PRELIMINARY AND FINAL DRAINAGE PLAN AND REPORT

FALCON STORAGE SUBDIVISION

PART OF THE SW1/4 SECTION 1, T.13S. R.65W. OF THE 6TH P.M. EL PASO COUNTY

February 4, 2021

Revised November 23, 2022

> Revised June 7.2023

Revised June 22, 2023

Revised August 31, 2023

PCD File No. PPR2232 PCD File No. MS232

Prepared for

Falcon Storage Partners LLLP 4615 Northpark Drive Colorado Springs, CO 80918

Oliver E. Watts, Consulting Engineer, Inc. Colorado Springs, Colorado

OLIVER E. WATTS, PE-LS

OLIVER E. WATTS, CONSULTING ENGINEER, INC. CIVIL ENGINEERING AND SURVEYING 614 ELKTON DRIVE COLORADO SPRINGS, COLORADO 80907 (719) 593-0173 fax (719) 265-9660 <u>olliewatts@aol.com</u> Celebrating over 43 years in business

August 31, 2023

El Paso County Planning and Community Development 2880 International Circle Colorado Springs, CO 80910

ATTN: Joshua Palmer, P.E.

SUBJECT: Preliminary and Final Drainage Plan and Report Falcon Storage Subdivision

Transmitted herewith for your review and approval is the drainage plan and report for The Falcon Storage Subdivision in El Paso County. This report will accompany the development plan and subdivision plat submittal. This report has been revised in accordance with your review comments of November 23, 2022, March 2, 2023, and August 18, 2023.

Please contact me if I may provide any further information.

Oliver E. Watts, Consulting Engineer, Inc.

BY:

Oliver E. Watts, President

<u>FALCON STORAGE SUBDIVISION</u> <u>DRAINAGE REPORT</u> <u>TABLE OF CONTENTS</u>

Drainage Report 5 pages Computations, 7 pages Vicinity Map FEMA Panel No. 08041C0553 G SCS Soils Map and Interpretation Sheet Backup Information, 4 sheets Drainage Flow Path Map Falcon DBPS Map Drainage Plan, Falcon Meadows at Bent Grass Drainage Plan, Latigo Business Center Drainage Plan, Dwg 02-5523-04

FALCON STORAGE SUBDIVISION DRAINAGE REPORT REFERENCES

City-County Drainage Criteria, current edition Fema Firm Insurance Rate Map El Paso County Soils Survey, SCS Falcon Drainage Basin Planning Study Drainage Report, Falcon Meadows at Bent Grass Drainage Report, Latigo Business Center, Lot 1

<u>1. ENGINEER'S STATEMENT:</u>

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the County for drainage reports and said report is in conformity with the applicable master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.

Oliver E. Watts, Consulting Engineer, Inc.

Oliver E. Watts Colo. PE-LS No. 9853

date

2. OWNERS / DEVELOPER'S STATEMENT:

I the owner / developer have read and will comply with all of the requirements specified in this drainage report and plan.

Falcon Storage Partners LLLP

By: ______ Richard Graham 4615 Northpark Drive Colorado Springs, CO 80918

Date

3. EL PASO COUNTY:

Filed in accordance with the requirements of the El Paso Land Development Code, Drainage Criteria Manual Volumes 1 and 2, and the Engineering Criteria Manual, as amended.

Joshua Palmer, P.E.,
County Engineer / ECM Administrator

Conditions:

date

4. LOCATION AND DESCRIPTION:

The Falcon Storage Subdivision is located in the Latigo Business Center development of El Paso County as shown on the enclosed vicinity map. Occupying a portion of the West half of Section 1, Township 13 South, Range 65 West of the 6th P.M., totaling 5.004 acres. It is located in the Falcon Drainage Basin as shown on the enclosed basin map. It lies west of Bent Grass Meadows Drive north of the Latigo Business Center Filing No. 1 as shown on the enclosed drainage plan. The site will be developed into an RV Storage site as shown on the enclosed drainage plan, as an expansion to the one in the Latigo Business Center Filing No. 1, both owned by the developer.

5. FLOOD PLAIN STATEMENT:

This subdivision is not within the limits of a flood plain or flood hazard area, according to FEMA map panel number 08041C0553 G, dated December 7, 2018, a copy of which is enclosed for reference.

6. METHOD AND CRITERIA:

The method used for all computations is that specified in the City-County Drainage Criteria Manual, using the rational method for areas of the size of the development. All computations are enclosed for reference and review. Pertinent portions of the criteria are enclosed.

The soils in the subdivision have been mapped by the local USDA/SCS office, and a soils map and interpretation sheet are enclosed for reference. All soils in this area are of hydrologic group "A" within the development area.

7. DESCRIPTION OF RUNOFF:

A. Drainage Inflows: The drainage Report for Falcon Meadows at Bent Grass indicates an existing drainage swale above the north boundary to divert runoff from this site and route it to Bent Grass Meadows and then past this development in Bent Grass Meadows Drive to outfall points to an existing detention pond across the street. A copy of this drainage plan is enclosed. Also shown on this map is that portion of the Meadows Filing No. 1 that drains 0.62 cfs / 3.5 cfs (5-year / 100-year runoffs) into this subdivision along the westerly boundary (Basin O-1), and it indicates the historic undeveloped runoff of the site, Basin A (historic) totaling 1.25 cfs / 7.6 cfs at the lowest (southeast) portion of the subdivision.

B. Interior Routing: The area will be graded to conform to the existing topography shown on the drainage plan. The property has been rough graded, which complies with the historic runoff pattern. Additional grading is indicated which is intended to contain the runoff into the interior drive isle street network, and along the streets to the detention pond The westerly street (Basin A) will combine with offset basin O-1 to develop 3.0 cfs \ 6.2 cfs (5-yeaF \ 100-year runoffs) near the in the southwest corner of the plat (Design Point 1). Basin B will develope 1.3/2.5 cfs in the southerly driveway adjacent to the north entrance. It will combine with basin C along the same routing for 5.2/10.4 cfs at the southwest intersection (design point 2). This will combine basin D to outfall into the detention pond (design point 3). The total outfall at this point 5.5 cfs/12.5 cfs, into the sand filter basin.

Assign a name/number to all PBMPs and then update all submitted text and drawings accordingly with consistent labeling throughout (example: "Pond A" or "Pond 1"). Unresolved

C. Detention Storage: At the proposed outfall point a sand filter detention pond is proposed, as required by the County. The pond is sized for a temporary sedimentation basin to be used during the construction period and converted into a permanent sand filter basin upon completion. The sedimentation basin will contain 13000 +CF (at 1800 CF per acre). An 8-inch riser pipe is used as an outlet, with holes drilled as computed to detain the runoff as required. One foot of freeboard is provided with a spillway that will pass the 100-year runoff. Details are shown on the enclosed drainage plan. Following construction the basin will be converted to a sand filter basin. A 4-inch slotted underdrain will be placed in a 5-inch section of CDOT class C Filter material and drain into the grated inlet outlet structure set at the WQCV level, and sized for the 100-year runoff. An orifice plate will be provided on the end of the underdrain with an orifice

discuss flow path to existing detention facility and provide calcs for capacities and velocities to meet criteria for conveyance system

Falcon Storage Subdivision Preliminary and Final Drainage Plan and Report

developed flows. Address any by the sized for the installation. A detention basin stage-storage table County, the basin is used for water quality storage only and the improvements/upgrades needed to the Center Filing No. 1 to an existing full spectrum pond to the sou pond. If the existing pond did not account between Tamlin and Meridian Roads, in accordance with the a for developed flows from this site provide

D. Outfall Point: Discharge from the subdivision will be int upgrades needed for the existing pond and Latigo Business Center, filing no. 1, as shown on the drainage provide CD's of work to be done by this along the north boundary of Lot 1 as shown on the drainage pladevelopmentitive installation. The two properties are under common ownership and permission to outfall into the Latigo Business Center is granted. The drainage plan for the Latigo Business Center is enclosed. This report indicated two existing discharges: 0.2 cfs / 0.5 cfs near the southwest corner and 4.1 cfs / 10.1 cfs over the remaining south frontage. A 24 inch CMP will run from the CDOT Type C outlet box at a minimum slope of one percent into the existing ditch shown on the drainage plan.

WATER QUALITY

A sand filter basin water quality facility will be provided as described above.

FOUR STEP PROCESS

The following process has been followed to minimize adverse impacts of urbanization

this was not included

Runoff Reduction: The scope of the development has been minimized consistent with zoni requirements to present the minimum footprint in providing a RV Storage development. The portions are to be landscaped to reduce the impervious percent.

Water Quality

Provide WQCV: Detention water quality storage is being provided for this subdivision by a detention pond and runoff will be routed to a full spectrum pond located downstream, south o Road, north of Highway 24, between Tamlin and Meridian Roads, by others as a sub regional

Stabilize Drainage Ways: The site will be graded to route the runoff over improved street installations to provide channel stabilization in the natural erosive material over the site. Discharge from the site will be into adjacent and downstream facilities in accordance with the master drainage basin plan for the Falcon drainage basin and previously approved subdivision drainage reports. Copies of each plan are enclosed. There will be no adverse affect on downstream developments as a result of this subdivision

Consider need for Industrial and Commercial BMP's: This is a RV Storage site, so source control problems will be a minimum. During construction, standard site specific state of the art BMP's will be employed to minimize and mitigate erosive problems.

provide analysis of the ditch and downstream facilities and show that it is adequate to convey the flows down stream.

Item No.	Description	Quantity	Unit Cost	Cost
1	Pond/BMP Earthwork	881 CY	\$ 23.00	\$ 20263.00
2	Slotted drain	187 LF	40.00	7480.00
3	Riprap	14 Tons	80.00	1096.00
4	Grated Inlet	1 ea	5611.00	5611.00
4	12" PVC drain	106 LF	112.00	11872.00

8. COST ESTIMATE:

Please identify how the flow is conveyed to the full spectrum pond to the south of Woodmen from Lot 1. Will it enter an existing storm system? is the system adequate for this sites developed flows? Please address. The sites developed flows must be conveyed to a

please analyze and state whether the

existing pond accounted for this sites

detention onsite or identify the necessary

5	Concrete Pond Inlet	15 CY	589.00	10335.00
	\$ 56657.00			
	Engineering	10%		5665.71
	\$ 62322.70			

- Please revise to 2023

9. FEES: At plat recording.

2024 Falcon Basin Fees: 5.004 acres @62.3% Impervious = 3.1175 Impervious acres Drainage fees @ \$ 37,256 per acre = \$ 116,145.28Bridge fees @ \$ 5,118 per acre = \$ 15,955.32

Total Fees: \$ 132,100.61

10. SUMMARY

The Falcon Storage Subdivision is a proposed 1-lot, RV Storage subdivision containing 5.004 acres. The proposed street facilities will adequately convey, detain and outfall runoff from the site to existing sufficient adjacent and downstream facilities, as described in the respective drainage reports. Water Quality is being utilized in lieu of a full spectrum detention pond due to the existing regional facility as described earlier in this report. Flows from site will be greater than historic levels. Site appurtenances will not adversely affect the downstream and surrounding developments.

This report and findings is in general conformance with the MDDP and Preliminary Drainage Reports or other pertinent studies

Review 1 comment: Please identify and analyze whether the downstream facilities are adequate to accept the developments flows.

Additionally, compare the detained flows and the historical flow leaving the site. Indicate whether or not the sites flow is at or below historic flows leaving the site.

Review 2: unresolved. Please analyze the downstream facilities (ditches, culverts, storm pipes etc.) and indicate whether they are adequate to accept the developments flows. Please identify the total developed flows of the site and compare with what the existing facilities where designed to.

MAJOR BASIN	SUB BASIN	AF	REA	BA	SIN	Tc MIN	in.	I /hr.	SOIL GRP	DEV. TYPE	C	3	FL 5-ry	OW 100-yr		TURN RIOD
		PLANIM READ	ACRES	LENGTH -FT	HEIGHT -FT								qp -CFS-	qp -CFS-	-ye	ears-
FALCON	0-1	9.75	2.47	300	4.5	27			Α	SF 5AC.	0.12	0.39				
			V=0.82	+480	1.3	+10									-	
						37	2.1	3.6					0.62	3.5	5	100
HISTORIC	A	COGO	5.00	+525	9	+13										
			V=0.65			50	1.8	2.8	A	R/L	0.08	0.35				
	TOTAL		7.47							MIX	0.093	0.362	1.25	7.6	5	100
DEVELOPED	A	COGO	1.68	300	2.5	15.2			A	GRAVEL	0.59	0.70			5	100
			V=3.06	+300	7	+1.6										
						16.8	3.2	5.5					3.2	6.5	5	100
	O1 + A	(DP-1)	4.15	=400	8	+2	3.2	5.5	A	MIX	0.310	0.516				
			V=2.82			52	1.7	2.9	2				2.1	6.2	5	100
	В	COGO	0.66	. 370	2.4	16.4			A	GRAVEL	0.59	0.70	1.3	2.5	5 ·	100
	C	COGO	2.30	300	4	14.5			Α	GRAVEL	0.59	0.70				1
			V=2.66	+340	6	+2.1				18						
						16.6	3.3	5.5					4.5	8.9	5	100
	B+C			+360	8	+2.7										
		(DP-2)	2.96			19.3	3.0	5.1	A	GRAVEL	0.59	0.70	5.2	10.4	5	100
	D	COGO	0.36	240	4.5	11.6	3.8	6.4	A	GRAVEL	0.59	0.70	0.8	1.6	5	100
	B+C+D		V=2.22	+50		+0.4										100
		(DP-3)	3.32			19.7	3.0	5.1	A	GRAVEL	0.59	0.70	5.9	11.9	5	100
	+0-1+A		7.47	+240	2.4	+2					.á .					100
						54	1.7	2.8	A	MIX	0.434	0.598	5.5	12.5	5	100
							<u> </u>							<u> </u>	D 4	
HYDI PROJ: FALCON RATIONAL MET	STORAGE	SUB	UTATION BY: O.E. W ATE: 2/4/21	ATTS			OL	IVEF	E. WA 614 ELKT	TTS, CON	ISULTI	NG EN PRINGS, C	[GINEE] :0 80907_	R, INC.		GE 1 OF >

1

	UD-BMP (Version 3.06 O.E, Watts	6, November 2016)	Sheet 1 of					
esigner: ompany:	Oliver E. Watts, CE							
ate:	June 5, 2023		provide calculation					
roject:	Falcon Storage Subdivision		7					
ocation:			determined					
1. Basin Sto	rage Volume							
	ve Imperviousness of Tributary Area, Ia if all paved and roofed areas upstream of sand filter)	$I_a = 62.3$ %						
B) Tribut	ary Area's Imperviousness Ratio (i = I _s /100)	i =0.623						
	r Quality Capture Volume (WQCV) Based on 12-hour Drain Time CV= 0.8 * (0.91* i ³ - 1.19 * i ² + 0.78 * i)	WQCV = 0.20 watersh	ed inches					
D) Contri	ibuting Watershed Area (including sand filter area)	Area = <u>325,393</u> sq ft						
	r Quality Capture Volume (WQCV) Design Volume _{2V} = WQCV / 12 * Area	V _{wqcv} = <u>5,295</u> cu ft						
	latersheds Outside of the Denver Region, Depth of age Runoff Producing Storm	d ₆ = in						
	/atersheds Outside of the Denver Region, r Quality Capture Volume (WQCV) Design Volume	V _{WQCV OTHER} = cu ft						
	Input of Water Quality Capture Volume (WQCV) Design Volume if a different WQCV Design Volume is desired)	V _{wacv user} = cu ft						
2. Basin Ge	ometry	-						
A) WQC\	/ Depth	D _{wacv} = <u>3.0</u> ft						
	Filter Side Slopes (Horizontal distance per unit vertical, flatter preferred). Use "0" if sand filter has vertical walls.	Z = <u>3.00</u> ft / ft	The					
C) Minim	um Filter Area (Flat Surface Area)	A _{Min} = <u>2534</u> sq ft	spreadsheet					
D) Actual	Filter Area	A _{Actual} = <u>504007</u> sq ft	2534 should not be filled in					
E) Volum	e Provided	$V_{T} = 13027$ cu ft	by hand					
3. Filter Mat	erial	Choose One It is "CDOT Class B or C Filter O Other (Explain):	Material					
. Underdra	in System							
		Choose One						
	derdrains provided? drain system orifice diameter for 12 hour drain time	O NO						
ana - ang 2002/2012/2012/2022/20	 i) Distance From Lowest Elevation of the Storage Volume to the Center of the Orifice 	y= <u>0.5</u> ft						
	ii) Volume to Drain in 12 Hours	Vol ₁₂ =5,295 cu ft						
	iii) Orifice Diameter, 3/8" Minimum		orifice doesnt match GEC					

	Design Procedure F	Form: Sand Filter (SF)	
Designer:	O.E, Watts		Sheet 2 of
Company:	Oliver E. Watts, CE		
Date:	June 5, 2023		
Project:	Falcon Storage Subdivision		
Location:			
A) Is an i	able Geomembrane Liner and Geotextile Separator Fabric Impermeable liner provided due to proximity uctures or groundwater contamination?	Choose One O YES NO	,
	tlet Works ribe the type of energy dissipation at inlet points and means of aying flows in excess of the WQCV through the outlet	Riprap at inlet and outlet	
Notes:			

include inlet and outlet riprap protection calculations

					-							
		Depth at Outlet (ft)										
		1.0	1.5	2.0	2.5	3.0	3.5	4.0	4.5			
	2	15.04	7.71	5.10	3.76	2.95	2.41	2.02	1.73			
(acre-ft)	1	7.52	3.86	2.55	1.88	1.48	1.21	1.01	0.87			
	0.6	4.51	2.31	1.53	1.13	0.89	0.72	0.61	0.52			
	0.4	3.01	1.54	1.02	0.75	0.59	0.48	0.40	0.35			
	0.2	1.50	0.77	.0.51	0.38	0.30	0.24	0.20.	0.17			
me	0.1	0.75~	0.39	0.26	0.19	0.15	0.12	0.10	0.09			
Volume	0.06	0.45 .	0.23	0.15	0.11	0.09	0.07	0.06	0.05			
	0.04	0.30	0.15	0.10	0.08	0.06	0.05	0.04	0.03			
Design	0.02	0.15 .	0.08	0.05	0.04	0.03	0.02	0.02	0.02			
Ď	0.01	0.08	0.04	0.03	0.02	0.01	0.01	0.01	0.01			

TABLE SB-1

0-1+A-D WQCV 0.125AF = 5445CF 0.32251112 lea "/16" & 6"

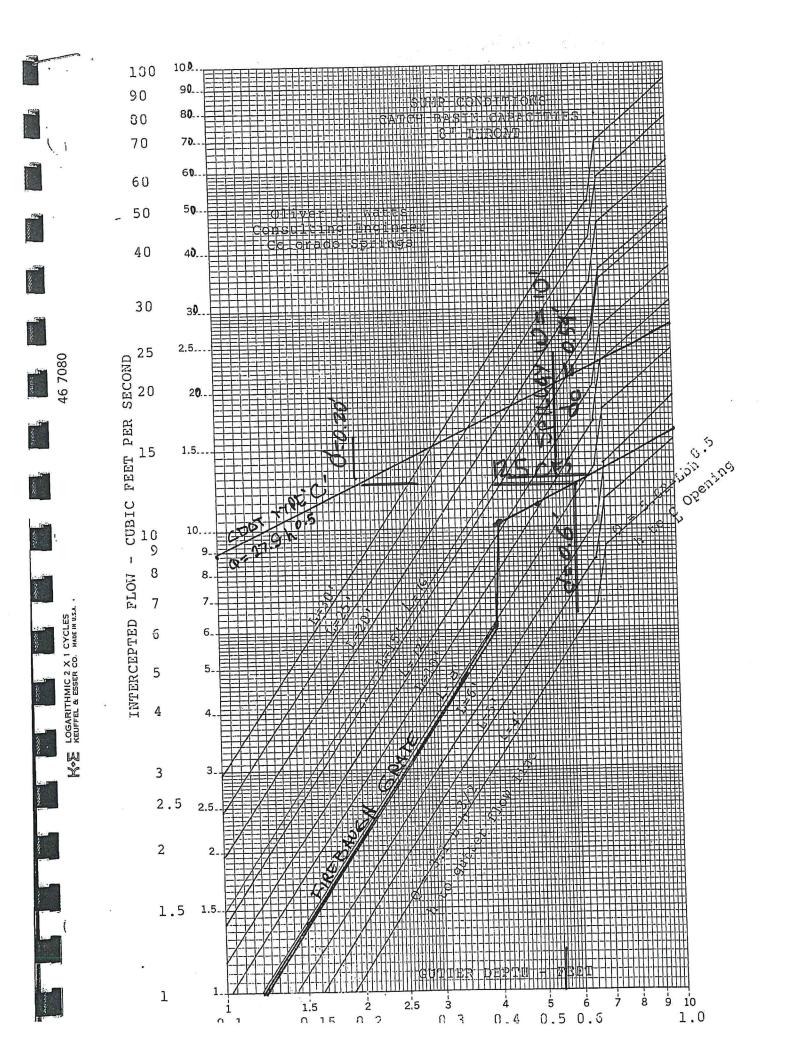
A439 W	1°,
9"1	6
34	
1. 8	
lea	

AF

Hole Diameter	Hole Diameter	Area per Row (in ²)						
(in)	(in)	n = 1	n = 2	n = 3				
1/4	0.250	0.05	0.10	0.15				
5/16	0.313	0.08	0.15	0.23				
3/8	0.375	0.11	0.22	0.33				
7/16	0.438	0.15 -	0.30 .	0.45				
1/2	0.500	0.20	0.39	0.59				
9/16	0.563	0.25	0.50	0.75				
5/8	0.625	0.31	0.61	0.92				
11/16	0.688	(132)	0.74	1.11				
3/4	0.750	0.44	0.88	1.33				
7/8	0.875	0.60	1.20	1.80				
1	1.000	0.79	1.57	2.36				
1 1/8	1.125	0.99	1.99	2.98				
1 1/4	1.250	1.23	2.45	3.68				
1 3/8	1.375	1.48	2.97	4.45				
1 1/2	1.500	1.77	3.53	5.30				
1 5/8	1.625	2.07	4.15	6.22				
1 3/4	1.750	2.41	4.81	7.22				
1 7/8	1.875	2.76	5.52	8.28				
2	2.000	3.14	6.28	9.42				
	n = Numi	ber of columns of perf	orations					

TABLE SB-2

City of Colorado Springs Stormwater Quality Figure SB-2 Outlet Sizing Application Techniques and Maintenance Requirements



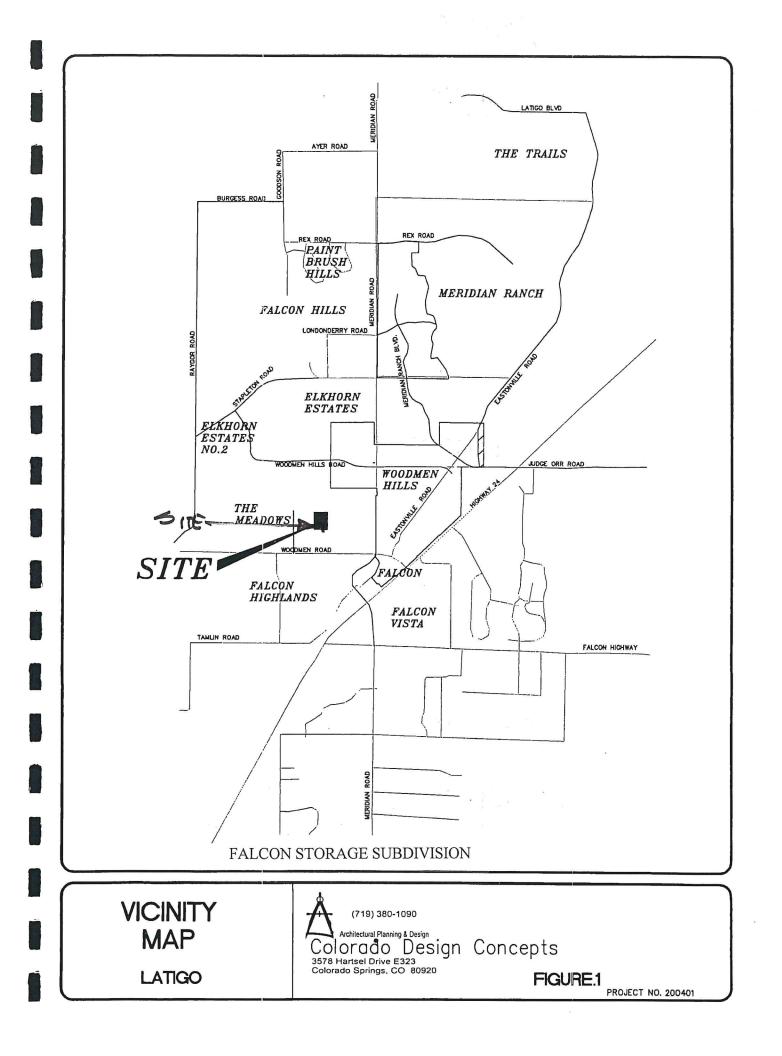
0 = 0.463	8/3 5 ¹ 2
v- n	D D
N	

Q=KS¹2

AMETER	AREA	D 8/3		К		
-IN	$-FT^2$ -	- FT -	N=0.010	N=0.013	N = 0.024	N = 0.026
- <u></u>						
2	0.02182	0.008413	0.3895			
4	0.08727	0.053420	2.4733			<u>,</u>
6	0.19630	0.157500	7.2922	5.609		
8	0.34910	0.339200	15.7050	12.081		
10	0.54540	0.615000	28.4745	21.903		
12	0.78540	1.000000	46.3000	35.615		
15	1.22720	1.813100	83.9465	64.574		
18	1.76710	2,948300	136.5100	105.000	56.88	52.50
$-\frac{10}{21}$	2.40530	4.447400	205.9100	158.400	85.80	79.20
24	3.14160	6.349600	293.9900	226.140	122.49	113.07
27	3.97610	8.692700	402.4700	309.590	167.70	154.79
30	4.90870	11.512600	533.0300	410.030	222.10	205.02
33	5.93960	14.844100		528.680		
36	7.06860	18.720800	866.7700	666.700	361.20	333.30
39	8.29580	23.175100		825.400		
42	9.62110	28.238900		1005.000	544.80	502.50
42	12.56640	40.317500		1436.000	777.80	718.00
54	15.90430	55.195000		1966.000	1065.00	983.00
60	19.63500	73.100400		2604.000	1410.00	1302.00
66	23.75830	94,254200		3357.000	1818.00	1678.00
72	28.27430	118.869400		4234.000	2293.00	2117.00
78	33.18310	147.152900		5241.000	2839.00	2620.00
84	38.48450	179.306000		6386.000	3459.00	3193.00
90	44.17860	215.524500		7676.000	4158.00	3838.00
96	50.26550	256.000000		9118.000	4939.00	4559.00
108	63.61730	350.466600		12480.000	6761.00	6140.00
$\frac{108}{120}$	78.53980	464.158900		16530.000	8954.00	8265.00
120	10.0000					
1					,	

Oliver E. Watts Consulting Engine Colorado Springs

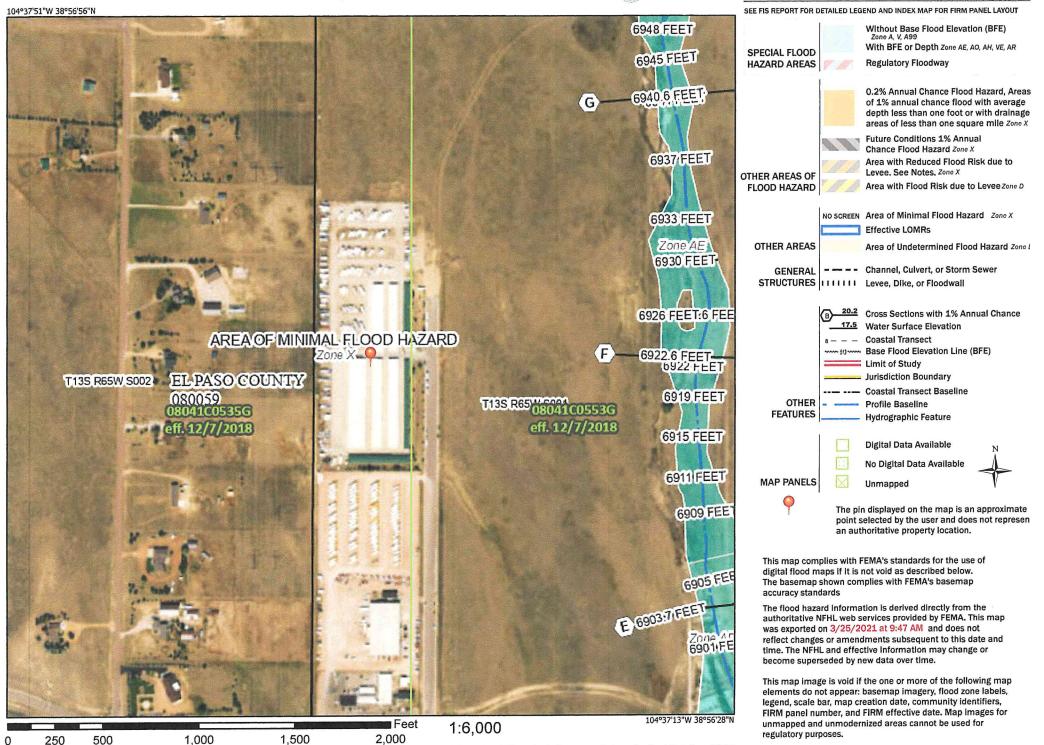
•



National Flood Hazard Layer FIRMette



Legend



1000 National Man. Outbainsadamy Data refracted October 2020

NOTES TO USERS

I may is for use in administering the National Flood Insurance Program. It does necessarily identify all areas subject to flood insurance Program. It does necessarily identify all areas subject to flooding, particularly from local drainage reces of small size. The community map repository should be consulted for saible updated or additional flood hazard information.

o obtain more detailed information in areas where Base Flood Elevations (BFEs) nd/or floodways have been determined, users are encouraged to consult the Flood rolles and Floodway Data and/or Summary of Stillware Elevations tables contained tithin the Flood Insurance Study (FIS) report that accompanies this FIRM. Users hould be aware that BFEs shown on the FIRM represent rounded whole-hould be aware due as the sole source of flood elevation information. Accordingly, odd elevation data present on the FIRM report should be the aware of FIRM for present consults. Accordingly, odd elevation data presented in the FIS report should be the aware ment.

Costal Base Flood Elevations shown on this map apply only landward of 0.0° Ionh American Versical Datum of 1986 (NAVD68). Users of this FIRM should be ware that costal flood elevations are also provided in the Summary of Silwater levations table in the Flood Insurance Study report for this jurisdiction. Elevations hown in the Summary of Silwater Elevations table should be used for construction ndfor floodplain management purposes when they are higher than the elevations hown on the FIRM.

Boundaries of the floodways were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations with regard to requirements of the National Flood Insurance Program. Floodway withs and other pertinent floodway data are provided in the Flood Insurance. Study report for this jurisdiction.

Certain areas not in Special Flood Hazard Areas may be protected by flood con structures. Refer to section 2.4 "Flood Protection Measures" of the Flood Insura Study report for Information on flood control structures for this jurisdiction. res" of the Flood Insurance

The projection used in the preparation of this map was Universal Transverse Mercator (UTM) zone 13. The horizontal datum was NADB3, GRSB0 spheroid, Differences in datum, spherodid, projection or UTM zones zones used in the production of FIRMs for adjacent jurisdictions may result in slight positional differences in map features across jurisdiction boundaries. These differences do not affect the accuracy of this FIRM.

Rood elevations on this map are referenced to the North American Vertical Datum of 1986 (NAVDB). These flood elevations must be compared to structure and ground elevations referenced to the same vertical datum. For information regarding conversion between the National Geodetic Vertical Datum of 1929 and the North American Vertical Datum of 1989, visit the valional Geodetic Survey verbise at http://www.ngs.noaa.gov/ or contact the National Geodetic Survey at the following address:

NGS Information Services NOAA, N/NGS12 National Geodetic Survey SSMC-3, #9202 1315 East-West Highway Silver Spring, MD 20910-3282

obtain current elevation, description, and/or location information for bench mark own on this map, please contact the Information Services Branch of the Nationa sodetic Survey at (301) 713-3242 or visit its website at http://www.ngs.ncaa.gov/.

iase Map information shown on this FIRM was provided in digital format by El Paso Jounty, Colorado Springa Utilities, City of Fountain, Bureau of Land Management, lational Oceanic and Almospheric Administration, United States Geological Survey, and Anderson Consulting Engineers, Inc. These data are current as of 2006.

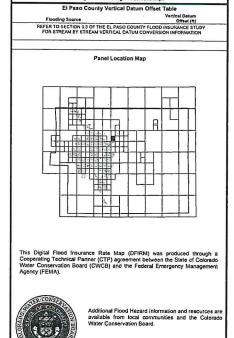
This map reflects more detailed and up-to-date stream channel configurations and floodplain delineations than those shown on the previous FIRM for this juriadicion. The floodplain delineations than those shown on the previous FIRM may have been adjusted to conform to these new stream channel configurations. As a result, the Flood Profiles and Floodway Data tables in the Flood Insurance Study Report (which contains authoritative hydraulic data) may reflect stream channel distances that offler from what is shown on this map. The profile baselines depicted on this map represent the hydraulic modeling baselines that match the flood profile asteriline that profiles the profiles of the FIS report. As a result, the profile asterilines may appear outside of the floodplain.

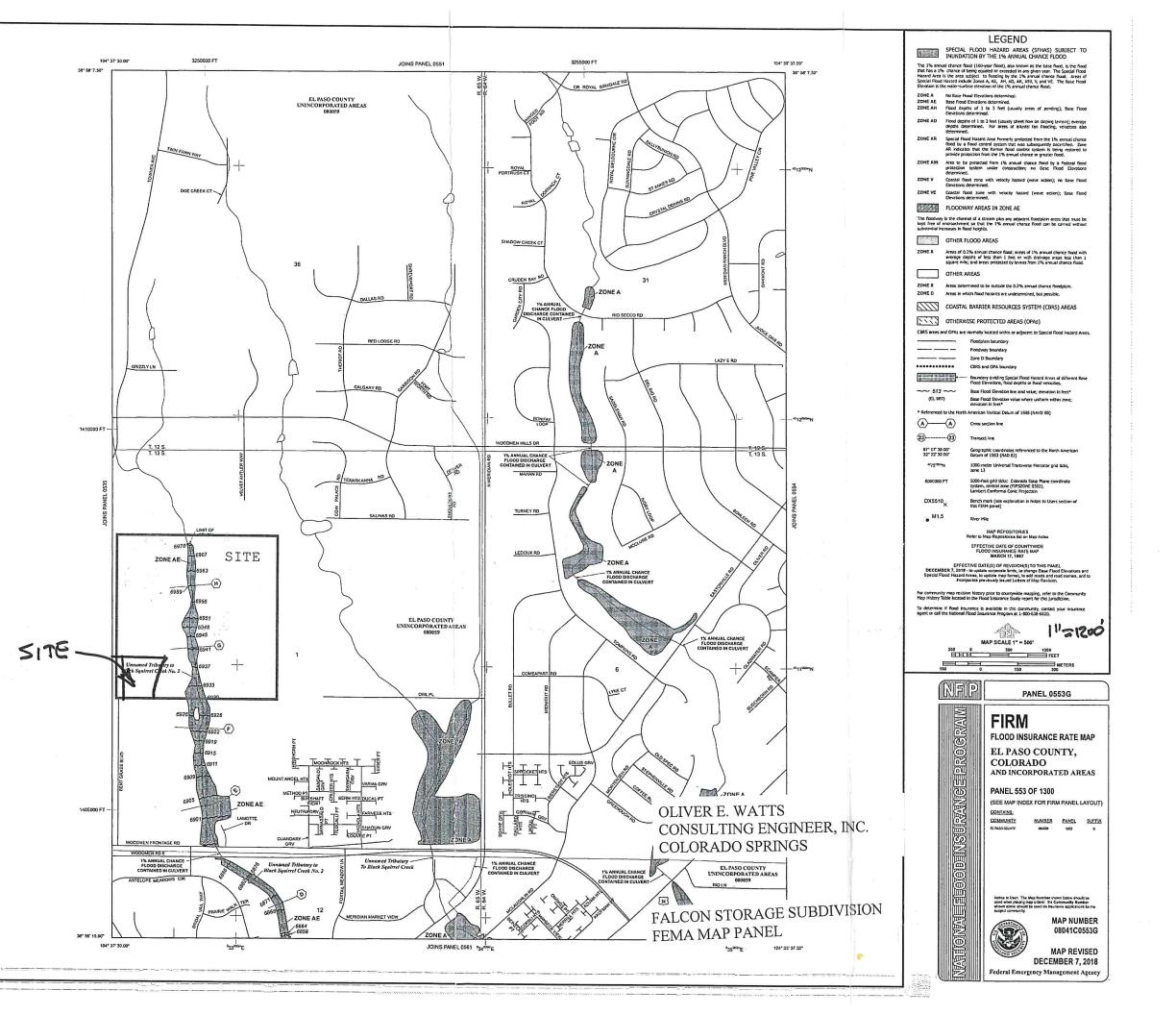
Corporate limits shown on this map are based on the best data available at the time of publication. Because changes due to annexations or de-annexations may have occurred utter this map was published, map users should contact appropriate community officials to verify current corporate limit locations.

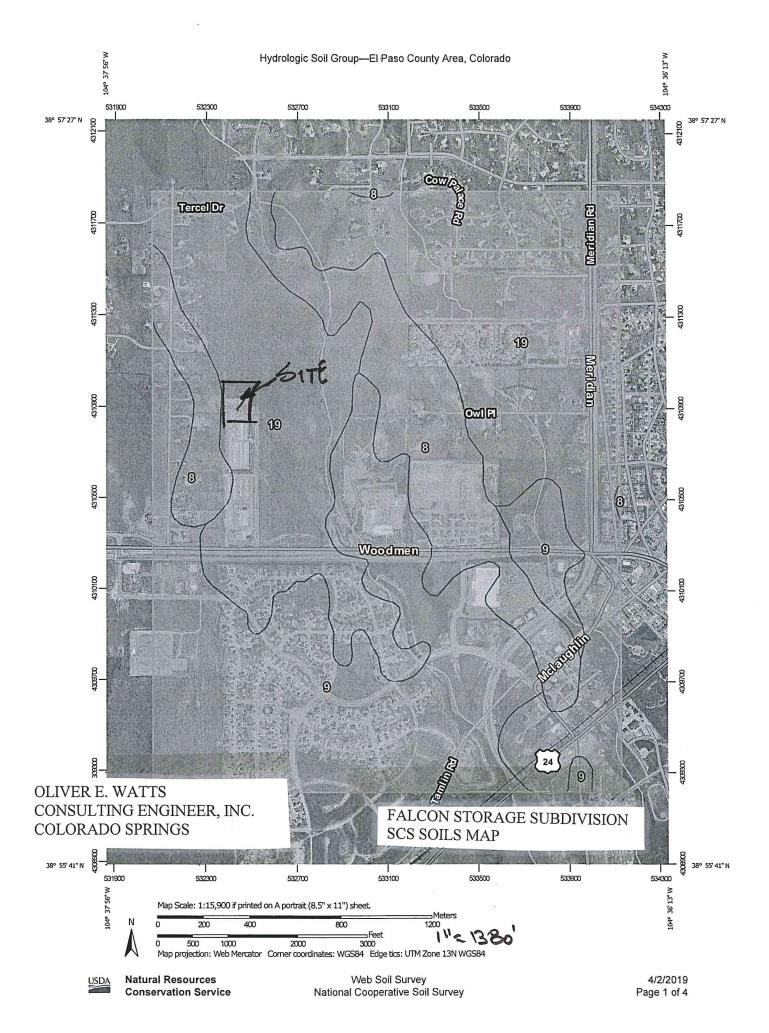
Please refer to the separately printed Map Index for an overview map of the count showing the layout of map panels; community map repository addresses; and Listing of Communities table containing National Flood Insurance Program dates fo each community as well as a listing of the panels on which each community is

Contact FEMA Map Service Center (MSC) via the FEMA Map Information eXchange (FMIX) 1-077-336-2627 for information on available products associated with this FRM. Available products may include previously issued Letters of Map Change, a Rood Insurance Study Report, and/or digital versions of this map. The MSC may also be reached by Fox at 1-800-358-8620 and its website at http://www.msc.lema.gov/

I you have questions about this map or questions concerning the National Flood nsurance Program in general, please cal 1-877-FEMA MAP (1-877-336-2627) or isit the FEMA website at http://www.fema.gov/business/nfp.







EL PASO COUNTY AREA, COLORADO

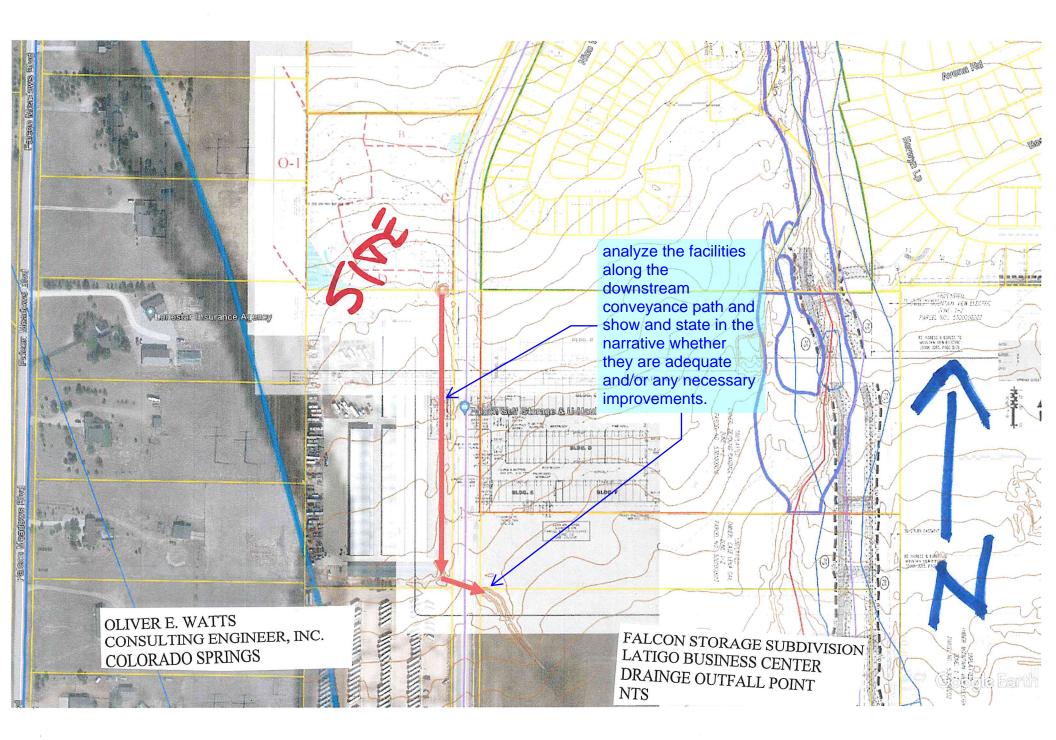
TABLE 16.--SOIL AND WATER FEATURES

Absence of an entry indicates the feature is not a concern. See "flooding" in Glessely for definition of terms as "rare," "brief," and "very brief." The symbol > means greater than]

	11		Flooding		Bedr	ock	_ Potential	
Soil name and map symbol	Hydro- logic group	Frequency	Duration	Months	Depth	Hardness	frost action	
llamosa: 1	С	Frequent	Brief	May-Jun	<u>In</u> >60		High.	
Iscalon: 2, 3	В	None			>60		Moderate:	
3adland: 4	D							
3ijou: 5, 6, 7	В	None			>60	 	Low.	
31akeland: 8	А	None			>60		Low.	
1g: Blakeland part-	A	None			>60		Low.	
Fluvaquentic Haplaquolls part	D	Common	Very brief	Mar-Aug	>60		High.	
Blendon: 10	В	None			>60		Moderate.	
Bresser: 11, 12, 13	В	None			>60		Low.	
Brussett: 14, 15	B	None	·		>60		Moderate.	
Chaseville: 16, 17	A A	None			>60		Low.	
¹ 18: Chaseville part	A	None			>60		Low.	
Midway part	D	None			10-20	Rippable	Moderate.	
Columbine: 19	$\left(\right)$	None to rare			>60		Low.	
Connerton: ¹ 20: Connerton part-	В	None			; >60		High.	
Rock outcrop part	D	,						
Cruckton: 21	В	None			>60		Moderate.	
Cushman: 22, 23	с	None			20-40	Rippable	Moderate.	
¹ 24: Cushman part	с	None			20-40	Rippable	Moderate.	
Kutch part	С	None			20-40	Rippable	Moderate.	
Elbeth: 25, 26	В	None			>60		Moderate.	
¹ 27: Elbeth part	В	None			>60		Moderate.	

See footnote at end of table.

MSV



Land Use or Surface	Percent Impervious	Runoff Coefficients											
Characteristics		2-year		5-year		10-year		25-year		50-year		100-year	
		HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D
Business													
Commercial Areas	95	0.79	0.80	0.81	0.82	0.83	0.84	0.85	0.87	0.87	0.88	0.88	0.89
Nelghborhood Areas	70	0.45	0.49	0.49	0.53	0.53	0.57	0.58	0.62	0.60	0.65	0.62	0.68
Residential													
1/8 Acre or less	65	0.41	0.45	0.45	0.49	0.49	0,54	0.54	0.59	0.57	0.62	0.59	0.65
1/4 Acre	40	0.23	0.28	0.30	0.35	0.36	0.42	0.42	0.59		0.62		
1/3 Acre	30	0.18	0.22	0.25	0.30	0.30	0.42	0.42	0.30	0.46		0.50	0.58
1/2 Acre	25	0.15	0.20	0.22	0.28	0.30	0.36	0.33	0.47	0.43	0.52	0.47	0.57
1 Acre	20	0.12	0.17	0.22	0.26	0.30	0.38	0.37	0.46	0.41	0.51	0.46	0.56
												0.11	0.55
Industrial		9											
Light Areas	80	0.57	0.60	0.59	0.63	0.63	0.66	0.66	0.70	0.68	0.72	0.70	0.74
Heavy Areas	90	0.71	0.73	0.73	0.75	0.75	0.77	0.78	0.80	0.80	0.82	0.81	0.83
Parks and Cemeteries	7	0.05	0.09	0.12	0.19	0.20	0.29	0.30	0.40	0.34	0.46	0.39	0.52
Playgrounds	13	0.07	0.13	0.16	0.23	0.24	0.31	0.32	0.40	0.37	0.48	0.33	0.52
Railroad Yard Areas	40	0.23	0.28	0.30	0.35	0.36	0.42	0.42	0.50	0.46	0.54	0.41	0.54
Undeveloped Areas									12				
Historic Flow Analysis	2												
Greenbelts, Agriculture		0.03	0.05	0.09	0.16	0.17	0.26	0.26	· .0.38	0.31	0.45	0.36	0.51
Pasture/Meadow	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50
Forest	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50
Exposed Rock	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0,94	0.95	0.95	0.96	0.96
Offsite Flow Analysis (when	45												
landuse is undefined)		0.26	0.31	0.32	0.37	0.38	0.44	0.44	0.51	0.48	0.55	0.51	0.59
Streets	.												
Paved	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Gravel	80	0.57	0.60	0.59	0.63	0.63	0.66	0.66	0.70	0.68	0.33	0.98	0.96
				-								-	
Drive and Walks	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Roofs	90	0.71	0.73	0.73	0.75	0.75	0.77	0.78	0.80	0.80	0.82	0.81	0.83
awns	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0,37	0.30	0.44	0.35	0.50

Table 6-6. Runoff Coefficients for Rational Method (Source: UDFCD 2001)

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3.2 Time of Concentration

One of the basic assumptions underlying the Rational Method is that runoff is a function of the average rainfall rate during the time required for water to flow from the hydraulically most remote part of the drainage area under consideration to the design point. However, in practice, the time of concentration can be an empirical value that results in reasonable and acceptable peak flow calculations.

For urban areas, the time of concentration (t_c) consists of an initial time or overland flow time (t_i) plus the travel time (t_i) in the storm sewer, paved gutter, roadside drainage ditch, or drainage channel. For nonurban areas, the time of concentration consists of an overland flow time (t_i) plus the time of travel in a concentrated form, such as a swale or drainageway. The travel portion (t_i) of the time of concentration can be estimated from the hydraulic properties of the storm sewer, gutter, swale, ditch, or drainageway. Initial time, on the other hand, will vary with surface slope, depression storage, surface cover, antecedent rainfall, and infiltration capacity of the soil, as well as distance of surface flow. The time of concentration is represented by Equation 6-7 for both urban and non-urban areas.

(Eq. 6-7)

$$t_c = t_i + t_i$$

Where:

 t_c = time of concentration (min)

 t_i = overland (initial) flow time (min)

 t_t = travel time in the ditch, channel, gutter, storm sewer, etc. (min)

3.2.1 Overland (Initial) Flow Time

The overland flow time, t_i , may be calculated using Equation 6-8.

$$t_i = \frac{0.395(1.1 - C_5)\sqrt{L}}{S^{0.33}}$$
(Eq. 6-8)

Where:

 t_i = overland (initial) flow time (min)

- C_5 = runoff coefficient for 5-year frequency (see Table 6-6)
- L = length of overland flow (300 ft maximum for non-urban land uses, 100 ft maximum for urban land uses)

S = average basin slope (ft/ft)

Note that in some urban watersheds, the overland flow time may be very small because flows quickly concentrate and channelize.

3.2.2 Travel Time

For catchments with overland and channelized flow, the time of concentration needs to be considered in combination with the travel time, t_t , which is calculated using the hydraulic properties of the swale, ditch, or channel. For preliminary work, the overland travel time, t_t , can be estimated with the help of Figure 6-25 or Equation 6-9 (Guo 1999).

$$V = C S^{0.1}$$

Where:

V = velocity (ft/s)

 C_{ν} = conveyance coefficient (from Table 6-7)

 S_w = watercourse slope (ft/ft)

ai is

(Eq. 6-9)

Type of Land Surface	C_{ν}
Heavy meadow	2.5
Tillage/field	5
Riprap (not buried)*	6.5
Short pasture and lawns	7
Nearly bare ground	10
Grassed waterway	15
Paved areas and shallow paved swales	20

Table 6-7.	Conveyance	Coefficient, C_{ν}
------------	------------	------------------------

For buried riprap, select C_v value based on type of vegetative cover.

The travel time is calculated by dividing the flow distance (in feet) by the velocity calculated using Equation 6-9 and converting units to minutes.

The time of concentration (t_c) is then the sum of the overland flow time (t_l) and the travel time (t_l) per Equation 6-7.

3.2.3 First Design Point Time of Concentration in Urban Catchments

Using this procedure, the time of concentration at the first design point (typically the first inlet in the system) in an urbanized catchment should not exceed the time of concentration calculated using Equation 6-10. The first design point is defined as the point where runoff first enters the storm sewer system.

$$t_c = \frac{L}{180} + 10$$

(Eq. 6-10)

Where:

 t_c = maximum time of concentration at the first design point in an urban watershed (min)

L = waterway length (ft)

Equation 6-10 was developed using the rainfall-runoff data collected in the Denver region and, in essence, represents regional "calibration" of the Rational Method. Normally, Equation 6-10 will result in a lesser time of concentration at the first design point and will govern in an urbanized watershed. For subsequent design points, the time of concentration is calculated by accumulating the travel times in downstream drainageway reaches.

3.2.4 Minimum Time of Concentration

If the calculations result in a t_c of less than 10 minutes for undeveloped conditions, it is recommended that a minimum value of 10 minutes be used. The minimum t_c for urbanized areas is 5 minutes.

3.2.5 Post-Development Time of Concentration

As Equation 6-8 indicates, the time of concentration is a function of the 5-year runoff coefficient for a drainage basin. Typically, higher levels of imperviousness (higher 5-year runoff coefficients) correspond to shorter times of concentration, and lower levels of imperviousness correspond to longer times of

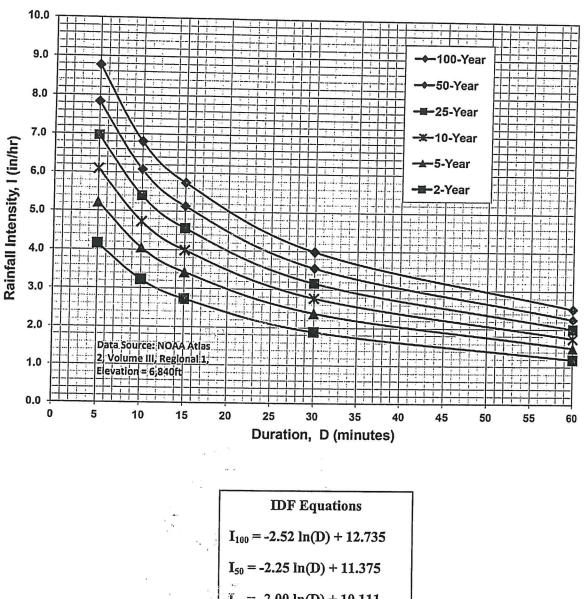


Figure 6-5. Colorado Springs Rainfall Intensity Duration Frequency

