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PRELIMINARY AND FINAL DRAINAGE PLAN AND REPORT

FALCON STORAGE SUBDIVISION

PART OF THE SW1/4 SECTION 1, T.13S.. R.65W. OF THE 6TH P.M.

EL PASO COUNTY

February 4, 2021

Revised November 23, 2022

PCD File No. PPR2232

Please also add PCD File No. MS232 Prepared for

Falcon Storage Partners LLLP

Oliver E. Watts, Consulting Engineer, Inc. Colorado Springs, Colorado

Due to the type and quantity of comments provided additional comments may be generated on the resubmittal.

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OLIVER E. WATTS, PE-LS

OLIVER E. WATTS, CONSULTING ENGINEER, INC. CIVIL ENGINEERING AND SURVEYING 614 ELKTON DRIVE COLORADO SPRINGS, COLORADO 80907 (719) 593-0173 fax (719) 265-9660 <u>olliewatts@aol.com</u> Celebrating over 41 years in business

November 23, 2022

El Paso County Planning and Community Development 2880 International Circle Colorado Springs, CO 80910

ATTN: Joshua Palmer, P.E.

SUBJECT: Preliminary and Final Drainage Plan and Report Falcon Storage Subdivision

Transmitted herewith for your review and approval is the drainage plan and report for The Falcon Storage Subdivision in El Paso County. This report will accompany the development plan and subdivision plat submittal. This report has been revised in accordance with your review comments.

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Please contact me if I may provide any further information.

Oliver E. Watts, Consulting Engineer, Inc.

BY:

Oliver E. Watts, President

<u>FALCON STORAGE SUBDIVISION</u> <u>DRAINAGE REPORT</u> <u>TABLE OF CONTENTS</u>

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Drainage Report 5 pages Computations, 7 pages Vicinity Map FEMA Panel No. 08041C0553 G SCS Soils Map and Interpretation Sheet Backup Information, 4 sheets Falcon DBPS Map Drainage Plan, Falcon Meadows at Bent Grass Drainage Plan, Latigo Business Center Drainage Plan, Dwg 02-5523-04

FALCON STORAGE SUBDIVISION DRAINAGE REPORT <u>REFERENCES</u>

City-County Drainage Criteria, current edition Fema Firm Insurance Rate Map El Paso County Soils Survey, SCS Falcon Drainage Basin Planning Study Drainage Report, Falcon Meadows at Bent Grass Drainage Report, Latigo Business Center, Lot 1

1. ENGINEER'S STATEMENT:

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the County for drainage reports and said report is in conformity with the applicable master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.

Oliver E. Watts, Consulting Engineer, Inc.

Oliver E. Watts Colo

Colo. PE-LS No. 9853

2. OWNERS / DEVELOPER'S STATEMENT:

I the owner / developer have read and will comply with all of the requirements specified in this drainage report and plan.

Falcon Storage Partners LLLP

By: _____ Richard Graham 4615 Northpark Drive Colorado Springs, CO 80918

Date

date

3. EL PASO COUNTY:

Filed in accordance with the requirements of the El Paso Land Development Code, Drainage Criteria Manual Volumes 1 and 2, and the Engineering Criteria Manual, as amended.

Joshua Palmer, P.E., County Engineer / ECM Administrator date

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Conditions:

Filing 1

4. LOCATION AND DESCRIPTION:

The Falcon Storage Subdivision is located in the Latigo Business Center development of El Paso County as shown on the enclosed vicinity map. Occupying a portion of the West half of Section 1, Township 13 South, Range 65 West of the 6th P.M., totaling 5.004 acres. It is located in the Falcon Drainage Basin as shown on the enclosed basin map. It lies west of Bent Grass Meadows Drive north of the Latigo Business Center as shown on the enclosed drainage plan. The site will be developed into an RV Storage site as shown on the enclosed drainage plan, as an expansion to the one in the Latigo Business Center, both owned by the developer.

5. FLOOD PLAIN STATEMENT:

This subdivision is not within the limits of a flood plain or flood hazard area, according to FEMA map panel number 08041C0553 G, dated December 7, 2018, a copy of which is enclosed for reference.

6. METHOD AND CRITERIA:

The method used for all computations is that specified in the City-Cou Manual, using the rational method for areas of the size of the developr enclosed for reference and review. Pertinent portions of the criteria are

The soils in the subdivision have been mapped by the local USDA/SC interpretation sheet are enclosed for reference. All soils in this area ar within the development area.

Please see comments on the drainage plan regarding the conveyance of flows from the basins into the pond as portions of each of the basins do not reach the pond. Elaborate in your description of each of the basins and how the flow is conveyed to the pond and/or subsequent basin that will convey the flow to the pond.

7. DESCRIPTION OF RUNOFF:

A. Drainage Inflows: The drainage Report for Falcon Meadows at Bent Grass indicates an existing drainage swale above the north boundary to divert runoff from this site and route it to Bent Grass Meadows and then past this development in Bent Grass Meadows Drive to outfall points to an existing detention pond across the street. A copy of this drainage plan is enclosed. Also shown on this map is that portion of the Meadows Filing No. 1 that drains 0.62 cfs / 3.5 cfs (5-year / 100-year runoffs) into this subdivision along the westerly boundary, and it indicates the historic undeveloped runoff of the site, totaling 1.25 cfs / 7.6 cfs at the lowest (southeast) portion of the subdivision.

B. Interior Routing: The area will be graded to conform to the existing topography shown on the drainage plan. The property has been rough graded, which complies with the historic runoff pattern. Minor grading is indicated which is intended to contain the runoff into the interior drive isle street network. The site will be graded to route and contain all runoff within the private north-south streets, terminating at the south boundary. The westerly street (Basin A) will develop 4.1 cfs \ 11.8 cfs (5-year / 100-year runoffs) near the in the southwest corner of the plat. Basins B, C, and D will develop 5.9 cfs / 11.9 cfs in the easterly street near the southeast corner. The total outfall into the detention pond near the southeast corner is 5.5 cfs/12.5 cfs.

C. Detention Storage: At the proposed outfall point a detention pond is proposed Please state that. sized for sedimentation basins to be used during the construction period and converted into a sand filter basins upon completion. The basin will contain 13320 CF (at 1800 CF per acre). An 8-inch riser pipe is used as an outlet, with holes drilled as computed to detain the runoff as required. One

Please identify these as basins O-1 and AH in the narrative as shown on the drainage plan.

Temporary Sediment

6

singular

 IT
 18-inch (minimum) filter layer

 Falcon Storage Subdivision
 Storage Subdivision

4.1 cfs per the excerpt provided. revise accordingly.

Reliminary and Final Drainage Plan and Report foot of freeboard is provided with a spillway that will pass the 100-year runoff. Details are shown on the enclosed drainage plan. Following construction the basin will be modified to a sand filter basin, with one foot of sand in the bottom. A 4-inch underdrain will drain into the grated inlet outlet structures set at the WQCV level, and sized for the 100-year runoff. An orifice plate will be provided on the end of the underdrain with an orifice sized for the installation. Detention basin

slotted

Temporary Sediment

Assign a name/number to all PBMPs and then update all submitted text and drawings accordingly with consistent labeling throughout (example: "Pond A" or "Pond 1").

C. Outfall Point: Discharge from the subdivision will be into existing north-south street of Lot 1 of the Latigo Business Center. Some minor construction is shown along the north boundary of Lot 1. The two properties are under common ownership. The drainage plan for this property is enclosed. This report indicated two existing discharges: 0.2 cfs / 0.5 cfs near the southwest corner and 0.1 cfs / 10.1 cfs over the remaining south frontage.

WATER QUALITY

Water quality facilities will be provided as described above.

stage-storage tables are included for each basin.

FOUR STEP PROCESS

Per the drainage plan the spillway is located in the landscape strip along Bentgrass. The outfall pipe is not shown on the plan. Please clarify where the outfall is and where the developments

please revise.

The following process has been followed to minimize adverse flow will be ultimately conveyed to.

<u>Runoff Reduction:</u> The scope of the development has been minimized consistent with zoning requirements to present the minimum footprint in providing a RV Storage development. The undisturbed portions are to be landscaped to reduce the impervious percent. Show these locations on the plane.

Treat and Slowly Release: Detention storage is being provided downstream by others with sub regional facilities. Identify that detention/WQCV is being provided by the sand filter detention pond as identified above.

<u>Channel Stabilizing</u>: The site will be graded to route the runoff over improved street installations to provide channel stabilization in the natural erosive material over the site. Discharge from the site will be into adjacent and downstream facilities in accordance with the master drainage basin plan for the Falcon drainage basin and previously approved subdivision drainage reports. Copies of each plan are enclosed. There will be no adverse affect on downstream developments as a result of this subdivision

Source Controls: This is a RV Storage site, so source control problems will be a minimum. During construction, standard site specific state of revise the 4-step headings to match ECM Appendix 1.7.2, (Runoff reduction, stabilize

Item No. Description Quantity Unit Cost Cost \$4000.00 \$4000.00 Sand Filter Basin 1 ea 1 2 Grated inlet 1800.00 1800.00 1 ea 3 24" CMP drainage pipe 1051 40.00 4200,00 Subtotal Construction Cost \$ 10,000.00 Engineering 10% 1,000.00 These costs do not Please show on the match the FAE

drainage plan

7

8. COST ESTIMATE:

drainage ways, provide WQCV, Consider need for industrial and Commercial BMPs).



The underdrain system should be placed within an 5-inch-thick section of CDOT Class C filter

As the subdivision was submitted in Total Estimat 2023, the site is subject to the 2023 drainage basin fees (\$37,256 drainage & \$5,118 bridge). Please revise

\$ 11,000.00

9. FEES: At plat recording.

2021 Falcon Basin Fees: 5.004 acres @80% Impervious = 4.0032 Impervious acres Drainage fees @ \$ 34,117 per acre = \$ 136,577.17 Bridge fees @ \$ 4,687 per acre = \$ 10,762.99 Total Fees: \$ 155,340.17

10. SUMMARY

The Falcon Storage Subdivision is a proposed 1-lot, RV Storage subdivision containing 5.004 acres. The proposed street facilities will adequately convey, detain and outfall runoff from the site to existing sufficient adjacent and downstream facilities. Site appurtenances will not adversely affect the downstream and surrounding developments.

This report and findings is in general conformance with the MDDP and Preliminary Drainage Reports or other pertinent studies

> Please identify and analyze whether the downstream facilities are adequate to accept the developments flows.

Additionally, compare the detained flows and the historical flow leaving the site. Indicate whether or not the sites flow is at or below historic flows leaving the site.

MAJOR BASIN	SUB BASIN	AI	REA	BA	SIN	Tc MIN	in.	I /hr.	SOIL GRP	DEV. TYPE	C	2	FL 5-ry	.OW 100-yr	RE'	FURN RIOD
		PLANIM READ	ACRES	LENGTH -FT	HEIGHT -FT	1							qp -CFS-	qp -CFS-	-y	ears-
FALCON	0-1	9.75	2.47	300	4.5	27			A	SF 5AC.	0.12	0.39				
			V=0.82	+480	1.3	+10										
						37	2.1	3.6					0.62	3.5	5	100
HISTORIC	Α	COGO	5.00	+525	9	+13										
			V=0.65			50	1.8	2.8	A	R/L	0.08	0.35				
	TOTAL		7.47							MIX	0.093	0.362	1.25	7.6	5	100
DEVELOPED	Α	COGO	1.68	300	2.5	15.2			A	GRAVEL	0.59	0.70		2	5	100
			V=3.06	+300	7	+1.6										
						16.8	3.2	5.5					3.2	6.5	5	100
and an a faile by an	01 + A	(DP-1)	4.15	=400	8	+2	3.2	5.5	A	MIX	0.310	0.516				
		The second secon	V=2.82			52	1.7	2.9	-				2.1	6.2	5	100
	В	COGO	0.66	. 370	2.4	16.4			A	GRAVEL	0.59	0.70	13	2.5	5 ·	100
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						16.6	3.3	5.5			- /	[4.5	8.9	5	100
	B+C			+360	8	+2.7										
		(DP-2)	2.96			19.3	3.0	5.1	A	GRAVEL	0.59	0.70	5.2	10.4	5	100
	D	COGO	0.36	240	4.5	11.6	3.8	6.4	A	GRAVEL	0.59	0.70	0.8	1.6	- 5	100
	B+C+D		V=2.22	+50		+0.4					a					
		(DP-3)	3.32			19.7	3.0	5.1	A	GRAVEL	0.59	0.70	5.9	11.9	5	100
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Mi Project: Falcon Storage Sub.	IFD-Detention, Versio	on 4.06 (Ju	ly 2022)	•						
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PERMANENT OFFICE	Depth Increment =	1.00	ft Optional		· · · · · · · · · · · · · · · · · · ·		Optional			
Example Zone Configuration (Retention Pond)	Stage - Storage Description	Stage (ft)	Override Stage (ft)	Length (ft)	Width (ft)	Area (ft ²)	Override Area (ft ²)	Area (acre)	Volume (ft ³)	Volume (ac-ft)
Vatershed Information	Media Surface		0.00				5,432	0.125		國際影響
Selected BMP Type = SF Note: L/W Ratio > 8			1.00				6,800	0.156	6,116	0.140
Watershed Length = 1,640 ft			3.00				9,752	0.189	22,632	0.313
Watershed Length to Centrold = 790 ft	Sold States of B		SHORE AND				essain (da			
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Percentage Hydrologic Soil Group B = 0.0% percent	and the state of the state		の時代の正規作							· · · · · ·
Target WQCV Drain Time = 12.0 hours			以此,我把你				Secondary Recorded			
Location for 1-hr Rainfall Depths = User Input	and the second s						目的			
After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using			ALCONTROLLAR PRECEDUAL				NEW PROPERTY.			
the embedded Colorado Urban Hydrograph Procedure. Optional User Overrides	Cash Alarchi See		429220200				Notestin-			
Water Quality Capture Volume (WQCV) = 0.125 acre-feet acre-feet	CONTRACTOR ACTION		加払いたのな				· 通知者(中) (中) (中)			
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25-yr Runoff Volume (P1 = 1.75 In.) = 0.829 acre-feet 2.00 linches			CONSTRUCTION OF				Standard Stand			
50-yr Runoff Volume (P1 = 2.25 in.) = 0.971 acre-feet 2.25 inches	and the law of the		15 17 Hills				NASA-150			
100-yr Runoff Volume (P1 = 2.52 in.) = 1.145 acre-feet 2.52 inches		••	Section and			-	STATES AND A STATE			
Approximate 2-yr Detention Volume = 0.384 acre-feet	12-415 (1997-1997)		100 B/G 1				Providence and a second			
Approximate 5-yr Detention Volume = 0.502 acre-feet	to a date in the part of the		A GARANT AN	· • •			校明明编组队			
Approximate 10-yr Detention Volume = 0.606 acre-feet Approximate 25-yr Detention Volume = 0.730 acre-feet			Salara Car				Tell States			
Approximate 50-yr Detention Volume = 0.805 acre-feet	A REPORT OF THE PARTY OF		and a case				1.8 Selface			
Approximate 100-yr Detention Volume = 0.883 acre-feet			REAL PROPERTY							
Define Zones and Basin Geometry			19.4546522				CELEBRA			
Select Zone 1 Storage Volume (Regulrent) =acre-feet	and share to be a		1990 <u>1996</u>	-			行的事件的目标			
Select Zone 2 Storage Volume (Optional) = acre-feet							AND			
Total Detention Basin Volume =acre-feet			elis pendela				A STATISTICS			
Initial Surcharge Volume (ISW) = N/A ft 3	The second second		all and the second				The state			
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	DE		pectrum	etention	Sand filter	basin			
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Basin ID:	Basins 0-1 AND A-		orkeboot	Estimated	Estimated				
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PERMANENT ORIFICES POOL Example Zone	Configuration (Re	tention Pond	/ill be prov	ided onc	e design o	pond			
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Underdrain Orifice Invert Depth =	1.00	ft (distance below	the filtration media	surface)	Underdi	ain Orifice Area =	0.1	ft ²	
Underdrain Orifice Diameter =	4.00	inches			Underdrain	Orifice Centroid =	0.17	feet	
User Input: Orifice Plate with one or more orific	es or Elliptical Slot	Weir (typically use	d to drain WQCV and	d/or EURV in a se	edimentation BMP)		Calculated Paramet	ters for Plate	
Centroid of Lowest Orifice =	的和中心的中心法	ft (relative to bas	in bottom at Stage =	• 0 ft)	WQ Orific	e Area per Row =	N/A	ft ²	
Depth at top of Zone using Orifice Plate =	2月11月2日月1日月1日	ft (relative to bas	in bottom at Stage =	= 0 ft)	Ellip	tical Half-Width =	N/A	feet	
Orifice Plate: Orifice Vertical Spacing =		inches			Elliptic	al Slot Centroid =	N/A N/A	feet	
Office Plate. Office Area per Now -	CONTRACTOR CONTRACTOR	Jsq. menes			LI		N/A	n.	
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User Input: Vertical Orifice (Circular or Rectang	ular)						Calculated Parame	ters for Vertical Ori	ifice
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	7			· · ·					
Licer Input: Overflow Weir (Dropbox with Elat o	r Sloped Crate and	Outlet Dine OP P	ectangular/Transzoid	al Weir and No (Jutlet Pine)		Calculated Parame	ters for Overflow	Voir
User input. Overnow weir (Diopbox with hat o	Not Selected	Not Selected			Juliet Figer	1	Not Selected	Not Selected	
Overflow Weir Front Edge Height, Ho =	de ante de la composition de la composi	ATTACK CONTRACT	ft (relative to basin I	oottom at Stage =	0 ft) Height of Grate	Upper Edge, $H_t =$		Hot beletted	feet
Overflow Weir Front Edge Length =	同时的法法法法 的问题	的時代的情報的時代目的	feet		Overflow W	eir Slope Length =			feet
Overflow Weir Grate Slope =			H:V		Grate Open Area / 10	-yr Orifice Area =			a2
Overflow Grate Type =		And Andrews			Overflow Grate Open	Area w/ Debris =			ft ²
Debris Clogging % =	和社会的政治公司	1014日14日 10月	%			10-2003-0123 530 2 00-2020-0220-022		L	7.4
	(Circular 0.15 1		Deather 1 - 0.(0-1)		6-1		(
User Input: Outlet Pipe w/ Flow Restriction Plate	Not Selected	Not Selected	Rectangular Orifice)		<u>Ca</u>	culated Parameters	Not Selected	Flow Restriction P	<u>late</u> T
Depth to Invert of Outlet Pipe =	Hot Selected	Hot Sciected	ft (distance below b	asin bottom at Stag	ge = 0 ft) Ou	tlet Orifice Area =	Hot Sciected	Not Selected	ft ²
Circular Orifice Diameter =		Nandes Address	inches		Outlet	Orifice Centroid =			feet
				Half-Ce	entral Angle of Restrict	or Plate on Pipe =	N/A	N/A	radians
User Input: Emergency Spillway (Rectangular or	Trapezoidal)						Calculated Parame	ters for Spillway	
Spillway Invert Stage=	1.00	ft (relative to ba	in bottom at Stage =	= 0 ft)	Spillway De	sign Flow Depth=	0.53	feet	
Spillway Crest Length =	10.00	feet pro	vide spillway	riprap	Stage at T	op of Freeboard =	2.53	feet	
Spillway End Slopes =	2 00	LUN I	substions Sho	w datail	Basin Area at T		0.21	acres	
Freedoard above Max water Surface =	3.00	cal	Julations. Ono	wdetall	Deale Makers at T	op of Freeboard =	0.21	1	
	1.00	feet and	riprap gradat	tion on	Basin Volume at T	op of Freeboard = op of Freeboard =	0.42]acre-ft	
	3.00	feet and GE	l riprap gradat C Plans	tion on	Basin Volume at T	op of Freeboard = op of Freeboard =	0.42]acre-ft	
Routed Hydrograph Results	3.00 1.00 The user can over	feet and GE	I riprap gradat C Plans UHP hydrographs an 2 Year	tion on <i>d runoff volumes</i>	Basin Volume at T Basin Volume at T	op of Freeboard = op of Freeboard = es in the Inflow Hy 25 Year	0.21 0.42 drographs table (Co	acre-ft	<i>AF).</i>
Routed Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) =	3.00 1.00 The user can over WQCV N/A	ride the default C	C Plans UHP hydrographs and 2 Year 1.19	d runoff volumes	Basin Volume at T by entering new value 10 Year 1.75	op of Freeboard = op of Freeboard = es in the Inflow Hyn 25 Year 2.00	0.21 0.42 drographs table (Co 50 Year 2.25	acre-ft olumns W through 100 Year 2.52	AF). 500 Year 3.14
Routed Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) =	3.00 1.00 The user can over WQCV N/A 0.125 N/A	ride the default C N/A 0.591 N/A	C Plans UHP hydrographs an 2 Year 1.19 0.438 0.438	d runoff volumess 5 Year 0.575 0.575	Basin Volume at T Basin Volume at T 10 Year 1.75 0.685 0.685	op of Freeboard = op of Freeboard = es in the Inflow Hy 25 Year 2.00 0.829 0.829	0.21 0.42 drographs table (Co 50 Year 2.25 0.971 0.921	acre-ft olumns W through 100 Year 2.52 1.145 1 145	AF). 500 Year 3.14 1.523 1.523
Routed Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = CUHP Predevelopment Peak Q (cfs) =	3.00 1.00 The user can over WQCV N/A 0.125 N/A N/A	ride the default C EURV N/A N/A N/A	UHP hydrographs an 2 Year 1.19 0.438 0.0	d runoff volumes 5 Year 1.50 0.575 0.575 0.0	Basin Volume at T Basin Volume at T 10 Year 1.75 0.685 0.685 0.1	op of Freeboard = op of Freeboard = es in the Inflow Hy 25 Year 2.00 0.829 0.829 0.6	0.21 0.42 drographs table (G 50 Year 2.25 0.971 0.971 1.3	acre-ft 0/umns W through 100 Year 2.52 1.145 1.145 2.2	AF). 500 Year 3.14 1.523 1.523 4.1
Routed Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = CUHP Predevelopment Peak Q (cfs) = OPTIONAL Override Predevelopment Peak Q (cfs) = Predevelopment Linit Peak Elow o (cfs)(crs) =	3.00 1.00 The user can over N/A 0.125 N/A N/A N/A N/A	n.v Call feet and cet GE ride the default C U N/A N/A N/A N/A N/A N/A N/A N/A	Utations: one riprap gradat C Plans UHP hydrographs an 2 Year 1.19 0.438 0.438 0.438	d runoff volumes 5 Year 1.50 0.575 0.575 0.00	Basin Volume at T Basin Volume at T 10 Year 1.75 0.685 0.685 0.1	op of Freeboard = op of Freeboard = es in the Inflow Hyu 25 Year 2.00 0.829 0.829 0.6	0.21 0.42 drographs table (C 50 Year 2.25 0.971 0.971 1.3	acre-ft 100 Year 2.52 1.145 1.145 2.2 0.20	AF). 500 Year 3.14 1.523 1.523 4.1 0.54
Routed Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = CUHP Predevelopment Peak Q (cfs) = OPTIONAL Override Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, q (cfs/acre) = Peak Inflow Q (cfs) =	3.00 1.00 The user can over N/A 0.125 N/A N/A N/A N/A N/A	n.v Call feet and GE GE ride the default C U 0.591 N/A N/A N/A N/A N/A N/A N/A	Literations Constraints c plans 2 Year 0.19 0.438 0.438 0.0 0.00 4.1	d runoff volumes 5 Year 1.50 0.575 0.575 0.0 0.01	Basin Volume at T Basin Volume at T 10 Year 1.75 0.685 0.685 0.685 0.1 0.01	op of Freeboard = op of Freeboard = es in the Inflow Hyu 25 Year 2.00 0.829 0.829 0.829 0.6 0.09 8.3	0.21 0.42 drographs table (C 50 Year 2.25 0.971 0.971 1.3 0.17 9.9	acre-ft 100 Year 2.52 1.145 1.145 2.2 0.29 1.1.8	AF). 500 Year 3.14 1.523 1.523 4.1 0.54 15.8
Routed Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = CUHP Predevelopment Peak Q (cfs) = OPTIONAL Override Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, q (cfs/acre) = Peak Inflow Q (cfs) = Peak Outflow Q (cfs) = Peak Outflow Q (cfs) = Peak Outflow Q (cfs) =	3.00 1.00 The user can over N/A 0.125 N/A N/A N/A N/A N/A N/A N/A	ride the default C ride the default C EURV N/A N/A N/A N/A N/A N/A N/A N/A	C Plans 2 Year 1.19 0.438 0.438 0.00 4.1 2.8 N/A	d runoff volumes 5 Year 1.50 0.575 0.575 0.00 0.01 Y 5.3 4.1 81 7	Basin Volume at T Basin Volume at T 10 Year 1.75 0.685 0.685 0.1 0.01 Y 8(2 5.0 7.16	op of Freeboard = op of Freeboard = 25 Year 2.00 0.829 0.829 0.6 0.09 8.3 7.4 11.4	0.21 0.42 drographs table (C 50 Year 2.25 0.971 0.971 1.3 0.17 9.9 9.0 6 0	acre-ft 100 Year 2.52 1.145 2.2 0.29 1.145 2.2 0.29 11.8 11.2 5.2	AF). 500 Year 3.14 1.523 4.1 0.54 15.8 15.3 2.0
Routed Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (In) = CUHP Runoff Volume (acre-ft) = CUHP Predevelopment Peak Q (cfs) = CUHP Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, q (cfs/acre) = Peak Inflow Q (cfs) = Peak Nufflow Q (cfs) = Peak Outflow to Predevelopment Q = Structure Controlling Flow =	3.00 1.00 <i>The user can over</i> N/A 0.125 N/A N/A N/A N/A N/A N/A N/A N/A	ride the default C ride the default C N/A N/A N/A N/A N/A N/A N/A N/A	C Plans C Plans UHP hydrographs and 2 Year 1.19 0.438 0.0 0.00 4.1 2.8 N/A Spillway	d runoff volumes 5 Year 1.50 0.575 0.575 0.0 0.01 Y 5.3 4.1 81.7 Spillway	Basin Volume at T Basin Volume at T 10 Year 1.75 0.685 0.685 0.1 0.01 0.01 0.01 0.01 71.6 Spillway	op of Freeboard = op of Freeboard = 25 Year 2.00 0.829 0.6 0.829 0.6 0.09 Y 8.3 Y 7.4 11.4 Spillway	0.21 0.42 0.42 0.971 0.971 0.971 1.3 0.17 9.0 9.0 6.9 Spillway	acre-ft olumns W through 100 Year 2.52 1.145 1.145 2.2 0.29	AF). 500 Year 3.14 1.523 1.523 4.1 0.54 15.8 15.3 3.8 Spillway
Routed Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = CUHP Predevelopment Peak Q (cfs) = CUHP Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, q (cfs/acre) = Peak Inflow Q (cfs) = Peak Outflow Q (cfs) = Ratio Peak Outflow to Predevelopment Q = Structure Controlling Flow = Max Velocity through Grate 1 (fps) = Max Velocity through Grate 1 (fps) =	3.00 1.00 <i>The user can over</i> N/A 0.125 N/A N/A N/A N/A 0.6 N/A Filtration Media N/A N/A	ride the default C Real N/A N/A N/A N/A N/A N/A N/A N/A	Iriprap gradat C Plans 2 Year 1.19 0.438 0.00 4.1 2.8 N/A Spillway	d runoff volumes 5 Year 1.50 0.575 0.575 0.0 4.1 81.7 Spillway N/A	Basin Volume at T Basin Volume at T 10 Year 1.75 0.685 0.1 0.01 0.01 0.01 0.01 0.01 71.6 Spillway N/A	op of Freeboard = op of Freeboard = 25 Year 2.00 0.829 0.6 0.829 0.6 0.09 8.3 7.4 11.4 Spillway N/A	0.21 0.42 drographs table (C 50 Year 2.25 0.971 0.971 1.3 0.17 9.0 6.9 Spillway N/A	acre-ft olumns W through 100 Year 2.52 1.145 1.145 2.2 0.29	AF). 500 Year 3.14 1.523 1.523 4.1 0.54 15.3 3.8 Spillway N/A N/A
Routed Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = CUHP Predevelopment Peak Q (cfs) = OPTIONAL Override Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, q (cfs/acre) = Peak Inflow Q (cfs) = Peak Unflow Q (cfs) = Ratio Peak Outflow to Predevelopment Q = Structure Controlling Flow = Max Velocity through Grate 1 (fps) = Max Velocity through Grate 2 (fps) = Time to Draln 97% of Inflow Volume (hours) =	3.00 1.00 <i>The user can over</i> N/A 0.125 N/A N/A N/A N/A N/A 0.6 N/A Filtration Media N/A N/A 3	ride the default C Real of the default C ride the default C N/A N/A N/A N/A N/A N/A N/A N/A	Iriprap gradat C Plans 2 Year 1.19 0.438 0.438 0.00 4.1 2.8 N/A Spillway N/A N/A	d runoff volumes 5 Year 1.50 0.575 0.575 0.0 4.1 81.7 Spillway N/A N/A 6	Basin Volume at T Basin Volume at T 10 Year 1.75 0.685 0.1 0.1 0.01 0.01 0.01 0.01 0.01 0.01	op of Freeboard = op of Freeboard = 25 Year 2.00 0.829 0.6 0.829 0.6 0.829 0.6 7.4 11.4 Spillway N/A N/A 6	0.21 0.42 drographs table (Cl 50 Year 2.25 0.971 0.971 1.3 0.17 9.0 6.9 Spillway N/A MA <u>6</u>	acre-ft <i>olumns W through</i> 100 Year 2.52 1.145 1.145 2.2 0.29 Y 11.8 11.2 5.2 Spillway N/A N/A 6	AF). 500 Year 3.14 1.523 1.523 4.1 0.54 (15.8 15.3 3.8 Spillway N/A N/A) 5
Routed Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = CUHP Predevelopment Peak Q (cfs) = OPTIONAL Override Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, q (cfs/acre) = Peak Inflow Q (cfs) = Peak Outflow Q (cfs) = Ratio Peak Outflow to Predevelopment Q = Structure Controlling Flow = Max Velocity through Grate 1 (fps) = Max Velocity through Grate 2 (fps) = Time to Drain 97% of Inflow Volume (hours) = Time to Drain 99% of Inflow Volume (hours) =	3.00 1.00 <i>The user can over</i> WQCV N/A 0.125 N/A N/A N/A N/A N/A N/A Filtration Media N/A N/A 3 2.00	ride the default C Ride the default C N/A N/A N/A N/A N/A N/A N/A N/A	C Plans 2 Year 1.19 0.438 0.438 0.00 4.1 2.8 N/A N/A N/A 6 6 1.17	d runoff volumes 5 Year 1.50 0.575 0.575 0.01 0.01 0.01 0.01 0.01 0.01 0.1 0.	Basin Volume at T Basin Volume at T 10 Year 1.75 0.685 0.685 0.1 0.1 0.01 0.01 0.01 5.0 71.6 Spillway N/A 6 6	op of Freeboard = op of Freeboard = 25 Year 2.00 0.829 0.6 0.829 0.6 7.4 11.4 Spillway N/A N/A 6 6	0.21 0.42 drographs table (CC 50 Year 2.25 0.971 0.971 1.3 0.17 9.0 6.9 Spillway N/A N/A 6 6 1.40	acre-ft <u>olumns W through</u> <u>100 Year</u> <u>2.52</u> <u>1.145</u> <u>2.2</u> <u>0.29</u> <u>1.18</u> <u>1.12</u> <u>5.2</u> <u>Splilway</u> <u>N/A</u> <u>6</u> <u>6</u>	AF). 500 Year 3.14 1.523 1.523 4.1 0.54 (15.8 15.3 3.8 Spillway N/A 5 6
Routed Hydrograph Results Design Storm Return Period = One-Hour Rainfail Depth (in) = CUHP Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = CUHP Predevelopment Peak Q (cfs) = DPTIONAL Override Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, q (cfs/acre) = Peak Inflow Q (cfs) = Peak Outflow Q (cfs) = Ratio Peak Outflow to Predevelopment Q = Structure Controlling Flow = Max Velocity through Grate 1 (fps) = Max Velocity through Grate 2 (fps) = Time to Drain 97% of Inflow Volume (hours) = Time to Drain 97% of Inflow Volume (hours) = Maximum Ponding Depth (ft) = Area at Maximum Ponding Depth (ft) =	3.00 1.00 <i>The user can over</i> WQCV N/A 0.125 N/A N/A N/A N/A N/A N/A Filtration Media N/A N/A 3 0.91 0.15	n:v Cali feet and C GE C EURV N/A 0.591 N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A	C Plans 2 Year 1.19 0.438 0.438 0.00 4.1 2.8 N/A Spillway N/A 6 6 1.17 0.16	d runoff volumes 5 Year 1.50 0.575 0.575 0.00 4.1 81.7 Spillway N/A N/A 6 6 1.23 0.16	Basin Volume at T Basin Volume at T 10 Year 1.75 0.685 0.685 0.1 0.1 0.01 5.0 71.6 Spillway N/A N/A 6 6 6 1.27 0.16	op of Freeboard = op of Freeboard = 25 Year 2.00 0.829 0.6 0.09 Y 8.3 7.4 11.4 Spillway N/A N/A N/A 6 6 1.35 0.17	0.21 0.42 drographs table (C 50 Year 2.25 0.971 0.971 1.3 0.17 9.0 6.9 Spillway N/A N/A 6 6 1.40 0.17	acre-ft 100 Year 2.52 1.145 1.145 2.2 0.29 1.18 1.1.2 5.2 Spillway N/A A A A A A A A A A A A A A	AF). 500 Year 3.14 1.523 1.523 4.1 0.54 (15.8) 15.3 3.8 Spillway N/A N/A 5 6 1.57 0.17

revise so that peak outflow is less than predevelopment flow. Design must comply for the full spectrum of storms. 5



DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename:

Inflow Hydrographs

							СЦНВ		CUHP	CLIHR
Time Interval	TIME	WOOV Infal		2 Year [cfc]	E Voor [cfc]	10 Year [cfc]	2E Voor [cfc]	50 Year [cfc]	100 Year [cfc]	500 Year [cfc]
Time Interval	0.00.00	wQCv [cis]	EURV [CIS]		5 rear [cis]					
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.04	0.00	0.14
	0:15:00	0.00	0.00	0.40	0.65	0.80	0.54	0.68	0.66	2.38
	0:25:00	0.00	0.00	3.10	4.12	4.97	3.10	3.55	3.81	5.08
	0:30:00	0.00	0.00	3.94	5.18	6.11	6.41	7.66	8.63	11.65
	0:35:00	0.00	0.00	4.07	5.28	6.19	7.90	9.41	11.18	14.97
	0:40:00	0.00	0.00	3.97	5.08	5.93	8.31	9.91	11.82	15.81
	0:45:00	0.00	0.00	3.73	4.80	5.62	8.01	9.52	11.60	15.55
	0:50:00	0.00	0.00	3.50	4.55	5.29	7.70	9.13	11.09	14.90
	0:55:00	0.00	0.00	3.29	4.29	5.00	7.19	8.50	10.44	14.02
	1:00:00	0.00	0.00	3.13	4.07	4.77	6.71	7.91	9.84	13.20
	1:05:00	0.00	0.00	2.99	3.88	4.57	6.32	7.43	9.36	12.58
	1:10:00	0.00	0.00	2.79	3./0	4.3/	5.89	6.90	8.62	10.53
	1.15.00	0.00	0.00	2.50	3.40	3.88	4 00	5.82	7.88	9.40
	1:25:00	0.00	0.00	2.30	2.98	3.58	4 55	5.02	6.29	8.35
	1:30:00	0.00	0.00	2.08	2.82	3.34	4.10	4.76	5.59	7.41
	1:35:00	0.00	0.00	1.99	2.70	3.16	3.76	4.36	5.07	6.70
	1:40:00	0.00	0.00	1.91	2.54	3.01	3.49	4.04	4.66	6.15
	1:45:00	0.00	0.00	1.84	2.38	2.86	3.26	3.77	4.31	5.66
	1:50:00	0.00	0.00	1.76	2.23	2.72	3.05	3.52	3.98	5.22
	1:55:00	0.00	0.00	1.63	2.09	2.57	2.85	3.29	3.68	4.81
	2:00:00	0.00	0.00	1.49	1.94	2.38	2.66	3.06	3.39	4.41
	2:05:00	0.00	0.00	1.29	1.69	2.06	2.32	2.66	2.94	3.82
	2:10:00	0.00	0.00	1.10	1.43	1.75	1.98	2.27	2.50	3.25
	2:15:00	0.00	0.00	0.92	1.20	1.46	1.65	1.89	2.08	2.69
	2:20:00	0.00	0.00	0.75	0.98	0.98	1.35	1.54	1.69	1.71
	2:30:00	0.00	0.00	0.50	0.65	0.50	0.85	0.96	1.02	1.30
	2:35:00	0.00	0.00	0.41	0.54	0.68	0.68	0.76	0.80	1.01
	2:40:00	0.00	0.00	0.34	0.45	0.57	0.55	0.62	0.64	0.80
	2:45:00	0.00	0.00	0.29	· 0.38	0.47	0.45	0.51	0.51	0.64
	2:50:00	0.00	0.00	0.24	0.32	0.39	0.37	0.41	0.41	0.51
	2:55:00	0.00	0.00	0.20	0.26	0.33	0.30	0.34	0.32	0.40
	3:00:00	0.00	0.00	0.17	0.21	0.27	0.24	0.27	0.26	0.32
	3:05:00	0.00	0.00	0.14	0.18	0.22	0.20	0.22	0.21	0.26
	3:10:00	0.00	0.00	0.11	0.14	0.18	0.16	0.18	0.17	0.21
	3:15:00	0.00	0.00	0.09	0.12	0.14	0.13	0.13	0.14	0.1/
	3:25:00	0.00	0.00	0.05	0.03	0.09	0.08	0.09	0.09	0.11
	3:30:00	0.00	0.00	0.04	0.05	0.07	0.06	0.07	0.07	0.08
	3:35:00	0.00	0.00	0.03	0.04	0.05	0.05	0.05	0.05	0.06
	3:40:00	0.00	0.00	0.02	0.03	0.03	0.03	0.03	0.03	0.04
	3:45:00	0.00	0.00	0.01	0.02	0.02	0.02	0.02	0.02	0.02
	3:50:00	0.00	0.00	0.01	0.01	0.01	0.01	0.01	0.01	0.01
	3:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

					Depth at (Outlet (ft)			
		1.0	1.5	2.0	2.5	3.0	3.5	4.0	4.5
	2	15.04	7.71	5.10	3.76	2.95	2.41	2.02	1.73
	1	7.52	3.86	2.55	1.88	1.48	1.21	1.01	0.87
(if	0.6	4.51	2.31	1.53	1.13	0.89	0.72	0.61	0.52
cre-	0.4	3.01	1.54	1.02	0.75	0.59	0.48	0.40	0.35
a (ai	0.2	1.50	0.77	.0.51	0.38	0.30	0.24	0.20	0.17
me	0.1	0.75~	0.39	0.26	0.19	0.15	0.12	0.10	0.09
lo'	0.06	0.45 .	0.23	0.15	0.11	· 0.09	0.07	0.06	0.05
2	0.04	0.30	0.15	0.10	0.08	0.06	0.05	0.04	0.03
esig	0.02	0.15	0.08	0.05	0.04	0.03	0.02	0.02	0.02
ă	0.01	0.08	0.04	0.03	0.02	0.01	0.01	0.01	0.01

TABLE SB-1

0-1+ A-D WQCV 0.125 AF = 5445CF 16" 40 6"

		0.322	5?42
Circular Perforati	on Sizing	10	ea "116"
Hole Diameter	Hole Diameter	AI	rea per Row (in ²)
(in)	(in)	n = 1	n = 2
1/4	0.250	0.05	0.10
5/16	0.313	0.08	0.15
3/8	0.375	0.11	0.22
7/16	0.438	0.15 -	0.30 .
1/2	0.500	0.20	0.39
9/16	0.563	0.25	0.50
5/8	0.625	0.31	0.61
11/16	0.688	(032)	0.74
3/4	0.750	0.44	0.88
7/8	0.875	0.60	1.20
1	1.000	0.79	1.57
1 1/8	1.125	0.99	1.99
1 1/4	1.250	1.23	2.45
1 3/8	1.375	1.48	2.97
1 1/2	1.500	1.77	3.53

1 5/8 1.625 2.07 4.15 1 3/4 1.750 2.41 4.81 17/8 1.875 2.76 5.52 2 2.000 3.14 6.28 n = Number of columns of perforations Minimum steel plate thickness 1/4" 5/16"

TABLE SB-2

City of Colorado Springs **Stormwater Quality**

\ea

Figure SB-2 **Outlet Sizing** Application Techniques and Maintenance Requirements

n = 3 0.15 0.23

0.33 0.45 0.59 0.75 0.92 1.11 1.33 1.80 2.36 2.98 3.68 4.45 5.30

6.22

7.22

8.28

9.42

3/8"



~_l	0.463	8/3_12
Q	n	0 0
	N	

Í

TAMETER	AREA	D 8/3		K		
-TN -	- FT2 -	- FT -	N=0.010	N=0.013	N = 0.024	N = 0.026
- 1 IV.						
2	0.02182	0.008413	0.3895			
	0.08727	0.053420	2.4733			<u>,</u>
6	0,19630	0.157500	7.2922	5.609		
8	0.34910	0.339200	15.7050	12.081		
10	0.54540	0.615000	28.4745	21.903		
1	0.78540	1.000000	46.3000	35.615		
- 15	1,22720	1.813100	83.9465	64.574		
18	1,76710	2.948300	136.5100	105.000	56.88	52.50
21	2 40530	4,447400	205.9100	158.400	85.80	79.20
21	3 14160	6.349600	293.9900	226.140	122.49	113.07
27	3 97610	8,692700	402.4700	309.590	167.70	154.79
30	4 90870	11.512600	533.0300	410.030	222.10	205.02
30	5 93960	14.844100		528.680		
35	7 06860	18,720800	866.7700	666.700	361.20	333.30
30	8 29580	23,175100		825.400		
39	0 62110	28,238900		1005.000	544.80	502.50
42	12 56640	40.317500		1436.000	777.80	718.00
40 F1	15 90430	55,195000		1966.000	1065.00	983.00
54	10 63500	73,100400		2604.000	1410.00	1302.00
66	23 75830	94 254200		3357.000	1818.00	1678.00
72	28 27/30	118 869400		4234.000	2293.00	2117.00
70	23.19310	147 152900		5241.000	2839.00	2620.00
04	79 18150	179 306000		6386.000	3459.00	3193.00
84	11 17960	215 524500		7676.000	4158.00	3838.00
90	F0 26550	256 000000		9118.000	4939.00	4559.00
90	67 61770	350 466600		12480.000	6761.00	6140.00
108	70 5300	164 158900		16530.000	8954.00	8265.00
<u> </u>	10.33300	+0+.100000				
	8					
				+		

Oliver E. Watts Consulting Engine Colorado Springs

Q=KS¹2



National Flood Hazard Layer FIRMette



Legend



NOTES TO USERS

This map is for use in administering the National Flood Insurance Program. It does not necessarily identify all areas subject to flooding, particularly from local drainage sources of small size. The community map repository should be consulted for possible updated or additional flood hazard information.

To obtain more detailed information in areas where Base Flood Elevations (BFEs) and/or floodways have been determined, users are encouraged to consult the Flood Profiles and Floodway Data and/or Summary of Sillwater Elevations tables contained within the Flood Insurance Study (FIS) report that accompanies this FIRM. Users should be aware that BFEs shown on the FIRM represent rounded whole-foot elevations. These BFEs are intended for flood Insurance railing purposes only and should not be used as the sole source of flood elevation information. Accordingly, flood elevation data presented in the FIS report bhould be utiled in conjunction with the FIRM for purposes of construction and/or floodplain management.

Coastal Base Flood Elevations shown on this map apply only landward of 0.0' North American Vertical Datum of 1988 (NAVD83). Users of this FiRM should be haven that coastal flood levations are also provided in the Summary of Stilwater Elevations table in the Flood Insurance Study report for this jurisdiction. Elevations shown in the Summary of Stilwater Elevations table should be used for construction and/or floodplain management purposes when they are higher than the elevations shown on this FIRM.

Boundaries of the floodways were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations with regard to requirements of the National Flood Insurance Program. Floodway widths and other pertinent floodway data are provided in the Flood Insurance Study report for this juriadiction.

Certain areas not in Special Flood Hazard Areas may be protected by flood control structures. Refer to section 2.4 "Flood Protection Measures" of the Flood Insurance Study report for information on flood control structures for this jurisdiction.

The projection used in the preparation of this map was Universal Transverse Mercator (UTM) zone 13. The horizontal datum was NAD83, GRSg0 spheroid. Differences in datum, spheroid, projection or UTM zones zones used in the production of FIRMs for edjacent jurisdictions may result in slight positional differences in map features across jurisdiction boundaries. These differences do not affect the accuracy of this FIRM.

Rood elevations on this map are referenced to the North American Vertical Datum of 1988 (NAVD88). These flood elevations must be compared to structure and ground elevations referenced to the same vertical datum. For information regarding conversion between the National Geodetic Vertical Datum of 1929 and the North American Vertica Datum of 1980, visit the National Geodetic Survey velaties hold/www.ngs.nosa.gov/ or contact the National Geodetic Survey at the following address:

NGS Information Services NOAA, N/NGS12 National Geodetic Survey SSMC-3, #9202 1315 East-West Highway Silver Spring, MD 20910-3282

To obtain current elevation, description, and/or location information for bench marks shown on this map, please contact the Information Services Branch of the National Geodetic Survey at (301) 713-3242 or visit its website at http://www.ngs.ncaa.gov/.

Base Map information shown on this FIRM was provided in digital format by EI Paso County, Colorado Springs Utilites, City of Fountain, Bureau of Land Management, National Oceanic and Atmospheric Administration, United States Geological Survey, and Anderson Consulting Engineers, Inc. These data are current as of 2006.

This map reflects more detailed and up-to-date stream channel configurations and floodplain delineatione than those shown on the previous FIRM for this juriadicion. The floodplain and floodways that were transferred from the previous FIRM may have been adjusted to conform to these new stream channel configurations. As a result, the Flood Profiles and Floodway Data tables in the Flood Insurance Study Report (which contains authoritative hydraulic data) may reflect stream channel distances that differ from what is shown on this map. The profile baselines depicted on this map represent the hydraulic modeling baselines that match the flood profiles and explicitly the profile baselines depicted to the strength of the profile baselines depicted and may appear outside of the floodplain.

Corporate limits shown on this map are based on the best data available at the time of publication. Because changes due to annexations or de-annexations may have occurred unter this map was published, map users should contact appropriate community officials to verify current corporate limit locations.

Please refer to the separately printed Map Index for an overview map of the county showing the layout of map panels; community map repository addresses; and a Listing of Communities table containing National Flood Insurance Program dates for each community as well as a listing of the panels on which each community is located.

Contact FEMA Map Service Center (MSC) via the FEMA Map Information exchange (FMX) 1-077-336-2627 for information on available products associated with this FIRM. Available products may include previouwly issued Letters of Map Change, a Flood Insurance Study Report, and/or digital versions of this map. The MSC may also be reached by Ficx at 1-600-356-9620 and its website at http://www.msc.iema.gov/.

If you have questions about this map or questions concerning the National Flood Insurance Program in general, please call 1-877-FEMA MAP (1-877-336-2627) or visit the FEMA website at http://www.fema.gov/business/nfip.



Additional Flood Hazard information and resources are available from local communities and the Colorado Water Conservation Board.

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	B assessan	SPECIAL FLO	LEGEND DD HAZARD AREAS (SFHAS) SUBJECT TO
	The 1% ann	INUNDATION	BY THE 1% ANNUAL CHANCE FLOOD
	that has a 19 Hazard Area Special Flood Elevation is t	 chance of being e is the area subject Hazard include Zon he water-surface ele 	valued or extreded in any over the base fract, to be inded quicked or extreded in any over the Special Flood to flooding by the 1% annual chance flood. Areas of res A, AE, AY, AQ, AR, A9, V, and VE. The Base Flood values of the 1% annual chance flood.
	ZONE AE	No Base Flood Ele Base Flood Elevati Flood deaths of	vations determined. ions determined.
	ZONE AD	Elevations determ Flood depths of 1	to 3 feet (usually sheet flow on sloping (cmpin); everage
	ZONE AR	depths determined determined. Special Flood Haz	d. For areas of allument fan fraading, velocroes also and Areas Formerly protected from the 1% annual chance
		flood by a flood of AR indicates that provide protection	control system that was subsequently decertified. Zone the former flood control system is being restored to from the 1% annual chance or greater flood.
	ZONE A99	Area to be prote protection system determined.	cted from 1% annual chance flood by a Federal flood m under construction; no Base Flood Elevations
	ZONE V	Coastal flood zor Devations determ	ie with velocity hazard (wave action); no Base Ficod ined.
	ZONE VE	Ceasta) flood zo Elevations determ	ne with velocity hazard (wave scilion); Base Flood ined.
	The Roodway	HLOODWAY AF	REAS IN ZONE AE
- 1	kept free of substantial in	encroachment, so th creases in flood help	hat the 1% annual chance flood can be carried without phis.
	ZONE	OTHER FLOOD	AREAS
	20m2 X	average depths o square mile; and a	I less than 1 foot or with drainage areas less than 1 areas protected by leves from 1% annual chance flood.
		OTHER AREAS	
	ZONE X ZONE D	Areas determined Areas in which flo	to be outside the 0.2% ennual chance floodplein. of hazards are undetermined, but possible.
	1117	COASTAL BAR	RIER RESOURCES SYSTEM (CBRS) AREAS
	2223	OTHERWISE P	ROTECTED AREAS (OPAs)
	CBRS areas a	nd OPAs are normal	ly located within or adjacent to Special Flood Hazard Areas.
		Flood	ipian boundary Iway boundary
		Zone CERS	D Boundary and OPA boundary
	12 32 67 4 16 16 19 70 19 20 19 19	Boun Flood	dary dividing Special Flood Hazerd Areas of different Base Elevations, flood depths or flood velocities.
	~~ 513 (EL 98)	Base	Flood Elevation line and value; elevation in feet*
	* Referenced	eleva to the North Americ	tion in feet* ian Vertical Datum of 1988 (NAVD 88)
	A	-(A) Cross	section line
	23		sect line
	97° 57° 30 32° 22' 30	.00* Geog .00* Datur	raphic coordinates referenced to the North American m of 1983 (NAD 83)
	475000	N 1000 zone	-meter Universal Transverse Mercator grid ticks, 13
	6000000	FT 5000 syste	-fool grid Ucks: Colorado State Plane coordinate m, central zone (FIPSZONE 0502), act Conformal Comis Deviation
	DX5510) Bend X this F	h mark (see explanation in Notes to Users section of
	. M1.5	River	Mie
		Refer	MAP REPOSITORIES
		EFF	ECTIVE DATE OF COUNTYWIDE OOD INSURANCE RATE MAP
			MARCH 17, 1997
	DECEN	EFFECTIVE D	DATE(S) OF REVISION(S) TO THIS PANEL
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EL PASO COUNTY AREA, COLORADO

TABLE 16.--SOIL AND WATER FEATURES

[Absence of an entry indicates the feature is not a concern. See "flooding" in Glossary for definition of terms as "rare," "brief," and "very brief." The symbol > means greater than]

1			Flooding	1	Bedr	ock	
Soil name and map symbol	Hydro- logic group	Frequency	Duration	Months	Depth	Hardness	Potential frost action
Alamosa:					In		
1	с	Frequent	Brief	May-Jun	>60		High.
Ascalon: 2, 3	В	None			>60		Moderate:
Badland: 4	D						
Bijou: 5, 6, 7	В	None			>60		Low.
Blakeland: 8	A	None			>60		Low.
¹ 9: Blakeland part-	A	None			>60		Low.
Fluvaquentic Haplaquolls part	D	Common	Very brief	Mar-Aug	>60		High.
Blendon: 10	В	None	· • •		>60		Moderate.
Bresser: 11, 12, 13	В	None			>60		Low.
Brussett: 14, 15	В	None	·		>60		Moderate.
Chaseville: 16, 17	A	None			>60		Low.
¹ 18: Chaseville part	A	None			>60		Low.
Midway part	D	None			10-20	Rippable	Moderate.
Columbine: 19		None to rare			>60		Low.
Connerton: ¹ 20: Connerton part-	В	 None			; >60		High.
Rock outcrop part	D						
Cruckton: 21	в	 None			>60		Moderate.
Cushman: 22, 23	с	None			20-40	Rippable	Moderate.
¹ 24: Cushman part	с	None	ана на селото на село На селото на селото на На селото на		20-40	Rippable	Moderate.
Kutch part	с	None			20-40	Rippable	Moderate.
Elbeth: 25, 26	В	None			>60		Moderate.
¹ 27: Elbeth part	B	None			>60		Moderate.

See footnote at end of table.

MN

Land Use or Surface	Percent						Runoff Co	peffidents					
Characteristics	Impervious	2-y	/ear	5-y	ear	10-1	year	25-1	year	50-	year	100-	year
		HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D
Business													
Commercial Areas	95	0.79	0.80	0.81	0.82	0.83	0.84	0.85	0.87	0.87	0.88	0.88	0.89
Nelghborhood Areas	70	0.45	0.49	0.49	0.53	0.53	0.57	0.58	0.62	0.60	0.65	0.62	0.68
Residential	1												
1/8 Acre or less	65	0.41	0.45	0.45	0.49	0.49	0.54	0.54	0.59	0.57	0.67	0.50	0.05
1/4 Acre	40	0.23	0.28	0.30	0.35	0.36	0.42	0.42	0.55	0.57	0.02	0.59	0.65
1/3 Acre	30	0.18	0.22	0.25	0.30	0.32	0.38	0.39	0.30	0.40	0.54	0.50	0.58
1/2 Acre	25	0.15	0.20	0.22	0.28	0.30	0.36	0.37	0.47	0.43	0.52	0.47	0.57
1 Acre	20	0.12	0.17	0.20	0.26	0.27	0.34	0.37	0.46	0.41	0.51	0.46	0.55
Industrial													
Light Areas	80	0.57	0.50	0.50	0.63	0.62	0.66	0.66	0.70	0.00	0.70	0.70	
Heavy Areas	90	0.71	0.73	0.73	0.75	0.75	0.77	0.00	0.80	0.80	0.72	0.70	0.74
Parks and Cemeteries	7	0.05	0.09	0.12	0.10							_	
Playgrounds	12	0.03	0.09	0.12	0.19	0.20	0.29	0,30	0.40	0,34	0.46	0.39	0.52
Railroad Yard Areas	40	0.23	0.13	0.18	0.25	0.24	0.31	0.32	0.42	0.37	0.48	0.41	0.54
Indeveloped Areas										1			
Historic Flow Applycia:													
Greenbelts, Agriculture	2	0.03	0.05	0.09	0.16	0.17	0.26	0.26	0.38	0.31	0.45	0.36	0.51
Pasture/Meadow	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50
Forest	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50
Exposed Rock	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Offsite Flow Analysis (when landuse is undefined)	45	0.26	0.31	0.32	0.37	0.38	0.44	0,44	0.51	0.48	0.55	0.51	0.59
													0155
Davied													
Gravel	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Gravel	80	0.57	0.60	0.59	0,63	0.63	0.66	0.66	0.70	0.68	0.72	0.70	0.74
Drive and Walks	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Roofs	90	0.71	0.73	0.73	0.75	0.75	0.77	0.78	0.80	0.80	0.82	0.81	0.83
lawns	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0 37	0.30	0.44	0.35	0.50

Table 6-6. Runoff Coefficients for Rational Method (Source: UDFCD 2001)

3.2 Time of Concentration

One of the basic assumptions underlying the Rational Method is that runoff is a function of the average rainfall rate during the time required for water to flow from the hydraulically most remote part of the drainage area under consideration to the design point. However, in practice, the time of concentration can be an empirical value that results in reasonable and acceptable peak flow calculations.

For urban areas, the time of concentration (t_c) consists of an initial time or overland flow time (t_i) plus the travel time (t_i) in the storm sewer, paved gutter, roadside drainage ditch, or drainage channel. For nonurban areas, the time of concentration consists of an overland flow time (t_i) plus the time of travel in a concentrated form, such as a swale or drainageway. The travel portion (t_i) of the time of concentration can be estimated from the hydraulic properties of the storm sewer, gutter, swale, ditch, or drainageway. Initial time, on the other hand, will vary with surface slope, depression storage, surface cover, antecedent rainfall, and infiltration capacity of the soil, as well as distance of surface flow. The time of concentration is represented by Equation 6-7 for both urban and non-urban areas.

(Eq. 6-7)

$$t_c = t_i + t_i$$

Where:

 t_c = time of concentration (min)

 t_i = overland (initial) flow time (min)

 t_t = travel time in the ditch, channel, gutter, storm sewer, etc. (min)

3.2.1 Overland (Initial) Flow Time

The overland flow time, t_i , may be calculated using Equation 6-8.

$$t_i = \frac{0.395(1.1 - C_5)\sqrt{L}}{S^{0.33}}$$
(Eq. 6-8)

' .5 11

Where:

 $t_i = \text{overland (initial) flow time (min)}$

 C_5 = runoff coefficient for 5-year frequency (see Table 6-6)

 $\mathcal{S}^{(2)} \geq 1$

L = length of overland flow (300 ft maximum for non-urban land uses, 100 ft maximum for urban land uses)

S = average basin slope (ft/ft)

Note that in some urban watersheds, the overland flow time may be very small because flows quickly concentrate and channelize.

3.2.2 Travel Time

For catchments with overland and channelized flow, the time of concentration needs to be considered in combination with the travel time, t_i , which is calculated using the hydraulic properties of the swale, ditch, or channel. For preliminary work, the overland travel time, t_i , can be estimated with the help of Figure 6-25 or Equation 6-9 (Guo 1999).

$$V = C_{..}S_{...}^{0.5}$$

Where:

V = velocity (ft/s)

 C_{ν} = conveyance coefficient (from Table 6-7)

 S_{w} = watercourse slope (ft/ft)

 $\Delta T = 1$

(Eq. 6-9)

Type of Land Surface	C_{ν}
Heavy meadow	2.5
Tillage/field	5
Riprap (not buried)*	6.5
Short pasture and lawns	7
Nearly bare ground	10
Grassed waterway	15
Paved areas and shallow paved swales	20

Table 6-7.	Conveyance	Coefficient, C_{ν}
------------	------------	------------------------

For buried riprap, select C_v value based on type of vegetative cover.

The travel time is calculated by dividing the flow distance (in feet) by the velocity calculated using Equation 6-9 and converting units to minutes.

The time of concentration (t_c) is then the sum of the overland flow time (t_i) and the travel time (t_i) per Equation 6-7.

3.2.3 First Design Point Time of Concentration in Urban Catchments

Using this procedure, the time of concentration at the first design point (typically the first inlet in the system) in an urbanized catchment should not exceed the time of concentration calculated using Equation 6-10. The first design point is defined as the point where runoff first enters the storm sewer system.

$$t_c = \frac{L}{180} + 10$$

(Eq. 6-10)

Where:

 t_c = maximum time of concentration at the first design point in an urban watershed (min)

L = waterway length (ft)

Equation 6-10 was developed using the rainfall-runoff data collected in the Denver region and, in essence, represents regional "calibration" of the Rational Method. Normally, Equation 6-10 will result in a lesser time of concentration at the first design point and will govern in an urbanized watershed. For subsequent design points, the time of concentration is calculated by accumulating the travel times in downstream drainageway reaches.

Minimum Time of Concentration 3.2.4

If the calculations result in a t_c of less than 10 minutes for undeveloped conditions, it is recommended that a minimum value of 10 minutes be used. The minimum t_c for urbanized areas is 5 minutes.

3.2.5 Post-Development Time of Concentration

As Equation 6-8 indicates, the time of concentration is a function of the 5-year runoff coefficient for a drainage basin. Typically, higher levels of imperviousness (higher 5-year runoff coefficients) correspond to shorter times of concentration, and lower levels of imperviousness correspond to longer times of



Figure 6-5. Colorado Springs Rainfall Intensity Duration Frequency









