

PRELIMINARY AND FINAL DRAINAGE PLAN AND REPORT FALCON STORAGE SUBDIVISION

PART OF THE SW1/4 SECTION 1, T.13S. R.65W. OF THE 6^{TH} P.M. EL PASO COUNTY

February 4, 2021

Revised November 23, 2022

> Revised June 7, 2023

Revised June 22, 2023

Revised August 31, 2023

Revised December 12, 2023

PCD File No. PPR2232 PCD File No. MS232

Prepared for Falcon Storage Partners LLLP 4615 Northpark Drive Colorado Springs, CO 80918

Oliver E. Watts, Consulting Engineer, Inc. Colorado Springs, Colorado

OLIVER E. WATTS, PE-LS

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Celebrating over 44 years in business

December 13, 2023

El Paso County Planning and Community Development 2880 International Circle Colorado Springs, CO 80910

ATTN: Joshua Palmer, P.E.

SUBJECT: Preliminary and Final Drainage Plan and Report Falcon Storage Subdivision

Transmitted herewith for your review and approval is the drainage plan and report for The Falcon Storage Subdivision in El Paso County. This report will accompany the development plan and subdivision plat submittal. This report has been revised in accordance with your review comments of November 23, 2022, March 2, 2023, August 18, 2023 and October 16, 2023.

Please contact me if I may provide any further information.

Oliver E. Watts, Consulting Engineer, Inc.

BY:	
Oliver E. Watts, President	

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FALCON STORAGE SUBDIVISION DRAINAGE REPORT REFERENCES

City-County Drainage Criteria, current edition
Fema Firm Insurance Rate Map
El Paso County Soils Survey, SCS
Falcon Drainage Basin Planning Study
Drainage Report, Falcon Meadows at Bent Grass
Drainage Report, Latigo Business Center, Lot 1

1. ENGINEER'S STATEMENT:

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the County for drainage reports and said report is in conformity with the applicable master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.

Oliver E. Watts, C	onsulting Engineer, Inc.	
Oliver E. Watts	Colo. PE-LS No. 9853	date
2. OWNERS / DE	VELOPER'S STATEMENT:	
I the owner / devel drainage report and		with all of the requirements specified in this
Falcon Storage Par	tners LLLP	
By:		
Richard Graham		Date
4615 Northpark Dr Colorado Springs,		
3. EL PASO COU	UNTY:	
	•	Paso Land Development Code, Drainage ring Criteria Manual, as amended.
Joshua Palmer, P.F. County Engineer /	E., ECM Administrator	date
Conditions:		

4. LOCATION AND DESCRIPTION:

The Falcon Storage Subdivision is located in the Latigo Business Center development of El Paso County as shown on the enclosed vicinity map. Occupying a portion of the West half of Section 1, Township 13 South, Range 65 West of the 6th P.M., totaling 5.004 acres. It is located in the Falcon Drainage Basin as shown on the enclosed basin map. It lies west of Bent Grass Meadows Drive north of the Latigo Business Center Filing No. 1 as shown on the enclosed drainage plan. The site will be developed into an RV Storage site as shown on the enclosed drainage plan, as an expansion to the one in the Latigo Business Center Filing No. 1, both owned by the developer.

5. FLOOD PLAIN STATEMENT:

This subdivision is not within the limits of a flood plain or flood hazard area, according to FEMA map panel number 08041C0553 G, dated December 7, 2018, a copy of which is enclosed for reference.

6. METHOD AND CRITERIA:

The method used for all computations is that specified in the City-County Drainage Criteria Manual, using the rational method for areas of the size of the development. All computations are enclosed for reference and review. Pertinent portions of the criteria are enclosed.

The soils in the subdivision have been mapped by the local USDA/SCS office, and a soils map and interpretation sheet are enclosed for reference. All soils in this area are of hydrologic group "A" within the development area.

7. DESCRIPTION OF RUNOFF:

A. Drainage Inflows: The drainage Report for Falcon Meadows at Bent Grass indicates an existing drainage swale above the north boundary to divert runoff from this site and route it to Bent Grass Meadows and then past this development in Bent Grass Meadows Drive to outfall points to an existing detention pond across the street. A copy of this drainage plan is enclosed. Also shown on this map is that portion of the Meadows Filing No. 1 that drains 0.62 cfs / 3.5 cfs (5-year / 100-year runoffs) into this subdivision along the westerly boundary (Basin O-1), and it indicates the historic undeveloped runoff of the site, Basin A (historic) totaling 1.25 cfs / 7.6 cfs at the lowest (southeast) portion of the subdivision.

B. Interior Routing: The area will be graded to conform to the existing topography shown on the drainage plan. The property has been rough graded, which complies with the historic runoff pattern. Additional grading is indicated which is intended to contain the runoff into the interior drive isle street network, and along the streets to the water quality pond The westerly street (Basin A) will combine with offset basin O-1 to develop 3.0 cfs \ 6.2 cfs (5-year / 100-year runoffs) near the in the southwest corner of the plat (Design Point 1). Basin B will develop 1.3/2.5 cfs in the southerly driveway adjacent to the north entrance. It will combine with basin C along the same routing for 5.2/10.4 cfs at the southwest intersection (design point 2). This will combine basin D to outfall into the water quality pond (design point 3). The total outfall at this point 5.5 cfs/12.5 cfs, into the sand filter basin.

C. Detention Storage: At the proposed outfall point a sand filter water quality pond is proposed, as required by the County. The pond is sized for a temporary sedimentation basin to be used during the construction period and converted into a permanent sand filter basin upon completion. The sedimentation basin will contain 9000 +CF (at 1800 CF per acre). An 8-inch riser pipe is used as an outlet, with holes drilled as computed to detain the runoff as required. One foot of freeboard is provided with a spillway that will pass the 100-year runoff. Details are shown on the enclosed drainage plan. Following construction the basin will be converted to a sand filter basin. A 4-inch slotted underdrain will be placed in a section of CDOT class C Filter material and drain into the grated inlet outlet structure set at the WQCV level, and sized for the 100-year runoff. An orifice plate will be provided on the end of the underdrain with an orifice sized for the installation. Sand filter water quality basin computation sheet is included for the basin. Fully

developed runoffs are analyzed for the basin. As required by the County, the basin is used for water quality storage only and the outfall will run across Latigo Business Center Filing No. 1 to an existing full spectrum pond (Pond WU) to the south of Woodmen Road, north of Highway 24, between Tamlin and Meridian Roads, in accordance with the approved drainage reports for the area. This outfall run is described below.

D. Outfall Point: Discharge from the subdivision will be into existing north-south street of Lot 1 of the Latigo Business Center, filing no. 1, as shown on the drainage plan. Some minor construction is shown along the north boundary of Lot 1 as shown on the drainage plan to create a positive installation. The two properties are under common ownership and permission to outfall into the Latigo Business Center is granted. The drainage plan for the Latigo Business Center is enclosed. This report indicated two existing discharges: 0.2 cfs / 0.5 cfs near the southwest corner and 4.1 cfs / 10.1 cfs over the remaining south frontage. A 24 inch RCP will run from the CDOT Type C outlet box at a minimum slope of 0.22% into the existing ditch shown on the drainage plan.

As shown on the enclosed drainage plan for Lot 1 of the Latigo Business Park and the enclosed sheet 7 of the computations the swales along said Lot 1 adjacent to Bent Grass Meadows Boulevard are more than adequate to safely contain the drainage outfall from this subdivision. The depth of runoff from the pond is 0.21 feet in the upper swale and 0.49 feet below the entrance to Lot 1. These swales also indicate more that adequate freeboard according to the grading plan. At the bottom (South) of Lot 1 is the storm sewer system that diverts the runoff from the District 49 bus facility and Bent Grass Meadows Boulevard eastward toward the above mentioned full spectrum pond. This being the limit of the first public storm sewer and our required justification.

WATER QUALITY

A sand filter basin water quality facility will be provided:

FOUR STEP PROCESS

The following process has been followed to minimize adv

As indicated in the meeting with staff, Please analyze this storm pipe and indicate whether it is adequate for the increase in flows. As indicated above this site will increase flows 2.4 cfs (100yr) from what the Lot 1 report indicates.

Runoff Reduction: The scope of the development has b what the Lot Treport indicates. ments to present the minimum footprint in providing a RV Storage development. The undisturbed portions are to be landscaped to reduce the impervious percent.

Water Quality Unresolved.

<u>Provide WQCV:</u> <u>Detention</u> water quality storage is being provided for this subdivision by a sand filter <u>detention</u> pond and runoff will be routed to a full spectrum pond located downstream, south of Woodmen Road, north of Highway 24, between Tamlin and Meridian Roads, by others as a sub regional facility.

<u>Stabilize Drainage Ways:</u> The site will be graded to route the runoff over improved street installations to provide channel stabilization in the natural erosive material over the site. Discharge from the site will be into adjacent and downstream facilities in accordance with the master drainage basin plan for the Falcon drainage basin and previously approved subdivision drainage reports. Copies of each plan are enclosed. There will be no adverse affect on downstream developments as a result of this subdivision

<u>Consider need for Industrial and Commercial BMP's:</u> This is a RV Storage site, so source control problems will be a minimum. During construction, standard site specific state of the art BMP's will be employed to minimize and mitigate erosive problems.

8. COST ESTIMATE:

Item No.	<u>Description</u>	Quantity	<u>Unit Cost</u>	<u>Cost</u>
1	Pond/BMP Earthwork	881 CY	\$ 23.00	\$ 20263.00
2	Slotted drain	187 LF	40.00	7480.00
3	Riprap	14 Tons	80.00	1096.00
4	Grated Inlet	1 ea	5611.00	5611.00
4	12" PVC drain	106 LF	112.00	11872.00
5	Concrete Pond Inlet	15 CY	589.00	10335.00
6	24" RCP Pond Outlet	106 LF	91.00	9646.00
	Subtotal Construction Cost			\$ 66303.00
	Engineering	10%		6630.30
	Total Estimated Cost			\$ 72933.30

9. FEES: Due at plat recording.

2023 Falcon Basin Fees: 5.004 acres @46.4% Impervious = 3.1175 Impervious acres (see p. 6-17)

Drainage fees @ \$ 37,256 per acre = \$ 86,503.07 Bridge fees @ \$ 5,118 per acre = \$ 11,083.26

Total Fees: \$ 90,386.33

10. SUMMARY

The Falcon Storage Subdivision is a proposed 1-lot, RV Storage subdivision containing 5.004 acres. The proposed street facilities will adequately convey, detain and outfall runoff from the site to existing sufficient adjacent and downstream facilities, as described in this report and the respective drainage reports. Water Quality is being utilized in lieu of a full spectrum detention pond due to the existing regional facility as described earlier in this report. Flows from site will be greater than historic levels. Site appurtenances will not adversely affect the downstream and surrounding developments.

This report and findings is in general conformance with the MDDP and Preliminary Drainage Reports or other pertinent studies

MAJOR BASIN	SUB BASIN	AI	REA	BA	SIN	Tc MIN	1000	I /hr.	SOIL GRP	DEV. TYPE	(FL 5-ry	OW 100-yr		TURN RIOD	
		PLANIM READ	ACRES	LENGTH -FT	HEIGHT -FT		1						qp -CFS-	qp -CFS-	-у	ears-	
FALCON	0-1	0-1	9.75	2.47	300	4.5	27			A	SF 5AC.	0.12	0.39			-	
	2		V=0.82	+480	1.3	+10						+ 1	in A Top to	7 7 1	153	1	
					11 14 77	37	2.1	3.6				-	0.62	3.5	5	10	
HISTORIC	A	COGO	5.00	+525	9	+13											
			V=0.65	1 - 11		50	1.8	2.8	A	R/L	0.08	0.35	1-1		-		
	TOTAL		7.47							MIX	0.093	0.362	1.25	7.6	5	10	
DEVELOPED	Α	COGO	1.68	300	2.5	15.2			A	GRAVEL	0.59	0.70			5	10	
			V=3.06	+300	7	+1.6		1 -= 1	11								
					1000	16.8	3.2	5.5				1 -2	3.2	6.5	5	10	
	01+A	(DP-1)	4.15	=400	8	+2	3.2	5.5	A	MIX	0.310	0.516			100	1 -	
			V=2.82			52	1.7	2.9				L = 43	2.1	6.2	5	10	
	В	COGO	0.66	370	2.4	164			4	CDAVEL	0.50	0.70	1.3	2.5	5.	10	
	C		0.66	300		16.4			A	GRAVEL	0.59	0.70	1,3	2.3	3.	10	
	C	COGO	2.30	X516071	4	1 2 2 2 2 2 2			Α	GRAVEL	0.39	0.70				-	
	-		V=2.66	+340	6	+2.1	2.2				-		1.5	0.0	5	10	
	B+C	-		+360	8	16.6	3.3	5.5			-		4.5	8.9	3	10	
	B+C	(DP-2)	2.96	+300	0	19.3	3.0	5.1	A	GRAVEL	0.59	0.70	5.2	10.4	5	10	
	D	COGO	0.36	240	4.5	11.6	3.8	6.4	A	GRAVEL	0.59	0.70	0.8	1.6	5	10	
	B+C+D	0000	V=2.22	+50	1.0	+0.4	5.0	0.1		Oldital	0.05	0.70	V.0	110	-	1	
		(DP-3)	3.32	3.8.6		19.7	3.0	5.1	A	GRAVEL	0.59	0.70	5.9	11.9	5	10	
	+0-1+A	,/	7.47	+240	2.4	+2			1		~						
			7.53 (- 1		54	1.7	2.8	Α	MIX	0.434	0.598	5.5	12.5	5	10	
HYDI ROJ: FALCON ATIONAL MET		SUB	BY: O.E. W		N. J. J.		OL	IVER		TTS, CON				R, INC.		GE 1	

	Design Procedure Fo	orm: Sand Filter (SF)
Designer: Company: Date: Project: Location:	UD-BMP (Version 3 Oliver E. Watts Olier E. Watts, Consulting Engineer, Inc. December 15, 2023 Falcon Storage	.07, March 2018) Sheet 1 of 2
A) Effective (100%) B) Tribut C) Wate WQC D) Contr E) Wate Vwate F) For WAvers G) For V Wate H) User	orage Volume live Imperviousness of Tributary Area, I _a 6 if all paved and roofed areas upstream of sand filter) lary Area's Imperviousness Ratio (I = I _a /100) If Quality Capture Volume (WQCV) Based on 12-hour Drain Time CV= 0.8 * (0.91* I ³ - 1.19 * I ² + 0.78 * I) Inbuting Watershed Area (including sand filter area) If Quality Capture Volume (WQCV) Design Volume CV = WQCV / 12 * Area Vatersheds Outside of the Denver Region, Depth of age Runoff Producing Storm Vatersheds Outside of the Denver Region, Input of Water Quality Capture Volume (WQCV) Design Volume Input of Water Quality Capture Volume (WQCV) Design Volume Input of Water Quality Capture Volume is desired)	provide calculations for determining percentage Unresolved. = 0.464 Wacv = 0.16 watershed inches Area = 325,393 sq ft Vwacv = 4,265 cu ft d _g = in Vwacv other = cu ft
4:1 or C) Minim D) Actua	V Depth Filter Side Slopes (Horizontal distance per unit vertical, flatter preferred). Use "0" if sand filter has vertical walls. um Filter Area (Flat Surface Area) i Filter Area	D _{WQCV} = 3.0 ft Z = 3.00 ft / ft DIFFICULT TO MAINTAIN, INCREASE WHERE POSSIBLE A _{Min} = 1887 sq ft A _{Actual} = 2100 sq ft V _T = 11278 cu ft Choose One © 18" CDOT Class B or C Filter Material O Other (Explain):
	ain System Inderdrains provided? Indrain system orifice diameter for 12 hour drain time I) Distance From Lowest Elevation of the Storage Volume to the Center of the Orifice II) Volume to Drain in 12 Hours III) Orifice Diameter, 3/8" Minimum	Choose One YES NO $y = 0.5$ ft $t = 0.5$ ft $t = 0.5$ cu ft $t = 0.5$ in

	Design Procedure	Form: Sand Filter (SF)	
Situata	TENTO CONTRACTOR OF THE PERSON		Sheet 2 of 2
Designer:	Oliver E. Watts		
Company:	Oller E. Watts, Consulting Engineer, Inc.		
Date:	December 15, 2023		
Project: Location:	Falcon Storage		
A) Is an	able Geomembrane Liner and Geotextile Separator Fabric impermeable liner provided due to proximity uctures or groundwater contamination?	Choose One O YES NO	
	tlet Works ribe the type of energy dissipation at inlet points and means of eying flows in excess of the WQCV through the outlet	Riprap at inlet and spilliway and pipe end	

Required Area per Row (in²)

	1	Depth at Outlet (ft)											
		1.0	1.5	2.0	2.5	3.0	3,5	4.0	4.5				
	2	15.04	7.71	5.10	3.76	2.95	2.41	2.02	1.73				
	1	7.52	3.86	2.55	1.88	1.48	1.21	1.01	0.87				
9	0.6	4.51	2,31	1.53	1.13	0.89	0.72	0.61	0.52				
(acre-ft)	0.4	3.01	1.54	1.02	0.75	0.59	0.48	0.40	0.35				
1000	0.2	1.50	0.77	.0.51	0.38	0.30	0.24	0.20	0.17				
E	0.1	0.75	0.39	0.26	0.19	0.15	0.12	0.10	0.09				
Volume	0.06	0.45 .	0.23	0.15	0.11	0.09	0.07	0.06	0.05				
2	0.04	0.30	0.15	0.10	0.08	0.06	0.05	0.04	0.03				
Design	0.02	0.15	0.08	0.05	0.04	0.03	0.02	0.02	0.02				
ă	0.01	0.08	0.04	0.03	0.02	0.01	0.01	0.01	0.01				

TABLE SB-1

0-1+ A-D wacr 0.125 AF = 5445CF 0.3225 1112 GC 6"

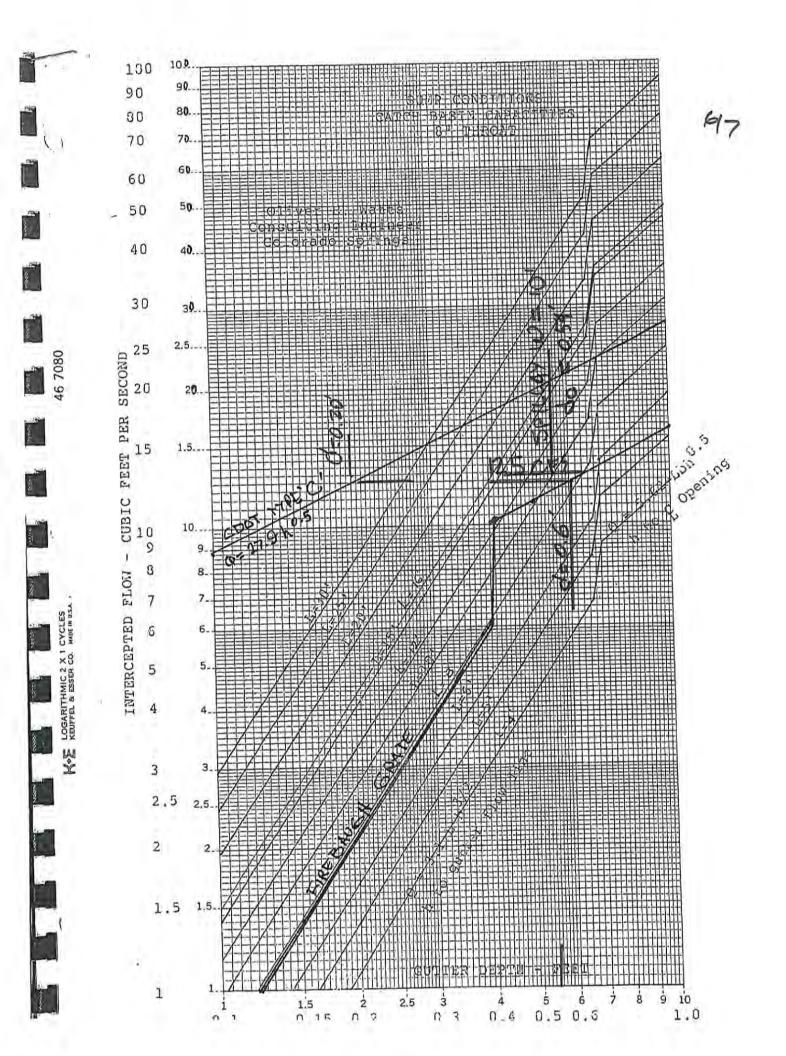
Hole Diameter	Hole Diameter	Are	a per Row (in²)	
(in)	(in)	n = 1	n = 2	n = 3
1/4	0.250	0.05	0.10	0.15
5/16	0.313	0.08	0.15	0.23
3/8	0.375	0.11	0.22	0.33
7/16	0.438	0.15 :	0.30	0.45
1/2	0.500	0.20	0.39	0.59
9/16	0.563	0.25	0.50	0.75
5/8	0.625	0.31	0.61	0.92
11/16	0.688	(233)	0.74	1.11
3/4	0.750	0.44	0.88	1.33
7/8	0.875	0.60	1.20	1.80
1	1.000	0.79	1.57	2.36
1 1/8	1.125	0.99	1.99	2.98
1 1/4	1.250	1.23	2.45	3,68
1 3/8	1.375	1.48	2.97	4.45
1 1/2	1.500	1.77	3.53	5.30
1 5/8	1.625	2.07	4.15	6.22
1 3/4	1.750	2.41	4.81	7.22
1 7/8	1.875	2.76	5.52	8.28
2	2.000	3.14	6.28	9.42
	n = Numb	er of columns of perfo	rations	11.0
Minimum steel	plate thickness	1/4"	5/16"	3/8"

TABLE SB-2

City of Colorado Springs Stormwater Quality

Figure SB-2 **Outlet Sizing**

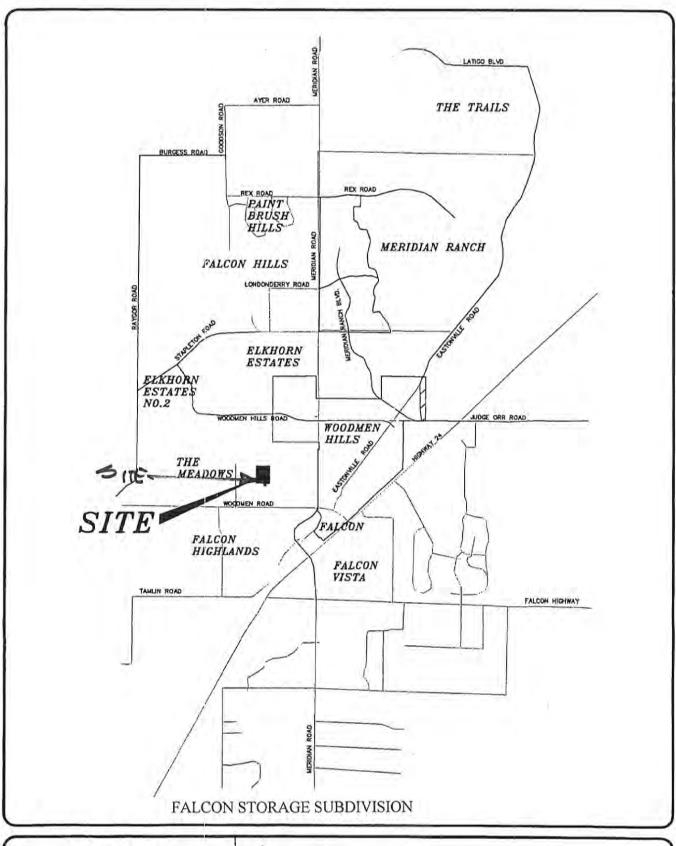
Application Techniques and Maintenance Requirements



D= 1.486 AR 351/2 Q= 125 CF9 5= 1/5372= 0.0186 A = 16 d WP=16.03 dx2 4 9 0 40 upper N=0.035 5.70 Half 3.61 0.50 0.30 12.00 2565 0499 26.6 16.0312 0.499 1,65 0.50 8.00 4.30 9.618 17.5 0.30 12.2 6.4125 0.20 3,20 6.733 3.36 15.0 14.37 B. 036 0.25 4.00 A= 6d ADWEV. wp = 2100 Halt 5=1/92=0.0103 B-B 7.60 0.9487 1.30 1.897 0.3 30TZ 12,84 3.162 3.00 0.5 8.99 0.9487 0.35 22136 2.10 0.9487 10.27 0.40 2529 2.40 0.9487 12.58 049 3.000 2.94

IAMETER	AREA	D 8/3		K		D. 6 657
-IN	-FT2-	-FT-	N=0.010	N=0.013	N=0.024	N=0.026
2.11						
2	0.02182	0.008413	0.3895			444
4	0.08727	0.053420	2.4733	H H H	224	
6	0.19630	0.157500	7.2922	5.609		375
1 8	0.34910	0.339200	15.7050	12.081		
10	0.54540	0.615000	28.4745	21.903	377	
12	0.78540	1.000000	46.3000	35.615		
15	1.22720	1.813100	83.9465	64.574		
18	1.76710	2.948300	136.5100	105.000	56.88	52.5
$\frac{10}{21}$	2.40530	4.447400	205.9100	158.400	85.80	79.2
24	3.14160	6.349600	293.9900	226.140	122.49	113.0
27	3.97610	8.692700	402.4700	309.590	167.70	154.7
30	4.90870	11.512600	533.0300	410.030	222.10	205.0
33	5.93960	14.844100		528.680		
36	7.06860	18.720800	866.7700	666.700	361.20	333.3
39	8.29580	23.175100	3	825.400		
42	9.62110	28.238900	7,1,1	1005.000	544.80	502.5
48	12.56640	40.317500		1436.000	777.80	718.0
54	15.90430	55.195000	1444	1966.000	1065.00	983.0
60	19.63500	73.100400	F)+(+	2604.000	1410.00	1302.0
66	23.75830	94.254200		3357.000	1818.00	1678.0
72	28.27430	118.869400		4234.000	2293.00	2117.0
78	33.18310	147.152900	F 4 F	5241.000	2839.00	2620.0
84	38.48450	179.306000	- + + +	6386.000	3459.00	3193.0
90	44.17860	215.524500		7676.000	4158.00	3838.
96	50.26550	256,000000	- + + +	9118.000	4939.00	4559.
108	63.61730	350,466600	PERMIT	12480.000	6761.00	6140.
120	78.53980	464.158900		16530.000	8954.00	8265.
120	10,000					

Oliver E. Watts Consulting Engine Colorado Springs



VICINITY MAP

LATIGO

(719) 380-1090

Colorado Design Concepts
3578 Hartsel Drive E323
Colorado Springs, CO 80920

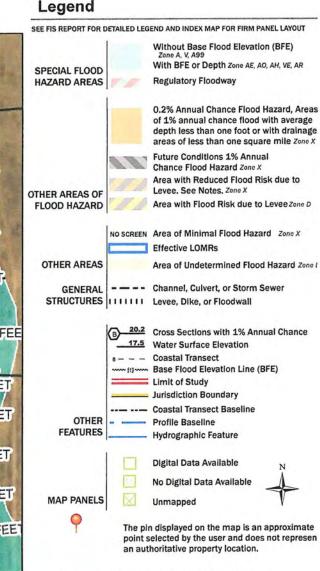
FIGURE:1

PROJECT NO. 200401

National Flood Hazard Layer FIRMette



Legend



This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The basemap shown complies with FEMA's basemap accuracy standards

The flood hazard information is derived directly from the authoritative NFHL web services provided by FEMA. This map was exported on 3/25/2021 at 9:47 AM and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or become superseded by new data over time.

This map image is void if the one or more of the following map elements do not appear: basemap imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for unmapped and unmodernized areas cannot be used for regulatory purposes.



NOTES TO USERS

s map is for use in administering the National Flood Insurance Pr necessarily identify all areas subject to flooding, particularly from trees of small size. The community map repository should be ssible updated or additional flood hazard information.

obtain more detailed information in areas where Base Flood Elevations (BFEs) clidor floodways have been determined, users are encouraged to consult the Flood offiles and Floodway Data and/or Summary of Stilwater Elevations tables contained thin the Flood Insurance Study (FIS) report that eccompanies this FIRM. Users ould be aware that BFEs shown on the FIRM represent rounded whole-foot availors. These BFEs are intended for flood insurance rating purposes only and ould not be used as the sole source of flood elevation information. Accordingly, od elevation data presented in the FIS report should be utilized in conjunction with

Coastal Base Flood Elevations shown on this map apply only landward of 0.0 onth American Vertical Datum of 1998 (NAVD88). Users of this FIRM should be ware that coastal flood elevations are also provided in the Summary of Sithwater clevations table in the Flood Insurance Study report for this jurisdiction. Elevationshown in the Summary of Sithwater Elevations table should be used for construction and/or flood/plain management purposes when they are higher than the elevations thow on this Elina Study in the study of the

Boundaries of the floodways were computed at cross sections and interpolated between cross sections. The floodways were based on hydrautic considerations with separt to requirements of the National Flood Insurance Program, Floodway shall have deep pertinent floodway data are provided in the Flood Insurance Study report on this interdiction.

The projection used in the preparation of this map was Universal Transverse Mercator (UTM) zone 13. The horizontal datum was NADB3, GRS80 spheroid, Differences in datum, spheroid, projection or UTM zones zones used in production of PTRMs for adjacent jurisdictions may result in slight positional different the productions of the TRMS of adjacent jurisdictions may result in slight positional different the provision of this EDIOse purisdiction for the transport of the EDIOse purisdiction for th

Flood elevations on this map are referenced to the North American Vartical Datum of 1988 (NAVD88). These flood elevations must be compared to structure and orgound elevations referenced to the same vartical datum. For information regarding conversion between the National Geodetic Vertical Datum of 1928 and the North American Vertical Datum of 1988, visit the National Geodetic Survey website at http://www.ngs.noaa.gov/ or contact the National Geodetic Survey at the following address:

NGS Information Services NOAA, N/NGS12 National Geodetic Survey SSMC-3, #9202 315 East-West Highway lilver Spring, MD 20910-3282

se Map information shown on this FIRM was provided in digital format by EJ Pas unty, Colorado Springs Utilities, City of Fountain, Bureau of Land Management blonal Oceanic and Atmospheric Administration, United States Geological Survey of Anderson Consulting Engineers, Inc. These data are current as of 2006.

map reflects more detailed and up-to-date stream channel configurations and obtained affineations than those shown on the previous FIRM for this jurisdiction floodplains and floodpains and there transferred from the previous FIRM map been adjusted to conform to these new stream channel configurations. As if, the Flood Profises and Floodway Data tables in the Flood Insurance Student (which contains authoritative hydraulic data) may reflect stream channences that differ from what is shown on this map. The profile beselines depicted his map represent the hydraulic modeling baseliness that match the flood profile Floodway Data Tables if applicable, in the FIS report. As a result, the profile may devide significantly from the new base map channel representation may pepare outside of the floodplain.

rporate limits shown on this man are based on the best data available at the por au minus shown or this map are based on the best data available at the bri ublication. Because changes due to annexations or de-annexations may have urred after this map was published, map users should contact appropriat munity officials to verify current corporate limit locations.

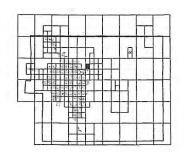
lease refer to the separately printed Map Index for an overview map of the county rowing the layout of map panels; community map repository addresses; and a string of Communities table containing National Flood Insurance Program dates for ach community as well as a listing of the panels on which each community is

Contact FEMA Map Service Center (MSC) via the FEMA Map Information exchange (FMIX) 1-077-336-2627 for information on available products associated with this FIRIM. Available products may include previously issued Letters of Map Change, a drop of the map. The MSC may be reached by Fax at 1-800-358-8520 and its website at http://www.msc.fema.gov/.

you have questions about this map or questions concerning the National Floo surance Program in general, please call 1-877-FEMA MAP (1-877-336-2627) o sit the FEMA website at http://www.fema.gov/business/nfip.

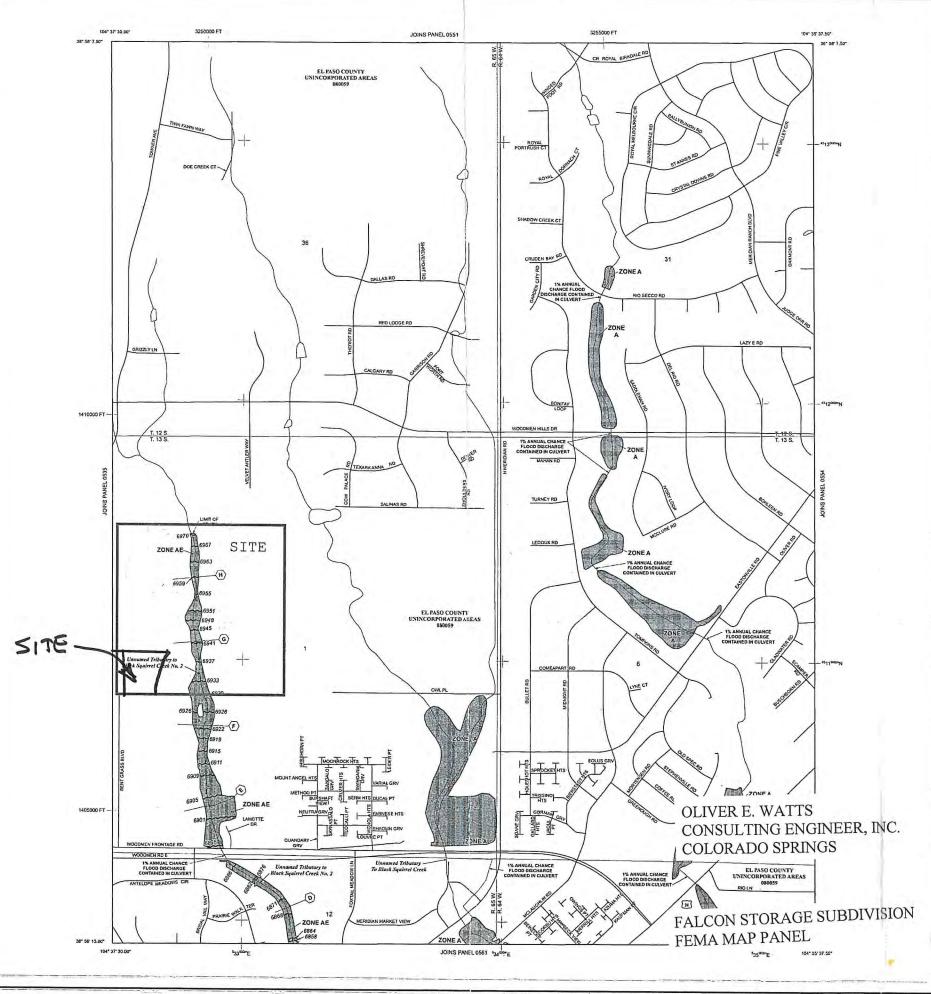
Flooding Source Vertical Datum
Offset (f)
REFER TO SECTION 3.3 OF THE EL PASO COUNTY FLOOD INSURANCE STUD
FOR STREAM BY STREAM VERTICAL DATUM CONVERSION INFORMATION

Panel Location Map



This Digital Flood Insurance Rate Map (DFIRM) was produced through a Cooperating Technical Partner (CTP) agreement between the State of Colorado Water Conservation Board (CWCB) and the Federal Emergency Management Agency





LEGEND

SPECIAL FLOOD HAZARD AREAS (SFHAS) SUBJECT TO INUNDATION BY THE 1% ANNUAL CHANCE FLOOD

The 1% annual chance flood (100-year flood), size known as the base flood, is the flood that has a 1% chance of being equated or excreted in any given yeat. The Special Flood hazard Aris is the ends subject to flooding by the 1% annual chance flood. Areas of Sector 1840 of the 1840

ZONE A No Base Flood Elevations determined.

ZONE AE Base Flood Elevations determined.

ZONE AF Flood deprise of 1 to 3 feet (usually areas of ponding); Base Flood Elevations determined.

Flood depths of 1 to 3 feet (usually sheet flow on sloping terrain); everage depths determined. For areas of altuvial fan flooding, veloctoes also determined.

Special Rood Nazard Area Formerly protected from the 1% ennual chance flood by a flood control system that was subsequently eccentried. Zone AR, indicates that the former flood control system is being restored to provide protection from the 1% annual chance or greater flood. ZONE AR

ZDNE VE Coastal floor zone with velocity hazard (wave action); base Flood Elevations determined.

The floodway is the channel of a stream plus any adjacent floodplain areas that must be kept free of encoachment so that the 1% annual chance flood can be carried without substantial increases in flood heights.

OTHER FLOOD AREAS

Areas of 0.2% annual chance flood; areas of 1% annual chance flood with average depths of less than 1 fool or with drainage areas less than 1 square mile; and areas protected by levees from 1% annual chance flood.

OTHER AREAS

ZONE D Areas in which flood hazards are undetermined, but possible. COASTAL BARRIER RESOURCES SYSTEM (CBRS) AREAS

OTHERWISE PROTECTED AREAS (OPAS)

Zone D Boundary

productive and

Base Flood Elevation value where uniform within zone; elevation in feet*

(A)—(A)

--23

(EL 987)

97° 07' 30' 00" 32° 22' 30' 00"

Bench mark (see explanation in Notes to Users section of this FIRM navel) DX5510_X

To determine if flood insurance is available in this community, contact your insurance agent or call the National Flood Insurance Program at 1-800-638-6620.



PANEL 0553G

FIRM

FLOOD INSURANCE RATE MAP EL PASO COUNTY, COLORADO

PANEL 553 OF 1300

(SEE MAP INDEX FOR FIRM PANEL LAYOUT)

AND INCORPORATED AREAS

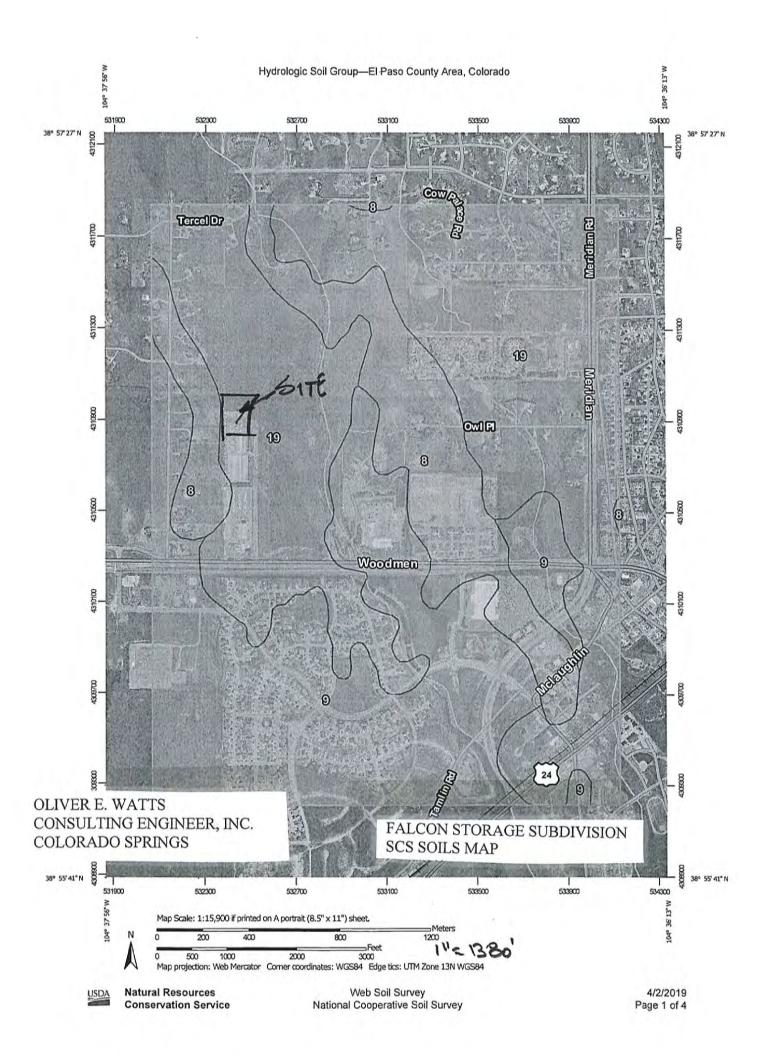
CONTAINS:



MAP NUMBER 08041C0553G

MAP REVISED DECEMBER 7, 2018

Federal Emergency Management Agency



EL PASO COUNTY AREA, COLORADO

TABLE 16. -- SOIL AND WATER FEATURES

Absence of an entry indicates the feature is not a concern. See "flooding" in Glass y for definition of terms as "rare," "brief," and "very brief." The symbol > means greater than

Cost Handalan	under		Flooding		Bed	irock	Potential
Soil name and map symbol	Hydro- logic group	Frequency	Duration	Months	Depth	Hardness	frost
.,					In		
lamosa:	c	Frequent	Brief	May-Jun	>60	777	High.
\scalon: 2, 3	В	None	777		>60		Moderate;
3adland: 4	D			444		(855)	
3ijou: 5, 6, 7	В	None	-	222	>60		Low.
Blakeland: B	A	None	Φ.		>60		Low.
19: Blakeland part-	A	None		444	>60	15-55-	Law.
Fluvaquentic Haplaquolls part	D	Common	Very brief	Mar-Aug	>60	5	High.
Blendon: 10	В	None		Ann	>60		 Moderate,
Bresser: 11, 12, 13	В	None		4-4	>60		Low.
Brussett: 14, 15	В	None			>60		Moderate.
Chaseville: 16, 17	A	None		944	>60		Low.
118: Chaseville part	A	None			>60		Low.
Midway part	D	None			10-20	Rippable	Moderate.
Columbine: 19		None to rare		1	>60		Low.
Connerton: 120: Connerton part-	В	None			>60		High.
Rock outcrop	D					220	2.2
Cruckton: 21	В	None			>60	202	Moderate.
Cushman: 22, 23	c	None			20-40	Rippable	Moderate.
124: Cushman part	С	None	()	222	20-40	Rippable	Moderate.
Kutch part	С	None		ISK4	20-40	Rippable	Moderate.
Elbeth: 25, 26	В	None			>60		Moderate.
127: Elbeth part	В	None	1		>60		Moderate.

See footnote at end of table,

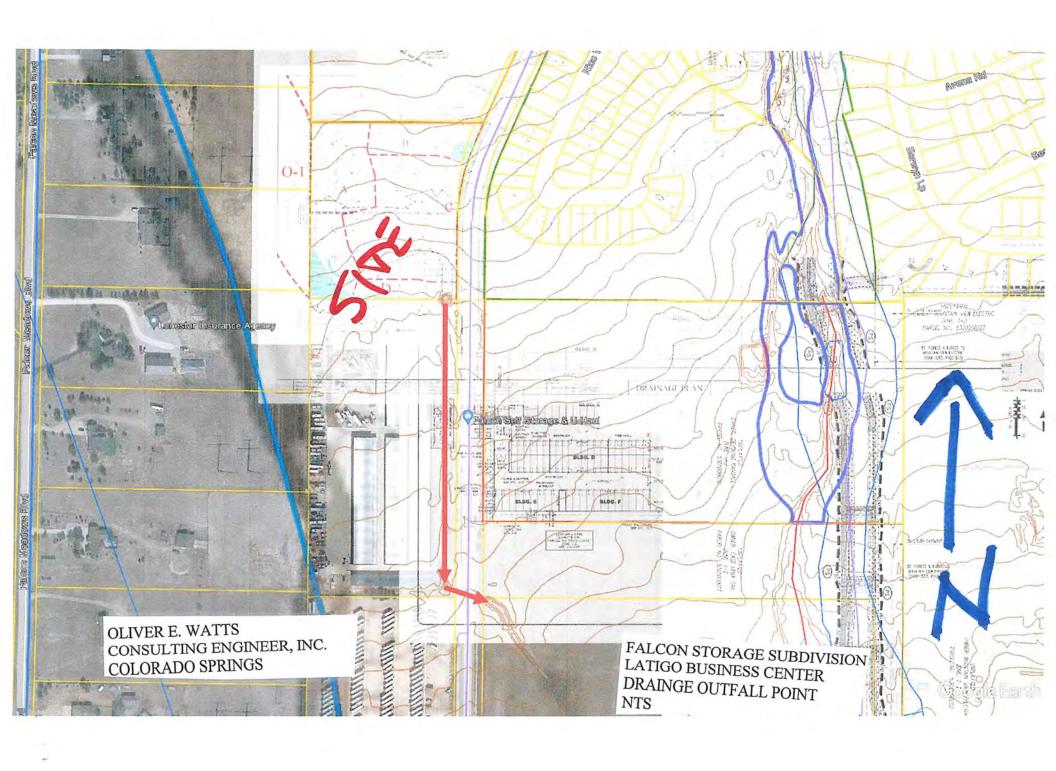


Table 6-6. Runoff Coefficients for Rational Method

(Source: UDFCD 2001)

Land Use or Surface	Percent	nt Runoff Coefficients											
Characteristics	Impervious	2-year		51	5-year		10-year		25-year		50-year		year
		HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG CAD	HSG A&B	HSG CAL
Business	7-9-	2.0					15.5	1 1 1		THEFT	1150 Cal	HJG AGO	noo cat
Commercial Areas	95	0.79	0.80	0.81	0.82	0.83	0.84	0.85	0.87	0.87	0.88	0.88	0.89
Neighborhood Areas	70	0,45	0.49	0.49	0.53	0.53	0.57	0.58	0.62	0.60	0.65	0.62	0.68
Residential		-										_	
1/8 Acre or less	65	0.41	0.45	C.45	0.49	0.49	0.54	0.54	0.59	257	2.00		
1/4 Acre	40	0.23	0.28	0.30	0.35	0.36	0.42	0.42		0.57	0.62	0.59	0.65
1/3 Acre	30	0.18	0.22	0.25	0.30	0.32	0.38	0.42	0.50	0.46	0.54	0.50	0.58
1/2 Acre	25	0.15	0.20	0.22	0.28	0.30	0,36	0.39	0.47	0.43	0.52	0.47	0.57
1 Acre	20	0.12	0.17	0.20	0.26	0.27	0.34	0,37	0.46	0.41	0.51	0.46	0.56
Industrial	= 9.5	1000			-								
Light Areas	80	0.57	0.50	0.59	0.63	0.63	0.66	0.66	0.70	0.68	0.72	0.70	
Heavy Areas	90	0.71	0.73	0.73	0.75	0.75	0.77	0.78	0.80	0,80	0.72	0.70	0.74
Parks and Cemeteries	7	0.05	0.09	0.12	0.19	0.20	0.29	0.30	0.40	0.34	0.46	0.39	0.52
Playgrounds	13	0.07	0.13	0.16	0.23	0.24	0.31	0.32	0.42	0.37	0.48	0.41	0.54
Railroad Yard Areas	40	0.23	0.28	0.30	0.35	0.36	0.42	0.42	0.50	0.46	0.54	0.50	0,54
Undeveloped Areas										Taranta (
Historic Flow Analysis Greenbelts, Agriculture	2	0.03	0.05	0.09	0.16	0.17	0.26	0.26	.0.38	0.31	0.45	0.36	0.51
Pasture/Meadow	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50
Forest	0	0.02	0.04	0.06	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50
Exposed Rock	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Offsite Flow Analysis (when landuse is undefined)	45	0.26	0.31	0.32	0.37	0.38	0.44	0,44	0.51	0.48	0.55	0.51	0.59
Streets		-											
Paved	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Gravel	80	0,57	0.60	0.59	0.63	0.63	0.66	0.66	0.70	0.68	0.72	0.70	0.74
Drive and Walks	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.95
Roofs	90	0.71	0.73	0.73	0.75	0.75	0.77	0.78	0.80	0.80	0.82	0.81	0.98
Lawns	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50

3.2 Time of Concentration

One of the basic assumptions underlying the Rational Method is that runoff is a function of the average rainfall rate during the time required for water to flow from the hydraulically most remote part of the drainage area under consideration to the design point. However, in practice, the time of concentration can be an empirical value that results in reasonable and acceptable peak flow calculations.

For urban areas, the time of concentration (t_c) consists of an initial time or overland flow time (t_i) plus the travel time (t_i) in the storm sewer, paved gutter, roadside drainage ditch, or drainage channel. For non-urban areas, the time of concentration consists of an overland flow time (t_i) plus the time of travel in a concentrated form, such as a swale or drainageway. The travel portion (t_i) of the time of concentration can be estimated from the hydraulic properties of the storm sewer, gutter, swale, ditch, or drainageway. Initial time, on the other hand, will vary with surface slope, depression storage, surface cover, antecedent rainfall, and infiltration capacity of the soil, as well as distance of surface flow. The time of concentration is represented by Equation 6-7 for both urban and non-urban areas.

$$t_c = t_i + t_t \tag{Eq. 6-7}$$

Where:

 $t_c = \text{time of concentration (min)}$

 t_i = overland (initial) flow time (min)

 t_l = travel time in the ditch, channel, gutter, storm sewer, etc. (min)

3.2.1 Overland (Initial) Flow Time

The overland flow time, t_i , may be calculated using Equation 6-8.

$$t_i = \frac{0.395(1.1 - C_5)\sqrt{L}}{S^{0.33}}$$
 (Eq. 6-8)

Where:

 t_i = overland (initial) flow time (min)

 C_5 = runoff coefficient for 5-year frequency (see Table 6-6)

 $L = \text{length of overland flow (300 ft } \underline{\text{maximum}} \text{ for non-urban land uses, 100 ft } \underline{\text{maximum}} \text{ for urban land uses)}$

S = average basin slope (ft/ft)

Note that in some urban watersheds, the overland flow time may be very small because flows quickly concentrate and channelize.

3.2.2 Travel Time

For catchments with overland and channelized flow, the time of concentration needs to be considered in combination with the travel time, t_i , which is calculated using the hydraulic properties of the swale, ditch, or channel. For preliminary work, the overland travel time, t_i , can be estimated with the help of Figure 6-25 or Equation 6-9 (Guo 1999).

$$V = C_{\nu} S_{\nu}^{0.5}$$
 (Eq. 6-9)

Where:

V = velocity (ft/s)

 C_{ν} = conveyance coefficient (from Table 6-7)

 S_w = watercourse slope (ft/ft)

Type of Land Surface C_{ν} Heavy meadow2.5Tillage/field5Riprap (not buried)*6.5Short pasture and lawns7

10

15

20

Table 6-7. Conveyance Coefficient, C_{ν}

The travel time is calculated by dividing the flow distance (in feet) by the velocity calculated using Equation 6-9 and converting units to minutes.

Paved areas and shallow paved swales

The time of concentration (t_c) is then the sum of the overland flow time (t_i) and the travel time (t_i) per Equation 6-7.

3.2.3 First Design Point Time of Concentration in Urban Catchments

Nearly bare ground

Grassed waterway

Using this procedure, the time of concentration at the first design point (typically the first inlet in the system) in an urbanized catchment should not exceed the time of concentration calculated using Equation 6-10. The first design point is defined as the point where runoff first enters the storm sewer system.

$$t_c = \frac{L}{180} + 10 \tag{Eq. 6-10}$$

Where:

 t_c = maximum time of concentration at the first design point in an urban watershed (min)

L =waterway length (ft)

Equation 6-10 was developed using the rainfall-runoff data collected in the Denver region and, in essence, represents regional "calibration" of the Rational Method. Normally, Equation 6-10 will result in a lesser time of concentration at the first design point and will govern in an urbanized watershed. For subsequent design points, the time of concentration is calculated by accumulating the travel times in downstream drainageway reaches.

3.2.4 Minimum Time of Concentration

If the calculations result in a t_c of less than 10 minutes for undeveloped conditions, it is recommended that a minimum value of 10 minutes be used. The minimum t_c for urbanized areas is 5 minutes.

3.2.5 Post-Development Time of Concentration

As Equation 6-8 indicates, the time of concentration is a function of the 5-year runoff coefficient for a drainage basin. Typically, higher levels of imperviousness (higher 5-year runoff coefficients) correspond to shorter times of concentration, and lower levels of imperviousness correspond to longer times of

For buried riprap, select C_v value based on type of vegetative cover.

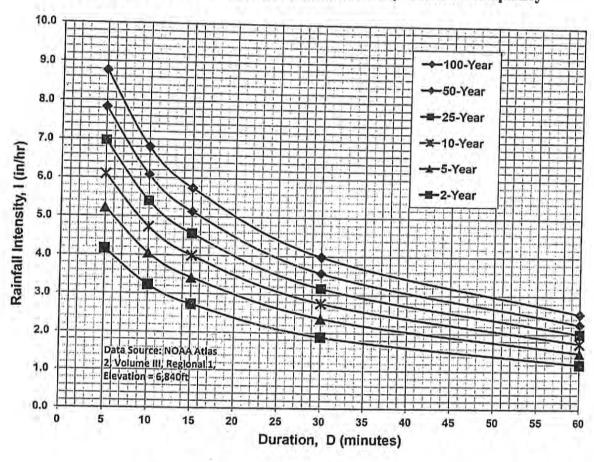


Figure 6-5. Colorado Springs Rainfall Intensity Duration Frequency

IDF Equations

$$I_{100} = -2.52 \ln(D) + 12.735$$

$$I_{50} = -2.25 \ln(D) + 11.375$$

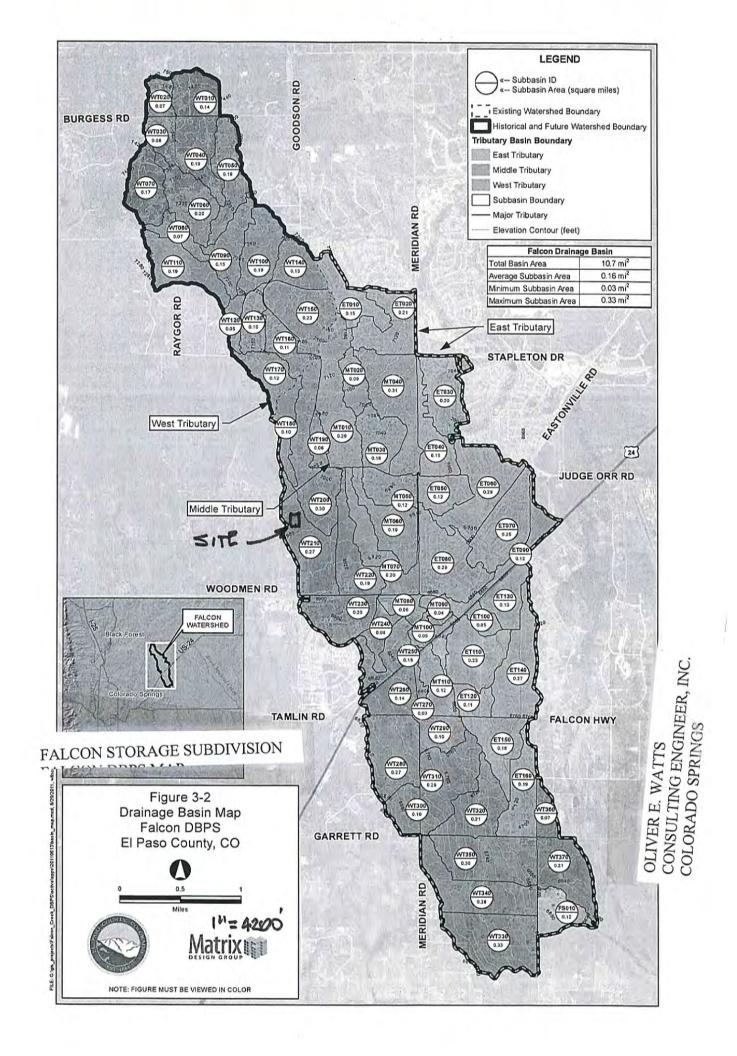
$$I_{25} = -2.00 \ln(D) + 10.111$$

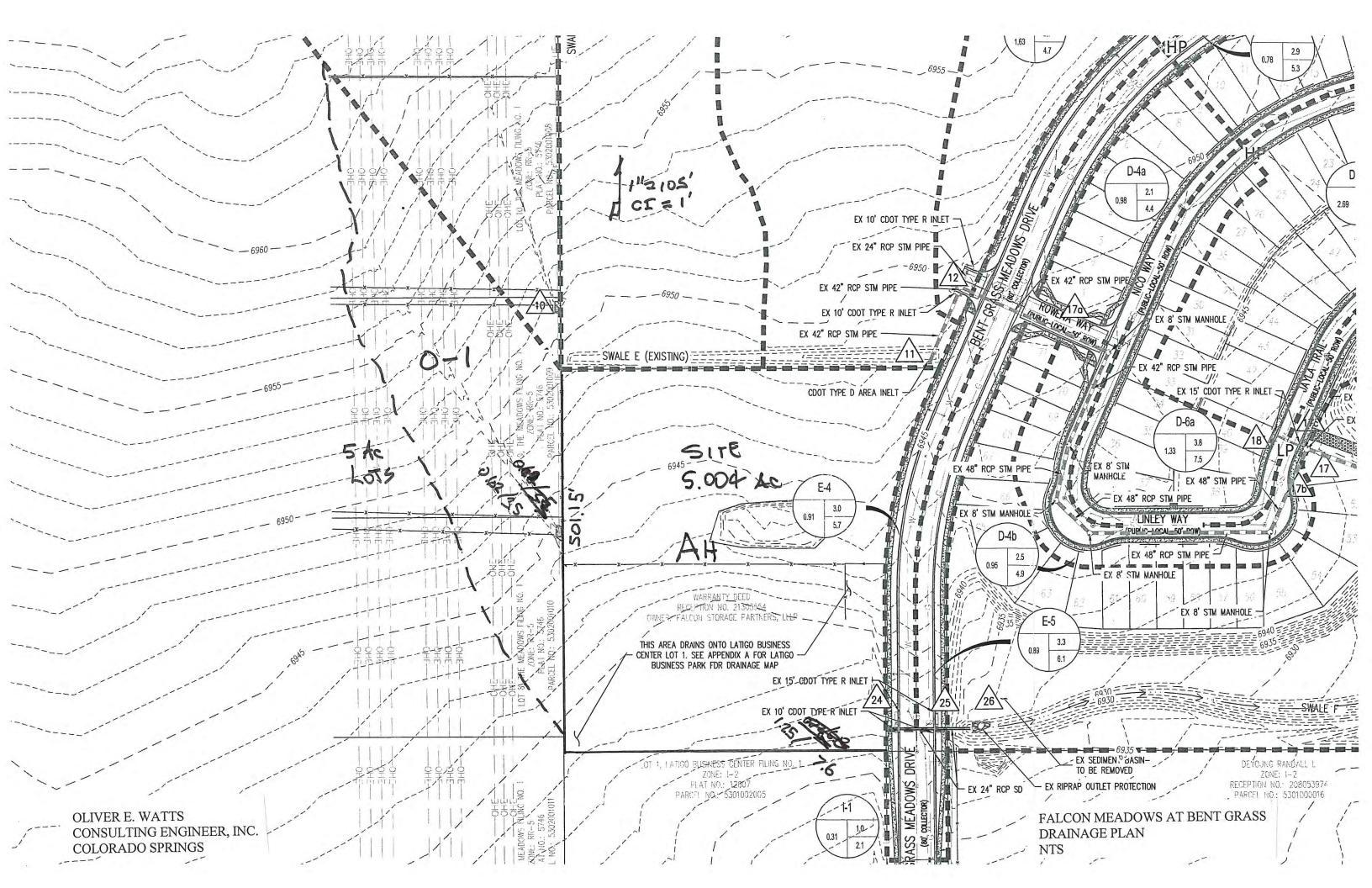
$$I_{10} = -1.75 \ln(D) + 8.847$$

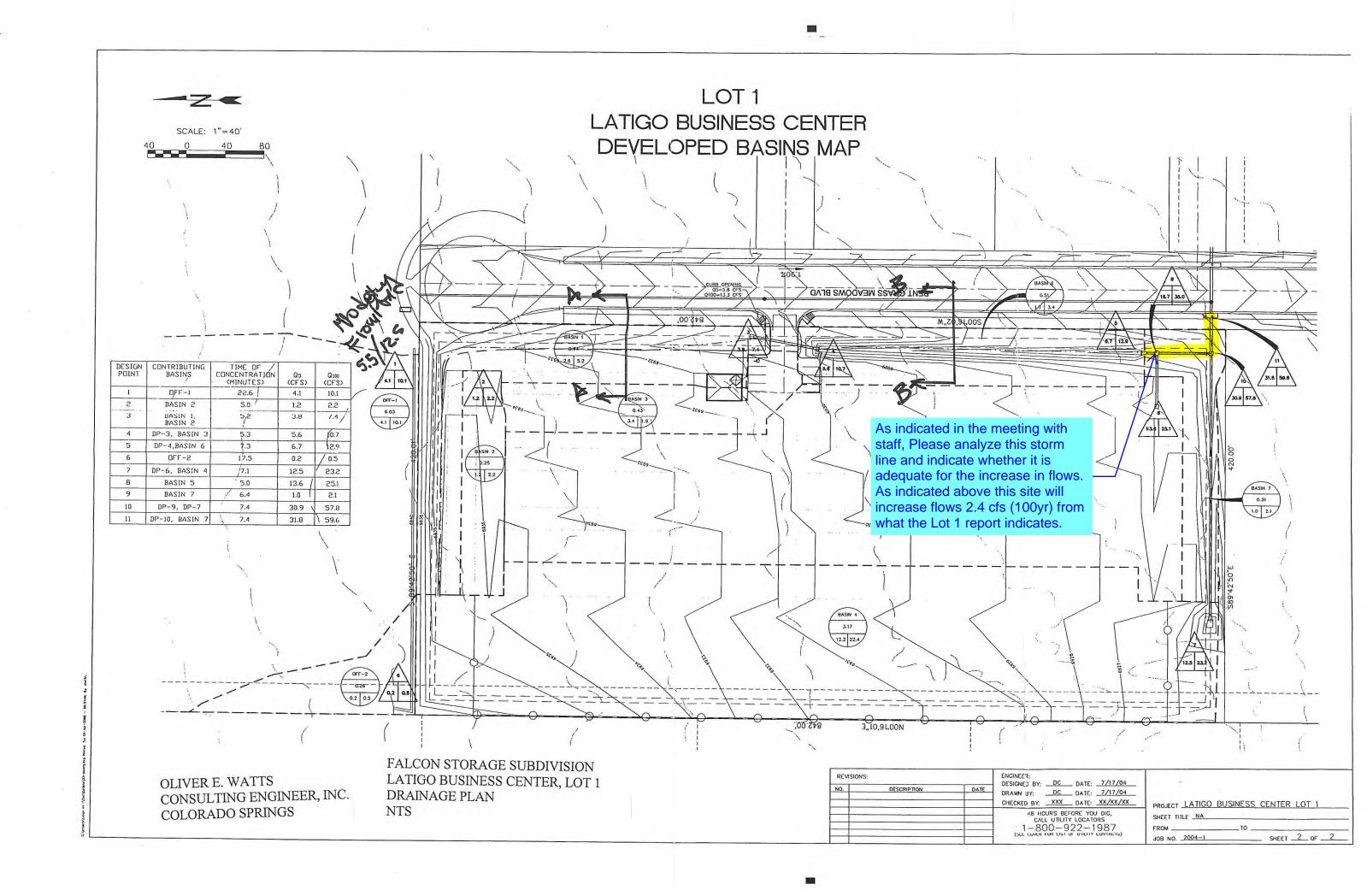
$$I_5 = -1.50 \ln(D) + 7.583$$

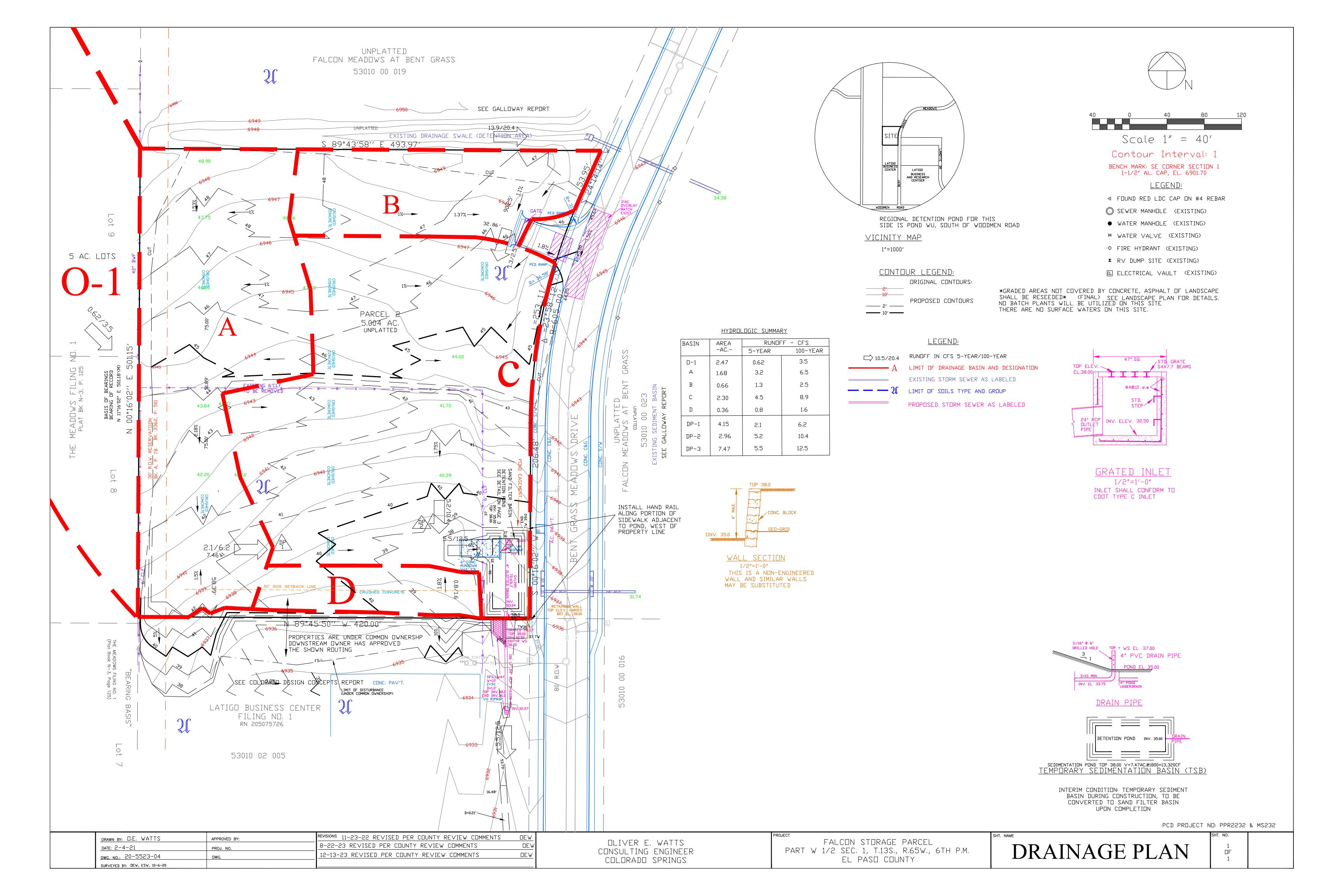
$$I_2 = -1.19 \ln(D) + 6.035$$

Note: Values calculated by equations may not precisely duplicate values read from figure.









please remove the previous submittal report from this set.

PRELIMINARY AND FINAL DRAINAGE PLAN AND REPORT

FALCON STORAGE SUBDIVISION

PART OF THE SW1/4 SECTION 1, T.13S. R.65W. OF THE 6^{TH} P.M. EL PASO COUNTY

February 4, 2021

Revised November 23, 2022

Revised June 7.2023

Revised June 22, 2023

Revised August 31, 2023

PCD File No. PPR2232 PCD File No. MS232

Prepared for

Falcon Storage Partners LLLP 4615 Northpark Drive Colorado Springs, CO 80918

Oliver E. Watts, Consulting Engineer, Inc. Colorado Springs, Colorado

OLIVER E. WATTS, PE-LS

OLIVER E. WATTS, CONSULTING ENGINEER, INC.
CIVIL ENGINEERING AND SURVEYING
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COLORADO SPRINGS, COLORADO 80907
(719) 593-0173
fax (719) 265-9660
olliewatts@aol.com
Celebrating over 43 years in business

August 31, 2023

El Paso County Planning and Community Development 2880 International Circle Colorado Springs, CO 80910

ATTN: Joshua Palmer, P.E.

SUBJECT: Preliminary and Final Drainage Plan and Report Falcon Storage Subdivision

Transmitted herewith for your review and approval is the drainage plan and report for The Falcon Storage Subdivision in El Paso County. This report will accompany the development plan and subdivision plat submittal. This report has been revised in accordance with your review comments of November 23, 2022, March 2, 2023, and August 18, 2023.

Please contact me if I may provide any further information.

Oliver E. Watts, Consulting Engineer, Inc.

BY:	
Oliver E. Watts, President	

FALCON STORAGE SUBDIVISION DRAINAGE REPORT TABLE OF CONTENTS

Drainage Report 5 pages
Computations, 7 pages
Vicinity Map
FEMA Panel No. 08041C0553 G
SCS Soils Map and Interpretation Sheet
Backup Information, 4 sheets
Drainage Flow Path Map
Falcon DBPS Map
Drainage Plan, Falcon Meadows at Bent Grass
Drainage Plan, Latigo Business Center
Drainage Plan, Dwg 02-5523-04

FALCON STORAGE SUBDIVISION DRAINAGE REPORT REFERENCES

City-County Drainage Criteria, current edition
Fema Firm Insurance Rate Map
El Paso County Soils Survey, SCS
Falcon Drainage Basin Planning Study
Drainage Report, Falcon Meadows at Bent Grass
Drainage Report, Latigo Business Center, Lot 1

1. ENGINEER'S STATEMENT:

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the County for drainage reports and said report is in conformity with the applicable master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.

Oliver E. Watts, Consulting Engineer, Inc.					
Oliver E. Watts	Colo. PE-LS No. 9853	date			
2. OWNERS / DE	EVELOPER'S STATEMENT:				
I the owner / devel drainage report and		with all of the requirements specified in this			
Falcon Storage Par	tners LLLP				
By:					
Richard Graham 4615 Northpark Di	rive	Date			
Colorado Springs,					
3. EL PASO COU	UNTY:				
		Paso Land Development Code, Drainage ing Criteria Manual, as amended.			
Joshua Palmer, P.E	E.,	date			
· ·	ECM Administrator				
Conditions:					

4. LOCATION AND DESCRIPTION:

The Falcon Storage Subdivision is located in the Latigo Business Center development of El Paso County as shown on the enclosed vicinity map. Occupying a portion of the West half of Section 1, Township 13 South, Range 65 West of the 6th P.M., totaling 5.004 acres. It is located in the Falcon Drainage Basin as shown on the enclosed basin map. It lies west of Bent Grass Meadows Drive north of the Latigo Business Center Filing No. 1 as shown on the enclosed drainage plan. The site will be developed into an RV Storage site as shown on the enclosed drainage plan, as an expansion to the one in the Latigo Business Center Filing No. 1, both owned by the developer.

5. FLOOD PLAIN STATEMENT:

This subdivision is not within the limits of a flood plain or flood hazard area, according to FEMA map panel number 08041C0553 G, dated December 7, 2018, a copy of which is enclosed for reference.

6. METHOD AND CRITERIA:

The method used for all computations is that specified in the City-County Drainage Criteria Manual, using the rational method for areas of the size of the development. All computations are enclosed for reference and review. Pertinent portions of the criteria are enclosed.

The soils in the subdivision have been mapped by the local USDA/SCS office, and a soils map and interpretation sheet are enclosed for reference. All soils in this area are of hydrologic group "A" within the development area.

7. DESCRIPTION OF RUNOFF:

A. Drainage Inflows: The drainage Report for Falcon Meadows at Bent Grass indicates an existing drainage swale above the north boundary to divert runoff from this site and route it to Bent Grass Meadows and then past this development in Bent Grass Meadows Drive to outfall points to an existing detention pond across the street. A copy of this drainage plan is enclosed. Also shown on this map is that portion of the Meadows Filing No. 1 that drains 0.62 cfs / 3.5 cfs (5-year / 100-year runoffs) into this subdivision along the westerly boundary (Basin O-1), and it indicates the historic undeveloped runoff of the site, Basin A (historic) totaling 1.25 cfs / 7.6 cfs at the lowest (southeast) portion of the subdivision.

B. Interior Routing: The area will be graded to conform to the existing topography shown on the drainage plan. The property has been rough graded, which complies with the historic runoff pattern. Additional grading is indicated which is intended to contain the runoff into the interior drive isle street network, and along the streets to the detention pond The westerly street (Basin A) will combine with offset basin O-1 to develop 3.0 cfs \ 6.2 cfs (5-ye 100-year runoffs) near the in the southwest corner of the plat (Design Point 1). Basin B will develope 1.2.2.5 cfs in the southerly driveway adjacent to the north entrance. It will combine with basin C along the same routing for 5.2/10.4 cfs at the southwest intersection (design point 2). This will combine basin D to outfall into the detention pond (design point 3). The total outfall at this point 5.5 cfs/12.5 cfs, into the sand filter basin.

to all PBMPs and then update all submitted text and drawings accordingly with consistent labeling throughout (example: "Pond A" or "Pond 1"). Unresolved

C. Detention Storage: At the proposed outfall point a sand filter detention pond is proposed, as required by the County. The pond is sized for a temporary sedimentation basin to be used during the construction period and converted into a permanent sand filter basin upon completion. The sedimentation basin will contain 13000 +CF (at 1800 CF per acre). An 8-inch riser pipe is used as an outlet, with holes drilled as computed to detain the runoff as required. One foot of freeboard is provided with a spillway that will pass the 100-year runoff. Details are shown on the enclosed drainage plan. Following construction the basin will be converted to a sand filter basin. A 4-inch slotted underdrain will be placed in a 5-inch section of CDOT class C Filter material and drain into the grated inlet outlet structure set at the WQCV level, and sized for the 100-year runoff. An orifice plate will be provided on the end of the underdrain with an orifice

discuss flow path to existing detention facility and provide calcs for capacities and velocities to meet criteria for conveyance system

this was not included Falcon Storage Subdivision Preliminary and Final Drainage Plan and Report

sized for the installation. A detention basin stage-storage table County, the basin is used for water quality storage only and the improvements/upgrades needed to the Center Filing No. 1 to an existing full spectrum pond to the sou pond. If the existing pond did not account between Tamlin and Meridian Roads, in accordance with the a for developed flows from this site provide

please analyze and state whether the existing pond accounted for this sites developed flows. Address any by the detention onsite or identify the necessary D. Outfall Point: Discharge from the subdivision will be int upgrades needed for the existing pond and

Latigo Business Center, filing no. 1, as shown on the drainage provide CD's of work to be done by this along the north boundary of Lot 1 as shown on the drainage pladevelopmentitive installation. The two properties are under common ownership and permission to outfall into the Latigo Business Center is granted. The drainage plan for the Latigo Business Center is enclosed. This report indicated two existing discharges: 0.2 cfs / 0.5 cfs near the southwest corner and 4.1 cfs / 10.1 cfs over the remaining south frontage. A 24 inch CMP will run from the CDOT Type C outlet box at a minimum slope of one percent into the existing ditch shown on the drainage plan-

WATER QUALITY

A sand filter basin water quality facility will be provided as described above.

FOUR STEP PROCESS

The following process has been followed to minimize adverse impacts of urbanization

Runoff Reduction: The scope of the development has been minimized consistent with zoni requirements to present the minimum footprint in providing a RV Storage development. The portions are to be landscaped to reduce the impervious percent.

ater Quality

<u>Provide WQCV:</u> <u>Detention</u> water quality storage is being provided for this subdivision by a detention pond and runoff will be routed to a full spectrum pond located downstream, south of Road, north of Highway 24, between Tamlin and Meridian Roads, by others as a sub regional

Stabilize Drainage Ways: The site will be graded to route the runoff over improved street installations to provide channel stabilization in the natural erosive material over the site. Discharge from the site will be into adjacent and downstream facilities in accordance with the master drainage basin plan for the Falcon drainage basin and previously approved subdivision drainage reports. Copies of each plan are enclosed. There will be no adverse affect on downstream developments as a result of this subdivision

Consider need for Industrial and Commercial BMP's: This is a RV Storage site, so source control problems will be a minimum. During construction, standard site specific state of the art BMP's will be employed to minimize and mitigate erosive problems.

> provide analysis of the ditch and downstream facilities and show that it is adequate to convey the flows down stream.

8. COST ESTIMATE:

0, 0001 2012/2112				
<u>Item No.</u>	Description	Quantity	<u>Unit Cost</u>	Cost
1	Pond/BMP Earthwork	881 CY	\$ 23.00	\$ 20263.00
2	Slotted drain	187 LF	40.00	7480.00
3	Riprap	14 Tons	80.00	1096.00
4	Grated Inlet	1 ea	5611.00	5611.00
4	12" PVC drain	106 LF	112.00	11872.00

Please identify how the flow is conveyed to the full spectrum pond to the south of Woodmen from Lot 1. Will it enter an existing storm system? is the system adequate for this sites developed flows? Please address. The sites developed flows must be conveyed to a

5	Concrete Pond Inlet	15 CY	589.00	10335.00
	Subtotal Construction Cost			\$ 56657.00
	Engineering	10%		5665.71
	Total Estimated Cost			\$ 62322.70



Please revise to 2023

9. FEES: At plat recording.

2024 Falcon Basin Fees: 5.004 acres @62.3% Impervious = 3.1175 Impervious acres

Drainage fees @ \$ 37,256 per acre = \$ 116,145.28 Bridge fees @ \$ 5,118 per acre = \$ 15,955.32

Total Fees: \$ 132,100.61

10. SUMMARY

The Falcon Storage Subdivision is a proposed 1-lot, RV Storage subdivision containing 5.004 acres. The proposed street facilities will adequately convey, detain and outfall runoff from the site to existing sufficient adjacent and downstream facilities, as described in the respective drainage reports. Water Quality is being utilized in lieu of a full specifium detention pond due to the existing regional facility as described earlier in this report. Flows from site will be greater than historic levels. Site appurtenances will not adversely affect the downstream and surrounding developments.

This report and findings is in general conformance with the MDDP and Preliminary Drainage Reports or other pertinent studies

Review 1 comment: Please identify and analyze whether the downstream facilities are adequate to accept the developments flows.

Additionally, compare the detained flows and the historical flow leaving the site. Indicate whether or not the sites flow is at or below historic flows leaving the site.

Review 2: unresolved. Please analyze the downstream facilities (ditches, culverts, storm pipes etc.) and indicate whether they are adequate to accept the developments flows. Please identify the total developed flows of the site and compare with what the existing facilities where designed to.

MAJOR BASIN	SUB BASIN	AF	REA	BA	SIN	Tc MIN	in	I /hr.	SOIL	DEV. TYPE	(2	FL 5-ry	OW 100-yr		TURN RIOD	
		PLANIM READ	ACRES	LENGTH -FT	HEIGHT -FT								qp -CFS-	qp -CFS-	-у	ears-	
FALCON	0-1	0-1	9.75	2.47	300	4.5	27			A	SF 5AC.	0.12	0.39				
			V=0.82	+480	1.3	+10	1					11 1 - 1					
			C CT T			37	2.1	3.6					0.62	3.5	5	100	
HISTORIC	A	COGO	5.00	+525	9	+13	100	12.3					i ii				
			V=0.65			50	1.8	2.8	A	R/L	0.08	0.35					
	TOTAL	4 7 7	7.47							MIX	0.093	0.362	1.25	7.6	5	10	
DEVELOPED	A	COGO	1.68	300	2.5	15.2			A	GRAVEL	0.59	0.70	1	4 12 7	5	10	
	100		V=3.06	+300	7	+1.6		-					1.6	1 5.5			
	H		1			16.8	3.2	5,5					3.2	6.5	5	10	
	01 + A	(DP-1)	4.15	=400	8	+2	3.2	5.5	Α	MIX	0.310	0.516		11 1 1 1 1			
			V=2.82			52	1.7	2.9			7 1	10 = "	2,1	6.2	5	10	
	В	COGO	0.66	370	2.4	16.4			A	GRAVEL	0.59	0.70	1.3	2.5	5 .	10	
	C	COGO	2.30	300	4	14.5			A	GRAVEL	0.59	0.70				Ţ	
			V=2.66	+340	6	+2.1											
			1 2.50			16.6	3.3	5.5					4.5	8.9	5	10	
	B+C			+360	8	+2.7						ILE:				-	
		(DP-2)	2.96			19.3	3.0	5.1	Α	GRAVEL	0.59	0.70	5.2	10.4	5	10	
	D	COGO	0.36	240	4.5	11.6	3.8	6.4	Α	GRAVEL	0.59	0.70	0.8	1.6	5	10	
	B+C+D		V=2.22	+50		+0.4			1 - 1 - 1		2 4 5		-	1.7			
		(DP-3)	3.32			19.7	3.0	5.1	Α	GRAVEL	0.59	0.70	5.9	11.9	5	10	
	+0-1+A		7.47	+240	2.4	+2					2.57						
						54	1.7	2.8	Α	MIX	0.434	0.598	5.5	12.5	5	10	
HYDI PROJ: FALCON RATIONAL MET		SUB	BY: O.E. W				OL	IVEF		ATTS, CON				R, INC.	PA	GE 1 OF >	

 $\pm T \pm$

	Design Procedure Fo	orm: Sand Filter (SF)	
Ondo e	UD-BMP (Version 3.0	6, November 2016)	Sheet 1 of 2
Designer:	O.E, Watts	AND CARROLL SECTION	
Company:	Oliver E. Watts, CE		provide calculation
Date:	June 5, 2023 Falcon Storage Subdivision		to how this was
Project: Location:	Faicon Storage Subdivision		determined
1 Basin Str	orage Volume		
	William Manager and the second	I V	
	ve Imperviousness of Tributary Area, I. if all paved and roofed areas upstream of sand filter)	I _n = 62.3 %	
B) Tribut	ary Area's Imperviousness Ratio (i = I _a /100)	1 = 0,020	
	r Quality Capture Volume (WQCV) Based on 12-hour Drain Time CV= 0.8 * (0.91* i ³ -1.19 * i ² + 0.78 * i)	WQCV = 0.20 water	rshed inches
D) Contr	ibuting Watershed Area (including sand filter area)	Area = 325,393 sq ft	
	r Quality Capture Volume (WQCV) Design Volume cv = WQCV / 12 * Area	V _{wacv} =5,295 cu ft	
	atersheds Outside of the Denver Region, Depth of age Runoff Producing Storm	d ₆ = in	
	Vatersheds Outside of the Denver Region, r Quality Capture Volume (WQCV) Design Volume	VWQCV OTHER = cu ft	
	Input of Water Quality Capture Volume (WQCV) Design Volume if a different WQCV Design Volume is desired)	Vwacv user =cu ft	
2. Basin Ge	ometry		
A) WQC	/ Depth	D _{WQQV} =ft	
	Filter Side Slopes (Horizontal distance per unit vertical, flatter preferred). Use "0" if sand filter has vertical walls.	Z = 3.00 ft/ft	The
C) Minim	um Filter Area (Flat Surface Area)	A _{Min} = sq ft	spreadsheet
D) Actual	Filter Area	A _{Actual} =504007 sq ft	2534 should not be filled in
E) Volum	e Provided	$V_{\tau} = 13027$ cu ft	by hand
3. Filter Mai	lerial	Choose One ● 18" CDOT Class B or C Flit O Other (Explain):	ter Material
		123	
4. Underdra	in System	Choose One	
A) Are un	derdrains provided?	YES O NO	
B) Under	drain system crifice diameter for 12 hour drain time	- 12.000	_
	 Distance From Lowest Elevation of the Storage Volume to the Center of the Orifice 	y =ft	
	ii) Volume to Drain in 12 Hours	Vol ₁₂ =5,295 cu ft	b ¹
	iii) Orifice Diameter, 3/8" Minimum	D ₀ =5/8 in	orifice doesnt match GEC

	Design Procedure	Form: Sand Filter (SF)	
Designer:	O.E, Watts		Sheet 2 of
Company:	Oliver E. Watts, CE		
Date:	June 5, 2023		
Project: Location:	Falcon Storage Subdivision		
A) Is an	eable Geomembrane Liner and Geotextile Separator Fabric Impermeable liner provided due to proximity ructures or groundwater contamination?	Choose One O YES NO	
	utlet Works ribe the type of energy dissipation at inlet points and means of eying flows in excess of the WQCV through the outlet	Riprap at inlet and outlet	

include inlet and outlet riprap protection calculations



Required Area per Row (in²)

				- 4	Depth at	Outlet (ft)	1.1.		
		1.0	1.5	2.0	2.5	3.0	3.5	4.0	4.5
	2	15.04	7.71	5.10	3.76	2.95	2.41	2.02	1.73
	1	7.52	3.86	2.55	1.88	1.48	1.21	1.01	0.87
=	0.6	4.51	2.31	1.53	1.13	0.89	0.72	0.61	0.52
(acre-ft)	0.4	3.01	1.54	1.02	0.75	0.59	0.48	0.40	0.35
100	0.2	1.50	0.77	0.51	0.38	0.30	0.24	0.20	0.17
Volume	0.1	0.75	0.39	0.26	0.19	0.15	0.12	0.10	0.09
믕	0.06	0.45 .	0.23	0.15	0.11	0.09	0.07	0.06	0.05
	0.04	0.30	0.15	0.10	0.08	0.06	0.05	0.04	0.03
Design	0.02	0.15	0.08	0.05	0.04	0.03	0.02	0.02	0.02
ă	0.01	0.08	0.04	0.03	0.02	0.01	0.01	0.01	0.01

TABLE SB-1

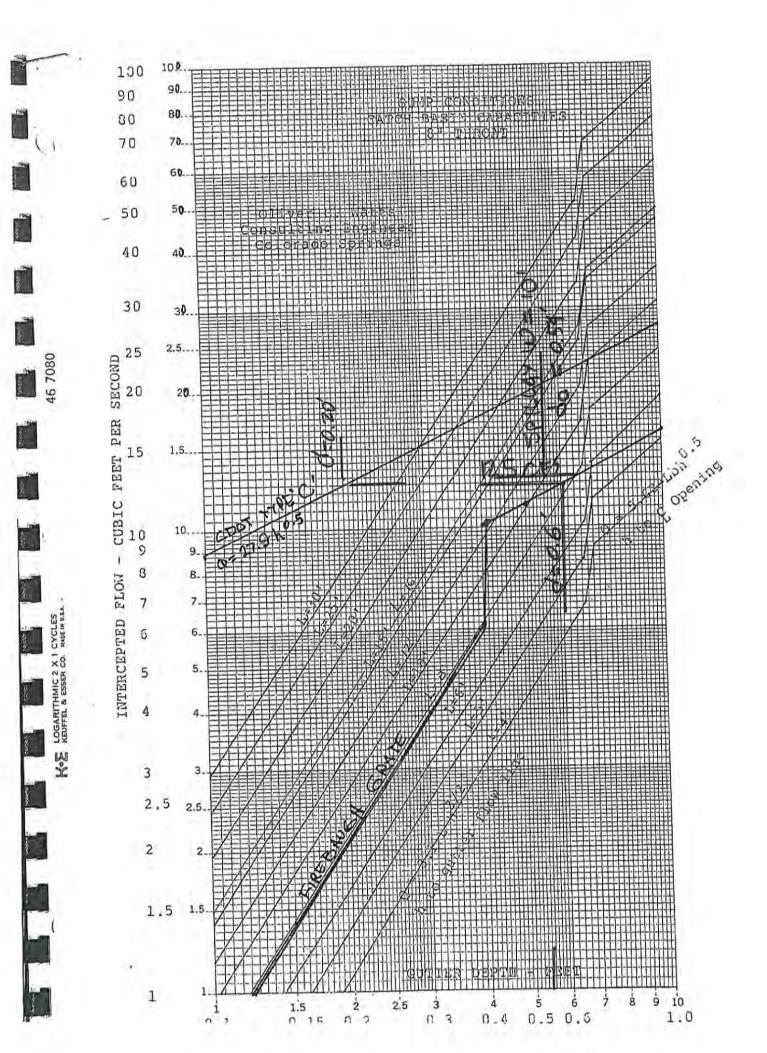
0-1+ A-D wacr 0.125 AF = 5445CF 0.3225 1112 lea 1/16" \$0 6"

Hole Diameter	Hole Diameter	. Are	a per Row (in ²)	
(in)	(in)	n=1	n = 2	n = 3
1/4	0.250	0.05	0.10	0.15
5/16	0.313	0.08	0.15	0.23
3/8	0.375	0.11	0.22	0.33
7/16	0.438	0.15	0.30	0.45
1/2	0.500	0.20	0.39	0.59
9/16	0.563	0.25	0.50	0.75
5/8	0.625	0.31	0.61	0.92
11/16	0.688	(837)	0.74	1.11
3/4	0.750	9.44	88.0	1.33
7/8	0.875	0.60	1.20	1.80
	1.000	0.79	1.57	2.36
1 1/8	1.125	0.99	1.99	2.98
1 1/4	1.250	1.23	2.45	3.68
1 3/8	1,375	1.48	2.97	4,45
1 1/2	1.500	1.77	3.53	5.30
1 5/8	1.625	2.07	4.15	6.22
1 3/4	1.750	2.41	4.81	7.22
1 7/8	1.875	2.76	5.52	8.28
2	2.000	3.14	6.28	9.42
	n = Numb	er of columns of perfo	rations	
Minimum steel	plate thickness	1/4"	5/16"	3/8"

TABLE SB-2

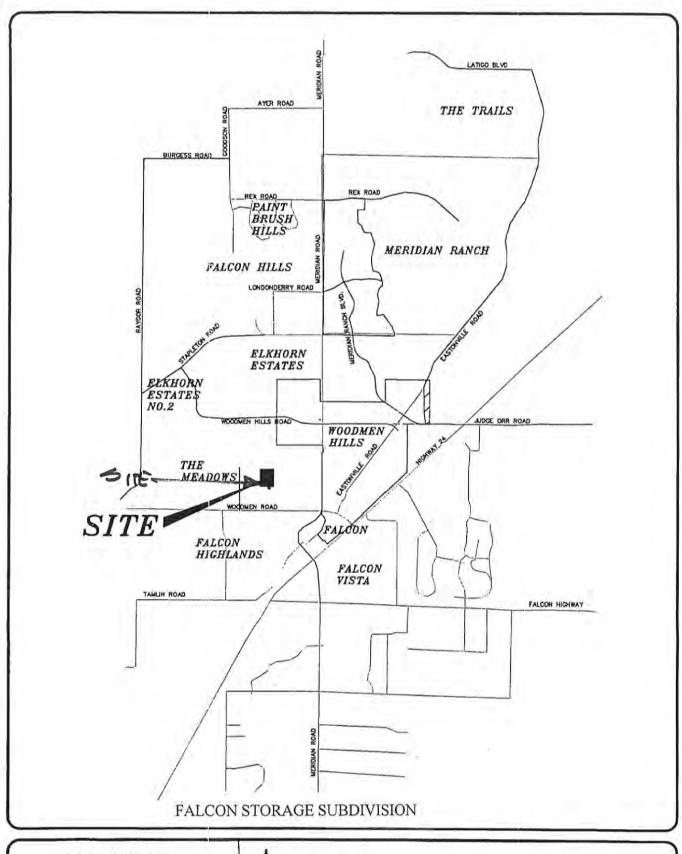
City of Colorado Springs **Stormwater Quality**

Figure SB-2 Outlet Sizing Application Techniques and Maintenance Requirements



IAMETER -IN	AREA -FT2-	D 8/3 -FT-	1 0 0 0	AV 6 64 9		
1111			N=0.010	N=0.013	N=0.024	N = 0.026
			W. W. W. O. W. I	1 - 1000 17 -	7 1 1 1 1 1 1 1 1	
2	0.02182	0.008413	0.3895	1999	HI- H	1444
4	0.08727	0.053420	2.4733	***		
6	0.19630	0.157500	7.2922	5.609	444	
1 8	0.34910	0.339200	15.7050	12.081	6-4	
10	0.54540	0.615000	28.4745	21,903	+++	# 5 t.
12	0.78540	1.000000	46.3000	35.615	999	1.2.2.1
15	1.22720	1.813100	83.9465	64.574	9.59	
18	1.76710	2,948300	136.5100	105.000	56.88	52.5
21	2.40530	4.447400	205.9100	158.400	85.80	79.2
24	3.14160	6.349600	293.9900	226.140	122.49	113.0
27	3.97610	8.692700	402.4700	309.590	167.70	154.7
30	4.90870	11.512600	533.0300	410.030	222.10	205.0
33	5.93960	14.844100		528.680		
36	7.06860	18,720800	866.7700	666.700	361.20	333.3
	8.29580	23.175100		825.400	444	11 11 11 11 11
39	9.62110	28.238900		1005.000	544.80	502.5
42	12.56640	40.317500		1436.000	777.80	718.0
	15.90430	55.195000		1966.000	1065.00	983.0
54	19.63500	73.100400		2604.000	1410.00	1302.0
60	23.75830	94.254200		3357.000	1818.00	1678.0
66	28.27430	118.869400		4234.000	2293.00	2117.0
78	33.18310	147.152900		5241.000	2839.00	2620.0
	38.48450	179.306000		6386.000	3459.00	3193.
84	44.17860	21.5.524500	4.44	7676.000	4158.00	3838.
90		256.000000		9118.000	4939.00	4559.
96	50.26550	350.466600		12480.000	6761.00	6140.
108	63.61730 78.53980	464.158900		16530.000	8954.00	8265.
120	78.53980	404,130300				

Oliver E. Watts Consulting Engine Colorado Springs



VICINITY MAP LATIGO

(719) 380-1090

Colorado Design Concepts

3578 Hartsel Drive E323 Colorado Springs, CO 80920

FIGURE:1

PROJECT NO. 200401

National Flood Hazard Layer FIRMette

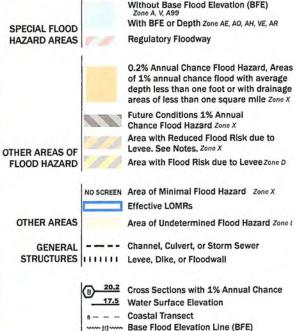


HOOP Notes -- 1 Man -- Outletonadem. Data waferahad Outshow 2020



Legend

SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT



Hydrographic Feature

Digital Data Available

OTHER

FEATURES

MAP PANELS

Limit of Study

Profile Baseline

Jurisdiction Boundary

Coastal Transect Baseline

No Digital Data Available

Unmapped

The pin displayed on the map is an approximate point selected by the user and does not represen an authoritative property location.

This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The basemap shown complies with FEMA's basemap accuracy standards

The flood hazard information is derived directly from the authoritative NFHL web services provided by FEMA. This map was exported on 3/25/2021 at 9:47 AM and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or become superseded by new data over time.

This map image is void if the one or more of the following map elements do not appear: basemap imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for unmapped and unmodernized areas cannot be used for regulatory purposes.

NOTES TO USERS

s map is for use in administering the National Flood Insurance Program. It does necessarily identify all areas subject to flooding, particularly from local drainage arces of small size. The community map repository should be consulted for satisfied updated or additional flood hazard information.

solide uposers or economics mountained to the solid possible upon the solid possible of the solid possible of

oestal Base Flood Elevations shown on this map apply only landward of 0,0° orth American Vertical Datum of 1986 (NAVDSB). Users of this FIRM should be ware that coastal flood elevations are also provided in the Summary of Sithwate levations table in the Flood Insurance Study report for this jurisdiction. Elevations shown in the Summary of Sithwater Elevations table should be used for construction odd/or floodplain management purposes when they are higher than the elevations how on this FIRM.

Boundaries of the floodways were computed at cross sections and interpolate between cross sections. The floodways were based on hydracliic considerations will regard to requirements of the National Flood Insurance Program. Floodway width and other pertinent floodway data are provided in the Flood Insurance Study report for this jurisdiction.

res" of the Flood Insurance

The projection used in the preparation of this map was Universal Transverse Mercator (UTM) zone 13. The horizontal datum was NAD83, GRS80 spheroid. Differences in datum, spheroid, projection or UTM zones zones used in the production of FIRMs for adjacent jurisdictions may result in slight positional differences in map features across jurisdiction boundaries. These differences do not affect the accuracy of this FIRMs.

Flood elevations on this map are referenced to the North American Vertical Datum of 1988 (NAVD88). These flood elevations must be compared to structure and orgonal elevations referenced to the same vertical adatum. For information regarding conversion between the National Geodetic Vertical Datum of 1929 and the North American Vertical Datum of 1988, visit the National Geodetic Survey at the following orders:

NGS Information Services NOAA, N/NGS12 National Geodetic Survey SSMC-3, #9202 1315 East-West Highway Silver Spring, MD 20910-3282

obtain current elevation, description, and/or location information for bench mark own on this map, please contact the Information Services Branch of the Nations sodetic Survey at (301) 713-3242 or visit its website at http://www.ngs.noae.gov/.

ase Map information shown on this FIRM was provided in digital format by El Paso ounly, Colorado Springs Utilities, Cily of Fountain, Bureau of Land Management, ational Cosanie and Almospheric Administration, United States Geological Survey, nd Anderson Consulting Engineers, Inc. These data are current as of 2006.

This map reflects more detailed and up-to-date stream channel configurations and floodplain delineations than those shown on the previous FIRM for this jurisdiction. The floodplain and floodways that were transferred from the previous FIRM may have been adjusted to conform to these new stream channel configurations. As a result, the Flood Profites and Floodway Data tables in the Flood Insurance Study Report (which contains authoritative hydrautic data) may reflect stream channel distances that differ from what is shown on this map. The profile baselines depicted on this map represent the hydrautic modeling baselines that match the flood profiles and Floodway Data Tables if applicable, in the FIS report. As a result, the profile and Floodway Data Tables if applicable, in the FIS report. As a result, the profile and floodway Data Tables if applicable, in the maximum profiles the profile and floodway that the floodway that th

Corporate limits shown on this map are based on the best data available at the time of publication. Because changes due to annexations or de-annexations may have occurred wher this map was published, map users should contact appropriate community officials to verify current corporate limit locations.

Please refer to the separately printed Map Index for an overview map of the count showing the layout of map panels; community map repository addresses; and a Listing of Communities table containing National Flood Insurance Program dates to each community as well as a listing of the panels on which each community is

Contact FEMA Map Service Center (MSC) via the FEMA Map Information eXchange (FMIX) 1-077-336-2627 for information on available products associated with this FIFM. Available products may include previously issued Letters of Map Change. Flood Insurance Study Report, and/or digital versions of this map. The MSC may also be reached by Fax at 1-800-358-9520 and its website a http://www.msc.fema.gov/.

you have questions about this map or questions concerning the National Flood isurance Program in general, please call 1-877-FEMA MAP (1-877-336-2627) or sit the FEMA website at http://www.fema.gov/business/nfip.

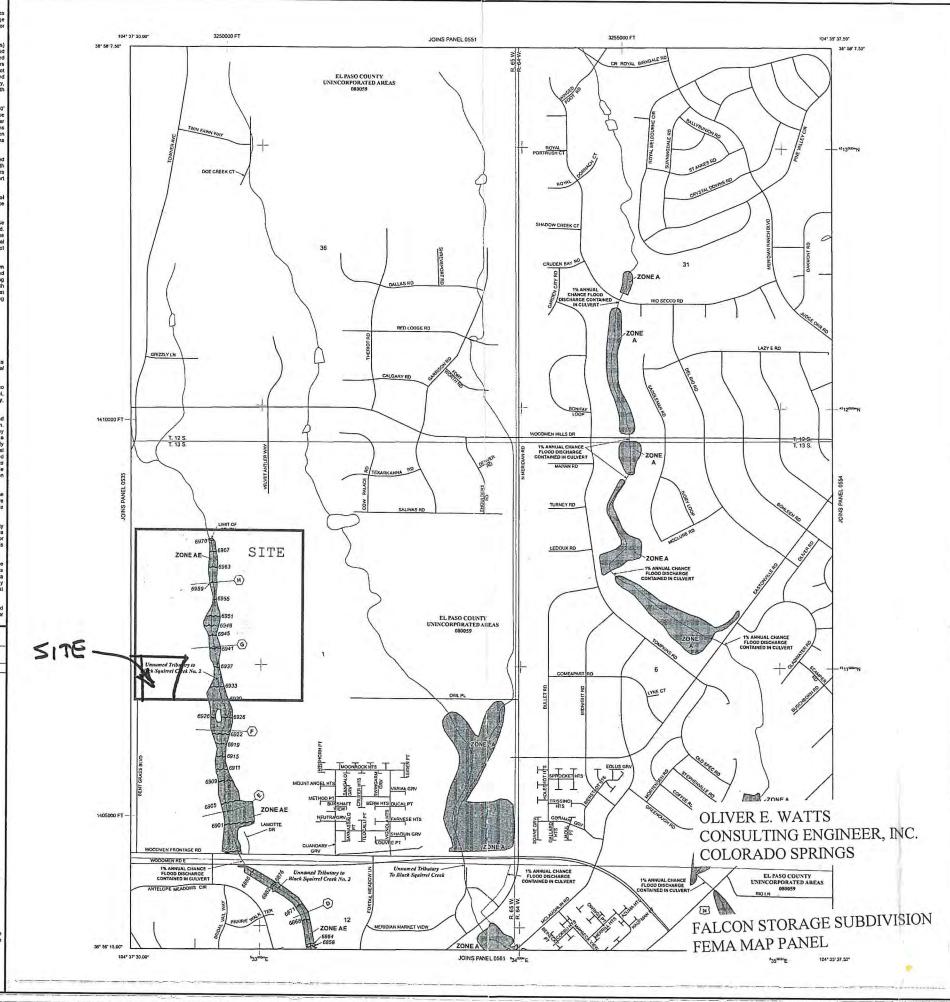
El Paso County Vertical Datum Offset Tabl Flooding Source

REFER TO SECTION 3.3 OF THE EL PASO COUNTY FLOOD INS
FOR STREAM BY STREAM VERTICAL DATUM CONVERSION

This Digital Flood Insurance Rate Map (DFIRM) was produced through a Cooperating Technical Partner (CTP) agreement between the State of Colorado Water Conservation Board (CWCB) and the Federal Emergency Management Agency



available from local communities and the Colora
Water Conservation Board.



LEGEND

SPECIAL FLOOD HAZARD AREAS (SFHAS) SUBJECT TO INUNDATION BY THE 1% ANNUAL CHANCE FLOOD

The 1% annual chance flood (100-year flood), also known as the base flood, is the flood that has a 1% chance of being equaled or exceeded in any given year. The Special Flood Hazard Area is the area subject to flooding by the "1% annual chance flood. Area of Special Flood Hazard area (and Leave and Leave flood. Area of Leave and Leave flood.

No Base Flood Elevations determined.
Base Flood Elevations determined.
Flood depths of 1 to 3 feet (usually areas of ponding); Base Flood Elevations determined.

Flood depths of 1 to 3 feet (usually sheet how on stoping terrain); everage depths determined. For areas of altivial fan flooding, velocities also determined.

occuminos.

Special Road Hazard Airal Formerly protected from the 1% annual chance flood by a flood control system that was subsequently secercified. Zone AR indicates that the former flood control system is being restored to provide protection from the 1% annual chance or greater flood. Area to be protected from 1% annual chance flood by a Federal flood protection system under construction; no Base Flood Elevations

determined.

Ceastal flood zone with velocity hazard (wave action); no Base Flood Elevations determined.

FLOODWAY AREAS IN ZONE AE

The floodway is the channel of a stream plus any adjacent floodplain areas that must be kept free of encroactioners so that the 1% annual chance flood can be carried without substantial increases in flood heights.

OTHER FLOOD AREAS

Areas of 0.2% annual chance flood; areas of 1% annual chance flood with average depths of less than 1 foot or with drainage areas less than 1 square mile; and areas protected by leves from 1% annual chance flood.

Areas determined to be outside the 0.2% ennual chance floodplain

COASTAL BARRIER RESOURCES SYSTEM (CBRS) AREAS

OTHERWISE PROTECTED AREAS (OPAS)

Floodway boundary

CERS and OPA boundary Property and a

Boundary dividing Special Flood Hazard Areas of differentiations, flood depths or flood velocities. Base Flood Elevation line and value: elevation in frett

(A)—(A)

23-----23 97° 57° 30.00° 32° 22° 30.00°

~~ 513 ~~

4750EM

Geographic coordinates referenced to the North American Datum of 1983 (NAD 83)

1000-meter Universal Transverse Mercator grid ticks, zone 13

6000000 FT

M1.5

MAP REPOSITORIES Refer to Map Repositories list on Map Index

EFFECTIVE DATE OF COUNTYWIDE FLOOD INSURANCE RATE MAP MARCH 17, 1897

For community map revision history prior to countywide mapping, refer to the Community Map History Table located in the Flood Insurance Study report for this jurisdiction.

11/21200 MAP SCALE 1" = 500" 250 0 500 1000 HHH FEET E METERS

NED

INSAURAN

MATIONAL

PANEL 0553G

AND INCORPORATED AREAS

FLOOD INSURANCE RATE MAP EL PASO COUNTY, COLORADO

PANEL 553 OF 1300

(SEE MAP INDEX FOR FIRM PANEL LAYOUT)

COMMUNITY EL FASO COUNTY

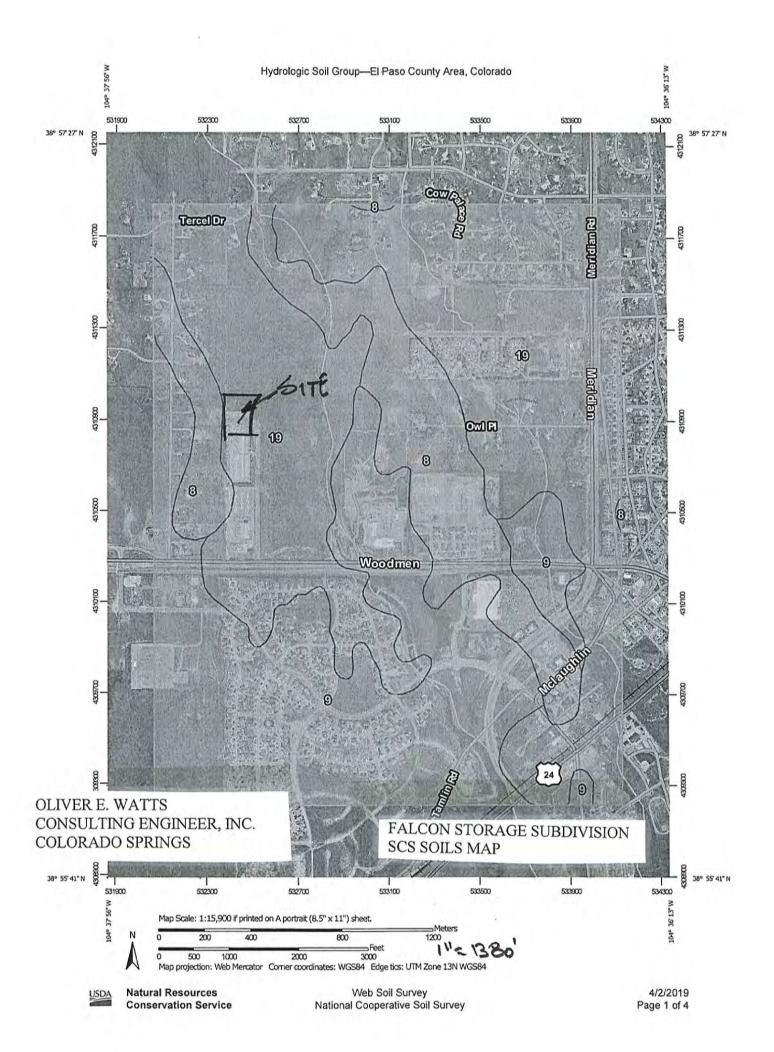
NUMBER PANEL SUFFIX



MAP NUMBER 08041C0553G

MAP REVISED **DECEMBER 7, 2018**

Federal Emergency Management Agency



EL PASO COUNTY AREA, COLORADO TABLE 16.--SOIL AND WATER FEATURES

Absence of an entry indicates the feature is not a concern. See "flooding" in Glassary for definition of terms as "rare," "brief," and "very brief." The symbol > means greater than]

0-11 mans and	Hydro-		Flooding	l Bed	rock	Potential	
Soil name and map symbol	logic group	Frequency	Duration	Months	Depth	Hardness	frost
11 amosa:	c	Frequent	Brief	May-Jun	<u>In</u> >60		High.
iscalon: 2, 3	В	None			>60		Moderate:
3adland: 4	D		444	444			
3ijou: 5, 6, 7	В	None			>60		Low.
3lakeland: 8	A	None		257	>60		Low.
19: Blakeland part-	A	None		4-5	>60		Law.
Fluvaquentic Haplaquolls part	D	Common	Very brief	Mar-Aug	>60	1444	High.
Blendon: 10	В	None		u12	>60	(44-)	Moderate.
Bresser: 11, 12, 13	В	None	42-	0.12	>60		Low.
Brussett: 14, 15	В	None	4.44	555	>60		Moderate.
Chaseville: 16, 17	Ä	None	242	1.44	>60		Low.
118: Chaseville part	A	None			>60		Low.
Midway part	D	None	-	1444	10-20	Rippable	Moderate.
Columbine:		None to rare		222	>60		Low.
Connerton: 120: Connerton part-	В	None			>60		High.
Rock outcrop part	D						
Cruckton: 21	В	None		1777	>60		Moderate.
Cushman: 22, 23	С	None			20-40	Rippable	Moderate.
124: Cushman part	c	None		244	20-40	Rippable	Moderate.
Kutch part	С	None	yy	4	20-40	Rippable	Moderate.
Elbeth: 25, 26	В	None	4 / 1		>60		Moderate.
127: Elbeth part	В	None		555	>60		Moderate.

See footnote at end of table.

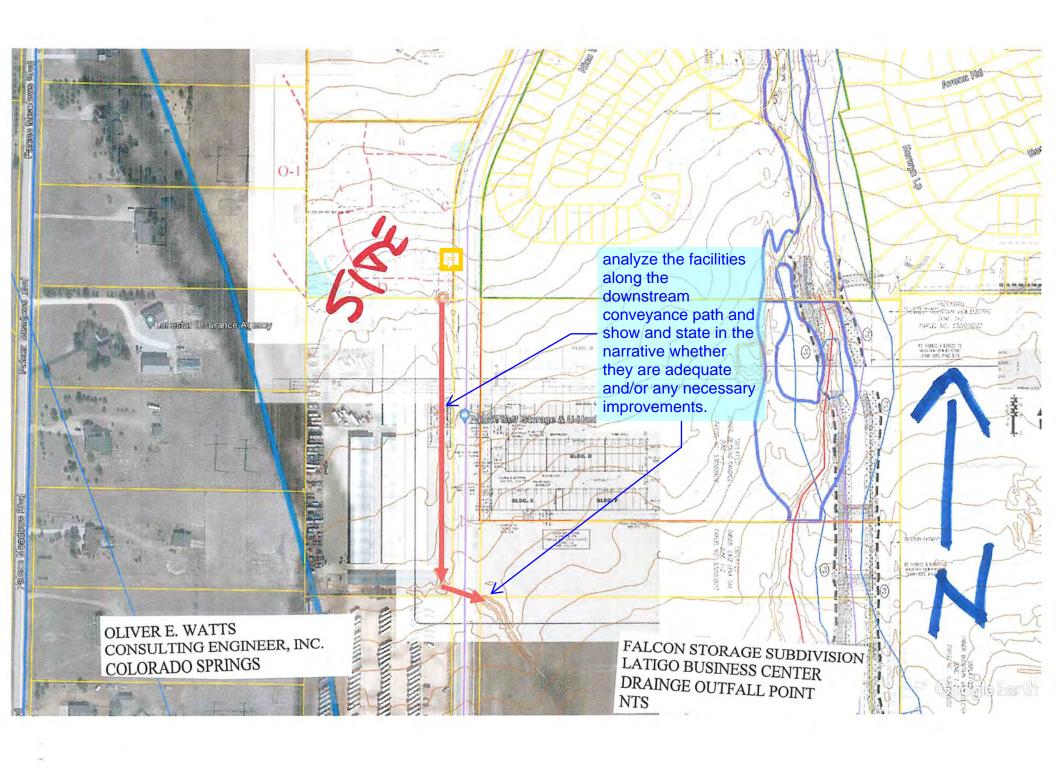


Table 6-6. Runoff Coefficients for Rational Method

(Source: UDFCD 2001)

Land Use or Surface	Percent	Runoff Coefficients											
Characteristics	Impervious	2-year		5-9	ear	10-	year	25-	year	50-year		100-	-year
		HSG AGB	HSG C&D	HSG A&B	HSG CAD	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG CAD	HSG A&B	HSG CBD
Business				11				30000	100 000	110011111	HIS CAD	H3G Mad	nou car
Commercial Areas	95	0,79	0.80	0.81	0.82	0.83	0.84	0.85	0.87	0.87	0.88	0.88	0.89
Neighborhood Areas	70	0.45	0.49	0.49	0.53	0.53	0.57	0.58	0.62	0.60	0.65	0.62	0.68
Residential			-	-		-							
1/8 Acre or less	65	0.41	0.45	0.45	0.49	0.49	0.54	0.54	0.59	0.57	0.62	0.59	0.00
1/4 Acre	40	0.23	0.28	0.30	0.35	0,36	0.42	0.42	0.50	0.46	0.54	0.50	0.65
1/3 Acre	30	0.18	0.22	0.25	0.30	0.32	0.38	0.42	0.47	0.48			0.58
1/2 Acre	25	0.15	0.20	0.22	0.28	0.30	0,36	0.37	0.46	0.43	0.52 0.51	0.47	0.57
1 Acre	20	0.12	0.17	0.20	0.26	0.27	0.34	0.35	0.44	0.40	0.50	0.44	0.56
Industrial				-			_						
Light Areas	80	0.57	0.50	0.59	0.63	0.63	0.66	0.66	0.70	0.68	0.72	0.70	0.74
Heavy Areas	90	0.71	0.73	0.73	0.75	0.75	0.77	0.78	0.80	0.80	0.72	0.70	0.83
Parks and Cometeries	7	0.05	0.09	0,12	0.19	0.20	0.29	0.30	0.40	0.34	0.46	0.39	0.52
Playgrounds	13	0.07	0.13	0.16	0.23	0.24	0.31	0.32	0.42	0.37	0.48	0.41	0.54
Railroad Yard Areas	40	0.23	0,28	0.30	0,35	0.36	0.42	0.42	0.50	0.46	0.54	0.50	0.58
Undeveloped Areas					-		-					9.7	
Historic Flow Analysis Greenbelts, Agriculture	2	0.03	0.05	0.09	0.16	0.17	0.26	0.26	.0.38	0.31	0.45	0.36	0.51
Pasture/Meadow	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50
Forest	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50
Exposed Rock	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Offsite Flow Analysis (when landuse is undefined)	45	0.26	0.31	0.32	0.37	0.38	0.44	0,44	0.51	0,48	0.55	0.51	0.59
Streets		-											
Paved	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Gravel	80	0.57	0.60	0.59	0.63	0,63	0.66	0.66	0.70	0.68	0.72	0.70	0.74
Drive and Walks	100	0.89	0.89	0,90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Roofs	90	0.71	0.73	0.73	0.75	0.75	0.77	0.78	0.80	0.80	0.82	0.81	0.83
Lawns	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50

3.2 Time of Concentration

One of the basic assumptions underlying the Rational Method is that runoff is a function of the average rainfall rate during the time required for water to flow from the hydraulically most remote part of the drainage area under consideration to the design point. However, in practice, the time of concentration can be an empirical value that results in reasonable and acceptable peak flow calculations.

For urban areas, the time of concentration (t_c) consists of an initial time or overland flow time (t_i) plus the travel time (t_i) in the storm sewer, paved gutter, roadside drainage ditch, or drainage channel. For non-urban areas, the time of concentration consists of an overland flow time (t_i) plus the time of travel in a concentrated form, such as a swale or drainageway. The travel portion (t_i) of the time of concentration can be estimated from the hydraulic properties of the storm sewer, gutter, swale, ditch, or drainageway. Initial time, on the other hand, will vary with surface slope, depression storage, surface cover, antecedent rainfall, and infiltration capacity of the soil, as well as distance of surface flow. The time of concentration is represented by Equation 6-7 for both urban and non-urban areas.

$$t_c = t_i + t_i \tag{Eq. 6-7}$$

Where:

 t_c = time of concentration (min)

 t_i = overland (initial) flow time (min)

 t_i = travel time in the ditch, channel, gutter, storm sewer, etc. (min)

3.2.1 Overland (Initial) Flow Time

The overland flow time, t_i , may be calculated using Equation 6-8.

$$t_i = \frac{0.395(1.1 - C_5)\sqrt{L}}{S^{0.33}}$$
 (Eq. 6-8)

Where:

 t_i = overland (initial) flow time (min)

 C_5 = runoff coefficient for 5-year frequency (see Table 6-6)

L = length of overland flow (300 ft <u>maximum</u> for non-urban land uses, 100 ft <u>maximum</u> for urban land uses)

S = average basin slope (ft/ft)

Note that in some urban watersheds, the overland flow time may be very small because flows quickly concentrate and channelize.

3.2.2 Travel Time

For catchments with overland and channelized flow, the time of concentration needs to be considered in combination with the travel time, t_i , which is calculated using the hydraulic properties of the swale, ditch, or channel. For preliminary work, the overland travel time, t_i , can be estimated with the help of Figure 6-25 or Equation 6-9 (Guo 1999).

$$V = C_{\nu} S_{\nu}^{0.5}$$
 (Eq. 6-9)

Where:

V = velocity (ft/s)

 $C_v = \text{conveyance coefficient (from Table 6-7)}$

 S_w = watercourse slope (ft/ft)

Table 6-7. Conveyance Coefficient, Cv

Type of Land Surface	C_{ν}
Heavy meadow	2.5
Tillage/field	5
Riprap (not buried)*	6.5
Short pasture and lawns	7
Nearly bare ground	10
Grassed waterway	15
Paved areas and shallow paved swales	20

For buried riprap, select C_v value based on type of vegetative cover.

The travel time is calculated by dividing the flow distance (in feet) by the velocity calculated using Equation 6-9 and converting units to minutes.

The time of concentration (t_c) is then the sum of the overland flow time (t_i) and the travel time (t_i) per Equation 6-7.

3.2.3 First Design Point Time of Concentration in Urban Catchments

Using this procedure, the time of concentration at the first design point (typically the first inlet in the system) in an urbanized catchment should not exceed the time of concentration calculated using Equation 6-10. The first design point is defined as the point where runoff first enters the storm sewer system.

$$t_c = \frac{L}{180} + 10 \tag{Eq. 6-10}$$

Where:

 t_c = maximum time of concentration at the first design point in an urban watershed (min)

L =waterway length (ft)

Equation 6-10 was developed using the rainfall-runoff data collected in the Denver region and, in essence, represents regional "calibration" of the Rational Method. Normally, Equation 6-10 will result in a lesser time of concentration at the first design point and will govern in an urbanized watershed. For subsequent design points, the time of concentration is calculated by accumulating the travel times in downstream drainageway reaches.

3.2.4 Minimum Time of Concentration

If the calculations result in a t_c of less than 10 minutes for undeveloped conditions, it is recommended that a minimum value of 10 minutes be used. The minimum t_c for urbanized areas is 5 minutes.

3.2.5 Post-Development Time of Concentration

As Equation 6-8 indicates, the time of concentration is a function of the 5-year runoff coefficient for a drainage basin. Typically, higher levels of imperviousness (higher 5-year runoff coefficients) correspond to shorter times of concentration, and lower levels of imperviousness correspond to longer times of

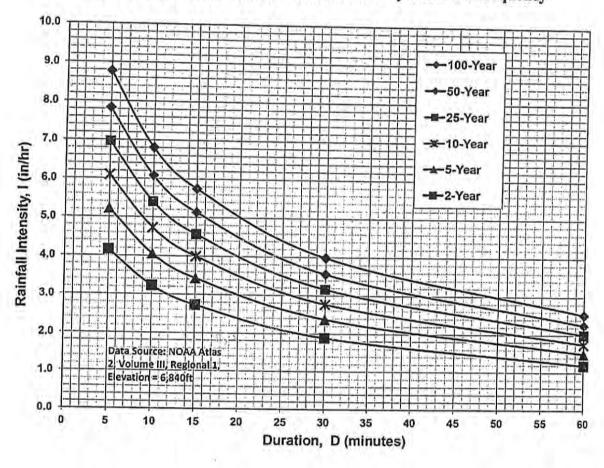


Figure 6-5. Colorado Springs Rainfall Intensity Duration Frequency

IDF Equations

$$I_{100} = -2.52 \ln(D) + 12.735$$

$$I_{50} = -2.25 \ln(D) + 11.375$$

$$I_{25} = -2.00 \ln(D) + 10.111$$

$$I_{10} = -1.75 \ln(D) + 8.847$$

$$I_5 = -1.50 \ln(D) + 7.583$$

$$I_2 = -1.19 \ln(D) + 6.035$$

Note: Values calculated by equations may not precisely duplicate values read from figure,

