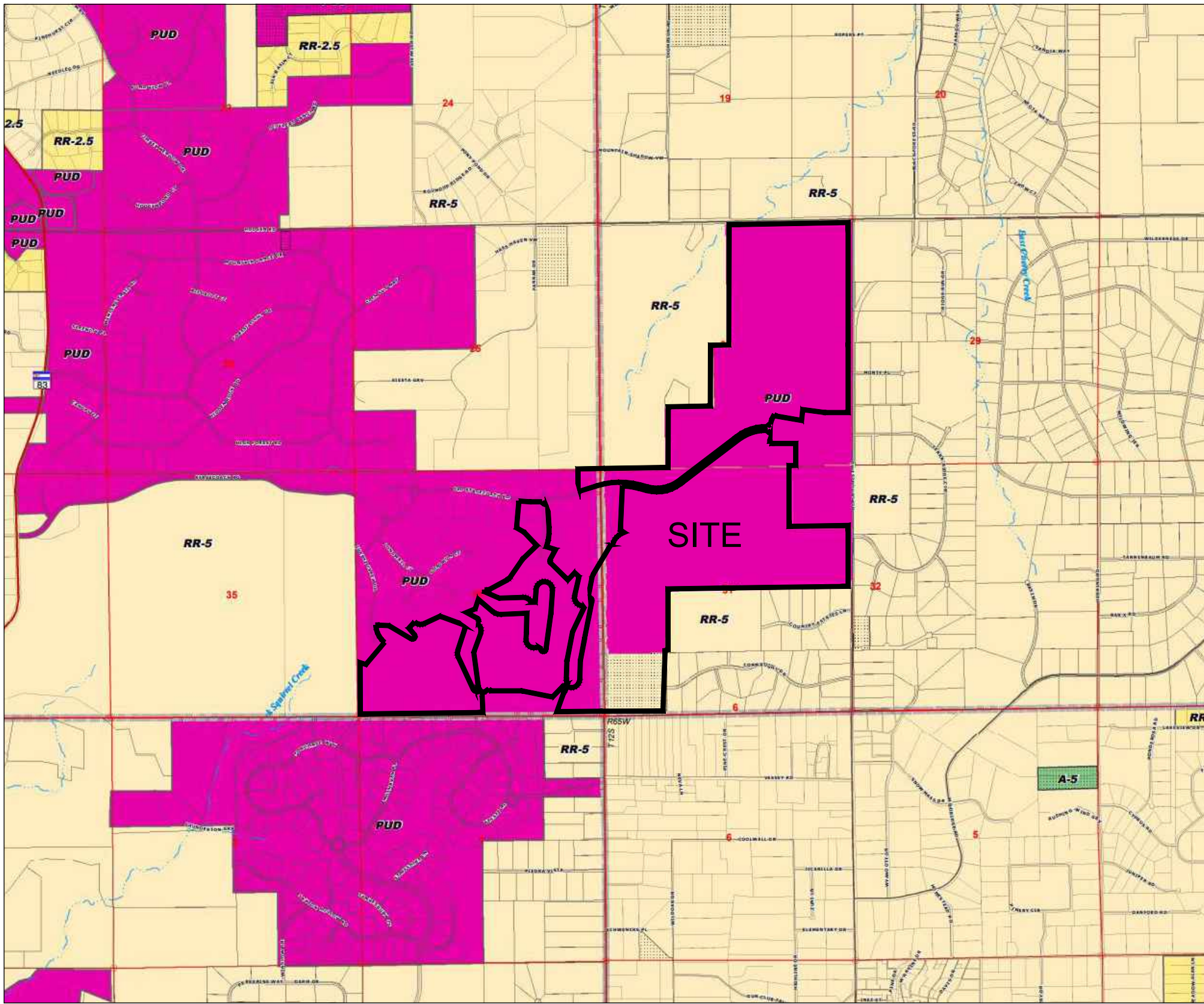
- THE FLYING HORSE NORTH PROJECT WILL BE DEVELOPED IN MULTIPLE PHASES AND PLATTED IN MULTIPLE FILINGS, WHICH HAVE YET TO BE DETERMINED. THE SEQUENCE OF CONSTRUCTION AND DEVELOPMENT IS NOT DEPENDENT UPON UTILITIES OR INFRASTRUCTURE.

### GEOLOGIC HAZARDS DISCLOSURE STATEMENT:

- AREAS OF PROPOSED SUBDIVISION HAVE BEEN FOUND TO BE IMPACTED BY GEOLOGICAL CONDITIONS, INCLUDING SEASONAL AND POTENTIALLY SEASONAL SHALLOW GROUND WATER, ARTIFICIAL FILL, LOOSE AND EXPANSIVE SOILS AND SLOPE STABILITY. THESE CONDITIONS CAN BE MITIGATED BY AVOIDANCE, RE-GRADING, PROPER ENGINEERING DESIGN, AND CONSTRUCTION TECHNIQUES. A MAP OF THE HAZARD AREAS AND PROPOSED MITIGATION MEASURES CAN BE FOUND IN THE GEOLOGICAL HAZARD STUDY AND WASTEWATER STUDY PREPARED BY ENTECH ENGINEERING INC., DATED JANUARY 15, 2019. FURTHER STUDIES OF THESE CONDITIONS SHALL BE PROVIDED WITH EITHER PRELIMINARY OR FINAL PLANS.

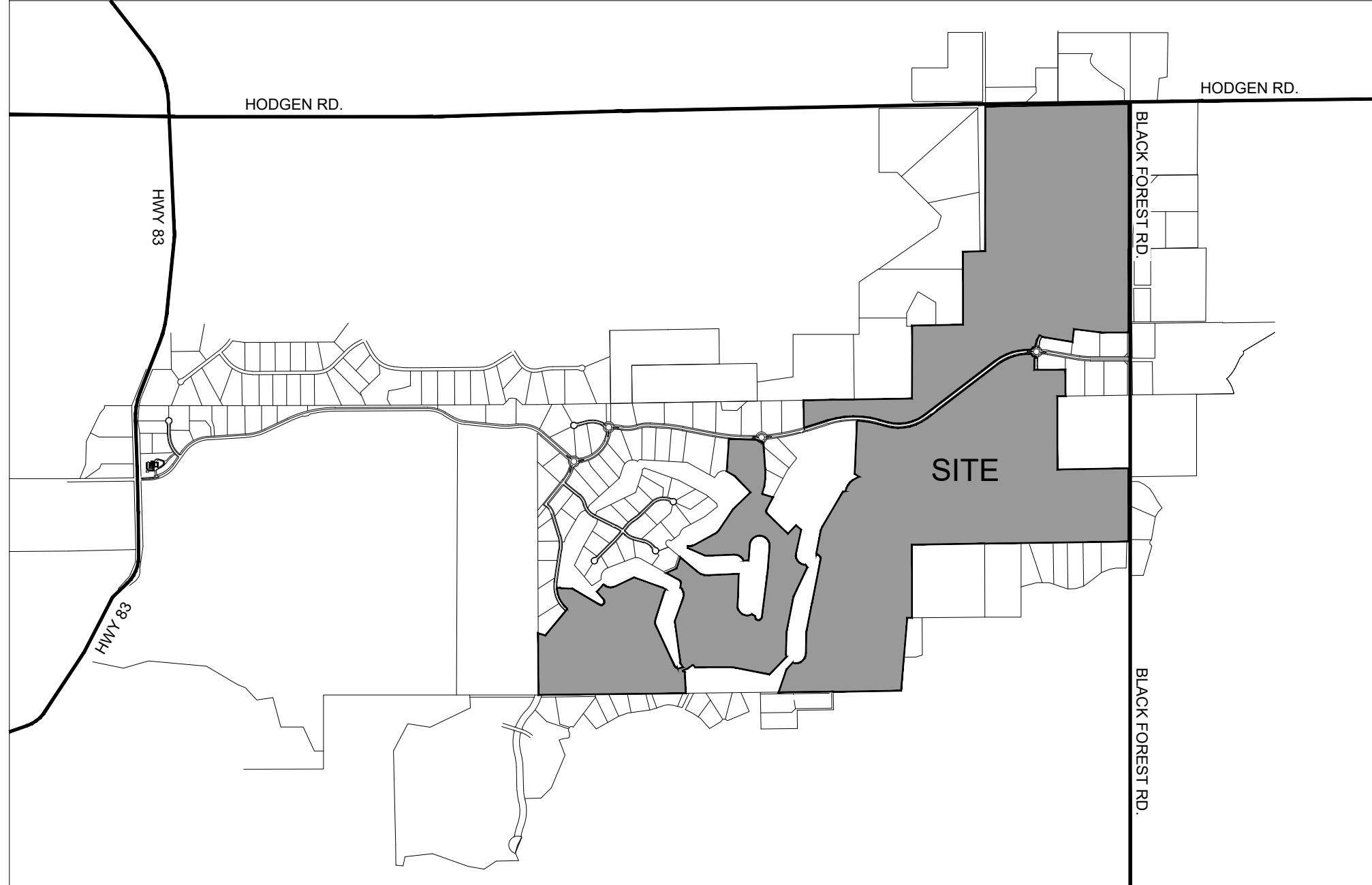
## ZONING MAP

SCALE = N.T.S



## VICINITY MAP

SCALE = N.T.S



## SHEET INDEX

SHEET 1 OF 5: COVER SHEET  
SHEET 2 OF 5: SKETCH PLAN  
SHEET 3 OF 5: ADJACENT PROPERTY MAP  
SHEET 4 OF 5: ADJACENT PROPERTY OWNERS  
SHEET 5 OF 5: ADJACENT PROPERTY OWNERS

OWNER/DEVELOPER:  
FLYING HORSE DEVELOPMENT LLC  
2138 FLYING HORSE CLUB DRIVE  
COLORADO SPRINGS, CO 80921

PLANNER/LANDSCAPE ARCHITECT:  
HRGREEN DEVELOPMENT, LLC  
1975 RESEARCH PARKWAY SUITE 230  
COLORADO SPRINGS, CO 80920  
720.602.4941

CIVIL ENGINEER:  
HRGREEN DEVELOPMENT, LLC  
1975 RESEARCH PARKWAY SUITE 230  
COLORADO SPRINGS, CO 80920  
720.602.4965

ECOLOGIST:  
BRISTLECONE ECOLOGY  
2023 W. SCOTT PLACE  
DENVER, CO 80211  
971.237.3906

TRANSPORTATION CONSULTANTS:  
SM ROCHA, LLC  
DENVER, CO 80211  
303.458.9798

## SITE DATA

EXISTING LAND USE: VACANT  
EXISTING ZONING: PUD & RR-5

SITE ACREAGE: 912.6 AC  
MAXIMUM NUMBER OF RESIDENTIAL UNITS: 846  
MAXIMUM GROSS DENSITY FOR RESIDENTIAL UNITS: 0.93 DU/AC

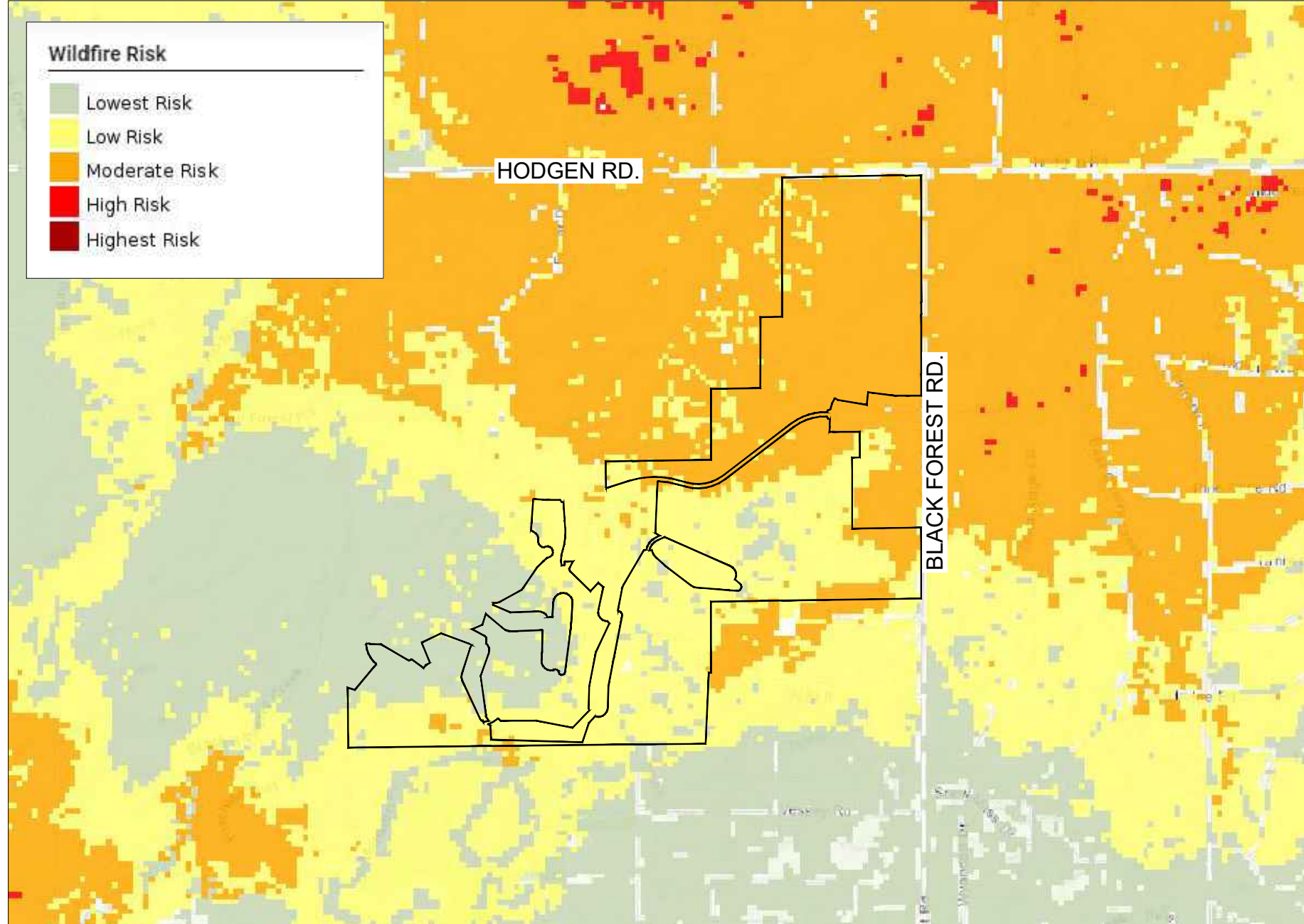
TOTAL AREAS (SEE LAND USE CHART ON SHEET 2)

|                         |          |
|-------------------------|----------|
| RESIDENTIAL:            | 853.8 AC |
| ESTATE LOTS (5 ACRES)   | 118.3 AC |
| ESTATE LOTS (2.5 ACRES) | 152.7 AC |
| LOW DENSITY             | 332.9 AC |
| MEDIUM DENSITY          | 46.0 AC  |
| ESTIMATED OPEN SPACE    | 203.9 AC |

|   |         |
|---|---------|
| HOTEL/CASITAS/FLATS                               | 32.2 AC |
| GOLF CLUB, RESTAURANT/BAR, GOLF AMENITIES (HOTEL) | 11.0 AC |
| ESTATE CLUBHOUSE (HOTEL)                          | 2.4 AC  |
| COMMERCIAL  | 9.1 AC  |
| FITNESS CENTER                                    | 4.1 AC  |

## WILDFIRE RISK MAP

SCALE = N.T.S



COUNTY FILE NUMBER: SKP223

DRAWN BY: JAG  
APPROVED: PLS  
CAD DATE: 9/15/2022  
CAD FILE: J:\2021\211030\CAD\Drawings\Sketch-Plan\COVER-SHEET

JOB DATE: 3/1/2022  
JOB NUMBER: 211030

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0" 1"  
IF NOT ONE INCH, ADJUST SCALE ACCORDINGLY.

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FLYING HORSE NORTH  
DEVELOPMENT, LLC.  
EL PASO COUNTY, COLORADO

FLYING HORSE NORTH SKETCH PLAN  
COVER SHEET

SHEET  
SP.1

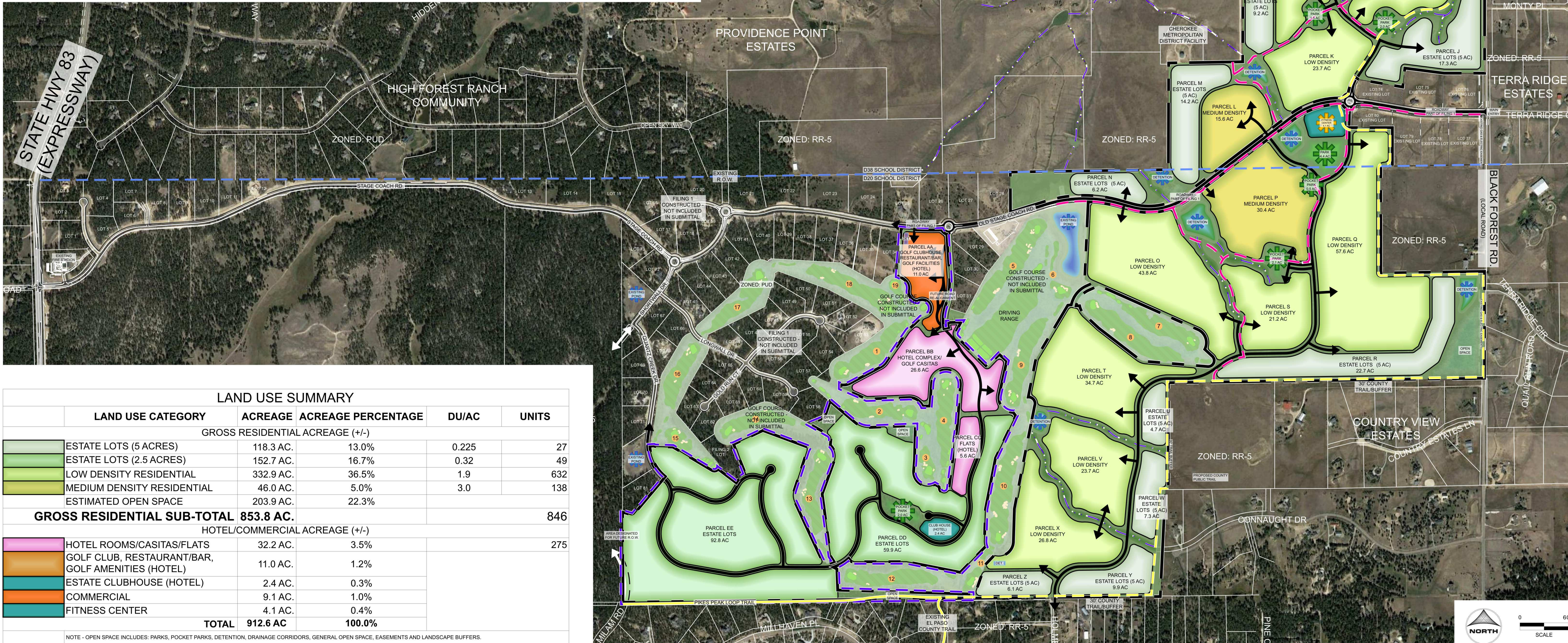
1



# FLYING HORSE NORTH SKETCH PLAN

## LEGEND

|  |   |  |                        |
|--|---|--|------------------------|
|  | ESTATE LOTS (5 AC)                                |  | HOTEL PARCELS          |
|  | ESTATE LOTS (2.5 AC)                              |  | SCHOOL DISTRICT LINE   |
|  | LOW DENSITY                                       |  | FHN TRAIL              |
|  | MEDIUM DENSITY                                    |  | PUBLIC COUNTY TRAIL    |
|  | COMMERCIAL  |  | EXISTING DRAINAGE WAY  |
|  | GOLF CLUB, FITNESS CENTER, RESTAURANT/BAR (HOTEL) |  | PARK/POCKET PARK       |
|  | HOTEL COMPLEX                                     |  | FITNESS CENTER         |
|  | CLUBHOUSE   |  | POTENTIAL FIRE STATION |
|  | ROADWAY   |  | DETENTION              |
|  | DETENTION   |  |                        |
|  | SITE BOUNDARY                                     |  |                        |



## LAND USE SUMMARY

| LAND USE CATEGORY                                 | ACREAGE   | ACREAGE PERCENTAGE | DU/AC | UNITS |
|---|-----------|--------------------|-------|-------|
| GROSS RESIDENTIAL ACREAGE (+/-)                   |           |                    |       |       |
| ESTATE LOTS (5 ACRES)                             | 118.3 AC. | 13.0%              | 0.225 | 27    |
| ESTATE LOTS (2.5 ACRES)                           | 152.7 AC. | 16.7%              | 0.32  | 49    |
| LOW DENSITY RESIDENTIAL                           | 332.9 AC. | 36.5%              | 1.9   | 632   |
| MEDIUM DENSITY RESIDENTIAL                        | 46.0 AC.  | 5.0%               | 3.0   | 138   |
| ESTIMATED OPEN SPACE                              | 203.9 AC. | 22.3%              |       |       |
| GROSS RESIDENTIAL SUB-TOTAL                       |           |                    |       | 846   |
| HOTEL/COMMERCIAL ACREAGE (+/-)                    |           |                    |       |       |
| HOTEL ROOMS/CASITAS/FLATS                         | 32.2 AC.  | 3.5%               |       | 275   |
| GOLF CLUB, RESTAURANT/BAR, GOLF AMENITIES (HOTEL) | 11.0 AC.  | 1.2%               |       |       |
| ESTATE CLUBHOUSE (HOTEL)                          | 2.4 AC.   | 0.3%               |       |       |
| COMMERCIAL  | 9.1 AC.   | 1.0%               |       |       |
| FITNESS CENTER                                    | 4.1 AC.   | 0.4%               |       |       |
| TOTAL   | 912.6 AC  | 100.0%             |       |       |

NOTE - OPEN SPACE INCLUDES: PARKS, POCKET PARKS, DETENTION, DRAINAGE CORRIDORS, GENERAL OPEN SPACE, EASEMENTS AND LANDSCAPE BUFFERS.

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APPROVED: PLS  
CAD DATE: 07/01/2022  
CAD FILE: J:\2021\211030\CAD\Drawings\Sketch-Plan\BUBBLE-PLAN

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ADJUST SCALE ACCORDINGLY.

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FLYING HORSE NORTH  
DEVELOPMENT, LLC.  
EL PASO COUNTY, COLORADO

FLYING HORSE NORTH SKETCH PLAN  
SKETCH PLAN DRAWING

SHEET  
SP.2  
2

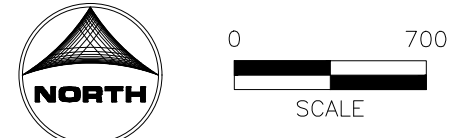
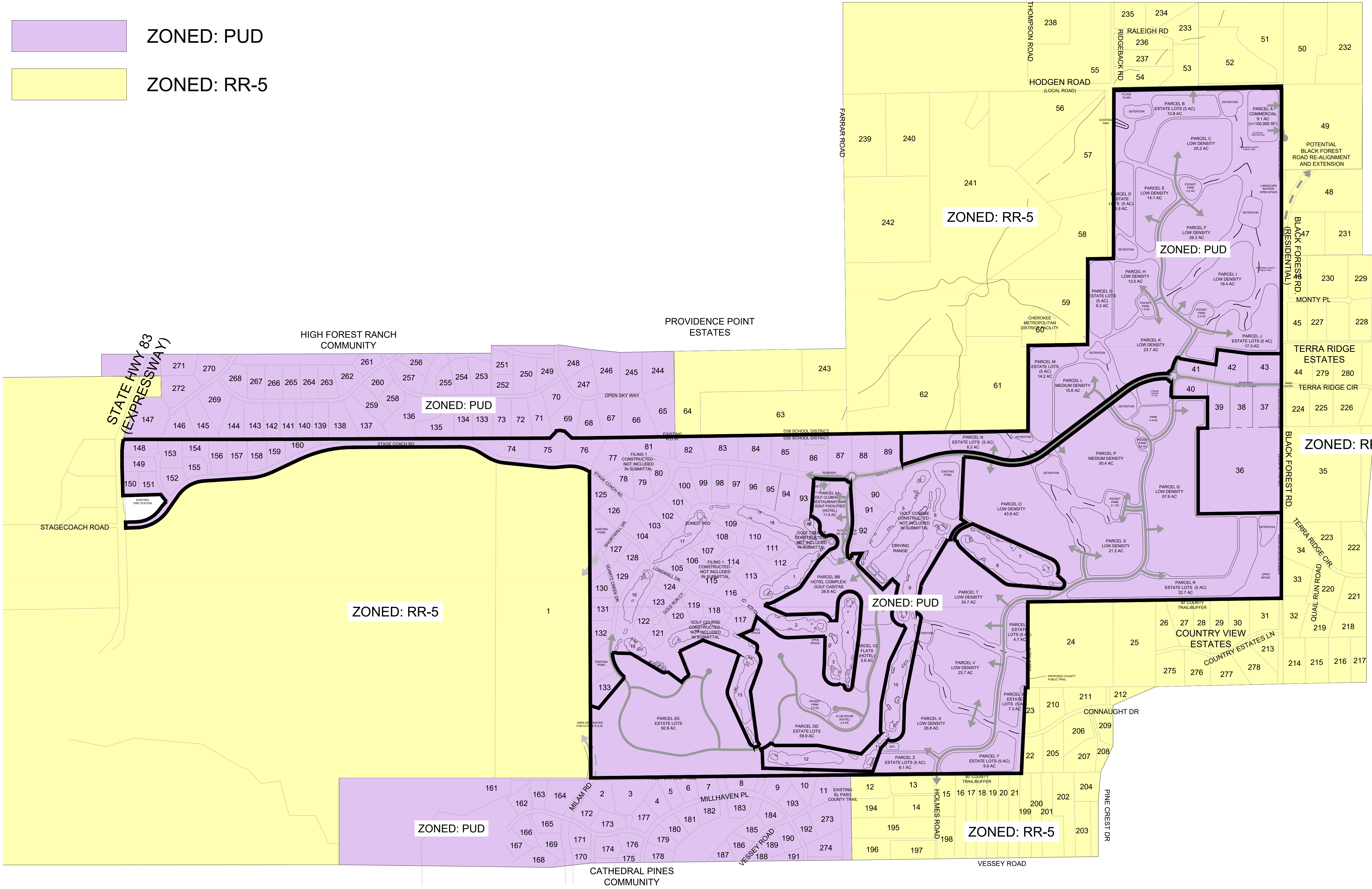
COUNTY FILE NUMBER: SKP223



# FLYING HORSE NORTH SKETCH PLAN

## LEGEND

- ZONED: PUD
- ZONED: RR-5



COUNTY FILE NUMBER: SKP223

DRAWN BY: JAG JOB DATE: 3/1/2022  
APPROVED: PLS JOB NUMBER: 211030  
CAD DATE: 2/21/2022  
CAD FILE: J:\2021\211030\CAD\Drawings\Sketch-Plan\ADJACENT-PROPERTY

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OFFICIAL DRAWINGS.  
0 1" IF NOT ONE INCH,  
ADJUST SCALE ACCORDINGLY.

| NO. | DATE | BY | REVISION DESCRIPTION |
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|     |      |    |                      |



FLYING HORSE NORTH  
DEVELOPMENT, LLC.  
EL PASO COUNTY, COLORADO

FLYING HORSE NORTH SKETCH PLAN  
ADJACENT PROPERTY DATA MAP

SHEET  
SP.3  
3



FLYING HORSE NORTH SKETCH PLAN

|   |  |   |   |   |  |   |   |  |
|---|--|---|---|---|--|---|---|--|
| 1. SHAMROCK SS LLC<br>ZONING - RR-5<br>15555 HWY 83<br>COLORADO SPRINGS, CO                     | 19. RUPP JERRREY D<br>ZONED - RR-5<br>5970 VESSEY ROAD<br>COLORADO SPRINGS, CO                       | 37. DERKSEN PROPERTIES LLC<br>ZONED - PUD<br>6755 OLD STAGECOACH ROAD<br>COLORADO SPRINGS, CO | 55. NAVARETTE JEANINE A<br>ZONED - RR-5<br>6280 HODGEN ROAD<br>COLORADO SPRINGS, CO                 | 72. JOHNSON LIVING TRUST<br>ZONED - PUD<br>4841 HIGH FOREST ROAD<br>COLORADO SPRINGS, CO      | 90. PECK MICHAEL S<br>ZONED - PUD<br>5555 OLD STAGECOACH ROAD<br>COLORADO SPRINGS, CO            | 108. HENDRICKS JAMES<br>ZONED - PUD<br>5202 GOLD RUN COURT<br>COLORADO SPRINGS, CO          | 126. HOWARTH WILLIAM<br>ZONED - PUD<br>15290 SHORTWALL DRIVE<br>COLORADO SPRINGS, CO              | 144. DESAUTELS BRUCE T<br>ZONED - PUD<br>4661 HIDDEN ROCK ROAD<br>COLORADO SPRINGS, CO             |
| 2. BRI J FAMILY TRUST<br>ZONED - PUD<br>4820 FOXCHASE WAY<br>COLORADO SPRINGS, CO               | 20. LITTLETON STANLEY<br>ZONED - RR-5<br>6010 VESSEY ROAD<br>COLORADO SPRINGS, CO                    | 38. NGUYEN LINH T<br>ZONED - PUD<br>6715 OLD STAGECOACH ROAD<br>COLORADO SPRINGS, CO          | 56. ANDREWS SCOTT W<br>ZONED - RR-5<br>HODGEN ROAD<br>COLORADO SPRINGS, CO                          | 73. RAMIREZ MELODY B<br>ZONED - PUD<br>4781 HIGH FOREST ROAD<br>COLORADO SPRINGS, CO          | 91. RENNER LLC<br>ZONED - PUD<br>15331 ALLEN RANCH ROAD<br>COLORADO SPRINGS, CO                  | 109. C&C LIVING TRUST<br>ZONED - PUD<br>5232 GOLD RUN COURT<br>COLORADO SPRINGS, CO         | 127. GERBER JOSEPH DAVID<br>ZONED - PUD<br>15262 SHORTWALL DRIVE<br>COLORADO SPRINGS, CO          | 145. HOUSE JAMIE GLEN<br>ZONED - PUD<br>15575 WINDING TRAIL ROAD<br>COLORADO SPRINGS, CO           |
| 3. PIASECKI NANCY L REVOC TRUST<br>ZONED - PUD<br>4940 FOXCHASE WAY<br>COLORADO SPRINGS, CO     | 21. SWANSON BRECK C<br>ZONED - RR-5<br>6030 VESSEY ROAD<br>COLORADO SPRINGS, CO                      | 39. MONACO57 LIVING TRUST<br>ZONED - PUD<br>6675 OLD STAGECOACH ROAD<br>COLORADO SPRINGS, CO  | 57. DEIM CONNIE<br>ZONED - RR-5<br>SUNDANCE RANCH LANE<br>COLORADO SPRINGS, CO                      | 74. FOWLER NORMAN W<br>ZONED - PUD<br>4670 STAGECOACH ROAD<br>COLORADO SPRINGS, CO            | 92. BOOGAARD RYAN<br>ZONED - PUD<br>15271 ALLEN RANCH ROAD<br>COLORADO SPRINGS, CO               | 110. ALBRIGHT MARK PHILLIP<br>ZONED - PUD<br>5262 GOLD RUN COURT<br>COLORADO SPRINGS, CO    | 128. COFFEY LAVANSON C III<br>ZONED - PUD<br>15192 SHORTWALL DRIVE<br>COLORADO SPRINGS, CO        | 146. MATALIUS ANDREW J III<br>ZONED - PUD<br>15525 WINDING TRAIL ROAD<br>COLORADO SPRINGS, CO      |
| 4. BRINGARD FAMILY LICING TRUST<br>ZONED - PUD<br>14465 MILLHAVEN PLACE<br>COLORADO SPRINGS, CO | 22. HOOKS GROUP LP<br>ZONED - RR-5<br>6005 CONNAUGHT DRIVE<br>COLORADO SPRINGS, CO                   | 40. ST HENRYS LLC<br>ZONED - PUD<br>6595 OLD STAGECOACH ROAD<br>COLORADO SPRINGS, CO          | 58. BR&C INC<br>ZONED - RR-5<br>30-11-65<br>COLORADO SPRINGS, CO                                    | 75. OLSON TYRONE L<br>ZONED - PUD<br>4760 STAGECOACH ROAD<br>COLORADO SPRINGS, CO             | 93. ALEXANDER SCOTT E<br>ZONED - PUD<br>5395 OLD STAGECOACH ROAD<br>COLORADO SPRINGS, CO         | 111. VILIESIS TRUST<br>ZONED - PUD<br>5292 GOLD RUN COURT<br>COLORADO SPRINGS, CO           | 129. ST AUBYN JARED<br>ZONED - PUD<br>15233 QUARTZ CREEK DRIVE<br>COLORADO SPRINGS, CO            | 147. WATSON RANDY<br>ZONED - PUD<br>15520 WINDING TRAIL ROAD<br>COLORADO SPRINGS, CO               |
| 5. ALLAN NEAL A<br>ZONED - PUD<br>14425 MILLHAVEN PLACE<br>COLORADO SPRINGS, CO                 | 23. MCILRATH WILLIAM F TRUSTEE<br>ZONED - RR-5<br>6010 CONNAUGHT DRIVE<br>COLORADO SPRINGS, CO       | 41. SMITH AARON<br>ZONED - PUD<br>6590 OLD STAGECOACH ROAD<br>COLORADO SPRINGS, CO            | 59. BR&C INC<br>ZONED - RR-5<br>30-11-65<br>COLORADO SPRINGS, CO                                    | 76. JONES CHRISTOPHER P<br>ZONED - PUD<br>4850 STAGECOACH ROAD<br>COLORADO SPRINGS, CO        | 94. CLAWSON MATTHEW R<br>ZONED - PUD<br>5355 OLD STAGECOACH ROAD<br>COLORADO SPRINGS, CO         | 112. SHOPTAUGH GLENN MARK<br>ZONED - PUD<br>5261 GOLD RUN COURT<br>COLORADO SPRINGS, CO     | 130. MOMBER SIMON R<br>ZONED - PUD<br>15232 QUARTZ CREEK DRIVE<br>COLORADO SPRINGS, CO            | 148. MARSHALL KARLYE<br>ZONED - PUD<br>15480 BILLINGS COURT<br>COLORADO SPRINGS, CO                |
| 6. ALEX & AUTUMM SIMPSON<br>ZONED - PUD<br>14385 MILLHAVEN PLACE<br>COLORADO SPRINGS, CO        | 24. WAY MARGARET E<br>ZONED - RR-5<br>14820 BLACK FOREST ROAD<br>COLORADO SPRINGS, CO                | 42. HARRIS GEORGE D<br>ZONED - PUD<br>6670 OLD STAGECOACH ROAD<br>COLORADO SPRINGS, CO        | 60. CHEROKEE METROPOLITAN DISTRICT<br>ZONED - RR-5<br>30-11-65<br>COLORADO SPRINGS, CO              | 77. WALTERS MICHAEL A<br>ZONED - PUD<br>4910 STAGECOACH ROAD<br>COLORADO SPRINGS, CO          | 95. PLAISTOWE NORMAN H<br>ZONED - PUD<br>5315 OLD STAGECOACH ROAD<br>COLORADO SPRINGS, CO        | 113. VILLAGREE LLC<br>ZONED - PUD<br>5231 GOLD RUN COURT<br>COLORADO SPRINGS, CO            | 131. SHABE ERIC M<br>ZONED - PUD<br>15182 QUARTZ CREEK DRIVE<br>COLORADO SPRINGS, CO              | 149. VANCE ERZA G<br>ZONED - PUD<br>15450 BILLINGS COURT<br>COLORADO SPRINGS, CO                   |
| 7. MAITHILI VENKATACHALLAM<br>ZONED - PUD<br>14345 MILLHAVEN PLACE<br>COLORADO SPRINGS, CO      | 25. ABELL LIVING TRUST<br>ZONED - RR-5<br>6620 COUNTRY ESTATES LANE<br>COLORADO SPRINGS, CO          | 43. MCCGRATH DONALD T<br>ZONED - PUD<br>6750 OLD STAGECOACH ROAD<br>COLORADO SPRINGS, CO      | 61. SUNDANCE RANCH OF BLACK FOREST<br>ZONED - RR-5<br>HODGEN ROAD<br>COLORADO SPRINGS, CO           | 78. YOUNG MICHAEL J<br>ZONED - PUD<br>4915 STAGECOACH ROAD<br>COLORADO SPRINGS, CO            | 96. RAMPART ENTERPRISES INC<br>ZONED - PUD<br>5235 OLD STAGECOACH ROAD<br>COLORADO SPRINGS, CO   | 114. S&J TRUST<br>ZONED - PUD<br>5201 GOLD RUN COURT<br>COLORADO SPRINGS, CO                | 132. ZACHAR MICHAEL R<br>ZONED - PUD<br>15132 QUARTZ CREEK DRIVE<br>COLORADO SPRINGS, CO          | 150. PRI #2 LLC<br>ZONED - PUD<br>HIGHWAY 83<br>COLORADO SPRINGS, CO                               |
| 8. DULANEY KIMBERLY L<br>ZONED - PUD<br>14325 MILLHAVEN PLACE<br>COLORADO SPRINGS, CO           | 26. HERRON PATRICK J<br>ZONED - RR-5<br>6650 COUNTRY ESTATES LANE<br>COLORADO SPRINGS, CO            | 44. MIKUSKA ERIC<br>ZONED - RR-5<br>15645 TERRA RIDGE CIRCLE<br>COLORADO SPRINGS, CO          | 62. SUNDANCE RANCH OF BLACK FOREST<br>ZONED - RR-5<br>HODGEN ROAD<br>COLORADO SPRINGS, CO           | 79. DAY GREGORY<br>ZONED -PUD<br>4955 OLD STAGECOACH ROAD<br>COLORADO SPRINGS, CO             | 97. KELLY J PHELAN TRUST<br>ZONED - PUD<br>5155 OLD STAGECOACH ROAD<br>COLORADO SPRINGS, CO      | 115. CHAVEZ XAVIER D<br>ZONED - PUD<br>5141 GOLD RUN COURT<br>COLORADO SPRINGS, CO          | 133. HARVEY SETH A<br>ZONED - PUD<br>15032 QUARTZ CREEK DRIVE<br>COLORADO SPRINGS, CO             | 151. MCKENZIE J THOMAS<br>ZONED - PUD<br>15420 BILLINGS COURT<br>COLORADO SPRINGS, CO              |
| 9. SMITH PAUL R<br>ZONED - PUD<br>14265 MILLHAVEN PLACE<br>COLORADO SPRINGS, CO                 | 27. ABELL LIVING TRUST<br>ZONED - RR-5<br>6620 COUNTRY ESTATES LANE<br>COLORADO SPRINGS, CO          | 45. GARD DIANA M<br>ZONED - RR-5<br>6835 MONTY PLACE<br>COLORADO SPRINGS, CO                  | 63. SHELL JAMES R II<br>ZONED - RR-5<br>15550 FARRAR ROAD<br>COLORADO SPRINGS, CO                   | 80. RZONCA THADDEUS<br>ZONED - PUD<br>4995 OLD STAGECOACH ROAD<br>COLORADO SPRINGS, CO        | 98. WINGO JAMES D<br>ZONED - PUD<br>5115 OLD STAGECOACH ROAD<br>COLORADO SPRINGS, CO             | 116. DALY FAMILY TRUST<br>ZONED - PUD<br>14911 LONGWALL DRIVE<br>COLORADO SPRINGS, CO       | 134. PITTS JOHN<br>ZONED - PUD<br>4661 HIGH FOREST ROAD<br>COLORADO SPRINGS, CO                   | 152. JONE LUCAS<br>ZONED - PUD<br>15419 BILLINGS COURT<br>COLORADO SPRINGS, CO                     |
| 10. ANDERSON MATTHEW P<br>ZONED - PUD<br>5025 VESSEY ROAD<br>COLORADO SPRINGS, CO               | 28. COPPOCK AARON O<br>ZONED - RR-5<br>6680 COUNTRY ESTATES LANE<br>COLORADO SPRINGS, CO             | 46. FRANKOVIS JESSE J<br>ZONED - RR-5<br>6840 MONTY PLACE<br>COLORADO SPRINGS, CO             | 64. SHELL JAMES R II<br>ZONED - RR-5<br>15550 FARRAR ROAD<br>COLORADO SPRINGS, CO                   | 81. SIDWELL DUSTIN JEFFREY<br>ZONED - PUD<br>4990 OLD STAGECOACH ROAD<br>COLORADO SPRINGS, CO | 99. KIM MICHAEL SANG-HAK<br>ZONED - PUD<br>5075 OLD STAGECOACH ROAD<br>COLORADO SPRINGS, CO      | 117. STIMPLE FAMILY LLLP<br>ZONED - PUD<br>14842 LONGWALL DRIVE<br>COLORADO SPRINGS, CO     | 135. LAVEZZO NICHOLAS J<br>ZONED - PUD<br>1601 HIGH FOREST ROAD<br>COLORADO SPRINGS, CO           | 153. ROGER WILLIAM T<br>ZONED - PUD<br>15479 BILLINGS COURT<br>COLORADO SPRINGS, CO                |
| 11. ESPENLAUB ECTON<br>ZONED - PUD<br>4985 VESSEY ROAD<br>COLORADO SPRINGS, CO                  | 29. MACEDO JUAN H LOMEIL<br>ZONED - RR-5<br>6710 COUNTRY ESTATES LANE<br>COLORADO SPRINGS, CO        | 47. OLIVAS SOCORRO J<br>ZONED - RR-5<br>6905 ALPACA HEIGHTS<br>COLORADO SPRINGS, CO           | 65. BREWER GEORGE F II<br>ZONED - PUD<br>15501 OPEN SKY WAY<br>COLORADO SPRINGS, CO                 | 82. SPARKS DUSTIN R<br>ZONED - PUD<br>5070 OLD STAGECOACH ROAD<br>COLORADO SPRINGS, CO        | 100. TEUSCHER KURT<br>ZONED - PUD<br>5035 OLD STAGECOACH ROAD<br>COLORADO SPRINGS, CO            | 118. CREPS DARREL E III<br>ZONED - PUD<br>14912 LONGWALL DRIVE<br>COLORADO SPRINGS, CO      | 136. HIGH FOREST RANCH HOMEOWNERS<br>ZONED - PUD<br>4541 HIGH FOREST ROAD<br>COLORADO SPRINGS, CO | 154. DOMBROWSKI MICHAEL J<br>ZONED - PUD<br>3680 STAGECOACH ROAD<br>COLORADO SPRINGS, CO           |
| 12. DILLINGHAM MICHAEL V<br>ZONED - RR-5<br>14498 HOLMES ROAD<br>COLORADO SPRINGS, CO           | 30. SOMBRIC WAYNE S<br>ZONED - RR-5<br>6740 COUNTRY ESTATES LANE<br>COLORADO SPRINGS, CO             | 48. HILL DOUGLAS E<br>ZONED - RR-5<br>6910 ALPACA HEIGHTS<br>COLORADO SPRINGS, CO             | 66. MONTGOMERY MONTIE C<br>ZONED - PUD<br>15547 OPEN SKY WAY<br>COLORADO SPRINGS, CO                | 83. SPILLERS STEVEN HOWARD<br>ZONED - PUD<br>5150 OLD STAGECOACH ROAD<br>COLORADO SPRINGS, CO | 101. DOWNS BRADLEY JAMES<br>ZONED - PUD<br>55305 OLD STAGECOACH ROAD<br>COLORADO SPRINGS, CO     | 119. CAIN JASON<br>ZONED - PUD<br>14982 LONGWALL DRIVE<br>COLORADO SPRINGS, CO              | 137. SALGADO PAUL R<br>ZONED - PUD<br>4415 HIDDEN ROCK ROAD<br>COLORADO SPRINGS, CO               | 155. ROBIN SCOTT BROWN LIVING TRUST<br>ZONED - PUD<br>3590 STAGECOACH ROAD<br>COLORADO SPRINGS, CO |
| 13. THOMAS JOHN K<br>ZONED - RR-5<br>14490 HOLMES ROAD<br>COLORADO SPRINGS, CO                  | 31. HOPSON SEAN<br>ZONED - RR-5<br>6770 COUNTRY ESTATES LANE<br>COLORADO SPRINGS, CO                 | 49. WHITNEY CHRISTOPHER D<br>ZONED - RR-5<br>16485 BLACK FOREST ROAD<br>COLORADO SPRINGS, CO  | 67. RANGER CANDACE S LIVING TRUST<br>ZONED - PUD<br>15593 OPEN SKY WAY<br>COLORADO SPRINGS, CO      | 84. PECK JAMES D<br>ZONED - PUD<br>5230 OLD STAGECOACH ROAD<br>COLORADO SPRINGS, CO           | 102. KAVERMAN JOSEPH A<br>ZONED - PUD<br>5215 OLD STAGECOACH ROAD<br>COLORADO SPRINGS, CO        | 120. DICKEY MICHAEL R<br>ZONED - PUD<br>5021 GOLD RUN CT<br>COLORADO SPRINGS, CO            | 138. JOHNSON GREGG<br>ZONED - PUD<br>4365 HIDDEN ROCK ROAD<br>COLORADO SPRINGS, CO                | 156. JACKOWIAK RYAN<br>ZONED - PUD<br>3770 STAGECOACH ROAD<br>COLORADO SPRINGS, CO                 |
| 14. ERNST CHARLES H<br>ZONED - RR-5<br>14410 HOMES ROAD<br>COLORADO SPRINGS, CO                 | 32. MCKINLEY DAVID R<br>ZONED - RR-5<br>14920 QUAIL RUN ROAD<br>COLORADO SPRINGS, CO                 | 50. BERENS MARK E<br>ZONED - RR-5<br>6850 HODGEN ROAD<br>COLORADO SPRINGS, CO                 | 68. JANNELLE EVA ALLEN REVOCABLE TRUST<br>ZONED - PUD<br>15639 OPEN SKY WAY<br>COLORADO SPRINGS, CO | 85. WELLER ERICH G<br>ZONED - PUD<br>5310 OLD STAGECOACH ROAD<br>COLORADO SPRINGS, CO         | 103. PIEPER RANDALL L<br>ZONED - PUD<br>5125 OLD STAGECOACH ROAD<br>COLORADO SPRINGS, CO         | 121. LIDDIARD JEREMY<br>ZONED - PUD<br>5013 GOLD RUN CT<br>COLORADO SPRINGS, CO             | 139. ROMANS LIVING TRUST<br>ZONED - PUD<br>4315 HIDDEN ROCK ROAD<br>COLORADO SPRINGS, CO          | 157. BALSICK LUKE A<br>ZONED - PUD<br>3860 STAGECOACH ROAD<br>COLORADO SPRINGS, CO                 |
| 15. WAUGH JOSHUA T<br>ZONED - RR-5<br>14445 HOLMES ROAD<br>COLORADO SPRINGS, CO                 | 33. WINNINGHAM AARON JASON<br>ZONED - RR-5<br>14940 QUAIL RUN ROAD<br>COLORADO SPRINGS, CO           | 51. MOLES JUSTIN<br>ZONED - RR-5<br>16550 BLACK FOREST ROAD<br>COLORADO SPRINGS, CO           | 69. STUDHOLME FAMILY TRUST<br>ZONED - PUD<br>15685 OPEN SKY WAY<br>COLORADO SPRINGS, CO             | 86. LAM TU T<br>ZONED - PUD<br>5390 OLD STAGECOACH ROAD<br>COLORADO SPRINGS, CO               | 104. SHECTER TRUST<br>ZONED - PUD<br>15291 LONGWALL DRIVE<br>COLORADO SPRINGS, CO                | 122. MILLER SCOTT G<br>ZONED - PUD<br>5012 GOLD RUN CT<br>COLORADO SPRINGS, CO              | 140. RYAN CHRISTOPHER J<br>ZONED - PUD<br>4265 HIDDEN ROCK ROAD<br>COLORADO SPRINGS, CO           | 158. HIMES ELMER S<br>ZONED - PUD<br>3950 STAGECOACH ROAD<br>COLORADO SPRINGS, CO                  |
| 16. HOFFPAUIR DAN W JR<br>ZONED - RR-5<br>14495 HOMES ROAD<br>COLORADO SPRINGS, CO              | 34. LYNDE ROBERT A<br>ZONED - RR-5<br>15015 TERRA RIDGE CIRCLE<br>COLORADO SPRINGS, CO               | 52. MUNSON BRANDON J<br>ZONED - RR-5<br>16710 BLACK FOREST ROAD<br>COLORADO SPRINGS, CO       | 70. MAHER FAMILY REVOC LIVING TRUST<br>ZONED - PUD<br>4961 HIGH FOREST ROAD<br>COLORADO SPRINGS, CO | 87. LUERS BEACH LLC<br>ZONED - PUD<br>5470 OLD STAGECOACH ROAD<br>COLORADO SPRINGS, CO        | 105. CHRISTOPHER MICHAEL MARSHALL<br>ZONED - PUD<br>15051 LONGWALL DRIVE<br>COLORADO SPRINGS, CO | 123. BRENNAN THOMAS LIVING TRUST<br>ZONED - PUD<br>5022 GOLD RUN CT<br>COLORADO SPRINGS, CO | 141. MARY CLAUDE F TRUSTEE<br>ZONED - PUD<br>4215 HIDDEN ROCK ROAD<br>COLORADO SPRINGS, CO        | 159. OTERO THEODAORE M III<br>ZONED - PUD<br>4040 STAGECOACH ROAD<br>COLORADO SPRINGS, CO          |
| 17. SELF BOB J<br>ZONED - RR-5<br>5910 VESSEY ROAD<br>COLORADO SPRINGS, CO                      | 35. SPLIT PINE RANCH LIVING TRUST<br>ZONED - RR-5<br>15385 BLACK FOREST ROAD<br>COLORADO SPRINGS, CO | 53. MILLER ROBERT S<br>ZONED - RR-5<br>6520 HODGEN ROAD<br>COLORADO SPRINGS, CO               | 71. STEPHENSON TRAVIS<br>ZONED - PUD<br>4901 HIGH FOREST ROAD<br>COLORADO SPRINGS, CO               | 88. GREENWOOD TAYLOR J<br>ZONED - PUD<br>5550 OLD STAGECOACH ROAD<br>COLORADO SPRINGS, CO     | 106. BECKER JACOB J<br>ZONED - PUD<br>5142 GOLD RUN COURT<br>COLORADO SPRINGS, CO                | 124. WINTER CHARLES C<br>ZONED - PUD<br>5082 GOLD RUN CT<br>COLORADO SPRINGS, CO            | 142. STREVELL MICHAEL W<br>ZONED - PUD<br>4165 HIDDEN ROCK ROAD<br>COLORADO SPRINGS, CO           | 160. HARRIS GUY MCALLISTER<br>ZONED - PUD<br>4130 STAGECOACH ROAD<br>COLORADO SPRINGS, CO          |
| 18. JONES INGRID L<br>ZONED - RR-5<br>5940 VESSEY ROAD<br>COLORADO SPRINGS, CO                  | 36. APODACA LESLIE E<br>ZONED - RR-5<br>15380 BLACK FOREST ROAD<br>COLORADO SPRINGS, CO              | 54. JOHN R SHANTZ & BELINDA S<br>ZONED - RR-5<br>16547 RIDGEBACK ROAD<br>COLORADO SPRINGS, CO |   | 89. LONG RUSSEL I<br>ZONED - PUD<br>5630 OLD STAGECOACH ROAD<br>COLORADO SPRINGS, CO          | 107. KEV PARTNERS LTD<br>ZONED - PUD<br>5172 GOLD RUN COURT<br>COLORADO SPRINGS, CO              | 125. THEOBARD CHARLES N<br>ZONED - PUD<br>4945 STAGECOACH ROAD<br>COLORADO SPRINGS, CO      | 143. GOULD TODD E<br>ZONED - PUD<br>4115 HIDDEN ROCK ROAD<br>COLORADO SPRINGS, CO                 |  |

COUNTY FILE NUMBER: SKP223

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| DRAWN BY: JAG   | JOB DATE: 3/1/2022 | BAR IS ONE INCH ON OFFICIAL DRAWINGS.      |
| APPROVED: PLS   | JOB NUMBER: 211030 | 0 1"                                       |
| CAD DATE: 9/15/2022   |                    | IF NOT ONE INCH, ADJUST SCALE ACCORDINGLY. |
| CAD FILE: J:\2021\211030\CAD\Drawgs\C\Sketch-Plan\ADJACENT-PROPERTY |                    |  |

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FLYING HORSE NORTH DEVELOPMENT, LLC.  
EL PASO COUNTY, COLORADO

FLYING HORSE NORTH SKETCH PLAN  
ADJACENT PROPERTY DATA OWNERS

SHEET  
SP.4

4

FLYING HORSE NORTH SKETCH PLAN

161. RED HORSE HILL LLC  
ZONED - PUD  
AUNDERTON GRV  
COLORADO SPRINGS, CO

162. WILKINSON SUZANNE ELIZABETH  
ZONED - PUD  
4540 FOXCHASE WAY  
COLORADO SPRINGS, CO

163. JOHNSON SAM CHRISTOPHER  
ZONED - PUD  
4580 FOXCHASE WAY  
COLORADO SPRINGS, CO

164. S&BT LIVING TRUST  
ZONED - PUD  
4660 FOXCHASE WAY  
COLORADO SPRINGS, CO

165. CURRAN LARRY DAVID  
ZONED - PUD  
4615 FOXCHASE WAY  
COLORADO SPRINGS, CO

166. LEE MARVIN  
ZONED - PUD  
4455 FOXCHASE WAY  
COLORADO SPRINGS, CO

167. JASMIN TREMBLAY REVOCABLE TRUST  
ZONED - PUD  
4415 FOXCHASE WAY  
COLORADO SPRINGS, CO

168. EVANS LIVING TRUST  
ZONED - PUD  
14190 MARBLE ARCH COURT  
COLORADO SPRINGS, CO

169. TAYLOR CHRISTINA MARIE  
ZONED - PUD  
4535 FOXCHASE WAY  
COLORADO SPRINGS, CO

170. LUTHY ROBERT EDWARD  
ZONED - PUD  
14250 FARNHAM ROYAL COURT  
COLORADO SPRINGS, CO

171. BEHNKEN CHAD L  
ZONED - PUD  
4735 FOXCHASE WAY  
COLORADO SPRINGS, CO

172. SWARTHOUT ANDREW T  
ZONED - PUD  
4740 FOXCHASE WAY  
COLORADO SPRINGS, CO

173. ERLING BRIAN F  
ZONED - PUD  
4780 FOXCHASE WAY  
COLORADO SPRINGS, CO

174. ARORA PRATHEEP  
ZONED - PUD  
14285 FARNHAM ROYAL COURT  
COLORADO SPRINGS, CO

175. ROSENBAUM DAVID A REVOC TRUST  
ZONED - PUD  
14585 MILLHAVEN PLACE  
COLORADO SPRINGS, CO

176. KELLY LIVING TRUST  
ZONED - PUD  
4975 FOXCHASE WAY  
COLORADO SPRINGS, CO

177. FLEMING FAMILY LIVING TRUST  
ZONED - PUD  
14505 MILLHAVEN PLACE  
COLORADO SPRINGS, CO

178. LONGHORNS 07 TURST  
ZONED - PUD  
14550 MILLHAVEN PLACE  
COLORADO SPRINGS, CO

179. KROEKER KARL  
ZONED - PUD  
14510 MILLHAVEN PLACE  
COLORADO SPRINGS, CO

180. COLOSSEE PARTNERS LLLP  
ZONED - PUD  
14470 MILLHAVEN PLACE  
COLORADO SPRINGS, CO

181. SEDDON JOHN TA  
ZONED - PUD  
14390 MILLHAVEN PLACE  
COLORADO SPRINGS, CO

182. MEDRICK JAMES G  
ZONED - PUD  
14350 MILLHAVEN PLACE  
COLORADO SPRINGS, CO

183. JAIN RUPESH  
ZONED - PUD  
14320 MILLHAVEN PLACE  
COLORADO SPRINGS, CO

184. KLAIBER LIVING TRUST  
ZONED - PUD  
14230 MILLHAVEN PLACE  
COLORADO SPRINGS, CO

185. SEXTON KENNETH R  
ZONED - PUD  
5225 VESSEY ROAD  
COLORADO SPRINGS, CO

186. POPE MARK S  
ZONED - PUD  
5265 VESSEY ROAD  
COLORADO SPRINGS, CO

187. ALDER FAMILY TRUST  
ZONED - PUD  
5345 VESSEY ROAD  
COLORADO SPRINGS, CO

188. LNB FAMILY TRUST  
ZONED - PUD  
5270 VESSEY ROAD  
COLORADO SPRINGS, CO

189. RAYMOND CHARLES DENT JR.  
ZONED - PUD  
5230 VESSEY ROAD  
COLORADO SPRINGS, CO

190. KOSZEWNIK JOHN JOSEPH  
ZONED - PUD  
5190 VESSEY ROAD  
COLORADO SPRINGS, CO

191. ENEA STEVEN A  
ZONED - PUD  
14150 MILLHAVEN PLACE  
COLORADO SPRINGS, CO

192. KARL C & DAWN M FINDLEY  
ZONED - PUD  
5070 VESSEY ROAD  
COLORADO SPRINGS, CO

193. MURPHY ROBERT C JR  
ZONED - PUD  
5065 VESSEY ROAD  
COLORADO SPRINGS, CO

194. HAWKINS JOSEPH C JR  
ZONED - PUD  
14450 HOLMES ROAD  
COLORADO SPRINGS, CO

195. KRISTY MICHAEL H  
ZONED - RR-5  
14350 HOLMES ROAD  
COLORADO SPRINGS, CO

196. GARLICK JEFFREY  
ZONED - RR-5  
14320 HOLMES ROAD  
COLORADO SPRINGS, CO

197. STELZEL DANIEL M  
ZONED - RR-5  
14290 HOLMES ROAD  
COLORADO SPRINGS, CO

198. MCGOWAN PATRICK J JR  
ZONED - RR-5  
14355 HOLMES ROAD  
COLORADO SPRINGS, CO

199. WANTY LISA M  
ZONED - RR-5  
6060 VESSEY ROAD  
COLORADO SPRINGS, CO

200. HAYES MARK G  
ZONED - RR-5  
6090 VESSEY ROAD  
COLORADO SPRINGS, CO

201. DOLES THOMAS ALBERT  
ZONED - RR-5  
6130 VESSEY ROAD  
COLORADO SPRINGS, CO

202. ELLEN KLEIN LIVING TRUST  
ZONED - PUD  
6180 VESSEY ROAD  
COLORADO SPRINGS, CO

203. BRADBURY DAVID J  
ZONED - PUD  
6220 VESSEY ROAD  
COLORADO SPRINGS, CO

204. STEWART ANTHONY NEIL  
ZONED - RR-5  
14450 PINE CREST DRIVE  
COLORADO SPRINGS, CO

205. CHAMBERS REVOCABLE TRUST  
ZONED - RR-5  
6065 CONNAUGHT DRIVE  
COLORADO SPRINGS, CO

206. CARTER THOMAS J  
ZONED - RR-5  
6125 CONNAUGHT DRIVE  
COLORADO SPRINGS, CO

207. MOREAU WILLIAM J  
ZONED - RR-5  
6185 CONNAUGHT DRIVE  
COLORADO SPRINGS, CO3

208. MOREAU WILLIAM J  
ZONED - RR-5  
6245 CONNAUGHT DRIVE  
COLORADO SPRINGS, CO

209. RODAS PETER G  
ZONED - RR-5  
6305 CONNAUGHT DRIVE  
COLORADO SPRINGS, CO

210. DAWSON FAMILY TRUST  
ZONED - RR-5  
6070 CONNAUGHT DRIVE  
COLORADO SPRINGS, CO

211. PALAZZARI ANTHONY A  
ZONED - RR-5  
6250 CONNAUGHT DRIVE  
COLORADO SPRINGS, CO

212. TRUMP CAROLYN D  
ZONED - PUD  
6370 CONNAUGHT DRIVE  
COLORADO SPRINGS, CO

213. CORBETT NORMAN  
ZONED - RR-5  
6745 COUNTY ESTATES LANE  
COLORADO SPRINGS, CO

214. BAHR JACOB  
ZONED - RR-5  
6818 MARSHBERN COURT  
COLORADO SPRINGS, CO

215. WESTOVER HOMES LLC  
ZONED - RR-5  
6902 MARSHBERN COURT  
COLORADO SPRINGS, CO

216. WESTOVER HOMES LLC  
ZONED - RR-5  
6986 MARSHBERN COURT  
COLORADO SPRINGS, CO

217. WESTOVER HOMES LLC  
ZONED - RR-5  
7070 MARSHBERN COURT  
COLORADO SPRINGS, CO

218. ELLSWORTH FRANK F  
ZONED - RR-5  
15105 TERRA RIDGE CIRCLE  
COLORADO SPRINGS, CO

219. DENNIS REBECCA L  
ZONED - RR-5  
14915 QUAIL RUN ROAD  
COLORADO SPRINGS, CO

220. JAMES P REEG REVOCABLE TRUST  
ZONED - RR-5  
14935 QUAIL RUN ROAD  
COLORADO SPRINGS, CO

221. FELLAR DENNIS W  
ZONED - RR-5  
15095 TERRA RIDGE CIRCLE  
COLORADO SPRINGS, CO

222. HUTCHINS-VAN TASSEL LESLIE  
ZONED - RR-5  
15090 TERRA RIDGE CIRCLE  
COLORADO SPRINGS, CO

223. FERL DIANE F  
ZONED - RR-5  
15010 TERRA RIDGE CIRCLE  
COLORADO SPRINGS, CO

224. CHAFFEE GREGORY B  
ZONED - RR-5  
15650 TERRA RIDGE CIRCLE  
COLORADO SPRINGS, CO

225. PETERSON JEFFREY L  
ZONED - RR-5  
15610 TERRA RIDGE CIRCLE  
COLORADO SPRINGS, CO

226. MCLELLAN CHRISTOPHER S  
ZONED - RR-5  
15570 TERRA RIDGE CIRCLE  
COLORADO SPRINGS, CO

227. BARR RHONDA LYN  
ZONED - RR-5  
6915 MONTY PLACE  
COLORADO SPRINGS, CO

228. KHALIQI DAVID H  
ZONED - RR-5  
6985 MONTY PLACE  
COLORADO SPRINGS, CO

229. ANDREWS TODD  
ZONED - RR-5  
6990 MONTY PLACE  
COLORADO SPRINGS, CO

230. LEVY JOEL D  
ZONED - RR-5  
6950 MONTY PLACE  
COLORADO SPRINGS, CO

231. SANCHEZ LAISSA  
ZONED - RR-5  
6925 ALPACA HEIGHTS  
COLORADO SPRINGS, CO

232. ENGET AARON  
ZONED - RR-5  
6950 HODGEN ROAD  
COLORADO SPRINGS, CO

233. SAVAGE JORDAN L  
ZONED - RR-5  
6498 RALEIGH ROAD  
COLORADO SPRINGS, CO

234. CONNOLLY ANDREW  
ZONED - RR-5  
6442 RALEIGH ROAD  
COLORADO SPRINGS, CO

235. VOLK SETH K  
ZONED - RR-5  
6386 RALEIGH ROAD  
COLORADO SPRINGS, CO

236. GIBB RONALD JESSE  
ZONED - RR-5  
6387 RALEIGH ROAD  
COLORADO SPRINGS, CO

237. SAVAGE JORDAN L  
ZONED - RR-5  
16587 RIDGEBACK ROAD  
COLORADO SPRINGS, CO

238. BISHOP BARBARA K  
ZONED - RR-5  
16755 THOMPSON ROAD  
COLORADO SPRINGS, CO

239. DUNSTON MATTHEW W  
ZONED - RR-5  
5525 HODGEN ROAD  
COLORADO SPRINGS, CO

240. LAVALLEY BRANDON DALE  
ZONED - RR-5  
5735 HODGEN ROAD  
COLORADO SPRINGS, CO

241. STEARNS KRYSTAL  
ZONED - RR-5  
HODGEN ROAD  
COLORADO SPRINGS, CO

242. STEARNS KRYSTAL  
ZONED - RR-5  
FARRAR DRIVE  
COLORADO SPRINGS, CO

243. HARVEY TINA MARIE  
ZONED - RR-5  
15975 FARRAR DRIVE  
COLORADO SPRINGS, CO

244. HARVEY CAROLYN C  
ZONED - RR-5  
15502 OPEN SKY WAY  
COLORADO SPRINGS, CO

245. ROEHRICH DN FAMILY TRUST  
ZONED - RR-5  
15548 OPEN SKY WAY  
COLORADO SPRINGS, CO

246. JAMES F BREGLIO LIVING TRUST  
ZONED - RR-5  
15594 OPEN SKY WAY  
COLORADO SPRINGS, CO

247. CARPER CHRISTOPHER  
ZONED - RR-5  
15686 OPEN SKY WAY  
COLORADO SPRINGS, CO

248. COYLE JOHN MORGAN LIVING TRUST  
ZONED - RR-5  
15778 OPEN SKY WAY  
COLORADO SPRINGS, CO

249. JONES CHARLES D  
ZONED - RR-5  
4781 SECLUDED CREEK COURT  
COLORADO SPRINGS, CO

250. SELVA MICHAEL D  
ZONED - RR-5  
4691 SECLUDED CREEK COURT  
COLORADO SPRINGS, CO

251. PRIBBLE FAMILY LIVING TRUST  
ZONED - RR-5  
4601 SECLUDED CREEK COURT  
COLORADO SPRINGS, CO

252. CHAMBERS MARK L  
ZONED - RR-5  
4782 HIGH FOREST ROAD  
COLORADO SPRINGS, CO

253. MURROW RICHARD C TRUST  
ZONED - RR-5  
4722 HIGH FOREST ROAD  
COLORADO SPRINGS, CO

254. MOORE DAVID S  
ZONED - RR-5  
4662 HIGH FOREST ROAD  
COLORADO SPRINGS, CO

255. CIABARRA JAIMIE K  
ZONED - RR-5  
4602 HIGH FOREST ROAD  
COLORADO SPRINGS, CO

256. VAN AUKEN LIVING TRUST  
ZONED - RR-5  
4715 HIDDEN ROCK ROAD  
COLORADO SPRINGS, CO

257. BRAY THEODORE C  
ZONED - RR-5  
4482 HIGH FOREST ROAD  
COLORADO SPRINGS, CO

258. CICCONE LYNDA M  
ZONED - RR-5  
4481 HIGH FOREST ROAD  
COLORADO SPRINGS, CO

259. CICCONE LYNDA M  
ZONED - RR-5  
4481 HIGH FOREST ROAD  
COLORADO SPRINGS, CO

260. STONESTREET JOHN B  
ZONED - RR-5  
4515 HIDDEN ROCK ROAD  
COLORADO SPRINGS, CO

261. OLIVIAS RAYMOND B  
ZONED - RR-5  
4301 HIGH FOREST ROAD  
COLORADO SPRINGS, CO

262. SUTHERLAND STEPHEN ARTHUR  
ZONED - RR-5  
4460 HIDDEN ROCK ROAD  
COLORADO SPRINGS, CO

263. WEBER CHARLES L  
ZONED - RR-5  
4360 HIDDEN ROCK ROAD  
COLORADO SPRINGS, CO

264. NELSON NORMAN D  
ZONED - RR-5  
4260 HIDDEN ROCK ROAD  
COLORADO SPRINGS, CO

265. JOHNSON TRACIE LIVING TRUST  
ZONED - RR-5  
4210 HIDDEN ROCK ROAD  
COLORADO SPRINGS, CO

266. BREWER STEVEN W  
ZONED - RR-5  
4160 HIDDEN ROCK ROAD  
COLORADO SPRINGS, CO

267. WOGEN BRYAN  
ZONED - RR-5  
4110 HIDDEN ROCK ROAD  
COLORADO SPRINGS, CO

268. FRANZ CHRISTOPHER A  
ZONED - RR-5  
4010 HIDDEN ROCK ROAD  
COLORADO SPRINGS, CO

269. PAESCHKE TRACY  
ZONED - RR-5  
4015 HIDDEN ROCK ROAD  
COLORADO SPRINGS, CO

270. OLSEN TODD A  
ZONED - RR-5  
3985 CANOPY COURT  
COLORADO SPRINGS, CO

271. DAHILL DEVIN  
ZONED - RR-5  
3955 CANOPY COURT  
COLORADO SPRINGS, CO

272. CASE FAMILY REVOC LIVING TRUST  
ZONED - RR-5  
15570 WINDING TRAIL ROAD  
COLORADO SPRINGS, CO

273. PARKER JEFFREY  
ZONED - RR-5  
5030 VESSEY ROAD  
COLORADO SPRINGS, CO

274. TERESA L FERGUSON LIVING TRUST  
ZONED - RR-5  
14145 MILLHAVEN PLACE  
COLORADO SPRINGS, CO

275. HOLLINGSWORTH KIMBERLEY  
ZONED - RR-5  
6625 COUNTRY ESTATES LANE  
COLORADO SPRINGS, CO

276. BURST DAVID K  
ZONED - RR-5  
6655 COUNTRY ESTATES LANE  
COLORADO SPRINGS, CO

277. PIRTLE CYNTHIA K  
ZONED - RR-5  
6685 COUNTRY ESTATES LANE  
COLORADO SPRINGS, CO

278. TWOMBLY MARCI  
ZONED - RR-5  
6715 COUNTRY ESTATES LANE  
COLORADO SPRINGS, CO

279. SUMPTER JUSTIN MICHAEL  
ZONED - RR-5  
15605 TERRA RIDGE CIRCLE  
COLORADO SPRINGS, CO

280. DAVIS MARK K  
ZONED - RR-5  
15565 TERRA RIDGE CIRCLE  
COLORADO SPRINGS, CO

SCOTT W ANDREWS  
PO BOX 158  
USAF ACADEMY, CO 80840

CHRISTOPHER A BOWMAN  
6425 CONNAUGHT DRIVE  
COLORADO SPRINGS, CO 80908

GREGORY B CHAFFEE  
15650 TERRA RIDGE CIRCLE  
COLORADO SPRINGS, CO 80908

AARON O COPPOCK  
6680 COUNTRY ESTATES LANE  
COLORADO SPRINGS, CO 80908

DERKSEN PROPERTIES LLC  
5491 PADDINGTON CREEK  
COLORADO SPRINGS, CO 80924

JOHN R AND BELINDA SHANTZ  
2651 19<sup>TH</sup> AVE  
KINGSBURG, CA 93631

DANIEL W LULCHUK  
6790 CONNAUGHT DRIVE  
COLORADO SPRINGS, CO 80908

ROBERT MELANSON  
14725 BLACK FOREST ROAD  
COLORADO SPRINGS, CO 80908

ERIC MIKUSKA  
15645 TERRA RIDGE CIRCLE  
COLORADO SPRINGS, CO 80908

ANTHONY A PALAZZARI  
6250 CONNAUGHT DRIVE  
COLORADO SPRINGS, CO 80908

PETER G RODAS  
6305 CONNAUGHT DRIVE  
COLORADO SPRINGS, CO 80908

ERIC J ROWE  
6670 CONNAUGHT DRIVE

COLORADO SPRINGS, CO 80908

RYE LLC  
16755 HAPPY LANDING  
MONUMENT, CO 80132

MARK A SLUTZ  
6730 CONNAUGHT DRIVE  
COLORADO SPRINGS, CO 80908

JEFFREY B SMITH  
13925 HIGHWAY 83  
COLORADO SPRINGS, CO 80921

BART W TIMM  
14695 BLACK FOREST ROAD  
COLORADO SPRINGS, CO 80908

MAYNARD MARCI L TWOMBLY  
6745 COUNTRY ESTATES LANE  
COLORADO SPRINGS, CO 80908

KEVIN J VIDER  
6365 CONNAUGHT DRIVE  
COLORADO SPRINGS, CO 80908

COUNTY FILE NUMBER: SKP223

DRAWN BY: JAG

JOB DATE: 3/1/2022

APPROVED: PLS

JOB NUMBER: 211030

CAD DATE: 9/15/2022

CAD FILE: J:\2021\211030\CAD\Draws\C\Sketch-Plan\ADJACENT-PROPERTY

BAR IS ONE INCH ON OFFICIAL DRAWINGS.

0 1"

IF NOT ONE INCH, ADJUST SCALE ACCORDINGLY.

| NO. | DATE | BY | REVISION DESCRIPTION |
|-----|------|----|----------------------|
|     |      |    |                      |
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FLYING HORSE NORTH DEVELOPMENT, LLC.  
EL PASO COUNTY, COLORADO

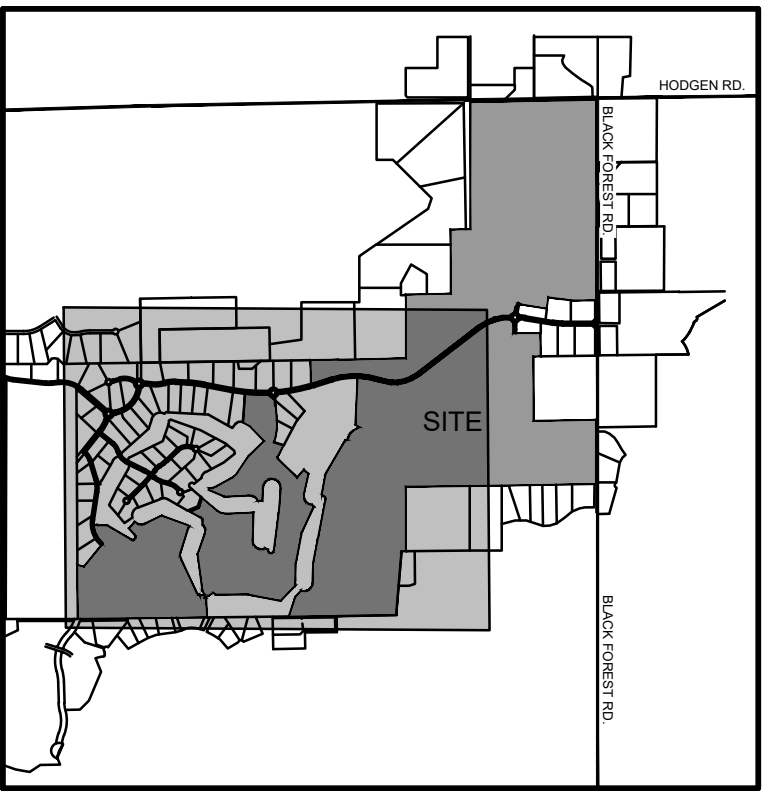
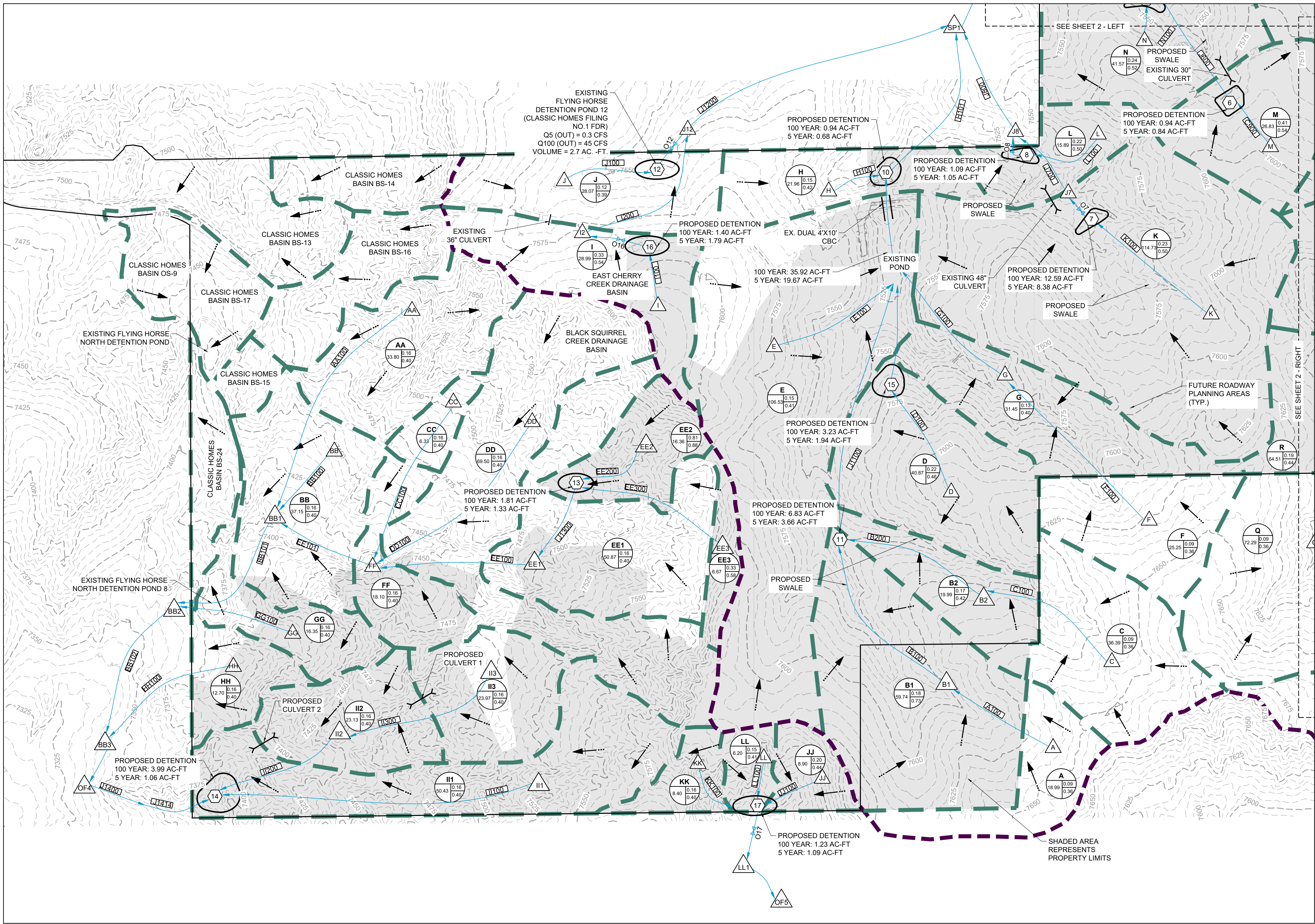
FLYING HORSE NORTH SKETCH PLAN  
ADJACENT PROPERTY DATA OWNERS

SHEET  
SP.5

5

HR GREEN Xrefs: xref-1-ARCH D101: BUBBLE-PLAN-EX-Parcels





VICINITY MAP

- LEGEND:**
- PROPOSED MAJOR CONTOUR
  - PROPOSED MINOR CONTOUR
  - EXISTING MAJOR CONTOUR
  - EXISTING MINOR CONTOUR
  - PROPOSED STORM DRAIN PIPE
  - EXISTING STORM DRAIN PIPE
  - PROPOSED DRAINAGE CHANNEL
  - PROPOSED ROAD
  - PROPERTY LINE
  - DIRECTIONAL FLOW ARROW
  - EMERGENCY OVERFLOW ARROW
  - EXISTING 100-YR FLOODWAY
  - EXISTING 100-YR FLOODPLAIN
  - PROPOSED 100-YR FLOODPLAIN
  - WATERSHED BOUNDARY
  - MAJOR BASIN LINE
  - 100YR ZONE A FLOODPLAIN
  - PROPOSED DETENTION LOCATION
  - POTENTIAL WATER QUALITY LOCATION
  - SWMM CONVEYANCE ELEMENT
  - PROPOSED PEAK FLOW RATE (CFS)
  - DESIGN POINT
  - PROPOSED BASIN LABEL
  - BASIN DESIGNATION
  - AREA (AC.)
  - C5
  - C100

**NOTES:**  
SEE SHEET 2 FOR DESIGN FLOWS



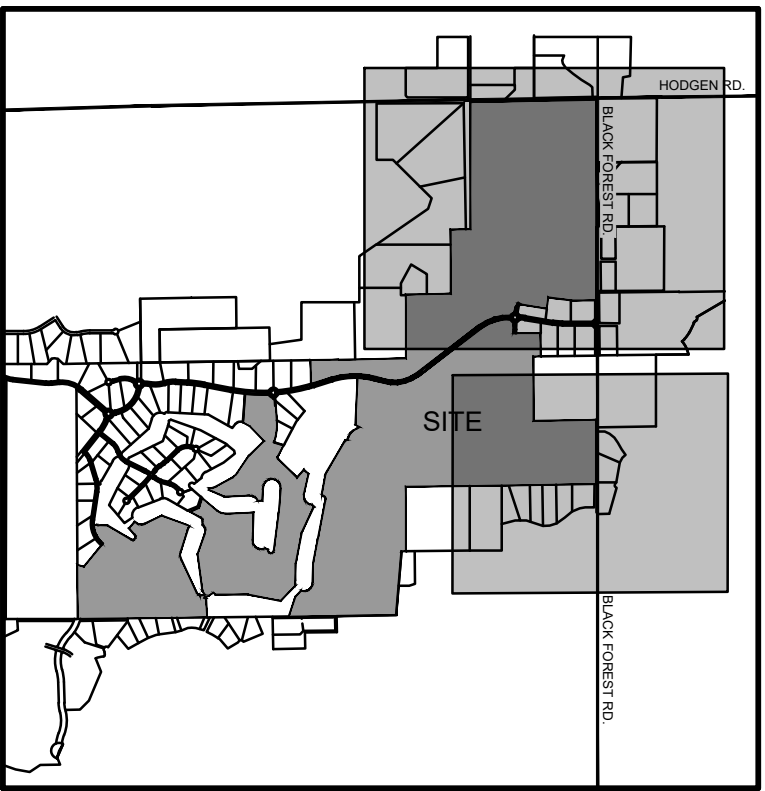
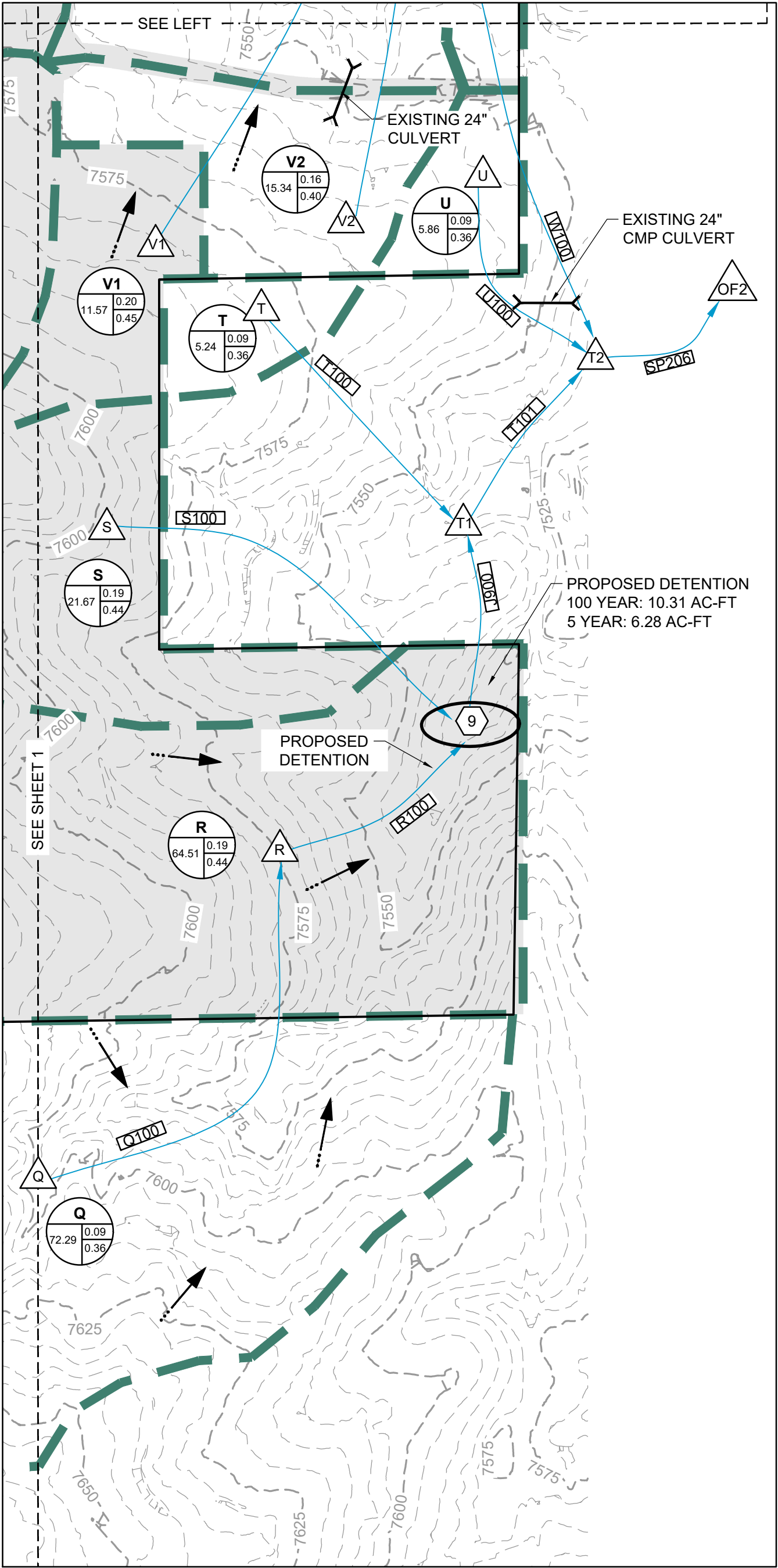
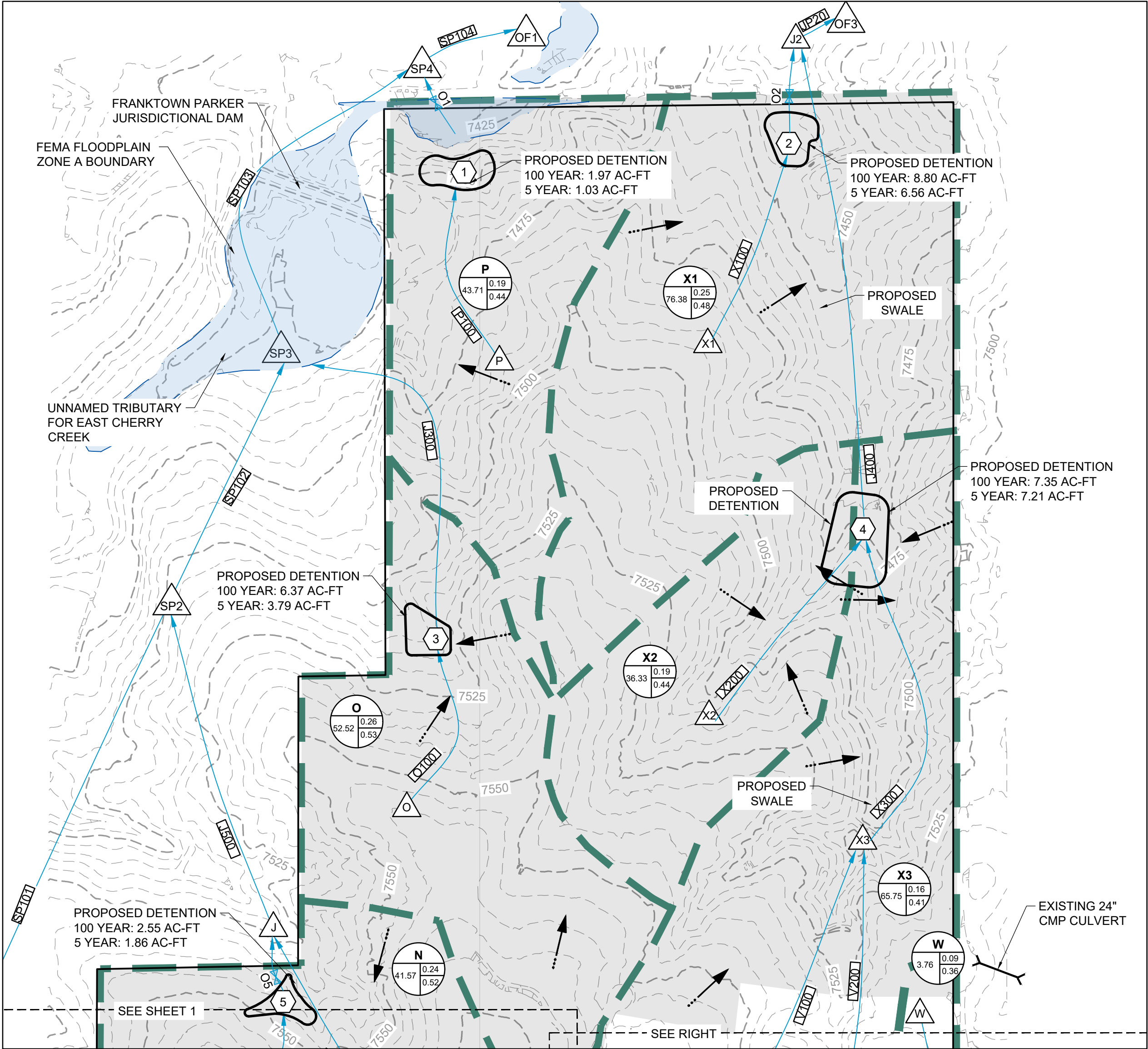
Job No.: 211030.01  
Prepared By: TBI  
Date: 9/9/2022

PROPOSED DRAINAGE BASINS

FIG.1



| BASIN | DESIGN POINT | 5 YEAR POST DEVELOPMENT | 100 YEAR POST DEVELOPMENT |
|-------|--------------|-------------------------|---------------------------|
| A     | A            | 20.84                   | 43.83                     |
| AA    | AA           | 39.23                   | 81.18                     |
| B1    | B1           | 66.93                   | 133.69                    |
| B2    | B2           | 17.99                   | 37.14                     |
| BB    | BB           | 40.62                   | 84.15                     |
|       | BB1          | 214.28                  | 483.72                    |
|       | BB2          | 229.61                  | 515.49                    |
|       | BB3          | 307.27                  | 646.46                    |
| C     | C            | 35.31                   | 75.28                     |
| CC    | CC           | 6.53                    | 13.57                     |
| D     | D            | 61.12                   | 117.38                    |
| DD    | DD           | 57.78                   | 122.41                    |
| E     | E            | 74.68                   | 157.91                    |
| EE1   | EE1          | 53.25                   | 156.68                    |
| EE2   | EE2          | 35.71                   | 63.62                     |
| EE3   | EE3          | 10.38                   | 19.33                     |
| F     | F            | 24.27                   | 51.63                     |
| FF    | FF           | 20.78                   | 330.28                    |
| G     | G            | 27.18                   | 108.76                    |
| GG    | GG           | 15.49                   | 32.48                     |
| H     | H            | 17.86                   | 37.80                     |
| HH    | HH           | 13.56                   | 28.16                     |
| I     | I            | 40.37                   | 78.06                     |
| II1   | II1          | 34.94                   | 74.39                     |
| II2   | II2          | 28.04                   | 116.26                    |
| II3   | II3          | 28.32                   | 58.65                     |
|       | IRR_J        | 114.18                  | 274.80                    |
|       | IRR_POND     | 243.77                  | 550.27                    |
| J     | J            | 24.45                   | 51.19                     |
| JJ    | JJ           | 11.49                   | 22.80                     |
| K     | K            | 200.94                  | 382.30                    |
| KK    | KK           | 8.14                    | 16.95                     |
| L     | L            | 15.97                   | 32.40                     |
| LL    | LL           | 7.36                    | 15.07                     |
| LL1   | LL1          | 0                       | 49.55                     |
| M     | M            | 46.54                   | 89.08                     |
| N     | N            | 73.48                   | 141.24                    |
| O     | O            | 63.86                   | 127.40                    |
|       | OF1          | 240.43                  | 705.93                    |
|       | OF2          | 104.34                  | 242.18                    |
|       | OF3          | 95.68                   | 271.49                    |
|       | OF4          | 307.27                  | 646.46                    |
|       | OF5          | 16.85                   | 49.55                     |
| P     | P            | 40                      | 82.83                     |
| Q     | Q            | 64.68                   | 137.80                    |
| R     | R            | 56.59                   | 253.86                    |
| S     | S            | 30.83                   | 58.96                     |
|       | SP1          | 189.85                  | 511.89                    |
|       | SP2          | 223.43                  | 618.35                    |
|       | SP3          | 212.45                  | 641.31                    |
|       | SP4          | 240.49                  | 706.05                    |
| T     | T            | 4.04                    | 8.68                      |
|       | T1           | 98.27                   | 228.33                    |
|       | T2           | 104.34                  | 242.18                    |
| U     | U            | 4.81                    | 10.51                     |
| V1    | V1           | 13.99                   | 27.67                     |
| V2    | V2           | 16.15                   | 33.25                     |
| W     | W            | 3.45                    | 7.46                      |
| X1    | X1           | 80.91                   | 163.27                    |
| X2    | X2           | 41.46                   | 82.46                     |
| X3    | X3           | 47.59                   | 100.73                    |



VICINITY MAP

LEGEND:

- PROPOSED MAJOR CONTOUR
- PROPOSED MINOR CONTOUR
- EXISTING MAJOR CONTOUR
- EXISTING MINOR CONTOUR
- PROPOSED STORM DRAIN PIPE
- EXISTING STORM DRAIN PIPE
- PROPOSED DRAINAGE CHANNEL
- PROPOSED ROAD
- PROPERTY LINE
- DIRECTIONAL FLOW ARROW
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- EXISTING 100-YR FLOODPLAIN
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- SWMM CONVEYANCE ELEMENT
- PROPOSED PEAK FLOW RATE (CFS)
- DESIGN POINT
- PROPOSED BASIN LABEL
- BASIN DESIGNATION
- AREA (AC.)

NOTES:



|              |           |
|--------------|-----------|
| Job No.:     | 211030.01 |
| Prepared By: | TBI       |
| Date:        | 9/9/2022  |

PROPOSED DRAINAGE BASINS

FIG.1