PRELIMINARY AND FINAL DRAINAGE PLAN AND REPORT FALCON STORAGE SUBDIVISION PART OF THE SW1/4 SECTION 1, T.13S. R.65W. OF THE 6TH P.M. EL PASO COUNTY

February 4, 2021

Revised November 23, 2022

> Revised June 7.2023

Revised June 22, 2023

Revised August 31, 2023

Revised December 12, 2023

> Revised March 3, 2024

PCD File No. PPR2232 PCD File No. MS232

Prepared for

Falcon Storage Partners LLLP 4615 Northpark Drive Colorado Springs, CO 80918

Oliver E. Watts, Consulting Engineer, Inc. Colorado Springs, Colorado

OLIVER E. WATTS, PE-LS

OLIVER E. WATTS, CONSULTING ENGINEER, INC. CIVIL ENGINEERING AND SURVEYING 614 ELKTON DRIVE COLORADO SPRINGS, COLORADO 80907 (719) 593-0173 fax (719) 265-9660 <u>olliewatts@aol.com</u> Celebrating over 45 years in business

March 3, 2024

El Paso County Planning and Community Development 2880 International Circle Colorado Springs, CO 80910

ATTN: Joshua Palmer, P.E.

SUBJECT: Preliminary and Final Drainage Plan and Report Falcon Storage Subdivision

Transmitted herewith for your review and approval is the drainage plan and report for The Falcon Storage Subdivision in El Paso County. This report will accompany the development plan and subdivision plat submittal. This report has been revised in accordance with your review comments of November 23, 2022, March 2, 2023, August 18, 2023, October 16, 2023 and February 8, 2024.

Please contact me if I may provide any further information.

Oliver E. Watts, Consulting Engineer, Inc.

BY: _____

Oliver E. Watts, President

FALCON STORAGE SUBDIVISION DRAINAGE REPORT TABLE OF CONTENTS

Drainage Report 5 pages Computations, 7 pages Vicinity Map FEMA Panel No. 08041C0553 G SCS Soils Map and Interpretation Sheet Backup Information, 4 sheets Falcon DBPS Map Drainage Plan, Falcon Meadows at Bent Grass Drainage Plan, Latigo Business Center Drainage Plan, Dwg 02-5523-04 Hydrology Map, Latigo Business & Research Center, Filing No. 1

FALCON STORAGE SUBDIVISION DRAINAGE REPORT REFERENCES

- 1. City-County Drainage Criteria, current edition
- 2. Fema Firm Insurance Rate Map
- 3. El Paso County Soils Survey, SCS
- 4. Falcon Drainage Basin Planning Study
- 5. Drainage Report, Falcon Meadows at Bent Grass
- 6. Drainage Report, Latigo Business Center, Lot 1
- 7. Final Drainage Report, Latigo Business & Research Center, Fil. No. 1

1. ENGINEER'S STATEMENT:

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the County for drainage reports and said report is in conformity with the applicable master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.



I the owner / developer have read and will comply with all of the requirements specified in this drainage report and plan.

Falcon Storage Partners LLLP

By **Richard Graham**

4615 Northpark Drive Colorado Springs, CO 80918

3. EL PASO COUNTY:

Filed in accordance with the requirements of the El Paso Land Development Code, Drainage Criteria Manual Volumes 1 and 2, and the Engineering Criteria Manual, as amended.

Joshua	Palmer, P	.E.,	
County	Engineer	/ ECM	Administrator

date

Conditions:

4. LOCATION AND DESCRIPTION:

The Falcon Storage Subdivision is located in the Latigo Business Center development of El Paso County as shown on the enclosed vicinity map. Occupying a portion of the West half of Section 1, Township 13 South, Range 65 West of the 6th P.M., totaling 5.004 acres. It is located in the Falcon Drainage Basin as shown on the enclosed basin map. It lies west of Bent Grass Meadows Drive north of the Latigo Business Center Filing No. 1 as shown on the enclosed drainage plan. The site will be developed into an RV Storage site as shown on the enclosed drainage plan, as an expansion to the one in the Latigo Business Center Filing No. 1, both owned by the developer.

5. FLOOD PLAIN STATEMENT:

This subdivision is not within the limits of a flood plain or flood hazard area, according to FEMA map panel number 08041C0553 G, dated December 7, 2018, a copy of which is enclosed for reference.

6. METHOD AND CRITERIA:

The method used for all computations is that specified in the City-County Drainage Criteria Manual, using the rational method for areas of the size of the development. All computations are enclosed for reference and review. Pertinent portions of the criteria are enclosed.

The soils in the subdivision have been mapped by the local USDA/SCS office, and a soils map and interpretation sheet are enclosed for reference. All soils in this area are of hydrologic group "A" within the development area.

7. DESCRIPTION OF RUNOFF:

A. Drainage Inflows: The drainage Report for Falcon Meadows at Bent Grass indicates an existing drainage swale above the north boundary to divert runoff from this site and route it to Bent Grass Meadows and then past this development in Bent Grass Meadows Drive to outfall points to an existing detention pond across the street. A copy of this drainage plan is enclosed. Also shown on this map is that portion of the Meadows Filing No. 1 that drains 0.62 cfs / 3.5 cfs (5-year / 100-year runoffs) into this subdivision along the westerly boundary (Basin O-1), and it indicates the historic undeveloped runoff of the site, Basin A (historic) totaling 1.25 cfs / 7.6 cfs at the lowest (southeast) portion of the subdivision.

B. Interior Routing: The area will be graded to conform to the existing topography shown on the drainage plan. The property has been rough graded, which complies with the historic runoff pattern. Additional grading is indicated which is intended to contain the runoff into the interior drive isle street network, and along the streets to the water quality pond The westerly street (Basin A) will combine with offset basin O-1 to develop $3.0 \text{ cfs} \ 6.2 \text{ cfs} \ (5-\text{year} / 100-\text{year runoffs})$ near the in the southwest corner of the plat (Design Point 1). Basin B will develop 1.3/2.5 cfs in the southerly driveway adjacent to the north entrance. It will combine with basin C along the same routing for 5.2/10.4 cfs at the southwest intersection (design point 2). This will combine basin D to outfall into the water quality pond (design point 3). The total outfall at this point 5.5 cfs/12.5 cfs, into the sand filter basin.

C. Detention Storage: At the proposed outfall point a sand filter water quality pond is proposed, as required by the County. The pond is sized for a temporary sedimentation basin to be used during the construction period and converted into a permanent sand filter basin upon completion. The sedimentation basin will contain 9000 +CF (at 1800 CF per acre). An 8-inch riser pipe is used as an outlet, with holes drilled as computed to detain the runoff as required. One foot of freeboard is provided with a spillway that will pass the 100-year runoff. Details are shown on the enclosed drainage plan. Following construction the basin will be converted to a sand filter basin. A 4-inch slotted underdrain will be placed in a section of CDOT class C Filter material and drain into the grated inlet outlet structure set at the WQCV level, and sized for the 100-year runoff. An orifice plate will be provided on the end of the underdrain with an orifice sized for the installation. Sand filter water quality basin computation sheet is included for the basin. Fully

Falcon Storage Subdivision Preliminary and Final Drainage Plan and Report

developed runoffs are analyzed for the basin. As required by the County, the basin is used for water quality storage only and the outfall will run across Latigo Business Center Filing No. 1 to an existing full spectrum pond (Pond WU) to the south of Woodmen Road, north of Highway 24, between Tamlin and Meridian Roads, in accordance with the approved drainage reports for the area. This outfall run is described below.

D. Outfall Point: Discharge from the subdivision will be into existing north-south street of Lot 1 of the Latigo Business Center, Filing no. 1, as shown on the drainage plan. Some minor construction is shown along the north boundary of Lot 1 as shown on the drainage plan to create a positive installation. The two properties are under common ownership and permission to outfall into the Latigo Business Center is granted. The drainage plan for the Latigo Business Center is enclosed. This report indicated two existing discharges: 0.2 cfs / 0.5 cfs near the southwest corner and 4.1 cfs / 10.1 cfs over the remaining south frontage. A 24 inch RCP will run from the CDOT Type C outlet box at a minimum slope of 0.22% into the existing ditch shown on the drainage plan.

As shown on the enclosed drainage plan for Lot 1 of the Latigo Business Park and the enclosed sheet 7 of the computations the swales along said Lot 1 adjacent to Bent Grass Meadows Boulevard are more than adequate to safely contain the drainage outfall from this subdivision. The depth of runoff from the pond is 0.21 feet in the upper swale and 0.49 feet below the entrance to Lot 1. These swales also indicate more than adequate freeboard according to the grading plan. At the bottom (South) of Lot 1 is the storm sewer system that diverts the runoff from the District 49 bus facility and Bent Grass Meadows Boulevard eastward toward the above mentioned full spectrum pond. This being the limit of the first public storm sewer and our required justification

The outfall for this runoff will be at the south termination of the above mentioned swale. The increase of 2.4 cfs from this 10.1 cfs would be into 42" RCP shown at design point 7 of the enclosed Latigo Business Center Filing No. 1, which would create a 100-year runoff of 57.9 cfs. As shown on page 1A of the enclosed computations the 0.5% slope of this 42" RCP is 71.1 CFS. There is more than ample capacity in this public system to accommodate our minor increase.

WATER QUALITY

A sand filter basin water quality facility will be provided as described above.

FOUR STEP PROCESS

The following process has been followed to minimize adverse impacts of urbanization

<u>Runoff Reduction</u>: The scope of the development has been minimized consistent with zoning requirements to present the minimum footprint in providing a RV Storage development. The undisturbed portions are to be landscaped to reduce the impervious percent.

<u>Provide WQCV</u>: Water quality storage is being provided for this subdivision by a sand filter water quality pond and runoff will be routed to a full spectrum pond located downstream, south of Woodmen Road, north of Highway 24, between Tamlin and Meridian Roads, by others as a sub regional facility.

<u>Stabilize Drainage Ways:</u> The site will be graded to route the runoff over improved street installations to provide channel stabilization in the natural erosive material over the site. Discharge from the site will be into adjacent and downstream facilities in accordance with the master drainage basin plan for the Falcon drainage basin and previously approved subdivision drainage reports. Copies of each plan are enclosed. There will be no adverse affect on downstream developments as a result of this subdivision.

<u>Consider need for Industrial and Commercial BMP's</u>: This is a RV Storage site, so source control problems will be a minimum. During construction, standard site specific state of the art BMP's will be employed to minimize and mitigate erosive problems.

Item No.	Description	Quantity	Unit Cost	<u>Cost</u>
1	Pond/BMP Earthwork	881 CY	\$ 23.00	\$ 20263.00
2	Slotted drain	187 LF	40.00	7480.00
3	Riprap	14 Tons	80.00	1096.00
4	Grated Inlet	1 ea	5611.00	5611.00
4	12" PVC drain	106 LF	112.00	11872.00
5	Concrete Pond Inlet	15 CY	589.00	10335.00
6	24" RCP Pond Outlet	106 LF	91.00	9646.00
	Subtotal Construction Cost			\$ 66303.00
	Engineering	10%		6630.30
	Total Estimated Cost			\$ 72933.30

8. COST ESTIMATE:

9. FEES: Due at plat recording. 2023 Falcon Basin Fees: 5.004 acres @46.4% Impervious = 3.1175 Impervious acres (see p. 6-17) Drainage fees @ \$ 37,256 per acre = \$ 86,503.07 Bridge fees @ \$ 5,118 per acre = \$ 11,083.26 **Total Fees: \$ 90,386.33**

10. SUMMARY

The Falcon Storage Subdivision is a proposed 1-lot, RV Storage subdivision containing 5.004 acres. The proposed street facilities will adequately convey, detain and outfall runoff from the site to existing sufficient adjacent and downstream facilities, as described in this report and the respective drainage reports. Water Quality is being utilized in lieu of a full spectrum detention pond due to the existing regional facility as described earlier in this report. Flows from site will be greater than historic levels. Site appurtenances will not adversely affect the downstream and surrounding developments.

This report and findings is in general conformance with the MDDP and Preliminary Drainage Reports or other pertinent studies

STREET AND STORM SEWER CALCULATIONS

STREET	LOCATION	DISTANCE -ft	ELEVATION & SLOPE	TOTAL RUNOFF -cfs- 5-yr./100-yr	STREET FLOW / CAPACITY -cfs- 5-yr./100-yr	PIPE FLOW -cfs-	TYPE PIPE, BASIN & SI	CATCH OPE %
BENT GRASS MEADOWS	DP 1							
				27.1/55.5		55.5	42" RCP S= CAPACITY =	
	PT 4							
						+2.4		
	REVISED				```	57.9	CA[P = 71.	1 CFS
						-		
STREET AN PROJECT: FAL		WER CALCUI GE BY: O.E DATE: March	. WATTS	OLIVER E. WA 614 ELKTO	ATTS, CONSULTI N DRIVE COLORADO S	NG ENGI Springs, C	NEER, INC. CO 80907	Page:1A Of Pages:7

MAJOR BASIN	SUB BASIN	AF	REA	BA	SIN	Tc MIN	in.	[/br	SOIL GRP	DEV. TYPE	0	С		OW 100-yr		FURN RIOD	
DAGIN	DASH	PLANIM READ	ACRES	LENGTH -FT	HEIGHT -FT		111./		ond				9p -CFS-	qp -CFS-		ears-	
FALCON	0-1	9.75	2.47	300	4.5	27			A	SF 5AC.	0.12	0.39					
			V=0.82	+480	1.3	+10											
						37	2.1	3.6					0.62	3.5	5	100	
HISTORIC	A	COGO	5.00	+525	9	+13											
			V=0.65			50	1.8	2.8	Α	R/L	0.08	0.35					
	TOTAL		7.47							MIX	0.093	0.362	1.25	7.6	5	100	
DEVELOPED	A	COGO	1.68	300	2.5	15.2			A	GRAVEL	0.59	0.70		м.	5	100	
			V=3.06	+300	7	+1.6											
						16.8	3.2	5.5					3.2	6.5	5	100	
	01 + A	(DP-1)	4.15	=400	8	+2	3.2	5.5	A	MIX	0.310	0.516					
			V=2.82			52	1.7	2.9					2.1	6.2	5	100	
																100	2 8
	В	COGO	0.66	. 370	2.4	16.4			A	GRAVEL	0.59	0.70	1.3	2.5	5 '	100	:
	C	COGO	2.30	300	4	14.5			A	GRAVEL	0.59	0.70				;	x - 1928)
			V=2.66	+340	6	+2.1										100	
						16.6	3.3	5.5			·		4.5	8.9	5	100	
	B+C			+360	8	+2.7				CD LIVE	0.50	0.70	5.0	10.4	5	100	ł.
3 		(DP-2)	2.96			19.3	3.0	5.1	A	GRAVEL	0.59	0.70	5.2	10.4	5	100	a s
	D	COGO	0.36	240	4.5	11.6	3.8	6.4	A	GRAVEL	0.59	0.70	0.8	1.6	• 3	100	e .roa - o
	B+C+D		V=2.22	+50		+0.4	2.0	C 1		CDAVEL	0.50	0.70	5.9	11.9	5	100	-
		(DP-3)	3.32	1010	0.1	19.7	3.0	5.1	A	GRAVEL	0.59	0.70	3.9	11.9	5	100	
	+0-1+A		7.47	+240	2.4	+2	17	2.0		MIX	0.424	0.598	5.5	12.5	5	100	•
						54	1.7	2.8	A	MIX	0.434	0.398	5.5	12.5	5	100	
HYDF PROJ: FALCON RATIONAL MET	STORAGE	SUB	UTATION BY: O.E. W ATE: 2/4/21	ATTS		I	OL	IVEF		ATTS, CON				R, INC.		GE 1 OF >	

an tha china an An tha china an	Design Procedure Fo	rm: Sand Filter (SF)	
Designer:	UD-BMP (Version 3.	07, March 2018)	Sheet 1 of 2
Company:	Olier E. Watts, Consulting Engineer, Inc.		_
Date:	December 15, 2023		- 3/
Project:	Falcon Storage		/ .
Location:			
1000110111			-
1. Basin Sto	rage Volume		Seep 6-17 Buckyp
	ve Imperviousness of Tributary Area, I _a if all paved and roofed areas upstream of sand filter)	I _a = 46.4 %	502 P 6-17 Butyl 0.598 - 0.50 0.65 - 0.50
B) Tribut	ary Area's Imperviousness Ratio (i = I _a /100)	i = 0.464	-0.257
	r Quality Capture Volume (WQCV) Based on 12-hour Drain Time CV= 0.8 * (0.91* i ³ - 1.19 * i ² + 0.78 * i)	WQCV = 0.16 waters	
D) Contri	ibuting Watershed Area (including sand filter area)	Area = <u>325,393</u> sq ft	$x = 5 = 64^{-2}$ + $40 = 46.4$
	r Quality Capture Volume (WQCV) Design Volume _{2V} = WQCV / 12 * Area	V _{wacv} = 4,265 cu ft	+40 = 46.4
	/atersheds Outside of the Denver Region, Depth of age Runoff Producing Storm	d ₆ = in	
	Vatersheds Outside of the Denver Region, r Quality Capture Volume (WQCV) Design Volume	Vwqcv other =cu ft	
H) User I	Input of Water Quality Capture Volume (WQCV) Design Volume if a different WQCV Design Volume is desired)	V _{WQCV USER} =cu ft	
2. Basin Ge	ometry		
A) WQC\	/ Depth	D _{wacv} = <u>3.0</u> ft	
	Filter Side Slopes (Horizontal distance per unit vertical, flatter preferred). Use "0" if sand filter has vertical walls.	Z = <u>3.00</u> ft / ft DIFFICULT TO MAIN	TAIN, INCREASE WHERE POSSIBLE
C) Minimu	um Filter Area (Flat Surface Area)	A _{Min} = <u>1887</u> sq ft	
D) Actual	Filter Area	A _{Actual} = 2100 sq ft	
E) Volum	e Provided	V _T = <u>11278</u> cu ft	
2 Eilter Mat		Choose One	
Filter Mat		18" CDOT Class B or C F	ilter Material
		O Other (Explain):	
4. Underdra	in System	r Choose One	-
A) Are un	derdrains provided?	YES O NO	
B) Under	drain system orifice diameter for 12 hour drain time		
	i) Distance From Lowest Elevation of the Storage Volume to the Center of the Orifice	y = 0.5 ft	
	ii) Volume to Drain in 12 Hours	Vol ₁₂ = 4,265 cu ft	
	iii) Orifice Diameter, 3/8" Minimum	D _o = 2 in	

int Anna Ro	Design Procedure F	orm: Sand Filter (SF)	
	Olliver Watts		Sheet 2 of
Designer: Company:	Oliver E Watts Consulting Engineer, inc		
)ate:	December 15, 2023		
Project:	Falcon Storage		
ocation:			
A) Is an	eable Geomembrane Liner and Geotextile Separator Fabric impermeable liner provided due to proximity ructures or groundwater contamination?	Choose One	
	utlet Works wribe the type of energy dissipation at inlet points and means of eying flows in excess of the WQCV through the outlet		

	POND)au vie	
GLEV	A-JE	V-(CE
35	2100	25625	D
36	3025		25625
37	4106	3565	6(280
38	6135	51505	11278.5

Required Area per Row (in²)

-												
			Depth at Outlet (ft)									
		1.0	1.5	2.0	2.5	3.0	3.5	4.0	4.5			
	2	15.04	7.71	5.10	3.76	2.95	2.41	2.02	1.73			
	1	7.52	3.86	2.55	1.88	1.48	1.21	1.01	0.87			
(t)	0.6	4.51	2.31	1.53	1.13	0.89	0.72	0.61	0.52			
(acre-ft)	0.4	3.01	1.54	1.02	0.75	0.59	0.48	0.40	0.35			
1222	0.2	1.50	. 0.77	.0.51	0.38	0.30	0.24	0.20.	0.17			
me	0.1	0.75~	0.39	0.26	0.19	0.15	0.12	0.10	0.09			
lo'	0.06	0.45 .	0.23	0.15	0.11	0.09	0.07	0.06	0.05			
2	0.04	0.30	0.15	0.10	0.08	0.06	0.05	0.04	0.03			
Design Volume	0.02	0.15	0.08	0.05	0.04	0.03	0.02	0.02	0.02			
ă	0.01	0.08	0.04	0.03	0.02	0.01	0.01	0.01	0.01			

A iea Q

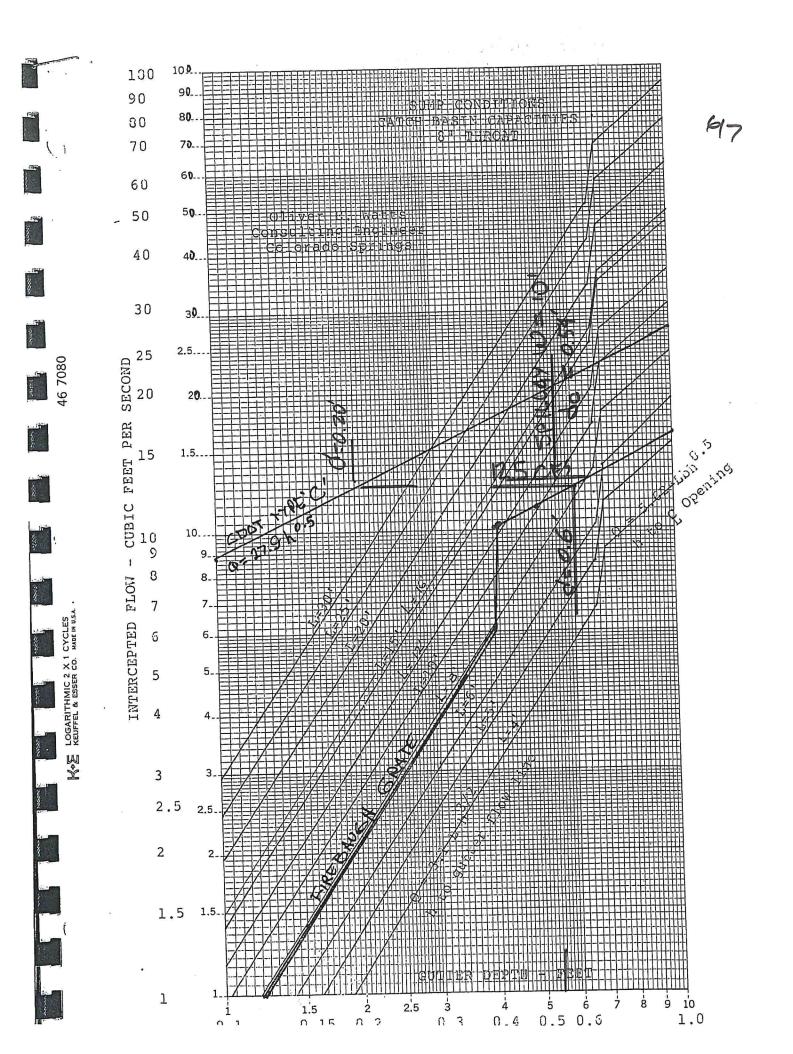
TABLE SB-1

0-1+ A-D WQCV 0.125 AF = 5445CF 0.3225 112 780 3/7

lole Diameter	Hole Diameter	Are	a per Row (in ²)	
(in)	(in)	n = 1	n = 2	n = 3
1/4	0.250	0.05	0.10	0.15
5/16	0.313	0.08	0.15	0.23
3/8	0.375	0.11	0.22	0.33
7/16	0.438	0.15 -	0.30 .	0.45
1/2	0.500	0.20	0.39	0.59
9/16	0.563	0.25	0.50	0.75
5/8	0.625	0.31	0.61	0.92
11/16	0.688	(937)	0.74	1.11
3/4	0.750	0.44	0.88	1.33
7/8	0.875	0.60	1.20	1.80
1	1.000	0.79	1.57	2.36
1 1/8	1.125	0.99	1.99	2.98
1 1/4	1.250	1.23	2.45	3.68
1 3/8	1.375	1.48	2.97	4.45
1 1/2	1.500	1.77	3.53	5.30
1 5/8	1.625	2.07	4.15	6.22
1 3/4	1.750	2.41	4.81	7.22
1 7/8	1.875	2.76	5.52	8.28
2	2.000	3.14	6.28	9.42

TABLE SB-2

City of Colorado Springs Stormwater Quality Figure SB-2 Outlet Sizing Application Techniques and Maintenance Requirements



02 1523 FALCON STORAGE ONFALL SWALE DEWAKTS 12/13/2 Q= 125 CFS Q= 1.4 26 AR 3512 5= 1/5312= 0.0186 A = 16 d WP= 16.03 d x Z 6 * 60 0 R Upper 9.0070 0.378' 5.78 N=0.035 4.00 0.25 Half 8.00 16.0312 0.9 3.61 0.50 A-A 12.30 25.65 0.499 0.30 46.6 16.0312 0.999 22.1 0.50 8.00 4.30 9.618 17.5 0.30 - National Brand 12.2 6.4725 0.20 3,20 F=6.72 1224 = 6.733 0.21 3.36 14.37 B. a 56 0.25 4.00 A=62 Aower. wp=ztod Halt 3 5=1/92=0.010) B-B 7.60 1.30 0.9487 1.897 0.3 2.2402 3012 12.84 3.162 3.00 0.5 8.99 2.9487 22136 0.35 2.10 0.9487 10.27 0.40 2529 2.40 0.9487 12.58 T= 2.94 C.P. 0 3.0.90 2.94

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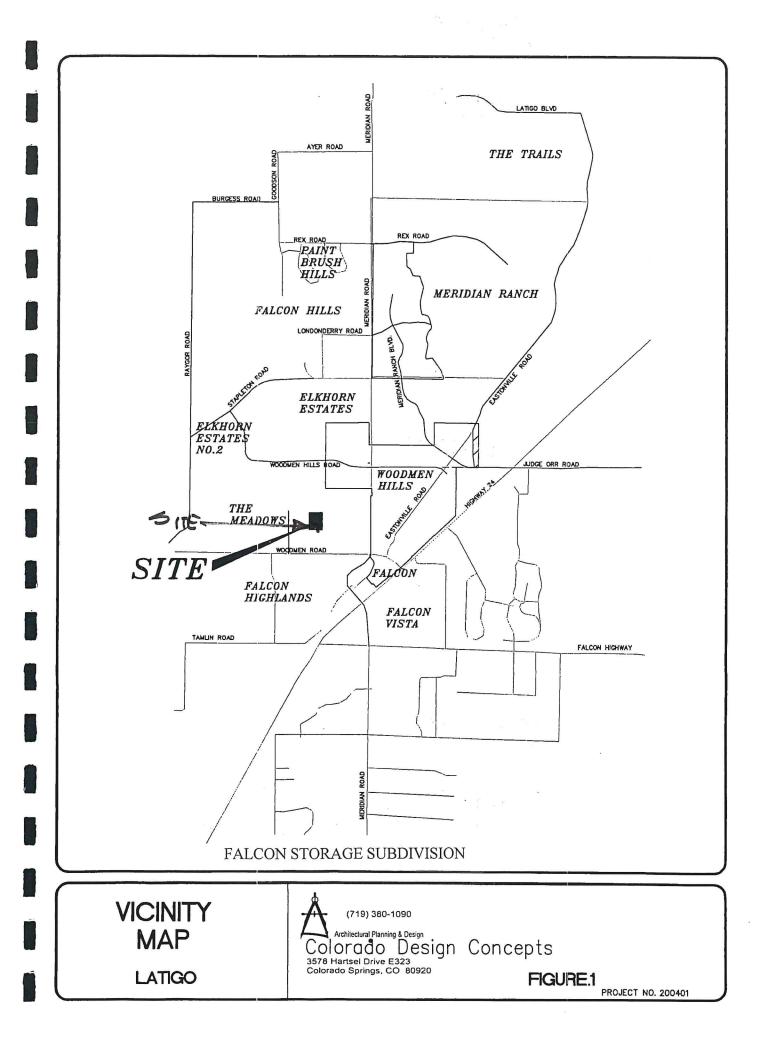
$Q = \frac{0.463}{n}$	D ^{8/3} S ¹ 2
·••	

(Accession of the second se

Q=KS¹2

		D 8/3		K		
IAMETER	AREA - FT2 -	- FT -	N=0.010	N=0.013	N = 0.024	N=0.026
-IN	-F12-	-1.1-	11 0.010			
-						
	0 02102	0.008413	0.3895			
2	0.02182	0.053420	2.4733			、
4	0.08727	0.157500	7.2922	5.609		
6	0.19630	0.339200	15.7050	12.081		
8	0.34910	0.615000	28.4745	21.903		
10	0.54540	<u> </u>	46.3000	35.615		
12	0.78540	1.813100	83.9465	64.574	i= = =	
15	1.22720	2.948300	136.5100	105.000	56.88	52.50
18	1.76710	4.447400	205.9100	158.400	85.80	79.20
21	2.40530	6.349600	293.9900	226.140	122.49	113.07
24	3.14160	8.692700	402.4700	309.590	167.70	154.79
27	3.97610	11.512600	533.0300	410.030	222.10	205.02
30	4.90870	14.844100		528.680		
33	5.93960	18.720800	866.7700	666.700	361.20	333.30
36	7.06860	23.175100		825.400		
39	8.29580	28.238900		1005.000	544.80	502.50
42	9.62110	40.317500		1436.000	777.80	718.00
48	12.56640	55.195000		1966.000	1065.00	983.00
54	15.90430	73.100400		2604.000	1410.00	1302.00
60	19.63500	94.254200		3357.000	1818.00	1678.00
66	23.75830	118.869400		4234.000	2293.00	2117.00
72	28.27430	147.152900		5241.000	2839.00	2620.00
78	33.18310	179.306000	+	6386.000	3459.00	3193.00
84	38.48450	215.524500		7676.000	4158.00	3838.00
90	44.17860			9118.000	4939.00	4559.00
96	50.26550	256.000000		12480.000	6761.00	6140.00
108	63.61730	350.466600		16530.000	8954.00	8265.00
120	78.53980	464.158900		10000.000		

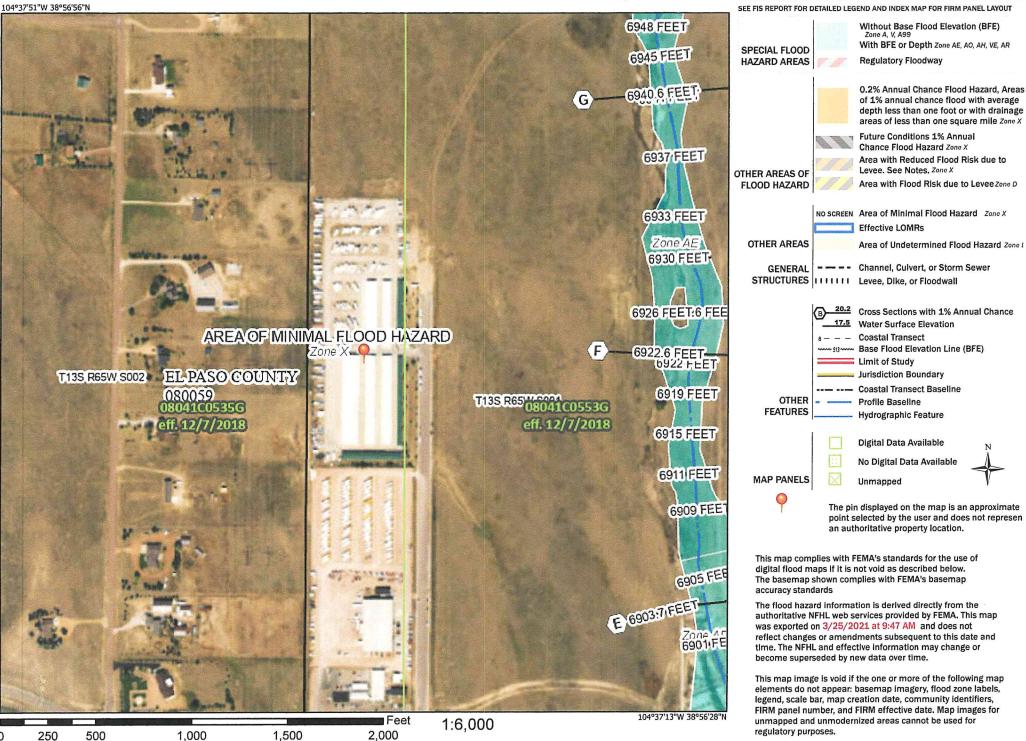
Oliver E. Watts Consulting Engine Colorado Springs



National Flood Hazard Layer FIRMette



Legend



Reseman IISGS National Man Orthoimagery Data refreshed October 2020

NOTES TO USERS

This map is for use in administering the National Flood Insurance Program. It does not necessarily identify all areas subject to flooding, particularly from local drainage sources of small size. The community map repository should be consulted for possible updated or additional flood hazard information.

To obtain more detailed information in areas where Base Flood Elevations (BFEs) and/or floodways have been determined, users are encouraged to consult the Flood Profiles and Floodway Data and/or Summary of Sillwater Elevations tables conlained within the Flood Insurance Study (FIS) report that accompanies this FIRM. Users should be aware that BFEs are intended for flood Insurance raing purposes only and should not even and are source of flood insurance raing purposes only and should not be avera that BFEs are intended for flood Insurance raing purposes only and should not be avera that BFEs are intended for flood Insurance raing purposes only and should not be used as the sole source of flood elevation information. Accordingly, flood televation data presented in the FIS report should be utilized in conjunction with the FIRM for purposes of construction and/or floodplain management.

Coastal Base Flood Elevations shown on this map apply only landward of 0.0' North American Verical Datum of 1988 (NAVD88). Users of this FIRM should be oware that coastal flood elevations are also provided in the Summary of Silwater Elevations table in the Flood Insurance Study report for this jurisdicion. Elevations shown in the Summary of Silwater Elevations table should be used for construction and/or floodplain management purposes when they are higher than the elevations shown on this FIRM.

Boundaries of the floodways were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations with regard to requirements of the National Flood Insurance Program. Floodway widths and other pertinent floodway data are provided in the Flood Insurance Study report for this jurisdiction.

Certain sreas not in Special Flood Hazard Areas may be protected by flood control structures. Refer to section 2.4 "Flood Protection Measures" of the Flood Insurance Study report for information on flood control structures for this jurisdiction.

The projection used in the preparation of this map was Universal Transverse Mercator (UTM) zone 13. The horizontal datum was NAD83, GRS80 spheroid. Differences in datum, spheroid, projection or UTM zones zones used in the production of FIRMs for adjacent jurisdictions may result in slight positional differences in map features across jurisdiction boundaries. These differences do not affect the accuracy of this FIRM.

Rood elevations on this map are referenced to the North American Vertical Datum of 1988 (NAVD86). These flood elevations must be compared to structure and ground elevations referenced to the same vertical datum. For information regarding conversion between the National Geodetic Vertical Datum of 1929 and the North American Vertical Datum of 1988, visit the National Geodetic Survey verbiste at http://www.ngs.noaa.gov/ or contact the National Geodetic Survey at the following address:

NGS Information Services NOAA, NI/NGS12 National Geodetic Survey SSMC-3, #9202 1315 East-West Highway Silver Spring, MD 20910-3282

To obtain current elevation, description, and/or location information for bench marks shown on this map, please contact the Information Services Branch of the Nationa Geodetic Survey at (301) 713-3242 or visit its website at http://www.ngs.ncaa.gov/.

Base Map information shown on this FIRM was provided in digital format by EI Paso County, Colorado Springs Utilities, City of Fountain, Bureau of Land Management, National Oceanic and Amespheric Administration, United States Goological Survey, and Anderson Consulting Engineers, Inc. These data are current as of 2006.

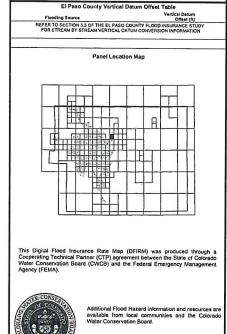
This map reflects more detailed and up-to-date stram channel configurations and floodplain delineatione than those shown on the previous FIRM for this juriadicton. The floodplain delineatione than those shown on the previous FIRM for this juriadicton. The floodplain and floodways that were transferred from the previous FIRM may have been adjusted to conform to these new stream channel configurations. As a result, the Flood Profess and Floodway Data tables in the Flood Insurance Study Report (which contains authoritative hydraulic data) may reflect stream channel distances that differ from what is shown on this map. The profile baselines depicted on this map represent the hydraulic modeling baselines that match the flood profiles baselines may deviate significantly from it the FIS report. As a result, the profile baselines may deviate significantly from the new base map channel representation and may appear outside of the floodplain.

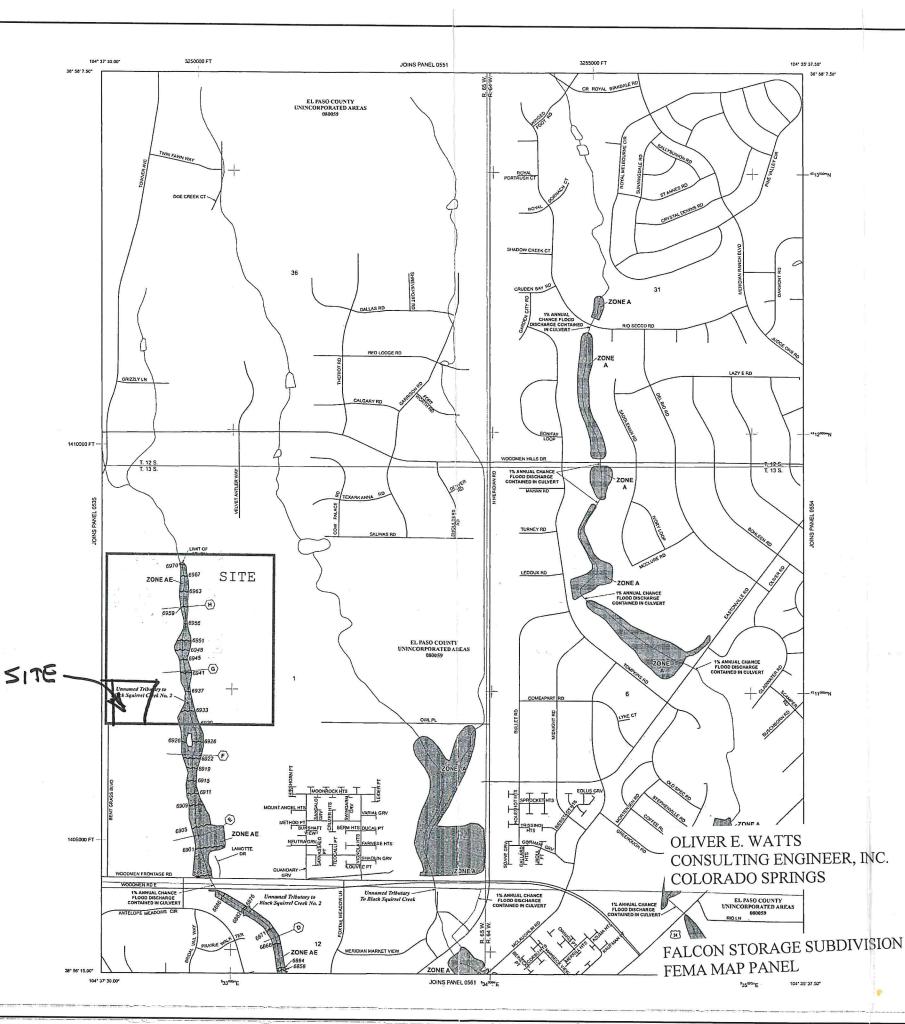
Corporate limits shown on this map are based on the best data available at the time of publication. Because changes due to annexations or de-annexations may have occurred utler this map was published, may users should contact appropriate community officials to verify current corporate limit locations.

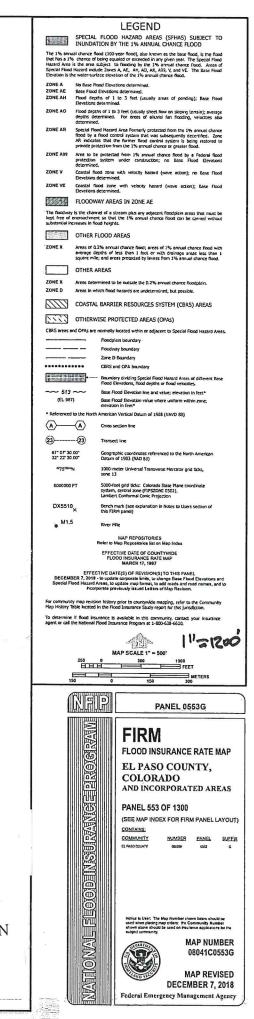
Please refer to the separately printed Map Index for an overview map of the county showing the layout of map panels; community map repository addresses; and a Listing of Communities table containing National Flood Insurance Program dates for sach community as well as a listing of the panels on which each community is located.

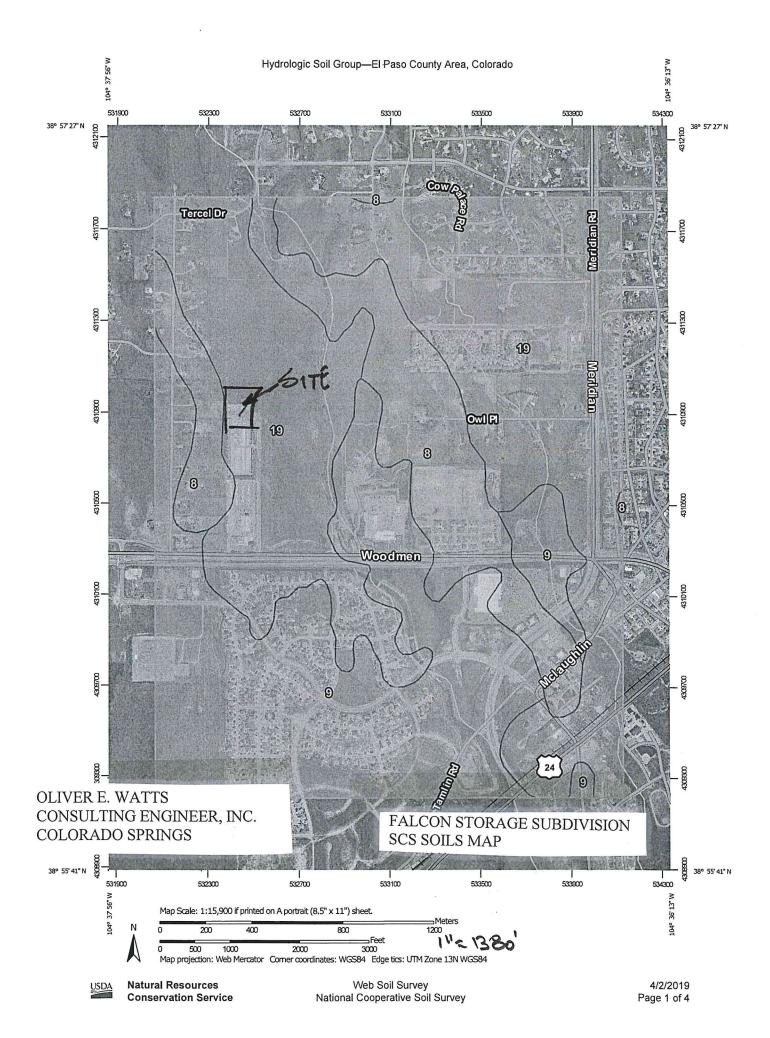
Contact FEMA Map Service Center (MSC) via the FEMA Map Information eXchange (FMIX) 1477-336-2627 for information on available products associated with this FIRM. Available products may include previously issued Letters of Map Change, a Flood Insurance Study Report, and/or digital versions of this map. The MSC may also be reached by Fax at 1-600-358-9620 and its websile at http://www.msc.fema.gov/.

If you have questions about this map or questions concerning the National Flood Insurance Program in general, please call 1-877-FEMA MAP (1-877-336-2527) or visit the FEMA website at http://www.fema.gov/businessinfip.









EL PASO COUNTY AREA, COLORADO

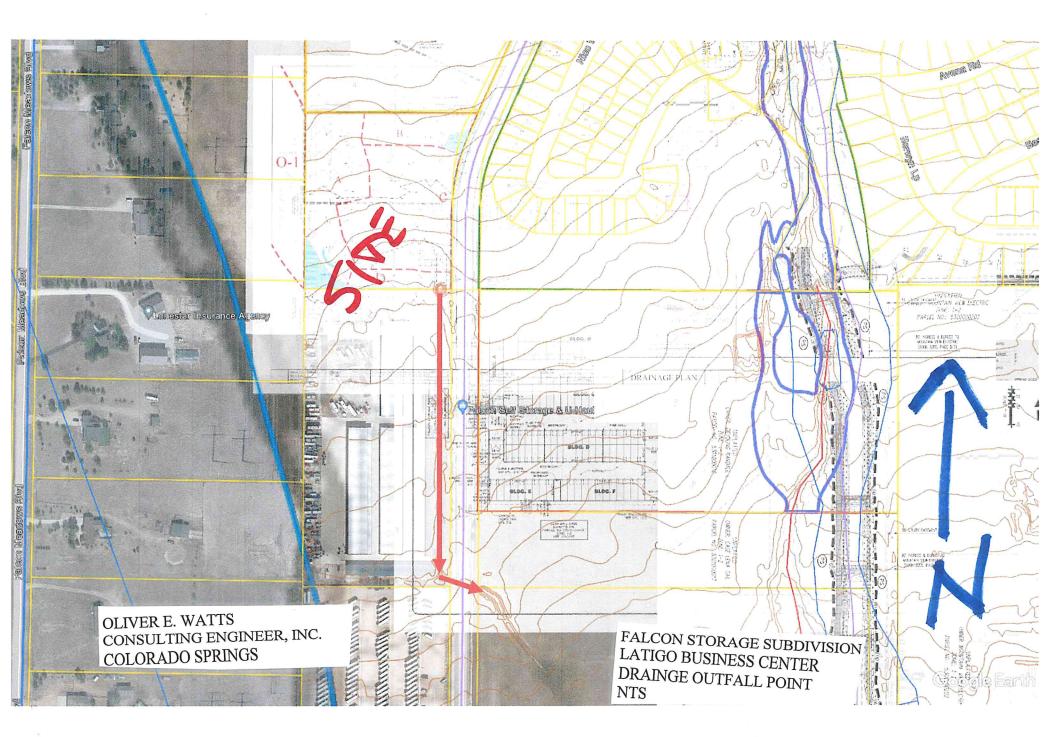
TABLE 16.--SOIL AND WATER FEATURES

Absence of an entry indicates the feature is not a concern. See "flooding" in Glessary for definition of terms as "rare," "brief," and "very brief." The symbol > means greater than]

	11		Flooding		Bedrock			
Soil name and map symbol	Hydro- logic group	Frequency	Duration	Months	Depth	Hardness	Potential frost action	
lamosa: 1	с	Frequent	Brief	May-Jun	<u>In</u> >60		High.	
scalon: 2, 3	В	None			>60		Moderate:	
adland: 4	D							
<pre>ijou: 5, 6, 7</pre>	В	None			>60		Low.	
<pre>3lakeland: 8</pre>	A	None			>60		Low.	
¹ 9: Blakeland part-	A	None	·		>60		Low.	
Fluvaquentic Haplaquolls part	D	Common	Very brief	Mar-Aug	>60		High.	
31endon: 10	В	None			>60		Moderate.	
Bresser: 11, 12, 13	B	None			>60		Low.	
3russett: 14, 15	В	None	· · · · · · · · · · · · · · · · · · ·		>60		Moderate.	
Chaseville: 16, 17	A	None			>60		Low.	
¹ 18: Chaseville part	A	None			>60		Low.	
Midway part	D	None			10-20	Rippable	Moderate.	
Columbine: 19	$\left(\right)$	None to rare			>60		Low.	
Connerton: ¹ 20: Connerton part-	В	None			>60		High.	
Rock outcrop part	D							
Cruckton: 21	В	None			>60		Moderate.	
Cushman: 22, 23	с	None			20-40	Rippable	Moderate.	
¹ 24: Cushman part	С	None	,		20-40	Rippable	Moderate.	
Kutch part	с	 None			20-40	Rippable	Moderate.	
Elbeth: 25, 26	В	None			>60		Moderate.	
¹ 27: Elbeth part	В	None			>60		Moderate.	

See footnote at end of table.

MSV



Land Use or Surface	Percent						Runoff Co	effidents					
Characteristics	Impervious	2-year		5-year		10-year		25-year		50-year		100-year	
		HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D
Business												110 G Flas	noo cab
Commercial Areas	95	0.79	0.80	0.81	0.82	0.83	0.84	0.85	0.87	0.87	0.88	0.88	0.89
Neighborhood Areas	70	0.45	0.49	0.49	0.53	0.53	0.57	0.58	0.62	0.60	0.65	0.62	0.68
Residential													
1/8 Acre or less	65	0.41	0.45	0.45	0.49	0.49	0.54	0.54	0.59	0.57	0.62	0.59	0.00
1/4 Acre	40	0.23	0.28	0.30	0.35	0.36	0.42	0.42	0.50	0.46	0.52		0.65
1/3 Acre	30	0.18	0.22	0.25	0.30	0.32	0.38	0.42	0.30	0.48	0.54	0.50	
1/2 Acre	25	0.15	0.20	0.22	0.28	0.30	0.36	0.35	0.47	0.43	0.52	0.47	0.57
1 Acre	20	0.12	0.17	0.20	0.26	0.27	0.34	0.35	0.46	0.41	0.51	0.46	0.55
ndustrial													
Light Areas	80	0.57	0.60	0.59	0.63								
Heavy Areas	90	0.71	0.30	0.39	0.63	0.63	0.66	0.66	0.70	0.68	0.72	0.70	0.74
								0170	0.00	0.00	0.02	0.81	0.65
Parks and Cemeteries	7	0.05	0.09	0.12	0.19	0.20	0.29	0.30	0.40	0.34	0.46	0.39	0.52
laygrounds	13	0.07	0.13	0.16	0.23	0.24	0.31	0.32	0.42	0.37	0.48	0.41	0.54
Railroad Yard Areas	40	0.23	0.28	0.30	0.35	0.36	0.42	0.42	0.50	0.46	0.54	0.50	0.58
Indeveloped Areas													
Historic Flow Analysis	2												
Greenbelts, Agriculture	2	0.03	0.05	0.09	0.16	0.17	0.26	0.26	.0.38	0.31	0.45	0.36	0.51
Pasture/Meadow	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50
Forest	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50
Exposed Rock	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0,95	0.95	0.96	0.96
Offsite Flow Analysis (when landuse is undefined)	45	0.26	0.31	0.12	0.77								
and die is and ennedy		0.20	0.31	0.32	0.37	0.38	0.44	0.44	0.51	0.48	0.55	0.51	0.59
treets	•												
Paved	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Gravel	80	0.57	0.60	0.59	0.63	0.63	0.66	0.66	0.70	0.53	0.93	0.96	0.96
						5.05	0.00	3,00	0.70	0.00	0.72	0.70	0.74
rive and Walks	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
loofs	90	0.71	0.73	0.73	0.75	0.75	0.77	0.78	0.80	0.80	0.82	0.81	0.83
awns	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50

Table 6-6. Runoff Coefficients for Rational Method (Source: UDFCD 2001)

3.2 Time of Concentration

One of the basic assumptions underlying the Rational Method is that runoff is a function of the average rainfall rate during the time required for water to flow from the hydraulically most remote part of the drainage area under consideration to the design point. However, in practice, the time of concentration can be an empirical value that results in reasonable and acceptable peak flow calculations.

For urban areas, the time of concentration (t_c) consists of an initial time or overland flow time (t_i) plus the travel time (t_i) in the storm sewer, paved gutter, roadside drainage ditch, or drainage channel. For nonurban areas, the time of concentration consists of an overland flow time (t_i) plus the time of travel in a concentrated form, such as a swale or drainageway. The travel portion (t_i) of the time of concentration can be estimated from the hydraulic properties of the storm sewer, gutter, swale, ditch, or drainageway. Initial time, on the other hand, will vary with surface slope, depression storage, surface cover, antecedent rainfall, and infiltration capacity of the soil, as well as distance of surface flow. The time of concentration is represented by Equation 6-7 for both urban and non-urban areas.

$$t_c = t_i + t_i$$

Where:

 t_c = time of concentration (min)

 t_i = overland (initial) flow time (min)

 t_t = travel time in the ditch, channel, gutter, storm sewer, etc. (min)

3.2.1 Overland (Initial) Flow Time

The overland flow time, t_i , may be calculated using Equation 6-8.

$$t_{i} = \frac{0.395(1.1 - C_{s})\sqrt{L}}{S^{0.33}}$$
(Eq. 6-8)

.5 · •

Where:

 t_i = overland (initial) flow time (min)

- C_5 = runoff coefficient for 5-year frequency (see Table 6-6)
- L =length of overland flow (300 ft <u>maximum</u> for non-urban land uses, 100 ft <u>maximum</u> for urban land uses)

S = average basin slope (ft/ft)

Note that in some urban watersheds, the overland flow time may be very small because flows quickly concentrate and channelize. ·:::

3.2.2 **Travel Time**

For catchments with overland and channelized flow, the time of concentration needs to be considered in combination with the travel time, t_i , which is calculated using the hydraulic properties of the swale, ditch, or channel. For preliminary work, the overland travel time, t_0 , can be estimated with the help of Figure 6-25 or Equation 6-9 (Guo 1999).

$$V = C_{..}S_{...}^{0.5}$$

Where:

V = velocity (ft/s)

 C_{ν} = conveyance coefficient (from Table 6-7)

 S_{w} = watercourse slope (ft/ft)

di S

(Eq. 6-7)

(Eq. 6-9)

Type of Land Surface	C_{v}
Heavy meadow	2.5
Tillage/field	5
Riprap (not buried)*	6.5
Short pasture and lawns	7
Nearly bare ground	10
Grassed waterway	15
Paved areas and shallow paved swales	20

Table 6-7. C	Conveyance	Coefficient,	C_{ν}
--------------	------------	--------------	-----------

For buried riprap, select C_v value based on type of vegetative cover.

The travel time is calculated by dividing the flow distance (in feet) by the velocity calculated using Equation 6-9 and converting units to minutes.

The time of concentration (t_c) is then the sum of the overland flow time (t_i) and the travel time (t_i) per Equation 6-7.

3.2.3 First Design Point Time of Concentration in Urban Catchments

en seguire

Using this procedure, the time of concentration at the first design point (typically the first inlet in the system) in an urbanized catchment should not exceed the time of concentration calculated using Equation 6-10. The first design point is defined as the point where runoff first enters the storm sewer system.

$$t_c = \frac{L}{180} + 10$$

Where:

 t_c = maximum time of concentration at the first design point in an urban watershed (min)

L = waterway length (ft)

Equation 6-10 was developed using the rainfall-runoff data collected in the Denver region and, in essence, represents regional "calibration" of the Rational Method. Normally, Equation 6-10 will result in a lesser time of concentration at the first design point and will govern in an urbanized watershed. For subsequent design points, the time of concentration is calculated by accumulating the travel times in downstream drainageway reaches.

3.2.4 **Minimum Time of Concentration**

If the calculations result in a t_c of less than 10 minutes for undeveloped conditions, it is recommended that a minimum value of 10 minutes be used. The minimum t_c for urbanized areas is 5 minutes.

3.2.5 Post-Development Time of Concentration

As Equation 6-8 indicates, the time of concentration is a function of the 5-year runoff coefficient for a drainage basin. Typically, higher levels of imperviousness (higher 5-year runoff coefficients) correspond to shorter times of concentration, and lower levels of imperviousness correspond to longer times of

(Eq. 6-10)

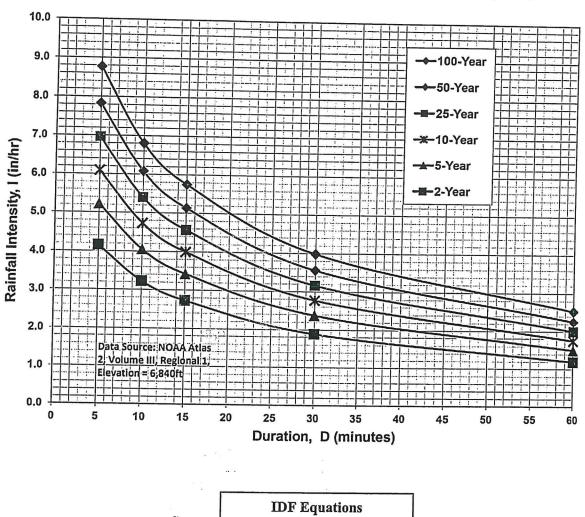
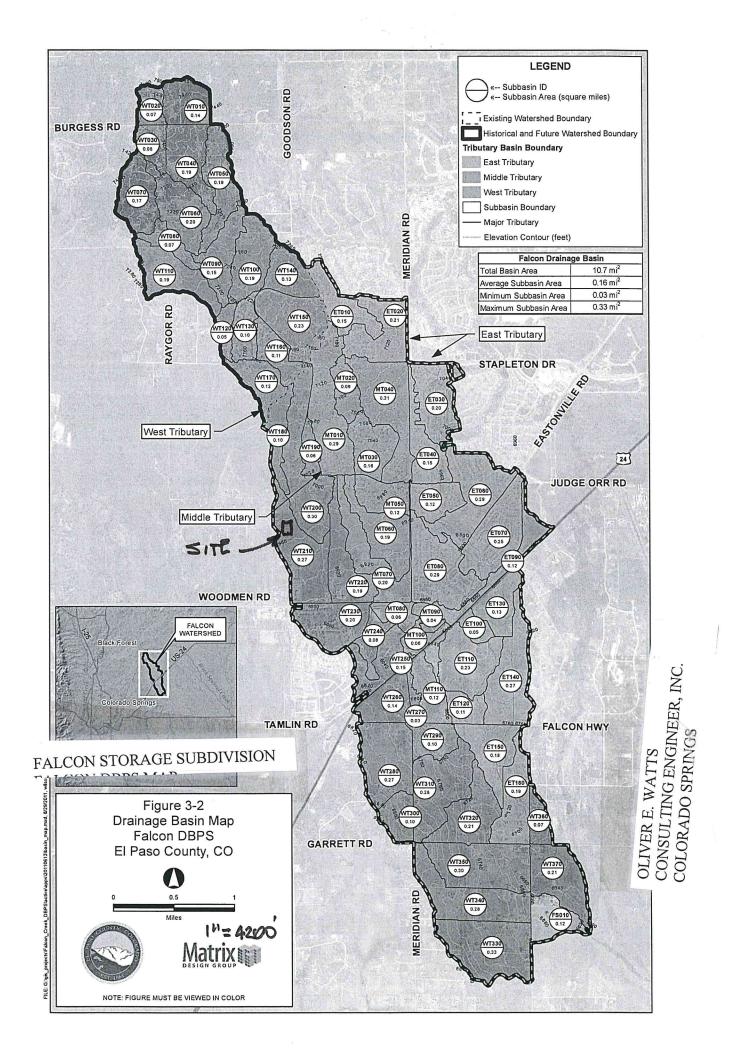
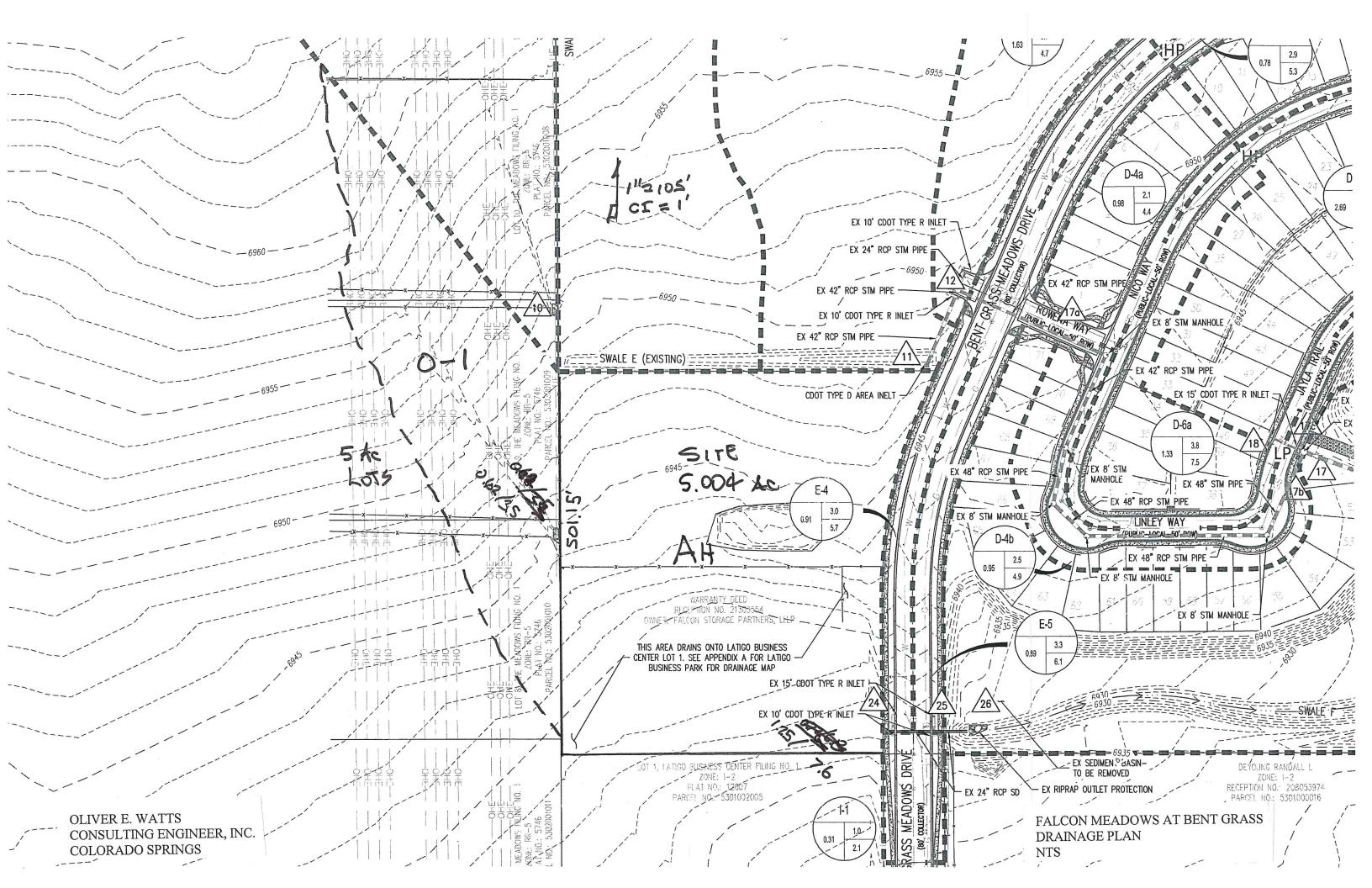
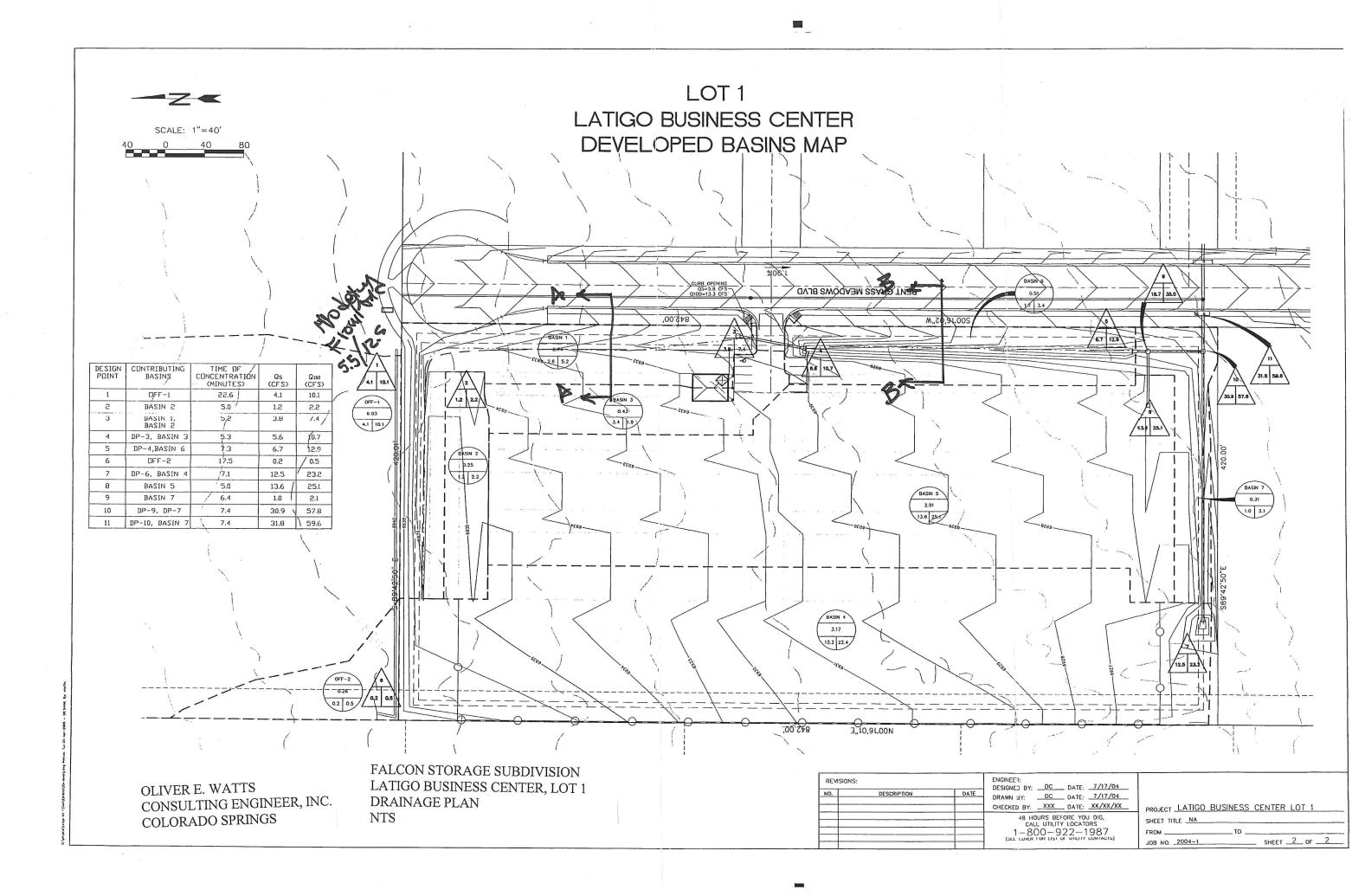


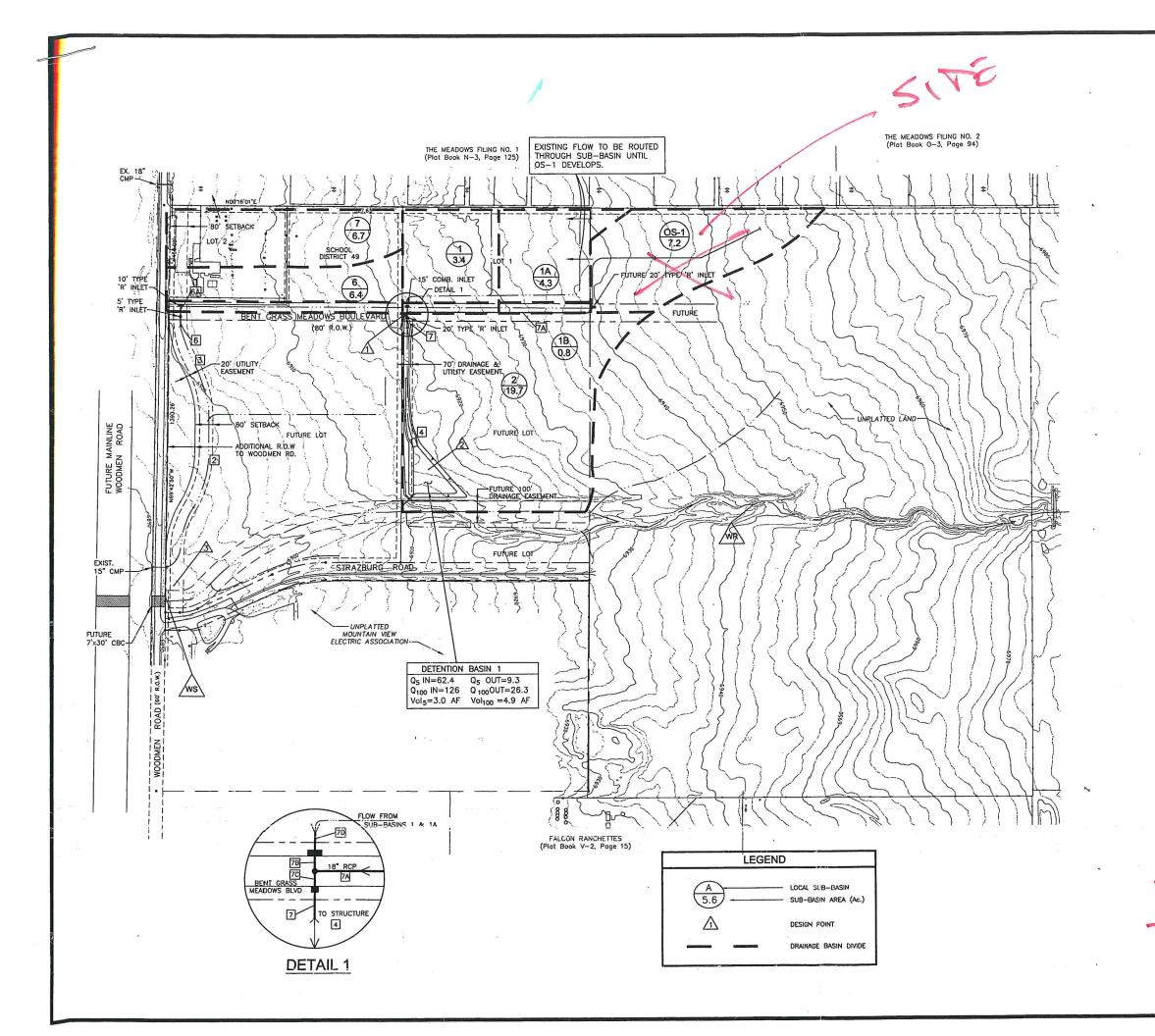
Figure 6-5. Colorado Springs Rainfall Intensity Duration Frequency

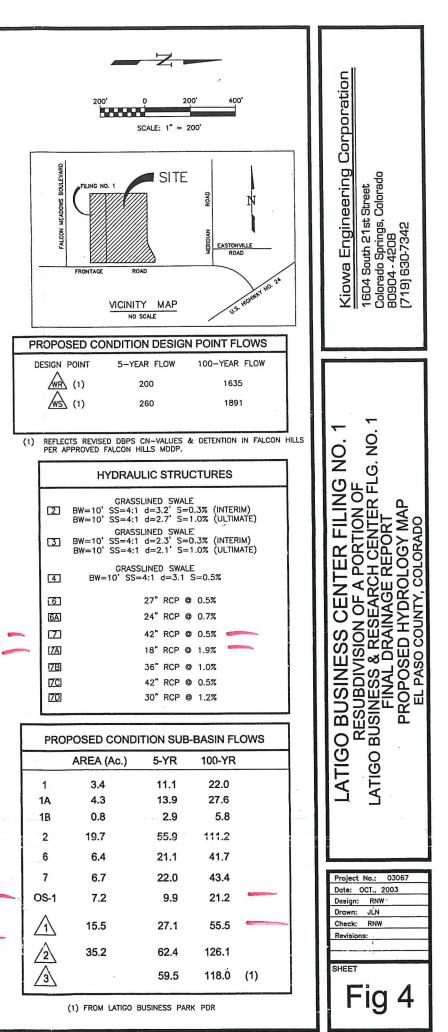
IDF Equations
$I_{100} = -2.52 \ln(D) + 12.735$
$I_{50} = -2.25 \ln(D) + 11.375$
$I_{25} = -2.00 \ln(D) + 10.111$
$I_{10} = -1.75 \ln(D) + 8.847$
$I_5 = -1.50 \ln(D) + 7.583$
$I_2 = -1.19 \ln(D) + 6.035$
Note: Values calculated by equations may not precisely duplicate values read from figure.











03067 FIG4.dwg/Mar 09, 200

