



505 ELKTON DRIVE COLORADO SPRINGS, CO 80907 PHONE (719) 531-5599 FAX (719) 531-5238

APPROVED **Engineering Department**

EPC Planning & Community Development Department

07/20/2021 3:52:14 PM dsdnijkamp



July 8, 2021 Revised: July 20, 2021

Classic Communities 2138 Flying Horse Club Drive Colorado Springs, CO 80921

Attn: Adam Doyle

Re: Pavement Recommendations - Revised

Hannah Ridge at Feathergrass, Filing No. 5

El Paso County, Colorado

Dear Mr. Doyle:

As requested, Entech Engineering, Inc. obtained samples of the pavement subgrade soils from the proposed roadways at the above referenced site. Laboratory testing was performed in order to determine the pavement support characteristics of the soil. This letter presents the results of the laboratory testing and pavement recommendations for the roadways.

Project Description

The project will consist of paving of sections of Electronic Drive, Equine Court, and Dapples Court in the Hannah Ridge at Feathergrass, Filing No. 5 subdivision in El Paso County, Colorado. Subsurface Soil Investigation and laboratory testing were performed to determine the pavement support characteristics on the soils. The general layout of the site is presented in the Test Boring Location Map in Figure 1.

Subgrade Conditions

A total of seven test borings were drilled along the roadways to depths of approximately 5 and 10 feet below the existing subgrade surface at the required sample frequency. The soils at the roadway subgrade depth consisted of clayey to very clayey sand fill (Soil Type 1) and clayey sand fill (Soil Type 2). The Test Boring Logs are presented in Appendix A. Sieve Analyses and Atterberg Limit testing were performed on subgrade soil samples obtained from the test borings for the purpose of classification. The percent passing the No. 200 sieve for the Type 1 soils ranged from approximately 36 to 47 percent and 21 to 35 percent for the Type 2 soils. The Type 3, 4, and 5 soils are beneath the subgrade influence zone.

The Type 1 soils classified as A-6, which commonly exhibit poor pavement support characteristics. The Type 2 soils classified as A-2-6 soils, which exhibit fair to good pavement support characteristics. Groundwater was not encountered in the test borings. Sulfate testing resulted in 0.00 percent soluble sulfate by weight, indicating a negligible potential for below grade concrete degradation due to sulfate attack.

Swell/Consolidation tests were performed on a majority of the subgrade soils due to their classification and plastic indexes. Swell tests on the soils resulted in volume changes of -0.4 to 0.7, which are below the levels in which mitigation is required. Mitigation for expansive soils is not required on this site.

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California Bearing Ratio (CBR) testing was performed on representative subgrade samples of the Type 1 and 2 materials to determine the support characteristics of the subgrade soils for the roadway sections. The results of the CBR testing, are presented in Appendix B and summarized as follows:

Soil Type 1 - Very Clayey Sand Fill	Soil Type 2 - Clayey Sand Fill
CBR 1	CBR 2
R @ 95% = 6.0	$R @ \overline{95\%} = 17.0$
R @ 90% = 17.0	R @ 90% = 40.0
Use $R = 17.0$ for design	Use $R = 40.0$ for design

Classification Testing		Classification Testing	
Liquid Limit	33	Liquid Limit	24
Plasticity Index	17	Plasticity Index	11
Percent Passing 200	46.9	Percent Passing 200	26.9
AASHTO Classification	A-6	AASHTO Classification	A-2-6
Group Index	4	Group Index	0
Unified Soils Classification	SC	Unified Soils Classification	SC

Pavement Design

CBR testing was used to determine pavement sections for the roadways. Pavement sections were determined utilizing El Paso County Pavement Design Criteria Manual. Electronic Drive and Equine Court east of Electronic Drive (approximately 250 feet) classify as Urban Local Roads, which used an 18k ESAL value of 292,000 for design purposes. Equine Court west of Electronic Drive and Dapples Court classify as Local Low Volume Roads, which used an 18K ESAL value of 36,500 for design purposes. Pavement sections were determined for asphalt on cement stabilized subgrade.

Design parameters used in the pavement analysis for the roadways are as follows:

Reliability	
Local Low Volume	80%
Local Residential	80%
Δρsi	
Local Low Volume	2.0
Local Residential	2.0
"R" Value Subgrade (Soil Type 1)	17.0
"R" Value Subgrade (Soil Type 2)	40.0
Resilient Modulus (Soil Type 1)	4,478 psi
Resilient Modulus (Soil Type 2)	9,497 psi
Hot Bituminous Pavement	0.44
Basecourse Subgrade	0.11

The pavement design calculations are presented in Appendix C. Pavement section alternatives for the roadway sections are presented below. Any additional grading may result in subgrade

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soils with different support characteristics. The following pavement sections should be reevaluated if additional grading is performed.

<u>Pavement Sections</u> <u>ESAL = 36,500 - Local Low Volume</u>

Soil Type 1

Alternative Asphalt (in) Cement Stabilized Subgrade (in)

1. Cement Stabilized Subgrade 4.0* 10.0

Soil Type 2

Alternative Asphalt (in) Cement Stabilized Subgrade (in)

1. Cement Stabilized Subgrade 4.0* 10.0

<u>Pavement Sections</u> <u>ESAL = 292,000 - Local Residential</u>

Soil Type 1

Alternative Asphalt (in) Cement Stabilized Subgrade (in)

1. Cement Stabilized Subgrade 4.0* 10.0

Soil Type 2

Alternative Asphalt (in) Cement Stabilized Subgrade (in)

1. Cement Stabilized Subgrade 4.0* 10.0

Mitigation

The El Paso County Engineering Criteria Manual requires mitigation of subgrade soils that have a swell of 2.0 percent or greater with a 200 pound per square foot surcharge. None of the swell tests exceeded the threshold. Mitigation of the subgrade soils is not required.

Roadway Construction - Cement Stabilized Subgrade

Prior to placement of the asphalt, the subgrade shall be stabilized by addition of cement to a depth of at least 10 inches. The amount of cement applied shall be 3.0 percent (by weight) of the subgrade's maximum dry density, as determined by the Standard Proctor Test (ASTM D-698), based on laboratory cement stabilization testing. The cement should be spread evenly on the subgrade surface and be thoroughly mixed into the subgrade over a 10-inch depth, such that a uniform blend of soil and cement is achieved. Prior to application or mixing of the cement, the upper 10-inches of subgrade should be thoroughly moisture conditioned to the soil's optimum water content, or as much as 2 percent more than the optimum water content as necessary to provide a compactable soil condition. Densification of the cement -stabilized subgrade should be completed to obtain a compaction of at least 95 percent of the subgrade maximum dry density as determined by the Standard Proctor Test (ASTM D-698). Satisfactory compaction of the subgrade shall occur within 90 minutes from the time of mixing the cement into the subgrade.

^{*}Minimum sections required per the El Paso County Engineering Criteria Manual.

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The following conditions shall be observed as part of the subgrade stabilization:

- Type I/II cement as supplied; a local supplier shall be used. All cement used for stabilization should come from the same source. If cement sources are changed, a new laboratory mix design should be completed.
- Moisture conditioning of the subgrade and/or mixing of the cement into the subgrade shall not occur when soil temperatures are below 40°F. Cement treated subgrades should be maintained at a temperature of 40°F or greater until the subgrade has been compacted as required.
- Cement placement, cement mixing, and compaction of the cement treated subgrade should be observed by a Soils Engineer. The Soils Engineer should complete in situ compaction tests and construct representative compacted specimens of the treated subgrade material for subsequent laboratory quality assurance testing.

If significant grading is performed, the soils at subgrade may change. Modification to the pavement sections should be evaluated after site grading is completed.

In addition to the above guidance, the asphalt, subgrade conditions, compaction of materials and roadway construction methods shall meet the El Paso County specifications.

We trust that this has provided you with the information you required. The pavement sections provided are based on general site soil types. If you have any questions or need additional information, please do not hesitate to contact us.

Reviewed by

Respectfully Submitted,

ENTECH ENGINEERING, INC.

Daniel P. Stegman

JCG/bs

Encl.

Entech Job No. 210984 AAprojects/2021/210984 pr

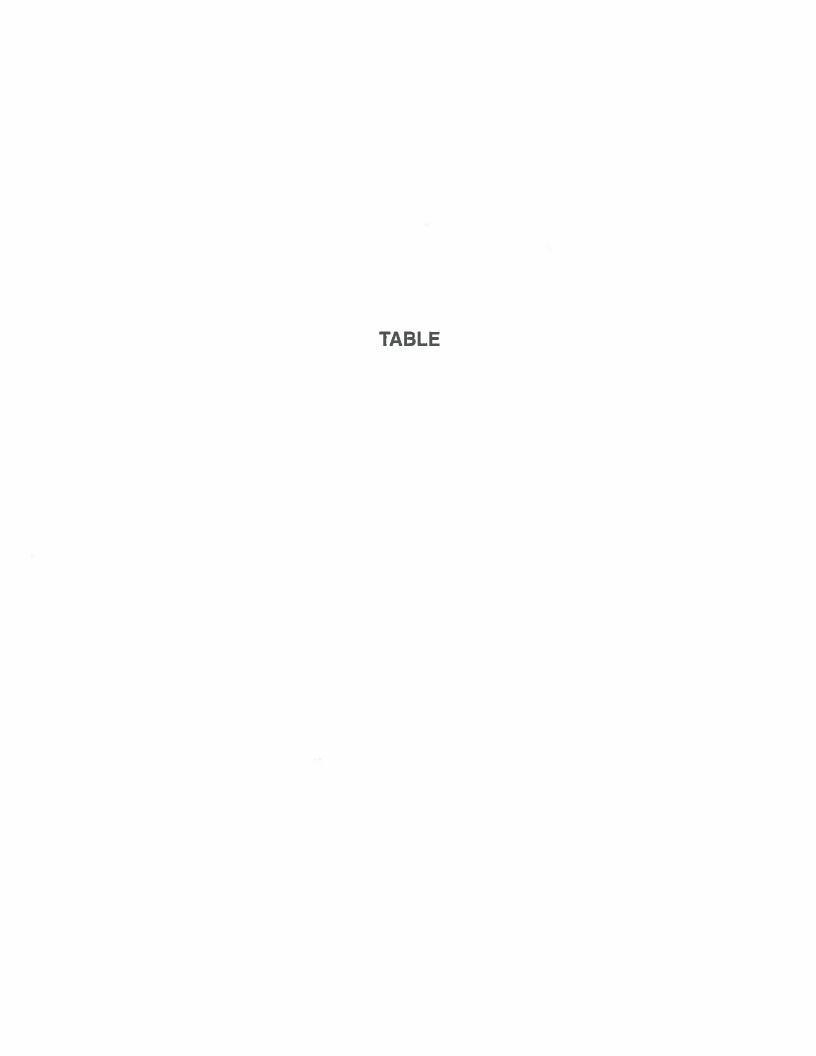


TABLE 1

SUMMARY OF LABORATORY TEST RESULTS

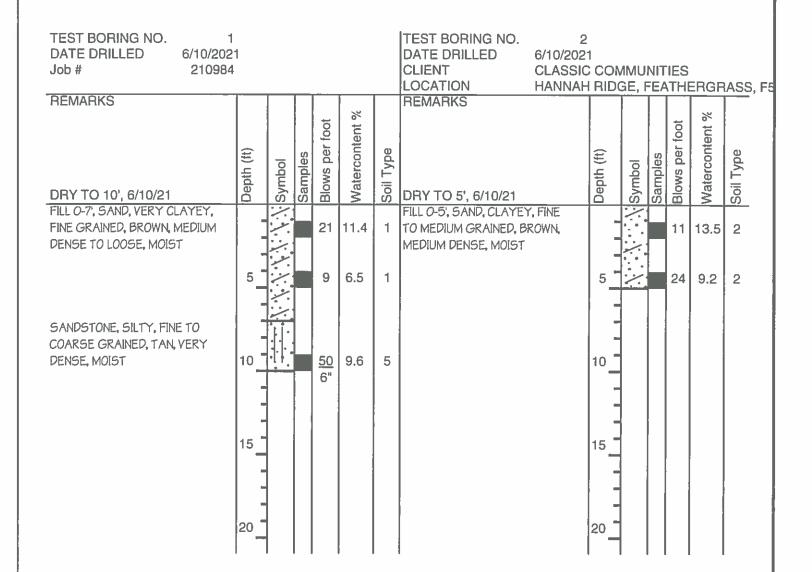
CLASSIC COMMUNITIES HANNAH RIDGE, FEATHERGRASS, F5 210984 CLIENT PROJECT JOB NO.

	SOIL DESCRIPTION	FILL, SAND, VERY CLAYEY	FILL, SAND, VERY CLAYEY	FILL, SAND, VERY CLAYEY	FILL, SAND, CLAYEY	SAND, SILTY	SAND, CLAYEY	SAND, VERY CLAYEY	SANDSTONE, SILTY					
UNIFIED	CLASSIFICATION	SC	SC	SC	SC	SC	SC	SC	SC	SC	SM	SC	SC	SM
SWELL	(%)	0.5	0.5	0.7		0.3	0.2	-0.2	0.1	0.0		-0.4	9.0	
AASHTO	CLASS.	A-6	A-6	A-6	A-2-6	A-2-6	A-2-6	A-2-6	A-2-6	A-2-6	A-2-4	A-2-6	A-6	A-2-4
SULFATE	(WT %)			00:00		00.00					00.00	00.00		
PLASTIC INDEX	(%)	17	16	20	11	17	11	12	16	12	ΝP	15	17	NP
LIQUID	(%)	33	33	39	24	38	31	28	32	29	NV	31	33	N N
PASSING NO. 200 SIEVE	(%)	46.9	36.3	36.1	26.9	21.6	31.4	24.8	34.6	20.8	23.8	23.5	45.7	23.0
DRY	(PCF)	115.2	115.7	114.5		94.6	97.1	95.1	98.9	113.0		92.6	94.1	
WATER	(%)	10.8	14.2	12.8		14.3	9.4	7.4	10.8	8.5		10.7	8.0	
DEPTH	(FT)	0-3	1-2	1-2	0-3	1-2	1-2	1-2	1-2	1-2	5	10	10	10
TEST	NO.	-	-	9	5	2	3	4	2	7	4	7	9	-
SOIL	TYPE	1, CBR	-	-	2, CBR	2	2	2	2	2	3	3	4	ഹ



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Name story Autor story Au	TB-1 TB-1	Constal (Constal (Con	TB-3 TB-3	The state of the s	*SOILS TRANSITIONS TO BE FIELD DETERMINED TB- APPROXIMATE TEST BORING LOCATION AND NUMBER







	TE	est Boring I	.og
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JOB NO.: 210984 FIG NO.:

A- 1

TEST BORING NO. ITEST BORING NO. 6/10/2021 DATE DRILLED DATE DRILLED 6/10/2021 Job# 210984 CLIENT **CLASSIC COMMUNITIES** LOCATION HANNAH RIDGE, FEATHERGRASS, FS REMARKS REMARKS Watercontent % Blows per foot Blows per foot Watercontent Type Depth (ft) Samples Samples Soil Type Symbol Symbol Depth (DRY TO 5', 6/10/21 DRY TO 5', 6/10/21 FILL O-5', SAND, CLAYEY, FINE FILL O-2', SAND, CLAYEY, FINE TO MEDIUM GRAINED, BROWN, 12 7.1 TO MEDIUM GRAINED, BROWN, 13 7.3 1 MEDIUM DENSE, MOIST MEDIUM DENSE, MOIST SAND, SILTY, FINE TO COARSE 311 13 8.2 2 GRAINED, TAN, MEDIUM DENSE, 12 8.0 3 MOIST. 10 10 15 15 20 20

(3)	ENTECH ENGINEERING, INC.
	505 ELKTON DRIVE COLORADO SPRINGS, COLORADO 80907

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JOB NO. 210984

FIG NO. A- 2

TEST BORING NO. TEST BORING NO. 6 DATE DRILLED 6/10/2021 DATE DRILLED 6/10/2021 Job# 210984 CLIENT **CLASSIC COMMUNITIES** LOCATION HANNAH RIDGE, FEATHERGRASS, F5 REMARKS REMARKS Blows per foot Blows per foot Watercontent Watercontent Type Depth (ft) Samples Samples Symbol Symbol Depth (DRY TO 5', 6/10/21 DRY TO 10', 6/10/21 FILL 0-5', SAND, CLAYEY, FINE FILL O-8', SAND, VERY CLAYEY, TO MEDIUM GRAINED, BROWN, 12 9.7 FINE GRAINED, BROWN, MEDIUM 15 12.3 1 MEDIUM DENSE TO LOOSE, DENSE TO DENSE, MOIST MOIST 5 9 9.9 2 5 30 6.4 1 SAND, VERY CLAYEY, FINE 10 GRAINED, TAN, MEDIUM DENSE. 10 27 7.3 MOIST 15 15 20 20



	TEST	F BORING LOG	
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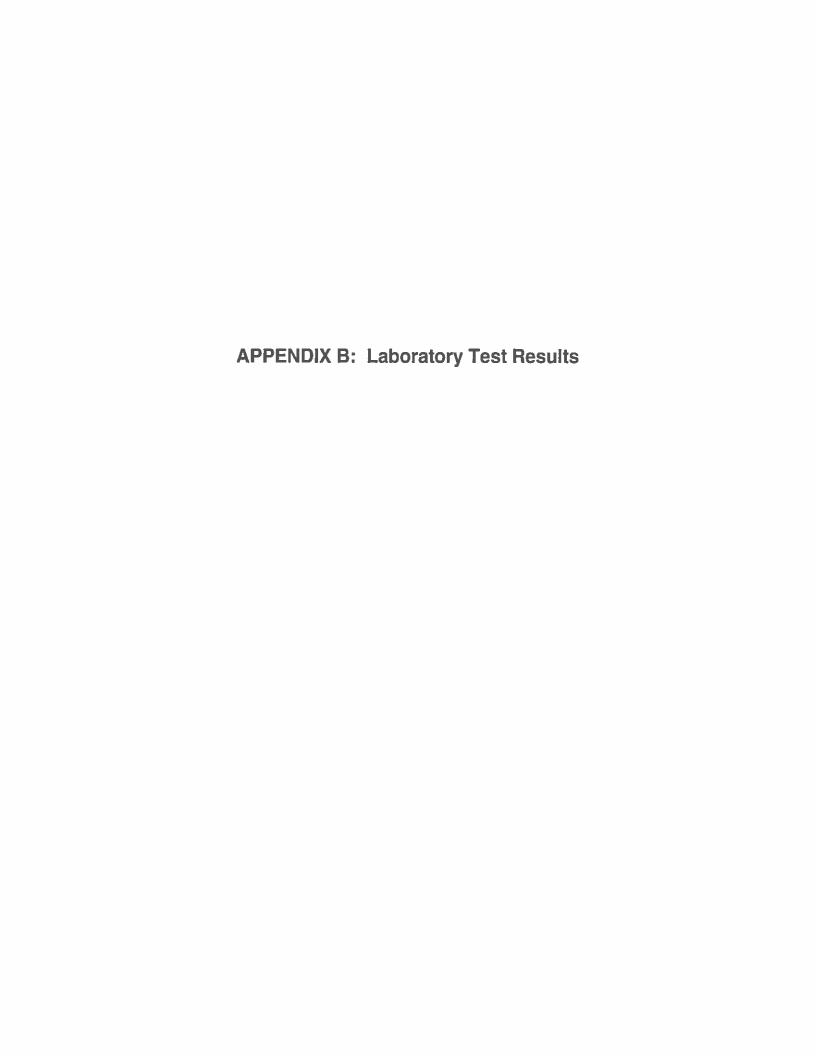
210984 FIG NO A- 3

TEST BORING NO. TEST BORING NO. 6/10/2021 DATE DRILLED DATE DRILLED Job# 210984 CLIENT **CLASSIC COMMUNITIES** HANNAH RIDGE, FEATHERGRASS, FS LOCATION REMARKS REMARKS Watercontent % Blows per foot Blows per foot Watercontent Soil Type Depth (ft) Soil Type Samples Samples Depth (ft) Symbol Symbol DRY TO 10', 6/10/21 FILL 0-9', SAND, CLAYEY, FINE TO MEDIUM GRAINED, BROWN, 25 6.3 2 MEDIUM DENSE, MOIST 5 16 14.3 2 5 10 13 12.0 SAND, CLAYEY, FINE GRAINED, 3 10 BROWN, MEDIUM DENSE, MOIST 15 15 20 20

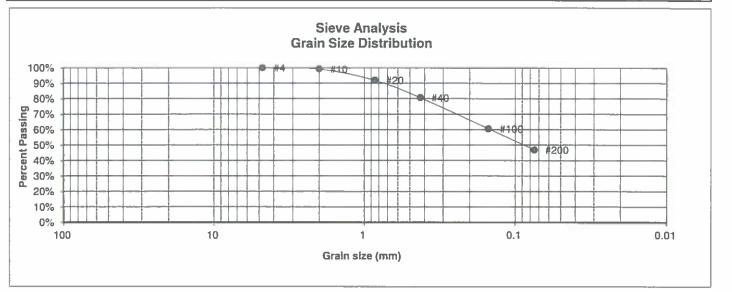
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	TES	T BORING LOG	
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JOB NO.: 210984 FIG NO.:



UNIFIED CLASSIFICATION	SC	CLIENT	CLASSIC COMMUNITIES
SOIL TYPE #	1, CBR	PROJECT	HANNAH RIDGE, FEATHERGRASS, F5
TEST BORING #	1	JOB NO.	210984
DEPTH (FT)	0-3	TEST BY	BL
AASHTO CLASSIFICATION	A-6	GROUP INDEX	4



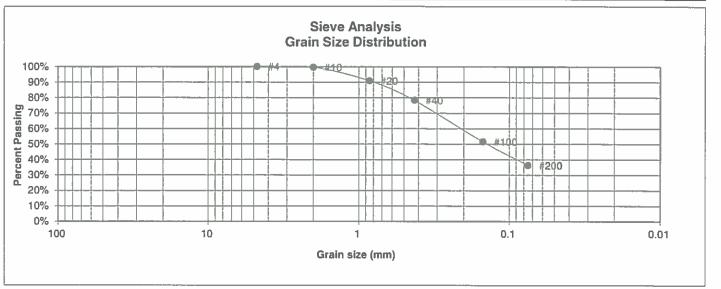
U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u>	Atterberg Limits Plastic Limit 16 Liquid Limit 33 Plastic Index 17
4	100.0%	Swell
10	99.2%	Moisture at start
20	91.9%	Moisture at finish
40	80.6%	Moisture increase
100	60.5%	Initial dry density (pcf)
200	46.9%	Swell (psf)



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210984 FIG NO.

UNIFIED CLASSIFICATION	SC	CLIENT	CLASSIC COMMUNITIES
SOIL TYPE #	1	PROJECT	HANNAH RIDGE, FEATHERGRASS, F5
TEST BORING #	1	JOB NO.	210984
DEPTH (FT)	1-2	TEST BY	BL
AASHTO CLASSIFICATION	A-6	GROUP INDEX	2



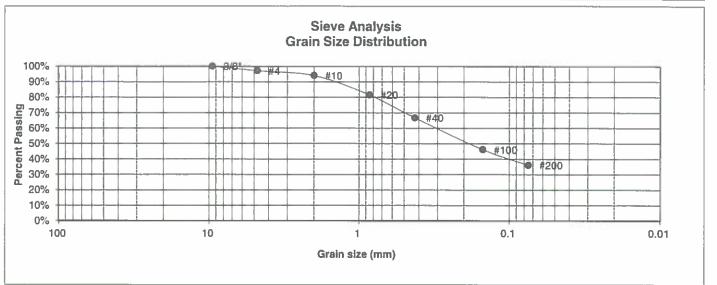
U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u>	Atterberg Limits Plastic Limit 17 Liquid Limit 33 Plastic Index 16
4	100.0%	Swell
10	99.6%	Moisture at start
20	90.9%	Moisture at finish
40	78.3%	Moisture increase
100	51.5%	Initial dry density (pcf)
200	36.3%	Swell (psf)



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JOB NO.: 210984 FIG NO.:

UNIFIED CLASSIFICATION	SC	CLIENT	CLASSIC COMMUNITIES
SOIL TYPE #	1	PROJECT	HANNAH RIDGE, FEATHERGRASS, F5
TEST BORING #	6	JOB NO.	210984
DEPTH (FT)	1-2	TEST BY	BL
AASHTO CLASSIFICATION	A-6	GROUP INDEX	2



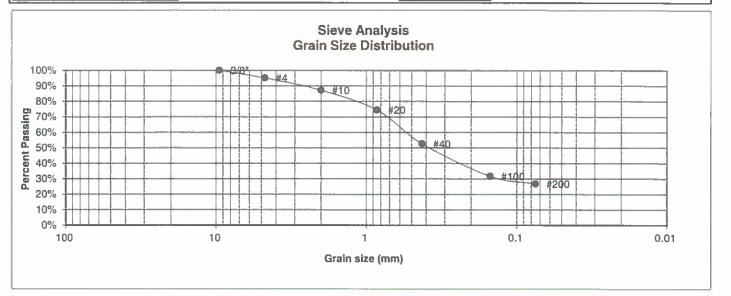
U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u>	Atterberg Limits Plastic Limit 19 Liquid Limit 39 Plastic Index 20
4	97.2%	Swell
10	94.0%	Moisture at start
20 40	81.6% 66.7%	Moisture at finish Moisture increase
100 200	46.1% 36.1%	Initial dry density (pcf) Swell (psf)



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JOB NO.: 210984 FIG NO.:

UNIFIED CLASSIFICATION	SC	CLIENT	CLASSIC COMMUNITIES
SOIL TYPE #	2, CBR	PROJECT	HANNAH RIDGE, FEATHERGRASS, F5
TEST BORING #	5	JOB NO.	210984
DEPTH (FT)	0-3	TEST BY	BL
AASHTO CLASSIFICATION	A-2-6	GROUP INDEX	0

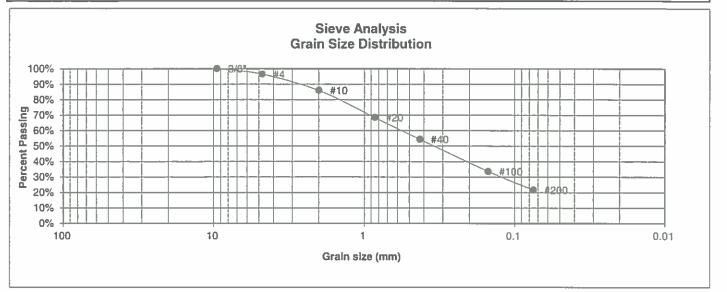


U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit 12 Liquid Limit 24 Plastic Index 11
3/8"	100.0%	
4	95.1%	Swell
10	87.2%	Moisture at start
20	74.5%	Moisture at finish
40	52.6%	Moisture increase
100	31.7%	Initial dry density (pcf)
200	26.9%	Swell (psf)



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UNIFIED CLASSIFICATION	SC	CLIENT	CLASSIC COMMUNITIES
SOIL TYPE #	2	PROJECT	HANNAH RIDGE, FEATHERGRASS, F5
TEST BORING #	2	JOB NO.	210984
DEPTH (FT)	1-2	TEST BY	BL
AASHTO CLASSIFICATION	A-2-6	GROUP INDEX	0



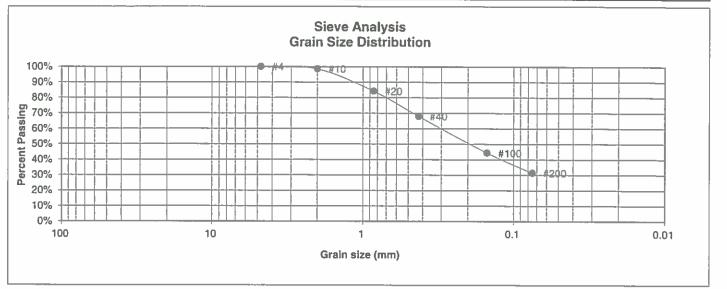
U.S. Sieve # 3" 1 1/2" 3/4" 1/2"	Percent <u>Finer</u>	Atterberg Limits Plastic Limit 21 Liquid Limit 38 Plastic Index 17
3/8"	100.0%	
4	96.5%	Swell
10	86.0%	Moisture at start
20	68.4%	Moisture at finish
40	54.4%	Moisture increase
100	33.6%	Initial dry density (pcf)
200	21.6%	Swell (psf)



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JOB NO.: 210984 FIG NO.:

UNIFIED CLASSIFICATION	SC	CLIENT	CLASSIC COMMUNITIES
SOIL TYPE #	2	PROJECT	HANNAH RIDGE, FEATHERGRASS, F5
TEST BORING #	3	JOB NO.	210984
DEPTH (FT)	1-2	TEST BY	BL
AASHTO CLASSIFICATION	A-2-6	GROUP INDEX	0



U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u>	Atterberg Limits Plastic Limit 21 Liquid Limit 31 Plastic Index 11
4	100.0%	Swell
10	98.5%	Moisture at start
20	84.2%	Moisture at finish
40	67.9%	Moisture increase
100	44.4%	Initial dry density (pcf)
200	31.4%	Swell (psf)

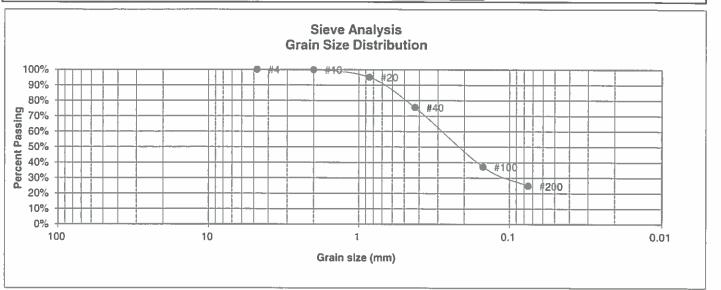


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FIG NO

UNIFIED CLASSIFICATION SC CLIENT CLASSIC COMMUNITIES **SOIL TYPE # PROJECT** 2 HANNAH RIDGE, FEATHERGRASS, F5 **TEST BORING #** 4 JOB NO. 210984 DEPTH (FT) 1-2 **TEST BY** BL AASHTO CLASSIFICATION A-2-6 **GROUP INDEX** 0



U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit Liquid Limit Plastic Index	16 28 12
4	100.0%	Swell	
10	99.8%	Moisture at start	
20	95.1%	Moisture at finish	
40	75.5%	Moisture increase	
100 200	37.1% 24.8%	Initial dry density (pcf) Swell (psf)	

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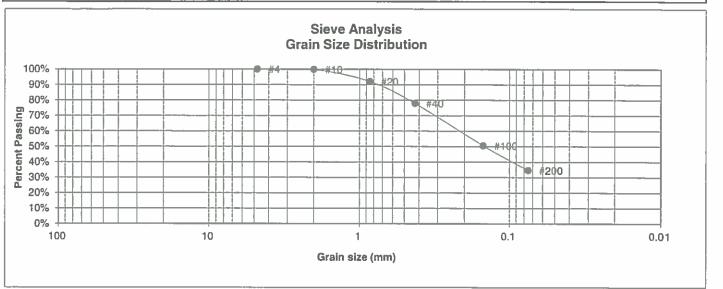


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UNIFIED CLASSIFICATION	SC	CLIENT	CLASSIC COMMUNITIES
SOIL TYPE #	2	PROJECT	HANNAH RIDGE, FEATHERGRASS, F5
TEST BORING #	5	JOB NO.	210984
DEPTH (FT)	1-2	TEST BY	BL
AASHTO CLASSIFICATION	A-2-6	GROUP INDEX	1



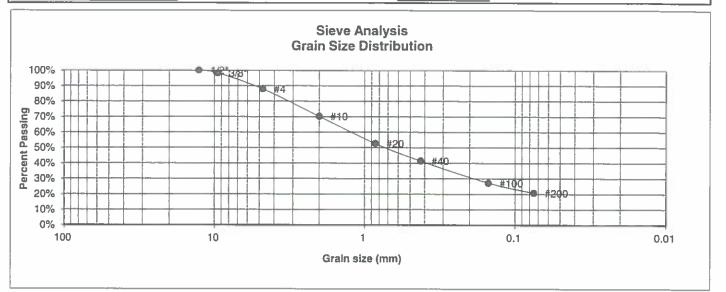
U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit 16 Liquid Limit 32 Plastic Index 16
4	100.0%	<u>Swell</u>
10	99.8%	Moisture at start
20	92.1%	Moisture at finish
40	78.0%	Moisture increase
100	50.5%	Initial dry density (pcf)
200	34.6%	Swell (psf)



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JOB NO: 210984 FIG NO:

UNIFIED CLASSIFICATION SC CLIENT **CLASSIC COMMUNITIES** SOIL TYPE # **PROJECT** 2 HANNAH RIDGE, FEATHERGRASS, F5 7 TEST BORING # JOB NO. 210984 DEPTH (FT) 1-2 **TEST BY** BL AASHTO CLASSIFICATION A-2-6 **GROUP INDEX** 0



U.S. <u>Sieve #</u> 3" 1 1/2" 3/4"	Percent <u>Finer</u>	Atterberg Limits Plastic Limit 17 Liquid Limit 29 Plastic Index 12
1/2"	100.0%	
3/8"	98.1%	
4	88.0%	<u>Swell</u>
10	70.2%	Moisture at start
20	52.7%	Moisture at finish
40	41.4%	Moisture increase
100	27.2%	Initial dry density (pcf)
200	20.8%	Swell (psf)

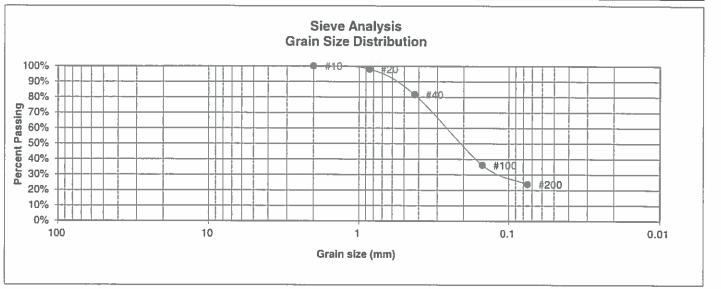
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JOB NO.: 210984 FIG NO.:

UNIFIED CLASSIFICATION	SM	CLIENT	CLASSIC COMMUNITIES
SOIL TYPE #	3	PROJECT	HANNAH RIDGE, FEATHERGRASS, F5
TEST BORING #	4	JOB NO.	210984
DEPTH (FT)	5	TEST BY	BL
AASHTO CLASSIFICATION	A-2-4	GROUP INDEX	0



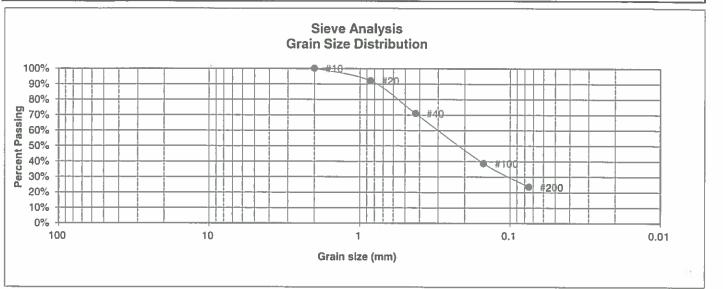
U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit NP Liquid Limit NV Plastic Index NP
4 10	100.0%	Swell Moisture at start
20 40	98.1% 81.6%	Moisture at start Moisture at finish Moisture increase
100 200	36.2% 23.8%	Initial dry density (pcf) Swell (psf)



LABORATORY TEST RESULTS				
	DATE:	CHECKED:	DATE:	

JOB NO.: 210984 FIG NO.: 1

UNIFIED CLASSIFICATION	SC	CLIENT	CLASSIC COMMUNITIES
SOIL TYPE #	3	PROJECT	HANNAH RIDGE, FEATHERGRASS, F5
TEST BORING #	7	JOB NO.	210984
DEPTH (FT)	10	TEST BY	BL
AASHTO CLASSIFICATION	A-2-6	GROUP INDEX	0



U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u>	Atterberg Limits Plastic Limit 15 Liquid Limit 31 Plastic Index 15
4		Swell
10	100.0%	Moisture at start
20	92.1%	Moisture at finish
40	71.0%	Moisture increase
100	38.7%	Initial dry density (pcf)
200	23.5%	Swell (psf)

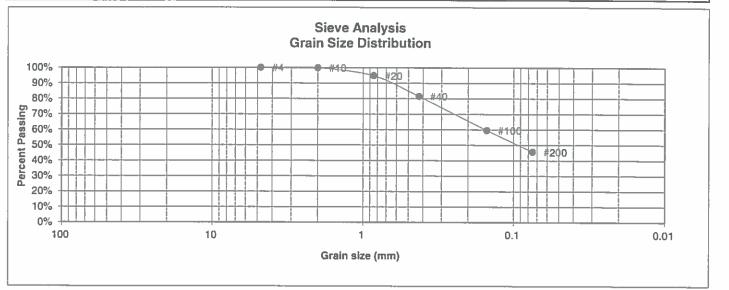


LABORATORY TEST RESULTS				
DRAWN:	DATE:	CHECKED:	7/8/21	

JOB NO.: 210984

FIG NO

UNIFIED CLASSIFICATION	SC	CLIENT	CLASSIC COMMUNITIES
SOIL TYPE #	4	PROJECT	HANNAH RIDGE, FEATHERGRASS, F5
TEST BORING #	6	JOB NO.	210984
DEPTH (FT)	10	TEST BY	BL
AASHTO CLASSIFICATION	A-6	GROUP INDEX	4



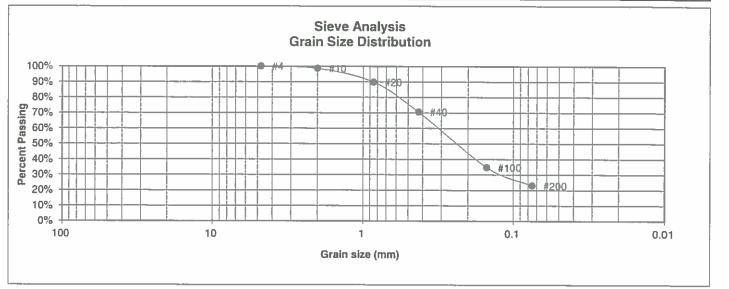
U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit 15 Liquid Limit 33 Plastic Index 17
4	100.0%	Swell
10	99.8%	Moisture at start
20	94.8%	Moisture at finish
40	81.5%	Moisture increase
100	59.6%	Initial dry density (pcf)
200	45.7%	Swell (psf)



LABO! RESUI	RATORY TEST LTS	
DATE:	CHECKED	-PATE/o

JOB NO: 210984 FIG NO: 210984

UNIFIED CLASSIFICATION	SM	CLIENT	CLASSIC COMMUNITIES
SOIL TYPE #	5	PROJECT	HANNAH RIDGE, FEATHERGRASS, F5
TEST BORING #	1	JOB NO.	210984
DEPTH (FT)	10	TEST BY	BL
AASHTO CLASSIFICATION	A-2-4	GROUP INDEX	0



U.S. <u>Sieve #</u> 3" 1 1/2" 3/4" 1/2" 3/8"	Percent <u>Finer</u>	Atterberg <u>Limits</u> Plastic Limit NP Liquid Limit NV Plastic Index NP
4	100.0%	Swell
10	98.6%	Moisture at start
20	89.8%	Moisture at finish
40	70.5%	Moisture increase
100	34.8%	Initial dry density (pcf)
200	23.0%	Swell (psf)

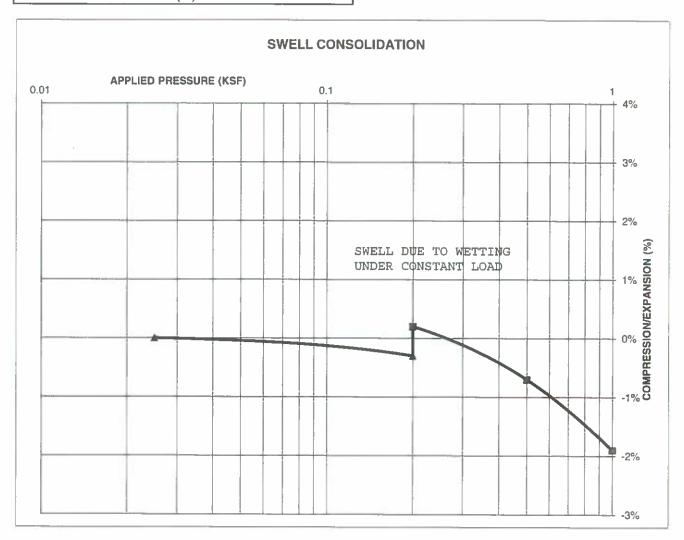


LABORATORY TEST RESULTS					
DRAWN:	DATE	CHECKED.	7/2/21		

210984 FIG NO.:-

TEST BORING # 1 DEPTH(ft) 0-3
DESCRIPTION SC SOIL TYPE 1, CBR
NATURAL UNIT DRY WEIGHT (PCF) 115
NATURAL MOISTURE CONTENT 10.8%
SWELL/CONSOLIDATION (%) 0.5%

JOB NO. 210984
CLIENT CLASSIC COMMUNITIES
PROJECT HANNAH RIDGE, FEATHERGRASS, F5





SWELL CONSOLIDATION TEST RESULTS	

DRAWN: DATE: CHECKED: DATE:

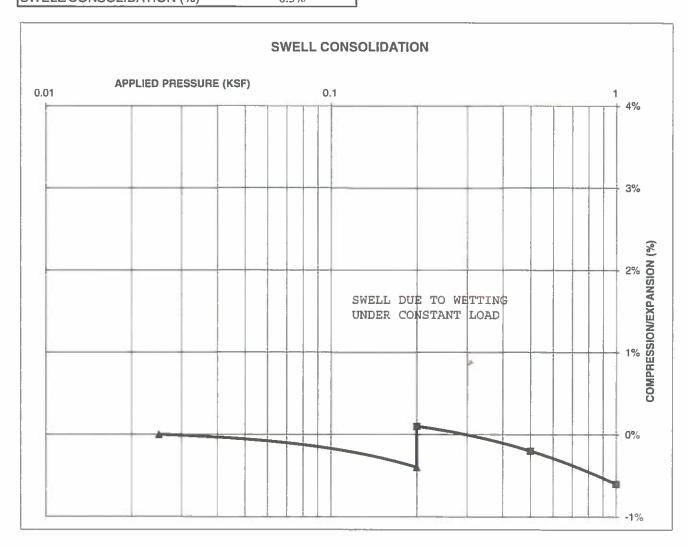
210984 FIG NO.:

TEST BORING #	1	DEPTH(ft)	1-2	
DESCRIPTION	SC	SOIL TYPE	1	
NATURAL UNIT DRY	WEIGI	HT (PCF)	116	
NATURAL MOISTURI			14.2%	
SWELL/CONSOLIDA	TION (%)	0.5%	

JOB NO. 210984

CLIENT CLASSIC COMMUNITIES

PROJECT HANNAH RIDGE, FEATHERGRASS, F5





SWELL CONSOLIDATION TEST RESULTS

DRAWN:

DATE:

CHECKED:

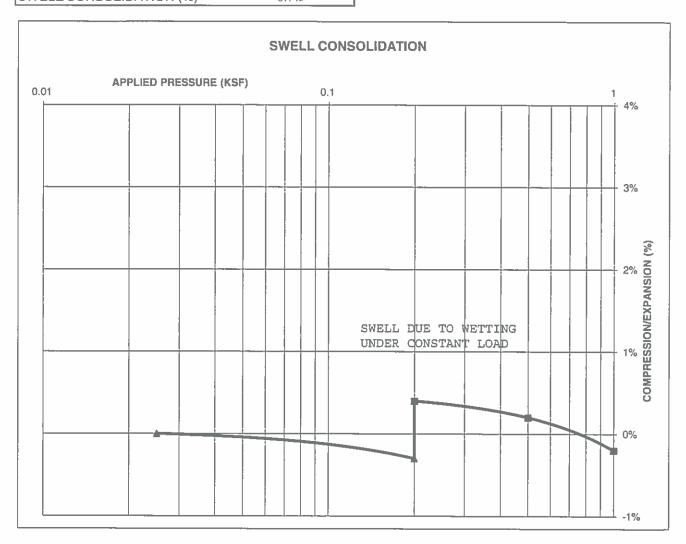
7/8/2/

JOB NO.: 210984

FIG NO.:

TEST BORING # 6 DEPTH(ft) 1-2
DESCRIPTION SC SOIL TYPE 1
NATURAL UNIT DRY WEIGHT (PCF) 115
NATURAL MOISTURE CONTENT 12.8%
SWELL/CONSOLIDATION (%) 0.7%

JOB NO. 210984
CLIENT CLASSIC COMMUNITIES
PROJECT HANNAH RIDGE, FEATHERGRASS, F5





SWELL CONSOLIDATION TEST RESULTS

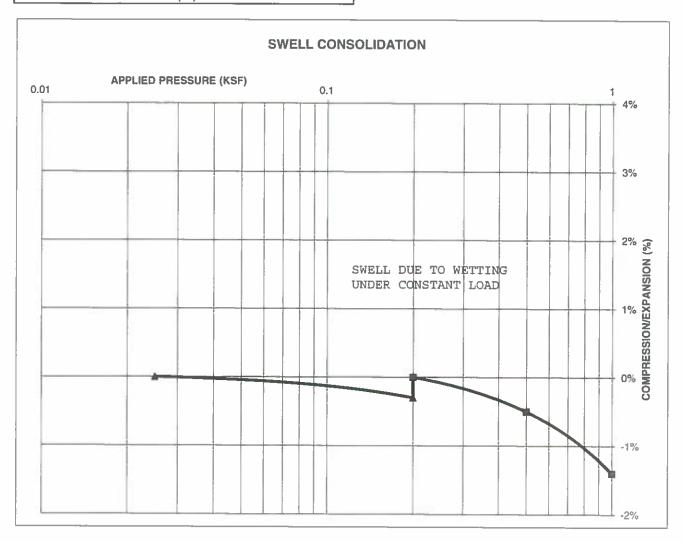
DRAWN: DATE: CHECKED: DATE:

JOB NO 210984

FIG NO.

TEST BORING # 2 DEPTH(ft) 1-2
DESCRIPTION SC SOIL TYPE 2
NATURAL UNIT DRY WEIGHT (PCF) 95
NATURAL MOISTURE CONTENT 14.3%
SWELL/CONSOLIDATION (%) 0.3%

JOB NO. 210984
CLIENT CLASSIC COMMUNITIES
PROJECT HANNAH RIDGE, FEATHERGRASS, F5





SWELL CONSOLIDATION TEST RESULTS

DRAWN:

DATE:

CHECKED:

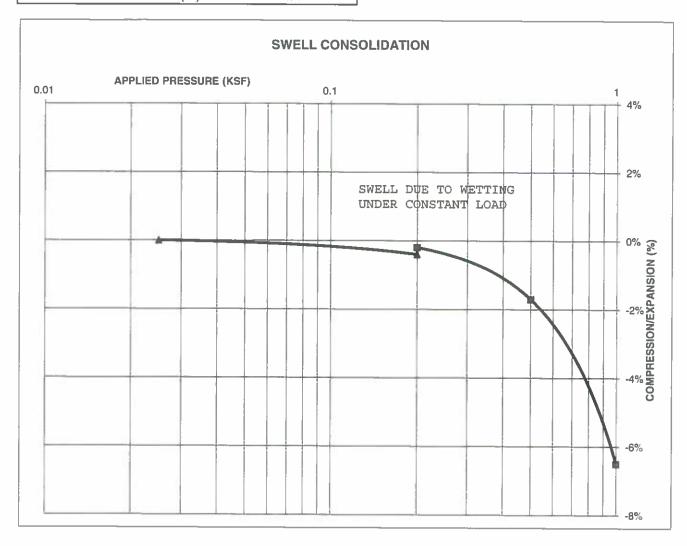
7/8/2

JOB NO.: 210984

FIG NO.;

TEST BORING #	3	DEPTH(ft)	1-2	
DESCRIPTION	SC	SOIL TYPE	2	
NATURAL UNIT DRY	WEIG	HT (PCF)	97	
NATURAL MOISTUR	E CON	TENT	9.4%	
SWELL/CONSOLIDA	TION (%)	0.2%	

JOB NO. 210984
CLIENT CLASSIC COMMUNITIES
PROJECT HANNAH RIDGE, FEATHERGRASS, F5





SWELL CONSOLIDATION TEST RESULTS

DRAWN:

DATE:

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JOB NO.:: 210984

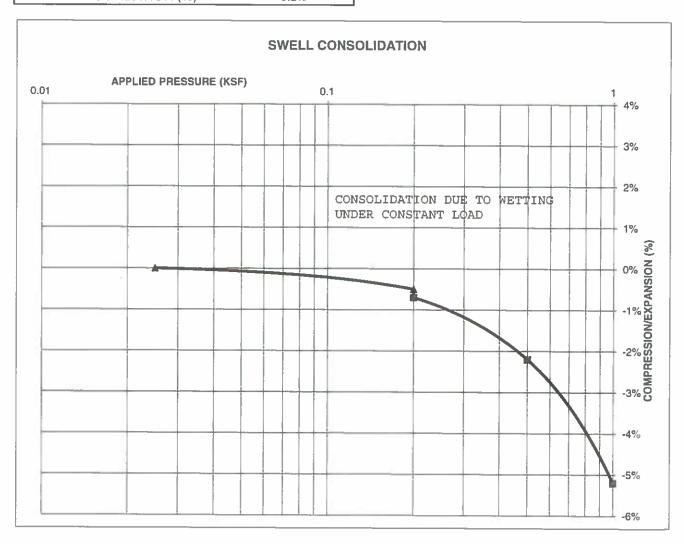


TEST BORING # 4 DEPTH(ft) 1-2
DESCRIPTION SC SOIL TYPE 2
NATURAL UNIT DRY WEIGHT (PCF) 95
NATURAL MOISTURE CONTENT 7.4%
SWELL/CONSOLIDATION (%) -0.2%

JOB NO. 210984

CLIENT CLASSIC COMMUNITIES

PROJECT HANNAH RIDGE, FEATHERGRASS, F5





SWELL CONSOLIDATION TEST RESULTS

DRAWN:

DATE:

CHECKED:

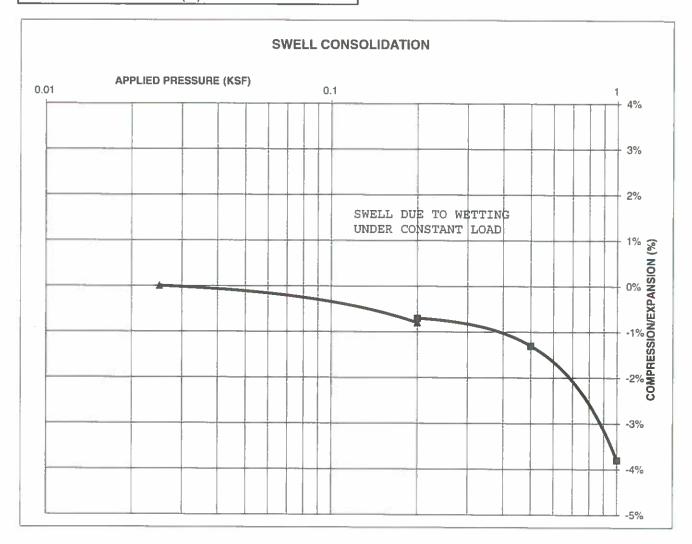
718/2/

JOB NO: 210984

FIG NO:

TEST BORING # 5 DEPTH(ft) 1-2 DESCRIPTION SC SOIL TYPE 2 NATURAL UNIT DRY WEIGHT (PCF) 99 NATURAL MOISTURE CONTENT 10.8% SWELL/CONSOLIDATION (%) 0.1%

JOB NO. 210984 CLIENT **CLASSIC COMMUNITIES** PROJECT HANNAH RIDGE, FEATHERGRASS, F5





SWELL CONSOLIDATION
TEST RESULTS

DRAWN: DATE: JOB NO.: 210984

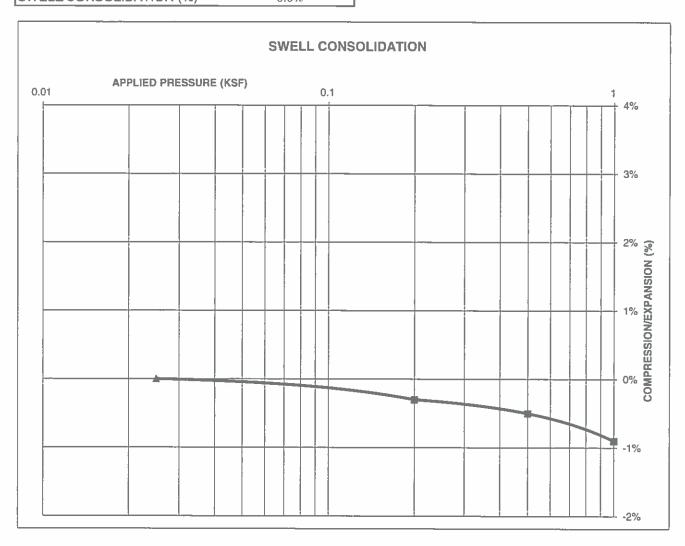
FIG NO.

B-20

7/8/21 CHECKED:

TEST BORING #	7	DEPTH(ft)	1-2	
DESCRIPTION	SC	SOIL TYPE	2	
NATURAL UNIT DRY	WEIGI	HT (PCF)	113	
NATURAL MOISTUR	E CON	TENT	8.5%	
SWELL/CONSOLIDA			0.0%	

JOB NO. 210984
CLIENT CLASSIC COMMUNITIES
PROJECT HANNAH RIDGE, FEATHERGRASS, F5





SWELL CONSOLIDATION TEST RESULTS

DRAWN:

DATE:

CHECKED:

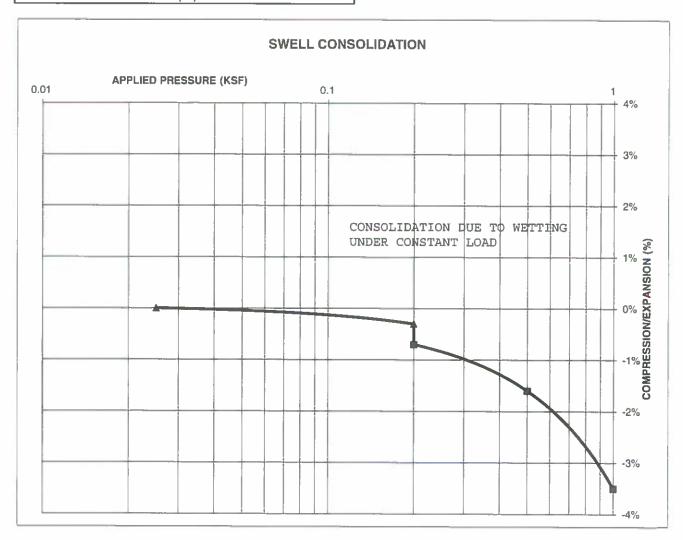
7/8/21

JOB NO.: 210984

FIG NO.

TEST BORING # 7 DEPTH(ft) 10
DESCRIPTION SC SOIL TYPE 3
NATURAL UNIT DRY WEIGHT (PCF) 96
NATURAL MOISTURE CONTENT 10.7%
SWELL/CONSOLIDATION (%) -0.4%

JOB NO. 210984
CLIENT CLASSIC COMMUNITIES
PROJECT HANNAH RIDGE, FEATHERGRASS, F5





SWELL CONSOLIDATION TEST RESULTS

DRAWN: DATE: CHECKED: DATE:

210984

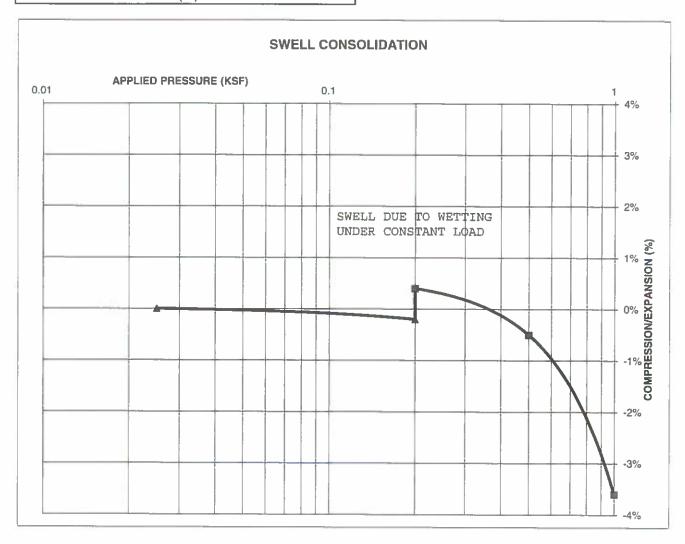


JOB NO.:

CONSOLIDATION TEST RESULTS

TEST BORING #	6	DEPTH(ft)	10	
DESCRIPTION	SC	SOIL TYPE	4	
NATURAL UNIT DRY	WEIGI	HT (PCF)	94	
NATURAL MOISTUR	E CON	TENT	8.0%	
SWELL/CONSOLIDA	TION (%)	0.6%	

JOB NO. 210984
CLIENT CLASSIC COMMUNITIES
PROJECT HANNAH RIDGE, FEATHERGRASS, F5





SWELL CONSOLIDATION TEST RESULTS

DRAWN: DATE: CHECKED: DATE:

JOB NO.: 210984

FIG NO:

CLIENT CLASSIC COMMUNITIES JOB NO. 210984

PROJECT HANNAH RIDGE, FEATHERGRASS, F5 DATE 6/17/2021

LOCATION HANNAH RIDGE, FEATHERGRASS, F5 TEST BY BL

BORING NUMBER	DEPTH, (ft)	SOIL TYPE NUMBER	UNIFIED CLASSIFICATION	WATER SOLUBLE SULFATE, (wt%)
TB-2	1-2	2	SC	0.00
TB-4	5	3	SM	0.00
TB-6	1-2	1	sc	0.00
TB-7	10	3	sc	0.00

QC BLANK PASS



LABORAT	ORY TEST
SULFATE	RESULTS

DRAWN: DATE: CHECKED: DATE:

210984 FIG NO

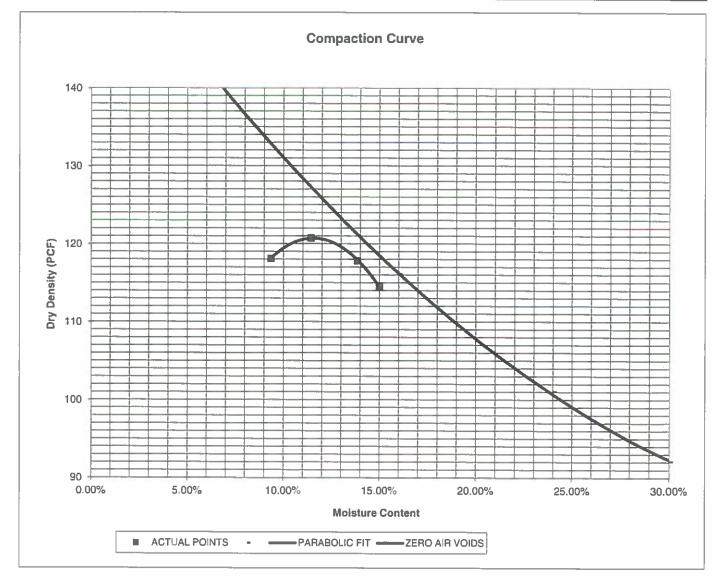
PROJECT HANNAH RIDGE, FEATHERGRASS, F5 CLIENT CLASSIC COMMUNITIES

SAMPLE LOCATION TB-1 @ 0-3' JOB NO. 210984 SOIL DESCRIPTION FILL, SAND, VERY CLAYEY, BROWN DATE 06/17/21

 IDENTIFICATION
 SC
 COMPACTION TEST # 1

 TEST DESIGNATION / METHOD
 ASTM D-698-A
 TEST BY
 BL

 MAXIMUM DRY DENSITY (PCF)
 120.9
 OPTIMUM MOISTURE
 11.5%





MOISTURE DENSITY RELATION

DRAWN: DATE: CHECKED: DATE

210984 FIG NO. B-25

JOB NO.

CBR TEST LOAD DATA

JOB NO:

210984

CLIENT: CLA

CLASSIC COMMUNITIES

 PISTON
 PISTON

 DIAMETER (cm)
 AREA (in²)

 4.958
 2.993

PROJECT: HANNAH RIDGE, FEATHERGRASS, F5 SOIL TYPE: 1

4,900	2.993					
	10 BLOWS		25 BLOWS		56 BLOWS	
PENETRATION	MOLD #	1	MOLD # :	2	MOLD #	3
DEPTH	LOAD(LBS)	STRESS	LOAD(LBS)	STRESS	LOAD(LBS)	STRESS
(INCHES)	(LBS)	(PSI)	(LBS)	(PSI)	(LBS)	(PSI)
0.000	0	0.00	0	0.00	0	0.00
0.025	72	24.06	102	34.09	177	59.15
0.050	118	39.43	172	57.48	246	82.21
0.075	169	56.47	225	75.19	291	97.24
0.100	190	63.49	253	84.54	334	111.61
0.125	225	75.19	290	96.91	358	119.63
0.150	241	80.53	318	106.27	386	128.99
0.175	273	91.23	338	112.95	429	143.36
0.200	306	102.26	363	121.30	466	155.72
0.300	343	114.62	434	145.03	572	191.14
0.400	374	124.98	497	166.08	672	224.56
0.500	401	134.00	552	184.46	768	256.64

FINAL MOISTURE CONTENT

	MOLD #	1	MOLD #	2	MOLD #	3
CAN #		309		310		307
WT. CAN		6.7		8.39	l 1	8.42
WT. CAN+WET		366.04		339.53		268.15
WT. CAN+DRY		315.53	l i	295.91	!	236.83
<u>WT. H20</u>		50.51		43.62		31.32
WT. DRY SOIL	i	308.83		287.52		228.41
MOISTURE CONTENT		16.36%		15.17%		13.71%

WET DENSITY (PCF)	124.5	127.2	132.9
DRY DENSITY (PCF)	111.6	114.1	119.2
DEADING DATIO			-
BEARING RATIO	6.35	8 45	11 16

DRAWN:

 90% OF DRY DENSITY
 107.3

 95% OF DRY DENSITY
 113.3

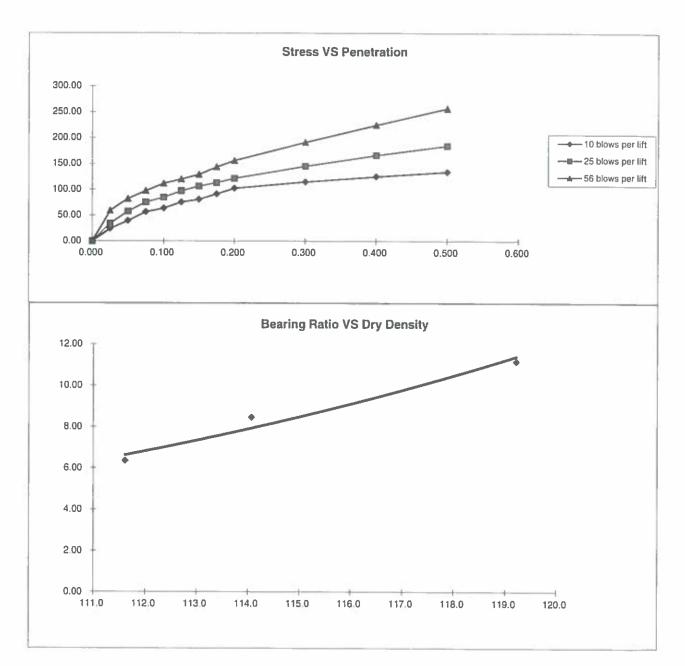
2.63 ~ R VALUE	6
7.75 ~ R VALUE	17



CB	R TEST DATA	
DATE:	CHECKED:	DATE:

JOB NO. 210984

FIG NO.:



 BEARING RATIO AT 90% OF MAX
 2.63 ~ R VALUE
 6.00

 BEARING RATIO AT 95% OF MAX
 7.75 ~ R VALUE
 17.00

JOB NO: 210984 SOIL TYPE: 1



	CALIFOR	CALIFORNIA BEARING RATIO						
DRAWN:	DATE:	CHECKED:	TIE/21					

JOB NO.: 210984

PROJECT HANNAH RIDGE, FEATHERGRASS, F5 CLIENT TB-5 @ 0-3'

CLASSIC COMMUNITIES JOB NO.

SAMPLE LOCATION SOIL DESCRIPTION

FILL, SAND, CLAYEY, BROWN

210984 DATE 06/17/21

IDENTIFICATION TEST DESIGNATION / METHOD SC

COMPACTION TEST #

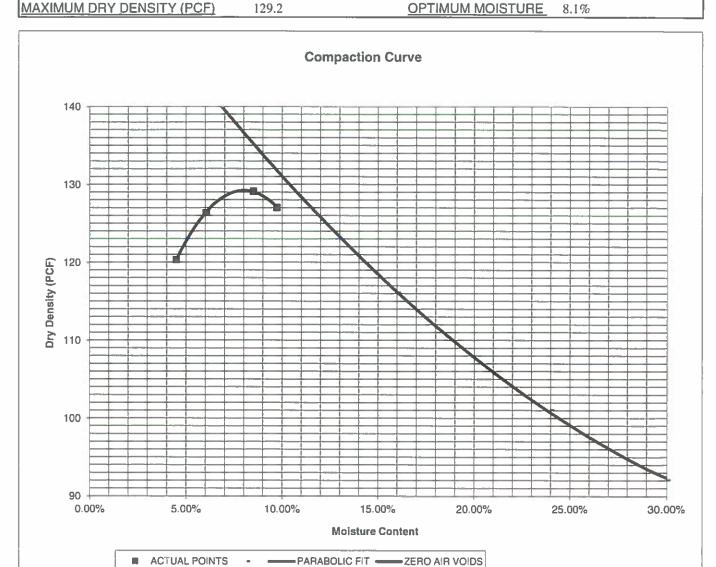
TEST BY ASTM D-1557-A

BL

129.2

OPTIMUM MOISTURE

8.1%







DRAWN:

DATE:

CHECKED DI

7/8/21

JOB NO.:

210984 FIG NO.

CBR TEST LOAD DATA

JOB NO:

210984

PISTON PISTON DIAMETER (cm) AREA (in²) 4.958 2.993

CLIENT:

CLASSIC COMMUNITIES PROJECT: HANNAH RIDGE, FEATHERGRASS, F5

SOIL TYPE: 2

11000	2,000					
	10 BLOWS		25 BLOWS		56 BLOWS	
PENETRATION	MOLD #	1	MOLD #	2	MOLD #	3
DEPTH	LOAD(LBS)	STRESS	LOAD(LBS)	STRESS	LOAD(LBS)	STRESS
(INCHES)	(LBS)	(PSI)	(LBS)	(PSI)	(LBS)	(PSI)
0.000	0	0.00	0	0.00	0	0.00
0.025	101	33.75	134	44.78	163	54.47
0.050	185	61.82	221	73.85	258	86.22
0.075	235	78.53	344	114.95	404	135.00
0.100	275	91.90	406	135.67	606	202.51
0.125	313	104.59	531	177.44	720	240.60
0.150	346	115.62	597	199.50	989	330.49
0.175	370	123.64	688	229.91	1124	375.60
0.200	409	136.67	830	277.36	1482	495.24
0.300	484	161.74	1207	403.34	2301	768.92
0.400	582	194.49	1521	508.27	2883	963.41
0.500	687	229.57	1622	542.02	3013	1006.85

FINAL MOISTURE CONTENT

	MOLD #	1	MOLD #	2	MOLD #	3
CAN #		300		306		314
WT. CAN		6.76		6.64		6.51
WT. CAN+WET		334.27		370.57		342.48
WT. CAN+DRY		297.42		334.055		311.13
WT. H20		36.85		36.515		31.35
WT. DRY SOIL		290.66		327.415		304.62
MOISTURE CONTENT		12.68%		11.15%		10.29%

WET DENSITY (PCF)	127.9	133.0	136.9
DRY DENSITY (PCF)	118.3	123.1	126.6
•			

BEARING RATIO 9.19 13.57 20.25

DRAWN:

90% OF DRY DENSITY 95% OF DRY DENSITY

116.3 122.7

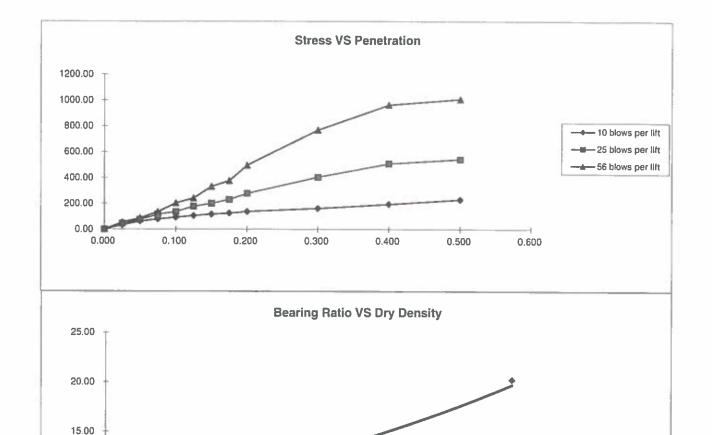
BEARING RATIO AT 90% OF MAX	7.28 ~ R VALUE	17
BEARING RATIO AT 95% OF MAX	13.26 ~ R VALUE	40

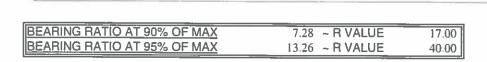


	CBR	TEST DATA	
DATE:		CHECKED:	7/8/2/

JOB NO.

210984 FIG NO





121.0

122.0

123.0

124.0

125.0 126.0 127.0

120.0

JOB NO: 210984 SOIL TYPE: 2

128.0



10.00

5.00

0.00

118.0

119.0

CALIFORNIA BEARING RATIO			
DRAWN	DATE:	CHECKED:	Allel2,

210984 FIG NO.: **APPENDIX C: Pavement Design Calculations**

FLEXIBLE PAVEMENT DESIGN

DESIGN DATA CLASSIC CO

CLASSIC COMMUNITIES - HANNAH RIDGE AT FEATHERGRASS, F5 SOILTYPE I - LOCAL LOW VOULME

Equivalent (18 kip) Single Axle Load Applications (ESAL): $ESAL (W_{18}) = 36,500$ Hveem Stabilometer (R Value) Results: R = 17Standard Deviation $S_{0} = 0.45$ Loss in Serviceability $\Delta psi = 2.0$ Reliability Reliability = 80

Reliability (z-statistic) $Z_R = -0.84$

Soil Resilient Modulus $M_R = 4478$

DESIGN TABLES AND EQUATIONS

Weighted Structural Number (WSN):

$$S_1 = [(R - 5) / 11.29] + 3$$

 $M_R = 10^{[(S_1 + 1872)/624]}$

 $k = M_R/19.4$

Where:

M_R = resilient modulus (psi)

 S_1 = the soil support value

R = R-value obtained from the Hveem stabilometer

CBR = California Bearing Ratio

Reliability (%)	Z _R (z-statistic)
80	-0.84
85	-1.04
90	-1.28
93	-1.48
94	-1.56
95	-1.65
96	1.75
97	-1.88
98	-2.05
99	-2.33
99.9	-3.09
99.99	-3.75

$$\log_{10}W_{18} = Z_{R}^{*} S_{O} + 9.36^{*}\log_{10}(SN+1) - 0.20 + \frac{\log_{10}\left[\Delta PSI\right]}{0.40 + \frac{1094}{(SN+1)^{5.19}}} + 2.32^{*}\log_{10}M_{R} - 8.07$$

Left	Right	Difference
4.56	4.56	0.0

Job No. 210894 Fig. No. C-1

WSN =

2.25

DESIGN CALCULATIONS

CEMENT TREATED SECTIONS - SOIL TYPE 1

DESIGN DATA: CLASSIC COMMUNITIES - HANNAH RIDGE AT FEATHERGRASS, F5 LOCAL LOW VOLUME

Equivalent (18 kip) Single Axle Load Applications (ESAL):

ESAL = 36,500

Hyeem Stabilometer (R Value) Results:

R = 17

Weighted Structural Number (WSN):

WSN = 2.25

DESIGN EQUATION

 $WSN = C_1D_1 + C_2D_2$

 $C_1 = 0.44$ Strength Coefficient - Hot Bituminous Asphalt $C_2 = 0.12$ Strength Coefficient - Cement Treated Subgrade

D₁ = Depth of Asphalt (inches)D₂ = Depth of Cement Treated Subgrade (inches)

FOR FULL DEPTH ASPHALT SECTION - (CURRENTLY NOT ALLOWED)

 $D_1 = (WSN)/C_1 = 5.1$ inches of Full Depth Asphalt Use 5.5 inches Full Depth

FOR ASPHALT + CEMENT TREATED SUBGRADE SECTION

Asphalt Thickness (t) = 4 inches $D_2 = ((WSN) - (t)(C_1))/C_2 = 4.1 \text{ inches}$ Use 10.0 inches of Cement Treated Subgrade

RECOMMENDED ALTERNATIVES

- 1. 4.0 inches of Asphalt + 10 inches of Cement Treated Subgrade
- 2. 5.5 inches of Full Depth Asphalt

Job No. 210984 Fig. No. C-2

FLEXIBLE PAVEMENT DESIGN

DESIGN DATA CLASSIC COMMUNITIES - HANNAH RIDGE AT FEATHERGRASS, F5 SOILTYPE 2 - LOCAL LOW VOULME

Equivalent (18 kip) Single Axle Load Applications (ESAL): $ESAL(W_{18}) =$ 36,500 Hveem Stabilometer (R Value) Results: R =40 Standard Deviation $S_o =$ 0.45 Loss in Serviceability $\Delta psi =$ 2.0 Reliability Reliability = 80 Reliability (z-statistic) -0.84 $Z_R =$ Soil Resilient Modulus $M_R =$ 9497

Weighted Structural Number (WSN):

DESIGN TABLES AND EQUATIONS

$$S_1 = [(R - 5) / 11.29] + 3$$

 $M_R = 10^{[(S_1 + 18.72) / 6.24]}$

 $k = M_R/19.4$

Where:

M_R = resilient modulus (psi)

 S_1 = the soil support value

R = R-value obtained from the Hveem stabilometer

CBR = California Bearing Ratio

Reliability (%)	Z _R (z-statistic)
80	-0.84
85	-1.04
90	-1.28
93	-1.48
94	-1.56
95	-1.65
96	-1.75
97	-1.88
98	-2.05
99	-2.33
99.9	-3.09
99.99	-3.75

$$\log_{10}W_{18} = Z_{R}^{*} S_{O}^{+} 9.36^{*}\log_{10}(SN+1) - 0.20 + \frac{\log_{10}\left[\frac{\Delta PSI}{4.2 - 1.5}\right]}{0.40 + \frac{1094}{(SN+1)^{5.19}}} + 2.32^{*}\log_{10}M_{R}^{-} 8.07$$

Left	Right	Difference
4.56	4.56	0.0

Job No. 210894 Fig. No. C-3 1.68

DESIGN CALCULATIONS

CEMENT TREATED SECTIONS - SOIL TYPE 2

DESIGN DATA: CLASSIC COMMUNITIES - HANNAH RIDGE AT FEATHERGRASS, F5

LOCAL LOW VOLUME

Equivalent (18 kip) Single Axle Load Applications (ESAL):

Hveem Stabilometer (R Value) Results:

R = 40

Weighted Structural Number (WSN):

WSN = 1.68

DESIGN EQUATION

 $WSN = C_1D_1 + C_2D_2$

 $C_1 = 0.44$ Strength Coefficient - Hot Bituminous Asphalt $C_2 = 0.12$ Strength Coefficient - Cement Treated Subgrade

 D_1 = Depth of Asphalt (inches)

 D_2 = Depth of Cement Treated Subgrade (inches)

FOR FULL DEPTH ASPHALT SECTION - (CURRENTLY NOT ALLOWED)

 $D_1 = (WSN)/C_1 = 3.8$ inches of Full Depth Asphalt

Use 4.0 inches Full Depth

FOR ASPHALT + CEMENT TREATED SUBGRADE SECTION

Asphalt Thickness (t) = 4 inches

 $D_2 = ((WSN) - (t)(C_1))/C_2 = -0.7$ inches

Use 10.0 inches of Cement Treated Subgrade

RECOMMENDED ALTERNATIVES

- 1. 4.0 inches of Asphalt + 10 inches of Cement Treated Subgrade
- 2. 4.0 inches of Full Depth Asphalt

Job No. 210984

Fig. No. C-4

FLEXIBLE PAVEMENT DESIGN

<u>DESIGN DATA</u> CLASSIC COMMUNITIES - HANNAH RIDGE AT FEATHERGRASS, F5 SOILTYPE 2 - LOCAL RESIDENTIAL

 $ESAL(W_{18}) =$ Equivalent (18 kip) Single Axle Load Applications (ESAL): 292,000 Hveem Stabilometer (R Value) Results: R =40 Standard Deviation $S_0 =$ 0.45 Loss in Serviceability $\Delta psi =$ 2.0 Reliability Reliability = 80 Reliability (z-statistic) -0.84 $Z_R =$ Soil Resilient Modulus 9497 $M_R =$

Weighted Structural Number (WSN): WSN = 2.37

DESIGN TABLES AND EQUATIONS

$$S_1 = [(R - 5) / 11.29] + 3$$

 $M_R = 10^{[(S_1 + 1872)/624]}$

 $k = M_R/19.4$

Where:

M_R = resilient modulus (psi)

 S_1 = the soil support value

R = R-value obtained from the Hveem stabilometer

CBR = California Bearing Ratio

Reliability (%)	Z _R (z-statistic)
80	-0.84
85	-1.04
90	-1.28
93	-1.48
94	-1.56
95	-1.65
96	-1.75
97	-1.88
98	-2.05
99	-2.33
99.9	-3.09
99.99	-3.75

$$\log_{10}W_{18} = Z_{R}^{*}S_{O}^{+} 9.36^{*}\log_{10}(SN+1) - 0.20 + \frac{\log_{10}\left[\frac{\Delta PSI}{4.2 - 1.5}\right]}{0.40 + \frac{1094}{(SN+1)^{5.19}}} + 2.32^{*}\log_{10}M_{R}^{-} 8.07$$

Left	Right	Difference
5.47	5.46	0.0

Job No. 210894 Fig. No. C-5

DESIGN CALCULATIONS

CEMENT TREATED SECTIONS - SOIL TYPE 2

<u>DESIGN DATA:</u> CLASSIC COMMUNITIES - HANNAH RIDGE AT FEATHERGRASS, F5

LOCAL RESIDENTIAL

Equivalent (18 kip) Single Axle Load Applications (ESAL):

ESAL = 292,000

Hveem Stabilometer (R Value) Results:

R = 40

Weighted Structural Number (WSN):

WSN = 2.37

DESIGN EQUATION

 $WSN = C_1D_1 + C_2D_2$

 $C_1 = 0.44$ Strength Coefficient - Hot Bituminous Asphalt

C₂ = 0.12 Strength Coefficient - Cement Treated Subgrade

 D_1 = Depth of Asphalt (inches)

 D_2 = Depth of Cement Treated Subgrade (inches)

FOR FULL DEPTH ASPHALT SECTION - (CURRENTLY NOT ALLOWED)

 $D_1 = (WSN)/C_1 = 5.4$ inches of Full Depth Asphalt

Use 5.5 inches Full Depth

FOR ASPHALT + CEMENT TREATED SUBGRADE SECTION

Asphalt Thickness (t) = 4 inches

 $D_2 = ((WSN) - (t)(C_1))/C_2 = 5.1$ inches

Use 10.0 inches of Cement Treated Subgrade

RECOMMENDED ALTERNATIVES

- 1. 4.0 inches of Asphalt + 10 inches of Cement Treated Subgrade
- 2. 5.5 inches of Full Depth Asphalt

Job No. 210984

Fig. No. C-6





505 ELKTON DRIVE COLORADO SPRINGS, CO 80907 PHONE (719) 531-5599 FAX (719) 531-5238

July 8, 2021

Classic Communities 2138 Flying Horse Club Drive Colorado Springs, CO 80921

Attn: Adam Doyle

Re: Cement Stabilized Subgrade Results - Laboratory Testing

Hannah Ridge at Feathergrass, Filing No. 5

El Paso County, Colorado

Ref: Pavement Recommendations Report by Entech Engineering, Inc., dated July 8, 2021,

Entech Job No. 210984.

Dear Mr. Doyle:

As requested, personnel of Entech Engineering, Inc. have performed strength testing on two sets of three soil/cement composite samples for Soil Type 1 and Soil Type 2 for the above referenced project. Testing was performed on soil samples prepared with 2% and 4% Portland Cement Type 1/2, from Martin Marietta, near Pueblo, Colorado.

A compression strength of 160 psi is recommended for cement stabilized subgrade. The 5-day average strength value of the Type 1 samples with a 2% mix was 175 psi, and the 5-day average strength value of the 4% mix was 188 psi. The 5-day average strength value of the Type 2 samples of the 2% mix was 196 psi, and the 5-day average strength value of the 4% was 216 psi. A 3% mix is recommended based on the laboratory test results. A summary of the testing results is attached.

Pending the results of the field density testing, microfracturing of the stabilized subgrade will likely be required on this site. Soil strengths in excess of 200 psi require microfracturing.

We trust this has provided you with the information you required. If you have any questions or need additional information, please do not hesitate to contact us.

Respectfully Submitted,

ENTECH ENGINEERING, INC.

Daniel P. Stegman

DPS/kc

Encl.

Entech Job No. 210984 AAprojects/2021/210984 cssr – lab

El Paso County File No. SF-18-038

President

SUMMARY OF CTS TEST RESULTS LAB TESTING

CLIENT CLASSIC COMMUNITIES

PROJECT HANNAH RIDGE, FEATHERGRASS, F5

FIELD SAMPLE ID

TB-1 @ 0-3', SOIL TYPE #1

SOIL ADDITIVE

TYPE I/II CEMENT

JOB NO
210984

DATE
7/7/21

BY

BL

ADDITIVE %	WATER %	DENSITY (dry)	AGE (days)	STRENGTH (psi)
2	11.5	114.9	5	161
2	11.5	115.0	5	185
2	11.5	114.7	5	178
			AVERAGE:	175
4	11.5	114.6	5	171
4	11.5	114.8	_ 5	214
4	11.5	115.0	5	178
			AVERAGE:	188

CURING METHOD

100° HUMIDIFIED OVEN

SUMMARY OF CTS TEST RESULTS LAB TESTING

CLIENT CLASSIC COMMUNITIES

PROJECT HANNAH RIDGE, FEATHERGRASS, F5

FIELD SAMPLE ID

TB-5 @ 0-3', SOIL TYPE #2

SOIL ADDITIVE

TYPE I/II CEMENT

JOB NO
210984

7/7/21

BY

BL

ADDITIVE %	WATER %	DENSITY (dry)	AGE (days)	STRENGTH (psi)
2	8.1	122.7	6	193
2	8.1	122.8	6	199
2	8.1	122.9	6	197
			AVERAGE:	196
4	8.1	123.0	6	222
4	8.1	122.7	6	211
4	8.1	122.6	6	216
			AVERAGE:	216

CURING METHOD

100° HUMIDIFIED OVEN