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# The Commons at Falcon Field - Preliminary Plan Traffic Impact Study PCD File No.: SP232 

(LSC \#S234070)
June 7, 2024

## Traffic Engineer's Statement

This traffic report and supporting information were prepared under my responsible charge and they comport with the standard of care. So far as is consistent with the standard of care, said report was prepared in general conformance with the criteria established by the County for traffic reports.


## Developer's Statement

I, the Developer, have read and will comply with all commitments made on my behalf within this report.

# The Commons at Falcon Field Traffic Impact Study PCD File No. SP232 

Prepared for:
P.J. Anderson

31 North Tejon, Suite 500
Colorado Springs, CO 80903

JUNE 7, 2024

LSC Transportation Consultants
Prepared by: Jeffrey C. Hodsdon, P.E. \& Kirstin D. Ferrin, P.E.

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June 7, 2024
P.J. Anderson

31 North Tejon, Suite 500
Colorado Springs, CO 80903

RE: The Commons at Falcon Field Preliminary Plan El Paso County, CO<br>Traffic Impact Study<br>PCD File No.: SP232<br>LSC \#S234220

Dear Mr. Anderson,

LSC Transportation Consultants, Inc. has prepared this Traffic Impact Study for the Commons at Falcon Field development in the Falcon area of El Paso County, Colorado. Commons at Falcon Field is a proposed development to be located southeast of the intersection of US Highway 24 (US Hwy 24) and Woodmen Road. This report has been prepared to accompany the resubmittal of the Preliminary Plan application to El Paso County and the Colorado Department of Transportation (CDOT). The Preliminary Plan shows a mix of commercial and residential land uses. LSC previously completed traffic reports for the original rezone, the prior Preliminary Plan, and the 2022 Rezone.

## REPORT CONTENTS

The preparation of this report included the following:

- An inventory of existing roadway and traffic conditions on the adjacent and nearby roadway system, including functional classification, widths, pavement markings, surface conditions, traffic, traffic-control signs, posted speed limits, intersection and access spacing, roadway and intersection alignments, roadway grades, and auxiliary turn lanes;
- Weekday peak-hour turning-movement traffic counts at the following intersections:
- Woodmen Road/US Highway 24
- Rio Lane/US Highway 24
- US Highway 24/ Meridian Road
- Estimated current average weekday traffic (AWT) volumes on the study-area streets including US Highway 24, Woodmen Road, Meridian Road, McLaughlin Road, and Rio Lane;
- Projections of 20-year background traffic volumes on the study-area streets;
- The proposed site land uses;
- Estimates of average weekday and weekday peak-hour trip generation for the proposed Falcon Field development and the estimated directional distribution of site-generated vehicle trips on the area street and roadway network;
- Projected site-generated and resulting total peak-hour intersection traffic volumes at the study-area intersections;
- Projected total daily (AWT) volumes on the study-area streets;
- Intersection level of service analysis at the study-area intersections;
- Vehicle queuing and sight-distance analysis at the proposed site-access points;
- Recommended street classifications;
- A list of deviations accompanying this application; and
- Findings and recommendations.


## LIST OF OTHER TRAFFIC REPORTS USED IN THE PREPARATION OF THIS REPORT

## Prior Falcon Field Traffic Reports for this Site:

- A master TIS report for the original Falcon Field rezone, dated February 24, 2020.
- The TIS report for the previously submitted Preliminary Plan (withdrawn prior to the 2022 rezone), dated November 5, 2020.
- A master TIS report for the 2022 Falcon Field rezone, dated January 21, 2022.

The initial submittal of this report was dated June 23, 2023; Revised (and one new) deviations included with this application were recently resubmitted on February 21, 2024 (EPC PCD File No. DEV238).

Compared to the TIS for the initial property rezone dated February 24, 2020 (and the TIS for the Preliminary Plan Report dated November 5, 2020), the site trip generation and site-generated traffic based on the currently-proposed zoning is significantly lower than for the strictly commercial zoning that was originally approved. Details are included in the Trip Generation section.

The most recent versions of the following traffic reports were utilized in preparing this report: Falcon Marketplace (LSC), Meadowlake Ranch (LSC), The Ranch (LSC), and the School District 49 Transportation Facility study (LSC), US Highway 24 Planning and Linkage Study (CDOT). This report is generally consistent with these reports. Minor adjustments to background traffic volumes have been made to account for newer traffic counts, and traffic projections in the CDOT PEL study.

## LAND USE AND ACCESS

Figure 1 shows the site location relative to the adjacent and nearby roadways. The development is planned to have commercial and residential land uses. The site is directly southeast of the intersection of Woodmen Road/US Highway 24 in Parcels 4307000001 and 4307200015.

## Land Use

Commons at Falcon Field is planned to include eight regional commercial lots and 170 single-family residential lots. This report assumes the eight regional commercial lots will be developed with up to 84,000 square feet of general retail floor space. Figure 2a shows the current site plan/Preliminary Plan.

## Access

As shown on the site plan, the primary access to the development will be a new southeast leg of the Woodmen Road/US Hwy 24 intersection (currently a T-intersection). This new section of Woodmen Road would be extended southeast to a roundabout intersection with a new Urban Non-Residential Collector, Retail Row Street with a modified cross section. A modified cross section is proposed for this street, which will require approval of a deviation to the criteria contained in The El Paso County Engineering Criteria Manual (ECM). This deviation (No. 5) was recently resubmitted.

The residential development areas are planned to be served by proposed Urban Local streets (that would be public). The commercial lots are planned to be served by private commercial (local) streets. Direct access to the individual commercial lots would be via three private commercial local streets shown on the Preliminary Plan (Jackdaw Point, Perula Way, and Dunlin Heights).

Figure $2 b$ shows the proposed internal public streets and commercial access points/intersections. The proposed spacing of the intersections/access points to Retail Row Street northeast of the proposed roundabout do not meet the prescribed minimum 330-foot spacing required for Urban Non-Residential Collectors, as shown on Table 2-7 of the ECM.

A right-in only access is proposed to Woodmen Road. This access will require approval of a deviation from the criteria contained in the ECM. This deviation (No. 2a) is included with the set of deviations for the project.

A street stub to the west is shown on the Preliminary Plan, which would allow for a future connection to future adjacent development if ever needed. The areas within Tracts B and G directly southeast of the proposed roundabout have been reserved to accommodate a potential future fourth leg of the roundabout to provide access to what is currently the northwest corner of Arrowhead Estates IF and when redevelopment happens to occur within that area. Currently,
these possible future connections are not proposed for use by this project. These are being provided for the benefit of US Hwy 24 access management and adjacent property owners, should future connections to adjacent future developments/redevelopment become necessary.

## Sight Distance

Figures 3a and 3b show the results of sight-distance analysis of the intersections and access points to Retail Row Street. The analysis is based on a design speed of 25 miles per hour ( mph ) for the modified cross section. As shown in Figures 3a and 3c, the required intersection sight distance of 280 feet from taken ECM Table 2-21 and the required stopping sight distance of 155 feet taken from ECM Table 2-17 can be met at all of the proposed intersections and access points to Retail Row Way. One reasonable exception (citing AASHTO criteria) is noted in Figure 3a for sight distance for drivers turning onto Retail Row Street from Jackdaw Point to vehicles traveling southbound to westbound via the Rio Lane/Retail Row Street knuckle located just east of the intersection.

Figure 3c shows the results of the sight distance analysis of the intersection of Woodmen Road/Dunlin Heights. As this access is proposed to be restricted to right-in only, the analysis was limited to stopping sight distance for south-eastbound traffic arriving from the intersection of US Hwy 24/Woodmen. Figure 3c shows the required stopping sight distance based on 40 mph for south-eastbound through vehicles from the intersection of US Hwy 24/Woodmen, based on a 15 mph for north-eastbound right-turning vehicles from the intersection of US Hwy 24/Woodmen, and based on 20 mph for south-westbound left-turning vehicles from the intersection of US Hwy 24/Woodmen. As shown in Figure 3c, the required stopping sight distance can be met for all three scenarios.

Figure 3d shows the results of sight-distance analysis of the intersections and access points to Rio Lane. The analysis is based on a design speed of 25 miles per hour (mph) for a Local. As shown in Figure 3d, the required intersection sight distance of 280 feet from taken ECM Table 2-21 and the required stopping sight distance of 155 feet taken from ECM Table 2-17 can be met at all of the proposed intersections and access points to Rio Lane. One reasonable exception (citing AASHTO criteria) is noted in Figure 3d for sight distance for drivers turning onto Rio Lane from Perula Way to vehicles traveling westbound to southbound via the knuckle located just north of the intersection.

## PROPOSED RIO LANE CLOSURE AT US HIGHWAY 24

The intersection of Rio Lane/US Highway 24 is proposed to be closed, as shown in the adopted US Highway 24 Access Management Plan and the US 24 Planning and Environmental Linkages Study, October 2017. The project will help implement the US Highway 24 Access Management Plan by providing an alternative to the Rio Lane/US Hwy 24 intersection.

The site plan shows the proposed internal public streets, Retail Row Street and the extension of Woodmen Road into the site, for site circulation and the new connection to Rio Lane that would allow for the prescribed closure of the US Hwy 24/Rio intersection per CDOT's US Highway 24 Access Management Plan.

## EXISTING ROADWAYS AND TRAFFIC VOLUMES

## Area Roadways

The major roadways in the site's vicinity are shown in Figure 1 and are described below.

US Highway 24 is a two-lane, category EX - Expressway/Major Bypass (CDOT Classification) adjacent to the site that runs northeast/southwest with a $55-$ mile-per hour (mph) posted speed limit adjacent to the site. The corridor was studied in-depth in the US 24 Planning and Environmental Linkages Study. CDOT will be completing a US Highway 24 corridor improvement project that will widen the roadway to four lanes from Garrett Road to Woodmen Road. Construction is expected to begin in 2025.

Woodmen Road is a four-lane east/west Expressway that ends at the intersection with US Highway 24. The intersections of Woodmen Road with Meridian Road, McLaughlin Road, and US Highway 24 are all signalized.

Meridian Road is a four-lane north/south Principal Arterial. Meridian Road (the arterial roadway portion) extends north from Falcon Highway to Hodgen Road. Note: the US Hwy 24/Old Meridian Road intersection was converted to a right-in/right-out intersection.

McLaughlin Road is a two-lane, Non-Residential Collector road that extends north from Rolling Thunder Avenue to Eastonville Road. The roadway provides retail and residential access, both north and south of Woodmen Road.

Rio Lane and Rio Road are two-lane Rural Local roadways that connect US Hwy 24 to Falcon Highway. The roadways are about 24 feet wide. The intersection with US Hwy 24 is stop-sign controlled. The intersection with US Hwy 24 is planned to be closed and the new internal roads planned as part of this development will serve as the replacement connection to US Hwy 24.

## Existing Traffic Volumes

Figure 4a shows the results of recent morning and afternoon peak-hour turning-movement traffic counts at the intersections of Woodmen Road/US Hwy 24, US Hwy 24/ Meridian Road, US Hwy 24/"Old" Meridian Road, Woodmen/McLaughlin, Woodmen/Meridian, and Rio Lane/US Hwy 24. The intersection-traffic counts were collected recently in May 2023.

## Existing Levels of Service

Level of service (LOS) is a quantitative measure of the level of delay at an intersection. Level of service is indicated on a scale from "A" to "F." LOS A represents control delay of less than 10 seconds for unsignalized and signalized intersections. LOS F represents control delay of more than 50 seconds for unsignalized intersections and more than 80 seconds for signalized intersections. Table 1 shows the level of service delay ranges.

Table 1. Intersection Levels of Service Delay Ranges

|  | Signalized Intersections <br> Level of Service | Unsignalized Intersections <br> Average Control Delay <br> (seconds per vehicle) |
| :---: | :---: | :---: |
| A | Average Control Delay <br> (seconds per vehicle) <br> $(\mathbf{1} \boldsymbol{)}$ |  |
| B | 10.0 sec or less | 10.0 sec or less |
| C | $10.1-20.0 \mathrm{sec}$ | $10.1-15.0 \mathrm{sec}$ |
| D | $20.1-35.0 \mathrm{sec}$ | $15.1-25.0 \mathrm{sec}$ |
| E | $35.1-55.0 \mathrm{sec}$ | $25.1-35.0 \mathrm{sec}$ |
| F | $55.1-80.0 \mathrm{sec}$ | $35.1-50.0 \mathrm{sec}$ |
| 80.1 sec or more | 50.1 sec or more |  |

(1) For unsignalized intersections, if $\mathrm{V} / \mathrm{C}$ ratio is greater than 1.0 the level of service is LOS F, regardless of the projected average control delay per vehicle.

Figure 4b presents the results of the existing intersection level of service analysis. The signalized intersections were analyzed using Synchro, while the unsignalized intersection of US Hwy 24/Rio Lane was analyzed based on the unsignalized method of analysis procedures from the Highway Capacity Manual, $6^{\text {th }}$ Edition by the Transportation Research Board. The level of service reports are attached.

## Woodmen Road/Meridian Road

The signalized intersection of Woodmen/Meridian is currently operating at an overall LOS C during the morning peak hour and an overall LOS D during the afternoon peak hour. Some of the left-turn movements are currently operating at LOS E during the peak hours.

## Woodmen Road/McLaughlin Road

The signalized intersection of Woodmen/McLaughlin is currently operating at an overall LOS B during the morning peak hour and an overall LOS C during the afternoon peak hour.

## Woodmen Road/US Highway 24

The signalized intersection of Woodmen/US Hwy 24 is currently operating at an overall LOS C during both the morning and afternoon peak hours.

## US Highway 24/Meridian Road

The signalized intersection of US Hwy 24/Meridian is currently operating at an overall LOS B during the morning peak hour and an overall LOS D during the afternoon peak hour. During the afternoon peak hour, the existing single northeast-bound left-turn lane is operating at LOS F and the southwest-bound through movement is operating at LOS E.

## US Highway 24/Rio Lane

The southwest-bound through/left at the stop-sign-controlled intersection of US Highway 24/Rio Lane currently operates at LOS B or better during the peak hours. The shared northwest-bound left-/right-turning movement on Rio Lane operates at LOS F during the peak hours. The levels of service F for this movement are due both to the volume of left-turning vehicles and the high volume of through vehicles on US Highway 24.

## TRIP GENERATION

Estimates of the vehicle trips projected to be generated by the proposed development have been made using the nationally-published trip-generation rates from Trip Generation, $11^{\text {th }}$ Edition, 2021 by the Institute of Transportation Engineers (ITE). Table 2 (attached) presents the estimated trip generation for The Commons at Falcon Field development.

## Internal Trips

Internal trips are trips that occur within a development and do not impact the external roadways. Because the site is planned to have multiple retail pads and housing, some of the generated trips will be traveling within the site. Table 2 includes estimates of internal trip capture to account for trips generated within the site. The internal trips were estimated using the NCHRP 684 Internal Trip Capture Estimation Tool. The results of the tool are attached.

## Total External Trip Generation

Approximately 6,825 total external daily trips are projected to enter and exit the site at the access point ("driveway trips") on the average weekday. During the morning peak hour, approximately 118 vehicles would enter and 142 vehicles would exit the site. During the evening peak, approximately 288 vehicles would enter and 254 vehicles would exit.

## Pass-by and Diverted Trips

The trips generated by the commercial portions of the site have also been aggregated by trip type to account for the pass-by phenomenon. A pass-by trip is one made by a motorist who would already be on an adjacent road regardless of the proposed development, but who stops in at the site while passing by. The pass-by motorist would then continue on his or her way to a final destination in the original direction. For purposes of this report, pass-by trips are trips by motorists already traveling through the intersection of US Highway 24/Woodmen Road.

Because the site is near the intersections of US Hwy 24/Falcon Hwy and US Hwy 24/Meridian Road, vehicles traveling through these intersections, but not through the intersection of US Hwy 24/Woodmen Road may still stop at the site on the way to their destination. Because these intersections are not directly adjacent to the site, these trips would be considered "diverted trips," based on ITE terminology, and therefore are referred to as such in this report. These trips would result in altered turning movements at the nearby major intersections of US Hwy 24/Falcon Hwy, US Hwy 24/Meridian Road, and Woodmen Road/Meridian Road and new turning movements at the intersection of US Hwy 24/Woodmen Road. In addition, it has been assumed that some of these diverted trips coming to and from Falcon Hwy to the east will use Rio Road and Rio Lane to access the site.

## Total External "New" Trip Generation

Estimates of Pass-by and diverted trips are shown in Table 2 and are based on Trip Generation Handbook - An ITE Proposed Recommended Practice, 3rd Edition, 2014 by ITE. The table shows the resulting external "new" trip generation, which reflects the subtraction of passby trips. Diverted trips are shown as "new" trips, as diverted trips will result in trips added to the Woodmen/US Hwy 24 intersection. Note that many of the diverted trips would not generally represent "new" trips at some off-site intersections - such as US Hwy 24/Meridian and Woodmen/Meridian - although some turning movements would be altered as part of travel route diversions.

## Trip Generation Comparison

Table 2 also includes comparison to the estimate presented in the 2022 property rezone TIS, dated December 15, 2021. About 220 fewer daily external vehicle trips are estimated to be generated, based on the currently-proposed site plan, than were assumed in the previous report.

## TRIP DISTRIBUTION

An estimate of the directional distribution of site-generated vehicle trips to the study-area roads and intersections is a necessary component in determining the site-generated traffic volumes. Figure 5 shows the directional-distribution estimate for the primary site-generated trips. The figure shows the percentages of the site-generated vehicle trips (primary trips) projected to be
oriented to and from the site's major approaches. Estimates have been based on the following factors: traffic counts conducted at major intersections adjacent to the proposed development, the proposed land uses, the access plan, the area road system serving the site, the site's geographic location, and previously-conducted LSC studies in the vicinity.

The directional-distribution estimates for primary trips are based on the anticipated service area for the retail portion of the development. This commercial center will primarily serve the Falcon area. The higher percentages for Meridian Road north of Woodmen, McLaughlin Road north of Woodmen Road, and US Hwy 24 east of the site reflect the higher current density of "rooftops" and the anticipated growth areas to the north and northeast. The ten-percent split is associated with current residential development and potential future developments to the east (Falcon Highway corridor) and southeast. The five-percent split to/from the southwest on US Hwy 24 (primary trips, like the other directional splits) is intended to account for some future Banning Lewis Ranch connections to US Hwy 24 and potentially some trips from the Cimarron Hills area (likely limited by the longer trip length and availability of retail shops in the Powers Boulevard corridor). The six-percent split to/from west Rolling Thunder Way reflects the residential development in that direction. While the seven-percent split to/from west Woodmen Road accounts for some traffic coming from areas to the west, including northern Colorado Springs, via this route.

Additionally, Figure 5 shows what percentage of overall pass-by and diverted trips have been pulled from each turning movement at the affected intersections to be rerouted as part of the site-generated traffic.

For the residential portion of the development, the directional distribution of the trips is based on residential-oriented destinations during peak hours, such as places of employment, shopping centers, schools, etc. It is anticipated that most trips will travel to/from the west either via Woodmen Road or US Hwy 24, as most retail and employment centers are to the west. Most of the remaining trips are expected to go to/from the north and east via US Hwy 24, McLaughlin Road, and Meridian Road.

## Site-Generated Traffic

Site-generated traffic volumes for the development during the weekday morning and evening peak hours are shown in Figure 6 for the following intersections:

- Woodmen Road/US Highway 24
- Woodmen Road/Meridian Road
- Woodmen Road/McLaughlin Road
- US Highway 24/Meridian Road
- US Highway 24/Old Meridian Road
- Internal roundabout
- Internal access points

Site-generated traffic volumes have been calculated by applying the directional-distribution percentages estimated by LSC (from Figure 5) to the trip-generation estimates (from Table 2). The pass-by trips and diverted trips were assigned, based on the magnitude and direction of the peak-hour traffic volumes projected for the major study-area streets/roads.

## BACKGROUND TRAFFIC VOLUMES

Background traffic is traffic on the adjacent roadways that is forecast to be present without the proposed development. Short-term and 2044 background traffic scenarios were developed.

Both future forecasts also assume that the intersection of US Hwy 24/Rio Lane has been closed and the associated traffic has been re-routed. Because Rio Lane will no longer directly access US Hwy 24, LSC projects that some of the trips currently using Rio Lane and Rio Road will reroute and use Falcon Hwy or Meridian Road to access US Hwy 24.

## Short Term

Figure 7 shows the estimated short-term background traffic volumes at the study-area intersections. The short-term background volumes assume that the US Hwy 24/Rio Lane intersection has been closed and traffic has been rerouted through the new fourth leg of the US Hwy 24/Woodmen Road intersection.

## Long Term

Figure 8 shows the estimated 2044 background traffic volumes. These projected volumes include estimates from planned future Falcon area development and increases in through traffic volumes on the study-area roadways. The 2044 background volumes were developed using the US Highway 24 PEL study. Volumes were modified as needed, based on newer count volumes and expected development in the study area. The 2044 background assumes future commercial development on the parcel to the west of the site with access through the proposed The Commons at Falcon Field development and the internal roundabout.

## TOTAL TRAFFIC VOLUMES

Site-generated traffic volumes from Figure 6 were added to short-term background traffic volumes from Figure 7 to calculate short-term total traffic volumes provided in Figure 9. Similarly, 2044 total traffic volumes provided in Figure 10 were calculated by adding the site-generated traffic (Figure 6) with the 2044 background traffic volumes (Figure 8).

## LEVEL OF SERVICE ANALYSIS

Levels of service were calculated for both the short-term background, 2044 background, short-term total traffic, and 2044 total traffic volumes. The results of the analysis are shown in Figures 7, 8, 9, and 10. Traffic lanes used in the analysis are also provided in these figures.

## Woodmen Road/Meridian Road

The signalized intersection of Woodmen/Meridian is projected to at an overall LOS C during the morning peak hour and an overall LOS D during the afternoon peak hour, based on both the short-term background and total traffic volumes. Some of the left-turn movements are projected to operate at LOS E during the peak hours, based on both the short-term background and total traffic volumes. By 2044, some of the through movements are projected to operate at LOS E and some of the left-turn movements are projected to operate at LOS F, based on both the 2044 background and total traffic volumes.

## Woodmen Road/McLaughlin Road

The signalized intersection of Woodmen/McLaughlin is projected to operate at an overall LOS D or better during the morning and afternoon peak hours, based on the short-term background, 2044 background, short-term total, and 2044 total traffic volumes.

## US Highway 24/Woodmen Road

In the short-term scenarios, it has been assumed that no baseline capacity improvements (additional northeast-bound/southwest-bound through lanes) will occur on US Hwy 24. However, per recent meetings with CDOT, coordination will continue as this project and the adjacent Highway 24 CDOT project move forward. Cooperation with respect to phasing of improvements, such as potential future use of eastbound right-turn deceleration and acceleration lanes that may be built by this project as future through lanes. The CDOT project would then add new lanes to replace them (for example). The improvements based on the Access Code and CDOT direction provided thus far at the intersection of US Hwy 24/Woodmen Road would include:

- The new fourth northwest bound leg of the intersection with a left lane, two through lanes, and right lane;
- Auxiliary turn lanes on US Hwy 24 to serve the trips/vehicle turning movements associated with the new fourth leg - the development, and the "replacement" Rio Lane connection;
- Raised right-turn islands for pedestrian accessibility;
- Lane alignment and median modifications on the existing south-east bound leg of the intersection to align with the new fourth leg. Note: The laneage is shown in Figure 11b.
- Signal modifications including installation of any traffic-signal components (including new signal pole(s) on the Woodmen side of the intersection) needed to accommodate the new intersection leg.

Overall, the signalized intersection is forecast to operate at LOS C or better during both peak hours in both the short-term background and short-term total scenarios.

By 2044, it has been assumed that US Hwy 24 will be widened to provide northeast-bound and southwest-bound through lanes per meetings with CDOT regarding the upcoming CDOT Highway 24 project. Overall, the signalized intersection is forecast to operate at LOS D or better during both peak hours in both the 2044 background and 2044 total scenarios.

## US Highway 24/Meridian Road

As shown in Figure 4a, the existing northeast-bound left-turn volume at the intersection of US Hwy 24/Meridian is 608 vehicles per hour during the afternoon peak hour. As dual left-turn lanes are typically considered when the left-turn volume exceeds 300 vph , it has been assumed that a second northeast-bound left-turn lane will be constructed in the short term (Potentially, this may be completed as part of the upcoming CDOT Highway 24 project). With the addition of a second turn lane, all movements at this intersection are projected to operate at LOS D or better during the peak hours, based on both the short-term background and short-term total traffic volumes.

By 2044, it has been assumed that US Hwy 24 will be widened to provide northeast-bound and southwest-bound through lanes. Overall, the signalized intersection is forecast to operate at LOS D or better during both peak hours in both the 2044 background and 2044 total scenarios.

## Woodmen Road/Retail Row Street

The proposed roundabout at the intersection of Woodmen Road/Retail Row Street has been analyzed using Sidra. The roundabout is expected to have all approaches operate at LOS A during both peak hours, based on the projected short-term and 2044 total traffic volumes.

## Retail Row Site-Access Points

The access points to the Retail Row Street have been analyzed as stop-sign-controlled (unsignalized) intersections. All yielding turning movements at the proposed access points are anticipated to operate at LOS C or better through 2044.

## Rio Lane Access Points

The proposed intersections of Rio Lane/Perula Lane, Rio Lane/Jacamar Way, and Rio Lane/Toddy Way been analyzed as stop-sign-controlled (unsignalized) intersections. All approaches are projected to operate at LOS B or better during the peak hours, based on the short-term total and 2044 total traffic volumes.

## QUEUING ANALYSIS

A queuing analysis was performed using Synchro/SimTraffic for the key approach turning movements at the intersection of US Hwy 24/Woodmen Road and the proposed Retail Row Street access points to determine the projected queue lengths, based on the 2044 total traffic volumes. The simulation was run five times. The queuing reports are attached. These queuing results have been used to develop auxiliary turn-lane recommendations. The results of the analysis are shown in Figure 11a and Table 3.

## INTERSECTION AND AUXILIARY TURN LANE RECOMMENDATIONS

The El Paso County Engineering Criteria Manual (ECM) and the Colorado State Highway Access Code standards were used as a basis for the following turn-lane and other recommendations at the intersections.

## US Highway 24/Woodmen Road

Figure 11b provides the recommendations for improvements at the intersection of US Highway 24/Woodmen Road, including auxiliary turn-lane dimensions and modifications needed with the new fourth leg of the intersection of US Hwy 24/Woodmen Road.

## Retail Row Intersections

Figure 11c shows the recommended turn-lane lengths at the proposed internal intersections/access points to Retail Row Street.

## Right-In-Only Access Point

Figures $2 a$ and $2 b$ show the proposed right-in-only access point to Woodmen Road, including the access spacing details. The proposed right-in-only access point would provide a low-impact, lowconflict secondary entry point to the commercial lot areas west of Woodmen.

The proposed right-turn lane would have abbreviated lane and taper lengths. The ECM standard is 155 -foot lane plus 160 -foot taper, plus storage. Figure 11d (a copy of Deviation Exhibit 2a-1 from Deviation 2a) shows the proposed lengths. The lane would be about 130 feet plus a 55 -foot
bay taper. The abbreviated length will be mitigated by the proposed 50 -foot corner radius. Please refer to Deviation No. 3, which addresses turn lane design.

The assumption is that site plans for specific development served by the proposed right-in-only access point will be designed such that traffic entering via the proposed right-in-only access will have a "free movement" onto internal private-access drives, parking bays, etc., such that queues will not form and back into the right-in access point or the main entry street (Woodmen Road). This would likely be accomplished with a sufficient entry "throat" and other site-plan-level design elements that would give priority to entering traffic. Please refer to the deviation request for the right-in-only access for additional details.

## ROADWAY SEGMENT IMPROVEMENTS

## Rio Lane

As identified above, Rio Lane and Rio Road are two-lane Rural Local roadways that connect US Hwy 24 to Falcon Highway. The roadways are 24 feet wide and were recently paved.

The project will generate trips using Rio Lane between Falcon Highway and the site, but it is important to note that the daily volume has already reduced with the opening of New Meridian Road north of Falcon Highway. Closing the direct Rio Lane connection to US Highway 24, the route used by cut-through traffic will create a significantly more circuitous route and will likely discourage some motorists continue to use Rio Lane as a cut-through route between Falcon Highway and US Highway 24.

The projected net volumes presented in this report are the estimated current volume (1,700 vehicles per day) plus increases due to site-generated traffic minus estimated reductions in cutthrough traffic and redistribution of area resident traffic (due to the closure of the direct connection of Rio Lane to US Hwy 24). There will be an overall net decrease from the 2021 volume of 2,700 vehicles per day shown in the January 2022 rezone report.

The current roadway cross section will be sufficient for accommodating the resulting net vehicular traffic volumes on Rio Lane and Rio Road. Given the large adjacent lots and driveway lengths, on-street parking, while allowed, is likely infrequent. Widening the drivable pavement width of Rio Road has the potential to encourage higher speeds. Therefore, any future enhancements/upgrades should be for non-motorized use (pedestrians and bicycles) that would fit within the right-of-way. Rio Road has a straight alignment, and the vertical profile is relatively level, which both allow for good sight distance.

Working within the available right-of-way, it may be feasible to add enhancements for pedestrians/bikes by creating segments of north-south gravel, separated pedestrian path combined with segments of widened gravel shoulder. Widened shoulders would provide
additional space for pedestrians, but do not offer physical protection. This project will be installing a sidewalk along the south side of the east-west segment adjacent to the site frontage and on both sides of the street for the section within the site. The project will also provide a street stub to Pinto Pony Road that could be used as a pedestrian collection to Chief Road and Pinto Pony Road.

Other measures to enhance pedestrian safety could potentially include roadway illumination. However, it is not likely practical or desirable to the area residents to improve pedestrian visibility with roadway illumination. Measures to educate and encourage the use of flashing LED lights, retroreflective clothing, vests, armbands etc. by local-residents clothing or armbands should be considered. Signs along the roadway could be placed to remind area residents and other users of the roadway for non-motorized travel, to wear retro-reflective gear.

## Retail Row Street

Aside from the extension of Woodmen Road into the site from the US Highway 24 intersection, Retail Row Street will be the main internal street serving the commercial and residential development, it will also provide the replacement Rio Lane connection to US Highway 24.

Retail Row Street is proposed as a Non-Residential Collector with a modified cross-section. Please refer to the Intersection improvements section for intersection recommendations. Please refer to deviation request No. 5 for details regarding the proposed cross section and other planning and design details.

## Jackdaw Point, Perula Way and Dunlin Heights

Direct access to the individual commercial lots would be via three private commercial streets shown on the Preliminary Plan (Jackdaw Point, Perula Way and Dunlin Heights). The Preliminary Plan has been revised since the last submittal to show the private streets on the east side (Perula Way and Jackdaw Point) meeting County Urban Local street standards with widths of 30 feet of pavement plus curb and gutter (34-feet of width flowline-to-flowline), with attached 5-foot-wide sidewalks.

## DEVIATIONS TO ECM CRITERIA

The following deviations to the criteria contained in the El Paso County Engineering Criteria Manual (ECM) have been recently submitted as part of this application:

- Public street intersection spacing along an Urban Non-Residential Collector - Woodmen Road (proposed) southeast of US Highway 24/Retail Row Street
- Right-in-Only access to an Urban Non-Residential Collector
- Full-movement access to an Urban Non-Residential Collector;
- ECM-standard auxiliary turn-lane lengths on an Urban Non-Residential Collector.
- Modification to the design standards of an Urban Non-Residential Collector Street (Retail Row Street)


## ROADWAY CLASSIFICATIONS

- The streets proposed for this project would be classified as either Urban Non-Residential Collector or Urban Local or "private commercial (Urban Local)" streets. Please refer to Figure 12, which presents the recommended classifications for the proposed streets shown on the Preliminary Plan. The figure also shows the classification of the adjacent existing roadways as described in the "Existing Roadways" section.


## MTCP-IDENTIFIED FUTURE NEEDED ROADWAY IMPROVEMENT PROJECTS

- The El Paso County Major Transportation Corridors Plan (MTCP) calls for improvement to US Hwy 24 from Garrett Road to Woodmen Road and upgrade to a rural six-lane Principal Arterial. As mentioned in the "Existing Roadways" section above, CDOT will be completing a US Hwy 24 corridor improvement project that will widen the roadway to four lanes from Garrett Road to Woodmen Road. Construction is expected to begin in 2025.
- Although not in the immediate area, the MTCP calls for an upgrade to Falcon Highway to a two-lane, rural Minor Arterial from US Hwy 24 to one mile east of Curtis Road. Also, the MTCP calls for an upgrade to Eastonville Road from McLaughlin to Latigo Boulevard as a rural road upgrade to a two-lane Rural Minor Arterial.
- The project would need to construct a sidewalk or potentially a multi-use trail, along the north side of Woodmen Road between the US Hwy 24 intersection and the current sidewalk located about 450 feet northwest of US Hwy 24. This point is adjacent to the connection.


## MULTI-MODAL TRANSPORTATION \& TRANSPORTATION DEMAND MANAGEMENT OPPORTUNITIES

- The following section describes the details of a pedestrian/bicycle connection between this project and the Rock Island Trail.
- Trail connections exist between the Rock Island Trail and the Woodmen Hills neighborhoods to the north of US Highway 24.
- A Park \& Ride facility has been developed nearby at the intersection of Meridian Road and Swingline Road. Future Mountain Metropolitan Transit bus service may be added to/from this Park \& Ride location.


## PEDESTRIAN \& BICYCLE FACILITIES

- The project would include urban street sections with sidewalks.
- Figure 11a shows the recommendation for curbed right-turn pedestrian islands. The traffic signal would be modified to provide full pedestrian access on all four legs of the intersection. These details would be shown as part of the traffic-signal modification plan
and the intersection-improvement construction drawings. These design details and plans would be part of the access permit process with CDOT and would need CDOT approval prior to issuance of a NTP (Notice-to-proceed).
- The project would need to construct a sidewalk or potentially a multi-use trail, along the north side of Woodmen Road between the US Highway 24 intersection and the current sidewalk on the north side of Woodmen Road, which currently ends about 450 feet northwest of Highway 24. This point is adjacent to the connection to the Rock Island Trail.
- Improvements to Rio Lane along the site frontage (sidewalk along the south side of the roadway adjacent to the site and on both sides of the street for the section within the site (development on both sides).
- "Rio Road"
- School Pedestrian Routes
- School pedestrian connection to Falcon Elementary School: Potentially, a pedestrian connection could be implemented to connect to the northeast corner of the school district property, along with a pedestrian path to the school on the school district property. However, about 140' of private property lies between the southeast corner of this project and the northeast corner of the school district property.
- If the above plan is not workable, the Preliminary Plan shows pedestrian connections to Rio Lane and Pinto Pony Road. Pinto Pony Road connects to Chief Road, which extends south to Falcon Highway. Pinto Pony Road and Chief Road are low volume, rural gravel roadways. Consideration could be given to providing a gravel-surface, pedestrian path/trail, with sufficient separation from the edge of the roadway along the north side of Falcon Highway between Chief Road and the school. Note: currently, there are almost no pedestrian facilities within the school district property and no sidewalks along Falcon Highway.


## COUNTY ROAD IMPROVEMENT FEE PROGRAM

- This project is subject to participation in the County Roadway Improvement Fee Program.


## US HIGHWAY ACCESS MANAGEMENT PLAN AND RIO LANE CLOSURE AT US HIGHWAY 24

- This project will implement part of the US Highway Access Management Plan. The intersection of Rio Lane/US Highway 24 is proposed to be closed, as shown in the adopted US Highway 24 Access Management Plan and the US 24 Planning and Environmental Linkages Study, October 2017. The project will help implement the US Highway 24 Access Management Plan by providing an alternative to the Rio Lane/US Highway 24 intersection. Also, the Preliminary Plan shows a street connection (Retail Row Street) extending southwest from the roundabout to the property line. Note (6-7-2024): The CDOT comment letter dated April 17, 2024 indicated: "It is imperative for El Paso County to work with the Falcon Fields Development to create a southern connection from the end of the southwestern leg off the proposed roundabout to Swingline Rd." The
applicant has no control over property to the southwest but provides the street stub to allow for a future street connection to the adjacent property.
- The site plan shows the proposed internal public streets for site circulation and the new connection to Rio Lane that would allow for the prescribed closure of the US Highway 24/Rio intersection, per CDOT’s US Highway 24 Access Management Plan.
- This will benefit safety and traffic operations on US Highway 24. The existing Rio Lane/US Highway 24 intersection is substandard, as there are no left- and right-turn lanes. The level of service during the peak hour is LOS F (96 seconds of delay per vehicle on average for vehicles wanting to turn onto US Highway 24).
- The project will generate trips using Rio Lane and Rio Road between Falcon Highway and the site, but it is important to note that by closing the direct Rio Lane connection to US Highway 24, the route used by cut-through traffic will be significantly more circuitous and will likely discourage motorists who currently use Rio Lane and Rio Road as a cut-through route to Falcon Highway.
- The recently completed Meridian Road extension south of Rolling Thunder, across US Highway 24 to Falcon Highway has improved the roadway connectivity to Falcon Highway (and traffic volumes show a resulting reduction in volume on Rio Lane and Rio Road).
- The County has indicated that they will require upgrades to Rio Lane and Rio Road, necessary to accommodate the resulting net traffic volumes on Rio Lane and Rio Road between Falcon Highway and the site. The details of recommended upgrades are included in the section above.
- The project will add a signal-controlled connection to US Highway 24 and Woodmen - not only for this development but also for the benefit of the residents in Falcon Ranch Estates and Arrowhead Estates Filing No. 1. This connection will have left- and right-turn lanes on US Highway 24.
- The proposed roundabout is proposed to be constructed as a T-intersection (no south leg). However, a fourth (south) leg could be added in the future if/when adjacent propert(ies) southeast of The Commons at Falcon Field redevelop in the future. The applicant will reserve land southeast of the roundabout as right-of-way preservation for a potential future extension to the adjacent property, if ever needed.


## ROUNDABOUT ANALYSIS \& DESIGN

A modern roundabout with a 180-foot inscribed circle diameter is proposed as the traffic control for the intersection of Woodmen Road/ Retail Row Street. Roundabout exhibits containing roundabout technical analysis are attached, along with a roundabout parameters table.

The horizontal layout and analysis exhibits have been completed using the criteria contained in the Wisconsin Department of Transportation roundabout design manual (as required by El Paso County). The attached roundabout exhibits and roundabout parameters table contain all the details for the currently proposed roundabout. The inscribed circle diameter is 180 feet and the design vehicles are a WB-50 truck and an El Paso County standard snowplow vehicle (per the ECM). However, the roundabout has also been designed to accommodate a larger WB-67 truck.

The roundabout will also accommodate the standard county snowplow vehicle. The roundabout will accommodate pedestrians and bicyclists. Please refer to the attached roundaboutparameters table and exhibits for details. The final roundabout design report will be submitted following the review and County staff acceptance of the horizontal layout shown on attached exhibits.

## CDOT ACCESS PERMITTING

CDOT access permits will be required for the street connection to the US Highway 24/Woodmen Road intersection and for the closure of Rio Lane at US Highway 24. Per recent meetings with CDOT, coordination will continue as this project and the adjacent Highway 24 CDOT project move forward.

## CONCLUSIONS AND RECOMMENDATIONS

## Trip Generation

- The Commons at Falcon Field is expected to generate about 3,592 new external vehicle trips on the average weekday, with about half entering and half exiting the site during a 24-hour period. During the morning peak hour, about 118 vehicles would enter and 142 vehicles would exit the site. During the afternoon peak hour, approximately 288 vehicles would enter and 254 vehicles would exit the site.


## Traffic Operations Analysis

- The signalized intersection of US Highway $24 /$ Woodmen Road is projected to operate at LOS D or better during both peak hours for the short-term and year-2044 scenarios. The El Paso County Engineering Criteria Manual (ECM) standards were followed to develop turn-lane recommendations at the intersections. Figure 11a provides the turn-lane conceptual design for this intersection. Please refer to the Level of Service and Queuing Analysis sections of this report for additional details and discussion.


## Recommended Improvements

- A list of recommended improvements within the site and in the study area is presented in Table 4.
- The intersection of US Highway $24 /$ Rio Lane is to be closed and the proposed Collector roads within the site will connect Rio Lane to the US Highway 24/Woodmen intersection.

Short-term improvements assumed at the intersection of US 24/Woodmen Road would include:

- The fourth leg of the intersection with a northwest-bound left-lane, two northwest-bound through-lanes, and northwest-bound right-lane as shown in Figure 11b;
- Raised right-turn islands for pedestrian accessibility;
- Lane alignment and median modifications on the existing northwest of the intersection as shown in Figure 11b;
- Signal modifications including installation of traffic-signal components needed for the new leg; and
- Auxiliary turn lanes on US Highway 24 to serve the trips/vehicle turning movements associated with the new fourth leg of this intersection. This new fourth leg would serve site traffic and background traffic shifted from the closure of the US Highway 24/ Rio Lane connection.

Based on the 2044 total traffic volumes shown in Figure 10 and the criteria contained in the State of Colorado Highway Access Code, the following deceleration and acceleration lanes are required on US Highway 24:

- A northeast-bound right-turn deceleration lane is warranted on US Highway 24 approaching Woodmen Road. Based on a posted speed limit of 55 mph , the prescribed lane length for the deceleration lane is 600 feet plus a 222 -foot taper.
- A southwest-bound left-turn deceleration lane is warranted on US Highway 24 approaching Woodmen Road. Based on a posted speed limit of 55 mph , the prescribed lane length for the deceleration lane is 600 feet plus 100 feet of storage and a 222 -foot taper.
- A northwest-bound right-turn acceleration lane is warranted on US Highway 24 east of Woodmen Road. Based on a posted speed limit of 55 mph , the prescribed lane length for the acceleration lane is 960 feet plus a 222-foot taper.

Based on the 2044 total traffic volumes shown in Figure 10 and the criteria contained in the ECM, the following deceleration and acceleration lanes are required on Retail Row Street:

- A southwest-bound left-turn lane is warranted on Retail Row Street approaching Nunbird Court. Based on a design speed limit of 25 mph , the ECM-required lane length would be 115 feet for deceleration, 50 to 75 feet for storage, and an 80-foot taper. Based on the available lane length and the $95^{\text {th }}$ percentile queue length analysis results shown in Figure 11a, LSC recommends a 100-foot left-turn lane plus 65-foot reverse curve bay taper.
- A northeast-bound left-turn lane is not projected to be warranted on Retail Row Street approaching Dunlin Heights. However, this lane will be needed to algin with the recommended left-turn lane approaching Nunbird Court. Based on a design speed limit of 25 mph , the ECM-required lane length would be 115 feet for deceleration, 50 to 75 feet for storage, and an 80-foot taper. Based on the available lane length and the $95^{\text {th }}$ percentile queue length analysis results shown in Table 3, LSC recommends a 165-foot left-turn lane plus 80-foot taper.
- A northeast-bound left-turn lane is projected to be warranted on Retail Row Street approaching. Based on a design speed limit of 25 mph , the ECM-required lane length would be 115 feet for deceleration, 100 feet for storage, and an 80-foot taper. Based on
the available lane length and the $95^{\text {th }}$ percentile queue length analysis results shown in Table 3, LSC recommends a 120 -foot left-turn lane plus a 50 to 75 -foot reverse curve bay taper.

Please contact me if you have any questions regarding this report.
Sincerely,

LSC TRANSPORTATION CONSULTANTS, INC.
By: Jeffrey C. Hodsdon, P.E.
Principal
JCH/KDF/JAB:jas
Enclosures: Tables 2-4
Figures 1-12
AutoTurn Exhibits 1-5
Roundabout Design Parameters Table
Roundabout Exhibits 1-9
Traffic Count Reports
Level of Service Reports
Queuing Report
NCHRP Report 684

References:
Trip Generation Handbook - An ITE Proposed Recommended Practice, Third Edition September 2017, Institute of Transportation Engineers
Trip Generation, $10^{\text {th }}$ Edition, 2017, Institute of Transportation Engineers
El Paso County Major Transportation Corridors Plan, 2016
Engineering Criteria Manual, 2016, El Paso County
NCHRP Report 684 Enhancing Internal Trip Capture Estimation for Mixed-Use Developments, 2011, Transportation Research Board
State Highway Access Code, Volume Two, 2002, Colorado Department of Transportation US 24 Access Control Plan, 2005
US 24/Meridian Road Construction Plans
US 24 PEL Final Corridor Conditions Report, December 2016

Tables 2-4


Table 3: Auxiliary Lane Analysis - Lane Dimensions and Projected Queues

| Intersection | Turning Movement | Recommended Length (feet) | ECM/CDOT Standard (feet) | Maximum Queue (feet) |
| :---: | :---: | :---: | :---: | :---: |
| US 24/Woodmen | Northwestbound Left* | 260 Decel + Storage 80 Bay Taper | 155 Decel 150 Storage 160 Bay Taper | 137 |
|  | Northwestbound Through | 260 (second through lane) | --- | 196 |
|  | Northwestbound Right | 260 Decel | 155 Decel | 0 |
|  | Northeastbound Right (Accel) | 960 Accel 225 Taper | 960 Accel 225 Taper | --- |
|  | Northeastbound Right | 600 Decel 225 Taper | 600 Decel 225 Taper | 64 |
|  | Southwestbound Left | 600 Decel <br> 100 Storage <br> 225 Taper | 600 Decel 100 Storage 225 Taper | 255 |
| Retail Row St/ Dunlin Heights/ Nunbird Ct | Eastbound Left | 165 (Decel + Storage) 80 Bay Taper | 115 Decel 50 Storage 80 Bay Taper | <5 |
|  | Westbound Left | 100 (Decel + Storage) 65 Bay Taper | 115 Decel 50 Storage 80 Bay Taper | 46 |
| Retail Row St/ Jackdaw Point | Eastbound Left | 120 (Decel + Storage) 50-75 Bay Taper | 115 Decel 100 Storage 80 Bay Taper | 36 |

Table 4. Recommended Improvements

| Item \# | Improvement | Timing | Responsibility |
| :---: | :---: | :---: | :---: |
| Roadway Segment Improvements |  |  |  |
| 1 | Construct Retail Row Street as an Urban Non-Residential Collector with a modified cross section | With the subdivision (plat) | Applicant |
| 2 | Rio Lane: add sidewalk, curb and gutter along Rio Lane adjacent to the site as shown on the Preliminary Plan; Please refer to the Rio Lane and Rio Road section of the narrative. | With adjacent development | Applicant |
| 3 | Widen US Highway 24 to provide two through lanes in each direction from Garrett Road to east of Woodmen Road, plus associated/other corridor improvements. | Per recent meeting with CDOT: Construction to begin 2025. | CDOT/US Highway 24 project |
| US Highway 24/Woodmen Road Intersection |  |  |  |
| 4 | Extend the southwestbound left-turn deceleration lane plus transition taper on US Hwy 24 (westbound) approaching Woodmen Road to 700 feet. This requires widening of the box culvert under US Hwy 24 just west of the US Hwy 24/Rio Lane intersection. | With site development, when the peakhour volume for this movement exceeds 10 vph <br> Requires the closure of Rio Lane | Applicant |
| 5 | Potential future lengthening/extension of the southwestbound right-turn deceleration lane on US Highway 24 at Woodmen Road to CDOT standards ( 600 feet plus transition taper). | To be determined by CDOT | CDOT (potentially as part of the US Highway 24 project) Note: any additional cost associated with any culvert widening needed specifically for the right-turn lane, and the lengthening of the right turn lane itself should not be the responsibility of this applicant. |
| 6 | Construct a 600 foot-long northeastbound right-turn deceleration lane plus transition taper on US Hwy 24 (eastbound) approaching Woodmen Road | With site development, when the peakhour volume for this movement exceeds 10 vph | Applicant |
| 7 | Construct a northwestbound right-turn acceleration lane on US Hwy 24 (eastbound) from the Woodmen Road intersection. Rio Lane would be closed with the added southern leg of the Woodmen/US Hwy 24 intersection and this will allow for the fulllength, CDOT standard acceleration lane. | With site development, when the peakhour volume for this movement exceeds 10 vph | Applicant |
| 8 | Construct a 960 foot-long northwestbound right-turn acceleration lane (plus transition taper) on US Hwy 24 (eastbound) east of Woodmen Road. | With the closure of Rio Lane | Applicant |
| 9 | Construct the southeast leg of the intersection. as shown in Figure 11b. Modify the northwest leg of this intersection such that lanes need to align across US Hwy 24 (also shown in Figure11b) (within allowable/acceptable lane offset tolerances and considering protected/permissive left-turn sight distance and left-turning vehicle paths). | With the subdivision (plat) | Applicant |
| 10 | Construct 260' northwestbound left-turn lane plus 80' Taper. | With the subdivision (plat) | Applicant |
| 11 | Construct 260' northwestbound right-turn decleration lane plus 80' Taper. | With the subdivision (plat) | Applicant |
| 12 | Modify the northwest leg (Woodmen Road) as needed so lanes align across US Hwy 24; construct raised/curbed right turn islands for pedestrians and for installing a signal pole on the northeast corner, construct a sidewalk connection to the Rock Island Trail (which connects to the sidewalk along the north side of Woodmen Road adjacent to the Falcon Town Center (Safeway). | With the subdivision (plat) | Applicant |
| 13 | Traffic signal system modifications, pedestrian accommodations, signing/striping improvements to convert the existing intersection from a T intersection to a four-leg intersection. | With the subdivision (plat) | Applicant |
| Retail Row Street |  |  |  |
| 14 | Construct a modern roundabout at Woodmen/Retail Row Street (See roundabout figures and design parameters table) | With the subdivision (plat) | Applicant |
| 15 | Construct 165 foot long northeastbound left-turn lane plus 80-foot taper on Retail Row Street approaching Dunlin Heights. | With the subdivision (plat) | Applicant |
| 16 | Construct 100 foot long southwestbound left-turn lane plus 65-foot reverse curve bay taper on Retail Row Street approaching Nunbird Court | With the subdivision (plat) | Applicant |
| 17 | Construct 120 foot long northeastbound left-turn lane plus 50 to 75 -foot reverse curve bay taper on Retail Row Street approaching Jackdaw Point | With the subdivision (plat) | Applicant |
| US Highway 24 Right-of-Way Dedication \& Preservation |  |  |  |
| 18 | CDOT required Right-of-way Dedication \& Preservation along US Highway 24 | With the subdivision (plat) | Applicant |
| US Highway 24/Rio Lane Intersection |  |  |  |
| 19 | Close intersection in conjuction with Improvement Nos. 1 and 9 | Short-Term - CDOT indicated at a recent meeting that the Rio Lane connection to Highway 24 will need to be closed with Improvement No. 9. | Applicant |
| Falcon Highway/Rio Lane Intersection |  |  |  |
| 20 | Construct westbound right-turn deceleration lane | Once westbound right-turning volume exceeds 50 right-turning vehicles per hour. | Applicant |
| Source: LSC Transportation Consultants, Inc. (6-7-2024) |  |  |  |

Figures 1-12




Available line of sight (passing over the proposed sidewalk)

Entering Sight Distance 280' (280' required based on a design speed of 25 mph )


(245') for the available line of sight. Exceeds the calculated sight distance requirement for a vehicle approach speed of $10-12 \mathrm{mph}$ ( $110^{\prime}-132$ '). For Single Unit Trucks: 125'-150'
Stopping sight distance (155') for a vehicle approaching at 25 mph . The distance to the downstream Willet Way
exceeds the stopping sight distance, so meets the
standard. This would be conservative, as the
approaching vehicle speed is $10-12 \mathrm{mph}$ at the
completion of the upstream cornering
maneuver/navigating the knuckle.

Required Stopping Sight

Calculated design speed of southbound to westbound vehicle traveling through this corner: $10-12 \mathrm{mph}$

Access Entering Sight Distance for Single-unit Trucks (325' from ECM Table 2-35 based on a posted speed of 25 mph which is just over the fastest path speed for the southbound to eastbound right turn in the roundabout (the R5 speed))*

EM Table 2-36 indicates for Commercial/Retail Access points with less than multi-unit trucks per day (average), use single-unit truck (which is shown on the exhibit).

There would be sufficient SSD for approaching vehicles should a multi-unit truck begin turning onto Retail Row St. from Dunlin Heights based on sight distance for single unit trucks.

Required Stopping Sight Distance (155' from ECM Table 2-17 based on a design speed of 25 mph )

Access Entering Sight Distance Access
 posted speed of 25 mph )

Note: based on AASHTO criteria, the departure sight distance to the left is $312^{\prime}$ for a design speed of 25 mph . [AASHTO Green Book Section 9.5.3.2.1

$$
n
$$

$\qquad$


Approximate
Scale

$$
1^{\prime \prime}=100^{\prime}
$$

Required Stopping Sight Distance (155' from ECM Table 2-17 based on a design speed of 25 mph )
















## AutoTurn Exhibits







## Roundabout Design Parameters Table

PCD File No．SP232
The Commons at Falcon Field
（LSC\＃S234220）
Woodmen Road \＆Retail Row Street
County：El Paso

## ROUNDABOUT CRITICAL DESIGN PARAMETERS

|  | LEG 1 | LEG 2 | LEG 3 | LEG 4 | LEG 5 |
| :--- | ---: | ---: | ---: | ---: | ---: |
|  |  |  |  | LEG 6 |  |
| DESIGN PARAMETERS | 18.0 | 18.0 | 18.0 |  |  |
| Approach Width，FT | 15.0 | 15.0 | 15.0 |  |  |
| Entry Width，FT | 14.5 | 36.0 | 31.0 |  |  |
| Entry Angle，PHI $\Phi$ ，DEG | 180.0 | 180.0 | 180.0 |  |  |
| Inscribed Circle Diameter，FT | 23.4 | 20.0 | 20.0 |  |  |
| Exit Width，FT | 18.0 | 18.0 | 18.0 |  |  |
| Circulating Roadway Width Upstream of Entry，FT |  |  |  |  |  |

## FASTEST SPEED PATH

| $R_{1}$ ，Radius／Speed，FT／MPH | 135 | 23 | 134 | 22 | 135 | 22 |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $R_{2}$ ，Radius／Speed，FT／MPH |  |  | 107 | 21 | 78 | 18 |  |  |  |  |  |  |
| $R_{3}$ ，Radius／Speed，FT／MPH | 900 | ＞40 | 850 | ＞40 | 345 | 31 |  |  |  |  |  |  |
| $R_{4}$, Radius／Speed，FT／MPH | 76 | 18 | 77 | 18 |  |  |  |  |  |  |  |  |
| $R_{5}$ ，Radius／Speed，FT／MPH | 130 | 22 |  |  | 110 | 21 |  |  |  |  |  |  |
| Bypass $R_{5}$ ，Radius／Speed，FT／MPH |  |  |  |  |  |  |  |  |  |  |  |  |

MINIMUM SIGHT PARAMETERS

| Approach Design Speed，MPH | 40.0 | 25.0 | 25.0 |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Horizontal Stopping Sight Distance，FT |  |  |  |  |  |  |  |
| Circulating Intersection Sight Distance，FT／MPH |  |  |  |  |  |  |  |
| Entering Intersection Sight Distance，FT／MPH |  |  |  |  |  |  |  |


| Design Vehicle： | WB－50，WB－67，EPC snowplow |  |
| :---: | :---: | :---: |
| Truck Apron Width： | 12＇ |  |
| OSOW Accommodations： | N／A |  |
| Circulating Roadway Cross－Slope： | 2\％or less |  |
| Access Control： | N／A |  |
| Parking Control： | No Parking |  |
| Bicycle \＆Pedestrian Accommodations： | Ped ramps and sidewalks |  |
| Designer：Matt Romero |  |  |
| Reviewer：Chris McGranahan，P．E．， | PTOE |  |
| ＊＊＊＊＊Preliminary＊＊＊＊＊＊＊＊ |  |  |
| SIGNATURE： | DATE： | 6／7／2024 |
| NAME：Christopher S．McGranahan，P．E． |  |  |
|  principals．The critical design elements have been addressed．The project design engineer in responsible charge of final plan development Lーーーーーーーーーーーーーーーーーーーーー will stamp the plans when applicable． will stamp the plans when applicable． |  |  |

[^0]









## Traffic Counts

# LSC Transportation Consultants, Inc. 

2504 E. Pikes Peak Ave, Suite 304
Colorado Springs, CO 80909
719-633-2868
File Name: Meridian Rd - Woodmen Rd AM 4-23
Site Code: S224050
Start Date : 4/13/2023
Page No : 1

Groups Printed- Unshifted

|  | Meridian Rd Southbound |  |  |  |  | Woodmen Rd Westbound |  |  |  |  | Meridian Rd Northbound |  |  |  |  | Woodmen Rd Eastbound |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Right | Thru | Left | Peds | App. Toal | Right | Thru | Left | Peds | App. Toal | Right | Thru | Left | Peds | App. Toal | Right | Thru | Left | Peds | App. Toal | Int. Total |
| 06:30 | 29 | 58 | 2 | 0 | 89 | 1 | 36 | 1 | 0 | 38 | 1 | 8 | 11 | 0 | 20 | 10 | 15 | 13 | 0 | 38 | 185 |
| 06:35 | 34 | 52 | 1 | 0 | 87 | 1 | 48 | 2 | 0 | 51 | 0 | 7 | 10 | 0 | 17 | 9 | 12 | 14 | 1 | 36 | 191 |
| 06:40 | 52 | 79 | 3 | 1 | 135 | 1 | 26 | 1 | 0 | 28 | 1 | 11 | 16 | 0 | 28 | 14 | 17 | 10 | 0 | 41 | 232 |
| 06:45 | 41 | 32 | 1 | 0 | 74 | 3 | 46 | 5 | 0 | 54 | 1 | 8 | 12 | 0 | 21 | 11 | 20 | 27 | 0 | 58 | 207 |
| 06:50 | 47 | 74 | 3 | 0 | 124 | 2 | 33 | 2 | 0 | 37 | 2 | 20 | 9 | 0 | 31 | 20 | 27 | 14 | 0 | 61 | 253 |
| 06:55 | 52 | 52 | 1 | 0 | 105 | 2 | 46 | 9 | 0 | 57 | 0 | 18 | 12 | 0 | 30 | 17 | 22 | 19 | 0 | 58 | 250 |
| Total | 255 | 347 | 11 | 1 | 614 | 10 | 235 | 20 | 0 | 265 | 5 | 72 | 70 | 0 | 147 | 81 | 113 | 97 | 1 | 292 | 1318 |
| 07:00 | 44 | 70 | 2 | 0 | 116 | 1 | 24 | 4 | 0 | 29 | 2 | 12 | 17 | 0 | 31 | 14 | 16 | 21 | 0 | 51 | 227 |
| 07:05 | 63 | 39 | 2 | 0 | 104 | 0 | 50 | 4 | 0 | 54 | 2 | 17 | 5 | 0 | 24 | 14 | 20 | 24 | 0 | 58 | 240 |
| 07:10 | 54 | 63 | 6 | 0 | 123 | 4 | 42 | 3 | 0 | 49 | 1 | 20 | 19 | 0 | 40 | 8 | 24 | 27 | 0 | 59 | 271 |
| 07:15 | 43 | 54 | 5 | 0 | 102 | 5 | 44 | 9 | 0 | 58 | 1 | 12 | 11 | 0 | 24 | 22 | 22 | 36 | 0 | 80 | 264 |
| 07:20 | 41 | 51 | 2 | 0 | 94 | 3 | 46 | 4 | 0 | 53 | 2 | 23 | 15 | 0 | 40 | 26 | 22 | 26 | 0 | 74 | 261 |
| 07:25 | 35 | 38 | 2 | 0 | 75 | 5 | 55 | 6 | 0 | 66 | 1 | 27 | 13 | 0 | 41 | 26 | 31 | 32 | 0 | 89 | 271 |
| 07:30 | 37 | 49 | 5 | 0 | 91 | 2 | 47 | 2 | 0 | 51 | 3 | 17 | 14 | 0 | 34 | 17 | 16 | 18 | 0 | 51 | 227 |
| 07:35 | 51 | 41 | 1 | 0 | 93 | 3 | 63 | 7 | 0 | 73 | 0 | 18 | 8 | 0 | 26 | 12 | 18 | 23 | 0 | 53 | 245 |
| 07:40 | 36 | 47 | 3 | 0 | 86 | 3 | 35 | 11 | 0 | 49 | 2 | 16 | 15 | 0 | 33 | 14 | 20 | 35 | 0 | 69 | 237 |
| 07:45 | 38 | 28 | 6 | 0 | 72 | 6 | 66 | 7 | 0 | 79 | 1 | 12 | 4 | 0 | 17 | 11 | 21 | 27 | 0 | 59 | 227 |
| 07:50 | 37 | 37 | 6 | 0 | 80 | 6 | 26 | 11 | 0 | 43 | 1 | 21 | 15 | 0 | 37 | 13 | 19 | 30 | 0 | 62 | 222 |
| 07:55 | 21 | 26 | 2 | 0 | 49 | 5 | 61 | 9 | 0 | 75 | 1 | 23 | 8 | 1 | 33 | 16 | 36 | 36 | 0 | 88 | 245 |
| Total | 500 | 543 | 42 | 0 | 1085 | 43 | 559 | 77 | 0 | 679 | 17 | 218 | 144 | 1 | 380 | 193 | 265 | 335 | 0 | 793 | 2937 |
| 08:00 | 23 | 53 | 6 | 0 | 82 | 2 | 31 | 5 | 0 | 38 | 0 | 19 | 12 | 0 | 31 | 12 | 18 | 24 | 0 | 54 | 205 |
| 08:05 | 23 | 30 | 3 | 0 | 56 | 2 | 47 | 6 | 0 | 55 | 1 | 17 | 13 | 1 | 32 | 10 | 20 | 30 | 0 | 60 | 203 |
| 08:10 | 35 | 42 | 5 | 0 | 82 | 3 | 19 | 6 | 0 | 28 | 0 | 31 | 14 | 0 | 45 | 8 | 30 | 33 | 0 | 71 | 226 |
| 08:15 | 30 | 32 | 6 | 0 | 68 | 5 | 57 | 9 | 0 | 71 | 3 | 20 | 10 | 0 | 33 | 8 | 33 | 20 | 0 | 61 | 233 |
| 08:20 | 31 | 44 | 7 | 0 | 82 | 3 | 41 | 5 | 0 | 49 | 2 | 23 | 19 | 0 | 44 | 7 | 10 | 22 | 0 | 39 | 214 |
| 08:25 | 29 | 32 | 7 | 0 | 68 | 1 | 48 | 14 | 0 | 63 | 3 | 12 | 6 | 0 | 21 | 11 | 24 | 33 | 0 | 68 | 220 |
| Grand Total | 926 | 1123 | 87 | 1 | 2137 | 69 | 1037 | 142 | 0 | 1248 | 31 | 412 | 288 | 2 | 733 | 330 | 513 | 594 | 1 | 1438 | 5556 |
| Apprch \% | 43.3 | 52.6 | 4.1 | 0 |  | 5.5 | 83.1 | 11.4 | 0 |  | 4.2 | 56.2 | 39.3 | 0.3 |  | 22.9 | 35.7 | 41.3 | 0.1 |  |  |
| Total \% | 16.7 | 20.2 | 1.6 | 0 | 38.5 | 1.2 | 18.7 | 2.6 | 0 | 22.5 | 0.6 | 7.4 | 5.2 | 0 | 13.2 | 5.9 | 9.2 | 10.7 | 0 | 25.9 |  |

# LSC Transportation Consultants, Inc. 

2504 E. Pikes Peak Ave, Suite 304
Colorado Springs, CO 80909
719-633-2868
File Name: Meridian Rd - Woodmen Rd AM 4-23
Site Code: S224050
Start Date : 4/13/2023
Page No :2

|  | Meridian Rd Southbound |  |  |  |  | Woodmen Rd Westbound |  |  |  |  | Meridian Rd Northbound |  |  |  |  | Woodmen Rd Eastbound |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Int. Total |
| Peak Hour Analysis From 06:30 to 08:25-Peak 1 of 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour | or Ent | re Int | rsect | on Be | ins at | 06:50 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 06:50 | 47 | 74 | 3 | 0 | 124 | 2 | 33 | 2 | 0 | 37 | 2 | 20 | 9 | 0 | 31 | 20 | 27 | 14 | 0 | 61 | 253 |
| 06:55 | 52 | 52 | 1 | 0 | 105 | 2 | 46 | 9 | 0 | 57 | 0 | 18 | 12 | 0 | 30 | 17 | 22 | 19 | 0 | 58 | 250 |
| 07:00 | 44 | 70 | 2 | 0 | 116 | 1 | 24 | 4 | 0 | 29 | 2 | 12 | 17 | 0 | 31 | 14 | 16 | 21 | 0 | 51 | 227 |
| 07:05 | 63 | 39 | 2 | 0 | 104 | 0 | 50 | 4 | 0 | 54 | 2 | 17 | 5 | 0 | 24 | 14 | 20 | 24 | 0 | 58 | 240 |
| 07:10 | 54 | 63 | 6 | 0 | 123 | 4 | 42 | 3 | 0 | 49 | 1 | 20 | 19 | 0 | 40 | 8 | 24 | 27 | 0 | 59 | 271 |
| 07:15 | 43 | 54 | 5 | 0 | 102 | 5 | 44 | 9 | 0 | 58 | 1 | 12 | 11 | 0 | 24 | 22 | 22 | 36 | 0 | 80 | 264 |
| 07:20 | 41 | 51 | 2 | 0 | 94 | 3 | 46 | 4 | 0 | 53 | 2 | 23 | 15 | 0 | 40 | 26 | 22 | 26 | 0 | 74 | 261 |
| 07:25 | 35 | 38 | 2 | 0 | 75 | 5 | 55 | 6 | 0 | 66 | 1 | 27 | 13 | 0 | 41 | 26 | 31 | 32 | 0 | 89 | 271 |
| 07:30 | 37 | 49 | 5 | 0 | 91 | 2 | 47 | 2 | 0 | 51 | 3 | 17 | 14 | 0 | 34 | 17 | 16 | 18 | 0 | 51 | 227 |
| 07:35 | 51 | 41 | 1 | 0 | 93 | 3 | 63 | 7 | 0 | 73 | 0 | 18 | 8 | 0 | 26 | 12 | 18 | 23 | 0 | 53 | 245 |
| 07:40 | 36 | 47 | 3 | 0 | 86 | 3 | 35 | 11 | 0 | 49 | 2 | 16 | 15 | 0 | 33 | 14 | 20 | 35 | 0 | 69 | 237 |
| 07:45 | 38 | 28 | 6 | 0 | 72 | 6 | 66 | 7 | 0 | 79 | 1 | 12 | 4 | 0 | 17 | 11 | 21 | 27 | 0 | 59 | 227 |
| Total Volume | 541 | 606 | 38 | 0 | 1185 | 36 | 551 | 68 | 0 | 655 | 17 | 212 | 142 | 0 | 371 | 201 | 259 | 302 | 0 | 762 | 2973 |
| \% App. Total | 45.7 | 51.1 | 3.2 | 0 |  | 5.5 | 84.1 | 10.4 | 0 |  | 4.6 | 57.1 | 38.3 | 0 |  | 26.4 | 34 | 39.6 | 0 |  |  |
| PHF | . 716 | . 682 | . 528 | . 000 | . 796 | . 500 | . 696 | . 515 | . 000 | . 691 | . 472 | . 654 | . 623 | . 000 | . 754 | . 644 | . 696 | . 699 | . 000 | . 713 | . 914 |



# LSC Transportation Consultants, Inc. 

2504 E. Pikes Peak Ave, Suite 304
Colorado Springs, CO 80909
719-633-2868
File Name: Meridian Rd - Woodmen Rd PM 4-23
Site Code: S224050
Start Date : 4/13/2023
Page No : 1

Groups Printed- Unshifted

|  | Meridian Rd Southbound |  |  |  |  | Woodmen Rd Westbound |  |  |  |  | Meridian Rd Northbound |  |  |  |  | Woodmen Rd Eastbound |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Right | Thru | Left | Peds | App. Toal | Right | Thru | Left | Peds | App. Toal | Right | Thru | Left | Peds | App. Toal | Right | Thru | Left | Peds | App. Toal | Int. Total |
| 16:00 | 22 | 34 | 11 | 0 | 67 | 12 | 35 | 9 | 0 | 56 | 3 | 29 | 10 | 0 | 42 | 6 | 47 | 57 | 0 | 110 | 275 |
| 16:05 | 29 | 49 | 5 | 1 | 84 | 3 | 25 | 4 | 0 | 32 | 10 | 55 | 20 | 0 | 85 | 4 | 40 | 40 | 0 | 84 | 285 |
| 16:10 | 15 | 32 | 8 | 0 | 55 | 2 | 38 | 13 | 0 | 53 | 6 | 28 | 14 | 0 | 48 | 8 | 39 | 55 | 0 | 102 | 258 |
| 16:15 | 25 | 61 | 10 | 0 | 96 | 9 | 22 | 12 | 0 | 43 | 11 | 52 | 24 | 0 | 87 | 8 | 28 | 30 | 0 | 66 | 292 |
| 16:20 | 21 | 21 | 1 | 0 | 43 | 10 | 25 | 9 | 0 | 44 | 9 | 40 | 20 | 0 | 69 | 4 | 52 | 65 | 0 | 121 | 277 |
| 16:25 | 32 | 37 | 10 | 0 | 79 | 2 | 27 | 4 | 0 | 33 | 11 | 51 | 34 | 0 | 96 | 7 | 32 | 47 | 0 | 86 | 294 |
| 16:30 | 15 | 30 | 4 | 0 | 49 | 4 | 28 | 17 | 0 | 49 | 10 | 39 | 19 | 0 | 68 | 8 | 50 | 65 | 0 | 123 | 289 |
| 16:35 | 27 | 34 | 15 | 0 | 76 | 6 | 12 | 21 |  | 40 | 9 | 57 | 31 | 0 | 97 | 7 | 24 | 44 | 0 | 75 | 288 |
| 16:40 | 27 | 18 | 5 | 0 | 50 | 4 | 30 | 20 | 0 | 54 | 8 | 47 | 18 | 0 | 73 | 15 | 52 | 58 | 0 | 125 | 302 |
| 16:45 | 28 | 33 | 5 | 0 | 66 | 4 | 18 | 12 | 0 | 34 | 6 | 38 | 29 | 0 | 73 | 11 | 31 | 50 | 0 | 92 | 265 |
| 16:50 | 21 | 29 | 8 | 0 | 58 | 6 | 34 | 6 | 0 | 46 | 8 | 30 | 18 | 0 | 56 | 10 | 47 | 64 | 0 | 121 | 281 |
| 16:55 | 30 | 41 | 16 | 0 | 87 | 5 | 30 | 3 | 0 | 38 | 3 | 51 | 22 | 0 | 76 | 9 | 35 | 42 | 0 | 86 | 287 |
| Total | 292 | 419 | 98 | 1 | 810 | 67 | 324 | 130 | 1 | 522 | 94 | 517 | 259 | 0 | 870 | 97 | 477 | 617 | 0 | 1191 | 3393 |
| 17:00 | 16 | 24 | 6 | 0 | 46 | 5 | 33 | 3 | 0 | 41 | 6 | 40 | 12 | 0 | 58 | 14 | 46 | 76 | 1 | 137 | 282 |
| 17:05 | 22 | 43 | 13 | 0 | 78 | 5 | 37 | 3 | 0 | 44 | 5 | 43 | 24 | 0 | 72 | 11 | 34 | 29 | 0 | 74 | 268 |
| 17:10 | 34 | 29 | 8 | 0 | 71 | 7 | 20 | 31 | 0 | 58 | 4 | 40 | 20 | 0 | 64 | 4 | 43 | 65 | 0 | 112 | 305 |
| 17:15 | 36 | 42 | 8 | 0 | 86 | 2 | 39 | 7 | 0 | 48 | 7 | 39 | 33 | 0 | 79 | 4 | 36 | 46 | 0 | 86 | 299 |
| 17:20 | 32 | 36 | 9 | 0 | 77 | 9 | 39 | 12 | 0 | 60 | 6 | 56 | 13 | 0 | 75 | 5 | 52 | 69 | 0 | 126 | 338 |
| 17:25 | 38 | 30 | 13 | 0 | 81 | 4 | 24 | 10 | 0 | 38 | 9 | 59 | 23 | 0 | 91 | 11 | 31 | 41 | 0 | 83 | 293 |
| 17:30 | 37 | 37 | 6 | 0 | 80 | 3 | 34 | 12 | 0 | 49 | 8 | 51 | 13 | 0 | 72 | 8 | 50 | 34 | 0 | 92 | 293 |
| 17:35 | 31 | 36 | 14 | 0 | 81 | 9 | 18 | 13 | 0 | 40 | 10 | 68 | 20 | 0 | 98 | 10 | 37 | 43 | 0 | 90 | 309 |
| 17:40 | 39 | 31 | 8 | 0 | 78 | 5 | 27 | 6 | 0 | 38 | 8 | 39 | 9 | 0 | 56 | 7 | 54 | 83 | 0 | 144 | 316 |
| 17:45 | 30 | 57 | 10 | 0 | 97 | 5 | 25 | 10 | 0 | 40 | 5 | 52 | 13 | 0 | 70 | 9 | 40 | 46 | 0 | 95 | 302 |
| 17:50 | 29 | 23 | 7 | 0 | 59 | 3 | 31 | 11 | 0 | 45 | 8 | 30 | 5 | , | 44 | 14 | 46 | 61 | 0 | 121 | 269 |
| 17:55 | 27 | 41 | 15 | 0 | 83 | 2 | 23 | 9 | 0 | 34 | 8 | 65 | 15 | 0 | 88 | 11 | 17 | 45 | 0 | 73 | 278 |
| Total | 371 | 429 | 117 | 0 | 917 | 58 | 350 | 127 | 0 | 535 | 84 | 582 | 200 | 1 | 867 | 108 | 486 | 638 | 1 | 1233 | 3552 |
| Grand Total | 663 | 848 | 215 | 1 | 1727 | 125 | 674 | 257 | 1 | 1057 | 178 | 1099 | 459 | 1 | 1737 | 205 | 963 | 1255 | 1 | 2424 | 6945 |
| Apprch \% | 38.4 | 49.1 | 12.4 | 0.1 |  | 11.8 | 63.8 | 24.3 | 0.1 |  | 10.2 | 63.3 | 26.4 | 0.1 |  | 8.5 | 39.7 | 51.8 | 0 |  |  |
| Total \% | 9.5 | 12.2 | 3.1 | 0 | 24.9 | 1.8 | 9.7 | 3.7 | 0 | 15.2 | 2.6 | 15.8 | 6.6 | 0 | 25 | 3 | 13.9 | 18.1 | 0 | 34.9 |  |

# LSC Transportation Consultants, Inc. 

2504 E. Pikes Peak Ave, Suite 304
Colorado Springs, CO 80909
719-633-2868
File Name: Meridian Rd - Woodmen Rd PM 4-23
Site Code: S224050
Start Date : 4/13/2023
Page No :2

|  | Meridian Rd Southbound |  |  |  |  | Woodmen Rd Westbound |  |  |  |  | Meridian Rd Northbound |  |  |  |  | Woodmen Rd Eastbound |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Int. Total |
| Peak Hour Analysis From 16:00 to 17:55-Peak 1 of 1 Peak Hour for Entire Intersection Begins at 16:50 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 16:50 | 21 | 29 | 8 | 0 | 58 | 6 | 34 | 6 | 0 | 46 | 8 | 30 | 18 | 0 | 56 | 10 | 47 | 64 | 0 | 121 | 281 |
| 16:55 | 30 | 41 | 16 | 0 | 87 | 5 | 30 | 3 | 0 | 38 | 3 | 51 | 22 | 0 | 76 | 9 | 35 | 42 | 0 | 86 | 287 |
| 17:00 | 16 | 24 | 6 | 0 | 46 | 5 | 33 | 3 | 0 | 41 | 6 | 40 | 12 | 0 | 58 | 14 | 46 | 76 | 1 | 137 | 282 |
| 17:05 | 22 | 43 | 13 | 0 | 78 | 4 | 37 | 3 | 0 | 44 | 5 | 43 | 24 | 0 | 72 | 11 | 34 | 29 | 0 | 74 | 268 |
| 17:10 | 34 | 29 | 8 | 0 | 71 | 7 | 20 | 31 | 0 | 58 | 4 | 40 | 20 | 0 | 64 | 4 | 43 | 65 | 0 | 112 | 305 |
| 17:15 | 36 | 42 | 8 | 0 | 86 | 2 | 39 | 7 | 0 | 48 | 7 | 39 | 33 | 0 | 79 | 4 | 36 | 46 | 0 | 86 | 299 |
| 17:20 | 32 | 36 | 9 | 0 | 77 | 9 | 39 | 12 | 0 | 60 | 6 | 56 | 13 | 0 | 75 | 5 | 52 | 69 | 0 | 126 | 338 |
| 17:25 | 38 | 30 | 13 | 0 | 81 | 4 | 24 | 10 | 0 | 38 | 9 | 59 | 23 | 0 | 91 | 11 | 31 | 41 | 0 | 83 | 293 |
| 17:30 | 37 | 37 | 6 | 0 | 80 | 3 | 34 | 12 | 0 | 49 | 8 | 51 | 13 | 0 | 72 | 8 | 50 | 34 | 0 | 92 | 293 |
| 17:35 | 31 | 36 | 14 | 0 | 81 | 9 | 18 | 13 | 0 | 40 | 10 | 68 | 20 | 0 | 98 | 10 | 37 | 43 | 0 | 90 | 309 |
| 17:40 | 39 | 31 | 8 | 0 | 78 | 5 | 27 | 6 | 0 | 38 | 8 | 39 | 9 | 0 | 56 | 7 | 54 | 83 | 0 | 144 | 316 |
| 17:45 | 30 | 57 | 10 | 0 | 97 | 5 | 25 | 10 | 0 | 40 | 5 | 52 | 13 | 0 | 70 | 9 | 40 | 46 | 0 | 95 | 302 |
| Total Volume | 366 | 435 | 119 | 0 | 920 | 64 | 360 | 116 | 0 | 540 | 79 | 568 | 220 | 0 | 867 | 102 | 505 | 638 | 1 | 1246 | 3573 |
| \% App. Total | 39.8 | 47.3 | 12.9 | 0 |  | 11.9 | 66.7 | 21.5 | 0 |  | 9.1 | 65.5 | 25.4 | 0 |  | 8.2 | 40.5 | 51.2 | 0.1 |  |  |
| PHF | . 782 | . 636 | . 620 | . 000 | . 790 | . 593 | . 769 | . 312 | . 000 | . 750 | . 658 | . 696 | . 556 | . 000 | . 737 | . 607 | . 779 | . 641 | . 083 | 721 | . 881 |



# LSC Transportation Consultants, Inc. 

2504 E. Pikes Peak Ave, Suite 304
Colorado Springs, CO 80909
719-633-2868
File Name : McLaughlin Rd - Woodmen Rd AM 5-23
Site Code : S234220
Start Date : 5/16/2023
Page No : 1

Groups Printed- Unshifted

|  | Mclaughlin Rd Southbound |  |  |  |  | Woodmen Rd Westbound |  |  |  |  | Mclaughlin Rd Northbound |  |  |  |  | Woodmen Rd Eastbound |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Right | Thru | Left | Peds | App. Toal | Right | Thru | Left | Peds | App. Toaa | Right | Thru | Left | Peds | App. Toatal | Right | Thru | Left | Peds | App. Total | Int. Total |
| 06:30 | 18 | 1 | 12 | 1 | 32 | 7 | 15 | 1 | 0 | 23 | 1 | 1 | 1 | 0 | 3 | 2 | 15 | 1 | 0 | 18 | 76 |
| 06:35 | 7 | 1 | 12 | 0 | 20 | 5 | 26 | 1 | 0 | 32 | 2 | 0 | 1 | 0 | 3 | 1 | 17 | 3 | 0 | 21 | 76 |
| 06:40 | 20 | 2 | 11 | 0 | 33 | 6 | 32 | 0 | 0 | 38 | 2 | 2 | 1 | 0 | 5 | 0 | 13 | 3 | 0 | 16 | 92 |
| 06:45 | 10 | 0 | 8 | 0 | 18 | 8 | 43 | 2 | 0 | 53 | 1 | 4 | 1 | 0 | 6 | 3 | 24 | 7 | 0 | 34 | 111 |
| 06:50 | 20 | 2 | 18 | 0 | 40 | 5 | 30 | 1 | 0 | 36 | 0 | 3 | 4 | 0 | 7 | 0 | 15 | 4 | 0 | 19 | 102 |
| 06:55 | 19 | 3 | 18 | 0 | 40 | 10 | 32 | 4 | 0 | 46 | 2 | 2 | 2 | 0 | 6 | 0 | 23 | 3 | 0 | 26 | 118 |
| Total | 94 | 9 | 79 | 1 | 183 | 41 | 178 | 9 | 0 | 228 | 8 | 12 | 10 | 0 | 30 | 6 | 107 | 21 | 0 | 134 | 575 |
| 07:00 | 19 | 6 | 20 | 0 | 45 | 8 | 25 | 2 | 0 | 35 | 1 | 1 | 2 | 0 | 4 | 0 | 24 | 3 | 0 | 27 | 111 |
| 07:05 | 30 | 9 | 13 | 0 | 52 | 15 | 26 | 1 | 0 | 42 | 2 | 3 | 3 | 0 | 8 | 2 | 26 | 2 | 0 | 30 | 132 |
| 07:10 | 27 | 10 | 8 | 0 | 45 | 12 | 36 | 1 | 0 | 49 | 1 | 5 | 2 | 0 | 8 | 1 | 26 | 9 | 0 | 36 | 138 |
| 07:15 | 28 | 6 | 13 | 0 | 47 | 9 | 31 | 0 | 0 | 40 | 0 | 2 | 0 | 0 | 2 | 6 | 16 | 5 | 0 | 27 | 116 |
| 07:20 | 20 | 8 | 6 | 0 | 34 | 14 | 40 | 3 | 0 | 57 | 0 | 3 | 3 | 0 | 6 | 1 | 17 | 3 | 1 | 22 | 119 |
| 07:25 | 30 | 13 | 10 | 0 | 53 | 10 | 28 | 4 | 0 | 42 | 1 | 4 | 2 | 0 | 7 | 4 | 21 | 4 | 0 | 29 | 131 |
| 07:30 | 32 | 15 | 5 | 0 | 52 | 7 | 28 | 4 | 1 | 40 | 2 | 4 | 4 | 0 | 10 | 2 | 15 | 7 | 0 | 24 | 126 |
| 07:35 | 30 | 9 | 9 | 0 | 48 | 11 | 25 | 0 | 0 | 36 | 1 | 3 | 5 | 0 | 9 | 3 | 26 | 6 | 0 | 35 | 128 |
| 07:40 | 25 | 11 | 9 | 0 | 45 | 16 | 43 | 3 | 0 | 62 | 0 | 2 | 1 | 0 | 3 | 1 | 14 | 13 | 0 | 28 | 138 |
| 07:45 | 20 | 14 | 17 | 0 | 51 | 9 | 22 | 3 | 0 | 34 | 1 | 8 | 4 | 0 | 13 | 6 | 12 | 8 | 0 | 26 | 124 |
| 07:50 | 19 | 15 | 7 | 0 | 41 | 17 | 20 | 4 | 0 | 41 | 0 | 3 | 5 | 0 | 8 | 5 | 22 | 21 | 0 | 48 | 138 |
| 07:55 | 18 | 8 | 12 | 0 | 38 | 10 | 29 | 3 | 0 | 42 | 0 | 3 | 4 | 0 | 7 | 11 | 17 | 10 | 0 | 38 | 125 |
| Total | 298 | 124 | 129 | 0 | 551 | 138 | 353 | 28 | 1 | 520 | 9 | 41 | 35 | 0 | 85 | 42 | 236 | 91 | 1 | 370 | 1526 |
| 08:00 | 14 | 7 | 12 | 0 | 33 | 13 | 21 | 2 | 0 | 36 | 2 | 5 | 6 | 0 | 13 | 4 | 24 | 13 | 0 | 41 | 123 |
| 08:05 | 16 | 11 | 9 | 0 | 36 | 6 | 25 | 1 | 0 | 32 | 3 | 5 | 1 | 0 | 9 | 10 | 25 | 8 | 0 | 43 | 120 |
| 08:10 | 16 | 3 | 9 | 0 | 28 | 17 | 23 | 0 | 0 | 40 | 5 | 4 | 3 | 0 | 12 | 2 | 7 | 7 | 0 | 16 | 96 |
| 08:15 | 15 | 8 | 14 | 0 | 37 | 17 | 26 | 3 | 0 | 46 | 1 | 4 | 3 | 0 | 8 | 4 | 15 | 13 | 0 | 32 | 123 |
| 08:20 | 15 | 3 | 19 | 0 | 37 | 15 | 29 | 2 | 0 | 46 | 1 | 5 | 4 | 0 | 10 | 4 | 16 | 4 | 0 | 24 | 117 |
| 08:25 | 17 | 6 | 16 | 0 | 39 | 10 | 30 | 1 | 0 | 41 | 0 | 4 | 2 | 0 | 6 | 6 | 17 | 6 | 0 | 29 | 115 |
| Grand Total | 485 | 171 | 287 | 1 | 944 | 257 | 685 | 46 | 1 | 989 | 29 | 80 | 64 | 0 | 173 | 78 | 447 | 163 | 1 | 689 | 2795 |
| Apprch \% | 51.4 | 18.1 | 30.4 | 0.1 |  | 26 | 69.3 | 4.7 | 0.1 |  | 16.8 | 46.2 | 37 | 0 |  | 11.3 | 64.9 | 23.7 | 0.1 |  |  |
| Total \% | 17.4 | 6.1 | 10.3 | 0 | 33.8 | 9.2 | 24.5 | 1.6 | 0 | 35.4 | 1 | 2.9 | 2.3 | 0 | 6.2 | 2.8 | 16 | 5.8 | 0 | 24.7 |  |

# LSC Transportation Consultants, Inc. 

2504 E. Pikes Peak Ave, Suite 304
Colorado Springs, CO 80909
719-633-2868
File Name : McLaughlin Rd - Woodmen Rd AM 5-23
Site Code: S234220
Start Date :5/16/2023
Page No :2

|  | Mclaughlin Rd Southbound |  |  |  |  | Woodmen Rd Westbound |  |  |  |  | Mclaughlin Rd Northbound |  |  |  |  | Woodmen Rd Eastbound |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Int. Total |
| Peak Hour Analysis From 06:30 to 08:25-Peak 1 of 1 Peak Hour for Entire Intersection Begins at 07:05 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 07:05 | 30 | 9 | 13 | 0 | 52 | 15 | 26 | 1 | 0 | 42 | 2 | 3 | 3 | 0 | 8 | 2 | 26 | 2 | 0 | 30 | 132 |
| 07:10 | 27 | 10 | 8 | 0 | 45 | 12 | 36 | 1 | 0 | 49 | 1 | 5 | 2 | 0 | 8 | 1 | 26 | 9 | 0 | 36 | 138 |
| 07:15 | 28 | 6 | 13 | 0 | 47 | 9 | 31 | 0 | 0 | 40 | 0 | 2 | 0 | 0 | 2 | 6 | 16 | 5 | 0 | 27 | 116 |
| 07:20 | 20 | 8 | 6 | 0 | 34 | 14 | 40 | 3 | 0 | 57 | 0 | 3 | 3 | 0 | 6 | 1 | 17 | 3 | 1 | 22 | 119 |
| 07:25 | 30 | 13 | 10 | 0 | 53 | 10 | 28 | 4 | 0 | 42 | 1 | 4 | 2 | 0 | 7 | 4 | 21 | 4 | 0 | 29 | 131 |
| 07:30 | 32 | 15 | 5 | 0 | 52 | 7 | 28 | 4 | 1 | 40 | 2 | 4 | 4 | 0 | 10 | 2 | 15 | 7 | 0 | 24 | 126 |
| 07:35 | 30 | 9 | 9 | 0 | 48 | 11 | 25 | 0 | 0 | 36 | 1 | 3 | 5 | 0 | 9 | 3 | 26 | 6 | 0 | 35 | 128 |
| 07:40 | 25 | 11 | 9 | 0 | 45 | 16 | 43 | 3 | 0 | 62 | 0 | 2 | 1 | 0 | 3 | 1 | 14 | 13 | 0 | 28 | 138 |
| 07:45 | 20 | 14 | 17 | 0 | 51 | 9 | 22 | 3 | 0 | 34 | 1 | 8 | 4 | 0 | 13 | 6 | 12 | 8 | 0 | 26 | 124 |
| 07:50 | 19 | 15 | 7 | 0 | 41 | 17 | 20 | 4 | 0 | 41 | 0 | 3 | 5 | 0 | 8 | 5 | 22 | 21 | 0 | 48 | 138 |
| 07:55 | 18 | 8 | 12 | 0 | 38 | 10 | 29 | 3 | 0 | 42 | 0 | 3 | 4 | 0 | 7 | 11 | 17 | 10 | 0 | 38 | 125 |
| 08:00 | 14 | 7 | 12 | 0 | 33 | 13 | 21 | 2 | 0 | 36 | 2 | 5 | 6 | 0 | 13 | 4 | 24 | 13 | 0 | 41 | 123 |
| Total Volume | 293 | 125 | 121 | 0 | 539 | 143 | 349 | 28 | 1 | 521 | 10 | 45 | 39 | 0 | 94 | 46 | 236 | 101 | 1 | 384 | 1538 |
| \% App. Total | 54.4 | 23.2 | 22.4 | 0 |  | 27.4 | 67 | 5.4 | 0.2 |  | 10.6 | 47.9 | 41.5 | 0 |  | 12 | 61.5 | 26.3 | 0.3 |  |  |
| PHF | . 763 | . 694 | . 593 | . 000 | . 847 | . 701 | . 676 | . 583 | . 083 | . 700 | . 417 | . 469 | . 542 | . 000 | . 603 | . 348 | . 756 | . 401 | . 083 | . 667 | . 929 |



# LSC Transportation Consultants, Inc. 

2504 E. Pikes Peak Ave, Suite 304
Colorado Springs, CO 80909
719-633-2868
File Name : McLaughlin Rd - Woodmen Rd PM 5-23
Site Code : S234220
Start Date : 5/16/2023
Page No : 1

Groups Printed- Unshifted

|  | Mclaughlin Rd Southbound |  |  |  |  | Woodmen Rd Westbound |  |  |  |  | McLughlin Rd Northbound |  |  |  |  | Woodmen Rd Eastbound |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Int. Total |
| 16:00 | 9 | 5 | 21 | 0 | 35 | 19 | 26 | 2 | 0 | 47 | 8 | 10 | 6 | 0 | 24 | 12 | 31 | 14 | 0 | 57 | 163 |
| 16:05 | 18 | 13 | 9 | 0 | 40 | 13 | 24 | 3 | 0 | 40 | 6 | 27 | 10 | 0 | 43 | 11 | 24 | 21 | 0 | 56 | 179 |
| 16:10 | 16 | 9 | 15 | 0 | 40 | 28 | 38 | 5 | 0 | 71 | 9 | 10 | 2 | 0 | 21 | 7 | 24 | 37 | 0 | 68 | 200 |
| 16:15 | 17 | 11 | 17 | 0 | 45 | 18 | 26 | 2 | 0 | 46 | 4 | 16 | 7 | 0 | 27 | 8 | 39 | 21 | 0 | 68 | 186 |
| 16:20 | 14 | 11 | 11 | 0 | 36 | 18 | 41 | 7 | 0 | 66 | 11 | 15 | 7 | 0 | 33 | 10 | 24 | 24 | 0 | 58 | 193 |
| 16:25 | 10 | 15 | 22 | 0 | 47 | 28 | 12 | 5 | 0 | 45 | 8 | 14 | 11 | 0 | 33 | 5 | 23 | 24 | 0 | 52 | 177 |
| 16:30 | 24 | 9 | 14 | 2 | 49 | 18 | 33 | 4 | 0 | 55 | 9 | 12 | 6 | 0 | 27 | 8 | 28 | 20 | 0 | 56 | 187 |
| 16:35 | 15 | 8 | 19 | 0 | 42 | 18 | 30 | 4 | 0 | 52 | 11 | 18 | 4 | 0 | 33 | 7 | 42 | 31 | 0 | 80 | 207 |
| 16:40 | 11 | 15 | 20 | 0 | 46 | 25 | 30 | 5 | 0 | 60 | 3 | 12 | 10 | 0 | 25 | 3 | 18 | 19 | 0 | 40 | 171 |
| 16:45 | 7 | 7 | 17 | 0 | 31 | 20 | 38 | 5 | 0 | 63 | 3 | 10 | 5 | 0 | 18 | 8 | 32 | 33 | 0 | 73 | 185 |
| 16:50 | 18 | 8 | 14 | 0 | 40 | 32 | 37 | 2 | 1 | 72 | 8 | 16 | 7 | 0 | 31 | 8 | 28 | 17 | 0 | 53 | 196 |
| 16:55 | 22 | 8 | 10 | 0 | 40 | 21 | 32 | 1 | 0 | 54 | 7 | 14 | 7 | 0 | 28 | 10 | 23 | 24 | 0 | 57 | 179 |
| Total | 181 | 119 | 189 | 2 | 491 | 258 | 367 | 45 | 1 | 671 | 87 | 174 | 82 | 0 | 343 | 97 | 336 | 285 | 0 | 718 | 2223 |
| 17:00 | 13 | 4 | 16 | 0 | 33 | 17 | 35 | 2 | 0 | 54 | 9 | 15 | 15 | 0 | 39 | 8 | 16 | 16 | 0 | 40 | 166 |
| 17:05 | 27 | 8 | 10 | 0 | 45 | 23 | 36 | 3 | 0 | 62 | 5 | 13 | 5 | 0 | 23 | 15 | 31 | 30 | 0 | 76 | 206 |
| 17:10 | 26 | 6 | 18 | 0 | 50 | 21 | 18 | 4 | 0 | 43 | 5 | 13 | 16 | 0 | 34 | 6 | 25 | 16 | 1 | 48 | 175 |
| 17:15 | 19 | 9 | 11 | 0 | 39 | 26 | 32 | 4 | 0 | 62 | 1 | 19 | 6 | 0 | 26 | 10 | 34 | 23 | 0 | 67 | 194 |
| 17:20 | 17 | 5 | 14 | 0 | 36 | 17 | 24 | 5 | 0 | 46 | 5 | 6 | 3 | 0 | 14 | 4 | 36 | 20 | 1 | 61 | 157 |
| 17:25 | 19 | 8 | 21 | 0 | 48 | 31 | 37 | 0 | 0 | 68 | 2 | 21 | 7 | 0 | 30 | 11 | 33 | 19 | 0 | 63 | 209 |
| 17:30 | 15 | 6 | 16 | 0 | 37 | 16 | 33 | 2 | 0 | 51 | 10 | 19 | 6 | 0 | 35 | 13 | 37 | 24 | 0 | 74 | 197 |
| 17:35 | 14 | 6 | 19 | 0 | 39 | 17 | 30 | 3 | 0 | 50 | 8 | 19 | 8 | 0 | 35 | 12 | 34 | 24 | 0 | 70 | 194 |
| 17:40 | 12 | 5 | 11 | 0 | 28 | 20 | 21 | 5 | 0 | 46 | 5 | 12 | 9 | 0 | 26 | 7 | 19 | 27 | 0 | 53 | 153 |
| 17:45 | 12 | 7 | 10 | 0 | 29 | 31 | 27 | 4 | 0 | 62 | 2 | 9 | 7 | 0 | 18 | 14 | 40 | 20 | 0 | 74 | 183 |
| 17:50 | 11 | 2 | 12 | 0 | 25 | 18 | 23 | 1 | 0 | 42 | 14 | 12 | 4 | 0 | 30 | 5 | 25 | 19 | 0 | 49 | 146 |
| 17:55 | 12 | 4 | 15 | 0 | 31 | 24 | 27 | 4 | 0 | 55 | 8 | 7 | 4 | 0 | 19 | 13 | 31 | 30 | 0 | 74 | 179 |
| Total | 197 | 70 | 173 | 0 | 440 | 261 | 343 | 37 | 0 | 641 | 74 | 165 | 90 | 0 | 329 | 118 | 361 | 268 | 2 | 749 | 2159 |
| Grand Total | 378 | 189 | 362 | 2 | 931 | 519 | 710 | 82 | 1 | 1312 | 161 | 339 | 172 | 0 | 672 | 215 | 697 | 553 | 2 | 1467 | 4382 |
| Apprch \% | 40.6 | 20.3 | 38.9 | 0.2 |  | 39.6 | 54.1 | 6.2 | 0.1 |  | 24 | 50.4 | 25.6 | 0 |  | 14.7 | 47.5 | 37.7 | 0.1 |  |  |
| Total \% | 8.6 | 4.3 | 8.3 | 0 | 21.2 | 11.8 | 16.2 | 1.9 | 0 | 29.9 | 3.7 | 7.7 | 3.9 | 0 | 15.3 | 4.9 | 15.9 | 12.6 | 0 | 33.5 |  |

# LSC Transportation Consultants, Inc. 

2504 E. Pikes Peak Ave, Suite 304
Colorado Springs, CO 80909
719-633-2868
File Name : McLaughlin Rd - Woodmen Rd PM 5-23
Site Code : S234220
Start Date : 5/16/2023
Page No : 2

|  | Mclaughlin Rd Southbound |  |  |  |  | Woodmen Rd Westbound |  |  |  |  | McLughlin Rd Northbound |  |  |  |  | Woodmen Rd Eastbound |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Int. Total |
| Peak Hour Analysis From 16:00 to 17:55-Peak 1 of 1 Peak Hour for Entire Intersection Begins at 16:10 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 16:10 | 16 | 9 | 15 | 0 | 40 | 28 | 38 | 5 | 0 | 71 | 9 | 10 | 2 | 0 | 21 | 7 | 24 | 37 | 0 | 68 | 200 |
| 16:15 | 17 | 11 | 17 | 0 | 45 | 18 | 26 | 2 | 0 | 46 | 4 | 16 | 7 | 0 | 27 | 8 | 39 | 21 | 0 | 68 | 186 |
| 16:20 | 14 | 11 | 11 | 0 | 36 | 18 | 41 | 7 | 0 | 66 | 11 | 15 | 7 | 0 | 33 | 10 | 24 | 24 | 0 | 58 | 193 |
| 16:25 | 10 | 15 | 22 | 0 | 47 | 28 | 12 | 5 | 0 | 45 | 8 | 14 | 11 | 0 | 33 | 5 | 23 | 24 | 0 | 52 | 177 |
| 16:30 | 24 | 9 | 14 | 2 | 49 | 18 | 33 | 4 | 0 | 55 | 9 | 12 | 6 | 0 | 27 | 8 | 28 | 20 | 0 | 56 | 187 |
| 16:35 | 15 | 8 | 19 | 0 | 42 | 18 | 30 | 4 | 0 | 52 | 11 | 18 | 4 | 0 | 33 | 7 | 42 | 31 | 0 | 80 | 207 |
| 16:40 | 11 | 15 | 20 | 0 | 46 | 25 | 30 | 5 | 0 | 60 | 3 | 12 | 10 | 0 | 25 | 3 | 18 | 19 | 0 | 40 | 171 |
| 16:45 | 7 | 7 | 17 | 0 | 31 | 20 | 38 | 5 | 0 | 63 | 3 | 10 | 5 | 0 | 18 | 8 | 32 | 33 | 0 | 73 | 185 |
| 16:50 | 18 | 8 | 14 | 0 | 40 | 32 | 37 | 2 | 1 | 72 | 8 | 16 | 7 | 0 | 31 | 8 | 28 | 17 | 0 | 53 | 196 |
| 16:55 | 22 | 8 | 10 | 0 | 40 | 21 | 32 | 1 | 0 | 54 | 7 | 14 | 7 | 0 | 28 | 10 | 23 | 24 | 0 | 57 | 179 |
| 17:00 | 13 | 4 | 16 | 0 | 33 | 17 | 35 | 2 | 0 | 54 | 9 | 15 | 15 | 0 | 39 | 8 | 16 | 16 | 0 | 40 | 166 |
| 17:05 | 27 | 8 | 10 | 0 | 45 | 23 | 36 | 3 | 0 | 62 | 5 | 13 | 5 | 0 | 23 | 15 | 31 | 30 | 0 | 76 | 206 |
| Total Volume | 194 | 113 | 185 | 2 | 494 | 266 | 388 | 45 | 1 | 700 | 87 | 165 | 86 | 0 | 338 | 97 | 328 | 296 | 0 | 721 | 2253 |
| \% App. Total | 39.3 | 22.9 | 37.4 | 0.4 |  | 38 | 55.4 | 6.4 | 0.1 |  | 25.7 | 48.8 | 25.4 | 0 |  | 13.5 | 45.5 | 41.1 | 0 |  |  |
| PHF | . 599 | . 628 | . 701 | . 083 | . 840 | . 693 | . 789 | . 536 | . 083 | . 810 | . 659 | . 764 | . 478 | . 000 | . 722 | . 539 | . 651 | . 667 | . 000 | 751 | . 907 |



# LSC Transportation Consultants, Inc. 

2504 E. Pikes Peak Ave, Suite 304
Colorado Springs, CO 80909
719-633-2868
File Name : Hwy 24 - Woodmen Rd AM 5-23
Site Code : S214730
Start Date : 5/2/2023
Page No : 1

Groups Printed- Unshifted

|  | Hwy 24 Southbound |  |  |  |  | Westbound |  |  |  |  | Hwy 24 Northbound |  |  |  |  | Woodmen Rd Eastbound |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Right | Thru | Left | Peds | App. Toal | Right | Thru | Left | Peds | App. Toal | Right | Thru | Left | Peds | App. Toal | Right | Thru | Left | Peds | App. Toal | Int. Total |
| 06:30 | 36 | 45 | 0 | 0 | 81 | 0 | 0 | 0 | 0 | 0 | 0 | 16 | 15 | 0 | 31 | 14 | 0 | 9 | 0 | 23 | 135 |
| 06:35 | 29 | 50 | 0 | 0 | 79 | 0 | 0 | 0 | 0 | 0 | 0 | 27 | 5 | 0 | 32 | 7 | 0 | 12 | 0 | 19 | 130 |
| 06:40 | 39 | 53 | 0 | 0 | 92 | 0 | 0 | 0 | 0 | 0 | 0 | 24 | 5 | 0 | 29 | 14 | 0 | 15 | 0 | 29 | 150 |
| 06:45 | 36 | 54 | 0 | 0 | 90 | 0 | 0 | 0 | 0 | 0 | 0 | 24 | 12 | 0 | 36 | 12 | 0 | 20 | 0 | 32 | 158 |
| 06:50 | 19 | 46 | 9 | 0 | 74 | 0 | 0 | 0 | 0 | 0 | 0 | 14 | 4 | 0 | 18 | 16 | 0 | 27 | 0 | 43 | 135 |
| 06:55 | 20 | 40 | 0 | 0 | 60 | 0 | 0 | 0 | 0 | 0 | 0 | 17 | 11 | 0 | 28 | 12 | 0 | 21 | 0 | 33 | 121 |
| Total | 179 | 288 | 9 | 0 | 476 | 0 | 0 | 0 | 0 | 0 | 0 | 122 | 52 | 0 | 174 | 75 | 0 | 104 | 0 | 179 | 829 |
| 07:00 | 27 | 50 | 0 | 0 | 77 | 0 | 0 | 0 | 0 | 0 | 0 | 15 | 6 | 0 | 21 | 18 | 0 | 26 | 0 | 44 | 142 |
| 07:05 | 25 | 42 | 0 | 0 | 67 | 0 | 0 | 0 | 0 | 0 | 0 | 25 | 9 | 0 | 34 | 17 | 0 | 20 | 0 | 37 | 138 |
| 07:10 | 25 | 52 | 0 | 0 | 77 | 0 | 0 | 0 | 0 | 0 | 0 | 23 | 12 | 0 | 35 | 8 | 0 | 26 | 0 | 34 | 146 |
| 07:15 | 34 | 48 | 0 | 0 | 82 | 0 | 0 | 0 | 0 | 0 | 0 | 23 | 10 | 0 | 33 | 15 | 0 | 13 | 0 | 28 | 143 |
| 07:20 | 30 | 39 | 0 | 0 | 69 | 0 | 0 | 0 | 0 | 0 | 0 | 21 | 11 | 0 | 32 | 10 | 1 | 17 | 0 | 28 | 129 |
| 07:25 | 28 | 32 | 0 | 1 | 61 | 0 | 0 | 0 | 0 | 0 | 0 | 19 | 11 | 0 | 30 | 9 | 0 | 19 | 0 | 28 | 119 |
| 07:30 | 29 | 36 | 0 | 0 | 65 | 0 | 0 | 0 | 0 | 0 | 0 | 20 | 18 | 0 | 38 | 12 | 0 | 22 | 0 | 34 | 137 |
| 07:35 | 34 | 29 | 0 | 0 | 63 | 0 | 0 | 0 | 0 | 0 | 0 | 22 | 17 | 0 | 39 | 8 | 0 | 12 | 0 | 20 | 122 |
| 07:40 | 39 | 37 | 0 | 0 | 76 | 0 | 0 | 0 | 0 | 0 | 0 | 16 | 14 | 0 | 30 | 10 | 0 | 20 | 0 | 30 | 136 |
| 07:45 | 29 | 31 | 0 | 0 | 60 | 0 | 0 | 0 | 0 | 0 | 0 | 13 | 10 | 0 | 23 | 13 | 0 | 22 | 0 | 35 | 118 |
| 07:50 | 36 | 40 | 0 | 0 | 76 | 0 | 0 | 0 | 0 | 0 | 0 | 22 | 10 | 0 | 32 | 9 | 0 | 19 | 0 | 28 | 136 |
| 07:55 | 29 | 28 | 0 | 0 | 57 | 0 | 0 | 0 | 0 | 0 | 0 | 14 | 22 | 0 | 36 | 8 | 0 | 19 | 0 | 27 | 120 |
| Total | 365 | 464 | 0 | 1 | 830 | 0 | 0 | 0 | 0 | 0 | 0 | 233 | 150 | 0 | 383 | 137 | 1 | 235 | 0 | 373 | 1586 |
| 08:00 | 24 | 29 | 0 | 0 | 53 | 0 | 0 | 0 | 0 | 0 | 0 | 16 | 14 | 0 | 30 | 10 | 0 | 28 | 0 | 38 | 121 |
| 08:05 | 30 | 27 | 0 | 0 | 57 | 0 | 0 | 0 | 0 | 0 | 0 | 15 | 10 | 0 | 25 | 5 | 0 | 18 | 0 | 23 | 105 |
| 08:10 | 27 | 37 | 0 | 0 | 64 | 0 | 0 | 0 | 0 | 0 | 0 | 19 | 10 | 0 | 29 | 11 | 0 | 13 | 0 | 24 | 117 |
| 08:15 | 32 | 40 | 0 | 0 | 72 | 0 | 0 | 0 | 0 | 0 | 0 | 18 | 9 | 0 | 27 | 12 | 0 | 24 | 0 | 36 | 135 |
| 08:20 | 25 | 44 | 0 | 0 | 69 | 0 | 0 | 0 | 0 | 0 | 0 | 17 | 10 | 0 | 27 | 13 | 0 | 24 | 0 | 37 | 133 |
| 08:25 | 29 | 33 | 0 | 0 | 62 | 0 | 0 | 0 | 0 | 0 | 0 | 16 | 12 | 0 | 28 | 13 | 0 | 13 | 0 | 26 | 116 |
| Grand Total | 711 | 962 | 9 | 1 | 1683 | 0 | 0 | 0 | 0 | 0 | 0 | 456 | 267 | 0 | 723 | 276 | 1 | 459 | 0 | 736 | 3142 |
| Apprch \% | 42.2 | 57.2 | 0.5 | 0.1 |  | 0 | 0 | 0 | 0 |  | 0 | 63.1 | 36.9 | 0 |  | 37.5 | 0.1 | 62.4 | 0 |  |  |
| Total \% | 22.6 | 30.6 | 0.3 | 0 | 53.6 | 0 | 0 | 0 | 0 | 0 | 0 | 14.5 | 8.5 | 0 | 23 | 8.8 | 0 | 14.6 | 0 | 23.4 |  |

# LSC Transportation Consultants, Inc. 

2504 E. Pikes Peak Ave, Suite 304
Colorado Springs, CO 80909
719-633-2868
File Name : Hwy 24 - Woodmen Rd AM 5-23
Site Code : S214730
Start Date : 5/2/2023
Page No : 2

|  | Hwy 24 Southbound |  |  |  |  | Westbound |  |  |  |  | Hwy 24 Northbound |  |  |  |  | Woodmen Rd Eastbound |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Int. Total |
| Peak Hour Analysis From 06:30 to 08:25-Peak 1 of 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour | or Ent | re Int | rsect | on Be | ins at | 06:35 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 06:35 | 29 | 50 | 0 | 0 | 79 | 0 | 0 | 0 | 0 | 0 | 0 | 27 | 5 | 0 | 32 | 7 | 0 | 12 | 0 | 19 | 130 |
| 06:40 | 39 | 53 | 0 | 0 | 92 | 0 | 0 | 0 | 0 | 0 | 0 | 24 | 5 | 0 | 29 | 14 | 0 | 15 | 0 | 29 | 150 |
| 06:45 | 36 | 54 | 0 | 0 | 90 | 0 | 0 | 0 | 0 | 0 | 0 | 24 | 12 | 0 | 36 | 12 | 0 | 20 | 0 | 32 | 158 |
| 06:50 | 19 | 46 | 9 | 0 | 74 | 0 | 0 | 0 | 0 | 0 | 0 | 14 | 4 | 0 | 18 | 16 | 0 | 27 | 0 | 43 | 135 |
| 06:55 | 20 | 40 | 0 | 0 | 60 | 0 | 0 | 0 | 0 | 0 | 0 | 17 | 11 | 0 | 28 | 12 | 0 | 21 | 0 | 33 | 121 |
| 07:00 | 27 | 50 | 0 | 0 | 77 | 0 | 0 | 0 | 0 | 0 | 0 | 15 | 6 | 0 | 21 | 18 | 0 | 26 | 0 | 44 | 142 |
| 07:05 | 25 | 42 | 0 | 0 | 67 | 0 | 0 | 0 | 0 | 0 | 0 | 25 | 9 | 0 | 34 | 17 | 0 | 20 | 0 | 37 | 138 |
| 07:10 | 25 | 52 | 0 | 0 | 77 | 0 | 0 | 0 | 0 | 0 | 0 | 23 | 12 | 0 | 35 | 8 | 0 | 26 | 0 | 34 | 146 |
| 07:15 | 34 | 48 | 0 | 0 | 82 | 0 | 0 | 0 | 0 | 0 | 0 | 23 | 10 | 0 | 33 | 15 | 0 | 13 | 0 | 28 | 143 |
| 07:20 | 30 | 39 | 0 | 0 | 69 | 0 | 0 | 0 | 0 | 0 | 0 | 21 | 11 | 0 | 32 | 10 | 1 | 17 | 0 | 28 | 129 |
| 07:25 | 28 | 32 | 0 | 1 | 61 | 0 | 0 | 0 | 0 | 0 | 0 | 19 | 11 | 0 | 30 | 9 | 0 | 19 | 0 | 28 | 119 |
| 07:30 | 29 | 36 | 0 | 0 | 65 | 0 | 0 | 0 | 0 | 0 | 0 | 20 | 18 | 0 | 38 | 12 | 0 | 22 | 0 | 34 | 137 |
| Total Volume | 341 | 542 | 9 | 1 | 893 | 0 | 0 | 0 | 0 | 0 | 0 | 252 | 114 | 0 | 366 | 150 | 1 | 238 | 0 | 389 | 1648 |
| \% App. Total | 38.2 | 60.7 | 1 | 0.1 |  | 0 | 0 | 0 | 0 |  | 0 | 68.9 | 31.1 | 0 |  | 38.6 | 0.3 | 61.2 | 0 |  |  |
| PHF | . 729 | . 836 | . 083 | . 083 | . 809 | . 000 | . 000 | . 000 | . 000 | . 000 | . 000 | . 778 | . 528 | . 000 | . 803 | . 694 | . 083 | . 735 | . 000 | 737 | . 869 |



# LSC Transportation Consultants, Inc. 

2504 E. Pikes Peak Ave, Suite 304
Colorado Springs, CO 80909
719-633-2868
File Name : Hwy 24 - Woodmen Rd PM 5-23
Site Code : S214730
Start Date : 5/2/2023
Page No : 1

Groups Printed- Unshifted

| Groups Printed- Unshifte |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | t. Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Hwy 24 Southbound |  |  |  |  | Westbound |  |  |  |  | Hwy 24 Northbound |  |  |  |  | Woodmen Rd Eastbound |  |  |  |  |  |
| Start Time | Right | Thru | Left | Peds | App. Toala | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Toal | Right | Thru | Left | Peds | App. Toal |  |
| 16:00 | 26 | 17 | 0 | 0 | 43 | 0 | 0 | 0 | 0 | 0 | 0 | 39 | 33 | 0 | 72 | 4 | 0 | 48 | 0 | 52 | 167 |
| 16:05 | 28 | 28 | 0 | 0 | 56 | 0 | 0 | 0 | 0 | 0 | 0 | 41 | 24 | 0 | 65 | 9 | 0 | 41 | 1 | 51 | 172 |
| 16:10 | 28 | 30 | 0 | 0 | 58 | 0 | 0 | 0 | 0 | 0 | 0 | 37 | 21 | 0 | 58 | 8 | 0 | 14 | 0 | 22 | 138 |
| 16:15 | 31 | 28 | 0 | 0 | 59 | 0 | 0 | 0 | 0 | 0 | 0 | 40 | 29 | 0 | 69 | 9 | 0 | 53 | 0 | 62 | 190 |
| 16:20 | 24 | 19 | 0 | 0 | 43 | 0 | 0 | 0 | 0 | 0 | 0 | 42 | 23 | 0 | 65 | 5 | 0 | 52 | 0 | 57 | 165 |
| 16:25 | 38 | 26 | 0 | 0 | 64 | 0 | 0 | 0 | 0 | 0 | 0 | 41 | 17 | 0 | 58 | 9 | 0 | 43 | 0 | 52 | 174 |
| 16:30 | 20 | 23 | 0 | 0 | 43 | 0 | 0 | 0 | 0 | 0 | 0 | 35 | 21 | 0 | 56 | 11 | 0 | 38 | 0 | 49 | 148 |
| 16:35 | 25 | 19 | 0 | 2 | 46 | 0 | 0 | 0 | 0 | 0 | 0 | 40 | 18 | 0 | 58 | 12 | 0 | 44 | 0 | 56 | 160 |
| 16:40 | 32 | 18 | 0 | 0 | 50 | 0 | 0 | 0 | 0 | 0 | 0 | 41 | 28 | 0 | 69 | 6 | 0 | 38 | 0 | 44 | 163 |
| 16:45 | 33 | 26 | 9 | 0 | 68 | 0 | 0 | 0 | 0 | 0 | 0 | 59 | 19 | 0 | 78 | 9 | 0 | 5 | 0 | 14 | 160 |
| 16:50 | 32 | 25 | 0 | 0 | 57 | 0 | 0 | 0 | 0 | 0 | 0 | 45 | 22 | 0 | 67 | 10 | 0 | 54 | 1 | 65 | 189 |
| 16:55 | 23 | 14 | 0 | 0 | 37 | 0 | 0 | 0 | 0 | 0 | 0 | 35 | 18 | 0 | 53 | 6 | 0 | 50 | 0 | 56 | 146 |
| Total | 340 | 273 | 9 | 2 | 624 | 0 | 0 | 0 | 0 | 0 | 0 | 495 | 273 | 0 | 768 | 98 | 0 | 480 | 2 | 580 | 1972 |
| 17:00 | 35 | 23 | 0 | 0 | 58 | 0 | 0 | 0 | 0 | 0 | 0 | 44 | 24 | 0 | 68 | 10 | 0 | 44 | 0 | 54 | 180 |
| 17:05 | 26 | 23 | 0 | 0 | 49 | 0 | 0 | 0 | 0 | 0 | 0 | 27 | 26 | 0 | 53 | 9 | 0 | 45 | 0 | 54 | 156 |
| 17:10 | 23 | 34 | 0 | 0 | 57 | 0 | 0 | 0 | 0 | 0 | 0 | 50 | 28 | 0 | 78 | 4 | 0 | 43 | 0 | 47 | 182 |
| 17:15 | 26 | 37 | 0 | 0 | 63 | 0 | 0 | 0 | 0 | 0 | 0 | 71 | 37 | 0 | 108 | 8 | 0 | 34 | 0 | 42 | 213 |
| 17:20 | 27 | 28 | 0 | 4 | 59 | 0 | 0 | 0 | 0 | 0 | 0 | 42 | 24 | 0 | 66 | 6 | 0 | 46 | 0 | 52 | 177 |
| 17:25 | 37 | 30 | 0 | 1 | 68 | 0 | 0 | 0 | 0 | 0 | 0 | 42 | 26 | 0 | 68 | 10 | 0 | 51 | 0 | 61 | 197 |
| 17:30 | 22 | 13 | 0 | 0 | 35 | 0 | 0 | 0 | 0 | 0 | 0 | 37 | 27 | 0 | 64 | 10 | 0 | 39 | 0 | 49 | 148 |
| 17:35 | 29 | 16 | 0 | 1 | 46 | 0 | 0 | 0 | 0 | 0 | 0 | 24 | 23 | 0 | 47 | 10 | 0 | 53 | 0 | 63 | 156 |
| 17:40 | 21 | 19 | 0 | 1 | 41 | 0 | 0 | 0 | 0 | 0 | 0 | 35 | 18 | 0 | 53 | 7 | 0 | 61 | 0 | 68 | 162 |
| 17:45 | 16 | 19 | 0 | 0 | 35 | 0 | 0 | 0 | 0 | 0 | 0 | 43 | 34 | 0 | 77 | 5 | 0 | 46 | 0 | 51 | 163 |
| 17:50 | 26 | 16 | 0 | 0 | 42 | 0 | 0 | 0 | 0 | 0 | 0 | 44 | 22 | 0 | 66 | 8 | 0 | 25 | 0 | 33 | 141 |
| 17:55 | 23 | 15 | 0 | 1 | 39 | 0 | 0 | 0 | 0 | 0 | 0 | 41 | 26 | 0 | 67 | 6 | 0 | 33 | 0 | 39 | 145 |
| Total | 311 | 273 | 0 | 8 | 592 | 0 | 0 | 0 | 0 | 0 | 0 | 500 | 315 | 0 | 815 | 93 | 0 | 520 | 0 | 613 | 2020 |
| Grand Total | 651 | 546 | 9 | 10 | 1216 | 0 | 0 | 0 | 0 | 0 | 0 | 995 | 588 | 0 | 1583 | 191 | 0 | 1000 | 2 | 1193 | 3992 |
| Apprch \% | 53.5 | 44.9 | 0.7 | 0.8 |  | 0 | 0 | 0 | 0 |  | 0 | 62.9 | 37.1 | 0 |  | 16 | 0 | 83.8 | 0.2 |  |  |
| Total \% | 16.3 | 13.7 | 0.2 | 0.3 | 30.5 | 0 | 0 | 0 | 0 | 0 | 0 | 24.9 | 14.7 | 0 | 39.7 | 4.8 | 0 | 25.1 | 0.1 | 29.9 |  |

# LSC Transportation Consultants, Inc. 

2504 E. Pikes Peak Ave, Suite 304
Colorado Springs, CO 80909
719-633-2868
File Name : Hwy 24 - Woodmen Rd PM 5-23
Site Code : S214730
Start Date : 5/2/2023
Page No : 2

|  | Hwy 24 Southbound |  |  |  |  | Westbound |  |  |  |  | Hwy 24 Northbound |  |  |  |  | Woodmen Rd Eastbound |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Int. Total |
| Peak Hour Analysis From 16:00 to 17:55-Peak 1 of 1 Peak Hour for Entire Intersection Begins at 16:30 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 16:30 | 20 | 23 | 0 | 0 | 43 | 0 | 0 | 0 | 0 | 0 | 0 | 35 | 21 | 0 | 56 | 11 | 0 | 38 | 0 | 49 | 148 |
| 16:35 | 25 | 19 | 0 | 2 | 46 | 0 | 0 | 0 | 0 | 0 | 0 | 40 | 18 | 0 | 58 | 12 | 0 | 44 | 0 | 56 | 160 |
| 16:40 | 32 | 18 | 0 | 0 | 50 | 0 | 0 | 0 | 0 | 0 | 0 | 41 | 28 | 0 | 69 | 6 | 0 | 38 | 0 | 44 | 163 |
| 16:45 | 33 | 26 | 9 | 0 | 68 | 0 | 0 | 0 | 0 | 0 | 0 | 59 | 19 | 0 | 78 | 9 | 0 | 5 | 0 | 14 | 160 |
| 16:50 | 32 | 25 | 0 | 0 | 57 | 0 | 0 | 0 | 0 | 0 | 0 | 45 | 22 | 0 | 67 | 10 | 0 | 54 | 1 | 65 | 189 |
| 16:55 | 23 | 14 | 0 | 0 | 37 | 0 | 0 | 0 | 0 | 0 | 0 | 35 | 18 | 0 | 53 | 6 | 0 | 50 | 0 | 56 | 146 |
| 17:00 | 35 | 23 | 0 | 0 | 58 | 0 | 0 | 0 | 0 | 0 | 0 | 44 | 24 | 0 | 68 | 10 | 0 | 44 | 0 | 54 | 180 |
| 17:05 | 26 | 23 | 0 | 0 | 49 | 0 | 0 | 0 | 0 | 0 | 0 | 27 | 26 | 0 | 53 | 9 | 0 | 45 | 0 | 54 | 156 |
| 17:10 | 23 | 34 | 0 | 0 | 57 | 0 | 0 | 0 | 0 | 0 | 0 | 50 | 28 | 0 | 78 | 4 | 0 | 43 | 0 | 47 | 182 |
| 17:15 | 26 | 37 | 0 | 0 | 63 | 0 | 0 | 0 | 0 | 0 | 0 | 71 | 37 | 0 | 108 | 8 | 0 | 34 | 0 | 42 | 213 |
| 17:20 | 27 | 28 | 0 | 4 | 59 | 0 | 0 | 0 | 0 | 0 | 0 | 42 | 24 | 0 | 66 | 6 | 0 | 46 | 0 | 52 | 177 |
| 17:25 | 37 | 30 | 0 | 1 | 68 | 0 | 0 | 0 | 0 | 0 | 0 | 42 | 26 | 0 | 68 | 10 | 0 | 51 | 0 | 61 | 197 |
| Total Volume | 339 | 300 | 9 | 7 | 655 | 0 | 0 | 0 | 0 | 0 | 0 | 531 | 291 | 0 | 822 | 101 | 0 | 492 | 1 | 594 | 2071 |
| \% App. Total | 51.8 | 45.8 | 1.4 | 1.1 |  | 0 | 0 | 0 | 0 |  | 0 | 64.6 | 35.4 | 0 |  | 17 | 0 | 82.8 | 0.2 |  |  |
| PHF | . 764 | . 676 | . 083 | . 146 | . 803 | . 000 | . 000 | . 000 | . 000 | . 000 | . 000 | . 623 | . 655 | . 000 | . 634 | . 701 | . 000 | . 759 | . 083 | 762 | . 810 |



# LSC Transportation Consultants, Inc. 

2504 E. Pikes Peak Ave, Suite 304
Colorado Springs, CO 80909
719-633-2868
File Name : Hwy 24 - New Meridian Rd AM 5-23
Site Code : S214730
Start Date : 5/4/2023
Page No : 1

Groups Printed- Unshifted

|  | Hwy 24 Southbound |  |  |  |  | New Meridian Westbound |  |  |  |  | Hwy 24 Northbound |  |  |  |  | New Meridian Eastbound |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Right | Thru | Left | Peds | App. Toaal | Right | Thru | Left | Peds | ${ }_{\text {App }}$ Total | Right | Thru | Left | Peds | App. Toaal | Right | Thru | Left | Peds | App. Toat | Int. Total |
| 06:30 | 0 | 59 | 4 | 0 | 63 | 1 | 14 | 0 | 0 | 15 | 0 | 20 | 16 | 0 | 36 | 49 | 17 | 0 | 0 | 66 | 180 |
| 06:35 | 1 | 60 | 5 | 0 | 66 | 2 | 13 | 0 | 0 | 15 | 0 | 22 | 15 | 0 | 37 | 52 | 15 | 1 | 0 | 68 | 186 |
| 06:40 | 0 | 58 | 6 | 0 | 64 | 0 | 12 | 0 | 0 | 12 | 1 | 19 | 14 | 0 | 34 | 50 | 18 | 0 | 0 | 68 | 178 |
| 06:45 | 1 | 60 | 7 | 0 | 68 | 2 | 16 | 0 | 0 | 18 | 0 | 33 | 15 | 0 | 48 | 52 | 14 | 0 | 0 | 66 | 200 |
| 06:50 | 2 | 52 | 4 | 0 | 58 | 1 | 16 | 0 | 0 | 17 | 0 | 22 | 17 | 0 | 39 | 54 | 15 | 1 | 0 | 70 | 184 |
| 06:55 | 1 | 70 | 1 | 0 | 72 | 1 | 10 | 1 | 0 | 12 | 0 | 23 | 13 | 0 | 36 | 55 | 22 | 1 | 0 | 78 | 198 |
| Total | 5 | 359 | 27 | 0 | 391 | 7 | 81 | 1 | 0 | 89 | 1 | 139 | 90 | 0 | 230 | 312 | 101 | 3 | 0 | 416 | 1126 |
| 07:00 | 0 | 70 | 1 | 0 | 71 | 2 | 5 | 0 | 0 | 7 | 2 | 28 | 21 | 0 | 51 | 69 | 26 | 0 | 0 | 95 | 224 |
| 07:05 | 1 | 49 | 4 | 0 | 54 | 0 | 17 | 0 | 0 | 17 | 2 | 21 | 10 | 0 | 33 | 74 | 29 | 2 | 0 | 105 | 209 |
| 07:10 | 1 | 69 | 3 | 0 | 73 | 2 | 6 | 0 | 0 | 8 | 0 | 24 | 19 | 0 | 43 | 56 | 20 | 0 | 0 | 76 | 200 |
| 07:15 | 0 | 64 | 3 | 0 | 67 | 1 | 0 | 0 | 0 | 1 | 0 | 21 | 27 | 0 | 48 | 69 | 27 | 0 | 0 | 96 | 212 |
| 07:20 | 0 | 40 | 4 | 0 | 44 | 2 | 24 | 0 | 0 | 26 | 0 | 27 | 15 | 0 | 42 | 64 | 27 | 0 | 0 | 91 | 203 |
| 07:25 | 0 | 39 | 3 | 0 | 42 | 5 | 20 | 2 | 0 | 27 | 1 | 25 | 14 | 0 | 40 | 65 | 31 | 2 | 0 | 98 | 207 |
| 07:30 | 0 | 42 | 1 | 0 | 43 | 2 | 24 | 2 | 0 | 28 | 2 | 19 | 11 | 0 | 32 | 71 | 38 | 1 | 0 | 110 | 213 |
| 07:35 | 0 | 44 | 2 | 0 | 46 | 0 | 27 | 4 | 0 | 31 | 0 | 34 | 17 | 0 | 51 | 43 | 48 | 0 | 0 | 91 | 219 |
| 07:40 | 0 | 35 | 5 | 0 | 40 | 0 | 19 | 1 | 0 | 20 | 0 | 22 | 16 | 0 | 38 | 58 | 41 | 1 | 1 | 101 | 199 |
| 07:45 | 0 | 38 | 2 | 0 | 40 | 2 | 18 | 2 | 0 | 22 | 1 | 18 | 17 | 0 | 36 | 55 | 27 | 0 | 0 | 82 | 180 |
| 07:50 | 0 | 59 | 0 | 0 | 59 | 1 | 2 | 0 | 0 | 3 | 2 | 31 | 16 | 0 | 49 | 67 | 19 | 1 | 0 | 87 | 198 |
| 07:55 | 0 | 70 | 7 | 0 | 77 | 2 | 7 | 0 | 0 |  | 2 | 31 | 23 | 0 | 56 | 37 | 27 | 0 | 0 | 64 | 206 |
| Total | 2 | 619 | 35 | 0 | 656 | 19 | 169 | 11 | 0 | 199 | 12 | 301 | 206 | 0 | 519 | 728 | 360 | 7 | 1 | 1096 | 2470 |
| 08:00 | 1 | 51 | 5 | 0 | 57 | 2 | 18 | 1 | 0 | 21 | 0 | 33 | 33 | 0 | 66 | 39 | 12 | , | 0 | 52 | 196 |
| 08:05 | 0 | 30 | 4 | 0 | 34 | 2 | 16 | 1 | 0 | 19 | 3 | 31 | 28 | 0 | 62 | 31 | 17 | 0 | 0 | 48 | 163 |
| 08:10 | 1 | 52 | 5 | 0 | 58 | 1 | 17 | 1 | 0 | 19 | 1 | 30 | 22 | 0 | 53 | 45 | 17 | 0 | 0 | 62 | 192 |
| 08:15 | 0 | 36 | 2 | 0 | 38 | 4 | 26 | 2 | 0 | 32 | 3 | 13 | 17 | 0 | 33 | 29 | 24 | 3 | 0 | 56 | 159 |
| 08:20 | 0 | 39 | 4 | 0 | 43 | 2 | 24 | 1 | 0 | 27 | 2 | 24 | 20 | 0 | 46 | 41 | 20 | 2 | 0 | 63 | 179 |
| 08:25 | 1 | 39 | 8 | 0 | 48 | 3 | 25 | 0 | 0 | 28 | 0 | 15 | 24 | 0 | 39 | 45 | 17 | 0 | 0 | 62 | 177 |
| Grand Total | 10 | 1225 | 90 | 0 | 1325 | 40 | 376 | 18 | 0 | 434 | 22 | 586 | 440 | 0 | 1048 | 1270 | 568 | 16 | 1 | 1855 | 4662 |
| Apprch \% | 0.8 | 92.5 | 6.8 | 0 |  | 9.2 | 86.6 | 4.1 | 0 |  | 2.1 | 55.9 | 42 | 0 |  | 68.5 | 30.6 | 0.9 | 0.1 |  |  |
| Total \% | 0.2 | 26.3 | 1.9 | 0 | 28.4 | 0.9 | 8.1 | 0.4 | 0 | 9.3 | 0.5 | 12.6 | 9.4 | 0 | 22.5 | 27.2 | 12.2 | 0.3 | 0 | 39.8 |  |

# LSC Transportation Consultants, Inc. 

2504 E. Pikes Peak Ave, Suite 304
Colorado Springs, CO 80909
719-633-2868
File Name : Hwy 24 - New Meridian Rd AM 5-23
Site Code : S214730
Start Date : 5/4/2023
Page No : 2

|  | Hwy 24 Southbound |  |  |  |  | New Meridian Westbound |  |  |  |  | Hwy 24 Northbound |  |  |  |  | New Meridian Eastbound |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Int. Total |
| Peak Hour Analysis From 06:30 to 08:25-Peak 1 of 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour | or Ent | re Int | rsect | on Be | ins at | 07:00 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 07:00 | 0 | 70 | 1 | 0 | 71 | 2 | 5 | 0 | 0 | 7 | 2 | 28 | 21 | 0 | 51 | 69 | 26 | 0 | 0 | 95 | 224 |
| 07:05 | 1 | 49 | 4 | 0 | 54 | 0 | 17 | 0 | 0 | 17 | 2 | 21 | 10 | 0 | 33 | 74 | 29 | 2 | 0 | 105 | 209 |
| 07:10 | 1 | 69 | 3 | 0 | 73 | 2 | 6 | 0 | 0 | 8 | 0 | 24 | 19 | 0 | 43 | 56 | 20 | 0 | 0 | 76 | 200 |
| 07:15 | 0 | 64 | 3 | 0 | 67 | 1 | 0 | 0 | 0 | 1 | 0 | 21 | 27 | 0 | 48 | 69 | 27 | 0 | 0 | 96 | 212 |
| 07:20 | 0 | 40 | 4 | 0 | 44 | 2 | 24 | 0 | 0 | 26 | 0 | 27 | 15 | 0 | 42 | 64 | 27 | 0 | 0 | 91 | 203 |
| 07:25 | 0 | 39 | 3 | 0 | 42 | 5 | 20 | 2 | 0 | 27 | 1 | 25 | 14 | 0 | 40 | 65 | 31 | 2 | 0 | 98 | 207 |
| 07:30 | 0 | 42 | 1 | 0 | 43 | 2 | 24 | 2 | 0 | 28 | 2 | 19 | 11 | 0 | 32 | 71 | 38 | 1 | 0 | 110 | 213 |
| 07:35 | 0 | 44 | 2 | 0 | 46 | 0 | 27 | 4 | 0 | 31 | 0 | 34 | 17 | 0 | 51 | 43 | 48 | 0 | 0 | 91 | 219 |
| 07:40 | 0 | 35 | 5 | 0 | 40 | 0 | 19 | 1 | 0 | 20 | 0 | 22 | 16 | 0 | 38 | 58 | 41 | 1 | 1 | 101 | 199 |
| 07:45 | 0 | 38 | 2 | 0 | 40 | 2 | 18 | 2 | 0 | 22 | 1 | 18 | 17 | 0 | 36 | 55 | 27 | 0 | 0 | 82 | 180 |
| 07:50 | 0 | 59 | 0 | 0 | 59 | 1 | 2 | 0 | 0 | 3 | 2 | 31 | 16 | 0 | 49 | 67 | 19 | 1 | 0 | 87 | 198 |
| 07:55 | 0 | 70 | 7 | 0 | 77 | 2 | 7 | 0 | 0 | 9 | 2 | 31 | 23 | 0 | 56 | 37 | 27 | 0 | 0 | 64 | 206 |
| Total Volume | 2 | 619 | 35 | 0 | 656 | 19 | 169 | 11 | 0 | 199 | 12 | 301 | 206 | 0 | 519 | 728 | 360 | 7 | 1 | 1096 | 2470 |
| \% App. Total | 0.3 | 94.4 | 5.3 | 0 |  | 9.5 | 84.9 | 5.5 | 0 |  | 2.3 | 58 | 39.7 | 0 |  | 66.4 | 32.8 | 0.6 | 0.1 |  |  |
| PHF | . 167 | . 737 | . 417 | . 000 | . 710 | . 317 | . 522 | . 229 | . 000 | . 535 | . 500 | . 738 | . 636 | . 000 | . 772 | . 820 | . 625 | . 292 | . 083 | . 830 | . 919 |



# LSC Transportation Consultants, Inc. <br> 2504 E. Pikes Peak Ave, Suite 304 <br> Colorado Springs, CO 80909 <br> 719-633-2868 

File Name : Hwy 24 - New Meridian PM
Site Code: S214730
Start Date : 5/4/2023
Page No : 1

Groups Printed- Unshifted

|  | Hwy 24 Southbound |  |  |  |  | New Meridian Westbound |  |  |  |  | Hwy 24 Northbound |  |  |  |  | New Meridian Eastbound |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Int. Total |
| 16:00 | 1 | 37 | 4 | 0 | 42 | 1 | 48 | 2 | 0 | 51 | 1 | 47 | 40 | 0 | 88 | 23 | 21 | 2 | 0 | 46 | 227 |
| 16:05 | 0 | 29 | 8 | 0 | 37 | 6 | 28 | 3 | 0 | 37 | 0 | 58 | 41 | 0 | 99 | 31 | 21 | 0 | 0 | 52 | 225 |
| 16:10 | 2 | 35 | 3 | 0 | 40 | 4 | 29 | 0 | 0 | 33 | 0 | 55 | 52 | 0 | 107 | 18 | 11 | 4 | 0 | 33 | 213 |
| 16:15 | 0 | 33 | 5 | 0 | 38 | 6 | 34 | 1 | 0 | 41 | 1 | 63 | 53 | 0 | 117 | 33 | 20 | 0 | 0 | 53 | 249 |
| 16:20 | 0 | 44 | 5 | 0 | 49 | 4 | 23 | 1 | 0 | 28 | 2 | 65 | 53 | 0 | 120 | 30 | 15 | 1 | 0 | 46 | 243 |
| 16:25 | 1 | 50 | 4 | 0 | 55 | 2 | 28 | 1 | 0 | 31 | 0 | 55 | 50 | 0 | 105 | 21 | 17 | 1 | 0 | 39 | 230 |
| 16:30 | 1 | 21 | 4 | 0 | 26 | 4 | 26 | 0 | 0 | 30 | 1 | 51 | 60 | 0 | 112 | 16 | 20 | 2 | 0 | 38 | 206 |
| 16:35 | 0 | 29 | 5 | 0 | 34 | 2 | 37 | 0 | 0 | 39 | 0 | 69 | 54 | 0 | 123 | 17 | 19 | 0 | 1 | 37 | 233 |
| 16:40 | 0 | 29 | 3 | 0 | 32 | 3 | 33 | 1 | 0 | 37 | 0 | 42 | 51 | 0 | 93 | 24 | 22 | 2 | 0 | 48 | 210 |
| 16:45 | 0 | 26 | 5 | 0 | 31 | 4 | 22 | 0 | 0 | 26 | 0 | 73 | 63 | 0 | 136 | 47 | 15 | 4 | 0 | 66 | 259 |
| 16:50 | 0 | 22 | 7 | 0 | 29 | 6 | 21 | 1 | 0 | 28 | 1 | 53 | 48 | 0 | 102 | 25 | 24 | 3 | 0 | 52 | 211 |
| 16:55 | 2 | 48 | 2 | 0 | 52 | 1 | 22 | 1 | 0 | 24 | 0 | 53 | 43 | 0 | 96 | 22 | 22 | 0 | 0 | 44 | 216 |
| Total | 7 | 403 | 55 | 0 | 465 | 43 | 351 | 11 | 0 | 405 | 6 | 684 | 608 | 0 | 1298 | 307 | 227 | 19 | 1 | 554 | 2722 |
| 17:00 | 1 | 33 | 4 | 0 | 38 | 4 | 18 | 0 | 0 | 22 | 0 | 59 | 61 | 0 | 120 | 30 | 14 | 2 | 0 | 46 | 226 |
| 17:05 | 0 | 30 | 8 | 0 | 38 | 2 | 24 | 2 | 0 | 28 | 0 | 46 | 49 | 0 | 95 | 20 | 21 | 2 | 0 | 43 | 204 |
| 17:10 | 1 | 38 | 2 | 0 | 41 | 1 | 33 | 3 | 0 | 37 | 0 | 47 | 45 | 1 | 93 | 27 | 16 | 0 | 0 | 43 | 214 |
| 17:15 | 0 | 31 | 7 | 0 | 38 | 6 | 25 | 1 | 0 | 32 | 0 | 34 | 34 | 0 | 68 | 25 | 33 | 2 | 0 | 60 | 198 |
| 17:20 | 0 | 39 | 6 | 0 | 45 | 1 | 14 | 0 | 0 | 15 | 1 | 72 | 50 | 0 | 123 | 25 | 11 | 0 | 0 | 36 | 219 |
| 17:25 | 1 | 32 | 9 | 0 | 42 | 3 | 20 | 0 | 0 | 23 | 0 | 73 | 42 | 0 | 115 | 25 | 16 | 0 | 0 | 41 | 221 |
| 17:30 | 1 | 19 | 4 | 0 | 24 | 3 | 13 | 0 | 0 | 16 | 0 | 63 | 52 | 0 | 115 | 20 | 18 | 0 | 0 | 38 | 193 |
| 17:35 | 0 | 26 | 1 | 0 | 27 | 1 | 20 | 1 | 0 | 22 | 1 | 55 | 53 | 0 | 109 | 20 | 11 | 3 | 0 | 34 | 192 |
| 17:40 | 0 | 33 | 7 | 0 | 40 | 2 | 10 | 0 | 0 | 12 | 1 | 47 | 42 | 0 | 90 | 25 | 12 | 0 | 0 | 37 | 179 |
| 17:45 | 0 | 26 | 3 | 0 | 29 | 5 | 15 | 0 | 0 | 20 | 0 | 48 | 43 | 0 | 91 | 19 | 26 | 2 | 0 | 47 | 187 |
| 17:50 | 2 | 20 | 5 | 0 | 27 | 3 | 15 | 0 | 0 | 18 | 0 | 49 | 41 | 0 | 90 | 17 | 20 | 2 | 0 | 39 | 174 |
| 17:55 | 0 | 37 | 5 | 0 | 42 | 1 | 11 | 1 | 0 | 13 | 0 | 41 | 38 | 0 | 79 | 14 | 12 | 2 | 0 | 28 | 162 |
| Total | 6 | 364 | 61 | 0 | 431 | 32 | 218 | 8 | 0 | 258 | 3 | 634 | 550 | 1 | 1188 | 267 | 210 | 15 | 0 | 492 | 2369 |
| Grand Total | 13 | 767 | 116 | 0 | 896 | 75 | 569 | 19 | 0 | 663 | 9 | 1318 | 1158 | 1 | 2486 | 574 | 437 | 34 | 1 | 1046 | 5091 |
| Apprch \% | 1.5 | 85.6 | 12.9 | 0 |  | 11.3 | 85.8 | 2.9 | 0 |  | 0.4 | 53 | 46.6 | 0 |  | 54.9 | 41.8 | 3.3 | 0.1 |  |  |
| Total \% | 0.3 | 15.1 | 2.3 | 0 | 17.6 | 1.5 | 11.2 | 0.4 | 0 | 13 | 0.2 | 25.9 | 22.7 | 0 | 48.8 | 11.3 | 8.6 | 0.7 | 0 | 20.5 |  |

# LSC Transportation Consultants, Inc. 

2504 E. Pikes Peak Ave, Suite 304
Colorado Springs, CO 80909
719-633-2868
File Name : Hwy 24 - New Meridian PM
Site Code : S214730
Start Date : 5/4/2023
Page No : 2

|  | Hwy 24 Southbound |  |  |  |  | New Meridian Westbound |  |  |  |  | Hwy 24 Northbound |  |  |  |  | New Meridian Eastbound |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Int. Total |
| Peak Hour Analysis From 16:00 to 17:55-Peak 1 of 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour | or Ent | Int | rsect | on Be | ins at | 16:00 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 16:00 | 1 | 37 | 4 | 0 | 42 | 1 | 48 | 2 | 0 | 51 | 1 | 47 | 40 | 0 | 88 | 23 | 21 | 2 | 0 | 46 | 227 |
| 16:05 | 0 | 29 | 8 | 0 | 37 | 6 | 28 | 3 | 0 | 37 | 0 | 58 | 41 | 0 | 99 | 31 | 21 | 0 | 0 | 52 | 225 |
| 16:10 | 2 | 35 | 3 | 0 | 40 | 4 | 29 | 0 | 0 | 33 | 0 | 55 | 52 | 0 | 107 | 18 | 11 | 4 | 0 | 33 | 213 |
| 16:15 | 0 | 33 | 5 | 0 | 38 | 6 | 34 | 1 | 0 | 41 | 1 | 63 | 53 | 0 | 117 | 33 | 20 | 0 | 0 | 53 | 249 |
| 16:20 | 0 | 44 | 5 | 0 | 49 | 4 | 23 | 1 | 0 | 28 | 2 | 65 | 53 | 0 | 120 | 30 | 15 | 1 | 0 | 46 | 243 |
| 16:25 | 1 | 50 | 4 | 0 | 55 | 2 | 28 | 1 | 0 | 31 | 0 | 55 | 50 | 0 | 105 | 21 | 17 | 1 | 0 | 39 | 230 |
| 16:30 | 1 | 21 | 4 | 0 | 26 | 4 | 26 | 0 | 0 | 30 | 1 | 51 | 60 | 0 | 112 | 16 | 20 | 2 | 0 | 38 | 206 |
| 16:35 | 0 | 29 | 5 | 0 | 34 | 2 | 37 | 0 | 0 | 39 | 0 | 69 | 54 | 0 | 123 | 17 | 19 | 0 | 1 | 37 | 233 |
| 16:40 | 0 | 29 | 3 | 0 | 32 | 3 | 33 | 1 | 0 | 37 | 0 | 42 | 51 | 0 | 93 | 24 | 22 | 2 | 0 | 48 | 210 |
| 16:45 | 0 | 26 | 5 | 0 | 31 | 4 | 22 | 0 | 0 | 26 | 0 | 73 | 63 | 0 | 136 | 47 | 15 | 4 | 0 | 66 | 259 |
| 16:50 | 0 | 22 | 7 | 0 | 29 | 6 | 21 | 1 | 0 | 28 | 1 | 53 | 48 | 0 | 102 | 25 | 24 | 3 | 0 | 52 | 211 |
| 16:55 | 2 | 48 | 2 | 0 | 52 | 1 | 22 | 1 | 0 | 24 | 0 | 53 | 43 | 0 | 96 | 22 | 22 | 0 | 0 | 44 | 216 |
| Total Volume | 7 | 403 | 55 | 0 | 465 | 43 | 351 | 11 | 0 | 405 | 6 | 684 | 608 | 0 | 1298 | 307 | 227 | 19 | 1 | 554 | 2722 |
| \% App. Total | 1.5 | 86.7 | 11.8 | 0 |  | 10.6 | 86.7 | 2.7 | 0 |  | 0.5 | 52.7 | 46.8 | 0 |  | 55.4 | 41 | 3.4 | 0.2 |  |  |
| PHF | . 292 | . 672 | . 573 | . 000 | . 705 | . 597 | . 609 | . 306 | . 000 | . 662 | . 250 | . 781 | . 804 | . 000 | . 795 | . 544 | . 788 | . 396 | . 083 | .699 | . 876 |



## LSC Transportation Consultants, Inc.

2504 E. Pikes Peak Ave, Suite 304
Colorado Springs, CO 80909
719-633-2868
File Name : Hwy 24 - Rio Ln TM AM 5-23
Site Code : S214730
Start Date : 5/16/2023
Page No : 1

|  | Hwy 24 Southbound |  |  |  |  | Rio Ln Westbound |  |  |  |  | $\begin{gathered} \text { Hwy } 24 \\ \text { Northbound } \end{gathered}$ |  |  |  |  | Eastbound |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | R | T | L | U | App. Total | R | T | L | U | App. Total | $\mathbf{R}$ | T | L | U | App. Total | R | T | L | U | App. Total | Int. Total |
| 06:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 3 | 4 | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 7 |
| 06:35 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 3 | 5 | 0 | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 8 |
| 06:40 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 8 | 0 | 8 | 4 | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 12 |
| 06:45 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 7 | 0 | 7 | 2 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 10 |
| 06:50 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 4 | 0 | 5 | 5 | 0 | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 10 |
| 06:55 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 4 | 5 | 0 | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 9 |
| Total | 0 | 0 | 1 | 0 | 1 | 1 | 0 | 29 | 0 | 30 | 25 | 0 | 0 | 0 | 25 | 0 | 0 | 0 | 0 | 0 | 56 |
| 07:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 0 | 7 | 6 | 0 | 0 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 13 |
| 07:05 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 2 | 5 | 0 | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 7 |
| 07:10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 3 | 3 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 6 |
| 07:15 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 4 | 0 | 6 | 10 | 0 | 0 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 16 |
| 07:20 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 2 | 6 | 0 | 0 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 8 |
| 07:25 | 0 | 0 | 1 | 0 | 1 | 1 | 0 | 3 | 0 | 4 | 6 | 0 | 0 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 11 |
| 07:30 | 0 | 0 | 1 | 0 | 1 | 1 | 0 | 1 | 0 | 2 | 8 | 0 | 0 | 0 | 8 | 0 | 0 | 0 | 0 | 0 | 11 |
| 07:35 | 0 | 0 | 1 | 0 | 1 | 1 | 0 | 5 | 0 | 6 | 11 | 0 | 0 | 0 | 11 | 0 | 0 | 0 | 0 | 0 | 18 |
| 07:40 | 0 | 0 | 3 | 0 | 3 | 0 | 0 | 4 | 0 | 4 | 8 | 0 | 0 | 0 | 8 | 0 | 0 | 0 | 0 | 0 | 15 |
| 07:45 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 3 | 0 | 4 | 3 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 7 |
| 07:50 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 5 | 0 | 9 | 7 | 0 | 0 | 0 | 7 | 0 | 0 | 0 | 0 | 0 | 16 |
| 07:55 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 8 | 0 | 9 | 3 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 12 |
| Total | 0 | 0 | 6 | 0 | 6 | 11 | 0 | 47 | 0 | 58 | 76 | 0 | 0 | 0 | 76 | 0 | 0 | 0 | 0 | 0 | 140 |
| 08:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 4 | 5 | 0 | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 9 |

## LSC Transportation Consultants, Inc.

2504 E. Pikes Peak Ave, Suite 304
Colorado Springs, CO 80909
719-633-2868
File Name : Hwy 24 - Rio Ln TM AM 5-23
Site Code : S214730
Start Date : 5/16/2023
Page No : 2

|  | Hwy 24 Southbound |  |  |  |  | Rio Ln <br> Westbound |  |  |  |  | Hwy 24 <br> Northbound |  |  |  |  | Eastbound |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start <br> Time | R | T | L | U | App. Total | R | T | L | U | App. Total | R | T | L | U | App. Total | R | T | L | U | App. Total | Int. Total |
| 08:05 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 5 | 0 | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 6 |
| 08:10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 2 | 2 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 4 |
| 08:15 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 6 | 0 | 7 | 2 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 9 |
| 08:20 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 4 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 5 |
| 08:25 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 3 | 2 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 5 |
| Grand Total | 0 | 0 | 7 | 0 | 7 | 13 | 0 | 96 | 0 | 109 | 118 | 0 | 0 | 0 | 118 | 0 | 0 | 0 | 0 | 0 | 234 |
| Apprch \% | 0 | 0 | 100 | 0 |  | 11.9 | 0 | 88.1 | 0 |  | 100 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |  |  |
| Total \% | 0 | 0 | 3 | 0 | 3 | 5.6 | 0 | 41 | 0 | 46.6 | 50.4 | 0 | 0 | 0 | 50.4 | 0 | 0 | 0 | 0 | 0 |  |

## LSC Transportation Consultants, Inc.

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File Name : Hwy 24 - Rio Ln TM AM 5-23
Site Code : S214730
Start Date : 5/16/2023
Page No : 3

|  | Hwy 24 Southbound |  |  |  |  | $\begin{gathered} \text { Rio Ln } \\ \text { Westbound } \end{gathered}$ |  |  |  |  | Hwy 24 Northbound |  |  |  |  | Eastbound |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | R | T | L | U | App. Total | R | T | L | U | App. Total | R | T | L | U | App. Total | R | T | L | U | App. Total |  | Int. Total | Peak Hour Analysis From 06:30 to 08:25 - Peak 1 of 1



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## LSC Transportation Consultants, Inc.

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719-633-2868
File Name : Hwy 24 - Rio Ln TM PM 5-23
Site Code : S214730
Start Date : 5/16/2023
Page No : 1

|  | Hwy 24 Southbound |  |  |  |  | $\begin{gathered} \text { Rio Ln } \\ \text { Westbound } \end{gathered}$ |  |  |  |  | Hwy 24 <br> Northbound |  |  |  |  | Eastbound |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | R | T | L | U | App. Total | R | T | L | U | App. Total | R | T | L | U | App. Total | R | T | L | U | App. Total | Int. Total |
| 16:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 13 | 0 | 13 | 33 | 0 | 0 | 0 | 33 | 0 | 0 | 0 | 0 | 0 | 46 |
| 16:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 16 | 0 | 16 | 15 | 0 | 0 | 0 | 15 | 0 | 0 | 0 | 0 | 0 | 31 |
| 16:30 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 21 | 0 | 23 | 23 | 0 | 0 | 0 | 23 | 0 | 0 | 0 | 0 | 0 | 46 |
| 16:45 | 0 | 0 | 2 | 0 | 2 | 2 | 0 | 16 | 0 | 18 | 28 | 0 | 0 | 0 | 28 | 0 | 0 | 0 | 0 | 0 | 48 |
| Total | 0 | 0 | 2 | 0 | 2 | 4 | 0 | 66 | 0 | 70 | 99 | 0 | 0 | 0 | 99 | 0 | 0 | 0 | 0 | 0 | 171 |
| 17:00 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 5 | 0 | 5 | 28 | 0 | 0 | 0 | 28 | 0 | 0 | 0 | 0 | 0 | 34 |
| 17:15 | 0 | 0 | 1 | 0 | 1 | 1 | 0 | 10 | 0 | 11 | 19 | 0 | 0 | 0 | 19 | 0 | 0 | 0 | 0 | 0 | 31 |
| 17:30 | 0 | 0 | 1 | 0 | 1 | 2 | 0 | 5 | 0 | 7 | 32 | 0 | 0 | 0 | 32 | 0 | 0 | 0 | 0 | 0 | 40 |
| 17:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 12 | 0 | 12 | 21 | 0 | 0 | 0 | 21 | 0 | 0 | 0 | 0 | 0 | 33 |
| Total | 0 | 0 | 3 | 0 | 3 | 3 | 0 | 32 | 0 | 35 | 100 | 0 | 0 | 0 | 100 | 0 | 0 | 0 | 0 | 0 | 138 |
| Grand Total | 0 | 0 | 5 | 0 | 5 | 7 | 0 | 98 | 0 | 105 | 199 | 0 | 0 | 0 | 199 | 0 | 0 | 0 | 0 | 0 | 309 |
| Apprch \% | 0 | 0 | 100 | 0 |  | 6.7 | 0 | 93.3 | 0 |  | 100 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |  |  |
| Total \% | 0 | 0 | 1.6 | 0 | 1.6 | 2.3 | 0 | 31.7 | 0 | 34 | 64.4 | 0 | 0 | 0 | 64.4 | 0 | 0 | 0 | 0 | 0 |  |

## LSC Transportation Consultants, Inc.

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File Name : Hwy 24 - Rio Ln TM PM 5-23
Site Code : S214730
Start Date : 5/16/2023
Page No : 2

|  | Hwy 24 <br> Southbound |  |  |  |  | $\begin{gathered} \text { Rio Ln } \\ \text { Westbound } \end{gathered}$ |  |  |  |  | Hwy 24Northbound |  |  |  |  | Eastbound |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | R | T | L | U | App. Total | R | T | L | U | App. Total | R | T | L | U | App. Total | R | T | L | U | App. Total | Int. Total |
| Peak Hour Analysis From 4:00:00 PM to 5:45:00 PM - Peak 1 of 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour for Entire Intersection Begins at 4:00:00 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4:00:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 13 | 0 | 13 | 33 | 0 | 0 | 0 | 33 | 0 | 0 | 0 | 0 | 0 | 46 |
| 4:15:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 16 | 0 | 16 | 15 | 0 | 0 | 0 | 15 | 0 | 0 | 0 | 0 | 0 | 31 |
| 4:30:00 PM | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 21 | 0 | 23 | 23 | 0 | 0 | 0 | 23 | 0 | 0 | 0 | 0 | 0 | 46 |
| 4:45:00 PM | 0 | 0 | 2 | 0 | 2 | 2 | 0 | 16 | 0 | 18 | 28 | 0 | 0 | 0 | 28 | 0 | 0 | 0 | 0 | 0 | 48 |
| Total Volume | 0 | 0 | 2 | 0 | 2 | 4 | 0 | 66 | 0 | 70 | 99 | 0 | 0 | 0 | 99 | 0 | 0 | 0 | 0 | 0 | 171 |
| \% App. Total | 0 | 0 | 100 | 0 |  | 5.7 | 0 | 94.3 | 0 |  | 100 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |  |  |
| PHF | . 000 | . 000 | . 250 | . 000 | . 250 | . 500 | . 000 | . 786 | . 000 | . 761 | . 750 | . 000 | . 000 | . 000 | . 750 | . 000 | . 000 | . 000 | . 000 | . 000 | . 891 |

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File Name : Hwy 24 - Rio Ln TM PM 5-23
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## LSC Transportation Consultants, Inc.

2504 E. Pikes Peak Ave, Suite 304
Colorado Springs, CO 80909
719-633-2868
File Name : Hwy 24 - Old Meridian Rd AM
Site Code : 00000000
Start Date : 11/30/2021
Page No : 1

Groups Printed- Unshifted

|  | Hwy 24 Southbound |  |  |  |  | Old Meridian Rd Westbound |  |  |  |  | Hwy 24Northbound |  |  |  |  | Old Meridian Rd Eastbound |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start <br> Time | L | T | R | U | App. Total | L | T | R | U | App. Total | L | T | R | U | App. Total | L | T | R | U | App. Total | Int. Total |
| 06:30 AM | 0 | 187 | 0 | 0 | 187 | 0 | 0 | 4 | 0 | 4 | 0 | 76 | 2 | 0 | 78 | 0 | 0 | 7 | 0 | 7 | 276 |
| 06:45 AM | 0 | 183 | 0 | 0 | 183 | 0 | 0 | 2 | 0 | 2 | 0 | 116 | 5 | 0 | 121 | 0 | 0 | 7 | 0 | 7 | 313 |
| Total | 0 | 370 | 0 | 0 | 370 | 0 | 0 | 6 | 0 | 6 | 0 | 192 | 7 | 0 | 199 | 0 | 0 | 14 | 0 | 14 | 589 |
| 07:00 AM | 0 | 182 | 2 | 0 | 184 | 0 | 0 | 7 | 0 | 7 | 0 | 115 | 7 | 0 | 122 | 0 | 0 | 4 | 0 | 4 | 317 |
| 07:15 AM | 0 | 125 | 1 | 0 | 126 | 0 | 0 | 7 | 0 | 7 | 0 | 92 | 2 | 0 | 94 | 0 | 0 | 6 | 0 | 6 | 233 |
| 07:30 AM | 0 | 155 | 1 | 0 | 156 | 0 | 0 | 7 | 0 | 7 | 0 | 105 | 4 | 0 | 109 | 0 | 0 | 8 | 0 | 8 | 280 |
| 07:45 AM | 0 | 167 | 3 | 0 | 170 | 0 | 0 | 11 | 0 | 11 | 0 | 95 | 4 | 0 | 99 | 0 | 0 | 3 | 0 | 3 | 283 |
| Total | 0 | 629 | 7 | 0 | 636 | 0 | 0 | 32 | 0 | 32 | 0 | 407 | 17 | 0 | 424 | 0 | 0 | 21 | 0 | 21 | 1113 |


| 08:00 AM | 0 | 112 | 0 | 0 | 112 | 0 | 0 | 10 | 0 | 10 | 0 | 82 | 5 | 0 | 87 | 0 | 0 | 9 | 0 | 9 | 218 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 08:15 AM | 0 | 144 | 4 | 0 | 148 | 0 | 0 | 6 | 0 | 6 | 0 | 91 | 5 | 0 | 96 | 0 | 1 | 8 | 0 | 9 | 259 |
| Grand Total | 0 | 1255 | 11 | 0 | 1266 | 0 | 0 | 54 | 0 | 54 | 0 | 772 | 34 | 0 | 806 | 0 | 1 | 52 | 0 | 53 | 2179 |
| Apprch \% | 0 | 99.1 | 0.9 | 0 |  | 0 | 0 | 100 | 0 |  | 0 | 95.8 | 4.2 | 0 |  | 0 | 1.9 | 98.1 | 0 |  |  |
| Total \% | 0 | 57.6 | 0.5 | 0 | 58.1 | 0 | 0 | 2.5 | 0 | 2.5 | 0 | 35.4 | 1.6 | 0 | 37 | 0 | 0 | 2.4 | 0 | 2.4 |  |

## LSC Transportation Consultants, Inc.

2504 E. Pikes Peak Ave, Suite 304
Colorado Springs, CO 80909
719-633-2868

File Name : Hwy 24 - Old Meridian Rd AM
Site Code : 00000000
Start Date : 11/30/2021
Page No : 2

|  | Hwy 24 <br> Southbound |  |  |  |  | Old Meridian Rd Westbound |  |  |  |  | Hwy 24Northbound |  |  |  |  | Old Meridian Rd Eastbound |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | L | T | R | U | App. Total | L | T | R | U | App. Total | L | T | R | U | App. Total | L | T | R | U | App. Total | Int. Total |
| Peak Hour Analysis From 6:30:00 AM to 8:15:00 AM - Peak 1 of 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour for Entire Intersection Begins at 6:45:00 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 6:45:00 AM | 0 | 183 | 0 | 0 | 183 | 0 | 0 | 2 | 0 | 2 | 0 | 116 | 5 | 0 | 121 | 0 | 0 | 7 | 0 | 7 | 313 |
| 7:00:00 AM | 0 | 182 | 2 | 0 | 184 | 0 | 0 | 7 | 0 | 7 | 0 | 115 | 7 | 0 | 122 | 0 | 0 | 4 | 0 | 4 | 317 |
| 7:15:00 AM | 0 | 125 | 1 | 0 | 126 | 0 | 0 | 7 | 0 | 7 | 0 | 92 | 2 | 0 | 94 | 0 | 0 | 6 | 0 | 6 | 233 |
| 7:30:00 AM | 0 | 155 | 1 | 0 | 156 | 0 | 0 | 7 | 0 | 7 | 0 | 105 | 4 | 0 | 109 | 0 | 0 | 8 | 0 | 8 | 280 |
| Total Volume | 0 | 645 | 4 | 0 | 649 | 0 | 0 | 23 | 0 | 23 | 0 | 428 | 18 | 0 | 446 | 0 | 0 | 25 | 0 | 25 | 1143 |
| \% App. Total | 0 | 99.4 | 0.6 | 0 |  | 0 | 0 | 100 | 0 |  | 0 | 96 | 4 | 0 |  | 0 | 0 | 100 | 0 |  |  |
| PHF | . 000 | . 881 | . 500 | . 000 | . 882 | . 000 | . 000 | . 821 | . 000 | . 821 | . 000 | . 922 | . 643 | . 000 | . 914 | . 000 | . 000 | . 781 | . 000 | . 781 | . 901 |

LSC Transportation Consultants, Inc.
2504 E. Pikes Peak Ave, Suite 304
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719-633-2868
File Name : Hwy 24 - Old Meridian Rd AM
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## LSC Transportation Consultants, Inc.

2504 E. Pikes Peak Ave, Suite 304
Colorado Springs, CO 80909
719-633-2868

File Name : Hwy 24 - Old Meridian Rd PM
Site Code : 00000000
Start Date : 12/1/2021
Page No : 1

Groups Printed- Unshifted

|  | Hwy 24 Southbound |  |  |  |  | Old Meridian Rd Westbound |  |  |  |  | $\begin{gathered} \text { Hwy } 24 \\ \text { Northbound } \end{gathered}$ |  |  |  |  | Old Meridian Rd Eastbound |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start <br> Time | L | T | R | U | App. Total | L | T | R | U | App. Total | L | T | R | U | App. Total | L | T | R | U | App. Total | Int. Total |
| 04:00 PM | 0 | 118 | 3 | 0 | 121 | 0 | 0 | 12 | 0 | 12 | 0 | 152 | 7 | 0 | 159 | 0 | 0 | 19 | 0 | 19 | 311 |
| 04:15 PM | 0 | 106 | 3 | 0 | 109 | 0 | 0 | 11 | 0 | 11 | 0 | 178 | 1 | 0 | 179 | 0 | 0 | 11 | 0 | 11 | 310 |
| 04:30 PM | 0 | 109 | 3 | 0 | 112 | 0 | 0 | 12 | 0 | 12 | 0 | 219 | 1 | 0 | 220 | 0 | 0 | 12 | 0 | 12 | 356 |
| 04:45 PM | 0 | 82 | 1 | 0 | 83 | 0 | 0 | 12 | 0 | 12 | 0 | 191 | 1 | 0 | 192 | 0 | 0 | 15 | 0 | 15 | 302 |
| Total | 0 | 415 | 10 | 0 | 425 | 0 | 0 | 47 | 0 | 47 | 0 | 740 | 10 | 0 | 750 | 0 | 0 | 57 | 0 | 57 | 1279 |
| 05:00 PM | 0 | 119 | 1 | 0 | 120 | 0 | 0 | 8 | 0 | 8 | 0 | 192 | 6 | 0 | 198 | 0 | 0 | 17 | 0 | 17 | 343 |
| 05:15 PM | 0 | 130 | 0 | 0 | 130 | 0 | 0 | 13 | 0 | 13 | 0 | 195 | 6 | 0 | 201 | 0 | 0 | 8 | 0 | 8 | 352 |
| 05:30 PM | 0 | 89 | 2 | 0 | 91 | 0 | 0 | 12 | 0 | 12 | 0 | 179 | 5 | 0 | 184 | 0 | 0 | 16 | 0 | 16 | 303 |
| 05:45 PM | 0 | 100 | 1 | 0 | 101 | 0 | 0 | 6 | 0 | 6 | 0 | 208 | 6 | 0 | 214 | 0 | 0 | 10 | 0 | 10 | 331 |
| Total | 0 | 438 | 4 | 0 | 442 | 0 | 0 | 39 | 0 | 39 | 0 | 774 | 23 | 0 | 797 | 0 | 0 | 51 | 0 | 51 | 1329 |
| Grand Total | 0 | 853 | 14 | 0 | 867 | 0 | 0 | 86 | 0 | 86 | 0 | 1514 | 33 | 0 | 1547 | 0 | 0 | 108 | 0 | 108 | 2608 |
| Apprch \% | 0 | 98.4 | 1.6 | 0 |  | 0 | 0 | 100 | 0 |  | 0 | 97.9 | 2.1 | 0 |  | 0 | 0 | 100 | 0 |  |  |
| Total \% | 0 | 32.7 | 0.5 | 0 | 33.2 | 0 | 0 | 3.3 | 0 | 3.3 | 0 | 58.1 | 1.3 | 0 | 59.3 | 0 | 0 | 4.1 | 0 | 4.1 |  |

## LSC Transportation Consultants, Inc.

2504 E. Pikes Peak Ave, Suite 304
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719-633-2868

File Name : Hwy 24-Old Meridian Rd PM
Site Code : 00000000
Start Date : 12/1/2021
Page No : 2

|  | Hwy 24 Southbound |  |  |  |  | Old Meridian Rd Westbound |  |  |  |  | Hwy 24Northbound |  |  |  |  | Old Meridian Rd Eastbound |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | L | T | R | U | App. Total | L | T | R | U | App. Total | L | T | R | U | App. Total | L | T | R | U | App. Total | Int. Total |
| Peak Hour Analysis From 4:00:00 PM to 5:45:00 PM - Peak 1 of 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour for Entire Intersection Begins at 4:30:00 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4:30:00 PM | 0 | 109 | 3 | 0 | 112 | 0 | 0 | 12 | 0 | 12 | 0 | 219 | 1 | 0 | 220 | 0 | 0 | 12 | 0 | 12 | 356 |
| 4:45:00 PM | 0 | 82 | 1 | 0 | 83 | 0 | 0 | 12 | 0 | 12 | 0 | 191 | 1 | 0 | 192 | 0 | 0 | 15 | 0 | 15 | 302 |
| 5:00:00 PM | 0 | 119 | 1 | 0 | 120 | 0 | 0 | 8 | 0 | 8 | 0 | 192 | 6 | 0 | 198 | 0 | 0 | 17 | 0 | 17 | 343 |
| 5:15:00 PM | 0 | 130 | 0 | 0 | 130 | 0 | 0 | 13 | 0 | 13 | 0 | 195 | 6 | 0 | 201 | 0 | 0 | 8 | 0 | 8 | 352 |
| Total Volume | 0 | 440 | 5 | 0 | 445 | 0 | 0 | 45 | 0 | 45 | 0 | 797 | 14 | 0 | 811 | 0 | 0 | 52 | 0 | 52 | 1353 |
| \% App. Total | 0 | 98.9 | 1.1 | 0 |  | 0 | 0 | 100 | 0 |  | 0 | 98.3 | 1.7 | 0 |  | 0 | 0 | 100 | 0 |  |  |
| PHF | . 000 | . 846 | . 417 | . 000 | . 856 | . 000 | . 000 | . 865 | . 000 | . 865 | . 000 | . 910 | . 583 | . 000 | . 922 | . 000 | . 000 | . 765 | . 000 | . 765 | . 950 |

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: 3


|  | 4 |  |  | 7 |  |  | 4 | $\uparrow$ |  |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \％ | 个4 | F | \％${ }^{*}$ | 个4 | F | ${ }^{7}$ | 个4 | F | \％${ }^{\text {\％}}$ | 个个 | F |
| Traffic Volume（vph） | 302 | 349 | 201 | 68 | 577 | 36 | 142 | 212 | 17 | 38 | 606 | 541 |
| Future Volume（vph） | 302 | 349 | 201 | 68 | 577 | 36 | 142 | 212 | 17 | 38 | 606 | 541 |
| Turn Type | Prot | NA | Free | Prot | NA | Perm | Prot | NA | Free | Prot | NA | Free |
| Protected Phases | 7 | 4 |  | 3 | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Permitted Phases |  |  | Free |  |  | 8 |  |  | Free |  |  | Free |
| Detector Phase | 7 | 4 |  | 3 | 8 | 8 | 5 | 2 |  | 1 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 5.0 | 15.0 |  | 5.0 | 15.0 | 15.0 | 5.0 | 15.0 |  | 5.0 | 15.0 |  |
| Minimum Split（s） | 13.5 | 25.0 |  | 13.5 | 22.0 | 22.0 | 13.5 | 22.0 |  | 13.5 | 22.0 |  |
| Total Split（s） | 25.0 | 40.0 |  | 15.0 | 30.0 | 30.0 | 15.0 | 45.0 |  | 15.0 | 45.0 |  |
| Total Split（\％） | 21．7\％ | 34．8\％ |  | 13．0\％ | 26．1\％ | 26．1\％ | 13．0\％ | 39．1\％ |  | 13．0\％ | 39．1\％ |  |
| Yellow Time（s） | 4.0 | 5.0 |  | 4.0 | 5.0 | 5.0 | 5.0 | 5.0 |  | 5.0 | 5.0 |  |
| All－Red Time（s） | 3.5 | 2.0 |  | 3.5 | 2.0 | 2.0 | 3.5 | 2.0 |  | 3.5 | 2.0 |  |
| Lost Time Adjust（s） | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time（s） | 7.5 | 7.0 |  | 7.5 | 7.0 | 7.0 | 8.5 | 7.0 |  | 8.5 | 7.0 |  |
| Lead／Lag | Lead | Lag |  | Lead | Lag | Lag | Lead | Lag |  | Lead | Lag |  |
| Lead－Lag Optimize？ | Yes | Yes |  | Yes | Yes | Yes | Yes | Yes |  | Yes | Yes |  |
| Recall Mode | None | None |  | None | None | None | None | C－Max |  | None | C－Max |  |
| Act Effct Green（s） | 15.3 | 33.5 | 115.0 | 7.1 | 22.6 | 22.6 | 7.3 | 46.6 | 115.0 | 6.2 | 39.8 | 115.0 |
| Actuated g／C Ratio | 0.13 | 0.29 | 1.00 | 0.06 | 0.20 | 0.20 | 0.06 | 0.41 | 1.00 | 0.05 | 0.35 | 1.00 |
| v／c Ratio | 0.69 | 0.35 | 0.13 | 0.34 | 0.86 | 0.07 | 0.68 | 0.15 | 0.01 | 0.22 | 0.52 | 0.36 |
| Control Delay | 55.8 | 33.7 | 0.2 | 76.7 | 50.3 | 0.6 | 66.8 | 22.4 | 0.0 | 54.8 | 32.3 | 0.6 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 55.8 | 33.7 | 0.2 | 76.7 | 50.3 | 0.6 | 66.8 | 22.4 | 0.0 | 54.8 | 32.3 | 0.6 |
| LOS | E | C | A | E | D | A | E | C | A | D | C | A |
| Approach Delay |  | 33.7 |  |  | 50.2 |  |  | 38.3 |  |  | 18.6 |  |
| Approach LOS |  | C |  |  | D |  |  | D |  |  | B |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

Cycle Length： 115
Actuated Cycle Length： 115
Offset： $0(0 \%)$ ，Referenced to phase 2：NBT and 6：SBT，Start of FDW or yellow，Master Intersection
Natural Cycle： 75
Control Type：Actuated－Coordinated
Maximum v／c Ratio： 0.86
Intersection Signal Delay： 32.1
Intersection LOS：C
Intersection Capacity Utilization 70．5\％
ICU Level of Service C
Analysis Period（min） 15
Splits and Phases：7：Meridian Rd \＆Woodmen Rd


|  | $\rangle$ |  |  |  |  |  | 4 | 4 |  |  | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \％ | 性 | F | \％ | 性 | F | \％ | 4 | 「 | ${ }^{7}$ | $\uparrow$ | F |
| Traffic Volume（vph） | 101 | 257 | 46 | 28 | 349 | 143 | 39 | 45 | 10 | 121 | 125 | 293 |
| Future Volume（vph） | 101 | 257 | 46 | 28 | 349 | 143 | 39 | 45 | 10 | 121 | 125 | 293 |
| Turn Type | pm＋pt | NA | Perm | pm＋pt | NA | Perm | pm＋pt | NA | Perm | pm＋pt | NA | Perm |
| Protected Phases | 5 | 2 |  | 1 | 6 |  | 3 | 8 |  | 7 | 4 |  |
| Permitted Phases | 2 |  | 2 | 6 |  | 6 | 8 |  | 8 | 4 |  | 4 |
| Detector Phase | 5 | 2 | 2 | 1 | 6 | 6 | 3 | 8 | 8 | 7 | 4 | 4 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Minimum Split（s） | 12.5 | 25.0 | 25.0 | 12.5 | 25.0 | 25.0 | 13.5 | 25.0 | 25.0 | 13.5 | 25.0 | 25.0 |
| Total Split（s） | 15.0 | 60.0 | 60.0 | 15.0 | 60.0 | 60.0 | 15.0 | 25.0 | 25.0 | 15.0 | 25.0 | 25.0 |
| Total Split（\％） | 13．0\％ | 52．2\％ | 52．2\％ | 13．0\％ | 52．2\％ | 52．2\％ | 13．0\％ | 21．7\％ | 21．7\％ | 13．0\％ | 21．7\％ | 21．7\％ |
| Yellow Time（s） | 4.0 | 5.0 | 5.0 | 4.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| All－Red Time（s） | 3.5 | 2.0 | 2.0 | 3.5 | 2.0 | 2.0 | 3.5 | 2.0 | 2.0 | 3.5 | 2.0 | 2.0 |
| Lost Time Adjust（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） | 7.5 | 7.0 | 7.0 | 7.5 | 7.0 | 7.0 | 8.5 | 7.0 | 7.0 | 8.5 | 7.0 | 7.0 |
| Lead／Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | Lag |
| Lead－Lag Optimize？ | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Recall Mode | None | C－Max | C－Max | None | C－Max | C－Max | None | Max | Max | None | Max | Max |
| Act Effct Green（s） | 63.5 | 59.5 | 59.5 | 59.0 | 53.2 | 53.2 | 22.8 | 18.0 | 18.0 | 26.4 | 24.0 | 24.0 |
| Actuated g／C Ratio | 0.55 | 0.52 | 0.52 | 0.51 | 0.46 | 0.46 | 0.20 | 0.16 | 0.16 | 0.23 | 0.21 | 0.21 |
| V／c Ratio | 0.18 | 0.14 | 0.05 | 0.05 | 0.22 | 0.18 | 0.14 | 0.16 | 0.02 | 0.40 | 0.33 | 0.53 |
| Control Delay | 8.7 | 9.9 | 0.2 | 14.6 | 25.2 | 5.1 | 32.8 | 43.6 | 0.1 | 38.6 | 44.1 | 8.7 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 8.7 | 9.9 | 0.2 | 14.6 | 25.2 | 5.1 | 32.8 | 43.6 | 0.1 | 38.6 | 44.1 | 8.7 |
| LOS | A | A | A | B | C | A | C | D | A | D | D | A |
| Approach Delay |  | 8.5 |  |  | 19.1 |  |  | 34.6 |  |  | 23.6 |  |
| Approach LOS |  | A |  |  | B |  |  | C |  |  | C |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length： 115 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length： 115 |  |  |  |  |  |  |  |  |  |  |  |  |
| Offset： $0(0 \%)$ ，Referenced to phase 2：EBTL and 6：WBTL，Start of Green |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle： 80 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type：Actuated－Coordinated |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v／c Ratio： 0.53 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay： 18.9 |  |  |  | Intersection LOS：B |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 49．9\％ |  |  |  | ICU Level of Service A |  |  |  |  |  |  |  |  |
| Analysis Period（min） 15 |  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases：8：McLaughlin Rd \＆Woodmen Rd






| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 2 |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | MF |  | 个 |  |  | $\uparrow$ |
| Traffic Vol, veh/h | 47 | 11 | 414 | 76 | 6 | 885 |
| Future Vol, veh/h | 47 | 11 | 414 | 76 | 6 | 885 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 88 | 88 | 88 | 88 | 88 | 88 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 53 | 13 | 470 | 86 | 7 | 1006 |


| Major/Minor | Minor1 | Major1 |  | Major2 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 1533 | 513 | 0 | 0 | 556 | 0 |
| Stage 1 | 513 |  |  | - | - |  |
| Stage 2 | 1020 |  | - | - | - |  |
| Critical Hdwy | 6.42 | 6.22 | - | - | 4.12 |  |
| Critical Hdwy Stg 1 | 5.42 |  | - | - | - |  |
| Critical Hdwy Stg 2 | 5.42 | - |  | - | - |  |
| Follow-up Hdwy | 3.518 | 3.318 | - |  | 2.218 |  |
| Pot Cap-1 Maneuver | 128 | 561 | - | - | 1015 |  |
| Stage 1 | 601 | - | - | - | - |  |
| Stage 2 | 348 |  | - | - | - |  |
| Platoon blocked, \% |  |  | - | - |  |  |
| Mov Cap-1 Maneuver | 126 | 561 | - | - | 1015 |  |
| Mov Cap-2 Maneuver | 126 | - | - | - | - |  |
| Stage 1 | 601 | - | - | - | - |  |
| Stage 2 | 342 | - | - | - | - |  |


| Approach | WB | NB | SB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 47.5 | 0 | 0.1 |
| HCM LOS | E |  |  |


| Minor Lane/Major Mvmt | NBT | NBRWBLn1 | SBL | SBT |
| :--- | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | - | -148 | 1015 | - |
| HCM Lane V/C Ratio | - | -0.445 | 0.007 | - |
| HCM Control Delay (s) | - | -47.5 | 8.6 | 0 |
| HCM Lane LOS | - | - | E | A |
| HCM 95th \%tile Q(veh) | - | - | 2 | 0 |
| H | - |  |  |  |


|  | 4 |  |  | $\dagger$ |  |  | 4 | $\uparrow$ |  |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \％${ }^{*}$ | 个个 | 「 | ${ }^{7} 1$ | 个个 | 「 | ${ }^{1+1}$ | 个4 | 「 | ${ }^{1 *}$ | 个个 | 「 |
| Traffic Volume（vph） | 638 | 523 | 102 | 116 | 488 | 64 | 220 | 568 | 79 | 119 | 435 | 366 |
| Future Volume（vph） | 638 | 523 | 102 | 116 | 488 | 64 | 220 | 568 | 79 | 119 | 435 | 366 |
| Turn Type | Prot | NA | Free | Prot | NA | Perm | Prot | NA | Free | Prot | NA | Free |
| Protected Phases | 7 | 4 |  | 3 | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Permitted Phases |  |  | Free |  |  | 8 |  |  | Free |  |  | Free |
| Detector Phase | 7 | 4 |  | 3 | 8 | 8 | 5 | 2 |  | 1 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 5.0 | 15.0 |  | 5.0 | 15.0 | 15.0 | 5.0 | 15.0 |  | 5.0 | 15.0 |  |
| Minimum Split（s） | 12.5 | 22.0 |  | 12.5 | 22.0 | 22.0 | 13.5 | 22.0 |  | 13.5 | 22.0 |  |
| Total Split（s） | 25.0 | 33.0 |  | 15.0 | 23.0 | 23.0 | 18.0 | 27.0 |  | 15.0 | 24.0 |  |
| Total Split（\％） | 27．8\％ | 36．7\％ |  | 16．7\％ | 25．6\％ | 25．6\％ | 20．0\％ | 30．0\％ |  | 16．7\％ | 26．7\％ |  |
| Yellow Time（s） | 4.0 | 5.0 |  | 4.0 | 5.0 | 5.0 | 5.0 | 5.0 |  | 5.0 | 5.0 |  |
| All－Red Time（s） | 3.5 | 2.0 |  | 3.5 | 2.0 | 2.0 | 3.5 | 2.0 |  | 3.5 | 2.0 |  |
| Lost Time Adjust（s） | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time（s） | 7.5 | 7.0 |  | 7.5 | 7.0 | 7.0 | 8.5 | 7.0 |  | 8.5 | 7.0 |  |
| Lead／Lag | Lead | Lag |  | Lead | Lag | Lag | Lead | Lag |  | Lead | Lag |  |
| Lead－Lag Optimize？ | Yes | Yes |  | Yes | Yes | Yes | Yes | Yes |  | Yes | Yes |  |
| Recall Mode | None | None |  | None | None | None | None | C－Max |  | None | C－Max |  |
| Act Effct Green（s） | 17.5 | 26.0 | 90.0 | 7.3 | 15.8 | 15.8 | 9.2 | 20.2 | 90.0 | 6.5 | 17.5 | 90.0 |
| Actuated g／C Ratio | 0.19 | 0.29 | 1.00 | 0.08 | 0.18 | 0.18 | 0.10 | 0.22 | 1.00 | 0.07 | 0.19 | 1.00 |
| $\mathrm{V} / \mathrm{C}$ Ratio | 1.00 | 0.53 | 0.07 | 0.44 | 0.82 | 0.12 | 0.65 | 0.74 | 0.05 | 0.50 | 0.66 | 0.24 |
| Control Delay | 71.9 | 29.2 | 0.1 | 65.4 | 42.3 | 1.6 | 58.4 | 24.8 | 0.1 | 47.8 | 39.0 | 0.4 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 71.9 | 29.2 | 0.1 | 65.4 | 42.3 | 1.6 | 58.4 | 24.8 | 0.1 | 47.8 | 39.0 | 0.4 |
| LOS | E | C | A | E | D | A | E | C | A | D | D | A |
| Approach Delay |  | 48.4 |  |  | 42.4 |  |  | 31.1 |  |  | 24.8 |  |
| Approach LOS |  | D |  |  | D |  |  | C |  |  | C |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

Cycle Length： 90
Actuated Cycle Length： 90
Offset： $0(0 \%)$ ，Referenced to phase 2：NBT and 6：SBT，Start of FDW or yellow，Master Intersection
Natural Cycle： 80
Control Type：Actuated－Coordinated
Maximum v／c Ratio： 1.00
Intersection Signal Delay： $37.4 \quad$ Intersection LOS：D
Intersection Capacity Utilization 76．1\％
ICU Level of Service D
Analysis Period（min） 15
Splits and Phases：7：Meridian Rd \＆Woodmen Rd


|  | $\stackrel{ }{*}$ |  |  |  |  |  | 4 | $\dagger$ | 7 |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \％ | 个4 | 「 | \％ | 个 $\uparrow$ | F | \％ | $\uparrow$ | 「 | \％ | 4 | F |
| Trafic Volume（vph） | 296 | 328 | 97 | 45 | 388 | 266 | 86 | 165 | 87 | 185 | 113 | 194 |
| Future Volume（vph） | 296 | 328 | 97 | 45 | 388 | 266 | 86 | 165 | 87 | 185 | 113 | 194 |
| Turn Type | pm＋pt | NA | Perm | pm＋pt | NA | Perm | pm＋pt | NA | Perm | pm＋pt | NA | Perm |
| Protected Phases | 5 | 2 |  | 1 | 6 |  | 3 | 8 |  | 7 | 4 |  |
| Permitted Phases | 2 |  | 2 | 6 |  | 6 | 8 |  | 8 | 4 |  | 4 |
| Detector Phase | 5 | 2 | 2 | 1 | 6 | 6 | 3 | 8 | 8 | 7 | 4 | 4 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Minimum Split（s） | 12.5 | 25.0 | 25.0 | 12.5 | 25.0 | 25.0 | 13.5 | 25.0 | 25.0 | 13.5 | 25.0 | 25.0 |
| Total Split（s） | 14.0 | 37.0 | 37.0 | 14.0 | 37.0 | 37.0 | 14.0 | 25.0 | 25.0 | 14.0 | 25.0 | 25.0 |
| Total Split（\％） | 15．6\％ | 41．1\％ | 41．1\％ | 15．6\％ | 41．1\％ | 41．1\％ | 15．6\％ | 27．8\％ | 27．8\％ | 15．6\％ | 27．8\％ | 27．8\％ |
| Yellow Time（s） | 4.0 | 5.0 | 5.0 | 4.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| All－Red Time（s） | 3.5 | 2.0 | 2.0 | 3.5 | 2.0 | 2.0 | 3.5 | 2.0 | 2.0 | 3.5 | 2.0 | 2.0 |
| Lost Time Adjust（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） | 7.5 | 7.0 | 7.0 | 7.5 | 7.0 | 7.0 | 8.5 | 7.0 | 7.0 | 8.5 | 7.0 | 7.0 |
| Lead／Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | Lag |
| Lead－Lag Optimize？ | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Recall Mode | None | C－Max | C－Max | None | C－Max | C－Max | None | Max | Max | None | Max | Max |
| Act Effct Green（s） | 39.0 | 35.6 | 35.6 | 35.7 | 30.0 | 30.0 | 22.0 | 18.0 | 18.0 | 23.7 | 20.8 | 20.8 |
| Actuated g／C Ratio | 0.43 | 0.40 | 0.40 | 0.40 | 0.33 | 0.33 | 0.24 | 0.20 | 0.20 | 0.26 | 0.23 | 0.23 |
| v／c Ratio | 0.71 | 0.24 | 0.13 | 0.10 | 0.34 | 0.39 | 0.26 | 0.46 | 0.18 | 0.57 | 0.27 | 0.36 |
| Control Delay | 47.4 | 38.6 | 8.7 | 16.5 | 30.9 | 14.4 | 23.6 | 36.3 | 0.8 | 32.6 | 32.3 | 4.2 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 47.4 | 38.6 | 8.7 | 16.5 | 30.9 | 14.4 | 23.6 | 36.3 | 0.8 | 32.6 | 32.3 | 4.2 |
| LOS | D | D | A | B | C | B | C | D | A | C | C | A |
| Approach Delay |  | 38.2 |  |  | 23.7 |  |  | 23.9 |  |  | 21.3 |  |
| Approach LOS |  | D |  |  | C |  |  | C |  |  | C |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

Cycle Length： 90
Actuated Cycle Length： 90
Offset： $0(0 \%)$ ，Referenced to phase 2：EBTL and 6：WBTL，Start of Green
Natural Cycle： 80
Control Type：Actuated－Coordinated
Maximum v／c Ratio： 0.71

Intersection Signal Delay： 27.8
Intersection Capacity Utilization 69．4\％
Analysis Period（min） 15

Intersection LOS：C
ICU Level of Service C

Splits and Phases：8：McLaughlin Rd \＆Woodmen Rd


|  | 4 |  | 4 |  |  | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | F | \% | 4 | 4 | 「 |
| Traffic Volume (vph) | 498 | 102 | 323 | 531 | 316 | 376 |
| Future Volume (vph) | 498 | 102 | 323 | 531 | 316 | 376 |
| Turn Type | Prot | Perm | pm+pt | NA | NA | Perm |
| Protected Phases | 2 |  | 3 | 8 | 4 |  |
| Permitted Phases |  | 2 | 8 |  |  | 4 |
| Detector Phase | 2 | 2 | 3 | 8 | 4 | 4 |
| Switch Phase |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Minimum Split (s) | 23.5 | 23.5 | 10.5 | 23.5 | 23.5 | 23.5 |
| Total Split (s) | 30.0 | 30.0 | 20.0 | 60.0 | 40.0 | 40.0 |
| Total Split (\%) | 33.3\% | 33.3\% | 22.2\% | 66.7\% | 44.4\% | 44.4\% |
| Yellow Time (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| All-Red Time (s) | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Lead/Lag |  |  | Lead |  | Lag | Lag |
| Lead-Lag Optimize? |  |  | Yes |  | Yes | Yes |
| Recall Mode | C-Max | C-Max | None | None | None | None |
| Act Effct Green (s) | 37.9 | 37.9 | 42.1 | 42.1 | 25.5 | 25.5 |
| Actuated g/C Ratio | 0.42 | 0.42 | 0.47 | 0.47 | 0.28 | 0.28 |
| v/c Ratio | 0.70 | 0.15 | 0.51 | 0.72 | 0.70 | 0.57 |
| Control Delay | 33.1 | 7.2 | 26.8 | 37.5 | 35.2 | 5.4 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 33.1 | 7.2 | 26.8 | 37.5 | 35.2 | 5.4 |
| LOS | C | A | C | D | D | A |
| Approach Delay | 28.7 |  |  | 33.4 | 19.0 |  |
| Approach LOS | C |  |  | C | B |  |
| Intersection Summary |  |  |  |  |  |  |
| Cycle Length: 90 |  |  |  |  |  |  |
| Actuated Cycle Leng |  |  |  |  |  |  |
| Offset: 0 (0\%), Refer | phase 2: | EBL and | 6., Start | f Green |  |  |
| Natural Cycle: 60 |  |  |  |  |  |  |
| Control Type: Actuated | dinated |  |  |  |  |  |
| Maximum v/c Ratio: 0. |  |  |  |  |  |  |
| Intersection Signal D |  |  |  |  | ersectio | LOS: C |
| Intersection Capacity | n 65.9\% |  |  |  | U Level | f Service C |
| Analysis Period (min) |  |  |  |  |  |  |
| Splits and Phases: 9: US 24 \& Woodmen Rd |  |  |  |  |  |  |
| $\square 2(\mathrm{R})$ |  |  | $\psi_{\varnothing 3}$ |  |  | - 04 |
| 30 s |  |  | 20 s |  |  | 40 s |
|  |  |  | $\psi_{08}$ |  |  |  |
|  |  |  | 60 s |  |  |  |



Splits and Phases: 10: US 24 \& Meridian Rd




| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 388.2 |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | Mr |  | $\uparrow$ |  |  | $\uparrow$ |
| Traffic Vol, veh/h | 66 | 4 | 930 | 99 | 2 | 626 |
| Future Vol, veh/h | 66 | 4 | 930 | 99 | 2 | 626 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 87 | 87 | 87 | 87 | 87 | 87 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 76 | 5 | 1069 | 114 | 2 | 720 |


| Major/Minor | Major1 | Minor2 |  |  |
| :--- | ---: | ---: | ---: | ---: |
| Conflicting Flow All | 0 | 0 | 1126 | 1183 |
| $\quad$ Stage 1 | - | - | 0 | 0 |
| $\quad$ Stage 2 | - | - | 1126 | 1183 |
| Critical Hdwy | - | - | 6.42 | 6.52 |
| Critical Hdwy Stg 1 | - | - | - | - |
| Critical Hdwy Stg 2 | - | - | 5.42 | 5.52 |
| Follow-up Hdwy | - | - | 3.518 | 4.018 |
| Pot Cap-1 Maneuver | - | - | 227 | $\sim 189$ |
| $\quad$ Stage 1 | - | - | - | - |
| $\quad$ Stage 2 | - | - | 310 | $\sim 263$ |
| Platoon blocked, \% | - | - |  |  |
| Mov Cap-1 Maneuver | - | - | 227 | 0 |
| Mov Cap-2 Maneuver | - | - | 227 | 0 |
| Stage 1 | - | - | - | 0 |
| Stage 2 | - | - | 310 | 0 |


| Approach | NB | SB |
| :--- | ---: | ---: |
| HCM Control Delay, s | 0 | $\$ 1024.4$ |
| HCM LOS |  | F |


| Minor Lane/Major Mvmt | NBT | NBR SBLn1 |
| :--- | :---: | ---: |
| Capacity (veh/h) | - | -227 |
| HCM Lane V/C Ratio | - | -3.18 |
| HCM Control Delay (s) | - | $\$ 1024.4$ |
| HCM Lane LOS | - | - |
| HCM 95th \%tile Q(veh) | - | - |

## Notes

$\sim$ : Volume exceeds capacity $\quad \$$ : Delay exceeds 300s $\quad+$ : Computation Not Defined $\quad$ : All major volume in platoon

|  | 4 |  |  | 7 |  |  | 4 | 4 |  |  | $\frac{1}{\downarrow}$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \％${ }^{1+1}$ | ¢4 | 「 | \％${ }^{1+1}$ | 坐 | 「 | \％${ }^{1+1}$ | 个4 | 「 | \％${ }^{1+1}$ | 个个 | F |
| Traffic Volume（vph） | 302 | 367 | 233 | 68 | 600 | 36 | 165 | 212 | 17 | 38 | 606 | 541 |
| Future Volume（vph） | 302 | 367 | 233 | 68 | 600 | 36 | 165 | 212 | 17 | 38 | 606 | 541 |
| Turn Type | Prot | NA | Free | Prot | NA | Perm | Prot | NA | Free | Prot | NA | Free |
| Protected Phases | 7 | 4 |  | 3 | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Permitted Phases |  |  | Free |  |  | 8 |  |  | Free |  |  | Free |
| Detector Phase | 7 | 4 |  | 3 | 8 | 8 | 5 | 2 |  | 1 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 5.0 | 15.0 |  | 5.0 | 15.0 | 15.0 | 5.0 | 15.0 |  | 5.0 | 15.0 |  |
| Minimum Split（s） | 12.5 | 22.0 |  | 12.5 | 22.0 | 22.0 | 13.5 | 22.0 |  | 13.5 | 22.0 |  |
| Total Split（s） | 25.0 | 33.0 |  | 15.0 | 23.0 | 23.0 | 18.0 | 27.0 |  | 15.0 | 24.0 |  |
| Total Split（\％） | 27．8\％ | 36．7\％ |  | 16．7\％ | 25．6\％ | 25．6\％ | 20．0\％ | 30．0\％ |  | 16．7\％ | 26．7\％ |  |
| Yellow Time（s） | 4.0 | 5.0 |  | 4.0 | 5.0 | 5.0 | 5.0 | 5.0 |  | 5.0 | 5.0 |  |
| All－Red Time（s） | 3.5 | 2.0 |  | 3.5 | 2.0 | 2.0 | 3.5 | 2.0 |  | 3.5 | 2.0 |  |
| Lost Time Adjust（s） | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time（s） | 7.5 | 7.0 |  | 7.5 | 7.0 | 7.0 | 8.5 | 7.0 |  | 8.5 | 7.0 |  |
| Lead／Lag | Lead | Lag |  | Lead | Lag | Lag | Lead | Lag |  | Lead | Lag |  |
| Lead－Lag Optimize？ | Yes | Yes |  | Yes | Yes | Yes | Yes | Yes |  | Yes | Yes |  |
| Recall Mode | None | None |  | None | None | None | None | C－Max |  | None | C－Max |  |
| Act Effct Green（s） | 13.5 | 28.6 | 90.0 | 6.9 | 19.4 | 19.4 | 8.9 | 26.6 | 90.0 | 6.2 | 18.3 | 90.0 |
| Actuated g／C Ratio | 0.15 | 0.32 | 1.00 | 0.08 | 0.22 | 0.22 | 0.10 | 0.30 | 1.00 | 0.07 | 0.20 | 1.00 |
| $\mathrm{V} / \mathrm{C}$ Ratio | 0.61 | 0.34 | 0.15 | 0.27 | 0.82 | 0.06 | 0.51 | 0.21 | 0.01 | 0.17 | 0.88 | 0.36 |
| Control Delay | 40.8 | 25.5 | 0.2 | 59.7 | 38.2 | 0.2 | 47.7 | 14.7 | 0.0 | 41.1 | 50.9 | 0.6 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 40.8 | 25.5 | 0.2 | 59.7 | 38.2 | 0.2 | 47.7 | 14.7 | 0.0 | 41.1 | 50.9 | 0.6 |
| LOS | D | C | A | E | D | A | D | B | A | D | D | A |
| Approach Delay |  | 24.1 |  |  | 38.3 |  |  | 27.9 |  |  | 27.6 |  |
| Approach LOS |  | C |  |  | D |  |  | C |  |  | C |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

Cycle Length： 90
Actuated Cycle Length： 90
Offset： $0(0 \%)$ ，Referenced to phase 2：NBT and 6：SBT，Start of FDW or yellow，Master Intersection
Natural Cycle： 75
Control Type：Actuated－Coordinated
Maximum v／c Ratio： 0.88
Intersection Signal Delay： 29.0
Intersection LOS：C
Intersection Capacity Utilization 71．7\％
ICU Level of Service C
Analysis Period（min） 15

Splits and Phases：7：Meridian Rd \＆Woodmen Rd


|  | $\rangle$ |  |  | 7 |  |  | 4 | $\dagger$ | $p$ |  | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \% | 个 4 | 7 | ${ }^{7}$ | 个 $\uparrow$ | F | ${ }^{7}$ | $\uparrow$ | 7 | \% | $\uparrow$ | F |
| Trafic Volume (vph) | 101 | 275 | 46 | 28 | 372 | 143 | 39 | 45 | 10 | 121 | 125 | 293 |
| Future Volume (vph) | 101 | 275 | 46 | 28 | 372 | 143 | 39 | 45 | 10 | 121 | 125 | 293 |
| Turn Type | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | Perm |
| Protected Phases | 5 | 2 |  | 1 | 6 |  | 3 | 8 |  | 7 | 4 |  |
| Permitted Phases | 2 |  | 2 | 6 |  | 6 | 8 |  | 8 | 4 |  | 4 |
| Detector Phase | 5 | 2 | 2 | 1 | 6 | 6 | 3 | 8 | 8 | 7 | 4 | 4 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Minimum Split (s) | 12.5 | 25.0 | 25.0 | 12.5 | 25.0 | 25.0 | 13.5 | 25.0 | 25.0 | 13.5 | 25.0 | 25.0 |
| Total Split (s) | 14.0 | 37.0 | 37.0 | 14.0 | 37.0 | 37.0 | 14.0 | 25.0 | 25.0 | 14.0 | 25.0 | 25.0 |
| Total Split (\%) | 15.6\% | 41.1\% | 41.1\% | 15.6\% | 41.1\% | 41.1\% | 15.6\% | 27.8\% | 27.8\% | 15.6\% | 27.8\% | 27.8\% |
| Yellow Time (s) | 4.0 | 5.0 | 5.0 | 4.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| All-Red Time (s) | 3.5 | 2.0 | 2.0 | 3.5 | 2.0 | 2.0 | 3.5 | 2.0 | 2.0 | 3.5 | 2.0 | 2.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 7.5 | 7.0 | 7.0 | 7.5 | 7.0 | 7.0 | 8.5 | 7.0 | 7.0 | 8.5 | 7.0 | 7.0 |
| Lead/Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | Lag |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Recall Mode | None | C-Max | C-Max | None | C-Max | C-Max | None | Max | Max | None | Max | Max |
| Act Effct Green (s) | 40.5 | 38.4 | 38.4 | 37.3 | 32.8 | 32.8 | 22.0 | 18.0 | 18.0 | 25.4 | 23.6 | 23.6 |
| Actuated g/C Ratio | 0.45 | 0.43 | 0.43 | 0.41 | 0.36 | 0.36 | 0.24 | 0.20 | 0.20 | 0.28 | 0.26 | 0.26 |
| v/c Ratio | 0.23 | 0.19 | 0.06 | 0.06 | 0.29 | 0.20 | 0.12 | 0.12 | 0.02 | 0.32 | 0.26 | 0.47 |
| Control Delay | 34.1 | 38.8 | 4.8 | 12.9 | 22.2 | 0.7 | 21.6 | 30.7 | 0.1 | 25.1 | 30.7 | 6.7 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 34.1 | 38.8 | 4.8 | 12.9 | 22.2 | 0.7 | 21.6 | 30.7 | 0.1 | 25.1 | 30.7 | 6.7 |
| LOS | C | D | A | B | C | A | C | C | A | C | C | A |
| Approach Delay |  | 34.0 |  |  | 16.0 |  |  | 23.7 |  |  | 16.4 |  |
| Approach LOS |  | C |  |  | B |  |  | C |  |  | B |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

Cycle Length: 90
Actuated Cycle Length: 90
Offset: $0(0 \%)$, Referenced to phase 2:EBTL and 6:WBTL, Start of Green
Natural Cycle: 80
Control Type: Actuated-Coordinated
Maximum v/c Ratio: 0.47
Intersection Signal Delay: 21.4 Intersection LOS: C
Intersection Capacity Utilization 50.5\%
ICU Level of Service A
Analysis Period (min) 15
Splits and Phases: 8: McLaughlin Rd \& Woodmen Rd



|  | $\rangle$ |  |  | 7 |  | 4 | 4 | $\dagger$ | $p$ |  | $\dagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \％ | 个个 | 「 | ${ }^{4}$ | 个个 | 「 | ${ }^{7} 1$ | $\uparrow$ | 「 | ＊ | $\uparrow$ | F |
| Traffic Volume（vph） | 7 | 392 | 728 | 32 | 192 | 24 | 206 | 326 | 18 | 69 | 659 | 2 |
| Future Volume（vph） | 7 | 392 | 728 | 32 | 192 | 24 | 206 | 326 | 18 | 69 | 659 | 2 |
| Turn Type | pm＋pt | NA | Free | pm＋pt | NA | Free | Prot | NA | Perm | pm＋pt | NA | Perm |
| Protected Phases | 5 | 2 |  | 1 | ， |  | 3 | 8 |  | 7 | 4 |  |
| Permitted Phases | 2 |  | Free | 6 |  | Free |  |  | 8 | 4 |  | 4 |
| Detector Phase | 5 | 2 |  | 1 | 6 |  | 3 | 8 | 8 | 7 | 4 | 4 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 5.0 | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Minimum Split（s） | 11.0 | 20.0 |  | 11.0 | 20.0 |  | 11.0 | 20.0 | 20.0 | 11.0 | 20.0 | 20.0 |
| Total Split（s） | 11.0 | 20.0 |  | 11.0 | 20.0 |  | 15.0 | 47.0 | 47.0 | 12.0 | 44.0 | 44.0 |
| Total Split（\％） | 12．2\％ | 22．2\％ |  | 12．2\％ | 22．2\％ |  | 16．7\％ | 52．2\％ | 52．2\％ | 13．3\％ | 48．9\％ | 48．9\％ |
| Yellow Time（s） | 3.0 | 5.0 |  | 3.0 | 5.0 |  | 3.0 | 4.5 | 4.5 | 3.0 | 4.5 | 4.5 |
| All－Red Time（s） | 3.0 | 2.0 |  | 3.0 | 2.0 |  | 3.0 | 2.0 | 2.0 | 3.0 | 2.0 | 2.0 |
| Lost Time Adjust（s） | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） | 6.0 | 7.0 |  | 6.0 | 7.0 |  | 6.0 | 6.5 | 6.5 | 6.0 | 6.5 | 6.5 |
| Lead／Lag | Lead | Lag |  | Lead | Lag |  | Lead | Lag | Lag | Lead | Lag | Lag |
| Lead－Lag Optimize？ | Yes | Yes |  | Yes | Yes |  | Yes | Yes | Yes | Yes | Yes | Yes |
| Recall Mode | None | C－Max |  | None | C－Max |  | None | None | None | None | None | None |
| Act Effct Green（s） | 23.8 | 19.8 | 90.0 | 26.2 | 24.2 | 90.0 | 8.8 | 40.5 | 40.5 | 41.8 | 35.4 | 35.4 |
| Actuated g／C Ratio | 0.26 | 0.22 | 1.00 | 0.29 | 0.27 | 1.00 | 0.10 | 0.45 | 0.45 | 0.46 | 0.39 | 0.39 |
| $\mathrm{V} / \mathrm{C}$ Ratio | 0.02 | 0.51 | 0.47 | 0.12 | 0.21 | 0.02 | 0.63 | 0.40 | 0.02 | 0.13 | 0.92 | 0.00 |
| Control Delay | 26.4 | 35.6 | 2.0 | 25.1 | 28.5 | 0.0 | 48.0 | 18.5 | 0.1 | 9.2 | 45.0 | 0.0 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 26.4 | 35.6 | 2.0 | 25.1 | 28.5 | 0.0 | 48.0 | 18.5 | 0.1 | 9.2 | 45.0 | 0.0 |
| LOS | C | D | A | C | C | A | D | B | A | A | D | A |
| Approach Delay |  | 13.8 |  |  | 25.4 |  |  | 28.9 |  |  | 41.5 |  |
| Approach LOS |  | B |  |  | C |  |  | C |  |  | D |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

Cycle Length： 90
Actuated Cycle Length： 90
Offset： $71(79 \%)$ ，Referenced to phase 2：EBTL and 6 ：WBTL，Start of FDW or yellow
Natural Cycle： 80
Control Type：Actuated－Coordinated
Maximum v／c Ratio： 0.92
Intersection Signal Delay： 25.6
Intersection LOS：C
Intersection Capacity Utilization 76．8\％
ICU Level of Service D
Analysis Period（min） 15
Splits and Phases：10：US 24 \＆Meridian Rd


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay，s／veh | 0 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |  |
| Lane Configurations |  |  | 「＂ |  |  | 「＇ |  | 4 | 「＇ |  | 4 | 7 |  |
| Traffic Vol，veh／h | 0 | 0 | 25 | 0 | 0 | 51 | 0 | 328 | 29 | 0 | 705 | 4 |  |
| Future Vol，veh／h | 0 | 0 | 25 | 0 | 0 | 51 | 0 | 328 | 29 | 0 | 705 | 4 |  |
| Conflicting Peds，\＃／hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Sign Control Star | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |  |
| RT Channelized | － | － | Free | － | － | Free | － | － | None | － | － | None |  |
| Storage Length | － | － | 0 | － | － | 0 | － | － | 400 | － | － | 400 |  |
| Veh in Median Storage，\＃ | \＃ | 0 | － | － | 0 | － | － | 0 | － | － | 0 | － |  |
| Grade，\％ | － | 0 | － | － | 0 | － | － | 0 | － | － | 0 | － |  |
| Peak Hour Factor | 91 | 91 | 91 | 91 | 91 | 91 | 91 | 91 | 91 | 91 | 91 | 91 |  |
| Heavy Vehicles，\％ | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |  |
| Mvmt Flow | 0 | 0 | 27 | 0 | 0 | 56 | 0 | 360 | 32 | 0 | 775 | 4 |  |



|  | $\stackrel{ }{*}$ |  |  | 7 |  |  | 4 | 4 |  | $\checkmark$ | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \％${ }^{1 / 1}$ | 个4 | F | \％＊ | 个4 | F | \％＊ | ¢4 | 「 | \％＊ | 个4 | 「 |
| Trafic Volume（vph） | 638 | 541 | 134 | 116 | 511 | 64 | 243 | 568 | 79 | 119 | 435 | 366 |
| Future Volume（vph） | 638 | 541 | 134 | 116 | 511 | 64 | 243 | 568 | 79 | 119 | 435 | 366 |
| Turn Type | Prot | NA | Free | Prot | NA | Perm | Prot | NA | Free | Prot | NA | Free |
| Protected Phases | 7 | 4 |  | 3 | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Permitted Phases |  |  | Free |  |  | 8 |  |  | Free |  |  | Free |
| Detector Phase | 7 | 4 |  | 3 | 8 | 8 | 5 | 2 |  | 1 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 5.0 | 15.0 |  | 5.0 | 15.0 | 15.0 | 5.0 | 15.0 |  | 5.0 | 15.0 |  |
| Minimum Split（s） | 12.5 | 22.0 |  | 12.5 | 22.0 | 22.0 | 13.5 | 22.0 |  | 13.5 | 22.0 |  |
| Total Split（s） | 25.0 | 33.0 |  | 15.0 | 23.0 | 23.0 | 18.0 | 27.0 |  | 15.0 | 24.0 |  |
| Total Split（\％） | 27．8\％ | 36．7\％ |  | 16．7\％ | 25．6\％ | 25．6\％ | 20．0\％ | 30．0\％ |  | 16．7\％ | 26．7\％ |  |
| Yellow Time（s） | 4.0 | 5.0 |  | 4.0 | 5.0 | 5.0 | 5.0 | 5.0 |  | 5.0 | 5.0 |  |
| All－Red Time（s） | 3.5 | 2.0 |  | 3.5 | 2.0 | 2.0 | 3.5 | 2.0 |  | 3.5 | 2.0 |  |
| Lost Time Adjust（s） | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time（s） | 7.5 | 7.0 |  | 7.5 | 7.0 | 7.0 | 8.5 | 7.0 |  | 8.5 | 7.0 |  |
| Lead／Lag | Lead | Lag |  | Lead | Lag | Lag | Lead | Lag |  | Lead | Lag |  |
| Lead－Lag Optimize？ | Yes | Yes |  | Yes | Yes | Yes | Yes | Yes |  | Yes | Yes |  |
| Recall Mode | None | None |  | None | None | None | None | C－Max |  | None | C－Max |  |
| Act Effct Green（s） | 17.5 | 26.0 | 90.0 | 7.3 | 15.8 | 15.8 | 9.3 | 20.2 | 90.0 | 6.5 | 17.4 | 90.0 |
| Actuated g／C Ratio | 0.19 | 0.29 | 1.00 | 0.08 | 0.18 | 0.18 | 0.10 | 0.22 | 1.00 | 0.07 | 0.19 | 1.00 |
| v／c Ratio | 1.00 | 0.55 | 0.09 | 0.44 | 0.86 | 0.12 | 0.71 | 0.74 | 0.05 | 0.50 | 0.66 | 0.24 |
| Control Delay | 71.9 | 29.5 | 0.1 | 65.0 | 44.1 | 1.3 | 62.9 | 21.3 | 0.1 | 47.8 | 39.2 | 0.4 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 71.9 | 29.5 | 0.1 | 65.0 | 44.1 | 1.3 | 62.9 | 21.3 | 0.1 | 47.8 | 39.2 | 0.4 |
| LOS | E | C | A | E | D | A | E | C | A | D | D | A |
| Approach Delay |  | 47.1 |  |  | 43.6 |  |  | 30.8 |  |  | 24.9 |  |
| Approach LOS |  | D |  |  | D |  |  | C |  |  | C |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

Cycle Length： 90
Actuated Cycle Length： 90
Offset： $0(0 \%)$ ，Referenced to phase 2：NBT and 6：SBT，Start of FDW or yellow，Master Intersection
Natural Cycle： 90
Control Type：Actuated－Coordinated
Maximum v／c Ratio： 1.00
Intersection Signal Delay：37．3 Intersection LOS：D
Intersection Capacity Utilization 76．8\％
ICU Level of Service D
Analysis Period（min） 15
Splits and Phases：7：Meridian Rd \＆Woodmen Rd


|  | $\stackrel{ }{*}$ |  |  |  |  |  | 4 | $\dagger$ | 7 |  | $\frac{1}{7}$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \％ | 个4 | 「 | \％ | 个4 | F | \％ | $\uparrow$ | 「 | \％ | 4 | F |
| Trafic Volume（vph） | 296 | 346 | 97 | 45 | 411 | 266 | 86 | 165 | 87 | 185 | 113 | 194 |
| Future Volume（vph） | 296 | 346 | 97 | 45 | 411 | 266 | 86 | 165 | 87 | 185 | 113 | 194 |
| Turn Type | pm＋pt | NA | Perm | pm＋pt | NA | Perm | pm＋pt | NA | Perm | pm＋pt | NA | Perm |
| Protected Phases | 5 | 2 |  | 1 | 6 |  | 3 | 8 |  | 7 | 4 |  |
| Permitted Phases | 2 |  | 2 | 6 |  | 6 | 8 |  | 8 | 4 |  | 4 |
| Detector Phase | 5 | 2 | 2 | 1 | 6 | 6 | 3 | 8 | 8 | 7 | 4 | 4 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Minimum Split（s） | 12.5 | 25.0 | 25.0 | 12.5 | 25.0 | 25.0 | 13.5 | 25.0 | 25.0 | 13.5 | 25.0 | 25.0 |
| Total Split（s） | 14.0 | 37.0 | 37.0 | 14.0 | 37.0 | 37.0 | 14.0 | 25.0 | 25.0 | 14.0 | 25.0 | 25.0 |
| Total Split（\％） | 15．6\％ | 41．1\％ | 41．1\％ | 15．6\％ | 41．1\％ | 41．1\％ | 15．6\％ | 27．8\％ | 27．8\％ | 15．6\％ | 27．8\％ | 27．8\％ |
| Yellow Time（s） | 4.0 | 5.0 | 5.0 | 4.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| All－Red Time（s） | 3.5 | 2.0 | 2.0 | 3.5 | 2.0 | 2.0 | 3.5 | 2.0 | 2.0 | 3.5 | 2.0 | 2.0 |
| Lost Time Adjust（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） | 7.5 | 7.0 | 7.0 | 7.5 | 7.0 | 7.0 | 8.5 | 7.0 | 7.0 | 8.5 | 7.0 | 7.0 |
| Lead／Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | Lag |
| Lead－Lag Optimize？ | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Recall Mode | None | C－Max | C－Max | None | C－Max | C－Max | None | Max | Max | None | Max | Max |
| Act Effct Green（s） | 39.0 | 35.6 | 35.6 | 35.7 | 30.0 | 30.0 | 22.0 | 18.0 | 18.0 | 23.7 | 20.8 | 20.8 |
| Actuated g／C Ratio | 0.43 | 0.40 | 0.40 | 0.40 | 0.33 | 0.33 | 0.24 | 0.20 | 0.20 | 0.26 | 0.23 | 0.23 |
| v／c Ratio | 0.73 | 0.26 | 0.13 | 0.10 | 0.36 | 0.39 | 0.26 | 0.46 | 0.18 | 0.57 | 0.27 | 0.36 |
| Control Delay | 48.7 | 38.8 | 8.7 | 13.3 | 23.8 | 4.6 | 23.6 | 36.3 | 0.8 | 32.6 | 32.3 | 4.2 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 48.7 | 38.8 | 8.7 | 13.3 | 23.8 | 4.6 | 23.6 | 36.3 | 0.8 | 32.6 | 32.3 | 4.2 |
| LOS | D | D | A | B | C | A | C | D | A | C | C | A |
| Approach Delay |  | 38.8 |  |  | 16.1 |  |  | 23.9 |  |  | 21.3 |  |
| Approach LOS |  | D |  |  | B |  |  | C |  |  | C |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

Cycle Length： 90
Actuated Cycle Length： 90
Offset： $0(0 \%)$ ，Referenced to phase 2：EBTL and 6：WBTL，Start of Green
Natural Cycle： 80
Control Type：Actuated－Coordinated
Maximum v／c Ratio： 0.73

Intersection Signal Delay： 25.7
Intersection LOS：C
Intersection Capacity Utilization 70．0\％
ICU Level of Service C
Analysis Period（min） 15

Splits and Phases：8：McLaughlin Rd \＆Woodmen Rd


|  | $\rangle$ |  |  |  |  |  | 4 | $\uparrow$ | + |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \% | $\uparrow$ | F | \% | 性 | 「 | \% ${ }^{1+1}$ | $\uparrow$ | F | \% | $\uparrow$ | 7 |
| Traffic Volume (vph) | 433 | 65 | 120 | 5 | 65 | 4 | 346 | 507 | 5 | 2 | 331 | 311 |
| Future Volume (vph) | 433 | 65 | 120 | 5 | 65 | 4 | 346 | 507 | 5 | 2 | 331 | 311 |
| Turn Type | pm+pt | NA | Free | pm+pt | NA | Free | pm+pt | NA | Free | pm+pt | NA | Free |
| Protected Phases | 7 | 4 |  | 3 | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Permitted Phases | 4 |  | Free | 8 |  | Free | 2 |  | Free | 6 |  | Free |
| Detector Phase | 7 | 4 |  | 3 | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 15.0 |  | 5.0 | 15.0 |  | 5.0 | 15.0 |  | 5.0 | 15.0 |  |
| Minimum Split (s) | 10.0 | 23.0 |  | 10.0 | 23.0 |  | 10.0 | 23.0 |  | 10.0 | 23.0 |  |
| Total Split (s) | 31.0 | 46.0 |  | 10.0 | 25.0 |  | 15.0 | 54.0 |  | 10.0 | 49.0 |  |
| Total Split (\%) | 25.8\% | 38.3\% |  | 8.3\% | 20.8\% |  | 12.5\% | 45.0\% |  | 8.3\% | 40.8\% |  |
| Yellow Time (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| All-Red Time (s) | 2.0 | 2.0 |  | 2.0 | 2.0 |  | 2.0 | 2.0 |  | 2.0 | 2.0 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time (s) | 5.0 | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 5.0 |  |
| Lead/Lag | Lead | Lag |  | Lead | Lag |  | Lead | Lag |  | Lead | Lag |  |
| Lead-Lag Optimize? | Yes | Yes |  | Yes | Yes |  | Yes | Yes |  | Yes | Yes |  |
| Recall Mode | None | None |  | None | None |  | None | C-Max |  | None | C-Max |  |
| Act Effct Green (s) | 42.0 | 40.0 | 120.0 | 17.0 | 15.0 | 120.0 | 68.0 | 65.8 | 120.0 | 56.1 | 50.5 | 120.0 |
| Actuated g/C Ratio | 0.35 | 0.33 | 1.00 | 0.14 | 0.12 | 1.00 | 0.57 | 0.55 | 1.00 | 0.47 | 0.42 | 1.00 |
| v/c Ratio | 0.88 | 0.11 | 0.08 | 0.02 | 0.16 | 0.00 | 0.45 | 0.58 | 0.00 | 0.01 | 0.49 | 0.23 |
| Control Delay | 52.6 | 27.5 | 0.1 | 26.0 | 48.0 | 0.0 | 15.5 | 23.2 | 0.0 | 14.0 | 30.2 | 0.3 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 52.6 | 27.5 | 0.1 | 26.0 | 48.0 | 0.0 | 15.5 | 23.2 | 0.0 | 14.0 | 30.2 | 0.3 |
| LOS | D | C | A | C | D | A | B | C | A | B | C | A |
| Approach Delay |  | 39.7 |  |  | 44.2 |  |  | 19.9 |  |  | 15.7 |  |
| Approach LOS |  | D |  |  | D |  |  | B |  |  | B |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

Cycle Length: 120
Actuated Cycle Length: 120
Offset: $63(53 \%)$, Referenced to phase 2:NBTL and $6:$ SBTL, Start of Green
Natural Cycle: 80
Control Type: Actuated-Coordinated
Maximum v/c Ratio: 0.88

Intersection Signal Delay: 24.6
Intersection Capacity Utilization 74.0\%
Analysis Period (min) 15

Intersection LOS: C
ICU Level of Service D

Splits and Phases: 9: US 24 \& Woodmen Rd


|  | $\star$ |  |  |  |  |  | 4 | $\uparrow$ | $p$ |  | $\frac{1}{7}$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \％ | 性 | F | \％ | 个 4 | 「 | \％${ }^{1 / 1}$ | $\uparrow$ | 「 | \％ | $\uparrow$ | 7 |
| Traffic Volume（vph） | 19 | 259 | 307 | 32 | 374 | 48 | 608 | 743 | 12 | 89 | 407 | 7 |
| Future Volume（vph） | 19 | 259 | 307 | 32 | 374 | 48 | 608 | 743 | 12 | 89 | 407 | 7 |
| Turn Type | pm＋pt | NA | Free | pm＋pt | NA | Free | Prot | NA | Perm | pm＋pt | NA | Perm |
| Protected Phases | 5 | 2 |  | 1 | 6 |  | ， | 8 |  | 7 | 4 |  |
| Permitted Phases | 2 |  | Free | 6 |  | Free |  |  | 8 | 4 |  | 4 |
| Detector Phase | 5 | 2 |  | 1 | 6 |  | 3 | 8 | 8 | 7 | 4 | 4 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 5.0 | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Minimum Split（s） | 11.0 | 20.0 |  | 11.0 | 20.0 |  | 11.0 | 20.0 | 20.0 | 11.0 | 20.0 | 20.0 |
| Total Split（s） | 11.0 | 20.0 |  | 11.0 | 20.0 |  | 25.0 | 47.0 | 47.0 | 12.0 | 34.0 | 34.0 |
| Total Split（\％） | 12．2\％ | 22．2\％ |  | 12．2\％ | 22．2\％ |  | 27．8\％ | 52．2\％ | 52．2\％ | 13．3\％ | 37．8\％ | 37．8\％ |
| Yellow Time（s） | 3.0 | 5.0 |  | 3.0 | 5.0 |  | 3.0 | 4.5 | 4.5 | 3.0 | 4.5 | 4.5 |
| All－Red Time（s） | 3.0 | 2.0 |  | 3.0 | 2.0 |  | 3.0 | 2.0 | 2.0 | 3.0 | 2.0 | 2.0 |
| Lost Time Adjust（s） | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） | 6.0 | 7.0 |  | 6.0 | 7.0 |  | 6.0 | 6.5 | 6.5 | 6.0 | 6.5 | 6.5 |
| Lead／Lag | Lead | Lag |  | Lead | Lag |  | Lead | Lag | Lag | Lead | Lag | Lag |
| Lead－Lag Optimize？ | Yes | Yes |  | Yes | Yes |  | Yes | Yes | Yes | Yes | Yes | Yes |
| Recall Mode | None | C－Max |  | None | C－Max |  | None | None | None | None | None | None |
| Act Effct Green（s） | 23.4 | 19.4 | 90.0 | 24.6 | 21.6 | 90.0 | 18.8 | 40.9 | 40.9 | 32.2 | 25.7 | 25.7 |
| Actuated g／C Ratio | 0.26 | 0.22 | 1.00 | 0.27 | 0.24 | 1.00 | 0.21 | 0.45 | 0.45 | 0.36 | 0.29 | 0.29 |
| v／c Ratio | 0.07 | 0.36 | 0.21 | 0.11 | 0.47 | 0.03 | 0.90 | 0.93 | 0.02 | 0.48 | 0.82 | 0.01 |
| Control Delay | 25.9 | 32.4 | 0.3 | 25.1 | 34.1 | 0.0 | 52.6 | 43.7 | 0.0 | 20.8 | 43.2 | 0.0 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 25.9 | 32.4 | 0.3 | 25.1 | 34.1 | 0.0 | 52.6 | 43.7 | 0.0 | 20.8 | 43.2 | 0.0 |
| LOS | C | C | A | C | C | A | D | D | A | C | D | A |
| Approach Delay |  | 15.4 |  |  | 29.9 |  |  | 47.3 |  |  | 38.6 |  |
| Approach LOS |  | B |  |  | C |  |  | D |  |  | D |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

Cycle Length： 90
Actuated Cycle Length： 90
Offset： $71(79 \%)$ ，Referenced to phase 2：EBTL and 6 ：WBTL，Start of FDW or yellow
Natural Cycle： 90
Control Type：Actuated－Coordinated
Maximum v／c Ratio： 0.93
Intersection Signal Delay： 36.6 Intersection LOS：D
Intersection Capacity Utilization 79．8\％ICU Level of Service D
Analysis Period（min） 15
Splits and Phases：10：US 24 \＆Meridian Rd







| Major/Minor M | Major1 |  | Major2 |  | Minor2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 89 | 0 | - | 0 | 255 | 89 |
| Stage 1 | - | - | - | - | 89 | - |
| Stage 2 | - | - | - | - | 166 | - |
| Critical Hdwy | 4.12 | - | - | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |
| Follow-up Hdwy | 2.218 | - | - | - | 3.518 | 3.318 |
| Pot Cap-1 Maneuver | 1506 | - | - | - | 734 | 969 |
| Stage 1 | - | - | - | - | 934 | - |
| Stage 2 | - | - | - | - | 863 | - |
| Platoon blocked, \% |  | - | - | - |  |  |
| Mov Cap-1 Maneuver | 1506 | - | - | - | 710 | 969 |
| Mov Cap-2 Maneuver | - | - | - | - | 710 | - |
| Stage 1 | - | - | - | - | 903 | - |
| Stage 2 | - | - | - | - | 863 | - |
|  |  |  |  |  |  |  |
| Approach | EB |  | WB |  | SB |  |
| HCM Control Delay, s | 3.1 |  | 0 |  | 8.8 |  |
| HCM LOS |  |  |  |  | A |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | EBL | EBT | WBT WBR SBLn1 |  |  |
| Capacity (veh/h) |  | 1506 | - | - | - | 969 |
| HCM Lane V/C Ratio |  | 0.032 | - | - | - | 0.034 |
| HCM Control Delay (s) |  | 7.5 | - | - | - | 8.8 |
| HCM Lane LOS |  | A | - | - | - | A |
| HCM 95th \%tile Q(veh) |  | 0.1 | - | - | - | 0.1 |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 1.9 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | $\uparrow$ |  |  | -1 | Mr |  |
| Traffic Vol, veh/h | 52 | 10 | 0 | 56 | 30 | 1 |
| Future Vol, veh/h | 52 | 10 | 0 | 56 | 30 | 1 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 57 | 11 | 0 | 61 | 33 | 1 |


| Major/Minor | Major1 |  | Major2 |  | Minor1 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 0 | 0 | 68 | 0 | 124 | 63 |
| Stage 1 | - | - | - | - | 63 | - |
| Stage 2 | - | - | - | - | 61 | - |
| Critical Hdwy | - | - | 4.12 | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |
| Follow-up Hdwy | - | - | 2.218 | - | 3.518 | 3.318 |
| Pot Cap-1 Maneuver | - | - | 1533 | - | 871 | 1002 |
| Stage 1 | - | - | - | - | 960 | - |
| Stage 2 | - | - | - | - | 962 | - |
| Platoon blocked, \% | - | - |  | - |  |  |
| Mov Cap-1 Maneuver | - | - | 1533 | - | 871 | 1002 |
| Mov Cap-2 Maneuver | - | - | - | - | 871 | - |
| Stage 1 | - | - | - | - | 960 | - |
| Stage 2 | - | - | - | - | 962 | - |
|  |  |  |  |  |  |  |
| Approach | EB |  | WB |  | NB |  |
| HCM Control Delay, s | 0 |  | 0 |  | 9.3 |  |
| HCM LOS |  |  |  |  | A |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NBLn1 EBT EBR WBL WBT |  |  |  |  |
| Capacity (veh/h) |  | 875 | - | - | 1533 | - |
| HCM Lane V/C Ratio |  | 0.039 | - | - | - | - |
| HCM Control Delay (s) |  | 9.3 | - | - | 0 | - |
| HCM Lane LOS |  | A | - | - | A | - |
| HCM 95th \%tile Q(veh) |  | 0.1 | - | - | 0 | - |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.8 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | $\uparrow$ |  |  | -1 | Mr |  |
| Traffic Vol, veh/h | 50 | 2 | 1 | 49 | 7 | 2 |
| Future Vol, veh/h | 50 | 2 | 1 | 49 | 7 | 2 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 54 | 2 | 1 | 53 | 8 | 2 |


| Major/Minor | Major1 |  | Major2 |  | Minor1 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 0 | 0 | 56 | 0 | 110 | 55 |
| Stage 1 | - | - | - | - | 55 | - |
| Stage 2 | - | - | - | - | 55 | - |
| Critical Hdwy | - | - | 4.12 | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |
| Follow-up Hdwy | - | - | 2.218 | - | 3.518 | 3.318 |
| Pot Cap-1 Maneuver | - | - | 1549 | - | 887 | 1012 |
| Stage 1 | - | - | - | - | 968 | - |
| Stage 2 | - | - | - | - | 968 | - |
| Platoon blocked, \% | - | - |  | - |  |  |
| Mov Cap-1 Maneuver | - | - | 1549 | - | 886 | 1012 |
| Mov Cap-2 Maneuver | - | - | - | - | 886 | - |
| Stage 1 | - | - | - | - | 968 | - |
| Stage 2 | - | - | - | - | 967 | - |
|  |  |  |  |  |  |  |
| Approach | EB |  | WB |  | NB |  |
| HCM Control Delay, s | 0 |  | 0.1 |  | 9 |  |
| HCM LOS |  |  |  |  | A |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NBLn1 EBT EBR WBL WBT |  |  |  |  |
| Capacity (veh/h) |  | 911 | - | - | 1549 | - |
| HCM Lane V/C Ratio |  | 0.011 | - |  | 0.001 | - |
| HCM Control Delay (s) |  | 9 | - | - | 7.3 | 0 |
| HCM Lane LOS |  | A | - | - | A | A |
| HCM 95th \%tile Q(veh) |  | 0 | - | - | 0 | - |


|  | $\stackrel{ }{*}$ |  |  | $\checkmark$ |  |  | 4 | 4 |  | ＊ | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \％${ }^{1 / 1}$ | 个4 | F | \％＊ | 性 | F | \％＊ | 个4 | 「 | \％＊ | 个4 | F |
| Trafic Volume（vph） | 302 | 383 | 232 | 70 | 638 | 49 | 167 | 209 | 20 | 62 | 597 | 541 |
| Future Volume（vph） | 302 | 383 | 232 | 70 | 638 | 49 | 167 | 209 | 20 | 62 | 597 | 541 |
| Turn Type | Prot | NA | Free | Prot | NA | Perm | Prot | NA | Free | Prot | NA | Free |
| Protected Phases | 7 | 4 |  | 3 | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Permitted Phases |  |  | Free |  |  | 8 |  |  | Free |  |  | Free |
| Detector Phase | 7 | 4 |  | 3 | 8 | 8 | 5 | 2 |  | 1 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 5.0 | 15.0 |  | 5.0 | 15.0 | 15.0 | 5.0 | 15.0 |  | 5.0 | 15.0 |  |
| Minimum Split（s） | 12.5 | 22.0 |  | 12.5 | 22.0 | 22.0 | 13.5 | 22.0 |  | 13.5 | 22.0 |  |
| Total Split（s） | 25.0 | 33.0 |  | 15.0 | 23.0 | 23.0 | 18.0 | 27.0 |  | 15.0 | 24.0 |  |
| Total Split（\％） | 27．8\％ | 36．7\％ |  | 16．7\％ | 25．6\％ | 25．6\％ | 20．0\％ | 30．0\％ |  | 16．7\％ | 26．7\％ |  |
| Yellow Time（s） | 4.0 | 5.0 |  | 4.0 | 5.0 | 5.0 | 5.0 | 5.0 |  | 5.0 | 5.0 |  |
| All－Red Time（s） | 3.5 | 2.0 |  | 3.5 | 2.0 | 2.0 | 3.5 | 2.0 |  | 3.5 | 2.0 |  |
| Lost Time Adjust（s） | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time（s） | 7.5 | 7.0 |  | 7.5 | 7.0 | 7.0 | 8.5 | 7.0 |  | 8.5 | 7.0 |  |
| Lead／Lag | Lead | Lag |  | Lead | Lag | Lag | Lead | Lag |  | Lead | Lag |  |
| Lead－Lag Optimize？ | Yes | Yes |  | Yes | Yes | Yes | Yes | Yes |  | Yes | Yes |  |
| Recall Mode | None | None |  | None | None | None | None | C－Max |  | None | C－Max |  |
| Act Effct Green（s） | 13.5 | 29.2 | 90.0 | 6.9 | 20.0 | 20.0 | 8.9 | 23.0 | 90.0 | 6.3 | 17.6 | 90.0 |
| Actuated g／C Ratio | 0.15 | 0.32 | 1.00 | 0.08 | 0.22 | 0.22 | 0.10 | 0.26 | 1.00 | 0.07 | 0.20 | 1.00 |
| v／c Ratio | 0.61 | 0.35 | 0.15 | 0.28 | 0.84 | 0.08 | 0.52 | 0.24 | 0.01 | 0.27 | 0.90 | 0.36 |
| Control Delay | 40.8 | 25.4 | 0.2 | 60.6 | 39.0 | 0.4 | 48.0 | 16.5 | 0.0 | 42.6 | 53.4 | 0.6 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 40.8 | 25.4 | 0.2 | 60.6 | 39.0 | 0.4 | 48.0 | 16.5 | 0.0 | 42.6 | 53.4 | 0.6 |
| LOS | D | C | A | E | D | A | D | B | A | D | D | A |
| Approach Delay |  | 24.1 |  |  | 38.5 |  |  | 28.9 |  |  | 29.1 |  |
| Approach LOS |  | C |  |  | D |  |  | C |  |  | C |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

Cycle Length： 90
Actuated Cycle Length： 90
Offset： $0(0 \%)$ ，Referenced to phase 2：NBT and 6：SBT，Start of FDW or yellow，Master Intersection
Natural Cycle： 80
Control Type：Actuated－Coordinated
Maximum v／c Ratio： 0.90
Intersection Signal Delay： 29.8
Intersection LOS：C
Intersection Capacity Utilization 72．5\％
ICU Level of Service C
Analysis Period（min） 15
Splits and Phases：7：Meridian Rd \＆Woodmen Rd


|  | $\stackrel{ }{*}$ |  |  |  |  |  | 4 | $\dagger$ | 7 |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | 个4 | F | \% | 个 $\uparrow$ | F | \% | $\uparrow$ | F | \% | 4 | F |
| Trafic Volume (vph) | 101 | 318 | 46 | 28 | 426 | 152 | 39 | 45 | 10 | 130 | 125 | 293 |
| Future Volume (vph) | 101 | 318 | 46 | 28 | 426 | 152 | 39 | 45 | 10 | 130 | 125 | 293 |
| Turn Type | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | Perm |
| Protected Phases | 5 | 2 |  | 1 | 6 |  | 3 | 8 |  | 7 | 4 |  |
| Permitted Phases | 2 |  | 2 | 6 |  | 6 | 8 |  | 8 | 4 |  | 4 |
| Detector Phase | 5 | 2 | 2 | 1 | 6 | 6 | 3 | 8 | 8 | 7 | 4 | 4 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Minimum Split (s) | 12.5 | 25.0 | 25.0 | 12.5 | 25.0 | 25.0 | 13.5 | 25.0 | 25.0 | 13.5 | 25.0 | 25.0 |
| Total Split (s) | 14.0 | 37.0 | 37.0 | 14.0 | 37.0 | 37.0 | 14.0 | 25.0 | 25.0 | 14.0 | 25.0 | 25.0 |
| Total Split (\%) | 15.6\% | 41.1\% | 41.1\% | 15.6\% | 41.1\% | 41.1\% | 15.6\% | 27.8\% | 27.8\% | 15.6\% | 27.8\% | 27.8\% |
| Yellow Time (s) | 4.0 | 5.0 | 5.0 | 4.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| All-Red Time (s) | 3.5 | 2.0 | 2.0 | 3.5 | 2.0 | 2.0 | 3.5 | 2.0 | 2.0 | 3.5 | 2.0 | 2.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 7.5 | 7.0 | 7.0 | 7.5 | 7.0 | 7.0 | 8.5 | 7.0 | 7.0 | 8.5 | 7.0 | 7.0 |
| Lead/Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | Lag |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Recall Mode | None | C-Max | C-Max | None | C-Max | C-Max | None | Max | Max | None | Max | Max |
| Act Effct Green (s) | 40.5 | 38.4 | 38.4 | 37.3 | 32.8 | 32.8 | 22.0 | 18.0 | 18.0 | 25.4 | 23.6 | 23.6 |
| Actuated g/C Ratio | 0.45 | 0.43 | 0.43 | 0.41 | 0.36 | 0.36 | 0.24 | 0.20 | 0.20 | 0.28 | 0.26 | 0.26 |
| v/c Ratio | 0.24 | 0.21 | 0.06 | 0.06 | 0.34 | 0.21 | 0.12 | 0.12 | 0.02 | 0.35 | 0.26 | 0.47 |
| Control Delay | 33.0 | 38.0 | 4.0 | 13.0 | 22.7 | 1.0 | 21.6 | 30.7 | 0.1 | 25.8 | 30.7 | 6.7 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 33.0 | 38.0 | 4.0 | 13.0 | 22.7 | 1.0 | 21.6 | 30.7 | 0.1 | 25.8 | 30.7 | 6.7 |
| LOS | C | D | A | B | C | A | C | C | A | C | C | A |
| Approach Delay |  | 33.5 |  |  | 16.8 |  |  | 23.7 |  |  | 16.7 |  |
| Approach LOS |  | C |  |  | B |  |  | C |  |  | B |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

Cycle Length: 90
Actuated Cycle Length: 90
Offset: $0(0 \%)$, Referenced to phase 2:EBTL and 6:WBTL, Start of Green
Natural Cycle: 80
Control Type: Actuated-Coordinated
Maximum v/c Ratio: 0.47
Intersection Signal Delay: 21.7 Intersection LOS: C

Intersection Capacity Utilization 52.5\%
ICU Level of Service A
Analysis Period (min) 15
Splits and Phases: 8: McLaughlin Rd \& Woodmen Rd



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.4 |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | Mr |  |  | 4 | 个 |  |
| Traffic Vol, veh/h | 2 | 1 | 4 | 60 | 81 | 4 |
| Future Vol, veh/h | 2 | 1 | 4 | 60 | 81 | 4 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 2 | 1 | 4 | 65 | 88 | 4 |



|  | 4 |  |  |  |  |  | 4 | $\uparrow$ | $p$ |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | 个4 | F | \％ | 性 | F | \％${ }^{\text {\％}}$ | 4 | 「 | ${ }^{7}$ | $\uparrow$ | F |
| Traffic Volume（vph） | 7 | 391 | 719 | 32 | 190 | 26 | 203 | 340 | 18 | 70 | 696 | 2 |
| Future Volume（vph） | 7 | 391 | 719 | 32 | 190 | 26 | 203 | 340 | 18 | 70 | 696 | 2 |
| Turn Type | pm＋pt | NA | Free | pm＋pt | NA | Free | Prot | NA | Perm | pm＋pt | NA | Perm |
| Protected Phases | 5 | 2 |  | 1 | 6 |  | 3 | 8 |  | 7 | 4 |  |
| Permitted Phases | 2 |  | Free | 6 |  | Free |  |  | 8 | 4 |  | 4 |
| Detector Phase | 5 | 2 |  | 1 | 6 |  | 3 | 8 | 8 | 7 | 4 | 4 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 5.0 | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Minimum Split（s） | 11.0 | 20.0 |  | 11.0 | 20.0 |  | 11.0 | 20.0 | 20.0 | 11.0 | 20.0 | 20.0 |
| Total Split（s） | 11.0 | 20.0 |  | 11.0 | 20.0 |  | 15.0 | 47.0 | 47.0 | 12.0 | 44.0 | 44.0 |
| Total Split（\％） | 12．2\％ | 22．2\％ |  | 12．2\％ | 22．2\％ |  | 16．7\％ | 52．2\％ | 52．2\％ | 13．3\％ | 48．9\％ | 48．9\％ |
| Yellow Time（s） | 3.0 | 5.0 |  | 3.0 | 5.0 |  | 3.0 | 4.5 | 4.5 | 3.0 | 4.5 | 4.5 |
| All－Red Time（s） | 3.0 | 2.0 |  | 3.0 | 2.0 |  | 3.0 | 2.0 | 2.0 | 3.0 | 2.0 | 2.0 |
| Lost Time Adjust（s） | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） | 6.0 | 7.0 |  | 6.0 | 7.0 |  | 6.0 | 6.5 | 6.5 | 6.0 | 6.5 | 6.5 |
| Lead／Lag | Lead | Lag |  | Lead | Lag |  | Lead | Lag | Lag | Lead | Lag | Lag |
| Lead－Lag Optimize？ | Yes | Yes |  | Yes | Yes |  | Yes | Yes | Yes | Yes | Yes | Yes |
| Recall Mode | None | C－Max |  | None | C－Max |  | None | None | None | None | None | None |
| Act Effct Green（s） | 22.7 | 18.7 | 90.0 | 25.1 | 23.1 | 90.0 | 8.7 | 41.6 | 41.6 | 42.8 | 36.4 | 36.4 |
| Actuated g／C Ratio | 0.25 | 0.21 | 1.00 | 0.28 | 0.26 | 1.00 | 0.10 | 0.46 | 0.46 | 0.48 | 0.40 | 0.40 |
| $\mathrm{V} / \mathrm{c}$ Ratio | 0.02 | 0.54 | 0.46 | 0.13 | 0.21 | 0.02 | 0.62 | 0.40 | 0.02 | 0.14 | 0.94 | 0.00 |
| Control Delay | 26.6 | 36.5 | 1.9 | 25.4 | 29.0 | 0.0 | 47.7 | 18.2 | 0.1 | 9.1 | 48.2 | 0.0 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 26.6 | 36.5 | 1.9 | 25.4 | 29.0 | 0.0 | 47.7 | 18.2 | 0.1 | 9.1 | 48.2 | 0.0 |
| LOS | C | D | A | C | C | A | D | B | A | A | D | A |
| Approach Delay |  | 14.2 |  |  | 25.5 |  |  | 28.3 |  |  | 44.6 |  |
| Approach LOS |  | B |  |  | C |  |  | C |  |  | D |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

Cycle Length： 90
Actuated Cycle Length： 90
Offset： $71(79 \%)$ ，Referenced to phase 2：EBTL and 6 ：WBTL，Start of FDW or yellow
Natural Cycle： 80
Control Type：Actuated－Coordinated
Maximum v／c Ratio： 0.94
Intersection Signal Delay： 26.8
Intersection LOS：C
Intersection Capacity Utilization 78．6\％
ICU Level of Service D
Analysis Period（min） 15
Splits and Phases：10：US 24 \＆Meridian Rd


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 0 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |  |
| Lane Configurations |  |  | 7 |  |  | 「 |  | 4 | 「 |  | 4 | F |  |
| Traffic Vol, veh/h | 0 | 0 | 25 | 0 | 0 | 51 | 0 | 344 | 29 | 0 | 743 | 4 |  |
| Future Vol, veh/h | 0 | 0 | 25 | 0 | 0 | 51 | 0 | 344 | 29 | 0 | 743 | 4 |  |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Sign Control Star | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |  |
| RT Channelized | - | - | Free | - | - | Free | - | - | None | - | - | None |  |
| Storage Length | - | - | 0 | - | - | 0 | - | - | 400 | - | - | 400 |  |
| Veh in Median Storage, \# | \# | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |  |
| Peak Hour Factor | 91 | 91 | 91 | 91 | 91 | 91 | 91 | 91 | 91 | 91 | 91 | 91 |  |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |  |
| Mvmt Flow | 0 | 0 | 27 | 0 | 0 | 56 | 0 | 378 | 32 | 0 | 816 | 4 |  |



| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 7.8 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |  |
| Lane Configurations | ${ }^{*}$ | $\hat{\beta}$ |  | * | $\uparrow$ |  |  | ¢ |  |  | * |  |  |
| Traffic Vol, veh/h | 0 | 0 | 0 | 53 | 0 | 23 | 0 | 0 | 21 | 85 | 0 | 0 |  |
| Future Vol, veh/h | 0 | 0 | 0 | 53 | 0 | 23 | 0 | 0 | 21 | 85 | 0 | 0 |  |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Sign Control F | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |  |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |  |
| Storage Length | 135 | - | - | 190 | - | - | - | - | - | - | - | - |  |
| Veh in Median Storage, \# | \# | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |  |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |  |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |  |
| Mvmt Flow | 0 | 0 | 0 | 58 | 0 | 25 | 0 | 0 | 23 | 92 | 0 | 0 |  |






| Major/Minor $\quad$ N | Major1 |  | Major2 |  | Minor1 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 0 | 0 | 137 | 0 | 221 | 120 |
| Stage 1 | - | - | - | - | 120 | - |
| Stage 2 | - | - | - | - | 101 | - |
| Critical Hdwy | - | - | 4.12 | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - |  | 5.42 | - |
| Follow-up Hdwy | - | - | 2.218 |  | 3.518 | 3.318 |
| Pot Cap-1 Maneuver | - | - | 1447 | - | 767 | 931 |
| Stage 1 | - | - | - |  | 905 | - |
| Stage 2 | - | - | - |  | 923 | - |
| Platoon blocked, \% | - | - |  | - |  |  |
| Mov Cap-1 Maneuver | - | - | 1447 |  | 766 | 931 |
| Mov Cap-2 Maneuver | - | - | - | - | 766 | - |
| Stage 1 | - | - | - |  | 905 | - |
| Stage 2 | - | - | - |  | 922 | - |
|  |  |  |  |  |  |  |
| Approach | EB |  | WB |  | NB |  |
| HCM Control Delay, s | 0 |  | 0.1 |  | 9.8 |  |
| HCM LOS |  |  |  |  | A |  |
| HCMLOS |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NBLn1 | EBT | EBR | WBL | WBT |
| Capacity (veh/h) |  | 766 | - | - | 1447 | - |
| HCM Lane V/C Ratio |  | 0.018 | - | - | 0.001 | - |
| HCM Control Delay (s) |  | 9.8 | - | - | 7.5 | O |
| HCM Lane LOS |  | A | - | - | A | A |
| HCM 95th \%tile Q(veh) |  | 0.1 | - | - | 0 | - |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.3 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | $\uparrow$ |  |  | -1 | Mr |  |
| Traffic Vol, veh/h | 88 | 7 | 2 | 88 | 3 | 1 |
| Future Vol, veh/h | 88 | 7 | 2 | 88 | 3 | 1 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 96 | 8 | 2 | 96 | 3 | 1 |



|  | $\rangle$ |  |  | $\dagger$ |  |  | 4 | $\uparrow$ |  |  | $\frac{1}{\downarrow}$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \％${ }^{1}$ | ¢ $\uparrow$ | 「 | \％${ }^{1 / 1}$ | 性 | $\stackrel{7}{7}$ | \％＊ | 性 | 「 | \％＊＊ | 性 | F |
| Traffic Volume（vph） | 638 | 586 | 131 | 122 | 538 | 114 | 248 | 547 | 85 | 159 | 422 | 366 |
| Future Volume（vph） | 638 | 586 | 131 | 122 | 538 | 114 | 248 | 547 | 85 | 159 | 422 | 366 |
| Turn Type | Prot | NA | Free | Prot | NA | Perm | Prot | NA | Free | Prot | NA | Free |
| Protected Phases | 7 | 4 |  | 3 | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Permitted Phases |  |  | Free |  |  | 8 |  |  | Free |  |  | Free |
| Detector Phase | 7 | 4 |  | 3 | 8 | 8 | 5 | 2 |  | 1 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 5.0 | 15.0 |  | 5.0 | 15.0 | 15.0 | 5.0 | 15.0 |  | 5.0 | 15.0 |  |
| Minimum Split（s） | 12.5 | 22.0 |  | 12.5 | 22.0 | 22.0 | 13.5 | 22.0 |  | 13.5 | 22.0 |  |
| Total Split（s） | 25.0 | 33.0 |  | 15.0 | 23.0 | 23.0 | 18.0 | 27.0 |  | 15.0 | 24.0 |  |
| Total Split（\％） | 27．8\％ | 36．7\％ |  | 16．7\％ | 25．6\％ | 25．6\％ | 20．0\％ | 30．0\％ |  | 16．7\％ | 26．7\％ |  |
| Yellow Time（s） | 4.0 | 5.0 |  | 4.0 | 5.0 | 5.0 | 5.0 | 5.0 |  | 5.0 | 5.0 |  |
| All－Red Time（s） | 3.5 | 2.0 |  | 3.5 | 2.0 | 2.0 | 3.5 | 2.0 |  | 3.5 | 2.0 |  |
| Lost Time Adjust（s） | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time（s） | 7.5 | 7.0 |  | 7.5 | 7.0 | 7.0 | 8.5 | 7.0 |  | 8.5 | 7.0 |  |
| Lead／Lag | Lead | Lag |  | Lead | Lag | Lag | Lead | Lag |  | Lead | Lag |  |
| Lead－Lag Optimize？ | Yes | Yes |  | Yes | Yes | Yes | Yes | Yes |  | Yes | Yes |  |
| Recall Mode | None | None |  | None | None | None | None | C－Max |  | None | C－Max |  |
| Act Effct Green（s） | 17.5 | 26.1 | 90.0 | 7.3 | 15.9 | 15.9 | 9.4 | 20.0 | 90.0 | 6.6 | 17.2 | 90.0 |
| Actuated g／C Ratio | 0.19 | 0.29 | 1.00 | 0.08 | 0.18 | 0.18 | 0.10 | 0.22 | 1.00 | 0.07 | 0.19 | 1.00 |
| $\mathrm{V} / \mathrm{c}$ Ratio | 1.00 | 0.59 | 0.09 | 0.46 | 0.89 | 0.21 | 0.72 | 0.73 | 0.06 | 0.66 | 0.65 | 0.24 |
| Control Delay | 71.9 | 30.3 | 0.1 | 66.6 | 46.3 | 3.4 | 63.5 | 20.5 | 0.1 | 54.5 | 38.9 | 0.4 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 71.9 | 30.3 | 0.1 | 66.6 | 46.3 | 3.4 | 63.5 | 20.5 | 0.1 | 54.5 | 38.9 | 0.4 |
| LOS | E | C | A | E | D | A | E | C | A | D | D | A |
| Approach Delay |  | 47.0 |  |  | 43.2 |  |  | 30.6 |  |  | 26.6 |  |
| Approach LOS |  | D |  |  | D |  |  | C |  |  | C |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

Cycle Length： 90
Actuated Cycle Length： 90
Offset： $0(0 \%)$ ，Referenced to phase 2：NBT and 6：SBT，Start of FDW or yellow，Master Intersection
Natural Cycle： 90
Control Type：Actuated－Coordinated
Maximum v／c Ratio： 1.00

```
Intersection Signal Delay： 37.7
Intersection LOS：D
```

Intersection Capacity Utilization 77．3\％
ICU Level of Service D
Analysis Period（min） 15
Splits and Phases：7：Meridian Rd \＆Woodmen Rd


|  | $\stackrel{ }{*}$ |  |  |  |  |  | 4 | $\dagger$ | 7 |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \％ | 个4 | 「 | \％ | 个 $\uparrow$ | F | \％ | $\uparrow$ | 「 | \％ | 4 | F |
| Trafic Volume（vph） | 296 | 438 | 97 | 45 | 494 | 282 | 86 | 165 | 87 | 202 | 113 | 194 |
| Future Volume（vph） | 296 | 438 | 97 | 45 | 494 | 282 | 86 | 165 | 87 | 202 | 113 | 194 |
| Turn Type | pm＋pt | NA | Perm | pm＋pt | NA | Perm | pm＋pt | NA | Perm | pm＋pt | NA | Perm |
| Protected Phases | 5 | 2 |  | 1 | 6 |  | 3 | 8 |  | 7 | 4 |  |
| Permitted Phases | 2 |  | 2 | 6 |  | 6 | 8 |  | 8 | 4 |  | 4 |
| Detector Phase | 5 | 2 | 2 | 1 | 6 | 6 | 3 | 8 | 8 | 7 | 4 | 4 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Minimum Split（s） | 12.5 | 25.0 | 25.0 | 12.5 | 25.0 | 25.0 | 13.5 | 25.0 | 25.0 | 13.5 | 25.0 | 25.0 |
| Total Split（s） | 14.0 | 37.0 | 37.0 | 14.0 | 37.0 | 37.0 | 14.0 | 25.0 | 25.0 | 14.0 | 25.0 | 25.0 |
| Total Split（\％） | 15．6\％ | 41．1\％ | 41．1\％ | 15．6\％ | 41．1\％ | 41．1\％ | 15．6\％ | 27．8\％ | 27．8\％ | 15．6\％ | 27．8\％ | 27．8\％ |
| Yellow Time（s） | 4.0 | 5.0 | 5.0 | 4.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| All－Red Time（s） | 3.5 | 2.0 | 2.0 | 3.5 | 2.0 | 2.0 | 3.5 | 2.0 | 2.0 | 3.5 | 2.0 | 2.0 |
| Lost Time Adjust（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） | 7.5 | 7.0 | 7.0 | 7.5 | 7.0 | 7.0 | 8.5 | 7.0 | 7.0 | 8.5 | 7.0 | 7.0 |
| Lead／Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | Lag |
| Lead－Lag Optimize？ | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Recall Mode | None | C－Max | C－Max | None | C－Max | C－Max | None | Max | Max | None | Max | Max |
| Act Effct Green（s） | 39.0 | 35.6 | 35.6 | 35.7 | 30.0 | 30.0 | 22.0 | 18.0 | 18.0 | 23.7 | 20.8 | 20.8 |
| Actuated g／C Ratio | 0.43 | 0.40 | 0.40 | 0.40 | 0.33 | 0.33 | 0.24 | 0.20 | 0.20 | 0.26 | 0.23 | 0.23 |
| v／c Ratio | 0.81 | 0.32 | 0.13 | 0.11 | 0.43 | 0.40 | 0.26 | 0.46 | 0.18 | 0.62 | 0.27 | 0.36 |
| Control Delay | 53.9 | 38.9 | 7.7 | 13.4 | 24.8 | 4.6 | 23.6 | 36.3 | 0.8 | 35.1 | 32.3 | 4.2 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 53.9 | 38.9 | 7.7 | 13.4 | 24.8 | 4.6 | 23.6 | 36.3 | 0.8 | 35.1 | 32.3 | 4.2 |
| LOS | D | D | A | B | C | A | C | D | A | D | C | A |
| Approach Delay |  | 40.6 |  |  | 17.2 |  |  | 23.9 |  |  | 22.7 |  |
| Approach LOS |  | D |  |  | B |  |  | C |  |  | C |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

Cycle Length： 90
Actuated Cycle Length： 90
Offset： $0(0 \%)$ ，Referenced to phase 2：EBTL and 6：WBTL，Start of Green
Natural Cycle： 80
Control Type：Actuated－Coordinated
Maximum v／c Ratio： 0.81
Intersection Signal Delay：27．0 Intersection LOS：C
Intersection Capacity Utilization 73．3\％
ICU Level of Service D
Analysis Period（min） 15
Splits and Phases：8：McLaughlin Rd \＆Woodmen Rd



|  | $\rangle$ |  |  |  |  |  | 4 | $\uparrow$ | ＋ |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | 性 | 「 | ${ }^{7}$ | 性 | 「 | \％＊ | 4 | F | \％ | $\uparrow$ | 「 |
| Traffic Volume（vph） | 19 | 256 | 294 | 32 | 369 | 53 | 587 | 800 | 12 | 92 | 440 | 7 |
| Future Volume（vph） | 19 | 256 | 294 | 32 | 369 | 53 | 587 | 800 | 12 | 92 | 440 | 7 |
| Turn Type | pm＋pt | NA | Free | pm＋pt | NA | Free | Prot | NA | Perm | pm＋pt | NA | Perm |
| Protected Phases | 5 | 2 |  | 1 | 6 |  | 3 | 8 |  | 7 | 4 |  |
| Permitted Phases | 2 |  | Free | 6 |  | Free |  |  | 8 | 4 |  | 4 |
| Detector Phase | 5 | 2 |  | 1 | 6 |  | 3 | 8 | 8 | 7 | 4 | 4 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 5.0 | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Minimum Split（s） | 11.0 | 20.0 |  | 11.0 | 20.0 |  | 11.0 | 20.0 | 20.0 | 11.0 | 20.0 | 20.0 |
| Total Split（s） | 11.0 | 20.0 |  | 11.0 | 20.0 |  | 25.0 | 47.0 | 47.0 | 12.0 | 34.0 | 34.0 |
| Total Split（\％） | 12．2\％ | 22．2\％ |  | 12．2\％ | 22．2\％ |  | 27．8\％ | 52．2\％ | 52．2\％ | 13．3\％ | 37．8\％ | 37．8\％ |
| Yellow Time（s） | 3.0 | 5.0 |  | 3.0 | 5.0 |  | 3.0 | 4.5 | 4.5 | 3.0 | 4.5 | 4.5 |
| All－Red Time（s） | 3.0 | 2.0 |  | 3.0 | 2.0 |  | 3.0 | 2.0 | 2.0 | 3.0 | 2.0 | 2.0 |
| Lost Time Adjust（s） | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） | 6.0 | 7.0 |  | 6.0 | 7.0 |  | 6.0 | 6.5 | 6.5 | 6.0 | 6.5 | 6.5 |
| Lead／Lag | Lead | Lag |  | Lead | Lag |  | Lead | Lag | Lag | Lead | Lag | Lag |
| Lead－Lag Optimize？ | Yes | Yes |  | Yes | Yes |  | Yes | Yes | Yes | Yes | Yes | Yes |
| Recall Mode | None | C－Max |  | None | C－Max |  | None | None | None | None | None | None |
| Act Effct Green（s） | 22.5 | 18.5 | 90.0 | 23.7 | 20.7 | 90.0 | 18.6 | 41.8 | 41.8 | 33.3 | 26.8 | 26.8 |
| Actuated g／C Ratio | 0.25 | 0.21 | 1.00 | 0.26 | 0.23 | 1.00 | 0.21 | 0.46 | 0.46 | 0.37 | 0.30 | 0.30 |
| v／c Ratio | 0.07 | 0.37 | 0.20 | 0.11 | 0.48 | 0.04 | 0.88 | 0.98 | 0.02 | 0.49 | 0.84 | 0.01 |
| Control Delay | 25.8 | 32.5 | 0.3 | 25.1 | 34.6 | 0.0 | 50.2 | 53.2 | 0.0 | 22.0 | 45.1 | 0.0 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 25.8 | 32.5 | 0.3 | 25.1 | 34.6 | 0.0 | 50.2 | 53.2 | 0.0 | 22.0 | 45.1 | 0.0 |
| LOS | C | C | A | C | C | A | D | D | A | C | D | A |
| Approach Delay |  | 15.6 |  |  | 29.9 |  |  | 51.5 |  |  | 40.6 |  |
| Approach LOS |  | B |  |  | C |  |  | D |  |  | D |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

Cycle Length： 90
Actuated Cycle Length： 90
Offset： $71(79 \%)$ ，Referenced to phase 2：EBTL and 6 ：WBTL，Start of FDW or yellow
Natural Cycle： 90
Control Type：Actuated－Coordinated
Maximum v／c Ratio： 0.98
Intersection Signal Delay： $39.3 \quad$ Intersection LOS：D
Intersection Capacity Utilization 82．8\％
ICU Level of Service E
Analysis Period（min） 15
Splits and Phases：10：US 24 \＆Meridian Rd




| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.9 |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | Mr |  |  | 4 | 个 |  |
| Traffic Vol, veh/h | 10 | 8 | 6 | 116 | 97 | 6 |
| Future Vol, veh/h | 10 | 8 | 6 | 116 | 97 | 6 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 11 | 9 | 7 | 126 | 105 | 7 |


| Major/Minor | Minor2 |  | Major1 |  | Major2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 249 | 109 | 112 | 0 | - | 0 |
| Stage 1 | 109 | - | - | - | - | - |
| Stage 2 | 140 | - | - | - | - | - |
| Critical Hdwy | 6.42 | 6.22 | 4.12 | - | - | - |
| Critical Hdwy Stg 1 | 5.42 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - | - |
| Follow-up Hdwy | 3.518 | 3.318 | 2.218 | - | - | - |
| Pot Cap-1 Maneuver | 739 | 945 | 1478 | - | - | - |
| Stage 1 | 916 | - | - | - | - | - |
| Stage 2 | 887 | - | - | - | - | - |
| Platoon blocked, \% |  |  |  | - | - | - |
| Mov Cap-1 Maneuver | 735 | 945 | 1478 | - | - | - |
| Mov Cap-2 Maneuver | 735 | - | - | - | - | - |
| Stage 1 | 911 | - | - | - | - | - |
| Stage 2 | 887 | - | - | - | - | - |
|  |  |  |  |  |  |  |
| Approach | EB |  | NB |  | SB |  |
| HCM Control Delay, s | 9.5 |  | 0.4 |  | 0 |  |
| HCM LOS | A |  |  |  |  |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NBL | NBT EBLn1 |  | SBT | SBR |
| Capacity (veh/h) |  | 1478 | - | 816 | - | - |
| HCM Lane V/C Ratio |  | 0.004 | - | 0.024 | - | - |
| HCM Control Delay (s) |  | 7.4 | - | 9.5 | - | - |
| HCM Lane LOS |  | A | - | A | - | - |
| HCM 95th \%tile Q(veh) |  | 0 | - | 0.1 | - | - |


|  | 4 |  |  |  |  |  |  | $\uparrow$ | $>$ |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{*}{ }^{1}$ | ¢ $\uparrow$ | 「 | ${ }^{*} 1$ | 个4 | 「 | ${ }^{7} 1$ | ¢ $\uparrow$ | 「 | ＊＊ | 个4 | 「 |
| Traffic Volume（vph） | 472 | 470 | 176 | 148 | 808 | 155 | 326 | 347 | 97 | 270 | 950 | 1041 |
| Future Volume（vph） | 472 | 470 | 176 | 148 | 808 | 155 | 326 | 347 | 97 | 270 | 950 | 1041 |
| Turn Type | Prot | NA | Free | Prot | NA | Perm | Prot | NA | Free | Prot | NA | Free |
| Protected Phases | 7 | 4 |  | 3 | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Permitted Phases |  |  | Free |  |  | 8 |  |  | Free |  |  | Free |
| Detector Phase | 7 | 4 |  | 3 | 8 | 8 | 5 | 2 |  | 1 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 5.0 | 15.0 |  | 5.0 | 15.0 | 15.0 | 5.0 | 15.0 |  | 5.0 | 15.0 |  |
| Minimum Split（s） | 12.5 | 22.0 |  | 12.5 | 22.0 | 22.0 | 13.5 | 22.0 |  | 13.5 | 22.0 |  |
| Total Split（s） | 21.0 | 41.0 |  | 19.0 | 39.0 | 39.0 | 20.0 | 34.0 |  | 26.0 | 40.0 |  |
| Total Split（\％） | 17．5\％ | 34．2\％ |  | 15．8\％ | 32．5\％ | 32．5\％ | 16．7\％ | 28．3\％ |  | 21．7\％ | 33．3\％ |  |
| Yellow Time（s） | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| All－Red Time（s） | 2.0 | 2.0 |  | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |  | 2.0 | 2.0 |  |
| Lost Time Adjust（s） | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time（s） | 5.0 | 5.0 |  | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |  | 5.0 | 5.0 |  |
| Lead／Lag | Lead | Lag |  | Lead | Lag | Lag | Lead | Lag |  | Lead | Lag |  |
| Lead－Lag Optimize？ | Yes | Yes |  | Yes | Yes | Yes | Yes | Yes |  | Yes | Yes |  |
| Recall Mode | None | None |  | None | None | None | None | C－Max |  | None | C－Max |  |
| Act Effict Green（s） | 16.0 | 37.8 | 120.0 | 10.7 | 32.5 | 32.5 | 14.7 | 36.4 | 120.0 | 15.1 | 36.8 | 120.0 |
| Actuated g／C Ratio | 0.13 | 0.32 | 1.00 | 0.09 | 0.27 | 0.27 | 0.12 | 0.30 | 1.00 | 0.13 | 0.31 | 1.00 |
| v／c Ratio | 1.08 | 0.44 | 0.12 | 0.50 | 0.88 | 0.29 | 0.81 | 0.34 | 0.06 | 0.65 | 0.91 | 0.68 |
| Control Delay | 113.1 | 34.2 | 0.1 | 57.5 | 53.2 | 6.4 | 66.8 | 34.6 | 0.1 | 57.1 | 54.0 | 2.4 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 113.1 | 34.2 | 0.1 | 57.5 | 53.2 | 6.4 | 66.8 | 34.6 | 0.1 | 57.1 | 54.0 | 2.4 |
| LOS | F | C | A | E | D | A | E | C | A | E | D | A |
| Approach Delay |  | 62.2 |  |  | 47.3 |  |  | 43.9 |  |  | 30.6 |  |
| Approach LOS |  | E |  |  | D |  |  | D |  |  | C |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length： 120 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length： 120 |  |  |  |  |  |  |  |  |  |  |  |  |
| Offset： 0 （0\％），Referenced to phase 2：NBT and 6：SBT，Start of FDW or yellow，Master Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle： 90 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type：Actuated－Coordinated |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v／c Ratio： 1.08 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay： 42.8 |  |  |  | Intersection LOS：D |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 88．0\％ |  |  |  | ICU Level of Service E |  |  |  |  |  |  |  |  |
| Analysis Period（min） 15 |  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases：7：Meridian Rd \＆Woodmen Rd


|  | $\stackrel{ }{*}$ |  |  |  |  |  | 4 | $\dagger$ | 7 |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \％ | 个4 | 「 | \％ | 个 $\uparrow$ | F | \％ | $\uparrow$ | F | \％ | 4 | F |
| Trafic Volume（vph） | 100 | 637 | 100 | 50 | 736 | 150 | 75 | 50 | 50 | 125 | 125 | 300 |
| Future Volume（vph） | 100 | 637 | 100 | 50 | 736 | 150 | 75 | 50 | 50 | 125 | 125 | 300 |
| Turn Type | pm＋pt | NA | Perm | pm＋pt | NA | Perm | pm＋pt | NA | Perm | pm＋pt | NA | Perm |
| Protected Phases | 5 | 2 |  | 1 | 6 |  | 3 | 8 |  | 7 | 4 |  |
| Permitted Phases | 2 |  | 2 | 6 |  | 6 | 8 |  | 8 | 4 |  | 4 |
| Detector Phase | 5 | 2 | 2 | 1 | 6 | 6 | 3 | 8 | 8 | 7 | 4 | 4 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Minimum Split（s） | 12.5 | 25.0 | 25.0 | 12.5 | 25.0 | 25.0 | 13.5 | 25.0 | 25.0 | 13.5 | 25.0 | 25.0 |
| Total Split（s） | 14.0 | 37.0 | 37.0 | 14.0 | 37.0 | 37.0 | 14.0 | 25.0 | 25.0 | 14.0 | 25.0 | 25.0 |
| Total Split（\％） | 15．6\％ | 41．1\％ | 41．1\％ | 15．6\％ | 41．1\％ | 41．1\％ | 15．6\％ | 27．8\％ | 27．8\％ | 15．6\％ | 27．8\％ | 27．8\％ |
| Yellow Time（s） | 4.0 | 5.0 | 5.0 | 4.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| All－Red Time（s） | 3.5 | 2.0 | 2.0 | 3.5 | 2.0 | 2.0 | 3.5 | 2.0 | 2.0 | 3.5 | 2.0 | 2.0 |
| Lost Time Adjust（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） | 7.5 | 7.0 | 7.0 | 7.5 | 7.0 | 7.0 | 8.5 | 7.0 | 7.0 | 8.5 | 7.0 | 7.0 |
| Lead／Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | Lag |
| Lead－Lag Optimize？ | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Recall Mode | None | C－Max | C－Max | None | C－Max | C－Max | None | Max | Max | None | Max | Max |
| Act Effct Green（s） | 39.0 | 35.6 | 35.6 | 37.4 | 32.8 | 32.8 | 22.0 | 18.0 | 18.0 | 23.7 | 20.8 | 20.8 |
| Actuated g／C Ratio | 0.43 | 0.40 | 0.40 | 0.42 | 0.36 | 0.36 | 0.24 | 0.20 | 0.20 | 0.26 | 0.23 | 0.23 |
| v／c Ratio | 0.36 | 0.46 | 0.13 | 0.15 | 0.58 | 0.21 | 0.23 | 0.14 | 0.10 | 0.35 | 0.30 | 0.52 |
| Control Delay | 16.9 | 22.9 | 0.3 | 13.9 | 26.3 | 0.9 | 22.9 | 30.8 | 0.4 | 25.7 | 32.7 | 8.3 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 16.9 | 22.9 | 0.3 | 13.9 | 26.3 | 0.9 | 22.9 | 30.8 | 0.4 | 25.7 | 32.7 | 8.3 |
| LOS | B | C | A | B | C | A | C | C | A | C | C | A |
| Approach Delay |  | 19.5 |  |  | 21.6 |  |  | 18.8 |  |  | 17.8 |  |
| Approach LOS |  | B |  |  | C |  |  | B |  |  | B |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

Cycle Length： 90
Actuated Cycle Length： 90
Offset： $0(0 \%)$ ，Referenced to phase 2：EBTL and 6：WBTL，Start of Green
Natural Cycle： 80
Control Type：Actuated－Coordinated
Maximum v／c Ratio： 0.58
Intersection Signal Delay： 19.9 Intersection LOS：B
Intersection Capacity Utilization 60．7\％ ICU Level of Service B
Analysis Period（min） 15
Splits and Phases：8：McLaughlin Rd \＆Woodmen Rd


|  | $\rangle$ |  |  | 7 |  |  | 4 | $\dagger$ | $p$ |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ＊＊ | $\uparrow$ | F | ${ }^{*}$ | 个 4 | $\stackrel{7}{ }$ | ${ }^{1 *}$ | 个种 | F | ${ }^{7}$ | 种 | F |
| Trafic Volume（vph） | 375 | 87 | 350 | 21 | 51 | 33 | 400 | 750 | 17 | 44 | 925 | 485 |
| Future Volume（vph） | 375 | 87 | 350 | 21 | 51 | 33 | 400 | 750 | 17 | 44 | 925 | 485 |
| Turn Type | Prot | NA | Free | pm＋pt | NA | Free | Prot | NA | Perm | pm＋pt | NA | Free |
| Protected Phases | 7 | 4 |  | 3 | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Permitted Phases |  |  | Free | 8 |  | Free |  |  | 2 | 6 |  | Free |
| Detector Phase | 7 | 4 |  | 3 | 8 |  | 5 | 2 | 2 | 1 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 20.0 | 15.0 |  | 5.0 | 15.0 |  | 5.0 | 15.0 | 15.0 | 5.0 | 15.0 |  |
| Minimum Split（s） | 25.0 | 23.0 |  | 10.0 | 23.0 |  | 10.0 | 23.0 | 23.0 | 10.0 | 23.0 |  |
| Total Split（s） | 27.0 | 37.0 |  | 15.0 | 25.0 |  | 20.0 | 58.0 | 58.0 | 10.0 | 48.0 |  |
| Total Split（\％） | 22．5\％ | 30．8\％ |  | 12．5\％ | 20．8\％ |  | 16．7\％ | 48．3\％ | 48．3\％ | 8．3\％ | 40．0\％ |  |
| Yellow Time（s） | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  |
| All－Red Time（s） | 2.0 | 2.0 |  | 2.0 | 2.0 |  | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |  |
| Lost Time Adjust（s） | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |
| Total Lost Time（s） | 5.0 | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |  |
| Lead／Lag | Lead | Lag |  | Lead | Lag |  | Lead | Lag | Lag | Lead | Lag |  |
| Lead－Lag Optimize？ | Yes | Yes |  | Yes | Yes |  | Yes | Yes | Yes | Yes | Yes |  |
| Recall Mode | None | None |  | None | None |  | None | C－Max | C－Max | None | C－Max |  |
| Act Effct Green（s） | 20.6 | 29.3 | 120.0 | 18.6 | 15.0 | 120.0 | 21.0 | 63.5 | 63.5 | 54.3 | 47.4 | 120.0 |
| Actuated g／C Ratio | 0.17 | 0.24 | 1.00 | 0.16 | 0.12 | 1.00 | 0.18 | 0.53 | 0.53 | 0.45 | 0.40 | 1.00 |
| v／c Ratio | 0.68 | 0.21 | 0.24 | 0.10 | 0.12 | 0.02 | 0.72 | 0.30 | 0.02 | 0.14 | 0.50 | 0.33 |
| Control Delay | 53.1 | 37.2 | 0.4 | 28.9 | 47.5 | 0.0 | 54.4 | 18.0 | 0.1 | 13.8 | 29.6 | 0.6 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 53.1 | 37.2 | 0.4 | 28.9 | 47.5 | 0.0 | 54.4 | 18.0 | 0.1 | 13.8 | 29.6 | 0.6 |
| LOS | D | D | A | C | D | A | D | B | A | B | C | A |
| Approach Delay |  | 28.7 |  |  | 28.8 |  |  | 30.3 |  |  | 19.4 |  |
| Approach LOS |  | C |  |  | C |  |  | C |  |  | B |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

Cycle Length： 120
Actuated Cycle Length： 120
Offset： 118 （98\％），Referenced to phase 2：NBT and 6：SBTL，Start of Green
Natural Cycle： 85
Control Type：Actuated－Coordinated
Maximum v／c Ratio： 0.72

Intersection Signal Delay： 25.4
Intersection Capacity Utilization 59．1\％
Analysis Period（min） 15

Intersection LOS：C
ICU Level of Service B

Splits and Phases：9：US 24 \＆Woodmen Rd


|  | 4 |  |  |  |  |  | 4 | $\dagger$ |  |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | 乐 | F | ${ }^{7}$ | 个4 | 「 | \％${ }^{*}$ | 个坐个 | F | ${ }_{1}$ | 性中 | F |
| Traffic Volume（vph） | 30 | 525 | 1000 | 40 | 275 | 245 | 275 | 892 | 30 | 215 | 1056 | 40 |
| Future Volume（vph） | 30 | 525 | 1000 | 40 | 275 | 245 | 275 | 892 | 30 | 215 | 1056 | 40 |
| Turn Type | pm＋pt | NA | Free | pm＋pt | NA | Free | Prot | NA | Perm | pm＋pt | NA | Perm |
| Protected Phases | 5 | 2 |  | 1 | 6 |  | 3 | 8 |  | 7 | 4 |  |
| Permitted Phases | 2 |  | Free | 6 |  | Free |  |  | 8 | 4 |  | 4 |
| Detector Phase | 5 | 2 |  | 1 | 6 |  | 3 | 8 | 8 | 7 | 4 | 4 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 5.0 | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Minimum Split（s） | 11.0 | 20.0 |  | 11.0 | 20.0 |  | 11.0 | 20.0 | 20.0 | 11.0 | 20.0 | 20.0 |
| Total Split（s） | 11.0 | 21.0 |  | 11.0 | 21.0 |  | 16.0 | 42.0 | 42.0 | 16.0 | 42.0 | 42.0 |
| Total Split（\％） | 12．2\％ | 23．3\％ |  | 12．2\％ | 23．3\％ |  | 17．8\％ | 46．7\％ | 46．7\％ | 17．8\％ | 46．7\％ | 46．7\％ |
| Yellow Time（s） | 3.0 | 5.0 |  | 3.0 | 5.0 |  | 3.0 | 4.5 | 4.5 | 3.0 | 4.5 | 4.5 |
| All－Red Time（s） | 3.0 | 2.0 |  | 3.0 | 2.0 |  | 3.0 | 2.0 | 2.0 | 3.0 | 2.0 | 2.0 |
| Lost Time Adjust（s） | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） | 6.0 | 7.0 |  | 6.0 | 7.0 |  | 6.0 | 6.5 | 6.5 | 6.0 | 6.5 | 6.5 |
| Lead／Lag | Lead | Lag |  | Lead | Lag |  | Lead | Lag | Lag | Lead | Lag | Lag |
| Lead－Lag Optimize？ | Yes | Yes |  | Yes | Yes |  | Yes | Yes | Yes | Yes | Yes | Yes |
| Recall Mode | None | C－Max |  | None | C－Max |  | None | None | None | None | None | None |
| Act Effct Green（s） | 30.7 | 25.6 | 90.0 | 31.1 | 25.8 | 90.0 | 9.9 | 27.3 | 27.3 | 37.3 | 27.1 | 27.1 |
| Actuated g／C Ratio | 0.34 | 0.28 | 1.00 | 0.35 | 0.29 | 1.00 | 0.11 | 0.30 | 0.30 | 0.41 | 0.30 | 0.30 |
| v／c Ratio | 0.07 | 0.53 | 0.64 | 0.13 | 0.28 | 0.16 | 0.75 | 0.59 | 0.05 | 0.70 | 0.70 | 0.07 |
| Control Delay | 17.9 | 29.3 | 4.4 | 21.0 | 29.1 | 0.2 | 52.2 | 27.9 | 0.2 | 25.9 | 30.2 | 0.2 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 17.9 | 29.3 | 4.4 | 21.0 | 29.1 | 0.2 | 52.2 | 27.9 | 0.2 | 25.9 | 30.2 | 0.2 |
| LOS | B | C | A | C | C | A | D | C | A | C | C | A |
| Approach Delay |  | 13.0 |  |  | 15.9 |  |  | 32.8 |  |  | 28.6 |  |
| Approach LOS |  | B |  |  | B |  |  | C |  |  | C |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

Cycle Length： 90
Actuated Cycle Length： 90
Offset： $71(79 \%)$ ，Referenced to phase 2：EBTL and 6 ：WBTL，Start of FDW or yellow
Natural Cycle： 65
Control Type：Actuated－Coordinated
Maximum v／c Ratio： 0.75
Intersection Signal Delay： 22.9
Intersection LOS：C
Intersection Capacity Utilization 69．1\％
ICU Level of Service C
Analysis Period（min） 15
Splits and Phases：10：US 24 \＆Meridian Rd




|  | 4 |  |  |  |  |  | 4 |  |  |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \％${ }^{1 / 1}$ | 个4 | F＇ | \％${ }^{1 / 1}$ | 性 | F | \％${ }^{1 / 1}$ | 性 | F | \％＊ | 性 | 7 |
| Trafic Volume（vph） | 785 | 659 | 376 | 223 | 595 | 249 | 463 | 896 | 197 | 459 | 713 | 602 |
| Future Volume（vph） | 785 | 659 | 376 | 223 | 595 | 249 | 463 | 896 | 197 | 459 | 713 | 602 |
| Turn Type | Prot | NA | Free | Prot | NA | Perm | Prot | NA | Free | Prot | NA | Free |
| Protected Phases | 7 | 4 |  | 3 | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Permitted Phases |  |  | Free |  |  | 8 |  |  | Free |  |  | Free |
| Detector Phase | 7 | 4 |  | 3 | 8 | 8 | 5 | 2 |  | 1 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 5.0 | 15.0 |  | 5.0 | 15.0 | 15.0 | 5.0 | 15.0 |  | 5.0 | 15.0 |  |
| Minimum Split（s） | 12.5 | 22.0 |  | 12.5 | 22.0 | 22.0 | 13.5 | 22.0 |  | 13.5 | 22.0 |  |
| Total Split（s） | 32.0 | 43.0 |  | 18.0 | 29.0 | 29.0 | 23.0 | 36.0 |  | 23.0 | 36.0 |  |
| Total Split（\％） | 26．7\％ | 35．8\％ |  | 15．0\％ | 24．2\％ | 24．2\％ | 19．2\％ | 30．0\％ |  | 19．2\％ | 30．0\％ |  |
| Yellow Time（s） | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| All－Red Time（s） | 2.0 | 2.0 |  | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |  | 2.0 | 2.0 |  |
| Lost Time Adjust（s） | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time（s） | 5.0 | 5.0 |  | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |  | 5.0 | 5.0 |  |
| Lead／Lag | Lead | Lag |  | Lead | Lag | Lag | Lead | Lag |  | Lead | Lag |  |
| Lead－Lag Optimize？ | Yes | Yes |  | Yes | Yes | Yes | Yes | Yes |  | Yes | Yes |  |
| Recall Mode | None | None |  | None | None | None | None | C－Max |  | None | C－Max |  |
| Act Effct Green（s） | 27.0 | 38.5 | 120.0 | 12.1 | 23.6 | 23.6 | 18.1 | 31.3 | 120.0 | 18.1 | 31.3 | 120.0 |
| Actuated g／C Ratio | 0.22 | 0.32 | 1.00 | 0.10 | 0.20 | 0.20 | 0.15 | 0.26 | 1.00 | 0.15 | 0.26 | 1.00 |
| $\mathrm{v} / \mathrm{C}$ Ratio | 1.06 | 0.60 | 0.25 | 0.67 | 0.89 | 0.50 | 0.93 | 1.01 | 0.13 | 0.93 | 0.81 | 0.40 |
| Control Delay | 94.0 | 37.2 | 0.4 | 78.1 | 51.7 | 11.8 | 76.2 | 76.3 | 0.2 | 75.5 | 49.5 | 0.7 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 94.0 | 37.2 | 0.4 | 78.1 | 51.7 | 11.8 | 76.2 | 76.3 | 0.2 | 75.5 | 49.5 | 0.7 |
| LOS | F | D | A | E | D | B | E | E | A | E | D | A |
| Approach Delay |  | 54.1 |  |  | 47.9 |  |  | 66.7 |  |  | 39.7 |  |
| Approach LOS |  | D |  |  | D |  |  | E |  |  | D |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length： 120 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length： 120 |  |  |  |  |  |  |  |  |  |  |  |  |
| Offset： $0(0 \%)$ ，Referenced to phase 2：NBT and 6：SBT，Start of FDW or yellow，Master Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle： 110 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type：Actuated－Coordinated |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v／c Ratio： 1.06 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay： 52.1 |  |  |  | Intersection LOS：D |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 93．4\％ |  |  |  | ICU Level of Service F |  |  |  |  |  |  |  |  |
| Analysis Period（min） 15 |  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases：7：Meridian Rd \＆Woodmen Rd



Splits and Phases: 8: McLaughlin Rd \& Woodmen Rd



|  | $\rangle$ |  |  |  |  |  | 4 | $\uparrow$ | $p$ |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \％ | 性 | 「 | \％ | 性 | 「 | \％${ }^{1+1}$ | 个快 | F | ＊ | 个忡 | F |
| Traffic Volume（vph） | 80 | 350 | 425 | 60 | 500 | 235 | 825 | 1757 | 80 | 170 | 1152 | 60 |
| Future Volume（vph） | 80 | 350 | 425 | 60 | 500 | 235 | 825 | 1757 | 80 | 170 | 1152 | 60 |
| Turn Type | pm＋pt | NA | Free | pm＋pt | NA | Free | Prot | NA | Perm | pm＋pt | NA | Perm |
| Protected Phases | 5 | 2 |  | 1 | 6 |  | 3 | 8 |  | 7 | 4 |  |
| Permitted Phases | 2 |  | Free | 6 |  | Free |  |  | 8 | 4 |  | 4 |
| Detector Phase | 5 | 2 |  | 1 | 6 |  | 3 | 8 | 8 | 7 | 4 | 4 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 5.0 | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Minimum Split（s） | 11.0 | 20.0 |  | 11.0 | 20.0 |  | 11.0 | 20.0 | 20.0 | 11.0 | 20.0 | 20.0 |
| Total Split（s） | 11.0 | 21.0 |  | 11.0 | 21.0 |  | 28.0 | 42.0 | 42.0 | 16.0 | 30.0 | 30.0 |
| Total Split（\％） | 12．2\％ | 23．3\％ |  | 12．2\％ | 23．3\％ |  | 31．1\％ | 46．7\％ | 46．7\％ | 17．8\％ | 33．3\％ | 33．3\％ |
| Yellow Time（s） | 3.0 | 5.0 |  | 3.0 | 5.0 |  | 3.0 | 4.5 | 4.5 | 3.0 | 4.5 | 4.5 |
| All－Red Time（s） | 3.0 | 2.0 |  | 3.0 | 2.0 |  | 3.0 | 2.0 | 2.0 | 3.0 | 2.0 | 2.0 |
| Lost Time Adjust（s） | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） | 6.0 | 7.0 |  | 6.0 | 7.0 |  | 6.0 | 6.5 | 6.5 | 6.0 | 6.5 | 6.5 |
| Lead／Lag | Lead | Lag |  | Lead | Lag |  | Lead | Lag | Lag | Lead | Lag | Lag |
| Lead－Lag Optimize？ | Yes | Yes |  | Yes | Yes |  | Yes | Yes | Yes | Yes | Yes | Yes |
| Recall Mode | None | C－Max |  | None | C－Max |  | None | None | None | None | None | None |
| Act Effct Green（s） | 21.2 | 16.2 | 90.0 | 21.2 | 16.2 | 90.0 | 22.0 | 36.3 | 36.3 | 33.2 | 23.5 | 23.5 |
| Actuated g／C Ratio | 0.24 | 0.18 | 1.00 | 0.24 | 0.18 | 1.00 | 0.24 | 0.40 | 0.40 | 0.37 | 0.26 | 0.26 |
| v／c Ratio | 0.45 | 0.58 | 0.29 | 0.26 | 0.84 | 0.16 | 1.05 | 0.91 | 0.11 | 0.68 | 0.92 | 0.10 |
| Control Delay | 28.2 | 32.9 | 0.8 | 26.7 | 50.4 | 0.2 | 78.5 | 33.7 | 0.3 | 31.3 | 45.3 | 0.3 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 28.2 | 32.9 | 0.8 | 26.7 | 50.4 | 0.2 | 78.5 | 33.7 | 0.3 | 31.3 | 45.3 | 0.3 |
| LOS | C | C | A | C | D | A | E | C | A | C | D | A |
| Approach Delay |  | 16.5 |  |  | 33.8 |  |  | 46.6 |  |  | 41.6 |  |
| Approach LOS |  | B |  |  | C |  |  | D |  |  | D |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

Cycle Length： 90
Actuated Cycle Length： 90
Offset： $71(79 \%)$ ，Referenced to phase 2：EBTL and 6 ：WBTL，Start of FDW or yellow
Natural Cycle： 90
Control Type：Actuated－Coordinated
Maximum v／c Ratio： 1.05
Intersection Signal Delay： $39.1 \quad$ Intersection LOS：D
Intersection Capacity Utilization 85．3\％ ICU Level of Service E
Analysis Period（min） 15
Splits and Phases：10：US 24 \＆Meridian Rd






## MOVEMENT FLOWS FOR SITE (INPUT)

Approach movement input flow rates (veh/h)

## All Movement Classes

- Site: 2 [2043 Total AM - Single Southeastbound Approach (Site

Folder: General)]
Woodmen/Retail Row

Site Category: 2043 Total AM
Roundabout

Use the button below to open or close all popup boxes. Click value labels to open selected ones.
Click and drag popup boxes to move to preferred positions.

## Close All Popups



## LANE SUMMARY

$\nabla$ Site: 2 [2043 Total AM - Single Southeastbound Approach (Site<br>Folder: General)]

Woodmen/Retail Row
Site Category: 2043 Total AM
Roundabout

| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{array}{r} \text { DEM } \\ \text { FLC } \\ \text { [ Total } \\ \text { veh/h } \end{array}$ | $\begin{aligned} & \text { IND } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Cap. <br> veh/h | Deg. Satn v/c | Lane Util. \% | Aver. Delay <br> sec | Level of Service | $\begin{gathered} 95 \% \\ \text { Q } \\ \text { [ Veh } \end{gathered}$ | $\begin{gathered} \hline \mathrm{K} \text { OF } \\ \text { JE } \\ \text { Dist ] } \\ \text { ft } \end{gathered}$ | Lane Config | Lane Length <br> ft | Cap. Adj. \% | Prob. Block. $\qquad$ |
| NorthEast: Retail Row ST |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 132 | 2.0 | 1163 | 0.113 | 100 | 4.1 | LOS A | 0.5 | 12.8 | Full | 1600 | 0.0 | 0.0 |
| Approach | 132 | 2.0 |  | 0.113 |  | 4.1 | LOS A | 0.5 | 12.8 |  |  |  |  |
| NorthWest: Woodmen Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 253 | 2.0 | 1335 | 0.190 | 100 | 4.3 | LOS A | 1.0 | 24.2 | Full | 1600 | 0.0 | 0.0 |
| Approach | 253 | 2.0 |  | 0.190 |  | 4.3 | LOS A | 1.0 | 24.2 |  |  |  |  |
| SouthWest: Retail Row St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 401 | 2.0 | 1197 | 0.335 | 100 | 6.2 | LOS A | 1.9 | 48.5 | Full | 1600 | 0.0 | 0.0 |
| Approach | 401 | 2.0 |  | 0.335 |  | 6.2 | LOS A | 1.9 | 48.5 |  |  |  |  |
| Intersection | 786 | 2.0 |  | 0.335 |  | 5.2 | LOS A | 1.9 | 48.5 |  |  |  |  |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: Same as Sign Control.
Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.
LOS F will result if v/c > 1 irrespective of lane delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 6).
Roundabout Capacity Model: US HCM 6.
Delay Model: HCM Delay Formula (Geometric Delay is not included).
Queue Model: HCM Queue Formula.
Gap-Acceptance Capacity: Traditional M1.
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
d Dominant lane on roundabout approach

SIDRA INTERSECTION 9.0 | Copyright © 2000-2020 Akcelik and Associates Pty Ltd | sidrasolutions.com
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Project: G:IShared drives\CS Engineering - 2019-currentl2020\204120 - FalconField Prelim Plan\Sidra\2020-06-JunelWoodmen \& Retail Row St single sb approach.sip9

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 2.6 |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations | i | 4 | $\boldsymbol{F}$ |  | Y |  |
| Traffic Vol, veh/h | 45 | 67 | 90 | 0 | 0 | 30 |
| Future Vol, veh/h | 45 | 67 | 90 | 0 | 0 | 30 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 120 | - | - | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 49 | 73 | 98 | 0 | 0 | 33 |


| Major/Minor M | Major1 |  | Major2 |  | Minor2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 98 | 0 | - | 0 | 269 | 98 |
| Stage 1 | - | - | - | - | 98 | - |
| Stage 2 | - | - | - | - | 171 | - |
| Critical Hdwy | 4.12 | - | - | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |
| Follow-up Hdwy | 2.218 | - | - | - | 3.518 | 3.318 |
| Pot Cap-1 Maneuver | 1495 | - | - | - | 720 | 958 |
| Stage 1 | - | - | - | - | 926 | - |
| Stage 2 | - | - | - | - | 859 | - |
| Platoon blocked, \% |  | - | - | - |  |  |
| Mov Cap-1 Maneuver | 1495 | - | - | - | 696 | 958 |
| Mov Cap-2 Maneuver | - | - | - | - | 696 | - |
| Stage 1 | - | - | - | - | 895 | - |
| Stage 2 | - | - | - | - | 859 | - |
|  |  |  |  |  |  |  |
| Approach | EB |  | WB |  | SB |  |
| HCM Control Delay, s | 3 |  | 0 |  | 8.9 |  |
| HCM LOS |  |  |  |  | A |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | EBL EBT WBT WBR SBLn1 |  |  |  |  |
| Capacity (veh/h) |  | 1495 |  | - | - | 958 |
| HCM Lane V/C Ratio |  | 0.033 | - | - | - | 0.034 |
| HCM Control Delay (s) |  | 7.5 | - | - | - | 8.9 |
| HCM Lane LOS |  | A | - | - | - | A |
| HCM 95th \%tile Q(veh) |  | 0.1 | - | - | - | 0.1 |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 1.8 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | $\uparrow$ |  |  | $\uparrow$ | Mr |  |
| Traffic Vol, veh/h | 55 | 10 | 0 | 64 | 30 | 1 |
| Future Vol, veh/h | 55 | 10 | 0 | 64 | 30 | 1 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 60 | 11 | 0 | 70 | 33 | 1 |


| Major/Minor | Major1 |  | Major2 |  | Minor1 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 0 | 0 | 71 | 0 | 136 | 66 |
| Stage 1 | - | - | - | - | 66 | - |
| Stage 2 | - | - | - | - | 70 | - |
| Critical Hdwy | - | - | 4.12 | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |
| Follow-up Hdwy | - | - | 2.218 | - | 3.518 | 3.318 |
| Pot Cap-1 Maneuver | - | - | 1529 | - | 857 | 998 |
| Stage 1 | - | - | - | - | 957 | - |
| Stage 2 | - | - | - | - | 953 | - |
| Platoon blocked, \% | - | - |  | - |  |  |
| Mov Cap-1 Maneuver | - | - | 1529 | - | 857 | 998 |
| Mov Cap-2 Maneuver | - | - | - | - | 857 | - |
| Stage 1 | - | - | - | - | 957 | - |
| Stage 2 | - | - | - | - | 953 | - |
|  |  |  |  |  |  |  |
| Approach | EB |  | WB |  | NB |  |
| HCM Control Delay, s | 0 |  | 0 |  | 9.4 |  |
| HCM LOS |  |  |  |  | A |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NBLn1 | EBT | EBR | - WBL WBT |  |
| Capacity (veh/h) |  | 861 | - | - |  |  |
| HCM Lane V/C Ratio |  | 0.039 | - | - | - | - |
| HCM Control Delay (s) |  | 9.4 | - | - | 0 | - |
| HCM Lane LOS |  | A | - | - | A | - |
| HCM 95th \%tile Q(veh) |  | 0.1 | - | - | 0 | - |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.7 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | $\uparrow$ |  |  | $\mathbf{7}$ | Mr |  |
| Traffic Vol, veh/h | 54 | 2 | 1 | 57 | 7 | 2 |
| Future Vol, veh/h | 54 | 2 | 1 | 57 | 7 | 2 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 59 | 2 | 1 | 62 | 8 | 2 |




Splits and Phases: 7: Meridian Rd \& Woodmen Rd


|  | $\stackrel{ }{*}$ |  |  |  |  |  | 4 | $\dagger$ | 7 |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \％ | 个4 | 「 | \％ | 个 $\uparrow$ | F | \％ | $\uparrow$ | F | \％ | 4 | F |
| Trafic Volume（vph） | 100 | 680 | 100 | 50 | 790 | 159 | 75 | 50 | 50 | 134 | 125 | 300 |
| Future Volume（vph） | 100 | 680 | 100 | 50 | 790 | 159 | 75 | 50 | 50 | 134 | 125 | 300 |
| Turn Type | pm＋pt | NA | Perm | pm＋pt | NA | Perm | pm＋pt | NA | Perm | pm＋pt | NA | Perm |
| Protected Phases | 5 | 2 |  | 1 | 6 |  | 3 | 8 |  | 7 | 4 |  |
| Permitted Phases | 2 |  | 2 | 6 |  | 6 | 8 |  | 8 | 4 |  | 4 |
| Detector Phase | 5 | 2 | 2 | 1 | 6 | 6 | 3 | 8 | 8 | 7 | 4 | 4 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Minimum Split（s） | 12.5 | 25.0 | 25.0 | 12.5 | 25.0 | 25.0 | 13.5 | 25.0 | 25.0 | 13.5 | 25.0 | 25.0 |
| Total Split（s） | 14.0 | 37.0 | 37.0 | 14.0 | 37.0 | 37.0 | 14.0 | 25.0 | 25.0 | 14.0 | 25.0 | 25.0 |
| Total Split（\％） | 15．6\％ | 41．1\％ | 41．1\％ | 15．6\％ | 41．1\％ | 41．1\％ | 15．6\％ | 27．8\％ | 27．8\％ | 15．6\％ | 27．8\％ | 27．8\％ |
| Yellow Time（s） | 4.0 | 5.0 | 5.0 | 4.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| All－Red Time（s） | 3.5 | 2.0 | 2.0 | 3.5 | 2.0 | 2.0 | 3.5 | 2.0 | 2.0 | 3.5 | 2.0 | 2.0 |
| Lost Time Adjust（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） | 7.5 | 7.0 | 7.0 | 7.5 | 7.0 | 7.0 | 8.5 | 7.0 | 7.0 | 8.5 | 7.0 | 7.0 |
| Lead／Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | Lag |
| Lead－Lag Optimize？ | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Recall Mode | None | C－Max | C－Max | None | C－Max | C－Max | None | Max | Max | None | Max | Max |
| Act Effct Green（s） | 39.0 | 35.6 | 35.6 | 37.4 | 32.8 | 32.8 | 22.0 | 18.0 | 18.0 | 23.7 | 20.8 | 20.8 |
| Actuated g／C Ratio | 0.43 | 0.40 | 0.40 | 0.42 | 0.36 | 0.36 | 0.24 | 0.20 | 0.20 | 0.26 | 0.23 | 0.23 |
| v／c Ratio | 0.39 | 0.50 | 0.13 | 0.16 | 0.63 | 0.22 | 0.23 | 0.14 | 0.10 | 0.37 | 0.30 | 0.52 |
| Control Delay | 17.7 | 23.4 | 0.3 | 14.0 | 27.2 | 1.3 | 22.9 | 30.8 | 0.4 | 26.3 | 32.7 | 8.9 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 17.7 | 23.4 | 0.3 | 14.0 | 27.2 | 1.3 | 22.9 | 30.8 | 0.4 | 26.3 | 32.7 | 8.9 |
| LOS | B | C | A | B | C | A | C | C | A | C | C | A |
| Approach Delay |  | 20.1 |  |  | 22.4 |  |  | 18.8 |  |  | 18.4 |  |
| Approach LOS |  | C |  |  | C |  |  | B |  |  | B |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

Cycle Length： 90
Actuated Cycle Length： 90
Offset： $0(0 \%)$ ，Referenced to phase 2：EBTL and 6：WBTL，Start of Green
Natural Cycle： 80
Control Type：Actuated－Coordinated
Maximum v／c Ratio： 0.63
Intersection Signal Delay： 20.5 Intersection LOS：C
Intersection Capacity Utilization 62．7\％
ICU Level of Service B
Analysis Period（min） 15
Splits and Phases：8：McLaughlin Rd \＆Woodmen Rd


|  | $\Rightarrow$ |  |  |  |  |  |  | 4 |  |  | $\frac{1}{7}$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \％${ }^{\text {\％}}$ | $\uparrow$ | F | \％ | 性 | F | \％${ }^{*}$ | 率 | F | ${ }^{7}$ | 坐虫 | F |
| Traffic Volume（vph） | 372 | 145 | 347 | 70 | 118 | 54 | 399 | 744 | 40 | 72 | 917 | 482 |
| Future Volume（vph） | 372 | 145 | 347 | 70 | 118 | 54 | 399 | 744 | 40 | 72 | 917 | 482 |
| Turn Type | Prot | NA | Free | pm＋pt | NA | Free | Prot | NA | Perm | pm＋pt | NA | Free |
| Protected Phases | 7 | 4 |  | 3 | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Permitted Phases |  |  | Free | 8 |  | Free |  |  | 2 | 6 |  | Free |
| Detector Phase | 7 | 4 |  | 3 | 8 |  | 5 | 2 | 2 | 1 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 20.0 | 15.0 |  | 5.0 | 15.0 |  | 5.0 | 15.0 | 15.0 | 5.0 | 15.0 |  |
| Minimum Split（s） | 25.0 | 23.0 |  | 10.0 | 23.0 |  | 10.0 | 23.0 | 23.0 | 10.0 | 23.0 |  |
| Total Split（s） | 27.0 | 37.0 |  | 15.0 | 25.0 |  | 20.0 | 58.0 | 58.0 | 10.0 | 48.0 |  |
| Total Split（\％） | 22．5\％ | 30．8\％ |  | 12．5\％ | 20．8\％ |  | 16．7\％ | 48．3\％ | 48．3\％ | 8．3\％ | 40．0\％ |  |
| Yellow Time（s） | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  |
| All－Red Time（s） | 2.0 | 2.0 |  | 2.0 | 2.0 |  | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |  |
| Lost Time Adjust（s） | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |
| Total Lost Time（s） | 5.0 | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |  |
| Lead／Lag | Lead | Lag |  | Lead | Lag |  | Lead | Lag | Lag | Lead | Lag |  |
| Lead－Lag Optimize？ | Yes | Yes |  | Yes | Yes |  | Yes | Yes | Yes | Yes | Yes |  |
| Recall Mode | None | None |  | None | None |  | None | C－Max | C－Max | None | C－Max |  |
| Act Effct Green（s） | 20.6 | 29.3 | 120.0 | 23.5 | 15.0 | 120.0 | 20.7 | 58.8 | 58.8 | 51.5 | 43.7 | 120.0 |
| Actuated g／C Ratio | 0.17 | 0.24 | 1.00 | 0.20 | 0.12 | 1.00 | 0.17 | 0.49 | 0.49 | 0.43 | 0.36 | 1.00 |
| V／c Ratio | 0.67 | 0.34 | 0.23 | 0.27 | 0.29 | 0.04 | 0.72 | 0.32 | 0.05 | 0.22 | 0.53 | 0.32 |
| Control Delay | 52.8 | 41.4 | 0.3 | 31.1 | 49.6 | 0.0 | 54.5 | 19.7 | 0.1 | 14.4 | 31.4 | 0.5 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 52.8 | 41.4 | 0.3 | 31.1 | 49.6 | 0.0 | 54.5 | 19.7 | 0.1 | 14.4 | 31.4 | 0.5 |
| LOS | D | D | A | C | D | A | D | B | A | B | C | A |
| Approach Delay |  | 29.8 |  |  | 33.3 |  |  | 30.8 |  |  | 20.5 |  |
| Approach LOS |  | C |  |  | C |  |  | C |  |  | C |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length： 120 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length： 120 |  |  |  |  |  |  |  |  |  |  |  |  |
| Offset： $0(0 \%)$ ，Referenced to phase 2：NBT and 6：SBTL，Start of Green |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle： 85 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type：Actuated－Coordinated |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v／c Ratio： 0.72 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay： 26.7 |  |  |  | Intersection LOS：C |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 70．8\％ |  |  |  | ICU Level of Service C |  |  |  |  |  |  |  |  |
| Analysis Period（min） 15 |  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases：9：US 24 \＆Woodmen Rd


|  | $\rangle$ |  |  |  |  |  | 4 | 4 | $p$ |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \％ | 个 $\uparrow$ | 「 | \％ | 个 $\uparrow$ | 「 | \％${ }^{1+1}$ | 个4ヶ | F | \％ | 性 | F |
| Traffic Volume（vph） | 30 | 524 | 991 | 40 | 273 | 247 | 272 | 906 | 30 | 216 | 1093 | 40 |
| Future Volume（vph） | 30 | 524 | 991 | 40 | 273 | 247 | 272 | 906 | 30 | 216 | 1093 | 40 |
| Turn Type | pm＋pt | NA | Free | pm＋pt | NA | Free | Prot | NA | Perm | pm＋pt | NA | Perm |
| Protected Phases | 5 | 2 |  | 1 | 6 |  | 3 | 8 |  | 7 | 4 |  |
| Permitted Phases | 2 |  | Free | 6 |  | Free |  |  | 8 | 4 |  | 4 |
| Detector Phase | 5 | 2 |  | 1 | 6 |  | 3 | 8 | 8 | 7 | 4 | 4 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 5.0 | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Minimum Split（s） | 11.0 | 20.0 |  | 11.0 | 20.0 |  | 11.0 | 20.0 | 20.0 | 11.0 | 20.0 | 20.0 |
| Total Split（s） | 11.0 | 21.0 |  | 11.0 | 21.0 |  | 16.0 | 42.0 | 42.0 | 16.0 | 42.0 | 42.0 |
| Total Split（\％） | 12．2\％ | 23．3\％ |  | 12．2\％ | 23．3\％ |  | 17．8\％ | 46．7\％ | 46．7\％ | 17．8\％ | 46．7\％ | 46．7\％ |
| Yellow Time（s） | 3.0 | 5.0 |  | 3.0 | 5.0 |  | 3.0 | 4.5 | 4.5 | 3.0 | 4.5 | 4.5 |
| All－Red Time（s） | 3.0 | 2.0 |  | 3.0 | 2.0 |  | 3.0 | 2.0 | 2.0 | 3.0 | 2.0 | 2.0 |
| Lost Time Adjust（s） | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） | 6.0 | 7.0 |  | 6.0 | 7.0 |  | 6.0 | 6.5 | 6.5 | 6.0 | 6.5 | 6.5 |
| Lead／Lag | Lead | Lag |  | Lead | Lag |  | Lead | Lag | Lag | Lead | Lag | Lag |
| Lead－Lag Optimize？ | Yes | Yes |  | Yes | Yes |  | Yes | Yes | Yes | Yes | Yes | Yes |
| Recall Mode | None | C－Max |  | None | C－Max |  | None | None | None | None | None | None |
| Act Effct Green（s） | 29.7 | 24.7 | 90.0 | 30.1 | 24.8 | 90.0 | 9.9 | 28.3 | 28.3 | 38.4 | 28.1 | 28.1 |
| Actuated g／C Ratio | 0.33 | 0.27 | 1.00 | 0.33 | 0.28 | 1.00 | 0.11 | 0.31 | 0.31 | 0.43 | 0.31 | 0.31 |
| V／c Ratio | 0.08 | 0.55 | 0.64 | 0.14 | 0.29 | 0.16 | 0.74 | 0.58 | 0.05 | 0.69 | 0.70 | 0.07 |
| Control Delay | 18.5 | 30.2 | 4.3 | 21.8 | 29.8 | 0.2 | 51.8 | 27.0 | 0.1 | 24.8 | 29.5 | 0.2 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 18.5 | 30.2 | 4.3 | 21.8 | 29.8 | 0.2 | 51.8 | 27.0 | 0.1 | 24.8 | 29.5 | 0.2 |
| LOS | B | C | A | C | C | A | D | C | A | C | C | A |
| Approach Delay |  | 13.4 |  |  | 16.2 |  |  | 31.9 |  |  | 27.8 |  |
| Approach LOS |  | B |  |  | B |  |  | C |  |  | C |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

Cycle Length： 90
Actuated Cycle Length： 90
Offset： $71(79 \%)$ ，Referenced to phase 2：EBTL and 6 ：WBTL，Start of FDW or yellow
Natural Cycle： 65
Control Type：Actuated－Coordinated
Maximum v／c Ratio： 0.74
Intersection Signal Delay： 22.7
Intersection LOS：C
Intersection Capacity Utilization 69．4\％
ICU Level of Service C
Analysis Period（min） 15
Splits and Phases：10：US 24 \＆Meridian Rd








## MOVEMENT FLOWS FOR SITE (INPUT)

Approach movement input flow rates (veh/h)

## All Movement Classes

$\nabla$ Site: 2 [2043 Total PM - Single Southeastbound Approach Copy (Site Folder: General)]

Woodmen/Retail Row
Site Category: 2043 Total PM
Roundabout

Use the button below to open or close all popup boxes. Click value labels to open selected ones.
Click and drag popup boxes to move to preferred positions.

## Close All Popups



## LANE SUMMARY

$\square$ Site: 2 [2043 Total PM - Single Southeastbound Approach -
Copy (Site Folder: General)]
Woodmen/Retail Row
Site Category: 2043 Total PM
Roundabout

| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{aligned} & \text { ND } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \\ & \hline \end{aligned}$ | Cap. <br> veh/h | Deg. Satn v/c | Lane Util. \% | Aver. Delay sec | Level of Service | $\begin{gathered} 95 \% \\ \text { Q } \\ \text { [ Veh } \end{gathered}$ | $\begin{aligned} & \mathrm{K} \text { OF } \\ & \mathrm{JE} \\ & \text { Dist ] } \\ & \mathrm{ft} \end{aligned}$ | Lane Config | Lane Length ft | Cap. Adj. \% | Prob. Block. \% |
| NorthEast: Retail Row ST |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 255 | 2.0 | 908 | 0.281 | 100 | 6.9 | LOS A | 1.3 | 34.0 | Full | 1600 | 0.0 | 0.0 |
| Approach | 255 | 2.0 |  | 0.281 |  | 6.9 | LOS A | 1.3 | 34.0 |  |  |  |  |
| NorthWest: Woodmen Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 577 | 2.0 | 1315 | 0.439 | 100 | 7.1 | LOS A | 3.1 | 78.5 | Full | 1600 | 0.0 | 0.0 |
| Approach | 577 | 2.0 |  | 0.439 |  | 7.1 | LOS A | 3.1 | 78.5 |  |  |  |  |
| SouthWest: Retail Row St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 409 | 2.0 | 1053 | 0.388 | 100 | 7.5 | LOS A | 2.2 | 55.5 | Full | 1600 | 0.0 | 0.0 |
| Approach | 409 | 2.0 |  | 0.388 |  | 7.5 | LOS A | 2.2 | 55.5 |  |  |  |  |
| Intersection | 1241 | 2.0 |  | 0.439 |  | 7.2 | LOS A | 3.1 | 78.5 |  |  |  |  |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: Same as Sign Control.
Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.
LOS F will result if v/c>1 irrespective of lane delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 6).
Roundabout Capacity Model: US HCM 6.
Delay Model: HCM Delay Formula (Geometric Delay is not included).
Queue Model: HCM Queue Formula.
Gap-Acceptance Capacity: Traditional M1.
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
d Dominant lane on roundabout approach

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Project: G:IShared drives\CS Engineering - 2019-currentl2020\204120 - FalconField Prelim Plan\Sidral2020-06-JunelWoodmen \& Retail Row St single sb approach.sip9

| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 4 |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations | ${ }^{7}$ | 4 | $\uparrow$ |  | M |  |
| Traffic Vol, veh/h | 105 | 139 | 121 | 1 | 1 | 113 |
| Future Vol, veh/h | 105 | 139 | 121 | 1 | 1 | 113 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control F | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 120 | - | - | - | 0 | - |
| Veh in Median Storage, \# | \# | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 114 | 151 | 132 | 1 | 1 | 123 |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.5 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | $\uparrow$ |  |  | $\uparrow$ | M |  |
| Traffic Vol, veh/h | 113 | 31 | 1 | 107 | 13 | 0 |
| Future Vol, veh/h | 113 | 31 | 1 | 107 | 13 | 0 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 123 | 34 | 1 | 116 | 14 | 0 |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.2 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | $\uparrow$ |  |  | -1 | M |  |
| Traffic Vol, veh/h | 106 | 7 | 2 | 105 | 3 | 1 |
| Future Vol, veh/h | 106 | 7 | 2 | 105 | 3 | 1 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 115 | 8 | 2 | 114 | 3 | 1 |


| Major/Minor | Major1 | Major2 |  |  | Minor1 |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Conflicting Flow All | 0 | 0 | 123 | 0 | 237 | 119 |
| $\quad$ Stage 1 | - | - | - | - | 119 | - |
| $\quad$ Stage 2 | - | - | - | - | 118 | - |
| Critical Hdwy | - | - | 4.12 | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |
| Follow-up Hdwy | - | -2.218 | - | 3.518 | 3.318 |  |
| Pot Cap-1 Maneuver | - | - | 1464 | - | 751 | 933 |
| $\quad$ Stage 1 | - | - | - | - | 906 | - |
| Stage 2 | - | - | - | - | 907 | - |
| Platoon blocked, \% | - | - |  | - |  |  |
| Mov Cap-1 Maneuver | - | - | 1464 | - | 750 | 933 |
| Mov Cap-2 Maneuver | - | - | - | - | 750 | - |
| Stage 1 | - | - | - | - | 906 | - |
| Stage 2 | - | - | - | - | 906 | - |


| Approach | EB | WB | NB |
| :--- | :---: | :---: | :---: |
| HCM Control Delay, s | 0 | 0.1 | 9.6 |
| HCM LOS |  | A |  |


| Minor Lane/Major Mvmt | NBLn1 | EBT | EBR | WBL | WBT |
| :--- | ---: | ---: | ---: | ---: | :---: |
| Capacity (veh/h) | 789 | - | -1464 | - |  |
| HCM Lane V/C Ratio | 0.006 | - | -0.001 | - |  |
| HCM Control Delay (s) | 9.6 | - | - | 7.5 | 0 |
| HCM Lane LOS | A | - | - | A | A |
| HCM 95th \%tile Q(veh) | 0 | - | - | 0 | - |



|  | $\rangle$ |  |  |  |  |  |  | $\dagger$ |  |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | 性 | 「 | \％ | 个个 | 「 | \％ | $\uparrow$ | 「 | \％ | $\uparrow$ | F |
| Traffic Volume（vph） | 300 | 957 | 150 | 100 | 800 | 291 | 150 | 200 | 150 | 217 | 150 | 200 |
| Future Volume（vph） | 300 | 957 | 150 | 100 | 800 | 291 | 150 | 200 | 150 | 217 | 150 | 200 |
| Turn Type | pm＋pt | NA | Perm | pm＋pt | NA | Perm | pm＋pt | NA | Perm | pm＋pt | NA | Perm |
| Protected Phases | 5 | 2 |  | 1 | 6 |  | 3 | 8 |  | 7 | 4 |  |
| Permitted Phases | 2 |  | 2 | 6 |  | 6 | 8 |  | 8 | 4 |  | 4 |
| Detector Phase | 5 | 2 | 2 | 1 | 6 | 6 | 3 | 8 | 8 | 7 | 4 | 4 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Minimum Split（s） | 12.5 | 25.0 | 25.0 | 12.5 | 25.0 | 25.0 | 13.5 | 25.0 | 25.0 | 13.5 | 25.0 | 25.0 |
| Total Split（s） | 24.0 | 57.0 | 57.0 | 15.0 | 48.0 | 48.0 | 15.0 | 29.0 | 29.0 | 19.0 | 33.0 | 33.0 |
| Total Split（\％） | 20．0\％ | 47．5\％ | 47．5\％ | 12．5\％ | 40．0\％ | 40．0\％ | 12．5\％ | 24．2\％ | 24．2\％ | 15．8\％ | 27．5\％ | 27．5\％ |
| Yellow Time（s） | 4.0 | 5.0 | 5.0 | 4.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| All－Red Time（s） | 3.5 | 2.0 | 2.0 | 3.5 | 2.0 | 2.0 | 3.5 | 2.0 | 2.0 | 3.5 | 2.0 | 2.0 |
| Lost Time Adjust（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） | 7.5 | 7.0 | 7.0 | 7.5 | 7.0 | 7.0 | 8.5 | 7.0 | 7.0 | 8.5 | 7.0 | 7.0 |
| Lead／Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | Lag |
| Lead－Lag Optimize？ | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Recall Mode | None | C－Max | C－Max | None | C－Max | C－Max | None | Max | Max | None | Max | Max |
| Act Efft Green（s） | 64.4 | 50.2 | 50.2 | 48.4 | 41.6 | 41.6 | 27.0 | 22.0 | 22.0 | 35.0 | 26.0 | 26.0 |
| Actuated g／C Ratio | 0.54 | 0.42 | 0.42 | 0.40 | 0.35 | 0.35 | 0.22 | 0.18 | 0.18 | 0.29 | 0.22 | 0.22 |
| v／c Ratio | 0.86 | 0.67 | 0.20 | 0.44 | 0.67 | 0.40 | 0.51 | 0.60 | 0.31 | 0.73 | 0.38 | 0.38 |
| Control Delay | 55.0 | 51.6 | 15.6 | 27.0 | 42.3 | 12.3 | 39.7 | 53.4 | 1.7 | 48.2 | 43.5 | 4.2 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 55.0 | 51.6 | 15.6 | 27.0 | 42.3 | 12.3 | 39.7 | 53.4 | 1.7 | 48.2 | 43.5 | 4.2 |
| LOS | D | D | B | C | D | B | D | D | A | D | D | A |
| Approach Delay |  | 48.5 |  |  | 33.7 |  |  | 33.7 |  |  | 31.4 |  |
| Approach LOS |  | D |  |  | C |  |  | C |  |  | C |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length： 120 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length： 120 |  |  |  |  |  |  |  |  |  |  |  |  |
| Offset： $118(98 \%)$ ，Referenced to phase 2：EBTL and 6：WBTL，Start of Green |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle： 90 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type：Actuated－Coordinated |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v／c Ratio： 0.86 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay： 39.0 |  |  |  | Intersection LOS：D |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 85．0\％ |  |  |  | ICU Level of Service E |  |  |  |  |  |  |  |  |
| Analysis Period（min） 15 |  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases：8：McLaughlin Rd \＆Woodmen Rd



|  | $\rangle$ |  |  |  |  |  | 4 | 4 | $p$ |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | 个 $\uparrow$ | 「 | \％ | 个 $\uparrow$ | 「 | \％${ }^{1 / 4}$ | 帆 | F | \％ | 性中 | F |
| Traffic Volume（vph） | 80 | 347 | 412 | 60 | 495 | 240 | 804 | 1814 | 80 | 173 | 1185 | 60 |
| Future Volume（vph） | 80 | 347 | 412 | 60 | 495 | 240 | 804 | 1814 | 80 | 173 | 1185 | 60 |
| Turn Type | pm＋pt | NA | Free | pm＋pt | NA | Free | Prot | NA | Perm | pm＋pt | NA | Perm |
| Protected Phases | 5 | 2 |  | 1 | 6 |  | 3 | 8 |  | 7 | 4 |  |
| Permitted Phases | 2 |  | Free | 6 |  | Free |  |  | 8 | 4 |  | 4 |
| Detector Phase | 5 | 2 |  | 1 | 6 |  | 3 | 8 | 8 | 7 | 4 | 4 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 5.0 | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Minimum Split（s） | 11.0 | 20.0 |  | 11.0 | 20.0 |  | 11.0 | 20.0 | 20.0 | 11.0 | 20.0 | 20.0 |
| Total Split（s） | 11.0 | 21.0 |  | 11.0 | 21.0 |  | 28.0 | 42.0 | 42.0 | 16.0 | 30.0 | 30.0 |
| Total Split（\％） | 12．2\％ | 23．3\％ |  | 12．2\％ | 23．3\％ |  | 31．1\％ | 46．7\％ | 46．7\％ | 17．8\％ | 33．3\％ | 33．3\％ |
| Yellow Time（s） | 3.0 | 5.0 |  | 3.0 | 5.0 |  | 3.0 | 4.5 | 4.5 | 3.0 | 4.5 | 4.5 |
| All－Red Time（s） | 3.0 | 2.0 |  | 3.0 | 2.0 |  | 3.0 | 2.0 | 2.0 | 3.0 | 2.0 | 2.0 |
| Lost Time Adjust（s） | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） | 6.0 | 7.0 |  | 6.0 | 7.0 |  | 6.0 | 6.5 | 6.5 | 6.0 | 6.5 | 6.5 |
| Lead／Lag | Lead | Lag |  | Lead | Lag |  | Lead | Lag | Lag | Lead | Lag | Lag |
| Lead－Lag Optimize？ | Yes | Yes |  | Yes | Yes |  | Yes | Yes | Yes | Yes | Yes | Yes |
| Recall Mode | None | C－Max |  | None | C－Max |  | None | None | None | None | None | None |
| Act Effct Green（s） | 21.2 | 16.2 | 90.0 | 21.2 | 16.2 | 90.0 | 22.0 | 36.3 | 36.3 | 33.2 | 23.5 | 23.5 |
| Actuated g／C Ratio | 0.24 | 0.18 | 1.00 | 0.24 | 0.18 | 1.00 | 0.24 | 0.40 | 0.40 | 0.37 | 0.26 | 0.26 |
| V／c Ratio | 0.45 | 0.58 | 0.28 | 0.25 | 0.83 | 0.16 | 1.02 | 0.94 | 0.11 | 0.69 | 0.95 | 0.10 |
| Control Delay | 28.2 | 32.7 | 0.8 | 26.7 | 49.7 | 0.2 | 71.0 | 37.1 | 0.3 | 32.0 | 48.9 | 0.3 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 28.2 | 32.7 | 0.8 | 26.7 | 49.7 | 0.2 | 71.0 | 37.1 | 0.3 | 32.0 | 48.9 | 0.3 |
| LOS | C | C | A | C | D | A | E | D | A | C | D | A |
| Approach Delay |  | 16.6 |  |  | 33.1 |  |  | 46.1 |  |  | 44.8 |  |
| Approach LOS |  | B |  |  | C |  |  | D |  |  | D |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

Cycle Length： 90
Actuated Cycle Length： 90
Offset： $71(79 \%)$ ，Referenced to phase 2：EBTL and 6 ：WBTL，Start of FDW or yellow
Natural Cycle： 90
Control Type：Actuated－Coordinated
Maximum v／c Ratio： 1.02
Intersection Signal Delay： 39.7 Intersection LOS：D

Intersection Capacity Utilization 85．2\％ ICU Level of Service E
Analysis Period（min） 15
Splits and Phases：10：US 24 \＆Meridian Rd




| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.8 |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | M |  |  | $\uparrow$ | F |  |
| Traffic Vol, veh/h | 10 | 8 | 6 | 134 | 114 | 6 |
| Future Vol, veh/h | 10 | 8 | 6 | 134 | 114 | 6 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 11 | 9 | 7 | 146 | 124 | 7 |


| Major/Minor | Minor2 |  | Major1 |  | Major2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 288 | 128 | 131 | 0 | - | 0 |
| Stage 1 | 128 | - | - | - | - | - |
| Stage 2 | 160 | - | - | - | - | - |
| Critical Hdwy | 6.42 | 6.22 | 4.12 | - | - | - |
| Critical Hdwy Stg 1 | 5.42 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - | - |
| Follow-up Hdwy | 3.518 | 3.318 | 2.218 | - | - | - |
| Pot Cap-1 Maneuver | 702 | 922 | 1454 | - | - | - |
| Stage 1 | 898 | - | - | - | - | - |
| Stage 2 | 869 | - | - | - | - | - |
| Platoon blocked, \% |  |  |  | - | - | - |
| Mov Cap-1 Maneuver | 698 | 922 | 1454 | - | - | - |
| Mov Cap-2 Maneuver | 698 | - | - | - | - | - |
| Stage 1 | 894 | - | - | - | - | - |
| Stage 2 | 869 | - | - | - | - | - |
|  |  |  |  |  |  |  |
| Approach | EB |  | NB |  | SB |  |
| HCM Control Delay, s | 9.7 |  | 0.3 |  | 0 |  |
| HCM LOS | A |  |  |  |  |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NBL | NBT EBLn1 |  | SBT | SBR |
| Capacity (veh/h) |  | 1454 | - | 782 | - | - |
| HCM Lane V/C Ratio |  | 0.004 | - | 0.025 | - | - |
| HCM Control Delay (s) |  | 7.5 | 0 | 9.7 | - | - |
| HCM Lane LOS |  | A | A | A | - | - |
| HCM 95th \%tile Q(veh) |  | 0 | - | 0.1 | - | - |

## Queuing Reports

Intersection: 1: Nunbird Ct/Dunlin Heights \& Retail Row St

| Movement | WB | NB | SB |
| :--- | ---: | ---: | ---: |
| Directions Served | L | LTR | LTR |
| Maximum Queue (ft) | 23 | 57 | 44 |
| Average Queue (ft) | 1 | 25 | 15 |
| 95th Queue (ft) | 12 | 50 | 40 |
| Link Distance (ft) |  | 143 | 96 |
| Upstream Blk Time (\%) |  |  |  |
| Queuing Penalty (veh) |  |  |  |
| Storage Bay Dist (ft) | 190 |  |  |
| Storage Blk Time (\%) |  |  |  |

Intersection: 3: Retail Row St \& Jackdaw Point

| Movement | EB | SB |
| :--- | ---: | ---: |
| Directions Served | L | LR |
| Maximum Queue (ft) | 34 | 47 |
| Average Queue (ft) | 3 | 19 |
| 95th Queue (ft) | 21 | 45 |
| Link Distance (ft) |  | 174 |
| Upstream Blk Time (\%) |  |  |
| Queuing Penalty (veh) |  |  |
| Storage Bay Dist (ft) | 120 |  |
| Storage Blk Time (\%) |  |  |
| Queuing Penalty (veh) |  |  |
| Zone Summary |  |  |

Zone wide Queuing Penalty: 0

Intersection: 9: US 24 \& Woodmen Rd

| Movement | EB | EB | EB | WB | WB | WB | NB | NB | NB | NB | NB | NB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | L | L | T | L | T | T | L | L | T | T | T | R |
| Maximum Queue (ft) | 195 | 218 | 222 | 103 | 93 | 117 | 231 | 240 | 162 | 192 | 208 | 25 |
| Average Queue (ft) | 109 | 128 | 97 | 44 | 45 | 52 | 123 | 147 | 57 | 86 | 104 | 1 |
| 95th Queue (ft) | 184 | 200 | 176 | 85 | 85 | 93 | 203 | 218 | 135 | 170 | 185 | 11 |
| Link Distance (ft) |  |  | 643 |  | 452 | 452 |  |  | 2146 | 2146 | 2146 |  |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Storage Bay Dist (ft) | 350 | 350 |  | 260 |  |  | 855 | 855 |  |  |  | 600 |
| Storage Blk Time (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |  |  |  |  |

Intersection: 9: US 24 \& Woodmen Rd

| Movement | B36 | B36 | SB | SB | SB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | T | T | L | T | T | T | R |
| Maximum Queue (ft) | 9 | 14 | 116 | 284 | 270 | 246 | 25 |
| Average Queue (ft) | 0 | 0 | 39 | 188 | 177 | 143 | 1 |
| 95th Queue (ft) | 7 | 10 | 83 | 258 | 252 | 229 | 18 |
| Link Distance (ft) | 539 | 539 |  | 1706 | 1706 | 1706 |  |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  | 700 |  |  | 375 |  |
| Storage Bay Dist (ft) |  |  |  |  |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |
| Zone Summary |  |  |  |  |  |  |  |

Zone wide Queuing Penalty: 0

Intersection: 1: Nunbird Ct/Dunlin Heights \& Retail Row St

| Movement | WB | NB | SB |
| :--- | ---: | ---: | ---: |
| Directions Served | L | LTR | LTR |
| Maximum Queue (ft) | 46 | 31 | 87 |
| Average Queue (ft) | 13 | 14 | 38 |
| 95th Queue (ft) | 39 | 39 | 71 |
| Link Distance (ft) |  | 143 | 96 |
| Upstream Blk Time (\%) |  |  | 0 |
| Queuing Penalty (veh) |  |  | 0 |
| Storage Bay Dist (ft) | 190 |  |  |
| Storage Blk Time (\%) |  |  |  |

Intersection: 3: Retail Row St \& Jackdaw Point

| Movement | EB | SB |
| :--- | ---: | ---: |
| Directions Served | L | LR |
| Maximum Queue (ft) | 36 | 66 |
| Average Queue (ft) | 12 | 35 |
| 95th Queue (ft) | 37 | 58 |
| Link Distance (ft) |  | 174 |
| Upstream Blk Time (\%) |  |  |
| Queuing Penalty (veh) |  |  |
| Storage Bay Dist (ft) | 120 |  |
| Storage Blk Time (\%) |  |  |
| Queuing Penalty (veh) |  |  |

Intersection: 9: US 24 \& Woodmen Rd

| Movement | EB | EB | EB | B31 | WB | WB | WB | NB | NB | NB | NB | NB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | L | T | T | L | T | T | L | L | T | T | T |
| Maximum Queue (ft) | 328 | 339 | 272 | 4 | 137 | 186 | 196 | 243 | 258 | 443 | 476 | 492 |
| Average Queue (ft) | 227 | 243 | 131 | 0 | 51 | 97 | 113 | 112 | 144 | 216 | 261 | 280 |
| 95th Queue (ft) | 309 | 323 | 218 | 3 | 104 | 156 | 171 | 194 | 229 | 355 | 405 | 415 |
| Link Distance (ft) |  |  | 643 | 433 |  | 452 | 452 |  |  | 2146 | 2146 | 2146 |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Storage Bay Dist (ft) | 350 | 350 |  |  | 260 |  |  | 855 | 855 |  |  |  |
| Storage Blk Time (\%) | 0 | 0 |  |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) | 0 | 0 |  |  |  |  |  |  |  |  |  |  |

Intersection: 9: US 24 \& Woodmen Rd

| Movement | NB | B36 | B36 | B36 | SB | SB | SB | SB | SB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | R | T | T | T | L | T | T | T | R |
| Maximum Queue (ft) | 64 | 10 | 11 | 11 | 255 | 392 | 401 | 379 | 95 |
| Average Queue (ft) | 7 | 0 | 0 | 0 | 77 | 259 | 250 | 216 | 3 |
| 95th Queue (ft) | 36 | 8 | 8 | 8 | 171 | 365 | 355 | 325 | 69 |
| Link Distance (ft) |  | 539 | 539 | 539 |  | 1706 | 1706 | 1706 |  |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |  |
| Storage Bay Dist (ft) | 600 |  |  |  | 700 |  |  |  | 375 |
| Storage Blk Time (\%) |  |  |  |  |  |  |  | 1 |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  | 2 |  |
| Zone Summary |  |  |  |  |  |  |  |  |  |

## Zone wide Queuing Penalty: 3

TRANSPORTATION CONSULTANTS, INC.

| NCHRP 684 Internal Trip Capture Estimation Tool |  |  |  |  |
| ---: | :---: | ---: | ---: | ---: |
| Project Name: | The Commons at Falcon Field |  | Organization: | LSC Transportation Consultants, Inc |
| Project Location: | El Paso County, CO | KDF |  |  |
| Scenario Description: | Buildout | Performed By: | Date: | $3 / 26 / 2024$ |
| Analysis Year: | 2044 | Checked By: |  |  |
| Analysis Period: | AM Street Peak Hour | Date: |  |  |
|  |  |  |  |  |


| Table 1-A: Base Vehicle-Trip Generation Estimates (Single-Use Site Estimate) |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Land Use | Development Data (For Information Only) |  |  | Estimated Vehicle-Trips ${ }^{3}$ |  |  |
|  | ITE LUCs ${ }^{1}$ | Quantity | Units | Total | Entering | Exiting |
| Office |  |  |  | 0 |  |  |
| Retail |  |  |  | 145 | 90 | 55 |
| Restaurant |  |  |  | 0 |  |  |
| Cinema/Entertainment |  |  |  | 0 |  |  |
| Residential |  |  |  | 119 | 30 | 89 |
| Hotel |  |  |  | 0 |  |  |
| All Other Land Uses ${ }^{2}$ |  |  |  | 0 |  |  |
|  |  |  |  | 264 | 120 | 144 |


| Table 2-A: Mode Split and Vehicle Occupancy Estimates |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Land Use | Entering Trips |  |  | Exiting Trips |  |  |
|  | Veh. Occ. ${ }^{4}$ | \% Transit | \% Non-Motorized | Veh. Occ. ${ }^{4}$ | \% Transit | \% Non-Motorized |
| Office |  |  |  |  |  |  |
| Retail |  |  |  |  |  |  |
| Restaurant |  |  |  |  |  |  |
| Cinema/Entertainment |  |  |  |  |  |  |
| Residential |  |  |  |  |  |  |
| Hotel |  |  |  |  |  |  |
| All Other Land Uses ${ }^{2}$ |  |  |  |  |  |  |


| Table 3-A: Average Land Use Interchange Distances (Feet Walking Distance) |  |  |  |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :---: | :---: |
| Origin (From) |  |  |  |  |  |  |  |  |
|  | Office | Retail | Restaurant | Cinema/Entertainment | Residential |  |  |  |
| Office |  |  |  |  |  |  |  |  |
| Retail |  |  |  |  |  |  |  |  |
| Restaurant |  |  |  |  |  |  |  |  |
| Cinema/Entertainment |  |  |  |  |  |  |  |  |
| Residential |  |  |  |  |  |  |  |  |
| Hotel |  |  |  |  |  |  |  |  |


| Table 4-A: Internal Person-Trip Origin-Destination Matrix* |  |  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Origin (From) |  | Destination (To) |  |  |  |  |  |
|  | Office | Retail | Restaurant | Cinema/Entertainment | Residential | Hotel |  |
| Office |  | 0 | 0 | 0 | 0 | 0 |  |
| Retail | 0 |  | 0 | 0 | 1 | 0 |  |
| Restaurant | 0 | 0 |  | 0 | 0 | 0 |  |
| Cinema/Entertainment | 0 | 0 | 0 |  | 0 |  |  |
| Residential | 0 | 1 | 0 | 0 | 0 | 0 |  |
| Hotel | 0 | 0 | 0 | 0 | 0 | 0 |  |


| Table 5-A: Computations Summary |  |  |  | Table 6-A: Internal Trip Capture Percentages by Land Use |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Total | Entering | Exiting | Land Use | Entering Trips | Exiting Trips |
| All Person-Trips | 264 | 120 | 144 | Office | N/A | N/A |
| Internal Capture Percentage | 2\% | 2\% | 1\% | Retail | 1\% | 2\% |
|  |  |  |  | Restaurant | N/A | N/A |
| External Vehicle-Trips ${ }^{5}$ | 260 | 118 | 142 | Cinema/Entertainment | N/A | N/A |
| External Transit-Trips ${ }^{6}$ | 0 | 0 | 0 | Residential | 3\% | 1\% |
| External Non-Motorized Trips ${ }^{6}$ | 0 | 0 | 0 | Hotel | N/A | N/A |

[^1]| Project Name: | The Commons at Falcon Field |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Analysis Period: | AM Street Peak Hour |  |  |  |  |  |
| Table 7-A: Conversion of Vehicle-Trip Ends to Person-Trip Ends |  |  |  |  |  |  |
| Land Use | Table 7-A (D): Entering Trips |  |  | Table 7-A (0): Exiting Trips |  |  |
|  | Veh. Occ. | Vehicle-Trips | Person-Trips* | Veh. Occ. | Vehicle-Trips | Person-Trips* |
| Office | 1.00 | 0 | 0 | 1.00 | 0 | 0 |
| Retail | 1.00 | 90 | 90 | 1.00 | 55 | 55 |
| Restaurant | 1.00 | 0 | 0 | 1.00 | 0 | 0 |
| Cinema/Entertainment | 1.00 | 0 | 0 | 1.00 | 0 | 0 |
| Residential | 1.00 | 30 | 30 | 1.00 | 89 | 89 |
| Hotel | 1.00 | 0 | 0 | 1.00 | 0 | 0 |


| Table 8-A (O): Internal Person-Trip Origin-Destination Matrix (Computed at Origin) |  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Origin (From) |  | Destination (To) |  |  |  |  |
|  | Office | Retail | Restaurant | Cinema/Entertainment | Residential |  |
| Office |  | 0 | 0 | 0 | 0 | 0 |
| Retail | 16 |  | 7 | 0 | 0 |  |
| Restaurant | 0 | 0 |  | 0 | 0 |  |
| Cinema/Entertainment | 0 | 0 | 0 |  | 0 |  |
| Residential | 2 | 1 | 18 | 0 | 0 |  |
| Hotel | 0 | 0 | 0 | 0 | 0 |  |


| Table 8-A (D): Internal Person-Trip Origin-Destination Matrix (Computed at Destination) |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Origin (From) | Destination (To) |  |  |  |  |  |
|  | Office | Retail | Restaurant | Cinema/Entertainment | Residential | Hotel |
| Office |  | 29 | 0 | 0 | 0 | 0 |
| Retail | 0 |  | 0 | 0 | 1 | 0 |
| Restaurant | 0 | 7 |  | 0 | 2 | 0 |
| Cinema/Entertainment | 0 | 0 | 0 |  | 0 | 0 |
| Residential | 0 | 15 | 0 | 0 |  | 0 |
| Hotel | 0 | 4 | 0 | 0 | 0 |  |


| Table 9-A (D): Internal and External Trips Summary (Entering Trips) |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Destination Land Use | Person-Trip Estimates |  |  | External Trips by Mode* |  |  |
|  | Internal | External | Total | Vehicles ${ }^{1}$ | Transit ${ }^{2}$ | Non-Motorized ${ }^{2}$ |
| Office | 0 | 0 | 0 | 0 | 0 | 0 |
| Retail | 1 | 89 | 90 | 89 | 0 | 0 |
| Restaurant | 0 | 0 | 0 | 0 | 0 | 0 |
| Cinema/Entertainment | 0 | 0 | 0 | 0 | 0 | 0 |
| Residential | 1 | 29 | 30 | 29 | 0 | 0 |
| Hotel | 0 | 0 | 0 | 0 | 0 | 0 |
| All Other Land Uses ${ }^{3}$ | 0 | 0 | 0 | 0 | 0 | 0 |


| Table 9-A (0): Internal and External Trips Summary (Exiting Trips) |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Origin Land Use | Person-Trip Estimates |  |  | External Trips by Mode* |  |  |
|  | Internal | External | Total | Vehicles ${ }^{1}$ | Transit ${ }^{2}$ | Non-Motorized ${ }^{2}$ |
| Office | 0 | 0 | 0 | 0 | 0 | 0 |
| Retail | 1 | 54 | 55 | 54 | 0 | 0 |
| Restaurant | 0 | 0 | 0 | 0 | 0 | 0 |
| Cinema/Entertainment | 0 | 0 | 0 | 0 | 0 | 0 |
| Residential | 1 | 88 | 89 | 88 | 0 | 0 |
| Hotel | 0 | 0 | 0 | 0 | 0 | 0 |
| All Other Land Uses ${ }^{3}$ | 0 | 0 | 0 | 0 | 0 | 0 |

[^2]| NCHRP 684 Internal Trip Capture Estimation Tool |  |  |  |  |  |  |
| ---: | :---: | :---: | ---: | ---: | :---: | :---: |
| Project Name: | The Commons at Falcon Field |  | Organization: | LSC Transportation Consultants, Inc |  |  |
| Project Location: | El Paso County, CO | Performed By: | KDF |  |  |  |
| Scenario Description: | Buildout | Date: | $3 / 26 / 2024$ |  |  |  |
| Analysis Year: | 2044 | Checked By: |  |  |  |  |
| Analysis Period: | PM Street Peak Hour | Date: |  |  |  |  |


| Table 1-P: Base Vehicle-Trip Generation Estimates (Single-Use Site Estimate) |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Land Use | Development Data (For Information Only) |  |  | Estimated Vehicle-Trips ${ }^{3}$ |  |  |
|  | ITE LUCs ${ }^{1}$ | Quantity | Units | Total | Entering | Exiting |
| Office |  |  |  | 0 |  |  |
| Retail |  |  |  | 436 | 214 | 222 |
| Restaurant |  |  |  | 0 |  |  |
| Cinema/Entertainment |  |  |  | 0 |  |  |
| Residential |  |  |  | 160 | 101 | 59 |
| Hotel |  |  |  | 0 |  |  |
| All Other Land Uses ${ }^{2}$ |  |  |  | 0 |  |  |
|  |  |  |  | 596 | 315 | 281 |


| Table 2-P: Mode Split and Vehicle Occupancy Estimates |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Land Use | Entering Trips |  |  | Exiting Trips |  |  |
|  | Veh. Occ. ${ }^{4}$ | \% Transit | \% Non-Motorized | Veh. Occ. ${ }^{4}$ | \% Transit | \% Non-Motorized |
| Office |  |  |  |  |  |  |
| Retail |  |  |  |  |  |  |
| Restaurant |  |  |  |  |  |  |
| Cinema/Entertainment |  |  |  |  |  |  |
| Residential |  |  |  |  |  |  |
| Hotel |  |  |  |  |  |  |
| All Other Land Uses ${ }^{2}$ |  |  |  |  |  |  |

Table 3-P: Average Land Use Interchange Distances (Feet Walking Distance)

| Table 3-P: Average Land Use Interchange Distances (Feet Walking Distance) |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Origin (From) | Destination (To) |  |  |  |  |  |
|  | Office | Retail | Restaurant | Cinema/Entertainment | Residential | Hotel |
| Office |  |  |  |  |  |  |
| Retail |  |  |  |  | 5280 |  |
| Restaurant |  |  |  |  |  |  |
| Cinema/Entertainment |  |  |  |  |  |  |
| Residential |  |  |  |  |  |  |
| Hotel |  |  |  |  |  |  |


| Table 4-P: Internal Person-Trip Origin-Destination Matrix* |  |  |  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Origin (From) |  | Destination (To) |  |  |  |  |  |  |
|  | Office | Retail | Restaurant | Cinema/Entertainment | Residential | Hotel |  |  |
| Office |  | 0 | 0 | 0 | 0 | 0 |  |  |
| Retail | 0 |  | 0 | 0 | 6 | 0 |  |  |
| Restaurant | 0 | 0 |  | 0 | 0 | 0 |  |  |
| Cinema/Entertainment | 0 | 0 | 0 |  | 0 | 0 |  |  |
| Residential | 0 | 21 | 0 | 0 | 0 |  |  |  |
| Hotel | 0 | 0 | 0 | 0 | 0 |  |  |  |


| Table 5-P: Computations Summary |  |  |  | Table 6-P: Internal Trip Capture Percentages by Land Use |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Total | Entering | Exiting | Land Use | Entering Trips | Exiting Trips |
| All Person-Trips | 596 | 315 | 281 | Office | N/A | N/A |
| Internal Capture Percentage | 9\% | 9\% | 10\% | Retail | 10\% | 3\% |
|  |  |  |  | Restaurant | N/A | N/A |
| External Vehicle-Trips ${ }^{5}$ | 542 | 288 | 254 | Cinema/Entertainment | N/A | N/A |
| External Transit-Trips ${ }^{6}$ | 0 | 0 | 0 | Residential | 6\% | 36\% |
| External Non-Motorized Trips ${ }^{6}$ | 0 | 0 | 0 | Hotel | N/A | N/A |

[^3]| Project Name: | The Commons at Falcon Field |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Analysis Period: | PM Street Peak Hour |  |  |  |  |  |
| Table 7-P: Conversion of Vehicle-Trip Ends to Person-Trip Ends |  |  |  |  |  |  |
| Land Use | Table 7-P (D): Entering Trips |  |  | Table 7-P (0): Exiting Trips |  |  |
|  | Veh. Occ. | Vehicle-Trips | Person-Trips* | Veh. Occ. | Vehicle-Trips | Person-Trips* |
| Office | 1.00 | 0 | 0 | 1.00 | 0 | 0 |
| Retail | 1.00 | 214 | 214 | 1.00 | 222 | 222 |
| Restaurant | 1.00 | 0 | 0 | 1.00 | 0 | 0 |
| Cinema/Entertainment | 1.00 | 0 | 0 | 1.00 | 0 | 0 |
| Residential | 1.00 | 101 | 101 | 1.00 | 59 | 59 |
| Hotel | 1.00 | 0 | 0 | 1.00 | 0 | 0 |


| Table 8-P (O): Internal Person-Trip Origin-Destination Matrix (Computed at Origin) |  |  |  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Origin (From) |  | Destination (To) |  |  |  |  |  |  |
|  | Office | Retail | Restaurant | Cinema/Entertainment | Residential |  |  |  |
| Office |  | 0 | 0 | 0 | 0 | Hotel |  |  |
| Retail | 4 |  | 64 | 0 | 6 |  |  |  |
| Restaurant | 0 | 0 |  | 0 | 0 |  |  |  |
| Cinema/Entertainment | 0 | 0 | 0 |  | 0 |  |  |  |
| Residential | 2 | 25 | 12 | 0 | 0 |  |  |  |
| Hotel | 0 | 0 | 0 | 0 | 0 |  |  |  |


| Table 8-P (D): Internal Person-Trip Origin-Destination Matrix (Computed at Destination) |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Origin (From) | Destination (To) |  |  |  |  |  |
|  | Office | Retail | Restaurant | Cinema/Entertainment | Residential | Hotel |
| Office |  | 17 | 0 | 0 | 4 | 0 |
| Retail | 0 |  | 0 | 0 | 46 | 0 |
| Restaurant | 0 | 107 |  | 0 | 16 | 0 |
| Cinema/Entertainment | 0 | 9 | 0 |  | 4 | 0 |
| Residential | 0 | 21 | 0 | 0 |  | 0 |
| Hotel | 0 | 4 | 0 | 0 | 0 |  |


| Table 9-P (D): Internal and External Trips Summary (Entering Trips) |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Destination Land Use | Person-Trip Estimates |  |  | External Trips by Mode* |  |  |
|  | Internal | External | Total | Vehicles ${ }^{1}$ | Transit ${ }^{2}$ | Non-Motorized ${ }^{2}$ |
| Office | 0 | 0 | 0 | 0 | 0 | 0 |
| Retail | 21 | 193 | 214 | 193 | 0 | 0 |
| Restaurant | 0 | 0 | 0 | 0 | 0 | 0 |
| Cinema/Entertainment | 0 | 0 | 0 | 0 | 0 | 0 |
| Residential | 6 | 95 | 101 | 95 | 0 | 0 |
| Hotel | 0 | 0 | 0 | 0 | 0 | 0 |
| All Other Land Uses ${ }^{3}$ | 0 | 0 | 0 | 0 | 0 | 0 |


| Table 9-P (0): Internal and External Trips Summary (Exiting Trips) |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Origin Land Use | Person-Trip Estimates |  |  | External Trips by Mode* |  |  |
|  | Internal | External | Total | Vehicles ${ }^{1}$ | Transit ${ }^{2}$ | Non-Motorized ${ }^{2}$ |
| Office | 0 | 0 | 0 | 0 | 0 | 0 |
| Retail | 6 | 216 | 222 | 216 | 0 | 0 |
| Restaurant | 0 | 0 | 0 | 0 | 0 | 0 |
| Cinema/Entertainment | 0 | 0 | 0 | 0 | 0 | 0 |
| Residential | 21 | 38 | 59 | 38 | 0 | 0 |
| Hotel | 0 | 0 | 0 | 0 | 0 | 0 |
| All Other Land Uses ${ }^{3}$ | 0 | 0 | 0 | 0 | 0 | 0 |

${ }^{1}$ Vehicle-trips computed using the mode split and vehicle occupancy values provided in Table 2-P

[^4]LSC TRANSPORTATION CONSULTANTS, INC.
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FAX (719) 633-5430
E-mail: Isc@Isctrans.com
Website: http://www.Isctrans.com

## MEMORANDUM

DATE: June 7, 2024

| TO: | Arthur Gonzales - Access Manager |
| :--- | :--- |
| FROM: | Jeffrey C. Hodsdon, P.E. - LSC Transportation Consultants, Inc. |
| SUBJECT: | The Commons at Falcon Field <br>  <br>  <br>  <br>  <br>  <br>  <br>  <br> Re: Traffic Impact Study <br> LSC \#S234220 to CDOT Comments Memorandum |

Following are the LSC Transportation Consultants, Inc. responses to the April 17, 2024 Comment Letter prepared by CDOT - Region 2 - Traffic \& Safety - Permits regarding PCD-SP-232.
a. It is imperative for EI Paso County to work with the Falcon Fields Development to create a southern connection from the end of the southwestern leg off the proposed roundabout to Swingline Rd.

LSC Response: This note has been added to the TIS report, but The TIS also adds clarification that applicant has no control over property to the southwest but provides the street stub to allow for a future street connection to the adjacent property.

## Traffic comments:

The Traffic impact Study dated April 5, 2024, has been reviewed by a CDOT Traffic Engineer. Their comments follow:
b. The site will require an access permit for the construction of the 4th leg of Woodman and the closure of Rio.

LSC Response: Comment noted.
c. The applicant will be responsible for constructing improvements as described in the TIS, namely:

1. $E B$ to $S B$ right turn deceleration lane
2. NB to $E B$ right turn acceleration lane
3. Signalization of 4 th leg of the intersection
4. Laneage as described in the TIS for the NB Woodmen movement

## LSC Response: Comments noted.

Access Comments:
This development impacts CDOT Access and CDOT infrastructure. My comment follows:
d. Two CDOT Access Permit will be required for this development. One for the connection point of Woodman Road to SH24G and the other for the closure of Rio Lane.

## LSC Response: Comment noted.

e. Roadway improvements will be required and detailed in the terms and conditions of the access permits.

## LSC Response: Comment noted.

f. Future roadway dedication and or preservation is required of this development.

## LSC Response: Comment noted.

g. It is critical for the SH24G Highway Widening Project and Falcon Fields to continue to coordinate projects.

LSC Response: Comment noted.
h. Section 1.4(1) of the State Highway Access Code, states in part that no person, shall construct any access providing direct vehicular movement to or from any state highway from or to property in close proximity or abutting a state highway without an access permit issued by the designated issuing authority with the written approval of the Department.

## LSC Response: Comment noted.

i. Under Section 2.6 (Change in Land Use and Access Use) of the State Highway Access Code, states the requirements of a new access permit. It states in part that if any significant changes are made or will be made in the use of the property which will affect access operation, traffic volume increases by $20 \%$ and or vehicle type, the permittee or property owner will coordinates with the local authority and the Department to determine if a new access permit and modifications to the access are required.
j. LSC Response: Comment noted.

# The Commons at Falcon Field - Preliminary Plan Traffic Impact Study PCD File No.: SP232 <br> (LSC \#S234070) <br> April 5, 2024 <br> <div class="inline-tabular"><table id="tabular" data-type="subtable">
<tbody>
<tr style="border-top: none !important; border-bottom: none !important;">
<td style="text-align: left; border-left-style: solid !important; border-left-width: 1px !important; border-right-style: solid !important; border-right-width: 1px !important; border-bottom: none !important; border-top-style: solid !important; border-top-width: 1px !important; width: auto; vertical-align: middle; ">LSC Responses</td>
</tr>
<tr style="border-top: none !important; border-bottom: none !important;">
<td style="text-align: left; border-left-style: solid !important; border-left-width: 1px !important; border-right-style: solid !important; border-right-width: 1px !important; border-bottom: none !important; border-top: none !important; width: auto; vertical-align: middle; ">to TIS Redline</td>
</tr>
<tr style="border-top: none !important; border-bottom: none !important;">
<td style="text-align: left; border-left-style: solid !important; border-left-width: 1px !important; border-right-style: solid !important; border-right-width: 1px !important; border-bottom-style: solid !important; border-bottom-width: 1px !important; border-top: none !important; width: auto; vertical-align: middle; ">Comments</td>
</tr>
</tbody>
</table>
<table-markdown style="display: none">| LSC Responses |
| :--- |
| to TIS Redline |
| Comments |</table-markdown></div> 

## Traffic Engineer's Statement

This traffic report and supporting information were prepared under my responsible charge and they comport with the standard of care. So far as is consistent with the standard of care, said report was prepared in general conformance with the criteria established by the County for traffic reports.


## Developer's Statement

I, the Developer, have read and will comply with all commitments made on my behalf within this report.

## LSC Responses to EPC TIS Redline Comments

Page: 1
$\equiv$ Number: $1 \quad$ Author: jchodsdon Subject: Text Box Date: 6/7/2024 17:55:56
LSC Responses to TIS Redline Comments
these possible future connections are not proposed for use by this project. These are being provided for the benefit of US/Lwy 24 access management and adjacent property owners, should future connections to adjacent future developments/redevelopment become necessary.

Sight Distance


Figures 3a and 啇 show the results of sight-distance analysis of the intersections and access points to Retail Row Street. The analysis is based on a design speed of 25 miles per hour (mph) for the modified cross section. As shown in Figures 3a and 3d, the required intersection sight distance of 280 feet from taken ECM Table 2-21 and the required stopping sight distance of 155 feet taken from ECM Table 2-17 can be met at all of the proposed intersections and access points to Retail Row Way. One reasonable exception (citing AASHTO criteria) is noted in Figure 3a for sight distance for drivers turning onto Retail Row Street from Willet Way to vehicles traveling southbound to westbound via the Rio Lane/Retail Row Street knuckle located just east of the intersection.

Figure 3b shows the results of the sight distance analysis of the intersection of Woodmen Road/4Unlin Drive. As this access is proposed to be restricted to right-in only, the analysis was limited to stopping sight distance for south-eastbound traffic arriving from the intersection of US Hwy 24/Woodmen. 5igure 3c shows the required stopping sight distance based on 40 mph for south-eastbound through vehickes from the intersection of US Hwy 24/Woodmen, based on a 15 mph for north-eastbound right-turning vehicles from the intersection of US Hwy 24/Woodmen, and based on 20 mph for south-westbound left-turning vehicles from the intersection of US Hwy 24/Woodmen. As shown in Figure 3c, the required stopping sight distance can be met for all three scenarios. This should be 3b

Figure 3d shows the results of sight-distance analysis of the intersections and access points to Rio Lane. The analysis is based on a design speed of 25 miles per hour (mph) for a Local. As shown in Figure 3d, the required intersection sight distance of 280 feet from taken ECM Table 2-21 and the required stopping sight distance of 155 feet taken from ECM Table 2-17 can be met at all of the proposed intersections and access points to Rio Lane. One reasonable-exception (citing AASHTO criteria) is noted in Figure 3d for sight distance for drivers turning onto Riolane from Perula Way to vehicles traveling westbound to southbound via the knuckle located just notth of the intersection.

## PROPOSED RIO LANE CLOSURE AT US HIGHWAY 24

The intersection of Rio Lane/US Highway 24 is proposed to be closed, as sho US Highway 24 Access Management Plan and the US 24 Planning and Enviro
Study, October 2017. The project will help implement the US Highway 24 Access ivianagement Plan by providing an alternative to the Rio Lane/US Hwy 24 intersection.


Site-generated traffic volumes have been calculated by applying the directional-distribution percentages estimated by LSC (from Figure 5) to the trip-generation estimates (from Table 2). The pass-by trips and diverted trips were assigned, based on the magnitude and direction of the peak-hour traffic volumes projected for the major study-area streets/roads.

## BACKGROUND TRAFFIC VOLUMES

Background traffic is traffic on the adjacent roadways that is forecast to be present without the proposed development. Short-term and 2044 background traffic scenarios were developed.

Both future forecasts also assume that the intersection of US Hwy 24/Rio Lane has been closed and the associated traffic has been re-routed. Because Rio Lane will no longer directly access US Hwy 24, LSC projects that some of the trips currently using Rio Lane and Rio Road will reroute and use Falcon Hwy or Meridian Road to access US Hwy 24.

## Short Term Figure 7

Figure 7 a shows the estimated short-term background traffic volumes at the study-area intersections. The short-term background volumes assume that the US Hwy 24/Rio Lane intersection has been closed and traffic has been rerouted through the new fourth leg of the US Hwy 24/Woodmen Road intersection.

## Long Term

Figure 8 shows the estimated 2044 background traffic volumes. These projected volumes include estimates from planned future Falcon area development and increases in through traffic volumes on the study-area roadways. The 2044 background volumes were developed using the US Highway 24 PEL study. Volumes were modified as needed, based on newer count volumes and expected development in the study area. The 2044 background assumes future commercial development on the parcel to the west of the site with access through the proposed The Commons at Falcon Field development and the internal roundabout.

## TOTAL TRAFFIC VOLUMES

Site-generated traffic volumes from Figure 6 were added to short-term background traffic volumes from Figure 7 to calculate short-term total traffic volumes provided in Figure 9. Similarly, 2044 total traffic volumes provided in Figure 10 were calculated by adding the site-generated traffic (Figure 6) with the 2044 background traffic volumes (Figure 8).

Page: 15
Ent Number: $1 \quad$ Author: HaoVo $\quad$ Subject: Callout $\quad$ Date: $5 / 1 / 2024$ 14:17:48

Figure 7
Author: Kirstin Ferrin Subject: Sticky Note Date: 6/7/2024 14:22:03
LSC Response: The text has been revised.

## LEVEL OF SERVICE ANALYSIS

Levels of service were calculated for both the short-term background, 2044 background, short-term total traffic, and 2044 total traffic volumes. The results of the analysis are shown in Figures 7, 8, 9, and 10. Traffic lanes used in the analysis are also provided in these figures.

## Woodmen Road/Meridian Road

The signalized intersection of Woodmen/Meridian is projected to at an overall LOS C during the morning peak hour and an overall LOS D during the afternoon peak hour, based on both the short-term background and total traffic volumes. Some of the left-turn movements are projected to operate at LOS E during the peak hours, based on both the short-term background and total traffic volumes. By 2044, some of the through movements are projected to operate at LOS E and some of the left-turn movements are projected to operate at LOS F, based on both the 2044 background and total traffic volumes.

## Woodmen Road/McLaughlin Road

The signalized intersection of Woodmen/McLaughlin is projected to operate at an overall LOS D or better during the morning and afternoon peak hours, based on the short-term background, 2044 background, short-term total, and 2044 total traffic volumes.

## US Highway 24/Woodmen Road

In the short-term scenarios, it has been assumed that no baseline capacity improvements (additional northeast-bound/southwest-bound through lanes) will occur on US Hwy 24. However, per recent meetings with CDOT, coordination will continue as this project and the adjacent Highway 24 CDOT project move forward. Cooperation with respect to phasing of improvements, such as potential future use of eastbound right-turn deceleration and acceleration lanes that may be built by this project as future through lanes. The CDOT project would then add new lanes to replace them (for example). The improvements based on the Access Code and CDOT direction provided thus far at the intersection of US Hwy 24/Woodmen Road would include:

- The new fourth northwest bound leg of the intersection with a left lane, two through lanes, and right lane;
- Auxiliary turn lanes on US Hwy 24 to serve the trips/vehicle turning movements associated with the new fourth leg - the development, and the "replacement" Rio Lane connection;
- Raised right-turn islands for pedestrian accessibility;

Review C2: dual lefts are shown in the figure

Page: 16
Ent: Number: $1 \quad$ Author: Haovo Subject: Callout Date: $5 / 1 / 2024$ 14:44:11
Review C2: dual lefts are shown in the figureReview C3: Unresolved.
$\frac{\text { Author: Kirstin Ferrin Subject: Sticky Note Date: 6/7/2024 14:22:22 }}{}$
$\overline{\text { LSC Response: The figures show a single left-turn lane and a striped-out area to properly align the northwest bound lanes with the }}$ southeast leg.

## Rio Lane Access Points

The proposed intersections of Rio Lane/Perula Lane, Rio Lane/Jacamar Way and Rio Lane/Toddy Way been analyzed as a stop-sign-controlled (unsignalized) intersections. All approaches are projected to operate at LOS B or better during the peak hours, based on the short-term total and 2044 total traffic volumes.

## QUEUING ANALYSIS

A queuing analysis was performed using Synchro/SimTraffic for the key approach turning movements at the intersection of US Hwy 24/Woodmen Road and the proposed Retail Row Street access points to determine the projected queue lengths, based on the 2044 total traffic volumes. The simulation was run five times. The queuing reports are attached. These queuing results have been used to develop auxiliary turn-lane recommendations. The results of the analysis are shown in Table 3.

## INTERSECTION AND AUXILIARY TURN LANE RECOMMENDATIONS

The El Paso County Engineering Criteria Manual (ECM) and the Colorado State Highway Access Code standards were used as a basis for the following turn-lane and other recommendations at the intersections.

## US Highway 24/Woodmen Road

 Figure 11b11
Figure 11 亿 $\ddagger$ rovides the recommendations for improvements at the intersection of US Highway 24/Woodmen Road, including auxiliary turn-lane dimensions and modifications needed with the new fourth leg of the intersection of US Hwy 24/Woodmen Road.

Retail Row Intersections Figure 11c

Figure 146 shows the recommended turn-lane lengths at the proposed internal intersections/access points to Retail Row Street.

## Right-In-Only Access Point

Figures $2 a$ and $2 b$ show the proposed right-in-only access point to Woodmen Road, including the access spacing details. The proposed right-in-only access point would provide a low-impact, lowconflict secondary entry point to the commercial lot areas west of Woodmen.

The proposed right-turn lane would have abbreviated lane and taper lengths. The ECM standard is 155 -foot lane plus 160 -foot taper, plus storage. Figure 11d (a copy of Deviation Exhibit 2a-1 from Deviation 2a) shows the proposed lengths. The lane would be about 130 feet plus a 55 -foot

Page: 18

| Enumber: 1 | Author: HaoVo | Subject: Callout |
| :--- | :--- | :--- |
| Figure 11b | Date: $5 / 1 / 2024$ 14:56:59 |  |
|  |  |  |
| SHAuthor: Kirstin Ferrin | Subject: Sticky Note | Date: $6 / 7 / 2024$ 14:22:31 |
| LSC Response: The text has been revised. |  |  |

$\equiv$ Number: $2 \quad$ Author: HaoVo Subject: Callout Date: 5/1/2024 14:56:29

Figure 11c
$\frac{\text { Author: } \text { Kirstin Ferrin } \quad \text { Subject: Sticky Note } \quad \text { Date: 6/7/2024 14:22:41 }}{\text { LSC Response: The text has been revised. }}$
additional space for pedestrians, but don't offer physical protection. This project will be installing a sidewalk along the south side of the east-west segment adjacent to the site frontage and on both sides of the street for the section within the site. The project will also provide a street stub to Pinto Pony Road that could be used as a pedestrian collection to Chief Road and Pinto Pony Road.

Other measures to enhance pedestrian safety could potentially include roadway illumination. However, it is not likely practical or desirable to the area residents to improve pedestrian visibility with roadway illumination. Measures to educate and encourage the use of flashing LED lights, retroreflective clothing, vests, armbands etc. by local-residents clothing or armbands should be considered. Signs along the roadway could be placed to remind area residents and other users of the roadway for non-motorized travel, to wear retro-reflective gear.

## Retail Row Street

Aside from the extension of Woodmen Road into the site from the US Highway 24 intersection, Retail Row Street will be the main internal street serving the commercial and residential development, it will also provide the replacement Rio Lane connection to US Highway 24.

Retail Row Street is proposed as a Non-Residential Collector with a modified cross-section. Please refer to the Intersection improvements section for intersection recommendations. Please refer to deviation request No. 5 for details regarding the nronosed cross section and other planning and design details. Comments have been provided that the private roadways on the east side
Willet Way, Perula Way and Dunlin Drive (Perula Way) shall meet County standards. Please revise.

Direct access to the individual commercial luıs vuvuiu ne via uriee private cuminerial (local)" streets shown on the Preliminary Plan (Willet Way, Perula Way and Dunlin Drive). These streets would be 26 -feet wide plus curb and gutter ( 30 -feet of width flowline-to-flowline), with attached 5 -foot-wide sidewalks.

## DEVIATIONS TO ECM CRITERIA

The following deviations to the criteria contained in the El Paso County Engineering Criteria Manual (ECM) have been recently submitted as part of this application:

- Public street intersection spacing along an Urban Non-Residential Collector - Woodmen Road (proposed) southeast of US Highway 24/Retail Row Street
- Right-in-Only access to an Urban Non-Residential Collector
- Full-movement access to an Urban Non-Residential Collector;
- ECM-standard auxiliary turn-lane lengths on an Urban Non-Residential Collector.
- Modification to the design standards of an Urban Non-Residential Collector Street (Retail Row Street)


## Page: 20

| Number: $1 \quad$ Author: Daniel Torres $\quad$ Subject: Callout $\quad$ Date: $5 / 7 / 2024$ 22:40:06 |
| :--- |
| Comments have been provided that the private roadways on the east side (Perula Way) shall meet County standards. |
| Please revise. |

Please revise.
Author: jchodsdon Subject: Sticky Note Date: 6/7/2024 14:22:52
LSC Response: This paragraph has been revised to reflect the updates by Drexel Barrell to the plan (in response to this comment).

## ROADWAY CLASSIFICATIONS

## revise to urban local

- The streets proposed for this project would be classified as either Urban Non-Residential Collector or Urban Local or "private commercial (i@cal)" streets. Please refer to Figure 12, which presents the recommended classifications for the proposed streets shown on the Preliminary Plan. The figure also shows the classification of the adjacent existing roadways as described in the "Existing Roadways" section.


## MTCP-IDENTIFIED FUTURE NEEDED ROADWAY IMPROVEMENT PROJECTS

- The EI Paso County Major Transportation Corridors Plan (MTCP) calls for improvement to US Hwy 24 from Garrett Road to Woodmen Road and upgrade to a rural six-lane Principal Arterial. As mentioned in the "Existing Roadways" section above, CDOT will be completing a US Hwy 24 corridor improvement project that will widen the roadway to four lanes from Garrett Road to Woodmen Road. Construction is expected to begin in 2025.
- Although not in the immediate area, the MTCP calls for an upgrade to Falcon Highway to a two-lane, rural Minor Arterial from US Hwy 24 to one mile east of Curtis Road. Also, the MTCP calls for an upgrade to Eastonville Road from McLaughlin to Latigo Boulevard as a rural road upgrade to a two-lane Rural Minor Arterial.
- The project would need to construct a sidewalk or potentially a multi-use trail, along the north side of Woodmen Road between the US Hwy 24 intersection and the current sidewalk located about 450 feet northwest of US Hwy 24 . This point is adjacent to the connection.


## MULTI-MODAL TRANSPORTATION \& TRANSPORTATION DEMAND MANAGEMENT OPPORTUNITIES

- The following section describes the details of a pedestrian/bicycle connection between this project and the Rock Island Trail.
- Trail connections exist between the Rock Island Trail and the Woodmen Hills neighborhoods to the north of US Highway 24.
- A Park \& Ride facility has been developed nearby at the intersection of Meridian Road and Swingline Road. Future Mountain Metropolitan Transit bus service may be added to/from this Park \& Ride location.


## PEDESTRIAN \& BICYCLE FACILITIES

- The project would include urban street sections with sidewalks.
- Figure 11a shows the recommendation for curbed right-turn pedestrian islands. The traffic signal would be modified to provide full pedestrian access on all four legs of the intersection. These details would be shown as part of the traffic-signal modification plan and the intersection-improvement construction drawings. These design details and plans

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## CDOT ACCESS PERMITTING

 Review C3: Unresolved. It is 3594 in table 2.CDOT access permits will be required for the street connection to the US Highway 24/Woodmen Road intersection and for the closure of Rio Lane at US Highway 24. Per recent meetings with CDOT, coordination will continue as this project and the adjacent Highway 24 CDOT project move forward.

## CONCLUSIONS AND RECOMMENDATIONS

## Trip Generation

- The Commons at Falcon Field is expected to generate about 3,592 new external vehicle trips on the average weekday, with about half entering and half exiting the site during a 24 -hour period. During the morning peak hour, about 118 vehicles would enter and 142 vehicles would exit the site. During the afternoon peak hour, approximately 288 vehicles would enter and 254 vehicles would exit the site.


## Traffic Operations Analysis

- The signalized intersection of US Highway $24 /$ Woodmen Road is projected to operate at LOS D or better during both peak hours for the short-term and year-2044 scenarios. The El Paso County Engineering Criteria Manual (ECM) standards were followed to develop turn-lane recommendations at the intersections. Figure 11a provides the turn-lane conceptual design for this intersection. Please refer to the Level of Service and Queuing Analysis sections of this report for additional details and discussion.


## Recommended Improvements

- A list of recommended improvements within the site and in the study area is presented in Table 4.
- The intersection of US Highway 24/Rio Lane is to be closed and the proposed Collector roads within the site will connect Rio Lane to the US Highway 24/Woodmen intersection.

Short-term improvements assumed at the intersection of US 24/Woodmen Road would include:

- The fourth leg of the intersection with a northwest-bound left-lane, two northwest-bound through-lanes, and northwest-bound right-lane as shown in 2igure 11a;
- Raised right-turn islands for pedestrian accessibility; 11b
- Lane alignment and median modifications on the existing northwest of the intersection as shown in $\mathrm{F}_{4}$ ure 12a; $<$
- Signal modifications including installation of traffic-signal components needed for the new leg; and

Page: 24


- Auxiliary turn lanes on US Highway 24 to serve the trips/vehicle turning movements associated with the new fourth leg of this intersection. This new fourth leg would serve site traffic and background traffic shifted from the closure of the US Highway 24/ Rio Lane connection.

Based on the 2044 total traffic volumes shown in Figure 10 and the criteria contained in the State of Colorado Highway Access Code, the following deceleration and acceleration lanes are required on US Highway 24:

- A northeast-bound right-turn deceleration lane is warranted on US Highway 24 approaching Woodmen Road. Based on a posted speed limit of 55 mph , the prescribed lane length for the deceleration lane is 600 feet plus a 222 -foot taper.
- A southwest-bound left-turn deceleration lane is warranted on US Highway 24 approaching Woodmen Road. Based on a posted speed limit of 55 mph , the prescribed lane length for the deceleration lane is 600 feet plus 100 feet of storage and a 222 -foot taper.
- A northwest-bound right-turn acceleration lane is warranted on US Highway 24 east of Woodmen Road. Based on a posted speed limit of 55 mph , the prescribed lane length for the acceleration lane is 960 feet plus a 222 -foot taper.

Based on the 2044 total traffic volumes shown in Figure 10 and the criteria contained in the ECM, the following deceleration and acceleration lanes are required on Retail Row Street:

- A southwest-bound left-turn lane is warranted on Retail Row Street approaching Nunbird Court. Based on a design speed limit of 25 mph , the ECM-required lane length would be 115 feet for deceleration, 50 to 75 feet for storage, and a 80 -foot taper. Based on the available lane length and the $95^{\text {th }}$ percentile queue length analysis results shown in Figyce 11, LSC recommends a 100-foot left-turn lane plus 65 -foot reverse curve bay taper.
- A noltheast-bound left-turn lane is not projected to be warranted on Retail Row Street approaching Dunlin Drive. However, this lane will be needed to algin with the recommended left-turn lane approaching Nunbird Court. Based on a design speed limit of 25 mph , the ECM-required lane length would be 115 feet for deceleration, 50 to 75 feet for storage, and an 80 -foot taper. Based on the available lane length and the $95^{\text {th }}$ percentile queue length analysis results shown in Table 3, LSC recommends a 165 -foot left-turn lane plus 80 -foot taper.
- A northeast-bound left-turn lane is projected to be warranted on Retail Row Street approaching Willet Way. Based on a design speed limit of 25 mph , the ECM-required lane length would be 115 feet for deceleration, 100 feet for storage, and a 80 -foot taper. Based on the available lane length and the $95^{\text {th }}$ percentile queue length analysis results shown in Table 3, LSC recommends a 120-foot left-turn lane plus a 50 to 75 -foot reverse curve bay taper.

Please provide
figure 11.

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気 Number: $1 \quad$ Author: HaoVo Subject: Callout Date: 5/1/2024 15:26:45

Please provide figure 11.
Author: Kirstin Ferrin Subject: Sticky Note Date: 6/7/2024 14:23:16
LSC Response: The text has been revised to Figure 11a.


Note: This figure is an expanded copy of Deviation Exhibit 3-1 in Deviation No. 3


Figure 11b
Intersection Improvements at the Intersection of US 24/Woodmen Rd

Page: 48

| $\equiv$ | Number: 1 | Author: Daniel Torres | Subject: Callout |
| :--- | :--- | :--- | :--- |
| decel lane | Date: 5/7/2024 22:07:49 |  |  |
|  |  |  |  |
|  |  |  |  |
|  |  |  |  |
| Author: Kirstin Ferrin | Subject: Sticky Note | Date: 6/7/2024 14:23:25 |  |
| LSC Response: Revised as requested. |  |  |  |

## AutoTurn Exhibits 1-5

Review 2 comment:
1 please also provide snow plow turn movements.
Review 3: unresolved

Page: 52
$\equiv \frac{\text { Number: } 1 \quad \text { Author: Daniel Torres }}{\text { Review } 2 \text { comment: please also provide snow plow turn movements.Review 3: unresolved }}$

Author: jchodsdon Subject: Sticky Note Date: 6/7/2024 17:54:31
LSC Response: While this comment is posted on the cover page of the access point autoturn exhibits, the review comment from Review 2 was to provide snowplow Autoturn movements through the roundabout, not each of the access points. The Falcon Marketplace deviation did not show the snowplow vehicles at the individual access points. The access points will be private roads and will be plowed by private contractor plowing company (so the County plow vehicle template would not apply). Typically snowplow vehicles used within small commercial centers are smaller than the County plow vehicles.

Regarding the snowplow vehicles through the proposed roundabout, 1) The roundabout exhibits show this roundabout accommodating much larger vehicles than the county snowplow vehicle. 2) The snowplow vehicle is wider due to the snowplow blade, but we have previously demonstrated that the county snowplow can negotiate a roundabout of significantly smaller size. Therefore, it will work for this one as well. Please see attached exhibit (attached to these comment responses) showing the county standard snowplow vehicle negotiating a smaller, 120' inscribed circle roundabout.


Page: 54
$\square \square$ Number: $1 \quad$ Author: Daniel Torres $\quad$ Subject: Cloud $+\quad$ Date: 5/7/2024 22:53:13

[^5]

## Page: 55

Sumber: $1 \quad$ Author: Daniel Torres Subject: Callout Date: 5/7/2024 22:55:09
Southwest bound right turning design vehicle is shown in the left turn bay. Revise
Author: Kirstin Ferrin $\quad$ Subject: Sticky Note $\quad$ Date: 6/7/2024 14:24:19

| LSC Response: This figure has been fixed to show the truck completing the right turn and maneuvering into the westbound through |
| :--- |
| (and associated deviation) has has been based on the Falcon Marketplace deviation. |

PCD File No. SP232
The Commons at Falcon Field
(LSC\#S234220)
Woodmen Road \& Retail Row Street County: El Paso

## ROUNDABOUT CRITICAL DESIGN PARAMETERS

| DESIGN PARAMETERS | LEG 1 | LEG 2 | LEG 3 | LEG 4 | LEG 5 | LEG 6 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Approach Width, FT | 18.0 | 18.0 | 18.0 |  |  |  |
| Entry Width, FT | 15.0 | 15.0 | 15.0 |  |  |  |
| Entry Angle, PHI $\Phi$, DEG | 14.5 | 36.0 | 31.0 |  |  |  |
| Inscribed Circle Diameter, FT | 180.0 | 180.0 | 180.0 |  |  |  |
| Exit Width, FT | 23.4 | 20.0 | 20.0 |  |  |  |
| Circulating Roadway Width Upstream of Entry, FT | 18.0 | 18.0 | 18.0 |  |  |  |

FASTEST SPEED PATH

| $R_{1}$, Radius/Speed, FT/MPH | 135 | 23 | 134 | 22 | 135 | 22 |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $R_{2}$, Radius/Speed, FT/MPH |  |  | 107 | 21 | 78 | 18 |  |  |  |  |  |
| $R_{3}$, Radius/Speed, FT/MPH | 900 | $>40$ | 850 | $>40$ | 345 | 31 |  |  |  |  |  |
| $R_{4}$, Radius/Speed, FT/MPH | 76 | 18 | 77 | 18 |  |  |  |  |  |  |  |
| $R_{5}$, Radius/Speed, FT/MPH | 130 | 22 |  |  | 110 | 21 |  |  |  |  |  |
| Bypass $R_{5}$, Radius/Speed, FT/MPH |  |  |  |  |  |  |  |  |  |  |  |

## MINIMUM SIGHT PARAMETERS



Design Vehicle:

Truck Apron Width:
OSOW Accommodations:
Circulating Roadway Cross-Slope:
Access Control:

Parking Control:

Bicycle \& Pedestrian Accommodations:

WB-50, WB-67, EPC snowplow
 per WisDOT criteria truck apron shall be a min. 12 ft . wide

Designer: Matt Romero
Reviewer: Chris McGranahan, P.E., PTOE
***** Preliminary ********
SIGNATURE: $\qquad$ DATE:
3/8/2024

NAME: Christopher S. McGranahan, P.E.

I roundabout principals. The critical design elements have been addressed. The project design engineer in responsible charge of final planl
!
G:IShared drivesICS Engineering - 2019-currentl2023IS234220 - Falcon Field Preliminary Plan 20231Roundabout

## Page: 59

| E Number: $1 \quad$ Author: Daniel Torres $\quad$ Subject: Callout Date: 5/7/2024 23:02:19 |
| :--- |
| per WisDOT criteria truck apron shall be a min. 12 ft. wide |
|  |
| Author: jchodsdon Subject: Sticky Note $\quad$ Date: 6/7/2024 14:24:30 |
| LSC Response: The truck apron has been revised to 12 feet wide. |




[^0]:    G：IShared drivesICS Engineering－2019－current｜2023IS234220－Falcon Field Preliminary Plan 2023\Roundabout
    Exhibits\2024－06－JunelRoundabout Design Parameters Table rev 6－7－2024
    6／7／2024，2：48 PM

[^1]:    ${ }^{1}$ Land Use Codes (LUCs) from Trip Generation Manual , published by the Institute of Transportation Engineers.
    ${ }^{2}$ Total estimate for all other land uses at mixed-use development site is not subject to internal trip capture computations in this estimator.
    ${ }^{3}$ Enter trips assuming no transit or non-motorized trips (as assumed in ITE Trip Generation Manual).
    ${ }^{4}$ Enter vehicle occupancy assumed in Table 1-A vehicle trips. If vehicle occupancy changes for proposed mixed-use project, manual adjustments must be made to Tables 5-A, 9-A (O and D). Enter transit, non-motorized percentages that will result with proposed mixed-use project complete.
    ${ }^{5}$ Vehicle-trips computed using the mode split and vehicle occupancy values provided in Table 2-A.

    ## Person-Trips

    Indicates computation that has been rounded to the nearest whole number.
    Estimation Tool Developed by the Texas A\&M Transportation Institute - Version 2013.1

[^2]:    ${ }^{1}$ Vehicle-trips computed using the mode split and vehicle occupancy values provided in Table 2-A
    ${ }^{2}$ Person-Trips
    ${ }^{3}$ Total estimate for all other land uses at mixed-use development site is not subject to internal trip capture computations in this estimator
    *Indicates computation that has been rounded to the nearest whole number.

[^3]:    ${ }^{1}$ Land Use Codes (LUCs) from Trip Generation Manual, published by the Institute of Transportation Engineers.
    ${ }^{2}$ Total estimate for all other land uses at mixed-use development site is not subject to internal trip capture computations in this estimator.
    ${ }^{3}$ Enter trips assuming no transit or non-motorized trips (as assumed in ITE Trip Generation Manual).
    ${ }^{4}$ Enter vehicle occupancy assumed in Table 1-P vehicle trips. If vehicle occupancy changes for proposed mixed-use project, manual adjustments must be
    ${ }^{5}$ Vehicle-trips computed using the mode split and vehicle occupancy values provided in Table 2-P.
    ${ }^{6}$ Person-Trips
    *Indicates computation that has been rounded to the nearest whole number.
    Estimation Tool Developed by the Texas A\&M Transportation Institute - Version 2013.1

[^4]:    ${ }^{2}$ Person-Trips
    ${ }^{3}$ Total estimate for all other land uses at mixed-use development site is not subject to internal trip capture computations in this estimator
    Indicates computation that has been rounded to the nearest whole number.

[^5]:    Author: jchodsdon Subject: Sticky Note Date: 6/7/2024 14:23:42
    LSC Response: This figure has been fixed accordingly.

