## PRELIMINARY DRAINAGE REPORT FOR ESTEBAN RODRIGUEZ SUBDIVISION EL PASO COUNTY, COLORADO

October 2024

Due to the nature and volume of comments provided additional new comments may be generated on the re-submittal.

Prepared For:

Brent Houser Enterprises, LLC 11890 Garrett Road Peyton, CO 80831-7685

Prepared By:

JR ENGINEERING

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Job No. 25277.00

PCD File No.: SP245

#### **ENGINEER'S STATEMENT:**

The attached drainage report and plan was prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by El Paso County for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors, or omissions on my part in preparing this report.

Bryan T. Law, Colorado P.E. # 25043	
For and On Behalf of JR Engineering, LLC	

Date

#### **DEVELOPER'S STATEMENT:**

I, the developer, have read and will comply with all of the requirements specified in this drainage report and plan.

Business Name:

Brent Houser Enterprises, LLC

By:

Esteban Rodriguez

Title: Address:

11890 Garrett Road Peyton, CO 80831-7685

#### **El Paso County:**

Filed in accordance with the requirements of the El Paso County Land Development Code, Drainage Criteria Manual, Volumes 1 and 2 and Engineering Criteria Manual, as amended.

Joshua Palmer, P.E. County Engineer/ ECM Administrator

Date

Conditions:



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## PURPOSE

This document is the Preliminary Drainage Report for Esteban Rodriguez Subdivision. The purpose of this report is to identify on-site and off-site drainage patterns, culverts, areas tributary to the site, and to safely route developed storm water to adequate outfall facilities.

## **GENERAL LOCATION AND DESCRIPTION**

### **General Location**

The proposed Esteban Rodriguez Subdivision development (hereby referred to as the "site") is located within the west half of Section 2, the southwest quarter of the southeast quarter of the east half of Section 2, and the north half of the north half of Section 11, Township 13 South, Range 64 West of the Sixth Principal Meridian, El Paso County, Colorado. The site is bound by existing large acre Cowboy Ranch VW developments to the east, existing Judge Orr Road to the north, the future Saddlehorn Ranch to the west, and by the existing Sagecreek North development and 7360 Falcon Grassy Hts. to the south. A vicinity map is presented in Appendix A.

#### **Description of Property**

The proposed Esteban Rodriguez Subdivision development contains approximately 496 acres and will be comprised of 2.5-acre single-family lots, 5-acre single-family lots, commercial areas and detention pond areas. The site is currently unoccupied and undeveloped. The existing ground cover is sparse short and mixed grass prairie vegetation. Currently there is one major drainageway located on-site, which is titled Geick Ranch WF-R8a per the "Gieck Ranch Drainage Basin Planning Study" by Drexel, Barrel dated October, 2007 and updated in February 2010. This drainageway was analyzed hydrologically and hydraulically later in this report.

Per a NRCS web soil survey of the area, the site is made up of Hydrologic Group A and D soils. Type A soils are typically deep well-drained to excessively drained sands that have a high infiltration rate when thoroughly wet. Type D soils are typically clays and soils with a high water table that have a very slow infiltration rate. Most of the developable area of the site has Type A soils. The Type D soils are located mostly within the undevelopable floodplain area. A NRCS soil survey map is presented in Appendix A.

### **Floodplain Statement**

Based on the FEMA FIRM numbers 08041C0558G, 08041C0559G, 08041C0566G, and 08041C0567G dated December 7, 2018, the site lies within Zone A and Zone X. Zone A is defined as area within the Special Flood Hazard Area (SFHA) with no base flood elevations determined. Zone X is defined as area outside the SFHA and higher than the elevation of the 0.2-percent-annual-chance (or 500-year) flood. The floodplains throughout the site shall be considered no-build areas and all proposed development within the site will occur in Zone X. Draft model backed BFEs for this area have been developed as part of Phase 1 for the ongoing El Paso County, CO, Risk MAP project.

FEMA approved floodplain elevations will be required on the final plat. The FIRM panels are presented in Appendix A.

#### **Environmental Statement**

The "Wetland, Wildlife and Natural Features Report for Esteban Rodriguez Subdivision in El Paso County, Colorado" by ECOS dated June 19, 2023 describes the existing environmental features of the site. No critical habitat, wildlife refuges, or hatcheries are found in the vicinity of the site. The site does have existing wetland and riparian habitats located within the drainageway. In compliance with the environmental report, these areas will not be impacted by development except for around the two proposed roadway crossings, as well as required channel improvements. As mentioned in the environmental report, a portion of the creek below the existing stock pond is head-cutting severely. If not addressed, the headcut will completely degrade the abutting wetland and therefore should be stabilized immediately. The proposed development will also remove the existing stock pond and improve the channel against possible erosion. See Appendix D for excerpts of the afore mentioned environmental report.

## MAJOR DRAINAGE BASINS AND SUB-BASINS

#### **Major Basin Descriptions**

#### Gieck Ranch

A portion of the site lies within the Gieck Ranch Drainage Basin. The "Gieck Ranch Drainage Basin Planning Study" by Drexel, Barrel dated October, 2007 and updated in February 2010 has not been approved by El Paso County as of the date of this report. The Gieck Ranch Drainage Basin covers approximately 22 square miles beginning approximately 5 miles northeast of the Town of Falcon and extends approximately 15 miles to the southeast. The Gieck Ranch Drainage Bain is tributary to Black Squirrel Creek, which drains south to its confluence with the Arkansas River near Pueblo, Colorado. In general, the Gieck Ranch Drainage Basin flows from west to east across the proposed site.

As described in the report, a portion of the west fork of the Gieck Ranch drainageway flows from west to east across the proposed site. The specific channel reaches are WF-R7a, WF-R7b, and WF-R8a. The proposed improvements described within that report are described as vegetation augmentation and selective stabilization along these reaches. The report proposes several grade control structures as well as the removal of the existing stock pond located within the channel near the east site boundary to avoid further headcutting. Excerpts of the Gieck Ranch DBPS are shown in Appendix D for information only. The proposed rural local roadways crossing the existing Gieck Ranch West Tributary drainageway in two locations, a No Rise Letter shall be provided with the future Final Draiange Report. The No Rise Letter shall show that the proposed channel improvements will not adversely affect the floodplain width and water surface elevation. See the

Channel Analysis and Design portion of the report for proposed improvements and drainage infrastructure.

#### Haegler Ranch

A portion of the site also lies within the Haegler Ranch Drainage Basin. The "Haegler Ranch Basin Drainage Basin Planning Study" by URS Corporation dated May, 2009 describes the characteristics of the Haegler Ranch basin. The Haegler Ranch Drainage Basin covers approximately 17 square miles located in the central portion of El Paso County. The Haegler Ranch Drainage Bain is tributary to Ellicott Consolidated Drainage Basin unnamed tributary, which is tributary to Black Squirrel Creek. In general, the Haegler Ranch Drainage Basin flows from north to south to the west of the proposed site.

As described in the report, a portion of the main stem flows north to south to the west of the proposed site. The specific channel reaches adjacent to the proposed site are MS-5 and MS-6. The proposed improvements described within the Haegler Ranch DPBS suggest sub-regional detention facilities as the selected design alternative. None of the Haegler Ranch drainageway floodplains are located onsite, and there will therefore be no impacts due to the proposed development. The proposed development does not intend to change peak flows in the existing drainageways. Excerpts of the Haegler Ranch DBPS are shown in Appendix D.

### **EXISTING DRAINAGE CONDITIONS**

#### **Existing Sub-basin Drainage**

The existing basin delineation for Esteban Podriguez Subdivision as shown on the map within Appendix E is as follows:

 generated by these basins

Basin OS1 is approximately 1.56 acres view and a scomprised of undeveloped areas to the west of the project site, a future tract within the Saddlehorn Ranch Filing No. 4 development. Flow will follow the historic path overland from the northwest to the southeast where it will enter Basin EXA and follow the drainage patterns of that basin. The basin flows will combine at DP1.

Basin OS2 is approximately 17.5 acres with a 10% impervious and is comprised of future portions of Saddlehorn Ranch Filing No. 4 and 5 to the west of the project site. Flow will follow the historic path overland from the southwest to the northeast where it will enter Basin EXA and follow the drainage patterns of that basin. The basin flows will combine at DP1.

Existing Basin EXA is approximately 179.6 acres with a 2% impervious and in the existing condition is comprised of undeveloped land and part of the FEMA floodplain for Gieck Ranch West Tributary. Historically runoff from this basin flows from northwest and southwest to the drainageway in the middle where the flows enter the existing drainageway. Flows from the off-site basins OS1 and OS2 will combine with Basin EXA at DP1 ( $Q_5=86$  cfs,  $Q_{100}=753$  cfs). These flows are from the reach

please also provide total flow within this basin only. Please verify/revise. Saddlehorn dervelopment filing 4 by JR identifies the flows just upstream of this development as 1017 cfs. WF-R8a within the "Gieck Ranch Drainage Basin Planning Study" by Drexel, Barrell & Co. dated October 2007. Flows then continue flowing east off-site within the existing Gieck Ranch drainageway.

Existing Basin EXB is approximately 32.2 acres with a 2% impervious and in the existing condition is comprised of undeveloped land. Historically runoff from this basin flows from northwest to the southeast where the flows follow the existing path flowing to the southeast off-site at DP2 ( $Q_5=7$  cfs,  $Q_{100}=44$  cfs). Flows then continue flowing southeast onto the 16365 Judge Orr Road property before entering the existing Gieck Ranch drainageway.

Existing Basin EXC is approximately 29.0 acres with a 2% impervious and in the existing condition is comprised of undeveloped land. Historically runoff from this basin flows from south to the north where the flows follow the existing path flowing to the northeast off-site at DP3 ( $Q_5=6$  cfs,  $Q_{100}=40$  cfs). Flows then continue flowing northeast onto the Cowboy Ranch VW property before entering the existing Gieck Ranch drainageway.

Existing Basin EXD is approximately 48.2 acres with a 2% impervious and in the existing condition is comprised of undeveloped land. Historically runoff from this basin flows from north to the south where the flows follow the existing path flowing to the southwest off-site at DP4 ( $Q_5=7$  cfs,  $Q_{100}=48$  cfs). Flows then continue flowing south onto the 7120 Fak refer to comment on the drainage the existing Haegler Ranch drainageway.

Existing Basin EXE is approximately 152.2 acres with a 2%

is comprised of undeveloped land. Historically runoff from this basin flows from north to the south where the flows follow the existing path flowing to the southwest off-site at DP5 ( $Q_5=22$  cfs,  $Q_{100}=145$  cfs). Flows then continue flowing south onto the Sagecreek North Development property. Runoff then continues following the historic path within the Haegler Ranch drainage basin.

Existing Basin EXF is approximately 50.2 acres with a 2% impervious and in the existing condition is comprised of undeveloped land. Historically runoff from this basin flows from north to the south where the flows follow the existing path flowing to the southwest off-site at DP6 ( $Q_5=8$  cfs,  $Q_{100}=55$  cfs). Flows then continue flowing south within an existing natural ditch onto the 7360 Falcon Grassy Hts and Sagecreek North Development properties. Runoff then continues following the historic path within the Haegler Ranch drainage basin.

A summary of existing basin parameters is presented in Appendix B.

this parcel is west of Basin EXF. Remove

## **PROPOSED DRAINAGE CONDITIONS**

#### **Proposed Drainage Conveyance**

In general, developed flows are collected in proposed roadside swales, which convey water to the proposed detention areas. Proposed rural minor collector roadways with 80' right-of-ways as well as rural local roadways with 60' right-of-ways are used throughout the site and are per the typical El Paso County section. Proposed swales will be designed per the typical county rural roadside ditch section and designed to ensure they are stable and have required capacity to satisfy criteria. A swale is considered stable with a velocity of 5 ft/s or less. If velocities exceed 5 ft/s, swales shall be protected by buried soil riprap to limit potential erosion. To ensure capacity, swales will have a minimum of 1 ft. of freeboard over the water surface for flows anticipated in a 100-year storm event. please clarify whether II comply with Table 6-1 of the EPC DCM Volume 1. In addition to the the judge orr roadside sulverts also convey flows under proposed roadways. Culverts under paved ditch is also part of t overtop the roadways with flows from a 100-year storm event. The inlets this basin and will be sed culverts will be protected with riprap to limit potential erosion. More conveyed to DP1 provided in the future Final Drainage Report.

#### **Proposed Sub-basin Drainage**

Appendix  $\mathbf{E}$  is as follows:

please also account/address the improvements to Judge Orr Road as well as the turn lane The proposed basin delineation for Esteb improvements at each of the proposed intersections to Judge Orr.

Basin A1 is approximately 12.1 acres with an 85% impervious and is comprised of proposed

consider accounting for a higher impervious for this commercial area to avoid limitations at site development of this area. Typical commercial/industrial areas are 80-95% impervious per table 6-6 in DCM

north half of Glorietta Street and west half of Cabarillo Circle East. Runoff collected in a proposed roadside swale. Flows will be piped across Cabarillo rt at DP1 ( $Q_5=33$  cfs,  $Q_{100}=62$  cfs). Flows continue within a proposed swale to 2.1. show the culvert on

the drainage map

mately 4.18 acres with  $\sim 72\%$  impervious and is comprised of proposed east half of Cabarillo Circle East and a proposed swale. Runoff from this basin proposed swale along the southern basin line at DP2 ( $Q_5=12$  cfs,  $Q_{100}=23$  cfs). )P1 at the proposed culvert at DP2.1 ( $Q_5 = 44$  cfs,  $Q_{100} = 84$  cfs). Flows continue

within a proposed Highlighted flows here and on the following pages do not match calcs. Please round up for values that are .5 or greater. Please use one decimal point for flows less than 1 cfs. Basin A3 is approximately 3.84 acres with an 88% impervious and is comprised of proposed

commercial areas and a proposed swale. Runoff from this basin will be collected in a proposed swale along the southern basin line to the proposed swale at DP3 ( $Q_5=12$  cfs,  $Q_{100}=23$  cfs). DP3 flows combine with DP2.1 within the proposed swale at DP3.1 ( $Q_5=54$  cfs,  $Q_{100}=102$  cfs). Flows continue within a proposed swale to the combination at DP4.1

Basin A4 is approximately 4.15 acres with a 26% impervious and is comprised of a large singlefamily lot and the east half of Cabrillo Circle East. Runoff from this basin will be collected in

please clarify if this is intended to be the roadside ditch/swale along Cabrillo Circle

See comment on drainage map about sub-basins. If there is a swale to DP3, please show it. The existing topography appears to be falling to the east.

proposed roadside swales at DP4 ( $Q_5=3$  cfs,  $Q_{100}=10$  cfs). DP4 flows combine with DP3.1 flows at the culvert at DP4.1 ( $Q_5=56$  cfs,  $Q_{100}=102$  cfs). Flows enter into vities to the transformation of the transfo

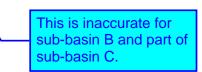
Basin OS1 is approximately 1.56 acres with a 10% impervious and is comprised of undeveloped areas to the west of the project site (a future tract within the Saddlehorn Ranch Filing No. 4 development) as well as the west half of proposed Elbert Road. This basin is off-site and only a proposed Elbert Road connection is proposed. Runoff from this basin will follow the historic path overland from the northwest to the southeast and flow to the proposed roadside swale at DP5 ( $Q_5=1$  cfs,  $Q_{100}=3$  cfs). Flows continue along the roadside swale to the combination at DP6.1.

Basin A5 is approximately 5.99 acres with a 26% impervious and is comprised of large single-family lots, the south half of Elbert Road and the west half of Cabrillo Circle West. Runoff from this basin will be collected in proposed roadside swales to DP6 ( $Q_5=4$  cfs,  $Q_{100}=13$  cfs). Flows combine with DP5 at the proposed culvert at DP6.1 ( $Q_5=5$  cfs,  $Q_{100}=16$  cfs). Runoff is then directed to Pond 1 along a proposed swale. DP6.1 flows enter Pond 1 via a forebay and combine with other inflows at DP8.1.

Basin A6 is approximately 38.2 acres with a 15% impervious and is comprised of large single-family lots, the south half of Glorietta Street, the north half of Elbert Road and the east half of Cabrillo Circle East. Runoff from this basin will be collected in proposed roadside swales DP7 ( $Q_5=19$  cfs,  $Q_{100}=70$  cfs). DP7 flows enter Pond 1 via a forebay and combine with other inflows at DP8.1.

Basin A7 is approximately 7.57 acres with a 21% impervious and is comprised of is comprised of large single-family lots, the south half of Elbert Road, the east half of Cabrillo Circle West, the west half of Cabrillo Circle East and proposed Pond 1. Runoff from this basin will be collected in proposed roadside swales and sheet flow towards Pond 1 at DP8 ( $Q_5=7$  cfs,  $Q_{100}=22$  cfs). The inflows combine within Pond 1 at DP8.1 ( $Q_5=68$  cfs,  $Q_{100}=178$  cfs). Runoff is treated within Pond 1 and then released through the outlet structure at DP8.2 ( $Q_5=1$  cfs,  $Q_{100}=32$  cfs). DP8.2 flows then are directed to the proposed channel within the existing drainageway. Flows will ultimately follow the historic conveyance to the existing Gieck Ranch West Tributary drainageway then continue flowing east.

Basin B is approximately 0.74 acres with a 2% impervious and is comprised of an existing electric transmission easement. Runoff from this basin ( $Q_5=0$  cfs,  $Q_{100}=2$  cfs) will flow southeast overland towards the eastern site boundary. The existing utility easement does not allow for any proposed development in this area. Flows will therefore follow the historic path to the existing Gieck Ranch West Tributary drainageway without a permanent stormwater quality measure and are excluded from water quality treatment. This in accordance with Section I.7.1.B.5 of the ECM Stormwater Quality Policy and Procedure. Basin B and C flows combine at DP9.



Basin C is approximately 15.8 acres with a 10% impervious and is comprised of large single-family lots. Runoff from this basin ( $Q_5=8$  cfs,  $Q_{100}=34$  cfs) will flow southeast overland towards the eastern site boundary. Runoff from this basin is comprised of only large single-family lots and does not include any proposed roadway flows. Flows will therefore follow the historic path to the existing Gieck Ranch West Tributary drainageway without a permanent stormwater quality measure and are excluded from water quality treatment. This in accordance with Section I.7.1.B.5 of the ECM Stormwater Quality Policy and Procedure. Basin B and C flows combine at DP9 ( $Q_5=8$  cfs,  $Q_{100}=36$ cfs) representing the flow leaving the site to the east.

Basin D1 is approximately 4.49 acres with a 10% impervious and is comprised of large single-family lots. Runoff from this basin will flow southeast overland towards the existing drainageway. Runoff from this basin is comprised of only large single-family lots and does not include any proposed roadway flows. Flows will therefore follow the historic path to the existing Gieck Ranch West Tributary drainageway without a permanent stormwater quality measure and are excluded from water quality treatment. This in accordance with Section I.7.1.B.5 of the ECM Stormwater Quality Policy and Procedure. Runoff will follow the his at DP10.

impact to the channel due to the increase in flows from the lots within these basins will need to be analyzed

Basin OS2a is approximately 14.5 acres with a 2% impervious and is comprised or portions of ruture Saddlehorn Ranch Filing No. 4 and 5 to the west of the project site. Flow will follow the historic path overland from the southwest to the northeast where it will enter Basin D2 and follow the drainage patterns of that basin. 10% is shown in the impervious calculations to include build out of Saddlehorn Ranch lots. This imperviousness will increase the flows going into Geick Ranch Tributary

Basin D2 is approximately 11.0 acres with a 10% impervious and is comprised of large single-family lots. Runoff from this basin will flow northeast overland towards the existing drainageway. Runoff from this basin is comprised of only large single-family lots and does not include any proposed roadway flows. Flows will therefore follow the historic path to the existing Gieck Ranch West Tributary drainageway without a permanent stormwater quality measure and are excluded from water quality treatment. This in accordance with Section I.7.1.B.5 of the ECM Stormwater Quality Policy

and Procedure. Runoff w at DP10. Provide a design point at the culvert crossings and identify the total flows at this crossings inclusive of the increase in flows from this site and saddlehorn lots that drain to the channel that have not been

Basin D3 is approximate detained.

Gieck Ranch West Tributary floodplain that crosses the site. Proposed Cabrillo Circle West crosses the floodplain and is also the boundary of the basin. The only proposed disturbances within this basin are channel improvements and a dual 12' x 5' RCBC to cross the roadway. The basin does not have a permanent stormwater quality measure and is excluded from water quality treatment in accordance with Section I.7.1.B.8 of the ECM Stormwater Quality Policy and Procedure. Flows will follow the historic drainage pattern from west to east to the site boundary at DP10.

Basin D4 is approximately 5.75 acres with a 2% impervious and is the boundary of the existing Gieck Ranch West Tributary floodplain that crosses the site. Proposed Cabrillo Circle West and

For D1 and D2, 10% imperviousness seems too low since only the buildable part of these lots is included in the sub-basin. Please verify. Cabrillo Circle East cross the floodplain and are also the boundary of the basin. The only proposed disturbances within this basin are channel improvements and the two sets of dual 12' x 5' RCBC to cross the two roadways. The basin does not have a permanent stormwater quality measure and is excluded from water quality treatment in accordance with Section I.7.1.B.8 of the ECM Stormwater e pattern from west to east to the

### Quality Policy and Proce Total flows for this development should be analyzed and not just depend on the DBPS flows.

Basin D5 is approximately 4.55 acres with a 270 impervious and is the boundary of the existing Gieck Ranch West Tributary floodplain that crosses the site. Proposed Cabrillo Circle East crosses the floodplain and is also the boundary of the basin. The only proposed disturbances within this basin are channel improvements and the dual 12' x 5' RCBC to cross the roadway. The basin does not have a permanent stormwater quality measure and is excluded from water quality treatment in accordance with Section I.7.1.B.8 of the ECM Stormwater Quality Policy and Procedure. Flows will follow the historic drainage pattern from west to east to the site boundary at DP10 ( $O_5=86$  cfs,  $O_{100}=753$  cfs). These flows are from reach WF-R8a within the "Gieck Ranch Drainage Basin Planning Study" by Drexel, Barrell & Co. dated October 2007. Flows then continue flowing east off-site within the existing drainageway. 10% from impervious calcs.

Basin OS2b is approximately 3.06 acres with a 2% impervious and is comprised of portions of future Saddlehorn Ranch Filing No. 5 to the west of the project site. Flow will follow the historic path overland from the southwest to the northeast where it will enter Basin E1 at DP11 ( $Q_5=1$  cfs,  $Q_{100}=5$ cfs). DP11 runoff combines at DP12.1.

Please include the culvert under Adella Place in the narrative.

Basin E1 is approximately 28.7 acres with a 16% impervious and is comprised of large single-family lots, La Noria Way, Adella Place and the west half of Cabrillo Circle West. Runoff from this basin will be collected in proposed roadside swales to DP12 ( $Q_5=19$  cfs,  $Q_{100}=69$  cfs). Flows combine with DP11 at the proposed culvert at DP12.1 ( $Q_5=20$  cfs,  $Q_{100}=75$  cfs). Runoff is then directed to Pond 2 along a proposed swale. DP12.1 flows enter Pond 2 via a forebay and combine with other inflows at DP14.1.

Basin E2 is approximately 1.63 acres with a 55% impervious and is comprised of the east half of Cabrillo Circle East. Runoff from this basin will be collected in proposed roadside swales towards the culvert at DP13 ( $Q_5=3$  cfs,  $Q_{100}=6$  cfs). Flows enter into Pond 2 via a forebay and combine with other inflows at DP14.1.

Basin E3 is approximately 43.5 acres with a 16% impervious and is comprised of is comprised of large single-family lots, La Noria Way, the east half of Cabrillo Circle West, west half of Cabrillo Circle East and proposed Pond 2. Runoff from this basin will be collected in proposed roadside swales towards Pond 2 at DP14 ( $O_5=26$  cfs,  $O_{100}=93$  cfs). DP14 flows enter Pond 2 via a forebay and combine with other inflows at DP14.1 ( $Q_5=46$  cfs,  $Q_{100}=165$  cfs). Runoff is treated within Pond 2 and then released through the outlet structure at DP14.2 ( $Q_5=0$  cfs,  $Q_{100}=45$  cfs). DP14.2 flows then are directed to the proposed channel within the existing drainageway. Flows will ultimately follow the

historic conveyance to the existing Gieck Ranch West Tributary drainageway then continue flowing east.

Basin F is approximately 22.0 acres with a 10% impervious and is comprised of large single-family lots. Runoff from this basin will flow northeast overland towards the existing drainageway at DP15 ( $Q_5=9$  cfs,  $Q_{100}=40$  cfs). Runoff from this basin is comprised of only large single-family lots and does not include any proposed roadway flows. Flows will therefore follow the historic path to the existing Gieck Ranch West Tributary drainageway without a permanent stormwater quality measure and are excluded from water quality treatment. This in accordance with Section I.7.1.B.5 of the ECM Stormwater Quality Policy and Procedure.

Basin G1 is approximately 17.6 acres with a 13% impervious and is comprised of large single-family lots, north half of Visalia Court and the east half of Cabrillo Circle West. Runoff from this basin will be collected in proposed roadside swales to DP16 ( $Q_5=9$  cfs,  $Q_{100}=35$  cfs). DP16 flows combine at the DP17.1 roadside swale.

#### See notes on Drainage Map regarding sub-basins G1, G2, G3, H2.

Basin G2 is approximately 17.6 acres with a 15% impervious and is comprised of large single-family lots, south half of Visalia Court, north half of Tulago Place and the east half of Cabrillo Circle West. Runoff from this basin will be collected in proposed roadside swales to DP17 ( $Q_5=9$  cfs,  $Q_{100}=33$  cfs). DP17 flows combine at DP17.1 ( $Q_5=16$  cfs,  $Q_{100}=63$  cfs). DP17.1 flows combine at the DP18.1 culvert.

Basin G3 is approximately 5.70 acres with a 22% impervious and is comprised of large single-family lots, south half of Tulago Place and the east half of Cabrillo Circle West. Runoff from this basin will be collected in proposed roadside swales to DP18 ( $Q_5=5$  cfs,  $Q_{100}=15$  cfs). DP18 flows combine at DP18.1 ( $Q_5=19$  cfs,  $Q_{100}=72$  cfs). DP18.1 flows combine at the DP19.1 swale.

Basin G4 is approximately 20.4 acres with a 14% impervious and is comprised of large single-family lots and the west half of Cabrillo Circle West. Runoff from this basin will be collected in proposed roadside swales to DP19 ( $Q_5=10$  cfs,  $Q_{100}=39$  cfs). DP19 flows combine at DP19.1 ( $Q_5=27$  cfs,  $Q_{100}=108$  cfs). DP19.1 flows enter into Pond 3 via a forebay and combine at DP20.1.

Basin G5 is approximately 10.4 acres with a 12% impervious and is comprised of is comprised of large single-family lots and proposed Pond 3. Runoff from this basin will be collected in a proposed swale along the western basin boundary and sheet flow towards Pond 3 at DP20 ( $Q_5=6$  cfs,  $Q_{100}=23$  cfs). The inflows combine within Pond 3 at DP20.1 ( $Q_5=29$  cfs,  $Q_{100}=120$  cfs). Runoff is treated within Pond 3 and then released through the outlet structure at DP20.2 ( $Q_5=0$  cfs,  $Q_{100}=32$  cfs). DP20.2 flows then are directed to a proposed flow spreader before flowing offsite towards the 7120 Falcon Grassy Hts property and then enter the existing Haegler Ranch drainageway. Flows will ultimately follow the historic flowing west.

Basin H1 is approximately 24.0 acres with a 12% impervious and is comprised of large single-family lots, the west half of Cabrillo Circle East and Tarawa Place. Runoff from this basin will be collected in proposed roadside swales to DP21 ( $Q_5=12$  cfs,  $Q_{100}=47$  cfs). DP21 flows around Tarawa Place via a roadside swale and continue within a proposed swale to combine at DP22.1.

Basin H2 is approximately 41.8 acres with a 12% impervious and is comprised of large single-family lots and north half of Cabrillo Circle West. Runoff from this basin will sheet flow to the proposed swale to DP22 ( $Q_5=17$  cfs,  $Q_{100}=67$  cfs). DP21 and DP22 flows combine at DP22.1 ( $Q_5=26$  cfs,  $Q_{100}=106$  cfs). DP23.1 flows continue within a roadside swale to the combination at DP23.1 culvert.

Basin H3 is approximately 21.3 acres with a 15% impervious and is comprised of large single-family lots and west north half of Cabrillo Circle East. Runoff from this basin will sheet flow to the proposed swale to DP23 ( $Q_5=11$  cfs,  $Q_{100}=41$  cfs). DP23 and DP22.1 flows combine at DP23.1 ( $Q_5=34$  cfs,  $Q_{100}=139$  cfs). DP23.1 flows enter the proposed culvert under Cabrillo Circle East to the proposed swale at DP24.1.

Basin H4 is approximately 1.96 acres with a 54% impervious and is comprised of the south half of Cabrillo Circle West/ Cabrillo Circle Fast Runoff from this basin roadside swale at DP24 ( $Q_5$ = this should be broken up into two basin for east and west Cabrillo Circle to accurately indicate the flows in the roadside swales

Basin H5 is approximately 3.10 uncertained of large single-family lots and Cabrillo Circle East. Runoff from this basin will be collected in proposed channel to DP25 ( $Q_5$ =4 cfs,  $Q_{100}$ =9 cfs). DP25 flows around Tarawa Place via a proposed channel to the combination at DP25.1 ( $Q_5$ =37 cfs,  $Q_{100}$ =145 cfs).

Basin H6 is approximately 36.6 acres with a 11% impervious and is comprised of large single-family lots, the east half of Cabrillo Circle East and proposed Pond 4. Runoff from this basin will be collected in proposed channel to DP26 ( $Q_5=13 \text{ cfs}$ ,  $Q_{100}=54 \text{ cfs}$ ). DP26 flows via a proposed channel to the combination at DP26.1 ( $Q_5=47 \text{ cfs}$ ,  $Q_{100}=196 \text{ cfs}$ ). DP26.1 flows to Pond 4 via a forebay. Runoff is treated within Pond 4 and then released through the outlet structure at DP26.2 ( $Q_5=0 \text{ cfs}$ ,  $Q_{100}=42 \text{ cfs}$ ). DP14.2 flows then are directed to a proposed flow spreader before flowing offsite existing natural dich adjacent to the existing platted right-of-way and Sagecreek North development. The existing natural ditch will convey the flows as it does in the existing condition.

Basin I is approximately 46.8 acres with a 10% impervious and is comprised of large single-family lots. Runoff from this basin will flow south overland towards the site boundary at DP27 ( $Q_5=24$  cfs,  $Q_{100}=103$  cfs). Runoff from this basin is comprised of only large single-family lots and does not include any proposed roadway flows. Flows will therefore follow the historic path to the 7360 Falcon Grassy Hts property without a permanent stormwater quality measure and are excluded from water quality treatment. This in accordance with Section I.7.1.B.5 of the ECM Stormwater Quality Policy and Procedure.

Flows go to several properties to the south, not just 7360.

this basin should be broken into multiple basins as the flow leaves the site at multiple locations A summary of proposed basin parameters is presented in Appendix B.

	see comments on	
Comparison of Flows <	drainage map and	
There are several locations where the existing	adjust accordingly.	ne site:

- Flows leave the mid-eastern part of the site at existing DP1 and proposed DP10. Existing DP1 flows ( $Q_5=86$  cfs,  $Q_{100}=753$  cfs) are the same as the proposed DP10 flows ( $Q_5=86$  cfs,  $Q_{100}=753$  cfs). These values are from the Gieck Ranch DBPS. The proposed Pond 1 and Pond 2 will release flows into the existing drainageway at the rate required to ensure proposed values are less than or equal to existing flows.
- Flows leave the northeastern part of the site at existing DP2 and proposed DP9. Existing DP2 flows ( $Q_5=7$  cfs,  $Q_{100}=44$  cfs) are greater in the major storm than the proposed DP9 ( $Q_5=8$  cfs,  $Q_{100}=36$  cfs).
- Existing 100 year flows are smaller but 5 year flows are larger for some DP's. Please address.
- Flows also leave the mid-eastern part of the site at existing DP3 and proposed DP15. Existing DP3 flows ( $Q_5=7$  cfs,  $Q_{100}=48$  cfs) are the more than the proposed DP15 flows ( $Q_5=9$  cfs,  $Q_{100}=40$  cfs).
- Flows leave the southwestern part of the site at existing DP4 and proposed Pond 3 discharge at DP20.2. Existing DP4 flows (Q<sub>5</sub>=7 cfs, Q<sub>100</sub>=48 cfs) are the less than the proposed Pond 3 discharge at DP20.2 (Q<sub>5</sub>=0 cfs, Q<sub>100</sub>=32 cfs). The proposed Pond 4 will release flows at the rate required to ensure proposed values are less than or equal to existing flows.
- Flows also leave the southern part of the site at existing DP5 and proposed DP27. Existing DP5 flows ( $Q_5=22 \text{ cfs}$ ,  $Q_{100}=145 \text{ cfs}$ ) are greater in the major storm than the proposed DP27 flows ( $Q_5=24 \text{ cfs}$ ,  $Q_{100}=103 \text{ cfs}$ ).
- Flows leave the southeastern part of the site at existing DP6 and proposed Pond 4 discharge at DP26.2. Existing DP6 flows ( $Q_5=8$  cfs,  $Q_{100}=55$  cfs) are the greater than the proposed Pond 4 discharge at DP26.2 ( $Q_5=0$  cfs,  $Q_{100}=42$  cfs). The proposed Pond 4 will release flows at the rate required to ensure proposed values are less than or equal to existing flows.

Please include comparison for ponds 1 and 2 as well as the increase from OS2.

All proposed flows in the major storm leave the site at less than or equal to the historic flow rates. Therefore, there is no negative impact anticipated to downstream properties. All pond outfalls shall be designed with level flow spreaders to ensure that outflows from the pond are not concentrated and remain in sheet flow conditions to prevent erosive potential.

### **Channel Analysis and Design**

Drainageway WF-R8a was evaluated in its existing condition to analyze the existing floodplain and channel stability. In its current condition, WF-R8a is a heavily vegetated channel with weeds as tall as the typical flow depth meaning this would classify that channel as a natural minor stream with sluggish reaches, weedy and deep pools, per the El Paso County Drainage Criteria Manual Table 10-2. Given this classification, a Manning's roughness coefficient of 0.060 was used when analyzing the channel bottom and 0.045 on the sides which have less vegetation cover. The GeoHECRAS model determined that the existing channel has stable average velocities, with isolated instances of high

Pond 3 and 4.

velocities, ranging from 0.3 fps to 11.6 fps. Velocities are allowable based on the max stable velocity of 7 fps for erosion resistant channels, per Table 8-1 from MHFCD. There are only three instances where the velocities exceed that maximum value of 7 fps. Those are located in the middle of the drainageway crossing the site and shall be stabilized in the proposed condition. In the evaluated channel model, there is one instance where the Froude number exceeds the El Paso County maximum of 0.90. This are located at the middle of the drainageway. This part of the existing channel shall be revised in the proposed condition and stabilization measures shall be taken.

In the proposed section of the channel, there are several boulder drop structures proposed. Due to this, some velocities in the channel reach 19.2 fps and a Froude max of 2.8. These sections will be lined with riprap along bottom of the proposed channel and lined with erosion control blankets; this will mitigate the erosion risk associated with these higher velocities and Froude's. In addition to the protection discussed above, cutoff walls and reinforced rock berms will also be installed at all location where the Froude numbers exceed 0.90 to stabilize the channel against erosion.

Shear stresses present in the channel in its existing condition are approximately 1.50 lbs/sf on average, above the MHFCD Maximum Shear Stress of 1.2 lbs/sf per Table 8-3. In the proposed condition, the average shear stresses shall be improved using erosion prevention designs. The proposed dual 12'x5' RCBC culverts shall be designed with riprap, which will prevent soil erosion. The area just upstream of the proposed channel improvements will be lined in a TRM that will mitigate the potential for erosion due to the excess shear. The modeled results of the existing and proposed channel can be found in Appendix C. please identify whether the

Table 1: Cha	consistent with the DBPS. how						
Design Deremator	<b>Erosive Soils or</b>	F	do the proposed				
Design Parameter	<b>Poor Vegetation</b>	So	recommendations compare to				
Max Low-flow Velocity (ft/s)	3.5		the DBPS recommendations?				
Max 100-year Velocity (ft/s)	5.0		7.0				
Froude Number Low Flow	0.5		0.7				
Froude Number 100-year Flow	0.6		0.9				

proposed improvements are

In the Final Drainage Report, a No Rise Letter shall be provided evaluating how the proposed channel improvements will not adversely affect the floodplain width and water surface elevation.

## **DRAINAGE DESIGN CRITERIA**

### **Development Criteria Reference**

Storm drainage analysis and design criteria for the project were taken from the "City of Colorado Spring/El Paso County Drainage Criteria Manual" Volumes 1 and 2 (EPCDCM), dated October 12, 1994, the "Urban Storm Drainage Criteria Manual" Volumes 1 - 3 (USDCM) and Chapter 6 and Section 3.2.1 of Chapter 13 of the "Colorado Springs Drainage Criteria Manual (CCSDCM)", dated May 2014, as adopted by El Paso County, as well as the El Paso County "Engineering Criteria Manual" (ECM), dated October 14, 2020.

### Hydrologic Criteria

All hydrologic data was obtained from the "El Paso Drainage Criteria Manual" Volumes 1 and 2, and the "Urban Drainage and Flood Control District Urban Storm Drainage Criteria Manual" Volumes 1, 2, and 3. On-site flows were determined based on the 5-year (minor) storm event and the 100-year (major) storm event. Runoff was calculated using the Rational Method, and rainfall intensities for the 5-year and the 100-year storm return frequencies were obtained from Figure 6-5 Intensity Duration Frequency Curve of the Colorado Springs DCM. Runoff coefficients were determined based on proposed land use and from data in Table 6-6 from the DCM. One-hour point rainfall data for the storm events are 1.50 inches for the 5-year and 2.52 inches for the 100-year storm.

### Hydraulic Criteria

The Rational Method and USDCM's SF-2 and SF-3 forms were used to determine the runoff from the minor and major storms on the site. Autodesk Inc.'s Hydraflow Express Extension (Volume 10.5) was used to size the roadside ditches and drainage swales per criteria. Per Section 6.4.1 of the EPCDCM, culverts were sized as to not overtop the road in the 100-year storm. The MHFD-Detention\_v4.06 spreadsheet was utilized for evaluating proposed detention and water quality for the five ponds. Required detention volumes and allowable release rates were designed per USDCM and CCS/EPCDCM. CivilGEO Inc.'s GeoHECRAS was used to analyze the existing drainageway and the two proposed roadway crossings. See Appendix C for calculations. The hydraulic design will be finalized with the Final Drainage Report.

## **DRAINAGE FACILITY DESIGN**

### **General Concept**

The proposed stormwater conveyance system was designed to convey the developed Esteban Rodriguez Subdivision flows to one of four full-spectrum EDBs via roadside ditches and roadway culverts. All proposed full-spectrum EDBs will be designed to release flows at less than historic to minimize adverse impacts downstream. Due to this, there are no drainage problems anticipated downstream of the Esteban Rodriguez Subdivision development. The EDBs will outfall at two points of the existing drainageway and all proposed development shall stay out of the floodplain besides specific channel improvements and outfall stabilization.

The "Soil and Geology Study: Esteban Subdivision" prepared by Rocky Mountain Group showed some bore test results with groundwater located within 10 feet of the surface. The test borings taken were not located in the immediate vicinity of the proposed full-spectrum EDBs, but Ponds 1 and 2 may have some risk for shallow groundwater. When the final pond locations are determined with future analysis within the drainage reports submitted for development plans, additional test bore holes may be required. If shallow groundwater is an issue for any of the full-spectrum EDBs,

mitigation options such as clay or geomembrane layers shall be defined in the future drainage reports.

In accordance with Section I.7.1.B.5 of the ECM Stormwater Quality Policy and Procedure, developed basins with large lot single-family sites with a maximum of 10% impervious area shall be allowed to release runoff without a downstream permanent stormwater quality measure. In accordance with Section I.7.1.B.8, sites with constructing activity that is for the purpose of stream stabilization are also excluded from having a downstream permanent stormwater quality measure. See highlighted areas in the drainage map presented in Appendix E, as well as Table 2 in the Water Quality section.

#### **Specific Details**

All full-spectrum EDBs will have proposed forebays at inflow points, concrete trickle channels, and outlet structures. The proposed pond forebays and weir contain the required percentage of the Water Quality Capture Volume (WQCV). The forebays weir will release 2% or 3% of the undetained peak 100-year inflow (depending on impervious acres per EDB-4) into the full-spectrum EDB to the proposed concrete trickle channel. The trickle channel will direct flows into the proposed full-spectrum EDB outlet structure, which will detain water per times specified by criteria. The WQCV will be released within 40 hours and the EURV will be released within 72 hours.

#### Four Step Process to Minimize Adverse Impacts of Urbanization

In accordance with the El Paso County Drainage Criteria Manual Volume 2, this site has implemented the four step process to minimize adverse impacts of urbanization. The four step process includes reducing runoff volumes, treating the water quality capture volume (WQCV), stabilizing drainageways and implementing source controls.

Step 1: Reducing Runoff Volumes - The development of the project site is proposed as single-family residential (2.5-acre min.) with lawn areas interspersed within the development which helps disconnect impervious areas and reduce runoff volumes. Roadways will utilize roadside ditches to further disconnect impervious areas. Proposed flow in general follows the historic path over pervious surfaces into existing drainage paths. These practices will also allow for increased infiltration and reduce runoff volume.

Step 2: Provide WQCV - Runoff from this development is treated through capture and slow release of the WQCV in one of several on-site permanent full-spectrum EDBs that are be designed per current El Paso County drainage criteria. The 2.5-acre (minimum) residential lots will be limited to a maximum of 10% imperviousness to meet the requirements of Section I.7.1.B.5 of the ECM Stormwater Quality Policy and Procedure for water quality through a plat note. Should any lot exceed 10% imperviousness, a lot specific drainage report addressing the increased imperviousness must be submitted.

Also state that some areas are excluded from WQ treatment because of exclusion I.7.1.B.8 Step 3: Stabilize Drainageways - This site utilizes roadside ditches with culvert crossings throughout the site. Roadside ditches will be stabilized by keeping velocities below 5 ft/s, or providing additional erosion protection. These roadside ditches will then direct the applicable on-site and off-site development flows to one of several proposed full-spectrum EDBs within the project. Developed flows leaving the site are limited to below existing rates, and therefore no impact to downstream drainageways is anticipated. As part of the development the existing WF-R8a channel shall be improved for stability using boulder drop structures, riprap along bottom of the proposed channel lined with erosion control blankets, cutoff walls and reinforced rock berms. The existing stock pond shall be removed as well, which will prevent continued erosion.

Step 4: Implement Source Controls - A site specific stormwater quality and erosion control plan and narrative shall be prepared in conjunction with the final drainage report. Site specific temporary source control BMPs as well as permanent BMP's will be detailed in this plan and narrative to protect receiving waters.

#### Water Quality

In accordance with Section 13.3.2.1 of the CCS/EPCDCM, full-spectrum water quality and detention will be provided for all of the development site not meeting exclusions present in the ECM - Stormwater Quality Policy and Procedures Section I.7.1.B. As previously stated, the applicable exclusions for Basins B, C, D1-D2, F and I fall under Section I.7.1.B.5 of the ECM Stormwater Quality Policy and Procedure for areas with large single-family lots (2.5-acre min.). In addition, Basins D3-D5 fall under the Section I.7.1.B.8 of the ECM Stormwater Quality Policy and Procedure for stream stabilization sites. The proposed roadway will be treated within the proposed full-spectrum EDBs. Outlet structure release rates will be limited to less than historic rates to minimize adverse impacts to downstream stormwater facilities.

See Table 2 below for the water quality treatment summary table indicating which basins are treated and which are excluded.

PBMP Summary Table									
Basins	Tributary Area (acres)	PBMP							
A1-A7	76.0	POND 1							
В	0.74	EXCLUDED**							
С	15.8	EXCLUDED*							
D1-D2	15.5	EXCLUDED*							
D3-D5	39.9	EXCLUDED***							
E1-E3	73.8	POND 2							
F	22.0	EXCLUDED*							
G1-G5	71.7	POND 3							
H1-H6	128.8	POND 4							
I	46.8	EXCLUDED*							
*EXCLUDED BASED	ON LARGE-LOT SING ECM APP. 1.7.B.5	LE FAMILY SITE PER							
**EXCLUDED BASED	ON LAND DIST. TO U	NDEVELOPED LAND							
TO REMAIN U	NDEVELOPED PER EC	MAPP. I.7.B.7							
*** EXCLUDED BASI	ED ON STREAM STAB	ILIZATION SITE PER							
	ECM APP. I.7.B.8								

 Table 2 - Water quality treatment summary table.

See my comment on the WQ Treatment Summary Map on pg 185 below.

#### Proposed Full-Spectrum EDBs

Water quality is provided for the site by four private full-spectrum detention and water quality EDBs. Table 3 below shows the basin parameters for all four ponds. Refer to Appendix C for the MHFD-Detention design sheets that include the tributary basin parameters as well as the stage-storage table and outlet structure design. The outlet structure includes an orifice plate, overflow grate, and restrictor plate to release stormwater at the appropriate rates. The WQCV will be released within 40 hours, the EURV will be released within 72 hours, and the minor and major flows will be released at or below the pre-development flow rate. Table 4 below gives the designed results for Pond 1-4.

 Table 3 - Watershed design parameters for both EDBs.

Name	Watershed Area	Percent Impervious	Watershed Slope
Pond 1	78.0 ac	34.5%	0.035 ft/ft
Pond 2	77.0 ac	16.0%	0.040 ft/ft
Pond 3	72.0 ac	14.5%	0.040 ft/ft
Pond 4	129.0 ac	14.0%	0.045 ft/ft

Name	Required Volume (ac-ft)	Provided Volume (ac-ft)	WQCV (ac-ft)	EURV (ac-ft)	5-year Release (cfs)	100-year Release (cfs)
Pond 1	5.0	5.7	1.1	2.8	0.8	32.0
Pond 2	2.5	2.9	0.6	1.0	0.3	45.0
Pond 3	2.2	2.5	0.5	0.9	0.2	32.0
Pond 4	3.8	4.5	1.0	1.5	0.3	41.5

Calculations and pond design parameters are presented in Appendix C.

- For Pond 1, a broad-crested weir lined with buried soil riprap is provided as an emergency spillway along the southern embankment of the pond. Pond 1 emergency flows are conveyed via a proposed drainage swale to the proposed channel within the existing drainageway.
- For Pond 2, a broad-crested weir lined with buried soil riprap is provided as an emergency spillway along the northern embankment of the pond. Pond 2 emergency flows are conveyed via a proposed drainage swale to the proposed channel within the existing drainageway.
- For Pond 3, a broad-crested weir lined with buried soil riprap is provided as an emergency spillway along the southern embankment of the pond. Pond 3 emergency flows are conveyed via a proposed drainage swale to the proposed flow spreader before going off-site to the west, following the historic drainage patterns.
- For Pond 4, a broad-crested weir lined with buried soil riprap is provided as an emergency spillway along the southern embankment of the pond. Pond 4 emergency flows are conveyed via a proposed drainage swale to the proposed flow spreader before going off-site to the east, following the historic drainage patterns.

#### Erosion Control Plan

We respectfully request that the Final Erosion Control Plan and associated Cost Estimate to be submitted in conjunction with the construction drawings and plat prior to obtaining a grading permit.

#### **Operation & Maintenance**

In order to ensure the function and effectiveness of the stormwater infrastructure, maintenance activities such as inspection, routine maintenance, restorative maintenance, rehabilitation and repair, are required. All proposed drainage structures within any platted County R.O.W. (roadside ditches and local road culverts) will be owned and maintained by El Paso County. All proposed drainage structures within easements or tracts (full-spectrum water quality ponds, drainageway culverts and drainageway improvements) will be owned and maintained by the property owner unless another party accepts such responsibility in writing and responsibility is properly assigned through legal documentation. Inspection access for El Paso County will be provided through maintenance easements.

The LOI states that Public Open Space areas will be maintained by the Esteban Rodriguez Subdivision Metropolitan District or HOA. Please revise the above statement.

#### Drainage and Bridge Fees

The proposed site lies within both the Gieck Ranch and Haegler Ranch Drainage Basins. The drainage and basin fees will be assessed in conjunction with the construction drawings and plat prior to obtaining a grading permit.

#### **Construction Cost Opinion**

A construction cost opinion for the drainage infrastructure will be provided in conjunction with the construction drawings and plat prior to obtaining a grading permit.

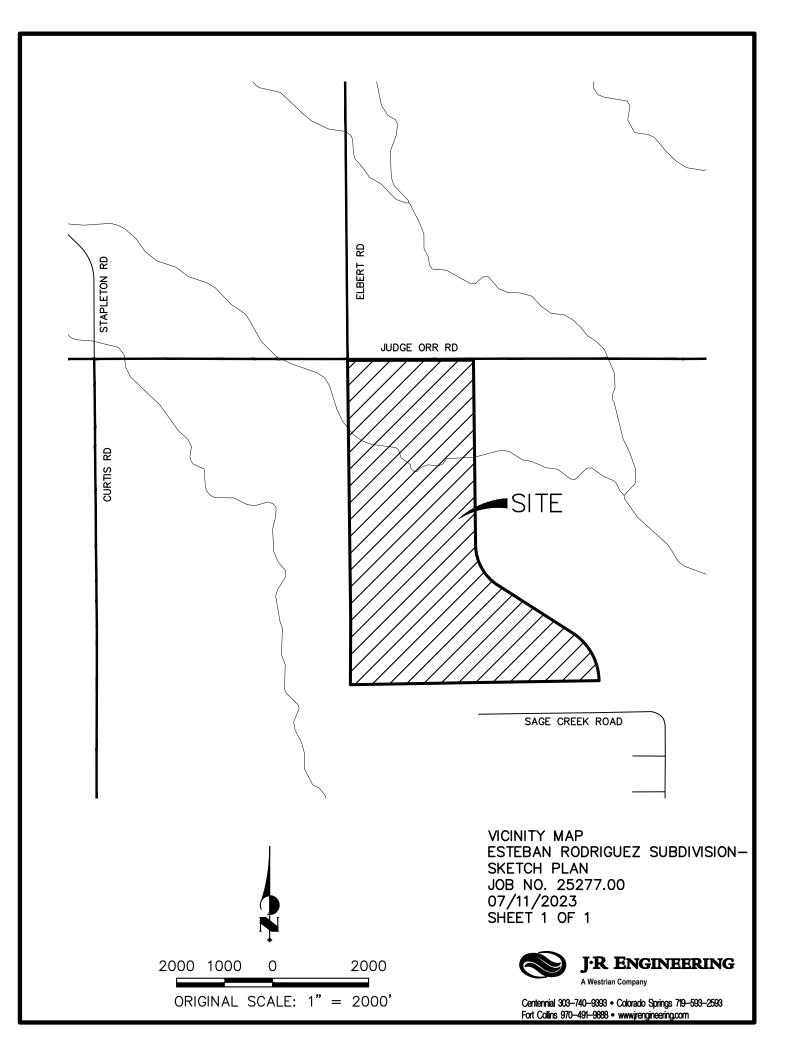
### SUMMARY

The Preliminary Drainage Report for Esteban Rodriguez Subdivision identifies on-site and off-site drainage patterns, storm sewer, culvert locations, areas tributary to the site, and safely routes developed storm water to adequate outfall facilities. The proposed Esteban Rodriguez Subdivision development will not adversely affect the off-site major drainageways or surrounding development. This report meets the latest El Paso County Drainage Criteria requirements for this site.

Preliminary Drainage Report for Esteban Rodriguez Subdivision

## APPENDIX A

## FIGURES AND EXHIBITS



This map is for use in administering the National Flood Insurance Program. It does not necessarily identify all areas subject to flooding, particularly from local drainage sources of small size. The community map repository should be consulted for possible updated or additional flood hazard information.

To obtain more detailed information in areas where Base Flood Elevations (BFEs) and/or floodways have been determined, users are encouraged to consult the Flood Profiles and Floodway Data and/or Summary of Stillwater Elevations tables contained within the Flood Insurance Study (FIS) report that accompanies this FIRM. Users should be aware that BFEs shown on the FIRM represent rounded whole-foot elevations. These BFEs are intended for flood insurance rating purposes only and should not be used as the sole source of flood elevation information. Accordingly, flood elevation data presented in the FIS report should be utilized in conjunction with the FIRM for purposes of construction and/or floodplain management.

Coastal Base Flood Elevations shown on this map apply only landward of 0.0' North American Vertical Datum of 1988 (NAVD88). Users of this FIRM should be aware that coastal flood elevations are also provided in the Summary of Stillwater Elevations table in the Flood Insurance Study report for this jurisdiction. Elevations shown in the Summary of Stillwater Elevations table should be used for construction and/or loodplain management purposes when they are higher than the elevations shown on this FIRM.

Boundaries of the floodways were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations with regard to requirements of the National Flood Insurance Program. Floodway widths and other pertinent floodway data are provided in the Flood Insurance Study report for this jurisdiction.

Certain areas not in Special Flood Hazard Areas may be protected by flood control structures. Refer to section 2.4 "Flood Protection Measures" of the Flood Insurance Study report for information on flood control structures for this jurisdiction.

The projection used in the preparation of this map was Universal Transverse Mercator (UTM) zone 13. The horizontal datum was NAD83, GRS80 spheroid. Differences in datum, spheroid, projection or UTM zones zones used in the production of FIRMs for adjacent jurisdictions may result in slight positional differences in map features across jurisdiction boundaries. These differences do not affect the accuracy of this FIRM.

Flood elevations on this map are referenced to the North American Vertical Datum of 1988 (NAVD88). These flood elevations must be compared to structure and ground elevations referenced to the same vertical datum. For information regarding conversion between the National Geodetic Vertical Datum of 1929 and the North American Vertical Datum of 1988, visit the National Geodetic Survey website a http://www.ngs.noaa.gov/ or contact the National Geodetic Survey at the following address:

NGS Information Services

NOAA, N/NGS12 National Geodetic Survey SSMC-3, #9202

1315 East-West Highway Silver Spring, MD 20910-3282

To obtain current elevation, description, and/or location information for bench marks shown on this map, please contact the Information Services Branch of the National Geodetic Survey at (301) 713-3242 or visit its website at http://www.ngs.noaa.gov/.

Base Map information shown on this FIRM was provided in digital format by El Paso County, Colorado Springs Utilities, and Anderson Consulting Engineers, Inc. These data are current as of 2008.

This map reflects more detailed and up-to-date stream channel configurations and floodplain delineations than those shown on the previous FIRM for this jurisdiction. The floodplains and floodways that were transferred from the previous FIRM may have been adjusted to conform to these new stream channel configurations. As a result, the Flood Profiles and Floodway Data tables in the Flood Insurance Study Report (which contains authoritative hydraulic data) may reflect stream channel distances that differ from what is shown on this map. The profile baselines depicted on this map represent the hydraulic modeling baselines that match the flood profiles and Floodway Data Tables if applicable, in the FIS report. As a result, the profile baselines may deviate significantly from the new base map channel representation ind may appear outside of the floodplain

Corporate limits shown on this map are based on the best data available at the time of publication. Because changes due to annexations or de-annexations may have occurred after this map was published, map users should contact appropriate community officials to verify current corporate limit locations.

Please refer to the separately printed Map Index for an overview map of the county showing the layout of map panels; community map repository addresses; and a Listing of Communities table containing National Flood Insurance Program dates for each community as well as a listing of the panels on which each community is located.

Contact FEMA Map Service Center (MSC) via the FEMA Map Information eXchange (FMIX) 1-877-336-2627 for information on available products associated with this FIRM. Available products may include previously issued Letters of Map Change, a Flood Insurance Study Report, and/or digital versions of this map. The MSC may also be reached by Fax at 1-800-358-9620 and its website at http://www.msc.fema.gov/.

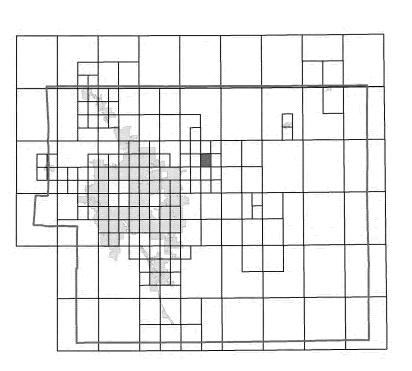
If you have **questions about this map** or questions concerning the National Flood Insurance Program in general, please call **1-877-FEMA MAP** (1-877-336-2627) or visit the FEMA website at http://www.fema.gov/business/nfip.

> El Paso County Vertical Datum Offset Table **Vertical Datum**

**Flooding Source** 

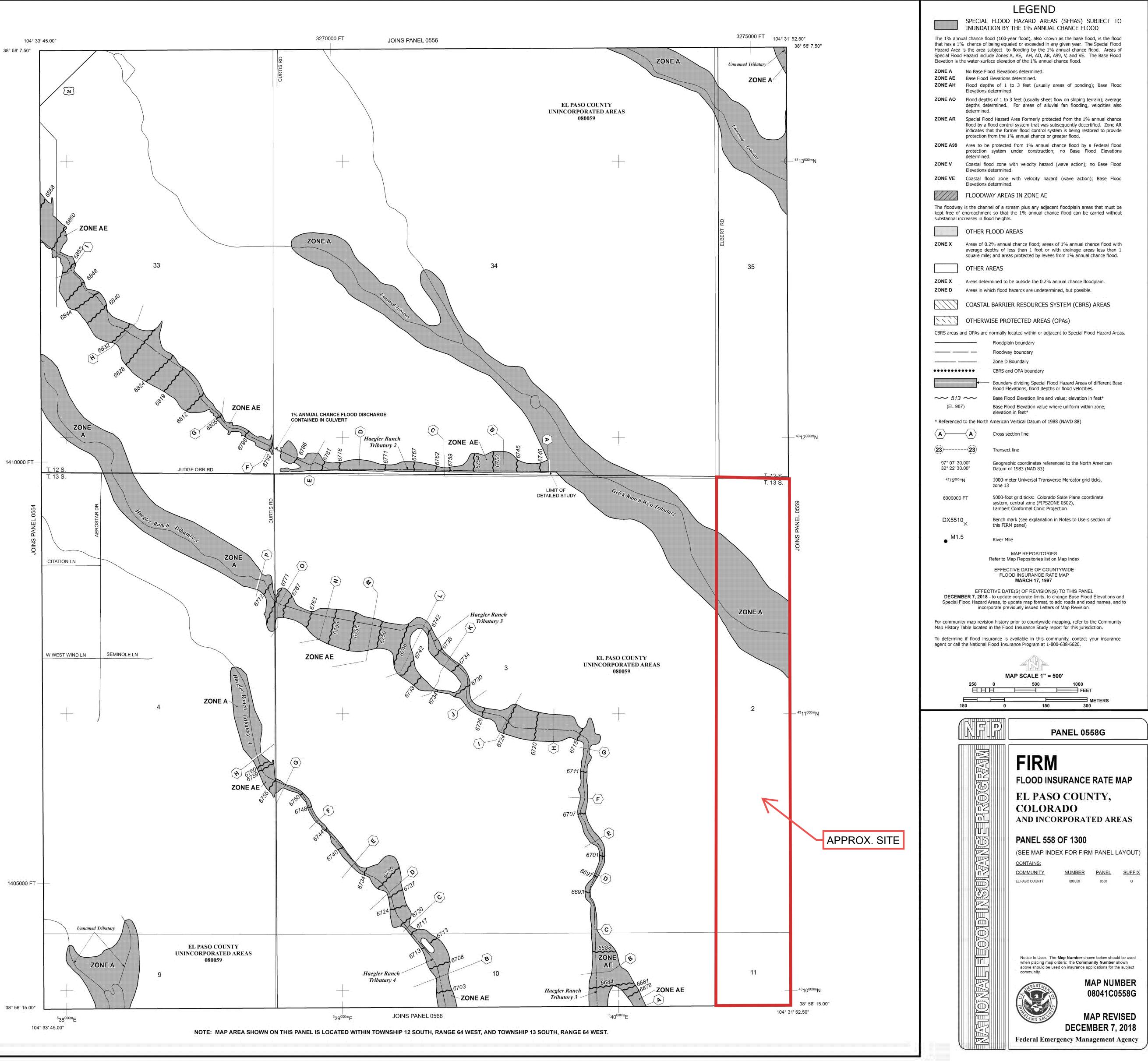
REFER TO SECTION 3.3 OF THE EL PASO COUNTY FLOOD INSURANCE STUDY FOR STREAM BY STREAM VERTICAL DATUM CONVERSION INFORMATION

#### Panel Location Map



This Digital Flood Insurance Rate Map (DFIRM) was produced through a Cooperating Technical Partner (CTP) agreement between the State of Colorado Water Conservation Board (CWCB) and the Federal Emergency Management Agency (FEMA).





This map is for use in administering the National Flood Insurance Program. It does not necessarily identify all areas subject to flooding, particularly from local drainage sources of small size. The community map repository should be consulted for possible updated or additional flood hazard information.

To obtain more detailed information in areas where Base Flood Elevations (BFEs) and/or floodways have been determined, users are encouraged to consult the Flood Profiles and Floodway Data and/or Summary of Stillwater Elevations tables contained within the Flood Insurance Study (FIS) report that accompanies this FIRM. Users should be aware that BFEs shown on the FIRM represent rounded whole-foot elevations. These BFEs are intended for flood insurance rating purposes only and should not be used as the sole source of flood elevation information. Accordingly, flood elevation data presented in the FIS report should be utilized in conjunction with the FIRM for purposes of construction and/or floodplain management.

Coastal Base Flood Elevations shown on this map apply only landward of 0.0' North American Vertical Datum of 1988 (NAVD88). Users of this FIRM should be aware that coastal flood elevations are also provided in the Summary of Stillwater Elevations table in the Flood Insurance Study report for this jurisdiction. Elevations shown in the Summary of Stillwater Elevations table should be used for construction and/or floodplain management purposes when they are higher than the elevations shown on this FIRM.

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NGS Information Services NOAA, N/NGS12

National Geodetic Survey SSMC-3, #9202

1315 East-West Highway Silver Spring, MD 20910-3282

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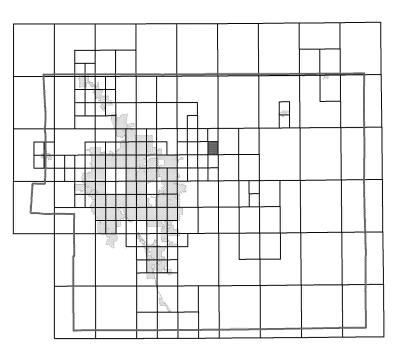
> El Paso County Vertical Datum Offset Table Vertical Datum

> > Offset (ft)

Flooding Source

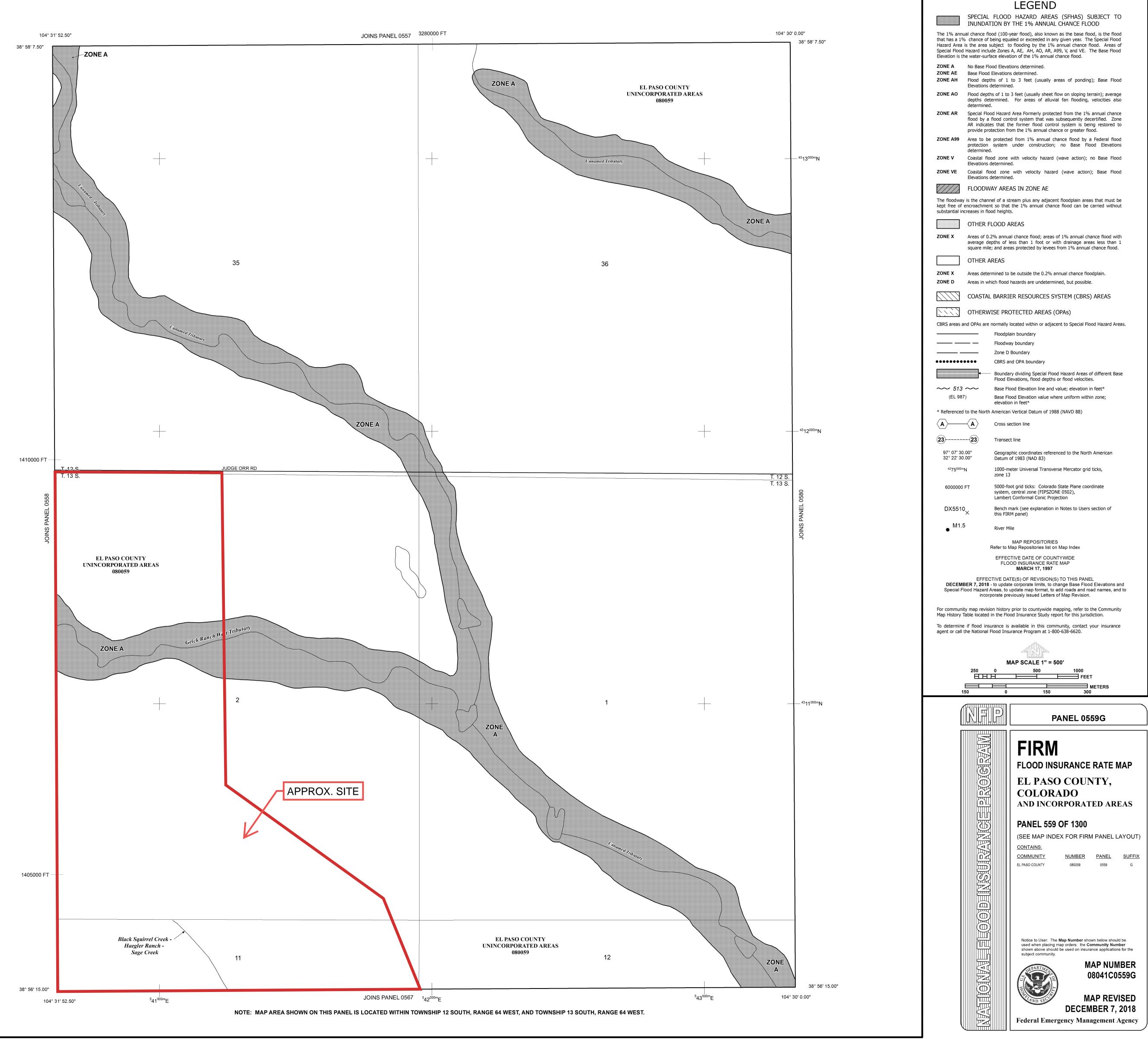
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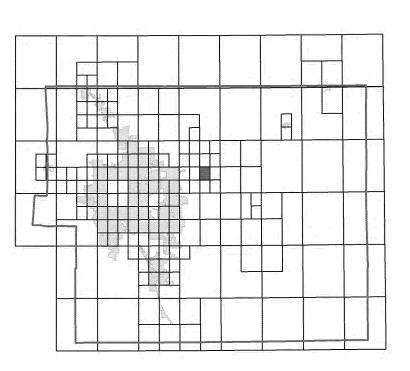
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**Flooding Source** 

El Paso County Vertical Datum Offset Table Vertical Datum

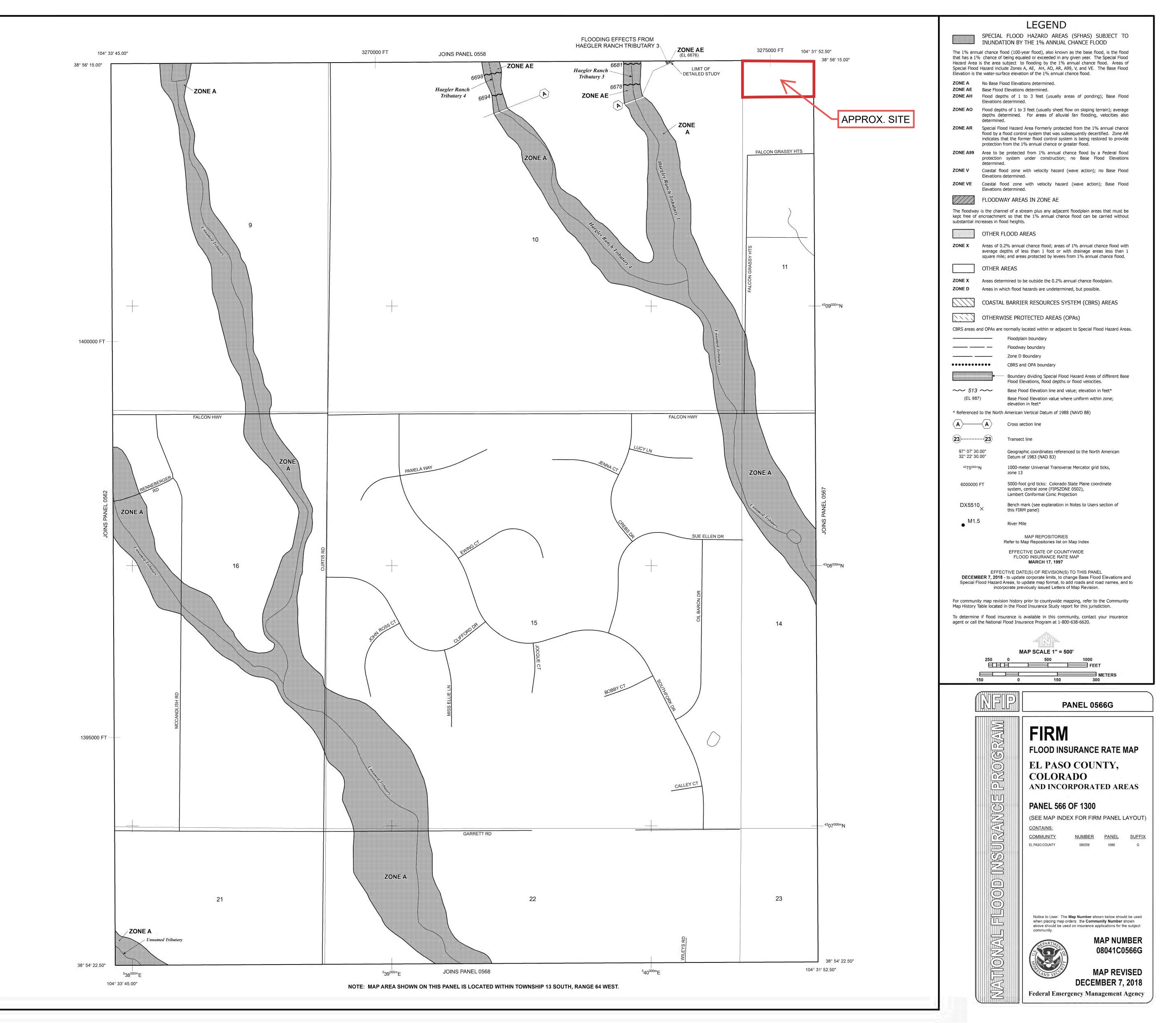
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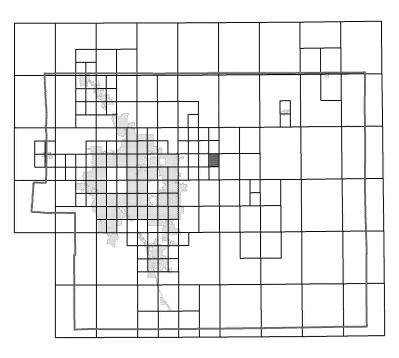
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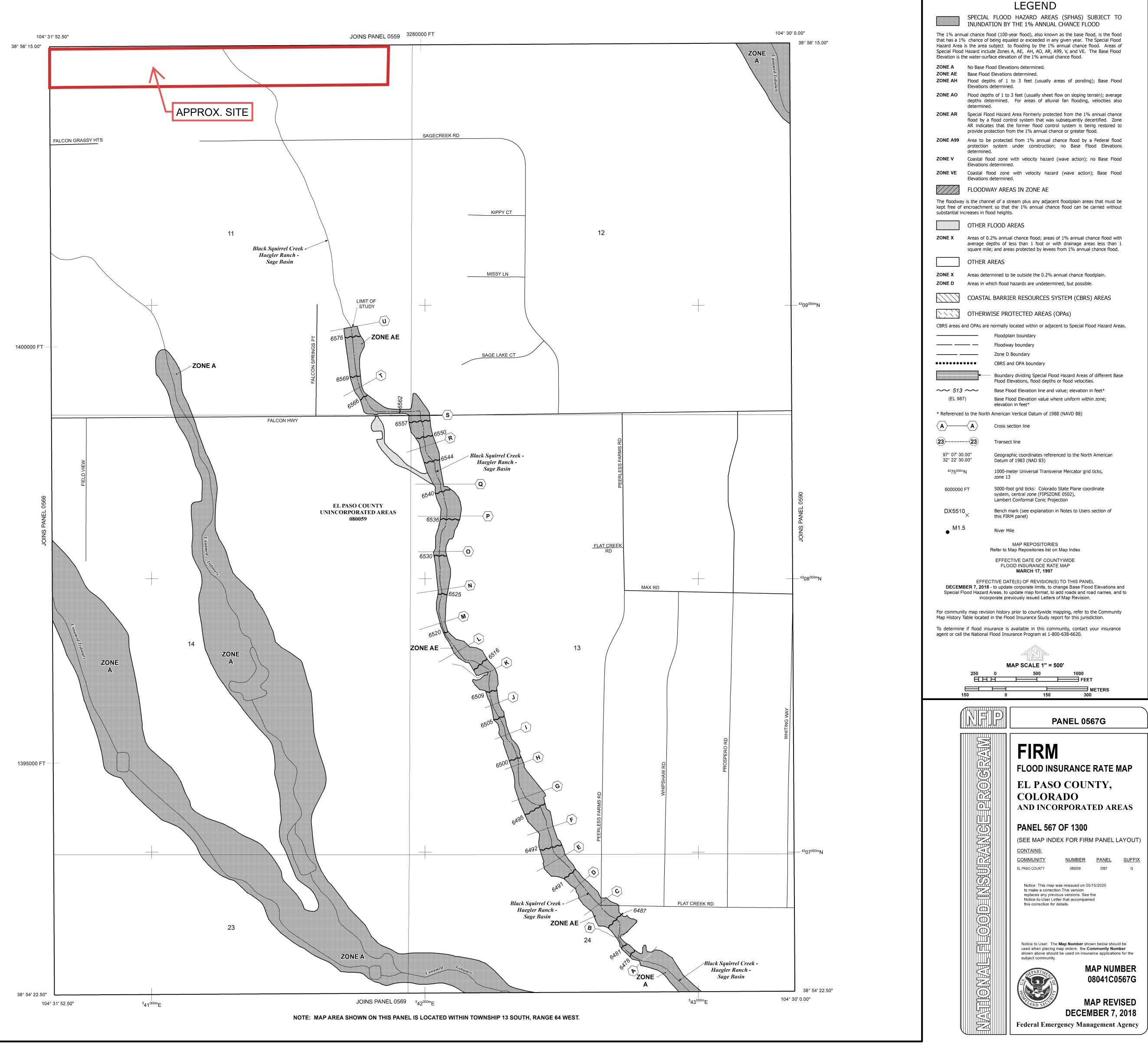
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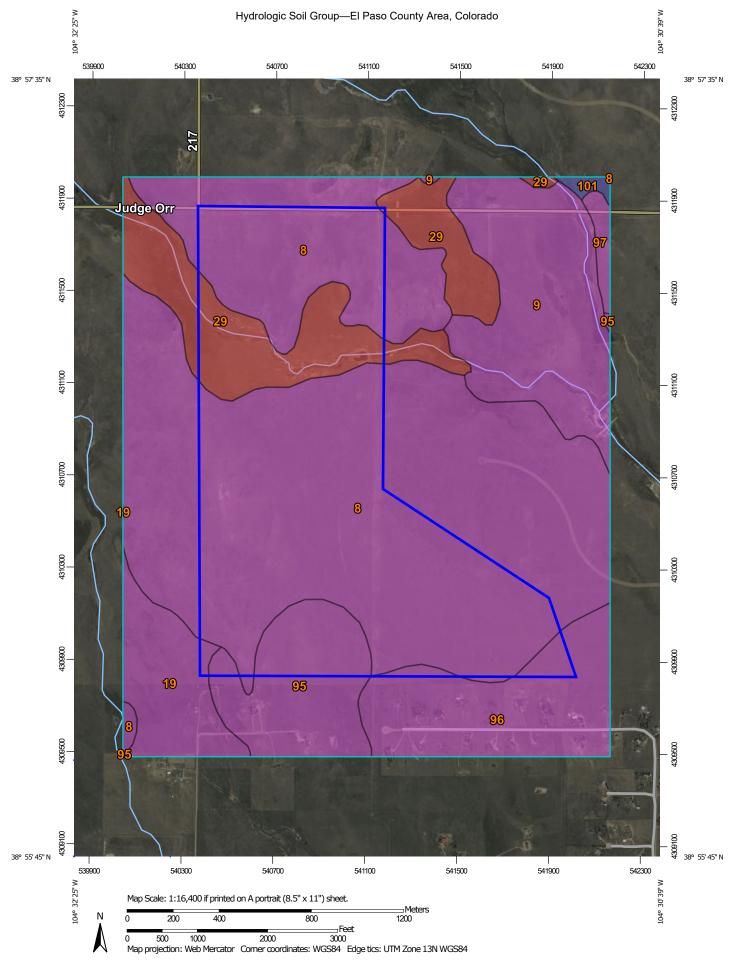
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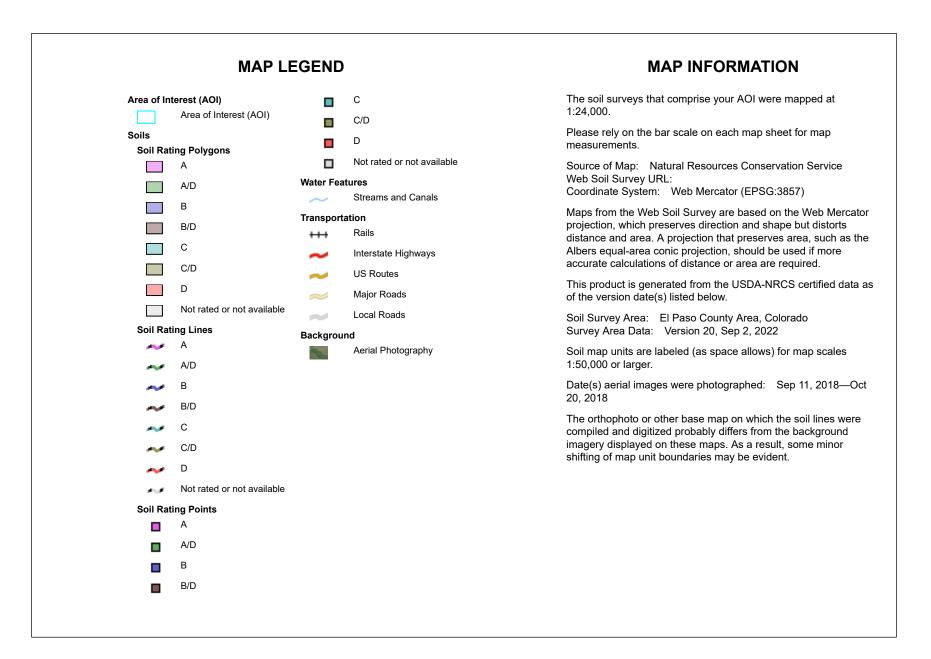
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USDA Natural Resources Conservation Service Web Soil Survey National Cooperative Soil Survey



# Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
8	Blakeland loamy sand, 1 to 9 percent slopes	A	759.5	57.4%
9	Blakeland-Fluvaquentic Haplaquolls	A	145.9	11.0%
19	Columbine gravelly sandy loam, 0 to 3 percent slopes	A	63.8	4.8%
29	Fluvaquentic Haplaquolls, nearly level	D	139.2	10.5%
95	Truckton loamy sand, 1 to 9 percent slopes	A	89.4	6.8%
96	Truckton sandy loam, 0 to 3 percent slopes	A	113.3	8.6%
97	Truckton sandy loam, 3 to 9 percent slopes	A	8.3	0.6%
101	Ustic Torrifluvents, loamy	В	3.8	0.3%
Totals for Area of Inter	rest		1,323.3	100.0%

### Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

### **Rating Options**

Aggregation Method: Dominant Condition Component Percent Cutoff: None Specified Tie-break Rule: Higher Preliminary Drainage Report for Esteban Rodriguez Subdivision

## APPENDIX B

## HYDROLOGIC CALCULATIONS

### EXISTING COMPOSITE % IMPERVIOUS/C VALUE CALCULATIONS

Subdivision: Esteban Rodriguez Subdivision

Location: El Paso County

Project Name: Esteban Rodriguez Subdivision-PDR

Project No.: 25277.00

Calculated By: GAG

Checked By:

Date: 8/6/24

				ardsca Impei	pe rvious)	Sin		mily (2 Imper	5-5 acre) vious)			develo Imperv				Basins Total Weighted %
Basin ID	Total Area (ac)	C <sub>5</sub>	C <sub>100</sub>	Area (ac)	Weighted % Imp.	$C_5$	C <sub>100</sub>	Area (ac)	Weighted % Imp.	$C_5$	C <sub>100</sub>	Area (ac)	Weighted % Imp.	C <sub>5</sub>	C <sub>100</sub>	Imp.
EXA	179.6	0.90	0.96	0.00	0.0%	0.16	0.4	0.00	0.0%	0.09	0.4	179.6	2.0%	0.09	0.36	2.0%
EXB	32.2	0.90	0.96	0.00	0.0%	0.16	0.4	0.00	0.0%	0.09	0.4	32.2	2.0%	0.09	0.36	2.0%
EXC	29.0	0.90	0.96	0.00	0.0%	0.16	0.4	0.00	0.0%	0.09	0.4	29.0	2.0%	0.09	0.36	2.0%
EXD	48.2	0.90	0.96	0.00	0.0%	0.16	0.4	0.00	0.0%	0.09	0.4	48.2	2.0%	0.09	0.36	2.0%
EXE	152.2	0.90	0.96	0.00	0.0%	0.16	0.4	0.00	0.0%	0.09	0.4	152.2	2.0%	0.09	0.36	2.0%
EXF	50.2	0.90	0.96	0.00	0.0%	0.16	0.4	0.00	0.0%	0.09	0.4	50.2	2.0%	0.09	0.36	2.0%
OS1	1.56	0.90	0.96	0.00	0.0%	0.16	0.4	0.00	0.0%	0.09	0.4	1.6	2.0%	0.09	0.36	2.0%
OS2	17.5	0.90	0.96	0.00	0.0%	0.16	0.4	17.5	10.0%	0.09	0.4	0.0	0.0%	0.16	0.41	10.0%
Total On-Site	491.40															<mark>2.0%</mark>

Should be a little higher than 2% because of the 10% imperviousness of OS2

#### **EXISTING STANDARD FORM SF-2** TIME OF CONCENTRATION

Subdivision: Esteban Rodriguez Subdivision

Location: El Paso County

Project Name: Esteban Rodriguez Subdivision-PDR

Project No.: 25277.00

Calculated By: GAG Checked By:

Date: 8/6/24

		SUB-	BASIN			INITI	AL/OVER	LAND		TRAVEL TIME					tc CHECK				
		DA	ATA				(T <sub>i</sub> ) (T <sub>t</sub> )							(URBANIZED BASINS)					
BASIN	D.A.	Hydrologic	Impervious	C <sub>5</sub>	C <sub>100</sub>	L	S <sub>o</sub>	t,	L <sub>t</sub>	S <sub>t</sub>	Κ	VEL.	t <sub>t</sub>	COMP. t <sub>c</sub>	TOTAL	Urbanized $t_c$	t <sub>c</sub>		
ID	(ac)	Soils Group	(%)			(ft)	(%)	(min)	(ft)	(%)		(ft/s)	(min)	(min)	LENGTH (ft)	(min)	(min)		
EXA	179.6	A	2%	0.09	0.36	-	-	-	-	-	-	-	-	-	-	-	-		
EXB	32.2	A	2%	0.09	0.36	300	3.0%	22.0	800	2.2%	7.0	1.0	12.8	34.8	1100.0	35.3	34.		
EXC	29.0	А	2%	0.09	0.36	300	2.7%	22.8	800	2.7%	7.0	1.2	11.6	34.3	1100.0	34.4	34.		
EXD	48.2	А	2%	0.09	0.36	300	3.1%	21.7	2635	3.1%	7.0	1.2	35.6	57.4	2935.0	52.5	52.		
EXE	152.2	А	2%	0.09	0.36	300	3.5%	20.9	3035	3.5%	7.0	1.3	38.6	59.5	3335.0	54.8	54.		
EXF	50.2	А	2%	0.09	0.36	300	3.8%	20.3	2330	3.8%	7.0	1.4	28.5	48.8	2630.0	47.1	47.		
OS1	1.56	А	2%	0.09	0.36	300	3.0%	22.0	30	1.0%	7.0	0.7	0.7	22.7	330.0	26.2	22.		
OS2	17.5	А	10%	0.16	0.41	300	3.5%	19.4	510	3.7%	7.0	1.3	6.3	25.8	810.0	28.5	25.8		
NOTES:														Table	e 6-2. NRCS Conv	veyance factors, K			
$t_c =$	$t_i + t_t$				Equation	6-2	$t_i = \frac{0.395}{1000}$	$\frac{(1.1-C_5)\sqrt{L_1}}{S_0^{0.33}}$				Equation	6-3	Type of Land	Conveyance				
Where:													Heavy me Tillage/f	2.5					
$t_c = c_c$	omputed time	of concentration (	minutes)			Where	Where:							Short pasture a	7				
$t_i = or$	$t_i$ = overland (initial) flow time (minutes)						$t_i$ = overland (initial) flow time (minutes) $C_5$ = runoff coefficient for 5-year frequency (from Table 6-4)							Nearly bare	10	8			
								$L_i = \text{length of overland flow (ft)}$							terway	15			

 $t_t$  = channelized flow time (minutes).

$$t_t = \frac{L_t}{60K_2/S_0} = \frac{L_t}{60V_2}$$

Where:

 $t_t =$  channelized flow time (travel time, min)

<i>t<sub>i</sub></i> = overland (initial) flow time (minutes)	
$C_5$ = runoff coefficient for 5-year frequency (from Table 6-4)	
$L_i$ = length of overland flow (ft)	
$S_o$ = average slope along the overland flow path (ft/ft).	

 $t_c$  = minimum time of concentration for first design point when less than  $t_c$  from Equation 6-1.

Equation 6-4 
$$t_c = (26 - 17i) + \frac{L_t}{60(14i + 9)\sqrt{S_t}}$$

Where:

Equation 6-5

Paved areas and shallow paved swales

 $L_t =$ waterway length (ft)  $S_o =$  waterway slope (ft/ft)  $V_t$  = travel time velocity (ft/sec) = K $\sqrt{S_o}$ K = NRCS conveyance factor (see Table 6-2).

 $L_t$  = length of channelized flow path (ft) *i* = imperviousness (expressed as a decimal)

 $S_t =$  slope of the channelized flow path (ft/ft).

Use a minimum  $t_c$  value of 5 minutes for urbanized areas and a minimum  $t_c$  value of 10 minutes for areas that are not considered urban. Use minimum values even when calculations result in a lesser time of concentration.

20

#### **EXISTING STANDARD FORM SF-3** STORM DRAINAGE SYSTEM DESIGN (RATIONAL METHOD PROCEDURE)

	Project Name: Esteban Rodriguez Subdivision-PDR	
Subdivision: Esteban Rodriguez Subdivision	Project No.: 25277.00	_
Location: El Paso County	Calculated By: GAG	_
Design Storm: 5-Year	Checked By:	_
	Date: 8/6/24	
		_

		DIRECT RUNOFF								TOTAL	RUNOFF	9	STREE	Т		PII	PE		TRAV	'EL TIN	ЛE		
STREET	Design Point	Basin ID	Area (Ac)	Runoff Coeff.	t <sub>c</sub> (min)	C*A (Ac)	l (in/hr)	Q (cfs)	tc (min)	C*A (ac)	l (in/hr)	Q (cfs)	O <sub>street</sub> (cfs)	C*A (ac)	Slope (%)	Q <sub>pipe</sub> (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	t <sub>t</sub> (min)	REMARKS
		OS1	1.56	0.09			2.90																Off-site flows onto the site on the west side Combines flow in Gieck Ranch West Tributary at DP1
		OS2	17.5	0.16		2.80																	Off-site flows onto the site on the west side Combines flow in Gieck Ranch West Tributary at DP1
		EXA	179.6	0.09	-	16.16	-	-															On-site flows sheet flow to Gieck Ranch West Tributary at DP1. Flows not anlyzed since studied
	1								-	-	-	86											Combined flows of OS1, OS2, and EXA Used Gieck Ranch DBPS reach flows from reference
	2	EXB	32.2	0.09	34.8	2.90	2.26	6.5															On-site flows sheet flow to east boudary at DP2 Historic path off-site to 16365 Judge Orr Road property
	3	EXC	29.0	0.09	34.3	2.61	2.28	5.9															On-site flows sheet flow to east boudary at DP3 Historic path off-site to Cowboy Ranch VW
	4	EXD	48.2	0.09	52.5	4.34	1.64	7.1															On-site flows sheet flow to southwest boundary at DP4 Historic path off-site to 7120 Falcon Grassy Hts
	5	EXE	152.2	0.09	54.8	13.70	1.58	21.6															On-site flows sheet flow to south boundary at DP5 Historic path off-site to 7360 Falcon Grassy Hts
	6	EXF	50.2	0.09	47.1	4.52	1.80	8.2															On-site flows sheet flow to southeast boundary at DP6 Historic path off-site to Sagecreek North Development

street and Pipe C^A values are determined by Q/I using the catchment's intensity value. \*Basin specific flows not analyzed since tributatry to Gieck Ranch West Tributary. Used reach flow from Gieck Ranch DBPS by Drexel, Barrel & Co. dated October 2007

#### **EXISTING STANDARD FORM SF-3** STORM DRAINAGE SYSTEM DESIGN (RATIONAL METHOD PROCEDURE)

					Project Name:	Esteban Rodriguez Sub	division-PDR	
Subdivision:	Esteb	an Rodriguez Subdivision			Project No.:	25277.00		
Location:	El Pas	o County			Calculated By:	GAG		
Design Storm:	100-Y	ear			Checked By:			
					Date:	8/6/24		
		DIRECT RUNOFF	TOTAL RUNOFF	STREET	PIPE	TRAVEL TIME		

		DIRECT RUNOFF							TOTAL RUNOFF					STREET			PIPE				EL TIN	ЛE	
STREET	Design Point	Basin ID	Area (ac)	Runoff Coeff.	t <sub>c</sub> (min)	C*A (ac)	(in/hr)	Q (cfs)	tc (min)	C*A (ac)	(in/hr)	Q (cfs)	O <sub>street</sub> (cfs)	C*A (ac)	Slope (%)	O <sub>pipe</sub> (cfs)	C*A (ac)	Slope (%)	<sup>o</sup> ipe Size (inches)	-ength (ft)	Velocity (fps)	t <sub>t</sub> (min)	REMARKS
																							Off-site flows onto the site on the west side
		OS1	1.56	0.36	22.7	0.56	4.87	2.7															Combines flow in Gieck Ranch West Tributary at DP1
		OS2	17.5	0.41	25.8	7.18	4.55	32.7															Off-site flows onto the site on the west side Combines flow in Gieck Ranch West Tributary at DP1
		EXA	170.6	0.36	_	64.66																	On-site flows sheet flow to Gieck Ranch West Tributary at DP1. Flows not anlyzed since studied
		LVU	179.0	0.30	-	04.00	-	-															Combined flows of OS1, OS2, and EXA
	1								-	-	-	753											Used Gieck Ranch DBPS reach flows from reference
	2	EXB	32.2	0.36	34.8	11.59	3.79	43.9															On-site flows sheet flow to east boudary at DP2 Historic path off-site to 16365 Judge Orr Road property
	3	EXC	29.0	0.36	34.3	10.44	3.82	39.9															On-site flows sheet flow to east boudary at DP3 Historic path off-site to Cowboy Ranch VW
	4	EXD	48.2	0.36	52.5	17.35	2.75	47.7															On-site flows sheet flow to southwest boundary at DP4 Historic path off-site to 7120 Falcon Grassy Hts
	5	EXE	152.2	0.36	54.8	54.79	2.65	145.0															On-site flows sheet flow to south boundary at DP5 Historic path off-site to 7360 Falcon Grassy Hts
	6	EXF	50.2	0.36	47.1	18.07	3.03	54.7															On-site flows sheet flow to southeast boundary at DP6 Historic path off-site to Sagecreek North Development
otes: reet and Pipe C*A val	ues are	determ	nined by	/ O/i usi	ina the	catchm	ent's in	tensity	value.														

Street and Pipe C\*A values are determined by Q/i using the catchment's intensity value. \*Basin specific flows not analyzed since tributatry to Gieck Ranch West Tributary. Used reach flow from Gieck Ranch DBPS by Drexel, Barrel & Co. dated October 2007

#### PROPOSED COMPOSITE % IMPERVIOUS/C VALUE CALCULATIONS

Subdivision: Esteban Rodriguez Subdivision Location: El Paso County 

 Project Name:
 Esteban Rodriguez Subdivision-PDR

 Project No.:
 25277.00

 Calculated By:
 GAG

 Checked By:
 Checked By:

				Hardscape )% Impervio			(80	Gravel % Impervio	us)			Commercia % Impervic		(2.5		Single-Fami re) (10% Im	5			Jndevelope % Impervic			l Weighted	Basins Total
Basin ID	Total Area	C	C	Area (ac)	Weighted	C	C	Area (ac)	Weighted	C	C	Area (ac)	Weighted	C	C	Area (ac)	Weighted	C	C	Area (ac)	Weighted	1 '		Weighted % Imp.
Basiii iD	(ac)	C <sub>5</sub>	C <sub>100</sub>	Alea (ac)	% Imp.	C <sub>5</sub>	C <sub>100</sub>	Alea (ac)	% Imp.	C <sub>5</sub>	C <sub>100</sub>	Alea (ac)	% Imp.	C <sub>5</sub>	C <sub>100</sub>	Alea (ac)	% Imp.	C <sub>5</sub>	C <sub>100</sub>	Alea (ac)	% Imp.	C <sub>5</sub>	C <sub>100</sub>	
A1	12.1	0.90	0.96	1.28	10.6%	0.59	0.70	0.00	0.0%	0.81	0.88	9.44	74.1%	0.16	0.41	0.00	0.0%	0.09	0.36	1.38	0.2%	0.74	0.83	84.9%
A2	4.18	0.90	0.96	0.88	21.2%	0.59	0.70	0.00	0.0%	0.81	0.88	2.21	50.3%	0.16	0.41	0.00	0.0%	0.09	0.36	1.08	0.5%	0.64	0.76	72.0%
A3	3.84	0.90	0.96	0.36	9.3%	0.59	0.70	0.00	0.0%	0.81	0.88	3.17	78.4%	0.16	0.41	0.00	0.0%	0.09	0.36	0.31	0.2%	0.76	0.85	87.9%
A4	4.15	0.90	0.96	0.78	18.7%	0.59	0.70	0.00	0.0%	0.81	0.88	0.00	0.0%	0.16	0.41	2.69	6.5%	0.09	0.36	0.68	0.3%	0.29	0.50	25.5%
A5	5.99	0.90	0.96	1.18	19.6%	0.59	0.70	0.00	0.0%	0.81	0.88	0.00	0.0%	0.16	0.41	3.48	5.8%	0.09	0.36	1.33	0.4%	0.29	0.51	25.9%
A6	38.2	0.90	0.96	2.23	5.8%	0.59	0.70	0.00	0.0%	0.81	0.88	0.00	0.0%	0.16	0.41	33.6	8.8%	0.09	0.36	2.35	0.1%	0.20	0.44	14.8%
A7	7.57	0.90	0.96	0.89	11.7%	0.59	0.70	0.14	1.5%	0.81	0.88	0.00	0.0%	0.16	0.41	5.8	7.6%	0.09	0.36	0.78	0.2%	0.25	0.47	21.0%
В	0.74	0.90	0.96	0.00	0.0%	0.59	0.70	0.00	0.0%	0.81	0.88	0.00	0.0%	0.16	0.41	0.00	0.0%	0.09	0.36	0.74	2.0%	0.09	0.36	2.0%
С	15.8	0.90	0.96	0.00	0.0%	0.59	0.70	0.00	0.0%	0.81	0.88	0.00	0.0%	0.16	0.41	15.8	10.0%	0.09	0.36	0.00	0.0%	0.16	0.41	10.0%
D1	4.49	0.90	0.96	0.00	0.0%	0.59	0.70	0.00	0.0%	0.81	0.88	0.00	0.0%	0.16	0.41	4.49	10.0%	0.09	0.36	0.00	0.0%	0.16	0.41	10.0%
D2	11.0	0.90	0.96	0.00	0.0%	0.59	0.70	0.00	0.0%	0.81	0.88	0.00	0.0%	0.16	0.41	11.0	10.0%	0.09	0.36	0.00	0.0%	0.16	0.41	10.0%
D3	29.6	0.90	0.96	0.00	0.0%	0.59	0.70	0.00	0.0%	0.81	0.88	0.00	0.0%	0.16	0.41	0.00	0.0%	0.09	0.36	29.6	2.0%	0.09	0.36	2.0%
D4	5.75	0.90	0.96	0.00	0.0%	0.59	0.70	0.00	0.0%	0.81	0.88	0.00	0.0%	0.16	0.41	0.00	0.0%	0.09	0.36	5.8	2.0%	0.09	0.36	2.0%
D5	4.53	0.90	0.96	0.00	0.0%	0.59	0.70	0.00	0.0%	0.81	0.88	0.00	0.0%	0.16	0.41	0.00	0.0%	0.09	0.36	4.5	2.0%	0.09	0.36	2.0%
E1	28.7	0.90	0.96	1.94	6.8%	0.59	0.70	0.00	0.0%	0.81	0.88	0.00	0.0%	0.16	0.41	25.1	8.7%	0.09	0.36	1.70	0.1%	0.21	0.44	15.6%
E2	1.63	0.90	0.96	0.88	53.7%	0.59	0.70	0.00	0.0%	0.81	0.88	0.00	0.0%	0.16	0.41	0.0	0.0%	0.09	0.36	0.76	0.9%	0.53	0.68	54.6%
E3	43.5	0.90	0.96	2.82	6.5%	0.59	0.70	0.14	0.3%	0.81	0.88	0.00	0.0%	0.16	0.41	38.1	8.8%	0.09	0.36	2.42	0.1%	0.21	0.44	15.6%
F	22.0	0.90	0.96	0.00	0.0%	0.59	0.70	0.00	0.0%	0.81	0.88	0.00	0.0%	0.16	0.41	22.0	10.0%	0.09	0.36	0.00	0.0%	0.16	0.41	10.0%
G1	17.6	0.90	0.96	0.72	4.1%	0.59	0.70	0.00	0.0%	0.81	0.88	0.00	0.0%	0.16	0.41	16.3	9.2%	0.09	0.36	0.63	0.1%	0.19	0.43	13.4%
G2	17.6	0.90	0.96	1.09	6.2%	0.59	0.70	0.00	0.0%	0.81	0.88	0.00	0.0%	0.16	0.41	15.6	8.8%	0.09	0.36	0.95	0.1%	0.20	0.44	15.1%
G3	5.70	0.90	0.96	0.85	15.0%	0.59	0.70	0.00	0.0%	0.81	0.88	0.00	0.0%	0.16	0.41	4.10	7.2%	0.09	0.36	0.75	0.3%	0.26	0.49	22.4%
G4	20.4	0.90	0.96	0.82	4.0%	0.59	0.70	0.05	0.2%	0.81	0.88	0.00	0.0%	0.16	0.41	18.8	9.2%	0.09	0.36	0.72	0.1%	0.19	0.43	13.5%
G5	10.4	0.90	0.96	0.03	0.3%	0.59	0.70	0.27	2.1%	0.81	0.88	0.00	0.0%	0.16	0.41	10.1	9.7%	0.09	0.36	0.00	0.0%	0.17	0.42	12.1%
H1	24.0	0.90	0.96	0.51	2.1%	0.59	0.70	0.00	0.0%	0.81	0.88	0.00	0.0%	0.16	0.41	23.1	9.6%	0.09	0.36	0.44	0.0%	0.17	0.42	11.7%
H2	41.8	0.90	0.96	0.87	2.1%	0.59	0.70	0.00	0.0%	0.81	0.88	0.00	0.0%	0.16	0.41	40.2	9.6%	0.09	0.36	0.76	0.0%	0.17	0.42	11.7%
H3	21.3	0.90	0.96	1.17	5.5%	0.59	0.70	0.00	0.0%	0.81	0.88	0.00	0.0%	0.16	0.41	19.1	9.0%	0.09	0.36	1.03	0.1%	0.20	0.44	14.6%
H4	1.96	0.90	0.96	1.04	53.2%	0.59	0.70	0.00	0.0%	0.81	0.88	0.00	0.0%	0.16	0.41	0.00	0.0%	0.09	0.36	0.91	0.9%	0.52	0.68	54.2%
H5	3.18	0.90	0.96	1.54	48.3%	0.59	0.70	0.00	0.0%	0.81	0.88	0.00	0.0%	0.16	0.41	0.30	0.9%	0.09	0.36	1.34	0.8%	0.49	0.65	50.1%
H6	36.6	0.90	0.96	0.08	0.2%	0.59	0.70	0.33	0.7%	0.81	0.88	0.00	0.0%	0.16	0.41	36.2	9.9%	0.09	0.36	0.00	0.0%	0.17	0.41	10.8%
1	46.8	0.90	0.96	0.00	0.0%	0.59	0.70	0.00	0.0%	0.81	0.88	0.00	0.0%	0.16	0.41	46.8	10.0%	0.09	0.36	0.00	0.0%	0.16	0.41	10.0%

				Hardscape 0% Impervi			(80	Gravel % Impervic	ous)			Commercia i% Impervio		(2.		Single-Fami cre) (10% Im	2			Jndevelope % Impervio		Basin Tota	al Weighted C	Basins Total
Basin ID	Total Area (ac)	$C_5$	C <sub>100</sub>	Area (ac)	Weighted % Imp.	$C_5$	C <sub>100</sub>	Area (ac)	Weighted % Imp.	$C_5$	C <sub>100</sub>	Area (ac)	Weighted % Imp.	$C_5$	C <sub>100</sub>	Area (ac)	Weighted % Imp.	$C_5$	C <sub>100</sub>	Area (ac)	Weighted % Imp.	C <sub>5</sub>	C <sub>100</sub>	Weighted % Imp.
OS1	1.56	0.90	0.96	0.13	8.1%	0.59	0.70	0.00		0.81	0.88	0.00		0.16	0.41	0.00		0.09	0.36	1.43	1.8%	0.16	0.41	9.9%
OS2a	14.5	0.90	0.96	0.00	0.0%	0.59	0.70	0.00	0.0%	0.81	0.88	0.00	0.0%	0.16	0.41	0.00	0.0%	0.09	0.36	14.5	2.0%	0.09	0.36	<b>2.0%</b>
OS2b	3.06	0.90	0.96	0.00	0.0%	0.59	0.70	0.00	0.0%	0.81	0.88	0.00	0.0%	0.16	0.41	0.00	0.0%	0.09	0.36	3.06	2.0%	0.09	0.36	2.0%
Total On-Site	491.1																							15.7%
Total Pond 1 (Basin OS1, A1-A7)	77.6																							34.4%
Total Pond 2 (Basin OS2b, E1-E3)	76.9																							15.9%
Total Pond 3 (Basin G1, G5)	71.7																							14.4%
Total Pond 4 (Basin H1 - H6)	128.8																					Y		13.5%

10% in existing calcs

### PROPOSED STANDARD FORM SF-2 TIME OF CONCENTRATION

Subdivision: Esteban Rodriguez Subdivision

Location: El Paso County

Project Name: Esteban Rodriguez Subdivision-PDR

Project No.: 25277.00

Calculated By: GAG

Checked By: \_\_\_\_\_\_ Date: #######

		SUB-I	BASIN			INITI	AL/OVER	LAND		TI	RAVEL TIM	E			tc CHECK		
		DA	ATA				(T <sub>i</sub> )				(T <sub>t</sub> )			(U	RBANIZED BA	SINS)	FINAL
BASIN	D.A.	Hydrologic	Impervious	C <sub>5</sub>	C <sub>100</sub>	L	S <sub>o</sub>	t <sub>i</sub>	L <sub>t</sub>	<i>S</i> <sub>t</sub>	K	VEL.	t <sub>t</sub>	COMP. t <sub>c</sub>	TOTAL	Urbanized $t_c$	t <sub>c</sub>
ID	(ac)	Soils Group	(%)			(ft)	(%)	(min)	(ft)	(%)		(ft/s)	(min)	(min)	LENGTH (ft)	(min)	(min)
A1	12.1	А	85%	0.74	0.83	100	2.0%	5.2	1390	2.0%	20.0	2.8	8.2	13.4	1490.0	19.4	13.4
A2	4.18	А	72%	0.64	0.76	31	2.0%	3.7	850	2.0%	20.0	2.8	5.0	8.7	881.0	19.0	8.7
A3	3.84	А	88%	0.76	0.85	31	2.0%	2.7	1150	2.0%	20.0	2.8	6.8	9.5	1181.0	17.4	9.5
A4	4.2	А	26%	0.29	0.50	100	3.0%	10.2	1935	2.0%	15.0	2.1	15.2	25.4	2035.0	39.8	25.4
A5	6.0	А	26%	0.29	0.51	26	2.0%	5.9	2905	2.0%	15.0	2.1	22.8	28.8	2931.0	48.7	28.8
A6	38.2	А	15%	0.20	0.44	26	2.0%	6.6	2945	2.0%	15.0	2.1	23.1	29.7	2971.0	54.8	29.7
A7	7.6	А	21%	0.25	0.47	26	2.0%	6.2	880	2.0%	15.0	2.1	6.9	13.2	906.0	31.1	13.2
В	0.74	А	2%	0.09	0.36	160	2.5%	17.0	0	0.0%	7.0	0.0	0.0	17.0	160.0	25.7	17.0
С	15.8	А	10%	0.16	0.41	100	2.5%	12.5	970	2.7%	15.0	2.5	6.6	19.1	1070.0	33.8	19.1
D1	4.49	D	10%	0.16	0.41	100	2.0%	13.5	175	3.0%	15.0	2.6	1.1	14.6	275.0	25.9	14.6
D2	11.0	D	10%	0.16	0.41	100	2.0%	13.5	580	3.0%	15.0	2.6	3.7	17.2	680.0	29.7	17.2
D3	29.6	D	2%	0.09	0.36	-	-	-	-	-	-	-	-	-	-	-	-
D4	5.75	D	2%	0.09	0.36	-	-	-	-	-	-	-	-	-	-	-	-
D5	4.53	D	2%	0.09	0.36	-	-	-	-	-	-	-	-	-	-	-	-
E1	28.7	А	16%	0.21	0.44	20	2.0%	5.7	2215	4.0%	15.0	3.0	12.3	18.0	2235.0	39.8	18.0
E2	1.6	А	55%	0.53	0.68	20	2.0%	3.7	2135	4.0%	15.0	3.0	11.9	15.6	2155.0	27.4	15.6
E3	43.5	А	16%	0.21	0.44	20	2.0%	5.7	3140	4.0%	15.0	3.0	17.4	23.2	3160.0	46.7	23.2
F	22.0	А	10%	0.16	0.41	100	2.3%	12.9	1800	2.0%	15.0	2.1	14.1	27.0	1900.0	44.7	27.0
G1	17.6	А	13%	0.19	0.43	100	3.0%	11.5	1675	2.0%	15.0	2.1	13.2	24.6	1775.0	41.9	24.6
G2	17.6	А	15%	0.20	0.44	100	3.0%	11.3	2175	2.0%	15.0	2.1	17.1	28.4	2275.0	46.5	28.4
G3	5.7	А	22%	0.26	0.49	31	2.0%	6.7	1415	2.0%	15.0	2.1	11.1	17.8	1446.0	35.9	17.8
G4	20.4	А	14%	0.19	0.43	100	4.0%	10.4	2655	3.0%	15.0	2.6	17.0	27.4	2755.0	47.2	27.4
G5	10.4	А	12%	0.17	0.42	100	3.0%	11.6	1065	2.0%	15.0	2.1	8.4	20.0	1165.0	35.7	20.0

### **PROPOSED STANDARD FORM SF-2** TIME OF CONCENTRATION

Subdivision: Esteban Rodriguez Subdivision

Location: El Paso County

Project Name: Esteban Rodriguez Subdivision-PDR

Project No.: 25277.00

Calculated By: GAG

Checked By:

Date: #######

		SUB-	BASIN			INITI	AL/OVER	LAND		T	RAVEL TIM	E			tc CHECK		
		DA	ATA				(T <sub>i</sub> )				(T <sub>t</sub> )			(U	RBANIZED BA	SINS)	FINAL
BASIN	D.A.	Hydrologic	Impervious	C <sub>5</sub>	C <sub>100</sub>	L	S <sub>o</sub>	t <sub>i</sub>	L <sub>t</sub>	S <sub>t</sub>	К	VEL.	t <sub>t</sub>	COMP. t <sub>c</sub>	TOTAL	Urbanized $t_c$	t <sub>c</sub>
ID	(ac)	Soils Group	(%)			(ft)	(%)	(min)	(ft)	(%)		(ft/s)	(min)	(min)	LENGTH (ft)	(min)	(min)
H1	24.0	А	12%	0.17	0.42	100	3.0%	11.6	1620	2.0%	15.0	2.1	12.7	24.4	1720.0	41.9	24.4
H2	41.8	А	12%	0.17	0.42	100	3.0%	11.6	2870	2.0%	15.0	2.1	22.5	34.2	2970.0	55.8	34.2
H3	21.3	А	15%	0.20	0.44	31	2.0%	7.2	2615	2.0%	15.0	2.1	20.5	27.8	2646.0	51.4	27.8
H4	1.96	А	54%	0.52	0.68	20	2.0%	3.7	3240	2.0%	15.0	2.1	25.5	29.2	3260.0	39.8	29.2
H5	3.2	А	50%	0.49	0.65	20	2.0%	3.9	3095	2.0%	15.0	2.1	24.3	28.2	3115.0	40.3	28.2
H6	36.6	А	11%	0.17	0.41	100	2.0%	13.4	3115	2.0%	15.0	2.1	24.5	37.9	3215.0	59.1	37.9
I	46.8	А	10%	0.16	0.41	100	7.0%	8.9	1500	3.0%	15.0	2.6	9.6	18.6	1600.0	38.2	18.6
OS1	1.56	А	10%	0.16	0.41	300	3.0%	20.6	30	1.0%	7.0	0.7	0.7	21.3	330.0	24.8	21.3
OS2a	14.5	А	2%	0.09	0.36	300	3.5%	20.9	515	3.7%	7.0	1.3	6.4	27.3	815.0	30.5	27.3
OS2b	3.06	А	2%	0.09	0.36	300	3.5%	20.9	190	3.0%	7.0	1.2	2.6	23.5	490.0	27.6	23.5
NOTES:						t,	$=\frac{0.395(1.1+1)}{S_o^0}$	$-C_5)\sqrt{L_i}$			Eq	juation 6-3		Table	6-2. NRCS Conve	yance factors, K	
$t_c =$	$t_i + t_t$			E	iquation 6-2	1	S,					с.		Type of Land S	Surface	Conveyance Fa	actor, K
Where:						Where:								Heavy mead		2.5	
$t_c = cc$	omputed time	of concentration (mir	utes)					itial) flow time	(minutes) ear frequency (fr	Table ( 4)				Tillage/fie Short pasture an	0.0050	5	
$t_i = \infty$	erland (initial	) flow time (minutes)	6			$L_i$	= length of o	verland flow (f	t)				-	Nearly bare g	200.2012 2021 2022	10	
$t_t = ch$	annelized flov	v time (minutes).						and the second se	verland flow path	$n(\pi/tt)$ .				Grassed wate	And Colored	15	
$t_t =$	$\frac{L_t}{60 K / S}$	$=\frac{L_t}{L_t}$		Equati	on 6-4	$t_c = (26 - 1)$	$7i) + \frac{L}{60(14i+1)}$	+9)√S,			Equ	ation 6-5	Paved	areas and shallow	w paved swales	20	

Equation 6-4 60K \S. 60V,

Where

tr = channelized flow time (travel time, min)

 $L_t =$ waterway length (ft)

 $S_o$  = waterway slope (ft/ft)  $V_t$  = travel time velocity (ft/sec) = K $\sqrt{S_o}$ 

K = NRCS conveyance factor (see Table 6-2).

Where:

 $t_c$  = minimum time of concentration for first design point when less than  $t_c$  from Equation 6-1.

 $L_t$  = length of channelized flow path (ft)

i = imperviousness (expressed as a decimal)  $S_t = \text{slope of the channelized flow path (ft/ft)}.$ 

Use a minimum  $t_c$  value of 5 minutes for urbanized areas and a minimum  $t_c$  value of 10 minutes for areas that are not considered urban. Use minimum values even when calculations result in a lesser time of concentration.

Subdivision:	Esteban Rodriguez Subdivision
Location:	El Paso County
Design Storm:	5-Year

Project Name: Esteban Rodriguez Subdivision-PDR Project No.: 25277.00 Calculated By: GAG

				DIRE	CT RUN	NOFF			Т	OTAL I	RUNOI	F		STREE	Т		PI	PE		TR	AVEL TI	ME	
STREET	Design Point	Basin ID	Area (Ac)	Runoff Coeff.	t <sub>c</sub> (min)	C*A (Ac)	l (in/hr)	Q (cfs)	tc (min)	C*A (ac)	l (in/hr)	Q (cfs)	O <sub>street</sub> (cfs)	C*A (ac)	Slope (%)	Q <sub>pipe</sub> (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	l endth (ft)	Velocity (fps)	t <sub>t</sub> (min)	REMARKS
																				Ī			Flows along roadside swales to the culvert at DP1
	1	A1	12.10	0.74	13.4	8.92	3.69	32.9					_			_							Combines flow at swale at DP2.1 Flows to the roadside swale at DP2
	2	A2	4 18	0.64	8.7	2.69	4 34	11.7															Combines flow at roadside swale at DP2
	-	7.2	1.10	0.01	0.7	2.07	1.01													-			Combines flow of DP1 and DP2 in roadside swale
	2.1								13.4	11.61	3.69	42.8											Flow combines at proposed swale at DP3.1
																							Flows to the proposed swale at DP3
	3	A3	3.84	0.76	9.5	2.92	4.21	12.3															Flow combines at proposed swale at DP3.1
	3.1								12.4	14.53	2 4 0	53.6								2	20 3.6	5 1.5	Combines flow of DP2.1 and DP3 at proposed swale Flow combines at roadside swale at DP4.1
	3.1								13.4	14.53	3.09	53.0								3.	20 3.0	0 1.0	Flows to the roadside swale at DP4.1
	4	A4	4.15	0.29	25.4	1.19	2.73	3.2															Flow combines at roadside swale at DP4.1
																							Combines flow of DP3.1 and DP4 at culvert
	4.1								14.9	15.72	3.53	55.5											Combines flow within Pond 1 at DP8.1
																							Off-site flows onto the site at DP5
	5	OS1	1.56	0.16	21.3	0.24	3.00	0.7															Enters Basin B2 and combines at DP6.1
																							Flows along roadside swale to DP6
	6	A5	5.99	0.29	28.8	1.74	2.54	4.4												_			Combines flow at DP6.1 Combines flow of DP5 and DP6 at swale and culvert
	6.1								20.0	1.98	2.54	5.0											Flow continues within a swale and combines at DP8.1
	0.1								20.0	1.90	2.34	5.0								-			Flow continues within a swale and combines at DP8. T Flows to roadside swales to culvert at DP7
	7	A6	38.20	0.20	29.7	7.60	2.49	19.0															Combines flow within Pond 1 at DP8.1
		7.0	00.20	0.20	2717	7100	2.17	1710															Sheet flows to swales and enter Pond 1 at DP8
	8	A7	7.57	0.25	13.2	1.87	3.72	7.0															Combines flow within Pond 1 at DP8.1
																							Combines flow of DP4, DP6.1, DP7 and DP8 in Pond 1
	8.1								29.7	27.17	2.49	67.8											Flows released through Pond 1 EDB outlet DP8.2
																							Controlled release from Pond 1 outlet at DP8.2
	8.2								-	-	-	0.8											Released into drainageway, follows historic path east
							0.07													Γ			Sheet flows overland to east boundary
	<u> </u>	В	0.74	0.09	17.0	0.07	3.33	0.2							<u> </u>		<u> </u>			-			Combines flow along eastern boundary at DP9
	1	С	15.80	0.14	19.1	2.53	3.16	8.0												1			Sheet flows overland to east boundary Combines flow along eastern boundary at DP9
		U.	15.00	0.10	17.1	2.55	5.10	0.0												$\vdash$	_		Combines flow of Basins B and C at east boundary
	9								19,1	2.60	3.16	8.2											Historic path off-site to 16365 Judge Orr Road property

Subdivision:	Esteban Rodriguez Subdivision
Location:	El Paso County

Design Storm: 5-Year

Project Name: Esteban Rodriguez Subdivision-PDR Project No.: 25277.00 Calculated By: GAG

				DIREC	CT RUN	NOFF			T	OTAL	RUNO	F		STREE	Г		Р	IPE		TRA	/EL TI	ИE	
STREET	Design Point	Basin ID	Area (Ac)	Runoff Coeff.	$t_c$ (min)	C*A (Ac)	l (in/hr)	Q (cfs)	tc (min)	C*A (ac)	l (in/hr)	Q (cfs)	Q <sub>street</sub> (cfs)	C*A (ac)	Slope (%)	Q <sub>pipe</sub> (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	t <sub>t</sub> (min)	REMARKS
		OS2a	14.50	0.09	27.3	1.31	2.62	3.4															Off-site flows from Saddlehorn Ranch F4 & F5 Flows through Basin D2 to drainageway then DP4 On-site flows follow historic path to drainageway
		D1	4.49	0.16	14.6	0.72	3.56	2.6															Flows east and to east site boundary at DP4
		D2	11.00	0.16	17.2	1.76	3.31	5.8															On-site flows follow historic path to drainageway Flows east and to east site boundary at DP4
		D3	29.60			2.66	-	-															On-site flows within Gieck Ranch West Tributary Flows east and to east site boundary at DP4
		D4	5.75	0.09	-	0.52	-	-															On-site flows within Gieck Ranch West Tributary Flows east and to east site boundary at DP4
		D5	4.53		_	0.41	_	_															On-site flows within Gieck Ranch West Tributary Flows east and to east site boundary at DP4
	10			0107		0.111			-	-	-	86											Combination of Basins OS2a and D1-D5 Used Gieck Ranch DBPS reach flow from reference
	11	OS2b	3.06	0.09	23.5	0.28	2.85	0.8															Off-site flows from Saddlehorn Ranch F5 to DP11 Flows through Basin E1 to DP12.1
	12	E1	28.70	0.21	18.0	5.91	3.24	19.2															Flows along roadside swale to DP12 Combines at culvert at DP12.1
	12.1								18.0	6.19	3.24	20.1											Combines flow of DP11 and DP12 Flows along swale and combines at DP14.1
	13	E2	1.63	0.53	15.6	0.86	3.47	3.0															Flows along roadside swale to DP13 Combines flow within Pond 2 at DP14.1
	14	E3	43.50	0.21	23.2	8.93	2.87	25.6															Flows along roadside swales to DP14 Combines flow within Pond 2 at DP14.1
	14.1								23.2	15.98	2.87	45.8											Combines flow of DP4, DP6.1, DP7 and DP8 in Pond 2 Flows released through Pond 2 EDB outlet DP8.2
	14.2								-	-	-	0.3											Controlled release from Pond 2 outlet at DP8.2 Released into drainageway, follows historic path east
	15	F	22.00	0.16	27.0	3.52	2.64	9.3															Sheet flows overland to east boundary at DP6 Historic path off-site to Cowboy Ranch VW property

	Project Name: E	.stebar
Subdivision: Esteban Rodriguez Subdivision	Project No.: 2	5277.0
Location: El Paso County	Calculated By: G	GAG
Design Storm: 5-Year	Checked By:	
	Date: 1	0/21/2

	1				CT RUN				т	OTAL I		-г	6	STREE	г		ים	IPE		TDAY	EL TIN	1	
				DIRE		NOFF					KUINOI	1		SIKEE	I		PI	IPE		IKAV		/IÉ	
STREET	Design Point	Basin ID	Area (Ac)	Runoff Coeff.	t <sub>c</sub> (min)	C*A (Ac)	l (in/hr)	Q (cfs)	tc (min)	C*A (ac)	l (in/hr)	Q (cfs)	O <sub>street</sub> (cfs)	C*A (ac)	Slope (%)	Q <sub>pipe</sub> (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	$t_t$ (min)	REMARKS
	16	G1	17.60	0.19	24.6	3.30	2.78	9.2												1760	3.5	8.4	Flows along roadside swale to DP16 Combines flow at DP17.1 culvert
	17	G2	17.60	0.20	28.4	3.55	2.56	9.1															Flows along roadside swale to DP17 Combines flow at DP17.1 culvert
	17.1									6.85	2.34	16.0								475	3.5	2.3	Combines flow of DP16 and DP17 at culvert Combines flow at DP18.1 culvert
	18	G3	5.70	0.26	17.8	1.49	3.26	4.9															Flows along roadside swales to DP18 Combines flow at DP18.1 culvert
	18.1									8.34	2 24	18.7											Combines flow of DP17.1 and DP18 at culvert Combines flow at DP19.1 swale
	19	G4	20.40	0.19	27.4	3.84	2.61	10.0															Flows along roadside swale to DP19 Combines flow at DP19.1 swale
	19.1									12.18	2.24	27.3								685	3.5	3.3	Combines flow of DP18.1 and DP19 at swale Flows along proposed swale to Pond 3 at DP20.1
	20	G5	10.40	0.17	20.0	1.80	3.09	5.6															Flows along proposed swale to DP20 Flows along proposed swale to Pond 3 at DP20.1
	20.1								38.5	13.98	2.11	29.4											Combines flow of DP19.1 and DP20 into Pond 3 Flows released through Pond 3 EDB outlet DP20.2
	20.2								-	-	-	0.2											Controlled release from Pond 3 outlet at DP20.2 Flow spreader and then follows historic path west
	21	H1	24.00	0.17	24.4	4.18	2.79	11.7												1435	3.6	6.6	Flows along roadside swales to DP21 Combines flow at DP22.1
	22	H2	41.80	0.17	34.2	7.28	2.29	16.6															Flows along roadside swales to DP22 Combines flow at DP22.1
	22.1									11.46	2.29	26.2								430	3.6	2.0	Combines flow of DP21 and DP22 Flows along roadside swale to DP23.1
	23	H3	21.30	0.20	27.8	4.20	2.60	10.9															Flows along roadside swale to DP23.1 Combines flow at DP23.1 culvert
	23.1									15.66	2.20	34.5											Combines flow of DP22.1 and DP23 Flow continues to DP25.1
	24	H4	1.96	0.52	29.2	1.02	2.52	2.6															Flows along roadside swale to DP24 Combines flow at DP24.1 swale

Project Name: Esteban Rodriguez Subdivision-PDR Project No.: 25277.00

Subdivision:	Esteban Rodriguez Subdivision
Location:	El Paso County

Design Storm: 5-Year

Project Name: Esteban Rodriguez Subdivision-PDR Project No.: 25277.00 Calculated By: GAG Checked By: \_\_\_\_\_\_

Date: 10/21/24

				DIRE	CT RUN	NOFF			Т	OTAL F	RUNOF	F	0,	STREE	Г		PI	PE		TRAV	EL TIN	1E	
STREET	Design Point	Basin ID	Area (Ac)	Runoff Coeff.	t <sub>c</sub> (min)	C*A (Ac)	l (in/hr)	Q (cfs)	tc (min)	C*A (ac)	l (in/hr)	Q (cfs)	O <sub>street</sub> (cfs)	C*A (ac)	Slope (%)	Q <sub>pipe</sub> (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	t <sub>t</sub> (min)	REMARKS
	24.1								36.2	16.68	2.20	36.7								1040	3.6	4.8	Combines flow of DP23.1 and DP24 Flow continues to DP25.1 swale
	25	H5	3.18	0.49	28.2	1.55	2.57	4.0															Flows within swale to DP25 Combines flow within Pond 4 at DP24.1
	25.1								41.0	18.23	2.01	36.7								435	3.6	2.0	Combines flow of DP24.1 and DP25 Combines flow within Pond 4 at DP26.1
	26	H6	36.60	0.17	37.9	6.06	2.13	12.9															Flows along roadside swales to DP26 Combines flow at DP26.1
	26.1								43.0	24.29	1.94	47.1											Combines flow of DP25.1 and DP26 into Pond 4 Flows released through Pond 4 EDB outlet DP26.2
	26.2								-	-	-	0.3											Controlled release from Pond 4 outlet at DP26.2 Flow spreader and then follows historic path south
																							Sheet flows overland to southern boundary at DP27
	27	1	46.80	0.16	18.6	7.49	3.20	24.0															Historic path off-site to 7360 Falcon Grassy Hts

\*Basin specific flows not analyzed since tributary to Gieck Ranch West Tributary. Used reach flow from Gieck Ranch DBPS by Drexel, Barrel & Co. dated October 2007

n Rodriguez Subdivision County ar	Project Name: Esteban Rodriguez Subdivision-PDR Project No.: 25277.00 Calculated By: GAG Checked By: 10/21/24	_
	Date: 10/21/24	_

	Esteban Rodriguez Subdivision
	El Paso County
Design Storm:	100-Year
•	

	Ι	Ι		DIRE	CT RUN	IOFF				OTAL	RUNO	FF		STREE	Т		PI	IPE		TRAV	'EL TIN	ЛE	
STREET	Design Point	Basin ID	Area (ac)	Runoff Coeff.	t <sub>c</sub> (min)	C*A (ac)	l (in/hr)	Q (cfs)	tc (min)	C*A (ac)	l (in/hr)	Q (cfs)	Q <sub>street</sub> (cfs)	C*A (ac)	Slope (%)	Q <sub>pipe</sub> (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	t <sub>t</sub> (min)	REMARKS
																							Flows along roadside swales to the culvert at DP1
	1	A1	12.10	0.83	13.4	10.03	6.20	62.1															Combines flow at swale at DP2.1 Flows to the roadside swale at DP2
	2	A2	4.18	0.76	8.7	3.19	7.29	23.3															Combines flow at roadside swale at DP2.1
	2.1					-			13.4	13.22	6.20	81.9											Combines flow of DP1 and DP2 in roadside swale Flow combines at proposed swale at DP3.1
																							Flows to the proposed swale at DP3
	3	A3	3.84	0.85	9.5	3.24	7.06	22.9															Flow combines at proposed swale at DP3.1
																							Combines flow of DP2.1 and DP3 at proposed swale
	3.1								13.4	16.46	6.20	102.0								320	5.0	1.1	Flow combines at roadside swale at DP4.1 Flows to the roadside swale at DP4
	4	A4	4 15	0.50	25.4	2.09	4 58	9.6															Flow combines at roadside swale at DP4.1
				0.00	2011	2.07		7.0															Combines flow of DP3.1 and DP4 at culvert
	4.1								14.5	18.55	6.00	111.3											Combines flow within Pond 1 at DP8.1
																							Off-site flows onto the site at DP5
	5	OS1	1.56	0.41	21.3	0.64	5.03	3.2															Enters Basin B2 and combines at DP6.1
	6	A5	5.99	0 5 1	<u> 10 0</u>	3.04	1 27	13.0															Flows along roadside swale to DP6 Combines flow at DP6.1
	0	AD	5.99	0.51	28.8	3.04	4.27	13.0															Combines flow of DP5 and DP6 at swale and culvert
	6.1								28.8	3.68	4.27	15.7											Flow continues within a swale and combines at DP8.1
												_											Flows to roadside swales to culvert at DP7
	7	A6	38.20	0.44	29.7	16.77	4.19	70.2															Combines flow within Pond 1 at DP8.1
	8	A7	7.57	0.47	13.2	3.59	6.24	22.4															Sheet flows to swales and enter Pond 1 at DP8 Combines flow within Pond 1 at DP8.1
																							Combines flow of DP4, DP6.1, DP7 and DP8 in Pond 1
	8.1								29.7	42.59	4.19	178.3											Flows released through Pond 1 EDB outlet DP8.2
	0.0																						Controlled release from Pond 1 outlet at DP8.2
	8.2								-	-	-	32.0											Released into drainageway, follows historic path east
							_																Sheet flows overland to east boundary
		В	0.74	0.36	17.0	0.27	5.59	1.5					<u> </u>										Combines flow along eastern boundary at DP9
		С	15.80	0.41	19.1	6.48	5.30	34.4															Sheet flows overland to east boundary Combines flow along eastern boundary at DP9
	9								19.1	6.75	5.30	35.8											Combines flow of Basins B and C at east boundary Historic path off-site to 16365 Judge Orr Road property

	Project Name: Esteban Rodriguez Subdivision-PDR
Subdivision: Esteban Rodriguez Subdivision	Project No.: 25277.00
	Calculated By: GAG
Design Storm: 100-Year	Checked By:
	Date: 10/21/24

		DIRECT RUNOFF								TOTAL RUNOFF STREET								IPE		TRA	EL TIN	ЛF	
	<u> </u>	<u> </u>		DINE						5 IVE		•	<u> </u>										
STREET	Design Point	Basin ID	Area (ac)	Runoff Coeff.	t <sub>c</sub> (min)	C*A (ac)	l (in/hr)	Q (cfs)	tc (min)	C*A (ac)	l (in/hr)	Q (cfs)	Q <sub>street</sub> (cfs)	C*A (ac)	Slope (%)	O <sub>pipe</sub> (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	$t_t$ (min)	REMARKS
		OS2a	14.50	0.36	27.3	5.22	4.40	23.0															Off-site flows from Saddlehorn Ranch F4 & F5 Flows through Basin D2 to drainageway then DP4
		D1	4.49	0.41	14.6	1.84	5.97	11.0															On-site flows follow historic path to drainageway Flows east and to east site boundary at DP4
		D2	11.00																				On-site flows follow historic path to drainageway Flows east and to east site boundary at DP4
		D2	29.60			10.66	-	-															On-site flows within Gieck Ranch West Tributary
																							Flows east and to east site boundary at DP4 On-site flows within Gieck Ranch West Tributary
		D4	5.75			2.07	-	-															Flows east and to east site boundary at DP4 On-site flows within Gieck Ranch West Tributary
		D5	4.53	0.36	-	1.63	-	-															Flows east and to east site boundary at DP4 Combination of Basins OS2a and D1-D5
	10								-	-	-	753											Used Gieck Ranch DBPS reach flow from reference
	11	OS2b	3.06	0.36	23.5	1.10	4.78	5.3															Off-site flows from Saddlehorn Ranch F5 to DP11 Flows through Basin E1 to DP12.1
	12	E1	28.70	0.44	18.0	12.75	5.44	69.4															Flows along roadside swale to DP12 Combines at culvert at DP12.1
	12.1								18.0	13.85	5.44	75.4											Combines flow of DP11 and DP12 Flows along swale and combines at DP14.1
	13	E2	1.63	0.68	15.6	1.11	5.82	6.5															Flows along roadside swale to DP13 Combines flow within Pond 2 at DP14.1
	14	E3		0.44		19.30																	Flows along roadside swales to DP14 Combines flow within Pond 2 at DP14.1
		EG	43.00	0.44	23.2	19.30	4.01	72.9		24.07	4.07	1/ 1 2											Combines flow of DP4, DP6.1, DP7 and DP8 in Pond 2
	14.1								23.2	34.26	4.81	164.9											Flows released through Pond 2 EDB outlet DP8.2 Controlled release from Pond 2 outlet at DP8.2
	14.2								-	-	-	45.0											Released into drainageway, follows historic path east
																							Sheet flows overland to east boundary at DP6
	15	F	22.00	0.41	27.0	9.02	4.43	39.9															Historic path off-site to Cowboy Ranch VW property

	Project Name: Esteban Rodriguez Subdivision-PDR
Subdivision: Esteban Rodriguez Subdivision	Project No.: 25277.00
Location: El Paso County	Calculated By: GAG
Design Storm: 100-Year	Checked By:
	Date: 10/21/24

	1			DIRE	CT RUN	IOFF				TOTAL	RUNO	FF		STREE	Т	1	PI	PE		TRAV	EL TIN	ЛE		
STREET	Design Point	Basin ID	Area (ac)	Runoff Coeff.	t <sub>c</sub> (min)	C*A (ac)	l (in/hr)	Q (cfs)	tc (min)	C*A (ac)	l (in/hr)	Q (cfs)	O <sub>street</sub> (cfs)	C*A (ac)	Slope (%)	O <sub>pipe</sub> (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	$t_t$ (min)	REMARKS	
	16	G1	17.60	0.43	24.6	7.58	4.66	35.3												1760	5.0	5.9	Flows along roadside swale to DP16 Combines flow at DP17.1 culvert	
	17	G2	17.60	0.44	28.4	7.77	4.30	33.4															Flows along roadside swale to DP17 Combines flow at DP17.1 culvert	
	17.1								30.5	15.35	4.12	63.3								475	5.0	1.6	Combines flow of DP16 and DP17 at culvert Combines flow at DP18.1 culvert	
	18	G3	5.70	0.49	17.8	2.77	5.48	15.2															Flows along roadside swales to DP18 Combines flow at DP18.1 culvert	
	18.1								32.1	18.12	4.00	72.4											Combines flow of DP17.1 and DP18 at culvert Combines flow at DP19.1 swale	
	19	G4	20.40	0.43	27.4	8.79	4.39	38.6															Flows along roadside swale to DP19 Combines flow at DP19.1 swale	
	19.1								32.1	26.91	4.00	107.5								685	5.0	2.3	Combines flow of DP18.1 and DP19 at swale Flows along proposed swale to Pond 3 at DP20.1	
	20	G5	10.40	0.42	20.0	4.36	5.18	22.6															Flows along proposed swale to DP20 Flows along proposed swale to Pond 3 at DP20.1	
	20.1								34.4	31.27	3.82	119.5											Combines flow of DP19.1 and DP20 into Pond 3 Flows released through Pond 3 EDB outlet DP20.2	
	20.2								-	-	-	32.0											Controlled release from Pond 3 outlet at DP20.2 Flow spreader and then follows historic path west	
	21	H1	24.00	0.42	24.4	10.10	4.69	47.4												1435	5.0	4.8	Flows along roadside swales to DP21 Combines flow at DP22.1	
	22	H2	41.80		34.2																		Flows along roadside swales to DP22 Combines flow at DP22.1	
	22.1								34.2	27.68	3.84	106.2								430	6.0	1.2	Combines flow of DP21 and DP22 Flows along roadside swale to DP23.1	
	23	H3	21.30	0.44	27.8	9.33	4.36	40.7															Flows along roadside swale to DP23.1 Combines flow at DP23.1 culvert	
	23.1								35.4	37.01	3.75	138.7											Combines flow of DP22.1 and DP23 Flow continues to DP25.1	
	24	H4	1.96	0.68	29.2	1.33	4.23	5.6		57.01	00	100.7											Flows along roadside swale to DP24 Combines flow at DP24.1 swale	

ban Rodriguez Subdivision	
iso County	

Subdivision: Esteban R Location: El Paso Co Design Storm: 100-Year

ject Name: Esteban Rodriguez Subdivision-PDR
--

Project Name: Esteban Ro Project No.: 25277.00 Calculated By: GAG Checked By: Date: 10/21/24

		DIRECT RUNOFF								OTAL	runo	FF		STREE	Т		PI	PE		TRAV	'EL TIN	ЛE	
STREET	Design Point	Basin ID	Area (ac)	Runoff Coeff.	t <sub>c</sub> (min)	C*A (ac)	l (in/hr)	Q (cfs)	tc (min)	C*A (ac)	l (in/hr)	Q (cfs)	O <sub>street</sub> (cfs)	C*A (ac)	Slope (%)	O <sub>pipe</sub> (cfs)	C*A (ac)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	$t_t$ (min)	REMARKS
	24.1								35.4	38.34	3.75	143.7								1040	7.5	2.3	Combines flow of DP23.1 and DP24 Flow continues to DP25.1 swale
	25	H5	3.18	0.65	28.2	2.08	4.32	9.0															Flows within swale to DP25 Combines flow within Pond 4 at DP24.1
	25.1								37.7	40.42	3.59	145.1								435	7.5	1.0	Combines flow of DP24.1 and DP25 Combines flow within Pond 4 at DP26.1
	26	H6	36.60	0.41	37.9	15.15	3.58	54.2															Flows along roadside swales to DP26 Combines flow at DP26.1
	26.1								38.7	55.57	3.53	195.9											Combines flow of DP25.1 and DP26 into Pond 4 Flows released through Pond 4 EDB outlet DP26.2
	26.2									-		41.5											Controlled release from Pond 4 outlet at DP26.2 Flow spreader and then follows historic path south
	27	I	46.80	0.41	18.6	19.19	5.38	103.1															Sheet flows overland to southern boundary at DP27 Historic path off-site to 7360 Falcon Grassy Hts
tes: eet and Pipe C*A val asin specific flows no	lues are	determ	nined by	Q/i usi	ng the o	catchme	nt's int	ensity v	value.		5	0: 1.2					10.0				0.07		

### APPENDIX C

### HYDRAULIC CALCULATIONS

as this is a preliminary drainage report , further review of the hydraulic calculations will be provided with the final drainage report in conjuction with the CD's. These hydraulic calcs. should be removed.

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### **DP1-Culvert**

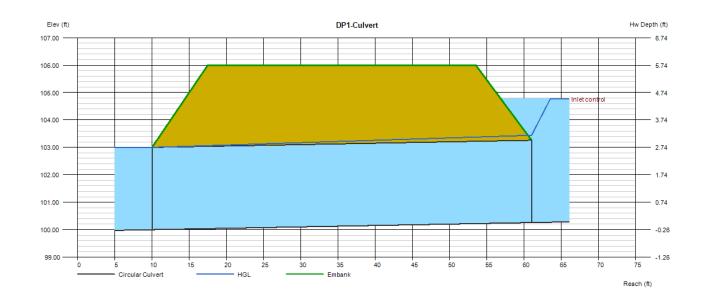
Invert Elev Dn (ft)	= 100.00	Calculations	
Pipe Length (ft)	= 51.00	Qmin (cfs)	= 62.00
Slope (%)	= 0.51	Qmax (cfs)	= 62.00
Invert Elev Up (ft)	= 100.26	Tailwater Elev (ft)	= Normal
Rise (in)	= 36.0		
Shape	= Circular	Highlighted	
Span (in)	= 36.0	Qtotal (cfs)	= 62.00
No. Barrels	= 1	Qpipe (cfs)	= 62.00
n-Value	= 0.013	Qovertop (cfs)	= 0.00
Culvert Type	= Circular Concrete	Veloc Dn (ft/s)	= 8.77
Culvert Entrance	= Groove end projecting (C)	Veloc Up (ft/s)	= 8.77
Coeff. K,M,c,Y,k	= 0.0045, 2, 0.0317, 0.69, 0.2	HGL Dn (ft)	= 103.00
		HGL Up (ft)	= 103.44
Embankment		Hw Elev (ft)	= 104.76

### Embankment

Top Elevation (ft) Top Width (ft) Crest Width (ft)

=	106.00
=	36.00
=	100.00

inginginea		
Qtotal (cfs)	=	62.00
Qpipe (cfs)	=	62.00
Qovertop (cfs)	=	0.00
Veloc Dn (ft/s)	=	8.77
Veloc Up (ft/s)	=	8.77
HGL Dn (ft)	=	103.00
HGL Up (ft)	=	103.44
Hw Elev (ft)	=	104.76
Hw/D (ft)	=	1.50
Flow Regime	=	Inlet Control

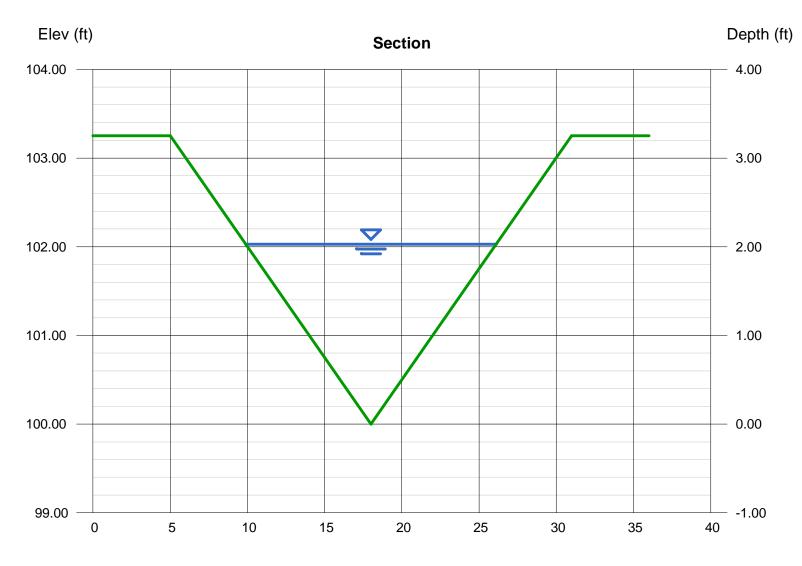


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Tuesday, Aug 13 2024

### **DP2.1-Swale**

Triangular		Highlighted	
Side Slopes (z:1)	= 4.00, 4.00	Depth (ft)	= 2.03
Total Depth (ft)	= 3.25	Q (cfs)	= 82.00
		Area (sqft)	= 16.48
Invert Elev (ft)	= 100.00	Velocity (ft/s)	= 4.97
Slope (%)	= 1.05	Wetted Perim (ft)	= 16.74
N-Value	= 0.030	Crit Depth, Yc (ft)	= 1.93
		Top Width (ft)	= 16.24
Calculations		EGL (ft)	= 2.41
Compute by:	Known Q		
Known Q (cfs)	= 82.00		



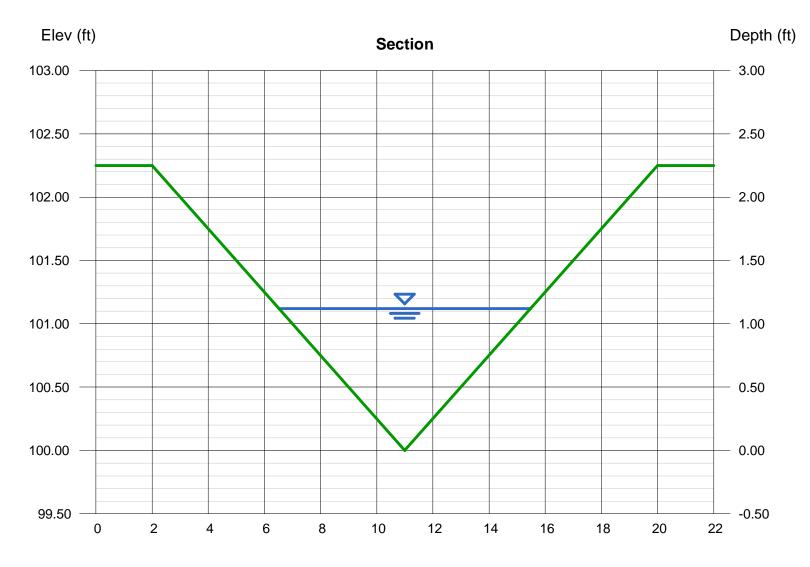
Reach (ft)

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### **DP3-Swale**

Triangular		Highlighted	
Side Slopes (z:1)	= 4.00, 4.00	Depth (ft)	= 1.12
Total Depth (ft)	= 2.25	Q (cfs)	= 23.00
		Area (sqft)	= 5.02
Invert Elev (ft)	= 100.00	Velocity (ft/s)	= 4.58
Slope (%)	= 2.00	Wetted Perim (ft)	= 9.24
N-Value	= 0.030	Crit Depth, Yc (ft)	= 1.16
		Top Width (ft)	= 8.96
Calculations		EGL (ft)	= 1.45
Compute by:	Known Q		
Known Q (cfs)	= 23.00		



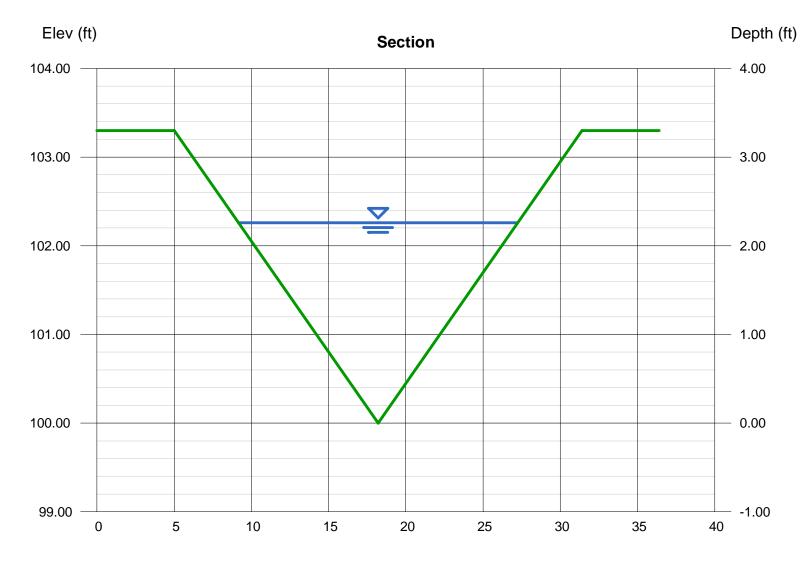
Reach (ft)

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### **DP3.1-Swale**

Triangular		Highlighted	
Side Slopes (z:1)	= 4.00, 4.00	Depth (ft)	= 2.26
Total Depth (ft)	= 3.30	Q (cfs)	= 102.00
		Area (sqft)	= 20.43
Invert Elev (ft)	= 100.00	Velocity (ft/s)	= 4.99
Slope (%)	= 0.90	Wetted Perim (ft)	= 18.64
N-Value	= 0.030	Crit Depth, Yc (ft)	= 2.10
		Top Width (ft)	= 18.08
Calculations		EGL (ft)	= 2.65
Compute by:	Known Q		
Known Q (cfs)	= 102.00		



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### **DP4.1-Pond 1 Inflow**

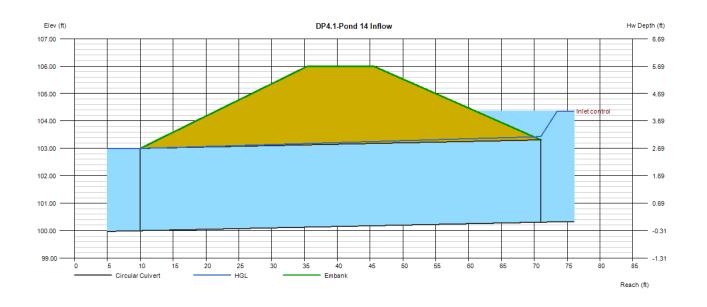
Invert Elev Dn (ft) Pipe Length (ft) Slope (%) Invert Elev Up (ft) Rise (in)	= 100.00 = 61.00 = 0.51 = 100.31 = 36.0	<b>Calculations</b> Qmin (cfs) Qmax (cfs) Tailwater Elev (ft)	= 112.00 = 112.00 = Normal
Shape	= Circular	Highlighted	
Span (in)	= 36.0	Qtotal (cfs)	= 112.00
No. Barrels	= 2	Qpipe (cfs)	= 112.00
n-Value	= 0.013	Qovertop (cfs)	= 0.00
Culvert Type	= Circular Concrete	Veloc Dn (ft/s)	= 7.92
Culvert Entrance	<ul> <li>Groove end projecting (C)</li> </ul>	Veloc Up (ft/s)	= 7.92
Coeff. K,M,c,Y,k	= 0.0045, 2, 0.0317, 0.69, 0.2	HGL Dn (ft)	= 103.00
		HGL Up (ft)	= 103.43
Embankment		Hw Elev (ft)	= 104.36

Top Elevation (ft)

Top Width (ft) Crest Width (ft)

=	106.00
=	10.00
=	100.00

Inginginea		
Qtotal (cfs)	=	112.00
Qpipe (cfs)	=	112.00
Qovertop (cfs)	=	0.00
Veloc Dn (ft/s)	=	7.92
Veloc Up (ft/s)	=	7.92
HGL Dn (ft)	=	103.00
HGL Up (ft)	=	103.43
Hw Elev (ft)	=	104.36
Hw/D (ft)	=	1.35
Flow Regime	=	Inlet Control



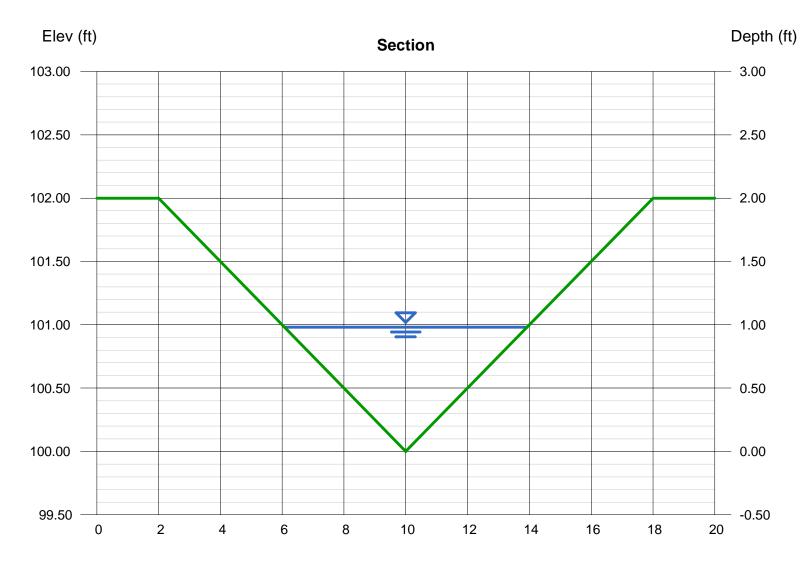
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### DP6.1-Swale

Triangular		Highlighted	
Side Slopes (z:1)	= 4.00, 4.00	Depth (ft)	= 0.98
Total Depth (ft)	= 2.00	Q (cfs)	= 16.00
		Area (sqft)	= 3.84
Invert Elev (ft)	= 100.00	Velocity (ft/s)	= 4.16
Slope (%)	= 2.00	Wetted Perim (ft)	= 8.08
N-Value	= 0.030	Crit Depth, Yc (ft)	= 1.00
		Top Width (ft)	= 7.84
Calculations		EGL (ft)	= 1.25
Compute by:	Known Q		
Known Q (cfs)	= 16.00		



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### **DP6.1-Culvert/ Pond 1 Inflow**

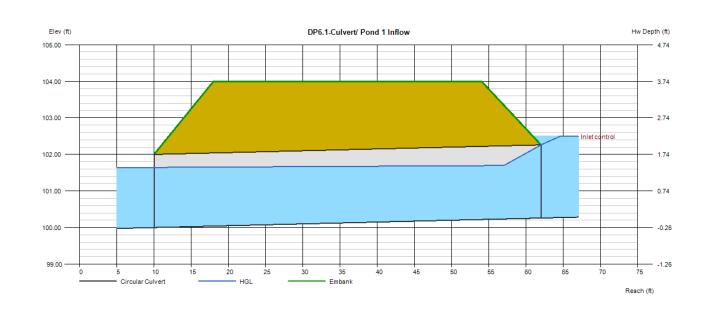
Invert Elev Dn (ft)	= 100.00	Calculations	
Pipe Length (ft)	= 52.00	Qmin (cfs)	= 16.00
Slope (%)	= 0.50	Qmax (cfs)	= 16.00
Invert Elev Up (ft)	= 100.26	Tailwater Elev (ft)	= Normal
Rise (in)	= 24.0		
Shape	= Circular	Highlighted	
Span (in)	= 24.0	Qtotal (cfs)	= 16.00
No. Barrels	= 1	Qpipe (cfs)	= 16.00
n-Value	= 0.013	Qovertop (cfs)	= 0.00
Culvert Type	= Circular Concrete	Veloc Dn (ft/s)	= 5.79
Culvert Entrance	<ul> <li>Groove end projecting (C)</li> </ul>	Veloc Up (ft/s)	= 6.60
Coeff. K,M,c,Y,k	= 0.0045, 2, 0.0317, 0.69, 0.2	HGL Dn (ft)	= 101.64
		HGL Up (ft)	= 101.70
Embankment		Hw Elev (ft)	= 102.49
Top Elevation (ft)	= 104.00	Hw/D (ft)	= 1.12
Top Width (ft)	= 36.00	Flow Regime	= Inlet Control

Top Width (ft) Crest Width (ft)

=	104.00
=	36.00
=	100 00

= 100.00

- - = Inlet Control

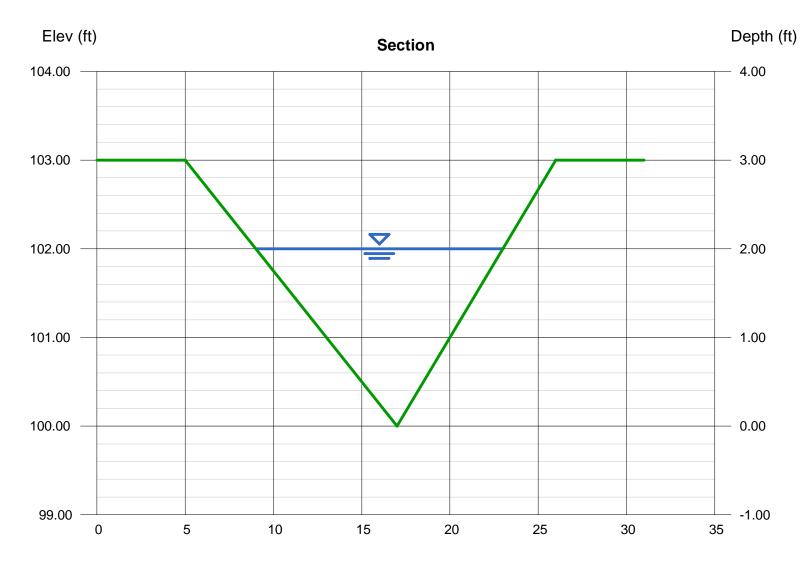


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### **DP7-Swale**

Triangular		Highlighted	
Side Slopes (z:1)	= 4.00, 3.00	Depth (ft)	= 2.00
Total Depth (ft)	= 3.00	Q (cfs)	= 70.00
		Area (sqft)	= 14.00
Invert Elev (ft)	= 100.00	Velocity (ft/s)	= 5.00
Slope (%)	= 1.10	Wetted Perim (ft)	= 14.57
N-Value	= 0.030	Crit Depth, Yc (ft)	= 1.91
		Top Width (ft)	= 14.00
Calculations		EGL (ft)	= 2.39
Compute by:	Known Q		
Known Q (cfs)	= 70.00		



Reach (ft)

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

#### **DP7-Pond 1 Inflow**

Invert Elev Dn (ft) Pipe Length (ft) Slope (%) Invert Elev Up (ft) Rise (in)	= 100.00 = 61.00 = 0.51 = 100.31 = 42.0	<b>Calculations</b> Qmin (cfs) Qmax (cfs) Tailwater Elev (ft)	= 70.00 = 70.00 = Normal
Shape	= Circular	Highlighted	
Span (in)	= 42.0	Qtotal (cfs)	= 70.00
No. Barrels	= 1	Qpipe (cfs)	= 70.00
n-Value	= 0.013	Qovertop (cfs)	= 0.00
Culvert Type	= Circular Concrete	Veloc Dn (ft/s)	= 8.48
Culvert Entrance	<ul> <li>Groove end projecting (C)</li> </ul>	Veloc Up (ft/s)	= 9.04
Coeff. K,M,c,Y,k	= 0.0045, 2, 0.0317, 0.69, 0.2	HGL Dn (ft)	= 102.80
		HGL Up (ft)	= 102.94
Embankment		Hw Elev (ft)	= 104.44

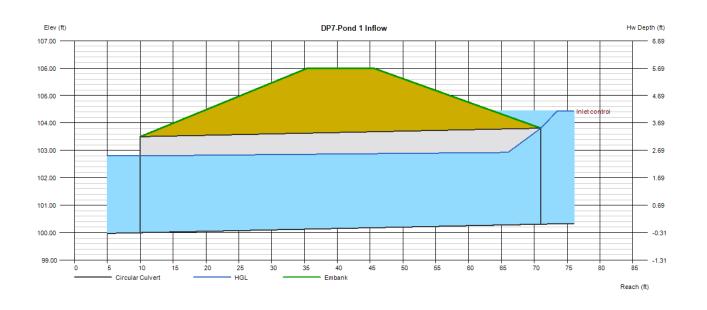
Top Elevation (ft) Top Width (ft) Crest Width (ft)

= 106.00= 10.00 = 100.00

Monday, Oct 21 2024

Qtotal (cts)	=	70.00
Qpipe (cfs)	=	70.00
Qovertop (cfs)	=	0.00
Veloc Dn (ft/s)	=	8.48
Veloc Up (ft/s)	=	9.04
HGL Dn (ft)	=	102.8
HGL Up (ft)	=	102.9
Hw Elev (ft)	=	104.4
Hw/D (ft)	=	1.18
Flow Regime	=	Inlet

= Inlet Control

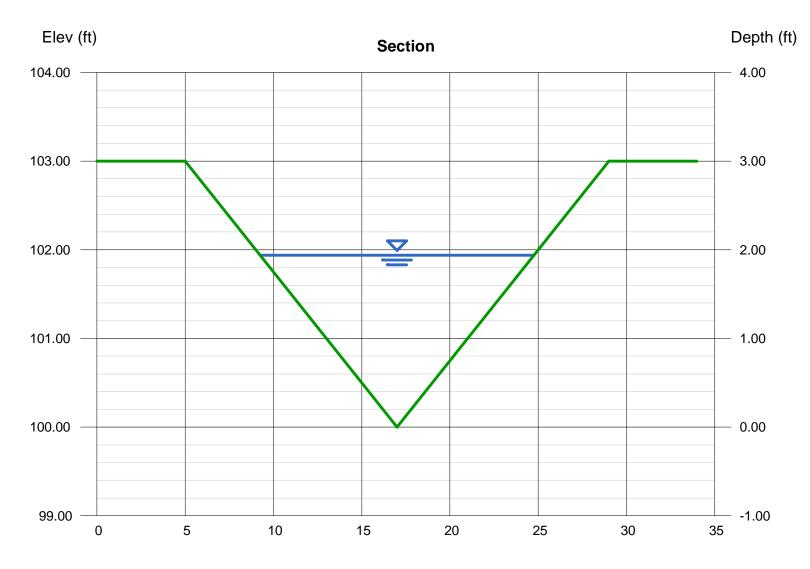


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### DP12.1-Swale

Triangular		Highlighted	
Side Slopes (z:1)	= 4.00, 4.00	Depth (ft)	= 1.94
Total Depth (ft)	= 3.00	Q (cfs)	= 75.00
		Area (sqft)	= 15.05
Invert Elev (ft)	= 100.00	Velocity (ft/s)	= 4.98
Slope (%)	= 1.10	Wetted Perim (ft)	= 16.00
N-Value	= 0.030	Crit Depth, Yc (ft)	= 1.86
		Top Width (ft)	= 15.52
Calculations		EGL (ft)	= 2.33
Compute by:	Known Q		
Known Q (cfs)	= 75.00		



Reach (ft)

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

### **DP12.1-Culvert**

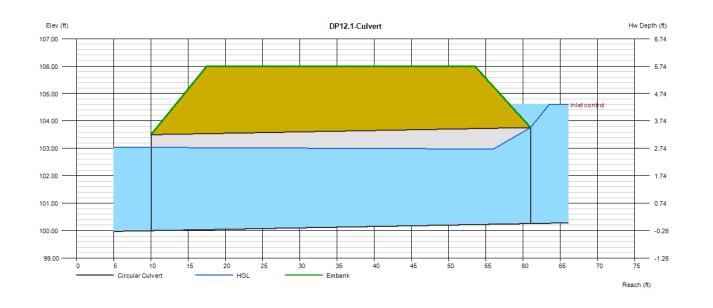
Invert Elev Dn (ft) Pipe Length (ft)	= 100.00 = 51.00	Calculations Qmin (cfs)	= 75.00
Slope (%)	= 0.51	Qmax (cfs)	= 75.00
Invert Elev Up (ft)	= 100.26	Tailwater Elev (ft)	= Normal
Rise (in)	= 42.0		
Shape	= Circular	Highlighted	
Span (in)	= 42.0	Qtotal (cfs)	= 75.00
No. Barrels	= 1	Qpipe (cfs)	= 75.00
n-Value	= 0.013	Qovertop (cfs)	= 0.00
Culvert Type	= Circular Concrete	Veloc Dn (ft/s)	= 8.46
Culvert Entrance	<ul> <li>Groove end projecting (C)</li> </ul>	Veloc Up (ft/s)	= 9.39
Coeff. K,M,c,Y,k	= 0.0045, 2, 0.0317, 0.69, 0.2	HGL Dn (ft)	= 103.03
		HGL Up (ft)	= 102.97
Embankment		Hw Elev (ft)	= 104 60

### Embankment

Top Elevation (ft) Top Width (ft) Crest Width (ft)

=	106.00
=	36.00
=	100.00

Inginginea		
Qtotal (cfs)	=	75.00
Qpipe (cfs)	=	75.00
Qovertop (cfs)	=	0.00
Veloc Dn (ft/s)	=	8.46
Veloc Up (ft/s)	=	9.39
HGL Dn (ft)	=	103.03
HGL Up (ft)	=	102.97
Hw Elev (ft)	=	104.60
Hw/D (ft)	=	1.24
Flow Regime	=	Inlet Control



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### DP12.1-Pond 2 Inflow

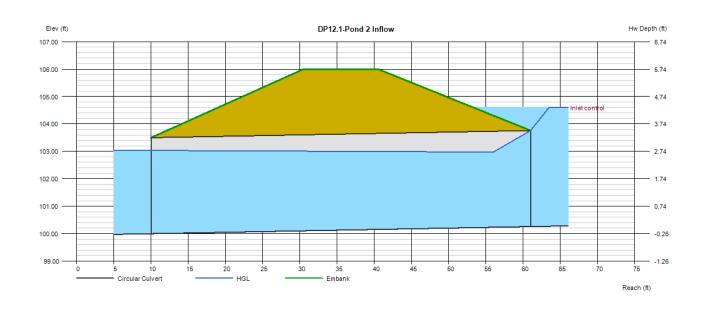
Invert Elev Dn (ft) Pipe Length (ft) Slope (%) Invert Elev Up (ft)	= 100.00 = 51.00 = 0.51 = 100.26	<b>Calculations</b> Qmin (cfs) Qmax (cfs) Tailwater Elev (ft)	= 75.00 = 75.00 = Normal
Rise (in)	= 42.0		
Shape	= Circular	Highlighted	
Span (in)	= 42.0	Qtotal (cfs)	= 75.00
No. Barrels	= 1	Qpipe (cfs)	= 75.00
n-Value	= 0.013	Qovertop (cfs)	= 0.00
Culvert Type	= Circular Concrete	Veloc Dn (ft/s)	= 8.46
Culvert Entrance	<ul> <li>Groove end projecting (C)</li> </ul>	Veloc Up (ft/s)	= 9.39
Coeff. K,M,c,Y,k	= 0.0045, 2, 0.0317, 0.69, 0.2	HGL Dn (ft)	= 103.03
		HGL Up (ft)	= 102.97
Embankment		Hw Elev (ft)	= 104.60

Top Elevation (ft) Top Width (ft) Crest Width (ft)

= 106.00 = 10.00 = 100.00

#### Monday, Oct 21 2024

Qtotal (cfs)	=	75.00
Qpipe (cfs)	=	75.00
Qovertop (cfs)	=	0.00
Veloc Dn (ft/s)	=	8.46
Veloc Up (ft/s)	=	9.39
HGL Dn (ft)	=	103.03
HGL Up (ft)	=	102.97
Hw Elev (ft)	=	104.60
Hw/D (ft)	=	1.24
Flow Regime	=	Inlet Control



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### **DP13-Culvert**

Invert Elev Dn (ft) Pipe Length (ft) Slope (%) Invert Elev Up (ft)	= 100.00 = 51.00 = 0.51 = 100.26	<b>Calculations</b> Qmin (cfs) Qmax (cfs) Tailwater Elev (ft)	=
Rise (in)	= 18.0		
Shape	= Circular	Highlighted	
Span (in)	= 18.0	Qtotal (cfs)	=
No. Barrels	= 1	Qpipe (cfs)	=
n-Value	= 0.013	Qovertop (cfs)	=
Culvert Type	= Circular Concrete	Veloc Dn (ft/s)	=
Culvert Entrance	<ul> <li>Groove end projecting (C)</li> </ul>	Veloc Up (ft/s)	=
Coeff. K,M,c,Y,k	= 0.0045, 2, 0.0317, 0.69, 0.2	HGL Dn (ft)	=
		HGL Up (ft)	=

#### Embankment

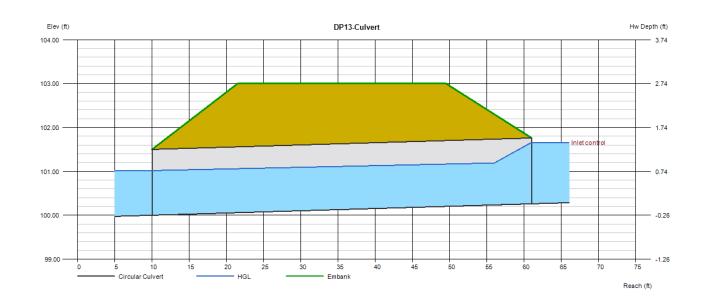
Top Elevation (ft) Top Width (ft) Crest Width (ft)

=	103.00
=	28.00
=	100.00

#### Calculations

Qmin (cfs)	= 6.00
Qmax (cfs)	= 6.00
Tailwater Elev (ft)	= Normal

2
5
ontrol



#### Tuesday, Aug 13 2024

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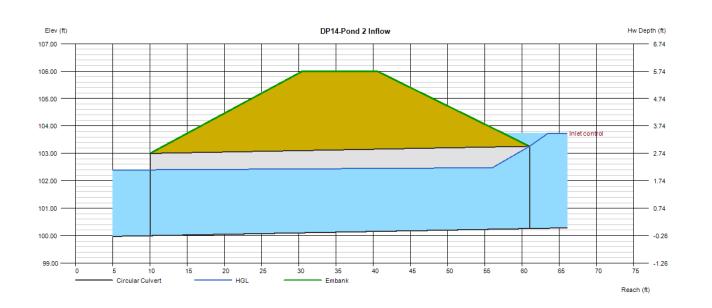
#### **DP14-Pond 2 Inflow**

Invert Elev Dn (ft) Pipe Length (ft) Slope (%) Invert Elev Up (ft) Rise (in)	= 100.00 = 51.00 = 0.51 = 100.26 = 36.0	<b>Calculations</b> Qmin (cfs) Qmax (cfs) Tailwater Elev (ft)	= 93.00 = 93.00 = Normal
Shape	= Circular	Highlighted	
Span (in)	= 36.0	Qtotal (cfs)	= 93.00
No. Barrels	= 2	Qpipe (cfs)	= 93.00
n-Value	= 0.013	Qovertop (cfs)	= 0.00
Culvert Type	= Circular Concrete	Veloc Dn (ft/s)	= 7.67
Culvert Entrance	= Groove end projecting (C)	Veloc Up (ft/s)	= 8.27
Coeff. K,M,c,Y,k	= 0.0045, 2, 0.0317, 0.69, 0.2	HGL Dn (ft)	= 102.40
		HGL Up (ft)	= 102.49
Embankment		Hw Elev (ft)	= 103.74

Top Elevation (ft) Top Width (ft) Crest Width (ft)

= 106.00 = 10.00 = 100.00

Qtotal (cfs)	= 93.00
Qpipe (cfs)	= 93.00
Qovertop (cfs)	= 0.00
Veloc Dn (ft/s)	= 7.67
Veloc Up (ft/s)	= 8.27
HGL Dn (ft)	= 102.40
HGL Up (ft)	= 102.49
Hw Elev (ft)	= 103.74
Hw/D (ft)	= 1.16
Flow Regime	= Inlet Control



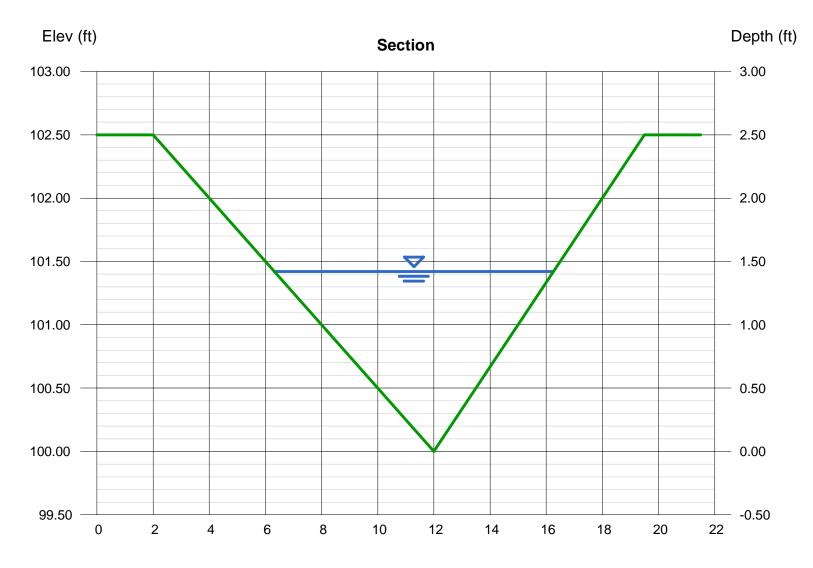
Monday, Oct 21 2024

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

### **DP16-Roadside Swale**

#### Triangular

Triangular		Highlighted	
Side Slopes (z:1)	= 4.00, 3.00	Depth (ft)	= 1.42
Total Depth (ft)	= 2.50	Q (cfs)	= 35.00
		Area (sqft)	= 7.06
Invert Elev (ft)	= 100.00	Velocity (ft/s)	= 4.96
Slope (%)	= 1.70	Wetted Perim (ft)	= 10.35
N-Value	= 0.030	Crit Depth, Yc (ft)	= 1.45
		Top Width (ft)	= 9.94
Calculations		EGL (ft)	= 1.80
Compute by:	Known Q		
Known Q (cfs)	= 35.00		
Compute by:			



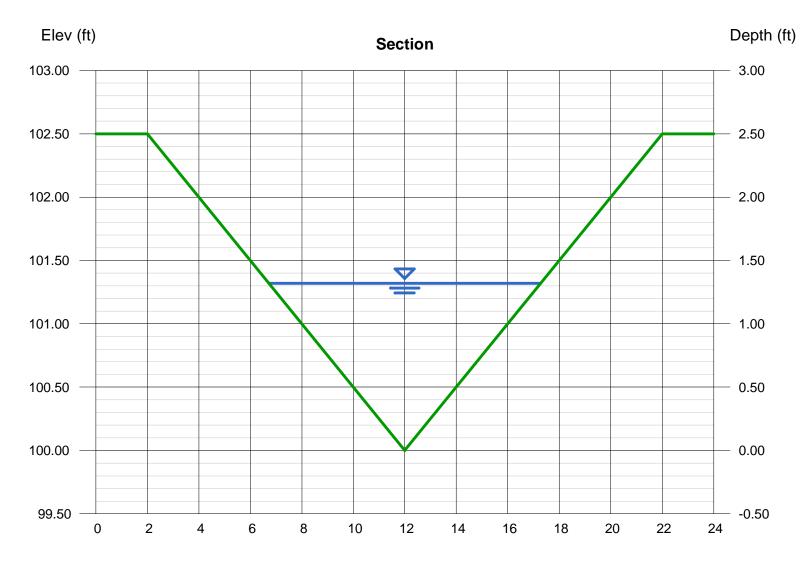
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### **DP16-Swale**

Triangular		Highlighted	
Side Slopes (z:1)	= 4.00, 4.00	Depth (ft)	= 1.32
Total Depth (ft)	= 2.50	Q (cfs)	= 35.00
		Area (sqft)	= 6.97
Invert Elev (ft)	= 100.00	Velocity (ft/s)	= 5.02
Slope (%)	= 1.90	Wetted Perim (ft)	= 10.88
N-Value	= 0.030	Crit Depth, Yc (ft)	= 1.37
		Top Width (ft)	= 10.56
Calculations		EGL (ft)	= 1.71
Compute by:	Known Q		
Known Q (cfs)	= 35.00		



Reach (ft)

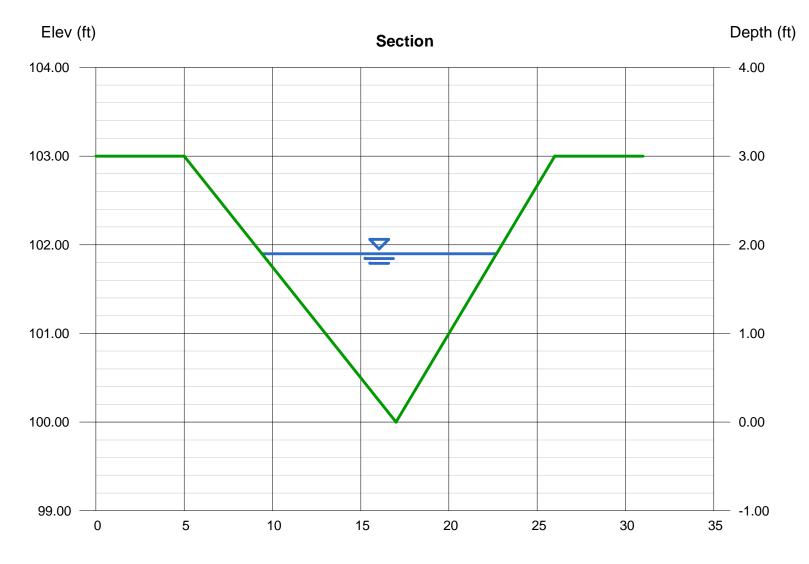
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### **DP17.1-Roadside Swale**

#### Triangular

Triangular		Highlighted	
Side Slopes (z:1)	= 4.00, 3.00	Depth (ft)	= 1.90
Total Depth (ft)	= 3.00	Q (cfs)	= 63.00
		Area (sqft)	= 12.63
Invert Elev (ft)	= 100.00	Velocity (ft/s)	= 4.99
Slope (%)	= 1.15	Wetted Perim (ft)	= 13.84
N-Value	= 0.030	Crit Depth, Yc (ft)	= 1.83
		Top Width (ft)	= 13.30
Calculations		EGL (ft)	= 2.29
Compute by:	Known Q		
Known Q (cfs)	= 63.00		



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### **DP17.1-Culvert**

Invert Elev Dn (ft)	= 100.00	Calculations	
Pipe Length (ft)	= 60.00	Qmin (cfs)	= 63.00
Slope (%)	= 0.50	Qmax (cfs)	= 63.00
Invert Elev Up (ft)	= 100.30	Tailwater Élev (ft)	= Norma
Rise (in)	= 42.0		
Shape	= Circular	Highlighted	
Span (in)	= 42.0	Qtotal (cfs)	= 63.00
No. Barrels	= 1	Qpipe (cfs)	= 63.00
n-Value	= 0.013	Qovertop (cfs)	= 0.00
Culvert Type	= Circular Concrete	Veloc Dn (ft/s)	= 8.34
Culvert Entrance	= Square edge w/headwall (C)	Veloc Up (ft/s)	= 8.59
Coeff. K,M,c,Y,k	= 0.0098, 2, 0.0398, 0.67, 0.5	HGL Dn (ft)	= 102.56
		HGL Up (ft)	= 102.79
Embankmont		Hw Elev (ft)	- 104 35

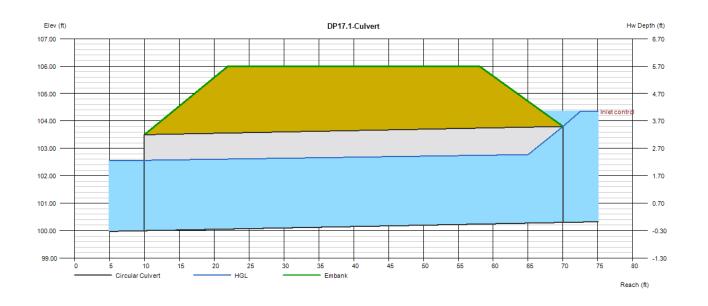
### Embankment

Top Elevation (ft) Top Width (ft) Crest Width (ft)

=	106.00
=	36.00
=	100.00

Qmin (cfs)	= 63.00
Qmax (cfs)	= 63.00
Tailwater Elev (ft)	= Normal

inginginoa		
Qtotal (cfs)	=	63.00
Qpipe (cfs)	=	63.00
Qovertop (cfs)	=	0.00
Veloc Dn (ft/s)	=	8.34
Veloc Up (ft/s)	=	8.59
HGL Dn (ft)	=	102.56
HGL Up (ft)	=	102.79
Hw Elev (ft)	=	104.35
Hw/D (ft)	=	1.16
Flow Regime	=	Inlet Control



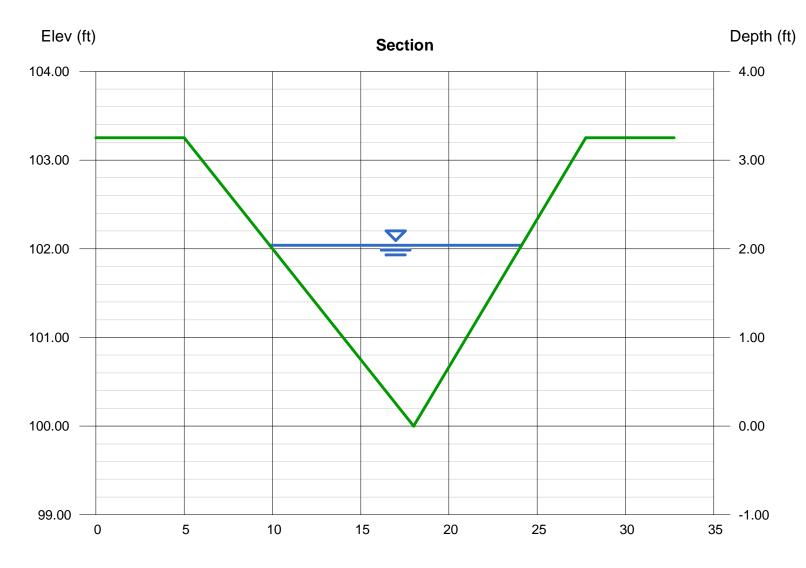
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### DP18.1-Roadside Swale

Triangular		Highlighted	
Side Slopes (z:1)	= 4.00, 3.00	Depth (ft)	= 2.04
Total Depth (ft)	= 3.25	Q (cfs)	= 72.00
		Area (sqft)	= 14.57
Invert Elev (ft)	= 100.00	Velocity (ft/s)	= 4.94
Slope (%)	= 1.05	Wetted Perim (ft)	= 14.86
N-Value	= 0.030	Crit Depth, Yc (ft)	= 1.93
		Top Width (ft)	= 14.28
Calculations		EGL (ft)	= 2.42
Compute by:	Known Q		
Known Q (cfs)	= 72.00		



Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

#### **DP18.1-Culvert**

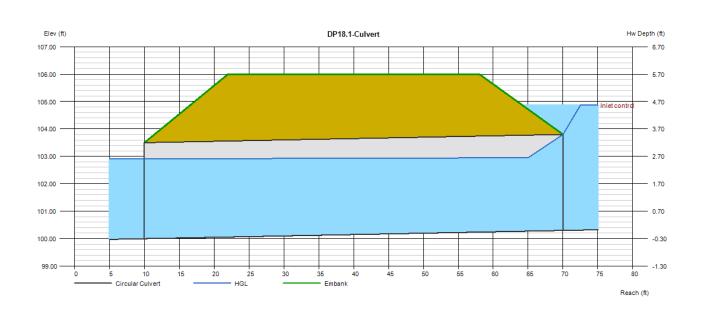
Invert Elev Dn (ft) Pipe Length (ft) Slope (%) Invert Elev Up (ft) Rise (in)	= 100.00 = 60.00 = 0.50 = 100.30 = 42.0	<b>Calculations</b> Qmin (cfs) Qmax (cfs) Tailwater Elev (ft)	= 72.00 = 72.00 = Normal
Shape	= Circular	Highlighted	
Span (in)	= 42.0	Qtotal (cfs)	= 72.00
No. Barrels	= 1	Qpipe (cfs)	= 72.00
n-Value	= 0.013	Qovertop (cfs)	= 0.00
Culvert Type	= Circular Concrete	Veloc Dn (ft/s)	= 8.42
Culvert Entrance	= Square edge w/headwall (C)	Veloc Up (ft/s)	= 9.19
Coeff. K,M,c,Y,k	= 0.0098, 2, 0.0398, 0.67, 0.5	HGL Dn (ft)	= 102.91
		HGL Up (ft)	= 102.96
Embankment		Hw Elev (ft)	= 104.87

### Embankment

Top Elevation (ft) Top Width (ft) Crest Width (ft)

=	106.00
=	36.00
=	100.00

Qovertop (cfs)	= 0.00
Veloc Dn (ft/s)	= 8.42
Veloc Up (ft/s)	= 9.19
HGL Dn (ft)	= 102.91
HGL Up (ft)	= 102.96
Hw Elev (ft)	= 104.87
Hw/D (ft)	= 1.30
Flow Regime	= Inlet Control



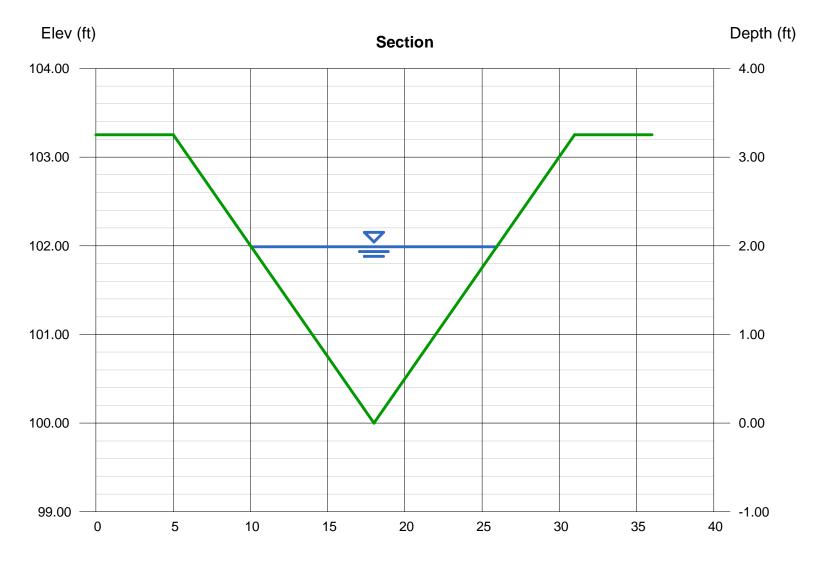
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### DP19.1-Swale

Triangular		Highlighted
Side Slopes (z:1)	= 4.00, 4.00	Depth (ft) $= 1.99$
Total Depth (ft)	= 3.25	Q(cfs) = 108.00
		Area (sqft) = 15.84
Invert Elev (ft)	= 100.00	Velocity (ft/s) = 6.82
Slope (%)	= 2.00	Wetted Perim (ft) $= 16.41$
N-Value	= 0.030	Crit Depth, Yc (ft) $= 2.15$
		Top Width (ft) $= 15.92$
Calculations		EGL (ft) = 2.71
Compute by:	Known Q	
Known Q (cfs)	= 108.00	
		Swale to be protected w/ soil
		riprap where above 5 ft/s



Reach (ft)

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

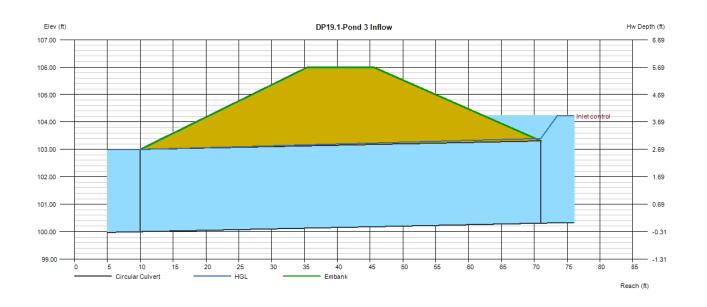
### **DP19.1-Pond 3 Inflow**

Invert Elev Dn (ft) Pipe Length (ft) Slope (%) Invert Elev Up (ft) Rise (in)	= 100.00 = 61.00 = 0.51 = 100.31 = 36.0	<b>Calculations</b> Qmin (cfs) Qmax (cfs) Tailwater Elev (ft)	= 108.00 = 108.00 = Normal
Shape	= Circular	Highlighted	
Span (in)	= 36.0	Qtotal (cfs)	= 108.00
No. Barrels	= 2	Qpipe (cfs)	= 108.00
n-Value	= 0.013	Qovertop (cfs)	= 0.00
Culvert Type	= Circular Concrete	Veloc Dn (ft/s)	= 7.64
Culvert Entrance	<ul> <li>Groove end projecting (C)</li> </ul>	Veloc Up (ft/s)	= 7.64
Coeff. K,M,c,Y,k	= 0.0045, 2, 0.0317, 0.69, 0.2	HGL Dn (ft)	= 103.00
		HGL Up (ft)	= 103.40
Embankment		Hw Elev (ft)	= 104.22

Top Elevation (ft) Top Width (ft) Crest Width (ft)

=	106.00
=	10.00
=	100.00

Qtotal (cfs)	=	108.00
Qpipe (cfs)	=	108.00
Qovertop (cfs)	=	0.00
Veloc Dn (ft/s)	=	7.64
Veloc Up (ft/s)	=	7.64
HGL Dn (ft)	=	103.00
HGL Up (ft)	=	103.40
Hw Elev (ft)	=	104.22
Hw/D (ft)	=	1.30
Flow Regime	=	Inlet Control



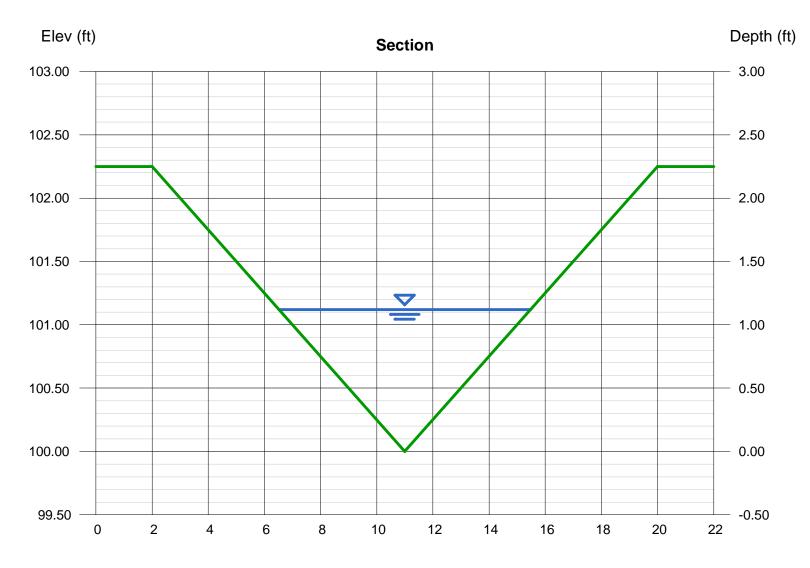
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### **DP20-Swale**

Triangular		Highlighted	
Side Slopes (z:1)	= 4.00, 4.00	Depth (ft)	= 1.12
Total Depth (ft)	= 2.25	Q (cfs)	= 23.00
		Area (sqft)	= 5.02
Invert Elev (ft)	= 100.00	Velocity (ft/s)	= 4.58
Slope (%)	= 2.00	Wetted Perim (ft)	= 9.24
N-Value	= 0.030	Crit Depth, Yc (ft)	= 1.16
		Top Width (ft)	= 8.96
Calculations		EGL (ft)	= 1.45
Compute by:	Known Q		
Known Q (cfs)	= 23.00		



## **Culvert Report**

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

### **DP20-Pond 3 Inflow**

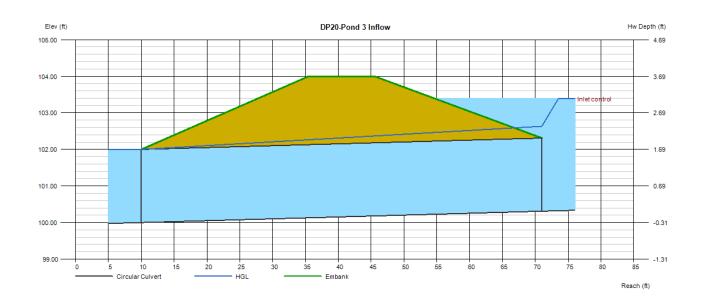
Invert Elev Dn (ft)	= 100.00	Calculations	
			~~~~
Pipe Length (ft)	= 61.00	Qmin (cfs)	= 23.00
Slope (%)	= 0.51	Qmax (cfs)	= 23.00
Invert Elev Up (ft)	= 100.31	Tailwater Elev (ft)	= Normal
Rise (in)	= 24.0		
Shape	= Circular	Highlighted	
Span (in)	= 24.0	Qtotal (cfs)	= 23.00
No. Barrels	= 1	Qpipe (cfs)	= 23.00
n-Value	= 0.013	Qovertop (cfs)	= 0.00
Culvert Type	= Circular Concrete	Veloc Dn (ft/s)	= 7.32
Culvert Entrance	<ul> <li>Groove end projecting (C)</li> </ul>	Veloc Up (ft/s)	= 7.32
Coeff. K,M,c,Y,k	= 0.0045, 2, 0.0317, 0.69, 0.2	HGL Dn (ft)	= 102.00
		HGL Up (ft)	= 102.63
Embankment		Hw Elev (ft)	= 103.38

Top Elevation (ft) Top Width (ft)

Crest Width (ft)

=	104.00
=	10.00
=	100.00

inginginea		
Qtotal (cfs)	=	23.00
Qpipe (cfs)	=	23.00
Qovertop (cfs)	=	0.00
Veloc Dn (ft/s)	=	7.32
Veloc Up (ft/s)	=	7.32
HGL Dn (ft)	=	102.00
HGL Up (ft)	=	102.63
Hw Elev (ft)	=	103.38
Hw/D (ft)	=	1.54
Flow Regime	=	Inlet Control



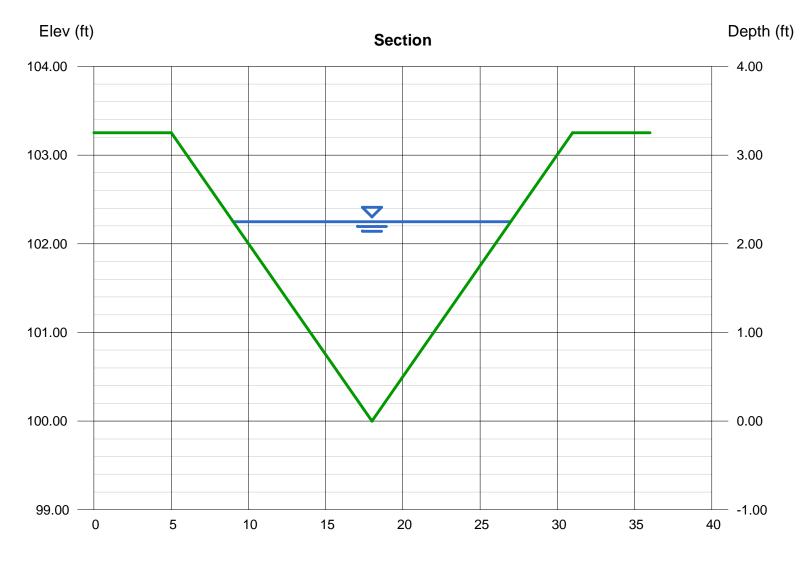
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Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

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## DP22.1-Swale

Triangular		Highlighted
Side Slopes (z:1)	= 4.00, 4.00	Depth (ft) $= 2.25$
Total Depth (ft)	= 3.25	Q(cfs) = 106.00
		Area (sqft) = 20.25
Invert Elev (ft)	= 100.00	Velocity (ft/s) = 5.23
Slope (%)	= 1.00	Wetted Perim (ft) = 18.55
N-Value	= 0.030	Crit Depth, Yc (ft) $= 2.13$
		Top Width (ft) $= 18.00$
Calculations		EGL (ft) $= 2.68$
Compute by:	Known Q	
Known Q (cfs)	= 106.00	
× ,		Swale to be protected w/ soil
		riprap where above 5 ft/s



## **Culvert Report**

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

### DP23.1-Culvert

Invert Elev Dn (ft)	= 100.00	Calculations	
Pipe Length (ft)	= 60.00	Qmin (cfs)	= 139.00
Slope (%)	= 0.50	Qmax (cfs)	= 139.00
Invert Elev Up (ft)	= 100.30	Tailwater Elev (ft)	= Norma
Rise (in)	= 36.0		
Shape	= Circular	Highlighted	
Span (in)	= 36.0	Qtotal (cfs)	= 139.00
No. Barrels	= 3	Qpipe (cfs)	= 139.00
n-Value	= 0.013	Qovertop (cfs)	= 0.00
Culvert Type	= Circular Concrete	Veloc Dn (ft/s)	= 7.60
Culvert Entrance	= Square edge w/headwall (C)	Veloc Up (ft/s)	= 8.28
Coeff. K,M,c,Y,k	= 0.0098, 2, 0.0398, 0.67, 0.5	HGL Dn (ft)	= 102.41
		HGL Up (ft)	= 102.52
			404.04

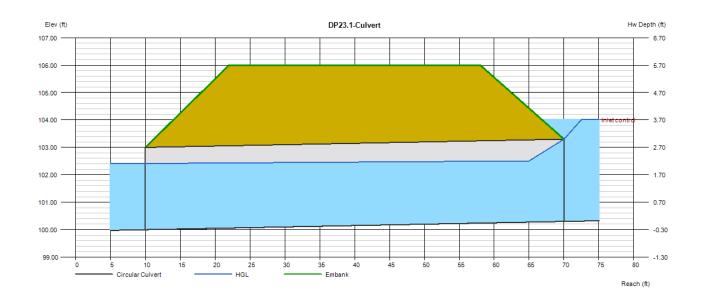
### Embankment

Top Elevation (ft) Top Width (ft) Crest Width (ft)

=	106.00
=	36.00
=	100.00

Qmin (cfs)	= 139.00
Qmax (cfs)	= 139.00
Tailwater Elev (ft)	= Normal

inginginea		
Qtotal (cfs)	=	139.00
Qpipe (cfs)	=	139.00
Qovertop (cfs)	=	0.00
Veloc Dn (ft/s)	=	7.60
Veloc Up (ft/s)	=	8.28
HGL Dn (ft)	=	102.41
HGL Up (ft)	=	102.52
Hw Elev (ft)	=	104.01
Hw/D (ft)	=	1.24
Flow Regime	=	Inlet Control



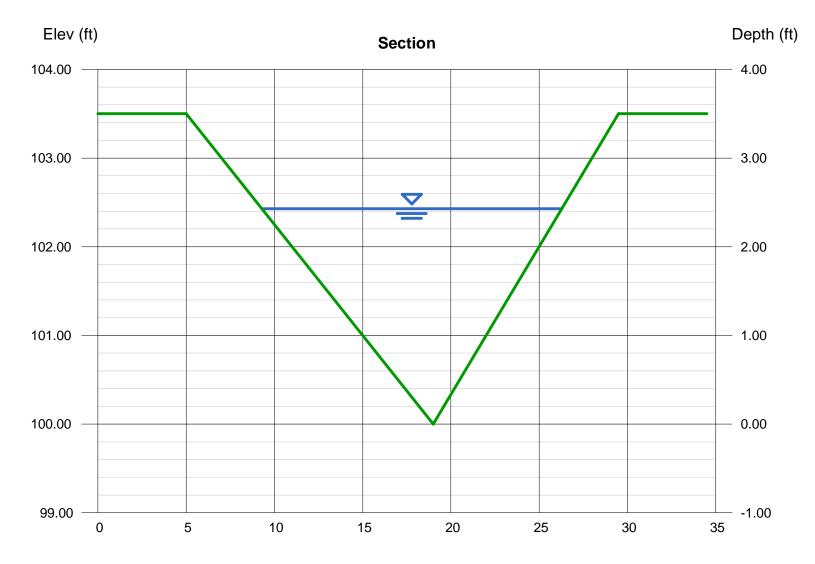
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## DP23.1-Roadside Swale

Triangular		Highlighted
Side Slopes (z:1)	= 4.00, 3.00	Depth (ft) $= 2.43$
Total Depth (ft)	= 3.50	Q(cfs) = 139.00
		Area (sqft) $= 20.67$
Invert Elev (ft)	= 100.00	Velocity (ft/s) = 6.73
Slope (%)	= 1.50	Wetted Perim (ft) $= 17.70$
N-Value	= 0.030	Crit Depth, Yc (ft) $= 2.51$
		Top Width (ft) $= 17.01$
Calculations		EGL (ft) $= 3.13$
Compute by:	Known Q	
Known Q (cfs)	= 139.00	
		Swale to be protected w/ soil
		riprap where above 5 ft/s

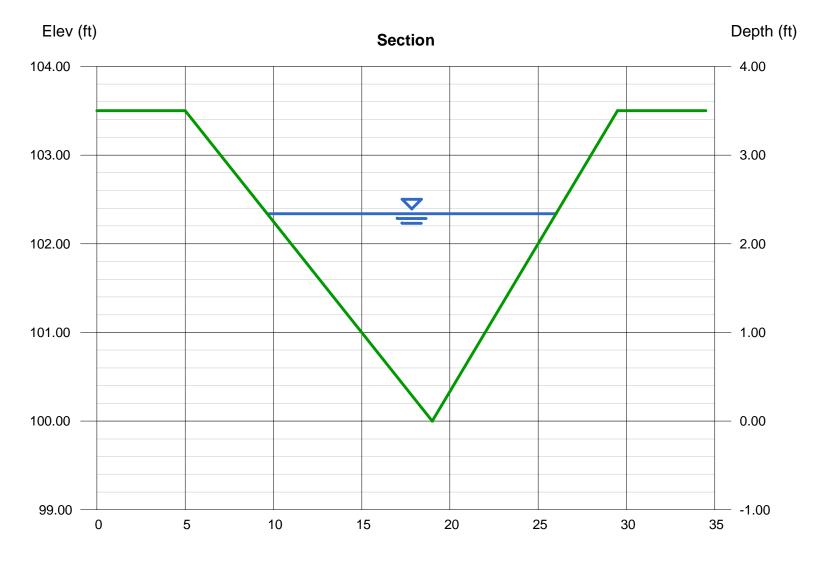


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## DP24.1-Roadside Swale

Triangular		Highlighted
Side Slopes (z:1)	= 4.00, 3.00	Depth (ft) $= 2.34$
Total Depth (ft)	= 3.50	Q(cfs) = 144.00
		Area (sqft) $= 19.16$
Invert Elev (ft)	= 100.00	Velocity (ft/s) = 7.51
Slope (%)	= 2.00	Wetted Perim (ft) $= 17.05$
N-Value	= 0.030	Crit Depth, Yc (ft) $= 2.54$
		Top Width (ft) $= 16.38$
Calculations		EGL (ft) $= 3.22$
Compute by:	Known Q	
Known Q (cfs)	= 144.00	
		Swale to be protected w/ soil
		riprap where above 5 ft/s

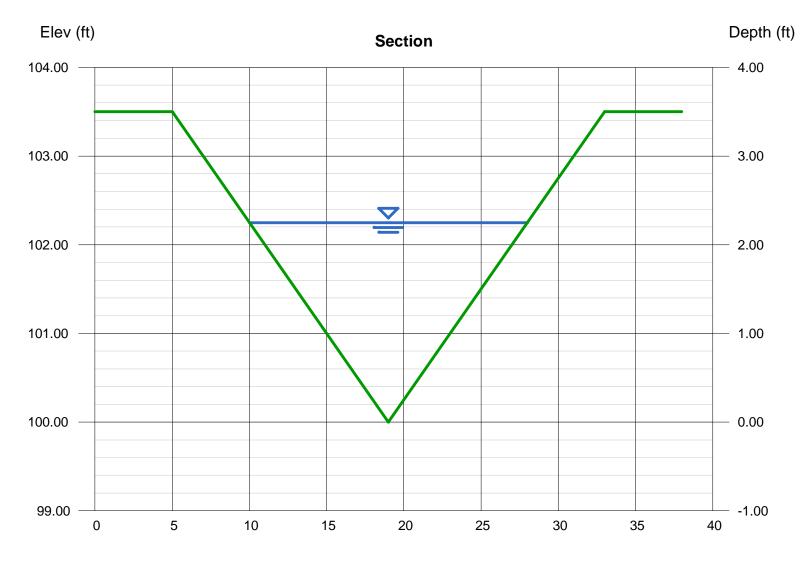


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## DP25.1-Swale

Triangular		Highlighted
Side Slopes (z:1)	= 4.00, 4.00	Depth (ft) $= 2.25$
Total Depth (ft)	= 3.50	Q(cfs) = 150.00
		Area (sqft) = 20.25
Invert Elev (ft)	= 100.00	Velocity (ft/s) = 7.41
Slope (%)	= 2.00	Wetted Perim (ft) /= 18.55
N-Value	= 0.030	Crit Depth, Yc (ft) $= 2.45$
		Top Width (ft) $= 18.00$
Calculations		EGL (ft) $= 3.10$
Compute by:	Known Q	
Known Q (cfs)	= 150.00	
		Swale to be protected w/ soil
		riprap where above 5 ft/s



## **Culvert Report**

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

### DP26.1-Pond 4 Inflow

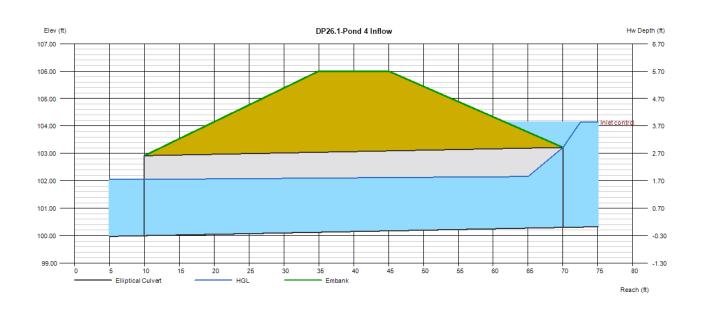
Invert Elev Dn (ft) Pipe Length (ft) Slope (%) Invert Elev Up (ft) Rise (in)	= 100.00 = 60.00 = 0.50 = 100.30 = 35.0	<b>Calculations</b> Qmin (cfs) Qmax (cfs) Tailwater Elev (ft)	= 202.00 = 202.00 = Normal
Shape	= Elliptical	Highlighted	
Span (in)	= 53.0	Qtotal (cfs)	= 202.00
No. Barrels	= 3	Qpipe (cfs)	= 202.00
n-Value	= 0.013	Qovertop (cfs)	= 0.00
Culvert Type	<ul> <li>Horizontal Ellipse Concrete</li> </ul>	Veloc Dn (ft/s)	= 8.37
Culvert Entrance	= Square edge w/headwall (H)	Veloc Up (ft/s)	= 9.51
Coeff. K,M,c,Y,k	= 0.01, 2, 0.0398, 0.67, 0.5	HGL Dn (ft)	= 102.05
		HGL Up (ft)	= 102.17
Embankment		Hw Elev (ft)	= 104.14

### Embankment

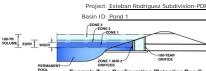
Top Elevation (ft) Top Width (ft) Crest Width (ft)

= 106.00= 10.00 = 100.00

Veloc Dn (ft/s)	= 8.37
Veloc Up (ft/s)	= 9.51
HGL Dn (ft)	= 102.05
HGL Up (ft)	= 102.17
Hw Elev (ft)	= 104.14
Hw/D (ft)	= 1.32
Flow Regime	= Inlet Control



Monday, Oct 21 2024



Example Zone Configuration (Retention Pond)

Depth Increment = 0.25

inches 1.50

1.19 inches

1.75 inches inches

2.00 inches 2.25 2.52 inches

#### Watershed Information

tersneu mitormation		
Selected BMP Type =	EDB	
Watershed Area =	78.00	acres
Watershed Length =	4,400	ft
Watershed Length to Centroid =	2,200	ft
Watershed Slope =	0.035	ft/ft
Watershed Imperviousness =	34.50%	percent
Percentage Hydrologic Soil Group A =	100.0%	percent
Percentage Hydrologic Soil Group B =	0.0%	percent
Percentage Hydrologic Soil Groups C/D =	0.0%	percent
Target WQCV Drain Time =	40.0	hours
Location for 1 br Painfall Donths -	Liser Innut	

## After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

the embedded Colorado orban Hydro	igraph Procedu	ie.
Water Quality Capture Volume (WQCV) =	1.071	acre-feet
Excess Urban Runoff Volume (EURV) =	2.797	acre-feet
2-yr Runoff Volume (P1 = 1.19 in.) =	2.042	acre-feet
5-yr Runoff Volume (P1 = 1.5 in.) =	2.779	acre-feet
10-yr Runoff Volume (P1 = 1.75 in.) =	3.377	acre-feet
25-yr Runoff Volume (P1 = 2 in.) =	4.712	acre-feet
50-yr Runoff Volume (P1 = 2.25 in.) =	5.971	acre-feet
100-yr Runoff Volume (P1 = 2.52 in.) =	7.646	acre-feet
500-yr Runoff Volume (P1 = 3.14 in.) =	11.235	acre-feet
Approximate 2-yr Detention Volume =	1.769	acre-feet
Approximate 5-yr Detention Volume =	2.352	acre-feet
Approximate 10-yr Detention Volume =	2.920	acre-feet
Approximate 25-yr Detention Volume =	3.657	acre-feet
Approximate 50-yr Detention Volume =	4.180	acre-feet
Approximate 100-yr Detention Volume =	4.968	acre-feet

#### Define Zones and Basin Geometry Zone 1 Volume (WQCV) Zone 2 Volume (EURV - Zone 1) = Zone 3 Volume (100-year - Zones 1 & 2) = Total Initial Initia

Total Available Depth Slope

ne 3 Volume (100-year - Zones 1 & 2) =	2.172	acre-feet
Total Detention Basin Volume =	4.968	acre-feet
Initial Surcharge Volume (ISV) =	140	ft <sup>3</sup>
Initial Surcharge Depth (ISD) =	0.33	ft
tal Available Detention Depth (H <sub>total</sub> ) =	6.00	ft
Depth of Trickle Channel $(H_{TC}) =$	0.50	ft
Slope of Trickle Channel ( $S_{TC}$ ) =	0.007	ft/ft
Slopes of Main Basin Sides (Smain) =	4	H:V
Basin Length-to-Width Ratio ( $R_{L/W}$ ) =	2	

1.071 acre-feet

acre-feet

1.725

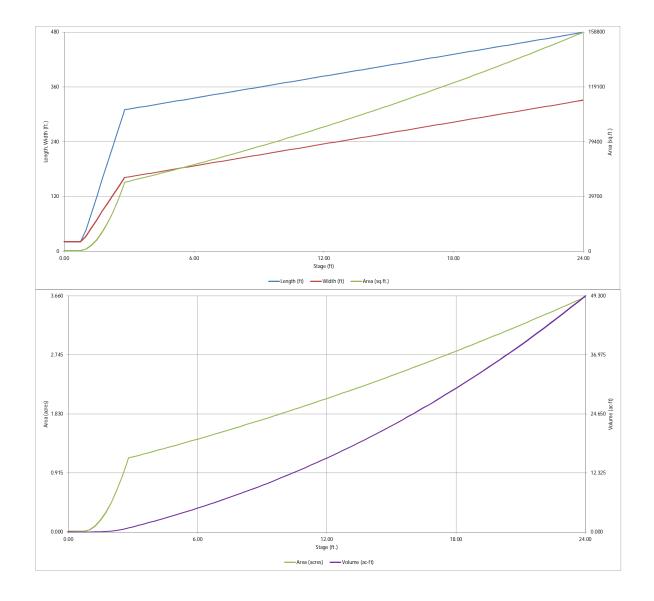
#### Initial Surcharge Area (A<sub>ISV</sub>) = 424 Surcharge Volume Length (LISV) = 20.6 Surcharge Volume Width (WISV) = 20.6 Depth of Basin Floor (H<sub>FLOOR</sub>) = 1.97 Length of Basin Floor (L<sub>FLOOR</sub>) 309.9 Width of Basin Floor ( $W_{FLOOR}$ ) = 161.3 Area of Basin Floor (A<sub>FLOOR</sub>) = 49,992 Volume of Basin Floor (V<sub>FLOOR</sub>) 36,131 Depth of Main Basin (H<sub>MAIN</sub>) = 3.20 Length of Main Basin (LMAIN) 335.5 Width of Main Basin (W<sub>MAIN</sub>) = 186.9 62,710

Area of Main Basin  $(A_{MAIN}) =$ Volume of Main Basin  $(V_{MAIN}) =$ 179,939 Calculated Total Basin Volume (Vtotal) = 4.968

Note: all pond calcs will be more thoroughly reviewed with the Final Plat (SF) submittal once pond CDs have been provided.

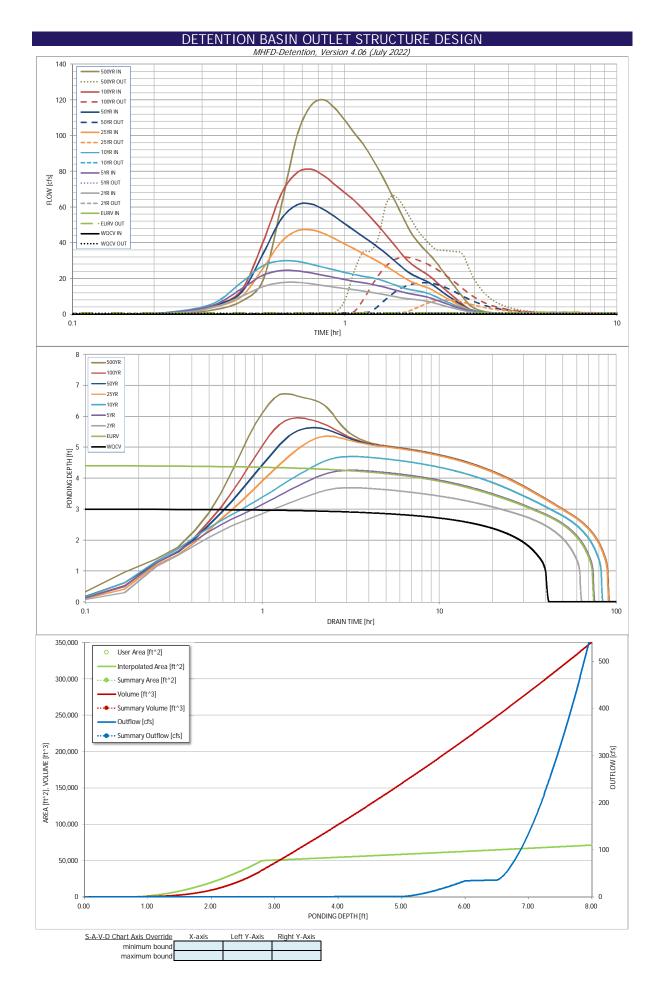
Stage         Stage Description (h)         Stage (h)         Optimal Stage (h)         Under (h)         Width (h)         Area (h)         Volume (acc)           1SV         0.33         20.6         20.6         424         0.010         140           1SV         0.33         20.6         20.6         424         0.010         318           0.75         20.6         20.6         424         0.010         318           1.00         45.6         32.7         1.422         0.034         566           1.15         22.3         50.6         4.163         0.064         58.8           1.150         119.0         68.5         8.146         0.107         2.67           2.00         12.2         2.90.0         0.642         15.49           2.20         2.25         22.91         31.88         0.854         23.61           2.20         2.25         2.27.1         1.90.0         6.422         15.49           2.20         2.25         2.29.1         12.21         7.90.0         6.422         15.49           2.20         2.26         12.91         11.80         4.633         11.48         3.64.233           2.20	With (ft)         Area (ft)         Cverride (acre)         Volume (acre)         Volume (acre)           20.6         424         0.010         140         0.033           20.6         424         0.010         140         0.033           20.6         424         0.010         140         0.033           20.6         424         0.010         110         0.033           20.6         424         0.010         318         0.007           32.7         1.422         0.034         506         0.012           50.6         4.163         0.096         1.168         0.027           65.5         8.146         0.187         2.697         0.062           86.3         13.49         0.309         5.368         0.123           104.2         20.044         0.400         9.56         0.219           105.2         20.760         0.462         15.49         0.356           139.9         37.188         0.844         1.65         0.411           162.9         50.748         1.165         40.719         103           164.9         51.601         1.231         85.857         1.367           174.9 </th
Description         (ff)         Stage (f)         (f)         (f)         (ff)	(ft)         (ft)         Area (ft)         (acre)         (ft)         (acre)           20.6         424         0.010         140         0.003           20.6         424         0.010         140         0.003           20.6         424         0.010         318         0.007           20.6         424         0.010         318         0.007           20.6         424         0.010         318         0.007           32.7         1.492         0.034         506         0.012           26.6         414         0.187         2.697         0.062           86.3         1.143         0.096         1.186         0.021           68.5         8.146         0.187         2.697         0.062           86.3         1.349         0.309         5.368         0.121           102.0         27.960         0.642         15.499         0.356           139.9         37.188         0.854         23.616         0.542           161.3         49.992         1.148         36.455         0.841           162.9         50.748         1.129         72.570         1.666           164.9
Top of Micropool         0.00         20.6         20.6         424         0.010         140           1SV         0.33         20.6         20.6         424         0.010         140           0.50         20.6         20.6         424         0.010         212           0.50         20.6         20.6         424         0.010         318           0.57         20.6         20.6         424         0.010         318           1.00         45.6         32.7         1.492         0.034         506           1.150         1190         68.5         8.16         0.172         2.697           1.75         155.7         8.3         13.439         0.309         5.88           1.250         2261         122.0         27960         0.642         15.499           1.175         302.6         157.7         47.727         1.096         34.203           Floor         2.80         300.9         161.3         49.92         1.148         36.454           Core 1(WOCV)         3.00         311.5         164.9         51.61         1.297         25.748           Floor         2.80         301.95         170.9<	20.6 $424$ $0.010$ $140$ $0.003$ $20.6$ $424$ $0.010$ $140$ $0.003$ $20.6$ $424$ $0.010$ $140$ $0.003$ $20.6$ $424$ $0.010$ $318$ $0.007$ $32.7$ $1.492$ $0.034$ $506$ $0.012$ $50.6$ $4.163$ $0.096$ $1.186$ $0.027$ $50.6$ $4.163$ $0.096$ $1.186$ $0.027$ $68.5$ $8.146$ $0.187$ $2.697$ $0.062$ $83.3$ $13.439$ $0.399$ $5.368$ $0.123$ $104.2$ $2.0044$ $0.460$ $9.526$ $0.219$ $122.0$ $2.960$ $0.642$ $15.499$ $0.561$ $157.7$ $47.727$ $1.096$ $34.203$ $0.785$ $157.7$ $47.727$ $1.096$ $34.203$ $0.785$ $157.7$ $47.727$ $1.966$ $34.271$ $1.771$ $1.76$ $5.750$
ISV         0.33         20.6         20.6         424         0.010         140           0.50         20.6         20.6         424         0.010         212           0.75         20.6         20.6         424         0.010         212           1.00         45.6         32.7         1.492         0.034         556           1.25         82.3         50.6         4.163         0.096         1.186           1.50         1190         68.5         8.146         0.187         2.697           2.00         192.4         104.2         20.044         0.460         9.526           2.25         2.291         122.0         27.960         0.642         15.491           2.50         265.8         139.9         3.188         0.854         23.616           2.75         302.6         157.7         47.727         1.096         34.203           Floor         2.80         300.9         161.3         49.992         1.148         36.455           Cone 1 (WOCV)         3.00         311.5         164.9         51.701         1.187         59.525           Cone 1 (WOCV)         3.00         313.5         164.9	20.6         424         0.010         140         0.003           20.6         424         0.010         212         0.005           20.6         424         0.010         318         0.007           20.6         424         0.010         318         0.007           20.6         424         0.010         318         0.007           32.7         1.42         0.034         506         0.012           50.6         4.163         0.096         1.186         0.027           68.5         8.146         0.187         2.697         0.062           104.2         20.044         0.460         9.526         0.219           122.0         27.960         0.642         15.49         0.352           157.7         47.727         1.096         34.203         0.785           161.3         49.992         1.148         36.45         0.841           162.9         50.748         1.165         46.719         1.073           164.9         51.701         1.187         59.525         1.367           164.9         53.631         1.231         85.57         1.971           172.9         55.592
erids         0.50         20.6         20.6         424         0.010         212           0.75         20.6         20.6         424         0.010         318           1.00         45.6         32.7         1.492         0.034         506           1.125         82.3         50.6         4.163         0.096         1.186           1.50         119.0         68.5         8.146         0.187         2.697           1.75         155.7         86.3         13.439         0.309         5.366           2.200         122.4         104.2         2.044         0.420         9.526           2.25         2.291         122.0         27.960         0.642         15.499           2.50         2.668.8         139.9         37.188         0.854         23.616           2.75         302.6         157.7         47.727         1.966         34.203           Floor         2.80         309.9         161.3         49.992         1.148         36.455           Zone 1 (WCV)         3.00         311.5         164.9         51.701         1.187         59.525           Cone 2 (EURV)         4.41         322.8         174.	20.6 $424$ $0.010$ $212$ $0.005$ $20.6$ $424$ $0.010$ $318$ $0.007$ $32.7$ $1.492$ $0.034$ $506$ $0.012$ $32.7$ $1.492$ $0.034$ $506$ $0.012$ $32.7$ $1.492$ $0.034$ $506$ $0.012$ $26.6$ $1.163$ $0.096$ $1.186$ $0.027$ $86.3$ $13.439$ $0.309$ $5.368$ $0.123$ $104.2$ $20.044$ $0.460$ $9.526$ $0.219$ $104.2$ $20.044$ $0.464$ $15.499$ $0.366$ $139.9$ $37.188$ $0.854$ $23.616$ $0.542$ $157.7$ $47.772$ $1.966$ $34.03$ $0.785$ $151.3$ $49.992$ $1.148$ $36.455$ $0.841$ $164.9$ $57.01$ $1.166$ $67.19$ $1.367$ $170.9$ $55.692$ $1.264$ $97.2570$ $1.666$ $174.2$
0.75         20.6         20.6         424         0.010         318           1.00         45.6         32.7         1.492         0.034         506           1.25         82.3         50.6         4.16.3         0.096         1.186           1.50         119.0         68.5         8.146         0.187         2.697           1.75         155.7         86.3         13.439         0.309         5.368           2.00         192.4         104.2         2.044         0.640         9.526           2.25         229.1         122.0         27,660         0.642         15,499           2.50         2.66.8         139.9         37,188         0.884         23,61           2.75         302.6         15.7         47,727         10.966         34,203           Floor         2.80         309.9         161.3         49.992         1.148         36,645           2.01<(WCV)	$\begin{array}{c c c c c c c c c c c c c c c c c c c $
0.75         20.6         20.6         424         0.010         318           1.00         45.6         32.7         1.492         0.034         506           1.25         82.3         50.6         4.163         0.096         1.186           1.50         119.0         68.5         8.146         0.187         2.697           1.75         155.7         86.3         13.439         0.309         5.38           2.00         192.4         104.2         2.044         0.640         9.526           2.25         2.29.1         122.0         27,960         0.642         15,499           2.75         302.6         15.7         47,727         1096         34,203           Floor         2.80         309.9         161.3         49.992         1.148         36.645           Zone1 (WOCV)         3.00         311.5         164.9         57.01         1187         59.52           4.00         315.5         164.9         52.662         12.09         72.570           Creet         3.75         317.5         168.9         53.631         1.231         89.585           es         4.00         322.5         321.5	$\begin{array}{c c c c c c c c c c c c c c c c c c c $
Incol         45.6         32.7         1.492         0.034         506           1.25         82.3         50.6         4.163         0.096         1,186           1.50         119.0         68.5         8.146         0.187         2.697           1.75         155.7         86.3         13.439         0.309         5.368           2.00         192.4         104.2         20.044         0.660         9.526           2.25         2.291         122.0         2.7960         0.642         15.499           2.250         2.265         139.9         3.7188         0.864         3.261           Floor         2.80         309.9         161.3         49.992         1148         36.451           Zone 1 (WOCV)         3.00         311.5         162.9         50.748         1.165         46.719           Floor         2.80         309.9         161.3         49.992         1148         36.455           Greft         3.50         315.5         166.9         52.662         1.209         72.570           Fet         3.50         317.5         172.9         55.692         1.274         93.366           ses         4.	$\begin{array}{c c c c c c c c c c c c c c c c c c c $
International         Internaternat         International         Internat	$\begin{array}{c c c c c c c c c c c c c c c c c c c $
1.50         119.0         66.5         8.16         0.187         2.697           1.75         155.7         86.3         13.439         0.300         5.38           2.00         192.4         104.2         20.044         0.460         9.526           2.25         2.291         122.0         27,960         0.642         15,499           2.50         2.66.8         139.9         37,188         0.884         23,616           2.75         302.6         157.7         47,727         1096         34,203           Floor         2.80         209.9         161.3         49,992         1.148         36,645           2.01 (WOCV)         3.00         311.5         164.9         57,71         1.187         59,555           feet         3.50         315.5         164.9         52,662         1.209         72,570           refet         3.50         315.5         164.9         53,631         1.231         85,857           s         4.00         319.5         170.9         54,607         1.244         93,86           s         4.05         323.5         174.9         55,592         1.276         113,161           z	68.5         8,146         0.187         2,677         0.062 $86.3$ 13,439         0.309         5,368         0.123 $104.2$ 20,044         0.400         9,526         0.219 $1122$ 27,960         0.642         15,499         0.356 $139.9$ 37,188         0.854         23,616         0.542 $157.7$ 47,727         1.066         34,203         0.785 $161.3$ 49,992         1.148         36,645         0.841 $164.9$ 50,748         1.165         46,179         1.073 $166.9$ 52,662         1.209         72,570         1.666 $168.9$ 53,631         1.231         85,857         1.971 $170.9$ 54,607         1.254         9,9386         2.282 $172.9$ 55,592         1.276         113,161         2.598 $174.2$ 56,585         1.322         141,454         3.247 $178.9$ 55,595         1.345         155,773         3.581 $180.9$ 66,637         1.322         141,454         <
1.50         119.0         66.5         8.166         0.187         2.697           1.75         155.7         86.3         13.439         0.300         5.38           2.00         192.4         104.2         20.044         0.460         9.526           2.25         2.261         122.0         27,960         0.642         15,499           2.50         2.65.8         139.9         37,188         0.884         23,616           2.75         302.6         157.7         47,727         1096         34,203           Floor         2.80         209.9         161.3         49,992         1.148         36,645           Zone 1 (WOCV)         3.00         311.5         162.9         50,748         1.165         46,71           Stat         4.00         319.5         164.9         52,662         12.09         72,570           Greet         3.50         315.5         166.9         52,662         12.99         93,86           Stat         4.00         319.5         172.9         55,592         12.76         113,161           Zone 2 (EURV)         4.41         322.8         174.2         56,555         1.299         12.718	68.5         8,146         0.187         2,677         0.062 $86.3$ 13,439         0.309         5,368         0.123 $104.2$ 20,044         0.400         9,526         0.219 $1122$ 27,960         0.642         15,499         0.356 $139.9$ 37,188         0.854         23,616         0.542 $157.7$ 47,727         1.066         34,203         0.785 $161.3$ 49,992         1.148         36,645         0.841 $164.9$ 50,748         1.165         46,179         1.073 $166.9$ 52,662         1.209         72,570         1.666 $168.9$ 53,631         1.231         85,857         1.971 $170.9$ 54,607         1.254         9,9386         2.282 $172.9$ 55,592         1.276         113,161         2.598 $174.2$ 56,585         1.322         141,454         3.247 $178.9$ 55,595         1.345         155,773         3.581 $180.9$ 66,637         1.322         141,454         <
1.75         155.7         86.3         13,439         0.309         5,388           2.00         192.4         104.2         200.44         0.460         9,52           2.25         2291         122.0         27,940         0.642         15,499           2.50         265.8         139.9         37,188         0.854         23,616           2.75         302.6         157.7         47,727         1.096         34,203           Floor         2.80         209.9         161.3         49,992         1.148         36,645           Zone 1 (WOCV)         3.00         311.5         164.9         51,701         1.187         59,525           Get         3.75         317.5         166.9         52,662         1.209         72,570           fet         3.75         317.5         166.9         52,662         1.209         72,570           fst         4.00         319.5         170.9         54,607         1254         93,366           st         4.00         319.5         170.9         55,692         1.201         122,107           st         5.00         327.5         176.9         55,582         1.221         121,1183	$\begin{array}{c c c c c c c c c c c c c c c c c c c $
Image: second	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
Image: state	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\begin{array}{c c c c c c c c c c c c c c c c c c c $
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	139.9         37.188         0.854         23.616         0.542           157.7         47,727         1.0%         34,203         0.785           161.3         49.992         1.148         36.645         0.841           162.9         50,748         1.165         46,719         1.073           164.9         51,701         1.187         59,525         1.367           164.9         53,631         1.231         85,857         1.971           170.9         54,607         1.254         99,386         2.282           172.9         55,592         1.276         113,161         2.598           174.9         56,585         1.229         122,107         2.803           174.9         56,595         1.322         141,454         3.247           178.9         59,595         1.345         155,977         3.920           182.9         60,637         1.392         185,873         3.920           182.9         60,637         1.392         185,873         3.265           184.9         61,669         1.416         201,071         4.616           184.9         63,759         1.464         232,427         5.33
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
Floor         2.80         309.9         161.3         49.992         1.148         36.645           Zone 1 (WOCV)         3.00         311.5         162.9         50.748         1.165         46,719           feet         3.50         313.5         164.9         51,701         11817         59,525           feet         3.50         315.5         166.9         52,662         1.209         72,570           feet         3.75         317.5         166.9         53,631         1.234         99,386           feet         3.75         321.5         170.9         54,607         1.254         99,386           feet         4.25         321.5         172.9         55,592         1.276         113,161           Zone 2 (EURV)         4.41         322.8         174.2         56,565         1.294         19,386           fs         4.75         325.5         176.9         57,566         1.322         141,454           fs         5.50         331.5         182.9         60,637         1.392         185,783           fs         5.50         331.5         184.9         61,669         1.416         201,071           con 3 (100-yean)	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
Zone 1 (WOCV)         3.00         311.5         162.9         50.748         1.165         46.719           rides         3.25         313.5         164.9         51.701         1.187         59.525           feet         3.50         315.5         166.9         52.642         1209         72.570           feet         3.75         317.5         166.9         53.631         1231         85.857           s         4.00         319.5         170.9         54.607         1.254         93.86           S         4.25         321.5         172.9         55.592         1.271         131.61           S         4.50         323.5         174.2         56.527         1.291         122.107           S         4.50         323.5         174.9         56.585         1.299         127.183           S         4.75         325.5         178.9         58.595         1.345         155.977           S         5.26         329.5         180.9         59.612         1.368         170.753           S         5.50         331.5         182.9         60.637         1.392         185.983           S         5.75         333.5	$\begin{array}{c c c c c c c c c c c c c c c c c c c $
rides         3.25         313.5         164.9         51.701         1.187         59.525           feet         3.50         315.5         166.9         52.662         1.209         72.570           feet         3.75         317.5         166.9         52.662         1.209         72.570           feet         3.75         317.5         166.9         52.642         1.211         85.857           s         4.00         319.5         170.9         54.607         1.254         99.386           Zone 2 (EURV)         4.41         322.8         174.2         55.592         1.274         13.161           s         5.00         323.5         174.9         56.585         1.291         122.107           s         5.00         323.5         174.9         56.585         1.292         127.183           s         5.00         327.5         178.9         57.586         1.322         141.454           s         5.00         331.5         182.9         60.637         1.392         185.878           s         5.00         331.5         182.9         60.637         1.392         185.878           con 3 (100-year) 6.00         335.5 </td <td>164.9         51,701         1.187         59,525         1.367           166.9         52,662         1.209         72,570         1.666           168.9         53,631         1.231         85,857         1.971           170.9         54,607         1.254         99,386         2.282           172.9         55,592         1.276         113,161         2.598           174.9         56,585         1.299         122,107         2.803           174.9         56,585         1.299         122,107         2.803           174.9         56,585         1.299         127,183         2.920           176.9         57,586         1.322         141,454         3.247           178.9         58,595         1.345         155,977         3.881           180.9         59,612         1.368         170,753         3.920           182.9         60,637         1.392         185,783         4.265           184.9         61,669         1.416         201,071         4.616           184.9         63,759         1.464         232,427         5.336           190.9         64,816         1.488         248,499         5.705</td>	164.9         51,701         1.187         59,525         1.367           166.9         52,662         1.209         72,570         1.666           168.9         53,631         1.231         85,857         1.971           170.9         54,607         1.254         99,386         2.282           172.9         55,592         1.276         113,161         2.598           174.9         56,585         1.299         122,107         2.803           174.9         56,585         1.299         122,107         2.803           174.9         56,585         1.299         127,183         2.920           176.9         57,586         1.322         141,454         3.247           178.9         58,595         1.345         155,977         3.881           180.9         59,612         1.368         170,753         3.920           182.9         60,637         1.392         185,783         4.265           184.9         61,669         1.416         201,071         4.616           184.9         63,759         1.464         232,427         5.336           190.9         64,816         1.488         248,499         5.705
rides         3.25         313.5         164.9         51.701         1.187         59.525           feet         3.50         315.5         166.9         52.662         1.209         72.570           feet         3.75         317.5         166.9         52.662         1.209         72.570           feet         3.75         317.5         166.9         52.642         1.211         85.857           s         4.00         319.5         170.9         54.607         1.254         99.386           Zone 2 (EURV)         4.41         322.8         174.2         55.592         1.274         13.161           s         5.00         323.5         174.9         56.585         1.291         122.107           s         5.00         323.5         174.9         56.585         1.292         127.183           s         5.00         327.5         178.9         57.586         1.322         141.454           s         5.00         331.5         182.9         60.637         1.392         185.878           s         5.00         331.5         182.9         60.637         1.392         185.878           con 3 (100-year) 6.00         335.5 </td <td>164.9         51,701         1.187         59,525         1.367           166.9         52,662         1.209         72,570         1.666           168.9         53,631         1.231         85,857         1.971           170.9         54,607         1.254         99,386         2.282           172.9         55,592         1.276         113,161         2.598           174.9         56,585         1.299         122,107         2.803           174.9         56,585         1.299         122,107         2.803           174.9         56,585         1.299         127,183         2.920           176.9         57,586         1.322         141,454         3.247           178.9         58,595         1.345         155,977         3.881           180.9         59,612         1.368         170,753         3.920           182.9         60,637         1.392         185,783         4.265           184.9         61,669         1.416         201,071         4.616           184.9         63,759         1.464         232,427         5.336           190.9         64,816         1.488         248,499         5.705</td>	164.9         51,701         1.187         59,525         1.367           166.9         52,662         1.209         72,570         1.666           168.9         53,631         1.231         85,857         1.971           170.9         54,607         1.254         99,386         2.282           172.9         55,592         1.276         113,161         2.598           174.9         56,585         1.299         122,107         2.803           174.9         56,585         1.299         122,107         2.803           174.9         56,585         1.299         127,183         2.920           176.9         57,586         1.322         141,454         3.247           178.9         58,595         1.345         155,977         3.881           180.9         59,612         1.368         170,753         3.920           182.9         60,637         1.392         185,783         4.265           184.9         61,669         1.416         201,071         4.616           184.9         63,759         1.464         232,427         5.336           190.9         64,816         1.488         248,499         5.705
feet         3.50         315.5         166.9         52.662         1.209         72.570           feet         3.75         317.5         166.9         53.631         1.231         85.85           4.00         319.5         170.9         54.607         1.254         99.386           s         4.00         319.5         170.9         55.692         1.276         113.161           Zon 2 (EURV)         4.41         322.8         174.2         56.592         1.276         113.161           Zon 2 (EURV)         4.41         322.8         174.2         56.565         1.299         122.107           s         4.75         323.5         174.9         55.6565         1.299         122.107           s         5.00         327.5         178.9         58.505         1.342         141.454           5.50         331.5         180.9         59.612         1.368         170.753           5.50         331.5         180.9         59.612         1.368         170.753           5.50         331.5         184.9         61.669         1.464         201.071           con 3 (100-year)         6.00         335.5         188.9         63.759	166.9         52.662         1.209         72.570         1.666           168.9         53.631         1.231         85.857         1.971           170.9         54.607         1.254         99.386         2.282           172.9         55.592         1.276         113.161         2.588           174.9         56.585         1.291         122.107         2.033           174.9         56.585         1.322         141.454         3.247           178.9         55.592         1.345         155.977         3.581           180.9         59.612         1.345         155.977         3.581           184.9         61.669         1.416         201.071         4.616           184.9         61.669         1.416         201.071         4.616           196.9         63.759         1.464         232.427         5.336           190.9         64.816         1.488         248.499         5.705           192.9         65.881         1.512         264.836         6.080           194.9         66.954         1.537         281.440         6.461           196.9         66.034         1.562         298.313         6.848
feet         3.75         317.5         168.9         53.631         1.231         85.857           4.00         319.5         170.9         54.607         1.254         99.386           4.25         321.5         172.9         55.592         1.276         113.161           Zone 2 (EURV)         4.41         322.8         174.2         56.227         1.294         122.107           5         4.50         323.5         174.9         56.585         1.299         127.183           5         4.50         323.5         174.9         56.585         1.294         122.107           5         5.00         327.5         178.9         58.595         1.345         155.977           5         5.00         327.5         178.9         58.595         1.345         155.977           5.55         329.5         180.9         59.612         1.368         170.753           5.50         331.5         182.9         60.637         1.392         195.783           5.75         333.5         184.9         61.699         1.444         232.427           6.60         339.5         190.9         64.816         1.448         248.499	168.9         53,631         1.231         85,857         1.971           170.9         54,607         1.254         99,386         2.282           172.9         55,592         1.276         113,161         2.582           174.2         56,227         1.291         122,107         2.803           174.9         55,585         1.299         122,107         2.803           174.9         56,585         1.299         127,183         2.920           176.9         57,586         1.322         141,454         3.247           178.9         58,595         1.345         155,977         3.581           180.9         59,612         1.368         170,753         3.920           184.9         61,669         1.416         201,071         4.616           186.9         62,710         1.440         216,619         4.973           188.9         63,759         1.464         232,427         5.33           190.9         64,816         1.488         248,499         5.705           192.9         65,681         1.512         246,436         6.080           194.9         66,954         1.537         281,440         6.461
4.00         319.5         170.9         54,607         1.254         99,386           4.25         321.5         172.9         55,592         1.276         113,161           Zone 2 (EURV)         4.41         322.8         174.2         55,592         1.274         113,161           5         4.50         323.5         174.9         56,585         1.299         122,107           5         4.50         323.5         174.9         56,585         1.299         127,183           5         4.75         325.5         176.9         57,586         1.322         141,454           5         5.00         327.5         178.9         58,595         1.345         155,977           5.52         329.5         180.9         59,612         1.382         140,758           5.50         331.5         182.9         60,637         1.392         185,783           5.75         333.5         184.9         61,669         1.416         201,071           2one 3 (100-year)         6.00         335.5         188.9         62,710         1.444         232,427           6.50         339.5         190.9         64,816         1.488         248,479     <	170.9         54,607         1.254         99,386         2.282           172.9         55,592         1.276         113,161         2.598           174.2         55,592         1.276         113,161         2.598           174.9         56,585         1.299         122,107         2.803           174.9         56,585         1.299         127,183         2.920           176.9         57,586         1.322         141,454         3.247           178.9         58,595         1.345         155,977         3.920           180.9         59,612         1.368         170,753         3.920           182.9         60,637         1.392         185,783         4.265           184.9         61,669         1.416         201,014         4.913           186.9         62,710         1.440         216,619         4.973           192.9         65,881         1.482         248,499         5.705           192.9         65,881         1.512         204,836         6.080           194.9         66,954         1.537         281,440         6.461           198.9         63,376         1.542         208,336         6.462
4         4         321.5         172.9         55.592         1.276         113.161           20ne 2 (EURV)         4.41         322.8         174.2         56.227         1.291         122.107           4.50         323.5         174.9         56.585         1.276         113.161           5         4.75         323.5         174.9         56.585         1.299         127.183           4.75         325.5         176.9         57.586         1.322         141.454           5         5.00         327.5         178.9         58.595         1.345         155.977           5.50         331.5         180.9         59.412         1.368         170.753           5.50         331.5         184.9         61.669         1.416         201.071           Zone 3 (100-year)         6.00         335.5         184.9         61.669         1.416         201.071           Zone 3 (100-year)         6.00         335.5         184.9         61.669         1.444         232.427           6.50         339.5         190.9         64.816         1.484         248.499           6.75         341.5         192.9         65.811         1.512         2264	$\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$
s         4.25         321.5         172.9         55.592         1.276         113.161           2one 2 (EURV)         4.41         322.8         174.2         56.227         1.291         122.101           4.50         323.5         174.9         56.585         1.299         127.183           4.75         323.5         174.9         56.585         1.322         141.454           5.0         327.5         176.9         57.586         1.322         141.454           5.0         327.5         176.9         57.586         1.322         141.454           5.50         323.5         180.9         59.412         1.368         170.753           5.50         331.5         182.9         60.637         1.392         185.783           5.75         333.5         184.9         61.669         1.416         201.071           7.00         335.5         188.9         63.759         1.464         232.427           6.50         339.5         190.9         64.816         1.488         248.499           6.75         341.5         192.9         65.811         1512         2264.383           7.00         343.5         194.9 <td< td=""><td><math display="block">\begin{array}{c ccccccccccccccccccccccccccccccccccc</math></td></td<>	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
Zone 2 (EURV)         4.41         322.8         174.2         56,227         1.291         122,107           s         4.50         323.5         174.9         56,585         1.299         127,183           4.75         325.5         176.9         57,586         1.322         141,454           s         5.00         327.5         178.9         58,595         1.345         155,977           5.50         331.5         180.9         59,612         1.348         170,753           5.50         331.5         184.9         61,669         1.414         216,619           5.75         333.5         184.9         61,669         1.440         216,619           6.50         337.5         188.9         63,759         1.444         232,427           6.50         337.5         189.9         63,759         1.444         224,429           6.75         341.5         192.9         65,811         1.512         264,436           7.00         343.5         194.9         66,954         1.557         284,430           7.25         345.5         196.9         60,31         1.552         284,430           7.50         347.5         19	174.2         56,227         1.291         122,107         2.803           174.4         56,585         1.299         127,183         2.920           176.9         57,586         1.322         141,454         3.447           178.9         58,595         1.345         155,977         3.581           180.9         59,612         1.368         170,753         3.920           182.9         60,637         1.392         185,783         4.265           184.9         61,669         1.416         201,071         4.616           186.9         62,710         1.4440         216,619         4.973           188.9         63,759         1.464         232,427         5.336           190.9         64,816         1.488         248,99         5.705           192.9         65,881         1.512         264,836         6.080           194.9         66,954         1.537         281,440         6.461           196.9         68,034         1.562         298,313         6.84           198.9         61,13         1587         315,458         7.242           200.9         70,220         1.612         332,876         7.642
4.50         323.5         174.9         56.585         1.299         127,183           4.75         325.5         176.9         57.586         1.325         141,64           5.00         327.5         176.9         57.586         1.325         155.97           5.02         327.5         180.9         59,612         1.368         170,753           5.50         331.5         182.9         60,637         1.392         185,783           5.50         331.5         182.9         60,637         1.392         180,701           2one 3 (100-year)         6.00         335.5         186.9         62,710         1.444         232,427           6.50         339.5         190.9         64,816         1.482         246,499           6.75         341.5         192.9         65,881         1.512         2264,836           7.00         343.5         194.9         66,954         1.537         281,440           7.25         345.5         196.9         60,834         1.552         206,313           7.50         347.5         196.9         60,91.23         1.587         315,458           7.75         349.5         200.9         70,202	174.9         56,585         1.2.99         127,183         2.920           176.9         57,586         1.3.22         141,454         3.247           178.9         55,595         1.3.22         141,454         3.247           178.9         55,695         1.3.45         155,977         3.581           180.9         59,612         1.366         170,753         3.920           182.9         60,637         1.392         185,783         4.265           184.9         61,669         1.416         201,071         4.616           186.9         62,710         1.444         223,427         5.336           190.9         64,816         1.488         248,499         5.705           192.9         66,881         1.512         264,836         6.080           194.9         66,954         1.537         281,440         6.461           194.9         66,954         1.537         281,440         6.461           194.9         66,954         1.552         208,313         6.84           194.9         66,9123         1.587         315,458         7.242           200.9         70,220         1.612         332,876         7.642<
s         4.75         325.5         176.9         57.586         1.322         141,454           5.00         327.5         178.9         58.595         1.345         155.97           5.25         329.5         180.9         59.412         1.348         170.753           5.50         331.5         182.9         60.637         1.392         185.783           5.75         333.5         184.9         61.669         1.416         201.071           Zone 3 (100-year)         6.00         335.5         188.9         62.710         1.464         232.427           6.50         339.5         190.9         54.816         1.482         248.499           6.75         341.5         192.9         65.811         1512         2264.386           7.00         343.5         194.9         66.954         1.537         281,440           7.25         345.5         196.9         60.334         1.552         298.313           7.50         347.5         196.9         60.713         1.582         298.313           7.75         349.5         200.9         70.220         1.612         32.876	176.9         57.586         1.322         141,454         3.247           178.9         58.595         1.345         155.977         3.581           180.9         59.612         1.368         170.753         3.92           182.9         60.637         1.392         185.783         4.265           184.9         61.669         1.416         201.071         4.616           186.9         62.710         1.440         221.619         4.973           188.9         63.759         1.464         222.427         5.336           190.9         64.816         1.488         248.499         5.705           192.9         65.881         1.512         204.836         6.060           194.9         66.954         1.537         281.440         6.461           196.9         68.034         1.562         298.313         6.848           198.9         61.12         1.587         315.458         7.242           200.9         70.220         1.612         332.876         7.642
S         5.00         327.5         178.9         58.595         1.345         155,977           5.52         329.5         180.9         59,612         1.348         170,753           5.50         331.5         182.9         60,637         1.392         185,783           5.75         333.5         184.9         61,669         1.416         201,071           Zone 3 (100-year)         6.00         335.5         186.9         62,710         1.444         222,427           6.50         339.5         190.9         64,816         1.488         248,499           6.75         343.5         192.9         65,881         1.512         224,438           7.00         343.5         194.9         66,954         1.537         281,400           7.25         345.5         196.9         69,123         1.562         290,313           7.75         349.5         200.9         70,220         1.612         332,876	178.9         58.595         1.345         155.977         3.581           180.0         59.612         1.368         170.753         3.920           182.9         60.637         1.392         185.783         4.265           184.9         61.669         1.416         201.071         4.616           186.9         62.710         1.440         216.619         4.973           188.9         63.759         1.464         232.427         5.336           190.9         64.816         1.482         248.499         5.705           192.9         65.881         1.512         264.836         6.080           194.9         66.954         1.537         281.440         6.461           196.9         68.034         1.562         298.313         6.848           198.9         60.712         1.587         315.458         7.242           200.9         70.220         1.612         332.876         7.642
S         5.00         327.5         178.9         58.595         1.345         155,977           5.52         329.5         180.9         59,612         1.348         170,753           5.50         331.5         182.9         60,637         1.392         185,783           5.75         333.5         184.9         61,669         1.416         201,071           Zone 3 (100-year)         6.00         335.5         186.9         62,710         1.444         222,427           6.50         339.5         190.9         64,816         1.488         248,499           6.75         343.5         192.9         65,881         1.512         224,438           7.00         343.5         194.9         66,954         1.537         281,400           7.25         345.5         196.9         68,034         1.562         298,313           7.50         347.5         198.9         69,123         1.517         231,548           7.75         349.5         200.9         70,220         1.612         332,876	178.9         58.595         1.345         155,977         3.581           180.9         59,612         1.368         170,753         3.920           182.9         60,637         1.392         185,783         4.265           184.9         61,669         1.416         201,071         4.616           186.9         62,710         1.440         216,619         4.973           188.9         63,759         1.464         232,427         5.36           190.9         64.816         1.482         248,499         5.705           192.9         65.881         1.512         264,836         6.080           194.9         66,954         1.537         281,440         6.461           196.9         68,034         1.562         298,313         6.848           198.9         60,712         1.587         315,458         7.242           200.9         70,220         1.612         332,876         7.642
5.25         329.5         180.9         59,612         1.368         170,753           5.50         331.5         182.9         60,637         1.392         185,783           5.75         333.5         184.9         61,669         1.416         201,071           Zone 3 (100-year)         6.00         335.5         184.9         61,669         1.446         232,427           6.50         337.5         188.9         63,759         1.464         232,427           6.50         339.5         190.9         64,816         1.488         248,499           6.75         341.5         192.9         65,881         1.512         264,836           7.00         343.5         194.9         66,954         1.537         281,440           7.25         345.5         196.9         60,314         1.552         296,313           7.50         347.5         196.9         60,9123         1.552         296,313           7.75         349.5         200.9         70,202         1.612         332,876	180.9         59,612         1.368         170,753         3.920           182.9         60,637         1.392         185,783         4.265           184.9         61,669         1.416         201,071         4.616           186.9         62,710         1.440         216,619         4.973           188.9         63,759         1.464         222,427         5.336           190.9         64,816         1.488         248,499         5.705           192.9         65,881         1.512         264,836         6.080           194.9         66,954         1.537         281,440         6.461           196.9         60,912         1.562         298,313         6.848           198.9         61,712         135,488         7.642           200.9         70,220         1.612         332,876         7.642
5.50         331.5         182.9         60,637         1.392         185,783           5.75         333.5         184.9         61,669         1.416         201,071           2one 3 (100-year)         6.00         335.5         188.9         62,710         1.440         216,619           6.25         337.5         188.9         63,759         1.464         232,427           6.50         339.5         190.9         64,816         1.482         248,499           6.75         341.5         192.9         65,881         1512         2264,836           7.00         343.5         194.9         66,954         1.537         281,440           7.25         345.5         196.9         60,213         1.562         208,313           7.50         347.5         196.9         60,123         1.562         209,313           7.75         349.5         200.9         70,220         1.612         32,876	182.9         60.637         1.392         185,783         4.265           184.9         61.669         1.416         201,071         4.616           186.9         62,710         1.440         221,619         4.973           188.9         63,759         1.464         232,427         5.336           190.9         64,816         1.488         248,499         5.705           192.9         65,881         1.512         204,836         6.080           194.9         66,954         1.537         281,440         6.461           196.9         68,034         1.562         298,313         6.848           198.9         61,123         1.587         315,458         7.242           200.9         70,220         1.612         332,876         7.642
5.75         333.5         184.9         61.669         1.416         201.071           Zone 3 (100-year)         6.00         335.5         188.9         62.710         1.440         216.619           6.25         337.5         188.9         63.759         1.464         232.427           6.50         339.5         190.9         64.816         1.488         248.499           6.75         341.5         192.9         65.881         1.512         264.836           7.00         343.5         194.9         66.954         1.537         281.440           7.25         345.5         196.9         68.034         1.562         298.313           7.50         347.5         198.9         69.733         1.587         315.458           7.75         349.5         200.9         70.20         1.612         332.876	184.9         61,669         1.416         201,071         4.616           186.9         62,710         1.440         216,619         4.973           188.9         63,759         1.464         232,427         5.336           190.9         64,816         1.488         248,499         5.705           192.9         65,881         1.512         264,836         6.080           194.9         66,954         1.537         281,440         6.461           196.9         68,034         1.562         298,313         6.848           198.9         69,123         1.587         315,458         7.242           200.9         70,220         1.612         332,876         7.642
5.75         333.5         184.9         61.669         1.416         201,071           Zone 3 (100-year)         6.00         335.5         186.9         62,710         1.440         216,619           6.25         337.5         188.9         63,759         1.446         232,427           6.50         339.5         190.9         64,816         1.488         248,499           6.75         341.5         192.9         65,881         1.512         264,836           7.00         343.5         194.9         66,954         1.537         281,440           7.25         345.5         196.9         68,034         1.562         298,313           7.50         347.5         198.9         69,723         1.587         315,458           7.75         349.5         200.9         70,20         1.612         332,876	184.9         61,669         1.416         201,071         4.616           186.9         62,710         1.440         216,619         4.973           188.9         63,759         1.464         232,427         5.336           190.9         64,816         1.488         248,499         5.705           192.9         65,881         1.512         264,836         6.080           194.9         66,954         1.537         281,440         6.461           196.9         68,034         1.562         298,313         6.848           198.9         69,123         1.587         315,458         7.242           200.9         70,220         1.612         332,876         7.642
Zone 3 (100-year)         6.00         335.5         186.9         62.710         1.440         216,619           6.25         337.5         188.9         63.759         1.464         232,427           6.50         339.5         190.9         64.816         1.488         248,499           6.75         341.5         192.9         65.881         1.512         264,386           7.00         343.5         194.9         66,954         1.537         281,400           7.25         345.5         196.9         60.304         1.562         298,313           7.50         347.5         198.9         90,73         158.78         315,458           7.75         349.5         200.9         70,220         1.612         332,876	186.9         62,710         1.440         216,619         4.973           188.9         63,759         1.464         223,427         5.36           190.9         64,816         1.488         248,499         5.705           192.9         65,881         1.512         264,836         6.080           194.9         66,954         1.537         281,440         6.461           196,9         69,034         1.562         298,313         6.848           198,9         69,123         1.587         315,458         7.242           200.9         70,220         1.612         332,876         7.642
6.25         337.5         188.9         63.759         1.464         232,427           6.50         339.5         190.9         64.816         1.488         248,499           6.75         341.5         192.9         65.881         1.512         2264,836           7.00         343.5         194.9         66,954         1.537         281,440           7.25         345.5         196.9         68.034         1.562         208,313           7.50         347.5         196.9         69,123         1.587         315,458           7.75         349.5         200.9         70,220         1.612         332,876	188.9         63,759         1.464         232,427         5.336           190.9         64,816         1.488         248,499         5.705           192.9         65,881         1.512         224,826         6.080           194.9         66,954         1.537         281,440         6.461           196.9         68,034         1.552         298,313         6.848           198.9         61,23         1.587         315,458         7.242           200.9         70,220         1.612         332,876         7.642
6.50         339.5         190.9         64,816         1.488         248,499           6.75         341.5         192.9         65,881         1.512         264,836           7.00         343.5         194.9         66,954         1.537         281,440           7.25         345.5         196.9         68,034         1.562         298,313           7.50         347.5         198.9         69,123         1.587         315,458           7.75         349.5         200.9         70,220         1.612         332,876	190.9         64,816         1.488         248,499         5.705           192.9         65,881         1.512         264,836         0.609           194.9         66,954         1.537         281,440         6.461           196.9         68,034         1.562         298,313         6.848           198.9         69,123         1.587         315,458         7.242           200.9         70,220         1.612         332,876         7.642
6.75         341.5         192.9         65.881         1.512         264.836           7.00         343.5         194.9         66.954         1.537         281.440           7.25         345.5         196.9         68.034         1.562         298.313           7.50         347.5         198.9         69.123         1.587         315.458           7.75         349.5         200.9         70.202         1.612         332.876	192.9         65.881         1.512         264.836         6.080           194.9         66.954         1.537         281.440         6.461           196.9         68.034         1.562         298.313         6.848           198.9         69.123         1.562         315.458         7.242           200.9         70.220         1.612         332.876         7.642
6.75         341.5         192.9         65.881         1.512         264.836           7.00         343.5         194.9         66.954         1.537         281.440           7.25         345.5         196.9         68.034         1.562         298.313           7.50         347.5         198.9         69.123         1.587         315.458           7.75         349.5         200.9         70.202         1.612         332.876	192.9         65.881         1.512         264.836         6.080           194.9         66.954         1.537         281.440         6.461           196.9         68.034         1.562         298.313         6.848           198.9         69.123         1.562         315.458         7.242           200.9         70.220         1.612         332.876         7.642
7.00         343.5         194.9         66.954         1.537         281,440           7.25         345.5         196.9         68.034         1.562         298,313           7.50         347.5         198.9         69,123         1587         315,458           7.75         349.5         200.9         70,220         1.612         332,876	194.9         66.954         1.537         281.440         6.461           196.9         68.034         1.562         298.313         6.842           198.9         69.123         1.587         315.458         7.842           200.9         70.220         1.612         332.876         7.642
7.25         345.5         196.9         68.034         1.562         298.313           7.50         347.5         198.9         69.123         1.587         315.458           7.75         349.5         200.9         70.220         1.612         332.876	196.9         68,034         1.562         298,313         6.848           198.9         69,123         1.587         315,458         7.242           200.9         70,220         1.612         332,876         7.642
7.50         347.5         198.9         69,123         1.587         315,458           7.75         349.5         200.9         70,220         1.612         332,876	198.9         69,123         1.587         315,458         7.242           200.9         70,220         1.612         332,876         7.642
7.75 349.5 200.9 70,220 1.612 332,876	200.9 70,220 1.612 332,876 7.642
7.75 349.5 200.9 70,220 1.612 332,876	200.9 70,220 1.612 332,876 7.642
8.00         351.5         202.9         71.325         1.637         350.568           Image: Solution of the second	202.9         71,325         1.637         350,568         8.048
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MHFD-Detention, Version 4.06 (July 2022)



## DETENTION BASIN OUTLET STRUCTURE DESIGN

				ersion 4.06 (July .	2022)				
	Esteban Rodrigue	z Subdivision-PDR							
Basin I D: ZONE 3	Pond 1								
ZONE 2 ZONE 1	$\frown$			Estimated	Estimated				
100-YR				Stage (ft)	Volume (ac-ft)	Outlet Type	1		
			Zone 1 (WQCV)	3.00	1.071	Orifice Plate			
	100-YEAR ORIFICE		Zone 2 (EURV)	4.41	1.725	Orifice Plate			
PERMANENT ORIFICES	ONITIOE		Zone 3 (100-year)	6.00	2.172	Weir&Pipe (Restrict)			
POOL Example Zone	Configuration (Re	tention Pond)		Total (all zones)	4.968		1		
User Input: Orifice at Underdrain Outlet (typical	v used to drain WO	CV in a Filtration Bl	MP)			1	Calculated Parame	ters for Underdrain	ı
Underdrain Orifice Invert Depth =	N/A		the filtration media	surface)	Underg	Irain Orifice Area =	N/A	ft <sup>2</sup>	-
Underdrain Orifice Diameter =									
User Input: Orifice Plate with one or more orific	es or Elliptical Slot	Weir (typically used	to drain WOCV an	d/or FURV in a sedi	imentation BMP)		Calculated Parame	ters for Plate	
Centroid of Lowest Orifice =	0.00		n bottom at Stage =			ce Area per Row =	2.840E-02	ft <sup>2</sup>	
Depth at top of Zone using Orifice Plate =	4.41		n bottom at Stage =			iptical Half-Width =	N/A	feet	
Orifice Plate: Orifice Vertical Spacing =	N/A	inches	i bottom ut otago	0.10		ical Slot Centroid =	N/A	feet	
Orifice Plate: Orifice Area per Row =	4.09		tangular openings)			Iliptical Slot Area =	N/A	ft <sup>2</sup>	
	1107	sq. monos (aco roc	stangalar oponings)		-	inprior of or a or			
User Input: Stage and Total Area of Each Orific	e Row (numbered f	rom lowest to high	(tao						
Stor input. Stage and rotal Area of Each Office	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)	1
Stage of Oriflee Controld (4)		1.47	2.94	3.40	Row 5 (optional)			Now o (optional)	1
Stage of Orifice Centroid (ft) Orifice Area (sg. inches)	4.09	4.09	4.09	4.09					
Office Area (sq. Inches,	4.09	4.09	4.09	4.09					1
	Dow O (anti)	Dow 10 (or the "	Dow 11 (orthogon	Dow 12 (anti*	Dow 12 (on the and	Dow 14 (anti*	Dow 15 (anti	Dow 16 (on the and	1
	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)	1
Stage of Orifice Centroid (ft)									1
Orifice Area (sq. inches)									1
User Inputs Vertical Orifice (Circular or Destand	ular)						Calculated Percent	ters for Vertical Ori	ifico
User Input: Vertical Orifice (Circular or Rectang		Net Colored	7						<u>Ince</u>
	Not Selected	Not Selected	G. (		0.61		Not Selected	Not Selected	- 2
Invert of Vertical Orifice =	N/A	N/A		h bottom at Stage =		tical Orifice Area =	N/A	N/A	ft <sup>2</sup>
Depth at top of Zone using Vertical Orifice =	N/A	N/A		n bottom at Stage =	= 0 ft) Vertica	I Orifice Centroid =	N/A	N/A	feet
Vertical Orifice Diameter =	N/A	N/A	inches						
User Input: Overflow Weir (Dropbox with Flat of	r Sloped Grate and	Outlet Pipe OR Red	ctangular/Trapezoid	al Weir and No Out	let Pine)		Calculated Parame	ters for Overflow W	Veir
							calculated rarame		1011
	Zone 3 Weir	Not Selected					Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	Zone 3 Weir 5.00	Not Selected N/A	ft (relative to basin	bottom at Stage = 0		e Upper Edge, H <sub>t</sub> =			feet
Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length =			ft (relative to basin feet		ft) Height of Grate	e Upper Edge, H <sub>t</sub> = /eir Slope Length =	Zone 3 Weir	Not Selected	]
	5.00	N/A		bottom at Stage = 0	ft) Height of Grate	/eir Slope Length =	Zone 3 Weir 5.00	Not Selected N/A	feet
Overflow Weir Front Edge Length =	5.00 5.00	N/A N/A	feet	bottom at Stage = 0 Gr	ft) Height of Grate Overflow W	/eir Slope Length = 0-yr Orifice Area =	Zone 3 Weir 5.00 5.00	Not Selected N/A N/A	feet
Overflow Weir Front Edge Length = Overflow Weir Grate Slope =	5.00 5.00 0.00 5.00	N/A N/A N/A	feet H:V	bottom at Stage = 0 Gr. Ov	ft) Height of Grate Overflow W ate Open Area / 10	/eir Slope Length = 0-yr Orifice Area = Area w/o Debris =	Zone 3 Weir 5.00 5.00 6.43	Not Selected N/A N/A N/A	feet feet
Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type =	5.00 5.00 0.00 5.00	N/A N/A N/A N/A	feet H:V	bottom at Stage = 0 Gr. Ov	ft) Height of Grate Overflow W ate Open Area / 10 verflow Grate Open	/eir Slope Length = 0-yr Orifice Area = Area w/o Debris =	Zone 3 Weir 5.00 5.00 6.43 19.78	Not Selected N/A N/A N/A N/A	feet feet ft <sup>2</sup>
Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides =	5.00 5.00 0.00 5.00 Close Mesh Grate	N/A N/A N/A N/A N/A	feet H:V feet	bottom at Stage = 0 Gr. Ov	ft) Height of Grate Overflow W ate Open Area / 10 verflow Grate Open	/eir Slope Length = 0-yr Orifice Area = Area w/o Debris =	Zone 3 Weir 5.00 5.00 6.43 19.78	Not Selected N/A N/A N/A N/A	feet feet ft <sup>2</sup>
Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type =	5.00 5.00 0.00 5.00 Close Mesh Grate 50%	N/A N/A N/A N/A N/A N/A	feet H:V feet %	bottom at Stage = 0 Gr. Ov	ft) Height of Grate Overflow W ate Open Area / 10 verflow Grate Open Overflow Grate Open	/eir Slope Length = 0-yr Orifice Area = Area w/o Debris = n Area w/ Debris =	Zone 3 Weir 5.00 5.00 6.43 19.78 9.89	Not Selected N/A N/A N/A N/A	feet feet ft <sup>2</sup> ft <sup>2</sup>
Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % =	5.00 5.00 0.00 5.00 Close Mesh Grate 50%	N/A N/A N/A N/A N/A N/A estrictor Plate, or R	feet H:V feet %	bottom at Stage = 0 Gr. Ov	ft) Height of Grate Overflow W ate Open Area / 10 verflow Grate Open Overflow Grate Open	/eir Slope Length = 0-yr Orifice Area = Area w/o Debris = n Area w/ Debris =	Zone 3 Weir 5.00 5.00 6.43 19.78 9.89 s for Outlet Pipe w/	Not Selected N/A N/A N/A N/A N/A Flow Restriction Pl	feet feet ft <sup>2</sup> ft <sup>2</sup>
Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = <u>User Input: Outlet Pipe w/ Flow Restriction Plate</u>	5.00 5.00 0.00 5.00 Close Mesh Grate 50% e (Circular Orifice, R Zone 3 Restrictor	N/A N/A N/A N/A N/A estrictor Plate, or F Not Selected	feet H:V feet % <u>Rectangular Orifice)</u>	bottom at Stage = 0 Gr. Ov C	ft) Height of Grate Overflow W ate Open Area / 10 verflow Grate Open Overflow Grate Open Overflow Grate Open	/eir Slope Length = 0-yr Orifice Area = Area w/o Debris = n Area w/ Debris = Iculated Parameter;	Zone 3 Weir           5.00           5.00           6.43           19.78           9.89           s for Outlet Pipe w/           Zone 3 Restrictor	Not Selected N/A N/A N/A N/A N/A Flow Restriction PI Not Selected	feet feet ft <sup>2</sup> ft <sup>2</sup> <u>ate</u>
Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = <u>User Input: Outlet Pipe w/ Flow Restriction Plate</u> Depth to Invert of Outlet Pipe =	5.00 5.00 0.00 5.00 Close Mesh Grate 50% e (Circular Orlfice, R Zone 3 Restrictor 0.25	N/A N/A N/A N/A N/A estrictor Plate, or F Not Selected N/A	feet H:V feet % Rectangular Orifice) ft (distance below b	bottom at Stage = 0 Gr. Ov	ft) Height of Grate Overflow W ate Open Area / 10 verflow Grate Open Overflow Grate Open <u>Ca</u> = 0 ft) O	<pre>//eir Slope Length = 0-yr Orifice Area = Area w/o Debris = n Area w/ Debris = lculated Parameter: utlet Orifice Area =</pre>	Zone 3 Weir 5.00 5.00 6.43 19.78 9.89 s for Outlet Pipe w/ Zone 3 Restrictor 3.08	Not Selected N/A N/A N/A N/A N/A Flow Restriction PI Not Selected N/A	feet feet ft <sup>2</sup> ft <sup>2</sup> ate ft <sup>2</sup>
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Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = <u>User Input: Outlet Pipe w/ Flow Restriction Plate</u> Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = <u>User Input: Emergency Spillway (Rectangular or</u>	5.00 5.00 0.00 5.00 Close Mesh Grate 50% e (Circular Orifice, R Zone 3 Restrictor 0.25 30.00 18.00 Trapezoidal)	N/A N/A N/A N/A N/A estrictor Plate, or F Not Selected N/A N/A	feet H:V feet % Rectangular Orifice) ft (distance below b inches inches	bottom at Stage = 0 Gr: Ov C asin bottom at Stage Half-Cent	ft) Height of Grate Overflow W ate Open Area / 10 verflow Grate Open Dverflow Grate Open <u>Ca</u> = 0 ft) Or Outle tral Angle of Restric	<pre>/eir Slope Length = 0-yr Orifice Area = Area w/o Debris = n Area w/ Debris = lculated Parameter: utlet Orifice Area = t Orifice Centroid = tor Plate on Pipe =</pre>	Zone 3 Weir 5.00 5.00 6.43 19.78 9.89 s for Outlet Pipe w/ Zone 3 Restrictor 3.08 0.85 1.77 <u>Calculated Parame</u>	Not Selected N/A N/A N/A N/A N/A <u>Flow Restriction Pl</u> Not Selected N/A N/A N/A N/A	feet feet ft <sup>2</sup> ft <sup>2</sup> ft <sup>2</sup> ft <sup>2</sup>
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Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Crest Length = Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway Invert Stage Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Reuted Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (n) CUHP Predevelopment Peak Q (cfs) = OPTIONAL Override Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, q (cfs/acr) = Peak Inflow Q (cfs) = Peak Outflow Q (cfs) = Ratio Peak Outflow to Predevelopment Q (cfs) = Max Velocity through Grate 1 (fps) =	5.00 5.00 5.00 Close Mesh Grate 50% e (Circular Orifice, R Zone 3 Restrictor 0.25 30.00 18.00 Trapezoidal) 6.50 90.00 4.00 1.00 The user can over WOCV N/A N/A N/A N/A N/A N/A N/A N/A	N/A	feet H:V feet 9% Rectangular Orifice) ft (distance below b inches inches h bottom at Stage = HP hydrographs and 2 Year 1.19 2.042 2.042 2.042 0.4 0.01 17.9 0.7 N/A Plate N/A Plate N/A S8 62	bottom at Stage = 0 Gr Ov c asin bottom at Stage Half-Cent = 0 ft)	ft) Height of Grate Overflow W ate Open Area / 10 verflow Grate Open Dverflow Grate Open Dverflow Grate Open Dverflow Grate Open Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller	<pre>/eir Slope Length = 0-yr Orifice Area = Area w/o Debris = n Area w/ Debris = n Area w/ Debris = iculated Parameter: utlet Orifice Area = t Orifice Centroid = tor Plate on Pipe = esign Flow Depth= for of Freeboard = for of Freeboard = fo</pre>	Zone 3 Weir           5.00           5.00           6.43           19.78           9.89           s for Outlet Pipe w/           Zone 3 Restrictor           3.08           0.85           1.77           Calculated Parame           0.44           7.94           1.63           7.95           chographs table (Ccc           50 Year           2.25           5.971           5.971           1.9.6           0.25           61.8           17.6           0.9           Overflow Weir 1           0.8           N/A           80           86	Not Selected N/A	feet feet ft <sup>2</sup> ft <sup>2</sup> feet radians 500 Year radians 500 Year 3.14 11.235 60.8 0.78 120.1 66.5 1.1.1 Spillway 1.8 N/A 74 83
Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Reuted Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = CUHP Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, q (cfs/acre) Predevelopment Unit Peak Flow Q (cfs) = Peak Inflow Q (cfs) = Ratio Peak Outflow to Predevelopment Q = Max Velocity through Grate 1 (fps) = Max Velocity through Grate 1 (fps) = Max Velocity through Grate 2 (fps) = Time to Drain 97% of Inflow Volume (hours) = Time to Drain 99% of Inflow Volume (hours) =	5.00 5.00 0.00 5.00 Close Mesh Grate 50% 2 (Circular Orifice, R Zone 3 Restrictor 0.25 30.00 18.00 Trapezoidal) 6.50 90.00 4.00 1.00 7 MOCV N/A 1.071 N/A N/A N/A N/A N/A N/A N/A N/A	N/A	feet H:V feet % Rectangular Orifice) ft (distance below b inches inches h bottom at Stage = h bottom at Stage = 2.042 2.042 0.4 0.01 17.9 0.7 N/A Plate N/A N/A 58 62 3.69	bottom at Stage = 0 Gr: Ov c asin bottom at Stage Half-Cent = 0 ft)	ft) Height of Grate Overflow W ate Open Area / 10 verflow Grate Open Noverflow Grate Open Diverflow Grate Open Diverflow Grate Open (Call (Call Comparison of Call Comparison (Call Comparison of Call Comparison of Call Comparison of Call Comparison (Call Comparison of Call Compari	<pre>/eir Slope Length = 0-yr Orifice Area = Area w/o Debris = n Area w/ Debris = in Area w/ Debris = itulated Parameter: utlet Orifice Area = t Orifice Centroid = tor Plate on Pipe = itor Plate on Pipe = itor of Freeboard = i</pre>	Zone 3 Weir 5.00 5.00 6.43 19.78 9.89 5 for Outlet Pipe w/ Zone 3 Restrictor 3.08 0.85 1.77 Calculated Parame 0.44 7.94 1.63 7.95 drographs table (Ccc 5.971 5.971 19.6 0.25 6.18 17.6 0.9 Overflow Weir 1 0.8 N/A 80 86 5.63	Not Selected N/A N/A N/A N/A N/A N/A N/A CELOW Restriction PI Not Selected N/A N/A N/A N/A N/A N/A ters for Spillway feet feet acres acres acre-ft Dumns W through A 100 Year 2.52 7.646 7.646 7.646 32.8 0.42 81.2 32.0 1.0 Overflow Weir 1 1.6 N/A 78 85 5.95	feet feet ft <sup>2</sup> ft <sup>2</sup> ft <sup>2</sup> feet radians 500 Year 3.14 11.235 11.235 11.235 6.0.8 0.78 120.1 66.5 1.1.1 Spillway 1.8 N/A 74 83 6.73
Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Crest Length = Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway Invert Stage Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Reuted Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (n) CUHP Predevelopment Peak Q (cfs) = OPTIONAL Override Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, q (cfs/acr) = Peak Inflow Q (cfs) = Peak Outflow Q (cfs) = Ratio Peak Outflow to Predevelopment Q (cfs) = Max Velocity through Grate 1 (fps) =	5.00 5.00 5.00 Close Mesh Grate 50% e (Circular Orifice, R Zone 3 Restrictor 0.25 30.00 18.00 Trapezoidal) 6.50 90.00 4.00 1.00 The user can over WOCV N/A N/A N/A N/A N/A N/A N/A N/A	N/A	feet H:V feet 9% Rectangular Orifice) ft (distance below b inches inches h bottom at Stage = HP hydrographs and 2 Year 1.19 2.042 2.042 2.042 0.4 0.01 17.9 0.7 N/A Plate N/A Plate N/A S8 62	bottom at Stage = 0 Gr Ov c asin bottom at Stage Half-Cent = 0 ft)	ft) Height of Grate Overflow W ate Open Area / 10 verflow Grate Open Dverflow Grate Open Dverflow Grate Open Dverflow Grate Open Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller Caller	<pre>feir Slope Length = 0-yr Orifice Area = Area w/o Debris = n Area w/ Debris = n Area w/ Debris = iculated Parameter: utlet Orifice Area = t Orifice Centroid = tor Plate on Pipe = esign Flow Depth= fop of Freeboard = fop of Freeboard = fo</pre>	Zone 3 Weir           5.00           5.00           6.43           19.78           9.89           s for Outlet Pipe w/           Zone 3 Restrictor           3.08           0.85           1.77           Calculated Parame           0.44           7.94           1.63           7.95           chographs table (Ccc           50 Year           2.25           5.971           5.971           1.9.6           0.25           61.8           17.6           0.9           Overflow Weir 1           0.8           N/A           80           86	Not Selected N/A	feet feet ft <sup>2</sup> ft <sup>2</sup> feet radians 500 Year radians 500 Year 3.14 11.235 60.8 0.78 120.1 66.5 1.1.1 Spillway 1.8 N/A 74 83



# DETENTION BASIN OUTLET STRUCTURE DESIGN Outflow Hydrograph Workbook Filename:

Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

								ed in a separate		011110
Time Interval	SOURCE	CUHP WQCV [cfs]	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
	TIME 0:00:00		EURV [cfs]	2 Year [cfs]	5 Year [cfs]		25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	
5.00 min	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.11	0.01	0.36
	0:20:00	0.00	0.00	3.95	5.38	6.49	4.20	5.04	5.30	7.23
	0:25:00	0.00	0.00	9.91	14.12	17.69	9.76	12.07	13.28	18.74
	0:30:00	0.00	0.00	15.45	21.82	27.06	25.55	33.61	39.94	59.89
	0:35:00	0.00	0.00	17.67	24.42	29.93	40.37	53.07	67.05	99.52
	0:40:00	0.00	0.00	17.87	24.32	29.66	46.68	61.22	79.13	116.66
	0:45:00 0:50:00	0.00	0.00	17.12	23.17 21.85	28.11 26.37	47.26 45.32	61.80 58.80	81.23 77.80	120.14 115.60
	0:55:00	0.00	0.00	15.17	20.62	24.82	42.42	54.84	72.82	108.65
	1:00:00	0.00	0.00	14.36	19.46	23.42	39.38	50.75	68.09	101.70
	1:05:00	0.00	0.00	13.66	18.43	22.23	36.63	47.05	63.74	95.44
	1:10:00	0.00	0.00	12.97	17.65	21.33	33.97	43.49	58.90	88.33
	1:15:00	0.00	0.00	12.26	16.85	20.53	31.64	40.32	54.09	80.98
	1:20:00	0.00	0.00	11.54 10.82	15.93 14.95	19.54 18.25	29.34 27.00	37.20 34.05	49.28 44.47	73.47 65.94
	1:30:00	0.00	0.00	10.82	13.96	16.25	24.62	30.88	39.90	58.84
	1:35:00	0.00	0.00	9.43	13.03	15.56	22.27	27.76	35.53	52.05
	1:40:00	0.00	0.00	8.87	12.12	14.51	20.08	24.87	31.50	45.84
	1:45:00	0.00	0.00	8.49	11.40	13.80	18.34	22.68	28.47	41.45
	1:50:00	0.00	0.00	8.22	10.81	13.22	17.07	21.06	26.21	38.02
	1:55:00 2:00:00	0.00	0.00	7.81	10.26	12.64	16.03	19.70	24.27	35.01
	2:05:00	0.00	0.00	7.32	9.71 8.91	11.96 10.94	15.08 13.81	18.46 16.86	22.51 20.44	32.25 29.14
	2:10:00	0.00	0.00	5.97	7.98	9.75	12.36	15.04	18.18	25.82
	2:15:00	0.00	0.00	5.29	7.07	8.60	10.93	13.26	16.00	22.62
	2:20:00	0.00	0.00	4.65	6.20	7.50	9.56	11.55	13.93	19.60
	2:25:00	0.00	0.00	4.05	5.39	6.49	8.27	9.94	11.96	16.70
	2:30:00 2:35:00	0.00	0.00	3.49	4.64	5.54	7.05	8.40	10.05	13.89
	2:40:00	0.00	0.00	2.96 2.45	3.92 3.23	4.65	5.87 4.75	6.91 5.50	8.19 6.42	11.17 8.56
	2:45:00	0.00	0.00	1.98	2.61	3.07	3.71	4.19	4.77	6.17
	2:50:00	0.00	0.00	1.58	2.07	2.48	2.77	3.05	3.40	4.43
	2:55:00	0.00	0.00	1.29	1.71	2.07	2.12	2.34	2.53	3.32
	3:00:00	0.00	0.00	1.09	1.44	1.75	1.69	1.87	1.97	2.55
	3:05:00 3:10:00	0.00	0.00	0.92	1.22	1.48 1.25	1.38 1.13	1.52 1.24	1.55	1.97 1.54
	3:15:00	0.00	0.00	0.78	0.87	1.05	0.94	1.24	0.98	1.34
	3:20:00	0.00	0.00	0.56	0.73	0.89	0.78	0.85	0.78	0.94
	3:25:00	0.00	0.00	0.47	0.61	0.73	0.64	0.69	0.63	0.75
	3:30:00	0.00	0.00	0.39	0.50	0.60	0.52	0.57	0.51	0.61
	3:35:00	0.00	0.00	0.32	0.41	0.48	0.42	0.45	0.41	0.49
	3:40:00 3:45:00	0.00	0.00	0.26	0.32	0.38	0.33	0.36	0.33	0.38
	3:50:00	0.00	0.00	0.20	0.25	0.30	0.26	0.28	0.25	0.29
	3:55:00	0.00	0.00	0.13	0.14	0.25	0.14	0.21	0.19	0.15
	4:00:00	0.00	0.00	0.07	0.10	0.11	0.10	0.10	0.09	0.09
	4:05:00	0.00	0.00	0.05	0.06	0.07	0.06	0.06	0.05	0.05
	4:10:00 4:15:00	0.00	0.00	0.03	0.04	0.04	0.03	0.03	0.02	0.02
	4:15:00	0.00	0.00	0.00	0.02	0.02	0.00	0.00	0.00	0.00
	4:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:30:00 4:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:50:00 4:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:10:00 5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:25:00 5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:45:00 5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

ZONE 1 AND 2 ORIFICES Example Zone Configuration (Retention Pond)

-100-YEAR ORIFICE

Depth Increment = 0.25 ft

Watershed	Information

PERMA

itersned information		
Selected BMP Type =	EDB	
Watershed Area =	77.00	acres
Watershed Length =	2,900	ft
Watershed Length to Centroid =	1,300	ft
Watershed Slope =	0.040	ft/ft
Watershed Imperviousness =	16.00%	percent
Percentage Hydrologic Soil Group A =	100.0%	percent
Percentage Hydrologic Soil Group B =	0.0%	percent
Percentage Hydrologic Soil Groups C/D =	0.0%	percent
Target WQCV Drain Time =	40.0	hours
Location for 1-hr Rainfall Depths =	User Input	

## After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

the embedded colorado orban nyard	graphinoceue	10.
Water Quality Capture Volume (WQCV) =	0.629	acre-feet
Excess Urban Runoff Volume (EURV) =	1.033	acre-feet
2-yr Runoff Volume (P1 = 1.19 in.) =	0.614	acre-feet
5-yr Runoff Volume (P1 = 1.5 in.) =	0.919	acre-feet
10-yr Runoff Volume (P1 = 1.75 in.) =	1.196	acre-feet
25-yr Runoff Volume (P1 = 2 in.) =	2.333	acre-feet
50-yr Runoff Volume (P1 = 2.25 in.) =	3.430	acre-feet
100-yr Runoff Volume (P1 = 2.52 in.) =	4.942	acre-feet
500-yr Runoff Volume (P1 = 3.14 in.) =	8.258	acre-feet
Approximate 2-yr Detention Volume =	0.632	acre-feet
Approximate 5-yr Detention Volume =	0.856	acre-feet
Approximate 10-yr Detention Volume =	1.102	acre-feet
Approximate 25-yr Detention Volume =	1.449	acre-feet
Approximate 50-yr Detention Volume =	1.797	acre-feet
Approximate 100-yr Detention Volume =	2.534	acre-feet

Define	Zones	and	Basi	in	Geome	etry
		ž	Zone	1	Volume	(W0

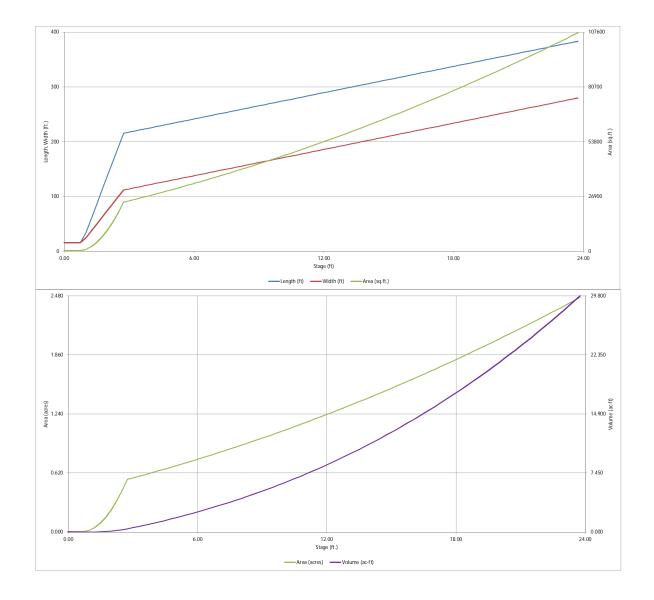
Jenne Zones and Basin Geometry		
Zone 1 Volume (WQCV) =	0.629	acre-feet
Zone 2 Volume (EURV - Zone 1) =	0.403	acre-feet
Zone 3 Volume (100-year - Zones 1 & 2) =	1.501	acre-feet
Total Detention Basin Volume =	2.534	acre-feet
Initial Surcharge Volume (ISV) =	82	ft <sup>3</sup>
Initial Surcharge Depth (ISD) =	0.33	ft
Total Available Detention Depth (H <sub>total</sub> ) =	6.00	ft
Depth of Trickle Channel (H <sub>TC</sub> ) =	0.50	ft
Slope of Trickle Channel (S <sub>TC</sub> ) =	0.010	ft/ft
Slopes of Main Basin Sides (Smain) =	4	H:V
Basin Length-to-Width Ratio (R <sub>L/W</sub> ) =	2	

Initial Surcharge Area (A <sub>ISV</sub> ) =	249	ft 2
Surcharge Volume Length ( $L_{ISV}$ ) =	15.8	ft
Surcharge Volume Width (WISV) =	15.8	ft
Depth of Basin Floor $(H_{FLOOR})$ =	1.92	ft
Length of Basin Floor $(L_{FLOOR})$ =	215.5	ft
Width of Basin Floor ( $W_{FLOOR}$ ) =	111.8	ft
Area of Basin Floor $(A_{FLOOR}) =$		ft 2
Volume of Basin Floor ( $V_{FLOOR}$ ) =	17,142	ft <sup>3</sup>
Depth of Main Basin (H <sub>MAIN</sub> ) =	3.25	ft
Length of Main Basin ( $L_{MAIN}$ ) =	241.5	ft
Width of Main Basin ( $W_{MAIN}$ ) =	137.8	ft
Area of Main Basin (A <sub>MAIN</sub> ) =	33,270	ft 2
Volume of Main Basin (VMAN) =	92.803	ft 3

Volume of Main Basin (V<sub>MAIN</sub>) : ft <sup>:</sup> Volume of Main Basin ( $V_{MAIN}$ ) = 92,803 ft <sup>3</sup> Calculated Total Basin Volume ( $V_{total}$ ) = 2.529 acre-feet

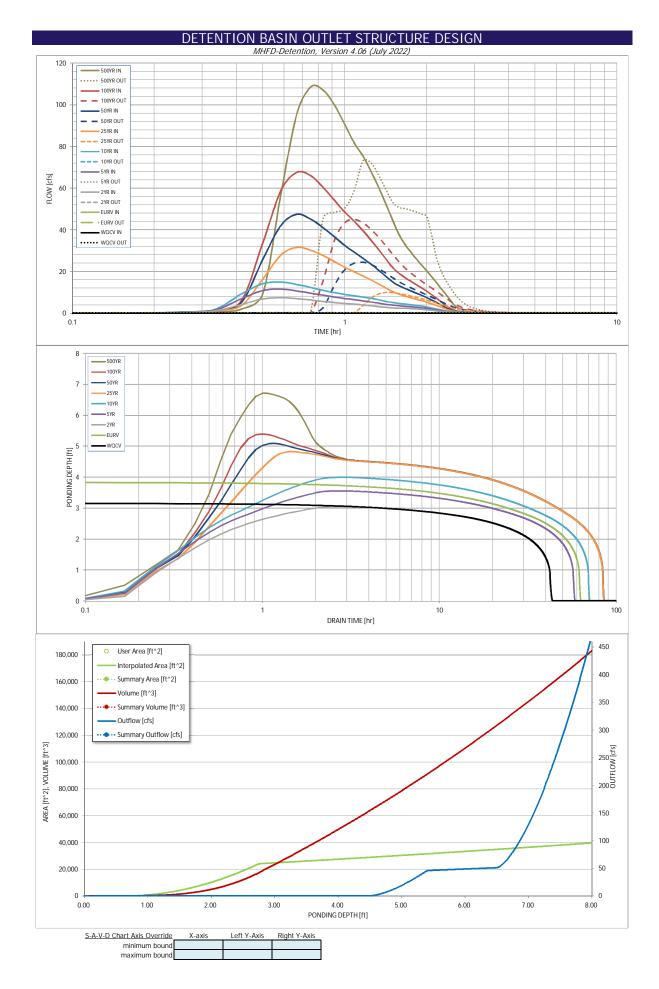
E	Depth Increment =	0.25	ft				Ontingel			
			Optional				Optional			
ntion Pond)	Stage - Storage	Stage	Override	Length	Width	Area	Override	Area	Volume	Volume
	Description	(ft)	Stage (ft)	(fť)	(ft)	(ft 2)	Area (ft <sup>2</sup> )	(acre)	(ft 3)	(ac-ft)
	Top of Micropool	0.00		15.8	15.8	249		0.006		
	ISV	0.33		15.8	15.8	249		0.006	82	0.002
		0.50		15.8	15.8	249		0.006	125	0.003
	L									
	1	0.75		15.8	15.8	249		0.006	187	0.004
		1.00		33.5	24.3	813		0.019	293	0.007
	L									
	1	1.25		59.5	36.8	2,187		0.050	654	0.015
		1.50		85.5	49.3	4,212		0.097	1,441	0.033
	1	1.75		111.5	61.8	6,887		0.158	2,815	0.065
		2.00		137.5	74.3	10,212		0.234	4,938	0.113
		2.25		163.5	86.8	14,186		0.326	7,975	0.183
		2.50		189.5	99.3	18,811		0.432	12,086	0.277
	Floor	2.75		215.5	111.8	24,086		0.553	17,434	0.400
		3.00		217.5	113.8	24,744		0.568	23,538	0.540
	Zone 1 (WQCV)	3.16		218.7	115.1	25,170		0.578	27,531	0.632
Optional User Overrides		3.25		219.5	115.8	25,411		0.583	29,807	0.684
acre-feet		3.50		221.5	117.8	26,085		0.599	36,244	0.832
acre-feet		3.75		223.5	119.8	26,768		0.615	42,851	0.984
1.19 inches	Zone 2 (EURV)	3.83		224.1	120.4	26,988		0.620	45,001	1.033
	ZUTIE Z (EURV)									
1.50 inches		4.00		225.5	121.8	27,458		0.630	49,629	1.139
1.75 inches		4.25		227.5	123.8	28,157		0.646	56,580	1.299
2.00 inches		4.50		229.5	125.8	28,863		0.663	63,708	1.463
2.25 inches		4.75		231.5	127.8	29,578		0.679	71,013	1.630
2.52 inches	L	5.00		233.5	129.8	30,300		0.696	78,497	1.802
inches		5.25		235.5	131.8	31,031		0.712	86,164	1.978
	1	5.50			133.8					
	L			237.5		31,769		0.729	94,014	2.158
	1	5.75		239.5	135.8	32,516		0.746	102,049	2.343
		6.00		241.5	137.8	33,270		0.764	110,272	2.531
	<u> </u>									
	Zone 3 (100-year)	6.01		241.5	137.9	33,301		0.764	110,605	2.539
		6.25		243.5	139.8	34,033		0.781	118,685	2.725
		6.50		245.5	141.8	34,803		0.799	127,289	2.922
		6.75		247.5	143.8	35,582		0.817	136,087	3.124
		7.00		249.5	145.8	36,368		0.835	145,081	3.331
	1	7.25		251.5	147.8	37,163		0.853	154,272	3.542
		7.50		253.5	149.8	37,965		0.872	163,663	3.757
		7.75		255.5	151.8	38,776		0.890	173,255	3.977
							-			
	L	8.00		257.5	153.8	39,594		0.909	183,052	4.202
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MHFD-Detention, Version 4.06 (July 2022)



### DETENTION BASIN OUTLET STRUCTURE DESIGN MHFD-Detention, Version 4.06 (July 2022)

Project				ersion 4.06 (July L	2022)				
Basin ID:	Esteban Rodrigue	z Subdivision-PDR							
ZONE 3	Pond 2								
ZONE 2	$\bigcirc$			Estimated	Estimated				
				Stage (ft)	Volume (ac-ft)	Outlet Type	1		
			Zone 1 (WQCV)	3.16	0.629	Orifice Plate			
1	100-YEAR ORIFICE		Zone 2 (EURV)	3.83	0.403	Orifice Plate			
PERMANENT ORIFICES	ONITIOL		Zone 3 (100-year)	6.01	1.501	Weir&Pipe (Restrict)			
POOL Example Zone	Configuration (Re	tention Pond)		Total (all zones)	2.534	,	1		
User Input: Orifice at Underdrain Outlet (typical	v used to drain WC	CV in a Filtration Bl	MP)			1	Calculated Parame	ters for Underdrain	
Underdrain Orifice Invert Depth =	N/A		the filtration media	surface)	Underd	Irain Orifice Area =	N/A	ft <sup>2</sup>	
Underdrain Orifice Diameter =	N/A	inches	the fill alon filedia	Surrace)		Orifice Centroid =	N/A	feet	
	N/A	inches			Underdrai		N/A	leet	
User Input: Orifice Plate with one or more orific	os or Elliptical Slot	Wair (typically used	to drain WOCV an	d/or FLIPV in a sodi	mentation BMP)		Calculated Parame	tors for Diata	
Centroid of Lowest Orifice =	0.00		n bottom at Stage =			ce Area per Row =	N/A	ft <sup>2</sup>	
			•				-	feet	
Depth at top of Zone using Orifice Plate =	3.83 N/A	inches	n bottom at Stage =	= 0 1()		iptical Half-Width = ical Slot Centroid =	N/A N/A	feet	
Orifice Plate: Orifice Vertical Spacing =							-	ft <sup>2</sup>	
Orifice Plate: Orifice Area per Row =	N/A	sq. inches			E	Iliptical Slot Area =	N/A	ft-	
User Input: Stage and Total Area of Each Orific									1
	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)	
Stage of Orifice Centroid (ft)	0.00	1.20	2.40	3.00					
Orifice Area (sq. inches)	2.70	0.90	0.70	0.50					]
		n	1	n	1	n	1	1	1
	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)	
Stage of Orifice Centroid (ft)									
Orifice Area (sq. inches)									
		·		·			·	·	·
User Input: Vertical Orifice (Circular or Rectang	ular)						Calculated Parame	ters for Vertical Ori	fice
	Not Selected	Not Selected	1				Not Selected	Not Selected	
Invert of Vertical Orifice =	N/A	N/A	ft (relative to basi	n bottom at Stage =	= 0 ft) Ver	tical Orifice Area =	N/A	N/A	ft <sup>2</sup>
Depth at top of Zone using Vertical Orifice =	N/A	N/A		bottom at Stage =		I Orifice Centroid =	N/A	N/A	feet
Vertical Orifice Diameter =	N/A	N/A	inches	i bottom at olugo					
Vertical Office Diameter =	11/74	11/74	Inches						
Llean Innut. Quanflaus Wain (Drenkess with Elet a	- Classed Crate and		aton au don /Tron on oir	al Main and No. Out	lat Dina)		Coloulated Danama	tore for Overflow M	/ a la
User Input: Overflow Weir (Dropbox with Flat o			Tangular/Trapezoid	al weir and No Out	<u>let Pipe)</u>			ters for Overflow V	ven
	Zone 3 Weir	Not Selected					Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	4.50	N/A		bottom at Stage = 0 1	-		4.50	N/A	feet
Overflow Weir Front Edge Length =	8.00	N/A	feet		Overflow W	/eir Slope Length =	8.00	N/A	feet
Overflow Weir Grate Slope =	0.00	N/A	H:V	Gra	ate Open Area / 10	0-yr Orifice Area =	11.43	N/A	
Horiz. Length of Weir Sides =	8.00	N/A	feet	Ον	orflow Crate Open	Area w/o Debris =			
Overflow Grate Type =	Close Mesh Grate	N/A			ernow Grate Open		50.62	N/A	ft <sup>2</sup>
Debris Clogging % =				0	verflow Grate Open		50.62 25.31	N/A N/A	ft <sup>2</sup> ft <sup>2</sup>
	50%	N/A	%	C					
	50%		%	C					
User Input: Outlet Pipe w/ Flow Restriction Plate		N/A	-	C	verflow Grate Oper	n Area w/ Debris =	25.31		ft²
	e (Circular Orifice, R	N/A estrictor Plate, or F	-	C	verflow Grate Oper	n Area w/ Debris =	25.31 s for Outlet Pipe w/	N/A 7 Flow Restriction Pl	ft²
User Input: Outlet Pipe w/ Flow Restriction Plate		N/A estrictor Plate, or F Not Selected	Rectangular Orifice)		verflow Grate Oper	n Area w/ Debris =	25.31 s for Outlet Pipe w/ Zone 3 Restrictor	N/A	ft <sup>2</sup>
User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe =	e (Circular Orifice, R Zone 3 Restrictor 0.25	N/A estrictor Plate, or F Not Selected N/A	Rectangular Orifice) ft (distance below b	C asin bottom at Stage	verflow Grate Oper <u>Ca</u> = 0 ft) Ot	n Area w/ Debris = Iculated Parameters utlet Orifice Area =	25.31 s for Outlet Pipe w/ Zone 3 Restrictor 4.43	N/A / Flow Restriction Pl Not Selected N/A	ft <sup>2</sup>
User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter =	e (Circular Orifice, R Zone 3 Restrictor 0.25 36.00	N/A estrictor Plate, or F Not Selected	Rectangular Orifice) ft (distance below b inches	asin bottom at Stage	verflow Grate Oper Ca = 0 ft) Or Outlet	n Area w/ Debris = <u>lculated Parameter</u> ; utlet Orifice Area = t Orifice Centroid =	25.31 s for Outlet Pipe w/ Zone 3 Restrictor 4.43 1.02	N/A Flow Restriction PI Not Selected N/A N/A	ft <sup>2</sup> ate ft <sup>2</sup> feet
User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe =	2 (Circular Orifice, R Zone 3 Restrictor 0.25 36.00	N/A estrictor Plate, or F Not Selected N/A	Rectangular Orifice) ft (distance below b	asin bottom at Stage	verflow Grate Oper <u>Ca</u> = 0 ft) Ot	n Area w/ Debris = <u>lculated Parameter</u> ; utlet Orifice Area = t Orifice Centroid =	25.31 s for Outlet Pipe w/ Zone 3 Restrictor 4.43	N/A / Flow Restriction Pl Not Selected N/A	ft <sup>2</sup>
User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert =	e (Circular Orifice, R Zone 3 Restrictor 0.25 36.00 21.60	N/A estrictor Plate, or F Not Selected N/A	Rectangular Orifice) ft (distance below b inches	asin bottom at Stage	verflow Grate Oper Ca = 0 ft) Or Outlet	n Area w/ Debris = <u>lculated Parameter</u> ; utlet Orifice Area = t Orifice Centroid =	25.31 zone 3 Restrictor 4.43 1.02 1.77	N/A Flow Restriction PI Not Selected N/A N/A N/A	ft <sup>2</sup> ate ft <sup>2</sup> feet
User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or	e (Circular Orifice, R Zone 3 Restrictor 0.25 36.00 21.60 <u>Trapezoidal)</u>	N/A estrictor Plate, or F Not Selected N/A N/A	Rectangular Orifice) ft (distance below b inches inches	asin bottom at Stage Half-Cent	verflow Grate Oper <u>Ca</u> = 0 ft) Or Outlei ral Angle of Restric	n Area w/ Debris = <u>lculated Parameter</u> : utlet Orifice Area = t Orifice Centroid = tor Plate on Pipe =	25.31 s for Outlet Pipe w/ Zone 3 Restrictor 4.43 1.02 1.77 <u>Calculated Parame</u>	N/A / Flow Restriction PI Not Selected N/A N/A N/A ters for Spillway	ft <sup>2</sup> ate ft <sup>2</sup> feet
User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage=	e (Circular Orifice. R Zone 3 Restrictor 0.25 36.00 21.60 Trapezoidal) 6.50	N/A estrictor Plate, or R Not Selected N/A N/A ft (relative to basin	Rectangular Orifice) ft (distance below b inches	asin bottom at Stage Half-Cent	verflow Grate Oper <u>Ca</u> = 0 ft) Or Outlet ral Angle of Restric Spillway D	n Area w/ Debris = <u>lculated Parameter</u> : utlet Orifice Area = t Orifice Centroid = tor Plate on Pipe = vesign Flow Depth=	25.31 s for Outlet Pipe w/ Zone 3 Restrictor 4.43 1.02 1.77 Calculated Parame 0.46	N/A Flow Restriction Pl Not Selected N/A N/A N/A ters for Spillway feet	ft <sup>2</sup> ft <sup>2</sup> ft <sup>2</sup> feet
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User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage = Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Routed Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = CUHP Predevelopment Peak Q (cfs) = OPTIONAL Override Predevelopment Peak Q (cfs) =	E (Circular Orifice, R           Zone 3 Restrictor           0.25           36.00           21.60           Trapezoidal)           6.50           70.00           4.00           1.00	N/A estrictor Plate, or F Not Selected N/A N/A ft (relative to basin feet H:V feet ride the default CU EURV N/A 1.033 N/A N/A N/A	Rectangular Orifice) ft (distance below b inches inches n bottom at Stage = HP hydrographs an 2 Year 1.19 0.614 0.614 0.6	asin bottom at Stage Half-Cent = 0 ft) 5 Year 1.50 0.919 0.919 1.2	verflow Grate Oper <u>Ca</u> = 0 ft) Or Outled ral Angle of Restric Spillway D Stage at T Basin Area at T Basin Volume at T <u>entering new value</u> <u>10 Year</u> <u>1.75</u> <u>1.196</u> <u>1.7</u>	n Area w/ Debris = lculated Parameter: utlet Orifice Area = t Orifice Centroid = tor Plate on Pipe = lesign Flow Depth= Top of Freeboard = op of Freeboard = op of Freeboard = les in the Inflow Hyy 25 Year 2.00 2.333 2.333 15.2	25.31 Zone 3 Restrictor 4.43 1.02 1.77 <u>Calculated Parame</u> 0.46 7.96 0.91 4.17 <i>drographs table (Ccc</i> 50 Year 2.25 3.430 3.430 3.2	N/A Flow Restriction PI Not Selected N/A N/A N/A N/A ters for Spillway feet feet acres acre-ft 100 Year 2.52 4.942 4.942 4.91	<i>F).</i> 500 Year 3.14 8.258 8.258 8.9.1
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User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length = Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Routed Hydrograph Results Design Storm Return Period = One-Hour Rainfail Depth (in) = CUHP Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = CUHP Predevelopment Peak Q (cfs) = OPTIONAL Override Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, q (cfs/acre) = Peak Inflow Q (cfs) =	E (Circular Orifice, R           Zone 3 Restrictor           0.25           36.00           21.60             Trapezoidal)           6.50           70.00           4.00           1.00             The user can over           WOCV           N/A           N/A           N/A           N/A           N/A           N/A           N/A	N/A estrictor Plate, or F Not Selected N/A N/A ft (relative to basin feet H:V feet ride the default CU EURV N/A 1.033 N/A N/A N/A N/A N/A N/A N/A N/A	Rectangular Orifice) ft (distance below b inches inches in bottom at Stage = <i>IHP hydrographs an</i> 2 Year 1.19 0.614 0.614 0.61 0.01 7.4	asin bottom at Stage Half-Cent = 0 ft) d runoff volumes by 5 Year 1.50 0.919 0.919 1.2 0.02 11.6	verflow Grate Open <u>Ca</u> = 0 ft) Or Outlef ral Angle of Restric Spillway D Stage at T Basin Area at T Basin Area at T Basin Volume at T <u>entering new value</u> <u>1.75</u> <u>1.196</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u>	n Area w/ Debris = lculated Parameter: utlet Orifice Area = t Orifice Centroid = tor Plate on Pipe = lesign Flow Depth = op of Freeboard = op of Freeboard = op of Freeboard = cop of Freeboard = log of Freeboard = 25 Year 2.00 2.333 15.2 0.20 31.6	25.31 25.31 20ne 3 Restrictor 4.43 1.02 1.77 2alculated Parame 0.46 7.96 0.91 4.17 drographs table (Ccc 50 Year 2.25 3.430 3.430 3.0.2 0.39 47.5	N/A  Flow Restriction PI Not Selected N/A N/A N/A N/A ters for Spillway feet feet acres acre-ft  fourns W through A 100 Year 2.52 4.942 4.942 4.942 4.942 4.942 6.64	<i>F).</i> 500 Year 3.14 8.258 8.258 8.258 8.1.16 1.1.6 108.6
User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Routed Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = CUHP Predevelopment Peak Q (cfs) = Predevelopment Peak Q (cfs) = Peak Inflow Q (cfs) = Peak Nufflow Q (cfs) = Peak Nufflow Q (cfs) =	E. (Circular Orifice, R           Zone 3 Restrictor           0.25           36.00           21.60             Trapezoidal)           6.50           70.00           4.00           1.00             The user can over           WQCV           N/A	N/A estrictor Plate, or F Not Selected N/A N/A If (relative to basin feet H:V feet ride the default CU EURV N/A 1.033 N/A N/A N/A N/A N/A N/A N/A N/A	Rectangular Orifice)         ft (distance below b         inches         inches         inches         n bottom at Stage =         HP hydrographs and         2 Year         1.19         0.614         0.6         0.01         7.4         0.2	asin bottom at Stage Half-Cent = 0 ft)	verflow Grate Oper <u>Ca</u> = 0 ft) Ou Outlef ral Angle of Restric Spillway D Stage at T Basin Area at T Basin Volume at T <u>entering new value</u> <u>1.75</u> <u>1.196</u> <u>1.796</u> <u>1.796</u> <u>1.70</u> <u>0.02</u> <u>14.9</u> <u>0.3</u>	n Area w/ Debris = lculated Parameter: utlet Orifice Area = t Orifice Centroid = tor Plate on Pipe = tor Plate on Plat	25.31 Zone 3 Restrictor 4.43 1.02 1.77 <u>Calculated Parame</u> 0.46 7.96 0.91 4.17 <i>drographs table (Ccc</i> 50 Year 2.25 3.430 3.430 3.430 3.430 3.435	N/A Flow Restriction PI Not Selected N/A N/A N/A N/A ters for Spillway feet feet acres acre-ft acres acre-ft 100 Year 2.52 4.942 4.942 4.942 0.64 67.6 45.0	<ul> <li><i>F</i>).</li> <li><i>5</i>00 Year</li> <li>3.14</li> <li>8.258</li> <li>8.258</li> <li>8.258</li> <li>8.258</li> <li>7.16</li> <li>108.6</li> <li>73.1</li> </ul>
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User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage = Spillway Crest Length = Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Routed Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = CUHP Redevelopment Peak Q (cfs) = OPTIONAL Override Predevelopment Peak Q (cfs) = Peak Inflow Q (cfs) = Peak Inflow Q (cfs) = Ratio Peak Outflow Q for = Structure Controlling Flow =	e (Circular Orifice, R Zone 3 Restrictor 0.25 36.00 21.60 Trapezoidal) 6.50 70.00 4.00 1.00 700 N/A N/A N/A N/A N/A N/A N/A Plate	N/A estrictor Plate, or F Not Selected N/A N/A ft (relative to basin feet H:V feet ride the default CU EURV N/A 1.033 N/A	Rectangular Orifice) ft (distance below b inches inches inches n bottom at Stage = HP hydrographs an 2 Year 1.19 0.614 0.614 0.614 0.614 0.614 0.7.4 0.2 N/A Plate	asin bottom at Stage Half-Cent = 0 ft) 5 Year 1.50 0.919 0.919 1.2 0.02 11.6 0.3 0.2 Plate	verflow Grate Open <u>Ca</u> = 0 ft) Ou Outlet ral Angle of Restric Spillway D Stage at T Basin Area at T Basin Volume at T <u>entering new value</u> <u>10 Year</u> <u>1.75</u> <u>1.196</u> <u>1.196</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.296</u> <u>1.4.9</u> <u>0.2</u> Plate	n Area w/ Debris = lculated Parameter: utlet Orifice Area = t Orifice Centroid = tor Plate on Pipe = lesign Flow Depth= op of Freeboard = op of Freeboard = op of Freeboard = log of Freeboard = log of Freeboard = log of Freeboard = log of Stear 2.00 2.333 1.5.2 0.20 31.6 10.0 0.7 Overflow Weir 1	25.31 25.31 Zone 3 Restrictor 4.43 1.02 1.77 Calculated Parame 0.46 7.96 0.91 4.17 drographs table (CCC 50 Year 2.25 3.430 3.430 3.02 0.39 47.5 24.5 0.8 Overflow Weir 1	N/A  Flow Restriction PI Not Selected N/A N/A N/A N/A ters for Spillway feet feet acres acre-ft  Nums W through A 100 Year 2.52 4.942 4.942 4.942 4.942 4.942 4.942 4.942 4.942 0.64 67.6 45.0 0.9 Overflow Weir 1	<i>F).</i> 500 Year 3.14 8.258 8.258 8.258 8.9.1 1.16 108.6 7.3.1 0.8 Spillway
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N/A N/A N/A N/A	N/A estrictor Plate, or F Not Selected N/A N/A ft (relative to basin feet H:V feet ride the default CU EURV N/A 1.033 N/A	Rectangular Orifice)         ft (distance below b         inches         inches         inches         n bottom at Stage =         HP hydrographs an         2 Year         1.19         0.614         0.614         0.614         0.2         N/A         Plate         N/A         N/A         A1         42	asin bottom at Stage Half-Cent = 0 ft) 5 Year 1.50 0.919 0.919 1.2 0.02 11.6 0.3 0.2 Plate N/A N/A N/A 55 55 57	verflow Grate Open <u>Ca</u> = 0 ft) Ou Outlet ral Angle of Restric Spillway D Stage at T Basin Area at T Basin Volume at T <i>entering new valuk</i> <u>10 Year</u> <u>1.75</u> <u>1.196</u> <u>1.196</u> <u>1.75</u> <u>1.196</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> 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<u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.796</u> <u>1.707</u> <u>0.22000</u> <u>Plate</u> <u>N/A</u> <u>666</u> <u>669</u>	n Area w/ Debris = lculated Parameter: utlet Orifice Area = t Orifice Centroid = tor Plate on Pipe = lesign Flow Depth= op of Freeboard = op of Freeboard = op of Freeboard = log of Streeboard =	25.31 Zone 3 Restrictor 4.43 1.02 1.77 Calculated Parame 0.46 7.96 0.91 4.17 drographs table (CCC 50 Year 2.25 3.430 3.430 3.430 3.02 0.39 47.5 2.4.5 0.8 Overflow Weir 1 0.5 N/A 75 81	N/A  Flow Restriction PI Not Selected N/A N/A N/A N/A ters for Spillway feet feet acres acre-ft  Nums W through A 100 Year 2.52 4.942 4.942 4.942 4.942 4.942 4.942 4.942 4.942 4.942 4.942 4.942 4.942 4.942 4.942 4.942 4.942 4.942 4.942 4.942 4.942 4.942 4.942 4.942 4.942 4.942 4.942 4.942 4.942 4.942 4.942 4.942 4.942 4.942 4.942 4.942 4.942 4.942 4.942 4.942 4.942 4.942 4.942 4.942 4.942 4.942 4.942 4.942 4.942 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User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length = Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Routed Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = CUHP Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, Q (cfs/acre) = Predevelopment Unit Peak Flow, Q (cfs/acre) = Peak Inflow Q (cfs) = Peak Outflow to Predevelopment Q = Structure Controlling Flow = Max Velocity through Grate 1 (fps) = Max Velocity through Grate 1 (fps) = Time to Drain 97% of Inflow Volume (hours) = Time to Drain 99% of Inflow Volume (hours) = Maximum Ponding Depth (ft) =	E (Circular Orifice, R           Zone 3 Restrictor           0.25           36.00           21.60           Trapezoidal)           6.50           70.00           4.00           1.00             The user can over           WOCV           N/A           0.629           N/A           A1           42           3.16	N/A estrictor Plate, or F Not Selected N/A N/A It (relative to basin feet H:V feet ride the default CU EURV N/A 1.033 N/A 1.033 N/A	Rectangular Orifice)           ft (distance below b           inches           inches           inches           n bottom at Stage = <i>HP hydrographs an</i> 2 Year           1.19           0.614           0.614           0.6 <i>N/A Plate N/A N/A A</i> 1           42           3.05	asin bottom at Stage Half-Cent = 0 ft) = 0 ft) = 0 ft = 0.919 0.919 0.919 1.2 = 0.02 11.6 0.3 0.2 Plate N/A N/A 55 57 3.55	verflow Grate Open Ca = 0 ft) Or Outlef ral Angle of Restric Spillway D Stage at T Basin Area at T Ca Ca Ca Ca Ca Ca Ca Ca Ca Ca	n Area w/ Debris = lculated Parameter: utlet Orifice Area = t Orifice Centroid = tor Plate on Pipe = lesign Flow Depth = op of Freeboard = op of Freeboard = op of Freeboard = 2.00 2.333 15.2 2.333 15.2 0.20 31.6 10.0 0.7 Overflow Weir 1 0.2 N/A 78 82 4.82	25.31 Zone 3 Restrictor 4.43 1.02 1.77 <u>Calculated Parame</u> 0.46 7.96 0.91 4.17 <i>drographs table (Ccc</i> 50 Year 2.25 3.430 3.430 3.430 3.430 3.02 0.39 47.5 24.5 0.8 Overflow Weir 1 0.5 N/A 75 81 5.09	N/A  Flow Restriction PI Not Selected N/A N/A N/A N/A ters for Spillway feet feet acres acre-ft  N/A 100 Year 2.52 4.942 4.942 4.942 4.942 4.942 4.942 0.64 67.6 45.0 0.9 Overflow Weir 1 0.9 N/A 72 80 5.39	<ul> <li><i>F</i>).</li> <li>500 Year</li> <li>3.14</li> <li>8.258</li> <li>8.9.1</li> <li>1.16</li> <li>108.6</li> <li>73.1</li> <li>0.8</li> <li>Spillway</li> <li>1.0</li> <li>N/A</li> <li>65</li> <li>77</li> <li>6.71</li> </ul>



# DETENTION BASIN OUTLET STRUCTURE DESIGN Outflow Hydrograph Workbook Filename:

Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

BUDC         DUPP         DUPP <thdupp< th="">         DUPP         DUPP         <th< th=""><th></th><th>The user can o</th><th>verride the calcu</th><th>ulated inflow hyd</th><th>drographs from</th><th>this workbook w</th><th>ith inflow hydro</th><th>graphs develop</th><th>ed in a separate</th><th>program.</th><th></th></th<></thdupp<>		The user can o	verride the calcu	ulated inflow hyd	drographs from	this workbook w	ith inflow hydro	graphs develop	ed in a separate	program.	
xxxxxxxxxxxxxxxxxxxxxxxxxxxxxxxxxxxx		SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00 <th< th=""><th>Time Interval</th><th>TIME</th><th>WQCV [cfs]</th><th>EURV [cfs]</th><th>2 Year [cfs]</th><th>5 Year [cfs]</th><th>10 Year [cfs]</th><th>25 Year [cfs]</th><th>50 Year [cfs]</th><th>100 Year [cfs]</th><th>500 Year [cfs]</th></th<>	Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00 <th< th=""><th>E 00 min</th><th>0:00:00</th><th>0.00</th><th>0.00</th><th>0.00</th><th>0.00</th><th>0.00</th><th>0.00</th><th>0.00</th><th>0.00</th><th>0.00</th></th<>	E 00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.100         0.02         0.02         0.02         0.02         0.02         0.02         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01 <t< td=""><th>5.00 mm</th><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></t<>	5.00 mm										
0.1500         0.00         0.02         0.04         0.04         0.051         0.49         0.75           0.2500         0.00         0.00         4.18         0.51         1.55         1.31         1.40         1.77           0.2500         0.00         0.00         4.18         0.54         3.71         5.11         5.92         9.36           0.3500         0.00         0.00         7.44         1155         14.64         2.766         4.219         55.01         10.71           0.400         0.00         0.00         5.12         7.71         1.827         3.127         4.517         46.03         10.71           0.400         0.00         0.00         5.15         7.77         9.69         2.463         14.57         8.18           0.400         0.00         0.00         4.37         A.53         8.56         10.00         4.437         A.51         8.56         10.20         2.21         14.141           1.100         0.00         0.00         2.241         4.237         7.70         17.00         12.24         4.21         11.11         11.11         11.11         12.11         12.11         12.11         12.11         1											
0.2000         0.000         116         156         156         148         147           0.2000         0.000         0.000         6.00         16.01         16.41         15.41         15.41         15.41         15.41         15.41         15.41         15.41         15.41         15.41         15.41         15.42         41.23         31.42         41.25         45.41         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01											
0.2500         0.00         0.00         4.11         6.91         9.26         3.11         5.91         5.92         9.26           0.5500         0.00         0.00         7.44         1156         11418         1144         256         7.56         10.24           0.4500         0.00         0.00         7.24         1122         3122         47.55         67.64         100.41           0.500         0.00         0.00         5.18         7.77         9.97         24.83         9.57         9.56           0.500         0.00         0.00         5.17         7.77         9.97         24.83         9.57         9.56         9.64           1.100         0.00         0.00         3.97         5.97         7.76         17.92         2.53         3.64         6.31           1.150         0.00         0.00         3.97         5.97         7.76         17.72         1.97         3.80         6.31           1.150         0.00         0.00         2.44         3.44         1.137         1.130         3.247         5.27           1.500         0.00         2.46         3.44         4.27         1.137         1.247         <											
0.300         0.00         0.400         10.97         11.18         16.41         25.86         23.91         95.41           0.400         0.00         0.00         7.02         10.22         13.82         31.62         47.50         47.44         10.84           0.400         0.00         0.00         5.44         8.44         11.06         27.2         41.09         46.03         0.97           0.500         0.00         0.00         5.47         8.44         11.06         27.2         41.09         46.03         0.97           1.550         0.00         0.00         4.72         7.67         9.02         2.260         3.25         4.82         81.73           1.150         0.00         0.00         1.39         5.37         7.76         17.92         2.33         4.41         17.93         2.637         7.84         63.14           1.150         0.00         0.00         2.244         4.27         7.158         2.325         5.84         60.14           1.1300         0.00         0.00         2.244         4.67         11.21         11.11         7.17         2.201         1.318         2.47         11.11         11.11         <											
0.3500         0.00         7.44         115.6         11.94         27.96         42.19         193.0         162.4           0.4500         0.00         0.00         6.22         9.59         12.34         30.20         45.17         66.30         107.12           0.5500         0.00         0.00         5.54         8.44         11.06         20.27         41.09         40.37         9994           0.5500         0.00         0.00         5.15         7.77         9.02         24.81         38.76         54.23         9064           10.00         0.00         0.00         4.37         4.51         8.35         19.92         20.31         4.81         7.44           11.000         0.00         0.00         3.59         5.39         7.70         17.92         2.37         9.94         4.91           12.000         0.00         0.00         2.32         3.47         4.47         10.10         2.09         2.37           13.000         0.00         0.00         2.24         3.34         4.42         2.24         1.37         1.32         2.07           13.000         0.00         0.00         2.24         3.34         4.45<											
04000         0.00         0.00         10.27         13.80         31.62         17.56         10.00         10.01         10.00         10.01         10.00         10.01         10.00         10.01         10.00         10.01         10.00         10.01         10.00         10.01         10.00         10.01         10.00         10.01         10.00         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         10.01         1											
0.4500         0.00         0.59         8.54         11368         27.72         41307         0.66.01         107.12           0.5500         0.00         0.00         5.55         7.77         9.99         24.85         36.70         54.27         90.44           10500         0.00         0.00         4.32         7.651         8.35         11.97         29.41         44.81         7.64           11000         0.00         0.00         3.39         5.77         7.78         11.97         29.34         46.81           11500         0.00         0.00         3.39         5.79         7.20         15.99         30.41         52.37           12700         0.00         0.00         2.24         5.86         12.14         17.17         12.83         4.71           13700         0.00         0.00         2.24         3.84         4.27         13.11         13.31         4.38         2.11         17.17         12.43         17.11         12.43         17.11         12.43         17.11         12.43         17.11         12.43         12.11         13.11         13.33         2.007         13.35         10.37         11.44         1.47         17.11 <th></th>											
0.500         0.00         0.00         5.49         8.64         11.00         21.72         41.09         46.37         69.06           10.000         0.00         0.00         4.72         7.07         9.89         22.00         32.55         48.37         81.73           11.000         0.00         0.00         4.72         6.51         81.35         11.99         7.24         44.38         7.64           11.000         0.00         0.00         3.99         5.97         7.76         11.99         7.24         44.37         46.34           12.000         0.00         0.00         3.20         4.77         6.47         1.100         2.017         12.84         47.71           13.000         0.00         0.00         2.24         4.27         5.47         10.114         17.71         12.02         4.497         10.77         15.13         12.91         17.14         2.20         1.471         10.77         15.13         2.24         1.471         10.77         15.13         2.24         1.471         10.77         15.13         2.24         1.471         10.77         15.13         2.24         1.471         10.77         15.13         2.24         1.14											
10000         0001         470         470         600         72.90         72.95         44.87         61.77           11000         000         000         399         597         77.9         1772         28.37         44.18         77.46           11000         000         000         399         5.99         72.00         15.98         32.52         35.64         66.31           12000         0.00         0.00         284         422         5.67         17.14         17.17         26.33         44.37           13000         0.00         0.00         284         442         5.84         13.02         13.94         23.92           14000         0.00         2.00         2.46         3.44         4.47         17.10         22.82         3.44         3.24         13.27         15.33         2.82.25         13.93         13.99         2.00         13.99         2.00         13.99         2.00         13.99         2.20         13.99         2.21         13.99         2.21         13.99         2.21         13.99         2.21         13.99         2.21         13.99         2.21         13.99         2.21         13.99         2.21         13.99		0:50:00	0.00	0.00		8.64		27.72			99.94
108:00         0.00         437         651         635         1932         2934         44:00         75:0           11500         0.00         0.00         379         579         77.0         15:90         2637         19:64         6611           11500         0.00         0.00         220         477         6.47         14:31         25:05         10:37         5:39           12500         0.00         0.00         2.46         3.47         6.47         11:1         17:17         24:63         44:17           12500         0.00         0.00         2.46         3.44         4.42         6.24         11:37         17:10         224:1           14500         0.00         0.00         2.46         3.44         4.42         6.24         11:37         17:10         224:1           14500         0.00         0.00         1.18         12:44         12:4         13:47         16:33         26:00         13:49         26:00         12:47         14:64         3:04         4:147         7:16         23:33         2:00         14:47         14:41         2:3:00         14:47         14:41         2:3:00         14:491         2:4:41         1		0:55:00	0.00	0.00	5.15	7.77	9.89	24.83	36.70	54.25	90.66
11000         000         1390         597         778         1792         28.37         296.1         6613           12000         0.00         100         120         4.77         6.61         1613         2057         30.47         5232         35.44         6433           12900         0.00         0.00         2.84         4.22         5.61         1214         1717         2.663         4471           1.2000         0.00         0.00         2.24         3.84         4.42         8.44         1187         1160         4264         144         4.77         4.12         1187         1160         4264         144         4.77         4.12         1187         1162         4214           1.4500         0.00         0.00         1.22         3.34         4.66         8.58         11211         2030           1.5500         0.00         0.00         1.67         2.33         3.07         5.38         7.56         15.71         7.64         12.23           1.500         0.00         0.00         1.17         1.42         2.12         3.76         12.23         12.33         12.23         12.35         12.64         1.87         1		1:00:00	0.00	0.00	4.72	7.07	9.02	22.09	32.55	48.57	81.78
11500         0.00         309         5.39         7.20         15.80         23.52         35.44         60.34           125.00         0.00         0.00         284         4.22         5.67         12.14         17.71         20.03         44.71           135.00         0.00         0.00         2.81         3.84         4.27         9.12         13.21         1.18         11.14         3.29           145.00         0.00         0.00         2.12         3.38         4.42         8.24         1.18         1.11         3.20           145.00         0.00         0.00         2.18         3.11         4.48         7.47         10.12         15.33         6.40           15.00         0.00         0.00         1.06         2.26         3.16         6.14         9.61         12.01         2.23           200.00         0.00         0.00         1.16         2.26         3.26         12.21         3.74         5.26         7.35         12.23           21000         0.00         0.00         1.12         1.24         3.04         4.21         7.61           21000         0.00         0.01         1.12         1.24		1:05:00	0.00	0.00	4.37	6.51	8.35	19.92	29.34	44.18	75.49
1.2000         0.00         2.20         2.24         4.77         1.401         20.29         3.47         52.39           1.2500         0.00         0.00         2.24         3.87         5.16         10.38         15.22         2.108         3.77           1.2500         0.00         0.00         2.24         3.84         4.47         10.23         11.11         11.10         2.24           1.4000         0.00         0.00         2.18         3.11         4.08         7.47         10.72         11.30         2.462           1.5000         0.00         0.00         1.66         2.59         3.43         6.65         8.58         1.71         10.72         11.10         2.462           1.5000         0.00         0.00         1.42         2.59         3.43         6.65         8.58         1.71         1.64         3.00         1.72         1.75         1.65         1.057         1.74         1.41           2.1500         0.00         0.00         1.177         1.42         1.52         2.24         3.75         1.72         3.74         5.58         7.35         1.72         2.500         3.00         0.00         1.73         1.24 <th></th> <td>1:10:00</td> <td>0.00</td> <td>0.00</td> <td>3.99</td> <td>5.97</td> <td>7.76</td> <td>17.92</td> <td>26.37</td> <td>39.63</td> <td>68.11</td>		1:10:00	0.00	0.00	3.99	5.97	7.76	17.92	26.37	39.63	68.11
1.25:00         0.00         0.24         4.22         6.67         12:14         17.17         2.03         44.11           1.55:00         0.00         0.00         2.46         3.84         4.17         9.12         13.21         10.14         3.92           1.40:00         0.00         0.00         2.12         3.38         4.42         11.87         10.12         13.31         2.21           1.40:00         0.00         0.00         2.18         3.11         4.08         7.47         10.72         15.33         2.60           1.50:00         0.00         0.00         1.67         2.33         3.07         5.38         7.56         10.57         17.44           2.05:00         0.00         0.00         1.42         1.78         2.26         4.52         8.64         14.91           2.15:00         0.00         0.00         1.12         1.46         3.00         4.22         5.75         12.23           2.75:00         0.00         0.00         1.42         1.76         3.99         2.24         3.02         4.21         7.01           2.75:00         0.00         0.00         0.43         0.55         0.57         0.54											
1.3200         0.00         0.20         2.41         3.87         1.16         10.26         15.77         1.17           1.4000         0.00         0.00         2.46         3.64         4.77         9.12         13.21         19.14         3.29.21           1.4000         0.00         0.00         2.18         3.11         4.08         7.47         10.72         15.33         2.66.22           1.5000         0.00         0.00         1.06         2.25         3.76         6.74         9.65         1.75         17.74           2.0000         0.00         0.00         1.67         2.33         3.07         5.38         7.56         10.75         17.74           2.0100         0.00         0.00         1.62         2.12         3.97         5.26         7.35         12.22           2.0000         0.00         0.00         1.17         1.66         3.00         4.12         5.76         9.97           2.7500         0.00         0.00         0.31         0.77         0.64         0.70         0.87         1.64         2.86           2.3500         0.00         0.00         0.33         0.34         0.42         0.21											
13500         0.00         0.00         226         338         442         824         1187         17.10         29.24           14500         0.00         0.00         225         2.85         1.76         0.74         10.72         15.33         26.02           1500         0.00         0.00         1.80         2.26         2.85         1.76         6.74         46.3         11.11         2.03           1500         0.00         0.00         1.62         2.33         1.07         5.38         7.66         11.11         2.03           2.00.00         0.00         0.00         1.12         1.36         3.00         4.22         7.35         12.23           2.15.00         0.00         0.00         1.12         1.64         3.00         4.12         5.76         9.39           2.23.00         0.00         0.00         0.71         0.94         1.33         1.99         2.73         4.56           2.85.00         0.00         0.00         0.36         0.76         0.99         1.26         2.86           2.95.00         0.00         0.00         0.35         0.54         0.64         0.77         1.91      <											
14000         000         232         338         4.42         82.4         11.77         17.10         29.4           15000         0.00         0.00         215         3.11         4.08         7.47         10.22         15.33         28.02           15000         0.00         0.00         1.86         2.99         3.43         6.05         8.58         12.11         20.39           15000         0.00         0.00         1.42         1.98         2.60         4.59         6.42         8.66         11.7         17.64           20500         0.00         0.00         1.42         1.98         2.60         4.59         6.42         8.66         14.91           21000         0.00         0.00         0.71         1.42         1.72         1.66         3.00         4.12         5.76         9.59           225000         0.00         0.00         0.34         0.71         0.44         1.33         1.99         2.73         4.56           23500         0.00         0.00         0.30         0.39         0.42         0.51         0.51         0.51         0.51         0.51         0.51         0.51         0.51         0.51 </td <th></th> <td></td>											
14500         0.00         2.18         3.11         4.08         7.47         10.72         15.33         26.07           15000         0.00         0.00         1.86         2.59         3.43         6.07         9.43         15.01         10.02         11.02         3.33           200.00         0.00         0.00         1.47         2.33         1.07         5.38         7.54         10.57         17.44           205.00         0.00         0.00         1.47         1.82         2.12         3.79         5.26         7.35         12.37           215.00         0.00         0.00         0.01         0.71         1.66         3.00         4.21         7.01           22000         0.00         0.00         0.34         0.71         0.46         1.75         1.92         2.73         4.55           23000         0.00         0.00         0.34         0.71         0.44         0.53         0.54         0.66         1.07         1.33           245.00         0.00         0.00         0.22         0.33         0.44         0.42         0.51         0.57         0.44           250.00         0.00         0.00											
15000         0.00         0.00         186         259         3.6         6.74         9.63         13.97         23.07           15500         0.00         0.00         1.86         2.59         3.43         6.05         8.88         12.11         20.33           200.00         0.00         0.00         1.42         1.98         2.60         4.59         6.42         8.96         14.21           210.00         0.00         0.00         0.93         1.27         1.66         3.00         4.12         5.76         9.59           230.00         0.00         0.00         0.71         0.96         1.53         1.99         2.73         4.56           230.00         0.00         0.00         0.43         0.56         0.76         0.44         0.51         1.99         2.73         4.56           230.00         0.00         0.00         0.25         0.33         0.44         0.44         0.44         0.44         0.41         0.44         0.51         0.57         0.44           250.00         0.00         0.00         0.25         0.33         0.44         0.42         0.51         0.57         0.44           250.00<											
15500         0.00         1.00         1.67         2.33         3.47         6.05         8.58         1.211         20.33           20500         0.00         0.00         1.47         2.33         3.07         5.38         7.56         10.57         17.64           20500         0.00         0.00         1.42         1.46         2.40         4.59         6.42         8.96         14.91           21500         0.00         0.00         0.71         1.66         3.00         4.12         5.76         9.59           22000         0.00         0.00         0.71         0.66         1.25         2.24         3.02         4.21         7.01           23000         0.00         0.00         0.43         0.56         0.76         0.99         1.26         1.66         2.86           23000         0.00         0.00         0.25         0.33         0.44         0.42         0.51         0.57         0.94           24600         0.00         0.00         0.22         0.29         0.26         0.31         0.30         0.42         0.64           25500         0.00         0.00         0.17         0.22         0.29											
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20500         0.00         0.00         1.42         1.89         2.40         4.59         6.42         8.96         1.147           210.00         0.00         0.00         0.00         1.07         1.66         3.00         4.12         5.76         9.59           22000         0.00         0.00         0.71         0.96         1.25         2.24         3.02         4.21         7.01           2.25.00         0.00         0.00         0.43         0.55         0.76         0.99         1.26         1.66         2.86           2.35.00         0.00         0.00         0.36         0.47         0.64         0.70         0.87         1.99         1.92           2.40.00         0.00         0.00         0.36         0.47         0.64         0.70         0.87         1.33           2.45.00         0.00         0.00         0.22         0.33         0.34         0.42         0.57         0.44           2.50.00         0.00         0.00         0.17         0.22         0.29         0.26         0.31         0.30         0.45           3.05.00         0.00         0.00         0.17         0.12         0.11											
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2:15:00         0.00         0.00         0.71         0.96         1.25         2.24         3.02         4.21         7.01           2:20:00         0.00         0.00         0.54         0.71         0.96         1.53         1.99         2.73         4.85           2:30:00         0.00         0.00         0.54         0.74         0.94         1.66         2.86           2:30:00         0.00         0.30         0.37         0.54         0.76         0.97         1.19         1.92           2:40:00         0.00         0.30         0.33         0.54         0.66         0.77         1.33           2:45:00         0.00         0.00         0.25         0.33         0.44         0.42         0.66           2:50:00         0.00         0.00         0.27         0.36         0.33         0.39         0.42         0.62           2:50:00         0.00         0.00         0.17         0.22         0.29         0.26         0.31         0.30         0.44           2:50:00         0.00         0.00         0.17         0.22         0.30         0.41         0.18         0.14         0.18         0.31         0.31											
2.20:00         0.00         0.01         0.96         1.25         2.24         3.02         4.21         7.01           2.25:00         0.00         0.00         0.54         0.71         0.94         1.53         1.99         2.73         4.56           2.35:00         0.00         0.00         0.34         0.55         0.76         0.99         1.26         1.66         2.85           2.35:00         0.00         0.00         0.33         0.44         0.42         0.51         0.57         0.94           2.46:00         0.00         0.00         0.25         0.33         0.44         0.42         0.51         0.57         0.94           2.50:00         0.00         0.00         0.27         0.36         0.33         0.30         0.42         0.66           3.00:00         0.00         0.14         0.18         0.24         0.21         0.24         0.21         0.24         0.22         0.33           3.00:00         0.00         0.01         0.05         0.07         0.09         0.11         0.14         0.18           3.00:00         0.00         0.01         0.01         0.11         0.14         0.18		2:15:00									
23000         0.00         0.43         0.56         0.76         0.99         1.26         1.66         2.86           2.35.00         0.00         0.00         0.30         0.39         0.53         0.54         0.66         0.77         1.33           2.45.00         0.00         0.00         0.25         0.33         0.44         0.42         0.51         0.57         0.94           2.95.00         0.00         0.00         0.20         0.27         0.36         0.33         0.33         0.42         0.66         0.57         0.94           3.00.00         0.00         0.00         0.17         0.22         0.29         0.26         0.31         0.30         0.45           3.00.00         0.00         0.011         0.15         0.14         0.17         0.92         0.24         0.21         0.24         0.22         0.31         0.30         0.45           3.00.00         0.00         0.00         0.07         0.09         0.11         0.17         0.19         0.17         0.14         0.14         0.18           3.15.00         0.00         0.00         0.02         0.03         0.04         0.05         0.05         <		2:20:00		0.00							
$\begin{array}{c c c c c c c c c c c c c c c c c c c $		2:25:00	0.00	0.00	0.54	0.71	0.94	1.53	1.99	2.73	4.56
2:40:00         0:00         0:30         0:33         0:53         0:54         0.66         0.77         1.33           2:45:00         0:00         0:00         0:25         0:33         0:44         0:42         0:51         0:57         0:94           2:50:00         0:00         0:00         0:20         0:27         0:36         0:33         0:39         0:42         0:66           2:50:00         0:00         0:00         0:17         0:22         0:24         0:21         0:24         0:22         0:30           3:00:00         0:00         0:00         0:11         0:15         0:14         0:17         0:19         0:17         0:22           3:10:00         0:00         0:00         0:07         0:09         0:02         0:11         0:12         0:11         0:14         0:18           3:20:00         0:00         0:00         0:06         0:07         0:06         0:07         0:07         0:06         0:07         0:06         0:07         0:07         0:08         0:03         0:03         0:03         0:03         0:03         0:03         0:03         0:03         0:03         0:03         0:03         0:04		2:30:00	0.00	0.00	0.43	0.56	0.76	0.99	1.26	1.66	2.86
2:45:00         0.00         0.25         0.33         0.44         0.42         0.51         0.57         0.94           2:50:00         0.00         0.00         0.20         0.27         0.36         0.33         0.39         0.42         0.86           3:00:00         0.00         0.00         0.11         0.18         0.24         0.21         0.24         0.22         0.30           3:05:00         0.00         0.00         0.01         0.11         0.15         0.14         0.17         0.19         0.17         0.12         0.11         0.15         0.14         0.16         0.14         0.18         0.33         0.09         0.09         0.12         0.11         0.12         0.11         0.14         0.14         0.14         0.14         0.14         0.13         0.14         0.14         0.14         0.14         0.13         0.22         0.02         0.02         0.03         0.03         0.03         0.04         0.05         0.05         0.05         0.05         0.06         0.04         0.33         0.40         0.33         0.40         0.33         0.40         0.33         0.40         0.33         0.44         0.42         0.42		2:35:00	0.00	0.00	0.36	0.47	0.64	0.70	0.87	1.09	1.92
2:50:00         0.00         0.20         0.27         0.36         0.33         0.39         0.42         0.66           2:55:00         0.00         0.00         0.17         0.22         0.26         0.31         0.30         0.45           3:00:00         0.00         0.00         0.11         0.15         0.19         0.17         0.19         0.17         0.22         0.30           3:00:00         0.00         0.00         0.09         0.12         0.15         0.14         0.15         0.14         0.15         0.14         0.18         0.22           3:10:00         0.00         0.00         0.07         0.09         0.12         0.11         0.12         0.11         0.12         0.11         0.12         0.11         0.12         0.11         0.12         0.11         0.12         0.11         0.12         0.11         0.12         0.11         0.12         0.11         0.12         0.11         0.12         0.11         0.12         0.11         0.12         0.11         0.11         0.11         0.11         0.11         0.11         0.11         0.11         0.11         0.11         0.11         0.11         0.11         0.11			0.00	0.00	0.30	0.39	0.53	0.54	0.66	0.77	1.33
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$								0.42	0.51		0.94
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3:25:00         0.00         0.04         0.05         0.07         0.06         0.07         0.07         0.08           3:30:00         0.00         0.00         0.03         0.04         0.05         0.05         0.05         0.05         0.06           3:35:00         0.00         0.00         0.02         0.03         0.02         0.02         0.02         0.02         0.02         0.02         0.02         0.02         0.02         0.02         0.02         0.02         0.02         0.03         0.04         0.03         0.04           3:45:00         0.00         0.00         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00											
3:30:00         0.00         0.00         0.03         0.04         0.05         0.05         0.05         0.06           3:35:00         0.00         0.00         0.02         0.03         0.03         0.04         0.03         0.04           3:40:00         0.00         0.00         0.01         0.02         0.02         0.02         0.02         0.03           3:45:00         0.00         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00											
3:40:00         0.00         0.01         0.02         0.02         0.02         0.02         0.02         0.03           3:45:00         0.00         0.00         0.00         0.00         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.01         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00		3:30:00									
3:45:00         0:00         0:00         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01         0:01		3:35:00	0.00	0.00	0.02	0.03	0.03	0.03	0.04	0.03	0.04
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3:55:00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00			0.00	0.00	0.01	0.01	0.01	0.01	0.01	0.01	0.01
4:00:00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00           4:05:00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00											0.01
4:05:00         0.00         0.00         0.00         0.00         0.00         0.00         0.00           4:10:00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00           4:10:00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00           4:15:00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00           4:20:00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00           4:35:00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00           4:40:00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00           4:45:00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00           4:45:00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00           5:00:00         0.00         0.00											
4:10:00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00											
4:15:00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00											
4:20:00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00											
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5:10:00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00											
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5:25:00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00											
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5:35:00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00											
5:45:00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00											
5:50:00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00           5:55:00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00											
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ZONE 1 AND 2 ORIFICES Example Zone Configuration (Retention Pond)

-100-YEAR ORIFICE

Depth Increment = 0.25

ft

Watershed	Information

PERMA

atershed Information		
Selected BMP Type =	EDB	
Watershed Area =	72.00	acres
Watershed Length =	3,160	ft
Watershed Length to Centroid =	1,500	ft
Watershed Slope =	0.040	ft/ft
Watershed Imperviousness =	14.50%	percent
Percentage Hydrologic Soil Group A =	100.0%	percent
Percentage Hydrologic Soil Group B =	0.0%	percent
Percentage Hydrologic Soil Groups C/D =	0.0%	percent
Target WQCV Drain Time =	40.0	hours
Location for 1-hr Rainfall Depths =	User Input	

## After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

the embedded colorado orban nyard	graphinoceue	10.
Water Quality Capture Volume (WQCV) =	0.545	acre-feet
Excess Urban Runoff Volume (EURV) =	0.851	acre-feet
2-yr Runoff Volume (P1 = 1.19 in.) =	0.490	acre-feet
5-yr Runoff Volume (P1 = 1.5 in.) =	0.748	acre-feet
10-yr Runoff Volume (P1 = 1.75 in.) =	0.979	acre-feet
25-yr Runoff Volume (P1 = 2 in.) =	2.024	acre-feet
50-yr Runoff Volume (P1 = 2.25 in.) =	3.038	acre-feet
100-yr Runoff Volume (P1 = 2.52 in.) =	4.442	acre-feet
500-yr Runoff Volume (P1 = 3.14 in.) =	7.526	acre-feet
Approximate 2-yr Detention Volume =	0.518	acre-feet
Approximate 5-yr Detention Volume =	0.705	acre-feet
Approximate 10-yr Detention Volume =	0.911	acre-feet
Approximate 25-yr Detention Volume =	1.205	acre-feet
Approximate 50-yr Detention Volume =	1.517	acre-feet
Approximate 100-yr Detention Volume =	2.199	acre-feet

Define	Zones and Basin Geomet	ry
	Zone 1 Volume (	w
	Zone 2 Volume (EURV - 2	201

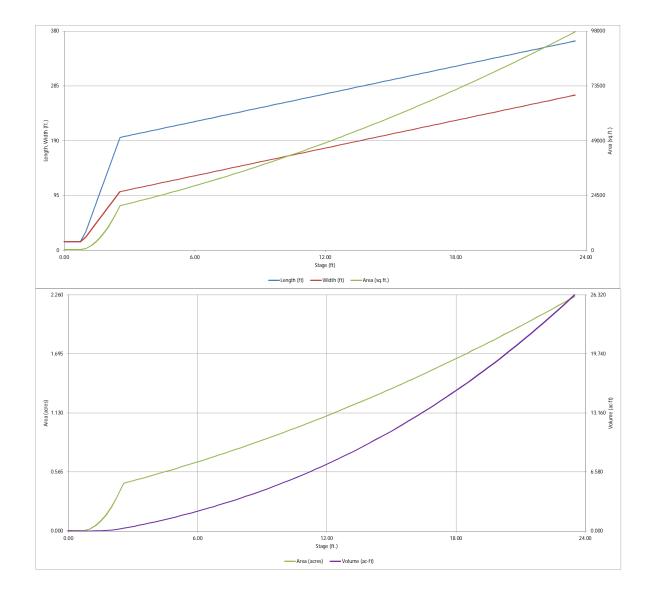
Zone 1 Volume (WQCV) =	0.545	acre-feet
Zone 2 Volume (EURV - Zone 1) =	0.306	acre-feet
Zone 3 Volume (100-year - Zones 1 & 2) =	1.348	acre-feet
Total Detention Basin Volume =	2.199	acre-feet
Initial Surcharge Volume (ISV) =	71	ft <sup>3</sup>
Initial Surcharge Depth (ISD) =	0.33	ft
Total Available Detention Depth (H <sub>total</sub> ) =	6.00	ft
Depth of Trickle Channel $(H_{TC}) =$	0.50	ft
Slope of Trickle Channel (S <sub>TC</sub> ) =	0.010	ft/ft
Slopes of Main Basin Sides (S <sub>main</sub> ) =	4	H:V
Basin Length-to-Width Ratio $(R_{L/W}) =$	2	

Initial Surcharge Area (A <sub>ISV</sub> ) =	216	ft <sup>2</sup>
Surcharge Volume Length ( $L_{ISV}$ ) =	14.7	ft
Surcharge Volume Width (WISV) =	14.7	ft
Depth of Basin Floor $(H_{FLOOR}) =$	1.74	ft
Length of Basin Floor $(L_{FLOOR}) =$	195.7	ft
Width of Basin Floor ( $W_{FLOOR}$ ) =	101.7	ft
Area of Basin Floor $(A_{FLOOR}) =$		ft <sup>2</sup>
Volume of Basin Floor ( $V_{FLOOR}$ ) =	12,867	ft <sup>3</sup>
Depth of Main Basin $(H_{MAIN}) =$	3.43	ft
Length of Main Basin $(L_{MAIN}) =$	223.1	ft
Width of Main Basin ( $W_{MAIN}$ ) =	129.1	ft
Area of Main Basin (A <sub>MAIN</sub> ) =		ft <sup>2</sup>
Volume of Main Basin (V <sub>MAIN</sub> ) =	83,059	ft <sup>3</sup>

Calculated Total Basin Volume (V<sub>total</sub>) = 2.206 acre-feet

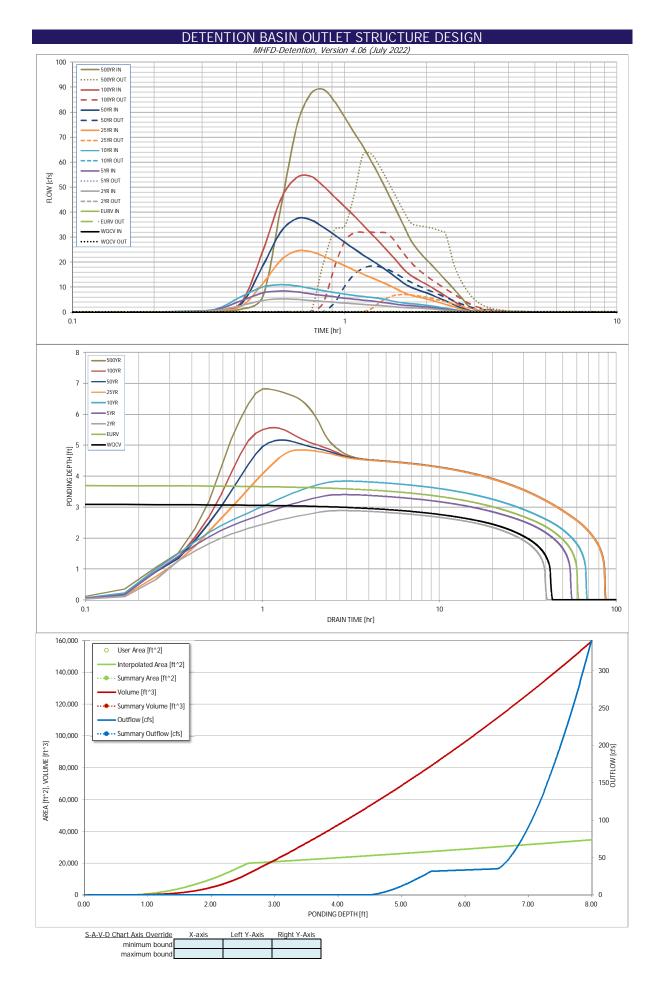
E	Depth Increment =	0.25	ft				Optional			
tion Dand)	Stage - Storage	Stage	Optional Override	Length	Width	Area	Override	Area	Volume	Volume
ntion Pond)	Description	(ft)	Stage (ft)	(ft)	(ft)	(ft 2)	Area (ft 2)	(acre)	(ft 3)	(ac-ft)
			Suga (II)	14.7	14.7				10 /	(00-11)
	Top of Micropool	0.00				216		0.005		
	ISV	0.33		14.7	14.7	216		0.005	71	0.002
		0.50		14.7	14.7	216		0.005	108	0.002
	<b>├</b> ────	0.75		14.7	14.7	216		0.005	162	0.004
		1.00		32.4	23.2	751		0.017	257	0.006
		1.25		58.4	35.7	2,083		0.048	598	0.014
		1.50		84.4	48.2	4,066		0.093	1,353	0.031
		1.75		110.4	60.7	6,699		0.154	2,685	0.062
		2.00		136.4	73.2	9,981		0.229	4,757	0.109
		2.25		162.4	85.7	13,914		0.319	7,730	0.177
		2.50		188.4	98.2	18,497		0.425	11,768	0.270
	Ele e e	2.50		195.7						0.301
	Floor				101.7	19,896		0.457	13,111	
		2.75		197.1	103.1	20,327		0.467	16,731	0.384
		3.00		199.1	105.1	20,931		0.481	21,888	0.502
Optional User Overrides	Zone 1 (WQCV)	3.09		199.8	105.9	21,151		0.486	23,782	0.546
acre-feet		3.25		201.1	107.1	21,544		0.495	27,197	0.624
acre-feet		3.50		203.1	109.1	22,164		0.509	32,661	0.750
1.19 inches	Zone 2 (EURV)	3.70		204.7	110.7	22,666		0.520	37,144	0.853
1.50 inches		3.75		205.1	111.1	22,792		0.523	38,280	0.879
1.75 inches		4.00		207.1	113.1	23,429		0.538	44,058	1.011
2.00 inches		4.25		209.1	115.1	24,073		0.553	49,995	1.148
2.25 inches		4.50		211.1	117.1	24,726		0.568	56,095	1.288
2.52 inches		4.75		213.1	119.1	25,386		0.583	62,359	1.432
inches		5.00		215.1	121.1	26,055		0.598	68,789	1.579
110103	<u>├</u>	5.25								
				217.1	123.1	26,731		0.614	75,387	1.731
		5.50		219.1	125.1	27,416		0.629	82,155	1.886
		5.75		221.1	127.1	28,108		0.645	89,095	2.045
	Zone 3 (100-year)	5.99		223.0	129.1	28,780		0.661	95,922	2.202
						28,809				
	<b>├</b> ──── <b>┤</b>	6.00		223.1	129.1			0.661	96,210	2.209
		6.25		225.1	131.1	29,517		0.678	103,500	2.376
		6.50		227.1	133.1	30,233		0.694	110,969	2.547
		6.75		229.1	135.1	30,958		0.711	118,618	2.723
										2.903
		7.00		231.1	137.1	31,690		0.728	126,448	
		7.25		233.1	139.1	32,431		0.745	134,463	3.087
		7.50		235.1	141.1	33,179		0.762	142,664	3.275
		7.75		237.1	143.1	33,936		0.779	151,054	3.468
		8.00		239.1	145.1	34,700		0.797	159,633	3.665
		0.00		237.1	145.1	34,700		0.777	137,033	3.005
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MHFD-Detention, Version 4.06 (July 2022)



### DETENTION BASIN OUTLET STRUCTURE DESIGN MHFD-Detention, Version 4.06 (July 2022)

			IHFD-Detention, V		2022)				
Project: Basin I D:	Esteban Rodrigue	z Subdivision-PDR							
ZONE 3	1 ond 0			Estimated	Estimated				
				Stage (ft)	Volume (ac-ft)	Outlet Type			
100-YR VOLUME EURY WOCY	1		Zone 1 (WQCV)	3.09	0.545	Orifice Plate	1		
	100-YEAR		Zone 2 (EURV)	3.70	0.306	Orifice Plate			
PERMANENT ORIFICES	ORIFICE		Zone 3 (100-year)	5.99	1.348	Weir&Pipe (Restrict)			
r Ennietteri	Configuration (Re	tention Pond)	Zone 3 (100-year)	Total (all zones)	2.199	weiraripe (Restrict)	J		
User Input: Orifice at Underdrain Outlet (typical	ly used to drain WO	ICV in a Filtration B	MP)	Total (all zones)	2.177	1	Calculated Parame	ters for Underdrain	
Underdrain Orifice Invert Depth =	N/A		the filtration media	surface)	Underg	drain Orifice Area =	N/A	ft <sup>2</sup>	
Underdrain Orifice Diameter =	N/A	inches				n Orifice Centroid =	N/A	feet	
								1	
User Input: Orifice Plate with one or more orifi	ces or Elliptical Slot	Weir (typically used	I to drain WQCV an	d/or EURV in a sedi	mentation BMP)		Calculated Parame	ters for Plate	
Centroid of Lowest Orifice =	0.00	ft (relative to basir	n bottom at Stage =	= 0 ft)	WQ Orifi	ice Area per Row =	N/A	ft <sup>2</sup>	
Depth at top of Zone using Orifice Plate =	4.39	· · ·	n bottom at Stage =	= 0 ft)		iptical Half-Width =	N/A	feet	
Orifice Plate: Orifice Vertical Spacing =	N/A	inches				ical Slot Centroid =	N/A	feet	
Orifice Plate: Orifice Area per Row =	N/A	sq. inches			E	Elliptical Slot Area =	N/A	ft <sup>2</sup>	
Licor Inputs Store and Total Area of Each Orific	o Dow (pumborod f	rom lowest to high	oct)						
User Input: Stage and Total Area of Each Orific	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)	l
Stage of Orifice Centroid (ft)		2.00	3.25	3.75	(optional)	o (optional)	(optional)	(optional)	
Orifice Area (sq. inches)		1.10	0.30	0.30					
	2.00		0.00	0.00					1
	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)	
Stage of Orifice Centroid (ft)								(1)	
Orifice Area (sq. inches)									
User Input: Vertical Orifice (Circular or Rectang	ular)		-				Calculated Parame	ters for Vertical Ori	fice
	Not Selected	Not Selected					Not Selected	Not Selected	
Invert of Vertical Orifice =	N/A	N/A	ft (relative to basin	n bottom at Stage =	= 0 ft) Ver	rtical Orifice Area =	N/A	N/A	ft <sup>2</sup>
Depth at top of Zone using Vertical Orifice =	N/A	N/A	ft (relative to basin	n bottom at Stage =	= 0 ft) Vertica	I Orifice Centroid =	N/A	N/A	feet
Vertical Orifice Diameter =	N/A	N/A	inches						
User Input: Overflow Weir (Dropbox with Flat of			ctangular/Trapezoid	al Weir and No Out	tlet Pipe)		Calculated Parame	ters for Overflow W	/eir
	Zone 3 Weir	Not Selected					Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	4.50	N/A		bottom at Stage = 0	ft) Height of Grat		4.50	N/A	feet
Overflow Weir Front Edge Length =	4.50 5.00	N/A N/A	feet		ft) Height of Grati Overflow W	/eir Slope Length =	4.50 5.00	N/A N/A	feet feet
Overflow Weir Front Edge Length = Overflow Weir Grate Slope =	4.50 5.00 0.00	N/A N/A N/A	feet H:V	Gr	ft) Height of Grat Overflow W ate Open Area / 10	/eir Slope Length = 00-yr Orifice Area =	4.50 5.00 6.56	N/A N/A N/A	feet
Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides =	4.50 5.00 0.00 5.00	N/A N/A N/A N/A	feet	Gr	ft) Height of Grat Overflow W ate Open Area / 10 verflow Grate Open	/eir Slope Length = 00-yr Orifice Area = Area w/o Debris =	4.50 5.00 6.56 19.78	N/A N/A N/A N/A	feet ft <sup>2</sup>
Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type =	4.50 5.00 0.00 5.00 Close Mesh Grate	N/A N/A N/A N/A N/A	feet H:V feet	Gr	ft) Height of Grat Overflow W ate Open Area / 10	/eir Slope Length = 00-yr Orifice Area = Area w/o Debris =	4.50 5.00 6.56	N/A N/A N/A	feet
Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides =	4.50 5.00 0.00 5.00	N/A N/A N/A N/A	feet H:V	Gr	ft) Height of Grat Overflow W ate Open Area / 10 verflow Grate Open	/eir Slope Length = 00-yr Orifice Area = Area w/o Debris =	4.50 5.00 6.56 19.78	N/A N/A N/A N/A	feet ft <sup>2</sup>
Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % =	4.50 5.00 0.00 5.00 Close Mesh Grate 50%	N/A N/A N/A N/A N/A N/A	feet H:V feet %	Gr	ft) Height of Grat Overflow W ate Open Area / 10 verflow Grate Open Overflow Grate Ope	/eir Slope Length = )0-yr Orifice Area = Area w/o Debris = n Area w/ Debris =	4.50 5.00 6.56 19.78 9.89	N/A N/A N/A N/A N/A	feet ft <sup>2</sup> ft <sup>2</sup>
Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type =	4.50 5.00 0.00 5.00 Close Mesh Grate 50%	N/A N/A N/A N/A N/A N/A estrictor Plate, or R	feet H:V feet %	Gr	ft) Height of Grat Overflow W ate Open Area / 10 verflow Grate Open Overflow Grate Ope	/eir Slope Length = )0-yr Orifice Area = Area w/o Debris = n Area w/ Debris =	4.50 5.00 6.56 19.78 9.89 s for Outlet Pipe w/	N/A N/A N/A N/A N/A	feet ft <sup>2</sup> ft <sup>2</sup>
Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = <u>User Input: Outlet Pipe w/ Flow Restriction Plate</u>	4.50 5.00 0.00 5.00 Close Mesh Grate 50% e (Circular Orifice, R Zone 3 Restrictor	N/A N/A N/A N/A N/A estrictor Plate, or R Not Selected	feet H:V feet % <u>ectangular Orifice)</u>	Gr Ov C	ft) Height of Grat Overflow W ate Open Area / 10 verflow Grate Open Overflow Grate Ope <u>Ca</u>	Veir Slope Length = 10-yr Orifice Area = Area w/o Debris = n Area w/ Debris = Iculated Parameter	4.50 5.00 6.56 19.78 9.89 s for Outlet Pipe w/ Zone 3 Restrictor	N/A N/A N/A N/A N/A Flow Restriction Pir Not Selected	feet ft <sup>2</sup> ft <sup>2</sup> <u>ate</u>
Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = <u>User Input: Outlet Pipe w/ Flow Restriction Plate</u> Depth to Invert of Outlet Pipe =	4.50 5.00 0.00 5.00 Close Mesh Grate 50% e (Circular Orlfice, R Zone 3 Restrictor 0.25	N/A N/A N/A N/A N/A N/A estrictor Plate, or R	feet H:V feet % <u>ectangular Orifice)</u>	Gr	ft) Height of Grat Overflow W ate Open Area / 10 verflow Grate Open Overflow Grate Ope <u>Ca</u> = 0 ft) O	/eir Slope Length = )0-yr Orifice Area = Area w/o Debris = n Area w/ Debris =	4.50 5.00 6.56 19.78 9.89 s for Outlet Pipe w/	N/A N/A N/A N/A N/A	feet ft <sup>2</sup> ft <sup>2</sup>
Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = <u>User Input: Outlet Pipe w/ Flow Restriction Plate</u>	4.50 5.00 0.00 5.00 Close Mesh Grate 50% 2 (Circular Orifice. R Zone 3 Restrictor 0.25 24.00	N/A N/A N/A N/A N/A estrictor Plate, or R Not Selected N/A	feet H:V feet % <u>Rectangular Orifice)</u> ft (distance below b	Gr Ov C	ft) Height of Grat Overflow W ate Open Area / 10 verflow Grate Open Overflow Grate Ope <u>Ca</u> = 0 ft) O	Veir Slope Length = 10-yr Orifice Area = Area w/o Debris = n Area w/ Debris = <u>Iculated Parameter</u> utlet Orifice Area = t Orifice Centroid =	4.50 5.00 6.56 19.78 9.89 s for Outlet Pipe w/ Zone 3 Restrictor 3.02	N/A N/A N/A N/A Y Flow Restriction Pla Not Selected N/A	feet ft <sup>2</sup> ft <sup>2</sup> <u>ate</u> ft <sup>2</sup>
Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = <u>User Input: Outlet Pipe w/ Flow Restriction Plate</u> Depth to Invert of Outlet Pipe = Outlet Pipe Diameter =	4.50 5.00 0.00 5.00 Close Mesh Grate 50% 2 (Circular Orifice, R Zone 3 Restrictor 0.25 24.00	N/A N/A N/A N/A N/A estrictor Plate, or R Not Selected N/A	feet H:V feet % <u>Rectangular Orifice)</u> ft (distance below b inches	Gr Ov C	ft) Height of Grat Overflow W ate Open Area / 10 verflow Grate Open Overflow Grate Ope <u>Ca</u> = 0 ft) O Outle	Veir Slope Length = 10-yr Orifice Area = Area w/o Debris = n Area w/ Debris = <u>Iculated Parameter</u> utlet Orifice Area = t Orifice Centroid =	4.50 5.00 6.56 19.78 9.89 s for Outlet Pipe w/ Zone 3 Restrictor 3.02 0.96	N/A N/A N/A N/A N/A Flow Restriction Pla Not Selected N/A N/A	feet ft <sup>2</sup> ft <sup>2</sup> ate ft <sup>2</sup> feet
Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = <u>User Input: Outlet Pipe w/ Flow Restriction Plate</u> Depth to Invert of Outlet Pipe = Outlet Pipe Diameter =	4.50 5.00 0.00 5.00 Close Mesh Grate 50% e (Circular Orifice, R Zone 3 Restrictor 0.25 24.00 22.00	N/A N/A N/A N/A N/A estrictor Plate, or R Not Selected N/A	feet H:V feet % <u>Rectangular Orifice)</u> ft (distance below b inches	Gr Ov C	ft) Height of Grat Overflow W ate Open Area / 10 verflow Grate Open Overflow Grate Ope <u>Ca</u> = 0 ft) O Outle	Veir Slope Length = 10-yr Orifice Area = Area w/o Debris = n Area w/ Debris = <u>Iculated Parameter</u> utlet Orifice Area = t Orifice Centroid =	4.50 5.00 6.56 19.78 9.89 s for Outlet Pipe w/ Zone 3 Restrictor 3.02 0.96	N/A N/A N/A N/A N/A N/A N/A N/A	feet ft <sup>2</sup> ft <sup>2</sup> ate ft <sup>2</sup> feet
Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = <u>User Input: Outlet Pipe w/ Flow Restriction Plate</u> Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert =	4.50 5.00 0.00 5.00 Close Mesh Grate 50% e (Circular Orifice, R Zone 3 Restrictor 0.25 24.00 22.00	N/A N/A N/A N/A N/A estrictor Plate, or R Not Selected N/A N/A	feet H:V feet % <u>Rectangular Orifice)</u> ft (distance below b inches	Gr O\ c asin bottom at Stage Half-Cent	ft) Height of Grat Overflow V ate Open Area / 10 verflow Grate Open Dverflow Grate Open <u>Ca</u> = 0 ft) O Outle tral Angle of Restric	Veir Slope Length = 10-yr Orifice Area = Area w/o Debris = n Area w/ Debris = <u>Iculated Parameter</u> utlet Orifice Area = t Orifice Centroid =	4.50 5.00 6.56 19.78 9.89 s for Outlet Pipe w/ Zone 3 Restrictor 3.02 0.96 2.56	N/A N/A N/A N/A N/A N/A N/A N/A	feet ft <sup>2</sup> ft <sup>2</sup> ate ft <sup>2</sup> feet
Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or	4.50 5.00 0.00 5.00 Close Mesh Grate 50% e (Circular Orifice, R Zone 3 Restrictor 0.25 24.00 22.00 Trapezoidal)	N/A N/A N/A N/A N/A estrictor Plate, or R Not Selected N/A N/A	feet H:V feet % tectangular Orifice) ft (distance below b inches inches	Gr O\ c asin bottom at Stage Half-Cent	ft) Height of Grat Overflow V ate Open Area / 10 verflow Grate Open Iverflow Grate Open Dverflow Grate Ope <u>Ca</u> = 0 ft) O Outle tral Angle of Restrict Spillway D	Veir Slope Length = 20-yr Orifice Area = Area w/o Debris = n Area w/ Debris = <u>luculated Parameter</u> <u>utlet Orifice Area =</u> t Orifice Centroid = tor Plate on Pipe =	4.50 5.00 6.56 19.78 9.89 s for Outlet Pipe w/ Zone 3 Restrictor 3.02 0.96 2.56 <u>Calculated Parame</u>	N/A N/A N/A N/A N/A N/A N/A N/A N/A ters for Spillway	feet ft <sup>2</sup> ft <sup>2</sup> ate ft <sup>2</sup> feet
Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage =	4.50 5.00 0.00 5.00 Close Mesh Grate 50% e (Circular Orifice. R Zone 3 Restrictor 0.25 24.00 22.00 Trapezoidal) 6.50	N/A N/A N/A N/A N/A estrictor Plate, or R Not Selected N/A N/A ft (relative to basin	feet H:V feet % tectangular Orifice) ft (distance below b inches inches	Gr O\ c asin bottom at Stage Half-Cent	ft) Height of Grat Overflow W ate Open Area / 10 verflow Grate Open Overflow Grate Open Overflow Grate Ope <u>Ca</u> = 0 ft) O Uutle tral Angle of Restric Spillway E Stage at 1	Veir Slope Length = No-yr Orifice Area = Area w/o Debris = n Area w/ Debris = Idulated Parameter utlet Orifice Area = t Orifice Centroid = tor Plate on Pipe = Design Flow Depth=	4.50 5.00 6.56 19.78 9.89 s for Outlet Pipe w/ Zone 3 Restrictor 3.02 0.96 2.56 Calculated Parame 0.49	N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A	feet ft <sup>2</sup> ft <sup>2</sup> ate ft <sup>2</sup> feet
Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length =	4.50 5.00 0.00 5.00 Close Mesh Grate 50% e (Circular Orifice, R Zone 3 Restrictor 0.25 24.00 22.00 Trapezoidal) 6.50 50.00	N/A N/A N/A N/A N/A estrictor Plate, or R Not Selected N/A N/A ft (relative to basin feet	feet H:V feet % tectangular Orifice) ft (distance below b inches inches	Gr O\ c asin bottom at Stage Half-Cent	ft) Height of Grat Overflow W ate Open Area / 10 verflow Grate Open Overflow Grate Open Overflow Grate Ope <u>Ca</u> = 0 ft) O Uutle tral Angle of Restric Spillway E Stage at 1	Veir Slope Length = 20-yr Orifice Area = Area w/o Debris = n Area w/ Debris = alculated Parameter utlet Orifice Area = t Orifice Centroid = ctor Plate on Pipe = Design Flow Depth= Fop of Freeboard = Fop of Freeboard =	4.50 5.00 6.56 19.78 9.89 s for Outlet Pipe w/ Zone 3 Restrictor 3.02 0.96 2.56 <u>Calculated Parame</u> 0.49 7.99	N/A N/A N/A N/A N/A N/A Selected N/A N/A N/A ters for Spillway feet feet	feet ft <sup>2</sup> ft <sup>2</sup> ate ft <sup>2</sup> feet
Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length = Spillway End Slopes =	4.50 5.00 0.00 5.00 Close Mesh Grate 50% e (Circular Orifice, R Zone 3 Restrictor 0.25 24.00 22.00 Trapezoidal) 6.50 50.00 4.00	N/A N/A N/A N/A N/A N/A Setrictor Plate, or R Not Selected N/A N/A ft (relative to basir feet H:V	feet H:V feet % tectangular Orifice) ft (distance below b inches inches	Gr O\ c asin bottom at Stage Half-Cent	ft) Height of Grat Overflow W ate Open Area / 10 verflow Grate Open Overflow Grate Open Dverflow Grate Ope Ca Ca Ca Ca Ca Ca Ca Ca Ca Ca Ca Ca Ca	Veir Slope Length = 20-yr Orifice Area = Area w/o Debris = n Area w/ Debris = alculated Parameter utlet Orifice Area = t Orifice Centroid = ctor Plate on Pipe = Design Flow Depth= Fop of Freeboard = Fop of Freeboard =	4.50 5.00 6.56 19.78 9.89 s for Outlet Pipe w/ Zone 3 Restrictor 3.02 0.96 2.56 <u>Calculated Parame</u> 0.49 7.99 0.80	N/A N/A N/A N/A N/A N/A N/A N/A N/A ters for Spillway feet feet acres	feet ft <sup>2</sup> ft <sup>2</sup> ate ft <sup>2</sup> feet
Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface =	4.50 5.00 0.00 5.00 Close Mesh Grate 50% 2 (Circular Orifice, R Zone 3 Restrictor 0.25 24.00 22.00 Trapezoidal) 6.50 50.00 4.00 1.00	N/A N/A N/A N/A N/A estrictor Plate, or R Not Selected N/A N/A ft (relative to basin feet H:V feet	feet H:V feet % tectangular Orifice) ft (distance below b inches inches inches	Gr Ov c asin bottom at Stage Half-Cent	ft) Height of Grat Overflow V ate Open Area / 10 verflow Grate Open Nverflow Grate Open Dverflow Grate Ope <u>Ca</u> = 0 ft) O Outle tral Angle of Restrict Spillway D Stage at T Basin Area at T Basin Volume at T	Veir Slope Length = No-yr Orifice Area = Area w/o Debris = n Area w/ Debris = In Area w/	4.50 5.00 6.56 19.78 9.89 s for Outlet Pipe w/ Zone 3 Restrictor 3.02 0.96 2.56 Calculated Parame 0.49 7.99 0.80 3.66	N/A N/A N/A N/A N/A N/A N/A N/A N/A ters for Spillway feet feet acres acre-ft	feet ft <sup>2</sup> ft <sup>2</sup> ft <sup>2</sup> ft <sup>2</sup> feet radians
Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface =	4.50           5.00           0.00           5.00           Close Mesh Grate           50%           e (Circular Orifice, R           Zone 3 Restrictor           0.25           24.00           22.00           Trapezoidal)           6.50           50.00           4.00           1.00	N/A N/A N/A N/A N/A N/A estrictor Plate, or R Not Selected N/A N/A ft (relative to basin feet H:V feet	feet H:V feet % Rectangular Orifice) ft (distance below b inches inches n bottom at Stage =	Gr Ov c asin bottom at Stage Half-Cent = 0 ft)	ft) Height of Grat Overflow W ate Open Area / 10 verflow Grate Open Overflow Grate Open Dverflow Grate Open C C C C C C C C C C C C C C C C C C C	Veir Slope Length = 20-yr Orifice Area = Area w/o Debris = n Area w/ Debris = alculated Parameter utlet Orifice Area = t Orifice Centroid = tor Plate on Pipe = Design Flow Depth= Fop of Freeboard = Fop of Freeboard =	4.50 5.00 6.56 19.78 9.89 s for Outlet Pipe w/ Zone 3 Restrictor 3.02 0.96 2.56 Calculated Parame 0.49 7.99 0.80 3.66	N/A N/A N/A N/A N/A N/A N/A N/A N/A ters for Spillway feet feet acres acre-ft	feet ft <sup>2</sup> ft <sup>2</sup> ft <sup>2</sup> feet radians
Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface =	4.50 5.00 0.00 5.00 Close Mesh Grate 50% 2 (Circular Orifice, R Zone 3 Restrictor 0.25 24.00 22.00 Trapezoidal) 6.50 50.00 4.00 1.00	N/A N/A N/A N/A N/A estrictor Plate, or R Not Selected N/A N/A ft (relative to basin feet H:V feet	feet H:V feet % tectangular Orifice) ft (distance below b inches inches inches	Gr Ov c asin bottom at Stage Half-Cent	ft) Height of Grat Overflow V ate Open Area / 10 verflow Grate Open Nverflow Grate Open Dverflow Grate Ope (Call Composition Composition) Call Composition Call	Veir Slope Length = No-yr Orifice Area = Area w/o Debris = n Area w/ Debris = In Area w/	4.50 5.00 6.56 19.78 9.89 s for Outlet Pipe w/ Zone 3 Restrictor 3.02 0.96 2.56 Calculated Parame 0.49 7.99 0.80 3.66	N/A N/A N/A N/A N/A N/A N/A N/A N/A ters for Spillway feet feet acres acre-ft	feet ft <sup>2</sup> ft <sup>2</sup> ft <sup>2</sup> ft <sup>2</sup> feet radians
Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = <u>Routed Hydrograph Results</u> Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) =	4.50           5.00           0.00           5.00           Close Mesh Grate           50%           2 (Circular Orifice, R           Zone 3 Restrictor           0.25           24.00           22.00           Trapezoidal)           6.50           50.00           4.00           1.00	N/A N/A N/A N/A N/A estrictor Plate, or R Not Selected N/A N/A ft (relative to basin feet H:V feet ride the default CU/ N/A 0.851	feet H:V feet % Rectangular Orifice) ft (distance below b inches inches n bottom at Stage = HP hydrographs and 2 Year 1.19 0.490	Gr Ov c asin bottom at Stage Half-Cent = 0 ft) 5 Year 1.50 0.748	ft) Height of Grat Overflow V ate Open Area / 10 verflow Grate Open Nverflow Grate Open Dverflow Grate Ope Call = 0 ft) O Outle tral Angle of Restrict Stage at 1 Basin Area at 1 Basin Volume at 1 destin Volume at 1 U <u>ventering new value</u> 1.75 0.979	Veir Slope Length = No-yr Orifice Area = Area w/o Debris = n Area w/ Debris = Iculated Parameter utlet Orifice Area = t Orifice Centroid = tor Plate on Pipe = Design Flow Depth= Fop of Freeboard = Fop of Freeboard = Fop of Freeboard = Cop of Cop of	4.50 5.00 6.56 19.78 9.89 s for Outlet Pipe w// Zone 3 Restrictor 3.02 0.96 2.56 Calculated Parame 0.49 7.99 0.80 3.66 drographs table (CC 50 Year 2.25 3.038	N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A	feet ft <sup>2</sup> ft <sup>2</sup> feet radians 500 Year 3.14 7.526
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Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage Spillway Crest Length = Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Restrictor Plate Height Above Max Water Surface = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = CUHP Runoff Volume (acre-ft) = CUHP Redevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, q (cfs/acre) = Peak Inflow Q (cfs) = Peak Untflow Q (cfs) = Peak Outflow Q (cfs) =	4.50 5.00 0.00 5.00 Close Mesh Grate 50% 2 (Circular Orifice, R Zone 3 Restrictor 0.25 24.00 22.00 Trapezoidal) 6.50 50.00 4.00 1.00 The user can over WOCV N/A 0.545 N/A N/A N/A N/A N/A	N/A N/A N/A N/A N/A N/A N/A N/A estrictor Plate, or R Not Selected N/A N/A ft (relative to basin feet H:V feet ride the default CU/ N/A 0.851 N/A	feet H:V feet % Rectangular Orifice) ft (distance below b inches inches h bottom at Stage = Vear 1.19 0.490 0.490 0.5 0.01 5.3 0.2 N/A	Gr Ov C asin bottom at Stage Half-Cent = 0 ft) 5 Year 1.50 0.748 1.0 0.748 1.0 0.748 1.0 0.2 0.2	ft) Height of Grat Overflow V ate Open Area / 10 verflow Grate Open Nverflow Grate Open Nverflow Grate Open Nverflow Grate Open Ca = 0 ft) O Outle tral Angle of Restrict Spillway D Stage at 1 Basin Volume at 1 Basin Volume at 1 <i>ventering new value</i> 10 Year 1.75 0.979 0.979 1.4 0.02 11.0 0.2 0.2	Veir Slope Length = No-yr Orifice Area = Area w/o Debris = n Area w/ Debris = Iculated Parameter utlet Orifice Area = t Orifice Centroid = tor Plate on Pipe = Design Flow Depth= Fop of Freeboard = Fop of Freeboard = Fop of Freeboard = Cop of Freeboard =	4.50 5.00 6.56 19.78 9.89 s for Outlet Pipe w// Zone 3 Restrictor 3.02 0.96 2.56 Calculated Parame 0.49 7.99 0.80 3.66 drographs table (CC 50 Year 2.25 3.038 3.038 24.7 0.34 37.5 18.5 0.7	N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A	feet ft <sup>2</sup> ft <sup>2</sup> feet radians 500 Year 3.14 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526
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Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Crest Length = Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Restrictor Plate Height Nolume (acref) = One-Hour Rainfall Depth (n) CUHP Prodevelopment Peak Q (cfs) = OPTIONAL Override Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, q (cfs/acre) = Peak Inflow Q (cfs) = Ratio Peak Outflow Predevelopment Q (cfs) = Ratio Peak Outflow Correl Inflow Volume (acref) = Structure Controlling Flow = Max Velocity through Grate 1 (fps) = Max Velocity through Grate 1 (fps) = Max Velocity through Grate 1 (fps) = Time to Drain 97% of Inflow Volume (hours) =	4.50 5.00 0.00 5.00 Close Mesh Grate 50% e (Circular Orifice, R Zone 3 Restrictor 0.25 24.00 22.00 Trapezoidal) 6.50 50.00 4.00 1.00 The user can over WOCV N/A N/A N/A N/A N/A N/A N/A N/A	N/A	feet H:V feet 9% Rectangular Orifice) ft (distance below b inches inches n bottom at Stage = HP hydrographs and 2 Year 1.19 0.490 0.490 0.5 0.01 5.3 0.2 N/A Plate N/A Plate N/A 38 40	Gr Ov C asin bottom at Stage Half-Cent = 0 ft) = 0 ft) = 0 ft) = 0.748 0.748 1.0 0.748 1.0 0.748 0.748 1.0 0.2 Plate N/A N/A N/A 53 55	ft) Height of Grat Overflow W ate Open Area / 10 verflow Grate Open Dverflow Grate Open Dverflow Grate Open Dverflow Grate Open Call = 0 ft) O Outle tral Angle of Restrict Spillway D Stage at T Basin Area at T Basin Volume at T Basin Volume at T Control Control Control Control Control Control Control Control Control Control Control Control Control	Veir Slope Length =         Vory Orifice Area =         Area w/o Debris =         n Area w/ Debris =         n Area w/ Debris =         ikulated Parameter         utlet Orifice Area =         t Orifice Centroid =         tor Plate on Pipe =         Design Flow Depth=         Fop of Freeboard =         Fop of Freeboard =         Poof Freeboard =         2.00         2.024         2.024         0.17         24.5         7.1         0.6         Overflow Weir 1         0.3         N/A         80         84	4.50 5.00 6.56 19.78 9.89 s for Outlet Pipe w// Zone 3 Restrictor 3.02 0.96 2.56 <u>Calculated Parame</u> 0.49 7.99 0.80 3.66 drographs table (CC 50 Year 2.25 3.038 3.038 3.038 3.038 2.4.7 0.34 37.5 18.5 0.7 Overflow Weir 1 0.9 N/A 77 83	N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A	feet ft <sup>2</sup> ft <sup>2</sup> feet radians <i>F).</i> 500 Year 3.14 7.526 7.526 7.4.8 1.04 89.2 63.4 0.8 Spillway 1.8 N/A 66 78
Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Crest Length = Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Routed Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = CUHP Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, q (cfs/acre) Predevelopment Unit Peak Flow, q (cfs/acre) Peak Inflow Q (cfs) = Ratio Peak Outflow to Predevelopment Q = Max Velocity through Grate 1 (fps) = Max Velocity through Grate 1 (fps) = Max Velocity through Grate 2 (fps) = Time to Drain 97% of Inflow Volume (hours) = Time to Drain 99% of Inflow Volume (hours) =	4.50 5.00 0.00 5.00 Close Mesh Grate 50% e (Circular Orlfice, R Zone 3 Restrictor 0.25 24.00 22.00 Trapezoidal) 6.50 50.00 4.00 1.00 The user can over WOCV N/A 0.545 N/A N/A N/A N/A N/A N/A N/A N/A	N/A	feet H:V feet 9% Rectangular Orifice) ft (distance below b inches inches h bottom at Stage = h bottom at Stage = Vear 1.19 0.490 0.490 0.490 0.490 0.5 0.01 5.3 0.2 N/A Plate N/A N/A 38 40 2.89	Gr Ov c asin bottom at Stage Half-Cent = 0 ft) = 0 ft) = 0 ft) = 0 ft) = 0 ft) = 0 ft = 0 ft	ft) Height of Grate Overflow V ate Open Area / 10 verflow Grate Open bverflow Grate Open bverflow Grate Open bverflow Grate Open can be for the op	Veir Slope Length = No-yr Orifice Area = Area w/o Debris = n Area w/ Debris = n Area w/ Debris = liculated Parameter utlet Orifice Area = t Orifice Centroid = tor Plate on Pipe = Cop of Freeboard = Fop of Freeboard = Fop of Freeboard = Fop of Freeboard = Fop of Freeboard = Cop of Freeboard =	4.50 5.00 6.56 19.78 9.89 s for Outlet Pipe w// Zone 3 Restrictor 3.02 0.96 2.56 <u>Calculated Parame</u> 0.49 7.99 0.80 3.66 drographs table (CC 50 Year 2.25 3.038 3.038 24.7 0.34 3.7.5 18.5 0.7 Overflow Weir 1 0.9 N/A 77 83 5.17	N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A	feet ft <sup>2</sup> ft <sup>2</sup> feet radians <i>F).</i> 500 Year 3.14 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.526 7.578 6.62
Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Crest Length = Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway Invert Stage Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Reuted Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (n) CUHP Predevelopment Peak Q (cfs) = OPTIONAL Override Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, q (cfs/acr) = Peak Inflow Q (cfs) = Peak Outflow Q (cfs) = Ratio Peak Outflow to Predevelopment 2 (fps) = Max Velocity through Grate 1 (fps) =	4.50 5.00 0.00 5.00 Close Mesh Grate 50% e (Circular Orifice, R Zone 3 Restrictor 0.25 24.00 22.00 Trapezoidal) 6.50 50.00 4.00 1.00 The user can over WOCV N/A N/A N/A N/A N/A N/A N/A N/A	N/A	feet H:V feet 9% Rectangular Orifice) ft (distance below b inches inches n bottom at Stage = HP hydrographs and 2 Year 1.19 0.490 0.490 0.5 0.01 5.3 0.2 N/A Plate N/A Plate N/A 38 40	Gr Ov C asin bottom at Stage Half-Cent = 0 ft) = 0 ft) = 0 ft) = 0.748 0.748 1.0 0.748 1.0 0.748 0.748 1.0 0.2 Plate N/A N/A N/A 53 55	ft) Height of Grat Overflow W ate Open Area / 10 verflow Grate Open Dverflow Grate Open Dverflow Grate Open Dverflow Grate Open Call = 0 ft) O Outle tral Angle of Restrict Spillway D Stage at T Basin Area at T Basin Volume at T Basin Volume at T Control Control Control Control Control Control Control Control Control Control Control Control Control	Veir Slope Length =         Vory Orifice Area =         Area w/o Debris =         n Area w/ Debris =         n Area w/ Debris =         ikulated Parameter         utlet Orifice Area =         t Orifice Centroid =         tor Plate on Pipe =         Design Flow Depth=         Fop of Freeboard =         Fop of Freeboard =         Poof Freeboard =         2.00         2.024         2.024         0.17         24.5         7.1         0.6         Overflow Weir 1         0.3         N/A         80         84	4.50 5.00 6.56 19.78 9.89 s for Outlet Pipe w// Zone 3 Restrictor 3.02 0.96 2.56 <u>Calculated Parame</u> 0.49 7.99 0.80 3.66 drographs table (CC 50 Year 2.25 3.038 3.038 3.038 3.038 2.4.7 0.34 37.5 18.5 0.7 Overflow Weir 1 0.9 N/A 77 83	N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A	feet ft <sup>2</sup> ft <sup>2</sup> feet radians <i>F).</i> 500 Year 3.14 7.526 7.4.8 7.526 7.4.8 1.04 89.2 63.4 0.8 Spillway 1.8 N/A 66 78



# DETENTION BASIN OUTLET STRUCTURE DESIGN Outflow Hydrograph Workbook Filename:

Inflow Hydrographs

the calculated inflow hydrographs from this workbook with inflow hydro ed in a separate progr The user can aranhs dovol

	The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.									
	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00 1111	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.07
	0:15:00	0.00	0.00	0.18	0.29	0.36	0.00	0.31	0.30	0.46
	0:20:00	0.00	0.00	0.73	0.99	1.17	0.75	0.89	0.93	1.26
	0:25:00	0.00	0.00	2.71	4.62	6.22	2.38	3.35	3.92	6.29
	0:30:00	0.00	0.00	4.74	7.75	10.14	11.49	18.57	24.42	42.15
	0:35:00	0.00	0.00	5.32	8.47	11.03	20.87	32.21	45.35	74.42
	0:40:00	0.00	0.00	5.17	8.12	10.57	24.49	37.48	53.86	87.35
	0:45:00	0.00	0.00	4.74	7.36	9.53	24.22	36.97	54.40	89.17
	0:50:00	0.00	0.00	4.33	6.72	8.68	22.52	34.05	50.57	84.36
	0:55:00 1:00:00	0.00	0.00	3.99	6.17	7.94	20.50	30.97	46.16	77.97
	1:05:00	0.00	0.00	3.67 3.41	5.63 5.19	7.22	18.61 16.88	28.05 25.38	42.23 38.54	71.86 66.41
	1:10:00	0.00	0.00	3.18	4.85	6.31	15.27	25.38	34.88	60.58
	1:15:00	0.00	0.00	2.94	4.50	5.99	13.90	20.91	31.52	54.92
	1:20:00	0.00	0.00	2.71	4.13	5.56	12.60	18.92	28.34	49.31
	1:25:00	0.00	0.00	2.47	3.76	5.03	11.32	16.93	25.24	43.81
	1:30:00	0.00	0.00	2.24	3.39	4.49	10.06	14.98	22.26	38.59
	1:35:00	0.00	0.00	2.03	3.04	3.98	8.81	13.05	19.34	33.49
	1:40:00	0.00	0.00	1.88	2.80	3.67	7.64	11.25	16.63	28.81
	1:45:00	0.00	0.00	1.80	2.62	3.45	6.83	10.05	14.74	25.58
	1:50:00	0.00	0.00	1.71	2.46	3.25	6.26	9.18	13.38	23.10
	1:55:00	0.00	0.00	1.61	2.30	3.04	5.78	8.44	12.21	20.94
	2:00:00 2:05:00	0.00	0.00	1.48 1.33	2.14	2.82 2.54	5.31 4.80	7.72	11.12 9.99	18.96 17.00
	2:10:00	0.00	0.00	1.33	1.70	2.54	4.80	6.18	9.99 8.86	15.05
	2:15:00	0.00	0.00	1.02	1.47	1.93	3.74	5.40	7.76	13.17
	2:20:00	0.00	0.00	0.88	1.26	1.64	3.23	4.65	6.70	11.38
	2:25:00	0.00	0.00	0.74	1.05	1.38	2.73	3.92	5.66	9.62
	2:30:00	0.00	0.00	0.61	0.86	1.12	2.24	3.20	4.62	7.87
	2:35:00	0.00	0.00	0.48	0.67	0.88	1.77	2.49	3.60	6.14
	2:40:00	0.00	0.00	0.37	0.50	0.65	1.30	1.80	2.59	4.43
	2:45:00	0.00	0.00	0.28	0.36	0.48	0.86	1.14	1.63	2.81
	2:50:00	0.00	0.00	0.22	0.29	0.39	0.54	0.70	0.96	1.73
	2:55:00	0.00	0.00	0.18	0.25	0.33	0.37	0.47	0.61	1.14
	3:00:00 3:05:00	0.00	0.00	0.16	0.21	0.28	0.28	0.35	0.43	0.78
	3:10:00	0.00	0.00	0.13	0.17 0.15	0.23	0.22	0.27	0.31	0.54
	3:15:00	0.00	0.00	0.09	0.12	0.16	0.14	0.21	0.23	0.36
	3:20:00	0.00	0.00	0.08	0.12	0.13	0.14	0.13	0.17	0.20
	3:25:00	0.00	0.00	0.06	0.08	0.11	0.09	0.11	0.10	0.13
	3:30:00	0.00	0.00	0.05	0.07	0.08	0.08	0.09	0.08	0.10
	3:35:00	0.00	0.00	0.04	0.05	0.07	0.06	0.07	0.06	0.08
	3:40:00	0.00	0.00	0.03	0.04	0.05	0.05	0.05	0.05	0.06
	3:45:00	0.00	0.00	0.02	0.03	0.04	0.04	0.04	0.04	0.05
	3:50:00	0.00	0.00	0.02	0.02	0.03	0.03	0.03	0.03	0.03
	3:55:00 4:00:00	0.00	0.00	0.01	0.01	0.02	0.02	0.02	0.02	0.02
	4:00:00	0.00	0.00	0.01	0.01	0.01	0.01	0.01	0.01	0.01
	4:10:00	0.00	0.00	0.00	0.01	0.01	0.01	0.01	0.01	0.01
	4:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:25:00 4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:50:00 4:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:15:00 5:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:35:00 5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

ZONE 1 AND 2 ORIFICES

Example Zone Configuration (Retention Pond)

-100-YEAR ORIFICE

Depth Increment = 0.25

Stage (ft)

Length (ft)

Stage (ft)

Stage - Storage Description

Watershed	Information

PERMA

atersned Information		
Selected BMP Type =	EDB	
Watershed Area =	129.00	acres
Watershed Length =	6,000	ft
Watershed Length to Centroid =	3,500	ft
Watershed Slope =	0.045	ft/ft
Watershed Imperviousness =	14.00%	percent
Percentage Hydrologic Soil Group A =	100.0%	percent
Percentage Hydrologic Soil Group B =	0.0%	percent
Percentage Hydrologic Soil Groups C/D =	0.0%	percent
Target WQCV Drain Time =	40.0	hours
Location for 1-hr Rainfall Depths =	User Input	

## After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

the embedded colorado orban nyard	graphinoceue	ile.
Water Quality Capture Volume (WQCV) =	0.950	acre-feet
Excess Urban Runoff Volume (EURV) =	1.458	acre-feet
2-yr Runoff Volume (P1 = 1.19 in.) =	0.830	acre-feet
5-yr Runoff Volume (P1 = 1.5 in.) =	1.278	acre-feet
10-yr Runoff Volume (P1 = 1.75 in.) =	1.674	acre-feet
25-yr Runoff Volume (P1 = 2 in.) =	3.538	acre-feet
50-yr Runoff Volume (P1 = 2.25 in.) =	5.349	acre-feet
100-yr Runoff Volume (P1 = 2.52 in.) =	7.862	acre-feet
500-yr Runoff Volume (P1 = 3.14 in.) =	13.384	acre-feet
Approximate 2-yr Detention Volume =	0.887	acre-feet
Approximate 5-yr Detention Volume =	1.206	acre-feet
Approximate 10-yr Detention Volume =	1.563	acre-feet
Approximate 25-yr Detention Volume =	2.072	acre-feet
Approximate 50-yr Detention Volume =	2.622	acre-feet
Approximate 100-yr Detention Volume =	3.839	acre-feet

Define	Zones	and	Basi	n	Geom	etry
		ž	Zone	1	Volume	(W0

Zone 1 Volume (WQCV) =	0.950	acre-feet
Zone 2 Volume (EURV - Zone 1) =	0.508	acre-feet
Zone 3 Volume (100-year - Zones 1 & 2) =	2.381	acre-feet
Total Detention Basin Volume =	3.839	acre-feet
Initial Surcharge Volume (ISV) =	124	ft <sup>3</sup>
Initial Surcharge Depth (ISD) =	0.33	ft
Total Available Detention Depth (H <sub>total</sub> ) =	6.00	ft
Depth of Trickle Channel $(H_{TC}) =$	0.50	ft
Slope of Trickle Channel (S <sub>TC</sub> ) =	0.010	ft/ft
Slopes of Main Basin Sides (S <sub>main</sub> ) =	4	H:V
Basin Length-to-Width Ratio $(R_{L/W}) =$	2	

Initial Surcharge Area (A <sub>ISV</sub> ) =	376	ft <sup>2</sup>
Surcharge Volume Length (L <sub>ISV</sub> ) =	19.4	ft
Surcharge Volume Width (WISV) =	19.4	ft
Depth of Basin Floor (H <sub>FLOOR</sub> ) =	2.63	ft
Length of Basin Floor $(L_{FLOOR}) =$	292.9	ft
Width of Basin Floor $(W_{FLODR}) =$	150.9	ft
Area of Basin Floor (A <sub>FLOOR</sub> ) =	44,200	ft <sup>2</sup>
Volume of Basin Floor ( $V_{FLODR}$ ) =	42,653	ft <sup>3</sup>
Depth of Main Basin (H <sub>MAIN</sub> ) =	2.54	ft
Length of Main Basin $(L_{MAIN}) =$	313.2	ft
Width of Main Basin ( $W_{MAIN}$ ) =	171.2	ft
Area of Main Basin (A <sub>MAIN</sub> ) =	53,631	ft <sup>2</sup>
Volume of Main Basin ( $V_{MAIN}$ ) =	124,052	ft <sup>3</sup>
Calculated Total Basin Volume ( $V_{total}$ ) =	3.834	acre-feet

		Description	(Π)	stage (II)	(ft)	(ft)	(π-)	Area (ft *)	(acre)	(π-)	(ac-π)
		Top of Micropool	0.00		19.4	19.4	376		0.009		
		ISV	0.33		19.4	19.4	376		0.009	124	0.003
			0.50		19.4	19.4	376		0.009	188	0.004
			0.75		19.4	19.4	376		0.009	282	0.006
			1.00		37.1	27.9	1,034		0.024	428	0.010
			1.25		63.1	40.4	2,548		0.058	862	0.020
			1.50		89.1	52.9	4,712		0.108	1,756	0.040
			1.75		115.1	65.4	7,526		0.173	3,272	0.075
			2.00		141.1	77.9	10,989		0.252	5,573	0.128
			2.00		167.1	90.4	15,103		0.347	8,821	0.203
			2.23								0.203
					193.1	102.9	19,867		0.456	13,179	
			2.75		219.1	115.4	25,280		0.580	18,809	0.432
			3.00		245.1	127.9	31,344		0.720	25,873	0.594
			3.25		271.1	140.4	38,058		0.874	34,535	0.793
Optional Use		Zone 1 (WQCV)	3.42		288.8	148.9	42,995		0.987	41,420	0.951
	acre-feet	Floor	3.46		292.9	150.9	44,200		1.015	43,164	0.991
	acre-feet		3.50		293.2	151.2	44,342		1.018	44,935	1.032
1.19	inches		3.75		295.2	153.2	45,235		1.038	56,132	1.289
1.50	inches	Zone 2 (EURV)	3.92		296.6	154.6	45,847		1.052	63,873	1.466
1.75	inches		4.00		297.2	155.2	46,136		1.059	67,553	1.551
2.00	inches		4.25		299.2	157.2	47,045		1.080	79,200	1.818
2.25	inches		4.50		301.2	159.2	47,962		1.101	91,076	2.091
2.52	inches		4.75		303.2	161.2	48,886		1.122	103,182	2.369
	inches		5.00		305.2	163.2	49,819		1.144	115,520	2.652
			5.25		307.2	165.2	50,760		1.165	128,092	2.941
			5.50		309.2	167.2	51,709		1.187	140,900	3.235
			5.75		311.2	169.2	52,666		1.209	153,947	3.534
		Zone 3 (100-year)	6.00		313.2	171.2	53,631		1.231	167,234	3.839
			6.25		315.2	173.2	54,604		1.254	180,763	4.150
			6.50		317.2	175.2	55,585		1.276	194,537	4.466
			6.75		319.2	177.2	56,574		1.299	208,556	4.788
			7.00		321.2	179.2	57,571		1.322	222,824	5.115
			7.25		323.2	181.2	58,576		1.345	237,342	5.449
			7.50		325.2	183.2	59,588		1.368	252,113	5.788
			7.75		327.2	185.2	60,609		1.391	267,137	6.133
			8.00		329.2	187.2	61,638		1.415	282,418	6.483
		L									
		L									
					<u> </u>		<u> </u>		<u> </u>		
						-					
		L									-

Area (ft <sup>2</sup>)

Override

Area (ft<sup>2</sup>)

Width

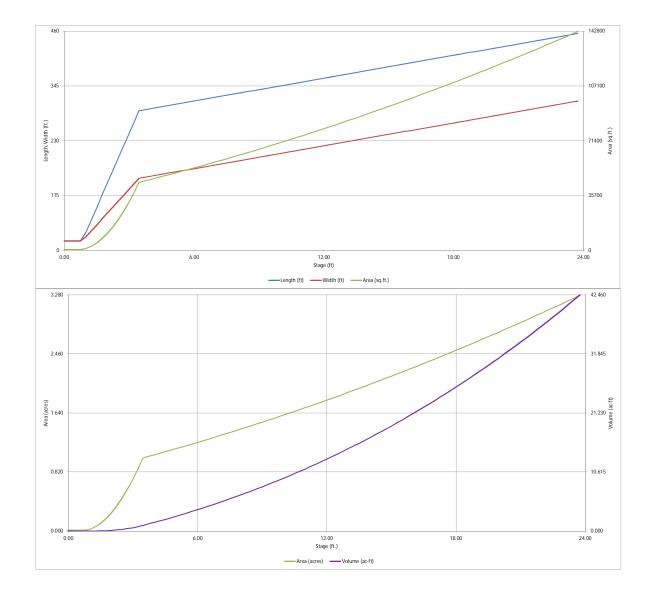
(ft)

Area (acre)

Volume (ft 3)

Volume (ac-ft)

MHFD-Detention, Version 4.06 (July 2022)



#### DETENTION BASIN OUTLET STRUCTURE DESIGN MHFD-Detention, Version 4.06 (July 2022) Project: Esteban Rodriguez Subdivision-PDR Basin ID: Pond 4 Estimated Estimated Stage (ft) Volume (ac-ft) Outlet Type EURV WOCV Zone 1 (WQCV) 3.42 0.950 Orifice Plate Zone 2 (EURV) 3.92 0.508 100-YEAR Orifice Plate ZONE 1 AND ORIFICES Zone 3 (100-year) 6.00 2.381 Weir&Pipe (Restrict) PERM/ Example Zone Configuration (Retention Pond) 3 839 Total (all zones User Input: Orifice at Underdrain Outlet (typically used to drain WOCV in a Filtration BMP) Calculated Parameters for Underdrain ft (distance below the filtration media surface) Underdrain Orifice Area = Underdrain Orifice Invert Depth : N/A N/A $ft^2$ Underdrain Orifice Diameter = N/A inches Underdrain Orifice Centroid = N/A feet User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP) Calculated Parameters for Plate Centroid of Lowest Orifice = 0.00 ft (relative to basin bottom at Stage = 0 ft) WQ Orifice Area per Row NI/A $ft^2$ ft (relative to basin bottom at Stage = 0 ft) Elliptical Half-Width N/A Depth at top of Zone using Orifice Plate 3.90 eet Orifice Plate: Orifice Vertical Spacing Elliptical Slot Centroid N/A inches N/A feet Orifice Plate: Orifice Area per Row = N/A sa, inches Elliptical Slot Area = N/A ft<sup>2</sup> User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest) Row 5 (optional) Row 1 (required) Row 2 (optional) Row 3 (optional) Row 4 (optional) Row 6 (optional) Row 7 (optional) Row 8 (optional) Stage of Orifice Centroid (ft 0.00 1.40 3.80 3.50 Orifice Area (sq. inches) 4 10 1 50 1 00 1 00 Row 9 (optional) Row 10 (optional) Row 11 (optional) Row 12 (optional) Row 13 (optional) Row 14 (optional) Row 15 (optional) Row 16 (optional) Stage of Orifice Centroid (ft Orifice Area (sg. inches) User Input: Vertical Orifice (Circular or Rectangular) Calculated Parameters for Vertical Orifice Not Selected Not Selected Not Selected Not Selected Vertical Orifice Area Invert of Vertical Orifice N/A N/A ft (relative to basin bottom at Stage = 0 ft) N/A N/A ft (relative to basin bottom at Stage = 0 ft) Depth at top of Zone using Vertical Orifice : N/A N/A Vertical Orifice Centroid N/A N/A feet Vertical Orifice Diameter = N/A N/A inches User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir and No Outlet Pipe) Calculated Parameters for Overflow Weir Zone 3 Weir Not Selected Zone 3 Weir Not Selected Overflow Weir Front Edge Height, Ho 4.50 N/A ft (relative to basin bottom at Stage = 0 ft) Height of Grate Upper Edge, Ht 4.50 N/A eet Overflow Weir Front Edge Length 6.00 N/A feet Overflow Weir Slope Length 6.00 N/A feet Overflow Weir Grate Slope 0.00 N/A H:V Grate Open Area / 100-yr Orifice Area 5.80 N/A Horiz. Length of Weir Sides Overflow Grate Open Area w/o Debris 28.48 6.00 N/A feet N/A Ft<sup>2</sup> Overflow Grate Type Close Mesh Grate N/A Overflow Grate Open Area w/ Debris 14.24 N/A ft<sup>2</sup> Debris Clogging % = 50% N/A User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice) Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate Zone 3 Restrictor Not Selected Zone 3 Restrictor Not Selected Depth to Invert of Outlet Pipe 0.25 N/A ft (distance below basin bottom at Stage = 0 ft) Outlet Orifice Area 4.91 N/A Outlet Pipe Diameter 30.00 N/A Outlet Orifice Centroid N/A inches 1.25 feet Restrictor Plate Height Above Pipe Invert = 30.00 inches Half-Central Angle of Restrictor Plate on Pipe 3.14 N/A radians User Input: Emergency Spillway (Rectangular or Trapezoidal) Calculated Parameters for Spillway Spillway Invert Stage= ft (relative to basin bottom at Stage = 0 ft) Spillway Design Flow Depth= 0.44 feet 6.00 Stage at Top of Freeboard = Spillway Crest Length 75.00 feet 7.44 feet Spillway End Slopes 4.00 H:V Basin Area at Top of Freeboard 1.36 acres feet Freeboard above Max Water Surface = 1.00 Basin Volume at Top of Freeboard = 5.71 acre-ft Routed Hydrograph Results user can ove ride the default CUHP hydrographs and runoff volumes by ntering new values in the Inflow Hydrographs table (Columns W through AF) Design Storm Return Period WOCV FURV 2 Year 5 Year 10 Year 25 Year 50 Year 100 Year 500 Year One-Hour Rainfall Depth (in) N/A N/A 1.19 1.50 1.75 2.00 2.52 3.14 2.25 0.950 1.674 7.862 CUHP Runoff Volume (acre-ft) 1.458 0.830 1.278 13.384 Inflow Hydrograph Volume (acre-ft) 1.278 3.538 5.349 13.384 N/A N/A 0.830 1.674 7.862 CUHP Predevelopment Peak Q (cfs) N/A N/A 0.6 1 1 1.6 14 7 29.5 49 1 91 9 OPTIONAL Override Predevelopment Peak Q (cfs) N/A N/A Predevelopment Unit Peak Flow, q (cfs/acre) 0.00 0.01 0.01 0.11 0.23 0.38 0.71 N/A N/A N/A Peak Inflow Q (cfs) N/A 9.7 110.6 6.1 12.7 29.5 45.3 66.6 Peak Outflow Q (cfs) 0.3 0.4 0.3 0.3 0.4 93 22.2 41.5 86.7 Ratio Peak Outflow to Predevelopment Q N/A N/A N/A 0.3 0.2 0.6 0.8 0.8 0.9 Structure Controlling Flow Plate Plate Overflow Weir 1 Overflow Weir 1 Overflow Weir Plate Plate Plate Spillway Max Velocity through Grate 1 (fps) N/A N/A N/A N/A N/A 1.9 0.8 0. Max Velocity through Grate 2 (fps) N/A N/A N/A N/A N/A N/A N/A N/A N/A Time to Drain 97% of Inflow Volume (hours) 40 57 37 52 64 78 75 72 64

Time to Drain 99% of Inflow Volume (hours)

Area at Maximum Ponding Depth (acres)

Maximum Ponding Depth (ft)

Maximum Volume Stored (acre-ft)

42

3.42

0.99

0.951

59

3.92

1.05

1.466

38

3.18

0.83

0.733

54

3.64

1.03

1.16

66

4.01

1.06

1.551

82

4.87

1.13

2.493

81

5.17

1.16

2.83

80

5.52

1.19

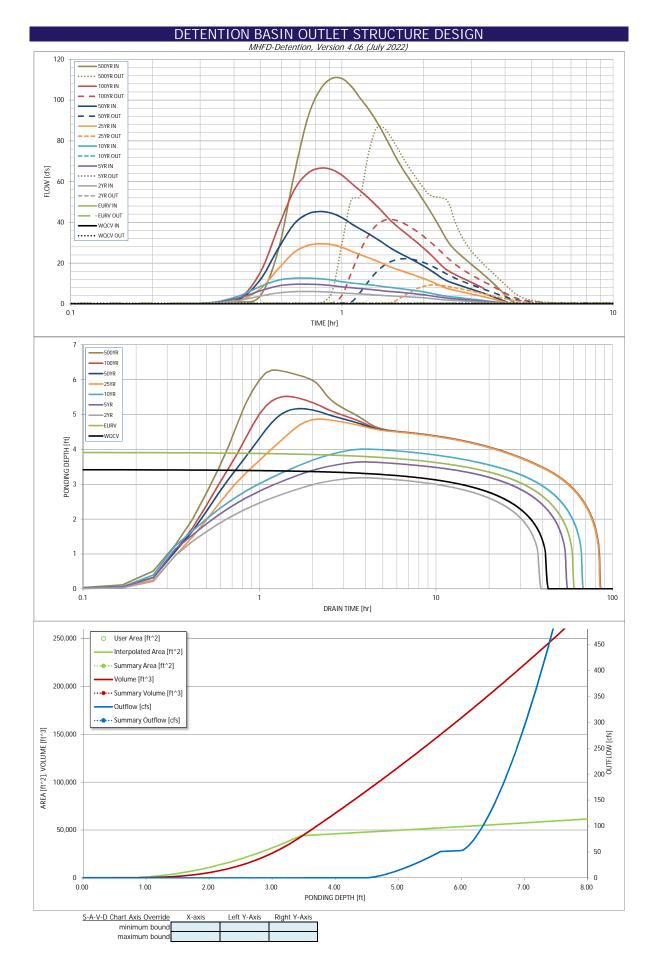
3.247

77

6.27

1.26

4.175



### DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename:

Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

	The user can o	verride the calcu	ulated inflow hy	drographs from	this workbook v	with inflow hydr	ographs develop	oed in a separate	program.	
	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
3.00 11111	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.03
	0:15:00	0.00	0.00	0.09	0.00	0.19	0.00	0.01	0.16	0.28
	0:20:00	0.00	0.00	0.46	0.65	0.78	0.51	0.62	0.63	0.89
	0:25:00	0.00	0.00	1.79	2.95	3.93	1.63	2.24	2.57	4.05
	0:30:00	0.00	0.00	3.88	6.47	8.58	7.48	11.96	15.56	26.81
-	0:35:00	0.00	0.00	5.45	8.88	11.67	17.38	27.45	37.88	63.55
	0:40:00	0.00	0.00	6.04	9.66	12.62	25.33	39.30	55.92	91.84
	0:45:00	0.00	0.00	6.12	9.71	12.68	28.72	44.25	64.27	105.39
	0:50:00	0.00	0.00	6.01	9.48	12.34	29.53	45.33	66.65	110.63
	0:55:00	0.00	0.00	5.75	9.04	11.72	29.12	44.50	65.91	110.56
	1:00:00 1:05:00	0.00	0.00	5.41 5.13	8.43 7.96	10.88 10.30	27.79 25.88	42.34 39.34	63.17 59.23	106.68 100.98
	1:10:00	0.00	0.00	4.91	7.60	9.87	23.88	36.81	55.60	95.82
	1:15:00	0.00	0.00	4.67	7.23	9.47	22.73	34.52	52.10	90.19
	1:20:00	0.00	0.00	4.42	6.84	9.05	21.26	32.26	48.50	84.06
	1:25:00	0.00	0.00	4.18	6.44	8.56	19.78	29.95	44.91	77.83
	1:30:00	0.00	0.00	3.98	6.14	8.15	18.34	27.69	41.39	71.74
	1:35:00	0.00	0.00	3.83	5.89	7.78	17.14	25.88	38.50	66.72
	1:40:00	0.00	0.00	3.68	5.64	7.41	16.14	24.31	36.07	62.34
	1:45:00	0.00	0.00	3.53	5.36	7.05	15.21	22.86	33.83	58.33
	1:50:00	0.00	0.00	3.39	5.08	6.68	14.29	21.43	31.66	54.47
	1:55:00 2:00:00	0.00	0.00	3.22	4.80	6.31	13.39	20.03	29.52	50.71
	2:00:00	0.00	0.00	3.03 2.82	4.51 4.19	5.93 5.50	12.50 11.57	18.64 17.21	27.40 25.26	47.00 43.28
	2:10:00	0.00	0.00	2.82	3.83	5.04	10.60	17.21	23.20	39.57
	2:15:00	0.00	0.00	2.35	3.48	4.57	9.62	14.25	20.92	35.85
	2:20:00	0.00	0.00	2.14	3.17	4.17	8.66	12.80	18.79	32.22
	2:25:00	0.00	0.00	1.99	2.94	3.88	7.85	11.62	17.03	29.29
	2:30:00	0.00	0.00	1.86	2.76	3.63	7.27	10.77	15.76	27.12
	2:35:00	0.00	0.00	1.74	2.58	3.40	6.81	10.10	14.75	25.33
	2:40:00	0.00	0.00	1.63	2.42	3.19	6.39	9.50	13.85	23.73
	2:45:00	0.00	0.00	1.52	2.26	2.97	6.00	8.92	13.01	22.24
	2:50:00	0.00	0.00	1.41	2.11	2.77	5.63	8.36	12.19	20.82
	2:55:00 3:00:00	0.00	0.00	1.32	1.96	2.57	5.26	7.81	11.40	19.45
	3:05:00	0.00	0.00	1.22	1.82	2.38	4.90 4.56	7.28 6.76	10.63 9.89	18.14 16.86
	3:10:00	0.00	0.00	1.13	1.68	2.20	4.56	6.25	9.89	15.60
	3:15:00	0.00	0.00	0.95	1.41	1.85	3.87	5.74	8.40	14.34
	3:20:00	0.00	0.00	0.86	1.28	1.68	3.53	5.23	7.66	13.08
	3:25:00	0.00	0.00	0.78	1.15	1.51	3.19	4.72	6.92	11.83
	3:30:00	0.00	0.00	0.70	1.03	1.35	2.86	4.22	6.19	10.58
	3:35:00	0.00	0.00	0.61	0.91	1.18	2.53	3.72	5.46	9.33
	3:40:00	0.00	0.00	0.53	0.78	1.02	2.20	3.22	4.73	8.08
	3:45:00	0.00	0.00	0.46	0.66	0.87	1.87	2.72	4.00	6.84
	3:50:00	0.00	0.00	0.38	0.55	0.71	1.54	2.23	3.27	5.60
	3:55:00 4:00:00	0.00	0.00	0.31	0.43	0.56	1.22	1.74	2.55	4.37
	4:00:00	0.00	0.00	0.23	0.32	0.42	0.90	1.26 0.80	1.84 1.15	3.14 1.97
	4:05:00	0.00	0.00	0.18	0.23	0.31	0.60	0.80	0.67	1.97
	4:15:00	0.00	0.00	0.12	0.16	0.22	0.25	0.32	0.42	0.79
	4:20:00	0.00	0.00	0.11	0.14	0.19	0.19	0.24	0.30	0.54
	4:25:00	0.00	0.00	0.09	0.12	0.16	0.15	0.19	0.22	0.38
	4:30:00 4:35:00	0.00	0.00	0.08	0.10	0.14 0.11	0.12 0.10	0.15 0.12	0.16 0.12	0.26 0.18
	4:40:00	0.00	0.00	0.06	0.07	0.09	0.08	0.09	0.09	0.12
	4:45:00	0.00	0.00	0.05	0.06	0.07	0.07	0.07	0.07	0.09
	4:50:00 4:55:00	0.00	0.00	0.04 0.03	0.05	0.06	0.05	0.06	0.05	0.07 0.05
	5:00:00	0.00	0.00	0.02	0.03	0.04	0.03	0.04	0.03	0.04
	5:05:00	0.00	0.00	0.02	0.02	0.03	0.03	0.03	0.03	0.03
	5:10:00 5:15:00	0.00	0.00	0.01 0.01	0.02	0.02 0.01	0.02	0.02	0.02	0.02
	5:15:00	0.00	0.00	0.01	0.01	0.01	0.01	0.01	0.01	0.02
	5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.01	0.00	0.01
	5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:35:00 5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

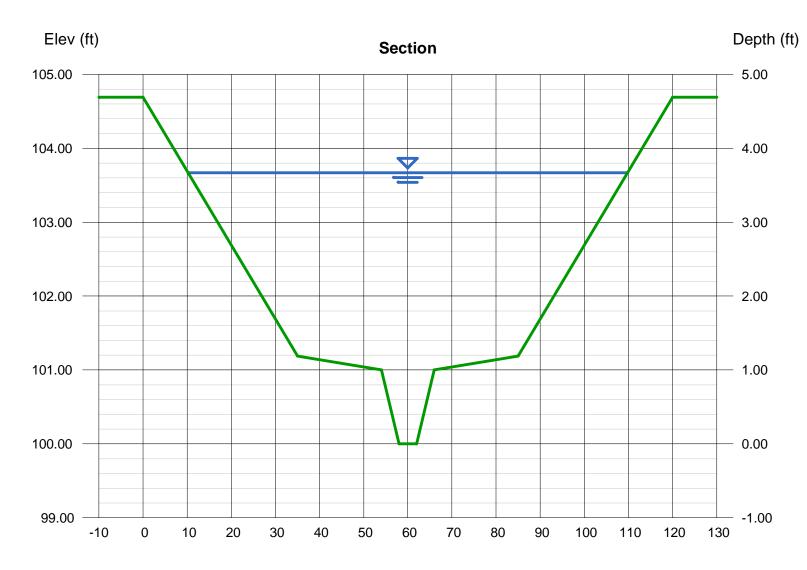
Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Wednesday, Jul 31 2024

### **WF-8a Typical Section**

User-defined		Highlighted	
Invert Elev (ft)	= 100.00	Depth (ft)	= 3.67
Slope (%)	= 0.50	Q (cfs)	= 753.00
N-Value	= 0.044	Area (sqft)	= 199.39
		Velocity (ft/s)	= 3.78
Calculations		Wetted Perim (ft)	= 100.10
Compute by:	Known Q	Crit Depth, Yc (ft)	= 2.71
Known Q (cfs)	= 753.00	Top Width (ft)	= 99.60
		EGL (ft)	= 3.89

(Sta, El, n)-(Sta, El, n)... (0.00, 104.69) -(35.00, 101.19, 0.045) -(54.00, 101.00, 0.045) -(58.00, 100.00, 0.030) -(62.00, 100.00, 0.030) -(66.00, 101.00, 0.045) -(85.00, 101.19, 0.045) -(120.00, 104.69, 0.045)



Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

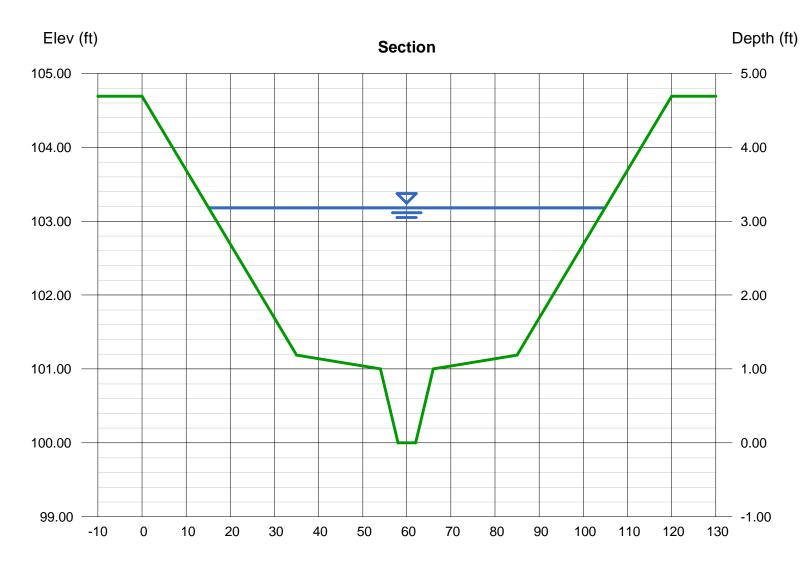
Wednesday, Jul 31 2024

## WF-8a Typical Section-Max Slope

User-defined		Highlighted	
Invert Elev (ft)	= 100.00	Depth (ft)	= 3.18
Slope (%)	= 1.05	Q (cfs)	= 753.00
N-Value	= 0.044	Area (sqft)	= 152.99
		Velocity (ft/s)	= 4.92
Calculations		Wetted Perim (ft)	= 90.25
Compute by:	Known Q	Crit Depth, Yc (ft)	= 2.71
Known Q (cfs)	= 753.00	Top Width (ft)	= 89.80
		EGL (ft)	= 3.56

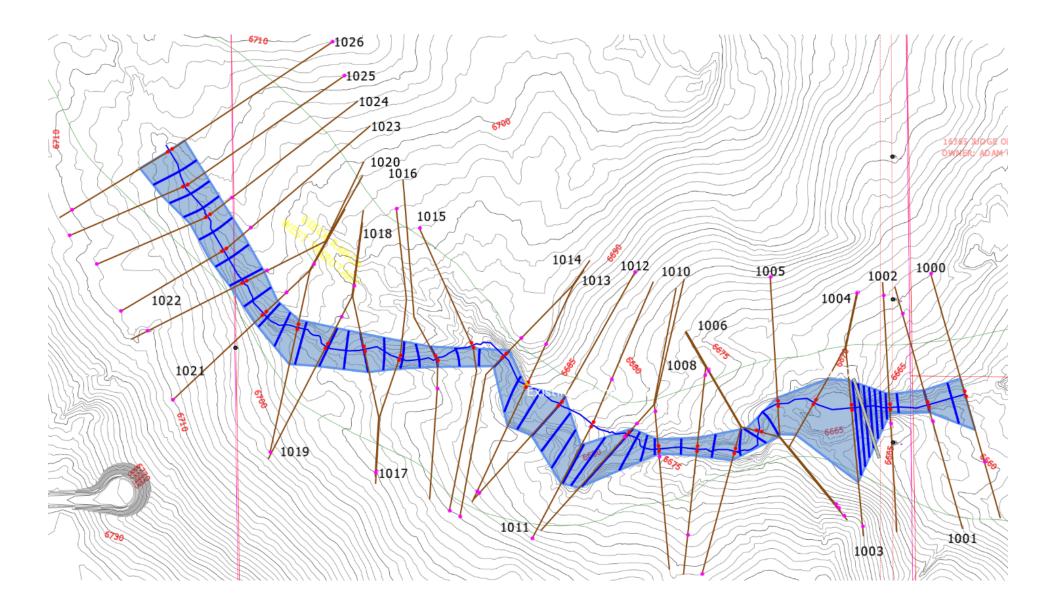
### (Sta, El, n)-(Sta, El, n)...

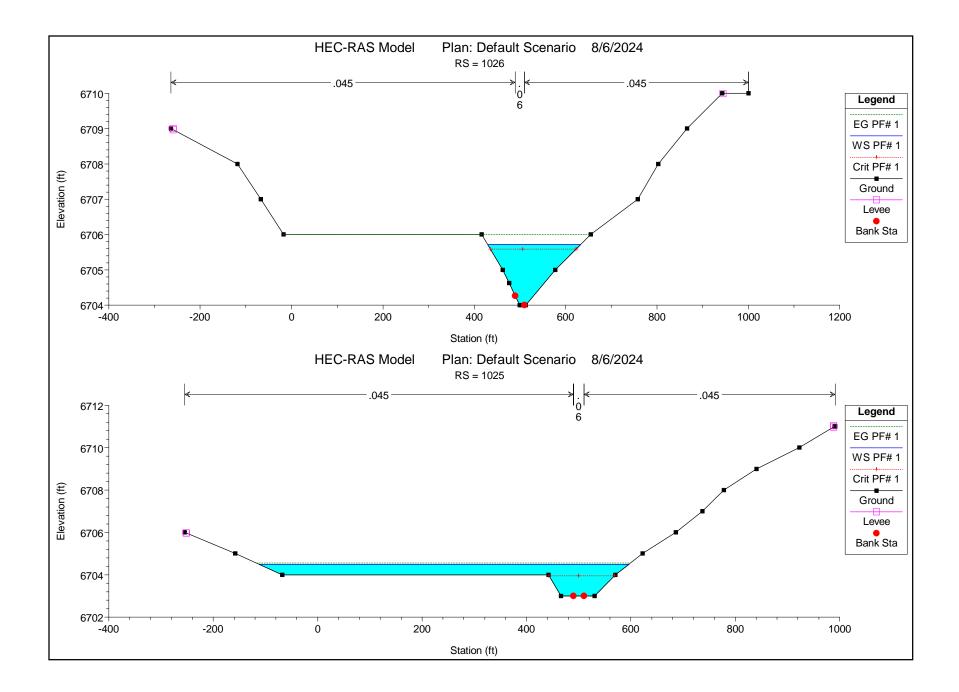
(0.00, 104.69) -(35.00, 101.19, 0.045) -(54.00, 101.00, 0.045) -(58.00, 100.00, 0.030) -(62.00, 100.00, 0.030) -(66.00, 101.00, 0.045) -(85.00, 101.19, 0.045) -(120.00, 104.69, 0.045)

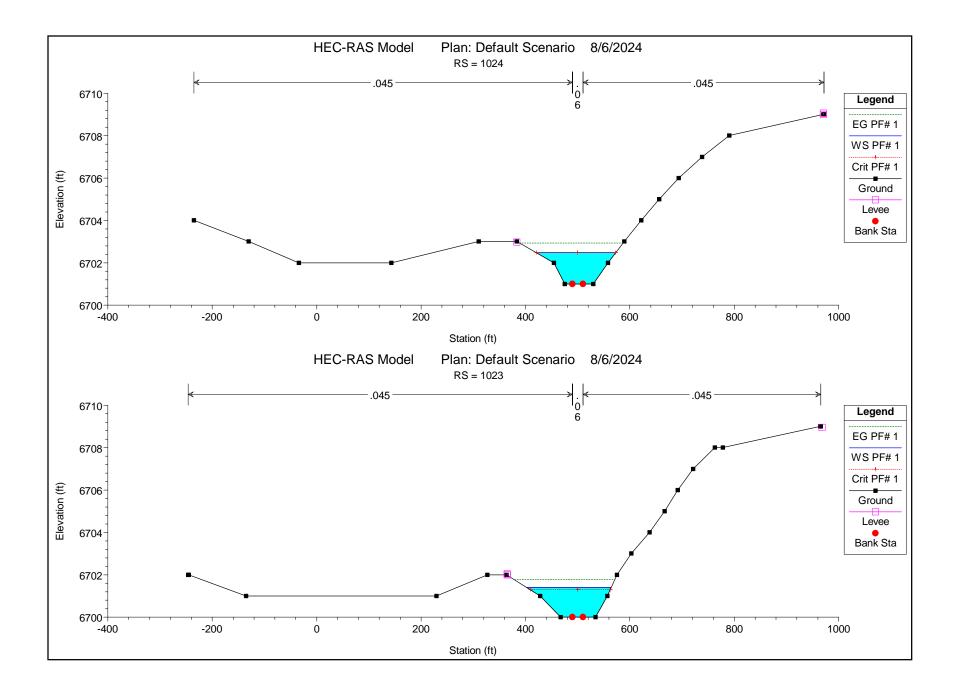


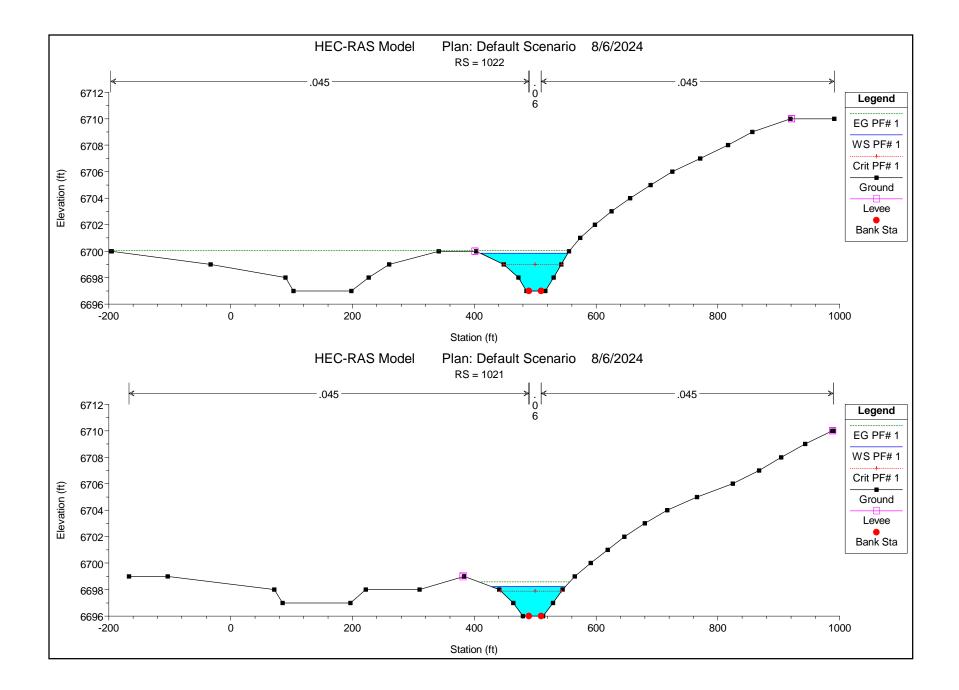
Reach	River Sta	Profile	Q Total	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope	Vel Chnl	Flow Area	Top Width	Froude # Chl	Shear LOB	Shear Chan	Shear ROB
			(cfs)	(ft)	(ft)	(ft)	(ft)	(ft/ft)	(ft/s)	(sq ft)	(ft)		(lb/sq ft)	(lb/sq ft)	(lb/sq ft)
I	1026	PF# 1	753.00	6704.00	6705.72	6705.59	6706.00	0.020598	4.97	177.96	203.77	0.68	0.88	2.13	1.08
l	1025	PF# 1	753.00	6703.00	6704.50	6703.95	6704.55	0.005174	2.33	432.84	709.10	0.34	0.17	0.48	0.29
l	1024	PF# 1	753.00	6701.00	6702.47	6702.47	6702.94	0.032142	5.74	139.51	151.91	0.83	1.45	2.95	1.92
l	1023	PF# 1	753.00	6700.00	6701.40	6701.30	6701.77	0.024287	4.82	155.74	161.56	0.72	1.25	2.12	1.56
l	1022	PF# 1	753.00	6697.00	6699.83	6699.00	6700.03	0.006406	3.97	219.11	142.26	0.42	0.46	1.13	0.66
l	1021	PF# 1	753.00	6696.00	6698.23	6697.88	6698.58	0.015583	5.28	160.05	121.76	0.62	1.07	2.17	1.15
l	1020	PF# 1	753.00	6693.00	6696.22	6695.95	6696.55	0.011829	5.74	188.49	174.71	0.57	0.66	2.30	0.59
I	1019	PF# 1	753.00	6693.00	6695.10	6694.84	6695.19	0.006470	3.27	336.52	442.89	0.40	0.27	0.85	0.32
l	1018	PF# 1	753.00	6691.00	6692.95	6692.95	6693.41	0.026496	6.29	145.17	154.78	0.79	1.75	3.22	1.00
l	1017	PF# 1	753.00	6688.00	6691.19	6690.01	6691.40	0.005345	3.92	210.92	141.17	0.39	0.29	1.06	0.70
I	1016	PF# 1	753.00	6687.00	6689.00	6689.00	6689.71	0.033645	7.22	112.38	86.21	0.90	2.30	4.21	2.27
l	1015	PF# 1	753.00	6685.00	6687.24	6686.53	6687.32	0.004092	2.71	385.06	643.91	0.32	0.33	0.57	0.08
l	1014	PF# 1	753.00	6683.00	6685.98	6685.37	6686.37	0.010382	5.23	156.44	85.93	0.53	1.40	1.93	0.75
I	1013	PF# 1	753.00	6684.54	6684.62	6684.21	6684.84	0.009447	0.29	203.77	167.20	0.25		0.02	0.73
l	1012	PF# 1	753.00	6682.62	6682.99	6682.70	6683.24	0.011975	1.18	191.74	200.70	0.39	0.08	0.22	0.89
l	1011	PF# 1	753.00	6681.00	6680.11	6680.11	6680.54	0.029771		144.69	165.59	0.00			1.62
I	1010	PF# 1	753.00	6677.00	6678.02	6678.02	6678.06	0.001549	0.99	448.08	308.00	0.17	0.06	0.10	0.15
l	1009	PF# 1	753.00	6673.00	6674.60	6675.36	6677.06	0.141052	11.55	61.29	54.72	1.73	10.11	12.19	3.53
l	1008	PF# 1	753.00	6671.00	6673.56	6673.56	6674.35	0.028897	7.71	107.89	68.76	0.86	2.34	4.47	1.76
I	1007	PF# 1	753.00	6669.00	6672.22	6670.98	6672.45	0.006132	4.23	229.63	194.15	0.42	0.27	1.23	0.84
l	1006	PF# 1	753.00	6669.00	6670.60	6670.38	6670.97	0.017857	4.53	156.63	128.96	0.63	1.01	1.78	1.41
l	1005	PF# 1	753.00	6667.00	6669.61	6668.73	6669.75	0.004229	2.85	249.61	141.45	0.33	0.25	0.62	0.46
I	1004	PF# 1	753.00	6665.00	6669.62	6666.51	6669.63	0.000190	0.93	785.78	246.70	0.08	0.04	0.05	0.04
I	1003	PF# 1	753.00	6665.00	6669.60	6666.16	6669.61	0.000142	0.82	1027.38	396.78	0.07	0.03	0.04	0.02
1	1002.7		Inl Struct												
	1002	PF# 1	753.00	6659.00	6662.27	6661.66	6662.64	0.009242	5.25	156.86	74.39	0.51	0.88	1.89	1.16
	1001	PF# 1	753.00	6658.00	6660.99	6660.13	6661.30	0.008447	4.73	171.54	88.46	0.48	0.91	1.58	0.74
	1000	PF# 1	753.00	6657.00	6659.43	6658.94	6659.72	0.013329	5.17	192.30	206.46	0.58	1.06	2.02	0.48

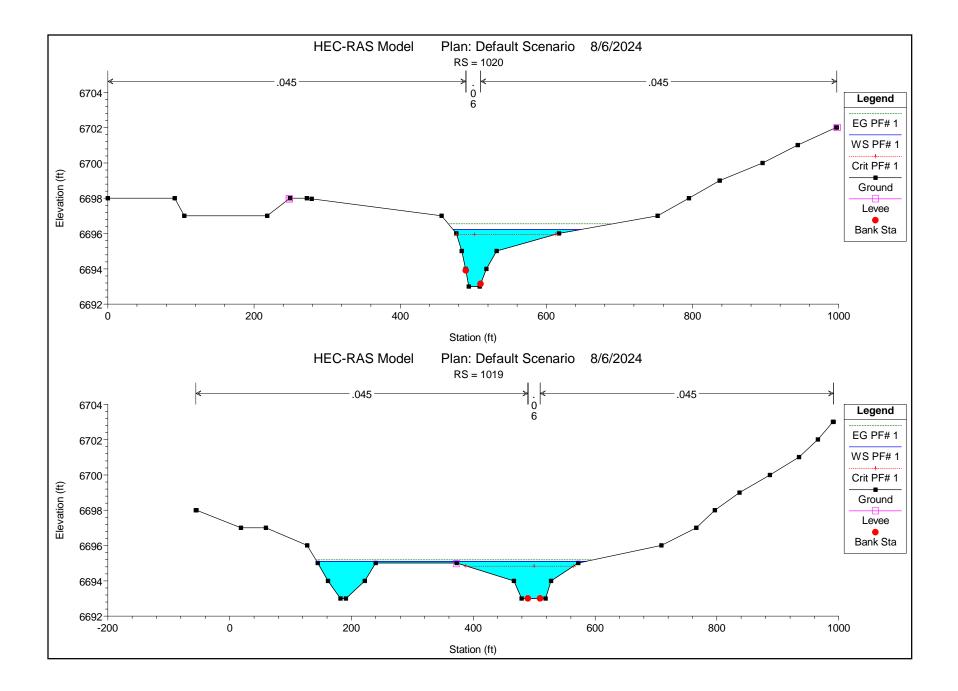
HEC-RAS Plan: Default Scenario River: Existing Channel Reach: 1 Profile: PF# 1

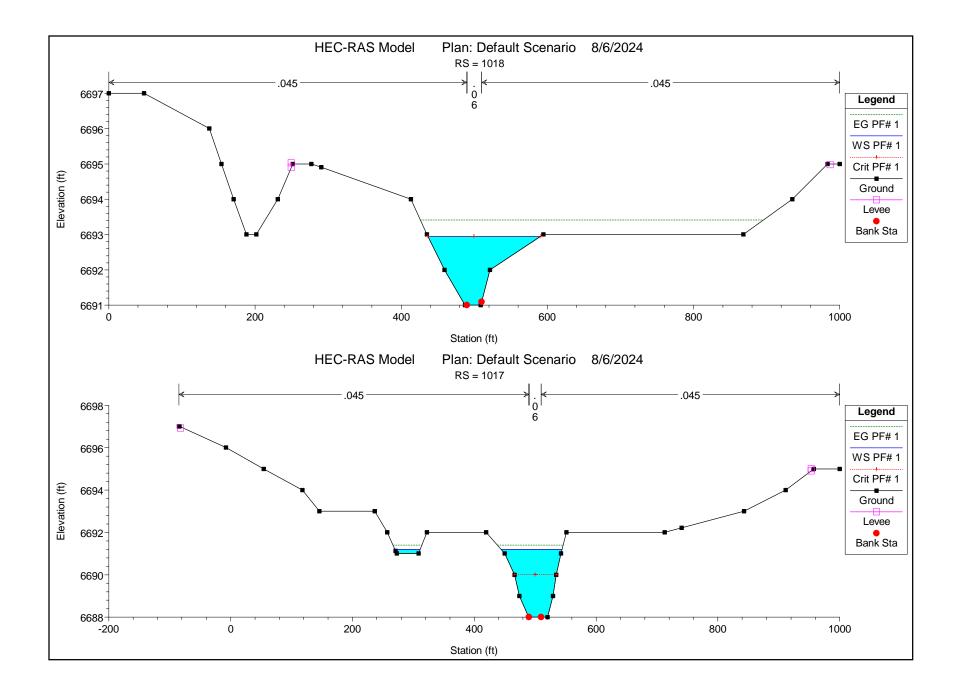


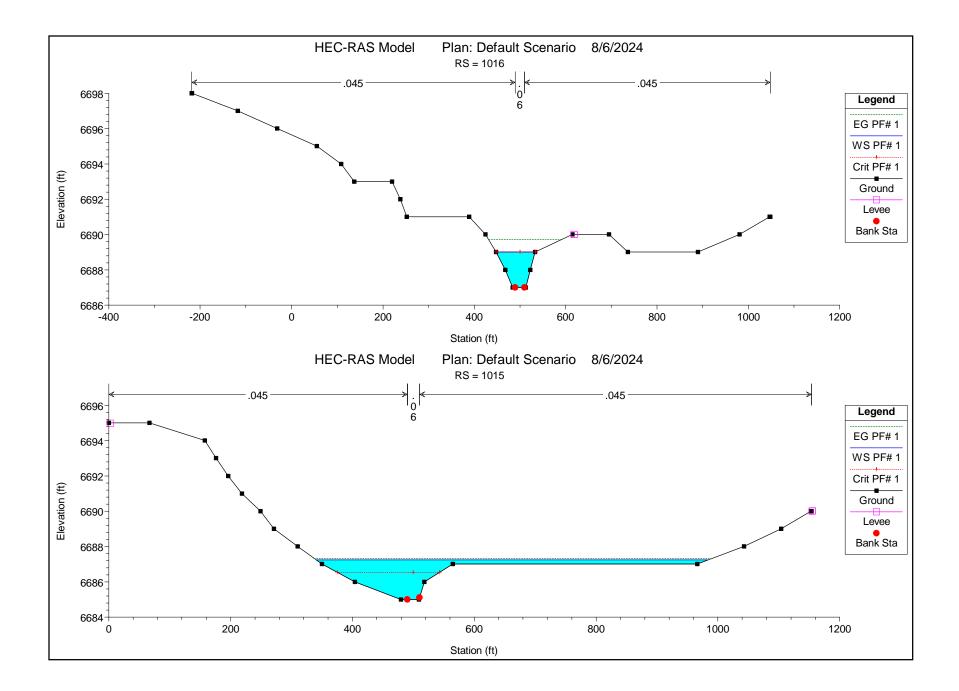


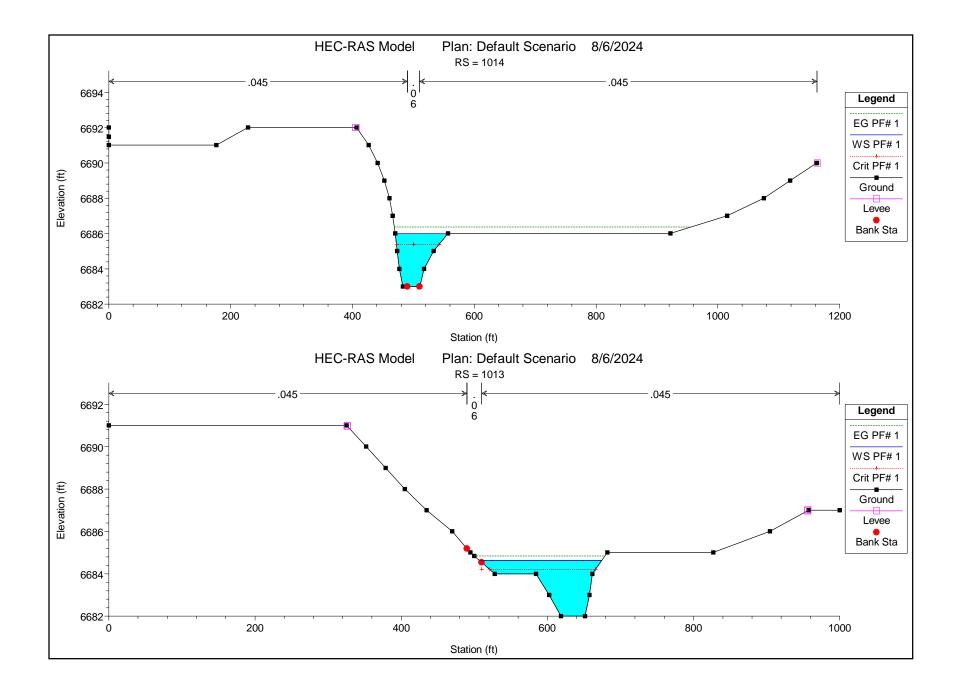


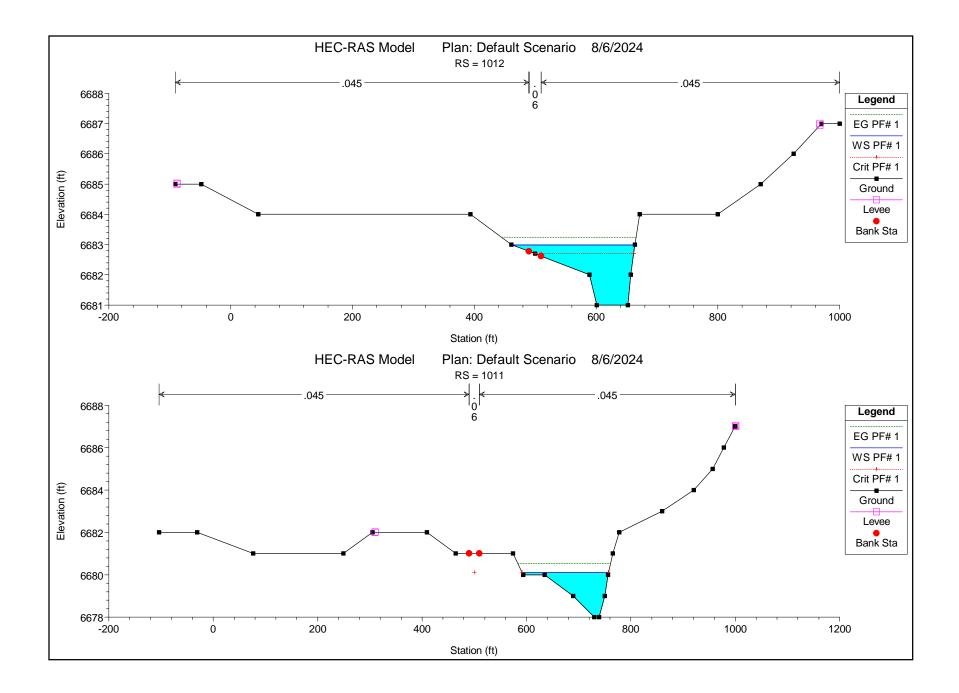


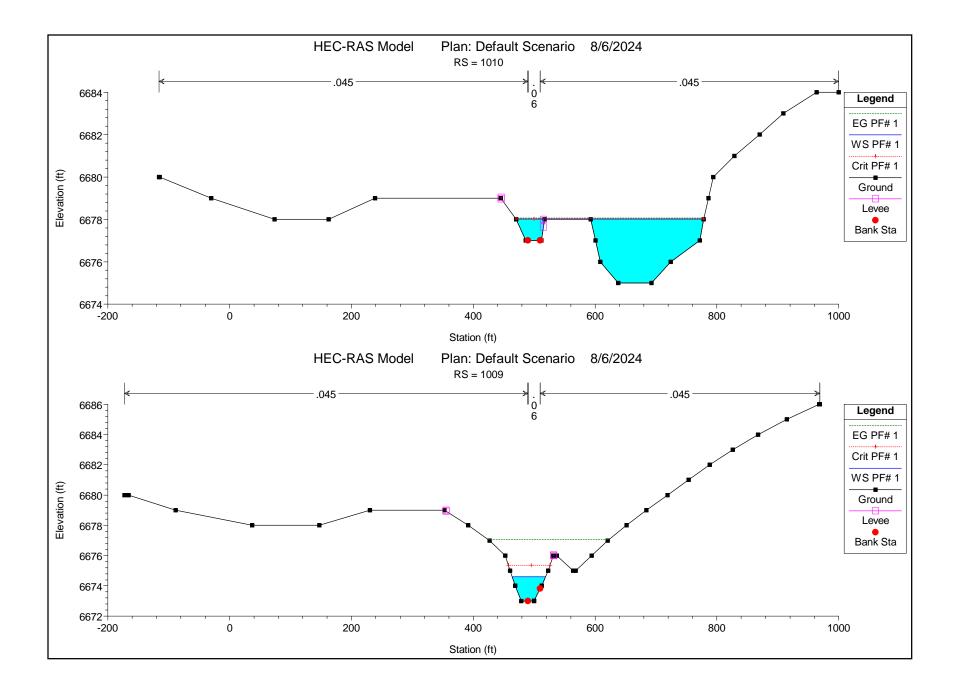


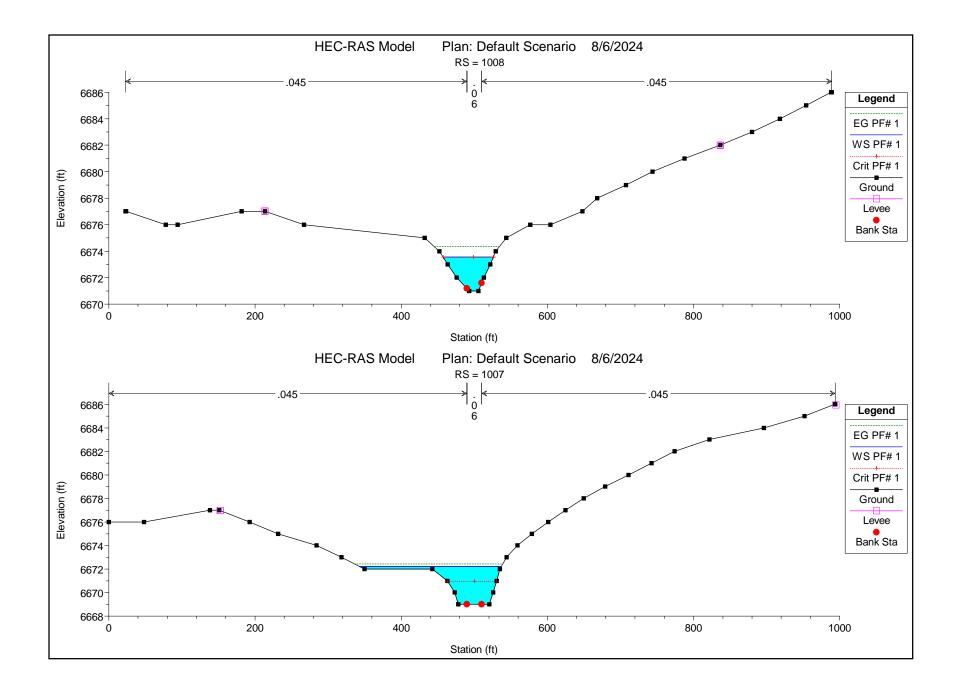


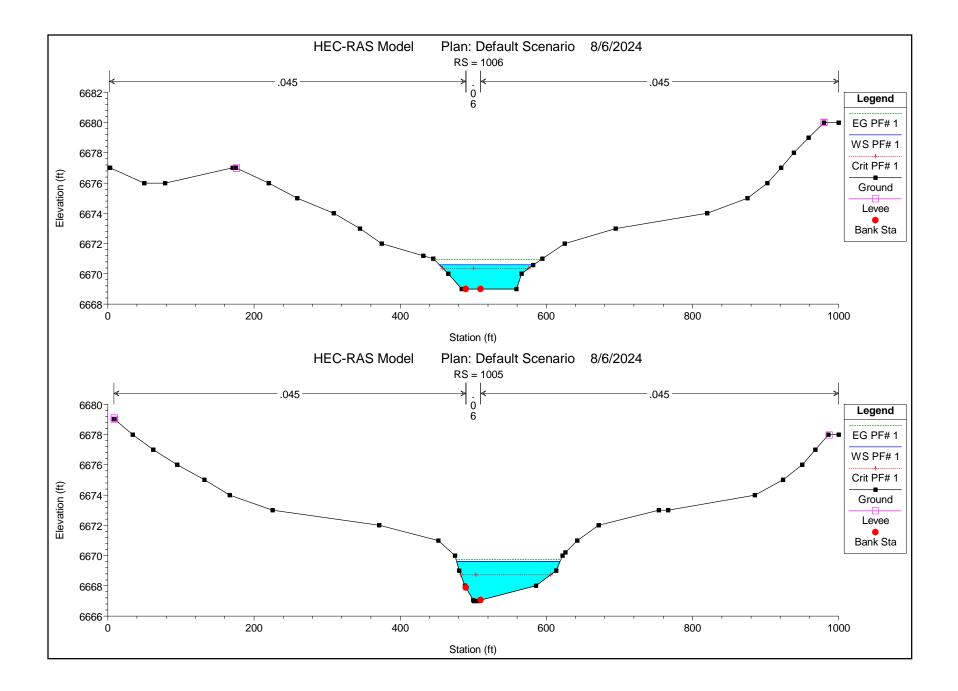


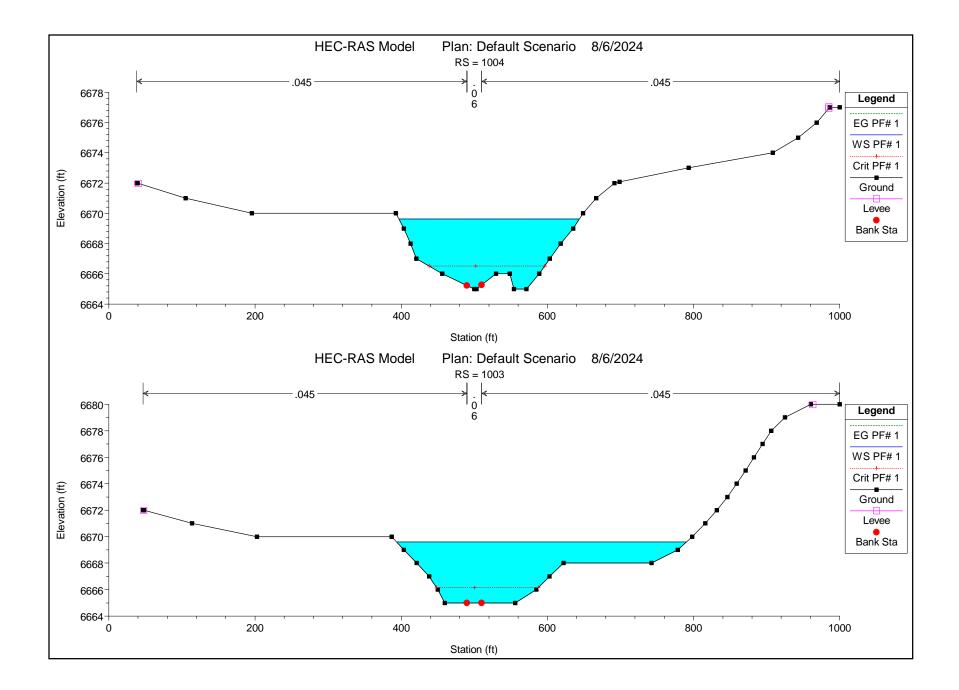


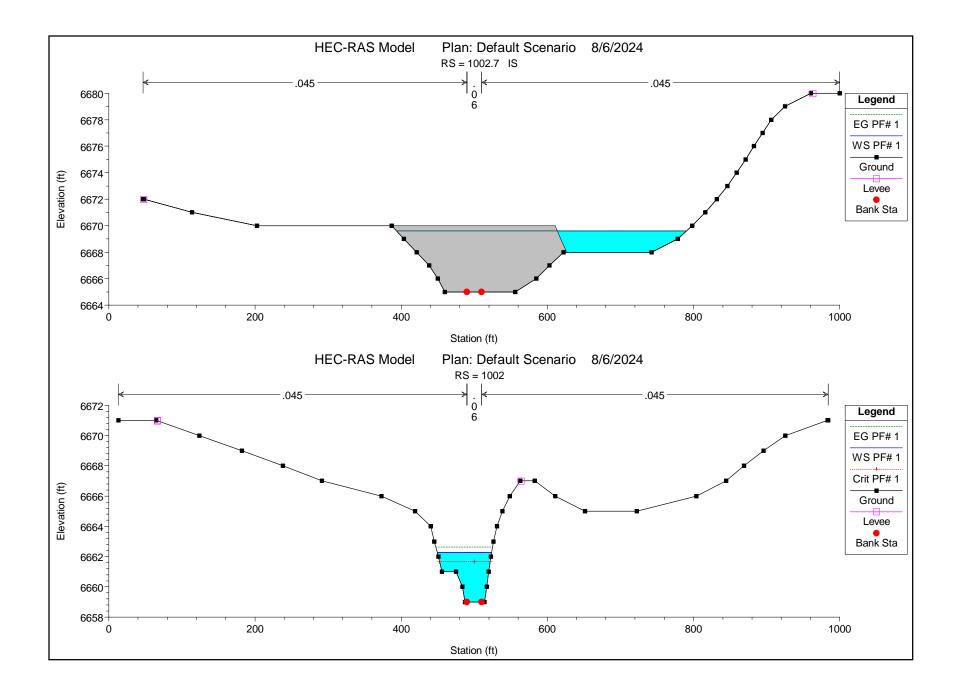


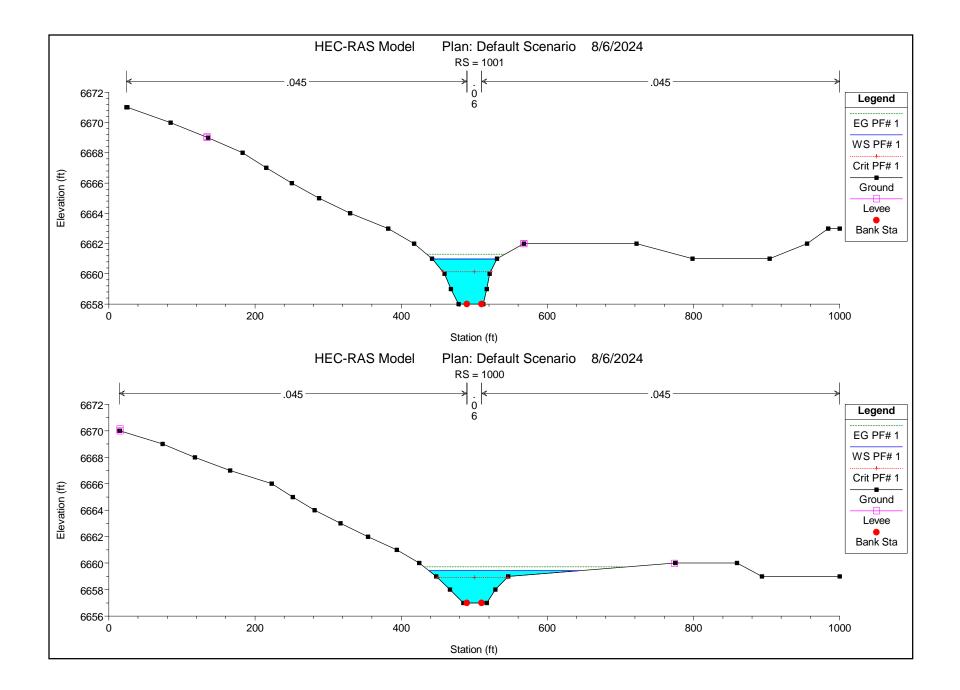


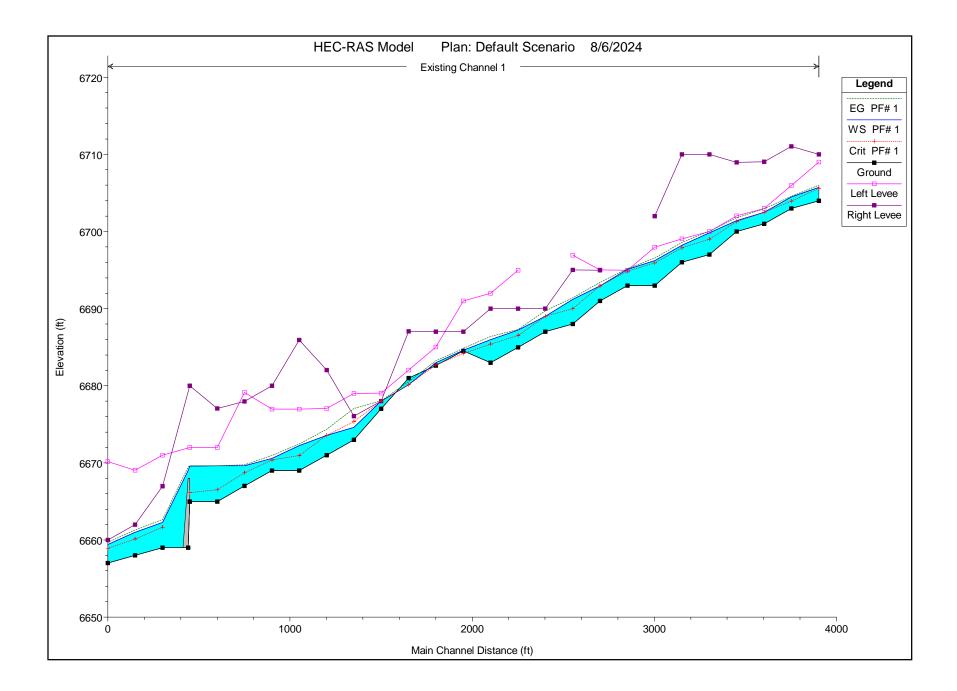






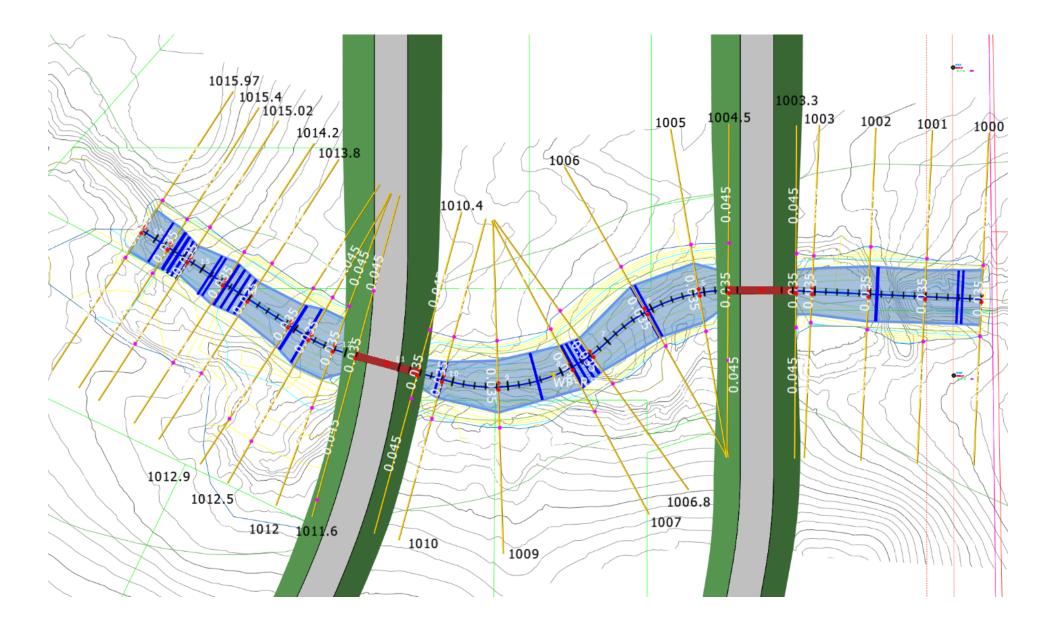


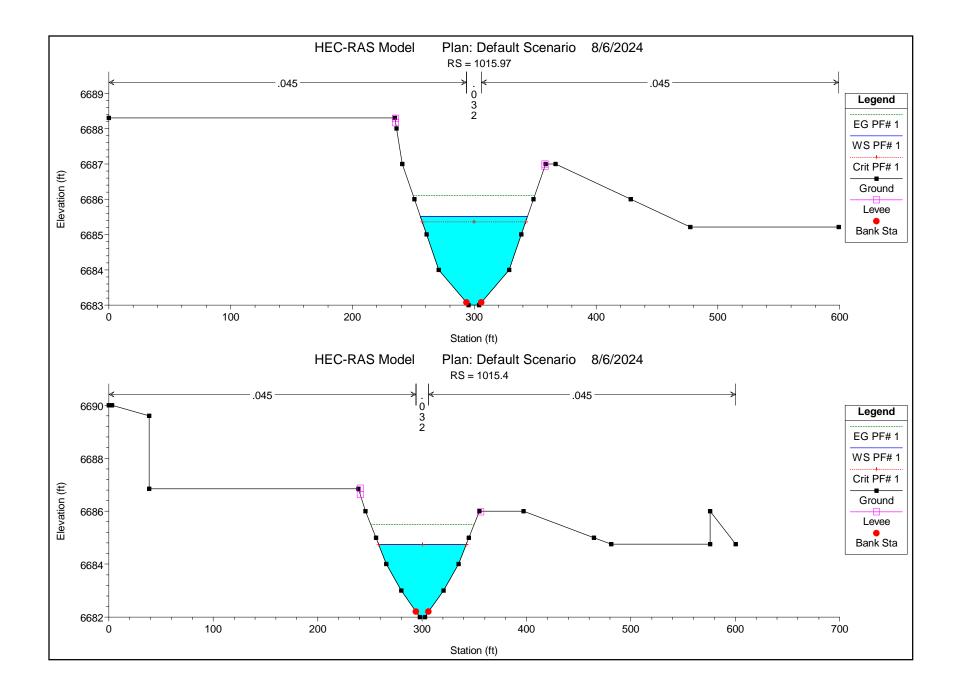


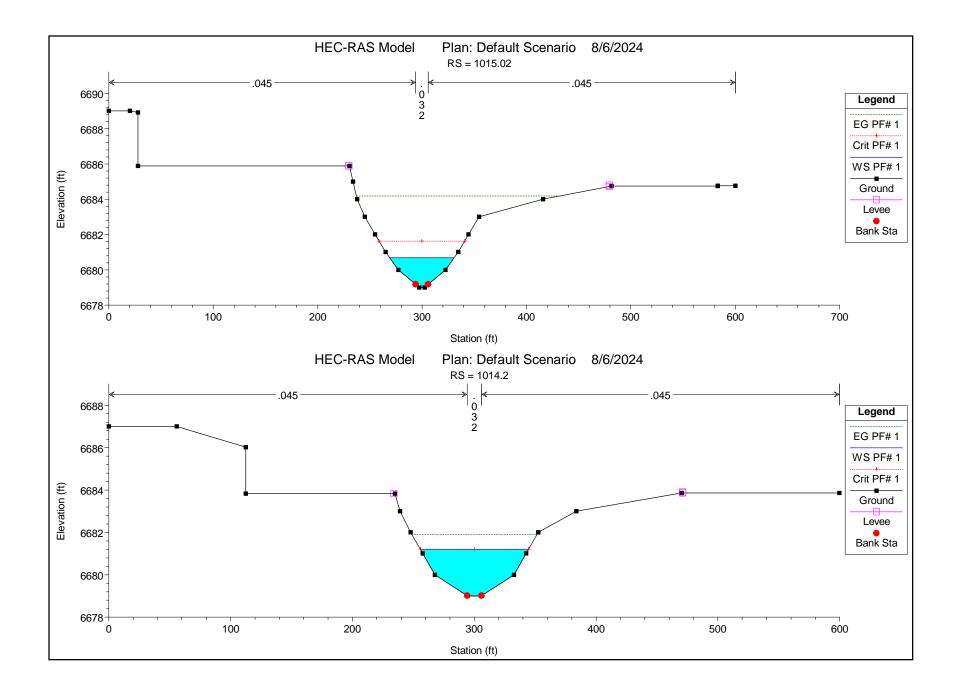


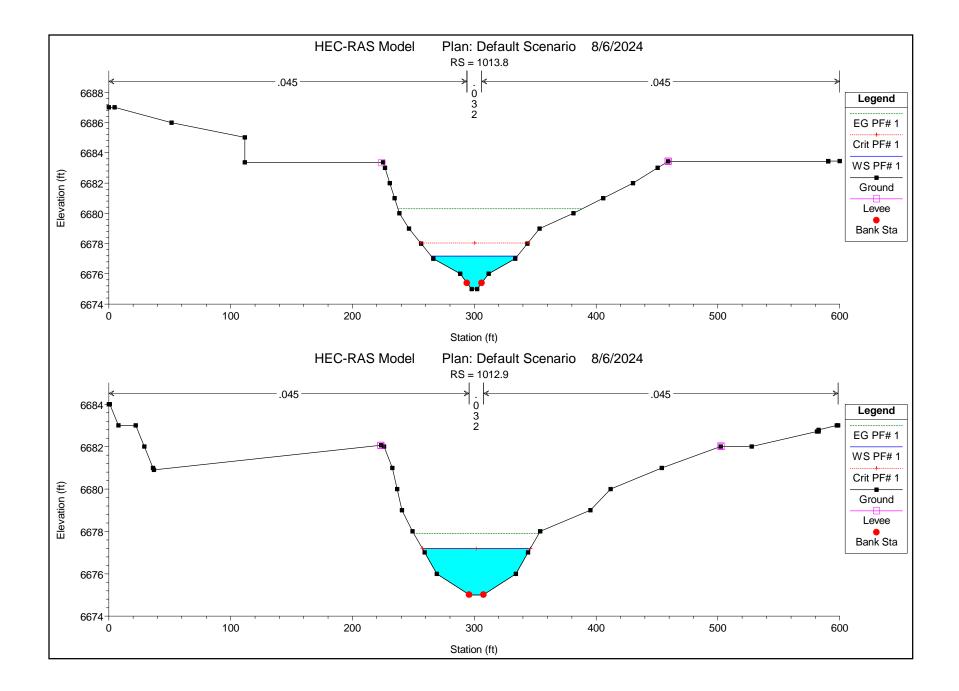
Н	EC-RAS F	Plan: Default Sce	enario River	WF-R8a	Reach: 1	Profile: I	PF# 1	

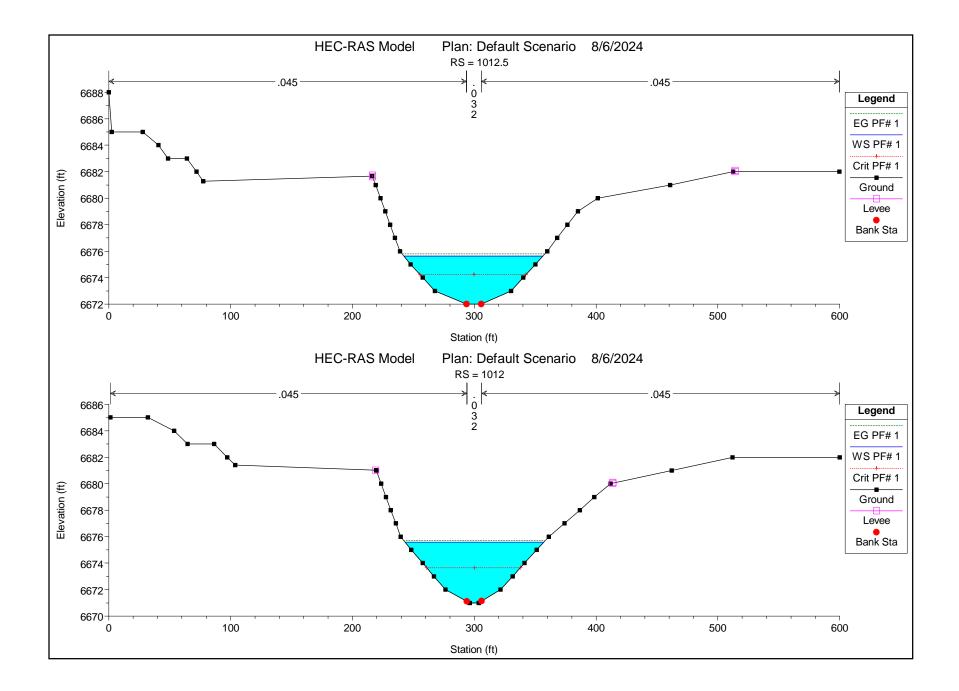
Reach	River Sta	Profile	Q Total	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope	Vel Chnl	Flow Area	Top Width	Froude # Chl	Shear LOB	Shear Chan	Shear ROB
			(cfs)	(ft)	(ft)	(ft)	(ft)	(ft/ft)	(ft/s)	(sq ft)	(ft)		(lb/sq ft)	(lb/sq ft)	(lb/sq ft)
1	1015.97	PF# 1	753.00	6683.00	6685.51	6685.35	6686.10	0.010298	8.67	143.03	87.96	0.97	0.95	1.61	0.95
1	1015.4	PF# 1	753.00	6682.00	6684.75	6684.75	6685.49	0.011127	9.46	134.27	83.93	1.02	0.98	1.87	0.98
1	1015.02	PF# 1	753.00	6679.00	6680.69	6681.63	6684.18	0.088569	19.23	62.17	61.97	2.65	4.69	9.08	4.69
1	1014.2	PF# 1	753.00	6679.00	6681.20	6681.20	6681.90	0.014473	9.45	130.18	88.72	1.12	1.22	1.99	1.22
1	1013.8	PF# 1	753.00	6675.00	6677.18	6678.05	6680.31	0.056049	17.72	71.70	70.93	2.18	2.79	7.16	2.79
1	1012.9	PF# 1	753.00	6675.00	6677.19	6677.19	6677.91	0.014796	9.52	129.15	88.48	1.13	1.24	2.02	1.24
1	1012.5	PF# 1	753.00	6672.00	6675.63	6674.23	6675.79	0.001856	4.72	270.12	114.11	0.44	0.26	0.42	0.25
1	1012	PF# 1	753.00	6671.00	6675.59	6673.64	6675.72	0.001100	4.23	312.08	113.95	0.35	0.18	0.31	0.17
1	1011.6	PF# 1	753.00	6670.15	6675.21	6673.60	6675.62	0.002228	6.46	178.01	53.10	0.51	0.41	0.70	0.36
1	1011.1		Culvert												
1	1010.4	PF# 1	753.00	6668.99	6671.29	6672.29	6674.38	0.043528	16.89	65.30	44.18	1.96	3.12	6.26	3.18
1	1010	PF# 1	753.00	6669.00	6671.32	6671.61	6672.48	0.020616	11.60	105.26	72.79	1.35	1.60	2.95	1.68
1	1009	PF# 1	753.00	6668.00	6670.81	6670.40	6671.26	0.006738	7.56	165.65	92.00	0.80	0.70	1.18	0.69
1	1007	PF# 1	753.00	6667.00	6669.23	6669.23	6669.94	0.014197	9.44	130.33	87.97	1.11	1.21	1.98	1.21
1	1006.8	PF# 1	753.00	6664.00	6665.41	6666.17	6668.39	0.101500	18.57	65.25	72.18	2.76	5.09	8.91	5.09
1	1006	PF# 1	753.00	6663.00	6665.96	6665.20	6666.24	0.004098	6.13	204.91	104.45	0.63	0.47	0.76	0.47
1	1005	PF# 1	753.00	6662.00	6665.72	6664.44	6665.92	0.002162	5.18	248.74	106.75	0.47	0.29	0.50	0.29
1	1004.5	PF# 1	753.00	6660.73	6665.36	6664.00	6665.77	0.002621	6.61	176.69	57.79	0.54	0.41	0.76	0.44
1	1004		Culvert												
1	1003.3	PF# 1	753.00	6660.12	6663.91	6663.23	6664.36	0.004159	7.28	177.09	82.85	0.66	0.49	0.98	0.47
1	1003	PF# 1	753.00	6660.00	6663.39	6663.26	6664.16	0.008748	9.36	138.19	80.78	0.92	0.79	1.73	0.79
1	1002	PF# 1	753.00	6660.00	6663.10	6662.38	6663.42	0.004289	6.45	196.20	98.93	0.65	0.49	0.83	0.49
1	1001	PF# 1	753.00	6659.00	6662.30	6662.09	6662.85	0.006822	8.22	160.79	93.05	0.82	0.64	1.34	0.64
1	1000	PF# 1	753.00	6659.00	6661.77	6661.27	6662.15	0.005981	7.06	177.26	97.85	0.75	0.64	1.03	0.61

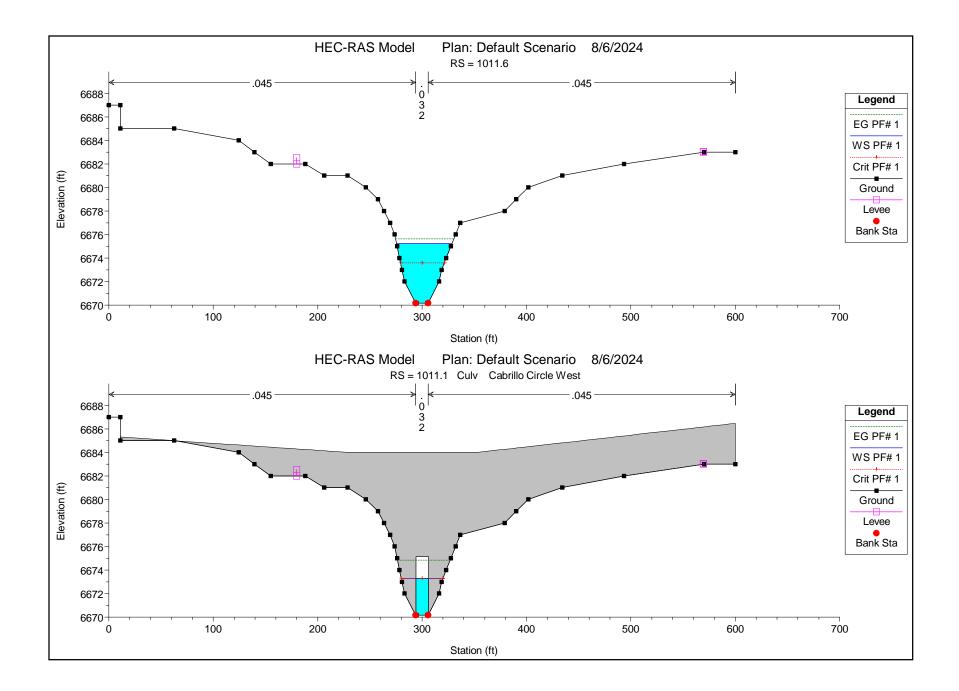


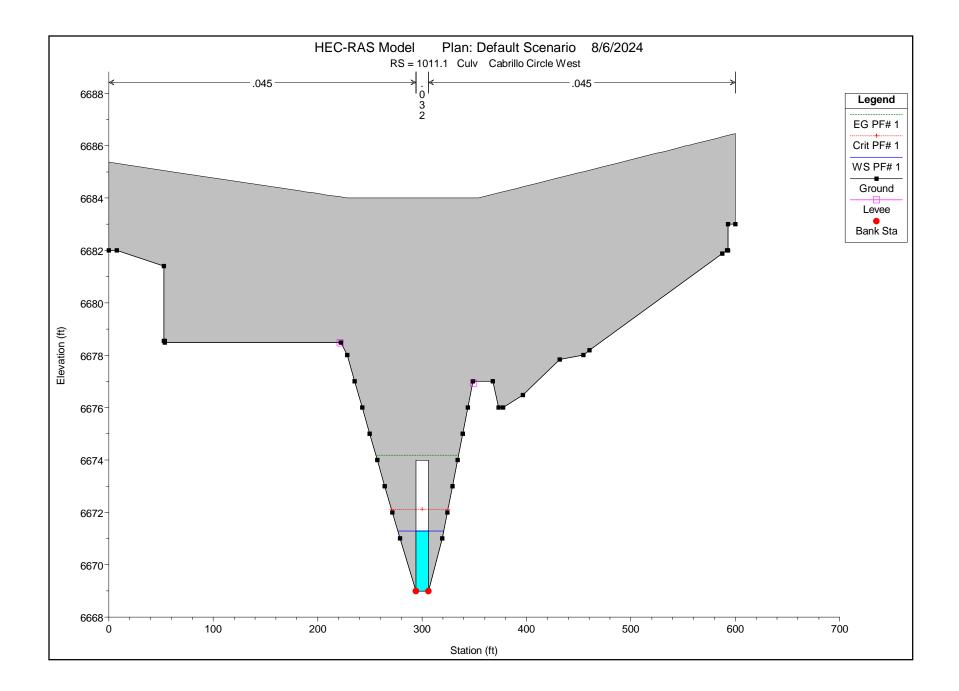


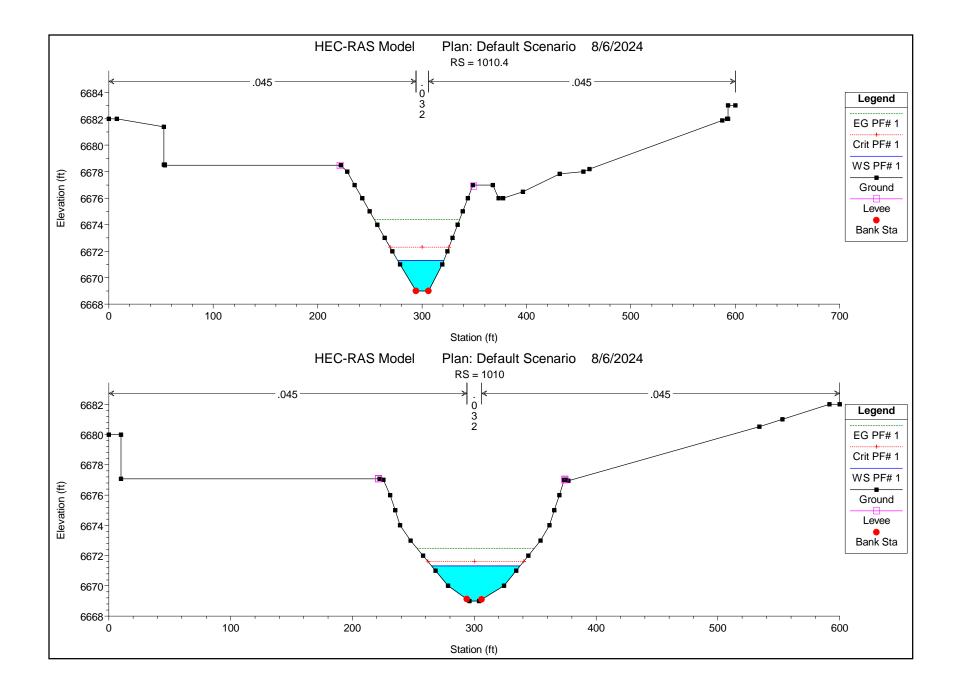


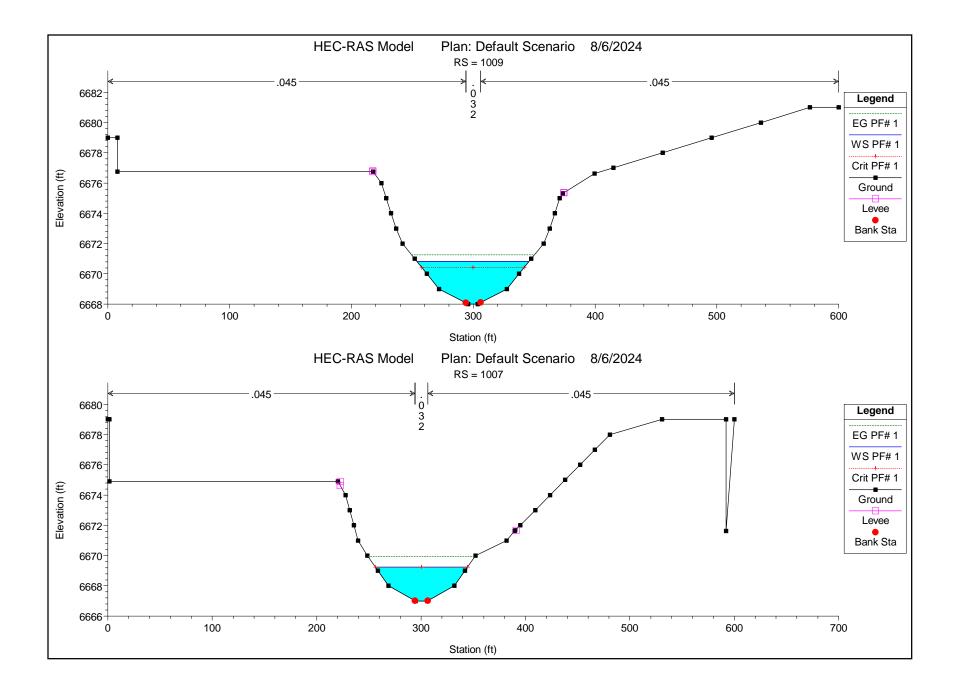


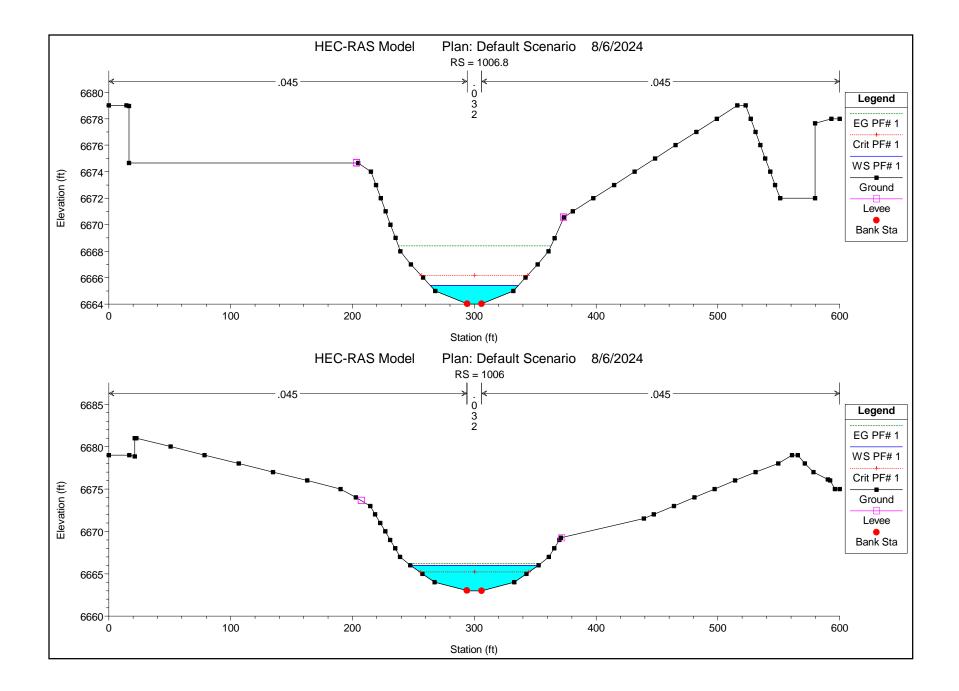


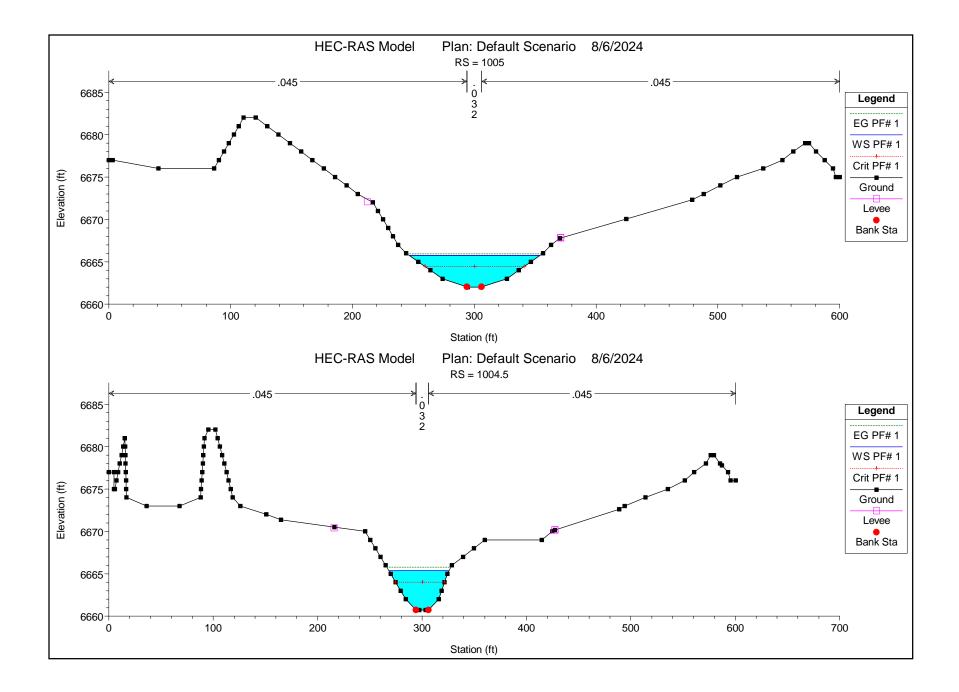


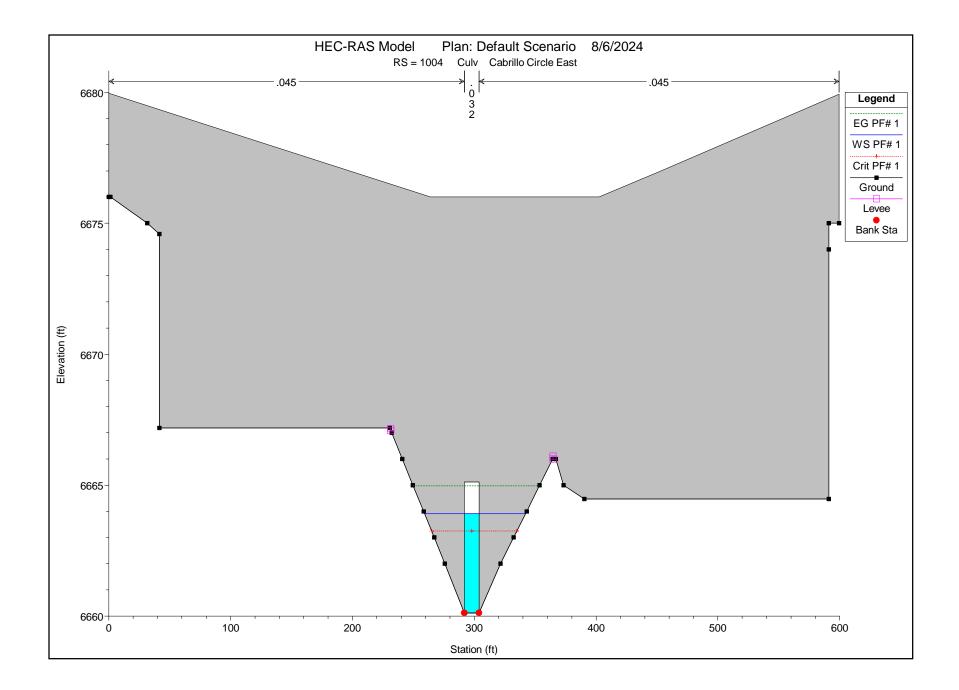


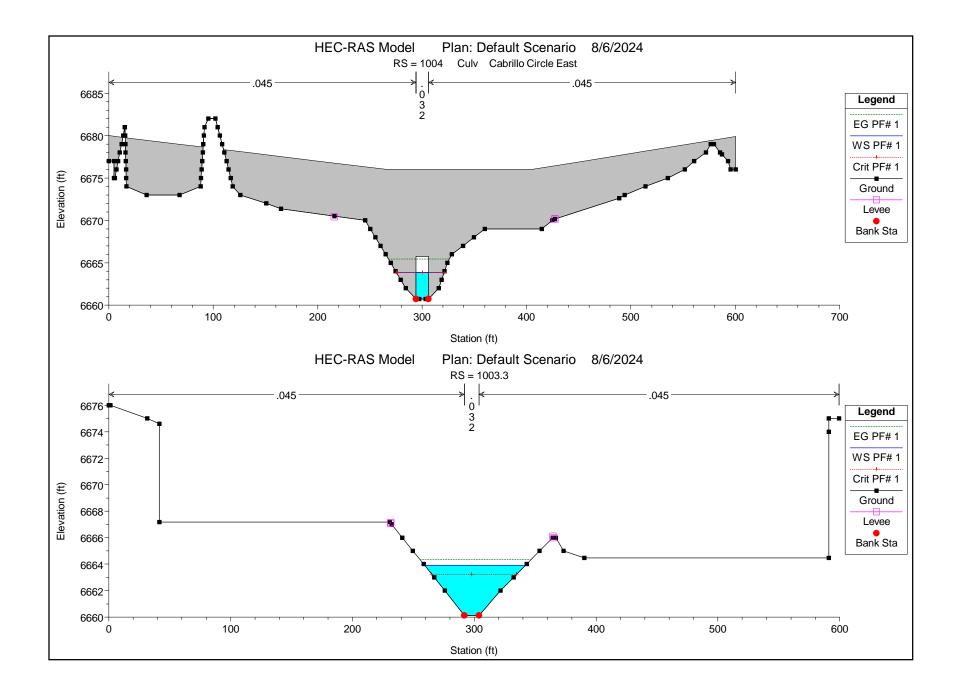


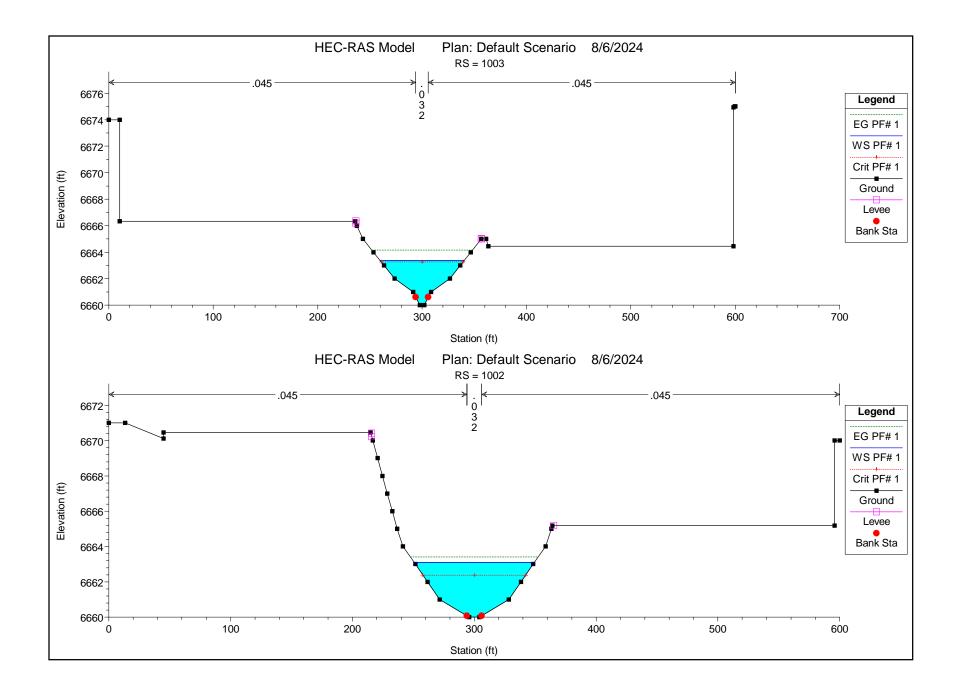


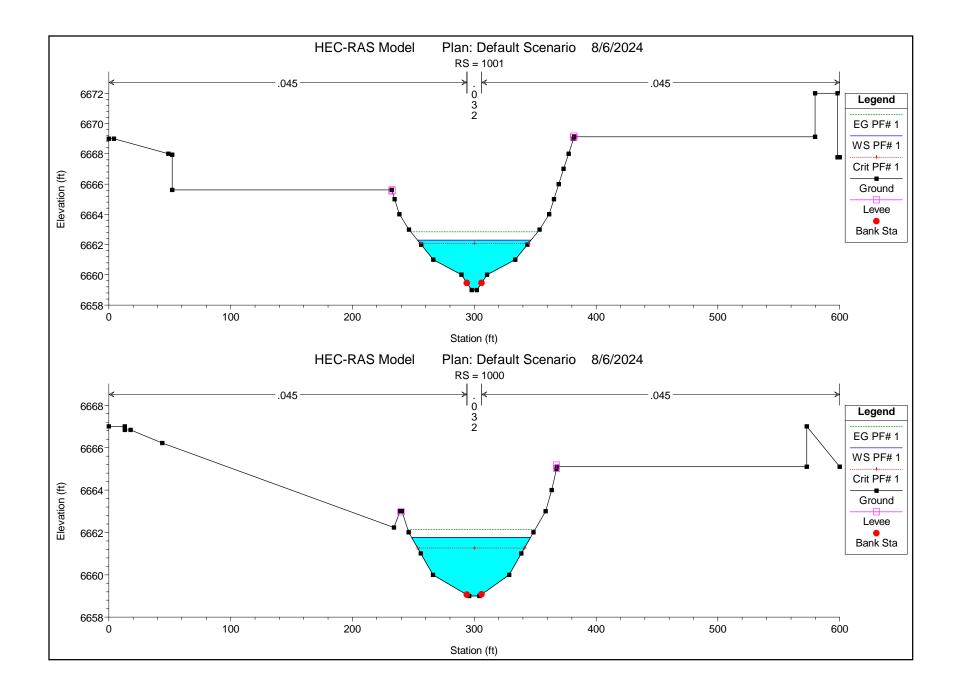


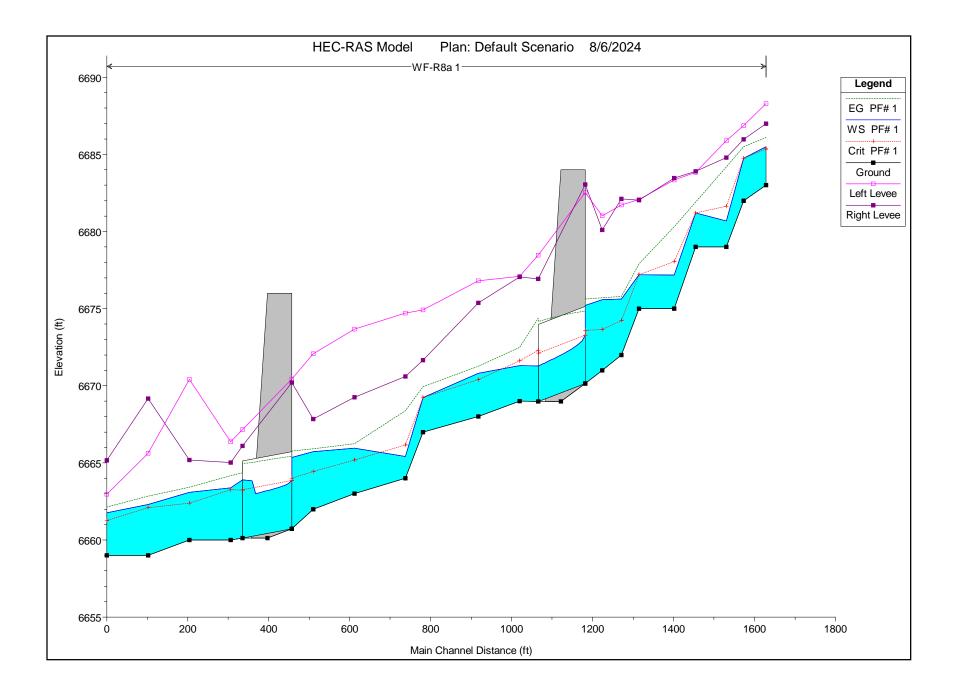












Preliminary Drainage Report for Esteban Rodriguez Subdivision

# APPENDIX D

## **REFERENCE MATERIALS**



## Wetland, Wildlife and Natural Features Report for Esteban Rodriguez Subdivision in El Paso County, Colorado

June 19, 2023

Prepared for:

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Project Number: 2022-23-1

- The Columbine gravelly sandy loam is not hydric; however, the 1% inclusion of Fluvaquentic Haplaquolls and 1% inclusion of Pleasant soils are both hydric;
- The Fluvaquentic Haplaquolls is hydric; and the 1% inclusion of Haplaquolls soil is hydric as well;
- The Truckton loamy sand, 1 to 9 percent slopes is not hydric and none of the soils types listed as inclusion are hydric;
- The Truckton sandy loam, 0 to 3 percent slopes is not hydric; however, the 2% inclusion of Pleasant soil is hydric

Hydric soils are defined by the National Technical Committee for Hydric Soils (NTCHS, 1994) as soils that formed under conditions of saturation, flooding, or ponding long enough during the growing season to develop anaerobic conditions in the upper part. Under natural conditions, these soils are either saturated or inundated long enough during the growing season to support the growth and reproduction of hydrophytic vegetation.

If soils are wet enough for a long enough period of time to be considered hydric, they should exhibit certain properties that can be easily observed in the field. These visible properties are indicators of hydric soils. The indicators used to make onsite determinations of hydric soils are specified in *Field Indicators of Hydric Soils in the United States* (USDA, NRCS, 2010).

## 3.3 Vegetation

## 3.3.1 Short- and Mixed-grass Prairie

The vegetation within the Site is primarily comprised of herbaceous short-grass prairie species with herbaceous wetland vegetation in the drainages and ephemeral swales flowing through the Site. Given the presence of certain midgrass prairie species mixed throughout the shortgrass prairie, we have referred to the vegetation community as "short- and mixed-grass prairie" (refer to Figure 4, Vegetation Community Map). The dominant prairie grass species is blue grama (Bouteloua gracilis), with occasional little bluestem (Schizachyrium scoparium) and Western wheatgrass (Pascopyrum smithii). The other most common associative prairie species are prairie aster (Machaeranthera tenacetifolia), smooth brome (Bromus inermis), fringed sage (Artemisia frigida), yucca (Yucca spp.) and prickly pear cactus (Opuntia sp.). Other species include Wood's rose (Rosa woodsii), false indigo bush (Amorpha fruticosa), sticky geranium (Geranium viscosissimum) and yarrow (Achillea millefolium). The Site is moderately grazed and there are scattered weeds, including Canada thistle (Cirsium arvense), musk thistle (Carduus nutans), Scotch thistle (Onopordum acanthium), common mullein (Verbascum thapsus), horseweed (Conyza canadensis) and field bindweed (Convolvulus arvensis).

### 3.3.2 Hydrophytic Vegetation

Discontinuous patches of hydrophytic vegetation (wetland vegetation) is present within the North-central ephemeral drainage where saturated (hydric) soils are present. Dominant wetland vegetation includes Nebraska sedge (*Carex* 

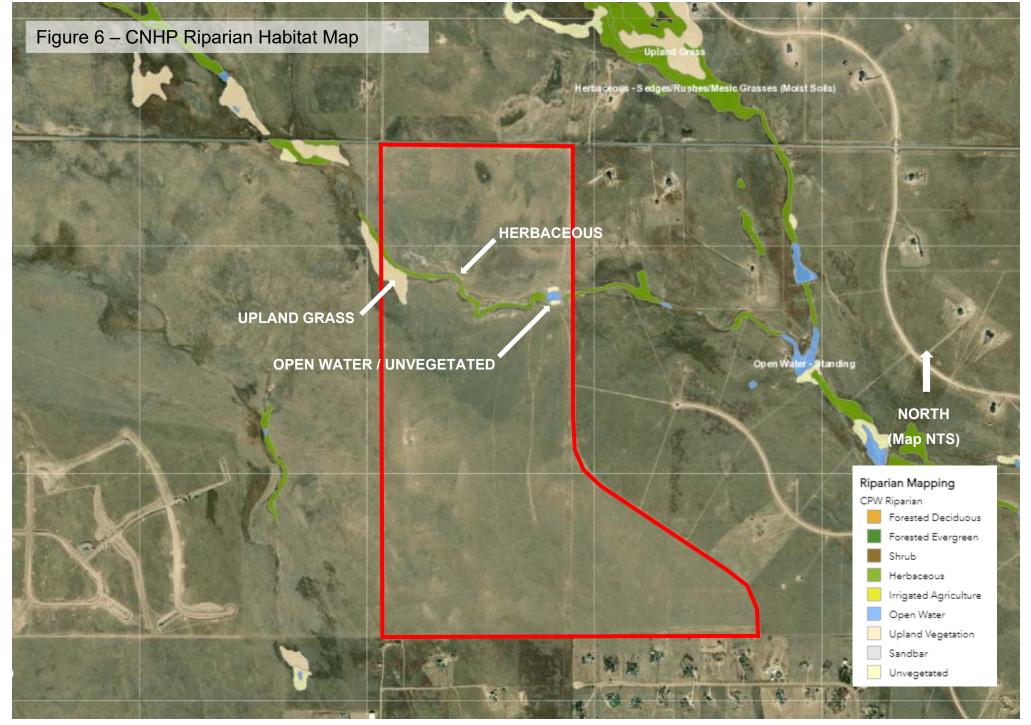
*nebrascensis*), common threesquare bulrush (*Schoenoplectus americanus*) and spikerush (*Eleocharis palustris*) with inclusions of Baltic rush (*Juncus balticus*), water mint (*Mentha aquatica*), narrowleaf cattail (*Typha angustifolia*) and Canada thistle (*Cirsium arvense*). Willow is notably absent. Dominant upland vegetation at the margin of the wetland boundary includes little bluestem and blue grama (*Bouteloua gracilis*), upland grasses, fringed sage and other miscellaneous upland weeds.

### 3.3.2 Riparian Vegetation

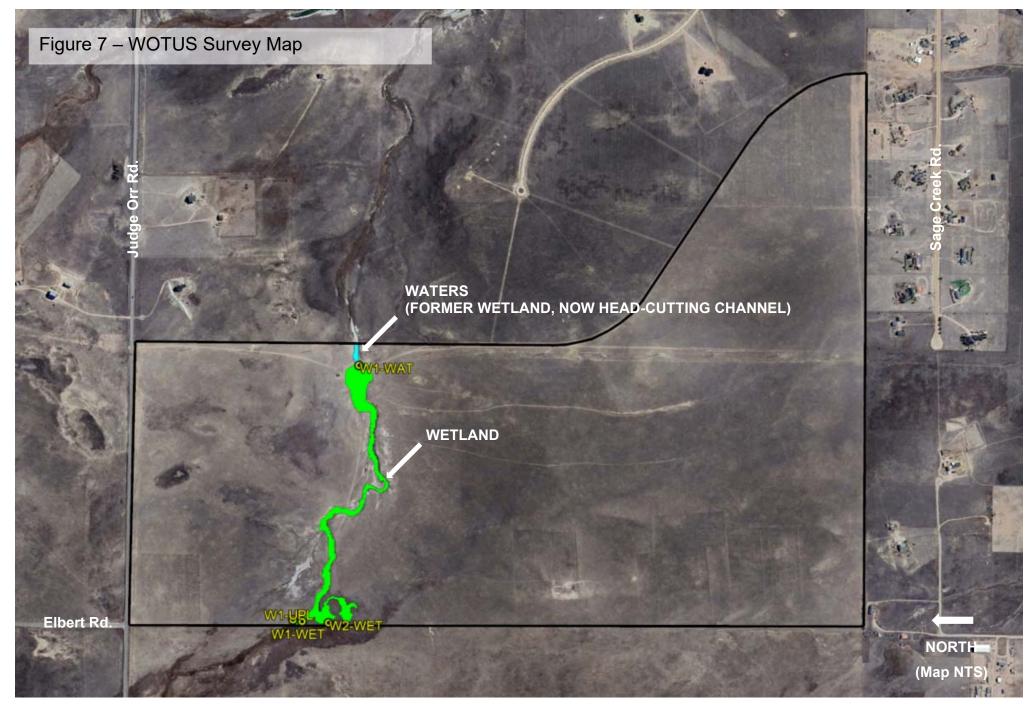
Riparian habitat within the Site is limited to one singe drainage in the Northcentral portion of the Site which consists of more robust short-grass prairie where moist, mesic soils are present adjacent to wetlands (described above). This North-central drainage does not support any riparian trees or shrubs.



Source: Google Earth Aerial Image, 10/31/2022 & Ecosystem Services, LLC Site Assessment, 5/23/2023



Source: Colorado Natural Heritage Program (CNHP) Wetland Mapper



Source: Google Earth Aerial Image, 10/31/2023 & Ecosystem Services, LLC Wetland Delineation, 5/23/2023

#### 3.5 Wildlife

The stated purpose and intent of the "El Paso County Development Standards" wildlife section is to ensure that proposed development is reviewed with consideration of the impacts to wildlife and wildlife habitat, and to implement the provisions of the Master Plan (El Paso County, 2021). The two primary vegetation types within the Site are herbaceous prairie and wetlands. ECOS has determined that the wildlife impact potential for development of this stand-alone Site is expected to be moderate to low, as the Site currently provides poor to moderate habitat for wildlife. Taken in a regional, watershed or larger landscape context, as more and more prairie is developed over time impacts to wildlife are expected to be moderate to high as wildlife run out of space and habitat.

The Site provides habitat for prairie species such as pronghorn (*Antilocapra americana*), black-tailed prairie dog (*Cynomys ludovicianus*), thirteen-lined ground squirrel (*Ictidomys tridecemlineatus*), voles (*Microtus spp.*) and jackrabbit (*Lepus townsendii*). The Site also provides foraging and breeding habitat for predators such as coyote and fox. The Site also provides good habitat for reptiles and moderate habitat for amphibians such as Woodhouse toad (*Anaxyrus woodhousii*).

The USFWS IPaC Trust Resources Report (USFWS, 2023a) (Appendix B) reports that bald eagle (*Haliaeetus leucocephalus*), golden eagle (*Aquila chrysaetos*) and ferruginous hawk (*Buteo regalis*) may utilize the area. The Site provides limited tree nesting habitat for raptors; however, ferruginous hawks may also use ground nests.

The Site contains no Critical Habitat, Wildlife Refuges or Hatcheries according to the USFWS IPaC Trust Resources Report (USFWS, 2023a) (Appendix B).

The project proposes to develop most of the prairie; however, the drainages and immediately adjacent prairie would be preserved as Open Space. A noxious weed management plan will be implemented per State and County requirements to improve wildlife habitat; and a native plant re-vegetation plan for the Open Space is recommended to provide additional benefit to wildlife habitat.

#### 4.0 FEDERAL LISTED SPECIES

A number of species that occur in El Paso County are listed as threatened and endangered (T&E) by the USFWS under the Endangered Species Act (ESA) (USFWS 2023). ECOS compiled the data regarding T&E species for the Site in Table 3 based on the Site-specific, USFWS IPaC Trust Resources Report we ran for the Project (Appendix B) and our onsite assessment. ECOS has provided our professional opinion regarding the probability that these species may occur within the Site and their probability of being impacted by the Project.

The likelihood that the Project would impact any of the species listed below is insignificant to none. Most are not expected occur in the project area and no downstream impacts are expected. The USFWS also states that there is no Critical Habitat for T&E species in the Site locations.

TABLE 3 - FEDERAL LISTED SPECIES POTENTIALLY IMPACTED BY THE PROJECT									
Species	Status	Habitat Requirements and Presence	Probability of Impact by Project						
FISH									
Greenback cutthroat trout ( <i>Oncorhynchus</i> <i>clarki stomias</i> )	Threatened	Cold, clear, gravely headwater streams and mountain lakes that provide an abundant food supply of insects.	None. Suitable habitat does not exist on the Site.						
Pallid sturgeon (Scaphirhynchus albus)	Endangered	Water-related activities/use in the N. Platte, S. Platte and Laramie River Basins may affect listed species in Nebraska.	None. The proposed project will not affect any of the listed river basins.						
BIRDS									

### 5.0 RAPTORS AND MIGRATORY BIRDS

Raptors and most birds are protected by the Colorado Nongame Wildlife Regulations, as well as by the federal Migratory Bird Treaty Act. Additionally, eagles are protected by the Bald and Golden Eagle Protection Act (BGEPA).

### 5.1 COGCC Database

ECOS utilized the Colorado Oil and Gas Conservation Commissions (COGCC) GIS Online data (https://cogccmap.state.co.us/cogcc\_gis\_online/) (COGCC, 2023) to screen the Site for potential raptor nests. No raptor nests have been mapped within one mile of the Site (COGCC, 202). The closest raptor nests to the Site are one Golden Eagle active nest and one Ferruginous Hawk active nest, both of which are located 2.39 miles east/northeast of the eastern edge of the Site.

### 5.2 USFWS IPaC Data

The USFWS IPaC data for the Site indicates the probability of presence of the four bird species (refer to Appendix B) in the vicinity of the Site. The birds listed by IPaC are birds of particular concern either because they occur on the USFWS Birds of Conservation Concern (BCC) list or warrant special attention in the Project location. The 1988 amendment to the Fish and Wildlife Conservation Act mandates the USFWS to "identify species, subspecies, and populations of all migratory nongame birds that, without additional conservation actions, are likely to become candidates for listing under the ESA. "Birds of Conservation Concern 2021 (BCC 2021)" is the most recent effort to carry out this mandate. The birds listed by IPaC include:

- Bald Eagle (*Haliaeetus leucocephalus*) This is not a BCC but is vulnerable and warrants attention because of the BGEPA.
- Ferruginous Hawk (*Buteo regalis*) This is a BCC only in particular Bird Conservation Regions (BCRs) including Colorado. Per the USFWS Environmental Conservation Online System data (USFWS 2022b) (<u>https://ecos.fws.gov/ecp/species/6038</u>), ideal habitat for Ferruginous Hawks is grassland and shrub-steppe habitat including pastures, hayland and cropland. Their nests can be found in trees and large shrubs and on roofs, utility structures and artificial platforms, or near the ground on river cutbanks, or less frequently other ground locations such as rockpiles and riverbed mounds. ECOS has observed their nests open prairie habitat in this vicinity.
- Long-eared Owl (*Asio otus*) This is a BCC throughout its range in the continental USA and Alaska. Per the USFWS Per the Nature Serve Explorer database (Nature Serve 2022)

   (<u>https://explorer.natureserve.org/Taxon/ELEMENT\_GLOBAL.2.101120/Asi</u> o otus) this species habitat is deciduous and evergreen forests, orchards, wooded parks, farm woodlots, river woods, desert oases. Wooded areas with dense vegetation needed for roosting and nesting, open areas for hunting; therefore, it is often associated with deciduous woods near water

in West. The Site does not comprise suitable habitat for roosting and nesting for this species but may provide hunting opportunities. However, the probability of presence in the Project vicinity is limited to the 2<sup>nd</sup> week of May.

### 5.3 Field Assessment

The prairie, riparian corridors and wetland habitat provides ground-nesting and foraging habitat for migratory birds such as western meadowlark (*Sturnella neglecta*). No existing nest sites or prairie dog burrows for raptors, including burrowing owl were found during the Site visit.

### 6.0 SUMMARY OF IMPACTS

### 6.1 Vegetation

The vegetation within the Site is primarily comprised of herbaceous shortgrass prairie species. Given the presence of certain tallgrass prairie and non-native species mixed throughout the shortgrass prairie, we have referred to the vegetation community as "short- and mixed-grass prairie". Wetland vegetation is comprised primarily of emergent, herbaceous, hydrophytic species in the ephemeral drainages and swales. Riparian habitat within the Site is comprised of upland grassland, herbaceous wetland species with small pockets of shallow open water. Refer to Figure 6, CNHP Riparian Habitat Map. Trees and shrubs are primarily absent. Refer to Figure 4, Vegetation Community Map.

The short and mixed grass prairie will be the primary vegetation/habitat type impacted by the proposed development. The proposed residential parcels are all planned to be low-density. Tthat should provide ample opportunity to preserve high guality, native habitat within private lots if building envelopes/disturbance footprints are limited. Parcel J, the only park proposed, will have no value for wildlife if isolated within a sea of housing and if completely developed for tot-lots, field sports, etc. If, however, it were to be located adjacent to the North-Central drainage floodplain and some portions of it were preserved as native habitat, this park would provide open space functions for wildlife and feel more expansive. The proposed Commercial parcels and the internal road system will have a maximum impact on short and mixed grass prairie (e.g., 100% of area beneath their footprint). The three Detention Ponds will result in the loss/impact primarily of short and mixed grass prairie. The Parcel E Detention Pond stormwater outfall will likely cause minor impacts to wetland habitat where it feeds into the North-Central drainage. Detention Pond impacts could be temporary and mitigated if prairie, riparian and wetland habitat are restored after construction.

In addition to preserving the highest value existing native vegetation on public and private open space, in order to reduce overall direct impacts from the development, proposed landscaping (private and public) should consist of native species from the same ecosystem that provide food and cover for wildlife. High, solid fences if proposed are a major impediment and impact wildlife movement through the landscape. Short, wildlife friendly fences that allow large and small species to move freely are recommended wherever fences are desired which will allow future residents to enjoy wildlife experiences in their everyday lives.

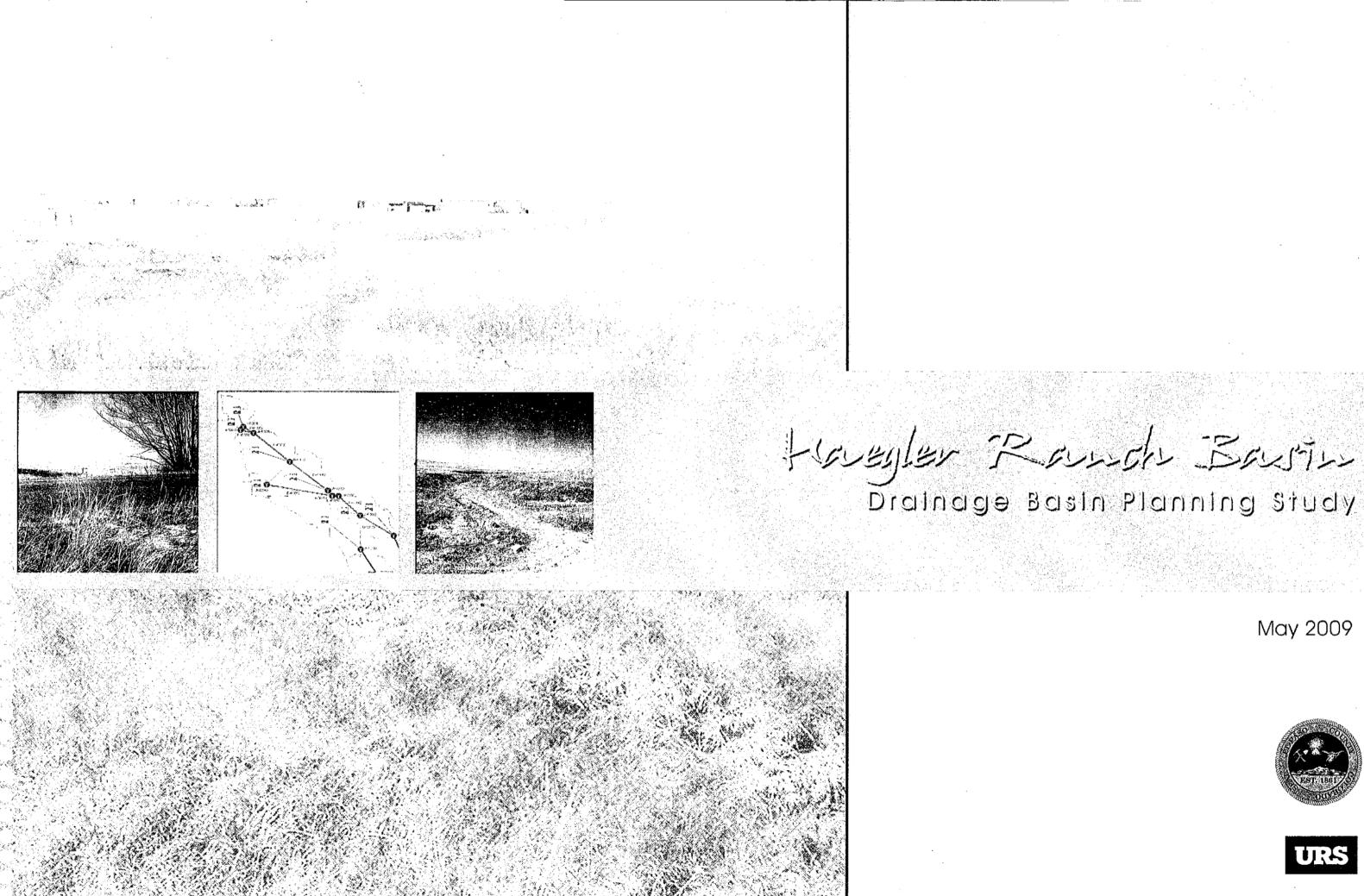
Over 80 percent of all wildlife species use riparian areas during some part of their life cycle. As such, floodplains, riparian areas including wetlands that together form linear natural corridors (i.e., greenways) should not be impacted by development and left intact. If necessary, road, trail and utility corridors (i.e., crossings) that must cut through riparian areas should be avoided or minimized to only a few locations where the riparian corridor are the narrowest and wetlands are absent. Any proposed crossings should be designed perpendicular to greenways. Greenways are ideal locations for trails that run parallel with the floodplain/riparian corridor to provide future neighborhood residents with positive natural outdoor and wildlife experiences such as bird watching (i.e., ecological benefits). The layout of the development at a sketch plan level is nebulous regarding the avoidance and minimization of impacts to greenways. During more detailed preliminary and final design, all man-made structures, including detention ponds should avoid impacting riparian areas and wetlands.

The creek channel at the downstream, eastern most end of the North-Central drainage below the stock pond was previously a wet swale. This portion of the creek is head-cutting severely, a result of recent large rainfall events. This headcut is about to completely breach and drain the stock pond and start migrating up the channel. This headcut, if left unaddressed, will completely degrade this valuable aquatic/open space resource, including all abutting wetlands and should be stabilized immediately.

Detention/water quality ponds, where required should be located adjacent to riparian areas and vegetated to the maximum extent possible utilizing native riparian and wetland vegetation in the pond bottoms; upland grasses, shrubs and trees along side-slopes, spillways and run-downs to expand riparian habitat for wildlife. Outfall structures from detention ponds with scour aprons are typically designed to extend into and impact wetlands and stream beds. These impacts can be mitigated by locating the outfall outside of riparian and/or wetland habitat then creating a riparian/wetland swale that extends to the receiving stream.

Soils in this region are very sandy and highly permeable which provides ideal conditions for implementing Low Impact Development (LID) systems and practices that mimic natural processes that result in the infiltration, evapotranspiration or use of stormwater throughout a development rather than a waste product. LID practices such as bioretention facilities, wetland swales, rain gardens, rain barrels and permeable pavements implemented throughout the development are recommended to help improve water quality through groundwater infiltration and to reduce and delay the quantity and erosive power of stormwater discharging from traditional single point detention ponds into natural streams.

Ground disturbance /removal of vegetation and exposure of soil instigates the invasion of common and noxious weeds, one of the most detrimental processes to the quality of any kind of habitat. As such, minimization of ground disturbing



# May 2009





## 3.0 AREA DESCRIPTION

The Haegler Ranch (El Paso County Basin Number CHMS0200) is an unnamed tributary to Ellicott Consolidated Drainage Basin unnamed tributary, which is a tributary of Black Squirrel Creek. Haegler Ranch lies in the central portion of El Paso County. Figure 1-1 shows the location of the Haegler Ranch in respect to El Paso County, Colorado. Haegler Ranch Basin is located in Sections 29, 32 and 33 of Township 12 South Range 64 West and sections 2, 3, 4, 9, 10, 11, 12, 13, 14, 15, 22, 23, and 24 of Township 13 South, Range, 64 West and sections 18, 19, 20, 28, 29, 30, 31, 32, 33, and 34 of Township 13 South, Range 63 West and sections 2, 3, and 4 of Township 14 South, Range 63 West.

### 3.1. Basin Description

The Haegler Ranch flows to the southeast from north of Eastonville Road to McDaniels Road with a total of 16.6 sq mi in unincorporated El Paso County, Colorado. In 2005, approximately 14% of the basin was developed. Mucb of the existing development consists of 2- and 5-acre (ac) residential lots surrounded by open space range land used for agriculture and large parcels with homes south of U.S. Highway 24 (US 24). High-density residential developments are being planned in the northern portions of the basin.

The maximum basin elevation is approximately 7,054 ft in the headwaters and falls to approximately 6,085 ft at the downstream confluence of the basin. The basin is typified by rolling rangeland with poor vegetative cover associated with semi-arid climates.

### 3.2. Climate

This area of El Paso County can be described as high plains with total precipitation amounts typical of a semi-arid region. Winters are generally cold and dry, while the springs and summer receive a majority of this precipitation in the form of rainfall. The average precipitation ranges from 14 to 16 in. per year. Thunderstorms are common during the summer months and are quick-moving low-pressure cells that draw moisture from the Gulf of Mexico into the region. The County has an average temperature ranging from a low of 14°F in the winter to a high of 81°F in the summer. The relative humidity ranges from 25% in the summer to 45% in the winter (SCS 1981).

## 3.3. Soils and Geology

Soils within the Haegler Ranch are classified according to the NRCS soil classification system. The predominant soils are in the Blakeland soil series, which consist of deep, somewhat excessively drained soils that formed in sandy alluvium and sediment on uplands. The soil series has high infiltration rates, and are extremely susceptible to wind and water erosion where poor vegetation cover exists. Figure 3-1 shows the soil distribution map for the Haegler Ranch (SCS 1981). The bedrock geology is predominately flat lying sandstone and siltstone, some of which is covered with recent alluvium.

# 3.4. Property Ownership and Land Use Information

Property ownership along the major drainageways within the Haegler Ranch varies from public to private. Along recent developments, drainage right-of-ways and greenbelts have been dedicated during the development of the adjacent residential and commercial land. A portion of Haegler Ranch has already been developed with 2- and 5-ac residential lots. The drainageways in the lower part of the basin remain under private ownership with no delineated drainage right-of-way or easements. A drainage easement or right-of-way must be granted to the County in order for DOT to perform any recommended improvements.

Roadway and utility easements abutting or crossing the major drainageways occur most frequently in the developed portions of the basin. The locations of roadways were obtained from the El Paso County Major Transportation Corridors Plan dated September 21, 2004 (EPC 2004). The El Paso County Rock Island Trail System runs parallel along the north side of US 24. The trail follows the abandoned Chicago and Rock Island Railroad between Falcon and Peyton, Colorado.

Land use information for the existing and future conditions models was obtained from El Paso County Planning Department in 2005. This information is used in the hydrologic analysis to predict runoff rates and volumes for the purposes of stormwater facility evaluation. The identification of land uses abutting the drainageways is also useful in the identification of feasible plans for stabilization and aesthetic treatment of the basin. Presented in Figure 3-2 and Figure 3-3 are the land use maps used for the evaluation of impervious land densities discussed in Section 4.0. These figures are not intended to reflect the future zoning or land use policies of the County.

# 3.5. Environmental Analysis

An environmental analysis was conducted for this DBPS to assess the present condition of the biological and environmental resources in the Haegler Ranch. Site visits were conducted to study these elements of the basin. Particular attention was paid to the drainageways and spring/seep areas to determine biological resources in riparian zones and wetlands.

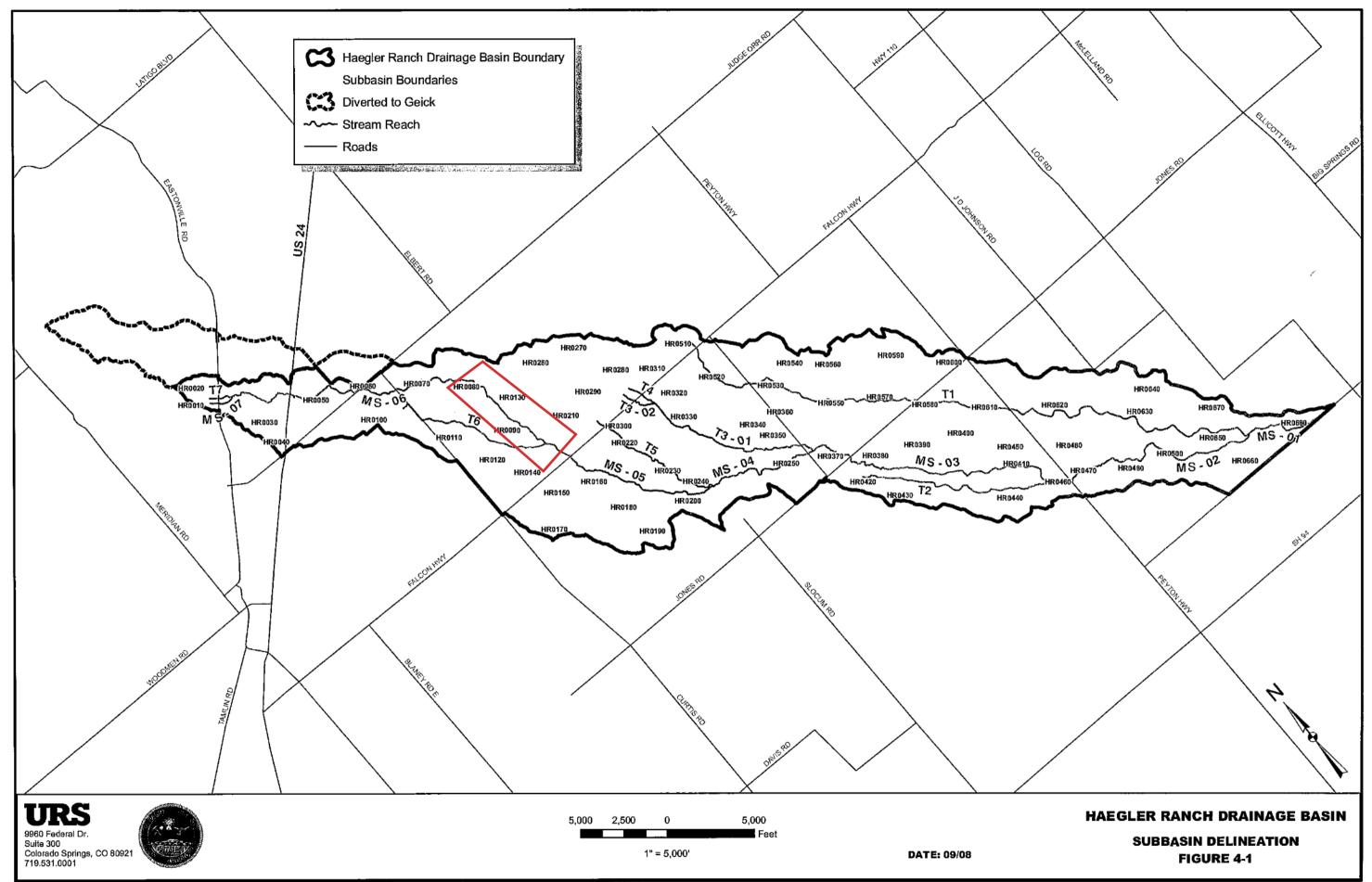
The Haegler Ranch consists of indistinct ephemeral streams that flow after storms for a short period of time. The main stem of Haegler Ranch consists of dry natural grass swales with some poor quality riparian zones and small wetlands in the floodplains. Most of the wetlands surround stock reservoirs and are heavily grazed in some of the rangeland pastures. As a result, the wetlands and riparian drainageways have been degraded in vegetative cover and ecological value. The existing wetlands are neither large nor extensive, and are mostly discontinuous. In their present condition, the wetlands are not a significant habitat resource within the basin. Figure 3-4 and Figure 4-4 show and potential wetlands that may require further study.

Most of the open space is used for agriculture or rangeland. Drainageways have been channelized principally only at roadway crossings. These areas of concentrated flow have defined channels that tend to become indistinct as they flow downstream. Vegetation in the Haegler Ranch in the open space does not vary dramatically. Vegetation patterns generally follow the physiographic region of the plains dominated by a short- to mid-height prairie grass with a few shrubs and sporadic trees such as cottonwoods. Wetlands consist of rushes and sedges such as little bluestem, grama grasses, needle and thread and western wheat grass.

Wildlife and animal species common to the open plains inhabit the basin. They consist of animals that tolerate the presence of roads and people including large and small mammals such as deer, antelope, coyotes and rodents, and several species of birds such as killdeer and red-winged blackbirds. Preliminary review indicates that the DBPS will not affect any threatened or endangered species or critical habitat.

Because of the sensitivity of wetlands, riparian areas, and wildlife to stormwater runoff, sedimentation and erosion should be evaluated and planned for in the alternatives. Wetland and riparian areas provide a habitat resource that should be preserved during the alternative development. These areas can be protected and enhanced to improve ecological value.

Haegler Ranch Drainage Basin Planning Study



URS NO. 21711039

- <u>Main Stem (MS-05)</u> This channel extends from the confluence of the main stem with Tributary 6 north of Falcon Highway in subbasin HR0140 to the confluence of the main stem with Tributary 5 in subbasin HR0200. The channel is a grass swale with one culvert crossing at Falcon Highway.
- <u>Main Stem (MS-06)</u> This channel extends from the confluence of the main stem with Tributary 7, southeast of Eastonville Road in subbasin HR0030, to the confluence of the main stem with Tributary 6, just north of Falcon Highway in subbasin HR0090. The channel is a grass swale with two culvert crossings, one bridge crossing, and one overtopped roadway at Judge Orr Road.
- <u>Main Stem (MS-07)</u> This channel extends from subbasin HR0010 northwest of Eastonville Road to the confluence of the main stem with Tributary 7, southeast of Eastonville Road in subbasin HR0030. The channel is a grass swale with one culvert crossing at Eastonville Road.
- <u>Tributary 1 (T1)</u> This channel extends from subbasin HR0510 just north of Falcon Highway to the confluence of the main stem at subbasin HR0650. The channel is long, dominated by a grass swale with low points along the channel, and has 4 culvert crossings.
- <u>Tributary 2 (T2)</u> This channel extends from subbasin HR0420 just south of Jones Road to the confluence of the main stem at subbasin HR0440 to the northwest of Peyton Highway. The channel is parallel to MS-03, and varies between a grass swale and an alluvial sand bed channel with diversion structures such as pond embankments and berms.
- <u>Tributary 3 (T3-01)</u> This channel extends from subbasin HR0330 at the confluence with Tributary 4, just south of Falcon Highway, to the confluence with the main stem east of Murr Road, at subbasin HR0360. The channel is a grass swale with two culvert crossings in a large lot residential development.
- <u>Tributary 3 (T3-02)</u> This channel extends from subbasin HR0290 just north of Falcon Highway to the confluence with Tributary 4, just south of Falcon Highway, in subbasin HR0300. The channel is a grass swale with one culvert crossing at Falcon Highway.
- <u>Tributary 4 (T4)</u> This channel extends from subbasin HR0280 north of Falcon Highway to the confluence with Tributary 3, just south of Falcon Highway, in subbasin HR0300. The channel is a grass swale with one culvert crossing at Falcon Highway.
- <u>Tributary 5 (T5)</u> This channel extends from subbasin HR0210 just north of Falcon Highway to to the confluence with the main stem in subbasin HR0230. The channel is a grass swale with one culvert crossing at Falcon Highway.
- <u>Tributary 6 (T6)</u> This channel extends from subbasin HR0100 west of Curtis Road to the confluence of the main stem north of Falcon Highway in subbasin HR0120. The channel is a grass swale with one culvert crossing at Curtis Road.
- <u>Tributary 7 (T7)</u> Tbis cbannel extends from subbasin HR0020 northwest of Eastonville Road to the confluence of the main stem, southeast of Eastonville Road, in subbasin HR0030. The channel is a grass swale with one culvert crossing at Eastonville Road.

# 5.6. Manning's Roughness Coefficients

Manning's roughness coefficients for each cross-section were estimated based on site visits and aerial photographs. Multiple Manning's roughness coefficients were used across the cross-section as necessary to accurately describe changes in vegetative cover between the main channel and overbank

areas. The values for the Manning's roughness coefficients in the channel and the floodplains are taken from the Guide for Selecting Manning's Roughness Coefficients for Natural Channels and Floodplains by the USGS (WSP 2339). This manual was used since the Manning's roughness coefficients can be adjusted for surface irregularities, variation in cross-sections, obstructions, vegetation, and meandering. The Manning's roughness coefficients for the channels and floodplains associated with different types of land cover are summarized in Table 5-1.

### Table 5-1 Manning's Roughness Coefficients for the Haegler Ranch Drainage Basin

Land Surface Type	Manning's Roughness Coefficients
Channel	
Grass swale	0.055
Grass-lined ditch	0.032
Sand bed	0.025
Floodplain	
Grass	0.065
Trees	0.150
Light Brush	0.074
Brush	0.100
Earth	0.038
Asphalt / Concrete	0.020

<sup>1</sup>Source: Guide for Selecting Manning's Roughness Coefficients for Natural Channels and Floodplains by the USGS (WSP 2339).

# 5.7. Cross-sections

Hydraulic cross-sections were initially placed approximately 500-ft apart along reaches, and additional cross-sections were added to represent confluences, road crossings and changes in channel form. Cross-sections were automatically stationed from downstream to upstream along the reacb. Each cross-section was adjusted to extend across the entire floodplain and was placed perpendicular to the anticipated direction of flow in both the main channel and left/right overbanks. The cross-sections were bent in some locations to meet this requirement, as described in Chapter 3 of HEC-RAS Hydraulic Reference Manual (Version 3.1, November 2002).

Additional cross-sections were added at structures such as bridges and culverts. At each structure, four cross-sections were added to the HEC-RAS model. These four cross-sections included an upstream cross-section prior to flow contraction, a cross-section at the upstream face of the structure, a cross-section at the downstream face of the structure, and a downstream cross-section where flow is fully expanded. All bridge and culvert crossings were field surveyed to determine their size, inverts, and material.

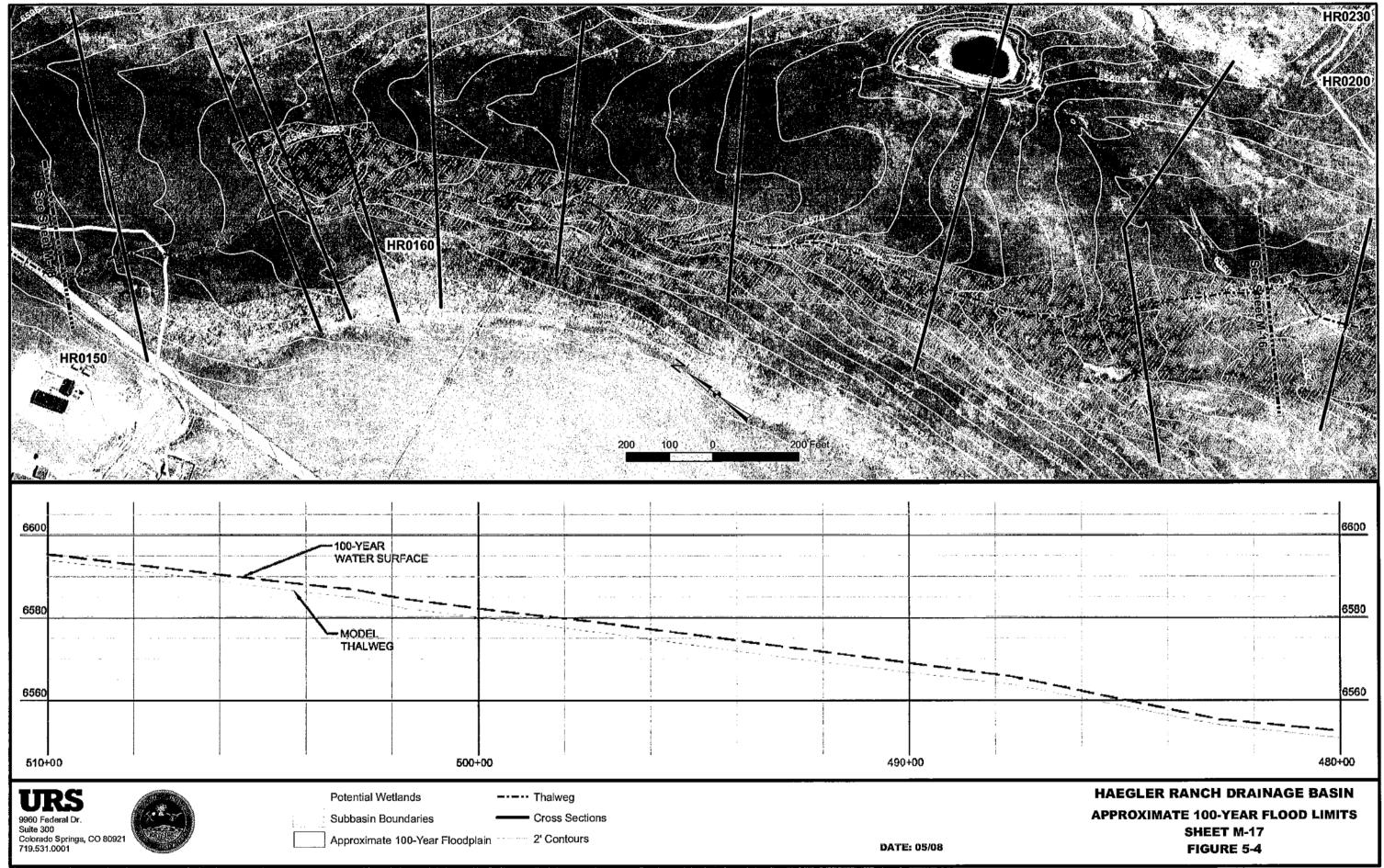
Expansion and contraction coefficients were estimated based on the ratio of expansion and contraction of the effective flow area in the floodplain occurring at cross-sections and at roadway crossings. For subcritical flow conditions and where the change in the stream cross-section was gradual, contraction and expansion coefficients of 0.1 and 0.3, respectively, were used. Wherever the change in effective

Key Location	Reach and HEC-RAS Result			Recurrence	e Intervals	an d Martin
Key Localion-	Station	IIIC-RAJ RESUL	2-yr	5-yr	10-yr	10
	Channel velocity (ft/sec)		1.1	1.63	1.98	2
Main stem at US 24	MS-06 72276	Water surface depth in channel (ft)	1.36	2.44	3.24	6
	12210	Top width (ft)	18.23	24.85	29.7	25
		Channel velocity (ft/sec)	3.33	4.09	1.76	3
Main stem at Judge Orr Road	MS-06 67666	Water surface depth in channel (ft)	0.52	1.04	1.05	1
	07000	Top width (ft)	174.53	534.34	535.52	56
		Channel velocity (ft/sec)	1.05	1.6	2.04	3
Main stem at Falcon Highway	MS-05 52353	Water surface depth in channel (ft)	1.79	3.69	4.96	5
	52555	Top width (ft)	31.42	83.76	556.41	59
		Channel velocity (ft/sec)	2.45	3.7	1.27	2
Main stem at Jones Road	MS-03 33189	Water surface depth in channel (ft)	3.2	5.83	9.25	1(
	55105	Top width (ft)	47.98	105.51	580.28	66
		Channel velocity (ft/sec)	0.16	0.4	0.59	1
Main stem at Peyton Highway	MS-02 18474	Water surface depth in channel (ft)	4.14	4.35	4.51	5
	10474	Top width (ft)	813.21	871.68	882.22	92
		Channel velocity (ft/sec)	0.62	1.02	1.47	
Southeast Tributary at Jones Road	Т1 22297	Water surface depth in channel (ft)	2.45	3.52	3.59	3
Road		Top width (ft)	197.35	345.68	351.74	37
		Channel velocity (ft/sec)	1.67	2.25	2.65	4
Southeast Tributary at Peyton Highway	T1 16611	Water surface dcpth in channel (ft)	0.08	0.17	0.24	0
Ingliway	10011	Top width (ft)	239.82	241.36	242.51	24
		Channel velocity (ft/sec)	3.44	0.11	0.18	0
Southeast Tributary at Confluencc with Main stem	Т1 410	Water surface depth in channel (ft)	1.69	2.01	2.01	2
	410	Top width (ft)	31.89	1169.3	1169.3	11
		Channel velocity (ft/sec)	2.68	3.85	19.89	1
At Confluence with Geick Basin	MS-01 82	Water surface depth in channel (ft)	1.45	2.17	1.11	2
Pasin	02	Top width (ft)	75.88	255.32	60.67	2

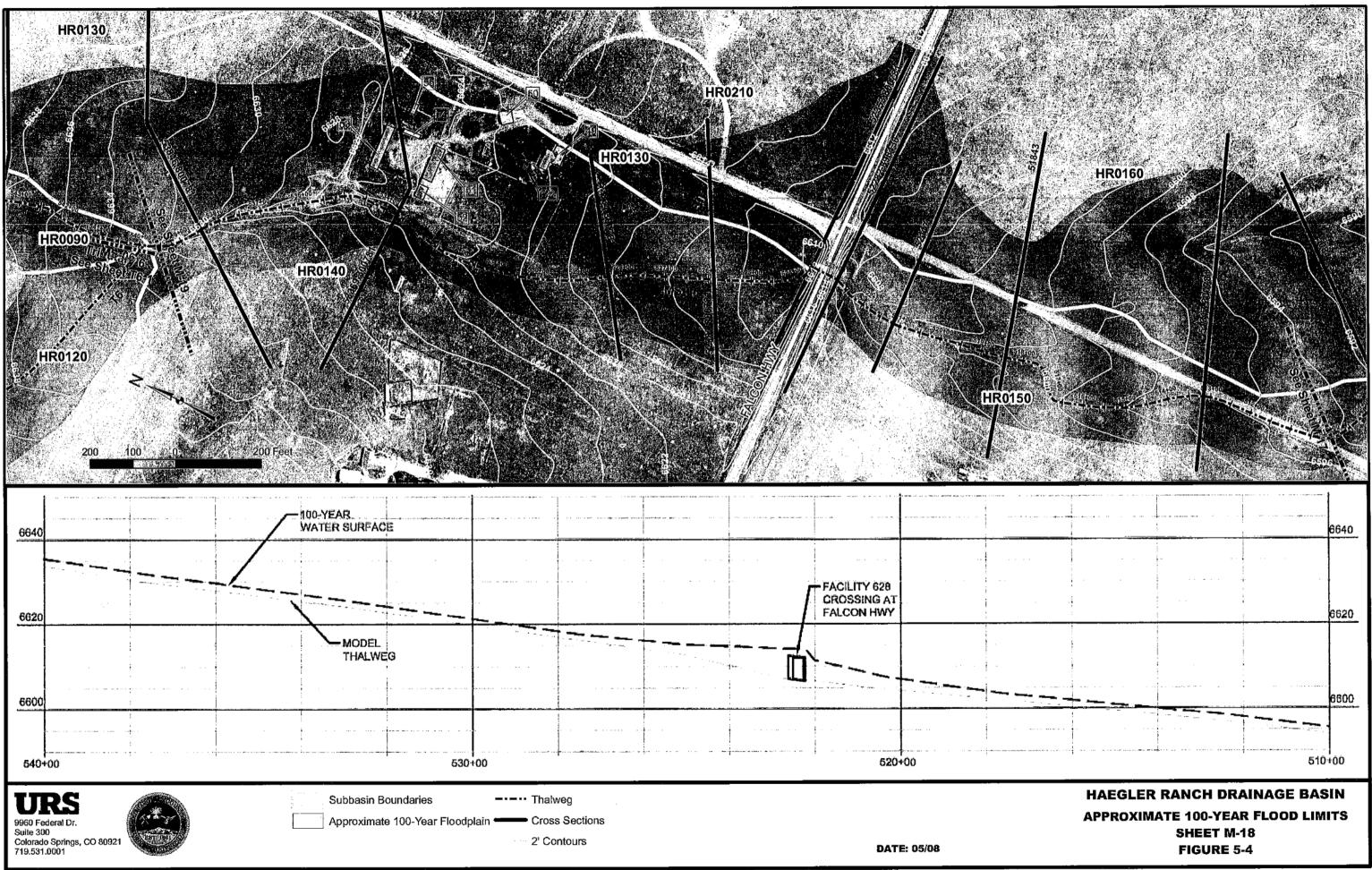
### Table 5-4 Existing Conditions HEC-RAS Model

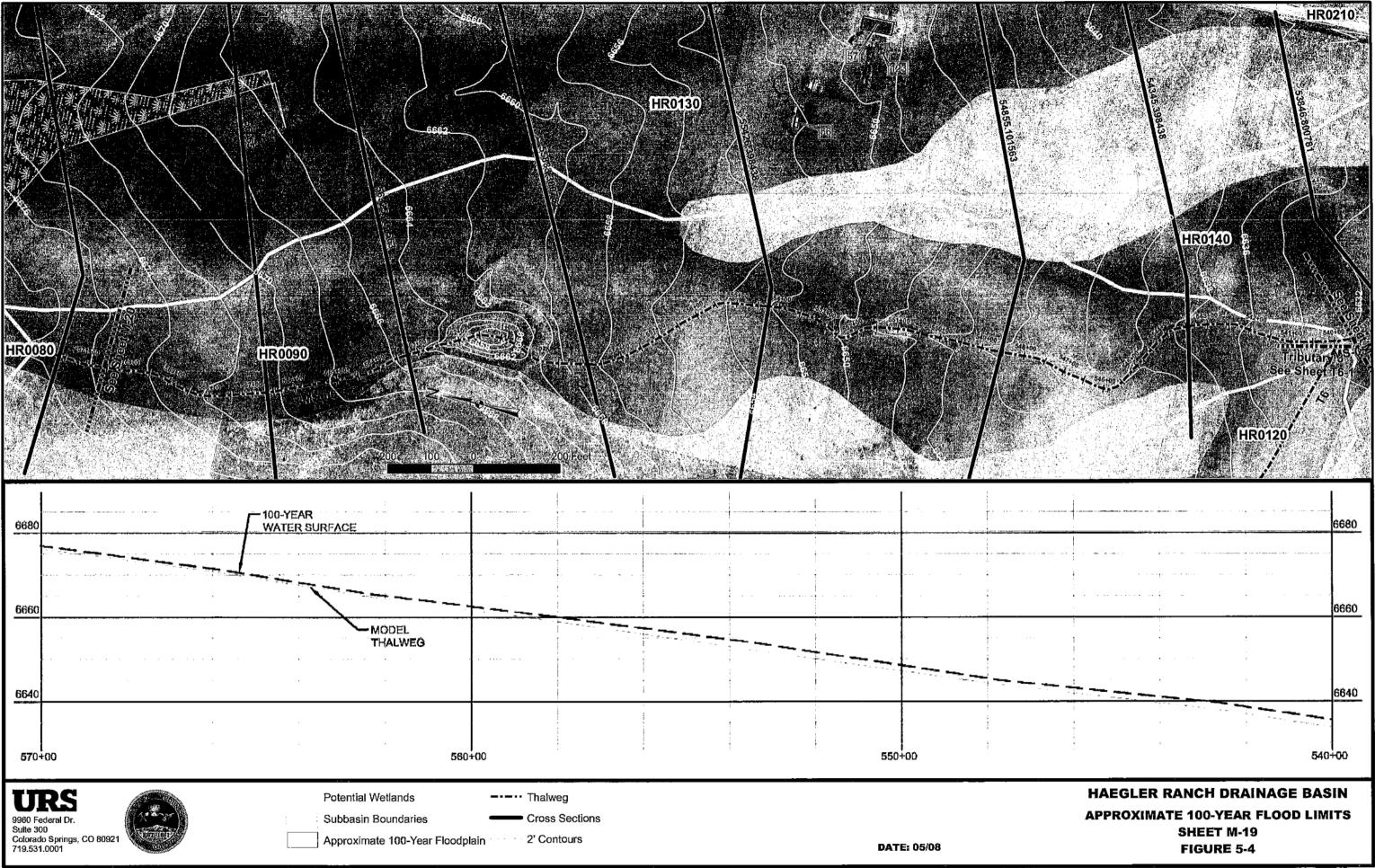
100-yr	
2.92	
6.49	
255.62	
3.48	
1.35	
569.34	
3.59	
5.74	
592.33	
2.51	
10.46	
667.17	
1.43	
5.15	
925.27	
3.2	
3.82	
372.17	
4.05	
0.51	
247.41	
0.67	
2.01	
1169.3	
17.33	
2.36	
262.84	

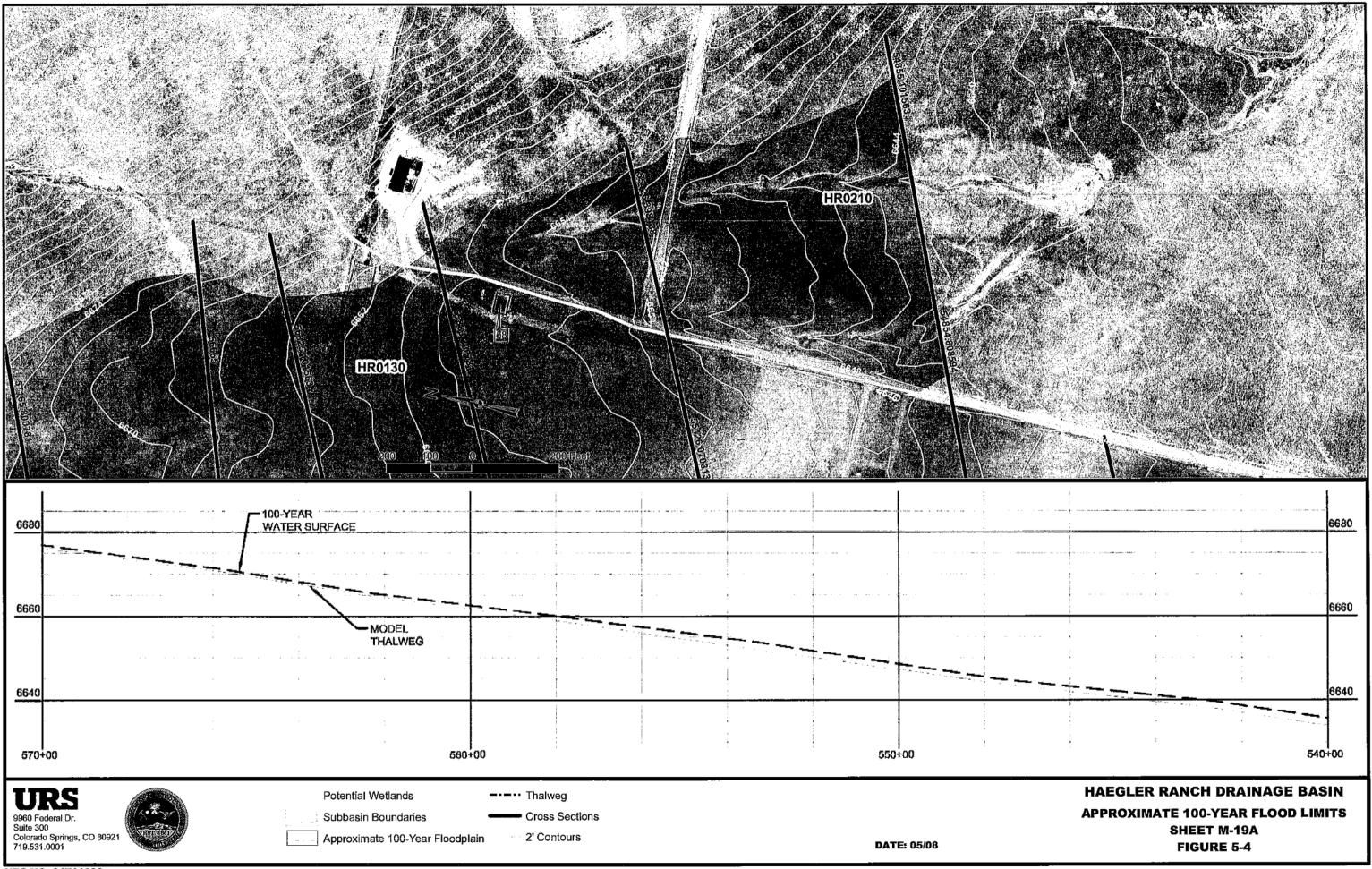
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Pond	Size (AF)	Peak Inflow (cfs)		Peak Ou	flow (cfs)
		2-yr	100-yr	2-yr	100-yr
SR-01	10	100	320	8	90
SR-02	5	14	300	3	250
SR-03	16	210	640	29	530
SR-04	25	200	1120	33	740
SR-05	24	76	570	9	250
SR-06	9	14	180	1	20
SR-07	5	6	140	1	88
SR-08	5	23	240	15	210
SR-09	20	50	430	3	66
SR-10	23	85	860	23	600
SR-11	2	3	70	1	61
SR-12	9	19	140	1	35
SR-13	3	12	120	6	110

Table 6-8 Subregional Detention Pond Summary

Subregional ponds have been sized using the hydrograph routing method described above. In this alternative, all proposed channels and culverts are sized for the existing 100-year peak flow rates, except within proposed developments where it is necessary to provide conveyance for developed flow rates. Flood impacts for the 100-year peak flow downstream of the subregional, full spectrum detention ponds will not increase.

### 6.3.2.1. Channels

In this alternative, only channel improvements through proposed developments are included, unless an area is undersized for existing conditions. Existing deficiencies are the responsibility of the current land owner or the County, and not the developer, and corrective measures for existing deficiencies are not included in the cost estimates. Proposed channel improvements along the corresponding reaches are summarized in Table 6-9.

					·
Channel.	Existing 100- yr Flow (cfs)	Proposed 100-yr Flow (cfs)	Design Flow (cfs)	Channel Length (ft)	Material
Main Stem (MS-05)	1460	1680	2000	1560	Grass
Main Stem (MS-06)	660	530	600	3120	Grass
Main Stem (MS-06)	720	970	1000	4535	Grass
Main Stem (MS-06)	750	740	800	3190	Grass
Tributary 3 (T3-01)	600	600	600	5000	Grass
Tributary 3 (T3-02)	220	500	500	420	Grass
Tributary 4 (T4)	220	500	500	940	Grass
Tributary 6 (T6)	200	440	500	4280	Grass
Tributary 6 (T6)	240	250	300	1400	Grass

Table 6-9 Channel Design for Subregional Detention Alternative

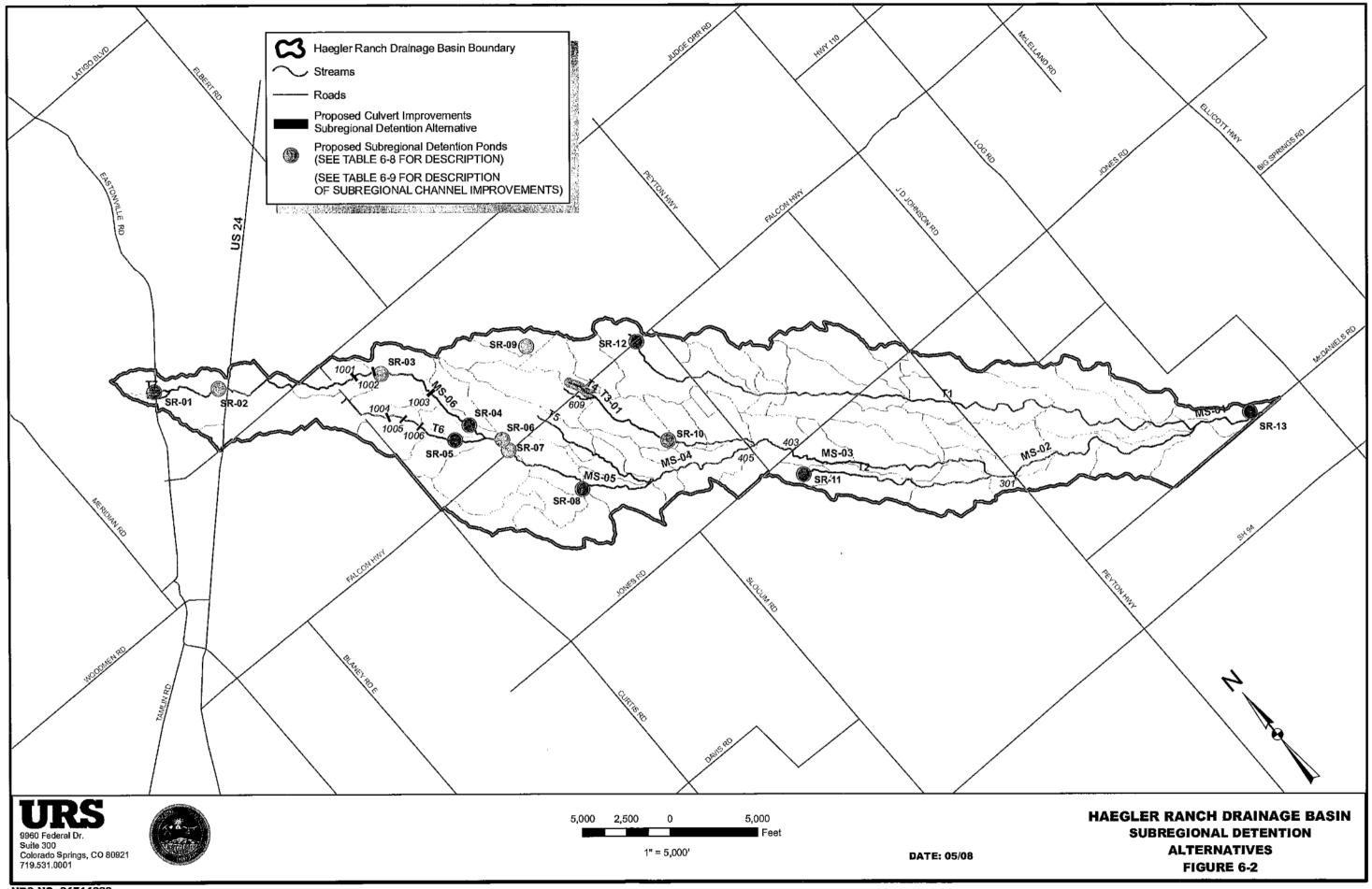
### 6.3.2.2. Culverts

As with the channels, only the culverts through proposed developments will be effected unless an area is undersized for existing conditions. Any existing deficiencies in the roadway culverts are the responsibility of the County and not the developer, and required culvert improvements are not included in the cost estimates for the alternative. Proposed culvert improvements are summarized in Table 6-10.

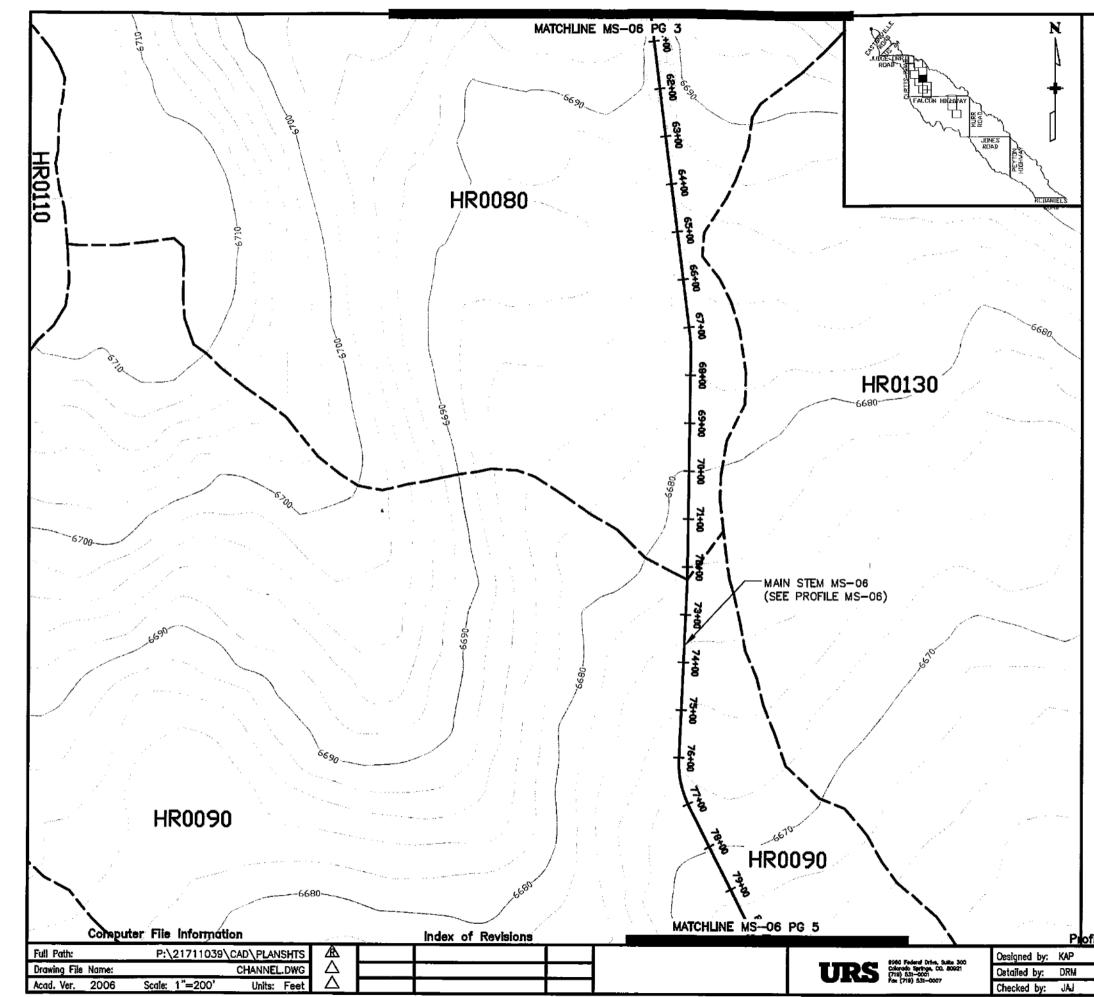
Facility Number	Road Crossing	Channel	Proposed 100-yr Flow (cfs)	Deficiency	Necessary Facility for Proposed 100- year Flow
301	Peyton Highway	Main Stem (MS-02)	3,370	Overtops	9-6'X6' RCBs
403	Jones Road	Main Stem (MS-03)	2,970	Overtops	8-6'X6' RCBs
405	Murr Road	Main Stem (MS-04)	2,870	Overtops	8-6'X6' RCBs
609	Falcon Highway	Tributary 3 (T3-02)	460	Overtops	2-6'X6' RCBs
1001	Future Pastura Street	Main Stem (MS-06)	930	Future Road	3-6'X6' RCBs
1002	Future Arroyo Hondo Blvd. N.	Main Stem (MS-06)	930	Future Road	3-6'X6' RCBs
1003	Future Arroyo Hondo Blvd. S.	Main Stem (MS-06)	1500	Future Road	4-6'X6' RCBs
1004	Future Pastura Street	Tributary 6 (T6)	440	Future Road	2-66" RCPs
1005	Future El Vado Road	Tributary 6 (T6)	440	Future Road	2-66" RCPs
1006	Future Socorro Trail	Tributary 6 (T6)	440	Future Road	2-66" RCPs

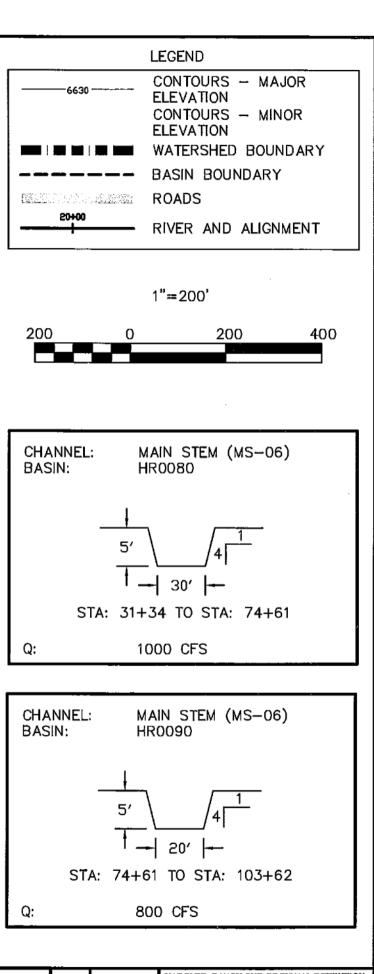
### Table 6-10 Culvert Design for Subregional Detention Alternative

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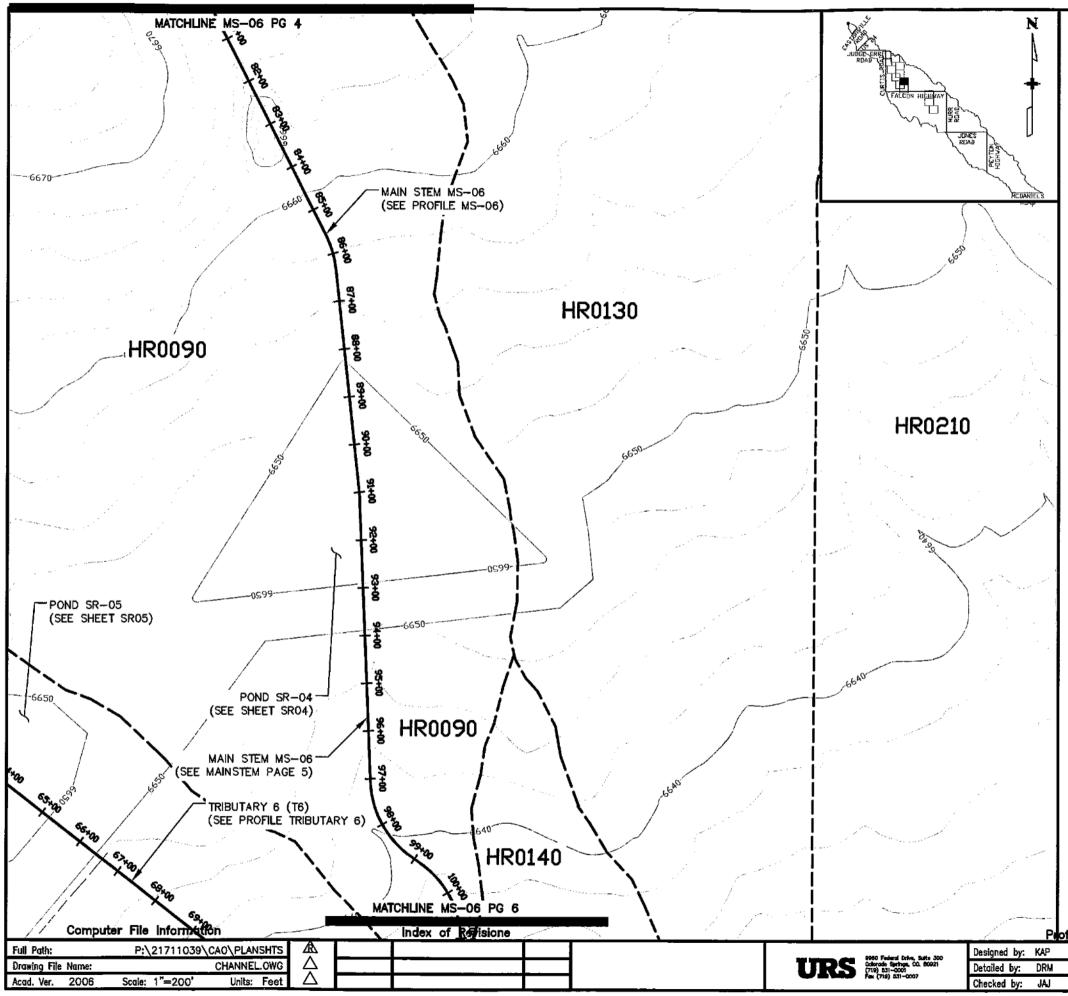


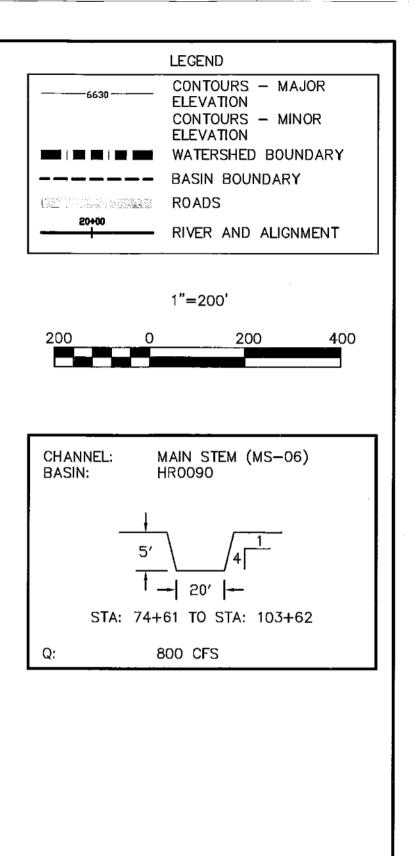
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	Structure	HAEGLER RANC				
	Numbers	Sheet Number	MAIN	STEM	PG	4





Tiles						
	Structure	HAEGLER RANG				ON
	Numbers	Sheet Number	MAIN	STEM	PG	5



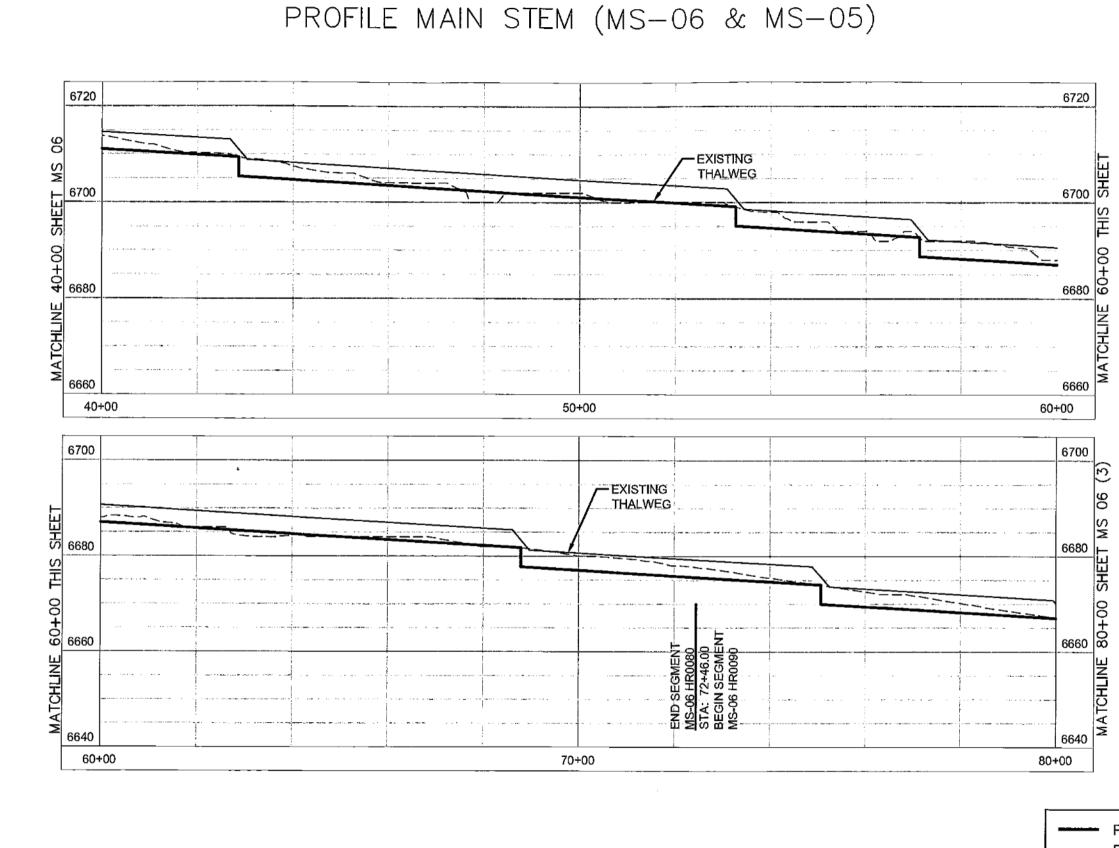
SLOPE = 0.60%

(7) 4' DROPS

MS-06 HR0090

SLOPE = 0.60%

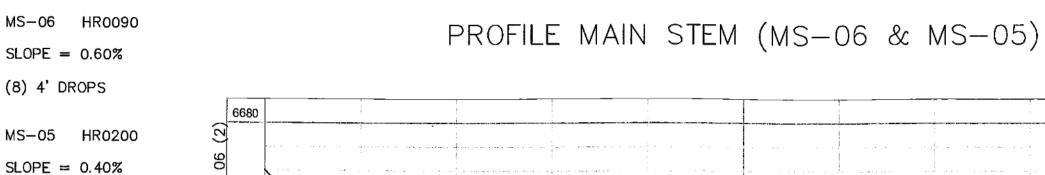
(8) 4' DROPS



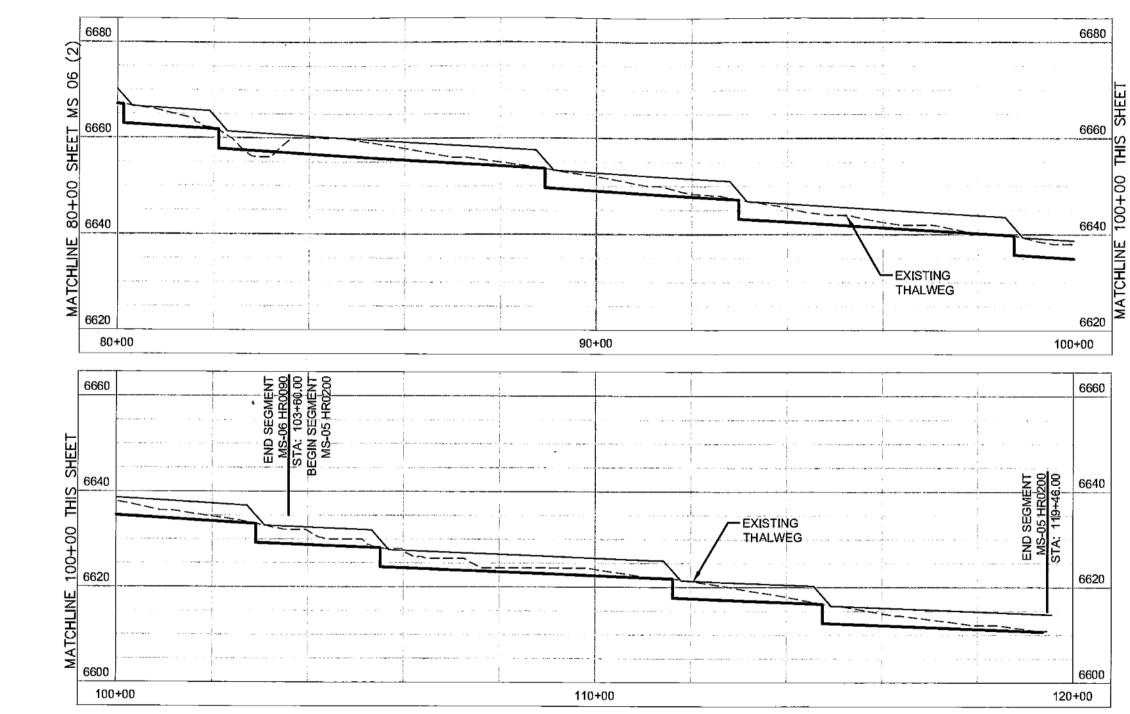
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LEGEND
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----- PROPOSED DROP STRUCTURE ---- EXISTING THALWEG ------ HYDRAULIC GRADE LINE



(4) 4' DROPS



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		PARTMENT OF TRANSPORTATION	Detailed by: DRM Structure Numbers	
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LEGEND
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 PROPOSED DROP STRUCTURE
 EXISTING THALWEG
 HYDRAULIC GRADE LINE

# GIECK RANCH DRAINAGE BASIN PLANNING STUDY El Paso County, Colorado

Volume 1 – Final Report

October 1, 2007 Revised: February 10, 2010

### PREPARED FOR:

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### Project Description, Location and Drainage

### A. Basin Description and Location

I.

Figure 1.0 shows the location of the Gieck Ranch Drainage Basin. The basin covers a total area of 22.05 square miles within unincorporated El Paso County. The basin begins approximately five miles northeast of the Town of Falcon in El Paso County at an elevation of approximately 7,300 feet above mean sea level (msl). From this point, drainage from the basin travels approximately 15 miles to the southeast. An aerial photograph of the basin is included as Figure 1.1 which is located in Volume 2 of this report. The minimum elevation within the basin is approximately 6,100 feet above msl. Channel slope varies considerably across the basin with average channel slopes ranging from 0.5% to 5%. In general, steeper slopes are located at the northern reaches of the basin, while the flatter slopes are located at the southern reaches. The Gieck Ranch Drainage Basin is tributary to Black Squirrel Creek which drains south to its confluence with the Arkansas River near the city of Pueblo, Colorado. The area encompassing the basin is characterized by rolling range land typically associated with Colorado's semi-arid climates. Existing vegetative cover in undeveloped areas is considered fair for the purposes of this report.

While developing this Drainage Basin Planning Study it was determined that a portion of the adjacent Haegler Ranch Basin, approximately 1.4 square miles, is diverted into the Gieck Ranch Basin as shown in Figure 1.0. This diversion occurs just east and immediately upstream of the intersection of Judge Orr Road and Curtis Road. The diversion exists because no culvert was constructed to convey the runoff from the north side of Judge Orr Road to the south side when the road was originally built. Instead, runoff flows east along the northern edge of the road to a culvert located within the Gieck Basin. This condition has existed since the construction of Judge Orr Road. A stakeholder's meeting was held April, 2005 to discuss the impacts of maintaining the diversion or removing it and restoring historic flows. It was decided to maintain the diversion as is, Documentation and correspondence related to the diversion can be found in Section 1 of the Technical Addenda. In addition to the diversion, while delineating the drainage basins using LIDAR based topography, it was determined that there is an additional 1.35 square miles of area in the southeast section that drains into the Gieck Ranch Basin that

was previously thought to drain into adjacent basins. The total square miles of drainage area for the Gieck Ranch Basin (22.05) includes the 1.4 square miles of drainage area diverted from the Haegler Ranch Basin and the 1.35 square miles of additional drainage area in the southeast section of the basin.

The drainage basin has been subdivided into six major sub-watersheds or drainageways. These include the Main Stem Channel (MS) and five main tributaries, the Haegler Diversion (HD), West Fork (WF), East Fork (EF), South Fork (SF), and Southeast Fork (SE). These major drainageways were determined as those existing drainageways that carry runoff from at least 100 to 160 acres. Figure 2.0 shows the locations of the six main drainageways.

There are several open water storage areas that exist within the basin. They appear to be remnants of former irrigation structures and/or stock watering ponds. They do not appear to be constructed for the purposes of flood control. For modeling purposes they were not evaluated as effective storage. Additionally, remnants of several irrigation facilities associated with former ranch lands can be found within the drainage basin. It is not apparent whether or not these irrigation structures are still used. There do not appear to be any active irrigation ditches within the basin.

### **B.** Climate and Flood History

The region surrounding the City of Falcon is generally classified as semi-arid, with annual precipitation in the range of 14 to 16 inches. The bulk of the precipitation is received during the spring and summer months in the form of thundershowers. Most of the flood-producing storms in El Paso County occur during the summer months when thunderstorms are most intense. Available flood history for El Paso County is almost exclusively concerned with the aspects of flooding on Fountain Creek or Monument Creek urbanized areas, so there is no history of flooding in the Gieck Ranch Basin listed in the El Paso County Flood Insurance Study. However, significant flooding events resulting in damage to roadways and drainage structures have been documented in nearby basins, such as that which occurred in the Haegler Basin in 1995. This indicates that flooding and related damage within the Gieck Ranch Drainage Basin and its tributaries is possible in the future.

				<u> </u>					
Design			Accumulative	Existing	Future	%	Existing	Future	% D:55
Point		Hydrologic	Area	Peak Flow	Peak Flow	Difference	Volume	Volume	Difference
ID	Design Point Location	Element	(mi <sup>2</sup> )	(cfs)	(cfs)	Peak Flow	(ac-ft)	(ac-ft)	Volume
1	Haegler Diversion at Eastonville Road	HD-J2	0.8	431	1060	146%	77	96	25%
2	West Fork at Eastonville Road	WF-J1	0.3	146	389	166%	29	39	33%
3	Main Channel at Eastonville Road	MS-J4	1.3	730	1233	69%	112	135	20%
4	Haegler Diversion at Highway 24	HD-J4	1.3	521	1223	135%	97	121	24%
5	West Fork at Highway 24	WF-J3	0.4	224	605	170%	49	62	26%
6	Main Channel at Highway 24	MS-J6	2.5	997	1896	90%	194	225	16%
7	East Fork at Highway 24	EF-J4	1.2	1054	1113	6%	124	126	1%
8	Main Channel at Elbert Road	MS-J7	3.0	1010	1896	88%	220	253	15%
9	East Fork at Elbert Road	EF-J6	2.1	1120	1172	5%	183	187	2%
10	West Fork at Judge Orr Road	WF-J6	1.5	1017	2213	117%	244	291	19%
11	Confluence of East Fork and Main Channel	MS-J9	5.7	1817	3068	69%	429	467	9%
12	Main Channel at Judge Orr Road	MS-J11	6.7	1968	3383	72%	487	564	16%
13	Confluence of West Fork and Main Channel	MS-J12	11.2	2732	6104	123%	805	993	23%
14	Main Channel at Falcon Highway	MS-J16	13.4	3045	6784	123%	936	1191	27%
15	Main Channel at Peyton Highway	MS-J19	15.1	3200	6946	117%	1012	1269	25%
16	Main Channel at Jones Road	MS-J20	15.6	3250	7056	117%	1040	1308	26%
17	South Fork at Jones Road	SF-J4	1.3	454	454	0%	133	133	0%
18	Confluence of South Fork and Main Channel	MS-J22	17.9	3650	7392	103%	1210	1489	23%
19	Southeast Fork at McDaniels Road	SE-J3	2.4	547	546	0%	210	210	0%
20	Main Channel at McDaniels Road	MS-J29	19.6	3791	7525	99%	1293	1597	23%
21	Total Combined Outfall	SE-J3 plus MS-J29	22.0	4326	7687	78%	1503	1807	20%

Table 6.4: Summary of Flows at Selected Design Points - 100-year Storm Event

The 100-year storm event future undetained peak flow is estimated to increase by 78% over the existing peak flow while the future volume of runoff is estimated to increase by 20%. During the hydrologic analysis it was observed that the Black Squirrel Creek lies very close to the eastern boundary of the Gieck Ranch Basin from Falcon Highway downstream to Log Road. It is possible that flow from Black Squirrel Creek could spill into the Gieck Ranch Basin during extreme storm events. The flows in Black Squirrel Creek in this area are expected to be more than 5,000 cfs for the 100-year event. If the Black Squirrel Creek were to overflow its' banks and flow into the Gieck Ranch Basin it could increase the flows shown in the above tables. Possible improvements to address this potential problem include channel improvements to increase the Black Squirrel Creek conveyance in this area or constructing berms on the east bank to prevent overflow.

35	Elbert Road south of structure 34	24" CMP	Good	100%	Y	
36	Elbert Road at Main Channel	2 - 48" CMP	Good	19%	N	3 - 12' x 4' CB
37	Elbert Road south of structure 36	24" CMP	Poor	55%	Y	
		67" x 95"				
38	Judge Orr Road at West Fork	CMP	Good	20%	N	<u>4 - 12' x 5' CB</u>
39	Judge Orr Road east of structure 38	36" CMP	Good	100%	Y	
40	Judge Orr Road west of structure 41	24" CMP	Poor	90%	Y	
41	Judge Orr Road at Main Channel	Bridge	Good	100%	Y	
42	Falcon Hwy at Main Channel	Bridge	Good	57%	N	85' Span
43	Peyton Road at headwaters of South Fork	24" CMP	Fair	75%	Y	
44	Peyton Road at Main Channel	4 - 24" RCP	Good	2%	N	<u>5 - 12' x 7' CB</u>
45	Peyton Road south of structure 44	36" CMP	Poor	100%	Y	
46	Peyton Road south of structure 45	24" CMP	Good	100%	Y	
47	East Garrett Road west of structure 48	24" CMP	Poor	100%	Y	
48	East Garrett Road at South Fork	48" CMP	Good	14%	N	2 - 5' x 4' CB
<u>4</u> 9	J.D. Johnson Road at South Fork	4 - 42" RCP	Good	63%	Ν	2 - 12' x 4' CB
50	J.D. Johnson Road south of structure 49	30" CMP	Fair	56%	Ν	36" CMP
51	J.D. Johnson Road south of structure 50	30" CMP	Fair	100%	Y	
52	Jones Road at Main Channel	60" CMP	Fair	4%	Ν	6 - 12' x 7' CB
53	J.D. Johnson Road at Jones Road	30" CMP	Fair	55%	Y	
54	Jones Road east of J.D. Johnson Road	30" CMP	Good	73%	Y	
55	Jones Road at South Fork	36" CMP	Good	6%	N	2 - 7' x 5' CB
56	Jones Road east of structure 55	30" CMP	Fair	67%	Y	
57	J.D. Johnson Road at Main Channel US of structure 58	3 - 60" RCP	Good	14%	N	85' Span
58	J.D. Johnson Road at Main Channel	30" CMP	Good	1%	N	120' Span
59	J.D. Johnson Road and Log Road	24" CMP	Fair	23%	N	2 - 6' x 3' CB
		48" CMP				
60	Main Channel at private driveway	(est.)	Unknown	2%	<u>N.E.</u>	
61	Log Road at Main Channel	Bridge	Good	36%	N	120' Span
(0)		30" x 48"		10/	2.5	10010
<u>62</u> 63	McDaniel Road at Main Channel         Log Road and McDaniels Road	Oval CMP 24" CMP	Good Good	<u> </u>	NN	120' Span 5 - 6' x 3' CB0

\* Road over-topping not included

\*\* Allowable road over-topping included in adequacy analysis

\*\*\* Based on proposed (with selected drainage basin plan) flows

N.E. Not Evaluated, not EPCDOT responsibility

### VII. Drainage Basin Plan Development

### A. Selected Plan

The selected plan consists of integrating the selected alternative outlined in the previous section. This includes the construction of the small regional full spectrum detention basins and the recommended channel improvements shown on the plan and profile sheets located in the Appendices. The future conditions hydrologic and hydraulic models were updated to determine the affect of the full spectrum regional ponds on peak flows, volumes and channel velocities. Revised hydrologic and hydraulic modeling results are provided in Sections 17 and 18 of the Technical Addenda. Table 11 presents a summary of discharge rates for the selected plan incorporating the full spectrum regional detention facilities.

Design						
Point		Hydrologic	Q2	Q5	Q10	Q100
ID	Design Point Location	Element	(cfs)	(cfs)	(cfs)	(cfs)
		POND HD-				
1	Haegler Diversion at Eastonville Road	S1	5	25	32	338
2	West Fork at Eastonville Road	WF-J2	2	17	45	114
3	Main Channel at Eastonville Road	POND MS- S1	28	119	253	573
			20		200	575
4	Main Channel Tributary 2 at Eastonville	POND MST2-S1	21	65	126	271
4	Road					
5	East Fork Tributary at Eastonville Road	EFT1-B1	25	46	73	134
6	East Fork at Eastonville Road	EF-B1	33	59	92	168
7	Haegler Diversion at Highway 24	HD-J4	7	33	138	429
8	West Fork at Highway 24	WF-J3	6	38	97	242
		POND				
9	West Fork Tributary at Highway 24	WFT1-S1	1	8	24	66
10	Main Channel at Highway 24	MS-J6	49	190	391	877
11	Main Channel Tributary 3 at Highway 24	MST3-B1	1	3	7	19
12	East Fork Tributary at Highway 24	EFT1-J2	43	95	164	337
13	East Fork at Highway 24	EF-J4	160	334	564	1102
	Main Channel at Elbert Road (Further					
14	South of)	MS-B10	_1	2	6	16
15	Main Channel at Elbert Road (South of)	MS-J8	1	3	6	18
16	Main Channel at Elbert Road	MS-J7	50	193	399	896

Table 11: Summary of Flows at Selected Design Points – Selected Plan Developed Conditions

17	East Fork at Elbert Road	EF-J6	162	344	588	1169
18	Confluence of East Fork and Main Channel	MS-J9	160	390	775	1774
		POND				
19	West Fork at Judge Orr Road	WF-SR1	18	86	273	753
		POND				
20	Main Channel at Judge Orr Road (West of)	WF-S3	1	2	4	11
21	Main Channel at Judge Orr Road	MS-J11	154	407	828	1920
	Confluence of West Fork and Main					
22	Channel	MS-J12	160	500	1085	2679
23	Main Channel at Falcon Highway	MS-J16	141	494	1103	2842
24	Main Channel at Falcon Highway (East of)	MS-B20	2	7	15	38
25	South Fork at Falcon Highway	SF-B1	4	13	27	65
26	Main Channel at Peyton Highway	MS-J19	150	520	1163	3003
27	South Fork at Peyton Highway	SF-J1	18	40	70	148
28	South Fork at J.D. Johnson Road	SF-J4	_ 51	117	212	455
29	Main Channel at Jones Road	MS-J20	154	528	1179	3054
30	South Fork at Jones Road	SF-J5	54	124	226	484
31	South Fork Tributary at Jones Road	SET1-B1	24	47	78	152
	Main Channel at J.D. Johnson Road					
32	(North)	MS-J21	154	529	1184	3068
	Confluence of South Fork and Main					
33	Channel	MS-J22	188	602	1341	3449
	Main Channel at J.D. Johnson Road					
34	(South)	MS-J23	193	612	1367	3520
35	South Fork Tributary at J.D. Johnson Road	SET1-J1	38	77	131	272
36	Main Channel at Log Road (North)	MS-J25	195	616	1375	3546
37	Main Channel at Log Road (South)	MS-J26	196	618	1378	3557
38	Southeast Fork at Log Road	SE-J2	70	145	247	498
39	Main Channel at McDaniels Road	MS-J29	199	626	1395	3594
40	Southeast Fork at McDaniels Road	SE-J3	73	153	263	537
		MS-J29				
41	Total Combined Outfall	and SE-J3	272	779	1657	4131

### **B. Small Regional Detention Basins**

The recommended plan includes the construction of 17 small regional detention storage basins, 15 of which would incorporate full spectrum detention. Ponds WF-SR1 and MS-SR1 exceed the contributing area size limitation for full spectrum detention. For these two ponds, the water quality

Gieck Ranch Drainage Basin Planning Study H:\C7706-2\Reports\Revised report submittal 02-10-10.doc

Comparison to the existing conditions flows presented in Tables 6.1 through 6.4 shows that implementation of the selected plan will result in developed peak discharge rates that are slightly lower than existing discharge rates. This should reduce potential for flood damage within the basin.

control volume should be provided. Pond WFT1-S1 will only provide detention for the property located in Basin WFT1-B1 and the pond should be constructed when this property is developed. The locations of the basins shown on the plan sheets are conceptual. The final location and sizes of the basins are to be determined during final design of proposed development projects. It is possible that the location and basin size may vary from the conceptual design as long as sufficient detention storage is provided to meet required discharge rates and the excess urban runoff volumes are provided as outlined in the Urban Drainage and Flood Control District Criteria for full spectrum detention. Table 12 lists the detention basin data for the selected plan. Some areas of the drainage basin may encounter seasonal high ground water tables. Final sizing of the detention basins should be done in such a way as to minimize the need for underdrains.

### **C.** Channel Improvements

Recommended channel improvements consist of vegetation augmentation, selective channel stabilization such as selectively armoring existing channel banks with riprap at outside channel bends and at bridge and culvert outlets, bio-engineered stabilization treatment, and low flow linings, some channelization, and construction of grade control structures. The recommended channel improvements have been selected to minimize environmental impacts and retain natural channel characteristics as much as possible since the basin is mostly undeveloped and the majority of the existing drainageways have not been disturbed at this time. There are large areas of the basin that are to remain as vacant or agricultural land based on the El Paso County 2030 Land Use Codes. Specific channel improvements to the drainageways in these areas were not recommended. It is assumed that these channels will remain in private ownership which lowers the feasibility of channel improvements that require permanent right-of-way or easements for construction and maintenance. The recommended approach for these areas is to provide as-needed improvements.

	Excess Urban	Detention Storage	Discharge
	Runoff Volume	Volume	Rate
Basin ID	(ac-ft)	(ac-ft)	(cfs)
HD-S1	21.4	41.0	345
HD-S2	2.4	7.0	92
WF-S1	7.3	17.0	115
WF-S2	2.7	13.8	134
WF-S3	4.3	9.0	11
WF-S4	29.7	52.0	359
WFT1-S1	2.2	9.0	70
WF-SR1	WQCV*	30.0	802
MS-S1	12.2	42.0	583
MS-S2	0.6	5.2	58
MS-S3	4.8	19.0	147
MS-S4	11.8	30.0	29
MS-S5	2.9	6.1	26
MS-SR1	WQCV*	50.0	2,900
MST2-S1	3.9	21.5	275
MST4-S1	6.4	20.0	137
MST5-S1	11.6	30.0	90

\* Use Water Quality Control Volume

Table 12: Detention Basin Data

Table 13 lists the recommended approach to channel improvements on a reach by reach basis. As land development projects proceed within the drainage basin the location and specific type of selective channel improvements will need to be identified during the project design phase based on site specific conditions. There may be some overlapping of approaches between reaches. For example, some selective stabilization may be needed in reaches designated for vegetation augmentation and vice-versa. The methods outlined in the City/County Drainage Criteria Manual and the El Paso County Engineering Manual should be applied during final design analysis. Some specific channel improvements have been identified for several areas such as the Haegler Diversion channel upsizing and realignment at Judge Orr Road. These improvements are called out on the selected plan drawings.

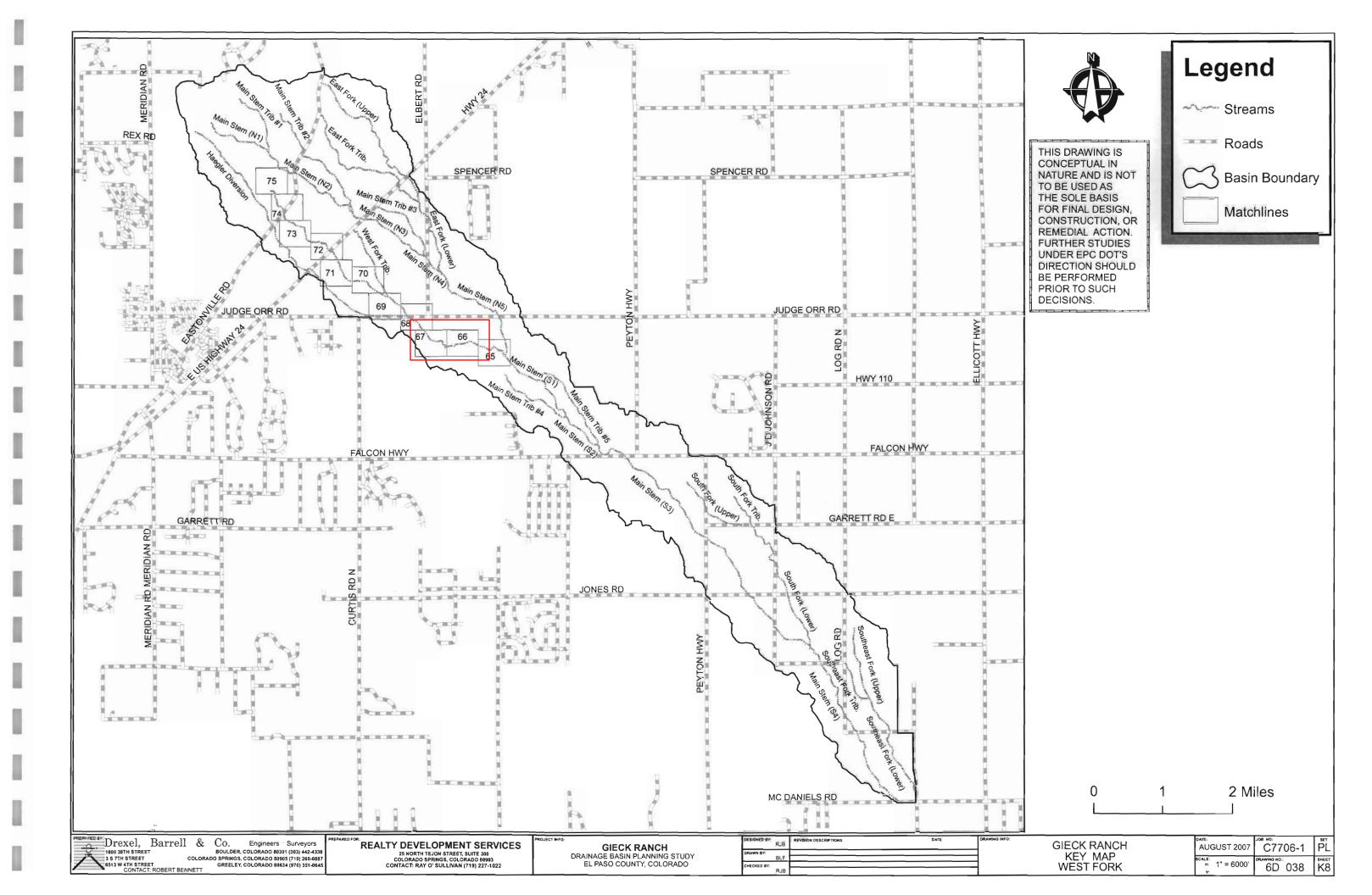
# Table 13: Channel Improvements By Reach

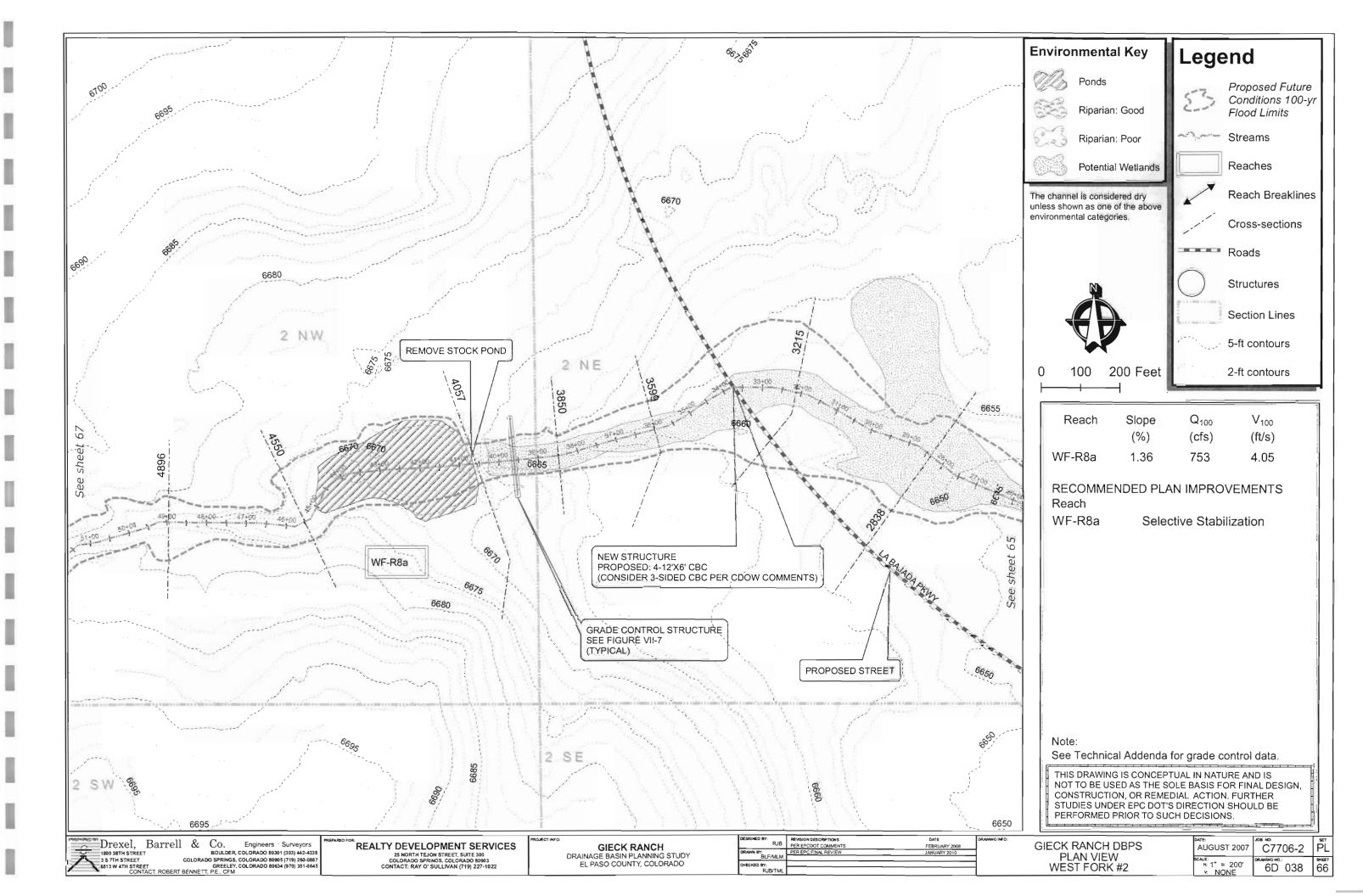
	vements By Reac	Reach Length	
Drainageway	Reach ID	(ft)	Channel Approach
Haegler Diversion	HD-R1a	3875	Selective Stabilization
Haegler Diversion	HD-R1b	5737	Channelization
Haegler Diversion	HD-R2	2826	Vegetation Augmentation
Haegler Diversion	HD-R3	2207	Selective Stabilization
Haegler Diversion	HD-R4	5161	Vegetation Augmentation
Haegler Diversion	HD-R5	3784	Selective Stabilization
West Fork	WF-R1	1775	Channelization
West Fork	WF-R2	2281	Vegetation Augmentation
West Fork	WF-R3	3029	Selective Stabilization
West Fork	WF-R4a	1717	Vegetation Augmentation
West Fork	WF-R4b	2001	Vegetation Augmentation
West Fork	WF-R4c	1601	Selective Stabilization
West Fork	WF-R4d	1198	Selective Stabilization
West Fork	WF-R5	1200	Selective Stabilization
West Fork	WF-R6	863	Selective Stabilization
West Fork	WF-R7a	2341	Vegetation Augmentation
West Fork	WF-R7b	1594	Vegetation Augmentation
West Fork	WF-R8a	4002	Selective Stabilization
West Fork	WF-R8b	1600	Selective Stabilization
West Fork - Trib. WF1	WFT1-RI	5601	Vegetation Augmentation
Gieck Main	MS-R1	2400	Vegetation Augmentation
Gieck Main	MS-R2	2000	Selective Stabilization
Gieck Main	MS-R3	1200	Selective Stabilization
Gieck Main	MS-R4a	1278	Channelization
Gieck Main	MS-R4b	1341	Channelization
Gieck Main	MS-R5	6181	Vegetation Augmentation
Gieck Main	MS-R6	804	Selective Stabilization
Gieck Main	MS-R7a	1554	Vegetation Augmentation
Gieck Main	MS-R7b	3191	Vegetation Augmentation
Gieck Main	MS-R7c	1354	Vegetation Augmentation
Gieck Main	MS-R8a	314	Vegetation Augmentation
Gieck Main	MS-R8b	783	Selective Stabilization
Gieck Main	MS-R8c	568	Selective Stabilization
Gieck Main	MS-R11a	3376	Selective Stabilization
Gieck Main	MS-R11b	2405	Selective Stabilization
Gieck Main	MS-R12	620	Selective Stabilization
Gieck Main	MS-R13	3158	Vegetation Augmentation
Gieck Main	MS-R14	7422	Selective Stabilization
Gieck Main	MS-R15	3306	Selective Stabilization
Gieck Main	MS-R16	2294	As-needed Improvements
Gieck Main	MS-R17	542	As-needed Improvements
Gieck Main	MS-R18	5457_	As-needed Improvements
Gieck Main	MS-R19	1604	As-needed Improvements
Gieck Main	MS-R20a	1197	As-needed Improvements

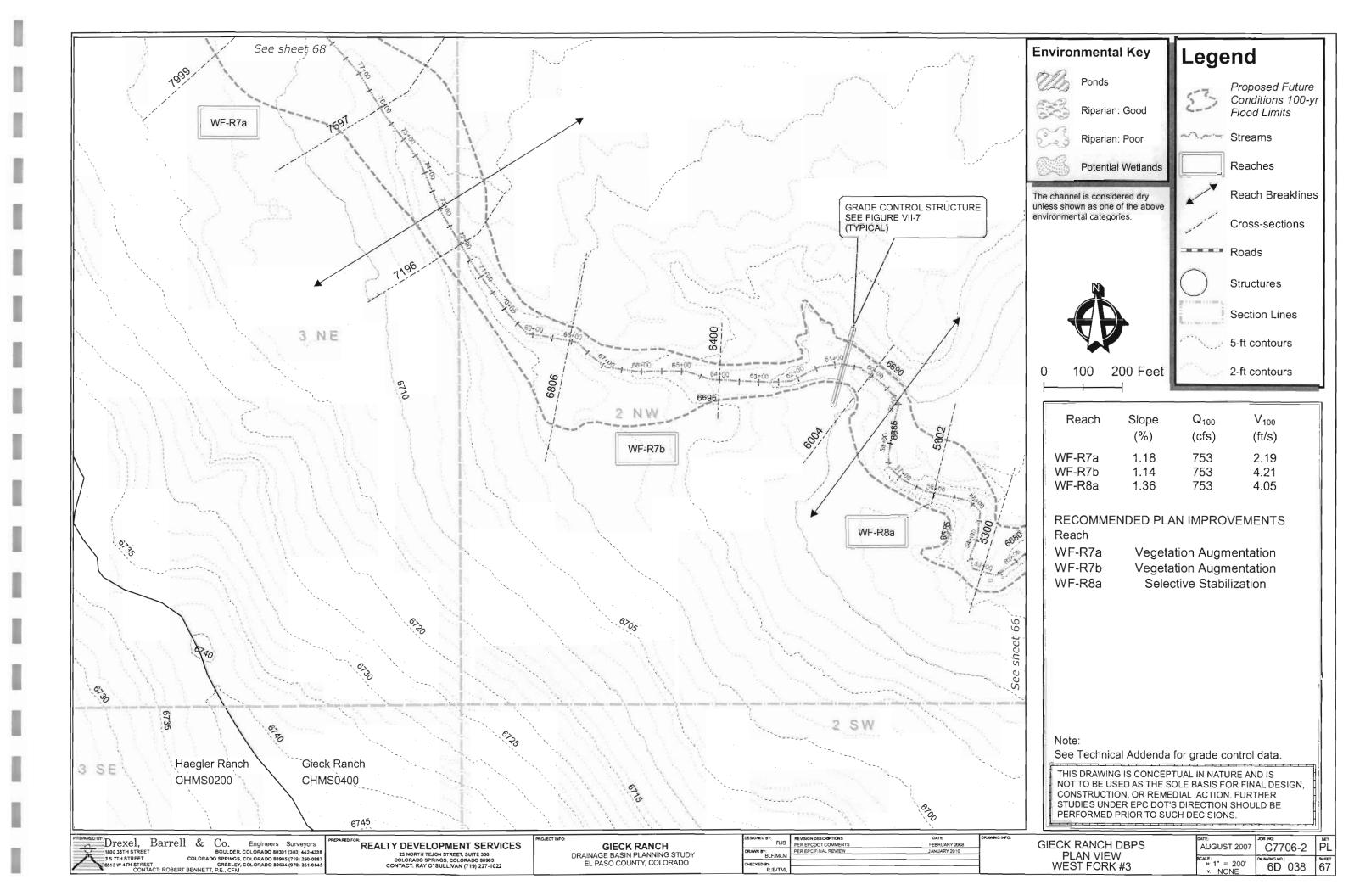
Table 13: Channel Improvements By Reach cont

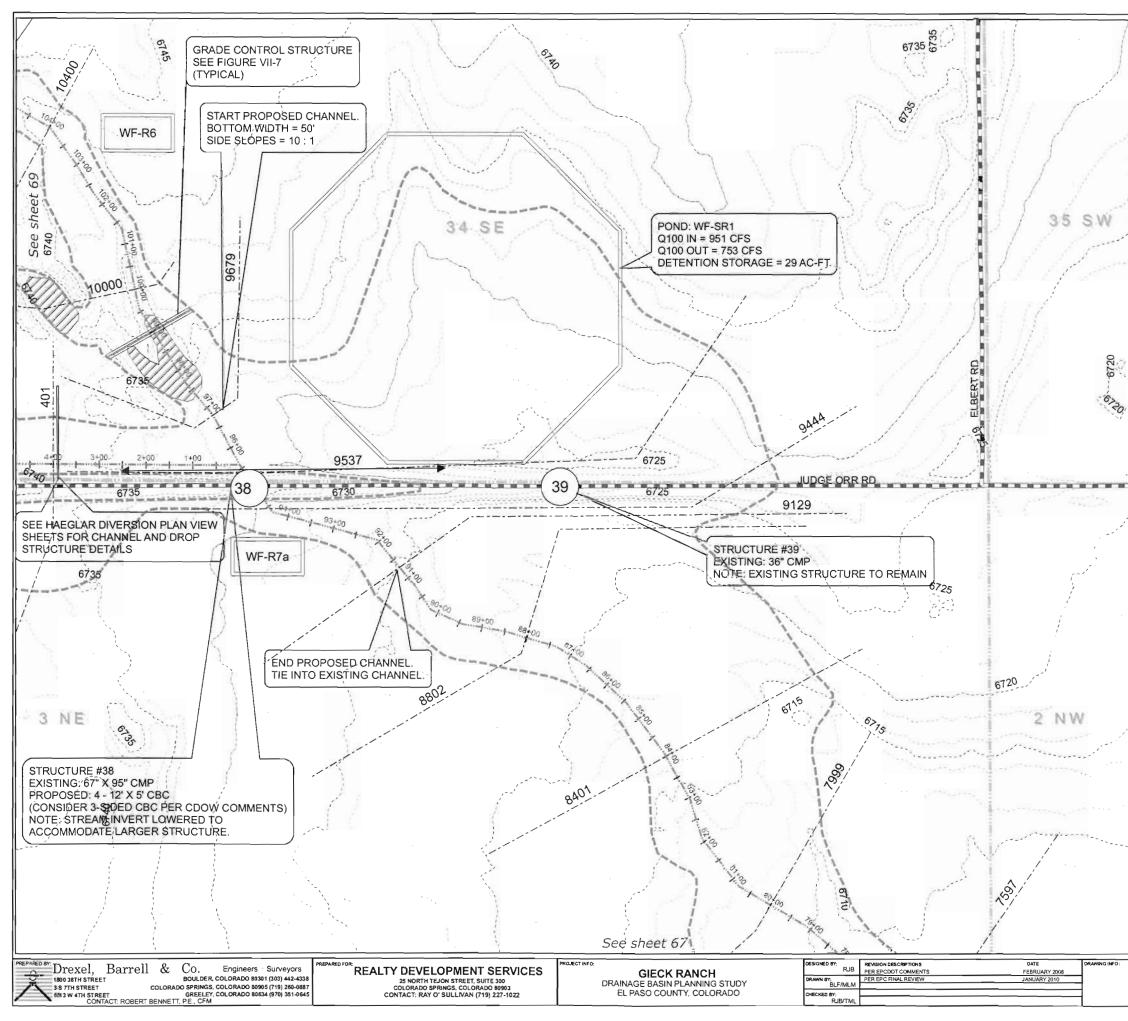
		Reach Length	
Drainageway	Reach ID	(ft)	Channel Approach
Gieck Main	MS-R20b	1227	As-needed Improvements
Gieck Main	MS-R21a	1990	As-needed Improvements
Gieck Main	MS-R21b	1584	As-needed Improvements
Gieck Main	MS-R21c	2242	As-needed Improvements
Gieck Main	MS-R22	3360	As-needed Improvements
Gieck Main	MS-R23	3268	As-needed Improvements
Gieck Main	MS-R24	1927	As-needed Improvements
Gieck Main	MS-R25a	1603	As-needed Improvements
Gieck Main	MS-R25b	1615	As-needed Improvements
Gieck Main	MS-R25c	384	As-needed Improvements
Gieck Main	MS-R26	803	As-needed Improvements
Gieck Main	MS-R27	1597	As-needed Improvements
Gieck Main	MS-R28	3599	As-needed Improvements
Gieck Main	MS-R29	797	As-needed Improvements
Gieck Main	MS-R30	2004	As-needed Improvements
Gieck Main - Sub Trib M1	MST1-R1	4799	Selective Stabilization
Gieck Main - Sub Trib M2	MST2-R1	3896	Selective Stabilization
Gieck Main - Sub Trib M2	MST2-R2	6504	Vegetation Augmentation
Gieck Main - Sub Trib M3	MST3-R1	5599	As-needed Improvements
Gieck Main - Sub Trib M4	MST4-R1	6000	Selective Stabilization
Gieck Main - Trib. M5	MST5-R1	7200	Selective Stabilization
East Fork	EF-R1	2659	As-needed Improvements
East Fork	EF-R2	2400	As-needed Improvements
East Fork	EF-R3	4800	As-needed Improvements
East Fork	EF-R4	1122	As-needed Improvements
East Fork	EF-R5	2161	As-needed Improvements
East Fork	EF-R6	1410	As-needed Improvements
East Fork	EF-R7	4876	As-needed Improvements
East Fork - Trib. EF1	EFT1-R1	3200	As-needed Improvements
East Fork - Trib. EF1	EFT1-R2a	2400	As-needed Improvements
East Fork - Trib. EF1	EFT1-R2b	4041	As-needed Improvements
East Fork - Trib. EF1	EFT1-R3	2394	As-needed Improvements
South Fork	SF-R1	2017	As-needed Improvements
South Fork	SF-R2	4120	As-needed Improvements
South Fork	SF-R3	3063	As-needed Improvements
South Fork	SF-R4	1167	As-needed Improvements
South Fork	SF-R5	2434	As-needed Improvements
South Fork	SF-R6	4799	As-needed Improvements
South Fork - Trib. SF1	SFT1-R1	2400	As-needed Improvements
Southeast Fork	SE-R1	5596	As-needed Improvements
Southeast Fork	SE-R2	2786	As-needed Improvements
Southeast Fork	SE-R3a	3209	As-needed Improvements
Southeast Fork	SE-R3b	2940	As-needed Improvements
Southeast Fork - Trib. SEF1	SET1-R1	3301	As-needed Improvements

Gieck Ranch Drainage Basin Planning Study H:\C7706-2\Reports\Revised report submittal 02-10-10.doc

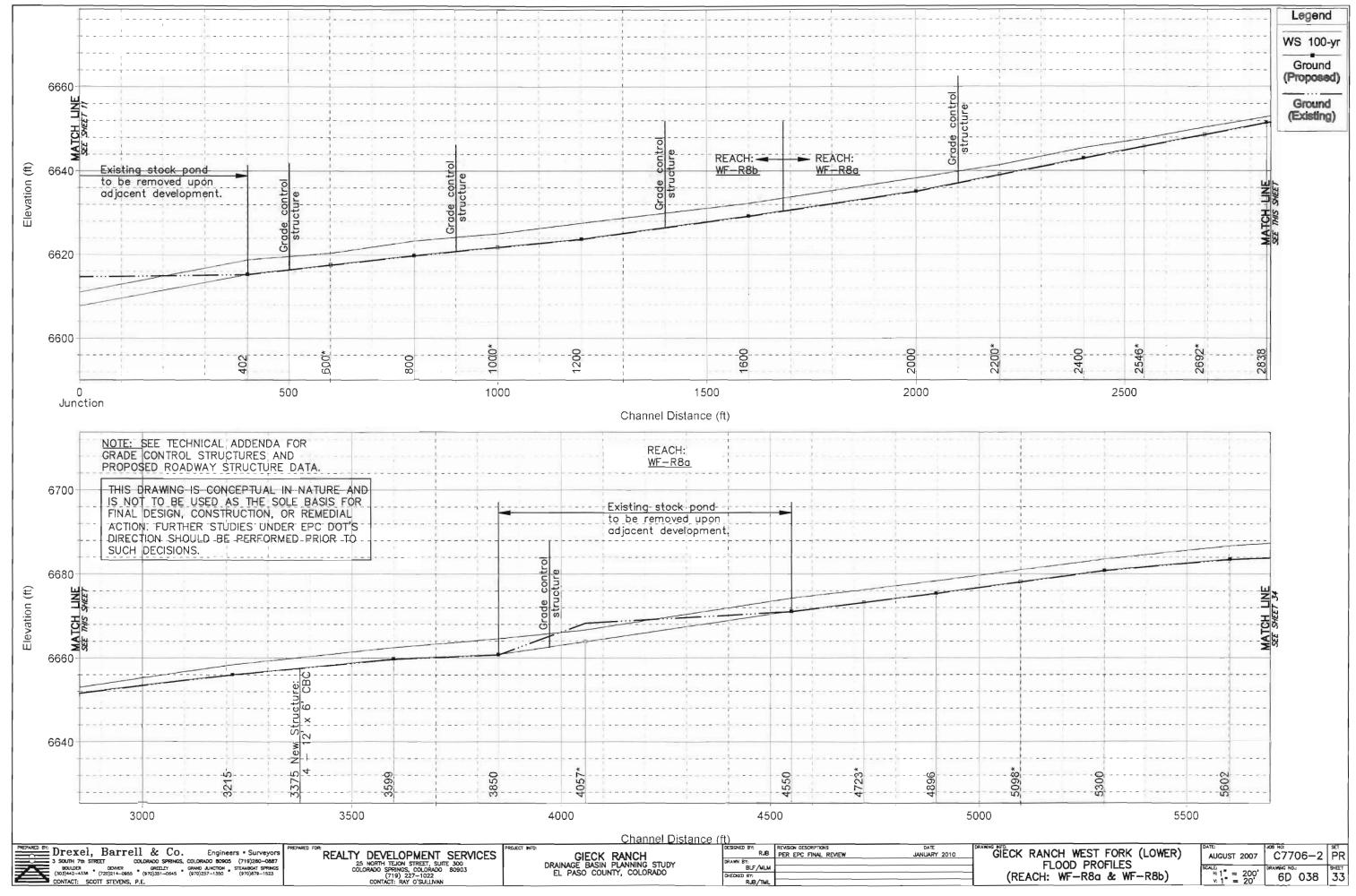


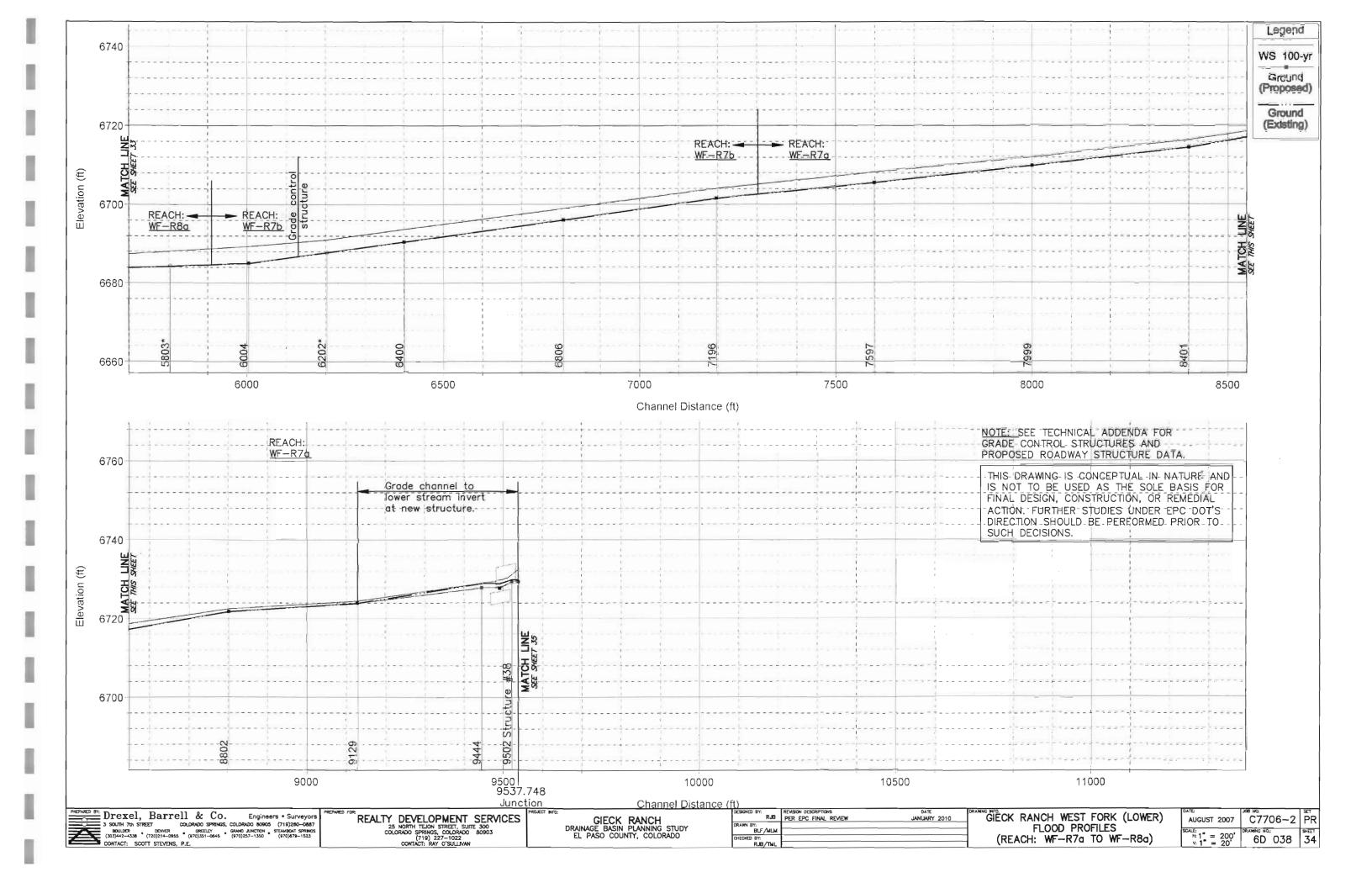






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ð.	E	~	Ripari	ian: Poor		Strea	ims	
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	en	vironme	ental cate	gories.		Cross	s-sections	
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			N	1	$\bigcirc$	Struc	tures	
~						Secti	on Lines	
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		F						
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		WI	F-R7a	Vegeta	ition Augr	nenta	tion	
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Architectural Structural Geotechnical



Materials Testing Forensic Civil/Planning

# SOIL AND GEOLOGY STUDY

Esteban Subdivsion 3 parcels totaling 496.25 acres EL Paso County, Colorado

# **PREPARED FOR:**

William Guman & Associates, Ltd 731 North Weber Street, Ste 10 Colorado Springs, CO 80903

**JOB NO. 190388** 

April 27, 2023

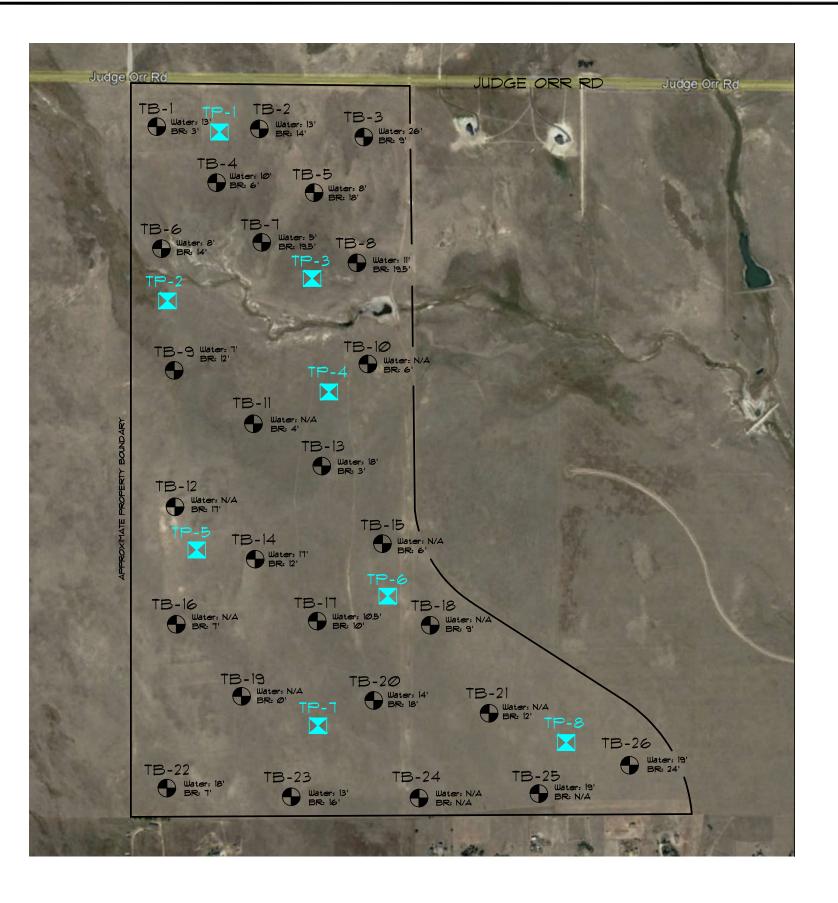
Respectfully Submitted, RMG – Rocky Mountain Group Reviewed by, RMG – Rocky Mountain Group



Tony Munger, P.E. Sr. Geotechnical Project Manager

Kelli Ziler

Kelli Zigler Project Geologist

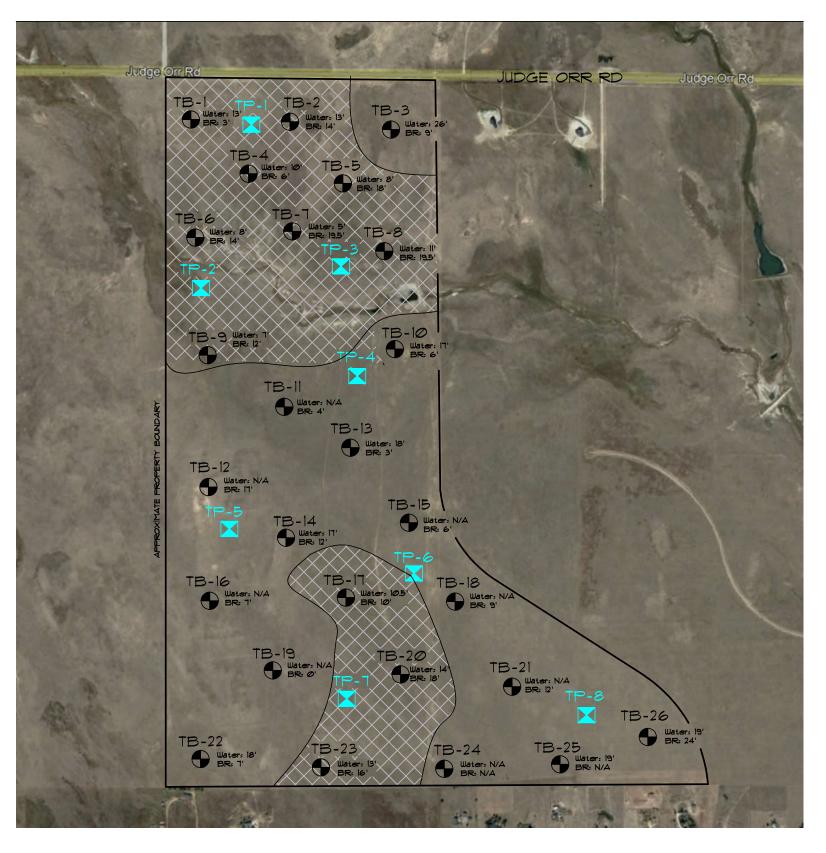




Water: Groundwater Depth on 2/28/23 BR: Bedrock depth at time of drilling DENOTES APPROXIMATE LOCATION OF TEST PITS



JOB No. 190388 Forens Engineer (719) 5 Southern 7 Architecture Structural Geotechnical PASO COUNTY, COLORADO WILLIAM GUMAN AND ASSOCIATES, LTD **ESTEBAN SUBDIVISION** Щ ENGINEER: DRAWN BY: CHECKED BY: 4-27-2023 ISSUED: TEST BORING/TEST PIT LAYOUT PLAN SHEET NO. FIG-3



DENOTES APPROXIMATE LOCATION OF TEST BORINGS

> Water: Groundwater Depth on 2/28/23 BR: Bedrock depth at time of drilling

DENOTES APPROXIMATE LOCATION OF TEST PITS



AREAS WHERE GROUNDWATER IS LESS THAN 15 FEET FROM THE SURFACE, ADDITIONAL INVESTIGATIONS MAY BE PROPOSED TO DETERMINE BASEMENT FEASIBILITY.

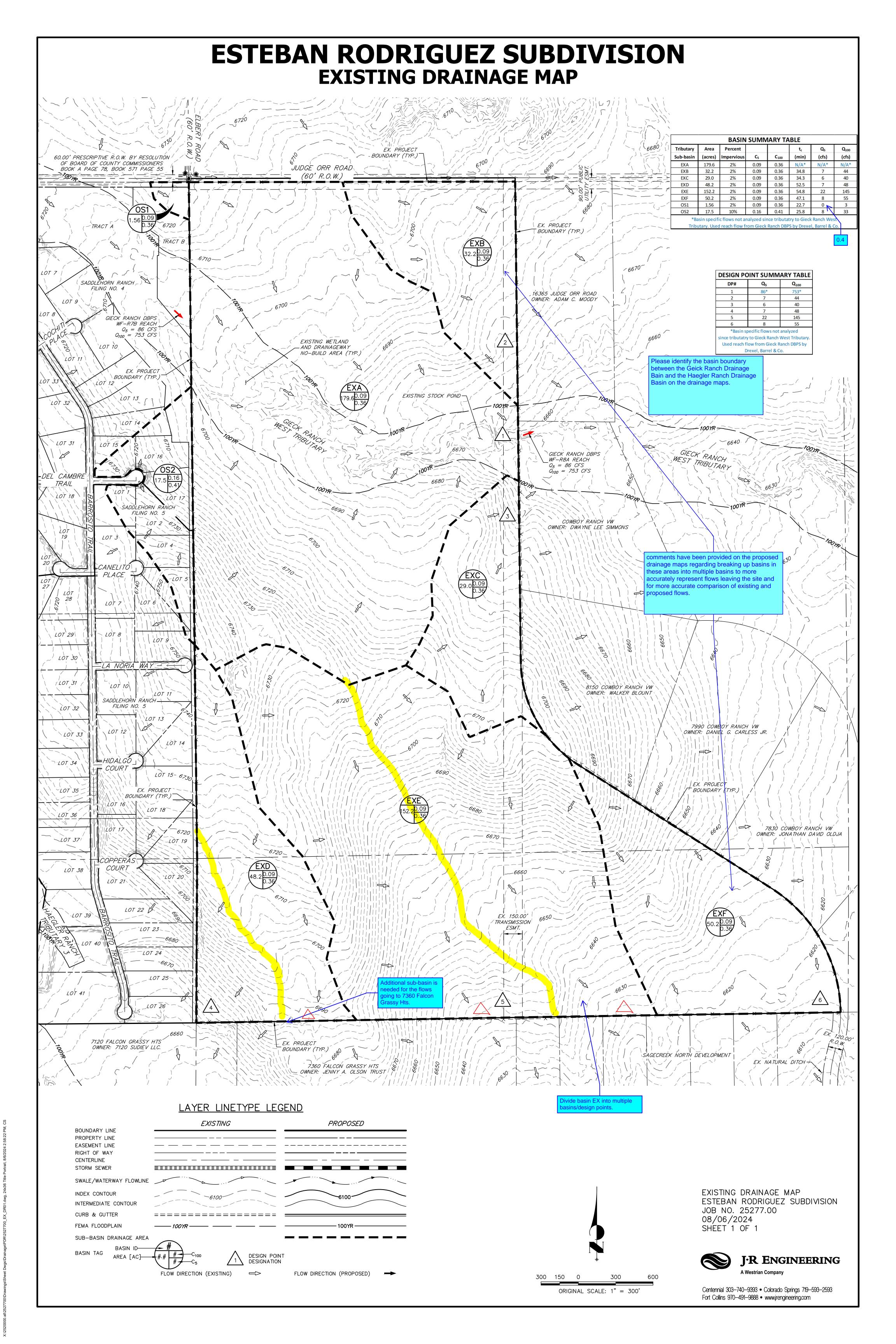


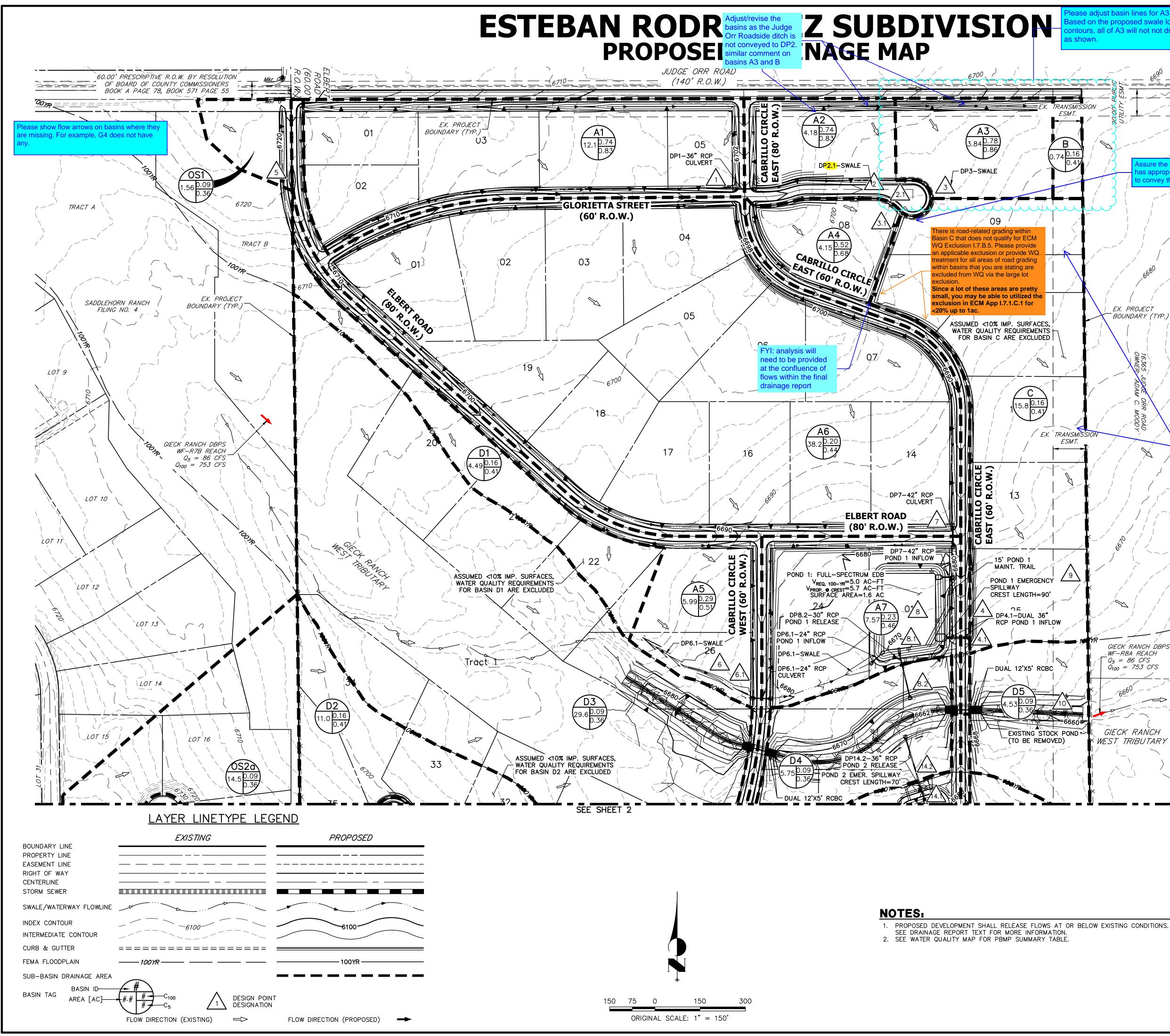
JOB No. 190388 (719) Thern <sup>1</sup> Architecture Structural Geotechnical PASO COUNTY, COLORADO WILLIAM GUMAN AND ASSOCIATES, LTD **ESTEBAN SUBDIVISION** Щ ENGINEER: DRAWN BY: CHECKED BY: 4-27-2023 ISSUED: BASEMENT FEASIBILITY MAP SHEET NO. FIG-31

Preliminary Drainage Report for Esteban Rodriguez Subdivision

# APPENDIX E

# **DRAINAGE MAPS**





		ART IA					d on the proposed swale location
$t_c$ $Q_5$ $Q_{100}$		<u> </u>	6	Percent	Area	Tributary	ours, all of A3 will not not drain to DP3
(min) (cfs) (cfs) 13.4 33 62		<b>C</b> <sub>100</sub>		Impervious 85%	(acres) 12.1	Sub-basin	iown.
8.7 12 23		0.85	100 BEAD	72%	4.18	A1 A2	
9.5 12 23		0.85	0.76	88%	3.84	A3	~ ~ ^ o
25.4 3 10 28.8 4 13 0.2		0.50		26%	4.15	A4	$\underline{}$
28.8         4         13         0.2           29.7         19         70		0.51 0.44		26% 15%	5.99 38.2	A5 A6	
13.2 7 22		0.47		21%	7.57	A7	
17.0 0 2		0.36		2%	0.74	B	
<u>19.1</u> 8 34		0.41		10%	15.8	C	
14.6         3         11           17.2         6         25		0.41 0.41		10% 10%	4.49 11.0	D1 D2	
N/A* N/A* N/A*		0.36		2%	29.6	D3	
N/A* N/A* N/A* Pr/A*		0.36	0.09	2%	5.75	D4	Assure the easement
N/A* N/A* N/A* be		0.36		2%	4.53	D5	has appropriate width
		0.44		16%	28.7	E1	to convey the flows.
15.6     3     6       23.2     26     93		0.68 0.44		55% 16%	1.63 43.5	E2 E3	
27.0 9 40		0.41		10%	22.0	F	i i
24.6 9 35		0.43		13%	17.6	G1	
28.4 9 33		0.44		15%	17.6	G2	L j (
17.8         5         15           27.4         10         39		0.49 0.43		22% 14%	5.70 20.4	G3 G4	
20.0 6 23		0.43		14%	10.4	G4 G5	
24.4 12 47		0.42		12%	24.0	H1	
34.2 17 67	34.2	0.42	0.17	12%	41.8	H2	6680
27.8 11 41		0.44		15%	21.3	H3	
29.2         3         6           28.2         4         9		0.68		54% 50%	1.96 3.18	H4 H5	$\mathbf{T}$
37.9 13 54		0.05		11%	36.6	H6	EX. PROJECT
18.6 24 103		0.41		10%	46.8	1	BOUNDARY (TYP.)
21.3 1 3		0.41		10%	1.56	OS1	
27.3         3         23           23.5         1         5		0.36 0.36		2% 2%	14.5 3.06	OS2a OS2b	
to Gieck Ranch West by Drexel, Barrel & Co.	ry to Gieck	e tributa	alyzed since	c flows not an	sin specifi	*Ba	0WNE
				ESIGN PO		THU	ER JU
	Q <sub>100</sub>		Q <sub>5</sub>	DP#			DAM
62			33	1			C SAR
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82			43	2.1		vhere in C flows wi	MOODY There a places we sub-base
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102         10         111         3         13         16         70         22         178         32         36	10         111         3         13         16         70         22         178         32         36		3 56 1 4 5 19 7 68 1 8	4.1 5 6 6.1 7 8 8 8.1 8.2 9		ely show how s are leaving	accurate the flow the site.
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102         10         111         3         13         16         70         22         178         32         36	10         111         3         13         16         70         22         178         32         36         753*         5		3 56 1 4 5 19 7 68 1 8	4.1 5 6 6.1 7 8 8 8.1 8.2 9		ely show how s are leaving	accurate the flow the site.
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$ \begin{array}{c} 102\\ 10\\ 111\\ 3\\ 13\\ 16\\ 70\\ 22\\ 178\\ 32\\ 36\\ 753*\\ 5\\ 6\\ 93\\ 165\\ 45\\ 40\\ 35\\ 33\\ \end{array} $	10         111         3         13         16         70         22         178         32         36         753*         5         69         75         6         93         165         45         40         35         33         63         15		3 56 1 4 5 19 7 68 1 8 $86^*$ 1 19 20 3 26 46 0 9 9 9 9 9	4.1         5         6         6.1         7         8         8.1         8.2         9         10         11         12         13         14         14.1         14.2         15         16         17		ely show how s are leaving	accurate the flow the site.

WEST TRIBUTARY

22.1 23.1 24.1 25.1 26.1 26.2 \*Basin specific flows not analyzed ince tributary to Gieck Ranch West Tributar

19.1

20.1

20.2

Used reach flow from Gieck Ranch DBPS by Drexel, Barrel & Co. PROPOSED DRAINAGE MAP ESTEBAN RODRIGUEZ SUBDIVISION JOB NO. 25277.00 10/22/2024

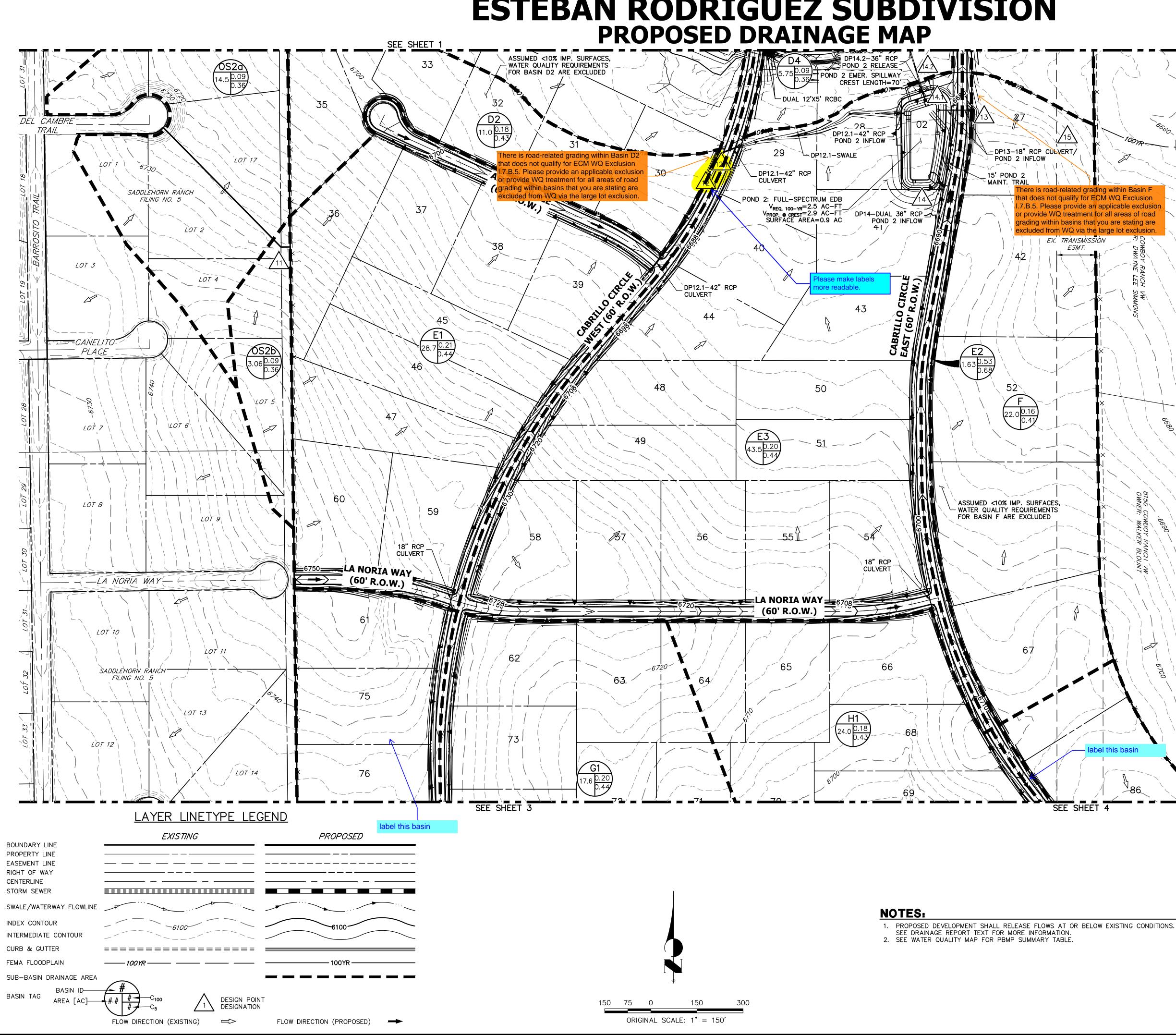
ounding error, should be 3

SHEET 1 OF 4



J·R ENGINEERING A Westrian Company

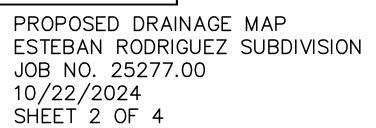
Centennial 303-740-9393 • Colorado Springs 719-593-2593 Fort Collins 970-491-9888 • www.jrengineering.com



# **ESTEBAN RODRIGUEZ SUBDIVISION**

Tributary	Area	Percent			t <sub>c</sub>	Q₅	<b>Q</b> <sub>100</sub>
Sub-basin	(acres)	Impervious	C₅	<b>C</b> <sub>100</sub>	(min)	(cfs)	(cfs)
A1	12.1	85%	0.74	0.83	13.4	33	62
A2	4.18	72%	0.64	0.76	8.7	12	23
A3	3.84	88%	0.76	0.85	9.5	12	23
A4	4.15	26%	0.29	0.50	25.4	3	10
A5	5.99	26%	0.29	0.51	28.8	4	13
A6	38.2	15%	0.20	0.44	29.7	19	70
A7	7.57	21%	0.25	0.47	13.2	7	22
В	0.74	2%	0.09	0.36	17.0	0	2
С	15.8	10%	0.16	0.41	19.1	8	34
D1	4.49	10%	0.16	0.41	14.6	3	11
D2	11.0	10%	0.16	0.41	17.2	6	25
D3	29.6	2%	0.09	0.36	N/A*	N/A*	N/A <sup>3</sup>
D4	5.75	2%	0.09	0.36	N/A*	N/A*	N/A
D5	4.53	2%	0.09	0.36	N/A*	N/A*	N/A
E1	28.7	16%	0.21	0.44	18.0	19	69
E2	1.63	55%	0.53	0.68	15.6	3	6
E3	43.5	16%	0.21	0.44	23.2	26	93
F	22.0	10%	0.16	0.41	27.0	9	40
G1	17.6	13%	0.19	0.43	24.6	9	35
G2	17.6	15%	0.20	0.44	28.4	9	33
G3	5.70	22%	0.26	0.49	17.8	5	15
G4	20.4	14%	0.19	0.43	27.4	10	39
G5	10.4	12%	0.17	0.42	20.0	6	23
H1	24.0	12%	0.17	0.42	24.4	12	47
H2	41.8	12%	0.17	0.42	34.2	17	67
H3	21.3	15%	0.20	0.44	27.8	11	41
H4	1.96	54%	0.52	0.68	29.2	3	6
H5	3.18	<b>50%</b>	0.49	0.65	28.2	4	9
H6	36.6	11%	0.17	0.41	37.9	13	54
I	46.8	10%	0.16	0.41	18.6	24	103
OS1	1.56	10%	0.16	0.41	21.3	1	3
OS2a	14.5	2%	0.09	0.36	27.3	3	23
OS2b	3.06	2%	0.09	0.36	23.5	1	5

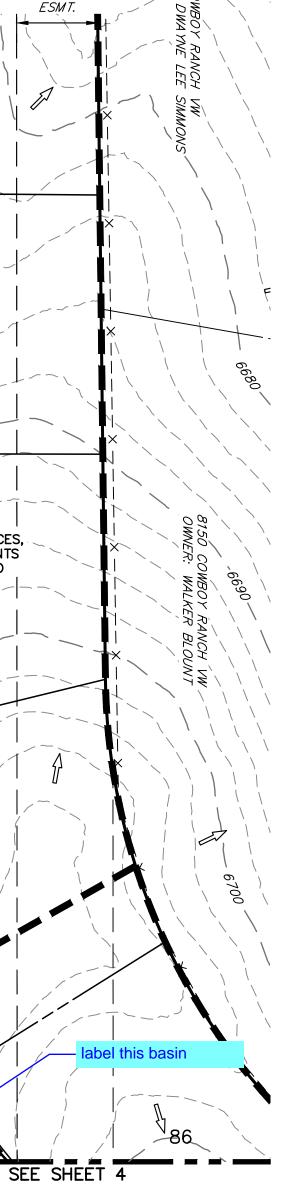
DP#	Q <sub>5</sub>	<b>Q</b> <sub>100</sub>
1	33	62
2	12	23
2.1	43	82
3	12	23
3.1	54	102
4	3	10
4.1	56	111
5	1	3
6	4	13
6.1	5	16
7	19	70
8	7	22
8.1	68	178
8.2	1	32
9	8	32
10	86*	753*
10	1	5
11	19	69
12.1	20	75 6
13		
14	26	93
14.1	46	165
14.2	0	45
15	9	40
16	9	35
17	9	33
17.1	16	63
18	5	15
18.1	19	72
19	10	39
19.1	27	108
20	6	23
20.1	29	120
20.2	0	32
21	12	47
22	17	67
22.1	26	106
23	11	41
23.1	34	139
24	3	6
24.1	37	144
25	4	9
25.1	37	145
26	13	54
26.1	47	196
26.2	0	42
27	24	103
	ecific flows not to Gieck Ranch V	4

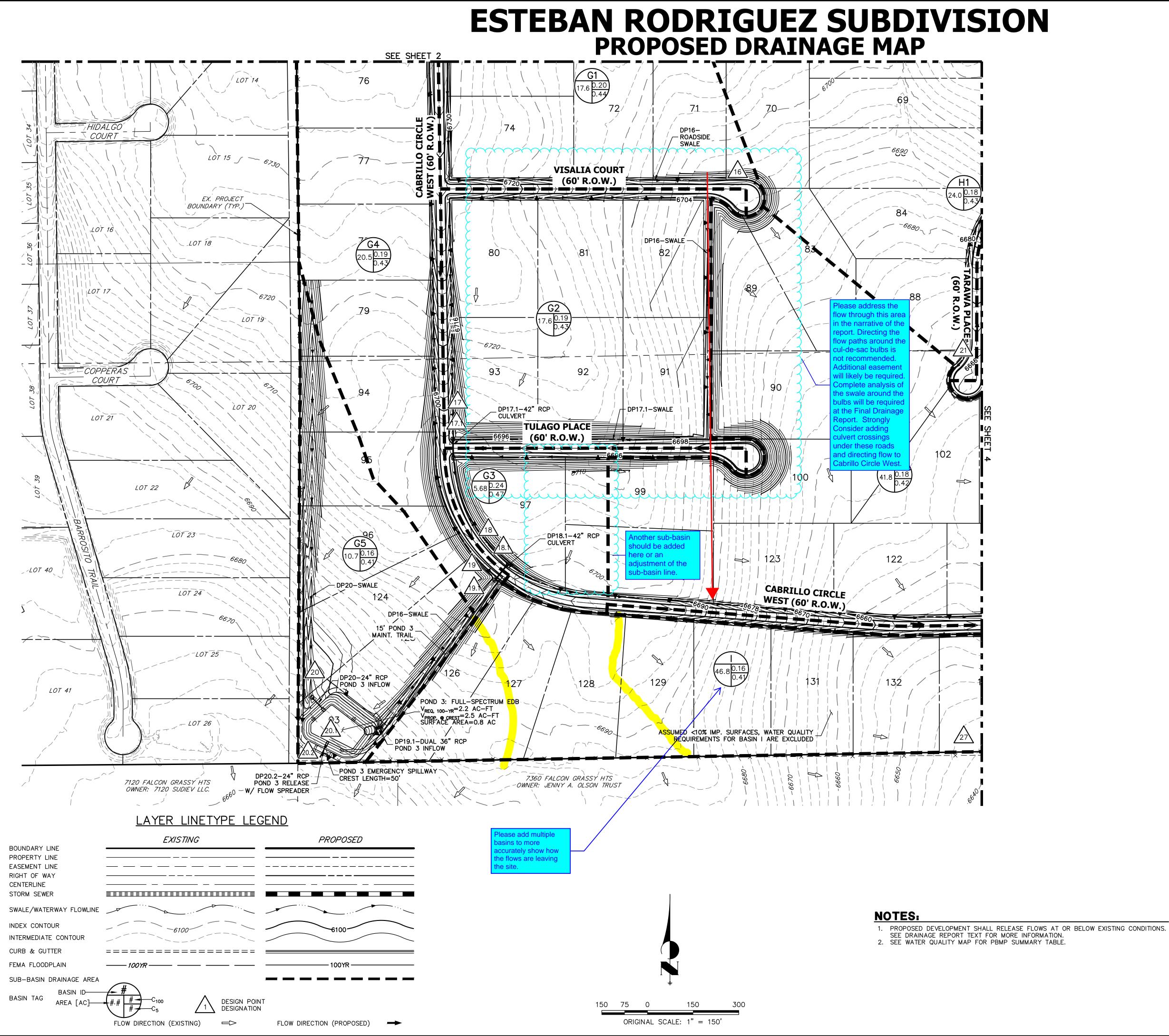




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BASIN SUMMARY TABLE							
Tributary	Area	Percent			t <sub>c</sub>	Q₅	<b>Q</b> <sub>100</sub>
Sub-basin	(acres)	Impervious	C <sub>5</sub>	<b>C</b> <sub>100</sub>	(min)	(cfs)	(cfs)
A1	12.1	85%	0.74	0.83	13.4	33	62
A2	4.18	72%	0.64	0.76	8.7	12	23
A3	3.84	88%	0.76	0.85	9.5	12	23
A4	4.15	26%	0.29	0.50	25.4	3	10
A5	5.99	<mark>26%</mark>	0.29	0.51	28.8	4	13
A6	38.2	15%	0.20	0.44	29.7	19	70
A7	7.57	21%	0.25	0.47	13.2	7	22
В	0.74	2%	0.09	0.36	17.0	0	2
С	15.8	10%	0.16	0.41	19.1	8	34
D1	4.49	10%	0.16	0.41	14.6	3	11
D2	11.0	10%	0.16	0.41	17.2	6	25
D3	29.6	2%	0.09	0.36	N/A*	N/A*	N/A*
D4	5.75	2%	0.09	0.36	N/A*	N/A*	N/A*
D5	4.53	2%	0.09	0.36	N/A*	N/A*	N/A*
E1	28.7	16%	0.21	0.44	18.0	19	69
E2	1.63	55%	0.53	0.68	15.6	3	6
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G5	10.4	12%	0.17	0.42	20.0	6	23
H1	24.0	12%	0.17	0.42	24.4	12	47
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H3	21.3	15%	0.20	0.44	27.8	11	41
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H5	3.18	50%	0.49	0.65	28.2	4	9
H6	36.6	11%	0.17	0.41	37.9	13	54
1	46.8	10%	0.16	0.41	18.6	24	103
OS1	1.56	10%	0.16	0.41	21.3	1	3
OS2a	14.5	2%	0.09	0.36	27.3	3	23
OS2b	3.06	2%	0.09	0.36	23.5	1	5
		ic flows not a I reach flow f					

DP#	Q <sub>5</sub>	<b>Q</b> <sub>100</sub>
1	33	62
2	12	23
2.1	43	82
3	12	23
3.1	54	102
4	3	10
4.1	56	111
5	1	3
6	4	13
6.1	5	16
7	19	70
8	7	22
8.1	68	178
8.2	1	32
9	8	36
10	86*	753*
10	1	5
11	19	69
12.1	20	75
13	3	6
14	26	93
14.1	46	165
14.2	0	45
15	9	40
16	9	35
17	9	33
17.1	16	63
18	5	15
18.1	19	72
19	10	39
19.1	27	108
20	6	23
20.1	29	120
20.2	0	32
21	12	47
22	17	67
22.1	26	106
23	11	41
23.1	34	139
24	3	6
24.1	37	144
25	4	9
25.1	37	145
26	13	54
26.1	47	196
26.2	0	42
27	24	103
*Basin sp e tributary 1	ecific flows not	

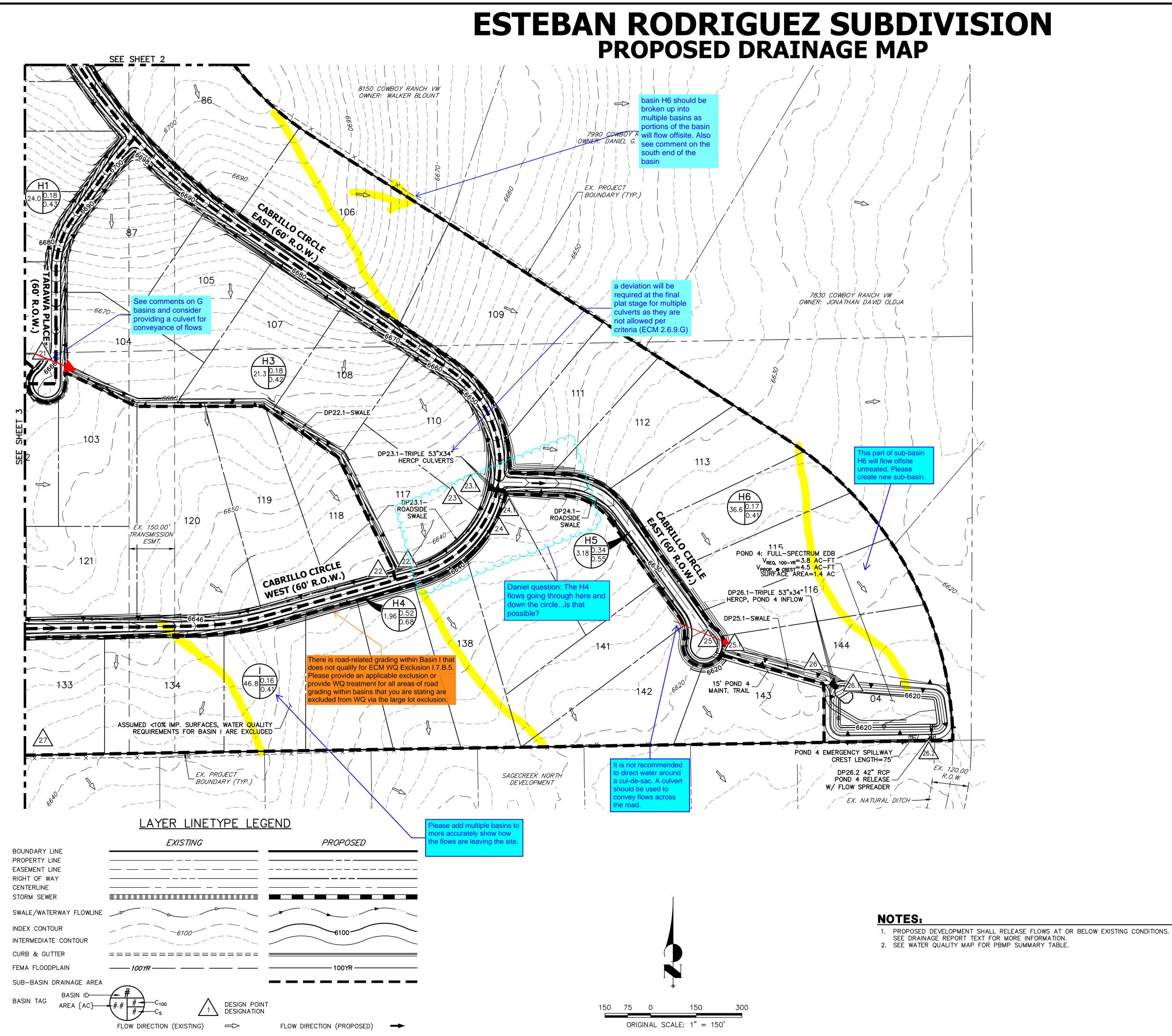
Drexel, Barrel & Co.

PROPOSED DRAINAGE MAP ESTEBAN RODRIGUEZ SUBDIVISION JOB NO. 25277.00 10/22/2024 SHEET 3 OF 4



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BASIN SUMMARY TABLE							
Tributary	Area	Percent			t <sub>c</sub>	Q₅	<b>Q</b> <sub>100</sub>
Sub-basin	(acres)	Impervious	C <sub>5</sub>	<b>C</b> <sub>100</sub>	(min)	(cfs)	(cfs)
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A3	3.84	88%	0.76	0.85	9.5	12	23
A4	4.15	26%	0.29	0.50	25.4	3	10
A5	5.99	<mark>26%</mark>	0.29	0.51	28.8	4	13
A6	38.2	15%	0.20	0.44	29.7	19	70
A7	7.57	21%	0.25	0.47	13.2	7	22
В	0.74	2%	0.09	0.36	17.0	0	2
С	15.8	10%	0.16	0.41	19.1	8	34
D1	4.49	10%	0.16	0.41	14.6	3	11
D2	11.0	10%	0.16	0.41	17.2	6	25
D3	29.6	2%	0.09	0.36	N/A*	N/A*	N/A*
D4	5.75	2%	0.09	0.36	N/A*	N/A*	N/A*
D5	4.53	2%	0.09	0.36	N/A*	N/A*	N/A*
E1	28.7	16%	0.21	0.44	18.0	19	69
E2	1.63	55%	0.53	0.68	15.6	3	6
E3	43.5	16%	0.21	0.44	23.2	26	93
F	22.0	10%	0.16	0.41	27.0	9	40
G1	17.6	13%	0.19	0.43	24.6	9	35
G2	17.6	15%	0.20	0.44	28.4	9	33
G3	5.70	22%	0.26	0.49	17.8	5	15
G4	20.4	14%	0.19	0.43	27.4	10	39
G5	10.4	12%	0.17	0.42	20.0	6	23
H1	24.0	12%	0.17	0.42	24.4	12	47
H2	41.8	12%	0.17	0.42	34.2	17	67
H3	21.3	15%	0.20	0.44	27.8	11	41
H4	1.96	54%	0.52	0.68	29.2	3	6
H5	3.18	50%	0.49	0.65	28.2	4	9
H6	36.6	11%	0.17	0.41	37.9	13	54
1	46.8	10%	0.16	0.41	18.6	24	103
OS1	1.56	10%	0.16	0.41	21.3	1	3
OS2a	14.5	2%	0.09	0.36	27.3	3	23
OS2b	3.06	2%	0.09	0.36	23.5	1	5
		ic flows not a I reach flow f					

DP#	$Q_5$	<b>Q</b> <sub>100</sub>
1	33	62
2	12	23
2.1	43	82
3	12	23
3.1	54	102
4	3	10
4.1	56	111
5	1	3
6	4	13
6.1	5	16
7	19	70
8	7	22
8.1	68	178
8.2	1	32
9	8	32
9 10	o 86*	753*
10	1	5
11	19	69
12.1	20	75
13	3	6
14	26	93
14.1	46	165
14.2	0	45
15	9	40
16	9	35
17	9	33
17.1	16	63
18	5	15
18.1	19	72
19	10	39
19.1	27	108
20	6	23
20.1	29	120
20.2	0	32
21	12	47
22	17	67
22.1	26	106
23	11	41
23.1	34	139
24	3	6
24.1	37	144
25	4	9
25.1	37	145
26	13	54
26.1	47	196
26.2	0	42
27	24	103
	<b>2</b> 7	105

Drexel, Barrel & Co. PROPOSED DRAINAGE MAP

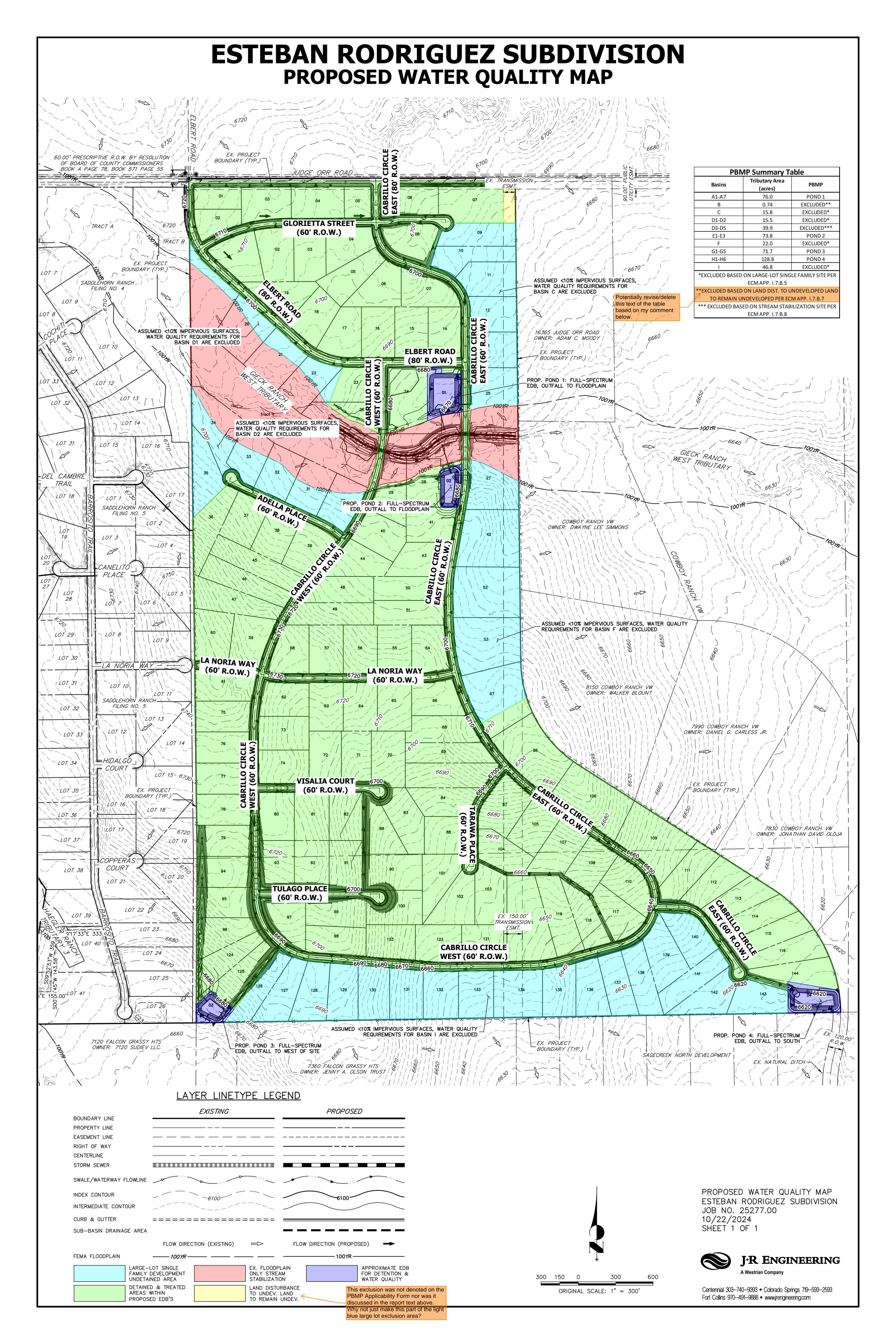
ESTEBAN RODRIGUEZ SUBDIVISION JOB NO. 25277.00 10/22/2024



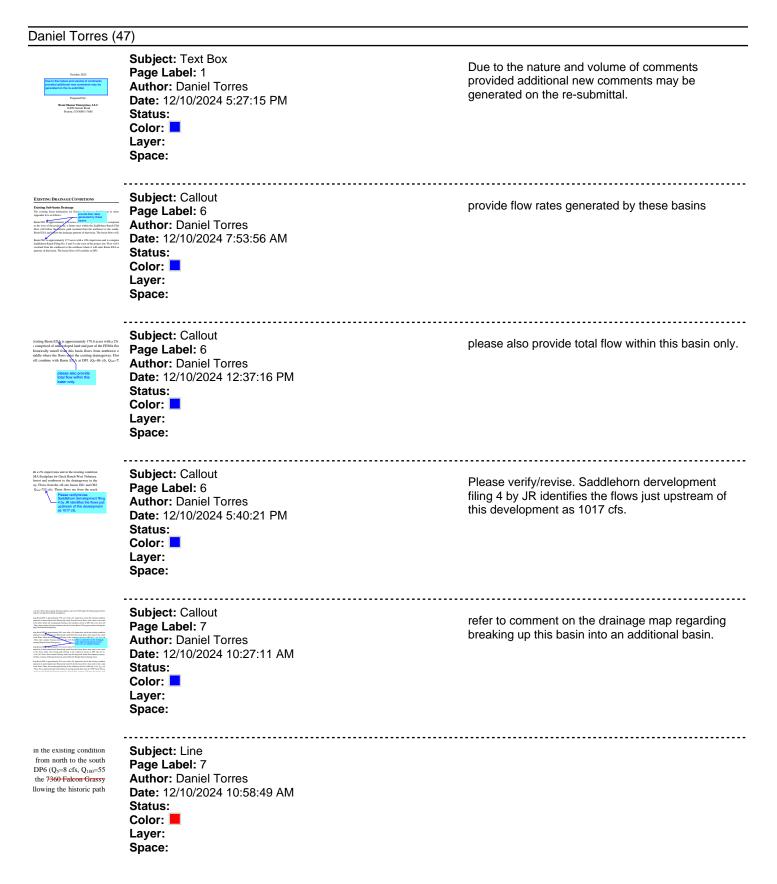
SHEET 4 OF 4

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# v1\_Drainage Report - Preliminary.pdf Markup Summary



s at DP6 (Q=8 cfs, Qnu=55 conto the 7350 Falcon Greasy s following the histof this parcel is west of Basin EXF. Remove	Subject: Callout Page Label: 7 Author: Daniel Torres Date: 12/10/2024 10:59:55 AM Status: Color: Layer: Space:	this parcel is west of Basin EXF. Remove
A first state is the state state state is the state st	Subject: Text Box Page Label: 8 Author: Daniel Torres Date: 12/10/2024 11:07:11 AM Status: Color: Layer: Space:	please also account/address the improvements to Judge Orr Road as well as the turn lane improvements at each of the proposed intersections to Judge Orr.
area with an SSN inspection and is computed of program (Gaussian States and seek thif of Cabasily, Cabas	Subject: Callout Page Label: 8 Author: Daniel Torres Date: 12/10/2024 11:11:03 AM Status: Color: Layer: Space:	show the culvert on the drainage map
remeased by headed and space to any measure of it is of relationships of the output production of the production of the composition of the strength of the production of the composition of the production of the strength of the production of the production of the strength of the strength of the strength of the production of the strength of the strength of the strength of the strength of the strength of the strength of the strength of the strength of the strength of the strength of the strength of the strength of the strength of the strength of the strength of the strength of the strength of the strength of the strength of the strength of the strength of the strength of the strength of the strength of the strength of the strength of the strength of the strength of the strength of the strength of the strength of the strength of the strength of the strength of the strength of the strength of the strength of the strength of the strength of the strength of the strength of the strength of the strength of the strength of the strength of the strength of the strength of the strength of the strength of the strength of the strength of the strength of the streng	Subject: Callout Page Label: 8 Author: Daniel Torres Date: 12/10/2024 11:12:44 AM Status: Color: Layer: Space:	please clarify whether the judge orr roadside ditch is also part of this basin and will be conveyed to DP1
<text><text><text><text></text></text></text></text>	Subject: Callout Page Label: 8 Author: Daniel Torres Date: 12/10/2024 4:14:43 PM Status: Color: Layer: Space:	consider accounting for a higher impervious for this commercial area to avoid limitations at site development of this area. Typical commercial/industrial areas are 80-95% impervious per table 6-6 in DCM
combine with DP2.1 within the pr within a proposed space in the com- monstrained space in the second space of the second family of second space of the second space of the second response of the second space of the second space of the results of the second space of the second space of the second space of the second space of the second space of the second space of the second space of the second space of the second space of the second space of the second space of t	Subject: Callout Page Label: 8 Author: Daniel Torres Date: 12/10/2024 11:56:33 AM Status: Color: Layer: Space:	please clarify if this is intended to be the roadside ditch/swale along Cabrillo Circle

Image: A status of the stat	Subject: Callout Page Label: 9 Author: Daniel Torres Date: 12/10/2024 12:01:39 PM Status: Color: Layer: Space:	revise as this total does not appear to include DP4+DP3.1 flows. 111 cfs indicated in the drainage table.
<text><text><text></text></text></text>	Subject: Callout Page Label: 10 Author: Daniel Torres Date: 12/10/2024 12:25:59 PM Status: Color: Layer: Space:	identify the flows generated from these basins. The impact to the channel due to the increase in flows from the lots within these basins will need to be analyzed
<text><text><text><text><text><text></text></text></text></text></text></text>	Subject: Callout Page Label: 10 Author: Daniel Torres Date: 12/10/2024 4:21:28 PM Status: Color: Layer: Space:	Provide a design point at the culvert crossings and identify the total flows at this crossings inclusive of the increase in flows from this site and saddlehorn lots that drain to the channel that have not been detained.
provide design points with proposed channel crossings by of the basis. The only proposed two sets of dual 12" 5.5" KCHC to construct a set of dual 12" 5.5" KCHC to the sets of dual 13" 5.5" KCHC to the sets of	Subject: Text Box Page Label: 11 Author: Daniel Torres Date: 12/10/2024 12:34:32 PM Status: Color: Layer: Space:	provide design points with total flows at the two proposed channel crossings
	Subject: Callout Page Label: 11 Author: Daniel Torres Date: 12/10/2024 5:24:15 PM Status: Color: Layer: Space:	Total flows for this development should be analyzed and not just depend on the DBPS flows.
Attive 2 (2) (2) (2) (2) (2) (2) (2) (2) (2) (	Subject: Callout Page Label: 13 Author: Daniel Torres Date: 12/10/2024 4:30:56 PM Status: Color: Layer: Space:	indicate which swale (i.e. DP22.1 Swale)

And the information of a location of the Pice and the analysis of the pice of	Subject: Callout Page Label: 13 Author: Daniel Torres Date: 12/10/2024 3:39:18 PM Status: Color: Layer: Space:	this should be broken up into two basin for east and west Cabrillo Circle to accurately indicate the flows in the roadside swales
<text></text>	Subject: Callout Page Label: 13 Author: Daniel Torres Date: 12/10/2024 3:45:29 PM Status: Color: Layer: Space:	this basin should be broken into multiple basins as the flow leaves the site at multiple locations
■ Report for E-Solven Rodrigues Subinion and how presenters represented and Appendix B. The solvent for calling and appendix and appendix and appendix and appendix append	Subject: Callout Page Label: 14 Author: Daniel Torres Date: 12/10/2024 5:34:20 PM Status: Color: Layer: Space:	see comments on drainage map and adjust accordingly.
i riprag, winch win prevent son crosses, want will be lined in a TRM that will The modeled results of the existing and proposed improvements are raneed consistent with the DBPS.how and be proposed and be pr	Subject: Text Box Page Label: 15 Author: Daniel Torres Date: 12/10/2024 5:53:10 PM Status: Color: Layer: Space:	please identify whether the proposed improvements are consistent with the DBPS. how do the proposed recommendations compare to the DBPS recommendations?
RAULIC CALCULATIONS as this is a prefirminary damage report, Juther review of the hydraulic calculations will be report in comparison with the CD's. These hydraulic calcu- athough be removed.	Subject: Text Box Page Label: 1 Author: Daniel Torres Date: 12/10/2024 4:44:59 PM Status: Color: Layer: Space:	as this is a preliminary drainage report , further review of the hydraulic calculations will be provided with the final drainage report in conjuction with the CD's. These hydraulic calcs. should be removed.
An example of the second secon	Subject: Text Box Page Label: 1 Author: Daniel Torres Date: 12/10/2024 4:46:15 PM Status: Color: Layer: Space:	Please identify the basin boundary between the Geick Ranch Drainage Bain and the Haegler Ranch Drainage Basin on the drainage maps.



Subject: Highlight Page Label: 1 Author: Daniel Torres Date: 12/10/2024 10:19:17 AM Status: Color: Layer: Space:



Subject: Polygon Page Label: 1 Author: Daniel Torres Date: 12/10/2024 10:21:58 AM Status: Color: Layer: Space:

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Subject: Polygon Page Label: 1 Author: Daniel Torres Date: 12/10/2024 10:22:06 AM Status: Color: Layer: Space:



Subject: Highlight Page Label: 1 Author: Daniel Torres Date: 12/10/2024 10:23:15 AM Status: Color: Layer: Space:



Subject: Highlight Page Label: 1 Author: Daniel Torres Date: 12/10/2024 10:23:23 AM Status: Color: Layer: Space:



Subject: Highlight Page Label: 1 Author: Daniel Torres Date: 12/10/2024 10:23:25 AM Status: Color: Layer: Space:

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Subject: Polygon Page Label: 1 Author: Daniel Torres Date: 12/10/2024 10:24:39 AM Status: Color: Layer: Space:



Subject: Text Box Page Label: 1 Author: Daniel Torres Date: 12/10/2024 5:33:37 PM Status: Color: Layer: Space:

Subject: Callout Page Label: [1] 2527700\_PR\_DR01-DP01 Author: Daniel Torres Date: 12/10/2024 11:21:35 AM Status: Color: comments have been provided on the proposed drainage maps regarding breaking up basins in these areas into multiple basins to more accurately represent flows leaving the site and for more accurate comparison of existing and proposed flows.

......

Adjust/revise the basins as the Judge Orr

Roadside ditch is not conveyed to DP2. similar

.....



Status: Color: Layer: Space:

Space:

FYI: analysis will need to be provided at the confluence of flows within the final drainage report

comment on basins A3 and B



Subject: Callout Page Label: [1] 2527700\_PR\_DR01-DP01 Author: Daniel Torres Date: 12/10/2024 4:55:39 PM Status: Color: Layer:

SEC SILET

Subject: Callout Page Label: [2] 2527700\_PR\_DR01-DP02 Author: Daniel Torres Date: 12/10/2024 3:33:53 PM Status: Color: Layer: Space:

label this basin



Subject: Callout Page Label: [2] 2527700\_PR\_DR01-DP02 Author: Daniel Torres Date: 12/10/2024 5:11:33 PM Status: Color: Layer: Space:

label this basin



Subject: Highlight Page Label: [3] 2527700\_PR\_DR01-DP03 Author: Daniel Torres Date: 12/10/2024 1:54:44 PM Status: Color: Layer: Space:



Subject: Highlight Page Label: [3] 2527700\_PR\_DR01-DP03 Author: Daniel Torres Date: 12/10/2024 1:55:05 PM Status: Color: Layer: Space:

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Subject: Callout Page Label: [4] 2527700\_PR\_DR01-DP04 Author: Daniel Torres Date: 12/10/2024 3:36:06 PM Status: Color: Layer: Space:

a deviation will be required at the final plat stage for multiple culverts as they are not allowed per criteria (ECM 2.6.9.G)



Subject: Highlight Page Label: [4] 2527700\_PR\_DR01-DP04 Author: Daniel Torres Date: 12/10/2024 3:41:17 PM Status: Color: Layer: Space:

106

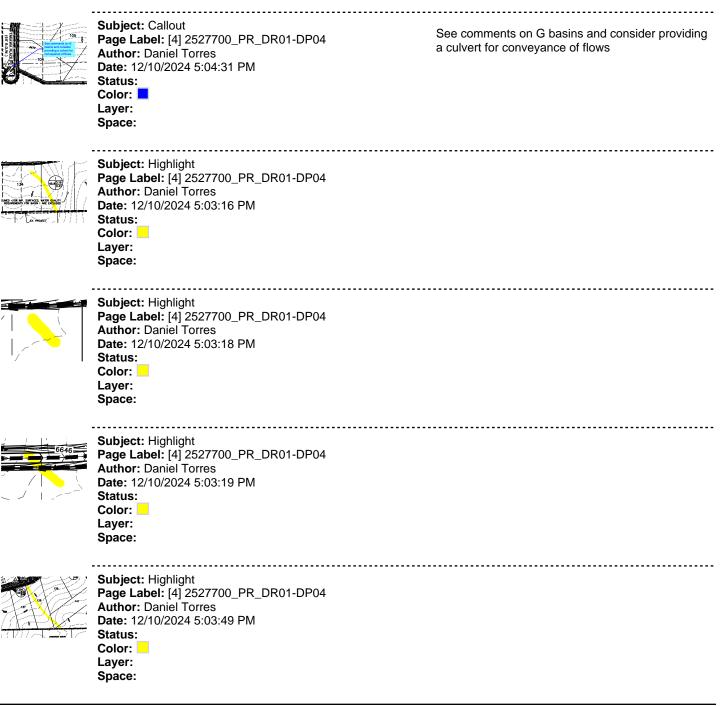
Subject: Highlight Page Label: [4] 2527700\_PR\_DR01-DP04 Author: Daniel Torres Date: 12/10/2024 3:42:40 PM Status: Color: Layer: Space:



Layer: Space:

Subject: Callout Page Label: [4] 2527700\_PR\_DR01-DP04 Author: Daniel Torres Date: 12/10/2024 3:43:59 PM Status: Color:

basin H6 should be broken up into multiple basins as portions of the basin will flow offisite. Also see comment on the south end of the basin



## Glenn Reese - EPC Stormwater (12)



Subject: SW - Textbox Page Label: 17 Author: Glenn Reese - EPC Stormwater Date: 12/5/2024 5:08:17 PM Status: Color: ■ Layer: Space:

Also state that some areas are excluded from WQ treatment because of exclusion 1.7.1.B.8

Subject: SW - Highlight with Section 13.3.2.1 of the CCS/EPCI ded for all of the development site a nality Policy and Procedures Section Basins B, C, D1-D2, F and I fall un and Procedure for areas with large s fall under the Section 1.7.1.B.8 of the F asins B, C, D1-D2, F and I Page Label: 18 Author: Glenn Reese - EPC Stormwater Date: 12/5/2024 4:44:22 PM sites. The proposed roadw ructure release rates will be Status: Color: 📕 Layer: Space: Subject: SW - Highlight \*\*EXCLUDED BASED ON LAND DIST. TO Page Label: 19 UNDEVELOPED LAND Author: Glenn Reese - EPC Stormwater TO REMAIN UNDEVELOPED PER ECM APP. Date: 12/5/2024 4:49:29 PM I.7.B.7 Status: Color: Layer: Space: \_\_\_\_\_ Subject: SW - Textbox with Arrow See my comment on the WQ Treatment Summary Page Label: 19 Map on pg 185 below. Author: Glenn Reese - EPC Stormwater Date: 12/5/2024 4:49:54 PM Status: Color: Laver: Space: Subject: SW - Textbox Note: all pond calcs will be more thoroughly Page Label: 1 reviewed with the Final Plat (SF) submittal once Author: Glenn Reese - EPC Stormwater pond CDs have been provided. Date: 12/5/2024 5:04:19 PM Status: Color: Layer: Space: Subject: SW - Textbox with Arrow There is road-related grading within Basin C that Page Label: [1] 2527700\_PR\_DR01-DP01 does not qualify for ECM WQ Exclusion I.7.B.5. Author: Glenn Reese - EPC Stormwater Please provide an applicable exclusion or provide Date: 12/5/2024 5:11:28 PM WQ treatment for all areas of road grading within Status: basins that you are stating are excluded from WQ Color: via the large lot exclusion. Layer: Since a lot of these areas are pretty small, you Space: may be able to utilized the exclusion in ECM App I.7.1.C.1 for <20% up to 1ac. Subject: SW - Textbox with Arrow There is road-related grading within Basin F that Page Label: [2] 2527700\_PR\_DR01-DP02 does not qualify for ECM WQ Exclusion I.7.B.5. Author: Glenn Reese - EPC Stormwater Please provide an applicable exclusion or provide Date: 12/5/2024 5:00:23 PM WQ treatment for all areas of road grading within Status: basins that you are stating are excluded from WQ Color: via the large lot exclusion. Layer:

Space:

	Subject: SW - Textbox with Arrow Page Label: [2] 2527700_PR_DR01-DP02 Author: Glenn Reese - EPC Stormwater Date: 12/5/2024 5:00:57 PM Status: Color: ■ Layer: Space:	There is road-related grading within Basin D2 that does not qualify for ECM WQ Exclusion I.7.B.5. Please provide an applicable exclusion or provide WQ treatment for all areas of road grading within basins that you are stating are excluded from WQ via the large lot exclusion.
	Subject: SW - Textbox with Arrow Page Label: [4] 2527700_PR_DR01-DP04 Author: Glenn Reese - EPC Stormwater Date: 12/5/2024 4:59:47 PM Status: Color: ■ Layer: Space:	There is road-related grading within Basin I that does not qualify for ECM WQ Exclusion I.7.B.5. Please provide an applicable exclusion or provide WQ treatment for all areas of road grading within basins that you are stating are excluded from WQ via the large lot exclusion.
A CONTRACTOR OF A CONTRACTOR O	Subject: SW - Textbox with Arrow Page Label: [1] 24x36 Title Portrait Author: Glenn Reese - EPC Stormwater Date: 12/5/2024 4:48:09 PM Status: Color: ■ Layer: Space:	This exclusion was not denoted on the PBMP Applicability Form nor was it discussed in the report text above. Why not just make this part of the light blue large lot exclusion area?
All Barrieds Market and All a	Subject: SW - Textbox with Arrow Page Label: [1] 24x36 Title Portrait Author: Glenn Reese - EPC Stormwater Date: 12/5/2024 4:50:56 PM Status: Color: ■ Layer: Space:	Potentially revise/delete this text of the table based on my comment below.
D.C.         D.         D.00007*           1         0.1         0.0007           1         0.1         0.0007           1         0.1         0.0007           1         0.1         0.0007           1         0.1         0.0007           1         0.1         0.0007           1         0.0007         0.0007           1         0.0007         0.0007           1         0.0007         0.0007           1         0.0007         0.0007           1         0.0007         0.0007           1         0.0007         0.0007           1         0.0007         0.0007           1         0.0007         0.0007           1         0.0007         0.0007           1         0.0007         0.0007           1         0.0007         0.0007	Subject: SW - Rectangle Page Label: [1] 24x36 Title Portrait Author: Glenn Reese - EPC Stormwater Date: 12/5/2024 4:51:03 PM Status: Color: Layer: Space:	
Joseph Sandstro	om (76)	

: SP245

Subject: Text Box Page Label: 1 Author: Joseph Sandstrom Date: 11/26/2024 10:48:37 AM Status: Color: Color: Color: Space:

SP245

<text></text>	Subject: Callout Page Label: 8 Author: Joseph Sandstrom Date: 12/2/2024 8:20:10 AM Status: Color: Layer: Space: Subject: Highlight	See comment on drainage map about sub-basins. If there is a swale to DP3, please show it. The existing topography appears to be falling to the east.
Control and Con	Page Label: 8 Author: Joseph Sandstrom Date: 12/2/2024 8:12:02 AM Status: Color: Layer: Space:	unoff from this basin will be collected in a proposed swale along the southern basin line to the proposed swale at DP3
2 ( $Q_5=12$ 100=84 cfs	Subject: Highlight Page Label: 8 Author: Joseph Sandstrom Date: 12/10/2024 12:47:14 PM Status: Color: Layer: Space:	84
In line at $Q_5 = \frac{44}{2} cfs$	Subject: Highlight Page Label: 8 Author: Joseph Sandstrom Date: 12/10/2024 12:47:23 PM Status: Color: Layer: Space:	44
<text><text><text><text></text></text></text></text>	Subject: Text Box Page Label: 8 Author: Joseph Sandstrom Date: 12/10/2024 5:19:18 PM Status: Color: Layer: Space:	Highlighted flows here and on the following pages do not match calcs. Please round up for values that are .5 or greater. Please use one decimal point for flows less than 1 cfs.
ed of large he <mark>east</mark> ha	Date: 11/26/2024 11:44:06 AM	east

e with other inflows a west d of brge single-family e east half of Cabrillo	Subject: Callout Page Label: 9 Author: Joseph Sandstrom Date: 11/26/2024 11:44:32 AM Status: Color: Layer: Space:	west
and is comprised of large single-family bern Road and the east half of Cabrillo poor randalise wales DP7 ( $0_{\rm C}$ )=9 cfs, time with other inflows at DP8.1. or and in comprised of its comprised of at half of Cabrillo Carle West, the west if a Cabrillo Carle West, the west is DPS ( $0_{\rm C}$ ) = Cabrillo Carle West, the west is DPS ( $0_{\rm C}$ ) = Cabrillo Carle West, the west is DPS ( $0_{\rm C}$ ) = Cabrillo Carle West, the west is DPS ( $0_{\rm C}$ ) = Cabrillo Cabrillo Carle West is DPS ( $0_{\rm C}$ ) = Cabrillo Cabrillo Cabrillo Cabrillo 7.6 ch, Ramoff is rested within Ford 1 1 cfs. O <sub>100</sub> =32 cfs). DPR 2 flows then are	Subject: Highlight Page Label: 9 Author: Joseph Sandstrom Date: 11/26/2024 11:49:48 AM Status: Color: Layer: Space:	is comprised of is comprised of
proximiting 0.14 mTeV with 4.56 mignitions and 0.47 memory. Result from the basic (QeO cft, Qyang- tam) and basiling the existing affinished on the second of the second second second second second second of the second second second second second second second second second second second second second second second second second s	Subject: Highlight Page Label: 9 Author: Joseph Sandstrom Date: 11/26/2024 1:09:36 PM Status: Color: Layer: Space:	Basin B and C flows combine at DP9
a single cost of a manufacture states and a manufacture of a single of the same of the sam	Subject: Callout Page Label: 9 Author: Joseph Sandstrom Date: 12/2/2024 8:44:08 AM Status: Color: Layer: Space:	This is inaccurate for sub-basin B and part of sub-basin C.
Imperviou		0
	Author: Joseph Sandstrom Date: 12/10/2024 12:50:04 PM	
v utility 20	Status: Color: - Layer: Space:	
of WHB a 10% supportance and is compresent of logge at the Q <sub>1</sub> Q <sub>2</sub> -16-45 vi WIB flow scalable cortend to wavel has in a comprised of only page single-family loss an ress. Poor will distribute for the state of the basic pages vi Wibb argument streamware angular gaus agreewing wibb and the stream of the stream of the streamware of the stream of the stream of the stream concluse. Rule R and C have scalable at RPM (Qr-8 C field in the stream of the stream of the stream of the streamware of the stream of the stream of the stream of the streamware of the stream of the stream of the stream of the stream of the stream of the stream of the stream of the stream of the stream of the stream of the stream of the stream of the stream of the stream of the stream of the stream have the stream of the stream of the stream of the stream of the stream of the stream of the stream of the stream of the stream of the stream of the stream of the stream of the stream of the stream of the stream of the stream of the stream of the stream of the stream of the stream of the stream of the stream of the stream of the stream of the stream of the stream of the stream of the stream of the stream of the stream of the stream of the stream of the stream of the stream of the stream of the stream of	Subject: Highlight Page Label: 10 Author: Joseph Sandstrom Date: 11/26/2024 1:09:43 PM Status: Color: Layer: Space:	Basin B and C flows combine at DP9

A spectra to the the twenty of the transfer to	Subject: Callout Page Label: 10 Author: Joseph Sandstrom Date: 12/2/2024 2:12:28 PM Status: Color: Layer: Space:	10% is shown in the impervious calculations to include build out of Saddlehorn Ranch lots. This imperviousness will increase the flows going into Geick Ranch Tributary
Horsen paragraphic and a constraint was have approximate a set of the set	Subject: Callout Page Label: 10 Author: Joseph Sandstrom Date: 12/10/2024 4:20:00 PM Status: Color: Layer: Space:	For D1 and D2, 10% imperviousness seems too low since only the buildable part of these lots is included in the sub-basin. Please verify.
Ion Provide design points and from for all basins. and is comprised of large single-family southeast overland towards the eastern large single-family lots and does not	Subject: Text Box Page Label: 10 Author: Joseph Sandstrom Date: 12/10/2024 11:28:43 AM Status: Color: Layer: Space:	Provide design points and flows for all basins.
<text><text><text></text></text></text>	Subject: Callout Page Label: 11 Author: Joseph Sandstrom Date: 12/2/2024 10:51:28 AM Status: Color: Layer: Space:	Please include the culvert under Adella Place in the narrative.
th <mark>a 2% i</mark> mj at of the pi	Subject: Highlight Page Label: 11 Author: Joseph Sandstrom Date: 12/2/2024 8:53:55 AM Status: Color: Layer: Space:	2%
a. a base of the second sec	Subject: Callout Page Label: 11 Author: Joseph Sandstrom Date: 12/2/2024 10:33:53 AM Status: Color: Layer: Space:	10% from impervious calcs.

A submitted on the structure of the stru	Subject: Highlight Page Label: 11 Author: Joseph Sandstrom Date: 12/2/2024 10:14:57 AM Status: Color: Layer: Space:	unoff from this basin will be collected in proposed roadside swales to DP12 (Q5=19 cfs, Q100=69 cfs).
no and is comprised of the east half of ef in proposed reaching which wants by Paul 2 vius a forethay and combine with extended the end of the semprised of wills for clicetal improposed reaching '14 flows enter Paul 2 via in forethy and eds). Reard'it reacted whith Paul 2 and efs). Reard'it reaches whith Paul 2 and efs, Onumi-16 etch. DP14.2 flows then are	Subject: Highlight Page Label: 11 Author: Joseph Sandstrom Date: 12/2/2024 10:43:52 AM Status: Color: Layer: Space:	is comprised of is comprised of
Which is the star is the st	Subject: Text Box Page Label: 11 Author: Joseph Sandstrom Date: 12/10/2024 4:26:28 PM Status: Color: Layer: Space:	For sub-basin E3, based on the contours, most of this basin will sheet flow into the DP12.1 swale and some will follow the swale along the east side of Cabrillo Circle West. Please account for the majority of E3 flow within the DP12.1 swale. Revise the narrative as necessary.
$_{0}$ =105 CIS $Q_{5}=0$ cfs, drainages	Subject: Highlight Page Label: 11 Author: Joseph Sandstrom Date: 12/10/2024 12:54:04 PM Status: Color: Layer: Space:	0
ch) SPUT from sorthur at DPT-12 (Q)-11 (A), QuestA column. The CH Approximately 5 Th serve vide 2.2% appears for softward and proposed and address vide at DPT (Q)-11 (A) (A) (A) (A) (A) (A) (A) (A) (A) (A)	Subject: Text Box Page Label: 12 Author: Joseph Sandstrom Date: 12/2/2024 11:10:45 AM Status: Color: Layer: Space:	Please mention culvert in narrative.
<text><text><text></text></text></text>	Subject: Text Box Page Label: 12 Author: Joseph Sandstrom Date: 12/2/2024 1:13:47 PM Status: Color: Layer: Space:	See notes on Drainage Map regarding sub-basins G1, G2, G3, H2.

U CIS). Ku $(Q_5=0 \text{ cfs}, \text{ offsite tox})$	Page Label: 12 Author: Joseph Sandstrom Date: 12/10/2024 12:56:39 PM	0
	Subject: Highlight Page Label: 13 Author: Joseph Sandstrom Date: 12/2/2024 1:19:44 PM Status: Color: Layer: Space:	large single-family lots
rised of the couth half of be collected in proposed and the proposed of the collected of the proposed of the collected of the collected of the exposed of the combination	Subject: Callout Page Label: 13 Author: Joseph Sandstrom Date: 12/2/2024 1:20:01 PM Status: Color: Layer: Space:	Swales, per map.
/ith a 50% impervious ; :om this basin will be c ound Tarawa Place via ;	Subject: Highlight Page Label: 13 Author: Joseph Sandstrom Date: 12/2/2024 1:22:34 PM Status: Color: Layer: Space:	Tarawa Place
reated within I 's). DP14.2 flo tural dich adjac	Author: Joseph Sandstrom Date: 12/2/2024 1:46:40 PM Status: Color: Layer: Space:	DP14.2
An experimentary of the second	Subject: Highlight Page Label: 13 Author: Joseph Sandstrom Date: 12/2/2024 2:02:41 PM Status: Color: Layer: Space:	7360 Falcon Grassy Hts property

Benchmark and State S	Subject: Callout Page Label: 13 Author: Joseph Sandstrom Date: 12/2/2024 2:03:13 PM Status: Color: Layer: Space:	Flows go to several properties to the south, not just 7360.
roposed s $Q_5 = \frac{34}{5} cfs$	Subject: Highlight Page Label: 13 Author: Joseph Sandstrom Date: 12/10/2024 12:57:40 PM Status: Color: Layer: Space:	34
torebay. $Q_5=0$ cfs, ng offsite	Subject: Highlight Page Label: 13 Author: Joseph Sandstrom Date: 12/10/2024 12:58:48 PM Status: Color: Layer: Space:	0
$ \begin{array}{c} \mbox{Work Source transmission}\\ Work Source transmi$	Subject: Text Box Page Label: 14 Author: Joseph Sandstrom Date: 12/10/2024 4:35:53 PM Status: Color: Layer: Space:	Existing 100 year flows are smaller but 5 year flows are larger for some DP's. Please address.
less than ond $\frac{4}{4}$ will	Subject: Highlight Page Label: 14 Author: Joseph Sandstrom Date: 12/2/2024 2:10:49 PM Status: Color: Layer: Space:	4
<text><list-item><list-item><list-item><list-item><list-item><list-item><list-item><list-item><list-item><list-item></list-item></list-item></list-item></list-item></list-item></list-item></list-item></list-item></list-item></list-item></text>	Subject: Text Box Page Label: 14 Author: Joseph Sandstrom Date: 12/2/2024 2:12:09 PM Status: Color: Layer: Space:	Please include comparison for ponds 1 and 2 as well as the increase from OS2.

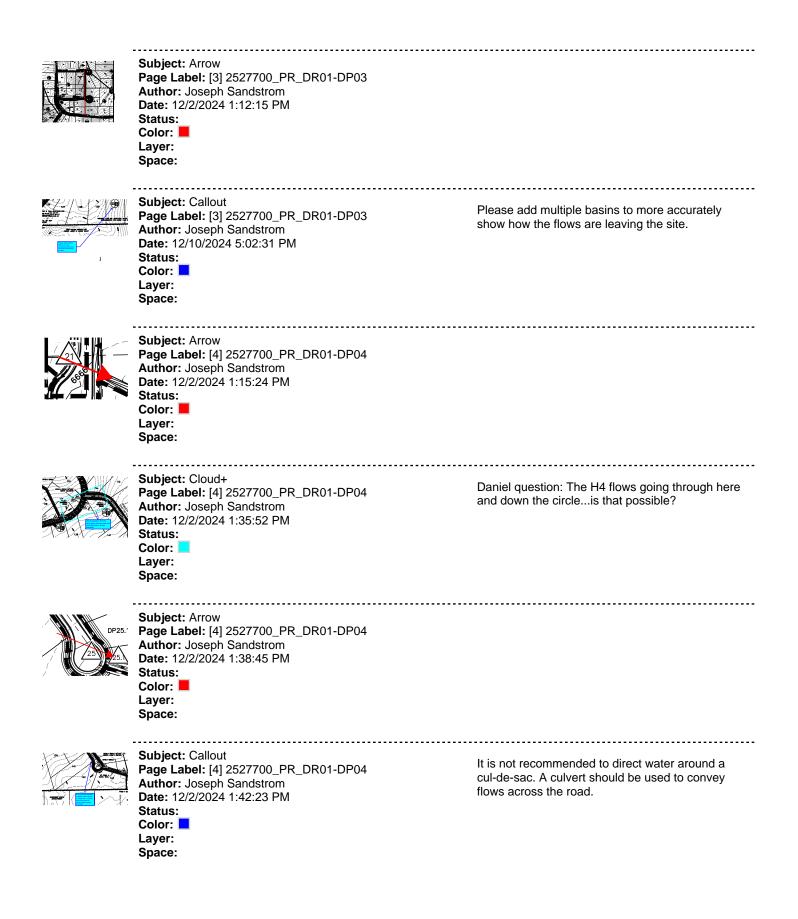
or equal to the instorte fit	Subject: Callout	Dand 2 and 4
n the pond are not concentrate	Page Label: 14 Author: Joseph Sandstrom	Pond 3 and 4.
Pond 3 and 4.	Date: 12/2/2024 2:14:20 PM Status:	
analyza the avisting floods	Color:	
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	· ·	
strong shows resulting systems. <b>Errors areas: Figu</b> shows a second strong the strong strong strong strong system in the strong strong strong strong strong strong strong strong strong <b>Strong strong strong <b>Strong strong </b></b>	Subject: Text Box	The LOI states that Public Open Space areas will
A refer to a spectra characterization of the spectra character	Page Label: 20 Author: Joseph Sandstrom	be maintained by the Esteban Rodriguez
	Date: 12/10/2024 4:43:12 PM Status:	Subdivision Metropolitan District or HOA. Please revise the above statement.
	Color:	
	Layer: Space:	
	Subject: Highlight Page Label: 1	2.0%
2.0%	Author: Joseph Sandstrom	
	Date: 12/2/2024 3:40:27 PM Status:	
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2.0%	Subject: Callout Page Label: 1	Should be a little higher than 2% because of the
Should be a little higher than 2% because of the 10%	Author: Joseph Sandstrom Date: 12/2/2024 3:40:57 PM	10% imperviousness of OS2
imperviousness of OS2 Page Lef 1: 86-2024	Status:	
	Color: Layer:	
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	Subject: Callout Page Label: 2	10% in existing calcs
	Author: Joseph Sandstrom Date: 12/2/2024 3:55:57 PM	
tês in wording calife	Status: Color:	
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2.0% 2.0%	Subject: Highlight Page Label: 2 Author: Joseph Sandstrom Date: 12/2/2024 3:55:52 PM Status: Color: Layer: Space:	2.0%
	Subject: Callout Page Label: 1 Author: Joseph Sandstrom Date: 12/2/2024 11:27:21 AM Status: Color: Layer: Space:	Additional sub-basin is needed for the flows going to 7360 Falcon Grassy Hts.
	Subject: Callout Page Label: 1 Author: Joseph Sandstrom Date: 12/10/2024 4:48:57 PM Status: Color: Layer: Space:	Divide basin EX into multiple basins/design points.
47.1 8 55 227 0 3 258 8 3 10 Girck Randh Wen y Drevel, Barrel & Co.	Subject: Callout Page Label: 1 Author: Joseph Sandstrom Date: 12/10/2024 10:57:12 AM Status: Color: Layer: Space:	0.4
	Subject: Cloud+ Page Label: [1] 2527700_PR_DR01-DP01 Author: Joseph Sandstrom Date: 11/26/2024 1:07:28 PM Status: Color: Layer: Space:	Please adjust basin lines for A3 and B. Based on the proposed swale location contours, all of A3 will not not drain to DP3 as shown.
	Subject: Callout Page Label: [1] 2527700_PR_DR01-DP01 Author: Joseph Sandstrom Date: 12/10/2024 4:55:25 PM Status: Color: Layer: Space:	Assure the easement has appropriate width to convey the flows.

DP <mark>2.1</mark> -S	Subject: Highlight Page Label: [1] 2527700_PR_DR01-DP01 Author: Joseph Sandstrom Date: 12/2/2024 8:28:13 AM Status: Color: Layer: Space:	
	Subject: Callout Page Label: [1] 2527700_PR_DR01-DP01 Author: Joseph Sandstrom Date: 12/10/2024 4:56:24 PM Status: Color: Layer: Space:	There are several places where sub-basin C flows will sheet flow offsite. Please add multiple basins to more accurately show how the flows are leaving the site.
BET A	Subject: Text Box Page Label: [1] 2527700_PR_DR01-DP01 Author: Joseph Sandstrom Date: 12/10/2024 4:52:22 PM Status: Color: Layer: Space:	Please show flow arrows on basins where they are missing. For example, G4 does not have any.
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	Subject: Callout Page Label: [1] 2527700_PR_DR01-DP01 Author: Joseph Sandstrom Date: 12/10/2024 1:01:55 PM Status: Color: Layer: Space:	0.2
11 25 N/A <sup>+</sup> N/A <sup>+</sup> N/A <sup>+</sup> N/A <sup>+</sup> 9 3 40	Subject: Callout Page Label: [1] 2527700_PR_DR01-DP01 Author: Joseph Sandstrom Date: 12/10/2024 1:02:34 PM Status: Color: Layer: Space:	Rounding error, should be 7.
75 6 93	Subject: Highlight Page Label: [1] 2527700_PR_DR01-DP01 Author: Joseph Sandstrom Date: 12/10/2024 1:03:03 PM Status: Color: Layer: Space:	

8         36           60*         753*           1         5           10         60           3         6           46         165           9         40           9         40           9         40	Subject: Callout Page Label: [1] 2527700_PR_DR01-DP01 Author: Joseph Sandstrom Date: 12/10/2024 1:03:27 PM Status: Color: Layer: Space:	0.3
29 0 12	Subject: Highlight Page Label: [1] 2527700_PR_DR01-DP01 Author: Joseph Sandstrom Date: 12/10/2024 1:03:46 PM Status: Color: Layer: Space:	
46 0 9	Subject: Highlight Page Label: [1] 2527700_PR_DR01-DP01 Author: Joseph Sandstrom Date: 12/10/2024 1:03:48 PM Status: Color: Layer: Space:	
69 6 93	Subject: Highlight Page Label: [1] 2527700_PR_DR01-DP01 Author: Joseph Sandstrom Date: 12/10/2024 1:03:53 PM Status: Color: Layer: Space:	
7 0 8	Subject: Highlight Page Label: [1] 2527700_PR_DR01-DP01 Author: Joseph Sandstrom Date: 12/10/2024 1:03:55 PM Status: Color: Layer: Space:	
	Subject: Callout Page Label: [1] 2527700_PR_DR01-DP01 Author: Joseph Sandstrom Date: 12/10/2024 1:04:57 PM Status: Color: Layer: Space:	Rounding error, should be 35

11 34 3 47 0 24	Subject: Highlight Page Label: [1] 2527700_PR_DR01-DP01 Author: Joseph Sandstrom Date: 12/10/2024 1:04:35 PM Status: Color:	
POND	Subject: Highlight Page Label: [2] 2527700_PR_DR01-DP02 Author: Joseph Sandstrom Date: 12/10/2024 11:30:13 AM Status: Color: Layer: Space:	
	Subject: Callout Page Label: [2] 2527700_PR_DR01-DP02 Author: Joseph Sandstrom Date: 12/10/2024 11:30:44 AM Status: Color: Layer: Space:	Please make labels more readable.
	Subject: Cloud+ Page Label: [3] 2527700_PR_DR01-DP03 Author: Joseph Sandstrom Date: 12/2/2024 1:56:34 PM Status: Color: Layer: Space:	Another sub-basin should be added here or an adjustment of the sub-basin line.
	Subject: Cloud+ Page Label: [3] 2527700_PR_DR01-DP03 Author: Joseph Sandstrom Date: 12/10/2024 4:59:49 PM Status: Color: Layer: Space:	Please address the flow through this area in the narrative of the report. Directing the flow paths around the cul-de-sac bulbs is not recommended. Additional easement will likely be required. Complete analysis of the swale around the bulbs will be required at the Final Drainage Report. Strongly Consider adding culvert crossings under these roads and directing flow to Cabrillo Circle West.





-----Subject: Callout Page Label: [4] 2527700\_PR\_DR01-DP04 Author: Joseph Sandstrom Date: 12/2/2024 1:45:25 PM Status: Color: Layer:

This part of sub-basin H6 will flow offsite untreated. Please create new sub-basin.



Space:

Subject: Callout Page Label: [4] 2527700\_PR\_DR01-DP04 Author: Joseph Sandstrom Date: 12/10/2024 5:03:08 PM Status: Color: Layer: Space:

Please add multiple basins to more accurately show how the flows are leaving the site.

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Subject: Highlight Page Label: [4] 2527700\_PR\_DR01-DP04 Author: Joseph Sandstrom Date: 12/10/2024 5:08:53 PM Status: Color: 📒 Layer: Space: